

Appendix E

Updated Geotechnical Report, Equestrian Estates Development,

Prepared by

Petra Geosciences, Inc., April 13, 2022.

**UPDATED GEOTECHNICAL REPORT
EQUESTRIAN ESTATES DEVELOPMENT
APN'S 751-020-002, 751-020-006, 751-020-007, AND 951-020-003
APPROXIMATELY 628 ACRES, NEC OF AVENUE 64 AND HARRISON STREET
THERMAL AREA, RIVERSIDE COUNTY, CALIFORNIA**

DESERT EQUESTRIAN HOLDINGS, LLC

*April 13, 2022
J.N. 21-483*

ENGINEERS + GEOLOGISTS + ENVIRONMENTAL SCIENTISTS

DESERT EQUESTRIAN HOLDINGS, LLC19312 Canyon Drive
Villa Park, California 92861

Attention:

Mr. Jeremy Smith

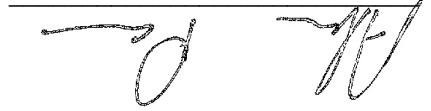
Subject:**Updated Geotechnical Report, Equestrian Estates Development, Assessor's Parcel
Numbers 751-020-002, 751-020-006, 751-020-007, and 951-020-003, Approximately
628 Acres, Northeast Corner of Avenue 64 and Harrison Street, Thermal Area,
Riverside County, California**

Dear Mr. Smith:

Petra Geosciences, Inc. (Petra) is submitting herewith the updated report of our geotechnical evaluation for design and construction of the proposed improvements within the subject site located at the northeast corner of Avenue 64 and Harrison Street, Thermal area of Riverside County, California. This work was performed in general accordance with the scope of services outlined in our Proposal No. 21-483P, dated December 23, 2021. This report presents the results of our review of the field investigation and laboratory testing performed by Earth Systems Southwest, the results of Petra's engineering and geologic analysis, judgment, opinions, conclusions and recommendations pertaining to geotechnical design aspects of the proposed development in general conformance with the 2019 California Building Code (2019 CBC).

It has been a pleasure to be of service to you on this project. Should you have any questions regarding the contents of this report, or should you require additional information, please do not hesitate to contact us.

Respectfully submitted,

PETRA GEOSCIENCES, INC.A handwritten signature in black ink, appearing to read "Alan Pace", written over a horizontal line.

Alan Pace

Vice President

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FIGURE –	SITE LOCATION MAP
APPENDIX A –	EXPLORATION BORING LOGS PERFORMED BY EARTH SYSTEMS SOUTHWEST
APPENDIX B –	LABORATORY TEST PROCEDURES / LABORATORY DATA SUMMARY PERFORMED BY EARTH SYSTEMS SOUTHWEST
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**UPDATED GEOTECHNICAL REPORT
EQUESTRIAN ESTATES DEVELOPMENT
APN'S 751-020-002, 751-020-006, 751-020-007, AND 951-020-003
APPROXIMATELY 628 ACRES, NORTHEAST CORNER OF AVENUE 64 AND HARRISON ST.
THERMAL AREA, RIVERSIDE COUNTY, CALIFORNIA**

PURPOSE AND SCOPE OF SERVICES

Petra Geosciences, Inc. (Petra) is presenting herein the updated report of our geotechnical evaluation of an existing report for the subject project site. The purpose of this evaluation was to review the geotechnical field investigation and laboratory data provided by Earth Systems Southwest (ESS), evaluate the engineering properties of the onsite soil materials, and to provide conclusions and recommendations for site remedial grading, design, and construction of the proposed equestrian estate development and ancillary improvements, all in conformance with the 2019 California Building Code (2019 CBC). To accomplish these objectives, our scope of services included the following:

1. Review of available published and unpublished literature and maps pertaining to regional faulting, seismic hazards and soil and geologic conditions within and adjacent to the site that could have an impact on the proposed development.
2. Review the field investigation and laboratory testing performed by the prior geotechnical engineer of record.
3. Engineering and geologic analyses of the field and laboratory data as they pertain to the proposed construction.
4. Perform a current seismic hazard analysis.
5. Perform a liquefaction analysis on previous Cone Penetrometer Test soundings.
6. Preparation of this geotechnical report presenting our findings, conclusions and recommendations for site grading and design of building foundation systems in conformance with requirements of the 2019 CBC.

LOCATION AND SITE DESCRIPTION

The site is located at the northeast corner of the prolongation of Avenue 64 and Harrison Street in the Thermal area of Riverside County, California. The approximately rectangular shaped parcel consists of four separate adjacent parcels (Assessor's Parcel Numbers 751-020-002, 751-020-006, 751-020-007, and 951-020-003) comprising approximately 628 acres. The site is bounded on the west by Harrison Street, an improved county road, with agricultural and unimproved land beyond; on the south by the prolongation of Avenue 64, currently unimproved and possibly situated with irrigation channels and unimproved vacant land beyond; on the east by the prolongation of Tyler Street, currently unimproved with unimproved and agricultural land beyond; and on the north by Avenue 62, an improved county road, with agricultural land beyond. The site is relatively flat, generally sloping gently down from north to south.

Site elevations range from -148 feet to -134 feet below Mean Sea Level (MSL). The ground surface appears to be graded to accommodate irrigated field crops. The site location is shown in Figure 1.

PROPOSED CONSTRUCTION

Based on a conceptual drawing titled Site Plan Option H (undated, unattributed) provided by the client, a majority of the perimeter areas of the site will contain residential housing including medium density, low density, estate, and condominium developments, as well as a retail center, hotel, and recreational vehicle park, common areas, and roadways to accommodate the proposed developments. These perimeter developments will surround a lagoon with beach recreation, a horse park and a horse show ring complex.

No structural details have been provided; it is assumed that the residential units will consist of conventional wood-framed construction on lightly loaded foundations. Similar construction for the retail center and hotel building is assumed, but could also include concrete masonry unit (CMU) or other structural systems. When structural design details for retail, hotel, and show ring improvements are available, Petra can provide additional foundation recommendations appropriate to the proposed construction.

No preliminary grading plans were available at the time this report was prepared, but based on the relatively flat site and limited elevation changes across the site, minor cuts and fills could range up to 6 or 8 feet from existing grade. It should be noted, however, that remedial grading (i.e., excavation and re-compaction of the any undocumented fill soils and loose native soils) will entail deeper cuts from exiting grades as recommended in subsequent sections of this report. No extensive subterranean construction is anticipated. It does not appear that tall slopes or retaining walls will be necessary to achieve the desired improvements.

FIELD EXPLORATION AND TESTING

The initial subsurface field exploration was performed by ESS on August 10 through 12, 2004 as reported in their Geotechnical Investigation Feasibility Report (ESS, 2004). The exploration consisted of 10 hollow-stem flight auger (HSFA) borings advanced to depths ranging from 14 to 49 feet below existing grade. The borings were logged and sampled by ESS staff. The sampling procedure elucidated in the report follows below:

Samples were obtained within the test borings using a Standard Penetration (SPT) sampler (ASTM D 1586) and a Modified California (MC) ring sampler (ASTM D 3550 with shoe similar to ASTM D 1586). The SPT sampler has a 2-inch outside diameter and a 1.38-inch inside diameter. The MC sampler has a 3-inch outside diameter and a 2.37-inch inside diameter. The samples were obtained by driving the sampler with a 140-pound hammer, manually activated by rope and cathead, dropping 30 inches in general accordance with ASTM D 1586. Recovered soil samples were sealed in containers and returned to the laboratory. Bulk samples were also obtained from auger cuttings, representing a mixture of soils encountered at the depths noted.

The approximate boring locations were shown in the referenced report as their Figure 2. Their boring logs and Figure 2 have been reproduced and are presented in Appendix A. Petra has reviewed the reported procedure followed during the exploration and the resultant boring logs and accepts the data as representative of the site conditions.

Subsequent to the HSFA borings, ESS conducted 8 Cone Penetrometer Test (CPT) soundings. The details of the soundings are presented in the ESS report (2004).

Subsurface exploration was conducted on September 7, 2004 using Holguin, Fahan & Associates, Inc. of Irvine, California to advance eight electric cone penetrometer (CPT) soundings to an approximate depth of 50 feet.

The CPT exploration was conducted by hydraulically advancing an instrument Hogentogler 10 cm² conical probe into the ground at a ground rate of 2 cm per second using a 23-ton truck as a reaction mass. An electronic data acquisition system recorded a nearly continuous log of the resistance of the soil against the cone tip (Qc) and soil friction against the cone sleeve (Fs) as the probe was advanced.

Graphical CPT sounding data was reproduced herein as Appendix A with the sounding locations shown on the reproduced Figure 2. Petra has reviewed the reported procedure followed during the CPT soundings and the resultant graphic data output and accepts the data as representative of the site conditions.

It should be noted that, in the absence of electronic CPT data, the graphical results were digitized by Petra for reuse in the current liquefaction and seismic settlement analysis presented herein.

Laboratory Testing

Laboratory testing was performed by ESS on samples obtained during their field exploration. Tests reported by ESS include soil classification, in-place moisture content and dry density, maximum dry density and optimum moisture content, grain size analysis, and corrosion potential.

The testing is reported to have been performed according to relevant ASTM Standards (where applicable). Test results obtained from the ESS report have been reproduced and are presented in Appendix B or on the relevant boring logs. Petra has reviewed the laboratory test data and accepts the data as representative of the site soil conditions.

FINDINGS

Previous Land Use

In a review of Google Earth™ historic imagery commencing around 1985 through 2021, the site appears to have been used for agricultural purposes. Recent imagery shows what appear to be agricultural sheds in the middle of the north half of the site, as well as a small parcel (approximately 0.2 acre) with unidentified structures thereon. Isolated tank-type structures are also located near the center of the parcel. Although not verified, it is likely that water conveyances for irrigation are located within the boundaries of the parcel.

Regional Physiographic Setting

The property lies within the Salton Trough that comprises a portion of the Colorado Desert Geomorphic Province. The Salton Trough region is well known for its exposures of the San Andreas and related faults that form the margin between the Pacific and North American Plates. In southern California, these plates move past each other along a somewhat diffuse array of faults comprising the San Andreas Fault System (Powell, 1993). Geologic development of the Salton Trough began as a major, half-graben basin when regional crustal extension affected much of western North America in Miocene time prior to the development of the San Andreas Fault System. During the past 12 to 15 million years, the modern Salton Trough has continued to develop during formation of the northern part of the Gulf of California rift basin. This is due to “pull-apart” oblique strike-slip motion between the North American and Pacific plates within the Sea of Cortez (Gulf of Mexico), which continues into the southern Salton Trough region.

The Salton Trough, part of which is below sea level, has progressively been filling with sediments eroded from the San Jacinto Mountains along the western margins, the San Bernardino Mountains and Little San Bernardino Mountains to the north and northeast respectively, the Orocopia Mountains to the east, and sediments deposited by the Colorado River to the southeast. Sediments in the Salton Trough are estimated to be over three miles thick.

Local Geology and Subsurface Conditions

Our review of published regional geologic maps (Lancaster, Hayhurst and Bedrossian, 2012) and the subsurface exploration and testing performed by ESS indicate that the subject property and surrounding areas are underlain by geologically young (late-Quaternary) alluvial deposits. These soils are described as generally consisting of unconsolidated, very fine-grained sand and silty sand.

Groundwater

During historical periods, a large lake (Ancient Lake Cahuilla) would extend over much of the current Salton Trough. A high water stands of approximately 43 feet above mean sea level occurred during numerous times from approximately 300 A.D. to about 1650 A.D. Ancient shorelines can be seen around the margins of the Salton Trough and are clearly visible in many aerial photographs. There have been approximately five to six high water stands of Lake Cahuilla in the area during the past twelve hundred years (Philibosian and others, 2011).

The site is located within the Coachella-Indio Groundwater Sub-Basin (California Department of Water Resources [CDWR], Water Data Library, 2018). Groundwater depth varies within the area as indicated from water level data obtained from the CDWR website.

Earth Systems (2004) encountered groundwater approximate 8 to 10 feet below ground surface in their investigation.

Tectonic Setting

Regional Surface Fault Systems

Based on our review of the referenced geologic maps and literature, no active faults are known to project through the property. Furthermore, the site does not lie within the boundaries of an “Earthquake Fault Zone” as defined by the State of California in the Alquist-Priolo Earthquake Fault Zoning Act (CGS, 2018). The Alquist-Priolo Earthquake Fault Zoning Act (AP Act) defines an *active fault* as one that “has had surface displacement within Holocene time (about the last 11,000 years).” The main objective of the AP Act is to prevent the construction of dwellings on top of active faults that could displace the ground surface resulting in loss of life and property.

However, it should be noted that according to the USGS Unified Hazard Tool website and/or 2010 CGS Fault Activity Map of California, the San Andreas Fault, located approximately 7 miles northeast of the site, would probably generate the most severe site ground motions and, therefore, is the majority contributor to the deterministic minimum component of the ground motion models. The subject site is located at a distance of less than 9.5 miles (15 km) from the surface projection of this fault system, which is capable of producing a magnitude 6 or larger events with a slip rate along the fault greater than 0.04 inch per year. As such, the site should be considered as a **Near-Fault Site** in accordance with ASCE 7-16, Section 11.4.1.

In spite of the active tectonic regime, earthquakes in the Coachella Valley region within historical times (i.e., the past couple hundred years) have been infrequent and typically of small magnitude. Table 1 shows earthquake activity within recent historical time for the Southern California region. A listing of historical earthquakes published by the National Earthquake Information Center (2006) The largest historic earthquake occurring within a radius of approximately 62 miles (100 kilometers) of the site was the Magnitude 7.3 Landers earthquake in 1992. This event, along with the associated aftershocks, occurred approximately 34 miles northeast of the subject property. The closest documented earthquake greater than Magnitude 6.0, was a Magnitude 6.3 Joshua Tree earthquake that occurred approximately 20 miles north of the site in 1992.

The most recent surface-rupturing earthquake on the Coachella segment of the San Andreas fault likely occurred in the late 1600's (Fumal *et al.*, 2002). Prior to that, apparently five paleo earthquakes occurred on the Coachella segment in about A.D. 825, 982, 1231, 1502, and 1680 based on a trenching study at Thousand Palms Oasis (Fumal *et al.*, 2002). These data indicate that the average repeat time for surface-rupturing earthquakes on the Coachella-Indio segment of the San Andreas fault is approximately 215 +/- 25 years, and that the last surface-rupturing event occurred approximately 325 years ago (Fumal *et al.*, 2002).

The following six historical earthquakes have significantly affected the immediate vicinity of the site in the last 100 years, based upon the available data:

- *El Mayor-Cucapah Earthquake:* On April 4, 2010 (Easter Sunday), an earthquake of moment magnitude of 7.2 occurred in northern Baja California, Mexico. This event was moderately felt in the Palm Springs area with minor damage reported.
- *Desert Hot Springs Earthquake:* On December 4, 1948, an earthquake of moment magnitude 6.0 occurred east of Desert Hot Springs. This event was strongly felt in the Palm Springs area.
- *Palm Springs Earthquake:* On July 8, 1986, an earthquake of moment magnitude 6.2 occurred in the Painted Hills causing minor surface creep of the Banning segment of the San Andreas Fault. This event was strongly felt in the Palm Springs area and reportedly caused various structural damage and injuries to the residents of that area.
- *Joshua Tree Earthquake:* On April 22, 1992, an earthquake of moment magnitude 6.1 occurred in the mountains 9 miles east of the Desert Hot Springs. Structural damage and minor injuries occurred in the Palm Springs area as a result of this earthquake.
- *Landers and Big Bear Earthquake:* On June 28, 1992, an earthquake of moment magnitude 7.3 occurred near Landers. Surface rupture reportedly occurred just south of the town of Yucca Valley and extended some 43 miles toward Barstow. Another earthquake, on the same day of moment

magnitude 6.4 occurred near Big Bear Lake. No structural damage from these earthquakes was reported in the Palm Springs area as a result of this earthquake.

- *Hector Mine Earthquake:* On October 16, 1999, an earthquake of moment magnitude 7.1 occurred on the Lavic Lake and Bullion Mountain faults north of Twentynine Palms. No structural damage from these earthquakes was reported in the Coachella Valley area as a result of this earthquake.

Table 1 lists other significant earthquakes in the Salton Trough region in addition to the ones discussed above.

TABLE 1
Notable Historical Earthquakes in the Salton Trough Region

Date	Location	Magnitude
2010	El Mayor-Cucapah	7.2
1999	Hector Mine, Mojave Desert	7.1
1992	Big Bear, San Bernardino Mountains	6.6
1992	Landers, Mojave Desert	7.3
1992	Joshua Tree, Mojave Desert	6.1
1987	Superstition Hills, Salton Trough	6.6
1986	Palm Springs, Salton Trough	5.9
1979	Imperial Valley, Salton Trough	6.4
1968	Borrego Mountain, Salton Trough	6.5
1948	Desert Hot Springs, Salton Trough	6.0
1944	San Geronio Pass	5.3
1940	Imperial Valley, Salton Trough	6.9
1934	Laguna Salada, Salton Trough	6.7
1934	Laguna Salada, Salton Trough	7.1
1923	Loma Linda, San Bernardino Valley	6.2
1915	Cerro Prieto, Salton Trough	6.0
1915	Cerro Prieto, Salton Trough	7.1
1907	Eastern San Bernardino Mountains	5.5-6
1899	Lytle Creek, Cajon Pass	6.5
1892	Laguna Salada, Salton Trough	> 7
1857	Fort Tejon, Transverse Ranges	7.8
1852	Cerro Prieto, Salton Trough	6.5

Nearby Seismic Sources

Published geologic maps and literature indicate that the site lies approximately 30 miles from a number of significant active and potentially active faults (including the various segments of the San Andreas fault zone) that are considered capable of generating strong ground motion at the subject site. The names and locations of these faults relative to the subject property are provided in Table 2.

TABLE 2
Significant Nearby Seismic Sources

Fault Name	Approximate Distance/ Direction from Site ⁽³⁾	Slip Rate (mm/yr) ¹	Maximum Magnitude ¹
South San Andreas (Coachella)	7 miles northeast	20	7.1
South San Andreas (combined segments)	7 miles northeast	20-35	8.2
Eureka Peak	21 miles north-northwest	0.6	6.7
Burnt Mountain	22 miles northwest	0.6	6.8
Pinto Mountain	30 miles northeast	2.5	7.3
So. Emerson-Copper Mountain	33 miles north	0.6	7.1
San Jacinto (Coyote Creek)	34 miles south	14	7.5 ⁽²⁾
San Jacinto (San Jacinto Valley)	35 miles southwest	18	7.5 ⁽²⁾
Calico-Hidalgo	40 miles north	1.8	7.4
Pisgah-Bullion Mountain	44 miles northeast	0.8	7.3
Johnson Valley	44 miles north	0.6	6.9
Earthquake Valley	47 miles southwest	2.0	6.8
North Frontal Fault	47 miles northwest	0.5	7.0
Elsinore (Julian Section)	49 miles southwest	3.0	7.4
Elmore Ranch	50 miles southeast	1.0	6.7

Note: ¹ Per USGS 2008 National Seismic Hazard Maps – Source Parameters

² Per Southern California Earthquake Data Center

³ Per CGS Fault Map of California 2010

Secondary Seismic Effects

The site area exhibits generally flat topography that is not prone to landsliding. Secondary effects of seismic activity normally considered as possible hazards to a site include several types of ground failure. Various general types of ground failures, which might occur as a consequence of severe ground shaking at the site, include ground subsidence, liquefaction, ground lurching and lateral spreading. The probability of occurrence of each type of ground failure depends on the severity of the earthquake, distance from faults,

topography, subsoil and groundwater conditions, in addition to other factors. Liquefaction, dynamic settlement, and lateral spreading potentials are discussed in the next sections.

Liquefaction and Seismically Induced Settlement

Liquefaction

Liquefaction occurs when strong seismic shaking of a saturated sand or silt causes intergranular fluid (pore-water) pressures to increase to levels where grain-to-grain contact is lost, and material temporarily behaves as a viscous fluid. Liquefaction can cause settlement of the ground surface, loss of bearing, settlement and tilting of structures, flotation and buoyancy of buried structures and fissuring of the ground surface. A common surface manifestation of liquefaction is the formation of sand boils – short-lived fountains of soil and water that emerge from fissures or vents and leave freshly deposited, usually conical mounds of sand or silt on the ground surface.

‘Dry Sand’

For sandy soils above the water table, strong seismic shaking can also result in rearrangement of the granular soil structure leading to densification of sandy soils, ground settlement and settlement and tilting of superstructures.

Seismically Induced Settlement Parameters

Assessment of liquefaction or dry sand settlement potential for a particular site requires knowledge of a number of regional as well as site-specific parameters, including the estimated design earthquake magnitude, and the associated probable peak horizontal ground acceleration at the site, subsurface stratigraphy and soil characteristics. Parameters such as estimated probable peak horizontal ground acceleration can readily be determined using published references, or by utilizing a commercially available computer program specifically designed to perform a probabilistic analysis. On the other hand, stratigraphy and soil characteristics can only be accurately determined by means of a site-specific subsurface investigation combined with appropriate laboratory analysis of representative samples of onsite soils.

The site is located in an area that has not been evaluated for seismic hazards. Site conditions, including near surface soil type and density, as well as current and historic groundwater level, suggest a potential for liquefaction during the design-level earthquake. A review of limited groundwater level data available on the California Department of Water Resources website for a nearby monitoring well (CASGEM Well ID 51659, located approximately 1 mile southeast of the site) indicates that high ground water for this area, within the timespan recorded for the well, is approximately 10 feet below ground surface. ESS reported in-

situ groundwater depth around 8 feet below existing grade at the time of their exploration. Based on the available data, a groundwater depth of 8 feet below ground surface was used in the liquefaction analysis.

Liquefaction Settlement

Petra used the above information, a moment magnitude of 7.34 and PGA_M of 0.73 g from the results of a seismic hazard analysis presented below (please see Table 4, discussed later in this report), and the re-digitized data from the graphical CPT soundings conducted by ESS to perform a liquefaction and seismic settlement analysis using the software program Cliq version 3.4.1.4 by Geologismiki. Petra evaluated the liquefaction potential and resultant dynamic settlement using two state-of-the-practice methodologies: Robertson (2009) and Boulanger and Idriss (2014). The Robertson method produced slightly more conservative results, and are presented herein. The complete analysis from both methods is presented in Appendix E. Total free-field liquefaction settlement is estimated to be on the order of $\frac{3}{4}$ to $1\frac{1}{2}$ inches with differential settlement estimated to be on the order of 1 inch over a span of 40 feet. The complete output from the seismic settlement analysis presented in Appendix E of this report.

Dry Sand (Dynamic) Settlement

Propagating earthquake waves induce shearing stresses and strains in soil materials during strong ground shaking. This process rearranges the structure of granular soils such that there is an increase in density, with a corresponding decrease in volume, which results in vertical settlement. Dynamic settlement has been well documented in wet, sandy deposits undergoing liquefaction (see Tokimatsu and Seed, 1987) and in relatively dry sediments as well (Stewart et al, 1996). Specific methods to analyze potential wet and dry dynamic settlement are reported in Tokimatsu and Seed (1987), Pradel (1998), and Stewart et al. (2001; 2002). Most of the referenced papers focus on the seismic effects on dry, clean sands of a uniform grain size, though several reports extend the literature to fine-grained soils (Stewart et al., 2001 & 2002). State guidelines for evaluating dynamic settlement are provided in the California Geological Survey Special Publication 117A (CGS, 2008).

Dry sand settlement was evaluated using data from the CPT soundings under the same site conditions and seismic demand set forth for liquefaction settlement. Presented dry sand settlement assumes removal and compaction of the upper 6 feet of existing soils, as recommended below. Dry sand settlement may contribute an additional $\frac{1}{4}$ inch of seismically induced settlement.

Total Seismically Induced Settlement

The minimum goal of dynamic (i.e., seismic) settlement mitigation should be to provide a foundation system that can withstand the expected movement without causing such structural damage resulting in a

life-safety hazard (such as structural collapse from excessive drift). The conclusions expressed herein are reached based on data obtained from CPT soundings and conventional borings.

As noted previously herein, the graphical data from eight CPT soundings performed by ESS was re-digitized and used in our analysis using GeoLogismiki software, Cliq V.3.4.1.4. The results of our preliminary analysis using available subsurface data indicate that the highest total seismically induced settlement at the site is anticipated to be less than 1¾ inches. SP 117A indicates that liquefaction settlement can typically be mitigated by structural methods alone when total settlements do not exceed 4 inches; therefore, Petra does not recommend deep ground improvement or other seismic related mitigations for this project. Notably, the seismic settlements are all relatively uniform, and the distance between CPT soundings relatively large, therefore Petra estimates that differential seismic settlements should not be expected to exceed about 1 inch over a distance of 40 feet. The complete analysis is presented in Appendix E. A summary of calculated liquefaction and dry sand settlements is presented in Table 3.

TABLE 3
Total Seismic Settlement

CPT Sounding Number	Estimated Liquefaction Settlement, in.	Estimated Dry Sand Settlement, in.	Total Combined Dry Sand and Liquefaction Settlement ¹ , in.
CPT-1	1.00	0.25	1.25
CPT-2	1.10	0.25	1.35
CPT-3	1.10	0.25	1.35
CPT-4	1.30	0.25	1.55
CPT-5	0.80	0.25	1.05
CPT-6	1.25	0.25	1.50
CPT-7	1.20	0.25	1.45
CPT-8	1.10	0.25	1.35

⁽¹⁾ Includes depth weighting after Cetin (2009)

Lateral Spreading

Lateral spreading is the tendency of liquefied soils to move, either downslope in the case of gently sloping ground, or toward an open face such as a channel. The subject site is relatively flat, and lateral spreading is not considered to be a likely occurrence.

CONCLUSIONS AND RECOMMENDATIONS

General Feasibility

From a soils engineering and engineering geologic point of view, the subject property is considered suitable for development. It is our opinion that the anticipated construction will not adversely affect the geologic stability of adjoining properties in an adverse manner provided grading and construction are performed in accordance with current standards of practice, all applicable grading ordinances and the recommendations presented in this report.

Earthwork and Grading

General Specifications

All earthwork and grading should be performed in accordance with all applicable requirements of the grading and excavation codes of the County of Riverside, and in compliance with all applicable provisions of the 2019 California Building Code (2019 CBC). Grading should also be performed in accordance with the recommendations provided in this report.

Geotechnical Observations and Testing

Prior to the start of earthwork, a meeting should be held at the site with the owner, contractor and geotechnical consultant to discuss the work schedule and geotechnical aspects of the grading. Earthwork, which in this instance will generally entail removal and re-compaction of the near surface soils, should be accomplished under full-time observation and testing by the geotechnical consultant. A representative of the project geotechnical consultant should be present onsite during all earthwork operations to document placement and compaction of fills, as well as to document compliance with the other recommendations presented herein.

Demolition, Clearing and Grubbing

All existing structures (if any), foundations, asphalt or concrete pavements, vegetation and subsurface utility installations throughout the site should be demolished and removed from the site. Following demolition, clearing operations should also include the removal of any remaining trash, debris, vegetation and similar deleterious materials including the root balls from any trees or other vegetation. Any cavities or excavations created upon removal of any unknown subsurface structures or inclusions should be cleared of loose soil, shaped to provide access for backfilling and compaction equipment and then backfilled with engineered fill. Note that buried deleterious materials may be encountered within the site (i.e., buried

organics or debris) due to the past site usage and may need to be removed by hand (i.e. root pickers), during grading operations.

The project geotechnical consultant should provide periodic observation and testing services during final clearing and grubbing operations to document compliance with the above recommendations. In addition, should unusual or adverse soil conditions or unanticipated buried structures be encountered during grading that are not described herein, these conditions should be brought to the immediate attention of the project geotechnical consultant for corrective recommendations.

Unsuitable Soil Removals and Bottom Processing

Any existing undocumented fill and near surface native soils are considered unsuitable for support of proposed structures and should be removed to underlying competent alluvial materials as approved by the project geotechnical consultant. The estimated depth of removal of fill soils is recommended to be approximately 6 feet below the existing ground surface in proposed building areas. The depth of removal may be on the order of about 2 feet for local streets, alleyways and drives. Consideration should be given to locally deepening the excavation at the location of tree roots, any underground structure and other proposed subterranean features in order to provide a uniform depth of compacted fill in all areas. Soil removals could be locally deeper depending upon the actual exposed conditions encountered during grading. At a minimum, the over-excavation should extend a distance beyond the perimeter of the structure equal to the depth of the over-excavation. The actual depths and horizontal limits of removals and over-excavations should be evaluated upon availability of the site grading plan and during grading on the basis of observations and testing performed by the project geotechnical consultant. Excavated soils, if free of deleterious materials, are considered acceptable for use as compacted fill.

Prior to placing engineered fill, the exposed bottom surfaces in the removal areas should be approved by a representative of project geotechnical consultant. The exposed bottom(s) should be scarified to a minimum depth of 12 inches, moisture-conditioned or air-dried to achieve approximately two percent above optimum moisture content and then compacted with a heavy construction equipment prior to placement of fill. Minimum compaction of the upper 12 inches of the removal bottom should meet or exceed 90 percent relative compaction. The laboratory maximum dry density, the standard for determining relative compaction and optimum moisture content, for each change in soil type should be determined in accordance with Test Method ASTM D 1557.

Grading at Site Boundaries

Average remedial removals within the building pad areas of the subject site are anticipated to be on the order of 6 feet below the existing ground surface, although locally deeper over-excavation is possible. If remedial grading is necessary immediately adjacent to the property boundaries, temporary backcut slopes should generally be restricted to a slope ratio of 1:1 (h:v) or flatter to protect adjacent offsite improvements (including pavement, sidewalks, walls, buried utilities, etc.). Depending on the actual horizontal extent of necessary remedial grading, a wedge of unsuitable soil may remain in place along the site perimeter that will extend into the site. Any new perimeter site improvements that are anticipated to be within this zone may need to be designed and constructed with deepened and/or strengthened foundation systems designed to withstand relative movement that is likely to result from settlement of these likely compressible surficial soils. Alternately, the remedial grading adjacent to the site boundaries may be accomplished by the slot-cutting method. More specific recommendations may be appropriate once the rough grading plan is available for review.

Excavation Characteristics

Based on the observed soils types in the reported borings, shallow excavation of soils within the site are expected to be readily excavatable with conventional earthmoving equipment.

Fill Placement

All fill materials should be placed in approximately 6- to 8-inch thick loose lifts, watered or air-dried as necessary to achieve a minimum moisture content at least 2 percent above the optimum moisture condition, and then compacted in-place to a minimum relative compaction of 90 percent. The laboratory maximum dry density and optimum moisture content for each change in soil type should be determined in accordance with ASTM D 1557.

Imported Soils

The size of the site and the presence of a large horse park should provide ample resources to balance proposed grading and avoid the necessity of importing or exporting soil. If, however, imported soils are required to complete the planned grading, these soils should consist of clean materials devoid of rock exceeding a maximum dimension of 3 inches, organics, trash and other deleterious materials. To avoid making revisions to the foundation design, imported soils should also be granular and exhibit a very low expansion potential (Expansion Index 0-20). Prospective import soils should be observed at the source, tested and approved by the geotechnical consultant prior to importing the soils to the site. It is recommended

that the project environmental consultant should also be notified so that they can confirm the suitability of the proposed import material from an environmental standpoint.

Volumetric Changes - Bulking, Shrinkage and Subsidence

An average shrinkage factor estimated at 19 to 25 percent is anticipated when excavated on-site soils are replaced as properly compacted fill. A subsidence, estimated at 0.15 to 0.25 feet may also occur when exposed bottom surfaces in removal areas are scarified and re-compacted as recommended herein. These estimates of shrinkage and subsidence are intended for use by project planners in estimating earthwork quantities and should not be considered absolute values. Contingencies should be made for balancing earthwork quantities based on actual shrinkage and subsidence that will occur during grading.

Temporary Excavations

Temporary excavations varying up to a depth of up to roughly 8 feet, with potentially deeper localized removals below existing grades may be required to accomplish the recommended over-excavation of existing soils and provide a uniform layer of compacted fill. Based on the physical properties of the onsite soils, temporary excavations which are constructed exceeding 4 feet in height should be cut back to an inclination of 1:1 (h:v) or flatter for the duration of the over-excavation of unsuitable soil material and replacement as compacted fill, as well as placement of underground utilities. The 1:1 (h:v) recommendation may possibly be adjusted, depending on conditions observed by a representative of the project geotechnical consultant. Other factors which should be considered with respect to the stability of the temporary slopes include construction traffic and/or storage of materials on or near the tops of the slopes, construction scheduling, presence of nearby walls, utilities, or structures on adjacent properties and weather conditions at the time of construction. Applicable requirements of the California Construction and General Industry Safety Orders, the Occupational Safety and Health act of 1970 and the Construction Safety Act should also be followed.

PRELIMINARY FOUNDATION DESIGN CONSIDERATIONS

Seismic Design Coefficients

Earthquake loads on earthen structures and buildings are a function of ground acceleration which may be determined from the site-specific ground motion analysis. Alternatively, a design response spectrum can be developed for certain sites based on the code guidelines. To provide the design team with the parameters necessary to construct the design acceleration response spectrum for this project, we used two computer applications. Specifically, the first computer application, which was jointly developed by Structural

Engineering Association of California (SEAOC) and California's Office of Statewide Health Planning and Development (OSHPD), the SEA/OSHPD Seismic Design Maps Tool website, <https://seismicmaps.org>, is used to calculate the ground motion parameters. The second computer application, the United States Geological Survey (USGS) Unified Hazard Tool website, <https://earthquake.usgs.gov/hazards/interactive/>, is used to estimate the earthquake magnitude and the distance to surface projection of the fault. The results obtained from these websites is presented in Appendix D.

To run the above computer applications, site latitude and longitude, seismic risk category and knowledge of site class are required. The site class definition depends on the direct measurement of certain soil properties and the ASCE 7-16 recommended procedure for calculating the average shear wave velocity within the upper 30 meters (approximately 100 feet) of site soils. Several methods exist to determine the shear wave velocity and determine the site class. When insufficient data exists to perform these calculations, it is permitted to use a designation of Site Class D – Default.

In fact, Section 20.3.1 of ASCE 7-16 requires the assignment of Site Class F if liquefiable soils are present, leading to a requirement to perform a site response analysis. However, an exception for structures that have fundamental periods of vibration equal to or less than 0.5 seconds allows the site class to be assigned pursuant to ASCE 7-16, §20.3. Based on this exception, notwithstanding the presence of liquefiable soil, Petra has determined that Site Class D – Default is appropriate for this project. The project structural engineer should verify the validity of the assumption regarding the fundamental period of vibration of the proposed structures. If design of the proposed structures results in a fundamental period of vibration that exceeds 0.5 seconds, a site response analysis will be required.

A seismic risk category of II was assigned to the proposed project in accordance with 2019 CBC, Table 1604.5. Table 4, below, provides parameters required to construct the design acceleration response spectrum based the 2019 CBC guidelines.

TABLE 4
Seismic Design Parameters

Ground Motion Parameters	Specific Reference	Parameter Value	Unit
Site Latitude (North)	-	33.5853	°
Site Longitude (West)	-	-116.1795	°
Site Class Definition	Section 1613.2.2 ⁽¹⁾ , Chapter 20 ⁽²⁾	D-Default ⁽⁴⁾	-
Assumed Risk Category	Table 1604.5 ⁽¹⁾	II	-
M _w - Earthquake Magnitude	USGS Unified Hazard Tool ⁽³⁾	7.34 ⁽³⁾	-
R – Distance to Surface Projection of Fault	USGS Unified Hazard Tool ⁽³⁾	11.8 ⁽³⁾	km
S _s - Mapped Spectral Response Acceleration Short Period (0.2 second)	Figure 1613.2.1(1) ⁽¹⁾	1.5 ⁽⁴⁾	g
S ₁ - Mapped Spectral Response Acceleration Long Period (1.0 second)	Figure 1613.2.1(2) ⁽¹⁾	0.6 ⁽⁴⁾	g
F _a – Short Period (0.2 second) Site Coefficient	Table 1613.2.3(1) ⁽¹⁾	1.2 ⁽⁴⁾	-
F _v – Long Period (1.0 second) Site Coefficient	Table 1613.2.3(2) ⁽¹⁾	Null ⁽⁴⁾	-
S _{MS} – MCE _R Spectral Response Acceleration Parameter Adjusted for Site Class Effect (0.2 second)	Equation 16-36 ⁽¹⁾	1.8 ⁽⁴⁾	g
S _{M1} - MCE _R Spectral Response Acceleration Parameter Adjusted for Site Class Effect (1.0 second)	Equation 16-37 ⁽¹⁾	Null ⁽⁴⁾	g
S _{DS} - Design Spectral Response Acceleration at 0.2-s	Equation 16-38 ⁽¹⁾	1.2 ⁽⁴⁾	g
S _{D1} - Design Spectral Response Acceleration at 1-s	Equation 16-39 ⁽¹⁾	Null ⁽⁴⁾	g
T ₀ = 0.2 S _{D1} / S _{DS}	Section 11.4.6 ⁽²⁾	Null	s
T _s = S _{D1} / S _{DS}	Section 11.4.6 ⁽²⁾	Null	s
T _L - Long Period Transition Period	Figure 22-14 ⁽²⁾	8 ⁽⁴⁾	s
PGA - Peak Ground Acceleration at MCE _G ^(*)	Figure 22-9 ⁽²⁾	0.612 ⁽⁴⁾	g
F _{PGA} - Site Coefficient Adjusted for Site Class Effect ⁽²⁾	Table 11.8-1 ⁽²⁾	1.2 ⁽⁴⁾	-
PGA _M –Peak Ground Acceleration ⁽²⁾ Adjusted for Site Class Effect	Equation 11.8-1 ⁽²⁾	0.734 ⁽⁴⁾	g
Design PGA ≈ (2/3 PGA _M) - Slope Stability ^(†)	Similar to Eqs. 16-38 & 16-39 ⁽²⁾	0.489	g
Design PGA ≈ (0.4 S _{DS}) – Short Retaining Walls ^(‡)	Equation 11.4-5 ⁽²⁾	0.48	g
C _{RS} - Short Period Risk Coefficient	Figure 22-18A ⁽²⁾	0.909 ⁽⁴⁾	-
C _{R1} - Long Period Risk Coefficient	Figure 22-19A ⁽²⁾	0.891 ⁽⁴⁾	-
SDC - Seismic Design Category ^(§)	Section 1613.2.5 ⁽¹⁾	Null ⁽⁴⁾	-
References: ⁽¹⁾ California Building Code (CBC), 2019, California Code of Regulations, Title 24, Part 2, Volume I and II. ⁽²⁾ American Society of Civil Engineers/Structural Engineering Institute (ASCE/SEI), 2016, Minimum Design Loads and Associated Criteria for Buildings and Other Structures, Standards 7-16. ⁽³⁾ USGS Unified Hazard Tool - https://earthquake.usgs.gov/hazards/interactive/ ⁽⁴⁾ SEI/OSHPD Seismic Design Map Application – https://seismicmaps.org Related References: Federal Emergency Management Agency (FEMA), 2015, NEHERP (National Earthquake Hazards Reduction Program) Recommended Seismic Provision for New Building and Other Structures (FEMA P-1050).			
Notes: * PGA Calculated at the MCE return period of 2475 years (2 percent chance of exceedance in 50 years). † PGA Calculated at the Design Level of 2/3 of MCE; approximately equivalent to a return period of 475 years (10 percent chance of exceedance in 50 years). ‡ PGA Calculated for short, stubby retaining walls with an infinitesimal (zero) fundamental period. § The designation provided herein may be superseded by the structural engineer in accordance with Section 1613.2.5.1, if applicable.			

Discussion

Owing to the characteristics of the subsurface soils, as defined by Site Class D-Default designation, and proximity of the site to the sources of major ground shaking, the site is expected to experience strong ground shaking during its anticipated life span. Under these circumstances, where the code-specified design response spectrum may not adequately characterize site response, the 2019 CBC typically requires a site-specific seismic response analysis to be performed. This requirement is signified/identified by the “null” values that are output using SEA/OSHPD software in determination of short period, but mostly, in determination of long period seismic parameters, see Table 4.

For conditions where a “null” value is reported for the site, a variety of design approaches are permitted by 2019 CBC and ASCE 7-16 in lieu of a site-specific seismic hazard analysis. For any specific site, these alternative design approaches, which include Equivalent Lateral Force (ELF) procedure, Modal Response Spectrum Analysis (MRSA) procedure, Linear Response History Analysis (LRHA) procedure and Simplified Design procedure, among other methods, are expected to provide results that may or may not be more economical than those that are obtained if a site-specific seismic hazards analysis is performed. These design approaches and their limitations should be evaluated by the project structural engineer.

Notwithstanding the above discussion, should the Equivalent Lateral Force (ELF) method is used for seismic design of structural elements, the value of Constant Velocity Domain Transition Period, T_s , is estimated to be 0.57 and the value of Long Period Transition Period, T_L , is provided in Table 4 for construction of Seismic Response Coefficient – Period (C_s -T) curve that is used in the ELF procedure.

Please note that the Seismic Design Category, SDC, is also designated as “null” in Table 4. For condition where the mapped spectral response acceleration parameter at 1 – second period, S_1 , is less than 0.75, the 2019 CBC, Section 1613.2.5.1 allows that seismic design category to be determined from Table 1613.2.5(1) alone provided that all 4 requirements concerning fundamental period of structure, story drift, seismic response coefficient, and relative rigidity of the diaphragms are met. Our interpretation of ASCE 7-16 is that for conditions where one or more of these 4 conditions are not met, seismic design category should be assigned based on: 1) 2019 CBC, Table 1613.2.5(1), 2) structure’s risk category and 3) the value of S_{DS} , at the discretion of the project structural engineer.

As stated herein, the subject site is within a Site Class D-Default. A site-specific ground motion hazard analysis is not required for structures on Site Class D-Default with $S_1 \geq 0.2$ provided that the Seismic Response Coefficient C_s is determined in accordance with ASCE 7-16, Article 12.8 and structural design is performed in accordance with Equivalent Lateral Force (ELF) procedure.

Expansive Soil Conditions

Based on available data, near-surface soils are classified as sandy Silt (SM-ML), silty Sand (SM), and low plasticity Silt (ML) with minimal clay encountered. Based on these soil classifications, the site soils are considered Very Low in expansion potential (Expansion Index not greater than 20). Additional sampling and testing should be performed during site grading for determining actual expansion potential of the supporting building pad soils.

FOUNDATION DESIGN GUIDELINES

Allowable Bearing Capacity, Estimated Settlement and Lateral Resistance

Allowable Soil Bearing Capacities

Pad Footings

An allowable soil bearing capacity of 1,500 pounds per square foot may be utilized for design of isolated 24-inch-square pad footings founded at a minimum depth of 12 inches below the lowest adjacent final grade for pad footings that are not a part of the slab system and are used for support of such features as roof overhang, second-story decks, patio covers, etc. This value may be increased by 20 percent for each additional foot of depth and by 10 percent for each additional foot of width, to a maximum value of 2,500 pounds per square foot. The recommended allowable bearing value includes both dead and live loads, and may be increased by one-third for short duration wind forces. Due to the potential for liquefaction, this temporary increase is *not* recommended for seismic loads.

Continuous Footings

An allowable soil bearing capacity of 1,500 pounds per square foot may be utilized for design of continuous footings founded at a minimum depth of 12 inches below the lowest adjacent final grade. This value may be increased by 20 percent for each additional foot of depth and by 10 percent for each additional foot of width, to a maximum value of 2,500 pounds per square foot. The recommended allowable bearing value includes both dead and live loads, and may be increased by one-third for short duration wind forces. Due to the potential for liquefaction, this temporary increase is *not* recommended for seismic loads.

Estimated Static Settlement

Based on the allowable bearing values provided above, total static settlement of the footings under the anticipated loads is expected to be on the order of 1 inch. Differential settlement is expected to be less than $\frac{3}{4}$ inch over a horizontal span of 30 feet. The majority of settlement is likely to take place as footing loads are applied or shortly thereafter.

Estimated Dynamic Settlement

As previously noted, if remedial grading removes and replaces the upper 6 feet of existing soils as compacted fill, the total seismic settlement is estimated to be on the order of 1¾ inches. Design differential dynamic settlement is estimated to be on the order of 2 inches over a span of 40 feet.

Lateral Resistance

A passive earth pressure of 250 pounds per square foot per foot of depth, to a maximum value of 2,500 pounds per square foot, may be used to determine lateral bearing resistance for footings. In addition, a coefficient of friction of 0.30 times the dead load forces may be used between concrete and the supporting soils to determine lateral sliding resistance. The above values may be increased by one-third when designing for transient wind or seismic forces. It should be noted that the above values are based on the condition where footings are cast in direct contact with compacted fill or competent native soils. In cases where the footing sides are formed, all backfill placed against the footings upon removal of forms should be compacted to at least 90 percent of the applicable maximum dry density.

Guidelines for Footings and Slabs on-Grade Design and Construction

The results of ESS field exploration suggest near-surface soils within the site predominantly exhibit non-expansive characteristics (expansion indices that are not greater than 20). As indicated in Section 1803.5.3 of 2019 California Building Code (2019 CBC), for soils that are considered non-expansive the design of slabs on-grade is considered to be exempt from the procedures outlined in Sections 1808.6.2 of the 2019 CBC and may be performed using any method deemed rational and appropriate by the project structural engineer. However, the following minimum recommendations are presented herein for conditions where the project design team may require geotechnical engineering guidelines for design and construction of footings and slabs on-grade the project site.

The design and construction guidelines that follow are based on the above soil conditions and may be considered for reducing the effects of variability in fabric, composition and, therefore, the detrimental behavior of the site soils such as excessive short- and long-term total and differential heave or settlement. These guidelines have been developed on the basis of the previous experience of this firm on projects with similar soil conditions. Although construction performed in accordance with these guidelines has been found to reduce post-construction movement and/or distress, they generally do not positively eliminate all potential effects of variability in soils characteristics and future heave or settlement.

It should also be noted that the suggestions for dimension and reinforcement provided herein are performance-based and intended only as preliminary guidelines to achieve adequate performance under the anticipated soil conditions. However, they should not be construed as replacement for structural engineering analyses, experience, and judgment. The project structural engineer, architect and/or civil engineer should make appropriate adjustments to slab and footing dimensions, and reinforcement type, size and spacing to account for internal concrete forces (e.g., thermal, shrinkage and expansion), as well as external forces (e.g., applied loads) as deemed necessary. Consideration should also be given to minimum design criteria as dictated by local building code requirements.

Conventional Slab-on-Grade System

Since the site soils do not appear to exhibit expansive characteristics, we recommend that footings and floor slabs be designed and constructed in accordance with the following minimum criteria.

Footings

1. Exterior continuous footings supporting one- and two-story structures should be founded at a minimum depth of 12 inches below the lowest adjacent final grade. Interior continuous footings may be founded at a minimum depth of 10 inches below the top of the adjacent finish floor slabs.
2. In accordance with Table 1809.7 of 2019 CBC for light-frame construction, all continuous footings should have minimum widths of 12 inches for one- and two-story construction. We recommend all continuous footings should be reinforced with a minimum of two No. 4 bars, one top and one bottom.
3. A minimum 12-inch-wide grade beam founded at the same depth as adjacent footings should be provided across garage entrances or similar openings (such as large doors or bay windows). The grade beam should be reinforced with a similar manner as provided above.
4. Interior isolated pad footings, if required, should be a minimum of 24 inches square and founded at a minimum depth of 12 inches below the bottoms of the adjacent floor slabs for one- and two-story buildings. . Pad footings should be reinforced with No. 4 bars spaced a maximum of 18 inches on centers, both ways, placed near the bottoms of the footings.
5. Exterior isolated pad footings intended for support of roof overhangs such as second-story decks, patio covers, and similar construction should be a minimum of 24 inches square and founded at a minimum depth of 18 inches below the lowest adjacent final grade. The pad footings should be reinforced with No. 4 bars spaced a maximum of 18 inches on centers, both ways, placed near the bottoms of the footings. Exterior isolated pad footings may need to be connected to adjacent pad and/or continuous footings via tie beams at the discretion of the project structural engineer.
6. The minimum footing dimensions and reinforcement recommended herein may be modified (increased or decreased subject to the constraints of Chapter 18 of the 2019 CBC) by the structural engineer responsible for foundation design based on calculations, engineering experience and judgment.

Building Floor Slabs

1. Concrete floor slabs should be a minimum 4 inches thick and reinforced with No. 3 bars spaced a maximum of 24 inches on centers, both ways. Alternatively, the structural engineer may recommend the use of prefabricated welded wire mesh for slab reinforcement. For this condition, the welded wire mesh should be of sheet type (not rolled) and should consist of 6x6/W2.9xW2.9 (per the Wire Reinforcement Institute, WRI, designation) or stronger. All slab reinforcement should be supported on concrete chairs or brick to ensure the desired placement near mid-depth. Care should be exercised to prevent warping of the welded wire mesh between the chairs in order to ensure its placement at the desired mid-slab position.

Slab dimension, reinforcement type, size and spacing need to account for internal concrete forces (e.g., thermal, shrinkage and expansion) as well as external forces (e.g., applied loads), as deemed necessary by the structural engineer.

2. Living area concrete floor slabs and areas to receive moisture sensitive floor covering should be underlain with a moisture vapor retarder consisting of a minimum 10-mil-thick polyethylene or polyolefin membrane that meets the minimum requirements of ASTM E96 and ASTM E1745 for vapor retarders (such as Husky Yellow Guard®, Stego® Wrap, or equivalent). All laps within the membrane should be sealed, and at least 2 inches of clean sand should be placed over the membrane to promote uniform curing of the concrete. To reduce the potential for punctures, the membrane should be placed on a pad surface that has been graded smooth without any sharp protrusions. If a smooth surface cannot be achieved by grading, consideration should be given to lowering the pad finished grade an additional inch and then placing a 1-inch-thick leveling course of sand across the pad surface prior to the placement of the membrane.

At the present time, some slab designers, geotechnical professionals and concrete experts view the sand layer below the slab (blotting sand) as a place for entrapment of excess moisture that could adversely impact moisture-sensitive floor coverings. As a preventive measure, the potential for moisture intrusion into the concrete slab could be reduced if the concrete is placed directly on the vapor retarder. However, if this sand layer is omitted, appropriate curing methods must be implemented to ensure that the concrete slab cures uniformly. A qualified materials engineer with experience in slab design and construction should provide recommendations for alternative methods of curing and supervise the construction process to ensure uniform slab curing. Additional steps would also need to be taken to prevent puncturing of the vapor retarder during concrete placement.

3. Garage floor slabs should be a minimum 4 inches thick and reinforced in a similar manner as living area floor slabs. Garage slabs should also be poured separately from adjacent wall footings with a positive separation maintained using ¾-inch-minimum felt expansion joint material. To control the propagation of shrinkage cracks, garage floor slabs should be quartered with weakened plane joints. Consideration should be given to placement of a moisture vapor retarder below the garage slab, similar to that provided in Item 2 above, should the garage slab be overlain with moisture sensitive floor covering.
4. Presaturation of the subgrade below floor slabs will not be required; however, prior to placing concrete, the subgrade below all dwelling and garage floor slab areas should be thoroughly moistened to achieve a moisture content that is at least equal to or slightly greater than optimum moisture content. This moisture content should penetrate to a minimum depth of 12 inches below the bottoms of the slabs.

5. The minimum dimensions and reinforcement recommended herein for building floor slabs may be modified (increased or decreased subject to the constraints of Chapter 18 of the 2019 CBC) by the structural engineer responsible for foundation design based on calculations, engineering experience and judgment.

Post-Tensioned Slabs on-Grade System

In consideration of the apparent non-expansive nature of the onsite soils (expansion index not greater than 20), any rational and appropriate procedure may be chosen by the project structural engineer for the design of post-tensioned slabs on-grade. Should the design engineer choose to follow the latest Code-adopted edition of the procedure published by the Post-Tensioning Institute (PTI DC 10.5), the following minimum design criteria are provided Table 5, below.

TABLE 5

Presumptive Post-Tensioned Slab on-Grade Design Parameters for PTI Procedure

Soil Information	
Approximate Depth of Constant Suction, feet	9
Approximate Soil Suction, pF	3.9
Inferred Thornthwaite Index:	-20
Average Edge Moisture Variation Distance, e_m in feet:	
Center Lift	9.0
Edge Lift	4.7
Anticipated Swell, y_m in inches:	
Center Lift	0.25
Edge Lift	0.45

Modulus of Subgrade Reaction

The modulus of subgrade reaction for design of load bearing elements depends on the size of the element and soil-structure interaction. However, as a first level of approximation, this value may be assumed to be 125 pounds per cubic inch.

Minimum Design Recommendations

The soil values provided above may be utilized by the project structural engineer to design post-tensioned slabs on-ground in accordance with Section 1808.6.2 of the 2019 CBC and the PTI publication. Thicker floor slabs and larger footing sizes may be required for structural reasons and should govern the design if more restrictive than the minimum recommendations provided below:

1. Exterior continuous footings for one- and two-story structures should be founded at a minimum depth of 12 inches below the lowest adjacent finished ground surface. Interior footings may be founded at a minimum depth of 10 inches below the tops of the adjacent finish floor slabs.
2. In accordance with Table 1809.7 of 2019 CBC for light-frame construction, all continuous footings should have minimum widths of 12 inches for one- and two-story construction. We recommend all continuous footings should be reinforced with a minimum of two No. 4 bars, one top and one bottom. Alternatively, post-tensioned tendons may be utilized in the perimeter continuous footings in lieu of the reinforcement bars.
3. A minimum 12-inch-wide grade beam founded at the same depth as adjacent footings should be provided across the garage entrances or similar openings (such as large doors or bay windows). The grade beam should be reinforced in a similar manner as provided above.
4. Interior isolated pad footings, if required, should be a minimum of 24 inches square and founded at a minimum depth of 12 inches below the bottoms of the adjacent floor slabs for one- and two-story buildings. Pad footings should be reinforced with No. 4 bars spaced a maximum of 18 inches on centers, both ways, placed near the bottoms of the footings.
5. Exterior isolated pad footings intended for support of roof overhangs such as second-story decks, patio covers, and similar construction should be a minimum of 24 inches square and founded at a minimum depth of 18 inches below the lowest adjacent final grade. The pad footings should be reinforced with No. 4 bars spaced a maximum of 18 inches on centers, both ways, placed near the bottoms of the footings. Exterior isolated pad footings may need to be connected to adjacent pad and/or continuous footings via tie beams at the discretion of the project structural engineer.
6. The thickness of the floor slabs should be determined by the project structural engineer with consideration given to the expansion index of the onsite soils; however, we recommend that a minimum slab thickness of 4 inches be considered.
7. As an alternative to designing 4-inch-thick post-tensioned slabs with perimeter footings as described in Items 1 and 2 above, the structural engineer may design the foundation system using a thickened slab design. The minimum thickness of this uniformly thick slab should be 7.5 inches. The engineer in charge of post-tensioned slab design may also opt to use any combination of slab thickness and footing embedment depth as deemed appropriate based on their engineering experience and judgment.
8. Living area concrete floor slabs and areas to receive moisture sensitive floor covering should be underlain with a moisture vapor retarder consisting of a minimum 10-mil-thick polyethylene or polyolefin membrane that meets the minimum requirements of ASTM E96 and ASTM E1745 for vapor retarders (such as Husky Yellow Guard®, Stego® Wrap, or equivalent). All laps within the membrane should be sealed, and at least 2 inches of clean sand should be placed over the membrane to promote uniform curing of the concrete. To reduce the potential for punctures, the membrane should be placed on a pad surface that has been graded smooth without any sharp protrusions. If a smooth surface cannot be achieved by grading, consideration should be given to lowering the pad finished grade an additional inch and then placing a 1-inch-thick leveling course of sand across the pad surface prior to the placement of the membrane.

At the present time, some slab designers, geotechnical professionals and concrete experts view the sand layer below the slab (blotting sand) as a place for entrapment of excess moisture that could adversely impact moisture-sensitive floor coverings. As a preventive measure, the potential for moisture intrusion into the concrete slab could be reduced if the concrete is placed directly on the vapor retarder. However, if this sand layer is omitted, appropriate curing methods must be implemented to ensure that the concrete slab cures uniformly. A qualified materials engineer with experience in slab design and construction should provide recommendations for alternative methods of curing and supervise the construction process to ensure uniform slab curing. Additional steps would also need to be taken to prevent puncturing of the vapor retarder during concrete placement.

9. Garage floor slabs should be designed in a similar manner as living area floor slabs. Consideration should be given to placement of a moisture vapor retarder below the garage slab, similar to that provided in Item 6 above, should the garage slab be overlain with moisture sensitive floor covering.
10. Presaturation of the subgrade below floor slabs will not be required; however, prior to placing concrete, the subgrade below all dwelling and garage floor slab areas should be thoroughly moistened to achieve a moisture content that is at least equal to or slightly greater than optimum moisture content. This moisture content should penetrate to a minimum depth of 12 inches below the bottoms of the slabs.
11. The minimum footing dimensions and reinforcement recommended herein may be modified (increased or decreased subject to the constraints of Chapter 18 of the 2019 CBC) by the structural engineer responsible for foundation design based on calculations, engineering experience and judgment.

Foundation Excavation Observations

Foundation excavations should be observed by a representative of this firm to document that they have been excavated into competent bearing soils prior to the placement of forms, reinforcement or concrete. The excavations should be trimmed neat, level and square. All loose, sloughed or moisture-softened soils and/or any construction debris should be removed prior to placing of concrete. Excavated soils derived from footing and/or utility trenches should not be placed in building slab-on-grade areas or exterior concrete flatwork areas unless the soils are compacted to at least 90 percent of maximum dry density.

General Corrosivity Screening

Corrosion testing was performed by ESS on a soil sample considered representative of the soils encountered. The methodology and results are presented in Appendix B. Petra has reviewed and accepted the results, but due to the size of the project site and the potential for substantial variability of soils they should be considered to be a screening level study and preliminary in nature to identify potentially corrosive characteristics of these soils. Additional testing is recommended during site grading. The common indicators associated with soil corrosivity include water-soluble sulfate and chloride levels, pH (a measure of acidity), and minimum electrical resistivity.

It should be noted that Petra does not practice corrosion engineering; therefore, the test results, opinion and engineering judgment provided herein should be considered as general guidelines only. Additional analyses would be warranted, especially, for cases where buried metallic building materials (such as copper and cast or ductile iron pipes) in contact with site soils are planned for the project. In many cases, the project geotechnical engineer may not be informed of these choices. Therefore, for conditions where such elements are considered, we recommend that other, relevant project design professionals (e.g., the architect, landscape architect, civil and/or structural engineer) also consider recommending a qualified corrosion engineer to conduct additional sampling and testing of near-surface soils during the final stages of site grading to provide a complete assessment of soil corrosivity. Recommendations to mitigate the detrimental effects of corrosive soils on buried metallic and other building materials that may be exposed to corrosive soils should be provided by the corrosion engineer as deemed appropriate.

In general, a soil's water-soluble sulfate levels and pH relate to the potential for concrete degradation; water-soluble chlorides in soils impact ferrous metals embedded or encased in concrete, e.g., reinforcing steel; and electrical resistivity is a measure of a soil's corrosion potential to a variety of buried metals used in the building industry, such as copper tubing and cast or ductile iron pipes. Table 6, below, presents single value of individual test results with an interpretation of current code indicators and guidelines that are commonly used in this industry. The table includes the code-related classifications of the soils as they relate to the various tests, as well as a general recommendation for possible mitigation measures in view of the potential adverse impact on various components of the proposed structures in direct contact with site soils. The guidelines provided herein should be evaluated and confirmed, or modified, in their entirety by the project structural engineer, corrosion engineer and/or the contractor responsible for concrete placement for structural concrete used in exterior and interior footings, interior slabs on-ground, garage slabs, wall foundations and concrete exposed to weather such as driveways, patios, porches, walkways, ramps, steps, curbs, etc.

TABLE 6
Soil Corrosivity Screening Results

Test	Test Results	Classification	General Recommendations
Soluble Sulfate (Cal 417)	0.088 to 0.234 percent	S1 to S2 ¹ Moderate to Severe	Type V cement with a maximum water/cement ratio not to exceed 0.45 and a minimum unconfined compressive strength, f'_c not less than 4,500 psi. (3,000 psi for post-tensioned slabs) Exceptions may apply. Petra recommends consulting a Professional Corrosion Engineer
pH (Cal 643)	7.68 to 8.04	Slightly to Moderately Alkaline	Petra recommends consulting a Professional Corrosion Engineer
Soluble Chloride (Cal 422)	2,771 to 5,972 ppm	C2 Severe	Water/cement ratio not to exceed 0.40, f'_c not less than 5,000 psi. Soluble Chloride levels in excess of 5,000 ppm are considered excessively detrimental to metals encased in concrete. Petra recommends consulting a Professional Corrosion Engineer
Resistivity (Cal 643)	65 to 118 ohm-cm	Extremely Corrosive ³	Protective wrapping/coating of buried pipes; corrosion resistant materials. Petra recommends consulting a Professional Corrosion Engineer

Notes:

1. ACI 318-14, Section 19.3
2. ACI 318-14, Section 19.3
3. Pierre R. Roberge, "Handbook of Corrosion Engineering"

Post-Grading Considerations

Utility Trenches

All utility trench backfill should be compacted to a minimum relative compaction of 90 percent. Due to the nature of the upper onsite earth materials, flooding and jetting techniques should be avoided. Therefore, trench backfill materials should be placed in lifts no greater than approximately 12 inches in thickness, watered or air-dried as necessary to achieve near optimum moisture conditions, and then mechanically compacted in place to a minimum relative compaction of 90 percent. A representative of the project geotechnical consultant should probe and test the backfills to verify adequate compaction.

As an alternative for shallow trenches where pipe or utility lines may be damaged by mechanical compaction equipment, such as under building floor slabs, imported clean sand having a sand equivalent (SE) value of 30 or greater may be utilized. The sand backfill materials should be watered to achieve near optimum moisture conditions and then tamped into place. No specific relative compaction will be required; however, observation, probing, and if deemed necessary, testing should be performed by a representative of the project geotechnical consultant to verify an adequate degree of compaction.

If clean, imported sand is to be used for backfill of exterior utility trenches, it is recommended that the upper 12 inches of trench backfill materials consist of properly compacted onsite soil materials. This is to mitigate infiltration of irrigation and rainwater into granular trench backfill materials.

Where an exterior and/or interior utility trench is proposed in a direction parallel to a building footing, the bottom of the trench should not extend below a 1:1 (horizontal to vertical) plane projected downward from the bottom edge of the adjacent footing. Where this condition occurs, the adjacent footing should be deepened or the utility constructed and the trench backfilled and compacted prior to footing construction. Where utility trenches cross under a building footing, these trenches should be backfilled with on-site soils at the point where the trench crosses under the footing to reduce the potential for water to migrate under the floor slabs.

Site Drainage

Positive surface drainage systems consisting of a combination of sloped concrete flatwork/asphalt pavement, sheet flow gradients, swales and surface area drains (where needed) should be provided around buildings and within any planter areas to collect and direct all surface waters to an appropriate drainage facility as determined by the project civil engineer. The ground surfaces of planter and landscape areas that are located within 10 feet of building foundations should be sloped at a minimum gradient of 5 percent away from the foundations and towards the nearest area drains. The ground surface of planter and landscape areas that are located more than 10 feet away from building foundations may be sloped at a minimum gradient of 2 percent away from the foundations and towards the nearest area drains.

Concrete flatwork surfaces that are located within 10 feet of building foundations should be inclined at a minimum gradient of one percent away from the building foundations and towards the nearest area drains. Concrete flatwork surfaces that are located more than 10 feet away from building foundations may be sloped at a minimum gradient of 1 percent towards the nearest area drains. Surface waters should not be allowed to collect or pond against building foundations and within the level areas of the site. All drainage devices should be properly maintained throughout the lifetime of the development. Future changes to site improvements, or planting and watering practices, should not be allowed to cause over-saturation of site soils adjacent to the structures.

Exterior Concrete Flatwork

General

Near-surface compacted fill soils within the site are expected to exhibit an expansion index of 0 to 20, i.e. non-expansive. We recommend that all exterior concrete flatwork such as sidewalks, patio slabs, large decorative slabs, concrete subslabs that will be covered with decorative pavers, private and/or public vehicular driveways and/or access roads within and adjacent to the site be designed by the project architect and/or structural engineer with consideration given to mitigating the potential cracking and uplift that can develop in soils exhibiting expansion index values that fall in the very low category. The guidelines that follow should be considered as minimums and are subject to review and revision by the project architect, structural engineer and/or landscape consultant as deemed appropriate.

Thickness and Joint Spacing

To reduce the potential of unsightly cracking, concrete walkways, patio-type slabs, large decorative slabs and concrete subslabs to be covered with decorative pavers should be at least 4 inches thick and provided with construction joints or expansion joints every 6 feet or less. Private driveways that will be designed for the use of passenger cars and RV parking should also be at least 4 inches thick and provided with construction joints or expansion joints every 10 feet or less. Concrete pavement that will be designed based on an unlimited number of applications of an 18-kip single-axle load in public access areas, segments of road that will be paved with concrete (such as bus stops and cross-walks) or access roads and driveways, which serve multiple residential units or garages, that will be subject to heavy truck loadings should have a minimum thickness of 5 inches and be provided with control joints spaced at maximum 10-foot intervals. A modulus of subgrade reaction of 125 pounds per cubic foot may be used for design of the interior roads.

Reinforcement

All concrete flatwork having their largest plan-view panel dimension exceeding 10 feet should be reinforced with a minimum of No. 3 bars spaced 24 inches on centers, both ways. Alternatively, the slab reinforcement may consist of welded wire mesh of the sheet type (not rolled) with 6x6/W1.4xW1.4 designation in accordance with the Wire Reinforcement Institute (WRI). The reinforcement should be properly positioned near the middle of the slabs.

The reinforcement recommendations provided herein are intended as guidelines to achieve adequate performance for anticipated soil conditions. The project architect, civil and/or structural engineer should make appropriate adjustments in reinforcement type, size and spacing to account for concrete internal (e.g., shrinkage and thermal) and external (e.g., applied loads) forces as deemed necessary.

Edge Beams (Optional)

Where the outer edges of concrete flatwork are to be bordered by landscaping, it is recommended that consideration be given to the use of edge beams (thickened edges) to prevent excessive infiltration and accumulation of water under the slabs. Edge beams, if used, should be 6 to 8 inches wide, extend 8 inches below the tops of the finish slab surfaces. Edge beams are not mandatory; however, their inclusion in flatwork construction adjacent to landscaped areas is intended to reduce the potential for vertical and horizontal movement and subsequent cracking of the flatwork related to uplift forces that can develop in expansive soils.

Subgrade Preparation

Compaction

To reduce the potential for distress to concrete flatwork, the subgrade soils below concrete flatwork areas not subject to regular vehicular traffic should be overexcavated to a minimum depth of 12 inches below proposed finished grade (or deeper, as either prescribed elsewhere in this report or determined in the field), moisture conditioned to at least equal to, or slightly greater than, the optimum moisture content, and then compacted to a relative compaction of no less than 90 percent. Where all-weather fire department access roads (including stabilized deconstructed granite road material), concrete public roads, concrete segments of roads and/or concrete access driveways, or any other concrete flatwork subject to regular vehicular traffic are proposed, the overexcavation should extend to 2 feet below proposed finished grade. The exposed overexcavation bottom should be scarified 8 to 12 inches, moisture conditioned, and compacted to a minimum of 90 percent relative compaction. Fill soils should then be placed in 6 to 8 inch lifts, moisture conditioned, and compacted to a minimum of 90 percent relative compaction, except for the upper 6 inches of subgrade soil, which should be compacted to no less than 95 percent relative compaction.

Pre-Moistening

As a further measure to reduce the potential for concrete flatwork cracking, subgrade soils should be thoroughly moistened prior to placing concrete. The moisture content of the soils should be at least 1.2 times the optimum moisture content and penetrate to a minimum depth of 12 inches into the subgrade. Flooding or ponding of the subgrade is not considered feasible to achieve the above moisture conditions since this method would likely require construction of numerous earth berms to contain the water. Therefore, moisture conditioning should be achieved with sprinklers or a light spray applied to the subgrade over a period of few to several days just prior to pouring concrete. Pre-watering of the soils is intended to promote uniform curing of the concrete, reduce the development of shrinkage cracks and reduce the potential for differential expansion pressure on freshly poured flatwork. A representative of the project

geotechnical consultant should observe and verify the density and moisture content of the soils, and the depth of moisture penetration prior to pouring concrete.

Drainage

Drainage from patios and other flatwork areas should be directed to local area drains and/or graded earth swales designed to carry runoff water to the adjacent streets or other approved drainage structures. The concrete flatwork should be sloped at a minimum gradient of one percent, or as prescribed by project civil engineer or local codes, away from building foundations, retaining walls, masonry garden walls and slope areas.

Tree Wells

Tree wells are not recommended in concrete flatwork areas since they introduce excessive water into the subgrade soils and allow root invasion, both of which can cause heaving and/or cracking of the flatwork.

ACCESS ROADS

The proposed site improvements may include construction of new asphalt-paved roads, as well as improvements to the existing nearby access roads. We have developed the following preliminary recommendations for flexible pavement design based on an assumed R-value of 40 and using Traffic Index (TI) values of 5.0 and 6.0. The pavement design presented herein is based on the assumption that the pavement will be placed directly over engineered, compacted fill placed as specified above in the section for *Subgrade Preparation of Exterior Concrete Flatwork*.

R-value and traffic index parameters presented herein have been assumed. We recommend that bulk samples of the actual subgrade materials be retrieved and R-Value tested after rough grading is completed. Additionally, the project civil engineer should be consulted to determine appropriate or required TI values. Once actual as-graded testing is complete and traffic loads are confirmed, additional or modified design recommendations may be presented.

The pavement section thicknesses presented in Table 7 are considered as minimums for the subject site under the assumed conditions and may be superseded by the project requirements or jurisdictional agency specifications if more stringent.

TABLE 7
Suggested Minimum Flexible Pavement Thickness

Traffic Index	R-Value	Hot Mix Asphalt (alternative) (inches)	Aggregate Base (inches)
5.0 (Light Traffic)	40	3	4
6.0 (Truck Traffic)	40	3	6.5

All aggregate base material should be compacted to a minimum relative compaction of 95 percent (ASTM D 1557) prior to placing asphalt pavement. Base material should conform to the requirements for Untreated Base Materials, Section 200-2 of the latest edition of Standard Specifications for Public Works Construction (Greenbook).

Subgrade drainage is an important factor that enhances pavement performance. Subgrade surfaces below the flexible pavement structural section should be sloped to direct run-off to suitable collection points and to prevent ponding. The roadways should be raised above the surrounding ground surface to facilitate drainage from the roadway.

GRADING AND STRUCTURAL PLAN REVIEWS

It must be emphasized that the recommendations provided throughout this report are based solely on assumed use and design of the project as illustrated in the conceptual design information from the Client. No finalized grading plans, structural plans or details were available for review as of the date of this report. As such, the conclusions and recommendations provided herein should be considered as tentative. Once such plans and details become available, our firm should be retained to review these documents to determine the applicability of our recommendations to the actual construction proposed. Additional recommendations and/or modification of the recommendations provided herein will be provided if necessary depending on the results of the grading plan and/or structural plan review. Additional field exploration may be required once the layout, configuration, and building loads are provided. If we are not provided the opportunity to review these documents with respect to the geotechnical aspects of new construction and grading, it should not be assumed that the recommendations provided herein are wholly or in part applicable to the proposed construction.

REPORT LIMITATIONS

This report is based on the proposed project and geotechnical data as described herein. The materials encountered on the project site as reported by ESS are believed representative of the project area, and the conclusions and recommendations contained in this report are presented on that basis. However, soil materials and moisture conditions can vary in characteristics between points of exploration, both laterally and vertically, and those variations could affect the conclusions and recommendations contained herein. As such, observation and testing by a geotechnical consultant during the grading and construction phases of the project are essential to confirming the basis of this report.

This report has been prepared consistent with that level of care being provided by other professionals providing similar services at the same locale and time period. The contents of this report are professional opinions and as such, are not to be considered a guarantee or warranty. This report should be reviewed and updated after a period of one year or if the project concept changes from that described herein. The information contained herein has not been prepared for use by parties or projects other than those named or described herein. This report may not contain sufficient information for other parties or other purposes.

This report is subject to review by the controlling authorities for this project. Should you have any questions, please do not hesitate to call.

Respectfully submitted,

PETRA GEOSCIENCES, INC.,


4/13/22

Siamak Jafroudi, PhD
Senior Principal Engineer
GE 2024



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Senior Associate Geologist
CEG 1952



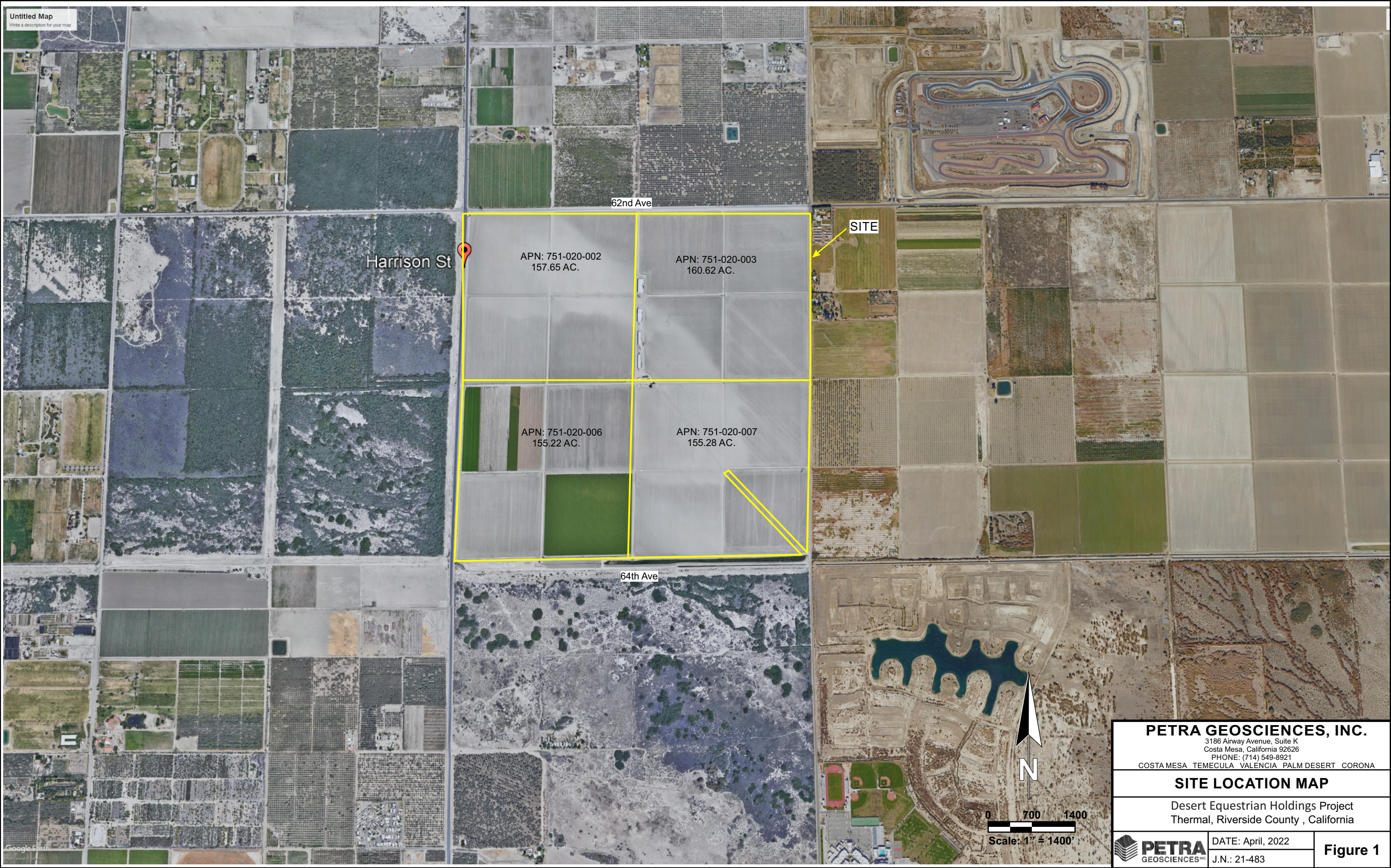
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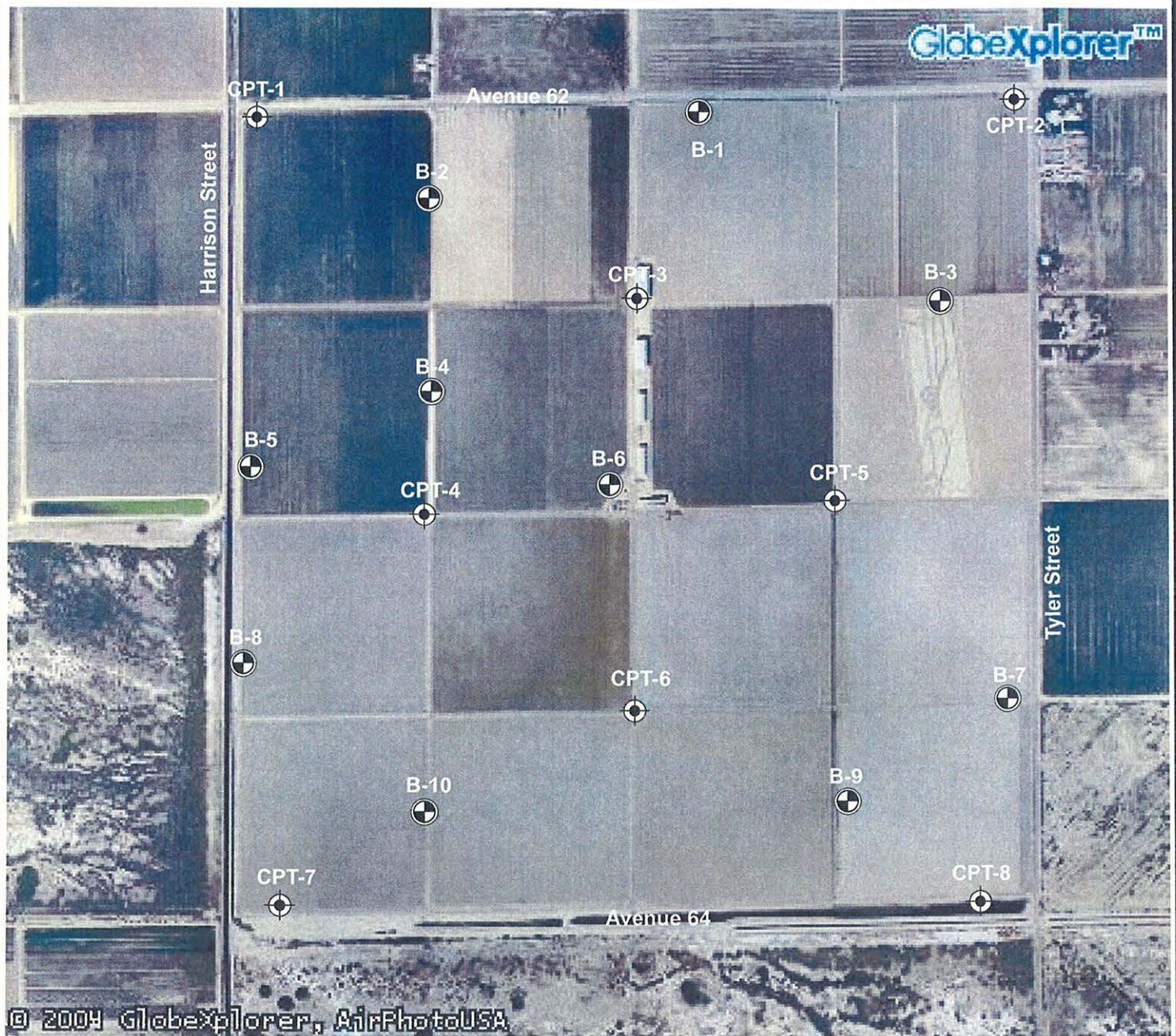
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FIGURE



APPENDIX A

EXPLORATION BORINGS LOGS PERFORMED BY EARTH SYSTEMS SOUTHWEST



LEGEND



Approximate Boring Test Locations



Approximate CPT Test Locations

Not to Scale



Figure 2 Boring Location Map

The La Quinta 628
SEC Avenue 62 & Harrison Street
Thermal, California



**Earth Systems
Southwest**

09/16/04

File No.: 09555-02

DESCRIPTIVE SOIL CLASSIFICATION

Soil classification is based on ASTM Designations D 2487 and D 2488 (Unified Soil Classification System). Information on each boring log is a compilation of subsurface conditions obtained from the field as well as from laboratory testing of selected samples. The indicated boundaries between strata on the boring logs are approximate only and may be transitional.

SOIL GRAIN SIZE

U.S. STANDARD SIEVE

12"	3"	3/4"	4	10	40	200		
BOULDERS	COBBLES	GRAVEL		SAND			SILT	CLAY
		COARSE	FINE	COARSE	MEDIUM	FINE		
305	76.2	19.1	4.76	2.00	0.42	0.074		0.002
SOIL GRAIN SIZE IN MILLIMETERS								

RELATIVE DENSITY OF GRANULAR SOILS (GRAVELS, SANDS, AND NON-PLASTIC SILTS)

Very Loose	*N=0-4	RD=0-30	Easily push a 1/2-inch reinforcing rod by hand
Loose	N=5-10	RD=30-50	Push a 1/2-inch reinforcing rod by hand
Medium Dense	N=11-30	RD=50-70	Easily drive a 1/2-inch reinforcing rod with hammer
Dense	N=31-50	RD=70-90	Drive a 1/2-inch reinforcing rod 1 foot with difficulty by a hammer
Very Dense	N>50	RD=90-100	Drive a 1/2-inch reinforcing rod a few inches with hammer

*N=Blows per foot in the Standard Penetration Test at 60% theoretical energy. For the 3-inch diameter Modified California sampler, 140-pound weight, multiply the blow count by 0.63 (about 2/3) to estimate N. If automatic hammer is used, multiply a factor of 1.3 to 1.5 to estimate N. RD=Relative Density (%). C=Undrained shear strength (cohesion).

CONSISTENCY OF COHESIVE SOILS (CLAY OR CLAYEY SOILS)

Very Soft	*N=0-1	*C=0-250 psf	Squeezes between fingers
Soft	N=2-4	C=250-500 psf	Easily molded by finger pressure
Medium Stiff	N=5-8	C=500-1000 psf	Molded by strong finger pressure
Stiff	N=9-15	C=1000-2000 psf	Dented by strong finger pressure
Very Stiff	N=16-30	C=2000-4000 psf	Dented slightly by finger pressure
Hard	N>30	C>4000	Dented slightly by a pencil point or thumbnail

MOISTURE DENSITY

Moisture Condition:	An observational term; dry, damp, moist, wet, saturated.
Moisture Content:	The weight of water in a sample divided by the weight of dry soil in the soil sample expressed as a percentage.
Dry Density:	The pounds of dry soil in a cubic foot.

MOISTURE CONDITION

Dry.....	Absence of moisture, dusty, dry to the touch
Damp.....	Slight indication of moisture
Moist.....	Color change with short period of air exposure (granular soil) Below optimum moisture content (cohesive soil)
Wet.....	High degree of saturation by visual and touch (granular soil) Above optimum moisture content (cohesive soil)
Saturated.....	Free surface water

RELATIVE PROPORTIONS

Trace.....	minor amount (<5%)
with/some.....	significant amount
modifier/and....	sufficient amount to influence material behavior (Typically >30%)

PLASTICITY

DESCRIPTION	FIELD TEST
Nonplastic	A 1/8 in. (3-mm) thread cannot be rolled at any moisture content.
Low	The thread can barely be rolled.
Medium	The thread is easy to roll and not much time is required to reach the plastic limit.
High	The thread can be rerolled several times after reaching the plastic limit.

LOG KEY SYMBOLS

	Bulk, Bag or Grab Sample
	Standard Penetration Split Spoon Sampler (2" outside diameter)
	Modified California Sampler (3" outside diameter)
	No Recovery

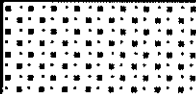
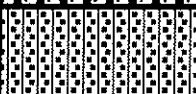
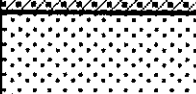
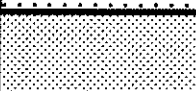
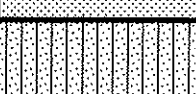
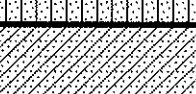
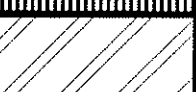
GROUNDWATER LEVEL

	Water Level (measured or after drilling)
	Water Level (during drilling)

Terms and Symbols used on Boring Logs



**Earth Systems
Southwest**

MAJOR DIVISIONS			GRAPHIC SYMBOL	LETTER SYMBOL	TYPICAL DESCRIPTIONS	
COARSE GRAINED SOILS More than 50% of material is <u>larger</u> than No. 200 sieve size	GRAVEL AND GRAVELLY SOILS More than 50% of coarse fraction <u>retained</u> on No. 4 sieve	CLEAN GRAVELS		GW	Well-graded gravels, gravel-sand mixtures, little or no fines	
				GP	Poorly-graded gravels, gravel-sand mixtures. Little or no fines	
		GRAVELS WITH FINES		GM	Silty gravels, gravel-sand-silt mixtures	
				GC	Clayey gravels, gravel-sand-clay mixtures	
	SAND AND SANDY SOILS	CLEAN SAND (Little or no fines)		SW	Well-graded sands, gravelly sands, little or no fines	
				SP	Poorly-graded sands, gravelly sands, little or no fines	
		SAND WITH FINES (appreciable amount of fines)		SM	Silty sands, sand-silt mixtures	
				SC	Clayey sands, sand-clay mixtures	
FINE-GRAINED SOILS More than 50% of material is <u>smaller</u> than No. 200 sieve size	SILTS AND CLAYS	LIQUID LIMIT <u>LESS</u> THAN 50		ML	Inorganic silts and very fine sands, rock flour, silty low clayey fine sands or clayey silts with slight plasticity	
				CL	Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays, lean clays	
				OL	Organic silts and organic silty clays of low plasticity	
		LIQUID LIMIT <u>GREATER</u> THAN 50		MH	Inorganic silty, micaceous, or diatomaceous fine sand or silty soils	
				CH	Inorganic clays of high plasticity, fat clays	
				OH	Organic clays of medium to high plasticity, organic silts	
		HIGHLY ORGANIC SOILS			PT	Peat, humus, swamp soils with high organic contents
		VARIOUS SOILS AND MAN MADE MATERIALS				Fill Materials
MAN MADE MATERIALS				Asphalt and concrete		
			Soil Classification System			
				Earth Systems Southwest		



Boring No: B-1

Project Name: The La Quinta 628, SEC Ave 62 and Harrison St., Thermal, CA

File Number: 09555-02

Boring Location: See Figure 2

Drilling Date: August 10, 2004

Drilling Method: 8" Hollow Stem Auger

Drill Type: CME 55 w/rope & cathead

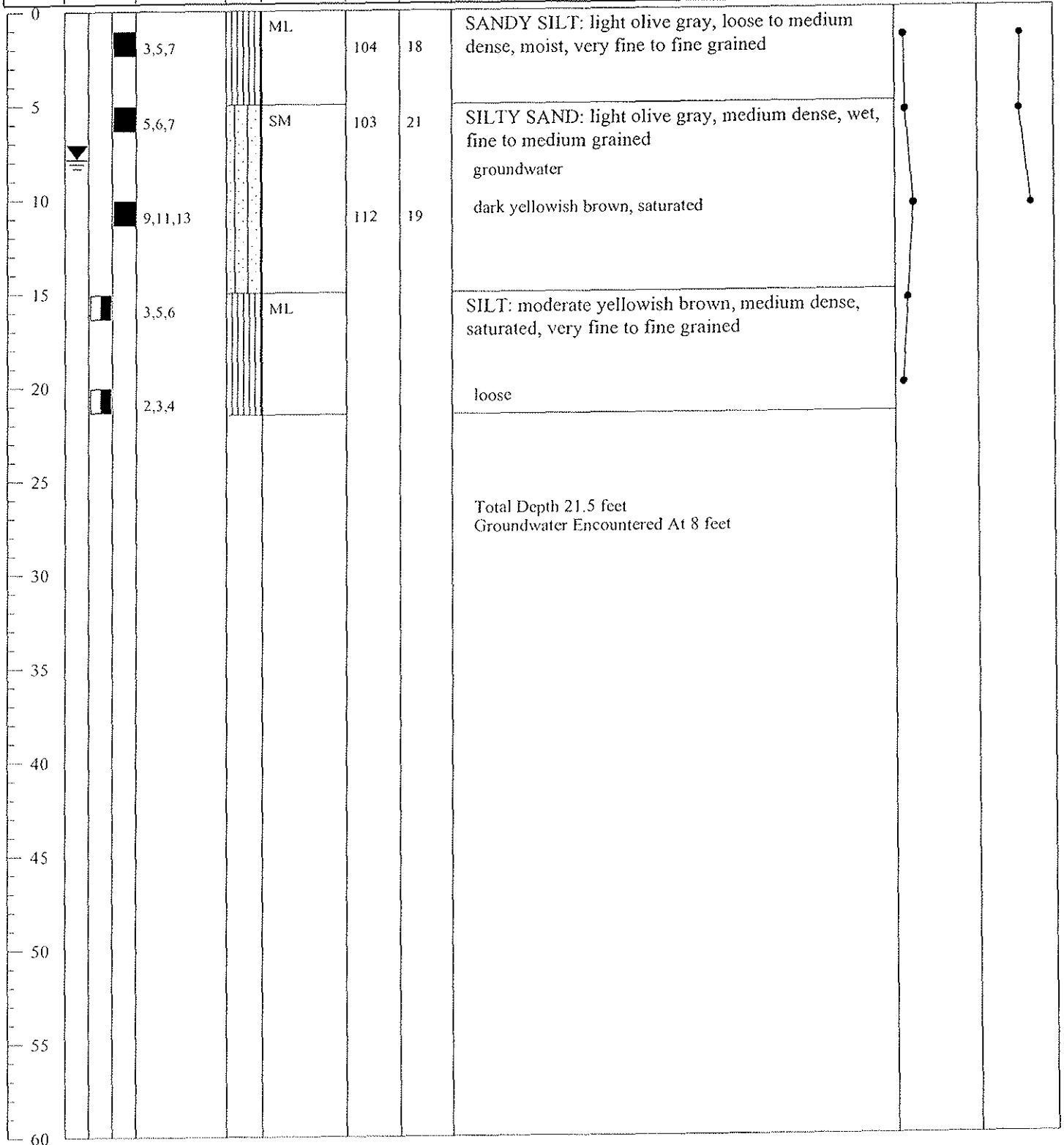
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Description of Units

Note: The stratification lines shown represent the approximate boundary between soil and/or rock types and the transition may be gradational.

Graphic Trend
Blow Count Dry Density





Boring No: B-2

Project Name: The La Quinta 628, SEC Ave 62 and Harrison St., Thermal, CA

File Number: 09555-02

Boring Location: See Figure 2

Drilling Date: August 11, 2004

Drilling Method: 8" Hollow Stem Auger

Drill Type: CME 55 w/rope & cathead

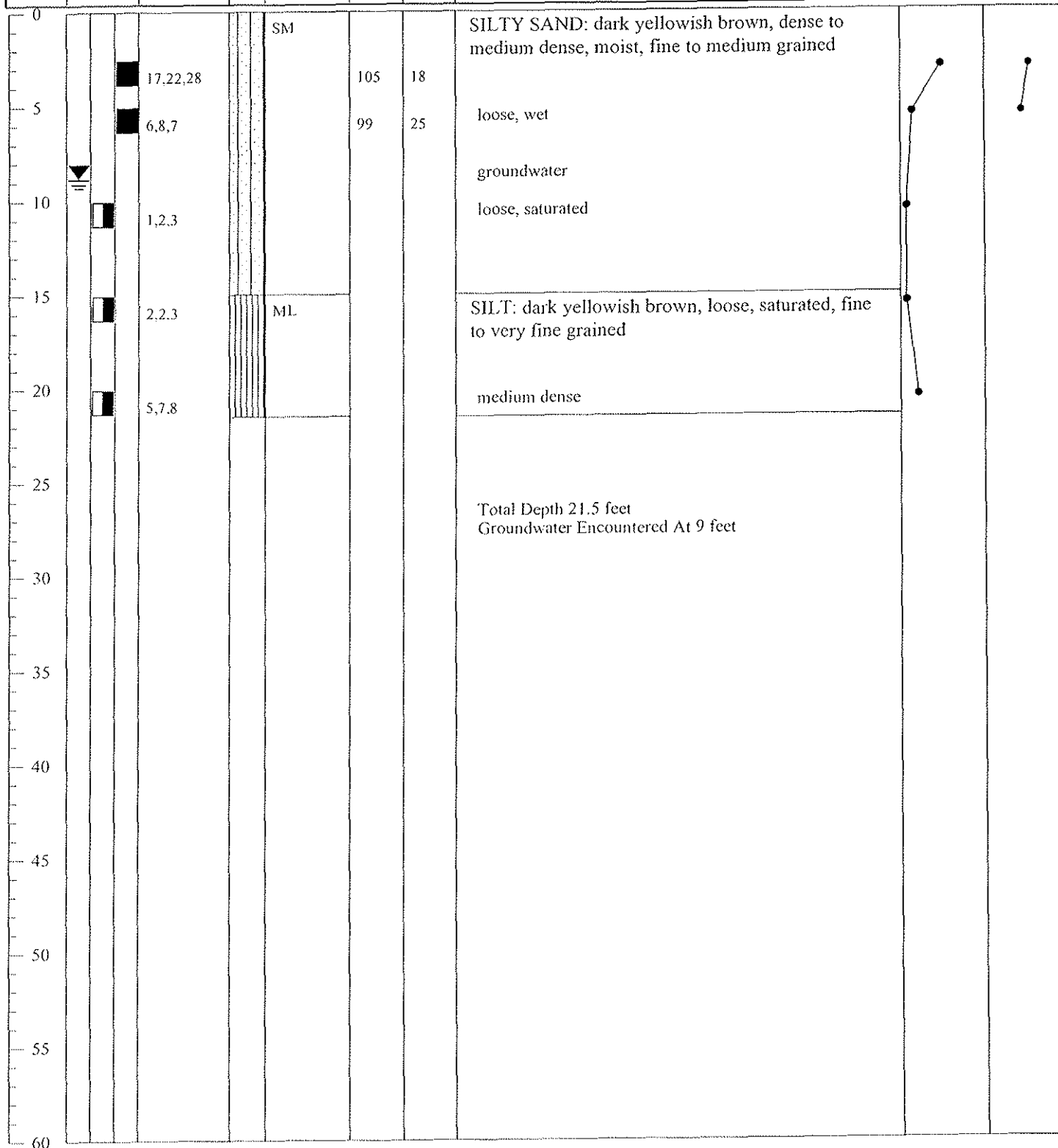
Logged By: Dirk Wiggins

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Description of Units

Note: The stratification lines shown represent the approximate boundary between soil and/or rock types and the transition may be gradational.

Graphic Trend
Blow Count Dry Density





Boring No: B-3

Project Name: The La Quinta 628, SEC Ave 62 and Harrison St., Thermal, CA

File Number: 09555-02

Boring Location: See Figure 2

Drilling Date: August 12, 2004

Drilling Method: 8" Hollow Stem Auger

Drill Type: CME 55 w/rope & cathead

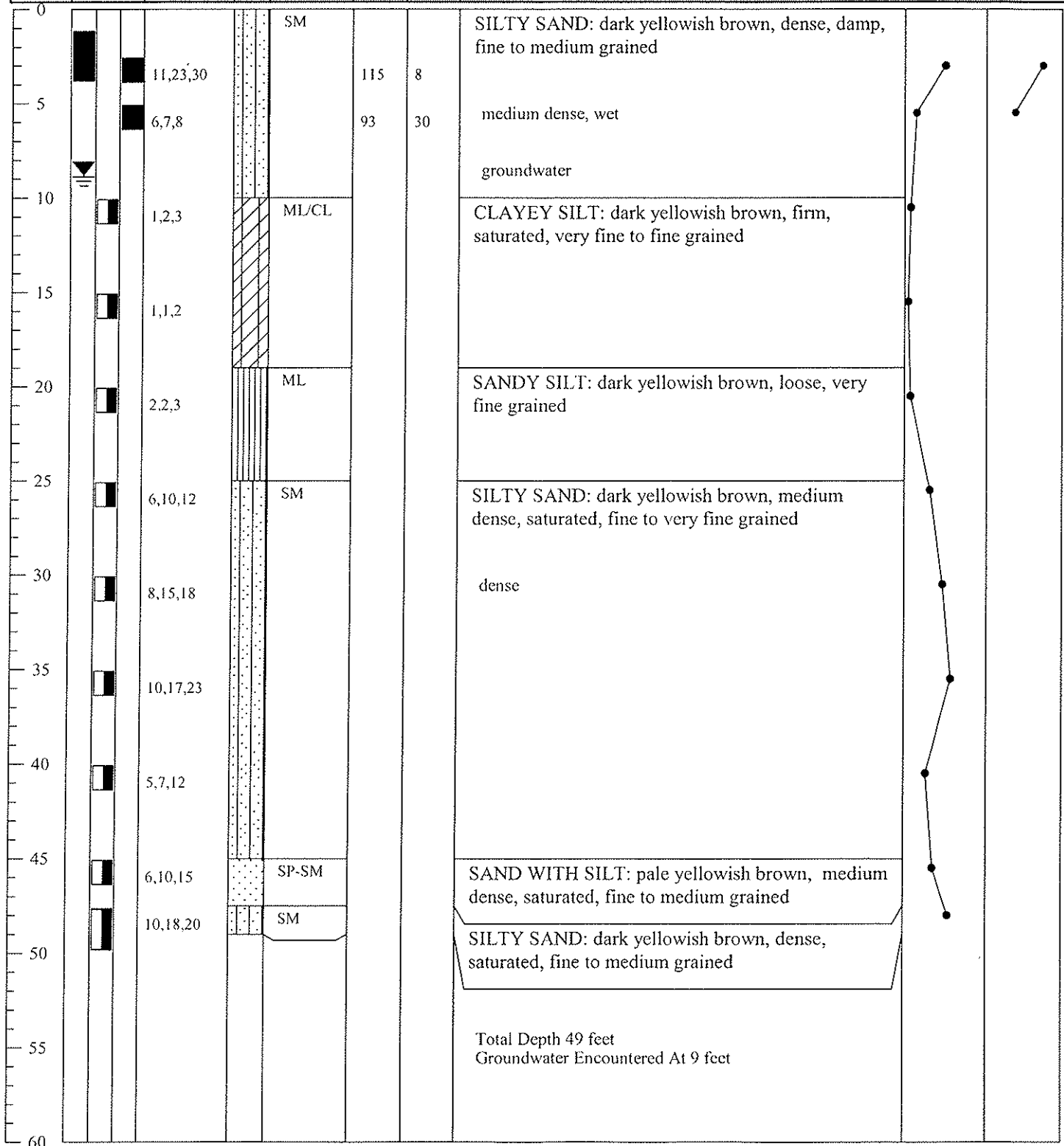
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Description of Units

Note: The stratification lines shown represent the approximate boundary between soil and/or rock types and the transition may be gradational.

Graphic Trend
Blow Count Dry Density





Boring No: B-4

Project Name: The La Quinta 628, SEC Ave 62 and Harrison St., Thermal, CA

File Number: 09555-02

Boring Location: See Figure 2

Drilling Date: August 11, 2004

Drilling Method: 8" Hollow Stem Auger

Drill Type: CME 55 w/rope & cathead

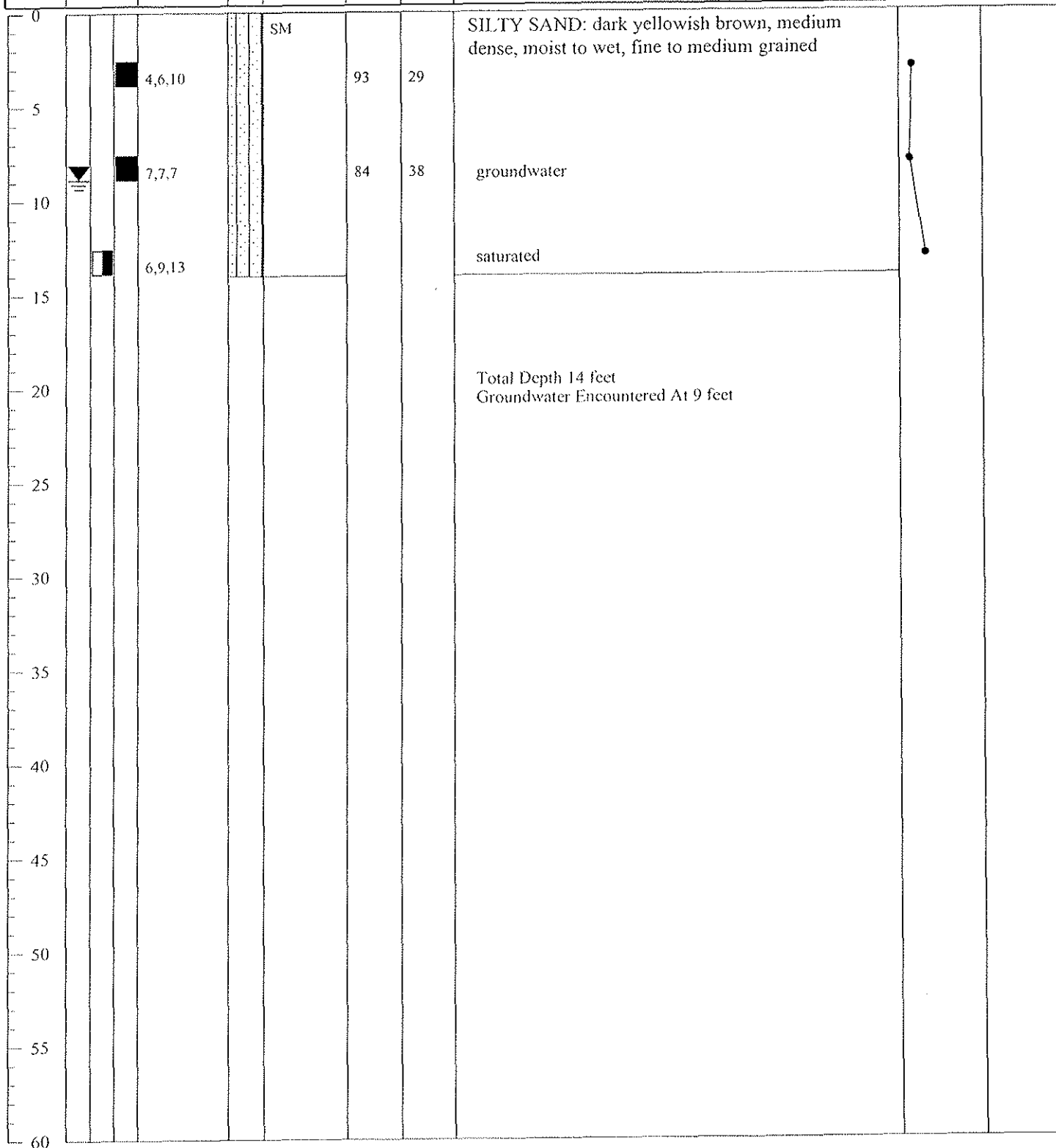
Logged By: Dirk Wiggins

Page 1 of 1

Description of Units

Note: The stratification lines shown represent the approximate boundary between soil and/or rock types and the transition may be gradational.

Graphic Trend
Blow Count Dry Density



**Boring No: B-5**

Project Name: The La Quinta 628, SEC Ave 62 and Harrison St., Thermal, CA

File Number: 09555-02

Boring Location: See Figure 2

Drilling Date: August 10, 2004

Drilling Method: 8" Hollow Stem Auger

Drill Type: CME 55 w/rope & cathead

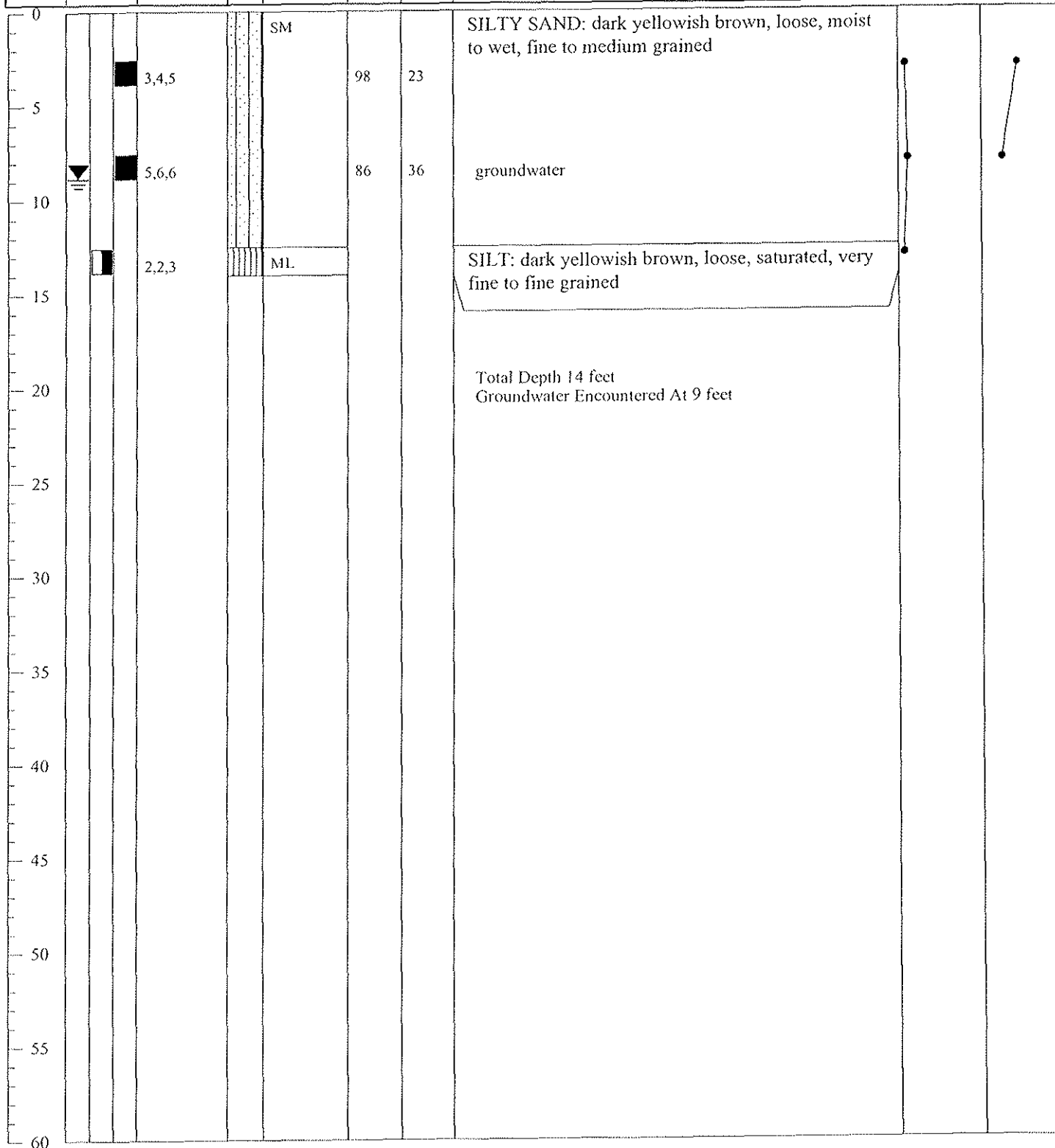
Logged By: Dirk Wiggins

Page 1 of 1

Description of Units

Note: The stratification lines shown represent the approximate boundary between soil and/or rock types and the transition may be gradational.

Graphic Trend
Blow Count Dry Density





Boring No: B-6

Project Name: The La Quinta 628, SEC Ave 62 and Harrison St., Thermal, CA

File Number: 09555-02

Boring Location: See Figure 2

Drilling Date: August 10, 2004

Drilling Method: 8" Hollow Stem Auger

Drill Type: CME 55 w/rope & cathead

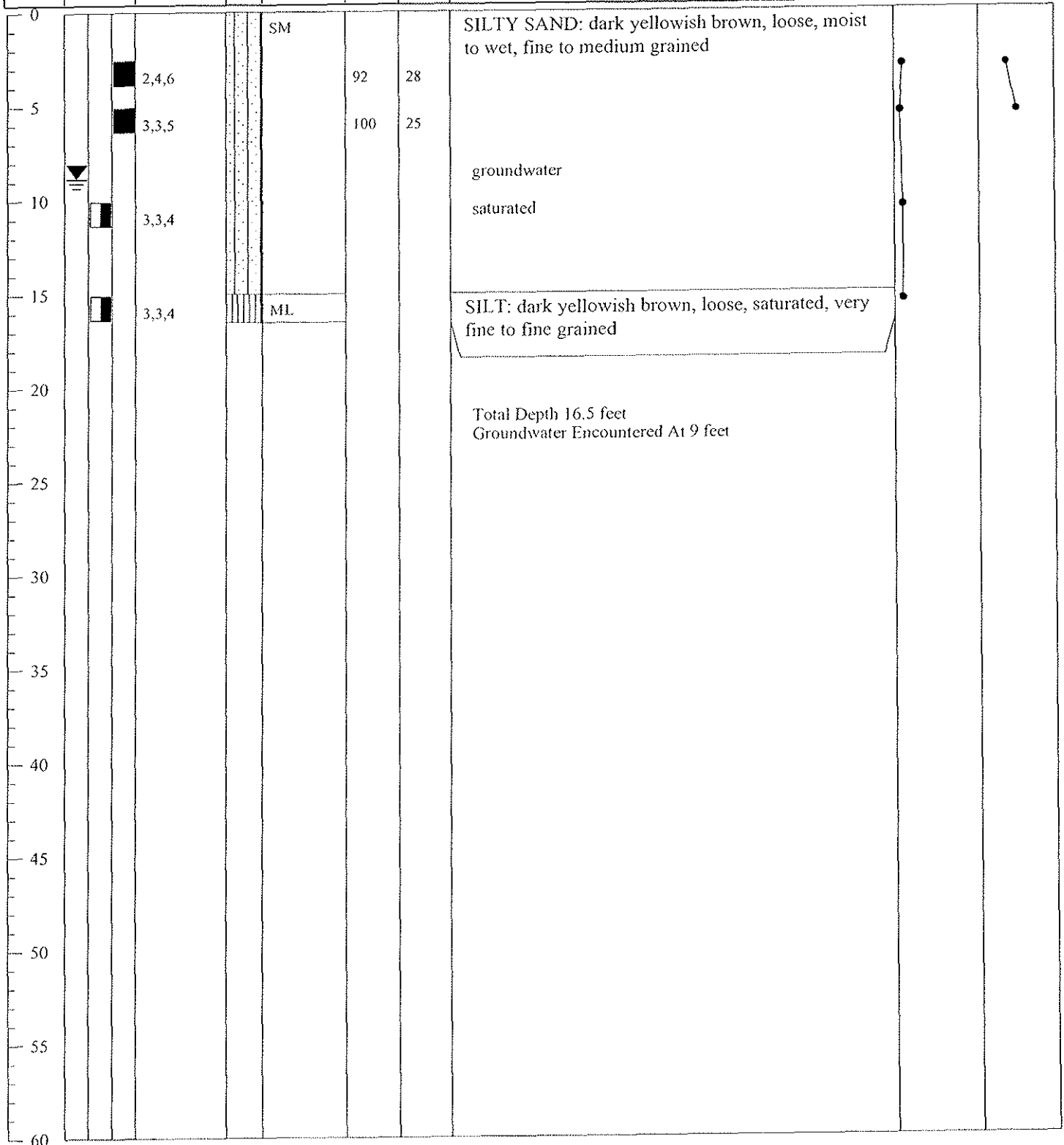
Logged By: Dirk Wiggins

Page 1 of 1

Description of Units

Note: The stratification lines shown represent the approximate boundary between soil and/or rock types and the transition may be gradational.

Graphic Trend
Blow Count Dry Density





Boring No: B-7

Project Name: The La Quinta 628, SEC Ave 62 and Harrison St., Thermal, CA

File Number: 09555-02

Boring Location: See Figure 2

Drilling Date: August 12, 2004

Drilling Method: 8" Hollow Stem Auger

Drill Type: CME 55 w/rope & cathead

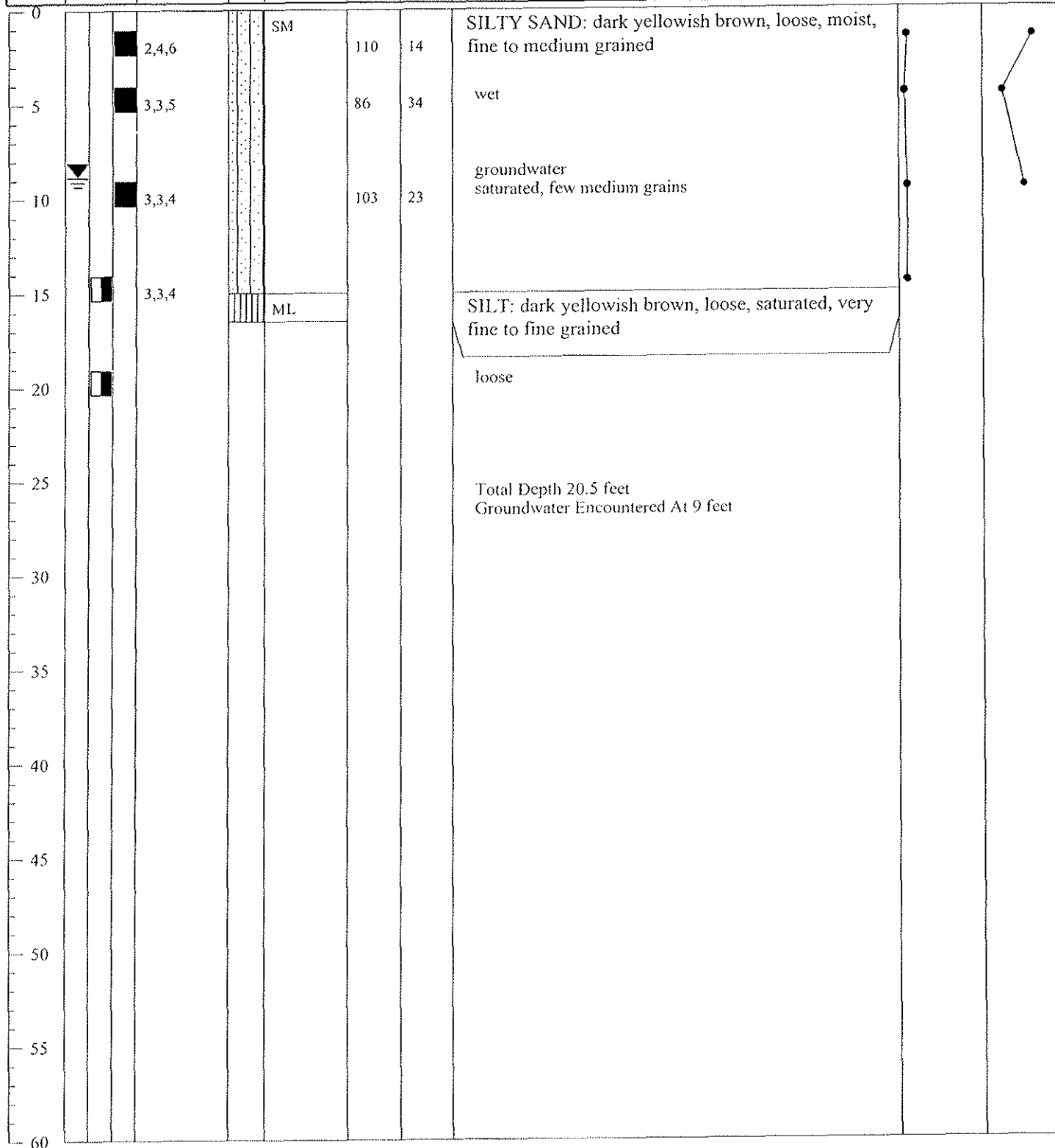
Logged By: Dirk Wiggins

Page 1 of 1

Description of Units

Note: The stratification lines shown represent the approximate boundary between soil and/or rock types and the transition may be gradational.

Graphic Trend
Blow Count Dry Density





Boring No: B-8

Project Name: The La Quinta 628, SEC Ave 62 and Harrison St., Thermal, CA
File Number: 09555-02
Boring Location: See Figure 2

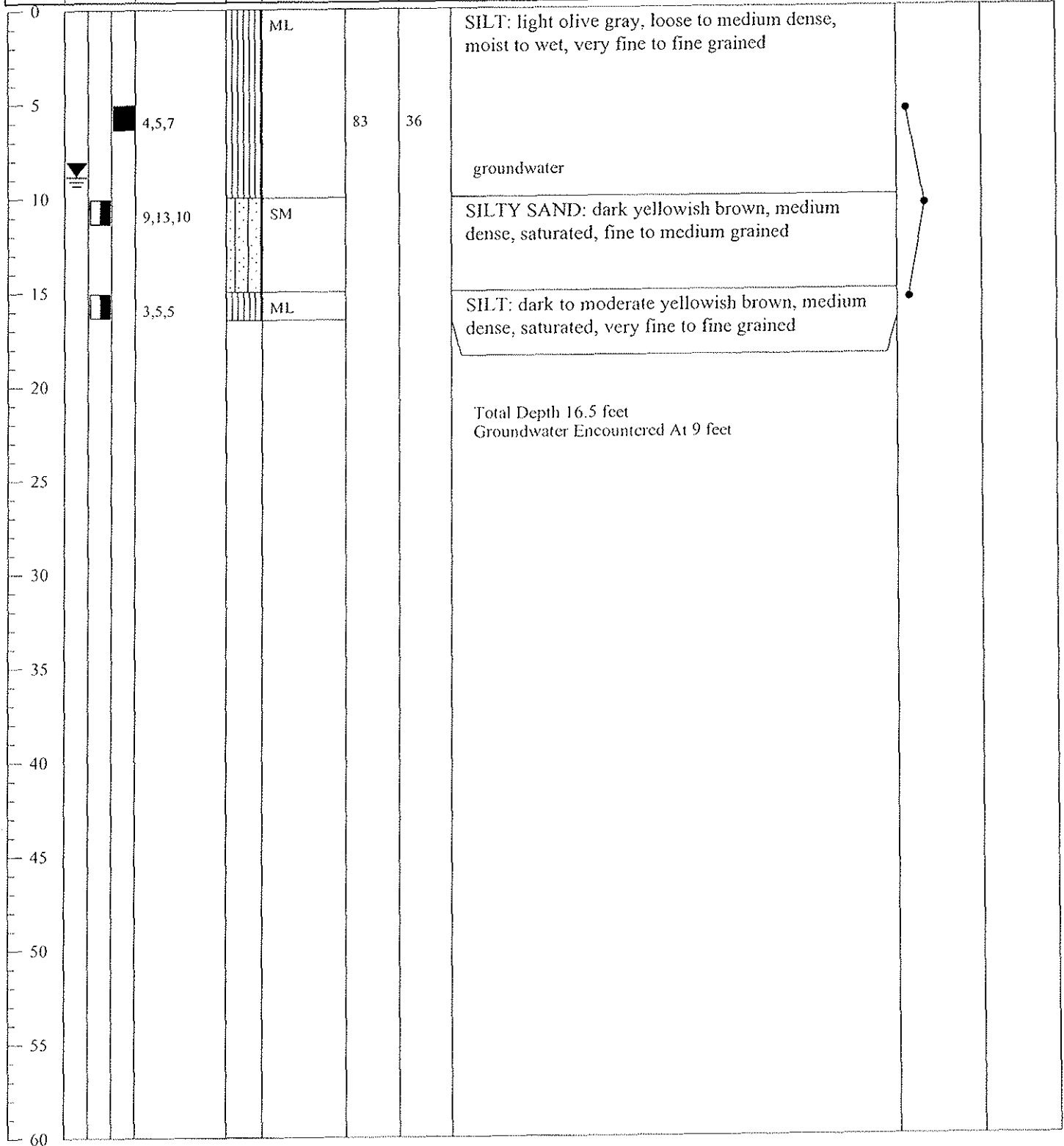
Drilling Date: August 10, 2004
Drilling Method: 8" Hollow Stem Auger
Drill Type: CME 55 w/rope & cathead
Logged By: Dirk Wiggins

Page 1 of 1

Description of Units

Note: The stratification lines shown represent the approximate boundary between soil and/or rock types and the transition may be gradational.

Graphic Trend
Blow Count Dry Density





79-811B Country Club Drive, Bermuda Dunes, CA 92203

Phone (760) 345-1588, Fax (760) 345-7315

Project Name: The La Quinta 628, SEC Ave 62 and Harrison St., Thermal, CA
File Number: 09555-02
Boring Location: See Figure 2

Drilling Method: 8" Hollow Stem Auger

Logged By: Dirk Wiggins

Page 1 of 1

Note: The stratification lines shown represent the approximate boundary between soil and/or rock types and the transition may be gradational.

Graphic Trend
Blow Count Dry Density



Boring No: B-10

Project Name: The La Quinta 628, SEC Ave 62 and Harrison St., Thermal, CA

File Number: 09555-02

Boring Location: See Figure 2

Drilling Date: August 11, 2004

Drilling Method: 8" Hollow Stem Auger

Drill Type: CME 55 w/rope & cathead

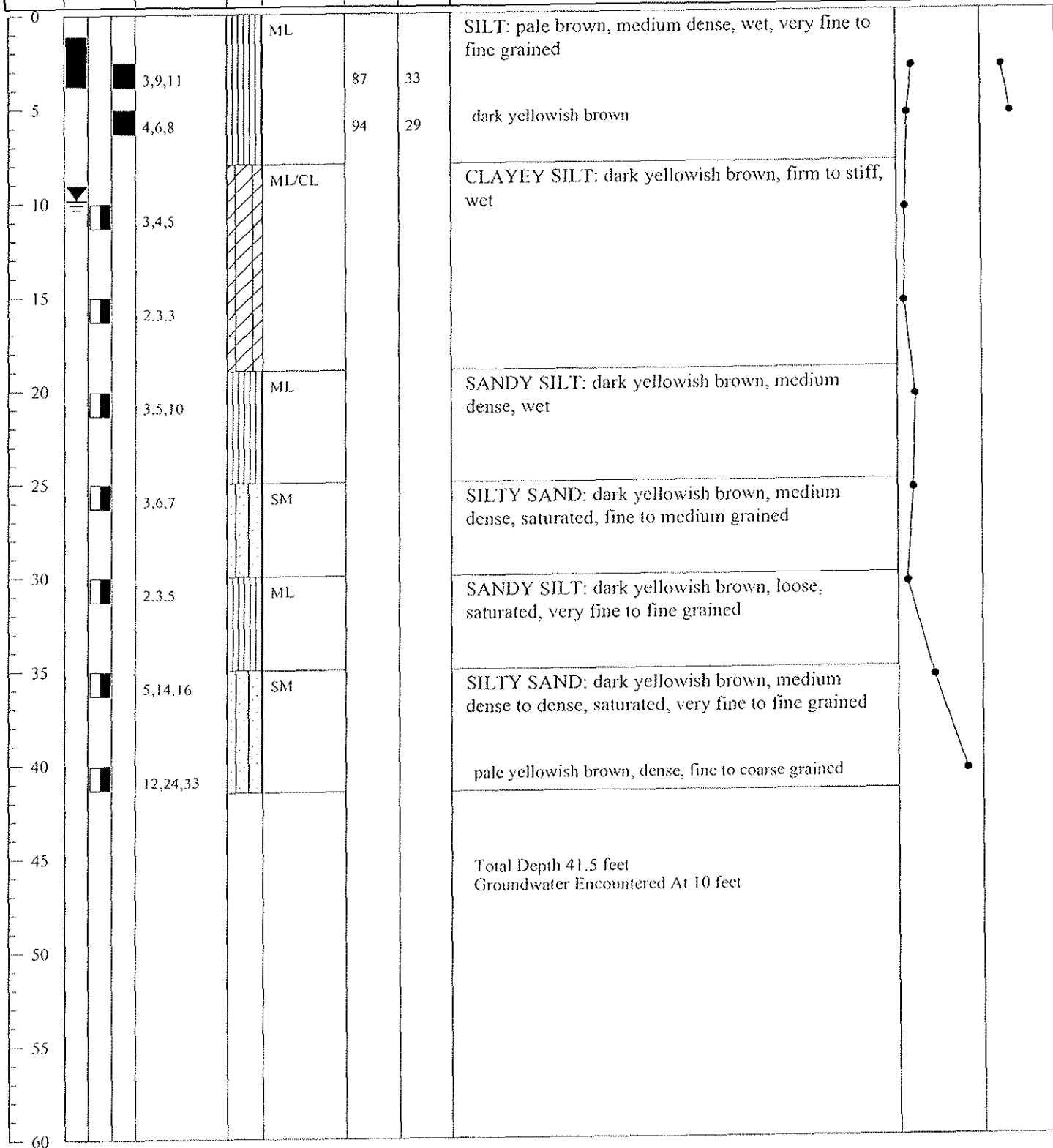
Logged By: Dirk Wiggins

Page 1 of 1

Description of Units

Note: The stratification lines shown represent the approximate boundary between soil and/or rock types and the transition may be gradational.

Graphic Trend
Blow Count Dry Density



APPENDIX B

LABORATORY TEST PROCEDURES

LABORATORY DATA SUMMARY PERFORMED BY EARTH SYSTEMS SOUTHWEST

UNIT DENSITIES AND MOISTURE CONTENT

ASTM D2937 & D2216

Job Name: La Quinta 628

Sample Location	Depth (feet)	Unit Dry Density (pcf)	Moisture Content (%)	USCS Group Symbol
B1	1	104	18	ML
B1	5	103	21	SM
B1	10	112	19	SM
B2	2.5	105	18	SM
B2	5	99	25	SM
B3	2.5	115	8	SM
B3	5	93	30	SM
B4	2.5	93	29	SM
B4	7.5	84	38	SM
B5	2.5	98	23	SM
B5	7.5	86	36	SM
B6	2	92	28	SM
B6	5	100	25	SM
B7	1	110	14	SM
B7	4	86	34	SM
B7	9	103	23	SM
B8	5	83	36	ML
B9	2.5	89	32	SM
B9	5	83	37	ML
B10	2.5	87	33	ML
B10	5	94	29	ML

File No.: 09555-02
Job Name: La Quinta 628

September 16, 2004

AMOUNT PASSING NO. 200 SIEVE

ASTM D 1140

Sample Location	Depth (feet)	Fines Content (%)	USCS Group Symbol
B3	20	65	ML
B10	20	62	ML
B10	30	66	ML

PARTICLE SIZE ANALYSIS

ASTM D-422

Job Name: La Quinta 628

Sample ID: B3 @ 1-5 Feet

Description: Brown, Silty Sand, w/Silt Clumps, (SM-ML)

Sieve Size	Percent Passing
1-1/2"	100
1"	100
3/4"	100
1/2"	100
3/8"	100
#4	100
#8	100
#16	99
#30	98
#50	97
#100	88
#200	75

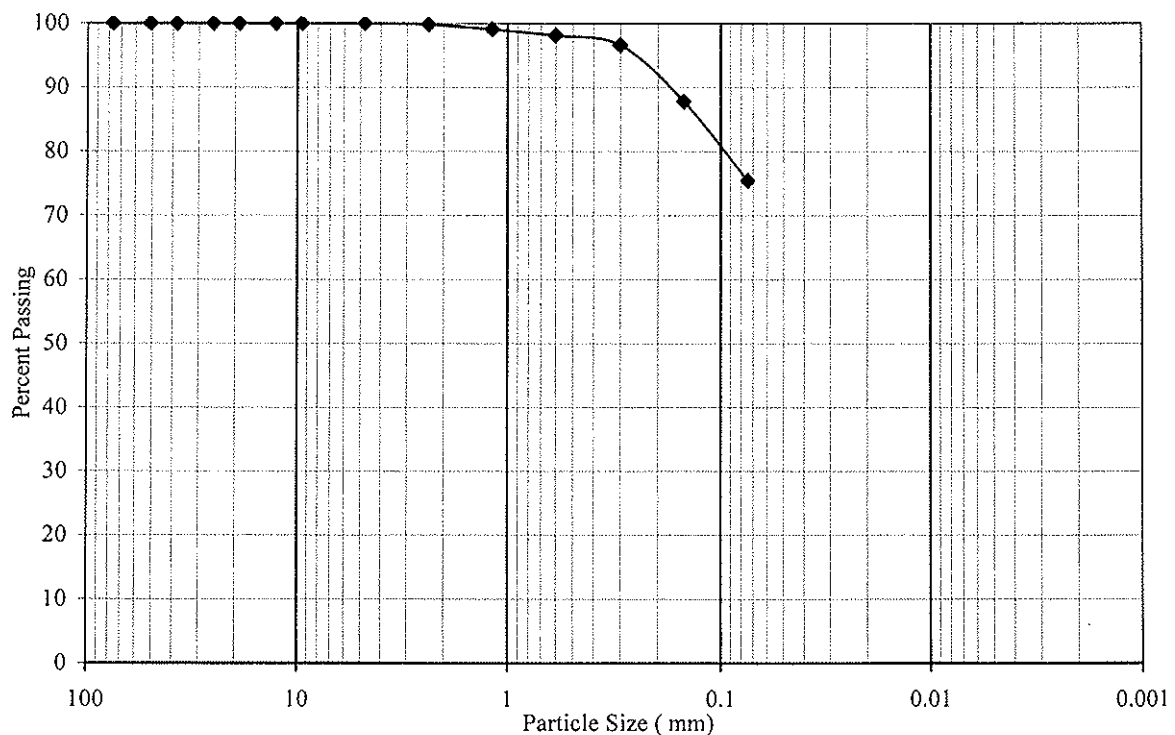
% Gravel: 0

% Sand: 25

% Silt: 54

% Clay (3 micron): 21

(Clay content by short hydrometer method)



PARTICLE SIZE ANALYSIS

ASTM D-422

Job Name: La Quinta 628

Sample ID: B10 @1-4 Feet

Description: Brown, Silty Sand, Clayey Silt, (SM-ML)

Sieve Size	Percent Passing
1-1/2"	100
1"	100
3/4"	100
1/2"	100
3/8"	100
#4	100
#8	100
#16	99
#30	98
#50	96
#100	89
#200	72

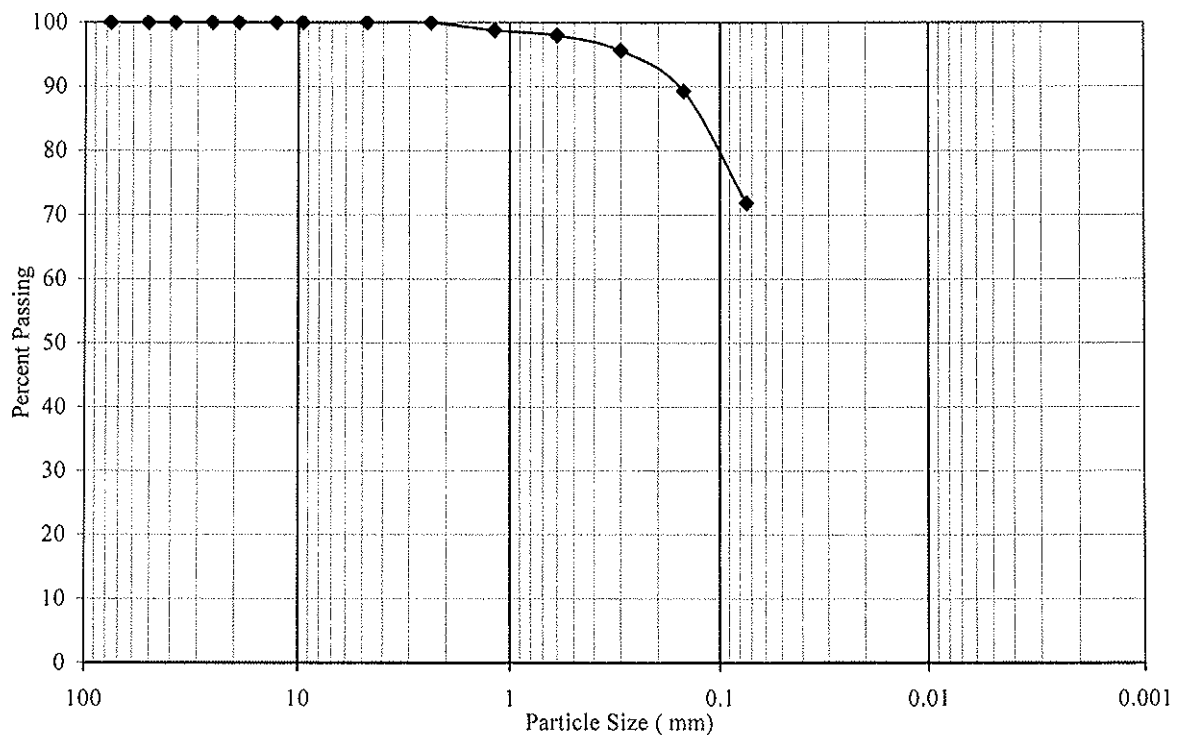
% Gravel: 0

% Sand: 28

% Silt: 50

% Clay (3 micron): 22

(Clay content by short hydrometer method)



PARTICLE SIZE ANALYSIS

ASTM D-422

Job Name: La Quinta 628

Sample ID: B10 @ 25 Feet

Description: Brown, Silty Clayey Sand, (SM-ML)

Sieve Size	% Passing
3"	100
2"	100
1-1/2"	100
1"	100
3/4"	100
1/2"	100
3/8"	100
#4	100
#8	100
#16	100
#30	99
#50	91
#100	50
#200	30

By Hydrometer Method:

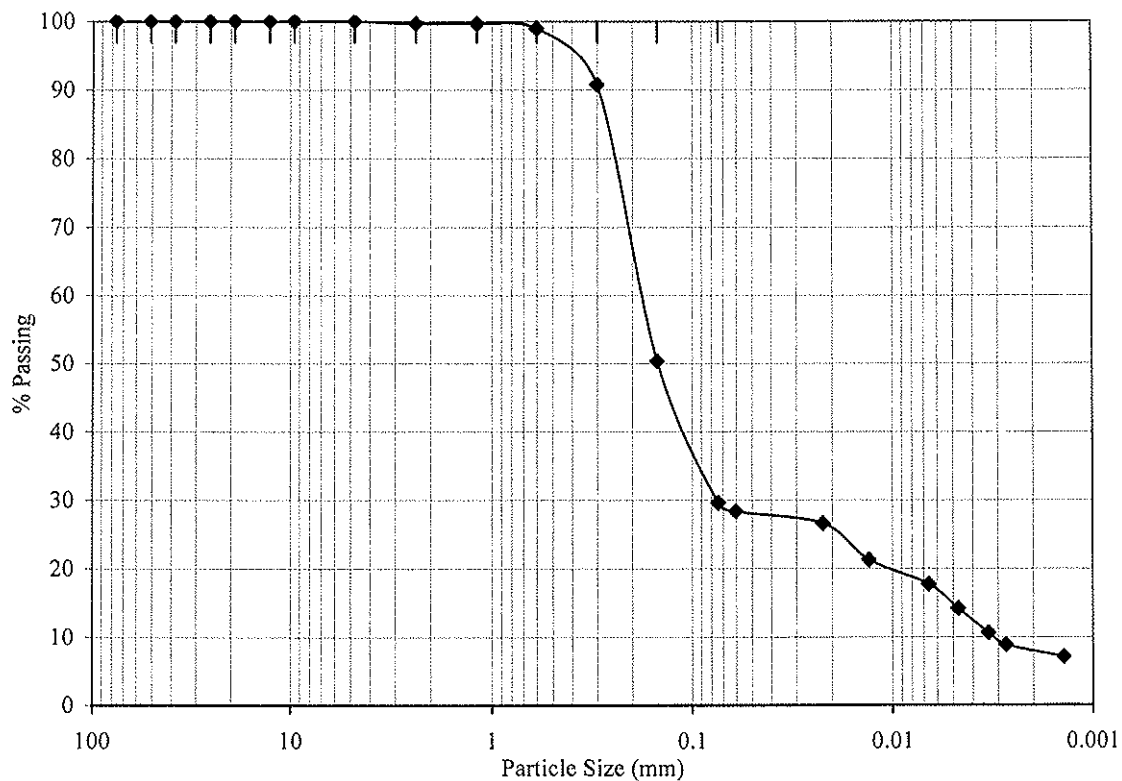
Particle Size	% Passing
60 Micron	28
22 Micron	27
13 Micron	21
7 Micron	18
5 Micron	14
3.3 Micron	11
2.7 Micron	9
1.4 Micron	7

% Gravel: 0

% Sand: 70

% Silt: 21

% Clay (3 micron): 9



MAXIMUM DENSITY / OPTIMUM MOISTURE

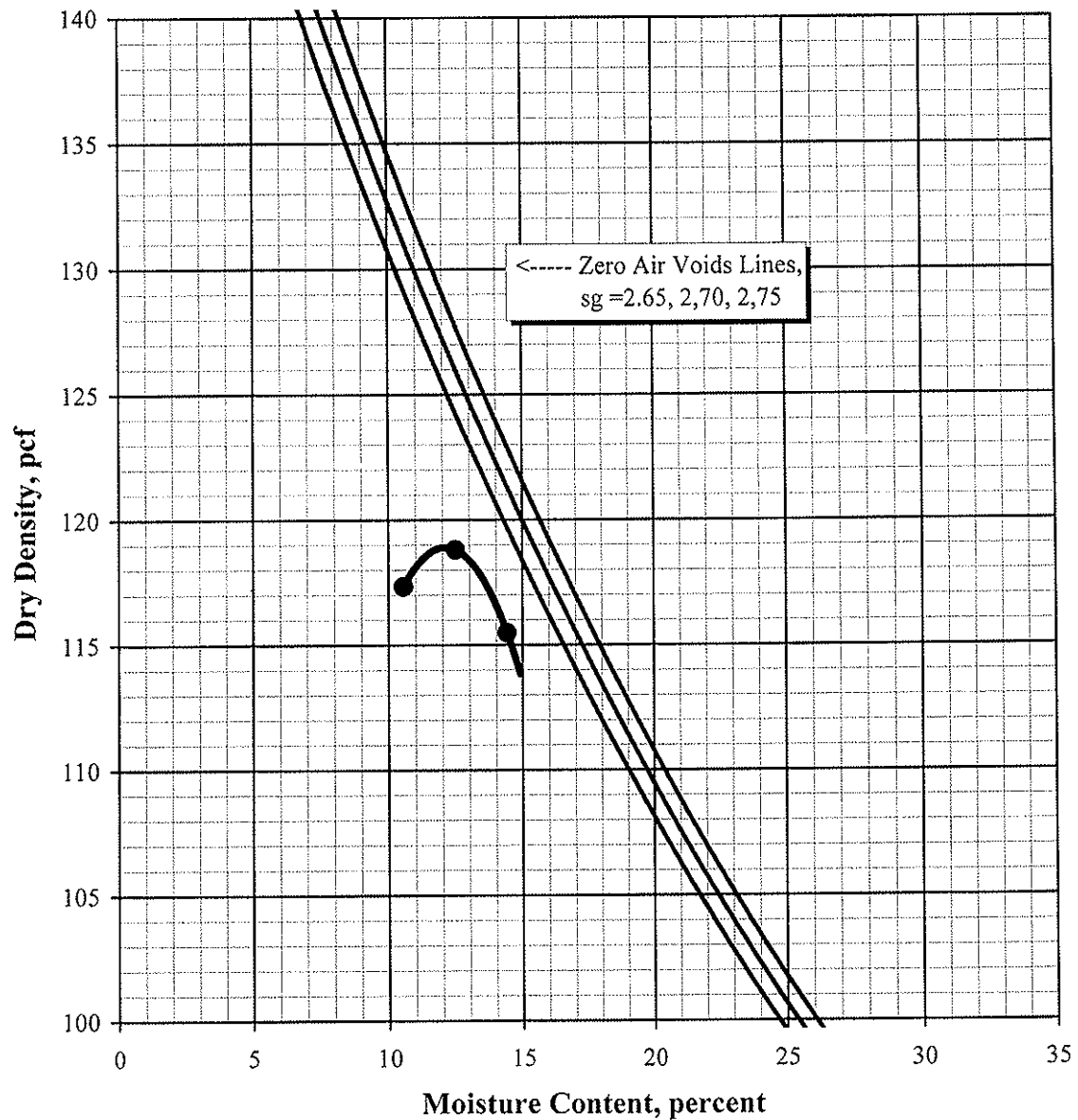
ASTM D 1557-91 (Modified)

Job Name: La Quinta 628
Sample ID: B3 @ 1-4' Feet

Procedure Used: A
Preparation Method: Moist
Rammer Type: Mechanical

Description: Brown, Silty Sand, w/Silt Clumps, (SM)

		Sieve Size	% Retained
Maximum Density:	119 pcf	3/4"	0.0
Optimum Moisture:	12.5%	3/8"	0.1
		#4	0.2



SOIL CHEMICAL ANALYSES

Job Name: La Quinta 628

Job No.: 09555-02

Sample ID: B3 @ 1-4'		B 10 @ 1-4'			
Sample Depth, feet:	1-4'	1-4'	DF	RL	
Sulfate, mg/Kg (ppm):	2,343	877	1	0.50	
Chloride, mg/Kg (ppm):	2,771	5,972	1	0.20	
pH, (pH Units):	7.68	8.04	1	0.41	
Resistivity, (ohm-cm):	118	65	N/A	N/A	
Conductivity, (µmhos-cm):	8,510	15,280	1	2.00	

Note: Tests performed by Subcontract Laboratory:
 Truesdail Laboratories, Inc.
 14201 Franklin Avenue
 Tustin, California 92780 Tel: (714) 730-6239

DF: Dilution Factor
 RL: Reporting Limit

General Guidelines for Soil Corrosivity		
Chemical Agent	Amount in Soil	Degree of Corrosivity
Soluble Sulfates	0 -1000 mg/Kg (ppm) [0-.1%]	Low
	1000 - 2000 mg/Kg (ppm) [0.1-0.2%]	Moderate
	2000 - 20,000 mg/Kg (ppm) [0.2-2.0%]	Severe
	> 20,000 mg/Kg (ppm) [>2.0%]	Very Severe
Resistivity	1-1000 ohm-cm	Very Severe
	1000-2000 ohm-cm	Severe
	2000-10,000 ohm-cm	Moderate
	10,000+ ohm-cm	Low

APPENDIX C

CONE PENETROMETER TEST (CPT) LOGS PERFORMED BY EARTH SYSTEMS SOUTHWEST



CPT No: CPT-1

Project Name: La Quinta 628 Sun Cal

Project No.: 09555-02

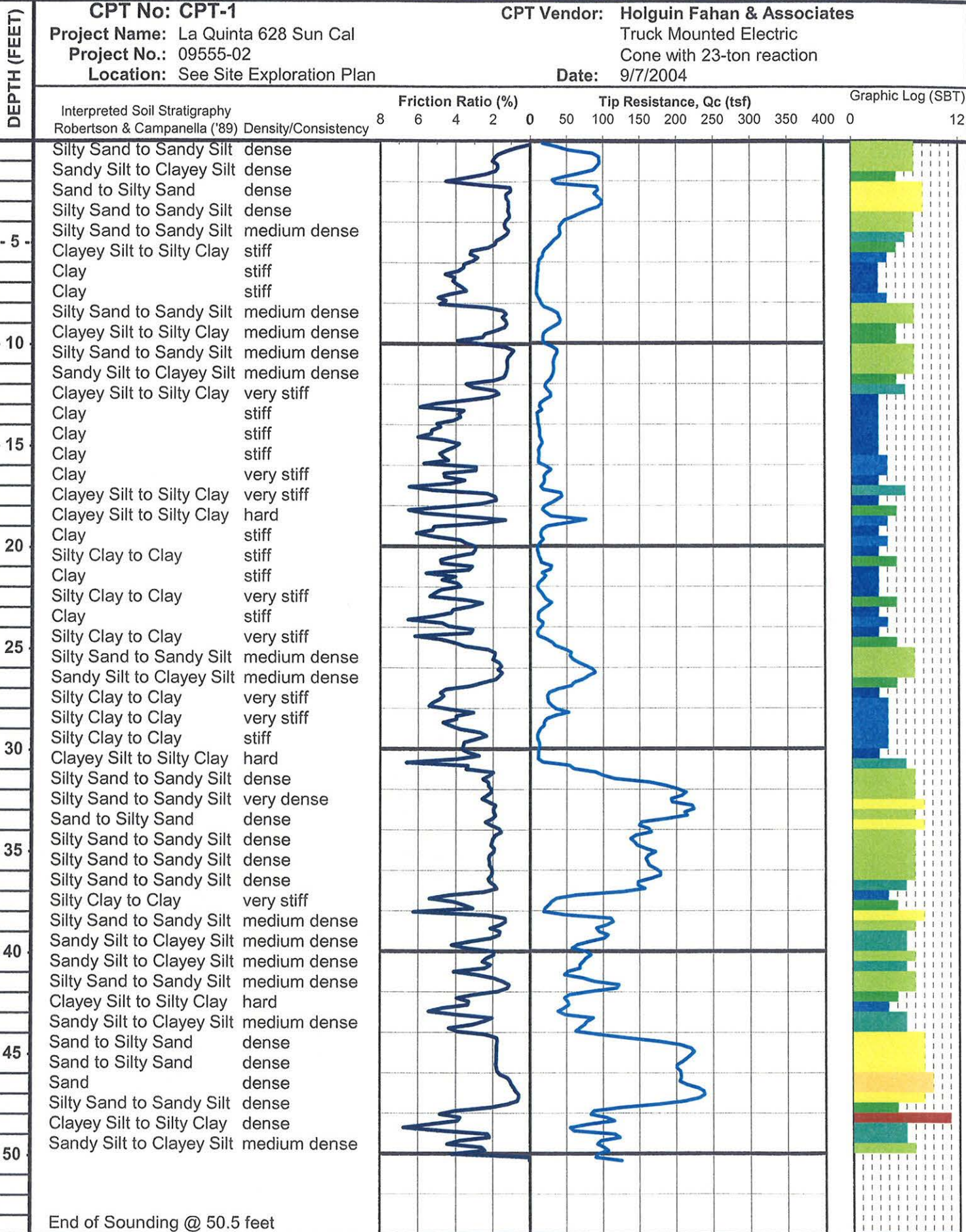
Location: See Site Exploration Plan

CPT Vendor: Holguin Fahan & Associates

Truck Mounted Electric

Cone with 23-ton reaction

Date: 9/7/2004





CPT No: CPT-2

Project Name: La Quinta 628 Sun Cal

Project No.: 09555-02

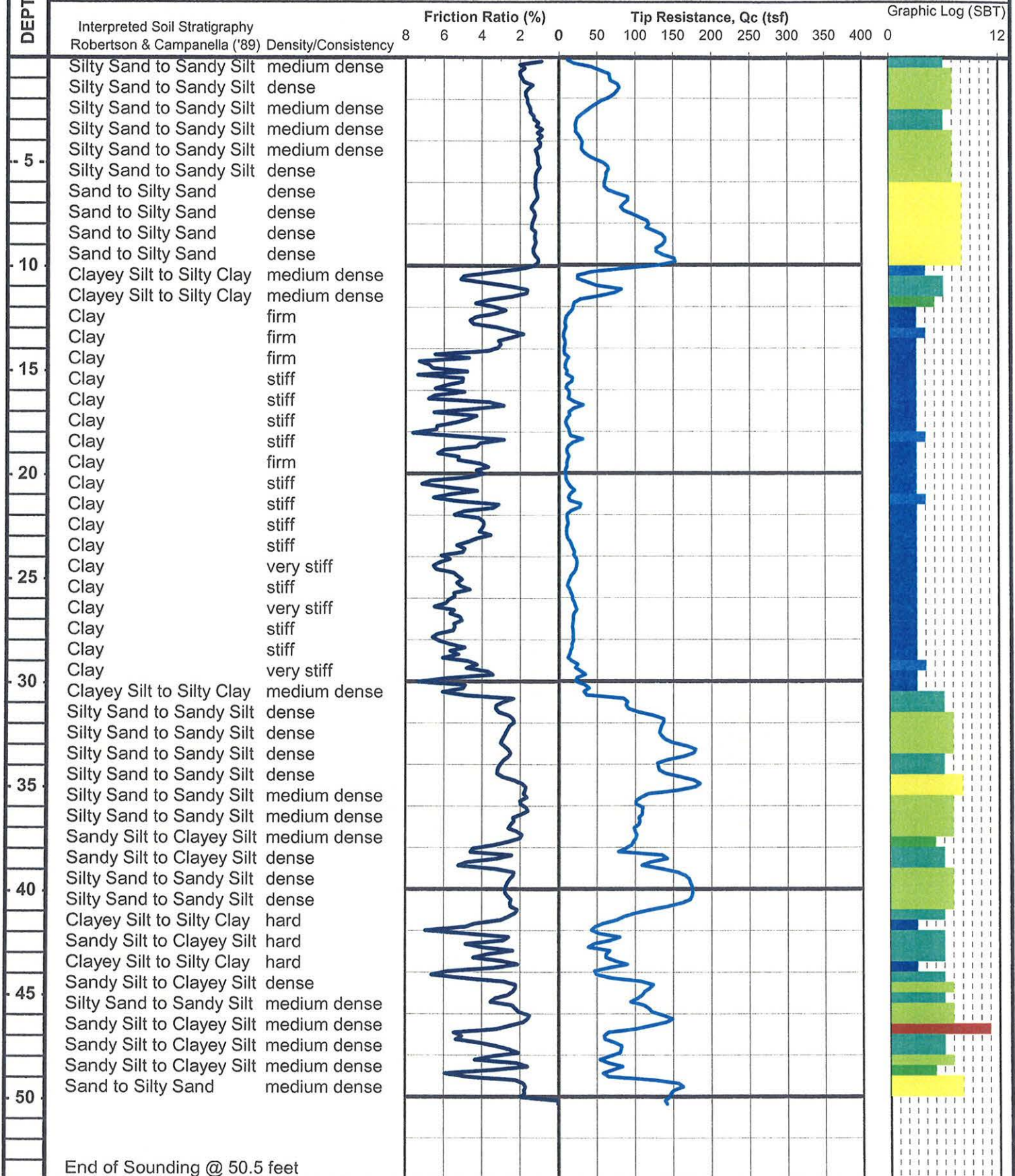
Location: See Site Exploration Plan

CPT Vendor: Holguin Fahan & Associates

Truck Mounted Electric

Cone with 23-ton reaction

Date: 9/7/2004





CPT No: CPT-3

Project Name: La Quinta 628 Sun Cal

Project No.: 09555-02

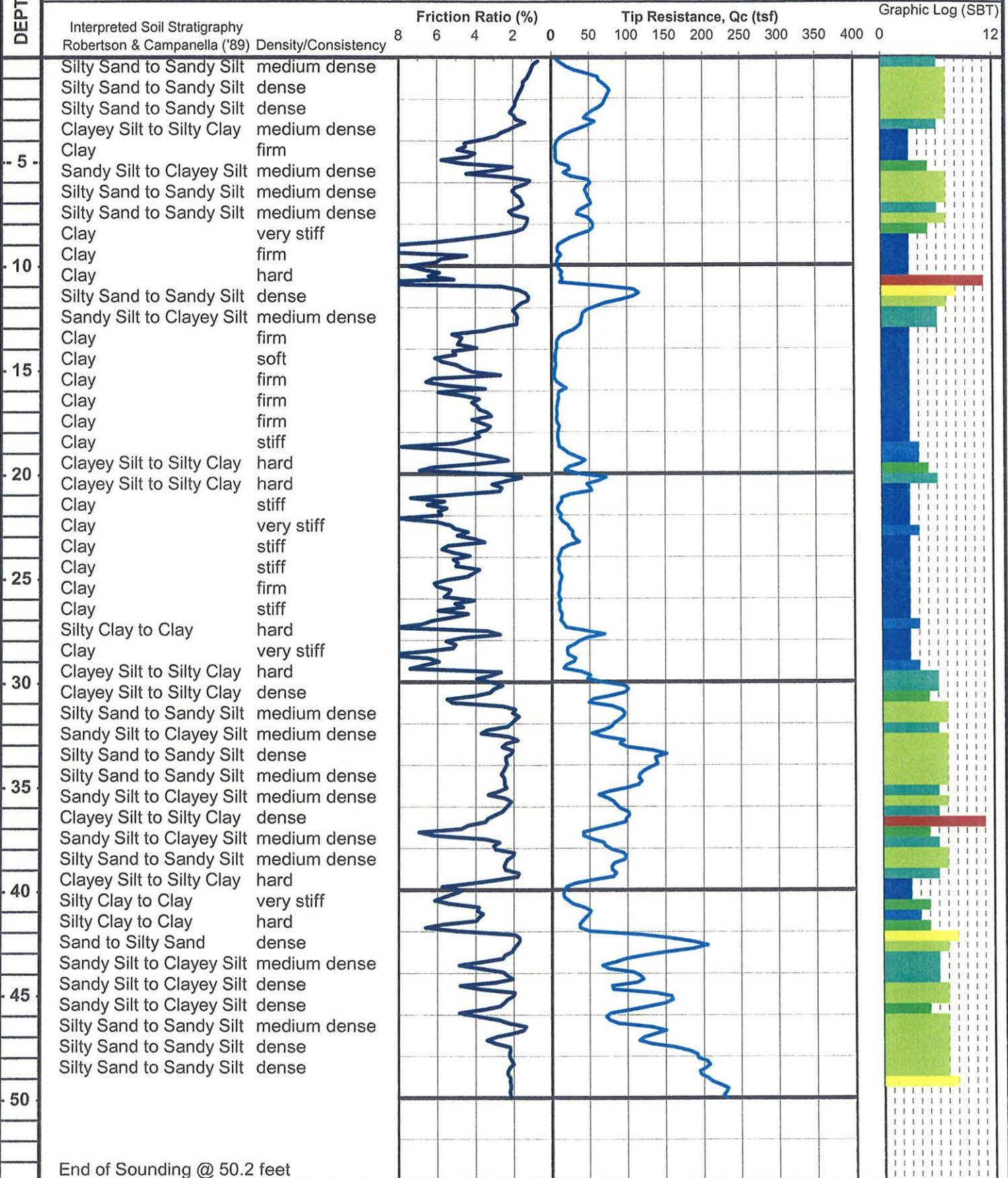
Location: See Site Exploration Plan

CPT Vendor: Holguin Fahan & Associates

Truck Mounted Electric

Cone with 23-ton reaction

Date: 9/7/2004





CPT No: CPT-4

Project Name: La Quinta 628 Sun Cal

Project No.: 09340-01

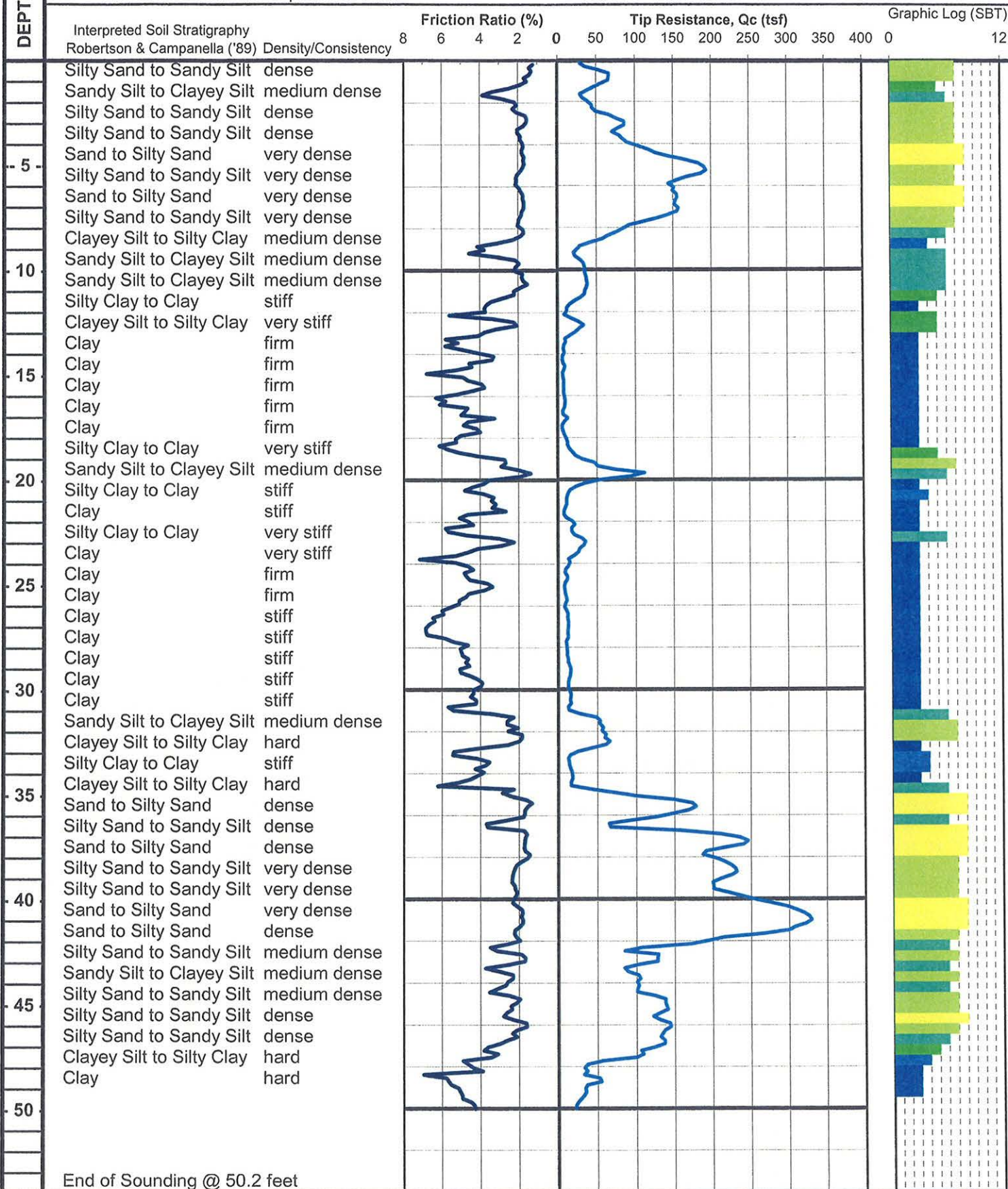
Location: See Site Exploration Plan

CPT Vendor: Holguin Fahan & Associates

Truck Mounted Electric

Cone with 23-ton reaction

Date: 10/27/2003





CPT No: CPT-5

Project Name: La Quinta 628 Sun Cal

Project No.: 09340-01

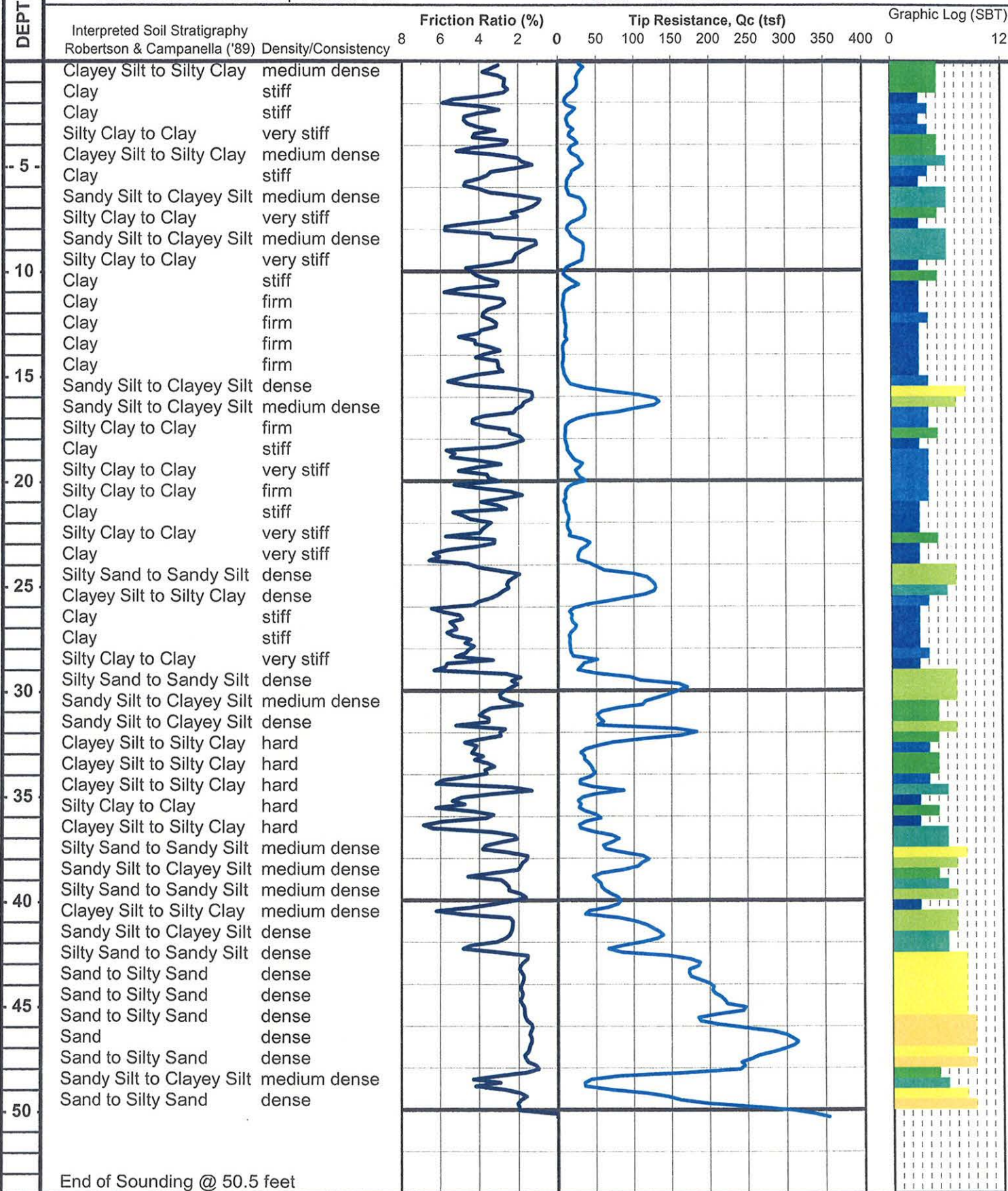
Location: See Site Exploration Plan

CPT Vendor: Holguin Fahan & Associates

Truck Mounted Electric

Cone with 23-ton reaction

Date: 10/27/2003





CPT No: CPT-6

CPT Vendor: Holguin Fahan & Associates

Project Name: La Quinta 628 Sun Cal

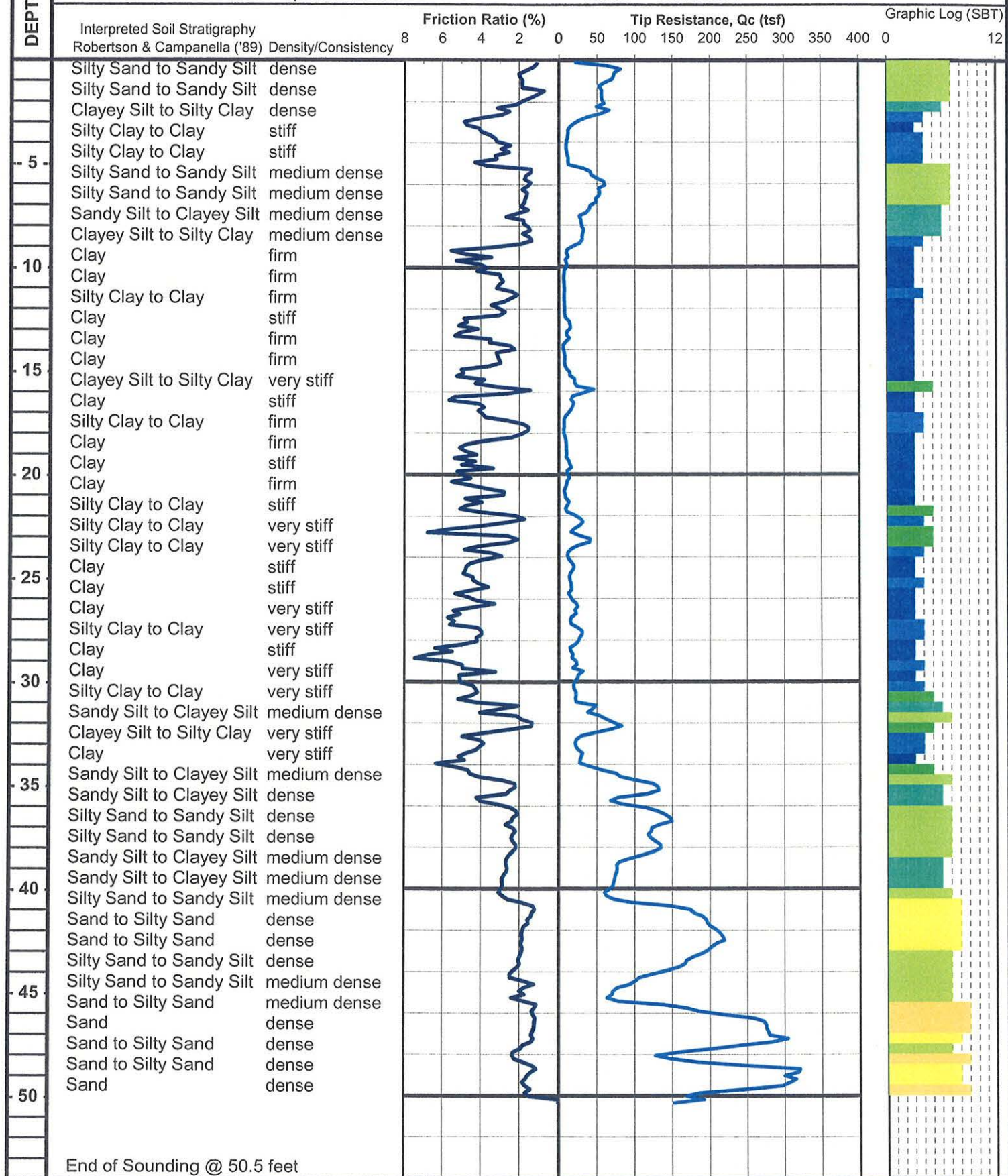
Project No.: 09340-01

Truck Mounted Electric

Cone with 23-ton reaction

Location: See Site Exploration Plan

Date: 10/27/2003





CPT No: CPT-7

Project Name: La Quinta 628 Sun Cal

Project No.: 09340-01

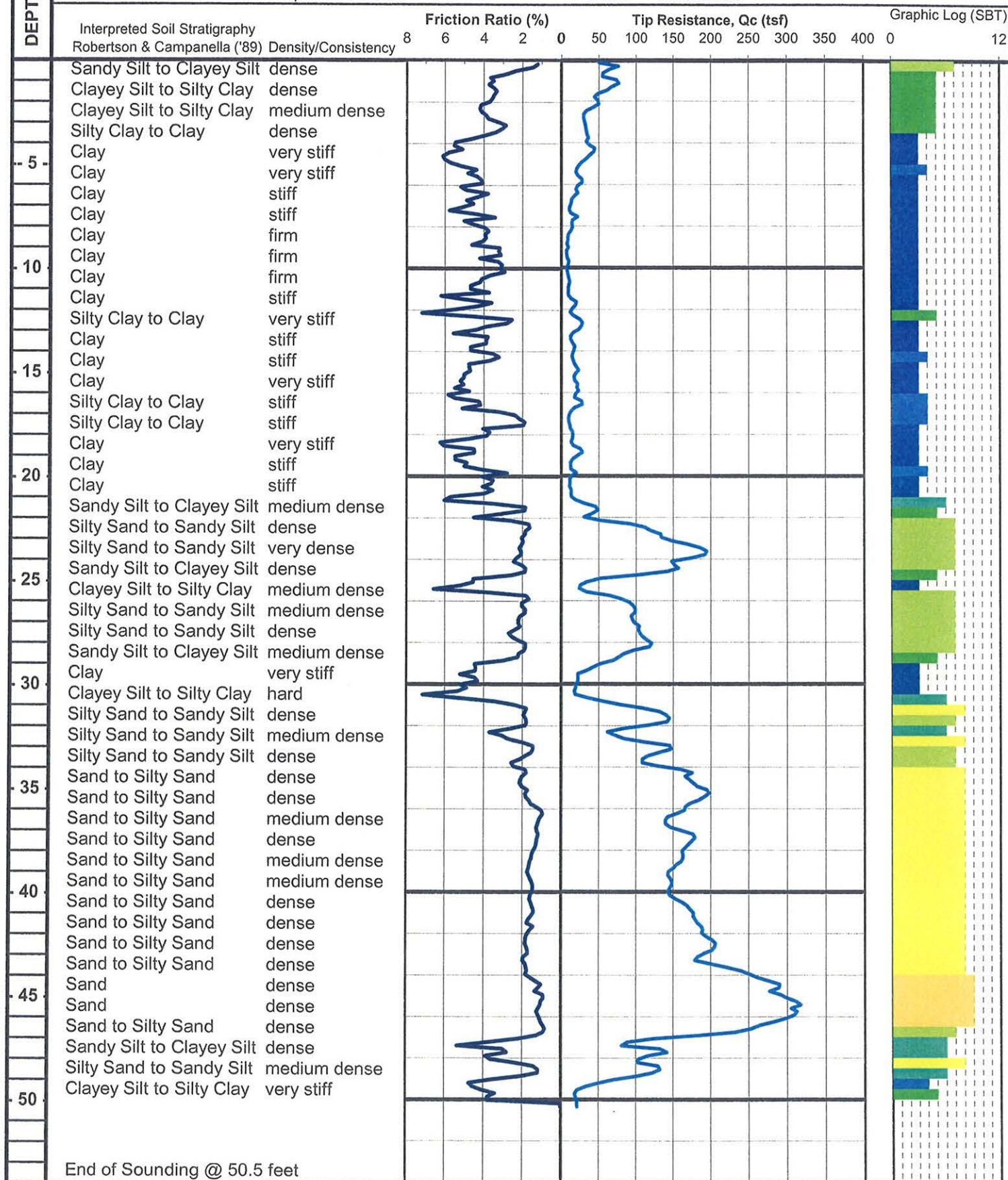
Location: See Site Exploration Plan

CPT Vendor: Holguin Fahan & Associates

Truck Mounted Electric

Cone with 23-ton reaction

Date: 10/27/2003





CPT No: CPT-8

Project Name: La Quinta 628 Sun Cal

Project No.: 09340-01

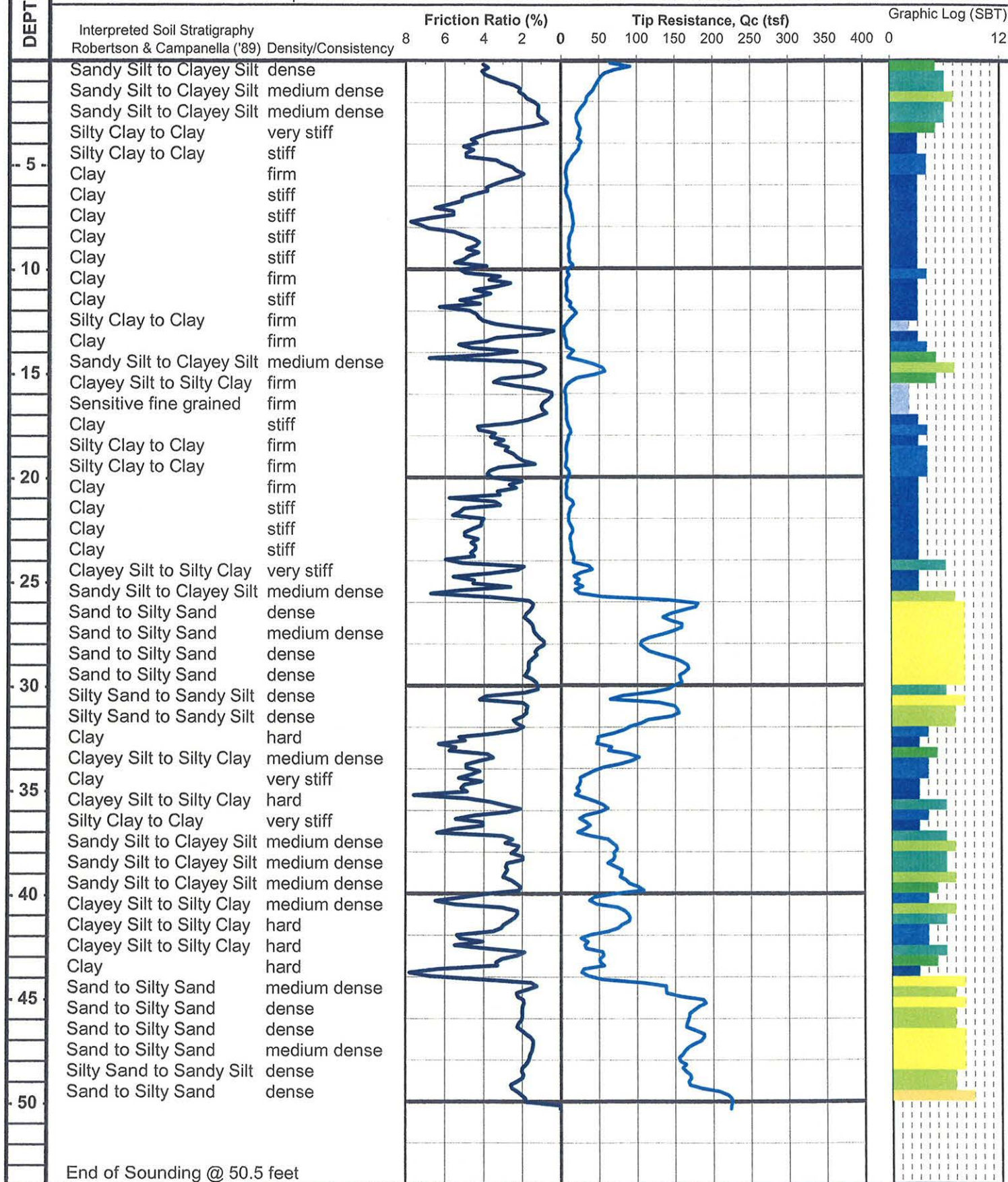
Location: See Site Exploration Plan

CPT Vendor: Holguin Fahan & Associates

Truck Mounted Electric

Cone with 23-ton reaction

Date: 10/27/2003

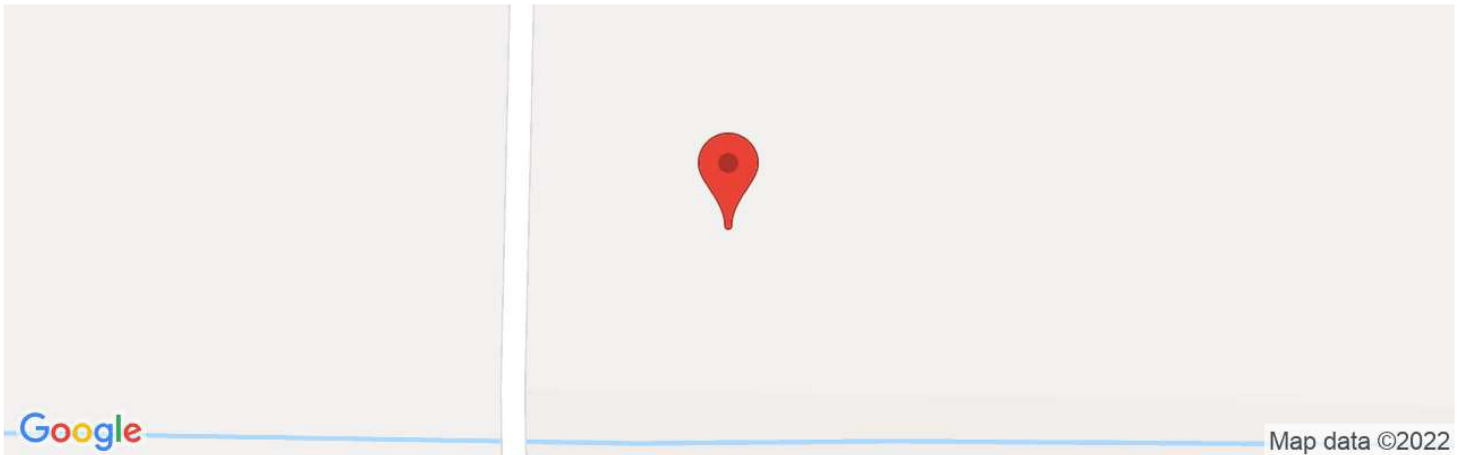


APPENDIX D

SEISMIC DESIGN PARAMETERS



Latitude, Longitude: 33.585278, -116.179547



Date	2/14/2022, 5:00:33 PM
Design Code Reference Document	ASCE7-16
Risk Category	III
Site Class	D - Default (See Section 11.4.3)

Type	Value	Description
S_S	1.5	MCE_R ground motion. (for 0.2 second period)
S_1	0.6	MCE_R ground motion. (for 1.0s period)
S_{MS}	1.8	Site-modified spectral acceleration value
S_{M1}	null -See Section 11.4.8	Site-modified spectral acceleration value
S_{DS}	1.2	Numeric seismic design value at 0.2 second SA
S_{D1}	null -See Section 11.4.8	Numeric seismic design value at 1.0 second SA

Type	Value	Description
SDC	null -See Section 11.4.8	Seismic design category
F_a	1.2	Site amplification factor at 0.2 second
F_v	null -See Section 11.4.8	Site amplification factor at 1.0 second
PGA	0.612	MCE_G peak ground acceleration
F_{PGA}	1.2	Site amplification factor at PGA
PGA_M	0.734	Site modified peak ground acceleration
T_L	8	Long-period transition period in seconds
SsRT	1.698	Probabilistic risk-targeted ground motion. (0.2 second)
SsUH	1.869	Factored uniform-hazard (2% probability of exceedance in 50 years) spectral acceleration
SsD	1.5	Factored deterministic acceleration value. (0.2 second)
S1RT	0.654	Probabilistic risk-targeted ground motion. (1.0 second)
S1UH	0.733	Factored uniform-hazard (2% probability of exceedance in 50 years) spectral acceleration.
S1D	0.6	Factored deterministic acceleration value. (1.0 second)
PGAd	0.612	Factored deterministic acceleration value. (Peak Ground Acceleration)
C_{RS}	0.909	Mapped value of the risk coefficient at short periods
C_{R1}	0.891	Mapped value of the risk coefficient at a period of 1 s

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Unified Hazard Tool



Please do not use this tool to obtain ground motion parameter values for the design code reference documents covered by the [U.S. Seismic Design Maps web tools](#) (e.g., the International Building Code and the ASCE 7 or 41 Standard). The values returned by the two applications are not identical.

^ Input

Edition

Dynamic: Conterminous U.S. 2014 (u...

Spectral Period

Peak Ground Acceleration

Latitude

Decimal degrees

33.585278

Time Horizon

Return period in years

2475

Longitude

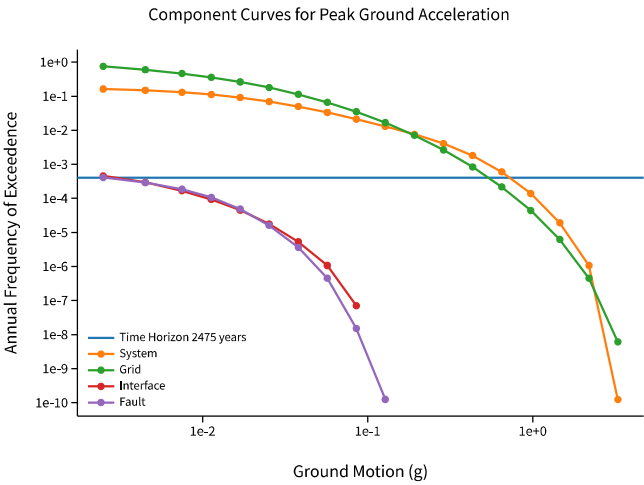
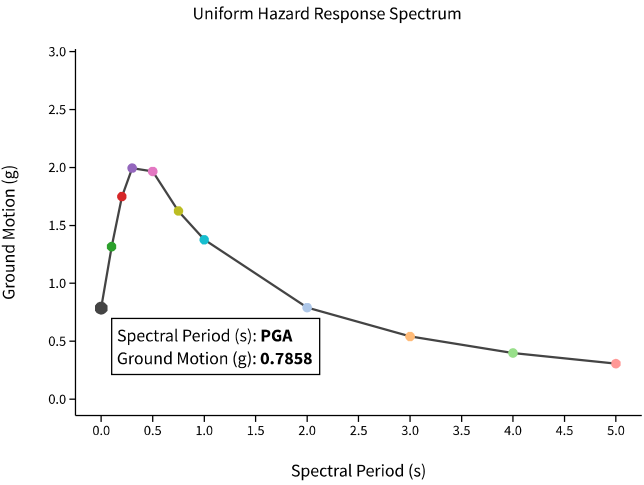
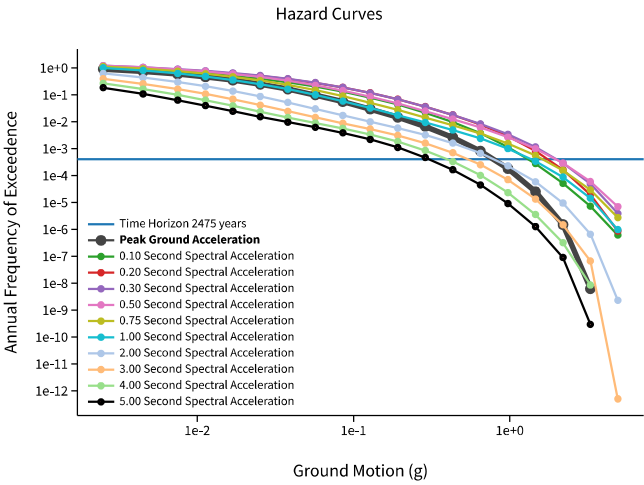
Decimal degrees, negative values for western longitudes

-116.179547

Site Class

259 m/s (Site class D)

^ Hazard Curve

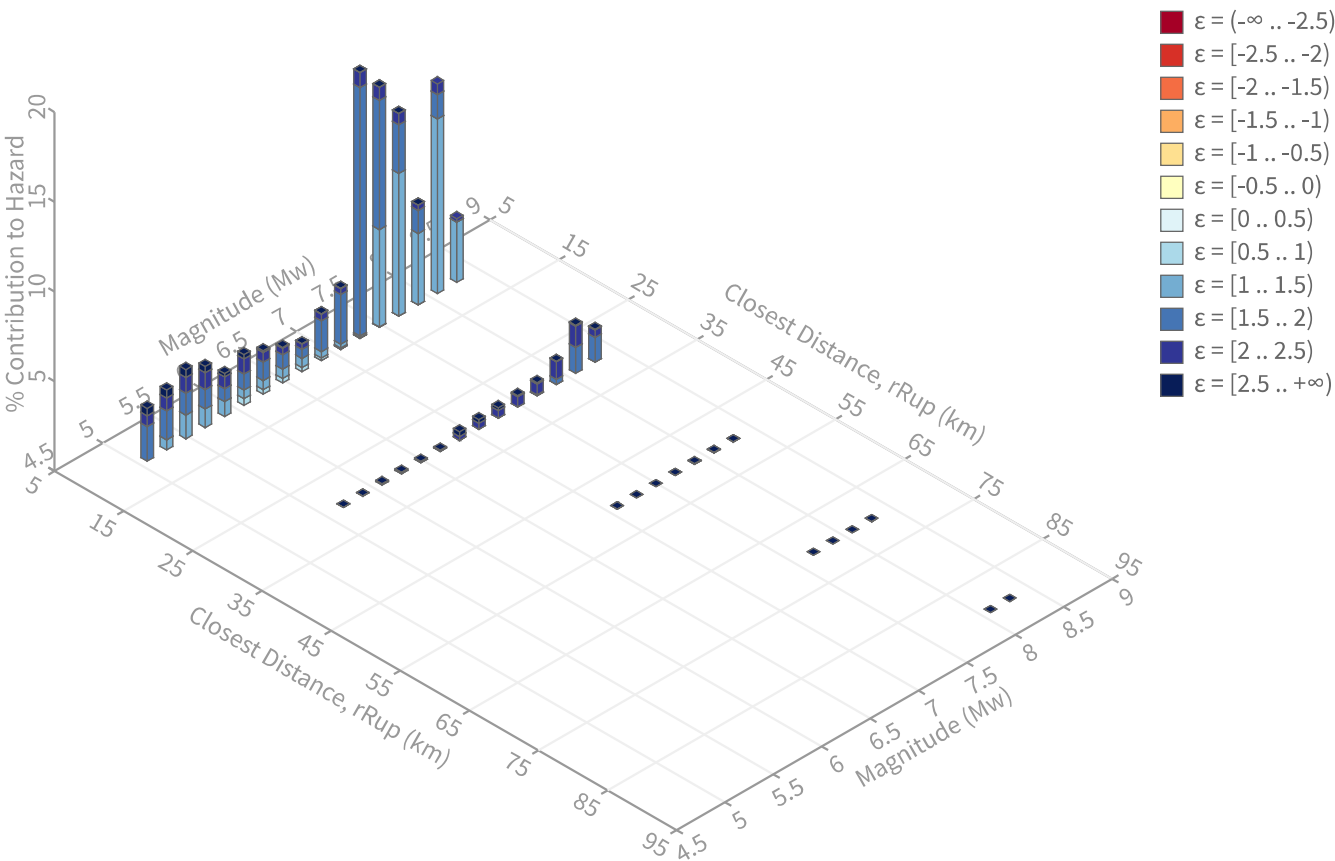


[View Raw Data](#)

^ Deaggregation

Component

Total



Summary statistics for, Deaggregation: Total

Deaggregation targets

Return period: 2475 yrs
Exceedance rate: 0.0004040404 yr⁻¹
PGA ground motion: 0.78576831 g

Recovered targets

Return period: 3040.7618 yrs
Exceedance rate: 0.00032886495 yr⁻¹

Totals

Binned: 100 %
Residual: 0 %
Trace: 0.08 %

Mean (over all sources)

m: 7.19
r: 12.47 km
ε₀: 1.65 σ

Mode (largest m-r bin)

m: 7.34
r: 11.78 km
ε₀: 1.65 σ
Contribution: 14.81 %

Mode (largest m-r-ε₀ bin)

m: 7.34
r: 11.82 km
ε₀: 1.61 σ
Contribution: 13.82 %

Discretization

r: min = 0.0, max = 1000.0, Δ = 20.0 km
m: min = 4.4, max = 9.4, Δ = 0.2
ε: min = -3.0, max = 3.0, Δ = 0.5 σ

Epsilon keys

- ε0:** [-∞ .. -2.5)
- ε1:** [-2.5 .. -2.0)
- ε2:** [-2.0 .. -1.5)
- ε3:** [-1.5 .. -1.0)
- ε4:** [-1.0 .. -0.5)
- ε5:** [-0.5 .. 0.0)
- ε6:** [0.0 .. 0.5)
- ε7:** [0.5 .. 1.0)
- ε8:** [1.0 .. 1.5)
- ε9:** [1.5 .. 2.0)
- ε10:** [2.0 .. 2.5)
- ε11:** [2.5 .. +∞]

Deaggregation Contributors

Source Set ↗ Source	Type	r	m	ε ₀	lon	lat	az	%
UC33brAvg_FM31	System							37.33
San Andreas (Coachella) rev [3]		11.81	7.64	1.52	116.088°W	33.659°N	45.77	31.53
San Jacinto (Clark) rev [2]		24.96	7.81	2.07	116.297°W	33.384°N	206.01	2.16
San Jacinto (Coyote Creek) [1]		32.02	8.03	2.16	116.427°W	33.384°N	225.85	1.57
UC33brAvg_FM32	System							37.18
San Andreas (Coachella) rev [3]		11.81	7.64	1.52	116.088°W	33.659°N	45.77	31.33
San Jacinto (Clark) rev [2]		24.96	7.82	2.06	116.297°W	33.384°N	206.01	2.09
San Jacinto (Coyote Creek) [1]		32.02	8.01	2.17	116.427°W	33.384°N	225.85	1.59
UC33brAvg_FM31 (opt)	Grid							12.75
PointSourceFinite: -116.180, 33.608		5.60	5.65	1.45	116.180°W	33.608°N	0.00	3.01
PointSourceFinite: -116.180, 33.608		5.60	5.65	1.45	116.180°W	33.608°N	0.00	2.98
PointSourceFinite: -116.180, 33.671		9.45	6.03	1.87	116.180°W	33.671°N	0.00	1.02
PointSourceFinite: -116.180, 33.671		9.45	6.03	1.87	116.180°W	33.671°N	0.00	1.00
UC33brAvg_FM32 (opt)	Grid							12.74
PointSourceFinite: -116.180, 33.608		5.60	5.65	1.45	116.180°W	33.608°N	0.00	3.01
PointSourceFinite: -116.180, 33.608		5.60	5.65	1.45	116.180°W	33.608°N	0.00	2.98
PointSourceFinite: -116.180, 33.671		9.45	6.03	1.87	116.180°W	33.671°N	0.00	1.02
PointSourceFinite: -116.180, 33.671		9.45	6.03	1.87	116.180°W	33.671°N	0.00	1.00

30	5.7	0.001	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.001
30	5.9	0.010	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.010
30	6.1	0.073	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.073
30	6.3	0.086	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.012	0.074
30	6.5	0.075	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.007	0.067
30	6.7	0.072	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.014	0.058
30	6.9	0.475	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.212	0.262
30	7.1	0.529	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.003	0.328	0.198
30	7.3	0.571	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.003	0.421	0.147
30	7.5	0.627	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.003	0.562	0.062
30	7.7	0.722	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.049	0.600	0.073
30	7.9	1.289	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.293	0.976	0.021
30	8.1	2.672	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.455	1.179	0.038
30	8.3	1.820	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.002	1.384	0.403	0.031
10	5.1	2.940	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.930	0.600	0.410
10	5.3	3.346	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.567	1.609	0.716	0.453
10	5.5	3.855	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.320	1.217	0.876	0.443
10	5.7	3.396	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.052	1.074	0.936	0.335
10	5.9	2.379	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.832	0.713	0.659	0.175
10	6.1	2.814	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.373	0.476	0.901	0.834	0.229
10	6.3	2.409	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.253	0.503	1.028	0.530	0.096
10	6.5	1.973	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.249	0.516	0.805	0.359	0.045
10	6.7	1.557	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.232	0.513	0.509	0.281	0.023
10	6.9	2.603	0.000	0.000	0.000	0.000	0.000	0.000	0.008	0.147	0.341	1.718	0.370	0.020
10	7.1	3.394	0.000	0.000	0.000	0.000	0.000	0.000	0.010	0.070	0.216	2.768	0.319	0.011
10	7.3	14.806	0.000	0.000	0.000	0.000	0.000	0.000	0.004	0.033	0.099	13.823	0.845	0.001
10	7.5	13.366	0.000	0.000	0.000	0.000	0.000	0.000	0.002	0.011	5.419	7.205	0.729	0.000
10	7.7	11.278	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.002	7.931	2.722	0.623	0.000
10	7.9	5.549	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.001	3.972	1.282	0.295	0.000
10	8.1	11.678	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	9.735	1.344	0.599	0.000
10	8.3	3.544	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	3.363	0.005	0.177	0.000

Principal Sources (faults, subduction, random seismicity having > 3% contribution

UC33brAvg_FM31:

Percent Contributed: 37.33

Distance (km): 13.801677

Magnitude: 7.6506542

Epsilon (mean values): 1.6054843

San Andreas (Coachella) rev [3]:

Percent Contributed: 31.53

Distance (km): 11.808984

Magnitude: 7.6442445

Epsilon (mean values): 1.5198782

Azimuth: 45.77243

Latitude: 33.659291

Longitude: -116.08815

San Jacinto (Clark) rev [2]:

Percent Contributed: 2.16

Distance (km): 24.959956

Magnitude: 7.8149043

Epsilon (mean values): 2.0660243

Azimuth: 206.01308

Latitude: 33.38395

Longitude: -116.29718

San Jacinto (Coyote Creek) [1]:

Percent Contributed: 1.57

Distance (km): 32.023487

Magnitude: 8.0259488

Epsilon (mean values): 2.1559329

Azimuth: 225.85202

Latitude: 33.38444

Longitude: -116.42703

UC33brAvg_FM32:

Percent Contributed: 37.18

Distance (km): 13.787704

Magnitude: 7.6444527

Epsilon (mean values): 1.6081289

San Andreas (Coachella) rev [3]:

Percent Contributed: 31.33

Distance (km): 11.808984

Magnitude: 7.6391584

Epsilon (mean values): 1.5228668
Azimuth: 45.77243
Latitude: 33.659291
Longitude: -116.08815
San Jacinto (Clark) rev [2]:
Percent Contributed: 2.09
Distance (km): 24.959956
Magnitude: 7.8194108
Epsilon (mean values): 2.0630822
Azimuth: 206.01308
Latitude: 33.38395
Longitude: -116.29718
San Jacinto (Coyote Creek) [1]:
Percent Contributed: 1.59
Distance (km): 32.023487
Magnitude: 8.0094633
Epsilon (mean values): 2.1672171
Azimuth: 225.85202
Latitude: 33.38444
Longitude: -116.42703
UC33brAvg_FM31 (opt):
Percent Contributed: 12.75
Distance (km): 8.5983886
Magnitude: 5.8530399
Epsilon (mean values): 1.7608723
PointSourceFinite: -116.180, 33.608:
Percent Contributed: 3.01
Distance (km): 5.6038696
Magnitude: 5.6468266
Epsilon (mean values): 1.4461112
Azimuth: 0
Latitude: 33.607761
Longitude: -116.17955
PointSourceFinite: -116.180, 33.608:
Percent Contributed: 2.98
Distance (km): 5.6038696
Magnitude: 5.6468266
Epsilon (mean values): 1.4461112
Azimuth: 0
Latitude: 33.607761
Longitude: -116.17955
PointSourceFinite: -116.180, 33.671:
Percent Contributed: 1.02
Distance (km): 9.448142
Magnitude: 6.0312322
Epsilon (mean values): 1.8666668
Azimuth: 0
Latitude: 33.670713
Longitude: -116.17955
PointSourceFinite: -116.180, 33.671:
Percent Contributed: 1
Distance (km): 9.448142
Magnitude: 6.0312322
Epsilon (mean values): 1.8666668
Azimuth: 0
Latitude: 33.670713
Longitude: -116.17955
UC33brAvg_FM32 (opt):
Percent Contributed: 12.74
Distance (km): 8.5986253
Magnitude: 5.8525001
Epsilon (mean values): 1.7610821
PointSourceFinite: -116.180, 33.608:
Percent Contributed: 3.01
Distance (km): 5.6040812
Magnitude: 5.6464357
Epsilon (mean values): 1.4462969
Azimuth: 0
Latitude: 33.607761
Longitude: -116.17955

```

PointSourceFinite: -116.180, 33.608:
  Percent Contributed: 2.98
  Distance (km): 5.6040812
  Magnitude: 5.6464357
  Epsilon (mean values): 1.4462969
  Azimuth: 0
  Latitude: 33.607761
  Longitude: -116.17955
PointSourceFinite: -116.180, 33.671:
  Percent Contributed: 1.02
  Distance (km): 9.4495831
  Magnitude: 6.0306167
  Epsilon (mean values): 1.8671345
  Azimuth: 0
  Latitude: 33.670713
  Longitude: -116.17955
PointSourceFinite: -116.180, 33.671:
  Percent Contributed: 1
  Distance (km): 9.4495831
  Magnitude: 6.0306167
  Epsilon (mean values): 1.8671345
  Azimuth: 0
  Latitude: 33.670713
  Longitude: -116.17955
PSHA Deaggregation. %contributions.
site: Test
longitude: 116.180°W
latitude: 33.585°E
imt: Peak Ground Acceleration
vs30 = 259 m/s (Site class D)
return period: 2475 yrs.
#This deaggregation corresponds to: GMM: Abrahamson, Silva & Kamai (2014)
Summary statistics for PSHA PGA deaggregation, r=distance, ε=epsilon:
Deaggregation targets:
  Return period: 2475 yrs
  Exceedance rate: 0.0004040404 yr-1
  PGA ground motion: 0.78576831 g
Recovered targets:
  Return period: 3040.7618 yrs
  Exceedance rate: 0.00032886495 yr-1
Totals:
  Binned: 25.77 %
  Residual: 0 %
  Trace: 0.06 %
Mean (over all sources):
  m: 7.12
  r: 12.87 km
  ε0: 1.79 σ
Mode (largest m-r bin):
  m: 7.34
  r: 11.79 km
  ε0: 1.72 σ
  Contribution: 3.71 %
Mode (largest m-r-ε0 bin):
  m: 7.34
  r: 11.82 km
  ε0: 1.72 σ
  Contribution: 3.68 %
Discretization:
  r: min = 0.0, max = 1000.0, Δ = 20.0 km
  m: min = 4.4, max = 9.4, Δ = 0.2
  ε: min = -3.0, max = 3.0, Δ = 0.5 σ
Epsilon keys:
  ε0: [-∞ .. -2.5)
  ε1: [-2.5 .. -2.0)
  ε2: [-2.0 .. -1.5)
  ε3: [-1.5 .. -1.0)
  ε4: [-1.0 .. -0.5)
  ε5: [-0.5 .. 0.0)

```

ϵ_6 : [0.0 .. 0.5)
 ϵ_7 : [0.5 .. 1.0)
 ϵ_8 : [1.0 .. 1.5)
 ϵ_9 : [1.5 .. 2.0)
 ϵ_{10} : [2.0 .. 2.5)
 ϵ_{11} : [2.5 .. + ∞]

	Closest Distance, rRup (km)				Magnitude (Mw)		ALL_ε	ε=(-∞,-2.5)		ε=[-2.5,-2)		ε=[-2,-1.5)	
	ε=[-1.5,-1)		ε=[-1,-0.5)		ε=[-0.5,0)			ε=[0,0.5)		ε=[0.5,1)		ε=[1,1.5)	
	ε=[2,2.5)		ε=[2.5,∞)										
90	8.1	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
90	8.3	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
70	7.7	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
70	7.9	0.001	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.001
70	8.1	0.001	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.001
70	8.3	0.001	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.001
50	7.3	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
50	7.5	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
50	7.7	0.001	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.001
50	7.9	0.016	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.016
50	8.1	0.015	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.009
50	8.3	0.003	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.001
30	5.7	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
30	5.9	0.002	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.002
30	6.1	0.027	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.027
30	6.3	0.032	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.032
30	6.5	0.022	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.022
30	6.7	0.025	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.023
30	6.9	0.182	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.127
30	7.1	0.181	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.101
30	7.3	0.190	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.024
30	7.5	0.200	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.032
30	7.7	0.233	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.001
30	7.9	0.397	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.017	0.001
30	8.1	0.804	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.289	0.000
30	8.3	0.532	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.312	0.000
10	5.1	1.367	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.781	0.211
10	5.3	1.131	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.603	0.197
10	5.5	0.941	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.466	0.175
10	5.7	0.790	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.369	0.121
10	5.9	0.558	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.304	0.070
10	6.1	0.671	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.156	0.201	0.070
10	6.3	0.611	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.120	0.290	0.019
10	6.5	0.493	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.098	0.265	0.005
10	6.7	0.385	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.026	0.106	0.163	0.002
10	6.9	0.674	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.032	0.054	0.501	0.000
10	7.1	0.888	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.015	0.035	0.762	0.000
10	7.3	3.714	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.006	0.019	3.685	0.000
10	7.5	3.277	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.002	0.005	3.269	0.000
10	7.7	2.715	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.005	2.710	0.000
10	7.9	1.265	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.012	1.252	0.000
10	8.1	2.628	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.312	1.317	0.000
10	8.3	0.795	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.790	0.005	0.000

Principal Sources (faults, subduction, random seismicity having > 3% contribution

UC33brAvg_FM31:

Percent Contributed: 9.32
 Distance (km): 14.332947
 Magnitude: 7.6404714
 Epsilon (mean values): 1.7242899

San Andreas (Coachella) rev [3]:

Percent Contributed: 7.57
 Distance (km): 11.808984
 Magnitude: 7.630479
 Epsilon (mean values): 1.6292111
 Azimuth: 45.77243
 Latitude: 33.659291
 Longitude: -116.08815

UC33brAvg_FM32:

Percent Contributed: 9.29
 Distance (km): 14.317507
 Magnitude: 7.6329863

Epsilon (mean values): 1.7270571
 San Andreas (Coachella) rev [3]:
 Percent Contributed: 7.52
 Distance (km): 11.808984
 Magnitude: 7.6240234
 Epsilon (mean values): 1.6326796
 Azimuth: 45.77243
 Latitude: 33.659291
 Longitude: -116.08815
 UC33brAvg_FM31 (opt):
 Percent Contributed: 3.58
 Distance (km): 9.0796449
 Magnitude: 5.7601099
 Epsilon (mean values): 1.9655032
 UC33brAvg_FM32 (opt):
 Percent Contributed: 3.58
 Distance (km): 9.0801236
 Magnitude: 5.7595998
 Epsilon (mean values): 1.9657251
 PSHA Deaggregation. %contributions.
 site: Test
 longitude: 116.180°W
 latitude: 33.585°E
 imt: Peak Ground Acceleration
 vs30 = 259 m/s (Site class D)
 return period: 2475 yrs.
 #This deaggregation corresponds to: GMM: Boore, Stewart, Seyhan & Atkinson (2014)
 Summary statistics for PSHA PGA deaggregation, r=distance, ϵ =epsilon:
 Deaggregation targets:
 Return period: 2475 yrs
 Exceedance rate: 0.0004040404 yr⁻¹
 PGA ground motion: 0.78576831 g
 Recovered targets:
 Return period: 3040.7618 yrs
 Exceedance rate: 0.00032886495 yr⁻¹
 Totals:
 Binned: 39.76 %
 Residual: 0 %
 Trace: 0.07 %
 Mean (over all sources):
 m: 7.13
 r: 12.57 km
 ϵ_0 : 1.53 σ
 Mode (largest m-r bin):
 m: 7.34
 r: 11.79 km
 ϵ_0 : 1.54 σ
 Contribution: 5.44 %
 Mode (largest m-r- ϵ_0 bin):
 m: 7.34
 r: 11.83 km
 ϵ_0 : 1.54 σ
 Contribution: 5.39 %
 Discretization:
 r: min = 0.0, max = 1000.0, Δ = 20.0 km
 m: min = 4.4, max = 9.4, Δ = 0.2
 ϵ : min = -3.0, max = 3.0, Δ = 0.5 σ
 Epsilon keys:
 ϵ_0 : [- ∞ .. -2.5)
 ϵ_1 : [-2.5 .. -2.0)
 ϵ_2 : [-2.0 .. -1.5)
 ϵ_3 : [-1.5 .. -1.0)
 ϵ_4 : [-1.0 .. -0.5)
 ϵ_5 : [-0.5 .. 0.0)
 ϵ_6 : [0.0 .. 0.5)
 ϵ_7 : [0.5 .. 1.0)
 ϵ_8 : [1.0 .. 1.5)
 ϵ_9 : [1.5 .. 2.0)
 ϵ_{10} : [2.0 .. 2.5)

ϵ_{11} : [2.5 .. $+\infty$]															
	Closest Distance, rRup (km)				Magnitude (Mw)		ALL_ ϵ	$\epsilon=(-\infty,-2.5)$		$\epsilon=[-2.5,-2)$		$\epsilon=[-2,-1.5)$			
	$\epsilon=[-1.5,-1)$		$\epsilon=[-1,-0.5)$		$\epsilon=[-0.5,0)$			$\epsilon=[0,0.5)$		$\epsilon=[0.5,1)$		$\epsilon=[1,1.5)$		$\epsilon=[1.5,2)$	
	$\epsilon=[2,2.5)$		$\epsilon=[2.5,\infty)$												
90	8.3	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
70	7.9	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
70	8.1	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
70	8.3	0.001	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.001	
50	7.1	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
50	7.3	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
50	7.5	0.001	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.001	
50	7.7	0.001	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.001	
50	7.9	0.019	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.004	0.014	
50	8.1	0.018	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.010	0.007	
50	8.3	0.004	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.003	0.001	
30	5.7	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
30	5.9	0.008	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.008	
30	6.1	0.045	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.045	
30	6.3	0.046	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.012	0.035	
30	6.5	0.049	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.007	0.042	
30	6.7	0.044	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.012	0.032	
30	6.9	0.239	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.155	0.084	
30	7.1	0.270	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.002	0.224	0.044	
30	7.3	0.280	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.002	0.248	0.030	
30	7.5	0.293	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.002	0.290	0.001	
30	7.7	0.332	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.049	0.283	0.000	
30	7.9	0.568	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.248	0.320	0.000	
30	8.1	1.170	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.938	0.232	0.000	
30	8.3	0.776	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.002	0.772	0.003	0.000	
10	5.1	0.853	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.741	0.026	0.086	
10	5.3	1.396	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.567	0.482	0.236	0.111	
10	5.5	2.087	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.320	0.275	0.367	0.125	
10	5.7	1.821	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.052	0.298	0.359	0.112	
10	5.9	1.217	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.648	0.265	0.261	0.042	
10	6.1	1.356	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.373	0.139	0.434	0.329	0.081	
10	6.3	1.061	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.253	0.245	0.401	0.145	0.017	
10	6.5	0.808	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.171	0.271	0.265	0.098	0.004	
10	6.7	0.599	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.106	0.252	0.180	0.061	0.000	
10	6.9	1.015	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.058	0.154	0.720	0.083	0.000	
10	7.1	1.271	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.028	0.091	1.144	0.007	0.000	
10	7.3	5.440	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.011	0.040	5.388	0.001	0.000	
10	7.5	4.838	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.003	3.336	1.499	0.000	0.000	
10	7.7	4.027	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.001	4.021	0.005	0.000	0.000	
10	7.9	2.080	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.073	0.006	0.000	0.000	
10	8.1	4.391	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	4.391	0.000	0.000	0.000	
10	8.3	1.334	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.334	0.000	0.000	0.000	

Principal Sources (faults, subduction, random seismicity having > 3% contribution

UC33brAvg_FM31:

Percent Contributed: 14.21

Distance (km): 14.179121

Magnitude: 7.6448873

Epsilon (mean values): 1.5150141

San Andreas (Coachella) rev [3]:

Percent Contributed: 11.63

Distance (km): 11.808984

Magnitude: 7.6413545

Epsilon (mean values): 1.4096519

Azimuth: 45.77243

Latitude: 33.659291

Longitude: -116.08815

UC33brAvg_FM32:

Percent Contributed: 14.16

Distance (km): 14.16203

Magnitude: 7.6398016

Epsilon (mean values): 1.5163311

San Andreas (Coachella) rev [3]:

Percent Contributed: 11.58

Distance (km): 11.808984

Magnitude: 7.6368295

Epsilon (mean values): 1.411655

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Azimuth: 45.77243
Latitude: 33.659291
Longitude: -116.08815
UC33brAvg_FM31 (opt):
  Percent Contributed: 5.7
  Distance (km): 8.5771535
  Magnitude: 5.8491851
  Epsilon (mean values): 1.5716884
PointSourceFinite: -116.180, 33.608:
  Percent Contributed: 1.45
  Distance (km): 5.6942439
  Magnitude: 5.6421595
  Epsilon (mean values): 1.2321319
  Azimuth: 0
  Latitude: 33.607761
  Longitude: -116.17955
PointSourceFinite: -116.180, 33.608:
  Percent Contributed: 1.44
  Distance (km): 5.6942439
  Magnitude: 5.6421595
  Epsilon (mean values): 1.2321319
  Azimuth: 0
  Latitude: 33.607761
  Longitude: -116.17955
UC33brAvg_FM32 (opt):
  Percent Contributed: 5.69
  Distance (km): 8.5774133
  Magnitude: 5.848731
  Epsilon (mean values): 1.5718604
PointSourceFinite: -116.180, 33.608:
  Percent Contributed: 1.45
  Distance (km): 5.6943568
  Magnitude: 5.6418384
  Epsilon (mean values): 1.2322882
  Azimuth: 0
  Latitude: 33.607761
  Longitude: -116.17955
PointSourceFinite: -116.180, 33.608:
  Percent Contributed: 1.44
  Distance (km): 5.6943568
  Magnitude: 5.6418384
  Epsilon (mean values): 1.2322882
  Azimuth: 0
  Latitude: 33.607761
  Longitude: -116.17955
PSHA Deaggregation. %contributions.
site: Test
longitude: 116.180°W
latitude: 33.585°E
imt: Peak Ground Acceleration
vs30 = 259 m/s (Site class D)
return period: 2475 yrs.
#This deaggregation corresponds to: GMM: Campbell & Bozorgnia (2014)
Summary statistics for PSHA PGA deaggregation, r=distance, ε=epsilon:
Deaggregation targets:
  Return period: 2475 yrs
  Exceedance rate: 0.0004040404 yr-1
  PGA ground motion: 0.78576831 g
Recovered targets:
  Return period: 3040.7618 yrs
  Exceedance rate: 0.00032886495 yr-1
Totals:
  Binned: 4.54 %
  Residual: 0 %
  Trace: 0.02 %
Mean (over all sources):
  m: 7.37
  r: 11.36 km
  ε0: 2.24 σ
Mode (largest m-r bin):

```

m: 7.34
 r: 11.76 km
 ϵ_0 : 2.29 σ
 Contribution: 0.85 %
 Mode (largest m-r- ϵ_0 bin):
 m: 7.34
 r: 11.81 km
 ϵ_0 : 2.3 σ
 Contribution: 0.84 %
 Discretization:
 r: min = 0.0, max = 1000.0, Δ = 20.0 km
 m: min = 4.4, max = 9.4, Δ = 0.2
 ϵ : min = -3.0, max = 3.0, Δ = 0.5 σ

Epsilon keys:

ϵ_0 : [- ∞ .. -2.5)
 ϵ_1 : [-2.5 .. -2.0)
 ϵ_2 : [-2.0 .. -1.5)
 ϵ_3 : [-1.5 .. -1.0)
 ϵ_4 : [-1.0 .. -0.5)
 ϵ_5 : [-0.5 .. 0.0)
 ϵ_6 : [0.0 .. 0.5)
 ϵ_7 : [0.5 .. 1.0)
 ϵ_8 : [1.0 .. 1.5)
 ϵ_9 : [1.5 .. 2.0)
 ϵ_{10} : [2.0 .. 2.5)
 ϵ_{11} : [2.5 .. + ∞)

	Closest Distance, rRup (km)				Magnitude (Mw)		ALL_ε	ε=(-∞,-2.5) ε=[0.5,1)	ε=[-2.5,-2) ε=[1,1.5)	ε=[-2,-1.5) ε=[1.5,2)					
	ε=[-1.5,-1)		ε=[-1,-0.5)		ε=[-0.5,0)						ε=[0,0.5)				
	ε=[2,2.5)		ε=[2.5,∞)												
30	6.5	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000		
30	6.7	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000		
30	6.9	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000		
30	7.1	0.001	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.001		
30	7.3	0.001	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.001		
30	7.5	0.006	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.006		
30	7.7	0.006	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.006		
30	7.9	0.013	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.013		
30	8.1	0.035	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.035		
30	8.3	0.031	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.031		
10	5.1	0.017	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.017		
10	5.3	0.029	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.029		
10	5.5	0.042	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.042		
10	5.7	0.053	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.010		
10	5.9	0.056	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.011		
10	6.1	0.114	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.019	0.060	0.036		
10	6.3	0.156	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.042	0.081	0.032		
10	6.5	0.175	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.025	0.065	0.059	0.025		
10	6.7	0.137	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.026	0.053	0.043	0.016		
10	6.9	0.186	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.015	0.030	0.121	0.019		
10	7.1	0.207	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.008	0.015	0.172	0.011		
10	7.3	0.848	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.003	0.007	0.837	0.001		
10	7.5	0.731	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.001	0.002	0.728	0.000		
10	7.7	0.623	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.622	0.000		
10	7.9	0.295	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.295	0.000		
10	8.1	0.599	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.599	0.000		
10	8.3	0.177	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.177	0.000		

Principal Sources (faults, subduction, random seismicity having > 3% contribution

UC33brAvg_FM32:

Percent Contributed: 1.85
 Distance (km): 12.222184
 Magnitude: 7.6081689
 Epsilon (mean values): 2.2562871

San Andreas (Coachella) rev [3]:

Percent Contributed: 1.73
 Distance (km): 11.808984
 Magnitude: 7.6183376
 Epsilon (mean values): 2.2335814
 Azimuth: 45.77243
 Latitude: 33.659291
 Longitude: -116.08815

[illegible]

70	8.3	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
50	7.3	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
50	7.5	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
50	7.7	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
50	7.9	0.003	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.003
50	8.1	0.005	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.005
50	8.3	0.002	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.001	0.001
30	6.1	0.001	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.001
30	6.3	0.008	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.008
30	6.5	0.003	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.003
30	6.7	0.003	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.001	0.002
30	6.9	0.053	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.002	0.051
30	7.1	0.077	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.001	0.024	0.052
30	7.3	0.099	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.001	0.006	0.092
30	7.5	0.128	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.001	0.105	0.022
30	7.7	0.151	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.085	0.066
30	7.9	0.312	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.028	0.277	0.006
30	8.1	0.663	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.228	0.432	0.003
30	8.3	0.480	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.301	0.179	0.000
10	5.1	0.703	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.408	0.198	0.097
10	5.3	0.790	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.525	0.149	0.116
10	5.5	0.785	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.475	0.209	0.101
10	5.7	0.731	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.407	0.233	0.091
10	5.9	0.549	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.184	0.144	0.169	0.051
10	6.1	0.673	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.181	0.248	0.201	0.042
10	6.3	0.582	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.138	0.294	0.122	0.027
10	6.5	0.497	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.077	0.121	0.211	0.076	0.012
10	6.7	0.436	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.100	0.129	0.113	0.087	0.005
10	6.9	0.729	0.000	0.000	0.000	0.000	0.000	0.000	0.008	0.057	0.118	0.466	0.078	0.001
10	7.1	1.029	0.000	0.000	0.000	0.000	0.000	0.000	0.010	0.028	0.081	0.845	0.064	0.000
10	7.3	4.803	0.000	0.000	0.000	0.000	0.000	0.000	0.004	0.016	0.037	4.743	0.003	0.000
10	7.5	4.520	0.000	0.000	0.000	0.000	0.000	0.000	0.002	0.006	2.077	2.435	0.000	0.000
10	7.7	3.912	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.001	3.904	0.007	0.000	0.000
10	7.9	1.910	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.886	0.023	0.000	0.000
10	8.1	4.059	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	4.032	0.027	0.000	0.000
10	8.3	1.239	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.239	0.000	0.000	0.000

Principal Sources (faults, subduction, random seismicity having > 3% contribution

UC33brAvg_FM31:

Percent Contributed: 11.95
Distance (km): 13.181649
Magnitude: 7.6706608
Epsilon (mean values): 1.519818

San Andreas (Coachella) rev [3]:

Percent Contributed: 10.59
Distance (km): 11.808984
Magnitude: 7.6604224
Epsilon (mean values): 1.4463115
Azimuth: 45.77243
Latitude: 33.659291
Longitude: -116.08815

UC33brAvg_FM32:

Percent Contributed: 11.88
Distance (km): 13.171764
Magnitude: 7.6646071
Epsilon (mean values): 1.5235668

San Andreas (Coachella) rev [3]:

Percent Contributed: 10.51
Distance (km): 11.808984
Magnitude: 7.655982
Epsilon (mean values): 1.4499734
Azimuth: 45.77243
Latitude: 33.659291
Longitude: -116.08815

UC33brAvg_FM31 (opt):

Percent Contributed: 3.05
Distance (km): 8.2246506
Magnitude: 5.9063837
Epsilon (mean values): 1.8203077

UC33brAvg_FM32 (opt):

Percent Contributed: 3.05

[illegible]

30	6.1	0.001	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.001
30	6.3	0.007	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.007
30	6.5	0.034	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.034
30	6.7	0.039	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.003	0.036
30	6.9	0.430	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.191	0.238
30	7.1	0.483	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.302	0.182
30	7.3	0.535	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.397	0.138
30	7.5	0.613	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.001	0.552	0.060
30	7.7	0.720	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.049	0.598	0.073
30	7.9	1.289	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.293	0.975	0.021
30	8.1	2.672	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.455	1.179	0.038
30	8.3	1.820	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.002	1.384	0.403	0.031
10	6.1	0.270	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.228	0.042
10	6.3	0.288	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.079	0.188	0.021
10	6.5	0.283	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.087	0.176	0.020
10	6.7	0.275	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.131	0.135	0.009
10	6.9	1.777	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.480	0.283	0.015
10	7.1	2.935	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.643	0.283	0.009
10	7.3	14.601	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	13.768	0.833	0.000
10	7.5	13.311	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	5.394	7.190	0.727	0.000
10	7.7	11.272	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	7.929	2.721	0.622	0.000
10	7.9	5.548	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	3.971	1.281	0.295	0.000
10	8.1	11.678	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	9.735	1.344	0.599	0.000
10	8.3	3.544	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	3.363	0.005	0.177	0.000

Principal Sources (faults, subduction, random seismicity having > 3% contribution

UC33brAvg_FM31:

Percent Contributed: 37.33

Distance (km): 13.801677

Magnitude: 7.6506542

Epsilon (mean values): 1.6054843

San Andreas (Coachella) rev [3]:

Percent Contributed: 31.53

Distance (km): 11.808984

Magnitude: 7.6442445

Epsilon (mean values): 1.5198782

Azimuth: 45.77243

Latitude: 33.659291

Longitude: -116.08815

San Jacinto (Clark) rev [2]:

Percent Contributed: 2.16

Distance (km): 24.959956

Magnitude: 7.8149043

Epsilon (mean values): 2.0660243

Azimuth: 206.01308

Latitude: 33.38395

Longitude: -116.29718

San Jacinto (Coyote Creek) [1]:

Percent Contributed: 1.57

Distance (km): 32.023487

Magnitude: 8.0259488

Epsilon (mean values): 2.1559329

Azimuth: 225.85202

Latitude: 33.38444

Longitude: -116.42703

UC33brAvg_FM32:

Percent Contributed: 37.18

Distance (km): 13.787704

Magnitude: 7.6444527

Epsilon (mean values): 1.6081289

San Andreas (Coachella) rev [3]:

Percent Contributed: 31.33

Distance (km): 11.808984

Magnitude: 7.6391584

Epsilon (mean values): 1.5228668

Azimuth: 45.77243

Latitude: 33.659291

Longitude: -116.08815

San Jacinto (Clark) rev [2]:

Percent Contributed: 2.09

Distance (km): 24.959956

50	7.3	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
50	7.5	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
50	7.7	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
50	7.9	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
30	5.7	0.001	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.001
30	5.9	0.010	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.010
30	6.1	0.072	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.072
30	6.3	0.079	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.012	0.068
30	6.5	0.041	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.007	0.034
30	6.7	0.033	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.011	0.022
30	6.9	0.045	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.021	0.024
30	7.1	0.045	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.003	0.027	0.016
30	7.3	0.035	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.003	0.024	0.008
30	7.5	0.014	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.002	0.010	0.002
30	7.7	0.002	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.001	0.001	0.000
30	7.9	0.001	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
10	5.1	2.940	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.930	0.600	0.410
10	5.3	3.346	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.567	1.609	0.716	0.453
10	5.5	3.855	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.320	1.217	0.876	0.443
10	5.7	3.396	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.052	1.074	0.936	0.335
10	5.9	2.379	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.832	0.713	0.659	0.175
10	6.1	2.544	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.373	0.476	0.901	0.606	0.187
10	6.3	2.122	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.253	0.503	0.948	0.342	0.075
10	6.5	1.690	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.249	0.516	0.718	0.182	0.025
10	6.7	1.282	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.232	0.513	0.378	0.146	0.013
10	6.9	0.826	0.000	0.000	0.000	0.000	0.000	0.000	0.008	0.147	0.341	0.238	0.087	0.005
10	7.1	0.459	0.000	0.000	0.000	0.000	0.000	0.000	0.010	0.070	0.216	0.125	0.036	0.002
10	7.3	0.205	0.000	0.000	0.000	0.000	0.000	0.000	0.004	0.033	0.099	0.056	0.012	0.001
10	7.5	0.054	0.000	0.000	0.000	0.000	0.000	0.000	0.002	0.011	0.024	0.015	0.002	0.000
10	7.7	0.006	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.002	0.002	0.001	0.000	0.000
10	7.9	0.002	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.001	0.001	0.000	0.000	0.000

Principal Sources (faults, subduction, random seismicity having > 3% contribution

UC33brAvg_FM31 (opt):

Percent Contributed: 12.75

Distance (km): 8.5983886

Magnitude: 5.8530399

Epsilon (mean values): 1.7608723

PointSourceFinite: -116.180, 33.608:

Percent Contributed: 3.01

Distance (km): 5.6038696

Magnitude: 5.6468266

Epsilon (mean values): 1.4461112

Azimuth: 0

Latitude: 33.607761

Longitude: -116.17955

PointSourceFinite: -116.180, 33.608:

Percent Contributed: 2.98

Distance (km): 5.6038696

Magnitude: 5.6468266

Epsilon (mean values): 1.4461112

Azimuth: 0

Latitude: 33.607761

Longitude: -116.17955

PointSourceFinite: -116.180, 33.671:

Percent Contributed: 1.02

Distance (km): 9.448142

Magnitude: 6.0312322

Epsilon (mean values): 1.8666668

Azimuth: 0

Latitude: 33.670713

Longitude: -116.17955

PointSourceFinite: -116.180, 33.671:

Percent Contributed: 1

Distance (km): 9.448142

Magnitude: 6.0312322

Epsilon (mean values): 1.8666668

Azimuth: 0

Latitude: 33.670713

Longitude: -116.17955

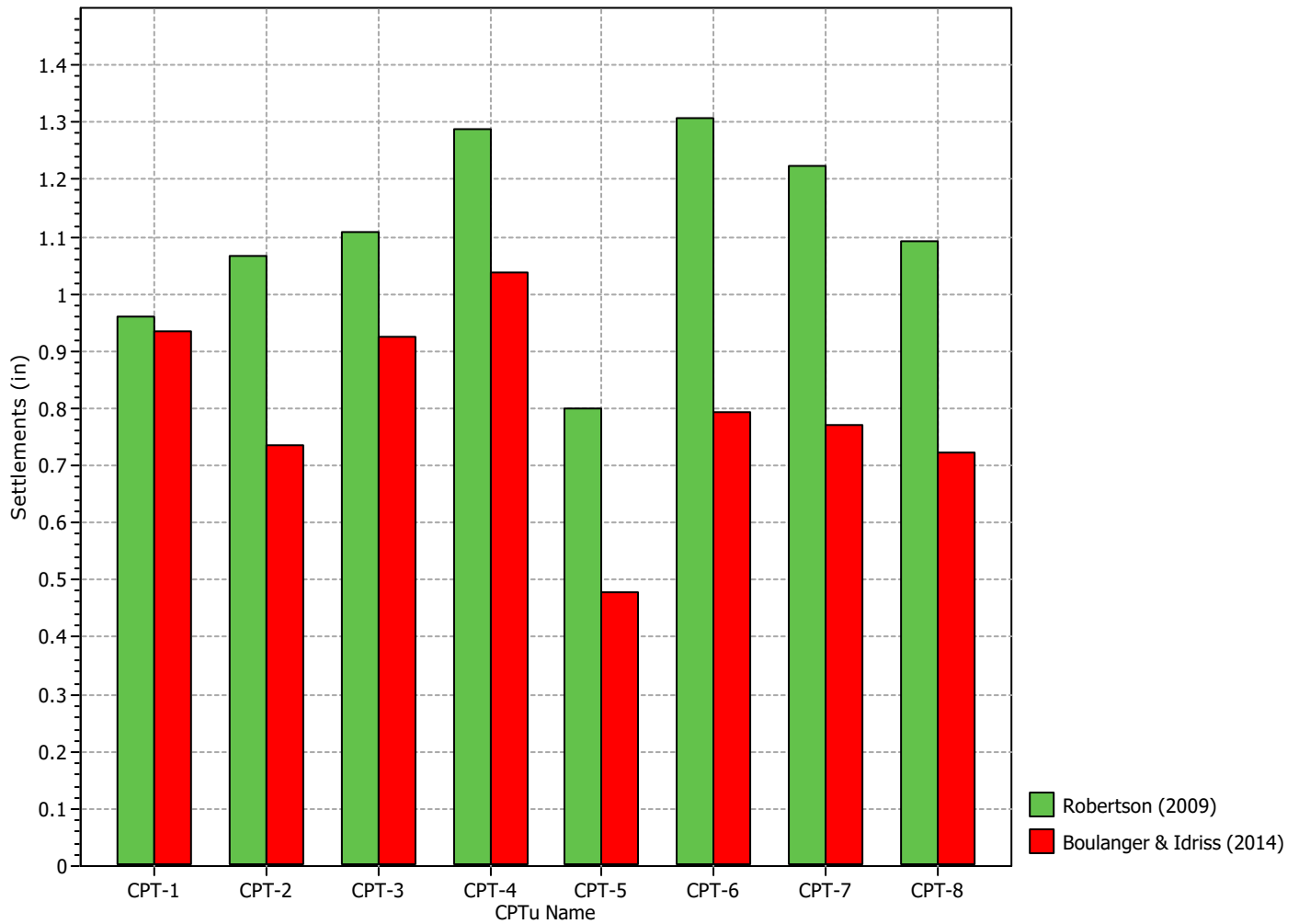
UC33brAvg_FM32 (opt):

Percent Contributed: 12.74
Distance (km): 8.5986253
Magnitude: 5.8525001
Epsilon (mean values): 1.7610821
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Percent Contributed: 3.01
Distance (km): 5.6040812
Magnitude: 5.6464357
Epsilon (mean values): 1.4462969
Azimuth: 0
Latitude: 33.607761
Longitude: -116.17955
PointSourceFinite: -116.180, 33.608:
Percent Contributed: 2.98
Distance (km): 5.6040812
Magnitude: 5.6464357
Epsilon (mean values): 1.4462969
Azimuth: 0
Latitude: 33.607761
Longitude: -116.17955
PointSourceFinite: -116.180, 33.671:
Percent Contributed: 1.02
Distance (km): 9.4495831
Magnitude: 6.0306167
Epsilon (mean values): 1.8671345
Azimuth: 0
Latitude: 33.670713
Longitude: -116.17955
PointSourceFinite: -116.180, 33.671:
Percent Contributed: 1
Distance (km): 9.4495831
Magnitude: 6.0306167
Epsilon (mean values): 1.8671345
Azimuth: 0
Latitude: 33.670713
Longitude: -116.17955

APPENDIX E

LIQUEFACTION ANALYSIS

Overall Parametric Assessment Method



:: CPT main liquefaction parameters details ::

CPT Name	Earthquake Mag.	Earthquake Accel.	GWT in situ (ft)	GWT earthq. (ft)
CPT-1	7.34	0.74	8.00	8.00
CPT-2	7.34	0.74	8.00	8.00
CPT-3	7.34	0.74	8.00	8.00
CPT-4	7.34	0.74	8.00	8.00
CPT-5	7.34	0.74	8.00	8.00
CPT-6	7.34	0.74	8.00	8.00
CPT-7	7.34	0.74	8.00	8.00
CPT-8	7.34	0.74	8.00	8.00

Project title : 21-483 Equestrian Estates

Location : Avenue 64 at Harrison Street, Thermal California

Overall vertical settlements report

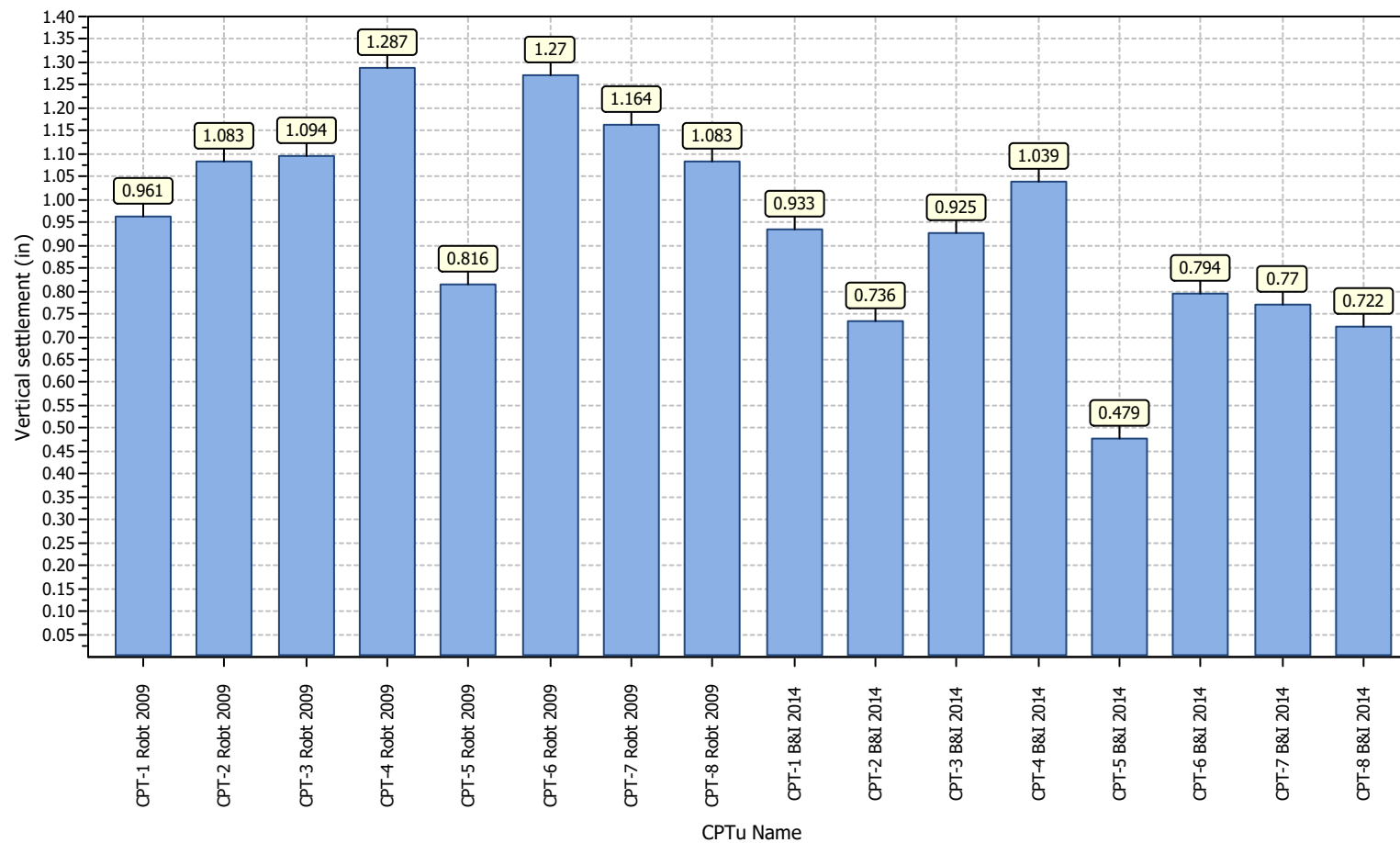


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LIQUEFACTION ANALYSIS REPORT

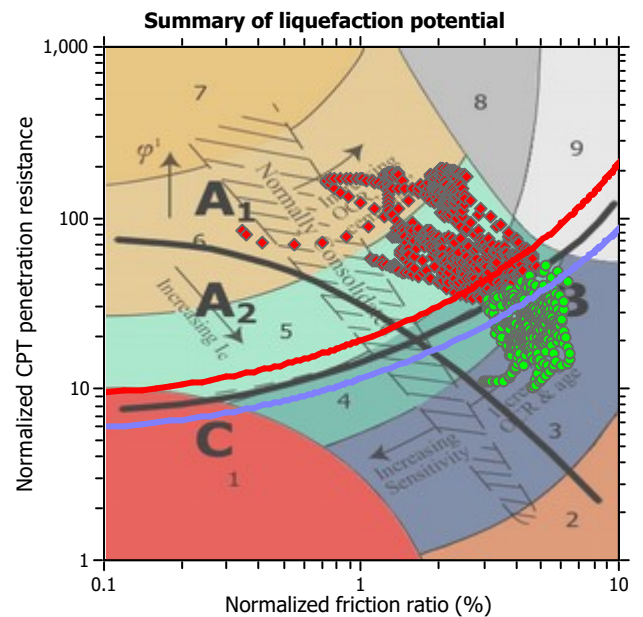
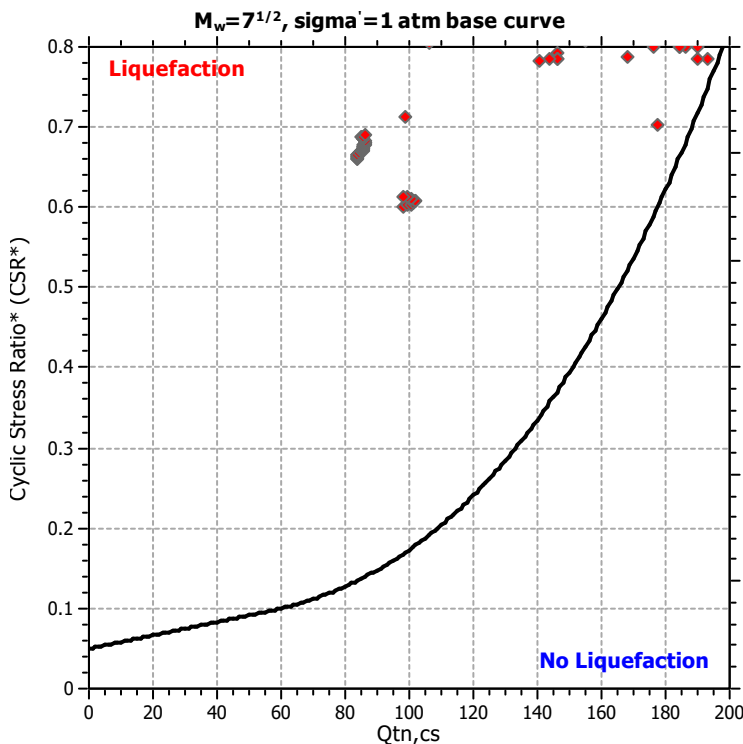
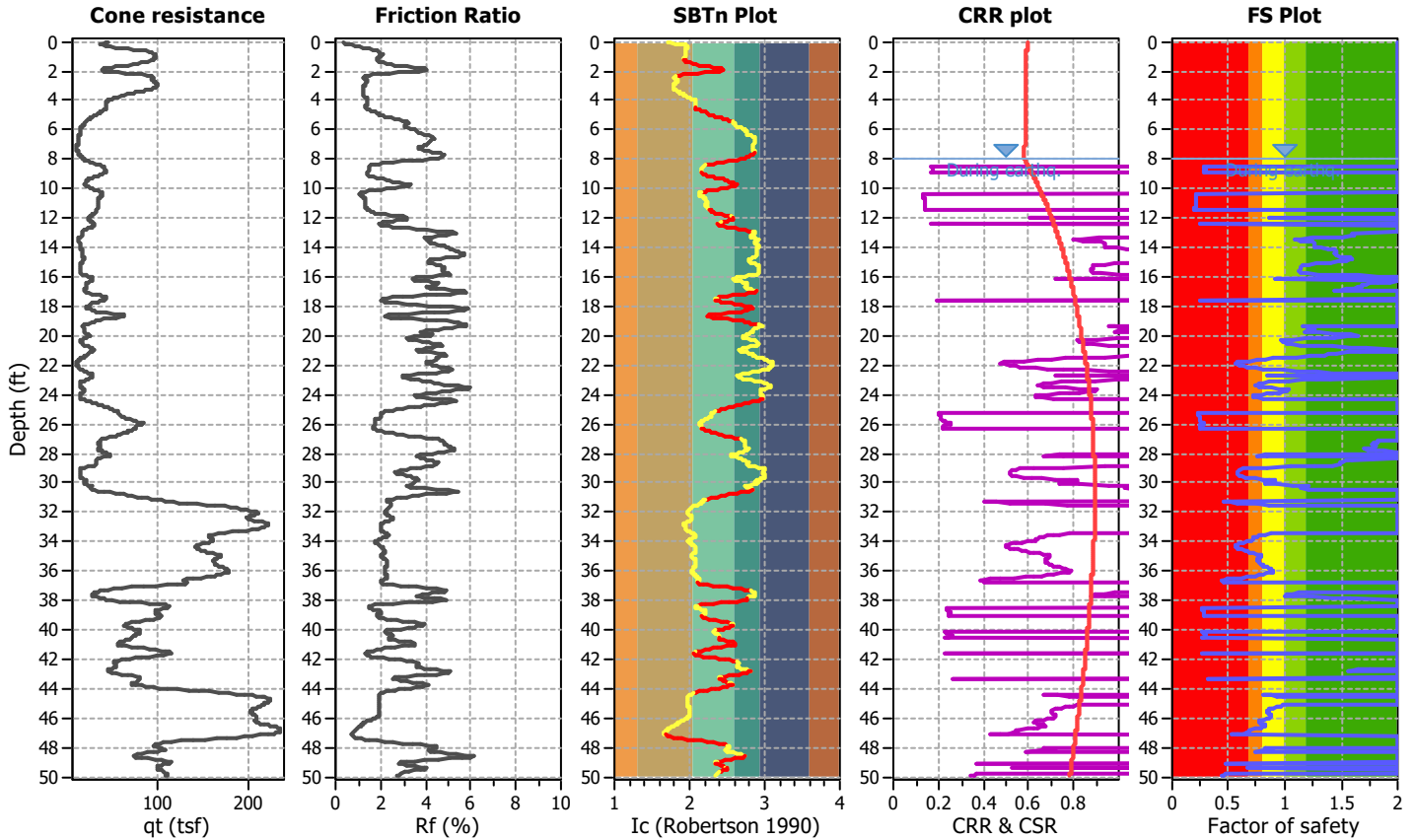
Project title : 21-483 Equestrian Estates

Location : Avenue 64 at Harrison Street, Thermal California

CPT file : CPT-1 Robt 2009

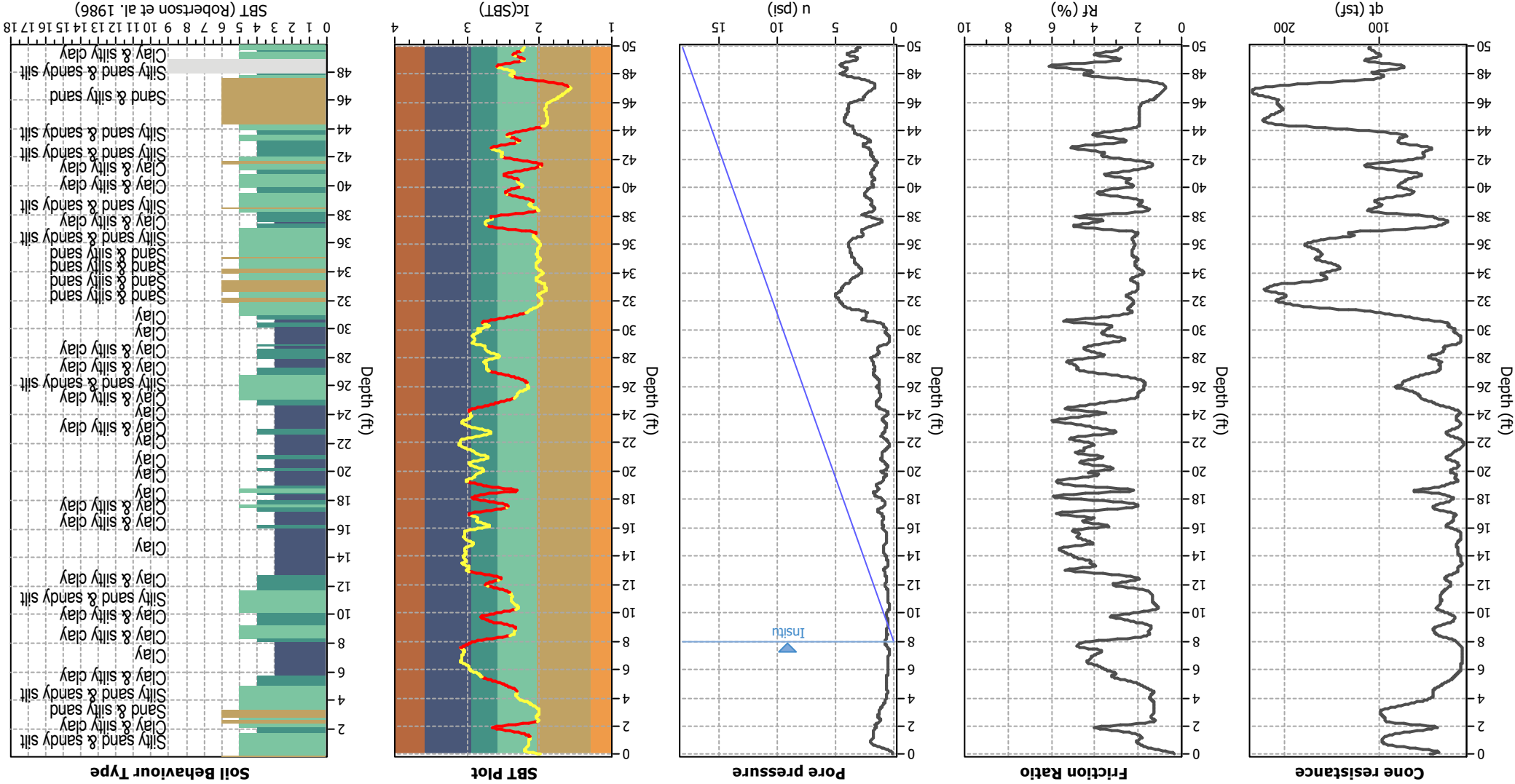
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Analysis method:	Robertson (2009)	G.W.T. (in-situ):	8.00 ft	Use fill:	No	Clay like behavior	
Fines correction method:	Robertson (2009)	G.W.T. (earthq.):	8.00 ft	Fill height:	N/A	applied:	All soils
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude M_w :	7.34	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.74	Unit weight calculation:	Based on SBT	K_o applied:	No	MSF method:	Method based



Zone A₁: Cyclic liquefaction likely depending on size and duration of cyclic loading
 Zone A₂: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
 Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
 Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



Input parameters and analysis data

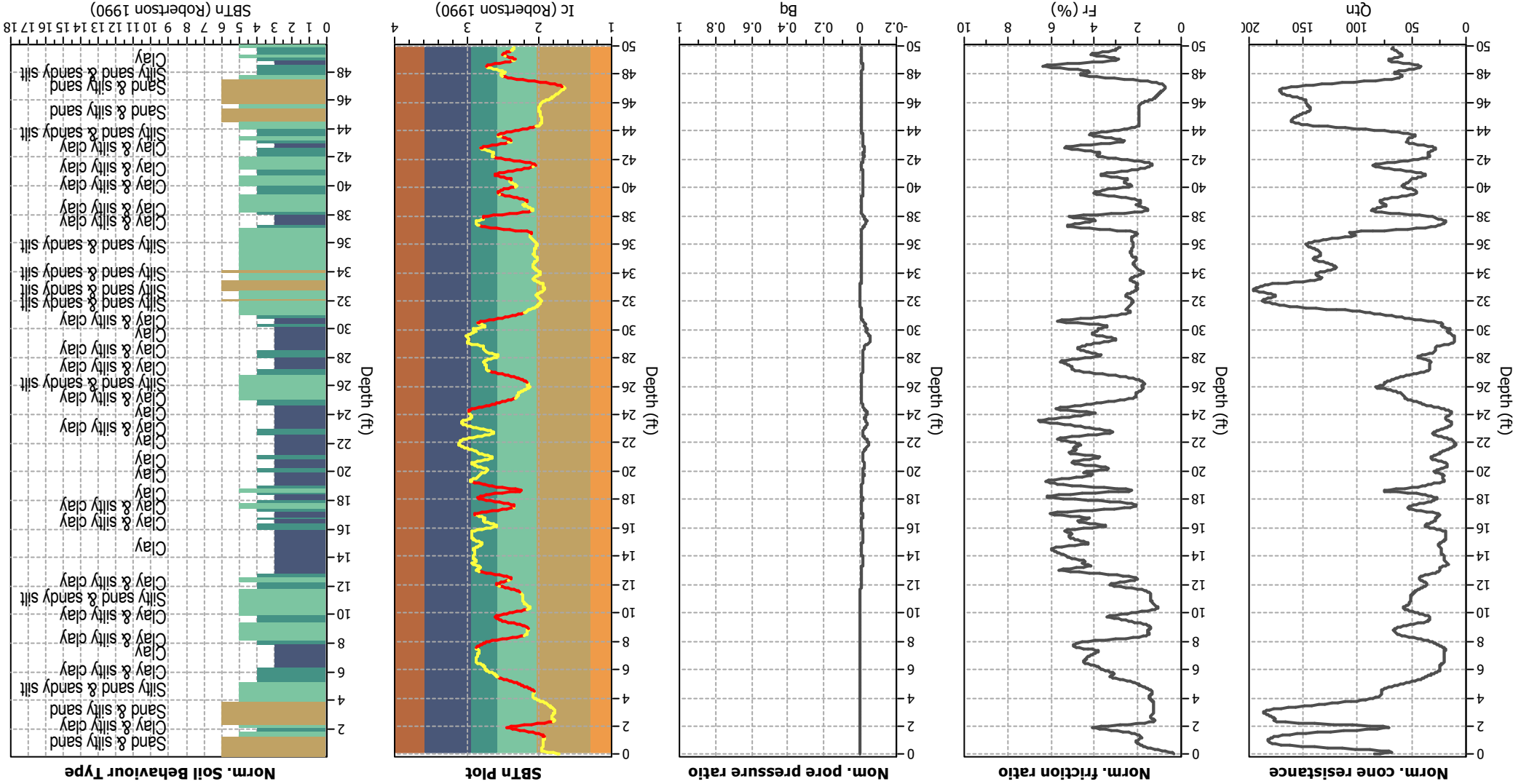
Analysis method: Robertson (2009)
Fines correction method: Robertson (2009)
Points to test: Based on Ic value
Earthquake magnitude M_w : 7.34
Peak ground acceleration: 0.74
Depth to water table (insitu): 8.00 ft

Fill height: N/A
Use fill: No
Unit weight calculation: Based on SBT
Ic cut-off value: 2.60
Average results interval: 3
Depth to water table (earthq.): 8.00 ft
Fill weight: N/A
Transition detect. applied: Yes
 K_0 applied: No
Clay like behavior applied: All soils
Limit depth applied: No
Limit depth: N/A

SBT legend

SBT	Soil Description
1	Sensitive fine grained
2	Organic material
3	Clay to silty clay
4	Clayey silt to silty
5	Silty sand to sandy silt
6	Clean sand to silty sand
7	Gravelly sand to sand
8	Very stiff sand to
9	Very stiff fine grained

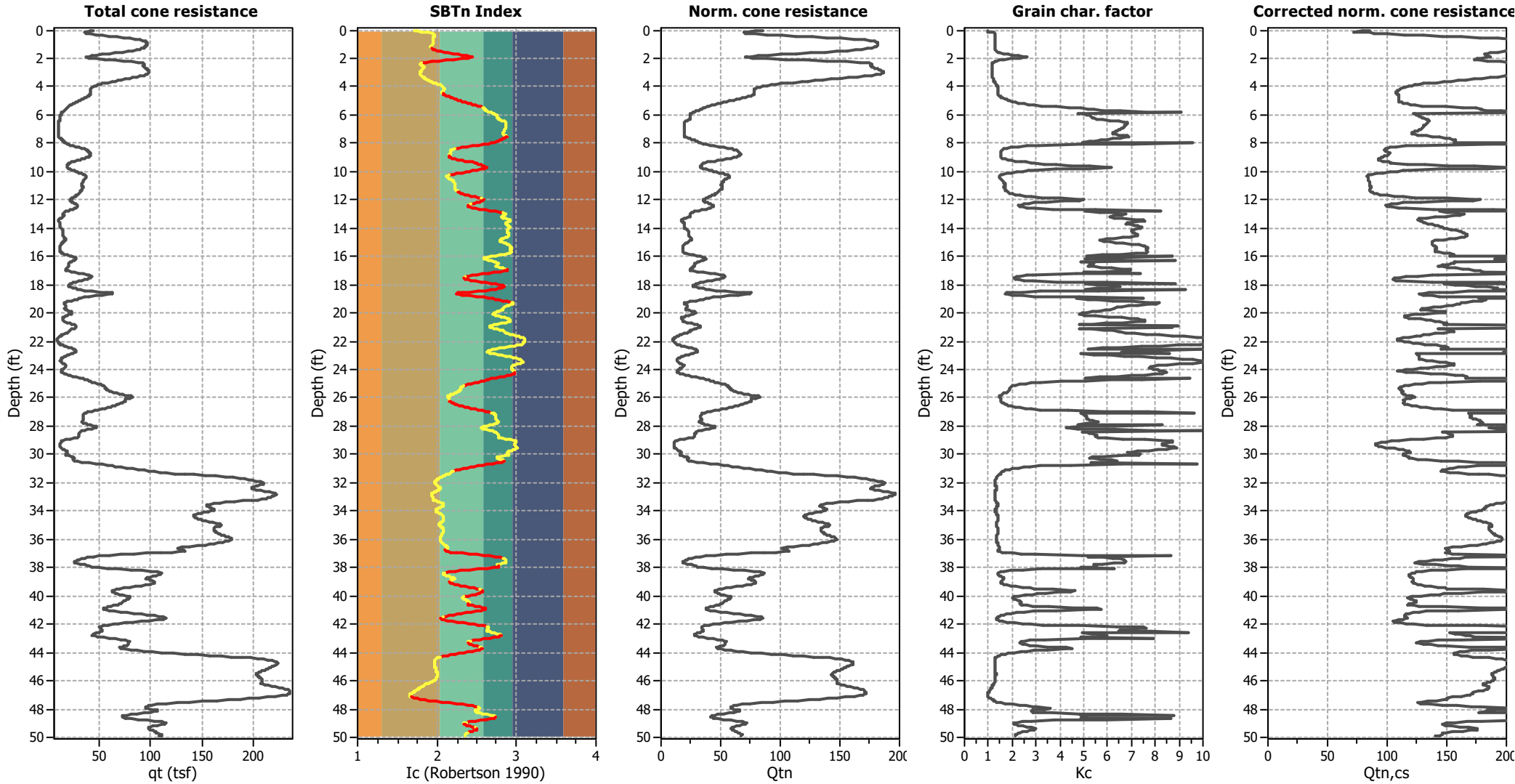
CPT basic interpretation plots (normalized)



Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (erthq.):	8.00 ft
Fines correction method:	Robertson (2009)	Average results interval:	3
Points to test:	Based on Ic value	Ic cut-off value:	2.60
Earthquake magnitude M_w :	7.34	Unit weight calculation:	Based on SBT
Peak ground acceleration:	0.74	Use fill:	No
Depth to water table (instu):	8.00 ft	Fill height:	N/A
		Limit depth:	N/A
		Clay like behavior applied:	No
		Limit depth applied:	No
		Transition detect. applied:	Yes
		K_g applied:	No
		All soils:	No
		Fill weight:	N/A

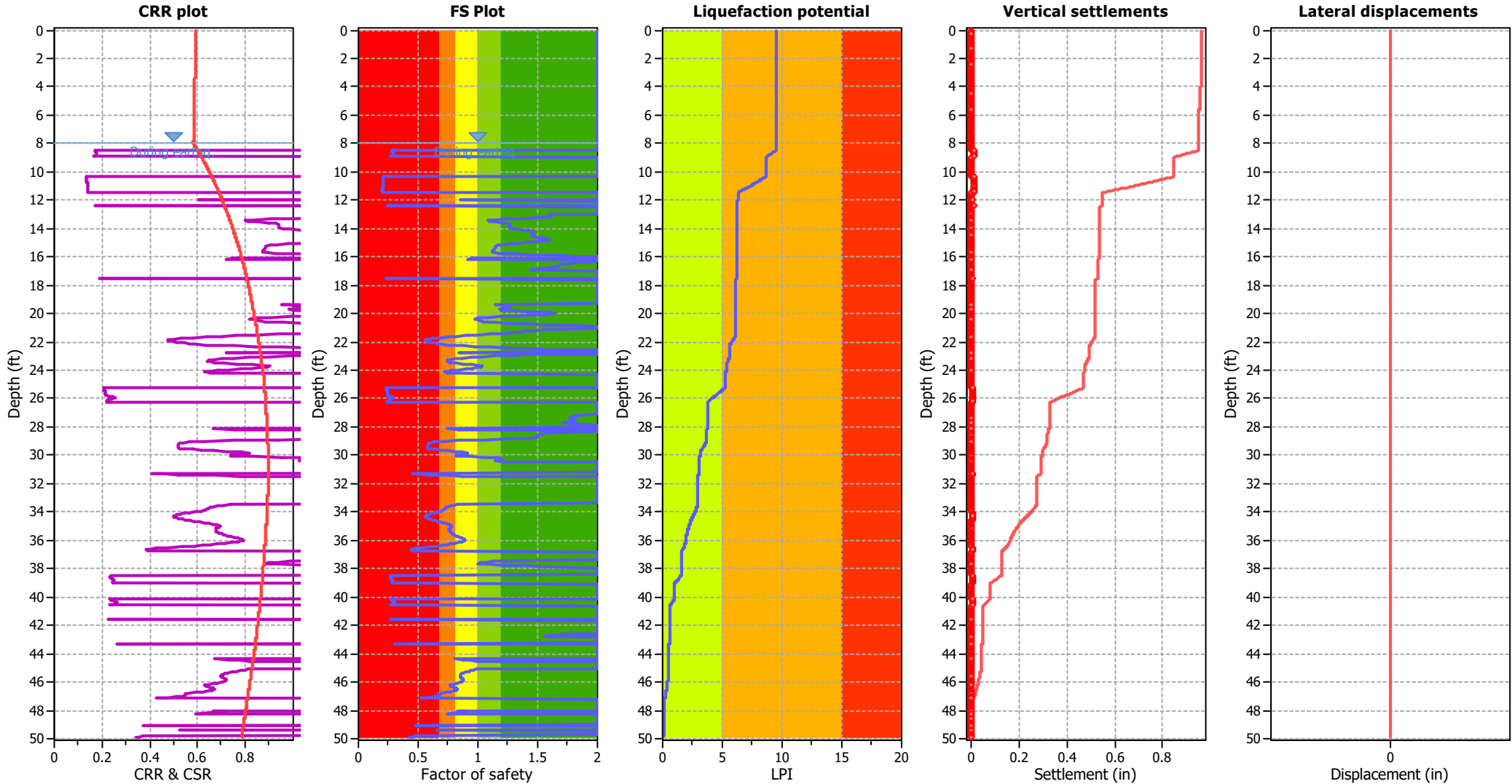
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	No
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	No
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

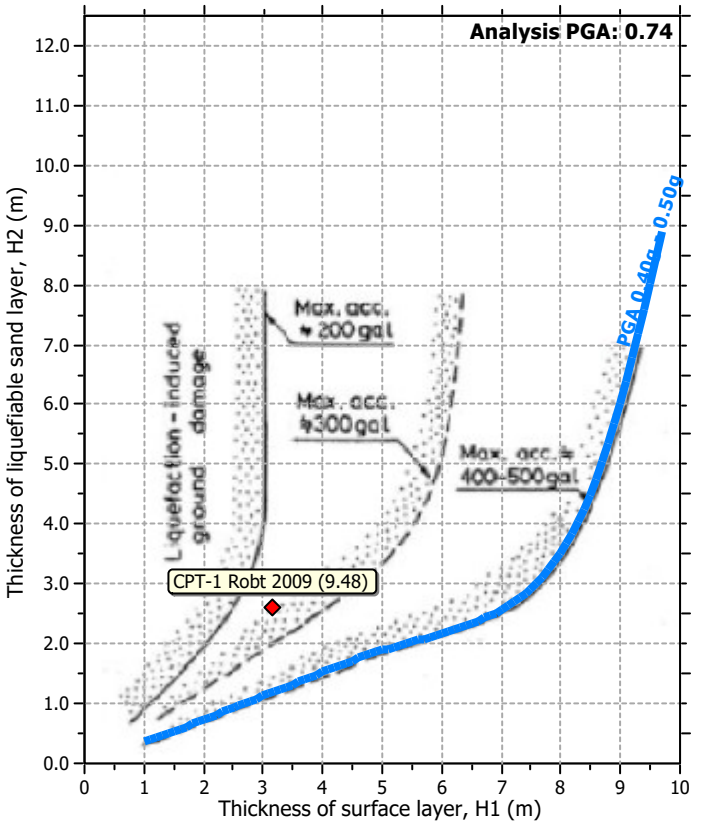
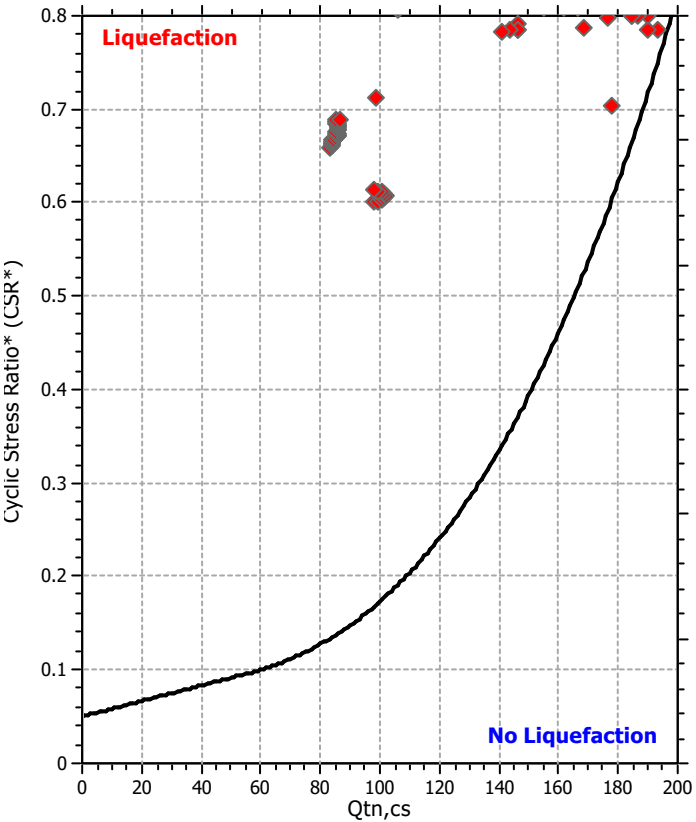
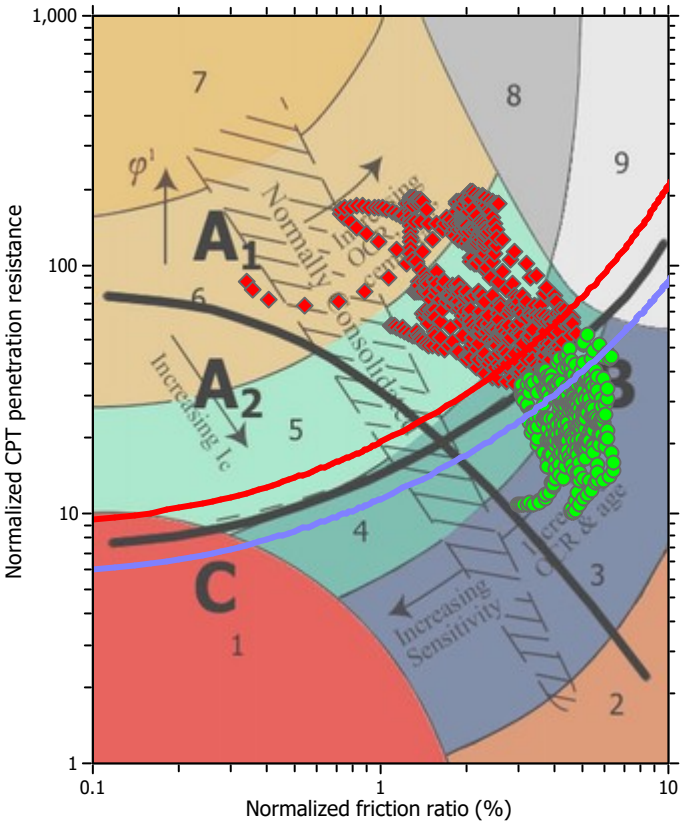
F.S. color scheme

- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

LPI color scheme

- Very high risk
- High risk
- Low risk

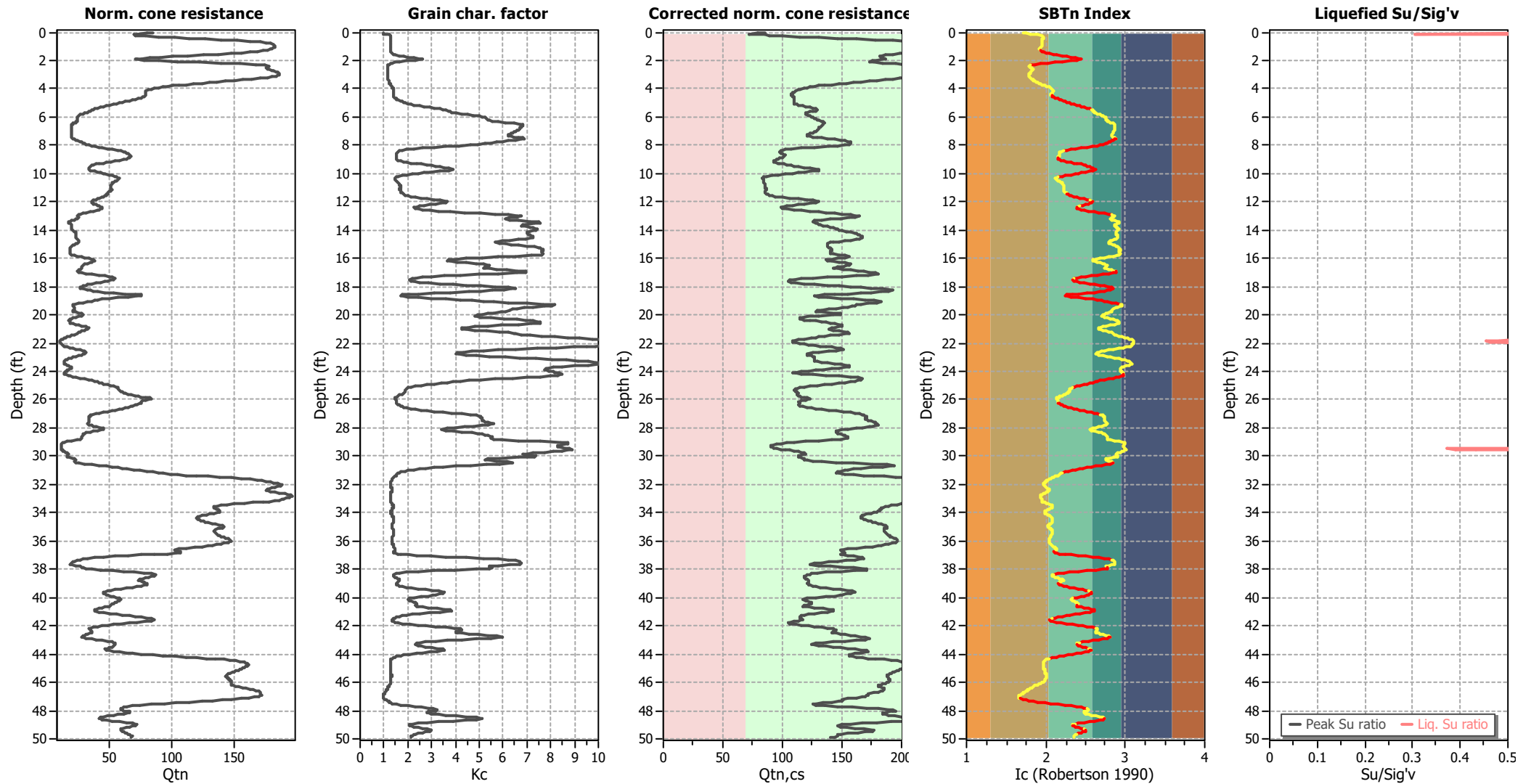
Liquefaction analysis summary plots



Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	No
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

Check for strength loss plots (Robertson (2010))



Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	No
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

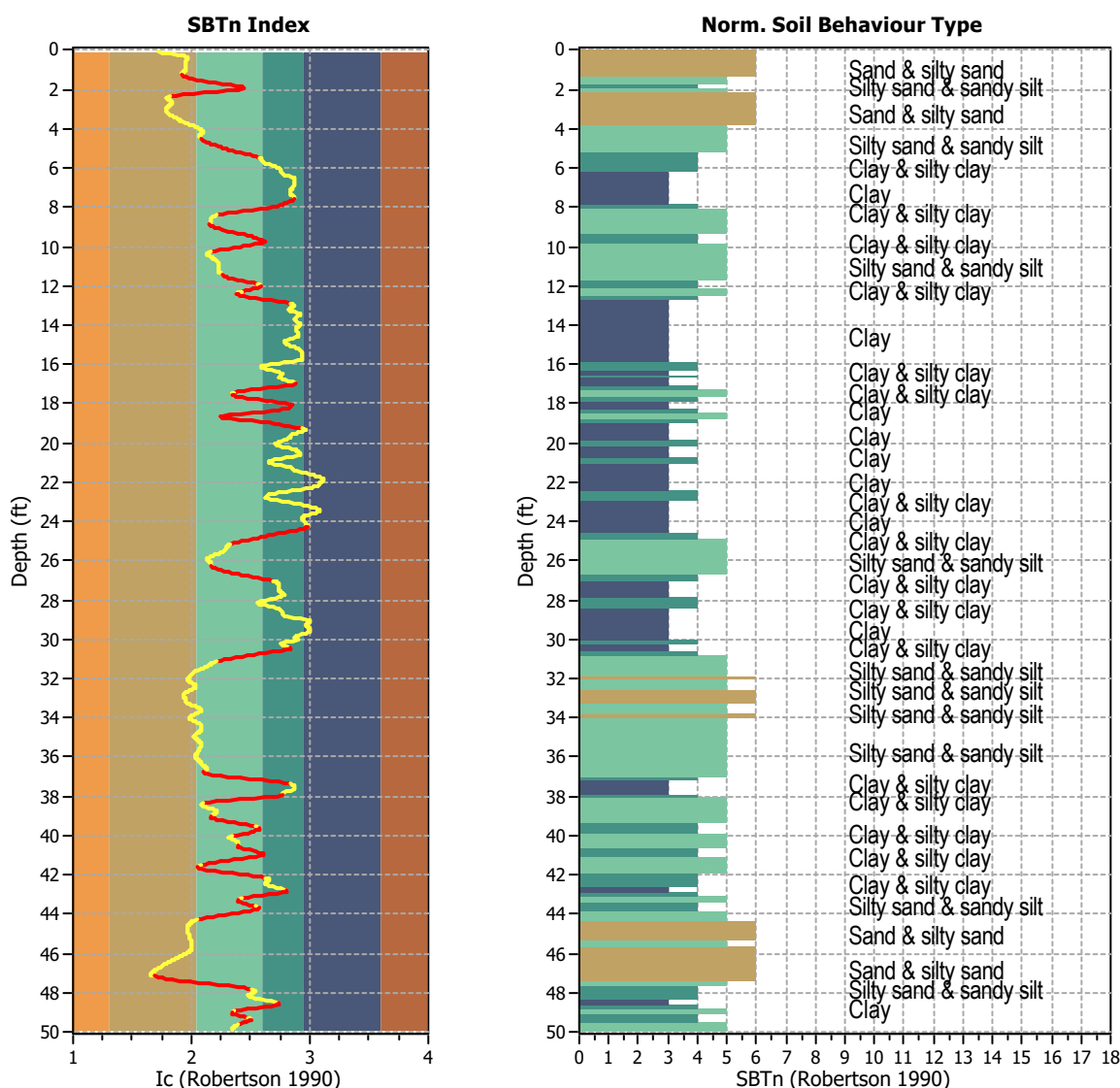
TRANSITION LAYER DETECTION ALGORITHM REPORT

Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vice-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between $1.80 < I_c < 3.0$) and a rate of change of I_c . Transitions typically occur when the rate of change of I_c is fast (i.e. ΔI_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties

I_c minimum check value: 1.70
 I_c maximum check value: 3.00
 I_c change ratio value: 0.0250
 Minimum number of points in layer: 4

General statistics

Total points in CPT file: 998
 Total points excluded: 354
 Exclusion percentage: 35.47%
 Number of layers detected: 30

Transition layer No	Number of points	Depth	SBT _n number	SBT _n description
Transition layer 1	13	Start depth: 1.30 (ft)	6	Sand & silty sand
		End depth: 1.90 (ft)	4	Clay & silty clay
Transition layer 2	10	Start depth: 1.95 (ft)	4	Clay & silty clay
		End depth: 2.40 (ft)	6	Sand & silty sand
Transition layer 3	20	Start depth: 4.55 (ft)	5	Silty sand & sandy silt
		End depth: 5.50 (ft)	4	Clay & silty clay
Transition layer 4	18	Start depth: 7.60 (ft)	3	Clay
		End depth: 8.45 (ft)	5	Silty sand & sandy silt
Transition layer 5	16	Start depth: 8.95 (ft)	5	Silty sand & sandy silt
		End depth: 9.70 (ft)	4	Clay & silty clay
Transition layer 6	12	Start depth: 9.75 (ft)	4	Clay & silty clay
		End depth: 10.30 (ft)	5	Silty sand & sandy silt
Transition layer 7	10	Start depth: 11.50 (ft)	5	Silty sand & sandy silt
		End depth: 11.95 (ft)	4	Clay & silty clay
Transition layer 8	7	Start depth: 12.05 (ft)	4	Clay & silty clay
		End depth: 12.35 (ft)	5	Silty sand & sandy silt
Transition layer 9	11	Start depth: 12.45 (ft)	5	Silty sand & sandy silt
		End depth: 12.95 (ft)	3	Clay
Transition layer 10	11	Start depth: 17.00 (ft)	3	Clay
		End depth: 17.50 (ft)	5	Silty sand & sandy silt
Transition layer 11	11	Start depth: 17.60 (ft)	5	Silty sand & sandy silt
		End depth: 18.10 (ft)	3	Clay
Transition layer 12	11	Start depth: 18.15 (ft)	3	Clay
		End depth: 18.65 (ft)	5	Silty sand & sandy silt
Transition layer 13	13	Start depth: 18.70 (ft)	5	Silty sand & sandy silt
		End depth: 19.30 (ft)	3	Clay
Transition layer 14	19	Start depth: 24.30 (ft)	3	Clay
		End depth: 25.20 (ft)	5	Silty sand & sandy silt
Transition layer 15	17	Start depth: 26.30 (ft)	5	Silty sand & sandy silt
		End depth: 27.10 (ft)	4	Clay & silty clay
Transition layer 16	15	Start depth: 30.50 (ft)	3	Clay
		End depth: 31.20 (ft)	5	Silty sand & sandy silt
Transition layer 17	13	Start depth: 36.80 (ft)	5	Silty sand & sandy silt
		End depth: 37.40 (ft)	3	Clay
Transition layer 18	10	Start depth: 37.95 (ft)	3	Clay
		End depth: 38.40 (ft)	5	Silty sand & sandy silt
Transition layer 19	11	Start depth: 39.10 (ft)	5	Silty sand & sandy silt
		End depth: 39.60 (ft)	4	Clay & silty clay
Transition layer 20	9	Start depth: 39.70 (ft)	4	Clay & silty clay
		End depth: 40.10 (ft)	5	Silty sand & sandy silt
Transition layer 21	7	Start depth: 40.60 (ft)	5	Silty sand & sandy silt
		End depth: 40.90 (ft)	4	Clay & silty clay
Transition layer 22	13	Start depth: 40.95 (ft)	4	Clay & silty clay
		End depth: 41.55 (ft)	5	Silty sand & sandy silt
Transition layer 23	12	Start depth: 41.65 (ft)	5	Silty sand & sandy silt
		End depth: 42.20 (ft)	4	Clay & silty clay

Transition layer No	Number of points	Depth	SBT _n number	SBT _n description
Transition layer 24	9	Start depth: 42.85 (ft)	3	Clay
		End depth: 43.25 (ft)	5	Silty sand & sandy silt
Transition layer 25	7	Start depth: 43.35 (ft)	5	Silty sand & sandy silt
		End depth: 43.65 (ft)	4	Clay & silty clay
Transition layer 26	13	Start depth: 43.75 (ft)	4	Clay & silty clay
		End depth: 44.35 (ft)	5	Silty sand & sandy silt
Transition layer 27	15	Start depth: 47.20 (ft)	6	Sand & silty sand
		End depth: 47.90 (ft)	4	Clay & silty clay
Transition layer 28	9	Start depth: 48.60 (ft)	3	Clay
		End depth: 49.00 (ft)	5	Silty sand & sandy silt
Transition layer 29	6	Start depth: 49.10 (ft)	5	Silty sand & sandy silt
		End depth: 49.35 (ft)	4	Clay & silty clay
Transition layer 30	6	Start depth: 49.45 (ft)	4	Clay & silty clay
		End depth: 49.70 (ft)	5	Silty sand & sandy silt

Start depth: Depth where the transition layer begins

End depth: Depth where the transition layer ends

:: Field input data ::						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1	0.05	46.61	0.17	0.17	5.00	105.92
2	0.10	41.73	0.12	0.12	5.00	105.56
3	0.15	38.20	0.16	0.16	5.00	105.58
4	0.20	34.72	0.19	0.19	10.20	107.29
5	0.25	36.71	0.26	0.26	11.44	109.44
6	0.30	41.02	0.36	0.36	11.84	112.03
7	0.35	47.26	0.49	0.49	12.02	114.59
8	0.40	53.15	0.65	0.65	11.97	116.94
9	0.45	60.84	0.84	0.84	11.99	118.98
10	0.50	66.84	1.03	1.03	11.86	120.73
11	0.55	74.08	1.22	1.22	11.79	122.20
12	0.60	80.26	1.41	1.41	11.63	123.46
13	0.65	86.58	1.59	1.59	11.54	124.46
14	0.70	90.81	1.73	1.73	11.49	125.22
15	0.75	93.59	1.84	1.84	11.52	125.73
16	0.80	95.01	1.91	1.91	11.61	126.08
17	0.85	95.71	1.96	1.96	11.69	126.29
18	0.90	96.26	1.99	1.99	11.76	126.42
19	0.95	96.40	2.00	2.00	11.71	126.42
20	1.00	96.47	1.96	1.96	11.59	126.32
21	1.05	96.35	1.91	1.91	11.36	126.11
22	1.10	96.08	1.83	1.83	11.15	125.87
23	1.15	95.50	1.78	1.78	10.95	125.61
24	1.20	94.73	1.73	1.73	10.91	125.45
25	1.25	93.78	1.73	1.73	11.01	125.33
26	1.30	91.81	1.72	1.72	11.31	125.31
27	1.35	89.77	1.74	1.74	11.73	125.23
28	1.40	86.25	1.73	1.73	12.31	125.19
29	1.45	82.97	1.75	1.75	13.09	125.13
30	1.50	78.61	1.77	1.77	14.11	125.06
31	1.55	72.91	1.77	1.77	15.47	124.95
32	1.60	66.87	1.80	1.80	17.13	124.66
33	1.65	59.23	1.73	1.73	19.09	124.35
34	1.70	53.45	1.73	1.73	21.23	123.87
35	1.75	47.26	1.65	1.65	23.42	123.51
36	1.80	43.36	1.66	1.66	25.48	123.03
37	1.85	39.40	1.58	1.58	27.19	122.67
38	1.90	37.27	1.54	1.54	28.18	122.23
39	1.95	36.39	1.47	1.47	27.88	122.19
40	2.00	40.23	1.54	1.54	26.02	122.36
41	2.05	45.90	1.54	1.54	22.96	122.99
42	2.10	55.81	1.63	1.63	19.51	123.39
43	2.15	64.60	1.55	1.55	16.31	123.69
44	2.20	73.88	1.49	1.49	13.49	123.64
45	2.25	82.86	1.40	1.40	11.21	123.41
46	2.30	89.17	1.27	1.27	9.50	123.05
47	2.35	93.51	1.20	1.20	8.41	122.64
48	2.40	94.40	1.14	1.14	7.96	122.43

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
49	2.45	93.84	1.15	1.15	7.93	122.39
50	2.50	93.33	1.18	1.18	8.20	122.59
51	2.55	92.98	1.24	1.24	8.50	122.89
52	2.60	93.48	1.29	1.29	8.75	123.19
53	2.65	94.13	1.33	1.33	8.83	123.41
54	2.70	95.28	1.34	1.34	8.76	123.49
55	2.75	96.16	1.33	1.33	8.59	123.49
56	2.80	97.09	1.31	1.31	8.40	123.43
57	2.85	97.81	1.30	1.30	8.21	123.35
58	2.90	98.36	1.28	1.28	8.04	123.27
59	2.95	98.74	1.26	1.26	7.91	123.18
60	3.00	98.69	1.25	1.25	7.85	123.10
61	3.05	98.31	1.24	1.24	7.84	123.02
62	3.10	97.40	1.23	1.23	7.89	122.93
63	3.15	96.27	1.21	1.21	7.99	122.78
64	3.20	93.65	1.18	1.18	8.13	122.56
65	3.25	91.01	1.15	1.15	8.35	122.22
66	3.30	86.75	1.09	1.09	8.60	121.84
67	3.35	83.29	1.05	1.05	8.91	121.39
68	3.40	79.32	1.00	1.00	9.23	120.94
69	3.45	75.50	0.95	0.95	9.57	120.47
70	3.50	72.09	0.91	0.91	9.91	120.00
71	3.55	68.64	0.87	0.87	10.25	119.56
72	3.60	65.87	0.83	0.83	10.62	119.09
73	3.65	62.43	0.79	0.79	11.00	118.61
74	3.70	59.25	0.75	0.75	11.48	118.12
75	3.75	55.87	0.72	0.72	12.01	117.70
76	3.80	53.31	0.70	0.70	12.64	117.43
77	3.85	51.22	0.70	0.70	13.28	117.22
78	3.90	48.90	0.69	0.69	13.90	117.06
79	3.95	47.23	0.68	0.68	14.43	116.80
80	4.00	45.38	0.66	0.66	14.83	116.52
81	4.05	44.01	0.64	0.64	15.17	116.21
82	4.10	42.79	0.62	0.62	15.42	115.96
83	4.15	42.03	0.61	0.61	15.56	115.75
84	4.20	41.69	0.60	0.60	15.57	115.60
85	4.25	41.69	0.59	0.59	15.43	115.43
86	4.30	41.69	0.57	0.57	15.22	115.24
87	4.35	41.69	0.55	0.55	14.96	115.02
88	4.40	41.69	0.54	0.54	14.83	114.90
89	4.45	41.69	0.54	0.54	14.83	114.90
90	4.50	41.69	0.55	0.55	15.08	115.09
91	4.55	41.51	0.58	0.58	15.45	115.33
92	4.60	41.14	0.60	0.60	15.99	115.57
93	4.65	40.22	0.62	0.62	16.57	115.71
94	4.70	39.19	0.63	0.63	17.27	115.75
95	4.75	37.70	0.63	0.63	18.05	115.77
96	4.80	36.46	0.64	0.64	18.93	115.75

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
97	4.85	34.91	0.64	0.64	19.81	115.72
98	4.90	33.65	0.65	0.65	20.64	115.58
99	4.95	32.20	0.63	0.63	21.42	115.38
100	5.00	30.82	0.62	0.62	22.25	115.17
101	5.05	29.53	0.62	0.62	23.22	114.98
102	5.10	28.00	0.61	0.61	24.39	114.90
103	5.15	26.77	0.63	0.63	25.70	114.79
104	5.20	25.24	0.62	0.62	27.15	114.75
105	5.25	23.95	0.63	0.63	28.68	114.64
106	5.30	22.59	0.63	0.63	30.23	114.56
107	5.35	21.49	0.64	0.64	31.64	114.45
108	5.40	20.65	0.64	0.64	32.88	114.35
109	5.45	19.88	0.63	0.63	33.85	114.20
110	5.50	19.26	0.62	0.62	34.61	113.94
111	5.55	18.51	0.59	0.59	35.04	113.61
112	5.60	18.15	0.57	0.57	35.25	113.23
113	5.65	17.78	0.55	0.55	35.42	112.80
114	5.70	17.02	0.51	0.51	35.88	112.37
115	5.75	16.27	0.49	0.49	36.81	111.86
116	5.80	15.11	0.47	0.47	38.05	111.45
117	5.85	14.40	0.46	0.46	39.48	111.08
118	5.90	13.70	0.45	0.45	40.77	110.93
119	5.95	13.34	0.46	0.46	41.86	110.86
120	6.00	13.10	0.46	0.46	42.61	110.93
121	6.05	13.10	0.47	0.47	43.06	111.02
122	6.10	13.10	0.48	0.48	43.30	111.13
123	6.15	13.10	0.48	0.48	43.49	111.22
124	6.20	13.10	0.49	0.49	43.72	111.32
125	6.25	13.10	0.50	0.50	44.03	111.46
126	6.30	13.10	0.51	0.51	44.58	111.60
127	6.35	12.87	0.52	0.52	45.58	111.56
128	6.40	12.10	0.50	0.50	46.99	111.36
129	6.45	11.47	0.49	0.49	48.67	110.96
130	6.50	10.74	0.47	0.47	49.85	110.70
131	6.55	10.72	0.47	0.47	50.43	110.50
132	6.60	10.72	0.47	0.47	50.37	110.46
133	6.65	10.72	0.46	0.46	50.18	110.37
134	6.70	10.72	0.45	0.45	49.99	110.29
135	6.75	10.72	0.45	0.45	49.85	110.23
136	6.80	10.72	0.45	0.45	49.78	110.19
137	6.85	10.72	0.45	0.45	49.73	110.17
138	6.90	10.72	0.45	0.45	49.62	110.11
139	6.95	10.72	0.44	0.44	49.43	110.03
140	7.00	10.72	0.43	0.43	49.16	109.91
141	7.05	10.72	0.42	0.42	48.89	109.79
142	7.10	10.72	0.42	0.42	48.57	109.64
143	7.15	10.72	0.41	0.41	48.25	109.50
144	7.20	10.72	0.40	0.40	47.90	109.34

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
145	7.25	10.72	0.39	0.39	47.72	109.25
146	7.30	10.72	0.39	0.39	47.73	109.25
147	7.35	10.72	0.40	0.40	48.14	109.43
148	7.40	10.72	0.42	0.42	48.77	109.70
149	7.45	10.72	0.44	0.44	49.63	110.07
150	7.50	10.72	0.46	0.46	50.35	110.47
151	7.55	10.87	0.49	0.49	50.55	111.08
152	7.60	11.65	0.55	0.55	50.08	111.82
153	7.65	12.44	0.60	0.60	48.92	112.71
154	7.70	13.57	0.66	0.66	47.66	113.41
155	7.75	14.27	0.68	0.68	46.42	113.98
156	7.80	14.94	0.71	0.71	45.35	114.39
157	7.85	15.69	0.74	0.74	44.29	114.73
158	7.90	16.31	0.75	0.75	43.15	115.02
159	7.95	17.08	0.77	0.77	41.72	115.18
160	8.00	17.93	0.76	0.76	39.95	115.28
161	8.05	19.02	0.75	0.75	37.48	115.27
162	8.10	20.72	0.72	0.72	34.60	115.18
163	8.15	22.44	0.67	0.67	31.38	114.98
164	8.20	25.12	0.62	0.62	28.27	114.74
165	8.25	27.59	0.59	0.59	25.24	114.65
166	8.30	31.03	0.58	0.58	22.88	114.68
167	8.35	33.67	0.57	0.57	20.95	114.84
168	8.40	36.38	0.58	0.58	19.58	114.90
169	8.45	37.83	0.56	0.56	18.70	115.02
170	8.50	38.90	0.57	0.57	18.22	115.11
171	8.55	39.68	0.58	0.58	18.06	115.35
172	8.60	40.30	0.60	0.60	17.99	115.60
173	8.65	41.04	0.62	0.62	17.95	115.81
174	8.70	41.40	0.63	0.63	17.85	115.92
175	8.75	41.69	0.63	0.63	17.74	115.90
176	8.80	41.69	0.61	0.61	17.59	115.77
177	8.85	41.56	0.60	0.60	17.46	115.56
178	8.90	41.17	0.58	0.58	17.44	115.29
179	8.95	40.14	0.56	0.56	17.61	114.99
180	9.00	38.72	0.54	0.54	18.12	114.64
181	9.05	36.25	0.52	0.52	18.93	114.30
182	9.10	34.02	0.51	0.51	20.07	113.93
183	9.15	31.32	0.50	0.50	21.39	113.67
184	9.20	29.34	0.50	0.50	22.89	113.39
185	9.25	27.07	0.49	0.49	24.50	113.21
186	9.30	25.10	0.50	0.50	26.22	112.94
187	9.35	23.13	0.49	0.49	27.99	112.74
188	9.40	21.64	0.49	0.49	29.60	112.57
189	9.45	20.74	0.49	0.49	30.91	112.58
190	9.50	20.35	0.51	0.51	31.92	112.72
191	9.55	20.03	0.53	0.53	32.85	112.93
192	9.60	19.67	0.55	0.55	33.94	113.25

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
193	9.65	19.33	0.59	0.59	35.09	113.59
194	9.70	19.06	0.62	0.62	36.21	114.01
195	9.75	19.06	0.66	0.66	36.33	114.26
196	9.80	19.97	0.65	0.65	35.17	114.57
197	9.85	22.27	0.67	0.67	32.86	114.70
198	9.90	24.20	0.64	0.64	30.44	114.87
199	9.95	26.24	0.64	0.64	28.50	114.86
200	10.00	27.33	0.62	0.62	26.88	114.78
201	10.05	28.63	0.59	0.59	25.01	114.58
202	10.10	31.35	0.55	0.55	22.88	114.23
203	10.15	33.32	0.50	0.50	20.71	113.84
204	10.20	35.56	0.46	0.46	18.95	113.35
205	10.25	36.96	0.43	0.43	17.61	112.98
206	10.30	38.16	0.41	0.41	16.82	112.71
207	10.35	38.54	0.41	0.41	16.54	112.68
208	10.40	38.45	0.42	0.42	16.68	112.72
209	10.45	37.68	0.42	0.42	17.10	112.82
210	10.50	36.81	0.43	0.43	17.63	112.83
211	10.55	35.74	0.43	0.43	18.14	112.81
212	10.60	35.04	0.43	0.43	18.59	112.80
213	10.65	34.55	0.44	0.44	18.97	112.89
214	10.70	34.55	0.45	0.45	19.27	113.03
215	10.75	34.37	0.46	0.46	19.55	113.15
216	10.80	34.00	0.46	0.46	19.77	113.16
217	10.85	33.67	0.46	0.46	19.94	113.10
218	10.90	33.38	0.45	0.45	19.99	113.08
219	10.95	33.75	0.46	0.46	19.97	113.12
220	11.00	34.06	0.46	0.46	19.87	113.22
221	11.05	34.45	0.47	0.47	19.80	113.29
222	11.10	34.55	0.47	0.47	19.77	113.34
223	11.15	34.55	0.47	0.47	19.78	113.35
224	11.20	34.55	0.47	0.47	19.81	113.34
225	11.25	34.44	0.47	0.47	19.92	113.26
226	11.30	33.67	0.46	0.46	20.15	113.15
227	11.35	33.06	0.45	0.45	20.51	113.03
228	11.40	32.29	0.45	0.45	20.90	113.04
229	11.45	32.16	0.46	0.46	21.26	113.14
230	11.50	32.14	0.48	0.48	21.67	113.28
231	11.55	31.42	0.49	0.49	22.24	113.43
232	11.60	30.70	0.50	0.50	23.13	113.58
233	11.65	29.54	0.52	0.52	24.34	113.88
234	11.70	28.61	0.57	0.57	25.85	114.25
235	11.75	27.49	0.61	0.61	27.68	114.74
236	11.80	26.19	0.66	0.66	29.60	115.11
237	11.85	24.90	0.69	0.69	31.59	115.42
238	11.90	23.77	0.72	0.72	33.17	115.56
239	11.95	23.10	0.73	0.73	34.37	115.66
240	12.00	22.71	0.74	0.74	34.73	115.61

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
241	12.05	22.87	0.72	0.72	34.49	115.49
242	12.10	23.23	0.70	0.70	33.43	115.28
243	12.15	24.27	0.66	0.66	32.08	115.09
244	12.20	25.30	0.64	0.64	30.35	114.92
245	12.25	26.84	0.62	0.62	28.76	114.76
246	12.30	27.90	0.59	0.59	27.22	114.58
247	12.35	29.04	0.57	0.57	26.21	114.45
248	12.40	29.46	0.57	0.57	25.66	114.44
249	12.45	29.74	0.58	0.58	25.96	114.63
250	12.50	29.00	0.61	0.61	26.82	114.93
251	12.55	28.16	0.65	0.65	28.37	115.26
252	12.60	26.61	0.69	0.69	30.27	115.52
253	12.65	24.94	0.72	0.72	32.61	115.61
254	12.70	22.74	0.73	0.73	35.45	115.59
255	12.75	20.36	0.75	0.75	38.68	115.40
256	12.80	18.25	0.74	0.74	42.19	115.26
257	12.85	16.73	0.76	0.76	45.24	115.16
258	12.90	15.93	0.78	0.78	47.76	115.29
259	12.95	15.55	0.82	0.82	49.30	115.47
260	13.00	15.49	0.84	0.84	50.15	115.65
261	13.05	15.49	0.85	0.85	49.96	115.67
262	13.10	15.85	0.82	0.82	49.23	115.56
263	13.15	16.08	0.79	0.79	48.01	115.23
264	13.20	16.08	0.73	0.73	47.20	114.64
265	13.25	15.33	0.65	0.65	47.06	113.65
266	13.30	13.83	0.55	0.55	47.96	112.48
267	13.35	12.50	0.49	0.49	49.66	111.27
268	13.40	11.28	0.44	0.44	51.72	110.60
269	13.45	10.90	0.46	0.46	53.26	110.39
270	13.50	10.97	0.47	0.47	53.43	110.72
271	13.55	11.75	0.50	0.50	52.48	111.12
272	13.60	12.38	0.52	0.52	51.00	111.58
273	13.65	13.09	0.53	0.53	50.28	111.93
274	13.70	13.10	0.56	0.56	50.24	112.25
275	13.75	13.10	0.58	0.58	50.93	112.55
276	13.80	13.10	0.60	0.60	51.58	112.81
277	13.85	13.10	0.62	0.62	52.22	113.07
278	13.90	13.10	0.64	0.64	52.66	113.24
279	13.95	13.10	0.65	0.65	52.96	113.37
280	14.00	13.15	0.65	0.65	52.71	113.62
281	14.05	13.88	0.69	0.69	52.19	114.02
282	14.10	14.51	0.74	0.74	51.48	114.64
283	14.15	15.28	0.80	0.80	51.13	115.14
284	14.20	15.49	0.82	0.82	51.08	115.49
285	14.25	15.49	0.84	0.84	51.25	115.63
286	14.30	15.49	0.84	0.84	51.47	115.71
287	14.35	15.49	0.85	0.85	51.73	115.80
288	14.40	15.49	0.87	0.87	52.02	115.90

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
289	14.45	15.49	0.88	0.88	52.30	116.00
290	14.50	15.49	0.88	0.88	52.25	116.06
291	14.55	15.74	0.89	0.89	51.86	116.11
292	14.60	16.10	0.89	0.89	50.82	116.17
293	14.65	16.81	0.88	0.88	49.51	116.19
294	14.70	17.36	0.86	0.86	47.93	116.07
295	14.75	17.75	0.82	0.82	46.63	115.84
296	14.80	17.87	0.78	0.78	45.50	115.49
297	14.85	17.87	0.74	0.74	45.07	115.10
298	14.90	17.27	0.70	0.70	45.15	114.67
299	14.95	16.61	0.67	0.67	45.95	114.28
300	15.00	15.86	0.66	0.66	46.99	113.95
301	15.05	15.24	0.64	0.64	48.33	113.68
302	15.10	14.46	0.63	0.63	49.69	113.40
303	15.15	13.83	0.61	0.61	51.20	113.10
304	15.20	13.12	0.60	0.60	52.38	112.95
305	15.25	13.10	0.61	0.61	53.22	112.94
306	15.30	13.10	0.62	0.62	53.58	113.07
307	15.35	13.10	0.63	0.63	53.82	113.15
308	15.40	13.10	0.63	0.63	53.93	113.18
309	15.45	13.10	0.63	0.63	53.92	113.15
310	15.50	13.10	0.62	0.62	53.83	113.10
311	15.55	13.10	0.62	0.62	53.74	113.04
312	15.60	13.10	0.62	0.62	53.76	113.03
313	15.65	13.10	0.62	0.62	54.02	113.12
314	15.70	13.10	0.64	0.64	54.11	113.44
315	15.75	13.72	0.69	0.69	53.72	114.07
316	15.80	14.83	0.77	0.77	51.83	115.00
317	15.85	17.13	0.85	0.85	49.12	116.00
318	15.90	19.41	0.93	0.93	45.59	116.84
319	15.95	22.07	0.95	0.95	42.37	117.38
320	16.00	24.09	0.96	0.96	39.16	117.64
321	16.05	26.39	0.93	0.93	36.82	117.76
322	16.10	27.56	0.93	0.93	35.08	117.84
323	16.15	28.58	0.93	0.93	34.85	118.02
324	16.20	27.86	0.98	0.98	35.50	118.23
325	16.25	26.98	1.02	1.02	37.32	118.38
326	16.30	25.04	1.04	1.04	39.25	118.37
327	16.35	23.68	1.03	1.03	41.34	118.18
328	16.40	22.18	1.01	1.01	42.79	117.91
329	16.45	21.45	0.98	0.98	43.82	117.59
330	16.50	20.85	0.95	0.95	44.04	117.29
331	16.55	20.85	0.91	0.91	43.83	117.00
332	16.60	20.85	0.88	0.88	43.18	116.68
333	16.65	20.85	0.83	0.83	42.84	116.43
334	16.70	20.62	0.83	0.83	42.97	116.31
335	16.75	20.26	0.84	0.84	43.94	116.46
336	16.80	19.91	0.90	0.90	45.35	116.74

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
337	16.85	19.46	0.94	0.94	47.30	116.99
338	16.90	18.31	0.96	0.96	49.22	117.14
339	16.95	17.87	0.99	0.99	50.95	117.33
340	17.00	17.87	1.05	1.05	50.92	117.87
341	17.05	20.05	1.16	1.16	49.31	118.73
342	17.10	22.85	1.29	1.29	45.77	119.77
343	17.15	27.25	1.39	1.39	41.96	120.62
344	17.20	31.00	1.43	1.43	37.79	121.21
345	17.25	35.65	1.42	1.42	34.25	121.43
346	17.30	38.77	1.36	1.36	30.83	121.32
347	17.35	42.09	1.23	1.23	28.22	120.87
348	17.40	42.92	1.10	1.10	26.01	120.14
349	17.45	43.34	0.97	0.97	24.74	119.31
350	17.50	42.20	0.88	0.88	24.04	118.54
351	17.55	40.99	0.82	0.82	24.11	117.94
352	17.60	39.06	0.78	0.78	24.65	117.49
353	17.65	36.97	0.77	0.77	25.72	117.14
354	17.70	34.50	0.75	0.75	27.50	116.83
355	17.75	30.68	0.75	0.75	29.89	116.54
356	17.80	27.72	0.75	0.75	33.02	116.47
357	17.85	25.47	0.81	0.81	36.10	116.64
358	17.90	24.13	0.87	0.87	39.28	117.08
359	17.95	22.88	0.95	0.95	42.21	117.46
360	18.00	21.52	1.00	1.00	45.25	117.79
361	18.05	20.28	1.06	1.06	47.67	118.20
362	18.10	20.66	1.16	1.16	48.99	118.87
363	18.15	21.92	1.30	1.30	48.29	119.97
364	18.20	25.41	1.52	1.52	46.71	120.94
365	18.25	27.34	1.59	1.59	44.58	121.63
366	18.30	29.14	1.59	1.59	42.36	121.90
367	18.35	31.56	1.58	1.58	39.64	122.06
368	18.40	34.82	1.57	1.57	35.64	122.57
369	18.45	43.65	1.70	1.70	31.45	123.16
370	18.50	50.71	1.71	1.71	27.08	123.68
371	18.55	59.41	1.64	1.64	23.83	123.68
372	18.60	62.81	1.51	1.51	21.21	123.31
373	18.65	65.16	1.35	1.35	20.42	122.78
374	18.70	59.74	1.32	1.32	20.90	122.31
375	18.75	54.39	1.31	1.31	23.49	122.07
376	18.80	45.86	1.37	1.37	26.79	121.90
377	18.85	40.54	1.40	1.40	30.93	121.72
378	18.90	35.18	1.41	1.41	34.51	121.57
379	18.95	32.48	1.45	1.45	37.92	121.50
380	19.00	30.21	1.50	1.50	40.48	121.53
381	19.05	28.89	1.52	1.52	42.71	121.44
382	19.10	26.97	1.49	1.49	44.90	120.92
383	19.15	23.31	1.31	1.31	47.56	119.97
384	19.20	20.17	1.15	1.15	51.07	118.56

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
385	19.25	16.67	0.97	0.97	54.00	117.45
386	19.30	16.32	0.95	0.95	55.93	116.74
387	19.35	16.24	0.94	0.94	55.43	116.66
388	19.40	17.01	0.93	0.93	54.16	116.65
389	19.45	17.63	0.92	0.92	52.22	116.62
390	19.50	18.39	0.89	0.89	50.63	116.45
391	19.55	18.46	0.84	0.84	49.24	116.10
392	19.60	18.40	0.78	0.78	48.55	115.52
393	19.65	17.66	0.71	0.71	48.08	114.87
394	19.70	17.25	0.66	0.66	47.90	114.31
395	19.75	17.17	0.64	0.64	47.24	114.39
396	19.80	18.72	0.72	0.72	46.29	115.34
397	19.85	21.25	0.88	0.88	44.96	116.68
398	19.90	23.41	1.00	1.00	43.79	117.89
399	19.95	25.02	1.09	1.09	42.57	118.18
400	20.00	24.62	0.96	0.96	41.67	117.70
401	20.05	23.26	0.81	0.81	41.00	116.46
402	20.10	21.60	0.68	0.68	41.21	115.17
403	20.15	19.79	0.61	0.61	42.32	114.06
404	20.20	17.97	0.56	0.56	44.37	113.20
405	20.25	16.28	0.53	0.53	46.94	112.52
406	20.30	14.87	0.51	0.51	49.31	112.20
407	20.35	14.63	0.53	0.53	50.83	112.34
408	20.40	15.09	0.58	0.58	51.57	112.92
409	20.45	15.46	0.63	0.63	52.12	113.52
410	20.50	15.49	0.67	0.67	52.91	114.03
411	20.55	15.53	0.71	0.71	53.50	114.44
412	20.60	15.91	0.75	0.75	53.44	114.98
413	20.65	16.90	0.81	0.81	51.94	115.76
414	20.70	19.21	0.90	0.90	49.52	116.69
415	20.75	21.61	0.98	0.98	46.39	117.61
416	20.80	24.43	1.05	1.05	43.58	118.30
417	20.85	26.56	1.08	1.08	41.14	118.73
418	20.90	28.15	1.08	1.08	39.40	118.89
419	20.95	28.92	1.06	1.06	38.33	118.80
420	21.00	28.65	1.02	1.02	38.25	118.61
421	21.05	27.52	1.00	1.00	39.16	118.40
422	21.10	25.95	1.00	1.00	41.06	118.30
423	21.15	24.28	1.03	1.03	43.51	118.18
424	21.20	22.41	1.02	1.02	46.06	118.13
425	21.25	21.44	1.05	1.05	47.80	118.08
426	21.30	21.44	1.06	1.06	48.74	118.00
427	21.35	20.78	1.01	1.01	49.07	117.61
428	21.40	19.69	0.91	0.91	50.03	116.76
429	21.45	17.48	0.79	0.79	51.57	115.61
430	21.50	15.60	0.69	0.69	53.86	114.51
431	21.55	14.45	0.65	0.65	56.09	113.67
432	21.60	13.53	0.61	0.61	58.17	112.94

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
433	21.65	12.38	0.55	0.55	60.16	112.10
434	21.70	11.41	0.50	0.50	62.17	111.04
435	21.75	10.40	0.43	0.43	63.93	110.08
436	21.80	9.86	0.40	0.40	65.29	109.26
437	21.85	9.53	0.38	0.38	66.12	108.91
438	21.90	9.53	0.39	0.39	66.34	108.95
439	21.95	9.83	0.41	0.41	66.00	109.44
440	22.00	10.38	0.45	0.45	65.33	110.09
441	22.05	10.84	0.49	0.49	64.75	110.83
442	22.10	11.27	0.53	0.53	64.38	111.51
443	22.15	11.71	0.57	0.57	63.95	112.23
444	22.20	12.34	0.63	0.63	62.83	113.09
445	22.25	13.56	0.70	0.70	61.23	113.97
446	22.30	14.61	0.76	0.76	59.20	114.81
447	22.35	15.79	0.82	0.82	56.36	115.77
448	22.40	18.45	0.93	0.93	52.98	116.74
449	22.45	20.86	1.01	1.01	49.12	117.73
450	22.50	23.95	1.07	1.07	45.81	118.31
451	22.55	25.72	1.06	1.06	42.76	118.52
452	22.60	27.23	1.00	1.00	40.41	118.33
453	22.65	27.97	0.94	0.94	38.38	117.95
454	22.70	28.53	0.88	0.88	37.28	117.50
455	22.75	27.79	0.83	0.83	36.87	117.04
456	22.80	26.94	0.79	0.79	37.63	116.69
457	22.85	25.39	0.79	0.79	39.06	116.41
458	22.90	23.70	0.78	0.78	41.37	116.14
459	22.95	21.52	0.76	0.76	44.03	115.71
460	23.00	19.45	0.72	0.72	47.04	115.18
461	23.05	17.63	0.69	0.69	49.97	114.57
462	23.10	16.10	0.66	0.66	52.76	114.04
463	23.15	15.02	0.64	0.64	55.53	113.55
464	23.20	13.88	0.61	0.61	57.90	113.25
465	23.25	13.44	0.62	0.62	60.02	113.12
466	23.30	13.10	0.63	0.63	61.48	113.26
467	23.35	13.10	0.66	0.66	62.79	113.62
468	23.40	13.20	0.71	0.71	63.64	114.16
469	23.45	13.58	0.78	0.78	63.98	114.85
470	23.50	14.29	0.85	0.85	63.25	115.61
471	23.55	15.40	0.93	0.93	61.63	116.37
472	23.60	16.72	0.99	0.99	59.33	116.97
473	23.65	17.91	1.01	1.01	57.26	117.26
474	23.70	18.29	0.99	0.99	55.65	117.15
475	23.75	18.20	0.92	0.92	54.85	116.65
476	23.80	17.43	0.83	0.83	54.44	115.93
477	23.85	16.79	0.75	0.75	54.35	115.07
478	23.90	16.08	0.68	0.68	54.59	114.18
479	23.95	15.02	0.60	0.60	55.05	113.20
480	24.00	14.14	0.53	0.53	55.76	112.21

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
481	24.05	13.37	0.48	0.48	56.07	111.36
482	24.10	13.10	0.45	0.45	56.48	110.96
483	24.15	13.10	0.47	0.47	56.65	111.18
484	24.20	13.67	0.52	0.52	57.22	112.08
485	24.25	14.42	0.62	0.62	57.01	113.51
486	24.30	16.28	0.77	0.77	56.63	115.18
487	24.35	17.94	0.93	0.93	55.20	116.82
488	24.40	20.27	1.09	1.09	53.62	118.21
489	24.45	22.36	1.23	1.23	51.19	119.26
490	24.50	24.92	1.31	1.31	48.38	120.15
491	24.55	28.24	1.41	1.41	45.23	120.85
492	24.60	31.36	1.47	1.47	42.27	121.53
493	24.65	34.81	1.55	1.55	39.82	121.97
494	24.70	36.94	1.55	1.55	37.86	122.27
495	24.75	38.78	1.55	1.55	36.30	122.35
496	24.80	40.19	1.52	1.52	34.83	122.32
497	24.85	41.70	1.47	1.47	33.30	122.27
498	24.90	44.02	1.46	1.46	31.56	122.17
499	24.95	46.24	1.39	1.39	29.65	122.14
500	25.00	49.61	1.37	1.37	27.74	122.01
501	25.05	51.98	1.31	1.31	25.96	121.91
502	25.10	54.59	1.26	1.26	24.60	121.66
503	25.15	55.10	1.20	1.20	23.61	121.39
504	25.20	55.43	1.14	1.14	23.04	121.13
505	25.25	55.81	1.13	1.13	22.69	121.01
506	25.30	56.31	1.13	1.13	22.48	121.05
507	25.35	57.28	1.15	1.15	22.31	121.15
508	25.40	57.95	1.16	1.16	22.19	121.30
509	25.45	58.66	1.19	1.19	22.02	121.48
510	25.50	60.18	1.22	1.22	21.75	121.66
511	25.55	61.67	1.23	1.23	21.26	121.83
512	25.60	63.98	1.24	1.24	20.58	121.93
513	25.65	66.38	1.23	1.23	19.76	122.08
514	25.70	69.87	1.25	1.25	18.98	122.24
515	25.75	72.46	1.26	1.26	18.31	122.46
516	25.80	75.09	1.29	1.29	17.77	122.72
517	25.85	78.43	1.34	1.34	17.35	123.07
518	25.90	81.26	1.40	1.40	17.00	123.51
519	25.95	84.86	1.48	1.48	16.93	123.79
520	26.00	83.19	1.47	1.47	17.07	123.72
521	26.05	78.81	1.37	1.37	17.41	123.32
522	26.10	76.00	1.30	1.30	17.64	122.80
523	26.15	74.13	1.24	1.24	17.63	122.56
524	26.20	76.04	1.27	1.27	17.57	122.51
525	26.25	76.16	1.28	1.28	17.65	122.59
526	26.30	74.43	1.28	1.28	17.97	122.58
527	26.35	72.86	1.28	1.28	18.48	122.55
528	26.40	71.12	1.29	1.29	19.06	122.54

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
529	26.45	69.18	1.30	1.30	19.83	122.64
530	26.50	67.53	1.37	1.37	20.74	122.81
531	26.55	65.60	1.42	1.42	21.82	123.05
532	26.60	63.73	1.48	1.48	23.02	123.27
533	26.65	61.25	1.54	1.54	24.37	123.44
534	26.70	58.32	1.58	1.58	25.97	123.59
535	26.75	55.40	1.66	1.66	27.69	123.70
536	26.80	52.58	1.70	1.70	29.59	123.86
537	26.85	49.97	1.77	1.77	31.56	123.86
538	26.90	46.20	1.76	1.76	33.68	123.78
539	26.95	42.98	1.76	1.76	35.96	123.50
540	27.00	39.29	1.71	1.71	38.11	123.21
541	27.05	37.08	1.68	1.68	40.00	122.93
542	27.10	35.49	1.67	1.67	41.21	122.81
543	27.15	35.23	1.69	1.69	41.91	122.77
544	27.20	35.08	1.69	1.69	42.14	122.78
545	27.25	34.96	1.68	1.68	42.29	122.72
546	27.30	34.57	1.65	1.65	42.44	122.62
547	27.35	34.18	1.64	1.64	42.55	122.60
548	27.40	34.67	1.67	1.67	42.62	122.71
549	27.45	35.09	1.72	1.72	42.60	122.93
550	27.50	35.60	1.77	1.77	42.74	123.13
551	27.55	35.52	1.80	1.80	43.03	123.25
552	27.60	35.16	1.81	1.81	43.65	123.21
553	27.65	33.84	1.77	1.77	44.43	123.08
554	27.70	32.92	1.75	1.75	44.85	123.06
555	27.75	34.06	1.81	1.81	44.64	123.20
556	27.80	35.25	1.85	1.85	43.68	123.49
557	27.85	37.07	1.89	1.89	42.41	123.72
558	27.90	38.91	1.90	1.90	40.76	123.88
559	27.95	41.04	1.88	1.88	38.72	124.11
560	28.00	45.10	1.94	1.94	36.51	124.26
561	28.05	47.74	1.89	1.89	34.72	124.28
562	28.10	48.12	1.80	1.80	33.61	123.90
563	28.15	46.63	1.64	1.64	33.57	123.33
564	28.20	43.45	1.54	1.54	34.38	122.62
565	28.25	39.78	1.44	1.44	36.14	121.98
566	28.30	36.17	1.37	1.37	38.22	121.35
567	28.35	33.20	1.31	1.31	40.25	120.89
568	28.40	31.71	1.29	1.29	41.63	120.66
569	28.45	31.56	1.31	1.31	42.48	120.67
570	28.50	31.27	1.33	1.33	43.10	120.77
571	28.55	30.88	1.35	1.35	43.79	120.84
572	28.60	30.41	1.37	1.37	44.41	120.88
573	28.65	30.18	1.37	1.37	44.65	120.95
574	28.70	30.76	1.40	1.40	44.56	120.97
575	28.75	30.75	1.37	1.37	44.29	120.85
576	28.80	30.24	1.31	1.31	44.82	120.20

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
577	28.85	26.57	1.11	1.11	46.41	118.94
578	28.90	22.16	0.88	0.88	49.63	116.93
579	28.95	17.49	0.66	0.66	53.54	114.60
580	29.00	14.68	0.52	0.52	56.89	112.55
581	29.05	13.90	0.46	0.46	58.28	111.15
582	29.10	13.49	0.42	0.42	58.27	110.30
583	29.15	13.12	0.38	0.38	57.72	109.60
584	29.20	13.10	0.36	0.36	57.08	109.09
585	29.25	13.10	0.34	0.34	56.48	108.80
586	29.30	13.10	0.34	0.34	56.44	108.76
587	29.35	13.10	0.35	0.35	56.86	108.93
588	29.40	13.10	0.37	0.37	57.67	109.28
589	29.45	13.10	0.39	0.39	58.59	109.66
590	29.50	13.12	0.41	0.41	58.99	110.23
591	29.55	13.84	0.46	0.46	58.91	110.92
592	29.60	14.47	0.50	0.50	58.21	111.71
593	29.65	15.24	0.54	0.54	57.32	112.48
594	29.70	16.23	0.59	0.59	55.86	113.32
595	29.75	17.73	0.66	0.66	54.20	114.17
596	29.80	19.06	0.71	0.71	52.32	114.86
597	29.85	20.25	0.73	0.73	51.04	115.18
598	29.90	20.25	0.72	0.72	50.49	115.07
599	29.95	19.51	0.68	0.68	51.56	114.45
600	30.00	17.18	0.60	0.60	52.61	113.99
601	30.05	17.83	0.62	0.62	52.45	113.96
602	30.10	19.63	0.67	0.67	49.47	114.87
603	30.15	23.44	0.77	0.77	46.00	115.89
604	30.20	26.21	0.83	0.83	43.70	116.61
605	30.25	26.21	0.83	0.83	43.04	116.91
606	30.30	25.88	0.84	0.84	43.88	117.02
607	30.35	25.12	0.88	0.88	45.43	117.37
608	30.40	24.81	0.97	0.97	47.50	118.00
609	30.45	24.79	1.10	1.10	48.48	119.36
610	30.50	28.91	1.43	1.43	48.25	121.15
611	30.55	33.14	1.79	1.79	46.13	123.25
612	30.60	40.25	2.23	2.23	43.50	124.97
613	30.65	46.61	2.52	2.52	40.09	126.34
614	30.70	54.51	2.72	2.72	36.89	127.02
615	30.75	58.83	2.62	2.62	33.94	127.25
616	30.80	62.66	2.51	2.51	31.46	127.13
617	30.85	66.39	2.43	2.43	29.31	127.03
618	30.90	70.51	2.37	2.37	27.29	127.13
619	30.95	77.25	2.44	2.44	25.41	127.29
620	31.00	82.60	2.41	2.41	23.62	127.49
621	31.05	88.38	2.39	2.39	21.93	127.55
622	31.10	94.04	2.34	2.34	20.46	127.59
623	31.15	98.69	2.31	2.31	19.28	127.67
624	31.20	103.34	2.35	2.35	18.54	127.95

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
625	31.25	108.29	2.49	2.49	18.06	128.48
626	31.30	115.33	2.72	2.72	17.74	129.25
627	31.35	123.56	3.02	3.02	17.38	130.09
628	31.40	132.15	3.29	3.29	16.94	130.94
629	31.45	142.74	3.59	3.59	16.38	131.64
630	31.50	152.00	3.78	3.78	15.70	132.32
631	31.55	164.56	4.04	4.04	15.03	132.84
632	31.60	172.85	4.17	4.17	14.42	133.30
633	31.65	181.49	4.31	4.31	13.93	133.58
634	31.70	186.78	4.36	4.36	13.52	133.78
635	31.75	191.24	4.38	4.38	13.19	133.90
636	31.80	195.01	4.41	4.41	12.93	134.00
637	31.85	198.22	4.45	4.45	12.72	134.12
638	31.90	202.41	4.52	4.52	12.53	134.26
639	31.95	206.31	4.58	4.58	12.36	134.42
640	32.00	210.25	4.66	4.66	12.26	134.52
641	32.05	210.25	4.67	4.67	12.27	134.60
642	32.10	209.54	4.71	4.71	12.40	134.62
643	32.15	206.82	4.72	4.72	12.64	134.66
644	32.20	204.44	4.79	4.79	12.96	134.70
645	32.25	201.49	4.85	4.85	13.34	134.80
646	32.30	199.41	4.97	4.97	13.68	134.88
647	32.35	197.74	5.01	5.01	13.94	134.97
648	32.40	197.74	5.07	5.07	13.99	134.99
649	32.45	199.01	5.01	5.01	13.84	134.99
650	32.50	202.48	4.98	4.98	13.47	134.92
651	32.55	206.10	4.85	4.85	13.01	134.85
652	32.60	210.31	4.77	4.77	12.48	134.74
653	32.65	214.96	4.67	4.67	12.00	134.65
654	32.70	218.74	4.60	4.60	11.58	134.58
655	32.75	222.22	4.55	4.55	11.29	134.52
656	32.80	222.80	4.50	4.50	11.14	134.46
657	32.85	221.68	4.46	4.46	11.15	134.40
658	32.90	219.51	4.45	4.45	11.25	134.35
659	32.95	217.27	4.44	4.44	11.37	134.31
660	33.00	215.77	4.43	4.43	11.45	134.24
661	33.05	214.29	4.37	4.37	11.49	134.14
662	33.10	211.97	4.30	4.30	11.52	133.98
663	33.15	208.73	4.20	4.20	11.60	133.80
664	33.20	204.40	4.12	4.12	11.78	133.58
665	33.25	197.51	4.01	4.01	12.08	133.35
666	33.30	190.65	3.94	3.94	12.54	133.06
667	33.35	180.28	3.81	3.81	13.13	132.82
668	33.40	173.09	3.81	3.81	13.80	132.59
669	33.45	165.46	3.75	3.75	14.45	132.47
670	33.50	160.87	3.77	3.77	14.96	132.30
671	33.55	156.56	3.68	3.68	15.25	132.15
672	33.60	154.73	3.61	3.61	15.28	131.93

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
673	33.65	154.17	3.49	3.49	15.08	131.76
674	33.70	156.11	3.43	3.43	14.68	131.55
675	33.75	157.34	3.29	3.29	14.23	131.35
676	33.80	158.61	3.18	3.18	13.71	131.09
677	33.85	160.27	3.05	3.05	13.25	130.86
678	33.90	161.65	2.97	2.97	12.84	130.61
679	33.95	161.48	2.86	2.86	12.60	130.39
680	34.00	159.88	2.79	2.79	12.54	130.13
681	34.05	155.64	2.71	2.71	12.73	129.96
682	34.10	152.39	2.72	2.72	13.08	129.85
683	34.15	148.87	2.73	2.73	13.56	129.86
684	34.20	145.66	2.78	2.78	14.03	129.89
685	34.25	143.14	2.81	2.81	14.48	129.94
686	34.30	141.21	2.84	2.84	14.82	130.02
687	34.35	140.93	2.90	2.90	15.05	130.13
688	34.40	141.68	2.95	2.95	15.15	130.27
689	34.45	142.92	3.00	3.00	15.19	130.42
690	34.50	144.29	3.06	3.06	15.20	130.60
691	34.55	146.16	3.14	3.14	15.23	130.80
692	34.60	147.94	3.22	3.22	15.22	131.02
693	34.65	150.65	3.30	3.30	15.13	131.21
694	34.70	153.30	3.34	3.34	14.93	131.36
695	34.75	156.56	3.37	3.37	14.64	131.47
696	34.80	160.35	3.38	3.38	14.29	131.56
697	34.85	163.76	3.39	3.39	13.94	131.63
698	34.90	167.21	3.40	3.40	13.69	131.71
699	34.95	168.56	3.42	3.42	13.58	131.77
700	35.00	168.56	3.44	3.44	13.68	131.83
701	35.05	166.95	3.49	3.49	13.90	131.88
702	35.10	164.91	3.52	3.52	14.22	131.94
703	35.15	163.08	3.57	3.57	14.53	132.00
704	35.20	161.81	3.61	3.61	14.81	132.07
705	35.25	161.03	3.65	3.65	14.99	132.13
706	35.30	160.81	3.67	3.67	15.10	132.17
707	35.35	160.81	3.68	3.68	15.13	132.20
708	35.40	161.44	3.69	3.69	15.12	132.23
709	35.45	162.14	3.71	3.71	15.09	132.28
710	35.50	163.28	3.73	3.73	15.05	132.34
711	35.55	164.20	3.76	3.76	15.00	132.40
712	35.60	165.36	3.78	3.78	14.92	132.45
713	35.65	166.80	3.79	3.79	14.80	132.49
714	35.70	168.57	3.79	3.79	14.62	132.54
715	35.75	171.06	3.80	3.80	14.43	132.59
716	35.80	173.20	3.82	3.82	14.24	132.66
717	35.85	175.52	3.85	3.85	14.10	132.72
718	35.90	177.01	3.86	3.86	13.97	132.78
719	35.95	178.52	3.87	3.87	13.89	132.81
720	36.00	178.68	3.88	3.88	13.88	132.84

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
721	36.05	178.51	3.89	3.89	13.95	132.82
722	36.10	176.27	3.87	3.87	14.09	132.77
723	36.15	173.83	3.83	3.83	14.30	132.65
724	36.20	169.57	3.77	3.77	14.56	132.52
725	36.25	165.90	3.73	3.73	14.87	132.35
726	36.30	161.54	3.67	3.67	15.18	132.19
727	36.35	158.06	3.61	3.61	15.44	131.98
728	36.40	154.18	3.51	3.51	15.74	131.66
729	36.45	146.13	3.31	3.31	16.05	131.18
730	36.50	138.82	3.09	3.09	16.48	130.49
731	36.55	128.72	2.81	2.81	16.75	129.85
732	36.60	126.07	2.68	2.68	16.88	129.33
733	36.65	124.83	2.59	2.59	16.59	129.15
734	36.70	129.68	2.61	2.61	16.24	129.19
735	36.75	133.03	2.67	2.67	15.90	129.36
736	36.80	134.88	2.71	2.71	16.04	129.50
737	36.85	130.66	2.76	2.76	16.69	129.49
738	36.90	121.79	2.73	2.73	18.19	129.38
739	36.95	109.14	2.78	2.78	20.33	129.14
740	37.00	96.56	2.75	2.75	23.25	128.80
741	37.05	82.92	2.70	2.70	26.54	128.34
742	37.10	71.96	2.64	2.64	30.46	127.61
743	37.15	58.55	2.39	2.39	34.64	126.84
744	37.20	50.87	2.32	2.32	39.07	125.87
745	37.25	43.47	2.11	2.11	42.75	125.10
746	37.30	39.57	1.99	1.99	45.63	124.20
747	37.35	36.23	1.80	1.80	47.64	123.28
748	37.40	32.76	1.58	1.58	48.93	122.23
749	37.45	30.86	1.41	1.41	49.73	121.20
750	37.50	29.35	1.27	1.27	49.89	120.31
751	37.55	28.32	1.15	1.15	49.93	119.51
752	37.60	27.29	1.06	1.06	50.03	118.70
753	37.65	25.80	0.95	0.95	49.84	118.20
754	37.70	26.71	0.96	0.96	47.90	118.61
755	37.75	32.44	1.16	1.16	45.74	119.96
756	37.80	36.33	1.43	1.43	43.87	121.72
757	37.85	40.48	1.73	1.73	44.11	123.05
758	37.90	39.91	1.91	1.91	44.62	123.92
759	37.95	40.56	2.00	2.00	44.13	124.86
760	38.00	48.45	2.38	2.38	41.19	125.83
761	38.05	56.92	2.51	2.51	36.54	127.00
762	38.10	70.06	2.71	2.71	31.58	127.55
763	38.15	80.78	2.52	2.52	26.94	127.80
764	38.20	92.06	2.38	2.38	22.78	127.47
765	38.25	101.52	2.09	2.09	19.62	127.07
766	38.30	108.15	1.94	1.94	17.22	126.48
767	38.35	112.03	1.76	1.76	15.91	126.05
768	38.40	112.18	1.69	1.69	15.26	125.63

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
769	38.45	110.32	1.63	1.63	15.34	125.46
770	38.50	107.72	1.66	1.66	15.75	125.39
771	38.55	105.09	1.69	1.69	16.48	125.50
772	38.60	102.06	1.75	1.75	17.30	125.65
773	38.65	99.59	1.81	1.81	18.25	125.83
774	38.70	96.51	1.87	1.87	19.04	126.02
775	38.75	95.89	1.93	1.93	19.60	126.18
776	38.80	95.89	1.96	1.96	19.67	126.29
777	38.85	97.66	1.95	1.95	19.41	126.31
778	38.90	99.32	1.93	1.93	18.86	126.26
779	38.95	101.64	1.88	1.88	18.32	126.20
780	39.00	103.32	1.87	1.87	17.83	126.18
781	39.05	105.21	1.87	1.87	17.72	126.25
782	39.10	104.28	1.92	1.92	17.94	126.37
783	39.15	102.78	1.97	1.97	18.68	126.54
784	39.20	99.07	2.05	2.05	19.69	126.74
785	39.25	95.81	2.14	2.14	21.05	126.96
786	39.30	91.42	2.24	2.24	22.65	127.18
787	39.35	86.40	2.34	2.34	24.56	127.28
788	39.40	79.80	2.37	2.37	26.74	127.35
789	39.45	74.71	2.46	2.46	28.93	127.33
790	39.50	70.30	2.49	2.49	31.01	127.38
791	39.55	66.90	2.56	2.56	32.63	127.33
792	39.60	64.56	2.53	2.53	33.89	127.21
793	39.65	62.15	2.48	2.48	34.21	126.98
794	39.70	62.82	2.38	2.38	33.87	126.77
795	39.75	64.20	2.33	2.33	32.93	126.64
796	39.80	65.76	2.30	2.30	32.07	126.60
797	39.85	67.26	2.29	2.29	31.24	126.65
798	39.90	69.59	2.31	2.31	29.94	126.57
799	39.95	72.81	2.15	2.15	27.97	126.35
800	40.00	77.65	1.99	1.99	25.71	125.85
801	40.05	79.56	1.80	1.80	23.92	125.38
802	40.10	80.88	1.72	1.72	23.20	125.08
803	40.15	79.75	1.75	1.75	23.30	125.07
804	40.20	78.69	1.79	1.79	23.96	125.19
805	40.25	77.15	1.83	1.83	24.66	125.31
806	40.30	75.88	1.88	1.88	25.38	125.41
807	40.35	74.46	1.90	1.90	25.96	125.44
808	40.40	73.40	1.89	1.89	26.33	125.37
809	40.45	72.44	1.85	1.85	26.42	125.15
810	40.50	71.29	1.76	1.76	26.32	124.83
811	40.55	70.36	1.68	1.68	26.14	124.44
812	40.60	69.22	1.60	1.60	26.33	124.20
813	40.65	67.32	1.62	1.62	26.97	124.10
814	40.70	65.17	1.66	1.66	28.40	124.26
815	40.75	62.21	1.77	1.77	30.13	124.48
816	40.80	59.64	1.84	1.84	32.27	124.70

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
817	40.85	56.25	1.91	1.91	34.07	124.80
818	40.90	54.53	1.93	1.93	35.56	124.81
819	40.95	53.07	1.93	1.93	35.79	124.84
820	41.00	55.63	1.95	1.95	35.05	124.94
821	41.05	58.75	1.95	1.95	32.86	125.14
822	41.10	65.48	1.95	1.95	30.34	125.31
823	41.15	71.00	1.92	1.92	27.48	125.43
824	41.20	77.99	1.87	1.87	25.03	125.48
825	41.25	83.90	1.83	1.83	22.80	125.53
826	41.30	90.29	1.81	1.81	20.82	125.57
827	41.35	97.44	1.76	1.76	19.06	125.58
828	41.40	103.25	1.72	1.72	17.44	125.53
829	41.45	109.26	1.66	1.66	16.18	125.44
830	41.50	113.00	1.62	1.62	15.13	125.33
831	41.55	116.73	1.58	1.58	14.55	125.18
832	41.60	115.67	1.53	1.53	14.30	124.99
833	41.65	113.62	1.50	1.50	14.63	124.71
834	41.70	106.46	1.45	1.45	15.38	124.44
835	41.75	99.85	1.44	1.44	16.74	124.13
836	41.80	90.26	1.42	1.42	18.66	124.04
837	41.85	82.70	1.52	1.52	21.22	124.03
838	41.90	74.27	1.58	1.58	24.02	124.20
839	41.95	69.10	1.67	1.67	26.71	124.27
840	42.00	64.39	1.71	1.71	29.27	124.27
841	42.05	58.46	1.71	1.71	31.81	124.17
842	42.10	54.53	1.74	1.74	34.57	124.07
843	42.15	50.52	1.77	1.77	36.62	124.16
844	42.20	50.59	1.85	1.85	37.92	124.37
845	42.25	51.29	1.94	1.94	38.02	124.64
846	42.30	52.40	1.95	1.95	37.74	124.79
847	42.35	53.12	1.95	1.95	37.17	124.78
848	42.40	53.51	1.90	1.90	36.83	124.72
849	42.45	53.39	1.90	1.90	36.76	124.67
850	42.50	53.03	1.91	1.91	37.30	124.71
851	42.55	51.71	1.95	1.95	38.22	124.76
852	42.60	50.25	1.98	1.98	39.74	124.78
853	42.65	47.58	2.00	2.00	41.51	124.79
854	42.70	45.57	2.03	2.03	43.69	124.80
855	42.75	43.27	2.08	2.08	45.41	124.93
856	42.80	43.40	2.18	2.18	46.59	125.21
857	42.85	44.19	2.30	2.30	46.03	125.74
858	42.90	48.88	2.48	2.48	44.40	126.35
859	42.95	53.41	2.61	2.61	41.44	126.99
860	43.00	60.38	2.69	2.69	38.33	127.40
861	43.05	65.96	2.67	2.67	34.89	127.62
862	43.10	72.69	2.58	2.58	31.93	127.56
863	43.15	76.58	2.42	2.42	29.30	127.29
864	43.20	79.81	2.25	2.25	27.44	126.82

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
865	43.25	79.81	2.06	2.06	26.26	126.36
866	43.30	79.43	1.98	1.98	25.91	126.03
867	43.35	78.27	1.98	1.98	26.18	126.08
868	43.40	78.49	2.11	2.11	26.87	126.45
869	43.45	79.21	2.29	2.29	27.88	126.95
870	43.50	77.48	2.44	2.44	29.09	127.37
871	43.55	75.54	2.55	2.55	30.68	127.61
872	43.60	71.69	2.62	2.62	32.21	127.79
873	43.65	70.11	2.71	2.71	33.62	127.99
874	43.70	69.73	2.85	2.85	34.03	128.41
875	43.75	74.52	3.07	3.07	33.60	129.02
876	43.80	80.44	3.31	3.31	32.12	129.61
877	43.85	87.45	3.37	3.37	30.38	130.03
878	43.90	93.33	3.39	3.39	28.31	130.23
879	43.95	100.55	3.33	3.33	26.24	130.40
880	44.00	109.39	3.36	3.36	23.95	130.61
881	44.05	121.50	3.39	3.39	21.80	130.95
882	44.10	133.73	3.48	3.48	19.84	131.30
883	44.15	145.26	3.53	3.53	18.11	131.61
884	44.20	157.84	3.53	3.53	16.61	131.82
885	44.25	167.43	3.51	3.51	15.22	131.94
886	44.30	178.57	3.47	3.47	14.20	132.12
887	44.35	187.35	3.59	3.59	13.46	132.42
888	44.40	196.70	3.76	3.76	13.05	132.82
889	44.45	203.90	3.90	3.90	12.75	133.18
890	44.50	209.59	4.01	4.01	12.53	133.46
891	44.55	214.62	4.11	4.11	12.36	133.68
892	44.60	217.90	4.17	4.17	12.22	133.85
893	44.65	221.27	4.23	4.23	12.13	133.97
894	44.70	222.76	4.26	4.26	12.06	134.06
895	44.75	223.91	4.29	4.29	12.04	134.10
896	44.80	223.54	4.28	4.28	12.05	134.10
897	44.85	222.85	4.27	4.27	12.09	134.06
898	44.90	221.31	4.24	4.24	12.14	134.00
899	44.95	219.81	4.21	4.21	12.20	133.93
900	45.00	218.02	4.17	4.17	12.26	133.86
901	45.05	216.62	4.15	4.15	12.32	133.80
902	45.10	215.34	4.12	4.12	12.38	133.73
903	45.15	213.80	4.09	4.09	12.44	133.67
904	45.20	212.24	4.06	4.06	12.52	133.58
905	45.25	209.95	4.02	4.02	12.60	133.49
906	45.30	208.00	3.98	3.98	12.69	133.40
907	45.35	206.00	3.94	3.94	12.79	133.33
908	45.40	204.53	3.94	3.94	12.90	133.29
909	45.45	203.39	3.95	3.95	13.02	133.28
910	45.50	202.22	3.95	3.95	13.10	133.28
911	45.55	202.33	3.95	3.95	13.11	133.27
912	45.60	203.06	3.94	3.94	13.04	133.27

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
913	45.65	204.07	3.93	3.93	12.95	133.26
914	45.70	204.99	3.92	3.92	12.88	133.27
915	45.75	205.75	3.94	3.94	12.83	133.29
916	45.80	206.51	3.94	3.94	12.77	133.30
917	45.85	207.67	3.93	3.93	12.65	133.27
918	45.90	208.12	3.87	3.87	12.46	133.16
919	45.95	208.46	3.75	3.75	12.17	132.94
920	46.00	208.46	3.59	3.59	11.82	132.65
921	46.05	208.29	3.42	3.42	11.39	132.25
922	46.10	207.52	3.20	3.20	10.94	131.82
923	46.15	207.09	3.02	3.02	10.43	131.32
924	46.20	206.71	2.79	2.79	9.97	130.90
925	46.25	208.16	2.69	2.69	9.51	130.54
926	46.30	209.99	2.60	2.60	9.16	130.38
927	46.35	213.74	2.58	2.58	8.85	130.30
928	46.40	216.96	2.57	2.57	8.56	130.30
929	46.45	221.22	2.55	2.55	8.28	130.28
930	46.50	224.45	2.52	2.52	7.95	130.22
931	46.55	228.05	2.46	2.46	7.63	130.10
932	46.60	230.85	2.40	2.40	7.29	129.95
933	46.65	233.34	2.34	2.34	7.01	129.79
934	46.70	234.67	2.28	2.28	6.77	129.61
935	46.75	234.67	2.22	2.22	6.54	129.37
936	46.80	234.67	2.11	2.11	6.30	129.07
937	46.85	234.67	2.02	2.02	6.03	128.73
938	46.90	234.67	1.92	1.92	5.76	128.38
939	46.95	234.28	1.83	1.83	5.51	127.97
940	47.00	231.86	1.72	1.72	5.32	127.54
941	47.05	227.98	1.63	1.63	5.27	127.14
942	47.10	222.05	1.58	1.58	5.44	126.86
943	47.15	213.33	1.58	1.58	5.82	126.70
944	47.20	204.34	1.58	1.58	6.37	126.63
945	47.25	195.72	1.60	1.60	7.01	126.58
946	47.30	186.09	1.62	1.62	7.77	126.60
947	47.35	176.89	1.67	1.67	8.93	126.80
948	47.40	163.37	1.84	1.84	10.44	127.10
949	47.45	151.42	1.96	1.96	12.43	127.48
950	47.50	138.07	2.12	2.12	14.68	127.79
951	47.55	125.10	2.28	2.28	17.29	128.11
952	47.60	114.45	2.46	2.46	20.25	128.48
953	47.65	104.04	2.70	2.70	23.13	128.93
954	47.70	99.74	2.96	2.96	25.85	129.56
955	47.75	97.86	3.35	3.35	27.91	130.24
956	47.80	96.67	3.65	3.65	29.76	130.94
957	47.85	95.57	4.01	4.01	31.19	131.45
958	47.90	94.82	4.19	4.19	32.23	131.89
959	47.95	95.95	4.40	4.40	32.35	132.25
960	48.00	100.76	4.55	4.55	31.86	132.55

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
961	48.05	104.27	4.60	4.60	30.84	132.71
962	48.10	108.12	4.54	4.54	30.09	132.68
963	48.15	107.18	4.40	4.40	29.62	132.51
964	48.20	105.47	4.26	4.26	29.98	132.24
965	48.25	99.84	4.18	4.18	30.87	131.97
966	48.30	94.56	4.11	4.11	32.52	131.69
967	48.35	87.16	4.04	4.04	34.46	131.42
968	48.40	81.18	4.00	4.00	36.90	131.19
969	48.45	75.16	4.04	4.04	39.22	131.14
970	48.50	72.92	4.20	4.20	41.31	131.28
971	48.55	71.86	4.41	4.41	42.36	131.51
972	48.60	72.80	4.49	4.49	42.48	131.76
973	48.65	75.61	4.59	4.59	41.30	131.91
974	48.70	80.23	4.53	4.53	39.12	132.11
975	48.75	88.04	4.56	4.56	36.10	132.17
976	48.80	95.88	4.34	4.34	32.78	132.20
977	48.85	105.37	4.19	4.19	29.63	131.98
978	48.90	111.15	3.85	3.85	27.00	131.65
979	48.95	115.44	3.57	3.57	25.16	131.15
980	49.00	115.24	3.32	3.32	24.10	130.69
981	49.05	113.81	3.16	3.16	23.94	130.32
982	49.10	110.19	3.13	3.13	24.39	130.14
983	49.15	106.83	3.16	3.16	25.49	130.14
984	49.20	102.19	3.28	3.28	26.83	130.29
985	49.25	99.75	3.44	3.44	28.45	130.63
986	49.30	97.87	3.73	3.73	29.73	131.03
987	49.35	97.97	3.91	3.91	30.67	131.41
988	49.40	98.43	4.05	4.05	30.76	131.59
989	49.45	100.30	3.98	3.98	30.29	131.58
990	49.50	101.97	3.84	3.84	29.22	131.37
991	49.55	104.29	3.64	3.64	28.08	131.03
992	49.60	104.83	3.41	3.41	26.89	130.55
993	49.65	104.83	3.13	3.13	25.95	130.18
994	49.70	106.85	3.11	3.11	25.30	130.03
995	49.75	108.90	3.18	3.18	24.88	130.17
996	49.80	111.97	3.24	3.24	24.63	130.26
997	49.85	111.42	3.18	3.18	24.38	130.02
998	49.90	107.22	2.89	2.89	24.27	129.71

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q _c :	Measured cone resistance (tsf)
f _s :	Sleeve friction resistance (tsf)
u:	Pore pressure (tsf)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (pcf)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1	0.05	0.00	0.00	0.00	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
2	0.10	0.01	0.00	0.01	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
3	0.15	0.01	0.00	0.01	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
4	0.20	0.01	0.00	0.01	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
5	0.25	0.01	0.00	0.01	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
6	0.30	0.02	0.00	0.02	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
7	0.35	0.02	0.00	0.02	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
8	0.40	0.02	0.00	0.02	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
9	0.45	0.02	0.00	0.02	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
10	0.50	0.03	0.00	0.03	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
11	0.55	0.03	0.00	0.03	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
12	0.60	0.03	0.00	0.03	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
13	0.65	0.04	0.00	0.04	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
14	0.70	0.04	0.00	0.04	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
15	0.75	0.04	0.00	0.04	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
16	0.80	0.05	0.00	0.05	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
17	0.85	0.05	0.00	0.05	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
18	0.90	0.05	0.00	0.05	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
19	0.95	0.06	0.00	0.06	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
20	1.00	0.06	0.00	0.06	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
21	1.05	0.06	0.00	0.06	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
22	1.10	0.07	0.00	0.07	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
23	1.15	0.07	0.00	0.07	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
24	1.20	0.07	0.00	0.07	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
25	1.25	0.07	0.00	0.07	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
26	1.30	0.08	0.00	0.08	1.00	0.480	1.06	0.455	1.00	1.30	2.000	Yes
27	1.35	0.08	0.00	0.08	1.00	0.480	1.06	0.455	1.00	1.30	2.000	Yes
28	1.40	0.08	0.00	0.08	1.00	0.480	1.06	0.455	1.00	1.30	2.000	Yes
29	1.45	0.09	0.00	0.09	1.00	0.480	1.06	0.455	1.00	1.30	2.000	Yes
30	1.50	0.09	0.00	0.09	1.00	0.480	1.06	0.455	1.00	1.30	2.000	Yes
31	1.55	0.09	0.00	0.09	1.00	0.480	1.06	0.455	1.00	1.30	2.000	Yes
32	1.60	0.10	0.00	0.10	1.00	0.480	1.06	0.455	1.00	1.30	2.000	Yes
33	1.65	0.10	0.00	0.10	1.00	0.480	1.06	0.454	1.00	1.30	2.000	Yes
34	1.70	0.10	0.00	0.10	1.00	0.480	1.06	0.454	1.00	1.30	2.000	Yes
35	1.75	0.11	0.00	0.11	1.00	0.480	1.06	0.454	1.00	1.30	2.000	Yes
36	1.80	0.11	0.00	0.11	1.00	0.480	1.06	0.454	1.00	1.30	2.000	Yes
37	1.85	0.11	0.00	0.11	1.00	0.480	1.06	0.454	1.00	1.30	2.000	Yes
38	1.90	0.12	0.00	0.12	1.00	0.480	1.06	0.454	1.00	1.30	2.000	Yes
39	1.95	0.12	0.00	0.12	1.00	0.480	1.06	0.454	1.00	1.30	2.000	Yes
40	2.00	0.12	0.00	0.12	1.00	0.480	1.06	0.454	1.00	1.30	2.000	Yes
41	2.05	0.12	0.00	0.12	1.00	0.480	1.06	0.454	1.00	1.30	2.000	Yes
42	2.10	0.13	0.00	0.13	1.00	0.480	1.06	0.454	1.00	1.30	2.000	Yes
43	2.15	0.13	0.00	0.13	1.00	0.480	1.06	0.454	1.00	1.30	2.000	Yes
44	2.20	0.13	0.00	0.13	1.00	0.479	1.06	0.454	1.00	1.30	2.000	Yes
45	2.25	0.14	0.00	0.14	1.00	0.479	1.06	0.454	1.00	1.30	2.000	Yes
46	2.30	0.14	0.00	0.14	1.00	0.479	1.06	0.454	1.00	1.30	2.000	Yes
47	2.35	0.14	0.00	0.14	1.00	0.479	1.06	0.454	1.00	1.30	2.000	Yes
48	2.40	0.15	0.00	0.15	1.00	0.479	1.06	0.454	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
49	2.45	0.15	0.00	0.15	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
50	2.50	0.15	0.00	0.15	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
51	2.55	0.16	0.00	0.16	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
52	2.60	0.16	0.00	0.16	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
53	2.65	0.16	0.00	0.16	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
54	2.70	0.16	0.00	0.16	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
55	2.75	0.17	0.00	0.17	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
56	2.80	0.17	0.00	0.17	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
57	2.85	0.17	0.00	0.17	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
58	2.90	0.18	0.00	0.18	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
59	2.95	0.18	0.00	0.18	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
60	3.00	0.18	0.00	0.18	0.99	0.479	1.06	0.453	1.00	1.30	2.000	No
61	3.05	0.19	0.00	0.19	0.99	0.479	1.06	0.453	1.00	1.30	2.000	No
62	3.10	0.19	0.00	0.19	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
63	3.15	0.19	0.00	0.19	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
64	3.20	0.20	0.00	0.20	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
65	3.25	0.20	0.00	0.20	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
66	3.30	0.20	0.00	0.20	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
67	3.35	0.20	0.00	0.20	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
68	3.40	0.21	0.00	0.21	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
69	3.45	0.21	0.00	0.21	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
70	3.50	0.21	0.00	0.21	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
71	3.55	0.22	0.00	0.22	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
72	3.60	0.22	0.00	0.22	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
73	3.65	0.22	0.00	0.22	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
74	3.70	0.23	0.00	0.23	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
75	3.75	0.23	0.00	0.23	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
76	3.80	0.23	0.00	0.23	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
77	3.85	0.23	0.00	0.23	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
78	3.90	0.24	0.00	0.24	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
79	3.95	0.24	0.00	0.24	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
80	4.00	0.24	0.00	0.24	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
81	4.05	0.25	0.00	0.25	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
82	4.10	0.25	0.00	0.25	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
83	4.15	0.25	0.00	0.25	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
84	4.20	0.25	0.00	0.25	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
85	4.25	0.26	0.00	0.26	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
86	4.30	0.26	0.00	0.26	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
87	4.35	0.26	0.00	0.26	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
88	4.40	0.27	0.00	0.27	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
89	4.45	0.27	0.00	0.27	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
90	4.50	0.27	0.00	0.27	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
91	4.55	0.27	0.00	0.27	0.99	0.477	1.06	0.451	1.00	1.30	2.000	Yes
92	4.60	0.28	0.00	0.28	0.99	0.477	1.06	0.451	1.00	1.30	2.000	Yes
93	4.65	0.28	0.00	0.28	0.99	0.477	1.06	0.451	1.00	1.30	2.000	Yes
94	4.70	0.28	0.00	0.28	0.99	0.477	1.06	0.451	1.00	1.30	2.000	Yes
95	4.75	0.29	0.00	0.29	0.99	0.477	1.06	0.451	1.00	1.30	2.000	Yes
96	4.80	0.29	0.00	0.29	0.99	0.477	1.06	0.451	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
97	4.85	0.29	0.00	0.29	0.99	0.476	1.06	0.451	1.00	1.30	2.000	Yes
98	4.90	0.29	0.00	0.29	0.99	0.476	1.06	0.451	1.00	1.30	2.000	Yes
99	4.95	0.30	0.00	0.30	0.99	0.476	1.06	0.451	1.00	1.30	2.000	Yes
100	5.00	0.30	0.00	0.30	0.99	0.476	1.06	0.451	1.00	1.30	2.000	Yes
101	5.05	0.30	0.00	0.30	0.99	0.476	1.06	0.451	1.00	1.30	2.000	Yes
102	5.10	0.31	0.00	0.31	0.99	0.476	1.06	0.451	1.00	1.30	2.000	Yes
103	5.15	0.31	0.00	0.31	0.99	0.476	1.06	0.451	1.00	1.30	2.000	Yes
104	5.20	0.31	0.00	0.31	0.99	0.476	1.06	0.451	1.00	1.30	2.000	Yes
105	5.25	0.32	0.00	0.32	0.99	0.476	1.06	0.451	1.00	1.30	2.000	Yes
106	5.30	0.32	0.00	0.32	0.99	0.476	1.06	0.451	1.00	1.30	2.000	Yes
107	5.35	0.32	0.00	0.32	0.99	0.476	1.06	0.451	1.00	1.30	2.000	Yes
108	5.40	0.32	0.00	0.32	0.99	0.476	1.06	0.450	1.00	1.30	2.000	Yes
109	5.45	0.33	0.00	0.33	0.99	0.476	1.06	0.450	1.00	1.30	2.000	Yes
110	5.50	0.33	0.00	0.33	0.99	0.476	1.06	0.450	1.00	1.30	2.000	Yes
111	5.55	0.33	0.00	0.33	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
112	5.60	0.33	0.00	0.33	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
113	5.65	0.34	0.00	0.34	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
114	5.70	0.34	0.00	0.34	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
115	5.75	0.34	0.00	0.34	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
116	5.80	0.35	0.00	0.35	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
117	5.85	0.35	0.00	0.35	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
118	5.90	0.35	0.00	0.35	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
119	5.95	0.35	0.00	0.35	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
120	6.00	0.36	0.00	0.36	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
121	6.05	0.36	0.00	0.36	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
122	6.10	0.36	0.00	0.36	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
123	6.15	0.37	0.00	0.37	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
124	6.20	0.37	0.00	0.37	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
125	6.25	0.37	0.00	0.37	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
126	6.30	0.37	0.00	0.37	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
127	6.35	0.38	0.00	0.38	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
128	6.40	0.38	0.00	0.38	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
129	6.45	0.38	0.00	0.38	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
130	6.50	0.39	0.00	0.39	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
131	6.55	0.39	0.00	0.39	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
132	6.60	0.39	0.00	0.39	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
133	6.65	0.39	0.00	0.39	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
134	6.70	0.40	0.00	0.40	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
135	6.75	0.40	0.00	0.40	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
136	6.80	0.40	0.00	0.40	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
137	6.85	0.40	0.00	0.40	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
138	6.90	0.41	0.00	0.41	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
139	6.95	0.41	0.00	0.41	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
140	7.00	0.41	0.00	0.41	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
141	7.05	0.42	0.00	0.42	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
142	7.10	0.42	0.00	0.42	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
143	7.15	0.42	0.00	0.42	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
144	7.20	0.42	0.00	0.42	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
145	7.25	0.43	0.00	0.43	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
146	7.30	0.43	0.00	0.43	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
147	7.35	0.43	0.00	0.43	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
148	7.40	0.43	0.00	0.43	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
149	7.45	0.44	0.00	0.44	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
150	7.50	0.44	0.00	0.44	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
151	7.55	0.44	0.00	0.44	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
152	7.60	0.45	0.00	0.45	0.98	0.473	1.06	0.448	1.00	1.30	2.000	Yes
153	7.65	0.45	0.00	0.45	0.98	0.473	1.06	0.448	1.00	1.30	2.000	Yes
154	7.70	0.45	0.00	0.45	0.98	0.473	1.06	0.448	1.00	1.30	2.000	Yes
155	7.75	0.45	0.00	0.45	0.98	0.473	1.06	0.448	1.00	1.30	2.000	Yes
156	7.80	0.46	0.00	0.46	0.98	0.473	1.06	0.448	1.00	1.30	2.000	Yes
157	7.85	0.46	0.00	0.46	0.98	0.473	1.06	0.448	1.00	1.30	2.000	Yes
158	7.90	0.46	0.00	0.46	0.98	0.473	1.06	0.448	1.00	1.30	2.000	Yes
159	7.95	0.47	0.00	0.47	0.98	0.473	1.06	0.448	1.00	1.30	2.000	Yes
160	8.00	0.47	0.00	0.47	0.98	0.473	1.06	0.448	1.00	1.30	2.000	Yes
161	8.05	0.47	0.00	0.47	0.98	0.475	1.06	0.449	1.00	1.30	2.000	Yes
162	8.10	0.47	0.00	0.47	0.98	0.476	1.06	0.451	1.00	1.30	2.000	Yes
163	8.15	0.48	0.00	0.47	0.98	0.478	1.06	0.452	1.00	1.30	2.000	Yes
164	8.20	0.48	0.01	0.47	0.98	0.479	1.06	0.453	1.00	1.30	2.000	Yes
165	8.25	0.48	0.01	0.48	0.98	0.481	1.06	0.455	1.00	1.30	2.000	Yes
166	8.30	0.49	0.01	0.48	0.98	0.482	1.06	0.456	1.00	1.30	2.000	Yes
167	8.35	0.49	0.01	0.48	0.98	0.483	1.06	0.458	1.00	1.30	2.000	Yes
168	8.40	0.49	0.01	0.48	0.98	0.485	1.06	0.459	1.00	1.30	2.000	Yes
169	8.45	0.49	0.01	0.48	0.98	0.486	1.06	0.460	1.00	1.30	2.000	Yes
170	8.50	0.50	0.02	0.48	0.98	0.488	1.06	0.462	1.00	1.30	0.600	No
171	8.55	0.50	0.02	0.48	0.98	0.489	1.06	0.463	1.00	1.30	0.602	No
172	8.60	0.50	0.02	0.48	0.98	0.491	1.06	0.464	1.00	1.30	0.604	No
173	8.65	0.51	0.02	0.49	0.98	0.492	1.06	0.466	1.00	1.30	0.606	No
174	8.70	0.51	0.02	0.49	0.98	0.493	1.06	0.467	1.00	1.30	0.607	No
175	8.75	0.51	0.02	0.49	0.98	0.495	1.06	0.468	1.00	1.30	0.609	No
176	8.80	0.51	0.02	0.49	0.98	0.496	1.06	0.470	1.00	1.30	0.611	No
177	8.85	0.52	0.03	0.49	0.98	0.498	1.06	0.471	1.00	1.30	0.612	No
178	8.90	0.52	0.03	0.49	0.98	0.499	1.06	0.472	1.00	1.30	0.614	No
179	8.95	0.52	0.03	0.49	0.98	0.500	1.06	0.474	1.00	1.30	2.000	Yes
180	9.00	0.53	0.03	0.49	0.98	0.502	1.06	0.475	1.00	1.30	2.000	Yes
181	9.05	0.53	0.03	0.50	0.98	0.503	1.06	0.476	1.00	1.30	2.000	Yes
182	9.10	0.53	0.03	0.50	0.98	0.504	1.06	0.478	1.00	1.30	2.000	Yes
183	9.15	0.53	0.04	0.50	0.98	0.506	1.06	0.479	1.00	1.30	2.000	Yes
184	9.20	0.54	0.04	0.50	0.98	0.507	1.06	0.480	1.00	1.30	2.000	Yes
185	9.25	0.54	0.04	0.50	0.98	0.508	1.06	0.481	1.00	1.30	2.000	Yes
186	9.30	0.54	0.04	0.50	0.98	0.510	1.06	0.483	1.00	1.30	2.000	Yes
187	9.35	0.55	0.04	0.50	0.98	0.511	1.06	0.484	1.00	1.30	2.000	Yes
188	9.40	0.55	0.04	0.51	0.98	0.512	1.06	0.485	1.00	1.30	2.000	Yes
189	9.45	0.55	0.05	0.51	0.98	0.514	1.06	0.486	1.00	1.30	2.000	Yes
190	9.50	0.55	0.05	0.51	0.98	0.515	1.06	0.487	1.00	1.30	2.000	Yes
191	9.55	0.56	0.05	0.51	0.98	0.516	1.06	0.489	1.00	1.30	2.000	Yes
192	9.60	0.56	0.05	0.51	0.98	0.518	1.06	0.490	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
193	9.65	0.56	0.05	0.51	0.98	0.519	1.06	0.491	1.00	1.30	2.000	Yes
194	9.70	0.57	0.05	0.51	0.98	0.520	1.06	0.492	1.00	1.30	2.000	Yes
195	9.75	0.57	0.05	0.51	0.98	0.521	1.06	0.493	1.00	1.30	2.000	Yes
196	9.80	0.57	0.06	0.52	0.98	0.523	1.06	0.495	1.00	1.30	2.000	Yes
197	9.85	0.57	0.06	0.52	0.98	0.524	1.06	0.496	1.00	1.30	2.000	Yes
198	9.90	0.58	0.06	0.52	0.98	0.525	1.06	0.497	1.00	1.30	2.000	Yes
199	9.95	0.58	0.06	0.52	0.98	0.526	1.06	0.498	1.00	1.30	2.000	Yes
200	10.00	0.58	0.06	0.52	0.98	0.527	1.06	0.499	1.00	1.30	2.000	Yes
201	10.05	0.59	0.06	0.52	0.98	0.529	1.06	0.500	1.00	1.30	2.000	Yes
202	10.10	0.59	0.07	0.52	0.98	0.530	1.06	0.502	1.00	1.30	2.000	Yes
203	10.15	0.59	0.07	0.52	0.98	0.531	1.06	0.503	1.00	1.30	2.000	Yes
204	10.20	0.59	0.07	0.53	0.98	0.532	1.06	0.504	1.00	1.30	2.000	Yes
205	10.25	0.60	0.07	0.53	0.98	0.533	1.06	0.505	1.00	1.30	2.000	Yes
206	10.30	0.60	0.07	0.53	0.98	0.535	1.06	0.506	1.00	1.30	2.000	Yes
207	10.35	0.60	0.07	0.53	0.98	0.536	1.06	0.507	1.00	1.30	0.659	No
208	10.40	0.61	0.07	0.53	0.98	0.537	1.06	0.508	1.00	1.30	0.661	No
209	10.45	0.61	0.08	0.53	0.98	0.538	1.06	0.509	1.00	1.30	0.662	No
210	10.50	0.61	0.08	0.53	0.98	0.539	1.06	0.510	1.00	1.30	0.664	No
211	10.55	0.61	0.08	0.53	0.98	0.540	1.06	0.512	1.00	1.30	0.665	No
212	10.60	0.62	0.08	0.54	0.98	0.542	1.06	0.513	1.00	1.30	0.666	No
213	10.65	0.62	0.08	0.54	0.98	0.543	1.06	0.514	1.00	1.30	0.668	No
214	10.70	0.62	0.08	0.54	0.98	0.544	1.06	0.515	1.00	1.30	0.669	No
215	10.75	0.63	0.09	0.54	0.98	0.545	1.06	0.516	1.00	1.30	0.671	No
216	10.80	0.63	0.09	0.54	0.98	0.546	1.06	0.517	1.00	1.30	0.672	No
217	10.85	0.63	0.09	0.54	0.98	0.547	1.06	0.518	1.00	1.30	0.673	No
218	10.90	0.63	0.09	0.54	0.98	0.548	1.06	0.519	1.00	1.30	0.675	No
219	10.95	0.64	0.09	0.54	0.98	0.549	1.06	0.520	1.00	1.30	0.676	No
220	11.00	0.64	0.09	0.55	0.98	0.551	1.06	0.521	1.00	1.30	0.677	No
221	11.05	0.64	0.10	0.55	0.98	0.552	1.06	0.522	1.00	1.30	0.679	No
222	11.10	0.65	0.10	0.55	0.98	0.553	1.06	0.523	1.00	1.30	0.680	No
223	11.15	0.65	0.10	0.55	0.98	0.554	1.06	0.524	1.00	1.30	0.681	No
224	11.20	0.65	0.10	0.55	0.98	0.555	1.06	0.525	1.00	1.30	0.683	No
225	11.25	0.65	0.10	0.55	0.98	0.556	1.06	0.526	1.00	1.30	0.684	No
226	11.30	0.66	0.10	0.55	0.98	0.557	1.06	0.527	1.00	1.30	0.685	No
227	11.35	0.66	0.10	0.55	0.98	0.558	1.06	0.528	1.00	1.30	0.687	No
228	11.40	0.66	0.11	0.56	0.98	0.559	1.06	0.529	1.00	1.30	0.688	No
229	11.45	0.67	0.11	0.56	0.98	0.560	1.06	0.530	1.00	1.30	0.689	No
230	11.50	0.67	0.11	0.56	0.98	0.561	1.06	0.531	1.00	1.30	2.000	Yes
231	11.55	0.67	0.11	0.56	0.98	0.562	1.06	0.532	1.00	1.30	2.000	Yes
232	11.60	0.67	0.11	0.56	0.98	0.563	1.06	0.533	1.00	1.30	2.000	Yes
233	11.65	0.68	0.11	0.56	0.98	0.564	1.06	0.534	1.00	1.30	2.000	Yes
234	11.70	0.68	0.12	0.56	0.98	0.565	1.06	0.535	1.00	1.30	2.000	Yes
235	11.75	0.68	0.12	0.57	0.98	0.566	1.06	0.536	1.00	1.30	2.000	Yes
236	11.80	0.68	0.12	0.57	0.98	0.567	1.06	0.537	1.00	1.30	2.000	Yes
237	11.85	0.69	0.12	0.57	0.98	0.568	1.06	0.538	1.00	1.30	2.000	Yes
238	11.90	0.69	0.12	0.57	0.98	0.569	1.06	0.539	1.00	1.30	2.000	Yes
239	11.95	0.69	0.12	0.57	0.98	0.570	1.06	0.540	1.00	1.30	2.000	Yes
240	12.00	0.70	0.12	0.57	0.97	0.571	1.06	0.541	1.00	1.30	0.703	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
241	12.05	0.70	0.13	0.57	0.97	0.572	1.06	0.542	1.00	1.30	2.000	Yes
242	12.10	0.70	0.13	0.57	0.97	0.573	1.06	0.543	1.00	1.30	2.000	Yes
243	12.15	0.71	0.13	0.58	0.97	0.574	1.06	0.544	1.00	1.30	2.000	Yes
244	12.20	0.71	0.13	0.58	0.97	0.575	1.06	0.544	1.00	1.30	2.000	Yes
245	12.25	0.71	0.13	0.58	0.97	0.576	1.06	0.545	1.00	1.30	2.000	Yes
246	12.30	0.71	0.13	0.58	0.97	0.577	1.06	0.546	1.00	1.30	2.000	Yes
247	12.35	0.72	0.14	0.58	0.97	0.578	1.06	0.547	1.00	1.30	2.000	Yes
248	12.40	0.72	0.14	0.58	0.97	0.579	1.06	0.548	1.00	1.30	0.713	No
249	12.45	0.72	0.14	0.58	0.97	0.580	1.06	0.549	1.00	1.30	2.000	Yes
250	12.50	0.73	0.14	0.58	0.97	0.581	1.06	0.550	1.00	1.30	2.000	Yes
251	12.55	0.73	0.14	0.59	0.97	0.582	1.06	0.551	1.00	1.30	2.000	Yes
252	12.60	0.73	0.14	0.59	0.97	0.583	1.06	0.552	1.00	1.30	2.000	Yes
253	12.65	0.73	0.15	0.59	0.97	0.584	1.06	0.553	1.00	1.30	2.000	Yes
254	12.70	0.74	0.15	0.59	0.97	0.585	1.06	0.553	1.00	1.30	2.000	Yes
255	12.75	0.74	0.15	0.59	0.97	0.585	1.06	0.554	1.00	1.30	2.000	Yes
256	12.80	0.74	0.15	0.59	0.97	0.586	1.06	0.555	1.00	1.30	2.000	Yes
257	12.85	0.75	0.15	0.59	0.97	0.587	1.06	0.556	1.00	1.30	2.000	Yes
258	12.90	0.75	0.15	0.60	0.97	0.588	1.06	0.557	1.00	1.30	2.000	Yes
259	12.95	0.75	0.15	0.60	0.97	0.589	1.06	0.558	1.00	1.30	2.000	Yes
260	13.00	0.75	0.16	0.60	0.97	0.590	1.06	0.558	1.00	1.30	0.726	No
261	13.05	0.76	0.16	0.60	0.97	0.591	1.06	0.559	1.00	1.30	0.727	No
262	13.10	0.76	0.16	0.60	0.97	0.592	1.06	0.560	1.00	1.30	0.728	No
263	13.15	0.76	0.16	0.60	0.97	0.593	1.06	0.561	1.00	1.30	0.729	No
264	13.20	0.77	0.16	0.60	0.97	0.593	1.06	0.562	1.00	1.30	0.730	No
265	13.25	0.77	0.16	0.60	0.97	0.594	1.06	0.563	1.00	1.30	0.731	No
266	13.30	0.77	0.17	0.61	0.97	0.595	1.06	0.563	1.00	1.30	0.733	No
267	13.35	0.77	0.17	0.61	0.97	0.596	1.06	0.564	1.00	1.30	0.734	No
268	13.40	0.78	0.17	0.61	0.97	0.597	1.06	0.565	1.00	1.30	0.735	No
269	13.45	0.78	0.17	0.61	0.97	0.598	1.06	0.566	1.00	1.30	0.736	No
270	13.50	0.78	0.17	0.61	0.97	0.599	1.06	0.567	1.00	1.30	0.737	No
271	13.55	0.79	0.17	0.61	0.97	0.600	1.06	0.568	1.00	1.30	0.738	No
272	13.60	0.79	0.17	0.61	0.97	0.600	1.06	0.568	1.00	1.30	0.739	No
273	13.65	0.79	0.18	0.61	0.97	0.601	1.06	0.569	1.00	1.30	0.740	No
274	13.70	0.79	0.18	0.62	0.97	0.602	1.06	0.570	1.00	1.30	0.741	No
275	13.75	0.80	0.18	0.62	0.97	0.603	1.06	0.571	1.00	1.30	0.742	No
276	13.80	0.80	0.18	0.62	0.97	0.604	1.06	0.572	1.00	1.30	0.743	No
277	13.85	0.80	0.18	0.62	0.97	0.605	1.06	0.572	1.00	1.30	0.744	No
278	13.90	0.80	0.18	0.62	0.97	0.606	1.06	0.573	1.00	1.30	0.745	No
279	13.95	0.81	0.19	0.62	0.97	0.606	1.06	0.574	1.00	1.30	0.746	No
280	14.00	0.81	0.19	0.62	0.97	0.607	1.06	0.575	1.00	1.30	0.747	No
281	14.05	0.81	0.19	0.62	0.97	0.608	1.06	0.576	1.00	1.30	0.748	No
282	14.10	0.82	0.19	0.63	0.97	0.609	1.06	0.576	1.00	1.30	0.749	No
283	14.15	0.82	0.19	0.63	0.97	0.610	1.06	0.577	1.00	1.30	0.750	No
284	14.20	0.82	0.19	0.63	0.97	0.610	1.06	0.578	1.00	1.30	0.751	No
285	14.25	0.82	0.20	0.63	0.97	0.611	1.06	0.579	1.00	1.30	0.752	No
286	14.30	0.83	0.20	0.63	0.97	0.612	1.06	0.579	1.00	1.30	0.753	No
287	14.35	0.83	0.20	0.63	0.97	0.613	1.06	0.580	1.00	1.30	0.754	No
288	14.40	0.83	0.20	0.63	0.97	0.613	1.06	0.581	1.00	1.30	0.755	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
289	14.45	0.84	0.20	0.64	0.97	0.614	1.06	0.581	1.00	1.30	0.756	No
290	14.50	0.84	0.20	0.64	0.97	0.615	1.06	0.582	1.00	1.30	0.757	No
291	14.55	0.84	0.20	0.64	0.97	0.616	1.06	0.583	1.00	1.30	0.758	No
292	14.60	0.85	0.21	0.64	0.97	0.616	1.06	0.584	1.00	1.30	0.759	No
293	14.65	0.85	0.21	0.64	0.97	0.617	1.06	0.584	1.00	1.30	0.760	No
294	14.70	0.85	0.21	0.64	0.97	0.618	1.06	0.585	1.00	1.30	0.761	No
295	14.75	0.85	0.21	0.64	0.97	0.619	1.06	0.586	1.00	1.30	0.761	No
296	14.80	0.86	0.21	0.64	0.97	0.619	1.06	0.586	1.00	1.30	0.762	No
297	14.85	0.86	0.21	0.65	0.97	0.620	1.06	0.587	1.00	1.30	0.763	No
298	14.90	0.86	0.22	0.65	0.97	0.621	1.06	0.588	1.00	1.30	0.764	No
299	14.95	0.87	0.22	0.65	0.97	0.622	1.06	0.589	1.00	1.30	0.765	No
300	15.00	0.87	0.22	0.65	0.97	0.622	1.06	0.589	1.00	1.30	0.766	No
301	15.05	0.87	0.22	0.65	0.97	0.623	1.06	0.590	1.00	1.30	0.767	No
302	15.10	0.87	0.22	0.65	0.97	0.624	1.06	0.591	1.00	1.30	0.768	No
303	15.15	0.88	0.22	0.65	0.97	0.625	1.06	0.591	1.00	1.30	0.769	No
304	15.20	0.88	0.22	0.65	0.97	0.625	1.06	0.592	1.00	1.30	0.770	No
305	15.25	0.88	0.23	0.66	0.97	0.626	1.06	0.593	1.00	1.30	0.771	No
306	15.30	0.89	0.23	0.66	0.97	0.627	1.06	0.593	1.00	1.30	0.771	No
307	15.35	0.89	0.23	0.66	0.97	0.628	1.06	0.594	1.00	1.30	0.772	No
308	15.40	0.89	0.23	0.66	0.97	0.628	1.06	0.595	1.00	1.30	0.773	No
309	15.45	0.89	0.23	0.66	0.97	0.629	1.06	0.595	1.00	1.30	0.774	No
310	15.50	0.90	0.23	0.66	0.97	0.630	1.06	0.596	1.00	1.30	0.775	No
311	15.55	0.90	0.24	0.66	0.97	0.630	1.06	0.597	1.00	1.30	0.776	No
312	15.60	0.90	0.24	0.67	0.97	0.631	1.06	0.597	1.00	1.30	0.777	No
313	15.65	0.90	0.24	0.67	0.97	0.632	1.06	0.598	1.00	1.30	0.778	No
314	15.70	0.91	0.24	0.67	0.97	0.633	1.06	0.599	1.00	1.30	0.778	No
315	15.75	0.91	0.24	0.67	0.97	0.633	1.06	0.599	1.00	1.30	0.779	No
316	15.80	0.91	0.24	0.67	0.97	0.634	1.06	0.600	1.00	1.30	0.780	No
317	15.85	0.92	0.24	0.67	0.97	0.635	1.06	0.601	1.00	1.30	0.781	No
318	15.90	0.92	0.25	0.67	0.97	0.635	1.06	0.601	1.00	1.30	0.782	No
319	15.95	0.92	0.25	0.67	0.97	0.636	1.06	0.602	1.00	1.30	0.783	No
320	16.00	0.93	0.25	0.68	0.97	0.637	1.06	0.603	1.00	1.30	0.783	No
321	16.05	0.93	0.25	0.68	0.97	0.637	1.06	0.603	1.00	1.30	0.784	No
322	16.10	0.93	0.25	0.68	0.97	0.638	1.06	0.604	1.00	1.30	0.785	No
323	16.15	0.93	0.25	0.68	0.97	0.638	1.06	0.604	1.00	1.30	0.786	No
324	16.20	0.94	0.26	0.68	0.97	0.639	1.06	0.605	1.00	1.30	0.787	No
325	16.25	0.94	0.26	0.68	0.97	0.640	1.06	0.606	1.00	1.30	0.787	No
326	16.30	0.94	0.26	0.68	0.97	0.640	1.06	0.606	1.00	1.30	0.788	No
327	16.35	0.95	0.26	0.69	0.97	0.641	1.06	0.607	1.00	1.30	0.789	No
328	16.40	0.95	0.26	0.69	0.97	0.642	1.06	0.607	1.00	1.30	0.790	No
329	16.45	0.95	0.26	0.69	0.97	0.642	1.06	0.608	1.00	1.30	0.790	No
330	16.50	0.95	0.27	0.69	0.97	0.643	1.06	0.609	1.00	1.30	0.791	No
331	16.55	0.96	0.27	0.69	0.97	0.643	1.06	0.609	1.00	1.30	0.792	No
332	16.60	0.96	0.27	0.69	0.97	0.644	1.06	0.610	1.00	1.30	0.793	No
333	16.65	0.96	0.27	0.69	0.96	0.645	1.06	0.610	1.00	1.30	0.793	No
334	16.70	0.97	0.27	0.69	0.96	0.645	1.06	0.611	1.00	1.30	0.794	No
335	16.75	0.97	0.27	0.70	0.96	0.646	1.06	0.611	1.00	1.30	0.795	No
336	16.80	0.97	0.27	0.70	0.96	0.647	1.06	0.612	1.00	1.30	0.796	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
337	16.85	0.98	0.28	0.70	0.96	0.647	1.06	0.613	1.00	1.30	0.796	No
338	16.90	0.98	0.28	0.70	0.96	0.648	1.06	0.613	1.00	1.30	0.797	No
339	16.95	0.98	0.28	0.70	0.96	0.648	1.06	0.614	1.00	1.30	0.798	No
340	17.00	0.98	0.28	0.70	0.96	0.649	1.06	0.614	1.00	1.30	2.000	Yes
341	17.05	0.99	0.28	0.70	0.96	0.650	1.06	0.615	1.00	1.30	2.000	Yes
342	17.10	0.99	0.28	0.71	0.96	0.650	1.06	0.615	1.00	1.30	2.000	Yes
343	17.15	0.99	0.29	0.71	0.96	0.651	1.06	0.616	1.00	1.30	2.000	Yes
344	17.20	1.00	0.29	0.71	0.96	0.651	1.06	0.616	1.00	1.30	2.000	Yes
345	17.25	1.00	0.29	0.71	0.96	0.652	1.06	0.617	1.00	1.30	2.000	Yes
346	17.30	1.00	0.29	0.71	0.96	0.652	1.06	0.618	1.00	1.30	2.000	Yes
347	17.35	1.01	0.29	0.71	0.96	0.653	1.06	0.618	1.00	1.30	2.000	Yes
348	17.40	1.01	0.29	0.71	0.96	0.653	1.06	0.619	1.00	1.30	2.000	Yes
349	17.45	1.01	0.29	0.72	0.96	0.654	1.06	0.619	1.00	1.30	2.000	Yes
350	17.50	1.01	0.30	0.72	0.96	0.655	1.06	0.620	1.00	1.30	2.000	Yes
351	17.55	1.02	0.30	0.72	0.96	0.655	1.06	0.620	1.00	1.30	0.806	No
352	17.60	1.02	0.30	0.72	0.96	0.656	1.06	0.621	1.00	1.30	2.000	Yes
353	17.65	1.02	0.30	0.72	0.96	0.656	1.06	0.621	1.00	1.30	2.000	Yes
354	17.70	1.03	0.30	0.72	0.96	0.657	1.06	0.622	1.00	1.30	2.000	Yes
355	17.75	1.03	0.30	0.72	0.96	0.657	1.06	0.622	1.00	1.30	2.000	Yes
356	17.80	1.03	0.31	0.73	0.96	0.658	1.06	0.623	1.00	1.30	2.000	Yes
357	17.85	1.03	0.31	0.73	0.96	0.658	1.06	0.623	1.00	1.30	2.000	Yes
358	17.90	1.04	0.31	0.73	0.96	0.659	1.06	0.624	1.00	1.30	2.000	Yes
359	17.95	1.04	0.31	0.73	0.96	0.659	1.06	0.624	1.00	1.30	2.000	Yes
360	18.00	1.04	0.31	0.73	0.96	0.660	1.06	0.625	1.00	1.30	2.000	Yes
361	18.05	1.05	0.31	0.73	0.96	0.661	1.06	0.625	1.00	1.30	2.000	Yes
362	18.10	1.05	0.32	0.73	0.96	0.661	1.06	0.626	1.00	1.30	2.000	Yes
363	18.15	1.05	0.32	0.74	0.96	0.662	1.06	0.626	1.00	1.30	2.000	Yes
364	18.20	1.06	0.32	0.74	0.96	0.662	1.06	0.627	1.00	1.30	2.000	Yes
365	18.25	1.06	0.32	0.74	0.96	0.663	1.06	0.627	1.00	1.30	2.000	Yes
366	18.30	1.06	0.32	0.74	0.96	0.663	1.06	0.628	1.00	1.30	2.000	Yes
367	18.35	1.06	0.32	0.74	0.96	0.664	1.06	0.628	1.00	1.30	2.000	Yes
368	18.40	1.07	0.32	0.74	0.96	0.664	1.06	0.629	1.00	1.30	2.000	Yes
369	18.45	1.07	0.33	0.74	0.96	0.665	1.06	0.629	1.00	1.30	2.000	Yes
370	18.50	1.07	0.33	0.75	0.96	0.665	1.06	0.629	1.00	1.30	2.000	Yes
371	18.55	1.08	0.33	0.75	0.96	0.665	1.06	0.630	1.00	1.30	2.000	Yes
372	18.60	1.08	0.33	0.75	0.96	0.666	1.06	0.630	1.00	1.30	2.000	Yes
373	18.65	1.08	0.33	0.75	0.96	0.666	1.06	0.631	1.00	1.30	2.000	Yes
374	18.70	1.09	0.33	0.75	0.96	0.667	1.06	0.631	1.00	1.30	2.000	Yes
375	18.75	1.09	0.34	0.75	0.96	0.667	1.06	0.632	1.00	1.30	2.000	Yes
376	18.80	1.09	0.34	0.76	0.96	0.668	1.06	0.632	1.00	1.30	2.000	Yes
377	18.85	1.10	0.34	0.76	0.96	0.668	1.06	0.633	1.00	1.30	2.000	Yes
378	18.90	1.10	0.34	0.76	0.96	0.669	1.06	0.633	1.00	1.30	2.000	Yes
379	18.95	1.10	0.34	0.76	0.96	0.669	1.06	0.633	1.00	1.30	2.000	Yes
380	19.00	1.10	0.34	0.76	0.96	0.670	1.06	0.634	1.00	1.30	2.000	Yes
381	19.05	1.11	0.34	0.76	0.96	0.670	1.06	0.634	1.00	1.30	2.000	Yes
382	19.10	1.11	0.35	0.76	0.96	0.671	1.06	0.635	1.00	1.30	2.000	Yes
383	19.15	1.11	0.35	0.77	0.96	0.671	1.06	0.635	1.00	1.30	2.000	Yes
384	19.20	1.12	0.35	0.77	0.96	0.671	1.06	0.636	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
385	19.25	1.12	0.35	0.77	0.96	0.672	1.06	0.636	1.00	1.30	2.000	Yes
386	19.30	1.12	0.35	0.77	0.96	0.672	1.06	0.637	1.00	1.30	2.000	Yes
387	19.35	1.12	0.35	0.77	0.96	0.673	1.06	0.637	1.00	1.30	0.828	No
388	19.40	1.13	0.36	0.77	0.96	0.673	1.06	0.637	1.00	1.30	0.829	No
389	19.45	1.13	0.36	0.77	0.96	0.674	1.06	0.638	1.00	1.30	0.829	No
390	19.50	1.13	0.36	0.77	0.96	0.674	1.06	0.638	1.00	1.30	0.830	No
391	19.55	1.14	0.36	0.78	0.96	0.675	1.06	0.639	1.00	1.30	0.830	No
392	19.60	1.14	0.36	0.78	0.96	0.675	1.06	0.639	1.00	1.30	0.831	No
393	19.65	1.14	0.36	0.78	0.96	0.676	1.06	0.640	1.00	1.30	0.832	No
394	19.70	1.15	0.37	0.78	0.96	0.676	1.06	0.640	1.00	1.30	0.832	No
395	19.75	1.15	0.37	0.78	0.96	0.677	1.06	0.641	1.00	1.30	0.833	No
396	19.80	1.15	0.37	0.78	0.96	0.677	1.06	0.641	1.00	1.30	0.833	No
397	19.85	1.15	0.37	0.78	0.96	0.678	1.06	0.641	1.00	1.30	0.834	No
398	19.90	1.16	0.37	0.79	0.96	0.678	1.06	0.642	1.00	1.30	0.834	No
399	19.95	1.16	0.37	0.79	0.96	0.678	1.06	0.642	1.00	1.30	0.835	No
400	20.00	1.16	0.37	0.79	0.96	0.679	1.06	0.643	1.00	1.30	0.835	No
401	20.05	1.17	0.38	0.79	0.96	0.679	1.06	0.643	1.00	1.30	0.836	No
402	20.10	1.17	0.38	0.79	0.96	0.680	1.06	0.643	1.00	1.30	0.837	No
403	20.15	1.17	0.38	0.79	0.96	0.680	1.06	0.644	1.00	1.30	0.837	No
404	20.20	1.17	0.38	0.79	0.96	0.681	1.06	0.644	1.00	1.30	0.838	No
405	20.25	1.18	0.38	0.79	0.96	0.681	1.06	0.645	1.00	1.30	0.838	No
406	20.30	1.18	0.38	0.80	0.96	0.682	1.06	0.645	1.00	1.30	0.839	No
407	20.35	1.18	0.39	0.80	0.96	0.682	1.06	0.646	1.00	1.30	0.839	No
408	20.40	1.19	0.39	0.80	0.96	0.683	1.06	0.646	1.00	1.30	0.840	No
409	20.45	1.19	0.39	0.80	0.96	0.683	1.06	0.647	1.00	1.30	0.840	No
410	20.50	1.19	0.39	0.80	0.96	0.683	1.06	0.647	1.00	1.30	0.841	No
411	20.55	1.19	0.39	0.80	0.96	0.684	1.06	0.647	1.00	1.30	0.842	No
412	20.60	1.20	0.39	0.80	0.96	0.684	1.06	0.648	1.00	1.30	0.842	No
413	20.65	1.20	0.39	0.81	0.96	0.685	1.06	0.648	1.00	1.30	0.843	No
414	20.70	1.20	0.40	0.81	0.96	0.685	1.06	0.649	1.00	1.30	0.843	No
415	20.75	1.21	0.40	0.81	0.95	0.686	1.06	0.649	1.00	1.30	0.844	No
416	20.80	1.21	0.40	0.81	0.95	0.686	1.06	0.649	1.00	1.30	0.844	No
417	20.85	1.21	0.40	0.81	0.95	0.686	1.06	0.650	1.00	1.30	0.845	No
418	20.90	1.21	0.40	0.81	0.95	0.687	1.06	0.650	1.00	1.30	0.845	No
419	20.95	1.22	0.40	0.81	0.95	0.687	1.06	0.650	1.00	1.30	0.846	No
420	21.00	1.22	0.41	0.81	0.95	0.687	1.06	0.651	1.00	1.30	0.846	No
421	21.05	1.22	0.41	0.82	0.95	0.688	1.06	0.651	1.00	1.30	0.846	No
422	21.10	1.23	0.41	0.82	0.95	0.688	1.06	0.652	1.00	1.30	0.847	No
423	21.15	1.23	0.41	0.82	0.95	0.689	1.06	0.652	1.00	1.30	0.847	No
424	21.20	1.23	0.41	0.82	0.95	0.689	1.06	0.652	1.00	1.30	0.848	No
425	21.25	1.24	0.41	0.82	0.95	0.689	1.06	0.653	1.00	1.30	0.848	No
426	21.30	1.24	0.41	0.82	0.95	0.690	1.06	0.653	1.00	1.30	0.849	No
427	21.35	1.24	0.42	0.82	0.95	0.690	1.06	0.653	1.00	1.30	0.849	No
428	21.40	1.24	0.42	0.83	0.95	0.691	1.06	0.654	1.00	1.30	0.850	No
429	21.45	1.25	0.42	0.83	0.95	0.691	1.06	0.654	1.00	1.30	0.850	No
430	21.50	1.25	0.42	0.83	0.95	0.691	1.06	0.654	1.00	1.30	0.851	No
431	21.55	1.25	0.42	0.83	0.95	0.692	1.06	0.655	1.00	1.30	0.851	No
432	21.60	1.26	0.42	0.83	0.95	0.692	1.06	0.655	1.00	1.30	0.852	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
433	21.65	1.26	0.43	0.83	0.95	0.693	1.06	0.656	1.00	1.30	0.852	No
434	21.70	1.26	0.43	0.83	0.95	0.693	1.06	0.656	1.00	1.30	0.853	No
435	21.75	1.26	0.43	0.83	0.95	0.693	1.06	0.656	1.00	1.30	0.853	No
436	21.80	1.27	0.43	0.84	0.95	0.694	1.06	0.657	1.00	1.30	0.854	No
437	21.85	1.27	0.43	0.84	0.95	0.694	1.06	0.657	1.00	1.30	0.854	No
438	21.90	1.27	0.43	0.84	0.95	0.695	1.06	0.658	1.00	1.30	0.855	No
439	21.95	1.27	0.44	0.84	0.95	0.695	1.06	0.658	1.00	1.30	0.855	No
440	22.00	1.28	0.44	0.84	0.95	0.695	1.06	0.658	1.00	1.30	0.856	No
441	22.05	1.28	0.44	0.84	0.95	0.696	1.06	0.659	1.00	1.30	0.856	No
442	22.10	1.28	0.44	0.84	0.95	0.696	1.06	0.659	1.00	1.30	0.857	No
443	22.15	1.29	0.44	0.84	0.95	0.697	1.06	0.659	1.00	1.30	0.857	No
444	22.20	1.29	0.44	0.85	0.95	0.697	1.06	0.660	1.00	1.30	0.858	No
445	22.25	1.29	0.44	0.85	0.95	0.697	1.06	0.660	1.00	1.30	0.858	No
446	22.30	1.29	0.45	0.85	0.95	0.698	1.06	0.660	1.00	1.30	0.859	No
447	22.35	1.30	0.45	0.85	0.95	0.698	1.06	0.661	1.00	1.30	0.859	No
448	22.40	1.30	0.45	0.85	0.95	0.698	1.06	0.661	1.00	1.30	0.859	No
449	22.45	1.30	0.45	0.85	0.95	0.699	1.06	0.661	1.00	1.30	0.860	No
450	22.50	1.31	0.45	0.85	0.95	0.699	1.06	0.662	1.00	1.30	0.860	No
451	22.55	1.31	0.45	0.86	0.95	0.699	1.06	0.662	1.00	1.30	0.861	No
452	22.60	1.31	0.46	0.86	0.95	0.700	1.06	0.662	1.00	1.30	0.861	No
453	22.65	1.31	0.46	0.86	0.95	0.700	1.06	0.663	1.00	1.30	0.862	No
454	22.70	1.32	0.46	0.86	0.95	0.700	1.06	0.663	1.00	1.30	0.862	No
455	22.75	1.32	0.46	0.86	0.95	0.701	1.06	0.663	1.00	1.30	0.862	No
456	22.80	1.32	0.46	0.86	0.95	0.701	1.06	0.664	1.00	1.30	0.863	No
457	22.85	1.33	0.46	0.86	0.95	0.701	1.06	0.664	1.00	1.30	0.863	No
458	22.90	1.33	0.46	0.86	0.95	0.702	1.06	0.664	1.00	1.30	0.864	No
459	22.95	1.33	0.47	0.87	0.95	0.702	1.06	0.665	1.00	1.30	0.864	No
460	23.00	1.34	0.47	0.87	0.95	0.702	1.06	0.665	1.00	1.30	0.864	No
461	23.05	1.34	0.47	0.87	0.95	0.703	1.06	0.665	1.00	1.30	0.865	No
462	23.10	1.34	0.47	0.87	0.95	0.703	1.06	0.666	1.00	1.30	0.865	No
463	23.15	1.34	0.47	0.87	0.95	0.703	1.06	0.666	1.00	1.30	0.866	No
464	23.20	1.35	0.47	0.87	0.95	0.704	1.06	0.666	1.00	1.30	0.866	No
465	23.25	1.35	0.48	0.87	0.95	0.704	1.06	0.666	1.00	1.30	0.866	No
466	23.30	1.35	0.48	0.87	0.95	0.704	1.06	0.667	1.00	1.30	0.867	No
467	23.35	1.36	0.48	0.88	0.95	0.705	1.06	0.667	1.00	1.30	0.867	No
468	23.40	1.36	0.48	0.88	0.95	0.705	1.06	0.667	1.00	1.30	0.868	No
469	23.45	1.36	0.48	0.88	0.95	0.705	1.06	0.668	1.00	1.30	0.868	No
470	23.50	1.36	0.48	0.88	0.95	0.706	1.06	0.668	1.00	1.30	0.868	No
471	23.55	1.37	0.49	0.88	0.95	0.706	1.06	0.668	1.00	1.30	0.869	No
472	23.60	1.37	0.49	0.88	0.95	0.706	1.06	0.669	1.00	1.30	0.869	No
473	23.65	1.37	0.49	0.88	0.95	0.707	1.06	0.669	1.00	1.30	0.870	No
474	23.70	1.38	0.49	0.89	0.95	0.707	1.06	0.669	1.00	1.30	0.870	No
475	23.75	1.38	0.49	0.89	0.95	0.707	1.06	0.669	1.00	1.30	0.870	No
476	23.80	1.38	0.49	0.89	0.95	0.707	1.06	0.670	1.00	1.30	0.871	No
477	23.85	1.38	0.49	0.89	0.95	0.708	1.06	0.670	1.00	1.30	0.871	No
478	23.90	1.39	0.50	0.89	0.95	0.708	1.06	0.670	1.00	1.30	0.871	No
479	23.95	1.39	0.50	0.89	0.95	0.708	1.06	0.671	1.00	1.30	0.872	No
480	24.00	1.39	0.50	0.89	0.95	0.709	1.06	0.671	1.00	1.30	0.872	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
481	24.05	1.40	0.50	0.89	0.95	0.709	1.06	0.671	1.00	1.30	0.873	No
482	24.10	1.40	0.50	0.90	0.94	0.709	1.06	0.671	1.00	1.30	0.873	No
483	24.15	1.40	0.50	0.90	0.94	0.710	1.06	0.672	1.00	1.30	0.873	No
484	24.20	1.40	0.51	0.90	0.94	0.710	1.06	0.672	1.00	1.30	0.874	No
485	24.25	1.41	0.51	0.90	0.94	0.710	1.06	0.672	1.00	1.30	0.874	No
486	24.30	1.41	0.51	0.90	0.94	0.711	1.06	0.673	1.00	1.30	2.000	Yes
487	24.35	1.41	0.51	0.90	0.94	0.711	1.06	0.673	1.00	1.30	2.000	Yes
488	24.40	1.42	0.51	0.90	0.94	0.711	1.06	0.673	1.00	1.30	2.000	Yes
489	24.45	1.42	0.51	0.91	0.94	0.711	1.06	0.673	1.00	1.30	2.000	Yes
490	24.50	1.42	0.51	0.91	0.94	0.712	1.06	0.674	1.00	1.30	2.000	Yes
491	24.55	1.42	0.52	0.91	0.94	0.712	1.06	0.674	1.00	1.30	2.000	Yes
492	24.60	1.43	0.52	0.91	0.94	0.712	1.06	0.674	1.00	1.30	2.000	Yes
493	24.65	1.43	0.52	0.91	0.94	0.712	1.06	0.674	1.00	1.30	2.000	Yes
494	24.70	1.43	0.52	0.91	0.94	0.712	1.06	0.674	1.00	1.30	2.000	Yes
495	24.75	1.44	0.52	0.91	0.94	0.713	1.06	0.675	1.00	1.30	2.000	Yes
496	24.80	1.44	0.52	0.92	0.94	0.713	1.06	0.675	1.00	1.30	2.000	Yes
497	24.85	1.44	0.53	0.92	0.94	0.713	1.06	0.675	1.00	1.30	2.000	Yes
498	24.90	1.45	0.53	0.92	0.94	0.713	1.06	0.675	1.00	1.30	2.000	Yes
499	24.95	1.45	0.53	0.92	0.94	0.714	1.06	0.675	1.00	1.30	2.000	Yes
500	25.00	1.45	0.53	0.92	0.94	0.714	1.06	0.676	1.00	1.30	2.000	Yes
501	25.05	1.45	0.53	0.92	0.94	0.714	1.06	0.676	1.00	1.30	2.000	Yes
502	25.10	1.46	0.53	0.92	0.94	0.714	1.06	0.676	1.00	1.30	2.000	Yes
503	25.15	1.46	0.54	0.93	0.94	0.714	1.06	0.676	1.00	1.30	2.000	Yes
504	25.20	1.46	0.54	0.93	0.94	0.715	1.06	0.676	1.00	1.30	2.000	Yes
505	25.25	1.47	0.54	0.93	0.94	0.715	1.06	0.677	1.00	1.30	0.880	No
506	25.30	1.47	0.54	0.93	0.94	0.715	1.06	0.677	1.00	1.30	0.880	No
507	25.35	1.47	0.54	0.93	0.94	0.715	1.06	0.677	1.00	1.30	0.880	No
508	25.40	1.48	0.54	0.93	0.94	0.715	1.06	0.677	1.00	1.30	0.880	No
509	25.45	1.48	0.54	0.93	0.94	0.716	1.06	0.677	1.00	1.30	0.881	No
510	25.50	1.48	0.55	0.94	0.94	0.716	1.06	0.678	1.00	1.30	0.881	No
511	25.55	1.49	0.55	0.94	0.94	0.716	1.06	0.678	1.00	1.30	0.881	No
512	25.60	1.49	0.55	0.94	0.94	0.716	1.06	0.678	1.00	1.30	0.881	No
513	25.65	1.49	0.55	0.94	0.94	0.716	1.06	0.678	1.00	1.30	0.882	No
514	25.70	1.49	0.55	0.94	0.94	0.717	1.06	0.678	1.00	1.30	0.882	No
515	25.75	1.50	0.55	0.94	0.94	0.717	1.06	0.679	1.00	1.30	0.882	No
516	25.80	1.50	0.56	0.95	0.94	0.717	1.06	0.679	1.00	1.30	0.882	No
517	25.85	1.50	0.56	0.95	0.94	0.717	1.06	0.679	1.00	1.30	0.883	No
518	25.90	1.51	0.56	0.95	0.94	0.717	1.06	0.679	1.00	1.30	0.883	No
519	25.95	1.51	0.56	0.95	0.94	0.717	1.06	0.679	1.00	1.30	0.883	No
520	26.00	1.51	0.56	0.95	0.94	0.718	1.06	0.679	1.00	1.30	0.883	No
521	26.05	1.52	0.56	0.95	0.94	0.718	1.06	0.680	1.00	1.30	0.883	No
522	26.10	1.52	0.56	0.95	0.94	0.718	1.06	0.680	1.00	1.30	0.884	No
523	26.15	1.52	0.57	0.96	0.94	0.718	1.06	0.680	1.00	1.30	0.884	No
524	26.20	1.53	0.57	0.96	0.94	0.718	1.06	0.680	1.00	1.30	0.884	No
525	26.25	1.53	0.57	0.96	0.94	0.718	1.06	0.680	1.00	1.30	0.884	No
526	26.30	1.53	0.57	0.96	0.94	0.719	1.06	0.680	1.00	1.30	2.000	Yes
527	26.35	1.53	0.57	0.96	0.94	0.719	1.06	0.680	1.00	1.30	2.000	Yes
528	26.40	1.54	0.57	0.96	0.94	0.719	1.06	0.681	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
529	26.45	1.54	0.58	0.96	0.94	0.719	1.06	0.681	1.00	1.30	2.000	Yes
530	26.50	1.54	0.58	0.97	0.94	0.719	1.06	0.681	1.00	1.30	2.000	Yes
531	26.55	1.55	0.58	0.97	0.94	0.719	1.06	0.681	1.00	1.30	2.000	Yes
532	26.60	1.55	0.58	0.97	0.94	0.720	1.06	0.681	1.00	1.30	2.000	Yes
533	26.65	1.55	0.58	0.97	0.94	0.720	1.06	0.681	1.00	1.30	2.000	Yes
534	26.70	1.56	0.58	0.97	0.94	0.720	1.06	0.681	1.00	1.30	2.000	Yes
535	26.75	1.56	0.59	0.97	0.94	0.720	1.06	0.682	1.00	1.30	2.000	Yes
536	26.80	1.56	0.59	0.98	0.94	0.720	1.06	0.682	1.00	1.30	2.000	Yes
537	26.85	1.57	0.59	0.98	0.93	0.720	1.06	0.682	1.00	1.30	2.000	Yes
538	26.90	1.57	0.59	0.98	0.93	0.720	1.06	0.682	1.00	1.30	2.000	Yes
539	26.95	1.57	0.59	0.98	0.93	0.721	1.06	0.682	1.00	1.30	2.000	Yes
540	27.00	1.57	0.59	0.98	0.93	0.721	1.06	0.682	1.00	1.30	2.000	Yes
541	27.05	1.58	0.59	0.98	0.93	0.721	1.06	0.682	1.00	1.30	2.000	Yes
542	27.10	1.58	0.60	0.98	0.93	0.721	1.06	0.683	1.00	1.30	2.000	Yes
543	27.15	1.58	0.60	0.99	0.93	0.721	1.06	0.683	1.00	1.30	0.887	No
544	27.20	1.59	0.60	0.99	0.93	0.721	1.06	0.683	1.00	1.30	0.888	No
545	27.25	1.59	0.60	0.99	0.93	0.721	1.06	0.683	1.00	1.30	0.888	No
546	27.30	1.59	0.60	0.99	0.93	0.722	1.06	0.683	1.00	1.30	0.888	No
547	27.35	1.60	0.60	0.99	0.93	0.722	1.06	0.683	1.00	1.30	0.888	No
548	27.40	1.60	0.61	0.99	0.93	0.722	1.06	0.683	1.00	1.30	0.888	No
549	27.45	1.60	0.61	1.00	0.93	0.722	1.06	0.683	1.00	1.30	0.888	No
550	27.50	1.61	0.61	1.00	0.93	0.722	1.06	0.684	1.00	1.30	0.889	No
551	27.55	1.61	0.61	1.00	0.93	0.722	1.06	0.684	1.00	1.30	0.889	No
552	27.60	1.61	0.61	1.00	0.93	0.722	1.06	0.684	1.00	1.30	0.889	No
553	27.65	1.61	0.61	1.00	0.93	0.722	1.06	0.684	1.00	1.30	0.889	No
554	27.70	1.62	0.61	1.00	0.93	0.723	1.06	0.684	1.00	1.30	0.889	No
555	27.75	1.62	0.62	1.00	0.93	0.723	1.06	0.684	1.00	1.30	0.889	No
556	27.80	1.62	0.62	1.01	0.93	0.723	1.06	0.684	1.00	1.30	0.889	No
557	27.85	1.63	0.62	1.01	0.93	0.723	1.06	0.684	1.00	1.30	0.890	No
558	27.90	1.63	0.62	1.01	0.93	0.723	1.06	0.684	1.00	1.30	0.890	No
559	27.95	1.63	0.62	1.01	0.93	0.723	1.06	0.684	1.00	1.30	0.890	No
560	28.00	1.64	0.62	1.01	0.93	0.723	1.06	0.685	1.00	1.30	0.890	No
561	28.05	1.64	0.63	1.01	0.93	0.723	1.06	0.685	1.00	1.30	0.890	No
562	28.10	1.64	0.63	1.02	0.93	0.723	1.06	0.685	1.00	1.30	0.890	No
563	28.15	1.65	0.63	1.02	0.93	0.723	1.06	0.685	1.00	1.30	0.890	No
564	28.20	1.65	0.63	1.02	0.93	0.724	1.06	0.685	1.00	1.30	0.890	No
565	28.25	1.65	0.63	1.02	0.93	0.724	1.06	0.685	1.00	1.30	0.891	No
566	28.30	1.65	0.63	1.02	0.93	0.724	1.06	0.685	1.00	1.30	0.891	No
567	28.35	1.66	0.63	1.02	0.93	0.724	1.06	0.685	1.00	1.30	0.891	No
568	28.40	1.66	0.64	1.02	0.93	0.724	1.06	0.685	1.00	1.30	0.891	No
569	28.45	1.66	0.64	1.03	0.93	0.724	1.06	0.685	1.00	1.30	0.891	No
570	28.50	1.67	0.64	1.03	0.93	0.724	1.06	0.686	1.00	1.30	0.891	No
571	28.55	1.67	0.64	1.03	0.93	0.724	1.06	0.686	1.00	1.30	0.891	No
572	28.60	1.67	0.64	1.03	0.93	0.724	1.06	0.686	1.00	1.30	0.891	No
573	28.65	1.68	0.64	1.03	0.93	0.724	1.06	0.686	1.00	1.30	0.892	No
574	28.70	1.68	0.65	1.03	0.93	0.725	1.06	0.686	1.00	1.30	0.892	No
575	28.75	1.68	0.65	1.03	0.93	0.725	1.06	0.686	1.00	1.30	0.892	No
576	28.80	1.68	0.65	1.04	0.93	0.725	1.06	0.686	1.00	1.30	0.892	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
577	28.85	1.69	0.65	1.04	0.93	0.725	1.06	0.686	1.00	1.30	0.892	No
578	28.90	1.69	0.65	1.04	0.93	0.725	1.06	0.686	1.00	1.30	0.892	No
579	28.95	1.69	0.65	1.04	0.93	0.725	1.06	0.686	1.00	1.30	0.892	No
580	29.00	1.70	0.66	1.04	0.93	0.725	1.06	0.687	1.00	1.30	0.893	No
581	29.05	1.70	0.66	1.04	0.93	0.725	1.06	0.687	1.00	1.30	0.893	No
582	29.10	1.70	0.66	1.04	0.92	0.726	1.06	0.687	1.00	1.30	0.893	No
583	29.15	1.70	0.66	1.04	0.92	0.726	1.06	0.687	1.00	1.30	0.893	No
584	29.20	1.71	0.66	1.05	0.92	0.726	1.06	0.687	1.00	1.30	0.893	No
585	29.25	1.71	0.66	1.05	0.92	0.726	1.06	0.687	1.00	1.30	0.894	No
586	29.30	1.71	0.66	1.05	0.92	0.726	1.06	0.688	1.00	1.30	0.894	No
587	29.35	1.72	0.67	1.05	0.92	0.726	1.06	0.688	1.00	1.30	0.894	No
588	29.40	1.72	0.67	1.05	0.92	0.727	1.06	0.688	1.00	1.30	0.894	No
589	29.45	1.72	0.67	1.05	0.92	0.727	1.06	0.688	1.00	1.30	0.894	No
590	29.50	1.72	0.67	1.05	0.92	0.727	1.06	0.688	1.00	1.30	0.895	No
591	29.55	1.73	0.67	1.05	0.92	0.727	1.06	0.688	1.00	1.30	0.895	No
592	29.60	1.73	0.67	1.06	0.92	0.727	1.06	0.688	1.00	1.30	0.895	No
593	29.65	1.73	0.68	1.06	0.92	0.727	1.06	0.688	1.00	1.30	0.895	No
594	29.70	1.73	0.68	1.06	0.92	0.727	1.06	0.689	1.00	1.30	0.895	No
595	29.75	1.74	0.68	1.06	0.92	0.727	1.06	0.689	1.00	1.30	0.895	No
596	29.80	1.74	0.68	1.06	0.92	0.728	1.06	0.689	1.00	1.30	0.895	No
597	29.85	1.74	0.68	1.06	0.92	0.728	1.06	0.689	1.00	1.30	0.896	No
598	29.90	1.75	0.68	1.06	0.92	0.728	1.06	0.689	1.00	1.30	0.896	No
599	29.95	1.75	0.68	1.06	0.92	0.728	1.06	0.689	1.00	1.30	0.896	No
600	30.00	1.75	0.69	1.07	0.92	0.728	1.06	0.689	1.00	1.30	0.896	No
601	30.05	1.75	0.69	1.07	0.92	0.728	1.06	0.689	1.00	1.30	0.896	No
602	30.10	1.76	0.69	1.07	0.92	0.728	1.06	0.689	1.00	1.30	0.896	No
603	30.15	1.76	0.69	1.07	0.92	0.728	1.06	0.689	1.00	1.30	0.896	No
604	30.20	1.76	0.69	1.07	0.92	0.728	1.06	0.690	1.00	1.30	0.896	No
605	30.25	1.77	0.69	1.07	0.92	0.728	1.06	0.690	1.00	1.30	0.896	No
606	30.30	1.77	0.70	1.07	0.92	0.729	1.06	0.690	1.00	1.30	0.897	No
607	30.35	1.77	0.70	1.08	0.92	0.729	1.06	0.690	1.00	1.30	0.897	No
608	30.40	1.78	0.70	1.08	0.92	0.729	1.06	0.690	1.00	1.30	0.897	No
609	30.45	1.78	0.70	1.08	0.92	0.729	1.06	0.690	1.00	1.30	0.897	No
610	30.50	1.78	0.70	1.08	0.92	0.729	1.06	0.690	1.00	1.30	2.000	Yes
611	30.55	1.78	0.70	1.08	0.92	0.729	1.06	0.690	1.00	1.30	2.000	Yes
612	30.60	1.79	0.71	1.08	0.92	0.729	1.06	0.690	1.00	1.30	2.000	Yes
613	30.65	1.79	0.71	1.08	0.92	0.729	1.06	0.690	1.00	1.30	2.000	Yes
614	30.70	1.79	0.71	1.09	0.92	0.729	1.06	0.690	1.00	1.30	2.000	Yes
615	30.75	1.80	0.71	1.09	0.92	0.729	1.06	0.690	1.00	1.30	2.000	Yes
616	30.80	1.80	0.71	1.09	0.92	0.729	1.06	0.690	1.00	1.30	2.000	Yes
617	30.85	1.80	0.71	1.09	0.92	0.729	1.06	0.690	1.00	1.30	2.000	Yes
618	30.90	1.81	0.71	1.09	0.92	0.729	1.06	0.690	1.00	1.30	2.000	Yes
619	30.95	1.81	0.72	1.09	0.92	0.729	1.06	0.690	1.00	1.30	2.000	Yes
620	31.00	1.81	0.72	1.10	0.92	0.729	1.06	0.690	1.00	1.30	2.000	Yes
621	31.05	1.82	0.72	1.10	0.92	0.729	1.06	0.690	1.00	1.30	2.000	Yes
622	31.10	1.82	0.72	1.10	0.91	0.729	1.06	0.690	1.00	1.30	2.000	Yes
623	31.15	1.82	0.72	1.10	0.91	0.729	1.06	0.690	1.00	1.30	2.000	Yes
624	31.20	1.83	0.72	1.10	0.91	0.729	1.06	0.690	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
625	31.25	1.83	0.73	1.10	0.91	0.729	1.06	0.690	1.00	1.30	0.897	No
626	31.30	1.83	0.73	1.11	0.91	0.729	1.06	0.690	1.00	1.30	0.897	No
627	31.35	1.84	0.73	1.11	0.91	0.729	1.06	0.690	1.00	1.30	0.897	No
628	31.40	1.84	0.73	1.11	0.91	0.728	1.06	0.690	1.00	1.30	0.896	No
629	31.45	1.84	0.73	1.11	0.91	0.728	1.06	0.690	1.00	1.30	0.896	No
630	31.50	1.85	0.73	1.11	0.91	0.728	1.06	0.689	1.00	1.30	0.896	No
631	31.55	1.85	0.73	1.11	0.91	0.728	1.06	0.689	1.00	1.30	0.896	No
632	31.60	1.85	0.74	1.12	0.91	0.728	1.06	0.689	1.00	1.30	0.896	No
633	31.65	1.86	0.74	1.12	0.91	0.728	1.06	0.689	1.00	1.30	0.896	No
634	31.70	1.86	0.74	1.12	0.91	0.728	1.06	0.689	1.00	1.30	0.896	No
635	31.75	1.86	0.74	1.12	0.91	0.728	1.06	0.689	1.00	1.30	0.896	No
636	31.80	1.87	0.74	1.12	0.91	0.728	1.06	0.689	1.00	1.30	0.896	No
637	31.85	1.87	0.74	1.12	0.91	0.728	1.06	0.689	1.00	1.30	0.896	No
638	31.90	1.87	0.75	1.13	0.91	0.728	1.06	0.689	1.00	1.30	0.896	No
639	31.95	1.88	0.75	1.13	0.91	0.728	1.06	0.689	1.00	1.30	0.895	No
640	32.00	1.88	0.75	1.13	0.91	0.728	1.06	0.689	1.00	1.30	0.895	No
641	32.05	1.88	0.75	1.13	0.91	0.727	1.06	0.689	1.00	1.30	0.895	No
642	32.10	1.89	0.75	1.13	0.91	0.727	1.06	0.689	1.00	1.30	0.895	No
643	32.15	1.89	0.75	1.14	0.91	0.727	1.06	0.688	1.00	1.30	0.895	No
644	32.20	1.89	0.76	1.14	0.91	0.727	1.06	0.688	1.00	1.30	0.895	No
645	32.25	1.90	0.76	1.14	0.91	0.727	1.06	0.688	1.00	1.30	0.895	No
646	32.30	1.90	0.76	1.14	0.91	0.727	1.06	0.688	1.00	1.30	0.895	No
647	32.35	1.90	0.76	1.14	0.91	0.727	1.06	0.688	1.00	1.30	0.895	No
648	32.40	1.91	0.76	1.14	0.91	0.727	1.06	0.688	1.00	1.30	0.894	No
649	32.45	1.91	0.76	1.15	0.91	0.727	1.06	0.688	1.00	1.30	0.894	No
650	32.50	1.91	0.76	1.15	0.91	0.727	1.06	0.688	1.00	1.30	0.894	No
651	32.55	1.92	0.77	1.15	0.91	0.726	1.06	0.688	1.00	1.30	0.894	No
652	32.60	1.92	0.77	1.15	0.91	0.726	1.06	0.688	1.00	1.30	0.894	No
653	32.65	1.92	0.77	1.15	0.91	0.726	1.06	0.687	1.00	1.30	0.894	No
654	32.70	1.93	0.77	1.16	0.91	0.726	1.06	0.687	1.00	1.30	0.894	No
655	32.75	1.93	0.77	1.16	0.91	0.726	1.06	0.687	1.00	1.30	0.893	No
656	32.80	1.93	0.77	1.16	0.90	0.726	1.06	0.687	1.00	1.30	0.893	No
657	32.85	1.94	0.78	1.16	0.90	0.726	1.06	0.687	1.00	1.30	0.893	No
658	32.90	1.94	0.78	1.16	0.90	0.726	1.06	0.687	1.00	1.30	0.893	No
659	32.95	1.94	0.78	1.16	0.90	0.726	1.06	0.687	1.00	1.30	0.893	No
660	33.00	1.95	0.78	1.17	0.90	0.725	1.06	0.687	1.00	1.30	0.893	No
661	33.05	1.95	0.78	1.17	0.90	0.725	1.06	0.687	1.00	1.30	0.893	No
662	33.10	1.95	0.78	1.17	0.90	0.725	1.06	0.687	1.00	1.30	0.893	No
663	33.15	1.96	0.78	1.17	0.90	0.725	1.06	0.686	1.00	1.30	0.892	No
664	33.20	1.96	0.79	1.17	0.90	0.725	1.06	0.686	1.00	1.30	0.892	No
665	33.25	1.96	0.79	1.18	0.90	0.725	1.06	0.686	1.00	1.30	0.892	No
666	33.30	1.97	0.79	1.18	0.90	0.725	1.06	0.686	1.00	1.30	0.892	No
667	33.35	1.97	0.79	1.18	0.90	0.725	1.06	0.686	1.00	1.30	0.892	No
668	33.40	1.97	0.79	1.18	0.90	0.725	1.06	0.686	1.00	1.30	0.892	No
669	33.45	1.98	0.79	1.18	0.90	0.724	1.06	0.686	1.00	1.30	0.892	No
670	33.50	1.98	0.80	1.18	0.90	0.724	1.06	0.686	1.00	1.30	0.891	No
671	33.55	1.98	0.80	1.19	0.90	0.724	1.06	0.686	1.00	1.30	0.891	No
672	33.60	1.99	0.80	1.19	0.90	0.724	1.06	0.685	1.00	1.30	0.891	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
673	33.65	1.99	0.80	1.19	0.90	0.724	1.06	0.685	1.00	1.30	0.891	No
674	33.70	1.99	0.80	1.19	0.90	0.724	1.06	0.685	1.00	1.30	0.891	No
675	33.75	2.00	0.80	1.19	0.90	0.724	1.06	0.685	1.00	1.30	0.891	No
676	33.80	2.00	0.80	1.19	0.90	0.724	1.06	0.685	1.00	1.30	0.891	No
677	33.85	2.00	0.81	1.20	0.90	0.724	1.06	0.685	1.00	1.30	0.890	No
678	33.90	2.01	0.81	1.20	0.90	0.723	1.06	0.685	1.00	1.30	0.890	No
679	33.95	2.01	0.81	1.20	0.90	0.723	1.06	0.685	1.00	1.30	0.890	No
680	34.00	2.01	0.81	1.20	0.90	0.723	1.06	0.685	1.00	1.30	0.890	No
681	34.05	2.02	0.81	1.20	0.90	0.723	1.06	0.684	1.00	1.30	0.890	No
682	34.10	2.02	0.81	1.20	0.90	0.723	1.06	0.684	1.00	1.30	0.890	No
683	34.15	2.02	0.82	1.21	0.90	0.723	1.06	0.684	1.00	1.30	0.890	No
684	34.20	2.03	0.82	1.21	0.90	0.723	1.06	0.684	1.00	1.30	0.889	No
685	34.25	2.03	0.82	1.21	0.90	0.723	1.06	0.684	1.00	1.30	0.889	No
686	34.30	2.03	0.82	1.21	0.90	0.722	1.06	0.684	1.00	1.30	0.889	No
687	34.35	2.03	0.82	1.21	0.90	0.722	1.06	0.684	1.00	1.30	0.889	No
688	34.40	2.04	0.82	1.21	0.89	0.722	1.06	0.684	1.00	1.30	0.889	No
689	34.45	2.04	0.83	1.22	0.89	0.722	1.06	0.684	1.00	1.30	0.889	No
690	34.50	2.04	0.83	1.22	0.89	0.722	1.06	0.683	1.00	1.30	0.888	No
691	34.55	2.05	0.83	1.22	0.89	0.722	1.06	0.683	1.00	1.30	0.888	No
692	34.60	2.05	0.83	1.22	0.89	0.722	1.06	0.683	1.00	1.30	0.888	No
693	34.65	2.05	0.83	1.22	0.89	0.722	1.06	0.683	1.00	1.30	0.888	No
694	34.70	2.06	0.83	1.22	0.89	0.721	1.06	0.683	1.00	1.30	0.888	No
695	34.75	2.06	0.83	1.23	0.89	0.721	1.06	0.683	1.00	1.30	0.888	No
696	34.80	2.06	0.84	1.23	0.89	0.721	1.06	0.683	1.00	1.30	0.887	No
697	34.85	2.07	0.84	1.23	0.89	0.721	1.06	0.683	1.00	1.30	0.887	No
698	34.90	2.07	0.84	1.23	0.89	0.721	1.06	0.682	1.00	1.30	0.887	No
699	34.95	2.07	0.84	1.23	0.89	0.721	1.06	0.682	1.00	1.30	0.887	No
700	35.00	2.08	0.84	1.24	0.89	0.721	1.06	0.682	1.00	1.30	0.887	No
701	35.05	2.08	0.84	1.24	0.89	0.720	1.06	0.682	1.00	1.30	0.887	No
702	35.10	2.08	0.85	1.24	0.89	0.720	1.06	0.682	1.00	1.30	0.886	No
703	35.15	2.09	0.85	1.24	0.89	0.720	1.06	0.682	1.00	1.30	0.886	No
704	35.20	2.09	0.85	1.24	0.89	0.720	1.06	0.682	1.00	1.30	0.886	No
705	35.25	2.09	0.85	1.24	0.89	0.720	1.06	0.681	1.00	1.30	0.886	No
706	35.30	2.10	0.85	1.25	0.89	0.720	1.06	0.681	1.00	1.30	0.886	No
707	35.35	2.10	0.85	1.25	0.89	0.719	1.06	0.681	1.00	1.30	0.885	No
708	35.40	2.10	0.85	1.25	0.89	0.719	1.06	0.681	1.00	1.30	0.885	No
709	35.45	2.11	0.86	1.25	0.89	0.719	1.06	0.681	1.00	1.30	0.885	No
710	35.50	2.11	0.86	1.25	0.89	0.719	1.06	0.681	1.00	1.30	0.885	No
711	35.55	2.11	0.86	1.25	0.89	0.719	1.06	0.680	1.00	1.30	0.885	No
712	35.60	2.12	0.86	1.26	0.89	0.719	1.06	0.680	1.00	1.30	0.884	No
713	35.65	2.12	0.86	1.26	0.89	0.718	1.06	0.680	1.00	1.30	0.884	No
714	35.70	2.12	0.86	1.26	0.89	0.718	1.06	0.680	1.00	1.30	0.884	No
715	35.75	2.13	0.87	1.26	0.89	0.718	1.06	0.680	1.00	1.30	0.884	No
716	35.80	2.13	0.87	1.26	0.88	0.718	1.06	0.680	1.00	1.30	0.883	No
717	35.85	2.13	0.87	1.26	0.88	0.718	1.06	0.679	1.00	1.30	0.883	No
718	35.90	2.14	0.87	1.27	0.88	0.718	1.06	0.679	1.00	1.30	0.883	No
719	35.95	2.14	0.87	1.27	0.88	0.717	1.06	0.679	1.00	1.30	0.883	No
720	36.00	2.14	0.87	1.27	0.88	0.717	1.06	0.679	1.00	1.30	0.883	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
721	36.05	2.15	0.88	1.27	0.88	0.717	1.06	0.679	1.00	1.30	0.882	No
722	36.10	2.15	0.88	1.27	0.88	0.717	1.06	0.679	1.00	1.30	0.882	No
723	36.15	2.15	0.88	1.28	0.88	0.717	1.06	0.678	1.00	1.30	0.882	No
724	36.20	2.16	0.88	1.28	0.88	0.716	1.06	0.678	1.00	1.30	0.882	No
725	36.25	2.16	0.88	1.28	0.88	0.716	1.06	0.678	1.00	1.30	0.881	No
726	36.30	2.16	0.88	1.28	0.88	0.716	1.06	0.678	1.00	1.30	0.881	No
727	36.35	2.17	0.88	1.28	0.88	0.716	1.06	0.678	1.00	1.30	0.881	No
728	36.40	2.17	0.89	1.28	0.88	0.716	1.06	0.678	1.00	1.30	0.881	No
729	36.45	2.17	0.89	1.29	0.88	0.716	1.06	0.677	1.00	1.30	0.881	No
730	36.50	2.18	0.89	1.29	0.88	0.715	1.06	0.677	1.00	1.30	0.880	No
731	36.55	2.18	0.89	1.29	0.88	0.715	1.06	0.677	1.00	1.30	0.880	No
732	36.60	2.18	0.89	1.29	0.88	0.715	1.06	0.677	1.00	1.30	0.880	No
733	36.65	2.19	0.89	1.29	0.88	0.715	1.06	0.677	1.00	1.30	0.880	No
734	36.70	2.19	0.90	1.29	0.88	0.715	1.06	0.677	1.00	1.30	0.879	No
735	36.75	2.19	0.90	1.30	0.88	0.714	1.06	0.676	1.00	1.30	0.879	No
736	36.80	2.20	0.90	1.30	0.88	0.714	1.06	0.676	1.00	1.30	2.000	Yes
737	36.85	2.20	0.90	1.30	0.88	0.714	1.06	0.676	1.00	1.30	2.000	Yes
738	36.90	2.20	0.90	1.30	0.88	0.714	1.06	0.676	1.00	1.30	2.000	Yes
739	36.95	2.21	0.90	1.30	0.88	0.714	1.06	0.676	1.00	1.30	2.000	Yes
740	37.00	2.21	0.90	1.30	0.88	0.714	1.06	0.675	1.00	1.30	2.000	Yes
741	37.05	2.21	0.91	1.31	0.88	0.713	1.06	0.675	1.00	1.30	2.000	Yes
742	37.10	2.22	0.91	1.31	0.88	0.713	1.06	0.675	1.00	1.30	2.000	Yes
743	37.15	2.22	0.91	1.31	0.87	0.713	1.06	0.675	1.00	1.30	2.000	Yes
744	37.20	2.22	0.91	1.31	0.87	0.713	1.06	0.675	1.00	1.30	2.000	Yes
745	37.25	2.22	0.91	1.31	0.87	0.713	1.06	0.675	1.00	1.30	2.000	Yes
746	37.30	2.23	0.91	1.31	0.87	0.713	1.06	0.675	1.00	1.30	2.000	Yes
747	37.35	2.23	0.92	1.32	0.87	0.712	1.06	0.674	1.00	1.30	2.000	Yes
748	37.40	2.23	0.92	1.32	0.87	0.712	1.06	0.674	1.00	1.30	2.000	Yes
749	37.45	2.24	0.92	1.32	0.87	0.712	1.06	0.674	1.00	1.30	0.876	No
750	37.50	2.24	0.92	1.32	0.87	0.712	1.06	0.674	1.00	1.30	0.876	No
751	37.55	2.24	0.92	1.32	0.87	0.712	1.06	0.674	1.00	1.30	0.876	No
752	37.60	2.25	0.92	1.32	0.87	0.712	1.06	0.674	1.00	1.30	0.876	No
753	37.65	2.25	0.93	1.32	0.87	0.711	1.06	0.674	1.00	1.30	0.876	No
754	37.70	2.25	0.93	1.33	0.87	0.711	1.06	0.673	1.00	1.30	0.875	No
755	37.75	2.26	0.93	1.33	0.87	0.711	1.06	0.673	1.00	1.30	0.875	No
756	37.80	2.26	0.93	1.33	0.87	0.711	1.06	0.673	1.00	1.30	0.875	No
757	37.85	2.26	0.93	1.33	0.87	0.711	1.06	0.673	1.00	1.30	0.875	No
758	37.90	2.26	0.93	1.33	0.87	0.711	1.06	0.673	1.00	1.30	0.875	No
759	37.95	2.27	0.93	1.33	0.87	0.710	1.06	0.673	1.00	1.30	2.000	Yes
760	38.00	2.27	0.94	1.33	0.87	0.710	1.06	0.672	1.00	1.30	2.000	Yes
761	38.05	2.27	0.94	1.34	0.87	0.710	1.06	0.672	1.00	1.30	2.000	Yes
762	38.10	2.28	0.94	1.34	0.87	0.710	1.06	0.672	1.00	1.30	2.000	Yes
763	38.15	2.28	0.94	1.34	0.87	0.710	1.06	0.672	1.00	1.30	2.000	Yes
764	38.20	2.28	0.94	1.34	0.87	0.709	1.06	0.672	1.00	1.30	2.000	Yes
765	38.25	2.29	0.94	1.34	0.87	0.709	1.06	0.671	1.00	1.30	2.000	Yes
766	38.30	2.29	0.95	1.34	0.87	0.709	1.06	0.671	1.00	1.30	2.000	Yes
767	38.35	2.29	0.95	1.35	0.87	0.709	1.06	0.671	1.00	1.30	2.000	Yes
768	38.40	2.30	0.95	1.35	0.86	0.709	1.06	0.671	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
769	38.45	2.30	0.95	1.35	0.86	0.708	1.06	0.671	1.00	1.30	0.872	No
770	38.50	2.30	0.95	1.35	0.86	0.708	1.06	0.670	1.00	1.30	0.872	No
771	38.55	2.31	0.95	1.35	0.86	0.708	1.06	0.670	1.00	1.30	0.871	No
772	38.60	2.31	0.95	1.35	0.86	0.708	1.06	0.670	1.00	1.30	0.871	No
773	38.65	2.31	0.96	1.36	0.86	0.708	1.06	0.670	1.00	1.30	0.871	No
774	38.70	2.31	0.96	1.36	0.86	0.707	1.06	0.670	1.00	1.30	0.871	No
775	38.75	2.32	0.96	1.36	0.86	0.707	1.06	0.670	1.00	1.30	0.870	No
776	38.80	2.32	0.96	1.36	0.86	0.707	1.06	0.669	1.00	1.30	0.870	No
777	38.85	2.32	0.96	1.36	0.86	0.707	1.06	0.669	1.00	1.30	0.870	No
778	38.90	2.33	0.96	1.36	0.86	0.707	1.06	0.669	1.00	1.30	0.870	No
779	38.95	2.33	0.97	1.36	0.86	0.706	1.06	0.669	1.00	1.30	0.869	No
780	39.00	2.33	0.97	1.37	0.86	0.706	1.06	0.668	1.00	1.30	0.869	No
781	39.05	2.34	0.97	1.37	0.86	0.706	1.06	0.668	1.00	1.30	0.869	No
782	39.10	2.34	0.97	1.37	0.86	0.706	1.06	0.668	1.00	1.30	2.000	Yes
783	39.15	2.34	0.97	1.37	0.86	0.706	1.06	0.668	1.00	1.30	2.000	Yes
784	39.20	2.35	0.97	1.37	0.86	0.705	1.06	0.668	1.00	1.30	2.000	Yes
785	39.25	2.35	0.98	1.37	0.86	0.705	1.06	0.667	1.00	1.30	2.000	Yes
786	39.30	2.35	0.98	1.38	0.86	0.705	1.06	0.667	1.00	1.30	2.000	Yes
787	39.35	2.36	0.98	1.38	0.86	0.705	1.06	0.667	1.00	1.30	2.000	Yes
788	39.40	2.36	0.98	1.38	0.86	0.704	1.06	0.667	1.00	1.30	2.000	Yes
789	39.45	2.36	0.98	1.38	0.86	0.704	1.06	0.667	1.00	1.30	2.000	Yes
790	39.50	2.37	0.98	1.38	0.86	0.704	1.06	0.666	1.00	1.30	2.000	Yes
791	39.55	2.37	0.98	1.38	0.85	0.704	1.06	0.666	1.00	1.30	2.000	Yes
792	39.60	2.37	0.99	1.39	0.85	0.703	1.06	0.666	1.00	1.30	2.000	Yes
793	39.65	2.38	0.99	1.39	0.85	0.703	1.06	0.666	1.00	1.30	0.865	No
794	39.70	2.38	0.99	1.39	0.85	0.703	1.06	0.665	1.00	1.30	2.000	Yes
795	39.75	2.38	0.99	1.39	0.85	0.703	1.06	0.665	1.00	1.30	2.000	Yes
796	39.80	2.38	0.99	1.39	0.85	0.702	1.06	0.665	1.00	1.30	2.000	Yes
797	39.85	2.39	0.99	1.39	0.85	0.702	1.06	0.665	1.00	1.30	2.000	Yes
798	39.90	2.39	1.00	1.40	0.85	0.702	1.06	0.665	1.00	1.30	2.000	Yes
799	39.95	2.39	1.00	1.40	0.85	0.702	1.06	0.664	1.00	1.30	2.000	Yes
800	40.00	2.40	1.00	1.40	0.85	0.702	1.06	0.664	1.00	1.30	2.000	Yes
801	40.05	2.40	1.00	1.40	0.85	0.701	1.06	0.664	1.00	1.30	2.000	Yes
802	40.10	2.40	1.00	1.40	0.85	0.701	1.06	0.664	1.00	1.30	2.000	Yes
803	40.15	2.41	1.00	1.40	0.85	0.701	1.06	0.663	1.00	1.30	0.862	No
804	40.20	2.41	1.00	1.41	0.85	0.701	1.06	0.663	1.00	1.30	0.862	No
805	40.25	2.41	1.01	1.41	0.85	0.700	1.06	0.663	1.00	1.30	0.862	No
806	40.30	2.42	1.01	1.41	0.85	0.700	1.06	0.663	1.00	1.30	0.862	No
807	40.35	2.42	1.01	1.41	0.85	0.700	1.06	0.663	1.00	1.30	0.861	No
808	40.40	2.42	1.01	1.41	0.85	0.700	1.06	0.662	1.00	1.30	0.861	No
809	40.45	2.43	1.01	1.41	0.85	0.699	1.06	0.662	1.00	1.30	0.861	No
810	40.50	2.43	1.01	1.41	0.85	0.699	1.06	0.662	1.00	1.30	0.860	No
811	40.55	2.43	1.02	1.42	0.85	0.699	1.06	0.662	1.00	1.30	0.860	No
812	40.60	2.43	1.02	1.42	0.85	0.699	1.06	0.661	1.00	1.30	2.000	Yes
813	40.65	2.44	1.02	1.42	0.85	0.698	1.06	0.661	1.00	1.30	2.000	Yes
814	40.70	2.44	1.02	1.42	0.84	0.698	1.06	0.661	1.00	1.30	2.000	Yes
815	40.75	2.44	1.02	1.42	0.84	0.698	1.06	0.661	1.00	1.30	2.000	Yes
816	40.80	2.45	1.02	1.42	0.84	0.698	1.06	0.660	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
817	40.85	2.45	1.02	1.43	0.84	0.697	1.06	0.660	1.00	1.30	2.000	Yes
818	40.90	2.45	1.03	1.43	0.84	0.697	1.06	0.660	1.00	1.30	2.000	Yes
819	40.95	2.46	1.03	1.43	0.84	0.697	1.06	0.660	1.00	1.30	2.000	Yes
820	41.00	2.46	1.03	1.43	0.84	0.697	1.06	0.659	1.00	1.30	2.000	Yes
821	41.05	2.46	1.03	1.43	0.84	0.696	1.06	0.659	1.00	1.30	2.000	Yes
822	41.10	2.47	1.03	1.43	0.84	0.696	1.06	0.659	1.00	1.30	2.000	Yes
823	41.15	2.47	1.03	1.43	0.84	0.696	1.06	0.659	1.00	1.30	2.000	Yes
824	41.20	2.47	1.04	1.44	0.84	0.696	1.06	0.659	1.00	1.30	2.000	Yes
825	41.25	2.48	1.04	1.44	0.84	0.695	1.06	0.658	1.00	1.30	2.000	Yes
826	41.30	2.48	1.04	1.44	0.84	0.695	1.06	0.658	1.00	1.30	2.000	Yes
827	41.35	2.48	1.04	1.44	0.84	0.695	1.06	0.658	1.00	1.30	2.000	Yes
828	41.40	2.48	1.04	1.44	0.84	0.695	1.06	0.658	1.00	1.30	2.000	Yes
829	41.45	2.49	1.04	1.44	0.84	0.694	1.06	0.657	1.00	1.30	2.000	Yes
830	41.50	2.49	1.05	1.45	0.84	0.694	1.06	0.657	1.00	1.30	2.000	Yes
831	41.55	2.49	1.05	1.45	0.84	0.694	1.06	0.657	1.00	1.30	2.000	Yes
832	41.60	2.50	1.05	1.45	0.84	0.694	1.06	0.657	1.00	1.30	0.853	No
833	41.65	2.50	1.05	1.45	0.84	0.693	1.06	0.656	1.00	1.30	2.000	Yes
834	41.70	2.50	1.05	1.45	0.84	0.693	1.06	0.656	1.00	1.30	2.000	Yes
835	41.75	2.51	1.05	1.45	0.84	0.693	1.06	0.656	1.00	1.30	2.000	Yes
836	41.80	2.51	1.05	1.46	0.83	0.692	1.06	0.656	1.00	1.30	2.000	Yes
837	41.85	2.51	1.06	1.46	0.83	0.692	1.06	0.655	1.00	1.30	2.000	Yes
838	41.90	2.52	1.06	1.46	0.83	0.692	1.06	0.655	1.00	1.30	2.000	Yes
839	41.95	2.52	1.06	1.46	0.83	0.692	1.06	0.655	1.00	1.30	2.000	Yes
840	42.00	2.52	1.06	1.46	0.83	0.691	1.06	0.654	1.00	1.30	2.000	Yes
841	42.05	2.53	1.06	1.46	0.83	0.691	1.06	0.654	1.00	1.30	2.000	Yes
842	42.10	2.53	1.06	1.46	0.83	0.691	1.06	0.654	1.00	1.30	2.000	Yes
843	42.15	2.53	1.07	1.47	0.83	0.691	1.06	0.654	1.00	1.30	2.000	Yes
844	42.20	2.53	1.07	1.47	0.83	0.690	1.06	0.653	1.00	1.30	2.000	Yes
845	42.25	2.54	1.07	1.47	0.83	0.690	1.06	0.653	1.00	1.30	0.849	No
846	42.30	2.54	1.07	1.47	0.83	0.690	1.06	0.653	1.00	1.30	0.849	No
847	42.35	2.54	1.07	1.47	0.83	0.689	1.06	0.653	1.00	1.30	0.848	No
848	42.40	2.55	1.07	1.47	0.83	0.689	1.06	0.652	1.00	1.30	0.848	No
849	42.45	2.55	1.07	1.48	0.83	0.689	1.06	0.652	1.00	1.30	0.848	No
850	42.50	2.55	1.08	1.48	0.83	0.689	1.06	0.652	1.00	1.30	0.847	No
851	42.55	2.56	1.08	1.48	0.83	0.688	1.06	0.652	1.00	1.30	0.847	No
852	42.60	2.56	1.08	1.48	0.83	0.688	1.06	0.651	1.00	1.30	0.847	No
853	42.65	2.56	1.08	1.48	0.83	0.688	1.06	0.651	1.00	1.30	0.846	No
854	42.70	2.57	1.08	1.48	0.83	0.687	1.06	0.651	1.00	1.30	0.846	No
855	42.75	2.57	1.08	1.48	0.83	0.687	1.06	0.651	1.00	1.30	0.846	No
856	42.80	2.57	1.09	1.49	0.83	0.687	1.06	0.650	1.00	1.30	0.845	No
857	42.85	2.58	1.09	1.49	0.82	0.687	1.06	0.650	1.00	1.30	2.000	Yes
858	42.90	2.58	1.09	1.49	0.82	0.686	1.06	0.650	1.00	1.30	2.000	Yes
859	42.95	2.58	1.09	1.49	0.82	0.686	1.06	0.649	1.00	1.30	2.000	Yes
860	43.00	2.58	1.09	1.49	0.82	0.686	1.06	0.649	1.00	1.30	2.000	Yes
861	43.05	2.59	1.09	1.49	0.82	0.685	1.06	0.649	1.00	1.30	2.000	Yes
862	43.10	2.59	1.10	1.50	0.82	0.685	1.06	0.649	1.00	1.30	2.000	Yes
863	43.15	2.59	1.10	1.50	0.82	0.685	1.06	0.648	1.00	1.30	2.000	Yes
864	43.20	2.60	1.10	1.50	0.82	0.685	1.06	0.648	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
865	43.25	2.60	1.10	1.50	0.82	0.684	1.06	0.648	1.00	1.30	2.000	Yes
866	43.30	2.60	1.10	1.50	0.82	0.684	1.06	0.647	1.00	1.30	0.842	No
867	43.35	2.61	1.10	1.50	0.82	0.684	1.06	0.647	1.00	1.30	2.000	Yes
868	43.40	2.61	1.10	1.51	0.82	0.683	1.06	0.647	1.00	1.30	2.000	Yes
869	43.45	2.61	1.11	1.51	0.82	0.683	1.06	0.647	1.00	1.30	2.000	Yes
870	43.50	2.62	1.11	1.51	0.82	0.683	1.06	0.646	1.00	1.30	2.000	Yes
871	43.55	2.62	1.11	1.51	0.82	0.682	1.06	0.646	1.00	1.30	2.000	Yes
872	43.60	2.62	1.11	1.51	0.82	0.682	1.06	0.646	1.00	1.30	2.000	Yes
873	43.65	2.63	1.11	1.51	0.82	0.682	1.06	0.645	1.00	1.30	2.000	Yes
874	43.70	2.63	1.11	1.52	0.82	0.681	1.06	0.645	1.00	1.30	0.839	No
875	43.75	2.63	1.12	1.52	0.82	0.681	1.06	0.645	1.00	1.30	2.000	Yes
876	43.80	2.64	1.12	1.52	0.82	0.681	1.06	0.644	1.00	1.30	2.000	Yes
877	43.85	2.64	1.12	1.52	0.82	0.680	1.06	0.644	1.00	1.30	2.000	Yes
878	43.90	2.64	1.12	1.52	0.81	0.680	1.06	0.644	1.00	1.30	2.000	Yes
879	43.95	2.65	1.12	1.52	0.81	0.680	1.06	0.644	1.00	1.30	2.000	Yes
880	44.00	2.65	1.12	1.53	0.81	0.679	1.06	0.643	1.00	1.30	2.000	Yes
881	44.05	2.65	1.12	1.53	0.81	0.679	1.06	0.643	1.00	1.30	2.000	Yes
882	44.10	2.66	1.13	1.53	0.81	0.679	1.06	0.643	1.00	1.30	2.000	Yes
883	44.15	2.66	1.13	1.53	0.81	0.678	1.06	0.642	1.00	1.30	2.000	Yes
884	44.20	2.66	1.13	1.53	0.81	0.678	1.06	0.642	1.00	1.30	2.000	Yes
885	44.25	2.67	1.13	1.53	0.81	0.678	1.06	0.642	1.00	1.30	2.000	Yes
886	44.30	2.67	1.13	1.54	0.81	0.677	1.06	0.641	1.00	1.30	2.000	Yes
887	44.35	2.67	1.13	1.54	0.81	0.677	1.06	0.641	1.00	1.30	2.000	Yes
888	44.40	2.67	1.14	1.54	0.81	0.677	1.06	0.641	1.00	1.30	0.833	No
889	44.45	2.68	1.14	1.54	0.81	0.676	1.06	0.640	1.00	1.30	0.832	No
890	44.50	2.68	1.14	1.54	0.81	0.676	1.06	0.640	1.00	1.30	0.832	No
891	44.55	2.68	1.14	1.54	0.81	0.676	1.06	0.640	1.00	1.30	0.832	No
892	44.60	2.69	1.14	1.55	0.81	0.675	1.06	0.639	1.00	1.30	0.831	No
893	44.65	2.69	1.14	1.55	0.81	0.675	1.06	0.639	1.00	1.30	0.831	No
894	44.70	2.70	1.15	1.55	0.81	0.675	1.06	0.639	1.00	1.30	0.830	No
895	44.75	2.70	1.15	1.55	0.81	0.674	1.06	0.638	1.00	1.30	0.830	No
896	44.80	2.70	1.15	1.55	0.81	0.674	1.06	0.638	1.00	1.30	0.829	No
897	44.85	2.71	1.15	1.56	0.81	0.674	1.06	0.638	1.00	1.30	0.829	No
898	44.90	2.71	1.15	1.56	0.80	0.673	1.06	0.637	1.00	1.30	0.828	No
899	44.95	2.71	1.15	1.56	0.80	0.673	1.06	0.637	1.00	1.30	0.828	No
900	45.00	2.72	1.15	1.56	0.80	0.672	1.06	0.637	1.00	1.30	0.828	No
901	45.05	2.72	1.16	1.56	0.80	0.672	1.06	0.636	1.00	1.30	0.827	No
902	45.10	2.72	1.16	1.56	0.80	0.672	1.06	0.636	1.00	1.30	0.827	No
903	45.15	2.73	1.16	1.57	0.80	0.671	1.06	0.636	1.00	1.30	0.826	No
904	45.20	2.73	1.16	1.57	0.80	0.671	1.06	0.635	1.00	1.30	0.826	No
905	45.25	2.73	1.16	1.57	0.80	0.671	1.06	0.635	1.00	1.30	0.825	No
906	45.30	2.74	1.16	1.57	0.80	0.670	1.06	0.635	1.00	1.30	0.825	No
907	45.35	2.74	1.17	1.57	0.80	0.670	1.06	0.634	1.00	1.30	0.824	No
908	45.40	2.74	1.17	1.57	0.80	0.670	1.06	0.634	1.00	1.30	0.824	No
909	45.45	2.75	1.17	1.58	0.80	0.669	1.06	0.634	1.00	1.30	0.824	No
910	45.50	2.75	1.17	1.58	0.80	0.669	1.06	0.633	1.00	1.30	0.823	No
911	45.55	2.75	1.17	1.58	0.80	0.668	1.06	0.633	1.00	1.30	0.823	No
912	45.60	2.76	1.17	1.58	0.80	0.668	1.06	0.632	1.00	1.30	0.822	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
913	45.65	2.76	1.17	1.58	0.80	0.668	1.06	0.632	1.00	1.30	0.822	No
914	45.70	2.76	1.18	1.59	0.80	0.667	1.06	0.632	1.00	1.30	0.821	No
915	45.75	2.77	1.18	1.59	0.80	0.667	1.06	0.631	1.00	1.30	0.821	No
916	45.80	2.77	1.18	1.59	0.80	0.667	1.06	0.631	1.00	1.30	0.820	No
917	45.85	2.77	1.18	1.59	0.80	0.666	1.06	0.631	1.00	1.30	0.820	No
918	45.90	2.78	1.18	1.59	0.79	0.666	1.06	0.630	1.00	1.30	0.820	No
919	45.95	2.78	1.18	1.59	0.79	0.666	1.06	0.630	1.00	1.30	0.819	No
920	46.00	2.78	1.19	1.60	0.79	0.665	1.06	0.630	1.00	1.30	0.819	No
921	46.05	2.79	1.19	1.60	0.79	0.665	1.06	0.629	1.00	1.30	0.818	No
922	46.10	2.79	1.19	1.60	0.79	0.664	1.06	0.629	1.00	1.30	0.818	No
923	46.15	2.79	1.19	1.60	0.79	0.664	1.06	0.629	1.00	1.30	0.817	No
924	46.20	2.79	1.19	1.60	0.79	0.664	1.06	0.628	1.00	1.30	0.817	No
925	46.25	2.80	1.19	1.60	0.79	0.663	1.06	0.628	1.00	1.30	0.816	No
926	46.30	2.80	1.19	1.61	0.79	0.663	1.06	0.628	1.00	1.30	0.816	No
927	46.35	2.80	1.20	1.61	0.79	0.663	1.06	0.627	1.00	1.30	0.816	No
928	46.40	2.81	1.20	1.61	0.79	0.662	1.06	0.627	1.00	1.30	0.815	No
929	46.45	2.81	1.20	1.61	0.79	0.662	1.06	0.627	1.00	1.30	0.815	No
930	46.50	2.81	1.20	1.61	0.79	0.662	1.06	0.626	1.00	1.30	0.814	No
931	46.55	2.82	1.20	1.61	0.79	0.661	1.06	0.626	1.00	1.30	0.814	No
932	46.60	2.82	1.20	1.62	0.79	0.661	1.06	0.626	1.00	1.30	0.813	No
933	46.65	2.82	1.21	1.62	0.79	0.661	1.06	0.625	1.00	1.30	0.813	No
934	46.70	2.83	1.21	1.62	0.79	0.660	1.06	0.625	1.00	1.30	0.812	No
935	46.75	2.83	1.21	1.62	0.79	0.660	1.06	0.625	1.00	1.30	0.812	No
936	46.80	2.83	1.21	1.62	0.79	0.660	1.06	0.624	1.00	1.30	0.812	No
937	46.85	2.84	1.21	1.63	0.78	0.659	1.06	0.624	1.00	1.30	0.811	No
938	46.90	2.84	1.21	1.63	0.78	0.659	1.06	0.624	1.00	1.30	0.811	No
939	46.95	2.84	1.22	1.63	0.78	0.658	1.06	0.623	1.00	1.30	0.810	No
940	47.00	2.85	1.22	1.63	0.78	0.658	1.06	0.623	1.00	1.30	0.810	No
941	47.05	2.85	1.22	1.63	0.78	0.658	1.06	0.623	1.00	1.30	0.809	No
942	47.10	2.85	1.22	1.63	0.78	0.657	1.06	0.622	1.00	1.30	0.809	No
943	47.15	2.86	1.22	1.63	0.78	0.657	1.06	0.622	1.00	1.30	0.809	No
944	47.20	2.86	1.22	1.64	0.78	0.657	1.06	0.622	1.00	1.30	2.000	Yes
945	47.25	2.86	1.22	1.64	0.78	0.656	1.06	0.621	1.00	1.30	2.000	Yes
946	47.30	2.87	1.23	1.64	0.78	0.656	1.06	0.621	1.00	1.30	2.000	Yes
947	47.35	2.87	1.23	1.64	0.78	0.656	1.06	0.621	1.00	1.30	2.000	Yes
948	47.40	2.87	1.23	1.64	0.78	0.655	1.06	0.620	1.00	1.30	2.000	Yes
949	47.45	2.88	1.23	1.64	0.78	0.655	1.06	0.620	1.00	1.30	2.000	Yes
950	47.50	2.88	1.23	1.65	0.78	0.655	1.06	0.620	1.00	1.30	2.000	Yes
951	47.55	2.88	1.23	1.65	0.78	0.654	1.06	0.619	1.00	1.30	2.000	Yes
952	47.60	2.88	1.24	1.65	0.78	0.654	1.06	0.619	1.00	1.30	2.000	Yes
953	47.65	2.89	1.24	1.65	0.78	0.654	1.06	0.619	1.00	1.30	2.000	Yes
954	47.70	2.89	1.24	1.65	0.78	0.653	1.06	0.618	1.00	1.30	2.000	Yes
955	47.75	2.89	1.24	1.65	0.78	0.653	1.06	0.618	1.00	1.30	2.000	Yes
956	47.80	2.90	1.24	1.66	0.78	0.652	1.06	0.618	1.00	1.30	2.000	Yes
957	47.85	2.90	1.24	1.66	0.77	0.652	1.06	0.617	1.00	1.30	2.000	Yes
958	47.90	2.90	1.24	1.66	0.77	0.652	1.06	0.617	1.00	1.30	2.000	Yes
959	47.95	2.91	1.25	1.66	0.77	0.651	1.06	0.617	1.00	1.30	0.802	No
960	48.00	2.91	1.25	1.66	0.77	0.651	1.06	0.616	1.00	1.30	0.801	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
961	48.05	2.91	1.25	1.66	0.77	0.651	1.06	0.616	1.00	1.30	0.801	No
962	48.10	2.92	1.25	1.67	0.77	0.650	1.06	0.616	1.00	1.30	0.800	No
963	48.15	2.92	1.25	1.67	0.77	0.650	1.06	0.615	1.00	1.30	0.800	No
964	48.20	2.92	1.25	1.67	0.77	0.649	1.06	0.615	1.00	1.30	0.799	No
965	48.25	2.93	1.26	1.67	0.77	0.649	1.06	0.614	1.00	1.30	0.799	No
966	48.30	2.93	1.26	1.67	0.77	0.649	1.06	0.614	1.00	1.30	0.798	No
967	48.35	2.93	1.26	1.68	0.77	0.648	1.06	0.614	1.00	1.30	0.798	No
968	48.40	2.94	1.26	1.68	0.77	0.648	1.06	0.613	1.00	1.30	0.797	No
969	48.45	2.94	1.26	1.68	0.77	0.648	1.06	0.613	1.00	1.30	0.797	No
970	48.50	2.94	1.26	1.68	0.77	0.647	1.06	0.613	1.00	1.30	0.796	No
971	48.55	2.95	1.27	1.68	0.77	0.647	1.06	0.612	1.00	1.30	0.796	No
972	48.60	2.95	1.27	1.68	0.77	0.646	1.06	0.612	1.00	1.30	2.000	Yes
973	48.65	2.95	1.27	1.69	0.77	0.646	1.06	0.612	1.00	1.30	2.000	Yes
974	48.70	2.96	1.27	1.69	0.77	0.646	1.06	0.611	1.00	1.30	2.000	Yes
975	48.75	2.96	1.27	1.69	0.77	0.645	1.06	0.611	1.00	1.30	2.000	Yes
976	48.80	2.96	1.27	1.69	0.76	0.645	1.06	0.611	1.00	1.30	2.000	Yes
977	48.85	2.97	1.27	1.69	0.76	0.645	1.06	0.610	1.00	1.30	2.000	Yes
978	48.90	2.97	1.28	1.69	0.76	0.644	1.06	0.610	1.00	1.30	2.000	Yes
979	48.95	2.97	1.28	1.70	0.76	0.644	1.06	0.609	1.00	1.30	2.000	Yes
980	49.00	2.98	1.28	1.70	0.76	0.643	1.06	0.609	1.00	1.30	2.000	Yes
981	49.05	2.98	1.28	1.70	0.76	0.643	1.06	0.609	1.00	1.30	0.791	No
982	49.10	2.98	1.28	1.70	0.76	0.643	1.06	0.608	1.00	1.30	2.000	Yes
983	49.15	2.99	1.28	1.70	0.76	0.642	1.06	0.608	1.00	1.30	2.000	Yes
984	49.20	2.99	1.29	1.70	0.76	0.642	1.06	0.608	1.00	1.30	2.000	Yes
985	49.25	2.99	1.29	1.71	0.76	0.642	1.06	0.607	1.00	1.30	2.000	Yes
986	49.30	3.00	1.29	1.71	0.76	0.641	1.06	0.607	1.00	1.30	2.000	Yes
987	49.35	3.00	1.29	1.71	0.76	0.641	1.06	0.607	1.00	1.30	2.000	Yes
988	49.40	3.00	1.29	1.71	0.76	0.640	1.06	0.606	1.00	1.30	0.788	No
989	49.45	3.01	1.29	1.71	0.76	0.640	1.06	0.606	1.00	1.30	2.000	Yes
990	49.50	3.01	1.29	1.71	0.76	0.640	1.06	0.606	1.00	1.30	2.000	Yes
991	49.55	3.01	1.30	1.72	0.76	0.639	1.06	0.605	1.00	1.30	2.000	Yes
992	49.60	3.02	1.30	1.72	0.76	0.639	1.06	0.605	1.00	1.30	2.000	Yes
993	49.65	3.02	1.30	1.72	0.76	0.639	1.06	0.605	1.00	1.30	2.000	Yes
994	49.70	3.02	1.30	1.72	0.76	0.638	1.06	0.604	1.00	1.30	2.000	Yes
995	49.75	3.03	1.30	1.72	0.76	0.638	1.06	0.604	1.00	1.30	0.785	No
996	49.80	3.03	1.30	1.73	0.75	0.637	1.06	0.603	1.00	1.30	0.785	No
997	49.85	3.03	1.31	1.73	0.75	0.637	1.06	0.603	1.00	1.30	0.784	No
998	49.90	3.04	1.31	1.73	0.75	0.637	1.06	0.603	1.00	1.30	0.784	No

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
 σ_v : Total overburden pressure at test point (tsf)
 u_0 : Water pressure at test point (tsf)
 σ_v' : Effective overburden pressure based on GWT during earthquake (tsf)
 r_d : Nonlinear shear mass factor
 CSR: Cyclic Stress Ratio
 MSF: Magnitude Scaling Factor
 CSR_{eq}: CSR adjusted for M=7.5
 K_σ : Effective overburden stress factor
 CSR*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::												
Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1	0.05	44.98	1.72	0.34	0.50	85.02	1.00	85.02	4.000	No	No	2.00
2	0.10	42.18	1.75	0.36	0.52	79.72	1.00	79.72	4.000	No	No	2.00
3	0.15	38.22	1.81	0.41	0.54	72.22	1.00	72.22	4.000	No	No	2.00
4	0.20	36.54	1.89	0.55	0.57	69.05	1.23	85.05	4.000	No	No	2.00
5	0.25	37.48	1.94	0.71	0.59	70.83	1.26	89.59	4.000	No	No	2.00
6	0.30	41.67	1.96	0.88	0.60	78.73	1.28	100.43	4.000	No	No	2.00
7	0.35	47.15	1.97	1.06	0.60	89.09	1.28	114.08	4.000	No	No	2.00
8	0.40	53.76	1.96	1.23	0.60	101.58	1.28	129.92	4.000	No	No	2.00
9	0.45	60.29	1.96	1.39	0.60	113.92	1.28	145.77	4.000	No	No	2.00
10	0.50	67.27	1.96	1.53	0.60	127.10	1.28	162.18	4.000	No	No	2.00
11	0.55	73.74	1.96	1.65	0.60	139.33	1.27	177.52	4.000	No	No	2.00
12	0.60	80.33	1.95	1.75	0.59	151.77	1.27	192.73	4.000	No	No	2.00
13	0.65	85.91	1.95	1.83	0.59	162.31	1.27	205.72	4.000	No	No	2.00
14	0.70	90.35	1.94	1.90	0.59	170.71	1.27	216.16	4.000	No	No	2.00
15	0.75	93.16	1.95	1.96	0.59	176.01	1.27	223.03	4.000	No	No	2.00
16	0.80	94.80	1.95	2.01	0.59	179.09	1.27	227.35	4.000	No	No	2.00
17	0.85	95.69	1.95	2.04	0.60	180.77	1.27	229.86	4.000	No	No	2.00
18	0.90	96.15	1.95	2.06	0.60	181.64	1.27	231.27	4.000	No	No	2.00
19	0.95	96.40	1.95	2.06	0.60	182.11	1.27	231.65	4.000	No	No	2.00
20	1.00	96.43	1.95	2.03	0.60	182.16	1.27	231.14	4.000	No	No	2.00
21	1.05	96.33	1.94	1.97	0.59	181.95	1.26	229.78	4.000	No	No	2.00
22	1.10	96.00	1.93	1.92	0.59	181.33	1.26	227.96	4.000	No	No	2.00
23	1.15	95.46	1.92	1.87	0.59	180.31	1.25	225.72	4.000	No	No	2.00
24	1.20	94.69	1.92	1.85	0.59	178.85	1.25	223.72	4.000	No	No	2.00
25	1.25	93.46	1.93	1.85	0.59	176.52	1.25	221.29	4.000	No	No	2.00
26	1.30	91.81	1.94	1.89	0.59	173.39	1.26	218.71	4.000	Yes	No	2.00
27	1.35	89.30	1.95	1.94	0.60	168.64	1.27	214.61	4.000	Yes	No	2.00
28	1.40	86.36	1.98	2.01	0.61	163.07	1.29	210.09	4.000	Yes	No	2.00
29	1.45	82.64	2.01	2.12	0.62	156.03	1.31	204.63	4.000	Yes	No	2.00
30	1.50	78.19	2.04	2.26	0.63	147.62	1.35	198.75	4.000	Yes	No	2.00
31	1.55	72.82	2.09	2.45	0.65	137.47	1.40	192.81	4.000	Yes	No	2.00
32	1.60	66.36	2.14	2.67	0.67	125.26	1.49	186.62	4.000	Yes	No	2.00
33	1.65	59.88	2.20	2.93	0.69	112.99	1.62	183.21	4.000	Yes	No	2.00
34	1.70	53.34	2.26	3.20	0.72	100.62	1.80	181.13	4.000	Yes	No	2.00
35	1.75	48.05	2.32	3.50	0.74	90.62	2.02	182.99	4.000	Yes	No	2.00
36	1.80	43.36	2.38	3.76	0.76	81.75	2.26	184.52	4.000	Yes	No	2.00
37	1.85	40.03	2.42	3.99	0.78	75.45	2.48	186.78	4.000	Yes	No	2.00
38	1.90	37.71	2.44	4.07	0.79	71.05	2.61	185.49	4.000	Yes	No	2.00
39	1.95	37.98	2.44	4.01	0.78	71.57	2.57	183.89	4.000	Yes	No	2.00
40	2.00	40.86	2.39	3.72	0.77	77.00	2.32	178.93	4.000	Yes	No	2.00
41	2.05	47.34	2.31	3.33	0.74	89.24	1.97	175.80	4.000	Yes	No	2.00
42	2.10	55.46	2.22	2.85	0.70	104.59	1.65	172.94	4.000	Yes	No	2.00
43	2.15	64.79	2.12	2.41	0.66	122.21	1.44	176.51	4.000	Yes	No	2.00
44	2.20	73.80	2.02	2.01	0.63	139.25	1.32	184.42	4.000	Yes	No	2.00
45	2.25	81.99	1.93	1.69	0.59	154.71	1.26	194.78	4.000	Yes	No	2.00
46	2.30	88.53	1.86	1.46	0.57	167.07	1.21	202.20	4.000	Yes	No	2.00
47	2.35	92.37	1.81	1.30	0.55	174.33	1.17	203.52	4.000	Yes	No	2.00
48	2.40	93.93	1.79	1.24	0.54	177.27	1.14	202.81	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
49	2.45	93.87	1.79	1.23	0.54	177.15	1.14	202.42	4.000	No	No	2.00
50	2.50	93.40	1.80	1.27	0.54	176.26	1.16	203.91	4.000	No	No	2.00
51	2.55	93.28	1.82	1.33	0.55	176.03	1.17	206.20	4.000	No	No	2.00
52	2.60	93.55	1.83	1.38	0.55	176.52	1.18	208.70	4.000	No	No	2.00
53	2.65	94.32	1.83	1.40	0.56	177.97	1.19	211.00	4.000	No	No	2.00
54	2.70	95.21	1.83	1.40	0.55	179.65	1.18	212.50	4.000	No	No	2.00
55	2.75	96.20	1.82	1.38	0.55	181.51	1.18	213.40	4.000	No	No	2.00
56	2.80	97.04	1.81	1.36	0.55	183.10	1.17	213.63	4.000	No	No	2.00
57	2.85	97.77	1.80	1.33	0.55	184.47	1.16	213.54	4.000	No	No	2.00
58	2.90	98.32	1.80	1.30	0.54	185.51	1.15	213.11	4.000	No	No	2.00
59	2.95	98.61	1.79	1.28	0.54	186.06	1.14	212.39	4.000	No	No	2.00
60	3.00	98.60	1.79	1.27	0.54	186.02	1.14	211.62	4.000	No	No	2.00
61	3.05	98.15	1.79	1.26	0.54	185.17	1.14	210.59	4.000	No	No	2.00
62	3.10	97.34	1.79	1.26	0.54	183.64	1.14	209.33	4.000	No	No	2.00
63	3.15	95.79	1.79	1.26	0.54	180.70	1.15	207.01	4.000	No	No	2.00
64	3.20	93.66	1.80	1.26	0.55	176.66	1.15	203.75	4.000	No	No	2.00
65	3.25	90.49	1.81	1.26	0.55	170.66	1.16	198.72	4.000	No	No	2.00
66	3.30	87.03	1.82	1.26	0.55	164.12	1.18	193.04	4.000	No	No	2.00
67	3.35	83.13	1.84	1.26	0.56	156.75	1.19	186.37	4.000	No	No	2.00
68	3.40	79.38	1.85	1.26	0.56	149.65	1.20	179.71	4.000	No	No	2.00
69	3.45	75.65	1.87	1.26	0.57	142.59	1.21	172.87	4.000	No	No	2.00
70	3.50	72.09	1.88	1.26	0.58	135.86	1.22	166.18	4.000	No	No	2.00
71	3.55	68.88	1.89	1.26	0.58	129.79	1.23	160.03	4.000	No	No	2.00
72	3.60	65.66	1.91	1.26	0.59	123.69	1.24	153.76	4.000	No	No	2.00
73	3.65	62.53	1.92	1.26	0.59	117.77	1.25	147.59	4.000	No	No	2.00
74	3.70	59.19	1.94	1.27	0.60	111.46	1.27	141.10	4.000	No	No	2.00
75	3.75	56.15	1.96	1.29	0.61	105.71	1.28	135.33	4.000	No	No	2.00
76	3.80	53.48	1.99	1.33	0.62	100.65	1.30	130.64	4.000	No	No	2.00
77	3.85	51.15	2.01	1.37	0.63	96.25	1.32	126.82	4.000	No	No	2.00
78	3.90	49.13	2.03	1.41	0.64	92.41	1.34	123.70	4.000	No	No	2.00
79	3.95	47.18	2.05	1.44	0.64	88.73	1.36	120.51	4.000	No	No	2.00
80	4.00	45.55	2.07	1.45	0.65	85.64	1.37	117.73	4.000	No	No	2.00
81	4.05	44.07	2.08	1.45	0.65	82.84	1.39	115.06	4.000	No	No	2.00
82	4.10	42.95	2.09	1.45	0.66	80.72	1.40	113.02	4.000	No	No	2.00
83	4.15	42.18	2.09	1.45	0.66	79.25	1.41	111.51	4.000	No	No	2.00
84	4.20	41.81	2.09	1.44	0.66	78.56	1.41	110.55	4.000	No	No	2.00
85	4.25	41.70	2.09	1.41	0.66	78.34	1.40	109.73	4.000	No	No	2.00
86	4.30	41.70	2.08	1.37	0.65	78.33	1.39	108.97	4.000	No	No	2.00
87	4.35	41.70	2.07	1.33	0.65	78.32	1.38	108.10	4.000	No	No	2.00
88	4.40	41.70	2.07	1.31	0.65	78.32	1.37	107.66	4.000	No	No	2.00
89	4.45	41.70	2.07	1.31	0.65	78.31	1.37	107.64	4.000	No	No	2.00
90	4.50	41.64	2.08	1.35	0.65	78.19	1.39	108.32	4.000	No	No	2.00
91	4.55	41.46	2.09	1.40	0.66	77.84	1.40	109.12	4.000	Yes	No	2.00
92	4.60	40.97	2.11	1.47	0.67	76.91	1.43	109.81	4.000	Yes	No	2.00
93	4.65	40.19	2.12	1.54	0.67	75.44	1.46	110.01	4.000	Yes	No	2.00
94	4.70	39.05	2.15	1.61	0.68	73.27	1.50	109.77	4.000	Yes	No	2.00
95	4.75	37.79	2.17	1.69	0.69	70.89	1.55	109.73	4.000	Yes	No	2.00
96	4.80	36.36	2.20	1.77	0.70	68.19	1.61	109.72	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _t (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
97	4.85	35.02	2.22	1.85	0.71	65.64	1.68	110.10	4.000	Yes	No	2.00
98	4.90	33.60	2.25	1.92	0.72	62.95	1.75	109.97	4.000	Yes	No	2.00
99	4.95	32.24	2.27	1.98	0.73	60.37	1.82	109.70	4.000	Yes	No	2.00
100	5.00	30.86	2.29	2.04	0.74	57.77	1.90	109.63	4.000	Yes	No	2.00
101	5.05	29.46	2.32	2.11	0.75	55.11	2.00	110.09	4.000	Yes	No	2.00
102	5.10	28.11	2.35	2.23	0.76	52.55	2.13	111.77	4.000	Yes	No	2.00
103	5.15	26.68	2.38	2.35	0.77	49.84	2.28	113.81	4.000	Yes	No	2.00
104	5.20	25.33	2.42	2.51	0.79	47.28	2.47	116.82	4.000	Yes	No	2.00
105	5.25	23.93	2.45	2.67	0.80	44.64	2.68	119.71	4.000	Yes	No	2.00
106	5.30	22.69	2.49	2.84	0.81	42.28	2.91	122.99	4.000	Yes	No	2.00
107	5.35	21.59	2.52	2.99	0.83	40.20	3.23	129.84	4.000	Yes	No	2.00
108	5.40	20.68	2.55	3.12	0.84	38.48	3.86	148.38	4.000	Yes	No	2.00
109	5.45	19.94	2.57	3.22	0.84	37.07	4.41	163.57	4.000	Yes	No	2.00
110	5.50	19.22	2.58	3.26	0.85	35.71	4.90	174.87	4.000	Yes	No	2.00
111	5.55	18.65	2.59	3.25	0.85	34.62	5.19	179.59	4.000	No	No	2.00
112	5.60	18.16	2.60	3.20	0.86	33.69	5.33	179.68	4.000	No	No	2.00
113	5.65	17.66	2.60	3.13	0.86	32.74	5.45	178.52	4.000	No	No	2.00
114	5.70	17.03	2.61	3.10	0.86	31.55	5.79	182.70	4.000	No	No	2.00
115	5.75	16.14	2.63	3.11	0.87	29.86	6.53	194.90	4.000	No	No	2.00
116	5.80	15.27	2.65	3.17	0.88	28.20	7.63	215.19	4.000	No	No	2.00
117	5.85	14.41	2.68	3.27	0.89	26.58	9.07	241.16	4.000	No	No	2.00
118	5.90	13.82	2.71	3.39	0.90	25.46	4.77	121.40	4.000	No	Yes	2.00
119	5.95	13.39	2.73	3.50	0.91	24.63	4.99	122.89	4.000	No	Yes	2.00
120	6.00	13.19	2.74	3.61	0.91	24.26	5.14	124.68	4.000	No	Yes	2.00
121	6.05	13.11	2.75	3.69	0.91	24.10	5.23	126.10	4.000	No	Yes	2.00
122	6.10	13.11	2.75	3.74	0.92	24.09	5.28	127.28	4.000	No	Yes	2.00
123	6.15	13.11	2.76	3.79	0.92	24.09	5.32	128.19	4.000	No	Yes	2.00
124	6.20	13.11	2.76	3.84	0.92	24.08	5.37	129.32	4.000	No	Yes	2.00
125	6.25	13.11	2.77	3.92	0.92	24.08	5.43	130.87	4.000	No	Yes	2.00
126	6.30	13.03	2.78	4.02	0.93	23.93	5.55	132.82	4.000	No	Yes	2.00
127	6.35	12.70	2.79	4.15	0.93	23.29	5.76	134.22	4.000	No	Yes	2.00
128	6.40	12.15	2.82	4.29	0.94	22.26	6.07	135.09	4.000	No	Yes	2.00
129	6.45	11.44	2.85	4.41	0.95	20.91	6.44	134.69	4.000	No	Yes	2.00
130	6.50	10.99	2.87	4.50	0.96	20.04	6.71	134.43	4.000	No	Yes	2.00
131	6.55	10.74	2.87	4.52	0.96	19.56	6.84	133.80	4.000	No	Yes	2.00
132	6.60	10.73	2.87	4.50	0.96	19.54	6.83	133.40	4.000	No	Yes	2.00
133	6.65	10.73	2.87	4.45	0.96	19.53	6.78	132.51	4.000	No	Yes	2.00
134	6.70	10.73	2.87	4.40	0.96	19.53	6.74	131.64	4.000	No	Yes	2.00
135	6.75	10.73	2.87	4.36	0.96	19.52	6.71	130.99	4.000	No	Yes	2.00
136	6.80	10.73	2.86	4.34	0.96	19.52	6.69	130.61	4.000	No	Yes	2.00
137	6.85	10.73	2.86	4.33	0.96	19.51	6.68	130.37	4.000	No	Yes	2.00
138	6.90	10.73	2.86	4.30	0.96	19.51	6.66	129.84	4.000	No	Yes	2.00
139	6.95	10.73	2.86	4.25	0.96	19.50	6.61	128.99	4.000	No	Yes	2.00
140	7.00	10.73	2.85	4.18	0.96	19.50	6.55	127.77	4.000	No	Yes	2.00
141	7.05	10.73	2.85	4.11	0.96	19.49	6.49	126.52	4.000	No	Yes	2.00
142	7.10	10.73	2.84	4.04	0.95	19.49	6.42	125.10	4.000	No	Yes	2.00
143	7.15	10.73	2.84	3.96	0.95	19.48	6.35	123.66	4.000	No	Yes	2.00
144	7.20	10.73	2.83	3.87	0.95	19.47	6.27	122.10	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _k (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
145	7.25	10.73	2.83	3.83	0.95	19.47	6.23	121.28	4.000	No	Yes	2.00
146	7.30	10.73	2.83	3.83	0.95	19.46	6.23	121.29	4.000	No	Yes	2.00
147	7.35	10.73	2.84	3.93	0.95	19.46	6.32	123.07	4.000	No	Yes	2.00
148	7.40	10.73	2.85	4.08	0.96	19.45	6.46	125.77	4.000	No	Yes	2.00
149	7.45	10.73	2.86	4.29	0.96	19.45	6.66	129.53	4.000	No	Yes	2.00
150	7.50	10.78	2.87	4.50	0.97	19.54	6.82	133.35	4.000	No	Yes	2.00
151	7.55	11.09	2.88	4.71	0.97	20.12	6.87	138.23	4.000	No	Yes	2.00
152	7.60	11.66	2.87	4.86	0.96	21.20	6.76	143.32	4.000	Yes	Yes	2.00
153	7.65	12.56	2.85	4.96	0.96	22.89	6.50	148.78	4.000	Yes	Yes	2.00
154	7.70	13.44	2.83	4.98	0.95	24.54	6.22	152.62	4.000	Yes	Yes	2.00
155	7.75	14.27	2.81	4.95	0.94	26.12	5.95	155.31	4.000	Yes	Yes	2.00
156	7.80	14.98	2.79	4.90	0.93	27.45	5.71	156.82	4.000	Yes	Yes	2.00
157	7.85	15.66	2.77	4.84	0.93	28.72	5.49	157.70	4.000	Yes	Yes	2.00
158	7.90	16.37	2.75	4.74	0.92	30.07	5.25	157.89	4.000	Yes	Yes	2.00
159	7.95	17.12	2.72	4.56	0.91	31.47	4.96	156.11	4.000	Yes	Yes	2.00
160	8.00	18.02	2.69	4.31	0.90	33.18	9.59	318.25	4.000	Yes	No	2.00
161	8.05	19.23	2.64	3.94	0.88	35.46	7.10	251.87	4.000	Yes	No	2.00
162	8.10	20.74	2.58	3.51	0.86	38.30	4.89	187.14	4.000	Yes	No	2.00
163	8.15	22.77	2.52	3.01	0.83	41.18	3.11	127.96	4.000	Yes	No	2.00
164	8.20	25.06	2.44	2.56	0.80	44.34	2.62	116.34	4.000	Yes	No	2.00
165	8.25	27.92	2.37	2.18	0.78	48.30	2.23	107.61	4.000	Yes	No	2.00
166	8.30	30.77	2.31	1.92	0.75	52.17	1.96	102.32	4.000	Yes	No	2.00
167	8.35	33.70	2.26	1.74	0.73	56.19	1.77	99.71	4.000	Yes	No	2.00
168	8.40	35.97	2.22	1.61	0.72	59.20	1.66	98.20	4.000	Yes	No	2.00
169	8.45	37.71	2.19	1.53	0.71	61.50	1.59	97.95	4.000	Yes	No	2.00
170	8.50	38.81	2.18	1.49	0.70	62.91	1.56	98.08	0.168	No	No	0.28
171	8.55	39.63	2.17	1.50	0.70	64.04	1.55	99.15	0.171	No	No	0.28
172	8.60	40.35	2.17	1.52	0.70	65.04	1.54	100.38	0.174	No	No	0.29
173	8.65	40.92	2.17	1.53	0.70	65.83	1.54	101.42	0.177	No	No	0.29
174	8.70	41.39	2.17	1.53	0.70	66.40	1.53	101.91	0.178	No	No	0.29
175	8.75	41.61	2.16	1.52	0.70	66.55	1.53	101.65	0.178	No	No	0.29
176	8.80	41.66	2.16	1.49	0.69	66.42	1.52	100.83	0.175	No	No	0.29
177	8.85	41.48	2.15	1.45	0.69	65.94	1.51	99.56	0.172	No	No	0.28
178	8.90	40.97	2.15	1.42	0.69	64.97	1.51	98.00	0.168	No	No	0.27
179	8.95	40.02	2.16	1.41	0.70	63.42	1.52	96.35	4.000	Yes	No	2.00
180	9.00	38.38	2.17	1.42	0.70	60.95	1.55	94.63	4.000	Yes	No	2.00
181	9.05	36.34	2.20	1.46	0.71	57.97	1.61	93.30	4.000	Yes	No	2.00
182	9.10	33.87	2.23	1.53	0.72	54.40	1.70	92.41	4.000	Yes	No	2.00
183	9.15	31.57	2.27	1.62	0.74	51.09	1.81	92.68	4.000	Yes	No	2.00
184	9.20	29.25	2.31	1.73	0.75	47.73	1.96	93.68	4.000	Yes	No	2.00
185	9.25	27.17	2.35	1.87	0.77	44.73	2.14	95.74	4.000	Yes	No	2.00
186	9.30	25.10	2.40	2.00	0.79	41.68	2.35	97.92	4.000	Yes	No	2.00
187	9.35	23.30	2.44	2.16	0.80	39.00	2.58	100.81	4.000	Yes	No	2.00
188	9.40	21.84	2.48	2.30	0.82	36.82	2.81	103.63	4.000	Yes	No	2.00
189	9.45	20.92	2.51	2.45	0.83	35.44	2.90	102.72	4.000	Yes	No	2.00
190	9.50	20.38	2.53	2.58	0.84	34.65	3.37	116.59	4.000	Yes	No	2.00
191	9.55	20.02	2.55	2.72	0.84	34.14	3.84	131.14	4.000	Yes	No	2.00
192	9.60	19.68	2.57	2.91	0.85	33.71	4.47	150.75	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
193	9.65	19.36	2.59	3.12	0.86	33.28	5.22	173.67	4.000	Yes	No	2.00
194	9.70	19.16	2.62	3.35	0.87	33.05	6.05	199.82	4.000	Yes	No	2.00
195	9.75	19.37	2.62	3.42	0.87	33.38	6.14	205.08	4.000	Yes	No	2.00
196	9.80	20.44	2.60	3.31	0.86	34.97	5.27	184.44	4.000	Yes	No	2.00
197	9.85	22.15	2.55	3.02	0.84	37.37	3.85	143.76	4.000	Yes	No	2.00
198	9.90	24.24	2.49	2.74	0.82	40.32	2.94	118.57	4.000	Yes	No	2.00
199	9.95	25.93	2.45	2.49	0.81	42.58	2.66	113.10	4.000	Yes	No	2.00
200	10.00	27.41	2.41	2.29	0.79	44.50	2.43	108.34	4.000	Yes	No	2.00
201	10.05	29.11	2.37	2.05	0.78	46.64	2.20	102.60	4.000	Yes	No	2.00
202	10.10	31.11	2.31	1.79	0.75	49.08	1.96	96.29	4.000	Yes	No	2.00
203	10.15	33.42	2.25	1.54	0.73	51.85	1.75	90.89	4.000	Yes	No	2.00
204	10.20	35.29	2.20	1.34	0.71	53.96	1.61	86.90	4.000	Yes	No	2.00
205	10.25	36.90	2.16	1.20	0.70	55.76	1.52	84.73	4.000	Yes	No	2.00
206	10.30	37.89	2.13	1.11	0.69	56.81	1.47	83.61	4.000	Yes	No	2.00
207	10.35	38.39	2.12	1.09	0.68	57.34	1.46	83.52	0.134	No	No	0.20
208	10.40	38.23	2.13	1.10	0.69	57.07	1.46	83.58	0.134	No	No	0.20
209	10.45	37.66	2.14	1.14	0.69	56.30	1.49	83.80	0.135	No	No	0.20
210	10.50	36.75	2.16	1.18	0.70	55.08	1.52	83.74	0.135	No	No	0.20
211	10.55	35.87	2.17	1.22	0.70	53.86	1.55	83.68	0.134	No	No	0.20
212	10.60	35.11	2.19	1.25	0.71	52.81	1.59	83.70	0.135	No	No	0.20
213	10.65	34.72	2.20	1.29	0.71	52.26	1.61	84.24	0.136	No	No	0.20
214	10.70	34.49	2.21	1.32	0.72	51.95	1.63	84.94	0.137	No	No	0.20
215	10.75	34.31	2.22	1.35	0.72	51.69	1.66	85.61	0.138	No	No	0.21
216	10.80	34.02	2.22	1.37	0.72	51.24	1.67	85.75	0.139	No	No	0.21
217	10.85	33.69	2.23	1.38	0.72	50.71	1.69	85.59	0.138	No	No	0.21
218	10.90	33.60	2.23	1.38	0.72	50.51	1.69	85.46	0.138	No	No	0.20
219	10.95	33.73	2.23	1.38	0.72	50.61	1.69	85.53	0.138	No	No	0.20
220	11.00	34.09	2.23	1.38	0.72	51.03	1.68	85.83	0.139	No	No	0.20
221	11.05	34.36	2.22	1.38	0.72	51.32	1.68	86.04	0.139	No	No	0.21
222	11.10	34.52	2.22	1.38	0.72	51.47	1.67	86.14	0.139	No	No	0.21
223	11.15	34.55	2.22	1.38	0.72	51.43	1.67	86.12	0.139	No	No	0.20
224	11.20	34.52	2.22	1.38	0.72	51.30	1.68	86.03	0.139	No	No	0.20
225	11.25	34.22	2.23	1.38	0.72	50.82	1.69	85.69	0.139	No	No	0.20
226	11.30	33.73	2.23	1.39	0.73	50.06	1.70	85.35	0.138	No	No	0.20
227	11.35	33.01	2.24	1.40	0.73	49.02	1.74	85.09	0.137	No	No	0.20
228	11.40	32.51	2.26	1.44	0.74	48.30	1.77	85.48	0.138	No	No	0.20
229	11.45	32.21	2.27	1.47	0.74	47.88	1.80	86.28	0.140	No	No	0.20
230	11.50	31.92	2.28	1.52	0.74	47.49	1.84	87.42	4.000	Yes	No	2.00
231	11.55	31.43	2.29	1.59	0.75	46.85	1.90	88.84	4.000	Yes	No	2.00
232	11.60	30.56	2.32	1.68	0.76	45.71	1.99	90.88	4.000	Yes	No	2.00
233	11.65	29.63	2.35	1.83	0.77	44.53	2.12	94.47	4.000	Yes	No	2.00
234	11.70	28.56	2.39	2.02	0.79	43.20	2.30	99.47	4.000	Yes	No	2.00
235	11.75	27.44	2.43	2.28	0.80	41.84	2.54	106.33	4.000	Yes	No	2.00
236	11.80	26.20	2.48	2.56	0.82	40.25	2.81	113.31	4.000	Yes	No	2.00
237	11.85	24.96	2.52	2.85	0.84	38.63	3.20	123.77	4.000	Yes	No	2.00
238	11.90	23.94	2.55	3.08	0.85	37.22	4.02	149.54	4.000	Yes	No	2.00
239	11.95	23.21	2.58	3.25	0.86	36.19	4.74	171.47	4.000	Yes	No	2.00
240	12.00	22.90	2.59	3.29	0.86	35.70	4.98	177.60	0.601	No	No	0.85

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
241	12.05	22.95	2.58	3.23	0.86	35.65	4.82	171.76	4.000	Yes	No	2.00
242	12.10	23.46	2.56	3.04	0.85	36.21	4.17	150.86	4.000	Yes	No	2.00
243	12.15	24.27	2.53	2.83	0.84	37.17	3.44	127.89	4.000	Yes	No	2.00
244	12.20	25.48	2.49	2.59	0.83	38.65	2.93	113.15	4.000	Yes	No	2.00
245	12.25	26.69	2.46	2.38	0.81	40.12	2.69	108.07	4.000	Yes	No	2.00
246	12.30	27.94	2.42	2.18	0.80	41.62	2.48	103.18	4.000	Yes	No	2.00
247	12.35	28.81	2.40	2.06	0.79	42.64	2.35	100.11	4.000	Yes	No	2.00
248	12.40	29.42	2.38	2.00	0.78	43.35	2.28	98.78	0.170	No	No	0.24
249	12.45	29.41	2.39	2.05	0.79	43.32	2.32	100.38	4.000	Yes	No	2.00
250	12.50	28.97	2.41	2.18	0.80	42.79	2.43	103.88	4.000	Yes	No	2.00
251	12.55	27.93	2.45	2.40	0.81	41.48	2.64	109.44	4.000	Yes	No	2.00
252	12.60	26.58	2.49	2.66	0.83	39.73	2.92	115.82	4.000	Yes	No	2.00
253	12.65	24.77	2.54	2.96	0.85	37.31	3.71	138.59	4.000	Yes	No	2.00
254	12.70	22.69	2.60	3.33	0.87	34.46	5.48	188.72	4.000	Yes	No	2.00
255	12.75	20.46	2.67	3.74	0.89	31.36	8.24	258.53	4.000	Yes	No	2.00
256	12.80	18.46	2.73	4.22	0.92	28.52	5.05	144.16	4.000	Yes	Yes	2.00
257	12.85	16.98	2.79	4.67	0.94	26.40	5.69	150.26	4.000	Yes	Yes	2.00
258	12.90	16.08	2.83	5.13	0.96	25.12	6.24	156.72	4.000	Yes	Yes	2.00
259	12.95	15.67	2.86	5.45	0.97	24.52	6.58	161.44	4.000	Yes	Yes	2.00
260	13.00	15.52	2.87	5.66	0.97	24.30	6.78	164.67	1.159	No	Yes	1.60
261	13.05	15.62	2.87	5.63	0.97	24.39	6.74	164.30	1.164	No	Yes	1.60
262	13.10	15.82	2.85	5.45	0.97	24.60	6.57	161.58	1.173	No	Yes	1.61
263	13.15	16.02	2.83	5.12	0.96	24.75	6.29	155.80	1.181	No	Yes	1.62
264	13.20	15.84	2.82	4.80	0.95	24.34	6.11	148.83	1.161	No	Yes	1.59
265	13.25	15.09	2.82	4.48	0.95	23.06	6.08	140.33	1.100	No	Yes	1.50
266	13.30	13.89	2.83	4.29	0.96	21.16	6.28	132.96	1.009	No	Yes	1.38
267	13.35	12.54	2.86	4.19	0.97	19.06	6.67	127.03	0.909	No	Yes	1.24
268	13.40	11.57	2.90	4.29	0.98	17.56	7.14	125.38	0.838	No	Yes	1.14
269	13.45	11.06	2.92	4.43	0.99	16.78	7.50	125.87	0.800	No	Yes	1.09
270	13.50	11.21	2.92	4.55	0.99	17.01	7.54	128.30	0.811	No	Yes	1.10
271	13.55	11.71	2.91	4.53	0.99	17.72	7.32	129.67	0.845	No	Yes	1.15
272	13.60	12.41	2.88	4.44	0.98	18.73	6.97	130.62	0.893	No	Yes	1.21
273	13.65	12.87	2.87	4.43	0.97	19.37	6.81	131.88	0.924	No	Yes	1.25
274	13.70	13.11	2.87	4.51	0.97	19.71	6.80	134.02	0.940	No	Yes	1.27
275	13.75	13.11	2.88	4.70	0.98	19.72	6.96	137.23	0.941	No	Yes	1.27
276	13.80	13.11	2.89	4.87	0.98	19.72	7.11	140.17	0.941	No	Yes	1.27
277	13.85	13.11	2.90	5.05	0.99	19.72	7.26	143.10	0.941	No	Yes	1.26
278	13.90	13.11	2.91	5.17	0.99	19.71	7.36	145.07	0.940	No	Yes	1.26
279	13.95	13.13	2.92	5.26	0.99	19.70	7.43	146.44	0.940	No	Yes	1.26
280	14.00	13.39	2.91	5.29	0.99	20.06	7.37	147.91	0.957	No	Yes	1.28
281	14.05	13.85	2.90	5.33	0.99	20.72	7.25	150.26	0.988	No	Yes	1.32
282	14.10	14.57	2.89	5.41	0.98	21.76	7.09	154.15	1.038	No	Yes	1.39
283	14.15	15.10	2.89	5.51	0.98	22.53	7.00	157.76	1.075	No	Yes	1.43
284	14.20	15.43	2.89	5.61	0.98	22.99	6.99	160.70	1.097	No	Yes	1.46
285	14.25	15.50	2.89	5.69	0.98	23.06	7.03	162.09	1.100	No	Yes	1.46
286	14.30	15.50	2.89	5.75	0.98	23.02	7.08	163.04	1.098	No	Yes	1.46
287	14.35	15.50	2.90	5.82	0.98	22.99	7.14	164.23	1.097	No	Yes	1.45
288	14.40	15.50	2.90	5.90	0.99	22.96	7.21	165.56	1.095	No	Yes	1.45

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
289	14.45	15.50	2.90	5.98	0.99	22.93	7.28	166.84	1.094	No	Yes	1.45
290	14.50	15.58	2.90	5.99	0.99	23.00	7.26	167.12	1.097	No	Yes	1.45
291	14.55	15.79	2.90	5.93	0.98	23.24	7.17	166.70	1.109	No	Yes	1.46
292	14.60	16.23	2.88	5.75	0.98	23.80	6.93	164.97	1.135	No	Yes	1.50
293	14.65	16.77	2.86	5.51	0.97	24.48	6.63	162.33	1.168	No	Yes	1.54
294	14.70	17.32	2.83	5.19	0.96	25.15	6.28	157.86	1.199	No	Yes	1.58
295	14.75	17.67	2.81	4.89	0.95	25.52	5.99	152.87	1.217	No	Yes	1.60
296	14.80	17.84	2.79	4.60	0.94	25.63	5.75	147.29	1.222	No	Yes	1.60
297	14.85	17.68	2.78	4.41	0.94	25.30	5.65	143.03	1.207	No	Yes	1.58
298	14.90	17.26	2.79	4.30	0.94	24.62	5.67	139.63	1.174	No	Yes	1.54
299	14.95	16.59	2.80	4.31	0.95	23.63	5.84	138.05	1.127	No	Yes	1.47
300	15.00	15.91	2.82	4.37	0.95	22.64	6.07	137.39	1.080	No	Yes	1.41
301	15.05	15.20	2.84	4.49	0.96	21.61	6.37	137.54	1.031	No	Yes	1.34
302	15.10	14.52	2.86	4.61	0.97	20.63	6.67	137.68	0.984	No	Yes	1.28
303	15.15	13.81	2.89	4.74	0.98	19.61	7.02	137.69	0.936	No	Yes	1.22
304	15.20	13.36	2.91	4.87	0.99	18.95	7.29	138.23	0.904	No	Yes	1.17
305	15.25	13.12	2.92	4.99	0.99	18.58	7.49	139.24	0.886	No	Yes	1.15
306	15.30	13.11	2.93	5.08	1.00	18.56	7.58	140.66	0.885	No	Yes	1.15
307	15.35	13.11	2.93	5.14	1.00	18.53	7.64	141.51	0.884	No	Yes	1.14
308	15.40	13.11	2.93	5.16	1.00	18.50	7.66	141.77	0.882	No	Yes	1.14
309	15.45	13.11	2.93	5.15	1.00	18.46	7.66	141.40	0.880	No	Yes	1.14
310	15.50	13.11	2.93	5.11	1.00	18.41	7.64	140.68	0.878	No	Yes	1.13
311	15.55	13.11	2.93	5.07	1.00	18.37	7.62	139.96	0.876	No	Yes	1.13
312	15.60	13.11	2.93	5.06	1.00	18.33	7.62	139.74	0.874	No	Yes	1.13
313	15.65	13.11	2.93	5.13	1.00	18.31	7.69	140.72	0.873	No	Yes	1.12
314	15.70	13.32	2.93	5.24	1.00	18.59	7.71	143.21	0.887	No	Yes	1.14
315	15.75	13.90	2.93	5.38	1.00	19.39	7.61	147.57	0.925	No	Yes	1.19
316	15.80	15.24	2.90	5.37	0.99	21.24	7.17	152.19	1.013	No	Yes	1.30
317	15.85	17.13	2.85	5.23	0.97	23.81	6.54	155.79	1.136	No	Yes	1.45
318	15.90	19.55	2.79	4.89	0.95	27.02	5.77	155.78	1.289	No	Yes	1.65
319	15.95	21.87	2.74	4.51	0.92	30.02	5.09	152.88	1.432	No	Yes	1.83
320	16.00	24.20	2.68	4.07	0.90	32.96	8.73	287.84	3.600	No	No	2.00
321	16.05	26.03	2.63	3.74	0.88	35.20	6.54	230.14	3.600	No	No	2.00
322	16.10	27.52	2.59	3.51	0.87	37.01	5.22	193.04	0.749	No	No	0.95
323	16.15	28.01	2.59	3.51	0.87	37.59	5.05	190.00	0.718	No	No	0.91
324	16.20	27.82	2.60	3.64	0.87	37.34	5.51	205.80	3.600	No	No	2.00
325	16.25	26.64	2.64	3.95	0.89	35.85	6.96	249.72	3.600	No	No	2.00
326	16.30	25.25	2.68	4.24	0.90	34.06	8.83	300.82	3.600	No	No	2.00
327	16.35	23.65	2.72	4.52	0.92	31.96	4.88	156.06	1.525	No	Yes	1.93
328	16.40	22.45	2.74	4.68	0.93	30.35	5.18	157.09	1.448	No	Yes	1.83
329	16.45	21.50	2.76	4.76	0.93	29.04	5.39	156.58	1.385	No	Yes	1.75
330	16.50	21.06	2.77	4.70	0.94	28.38	5.44	154.24	1.354	No	Yes	1.71
331	16.55	20.86	2.76	4.58	0.94	28.02	5.39	151.09	1.337	No	Yes	1.69
332	16.60	20.86	2.75	4.38	0.93	27.91	5.26	146.75	1.331	No	Yes	1.68
333	16.65	20.78	2.74	4.26	0.93	27.72	5.19	143.79	1.322	No	Yes	1.67
334	16.70	20.59	2.75	4.24	0.93	27.41	5.21	142.92	1.307	No	Yes	1.65
335	16.75	20.27	2.76	4.43	0.94	26.99	5.42	146.19	1.288	No	Yes	1.62
336	16.80	19.89	2.79	4.73	0.95	26.51	5.71	151.48	1.264	No	Yes	1.59

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
337	16.85	19.24	2.82	5.12	0.96	25.68	6.14	157.61	1.225	No	Yes	1.54
338	16.90	18.56	2.85	5.50	0.97	24.80	6.57	162.84	1.183	No	Yes	1.48
339	16.95	18.03	2.88	5.87	0.98	24.11	6.96	167.87	1.150	No	Yes	1.44
340	17.00	18.61	2.88	6.05	0.98	24.88	6.95	173.02	4.000	Yes	Yes	2.00
341	17.05	20.27	2.86	6.04	0.97	27.06	6.59	178.20	4.000	Yes	Yes	2.00
342	17.10	23.40	2.80	5.71	0.95	31.10	5.80	180.48	4.000	Yes	Yes	2.00
343	17.15	27.05	2.73	5.26	0.92	35.71	5.01	178.86	4.000	Yes	Yes	2.00
344	17.20	31.32	2.65	4.66	0.89	40.98	7.39	302.90	4.000	Yes	No	2.00
345	17.25	35.16	2.58	4.11	0.87	45.58	4.66	212.64	4.000	Yes	No	2.00
346	17.30	38.86	2.50	3.53	0.84	49.87	2.87	142.93	4.000	Yes	No	2.00
347	17.35	41.28	2.44	3.06	0.82	52.49	2.62	137.35	4.000	Yes	No	2.00
348	17.40	42.80	2.39	2.64	0.79	53.94	2.32	125.31	4.000	Yes	No	2.00
349	17.45	42.83	2.36	2.35	0.78	53.64	2.17	116.29	4.000	Yes	No	2.00
350	17.50	42.19	2.34	2.16	0.78	52.59	2.09	109.76	4.000	Yes	No	2.00
351	17.55	40.76	2.34	2.09	0.78	50.70	2.09	106.20	0.191	No	No	0.24
352	17.60	39.02	2.36	2.08	0.78	48.50	2.16	104.64	4.000	Yes	No	2.00
353	17.65	36.86	2.38	2.14	0.79	45.85	2.29	104.82	4.000	Yes	No	2.00
354	17.70	34.06	2.43	2.29	0.81	42.49	2.52	106.95	4.000	Yes	No	2.00
355	17.75	30.98	2.48	2.50	0.83	38.77	2.86	110.79	4.000	Yes	No	2.00
356	17.80	27.97	2.55	2.85	0.86	35.16	3.93	138.27	4.000	Yes	No	2.00
357	17.85	25.78	2.62	3.27	0.88	32.55	5.96	194.05	4.000	Yes	No	2.00
358	17.90	24.17	2.68	3.79	0.90	30.65	8.86	271.55	4.000	Yes	No	2.00
359	17.95	22.86	2.73	4.32	0.93	29.08	5.06	147.07	4.000	Yes	Yes	2.00
360	18.00	21.57	2.79	4.89	0.95	27.53	5.69	156.72	4.000	Yes	Yes	2.00
361	18.05	20.83	2.83	5.43	0.96	26.64	6.22	165.66	4.000	Yes	Yes	2.00
362	18.10	20.97	2.85	5.89	0.97	26.85	6.51	174.92	4.000	Yes	Yes	2.00
363	18.15	22.68	2.84	6.14	0.97	29.05	6.36	184.70	4.000	Yes	Yes	2.00
364	18.20	24.91	2.81	6.17	0.96	31.86	6.01	191.41	4.000	Yes	Yes	2.00
365	18.25	27.32	2.78	5.97	0.94	34.83	5.55	193.29	4.000	Yes	Yes	2.00
366	18.30	29.37	2.74	5.61	0.93	37.27	5.09	189.63	4.000	Yes	Yes	2.00
367	18.35	31.86	2.68	5.13	0.91	40.20	9.25	371.95	4.000	Yes	No	2.00
368	18.40	36.70	2.61	4.54	0.88	45.94	5.62	257.94	4.000	Yes	No	2.00
369	18.45	43.08	2.52	3.95	0.84	53.43	3.14	167.93	4.000	Yes	No	2.00
370	18.50	51.28	2.42	3.35	0.81	62.89	2.46	154.80	4.000	Yes	No	2.00
371	18.55	57.67	2.33	2.86	0.78	70.01	2.06	144.47	4.000	Yes	No	2.00
372	18.60	62.48	2.26	2.44	0.75	75.14	1.80	135.05	4.000	Yes	No	2.00
373	18.65	62.59	2.24	2.26	0.74	74.93	1.73	129.45	4.000	Yes	No	2.00
374	18.70	59.78	2.26	2.26	0.74	71.54	1.77	126.61	4.000	Yes	No	2.00
375	18.75	53.35	2.33	2.55	0.77	64.19	2.03	130.06	4.000	Yes	No	2.00
376	18.80	46.95	2.41	2.96	0.80	56.85	2.42	137.72	4.000	Yes	No	2.00
377	18.85	40.55	2.51	3.53	0.84	49.43	2.91	143.86	4.000	Yes	No	2.00
378	18.90	36.09	2.58	4.05	0.87	44.20	4.83	213.50	4.000	Yes	No	2.00
379	18.95	32.65	2.65	4.60	0.90	40.13	7.51	301.17	4.000	Yes	No	2.00
380	19.00	30.55	2.70	5.06	0.91	37.62	4.71	177.24	4.000	Yes	Yes	2.00
381	19.05	28.71	2.74	5.45	0.93	35.39	5.16	182.64	4.000	Yes	Yes	2.00
382	19.10	26.41	2.78	5.69	0.95	32.54	5.62	182.82	4.000	Yes	Yes	2.00
383	19.15	23.50	2.83	5.87	0.96	28.91	6.20	179.10	4.000	Yes	Yes	2.00
384	19.20	20.07	2.89	6.03	0.99	24.60	6.99	171.95	4.000	Yes	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _k (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
385	19.25	17.73	2.93	6.16	1.00	21.63	7.68	166.15	4.000	Yes	Yes	2.00
386	19.30	16.42	2.96	6.22	1.00	19.89	8.15	162.06	4.000	Yes	Yes	2.00
387	19.35	16.54	2.95	6.10	1.00	20.00	8.02	160.46	0.954	No	Yes	1.15
388	19.40	16.98	2.93	5.87	1.00	20.52	7.72	158.45	0.979	No	Yes	1.18
389	19.45	17.69	2.90	5.52	0.99	21.36	7.26	155.02	1.019	No	Yes	1.23
390	19.50	18.17	2.88	5.19	0.98	21.87	6.89	150.66	1.043	No	Yes	1.26
391	19.55	18.43	2.86	4.85	0.97	22.10	6.57	145.22	1.054	No	Yes	1.27
392	19.60	18.19	2.84	4.57	0.97	21.72	6.41	139.34	1.036	No	Yes	1.25
393	19.65	17.78	2.84	4.32	0.97	21.15	6.31	133.47	1.009	No	Yes	1.21
394	19.70	17.37	2.83	4.14	0.97	20.58	6.27	129.04	0.982	No	Yes	1.18
395	19.75	17.72	2.82	4.06	0.96	20.97	6.12	128.38	1.000	No	Yes	1.20
396	19.80	19.06	2.81	4.18	0.96	22.57	5.92	133.58	1.077	No	Yes	1.29
397	19.85	21.14	2.78	4.34	0.95	25.08	5.63	141.26	1.197	No	Yes	1.44
398	19.90	23.24	2.76	4.50	0.94	27.61	5.39	148.67	1.317	No	Yes	1.58
399	19.95	24.36	2.74	4.38	0.93	28.89	5.13	148.24	1.378	No	Yes	1.65
400	20.00	24.31	2.72	4.12	0.92	28.72	4.95	142.12	1.370	No	Yes	1.64
401	20.05	23.17	2.71	3.71	0.92	27.22	4.81	131.03	1.298	No	Yes	1.55
402	20.10	21.56	2.71	3.44	0.92	25.20	4.86	122.35	1.202	No	Yes	1.44
403	20.15	19.80	2.73	3.33	0.93	23.03	5.08	117.02	1.099	No	Yes	1.31
404	20.20	18.02	2.77	3.38	0.94	20.89	5.51	115.00	0.996	No	Yes	1.19
405	20.25	16.38	2.82	3.52	0.96	18.91	6.06	114.58	0.902	No	Yes	1.08
406	20.30	15.27	2.86	3.72	0.98	17.58	6.59	115.76	0.838	No	Yes	1.00
407	20.35	14.87	2.88	3.94	0.99	17.10	6.93	118.55	0.816	No	Yes	0.97
408	20.40	15.07	2.89	4.19	0.99	17.34	7.11	123.20	0.827	No	Yes	0.98
409	20.45	15.35	2.90	4.42	0.99	17.68	7.23	127.88	0.843	No	Yes	1.00
410	20.50	15.50	2.91	4.68	1.00	17.86	7.42	132.49	0.852	No	Yes	1.01
411	20.55	15.65	2.92	4.89	1.00	18.02	7.56	136.23	0.859	No	Yes	1.02
412	20.60	16.12	2.92	5.05	1.00	18.57	7.55	140.14	0.886	No	Yes	1.05
413	20.65	17.35	2.90	5.06	0.99	20.02	7.19	144.01	0.955	No	Yes	1.13
414	20.70	19.25	2.86	4.97	0.98	22.25	6.63	147.59	1.061	No	Yes	1.26
415	20.75	21.77	2.81	4.75	0.96	25.16	5.94	149.44	1.200	No	Yes	1.42
416	20.80	24.22	2.76	4.50	0.94	27.97	5.34	149.40	1.334	No	Yes	1.58
417	20.85	26.40	2.71	4.24	0.92	30.43	4.84	147.35	1.452	No	Yes	1.72
418	20.90	27.89	2.68	4.01	0.91	32.08	8.98	288.22	3.600	No	No	2.00
419	20.95	28.59	2.66	3.83	0.90	32.79	7.90	258.97	3.600	No	No	2.00
420	21.00	28.38	2.66	3.77	0.90	32.48	7.82	253.94	3.600	No	No	2.00
421	21.05	27.39	2.68	3.85	0.91	31.30	8.73	273.29	3.600	No	No	2.00
422	21.10	25.93	2.71	4.10	0.92	29.61	4.83	142.95	1.412	No	Yes	1.67
423	21.15	24.23	2.76	4.43	0.94	27.65	5.33	147.25	1.319	No	Yes	1.56
424	21.20	22.73	2.80	4.81	0.96	25.91	5.87	152.02	1.236	No	Yes	1.46
425	21.25	21.78	2.83	5.07	0.97	24.80	6.25	154.91	1.183	No	Yes	1.39
426	21.30	21.24	2.85	5.19	0.97	24.13	6.46	155.82	1.151	No	Yes	1.36
427	21.35	20.65	2.85	5.12	0.98	23.40	6.53	152.82	1.116	No	Yes	1.31
428	21.40	19.33	2.87	5.00	0.98	21.80	6.75	147.16	1.040	No	Yes	1.22
429	21.45	17.60	2.89	4.87	0.99	19.73	7.11	140.19	0.941	No	Yes	1.11
430	21.50	15.86	2.93	4.86	1.00	17.63	7.65	134.78	0.841	No	Yes	0.99
431	21.55	14.54	2.96	4.91	1.00	16.01	8.19	131.08	0.764	No	Yes	0.90
432	21.60	13.46	3.00	4.96	1.00	14.69	8.70	127.86	0.701	No	Yes	0.82

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
433	21.65	12.45	3.02	4.95	1.00	13.44	9.21	123.82	0.641	No	Yes	0.75
434	21.70	11.41	3.05	4.87	1.00	12.17	9.73	118.43	0.581	No	Yes	0.68
435	21.75	10.56	3.08	4.77	1.00	11.14	10.20	113.60	0.531	No	Yes	0.62
436	21.80	9.94	3.10	4.67	1.00	10.37	10.56	109.55	0.495	No	Yes	0.58
437	21.85	9.64	3.11	4.66	1.00	10.00	10.79	107.95	0.477	No	Yes	0.56
438	21.90	9.63	3.11	4.69	1.00	9.98	10.85	108.24	0.476	No	Yes	0.56
439	21.95	9.92	3.11	4.81	1.00	10.30	10.76	110.77	0.491	No	Yes	0.57
440	22.00	10.36	3.10	4.93	1.00	10.80	10.57	114.18	0.515	No	Yes	0.60
441	22.05	10.84	3.09	5.10	1.00	11.35	10.42	118.27	0.541	No	Yes	0.63
442	22.10	11.28	3.08	5.28	1.00	11.86	10.32	122.33	0.566	No	Yes	0.66
443	22.15	11.78	3.08	5.48	1.00	12.43	10.20	126.83	0.593	No	Yes	0.69
444	22.20	12.54	3.06	5.62	1.00	13.31	9.91	131.86	0.635	No	Yes	0.74
445	22.25	13.51	3.04	5.70	1.00	14.43	9.49	136.89	0.688	No	Yes	0.80
446	22.30	14.66	3.01	5.68	1.00	15.76	8.96	141.27	0.752	No	Yes	0.88
447	22.35	16.29	2.97	5.58	1.00	17.65	8.25	145.67	0.842	No	Yes	0.98
448	22.40	18.38	2.92	5.37	1.00	20.07	7.44	149.26	0.957	No	Yes	1.11
449	22.45	21.10	2.85	5.07	0.98	23.12	6.54	151.28	1.103	No	Yes	1.28
450	22.50	23.53	2.80	4.71	0.96	25.78	5.81	149.91	1.230	No	Yes	1.43
451	22.55	25.65	2.74	4.30	0.94	28.08	5.17	145.19	1.339	No	Yes	1.56
452	22.60	26.99	2.70	3.91	0.92	29.47	10.13	298.58	3.600	No	No	2.00
453	22.65	27.93	2.66	3.54	0.90	30.40	7.95	241.60	3.600	No	No	2.00
454	22.70	28.11	2.64	3.30	0.90	30.52	6.93	211.60	3.600	No	No	2.00
455	22.75	27.77	2.63	3.15	0.89	30.06	6.58	197.89	0.721	No	No	0.84
456	22.80	26.72	2.65	3.17	0.90	28.86	7.24	208.99	3.600	No	No	2.00
457	22.85	25.36	2.67	3.28	0.91	27.33	8.63	235.73	3.600	No	No	2.00
458	22.90	23.55	2.72	3.50	0.93	25.32	4.89	123.79	1.208	No	Yes	1.40
459	22.95	21.57	2.77	3.73	0.94	23.11	5.43	125.59	1.102	No	Yes	1.28
460	23.00	19.55	2.82	3.99	0.96	20.85	6.08	126.77	0.995	No	Yes	1.15
461	23.05	17.74	2.87	4.21	0.98	18.82	6.74	126.79	0.898	No	Yes	1.04
462	23.10	16.26	2.91	4.43	1.00	17.15	7.39	126.68	0.818	No	Yes	0.95
463	23.15	15.01	2.96	4.65	1.00	15.69	8.05	126.27	0.748	No	Yes	0.86
464	23.20	14.12	2.99	4.87	1.00	14.64	8.64	126.45	0.698	No	Yes	0.81
465	23.25	13.48	3.02	5.11	1.00	13.88	9.17	127.37	0.662	No	Yes	0.76
466	23.30	13.22	3.04	5.36	1.00	13.57	9.55	129.58	0.647	No	Yes	0.75
467	23.35	13.14	3.06	5.68	1.00	13.45	9.89	133.12	0.642	No	Yes	0.74
468	23.40	13.31	3.07	6.01	1.00	13.61	10.12	137.78	0.649	No	Yes	0.75
469	23.45	13.70	3.08	6.33	1.00	14.04	10.21	143.37	0.670	No	Yes	0.77
470	23.50	14.44	3.07	6.52	1.00	14.85	10.02	148.80	0.708	No	Yes	0.82
471	23.55	15.48	3.05	6.54	1.00	16.01	9.59	153.56	0.764	No	Yes	0.88
472	23.60	16.69	3.01	6.38	1.00	17.35	9.00	156.13	0.828	No	Yes	0.95
473	23.65	17.65	2.98	6.13	1.00	18.41	8.48	156.09	0.878	No	Yes	1.01
474	23.70	18.15	2.96	5.81	1.00	18.94	8.08	153.01	0.903	No	Yes	1.04
475	23.75	17.98	2.94	5.50	1.00	18.72	7.88	147.60	0.893	No	Yes	1.03
476	23.80	17.49	2.94	5.19	1.00	18.13	7.79	141.12	0.865	No	Yes	0.99
477	23.85	16.78	2.94	4.89	1.00	17.30	7.77	134.36	0.825	No	Yes	0.95
478	23.90	15.98	2.94	4.64	1.00	16.37	7.82	128.08	0.781	No	Yes	0.90
479	23.95	15.09	2.95	4.41	1.00	15.36	7.93	121.85	0.733	No	Yes	0.84
480	24.00	14.19	2.96	4.21	1.00	14.32	8.11	116.08	0.683	No	Yes	0.78

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
481	24.05	13.55	2.96	4.01	1.00	13.58	8.18	111.15	0.648	No	Yes	0.74
482	24.10	13.20	2.97	3.94	1.00	13.17	8.28	109.11	0.628	No	Yes	0.72
483	24.15	13.30	2.97	4.01	1.00	13.26	8.32	110.41	0.633	No	Yes	0.72
484	24.20	13.74	2.98	4.33	1.00	13.73	8.47	116.27	0.655	No	Yes	0.75
485	24.25	14.80	2.98	4.73	1.00	14.89	8.41	125.27	0.710	No	Yes	0.81
486	24.30	16.23	2.97	5.22	1.00	16.44	8.32	136.81	4.000	Yes	Yes	2.00
487	24.35	18.18	2.95	5.55	1.00	18.58	7.97	148.06	4.000	Yes	Yes	2.00
488	24.40	20.21	2.93	5.78	1.00	20.79	7.59	157.80	4.000	Yes	Yes	2.00
489	24.45	22.53	2.89	5.73	0.99	23.30	7.02	163.48	4.000	Yes	Yes	2.00
490	24.50	25.19	2.84	5.54	0.98	26.12	6.38	166.60	4.000	Yes	Yes	2.00
491	24.55	28.19	2.79	5.21	0.95	29.28	5.69	166.51	4.000	Yes	Yes	2.00
492	24.60	31.49	2.73	4.91	0.93	32.73	5.07	165.98	4.000	Yes	Yes	2.00
493	24.65	34.39	2.69	4.62	0.92	35.73	9.45	337.74	4.000	Yes	No	2.00
494	24.70	36.86	2.65	4.37	0.90	38.27	7.45	285.21	4.000	Yes	No	2.00
495	24.75	38.66	2.62	4.14	0.89	40.08	6.12	245.21	4.000	Yes	No	2.00
496	24.80	40.24	2.59	3.90	0.88	41.65	5.04	210.06	4.000	Yes	No	2.00
497	24.85	41.99	2.56	3.66	0.87	43.39	4.09	177.51	4.000	Yes	No	2.00
498	24.90	44.00	2.52	3.38	0.85	45.38	3.19	144.81	4.000	Yes	No	2.00
499	24.95	46.64	2.48	3.11	0.84	48.02	2.82	135.54	4.000	Yes	No	2.00
500	25.00	49.30	2.43	2.84	0.82	50.65	2.55	129.14	4.000	Yes	No	2.00
501	25.05	52.08	2.39	2.60	0.80	53.40	2.32	123.72	4.000	Yes	No	2.00
502	25.10	53.91	2.35	2.39	0.79	55.16	2.15	118.66	4.000	Yes	No	2.00
503	25.15	55.06	2.33	2.24	0.78	56.22	2.04	114.69	4.000	Yes	No	2.00
504	25.20	55.46	2.31	2.14	0.78	56.53	1.98	111.85	4.000	Yes	No	2.00
505	25.25	55.87	2.30	2.09	0.77	56.85	1.94	110.41	0.205	No	No	0.23
506	25.30	56.48	2.30	2.07	0.77	57.41	1.92	110.21	0.205	No	No	0.23
507	25.35	57.20	2.29	2.06	0.77	58.07	1.90	110.52	0.206	No	No	0.23
508	25.40	57.98	2.29	2.07	0.77	58.80	1.89	111.18	0.208	No	No	0.24
509	25.45	58.95	2.29	2.07	0.77	59.72	1.87	111.96	0.211	No	No	0.24
510	25.50	60.19	2.28	2.06	0.76	60.91	1.85	112.60	0.213	No	No	0.24
511	25.55	61.96	2.27	2.03	0.76	62.63	1.80	112.86	0.214	No	No	0.24
512	25.60	64.03	2.25	1.97	0.75	64.63	1.74	112.54	0.213	No	No	0.24
513	25.65	66.76	2.22	1.90	0.74	67.30	1.67	112.58	0.213	No	No	0.24
514	25.70	69.59	2.20	1.83	0.73	70.06	1.61	113.00	0.214	No	No	0.24
515	25.75	72.49	2.18	1.79	0.73	72.90	1.57	114.12	0.218	No	No	0.25
516	25.80	75.35	2.16	1.76	0.72	75.69	1.53	115.74	0.224	No	No	0.25
517	25.85	78.28	2.15	1.75	0.71	78.55	1.50	118.06	0.233	No	No	0.26
518	25.90	81.53	2.14	1.76	0.71	81.75	1.48	121.18	0.245	No	No	0.28
519	25.95	83.12	2.14	1.78	0.71	83.27	1.48	123.07	0.253	No	No	0.29
520	26.00	82.31	2.14	1.79	0.71	82.35	1.49	122.42	0.251	No	No	0.28
521	26.05	79.36	2.15	1.78	0.71	79.29	1.51	119.46	0.239	No	No	0.27
522	26.10	76.33	2.16	1.75	0.72	76.14	1.52	115.83	0.225	No	No	0.25
523	26.15	75.41	2.16	1.72	0.72	75.11	1.52	114.22	0.219	No	No	0.25
524	26.20	75.46	2.16	1.71	0.72	75.07	1.52	113.85	0.217	No	No	0.25
525	26.25	75.56	2.16	1.72	0.72	75.10	1.52	114.26	0.219	No	No	0.25
526	26.30	74.50	2.17	1.75	0.72	73.96	1.54	114.10	4.000	Yes	No	2.00
527	26.35	72.82	2.18	1.80	0.73	72.22	1.58	113.87	4.000	Yes	No	2.00
528	26.40	71.07	2.20	1.86	0.73	70.41	1.62	113.99	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
529	26.45	69.30	2.22	1.95	0.74	68.58	1.68	115.12	4.000	Yes	No	2.00
530	26.50	67.46	2.25	2.07	0.75	66.70	1.76	117.10	4.000	Yes	No	2.00
531	26.55	65.64	2.28	2.22	0.76	64.85	1.85	120.28	4.000	Yes	No	2.00
532	26.60	63.55	2.31	2.39	0.78	62.72	1.98	123.94	4.000	Yes	No	2.00
533	26.65	61.12	2.35	2.58	0.79	60.26	2.12	128.02	4.000	Yes	No	2.00
534	26.70	58.35	2.39	2.80	0.81	57.45	2.32	133.12	4.000	Yes	No	2.00
535	26.75	55.46	2.43	3.05	0.82	54.53	2.54	138.68	4.000	Yes	No	2.00
536	26.80	52.67	2.48	3.34	0.84	51.71	2.81	145.49	4.000	Yes	No	2.00
537	26.85	49.61	2.52	3.63	0.86	48.61	3.19	155.04	4.000	Yes	No	2.00
538	26.90	46.41	2.57	3.93	0.87	45.37	4.32	195.81	4.000	Yes	No	2.00
539	26.95	42.85	2.61	4.22	0.89	41.77	5.86	244.56	4.000	Yes	No	2.00
540	27.00	39.81	2.65	4.49	0.91	38.68	7.68	297.14	4.000	Yes	No	2.00
541	27.05	37.31	2.69	4.72	0.92	36.14	9.65	348.83	4.000	Yes	No	2.00
542	27.10	35.96	2.71	4.89	0.93	34.74	4.86	168.70	4.000	Yes	Yes	2.00
543	27.15	35.29	2.73	4.99	0.94	34.03	5.00	170.04	1.623	No	Yes	1.83
544	27.20	35.12	2.73	5.03	0.94	33.80	5.04	170.50	1.612	No	Yes	1.82
545	27.25	34.89	2.73	5.03	0.94	33.53	5.07	170.13	1.599	No	Yes	1.80
546	27.30	34.59	2.74	5.03	0.94	33.18	5.11	169.40	1.582	No	Yes	1.78
547	27.35	34.50	2.74	5.04	0.94	33.03	5.13	169.37	1.576	No	Yes	1.77
548	27.40	34.67	2.74	5.08	0.94	33.16	5.14	170.51	1.582	No	Yes	1.78
549	27.45	35.15	2.74	5.14	0.94	33.58	5.14	172.54	1.602	No	Yes	1.80
550	27.50	35.43	2.74	5.21	0.94	33.82	5.17	174.71	1.613	No	Yes	1.82
551	27.55	35.45	2.75	5.30	0.94	33.79	5.23	176.60	1.612	No	Yes	1.81
552	27.60	34.87	2.76	5.40	0.95	33.16	5.36	177.61	1.582	No	Yes	1.78
553	27.65	34.00	2.77	5.49	0.95	32.26	5.52	178.02	1.539	No	Yes	1.73
554	27.70	33.63	2.78	5.55	0.96	31.85	5.61	178.60	1.519	No	Yes	1.71
555	27.75	34.10	2.78	5.56	0.96	32.26	5.56	179.47	1.539	No	Yes	1.73
556	27.80	35.49	2.76	5.47	0.95	33.58	5.36	179.99	1.602	No	Yes	1.80
557	27.85	37.10	2.74	5.31	0.94	35.11	5.10	179.02	1.675	No	Yes	1.88
558	27.90	39.04	2.71	5.06	0.93	36.95	4.77	176.14	1.762	No	Yes	1.98
559	27.95	41.71	2.67	4.77	0.91	39.51	8.28	327.09	3.600	No	No	2.00
560	28.00	44.66	2.62	4.43	0.90	42.31	6.29	265.95	3.600	No	No	2.00
561	28.05	47.02	2.59	4.14	0.88	44.54	4.97	221.33	4.000	No	No	2.00
562	28.10	47.52	2.56	3.88	0.87	44.96	4.27	192.13	0.740	No	No	0.83
563	28.15	46.09	2.56	3.74	0.87	43.50	4.25	184.85	0.667	No	No	0.75
564	28.20	43.31	2.58	3.70	0.88	40.73	4.75	193.45	0.753	No	No	0.85
565	28.25	39.82	2.62	3.80	0.89	37.29	5.99	223.45	3.600	No	No	2.00
566	28.30	36.40	2.66	3.95	0.91	33.92	7.79	264.37	3.600	No	No	2.00
567	28.35	33.71	2.70	4.12	0.93	31.27	9.94	310.68	3.600	No	No	2.00
568	28.40	32.17	2.72	4.26	0.94	29.73	4.94	146.89	1.418	No	Yes	1.59
569	28.45	31.53	2.74	4.39	0.94	29.07	5.11	148.63	1.387	No	Yes	1.56
570	28.50	31.26	2.75	4.51	0.95	28.76	5.24	150.74	1.372	No	Yes	1.54
571	28.55	30.87	2.76	4.63	0.95	28.36	5.38	152.68	1.353	No	Yes	1.52
572	28.60	30.51	2.77	4.73	0.95	27.97	5.51	154.20	1.334	No	Yes	1.50
573	28.65	30.47	2.78	4.79	0.96	27.89	5.57	155.21	1.330	No	Yes	1.49
574	28.70	30.58	2.77	4.77	0.96	27.96	5.55	155.03	1.334	No	Yes	1.50
575	28.75	30.60	2.77	4.69	0.95	27.93	5.49	153.36	1.332	No	Yes	1.49
576	28.80	29.20	2.78	4.58	0.96	26.55	5.60	148.69	1.266	No	Yes	1.42

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q_c (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
577	28.85	26.34	2.81	4.46	0.97	23.76	5.94	141.17	1.133	No	Yes	1.27
578	28.90	22.09	2.86	4.34	0.99	19.64	6.66	130.78	0.937	No	Yes	1.05
579	28.95	18.12	2.92	4.19	1.00	15.80	7.57	119.61	0.754	No	Yes	0.84
580	29.00	15.37	2.98	4.02	1.00	13.13	8.39	110.11	0.626	No	Yes	0.70
581	29.05	14.03	3.00	3.79	1.00	11.83	8.73	103.30	0.564	No	Yes	0.63
582	29.10	13.51	3.00	3.57	1.00	11.32	8.73	98.81	0.540	No	Yes	0.60
583	29.15	13.24	2.99	3.34	1.00	11.05	8.59	94.90	0.527	No	Yes	0.59
584	29.20	13.11	2.98	3.16	1.00	10.91	8.43	91.97	0.520	No	Yes	0.58
585	29.25	13.11	2.97	3.04	1.00	10.89	8.28	90.19	0.519	No	Yes	0.58
586	29.30	13.11	2.97	3.03	1.00	10.87	8.27	89.95	0.519	No	Yes	0.58
587	29.35	13.11	2.98	3.10	1.00	10.86	8.38	90.96	0.518	No	Yes	0.58
588	29.40	13.11	2.99	3.25	1.00	10.84	8.58	93.04	0.517	No	Yes	0.58
589	29.45	13.11	3.00	3.42	1.00	10.83	8.81	95.44	0.517	No	Yes	0.58
590	29.50	13.36	3.01	3.60	1.00	11.05	8.91	98.49	0.527	No	Yes	0.59
591	29.55	13.81	3.01	3.77	1.00	11.47	8.89	101.95	0.547	No	Yes	0.61
592	29.60	14.52	3.00	3.90	1.00	12.12	8.71	105.65	0.578	No	Yes	0.65
593	29.65	15.32	2.98	4.01	1.00	12.86	8.49	109.24	0.614	No	Yes	0.69
594	29.70	16.41	2.96	4.07	1.00	13.87	8.13	112.82	0.662	No	Yes	0.74
595	29.75	17.69	2.93	4.10	1.00	15.06	7.73	116.36	0.718	No	Yes	0.80
596	29.80	19.03	2.91	4.06	1.00	16.30	7.28	118.68	0.778	No	Yes	0.87
597	29.85	19.87	2.88	3.98	1.00	17.07	6.98	119.18	0.814	No	Yes	0.91
598	29.90	20.01	2.88	3.89	1.00	17.18	6.86	117.81	0.820	No	Yes	0.92
599	29.95	18.99	2.89	3.85	1.00	16.20	7.10	115.07	0.773	No	Yes	0.86
600	30.00	18.18	2.91	3.85	1.00	15.42	7.35	113.32	0.735	No	Yes	0.82
601	30.05	18.22	2.91	3.82	1.00	15.43	7.31	112.87	0.736	No	Yes	0.82
602	30.10	20.31	2.86	3.70	0.99	17.37	6.62	115.01	0.828	No	Yes	0.92
603	30.15	23.10	2.80	3.55	0.97	19.96	5.85	116.84	0.952	No	Yes	1.06
604	30.20	25.29	2.76	3.44	0.95	21.99	5.36	117.94	1.049	No	Yes	1.17
605	30.25	26.11	2.75	3.43	0.95	22.72	5.23	118.75	1.084	No	Yes	1.21
606	30.30	25.75	2.76	3.55	0.95	22.35	5.40	120.72	1.066	No	Yes	1.19
607	30.35	25.28	2.79	3.82	0.96	21.88	5.73	125.41	1.044	No	Yes	1.16
608	30.40	24.92	2.83	4.25	0.98	21.51	6.18	132.98	1.026	No	Yes	1.14
609	30.45	26.19	2.84	4.78	0.98	22.65	6.40	144.96	1.081	No	Yes	1.20
610	30.50	28.97	2.84	5.29	0.98	25.20	6.35	160.00	4.000	Yes	Yes	2.00
611	30.55	34.13	2.80	5.62	0.97	29.94	5.88	176.16	4.000	Yes	Yes	2.00
612	30.60	40.03	2.76	5.70	0.95	35.37	5.32	188.27	4.000	Yes	Yes	2.00
613	30.65	47.16	2.69	5.49	0.93	41.93	9.75	408.80	4.000	Yes	No	2.00
614	30.70	53.35	2.63	5.08	0.90	47.61	6.60	314.00	4.000	Yes	No	2.00
615	30.75	58.70	2.57	4.60	0.88	52.51	4.47	234.60	4.000	Yes	No	2.00
616	30.80	62.66	2.52	4.14	0.86	56.12	3.15	176.64	4.000	Yes	No	2.00
617	30.85	66.56	2.47	3.77	0.84	59.66	2.77	165.44	4.000	Yes	No	2.00
618	30.90	71.42	2.42	3.47	0.82	64.10	2.49	159.58	4.000	Yes	No	2.00
619	30.95	76.82	2.38	3.21	0.81	69.03	2.25	155.17	4.000	Yes	No	2.00
620	31.00	82.78	2.33	2.98	0.79	74.46	2.04	151.92	4.000	Yes	No	2.00
621	31.05	88.37	2.28	2.75	0.77	79.56	1.87	148.44	4.000	Yes	No	2.00
622	31.10	93.74	2.24	2.55	0.76	84.44	1.73	146.17	4.000	Yes	No	2.00
623	31.15	98.72	2.21	2.41	0.74	88.96	1.64	145.53	4.000	Yes	No	2.00
624	31.20	103.47	2.19	2.35	0.74	93.25	1.58	147.45	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
625	31.25	109.02	2.17	2.35	0.73	98.24	1.55	152.11	0.407	No	No	0.45
626	31.30	115.77	2.16	2.41	0.73	104.33	1.53	159.36	0.456	No	No	0.51
627	31.35	123.72	2.15	2.47	0.72	111.51	1.50	167.81	0.519	No	No	0.58
628	31.40	132.87	2.14	2.52	0.72	119.76	1.48	177.11	0.597	No	No	0.67
629	31.45	142.35	2.12	2.53	0.71	128.33	1.45	185.77	0.676	No	No	0.75
630	31.50	153.16	2.10	2.52	0.70	138.10	1.41	195.20	0.772	No	No	0.86
631	31.55	163.20	2.07	2.48	0.69	147.16	1.38	203.54	4.000	No	No	2.00
632	31.60	173.03	2.05	2.44	0.68	156.02	1.36	211.85	4.000	No	No	2.00
633	31.65	180.44	2.04	2.40	0.68	162.64	1.34	217.88	4.000	No	No	2.00
634	31.70	186.57	2.02	2.36	0.67	168.09	1.33	222.79	4.000	No	No	2.00
635	31.75	191.07	2.01	2.32	0.67	172.05	1.31	226.20	4.000	No	No	2.00
636	31.80	194.89	2.00	2.29	0.66	175.37	1.31	229.14	4.000	No	No	2.00
637	31.85	198.61	1.99	2.27	0.66	178.59	1.30	232.22	4.000	No	No	2.00
638	31.90	202.38	1.98	2.25	0.66	181.85	1.29	235.46	4.000	No	No	2.00
639	31.95	206.39	1.98	2.24	0.66	185.31	1.29	239.04	4.000	No	No	2.00
640	32.00	209.00	1.97	2.24	0.66	187.50	1.29	241.32	4.000	No	No	2.00
641	32.05	210.08	1.97	2.25	0.66	188.27	1.29	242.36	4.000	No	No	2.00
642	32.10	208.94	1.98	2.27	0.66	187.01	1.29	241.44	4.000	No	No	2.00
643	32.15	207.00	1.99	2.31	0.66	185.02	1.30	240.15	4.000	No	No	2.00
644	32.20	204.32	2.00	2.36	0.67	182.34	1.31	238.41	4.000	No	No	2.00
645	32.25	201.85	2.01	2.43	0.67	179.85	1.32	237.31	4.000	No	No	2.00
646	32.30	199.62	2.03	2.50	0.68	177.59	1.33	236.38	4.000	No	No	2.00
647	32.35	198.37	2.04	2.55	0.68	176.23	1.34	236.18	4.000	No	No	2.00
648	32.40	198.24	2.04	2.56	0.68	175.91	1.34	236.04	4.000	No	No	2.00
649	32.45	199.82	2.03	2.54	0.68	177.15	1.34	236.75	4.000	No	No	2.00
650	32.50	202.60	2.02	2.47	0.67	179.52	1.32	237.65	4.000	No	No	2.00
651	32.55	206.36	2.00	2.38	0.67	182.79	1.31	239.27	4.000	No	No	2.00
652	32.60	210.53	1.98	2.28	0.66	186.43	1.29	241.11	4.000	No	No	2.00
653	32.65	214.74	1.96	2.20	0.65	190.11	1.28	243.31	4.000	No	No	2.00
654	32.70	218.70	1.95	2.12	0.65	193.56	1.27	245.52	4.000	No	No	2.00
655	32.75	221.32	1.94	2.07	0.64	195.76	1.26	246.83	4.000	No	No	2.00
656	32.80	222.30	1.93	2.04	0.64	196.48	1.26	246.97	4.000	No	No	2.00
657	32.85	221.39	1.93	2.04	0.64	195.47	1.26	245.74	4.000	No	No	2.00
658	32.90	219.55	1.93	2.05	0.64	193.60	1.26	243.89	4.000	No	No	2.00
659	32.95	217.58	1.94	2.06	0.64	191.62	1.26	242.03	4.000	No	No	2.00
660	33.00	215.84	1.94	2.06	0.65	189.86	1.27	240.19	4.000	No	No	2.00
661	33.05	214.08	1.94	2.06	0.65	188.09	1.27	238.17	4.000	No	No	2.00
662	33.10	211.73	1.95	2.04	0.65	185.81	1.27	235.40	4.000	No	No	2.00
663	33.15	208.42	1.95	2.04	0.65	182.68	1.27	231.84	4.000	No	No	2.00
664	33.20	203.60	1.96	2.04	0.65	178.18	1.27	226.98	4.000	No	No	2.00
665	33.25	197.58	1.97	2.06	0.66	172.60	1.28	221.31	4.000	No	No	2.00
666	33.30	189.54	1.98	2.09	0.66	165.23	1.29	213.96	4.000	No	No	2.00
667	33.35	181.40	2.01	2.15	0.67	157.75	1.31	207.08	4.000	No	No	2.00
668	33.40	173.00	2.03	2.22	0.68	150.06	1.34	200.33	4.000	No	No	2.00
669	33.45	166.53	2.05	2.29	0.69	144.09	1.36	195.86	0.779	No	No	0.87
670	33.50	161.02	2.07	2.35	0.70	139.02	1.38	191.82	0.736	No	No	0.83
671	33.55	157.44	2.08	2.37	0.70	135.69	1.39	189.00	0.708	No	No	0.79
672	33.60	155.20	2.08	2.35	0.70	133.59	1.39	186.21	0.680	No	No	0.76

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
673	33.65	155.05	2.08	2.29	0.70	133.36	1.39	184.71	0.666	No	No	0.75
674	33.70	155.92	2.06	2.21	0.69	134.06	1.37	183.45	0.654	No	No	0.73
675	33.75	157.40	2.05	2.12	0.69	135.31	1.35	182.75	0.648	No	No	0.73
676	33.80	158.78	2.03	2.03	0.68	136.49	1.33	181.82	0.639	No	No	0.72
677	33.85	160.22	2.01	1.94	0.67	137.70	1.32	181.31	0.634	No	No	0.71
678	33.90	161.17	2.00	1.86	0.67	138.50	1.30	180.58	0.628	No	No	0.71
679	33.95	161.04	1.99	1.81	0.66	138.31	1.30	179.34	0.616	No	No	0.69
680	34.00	159.04	1.98	1.77	0.66	136.45	1.30	176.73	0.593	No	No	0.67
681	34.05	156.01	1.99	1.78	0.67	133.64	1.30	173.80	0.568	No	No	0.64
682	34.10	152.34	2.00	1.81	0.67	130.25	1.31	170.80	0.543	No	No	0.61
683	34.15	149.01	2.02	1.87	0.68	127.13	1.33	168.66	0.526	No	No	0.59
684	34.20	145.93	2.04	1.93	0.68	124.24	1.34	166.90	0.512	No	No	0.58
685	34.25	143.37	2.05	1.99	0.69	121.81	1.36	165.70	0.503	No	No	0.57
686	34.30	141.80	2.07	2.04	0.69	120.26	1.37	165.25	0.500	No	No	0.56
687	34.35	141.31	2.07	2.08	0.70	119.67	1.38	165.60	0.502	No	No	0.57
688	34.40	141.88	2.08	2.11	0.70	120.02	1.39	166.64	0.510	No	No	0.57
689	34.45	143.01	2.08	2.13	0.70	120.85	1.39	167.98	0.521	No	No	0.59
690	34.50	144.50	2.08	2.15	0.70	122.01	1.39	169.67	0.534	No	No	0.60
691	34.55	146.18	2.08	2.18	0.70	123.31	1.39	171.61	0.550	No	No	0.62
692	34.60	148.30	2.08	2.20	0.70	125.00	1.39	173.90	0.569	No	No	0.64
693	34.65	150.68	2.08	2.21	0.70	126.93	1.39	176.09	0.588	No	No	0.66
694	34.70	153.55	2.07	2.20	0.70	129.30	1.38	178.30	0.607	No	No	0.68
695	34.75	156.78	2.06	2.17	0.69	132.00	1.37	180.38	0.626	No	No	0.71
696	34.80	160.27	2.05	2.13	0.69	134.93	1.35	182.58	0.646	No	No	0.73
697	34.85	163.82	2.04	2.09	0.68	137.92	1.34	184.80	0.667	No	No	0.75
698	34.90	166.56	2.03	2.07	0.68	140.18	1.33	186.64	0.685	No	No	0.77
699	34.95	168.16	2.02	2.06	0.68	141.44	1.33	187.78	0.696	No	No	0.78
700	35.00	168.07	2.03	2.08	0.68	141.20	1.33	187.93	0.697	No	No	0.79
701	35.05	166.85	2.03	2.11	0.68	139.96	1.34	187.36	0.692	No	No	0.78
702	35.10	165.03	2.05	2.16	0.69	138.17	1.35	186.60	0.684	No	No	0.77
703	35.15	163.32	2.06	2.21	0.69	136.50	1.36	185.97	0.678	No	No	0.77
704	35.20	162.03	2.07	2.26	0.70	135.19	1.37	185.69	0.675	No	No	0.76
705	35.25	161.27	2.07	2.29	0.70	134.37	1.38	185.58	0.674	No	No	0.76
706	35.30	160.94	2.08	2.31	0.70	133.92	1.39	185.60	0.675	No	No	0.76
707	35.35	161.08	2.08	2.31	0.70	133.89	1.39	185.75	0.676	No	No	0.76
708	35.40	161.52	2.08	2.32	0.70	134.13	1.39	186.05	0.679	No	No	0.77
709	35.45	162.34	2.08	2.32	0.70	134.69	1.39	186.63	0.685	No	No	0.77
710	35.50	163.26	2.07	2.32	0.70	135.34	1.38	187.29	0.691	No	No	0.78
711	35.55	164.33	2.07	2.32	0.70	136.12	1.38	188.07	0.699	No	No	0.79
712	35.60	165.51	2.07	2.31	0.70	136.99	1.38	188.81	0.706	No	No	0.80
713	35.65	166.97	2.07	2.30	0.70	138.11	1.37	189.67	0.715	No	No	0.81
714	35.70	168.87	2.06	2.28	0.69	139.62	1.37	190.72	0.725	No	No	0.82
715	35.75	171.00	2.05	2.25	0.69	141.33	1.36	191.99	0.738	No	No	0.84
716	35.80	173.32	2.05	2.23	0.69	143.18	1.35	193.48	0.754	No	No	0.85
717	35.85	175.30	2.04	2.22	0.69	144.75	1.35	194.80	0.767	No	No	0.87
718	35.90	177.07	2.04	2.21	0.69	146.14	1.34	195.98	0.780	No	No	0.88
719	35.95	178.13	2.03	2.20	0.69	146.90	1.34	196.61	0.787	No	No	0.89
720	36.00	178.63	2.03	2.20	0.68	147.17	1.34	196.90	0.790	No	No	0.90

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
721	36.05	177.88	2.04	2.21	0.69	146.38	1.34	196.23	0.783	No	No	0.89
722	36.10	176.26	2.04	2.22	0.69	144.84	1.35	194.88	0.768	No	No	0.87
723	36.15	173.28	2.05	2.23	0.69	142.14	1.35	192.38	0.742	No	No	0.84
724	36.20	169.82	2.06	2.25	0.69	139.04	1.36	189.59	0.714	No	No	0.81
725	36.25	165.72	2.07	2.27	0.70	135.41	1.38	186.35	0.682	No	No	0.77
726	36.30	161.89	2.08	2.30	0.70	132.00	1.39	183.40	0.654	No	No	0.74
727	36.35	157.98	2.09	2.31	0.71	128.56	1.40	180.16	0.624	No	No	0.71
728	36.40	152.84	2.10	2.31	0.71	124.11	1.42	175.67	0.584	No	No	0.66
729	36.45	146.42	2.11	2.29	0.71	118.61	1.43	169.73	0.535	No	No	0.61
730	36.50	137.93	2.12	2.26	0.72	111.40	1.45	161.92	0.475	No	No	0.54
731	36.55	131.24	2.13	2.21	0.72	105.74	1.47	155.26	0.428	No	No	0.49
732	36.60	126.58	2.13	2.16	0.72	101.79	1.48	150.19	0.395	No	No	0.45
733	36.65	126.90	2.13	2.11	0.72	102.02	1.46	148.88	0.387	No	No	0.44
734	36.70	129.22	2.11	2.07	0.72	103.91	1.44	149.66	0.392	No	No	0.45
735	36.75	132.57	2.10	2.04	0.71	106.64	1.42	151.77	0.405	No	No	0.46
736	36.80	132.90	2.11	2.08	0.71	106.77	1.43	152.68	4.000	Yes	No	2.00
737	36.85	129.15	2.13	2.15	0.72	103.43	1.46	151.48	4.000	Yes	No	2.00
738	36.90	120.57	2.18	2.33	0.74	95.99	1.56	149.44	4.000	Yes	No	2.00
739	36.95	109.20	2.24	2.58	0.76	86.26	1.72	148.40	4.000	Yes	No	2.00
740	37.00	96.25	2.32	2.92	0.80	75.25	2.00	150.52	4.000	Yes	No	2.00
741	37.05	83.85	2.40	3.31	0.83	64.83	2.39	154.97	4.000	Yes	No	2.00
742	37.10	71.18	2.50	3.74	0.86	54.30	2.94	159.91	4.000	Yes	No	2.00
743	37.15	60.50	2.59	4.21	0.90	45.50	4.91	223.60	4.000	Yes	No	2.00
744	37.20	51.00	2.67	4.66	0.93	37.77	8.64	326.21	4.000	Yes	No	2.00
745	37.25	44.67	2.74	5.04	0.96	32.64	5.17	168.73	4.000	Yes	Yes	2.00
746	37.30	39.79	2.79	5.23	0.98	28.73	5.77	165.90	4.000	Yes	Yes	2.00
747	37.35	36.21	2.83	5.26	0.99	25.89	6.21	160.83	4.000	Yes	Yes	2.00
748	37.40	33.31	2.85	5.13	1.00	23.61	6.50	153.47	4.000	Yes	Yes	2.00
749	37.45	31.01	2.86	4.92	1.00	21.83	6.68	145.85	1.041	No	Yes	1.19
750	37.50	29.53	2.87	4.67	1.00	20.68	6.72	138.90	0.986	No	Yes	1.13
751	37.55	28.34	2.87	4.44	1.00	19.75	6.73	132.88	0.942	No	Yes	1.08
752	37.60	27.15	2.87	4.23	1.00	18.83	6.75	127.12	0.898	No	Yes	1.03
753	37.65	26.61	2.86	4.06	1.00	18.40	6.71	123.40	0.878	No	Yes	1.00
754	37.70	28.33	2.83	3.93	0.99	19.71	6.27	123.59	0.940	No	Yes	1.07
755	37.75	31.84	2.80	4.01	0.98	22.41	5.80	129.95	1.069	No	Yes	1.22
756	37.80	36.44	2.76	4.22	0.97	25.93	5.40	140.08	1.237	No	Yes	1.41
757	37.85	38.93	2.77	4.61	0.97	27.78	5.45	151.43	1.325	No	Yes	1.51
758	37.90	40.34	2.78	4.94	0.97	28.79	5.56	160.06	1.374	No	Yes	1.57
759	37.95	43.01	2.77	5.15	0.97	30.79	5.45	167.96	4.000	Yes	Yes	2.00
760	38.00	48.68	2.71	4.95	0.95	35.20	4.85	170.85	4.000	Yes	Yes	2.00
761	38.05	58.51	2.62	4.51	0.91	42.95	6.31	271.06	4.000	Yes	No	2.00
762	38.10	69.29	2.52	3.85	0.87	51.60	3.20	165.13	4.000	Yes	No	2.00
763	38.15	81.00	2.41	3.22	0.83	61.13	2.44	149.34	4.000	Yes	No	2.00
764	38.20	91.48	2.31	2.61	0.79	69.87	1.95	136.32	4.000	Yes	No	2.00
765	38.25	100.61	2.22	2.17	0.76	77.55	1.66	128.87	4.000	Yes	No	2.00
766	38.30	107.26	2.15	1.84	0.73	83.27	1.50	124.52	4.000	Yes	No	2.00
767	38.35	110.81	2.10	1.66	0.72	86.35	1.42	122.93	4.000	Yes	No	2.00
768	38.40	111.54	2.08	1.55	0.71	87.02	1.39	121.21	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
769	38.45	110.10	2.08	1.54	0.71	85.78	1.40	119.80	0.240	No	No	0.28
770	38.50	107.73	2.10	1.57	0.71	83.72	1.42	118.55	0.235	No	No	0.27
771	38.55	104.98	2.12	1.65	0.72	81.28	1.45	118.12	0.233	No	No	0.27
772	38.60	102.27	2.15	1.75	0.73	78.87	1.50	118.33	0.234	No	No	0.27
773	38.65	99.41	2.18	1.86	0.74	76.33	1.56	119.14	0.237	No	No	0.27
774	38.70	97.36	2.20	1.97	0.75	74.48	1.62	120.46	0.243	No	No	0.28
775	38.75	96.13	2.22	2.05	0.76	73.33	1.66	121.75	0.248	No	No	0.28
776	38.80	96.51	2.22	2.07	0.76	73.55	1.67	122.50	0.251	No	No	0.29
777	38.85	97.65	2.21	2.04	0.76	74.42	1.65	122.48	0.251	No	No	0.29
778	38.90	99.57	2.20	1.97	0.75	75.96	1.60	121.86	0.248	No	No	0.29
779	38.95	101.45	2.18	1.91	0.75	77.49	1.57	121.34	0.246	No	No	0.28
780	39.00	103.41	2.16	1.85	0.74	79.06	1.53	121.23	0.246	No	No	0.28
781	39.05	104.30	2.16	1.85	0.74	79.71	1.53	121.67	0.248	No	No	0.28
782	39.10	104.12	2.17	1.89	0.74	79.44	1.54	122.39	4.000	Yes	No	2.00
783	39.15	102.07	2.19	1.98	0.75	77.60	1.59	123.48	4.000	Yes	No	2.00
784	39.20	99.25	2.22	2.12	0.76	75.11	1.67	125.26	4.000	Yes	No	2.00
785	39.25	95.46	2.26	2.30	0.78	71.83	1.78	128.08	4.000	Yes	No	2.00
786	39.30	91.24	2.30	2.52	0.79	68.21	1.94	132.15	4.000	Yes	No	2.00
787	39.35	85.91	2.35	2.77	0.81	63.72	2.15	136.82	4.000	Yes	No	2.00
788	39.40	80.34	2.41	3.07	0.83	59.09	2.42	142.78	4.000	Yes	No	2.00
789	39.45	74.97	2.46	3.36	0.85	54.68	2.72	148.58	4.000	Yes	No	2.00
790	39.50	70.67	2.51	3.67	0.87	51.14	2.94	150.55	4.000	Yes	No	2.00
791	39.55	67.29	2.54	3.90	0.88	48.38	3.73	180.26	4.000	Yes	No	2.00
792	39.60	64.57	2.57	4.06	0.89	46.18	4.44	205.13	4.000	Yes	No	2.00
793	39.65	63.21	2.58	4.05	0.90	45.08	4.64	209.10	4.000	No	No	2.00
794	39.70	63.09	2.57	3.95	0.89	44.98	4.43	199.08	4.000	Yes	No	2.00
795	39.75	64.30	2.55	3.77	0.89	45.91	3.88	178.29	4.000	Yes	No	2.00
796	39.80	65.78	2.53	3.64	0.88	47.05	3.44	161.70	4.000	Yes	No	2.00
797	39.85	67.57	2.51	3.53	0.87	48.42	3.04	147.35	4.000	Yes	No	2.00
798	39.90	69.92	2.48	3.33	0.86	50.27	2.87	144.07	4.000	Yes	No	2.00
799	39.95	73.38	2.44	3.03	0.84	53.05	2.58	136.93	4.000	Yes	No	2.00
800	40.00	76.70	2.38	2.66	0.82	55.79	2.29	127.51	4.000	Yes	No	2.00
801	40.05	79.39	2.34	2.38	0.81	58.04	2.07	120.37	4.000	Yes	No	2.00
802	40.10	80.09	2.32	2.26	0.80	58.63	2.00	117.00	4.000	Yes	No	2.00
803	40.15	79.80	2.32	2.27	0.80	58.34	2.01	117.02	0.229	No	No	0.27
804	40.20	78.56	2.34	2.36	0.81	57.24	2.08	118.96	0.237	No	No	0.27
805	40.25	77.27	2.36	2.45	0.81	56.10	2.16	121.10	0.245	No	No	0.28
806	40.30	75.86	2.37	2.55	0.82	54.88	2.24	123.19	0.254	No	No	0.29
807	40.35	74.61	2.39	2.62	0.83	53.81	2.32	124.64	0.260	No	No	0.30
808	40.40	73.46	2.40	2.65	0.83	52.85	2.36	124.90	0.261	No	No	0.30
809	40.45	72.40	2.40	2.62	0.83	52.00	2.37	123.47	0.255	No	No	0.30
810	40.50	71.39	2.40	2.56	0.83	51.21	2.36	120.96	0.245	No	No	0.28
811	40.55	70.32	2.39	2.47	0.83	50.39	2.34	117.87	0.232	No	No	0.27
812	40.60	68.99	2.40	2.46	0.83	49.33	2.36	116.60	4.000	Yes	No	2.00
813	40.65	67.26	2.41	2.51	0.84	47.92	2.45	117.24	4.000	Yes	No	2.00
814	40.70	64.92	2.45	2.69	0.85	45.97	2.64	121.43	4.000	Yes	No	2.00
815	40.75	62.36	2.49	2.93	0.87	43.85	2.89	126.93	4.000	Yes	No	2.00
816	40.80	59.39	2.53	3.24	0.88	41.41	3.54	146.49	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _k (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
817	40.85	56.83	2.57	3.48	0.90	39.33	4.55	178.93	4.000	Yes	No	2.00
818	40.90	54.64	2.60	3.68	0.91	37.58	5.56	208.85	4.000	Yes	No	2.00
819	40.95	54.44	2.61	3.72	0.91	37.37	5.73	214.01	4.000	Yes	No	2.00
820	41.00	55.85	2.59	3.64	0.91	38.41	5.19	199.38	4.000	Yes	No	2.00
821	41.05	59.98	2.55	3.39	0.89	41.56	3.85	159.89	4.000	Yes	No	2.00
822	41.10	65.10	2.49	3.10	0.87	45.50	2.93	133.14	4.000	Yes	No	2.00
823	41.15	71.52	2.43	2.77	0.84	50.49	2.51	126.96	4.000	Yes	No	2.00
824	41.20	77.66	2.37	2.49	0.82	55.32	2.20	121.83	4.000	Yes	No	2.00
825	41.25	84.09	2.31	2.25	0.80	60.40	1.95	117.94	4.000	Yes	No	2.00
826	41.30	90.57	2.25	2.04	0.78	65.55	1.76	115.56	4.000	Yes	No	2.00
827	41.35	97.02	2.20	1.87	0.76	70.71	1.62	114.48	4.000	Yes	No	2.00
828	41.40	103.34	2.15	1.70	0.74	75.81	1.51	114.35	4.000	Yes	No	2.00
829	41.45	108.53	2.11	1.57	0.72	80.03	1.44	115.04	4.000	Yes	No	2.00
830	41.50	113.02	2.08	1.47	0.71	83.70	1.39	116.12	4.000	Yes	No	2.00
831	41.55	115.16	2.06	1.40	0.70	85.45	1.36	116.49	4.000	Yes	No	2.00
832	41.60	115.36	2.05	1.36	0.70	85.63	1.35	115.88	0.225	No	No	0.26
833	41.65	111.94	2.06	1.36	0.70	82.85	1.37	113.19	4.000	Yes	No	2.00
834	41.70	106.66	2.09	1.40	0.71	78.55	1.40	109.84	4.000	Yes	No	2.00
835	41.75	98.88	2.13	1.49	0.73	72.23	1.47	105.98	4.000	Yes	No	2.00
836	41.80	90.96	2.19	1.65	0.75	65.75	1.59	104.54	4.000	Yes	No	2.00
837	41.85	82.43	2.26	1.88	0.78	58.83	1.80	105.82	4.000	Yes	No	2.00
838	41.90	75.38	2.34	2.18	0.81	53.10	2.08	110.70	4.000	Yes	No	2.00
839	41.95	69.28	2.41	2.47	0.84	48.21	2.41	116.29	4.000	Yes	No	2.00
840	42.00	64.01	2.47	2.75	0.86	44.03	2.77	121.84	4.000	Yes	No	2.00
841	42.05	59.15	2.52	3.03	0.88	40.23	3.31	133.15	4.000	Yes	No	2.00
842	42.10	54.53	2.58	3.34	0.90	36.64	4.87	178.38	4.000	Yes	No	2.00
843	42.15	51.91	2.63	3.62	0.92	34.58	6.38	220.45	4.000	Yes	No	2.00
844	42.20	50.83	2.65	3.84	0.93	33.68	7.51	252.86	4.000	Yes	No	2.00
845	42.25	51.46	2.65	3.91	0.93	34.07	7.60	259.02	3.600	No	No	2.00
846	42.30	52.30	2.65	3.91	0.93	34.64	7.34	254.21	3.600	No	No	2.00
847	42.35	53.04	2.64	3.83	0.92	35.17	6.84	240.47	3.600	No	No	2.00
848	42.40	53.37	2.63	3.77	0.92	35.39	6.55	231.68	3.600	No	No	2.00
849	42.45	53.34	2.63	3.74	0.92	35.34	6.49	229.32	3.600	No	No	2.00
850	42.50	52.74	2.64	3.82	0.93	34.84	6.94	241.94	3.600	No	No	2.00
851	42.55	51.69	2.66	3.96	0.93	34.00	7.79	264.67	3.600	No	No	2.00
852	42.60	49.87	2.69	4.17	0.94	32.58	9.36	304.96	3.600	No	No	2.00
853	42.65	47.83	2.72	4.43	0.96	31.01	4.92	152.45	1.479	No	Yes	1.75
854	42.70	45.50	2.76	4.75	0.97	29.23	5.36	156.77	1.394	No	Yes	1.65
855	42.75	44.11	2.79	5.05	0.98	28.14	5.73	161.19	1.342	No	Yes	1.59
856	42.80	43.65	2.81	5.32	0.99	27.72	5.98	165.81	1.322	No	Yes	1.56
857	42.85	45.52	2.80	5.40	0.99	28.99	5.86	169.89	4.000	Yes	Yes	2.00
858	42.90	48.86	2.77	5.32	0.98	31.33	5.51	172.70	4.000	Yes	Yes	2.00
859	42.95	54.26	2.72	5.02	0.96	35.19	4.90	172.48	4.000	Yes	Yes	2.00
860	43.00	59.96	2.66	4.63	0.93	39.32	7.90	310.57	4.000	Yes	No	2.00
861	43.05	66.38	2.59	4.15	0.91	44.07	5.09	224.15	4.000	Yes	No	2.00
862	43.10	71.78	2.53	3.69	0.88	48.15	3.37	162.30	4.000	Yes	No	2.00
863	43.15	76.39	2.47	3.27	0.86	51.71	2.77	143.28	4.000	Yes	No	2.00
864	43.20	78.77	2.42	2.94	0.84	53.63	2.51	134.57	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
865	43.25	79.71	2.40	2.71	0.83	54.45	2.35	128.17	4.000	Yes	No	2.00
866	43.30	79.20	2.39	2.62	0.83	54.10	2.31	124.94	0.261	No	No	0.31
867	43.35	78.76	2.39	2.66	0.83	53.69	2.34	125.89	4.000	Yes	No	2.00
868	43.40	78.69	2.41	2.80	0.84	53.47	2.43	130.11	4.000	Yes	No	2.00
869	43.45	78.43	2.44	3.01	0.85	53.06	2.57	136.32	4.000	Yes	No	2.00
870	43.50	77.44	2.46	3.24	0.86	52.12	2.74	142.81	4.000	Yes	No	2.00
871	43.55	74.94	2.50	3.51	0.87	50.08	2.98	149.15	4.000	Yes	No	2.00
872	43.60	72.49	2.53	3.76	0.89	48.11	3.50	168.61	4.000	Yes	No	2.00
873	43.65	70.55	2.56	4.01	0.90	46.54	4.28	199.07	4.000	Yes	No	2.00
874	43.70	71.50	2.57	4.17	0.90	47.08	4.53	213.05	4.000	No	No	2.00
875	43.75	74.94	2.56	4.25	0.90	49.44	4.27	210.98	4.000	Yes	No	2.00
876	43.80	80.85	2.53	4.16	0.89	53.66	3.46	185.82	4.000	Yes	No	2.00
877	43.85	87.12	2.49	3.97	0.87	58.21	2.93	170.73	4.000	Yes	No	2.00
878	43.90	93.83	2.45	3.69	0.85	63.18	2.63	166.08	4.000	Yes	No	2.00
879	43.95	101.14	2.40	3.41	0.84	68.65	2.35	161.46	4.000	Yes	No	2.00
880	44.00	110.53	2.34	3.11	0.81	75.73	2.08	157.27	4.000	Yes	No	2.00
881	44.05	121.59	2.28	2.86	0.79	84.08	1.85	155.83	4.000	Yes	No	2.00
882	44.10	133.55	2.22	2.65	0.77	93.17	1.68	156.49	4.000	Yes	No	2.00
883	44.15	145.66	2.17	2.46	0.75	102.44	1.55	158.95	4.000	Yes	No	2.00
884	44.20	156.89	2.13	2.28	0.73	111.13	1.46	162.31	4.000	Yes	No	2.00
885	44.25	168.00	2.08	2.12	0.72	119.81	1.39	166.68	4.000	Yes	No	2.00
886	44.30	177.83	2.05	2.01	0.70	127.46	1.35	172.03	4.000	Yes	No	2.00
887	44.35	187.59	2.02	1.95	0.69	134.95	1.32	178.61	4.000	Yes	No	2.00
888	44.40	196.04	2.00	1.94	0.69	141.30	1.31	185.16	0.670	No	No	0.80
889	44.45	203.45	1.99	1.94	0.68	146.83	1.30	191.06	0.729	No	No	0.88
890	44.50	209.43	1.98	1.94	0.68	151.26	1.29	195.82	0.778	No	No	0.94
891	44.55	214.10	1.98	1.94	0.68	154.68	1.29	199.50	0.818	No	No	0.98
892	44.60	217.99	1.97	1.94	0.67	157.52	1.29	202.56	4.000	No	No	2.00
893	44.65	220.70	1.97	1.94	0.67	159.45	1.28	204.64	4.000	No	No	2.00
894	44.70	222.71	1.97	1.94	0.67	160.85	1.28	206.15	4.000	No	No	2.00
895	44.75	223.47	1.97	1.94	0.67	161.28	1.28	206.62	4.000	No	No	2.00
896	44.80	223.50	1.97	1.94	0.67	161.17	1.28	206.50	4.000	No	No	2.00
897	44.85	222.63	1.97	1.94	0.67	160.37	1.28	205.63	4.000	No	No	2.00
898	44.90	221.39	1.97	1.94	0.67	159.29	1.28	204.47	4.000	No	No	2.00
899	44.95	219.77	1.97	1.94	0.67	157.93	1.29	203.00	4.000	No	No	2.00
900	45.00	218.21	1.97	1.94	0.68	156.60	1.29	201.57	4.000	No	No	2.00
901	45.05	216.72	1.98	1.94	0.68	155.34	1.29	200.21	4.000	No	No	2.00
902	45.10	215.31	1.98	1.94	0.68	154.14	1.29	198.92	0.812	No	No	0.98
903	45.15	213.85	1.98	1.94	0.68	152.90	1.29	197.59	0.797	No	No	0.97
904	45.20	212.05	1.98	1.94	0.68	151.41	1.29	195.99	0.780	No	No	0.94
905	45.25	210.12	1.99	1.94	0.68	149.82	1.30	194.28	0.762	No	No	0.92
906	45.30	208.04	1.99	1.94	0.68	148.13	1.30	192.46	0.743	No	No	0.90
907	45.35	206.23	1.99	1.94	0.68	146.62	1.30	190.94	0.727	No	No	0.88
908	45.40	204.69	2.00	1.95	0.69	145.30	1.31	189.71	0.715	No	No	0.87
909	45.45	203.43	2.00	1.97	0.69	144.18	1.31	188.79	0.706	No	No	0.86
910	45.50	202.70	2.01	1.98	0.69	143.47	1.31	188.21	0.700	No	No	0.85
911	45.55	202.59	2.01	1.98	0.69	143.27	1.31	187.99	0.698	No	No	0.85
912	45.60	203.21	2.00	1.97	0.69	143.64	1.31	188.19	0.700	No	No	0.85

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
913	45.65	204.10	2.00	1.95	0.69	144.23	1.31	188.55	0.703	No	No	0.86
914	45.70	204.99	2.00	1.94	0.69	144.82	1.31	189.00	0.708	No	No	0.86
915	45.75	205.81	2.00	1.94	0.69	145.33	1.30	189.43	0.712	No	No	0.87
916	45.80	206.70	1.99	1.93	0.68	145.89	1.30	189.91	0.717	No	No	0.87
917	45.85	207.49	1.99	1.91	0.68	146.44	1.30	190.12	0.719	No	No	0.88
918	45.90	208.14	1.98	1.88	0.68	146.95	1.29	189.95	0.717	No	No	0.88
919	45.95	208.40	1.97	1.82	0.68	147.27	1.28	189.18	0.710	No	No	0.87
920	46.00	208.46	1.96	1.75	0.67	147.51	1.27	188.06	0.699	No	No	0.85
921	46.05	208.14	1.94	1.66	0.66	147.56	1.26	186.44	0.683	No	No	0.83
922	46.10	207.68	1.92	1.57	0.66	147.52	1.25	184.66	0.666	No	No	0.81
923	46.15	207.15	1.90	1.47	0.65	147.51	1.24	182.64	0.647	No	No	0.79
924	46.20	207.36	1.88	1.38	0.64	148.01	1.22	181.28	0.634	No	No	0.78
925	46.25	208.33	1.86	1.31	0.64	149.06	1.21	180.46	0.627	No	No	0.77
926	46.30	210.67	1.85	1.26	0.63	151.03	1.20	180.98	0.631	No	No	0.77
927	46.35	213.60	1.83	1.23	0.62	153.39	1.19	181.99	0.641	No	No	0.79
928	46.40	217.34	1.82	1.20	0.62	156.32	1.17	183.58	0.655	No	No	0.80
929	46.45	220.91	1.81	1.17	0.61	159.14	1.16	184.76	0.667	No	No	0.82
930	46.50	224.61	1.79	1.13	0.61	162.13	1.14	185.42	0.673	No	No	0.83
931	46.55	227.82	1.78	1.09	0.60	164.78	1.12	185.18	0.671	No	No	0.82
932	46.60	230.78	1.76	1.05	0.60	167.27	1.10	184.06	0.660	No	No	0.81
933	46.65	232.99	1.75	1.02	0.59	169.16	1.08	182.33	0.644	No	No	0.79
934	46.70	234.26	1.73	0.99	0.59	170.31	1.06	179.97	0.622	No	No	0.77
935	46.75	234.70	1.72	0.95	0.58	170.85	1.03	176.65	0.593	No	No	0.73
936	46.80	234.70	1.71	0.91	0.58	171.09	1.01	172.39	0.556	No	No	0.69
937	46.85	234.70	1.70	0.87	0.57	171.39	1.00	171.39	0.548	No	No	0.68
938	46.90	234.57	1.68	0.83	0.57	171.59	1.00	171.59	0.550	No	No	0.68
939	46.95	233.63	1.67	0.79	0.56	171.17	1.00	171.17	0.546	No	No	0.67
940	47.00	231.40	1.66	0.76	0.56	169.71	1.00	169.71	0.535	No	No	0.66
941	47.05	227.32	1.65	0.73	0.56	166.66	1.00	166.66	0.511	No	No	0.63
942	47.10	221.14	1.66	0.73	0.56	161.73	1.00	161.73	0.473	No	No	0.59
943	47.15	213.26	1.68	0.75	0.57	155.25	1.00	155.25	0.428	No	No	0.53
944	47.20	204.49	1.71	0.79	0.58	147.97	1.02	150.23	4.000	Yes	No	2.00
945	47.25	195.41	1.75	0.83	0.59	140.45	1.08	151.39	4.000	Yes	No	2.00
946	47.30	186.26	1.78	0.89	0.61	132.87	1.13	150.49	4.000	Yes	No	2.00
947	47.35	175.48	1.84	0.99	0.63	123.85	1.19	147.35	4.000	Yes	No	2.00
948	47.40	163.92	1.90	1.13	0.65	114.23	1.24	141.44	4.000	Yes	No	2.00
949	47.45	150.98	1.98	1.33	0.68	103.60	1.29	133.84	4.000	Yes	No	2.00
950	47.50	138.23	2.06	1.57	0.71	93.33	1.37	127.72	4.000	Yes	No	2.00
951	47.55	125.91	2.15	1.86	0.75	83.54	1.50	125.29	4.000	Yes	No	2.00
952	47.60	114.57	2.24	2.22	0.78	74.65	1.71	127.91	4.000	Yes	No	2.00
953	47.65	106.12	2.32	2.62	0.81	68.01	1.99	135.18	4.000	Yes	No	2.00
954	47.70	100.59	2.39	3.07	0.84	63.55	2.30	146.32	4.000	Yes	No	2.00
955	47.75	98.14	2.44	3.48	0.86	61.38	2.57	157.93	4.000	Yes	No	2.00
956	47.80	96.75	2.48	3.91	0.87	59.98	2.84	170.33	4.000	Yes	No	2.00
957	47.85	95.75	2.51	4.26	0.89	58.96	3.02	178.27	4.000	Yes	No	2.00
958	47.90	95.51	2.53	4.54	0.89	58.52	3.52	205.82	4.000	Yes	No	2.00
959	47.95	97.24	2.54	4.64	0.90	59.53	3.58	212.95	4.000	No	No	2.00
960	48.00	100.39	2.53	4.63	0.89	61.57	3.34	205.41	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _t (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
961	48.05	104.45	2.50	4.49	0.88	64.31	2.87	184.56	0.665	No	No	0.83
962	48.10	106.59	2.49	4.35	0.88	65.79	2.89	190.05	0.718	No	No	0.90
963	48.15	106.99	2.48	4.23	0.87	66.10	2.82	186.27	0.681	No	No	0.85
964	48.20	104.22	2.48	4.23	0.88	64.19	2.87	184.38	0.663	No	No	0.83
965	48.25	100.01	2.50	4.31	0.88	61.25	2.88	176.50	0.591	No	No	0.74
966	48.30	93.91	2.54	4.52	0.90	56.98	3.67	208.88	4.000	No	No	2.00
967	48.35	87.69	2.58	4.78	0.91	52.66	4.80	252.71	4.000	No	No	2.00
968	48.40	81.23	2.63	5.14	0.93	48.17	6.61	318.33	3.600	No	No	2.00
969	48.45	76.48	2.68	5.55	0.95	44.84	8.80	394.56	3.600	No	No	2.00
970	48.50	73.37	2.72	5.99	0.96	42.61	4.88	207.76	2.032	No	Yes	2.00
971	48.55	72.59	2.74	6.27	0.97	41.95	5.09	213.46	2.001	No	Yes	2.00
972	48.60	73.49	2.74	6.38	0.97	42.43	5.11	216.91	4.000	Yes	Yes	2.00
973	48.65	76.28	2.72	6.19	0.96	44.22	4.87	215.57	4.000	Yes	Yes	2.00
974	48.70	81.36	2.67	5.82	0.95	47.58	8.69	413.39	4.000	Yes	No	2.00
975	48.75	88.11	2.62	5.26	0.93	52.18	5.96	310.93	4.000	Yes	No	2.00
976	48.80	96.50	2.55	4.67	0.90	57.97	3.80	220.33	4.000	Yes	No	2.00
977	48.85	104.19	2.48	4.08	0.87	63.46	2.82	178.92	4.000	Yes	No	2.00
978	48.90	110.71	2.41	3.59	0.85	68.23	2.45	167.17	4.000	Yes	No	2.00
979	48.95	113.99	2.37	3.22	0.83	70.82	2.22	157.06	4.000	Yes	No	2.00
980	49.00	114.88	2.34	2.99	0.82	71.66	2.09	150.09	4.000	Yes	No	2.00
981	49.05	113.12	2.34	2.91	0.82	70.53	2.08	146.41	0.372	No	No	0.47
982	49.10	110.32	2.35	2.94	0.83	68.53	2.13	145.75	4.000	Yes	No	2.00
983	49.15	106.45	2.38	3.08	0.84	65.67	2.26	148.28	4.000	Yes	No	2.00
984	49.20	102.97	2.41	3.29	0.85	63.02	2.43	153.06	4.000	Yes	No	2.00
985	49.25	99.99	2.45	3.59	0.86	60.66	2.65	160.67	4.000	Yes	No	2.00
986	49.30	98.58	2.48	3.86	0.88	59.41	2.83	168.36	4.000	Yes	No	2.00
987	49.35	98.15	2.50	4.10	0.88	58.85	2.98	175.16	4.000	Yes	No	2.00
988	49.40	98.96	2.50	4.15	0.88	59.27	2.84	168.16	0.522	No	No	0.66
989	49.45	100.29	2.49	4.07	0.88	60.15	2.92	175.55	4.000	Yes	No	2.00
990	49.50	102.24	2.47	3.85	0.87	61.57	2.76	169.89	4.000	Yes	No	2.00
991	49.55	103.75	2.44	3.60	0.86	62.76	2.60	162.96	4.000	Yes	No	2.00
992	49.60	104.70	2.41	3.34	0.85	63.62	2.44	154.97	4.000	Yes	No	2.00
993	49.65	105.55	2.39	3.14	0.84	64.37	2.32	149.05	4.000	Yes	No	2.00
994	49.70	106.91	2.37	3.02	0.84	65.36	2.23	146.04	4.000	Yes	No	2.00
995	49.75	109.29	2.36	2.99	0.83	66.93	2.18	146.21	0.371	No	No	0.47
996	49.80	110.81	2.36	2.97	0.83	67.91	2.15	146.33	0.371	No	No	0.47
997	49.85	110.25	2.35	2.89	0.83	67.58	2.13	143.64	0.356	No	No	0.45
998	49.90	108.66	2.35	2.83	0.83	66.55	2.11	140.65	0.339	No	No	0.43

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q _t :	Total cone resistance
I _c :	Soil behavior type index
Fr:	Normalized friction ratio (%)
n:	Stress exponent
Q _{tn} :	Normalized cone resistance
K _c :	Cone resistance correction factor due to fines
Q _{tn,cs} :	Normalized and adjusted cone resistance
CRR _{7.5} :	Cyclic resistance ratio for M _w =7.5
FS:	Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
0.05	2.00	0.00	0.00	0.05	0.00	0.10	2.00	0.00	0.00	0.05	0.00
0.15	2.00	0.00	0.00	0.05	0.00	0.20	2.00	0.00	0.00	0.05	0.00
0.25	2.00	0.00	0.00	0.05	0.00	0.30	2.00	0.00	0.00	0.05	0.00
0.35	2.00	0.00	0.00	0.05	0.00	0.40	2.00	0.00	0.00	0.05	0.00
0.45	2.00	0.00	0.00	0.05	0.00	0.50	2.00	0.00	0.00	0.05	0.00
0.55	2.00	0.00	0.00	0.05	0.00	0.60	2.00	0.00	0.00	0.05	0.00
0.65	2.00	0.00	0.00	0.05	0.00	0.70	2.00	0.00	0.00	0.05	0.00
0.75	2.00	0.00	0.00	0.05	0.00	0.80	2.00	0.00	0.00	0.05	0.00
0.85	2.00	0.00	0.00	0.05	0.00	0.90	2.00	0.00	0.00	0.05	0.00
0.95	2.00	0.00	0.00	0.05	0.00	1.00	2.00	0.00	0.00	0.05	0.00
1.05	2.00	0.00	0.00	0.05	0.00	1.10	2.00	0.00	0.00	0.05	0.00
1.15	2.00	0.00	0.00	0.05	0.00	1.20	2.00	0.00	0.00	0.05	0.00
1.25	2.00	0.00	0.00	0.05	0.00	1.30	2.00	0.00	0.00	0.05	0.00
1.35	2.00	0.00	0.00	0.05	0.00	1.40	2.00	0.00	0.00	0.05	0.00
1.45	2.00	0.00	0.00	0.05	0.00	1.50	2.00	0.00	0.00	0.05	0.00
1.55	2.00	0.00	0.00	0.05	0.00	1.60	2.00	0.00	0.00	0.05	0.00
1.65	2.00	0.00	0.00	0.05	0.00	1.70	2.00	0.00	0.00	0.05	0.00
1.75	2.00	0.00	0.00	0.05	0.00	1.80	2.00	0.00	0.00	0.05	0.00
1.85	2.00	0.00	0.00	0.05	0.00	1.90	2.00	0.00	0.00	0.05	0.00
1.95	2.00	0.00	0.00	0.05	0.00	2.00	2.00	0.00	0.00	0.05	0.00
2.05	2.00	0.00	0.00	0.05	0.00	2.10	2.00	0.00	0.00	0.05	0.00
2.15	2.00	0.00	0.00	0.05	0.00	2.20	2.00	0.00	0.00	0.05	0.00
2.25	2.00	0.00	0.00	0.05	0.00	2.30	2.00	0.00	0.00	0.05	0.00
2.35	2.00	0.00	0.00	0.05	0.00	2.40	2.00	0.00	0.00	0.05	0.00
2.45	2.00	0.00	0.00	0.05	0.00	2.50	2.00	0.00	0.00	0.05	0.00
2.55	2.00	0.00	0.00	0.05	0.00	2.60	2.00	0.00	0.00	0.05	0.00
2.65	2.00	0.00	0.00	0.05	0.00	2.70	2.00	0.00	0.00	0.05	0.00
2.75	2.00	0.00	0.00	0.05	0.00	2.80	2.00	0.00	0.00	0.05	0.00
2.85	2.00	0.00	0.00	0.05	0.00	2.90	2.00	0.00	0.00	0.05	0.00
2.95	2.00	0.00	0.00	0.05	0.00	3.00	2.00	0.00	0.00	0.05	0.00
3.05	2.00	0.00	0.00	0.05	0.00	3.10	2.00	0.00	0.00	0.05	0.00
3.15	2.00	0.00	0.00	0.05	0.00	3.20	2.00	0.00	0.00	0.05	0.00
3.25	2.00	0.00	0.00	0.05	0.00	3.30	2.00	0.00	0.00	0.05	0.00
3.35	2.00	0.00	0.00	0.05	0.00	3.40	2.00	0.00	0.00	0.05	0.00
3.45	2.00	0.00	0.00	0.05	0.00	3.50	2.00	0.00	0.00	0.05	0.00
3.55	2.00	0.00	0.00	0.05	0.00	3.60	2.00	0.00	0.00	0.05	0.00
3.65	2.00	0.00	0.00	0.05	0.00	3.70	2.00	0.00	0.00	0.05	0.00
3.75	2.00	0.00	0.00	0.05	0.00	3.80	2.00	0.00	0.00	0.05	0.00
3.85	2.00	0.00	0.00	0.05	0.00	3.90	2.00	0.00	0.00	0.05	0.00
3.95	2.00	0.00	0.00	0.05	0.00	4.00	2.00	0.00	0.00	0.05	0.00
4.05	2.00	0.00	0.00	0.05	0.00	4.10	2.00	0.00	0.00	0.05	0.00
4.15	2.00	0.00	0.00	0.05	0.00	4.20	2.00	0.00	0.00	0.05	0.00
4.25	2.00	0.00	0.00	0.05	0.00	4.30	2.00	0.00	0.00	0.05	0.00
4.35	2.00	0.00	0.00	0.05	0.00	4.40	2.00	0.00	0.00	0.05	0.00
4.45	2.00	0.00	0.00	0.05	0.00	4.50	2.00	0.00	0.00	0.05	0.00
4.55	2.00	0.00	0.00	0.05	0.00	4.60	2.00	0.00	0.00	0.05	0.00
4.65	2.00	0.00	0.00	0.05	0.00	4.70	2.00	0.00	0.00	0.05	0.00
4.75	2.00	0.00	0.00	0.05	0.00	4.80	2.00	0.00	0.00	0.05	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
4.85	2.00	0.00	0.00	0.05	0.00	4.90	2.00	0.00	0.00	0.05	0.00
4.95	2.00	0.00	0.00	0.05	0.00	5.00	2.00	0.00	0.00	0.05	0.00
5.05	2.00	0.00	0.00	0.05	0.00	5.10	2.00	0.00	0.00	0.05	0.00
5.15	2.00	0.00	0.00	0.05	0.00	5.20	2.00	0.00	0.00	0.05	0.00
5.25	2.00	0.00	0.00	0.05	0.00	5.30	2.00	0.00	0.00	0.05	0.00
5.35	2.00	0.00	0.00	0.05	0.00	5.40	2.00	0.00	0.00	0.05	0.00
5.45	2.00	0.00	0.00	0.05	0.00	5.50	2.00	0.00	0.00	0.05	0.00
5.55	2.00	0.00	0.00	0.05	0.00	5.60	2.00	0.00	0.00	0.05	0.00
5.65	2.00	0.00	0.00	0.05	0.00	5.70	2.00	0.00	0.00	0.05	0.00
5.75	2.00	0.00	0.00	0.05	0.00	5.80	2.00	0.00	0.00	0.05	0.00
5.85	2.00	0.00	0.00	0.05	0.00	5.90	2.00	0.00	0.00	0.05	0.00
5.95	2.00	0.00	0.00	0.05	0.00	6.00	2.00	0.00	0.00	0.05	0.00
6.05	2.00	0.00	0.00	0.05	0.00	6.10	2.00	0.00	0.00	0.05	0.00
6.15	2.00	0.00	0.00	0.05	0.00	6.20	2.00	0.00	0.00	0.05	0.00
6.25	2.00	0.00	0.00	0.05	0.00	6.30	2.00	0.00	0.00	0.05	0.00
6.35	2.00	0.00	0.00	0.05	0.00	6.40	2.00	0.00	0.00	0.05	0.00
6.45	2.00	0.00	0.00	0.05	0.00	6.50	2.00	0.00	0.00	0.05	0.00
6.55	2.00	0.00	0.00	0.05	0.00	6.60	2.00	0.00	0.00	0.05	0.00
6.65	2.00	0.00	0.00	0.05	0.00	6.70	2.00	0.00	0.00	0.05	0.00
6.75	2.00	0.00	0.00	0.05	0.00	6.80	2.00	0.00	0.00	0.05	0.00
6.85	2.00	0.00	0.00	0.05	0.00	6.90	2.00	0.00	0.00	0.05	0.00
6.95	2.00	0.00	0.00	0.05	0.00	7.00	2.00	0.00	0.00	0.05	0.00
7.05	2.00	0.00	0.00	0.05	0.00	7.10	2.00	0.00	0.00	0.05	0.00
7.15	2.00	0.00	0.00	0.05	0.00	7.20	2.00	0.00	0.00	0.05	0.00
7.25	2.00	0.00	0.00	0.05	0.00	7.30	2.00	0.00	0.00	0.05	0.00
7.35	2.00	0.00	0.00	0.05	0.00	7.40	2.00	0.00	0.00	0.05	0.00
7.45	2.00	0.00	0.00	0.05	0.00	7.50	2.00	0.00	0.00	0.05	0.00
7.55	2.00	0.00	0.00	0.05	0.00	7.60	2.00	0.00	0.00	0.05	0.00
7.65	2.00	0.00	0.00	0.05	0.00	7.70	2.00	0.00	0.00	0.05	0.00
7.75	2.00	0.00	0.00	0.05	0.00	7.80	2.00	0.00	0.00	0.05	0.00
7.85	2.00	0.00	0.00	0.05	0.00	7.90	2.00	0.00	0.00	0.05	0.00
7.95	2.00	0.00	0.00	0.05	0.00	8.00	2.00	0.00	0.00	0.05	0.00
8.05	2.00	0.00	0.00	0.05	0.00	8.10	2.00	0.00	0.00	0.05	0.00
8.15	2.00	0.00	0.00	0.05	0.00	8.20	2.00	0.00	0.00	0.05	0.00
8.25	2.00	0.00	0.00	0.05	0.00	8.30	2.00	0.00	0.00	0.05	0.00
8.35	2.00	0.00	0.00	0.05	0.00	8.40	2.00	0.00	0.00	0.05	0.00
8.45	2.00	0.00	0.00	0.05	0.00	8.50	0.28	0.00	0.00	0.05	0.10
8.55	0.28	0.00	0.00	0.05	0.09	8.60	0.29	0.00	0.00	0.05	0.09
8.65	0.29	0.00	0.00	0.05	0.09	8.70	0.29	0.00	0.00	0.05	0.09
8.75	0.29	0.00	0.00	0.05	0.09	8.80	0.29	0.00	0.00	0.05	0.09
8.85	0.28	0.00	0.00	0.05	0.09	8.90	0.27	0.00	0.00	0.05	0.10
8.95	2.00	0.00	0.00	0.05	0.00	9.00	2.00	0.00	0.00	0.05	0.00
9.05	2.00	0.00	0.00	0.05	0.00	9.10	2.00	0.00	0.00	0.05	0.00
9.15	2.00	0.00	0.00	0.05	0.00	9.20	2.00	0.00	0.00	0.05	0.00
9.25	2.00	0.00	0.00	0.05	0.00	9.30	2.00	0.00	0.00	0.05	0.00
9.35	2.00	0.00	0.00	0.05	0.00	9.40	2.00	0.00	0.00	0.05	0.00
9.45	2.00	0.00	0.00	0.05	0.00	9.50	2.00	0.00	0.00	0.05	0.00
9.55	2.00	0.00	0.00	0.05	0.00	9.60	2.00	0.00	0.00	0.05	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
9.65	2.00	0.00	0.00	0.05	0.00	9.70	2.00	0.00	0.00	0.05	0.00
9.75	2.00	0.00	0.00	0.05	0.00	9.80	2.00	0.00	0.00	0.05	0.00
9.85	2.00	0.00	0.00	0.05	0.00	9.90	2.00	0.00	0.00	0.05	0.00
9.95	2.00	0.00	0.00	0.05	0.00	10.00	2.00	0.00	0.00	0.05	0.00
10.05	2.00	0.00	0.00	0.05	0.00	10.10	2.00	0.00	0.00	0.05	0.00
10.15	2.00	0.00	0.00	0.05	0.00	10.20	2.00	0.00	0.00	0.05	0.00
10.25	2.00	0.00	0.00	0.05	0.00	10.30	2.00	0.00	0.00	0.05	0.00
10.35	0.20	0.80	0.28	0.05	0.10	10.40	0.20	0.80	0.28	0.05	0.10
10.45	0.20	0.80	0.28	0.05	0.10	10.50	0.20	0.80	0.28	0.05	0.10
10.55	0.20	0.80	0.28	0.05	0.10	10.60	0.20	0.80	0.28	0.05	0.10
10.65	0.20	0.80	0.28	0.05	0.10	10.70	0.20	0.80	0.28	0.05	0.10
10.75	0.21	0.79	0.28	0.05	0.10	10.80	0.21	0.79	0.28	0.05	0.10
10.85	0.21	0.79	0.28	0.05	0.10	10.90	0.20	0.80	0.28	0.05	0.10
10.95	0.20	0.80	0.28	0.05	0.10	11.00	0.20	0.80	0.28	0.05	0.10
11.05	0.21	0.79	0.28	0.05	0.10	11.10	0.21	0.79	0.28	0.05	0.10
11.15	0.20	0.80	0.28	0.05	0.10	11.20	0.20	0.80	0.28	0.05	0.10
11.25	0.20	0.80	0.28	0.05	0.10	11.30	0.20	0.80	0.28	0.05	0.10
11.35	0.20	0.80	0.28	0.05	0.10	11.40	0.20	0.80	0.28	0.05	0.10
11.45	0.20	0.80	0.28	0.05	0.10	11.50	2.00	0.00	0.00	0.05	0.00
11.55	2.00	0.00	0.00	0.05	0.00	11.60	2.00	0.00	0.00	0.05	0.00
11.65	2.00	0.00	0.00	0.05	0.00	11.70	2.00	0.00	0.00	0.05	0.00
11.75	2.00	0.00	0.00	0.05	0.00	11.80	2.00	0.00	0.00	0.05	0.00
11.85	2.00	0.00	0.00	0.05	0.00	11.90	2.00	0.00	0.00	0.05	0.00
11.95	2.00	0.00	0.00	0.05	0.00	12.00	0.85	0.00	0.00	0.05	0.02
12.05	2.00	0.00	0.00	0.05	0.00	12.10	2.00	0.00	0.00	0.05	0.00
12.15	2.00	0.00	0.00	0.05	0.00	12.20	2.00	0.00	0.00	0.05	0.00
12.25	2.00	0.00	0.00	0.05	0.00	12.30	2.00	0.00	0.00	0.05	0.00
12.35	2.00	0.00	0.00	0.05	0.00	12.40	0.24	0.76	0.29	0.05	0.09
12.45	2.00	0.00	0.00	0.05	0.00	12.50	2.00	0.00	0.00	0.05	0.00
12.55	2.00	0.00	0.00	0.05	0.00	12.60	2.00	0.00	0.00	0.05	0.00
12.65	2.00	0.00	0.00	0.05	0.00	12.70	2.00	0.00	0.00	0.05	0.00
12.75	2.00	0.00	0.00	0.05	0.00	12.80	2.00	0.00	0.00	0.05	0.00
12.85	2.00	0.00	0.00	0.05	0.00	12.90	2.00	0.00	0.00	0.05	0.00
12.95	2.00	0.00	0.00	0.05	0.00	13.00	1.60	0.00	0.00	0.05	0.00
13.05	1.60	0.00	0.00	0.05	0.00	13.10	1.61	0.00	0.00	0.05	0.00
13.15	1.62	0.00	0.00	0.05	0.00	13.20	1.59	0.00	0.00	0.05	0.00
13.25	1.50	0.00	0.00	0.05	0.00	13.30	1.38	0.00	0.00	0.05	0.00
13.35	1.24	0.00	0.00	0.05	0.00	13.40	1.14	0.00	0.00	0.05	0.00
13.45	1.09	0.00	0.00	0.05	0.00	13.50	1.10	0.00	0.00	0.05	0.00
13.55	1.15	0.00	0.00	0.05	0.00	13.60	1.21	0.00	0.00	0.05	0.00
13.65	1.25	0.00	0.00	0.05	0.00	13.70	1.27	0.00	0.00	0.05	0.00
13.75	1.27	0.00	0.00	0.05	0.00	13.80	1.27	0.00	0.00	0.05	0.00
13.85	1.26	0.00	0.00	0.05	0.00	13.90	1.26	0.00	0.00	0.05	0.00
13.95	1.26	0.00	0.00	0.05	0.00	14.00	1.28	0.00	0.00	0.05	0.00
14.05	1.32	0.00	0.00	0.05	0.00	14.10	1.39	0.00	0.00	0.05	0.00
14.15	1.43	0.00	0.00	0.05	0.00	14.20	1.46	0.00	0.00	0.05	0.00
14.25	1.46	0.00	0.00	0.05	0.00	14.30	1.46	0.00	0.00	0.05	0.00
14.35	1.45	0.00	0.00	0.05	0.00	14.40	1.45	0.00	0.00	0.05	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
14.45	1.45	0.00	0.00	0.05	0.00	14.50	1.45	0.00	0.00	0.05	0.00
14.55	1.46	0.00	0.00	0.05	0.00	14.60	1.50	0.00	0.00	0.05	0.00
14.65	1.54	0.00	0.00	0.05	0.00	14.70	1.58	0.00	0.00	0.05	0.00
14.75	1.60	0.00	0.00	0.05	0.00	14.80	1.60	0.00	0.00	0.05	0.00
14.85	1.58	0.00	0.00	0.05	0.00	14.90	1.54	0.00	0.00	0.05	0.00
14.95	1.47	0.00	0.00	0.05	0.00	15.00	1.41	0.00	0.00	0.05	0.00
15.05	1.34	0.00	0.00	0.05	0.00	15.10	1.28	0.00	0.00	0.05	0.00
15.15	1.22	0.00	0.00	0.05	0.00	15.20	1.17	0.00	0.00	0.05	0.00
15.25	1.15	0.00	0.00	0.05	0.00	15.30	1.15	0.00	0.00	0.05	0.00
15.35	1.14	0.00	0.00	0.05	0.00	15.40	1.14	0.00	0.00	0.05	0.00
15.45	1.14	0.00	0.00	0.05	0.00	15.50	1.13	0.00	0.00	0.05	0.00
15.55	1.13	0.00	0.00	0.05	0.00	15.60	1.13	0.00	0.00	0.05	0.00
15.65	1.12	0.00	0.00	0.05	0.00	15.70	1.14	0.00	0.00	0.05	0.00
15.75	1.19	0.00	0.00	0.05	0.00	15.80	1.30	0.00	0.00	0.05	0.00
15.85	1.45	0.00	0.00	0.05	0.00	15.90	1.65	0.00	0.00	0.05	0.00
15.95	1.83	0.00	0.00	0.05	0.00	16.00	2.00	0.00	0.00	0.05	0.00
16.05	2.00	0.00	0.00	0.05	0.00	16.10	0.95	0.00	0.00	0.05	0.01
16.15	0.91	0.00	0.00	0.05	0.01	16.20	2.00	0.00	0.00	0.05	0.00
16.25	2.00	0.00	0.00	0.05	0.00	16.30	2.00	0.00	0.00	0.05	0.00
16.35	1.93	0.00	0.00	0.05	0.00	16.40	1.83	0.00	0.00	0.05	0.00
16.45	1.75	0.00	0.00	0.05	0.00	16.50	1.71	0.00	0.00	0.05	0.00
16.55	1.69	0.00	0.00	0.05	0.00	16.60	1.68	0.00	0.00	0.05	0.00
16.65	1.67	0.00	0.00	0.05	0.00	16.70	1.65	0.00	0.00	0.05	0.00
16.75	1.62	0.00	0.00	0.05	0.00	16.80	1.59	0.00	0.00	0.05	0.00
16.85	1.54	0.00	0.00	0.05	0.00	16.90	1.48	0.00	0.00	0.05	0.00
16.95	1.44	0.00	0.00	0.05	0.00	17.00	2.00	0.00	0.00	0.05	0.00
17.05	2.00	0.00	0.00	0.05	0.00	17.10	2.00	0.00	0.00	0.05	0.00
17.15	2.00	0.00	0.00	0.05	0.00	17.20	2.00	0.00	0.00	0.05	0.00
17.25	2.00	0.00	0.00	0.05	0.00	17.30	2.00	0.00	0.00	0.05	0.00
17.35	2.00	0.00	0.00	0.05	0.00	17.40	2.00	0.00	0.00	0.05	0.00
17.45	2.00	0.00	0.00	0.05	0.00	17.50	2.00	0.00	0.00	0.05	0.00
17.55	0.24	0.76	0.29	0.05	0.09	17.60	2.00	0.00	0.00	0.05	0.00
17.65	2.00	0.00	0.00	0.05	0.00	17.70	2.00	0.00	0.00	0.05	0.00
17.75	2.00	0.00	0.00	0.05	0.00	17.80	2.00	0.00	0.00	0.05	0.00
17.85	2.00	0.00	0.00	0.05	0.00	17.90	2.00	0.00	0.00	0.05	0.00
17.95	2.00	0.00	0.00	0.05	0.00	18.00	2.00	0.00	0.00	0.05	0.00
18.05	2.00	0.00	0.00	0.05	0.00	18.10	2.00	0.00	0.00	0.05	0.00
18.15	2.00	0.00	0.00	0.05	0.00	18.20	2.00	0.00	0.00	0.05	0.00
18.25	2.00	0.00	0.00	0.05	0.00	18.30	2.00	0.00	0.00	0.05	0.00
18.35	2.00	0.00	0.00	0.05	0.00	18.40	2.00	0.00	0.00	0.05	0.00
18.45	2.00	0.00	0.00	0.05	0.00	18.50	2.00	0.00	0.00	0.05	0.00
18.55	2.00	0.00	0.00	0.05	0.00	18.60	2.00	0.00	0.00	0.05	0.00
18.65	2.00	0.00	0.00	0.05	0.00	18.70	2.00	0.00	0.00	0.05	0.00
18.75	2.00	0.00	0.00	0.05	0.00	18.80	2.00	0.00	0.00	0.05	0.00
18.85	2.00	0.00	0.00	0.05	0.00	18.90	2.00	0.00	0.00	0.05	0.00
18.95	2.00	0.00	0.00	0.05	0.00	19.00	2.00	0.00	0.00	0.05	0.00
19.05	2.00	0.00	0.00	0.05	0.00	19.10	2.00	0.00	0.00	0.05	0.00
19.15	2.00	0.00	0.00	0.05	0.00	19.20	2.00	0.00	0.00	0.05	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
19.25	2.00	0.00	0.00	0.05	0.00	19.30	2.00	0.00	0.00	0.05	0.00
19.35	1.15	0.00	0.00	0.05	0.00	19.40	1.18	0.00	0.00	0.05	0.00
19.45	1.23	0.00	0.00	0.05	0.00	19.50	1.26	0.00	0.00	0.05	0.00
19.55	1.27	0.00	0.00	0.05	0.00	19.60	1.25	0.00	0.00	0.05	0.00
19.65	1.21	0.00	0.00	0.05	0.00	19.70	1.18	0.00	0.00	0.05	0.00
19.75	1.20	0.00	0.00	0.05	0.00	19.80	1.29	0.00	0.00	0.05	0.00
19.85	1.44	0.00	0.00	0.05	0.00	19.90	1.58	0.00	0.00	0.05	0.00
19.95	1.65	0.00	0.00	0.05	0.00	20.00	1.64	0.00	0.00	0.05	0.00
20.05	1.55	0.00	0.00	0.05	0.00	20.10	1.44	0.00	0.00	0.05	0.00
20.15	1.31	0.00	0.00	0.05	0.00	20.20	1.19	0.00	0.00	0.05	0.00
20.25	1.08	0.00	0.00	0.05	0.00	20.30	1.00	0.00	0.00	0.05	0.00
20.35	0.97	0.00	0.00	0.05	0.00	20.40	0.98	0.00	0.00	0.05	0.00
20.45	1.00	0.00	0.00	0.05	0.00	20.50	1.01	0.00	0.00	0.05	0.00
20.55	1.02	0.00	0.00	0.05	0.00	20.60	1.05	0.00	0.00	0.05	0.00
20.65	1.13	0.00	0.00	0.05	0.00	20.70	1.26	0.00	0.00	0.05	0.00
20.75	1.42	0.00	0.00	0.05	0.00	20.80	1.58	0.00	0.00	0.05	0.00
20.85	1.72	0.00	0.00	0.05	0.00	20.90	2.00	0.00	0.00	0.05	0.00
20.95	2.00	0.00	0.00	0.05	0.00	21.00	2.00	0.00	0.00	0.05	0.00
21.05	2.00	0.00	0.00	0.05	0.00	21.10	1.67	0.00	0.00	0.05	0.00
21.15	1.56	0.00	0.00	0.05	0.00	21.20	1.46	0.00	0.00	0.05	0.00
21.25	1.39	0.00	0.00	0.05	0.00	21.30	1.36	0.00	0.00	0.05	0.00
21.35	1.31	0.00	0.00	0.05	0.00	21.40	1.22	0.00	0.00	0.05	0.00
21.45	1.11	0.00	0.00	0.05	0.00	21.50	0.99	0.00	0.00	0.05	0.00
21.55	0.90	0.00	0.00	0.05	0.01	21.60	0.82	0.00	0.00	0.05	0.02
21.65	0.75	0.00	0.00	0.05	0.03	21.70	0.68	0.32	0.85	0.05	0.03
21.75	0.62	0.38	0.68	0.05	0.04	21.80	0.58	0.42	0.59	0.05	0.04
21.85	0.56	0.44	0.56	0.05	0.04	21.90	0.56	0.44	0.55	0.05	0.05
21.95	0.57	0.43	0.58	0.05	0.04	22.00	0.60	0.40	0.63	0.05	0.04
22.05	0.63	0.37	0.70	0.05	0.04	22.10	0.66	0.34	0.78	0.05	0.03
22.15	0.69	0.31	0.89	0.05	0.03	22.20	0.74	0.00	0.00	0.05	0.03
22.25	0.80	0.00	0.00	0.05	0.02	22.30	0.88	0.00	0.00	0.05	0.01
22.35	0.98	0.00	0.00	0.05	0.00	22.40	1.11	0.00	0.00	0.05	0.00
22.45	1.28	0.00	0.00	0.05	0.00	22.50	1.43	0.00	0.00	0.05	0.00
22.55	1.56	0.00	0.00	0.05	0.00	22.60	2.00	0.00	0.00	0.05	0.00
22.65	2.00	0.00	0.00	0.05	0.00	22.70	2.00	0.00	0.00	0.05	0.00
22.75	0.84	0.00	0.00	0.05	0.02	22.80	2.00	0.00	0.00	0.05	0.00
22.85	2.00	0.00	0.00	0.05	0.00	22.90	1.40	0.00	0.00	0.05	0.00
22.95	1.28	0.00	0.00	0.05	0.00	23.00	1.15	0.00	0.00	0.05	0.00
23.05	1.04	0.00	0.00	0.05	0.00	23.10	0.95	0.00	0.00	0.05	0.01
23.15	0.86	0.00	0.00	0.05	0.01	23.20	0.81	0.00	0.00	0.05	0.02
23.25	0.76	0.00	0.00	0.05	0.02	23.30	0.75	0.00	0.00	0.05	0.02
23.35	0.74	0.00	0.00	0.05	0.03	23.40	0.75	0.00	0.00	0.05	0.02
23.45	0.77	0.00	0.00	0.05	0.02	23.50	0.82	0.00	0.00	0.05	0.02
23.55	0.88	0.00	0.00	0.05	0.01	23.60	0.95	0.00	0.00	0.05	0.00
23.65	1.01	0.00	0.00	0.05	0.00	23.70	1.04	0.00	0.00	0.05	0.00
23.75	1.03	0.00	0.00	0.05	0.00	23.80	0.99	0.00	0.00	0.05	0.00
23.85	0.95	0.00	0.00	0.05	0.01	23.90	0.90	0.00	0.00	0.05	0.01
23.95	0.84	0.00	0.00	0.05	0.02	24.00	0.78	0.00	0.00	0.05	0.02

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
24.05	0.74	0.00	0.00	0.05	0.02	24.10	0.72	0.00	0.00	0.05	0.03
24.15	0.72	0.00	0.00	0.05	0.03	24.20	0.75	0.00	0.00	0.05	0.02
24.25	0.81	0.00	0.00	0.05	0.02	24.30	2.00	0.00	0.00	0.05	0.00
24.35	2.00	0.00	0.00	0.05	0.00	24.40	2.00	0.00	0.00	0.05	0.00
24.45	2.00	0.00	0.00	0.05	0.00	24.50	2.00	0.00	0.00	0.05	0.00
24.55	2.00	0.00	0.00	0.05	0.00	24.60	2.00	0.00	0.00	0.05	0.00
24.65	2.00	0.00	0.00	0.05	0.00	24.70	2.00	0.00	0.00	0.05	0.00
24.75	2.00	0.00	0.00	0.05	0.00	24.80	2.00	0.00	0.00	0.05	0.00
24.85	2.00	0.00	0.00	0.05	0.00	24.90	2.00	0.00	0.00	0.05	0.00
24.95	2.00	0.00	0.00	0.05	0.00	25.00	2.00	0.00	0.00	0.05	0.00
25.05	2.00	0.00	0.00	0.05	0.00	25.10	2.00	0.00	0.00	0.05	0.00
25.15	2.00	0.00	0.00	0.05	0.00	25.20	2.00	0.00	0.00	0.05	0.00
25.25	0.23	0.77	0.29	0.05	0.07	25.30	0.23	0.77	0.29	0.05	0.07
25.35	0.23	0.77	0.29	0.05	0.07	25.40	0.24	0.76	0.29	0.05	0.07
25.45	0.24	0.76	0.29	0.05	0.07	25.50	0.24	0.76	0.29	0.05	0.07
25.55	0.24	0.76	0.29	0.05	0.07	25.60	0.24	0.76	0.29	0.05	0.07
25.65	0.24	0.76	0.29	0.05	0.07	25.70	0.24	0.76	0.29	0.05	0.07
25.75	0.25	0.75	0.30	0.05	0.07	25.80	0.25	0.75	0.30	0.05	0.07
25.85	0.26	0.74	0.30	0.05	0.07	25.90	0.28	0.72	0.31	0.05	0.07
25.95	0.29	0.71	0.32	0.05	0.07	26.00	0.28	0.72	0.31	0.05	0.07
26.05	0.27	0.73	0.31	0.05	0.07	26.10	0.25	0.75	0.30	0.05	0.07
26.15	0.25	0.75	0.30	0.05	0.07	26.20	0.25	0.75	0.30	0.05	0.07
26.25	0.25	0.75	0.30	0.05	0.07	26.30	2.00	0.00	0.00	0.05	0.00
26.35	2.00	0.00	0.00	0.05	0.00	26.40	2.00	0.00	0.00	0.05	0.00
26.45	2.00	0.00	0.00	0.05	0.00	26.50	2.00	0.00	0.00	0.05	0.00
26.55	2.00	0.00	0.00	0.05	0.00	26.60	2.00	0.00	0.00	0.05	0.00
26.65	2.00	0.00	0.00	0.05	0.00	26.70	2.00	0.00	0.00	0.05	0.00
26.75	2.00	0.00	0.00	0.05	0.00	26.80	2.00	0.00	0.00	0.05	0.00
26.85	2.00	0.00	0.00	0.05	0.00	26.90	2.00	0.00	0.00	0.05	0.00
26.95	2.00	0.00	0.00	0.05	0.00	27.00	2.00	0.00	0.00	0.05	0.00
27.05	2.00	0.00	0.00	0.05	0.00	27.10	2.00	0.00	0.00	0.05	0.00
27.15	1.83	0.00	0.00	0.05	0.00	27.20	1.82	0.00	0.00	0.05	0.00
27.25	1.80	0.00	0.00	0.05	0.00	27.30	1.78	0.00	0.00	0.05	0.00
27.35	1.77	0.00	0.00	0.05	0.00	27.40	1.78	0.00	0.00	0.05	0.00
27.45	1.80	0.00	0.00	0.05	0.00	27.50	1.82	0.00	0.00	0.05	0.00
27.55	1.81	0.00	0.00	0.05	0.00	27.60	1.78	0.00	0.00	0.05	0.00
27.65	1.73	0.00	0.00	0.05	0.00	27.70	1.71	0.00	0.00	0.05	0.00
27.75	1.73	0.00	0.00	0.05	0.00	27.80	1.80	0.00	0.00	0.05	0.00
27.85	1.88	0.00	0.00	0.05	0.00	27.90	1.98	0.00	0.00	0.05	0.00
27.95	2.00	0.00	0.00	0.05	0.00	28.00	2.00	0.00	0.00	0.05	0.00
28.05	2.00	0.00	0.00	0.05	0.00	28.10	0.83	0.00	0.00	0.05	0.01
28.15	0.75	0.00	0.00	0.05	0.02	28.20	0.85	0.00	0.00	0.05	0.01
28.25	2.00	0.00	0.00	0.05	0.00	28.30	2.00	0.00	0.00	0.05	0.00
28.35	2.00	0.00	0.00	0.05	0.00	28.40	1.59	0.00	0.00	0.05	0.00
28.45	1.56	0.00	0.00	0.05	0.00	28.50	1.54	0.00	0.00	0.05	0.00
28.55	1.52	0.00	0.00	0.05	0.00	28.60	1.50	0.00	0.00	0.05	0.00
28.65	1.49	0.00	0.00	0.05	0.00	28.70	1.50	0.00	0.00	0.05	0.00
28.75	1.49	0.00	0.00	0.05	0.00	28.80	1.42	0.00	0.00	0.05	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
28.85	1.27	0.00	0.00	0.05	0.00	28.90	1.05	0.00	0.00	0.05	0.00
28.95	0.84	0.00	0.00	0.05	0.01	29.00	0.70	0.30	0.93	0.05	0.03
29.05	0.63	0.37	0.70	0.05	0.03	29.10	0.60	0.40	0.64	0.05	0.03
29.15	0.59	0.41	0.61	0.05	0.03	29.20	0.58	0.42	0.60	0.05	0.04
29.25	0.58	0.42	0.60	0.05	0.04	29.30	0.58	0.42	0.59	0.05	0.04
29.35	0.58	0.42	0.59	0.05	0.04	29.40	0.58	0.42	0.59	0.05	0.04
29.45	0.58	0.42	0.59	0.05	0.04	29.50	0.59	0.41	0.61	0.05	0.03
29.55	0.61	0.39	0.65	0.05	0.03	29.60	0.65	0.35	0.74	0.05	0.03
29.65	0.69	0.31	0.86	0.05	0.03	29.70	0.74	0.00	0.00	0.05	0.02
29.75	0.80	0.00	0.00	0.05	0.02	29.80	0.87	0.00	0.00	0.05	0.01
29.85	0.91	0.00	0.00	0.05	0.01	29.90	0.92	0.00	0.00	0.05	0.01
29.95	0.86	0.00	0.00	0.05	0.01	30.00	0.82	0.00	0.00	0.05	0.01
30.05	0.82	0.00	0.00	0.05	0.01	30.10	0.92	0.00	0.00	0.05	0.01
30.15	1.06	0.00	0.00	0.05	0.00	30.20	1.17	0.00	0.00	0.05	0.00
30.25	1.21	0.00	0.00	0.05	0.00	30.30	1.19	0.00	0.00	0.05	0.00
30.35	1.16	0.00	0.00	0.05	0.00	30.40	1.14	0.00	0.00	0.05	0.00
30.45	1.20	0.00	0.00	0.05	0.00	30.50	2.00	0.00	0.00	0.05	0.00
30.55	2.00	0.00	0.00	0.05	0.00	30.60	2.00	0.00	0.00	0.05	0.00
30.65	2.00	0.00	0.00	0.05	0.00	30.70	2.00	0.00	0.00	0.05	0.00
30.75	2.00	0.00	0.00	0.05	0.00	30.80	2.00	0.00	0.00	0.05	0.00
30.85	2.00	0.00	0.00	0.05	0.00	30.90	2.00	0.00	0.00	0.05	0.00
30.95	2.00	0.00	0.00	0.05	0.00	31.00	2.00	0.00	0.00	0.05	0.00
31.05	2.00	0.00	0.00	0.05	0.00	31.10	2.00	0.00	0.00	0.05	0.00
31.15	2.00	0.00	0.00	0.05	0.00	31.20	2.00	0.00	0.00	0.05	0.00
31.25	0.45	0.55	0.43	0.05	0.04	31.30	0.51	0.49	0.49	0.05	0.04
31.35	0.58	0.42	0.59	0.05	0.03	31.40	0.67	0.33	0.79	0.05	0.03
31.45	0.75	0.00	0.00	0.05	0.02	31.50	0.86	0.00	0.00	0.05	0.01
31.55	2.00	0.00	0.00	0.05	0.00	31.60	2.00	0.00	0.00	0.05	0.00
31.65	2.00	0.00	0.00	0.05	0.00	31.70	2.00	0.00	0.00	0.05	0.00
31.75	2.00	0.00	0.00	0.05	0.00	31.80	2.00	0.00	0.00	0.05	0.00
31.85	2.00	0.00	0.00	0.05	0.00	31.90	2.00	0.00	0.00	0.05	0.00
31.95	2.00	0.00	0.00	0.05	0.00	32.00	2.00	0.00	0.00	0.05	0.00
32.05	2.00	0.00	0.00	0.05	0.00	32.10	2.00	0.00	0.00	0.05	0.00
32.15	2.00	0.00	0.00	0.05	0.00	32.20	2.00	0.00	0.00	0.05	0.00
32.25	2.00	0.00	0.00	0.05	0.00	32.30	2.00	0.00	0.00	0.05	0.00
32.35	2.00	0.00	0.00	0.05	0.00	32.40	2.00	0.00	0.00	0.05	0.00
32.45	2.00	0.00	0.00	0.05	0.00	32.50	2.00	0.00	0.00	0.05	0.00
32.55	2.00	0.00	0.00	0.05	0.00	32.60	2.00	0.00	0.00	0.05	0.00
32.65	2.00	0.00	0.00	0.05	0.00	32.70	2.00	0.00	0.00	0.05	0.00
32.75	2.00	0.00	0.00	0.05	0.00	32.80	2.00	0.00	0.00	0.05	0.00
32.85	2.00	0.00	0.00	0.05	0.00	32.90	2.00	0.00	0.00	0.05	0.00
32.95	2.00	0.00	0.00	0.05	0.00	33.00	2.00	0.00	0.00	0.05	0.00
33.05	2.00	0.00	0.00	0.05	0.00	33.10	2.00	0.00	0.00	0.05	0.00
33.15	2.00	0.00	0.00	0.05	0.00	33.20	2.00	0.00	0.00	0.05	0.00
33.25	2.00	0.00	0.00	0.05	0.00	33.30	2.00	0.00	0.00	0.05	0.00
33.35	2.00	0.00	0.00	0.05	0.00	33.40	2.00	0.00	0.00	0.05	0.00
33.45	0.87	0.00	0.00	0.05	0.01	33.50	0.83	0.00	0.00	0.05	0.01
33.55	0.79	0.00	0.00	0.05	0.02	33.60	0.76	0.00	0.00	0.05	0.02

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
33.65	0.75	0.00	0.00	0.05	0.02	33.70	0.73	0.00	0.00	0.05	0.02
33.75	0.73	0.00	0.00	0.05	0.02	33.80	0.72	0.00	0.00	0.05	0.02
33.85	0.71	0.00	0.00	0.05	0.02	33.90	0.71	0.29	0.94	0.05	0.02
33.95	0.69	0.31	0.89	0.05	0.02	34.00	0.67	0.33	0.80	0.05	0.02
34.05	0.64	0.36	0.72	0.05	0.03	34.10	0.61	0.39	0.65	0.05	0.03
34.15	0.59	0.41	0.61	0.05	0.03	34.20	0.58	0.42	0.59	0.05	0.03
34.25	0.57	0.43	0.57	0.05	0.03	34.30	0.56	0.44	0.56	0.05	0.03
34.35	0.57	0.43	0.57	0.05	0.03	34.40	0.57	0.43	0.58	0.05	0.03
34.45	0.59	0.41	0.60	0.05	0.03	34.50	0.60	0.40	0.63	0.05	0.03
34.55	0.62	0.38	0.67	0.05	0.03	34.60	0.64	0.36	0.72	0.05	0.03
34.65	0.66	0.34	0.78	0.05	0.02	34.70	0.68	0.32	0.86	0.05	0.02
34.75	0.71	0.29	0.94	0.05	0.02	34.80	0.73	0.00	0.00	0.05	0.02
34.85	0.75	0.00	0.00	0.05	0.02	34.90	0.77	0.00	0.00	0.05	0.02
34.95	0.78	0.00	0.00	0.05	0.02	35.00	0.79	0.00	0.00	0.05	0.02
35.05	0.78	0.00	0.00	0.05	0.02	35.10	0.77	0.00	0.00	0.05	0.02
35.15	0.77	0.00	0.00	0.05	0.02	35.20	0.76	0.00	0.00	0.05	0.02
35.25	0.76	0.00	0.00	0.05	0.02	35.30	0.76	0.00	0.00	0.05	0.02
35.35	0.76	0.00	0.00	0.05	0.02	35.40	0.77	0.00	0.00	0.05	0.02
35.45	0.77	0.00	0.00	0.05	0.02	35.50	0.78	0.00	0.00	0.05	0.02
35.55	0.79	0.00	0.00	0.05	0.01	35.60	0.80	0.00	0.00	0.05	0.01
35.65	0.81	0.00	0.00	0.05	0.01	35.70	0.82	0.00	0.00	0.05	0.01
35.75	0.84	0.00	0.00	0.05	0.01	35.80	0.85	0.00	0.00	0.05	0.01
35.85	0.87	0.00	0.00	0.05	0.01	35.90	0.88	0.00	0.00	0.05	0.01
35.95	0.89	0.00	0.00	0.05	0.01	36.00	0.90	0.00	0.00	0.05	0.01
36.05	0.89	0.00	0.00	0.05	0.01	36.10	0.87	0.00	0.00	0.05	0.01
36.15	0.84	0.00	0.00	0.05	0.01	36.20	0.81	0.00	0.00	0.05	0.01
36.25	0.77	0.00	0.00	0.05	0.02	36.30	0.74	0.00	0.00	0.05	0.02
36.35	0.71	0.00	0.00	0.05	0.02	36.40	0.66	0.34	0.79	0.05	0.02
36.45	0.61	0.39	0.65	0.05	0.03	36.50	0.54	0.46	0.53	0.05	0.03
36.55	0.49	0.51	0.46	0.05	0.03	36.60	0.45	0.55	0.43	0.05	0.04
36.65	0.44	0.56	0.42	0.05	0.04	36.70	0.45	0.55	0.42	0.05	0.04
36.75	0.46	0.54	0.44	0.05	0.04	36.80	2.00	0.00	0.00	0.05	0.00
36.85	2.00	0.00	0.00	0.05	0.00	36.90	2.00	0.00	0.00	0.05	0.00
36.95	2.00	0.00	0.00	0.05	0.00	37.00	2.00	0.00	0.00	0.05	0.00
37.05	2.00	0.00	0.00	0.05	0.00	37.10	2.00	0.00	0.00	0.05	0.00
37.15	2.00	0.00	0.00	0.05	0.00	37.20	2.00	0.00	0.00	0.05	0.00
37.25	2.00	0.00	0.00	0.05	0.00	37.30	2.00	0.00	0.00	0.05	0.00
37.35	2.00	0.00	0.00	0.05	0.00	37.40	2.00	0.00	0.00	0.05	0.00
37.45	1.19	0.00	0.00	0.05	0.00	37.50	1.13	0.00	0.00	0.05	0.00
37.55	1.08	0.00	0.00	0.05	0.00	37.60	1.03	0.00	0.00	0.05	0.00
37.65	1.00	0.00	0.00	0.05	0.00	37.70	1.07	0.00	0.00	0.05	0.00
37.75	1.22	0.00	0.00	0.05	0.00	37.80	1.41	0.00	0.00	0.05	0.00
37.85	1.51	0.00	0.00	0.05	0.00	37.90	1.57	0.00	0.00	0.05	0.00
37.95	2.00	0.00	0.00	0.05	0.00	38.00	2.00	0.00	0.00	0.05	0.00
38.05	2.00	0.00	0.00	0.05	0.00	38.10	2.00	0.00	0.00	0.05	0.00
38.15	2.00	0.00	0.00	0.05	0.00	38.20	2.00	0.00	0.00	0.05	0.00
38.25	2.00	0.00	0.00	0.05	0.00	38.30	2.00	0.00	0.00	0.05	0.00
38.35	2.00	0.00	0.00	0.05	0.00	38.40	2.00	0.00	0.00	0.05	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
38.45	0.28	0.72	0.31	0.05	0.05	38.50	0.27	0.73	0.31	0.05	0.05
38.55	0.27	0.73	0.31	0.05	0.05	38.60	0.27	0.73	0.31	0.05	0.05
38.65	0.27	0.73	0.31	0.05	0.05	38.70	0.28	0.72	0.31	0.05	0.05
38.75	0.28	0.72	0.31	0.05	0.04	38.80	0.29	0.71	0.32	0.05	0.04
38.85	0.29	0.71	0.32	0.05	0.04	38.90	0.29	0.71	0.31	0.05	0.04
38.95	0.28	0.72	0.31	0.05	0.04	39.00	0.28	0.72	0.31	0.05	0.04
39.05	0.28	0.72	0.31	0.05	0.04	39.10	2.00	0.00	0.00	0.05	0.00
39.15	2.00	0.00	0.00	0.05	0.00	39.20	2.00	0.00	0.00	0.05	0.00
39.25	2.00	0.00	0.00	0.05	0.00	39.30	2.00	0.00	0.00	0.05	0.00
39.35	2.00	0.00	0.00	0.05	0.00	39.40	2.00	0.00	0.00	0.05	0.00
39.45	2.00	0.00	0.00	0.05	0.00	39.50	2.00	0.00	0.00	0.05	0.00
39.55	2.00	0.00	0.00	0.05	0.00	39.60	2.00	0.00	0.00	0.05	0.00
39.65	2.00	0.00	0.00	0.05	0.00	39.70	2.00	0.00	0.00	0.05	0.00
39.75	2.00	0.00	0.00	0.05	0.00	39.80	2.00	0.00	0.00	0.05	0.00
39.85	2.00	0.00	0.00	0.05	0.00	39.90	2.00	0.00	0.00	0.05	0.00
39.95	2.00	0.00	0.00	0.05	0.00	40.00	2.00	0.00	0.00	0.05	0.00
40.05	2.00	0.00	0.00	0.05	0.00	40.10	2.00	0.00	0.00	0.05	0.00
40.15	0.27	0.73	0.31	0.05	0.04	40.20	0.27	0.73	0.31	0.05	0.04
40.25	0.28	0.72	0.31	0.05	0.04	40.30	0.29	0.71	0.32	0.05	0.04
40.35	0.30	0.70	0.32	0.05	0.04	40.40	0.30	0.70	0.32	0.05	0.04
40.45	0.30	0.70	0.32	0.05	0.04	40.50	0.28	0.72	0.31	0.05	0.04
40.55	0.27	0.73	0.31	0.05	0.04	40.60	2.00	0.00	0.00	0.05	0.00
40.65	2.00	0.00	0.00	0.05	0.00	40.70	2.00	0.00	0.00	0.05	0.00
40.75	2.00	0.00	0.00	0.05	0.00	40.80	2.00	0.00	0.00	0.05	0.00
40.85	2.00	0.00	0.00	0.05	0.00	40.90	2.00	0.00	0.00	0.05	0.00
40.95	2.00	0.00	0.00	0.05	0.00	41.00	2.00	0.00	0.00	0.05	0.00
41.05	2.00	0.00	0.00	0.05	0.00	41.10	2.00	0.00	0.00	0.05	0.00
41.15	2.00	0.00	0.00	0.05	0.00	41.20	2.00	0.00	0.00	0.05	0.00
41.25	2.00	0.00	0.00	0.05	0.00	41.30	2.00	0.00	0.00	0.05	0.00
41.35	2.00	0.00	0.00	0.05	0.00	41.40	2.00	0.00	0.00	0.05	0.00
41.45	2.00	0.00	0.00	0.05	0.00	41.50	2.00	0.00	0.00	0.05	0.00
41.55	2.00	0.00	0.00	0.05	0.00	41.60	0.26	0.74	0.30	0.05	0.04
41.65	2.00	0.00	0.00	0.05	0.00	41.70	2.00	0.00	0.00	0.05	0.00
41.75	2.00	0.00	0.00	0.05	0.00	41.80	2.00	0.00	0.00	0.05	0.00
41.85	2.00	0.00	0.00	0.05	0.00	41.90	2.00	0.00	0.00	0.05	0.00
41.95	2.00	0.00	0.00	0.05	0.00	42.00	2.00	0.00	0.00	0.05	0.00
42.05	2.00	0.00	0.00	0.05	0.00	42.10	2.00	0.00	0.00	0.05	0.00
42.15	2.00	0.00	0.00	0.05	0.00	42.20	2.00	0.00	0.00	0.05	0.00
42.25	2.00	0.00	0.00	0.05	0.00	42.30	2.00	0.00	0.00	0.05	0.00
42.35	2.00	0.00	0.00	0.05	0.00	42.40	2.00	0.00	0.00	0.05	0.00
42.45	2.00	0.00	0.00	0.05	0.00	42.50	2.00	0.00	0.00	0.05	0.00
42.55	2.00	0.00	0.00	0.05	0.00	42.60	2.00	0.00	0.00	0.05	0.00
42.65	1.75	0.00	0.00	0.05	0.00	42.70	1.65	0.00	0.00	0.05	0.00
42.75	1.59	0.00	0.00	0.05	0.00	42.80	1.56	0.00	0.00	0.05	0.00
42.85	2.00	0.00	0.00	0.05	0.00	42.90	2.00	0.00	0.00	0.05	0.00
42.95	2.00	0.00	0.00	0.05	0.00	43.00	2.00	0.00	0.00	0.05	0.00
43.05	2.00	0.00	0.00	0.05	0.00	43.10	2.00	0.00	0.00	0.05	0.00
43.15	2.00	0.00	0.00	0.05	0.00	43.20	2.00	0.00	0.00	0.05	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
43.25	2.00	0.00	0.00	0.05	0.00	43.30	0.31	0.69	0.33	0.05	0.04
43.35	2.00	0.00	0.00	0.05	0.00	43.40	2.00	0.00	0.00	0.05	0.00
43.45	2.00	0.00	0.00	0.05	0.00	43.50	2.00	0.00	0.00	0.05	0.00
43.55	2.00	0.00	0.00	0.05	0.00	43.60	2.00	0.00	0.00	0.05	0.00
43.65	2.00	0.00	0.00	0.05	0.00	43.70	2.00	0.00	0.00	0.05	0.00
43.75	2.00	0.00	0.00	0.05	0.00	43.80	2.00	0.00	0.00	0.05	0.00
43.85	2.00	0.00	0.00	0.05	0.00	43.90	2.00	0.00	0.00	0.05	0.00
43.95	2.00	0.00	0.00	0.05	0.00	44.00	2.00	0.00	0.00	0.05	0.00
44.05	2.00	0.00	0.00	0.05	0.00	44.10	2.00	0.00	0.00	0.05	0.00
44.15	2.00	0.00	0.00	0.05	0.00	44.20	2.00	0.00	0.00	0.05	0.00
44.25	2.00	0.00	0.00	0.05	0.00	44.30	2.00	0.00	0.00	0.05	0.00
44.35	2.00	0.00	0.00	0.05	0.00	44.40	0.80	0.00	0.00	0.05	0.01
44.45	0.88	0.00	0.00	0.05	0.01	44.50	0.94	0.00	0.00	0.05	0.00
44.55	0.98	0.00	0.00	0.05	0.00	44.60	2.00	0.00	0.00	0.05	0.00
44.65	2.00	0.00	0.00	0.05	0.00	44.70	2.00	0.00	0.00	0.05	0.00
44.75	2.00	0.00	0.00	0.05	0.00	44.80	2.00	0.00	0.00	0.05	0.00
44.85	2.00	0.00	0.00	0.05	0.00	44.90	2.00	0.00	0.00	0.05	0.00
44.95	2.00	0.00	0.00	0.05	0.00	45.00	2.00	0.00	0.00	0.05	0.00
45.05	2.00	0.00	0.00	0.05	0.00	45.10	0.98	0.00	0.00	0.05	0.00
45.15	0.97	0.00	0.00	0.05	0.00	45.20	0.94	0.00	0.00	0.05	0.00
45.25	0.92	0.00	0.00	0.05	0.00	45.30	0.90	0.00	0.00	0.05	0.00
45.35	0.88	0.00	0.00	0.05	0.01	45.40	0.87	0.00	0.00	0.05	0.01
45.45	0.86	0.00	0.00	0.05	0.01	45.50	0.85	0.00	0.00	0.05	0.01
45.55	0.85	0.00	0.00	0.05	0.01	45.60	0.85	0.00	0.00	0.05	0.01
45.65	0.86	0.00	0.00	0.05	0.01	45.70	0.86	0.00	0.00	0.05	0.01
45.75	0.87	0.00	0.00	0.05	0.01	45.80	0.87	0.00	0.00	0.05	0.01
45.85	0.88	0.00	0.00	0.05	0.01	45.90	0.88	0.00	0.00	0.05	0.01
45.95	0.87	0.00	0.00	0.05	0.01	46.00	0.85	0.00	0.00	0.05	0.01
46.05	0.83	0.00	0.00	0.05	0.01	46.10	0.81	0.00	0.00	0.05	0.01
46.15	0.79	0.00	0.00	0.05	0.01	46.20	0.78	0.00	0.00	0.05	0.01
46.25	0.77	0.00	0.00	0.05	0.01	46.30	0.77	0.00	0.00	0.05	0.01
46.35	0.79	0.00	0.00	0.05	0.01	46.40	0.80	0.00	0.00	0.05	0.01
46.45	0.82	0.00	0.00	0.05	0.01	46.50	0.83	0.00	0.00	0.05	0.01
46.55	0.82	0.00	0.00	0.05	0.01	46.60	0.81	0.00	0.00	0.05	0.01
46.65	0.79	0.00	0.00	0.05	0.01	46.70	0.77	0.00	0.00	0.05	0.01
46.75	0.73	0.00	0.00	0.05	0.01	46.80	0.69	0.31	0.86	0.05	0.01
46.85	0.68	0.32	0.83	0.05	0.01	46.90	0.68	0.32	0.84	0.05	0.01
46.95	0.67	0.33	0.82	0.05	0.01	47.00	0.66	0.34	0.78	0.05	0.01
47.05	0.63	0.37	0.70	0.05	0.02	47.10	0.59	0.41	0.60	0.05	0.02
47.15	0.53	0.47	0.52	0.05	0.02	47.20	2.00	0.00	0.00	0.05	0.00
47.25	2.00	0.00	0.00	0.05	0.00	47.30	2.00	0.00	0.00	0.05	0.00
47.35	2.00	0.00	0.00	0.05	0.00	47.40	2.00	0.00	0.00	0.05	0.00
47.45	2.00	0.00	0.00	0.05	0.00	47.50	2.00	0.00	0.00	0.05	0.00
47.55	2.00	0.00	0.00	0.05	0.00	47.60	2.00	0.00	0.00	0.05	0.00
47.65	2.00	0.00	0.00	0.05	0.00	47.70	2.00	0.00	0.00	0.05	0.00
47.75	2.00	0.00	0.00	0.05	0.00	47.80	2.00	0.00	0.00	0.05	0.00
47.85	2.00	0.00	0.00	0.05	0.00	47.90	2.00	0.00	0.00	0.05	0.00
47.95	2.00	0.00	0.00	0.05	0.00	48.00	2.00	0.00	0.00	0.05	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
48.05	0.83	0.00	0.00	0.05	0.01	48.10	0.90	0.00	0.00	0.05	0.00
48.15	0.85	0.00	0.00	0.05	0.01	48.20	0.83	0.00	0.00	0.05	0.01
48.25	0.74	0.00	0.00	0.05	0.01	48.30	2.00	0.00	0.00	0.05	0.00
48.35	2.00	0.00	0.00	0.05	0.00	48.40	2.00	0.00	0.00	0.05	0.00
48.45	2.00	0.00	0.00	0.05	0.00	48.50	2.00	0.00	0.00	0.05	0.00
48.55	2.00	0.00	0.00	0.05	0.00	48.60	2.00	0.00	0.00	0.05	0.00
48.65	2.00	0.00	0.00	0.05	0.00	48.70	2.00	0.00	0.00	0.05	0.00
48.75	2.00	0.00	0.00	0.05	0.00	48.80	2.00	0.00	0.00	0.05	0.00
48.85	2.00	0.00	0.00	0.05	0.00	48.90	2.00	0.00	0.00	0.05	0.00
48.95	2.00	0.00	0.00	0.05	0.00	49.00	2.00	0.00	0.00	0.05	0.00
49.05	0.47	0.53	0.45	0.05	0.02	49.10	2.00	0.00	0.00	0.05	0.00
49.15	2.00	0.00	0.00	0.05	0.00	49.20	2.00	0.00	0.00	0.05	0.00
49.25	2.00	0.00	0.00	0.05	0.00	49.30	2.00	0.00	0.00	0.05	0.00
49.35	2.00	0.00	0.00	0.05	0.00	49.40	0.66	0.34	0.79	0.05	0.01
49.45	2.00	0.00	0.00	0.05	0.00	49.50	2.00	0.00	0.00	0.05	0.00
49.55	2.00	0.00	0.00	0.05	0.00	49.60	2.00	0.00	0.00	0.05	0.00
49.65	2.00	0.00	0.00	0.05	0.00	49.70	2.00	0.00	0.00	0.05	0.00
49.75	0.47	0.53	0.45	0.05	0.02	49.80	0.47	0.53	0.45	0.05	0.02
49.85	0.45	0.55	0.43	0.05	0.02	49.90	0.43	0.57	0.41	0.05	0.02

Overall liquefaction potential: 9.48

LPI = 0.00 - Liquefaction risk very low

LPI between 0.00 and 5.00 - Liquefaction risk low

LPI between 5.00 and 15.00 - Liquefaction risk high

LPI > 15.00 - Liquefaction risk very high

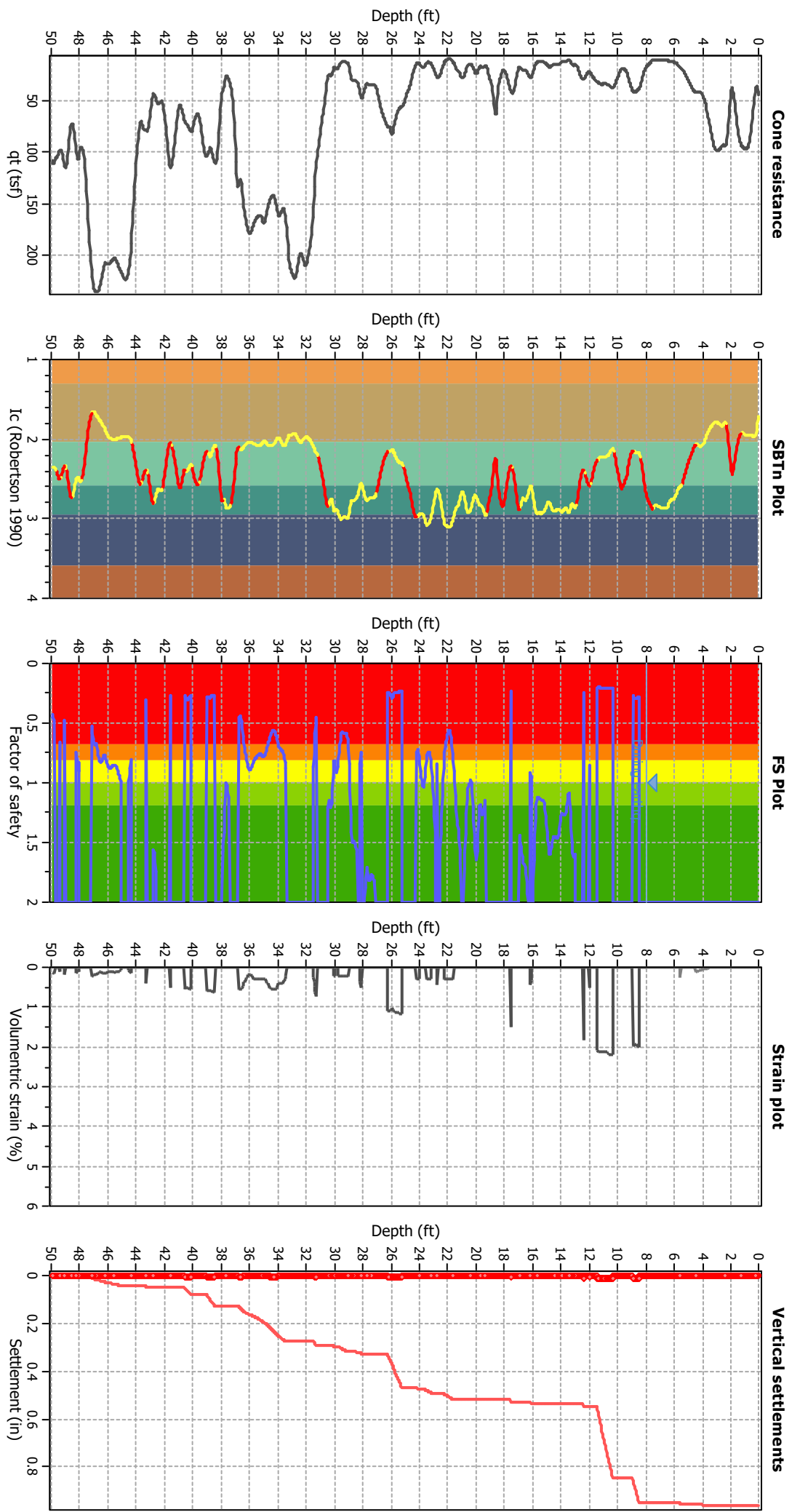
Abbreviations

FS: Calculated factor of safety for test point

F_L: 1 - FSw_z: Function value of the extend of soil liquefaction according to depthd_z: Layer thickness (ft)

LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

- q: Total cone resistance (cone resistance q_c corrected for pore water effects)
- Ic: Soil Behaviour Type Index
- FS: Calculated Factor of Safety against liquefaction
- Volumetric strain: Post-liquefaction volumetric strain

:: Post-earthquake settlement of dry sands ::												
Depth (ft)	Ic	Q _{tn}	Kc	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _r (%)	Settle. (in)
0.05	1.72	85.02	1.00	85.02	16	356	0.59	0.000	0.00	13.69	0.00	0.000
0.10	1.75	79.72	1.00	79.72	15	348	0.59	0.001	0.00	13.69	0.00	0.000
0.15	1.81	72.22	1.00	72.22	14	342	0.59	0.001	0.00	13.69	0.00	0.000
0.20	1.89	69.05	1.23	85.05	17	361	0.59	0.002	0.00	13.69	0.00	0.000
0.25	1.94	70.83	1.26	89.59	18	395	0.59	0.002	0.00	13.69	0.00	0.000
0.30	1.96	78.73	1.28	100.43	21	447	0.59	0.002	0.00	13.69	0.00	0.000
0.35	1.97	89.09	1.28	114.08	23	511	0.59	0.002	0.00	13.69	0.00	0.000
0.40	1.96	101.58	1.28	129.92	27	581	0.59	0.002	0.00	13.69	0.00	0.000
0.45	1.96	113.92	1.28	145.77	30	652	0.59	0.002	0.00	13.69	0.00	0.000
0.50	1.96	127.10	1.28	162.18	33	723	0.59	0.002	0.00	13.69	0.00	0.000
0.55	1.96	139.33	1.27	177.52	36	790	0.59	0.002	0.00	13.69	0.00	0.000
0.60	1.95	151.77	1.27	192.73	39	854	0.59	0.002	0.00	13.69	0.00	0.000
0.65	1.95	162.31	1.27	205.72	42	909	0.59	0.002	0.00	13.69	0.00	0.000
0.70	1.94	170.71	1.27	216.16	44	954	0.59	0.002	0.00	13.69	0.00	0.000
0.75	1.95	176.01	1.27	223.03	45	985	0.59	0.002	0.00	13.69	0.00	0.000
0.80	1.95	179.09	1.27	227.35	46	1006	0.59	0.003	0.00	13.69	0.00	0.000
0.85	1.95	180.77	1.27	229.86	47	1020	0.59	0.003	0.00	13.69	0.00	0.000
0.90	1.95	181.64	1.27	231.27	47	1028	0.59	0.003	0.00	13.69	0.00	0.000
0.95	1.95	182.11	1.27	231.65	47	1028	0.59	0.003	0.00	13.69	0.00	0.000
1.00	1.95	182.16	1.27	231.14	47	1023	0.59	0.003	0.00	13.69	0.00	0.000
1.05	1.94	181.95	1.26	229.78	47	1010	0.59	0.004	0.00	13.69	0.00	0.000
1.10	1.93	181.33	1.26	227.96	46	995	0.59	0.004	0.00	13.69	0.00	0.000
1.15	1.92	180.31	1.25	225.72	46	980	0.59	0.004	0.00	13.69	0.00	0.000
1.20	1.92	178.85	1.25	223.72	45	970	0.59	0.004	0.00	13.69	0.00	0.000
1.25	1.93	176.52	1.25	221.29	45	963	0.59	0.005	0.00	13.69	0.00	0.000
1.30	1.94	173.39	1.26	218.71	0	0	0.59	0.000	0.00	13.69	0.00	0.000
1.35	1.95	168.64	1.27	214.61	0	0	0.59	0.000	0.00	13.69	0.00	0.000
1.40	1.98	163.07	1.29	210.09	0	0	0.59	0.000	0.00	13.69	0.00	0.000
1.45	2.01	156.03	1.31	204.63	0	0	0.59	0.000	0.00	13.69	0.00	0.000
1.50	2.04	147.62	1.35	198.75	0	0	0.59	0.000	0.00	13.69	0.00	0.000
1.55	2.09	137.47	1.40	192.81	0	0	0.59	0.000	0.00	13.69	0.00	0.000
1.60	2.14	125.26	1.49	186.62	0	0	0.59	0.000	0.00	13.69	0.00	0.000
1.65	2.20	112.99	1.62	183.21	0	0	0.59	0.000	0.00	13.69	0.00	0.000
1.70	2.26	100.62	1.80	181.13	0	0	0.59	0.000	0.00	13.69	0.00	0.000
1.75	2.32	90.62	2.02	182.99	0	0	0.59	0.000	0.00	13.69	0.00	0.000
1.80	2.38	81.75	2.26	184.52	0	0	0.59	0.000	0.00	13.69	0.00	0.000
1.85	2.42	75.45	2.48	186.78	0	0	0.59	0.000	0.00	13.69	0.00	0.000
1.90	2.44	71.05	2.61	185.49	0	0	0.59	0.000	0.00	13.69	0.00	0.000
1.95	2.44	71.57	2.57	183.89	0	0	0.59	0.000	0.00	13.69	0.00	0.000
2.00	2.39	77.00	2.32	178.93	0	0	0.59	0.000	0.00	13.69	0.00	0.000
2.05	2.31	89.24	1.97	175.80	0	0	0.59	0.000	0.00	13.69	0.00	0.000
2.10	2.22	104.59	1.65	172.94	0	0	0.59	0.000	0.00	13.69	0.00	0.000
2.15	2.12	122.21	1.44	176.51	0	0	0.59	0.000	0.00	13.69	0.00	0.000
2.20	2.02	139.25	1.32	184.42	0	0	0.59	0.000	0.00	13.69	0.00	0.000
2.25	1.93	154.71	1.26	194.78	0	0	0.59	0.000	0.00	13.69	0.00	0.000
2.30	1.86	167.07	1.21	202.20	0	0	0.59	0.000	0.00	13.69	0.00	0.000
2.35	1.81	174.33	1.17	203.52	0	0	0.59	0.000	0.00	13.69	0.00	0.000
2.40	1.79	177.27	1.14	202.81	0	0	0.59	0.000	0.00	13.69	0.00	0.000

:: Post-earthquake settlement of dry sands :: (continued)												
Depth (ft)	Ic	Q _{tn}	Kc	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _r (%)	Settle. (in)
2.45	1.79	177.15	1.14	202.42	39	815	0.59	0.014	0.01	13.69	0.01	0.000
2.50	1.80	176.26	1.16	203.91	39	824	0.59	0.014	0.01	13.69	0.01	0.000
2.55	1.82	176.03	1.17	206.20	40	837	0.59	0.014	0.01	13.69	0.01	0.000
2.60	1.83	176.52	1.18	208.70	41	852	0.59	0.014	0.01	13.69	0.01	0.000
2.65	1.83	177.97	1.19	211.00	41	863	0.59	0.014	0.01	13.69	0.01	0.000
2.70	1.83	179.65	1.18	212.50	42	867	0.59	0.014	0.01	13.69	0.01	0.000
2.75	1.82	181.51	1.18	213.40	42	868	0.59	0.015	0.01	13.69	0.01	0.000
2.80	1.81	183.10	1.17	213.63	41	866	0.59	0.015	0.01	13.69	0.01	0.000
2.85	1.80	184.47	1.16	213.54	41	863	0.59	0.015	0.01	13.69	0.01	0.000
2.90	1.80	185.51	1.15	213.11	41	859	0.59	0.016	0.01	13.69	0.01	0.000
2.95	1.79	186.06	1.14	212.39	41	855	0.59	0.016	0.01	13.69	0.01	0.000
3.00	1.79	186.02	1.14	211.62	41	851	0.59	0.017	0.01	13.69	0.01	0.000
3.05	1.79	185.17	1.14	210.59	41	847	0.59	0.017	0.01	13.69	0.01	0.000
3.10	1.79	183.64	1.14	209.33	40	842	0.59	0.018	0.01	13.69	0.01	0.000
3.15	1.79	180.70	1.15	207.01	40	834	0.59	0.019	0.01	13.69	0.01	0.000
3.20	1.80	176.66	1.15	203.75	39	822	0.59	0.020	0.01	13.69	0.01	0.000
3.25	1.81	170.66	1.16	198.72	39	805	0.59	0.021	0.01	13.69	0.01	0.000
3.30	1.82	164.12	1.18	193.04	38	785	0.59	0.023	0.01	13.69	0.01	0.000
3.35	1.84	156.75	1.19	186.37	36	763	0.59	0.025	0.01	13.69	0.01	0.000
3.40	1.85	149.65	1.20	179.71	35	742	0.59	0.027	0.01	13.69	0.01	0.000
3.45	1.87	142.59	1.21	172.87	34	720	0.59	0.029	0.02	13.69	0.01	0.000
3.50	1.88	135.86	1.22	166.18	33	699	0.59	0.032	0.02	13.69	0.02	0.000
3.55	1.89	129.79	1.23	160.03	32	680	0.59	0.036	0.02	13.69	0.02	0.000
3.60	1.91	123.69	1.24	153.76	31	661	0.59	0.039	0.02	13.69	0.02	0.000
3.65	1.92	117.77	1.25	147.59	30	642	0.59	0.043	0.03	13.69	0.02	0.000
3.70	1.94	111.46	1.27	141.10	29	622	0.59	0.049	0.03	13.69	0.03	0.000
3.75	1.96	105.71	1.28	135.33	28	606	0.59	0.054	0.04	13.69	0.03	0.000
3.80	1.99	100.65	1.30	130.64	27	595	0.59	0.058	0.04	13.69	0.04	0.000
3.85	2.01	96.25	1.32	126.82	27	586	0.59	0.063	0.04	13.69	0.04	0.000
3.90	2.03	92.41	1.34	123.70	26	579	0.59	0.067	0.05	13.69	0.04	0.000
3.95	2.05	88.73	1.36	120.51	26	569	0.59	0.072	0.05	13.69	0.05	0.000
4.00	2.07	85.64	1.37	117.73	25	559	0.59	0.079	0.06	13.69	0.05	0.000
4.05	2.08	82.84	1.39	115.06	25	548	0.59	0.086	0.07	13.69	0.06	0.000
4.10	2.09	80.72	1.40	113.02	24	540	0.59	0.093	0.07	13.69	0.07	0.000
4.15	2.09	79.25	1.41	111.51	24	534	0.59	0.100	0.08	13.69	0.07	0.000
4.20	2.09	78.56	1.41	110.55	24	529	0.59	0.106	0.09	13.69	0.08	0.000
4.25	2.09	78.34	1.40	109.73	24	524	0.59	0.112	0.09	13.69	0.08	0.000
4.30	2.08	78.33	1.39	108.97	23	520	0.59	0.119	0.10	13.69	0.09	0.001
4.35	2.07	78.32	1.38	108.10	23	514	0.59	0.127	0.11	13.69	0.09	0.001
4.40	2.07	78.32	1.37	107.66	23	511	0.59	0.133	0.11	13.69	0.10	0.001
4.45	2.07	78.31	1.37	107.64	23	511	0.59	0.137	0.12	13.69	0.10	0.001
4.50	2.08	78.19	1.39	108.32	23	516	0.59	0.135	0.11	13.69	0.10	0.001
4.55	2.09	77.84	1.40	109.12	0	0	0.59	0.000	0.00	13.69	0.00	0.000
4.60	2.11	76.91	1.43	109.81	0	0	0.59	0.000	0.00	13.69	0.00	0.000
4.65	2.12	75.44	1.46	110.01	0	0	0.59	0.000	0.00	13.69	0.00	0.000
4.70	2.15	73.27	1.50	109.77	0	0	0.59	0.000	0.00	13.69	0.00	0.000
4.75	2.17	70.89	1.55	109.73	0	0	0.59	0.000	0.00	13.69	0.00	0.000
4.80	2.20	68.19	1.61	109.72	0	0	0.59	0.000	0.00	13.69	0.00	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	Ic	Q _{tn}	Kc	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _r (%)	Settle. (in)
4.85	2.22	65.64	1.68	110.10	0	0	0.59	0.000	0.00	13.69	0.00	0.000
4.90	2.25	62.95	1.75	109.97	0	0	0.59	0.000	0.00	13.69	0.00	0.000
4.95	2.27	60.37	1.82	109.70	0	0	0.59	0.000	0.00	13.69	0.00	0.000
5.00	2.29	57.77	1.90	109.63	0	0	0.59	0.000	0.00	13.69	0.00	0.000
5.05	2.32	55.11	2.00	110.09	0	0	0.59	0.000	0.00	13.69	0.00	0.000
5.10	2.35	52.55	2.13	111.77	0	0	0.59	0.000	0.00	13.69	0.00	0.000
5.15	2.38	49.84	2.28	113.81	0	0	0.59	0.000	0.00	13.69	0.00	0.000
5.20	2.42	47.28	2.47	116.82	0	0	0.59	0.000	0.00	13.69	0.00	0.000
5.25	2.45	44.64	2.68	119.71	0	0	0.59	0.000	0.00	13.69	0.00	0.000
5.30	2.49	42.28	2.91	122.99	0	0	0.59	0.000	0.00	13.69	0.00	0.000
5.35	2.52	40.20	3.13	125.75	0	0	0.59	0.000	0.00	13.69	0.00	0.000
5.40	2.55	38.48	3.33	128.09	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.45	2.57	37.07	3.49	129.39	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.50	2.58	35.71	3.62	129.35	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.55	2.59	34.62	3.70	127.99	35	440	0.59	0.462	0.24	13.69	0.21	0.001
5.60	2.60	33.69	3.73	125.78	34	430	0.59	0.532	0.28	13.69	0.24	0.001
5.65	2.60	32.74	3.76	123.21	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.70	2.61	31.55	3.84	121.30	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.75	2.63	29.86	4.01	119.83	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.80	2.65	28.20	4.24	119.69	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.85	2.68	26.58	4.52	120.03	0	0	0.58	0.000	0.00	0.00	0.00	0.000
5.90	2.71	25.46	4.77	121.40	0	0	0.58	0.000	0.00	0.00	0.00	0.000
5.95	2.73	24.63	4.99	122.89	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.00	2.74	24.26	5.14	124.68	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.05	2.75	24.10	5.23	126.10	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.10	2.75	24.09	5.28	127.28	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.15	2.76	24.09	5.32	128.19	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.20	2.76	24.08	5.37	129.32	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.25	2.77	24.08	5.43	130.87	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.30	2.78	23.93	5.55	132.82	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.35	2.79	23.29	5.76	134.22	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.40	2.82	22.26	6.07	135.09	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.45	2.85	20.91	6.44	134.69	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.50	2.87	20.04	6.71	134.43	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.55	2.87	19.56	6.84	133.80	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.60	2.87	19.54	6.83	133.40	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.65	2.87	19.53	6.78	132.51	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.70	2.87	19.53	6.74	131.64	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.75	2.87	19.52	6.71	130.99	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.80	2.86	19.52	6.69	130.61	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.85	2.86	19.51	6.68	130.37	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.90	2.86	19.51	6.66	129.84	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.95	2.86	19.50	6.61	128.99	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.00	2.85	19.50	6.55	127.77	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.05	2.85	19.49	6.49	126.52	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.10	2.84	19.49	6.42	125.10	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.15	2.84	19.48	6.35	123.66	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.20	2.83	19.47	6.27	122.10	0	0	0.58	0.000	0.00	0.00	0.00	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
7.25	2.83	19.47	6.23	121.28	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.30	2.83	19.46	6.23	121.29	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.35	2.84	19.46	6.32	123.07	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.40	2.85	19.45	6.46	125.77	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.45	2.86	19.45	6.66	129.53	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.50	2.87	19.54	6.82	133.35	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.55	2.88	20.12	6.87	138.23	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.60	2.87	21.20	6.76	143.32	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.65	2.85	22.89	6.50	148.78	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.70	2.83	24.54	6.22	152.62	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.75	2.81	26.12	5.95	155.31	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.80	2.79	27.45	5.71	156.82	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.85	2.77	28.72	5.49	157.70	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.90	2.75	30.07	5.25	157.89	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.95	2.72	31.47	4.96	156.11	0	0	0.58	0.000	0.00	0.00	0.00	0.000

Total estimated settlement: 0.01**Abbreviations**

Q_{tn}: Equivalent clean sand normalized cone resistance
 K_c: Fines correction factor
 Q_{tn,cs}: Post-liquefaction volumetric strain
 G_{max}: Small strain shear modulus
 CSR: Soil cyclic stress ratio
 γ: Cyclic shear strain
 e_{vol(15)}: Volumetric strain after 15 cycles
 N_c: Equivalent number of cycles
 e_v: Volumetric strain
 Settle.: Calculated settlement

:: Post-earthquake settlement due to soil liquefaction ::

Depth (ft)	Q _{tn,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	Q _{tn,cs}	FS	e _v (%)	DF	Settlement (in)
8.00	318.25	2.00	0.00	0.85	0.00	8.05	251.87	2.00	0.00	0.85	0.00
8.10	187.14	2.00	0.00	0.85	0.00	8.15	127.96	2.00	0.00	0.85	0.00
8.20	116.34	2.00	0.00	0.85	0.00	8.25	107.61	2.00	0.00	0.85	0.00
8.30	102.32	2.00	0.00	0.85	0.00	8.35	99.71	2.00	0.00	0.85	0.00
8.40	98.20	2.00	0.00	0.85	0.00	8.45	97.95	2.00	0.00	0.85	0.00
8.50	98.08	0.28	2.01	0.85	0.01	8.55	99.15	0.28	1.99	0.84	0.01
8.60	100.38	0.29	1.97	0.84	0.01	8.65	101.42	0.29	1.95	0.84	0.01
8.70	101.91	0.29	1.94	0.84	0.01	8.75	101.65	0.29	1.94	0.84	0.01
8.80	100.83	0.29	1.95	0.84	0.01	8.85	99.56	0.28	1.97	0.84	0.01
8.90	98.00	0.27	1.99	0.84	0.01	8.95	96.35	2.00	0.00	0.84	0.00
9.00	94.63	2.00	0.00	0.84	0.00	9.05	93.30	2.00	0.00	0.84	0.00
9.10	92.41	2.00	0.00	0.83	0.00	9.15	92.68	2.00	0.00	0.83	0.00
9.20	93.68	2.00	0.00	0.83	0.00	9.25	95.74	2.00	0.00	0.83	0.00
9.30	97.92	2.00	0.00	0.83	0.00	9.35	100.81	2.00	0.00	0.83	0.00
9.40	103.63	2.00	0.00	0.83	0.00	9.45	102.72	2.00	0.00	0.83	0.00
9.50	116.59	2.00	0.00	0.83	0.00	9.55	131.14	2.00	0.00	0.83	0.00
9.60	150.75	2.00	0.00	0.83	0.00	9.65	173.67	2.00	0.00	0.82	0.00
9.70	199.82	2.00	0.00	0.82	0.00	9.75	205.08	2.00	0.00	0.82	0.00
9.80	184.44	2.00	0.00	0.82	0.00	9.85	143.76	2.00	0.00	0.82	0.00
9.90	118.57	2.00	0.00	0.82	0.00	9.95	113.10	2.00	0.00	0.82	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
10.00	108.34	2.00	0.00	0.82	0.00	10.05	102.60	2.00	0.00	0.82	0.00
10.10	96.29	2.00	0.00	0.82	0.00	10.15	90.89	2.00	0.00	0.82	0.00
10.20	86.90	2.00	0.00	0.81	0.00	10.25	84.73	2.00	0.00	0.81	0.00
10.30	83.61	2.00	0.00	0.81	0.00	10.35	83.52	0.20	2.20	0.81	0.01
10.40	83.58	0.20	2.20	0.81	0.01	10.45	83.80	0.20	2.19	0.81	0.01
10.50	83.74	0.20	2.19	0.81	0.01	10.55	83.68	0.20	2.19	0.81	0.01
10.60	83.70	0.20	2.18	0.81	0.01	10.65	84.24	0.20	2.17	0.81	0.01
10.70	84.94	0.20	2.15	0.81	0.01	10.75	85.61	0.21	2.14	0.80	0.01
10.80	85.75	0.21	2.13	0.80	0.01	10.85	85.59	0.21	2.13	0.80	0.01
10.90	85.46	0.20	2.13	0.80	0.01	10.95	85.53	0.20	2.13	0.80	0.01
11.00	85.83	0.20	2.12	0.80	0.01	11.05	86.04	0.21	2.11	0.80	0.01
11.10	86.14	0.21	2.11	0.80	0.01	11.15	86.12	0.20	2.11	0.80	0.01
11.20	86.03	0.20	2.11	0.80	0.01	11.25	85.69	0.20	2.11	0.80	0.01
11.30	85.35	0.20	2.11	0.79	0.01	11.35	85.09	0.20	2.12	0.79	0.01
11.40	85.48	0.20	2.11	0.79	0.01	11.45	86.28	0.20	2.09	0.79	0.01
11.50	87.42	2.00	0.00	0.79	0.00	11.55	88.84	2.00	0.00	0.79	0.00
11.60	90.88	2.00	0.00	0.79	0.00	11.65	94.47	2.00	0.00	0.79	0.00
11.70	99.47	2.00	0.00	0.79	0.00	11.75	106.33	2.00	0.00	0.79	0.00
11.80	113.31	2.00	0.00	0.79	0.00	11.85	123.77	2.00	0.00	0.78	0.00
11.90	149.54	2.00	0.00	0.78	0.00	11.95	171.47	2.00	0.00	0.78	0.00
12.00	177.60	0.85	0.52	0.78	0.00	12.05	171.76	2.00	0.00	0.78	0.00
12.10	150.86	2.00	0.00	0.78	0.00	12.15	127.89	2.00	0.00	0.78	0.00
12.20	113.15	2.00	0.00	0.78	0.00	12.25	108.07	2.00	0.00	0.78	0.00
12.30	103.18	2.00	0.00	0.78	0.00	12.35	100.11	2.00	0.00	0.78	0.00
12.40	98.78	0.24	1.83	0.77	0.01	12.45	100.38	2.00	0.00	0.77	0.00
12.50	103.88	2.00	0.00	0.77	0.00	12.55	109.44	2.00	0.00	0.77	0.00
12.60	115.82	2.00	0.00	0.77	0.00	12.65	138.59	2.00	0.00	0.77	0.00
12.70	188.72	2.00	0.00	0.77	0.00	12.75	258.53	2.00	0.00	0.77	0.00
12.80	144.16	2.00	0.00	0.77	0.00	12.85	150.26	2.00	0.00	0.77	0.00
12.90	156.72	2.00	0.00	0.77	0.00	12.95	161.44	2.00	0.00	0.76	0.00
13.00	164.67	1.60	0.00	0.76	0.00	13.05	164.30	1.60	0.00	0.76	0.00
13.10	161.58	1.61	0.00	0.76	0.00	13.15	155.80	1.62	0.00	0.76	0.00
13.20	148.83	1.59	0.00	0.76	0.00	13.25	140.33	1.50	0.00	0.76	0.00
13.30	132.96	1.38	0.00	0.76	0.00	13.35	127.03	1.24	0.01	0.76	0.00
13.40	125.38	1.14	0.01	0.76	0.00	13.45	125.87	1.09	0.01	0.76	0.00
13.50	128.30	1.10	0.01	0.75	0.00	13.55	129.67	1.15	0.01	0.75	0.00
13.60	130.62	1.21	0.01	0.75	0.00	13.65	131.88	1.25	0.01	0.75	0.00
13.70	134.02	1.27	0.01	0.75	0.00	13.75	137.23	1.27	0.01	0.75	0.00
13.80	140.17	1.27	0.01	0.75	0.00	13.85	143.10	1.26	0.01	0.75	0.00
13.90	145.07	1.26	0.01	0.75	0.00	13.95	146.44	1.26	0.01	0.75	0.00
14.00	147.91	1.28	0.01	0.75	0.00	14.05	150.26	1.32	0.00	0.74	0.00
14.10	154.15	1.39	0.00	0.74	0.00	14.15	157.76	1.43	0.00	0.74	0.00
14.20	160.70	1.46	0.00	0.74	0.00	14.25	162.09	1.46	0.00	0.74	0.00
14.30	163.04	1.46	0.00	0.74	0.00	14.35	164.23	1.45	0.00	0.74	0.00
14.40	165.56	1.45	0.00	0.74	0.00	14.45	166.84	1.45	0.00	0.74	0.00
14.50	167.12	1.45	0.00	0.74	0.00	14.55	166.70	1.46	0.00	0.74	0.00
14.60	164.97	1.50	0.00	0.73	0.00	14.65	162.33	1.54	0.00	0.73	0.00
14.70	157.86	1.58	0.00	0.73	0.00	14.75	152.87	1.60	0.00	0.73	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
14.80	147.29	1.60	0.00	0.73	0.00	14.85	143.03	1.58	0.00	0.73	0.00
14.90	139.63	1.54	0.00	0.73	0.00	14.95	138.05	1.47	0.00	0.73	0.00
15.00	137.39	1.41	0.00	0.73	0.00	15.05	137.54	1.34	0.00	0.73	0.00
15.10	137.68	1.28	0.01	0.73	0.00	15.15	137.69	1.22	0.01	0.72	0.00
15.20	138.23	1.17	0.01	0.72	0.00	15.25	139.24	1.15	0.01	0.72	0.00
15.30	140.66	1.15	0.01	0.72	0.00	15.35	141.51	1.14	0.01	0.72	0.00
15.40	141.77	1.14	0.01	0.72	0.00	15.45	141.40	1.14	0.01	0.72	0.00
15.50	140.68	1.13	0.01	0.72	0.00	15.55	139.96	1.13	0.01	0.72	0.00
15.60	139.74	1.13	0.01	0.72	0.00	15.65	140.72	1.12	0.01	0.72	0.00
15.70	143.21	1.14	0.01	0.71	0.00	15.75	147.57	1.19	0.01	0.71	0.00
15.80	152.19	1.30	0.00	0.71	0.00	15.85	155.79	1.45	0.00	0.71	0.00
15.90	155.78	1.65	0.00	0.71	0.00	15.95	152.88	1.83	0.00	0.71	0.00
16.00	287.84	2.00	0.00	0.71	0.00	16.05	230.14	2.00	0.00	0.71	0.00
16.10	193.04	0.95	0.34	0.71	0.00	16.15	190.00	0.91	0.43	0.71	0.00
16.20	205.80	2.00	0.00	0.71	0.00	16.25	249.72	2.00	0.00	0.70	0.00
16.30	300.82	2.00	0.00	0.70	0.00	16.35	156.06	1.93	0.00	0.70	0.00
16.40	157.09	1.83	0.00	0.70	0.00	16.45	156.58	1.75	0.00	0.70	0.00
16.50	154.24	1.71	0.00	0.70	0.00	16.55	151.09	1.69	0.00	0.70	0.00
16.60	146.75	1.68	0.00	0.70	0.00	16.65	143.79	1.67	0.00	0.70	0.00
16.70	142.92	1.65	0.00	0.70	0.00	16.75	146.19	1.62	0.00	0.70	0.00
16.80	151.48	1.59	0.00	0.69	0.00	16.85	157.61	1.54	0.00	0.69	0.00
16.90	162.84	1.48	0.00	0.69	0.00	16.95	167.87	1.44	0.00	0.69	0.00
17.00	173.02	2.00	0.00	0.69	0.00	17.05	178.20	2.00	0.00	0.69	0.00
17.10	180.48	2.00	0.00	0.69	0.00	17.15	178.86	2.00	0.00	0.69	0.00
17.20	302.90	2.00	0.00	0.69	0.00	17.25	212.64	2.00	0.00	0.69	0.00
17.30	142.93	2.00	0.00	0.69	0.00	17.35	137.35	2.00	0.00	0.68	0.00
17.40	125.31	2.00	0.00	0.68	0.00	17.45	116.29	2.00	0.00	0.68	0.00
17.50	109.76	2.00	0.00	0.68	0.00	17.55	106.20	0.24	1.51	0.68	0.01
17.60	104.64	2.00	0.00	0.68	0.00	17.65	104.82	2.00	0.00	0.68	0.00
17.70	106.95	2.00	0.00	0.68	0.00	17.75	110.79	2.00	0.00	0.68	0.00
17.80	138.27	2.00	0.00	0.68	0.00	17.85	194.05	2.00	0.00	0.68	0.00
17.90	271.55	2.00	0.00	0.67	0.00	17.95	147.07	2.00	0.00	0.67	0.00
18.00	156.72	2.00	0.00	0.67	0.00	18.05	165.66	2.00	0.00	0.67	0.00
18.10	174.92	2.00	0.00	0.67	0.00	18.15	184.70	2.00	0.00	0.67	0.00
18.20	191.41	2.00	0.00	0.67	0.00	18.25	193.29	2.00	0.00	0.67	0.00
18.30	189.63	2.00	0.00	0.67	0.00	18.35	371.95	2.00	0.00	0.67	0.00
18.40	257.94	2.00	0.00	0.67	0.00	18.45	167.93	2.00	0.00	0.66	0.00
18.50	154.80	2.00	0.00	0.66	0.00	18.55	144.47	2.00	0.00	0.66	0.00
18.60	135.05	2.00	0.00	0.66	0.00	18.65	129.45	2.00	0.00	0.66	0.00
18.70	126.61	2.00	0.00	0.66	0.00	18.75	130.06	2.00	0.00	0.66	0.00
18.80	137.72	2.00	0.00	0.66	0.00	18.85	143.86	2.00	0.00	0.66	0.00
18.90	213.50	2.00	0.00	0.66	0.00	18.95	301.17	2.00	0.00	0.66	0.00
19.00	177.24	2.00	0.00	0.65	0.00	19.05	182.64	2.00	0.00	0.65	0.00
19.10	182.82	2.00	0.00	0.65	0.00	19.15	179.10	2.00	0.00	0.65	0.00
19.20	171.95	2.00	0.00	0.65	0.00	19.25	166.15	2.00	0.00	0.65	0.00
19.30	162.06	2.00	0.00	0.65	0.00	19.35	160.46	1.15	0.01	0.65	0.00
19.40	158.45	1.18	0.01	0.65	0.00	19.45	155.02	1.23	0.00	0.65	0.00
19.50	150.66	1.26	0.00	0.65	0.00	19.55	145.22	1.27	0.00	0.64	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
19.60	139.34	1.25	0.00	0.64	0.00	19.65	133.47	1.21	0.00	0.64	0.00
19.70	129.04	1.18	0.01	0.64	0.00	19.75	128.38	1.20	0.01	0.64	0.00
19.80	133.58	1.29	0.00	0.64	0.00	19.85	141.26	1.44	0.00	0.64	0.00
19.90	148.67	1.58	0.00	0.64	0.00	19.95	148.24	1.65	0.00	0.64	0.00
20.00	142.12	1.64	0.00	0.64	0.00	20.05	131.03	1.55	0.00	0.64	0.00
20.10	122.35	1.44	0.00	0.63	0.00	20.15	117.02	1.31	0.00	0.63	0.00
20.20	115.00	1.19	0.01	0.63	0.00	20.25	114.58	1.08	0.01	0.63	0.00
20.30	115.76	1.00	0.01	0.63	0.00	20.35	118.55	0.97	0.01	0.63	0.00
20.40	123.20	0.98	0.01	0.63	0.00	20.45	127.88	1.00	0.01	0.63	0.00
20.50	132.49	1.01	0.01	0.63	0.00	20.55	136.23	1.02	0.01	0.63	0.00
20.60	140.14	1.05	0.01	0.63	0.00	20.65	144.01	1.13	0.01	0.62	0.00
20.70	147.59	1.26	0.00	0.62	0.00	20.75	149.44	1.42	0.00	0.62	0.00
20.80	149.40	1.58	0.00	0.62	0.00	20.85	147.35	1.72	0.00	0.62	0.00
20.90	288.22	2.00	0.00	0.62	0.00	20.95	258.97	2.00	0.00	0.62	0.00
21.00	253.94	2.00	0.00	0.62	0.00	21.05	273.29	2.00	0.00	0.62	0.00
21.10	142.95	1.67	0.00	0.62	0.00	21.15	147.25	1.56	0.00	0.62	0.00
21.20	152.02	1.46	0.00	0.61	0.00	21.25	154.91	1.39	0.00	0.61	0.00
21.30	155.82	1.36	0.00	0.61	0.00	21.35	152.82	1.31	0.00	0.61	0.00
21.40	147.16	1.22	0.00	0.61	0.00	21.45	140.19	1.11	0.01	0.61	0.00
21.50	134.78	0.99	0.01	0.61	0.00	21.55	131.08	0.90	0.01	0.61	0.00
21.60	127.86	0.82	0.30	0.61	0.00	21.65	123.82	0.75	0.30	0.61	0.00
21.70	118.43	0.68	0.30	0.61	0.00	21.75	113.60	0.62	0.30	0.60	0.00
21.80	109.55	0.58	0.30	0.60	0.00	21.85	107.95	0.56	0.30	0.60	0.00
21.90	108.24	0.56	0.30	0.60	0.00	21.95	110.77	0.57	0.30	0.60	0.00
22.00	114.18	0.60	0.30	0.60	0.00	22.05	118.27	0.63	0.30	0.60	0.00
22.10	122.33	0.66	0.30	0.60	0.00	22.15	126.83	0.69	0.30	0.60	0.00
22.20	131.86	0.74	0.30	0.60	0.00	22.25	136.89	0.80	0.30	0.60	0.00
22.30	141.27	0.88	0.01	0.59	0.00	22.35	145.67	0.98	0.01	0.59	0.00
22.40	149.26	1.11	0.01	0.59	0.00	22.45	151.28	1.28	0.00	0.59	0.00
22.50	149.91	1.43	0.00	0.59	0.00	22.55	145.19	1.56	0.00	0.59	0.00
22.60	298.58	2.00	0.00	0.59	0.00	22.65	241.60	2.00	0.00	0.59	0.00
22.70	211.60	2.00	0.00	0.59	0.00	22.75	197.89	0.84	0.44	0.59	0.00
22.80	208.99	2.00	0.00	0.59	0.00	22.85	235.73	2.00	0.00	0.58	0.00
22.90	123.79	1.40	0.00	0.58	0.00	22.95	125.59	1.28	0.00	0.58	0.00
23.00	126.77	1.15	0.01	0.58	0.00	23.05	126.79	1.04	0.01	0.58	0.00
23.10	126.68	0.95	0.01	0.58	0.00	23.15	126.27	0.86	0.01	0.58	0.00
23.20	126.45	0.81	0.29	0.58	0.00	23.25	127.37	0.76	0.29	0.58	0.00
23.30	129.58	0.75	0.29	0.58	0.00	23.35	133.12	0.74	0.29	0.58	0.00
23.40	137.78	0.75	0.29	0.57	0.00	23.45	143.37	0.77	0.29	0.57	0.00
23.50	148.80	0.82	0.29	0.57	0.00	23.55	153.56	0.88	0.01	0.57	0.00
23.60	156.13	0.95	0.01	0.57	0.00	23.65	156.09	1.01	0.01	0.57	0.00
23.70	153.01	1.04	0.01	0.57	0.00	23.75	147.60	1.03	0.01	0.57	0.00
23.80	141.12	0.99	0.01	0.57	0.00	23.85	134.36	0.95	0.01	0.57	0.00
23.90	128.08	0.90	0.01	0.57	0.00	23.95	121.85	0.84	0.01	0.56	0.00
24.00	116.08	0.78	0.28	0.56	0.00	24.05	111.15	0.74	0.28	0.56	0.00
24.10	109.11	0.72	0.28	0.56	0.00	24.15	110.41	0.72	0.28	0.56	0.00
24.20	116.27	0.75	0.28	0.56	0.00	24.25	125.27	0.81	0.28	0.56	0.00
24.30	136.81	2.00	0.00	0.56	0.00	24.35	148.06	2.00	0.00	0.56	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
24.40	157.80	2.00	0.00	0.56	0.00	24.45	163.48	2.00	0.00	0.56	0.00
24.50	166.60	2.00	0.00	0.55	0.00	24.55	166.51	2.00	0.00	0.55	0.00
24.60	165.98	2.00	0.00	0.55	0.00	24.65	337.74	2.00	0.00	0.55	0.00
24.70	285.21	2.00	0.00	0.55	0.00	24.75	245.21	2.00	0.00	0.55	0.00
24.80	210.06	2.00	0.00	0.55	0.00	24.85	177.51	2.00	0.00	0.55	0.00
24.90	144.81	2.00	0.00	0.55	0.00	24.95	135.54	2.00	0.00	0.55	0.00
25.00	129.14	2.00	0.00	0.55	0.00	25.05	123.72	2.00	0.00	0.54	0.00
25.10	118.66	2.00	0.00	0.54	0.00	25.15	114.69	2.00	0.00	0.54	0.00
25.20	111.85	2.00	0.00	0.54	0.00	25.25	110.41	0.23	1.17	0.54	0.01
25.30	110.21	0.23	1.17	0.54	0.01	25.35	110.52	0.23	1.16	0.54	0.01
25.40	111.18	0.24	1.15	0.54	0.01	25.45	111.96	0.24	1.14	0.54	0.01
25.50	112.60	0.24	1.14	0.54	0.01	25.55	112.86	0.24	1.13	0.54	0.01
25.60	112.54	0.24	1.13	0.53	0.01	25.65	112.58	0.24	1.13	0.53	0.01
25.70	113.00	0.24	1.13	0.53	0.01	25.75	114.12	0.25	1.12	0.53	0.01
25.80	115.74	0.25	1.10	0.53	0.01	25.85	118.06	0.26	1.08	0.53	0.01
25.90	121.18	0.28	1.06	0.53	0.01	25.95	123.07	0.29	1.04	0.53	0.01
26.00	122.42	0.28	1.04	0.53	0.01	26.05	119.46	0.27	1.06	0.53	0.01
26.10	115.83	0.25	1.09	0.53	0.01	26.15	114.22	0.25	1.10	0.52	0.01
26.20	113.85	0.25	1.10	0.52	0.01	26.25	114.26	0.25	1.09	0.52	0.01
26.30	114.10	2.00	0.00	0.52	0.00	26.35	113.87	2.00	0.00	0.52	0.00
26.40	113.99	2.00	0.00	0.52	0.00	26.45	115.12	2.00	0.00	0.52	0.00
26.50	117.10	2.00	0.00	0.52	0.00	26.55	120.28	2.00	0.00	0.52	0.00
26.60	123.94	2.00	0.00	0.52	0.00	26.65	128.02	2.00	0.00	0.52	0.00
26.70	133.12	2.00	0.00	0.51	0.00	26.75	138.68	2.00	0.00	0.51	0.00
26.80	145.49	2.00	0.00	0.51	0.00	26.85	155.04	2.00	0.00	0.51	0.00
26.90	195.81	2.00	0.00	0.51	0.00	26.95	244.56	2.00	0.00	0.51	0.00
27.00	297.14	2.00	0.00	0.51	0.00	27.05	348.83	2.00	0.00	0.51	0.00
27.10	168.70	2.00	0.00	0.51	0.00	27.15	170.04	1.83	0.00	0.51	0.00
27.20	170.50	1.82	0.00	0.51	0.00	27.25	170.13	1.80	0.00	0.50	0.00
27.30	169.40	1.78	0.00	0.50	0.00	27.35	169.37	1.77	0.00	0.50	0.00
27.40	170.51	1.78	0.00	0.50	0.00	27.45	172.54	1.80	0.00	0.50	0.00
27.50	174.71	1.82	0.00	0.50	0.00	27.55	176.60	1.81	0.00	0.50	0.00
27.60	177.61	1.78	0.00	0.50	0.00	27.65	178.02	1.73	0.00	0.50	0.00
27.70	178.60	1.71	0.00	0.50	0.00	27.75	179.47	1.73	0.00	0.50	0.00
27.80	179.99	1.80	0.00	0.49	0.00	27.85	179.02	1.88	0.00	0.49	0.00
27.90	176.14	1.98	0.00	0.49	0.00	27.95	327.09	2.00	0.00	0.49	0.00
28.00	265.95	2.00	0.00	0.49	0.00	28.05	221.33	2.00	0.00	0.49	0.00
28.10	192.13	0.83	0.38	0.49	0.00	28.15	184.85	0.75	0.50	0.49	0.00
28.20	193.45	0.85	0.38	0.49	0.00	28.25	223.45	2.00	0.00	0.49	0.00
28.30	264.37	2.00	0.00	0.49	0.00	28.35	310.68	2.00	0.00	0.48	0.00
28.40	146.89	1.59	0.00	0.48	0.00	28.45	148.63	1.56	0.00	0.48	0.00
28.50	150.74	1.54	0.00	0.48	0.00	28.55	152.68	1.52	0.00	0.48	0.00
28.60	154.20	1.50	0.00	0.48	0.00	28.65	155.21	1.49	0.00	0.48	0.00
28.70	155.03	1.50	0.00	0.48	0.00	28.75	153.36	1.49	0.00	0.48	0.00
28.80	148.69	1.42	0.00	0.48	0.00	28.85	141.17	1.27	0.00	0.48	0.00
28.90	130.78	1.05	0.01	0.47	0.00	28.95	119.61	0.84	0.01	0.47	0.00
29.00	110.11	0.70	0.24	0.47	0.00	29.05	103.30	0.63	0.24	0.47	0.00
29.10	98.81	0.60	0.24	0.47	0.00	29.15	94.90	0.59	0.23	0.47	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
29.20	91.97	0.58	0.23	0.47	0.00	29.25	90.19	0.58	0.23	0.47	0.00
29.30	89.95	0.58	0.23	0.47	0.00	29.35	90.96	0.58	0.23	0.47	0.00
29.40	93.04	0.58	0.23	0.47	0.00	29.45	95.44	0.58	0.23	0.46	0.00
29.50	98.49	0.59	0.23	0.46	0.00	29.55	101.95	0.61	0.23	0.46	0.00
29.60	105.65	0.65	0.23	0.46	0.00	29.65	109.24	0.69	0.23	0.46	0.00
29.70	112.82	0.74	0.23	0.46	0.00	29.75	116.36	0.80	0.23	0.46	0.00
29.80	118.68	0.87	0.01	0.46	0.00	29.85	119.18	0.91	0.01	0.46	0.00
29.90	117.81	0.92	0.01	0.46	0.00	29.95	115.07	0.86	0.01	0.46	0.00
30.00	113.32	0.82	0.23	0.45	0.00	30.05	112.87	0.82	0.23	0.45	0.00
30.10	115.01	0.92	0.01	0.45	0.00	30.15	116.84	1.06	0.00	0.45	0.00
30.20	117.94	1.17	0.00	0.45	0.00	30.25	118.75	1.21	0.00	0.45	0.00
30.30	120.72	1.19	0.00	0.45	0.00	30.35	125.41	1.16	0.00	0.45	0.00
30.40	132.98	1.14	0.00	0.45	0.00	30.45	144.96	1.20	0.00	0.45	0.00
30.50	160.00	2.00	0.00	0.45	0.00	30.55	176.16	2.00	0.00	0.44	0.00
30.60	188.27	2.00	0.00	0.44	0.00	30.65	408.80	2.00	0.00	0.44	0.00
30.70	314.00	2.00	0.00	0.44	0.00	30.75	234.60	2.00	0.00	0.44	0.00
30.80	176.64	2.00	0.00	0.44	0.00	30.85	165.44	2.00	0.00	0.44	0.00
30.90	159.58	2.00	0.00	0.44	0.00	30.95	155.17	2.00	0.00	0.44	0.00
31.00	151.92	2.00	0.00	0.44	0.00	31.05	148.44	2.00	0.00	0.44	0.00
31.10	146.17	2.00	0.00	0.43	0.00	31.15	145.53	2.00	0.00	0.43	0.00
31.20	147.45	2.00	0.00	0.43	0.00	31.25	152.11	0.45	0.72	0.43	0.00
31.30	159.36	0.51	0.69	0.43	0.00	31.35	167.81	0.58	0.62	0.43	0.00
31.40	177.11	0.67	0.47	0.43	0.00	31.45	185.77	0.75	0.35	0.43	0.00
31.50	195.20	0.86	0.25	0.43	0.00	31.55	203.54	2.00	0.00	0.43	0.00
31.60	211.85	2.00	0.00	0.43	0.00	31.65	217.88	2.00	0.00	0.42	0.00
31.70	222.79	2.00	0.00	0.42	0.00	31.75	226.20	2.00	0.00	0.42	0.00
31.80	229.14	2.00	0.00	0.42	0.00	31.85	232.22	2.00	0.00	0.42	0.00
31.90	235.46	2.00	0.00	0.42	0.00	31.95	239.04	2.00	0.00	0.42	0.00
32.00	241.32	2.00	0.00	0.42	0.00	32.05	242.36	2.00	0.00	0.42	0.00
32.10	241.44	2.00	0.00	0.42	0.00	32.15	240.15	2.00	0.00	0.42	0.00
32.20	238.41	2.00	0.00	0.41	0.00	32.25	237.31	2.00	0.00	0.41	0.00
32.30	236.38	2.00	0.00	0.41	0.00	32.35	236.18	2.00	0.00	0.41	0.00
32.40	236.04	2.00	0.00	0.41	0.00	32.45	236.75	2.00	0.00	0.41	0.00
32.50	237.65	2.00	0.00	0.41	0.00	32.55	239.27	2.00	0.00	0.41	0.00
32.60	241.11	2.00	0.00	0.41	0.00	32.65	243.31	2.00	0.00	0.41	0.00
32.70	245.52	2.00	0.00	0.41	0.00	32.75	246.83	2.00	0.00	0.40	0.00
32.80	246.97	2.00	0.00	0.40	0.00	32.85	245.74	2.00	0.00	0.40	0.00
32.90	243.89	2.00	0.00	0.40	0.00	32.95	242.03	2.00	0.00	0.40	0.00
33.00	240.19	2.00	0.00	0.40	0.00	33.05	238.17	2.00	0.00	0.40	0.00
33.10	235.40	2.00	0.00	0.40	0.00	33.15	231.84	2.00	0.00	0.40	0.00
33.20	226.98	2.00	0.00	0.40	0.00	33.25	221.31	2.00	0.00	0.40	0.00
33.30	213.96	2.00	0.00	0.39	0.00	33.35	207.08	2.00	0.00	0.39	0.00
33.40	200.33	2.00	0.00	0.39	0.00	33.45	195.86	0.87	0.23	0.39	0.00
33.50	191.82	0.83	0.31	0.39	0.00	33.55	189.00	0.79	0.31	0.39	0.00
33.60	186.21	0.76	0.32	0.39	0.00	33.65	184.71	0.75	0.40	0.39	0.00
33.70	183.45	0.73	0.40	0.39	0.00	33.75	182.75	0.73	0.40	0.39	0.00
33.80	181.82	0.72	0.41	0.39	0.00	33.85	181.31	0.71	0.41	0.38	0.00
33.90	180.58	0.71	0.41	0.38	0.00	33.95	179.34	0.69	0.41	0.38	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
34.00	176.73	0.67	0.42	0.38	0.00	34.05	173.80	0.64	0.52	0.38	0.00
34.10	170.80	0.61	0.53	0.38	0.00	34.15	168.66	0.59	0.54	0.38	0.00
34.20	166.90	0.58	0.55	0.38	0.00	34.25	165.70	0.57	0.55	0.38	0.00
34.30	165.25	0.56	0.55	0.38	0.00	34.35	165.60	0.57	0.55	0.38	0.00
34.40	166.64	0.57	0.54	0.37	0.00	34.45	167.98	0.59	0.53	0.37	0.00
34.50	169.67	0.60	0.53	0.37	0.00	34.55	171.61	0.62	0.52	0.37	0.00
34.60	173.90	0.64	0.50	0.37	0.00	34.65	176.09	0.66	0.41	0.37	0.00
34.70	178.30	0.68	0.40	0.37	0.00	34.75	180.38	0.71	0.39	0.37	0.00
34.80	182.58	0.73	0.38	0.37	0.00	34.85	184.80	0.75	0.30	0.37	0.00
34.90	186.64	0.77	0.30	0.37	0.00	34.95	187.78	0.78	0.30	0.36	0.00
35.00	187.93	0.79	0.29	0.36	0.00	35.05	187.36	0.78	0.29	0.36	0.00
35.10	186.60	0.77	0.30	0.36	0.00	35.15	185.97	0.77	0.30	0.36	0.00
35.20	185.69	0.76	0.30	0.36	0.00	35.25	185.58	0.76	0.30	0.36	0.00
35.30	185.60	0.76	0.30	0.36	0.00	35.35	185.75	0.76	0.29	0.36	0.00
35.40	186.05	0.77	0.29	0.36	0.00	35.45	186.63	0.77	0.29	0.36	0.00
35.50	187.29	0.78	0.29	0.35	0.00	35.55	188.07	0.79	0.29	0.35	0.00
35.60	188.81	0.80	0.28	0.35	0.00	35.65	189.67	0.81	0.28	0.35	0.00
35.70	190.72	0.82	0.28	0.35	0.00	35.75	191.99	0.84	0.27	0.35	0.00
35.80	193.48	0.85	0.21	0.35	0.00	35.85	194.80	0.87	0.20	0.35	0.00
35.90	195.98	0.88	0.20	0.35	0.00	35.95	196.61	0.89	0.20	0.35	0.00
36.00	196.90	0.90	0.20	0.35	0.00	36.05	196.23	0.89	0.20	0.34	0.00
36.10	194.88	0.87	0.20	0.34	0.00	36.15	192.38	0.84	0.27	0.34	0.00
36.20	189.59	0.81	0.27	0.34	0.00	36.25	186.35	0.77	0.28	0.34	0.00
36.30	183.40	0.74	0.35	0.34	0.00	36.35	180.16	0.71	0.36	0.34	0.00
36.40	175.67	0.66	0.37	0.34	0.00	36.45	169.73	0.61	0.48	0.34	0.00
36.50	161.92	0.54	0.53	0.34	0.00	36.55	155.26	0.49	0.55	0.34	0.00
36.60	150.19	0.45	0.56	0.33	0.00	36.65	148.88	0.44	0.56	0.33	0.00
36.70	149.66	0.45	0.56	0.33	0.00	36.75	151.77	0.46	0.55	0.33	0.00
36.80	152.68	2.00	0.00	0.33	0.00	36.85	151.48	2.00	0.00	0.33	0.00
36.90	149.44	2.00	0.00	0.33	0.00	36.95	148.40	2.00	0.00	0.33	0.00
37.00	150.52	2.00	0.00	0.33	0.00	37.05	154.97	2.00	0.00	0.33	0.00
37.10	159.91	2.00	0.00	0.33	0.00	37.15	223.60	2.00	0.00	0.32	0.00
37.20	326.21	2.00	0.00	0.32	0.00	37.25	168.73	2.00	0.00	0.32	0.00
37.30	165.90	2.00	0.00	0.32	0.00	37.35	160.83	2.00	0.00	0.32	0.00
37.40	153.47	2.00	0.00	0.32	0.00	37.45	145.85	1.19	0.00	0.32	0.00
37.50	138.90	1.13	0.00	0.32	0.00	37.55	132.88	1.08	0.00	0.32	0.00
37.60	127.12	1.03	0.00	0.32	0.00	37.65	123.40	1.00	0.00	0.32	0.00
37.70	123.59	1.07	0.00	0.31	0.00	37.75	129.95	1.22	0.00	0.31	0.00
37.80	140.08	1.41	0.00	0.31	0.00	37.85	151.43	1.51	0.00	0.31	0.00
37.90	160.06	1.57	0.00	0.31	0.00	37.95	167.96	2.00	0.00	0.31	0.00
38.00	170.85	2.00	0.00	0.31	0.00	38.05	271.06	2.00	0.00	0.31	0.00
38.10	165.13	2.00	0.00	0.31	0.00	38.15	149.34	2.00	0.00	0.31	0.00
38.20	136.32	2.00	0.00	0.31	0.00	38.25	128.87	2.00	0.00	0.30	0.00
38.30	124.52	2.00	0.00	0.30	0.00	38.35	122.93	2.00	0.00	0.30	0.00
38.40	121.21	2.00	0.00	0.30	0.00	38.45	119.80	0.28	0.61	0.30	0.00
38.50	118.55	0.27	0.61	0.30	0.00	38.55	118.12	0.27	0.61	0.30	0.00
38.60	118.33	0.27	0.61	0.30	0.00	38.65	119.14	0.27	0.60	0.30	0.00
38.70	120.46	0.28	0.59	0.30	0.00	38.75	121.75	0.28	0.59	0.30	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
38.80	122.50	0.29	0.58	0.29	0.00	38.85	122.48	0.29	0.58	0.29	0.00
38.90	121.86	0.29	0.58	0.29	0.00	38.95	121.34	0.28	0.58	0.29	0.00
39.00	121.23	0.28	0.58	0.29	0.00	39.05	121.67	0.28	0.58	0.29	0.00
39.10	122.39	2.00	0.00	0.29	0.00	39.15	123.48	2.00	0.00	0.29	0.00
39.20	125.26	2.00	0.00	0.29	0.00	39.25	128.08	2.00	0.00	0.29	0.00
39.30	132.15	2.00	0.00	0.29	0.00	39.35	136.82	2.00	0.00	0.28	0.00
39.40	142.78	2.00	0.00	0.28	0.00	39.45	148.58	2.00	0.00	0.28	0.00
39.50	150.55	2.00	0.00	0.28	0.00	39.55	180.26	2.00	0.00	0.28	0.00
39.60	205.13	2.00	0.00	0.28	0.00	39.65	209.10	2.00	0.00	0.28	0.00
39.70	199.08	2.00	0.00	0.28	0.00	39.75	178.29	2.00	0.00	0.28	0.00
39.80	161.70	2.00	0.00	0.28	0.00	39.85	147.35	2.00	0.00	0.28	0.00
39.90	144.07	2.00	0.00	0.27	0.00	39.95	136.93	2.00	0.00	0.27	0.00
40.00	127.51	2.00	0.00	0.27	0.00	40.05	120.37	2.00	0.00	0.27	0.00
40.10	117.00	2.00	0.00	0.27	0.00	40.15	117.02	0.27	0.55	0.27	0.00
40.20	118.96	0.27	0.55	0.27	0.00	40.25	121.10	0.28	0.54	0.27	0.00
40.30	123.19	0.29	0.53	0.27	0.00	40.35	124.64	0.30	0.52	0.27	0.00
40.40	124.90	0.30	0.52	0.27	0.00	40.45	123.47	0.30	0.52	0.26	0.00
40.50	120.96	0.28	0.53	0.26	0.00	40.55	117.87	0.27	0.54	0.26	0.00
40.60	116.60	2.00	0.00	0.26	0.00	40.65	117.24	2.00	0.00	0.26	0.00
40.70	121.43	2.00	0.00	0.26	0.00	40.75	126.93	2.00	0.00	0.26	0.00
40.80	146.49	2.00	0.00	0.26	0.00	40.85	178.93	2.00	0.00	0.26	0.00
40.90	208.85	2.00	0.00	0.26	0.00	40.95	214.01	2.00	0.00	0.26	0.00
41.00	199.38	2.00	0.00	0.25	0.00	41.05	159.89	2.00	0.00	0.25	0.00
41.10	133.14	2.00	0.00	0.25	0.00	41.15	126.96	2.00	0.00	0.25	0.00
41.20	121.83	2.00	0.00	0.25	0.00	41.25	117.94	2.00	0.00	0.25	0.00
41.30	115.56	2.00	0.00	0.25	0.00	41.35	114.48	2.00	0.00	0.25	0.00
41.40	114.35	2.00	0.00	0.25	0.00	41.45	115.04	2.00	0.00	0.25	0.00
41.50	116.12	2.00	0.00	0.25	0.00	41.55	116.49	2.00	0.00	0.24	0.00
41.60	115.88	0.26	0.50	0.24	0.00	41.65	113.19	2.00	0.00	0.24	0.00
41.70	109.84	2.00	0.00	0.24	0.00	41.75	105.98	2.00	0.00	0.24	0.00
41.80	104.54	2.00	0.00	0.24	0.00	41.85	105.82	2.00	0.00	0.24	0.00
41.90	110.70	2.00	0.00	0.24	0.00	41.95	116.29	2.00	0.00	0.24	0.00
42.00	121.84	2.00	0.00	0.24	0.00	42.05	133.15	2.00	0.00	0.24	0.00
42.10	178.38	2.00	0.00	0.23	0.00	42.15	220.45	2.00	0.00	0.23	0.00
42.20	252.86	2.00	0.00	0.23	0.00	42.25	259.02	2.00	0.00	0.23	0.00
42.30	254.21	2.00	0.00	0.23	0.00	42.35	240.47	2.00	0.00	0.23	0.00
42.40	231.68	2.00	0.00	0.23	0.00	42.45	229.32	2.00	0.00	0.23	0.00
42.50	241.94	2.00	0.00	0.23	0.00	42.55	264.67	2.00	0.00	0.23	0.00
42.60	304.96	2.00	0.00	0.23	0.00	42.65	152.45	1.75	0.00	0.22	0.00
42.70	156.77	1.65	0.00	0.22	0.00	42.75	161.19	1.59	0.00	0.22	0.00
42.80	165.81	1.56	0.00	0.22	0.00	42.85	169.89	2.00	0.00	0.22	0.00
42.90	172.70	2.00	0.00	0.22	0.00	42.95	172.48	2.00	0.00	0.22	0.00
43.00	310.57	2.00	0.00	0.22	0.00	43.05	224.15	2.00	0.00	0.22	0.00
43.10	162.30	2.00	0.00	0.22	0.00	43.15	143.28	2.00	0.00	0.22	0.00
43.20	134.57	2.00	0.00	0.21	0.00	43.25	128.17	2.00	0.00	0.21	0.00
43.30	124.94	0.31	0.41	0.21	0.00	43.35	125.89	2.00	0.00	0.21	0.00
43.40	130.11	2.00	0.00	0.21	0.00	43.45	136.32	2.00	0.00	0.21	0.00
43.50	142.81	2.00	0.00	0.21	0.00	43.55	149.15	2.00	0.00	0.21	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
43.60	168.61	2.00	0.00	0.21	0.00	43.65	199.07	2.00	0.00	0.21	0.00
43.70	213.05	2.00	0.00	0.21	0.00	43.75	210.98	2.00	0.00	0.20	0.00
43.80	185.82	2.00	0.00	0.20	0.00	43.85	170.73	2.00	0.00	0.20	0.00
43.90	166.08	2.00	0.00	0.20	0.00	43.95	161.46	2.00	0.00	0.20	0.00
44.00	157.27	2.00	0.00	0.20	0.00	44.05	155.83	2.00	0.00	0.20	0.00
44.10	156.49	2.00	0.00	0.20	0.00	44.15	158.95	2.00	0.00	0.20	0.00
44.20	162.31	2.00	0.00	0.20	0.00	44.25	166.68	2.00	0.00	0.20	0.00
44.30	172.03	2.00	0.00	0.19	0.00	44.35	178.61	2.00	0.00	0.19	0.00
44.40	185.16	0.80	0.16	0.19	0.00	44.45	191.06	0.88	0.12	0.19	0.00
44.50	195.82	0.94	0.11	0.19	0.00	44.55	199.50	0.98	0.09	0.19	0.00
44.60	202.56	2.00	0.00	0.19	0.00	44.65	204.64	2.00	0.00	0.19	0.00
44.70	206.15	2.00	0.00	0.19	0.00	44.75	206.62	2.00	0.00	0.19	0.00
44.80	206.50	2.00	0.00	0.19	0.00	44.85	205.63	2.00	0.00	0.18	0.00
44.90	204.47	2.00	0.00	0.18	0.00	44.95	203.00	2.00	0.00	0.18	0.00
45.00	201.57	2.00	0.00	0.18	0.00	45.05	200.21	2.00	0.00	0.18	0.00
45.10	198.92	0.98	0.08	0.18	0.00	45.15	197.59	0.97	0.08	0.18	0.00
45.20	195.99	0.94	0.10	0.18	0.00	45.25	194.28	0.92	0.10	0.18	0.00
45.30	192.46	0.90	0.10	0.18	0.00	45.35	190.94	0.88	0.11	0.18	0.00
45.40	189.71	0.87	0.11	0.17	0.00	45.45	188.79	0.86	0.11	0.17	0.00
45.50	188.21	0.85	0.11	0.17	0.00	45.55	187.99	0.85	0.14	0.17	0.00
45.60	188.19	0.85	0.11	0.17	0.00	45.65	188.55	0.86	0.10	0.17	0.00
45.70	189.00	0.86	0.10	0.17	0.00	45.75	189.43	0.87	0.10	0.17	0.00
45.80	189.91	0.87	0.10	0.17	0.00	45.85	190.12	0.88	0.10	0.17	0.00
45.90	189.95	0.88	0.10	0.17	0.00	45.95	189.18	0.87	0.10	0.16	0.00
46.00	188.06	0.85	0.10	0.16	0.00	46.05	186.44	0.83	0.13	0.16	0.00
46.10	184.66	0.81	0.13	0.16	0.00	46.15	182.64	0.79	0.14	0.16	0.00
46.20	181.28	0.78	0.14	0.16	0.00	46.25	180.46	0.77	0.14	0.16	0.00
46.30	180.98	0.77	0.14	0.16	0.00	46.35	181.99	0.79	0.13	0.16	0.00
46.40	183.58	0.80	0.13	0.16	0.00	46.45	184.76	0.82	0.13	0.16	0.00
46.50	185.42	0.83	0.13	0.15	0.00	46.55	185.18	0.82	0.13	0.15	0.00
46.60	184.06	0.81	0.13	0.15	0.00	46.65	182.33	0.79	0.13	0.15	0.00
46.70	179.97	0.77	0.13	0.15	0.00	46.75	176.65	0.73	0.16	0.15	0.00
46.80	172.39	0.69	0.17	0.15	0.00	46.85	171.39	0.68	0.17	0.15	0.00
46.90	171.59	0.68	0.17	0.15	0.00	46.95	171.17	0.67	0.17	0.15	0.00
47.00	169.71	0.66	0.17	0.15	0.00	47.05	166.66	0.63	0.21	0.14	0.00
47.10	161.73	0.59	0.22	0.14	0.00	47.15	155.25	0.53	0.23	0.14	0.00
47.20	150.23	2.00	0.00	0.14	0.00	47.25	151.39	2.00	0.00	0.14	0.00
47.30	150.49	2.00	0.00	0.14	0.00	47.35	147.35	2.00	0.00	0.14	0.00
47.40	141.44	2.00	0.00	0.14	0.00	47.45	133.84	2.00	0.00	0.14	0.00
47.50	127.72	2.00	0.00	0.14	0.00	47.55	125.29	2.00	0.00	0.14	0.00
47.60	127.91	2.00	0.00	0.13	0.00	47.65	135.18	2.00	0.00	0.13	0.00
47.70	146.32	2.00	0.00	0.13	0.00	47.75	157.93	2.00	0.00	0.13	0.00
47.80	170.33	2.00	0.00	0.13	0.00	47.85	178.27	2.00	0.00	0.13	0.00
47.90	205.82	2.00	0.00	0.13	0.00	47.95	212.95	2.00	0.00	0.13	0.00
48.00	205.41	2.00	0.00	0.13	0.00	48.05	184.56	0.83	0.10	0.13	0.00
48.10	190.05	0.90	0.08	0.13	0.00	48.15	186.27	0.85	0.08	0.12	0.00
48.20	184.38	0.83	0.10	0.12	0.00	48.25	176.50	0.74	0.13	0.12	0.00
48.30	208.88	2.00	0.00	0.12	0.00	48.35	252.71	2.00	0.00	0.12	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
48.40	318.33	2.00	0.00	0.12	0.00	48.45	394.56	2.00	0.00	0.12	0.00
48.50	207.76	2.00	0.00	0.12	0.00	48.55	213.46	2.00	0.00	0.12	0.00
48.60	216.91	2.00	0.00	0.12	0.00	48.65	215.57	2.00	0.00	0.12	0.00
48.70	413.39	2.00	0.00	0.11	0.00	48.75	310.93	2.00	0.00	0.11	0.00
48.80	220.33	2.00	0.00	0.11	0.00	48.85	178.92	2.00	0.00	0.11	0.00
48.90	167.17	2.00	0.00	0.11	0.00	48.95	157.06	2.00	0.00	0.11	0.00
49.00	150.09	2.00	0.00	0.11	0.00	49.05	146.41	0.47	0.18	0.11	0.00
49.10	145.75	2.00	0.00	0.11	0.00	49.15	148.28	2.00	0.00	0.11	0.00
49.20	153.06	2.00	0.00	0.11	0.00	49.25	160.67	2.00	0.00	0.10	0.00
49.30	168.36	2.00	0.00	0.10	0.00	49.35	175.16	2.00	0.00	0.10	0.00
49.40	168.16	0.66	0.12	0.10	0.00	49.45	175.55	2.00	0.00	0.10	0.00
49.50	169.89	2.00	0.00	0.10	0.00	49.55	162.96	2.00	0.00	0.10	0.00
49.60	154.97	2.00	0.00	0.10	0.00	49.65	149.05	2.00	0.00	0.10	0.00
49.70	146.04	2.00	0.00	0.10	0.00	49.75	146.21	0.47	0.16	0.10	0.00
49.80	146.33	0.47	0.16	0.09	0.00	49.85	143.64	0.45	0.16	0.09	0.00
49.90	140.65	0.43	0.16	0.09	0.00						

Total estimated settlement: 0.95**Abbreviations**

$Q_{tn,cs}$:	Equivalent clean sand normalized cone resistance
FS:	Factor of safety against liquefaction
e_v (%):	Post-liquefaction volumetric strain
DF:	e_v depth weighting factor
Settlement:	Calculated settlement

:: Strength loss calculation (Robertson (2009)) ::

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.05	44.98	85.02	1.00	85.02	1.72	0.72	0.72
0.10	42.18	79.72	1.00	79.72	1.75	0.57	0.71
0.15	38.22	72.22	1.00	72.22	1.81	0.31	0.69
0.20	36.54	69.05	1.23	85.05	1.89	0.72	0.72
0.25	37.48	70.83	1.26	89.59	1.94	0.73	0.73
0.30	41.67	78.73	1.28	100.43	1.96	0.75	0.75
0.35	47.15	89.09	1.28	114.08	1.97	0.77	0.77
0.40	53.76	101.58	1.28	129.92	1.96	0.80	0.80
0.45	60.29	113.92	1.28	145.77	1.96	0.82	0.82
0.50	67.27	127.10	1.28	162.18	1.96	0.84	0.84
0.55	73.74	139.33	1.27	177.52	1.96	0.86	0.86
0.60	80.33	151.77	1.27	192.73	1.95	0.88	0.88
0.65	85.91	162.31	1.27	205.72	1.95	0.89	0.89
0.70	90.35	170.71	1.27	216.16	1.94	0.90	0.90
0.75	93.16	176.01	1.27	223.03	1.95	0.91	0.91
0.80	94.80	179.09	1.27	227.35	1.95	0.91	0.91
0.85	95.69	180.77	1.27	229.86	1.95	0.92	0.92
0.90	96.15	181.64	1.27	231.27	1.95	0.92	0.92
0.95	96.40	182.11	1.27	231.65	1.95	0.92	0.92
1.00	96.43	182.16	1.27	231.14	1.95	0.92	0.92
1.05	96.33	181.95	1.26	229.78	1.94	0.92	0.92
1.10	96.00	181.33	1.26	227.96	1.93	0.92	0.92
1.15	95.46	180.31	1.25	225.72	1.92	0.91	0.91
1.20	94.69	178.85	1.25	223.72	1.92	0.91	0.91
1.25	93.46	176.52	1.25	221.29	1.93	0.91	0.91
1.30	91.81	173.39	1.26	218.71	1.94	0.91	0.91
1.35	89.30	168.64	1.27	214.61	1.95	0.90	0.90
1.40	86.36	163.07	1.29	210.09	1.98	0.90	0.90
1.45	82.64	156.03	1.31	204.63	2.01	0.89	0.89
1.50	78.19	147.62	1.35	198.75	2.04	0.89	0.89
1.55	72.82	137.47	1.40	192.81	2.09	0.88	0.88
1.60	66.36	125.26	1.49	186.62	2.14	0.87	0.87
1.65	59.88	112.99	1.62	183.21	2.20	0.87	0.87
1.70	53.34	100.62	1.80	181.13	2.26	0.87	0.87
1.75	48.05	90.62	2.02	182.99	2.32	0.87	0.87
1.80	43.36	81.75	2.26	184.52	2.38	0.87	0.87
1.85	40.03	75.45	2.48	186.78	2.42	0.87	0.87
1.90	37.71	71.05	2.61	185.49	2.44	0.87	0.87
1.95	37.98	71.57	2.57	183.89	2.44	0.87	0.87
2.00	40.86	77.00	2.32	178.93	2.39	0.86	0.86
2.05	47.34	89.24	1.97	175.80	2.31	0.86	0.86
2.10	55.46	104.59	1.65	172.94	2.22	0.86	0.86
2.15	64.79	122.21	1.44	176.51	2.12	0.86	0.86
2.20	73.80	139.25	1.32	184.42	2.02	0.87	0.87
2.25	81.99	154.71	1.26	194.78	1.93	0.88	0.88
2.30	88.53	167.07	1.21	202.20	1.86	0.89	0.89
2.35	92.37	174.33	1.17	203.52	1.81	0.89	0.89
2.40	93.93	177.27	1.14	202.81	1.79	0.89	0.89

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
2.45	93.87	177.15	1.14	202.42	1.79	0.89	0.89
2.50	93.40	176.26	1.16	203.91	1.80	0.89	0.89
2.55	93.28	176.03	1.17	206.20	1.82	0.89	0.89
2.60	93.55	176.52	1.18	208.70	1.83	0.90	0.90
2.65	94.32	177.97	1.19	211.00	1.83	0.90	0.90
2.70	95.21	179.65	1.18	212.50	1.83	0.90	0.90
2.75	96.20	181.51	1.18	213.40	1.82	0.90	0.90
2.80	97.04	183.10	1.17	213.63	1.81	0.90	0.90
2.85	97.77	184.47	1.16	213.54	1.80	0.90	0.90
2.90	98.32	185.51	1.15	213.11	1.80	0.90	0.90
2.95	98.61	186.06	1.14	212.39	1.79	0.90	0.90
3.00	98.60	186.02	1.14	211.62	1.79	0.90	0.90
3.05	98.15	185.17	1.14	210.59	1.79	0.90	0.90
3.10	97.34	183.64	1.14	209.33	1.79	0.90	0.90
3.15	95.79	180.70	1.15	207.01	1.79	0.89	0.89
3.20	93.66	176.66	1.15	203.75	1.80	0.89	0.89
3.25	90.49	170.66	1.16	198.72	1.81	0.89	0.89
3.30	87.03	164.12	1.18	193.04	1.82	0.88	0.88
3.35	83.13	156.75	1.19	186.37	1.84	0.87	0.87
3.40	79.38	149.65	1.20	179.71	1.85	0.86	0.86
3.45	75.65	142.59	1.21	172.87	1.87	0.86	0.86
3.50	72.09	135.86	1.22	166.18	1.88	0.85	0.85
3.55	68.88	129.79	1.23	160.03	1.89	0.84	0.84
3.60	65.66	123.69	1.24	153.76	1.91	0.83	0.83
3.65	62.53	117.77	1.25	147.59	1.92	0.82	0.82
3.70	59.19	111.46	1.27	141.10	1.94	0.81	0.81
3.75	56.15	105.71	1.28	135.33	1.96	0.81	0.81
3.80	53.48	100.65	1.30	130.64	1.99	0.80	0.80
3.85	51.15	96.25	1.32	126.82	2.01	0.79	0.79
3.90	49.13	92.41	1.34	123.70	2.03	0.79	0.79
3.95	47.18	88.73	1.36	120.51	2.05	0.78	0.78
4.00	45.55	85.64	1.37	117.73	2.07	0.78	0.78
4.05	44.07	82.84	1.39	115.06	2.08	0.77	0.77
4.10	42.95	80.72	1.40	113.02	2.09	0.77	0.77
4.15	42.18	79.25	1.41	111.51	2.09	0.77	0.77
4.20	41.81	78.56	1.41	110.55	2.09	0.77	0.77
4.25	41.70	78.34	1.40	109.73	2.09	0.77	0.77
4.30	41.70	78.33	1.39	108.97	2.08	0.76	0.76
4.35	41.70	78.32	1.38	108.10	2.07	0.76	0.76
4.40	41.70	78.32	1.37	107.66	2.07	0.76	0.76
4.45	41.70	78.31	1.37	107.64	2.07	0.76	0.76
4.50	41.64	78.19	1.39	108.32	2.08	0.76	0.76
4.55	41.46	77.84	1.40	109.12	2.09	0.76	0.76
4.60	40.97	76.91	1.43	109.81	2.11	0.77	0.77
4.65	40.19	75.44	1.46	110.01	2.12	0.77	0.77
4.70	39.05	73.27	1.50	109.77	2.15	0.77	0.77
4.75	37.79	70.89	1.55	109.73	2.17	0.77	0.77
4.80	36.36	68.19	1.61	109.72	2.20	0.77	0.77

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
4.85	35.02	65.64	1.68	110.10	2.22	0.77	0.77
4.90	33.60	62.95	1.75	109.97	2.25	0.77	0.77
4.95	32.24	60.37	1.82	109.70	2.27	0.77	0.77
5.00	30.86	57.77	1.90	109.63	2.29	0.77	0.77
5.05	29.46	55.11	2.00	110.09	2.32	0.77	0.77
5.10	28.11	52.55	2.13	111.77	2.35	0.77	0.77
5.15	26.68	49.84	2.28	113.81	2.38	0.77	0.77
5.20	25.33	47.28	2.47	116.82	2.42	0.78	0.78
5.25	23.93	44.64	2.68	119.71	2.45	0.78	0.78
5.30	22.69	42.28	2.91	122.99	2.49	0.79	0.79
5.35	21.59	40.20	3.13	125.75	2.52	0.80	0.80
5.40	20.68	38.48	3.33	128.09	2.55	0.82	0.82
5.45	19.94	37.07	3.49	129.39	2.57	0.84	0.84
5.50	19.22	35.71	3.62	129.35	2.58	0.86	0.86
5.55	18.65	34.62	3.70	127.99	2.59	0.86	0.86
5.60	18.16	33.69	3.73	125.78	2.60	0.86	0.86
5.65	17.66	32.74	3.76	123.21	2.60	0.86	0.86
5.70	17.03	31.55	3.84	121.30	2.61	0.87	0.87
5.75	16.14	29.86	4.01	119.83	2.63	0.88	0.88
5.80	15.27	28.20	4.24	119.69	2.65	0.90	0.90
5.85	14.41	26.58	4.52	120.03	2.68	0.93	0.93
5.90	13.82	25.46	4.77	121.40	2.71	0.79	0.79
5.95	13.39	24.63	4.99	122.89	2.73	0.79	0.79
6.00	13.19	24.26	5.14	124.68	2.74	0.79	0.79
6.05	13.11	24.10	5.23	126.10	2.75	0.79	0.79
6.10	13.11	24.09	5.28	127.28	2.75	0.79	0.79
6.15	13.11	24.09	5.32	128.19	2.76	0.80	0.80
6.20	13.11	24.08	5.37	129.32	2.76	0.80	0.80
6.25	13.11	24.08	5.43	130.87	2.77	0.80	0.80
6.30	13.03	23.93	5.55	132.82	2.78	0.80	0.80
6.35	12.70	23.29	5.76	134.22	2.79	0.80	0.80
6.40	12.15	22.26	6.07	135.09	2.82	0.81	0.81
6.45	11.44	20.91	6.44	134.69	2.85	0.81	0.81
6.50	10.99	20.04	6.71	134.43	2.87	0.81	0.81
6.55	10.74	19.56	6.84	133.80	2.87	0.80	0.80
6.60	10.73	19.54	6.83	133.40	2.87	0.80	0.80
6.65	10.73	19.53	6.78	132.51	2.87	0.80	0.80
6.70	10.73	19.53	6.74	131.64	2.87	0.80	0.80
6.75	10.73	19.52	6.71	130.99	2.87	0.80	0.80
6.80	10.73	19.52	6.69	130.61	2.86	0.80	0.80
6.85	10.73	19.51	6.68	130.37	2.86	0.80	0.80
6.90	10.73	19.51	6.66	129.84	2.86	0.80	0.80
6.95	10.73	19.50	6.61	128.99	2.86	0.80	0.80
7.00	10.73	19.50	6.55	127.77	2.85	0.80	0.80
7.05	10.73	19.49	6.49	126.52	2.85	0.79	0.79
7.10	10.73	19.49	6.42	125.10	2.84	0.79	0.79
7.15	10.73	19.48	6.35	123.66	2.84	0.79	0.79
7.20	10.73	19.47	6.27	122.10	2.83	0.79	0.79

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
7.25	10.73	19.47	6.23	121.28	2.83	0.78	0.78
7.30	10.73	19.46	6.23	121.29	2.83	0.78	0.78
7.35	10.73	19.46	6.32	123.07	2.84	0.79	0.79
7.40	10.73	19.45	6.46	125.77	2.85	0.79	0.79
7.45	10.73	19.45	6.66	129.53	2.86	0.80	0.80
7.50	10.78	19.54	6.82	133.35	2.87	0.80	0.80
7.55	11.09	20.12	6.87	138.23	2.88	0.81	0.81
7.60	11.66	21.20	6.76	143.32	2.87	0.82	0.82
7.65	12.56	22.89	6.50	148.78	2.85	0.83	0.83
7.70	13.44	24.54	6.22	152.62	2.83	0.83	0.83
7.75	14.27	26.12	5.95	155.31	2.81	0.83	0.83
7.80	14.98	27.45	5.71	156.82	2.79	0.84	0.84
7.85	15.66	28.72	5.49	157.70	2.77	0.84	0.84
7.90	16.37	30.07	5.25	157.89	2.75	0.84	0.84
7.95	17.12	31.47	4.96	156.11	2.72	0.84	0.84
8.00	18.02	33.18	4.61	152.85	2.69	0.99	0.99
8.05	19.23	35.46	4.14	146.67	2.64	0.94	0.94
8.10	20.74	38.30	3.62	138.61	2.58	0.87	0.87
8.15	22.77	41.18	3.09	127.10	2.52	0.80	0.80
8.20	25.06	44.34	2.62	116.34	2.44	0.78	0.78
8.25	27.92	48.30	2.23	107.61	2.37	0.76	0.76
8.30	30.77	52.17	1.96	102.32	2.31	0.75	0.75
8.35	33.70	56.19	1.77	99.71	2.26	0.75	0.75
8.40	35.97	59.20	1.66	98.20	2.22	0.74	0.74
8.45	37.71	61.50	1.59	97.95	2.19	0.74	0.74
8.50	38.81	62.91	1.56	98.08	2.18	0.74	0.74
8.55	39.63	64.04	1.55	99.15	2.17	0.75	0.75
8.60	40.35	65.04	1.54	100.38	2.17	0.75	0.75
8.65	40.92	65.83	1.54	101.42	2.17	0.75	0.75
8.70	41.39	66.40	1.53	101.91	2.17	0.75	0.75
8.75	41.61	66.55	1.53	101.65	2.16	0.75	0.75
8.80	41.66	66.42	1.52	100.83	2.16	0.75	0.75
8.85	41.48	65.94	1.51	99.56	2.15	0.75	0.75
8.90	40.97	64.97	1.51	98.00	2.15	0.74	0.74
8.95	40.02	63.42	1.52	96.35	2.16	0.74	0.74
9.00	38.38	60.95	1.55	94.63	2.17	0.74	0.74
9.05	36.34	57.97	1.61	93.30	2.20	0.74	0.74
9.10	33.87	54.40	1.70	92.41	2.23	0.73	0.73
9.15	31.57	51.09	1.81	92.68	2.27	0.73	0.73
9.20	29.25	47.73	1.96	93.68	2.31	0.74	0.74
9.25	27.17	44.73	2.14	95.74	2.35	0.74	0.74
9.30	25.10	41.68	2.35	97.92	2.40	0.74	0.74
9.35	23.30	39.00	2.58	100.81	2.44	0.75	0.75
9.40	21.84	36.82	2.81	103.63	2.48	0.75	0.75
9.45	20.92	35.44	3.01	106.78	2.51	0.75	0.75
9.50	20.38	34.65	3.17	109.95	2.53	0.78	0.78
9.55	20.02	34.14	3.32	113.48	2.55	0.80	0.80
9.60	19.68	33.71	3.51	118.23	2.57	0.83	0.83

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.65	19.36	33.28	3.70	123.30	2.59	0.86	0.86
9.70	19.16	33.05	3.90	129.05	2.62	0.89	0.89
9.75	19.37	33.38	3.93	131.08	2.62	0.89	0.89
9.80	20.44	34.97	3.72	130.05	2.60	0.87	0.87
9.85	22.15	37.37	3.33	124.29	2.55	0.82	0.82
9.90	24.24	40.32	2.94	118.57	2.49	0.78	0.78
9.95	25.93	42.58	2.66	113.10	2.45	0.77	0.77
10.00	27.41	44.50	2.43	108.34	2.41	0.76	0.76
10.05	29.11	46.64	2.20	102.60	2.37	0.75	0.75
10.10	31.11	49.08	1.96	96.29	2.31	0.74	0.74
10.15	33.42	51.85	1.75	90.89	2.25	0.73	0.73
10.20	35.29	53.96	1.61	86.90	2.20	0.72	0.72
10.25	36.90	55.76	1.52	84.73	2.16	0.72	0.72
10.30	37.89	56.81	1.47	83.61	2.13	0.72	0.72
10.35	38.39	57.34	1.46	83.52	2.12	0.71	0.71
10.40	38.23	57.07	1.46	83.58	2.13	0.72	0.72
10.45	37.66	56.30	1.49	83.80	2.14	0.72	0.72
10.50	36.75	55.08	1.52	83.74	2.16	0.72	0.72
10.55	35.87	53.86	1.55	83.68	2.17	0.72	0.72
10.60	35.11	52.81	1.59	83.70	2.19	0.72	0.72
10.65	34.72	52.26	1.61	84.24	2.20	0.72	0.72
10.70	34.49	51.95	1.63	84.94	2.21	0.72	0.72
10.75	34.31	51.69	1.66	85.61	2.22	0.72	0.72
10.80	34.02	51.24	1.67	85.75	2.22	0.72	0.72
10.85	33.69	50.71	1.69	85.59	2.23	0.72	0.72
10.90	33.60	50.51	1.69	85.46	2.23	0.72	0.72
10.95	33.73	50.61	1.69	85.53	2.23	0.72	0.72
11.00	34.09	51.03	1.68	85.83	2.23	0.72	0.72
11.05	34.36	51.32	1.68	86.04	2.22	0.72	0.72
11.10	34.52	51.47	1.67	86.14	2.22	0.72	0.72
11.15	34.55	51.43	1.67	86.12	2.22	0.72	0.72
11.20	34.52	51.30	1.68	86.03	2.22	0.72	0.72
11.25	34.22	50.82	1.69	85.69	2.23	0.72	0.72
11.30	33.73	50.06	1.70	85.35	2.23	0.72	0.72
11.35	33.01	49.02	1.74	85.09	2.24	0.72	0.72
11.40	32.51	48.30	1.77	85.48	2.26	0.72	0.72
11.45	32.21	47.88	1.80	86.28	2.27	0.72	0.72
11.50	31.92	47.49	1.84	87.42	2.28	0.72	0.72
11.55	31.43	46.85	1.90	88.84	2.29	0.73	0.73
11.60	30.56	45.71	1.99	90.88	2.32	0.73	0.73
11.65	29.63	44.53	2.12	94.47	2.35	0.74	0.74
11.70	28.56	43.20	2.30	99.47	2.39	0.75	0.75
11.75	27.44	41.84	2.54	106.33	2.43	0.76	0.76
11.80	26.20	40.25	2.81	113.31	2.48	0.77	0.77
11.85	24.96	38.63	3.12	120.51	2.52	0.79	0.79
11.90	23.94	37.22	3.38	125.69	2.55	0.83	0.83
11.95	23.21	36.19	3.58	129.55	2.58	0.85	0.85
12.00	22.90	35.70	3.64	130.02	2.59	0.86	0.86

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
12.05	22.95	35.65	3.60	128.37	2.58	0.85	0.85
12.10	23.46	36.21	3.42	123.86	2.56	0.83	0.83
12.15	24.27	37.17	3.20	118.88	2.53	0.80	0.80
12.20	25.48	38.65	2.93	113.15	2.49	0.77	0.77
12.25	26.69	40.12	2.69	108.07	2.46	0.76	0.76
12.30	27.94	41.62	2.48	103.18	2.42	0.75	0.75
12.35	28.81	42.64	2.35	100.11	2.40	0.75	0.75
12.40	29.42	43.35	2.28	98.78	2.38	0.75	0.75
12.45	29.41	43.32	2.32	100.38	2.39	0.75	0.75
12.50	28.97	42.79	2.43	103.88	2.41	0.76	0.76
12.55	27.93	41.48	2.64	109.44	2.45	0.77	0.77
12.60	26.58	39.73	2.92	115.82	2.49	0.78	0.78
12.65	24.77	37.31	3.29	122.56	2.54	0.81	0.81
12.70	22.69	34.46	3.77	129.89	2.60	0.87	0.87
12.75	20.46	31.36	4.36	136.82	2.67	0.94	0.94
12.80	18.46	28.52	5.05	144.16	2.73	0.82	0.82
12.85	16.98	26.40	5.69	150.26	2.79	0.83	0.83
12.90	16.08	25.12	6.24	156.72	2.83	0.84	0.84
12.95	15.67	24.52	6.58	161.44	2.86	0.84	0.84
13.00	15.52	24.30	6.78	164.67	2.87	0.85	0.85
13.05	15.62	24.39	6.74	164.30	2.87	0.85	0.85
13.10	15.82	24.60	6.57	161.58	2.85	0.84	0.84
13.15	16.02	24.75	6.29	155.80	2.83	0.83	0.83
13.20	15.84	24.34	6.11	148.83	2.82	0.83	0.83
13.25	15.09	23.06	6.08	140.33	2.82	0.81	0.81
13.30	13.89	21.16	6.28	132.96	2.83	0.80	0.80
13.35	12.54	19.06	6.67	127.03	2.86	0.79	0.79
13.40	11.57	17.56	7.14	125.38	2.90	0.79	0.79
13.45	11.06	16.78	7.50	125.87	2.92	0.79	0.79
13.50	11.21	17.01	7.54	128.30	2.92	0.80	0.80
13.55	11.71	17.72	7.32	129.67	2.91	0.80	0.80
13.60	12.41	18.73	6.97	130.62	2.88	0.80	0.80
13.65	12.87	19.37	6.81	131.88	2.87	0.80	0.80
13.70	13.11	19.71	6.80	134.02	2.87	0.80	0.80
13.75	13.11	19.72	6.96	137.23	2.88	0.81	0.81
13.80	13.11	19.72	7.11	140.17	2.89	0.81	0.81
13.85	13.11	19.72	7.26	143.10	2.90	0.82	0.82
13.90	13.11	19.71	7.36	145.07	2.91	0.82	0.82
13.95	13.13	19.70	7.43	146.44	2.92	0.82	0.82
14.00	13.39	20.06	7.37	147.91	2.91	0.82	0.82
14.05	13.85	20.72	7.25	150.26	2.90	0.83	0.83
14.10	14.57	21.76	7.09	154.15	2.89	0.83	0.83
14.15	15.10	22.53	7.00	157.76	2.89	0.84	0.84
14.20	15.43	22.99	6.99	160.70	2.89	0.84	0.84
14.25	15.50	23.06	7.03	162.09	2.89	0.84	0.84
14.30	15.50	23.02	7.08	163.04	2.89	0.84	0.84
14.35	15.50	22.99	7.14	164.23	2.90	0.85	0.85
14.40	15.50	22.96	7.21	165.56	2.90	0.85	0.85

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
14.45	15.50	22.93	7.28	166.84	2.90	0.85	0.85
14.50	15.58	23.00	7.26	167.12	2.90	0.85	0.85
14.55	15.79	23.24	7.17	166.70	2.90	0.85	0.85
14.60	16.23	23.80	6.93	164.97	2.88	0.85	0.85
14.65	16.77	24.48	6.63	162.33	2.86	0.84	0.84
14.70	17.32	25.15	6.28	157.86	2.83	0.84	0.84
14.75	17.67	25.52	5.99	152.87	2.81	0.83	0.83
14.80	17.84	25.63	5.75	147.29	2.79	0.82	0.82
14.85	17.68	25.30	5.65	143.03	2.78	0.82	0.82
14.90	17.26	24.62	5.67	139.63	2.79	0.81	0.81
14.95	16.59	23.63	5.84	138.05	2.80	0.81	0.81
15.00	15.91	22.64	6.07	137.39	2.82	0.81	0.81
15.05	15.20	21.61	6.37	137.54	2.84	0.81	0.81
15.10	14.52	20.63	6.67	137.68	2.86	0.81	0.81
15.15	13.81	19.61	7.02	137.69	2.89	0.81	0.81
15.20	13.36	18.95	7.29	138.23	2.91	0.81	0.81
15.25	13.12	18.58	7.49	139.24	2.92	0.81	0.81
15.30	13.11	18.56	7.58	140.66	2.93	0.81	0.81
15.35	13.11	18.53	7.64	141.51	2.93	0.82	0.82
15.40	13.11	18.50	7.66	141.77	2.93	0.82	0.82
15.45	13.11	18.46	7.66	141.40	2.93	0.82	0.82
15.50	13.11	18.41	7.64	140.68	2.93	0.81	0.81
15.55	13.11	18.37	7.62	139.96	2.93	0.81	0.81
15.60	13.11	18.33	7.62	139.74	2.93	0.81	0.81
15.65	13.11	18.31	7.69	140.72	2.93	0.81	0.81
15.70	13.32	18.59	7.71	143.21	2.93	0.82	0.82
15.75	13.90	19.39	7.61	147.57	2.93	0.82	0.82
15.80	15.24	21.24	7.17	152.19	2.90	0.83	0.83
15.85	17.13	23.81	6.54	155.79	2.85	0.83	0.83
15.90	19.55	27.02	5.77	155.78	2.79	0.83	0.83
15.95	21.87	30.02	5.09	152.88	2.74	0.83	0.83
16.00	24.20	32.96	4.45	146.81	2.68	0.97	0.97
16.05	26.03	35.20	4.02	141.35	2.63	0.92	0.92
16.10	27.52	37.01	3.70	137.09	2.59	0.88	0.88
16.15	28.01	37.59	3.66	137.69	2.59	0.88	0.88
16.20	27.82	37.34	3.78	141.06	2.60	0.89	0.89
16.25	26.64	35.85	4.11	147.26	2.64	0.94	0.94
16.30	25.25	34.06	4.47	152.33	2.68	0.98	0.98
16.35	23.65	31.96	4.88	156.06	2.72	0.83	0.83
16.40	22.45	30.35	5.18	157.09	2.74	0.84	0.84
16.45	21.50	29.04	5.39	156.58	2.76	0.84	0.84
16.50	21.06	28.38	5.44	154.24	2.77	0.83	0.83
16.55	20.86	28.02	5.39	151.09	2.76	0.83	0.83
16.60	20.86	27.91	5.26	146.75	2.75	0.82	0.82
16.65	20.78	27.72	5.19	143.79	2.74	0.82	0.82
16.70	20.59	27.41	5.21	142.92	2.75	0.82	0.82
16.75	20.27	26.99	5.42	146.19	2.76	0.82	0.82
16.80	19.89	26.51	5.71	151.48	2.79	0.83	0.83

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
16.85	19.24	25.68	6.14	157.61	2.82	0.84	0.84
16.90	18.56	24.80	6.57	162.84	2.85	0.84	0.84
16.95	18.03	24.11	6.96	167.87	2.88	0.85	0.85
17.00	18.61	24.88	6.95	173.02	2.88	0.86	0.86
17.05	20.27	27.06	6.59	178.20	2.86	0.86	0.86
17.10	23.40	31.10	5.80	180.48	2.80	0.87	0.87
17.15	27.05	35.71	5.01	178.86	2.73	0.86	0.86
17.20	31.32	40.98	4.20	171.95	2.65	0.98	0.98
17.25	35.16	45.58	3.56	162.28	2.58	0.90	0.90
17.30	38.86	49.87	3.00	149.68	2.50	0.82	0.82
17.35	41.28	52.49	2.62	137.35	2.44	0.81	0.81
17.40	42.80	53.94	2.32	125.31	2.39	0.79	0.79
17.45	42.83	53.64	2.17	116.29	2.36	0.78	0.78
17.50	42.19	52.59	2.09	109.76	2.34	0.77	0.77
17.55	40.76	50.70	2.09	106.20	2.34	0.76	0.76
17.60	39.02	48.50	2.16	104.64	2.36	0.76	0.76
17.65	36.86	45.85	2.29	104.82	2.38	0.76	0.76
17.70	34.06	42.49	2.52	106.95	2.43	0.76	0.76
17.75	30.98	38.77	2.86	110.79	2.48	0.77	0.77
17.80	27.97	35.16	3.35	117.84	2.55	0.81	0.81
17.85	25.78	32.55	3.88	126.46	2.62	0.88	0.88
17.90	24.17	30.65	4.48	137.23	2.68	0.95	0.95
17.95	22.86	29.08	5.06	147.07	2.73	0.82	0.82
18.00	21.57	27.53	5.69	156.72	2.79	0.84	0.84
18.05	20.83	26.64	6.22	165.66	2.83	0.85	0.85
18.10	20.97	26.85	6.51	174.92	2.85	0.86	0.86
18.15	22.68	29.05	6.36	184.70	2.84	0.87	0.87
18.20	24.91	31.86	6.01	191.41	2.81	0.88	0.88
18.25	27.32	34.83	5.55	193.29	2.78	0.88	0.88
18.30	29.37	37.27	5.09	189.63	2.74	0.88	0.88
18.35	31.86	40.20	4.55	182.82	2.68	1.03	1.03
18.40	36.70	45.94	3.80	174.69	2.61	0.94	0.94
18.45	43.08	53.43	3.10	165.57	2.52	0.85	0.85
18.50	51.28	62.89	2.46	154.80	2.42	0.83	0.83
18.55	57.67	70.01	2.06	144.47	2.33	0.82	0.82
18.60	62.48	75.14	1.80	135.05	2.26	0.81	0.81
18.65	62.59	74.93	1.73	129.45	2.24	0.80	0.80
18.70	59.78	71.54	1.77	126.61	2.26	0.79	0.79
18.75	53.35	64.19	2.03	130.06	2.33	0.80	0.80
18.80	46.95	56.85	2.42	137.72	2.41	0.81	0.81
18.85	40.55	49.43	3.02	149.16	2.51	0.82	0.82
18.90	36.09	44.20	3.60	159.31	2.58	0.90	0.90
18.95	32.65	40.13	4.22	169.29	2.65	0.98	0.98
19.00	30.55	37.62	4.71	177.24	2.70	0.86	0.86
19.05	28.71	35.39	5.16	182.64	2.74	0.87	0.87
19.10	26.41	32.54	5.62	182.82	2.78	0.87	0.87
19.15	23.50	28.91	6.20	179.10	2.83	0.86	0.86
19.20	20.07	24.60	6.99	171.95	2.89	0.85	0.85

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
19.25	17.73	21.63	7.68	166.15	2.93	0.85	0.85
19.30	16.42	19.89	8.15	162.06	2.96	0.84	0.84
19.35	16.54	20.00	8.02	160.46	2.95	0.84	0.84
19.40	16.98	20.52	7.72	158.45	2.93	0.84	0.84
19.45	17.69	21.36	7.26	155.02	2.90	0.83	0.83
19.50	18.17	21.87	6.89	150.66	2.88	0.83	0.83
19.55	18.43	22.10	6.57	145.22	2.86	0.82	0.82
19.60	18.19	21.72	6.41	139.34	2.84	0.81	0.81
19.65	17.78	21.15	6.31	133.47	2.84	0.80	0.80
19.70	17.37	20.58	6.27	129.04	2.83	0.80	0.80
19.75	17.72	20.97	6.12	128.38	2.82	0.80	0.80
19.80	19.06	22.57	5.92	133.58	2.81	0.80	0.80
19.85	21.14	25.08	5.63	141.26	2.78	0.81	0.81
19.90	23.24	27.61	5.39	148.67	2.76	0.83	0.83
19.95	24.36	28.89	5.13	148.24	2.74	0.82	0.82
20.00	24.31	28.72	4.95	142.12	2.72	0.82	0.82
20.05	23.17	27.22	4.81	131.03	2.71	0.80	0.80
20.10	21.56	25.20	4.86	122.35	2.71	0.79	0.79
20.15	19.80	23.03	5.08	117.02	2.73	0.78	0.78
20.20	18.02	20.89	5.51	115.00	2.77	0.77	0.77
20.25	16.38	18.91	6.06	114.58	2.82	0.77	0.77
20.30	15.27	17.58	6.59	115.76	2.86	0.78	0.78
20.35	14.87	17.10	6.93	118.55	2.88	0.78	0.78
20.40	15.07	17.34	7.11	123.20	2.89	0.79	0.79
20.45	15.35	17.68	7.23	127.88	2.90	0.80	0.80
20.50	15.50	17.86	7.42	132.49	2.91	0.80	0.80
20.55	15.65	18.02	7.56	136.23	2.92	0.81	0.81
20.60	16.12	18.57	7.55	140.14	2.92	0.81	0.81
20.65	17.35	20.02	7.19	144.01	2.90	0.82	0.82
20.70	19.25	22.25	6.63	147.59	2.86	0.82	0.82
20.75	21.77	25.16	5.94	149.44	2.81	0.83	0.83
20.80	24.22	27.97	5.34	149.40	2.76	0.83	0.83
20.85	26.40	30.43	4.84	147.35	2.71	0.82	0.82
20.90	27.89	32.08	4.50	144.36	2.68	0.97	0.97
20.95	28.59	32.79	4.30	140.89	2.66	0.94	0.94
21.00	28.38	32.48	4.28	139.05	2.66	0.94	0.94
21.05	27.39	31.30	4.45	139.41	2.68	0.96	0.96
21.10	25.93	29.61	4.83	142.95	2.71	0.82	0.82
21.15	24.23	27.65	5.33	147.25	2.76	0.82	0.82
21.20	22.73	25.91	5.87	152.02	2.80	0.83	0.83
21.25	21.78	24.80	6.25	154.91	2.83	0.83	0.83
21.30	21.24	24.13	6.46	155.82	2.85	0.83	0.83
21.35	20.65	23.40	6.53	152.82	2.85	0.83	0.83
21.40	19.33	21.80	6.75	147.16	2.87	0.82	0.82
21.45	17.60	19.73	7.11	140.19	2.89	0.81	0.81
21.50	15.86	17.63	7.65	134.78	2.93	0.81	0.81
21.55	14.54	16.01	8.19	131.08	2.96	0.80	0.80
21.60	13.46	14.69	8.70	127.86	3.00	0.80	0.80

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
21.65	12.45	13.44	9.21	123.82	3.02	0.66	0.96
21.70	11.41	12.17	9.73	118.43	3.05	0.60	0.87
21.75	10.56	11.14	10.20	113.60	3.08	0.52	0.80
21.80	9.94	10.37	10.56	109.55	3.10	0.48	0.74
21.85	9.64	10.00	10.79	107.95	3.11	0.45	0.71
21.90	9.63	9.98	10.85	108.24	3.11	0.46	0.71
21.95	9.92	10.30	10.76	110.77	3.11	0.49	0.74
22.00	10.36	10.80	10.57	114.18	3.10	0.53	0.77
22.05	10.84	11.35	10.42	118.27	3.09	0.58	0.81
22.10	11.28	11.86	10.32	122.33	3.08	0.63	0.85
22.15	11.78	12.43	10.20	126.83	3.08	0.68	0.89
22.20	12.54	13.31	9.91	131.86	3.06	0.74	0.95
22.25	13.51	14.43	9.49	136.89	3.04	0.83	1.03
22.30	14.66	15.76	8.96	141.27	3.01	0.90	1.13
22.35	16.29	17.65	8.25	145.67	2.97	0.82	0.82
22.40	18.38	20.07	7.44	149.26	2.92	0.83	0.83
22.45	21.10	23.12	6.54	151.28	2.85	0.83	0.83
22.50	23.53	25.78	5.81	149.91	2.80	0.83	0.83
22.55	25.65	28.08	5.17	145.19	2.74	0.82	0.82
22.60	26.99	29.47	4.70	138.46	2.70	0.98	0.98
22.65	27.93	30.40	4.31	130.92	2.66	0.93	0.93
22.70	28.11	30.52	4.10	125.14	2.64	0.90	0.90
22.75	27.77	30.06	4.03	121.00	2.63	0.88	0.88
22.80	26.72	28.86	4.17	120.20	2.65	0.90	0.90
22.85	25.36	27.33	4.43	121.19	2.67	0.92	0.92
22.90	23.55	25.32	4.89	123.79	2.72	0.79	0.79
22.95	21.57	23.11	5.43	125.59	2.77	0.79	0.79
23.00	19.55	20.85	6.08	126.77	2.82	0.79	0.79
23.05	17.74	18.82	6.74	126.79	2.87	0.79	0.79
23.10	16.26	17.15	7.39	126.68	2.91	0.79	0.79
23.15	15.01	15.69	8.05	126.27	2.96	0.79	0.79
23.20	14.12	14.64	8.64	126.45	2.99	0.79	0.79
23.25	13.48	13.88	9.17	127.37	3.02	0.70	0.99
23.30	13.22	13.57	9.55	129.58	3.04	0.72	0.97
23.35	13.14	13.45	9.89	133.12	3.06	0.76	0.96
23.40	13.31	13.61	10.12	137.78	3.07	0.81	0.97
23.45	13.70	14.04	10.21	143.37	3.08	0.88	1.00
23.50	14.44	14.85	10.02	148.80	3.07	0.97	1.06
23.55	15.48	16.01	9.59	153.56	3.05	1.05	1.14
23.60	16.69	17.35	9.00	156.13	3.01	1.12	1.24
23.65	17.65	18.41	8.48	156.09	2.98	0.84	0.84
23.70	18.15	18.94	8.08	153.01	2.96	0.83	0.83
23.75	17.98	18.72	7.88	147.60	2.94	0.82	0.82
23.80	17.49	18.13	7.79	141.12	2.94	0.81	0.81
23.85	16.78	17.30	7.77	134.36	2.94	0.80	0.80
23.90	15.98	16.37	7.82	128.08	2.94	0.80	0.80
23.95	15.09	15.36	7.93	121.85	2.95	0.79	0.79
24.00	14.19	14.32	8.11	116.08	2.96	0.78	0.78

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
24.05	13.55	13.58	8.18	111.15	2.96	0.77	0.77
24.10	13.20	13.17	8.28	109.11	2.97	0.76	0.76
24.15	13.30	13.26	8.32	110.41	2.97	0.77	0.77
24.20	13.74	13.73	8.47	116.27	2.98	0.78	0.78
24.25	14.80	14.89	8.41	125.27	2.98	0.79	0.79
24.30	16.23	16.44	8.32	136.81	2.97	0.81	0.81
24.35	18.18	18.58	7.97	148.06	2.95	0.82	0.82
24.40	20.21	20.79	7.59	157.80	2.93	0.84	0.84
24.45	22.53	23.30	7.02	163.48	2.89	0.84	0.84
24.50	25.19	26.12	6.38	166.60	2.84	0.85	0.85
24.55	28.19	29.28	5.69	166.51	2.79	0.85	0.85
24.60	31.49	32.73	5.07	165.98	2.73	0.85	0.85
24.65	34.39	35.73	4.58	163.76	2.69	1.01	1.01
24.70	36.86	38.27	4.21	161.05	2.65	0.97	0.97
24.75	38.66	40.08	3.92	157.16	2.62	0.93	0.93
24.80	40.24	41.65	3.66	152.45	2.59	0.90	0.90
24.85	41.99	43.39	3.40	147.45	2.56	0.86	0.86
24.90	44.00	45.38	3.12	141.37	2.52	0.82	0.82
24.95	46.64	48.02	2.82	135.54	2.48	0.81	0.81
25.00	49.30	50.65	2.55	129.14	2.43	0.80	0.80
25.05	52.08	53.40	2.32	123.72	2.39	0.79	0.79
25.10	53.91	55.16	2.15	118.66	2.35	0.78	0.78
25.15	55.06	56.22	2.04	114.69	2.33	0.77	0.77
25.20	55.46	56.53	1.98	111.85	2.31	0.77	0.77
25.25	55.87	56.85	1.94	110.41	2.30	0.77	0.77
25.30	56.48	57.41	1.92	110.21	2.30	0.77	0.77
25.35	57.20	58.07	1.90	110.52	2.29	0.77	0.77
25.40	57.98	58.80	1.89	111.18	2.29	0.77	0.77
25.45	58.95	59.72	1.87	111.96	2.29	0.77	0.77
25.50	60.19	60.91	1.85	112.60	2.28	0.77	0.77
25.55	61.96	62.63	1.80	112.86	2.27	0.77	0.77
25.60	64.03	64.63	1.74	112.54	2.25	0.77	0.77
25.65	66.76	67.30	1.67	112.58	2.22	0.77	0.77
25.70	69.59	70.06	1.61	113.00	2.20	0.77	0.77
25.75	72.49	72.90	1.57	114.12	2.18	0.77	0.77
25.80	75.35	75.69	1.53	115.74	2.16	0.78	0.78
25.85	78.28	78.55	1.50	118.06	2.15	0.78	0.78
25.90	81.53	81.75	1.48	121.18	2.14	0.78	0.78
25.95	83.12	83.27	1.48	123.07	2.14	0.79	0.79
26.00	82.31	82.35	1.49	122.42	2.14	0.79	0.79
26.05	79.36	79.29	1.51	119.46	2.15	0.78	0.78
26.10	76.33	76.14	1.52	115.83	2.16	0.78	0.78
26.15	75.41	75.11	1.52	114.22	2.16	0.77	0.77
26.20	75.46	75.07	1.52	113.85	2.16	0.77	0.77
26.25	75.56	75.10	1.52	114.26	2.16	0.77	0.77
26.30	74.50	73.96	1.54	114.10	2.17	0.77	0.77
26.35	72.82	72.22	1.58	113.87	2.18	0.77	0.77
26.40	71.07	70.41	1.62	113.99	2.20	0.77	0.77

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
26.45	69.30	68.58	1.68	115.12	2.22	0.77	0.77
26.50	67.46	66.70	1.76	117.10	2.25	0.78	0.78
26.55	65.64	64.85	1.85	120.28	2.28	0.78	0.78
26.60	63.55	62.72	1.98	123.94	2.31	0.79	0.79
26.65	61.12	60.26	2.12	128.02	2.35	0.80	0.80
26.70	58.35	57.45	2.32	133.12	2.39	0.80	0.80
26.75	55.46	54.53	2.54	138.68	2.43	0.81	0.81
26.80	52.67	51.71	2.81	145.49	2.48	0.82	0.82
26.85	49.61	48.61	3.11	151.41	2.52	0.83	0.83
26.90	46.41	45.37	3.46	157.14	2.57	0.88	0.88
26.95	42.85	41.77	3.86	161.23	2.61	0.93	0.93
27.00	39.81	38.68	4.25	164.56	2.65	0.98	0.98
27.05	37.31	36.14	4.62	166.86	2.69	1.01	1.01
27.10	35.96	34.74	4.86	168.70	2.71	0.85	0.85
27.15	35.29	34.03	5.00	170.04	2.73	0.85	0.85
27.20	35.12	33.80	5.04	170.50	2.73	0.85	0.85
27.25	34.89	33.53	5.07	170.13	2.73	0.85	0.85
27.30	34.59	33.18	5.11	169.40	2.74	0.85	0.85
27.35	34.50	33.03	5.13	169.37	2.74	0.85	0.85
27.40	34.67	33.16	5.14	170.51	2.74	0.85	0.85
27.45	35.15	33.58	5.14	172.54	2.74	0.86	0.86
27.50	35.43	33.82	5.17	174.71	2.74	0.86	0.86
27.55	35.45	33.79	5.23	176.60	2.75	0.86	0.86
27.60	34.87	33.16	5.36	177.61	2.76	0.86	0.86
27.65	34.00	32.26	5.52	178.02	2.77	0.86	0.86
27.70	33.63	31.85	5.61	178.60	2.78	0.86	0.86
27.75	34.10	32.26	5.56	179.47	2.78	0.86	0.86
27.80	35.49	33.58	5.36	179.99	2.76	0.86	0.86
27.85	37.10	35.11	5.10	179.02	2.74	0.86	0.86
27.90	39.04	36.95	4.77	176.14	2.71	0.86	0.86
27.95	41.71	39.51	4.37	172.64	2.67	1.00	1.00
28.00	44.66	42.31	3.96	167.52	2.62	0.95	0.95
28.05	47.02	44.54	3.64	162.17	2.59	0.91	0.91
28.10	47.52	44.96	3.45	155.18	2.56	0.88	0.88
28.15	46.09	43.50	3.44	149.84	2.56	0.87	0.87
28.20	43.31	40.73	3.58	145.94	2.58	0.88	0.88
28.25	39.82	37.29	3.89	145.14	2.62	0.91	0.91
28.30	36.40	33.92	4.28	145.06	2.66	0.95	0.95
28.35	33.71	31.27	4.67	145.87	2.70	0.99	0.99
28.40	32.17	29.73	4.94	146.89	2.72	0.82	0.82
28.45	31.53	29.07	5.11	148.63	2.74	0.83	0.83
28.50	31.26	28.76	5.24	150.74	2.75	0.83	0.83
28.55	30.87	28.36	5.38	152.68	2.76	0.83	0.83
28.60	30.51	27.97	5.51	154.20	2.77	0.83	0.83
28.65	30.47	27.89	5.57	155.21	2.78	0.83	0.83
28.70	30.58	27.96	5.55	155.03	2.77	0.83	0.83
28.75	30.60	27.93	5.49	153.36	2.77	0.83	0.83
28.80	29.20	26.55	5.60	148.69	2.78	0.83	0.83

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
28.85	26.34	23.76	5.94	141.17	2.81	0.81	0.81
28.90	22.09	19.64	6.66	130.78	2.86	0.80	0.80
28.95	18.12	15.80	7.57	119.61	2.92	0.78	0.78
29.00	15.37	13.13	8.39	110.11	2.98	0.77	0.77
29.05	14.03	11.83	8.73	103.30	3.00	0.75	0.75
29.10	13.51	11.32	8.73	98.81	3.00	0.75	0.75
29.15	13.24	11.05	8.59	94.90	2.99	0.74	0.74
29.20	13.11	10.91	8.43	91.97	2.98	0.73	0.73
29.25	13.11	10.89	8.28	90.19	2.97	0.73	0.73
29.30	13.11	10.87	8.27	89.95	2.97	0.73	0.73
29.35	13.11	10.86	8.38	90.96	2.98	0.73	0.73
29.40	13.11	10.84	8.58	93.04	2.99	0.73	0.73
29.45	13.11	10.83	8.81	95.44	3.00	0.37	0.77
29.50	13.36	11.05	8.91	98.49	3.01	0.39	0.79
29.55	13.81	11.47	8.89	101.95	3.01	0.43	0.82
29.60	14.52	12.12	8.71	105.65	3.00	0.76	0.76
29.65	15.32	12.86	8.49	109.24	2.98	0.76	0.76
29.70	16.41	13.87	8.13	112.82	2.96	0.77	0.77
29.75	17.69	15.06	7.73	116.36	2.93	0.78	0.78
29.80	19.03	16.30	7.28	118.68	2.91	0.78	0.78
29.85	19.87	17.07	6.98	119.18	2.88	0.78	0.78
29.90	20.01	17.18	6.86	117.81	2.88	0.78	0.78
29.95	18.99	16.20	7.10	115.07	2.89	0.77	0.77
30.00	18.18	15.42	7.35	113.32	2.91	0.77	0.77
30.05	18.22	15.43	7.31	112.87	2.91	0.77	0.77
30.10	20.31	17.37	6.62	115.01	2.86	0.77	0.77
30.15	23.10	19.96	5.85	116.84	2.80	0.78	0.78
30.20	25.29	21.99	5.36	117.94	2.76	0.78	0.78
30.25	26.11	22.72	5.23	118.75	2.75	0.78	0.78
30.30	25.75	22.35	5.40	120.72	2.76	0.78	0.78
30.35	25.28	21.88	5.73	125.41	2.79	0.79	0.79
30.40	24.92	21.51	6.18	132.98	2.83	0.80	0.80
30.45	26.19	22.65	6.40	144.96	2.84	0.82	0.82
30.50	28.97	25.20	6.35	160.00	2.84	0.84	0.84
30.55	34.13	29.94	5.88	176.16	2.80	0.86	0.86
30.60	40.03	35.37	5.32	188.27	2.76	0.87	0.87
30.65	47.16	41.93	4.63	194.28	2.69	1.05	1.05
30.70	53.35	47.61	4.03	191.77	2.63	0.99	0.99
30.75	58.70	52.51	3.51	184.10	2.57	0.92	0.92
30.80	62.66	56.12	3.10	173.99	2.52	0.86	0.86
30.85	66.56	59.66	2.77	165.44	2.47	0.85	0.85
30.90	71.42	64.10	2.49	159.58	2.42	0.84	0.84
30.95	76.82	69.03	2.25	155.17	2.38	0.83	0.83
31.00	82.78	74.46	2.04	151.92	2.33	0.83	0.83
31.05	88.37	79.56	1.87	148.44	2.28	0.82	0.82
31.10	93.74	84.44	1.73	146.17	2.24	0.82	0.82
31.15	98.72	88.96	1.64	145.53	2.21	0.82	0.82
31.20	103.47	93.25	1.58	147.45	2.19	0.82	0.82

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
31.25	109.02	98.24	1.55	152.11	2.17	0.83	0.83
31.30	115.77	104.33	1.53	159.36	2.16	0.84	0.84
31.35	123.72	111.51	1.50	167.81	2.15	0.85	0.85
31.40	132.87	119.76	1.48	177.11	2.14	0.86	0.86
31.45	142.35	128.33	1.45	185.77	2.12	0.87	0.87
31.50	153.16	138.10	1.41	195.20	2.10	0.88	0.88
31.55	163.20	147.16	1.38	203.54	2.07	0.89	0.89
31.60	173.03	156.02	1.36	211.85	2.05	0.90	0.90
31.65	180.44	162.64	1.34	217.88	2.04	0.91	0.91
31.70	186.57	168.09	1.33	222.79	2.02	0.91	0.91
31.75	191.07	172.05	1.31	226.20	2.01	0.91	0.91
31.80	194.89	175.37	1.31	229.14	2.00	0.92	0.92
31.85	198.61	178.59	1.30	232.22	1.99	0.92	0.92
31.90	202.38	181.85	1.29	235.46	1.98	0.92	0.92
31.95	206.39	185.31	1.29	239.04	1.98	0.93	0.93
32.00	209.00	187.50	1.29	241.32	1.97	0.93	0.93
32.05	210.08	188.27	1.29	242.36	1.97	0.93	0.93
32.10	208.94	187.01	1.29	241.44	1.98	0.93	0.93
32.15	207.00	185.02	1.30	240.15	1.99	0.93	0.93
32.20	204.32	182.34	1.31	238.41	2.00	0.93	0.93
32.25	201.85	179.85	1.32	237.31	2.01	0.92	0.92
32.30	199.62	177.59	1.33	236.38	2.03	0.92	0.92
32.35	198.37	176.23	1.34	236.18	2.04	0.92	0.92
32.40	198.24	175.91	1.34	236.04	2.04	0.92	0.92
32.45	199.82	177.15	1.34	236.75	2.03	0.92	0.92
32.50	202.60	179.52	1.32	237.65	2.02	0.92	0.92
32.55	206.36	182.79	1.31	239.27	2.00	0.93	0.93
32.60	210.53	186.43	1.29	241.11	1.98	0.93	0.93
32.65	214.74	190.11	1.28	243.31	1.96	0.93	0.93
32.70	218.70	193.56	1.27	245.52	1.95	0.93	0.93
32.75	221.32	195.76	1.26	246.83	1.94	0.93	0.93
32.80	222.30	196.48	1.26	246.97	1.93	0.93	0.93
32.85	221.39	195.47	1.26	245.74	1.93	0.93	0.93
32.90	219.55	193.60	1.26	243.89	1.93	0.93	0.93
32.95	217.58	191.62	1.26	242.03	1.94	0.93	0.93
33.00	215.84	189.86	1.27	240.19	1.94	0.93	0.93
33.05	214.08	188.09	1.27	238.17	1.94	0.93	0.93
33.10	211.73	185.81	1.27	235.40	1.95	0.92	0.92
33.15	208.42	182.68	1.27	231.84	1.95	0.92	0.92
33.20	203.60	178.18	1.27	226.98	1.96	0.91	0.91
33.25	197.58	172.60	1.28	221.31	1.97	0.91	0.91
33.30	189.54	165.23	1.29	213.96	1.98	0.90	0.90
33.35	181.40	157.75	1.31	207.08	2.01	0.89	0.89
33.40	173.00	150.06	1.34	200.33	2.03	0.89	0.89
33.45	166.53	144.09	1.36	195.86	2.05	0.88	0.88
33.50	161.02	139.02	1.38	191.82	2.07	0.88	0.88
33.55	157.44	135.69	1.39	189.00	2.08	0.87	0.87
33.60	155.20	133.59	1.39	186.21	2.08	0.87	0.87

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
33.65	155.05	133.36	1.39	184.71	2.08	0.87	0.87
33.70	155.92	134.06	1.37	183.45	2.06	0.87	0.87
33.75	157.40	135.31	1.35	182.75	2.05	0.87	0.87
33.80	158.78	136.49	1.33	181.82	2.03	0.87	0.87
33.85	160.22	137.70	1.32	181.31	2.01	0.87	0.87
33.90	161.17	138.50	1.30	180.58	2.00	0.87	0.87
33.95	161.04	138.31	1.30	179.34	1.99	0.86	0.86
34.00	159.04	136.45	1.30	176.73	1.98	0.86	0.86
34.05	156.01	133.64	1.30	173.80	1.99	0.86	0.86
34.10	152.34	130.25	1.31	170.80	2.00	0.85	0.85
34.15	149.01	127.13	1.33	168.66	2.02	0.85	0.85
34.20	145.93	124.24	1.34	166.90	2.04	0.85	0.85
34.25	143.37	121.81	1.36	165.70	2.05	0.85	0.85
34.30	141.80	120.26	1.37	165.25	2.07	0.85	0.85
34.35	141.31	119.67	1.38	165.60	2.07	0.85	0.85
34.40	141.88	120.02	1.39	166.64	2.08	0.85	0.85
34.45	143.01	120.85	1.39	167.98	2.08	0.85	0.85
34.50	144.50	122.01	1.39	169.67	2.08	0.85	0.85
34.55	146.18	123.31	1.39	171.61	2.08	0.85	0.85
34.60	148.30	125.00	1.39	173.90	2.08	0.86	0.86
34.65	150.68	126.93	1.39	176.09	2.08	0.86	0.86
34.70	153.55	129.30	1.38	178.30	2.07	0.86	0.86
34.75	156.78	132.00	1.37	180.38	2.06	0.86	0.86
34.80	160.27	134.93	1.35	182.58	2.05	0.87	0.87
34.85	163.82	137.92	1.34	184.80	2.04	0.87	0.87
34.90	166.56	140.18	1.33	186.64	2.03	0.87	0.87
34.95	168.16	141.44	1.33	187.78	2.02	0.87	0.87
35.00	168.07	141.20	1.33	187.93	2.03	0.87	0.87
35.05	166.85	139.96	1.34	187.36	2.03	0.87	0.87
35.10	165.03	138.17	1.35	186.60	2.05	0.87	0.87
35.15	163.32	136.50	1.36	185.97	2.06	0.87	0.87
35.20	162.03	135.19	1.37	185.69	2.07	0.87	0.87
35.25	161.27	134.37	1.38	185.58	2.07	0.87	0.87
35.30	160.94	133.92	1.39	185.60	2.08	0.87	0.87
35.35	161.08	133.89	1.39	185.75	2.08	0.87	0.87
35.40	161.52	134.13	1.39	186.05	2.08	0.87	0.87
35.45	162.34	134.69	1.39	186.63	2.08	0.87	0.87
35.50	163.26	135.34	1.38	187.29	2.07	0.87	0.87
35.55	164.33	136.12	1.38	188.07	2.07	0.87	0.87
35.60	165.51	136.99	1.38	188.81	2.07	0.87	0.87
35.65	166.97	138.11	1.37	189.67	2.07	0.88	0.88
35.70	168.87	139.62	1.37	190.72	2.06	0.88	0.88
35.75	171.00	141.33	1.36	191.99	2.05	0.88	0.88
35.80	173.32	143.18	1.35	193.48	2.05	0.88	0.88
35.85	175.30	144.75	1.35	194.80	2.04	0.88	0.88
35.90	177.07	146.14	1.34	195.98	2.04	0.88	0.88
35.95	178.13	146.90	1.34	196.61	2.03	0.88	0.88
36.00	178.63	147.17	1.34	196.90	2.03	0.88	0.88

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
36.05	177.88	146.38	1.34	196.23	2.04	0.88	0.88
36.10	176.26	144.84	1.35	194.88	2.04	0.88	0.88
36.15	173.28	142.14	1.35	192.38	2.05	0.88	0.88
36.20	169.82	139.04	1.36	189.59	2.06	0.88	0.88
36.25	165.72	135.41	1.38	186.35	2.07	0.87	0.87
36.30	161.89	132.00	1.39	183.40	2.08	0.87	0.87
36.35	157.98	128.56	1.40	180.16	2.09	0.86	0.86
36.40	152.84	124.11	1.42	175.67	2.10	0.86	0.86
36.45	146.42	118.61	1.43	169.73	2.11	0.85	0.85
36.50	137.93	111.40	1.45	161.92	2.12	0.84	0.84
36.55	131.24	105.74	1.47	155.26	2.13	0.83	0.83
36.60	126.58	101.79	1.48	150.19	2.13	0.83	0.83
36.65	126.90	102.02	1.46	148.88	2.13	0.83	0.83
36.70	129.22	103.91	1.44	149.66	2.11	0.83	0.83
36.75	132.57	106.64	1.42	151.77	2.10	0.83	0.83
36.80	132.90	106.77	1.43	152.68	2.11	0.83	0.83
36.85	129.15	103.43	1.46	151.48	2.13	0.83	0.83
36.90	120.57	95.99	1.56	149.44	2.18	0.83	0.83
36.95	109.20	86.26	1.72	148.40	2.24	0.82	0.82
37.00	96.25	75.25	2.00	150.52	2.32	0.83	0.83
37.05	83.85	64.83	2.39	154.97	2.40	0.83	0.83
37.10	71.18	54.30	2.94	159.91	2.50	0.84	0.84
37.15	60.50	45.50	3.63	165.02	2.59	0.91	0.91
37.20	51.00	37.77	4.44	167.57	2.67	1.00	1.00
37.25	44.67	32.64	5.17	168.73	2.74	0.85	0.85
37.30	39.79	28.73	5.77	165.90	2.79	0.85	0.85
37.35	36.21	25.89	6.21	160.83	2.83	0.84	0.84
37.40	33.31	23.61	6.50	153.47	2.85	0.83	0.83
37.45	31.01	21.83	6.68	145.85	2.86	0.82	0.82
37.50	29.53	20.68	6.72	138.90	2.87	0.81	0.81
37.55	28.34	19.75	6.73	132.88	2.87	0.80	0.80
37.60	27.15	18.83	6.75	127.12	2.87	0.79	0.79
37.65	26.61	18.40	6.71	123.40	2.86	0.79	0.79
37.70	28.33	19.71	6.27	123.59	2.83	0.79	0.79
37.75	31.84	22.41	5.80	129.95	2.80	0.80	0.80
37.80	36.44	25.93	5.40	140.08	2.76	0.81	0.81
37.85	38.93	27.78	5.45	151.43	2.77	0.83	0.83
37.90	40.34	28.79	5.56	160.06	2.78	0.84	0.84
37.95	43.01	30.79	5.45	167.96	2.77	0.85	0.85
38.00	48.68	35.20	4.85	170.85	2.71	0.85	0.85
38.05	58.51	42.95	3.96	170.30	2.62	0.95	0.95
38.10	69.29	51.60	3.12	160.90	2.52	0.85	0.85
38.15	81.00	61.13	2.44	149.34	2.41	0.83	0.83
38.20	91.48	69.87	1.95	136.32	2.31	0.81	0.81
38.25	100.61	77.55	1.66	128.87	2.22	0.80	0.80
38.30	107.26	83.27	1.50	124.52	2.15	0.79	0.79
38.35	110.81	86.35	1.42	122.93	2.10	0.79	0.79
38.40	111.54	87.02	1.39	121.21	2.08	0.78	0.78

:: Strength loss calculation (Robertson (2009)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
38.45	110.10	85.78	1.40	119.80	2.08	0.78	0.78
38.50	107.73	83.72	1.42	118.55	2.10	0.78	0.78
38.55	104.98	81.28	1.45	118.12	2.12	0.78	0.78
38.60	102.27	78.87	1.50	118.33	2.15	0.78	0.78
38.65	99.41	76.33	1.56	119.14	2.18	0.78	0.78
38.70	97.36	74.48	1.62	120.46	2.20	0.78	0.78
38.75	96.13	73.33	1.66	121.75	2.22	0.79	0.79
38.80	96.51	73.55	1.67	122.50	2.22	0.79	0.79
38.85	97.65	74.42	1.65	122.48	2.21	0.79	0.79
38.90	99.57	75.96	1.60	121.86	2.20	0.79	0.79
38.95	101.45	77.49	1.57	121.34	2.18	0.78	0.78
39.00	103.41	79.06	1.53	121.23	2.16	0.78	0.78
39.05	104.30	79.71	1.53	121.67	2.16	0.79	0.79
39.10	104.12	79.44	1.54	122.39	2.17	0.79	0.79
39.15	102.07	77.60	1.59	123.48	2.19	0.79	0.79
39.20	99.25	75.11	1.67	125.26	2.22	0.79	0.79
39.25	95.46	71.83	1.78	128.08	2.26	0.80	0.80
39.30	91.24	68.21	1.94	132.15	2.30	0.80	0.80
39.35	85.91	63.72	2.15	136.82	2.35	0.81	0.81
39.40	80.34	59.09	2.42	142.78	2.41	0.82	0.82
39.45	74.97	54.68	2.72	148.58	2.46	0.83	0.83
39.50	70.67	51.14	3.03	154.93	2.51	0.83	0.83
39.55	67.29	48.38	3.29	159.10	2.54	0.86	0.86
39.60	64.57	46.18	3.50	161.57	2.57	0.89	0.89
39.65	63.21	45.08	3.55	160.17	2.58	0.90	0.90
39.70	63.09	44.98	3.49	157.17	2.57	0.89	0.89
39.75	64.30	45.91	3.34	153.20	2.55	0.86	0.86
39.80	65.78	47.05	3.20	150.41	2.53	0.84	0.84
39.85	67.57	48.42	3.06	148.38	2.51	0.82	0.82
39.90	69.92	50.27	2.87	144.07	2.48	0.82	0.82
39.95	73.38	53.05	2.58	136.93	2.44	0.81	0.81
40.00	76.70	55.79	2.29	127.51	2.38	0.79	0.79
40.05	79.39	58.04	2.07	120.37	2.34	0.78	0.78
40.10	80.09	58.63	2.00	117.00	2.32	0.78	0.78
40.15	79.80	58.34	2.01	117.02	2.32	0.78	0.78
40.20	78.56	57.24	2.08	118.96	2.34	0.78	0.78
40.25	77.27	56.10	2.16	121.10	2.36	0.78	0.78
40.30	75.86	54.88	2.24	123.19	2.37	0.79	0.79
40.35	74.61	53.81	2.32	124.64	2.39	0.79	0.79
40.40	73.46	52.85	2.36	124.90	2.40	0.79	0.79
40.45	72.40	52.00	2.37	123.47	2.40	0.79	0.79
40.50	71.39	51.21	2.36	120.96	2.40	0.78	0.78
40.55	70.32	50.39	2.34	117.87	2.39	0.78	0.78
40.60	68.99	49.33	2.36	116.60	2.40	0.78	0.78
40.65	67.26	47.92	2.45	117.24	2.41	0.78	0.78
40.70	64.92	45.97	2.64	121.43	2.45	0.79	0.79
40.75	62.36	43.85	2.89	126.93	2.49	0.79	0.79
40.80	59.39	41.41	3.23	133.71	2.53	0.82	0.82

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
40.85	56.83	39.33	3.53	138.79	2.57	0.86	0.86
40.90	54.64	37.58	3.79	142.38	2.60	0.90	0.90
40.95	54.44	37.37	3.83	143.11	2.61	0.90	0.90
41.00	55.85	38.41	3.70	142.02	2.59	0.89	0.89
41.05	59.98	41.56	3.33	138.21	2.55	0.84	0.84
41.10	65.10	45.50	2.93	133.14	2.49	0.80	0.80
41.15	71.52	50.49	2.51	126.96	2.43	0.79	0.79
41.20	77.66	55.32	2.20	121.83	2.37	0.79	0.79
41.25	84.09	60.40	1.95	117.94	2.31	0.78	0.78
41.30	90.57	65.55	1.76	115.56	2.25	0.78	0.78
41.35	97.02	70.71	1.62	114.48	2.20	0.77	0.77
41.40	103.34	75.81	1.51	114.35	2.15	0.77	0.77
41.45	108.53	80.03	1.44	115.04	2.11	0.77	0.77
41.50	113.02	83.70	1.39	116.12	2.08	0.78	0.78
41.55	115.16	85.45	1.36	116.49	2.06	0.78	0.78
41.60	115.36	85.63	1.35	115.88	2.05	0.78	0.78
41.65	111.94	82.85	1.37	113.19	2.06	0.77	0.77
41.70	106.66	78.55	1.40	109.84	2.09	0.77	0.77
41.75	98.88	72.23	1.47	105.98	2.13	0.76	0.76
41.80	90.96	65.75	1.59	104.54	2.19	0.76	0.76
41.85	82.43	58.83	1.80	105.82	2.26	0.76	0.76
41.90	75.38	53.10	2.08	110.70	2.34	0.77	0.77
41.95	69.28	48.21	2.41	116.29	2.41	0.78	0.78
42.00	64.01	44.03	2.77	121.84	2.47	0.79	0.79
42.05	59.15	40.23	3.16	126.93	2.52	0.80	0.80
42.10	54.53	36.64	3.61	132.43	2.58	0.86	0.86
42.15	51.91	34.58	3.98	137.59	2.63	0.91	0.91
42.20	50.83	33.68	4.22	142.10	2.65	0.94	0.94
42.25	51.46	34.07	4.24	144.40	2.65	0.94	0.94
42.30	52.30	34.64	4.18	144.97	2.65	0.94	0.94
42.35	53.04	35.17	4.08	143.50	2.64	0.93	0.93
42.40	53.37	35.39	4.02	142.17	2.63	0.92	0.92
42.45	53.34	35.34	4.00	141.51	2.63	0.92	0.92
42.50	52.74	34.84	4.10	142.94	2.64	0.93	0.93
42.55	51.69	34.00	4.27	145.32	2.66	0.95	0.95
42.60	49.87	32.58	4.57	148.79	2.69	0.98	0.98
42.65	47.83	31.01	4.92	152.45	2.72	0.83	0.83
42.70	45.50	29.23	5.36	156.77	2.76	0.84	0.84
42.75	44.11	28.14	5.73	161.19	2.79	0.84	0.84
42.80	43.65	27.72	5.98	165.81	2.81	0.85	0.85
42.85	45.52	28.99	5.86	169.89	2.80	0.85	0.85
42.90	48.86	31.33	5.51	172.70	2.77	0.86	0.86
42.95	54.26	35.19	4.90	172.48	2.72	0.86	0.86
43.00	59.96	39.32	4.30	168.95	2.66	0.99	0.99
43.05	66.38	44.07	3.67	161.80	2.59	0.91	0.91
43.10	71.78	48.15	3.18	152.89	2.53	0.84	0.84
43.15	76.39	51.71	2.77	143.28	2.47	0.82	0.82
43.20	78.77	53.63	2.51	134.57	2.42	0.81	0.81

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
43.25	79.71	54.45	2.35	128.17	2.40	0.80	0.80
43.30	79.20	54.10	2.31	124.94	2.39	0.79	0.79
43.35	78.76	53.69	2.34	125.89	2.39	0.79	0.79
43.40	78.69	53.47	2.43	130.11	2.41	0.80	0.80
43.45	78.43	53.06	2.57	136.32	2.44	0.81	0.81
43.50	77.44	52.12	2.74	142.81	2.46	0.82	0.82
43.55	74.94	50.08	2.98	149.15	2.50	0.83	0.83
43.60	72.49	48.11	3.22	154.85	2.53	0.85	0.85
43.65	70.55	46.54	3.45	160.67	2.56	0.89	0.89
43.70	71.50	47.08	3.52	165.81	2.57	0.90	0.90
43.75	74.94	49.44	3.45	170.55	2.56	0.90	0.90
43.80	80.85	53.66	3.21	172.00	2.53	0.87	0.87
43.85	87.12	58.21	2.93	170.73	2.49	0.85	0.85
43.90	93.83	63.18	2.63	166.08	2.45	0.85	0.85
43.95	101.14	68.65	2.35	161.46	2.40	0.84	0.84
44.00	110.53	75.73	2.08	157.27	2.34	0.84	0.84
44.05	121.59	84.08	1.85	155.83	2.28	0.83	0.83
44.10	133.55	93.17	1.68	156.49	2.22	0.84	0.84
44.15	145.66	102.44	1.55	158.95	2.17	0.84	0.84
44.20	156.89	111.13	1.46	162.31	2.13	0.84	0.84
44.25	168.00	119.81	1.39	166.68	2.08	0.85	0.85
44.30	177.83	127.46	1.35	172.03	2.05	0.86	0.86
44.35	187.59	134.95	1.32	178.61	2.02	0.86	0.86
44.40	196.04	141.30	1.31	185.16	2.00	0.87	0.87
44.45	203.45	146.83	1.30	191.06	1.99	0.88	0.88
44.50	209.43	151.26	1.29	195.82	1.98	0.88	0.88
44.55	214.10	154.68	1.29	199.50	1.98	0.89	0.89
44.60	217.99	157.52	1.29	202.56	1.97	0.89	0.89
44.65	220.70	159.45	1.28	204.64	1.97	0.89	0.89
44.70	222.71	160.85	1.28	206.15	1.97	0.89	0.89
44.75	223.47	161.28	1.28	206.62	1.97	0.89	0.89
44.80	223.50	161.17	1.28	206.50	1.97	0.89	0.89
44.85	222.63	160.37	1.28	205.63	1.97	0.89	0.89
44.90	221.39	159.29	1.28	204.47	1.97	0.89	0.89
44.95	219.77	157.93	1.29	203.00	1.97	0.89	0.89
45.00	218.21	156.60	1.29	201.57	1.97	0.89	0.89
45.05	216.72	155.34	1.29	200.21	1.98	0.89	0.89
45.10	215.31	154.14	1.29	198.92	1.98	0.89	0.89
45.15	213.85	152.90	1.29	197.59	1.98	0.88	0.88
45.20	212.05	151.41	1.29	195.99	1.98	0.88	0.88
45.25	210.12	149.82	1.30	194.28	1.99	0.88	0.88
45.30	208.04	148.13	1.30	192.46	1.99	0.88	0.88
45.35	206.23	146.62	1.30	190.94	1.99	0.88	0.88
45.40	204.69	145.30	1.31	189.71	2.00	0.88	0.88
45.45	203.43	144.18	1.31	188.79	2.00	0.87	0.87
45.50	202.70	143.47	1.31	188.21	2.01	0.87	0.87
45.55	202.59	143.27	1.31	187.99	2.01	0.87	0.87
45.60	203.21	143.64	1.31	188.19	2.00	0.87	0.87

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
45.65	204.10	144.23	1.31	188.55	2.00	0.87	0.87
45.70	204.99	144.82	1.31	189.00	2.00	0.87	0.87
45.75	205.81	145.33	1.30	189.43	2.00	0.88	0.88
45.80	206.70	145.89	1.30	189.91	1.99	0.88	0.88
45.85	207.49	146.44	1.30	190.12	1.99	0.88	0.88
45.90	208.14	146.95	1.29	189.95	1.98	0.88	0.88
45.95	208.40	147.27	1.28	189.18	1.97	0.87	0.87
46.00	208.46	147.51	1.27	188.06	1.96	0.87	0.87
46.05	208.14	147.56	1.26	186.44	1.94	0.87	0.87
46.10	207.68	147.52	1.25	184.66	1.92	0.87	0.87
46.15	207.15	147.51	1.24	182.64	1.90	0.87	0.87
46.20	207.36	148.01	1.22	181.28	1.88	0.87	0.87
46.25	208.33	149.06	1.21	180.46	1.86	0.87	0.87
46.30	210.67	151.03	1.20	180.98	1.85	0.87	0.87
46.35	213.60	153.39	1.19	181.99	1.83	0.87	0.87
46.40	217.34	156.32	1.17	183.58	1.82	0.87	0.87
46.45	220.91	159.14	1.16	184.76	1.81	0.87	0.87
46.50	224.61	162.13	1.14	185.42	1.79	0.87	0.87
46.55	227.82	164.78	1.12	185.18	1.78	0.87	0.87
46.60	230.78	167.27	1.10	184.06	1.76	0.87	0.87
46.65	232.99	169.16	1.08	182.33	1.75	0.87	0.87
46.70	234.26	170.31	1.06	179.97	1.73	0.86	0.86
46.75	234.70	170.85	1.03	176.65	1.72	0.86	0.86
46.80	234.70	171.09	1.01	172.39	1.71	0.86	0.86
46.85	234.70	171.39	1.00	171.39	1.70	0.85	0.85
46.90	234.57	171.59	1.00	171.59	1.68	0.85	0.85
46.95	233.63	171.17	1.00	171.17	1.67	0.85	0.85
47.00	231.40	169.71	1.00	169.71	1.66	0.85	0.85
47.05	227.32	166.66	1.00	166.66	1.65	0.85	0.85
47.10	221.14	161.73	1.00	161.73	1.66	0.84	0.84
47.15	213.26	155.25	1.00	155.25	1.68	0.83	0.83
47.20	204.49	147.97	1.02	150.23	1.71	0.83	0.83
47.25	195.41	140.45	1.08	151.39	1.75	0.83	0.83
47.30	186.26	132.87	1.13	150.49	1.78	0.83	0.83
47.35	175.48	123.85	1.19	147.35	1.84	0.82	0.82
47.40	163.92	114.23	1.24	141.44	1.90	0.82	0.82
47.45	150.98	103.60	1.29	133.84	1.98	0.80	0.80
47.50	138.23	93.33	1.37	127.72	2.06	0.79	0.79
47.55	125.91	83.54	1.50	125.29	2.15	0.79	0.79
47.60	114.57	74.65	1.71	127.91	2.24	0.80	0.80
47.65	106.12	68.01	1.99	135.18	2.32	0.81	0.81
47.70	100.59	63.55	2.30	146.32	2.39	0.82	0.82
47.75	98.14	61.38	2.57	157.93	2.44	0.84	0.84
47.80	96.75	59.98	2.84	170.33	2.48	0.85	0.85
47.85	95.75	58.96	3.06	180.27	2.51	0.86	0.86
47.90	95.51	58.52	3.22	188.60	2.53	0.89	0.89
47.95	97.24	59.53	3.24	192.99	2.54	0.90	0.90
48.00	100.39	61.57	3.16	194.79	2.53	0.89	0.89

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
48.05	104.45	64.31	3.00	193.12	2.50	0.87	0.87
48.10	106.59	65.79	2.89	190.05	2.49	0.88	0.88
48.15	106.99	66.10	2.82	186.27	2.48	0.87	0.87
48.20	104.22	64.19	2.87	184.38	2.48	0.87	0.87
48.25	100.01	61.25	3.01	184.19	2.50	0.86	0.86
48.30	93.91	56.98	3.27	186.32	2.54	0.90	0.90
48.35	87.69	52.66	3.60	189.36	2.58	0.94	0.94
48.40	81.23	48.17	4.03	194.16	2.63	0.99	0.99
48.45	76.48	44.84	4.47	200.28	2.68	1.04	1.04
48.50	73.37	42.61	4.88	207.76	2.72	0.90	0.90
48.55	72.59	41.95	5.09	213.46	2.74	0.90	0.90
48.60	73.49	42.43	5.11	216.91	2.74	0.90	0.90
48.65	76.28	44.22	4.87	215.57	2.72	0.90	0.90
48.70	81.36	47.58	4.45	211.56	2.67	1.06	1.06
48.75	88.11	52.18	3.88	202.68	2.62	0.99	0.99
48.80	96.50	57.97	3.31	191.96	2.55	0.91	0.91
48.85	104.19	63.46	2.82	178.92	2.48	0.86	0.86
48.90	110.71	68.23	2.45	167.17	2.41	0.85	0.85
48.95	113.99	70.82	2.22	157.06	2.37	0.84	0.84
49.00	114.88	71.66	2.09	150.09	2.34	0.83	0.83
49.05	113.12	70.53	2.08	146.41	2.34	0.82	0.82
49.10	110.32	68.53	2.13	145.75	2.35	0.82	0.82
49.15	106.45	65.67	2.26	148.28	2.38	0.82	0.82
49.20	102.97	63.02	2.43	153.06	2.41	0.83	0.83
49.25	99.99	60.66	2.65	160.67	2.45	0.84	0.84
49.30	98.58	59.41	2.83	168.36	2.48	0.85	0.85
49.35	98.15	58.85	2.98	175.16	2.50	0.86	0.86
49.40	98.96	59.27	2.99	177.28	2.50	0.85	0.85
49.45	100.29	60.15	2.92	175.55	2.49	0.86	0.86
49.50	102.24	61.57	2.76	169.89	2.47	0.85	0.85
49.55	103.75	62.76	2.60	162.96	2.44	0.84	0.84
49.60	104.70	63.62	2.44	154.97	2.41	0.83	0.83
49.65	105.55	64.37	2.32	149.05	2.39	0.83	0.83
49.70	106.91	65.36	2.23	146.04	2.37	0.82	0.82
49.75	109.29	66.93	2.18	146.21	2.36	0.82	0.82
49.80	110.81	67.91	2.15	146.33	2.36	0.82	0.82
49.85	110.25	67.58	2.13	143.64	2.35	0.82	0.82
49.90	108.66	66.55	2.11	140.65	2.35	0.81	0.81

Abbreviations

q_t :	Total cone resistance
K_c :	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c :	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

LIQUEFACTION ANALYSIS REPORT

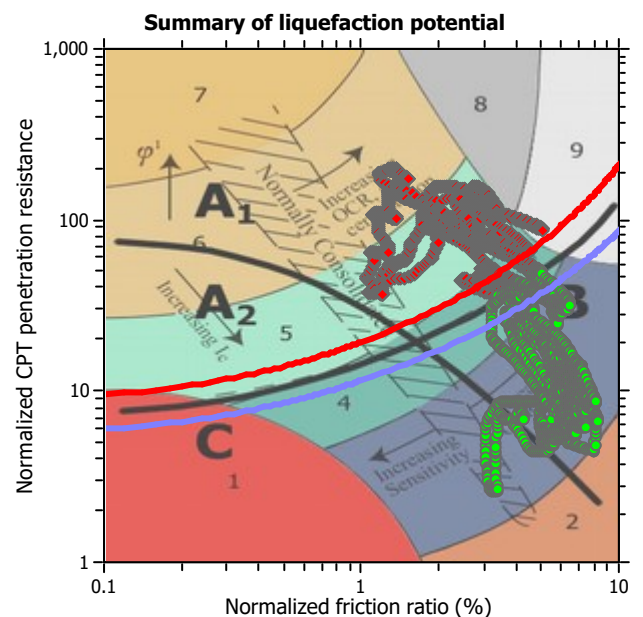
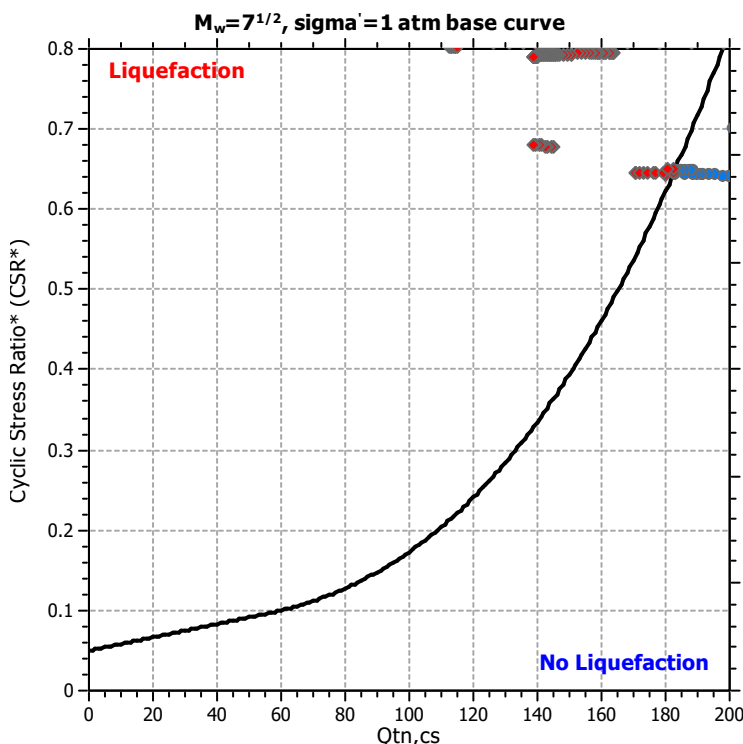
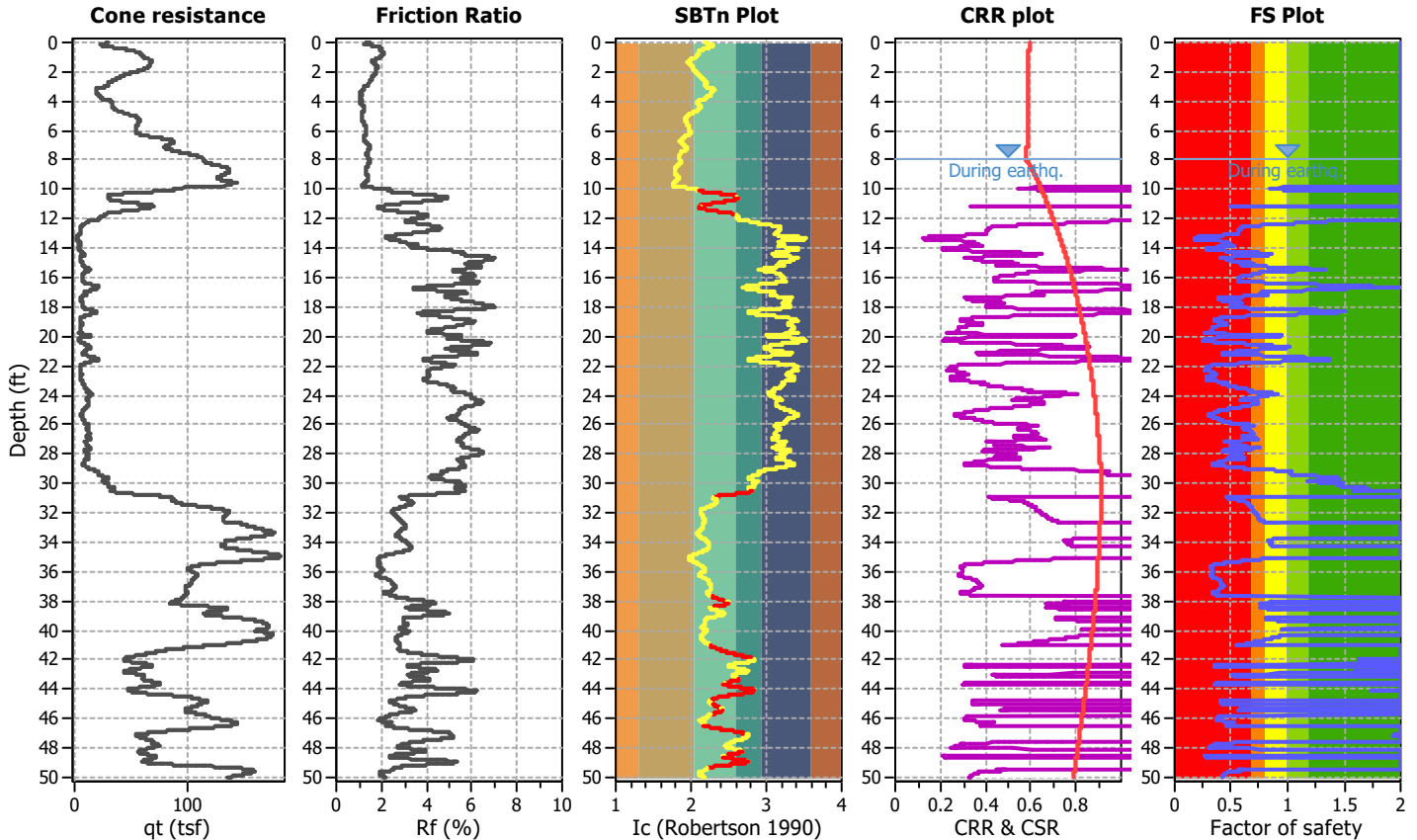
Project title : 21-483 Equestrian Estates

Location : Avenue 64 at Harrison Street, Thermal California

CPT file : CPT-2 Robt 2009

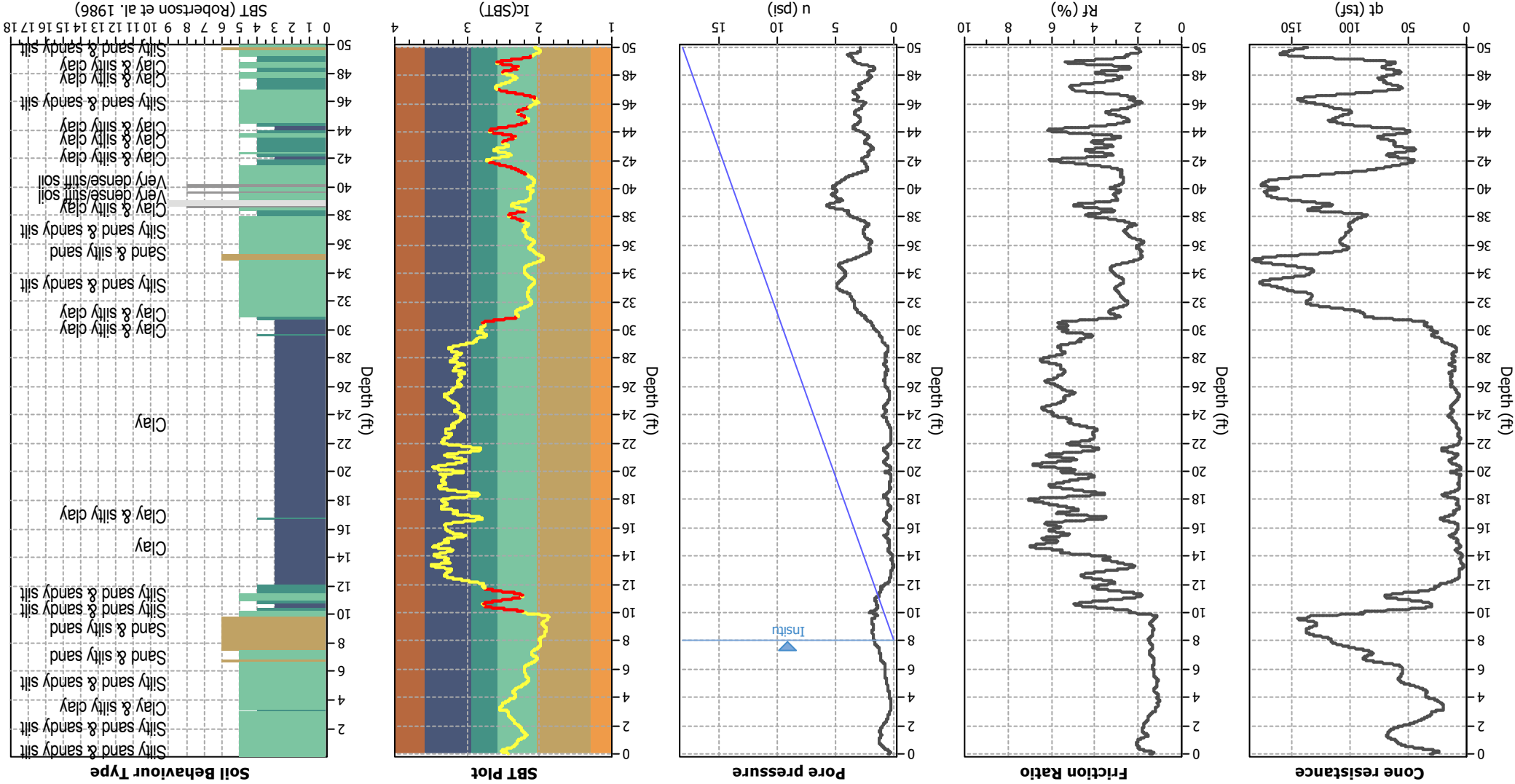
Input parameters and analysis data

Analysis method:	Robertson (2009)	G.W.T. (in-situ):	8.00 ft	Use fill:	No	Clay like behavior	
Fines correction method:	Robertson (2009)	G.W.T. (earthq.):	8.00 ft	Fill height:	N/A	applied:	All soils
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude M_w :	7.34	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	N/A
Peak ground acceleration:	0.74	Unit weight calculation:	Based on SBT	K_o applied:	No		Method based



Zone A₁: Cyclic liquefaction likely depending on size and duration of cyclic loading
 Zone A₂: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
 Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
 Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



Input parameters and analysis data

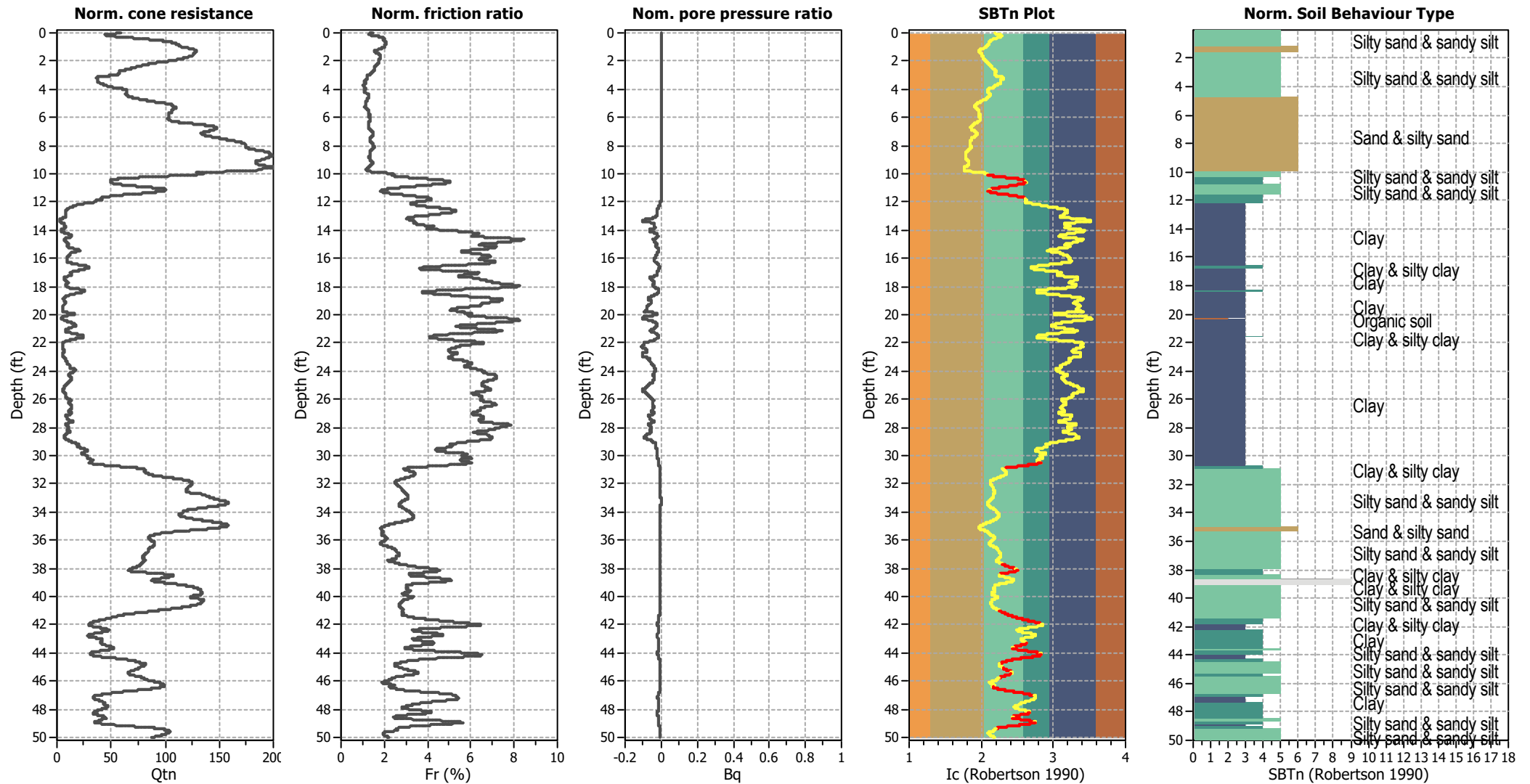
Analysis method: Robertson (2009)
Fines correction method: Robertson (2009)
Points to test: Based on Ic value
Earthquake magnitude M_w : 7.34
Peak ground acceleration: 0.74
Depth to water table (insitu): 8.00 ft

Fill height: N/A
Use fill: No
Unit weight calculation: Based on SBT
Ic cut-off value: 2.60
Average results interval: 3
Depth to water table (earthq.): 8.00 ft
Fill weight: N/A
Transition detect. applied: Yes
 K_g applied: No
Clay like behavior applied: All soils
Limit depth applied: No
Limit depth: N/A

SBT legend

- 1. Sensitive fine grained
- 2. Organic material
- 3. Clay to silty clay
- 4. Clayey silt to silty
- 5. Silty sand to sandy silt
- 6. Clean sand to silty sand
- 7. Gravely sand to sand
- 8. Very stiff sand to
- 9. Very stiff fine grained

CPT basic interpretation plots (normalized)



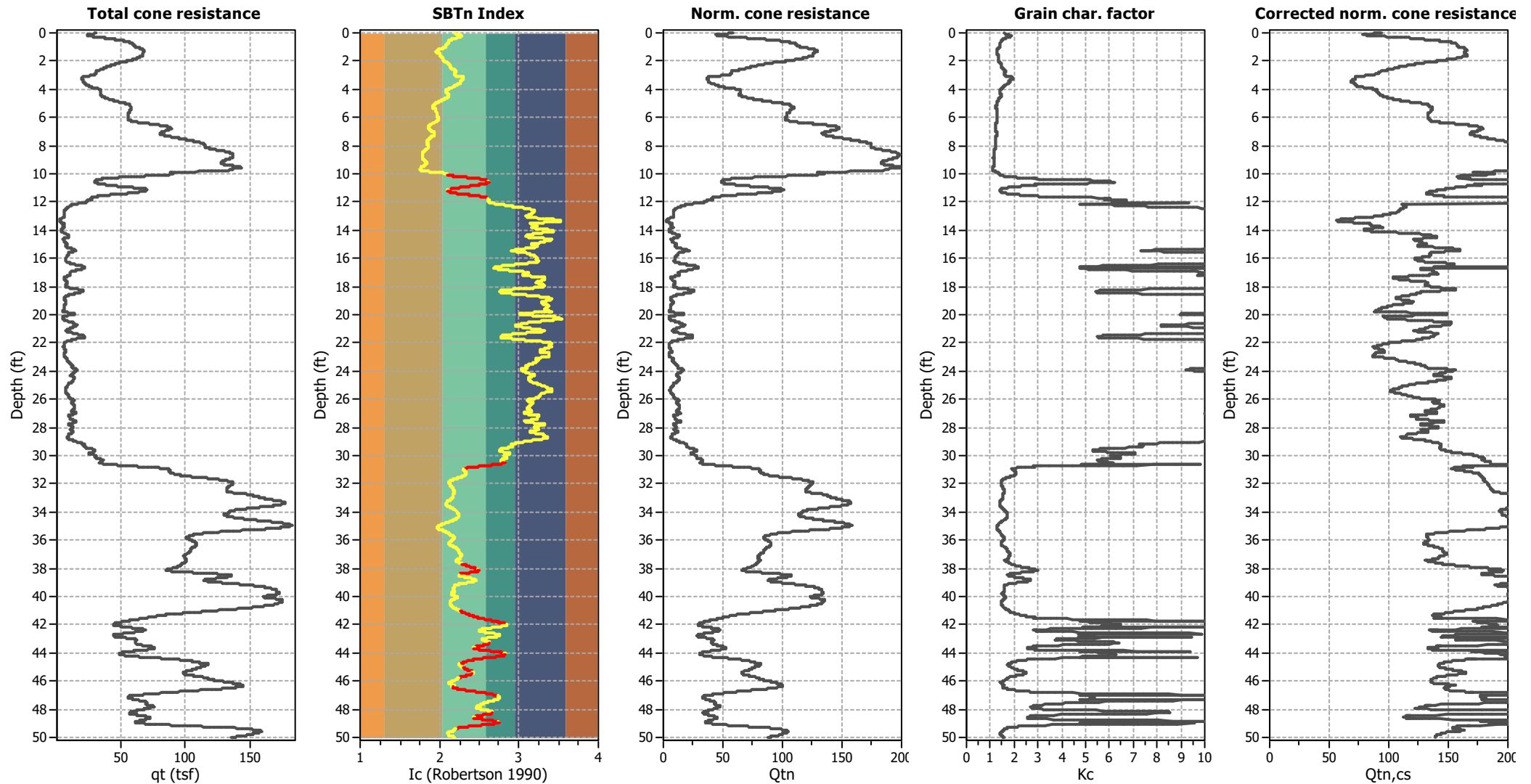
Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	No
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

SBTn legend

1. Sensitive fine grained	4. Clayey silt to silty	7. Gravely sand to sand
2. Organic material	5. Silty sand to sandy silt	8. Very stiff sand to
3. Clay to silty clay	6. Clean sand to silty sand	9. Very stiff fine grained

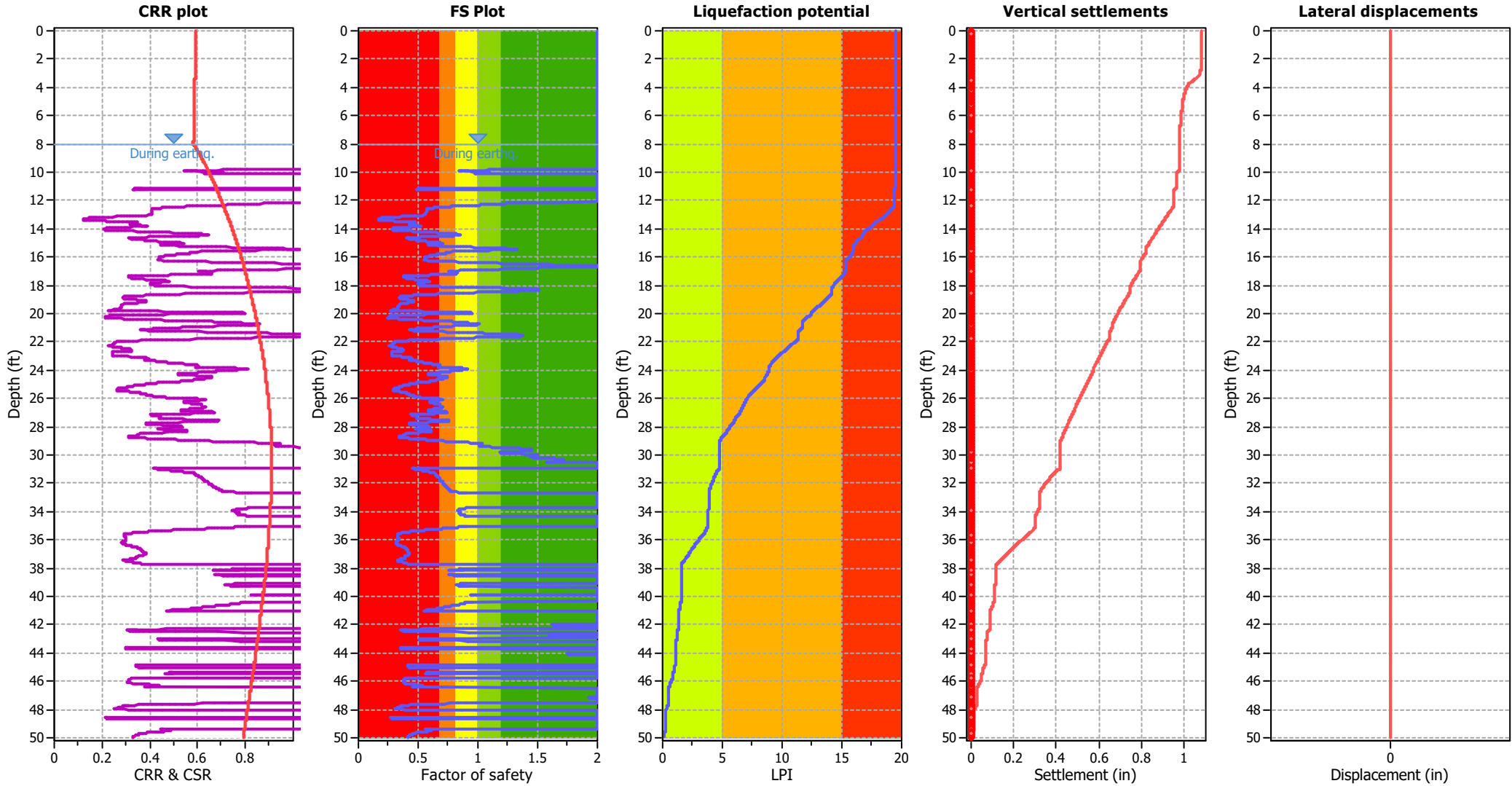
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	No
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (earthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	No
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

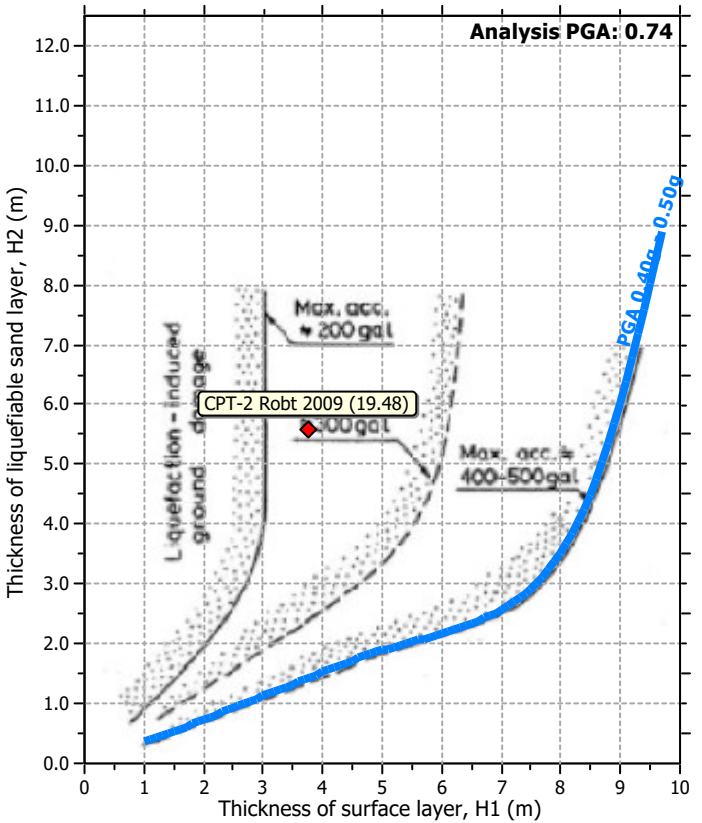
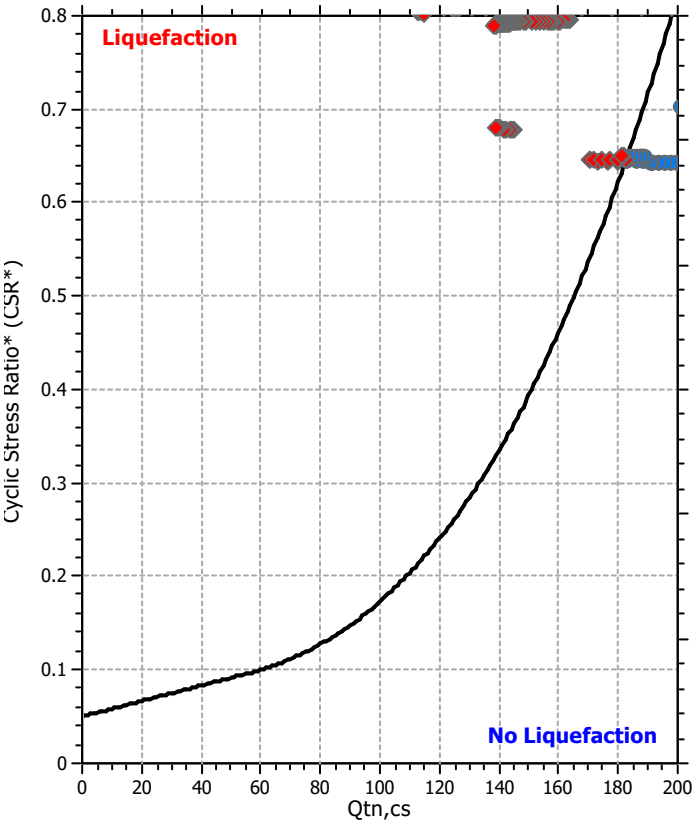
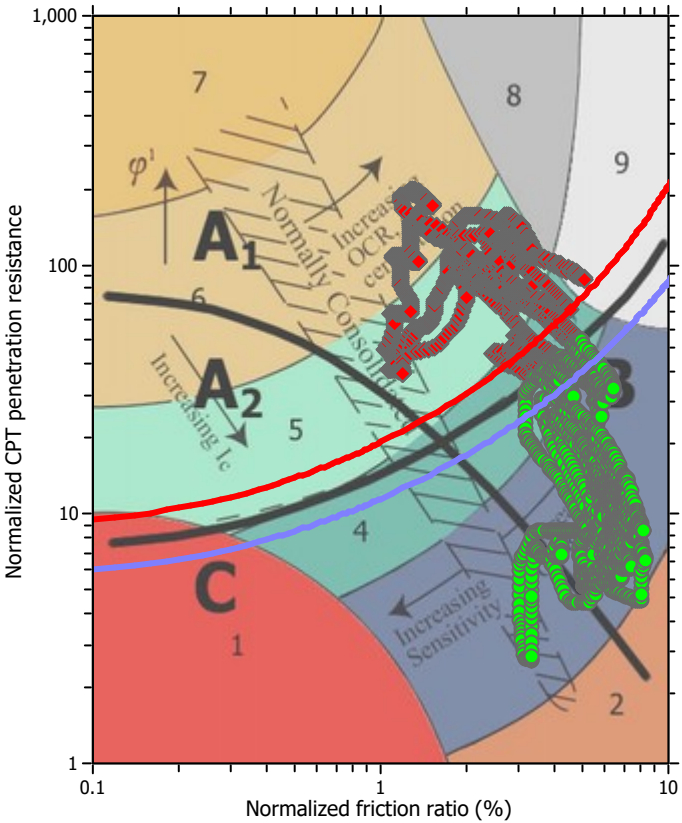
F.S. color scheme

Red	Almost certain it will liquefy
Orange	Very likely to liquefy
Yellow	Liquefaction and no liq. are equally likely
Green	Unlike to liquefy
Dark Green	Almost certain it will not liquefy

LPI color scheme

Red	Very high risk
Orange	High risk
Green	Low risk

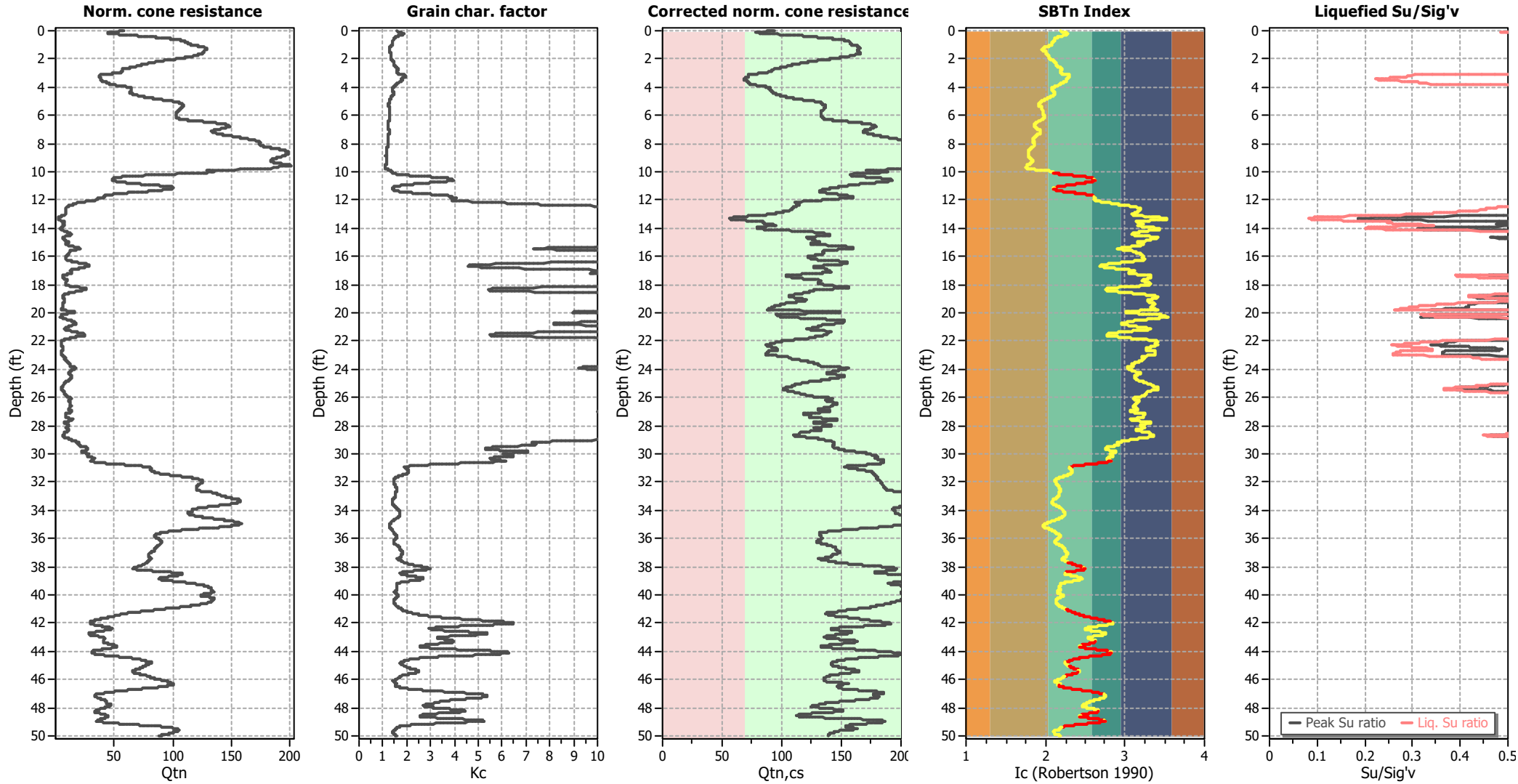
Liquefaction analysis summary plots



Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on I_c value	I_c cut-off value:	2.60	K_o applied:	No
Earthquake magnitude M_w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

Check for strength loss plots (Robertson (2010))



Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	No
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

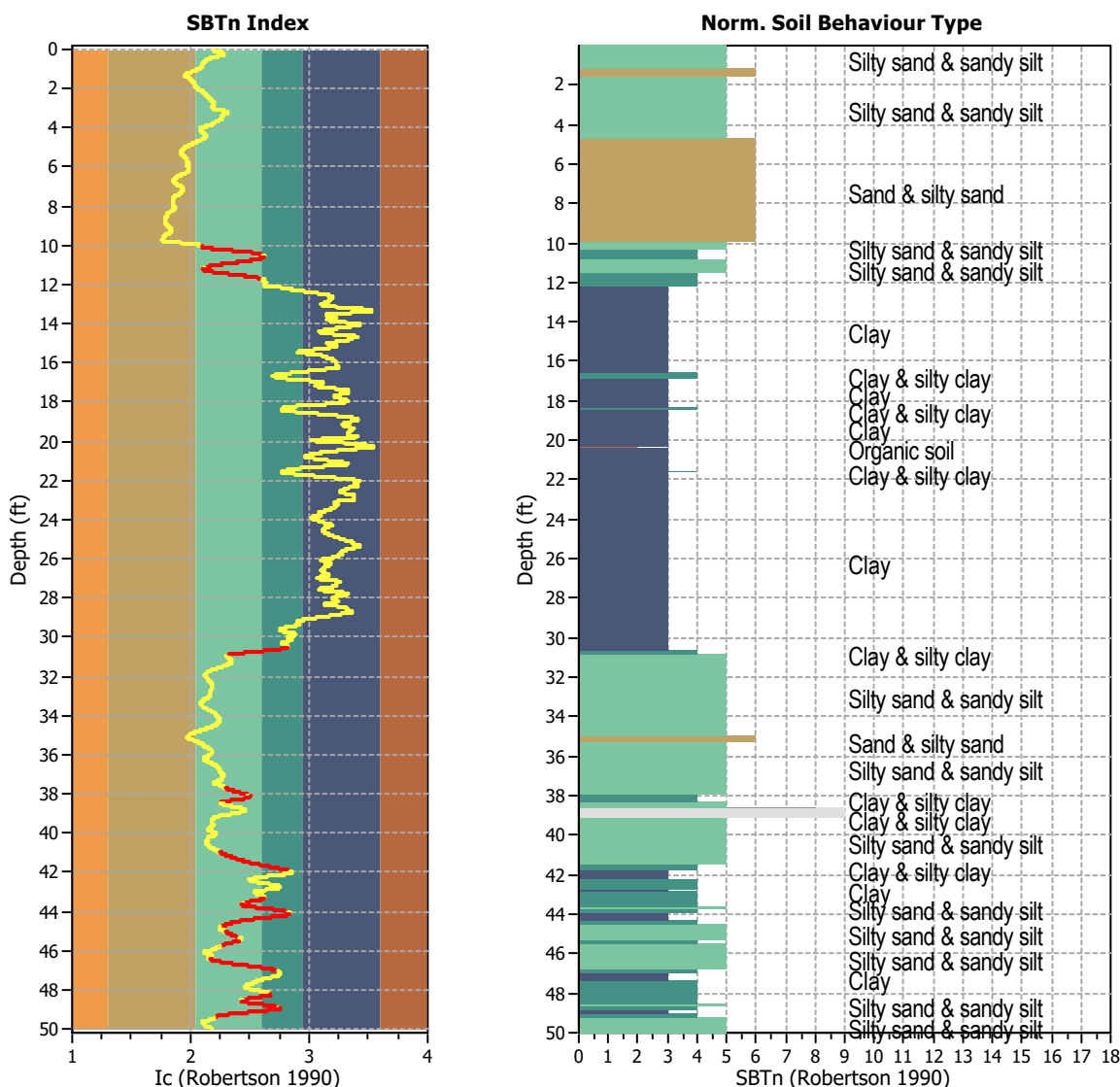
TRANSITION LAYER DETECTION ALGORITHM REPORT

Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vice-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between $1.80 < I_c < 3.0$) and a rate of change of I_c . Transitions typically occur when the rate of change of I_c is fast (i.e. ΔI_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties

I_c minimum check value: 1.70
 I_c maximum check value: 3.00
 I_c change ratio value: 0.0250
 Minimum number of points in layer: 4

General statistics

Total points in CPT file: 5000
 Total points excluded: 701
 Exclusion percentage: 14.02%
 Number of layers detected: 16

Transition layer No	Number of points	Depth	SBT _n number	SBT _n description
Transition layer 1	44	Start depth: 10.08 (ft)	5	Silty sand & sandy silt
		End depth: 10.51 (ft)	4	Clay & silty clay
Transition layer 2	52	Start depth: 10.62 (ft)	4	Clay & silty clay
		End depth: 11.13 (ft)	5	Silty sand & sandy silt
Transition layer 3	52	Start depth: 11.22 (ft)	5	Silty sand & sandy silt
		End depth: 11.73 (ft)	4	Clay & silty clay
Transition layer 4	43	Start depth: 30.53 (ft)	3	Clay
		End depth: 30.95 (ft)	5	Silty sand & sandy silt
Transition layer 5	36	Start depth: 37.71 (ft)	5	Silty sand & sandy silt
		End depth: 38.06 (ft)	4	Clay & silty clay
Transition layer 6	33	Start depth: 38.15 (ft)	4	Clay & silty clay
		End depth: 38.47 (ft)	5	Silty sand & sandy silt
Transition layer 7	94	Start depth: 41.02 (ft)	5	Silty sand & sandy silt
		End depth: 41.95 (ft)	3	Clay
Transition layer 8	27	Start depth: 43.34 (ft)	4	Clay & silty clay
		End depth: 43.60 (ft)	5	Silty sand & sandy silt
Transition layer 9	37	Start depth: 43.68 (ft)	5	Silty sand & sandy silt
		End depth: 44.04 (ft)	3	Clay
Transition layer 10	68	Start depth: 44.13 (ft)	3	Clay
		End depth: 44.80 (ft)	5	Silty sand & sandy silt
Transition layer 11	26	Start depth: 45.08 (ft)	5	Silty sand & sandy silt
		End depth: 45.33 (ft)	4	Clay & silty clay
Transition layer 12	27	Start depth: 45.50 (ft)	4	Clay & silty clay
		End depth: 45.76 (ft)	5	Silty sand & sandy silt
Transition layer 13	62	Start depth: 46.45 (ft)	5	Silty sand & sandy silt
		End depth: 47.06 (ft)	3	Clay
Transition layer 14	27	Start depth: 48.27 (ft)	4	Clay & silty clay
		End depth: 48.53 (ft)	5	Silty sand & sandy silt
Transition layer 15	28	Start depth: 48.62 (ft)	5	Silty sand & sandy silt
		End depth: 48.89 (ft)	3	Clay
Transition layer 16	45	Start depth: 48.96 (ft)	3	Clay
		End depth: 49.40 (ft)	5	Silty sand & sandy silt

Start depth: Depth where the transition layer begins

End depth: Depth where the transition layer ends

:: Field input data ::						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1	0.01	30.99	0.46	0.46	18.92	112.89
2	0.02	30.73	0.45	0.45	18.82	112.72
3	0.03	30.50	0.43	0.43	18.69	112.47
4	0.04	30.31	0.42	0.42	18.63	112.24
5	0.05	29.88	0.41	0.41	18.67	111.99
6	0.06	29.16	0.40	0.40	18.82	111.69
7	0.07	28.32	0.38	0.38	19.04	111.32
8	0.08	27.40	0.36	0.36	19.30	110.90
9	0.09	26.45	0.34	0.34	19.58	110.46
10	0.10	25.52	0.33	0.33	19.87	110.01
11	0.11	24.65	0.31	0.31	20.16	109.58
12	0.12	23.89	0.30	0.30	20.43	109.19
13	0.13	23.29	0.29	0.29	20.65	109.03
14	0.14	23.42	0.30	0.30	20.83	109.09
15	0.15	23.58	0.31	0.31	20.99	109.35
16	0.16	23.76	0.32	0.32	21.18	109.65
17	0.17	23.96	0.33	0.33	21.37	109.96
18	0.18	24.16	0.35	0.35	21.56	110.26
19	0.19	24.35	0.36	0.36	21.74	110.55
20	0.20	24.53	0.37	0.37	21.91	110.81
21	0.21	24.68	0.38	0.38	22.02	111.04
22	0.22	24.93	0.39	0.39	22.03	111.32
23	0.23	25.55	0.41	0.41	21.95	111.66
24	0.24	26.30	0.43	0.43	21.81	112.10
25	0.25	27.14	0.45	0.45	21.67	112.57
26	0.26	28.02	0.48	0.48	21.53	113.05
27	0.27	28.90	0.51	0.51	21.40	113.51
28	0.28	29.73	0.53	0.53	21.28	113.94
29	0.29	30.48	0.56	0.56	21.19	114.32
30	0.30	31.09	0.58	0.58	21.09	114.62
31	0.31	31.65	0.59	0.59	20.95	114.89
32	0.32	32.38	0.61	0.61	20.77	115.16
33	0.33	33.24	0.63	0.63	20.55	115.47
34	0.34	34.18	0.65	0.65	20.32	115.79
35	0.35	35.15	0.68	0.68	20.10	116.12
36	0.36	36.10	0.70	0.70	19.89	116.43
37	0.37	36.98	0.73	0.73	19.70	116.72
38	0.38	37.75	0.75	0.75	19.54	116.96
39	0.39	38.36	0.76	0.76	19.39	117.16
40	0.40	38.98	0.77	0.77	19.21	117.33
41	0.41	39.75	0.79	0.79	19.00	117.51
42	0.42	40.64	0.80	0.80	18.76	117.71
43	0.43	41.58	0.82	0.82	18.51	117.92
44	0.44	42.54	0.84	0.84	18.26	118.12
45	0.45	43.47	0.86	0.86	18.03	118.32
46	0.46	44.32	0.87	0.87	17.82	118.49
47	0.47	45.03	0.88	0.88	17.66	118.64
48	0.48	45.57	0.89	0.89	17.53	118.78

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
49	0.49	46.14	0.91	0.91	17.42	118.92
50	0.50	46.83	0.92	0.92	17.30	119.08
51	0.51	47.61	0.94	0.94	17.17	119.26
52	0.52	48.42	0.96	0.96	17.04	119.44
53	0.53	49.22	0.98	0.98	16.92	119.62
54	0.54	49.99	1.00	1.00	16.80	119.79
55	0.55	50.67	1.01	1.01	16.70	119.94
56	0.56	51.23	1.03	1.03	16.62	120.06
57	0.57	51.63	1.04	1.04	16.56	120.17
58	0.58	52.08	1.05	1.05	16.51	120.29
59	0.59	52.61	1.07	1.07	16.46	120.41
60	0.60	53.19	1.08	1.08	16.41	120.55
61	0.61	53.79	1.10	1.10	16.35	120.69
62	0.62	54.37	1.12	1.12	16.29	120.83
63	0.63	54.92	1.13	1.13	16.24	120.95
64	0.64	55.39	1.15	1.15	16.20	121.06
65	0.65	55.75	1.16	1.16	16.17	121.14
66	0.66	55.95	1.16	1.16	16.14	121.20
67	0.67	56.19	1.17	1.17	16.12	121.25
68	0.68	56.46	1.18	1.18	16.09	121.31
69	0.69	56.76	1.19	1.19	16.05	121.37
70	0.70	57.06	1.19	1.19	16.02	121.43
71	0.71	57.34	1.20	1.20	15.99	121.49
72	0.72	57.61	1.21	1.21	15.96	121.54
73	0.73	57.83	1.21	1.21	15.94	121.58
74	0.74	57.97	1.22	1.22	15.92	121.61
75	0.75	58.06	1.22	1.22	15.89	121.62
76	0.76	58.18	1.22	1.22	15.86	121.63
77	0.77	58.31	1.22	1.22	15.83	121.64
78	0.78	58.44	1.22	1.22	15.80	121.65
79	0.79	58.58	1.22	1.22	15.76	121.66
80	0.80	58.70	1.22	1.22	15.73	121.67
81	0.81	58.82	1.22	1.22	15.70	121.68
82	0.82	58.91	1.22	1.22	15.67	121.69
83	0.83	58.98	1.22	1.22	15.65	121.69
84	0.84	59.06	1.22	1.22	15.61	121.69
85	0.85	59.16	1.22	1.22	15.57	121.68
86	0.86	59.26	1.22	1.22	15.53	121.68
87	0.87	59.37	1.22	1.22	15.49	121.68
88	0.88	59.48	1.22	1.22	15.44	121.67
89	0.89	59.58	1.21	1.21	15.40	121.67
90	0.90	59.66	1.21	1.21	15.37	121.66
91	0.91	59.73	1.21	1.21	15.33	121.66
92	0.92	59.84	1.21	1.21	15.30	121.66
93	0.93	59.97	1.21	1.21	15.25	121.66
94	0.94	60.12	1.21	1.21	15.21	121.67
95	0.95	60.28	1.21	1.21	15.15	121.67
96	0.96	60.45	1.21	1.21	15.10	121.67

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
97	0.97	60.60	1.21	1.21	15.05	121.68
98	0.98	60.75	1.21	1.21	15.01	121.68
99	0.99	60.87	1.21	1.21	14.96	121.68
100	1.00	61.03	1.21	1.21	14.91	121.69
101	1.01	61.33	1.21	1.21	14.83	121.70
102	1.02	61.69	1.21	1.21	14.73	121.72
103	1.03	62.09	1.21	1.21	14.62	121.74
104	1.04	62.51	1.21	1.21	14.50	121.75
105	1.05	62.93	1.21	1.21	14.39	121.77
106	1.06	63.33	1.21	1.21	14.28	121.79
107	1.07	63.68	1.21	1.21	14.18	121.80
108	1.08	63.97	1.21	1.21	14.10	121.81
109	1.09	64.20	1.21	1.21	14.01	121.80
110	1.10	64.48	1.20	1.20	13.91	121.79
111	1.11	64.81	1.20	1.20	13.79	121.77
112	1.12	65.16	1.19	1.19	13.65	121.75
113	1.13	65.53	1.19	1.19	13.52	121.73
114	1.14	65.89	1.18	1.18	13.38	121.71
115	1.15	66.22	1.18	1.18	13.26	121.69
116	1.16	66.51	1.17	1.17	13.15	121.67
117	1.17	66.73	1.17	1.17	13.06	121.64
118	1.18	66.88	1.16	1.16	12.96	121.61
119	1.19	67.06	1.15	1.15	12.85	121.56
120	1.20	67.27	1.14	1.14	12.73	121.50
121	1.21	67.50	1.13	1.13	12.59	121.44
122	1.22	67.73	1.12	1.12	12.46	121.37
123	1.23	67.95	1.11	1.11	12.33	121.31
124	1.24	68.14	1.10	1.10	12.21	121.25
125	1.25	68.31	1.09	1.09	12.11	121.21
126	1.26	68.39	1.08	1.08	12.05	121.17
127	1.27	68.40	1.08	1.08	12.02	121.15
128	1.28	68.41	1.08	1.08	11.99	121.13
129	1.29	68.43	1.07	1.07	11.95	121.10
130	1.30	68.44	1.07	1.07	11.92	121.07
131	1.31	68.45	1.07	1.07	11.89	121.04
132	1.32	68.46	1.06	1.06	11.86	121.02
133	1.33	68.48	1.06	1.06	11.83	121.00
134	1.34	68.49	1.06	1.06	11.82	120.99
135	1.35	68.38	1.06	1.06	11.85	120.99
136	1.36	68.21	1.06	1.06	11.92	121.01
137	1.37	68.02	1.07	1.07	12.00	121.04
138	1.38	67.81	1.07	1.07	12.08	121.06
139	1.39	67.59	1.08	1.08	12.17	121.09
140	1.40	67.38	1.08	1.08	12.26	121.11
141	1.41	67.18	1.09	1.09	12.34	121.14
142	1.42	67.01	1.09	1.09	12.41	121.16
143	1.43	66.89	1.09	1.09	12.47	121.18
144	1.44	66.88	1.10	1.10	12.52	121.22

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
145	1.45	66.87	1.11	1.11	12.57	121.26
146	1.46	66.86	1.11	1.11	12.63	121.31
147	1.47	66.85	1.12	1.12	12.70	121.36
148	1.48	66.83	1.13	1.13	12.76	121.41
149	1.49	66.82	1.14	1.14	12.82	121.46
150	1.50	66.81	1.14	1.14	12.88	121.51
151	1.51	66.80	1.15	1.15	12.92	121.55
152	1.52	66.79	1.16	1.16	12.96	121.58
153	1.53	66.77	1.16	1.16	13.00	121.60
154	1.54	66.74	1.16	1.16	13.04	121.63
155	1.55	66.72	1.17	1.17	13.09	121.67
156	1.56	66.69	1.18	1.18	13.14	121.70
157	1.57	66.66	1.18	1.18	13.19	121.74
158	1.58	66.64	1.19	1.19	13.24	121.77
159	1.59	66.62	1.19	1.19	13.28	121.80
160	1.60	66.60	1.20	1.20	13.31	121.81
161	1.61	66.47	1.20	1.20	13.34	121.81
162	1.62	66.28	1.19	1.19	13.38	121.80
163	1.63	66.07	1.19	1.19	13.42	121.78
164	1.64	65.83	1.19	1.19	13.46	121.75
165	1.65	65.58	1.19	1.19	13.51	121.73
166	1.66	65.34	1.18	1.18	13.55	121.71
167	1.67	65.12	1.18	1.18	13.59	121.69
168	1.68	64.93	1.18	1.18	13.63	121.67
169	1.69	64.78	1.18	1.18	13.66	121.65
170	1.70	64.62	1.18	1.18	13.68	121.63
171	1.71	64.42	1.17	1.17	13.71	121.60
172	1.72	64.19	1.17	1.17	13.74	121.56
173	1.73	63.95	1.16	1.16	13.77	121.53
174	1.74	63.71	1.16	1.16	13.80	121.49
175	1.75	63.47	1.16	1.16	13.83	121.45
176	1.76	63.26	1.15	1.15	13.86	121.42
177	1.77	63.09	1.15	1.15	13.88	121.39
178	1.78	62.92	1.14	1.14	13.89	121.35
179	1.79	62.68	1.14	1.14	13.91	121.30
180	1.80	62.39	1.13	1.13	13.92	121.23
181	1.81	62.07	1.12	1.12	13.93	121.16
182	1.82	61.74	1.11	1.11	13.94	121.09
183	1.83	61.42	1.10	1.10	13.96	121.01
184	1.84	61.11	1.09	1.09	13.97	120.94
185	1.85	60.83	1.08	1.08	13.98	120.87
186	1.86	60.61	1.08	1.08	14.00	120.81
187	1.87	60.36	1.07	1.07	14.01	120.75
188	1.88	60.02	1.06	1.06	14.04	120.68
189	1.89	59.63	1.05	1.05	14.06	120.59
190	1.90	59.20	1.04	1.04	14.09	120.50
191	1.91	58.77	1.03	1.03	14.12	120.40
192	1.92	58.35	1.02	1.02	14.15	120.31

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
193	1.93	57.96	1.01	1.01	14.18	120.22
194	1.94	57.62	1.00	1.00	14.21	120.14
195	1.95	57.35	0.99	0.99	14.25	120.08
196	1.96	57.00	0.98	0.98	14.29	120.01
197	1.97	56.56	0.98	0.98	14.36	119.94
198	1.98	56.08	0.97	0.97	14.43	119.86
199	1.99	55.56	0.96	0.96	14.51	119.77
200	2.00	55.04	0.95	0.95	14.60	119.68
201	2.01	54.54	0.94	0.94	14.68	119.59
202	2.02	54.08	0.93	0.93	14.75	119.51
203	2.03	53.71	0.93	0.93	14.82	119.44
204	2.04	53.37	0.92	0.92	14.88	119.37
205	2.05	52.91	0.91	0.91	14.96	119.29
206	2.06	52.37	0.90	0.90	15.05	119.19
207	2.07	51.77	0.89	0.89	15.15	119.08
208	2.08	51.15	0.88	0.88	15.26	118.96
209	2.09	50.53	0.87	0.87	15.37	118.85
210	2.10	49.95	0.86	0.86	15.48	118.74
211	2.11	49.44	0.85	0.85	15.57	118.64
212	2.12	49.03	0.85	0.85	15.65	118.55
213	2.13	48.72	0.84	0.84	15.70	118.47
214	2.14	48.34	0.83	0.83	15.75	118.37
215	2.15	47.89	0.82	0.82	15.81	118.26
216	2.16	47.42	0.81	0.81	15.87	118.14
217	2.17	46.93	0.80	0.80	15.93	118.01
218	2.18	46.45	0.79	0.79	16.00	117.88
219	2.19	46.01	0.78	0.78	16.06	117.77
220	2.20	45.64	0.77	0.77	16.11	117.67
221	2.21	45.35	0.76	0.76	16.15	117.59
222	2.22	45.10	0.76	0.76	16.19	117.51
223	2.23	44.79	0.75	0.75	16.23	117.42
224	2.24	44.44	0.74	0.74	16.27	117.32
225	2.25	44.07	0.73	0.73	16.32	117.21
226	2.26	43.70	0.72	0.72	16.37	117.10
227	2.27	43.34	0.71	0.71	16.41	116.99
228	2.28	43.02	0.71	0.71	16.46	116.90
229	2.29	42.75	0.70	0.70	16.49	116.82
230	2.30	42.54	0.69	0.69	16.53	116.74
231	2.31	42.29	0.69	0.69	16.56	116.66
232	2.32	41.99	0.68	0.68	16.60	116.57
233	2.33	41.66	0.67	0.67	16.64	116.47
234	2.34	41.32	0.66	0.66	16.69	116.36
235	2.35	40.98	0.66	0.66	16.74	116.26
236	2.36	40.67	0.65	0.65	16.78	116.15
237	2.37	40.39	0.64	0.64	16.82	116.07
238	2.38	40.16	0.64	0.64	16.85	115.99
239	2.39	39.99	0.63	0.63	16.88	115.92
240	2.40	39.77	0.63	0.63	16.91	115.84

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
241	2.41	39.52	0.62	0.62	16.94	115.76
242	2.42	39.25	0.61	0.61	16.97	115.66
243	2.43	38.97	0.61	0.61	17.01	115.57
244	2.44	38.70	0.60	0.60	17.05	115.47
245	2.45	38.45	0.60	0.60	17.08	115.38
246	2.46	38.24	0.59	0.59	17.11	115.31
247	2.47	38.07	0.59	0.59	17.15	115.25
248	2.48	37.89	0.58	0.58	17.19	115.19
249	2.49	37.67	0.58	0.58	17.25	115.14
250	2.50	37.42	0.58	0.58	17.32	115.07
251	2.51	37.15	0.57	0.57	17.40	115.00
252	2.52	36.88	0.57	0.57	17.47	114.94
253	2.53	36.63	0.56	0.56	17.54	114.87
254	2.54	36.40	0.56	0.56	17.61	114.81
255	2.55	36.20	0.56	0.56	17.67	114.75
256	2.56	36.01	0.55	0.55	17.73	114.69
257	2.57	35.74	0.55	0.55	17.79	114.60
258	2.58	35.41	0.54	0.54	17.88	114.50
259	2.59	35.05	0.54	0.54	17.97	114.39
260	2.60	34.68	0.53	0.53	18.06	114.27
261	2.61	34.31	0.52	0.52	18.16	114.16
262	2.62	33.96	0.52	0.52	18.25	114.04
263	2.63	33.65	0.51	0.51	18.33	113.95
264	2.64	33.41	0.51	0.51	18.40	113.86
265	2.65	33.18	0.50	0.50	18.46	113.77
266	2.66	32.89	0.50	0.50	18.53	113.66
267	2.67	32.56	0.49	0.49	18.61	113.53
268	2.68	32.20	0.48	0.48	18.69	113.40
269	2.69	31.84	0.47	0.47	18.78	113.26
270	2.70	31.48	0.47	0.47	18.87	113.12
271	2.71	31.15	0.46	0.46	18.95	112.99
272	2.72	30.87	0.45	0.45	19.02	112.89
273	2.73	30.70	0.45	0.45	19.05	112.81
274	2.74	30.67	0.45	0.45	19.05	112.77
275	2.75	30.65	0.45	0.45	19.03	112.73
276	2.76	30.62	0.45	0.45	19.00	112.69
277	2.77	30.58	0.44	0.44	18.97	112.65
278	2.78	30.55	0.44	0.44	18.95	112.61
279	2.79	30.52	0.44	0.44	18.92	112.57
280	2.80	30.49	0.44	0.44	18.90	112.53
281	2.81	30.47	0.43	0.43	18.88	112.50
282	2.82	30.45	0.43	0.43	18.86	112.48
283	2.83	30.43	0.43	0.43	18.84	112.44
284	2.84	30.41	0.43	0.43	18.81	112.41
285	2.85	30.38	0.43	0.43	18.78	112.37
286	2.86	30.35	0.42	0.42	18.75	112.33
287	2.87	30.33	0.42	0.42	18.72	112.29
288	2.88	30.30	0.42	0.42	18.69	112.25

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
289	2.89	30.28	0.42	0.42	18.67	112.22
290	2.90	30.26	0.42	0.42	18.65	112.17
291	2.91	30.20	0.41	0.41	18.62	112.12
292	2.92	30.11	0.41	0.41	18.59	112.04
293	2.93	30.01	0.40	0.40	18.55	111.95
294	2.94	29.91	0.40	0.40	18.51	111.84
295	2.95	29.80	0.39	0.39	18.47	111.74
296	2.96	29.69	0.39	0.39	18.43	111.64
297	2.97	29.60	0.38	0.38	18.39	111.55
298	2.98	29.51	0.38	0.38	18.37	111.46
299	2.99	29.37	0.38	0.38	18.39	111.33
300	3.00	28.95	0.37	0.37	18.48	111.16
301	3.01	28.42	0.36	0.36	18.61	110.93
302	3.02	27.84	0.35	0.35	18.77	110.66
303	3.03	27.22	0.34	0.34	18.94	110.37
304	3.04	26.60	0.33	0.33	19.12	110.07
305	3.05	26.00	0.32	0.32	19.30	109.79
306	3.06	25.47	0.31	0.31	19.47	109.53
307	3.07	25.03	0.30	0.30	19.64	109.30
308	3.08	24.63	0.29	0.29	19.83	109.10
309	3.09	24.11	0.29	0.29	20.08	108.89
310	3.10	23.49	0.28	0.28	20.40	108.64
311	3.11	22.81	0.27	0.27	20.77	108.36
312	3.12	22.10	0.26	0.26	21.16	108.05
313	3.13	21.41	0.25	0.25	21.57	107.75
314	3.14	20.76	0.25	0.25	21.97	107.45
315	3.15	20.19	0.24	0.24	22.33	107.19
316	3.16	19.73	0.23	0.23	22.57	107.02
317	3.17	19.71	0.23	0.23	22.68	106.94
318	3.18	19.71	0.23	0.23	22.68	106.93
319	3.19	19.71	0.23	0.23	22.68	106.93
320	3.20	19.71	0.23	0.23	22.69	106.93
321	3.21	19.71	0.23	0.23	22.69	106.93
322	3.22	19.71	0.23	0.23	22.69	106.93
323	3.23	19.71	0.23	0.23	22.69	106.93
324	3.24	19.71	0.23	0.23	22.68	106.93
325	3.25	19.72	0.23	0.23	22.64	106.93
326	3.26	19.78	0.23	0.23	22.57	106.92
327	3.27	19.85	0.23	0.23	22.47	106.90
328	3.28	19.92	0.23	0.23	22.35	106.88
329	3.29	20.00	0.23	0.23	22.22	106.86
330	3.30	20.09	0.23	0.23	22.10	106.84
331	3.31	20.16	0.23	0.23	21.98	106.82
332	3.32	20.23	0.23	0.23	21.87	106.80
333	3.33	20.29	0.23	0.23	21.79	106.78
334	3.34	20.31	0.23	0.23	21.72	106.75
335	3.35	20.31	0.23	0.23	21.66	106.71
336	3.36	20.31	0.22	0.22	21.60	106.65

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
337	3.37	20.31	0.22	0.22	21.53	106.59
338	3.38	20.31	0.22	0.22	21.45	106.53
339	3.39	20.31	0.22	0.22	21.38	106.47
340	3.40	20.31	0.22	0.22	21.31	106.41
341	3.41	20.31	0.21	0.21	21.25	106.36
342	3.42	20.31	0.21	0.21	21.22	106.33
343	3.43	20.31	0.21	0.21	21.21	106.33
344	3.44	20.31	0.21	0.21	21.23	106.34
345	3.45	20.31	0.21	0.21	21.26	106.36
346	3.46	20.31	0.22	0.22	21.28	106.38
347	3.47	20.31	0.22	0.22	21.31	106.40
348	3.48	20.31	0.22	0.22	21.33	106.43
349	3.49	20.31	0.22	0.22	21.36	106.44
350	3.50	20.31	0.22	0.22	21.37	106.47
351	3.51	20.34	0.22	0.22	21.37	106.51
352	3.52	20.45	0.22	0.22	21.34	106.58
353	3.53	20.59	0.22	0.22	21.30	106.68
354	3.54	20.74	0.23	0.23	21.25	106.79
355	3.55	20.90	0.23	0.23	21.20	106.91
356	3.56	21.06	0.23	0.23	21.15	107.02
357	3.57	21.22	0.24	0.24	21.10	107.13
358	3.58	21.35	0.24	0.24	21.06	107.23
359	3.59	21.47	0.24	0.24	21.01	107.31
360	3.60	21.60	0.24	0.24	20.92	107.37
361	3.61	21.78	0.24	0.24	20.78	107.42
362	3.62	22.00	0.24	0.24	20.62	107.48
363	3.63	22.23	0.24	0.24	20.44	107.54
364	3.64	22.48	0.25	0.25	20.25	107.60
365	3.65	22.72	0.25	0.25	20.07	107.66
366	3.66	22.94	0.25	0.25	19.91	107.72
367	3.67	23.14	0.25	0.25	19.76	107.77
368	3.68	23.29	0.25	0.25	19.65	107.80
369	3.69	23.40	0.25	0.25	19.55	107.83
370	3.70	23.53	0.25	0.25	19.44	107.84
371	3.71	23.68	0.25	0.25	19.32	107.87
372	3.72	23.84	0.25	0.25	19.19	107.89
373	3.73	24.00	0.25	0.25	19.06	107.91
374	3.74	24.16	0.25	0.25	18.93	107.93
375	3.75	24.30	0.25	0.25	18.82	107.95
376	3.76	24.42	0.25	0.25	18.73	107.97
377	3.77	24.53	0.25	0.25	18.65	108.02
378	3.78	24.70	0.26	0.26	18.60	108.10
379	3.79	24.91	0.26	0.26	18.54	108.22
380	3.80	25.14	0.26	0.26	18.48	108.35
381	3.81	25.38	0.27	0.27	18.42	108.49
382	3.82	25.63	0.27	0.27	18.35	108.62
383	3.83	25.86	0.27	0.27	18.29	108.75
384	3.84	26.06	0.28	0.28	18.24	108.86

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
385	3.85	26.23	0.28	0.28	18.18	108.98
386	3.86	26.53	0.29	0.29	18.07	109.12
387	3.87	27.00	0.29	0.29	17.92	109.31
388	3.88	27.56	0.30	0.30	17.73	109.54
389	3.89	28.16	0.31	0.31	17.53	109.79
390	3.90	28.78	0.32	0.32	17.33	110.04
391	3.91	29.40	0.32	0.32	17.14	110.29
392	3.92	29.97	0.33	0.33	16.97	110.51
393	3.93	30.47	0.34	0.34	16.83	110.70
394	3.94	30.86	0.35	0.35	16.70	110.84
395	3.95	31.16	0.35	0.35	16.58	110.95
396	3.96	31.53	0.35	0.35	16.43	111.05
397	3.97	31.95	0.36	0.36	16.27	111.16
398	3.98	32.40	0.36	0.36	16.10	111.27
399	3.99	32.87	0.36	0.36	15.93	111.39
400	4.00	33.31	0.37	0.37	15.77	111.50
401	4.01	33.72	0.37	0.37	15.62	111.59
402	4.02	34.06	0.37	0.37	15.51	111.67
403	4.03	34.24	0.38	0.38	15.44	111.70
404	4.04	34.24	0.37	0.37	15.41	111.71
405	4.05	34.24	0.37	0.37	15.39	111.69
406	4.06	34.24	0.37	0.37	15.37	111.67
407	4.07	34.24	0.37	0.37	15.35	111.65
408	4.08	34.24	0.37	0.37	15.33	111.63
409	4.09	34.24	0.37	0.37	15.30	111.61
410	4.10	34.24	0.37	0.37	15.29	111.59
411	4.11	34.24	0.37	0.37	15.28	111.58
412	4.12	34.24	0.37	0.37	15.28	111.58
413	4.13	34.24	0.37	0.37	15.29	111.59
414	4.14	34.24	0.37	0.37	15.31	111.61
415	4.15	34.24	0.37	0.37	15.34	111.63
416	4.16	34.24	0.37	0.37	15.36	111.66
417	4.17	34.24	0.37	0.37	15.38	111.68
418	4.18	34.24	0.37	0.37	15.40	111.69
419	4.19	34.24	0.37	0.37	15.42	111.71
420	4.20	34.24	0.38	0.38	15.45	111.74
421	4.21	34.24	0.38	0.38	15.48	111.77
422	4.22	34.24	0.38	0.38	15.54	111.82
423	4.23	34.24	0.38	0.38	15.60	111.88
424	4.24	34.24	0.39	0.39	15.66	111.94
425	4.25	34.24	0.39	0.39	15.73	112.00
426	4.26	34.24	0.39	0.39	15.79	112.06
427	4.27	34.24	0.40	0.40	15.85	112.11
428	4.28	34.24	0.40	0.40	15.90	112.15
429	4.29	34.23	0.40	0.40	15.95	112.19
430	4.30	34.19	0.40	0.40	16.01	112.22
431	4.31	34.15	0.40	0.40	16.08	112.26
432	4.32	34.10	0.41	0.41	16.16	112.30

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
433	4.33	34.04	0.41	0.41	16.24	112.34
434	4.34	33.99	0.41	0.41	16.32	112.38
435	4.35	33.94	0.41	0.41	16.39	112.42
436	4.36	33.89	0.42	0.42	16.46	112.45
437	4.37	33.85	0.42	0.42	16.51	112.48
438	4.38	33.88	0.42	0.42	16.53	112.51
439	4.39	33.93	0.42	0.42	16.53	112.54
440	4.40	33.99	0.42	0.42	16.54	112.57
441	4.41	34.05	0.42	0.42	16.54	112.61
442	4.42	34.12	0.43	0.43	16.54	112.65
443	4.43	34.19	0.43	0.43	16.54	112.68
444	4.44	34.25	0.43	0.43	16.54	112.72
445	4.45	34.30	0.43	0.43	16.54	112.75
446	4.46	34.35	0.43	0.43	16.52	112.78
447	4.47	34.51	0.43	0.43	16.48	112.82
448	4.48	34.71	0.44	0.44	16.42	112.88
449	4.49	34.93	0.44	0.44	16.36	112.94
450	4.50	35.17	0.44	0.44	16.29	113.00
451	4.51	35.42	0.45	0.45	16.21	113.07
452	4.52	35.65	0.45	0.45	16.15	113.13
453	4.53	35.87	0.45	0.45	16.08	113.19
454	4.54	36.05	0.45	0.45	16.03	113.24
455	4.55	36.20	0.46	0.46	15.98	113.29
456	4.56	36.39	0.46	0.46	15.93	113.34
457	4.57	36.62	0.46	0.46	15.86	113.40
458	4.58	36.87	0.46	0.46	15.79	113.46
459	4.59	37.14	0.47	0.47	15.72	113.53
460	4.60	37.41	0.47	0.47	15.65	113.60
461	4.61	37.66	0.47	0.47	15.58	113.67
462	4.62	37.88	0.48	0.48	15.52	113.72
463	4.63	38.07	0.48	0.48	15.46	113.77
464	4.64	38.29	0.48	0.48	15.38	113.82
465	4.65	38.60	0.48	0.48	15.27	113.87
466	4.66	38.96	0.49	0.49	15.15	113.92
467	4.67	39.36	0.49	0.49	15.01	113.99
468	4.68	39.77	0.49	0.49	14.87	114.05
469	4.69	40.17	0.49	0.49	14.73	114.11
470	4.70	40.54	0.50	0.50	14.60	114.16
471	4.71	40.86	0.50	0.50	14.50	114.21
472	4.72	41.11	0.50	0.50	14.40	114.25
473	4.73	41.39	0.50	0.50	14.30	114.29
474	4.74	41.73	0.50	0.50	14.19	114.34
475	4.75	42.12	0.50	0.50	14.07	114.39
476	4.76	42.54	0.51	0.51	13.93	114.45
477	4.77	42.96	0.51	0.51	13.80	114.51
478	4.78	43.37	0.51	0.51	13.67	114.56
479	4.79	43.74	0.51	0.51	13.56	114.61
480	4.80	44.05	0.52	0.52	13.47	114.65

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
481	4.81	44.32	0.52	0.52	13.39	114.70
482	4.82	44.67	0.52	0.52	13.31	114.78
483	4.83	45.08	0.53	0.53	13.23	114.86
484	4.84	45.55	0.53	0.53	13.13	114.96
485	4.85	46.04	0.54	0.54	13.04	115.07
486	4.86	46.52	0.54	0.54	12.94	115.17
487	4.87	46.98	0.55	0.55	12.86	115.26
488	4.88	47.38	0.55	0.55	12.78	115.34
489	4.89	47.72	0.56	0.56	12.71	115.42
490	4.90	48.07	0.56	0.56	12.64	115.50
491	4.91	48.55	0.57	0.57	12.56	115.59
492	4.92	49.10	0.57	0.57	12.46	115.70
493	4.93	49.70	0.58	0.58	12.35	115.81
494	4.94	50.32	0.59	0.59	12.25	115.93
495	4.95	50.93	0.59	0.59	12.14	116.05
496	4.96	51.49	0.60	0.60	12.05	116.15
497	4.97	51.97	0.61	0.61	11.97	116.24
498	4.98	52.35	0.61	0.61	11.91	116.31
499	4.99	52.64	0.61	0.61	11.85	116.38
500	5.00	53.01	0.62	0.62	11.80	116.44
501	5.01	53.42	0.62	0.62	11.73	116.52
502	5.02	53.86	0.63	0.63	11.66	116.60
503	5.03	54.31	0.63	0.63	11.60	116.68
504	5.04	54.74	0.64	0.64	11.53	116.75
505	5.05	55.13	0.64	0.64	11.47	116.82
506	5.06	55.46	0.65	0.65	11.42	116.87
507	5.07	55.64	0.65	0.65	11.38	116.89
508	5.08	55.74	0.65	0.65	11.34	116.89
509	5.09	55.86	0.65	0.65	11.29	116.88
510	5.10	56.00	0.64	0.64	11.23	116.86
511	5.11	56.14	0.64	0.64	11.17	116.85
512	5.12	56.28	0.64	0.64	11.11	116.83
513	5.13	56.41	0.64	0.64	11.05	116.82
514	5.14	56.53	0.64	0.64	11.01	116.80
515	5.15	56.62	0.63	0.63	10.97	116.79
516	5.16	56.69	0.63	0.63	10.94	116.79
517	5.17	56.76	0.63	0.63	10.91	116.78
518	5.18	56.85	0.63	0.63	10.88	116.78
519	5.19	56.94	0.63	0.63	10.85	116.77
520	5.20	57.03	0.63	0.63	10.82	116.77
521	5.21	57.13	0.63	0.63	10.78	116.77
522	5.22	57.21	0.63	0.63	10.75	116.76
523	5.23	57.29	0.63	0.63	10.73	116.76
524	5.24	57.35	0.63	0.63	10.72	116.77
525	5.25	57.44	0.63	0.63	10.72	116.81
526	5.26	57.55	0.64	0.64	10.74	116.86
527	5.27	57.67	0.64	0.64	10.76	116.92
528	5.28	57.81	0.65	0.65	10.78	116.98

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
529	5.29	57.94	0.65	0.65	10.80	117.04
530	5.30	58.07	0.66	0.66	10.82	117.10
531	5.31	58.19	0.66	0.66	10.84	117.16
532	5.32	58.29	0.67	0.67	10.86	117.20
533	5.33	58.30	0.67	0.67	10.89	117.24
534	5.34	58.23	0.67	0.67	10.94	117.27
535	5.35	58.13	0.68	0.68	11.01	117.31
536	5.36	58.03	0.68	0.68	11.08	117.35
537	5.37	57.92	0.68	0.68	11.15	117.39
538	5.38	57.81	0.69	0.69	11.22	117.43
539	5.39	57.71	0.69	0.69	11.29	117.46
540	5.40	57.62	0.70	0.70	11.35	117.50
541	5.41	57.55	0.70	0.70	11.40	117.52
542	5.42	57.47	0.70	0.70	11.44	117.54
543	5.43	57.36	0.70	0.70	11.49	117.55
544	5.44	57.24	0.70	0.70	11.54	117.56
545	5.45	57.11	0.70	0.70	11.59	117.58
546	5.46	56.97	0.71	0.71	11.65	117.59
547	5.47	56.84	0.71	0.71	11.71	117.60
548	5.48	56.72	0.71	0.71	11.76	117.62
549	5.49	56.61	0.71	0.71	11.80	117.63
550	5.50	56.54	0.71	0.71	11.83	117.63
551	5.51	56.54	0.71	0.71	11.84	117.63
552	5.52	56.54	0.71	0.71	11.84	117.63
553	5.53	56.54	0.71	0.71	11.84	117.63
554	5.54	56.54	0.71	0.71	11.84	117.63
555	5.55	56.54	0.71	0.71	11.84	117.63
556	5.56	56.54	0.71	0.71	11.84	117.63
557	5.57	56.54	0.71	0.71	11.84	117.63
558	5.58	56.54	0.71	0.71	11.84	117.63
559	5.59	56.51	0.71	0.71	11.85	117.63
560	5.60	56.43	0.71	0.71	11.86	117.61
561	5.61	56.34	0.71	0.71	11.87	117.60
562	5.62	56.23	0.71	0.71	11.89	117.58
563	5.63	56.13	0.71	0.71	11.90	117.56
564	5.64	56.02	0.71	0.71	11.92	117.54
565	5.65	55.92	0.70	0.70	11.93	117.53
566	5.66	55.83	0.70	0.70	11.95	117.51
567	5.67	55.76	0.70	0.70	11.96	117.50
568	5.68	55.69	0.70	0.70	11.98	117.50
569	5.69	55.60	0.70	0.70	12.01	117.49
570	5.70	55.51	0.70	0.70	12.04	117.49
571	5.71	55.40	0.70	0.70	12.07	117.49
572	5.72	55.29	0.70	0.70	12.11	117.49
573	5.73	55.19	0.70	0.70	12.14	117.49
574	5.74	55.09	0.70	0.70	12.18	117.49
575	5.75	55.00	0.71	0.71	12.20	117.49
576	5.76	54.95	0.71	0.71	12.22	117.49

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
577	5.77	54.95	0.71	0.71	12.24	117.50
578	5.78	54.95	0.71	0.71	12.25	117.52
579	5.79	54.95	0.71	0.71	12.27	117.54
580	5.80	54.95	0.71	0.71	12.29	117.55
581	5.81	54.95	0.71	0.71	12.31	117.57
582	5.82	54.95	0.71	0.71	12.33	117.59
583	5.83	54.95	0.72	0.72	12.34	117.60
584	5.84	54.95	0.72	0.72	12.35	117.61
585	5.85	54.95	0.72	0.72	12.35	117.61
586	5.86	54.95	0.72	0.72	12.34	117.60
587	5.87	54.95	0.71	0.71	12.33	117.59
588	5.88	54.95	0.71	0.71	12.31	117.57
589	5.89	54.95	0.71	0.71	12.29	117.55
590	5.90	54.95	0.71	0.71	12.27	117.53
591	5.91	54.95	0.71	0.71	12.26	117.52
592	5.92	54.95	0.71	0.71	12.24	117.50
593	5.93	54.95	0.71	0.71	12.23	117.50
594	5.94	54.95	0.71	0.71	12.24	117.50
595	5.95	54.95	0.71	0.71	12.25	117.51
596	5.96	54.95	0.71	0.71	12.27	117.53
597	5.97	54.95	0.71	0.71	12.29	117.55
598	5.98	54.95	0.71	0.71	12.31	117.56
599	5.99	54.95	0.71	0.71	12.33	117.58
600	6.00	54.95	0.72	0.72	12.35	117.60
601	6.01	54.95	0.72	0.72	12.37	117.61
602	6.02	54.95	0.72	0.72	12.39	117.63
603	6.03	54.95	0.72	0.72	12.42	117.65
604	6.04	54.95	0.72	0.72	12.46	117.68
605	6.05	54.95	0.73	0.73	12.49	117.71
606	6.06	54.95	0.73	0.73	12.53	117.75
607	6.07	54.95	0.73	0.73	12.57	117.78
608	6.08	54.95	0.74	0.74	12.61	117.81
609	6.09	54.95	0.74	0.74	12.65	117.84
610	6.10	54.95	0.74	0.74	12.67	117.87
611	6.11	54.99	0.74	0.74	12.69	117.88
612	6.12	55.08	0.75	0.75	12.69	117.90
613	6.13	55.18	0.75	0.75	12.68	117.92
614	6.14	55.30	0.75	0.75	12.67	117.94
615	6.15	55.42	0.75	0.75	12.66	117.96
616	6.16	55.54	0.75	0.75	12.65	117.98
617	6.17	55.66	0.75	0.75	12.65	118.00
618	6.18	55.76	0.75	0.75	12.64	118.02
619	6.19	55.84	0.76	0.76	12.62	118.04
620	6.20	56.04	0.76	0.76	12.59	118.05
621	6.21	56.32	0.76	0.76	12.54	118.07
622	6.22	56.65	0.76	0.76	12.47	118.10
623	6.23	57.00	0.76	0.76	12.40	118.12
624	6.24	57.35	0.76	0.76	12.33	118.15

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
625	6.25	57.70	0.76	0.76	12.26	118.17
626	6.26	58.02	0.76	0.76	12.20	118.20
627	6.27	58.30	0.76	0.76	12.14	118.22
628	6.28	58.57	0.77	0.77	12.08	118.25
629	6.29	59.09	0.77	0.77	12.01	118.31
630	6.30	59.73	0.77	0.77	11.91	118.38
631	6.31	60.46	0.78	0.78	11.80	118.46
632	6.32	61.22	0.79	0.79	11.68	118.55
633	6.33	61.99	0.79	0.79	11.57	118.63
634	6.34	62.73	0.80	0.80	11.46	118.71
635	6.35	63.39	0.80	0.80	11.36	118.78
636	6.36	63.95	0.81	0.81	11.28	118.85
637	6.37	64.49	0.81	0.81	11.21	118.93
638	6.38	65.24	0.82	0.82	11.13	119.04
639	6.39	66.14	0.83	0.83	11.05	119.17
640	6.40	67.12	0.85	0.85	10.95	119.31
641	6.41	68.15	0.86	0.86	10.85	119.45
642	6.42	69.16	0.87	0.87	10.76	119.60
643	6.43	70.11	0.88	0.88	10.67	119.73
644	6.44	70.94	0.89	0.89	10.60	119.84
645	6.45	71.62	0.90	0.90	10.54	119.94
646	6.46	72.22	0.91	0.91	10.49	120.03
647	6.47	72.99	0.92	0.92	10.42	120.13
648	6.48	73.88	0.93	0.93	10.35	120.25
649	6.49	74.84	0.94	0.94	10.27	120.37
650	6.50	75.81	0.96	0.96	10.19	120.49
651	6.51	76.76	0.97	0.97	10.12	120.61
652	6.52	77.64	0.98	0.98	10.05	120.72
653	6.53	78.38	0.99	0.99	9.99	120.81
654	6.54	78.95	1.00	1.00	9.95	120.89
655	6.55	79.50	1.00	1.00	9.90	120.96
656	6.56	80.18	1.01	1.01	9.86	121.05
657	6.57	80.95	1.02	1.02	9.80	121.14
658	6.58	81.75	1.03	1.03	9.74	121.23
659	6.59	82.56	1.04	1.04	9.69	121.33
660	6.60	83.34	1.05	1.05	9.63	121.42
661	6.61	84.04	1.06	1.06	9.59	121.50
662	6.62	84.61	1.07	1.07	9.55	121.56
663	6.63	84.98	1.07	1.07	9.52	121.61
664	6.64	85.34	1.08	1.08	9.50	121.65
665	6.65	85.77	1.08	1.08	9.48	121.70
666	6.66	86.24	1.09	1.09	9.45	121.75
667	6.67	86.73	1.09	1.09	9.42	121.81
668	6.68	87.21	1.10	1.10	9.39	121.86
669	6.69	87.66	1.10	1.10	9.36	121.91
670	6.70	88.06	1.11	1.11	9.34	121.95
671	6.71	88.38	1.11	1.11	9.33	121.99
672	6.72	88.44	1.12	1.12	9.33	122.01

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
673	6.73	88.51	1.12	1.12	9.35	122.03
674	6.74	88.58	1.12	1.12	9.36	122.06
675	6.75	88.66	1.13	1.13	9.38	122.08
676	6.76	88.74	1.13	1.13	9.39	122.11
677	6.77	88.82	1.13	1.13	9.41	122.14
678	6.78	88.89	1.14	1.14	9.42	122.16
679	6.79	88.96	1.14	1.14	9.44	122.18
680	6.80	88.96	1.14	1.14	9.46	122.19
681	6.81	88.79	1.14	1.14	9.49	122.20
682	6.82	88.59	1.15	1.15	9.54	122.21
683	6.83	88.36	1.15	1.15	9.59	122.22
684	6.84	88.11	1.15	1.15	9.64	122.23
685	6.85	87.87	1.15	1.15	9.70	122.23
686	6.86	87.64	1.16	1.16	9.75	122.24
687	6.87	87.43	1.16	1.16	9.80	122.25
688	6.88	87.26	1.16	1.16	9.84	122.25
689	6.89	87.05	1.16	1.16	9.89	122.26
690	6.90	86.75	1.16	1.16	9.95	122.26
691	6.91	86.39	1.17	1.17	10.02	122.27
692	6.92	86.00	1.17	1.17	10.10	122.27
693	6.93	85.60	1.17	1.17	10.18	122.28
694	6.94	85.19	1.17	1.17	10.26	122.28
695	6.95	84.82	1.18	1.18	10.34	122.29
696	6.96	84.49	1.18	1.18	10.41	122.29
697	6.97	84.23	1.18	1.18	10.47	122.29
698	6.98	83.97	1.18	1.18	10.52	122.28
699	6.99	83.65	1.18	1.18	10.57	122.27
700	7.00	83.28	1.18	1.18	10.64	122.26
701	7.01	82.88	1.18	1.18	10.70	122.24
702	7.02	82.47	1.18	1.18	10.77	122.23
703	7.03	82.08	1.18	1.18	10.84	122.21
704	7.04	81.71	1.18	1.18	10.90	122.20
705	7.05	81.41	1.18	1.18	10.96	122.19
706	7.06	81.20	1.18	1.18	11.00	122.19
707	7.07	81.09	1.18	1.18	11.04	122.19
708	7.08	80.95	1.18	1.18	11.08	122.20
709	7.09	80.80	1.18	1.18	11.13	122.21
710	7.10	80.64	1.19	1.19	11.18	122.22
711	7.11	80.48	1.19	1.19	11.23	122.24
712	7.12	80.32	1.19	1.19	11.28	122.25
713	7.13	80.18	1.19	1.19	11.32	122.26
714	7.14	80.07	1.19	1.19	11.35	122.27
715	7.15	80.13	1.20	1.20	11.36	122.28
716	7.16	80.31	1.20	1.20	11.36	122.30
717	7.17	80.52	1.20	1.20	11.34	122.33
718	7.18	80.76	1.21	1.21	11.33	122.36
719	7.19	81.00	1.21	1.21	11.32	122.38
720	7.20	81.24	1.21	1.21	11.30	122.41

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
721	7.21	81.47	1.22	1.22	11.29	122.44
722	7.22	81.67	1.22	1.22	11.28	122.46
723	7.23	81.82	1.22	1.22	11.26	122.48
724	7.24	82.13	1.22	1.22	11.23	122.50
725	7.25	82.52	1.23	1.23	11.18	122.52
726	7.26	82.96	1.23	1.23	11.12	122.55
727	7.27	83.44	1.23	1.23	11.06	122.57
728	7.28	83.93	1.23	1.23	10.99	122.59
729	7.29	84.40	1.23	1.23	10.93	122.62
730	7.30	84.84	1.23	1.23	10.88	122.64
731	7.31	85.20	1.24	1.24	10.83	122.66
732	7.32	85.52	1.24	1.24	10.79	122.68
733	7.33	85.98	1.24	1.24	10.74	122.71
734	7.34	86.52	1.24	1.24	10.67	122.74
735	7.35	87.14	1.25	1.25	10.60	122.78
736	7.36	87.79	1.25	1.25	10.53	122.82
737	7.37	88.43	1.25	1.25	10.46	122.86
738	7.38	89.05	1.26	1.26	10.39	122.89
739	7.39	89.60	1.26	1.26	10.33	122.92
740	7.40	90.06	1.26	1.26	10.28	122.95
741	7.41	90.48	1.26	1.26	10.23	122.98
742	7.42	91.02	1.27	1.27	10.17	123.01
743	7.43	91.67	1.27	1.27	10.10	123.05
744	7.44	92.38	1.28	1.28	10.03	123.09
745	7.45	93.11	1.28	1.28	9.96	123.14
746	7.46	93.83	1.28	1.28	9.88	123.18
747	7.47	94.50	1.29	1.29	9.81	123.22
748	7.48	95.09	1.29	1.29	9.76	123.25
749	7.49	95.56	1.29	1.29	9.71	123.28
750	7.50	95.97	1.30	1.30	9.68	123.32
751	7.51	96.49	1.31	1.31	9.65	123.37
752	7.52	97.09	1.31	1.31	9.62	123.43
753	7.53	97.73	1.32	1.32	9.58	123.50
754	7.54	98.38	1.33	1.33	9.55	123.56
755	7.55	99.01	1.34	1.34	9.51	123.62
756	7.56	99.59	1.35	1.35	9.48	123.68
757	7.57	100.08	1.35	1.35	9.45	123.72
758	7.58	100.48	1.36	1.36	9.43	123.77
759	7.59	100.99	1.37	1.37	9.40	123.82
760	7.60	101.61	1.38	1.38	9.37	123.88
761	7.61	102.30	1.38	1.38	9.33	123.94
762	7.62	103.03	1.39	1.39	9.30	124.01
763	7.63	103.76	1.40	1.40	9.26	124.08
764	7.64	104.45	1.41	1.41	9.22	124.14
765	7.65	105.07	1.42	1.42	9.19	124.20
766	7.66	105.58	1.43	1.43	9.17	124.25
767	7.67	105.95	1.44	1.44	9.16	124.30
768	7.68	106.38	1.45	1.45	9.16	124.37

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
769	7.69	106.88	1.46	1.46	9.17	124.44
770	7.70	107.43	1.47	1.47	9.17	124.52
771	7.71	108.00	1.49	1.49	9.17	124.61
772	7.72	108.56	1.50	1.50	9.17	124.69
773	7.73	109.09	1.52	1.52	9.18	124.77
774	7.74	109.54	1.53	1.53	9.18	124.83
775	7.75	109.90	1.54	1.54	9.19	124.89
776	7.76	110.16	1.55	1.55	9.19	124.94
777	7.77	110.49	1.56	1.56	9.21	124.99
778	7.78	110.86	1.57	1.57	9.22	125.05
779	7.79	111.26	1.58	1.58	9.23	125.12
780	7.80	111.67	1.59	1.59	9.24	125.19
781	7.81	112.06	1.61	1.61	9.25	125.25
782	7.82	112.42	1.62	1.62	9.26	125.31
783	7.83	112.73	1.63	1.63	9.27	125.36
784	7.84	112.95	1.63	1.63	9.28	125.39
785	7.85	113.18	1.64	1.64	9.27	125.42
786	7.86	113.45	1.64	1.64	9.26	125.44
787	7.87	113.76	1.65	1.65	9.25	125.47
788	7.88	114.09	1.65	1.65	9.24	125.49
789	7.89	114.41	1.66	1.66	9.23	125.52
790	7.90	114.72	1.66	1.66	9.21	125.55
791	7.91	114.99	1.66	1.66	9.20	125.57
792	7.92	115.22	1.67	1.67	9.20	125.59
793	7.93	115.27	1.67	1.67	9.21	125.60
794	7.94	115.27	1.67	1.67	9.22	125.61
795	7.95	115.27	1.68	1.68	9.24	125.63
796	7.96	115.27	1.68	1.68	9.26	125.64
797	7.97	115.27	1.68	1.68	9.28	125.66
798	7.98	115.27	1.69	1.69	9.29	125.67
799	7.99	115.27	1.69	1.69	9.31	125.69
800	8.00	115.27	1.69	1.69	9.33	125.70
801	8.01	115.27	1.70	1.70	9.34	125.72
802	8.02	115.27	1.70	1.70	9.36	125.73
803	8.03	115.27	1.71	1.71	9.39	125.76
804	8.04	115.27	1.71	1.71	9.42	125.79
805	8.05	115.27	1.72	1.72	9.45	125.82
806	8.06	115.27	1.73	1.73	9.48	125.85
807	8.07	115.27	1.73	1.73	9.51	125.88
808	8.08	115.27	1.74	1.74	9.54	125.90
809	8.09	115.27	1.75	1.75	9.56	125.93
810	8.10	115.34	1.75	1.75	9.56	125.94
811	8.11	115.57	1.75	1.75	9.55	125.95
812	8.12	115.85	1.75	1.75	9.52	125.96
813	8.13	116.16	1.75	1.75	9.50	125.97
814	8.14	116.48	1.75	1.75	9.47	125.98
815	8.15	116.81	1.75	1.75	9.44	126.00
816	8.16	117.11	1.76	1.76	9.41	126.01

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
817	8.17	117.39	1.76	1.76	9.39	126.02
818	8.18	117.61	1.76	1.76	9.36	126.02
819	8.19	117.91	1.76	1.76	9.33	126.03
820	8.20	118.35	1.75	1.75	9.28	126.03
821	8.21	118.85	1.75	1.75	9.22	126.03
822	8.22	119.41	1.75	1.75	9.15	126.03
823	8.23	119.97	1.75	1.75	9.08	126.02
824	8.24	120.53	1.74	1.74	9.01	126.02
825	8.25	121.05	1.74	1.74	8.95	126.02
826	8.26	121.51	1.74	1.74	8.90	126.02
827	8.27	121.87	1.73	1.73	8.85	126.02
828	8.28	122.34	1.74	1.74	8.80	126.04
829	8.29	122.93	1.74	1.74	8.76	126.06
830	8.30	123.61	1.74	1.74	8.70	126.08
831	8.31	124.33	1.74	1.74	8.64	126.10
832	8.32	125.06	1.75	1.75	8.58	126.13
833	8.33	125.77	1.75	1.75	8.52	126.15
834	8.34	126.41	1.75	1.75	8.47	126.17
835	8.35	126.96	1.75	1.75	8.42	126.18
836	8.36	127.37	1.75	1.75	8.39	126.20
837	8.37	127.83	1.76	1.76	8.36	126.23
838	8.38	128.39	1.76	1.76	8.32	126.25
839	8.39	129.01	1.77	1.77	8.28	126.28
840	8.40	129.65	1.77	1.77	8.24	126.31
841	8.41	130.30	1.77	1.77	8.20	126.35
842	8.42	130.91	1.78	1.78	8.16	126.37
843	8.43	131.46	1.78	1.78	8.13	126.40
844	8.44	131.90	1.79	1.79	8.10	126.42
845	8.45	132.18	1.79	1.79	8.09	126.44
846	8.46	132.49	1.79	1.79	8.08	126.47
847	8.47	132.86	1.80	1.80	8.06	126.49
848	8.48	133.25	1.80	1.80	8.05	126.52
849	8.49	133.66	1.81	1.81	8.03	126.55
850	8.50	134.06	1.81	1.81	8.02	126.58
851	8.51	134.43	1.82	1.82	8.01	126.60
852	8.52	134.75	1.82	1.82	7.99	126.63
853	8.53	134.99	1.83	1.83	7.99	126.64
854	8.54	135.15	1.83	1.83	7.98	126.66
855	8.55	135.35	1.83	1.83	7.97	126.67
856	8.56	135.58	1.84	1.84	7.97	126.69
857	8.57	135.82	1.84	1.84	7.96	126.71
858	8.58	136.06	1.84	1.84	7.95	126.72
859	8.59	136.30	1.85	1.85	7.94	126.74
860	8.60	136.51	1.85	1.85	7.94	126.76
861	8.61	136.69	1.85	1.85	7.93	126.77
862	8.62	136.79	1.85	1.85	7.93	126.78
863	8.63	136.85	1.85	1.85	7.93	126.78
864	8.64	136.92	1.85	1.85	7.93	126.79

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
865	8.65	137.00	1.85	1.85	7.93	126.79
866	8.66	137.08	1.86	1.86	7.93	126.80
867	8.67	137.16	1.86	1.86	7.92	126.80
868	8.68	137.24	1.86	1.86	7.92	126.81
869	8.69	137.31	1.86	1.86	7.92	126.81
870	8.70	137.36	1.86	1.86	7.92	126.81
871	8.71	137.37	1.86	1.86	7.91	126.80
872	8.72	137.37	1.85	1.85	7.89	126.77
873	8.73	137.37	1.84	1.84	7.86	126.74
874	8.74	137.37	1.83	1.83	7.84	126.71
875	8.75	137.37	1.82	1.82	7.81	126.68
876	8.76	137.37	1.82	1.82	7.78	126.64
877	8.77	137.37	1.81	1.81	7.76	126.61
878	8.78	137.37	1.80	1.80	7.74	126.58
879	8.79	137.36	1.80	1.80	7.72	126.56
880	8.80	137.26	1.79	1.79	7.71	126.54
881	8.81	137.12	1.79	1.79	7.71	126.51
882	8.82	136.97	1.78	1.78	7.70	126.49
883	8.83	136.81	1.77	1.77	7.70	126.46
884	8.84	136.65	1.77	1.77	7.69	126.43
885	8.85	136.49	1.76	1.76	7.68	126.40
886	8.86	136.35	1.75	1.75	7.68	126.38
887	8.87	136.23	1.75	1.75	7.68	126.36
888	8.88	136.09	1.75	1.75	7.69	126.35
889	8.89	135.86	1.75	1.75	7.72	126.36
890	8.90	135.58	1.76	1.76	7.76	126.37
891	8.91	135.27	1.76	1.76	7.80	126.38
892	8.92	134.94	1.76	1.76	7.85	126.39
893	8.93	134.62	1.77	1.77	7.89	126.40
894	8.94	134.32	1.77	1.77	7.93	126.41
895	8.95	134.05	1.78	1.78	7.97	126.42
896	8.96	133.83	1.78	1.78	8.00	126.43
897	8.97	133.59	1.78	1.78	8.03	126.42
898	8.98	133.28	1.78	1.78	8.06	126.42
899	8.99	132.91	1.78	1.78	8.09	126.41
900	9.00	132.52	1.78	1.78	8.12	126.39
901	9.01	132.11	1.77	1.77	8.16	126.38
902	9.02	131.71	1.77	1.77	8.19	126.37
903	9.03	131.34	1.77	1.77	8.22	126.36
904	9.04	131.02	1.77	1.77	8.25	126.35
905	9.05	130.78	1.77	1.77	8.28	126.34
906	9.06	130.56	1.77	1.77	8.31	126.35
907	9.07	130.30	1.78	1.78	8.35	126.36
908	9.08	130.00	1.78	1.78	8.39	126.36
909	9.09	129.67	1.78	1.78	8.44	126.37
910	9.10	129.35	1.79	1.79	8.48	126.38
911	9.11	129.04	1.79	1.79	8.53	126.39
912	9.12	128.75	1.79	1.79	8.57	126.40

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
913	9.13	128.52	1.80	1.80	8.60	126.41
914	9.14	128.39	1.80	1.80	8.63	126.42
915	9.15	128.33	1.81	1.81	8.66	126.44
916	9.16	128.26	1.81	1.81	8.69	126.46
917	9.17	128.18	1.82	1.82	8.72	126.48
918	9.18	128.10	1.82	1.82	8.76	126.51
919	9.19	128.02	1.83	1.83	8.79	126.54
920	9.20	127.95	1.84	1.84	8.82	126.56
921	9.21	127.88	1.84	1.84	8.85	126.58
922	9.22	127.82	1.85	1.85	8.87	126.60
923	9.23	127.90	1.85	1.85	8.88	126.61
924	9.24	128.02	1.85	1.85	8.88	126.62
925	9.25	128.17	1.85	1.85	8.87	126.63
926	9.26	128.33	1.86	1.86	8.87	126.64
927	9.27	128.49	1.86	1.86	8.86	126.65
928	9.28	128.65	1.86	1.86	8.86	126.67
929	9.29	128.80	1.86	1.86	8.85	126.68
930	9.30	128.92	1.87	1.87	8.85	126.69
931	9.31	129.06	1.87	1.87	8.83	126.69
932	9.32	129.44	1.87	1.87	8.80	126.70
933	9.33	129.91	1.87	1.87	8.76	126.71
934	9.34	130.44	1.87	1.87	8.71	126.72
935	9.35	131.00	1.87	1.87	8.66	126.73
936	9.36	131.57	1.87	1.87	8.61	126.74
937	9.37	132.11	1.87	1.87	8.56	126.75
938	9.38	132.61	1.87	1.87	8.51	126.75
939	9.39	133.02	1.87	1.87	8.47	126.76
940	9.40	133.43	1.86	1.86	8.43	126.77
941	9.41	134.02	1.86	1.86	8.38	126.77
942	9.42	134.72	1.86	1.86	8.31	126.78
943	9.43	135.50	1.86	1.86	8.24	126.79
944	9.44	136.31	1.86	1.86	8.16	126.80
945	9.45	137.12	1.86	1.86	8.09	126.80
946	9.46	137.87	1.86	1.86	8.02	126.81
947	9.47	138.55	1.85	1.85	7.95	126.81
948	9.48	139.09	1.85	1.85	7.90	126.82
949	9.49	139.54	1.85	1.85	7.86	126.83
950	9.50	140.11	1.85	1.85	7.82	126.84
951	9.51	140.77	1.85	1.85	7.76	126.85
952	9.52	141.49	1.85	1.85	7.71	126.87
953	9.53	142.22	1.85	1.85	7.65	126.88
954	9.54	142.94	1.85	1.85	7.60	126.89
955	9.55	143.60	1.86	1.86	7.55	126.91
956	9.56	144.16	1.86	1.86	7.51	126.91
957	9.57	144.43	1.85	1.85	7.48	126.88
958	9.58	143.64	1.83	1.83	7.47	126.82
959	9.59	142.66	1.81	1.81	7.47	126.71
960	9.60	141.56	1.78	1.78	7.48	126.58

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
961	9.61	140.39	1.76	1.76	7.48	126.45
962	9.62	139.22	1.73	1.73	7.48	126.31
963	9.63	138.09	1.70	1.70	7.48	126.18
964	9.64	137.07	1.68	1.68	7.48	126.06
965	9.65	136.22	1.66	1.66	7.48	125.97
966	9.66	135.90	1.65	1.65	7.47	125.91
967	9.67	135.96	1.64	1.64	7.45	125.88
968	9.68	136.03	1.63	1.63	7.42	125.85
969	9.69	136.11	1.63	1.63	7.39	125.82
970	9.70	136.19	1.62	1.62	7.36	125.78
971	9.71	136.27	1.61	1.61	7.33	125.75
972	9.72	136.35	1.60	1.60	7.30	125.72
973	9.73	136.42	1.60	1.60	7.27	125.69
974	9.74	136.47	1.59	1.59	7.27	125.65
975	9.75	135.15	1.58	1.58	7.32	125.57
976	9.76	133.21	1.56	1.56	7.41	125.45
977	9.77	130.97	1.54	1.54	7.52	125.31
978	9.78	128.54	1.51	1.51	7.64	125.15
979	9.79	126.06	1.49	1.49	7.77	124.98
980	9.80	123.64	1.46	1.46	7.90	124.81
981	9.81	121.41	1.44	1.44	8.02	124.65
982	9.82	119.49	1.42	1.42	8.15	124.53
983	9.83	117.80	1.41	1.41	8.38	124.49
984	9.84	115.01	1.44	1.44	8.75	124.53
985	9.85	111.57	1.48	1.48	9.27	124.62
986	9.86	107.69	1.51	1.51	9.88	124.68
987	9.87	103.58	1.54	1.54	10.52	124.72
988	9.88	99.44	1.56	1.56	11.19	124.72
989	9.89	95.48	1.57	1.57	11.84	124.68
990	9.90	91.91	1.58	1.58	12.43	124.63
991	9.91	88.92	1.58	1.58	12.92	124.61
992	9.92	87.93	1.60	1.60	13.28	124.71
993	9.93	88.25	1.66	1.66	13.56	124.94
994	9.94	88.62	1.73	1.73	13.84	125.25
995	9.95	89.02	1.81	1.81	14.14	125.57
996	9.96	89.45	1.89	1.89	14.44	125.91
997	9.97	89.87	1.98	1.98	14.74	126.22
998	9.98	90.26	2.05	2.05	15.01	126.51
999	9.99	90.61	2.12	2.12	15.25	126.76
1000	10.00	90.89	2.18	2.18	15.40	126.89
1001	10.01	90.51	2.17	2.17	15.48	126.91
1002	10.02	89.92	2.15	2.15	15.50	126.83
1003	10.03	89.24	2.12	2.12	15.52	126.72
1004	10.04	88.51	2.09	2.09	15.54	126.61
1005	10.05	87.76	2.06	2.06	15.56	126.48
1006	10.06	87.03	2.03	2.03	15.58	126.37
1007	10.07	86.36	2.01	2.01	15.60	126.26
1008	10.08	85.79	1.99	1.99	15.63	126.16

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1009	10.09	85.12	1.97	1.97	15.72	126.04
1010	10.10	83.40	1.94	1.94	15.90	125.90
1011	10.11	81.28	1.90	1.90	16.17	125.70
1012	10.12	78.90	1.86	1.86	16.49	125.47
1013	10.13	76.38	1.82	1.82	16.84	125.21
1014	10.14	73.85	1.77	1.77	17.20	124.95
1015	10.15	71.43	1.73	1.73	17.56	124.68
1016	10.16	69.25	1.68	1.68	17.90	124.44
1017	10.17	67.43	1.65	1.65	18.22	124.24
1018	10.18	65.97	1.64	1.64	18.60	124.10
1019	10.19	64.19	1.63	1.63	19.08	124.00
1020	10.20	62.07	1.62	1.62	19.69	123.88
1021	10.21	59.74	1.61	1.61	20.36	123.74
1022	10.22	57.32	1.60	1.60	21.09	123.56
1023	10.23	54.92	1.58	1.58	21.83	123.37
1024	10.24	52.67	1.55	1.55	22.55	123.17
1025	10.25	50.70	1.53	1.53	23.21	122.97
1026	10.26	49.11	1.51	1.51	23.78	122.82
1027	10.27	47.96	1.51	1.51	24.34	122.70
1028	10.28	46.55	1.50	1.50	24.97	122.60
1029	10.29	44.93	1.49	1.49	25.70	122.47
1030	10.30	43.17	1.48	1.48	26.51	122.30
1031	10.31	41.38	1.46	1.46	27.36	122.11
1032	10.32	39.64	1.44	1.44	28.22	121.91
1033	10.33	38.04	1.42	1.42	29.04	121.70
1034	10.34	36.67	1.39	1.39	29.74	121.51
1035	10.35	35.74	1.38	1.38	30.30	121.39
1036	10.36	35.24	1.38	1.38	30.75	121.31
1037	10.37	34.63	1.38	1.38	31.19	121.26
1038	10.38	33.94	1.38	1.38	31.69	121.20
1039	10.39	33.21	1.37	1.37	32.23	121.13
1040	10.40	32.48	1.37	1.37	32.78	121.06
1041	10.41	31.79	1.36	1.36	33.32	120.98
1042	10.42	31.16	1.36	1.36	33.80	120.90
1043	10.43	30.64	1.35	1.35	34.18	120.85
1044	10.44	30.43	1.35	1.35	34.45	120.84
1045	10.45	30.37	1.36	1.36	34.64	120.87
1046	10.46	30.30	1.37	1.37	34.82	120.92
1047	10.47	30.22	1.39	1.39	35.02	120.98
1048	10.48	30.14	1.40	1.40	35.23	121.04
1049	10.49	30.06	1.41	1.41	35.44	121.09
1050	10.50	29.99	1.42	1.42	35.63	121.15
1051	10.51	29.92	1.43	1.43	35.80	121.19
1052	10.52	29.87	1.44	1.44	35.92	121.22
1053	10.53	29.86	1.44	1.44	36.00	121.25
1054	10.54	29.86	1.45	1.45	36.05	121.27
1055	10.55	29.86	1.45	1.45	36.11	121.30
1056	10.56	29.86	1.46	1.46	36.18	121.33

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1057	10.57	29.86	1.47	1.47	36.24	121.36
1058	10.58	29.86	1.47	1.47	36.30	121.39
1059	10.59	29.86	1.48	1.48	36.36	121.41
1060	10.60	29.86	1.48	1.48	36.39	121.44
1061	10.61	29.91	1.49	1.49	36.35	121.46
1062	10.62	30.13	1.49	1.49	36.22	121.49
1063	10.63	30.39	1.49	1.49	36.02	121.53
1064	10.64	30.68	1.49	1.49	35.79	121.57
1065	10.65	31.00	1.50	1.50	35.54	121.61
1066	10.66	31.31	1.50	1.50	35.30	121.65
1067	10.67	31.61	1.50	1.50	35.07	121.68
1068	10.68	31.87	1.51	1.51	34.86	121.71
1069	10.69	32.10	1.51	1.51	34.65	121.75
1070	10.70	32.43	1.51	1.51	34.38	121.80
1071	10.71	32.98	1.52	1.52	34.01	121.86
1072	10.72	33.62	1.53	1.53	33.55	121.94
1073	10.73	34.33	1.53	1.53	33.06	122.02
1074	10.74	35.06	1.54	1.54	32.56	122.10
1075	10.75	35.78	1.54	1.54	32.07	122.17
1076	10.76	36.46	1.55	1.55	31.61	122.23
1077	10.77	37.05	1.55	1.55	31.22	122.28
1078	10.78	37.52	1.55	1.55	30.85	122.34
1079	10.79	38.18	1.56	1.56	30.45	122.41
1080	10.80	39.03	1.57	1.57	29.97	122.49
1081	10.81	40.01	1.57	1.57	29.42	122.59
1082	10.82	41.06	1.58	1.58	28.84	122.68
1083	10.83	42.13	1.59	1.59	28.26	122.76
1084	10.84	43.17	1.59	1.59	27.70	122.84
1085	10.85	44.12	1.59	1.59	27.20	122.90
1086	10.86	44.93	1.59	1.59	26.77	122.95
1087	10.87	45.63	1.59	1.59	26.36	123.01
1088	10.88	46.64	1.60	1.60	25.91	123.09
1089	10.89	47.87	1.61	1.61	25.39	123.19
1090	10.90	49.25	1.62	1.62	24.81	123.29
1091	10.91	50.71	1.62	1.62	24.21	123.39
1092	10.92	52.17	1.63	1.63	23.62	123.47
1093	10.93	53.55	1.63	1.63	23.07	123.54
1094	10.94	54.80	1.63	1.63	22.58	123.60
1095	10.95	55.83	1.63	1.63	22.17	123.63
1096	10.96	56.64	1.62	1.62	21.81	123.66
1097	10.97	57.61	1.62	1.62	21.43	123.69
1098	10.98	58.75	1.61	1.61	21.00	123.71
1099	10.99	60.01	1.61	1.61	20.52	123.72
1100	11.00	61.31	1.60	1.60	20.04	123.73
1101	11.01	62.59	1.58	1.58	19.56	123.73
1102	11.02	63.79	1.57	1.57	19.12	123.72
1103	11.03	64.84	1.56	1.56	18.74	123.70
1104	11.04	65.68	1.55	1.55	18.45	123.68

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1105	11.05	66.10	1.54	1.54	18.21	123.64
1106	11.06	66.62	1.53	1.53	17.99	123.60
1107	11.07	67.21	1.51	1.51	17.73	123.55
1108	11.08	67.85	1.49	1.49	17.45	123.49
1109	11.09	68.51	1.47	1.47	17.17	123.42
1110	11.10	69.14	1.46	1.46	16.89	123.35
1111	11.11	69.71	1.44	1.44	16.64	123.29
1112	11.12	70.21	1.42	1.42	16.44	123.23
1113	11.13	70.45	1.41	1.41	16.30	123.16
1114	11.14	70.32	1.40	1.40	16.21	123.08
1115	11.15	70.16	1.38	1.38	16.14	122.98
1116	11.16	69.99	1.36	1.36	16.06	122.87
1117	11.17	69.81	1.34	1.34	15.97	122.75
1118	11.18	69.63	1.32	1.32	15.88	122.63
1119	11.19	69.45	1.30	1.30	15.79	122.51
1120	11.20	69.30	1.28	1.28	15.72	122.41
1121	11.21	69.17	1.26	1.26	15.68	122.32
1122	11.22	68.84	1.26	1.26	15.71	122.26
1123	11.23	68.28	1.25	1.25	15.80	122.21
1124	11.24	67.62	1.24	1.24	15.93	122.15
1125	11.25	66.89	1.24	1.24	16.07	122.08
1126	11.26	66.14	1.23	1.23	16.21	122.01
1127	11.27	65.41	1.22	1.22	16.36	121.94
1128	11.28	64.72	1.21	1.21	16.50	121.87
1129	11.29	64.12	1.21	1.21	16.62	121.81
1130	11.30	63.64	1.20	1.20	16.77	121.77
1131	11.31	62.93	1.20	1.20	16.96	121.74
1132	11.32	62.04	1.21	1.21	17.24	121.71
1133	11.33	61.01	1.21	1.21	17.55	121.68
1134	11.34	59.91	1.21	1.21	17.90	121.64
1135	11.35	58.79	1.21	1.21	18.25	121.59
1136	11.36	57.71	1.21	1.21	18.59	121.54
1137	11.37	56.72	1.21	1.21	18.91	121.49
1138	11.38	55.88	1.20	1.20	19.20	121.45
1139	11.39	55.13	1.20	1.20	19.51	121.40
1140	11.40	54.07	1.20	1.20	19.88	121.35
1141	11.41	52.77	1.20	1.20	20.35	121.28
1142	11.42	51.33	1.20	1.20	20.88	121.19
1143	11.43	49.81	1.19	1.19	21.45	121.08
1144	11.44	48.28	1.18	1.18	22.03	120.96
1145	11.45	46.84	1.18	1.18	22.60	120.84
1146	11.46	45.55	1.17	1.17	23.12	120.72
1147	11.47	44.48	1.16	1.16	23.57	120.62
1148	11.48	43.69	1.15	1.15	24.00	120.54
1149	11.49	42.75	1.15	1.15	24.47	120.46
1150	11.50	41.64	1.15	1.15	25.02	120.37
1151	11.51	40.44	1.14	1.14	25.64	120.26
1152	11.52	39.19	1.13	1.13	26.29	120.14

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1153	11.53	37.96	1.13	1.13	26.95	120.00
1154	11.54	36.82	1.11	1.11	27.58	119.87
1155	11.55	35.82	1.10	1.10	28.14	119.74
1156	11.56	35.03	1.10	1.10	28.61	119.64
1157	11.57	34.49	1.09	1.09	29.05	119.56
1158	11.58	33.81	1.09	1.09	29.53	119.50
1159	11.59	33.03	1.09	1.09	30.07	119.41
1160	11.60	32.20	1.08	1.08	30.67	119.32
1161	11.61	31.35	1.08	1.08	31.29	119.21
1162	11.62	30.54	1.07	1.07	31.90	119.10
1163	11.63	29.79	1.06	1.06	32.47	118.99
1164	11.64	29.16	1.05	1.05	32.95	118.90
1165	11.65	28.75	1.05	1.05	33.33	118.84
1166	11.66	28.48	1.05	1.05	33.65	118.80
1167	11.67	28.16	1.05	1.05	33.98	118.78
1168	11.68	27.80	1.05	1.05	34.35	118.76
1169	11.69	27.42	1.05	1.05	34.74	118.73
1170	11.70	27.05	1.05	1.05	35.14	118.70
1171	11.71	26.69	1.05	1.05	35.51	118.66
1172	11.72	26.37	1.05	1.05	35.85	118.63
1173	11.73	26.11	1.05	1.05	36.08	118.61
1174	11.74	26.10	1.05	1.05	36.18	118.63
1175	11.75	26.21	1.06	1.06	36.17	118.67
1176	11.76	26.33	1.07	1.07	36.13	118.72
1177	11.77	26.47	1.07	1.07	36.08	118.79
1178	11.78	26.61	1.08	1.08	36.03	118.85
1179	11.79	26.75	1.09	1.09	35.98	118.91
1180	11.80	26.88	1.10	1.10	35.93	118.96
1181	11.81	26.99	1.10	1.10	35.90	119.01
1182	11.82	27.07	1.11	1.11	35.91	118.99
1183	11.83	26.77	1.09	1.09	35.98	118.90
1184	11.84	26.41	1.07	1.07	36.10	118.72
1185	11.85	25.99	1.04	1.04	36.24	118.51
1186	11.86	25.54	1.02	1.02	36.40	118.29
1187	11.87	25.08	0.99	0.99	36.57	118.06
1188	11.88	24.64	0.96	0.96	36.74	117.83
1189	11.89	24.24	0.94	0.94	36.89	117.62
1190	11.90	23.90	0.92	0.92	37.01	117.45
1191	11.91	23.71	0.91	0.91	37.04	117.31
1192	11.92	23.63	0.90	0.90	37.00	117.19
1193	11.93	23.54	0.88	0.88	36.90	117.07
1194	11.94	23.44	0.87	0.87	36.78	116.93
1195	11.95	23.33	0.85	0.85	36.66	116.78
1196	11.96	23.22	0.84	0.84	36.54	116.63
1197	11.97	23.12	0.82	0.82	36.42	116.48
1198	11.98	23.03	0.81	0.81	36.32	116.35
1199	11.99	22.95	0.79	0.79	36.25	116.23
1200	12.00	22.78	0.78	0.78	36.24	116.08

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1201	12.01	22.51	0.76	0.76	36.29	115.89
1202	12.02	22.19	0.74	0.74	36.35	115.66
1203	12.03	21.84	0.72	0.72	36.42	115.41
1204	12.04	21.48	0.70	0.70	36.49	115.15
1205	12.05	21.13	0.68	0.68	36.57	114.89
1206	12.06	20.80	0.66	0.66	36.64	114.64
1207	12.07	20.52	0.64	0.64	36.72	114.42
1208	12.08	20.27	0.63	0.63	36.93	114.18
1209	12.09	19.64	0.61	0.61	37.35	113.88
1210	12.10	18.85	0.58	0.58	38.01	113.47
1211	12.11	17.95	0.55	0.55	38.81	112.99
1212	12.12	16.99	0.52	0.52	39.74	112.44
1213	12.13	16.01	0.49	0.49	40.76	111.86
1214	12.14	15.07	0.46	0.46	41.82	111.27
1215	12.15	14.21	0.44	0.44	42.88	110.70
1216	12.16	13.49	0.41	0.41	43.79	110.23
1217	12.17	13.08	0.40	0.40	44.48	109.93
1218	12.18	12.91	0.40	0.40	44.98	109.78
1219	12.19	12.70	0.40	0.40	45.44	109.70
1220	12.20	12.47	0.39	0.39	45.96	109.59
1221	12.21	12.23	0.39	0.39	46.52	109.48
1222	12.22	11.98	0.39	0.39	47.09	109.37
1223	12.23	11.75	0.38	0.38	47.64	109.26
1224	12.24	11.55	0.38	0.38	48.14	109.16
1225	12.25	11.38	0.38	0.38	48.60	109.07
1226	12.26	11.24	0.38	0.38	49.06	109.00
1227	12.27	11.05	0.37	0.37	49.60	108.92
1228	12.28	10.83	0.37	0.37	50.25	108.83
1229	12.29	10.60	0.37	0.37	50.97	108.73
1230	12.30	10.35	0.37	0.37	51.72	108.62
1231	12.31	10.11	0.36	0.36	52.48	108.50
1232	12.32	9.89	0.36	0.36	53.20	108.38
1233	12.33	9.70	0.36	0.36	53.84	108.28
1234	12.34	9.55	0.35	0.35	54.42	108.18
1235	12.35	9.39	0.35	0.35	55.03	108.08
1236	12.36	9.19	0.35	0.35	55.78	107.96
1237	12.37	8.96	0.34	0.34	56.65	107.82
1238	12.38	8.72	0.34	0.34	57.60	107.65
1239	12.39	8.48	0.33	0.33	58.61	107.48
1240	12.40	8.24	0.33	0.33	59.60	107.31
1241	12.41	8.03	0.33	0.33	60.53	107.14
1242	12.42	7.85	0.32	0.32	61.33	107.00
1243	12.43	7.72	0.32	0.32	62.01	106.88
1244	12.44	7.61	0.32	0.32	62.64	106.78
1245	12.45	7.47	0.31	0.31	63.35	106.67
1246	12.46	7.31	0.31	0.31	64.15	106.54
1247	12.47	7.15	0.31	0.31	65.01	106.40
1248	12.48	6.99	0.30	0.30	65.89	106.26

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1249	12.49	6.84	0.30	0.30	66.75	106.11
1250	12.50	6.70	0.29	0.29	67.53	105.98
1251	12.51	6.59	0.29	0.29	68.15	105.88
1252	12.52	6.53	0.29	0.29	68.64	105.80
1253	12.53	6.47	0.29	0.29	69.06	105.74
1254	12.54	6.40	0.29	0.29	69.52	105.67
1255	12.55	6.32	0.29	0.29	70.04	105.59
1256	12.56	6.24	0.28	0.28	70.58	105.50
1257	12.57	6.16	0.28	0.28	71.11	105.42
1258	12.58	6.08	0.28	0.28	71.62	105.34
1259	12.59	6.02	0.28	0.28	72.05	105.27
1260	12.60	5.97	0.28	0.28	72.32	105.23
1261	12.61	5.97	0.28	0.28	72.44	105.21
1262	12.62	5.97	0.28	0.28	72.45	105.21
1263	12.63	5.97	0.28	0.28	72.47	105.21
1264	12.64	5.97	0.28	0.28	72.48	105.21
1265	12.65	5.97	0.28	0.28	72.49	105.21
1266	12.66	5.97	0.28	0.28	72.51	105.21
1267	12.67	5.97	0.28	0.28	72.52	105.21
1268	12.68	5.97	0.28	0.28	72.52	105.21
1269	12.69	5.97	0.28	0.28	72.49	105.19
1270	12.70	5.97	0.27	0.27	72.41	105.16
1271	12.71	5.97	0.27	0.27	72.29	105.11
1272	12.72	5.97	0.27	0.27	72.16	105.06
1273	12.73	5.97	0.27	0.27	72.02	105.00
1274	12.74	5.97	0.27	0.27	71.87	104.94
1275	12.75	5.97	0.26	0.26	71.74	104.89
1276	12.76	5.97	0.26	0.26	71.63	104.84
1277	12.77	5.97	0.26	0.26	71.51	104.80
1278	12.78	5.97	0.26	0.26	71.38	104.74
1279	12.79	5.97	0.26	0.26	71.21	104.68
1280	12.80	5.97	0.25	0.25	71.00	104.59
1281	12.81	5.97	0.25	0.25	70.77	104.50
1282	12.82	5.97	0.25	0.25	70.53	104.41
1283	12.83	5.97	0.24	0.24	70.29	104.32
1284	12.84	5.97	0.24	0.24	70.08	104.23
1285	12.85	5.97	0.24	0.24	69.89	104.16
1286	12.86	5.97	0.24	0.24	69.71	104.09
1287	12.87	5.97	0.23	0.23	69.52	104.01
1288	12.88	5.97	0.23	0.23	69.29	103.92
1289	12.89	5.97	0.23	0.23	69.03	103.81
1290	12.90	5.97	0.22	0.22	68.75	103.70
1291	12.91	5.97	0.22	0.22	68.46	103.58
1292	12.92	5.97	0.22	0.22	68.17	103.47
1293	12.93	5.97	0.21	0.21	67.92	103.36
1294	12.94	5.97	0.21	0.21	67.69	103.27
1295	12.95	5.97	0.21	0.21	67.47	103.18
1296	12.96	5.97	0.21	0.21	67.22	103.08

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1297	12.97	5.97	0.20	0.20	66.91	102.95
1298	12.98	5.97	0.20	0.20	66.56	102.81
1299	12.99	5.97	0.19	0.19	66.19	102.65
1300	13.00	5.97	0.19	0.19	65.82	102.50
1301	13.01	5.97	0.19	0.19	65.47	102.35
1302	13.02	5.97	0.18	0.18	65.15	102.22
1303	13.03	5.97	0.18	0.18	65.04	102.06
1304	13.04	5.89	0.18	0.18	65.18	101.84
1305	13.05	5.76	0.17	0.17	65.59	101.54
1306	13.06	5.62	0.16	0.16	66.13	101.16
1307	13.07	5.46	0.15	0.15	66.75	100.75
1308	13.08	5.30	0.15	0.15	67.42	100.31
1309	13.09	5.14	0.14	0.14	68.11	99.87
1310	13.10	4.99	0.13	0.13	68.79	99.46
1311	13.11	4.86	0.13	0.13	69.43	99.08
1312	13.12	4.76	0.12	0.12	70.20	98.72
1313	13.13	4.60	0.12	0.12	71.24	98.30
1314	13.14	4.39	0.11	0.11	72.69	97.78
1315	13.15	4.17	0.10	0.10	74.49	97.16
1316	13.16	3.93	0.10	0.10	76.60	96.47
1317	13.17	3.68	0.09	0.09	78.99	95.73
1318	13.18	3.45	0.08	0.08	81.57	94.98
1319	13.19	3.24	0.08	0.08	84.21	94.27
1320	13.20	3.06	0.07	0.07	86.50	93.68
1321	13.21	2.96	0.07	0.07	88.20	93.25
1322	13.22	2.90	0.07	0.07	89.42	92.95
1323	13.23	2.83	0.06	0.06	90.59	92.67
1324	13.24	2.76	0.06	0.06	91.96	92.34
1325	13.25	2.67	0.06	0.06	93.47	91.99
1326	13.26	2.59	0.06	0.06	95.06	91.64
1327	13.27	2.52	0.05	0.05	96.66	91.29
1328	13.28	2.45	0.05	0.05	98.15	90.98
1329	13.29	2.40	0.05	0.05	100.00	90.79
1330	13.30	2.39	0.05	0.05	100.00	90.72
1331	13.31	2.39	0.05	0.05	100.00	90.75
1332	13.32	2.39	0.05	0.05	100.00	90.81
1333	13.33	2.39	0.05	0.05	100.00	90.87
1334	13.34	2.39	0.05	0.05	100.00	90.93
1335	13.35	2.39	0.05	0.05	100.00	90.99
1336	13.36	2.39	0.05	0.05	100.00	91.04
1337	13.37	2.39	0.05	0.05	100.00	91.12
1338	13.38	2.40	0.06	0.06	100.00	91.35
1339	13.39	2.51	0.06	0.06	98.24	91.78
1340	13.40	2.65	0.06	0.06	95.56	92.40
1341	13.41	2.80	0.07	0.07	92.85	93.07
1342	13.42	2.96	0.07	0.07	90.28	93.75
1343	13.43	3.12	0.08	0.08	87.95	94.40
1344	13.44	3.28	0.08	0.08	85.95	94.99

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1345	13.45	3.42	0.09	0.09	84.29	95.51
1346	13.46	3.54	0.09	0.09	82.87	95.96
1347	13.47	3.66	0.10	0.10	81.37	96.42
1348	13.48	3.84	0.10	0.10	79.63	96.94
1349	13.49	4.05	0.11	0.11	77.67	97.55
1350	13.50	4.28	0.12	0.12	75.70	98.19
1351	13.51	4.53	0.13	0.13	73.85	98.83
1352	13.52	4.77	0.14	0.14	72.19	99.43
1353	13.53	4.99	0.14	0.14	70.75	99.98
1354	13.54	5.19	0.15	0.15	69.59	100.44
1355	13.55	5.36	0.16	0.16	68.96	100.72
1356	13.56	5.35	0.16	0.16	68.85	100.83
1357	13.57	5.30	0.16	0.16	69.18	100.81
1358	13.58	5.25	0.16	0.16	69.62	100.76
1359	13.59	5.20	0.16	0.16	70.10	100.71
1360	13.60	5.15	0.16	0.16	70.59	100.65
1361	13.61	5.09	0.15	0.15	71.08	100.60
1362	13.62	5.05	0.15	0.15	71.54	100.55
1363	13.63	5.00	0.15	0.15	71.94	100.51
1364	13.64	4.98	0.15	0.15	72.29	100.53
1365	13.65	4.98	0.16	0.16	72.63	100.61
1366	13.66	4.98	0.16	0.16	73.00	100.75
1367	13.67	4.98	0.16	0.16	73.41	100.90
1368	13.68	4.98	0.17	0.17	73.84	101.06
1369	13.69	4.98	0.17	0.17	74.26	101.21
1370	13.70	4.98	0.17	0.17	74.66	101.36
1371	13.71	4.98	0.18	0.18	75.02	101.49
1372	13.72	4.98	0.18	0.18	75.18	101.61
1373	13.73	5.02	0.18	0.18	74.98	101.75
1374	13.74	5.12	0.19	0.19	74.41	101.94
1375	13.75	5.24	0.19	0.19	73.62	102.16
1376	13.76	5.37	0.19	0.19	72.78	102.40
1377	13.77	5.50	0.20	0.20	71.94	102.65
1378	13.78	5.64	0.20	0.20	71.14	102.88
1379	13.79	5.76	0.21	0.21	70.42	103.10
1380	13.80	5.87	0.21	0.21	69.80	103.29
1381	13.81	5.96	0.22	0.22	69.55	103.34
1382	13.82	5.88	0.21	0.21	69.67	103.23
1383	13.83	5.76	0.21	0.21	70.18	102.95
1384	13.84	5.61	0.20	0.20	70.84	102.61
1385	13.85	5.45	0.19	0.19	71.58	102.23
1386	13.86	5.29	0.18	0.18	72.38	101.84
1387	13.87	5.13	0.17	0.17	73.21	101.44
1388	13.88	4.98	0.17	0.17	74.01	101.07
1389	13.89	4.86	0.16	0.16	74.76	100.74
1390	13.90	4.76	0.16	0.16	75.59	100.49
1391	13.91	4.65	0.15	0.15	76.62	100.28
1392	13.92	4.51	0.15	0.15	77.95	100.06

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1393	13.93	4.36	0.15	0.15	79.53	99.80
1394	13.94	4.20	0.14	0.14	81.29	99.51
1395	13.95	4.04	0.14	0.14	83.18	99.20
1396	13.96	3.88	0.13	0.13	85.09	98.90
1397	13.97	3.74	0.13	0.13	86.93	98.61
1398	13.98	3.63	0.13	0.13	88.39	98.41
1399	13.99	3.58	0.13	0.13	89.35	98.36
1400	14.00	3.58	0.13	0.13	89.90	98.44
1401	14.01	3.58	0.13	0.13	90.34	98.58
1402	14.02	3.58	0.14	0.14	90.82	98.74
1403	14.03	3.58	0.14	0.14	91.32	98.90
1404	14.04	3.58	0.14	0.14	91.80	99.05
1405	14.05	3.58	0.14	0.14	92.24	99.19
1406	14.06	3.58	0.15	0.15	92.63	99.31
1407	14.07	3.58	0.15	0.15	92.59	99.51
1408	14.08	3.68	0.15	0.15	92.01	99.83
1409	14.09	3.80	0.16	0.16	90.93	100.30
1410	14.10	3.95	0.17	0.17	89.72	100.83
1411	14.11	4.11	0.19	0.19	88.52	101.39
1412	14.12	4.27	0.20	0.20	87.39	101.94
1413	14.13	4.43	0.21	0.21	86.37	102.45
1414	14.14	4.58	0.22	0.22	85.50	102.91
1415	14.15	4.70	0.23	0.23	84.76	103.30
1416	14.16	4.81	0.24	0.24	83.94	103.67
1417	14.17	4.98	0.25	0.25	82.94	104.08
1418	14.18	5.18	0.26	0.26	81.73	104.57
1419	14.19	5.41	0.28	0.28	80.45	105.09
1420	14.20	5.65	0.30	0.30	79.21	105.63
1421	14.21	5.90	0.32	0.32	78.06	106.15
1422	14.22	6.13	0.33	0.33	77.04	106.62
1423	14.23	6.34	0.35	0.35	76.18	107.04
1424	14.24	6.51	0.36	0.36	75.46	107.37
1425	14.25	6.66	0.37	0.37	74.72	107.66
1426	14.26	6.84	0.38	0.38	73.88	107.93
1427	14.27	7.05	0.39	0.39	72.92	108.23
1428	14.28	7.28	0.41	0.41	71.90	108.54
1429	14.29	7.53	0.42	0.42	70.90	108.86
1430	14.30	7.77	0.43	0.43	69.96	109.17
1431	14.31	7.99	0.45	0.45	69.12	109.45
1432	14.32	8.19	0.46	0.46	68.42	109.69
1433	14.33	8.35	0.47	0.47	67.87	109.87
1434	14.34	8.46	0.47	0.47	67.39	110.01
1435	14.35	8.59	0.48	0.48	66.92	110.14
1436	14.36	8.73	0.49	0.49	66.39	110.28
1437	14.37	8.89	0.49	0.49	65.83	110.44
1438	14.38	9.06	0.50	0.50	65.28	110.59
1439	14.39	9.21	0.51	0.51	64.75	110.74
1440	14.40	9.36	0.52	0.52	64.28	110.87

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1441	14.41	9.48	0.52	0.52	63.94	110.97
1442	14.42	9.54	0.52	0.52	63.88	111.03
1443	14.43	9.49	0.53	0.53	64.09	111.06
1444	14.44	9.42	0.53	0.53	64.52	111.07
1445	14.45	9.34	0.53	0.53	65.00	111.08
1446	14.46	9.26	0.53	0.53	65.50	111.09
1447	14.47	9.18	0.53	0.53	66.02	111.10
1448	14.48	9.10	0.54	0.54	66.51	111.10
1449	14.49	9.04	0.54	0.54	66.95	111.10
1450	14.50	8.98	0.54	0.54	67.46	111.07
1451	14.51	8.82	0.53	0.53	68.23	110.96
1452	14.52	8.54	0.52	0.52	69.37	110.76
1453	14.53	8.21	0.51	0.51	70.87	110.48
1454	14.54	7.84	0.50	0.50	72.61	110.15
1455	14.55	7.46	0.48	0.48	74.52	109.79
1456	14.56	7.09	0.46	0.46	76.54	109.41
1457	14.57	6.74	0.45	0.45	78.56	109.03
1458	14.58	6.43	0.43	0.43	80.44	108.67
1459	14.59	6.18	0.42	0.42	81.90	108.40
1460	14.60	6.07	0.41	0.41	83.01	108.18
1461	14.61	5.94	0.41	0.41	83.92	108.00
1462	14.62	5.80	0.40	0.40	84.98	107.79
1463	14.63	5.64	0.39	0.39	86.17	107.56
1464	14.64	5.47	0.38	0.38	87.43	107.32
1465	14.65	5.32	0.37	0.37	88.70	107.07
1466	14.66	5.17	0.36	0.36	89.92	106.84
1467	14.67	5.05	0.35	0.35	90.87	106.66
1468	14.68	5.00	0.35	0.35	91.13	106.62
1469	14.69	5.09	0.36	0.36	90.69	106.72
1470	14.70	5.21	0.36	0.36	89.75	106.91
1471	14.71	5.33	0.37	0.37	88.73	107.12
1472	14.72	5.47	0.38	0.38	87.69	107.33
1473	14.73	5.60	0.39	0.39	86.69	107.55
1474	14.74	5.73	0.40	0.40	85.77	107.74
1475	14.75	5.85	0.40	0.40	84.98	107.91
1476	14.76	5.94	0.41	0.41	84.42	108.03
1477	14.77	5.97	0.41	0.41	84.10	108.07
1478	14.78	5.97	0.41	0.41	83.96	108.06
1479	14.79	5.97	0.41	0.41	83.87	108.02
1480	14.80	5.97	0.40	0.40	83.76	107.98
1481	14.81	5.97	0.40	0.40	83.64	107.94
1482	14.82	5.97	0.40	0.40	83.53	107.90
1483	14.83	5.97	0.40	0.40	83.42	107.86
1484	14.84	5.97	0.39	0.39	83.33	107.83
1485	14.85	5.97	0.39	0.39	83.03	107.85
1486	14.86	6.07	0.40	0.40	82.44	107.93
1487	14.87	6.20	0.40	0.40	81.53	108.08
1488	14.88	6.35	0.41	0.41	80.51	108.25

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1489	14.89	6.51	0.42	0.42	79.45	108.42
1490	14.90	6.67	0.42	0.42	78.40	108.59
1491	14.91	6.83	0.43	0.43	77.42	108.74
1492	14.92	6.98	0.43	0.43	76.55	108.88
1493	14.93	7.10	0.44	0.44	75.82	109.00
1494	14.94	7.20	0.44	0.44	75.16	109.10
1495	14.95	7.31	0.44	0.44	74.49	109.20
1496	14.96	7.45	0.45	0.45	73.72	109.31
1497	14.97	7.60	0.45	0.45	72.87	109.44
1498	14.98	7.76	0.46	0.46	72.00	109.56
1499	14.99	7.92	0.46	0.46	71.14	109.68
1500	15.00	8.08	0.47	0.47	70.35	109.79
1501	15.01	8.22	0.47	0.47	69.66	109.89
1502	15.02	8.33	0.47	0.47	69.28	109.93
1503	15.03	8.29	0.47	0.47	69.33	109.88
1504	15.04	8.14	0.46	0.46	69.79	109.74
1505	15.05	7.98	0.45	0.45	70.46	109.55
1506	15.06	7.79	0.44	0.44	71.23	109.34
1507	15.07	7.60	0.43	0.43	72.05	109.12
1508	15.08	7.42	0.42	0.42	72.88	108.89
1509	15.09	7.24	0.41	0.41	73.69	108.67
1510	15.10	7.09	0.41	0.41	74.42	108.48
1511	15.11	6.97	0.40	0.40	74.87	108.41
1512	15.12	7.02	0.41	0.41	75.05	108.46
1513	15.13	7.08	0.42	0.42	75.00	108.63
1514	15.14	7.16	0.42	0.42	74.95	108.82
1515	15.15	7.24	0.44	0.44	74.89	109.02
1516	15.16	7.32	0.45	0.45	74.83	109.23
1517	15.17	7.40	0.46	0.46	74.78	109.42
1518	15.18	7.47	0.47	0.47	74.74	109.60
1519	15.19	7.53	0.48	0.48	74.62	109.77
1520	15.20	7.63	0.48	0.48	74.20	109.98
1521	15.21	7.86	0.50	0.50	73.43	110.26
1522	15.22	8.15	0.52	0.52	72.39	110.61
1523	15.23	8.47	0.54	0.54	71.29	111.00
1524	15.24	8.80	0.56	0.56	70.19	111.39
1525	15.25	9.14	0.59	0.59	69.16	111.76
1526	15.26	9.45	0.61	0.61	68.24	112.11
1527	15.27	9.74	0.63	0.63	67.46	112.41
1528	15.28	9.97	0.64	0.64	66.74	112.65
1529	15.29	10.20	0.66	0.66	65.96	112.87
1530	15.30	10.51	0.67	0.67	65.01	113.09
1531	15.31	10.87	0.69	0.69	63.90	113.34
1532	15.32	11.26	0.70	0.70	62.74	113.59
1533	15.33	11.67	0.72	0.72	61.59	113.84
1534	15.34	12.07	0.73	0.73	60.50	114.08
1535	15.35	12.44	0.75	0.75	59.53	114.29
1536	15.36	12.77	0.76	0.76	58.72	114.46

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1537	15.37	13.02	0.77	0.77	58.04	114.60
1538	15.38	13.24	0.78	0.78	57.40	114.72
1539	15.39	13.52	0.78	0.78	56.72	114.83
1540	15.40	13.83	0.79	0.79	55.95	114.96
1541	15.41	14.17	0.80	0.80	55.14	115.09
1542	15.42	14.51	0.81	0.81	54.35	115.22
1543	15.43	14.84	0.81	0.81	53.63	115.34
1544	15.44	15.14	0.82	0.82	52.99	115.44
1545	15.45	15.40	0.82	0.82	52.54	115.49
1546	15.46	15.44	0.82	0.82	52.44	115.44
1547	15.47	15.12	0.80	0.80	52.69	115.27
1548	15.48	14.74	0.78	0.78	53.18	115.00
1549	15.49	14.32	0.75	0.75	53.76	114.70
1550	15.50	13.87	0.73	0.73	54.39	114.37
1551	15.51	13.43	0.70	0.70	55.09	114.03
1552	15.52	13.01	0.68	0.68	55.79	113.70
1553	15.53	12.63	0.66	0.66	56.44	113.40
1554	15.54	12.32	0.64	0.64	57.05	113.15
1555	15.55	12.07	0.63	0.63	57.69	112.93
1556	15.56	11.76	0.61	0.61	58.44	112.71
1557	15.57	11.40	0.60	0.60	59.36	112.46
1558	15.58	11.01	0.58	0.58	60.41	112.17
1559	15.59	10.60	0.57	0.57	61.54	111.86
1560	15.60	10.20	0.55	0.55	62.72	111.54
1561	15.61	9.83	0.53	0.53	63.86	111.24
1562	15.62	9.50	0.52	0.52	64.91	110.96
1563	15.63	9.26	0.51	0.51	65.63	110.79
1564	15.64	9.23	0.51	0.51	66.07	110.72
1565	15.65	9.20	0.51	0.51	66.31	110.74
1566	15.66	9.16	0.51	0.51	66.59	110.75
1567	15.67	9.12	0.51	0.51	66.89	110.76
1568	15.68	9.08	0.51	0.51	67.19	110.78
1569	15.69	9.04	0.52	0.52	67.48	110.79
1570	15.70	9.00	0.52	0.52	67.75	110.80
1571	15.71	8.97	0.52	0.52	67.99	110.81
1572	15.72	8.94	0.52	0.52	68.24	110.80
1573	15.73	8.88	0.52	0.52	68.54	110.78
1574	15.74	8.81	0.52	0.52	68.91	110.75
1575	15.75	8.74	0.52	0.52	69.32	110.71
1576	15.76	8.66	0.51	0.51	69.75	110.67
1577	15.77	8.58	0.51	0.51	70.19	110.63
1578	15.78	8.50	0.51	0.51	70.61	110.59
1579	15.79	8.43	0.51	0.51	70.99	110.56
1580	15.80	8.37	0.51	0.51	71.30	110.52
1581	15.81	8.33	0.51	0.51	71.57	110.47
1582	15.82	8.26	0.50	0.50	71.84	110.41
1583	15.83	8.19	0.50	0.50	72.14	110.33
1584	15.84	8.11	0.50	0.50	72.48	110.24

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1585	15.85	8.03	0.49	0.49	72.83	110.16
1586	15.86	7.95	0.49	0.49	73.18	110.07
1587	15.87	7.88	0.48	0.48	73.51	109.98
1588	15.88	7.81	0.48	0.48	73.80	109.91
1589	15.89	7.76	0.48	0.48	74.02	109.83
1590	15.90	7.71	0.47	0.47	74.19	109.73
1591	15.91	7.64	0.46	0.46	74.35	109.61
1592	15.92	7.57	0.46	0.46	74.52	109.46
1593	15.93	7.49	0.45	0.45	74.72	109.30
1594	15.94	7.41	0.44	0.44	74.91	109.14
1595	15.95	7.33	0.43	0.43	75.11	108.98
1596	15.96	7.26	0.42	0.42	75.30	108.83
1597	15.97	7.20	0.42	0.42	75.43	108.72
1598	15.98	7.17	0.41	0.41	75.48	108.64
1599	15.99	7.17	0.41	0.41	75.44	108.60
1600	16.00	7.17	0.41	0.41	75.34	108.56
1601	16.01	7.17	0.41	0.41	75.23	108.52
1602	16.02	7.17	0.41	0.41	75.11	108.47
1603	16.03	7.17	0.40	0.40	74.99	108.43
1604	16.04	7.17	0.40	0.40	74.88	108.39
1605	16.05	7.17	0.40	0.40	74.78	108.35
1606	16.06	7.17	0.40	0.40	74.74	108.33
1607	16.07	7.17	0.40	0.40	74.77	108.33
1608	16.08	7.17	0.40	0.40	74.86	108.36
1609	16.09	7.17	0.40	0.40	74.98	108.40
1610	16.10	7.17	0.40	0.40	75.11	108.44
1611	16.11	7.17	0.41	0.41	75.24	108.48
1612	16.12	7.17	0.41	0.41	75.38	108.52
1613	16.13	7.17	0.41	0.41	75.50	108.55
1614	16.14	7.17	0.41	0.41	75.61	108.58
1615	16.15	7.17	0.41	0.41	75.73	108.62
1616	16.16	7.17	0.42	0.42	75.88	108.67
1617	16.17	7.17	0.42	0.42	76.07	108.73
1618	16.18	7.17	0.42	0.42	76.29	108.80
1619	16.19	7.17	0.43	0.43	76.52	108.87
1620	16.20	7.17	0.43	0.43	76.75	108.94
1621	16.21	7.17	0.44	0.44	76.98	109.01
1622	16.22	7.17	0.44	0.44	77.18	109.07
1623	16.23	7.17	0.44	0.44	77.21	109.16
1624	16.24	7.25	0.45	0.45	76.83	109.33
1625	16.25	7.48	0.47	0.47	76.00	109.61
1626	16.26	7.76	0.48	0.48	74.88	109.98
1627	16.27	8.07	0.51	0.51	73.70	110.38
1628	16.28	8.39	0.53	0.53	72.53	110.78
1629	16.29	8.72	0.55	0.55	71.45	111.16
1630	16.30	9.02	0.57	0.57	70.48	111.51
1631	16.31	9.29	0.59	0.59	69.66	111.81
1632	16.32	9.51	0.60	0.60	68.91	112.07

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1633	16.33	9.75	0.62	0.62	68.07	112.30
1634	16.34	10.06	0.63	0.63	67.05	112.55
1635	16.35	10.43	0.65	0.65	65.89	112.83
1636	16.36	10.82	0.67	0.67	64.69	113.11
1637	16.37	11.23	0.68	0.68	63.50	113.40
1638	16.38	11.63	0.70	0.70	62.40	113.66
1639	16.39	12.00	0.72	0.72	61.42	113.90
1640	16.40	12.32	0.73	0.73	60.60	114.09
1641	16.41	12.57	0.74	0.74	59.81	114.26
1642	16.42	12.89	0.75	0.75	58.93	114.42
1643	16.43	13.29	0.76	0.76	57.88	114.59
1644	16.44	13.74	0.77	0.77	56.72	114.77
1645	16.45	14.23	0.78	0.78	55.53	114.95
1646	16.46	14.71	0.79	0.79	54.36	115.12
1647	16.47	15.18	0.80	0.80	53.32	115.28
1648	16.48	15.61	0.81	0.81	52.40	115.40
1649	16.49	15.97	0.81	0.81	51.61	115.51
1650	16.50	16.32	0.82	0.82	50.81	115.65
1651	16.51	16.84	0.83	0.83	49.90	115.82
1652	16.52	17.47	0.84	0.84	48.83	116.02
1653	16.53	18.17	0.86	0.86	47.69	116.23
1654	16.54	18.90	0.87	0.87	46.53	116.42
1655	16.55	19.63	0.88	0.88	45.42	116.60
1656	16.56	20.31	0.89	0.89	44.40	116.75
1657	16.57	20.92	0.90	0.90	43.53	116.88
1658	16.58	21.42	0.90	0.90	42.90	116.93
1659	16.59	21.53	0.89	0.89	42.46	116.91
1660	16.60	21.58	0.88	0.88	42.14	116.81
1661	16.61	21.64	0.86	0.86	41.78	116.69
1662	16.62	21.71	0.85	0.85	41.40	116.55
1663	16.63	21.77	0.83	0.83	40.99	116.41
1664	16.64	21.83	0.81	0.81	40.60	116.26
1665	16.65	21.89	0.79	0.79	40.22	116.12
1666	16.66	21.94	0.78	0.78	39.92	115.99
1667	16.67	21.95	0.77	0.77	39.81	115.87
1668	16.68	21.68	0.76	0.76	39.89	115.74
1669	16.69	21.35	0.75	0.75	40.15	115.58
1670	16.70	20.97	0.73	0.73	40.44	115.40
1671	16.71	20.57	0.72	0.72	40.76	115.20
1672	16.72	20.16	0.70	0.70	41.10	114.99
1673	16.73	19.77	0.69	0.69	41.43	114.79
1674	16.74	19.42	0.67	0.67	41.74	114.61
1675	16.75	19.12	0.66	0.66	42.05	114.47
1676	16.76	18.89	0.66	0.66	42.44	114.38
1677	16.77	18.60	0.66	0.66	42.95	114.34
1678	16.78	18.27	0.66	0.66	43.60	114.32
1679	16.79	17.89	0.66	0.66	44.34	114.28
1680	16.80	17.50	0.66	0.66	45.11	114.23

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1681	16.81	17.12	0.66	0.66	45.89	114.18
1682	16.82	16.75	0.66	0.66	46.64	114.12
1683	16.83	16.43	0.66	0.66	47.32	114.06
1684	16.84	16.17	0.66	0.66	47.98	114.00
1685	16.85	15.82	0.66	0.66	48.77	113.92
1686	16.86	15.35	0.65	0.65	49.77	113.80
1687	16.87	14.80	0.65	0.65	50.99	113.64
1688	16.88	14.20	0.64	0.64	52.36	113.45
1689	16.89	13.59	0.63	0.63	53.82	113.24
1690	16.90	13.00	0.62	0.62	55.38	113.00
1691	16.91	12.44	0.61	0.61	56.90	112.77
1692	16.92	11.97	0.60	0.60	58.24	112.55
1693	16.93	11.63	0.59	0.59	59.29	112.40
1694	16.94	11.46	0.59	0.59	60.12	112.32
1695	16.95	11.26	0.59	0.59	60.91	112.26
1696	16.96	11.04	0.58	0.58	61.80	112.20
1697	16.97	10.79	0.58	0.58	62.78	112.12
1698	16.98	10.55	0.58	0.58	63.78	112.03
1699	16.99	10.32	0.58	0.58	64.76	111.95
1700	17.00	10.10	0.57	0.57	65.67	111.86
1701	17.01	9.93	0.57	0.57	66.31	111.80
1702	17.02	9.89	0.57	0.57	66.56	111.80
1703	17.03	9.98	0.58	0.58	66.42	111.86
1704	17.04	10.08	0.58	0.58	66.10	111.94
1705	17.05	10.20	0.59	0.59	65.74	112.04
1706	17.06	10.32	0.59	0.59	65.38	112.14
1707	17.07	10.44	0.60	0.60	65.02	112.23
1708	17.08	10.56	0.60	0.60	64.69	112.32
1709	17.09	10.66	0.61	0.61	64.40	112.40
1710	17.10	10.74	0.61	0.61	64.17	112.43
1711	17.11	10.75	0.61	0.61	63.95	112.41
1712	17.12	10.75	0.60	0.60	63.73	112.33
1713	17.13	10.75	0.59	0.59	63.46	112.23
1714	17.14	10.75	0.58	0.58	63.17	112.12
1715	17.15	10.75	0.57	0.57	62.87	112.00
1716	17.16	10.75	0.56	0.56	62.57	111.89
1717	17.17	10.75	0.56	0.56	62.29	111.78
1718	17.18	10.75	0.55	0.55	62.09	111.68
1719	17.19	10.72	0.54	0.54	62.15	111.53
1720	17.20	10.48	0.53	0.53	62.52	111.31
1721	17.21	10.19	0.51	0.51	63.18	110.99
1722	17.22	9.86	0.49	0.49	63.97	110.62
1723	17.23	9.51	0.47	0.47	64.86	110.22
1724	17.24	9.16	0.45	0.45	65.81	109.80
1725	17.25	8.82	0.43	0.43	66.78	109.38
1726	17.26	8.52	0.41	0.41	67.71	108.99
1727	17.27	8.26	0.40	0.40	68.58	108.66
1728	17.28	8.05	0.38	0.38	69.50	108.37

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1729	17.29	7.80	0.37	0.37	70.62	108.07
1730	17.30	7.49	0.36	0.36	72.03	107.71
1731	17.31	7.15	0.35	0.35	73.69	107.31
1732	17.32	6.80	0.33	0.33	75.55	106.86
1733	17.33	6.45	0.32	0.32	77.55	106.39
1734	17.34	6.13	0.30	0.30	79.58	105.92
1735	17.35	5.84	0.29	0.29	81.52	105.49
1736	17.36	5.60	0.28	0.28	82.86	105.21
1737	17.37	5.59	0.28	0.28	83.51	105.11
1738	17.38	5.61	0.28	0.28	83.56	105.17
1739	17.39	5.63	0.28	0.28	83.53	105.26
1740	17.40	5.66	0.29	0.29	83.50	105.35
1741	17.41	5.69	0.29	0.29	83.47	105.44
1742	17.42	5.71	0.29	0.29	83.44	105.53
1743	17.43	5.74	0.30	0.30	83.42	105.62
1744	17.44	5.76	0.30	0.30	83.40	105.69
1745	17.45	5.78	0.30	0.30	83.39	105.75
1746	17.46	5.79	0.30	0.30	83.39	105.82
1747	17.47	5.82	0.31	0.31	83.39	105.90
1748	17.48	5.84	0.31	0.31	83.38	106.00
1749	17.49	5.87	0.31	0.31	83.38	106.09
1750	17.50	5.90	0.32	0.32	83.38	106.19
1751	17.51	5.92	0.32	0.32	83.37	106.28
1752	17.52	5.95	0.32	0.32	83.37	106.37
1753	17.53	5.97	0.33	0.33	83.28	106.46
1754	17.54	6.02	0.33	0.33	82.99	106.61
1755	17.55	6.14	0.34	0.34	82.47	106.83
1756	17.56	6.29	0.35	0.35	81.79	107.10
1757	17.57	6.44	0.36	0.36	81.07	107.40
1758	17.58	6.60	0.38	0.38	80.36	107.71
1759	17.59	6.77	0.39	0.39	79.69	108.00
1760	17.60	6.92	0.40	0.40	79.09	108.27
1761	17.61	7.05	0.41	0.41	78.58	108.50
1762	17.62	7.16	0.42	0.42	78.14	108.70
1763	17.63	7.26	0.43	0.43	77.73	108.89
1764	17.64	7.38	0.44	0.44	77.26	109.10
1765	17.65	7.53	0.45	0.45	76.74	109.34
1766	17.66	7.69	0.46	0.46	76.19	109.59
1767	17.67	7.85	0.47	0.47	75.66	109.84
1768	17.68	8.01	0.49	0.49	75.16	110.08
1769	17.69	8.16	0.50	0.50	74.71	110.30
1770	17.70	8.28	0.51	0.51	74.38	110.47
1771	17.71	8.35	0.52	0.52	74.30	110.56
1772	17.72	8.30	0.51	0.51	74.47	110.57
1773	17.73	8.23	0.51	0.51	74.84	110.52
1774	17.74	8.15	0.51	0.51	75.27	110.46
1775	17.75	8.07	0.51	0.51	75.72	110.40
1776	17.76	7.99	0.50	0.50	76.17	110.34

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1777	17.77	7.91	0.50	0.50	76.62	110.28
1778	17.78	7.84	0.50	0.50	77.02	110.23
1779	17.79	7.79	0.50	0.50	77.38	110.18
1780	17.80	7.74	0.50	0.50	77.73	110.15
1781	17.81	7.68	0.50	0.50	78.13	110.11
1782	17.82	7.61	0.49	0.49	78.60	110.06
1783	17.83	7.53	0.49	0.49	79.12	110.01
1784	17.84	7.45	0.49	0.49	79.67	109.96
1785	17.85	7.37	0.49	0.49	80.22	109.90
1786	17.86	7.29	0.49	0.49	80.75	109.85
1787	17.87	7.22	0.48	0.48	81.21	109.80
1788	17.88	7.17	0.48	0.48	81.54	109.78
1789	17.89	7.17	0.49	0.49	81.76	109.79
1790	17.90	7.17	0.49	0.49	81.90	109.83
1791	17.91	7.17	0.49	0.49	82.05	109.87
1792	17.92	7.17	0.49	0.49	82.21	109.91
1793	17.93	7.17	0.50	0.50	82.37	109.96
1794	17.94	7.17	0.50	0.50	82.53	110.01
1795	17.95	7.17	0.50	0.50	82.68	110.05
1796	17.96	7.17	0.51	0.51	82.77	110.09
1797	17.97	7.18	0.51	0.51	82.67	110.14
1798	17.98	7.26	0.51	0.51	82.37	110.22
1799	17.99	7.35	0.52	0.52	81.89	110.32
1800	18.00	7.45	0.52	0.52	81.35	110.43
1801	18.01	7.56	0.53	0.53	80.80	110.55
1802	18.02	7.66	0.54	0.54	80.25	110.67
1803	18.03	7.77	0.54	0.54	79.74	110.78
1804	18.04	7.86	0.55	0.55	79.29	110.87
1805	18.05	7.94	0.55	0.55	78.70	110.99
1806	18.06	8.13	0.56	0.56	77.70	111.19
1807	18.07	8.47	0.58	0.58	76.20	111.47
1808	18.08	8.87	0.60	0.60	74.40	111.81
1809	18.09	9.31	0.62	0.62	72.53	112.16
1810	18.10	9.77	0.63	0.63	70.70	112.50
1811	18.11	10.23	0.65	0.65	69.00	112.82
1812	18.12	10.66	0.67	0.67	67.50	113.09
1813	18.13	11.03	0.68	0.68	66.24	113.32
1814	18.14	11.33	0.69	0.69	64.96	113.57
1815	18.15	11.86	0.72	0.72	63.46	113.88
1816	18.16	12.54	0.74	0.74	61.63	114.28
1817	18.17	13.33	0.77	0.77	59.64	114.70
1818	18.18	14.18	0.80	0.80	57.65	115.12
1819	18.19	15.05	0.83	0.83	55.76	115.51
1820	18.20	15.89	0.85	0.85	54.03	115.85
1821	18.21	16.67	0.87	0.87	52.59	116.13
1822	18.22	17.33	0.89	0.89	51.44	116.35
1823	18.23	17.78	0.90	0.90	50.57	116.47
1824	18.24	18.06	0.90	0.90	49.83	116.53

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1825	18.25	18.40	0.89	0.89	49.08	116.54
1826	18.26	18.78	0.89	0.89	48.24	116.55
1827	18.27	19.19	0.88	0.88	47.36	116.55
1828	18.28	19.59	0.87	0.87	46.49	116.54
1829	18.29	19.98	0.87	0.87	45.66	116.52
1830	18.30	20.33	0.86	0.86	44.92	116.49
1831	18.31	20.61	0.85	0.85	44.40	116.44
1832	18.32	20.60	0.84	0.84	44.13	116.32
1833	18.33	20.40	0.82	0.82	44.05	116.14
1834	18.34	20.15	0.79	0.79	44.04	115.91
1835	18.35	19.88	0.77	0.77	44.02	115.65
1836	18.36	19.60	0.74	0.74	44.00	115.38
1837	18.37	19.33	0.72	0.72	43.99	115.10
1838	18.38	19.07	0.70	0.70	43.97	114.84
1839	18.39	18.85	0.68	0.68	43.96	114.61
1840	18.40	18.67	0.66	0.66	44.09	114.42
1841	18.41	18.35	0.65	0.65	44.39	114.25
1842	18.42	17.95	0.64	0.64	44.91	114.07
1843	18.43	17.48	0.63	0.63	45.54	113.87
1844	18.44	16.98	0.62	0.62	46.24	113.64
1845	18.45	16.47	0.60	0.60	46.97	113.40
1846	18.46	15.98	0.59	0.59	47.72	113.15
1847	18.47	15.52	0.57	0.57	48.43	112.92
1848	18.48	15.14	0.56	0.56	49.07	112.72
1849	18.49	14.82	0.56	0.56	49.75	112.54
1850	18.50	14.42	0.55	0.55	50.57	112.37
1851	18.51	13.94	0.54	0.54	51.60	112.16
1852	18.52	13.40	0.53	0.53	52.81	111.91
1853	18.53	12.83	0.51	0.51	54.16	111.62
1854	18.54	12.25	0.50	0.50	55.64	111.32
1855	18.55	11.71	0.49	0.49	57.12	111.01
1856	18.56	11.22	0.47	0.47	58.53	110.71
1857	18.57	10.81	0.46	0.46	59.72	110.47
1858	18.58	10.55	0.46	0.46	60.74	110.26
1859	18.59	10.29	0.45	0.45	61.73	110.08
1860	18.60	9.97	0.44	0.44	62.86	109.88
1861	18.61	9.63	0.43	0.43	64.15	109.64
1862	18.62	9.27	0.42	0.42	65.55	109.37
1863	18.63	8.92	0.41	0.41	67.01	109.10
1864	18.64	8.59	0.40	0.40	68.43	108.83
1865	18.65	8.30	0.39	0.39	69.74	108.59
1866	18.66	8.07	0.38	0.38	70.82	108.39
1867	18.67	7.92	0.38	0.38	71.77	108.21
1868	18.68	7.74	0.37	0.37	72.73	108.05
1869	18.69	7.53	0.37	0.37	73.87	107.85
1870	18.70	7.30	0.36	0.36	75.14	107.62
1871	18.71	7.07	0.35	0.35	76.50	107.39
1872	18.72	6.85	0.34	0.34	77.87	107.15

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1873	18.73	6.64	0.34	0.34	79.18	106.92
1874	18.74	6.47	0.33	0.33	80.31	106.73
1875	18.75	6.35	0.33	0.33	81.22	106.60
1876	18.76	6.28	0.32	0.32	82.01	106.51
1877	18.77	6.18	0.32	0.32	82.82	106.44
1878	18.78	6.08	0.32	0.32	83.75	106.37
1879	18.79	5.97	0.32	0.32	84.75	106.28
1880	18.80	5.87	0.32	0.32	85.77	106.19
1881	18.81	5.76	0.32	0.32	86.76	106.10
1882	18.82	5.67	0.31	0.31	87.67	106.02
1883	18.83	5.60	0.31	0.31	88.36	105.97
1884	18.84	5.57	0.31	0.31	88.80	105.96
1885	18.85	5.57	0.31	0.31	89.06	106.01
1886	18.86	5.57	0.32	0.32	89.29	106.08
1887	18.87	5.57	0.32	0.32	89.54	106.15
1888	18.88	5.57	0.32	0.32	89.80	106.23
1889	18.89	5.57	0.33	0.33	90.05	106.30
1890	18.90	5.57	0.33	0.33	90.29	106.37
1891	18.91	5.57	0.33	0.33	90.49	106.43
1892	18.92	5.57	0.34	0.34	90.46	106.51
1893	18.93	5.64	0.34	0.34	90.15	106.62
1894	18.94	5.73	0.35	0.35	89.56	106.78
1895	18.95	5.83	0.35	0.35	88.91	106.96
1896	18.96	5.94	0.36	0.36	88.22	107.16
1897	18.97	6.04	0.37	0.37	87.55	107.35
1898	18.98	6.15	0.38	0.38	86.92	107.53
1899	18.99	6.25	0.38	0.38	86.36	107.70
1900	19.00	6.33	0.39	0.39	85.89	107.83
1901	19.01	6.39	0.39	0.39	85.42	107.94
1902	19.02	6.47	0.40	0.40	84.90	108.04
1903	19.03	6.56	0.40	0.40	84.28	108.15
1904	19.04	6.66	0.40	0.40	83.59	108.27
1905	19.05	6.77	0.41	0.41	82.88	108.39
1906	19.06	6.88	0.41	0.41	82.19	108.50
1907	19.07	6.98	0.42	0.42	81.55	108.61
1908	19.08	7.07	0.42	0.42	80.99	108.71
1909	19.09	7.15	0.42	0.42	80.59	108.77
1910	19.10	7.17	0.42	0.42	80.33	108.78
1911	19.11	7.17	0.42	0.42	80.18	108.74
1912	19.12	7.17	0.42	0.42	80.03	108.69
1913	19.13	7.17	0.41	0.41	79.87	108.63
1914	19.14	7.17	0.41	0.41	79.70	108.57
1915	19.15	7.17	0.41	0.41	79.53	108.52
1916	19.16	7.17	0.40	0.40	79.38	108.46
1917	19.17	7.17	0.40	0.40	79.25	108.41
1918	19.18	7.17	0.40	0.40	79.27	108.34
1919	19.19	7.10	0.39	0.39	79.46	108.24
1920	19.20	7.01	0.39	0.39	79.83	108.09

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1921	19.21	6.91	0.38	0.38	80.27	107.92
1922	19.22	6.80	0.37	0.37	80.76	107.73
1923	19.23	6.69	0.36	0.36	81.26	107.54
1924	19.24	6.59	0.36	0.36	81.76	107.35
1925	19.25	6.49	0.35	0.35	82.23	107.17
1926	19.26	6.41	0.34	0.34	82.65	107.02
1927	19.27	6.35	0.34	0.34	83.04	106.88
1928	19.28	6.27	0.33	0.33	83.47	106.73
1929	19.29	6.18	0.33	0.33	83.97	106.56
1930	19.30	6.08	0.32	0.32	84.55	106.36
1931	19.31	5.97	0.31	0.31	85.17	106.15
1932	19.32	5.86	0.31	0.31	85.82	105.94
1933	19.33	5.76	0.30	0.30	86.46	105.73
1934	19.34	5.67	0.29	0.29	87.04	105.55
1935	19.35	5.59	0.29	0.29	87.42	105.41
1936	19.36	5.57	0.29	0.29	87.54	105.31
1937	19.37	5.57	0.28	0.28	87.43	105.24
1938	19.38	5.57	0.28	0.28	87.22	105.17
1939	19.39	5.57	0.28	0.28	86.99	105.09
1940	19.40	5.57	0.27	0.27	86.75	105.01
1941	19.41	5.57	0.27	0.27	86.51	104.92
1942	19.42	5.57	0.27	0.27	86.29	104.85
1943	19.43	5.57	0.27	0.27	86.10	104.78
1944	19.44	5.57	0.26	0.26	85.93	104.72
1945	19.45	5.57	0.26	0.26	85.77	104.66
1946	19.46	5.57	0.26	0.26	85.58	104.59
1947	19.47	5.57	0.26	0.26	85.36	104.52
1948	19.48	5.57	0.25	0.25	85.12	104.43
1949	19.49	5.57	0.25	0.25	84.88	104.35
1950	19.50	5.57	0.25	0.25	84.64	104.26
1951	19.51	5.57	0.25	0.25	84.43	104.19
1952	19.52	5.57	0.24	0.24	84.25	104.12
1953	19.53	5.57	0.24	0.24	84.10	104.07
1954	19.54	5.57	0.24	0.24	83.97	104.02
1955	19.55	5.57	0.24	0.24	83.82	103.96
1956	19.56	5.57	0.24	0.24	83.66	103.90
1957	19.57	5.57	0.23	0.23	83.48	103.84
1958	19.58	5.57	0.23	0.23	83.30	103.77
1959	19.59	5.57	0.23	0.23	83.13	103.71
1960	19.60	5.57	0.23	0.23	82.99	103.66
1961	19.61	5.57	0.23	0.23	82.90	103.61
1962	19.62	5.57	0.23	0.23	82.88	103.58
1963	19.63	5.56	0.23	0.23	82.94	103.55
1964	19.64	5.55	0.22	0.22	83.01	103.52
1965	19.65	5.53	0.22	0.22	83.10	103.49
1966	19.66	5.52	0.22	0.22	83.18	103.45
1967	19.67	5.51	0.22	0.22	83.27	103.42
1968	19.68	5.49	0.22	0.22	83.35	103.38

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1969	19.69	5.48	0.22	0.22	83.43	103.36
1970	19.70	5.47	0.22	0.22	83.72	103.31
1971	19.71	5.40	0.22	0.22	84.29	103.24
1972	19.72	5.31	0.22	0.22	85.17	103.13
1973	19.73	5.21	0.21	0.21	86.21	103.01
1974	19.74	5.11	0.21	0.21	87.35	102.88
1975	19.75	5.00	0.21	0.21	88.54	102.74
1976	19.76	4.89	0.21	0.21	89.73	102.59
1977	19.77	4.80	0.20	0.20	90.85	102.46
1978	19.78	4.72	0.20	0.20	91.28	102.47
1979	19.79	4.82	0.21	0.21	90.03	102.86
1980	19.80	5.26	0.23	0.23	87.17	103.65
1981	19.81	5.78	0.26	0.26	83.57	104.70
1982	19.82	6.36	0.29	0.29	80.20	105.77
1983	19.83	6.96	0.33	0.33	77.21	106.81
1984	19.84	7.57	0.36	0.36	74.67	107.77
1985	19.85	8.14	0.40	0.40	72.59	108.62
1986	19.86	8.65	0.43	0.43	70.94	109.32
1987	19.87	9.07	0.46	0.46	69.59	109.92
1988	19.88	9.48	0.48	0.48	68.28	110.48
1989	19.89	10.02	0.52	0.52	66.86	111.08
1990	19.90	10.65	0.55	0.55	65.32	111.75
1991	19.91	11.33	0.60	0.60	63.82	112.44
1992	19.92	12.04	0.64	0.64	62.42	113.12
1993	19.93	12.73	0.69	0.69	61.18	113.75
1994	19.94	13.37	0.73	0.73	60.13	114.30
1995	19.95	13.93	0.77	0.77	59.33	114.75
1996	19.96	14.30	0.80	0.80	59.11	114.88
1997	19.97	13.84	0.77	0.77	59.47	114.70
1998	19.98	13.27	0.73	0.73	60.39	114.23
1999	19.99	12.61	0.68	0.68	61.52	113.67
2000	20.00	11.92	0.64	0.64	62.84	113.04
2001	20.01	11.21	0.59	0.59	64.32	112.37
2002	20.02	10.54	0.55	0.55	65.89	111.69
2003	20.03	9.92	0.51	0.51	67.48	111.04
2004	20.04	9.40	0.48	0.48	68.94	110.47
2005	20.05	9.02	0.46	0.46	70.34	109.96
2006	20.06	8.61	0.44	0.44	71.85	109.46
2007	20.07	8.12	0.41	0.41	73.72	108.86
2008	20.08	7.58	0.38	0.38	76.03	108.16
2009	20.09	7.01	0.35	0.35	78.76	107.38
2010	20.10	6.45	0.32	0.32	81.88	106.53
2011	20.11	5.91	0.29	0.29	85.28	105.67
2012	20.12	5.44	0.27	0.27	88.78	104.84
2013	20.13	5.05	0.25	0.25	91.54	104.25
2014	20.14	4.96	0.25	0.25	93.22	103.96
2015	20.15	4.94	0.25	0.25	93.90	103.94
2016	20.16	4.92	0.25	0.25	94.44	103.99

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2017	20.17	4.89	0.25	0.25	95.02	104.03
2018	20.18	4.87	0.25	0.25	95.63	104.07
2019	20.19	4.84	0.25	0.25	96.22	104.11
2020	20.20	4.81	0.26	0.26	96.77	104.15
2021	20.21	4.79	0.26	0.26	97.25	104.18
2022	20.22	4.78	0.26	0.26	97.71	104.21
2023	20.23	4.76	0.26	0.26	98.19	104.25
2024	20.24	4.74	0.26	0.26	98.77	104.31
2025	20.25	4.71	0.27	0.27	100.00	104.36
2026	20.26	4.68	0.27	0.27	100.00	104.42
2027	20.27	4.66	0.27	0.27	100.00	104.48
2028	20.28	4.63	0.27	0.27	100.00	104.54
2029	20.29	4.61	0.28	0.28	100.00	104.58
2030	20.30	4.59	0.28	0.28	100.00	104.67
2031	20.31	4.64	0.28	0.28	100.00	104.90
2032	20.32	4.82	0.30	0.30	100.00	105.27
2033	20.33	5.03	0.31	0.31	98.72	105.77
2034	20.34	5.26	0.33	0.33	96.87	106.30
2035	20.35	5.50	0.35	0.35	95.11	106.84
2036	20.36	5.75	0.37	0.37	93.50	107.35
2037	20.37	5.97	0.39	0.39	92.10	107.81
2038	20.38	6.18	0.41	0.41	90.94	108.21
2039	20.39	6.34	0.43	0.43	89.84	108.56
2040	20.40	6.54	0.44	0.44	88.58	108.91
2041	20.41	6.82	0.46	0.46	87.04	109.31
2042	20.42	7.13	0.48	0.48	85.33	109.76
2043	20.43	7.48	0.51	0.51	83.61	110.23
2044	20.44	7.83	0.53	0.53	81.98	110.69
2045	20.45	8.17	0.56	0.56	80.50	111.12
2046	20.46	8.49	0.58	0.58	79.22	111.51
2047	20.47	8.77	0.60	0.60	78.16	111.83
2048	20.48	8.99	0.62	0.62	77.17	112.10
2049	20.49	9.26	0.63	0.63	76.09	112.37
2050	20.50	9.59	0.65	0.65	74.82	112.66
2051	20.51	9.97	0.67	0.67	73.45	112.98
2052	20.52	10.37	0.69	0.69	72.06	113.31
2053	20.53	10.78	0.72	0.72	70.74	113.62
2054	20.54	11.17	0.74	0.74	69.53	113.91
2055	20.55	11.52	0.75	0.75	68.49	114.16
2056	20.56	11.82	0.77	0.77	67.67	114.35
2057	20.57	12.01	0.78	0.78	66.99	114.49
2058	20.58	12.19	0.78	0.78	66.37	114.58
2059	20.59	12.40	0.79	0.79	65.68	114.67
2060	20.60	12.63	0.79	0.79	64.94	114.77
2061	20.61	12.88	0.80	0.80	64.17	114.86
2062	20.62	13.12	0.80	0.80	63.43	114.95
2063	20.63	13.35	0.81	0.81	62.74	115.03
2064	20.64	13.55	0.81	0.81	62.14	115.10

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2065	20.65	13.71	0.81	0.81	61.62	115.15
2066	20.66	13.86	0.82	0.82	61.11	115.19
2067	20.67	14.05	0.82	0.82	60.53	115.23
2068	20.68	14.27	0.82	0.82	59.86	115.28
2069	20.69	14.51	0.82	0.82	59.15	115.32
2070	20.70	14.75	0.82	0.82	58.42	115.37
2071	20.71	14.99	0.82	0.82	57.72	115.40
2072	20.72	15.21	0.82	0.82	57.08	115.43
2073	20.73	15.40	0.82	0.82	56.55	115.45
2074	20.74	15.52	0.81	0.81	56.25	115.42
2075	20.75	15.44	0.80	0.80	56.12	115.34
2076	20.76	15.34	0.79	0.79	56.12	115.22
2077	20.77	15.22	0.78	0.78	56.12	115.07
2078	20.78	15.10	0.76	0.76	56.12	114.91
2079	20.79	14.98	0.75	0.75	56.11	114.75
2080	20.80	14.86	0.73	0.73	56.11	114.60
2081	20.81	14.76	0.72	0.72	56.11	114.46
2082	20.82	14.67	0.71	0.71	56.19	114.33
2083	20.83	14.51	0.70	0.70	56.47	114.20
2084	20.84	14.22	0.69	0.69	57.00	114.03
2085	20.85	13.87	0.68	0.68	57.74	113.83
2086	20.86	13.48	0.66	0.66	58.58	113.60
2087	20.87	13.07	0.65	0.65	59.50	113.35
2088	20.88	12.67	0.63	0.63	60.44	113.09
2089	20.89	12.29	0.61	0.61	61.37	112.84
2090	20.90	11.95	0.60	0.60	62.23	112.61
2091	20.91	11.68	0.59	0.59	62.97	112.44
2092	20.92	11.52	0.59	0.59	63.65	112.32
2093	20.93	11.33	0.58	0.58	64.37	112.24
2094	20.94	11.11	0.58	0.58	65.22	112.15
2095	20.95	10.87	0.58	0.58	66.15	112.05
2096	20.96	10.63	0.57	0.57	67.14	111.94
2097	20.97	10.39	0.57	0.57	68.12	111.83
2098	20.98	10.17	0.56	0.56	69.04	111.72
2099	20.99	9.98	0.56	0.56	69.86	111.62
2100	21.00	9.83	0.55	0.55	70.60	111.52
2101	21.01	9.67	0.55	0.55	71.36	111.41
2102	21.02	9.47	0.54	0.54	72.24	111.28
2103	21.03	9.24	0.54	0.54	73.27	111.12
2104	21.04	9.00	0.53	0.53	74.40	110.95
2105	21.05	8.75	0.52	0.52	75.57	110.76
2106	21.06	8.52	0.51	0.51	76.74	110.58
2107	21.07	8.31	0.50	0.50	77.83	110.41
2108	21.08	8.13	0.50	0.50	78.72	110.27
2109	21.09	8.03	0.49	0.49	79.39	110.15
2110	21.10	7.94	0.49	0.49	79.93	110.05
2111	21.11	7.83	0.48	0.48	80.48	109.94
2112	21.12	7.71	0.48	0.48	81.10	109.81

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2113	21.13	7.59	0.47	0.47	81.76	109.68
2114	21.14	7.47	0.46	0.46	82.43	109.54
2115	21.15	7.36	0.46	0.46	83.08	109.41
2116	21.16	7.26	0.45	0.45	83.67	109.30
2117	21.17	7.18	0.45	0.45	83.70	109.29
2118	21.18	7.34	0.46	0.46	83.02	109.41
2119	21.19	7.60	0.47	0.47	81.65	109.67
2120	21.20	7.89	0.48	0.48	80.06	109.96
2121	21.21	8.21	0.50	0.50	78.44	110.27
2122	21.22	8.53	0.51	0.51	76.86	110.57
2123	21.23	8.85	0.52	0.52	75.41	110.85
2124	21.24	9.14	0.54	0.54	74.14	111.10
2125	21.25	9.40	0.55	0.55	73.03	111.32
2126	21.26	9.63	0.56	0.56	71.75	111.58
2127	21.27	10.10	0.58	0.58	70.13	111.91
2128	21.28	10.68	0.60	0.60	68.14	112.34
2129	21.29	11.34	0.63	0.63	66.06	112.78
2130	21.30	12.03	0.65	0.65	64.01	113.21
2131	21.31	12.72	0.68	0.68	62.10	113.62
2132	21.32	13.39	0.70	0.70	60.39	113.98
2133	21.33	13.99	0.72	0.72	58.94	114.28
2134	21.34	14.49	0.73	0.73	57.81	114.50
2135	21.35	14.81	0.74	0.74	56.92	114.65
2136	21.36	15.10	0.75	0.75	56.11	114.75
2137	21.37	15.46	0.75	0.75	55.23	114.85
2138	21.38	15.85	0.75	0.75	54.28	114.94
2139	21.39	16.26	0.76	0.76	53.32	115.04
2140	21.40	16.66	0.76	0.76	52.41	115.12
2141	21.41	17.04	0.76	0.76	51.58	115.19
2142	21.42	17.37	0.76	0.76	50.86	115.24
2143	21.43	17.64	0.76	0.76	50.25	115.32
2144	21.44	17.95	0.77	0.77	49.67	115.42
2145	21.45	18.36	0.78	0.78	49.04	115.57
2146	21.46	18.84	0.79	0.79	48.34	115.73
2147	21.47	19.35	0.80	0.80	47.60	115.91
2148	21.48	19.87	0.82	0.82	46.87	116.08
2149	21.49	20.38	0.83	0.83	46.18	116.23
2150	21.50	20.85	0.84	0.84	45.56	116.37
2151	21.51	21.25	0.85	0.85	45.07	116.48
2152	21.52	21.50	0.85	0.85	44.77	116.54
2153	21.53	21.51	0.85	0.85	44.62	116.55
2154	21.54	21.53	0.85	0.85	44.57	116.53
2155	21.55	21.54	0.84	0.84	44.50	116.51
2156	21.56	21.56	0.84	0.84	44.43	116.49
2157	21.57	21.58	0.84	0.84	44.36	116.47
2158	21.58	21.59	0.83	0.83	44.29	116.45
2159	21.59	21.61	0.83	0.83	44.23	116.43
2160	21.60	21.62	0.83	0.83	44.28	116.38

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2161	21.61	21.37	0.82	0.82	44.55	116.27
2162	21.62	20.81	0.80	0.80	45.10	116.07
2163	21.63	20.14	0.78	0.78	45.85	115.81
2164	21.64	19.41	0.76	0.76	46.71	115.50
2165	21.65	18.65	0.74	0.74	47.66	115.17
2166	21.66	17.90	0.71	0.71	48.65	114.83
2167	21.67	17.20	0.69	0.69	49.62	114.49
2168	21.68	16.58	0.67	0.67	50.53	114.18
2169	21.69	16.09	0.65	0.65	51.32	113.94
2170	21.70	15.75	0.64	0.64	52.07	113.75
2171	21.71	15.34	0.63	0.63	52.89	113.58
2172	21.72	14.87	0.62	0.62	53.89	113.38
2173	21.73	14.36	0.61	0.61	55.02	113.15
2174	21.74	13.84	0.60	0.60	56.23	112.91
2175	21.75	13.33	0.58	0.58	57.45	112.65
2176	21.76	12.86	0.57	0.57	58.63	112.40
2177	21.77	12.46	0.56	0.56	59.67	112.18
2178	21.78	12.16	0.55	0.55	60.63	111.99
2179	21.79	11.85	0.54	0.54	61.61	111.78
2180	21.80	11.46	0.53	0.53	62.77	111.55
2181	21.81	11.03	0.52	0.52	64.13	111.27
2182	21.82	10.57	0.50	0.50	65.65	110.96
2183	21.83	10.11	0.49	0.49	67.27	110.63
2184	21.84	9.67	0.47	0.47	68.90	110.29
2185	21.85	9.28	0.46	0.46	70.47	109.97
2186	21.86	8.95	0.44	0.44	71.82	109.70
2187	21.87	8.72	0.43	0.43	73.02	109.46
2188	21.88	8.47	0.43	0.43	74.21	109.21
2189	21.89	8.18	0.41	0.41	75.62	108.93
2190	21.90	7.85	0.40	0.40	77.26	108.60
2191	21.91	7.52	0.39	0.39	79.07	108.24
2192	21.92	7.19	0.37	0.37	80.98	107.87
2193	21.93	6.88	0.36	0.36	82.90	107.50
2194	21.94	6.60	0.35	0.35	84.70	107.17
2195	21.95	6.38	0.34	0.34	86.02	106.91
2196	21.96	6.31	0.33	0.33	86.88	106.71
2197	21.97	6.22	0.33	0.33	87.41	106.54
2198	21.98	6.12	0.32	0.32	88.01	106.35
2199	21.99	6.02	0.31	0.31	88.67	106.15
2200	22.00	5.91	0.31	0.31	89.37	105.93
2201	22.01	5.80	0.30	0.30	90.07	105.72
2202	22.02	5.71	0.29	0.29	90.74	105.52
2203	22.03	5.62	0.29	0.29	91.28	105.36
2204	22.04	5.57	0.28	0.28	91.53	105.24
2205	22.05	5.57	0.28	0.28	91.50	105.16
2206	22.06	5.57	0.28	0.28	91.27	105.08
2207	22.07	5.57	0.27	0.27	91.01	104.99
2208	22.08	5.57	0.27	0.27	90.74	104.90

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2209	22.09	5.57	0.27	0.27	90.46	104.81
2210	22.10	5.57	0.26	0.26	90.19	104.72
2211	22.11	5.57	0.26	0.26	89.95	104.64
2212	22.12	5.57	0.26	0.26	89.75	104.57
2213	22.13	5.57	0.26	0.26	89.58	104.51
2214	22.14	5.57	0.25	0.25	89.40	104.45
2215	22.15	5.57	0.25	0.25	89.20	104.38
2216	22.16	5.57	0.25	0.25	88.97	104.30
2217	22.17	5.57	0.25	0.25	88.73	104.21
2218	22.18	5.57	0.24	0.24	88.50	104.13
2219	22.19	5.57	0.24	0.24	88.27	104.05
2220	22.20	5.57	0.24	0.24	88.08	103.99
2221	22.21	5.57	0.24	0.24	88.03	103.92
2222	22.22	5.54	0.23	0.23	88.15	103.83
2223	22.23	5.50	0.23	0.23	88.43	103.73
2224	22.24	5.45	0.23	0.23	88.76	103.61
2225	22.25	5.40	0.23	0.23	89.12	103.48
2226	22.26	5.34	0.22	0.22	89.50	103.34
2227	22.27	5.29	0.22	0.22	89.88	103.21
2228	22.28	5.24	0.22	0.22	90.23	103.09
2229	22.29	5.20	0.21	0.21	90.45	103.00
2230	22.30	5.19	0.21	0.21	90.32	103.00
2231	22.31	5.27	0.21	0.21	89.78	103.08
2232	22.32	5.36	0.22	0.22	88.93	103.23
2233	22.33	5.46	0.22	0.22	88.01	103.40
2234	22.34	5.57	0.23	0.23	87.07	103.57
2235	22.35	5.68	0.23	0.23	86.15	103.73
2236	22.36	5.78	0.23	0.23	85.31	103.89
2237	22.37	5.87	0.24	0.24	84.58	104.03
2238	22.38	5.95	0.24	0.24	84.03	104.13
2239	22.39	5.99	0.24	0.24	83.63	104.22
2240	22.40	6.03	0.24	0.24	83.32	104.29
2241	22.41	6.08	0.24	0.24	82.99	104.36
2242	22.42	6.13	0.25	0.25	82.64	104.44
2243	22.43	6.19	0.25	0.25	82.28	104.53
2244	22.44	6.24	0.25	0.25	81.93	104.61
2245	22.45	6.29	0.25	0.25	81.61	104.69
2246	22.46	6.34	0.25	0.25	81.33	104.75
2247	22.47	6.37	0.26	0.26	81.06	104.82
2248	22.48	6.42	0.26	0.26	80.76	104.90
2249	22.49	6.49	0.26	0.26	80.39	105.01
2250	22.50	6.56	0.26	0.26	79.96	105.13
2251	22.51	6.64	0.27	0.27	79.52	105.26
2252	22.52	6.72	0.27	0.27	79.07	105.38
2253	22.53	6.80	0.28	0.28	78.65	105.51
2254	22.54	6.87	0.28	0.28	78.28	105.62
2255	22.55	6.93	0.28	0.28	77.99	105.71
2256	22.56	6.97	0.28	0.28	77.84	105.76

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2257	22.57	6.97	0.28	0.28	77.81	105.78
2258	22.58	6.97	0.28	0.28	77.85	105.79
2259	22.59	6.97	0.28	0.28	77.89	105.80
2260	22.60	6.97	0.28	0.28	77.94	105.81
2261	22.61	6.97	0.29	0.29	77.98	105.82
2262	22.62	6.97	0.29	0.29	78.02	105.83
2263	22.63	6.97	0.29	0.29	78.06	105.84
2264	22.64	6.97	0.29	0.29	78.24	105.82
2265	22.65	6.89	0.28	0.28	78.69	105.72
2266	22.66	6.75	0.28	0.28	79.48	105.54
2267	22.67	6.58	0.27	0.27	80.52	105.30
2268	22.68	6.40	0.26	0.26	81.72	105.04
2269	22.69	6.21	0.26	0.26	83.02	104.75
2270	22.70	6.02	0.25	0.25	84.37	104.47
2271	22.71	5.85	0.24	0.24	85.70	104.19
2272	22.72	5.70	0.24	0.24	86.91	103.94
2273	22.73	5.57	0.23	0.23	87.68	103.78
2274	22.74	5.57	0.23	0.23	88.00	103.70
2275	22.75	5.57	0.23	0.23	87.96	103.69
2276	22.76	5.57	0.23	0.23	87.92	103.67
2277	22.77	5.57	0.23	0.23	87.86	103.64
2278	22.78	5.57	0.23	0.23	87.81	103.62
2279	22.79	5.57	0.23	0.23	87.76	103.60
2280	22.80	5.57	0.23	0.23	87.72	103.58
2281	22.81	5.57	0.23	0.23	87.68	103.56
2282	22.82	5.57	0.22	0.22	87.63	103.54
2283	22.83	5.57	0.22	0.22	87.58	103.52
2284	22.84	5.57	0.22	0.22	87.51	103.49
2285	22.85	5.57	0.22	0.22	87.42	103.46
2286	22.86	5.57	0.22	0.22	87.33	103.42
2287	22.87	5.57	0.22	0.22	87.25	103.39
2288	22.88	5.57	0.22	0.22	87.16	103.36
2289	22.89	5.57	0.22	0.22	87.09	103.33
2290	22.90	5.57	0.22	0.22	87.04	103.31
2291	22.91	5.57	0.22	0.22	87.02	103.30
2292	22.92	5.57	0.22	0.22	87.03	103.29
2293	22.93	5.57	0.22	0.22	87.05	103.29
2294	22.94	5.57	0.22	0.22	87.06	103.29
2295	22.95	5.57	0.22	0.22	87.07	103.29
2296	22.96	5.57	0.22	0.22	87.09	103.29
2297	22.97	5.57	0.22	0.22	87.10	103.29
2298	22.98	5.57	0.22	0.22	87.11	103.30
2299	22.99	5.58	0.22	0.22	86.66	103.41
2300	23.00	5.75	0.23	0.23	85.68	103.66
2301	23.01	5.97	0.24	0.24	84.15	104.06
2302	23.02	6.22	0.25	0.25	82.53	104.50
2303	23.03	6.49	0.26	0.26	80.92	104.95
2304	23.04	6.76	0.27	0.27	79.40	105.40

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2305	23.05	7.02	0.28	0.28	78.04	105.81
2306	23.06	7.26	0.30	0.30	76.87	106.18
2307	23.07	7.46	0.31	0.31	75.99	106.47
2308	23.08	7.59	0.31	0.31	75.43	106.69
2309	23.09	7.66	0.32	0.32	75.09	106.86
2310	23.10	7.76	0.32	0.32	74.83	107.04
2311	23.11	7.86	0.33	0.33	74.55	107.23
2312	23.12	7.97	0.34	0.34	74.26	107.43
2313	23.13	8.07	0.35	0.35	73.98	107.63
2314	23.14	8.18	0.35	0.35	73.72	107.81
2315	23.15	8.27	0.36	0.36	73.50	107.98
2316	23.16	8.34	0.37	0.37	73.41	108.09
2317	23.17	8.34	0.37	0.37	73.50	108.14
2318	23.18	8.30	0.37	0.37	73.78	108.15
2319	23.19	8.25	0.37	0.37	74.15	108.15
2320	23.20	8.20	0.37	0.37	74.56	108.15
2321	23.21	8.14	0.37	0.37	74.98	108.15
2322	23.22	8.09	0.37	0.37	75.40	108.14
2323	23.23	8.04	0.37	0.37	75.79	108.14
2324	23.24	8.00	0.37	0.37	76.12	108.14
2325	23.25	7.97	0.37	0.37	76.26	108.17
2326	23.26	8.04	0.38	0.38	76.18	108.26
2327	23.27	8.12	0.39	0.39	75.92	108.41
2328	23.28	8.22	0.39	0.39	75.63	108.58
2329	23.29	8.33	0.40	0.40	75.33	108.75
2330	23.30	8.44	0.41	0.41	75.03	108.93
2331	23.31	8.54	0.42	0.42	74.75	109.10
2332	23.32	8.64	0.42	0.42	74.50	109.25
2333	23.33	8.72	0.43	0.43	74.29	109.38
2334	23.34	8.78	0.44	0.44	74.10	109.49
2335	23.35	8.86	0.44	0.44	73.89	109.61
2336	23.36	8.95	0.45	0.45	73.66	109.75
2337	23.37	9.06	0.46	0.46	73.40	109.90
2338	23.38	9.16	0.46	0.46	73.14	110.06
2339	23.39	9.27	0.47	0.47	72.88	110.22
2340	23.40	9.37	0.48	0.48	72.64	110.37
2341	23.41	9.46	0.49	0.49	72.44	110.50
2342	23.42	9.54	0.49	0.49	72.25	110.60
2343	23.43	9.60	0.50	0.50	72.05	110.69
2344	23.44	9.69	0.50	0.50	71.80	110.78
2345	23.45	9.78	0.51	0.51	71.50	110.89
2346	23.46	9.89	0.51	0.51	71.19	111.00
2347	23.47	10.00	0.52	0.52	70.87	111.11
2348	23.48	10.10	0.53	0.53	70.56	111.22
2349	23.49	10.20	0.53	0.53	70.28	111.32
2350	23.50	10.29	0.54	0.54	70.04	111.41
2351	23.51	10.36	0.54	0.54	69.79	111.49
2352	23.52	10.45	0.55	0.55	69.47	111.57

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2353	23.53	10.58	0.55	0.55	69.07	111.66
2354	23.54	10.71	0.56	0.56	68.62	111.76
2355	23.55	10.86	0.56	0.56	68.15	111.87
2356	23.56	11.01	0.57	0.57	67.68	111.98
2357	23.57	11.15	0.57	0.57	67.23	112.09
2358	23.58	11.28	0.58	0.58	66.84	112.18
2359	23.59	11.39	0.58	0.58	66.52	112.25
2360	23.60	11.47	0.59	0.59	66.26	112.32
2361	23.61	11.55	0.59	0.59	66.04	112.38
2362	23.62	11.64	0.59	0.59	65.80	112.46
2363	23.63	11.75	0.60	0.60	65.54	112.54
2364	23.64	11.85	0.60	0.60	65.27	112.62
2365	23.65	11.96	0.61	0.61	65.00	112.70
2366	23.66	12.06	0.61	0.61	64.75	112.78
2367	23.67	12.15	0.62	0.62	64.53	112.85
2368	23.68	12.23	0.62	0.62	64.42	112.90
2369	23.69	12.23	0.62	0.62	64.44	112.92
2370	23.70	12.19	0.62	0.62	64.59	112.93
2371	23.71	12.16	0.63	0.63	64.79	112.94
2372	23.72	12.12	0.63	0.63	65.00	112.95
2373	23.73	12.08	0.63	0.63	65.22	112.96
2374	23.74	12.04	0.63	0.63	65.44	112.97
2375	23.75	12.00	0.63	0.63	65.64	112.98
2376	23.76	11.97	0.63	0.63	65.80	112.99
2377	23.77	11.97	0.64	0.64	65.72	113.09
2378	23.78	12.23	0.65	0.65	65.36	113.29
2379	23.79	12.56	0.68	0.68	64.75	113.59
2380	23.80	12.94	0.70	0.70	64.08	113.94
2381	23.81	13.34	0.73	0.73	63.40	114.29
2382	23.82	13.75	0.76	0.76	62.75	114.64
2383	23.83	14.14	0.79	0.79	62.16	114.97
2384	23.84	14.49	0.81	0.81	61.65	115.26
2385	23.85	14.79	0.83	0.83	61.26	115.49
2386	23.86	14.97	0.85	0.85	61.02	115.66
2387	23.87	15.09	0.86	0.86	60.86	115.79
2388	23.88	15.23	0.87	0.87	60.74	115.92
2389	23.89	15.38	0.89	0.89	60.61	116.06
2390	23.90	15.55	0.90	0.90	60.47	116.20
2391	23.91	15.71	0.92	0.92	60.33	116.35
2392	23.92	15.86	0.93	0.93	60.21	116.48
2393	23.93	15.99	0.94	0.94	60.10	116.60
2394	23.94	16.11	0.95	0.95	60.11	116.65
2395	23.95	15.98	0.95	0.95	60.29	116.62
2396	23.96	15.76	0.94	0.94	60.66	116.50
2397	23.97	15.49	0.92	0.92	61.13	116.34
2398	23.98	15.20	0.90	0.90	61.66	116.17
2399	23.99	14.90	0.89	0.89	62.21	115.99
2400	24.00	14.61	0.87	0.87	62.77	115.81

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2401	24.01	14.34	0.86	0.86	63.30	115.63
2402	24.02	14.10	0.84	0.84	63.77	115.48
2403	24.03	13.93	0.83	0.83	64.07	115.38
2404	24.04	13.90	0.83	0.83	64.24	115.32
2405	24.05	13.85	0.83	0.83	64.32	115.29
2406	24.06	13.80	0.82	0.82	64.41	115.25
2407	24.07	13.75	0.82	0.82	64.51	115.20
2408	24.08	13.69	0.81	0.81	64.60	115.15
2409	24.09	13.64	0.81	0.81	64.70	115.11
2410	24.10	13.60	0.81	0.81	64.79	115.07
2411	24.11	13.56	0.80	0.80	64.89	115.03
2412	24.12	13.49	0.80	0.80	65.08	114.97
2413	24.13	13.35	0.79	0.79	65.38	114.89
2414	24.14	13.19	0.78	0.78	65.77	114.79
2415	24.15	13.01	0.78	0.78	66.22	114.67
2416	24.16	12.82	0.77	0.77	66.70	114.55
2417	24.17	12.63	0.76	0.76	67.18	114.42
2418	24.18	12.45	0.75	0.75	67.64	114.30
2419	24.19	12.29	0.74	0.74	68.06	114.19
2420	24.20	12.17	0.73	0.73	68.44	114.10
2421	24.21	12.05	0.73	0.73	68.83	114.01
2422	24.22	11.90	0.72	0.72	69.28	113.92
2423	24.23	11.73	0.71	0.71	69.82	113.81
2424	24.24	11.55	0.71	0.71	70.41	113.69
2425	24.25	11.36	0.70	0.70	71.02	113.56
2426	24.26	11.17	0.69	0.69	71.64	113.43
2427	24.27	11.00	0.68	0.68	72.23	113.31
2428	24.28	10.85	0.67	0.67	72.72	113.22
2429	24.29	10.76	0.67	0.67	72.90	113.20
2430	24.30	10.89	0.68	0.68	72.77	113.28
2431	24.31	11.05	0.69	0.69	72.39	113.43
2432	24.32	11.22	0.70	0.70	71.96	113.61
2433	24.33	11.41	0.72	0.72	71.52	113.79
2434	24.34	11.60	0.73	0.73	71.09	113.97
2435	24.35	11.78	0.75	0.75	70.69	114.14
2436	24.36	11.95	0.76	0.76	70.33	114.30
2437	24.37	12.09	0.77	0.77	70.03	114.43
2438	24.38	12.20	0.78	0.78	69.76	114.54
2439	24.39	12.33	0.79	0.79	69.46	114.67
2440	24.40	12.50	0.80	0.80	69.12	114.81
2441	24.41	12.68	0.81	0.81	68.74	114.96
2442	24.42	12.87	0.83	0.83	68.36	115.12
2443	24.43	13.06	0.84	0.84	67.99	115.27
2444	24.44	13.23	0.85	0.85	67.65	115.41
2445	24.45	13.39	0.87	0.87	67.36	115.54
2446	24.46	13.52	0.88	0.88	67.17	115.62
2447	24.47	13.54	0.88	0.88	67.07	115.66
2448	24.48	13.54	0.88	0.88	67.05	115.65

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2449	24.49	13.54	0.87	0.87	67.04	115.65
2450	24.50	13.54	0.87	0.87	67.02	115.64
2451	24.51	13.54	0.87	0.87	67.01	115.63
2452	24.52	13.54	0.87	0.87	66.99	115.62
2453	24.53	13.54	0.87	0.87	66.98	115.61
2454	24.54	13.54	0.87	0.87	66.97	115.60
2455	24.55	13.53	0.87	0.87	67.00	115.57
2456	24.56	13.46	0.86	0.86	67.07	115.51
2457	24.57	13.37	0.85	0.85	67.19	115.42
2458	24.58	13.27	0.84	0.84	67.32	115.31
2459	24.59	13.16	0.83	0.83	67.46	115.20
2460	24.60	13.05	0.82	0.82	67.61	115.08
2461	24.61	12.95	0.81	0.81	67.75	114.97
2462	24.62	12.85	0.80	0.80	67.88	114.87
2463	24.63	12.77	0.79	0.79	67.99	114.78
2464	24.64	12.71	0.78	0.78	68.09	114.70
2465	24.65	12.63	0.78	0.78	68.21	114.60
2466	24.66	12.54	0.77	0.77	68.33	114.50
2467	24.67	12.43	0.76	0.76	68.48	114.38
2468	24.68	12.33	0.75	0.75	68.63	114.25
2469	24.69	12.22	0.74	0.74	68.78	114.13
2470	24.70	12.12	0.73	0.73	68.93	114.01
2471	24.71	12.03	0.72	0.72	69.06	113.90
2472	24.72	11.96	0.71	0.71	69.18	113.81
2473	24.73	11.89	0.70	0.70	69.31	113.73
2474	24.74	11.80	0.70	0.70	69.46	113.63
2475	24.75	11.71	0.69	0.69	69.63	113.52
2476	24.76	11.60	0.68	0.68	69.82	113.40
2477	24.77	11.49	0.67	0.67	70.02	113.27
2478	24.78	11.39	0.66	0.66	70.22	113.15
2479	24.79	11.29	0.65	0.65	70.41	113.03
2480	24.80	11.20	0.64	0.64	70.58	112.93
2481	24.81	11.13	0.64	0.64	70.82	112.82
2482	24.82	10.98	0.63	0.63	71.17	112.68
2483	24.83	10.80	0.61	0.61	71.65	112.51
2484	24.84	10.60	0.60	0.60	72.20	112.30
2485	24.85	10.39	0.59	0.59	72.82	112.08
2486	24.86	10.17	0.57	0.57	73.45	111.86
2487	24.87	9.96	0.56	0.56	74.09	111.63
2488	24.88	9.77	0.55	0.55	74.68	111.43
2489	24.89	9.62	0.54	0.54	75.16	111.27
2490	24.90	9.52	0.53	0.53	75.54	111.14
2491	24.91	9.44	0.53	0.53	75.84	111.03
2492	24.92	9.35	0.52	0.52	76.15	110.92
2493	24.93	9.25	0.51	0.51	76.51	110.80
2494	24.94	9.14	0.50	0.50	76.88	110.67
2495	24.95	9.03	0.50	0.50	77.26	110.53
2496	24.96	8.93	0.49	0.49	77.62	110.41

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2497	24.97	8.84	0.48	0.48	77.95	110.30
2498	24.98	8.77	0.48	0.48	78.25	110.20
2499	24.99	8.70	0.48	0.48	78.55	110.11
2500	25.00	8.62	0.47	0.47	78.89	110.00
2501	25.01	8.52	0.46	0.46	79.29	109.88
2502	25.02	8.41	0.46	0.46	79.74	109.75
2503	25.03	8.30	0.45	0.45	80.20	109.61
2504	25.04	8.20	0.44	0.44	80.67	109.48
2505	25.05	8.10	0.44	0.44	81.11	109.35
2506	25.06	8.02	0.43	0.43	81.49	109.24
2507	25.07	7.95	0.43	0.43	81.86	109.15
2508	25.08	7.88	0.43	0.43	82.25	109.05
2509	25.09	7.79	0.42	0.42	82.71	108.94
2510	25.10	7.69	0.42	0.42	83.25	108.81
2511	25.11	7.58	0.41	0.41	83.83	108.68
2512	25.12	7.47	0.40	0.40	84.43	108.54
2513	25.13	7.37	0.40	0.40	85.02	108.41
2514	25.14	7.27	0.39	0.39	85.56	108.28
2515	25.15	7.20	0.39	0.39	85.97	108.20
2516	25.16	7.17	0.39	0.39	86.21	108.15
2517	25.17	7.17	0.39	0.39	86.31	108.15
2518	25.18	7.17	0.39	0.39	86.35	108.16
2519	25.19	7.17	0.39	0.39	86.40	108.17
2520	25.20	7.17	0.39	0.39	86.46	108.18
2521	25.21	7.17	0.39	0.39	86.51	108.19
2522	25.22	7.17	0.39	0.39	86.56	108.21
2523	25.23	7.17	0.39	0.39	86.60	108.22
2524	25.24	7.17	0.39	0.39	86.75	108.19
2525	25.25	7.11	0.39	0.39	87.04	108.12
2526	25.26	7.02	0.38	0.38	87.51	107.99
2527	25.27	6.92	0.38	0.38	88.08	107.84
2528	25.28	6.82	0.37	0.37	88.72	107.68
2529	25.29	6.71	0.36	0.36	89.39	107.50
2530	25.30	6.60	0.36	0.36	90.06	107.33
2531	25.31	6.51	0.35	0.35	90.69	107.18
2532	25.32	6.42	0.35	0.35	91.22	107.04
2533	25.33	6.37	0.34	0.34	91.51	106.96
2534	25.34	6.37	0.34	0.34	91.57	106.91
2535	25.35	6.37	0.34	0.34	91.48	106.87
2536	25.36	6.37	0.34	0.34	91.38	106.84
2537	25.37	6.37	0.34	0.34	91.27	106.80
2538	25.38	6.37	0.33	0.33	91.15	106.76
2539	25.39	6.37	0.33	0.33	91.05	106.72
2540	25.40	6.37	0.33	0.33	90.95	106.69
2541	25.41	6.37	0.33	0.33	90.79	106.68
2542	25.42	6.41	0.33	0.33	90.43	106.71
2543	25.43	6.49	0.33	0.33	89.86	106.80
2544	25.44	6.58	0.34	0.34	89.13	106.91

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2545	25.45	6.69	0.34	0.34	88.34	107.03
2546	25.46	6.79	0.34	0.34	87.54	107.15
2547	25.47	6.90	0.35	0.35	86.77	107.27
2548	25.48	7.00	0.35	0.35	86.06	107.38
2549	25.49	7.09	0.36	0.36	85.46	107.47
2550	25.50	7.16	0.36	0.36	84.95	107.56
2551	25.51	7.23	0.36	0.36	84.47	107.64
2552	25.52	7.31	0.36	0.36	83.96	107.74
2553	25.53	7.41	0.37	0.37	83.38	107.86
2554	25.54	7.52	0.37	0.37	82.77	107.98
2555	25.55	7.63	0.38	0.38	82.15	108.11
2556	25.56	7.73	0.38	0.38	81.57	108.23
2557	25.57	7.83	0.39	0.39	81.05	108.33
2558	25.58	7.91	0.39	0.39	80.62	108.43
2559	25.59	7.98	0.39	0.39	80.28	108.52
2560	25.60	8.05	0.40	0.40	79.98	108.64
2561	25.61	8.14	0.41	0.41	79.67	108.79
2562	25.62	8.25	0.41	0.41	79.33	108.95
2563	25.63	8.35	0.42	0.42	78.98	109.12
2564	25.64	8.46	0.43	0.43	78.64	109.28
2565	25.65	8.56	0.44	0.44	78.32	109.44
2566	25.66	8.66	0.44	0.44	78.04	109.58
2567	25.67	8.73	0.45	0.45	77.86	109.69
2568	25.68	8.76	0.45	0.45	77.83	109.76
2569	25.69	8.76	0.46	0.46	77.92	109.81
2570	25.70	8.76	0.46	0.46	78.06	109.86
2571	25.71	8.76	0.46	0.46	78.22	109.91
2572	25.72	8.76	0.46	0.46	78.39	109.96
2573	25.73	8.76	0.47	0.47	78.55	110.01
2574	25.74	8.76	0.47	0.47	78.71	110.06
2575	25.75	8.76	0.47	0.47	78.84	110.10
2576	25.76	8.76	0.48	0.48	78.85	110.15
2577	25.77	8.82	0.48	0.48	78.71	110.23
2578	25.78	8.91	0.49	0.49	78.41	110.33
2579	25.79	9.01	0.49	0.49	78.06	110.45
2580	25.80	9.11	0.50	0.50	77.69	110.58
2581	25.81	9.22	0.51	0.51	77.33	110.71
2582	25.82	9.33	0.51	0.51	76.98	110.84
2583	25.83	9.43	0.52	0.52	76.67	110.95
2584	25.84	9.51	0.53	0.53	76.40	111.05
2585	25.85	9.57	0.53	0.53	76.17	111.14
2586	25.86	9.65	0.53	0.53	75.92	111.22
2587	25.87	9.74	0.54	0.54	75.63	111.32
2588	25.88	9.84	0.55	0.55	75.31	111.43
2589	25.89	9.95	0.55	0.55	74.98	111.55
2590	25.90	10.06	0.56	0.56	74.66	111.67
2591	25.91	10.16	0.57	0.57	74.35	111.78
2592	25.92	10.25	0.57	0.57	74.09	111.87

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2593	25.93	10.33	0.58	0.58	73.77	111.99
2594	25.94	10.48	0.59	0.59	73.27	112.15
2595	25.95	10.74	0.60	0.60	72.55	112.38
2596	25.96	11.05	0.62	0.62	71.67	112.67
2597	25.97	11.39	0.64	0.64	70.75	112.98
2598	25.98	11.75	0.66	0.66	69.85	113.28
2599	25.99	12.09	0.69	0.69	69.00	113.58
2600	26.00	12.42	0.70	0.70	68.24	113.85
2601	26.01	12.70	0.72	0.72	67.60	114.08
2602	26.02	12.93	0.74	0.74	67.18	114.24
2603	26.03	13.01	0.74	0.74	66.93	114.35
2604	26.04	13.09	0.75	0.75	66.78	114.43
2605	26.05	13.19	0.76	0.76	66.62	114.52
2606	26.06	13.30	0.76	0.76	66.45	114.62
2607	26.07	13.41	0.77	0.77	66.28	114.72
2608	26.08	13.51	0.78	0.78	66.12	114.81
2609	26.09	13.61	0.79	0.79	65.97	114.90
2610	26.10	13.69	0.79	0.79	65.89	114.96
2611	26.11	13.70	0.80	0.80	66.00	114.95
2612	26.12	13.53	0.79	0.79	66.32	114.88
2613	26.13	13.32	0.78	0.78	66.83	114.75
2614	26.14	13.09	0.77	0.77	67.41	114.61
2615	26.15	12.85	0.76	0.76	68.05	114.45
2616	26.16	12.61	0.74	0.74	68.70	114.29
2617	26.17	12.38	0.73	0.73	69.33	114.14
2618	26.18	12.17	0.72	0.72	69.92	113.99
2619	26.19	12.00	0.71	0.71	70.36	113.90
2620	26.20	11.95	0.71	0.71	70.62	113.86
2621	26.21	11.95	0.71	0.71	70.75	113.87
2622	26.22	11.95	0.72	0.72	70.85	113.90
2623	26.23	11.95	0.72	0.72	70.95	113.93
2624	26.24	11.95	0.72	0.72	71.06	113.97
2625	26.25	11.95	0.73	0.73	71.17	114.00
2626	26.26	11.95	0.73	0.73	71.27	114.03
2627	26.27	11.95	0.73	0.73	71.36	114.06
2628	26.28	11.95	0.74	0.74	71.38	114.10
2629	26.29	12.01	0.74	0.74	71.31	114.16
2630	26.30	12.10	0.75	0.75	71.16	114.25
2631	26.31	12.20	0.76	0.76	70.98	114.35
2632	26.32	12.31	0.77	0.77	70.79	114.46
2633	26.33	12.41	0.78	0.78	70.61	114.57
2634	26.34	12.52	0.79	0.79	70.43	114.67
2635	26.35	12.61	0.79	0.79	70.27	114.77
2636	26.36	12.70	0.80	0.80	70.13	114.85
2637	26.37	12.76	0.81	0.81	69.97	114.91
2638	26.38	12.84	0.81	0.81	69.77	114.96
2639	26.39	12.93	0.81	0.81	69.52	115.01
2640	26.40	13.03	0.82	0.82	69.25	115.07

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2641	26.41	13.14	0.82	0.82	68.95	115.13
2642	26.42	13.25	0.83	0.83	68.67	115.19
2643	26.43	13.35	0.83	0.83	68.39	115.25
2644	26.44	13.44	0.84	0.84	68.16	115.30
2645	26.45	13.52	0.84	0.84	67.98	115.33
2646	26.46	13.54	0.84	0.84	67.85	115.33
2647	26.47	13.54	0.83	0.83	67.75	115.30
2648	26.48	13.54	0.83	0.83	67.64	115.26
2649	26.49	13.54	0.82	0.82	67.53	115.22
2650	26.50	13.54	0.82	0.82	67.41	115.18
2651	26.51	13.54	0.81	0.81	67.29	115.13
2652	26.52	13.54	0.81	0.81	67.18	115.09
2653	26.53	13.54	0.81	0.81	67.08	115.05
2654	26.54	13.54	0.80	0.80	66.98	115.03
2655	26.55	13.57	0.80	0.80	66.86	115.03
2656	26.56	13.62	0.80	0.80	66.71	115.03
2657	26.57	13.67	0.80	0.80	66.54	115.04
2658	26.58	13.72	0.80	0.80	66.35	115.05
2659	26.59	13.77	0.80	0.80	66.16	115.06
2660	26.60	13.83	0.80	0.80	65.98	115.07
2661	26.61	13.87	0.80	0.80	65.82	115.07
2662	26.62	13.91	0.80	0.80	65.71	115.07
2663	26.63	13.92	0.80	0.80	65.70	115.05
2664	26.64	13.84	0.80	0.80	65.81	115.01
2665	26.65	13.75	0.79	0.79	66.00	114.94
2666	26.66	13.64	0.78	0.78	66.21	114.86
2667	26.67	13.54	0.78	0.78	66.44	114.78
2668	26.68	13.43	0.77	0.77	66.67	114.70
2669	26.69	13.33	0.76	0.76	66.89	114.62
2670	26.70	13.24	0.76	0.76	67.09	114.55
2671	26.71	13.16	0.75	0.75	67.28	114.48
2672	26.72	13.07	0.75	0.75	67.49	114.41
2673	26.73	12.95	0.74	0.74	67.75	114.31
2674	26.74	12.81	0.73	0.73	68.06	114.19
2675	26.75	12.65	0.72	0.72	68.40	114.05
2676	26.76	12.49	0.71	0.71	68.76	113.92
2677	26.77	12.33	0.70	0.70	69.13	113.78
2678	26.78	12.18	0.69	0.69	69.48	113.65
2679	26.79	12.05	0.68	0.68	69.78	113.53
2680	26.80	11.95	0.67	0.67	69.96	113.46
2681	26.81	11.95	0.67	0.67	70.01	113.41
2682	26.82	11.95	0.67	0.67	69.96	113.39
2683	26.83	11.95	0.67	0.67	69.90	113.37
2684	26.84	11.95	0.67	0.67	69.84	113.34
2685	26.85	11.95	0.66	0.66	69.77	113.32
2686	26.86	11.95	0.66	0.66	69.71	113.29
2687	26.87	11.95	0.66	0.66	69.65	113.27
2688	26.88	11.95	0.66	0.66	69.53	113.27

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2689	26.89	12.03	0.66	0.66	69.18	113.36
2690	26.90	12.32	0.68	0.68	68.55	113.54
2691	26.91	12.66	0.69	0.69	67.70	113.80
2692	26.92	13.05	0.71	0.71	66.79	114.08
2693	26.93	13.45	0.74	0.74	65.88	114.37
2694	26.94	13.86	0.76	0.76	65.01	114.65
2695	26.95	14.24	0.78	0.78	64.22	114.91
2696	26.96	14.58	0.80	0.80	63.54	115.13
2697	26.97	14.86	0.81	0.81	63.15	115.25
2698	26.98	14.83	0.81	0.81	63.10	115.26
2699	26.99	14.64	0.80	0.80	63.35	115.15
2700	27.00	14.43	0.78	0.78	63.73	114.99
2701	27.01	14.19	0.77	0.77	64.16	114.81
2702	27.02	13.94	0.75	0.75	64.62	114.62
2703	27.03	13.70	0.74	0.74	65.07	114.44
2704	27.04	13.48	0.72	0.72	65.51	114.27
2705	27.05	13.29	0.71	0.71	65.91	114.11
2706	27.06	13.13	0.70	0.70	66.42	113.93
2707	27.07	12.80	0.69	0.69	67.14	113.70
2708	27.08	12.38	0.66	0.66	68.16	113.39
2709	27.09	11.90	0.64	0.64	69.40	113.01
2710	27.10	11.40	0.61	0.61	70.81	112.60
2711	27.11	10.88	0.58	0.58	72.34	112.16
2712	27.12	10.38	0.56	0.56	73.94	111.71
2713	27.13	9.93	0.53	0.53	75.50	111.29
2714	27.14	9.55	0.51	0.51	76.76	110.96
2715	27.15	9.39	0.50	0.50	77.39	110.82
2716	27.16	9.48	0.51	0.51	77.40	110.86
2717	27.17	9.60	0.52	0.52	77.07	111.01
2718	27.18	9.73	0.53	0.53	76.71	111.18
2719	27.19	9.86	0.54	0.54	76.33	111.35
2720	27.20	10.00	0.55	0.55	75.97	111.51
2721	27.21	10.12	0.56	0.56	75.64	111.67
2722	27.22	10.24	0.57	0.57	75.35	111.81
2723	27.23	10.33	0.58	0.58	75.17	111.90
2724	27.24	10.35	0.58	0.58	75.08	111.95
2725	27.25	10.35	0.58	0.58	75.08	111.96
2726	27.26	10.35	0.58	0.58	75.10	111.97
2727	27.27	10.35	0.58	0.58	75.13	111.97
2728	27.28	10.35	0.58	0.58	75.15	111.97
2729	27.29	10.35	0.58	0.58	75.17	111.98
2730	27.30	10.35	0.58	0.58	75.19	111.98
2731	27.31	10.35	0.58	0.58	75.21	111.98
2732	27.32	10.35	0.58	0.58	75.22	111.98
2733	27.33	10.35	0.58	0.58	75.22	111.98
2734	27.34	10.35	0.58	0.58	75.21	111.97
2735	27.35	10.35	0.58	0.58	75.20	111.97
2736	27.36	10.35	0.58	0.58	75.18	111.96

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2737	27.37	10.35	0.58	0.58	75.17	111.95
2738	27.38	10.35	0.58	0.58	75.16	111.94
2739	27.39	10.35	0.58	0.58	75.15	111.94
2740	27.40	10.35	0.58	0.58	75.05	111.96
2741	27.41	10.44	0.58	0.58	74.68	112.06
2742	27.42	10.69	0.59	0.59	74.01	112.26
2743	27.43	10.99	0.61	0.61	73.10	112.53
2744	27.44	11.32	0.63	0.63	72.14	112.83
2745	27.45	11.67	0.65	0.65	71.18	113.13
2746	27.46	12.02	0.67	0.67	70.26	113.42
2747	27.47	12.36	0.69	0.69	69.44	113.69
2748	27.48	12.65	0.71	0.71	68.74	113.92
2749	27.49	12.89	0.72	0.72	68.17	114.12
2750	27.50	13.10	0.74	0.74	67.64	114.32
2751	27.51	13.37	0.75	0.75	67.10	114.53
2752	27.52	13.69	0.77	0.77	66.49	114.78
2753	27.53	14.03	0.80	0.80	65.86	115.04
2754	27.54	14.38	0.82	0.82	65.23	115.31
2755	27.55	14.73	0.84	0.84	64.64	115.57
2756	27.56	15.05	0.86	0.86	64.11	115.80
2757	27.57	15.33	0.88	0.88	63.69	115.99
2758	27.58	15.51	0.89	0.89	63.63	116.06
2759	27.59	15.28	0.89	0.89	63.93	116.02
2760	27.60	14.99	0.87	0.87	64.58	115.88
2761	27.61	14.67	0.86	0.86	65.34	115.72
2762	27.62	14.32	0.85	0.85	66.18	115.54
2763	27.63	13.97	0.83	0.83	67.06	115.35
2764	27.64	13.63	0.82	0.82	67.94	115.16
2765	27.65	13.32	0.80	0.80	68.75	114.99
2766	27.66	13.06	0.79	0.79	69.50	114.82
2767	27.67	12.82	0.78	0.78	70.30	114.64
2768	27.68	12.47	0.76	0.76	71.26	114.42
2769	27.69	12.05	0.74	0.74	72.48	114.13
2770	27.70	11.59	0.72	0.72	73.91	113.80
2771	27.71	11.10	0.69	0.69	75.50	113.44
2772	27.72	10.62	0.67	0.67	77.19	113.06
2773	27.73	10.16	0.64	0.64	78.90	112.68
2774	27.74	9.75	0.62	0.62	80.52	112.33
2775	27.75	9.42	0.60	0.60	81.67	112.09
2776	27.76	9.36	0.60	0.60	82.29	111.98
2777	27.77	9.36	0.60	0.60	82.46	111.98
2778	27.78	9.36	0.60	0.60	82.54	112.00
2779	27.79	9.36	0.60	0.60	82.63	112.02
2780	27.80	9.36	0.60	0.60	82.72	112.05
2781	27.81	9.36	0.61	0.61	82.80	112.07
2782	27.82	9.36	0.61	0.61	82.89	112.09
2783	27.83	9.36	0.61	0.61	82.93	112.12
2784	27.84	9.37	0.61	0.61	82.70	112.20

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2785	27.85	9.56	0.62	0.62	82.13	112.36
2786	27.86	9.80	0.64	0.64	81.25	112.59
2787	27.87	10.06	0.66	0.66	80.28	112.84
2788	27.88	10.34	0.68	0.68	79.29	113.10
2789	27.89	10.63	0.69	0.69	78.34	113.37
2790	27.90	10.90	0.71	0.71	77.46	113.61
2791	27.91	11.15	0.73	0.73	76.69	113.82
2792	27.92	11.36	0.74	0.74	76.09	113.99
2793	27.93	11.49	0.75	0.75	75.63	114.11
2794	27.94	11.59	0.76	0.76	75.23	114.20
2795	27.95	11.72	0.76	0.76	74.81	114.28
2796	27.96	11.86	0.77	0.77	74.35	114.38
2797	27.97	12.01	0.77	0.77	73.87	114.47
2798	27.98	12.16	0.78	0.78	73.41	114.56
2799	27.99	12.30	0.79	0.79	72.98	114.65
2800	28.00	12.42	0.79	0.79	72.61	114.73
2801	28.01	12.53	0.80	0.80	72.41	114.75
2802	28.02	12.47	0.79	0.79	72.41	114.71
2803	28.03	12.35	0.78	0.78	72.60	114.60
2804	28.04	12.22	0.77	0.77	72.85	114.46
2805	28.05	12.08	0.76	0.76	73.13	114.30
2806	28.06	11.93	0.74	0.74	73.42	114.14
2807	28.07	11.78	0.73	0.73	73.72	113.99
2808	28.08	11.64	0.72	0.72	74.00	113.84
2809	28.09	11.53	0.71	0.71	74.25	113.71
2810	28.10	11.44	0.70	0.70	74.47	113.59
2811	28.11	11.34	0.69	0.69	74.71	113.48
2812	28.12	11.22	0.68	0.68	74.98	113.34
2813	28.13	11.08	0.67	0.67	75.30	113.18
2814	28.14	10.93	0.66	0.66	75.64	113.01
2815	28.15	10.78	0.64	0.64	76.00	112.84
2816	28.16	10.64	0.63	0.63	76.35	112.67
2817	28.17	10.51	0.62	0.62	76.68	112.51
2818	28.18	10.40	0.61	0.61	76.80	112.42
2819	28.19	10.45	0.61	0.61	76.49	112.45
2820	28.20	10.71	0.62	0.62	75.71	112.61
2821	28.21	11.01	0.64	0.64	74.64	112.83
2822	28.22	11.35	0.65	0.65	73.50	113.08
2823	28.23	11.70	0.67	0.67	72.35	113.32
2824	28.24	12.05	0.68	0.68	71.27	113.56
2825	28.25	12.38	0.70	0.70	70.28	113.77
2826	28.26	12.67	0.71	0.71	69.45	113.95
2827	28.27	12.91	0.72	0.72	68.90	114.06
2828	28.28	12.94	0.72	0.72	68.60	114.10
2829	28.29	12.94	0.72	0.72	68.49	114.08
2830	28.30	12.94	0.71	0.71	68.40	114.05
2831	28.31	12.94	0.71	0.71	68.31	114.01
2832	28.32	12.94	0.71	0.71	68.21	113.97

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2833	28.33	12.94	0.70	0.70	68.11	113.93
2834	28.34	12.94	0.70	0.70	68.02	113.90
2835	28.35	12.94	0.70	0.70	67.97	113.86
2836	28.36	12.90	0.69	0.69	68.22	113.75
2837	28.37	12.59	0.68	0.68	68.83	113.56
2838	28.38	12.21	0.66	0.66	69.82	113.28
2839	28.39	11.78	0.63	0.63	71.00	112.94
2840	28.40	11.33	0.61	0.61	72.33	112.57
2841	28.41	10.87	0.59	0.59	73.76	112.18
2842	28.42	10.43	0.56	0.56	75.23	111.79
2843	28.43	10.03	0.54	0.54	76.64	111.42
2844	28.44	9.69	0.52	0.52	77.80	111.13
2845	28.45	9.52	0.52	0.52	78.61	110.95
2846	28.46	9.45	0.51	0.51	79.15	110.86
2847	28.47	9.35	0.51	0.51	79.62	110.79
2848	28.48	9.25	0.51	0.51	80.15	110.72
2849	28.49	9.14	0.50	0.50	80.72	110.64
2850	28.50	9.03	0.50	0.50	81.29	110.56
2851	28.51	8.93	0.50	0.50	81.83	110.48
2852	28.52	8.84	0.49	0.49	82.32	110.41
2853	28.53	8.77	0.49	0.49	82.65	110.36
2854	28.54	8.76	0.49	0.49	82.81	110.34
2855	28.55	8.76	0.49	0.49	82.83	110.34
2856	28.56	8.76	0.49	0.49	82.83	110.33
2857	28.57	8.76	0.49	0.49	82.83	110.33
2858	28.58	8.76	0.49	0.49	82.83	110.33
2859	28.59	8.76	0.49	0.49	82.83	110.32
2860	28.60	8.76	0.49	0.49	82.84	110.32
2861	28.61	8.76	0.49	0.49	82.86	110.31
2862	28.62	8.75	0.49	0.49	82.99	110.28
2863	28.63	8.68	0.48	0.48	83.26	110.21
2864	28.64	8.59	0.48	0.48	83.68	110.11
2865	28.65	8.49	0.47	0.47	84.16	109.99
2866	28.66	8.38	0.47	0.47	84.69	109.86
2867	28.67	8.27	0.46	0.46	85.22	109.74
2868	28.68	8.17	0.45	0.45	85.75	109.61
2869	28.69	8.07	0.45	0.45	86.24	109.50
2870	28.70	7.99	0.44	0.44	86.54	109.43
2871	28.71	8.01	0.44	0.44	86.52	109.46
2872	28.72	8.10	0.45	0.45	86.19	109.57
2873	28.73	8.22	0.46	0.46	85.69	109.73
2874	28.74	8.35	0.47	0.47	85.14	109.92
2875	28.75	8.49	0.48	0.48	84.59	110.10
2876	28.76	8.62	0.49	0.49	84.06	110.29
2877	28.77	8.75	0.50	0.50	83.58	110.45
2878	28.78	8.86	0.51	0.51	83.17	110.60
2879	28.79	8.95	0.51	0.51	82.65	110.76
2880	28.80	9.13	0.52	0.52	81.91	110.96

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2881	28.81	9.39	0.54	0.54	80.89	111.22
2882	28.82	9.68	0.56	0.56	79.73	111.51
2883	28.83	10.00	0.57	0.57	78.55	111.83
2884	28.84	10.33	0.59	0.59	77.40	112.14
2885	28.85	10.64	0.61	0.61	76.33	112.43
2886	28.86	10.94	0.63	0.63	75.40	112.69
2887	28.87	11.19	0.64	0.64	74.63	112.90
2888	28.88	11.38	0.65	0.65	73.99	113.06
2889	28.89	11.54	0.66	0.66	73.36	113.19
2890	28.90	11.74	0.67	0.67	72.67	113.32
2891	28.91	11.97	0.68	0.68	71.91	113.46
2892	28.92	12.21	0.68	0.68	71.12	113.60
2893	28.93	12.46	0.69	0.69	70.35	113.74
2894	28.94	12.69	0.70	0.70	69.63	113.86
2895	28.95	12.90	0.71	0.71	69.00	113.98
2896	28.96	13.08	0.71	0.71	68.42	114.08
2897	28.97	13.27	0.72	0.72	67.78	114.21
2898	28.98	13.57	0.73	0.73	67.01	114.36
2899	28.99	13.92	0.75	0.75	66.08	114.55
2900	29.00	14.31	0.76	0.76	65.10	114.75
2901	29.01	14.72	0.77	0.77	64.11	114.96
2902	29.02	15.12	0.79	0.79	63.17	115.15
2903	29.03	15.50	0.80	0.80	62.32	115.32
2904	29.04	15.83	0.81	0.81	61.59	115.47
2905	29.05	16.10	0.82	0.82	60.95	115.61
2906	29.06	16.40	0.83	0.83	60.32	115.76
2907	29.07	16.78	0.85	0.85	59.62	115.94
2908	29.08	17.22	0.86	0.86	58.82	116.14
2909	29.09	17.70	0.88	0.88	57.99	116.35
2910	29.10	18.19	0.90	0.90	57.17	116.57
2911	29.11	18.66	0.92	0.92	56.41	116.76
2912	29.12	19.10	0.93	0.93	55.72	116.94
2913	29.13	19.48	0.94	0.94	55.17	117.09
2914	29.14	19.74	0.95	0.95	54.76	117.19
2915	29.15	19.91	0.96	0.96	54.43	117.26
2916	29.16	20.11	0.96	0.96	54.12	117.33
2917	29.17	20.34	0.97	0.97	53.77	117.41
2918	29.18	20.58	0.98	0.98	53.41	117.48
2919	29.19	20.82	0.98	0.98	53.05	117.56
2920	29.20	21.06	0.99	0.99	52.71	117.63
2921	29.21	21.27	1.00	1.00	52.41	117.70
2922	29.22	21.44	1.00	1.00	52.21	117.74
2923	29.23	21.47	1.00	1.00	52.15	117.76
2924	29.24	21.41	1.00	1.00	52.21	117.75
2925	29.25	21.34	1.00	1.00	52.33	117.73
2926	29.26	21.26	1.00	1.00	52.46	117.71
2927	29.27	21.18	1.00	1.00	52.60	117.69
2928	29.28	21.10	0.99	0.99	52.74	117.67

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2929	29.29	21.03	0.99	0.99	52.87	117.65
2930	29.30	20.96	0.99	0.99	52.98	117.64
2931	29.31	20.91	0.99	0.99	53.03	117.63
2932	29.32	20.95	0.99	0.99	53.01	117.64
2933	29.33	21.02	0.99	0.99	52.92	117.65
2934	29.34	21.09	1.00	1.00	52.82	117.68
2935	29.35	21.17	1.00	1.00	52.70	117.70
2936	29.36	21.25	1.00	1.00	52.58	117.72
2937	29.37	21.33	1.00	1.00	52.46	117.74
2938	29.38	21.40	1.00	1.00	52.36	117.76
2939	29.39	21.46	1.00	1.00	52.24	117.78
2940	29.40	21.57	1.01	1.01	51.99	117.83
2941	29.41	21.90	1.01	1.01	51.56	117.90
2942	29.42	22.31	1.02	1.02	50.97	118.00
2943	29.43	22.77	1.03	1.03	50.32	118.11
2944	29.44	23.25	1.04	1.04	49.64	118.22
2945	29.45	23.74	1.05	1.05	48.97	118.33
2946	29.46	24.21	1.05	1.05	48.35	118.42
2947	29.47	24.62	1.06	1.06	47.80	118.50
2948	29.48	24.97	1.06	1.06	47.35	118.58
2949	29.49	25.26	1.07	1.07	46.97	118.66
2950	29.50	25.62	1.08	1.08	46.60	118.77
2951	29.51	26.05	1.10	1.10	46.19	118.89
2952	29.52	26.52	1.11	1.11	45.74	119.03
2953	29.53	27.00	1.12	1.12	45.29	119.16
2954	29.54	27.49	1.14	1.14	44.85	119.29
2955	29.55	27.94	1.15	1.15	44.46	119.41
2956	29.56	28.33	1.16	1.16	44.11	119.52
2957	29.57	28.65	1.17	1.17	43.89	119.60
2958	29.58	28.76	1.18	1.18	43.77	119.66
2959	29.59	28.89	1.19	1.19	43.73	119.73
2960	29.60	29.04	1.20	1.20	43.69	119.80
2961	29.61	29.20	1.21	1.21	43.65	119.88
2962	29.62	29.36	1.22	1.22	43.60	119.96
2963	29.63	29.52	1.23	1.23	43.56	120.04
2964	29.64	29.67	1.24	1.24	43.52	120.11
2965	29.65	29.79	1.25	1.25	43.51	120.16
2966	29.66	29.83	1.25	1.25	43.59	120.19
2967	29.67	29.66	1.26	1.26	43.77	120.20
2968	29.68	29.45	1.26	1.26	44.06	120.20
2969	29.69	29.22	1.26	1.26	44.37	120.20
2970	29.70	28.98	1.26	1.26	44.71	120.19
2971	29.71	28.74	1.26	1.26	45.05	120.18
2972	29.72	28.51	1.27	1.27	45.37	120.17
2973	29.73	28.30	1.27	1.27	45.67	120.17
2974	29.74	28.13	1.27	1.27	45.97	120.16
2975	29.75	27.89	1.27	1.27	46.35	120.15
2976	29.76	27.53	1.28	1.28	46.87	120.14

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2977	29.77	27.10	1.28	1.28	47.51	120.12
2978	29.78	26.63	1.28	1.28	48.23	120.10
2979	29.79	26.14	1.29	1.29	48.97	120.07
2980	29.80	25.66	1.29	1.29	49.72	120.03
2981	29.81	25.21	1.29	1.29	50.43	119.99
2982	29.82	24.82	1.29	1.29	51.05	119.95
2983	29.83	24.50	1.29	1.29	51.41	119.96
2984	29.84	24.68	1.30	1.30	51.52	120.04
2985	29.85	24.94	1.32	1.32	51.40	120.17
2986	29.86	25.24	1.35	1.35	51.25	120.33
2987	29.87	25.56	1.37	1.37	51.10	120.49
2988	29.88	25.89	1.40	1.40	50.95	120.66
2989	29.89	26.20	1.42	1.42	50.80	120.82
2990	29.90	26.49	1.45	1.45	50.68	120.97
2991	29.91	26.74	1.47	1.47	50.55	121.09
2992	29.92	26.97	1.48	1.48	50.33	121.20
2993	29.93	27.37	1.50	1.50	49.99	121.31
2994	29.94	27.85	1.52	1.52	49.54	121.44
2995	29.95	28.38	1.54	1.54	49.04	121.58
2996	29.96	28.95	1.56	1.56	48.53	121.72
2997	29.97	29.52	1.58	1.58	48.02	121.86
2998	29.98	30.05	1.60	1.60	47.56	121.99
2999	29.99	30.54	1.61	1.61	47.15	122.11
3000	30.00	30.94	1.63	1.63	46.90	122.18
3001	30.01	31.00	1.63	1.63	46.85	122.23
3002	30.02	30.87	1.64	1.64	46.99	122.24
3003	30.03	30.73	1.64	1.64	47.22	122.25
3004	30.04	30.57	1.65	1.65	47.47	122.26
3005	30.05	30.41	1.65	1.65	47.72	122.27
3006	30.06	30.25	1.66	1.66	47.98	122.28
3007	30.07	30.10	1.66	1.66	48.21	122.28
3008	30.08	29.97	1.66	1.66	48.42	122.29
3009	30.09	29.87	1.67	1.67	48.55	122.30
3010	30.10	29.91	1.67	1.67	48.61	122.32
3011	30.11	29.98	1.68	1.68	48.62	122.36
3012	30.12	30.05	1.69	1.69	48.62	122.40
3013	30.13	30.13	1.70	1.70	48.62	122.45
3014	30.14	30.21	1.71	1.71	48.63	122.50
3015	30.15	30.29	1.72	1.72	48.63	122.54
3016	30.16	30.37	1.72	1.72	48.63	122.58
3017	30.17	30.43	1.73	1.73	48.61	122.62
3018	30.18	30.55	1.74	1.74	48.46	122.66
3019	30.19	30.89	1.74	1.74	48.18	122.72
3020	30.20	31.30	1.75	1.75	47.77	122.78
3021	30.21	31.76	1.76	1.76	47.31	122.85
3022	30.22	32.25	1.77	1.77	46.84	122.92
3023	30.23	32.73	1.78	1.78	46.37	122.99
3024	30.24	33.19	1.79	1.79	45.93	123.05

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3025	30.25	33.61	1.79	1.79	45.55	123.11
3026	30.26	33.95	1.80	1.80	45.26	123.15
3027	30.27	34.14	1.80	1.80	45.07	123.20
3028	30.28	34.33	1.81	1.81	44.94	123.24
3029	30.29	34.54	1.82	1.82	44.82	123.30
3030	30.30	34.78	1.83	1.83	44.68	123.36
3031	30.31	35.02	1.84	1.84	44.55	123.42
3032	30.32	35.26	1.85	1.85	44.41	123.48
3033	30.33	35.49	1.87	1.87	44.29	123.54
3034	30.34	35.68	1.87	1.87	44.18	123.59
3035	30.35	35.84	1.88	1.88	44.17	123.62
3036	30.36	35.73	1.89	1.89	44.26	123.64
3037	30.37	35.60	1.89	1.89	44.44	123.65
3038	30.38	35.45	1.90	1.90	44.66	123.67
3039	30.39	35.29	1.91	1.91	44.89	123.68
3040	30.40	35.13	1.91	1.91	45.12	123.70
3041	30.41	34.97	1.92	1.92	45.35	123.71
3042	30.42	34.83	1.92	1.92	45.55	123.72
3043	30.43	34.71	1.93	1.93	45.73	123.73
3044	30.44	34.59	1.93	1.93	45.89	123.72
3045	30.45	34.42	1.93	1.93	46.04	123.70
3046	30.46	34.22	1.92	1.92	46.22	123.67
3047	30.47	33.99	1.92	1.92	46.43	123.63
3048	30.48	33.74	1.91	1.91	46.64	123.59
3049	30.49	33.50	1.90	1.90	46.85	123.55
3050	30.50	33.27	1.90	1.90	47.06	123.51
3051	30.51	33.06	1.89	1.89	47.24	123.47
3052	30.52	32.89	1.89	1.89	47.30	123.47
3053	30.53	33.12	1.89	1.89	47.15	123.50
3054	30.54	33.61	1.91	1.91	46.79	123.58
3055	30.55	34.19	1.93	1.93	46.33	123.69
3056	30.56	34.82	1.95	1.95	45.83	123.80
3057	30.57	35.47	1.96	1.96	45.33	123.91
3058	30.58	36.11	1.98	1.98	44.84	124.02
3059	30.59	36.70	2.00	2.00	44.39	124.11
3060	30.60	37.22	2.01	2.01	44.01	124.19
3061	30.61	37.65	2.02	2.02	43.53	124.30
3062	30.62	38.69	2.05	2.05	42.90	124.45
3063	30.63	40.00	2.09	2.09	42.05	124.66
3064	30.64	41.50	2.13	2.13	41.11	124.88
3065	30.65	43.10	2.16	2.16	40.14	125.10
3066	30.66	44.73	2.20	2.20	39.19	125.31
3067	30.67	46.30	2.23	2.23	38.30	125.49
3068	30.68	47.73	2.26	2.26	37.52	125.65
3069	30.69	48.95	2.28	2.28	36.85	125.78
3070	30.70	49.98	2.29	2.29	36.23	125.90
3071	30.71	51.35	2.32	2.32	35.55	126.04
3072	30.72	53.01	2.35	2.35	34.76	126.20

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3073	30.73	54.86	2.37	2.37	33.90	126.36
3074	30.74	56.81	2.39	2.39	33.03	126.51
3075	30.75	58.75	2.41	2.41	32.17	126.65
3076	30.76	60.59	2.43	2.43	31.39	126.76
3077	30.77	62.23	2.44	2.44	30.70	126.86
3078	30.78	63.58	2.44	2.44	30.13	126.93
3079	30.79	64.75	2.45	2.45	29.58	126.99
3080	30.80	66.23	2.45	2.45	28.99	127.06
3081	30.81	67.96	2.45	2.45	28.32	127.12
3082	30.82	69.86	2.45	2.45	27.59	127.18
3083	30.83	71.81	2.44	2.44	26.85	127.23
3084	30.84	73.73	2.43	2.43	26.14	127.26
3085	30.85	75.51	2.42	2.42	25.48	127.28
3086	30.86	77.06	2.40	2.40	24.92	127.29
3087	30.87	78.27	2.39	2.39	24.52	127.30
3088	30.88	79.01	2.40	2.40	24.22	127.33
3089	30.89	79.93	2.40	2.40	23.98	127.37
3090	30.90	80.98	2.41	2.41	23.70	127.42
3091	30.91	82.10	2.41	2.41	23.40	127.47
3092	30.92	83.24	2.42	2.42	23.11	127.51
3093	30.93	84.34	2.42	2.42	22.82	127.56
3094	30.94	85.34	2.42	2.42	22.57	127.59
3095	30.95	86.18	2.42	2.42	22.38	127.62
3096	30.96	86.64	2.43	2.43	22.31	127.67
3097	30.97	86.76	2.45	2.45	22.33	127.73
3098	30.98	86.89	2.48	2.48	22.41	127.80
3099	30.99	87.05	2.51	2.51	22.51	127.89
3100	31.00	87.21	2.54	2.54	22.60	127.98
3101	31.01	87.37	2.57	2.57	22.70	128.07
3102	31.02	87.53	2.59	2.59	22.79	128.15
3103	31.03	87.66	2.62	2.62	22.87	128.22
3104	31.04	87.77	2.64	2.64	22.94	128.28
3105	31.05	87.76	2.65	2.65	23.01	128.32
3106	31.06	87.70	2.67	2.67	23.10	128.37
3107	31.07	87.63	2.69	2.69	23.20	128.41
3108	31.08	87.55	2.70	2.70	23.31	128.46
3109	31.09	87.47	2.72	2.72	23.42	128.51
3110	31.10	87.39	2.74	2.74	23.53	128.56
3111	31.11	87.31	2.76	2.76	23.63	128.60
3112	31.12	87.25	2.78	2.78	23.72	128.64
3113	31.13	87.21	2.79	2.79	23.78	128.68
3114	31.14	87.31	2.80	2.80	23.83	128.72
3115	31.15	87.45	2.82	2.82	23.88	128.77
3116	31.16	87.60	2.84	2.84	23.93	128.82
3117	31.17	87.76	2.86	2.86	23.98	128.88
3118	31.18	87.92	2.89	2.89	24.03	128.94
3119	31.19	88.08	2.91	2.91	24.08	129.00
3120	31.20	88.22	2.93	2.93	24.13	129.05

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3121	31.21	88.34	2.94	2.94	24.16	129.10
3122	31.22	88.49	2.95	2.95	24.18	129.14
3123	31.23	88.78	2.97	2.97	24.17	129.18
3124	31.24	89.13	2.98	2.98	24.15	129.23
3125	31.25	89.52	3.00	3.00	24.12	129.28
3126	31.26	89.92	3.02	3.02	24.10	129.34
3127	31.27	90.33	3.04	3.04	24.07	129.40
3128	31.28	90.71	3.06	3.06	24.05	129.45
3129	31.29	91.05	3.08	3.08	24.03	129.50
3130	31.30	91.33	3.09	3.09	24.00	129.53
3131	31.31	91.64	3.10	3.10	23.95	129.57
3132	31.32	92.08	3.11	3.11	23.88	129.60
3133	31.33	92.59	3.11	3.11	23.79	129.63
3134	31.34	93.14	3.12	3.12	23.69	129.67
3135	31.35	93.71	3.13	3.13	23.59	129.71
3136	31.36	94.27	3.14	3.14	23.49	129.74
3137	31.37	94.79	3.15	3.15	23.40	129.78
3138	31.38	95.24	3.16	3.16	23.32	129.81
3139	31.39	95.62	3.17	3.17	23.23	129.84
3140	31.40	96.31	3.18	3.18	23.12	129.88
3141	31.41	97.17	3.19	3.19	22.97	129.93
3142	31.42	98.15	3.21	3.21	22.80	129.99
3143	31.43	99.19	3.22	3.22	22.61	130.05
3144	31.44	100.25	3.24	3.24	22.43	130.11
3145	31.45	101.27	3.25	3.25	22.26	130.16
3146	31.46	102.19	3.26	3.26	22.10	130.21
3147	31.47	102.97	3.28	3.28	21.97	130.25
3148	31.48	103.64	3.28	3.28	21.84	130.29
3149	31.49	104.51	3.29	3.29	21.69	130.34
3150	31.50	105.55	3.31	3.31	21.52	130.39
3151	31.51	106.72	3.32	3.32	21.33	130.45
3152	31.52	107.93	3.34	3.34	21.13	130.50
3153	31.53	109.14	3.35	3.35	20.94	130.56
3154	31.54	110.29	3.36	3.36	20.76	130.61
3155	31.55	111.30	3.37	3.37	20.60	130.65
3156	31.56	112.13	3.38	3.38	20.46	130.69
3157	31.57	112.87	3.38	3.38	20.32	130.72
3158	31.58	113.81	3.39	3.39	20.17	130.76
3159	31.59	114.90	3.40	3.40	19.99	130.79
3160	31.60	116.09	3.40	3.40	19.80	130.83
3161	31.61	117.31	3.41	3.41	19.60	130.87
3162	31.62	118.50	3.41	3.41	19.41	130.90
3163	31.63	119.61	3.42	3.42	19.23	130.93
3164	31.64	120.57	3.42	3.42	19.08	130.96
3165	31.65	121.31	3.42	3.42	18.95	130.98
3166	31.66	122.01	3.42	3.42	18.81	130.99
3167	31.67	122.87	3.42	3.42	18.66	131.00
3168	31.68	123.85	3.41	3.41	18.48	131.00

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3169	31.69	124.90	3.40	3.40	18.29	131.01
3170	31.70	125.96	3.40	3.40	18.10	131.01
3171	31.71	126.97	3.39	3.39	17.92	131.02
3172	31.72	127.89	3.38	3.38	17.76	131.02
3173	31.73	128.67	3.38	3.38	17.63	131.02
3174	31.74	129.18	3.37	3.37	17.53	131.02
3175	31.75	129.65	3.37	3.37	17.44	131.02
3176	31.76	130.21	3.37	3.37	17.35	131.03
3177	31.77	130.83	3.36	3.36	17.24	131.03
3178	31.78	131.48	3.36	3.36	17.14	131.03
3179	31.79	132.13	3.35	3.35	17.03	131.04
3180	31.80	132.74	3.35	3.35	16.93	131.04
3181	31.81	133.28	3.35	3.35	16.85	131.04
3182	31.82	133.71	3.34	3.34	16.78	131.04
3183	31.83	133.99	3.34	3.34	16.74	131.05
3184	31.84	134.30	3.35	3.35	16.71	131.07
3185	31.85	134.67	3.35	3.35	16.67	131.09
3186	31.86	135.06	3.36	3.36	16.64	131.10
3187	31.87	135.47	3.37	3.37	16.60	131.12
3188	31.88	135.87	3.37	3.37	16.56	131.14
3189	31.89	136.24	3.38	3.38	16.53	131.16
3190	31.90	136.56	3.38	3.38	16.50	131.18
3191	31.91	136.77	3.38	3.38	16.49	131.19
3192	31.92	136.77	3.39	3.39	16.49	131.19
3193	31.93	136.77	3.39	3.39	16.50	131.20
3194	31.94	136.77	3.39	3.39	16.52	131.21
3195	31.95	136.77	3.40	3.40	16.53	131.22
3196	31.96	136.77	3.40	3.40	16.55	131.23
3197	31.97	136.77	3.41	3.41	16.56	131.24
3198	31.98	136.77	3.41	3.41	16.58	131.25
3199	31.99	136.77	3.41	3.41	16.59	131.25
3200	32.00	136.73	3.42	3.42	16.61	131.26
3201	32.01	136.61	3.42	3.42	16.65	131.27
3202	32.02	136.47	3.43	3.43	16.69	131.29
3203	32.03	136.32	3.44	3.44	16.74	131.30
3204	32.04	136.15	3.45	3.45	16.79	131.32
3205	32.05	135.99	3.46	3.46	16.84	131.33
3206	32.06	135.84	3.47	3.47	16.89	131.35
3207	32.07	135.71	3.47	3.47	16.93	131.36
3208	32.08	135.60	3.48	3.48	16.97	131.37
3209	32.09	135.50	3.49	3.49	17.01	131.38
3210	32.10	135.37	3.49	3.49	17.05	131.39
3211	32.11	135.23	3.50	3.50	17.09	131.41
3212	32.12	135.07	3.51	3.51	17.14	131.42
3213	32.13	134.90	3.52	3.52	17.19	131.44
3214	32.14	134.74	3.53	3.53	17.24	131.45
3215	32.15	134.60	3.53	3.53	17.29	131.46
3216	32.16	134.47	3.54	3.54	17.33	131.47

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3217	32.17	134.37	3.54	3.54	17.37	131.49
3218	32.18	134.26	3.55	3.55	17.40	131.50
3219	32.19	134.13	3.56	3.56	17.45	131.51
3220	32.20	133.98	3.57	3.57	17.49	131.52
3221	32.21	133.82	3.57	3.57	17.54	131.53
3222	32.22	133.65	3.58	3.58	17.59	131.55
3223	32.23	133.50	3.59	3.59	17.64	131.56
3224	32.24	133.36	3.60	3.60	17.69	131.57
3225	32.25	133.24	3.60	3.60	17.72	131.58
3226	32.26	133.17	3.61	3.61	17.75	131.59
3227	32.27	133.11	3.61	3.61	17.78	131.60
3228	32.28	133.04	3.62	3.62	17.81	131.61
3229	32.29	132.96	3.62	3.62	17.84	131.62
3230	32.30	132.88	3.63	3.63	17.87	131.63
3231	32.31	132.80	3.64	3.64	17.90	131.64
3232	32.32	132.72	3.64	3.64	17.93	131.65
3233	32.33	132.66	3.65	3.65	17.96	131.66
3234	32.34	132.60	3.65	3.65	17.98	131.67
3235	32.35	132.59	3.66	3.66	18.00	131.68
3236	32.36	132.59	3.66	3.66	18.03	131.69
3237	32.37	132.59	3.67	3.67	18.05	131.71
3238	32.38	132.59	3.68	3.68	18.08	131.72
3239	32.39	132.59	3.69	3.69	18.10	131.74
3240	32.40	132.59	3.70	3.70	18.13	131.76
3241	32.41	132.59	3.70	3.70	18.15	131.77
3242	32.42	132.59	3.71	3.71	18.17	131.78
3243	32.43	132.59	3.71	3.71	18.19	131.79
3244	32.44	132.59	3.72	3.72	18.21	131.81
3245	32.45	132.59	3.73	3.73	18.24	131.82
3246	32.46	132.59	3.73	3.73	18.26	131.83
3247	32.47	132.59	3.74	3.74	18.29	131.85
3248	32.48	132.59	3.75	3.75	18.31	131.87
3249	32.49	132.59	3.76	3.76	18.34	131.88
3250	32.50	132.59	3.77	3.77	18.36	131.90
3251	32.51	132.59	3.77	3.77	18.38	131.91
3252	32.52	132.62	3.78	3.78	18.40	131.92
3253	32.53	132.68	3.79	3.79	18.42	131.94
3254	32.54	132.75	3.80	3.80	18.43	131.96
3255	32.55	132.83	3.81	3.81	18.45	131.98
3256	32.56	132.91	3.82	3.82	18.47	132.00
3257	32.57	132.99	3.83	3.83	18.49	132.02
3258	32.58	133.06	3.84	3.84	18.51	132.04
3259	32.59	133.13	3.85	3.85	18.53	132.06
3260	32.60	133.19	3.85	3.85	18.53	132.09
3261	32.61	133.92	3.88	3.88	18.51	132.15
3262	32.62	134.97	3.92	3.92	18.46	132.23
3263	32.63	136.18	3.96	3.96	18.40	132.33
3264	32.64	137.49	4.01	4.01	18.34	132.44

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3265	32.65	138.84	4.06	4.06	18.27	132.55
3266	32.66	140.15	4.10	4.10	18.21	132.65
3267	32.67	141.35	4.15	4.15	18.16	132.75
3268	32.68	142.39	4.18	4.18	18.11	132.83
3269	32.69	143.19	4.21	4.21	18.07	132.90
3270	32.70	144.02	4.24	4.24	18.04	132.97
3271	32.71	145.05	4.28	4.28	17.99	133.05
3272	32.72	146.21	4.32	4.32	17.95	133.15
3273	32.73	147.43	4.37	4.37	17.90	133.24
3274	32.74	148.67	4.41	4.41	17.85	133.34
3275	32.75	149.84	4.46	4.46	17.80	133.43
3276	32.76	150.91	4.50	4.50	17.76	133.51
3277	32.77	151.80	4.53	4.53	17.74	133.57
3278	32.78	152.18	4.55	4.55	17.73	133.61
3279	32.79	152.31	4.57	4.57	17.75	133.64
3280	32.80	152.46	4.58	4.58	17.77	133.67
3281	32.81	152.63	4.60	4.60	17.80	133.71
3282	32.82	152.81	4.62	4.62	17.82	133.74
3283	32.83	152.98	4.64	4.64	17.85	133.77
3284	32.84	153.15	4.66	4.66	17.87	133.80
3285	32.85	153.29	4.68	4.68	17.89	133.83
3286	32.86	153.41	4.69	4.69	17.91	133.86
3287	32.87	153.68	4.70	4.70	17.91	133.88
3288	32.88	154.05	4.72	4.72	17.90	133.91
3289	32.89	154.48	4.73	4.73	17.89	133.94
3290	32.90	154.94	4.75	4.75	17.87	133.98
3291	32.91	155.41	4.77	4.77	17.86	134.02
3292	32.92	155.87	4.79	4.79	17.85	134.05
3293	32.93	156.30	4.81	4.81	17.84	134.08
3294	32.94	156.66	4.82	4.82	17.83	134.11
3295	32.95	156.96	4.83	4.83	17.81	134.13
3296	32.96	157.39	4.84	4.84	17.77	134.15
3297	32.97	157.91	4.85	4.85	17.73	134.17
3298	32.98	158.50	4.86	4.86	17.68	134.19
3299	32.99	159.13	4.87	4.87	17.62	134.22
3300	33.00	159.76	4.88	4.88	17.57	134.24
3301	33.01	160.36	4.88	4.88	17.52	134.26
3302	33.02	160.89	4.89	4.89	17.47	134.28
3303	33.03	161.34	4.90	4.90	17.43	134.29
3304	33.04	161.72	4.90	4.90	17.38	134.30
3305	33.05	162.20	4.90	4.90	17.33	134.31
3306	33.06	162.77	4.90	4.90	17.26	134.32
3307	33.07	163.40	4.90	4.90	17.18	134.33
3308	33.08	164.05	4.90	4.90	17.11	134.33
3309	33.09	164.69	4.89	4.89	17.03	134.34
3310	33.10	165.29	4.89	4.89	16.96	134.35
3311	33.11	165.82	4.89	4.89	16.90	134.35
3312	33.12	166.25	4.89	4.89	16.84	134.36

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3313	33.13	166.73	4.89	4.89	16.78	134.37
3314	33.14	167.34	4.89	4.89	16.72	134.38
3315	33.15	168.05	4.89	4.89	16.64	134.39
3316	33.16	168.82	4.89	4.89	16.56	134.40
3317	33.17	169.60	4.90	4.90	16.48	134.41
3318	33.18	170.36	4.90	4.90	16.40	134.43
3319	33.19	171.06	4.90	4.90	16.33	134.44
3320	33.20	171.66	4.90	4.90	16.26	134.45
3321	33.21	172.11	4.90	4.90	16.21	134.45
3322	33.22	172.55	4.90	4.90	16.16	134.46
3323	33.23	173.09	4.89	4.89	16.09	134.46
3324	33.24	173.71	4.89	4.89	16.02	134.46
3325	33.25	174.35	4.88	4.88	15.95	134.47
3326	33.26	175.00	4.88	4.88	15.87	134.47
3327	33.27	175.62	4.88	4.88	15.80	134.47
3328	33.28	176.18	4.87	4.87	15.74	134.47
3329	33.29	176.64	4.87	4.87	15.69	134.47
3330	33.30	176.82	4.86	4.86	15.65	134.47
3331	33.31	176.88	4.85	4.85	15.62	134.45
3332	33.32	176.95	4.84	4.84	15.59	134.43
3333	33.33	177.03	4.83	4.83	15.55	134.41
3334	33.34	177.11	4.81	4.81	15.51	134.39
3335	33.35	177.19	4.80	4.80	15.48	134.37
3336	33.36	177.27	4.78	4.78	15.44	134.35
3337	33.37	177.33	4.77	4.77	15.41	134.34
3338	33.38	177.39	4.76	4.76	15.39	134.32
3339	33.39	177.15	4.75	4.75	15.39	134.30
3340	33.40	176.83	4.74	4.74	15.40	134.28
3341	33.41	176.46	4.72	4.72	15.40	134.25
3342	33.42	176.06	4.71	4.71	15.41	134.22
3343	33.43	175.65	4.69	4.69	15.42	134.19
3344	33.44	175.26	4.67	4.67	15.43	134.16
3345	33.45	174.89	4.66	4.66	15.44	134.13
3346	33.46	174.58	4.65	4.65	15.44	134.11
3347	33.47	174.28	4.64	4.64	15.46	134.08
3348	33.48	173.72	4.62	4.62	15.48	134.05
3349	33.49	173.04	4.60	4.60	15.52	134.01
3350	33.50	172.27	4.58	4.58	15.56	133.97
3351	33.51	171.46	4.56	4.56	15.60	133.92
3352	33.52	170.65	4.54	4.54	15.64	133.88
3353	33.53	169.88	4.52	4.52	15.67	133.84
3354	33.54	169.19	4.50	4.50	15.71	133.80
3355	33.55	168.61	4.49	4.49	15.75	133.76
3356	33.56	168.01	4.48	4.48	15.80	133.73
3357	33.57	167.16	4.47	4.47	15.86	133.70
3358	33.58	166.16	4.45	4.45	15.95	133.67
3359	33.59	165.06	4.44	4.44	16.04	133.63
3360	33.60	163.92	4.42	4.42	16.14	133.59

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3361	33.61	162.80	4.41	4.41	16.23	133.55
3362	33.62	161.75	4.39	4.39	16.32	133.51
3363	33.63	160.83	4.38	4.38	16.40	133.48
3364	33.64	160.10	4.37	4.37	16.48	133.45
3365	33.65	159.33	4.37	4.37	16.56	133.42
3366	33.66	158.36	4.36	4.36	16.66	133.40
3367	33.67	157.24	4.35	4.35	16.78	133.37
3368	33.68	156.05	4.34	4.34	16.91	133.33
3369	33.69	154.82	4.33	4.33	17.04	133.30
3370	33.70	153.64	4.32	4.32	17.16	133.27
3371	33.71	152.56	4.32	4.32	17.28	133.23
3372	33.72	151.63	4.31	4.31	17.38	133.21
3373	33.73	150.92	4.30	4.30	17.47	133.18
3374	33.74	150.13	4.29	4.29	17.56	133.15
3375	33.75	149.17	4.28	4.28	17.66	133.12
3376	33.76	148.10	4.27	4.27	17.77	133.08
3377	33.77	146.97	4.25	4.25	17.89	133.04
3378	33.78	145.83	4.24	4.24	18.01	132.99
3379	33.79	144.75	4.22	4.22	18.12	132.95
3380	33.80	143.79	4.21	4.21	18.22	132.91
3381	33.81	142.99	4.20	4.20	18.31	132.88
3382	33.82	142.34	4.19	4.19	18.40	132.85
3383	33.83	141.55	4.18	4.18	18.49	132.82
3384	33.84	140.62	4.17	4.17	18.59	132.78
3385	33.85	139.60	4.16	4.16	18.71	132.74
3386	33.86	138.54	4.14	4.14	18.83	132.70
3387	33.87	137.50	4.13	4.13	18.95	132.66
3388	33.88	136.52	4.12	4.12	19.06	132.62
3389	33.89	135.67	4.11	4.11	19.16	132.58
3390	33.90	135.00	4.10	4.10	19.23	132.57
3391	33.91	134.92	4.10	4.10	19.28	132.56
3392	33.92	134.83	4.11	4.11	19.32	132.57
3393	33.93	134.73	4.12	4.12	19.36	132.59
3394	33.94	134.62	4.13	4.13	19.40	132.60
3395	33.95	134.51	4.14	4.14	19.45	132.62
3396	33.96	134.41	4.15	4.15	19.49	132.63
3397	33.97	134.31	4.15	4.15	19.53	132.64
3398	33.98	134.23	4.16	4.16	19.57	132.65
3399	33.99	134.17	4.17	4.17	19.60	132.67
3400	34.00	134.12	4.17	4.17	19.63	132.68
3401	34.01	134.05	4.18	4.18	19.67	132.69
3402	34.02	133.97	4.19	4.19	19.71	132.71
3403	34.03	133.89	4.20	4.20	19.75	132.72
3404	34.04	133.81	4.21	4.21	19.79	132.74
3405	34.05	133.73	4.22	4.22	19.83	132.75
3406	34.06	133.66	4.23	4.23	19.87	132.77
3407	34.07	133.61	4.24	4.24	19.91	132.77
3408	34.08	133.41	4.24	4.24	19.94	132.77

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3409	34.09	133.06	4.23	4.23	19.99	132.76
3410	34.10	132.65	4.23	4.23	20.04	132.74
3411	34.11	132.21	4.22	4.22	20.10	132.72
3412	34.12	131.74	4.22	4.22	20.16	132.70
3413	34.13	131.29	4.21	4.21	20.21	132.69
3414	34.14	130.87	4.20	4.20	20.27	132.67
3415	34.15	130.50	4.20	4.20	20.32	132.65
3416	34.16	130.21	4.19	4.19	20.35	132.65
3417	34.17	130.26	4.20	4.20	20.37	132.65
3418	34.18	130.32	4.21	4.21	20.39	132.67
3419	34.19	130.40	4.22	4.22	20.41	132.69
3420	34.20	130.48	4.23	4.23	20.43	132.71
3421	34.21	130.56	4.24	4.24	20.45	132.73
3422	34.22	130.64	4.25	4.25	20.46	132.75
3423	34.23	130.71	4.26	4.26	20.48	132.76
3424	34.24	130.77	4.27	4.27	20.50	132.78
3425	34.25	130.88	4.28	4.28	20.50	132.80
3426	34.26	131.17	4.29	4.29	20.50	132.83
3427	34.27	131.51	4.31	4.31	20.50	132.87
3428	34.28	131.90	4.33	4.33	20.49	132.91
3429	34.29	132.30	4.35	4.35	20.49	132.95
3430	34.30	132.71	4.38	4.38	20.48	132.99
3431	34.31	133.09	4.40	4.40	20.48	133.04
3432	34.32	133.43	4.41	4.41	20.47	133.07
3433	34.33	133.72	4.43	4.43	20.46	133.10
3434	34.34	134.13	4.44	4.44	20.43	133.14
3435	34.35	134.74	4.46	4.46	20.39	133.17
3436	34.36	135.46	4.48	4.48	20.33	133.22
3437	34.37	136.25	4.50	4.50	20.26	133.27
3438	34.38	137.06	4.53	4.53	20.20	133.32
3439	34.39	137.86	4.55	4.55	20.13	133.37
3440	34.40	138.61	4.57	4.57	20.07	133.41
3441	34.41	139.26	4.59	4.59	20.02	133.45
3442	34.42	139.77	4.60	4.60	19.97	133.49
3443	34.43	140.40	4.61	4.61	19.90	133.52
3444	34.44	141.19	4.63	4.63	19.83	133.56
3445	34.45	142.08	4.64	4.64	19.74	133.60
3446	34.46	143.05	4.66	4.66	19.64	133.64
3447	34.47	144.02	4.68	4.68	19.55	133.69
3448	34.48	144.97	4.70	4.70	19.46	133.73
3449	34.49	145.83	4.71	4.71	19.37	133.77
3450	34.50	146.56	4.73	4.73	19.30	133.80
3451	34.51	147.17	4.73	4.73	19.22	133.82
3452	34.52	147.97	4.74	4.74	19.12	133.84
3453	34.53	148.94	4.74	4.74	18.99	133.86
3454	34.54	150.02	4.74	4.74	18.85	133.88
3455	34.55	151.15	4.74	4.74	18.71	133.90
3456	34.56	152.28	4.75	4.75	18.56	133.92

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3457	34.57	153.36	4.75	4.75	18.42	133.94
3458	34.58	154.31	4.75	4.75	18.30	133.96
3459	34.59	155.10	4.75	4.75	18.19	133.97
3460	34.60	155.89	4.74	4.74	18.07	133.98
3461	34.61	156.93	4.74	4.74	17.93	133.99
3462	34.62	158.16	4.73	4.73	17.76	133.99
3463	34.63	159.51	4.72	4.72	17.57	134.00
3464	34.64	160.89	4.71	4.71	17.38	134.01
3465	34.65	162.25	4.70	4.70	17.19	134.01
3466	34.66	163.51	4.69	4.69	17.02	134.01
3467	34.67	164.61	4.68	4.68	16.87	134.01
3468	34.68	165.47	4.67	4.67	16.74	134.01
3469	34.69	166.21	4.65	4.65	16.60	133.99
3470	34.70	167.13	4.63	4.63	16.44	133.96
3471	34.71	168.18	4.60	4.60	16.25	133.93
3472	34.72	169.30	4.56	4.56	16.06	133.89
3473	34.73	170.44	4.53	4.53	15.86	133.86
3474	34.74	171.54	4.49	4.49	15.66	133.82
3475	34.75	172.54	4.46	4.46	15.49	133.78
3476	34.76	173.39	4.44	4.44	15.34	133.75
3477	34.77	173.99	4.41	4.41	15.21	133.71
3478	34.78	174.56	4.38	4.38	15.08	133.67
3479	34.79	175.26	4.35	4.35	14.93	133.63
3480	34.80	176.03	4.31	4.31	14.76	133.57
3481	34.81	176.84	4.27	4.27	14.59	133.51
3482	34.82	177.65	4.23	4.23	14.41	133.45
3483	34.83	178.41	4.19	4.19	14.25	133.39
3484	34.84	179.10	4.15	4.15	14.10	133.34
3485	34.85	179.65	4.12	4.12	13.98	133.29
3486	34.86	180.00	4.10	4.10	13.88	133.25
3487	34.87	180.37	4.07	4.07	13.78	133.21
3488	34.88	180.80	4.04	4.04	13.67	133.16
3489	34.89	181.28	4.00	4.00	13.54	133.11
3490	34.90	181.77	3.97	3.97	13.42	133.05
3491	34.91	182.24	3.93	3.93	13.29	132.99
3492	34.92	182.69	3.90	3.90	13.18	132.94
3493	34.93	183.08	3.87	3.87	13.08	132.89
3494	34.94	183.35	3.85	3.85	13.00	132.84
3495	34.95	183.14	3.82	3.82	12.93	132.78
3496	34.96	182.87	3.78	3.78	12.87	132.70
3497	34.97	182.57	3.74	3.74	12.79	132.62
3498	34.98	182.25	3.69	3.69	12.71	132.52
3499	34.99	181.93	3.64	3.64	12.63	132.42
3500	35.00	181.61	3.60	3.60	12.55	132.33
3501	35.01	181.33	3.56	3.56	12.47	132.24
3502	35.02	181.09	3.52	3.52	12.42	132.17
3503	35.03	180.74	3.50	3.50	12.38	132.10
3504	35.04	180.05	3.47	3.47	12.36	132.03

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3505	35.05	179.21	3.43	3.43	12.35	131.94
3506	35.06	178.28	3.39	3.39	12.34	131.85
3507	35.07	177.31	3.35	3.35	12.32	131.75
3508	35.08	176.34	3.31	3.31	12.31	131.65
3509	35.09	175.42	3.27	3.27	12.29	131.55
3510	35.10	174.61	3.24	3.24	12.28	131.47
3511	35.11	173.94	3.21	3.21	12.28	131.39
3512	35.12	173.13	3.19	3.19	12.30	131.33
3513	35.13	172.01	3.16	3.16	12.34	131.25
3514	35.14	170.70	3.14	3.14	12.38	131.17
3515	35.15	169.28	3.10	3.10	12.43	131.08
3516	35.16	167.81	3.07	3.07	12.49	130.98
3517	35.17	166.38	3.04	3.04	12.54	130.89
3518	35.18	165.04	3.01	3.01	12.59	130.80
3519	35.19	163.89	2.99	2.99	12.64	130.72
3520	35.20	162.95	2.97	2.97	12.70	130.65
3521	35.21	161.62	2.95	2.95	12.78	130.58
3522	35.22	159.96	2.93	2.93	12.88	130.51
3523	35.23	158.08	2.90	2.90	13.01	130.42
3524	35.24	156.07	2.88	2.88	13.14	130.32
3525	35.25	154.04	2.85	2.85	13.28	130.22
3526	35.26	152.08	2.82	2.82	13.42	130.12
3527	35.27	150.31	2.80	2.80	13.54	130.03
3528	35.28	148.81	2.78	2.78	13.65	129.95
3529	35.29	147.61	2.76	2.76	13.76	129.87
3530	35.30	146.16	2.74	2.74	13.86	129.79
3531	35.31	144.41	2.71	2.71	13.99	129.70
3532	35.32	142.47	2.69	2.69	14.14	129.59
3533	35.33	140.44	2.66	2.66	14.30	129.48
3534	35.34	138.43	2.63	2.63	14.45	129.37
3535	35.35	136.52	2.60	2.60	14.61	129.25
3536	35.36	134.83	2.57	2.57	14.74	129.16
3537	35.37	133.45	2.55	2.55	14.85	129.07
3538	35.38	132.34	2.53	2.53	14.95	128.97
3539	35.39	130.96	2.50	2.50	15.03	128.86
3540	35.40	129.36	2.47	2.47	15.13	128.74
3541	35.41	127.61	2.43	2.43	15.24	128.59
3542	35.42	125.82	2.39	2.39	15.36	128.45
3543	35.43	124.07	2.35	2.35	15.48	128.30
3544	35.44	122.45	2.32	2.32	15.59	128.16
3545	35.45	121.04	2.29	2.29	15.68	128.04
3546	35.46	119.97	2.27	2.27	15.75	127.94
3547	35.47	119.17	2.25	2.25	15.81	127.85
3548	35.48	118.17	2.22	2.22	15.87	127.75
3549	35.49	117.04	2.19	2.19	15.93	127.64
3550	35.50	115.83	2.16	2.16	16.00	127.51
3551	35.51	114.61	2.13	2.13	16.08	127.39
3552	35.52	113.44	2.11	2.11	16.15	127.26

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3553	35.53	112.38	2.08	2.08	16.21	127.15
3554	35.54	111.49	2.06	2.06	16.27	127.06
3555	35.55	110.92	2.05	2.05	16.32	127.00
3556	35.56	110.45	2.04	2.04	16.38	126.96
3557	35.57	109.89	2.03	2.03	16.44	126.92
3558	35.58	109.27	2.02	2.02	16.52	126.88
3559	35.59	108.62	2.02	2.02	16.59	126.84
3560	35.60	107.98	2.01	2.01	16.67	126.79
3561	35.61	107.37	2.00	2.00	16.75	126.75
3562	35.62	106.83	1.99	1.99	16.81	126.71
3563	35.63	106.39	1.99	1.99	16.87	126.69
3564	35.64	106.07	1.99	1.99	16.94	126.67
3565	35.65	105.70	1.99	1.99	17.03	126.68
3566	35.66	105.26	1.99	1.99	17.13	126.68
3567	35.67	104.78	2.00	2.00	17.24	126.68
3568	35.68	104.29	2.00	2.00	17.36	126.69
3569	35.69	103.82	2.01	2.01	17.47	126.69
3570	35.70	103.37	2.01	2.01	17.57	126.69
3571	35.71	102.99	2.01	2.01	17.66	126.69
3572	35.72	102.71	2.01	2.01	17.74	126.70
3573	35.73	102.55	2.02	2.02	17.81	126.71
3574	35.74	102.35	2.03	2.03	17.88	126.73
3575	35.75	102.12	2.03	2.03	17.97	126.75
3576	35.76	101.88	2.04	2.04	18.06	126.78
3577	35.77	101.64	2.05	2.05	18.15	126.80
3578	35.78	101.40	2.06	2.06	18.23	126.82
3579	35.79	101.19	2.07	2.07	18.31	126.84
3580	35.80	101.01	2.07	2.07	18.37	126.85
3581	35.81	100.96	2.07	2.07	18.41	126.87
3582	35.82	101.02	2.08	2.08	18.42	126.88
3583	35.83	101.09	2.08	2.08	18.43	126.90
3584	35.84	101.17	2.09	2.09	18.44	126.92
3585	35.85	101.25	2.09	2.09	18.45	126.93
3586	35.86	101.33	2.10	2.10	18.46	126.95
3587	35.87	101.41	2.10	2.10	18.47	126.97
3588	35.88	101.47	2.11	2.11	18.47	126.99
3589	35.89	101.53	2.11	2.11	18.47	127.00
3590	35.90	101.70	2.11	2.11	18.45	127.01
3591	35.91	101.95	2.11	2.11	18.40	127.01
3592	35.92	102.25	2.11	2.11	18.34	127.02
3593	35.93	102.56	2.11	2.11	18.28	127.03
3594	35.94	102.89	2.11	2.11	18.22	127.04
3595	35.95	103.21	2.11	2.11	18.16	127.04
3596	35.96	103.50	2.11	2.11	18.10	127.05
3597	35.97	103.76	2.11	2.11	18.06	127.06
3598	35.98	103.95	2.11	2.11	18.01	127.06
3599	35.99	104.17	2.11	2.11	17.95	127.05
3600	36.00	104.44	2.10	2.10	17.87	127.04

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3601	36.01	104.74	2.09	2.09	17.78	127.02
3602	36.02	105.06	2.09	2.09	17.69	127.01
3603	36.03	105.39	2.08	2.08	17.60	126.99
3604	36.04	105.70	2.07	2.07	17.51	126.97
3605	36.05	105.98	2.07	2.07	17.43	126.96
3606	36.06	106.22	2.06	2.06	17.36	126.94
3607	36.07	106.39	2.05	2.05	17.29	126.92
3608	36.08	106.56	2.04	2.04	17.20	126.89
3609	36.09	106.78	2.03	2.03	17.10	126.84
3610	36.10	107.01	2.01	2.01	16.99	126.79
3611	36.11	107.25	2.00	2.00	16.87	126.74
3612	36.12	107.49	1.98	1.98	16.75	126.69
3613	36.13	107.72	1.97	1.97	16.64	126.64
3614	36.14	107.92	1.96	1.96	16.54	126.60
3615	36.15	108.08	1.94	1.94	16.47	126.57
3616	36.16	108.15	1.94	1.94	16.43	126.54
3617	36.17	108.21	1.94	1.94	16.39	126.53
3618	36.18	108.29	1.93	1.93	16.36	126.51
3619	36.19	108.36	1.93	1.93	16.32	126.49
3620	36.20	108.45	1.92	1.92	16.28	126.48
3621	36.21	108.53	1.91	1.91	16.24	126.46
3622	36.22	108.60	1.91	1.91	16.21	126.44
3623	36.23	108.66	1.91	1.91	16.18	126.43
3624	36.24	108.70	1.90	1.90	16.18	126.43
3625	36.25	108.70	1.91	1.91	16.22	126.46
3626	36.26	108.70	1.92	1.92	16.27	126.50
3627	36.27	108.70	1.94	1.94	16.34	126.55
3628	36.28	108.70	1.95	1.95	16.41	126.60
3629	36.29	108.70	1.97	1.97	16.47	126.65
3630	36.30	108.70	1.98	1.98	16.54	126.70
3631	36.31	108.70	1.99	1.99	16.60	126.74
3632	36.32	108.70	2.00	2.00	16.65	126.78
3633	36.33	108.68	2.01	2.01	16.73	126.83
3634	36.34	108.62	2.03	2.03	16.83	126.90
3635	36.35	108.55	2.05	2.05	16.95	126.97
3636	36.36	108.47	2.08	2.08	17.08	127.06
3637	36.37	108.39	2.11	2.11	17.22	127.15
3638	36.38	108.31	2.13	2.13	17.35	127.23
3639	36.39	108.23	2.15	2.15	17.48	127.31
3640	36.40	108.17	2.18	2.18	17.59	127.38
3641	36.41	108.11	2.19	2.19	17.69	127.44
3642	36.42	107.97	2.21	2.21	17.80	127.50
3643	36.43	107.78	2.23	2.23	17.93	127.56
3644	36.44	107.56	2.25	2.25	18.08	127.63
3645	36.45	107.32	2.28	2.28	18.24	127.70
3646	36.46	107.08	2.30	2.30	18.40	127.77
3647	36.47	106.84	2.33	2.33	18.56	127.85
3648	36.48	106.62	2.35	2.35	18.70	127.91

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3649	36.49	106.43	2.37	2.37	18.82	127.96
3650	36.50	106.29	2.38	2.38	18.92	128.00
3651	36.51	106.12	2.39	2.39	19.01	128.04
3652	36.52	105.92	2.41	2.41	19.11	128.07
3653	36.53	105.69	2.42	2.42	19.22	128.11
3654	36.54	105.45	2.43	2.43	19.33	128.14
3655	36.55	105.20	2.45	2.45	19.44	128.18
3656	36.56	104.97	2.46	2.46	19.55	128.21
3657	36.57	104.76	2.47	2.47	19.65	128.24
3658	36.58	104.59	2.48	2.48	19.73	128.27
3659	36.59	104.50	2.49	2.49	19.79	128.29
3660	36.60	104.44	2.50	2.50	19.83	128.31
3661	36.61	104.37	2.50	2.50	19.88	128.32
3662	36.62	104.29	2.51	2.51	19.93	128.34
3663	36.63	104.21	2.52	2.52	19.98	128.37
3664	36.64	104.13	2.53	2.53	20.04	128.39
3665	36.65	104.05	2.53	2.53	20.09	128.41
3666	36.66	103.98	2.54	2.54	20.13	128.42
3667	36.67	103.93	2.55	2.55	20.16	128.43
3668	36.68	103.93	2.55	2.55	20.18	128.44
3669	36.69	103.93	2.55	2.55	20.20	128.45
3670	36.70	103.93	2.55	2.55	20.21	128.46
3671	36.71	103.93	2.56	2.56	20.23	128.47
3672	36.72	103.93	2.56	2.56	20.25	128.48
3673	36.73	103.93	2.56	2.56	20.26	128.49
3674	36.74	103.93	2.57	2.57	20.28	128.50
3675	36.75	103.93	2.57	2.57	20.29	128.50
3676	36.76	103.91	2.57	2.57	20.31	128.51
3677	36.77	103.86	2.57	2.57	20.33	128.52
3678	36.78	103.79	2.58	2.58	20.37	128.53
3679	36.79	103.72	2.58	2.58	20.40	128.54
3680	36.80	103.63	2.59	2.59	20.44	128.55
3681	36.81	103.55	2.59	2.59	20.48	128.56
3682	36.82	103.48	2.60	2.60	20.52	128.57
3683	36.83	103.41	2.60	2.60	20.55	128.58
3684	36.84	103.35	2.60	2.60	20.59	128.59
3685	36.85	103.27	2.61	2.61	20.63	128.60
3686	36.86	103.15	2.61	2.61	20.68	128.61
3687	36.87	103.01	2.62	2.62	20.75	128.63
3688	36.88	102.85	2.63	2.63	20.82	128.65
3689	36.89	102.69	2.64	2.64	20.90	128.67
3690	36.90	102.53	2.65	2.65	20.97	128.69
3691	36.91	102.38	2.66	2.66	21.04	128.71
3692	36.92	102.25	2.66	2.66	21.10	128.73
3693	36.93	102.14	2.67	2.67	21.15	128.73
3694	36.94	101.95	2.67	2.67	21.20	128.73
3695	36.95	101.69	2.67	2.67	21.25	128.72
3696	36.96	101.39	2.67	2.67	21.31	128.71

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3697	36.97	101.07	2.66	2.66	21.38	128.70
3698	36.98	100.75	2.66	2.66	21.44	128.68
3699	36.99	100.43	2.66	2.66	21.51	128.67
3700	37.00	100.14	2.66	2.66	21.57	128.66
3701	37.01	99.89	2.65	2.65	21.62	128.65
3702	37.02	99.72	2.65	2.65	21.64	128.63
3703	37.03	99.61	2.65	2.65	21.65	128.61
3704	37.04	99.47	2.64	2.64	21.65	128.58
3705	37.05	99.32	2.63	2.63	21.64	128.55
3706	37.06	99.16	2.62	2.62	21.63	128.52
3707	37.07	99.00	2.61	2.61	21.63	128.49
3708	37.08	98.84	2.60	2.60	21.62	128.45
3709	37.09	98.70	2.59	2.59	21.62	128.43
3710	37.10	98.59	2.58	2.58	21.60	128.40
3711	37.11	98.58	2.57	2.57	21.57	128.37
3712	37.12	98.64	2.56	2.56	21.51	128.34
3713	37.13	98.71	2.54	2.54	21.43	128.30
3714	37.14	98.79	2.53	2.53	21.34	128.26
3715	37.15	98.87	2.51	2.51	21.25	128.21
3716	37.16	98.95	2.49	2.49	21.16	128.17
3717	37.17	99.03	2.48	2.48	21.07	128.12
3718	37.18	99.09	2.46	2.46	21.00	128.08
3719	37.19	99.14	2.45	2.45	20.95	128.06
3720	37.20	99.15	2.45	2.45	20.94	128.05
3721	37.21	99.15	2.45	2.45	20.94	128.05
3722	37.22	99.15	2.45	2.45	20.94	128.05
3723	37.23	99.15	2.45	2.45	20.95	128.05
3724	37.24	99.15	2.46	2.46	20.95	128.06
3725	37.25	99.15	2.46	2.46	20.96	128.06
3726	37.26	99.15	2.46	2.46	20.96	128.06
3727	37.27	99.15	2.46	2.46	20.96	128.06
3728	37.28	99.17	2.45	2.45	20.93	128.05
3729	37.29	99.28	2.44	2.44	20.87	128.02
3730	37.30	99.42	2.43	2.43	20.77	127.98
3731	37.31	99.57	2.41	2.41	20.66	127.93
3732	37.32	99.74	2.39	2.39	20.54	127.88
3733	37.33	99.90	2.37	2.37	20.43	127.83
3734	37.34	100.05	2.36	2.36	20.31	127.78
3735	37.35	100.19	2.34	2.34	20.21	127.73
3736	37.36	100.31	2.33	2.33	20.12	127.69
3737	37.37	100.37	2.31	2.31	20.03	127.64
3738	37.38	100.43	2.29	2.29	19.91	127.57
3739	37.39	100.50	2.26	2.26	19.77	127.49
3740	37.40	100.58	2.23	2.23	19.62	127.39
3741	37.41	100.66	2.20	2.20	19.45	127.29
3742	37.42	100.74	2.17	2.17	19.29	127.20
3743	37.43	100.82	2.14	2.14	19.14	127.10
3744	37.44	100.88	2.12	2.12	19.01	127.02

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3745	37.45	100.94	2.10	2.10	18.97	126.99
3746	37.46	100.84	2.12	2.12	19.02	127.02
3747	37.47	100.71	2.14	2.14	19.17	127.10
3748	37.48	100.56	2.17	2.17	19.35	127.19
3749	37.49	100.40	2.20	2.20	19.54	127.30
3750	37.50	100.24	2.24	2.24	19.73	127.40
3751	37.51	100.08	2.27	2.27	19.91	127.49
3752	37.52	99.94	2.29	2.29	20.08	127.58
3753	37.53	99.81	2.32	2.32	20.22	127.65
3754	37.54	99.72	2.34	2.34	20.33	127.70
3755	37.55	99.60	2.35	2.35	20.43	127.74
3756	37.56	99.47	2.36	2.36	20.53	127.79
3757	37.57	99.31	2.38	2.38	20.65	127.84
3758	37.58	99.15	2.40	2.40	20.77	127.89
3759	37.59	98.99	2.42	2.42	20.89	127.94
3760	37.60	98.84	2.43	2.43	21.01	127.98
3761	37.61	98.70	2.45	2.45	21.11	128.02
3762	37.62	98.58	2.46	2.46	21.20	128.06
3763	37.63	98.49	2.47	2.47	21.28	128.09
3764	37.64	98.37	2.49	2.49	21.38	128.13
3765	37.65	98.22	2.50	2.50	21.48	128.17
3766	37.66	98.06	2.52	2.52	21.60	128.22
3767	37.67	97.90	2.54	2.54	21.72	128.26
3768	37.68	97.74	2.55	2.55	21.84	128.31
3769	37.69	97.59	2.57	2.57	21.95	128.35
3770	37.70	97.46	2.58	2.58	22.04	128.39
3771	37.71	97.36	2.60	2.60	22.15	128.43
3772	37.72	97.25	2.62	2.62	22.29	128.49
3773	37.73	97.12	2.66	2.66	22.47	128.58
3774	37.74	96.97	2.69	2.69	22.67	128.68
3775	37.75	96.81	2.73	2.73	22.89	128.79
3776	37.76	96.65	2.78	2.78	23.12	128.89
3777	37.77	96.49	2.82	2.82	23.33	128.99
3778	37.78	96.35	2.85	2.85	23.52	129.08
3779	37.79	96.23	2.88	2.88	23.69	129.15
3780	37.80	96.10	2.91	2.91	23.85	129.22
3781	37.81	95.87	2.93	2.93	24.02	129.28
3782	37.82	95.60	2.97	2.97	24.23	129.35
3783	37.83	95.29	3.00	3.00	24.46	129.43
3784	37.84	94.97	3.04	3.04	24.70	129.51
3785	37.85	94.64	3.08	3.08	24.94	129.59
3786	37.86	94.34	3.11	3.11	25.17	129.66
3787	37.87	94.06	3.14	3.14	25.37	129.73
3788	37.88	93.83	3.17	3.17	25.55	129.78
3789	37.89	93.61	3.19	3.19	25.74	129.84
3790	37.90	93.30	3.23	3.23	25.96	129.91
3791	37.91	92.94	3.27	3.27	26.22	129.99
3792	37.92	92.55	3.31	3.31	26.51	130.07

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3793	37.93	92.14	3.35	3.35	26.80	130.16
3794	37.94	91.74	3.40	3.40	27.09	130.24
3795	37.95	91.37	3.44	3.44	27.35	130.31
3796	37.96	91.04	3.47	3.47	27.58	130.37
3797	37.97	90.78	3.50	3.50	27.78	130.42
3798	37.98	90.47	3.51	3.51	27.97	130.46
3799	37.99	90.08	3.54	3.54	28.18	130.50
3800	38.00	89.63	3.56	3.56	28.41	130.54
3801	38.01	89.15	3.59	3.59	28.67	130.58
3802	38.02	88.66	3.62	3.62	28.93	130.62
3803	38.03	88.19	3.64	3.64	29.18	130.66
3804	38.04	87.76	3.67	3.67	29.41	130.69
3805	38.05	87.40	3.69	3.69	29.59	130.72
3806	38.06	87.14	3.70	3.70	29.74	130.74
3807	38.07	86.91	3.71	3.71	29.86	130.75
3808	38.08	86.63	3.71	3.71	29.98	130.75
3809	38.09	86.33	3.72	3.72	30.11	130.76
3810	38.10	86.00	3.73	3.73	30.25	130.77
3811	38.11	85.68	3.74	3.74	30.39	130.77
3812	38.12	85.37	3.74	3.74	30.53	130.78
3813	38.13	85.10	3.75	3.75	30.65	130.79
3814	38.14	84.87	3.76	3.76	30.70	130.80
3815	38.15	85.18	3.77	3.77	30.65	130.82
3816	38.16	85.86	3.78	3.78	30.51	130.87
3817	38.17	86.65	3.80	3.80	30.32	130.92
3818	38.18	87.52	3.81	3.81	30.11	130.97
3819	38.19	88.42	3.83	3.83	29.89	131.03
3820	38.20	89.30	3.85	3.85	29.68	131.09
3821	38.21	90.11	3.86	3.86	29.49	131.14
3822	38.22	90.83	3.88	3.88	29.32	131.18
3823	38.23	91.41	3.89	3.89	29.10	131.23
3824	38.24	92.82	3.90	3.90	28.78	131.29
3825	38.25	94.59	3.92	3.92	28.33	131.36
3826	38.26	96.61	3.93	3.93	27.82	131.44
3827	38.27	98.78	3.94	3.94	27.28	131.51
3828	38.28	100.97	3.95	3.95	26.75	131.59
3829	38.29	103.09	3.96	3.96	26.24	131.65
3830	38.30	105.03	3.96	3.96	25.78	131.70
3831	38.31	106.67	3.96	3.96	25.39	131.74
3832	38.32	108.01	3.96	3.96	25.03	131.77
3833	38.33	109.67	3.96	3.96	24.65	131.81
3834	38.34	111.67	3.96	3.96	24.20	131.85
3835	38.35	113.91	3.95	3.95	23.70	131.88
3836	38.36	116.26	3.94	3.94	23.18	131.91
3837	38.37	118.60	3.93	3.93	22.67	131.93
3838	38.38	120.82	3.91	3.91	22.19	131.95
3839	38.39	122.81	3.90	3.90	21.77	131.95
3840	38.40	124.44	3.88	3.88	21.46	131.97

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3841	38.41	125.50	3.90	3.90	21.26	132.02
3842	38.42	126.67	3.93	3.93	21.14	132.10
3843	38.43	128.04	3.97	3.97	21.03	132.20
3844	38.44	129.54	4.02	4.02	20.91	132.31
3845	38.45	131.09	4.06	4.06	20.78	132.42
3846	38.46	132.61	4.11	4.11	20.66	132.53
3847	38.47	134.02	4.15	4.15	20.55	132.63
3848	38.48	135.25	4.19	4.19	20.46	132.72
3849	38.49	136.18	4.22	4.22	20.46	132.81
3850	38.50	136.18	4.28	4.28	20.57	132.90
3851	38.51	136.18	4.35	4.35	20.77	133.03
3852	38.52	136.18	4.44	4.44	21.00	133.16
3853	38.53	136.18	4.53	4.53	21.24	133.31
3854	38.54	136.18	4.62	4.62	21.49	133.45
3855	38.55	136.18	4.71	4.71	21.72	133.59
3856	38.56	136.18	4.79	4.79	21.93	133.71
3857	38.57	136.18	4.85	4.85	22.11	133.80
3858	38.58	135.96	4.90	4.90	22.31	133.88
3859	38.59	135.27	4.95	4.95	22.54	133.94
3860	38.60	134.43	5.00	5.00	22.82	134.01
3861	38.61	133.51	5.06	5.06	23.14	134.07
3862	38.62	132.54	5.12	5.12	23.46	134.14
3863	38.63	131.57	5.18	5.18	23.79	134.21
3864	38.64	130.65	5.24	5.24	24.10	134.27
3865	38.65	129.83	5.28	5.28	24.37	134.32
3866	38.66	129.16	5.32	5.32	24.62	134.36
3867	38.67	128.47	5.35	5.35	24.86	134.40
3868	38.68	127.53	5.40	5.40	25.15	134.43
3869	38.69	126.45	5.44	5.44	25.48	134.48
3870	38.70	125.26	5.49	5.49	25.84	134.52
3871	38.71	124.04	5.54	5.54	26.21	134.56
3872	38.72	122.84	5.59	5.59	26.58	134.59
3873	38.73	121.73	5.63	5.63	26.92	134.63
3874	38.74	120.77	5.66	5.66	27.21	134.65
3875	38.75	120.02	5.69	5.69	27.43	134.66
3876	38.76	119.49	5.69	5.69	27.61	134.66
3877	38.77	118.83	5.70	5.70	27.77	134.66
3878	38.78	118.08	5.70	5.70	27.95	134.65
3879	38.79	117.28	5.71	5.71	28.15	134.64
3880	38.80	116.46	5.71	5.71	28.35	134.63
3881	38.81	115.68	5.72	5.72	28.54	134.62
3882	38.82	114.97	5.72	5.72	28.72	134.61
3883	38.83	114.36	5.72	5.72	28.84	134.60
3884	38.84	114.18	5.72	5.72	28.87	134.59
3885	38.85	114.47	5.70	5.70	28.80	134.57
3886	38.86	114.81	5.68	5.68	28.67	134.55
3887	38.87	115.20	5.66	5.66	28.52	134.53
3888	38.88	115.61	5.64	5.64	28.37	134.51

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3889	38.89	116.01	5.61	5.61	28.22	134.49
3890	38.90	116.39	5.59	5.59	28.07	134.47
3891	38.91	116.73	5.57	5.57	27.95	134.45
3892	38.92	117.01	5.55	5.55	27.80	134.43
3893	38.93	117.67	5.53	5.53	27.59	134.41
3894	38.94	118.66	5.49	5.49	27.29	134.38
3895	38.95	119.83	5.45	5.45	26.93	134.35
3896	38.96	121.09	5.40	5.40	26.55	134.31
3897	38.97	122.40	5.35	5.35	26.14	134.27
3898	38.98	123.67	5.30	5.30	25.75	134.23
3899	38.99	124.85	5.25	5.25	25.39	134.18
3900	39.00	125.88	5.21	5.21	25.07	134.14
3901	39.01	126.71	5.17	5.17	24.77	134.10
3902	39.02	127.77	5.13	5.13	24.46	134.06
3903	39.03	129.10	5.08	5.08	24.08	134.02
3904	39.04	130.60	5.02	5.02	23.65	133.96
3905	39.05	132.21	4.95	4.95	23.19	133.89
3906	39.06	133.84	4.88	4.88	22.72	133.82
3907	39.07	135.40	4.81	4.81	22.27	133.74
3908	39.08	136.82	4.74	4.74	21.86	133.66
3909	39.09	138.02	4.68	4.68	21.52	133.60
3910	39.10	138.92	4.65	4.65	21.26	133.56
3911	39.11	139.91	4.63	4.63	21.02	133.54
3912	39.12	141.09	4.61	4.61	20.77	133.52
3913	39.13	142.41	4.58	4.58	20.50	133.50
3914	39.14	143.79	4.55	4.55	20.21	133.47
3915	39.15	145.16	4.51	4.51	19.92	133.44
3916	39.16	146.46	4.48	4.48	19.65	133.41
3917	39.17	147.61	4.45	4.45	19.41	133.38
3918	39.18	148.55	4.43	4.43	19.24	133.37
3919	39.19	149.26	4.44	4.44	19.12	133.39
3920	39.20	150.14	4.46	4.46	19.05	133.43
3921	39.21	151.16	4.48	4.48	18.97	133.49
3922	39.22	152.27	4.51	4.51	18.89	133.55
3923	39.23	153.41	4.54	4.54	18.80	133.61
3924	39.24	154.53	4.56	4.56	18.72	133.67
3925	39.25	155.56	4.59	4.59	18.64	133.72
3926	39.26	156.45	4.61	4.61	18.58	133.77
3927	39.27	157.13	4.63	4.63	18.54	133.82
3928	39.28	157.67	4.65	4.65	18.52	133.87
3929	39.29	158.34	4.68	4.68	18.51	133.93
3930	39.30	159.09	4.72	4.72	18.51	134.00
3931	39.31	159.90	4.76	4.76	18.50	134.07
3932	39.32	160.71	4.80	4.80	18.49	134.14
3933	39.33	161.49	4.84	4.84	18.49	134.21
3934	39.34	162.20	4.88	4.88	18.48	134.28
3935	39.35	162.79	4.91	4.91	18.48	134.33
3936	39.36	163.21	4.93	4.93	18.46	134.36

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3937	39.37	163.62	4.94	4.94	18.44	134.39
3938	39.38	164.11	4.95	4.95	18.40	134.41
3939	39.39	164.65	4.96	4.96	18.37	134.44
3940	39.40	165.22	4.97	4.97	18.33	134.47
3941	39.41	165.78	4.99	4.99	18.29	134.49
3942	39.42	166.32	5.00	5.00	18.26	134.52
3943	39.43	166.79	5.01	5.01	18.23	134.54
3944	39.44	167.17	5.02	5.02	18.21	134.57
3945	39.45	167.44	5.04	5.04	18.20	134.59
3946	39.46	167.75	5.06	5.06	18.21	134.63
3947	39.47	168.12	5.08	5.08	18.22	134.66
3948	39.48	168.51	5.11	5.11	18.23	134.71
3949	39.49	168.92	5.13	5.13	18.24	134.75
3950	39.50	169.32	5.16	5.16	18.26	134.79
3951	39.51	169.69	5.18	5.18	18.27	134.83
3952	39.52	170.00	5.20	5.20	18.28	134.86
3953	39.53	170.23	5.22	5.22	18.29	134.89
3954	39.54	170.28	5.24	5.24	18.33	134.92
3955	39.55	170.35	5.26	5.26	18.37	134.95
3956	39.56	170.42	5.29	5.29	18.42	134.99
3957	39.57	170.51	5.31	5.31	18.47	135.03
3958	39.58	170.59	5.34	5.34	18.52	135.07
3959	39.59	170.66	5.37	5.37	18.57	135.10
3960	39.60	170.74	5.39	5.39	18.61	135.14
3961	39.61	170.79	5.41	5.41	18.64	135.16
3962	39.62	170.87	5.41	5.41	18.62	135.15
3963	39.63	170.98	5.38	5.38	18.56	135.12
3964	39.64	171.12	5.35	5.35	18.47	135.08
3965	39.65	171.28	5.31	5.31	18.37	135.03
3966	39.66	171.44	5.27	5.27	18.27	134.98
3967	39.67	171.60	5.23	5.23	18.17	134.93
3968	39.68	171.75	5.19	5.19	18.07	134.88
3969	39.69	171.89	5.16	5.16	17.98	134.83
3970	39.70	172.00	5.13	5.13	17.91	134.79
3971	39.71	172.10	5.11	5.11	17.84	134.76
3972	39.72	172.22	5.08	5.08	17.76	134.72
3973	39.73	172.37	5.04	5.04	17.68	134.67
3974	39.74	172.53	5.01	5.01	17.58	134.62
3975	39.75	172.69	4.97	4.97	17.48	134.57
3976	39.76	172.85	4.93	4.93	17.38	134.52
3977	39.77	173.00	4.90	4.90	17.29	134.47
3978	39.78	173.12	4.87	4.87	17.22	134.43
3979	39.79	173.17	4.85	4.85	17.19	134.41
3980	39.80	172.88	4.85	4.85	17.20	134.39
3981	39.81	172.52	4.85	4.85	17.24	134.39
3982	39.82	172.12	4.85	4.85	17.28	134.38
3983	39.83	171.69	4.85	4.85	17.33	134.37
3984	39.84	171.26	4.85	4.85	17.38	134.36

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3985	39.85	170.84	4.84	4.84	17.43	134.36
3986	39.86	170.46	4.84	4.84	17.47	134.35
3987	39.87	170.15	4.84	4.84	17.52	134.34
3988	39.88	169.73	4.85	4.85	17.60	134.35
3989	39.89	169.02	4.86	4.86	17.71	134.36
3990	39.90	168.18	4.88	4.88	17.85	134.37
3991	39.91	167.24	4.90	4.90	18.00	134.38
3992	39.92	166.27	4.92	4.92	18.17	134.40
3993	39.93	165.30	4.94	4.94	18.33	134.41
3994	39.94	164.39	4.95	4.95	18.48	134.42
3995	39.95	163.59	4.97	4.97	18.62	134.43
3996	39.96	162.94	4.98	4.98	18.73	134.45
3997	39.97	162.70	5.00	5.00	18.84	134.47
3998	39.98	162.47	5.03	5.03	18.94	134.52
3999	39.99	162.20	5.07	5.07	19.07	134.57
4000	40.00	161.91	5.11	5.11	19.20	134.62
4001	40.01	161.61	5.16	5.16	19.34	134.68
4002	40.02	161.32	5.20	5.20	19.47	134.73
4003	40.03	161.05	5.23	5.23	19.59	134.78
4004	40.04	160.82	5.27	5.27	19.68	134.82
4005	40.05	160.78	5.29	5.29	19.70	134.84
4006	40.06	161.55	5.29	5.29	19.65	134.86
4007	40.07	162.49	5.29	5.29	19.53	134.88
4008	40.08	163.55	5.29	5.29	19.39	134.89
4009	40.09	164.68	5.29	5.29	19.25	134.91
4010	40.10	165.82	5.29	5.29	19.11	134.93
4011	40.11	166.91	5.29	5.29	18.97	134.94
4012	40.12	167.89	5.29	5.29	18.85	134.95
4013	40.13	168.71	5.29	5.29	18.74	134.96
4014	40.14	169.31	5.28	5.28	18.64	134.96
4015	40.15	169.96	5.26	5.26	18.52	134.94
4016	40.16	170.74	5.24	5.24	18.38	134.92
4017	40.17	171.60	5.21	5.21	18.22	134.90
4018	40.18	172.49	5.18	5.18	18.05	134.87
4019	40.19	173.37	5.15	5.15	17.89	134.85
4020	40.20	174.21	5.13	5.13	17.74	134.82
4021	40.21	174.94	5.10	5.10	17.61	134.80
4022	40.22	175.53	5.08	5.08	17.51	134.78
4023	40.23	175.60	5.07	5.07	17.46	134.76
4024	40.24	175.60	5.06	5.06	17.43	134.74
4025	40.25	175.60	5.04	5.04	17.40	134.72
4026	40.26	175.60	5.03	5.03	17.36	134.69
4027	40.27	175.60	5.01	5.01	17.33	134.67
4028	40.28	175.60	5.00	5.00	17.30	134.65
4029	40.29	175.60	4.98	4.98	17.27	134.63
4030	40.30	175.60	4.97	4.97	17.24	134.61
4031	40.31	175.58	4.96	4.96	17.22	134.59
4032	40.32	175.47	4.94	4.94	17.20	134.57

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4033	40.33	175.33	4.92	4.92	17.18	134.54
4034	40.34	175.18	4.90	4.90	17.15	134.51
4035	40.35	175.02	4.88	4.88	17.12	134.47
4036	40.36	174.86	4.86	4.86	17.10	134.44
4037	40.37	174.70	4.84	4.84	17.07	134.41
4038	40.38	174.56	4.82	4.82	17.05	134.38
4039	40.39	174.45	4.81	4.81	17.03	134.35
4040	40.40	174.30	4.79	4.79	17.02	134.33
4041	40.41	174.06	4.78	4.78	17.00	134.30
4042	40.42	173.77	4.75	4.75	16.99	134.26
4043	40.43	173.46	4.73	4.73	16.97	134.22
4044	40.44	173.14	4.70	4.70	16.95	134.17
4045	40.45	172.82	4.68	4.68	16.93	134.13
4046	40.46	172.51	4.66	4.66	16.91	134.09
4047	40.47	172.25	4.63	4.63	16.90	134.05
4048	40.48	172.03	4.62	4.62	16.89	134.03
4049	40.49	171.79	4.61	4.61	16.89	134.00
4050	40.50	171.47	4.59	4.59	16.90	133.98
4051	40.51	171.10	4.58	4.58	16.91	133.95
4052	40.52	170.70	4.56	4.56	16.92	133.92
4053	40.53	170.29	4.55	4.55	16.93	133.89
4054	40.54	169.90	4.53	4.53	16.94	133.86
4055	40.55	169.53	4.52	4.52	16.95	133.83
4056	40.56	169.22	4.50	4.50	16.96	133.80
4057	40.57	168.92	4.49	4.49	16.98	133.78
4058	40.58	168.37	4.48	4.48	17.00	133.74
4059	40.59	167.69	4.46	4.46	17.04	133.71
4060	40.60	166.93	4.44	4.44	17.09	133.66
4061	40.61	166.12	4.42	4.42	17.13	133.62
4062	40.62	165.31	4.40	4.40	17.18	133.57
4063	40.63	164.54	4.38	4.38	17.22	133.52
4064	40.64	163.84	4.36	4.36	17.26	133.48
4065	40.65	163.26	4.34	4.34	17.30	133.45
4066	40.66	162.69	4.33	4.33	17.34	133.41
4067	40.67	161.91	4.31	4.31	17.39	133.36
4068	40.68	160.99	4.28	4.28	17.44	133.31
4069	40.69	159.97	4.26	4.26	17.50	133.25
4070	40.70	158.92	4.23	4.23	17.57	133.18
4071	40.71	157.87	4.20	4.20	17.63	133.12
4072	40.72	156.89	4.17	4.17	17.69	133.06
4073	40.73	156.03	4.15	4.15	17.74	133.01
4074	40.74	155.34	4.13	4.13	17.80	132.97
4075	40.75	154.59	4.13	4.13	17.88	132.94
4076	40.76	153.63	4.12	4.12	17.99	132.91
4077	40.77	152.52	4.11	4.11	18.12	132.87
4078	40.78	151.32	4.10	4.10	18.25	132.84
4079	40.79	150.10	4.09	4.09	18.39	132.80
4080	40.80	148.91	4.08	4.08	18.53	132.76

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4081	40.81	147.82	4.07	4.07	18.65	132.72
4082	40.82	146.89	4.06	4.06	18.76	132.69
4083	40.83	146.12	4.05	4.05	18.86	132.65
4084	40.84	145.12	4.03	4.03	18.96	132.60
4085	40.85	143.90	4.01	4.01	19.08	132.54
4086	40.86	142.52	3.98	3.98	19.22	132.47
4087	40.87	141.07	3.95	3.95	19.36	132.40
4088	40.88	139.61	3.93	3.93	19.51	132.33
4089	40.89	138.22	3.90	3.90	19.65	132.25
4090	40.90	136.96	3.87	3.87	19.77	132.19
4091	40.91	135.92	3.85	3.85	19.88	132.12
4092	40.92	135.00	3.83	3.83	19.97	132.05
4093	40.93	133.80	3.79	3.79	20.05	131.95
4094	40.94	132.37	3.74	3.74	20.14	131.83
4095	40.95	130.80	3.69	3.69	20.24	131.70
4096	40.96	129.17	3.63	3.63	20.34	131.57
4097	40.97	127.57	3.58	3.58	20.45	131.43
4098	40.98	126.07	3.53	3.53	20.56	131.30
4099	40.99	124.75	3.48	3.48	20.65	131.19
4100	41.00	123.69	3.45	3.45	20.73	131.09
4101	41.01	122.72	3.42	3.42	20.82	131.00
4102	41.02	121.50	3.39	3.39	20.93	130.90
4103	41.03	120.09	3.34	3.34	21.05	130.78
4104	41.04	118.57	3.30	3.30	21.19	130.66
4105	41.05	117.02	3.26	3.26	21.33	130.53
4106	41.06	115.52	3.21	3.21	21.47	130.40
4107	41.07	114.15	3.17	3.17	21.60	130.28
4108	41.08	112.97	3.14	3.14	21.72	130.18
4109	41.09	112.02	3.11	3.11	21.84	130.08
4110	41.10	110.83	3.08	3.08	21.98	129.99
4111	41.11	109.38	3.05	3.05	22.15	129.87
4112	41.12	107.75	3.01	3.01	22.34	129.74
4113	41.13	106.03	2.96	2.96	22.55	129.60
4114	41.14	104.31	2.92	2.92	22.77	129.45
4115	41.15	102.67	2.88	2.88	22.98	129.31
4116	41.16	101.20	2.84	2.84	23.17	129.18
4117	41.17	99.98	2.81	2.81	23.33	129.07
4118	41.18	98.99	2.78	2.78	23.46	128.95
4119	41.19	97.78	2.74	2.74	23.59	128.81
4120	41.20	96.35	2.69	2.69	23.73	128.64
4121	41.21	94.78	2.63	2.63	23.89	128.46
4122	41.22	93.15	2.58	2.58	24.06	128.26
4123	41.23	91.55	2.52	2.52	24.23	128.07
4124	41.24	90.05	2.47	2.47	24.40	127.88
4125	41.25	88.73	2.43	2.43	24.55	127.72
4126	41.26	87.69	2.39	2.39	24.68	127.60
4127	41.27	87.07	2.38	2.38	24.82	127.52
4128	41.28	86.31	2.37	2.37	24.98	127.46

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4129	41.29	85.43	2.36	2.36	25.16	127.39
4130	41.30	84.50	2.34	2.34	25.36	127.31
4131	41.31	83.54	2.32	2.32	25.57	127.23
4132	41.32	82.61	2.31	2.31	25.77	127.16
4133	41.33	81.76	2.29	2.29	25.95	127.08
4134	41.34	81.04	2.28	2.28	26.12	127.02
4135	41.35	80.49	2.27	2.27	26.29	126.99
4136	41.36	79.93	2.27	2.27	26.49	126.96
4137	41.37	79.25	2.27	2.27	26.72	126.95
4138	41.38	78.48	2.28	2.28	26.99	126.93
4139	41.39	77.67	2.28	2.28	27.28	126.91
4140	41.40	76.86	2.28	2.28	27.57	126.89
4141	41.41	76.09	2.28	2.28	27.84	126.86
4142	41.42	75.40	2.28	2.28	28.09	126.84
4143	41.43	74.83	2.28	2.28	28.31	126.82
4144	41.44	74.37	2.28	2.28	28.52	126.81
4145	41.45	73.80	2.28	2.28	28.75	126.80
4146	41.46	73.14	2.28	2.28	29.02	126.78
4147	41.47	72.41	2.29	2.29	29.32	126.77
4148	41.48	71.66	2.29	2.29	29.63	126.75
4149	41.49	70.92	2.29	2.29	29.93	126.73
4150	41.50	70.23	2.29	2.29	30.22	126.71
4151	41.51	69.62	2.29	2.29	30.48	126.69
4152	41.52	69.14	2.29	2.29	30.73	126.68
4153	41.53	68.65	2.30	2.30	31.02	126.70
4154	41.54	68.03	2.32	2.32	31.38	126.72
4155	41.55	67.33	2.34	2.34	31.79	126.75
4156	41.56	66.57	2.35	2.35	32.24	126.77
4157	41.57	65.79	2.37	2.37	32.69	126.80
4158	41.58	65.05	2.39	2.39	33.14	126.82
4159	41.59	64.36	2.40	2.40	33.54	126.83
4160	41.60	63.78	2.41	2.41	33.89	126.84
4161	41.61	63.30	2.42	2.42	34.22	126.84
4162	41.62	62.69	2.42	2.42	34.56	126.83
4163	41.63	61.95	2.42	2.42	34.97	126.82
4164	41.64	61.13	2.43	2.43	35.42	126.80
4165	41.65	60.26	2.43	2.43	35.91	126.77
4166	41.66	59.39	2.44	2.44	36.39	126.75
4167	41.67	58.56	2.44	2.44	36.86	126.72
4168	41.68	57.82	2.44	2.44	37.29	126.69
4169	41.69	57.21	2.44	2.44	37.65	126.66
4170	41.70	56.73	2.44	2.44	38.00	126.64
4171	41.71	56.15	2.44	2.44	38.37	126.63
4172	41.72	55.46	2.45	2.45	38.81	126.61
4173	41.73	54.72	2.45	2.45	39.29	126.58
4174	41.74	53.94	2.45	2.45	39.79	126.55
4175	41.75	53.18	2.45	2.45	40.29	126.52
4176	41.76	52.47	2.45	2.45	40.76	126.49

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4177	41.77	51.85	2.45	2.45	41.18	126.46
4178	41.78	51.36	2.45	2.45	41.55	126.44
4179	41.79	50.95	2.45	2.45	41.93	126.43
4180	41.80	50.43	2.46	2.46	42.36	126.43
4181	41.81	49.83	2.47	2.47	42.85	126.43
4182	41.82	49.19	2.48	2.48	43.39	126.42
4183	41.83	48.54	2.49	2.49	43.93	126.41
4184	41.84	47.91	2.49	2.49	44.47	126.40
4185	41.85	47.33	2.50	2.50	44.96	126.38
4186	41.86	46.84	2.50	2.50	45.37	126.37
4187	41.87	46.52	2.51	2.51	45.72	126.38
4188	41.88	46.30	2.52	2.52	46.04	126.40
4189	41.89	46.02	2.54	2.54	46.40	126.44
4190	41.90	45.71	2.56	2.56	46.79	126.47
4191	41.91	45.39	2.58	2.58	47.21	126.51
4192	41.92	45.06	2.60	2.60	47.62	126.54
4193	41.93	44.76	2.61	2.61	48.02	126.57
4194	41.94	44.48	2.63	2.63	48.37	126.60
4195	41.95	44.26	2.64	2.64	48.61	126.62
4196	41.96	44.23	2.65	2.65	48.74	126.65
4197	41.97	44.29	2.66	2.66	48.77	126.67
4198	41.98	44.37	2.67	2.67	48.79	126.71
4199	41.99	44.44	2.68	2.68	48.80	126.74
4200	42.00	44.53	2.69	2.69	48.82	126.78
4201	42.01	44.61	2.70	2.70	48.83	126.81
4202	42.02	44.68	2.72	2.72	48.85	126.85
4203	42.03	44.75	2.72	2.72	48.86	126.88
4204	42.04	44.81	2.73	2.73	48.74	126.91
4205	42.05	45.28	2.74	2.74	48.46	126.94
4206	42.06	45.87	2.74	2.74	47.98	126.98
4207	42.07	46.54	2.74	2.74	47.44	127.02
4208	42.08	47.26	2.75	2.75	46.87	127.07
4209	42.09	47.99	2.75	2.75	46.29	127.11
4210	42.10	48.70	2.75	2.75	45.74	127.14
4211	42.11	49.35	2.75	2.75	45.24	127.17
4212	42.12	49.89	2.74	2.74	44.79	127.19
4213	42.13	50.41	2.74	2.74	44.30	127.21
4214	42.14	51.21	2.73	2.73	43.69	127.23
4215	42.15	52.18	2.72	2.72	42.93	127.24
4216	42.16	53.26	2.70	2.70	42.09	127.24
4217	42.17	54.40	2.68	2.68	41.22	127.24
4218	42.18	55.53	2.66	2.66	40.36	127.23
4219	42.19	56.60	2.63	2.63	39.54	127.20
4220	42.20	57.56	2.61	2.61	38.82	127.18
4221	42.21	58.34	2.59	2.59	38.23	127.15
4222	42.22	58.95	2.57	2.57	37.69	127.12
4223	42.23	59.70	2.55	2.55	37.14	127.09
4224	42.24	60.56	2.52	2.52	36.50	127.05

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4225	42.25	61.51	2.49	2.49	35.81	126.99
4226	42.26	62.49	2.46	2.46	35.10	126.93
4227	42.27	63.45	2.42	2.42	34.40	126.86
4228	42.28	64.34	2.38	2.38	33.75	126.79
4229	42.29	65.11	2.35	2.35	33.19	126.72
4230	42.30	65.71	2.33	2.33	32.78	126.67
4231	42.31	66.03	2.32	2.32	32.47	126.63
4232	42.32	66.42	2.30	2.30	32.22	126.61
4233	42.33	66.87	2.29	2.29	31.93	126.58
4234	42.34	67.35	2.27	2.27	31.61	126.54
4235	42.35	67.84	2.25	2.25	31.29	126.50
4236	42.36	68.31	2.24	2.24	30.99	126.46
4237	42.37	68.74	2.22	2.22	30.71	126.43
4238	42.38	69.11	2.21	2.21	30.51	126.39
4239	42.39	69.16	2.20	2.20	30.44	126.36
4240	42.40	68.79	2.19	2.19	30.51	126.33
4241	42.41	68.35	2.18	2.18	30.65	126.29
4242	42.42	67.85	2.18	2.18	30.82	126.24
4243	42.43	67.33	2.17	2.17	30.99	126.20
4244	42.44	66.81	2.16	2.16	31.16	126.15
4245	42.45	66.31	2.15	2.15	31.33	126.10
4246	42.46	65.87	2.14	2.14	31.47	126.06
4247	42.47	65.51	2.13	2.13	31.66	126.03
4248	42.48	65.00	2.14	2.14	31.93	126.02
4249	42.49	64.25	2.15	2.15	32.32	126.02
4250	42.50	63.38	2.16	2.16	32.80	126.02
4251	42.51	62.43	2.17	2.17	33.33	126.01
4252	42.52	61.46	2.18	2.18	33.87	126.00
4253	42.53	60.50	2.18	2.18	34.41	125.99
4254	42.54	59.61	2.19	2.19	34.92	125.97
4255	42.55	58.84	2.19	2.19	35.37	125.95
4256	42.56	58.23	2.19	2.19	35.77	125.94
4257	42.57	57.56	2.20	2.20	36.19	125.92
4258	42.58	56.73	2.20	2.20	36.69	125.89
4259	42.59	55.79	2.20	2.20	37.26	125.86
4260	42.60	54.78	2.20	2.20	37.88	125.82
4261	42.61	53.76	2.20	2.20	38.51	125.77
4262	42.62	52.78	2.20	2.20	39.13	125.72
4263	42.63	51.88	2.20	2.20	39.70	125.67
4264	42.64	51.13	2.19	2.19	40.17	125.61
4265	42.65	50.55	2.19	2.19	40.55	125.55
4266	42.66	49.92	2.16	2.16	40.88	125.45
4267	42.67	49.15	2.14	2.14	41.24	125.33
4268	42.68	48.30	2.11	2.11	41.65	125.19
4269	42.69	47.41	2.08	2.08	42.09	125.05
4270	42.70	46.52	2.05	2.05	42.53	124.90
4271	42.71	45.68	2.02	2.02	42.96	124.75
4272	42.72	44.93	2.00	2.00	43.36	124.62

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4273	42.73	44.32	1.97	1.97	43.60	124.51
4274	42.74	44.16	1.96	1.96	43.67	124.42
4275	42.75	44.10	1.94	1.94	43.57	124.34
4276	42.76	44.03	1.91	1.91	43.42	124.24
4277	42.77	43.95	1.89	1.89	43.26	124.14
4278	42.78	43.86	1.86	1.86	43.09	124.03
4279	42.79	43.79	1.83	1.83	42.92	123.92
4280	42.80	43.71	1.81	1.81	42.76	123.82
4281	42.81	43.65	1.79	1.79	42.61	123.74
4282	42.82	43.66	1.77	1.77	42.34	123.71
4283	42.83	44.35	1.78	1.78	41.89	123.73
4284	42.84	45.21	1.78	1.78	41.26	123.80
4285	42.85	46.19	1.79	1.79	40.54	123.87
4286	42.86	47.24	1.79	1.79	39.80	123.94
4287	42.87	48.29	1.79	1.79	39.05	124.00
4288	42.88	49.31	1.79	1.79	38.35	124.05
4289	42.89	50.23	1.79	1.79	37.72	124.09
4290	42.90	51.01	1.79	1.79	37.20	124.13
4291	42.91	51.66	1.79	1.79	36.75	124.18
4292	42.92	52.47	1.81	1.81	36.31	124.26
4293	42.93	53.45	1.82	1.82	35.82	124.35
4294	42.94	54.53	1.83	1.83	35.29	124.46
4295	42.95	55.67	1.85	1.85	34.74	124.56
4296	42.96	56.80	1.86	1.86	34.21	124.65
4297	42.97	57.87	1.87	1.87	33.71	124.74
4298	42.98	58.81	1.88	1.88	33.28	124.81
4299	42.99	59.58	1.88	1.88	32.99	124.87
4300	43.00	59.88	1.89	1.89	32.84	124.93
4301	43.01	60.13	1.91	1.91	32.80	124.99
4302	43.02	60.43	1.92	1.92	32.77	125.06
4303	43.03	60.74	1.94	1.94	32.74	125.14
4304	43.04	61.07	1.96	1.96	32.71	125.22
4305	43.05	61.39	1.98	1.98	32.69	125.30
4306	43.06	61.68	1.99	1.99	32.66	125.37
4307	43.07	61.94	2.01	2.01	32.65	125.43
4308	43.08	62.11	2.02	2.02	32.70	125.49
4309	43.09	62.06	2.04	2.04	32.84	125.57
4310	43.10	61.99	2.07	2.07	33.06	125.66
4311	43.11	61.92	2.10	2.10	33.31	125.76
4312	43.12	61.83	2.13	2.13	33.58	125.87
4313	43.13	61.75	2.16	2.16	33.84	125.97
4314	43.14	61.68	2.19	2.19	34.09	126.07
4315	43.15	61.60	2.22	2.22	34.32	126.16
4316	43.16	61.54	2.25	2.25	34.52	126.24
4317	43.17	61.50	2.27	2.27	34.70	126.31
4318	43.18	61.44	2.29	2.29	34.90	126.38
4319	43.19	61.37	2.32	2.32	35.13	126.47
4320	43.20	61.29	2.35	2.35	35.38	126.57

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4321	43.21	61.21	2.38	2.38	35.64	126.67
4322	43.22	61.13	2.42	2.42	35.90	126.76
4323	43.23	61.05	2.45	2.45	36.14	126.85
4324	43.24	60.99	2.48	2.48	36.35	126.93
4325	43.25	60.93	2.50	2.50	36.49	126.98
4326	43.26	60.95	2.51	2.51	36.57	127.02
4327	43.27	60.99	2.51	2.51	36.59	127.03
4328	43.28	61.04	2.52	2.52	36.60	127.05
4329	43.29	61.09	2.52	2.52	36.61	127.07
4330	43.30	61.15	2.53	2.53	36.62	127.09
4331	43.31	61.20	2.53	2.53	36.64	127.11
4332	43.32	61.25	2.54	2.54	36.65	127.13
4333	43.33	61.29	2.54	2.54	36.65	127.14
4334	43.34	61.35	2.55	2.55	36.58	127.14
4335	43.35	61.64	2.54	2.54	36.41	127.13
4336	43.36	61.99	2.52	2.52	36.15	127.11
4337	43.37	62.39	2.51	2.51	35.85	127.08
4338	43.38	62.82	2.49	2.49	35.54	127.05
4339	43.39	63.25	2.47	2.47	35.22	127.02
4340	43.40	63.66	2.46	2.46	34.91	126.98
4341	43.41	64.03	2.44	2.44	34.63	126.95
4342	43.42	64.35	2.43	2.43	34.38	126.93
4343	43.43	64.73	2.42	2.42	34.10	126.91
4344	43.44	65.38	2.41	2.41	33.75	126.91
4345	43.45	66.16	2.40	2.40	33.32	126.90
4346	43.46	67.02	2.39	2.39	32.84	126.89
4347	43.47	67.92	2.37	2.37	32.35	126.88
4348	43.48	68.82	2.36	2.36	31.86	126.86
4349	43.49	69.66	2.34	2.34	31.41	126.84
4350	43.50	70.40	2.32	2.32	31.01	126.82
4351	43.51	71.01	2.31	2.31	30.68	126.80
4352	43.52	71.45	2.30	2.30	30.40	126.78
4353	43.53	71.99	2.29	2.29	30.11	126.76
4354	43.54	72.62	2.28	2.28	29.78	126.74
4355	43.55	73.30	2.26	2.26	29.42	126.71
4356	43.56	74.00	2.24	2.24	29.05	126.68
4357	43.57	74.68	2.23	2.23	28.70	126.65
4358	43.58	75.31	2.21	2.21	28.37	126.62
4359	43.59	75.85	2.20	2.20	28.10	126.59
4360	43.60	76.22	2.18	2.18	27.93	126.56
4361	43.61	76.21	2.18	2.18	27.85	126.55
4362	43.62	76.21	2.18	2.18	27.83	126.53
4363	43.63	76.21	2.17	2.17	27.80	126.52
4364	43.64	76.21	2.17	2.17	27.78	126.50
4365	43.65	76.21	2.16	2.16	27.75	126.48
4366	43.66	76.21	2.16	2.16	27.72	126.46
4367	43.67	76.20	2.15	2.15	27.70	126.45
4368	43.68	76.20	2.15	2.15	27.72	126.44

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4369	43.69	75.97	2.15	2.15	27.86	126.45
4370	43.70	75.42	2.17	2.17	28.12	126.48
4371	43.71	74.76	2.19	2.19	28.48	126.52
4372	43.72	74.02	2.21	2.21	28.88	126.56
4373	43.73	73.26	2.23	2.23	29.29	126.60
4374	43.74	72.50	2.25	2.25	29.70	126.64
4375	43.75	71.79	2.26	2.26	30.09	126.67
4376	43.76	71.16	2.28	2.28	30.44	126.69
4377	43.77	70.65	2.29	2.29	30.80	126.72
4378	43.78	69.87	2.31	2.31	31.26	126.76
4379	43.79	68.81	2.34	2.34	31.86	126.80
4380	43.80	67.58	2.36	2.36	32.58	126.84
4381	43.81	66.25	2.39	2.39	33.35	126.88
4382	43.82	64.89	2.42	2.42	34.16	126.90
4383	43.83	63.56	2.44	2.44	34.95	126.92
4384	43.84	62.34	2.45	2.45	35.68	126.92
4385	43.85	61.28	2.47	2.47	36.32	126.92
4386	43.86	60.47	2.48	2.48	36.89	126.92
4387	43.87	59.68	2.50	2.50	37.48	126.94
4388	43.88	58.71	2.51	2.51	38.15	126.95
4389	43.89	57.61	2.53	2.53	38.92	126.96
4390	43.90	56.45	2.55	2.55	39.74	126.96
4391	43.91	55.27	2.57	2.57	40.58	126.96
4392	43.92	54.15	2.58	2.58	41.39	126.94
4393	43.93	53.14	2.59	2.59	42.13	126.92
4394	43.94	52.29	2.59	2.59	42.73	126.91
4395	43.95	51.81	2.60	2.60	43.22	126.92
4396	43.96	51.45	2.63	2.63	43.66	126.95
4397	43.97	51.03	2.65	2.65	44.14	127.00
4398	43.98	50.56	2.68	2.68	44.67	127.05
4399	43.99	50.07	2.71	2.71	45.22	127.10
4400	44.00	49.59	2.73	2.73	45.76	127.14
4401	44.01	49.14	2.75	2.75	46.27	127.18
4402	44.02	48.74	2.77	2.77	46.72	127.22
4403	44.03	48.41	2.79	2.79	47.04	127.26
4404	44.04	48.47	2.81	2.81	47.23	127.31
4405	44.05	48.59	2.84	2.84	47.34	127.39
4406	44.06	48.74	2.88	2.88	47.46	127.49
4407	44.07	48.90	2.92	2.92	47.58	127.59
4408	44.08	49.06	2.96	2.96	47.71	127.70
4409	44.09	49.22	2.99	2.99	47.83	127.80
4410	44.10	49.37	3.03	3.03	47.94	127.89
4411	44.11	49.49	3.06	3.06	48.01	127.97
4412	44.12	49.65	3.08	3.08	47.98	128.04
4413	44.13	50.09	3.10	3.10	47.83	128.11
4414	44.14	50.63	3.13	3.13	47.57	128.20
4415	44.15	51.24	3.16	3.16	47.28	128.29
4416	44.16	51.88	3.19	3.19	46.97	128.39

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4417	44.17	52.53	3.22	3.22	46.67	128.48
4418	44.18	53.15	3.24	3.24	46.38	128.57
4419	44.19	53.71	3.27	3.27	46.13	128.65
4420	44.20	54.18	3.29	3.29	45.85	128.73
4421	44.21	54.84	3.31	3.31	45.46	128.81
4422	44.22	55.95	3.33	3.33	44.89	128.91
4423	44.23	57.26	3.36	3.36	44.18	129.02
4424	44.24	58.70	3.39	3.39	43.41	129.14
4425	44.25	60.20	3.41	3.41	42.63	129.25
4426	44.26	61.68	3.44	3.44	41.88	129.36
4427	44.27	63.08	3.46	3.46	41.18	129.45
4428	44.28	64.30	3.47	3.47	40.59	129.52
4429	44.29	65.29	3.48	3.48	40.02	129.59
4430	44.30	66.52	3.49	3.49	39.41	129.66
4431	44.31	68.11	3.50	3.50	38.67	129.74
4432	44.32	69.95	3.51	3.51	37.83	129.82
4433	44.33	71.94	3.52	3.52	36.94	129.90
4434	44.34	73.97	3.52	3.52	36.04	129.97
4435	44.35	75.94	3.51	3.51	35.18	130.02
4436	44.36	77.76	3.50	3.50	34.40	130.06
4437	44.37	79.32	3.49	3.49	33.75	130.09
4438	44.38	80.52	3.48	3.48	33.20	130.12
4439	44.39	81.76	3.48	3.48	32.68	130.14
4440	44.40	83.29	3.48	3.48	32.11	130.18
4441	44.41	85.01	3.47	3.47	31.47	130.21
4442	44.42	86.83	3.46	3.46	30.80	130.23
4443	44.43	88.66	3.44	3.44	30.13	130.25
4444	44.44	90.40	3.42	3.42	29.50	130.26
4445	44.45	91.97	3.40	3.40	28.94	130.26
4446	44.46	93.28	3.38	3.38	28.48	130.25
4447	44.47	94.23	3.37	3.37	28.09	130.25
4448	44.48	95.30	3.36	3.36	27.71	130.25
4449	44.49	96.57	3.34	3.34	27.29	130.24
4450	44.50	97.96	3.32	3.32	26.83	130.23
4451	44.51	99.41	3.30	3.30	26.35	130.21
4452	44.52	100.84	3.27	3.27	25.87	130.19
4453	44.53	102.18	3.24	3.24	25.43	130.17
4454	44.54	103.36	3.22	3.22	25.05	130.14
4455	44.55	104.31	3.20	3.20	24.77	130.12
4456	44.56	104.60	3.19	3.19	24.58	130.09
4457	44.57	104.91	3.17	3.17	24.43	130.06
4458	44.58	105.26	3.15	3.15	24.27	130.02
4459	44.59	105.64	3.12	3.12	24.09	129.97
4460	44.60	106.03	3.10	3.10	23.91	129.93
4461	44.61	106.41	3.08	3.08	23.73	129.89
4462	44.62	106.76	3.06	3.06	23.57	129.84
4463	44.63	107.06	3.04	3.04	23.43	129.81
4464	44.64	107.35	3.03	3.03	23.29	129.79

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4465	44.65	107.86	3.02	3.02	23.15	129.78
4466	44.66	108.49	3.01	3.01	22.98	129.77
4467	44.67	109.20	3.00	3.00	22.79	129.76
4468	44.68	109.95	2.99	2.99	22.58	129.75
4469	44.69	110.70	2.98	2.98	22.38	129.74
4470	44.70	111.41	2.97	2.97	22.18	129.73
4471	44.71	112.05	2.96	2.96	22.01	129.72
4472	44.72	112.59	2.95	2.95	21.86	129.71
4473	44.73	113.03	2.94	2.94	21.72	129.70
4474	44.74	113.59	2.93	2.93	21.57	129.69
4475	44.75	114.24	2.92	2.92	21.39	129.67
4476	44.76	114.96	2.91	2.91	21.19	129.66
4477	44.77	115.71	2.89	2.89	20.99	129.64
4478	44.78	116.45	2.88	2.88	20.79	129.62
4479	44.79	117.14	2.87	2.87	20.61	129.60
4480	44.80	117.75	2.85	2.85	20.44	129.58
4481	44.81	118.23	2.84	2.84	20.35	129.56
4482	44.82	118.02	2.84	2.84	20.34	129.55
4483	44.83	117.70	2.84	2.84	20.39	129.54
4484	44.84	117.33	2.84	2.84	20.46	129.52
4485	44.85	116.93	2.84	2.84	20.53	129.51
4486	44.86	116.52	2.83	2.83	20.60	129.50
4487	44.87	116.12	2.83	2.83	20.67	129.48
4488	44.88	115.76	2.83	2.83	20.73	129.47
4489	44.89	115.45	2.83	2.83	20.79	129.46
4490	44.90	115.21	2.83	2.83	20.85	129.45
4491	44.91	114.93	2.83	2.83	20.92	129.45
4492	44.92	114.59	2.83	2.83	21.00	129.46
4493	44.93	114.21	2.84	2.84	21.10	129.46
4494	44.94	113.80	2.84	2.84	21.20	129.46
4495	44.95	113.40	2.85	2.85	21.30	129.46
4496	44.96	113.01	2.85	2.85	21.40	129.46
4497	44.97	112.66	2.85	2.85	21.49	129.47
4498	44.98	112.38	2.86	2.86	21.57	129.47
4499	44.99	112.17	2.86	2.86	21.65	129.48
4500	45.00	111.92	2.88	2.88	21.75	129.51
4501	45.01	111.64	2.89	2.89	21.87	129.54
4502	45.02	111.32	2.91	2.91	22.01	129.57
4503	45.03	111.00	2.92	2.92	22.14	129.60
4504	45.04	110.68	2.94	2.94	22.28	129.64
4505	45.05	110.38	2.95	2.95	22.40	129.66
4506	45.06	110.11	2.96	2.96	22.51	129.69
4507	45.07	109.90	2.98	2.98	22.61	129.71
4508	45.08	109.70	2.99	2.99	22.72	129.74
4509	45.09	109.44	3.00	3.00	22.84	129.77
4510	45.10	109.14	3.02	3.02	22.97	129.80
4511	45.11	108.82	3.04	3.04	23.12	129.84
4512	45.12	108.50	3.06	3.06	23.27	129.88

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4513	45.13	108.18	3.07	3.07	23.41	129.91
4514	45.14	107.89	3.09	3.09	23.54	129.94
4515	45.15	107.65	3.10	3.10	23.66	129.97
4516	45.16	107.43	3.11	3.11	23.78	129.99
4517	45.17	107.09	3.13	3.13	23.91	130.02
4518	45.18	106.68	3.15	3.15	24.07	130.05
4519	45.19	106.22	3.16	3.16	24.26	130.08
4520	45.20	105.73	3.18	3.18	24.45	130.11
4521	45.21	105.24	3.20	3.20	24.64	130.14
4522	45.22	104.78	3.22	3.22	24.83	130.17
4523	45.23	104.37	3.23	3.23	24.99	130.20
4524	45.24	104.03	3.25	3.25	25.13	130.22
4525	45.25	103.74	3.26	3.26	25.27	130.24
4526	45.26	103.37	3.27	3.27	25.43	130.26
4527	45.27	102.94	3.29	3.29	25.61	130.29
4528	45.28	102.47	3.31	3.31	25.81	130.33
4529	45.29	101.98	3.33	3.33	26.01	130.36
4530	45.30	101.50	3.35	3.35	26.21	130.39
4531	45.31	101.05	3.37	3.37	26.40	130.41
4532	45.32	100.66	3.38	3.38	26.57	130.44
4533	45.33	100.35	3.40	3.40	26.69	130.45
4534	45.34	100.14	3.40	3.40	26.79	130.46
4535	45.35	99.88	3.40	3.40	26.88	130.46
4536	45.36	99.58	3.41	3.41	26.98	130.46
4537	45.37	99.26	3.41	3.41	27.09	130.47
4538	45.38	98.93	3.42	3.42	27.19	130.47
4539	45.39	98.62	3.42	3.42	27.30	130.47
4540	45.40	98.33	3.42	3.42	27.40	130.47
4541	45.41	98.09	3.43	3.43	27.47	130.47
4542	45.42	97.98	3.43	3.43	27.47	130.46
4543	45.43	98.10	3.41	3.41	27.42	130.44
4544	45.44	98.23	3.40	3.40	27.32	130.41
4545	45.45	98.39	3.38	3.38	27.21	130.37
4546	45.46	98.55	3.36	3.36	27.09	130.33
4547	45.47	98.71	3.34	3.34	26.97	130.29
4548	45.48	98.86	3.32	3.32	26.86	130.26
4549	45.49	99.00	3.30	3.30	26.75	130.23
4550	45.50	99.12	3.29	3.29	26.64	130.20
4551	45.51	99.44	3.28	3.28	26.49	130.17
4552	45.52	99.99	3.26	3.26	26.27	130.14
4553	45.53	100.64	3.23	3.23	26.01	130.10
4554	45.54	101.35	3.20	3.20	25.72	130.06
4555	45.55	102.08	3.18	3.18	25.42	130.01
4556	45.56	102.80	3.15	3.15	25.12	129.96
4557	45.57	103.47	3.12	3.12	24.85	129.91
4558	45.58	104.06	3.09	3.09	24.61	129.87
4559	45.59	104.53	3.07	3.07	24.39	129.83
4560	45.60	105.10	3.06	3.06	24.18	129.80

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4561	45.61	105.81	3.04	3.04	23.93	129.77
4562	45.62	106.64	3.02	3.02	23.65	129.74
4563	45.63	107.52	2.99	2.99	23.34	129.69
4564	45.64	108.41	2.96	2.96	23.03	129.65
4565	45.65	109.28	2.94	2.94	22.73	129.60
4566	45.66	110.07	2.91	2.91	22.46	129.56
4567	45.67	110.74	2.89	2.89	22.24	129.52
4568	45.68	111.22	2.88	2.88	22.06	129.49
4569	45.69	111.68	2.86	2.86	21.90	129.47
4570	45.70	112.23	2.85	2.85	21.73	129.45
4571	45.71	112.84	2.84	2.84	21.54	129.43
4572	45.72	113.49	2.82	2.82	21.35	129.40
4573	45.73	114.14	2.80	2.80	21.15	129.37
4574	45.74	114.75	2.79	2.79	20.97	129.34
4575	45.75	115.30	2.77	2.77	20.80	129.32
4576	45.76	115.75	2.76	2.76	20.67	129.30
4577	45.77	116.01	2.76	2.76	20.58	129.28
4578	45.78	116.25	2.75	2.75	20.50	129.27
4579	45.79	116.54	2.74	2.74	20.42	129.26
4580	45.80	116.86	2.74	2.74	20.34	129.25
4581	45.81	117.18	2.73	2.73	20.25	129.24
4582	45.82	117.50	2.72	2.72	20.16	129.23
4583	45.83	117.80	2.72	2.72	20.08	129.21
4584	45.84	118.06	2.71	2.71	20.00	129.20
4585	45.85	118.27	2.70	2.70	19.93	129.19
4586	45.86	118.63	2.70	2.70	19.84	129.18
4587	45.87	119.09	2.69	2.69	19.72	129.17
4588	45.88	119.62	2.68	2.68	19.59	129.16
4589	45.89	120.18	2.67	2.67	19.45	129.14
4590	45.90	120.75	2.66	2.66	19.31	129.13
4591	45.91	121.30	2.65	2.65	19.17	129.11
4592	45.92	121.80	2.64	2.64	19.04	129.09
4593	45.93	122.22	2.63	2.63	18.93	129.08
4594	45.94	122.63	2.63	2.63	18.82	129.07
4595	45.95	123.26	2.62	2.62	18.69	129.07
4596	45.96	124.02	2.61	2.61	18.53	129.06
4597	45.97	124.87	2.61	2.61	18.35	129.05
4598	45.98	125.76	2.60	2.60	18.16	129.04
4599	45.99	126.65	2.59	2.59	17.98	129.03
4600	46.00	127.49	2.58	2.58	17.81	129.02
4601	46.01	128.25	2.57	2.57	17.65	129.01
4602	46.02	128.86	2.56	2.56	17.51	129.00
4603	46.03	129.40	2.55	2.55	17.38	128.99
4604	46.04	130.08	2.54	2.54	17.23	128.97
4605	46.05	130.87	2.53	2.53	17.05	128.94
4606	46.06	131.74	2.51	2.51	16.86	128.91
4607	46.07	132.64	2.49	2.49	16.66	128.88
4608	46.08	133.52	2.48	2.48	16.46	128.85

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4609	46.09	134.33	2.46	2.46	16.28	128.82
4610	46.10	135.04	2.45	2.45	16.12	128.79
4611	46.11	135.60	2.44	2.44	16.07	128.82
4612	46.12	136.07	2.48	2.48	16.11	128.92
4613	46.13	136.67	2.54	2.54	16.24	129.09
4614	46.14	137.34	2.60	2.60	16.39	129.29
4615	46.15	138.06	2.67	2.67	16.55	129.49
4616	46.16	138.80	2.75	2.75	16.71	129.69
4617	46.17	139.50	2.82	2.82	16.86	129.89
4618	46.18	140.14	2.88	2.88	16.99	130.06
4619	46.19	140.69	2.93	2.93	17.11	130.20
4620	46.20	141.09	2.98	2.98	17.23	130.34
4621	46.21	141.49	3.03	3.03	17.36	130.48
4622	46.22	141.97	3.10	3.10	17.51	130.64
4623	46.23	142.51	3.17	3.17	17.68	130.82
4624	46.24	143.08	3.25	3.25	17.86	131.01
4625	46.25	143.65	3.33	3.33	18.03	131.19
4626	46.26	144.18	3.41	3.41	18.19	131.36
4627	46.27	144.66	3.47	3.47	18.33	131.50
4628	46.28	145.05	3.53	3.53	18.41	131.59
4629	46.29	145.10	3.51	3.51	18.39	131.59
4630	46.30	145.04	3.47	3.47	18.28	131.51
4631	46.31	144.97	3.42	3.42	18.13	131.40
4632	46.32	144.89	3.36	3.36	17.97	131.28
4633	46.33	144.81	3.31	3.31	17.80	131.16
4634	46.34	144.73	3.25	3.25	17.63	131.03
4635	46.35	144.65	3.20	3.20	17.48	130.92
4636	46.36	144.59	3.15	3.15	17.35	130.82
4637	46.37	144.51	3.12	3.12	17.29	130.75
4638	46.38	143.98	3.12	3.12	17.30	130.71
4639	46.39	143.32	3.11	3.11	17.38	130.68
4640	46.40	142.56	3.10	3.10	17.47	130.66
4641	46.41	141.76	3.10	3.10	17.56	130.63
4642	46.42	140.95	3.09	3.09	17.66	130.60
4643	46.43	140.17	3.08	3.08	17.75	130.57
4644	46.44	139.45	3.08	3.08	17.84	130.54
4645	46.45	138.85	3.07	3.07	17.92	130.52
4646	46.46	138.25	3.07	3.07	18.05	130.51
4647	46.47	137.33	3.09	3.09	18.22	130.52
4648	46.48	136.21	3.10	3.10	18.45	130.54
4649	46.49	134.97	3.12	3.12	18.70	130.56
4650	46.50	133.68	3.14	3.14	18.97	130.57
4651	46.51	132.38	3.15	3.15	19.24	130.58
4652	46.52	131.16	3.16	3.16	19.49	130.59
4653	46.53	130.08	3.18	3.18	19.72	130.60
4654	46.54	129.19	3.19	3.19	19.93	130.60
4655	46.55	128.12	3.19	3.19	20.14	130.58
4656	46.56	126.66	3.18	3.18	20.39	130.55

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4657	46.57	124.95	3.18	3.18	20.69	130.51
4658	46.58	123.09	3.18	3.18	21.01	130.47
4659	46.59	121.18	3.17	3.17	21.36	130.41
4660	46.60	119.30	3.16	3.16	21.69	130.36
4661	46.61	117.57	3.15	3.15	22.01	130.31
4662	46.62	116.06	3.15	3.15	22.29	130.26
4663	46.63	114.87	3.14	3.14	22.58	130.24
4664	46.64	113.63	3.16	3.16	22.91	130.23
4665	46.65	112.09	3.18	3.18	23.33	130.25
4666	46.66	110.33	3.20	3.20	23.80	130.26
4667	46.67	108.46	3.22	3.22	24.32	130.27
4668	46.68	106.56	3.24	3.24	24.84	130.27
4669	46.69	104.74	3.26	3.26	25.35	130.26
4670	46.70	103.08	3.27	3.27	25.81	130.25
4671	46.71	101.69	3.28	3.28	26.22	130.24
4672	46.72	100.59	3.29	3.29	26.62	130.24
4673	46.73	99.30	3.32	3.32	27.07	130.26
4674	46.74	97.75	3.35	3.35	27.61	130.28
4675	46.75	96.03	3.37	3.37	28.22	130.30
4676	46.76	94.23	3.40	3.40	28.86	130.31
4677	46.77	92.43	3.42	3.42	29.50	130.31
4678	46.78	90.74	3.44	3.44	30.11	130.31
4679	46.79	89.24	3.46	3.46	30.65	130.30
4680	46.80	88.01	3.46	3.46	31.12	130.29
4681	46.81	87.03	3.48	3.48	31.56	130.28
4682	46.82	85.81	3.49	3.49	32.05	130.27
4683	46.83	84.38	3.50	3.50	32.61	130.26
4684	46.84	82.83	3.51	3.51	33.23	130.24
4685	46.85	81.24	3.52	3.52	33.88	130.21
4686	46.86	79.69	3.53	3.53	34.51	130.18
4687	46.87	78.25	3.53	3.53	35.11	130.14
4688	46.88	77.00	3.53	3.53	35.62	130.11
4689	46.89	76.03	3.53	3.53	36.05	130.06
4690	46.90	75.04	3.51	3.51	36.44	129.99
4691	46.91	73.81	3.48	3.48	36.86	129.89
4692	46.92	72.41	3.45	3.45	37.34	129.78
4693	46.93	70.92	3.41	3.41	37.87	129.65
4694	46.94	69.42	3.38	3.38	38.41	129.52
4695	46.95	67.98	3.34	3.34	38.94	129.39
4696	46.96	66.67	3.30	3.30	39.43	129.27
4697	46.97	65.56	3.27	3.27	39.84	129.16
4698	46.98	64.77	3.24	3.24	40.16	129.05
4699	46.99	63.94	3.20	3.20	40.44	128.93
4700	47.00	62.95	3.16	3.16	40.74	128.78
4701	47.01	61.85	3.10	3.10	41.08	128.62
4702	47.02	60.70	3.05	3.05	41.44	128.44
4703	47.03	59.56	2.99	2.99	41.82	128.26
4704	47.04	58.48	2.94	2.94	42.17	128.09

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4705	47.05	57.52	2.89	2.89	42.50	127.94
4706	47.06	56.75	2.86	2.86	42.74	127.83
4707	47.07	56.51	2.85	2.85	42.90	127.77
4708	47.08	56.33	2.84	2.84	43.01	127.75
4709	47.09	56.13	2.84	2.84	43.11	127.73
4710	47.10	55.91	2.83	2.83	43.23	127.71
4711	47.11	55.68	2.83	2.83	43.35	127.68
4712	47.12	55.45	2.82	2.82	43.47	127.66
4713	47.13	55.25	2.82	2.82	43.58	127.64
4714	47.14	55.07	2.81	2.81	43.67	127.62
4715	47.15	54.97	2.81	2.81	43.71	127.63
4716	47.16	55.19	2.83	2.83	43.70	127.66
4717	47.17	55.46	2.85	2.85	43.64	127.72
4718	47.18	55.76	2.87	2.87	43.58	127.79
4719	47.19	56.08	2.89	2.89	43.52	127.86
4720	47.20	56.41	2.92	2.92	43.45	127.94
4721	47.21	56.72	2.94	2.94	43.39	128.01
4722	47.22	57.00	2.96	2.96	43.33	128.07
4723	47.23	57.24	2.98	2.98	43.27	128.12
4724	47.24	57.50	2.99	2.99	43.14	128.16
4725	47.25	57.90	2.99	2.99	42.95	128.20
4726	47.26	58.38	3.00	3.00	42.69	128.23
4727	47.27	58.92	3.01	3.01	42.41	128.27
4728	47.28	59.47	3.02	3.02	42.11	128.31
4729	47.29	60.02	3.02	3.02	41.82	128.35
4730	47.30	60.54	3.03	3.03	41.55	128.39
4731	47.31	61.01	3.03	3.03	41.32	128.42
4732	47.32	61.38	3.04	3.04	41.10	128.44
4733	47.33	61.71	3.03	3.03	40.86	128.45
4734	47.34	62.13	3.02	3.02	40.57	128.44
4735	47.35	62.62	3.01	3.01	40.23	128.43
4736	47.36	63.15	3.00	3.00	39.86	128.42
4737	47.37	63.69	2.98	2.98	39.48	128.40
4738	47.38	64.22	2.97	2.97	39.11	128.38
4739	47.39	64.71	2.95	2.95	38.78	128.37
4740	47.40	65.13	2.94	2.94	38.48	128.35
4741	47.41	65.47	2.93	2.93	38.21	128.33
4742	47.42	65.86	2.91	2.91	37.92	128.31
4743	47.43	66.34	2.90	2.90	37.58	128.28
4744	47.44	66.88	2.87	2.87	37.18	128.25
4745	47.45	67.45	2.85	2.85	36.77	128.21
4746	47.46	68.03	2.82	2.82	36.35	128.16
4747	47.47	68.59	2.80	2.80	35.95	128.12
4748	47.48	69.09	2.78	2.78	35.58	128.08
4749	47.49	69.51	2.76	2.76	35.29	128.04
4750	47.50	69.71	2.74	2.74	35.06	127.98
4751	47.51	69.79	2.71	2.71	34.85	127.92
4752	47.52	69.89	2.68	2.68	34.62	127.83

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4753	47.53	69.99	2.64	2.64	34.37	127.74
4754	47.54	70.10	2.60	2.60	34.10	127.64
4755	47.55	70.21	2.56	2.56	33.84	127.53
4756	47.56	70.31	2.53	2.53	33.59	127.44
4757	47.57	70.40	2.50	2.50	33.36	127.35
4758	47.58	70.47	2.47	2.47	33.19	127.27
4759	47.59	70.39	2.45	2.45	33.06	127.19
4760	47.60	70.27	2.42	2.42	32.95	127.11
4761	47.61	70.12	2.39	2.39	32.82	127.00
4762	47.62	69.96	2.35	2.35	32.67	126.89
4763	47.63	69.80	2.32	2.32	32.52	126.77
4764	47.64	69.64	2.28	2.28	32.38	126.66
4765	47.65	69.49	2.25	2.25	32.24	126.55
4766	47.66	69.37	2.22	2.22	32.12	126.46
4767	47.67	69.36	2.20	2.20	31.98	126.42
4768	47.68	69.85	2.20	2.20	31.78	126.42
4769	47.69	70.46	2.21	2.21	31.54	126.44
4770	47.70	71.14	2.21	2.21	31.26	126.47
4771	47.71	71.87	2.21	2.21	30.96	126.49
4772	47.72	72.60	2.21	2.21	30.67	126.52
4773	47.73	73.30	2.21	2.21	30.39	126.54
4774	47.74	73.93	2.21	2.21	30.14	126.56
4775	47.75	74.46	2.21	2.21	29.94	126.57
4776	47.76	74.70	2.20	2.20	29.79	126.56
4777	47.77	74.79	2.19	2.19	29.66	126.53
4778	47.78	74.89	2.17	2.17	29.53	126.48
4779	47.79	75.01	2.16	2.16	29.38	126.42
4780	47.80	75.13	2.14	2.14	29.23	126.37
4781	47.81	75.25	2.12	2.12	29.07	126.31
4782	47.82	75.37	2.10	2.10	28.93	126.26
4783	47.83	75.47	2.09	2.09	28.80	126.21
4784	47.84	75.55	2.08	2.08	28.74	126.16
4785	47.85	75.17	2.06	2.06	28.76	126.10
4786	47.86	74.62	2.05	2.05	28.85	126.02
4787	47.87	73.98	2.03	2.03	28.97	125.93
4788	47.88	73.29	2.00	2.00	29.09	125.83
4789	47.89	72.59	1.98	1.98	29.23	125.73
4790	47.90	71.90	1.96	1.96	29.36	125.63
4791	47.91	71.27	1.94	1.94	29.48	125.53
4792	47.92	70.72	1.92	1.92	29.59	125.46
4793	47.93	70.33	1.91	1.91	29.74	125.43
4794	47.94	70.06	1.93	1.93	29.93	125.44
4795	47.95	69.73	1.95	1.95	30.19	125.49
4796	47.96	69.35	1.96	1.96	30.48	125.55
4797	47.97	68.95	1.98	1.98	30.78	125.61
4798	47.98	68.55	2.00	2.00	31.09	125.66
4799	47.99	68.17	2.02	2.02	31.38	125.71
4800	48.00	67.83	2.03	2.03	31.64	125.75

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4801	48.01	67.54	2.05	2.05	31.89	125.79
4802	48.02	67.20	2.06	2.06	32.18	125.83
4803	48.03	66.67	2.08	2.08	32.55	125.88
4804	48.04	66.03	2.10	2.10	32.99	125.93
4805	48.05	65.34	2.13	2.13	33.49	125.99
4806	48.06	64.61	2.15	2.15	34.00	126.04
4807	48.07	63.90	2.17	2.17	34.51	126.08
4808	48.08	63.23	2.19	2.19	34.99	126.12
4809	48.09	62.63	2.21	2.21	35.41	126.16
4810	48.10	62.16	2.22	2.22	35.76	126.18
4811	48.11	61.77	2.23	2.23	36.08	126.20
4812	48.12	61.29	2.24	2.24	36.41	126.21
4813	48.13	60.73	2.25	2.25	36.79	126.22
4814	48.14	60.12	2.26	2.26	37.21	126.23
4815	48.15	59.51	2.27	2.27	37.63	126.24
4816	48.16	58.91	2.28	2.28	38.04	126.24
4817	48.17	58.36	2.29	2.29	38.43	126.25
4818	48.18	57.88	2.29	2.29	38.74	126.25
4819	48.19	57.56	2.30	2.30	38.92	126.23
4820	48.20	57.41	2.28	2.28	38.99	126.19
4821	48.21	57.22	2.27	2.27	38.99	126.13
4822	48.22	57.01	2.25	2.25	38.99	126.06
4823	48.23	56.79	2.23	2.23	38.99	125.99
4824	48.24	56.57	2.21	2.21	38.99	125.91
4825	48.25	56.35	2.19	2.19	38.99	125.84
4826	48.26	56.16	2.17	2.17	38.99	125.78
4827	48.27	56.00	2.16	2.16	38.93	125.72
4828	48.28	56.09	2.14	2.14	38.75	125.66
4829	48.29	56.41	2.12	2.12	38.41	125.59
4830	48.30	56.78	2.09	2.09	37.96	125.51
4831	48.31	57.19	2.05	2.05	37.46	125.41
4832	48.32	57.62	2.02	2.02	36.94	125.30
4833	48.33	58.04	1.98	1.98	36.42	125.18
4834	48.34	58.43	1.95	1.95	35.94	125.07
4835	48.35	58.78	1.92	1.92	35.51	124.97
4836	48.36	59.06	1.89	1.89	35.11	124.90
4837	48.37	59.56	1.88	1.88	34.70	124.85
4838	48.38	60.22	1.86	1.86	34.22	124.80
4839	48.39	60.97	1.84	1.84	33.67	124.75
4840	48.40	61.79	1.82	1.82	33.07	124.69
4841	48.41	62.62	1.79	1.79	32.46	124.62
4842	48.42	63.43	1.76	1.76	31.87	124.55
4843	48.43	64.17	1.74	1.74	31.32	124.48
4844	48.44	64.81	1.72	1.72	30.87	124.41
4845	48.45	65.30	1.70	1.70	30.51	124.38
4846	48.46	65.82	1.70	1.70	30.20	124.37
4847	48.47	66.46	1.70	1.70	29.88	124.37
4848	48.48	67.18	1.69	1.69	29.53	124.37

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4849	48.49	67.94	1.68	1.68	29.15	124.37
4850	48.50	68.71	1.68	1.68	28.78	124.36
4851	48.51	69.43	1.67	1.67	28.43	124.36
4852	48.52	70.09	1.66	1.66	28.11	124.35
4853	48.53	70.63	1.65	1.65	27.89	124.35
4854	48.54	70.90	1.66	1.66	27.77	124.37
4855	48.55	71.09	1.67	1.67	27.74	124.41
4856	48.56	71.31	1.68	1.68	27.74	124.47
4857	48.57	71.55	1.69	1.69	27.74	124.53
4858	48.58	71.81	1.70	1.70	27.74	124.59
4859	48.59	72.06	1.72	1.72	27.74	124.65
4860	48.60	72.29	1.73	1.73	27.74	124.71
4861	48.61	72.50	1.74	1.74	27.74	124.76
4862	48.62	72.66	1.75	1.75	27.85	124.83
4863	48.63	72.41	1.78	1.78	28.11	124.94
4864	48.64	72.06	1.82	1.82	28.54	125.10
4865	48.65	71.66	1.87	1.87	29.04	125.27
4866	48.66	71.23	1.92	1.92	29.57	125.45
4867	48.67	70.79	1.97	1.97	30.11	125.63
4868	48.68	70.37	2.02	2.02	30.62	125.79
4869	48.69	69.98	2.06	2.06	31.09	125.93
4870	48.70	69.65	2.10	2.10	31.50	126.06
4871	48.71	69.36	2.14	2.14	31.96	126.20
4872	48.72	68.97	2.20	2.20	32.52	126.38
4873	48.73	68.49	2.27	2.27	33.21	126.60
4874	48.74	67.96	2.36	2.36	33.98	126.84
4875	48.75	67.39	2.44	2.44	34.78	127.07
4876	48.76	66.82	2.52	2.52	35.57	127.29
4877	48.77	66.28	2.60	2.60	36.31	127.49
4878	48.78	65.80	2.67	2.67	36.96	127.66
4879	48.79	65.40	2.73	2.73	37.51	127.79
4880	48.80	65.05	2.77	2.77	38.01	127.90
4881	48.81	64.61	2.81	2.81	38.52	128.01
4882	48.82	64.09	2.86	2.86	39.10	128.12
4883	48.83	63.52	2.92	2.92	39.74	128.24
4884	48.84	62.92	2.98	2.98	40.40	128.35
4885	48.85	62.34	3.03	3.03	41.05	128.46
4886	48.86	61.79	3.08	3.08	41.65	128.56
4887	48.87	61.32	3.12	3.12	42.17	128.64
4888	48.88	60.93	3.16	3.16	42.51	128.69
4889	48.89	60.92	3.17	3.17	42.70	128.73
4890	48.90	60.92	3.18	3.18	42.78	128.76
4891	48.91	60.92	3.19	3.19	42.86	128.79
4892	48.92	60.92	3.21	3.21	42.94	128.82
4893	48.93	60.92	3.22	3.22	43.03	128.86
4894	48.94	60.92	3.24	3.24	43.12	128.89
4895	48.95	60.92	3.25	3.25	43.19	128.92
4896	48.96	60.92	3.26	3.26	43.21	128.95

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4897	48.97	61.19	3.27	3.27	43.03	129.00
4898	48.98	62.26	3.30	3.30	42.60	129.08
4899	48.99	63.56	3.32	3.32	41.99	129.18
4900	49.00	65.02	3.35	3.35	41.31	129.29
4901	49.01	66.55	3.37	3.37	40.60	129.40
4902	49.02	68.09	3.39	3.39	39.91	129.50
4903	49.03	69.56	3.41	3.41	39.27	129.59
4904	49.04	70.87	3.42	3.42	38.70	129.67
4905	49.05	71.95	3.44	3.44	38.17	129.74
4906	49.06	73.25	3.45	3.45	37.58	129.82
4907	49.07	75.14	3.47	3.47	36.85	129.92
4908	49.08	77.36	3.49	3.49	35.99	130.03
4909	49.09	79.80	3.51	3.51	35.07	130.14
4910	49.10	82.32	3.52	3.52	34.14	130.24
4911	49.11	84.80	3.53	3.53	33.24	130.32
4912	49.12	87.12	3.53	3.53	32.41	130.39
4913	49.13	89.15	3.52	3.52	31.71	130.43
4914	49.14	90.76	3.52	3.52	31.09	130.49
4915	49.15	92.76	3.53	3.53	30.46	130.56
4916	49.16	95.28	3.55	3.55	29.74	130.65
4917	49.17	98.18	3.56	3.56	28.94	130.75
4918	49.18	101.28	3.57	3.57	28.10	130.84
4919	49.19	104.44	3.57	3.57	27.26	130.91
4920	49.20	107.49	3.56	3.56	26.47	130.97
4921	49.21	110.29	3.55	3.55	25.75	131.01
4922	49.22	112.67	3.54	3.54	25.16	131.04
4923	49.23	114.52	3.53	3.53	24.67	131.08
4924	49.24	116.61	3.54	3.54	24.21	131.14
4925	49.25	119.16	3.56	3.56	23.72	131.22
4926	49.26	122.00	3.57	3.57	23.17	131.29
4927	49.27	125.00	3.57	3.57	22.60	131.36
4928	49.28	127.99	3.58	3.58	22.05	131.43
4929	49.29	130.84	3.58	3.58	21.53	131.48
4930	49.30	133.38	3.57	3.57	21.07	131.52
4931	49.31	135.48	3.57	3.57	20.73	131.55
4932	49.32	136.79	3.58	3.58	20.48	131.60
4933	49.33	138.15	3.59	3.59	20.30	131.66
4934	49.34	139.74	3.61	3.61	20.11	131.72
4935	49.35	141.49	3.64	3.64	19.90	131.80
4936	49.36	143.30	3.66	3.66	19.69	131.88
4937	49.37	145.07	3.68	3.68	19.49	131.95
4938	49.38	146.73	3.70	3.70	19.30	132.01
4939	49.39	148.18	3.72	3.72	19.14	132.07
4940	49.40	149.32	3.73	3.73	19.04	132.13
4941	49.41	150.05	3.76	3.76	18.98	132.19
4942	49.42	150.96	3.79	3.79	18.95	132.27
4943	49.43	152.01	3.83	3.83	18.92	132.36
4944	49.44	153.13	3.88	3.88	18.89	132.46

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4945	49.45	154.27	3.92	3.92	18.85	132.56
4946	49.46	155.37	3.96	3.96	18.82	132.65
4947	49.47	156.38	4.00	4.00	18.79	132.74
4948	49.48	157.23	4.04	4.04	18.76	132.80
4949	49.49	157.74	4.04	4.04	18.68	132.81
4950	49.50	157.97	4.00	4.00	18.56	132.76
4951	49.51	158.25	3.95	3.95	18.38	132.67
4952	49.52	158.56	3.89	3.89	18.18	132.57
4953	49.53	158.88	3.83	3.83	17.97	132.47
4954	49.54	159.20	3.77	3.77	17.76	132.36
4955	49.55	159.51	3.72	3.72	17.56	132.25
4956	49.56	159.79	3.66	3.66	17.38	132.16
4957	49.57	160.01	3.62	3.62	17.22	132.06
4958	49.58	159.86	3.57	3.57	17.08	131.95
4959	49.59	159.50	3.51	3.51	16.93	131.81
4960	49.60	159.06	3.43	3.43	16.75	131.64
4961	49.61	158.59	3.34	3.34	16.55	131.45
4962	49.62	158.10	3.25	3.25	16.33	131.25
4963	49.63	157.62	3.16	3.16	16.12	131.04
4964	49.64	157.17	3.08	3.08	15.93	130.85
4965	49.65	156.79	3.01	3.01	15.75	130.68
4966	49.66	156.48	2.96	2.96	15.66	130.57
4967	49.67	156.11	2.95	2.95	15.64	130.52
4968	49.68	155.65	2.95	2.95	15.68	130.50
4969	49.69	155.13	2.94	2.94	15.73	130.48
4970	49.70	154.57	2.94	2.94	15.79	130.45
4971	49.71	154.00	2.93	2.93	15.84	130.43
4972	49.72	153.45	2.93	2.93	15.89	130.41
4973	49.73	152.94	2.92	2.92	15.94	130.39
4974	49.74	152.52	2.92	2.92	15.98	130.37
4975	49.75	152.20	2.91	2.91	16.01	130.35
4976	49.76	151.86	2.91	2.91	16.04	130.33
4977	49.77	151.44	2.90	2.90	16.07	130.30
4978	49.78	150.98	2.89	2.89	16.10	130.27
4979	49.79	150.49	2.88	2.88	16.14	130.24
4980	49.80	150.01	2.87	2.87	16.17	130.21
4981	49.81	149.55	2.86	2.86	16.20	130.18
4982	49.82	149.14	2.85	2.85	16.23	130.15
4983	49.83	148.80	2.85	2.85	16.28	130.14
4984	49.84	148.26	2.85	2.85	16.37	130.14
4985	49.85	147.46	2.86	2.86	16.50	130.15
4986	49.86	146.52	2.87	2.87	16.67	130.16
4987	49.87	145.49	2.89	2.89	16.86	130.17
4988	49.88	144.43	2.90	2.90	17.05	130.18
4989	49.89	143.39	2.91	2.91	17.24	130.19
4990	49.90	142.43	2.92	2.92	17.42	130.20
4991	49.91	141.59	2.93	2.93	17.57	130.21
4992	49.92	140.93	2.93	2.93	17.69	130.21

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4993	49.93	140.41	2.93	2.93	17.80	130.21
4994	49.94	139.75	2.93	2.93	17.90	130.20
4995	49.95	139.00	2.93	2.93	18.02	130.18
4996	49.96	138.20	2.93	2.93	18.15	130.17
4997	49.97	137.38	2.94	2.94	18.27	130.16
4998	49.98	136.60	2.94	2.94	18.40	130.14
4999	49.99	135.88	2.93	2.93	18.51	130.13
5000	50.00	135.28	2.93	2.93	18.58	130.12

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q _c :	Measured cone resistance (tsf)
f _s :	Sleeve friction resistance (tsf)
u:	Pore pressure (tsf)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (pcf)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1	0.01	0.00	0.00	0.00	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
2	0.02	0.00	0.00	0.00	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
3	0.03	0.00	0.00	0.00	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
4	0.04	0.00	0.00	0.00	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
5	0.05	0.00	0.00	0.00	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
6	0.06	0.00	0.00	0.00	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
7	0.07	0.00	0.00	0.00	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
8	0.08	0.00	0.00	0.00	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
9	0.09	0.01	0.00	0.01	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
10	0.10	0.01	0.00	0.01	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
11	0.11	0.01	0.00	0.01	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
12	0.12	0.01	0.00	0.01	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
13	0.13	0.01	0.00	0.01	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
14	0.14	0.01	0.00	0.01	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
15	0.15	0.01	0.00	0.01	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
16	0.16	0.01	0.00	0.01	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
17	0.17	0.01	0.00	0.01	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
18	0.18	0.01	0.00	0.01	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
19	0.19	0.01	0.00	0.01	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
20	0.20	0.01	0.00	0.01	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
21	0.21	0.01	0.00	0.01	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
22	0.22	0.01	0.00	0.01	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
23	0.23	0.01	0.00	0.01	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
24	0.24	0.01	0.00	0.01	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
25	0.25	0.01	0.00	0.01	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
26	0.26	0.01	0.00	0.01	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
27	0.27	0.01	0.00	0.01	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
28	0.28	0.02	0.00	0.02	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
29	0.29	0.02	0.00	0.02	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
30	0.30	0.02	0.00	0.02	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
31	0.31	0.02	0.00	0.02	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
32	0.32	0.02	0.00	0.02	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
33	0.33	0.02	0.00	0.02	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
34	0.34	0.02	0.00	0.02	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
35	0.35	0.02	0.00	0.02	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
36	0.36	0.02	0.00	0.02	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
37	0.37	0.02	0.00	0.02	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
38	0.38	0.02	0.00	0.02	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
39	0.39	0.02	0.00	0.02	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
40	0.40	0.02	0.00	0.02	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
41	0.41	0.02	0.00	0.02	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
42	0.42	0.02	0.00	0.02	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
43	0.43	0.02	0.00	0.02	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
44	0.44	0.02	0.00	0.02	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
45	0.45	0.03	0.00	0.03	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
46	0.46	0.03	0.00	0.03	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
47	0.47	0.03	0.00	0.03	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
48	0.48	0.03	0.00	0.03	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
49	0.49	0.03	0.00	0.03	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
50	0.50	0.03	0.00	0.03	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
51	0.51	0.03	0.00	0.03	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
52	0.52	0.03	0.00	0.03	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
53	0.53	0.03	0.00	0.03	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
54	0.54	0.03	0.00	0.03	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
55	0.55	0.03	0.00	0.03	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
56	0.56	0.03	0.00	0.03	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
57	0.57	0.03	0.00	0.03	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
58	0.58	0.03	0.00	0.03	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
59	0.59	0.03	0.00	0.03	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
60	0.60	0.03	0.00	0.03	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
61	0.61	0.04	0.00	0.04	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
62	0.62	0.04	0.00	0.04	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
63	0.63	0.04	0.00	0.04	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
64	0.64	0.04	0.00	0.04	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
65	0.65	0.04	0.00	0.04	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
66	0.66	0.04	0.00	0.04	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
67	0.67	0.04	0.00	0.04	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
68	0.68	0.04	0.00	0.04	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
69	0.69	0.04	0.00	0.04	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
70	0.70	0.04	0.00	0.04	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
71	0.71	0.04	0.00	0.04	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
72	0.72	0.04	0.00	0.04	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
73	0.73	0.04	0.00	0.04	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
74	0.74	0.04	0.00	0.04	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
75	0.75	0.04	0.00	0.04	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
76	0.76	0.04	0.00	0.04	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
77	0.77	0.04	0.00	0.04	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
78	0.78	0.05	0.00	0.05	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
79	0.79	0.05	0.00	0.05	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
80	0.80	0.05	0.00	0.05	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
81	0.81	0.05	0.00	0.05	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
82	0.82	0.05	0.00	0.05	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
83	0.83	0.05	0.00	0.05	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
84	0.84	0.05	0.00	0.05	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
85	0.85	0.05	0.00	0.05	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
86	0.86	0.05	0.00	0.05	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
87	0.87	0.05	0.00	0.05	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
88	0.88	0.05	0.00	0.05	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
89	0.89	0.05	0.00	0.05	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
90	0.90	0.05	0.00	0.05	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
91	0.91	0.05	0.00	0.05	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
92	0.92	0.05	0.00	0.05	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
93	0.93	0.05	0.00	0.05	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
94	0.94	0.06	0.00	0.06	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
95	0.95	0.06	0.00	0.06	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
96	0.96	0.06	0.00	0.06	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
97	0.97	0.06	0.00	0.06	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
98	0.98	0.06	0.00	0.06	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
99	0.99	0.06	0.00	0.06	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
100	1.00	0.06	0.00	0.06	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
101	1.01	0.06	0.00	0.06	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
102	1.02	0.06	0.00	0.06	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
103	1.03	0.06	0.00	0.06	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
104	1.04	0.06	0.00	0.06	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
105	1.05	0.06	0.00	0.06	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
106	1.06	0.06	0.00	0.06	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
107	1.07	0.06	0.00	0.06	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
108	1.08	0.06	0.00	0.06	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
109	1.09	0.06	0.00	0.06	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
110	1.10	0.06	0.00	0.06	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
111	1.11	0.07	0.00	0.07	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
112	1.12	0.07	0.00	0.07	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
113	1.13	0.07	0.00	0.07	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
114	1.14	0.07	0.00	0.07	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
115	1.15	0.07	0.00	0.07	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
116	1.16	0.07	0.00	0.07	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
117	1.17	0.07	0.00	0.07	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
118	1.18	0.07	0.00	0.07	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
119	1.19	0.07	0.00	0.07	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
120	1.20	0.07	0.00	0.07	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
121	1.21	0.07	0.00	0.07	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
122	1.22	0.07	0.00	0.07	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
123	1.23	0.07	0.00	0.07	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
124	1.24	0.07	0.00	0.07	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
125	1.25	0.07	0.00	0.07	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
126	1.26	0.07	0.00	0.07	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
127	1.27	0.08	0.00	0.08	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
128	1.28	0.08	0.00	0.08	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
129	1.29	0.08	0.00	0.08	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
130	1.30	0.08	0.00	0.08	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
131	1.31	0.08	0.00	0.08	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
132	1.32	0.08	0.00	0.08	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
133	1.33	0.08	0.00	0.08	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
134	1.34	0.08	0.00	0.08	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
135	1.35	0.08	0.00	0.08	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
136	1.36	0.08	0.00	0.08	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
137	1.37	0.08	0.00	0.08	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
138	1.38	0.08	0.00	0.08	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
139	1.39	0.08	0.00	0.08	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
140	1.40	0.08	0.00	0.08	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
141	1.41	0.08	0.00	0.08	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
142	1.42	0.08	0.00	0.08	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
143	1.43	0.08	0.00	0.08	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
144	1.44	0.09	0.00	0.09	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
145	1.45	0.09	0.00	0.09	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
146	1.46	0.09	0.00	0.09	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
147	1.47	0.09	0.00	0.09	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
148	1.48	0.09	0.00	0.09	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
149	1.49	0.09	0.00	0.09	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
150	1.50	0.09	0.00	0.09	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
151	1.51	0.09	0.00	0.09	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
152	1.52	0.09	0.00	0.09	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
153	1.53	0.09	0.00	0.09	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
154	1.54	0.09	0.00	0.09	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
155	1.55	0.09	0.00	0.09	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
156	1.56	0.09	0.00	0.09	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
157	1.57	0.09	0.00	0.09	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
158	1.58	0.09	0.00	0.09	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
159	1.59	0.09	0.00	0.09	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
160	1.60	0.10	0.00	0.10	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
161	1.61	0.10	0.00	0.10	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
162	1.62	0.10	0.00	0.10	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
163	1.63	0.10	0.00	0.10	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
164	1.64	0.10	0.00	0.10	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
165	1.65	0.10	0.00	0.10	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
166	1.66	0.10	0.00	0.10	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
167	1.67	0.10	0.00	0.10	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
168	1.68	0.10	0.00	0.10	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
169	1.69	0.10	0.00	0.10	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
170	1.70	0.10	0.00	0.10	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
171	1.71	0.10	0.00	0.10	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
172	1.72	0.10	0.00	0.10	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
173	1.73	0.10	0.00	0.10	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
174	1.74	0.10	0.00	0.10	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
175	1.75	0.10	0.00	0.10	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
176	1.76	0.10	0.00	0.10	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
177	1.77	0.11	0.00	0.11	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
178	1.78	0.11	0.00	0.11	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
179	1.79	0.11	0.00	0.11	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
180	1.80	0.11	0.00	0.11	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
181	1.81	0.11	0.00	0.11	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
182	1.82	0.11	0.00	0.11	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
183	1.83	0.11	0.00	0.11	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
184	1.84	0.11	0.00	0.11	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
185	1.85	0.11	0.00	0.11	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
186	1.86	0.11	0.00	0.11	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
187	1.87	0.11	0.00	0.11	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
188	1.88	0.11	0.00	0.11	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
189	1.89	0.11	0.00	0.11	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
190	1.90	0.11	0.00	0.11	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
191	1.91	0.11	0.00	0.11	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
192	1.92	0.11	0.00	0.11	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
193	1.93	0.12	0.00	0.12	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
194	1.94	0.12	0.00	0.12	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
195	1.95	0.12	0.00	0.12	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
196	1.96	0.12	0.00	0.12	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
197	1.97	0.12	0.00	0.12	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
198	1.98	0.12	0.00	0.12	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
199	1.99	0.12	0.00	0.12	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
200	2.00	0.12	0.00	0.12	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
201	2.01	0.12	0.00	0.12	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
202	2.02	0.12	0.00	0.12	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
203	2.03	0.12	0.00	0.12	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
204	2.04	0.12	0.00	0.12	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
205	2.05	0.12	0.00	0.12	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
206	2.06	0.12	0.00	0.12	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
207	2.07	0.12	0.00	0.12	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
208	2.08	0.12	0.00	0.12	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
209	2.09	0.12	0.00	0.12	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
210	2.10	0.13	0.00	0.13	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
211	2.11	0.13	0.00	0.13	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
212	2.12	0.13	0.00	0.13	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
213	2.13	0.13	0.00	0.13	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
214	2.14	0.13	0.00	0.13	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
215	2.15	0.13	0.00	0.13	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
216	2.16	0.13	0.00	0.13	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
217	2.17	0.13	0.00	0.13	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
218	2.18	0.13	0.00	0.13	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
219	2.19	0.13	0.00	0.13	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
220	2.20	0.13	0.00	0.13	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
221	2.21	0.13	0.00	0.13	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
222	2.22	0.13	0.00	0.13	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
223	2.23	0.13	0.00	0.13	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
224	2.24	0.13	0.00	0.13	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
225	2.25	0.13	0.00	0.13	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
226	2.26	0.13	0.00	0.13	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
227	2.27	0.14	0.00	0.14	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
228	2.28	0.14	0.00	0.14	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
229	2.29	0.14	0.00	0.14	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
230	2.30	0.14	0.00	0.14	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
231	2.31	0.14	0.00	0.14	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
232	2.32	0.14	0.00	0.14	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
233	2.33	0.14	0.00	0.14	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
234	2.34	0.14	0.00	0.14	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
235	2.35	0.14	0.00	0.14	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
236	2.36	0.14	0.00	0.14	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
237	2.37	0.14	0.00	0.14	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
238	2.38	0.14	0.00	0.14	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
239	2.39	0.14	0.00	0.14	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
240	2.40	0.14	0.00	0.14	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
241	2.41	0.14	0.00	0.14	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
242	2.42	0.14	0.00	0.14	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
243	2.43	0.14	0.00	0.14	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
244	2.44	0.15	0.00	0.15	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
245	2.45	0.15	0.00	0.15	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
246	2.46	0.15	0.00	0.15	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
247	2.47	0.15	0.00	0.15	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
248	2.48	0.15	0.00	0.15	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
249	2.49	0.15	0.00	0.15	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
250	2.50	0.15	0.00	0.15	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
251	2.51	0.15	0.00	0.15	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
252	2.52	0.15	0.00	0.15	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
253	2.53	0.15	0.00	0.15	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
254	2.54	0.15	0.00	0.15	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
255	2.55	0.15	0.00	0.15	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
256	2.56	0.15	0.00	0.15	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
257	2.57	0.15	0.00	0.15	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
258	2.58	0.15	0.00	0.15	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
259	2.59	0.15	0.00	0.15	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
260	2.60	0.15	0.00	0.15	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
261	2.61	0.15	0.00	0.15	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
262	2.62	0.16	0.00	0.16	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
263	2.63	0.16	0.00	0.16	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
264	2.64	0.16	0.00	0.16	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
265	2.65	0.16	0.00	0.16	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
266	2.66	0.16	0.00	0.16	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
267	2.67	0.16	0.00	0.16	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
268	2.68	0.16	0.00	0.16	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
269	2.69	0.16	0.00	0.16	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
270	2.70	0.16	0.00	0.16	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
271	2.71	0.16	0.00	0.16	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
272	2.72	0.16	0.00	0.16	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
273	2.73	0.16	0.00	0.16	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
274	2.74	0.16	0.00	0.16	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
275	2.75	0.16	0.00	0.16	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
276	2.76	0.16	0.00	0.16	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
277	2.77	0.16	0.00	0.16	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
278	2.78	0.16	0.00	0.16	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
279	2.79	0.17	0.00	0.17	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
280	2.80	0.17	0.00	0.17	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
281	2.81	0.17	0.00	0.17	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
282	2.82	0.17	0.00	0.17	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
283	2.83	0.17	0.00	0.17	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
284	2.84	0.17	0.00	0.17	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
285	2.85	0.17	0.00	0.17	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
286	2.86	0.17	0.00	0.17	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
287	2.87	0.17	0.00	0.17	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
288	2.88	0.17	0.00	0.17	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
289	2.89	0.17	0.00	0.17	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
290	2.90	0.17	0.00	0.17	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
291	2.91	0.17	0.00	0.17	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
292	2.92	0.17	0.00	0.17	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
293	2.93	0.17	0.00	0.17	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
294	2.94	0.17	0.00	0.17	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
295	2.95	0.17	0.00	0.17	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
296	2.96	0.17	0.00	0.17	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
297	2.97	0.18	0.00	0.18	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
298	2.98	0.18	0.00	0.18	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
299	2.99	0.18	0.00	0.18	0.99	0.479	1.06	0.453	1.00	1.30	2.000	No
300	3.00	0.18	0.00	0.18	0.99	0.479	1.06	0.453	1.00	1.30	2.000	No
301	3.01	0.18	0.00	0.18	0.99	0.479	1.06	0.453	1.00	1.30	2.000	No
302	3.02	0.18	0.00	0.18	0.99	0.479	1.06	0.453	1.00	1.30	2.000	No
303	3.03	0.18	0.00	0.18	0.99	0.479	1.06	0.453	1.00	1.30	2.000	No
304	3.04	0.18	0.00	0.18	0.99	0.479	1.06	0.453	1.00	1.30	2.000	No
305	3.05	0.18	0.00	0.18	0.99	0.479	1.06	0.453	1.00	1.30	2.000	No
306	3.06	0.18	0.00	0.18	0.99	0.479	1.06	0.453	1.00	1.30	2.000	No
307	3.07	0.18	0.00	0.18	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
308	3.08	0.18	0.00	0.18	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
309	3.09	0.18	0.00	0.18	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
310	3.10	0.18	0.00	0.18	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
311	3.11	0.18	0.00	0.18	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
312	3.12	0.18	0.00	0.18	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
313	3.13	0.18	0.00	0.18	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
314	3.14	0.18	0.00	0.18	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
315	3.15	0.19	0.00	0.19	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
316	3.16	0.19	0.00	0.19	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
317	3.17	0.19	0.00	0.19	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
318	3.18	0.19	0.00	0.19	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
319	3.19	0.19	0.00	0.19	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
320	3.20	0.19	0.00	0.19	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
321	3.21	0.19	0.00	0.19	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
322	3.22	0.19	0.00	0.19	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
323	3.23	0.19	0.00	0.19	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
324	3.24	0.19	0.00	0.19	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
325	3.25	0.19	0.00	0.19	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
326	3.26	0.19	0.00	0.19	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
327	3.27	0.19	0.00	0.19	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
328	3.28	0.19	0.00	0.19	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
329	3.29	0.19	0.00	0.19	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
330	3.30	0.19	0.00	0.19	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
331	3.31	0.19	0.00	0.19	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
332	3.32	0.19	0.00	0.19	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
333	3.33	0.19	0.00	0.19	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
334	3.34	0.20	0.00	0.20	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
335	3.35	0.20	0.00	0.20	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
336	3.36	0.20	0.00	0.20	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
337	3.37	0.20	0.00	0.20	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
338	3.38	0.20	0.00	0.20	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
339	3.39	0.20	0.00	0.20	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
340	3.40	0.20	0.00	0.20	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
341	3.41	0.20	0.00	0.20	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
342	3.42	0.20	0.00	0.20	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
343	3.43	0.20	0.00	0.20	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
344	3.44	0.20	0.00	0.20	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
345	3.45	0.20	0.00	0.20	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
346	3.46	0.20	0.00	0.20	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
347	3.47	0.20	0.00	0.20	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
348	3.48	0.20	0.00	0.20	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
349	3.49	0.20	0.00	0.20	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
350	3.50	0.20	0.00	0.20	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
351	3.51	0.20	0.00	0.20	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
352	3.52	0.20	0.00	0.20	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
353	3.53	0.21	0.00	0.21	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
354	3.54	0.21	0.00	0.21	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
355	3.55	0.21	0.00	0.21	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
356	3.56	0.21	0.00	0.21	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
357	3.57	0.21	0.00	0.21	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
358	3.58	0.21	0.00	0.21	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
359	3.59	0.21	0.00	0.21	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
360	3.60	0.21	0.00	0.21	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
361	3.61	0.21	0.00	0.21	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
362	3.62	0.21	0.00	0.21	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
363	3.63	0.21	0.00	0.21	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
364	3.64	0.21	0.00	0.21	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
365	3.65	0.21	0.00	0.21	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
366	3.66	0.21	0.00	0.21	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
367	3.67	0.21	0.00	0.21	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
368	3.68	0.21	0.00	0.21	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
369	3.69	0.21	0.00	0.21	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
370	3.70	0.21	0.00	0.21	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
371	3.71	0.22	0.00	0.22	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
372	3.72	0.22	0.00	0.22	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
373	3.73	0.22	0.00	0.22	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
374	3.74	0.22	0.00	0.22	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
375	3.75	0.22	0.00	0.22	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
376	3.76	0.22	0.00	0.22	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
377	3.77	0.22	0.00	0.22	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
378	3.78	0.22	0.00	0.22	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
379	3.79	0.22	0.00	0.22	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
380	3.80	0.22	0.00	0.22	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
381	3.81	0.22	0.00	0.22	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
382	3.82	0.22	0.00	0.22	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
383	3.83	0.22	0.00	0.22	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
384	3.84	0.22	0.00	0.22	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
385	3.85	0.22	0.00	0.22	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
386	3.86	0.22	0.00	0.22	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
387	3.87	0.22	0.00	0.22	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
388	3.88	0.22	0.00	0.22	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
389	3.89	0.22	0.00	0.22	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
390	3.90	0.23	0.00	0.23	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
391	3.91	0.23	0.00	0.23	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
392	3.92	0.23	0.00	0.23	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
393	3.93	0.23	0.00	0.23	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
394	3.94	0.23	0.00	0.23	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
395	3.95	0.23	0.00	0.23	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
396	3.96	0.23	0.00	0.23	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
397	3.97	0.23	0.00	0.23	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
398	3.98	0.23	0.00	0.23	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
399	3.99	0.23	0.00	0.23	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
400	4.00	0.23	0.00	0.23	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
401	4.01	0.23	0.00	0.23	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
402	4.02	0.23	0.00	0.23	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
403	4.03	0.23	0.00	0.23	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
404	4.04	0.23	0.00	0.23	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
405	4.05	0.23	0.00	0.23	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
406	4.06	0.23	0.00	0.23	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
407	4.07	0.23	0.00	0.23	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
408	4.08	0.24	0.00	0.24	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
409	4.09	0.24	0.00	0.24	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
410	4.10	0.24	0.00	0.24	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
411	4.11	0.24	0.00	0.24	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
412	4.12	0.24	0.00	0.24	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
413	4.13	0.24	0.00	0.24	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
414	4.14	0.24	0.00	0.24	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
415	4.15	0.24	0.00	0.24	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
416	4.16	0.24	0.00	0.24	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
417	4.17	0.24	0.00	0.24	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
418	4.18	0.24	0.00	0.24	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
419	4.19	0.24	0.00	0.24	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
420	4.20	0.24	0.00	0.24	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
421	4.21	0.24	0.00	0.24	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
422	4.22	0.24	0.00	0.24	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
423	4.23	0.24	0.00	0.24	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
424	4.24	0.24	0.00	0.24	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
425	4.25	0.24	0.00	0.24	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
426	4.26	0.25	0.00	0.25	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
427	4.27	0.25	0.00	0.25	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
428	4.28	0.25	0.00	0.25	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
429	4.29	0.25	0.00	0.25	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
430	4.30	0.25	0.00	0.25	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
431	4.31	0.25	0.00	0.25	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
432	4.32	0.25	0.00	0.25	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
433	4.33	0.25	0.00	0.25	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
434	4.34	0.25	0.00	0.25	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
435	4.35	0.25	0.00	0.25	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
436	4.36	0.25	0.00	0.25	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
437	4.37	0.25	0.00	0.25	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
438	4.38	0.25	0.00	0.25	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
439	4.39	0.25	0.00	0.25	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
440	4.40	0.25	0.00	0.25	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
441	4.41	0.25	0.00	0.25	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
442	4.42	0.25	0.00	0.25	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
443	4.43	0.26	0.00	0.26	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
444	4.44	0.26	0.00	0.26	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
445	4.45	0.26	0.00	0.26	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
446	4.46	0.26	0.00	0.26	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
447	4.47	0.26	0.00	0.26	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
448	4.48	0.26	0.00	0.26	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
449	4.49	0.26	0.00	0.26	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
450	4.50	0.26	0.00	0.26	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
451	4.51	0.26	0.00	0.26	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
452	4.52	0.26	0.00	0.26	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
453	4.53	0.26	0.00	0.26	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
454	4.54	0.26	0.00	0.26	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
455	4.55	0.26	0.00	0.26	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
456	4.56	0.26	0.00	0.26	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
457	4.57	0.26	0.00	0.26	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
458	4.58	0.26	0.00	0.26	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
459	4.59	0.26	0.00	0.26	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
460	4.60	0.26	0.00	0.26	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
461	4.61	0.27	0.00	0.27	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
462	4.62	0.27	0.00	0.27	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
463	4.63	0.27	0.00	0.27	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
464	4.64	0.27	0.00	0.27	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
465	4.65	0.27	0.00	0.27	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
466	4.66	0.27	0.00	0.27	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
467	4.67	0.27	0.00	0.27	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
468	4.68	0.27	0.00	0.27	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
469	4.69	0.27	0.00	0.27	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
470	4.70	0.27	0.00	0.27	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
471	4.71	0.27	0.00	0.27	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
472	4.72	0.27	0.00	0.27	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
473	4.73	0.27	0.00	0.27	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
474	4.74	0.27	0.00	0.27	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
475	4.75	0.27	0.00	0.27	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
476	4.76	0.27	0.00	0.27	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
477	4.77	0.27	0.00	0.27	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
478	4.78	0.27	0.00	0.27	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
479	4.79	0.28	0.00	0.28	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
480	4.80	0.28	0.00	0.28	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
481	4.81	0.28	0.00	0.28	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
482	4.82	0.28	0.00	0.28	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
483	4.83	0.28	0.00	0.28	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
484	4.84	0.28	0.00	0.28	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
485	4.85	0.28	0.00	0.28	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
486	4.86	0.28	0.00	0.28	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
487	4.87	0.28	0.00	0.28	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
488	4.88	0.28	0.00	0.28	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
489	4.89	0.28	0.00	0.28	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
490	4.90	0.28	0.00	0.28	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
491	4.91	0.28	0.00	0.28	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
492	4.92	0.28	0.00	0.28	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
493	4.93	0.28	0.00	0.28	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
494	4.94	0.28	0.00	0.28	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
495	4.95	0.28	0.00	0.28	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
496	4.96	0.29	0.00	0.29	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
497	4.97	0.29	0.00	0.29	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
498	4.98	0.29	0.00	0.29	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
499	4.99	0.29	0.00	0.29	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
500	5.00	0.29	0.00	0.29	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
501	5.01	0.29	0.00	0.29	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
502	5.02	0.29	0.00	0.29	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
503	5.03	0.29	0.00	0.29	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
504	5.04	0.29	0.00	0.29	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
505	5.05	0.29	0.00	0.29	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
506	5.06	0.29	0.00	0.29	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
507	5.07	0.29	0.00	0.29	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
508	5.08	0.29	0.00	0.29	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
509	5.09	0.29	0.00	0.29	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
510	5.10	0.29	0.00	0.29	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
511	5.11	0.29	0.00	0.29	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
512	5.12	0.29	0.00	0.29	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
513	5.13	0.30	0.00	0.30	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
514	5.14	0.30	0.00	0.30	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
515	5.15	0.30	0.00	0.30	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
516	5.16	0.30	0.00	0.30	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
517	5.17	0.30	0.00	0.30	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
518	5.18	0.30	0.00	0.30	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
519	5.19	0.30	0.00	0.30	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
520	5.20	0.30	0.00	0.30	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
521	5.21	0.30	0.00	0.30	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
522	5.22	0.30	0.00	0.30	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
523	5.23	0.30	0.00	0.30	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
524	5.24	0.30	0.00	0.30	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
525	5.25	0.30	0.00	0.30	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
526	5.26	0.30	0.00	0.30	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
527	5.27	0.30	0.00	0.30	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
528	5.28	0.30	0.00	0.30	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
529	5.29	0.30	0.00	0.30	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
530	5.30	0.31	0.00	0.31	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
531	5.31	0.31	0.00	0.31	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
532	5.32	0.31	0.00	0.31	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
533	5.33	0.31	0.00	0.31	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
534	5.34	0.31	0.00	0.31	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
535	5.35	0.31	0.00	0.31	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
536	5.36	0.31	0.00	0.31	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
537	5.37	0.31	0.00	0.31	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
538	5.38	0.31	0.00	0.31	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
539	5.39	0.31	0.00	0.31	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
540	5.40	0.31	0.00	0.31	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
541	5.41	0.31	0.00	0.31	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
542	5.42	0.31	0.00	0.31	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
543	5.43	0.31	0.00	0.31	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
544	5.44	0.31	0.00	0.31	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
545	5.45	0.31	0.00	0.31	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
546	5.46	0.31	0.00	0.31	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
547	5.47	0.32	0.00	0.32	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
548	5.48	0.32	0.00	0.32	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
549	5.49	0.32	0.00	0.32	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
550	5.50	0.32	0.00	0.32	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
551	5.51	0.32	0.00	0.32	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
552	5.52	0.32	0.00	0.32	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
553	5.53	0.32	0.00	0.32	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
554	5.54	0.32	0.00	0.32	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
555	5.55	0.32	0.00	0.32	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
556	5.56	0.32	0.00	0.32	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
557	5.57	0.32	0.00	0.32	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
558	5.58	0.32	0.00	0.32	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
559	5.59	0.32	0.00	0.32	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
560	5.60	0.32	0.00	0.32	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
561	5.61	0.32	0.00	0.32	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
562	5.62	0.32	0.00	0.32	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
563	5.63	0.32	0.00	0.32	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
564	5.64	0.33	0.00	0.33	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
565	5.65	0.33	0.00	0.33	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
566	5.66	0.33	0.00	0.33	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
567	5.67	0.33	0.00	0.33	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
568	5.68	0.33	0.00	0.33	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
569	5.69	0.33	0.00	0.33	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
570	5.70	0.33	0.00	0.33	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
571	5.71	0.33	0.00	0.33	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
572	5.72	0.33	0.00	0.33	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
573	5.73	0.33	0.00	0.33	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
574	5.74	0.33	0.00	0.33	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
575	5.75	0.33	0.00	0.33	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
576	5.76	0.33	0.00	0.33	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
577	5.77	0.33	0.00	0.33	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
578	5.78	0.33	0.00	0.33	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
579	5.79	0.33	0.00	0.33	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
580	5.80	0.33	0.00	0.33	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
581	5.81	0.34	0.00	0.34	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
582	5.82	0.34	0.00	0.34	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
583	5.83	0.34	0.00	0.34	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
584	5.84	0.34	0.00	0.34	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
585	5.85	0.34	0.00	0.34	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
586	5.86	0.34	0.00	0.34	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
587	5.87	0.34	0.00	0.34	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
588	5.88	0.34	0.00	0.34	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
589	5.89	0.34	0.00	0.34	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
590	5.90	0.34	0.00	0.34	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
591	5.91	0.34	0.00	0.34	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
592	5.92	0.34	0.00	0.34	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
593	5.93	0.34	0.00	0.34	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
594	5.94	0.34	0.00	0.34	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
595	5.95	0.34	0.00	0.34	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
596	5.96	0.34	0.00	0.34	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
597	5.97	0.34	0.00	0.34	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
598	5.98	0.35	0.00	0.35	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
599	5.99	0.35	0.00	0.35	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
600	6.00	0.35	0.00	0.35	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
601	6.01	0.35	0.00	0.35	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
602	6.02	0.35	0.00	0.35	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
603	6.03	0.35	0.00	0.35	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
604	6.04	0.35	0.00	0.35	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
605	6.05	0.35	0.00	0.35	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
606	6.06	0.35	0.00	0.35	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
607	6.07	0.35	0.00	0.35	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
608	6.08	0.35	0.00	0.35	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
609	6.09	0.35	0.00	0.35	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
610	6.10	0.35	0.00	0.35	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
611	6.11	0.35	0.00	0.35	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
612	6.12	0.35	0.00	0.35	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
613	6.13	0.35	0.00	0.35	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
614	6.14	0.35	0.00	0.35	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
615	6.15	0.36	0.00	0.36	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
616	6.16	0.36	0.00	0.36	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
617	6.17	0.36	0.00	0.36	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
618	6.18	0.36	0.00	0.36	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
619	6.19	0.36	0.00	0.36	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
620	6.20	0.36	0.00	0.36	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
621	6.21	0.36	0.00	0.36	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
622	6.22	0.36	0.00	0.36	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
623	6.23	0.36	0.00	0.36	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
624	6.24	0.36	0.00	0.36	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
625	6.25	0.36	0.00	0.36	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
626	6.26	0.36	0.00	0.36	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
627	6.27	0.36	0.00	0.36	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
628	6.28	0.36	0.00	0.36	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
629	6.29	0.36	0.00	0.36	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
630	6.30	0.36	0.00	0.36	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
631	6.31	0.36	0.00	0.36	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
632	6.32	0.37	0.00	0.37	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
633	6.33	0.37	0.00	0.37	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
634	6.34	0.37	0.00	0.37	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
635	6.35	0.37	0.00	0.37	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
636	6.36	0.37	0.00	0.37	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
637	6.37	0.37	0.00	0.37	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
638	6.38	0.37	0.00	0.37	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
639	6.39	0.37	0.00	0.37	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
640	6.40	0.37	0.00	0.37	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
641	6.41	0.37	0.00	0.37	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
642	6.42	0.37	0.00	0.37	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
643	6.43	0.37	0.00	0.37	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
644	6.44	0.37	0.00	0.37	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
645	6.45	0.37	0.00	0.37	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
646	6.46	0.37	0.00	0.37	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
647	6.47	0.37	0.00	0.37	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
648	6.48	0.37	0.00	0.37	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
649	6.49	0.38	0.00	0.38	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
650	6.50	0.38	0.00	0.38	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
651	6.51	0.38	0.00	0.38	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
652	6.52	0.38	0.00	0.38	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
653	6.53	0.38	0.00	0.38	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
654	6.54	0.38	0.00	0.38	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
655	6.55	0.38	0.00	0.38	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
656	6.56	0.38	0.00	0.38	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
657	6.57	0.38	0.00	0.38	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
658	6.58	0.38	0.00	0.38	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
659	6.59	0.38	0.00	0.38	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
660	6.60	0.38	0.00	0.38	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
661	6.61	0.38	0.00	0.38	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
662	6.62	0.38	0.00	0.38	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
663	6.63	0.38	0.00	0.38	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
664	6.64	0.38	0.00	0.38	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
665	6.65	0.38	0.00	0.38	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
666	6.66	0.39	0.00	0.39	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
667	6.67	0.39	0.00	0.39	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
668	6.68	0.39	0.00	0.39	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
669	6.69	0.39	0.00	0.39	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
670	6.70	0.39	0.00	0.39	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
671	6.71	0.39	0.00	0.39	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
672	6.72	0.39	0.00	0.39	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
673	6.73	0.39	0.00	0.39	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
674	6.74	0.39	0.00	0.39	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
675	6.75	0.39	0.00	0.39	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
676	6.76	0.39	0.00	0.39	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
677	6.77	0.39	0.00	0.39	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
678	6.78	0.39	0.00	0.39	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
679	6.79	0.39	0.00	0.39	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
680	6.80	0.39	0.00	0.39	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
681	6.81	0.39	0.00	0.39	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
682	6.82	0.40	0.00	0.40	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
683	6.83	0.40	0.00	0.40	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
684	6.84	0.40	0.00	0.40	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
685	6.85	0.40	0.00	0.40	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
686	6.86	0.40	0.00	0.40	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
687	6.87	0.40	0.00	0.40	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
688	6.88	0.40	0.00	0.40	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
689	6.89	0.40	0.00	0.40	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
690	6.90	0.40	0.00	0.40	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
691	6.91	0.40	0.00	0.40	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
692	6.92	0.40	0.00	0.40	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
693	6.93	0.40	0.00	0.40	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
694	6.94	0.40	0.00	0.40	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
695	6.95	0.40	0.00	0.40	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
696	6.96	0.40	0.00	0.40	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
697	6.97	0.40	0.00	0.40	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
698	6.98	0.41	0.00	0.41	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
699	6.99	0.41	0.00	0.41	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
700	7.00	0.41	0.00	0.41	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
701	7.01	0.41	0.00	0.41	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
702	7.02	0.41	0.00	0.41	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
703	7.03	0.41	0.00	0.41	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
704	7.04	0.41	0.00	0.41	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
705	7.05	0.41	0.00	0.41	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
706	7.06	0.41	0.00	0.41	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
707	7.07	0.41	0.00	0.41	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
708	7.08	0.41	0.00	0.41	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
709	7.09	0.41	0.00	0.41	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
710	7.10	0.41	0.00	0.41	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
711	7.11	0.41	0.00	0.41	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
712	7.12	0.41	0.00	0.41	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
713	7.13	0.41	0.00	0.41	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
714	7.14	0.41	0.00	0.41	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
715	7.15	0.42	0.00	0.42	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
716	7.16	0.42	0.00	0.42	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
717	7.17	0.42	0.00	0.42	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
718	7.18	0.42	0.00	0.42	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
719	7.19	0.42	0.00	0.42	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
720	7.20	0.42	0.00	0.42	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
721	7.21	0.42	0.00	0.42	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
722	7.22	0.42	0.00	0.42	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
723	7.23	0.42	0.00	0.42	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
724	7.24	0.42	0.00	0.42	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
725	7.25	0.42	0.00	0.42	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
726	7.26	0.42	0.00	0.42	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
727	7.27	0.42	0.00	0.42	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
728	7.28	0.42	0.00	0.42	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
729	7.29	0.42	0.00	0.42	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
730	7.30	0.42	0.00	0.42	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
731	7.31	0.43	0.00	0.43	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
732	7.32	0.43	0.00	0.43	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
733	7.33	0.43	0.00	0.43	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
734	7.34	0.43	0.00	0.43	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
735	7.35	0.43	0.00	0.43	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
736	7.36	0.43	0.00	0.43	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
737	7.37	0.43	0.00	0.43	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
738	7.38	0.43	0.00	0.43	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
739	7.39	0.43	0.00	0.43	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
740	7.40	0.43	0.00	0.43	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
741	7.41	0.43	0.00	0.43	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
742	7.42	0.43	0.00	0.43	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
743	7.43	0.43	0.00	0.43	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
744	7.44	0.43	0.00	0.43	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
745	7.45	0.43	0.00	0.43	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
746	7.46	0.43	0.00	0.43	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
747	7.47	0.44	0.00	0.44	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
748	7.48	0.44	0.00	0.44	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
749	7.49	0.44	0.00	0.44	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
750	7.50	0.44	0.00	0.44	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
751	7.51	0.44	0.00	0.44	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
752	7.52	0.44	0.00	0.44	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
753	7.53	0.44	0.00	0.44	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
754	7.54	0.44	0.00	0.44	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
755	7.55	0.44	0.00	0.44	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
756	7.56	0.44	0.00	0.44	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
757	7.57	0.44	0.00	0.44	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
758	7.58	0.44	0.00	0.44	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
759	7.59	0.44	0.00	0.44	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
760	7.60	0.44	0.00	0.44	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
761	7.61	0.44	0.00	0.44	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
762	7.62	0.44	0.00	0.44	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
763	7.63	0.45	0.00	0.45	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
764	7.64	0.45	0.00	0.45	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
765	7.65	0.45	0.00	0.45	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
766	7.66	0.45	0.00	0.45	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
767	7.67	0.45	0.00	0.45	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
768	7.68	0.45	0.00	0.45	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
769	7.69	0.45	0.00	0.45	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
770	7.70	0.45	0.00	0.45	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
771	7.71	0.45	0.00	0.45	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
772	7.72	0.45	0.00	0.45	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
773	7.73	0.45	0.00	0.45	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
774	7.74	0.45	0.00	0.45	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
775	7.75	0.45	0.00	0.45	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
776	7.76	0.45	0.00	0.45	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
777	7.77	0.45	0.00	0.45	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
778	7.78	0.45	0.00	0.45	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
779	7.79	0.46	0.00	0.46	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
780	7.80	0.46	0.00	0.46	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
781	7.81	0.46	0.00	0.46	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
782	7.82	0.46	0.00	0.46	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
783	7.83	0.46	0.00	0.46	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
784	7.84	0.46	0.00	0.46	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
785	7.85	0.46	0.00	0.46	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
786	7.86	0.46	0.00	0.46	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
787	7.87	0.46	0.00	0.46	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
788	7.88	0.46	0.00	0.46	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
789	7.89	0.46	0.00	0.46	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
790	7.90	0.46	0.00	0.46	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
791	7.91	0.46	0.00	0.46	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
792	7.92	0.46	0.00	0.46	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
793	7.93	0.46	0.00	0.46	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
794	7.94	0.46	0.00	0.46	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
795	7.95	0.47	0.00	0.47	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
796	7.96	0.47	0.00	0.47	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
797	7.97	0.47	0.00	0.47	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
798	7.98	0.47	0.00	0.47	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
799	7.99	0.47	0.00	0.47	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
800	8.00	0.47	0.00	0.47	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
801	8.01	0.47	0.00	0.47	0.98	0.473	1.06	0.448	1.00	1.30	0.583	No
802	8.02	0.47	0.00	0.47	0.98	0.474	1.06	0.448	1.00	1.30	0.583	No
803	8.03	0.47	0.00	0.47	0.98	0.474	1.06	0.449	1.00	1.30	0.583	No
804	8.04	0.47	0.00	0.47	0.98	0.474	1.06	0.449	1.00	1.30	0.584	No
805	8.05	0.47	0.00	0.47	0.98	0.475	1.06	0.449	1.00	1.30	0.584	No
806	8.06	0.47	0.00	0.47	0.98	0.475	1.06	0.450	1.00	1.30	0.584	No
807	8.07	0.47	0.00	0.47	0.98	0.475	1.06	0.450	1.00	1.30	0.585	No
808	8.08	0.47	0.00	0.47	0.98	0.475	1.06	0.450	1.00	1.30	0.585	No
809	8.09	0.47	0.00	0.47	0.98	0.476	1.06	0.450	1.00	1.30	0.585	No
810	8.10	0.47	0.00	0.47	0.98	0.476	1.06	0.451	1.00	1.30	0.586	No
811	8.11	0.48	0.00	0.47	0.98	0.476	1.06	0.451	1.00	1.30	0.586	No
812	8.12	0.48	0.00	0.47	0.98	0.477	1.06	0.451	1.00	1.30	0.587	No
813	8.13	0.48	0.00	0.47	0.98	0.477	1.06	0.452	1.00	1.30	0.587	No
814	8.14	0.48	0.00	0.47	0.98	0.477	1.06	0.452	1.00	1.30	0.587	No
815	8.15	0.48	0.00	0.47	0.98	0.478	1.06	0.452	1.00	1.30	0.588	No
816	8.16	0.48	0.00	0.47	0.98	0.478	1.06	0.452	1.00	1.30	0.588	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
817	8.17	0.48	0.01	0.47	0.98	0.478	1.06	0.453	1.00	1.30	0.588	No
818	8.18	0.48	0.01	0.47	0.98	0.478	1.06	0.453	1.00	1.30	0.589	No
819	8.19	0.48	0.01	0.47	0.98	0.479	1.06	0.453	1.00	1.30	0.589	No
820	8.20	0.48	0.01	0.47	0.98	0.479	1.06	0.453	1.00	1.30	0.590	No
821	8.21	0.48	0.01	0.47	0.98	0.479	1.06	0.454	1.00	1.30	0.590	No
822	8.22	0.48	0.01	0.48	0.98	0.480	1.06	0.454	1.00	1.30	0.590	No
823	8.23	0.48	0.01	0.48	0.98	0.480	1.06	0.454	1.00	1.30	0.591	No
824	8.24	0.48	0.01	0.48	0.98	0.480	1.06	0.455	1.00	1.30	0.591	No
825	8.25	0.48	0.01	0.48	0.98	0.481	1.06	0.455	1.00	1.30	0.591	No
826	8.26	0.48	0.01	0.48	0.98	0.481	1.06	0.455	1.00	1.30	0.592	No
827	8.27	0.49	0.01	0.48	0.98	0.481	1.06	0.455	1.00	1.30	0.592	No
828	8.28	0.49	0.01	0.48	0.98	0.481	1.06	0.456	1.00	1.30	0.592	No
829	8.29	0.49	0.01	0.48	0.98	0.482	1.06	0.456	1.00	1.30	0.593	No
830	8.30	0.49	0.01	0.48	0.98	0.482	1.06	0.456	1.00	1.30	0.593	No
831	8.31	0.49	0.01	0.48	0.98	0.482	1.06	0.457	1.00	1.30	0.594	No
832	8.32	0.49	0.01	0.48	0.98	0.483	1.06	0.457	1.00	1.30	0.594	No
833	8.33	0.49	0.01	0.48	0.98	0.483	1.06	0.457	1.00	1.30	0.594	No
834	8.34	0.49	0.01	0.48	0.98	0.483	1.06	0.457	1.00	1.30	0.595	No
835	8.35	0.49	0.01	0.48	0.98	0.483	1.06	0.458	1.00	1.30	0.595	No
836	8.36	0.49	0.01	0.48	0.98	0.484	1.06	0.458	1.00	1.30	0.595	No
837	8.37	0.49	0.01	0.48	0.98	0.484	1.06	0.458	1.00	1.30	0.596	No
838	8.38	0.49	0.01	0.48	0.98	0.484	1.06	0.458	1.00	1.30	0.596	No
839	8.39	0.49	0.01	0.48	0.98	0.485	1.06	0.459	1.00	1.30	0.596	No
840	8.40	0.49	0.01	0.48	0.98	0.485	1.06	0.459	1.00	1.30	0.597	No
841	8.41	0.49	0.01	0.48	0.98	0.485	1.06	0.459	1.00	1.30	0.597	No
842	8.42	0.49	0.01	0.48	0.98	0.485	1.06	0.460	1.00	1.30	0.597	No
843	8.43	0.50	0.01	0.48	0.98	0.486	1.06	0.460	1.00	1.30	0.598	No
844	8.44	0.50	0.01	0.48	0.98	0.486	1.06	0.460	1.00	1.30	0.598	No
845	8.45	0.50	0.01	0.48	0.98	0.486	1.06	0.460	1.00	1.30	0.598	No
846	8.46	0.50	0.01	0.48	0.98	0.487	1.06	0.461	1.00	1.30	0.599	No
847	8.47	0.50	0.01	0.48	0.98	0.487	1.06	0.461	1.00	1.30	0.599	No
848	8.48	0.50	0.01	0.48	0.98	0.487	1.06	0.461	1.00	1.30	0.600	No
849	8.49	0.50	0.02	0.48	0.98	0.487	1.06	0.461	1.00	1.30	0.600	No
850	8.50	0.50	0.02	0.48	0.98	0.488	1.06	0.462	1.00	1.30	0.600	No
851	8.51	0.50	0.02	0.48	0.98	0.488	1.06	0.462	1.00	1.30	0.601	No
852	8.52	0.50	0.02	0.48	0.98	0.488	1.06	0.462	1.00	1.30	0.601	No
853	8.53	0.50	0.02	0.49	0.98	0.489	1.06	0.463	1.00	1.30	0.601	No
854	8.54	0.50	0.02	0.49	0.98	0.489	1.06	0.463	1.00	1.30	0.602	No
855	8.55	0.50	0.02	0.49	0.98	0.489	1.06	0.463	1.00	1.30	0.602	No
856	8.56	0.50	0.02	0.49	0.98	0.489	1.06	0.463	1.00	1.30	0.602	No
857	8.57	0.50	0.02	0.49	0.98	0.490	1.06	0.464	1.00	1.30	0.603	No
858	8.58	0.50	0.02	0.49	0.98	0.490	1.06	0.464	1.00	1.30	0.603	No
859	8.59	0.51	0.02	0.49	0.98	0.490	1.06	0.464	1.00	1.30	0.603	No
860	8.60	0.51	0.02	0.49	0.98	0.491	1.06	0.464	1.00	1.30	0.604	No
861	8.61	0.51	0.02	0.49	0.98	0.491	1.06	0.465	1.00	1.30	0.604	No
862	8.62	0.51	0.02	0.49	0.98	0.491	1.06	0.465	1.00	1.30	0.604	No
863	8.63	0.51	0.02	0.49	0.98	0.491	1.06	0.465	1.00	1.30	0.605	No
864	8.64	0.51	0.02	0.49	0.98	0.492	1.06	0.465	1.00	1.30	0.605	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
865	8.65	0.51	0.02	0.49	0.98	0.492	1.06	0.466	1.00	1.30	0.605	No
866	8.66	0.51	0.02	0.49	0.98	0.492	1.06	0.466	1.00	1.30	0.606	No
867	8.67	0.51	0.02	0.49	0.98	0.493	1.06	0.466	1.00	1.30	0.606	No
868	8.68	0.51	0.02	0.49	0.98	0.493	1.06	0.466	1.00	1.30	0.606	No
869	8.69	0.51	0.02	0.49	0.98	0.493	1.06	0.467	1.00	1.30	0.607	No
870	8.70	0.51	0.02	0.49	0.98	0.493	1.06	0.467	1.00	1.30	0.607	No
871	8.71	0.51	0.02	0.49	0.98	0.494	1.06	0.467	1.00	1.30	0.607	No
872	8.72	0.51	0.02	0.49	0.98	0.494	1.06	0.468	1.00	1.30	0.608	No
873	8.73	0.51	0.02	0.49	0.98	0.494	1.06	0.468	1.00	1.30	0.608	No
874	8.74	0.51	0.02	0.49	0.98	0.494	1.06	0.468	1.00	1.30	0.608	No
875	8.75	0.52	0.02	0.49	0.98	0.495	1.06	0.468	1.00	1.30	0.609	No
876	8.76	0.52	0.02	0.49	0.98	0.495	1.06	0.469	1.00	1.30	0.609	No
877	8.77	0.52	0.02	0.49	0.98	0.495	1.06	0.469	1.00	1.30	0.609	No
878	8.78	0.52	0.02	0.49	0.98	0.496	1.06	0.469	1.00	1.30	0.610	No
879	8.79	0.52	0.02	0.49	0.98	0.496	1.06	0.469	1.00	1.30	0.610	No
880	8.80	0.52	0.02	0.49	0.98	0.496	1.06	0.470	1.00	1.30	0.610	No
881	8.81	0.52	0.03	0.49	0.98	0.496	1.06	0.470	1.00	1.30	0.611	No
882	8.82	0.52	0.03	0.49	0.98	0.497	1.06	0.470	1.00	1.30	0.611	No
883	8.83	0.52	0.03	0.49	0.98	0.497	1.06	0.470	1.00	1.30	0.611	No
884	8.84	0.52	0.03	0.50	0.98	0.497	1.06	0.471	1.00	1.30	0.612	No
885	8.85	0.52	0.03	0.50	0.98	0.497	1.06	0.471	1.00	1.30	0.612	No
886	8.86	0.52	0.03	0.50	0.98	0.498	1.06	0.471	1.00	1.30	0.612	No
887	8.87	0.52	0.03	0.50	0.98	0.498	1.06	0.471	1.00	1.30	0.613	No
888	8.88	0.52	0.03	0.50	0.98	0.498	1.06	0.472	1.00	1.30	0.613	No
889	8.89	0.52	0.03	0.50	0.98	0.499	1.06	0.472	1.00	1.30	0.613	No
890	8.90	0.53	0.03	0.50	0.98	0.499	1.06	0.472	1.00	1.30	0.614	No
891	8.91	0.53	0.03	0.50	0.98	0.499	1.06	0.472	1.00	1.30	0.614	No
892	8.92	0.53	0.03	0.50	0.98	0.499	1.06	0.473	1.00	1.30	0.614	No
893	8.93	0.53	0.03	0.50	0.98	0.500	1.06	0.473	1.00	1.30	0.615	No
894	8.94	0.53	0.03	0.50	0.98	0.500	1.06	0.473	1.00	1.30	0.615	No
895	8.95	0.53	0.03	0.50	0.98	0.500	1.06	0.473	1.00	1.30	0.615	No
896	8.96	0.53	0.03	0.50	0.98	0.500	1.06	0.474	1.00	1.30	0.616	No
897	8.97	0.53	0.03	0.50	0.98	0.501	1.06	0.474	1.00	1.30	0.616	No
898	8.98	0.53	0.03	0.50	0.98	0.501	1.06	0.474	1.00	1.30	0.616	No
899	8.99	0.53	0.03	0.50	0.98	0.501	1.06	0.474	1.00	1.30	0.617	No
900	9.00	0.53	0.03	0.50	0.98	0.501	1.06	0.475	1.00	1.30	0.617	No
901	9.01	0.53	0.03	0.50	0.98	0.502	1.06	0.475	1.00	1.30	0.617	No
902	9.02	0.53	0.03	0.50	0.98	0.502	1.06	0.475	1.00	1.30	0.618	No
903	9.03	0.53	0.03	0.50	0.98	0.502	1.06	0.475	1.00	1.30	0.618	No
904	9.04	0.53	0.03	0.50	0.98	0.502	1.06	0.476	1.00	1.30	0.618	No
905	9.05	0.53	0.03	0.50	0.98	0.503	1.06	0.476	1.00	1.30	0.619	No
906	9.06	0.54	0.03	0.50	0.98	0.503	1.06	0.476	1.00	1.30	0.619	No
907	9.07	0.54	0.03	0.50	0.98	0.503	1.06	0.476	1.00	1.30	0.619	No
908	9.08	0.54	0.03	0.50	0.98	0.504	1.06	0.477	1.00	1.30	0.620	No
909	9.09	0.54	0.03	0.50	0.98	0.504	1.06	0.477	1.00	1.30	0.620	No
910	9.10	0.54	0.03	0.50	0.98	0.504	1.06	0.477	1.00	1.30	0.620	No
911	9.11	0.54	0.03	0.50	0.98	0.504	1.06	0.477	1.00	1.30	0.621	No
912	9.12	0.54	0.03	0.50	0.98	0.505	1.06	0.478	1.00	1.30	0.621	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
913	9.13	0.54	0.04	0.50	0.98	0.505	1.06	0.478	1.00	1.30	0.621	No
914	9.14	0.54	0.04	0.50	0.98	0.505	1.06	0.478	1.00	1.30	0.622	No
915	9.15	0.54	0.04	0.50	0.98	0.505	1.06	0.478	1.00	1.30	0.622	No
916	9.16	0.54	0.04	0.51	0.98	0.506	1.06	0.479	1.00	1.30	0.622	No
917	9.17	0.54	0.04	0.51	0.98	0.506	1.06	0.479	1.00	1.30	0.623	No
918	9.18	0.54	0.04	0.51	0.98	0.506	1.06	0.479	1.00	1.30	0.623	No
919	9.19	0.54	0.04	0.51	0.98	0.506	1.06	0.479	1.00	1.30	0.623	No
920	9.20	0.54	0.04	0.51	0.98	0.507	1.06	0.480	1.00	1.30	0.624	No
921	9.21	0.54	0.04	0.51	0.98	0.507	1.06	0.480	1.00	1.30	0.624	No
922	9.22	0.55	0.04	0.51	0.98	0.507	1.06	0.480	1.00	1.30	0.624	No
923	9.23	0.55	0.04	0.51	0.98	0.507	1.06	0.480	1.00	1.30	0.624	No
924	9.24	0.55	0.04	0.51	0.98	0.508	1.06	0.481	1.00	1.30	0.625	No
925	9.25	0.55	0.04	0.51	0.98	0.508	1.06	0.481	1.00	1.30	0.625	No
926	9.26	0.55	0.04	0.51	0.98	0.508	1.06	0.481	1.00	1.30	0.625	No
927	9.27	0.55	0.04	0.51	0.98	0.508	1.06	0.481	1.00	1.30	0.626	No
928	9.28	0.55	0.04	0.51	0.98	0.509	1.06	0.482	1.00	1.30	0.626	No
929	9.29	0.55	0.04	0.51	0.98	0.509	1.06	0.482	1.00	1.30	0.626	No
930	9.30	0.55	0.04	0.51	0.98	0.509	1.06	0.482	1.00	1.30	0.627	No
931	9.31	0.55	0.04	0.51	0.98	0.509	1.06	0.482	1.00	1.30	0.627	No
932	9.32	0.55	0.04	0.51	0.98	0.510	1.06	0.483	1.00	1.30	0.627	No
933	9.33	0.55	0.04	0.51	0.98	0.510	1.06	0.483	1.00	1.30	0.628	No
934	9.34	0.55	0.04	0.51	0.98	0.510	1.06	0.483	1.00	1.30	0.628	No
935	9.35	0.55	0.04	0.51	0.98	0.510	1.06	0.483	1.00	1.30	0.628	No
936	9.36	0.55	0.04	0.51	0.98	0.511	1.06	0.483	1.00	1.30	0.629	No
937	9.37	0.55	0.04	0.51	0.98	0.511	1.06	0.484	1.00	1.30	0.629	No
938	9.38	0.56	0.04	0.51	0.98	0.511	1.06	0.484	1.00	1.30	0.629	No
939	9.39	0.56	0.04	0.51	0.98	0.511	1.06	0.484	1.00	1.30	0.629	No
940	9.40	0.56	0.04	0.51	0.98	0.512	1.06	0.484	1.00	1.30	0.630	No
941	9.41	0.56	0.04	0.51	0.98	0.512	1.06	0.485	1.00	1.30	0.630	No
942	9.42	0.56	0.04	0.51	0.98	0.512	1.06	0.485	1.00	1.30	0.630	No
943	9.43	0.56	0.04	0.51	0.98	0.512	1.06	0.485	1.00	1.30	0.631	No
944	9.44	0.56	0.04	0.51	0.98	0.513	1.06	0.485	1.00	1.30	0.631	No
945	9.45	0.56	0.05	0.51	0.98	0.513	1.06	0.486	1.00	1.30	0.631	No
946	9.46	0.56	0.05	0.51	0.98	0.513	1.06	0.486	1.00	1.30	0.632	No
947	9.47	0.56	0.05	0.52	0.98	0.513	1.06	0.486	1.00	1.30	0.632	No
948	9.48	0.56	0.05	0.52	0.98	0.514	1.06	0.486	1.00	1.30	0.632	No
949	9.49	0.56	0.05	0.52	0.98	0.514	1.06	0.487	1.00	1.30	0.633	No
950	9.50	0.56	0.05	0.52	0.98	0.514	1.06	0.487	1.00	1.30	0.633	No
951	9.51	0.56	0.05	0.52	0.98	0.514	1.06	0.487	1.00	1.30	0.633	No
952	9.52	0.56	0.05	0.52	0.98	0.515	1.06	0.487	1.00	1.30	0.633	No
953	9.53	0.56	0.05	0.52	0.98	0.515	1.06	0.487	1.00	1.30	0.634	No
954	9.54	0.57	0.05	0.52	0.98	0.515	1.06	0.488	1.00	1.30	0.634	No
955	9.55	0.57	0.05	0.52	0.98	0.515	1.06	0.488	1.00	1.30	0.634	No
956	9.56	0.57	0.05	0.52	0.98	0.516	1.06	0.488	1.00	1.30	0.635	No
957	9.57	0.57	0.05	0.52	0.98	0.516	1.06	0.488	1.00	1.30	0.635	No
958	9.58	0.57	0.05	0.52	0.98	0.516	1.06	0.489	1.00	1.30	0.635	No
959	9.59	0.57	0.05	0.52	0.98	0.516	1.06	0.489	1.00	1.30	0.636	No
960	9.60	0.57	0.05	0.52	0.98	0.517	1.06	0.489	1.00	1.30	0.636	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
961	9.61	0.57	0.05	0.52	0.98	0.517	1.06	0.489	1.00	1.30	0.636	No
962	9.62	0.57	0.05	0.52	0.98	0.517	1.06	0.490	1.00	1.30	0.636	No
963	9.63	0.57	0.05	0.52	0.98	0.517	1.06	0.490	1.00	1.30	0.637	No
964	9.64	0.57	0.05	0.52	0.98	0.518	1.06	0.490	1.00	1.30	0.637	No
965	9.65	0.57	0.05	0.52	0.98	0.518	1.06	0.490	1.00	1.30	0.637	No
966	9.66	0.57	0.05	0.52	0.98	0.518	1.06	0.490	1.00	1.30	0.638	No
967	9.67	0.57	0.05	0.52	0.98	0.518	1.06	0.491	1.00	1.30	0.638	No
968	9.68	0.57	0.05	0.52	0.98	0.519	1.06	0.491	1.00	1.30	0.638	No
969	9.69	0.58	0.05	0.52	0.98	0.519	1.06	0.491	1.00	1.30	0.639	No
970	9.70	0.58	0.05	0.52	0.98	0.519	1.06	0.491	1.00	1.30	0.639	No
971	9.71	0.58	0.05	0.52	0.98	0.519	1.06	0.492	1.00	1.30	0.639	No
972	9.72	0.58	0.05	0.52	0.98	0.520	1.06	0.492	1.00	1.30	0.639	No
973	9.73	0.58	0.05	0.52	0.98	0.520	1.06	0.492	1.00	1.30	0.640	No
974	9.74	0.58	0.05	0.52	0.98	0.520	1.06	0.492	1.00	1.30	0.640	No
975	9.75	0.58	0.05	0.52	0.98	0.520	1.06	0.493	1.00	1.30	0.640	No
976	9.76	0.58	0.05	0.52	0.98	0.521	1.06	0.493	1.00	1.30	0.641	No
977	9.77	0.58	0.06	0.52	0.98	0.521	1.06	0.493	1.00	1.30	0.641	No
978	9.78	0.58	0.06	0.53	0.98	0.521	1.06	0.493	1.00	1.30	0.641	No
979	9.79	0.58	0.06	0.53	0.98	0.521	1.06	0.493	1.00	1.30	0.641	No
980	9.80	0.58	0.06	0.53	0.98	0.522	1.06	0.494	1.00	1.30	0.642	No
981	9.81	0.58	0.06	0.53	0.98	0.522	1.06	0.494	1.00	1.30	0.642	No
982	9.82	0.58	0.06	0.53	0.98	0.522	1.06	0.494	1.00	1.30	0.642	No
983	9.83	0.58	0.06	0.53	0.98	0.522	1.06	0.494	1.00	1.30	0.643	No
984	9.84	0.58	0.06	0.53	0.98	0.522	1.06	0.495	1.00	1.30	0.643	No
985	9.85	0.59	0.06	0.53	0.98	0.523	1.06	0.495	1.00	1.30	0.643	No
986	9.86	0.59	0.06	0.53	0.98	0.523	1.06	0.495	1.00	1.30	0.644	No
987	9.87	0.59	0.06	0.53	0.98	0.523	1.06	0.495	1.00	1.30	0.644	No
988	9.88	0.59	0.06	0.53	0.98	0.523	1.06	0.495	1.00	1.30	0.644	No
989	9.89	0.59	0.06	0.53	0.98	0.524	1.06	0.496	1.00	1.30	0.644	No
990	9.90	0.59	0.06	0.53	0.98	0.524	1.06	0.496	1.00	1.30	0.645	No
991	9.91	0.59	0.06	0.53	0.98	0.524	1.06	0.496	1.00	1.30	0.645	No
992	9.92	0.59	0.06	0.53	0.98	0.524	1.06	0.496	1.00	1.30	0.645	No
993	9.93	0.59	0.06	0.53	0.98	0.525	1.06	0.497	1.00	1.30	0.646	No
994	9.94	0.59	0.06	0.53	0.98	0.525	1.06	0.497	1.00	1.30	0.646	No
995	9.95	0.59	0.06	0.53	0.98	0.525	1.06	0.497	1.00	1.30	0.646	No
996	9.96	0.59	0.06	0.53	0.98	0.525	1.06	0.497	1.00	1.30	0.646	No
997	9.97	0.59	0.06	0.53	0.98	0.526	1.06	0.497	1.00	1.30	0.647	No
998	9.98	0.59	0.06	0.53	0.98	0.526	1.06	0.498	1.00	1.30	0.647	No
999	9.99	0.59	0.06	0.53	0.98	0.526	1.06	0.498	1.00	1.30	0.647	No
1000	10.00	0.59	0.06	0.53	0.98	0.526	1.06	0.498	1.00	1.30	0.648	No
1001	10.01	0.60	0.06	0.53	0.98	0.526	1.06	0.498	1.00	1.30	0.648	No
1002	10.02	0.60	0.06	0.53	0.98	0.527	1.06	0.499	1.00	1.30	0.648	No
1003	10.03	0.60	0.06	0.53	0.98	0.527	1.06	0.499	1.00	1.30	0.648	No
1004	10.04	0.60	0.06	0.53	0.98	0.527	1.06	0.499	1.00	1.30	0.649	No
1005	10.05	0.60	0.06	0.53	0.98	0.527	1.06	0.499	1.00	1.30	0.649	No
1006	10.06	0.60	0.06	0.53	0.98	0.528	1.06	0.499	1.00	1.30	0.649	No
1007	10.07	0.60	0.06	0.53	0.98	0.528	1.06	0.500	1.00	1.30	0.650	No
1008	10.08	0.60	0.06	0.53	0.98	0.528	1.06	0.500	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1009	10.09	0.60	0.07	0.53	0.98	0.528	1.06	0.500	1.00	1.30	2.000	Yes
1010	10.10	0.60	0.07	0.54	0.98	0.529	1.06	0.500	1.00	1.30	2.000	Yes
1011	10.11	0.60	0.07	0.54	0.98	0.529	1.06	0.501	1.00	1.30	2.000	Yes
1012	10.12	0.60	0.07	0.54	0.98	0.529	1.06	0.501	1.00	1.30	2.000	Yes
1013	10.13	0.60	0.07	0.54	0.98	0.529	1.06	0.501	1.00	1.30	2.000	Yes
1014	10.14	0.60	0.07	0.54	0.98	0.529	1.06	0.501	1.00	1.30	2.000	Yes
1015	10.15	0.60	0.07	0.54	0.98	0.530	1.06	0.501	1.00	1.30	2.000	Yes
1016	10.16	0.60	0.07	0.54	0.98	0.530	1.06	0.502	1.00	1.30	2.000	Yes
1017	10.17	0.61	0.07	0.54	0.98	0.530	1.06	0.502	1.00	1.30	2.000	Yes
1018	10.18	0.61	0.07	0.54	0.98	0.530	1.06	0.502	1.00	1.30	2.000	Yes
1019	10.19	0.61	0.07	0.54	0.98	0.531	1.06	0.502	1.00	1.30	2.000	Yes
1020	10.20	0.61	0.07	0.54	0.98	0.531	1.06	0.502	1.00	1.30	2.000	Yes
1021	10.21	0.61	0.07	0.54	0.98	0.531	1.06	0.503	1.00	1.30	2.000	Yes
1022	10.22	0.61	0.07	0.54	0.98	0.531	1.06	0.503	1.00	1.30	2.000	Yes
1023	10.23	0.61	0.07	0.54	0.98	0.531	1.06	0.503	1.00	1.30	2.000	Yes
1024	10.24	0.61	0.07	0.54	0.98	0.532	1.06	0.503	1.00	1.30	2.000	Yes
1025	10.25	0.61	0.07	0.54	0.98	0.532	1.06	0.504	1.00	1.30	2.000	Yes
1026	10.26	0.61	0.07	0.54	0.98	0.532	1.06	0.504	1.00	1.30	2.000	Yes
1027	10.27	0.61	0.07	0.54	0.98	0.532	1.06	0.504	1.00	1.30	2.000	Yes
1028	10.28	0.61	0.07	0.54	0.98	0.533	1.06	0.504	1.00	1.30	2.000	Yes
1029	10.29	0.61	0.07	0.54	0.98	0.533	1.06	0.504	1.00	1.30	2.000	Yes
1030	10.30	0.61	0.07	0.54	0.98	0.533	1.06	0.505	1.00	1.30	2.000	Yes
1031	10.31	0.61	0.07	0.54	0.98	0.533	1.06	0.505	1.00	1.30	2.000	Yes
1032	10.32	0.61	0.07	0.54	0.98	0.533	1.06	0.505	1.00	1.30	2.000	Yes
1033	10.33	0.61	0.07	0.54	0.98	0.534	1.06	0.505	1.00	1.30	2.000	Yes
1034	10.34	0.62	0.07	0.54	0.98	0.534	1.06	0.505	1.00	1.30	2.000	Yes
1035	10.35	0.62	0.07	0.54	0.98	0.534	1.06	0.506	1.00	1.30	2.000	Yes
1036	10.36	0.62	0.07	0.54	0.98	0.534	1.06	0.506	1.00	1.30	2.000	Yes
1037	10.37	0.62	0.07	0.54	0.98	0.535	1.06	0.506	1.00	1.30	2.000	Yes
1038	10.38	0.62	0.07	0.54	0.98	0.535	1.06	0.506	1.00	1.30	2.000	Yes
1039	10.39	0.62	0.07	0.54	0.98	0.535	1.06	0.507	1.00	1.30	2.000	Yes
1040	10.40	0.62	0.07	0.54	0.98	0.535	1.06	0.507	1.00	1.30	2.000	Yes
1041	10.41	0.62	0.08	0.54	0.98	0.536	1.06	0.507	1.00	1.30	2.000	Yes
1042	10.42	0.62	0.08	0.54	0.98	0.536	1.06	0.507	1.00	1.30	2.000	Yes
1043	10.43	0.62	0.08	0.55	0.98	0.536	1.06	0.507	1.00	1.30	2.000	Yes
1044	10.44	0.62	0.08	0.55	0.98	0.536	1.06	0.508	1.00	1.30	2.000	Yes
1045	10.45	0.62	0.08	0.55	0.98	0.536	1.06	0.508	1.00	1.30	2.000	Yes
1046	10.46	0.62	0.08	0.55	0.98	0.537	1.06	0.508	1.00	1.30	2.000	Yes
1047	10.47	0.62	0.08	0.55	0.98	0.537	1.06	0.508	1.00	1.30	2.000	Yes
1048	10.48	0.62	0.08	0.55	0.98	0.537	1.06	0.508	1.00	1.30	2.000	Yes
1049	10.49	0.62	0.08	0.55	0.98	0.537	1.06	0.509	1.00	1.30	2.000	Yes
1050	10.50	0.63	0.08	0.55	0.98	0.538	1.06	0.509	1.00	1.30	2.000	Yes
1051	10.51	0.63	0.08	0.55	0.98	0.538	1.06	0.509	1.00	1.30	2.000	Yes
1052	10.52	0.63	0.08	0.55	0.98	0.538	1.06	0.509	1.00	1.30	0.662	No
1053	10.53	0.63	0.08	0.55	0.98	0.538	1.06	0.509	1.00	1.30	0.662	No
1054	10.54	0.63	0.08	0.55	0.98	0.538	1.06	0.510	1.00	1.30	0.663	No
1055	10.55	0.63	0.08	0.55	0.98	0.539	1.06	0.510	1.00	1.30	0.663	No
1056	10.56	0.63	0.08	0.55	0.98	0.539	1.06	0.510	1.00	1.30	0.663	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1057	10.57	0.63	0.08	0.55	0.98	0.539	1.06	0.510	1.00	1.30	0.663	No
1058	10.58	0.63	0.08	0.55	0.98	0.539	1.06	0.510	1.00	1.30	0.664	No
1059	10.59	0.63	0.08	0.55	0.98	0.539	1.06	0.511	1.00	1.30	0.664	No
1060	10.60	0.63	0.08	0.55	0.98	0.540	1.06	0.511	1.00	1.30	0.664	No
1061	10.61	0.63	0.08	0.55	0.98	0.540	1.06	0.511	1.00	1.30	0.664	No
1062	10.62	0.63	0.08	0.55	0.98	0.540	1.06	0.511	1.00	1.30	2.000	Yes
1063	10.63	0.63	0.08	0.55	0.98	0.540	1.06	0.512	1.00	1.30	2.000	Yes
1064	10.64	0.63	0.08	0.55	0.98	0.541	1.06	0.512	1.00	1.30	2.000	Yes
1065	10.65	0.63	0.08	0.55	0.98	0.541	1.06	0.512	1.00	1.30	2.000	Yes
1066	10.66	0.63	0.08	0.55	0.98	0.541	1.06	0.512	1.00	1.30	2.000	Yes
1067	10.67	0.64	0.08	0.55	0.98	0.541	1.06	0.512	1.00	1.30	2.000	Yes
1068	10.68	0.64	0.08	0.55	0.98	0.541	1.06	0.513	1.00	1.30	2.000	Yes
1069	10.69	0.64	0.08	0.55	0.98	0.542	1.06	0.513	1.00	1.30	2.000	Yes
1070	10.70	0.64	0.08	0.55	0.98	0.542	1.06	0.513	1.00	1.30	2.000	Yes
1071	10.71	0.64	0.08	0.55	0.98	0.542	1.06	0.513	1.00	1.30	2.000	Yes
1072	10.72	0.64	0.08	0.55	0.98	0.542	1.06	0.513	1.00	1.30	2.000	Yes
1073	10.73	0.64	0.09	0.55	0.98	0.543	1.06	0.514	1.00	1.30	2.000	Yes
1074	10.74	0.64	0.09	0.55	0.98	0.543	1.06	0.514	1.00	1.30	2.000	Yes
1075	10.75	0.64	0.09	0.55	0.98	0.543	1.06	0.514	1.00	1.30	2.000	Yes
1076	10.76	0.64	0.09	0.55	0.98	0.543	1.06	0.514	1.00	1.30	2.000	Yes
1077	10.77	0.64	0.09	0.56	0.98	0.543	1.06	0.514	1.00	1.30	2.000	Yes
1078	10.78	0.64	0.09	0.56	0.98	0.544	1.06	0.515	1.00	1.30	2.000	Yes
1079	10.79	0.64	0.09	0.56	0.98	0.544	1.06	0.515	1.00	1.30	2.000	Yes
1080	10.80	0.64	0.09	0.56	0.98	0.544	1.06	0.515	1.00	1.30	2.000	Yes
1081	10.81	0.64	0.09	0.56	0.98	0.544	1.06	0.515	1.00	1.30	2.000	Yes
1082	10.82	0.64	0.09	0.56	0.98	0.544	1.06	0.515	1.00	1.30	2.000	Yes
1083	10.83	0.65	0.09	0.56	0.98	0.545	1.06	0.516	1.00	1.30	2.000	Yes
1084	10.84	0.65	0.09	0.56	0.98	0.545	1.06	0.516	1.00	1.30	2.000	Yes
1085	10.85	0.65	0.09	0.56	0.98	0.545	1.06	0.516	1.00	1.30	2.000	Yes
1086	10.86	0.65	0.09	0.56	0.98	0.545	1.06	0.516	1.00	1.30	2.000	Yes
1087	10.87	0.65	0.09	0.56	0.98	0.545	1.06	0.516	1.00	1.30	2.000	Yes
1088	10.88	0.65	0.09	0.56	0.98	0.546	1.06	0.517	1.00	1.30	2.000	Yes
1089	10.89	0.65	0.09	0.56	0.98	0.546	1.06	0.517	1.00	1.30	2.000	Yes
1090	10.90	0.65	0.09	0.56	0.98	0.546	1.06	0.517	1.00	1.30	2.000	Yes
1091	10.91	0.65	0.09	0.56	0.98	0.546	1.06	0.517	1.00	1.30	2.000	Yes
1092	10.92	0.65	0.09	0.56	0.98	0.547	1.06	0.517	1.00	1.30	2.000	Yes
1093	10.93	0.65	0.09	0.56	0.98	0.547	1.06	0.518	1.00	1.30	2.000	Yes
1094	10.94	0.65	0.09	0.56	0.98	0.547	1.06	0.518	1.00	1.30	2.000	Yes
1095	10.95	0.65	0.09	0.56	0.98	0.547	1.06	0.518	1.00	1.30	2.000	Yes
1096	10.96	0.65	0.09	0.56	0.98	0.547	1.06	0.518	1.00	1.30	2.000	Yes
1097	10.97	0.65	0.09	0.56	0.98	0.548	1.06	0.518	1.00	1.30	2.000	Yes
1098	10.98	0.65	0.09	0.56	0.98	0.548	1.06	0.519	1.00	1.30	2.000	Yes
1099	10.99	0.66	0.09	0.56	0.98	0.548	1.06	0.519	1.00	1.30	2.000	Yes
1100	11.00	0.66	0.09	0.56	0.98	0.548	1.06	0.519	1.00	1.30	2.000	Yes
1101	11.01	0.66	0.09	0.56	0.98	0.548	1.06	0.519	1.00	1.30	2.000	Yes
1102	11.02	0.66	0.09	0.56	0.98	0.549	1.06	0.519	1.00	1.30	2.000	Yes
1103	11.03	0.66	0.09	0.56	0.98	0.549	1.06	0.520	1.00	1.30	2.000	Yes
1104	11.04	0.66	0.09	0.56	0.98	0.549	1.06	0.520	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1105	11.05	0.66	0.10	0.56	0.98	0.549	1.06	0.520	1.00	1.30	2.000	Yes
1106	11.06	0.66	0.10	0.56	0.98	0.549	1.06	0.520	1.00	1.30	2.000	Yes
1107	11.07	0.66	0.10	0.56	0.98	0.550	1.06	0.520	1.00	1.30	2.000	Yes
1108	11.08	0.66	0.10	0.56	0.98	0.550	1.06	0.520	1.00	1.30	2.000	Yes
1109	11.09	0.66	0.10	0.57	0.98	0.550	1.06	0.521	1.00	1.30	2.000	Yes
1110	11.10	0.66	0.10	0.57	0.98	0.550	1.06	0.521	1.00	1.30	2.000	Yes
1111	11.11	0.66	0.10	0.57	0.98	0.550	1.06	0.521	1.00	1.30	2.000	Yes
1112	11.12	0.66	0.10	0.57	0.98	0.551	1.06	0.521	1.00	1.30	2.000	Yes
1113	11.13	0.66	0.10	0.57	0.98	0.551	1.06	0.521	1.00	1.30	2.000	Yes
1114	11.14	0.66	0.10	0.57	0.98	0.551	1.06	0.522	1.00	1.30	0.678	No
1115	11.15	0.67	0.10	0.57	0.98	0.551	1.06	0.522	1.00	1.30	0.678	No
1116	11.16	0.67	0.10	0.57	0.98	0.551	1.06	0.522	1.00	1.30	0.679	No
1117	11.17	0.67	0.10	0.57	0.98	0.552	1.06	0.522	1.00	1.30	0.679	No
1118	11.18	0.67	0.10	0.57	0.98	0.552	1.06	0.522	1.00	1.30	0.679	No
1119	11.19	0.67	0.10	0.57	0.98	0.552	1.06	0.523	1.00	1.30	0.679	No
1120	11.20	0.67	0.10	0.57	0.98	0.552	1.06	0.523	1.00	1.30	0.680	No
1121	11.21	0.67	0.10	0.57	0.98	0.552	1.06	0.523	1.00	1.30	0.680	No
1122	11.22	0.67	0.10	0.57	0.98	0.553	1.06	0.523	1.00	1.30	2.000	Yes
1123	11.23	0.67	0.10	0.57	0.98	0.553	1.06	0.523	1.00	1.30	2.000	Yes
1124	11.24	0.67	0.10	0.57	0.98	0.553	1.06	0.524	1.00	1.30	2.000	Yes
1125	11.25	0.67	0.10	0.57	0.98	0.553	1.06	0.524	1.00	1.30	2.000	Yes
1126	11.26	0.67	0.10	0.57	0.98	0.553	1.06	0.524	1.00	1.30	2.000	Yes
1127	11.27	0.67	0.10	0.57	0.98	0.554	1.06	0.524	1.00	1.30	2.000	Yes
1128	11.28	0.67	0.10	0.57	0.98	0.554	1.06	0.524	1.00	1.30	2.000	Yes
1129	11.29	0.67	0.10	0.57	0.98	0.554	1.06	0.525	1.00	1.30	2.000	Yes
1130	11.30	0.67	0.10	0.57	0.98	0.554	1.06	0.525	1.00	1.30	2.000	Yes
1131	11.31	0.67	0.10	0.57	0.98	0.554	1.06	0.525	1.00	1.30	2.000	Yes
1132	11.32	0.68	0.10	0.57	0.98	0.555	1.06	0.525	1.00	1.30	2.000	Yes
1133	11.33	0.68	0.10	0.57	0.98	0.555	1.06	0.525	1.00	1.30	2.000	Yes
1134	11.34	0.68	0.10	0.57	0.98	0.555	1.06	0.525	1.00	1.30	2.000	Yes
1135	11.35	0.68	0.10	0.57	0.98	0.555	1.06	0.526	1.00	1.30	2.000	Yes
1136	11.36	0.68	0.10	0.57	0.98	0.555	1.06	0.526	1.00	1.30	2.000	Yes
1137	11.37	0.68	0.11	0.57	0.98	0.556	1.06	0.526	1.00	1.30	2.000	Yes
1138	11.38	0.68	0.11	0.57	0.98	0.556	1.06	0.526	1.00	1.30	2.000	Yes
1139	11.39	0.68	0.11	0.57	0.98	0.556	1.06	0.526	1.00	1.30	2.000	Yes
1140	11.40	0.68	0.11	0.57	0.98	0.556	1.06	0.527	1.00	1.30	2.000	Yes
1141	11.41	0.68	0.11	0.57	0.98	0.556	1.06	0.527	1.00	1.30	2.000	Yes
1142	11.42	0.68	0.11	0.57	0.98	0.557	1.06	0.527	1.00	1.30	2.000	Yes
1143	11.43	0.68	0.11	0.58	0.98	0.557	1.06	0.527	1.00	1.30	2.000	Yes
1144	11.44	0.68	0.11	0.58	0.98	0.557	1.06	0.527	1.00	1.30	2.000	Yes
1145	11.45	0.68	0.11	0.58	0.98	0.557	1.06	0.528	1.00	1.30	2.000	Yes
1146	11.46	0.68	0.11	0.58	0.98	0.557	1.06	0.528	1.00	1.30	2.000	Yes
1147	11.47	0.68	0.11	0.58	0.98	0.558	1.06	0.528	1.00	1.30	2.000	Yes
1148	11.48	0.69	0.11	0.58	0.98	0.558	1.06	0.528	1.00	1.30	2.000	Yes
1149	11.49	0.69	0.11	0.58	0.98	0.558	1.06	0.528	1.00	1.30	2.000	Yes
1150	11.50	0.69	0.11	0.58	0.98	0.558	1.06	0.528	1.00	1.30	2.000	Yes
1151	11.51	0.69	0.11	0.58	0.98	0.558	1.06	0.529	1.00	1.30	2.000	Yes
1152	11.52	0.69	0.11	0.58	0.98	0.559	1.06	0.529	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1153	11.53	0.69	0.11	0.58	0.98	0.559	1.06	0.529	1.00	1.30	2.000	Yes
1154	11.54	0.69	0.11	0.58	0.98	0.559	1.06	0.529	1.00	1.30	2.000	Yes
1155	11.55	0.69	0.11	0.58	0.98	0.559	1.06	0.529	1.00	1.30	2.000	Yes
1156	11.56	0.69	0.11	0.58	0.98	0.559	1.06	0.530	1.00	1.30	2.000	Yes
1157	11.57	0.69	0.11	0.58	0.98	0.560	1.06	0.530	1.00	1.30	2.000	Yes
1158	11.58	0.69	0.11	0.58	0.98	0.560	1.06	0.530	1.00	1.30	2.000	Yes
1159	11.59	0.69	0.11	0.58	0.98	0.560	1.06	0.530	1.00	1.30	2.000	Yes
1160	11.60	0.69	0.11	0.58	0.98	0.560	1.06	0.530	1.00	1.30	2.000	Yes
1161	11.61	0.69	0.11	0.58	0.98	0.560	1.06	0.531	1.00	1.30	2.000	Yes
1162	11.62	0.69	0.11	0.58	0.98	0.561	1.06	0.531	1.00	1.30	2.000	Yes
1163	11.63	0.69	0.11	0.58	0.98	0.561	1.06	0.531	1.00	1.30	2.000	Yes
1164	11.64	0.69	0.11	0.58	0.98	0.561	1.06	0.531	1.00	1.30	2.000	Yes
1165	11.65	0.70	0.11	0.58	0.98	0.561	1.06	0.531	1.00	1.30	2.000	Yes
1166	11.66	0.70	0.11	0.58	0.98	0.561	1.06	0.531	1.00	1.30	2.000	Yes
1167	11.67	0.70	0.11	0.58	0.98	0.562	1.06	0.532	1.00	1.30	2.000	Yes
1168	11.68	0.70	0.11	0.58	0.98	0.562	1.06	0.532	1.00	1.30	2.000	Yes
1169	11.69	0.70	0.12	0.58	0.98	0.562	1.06	0.532	1.00	1.30	2.000	Yes
1170	11.70	0.70	0.12	0.58	0.98	0.562	1.06	0.532	1.00	1.30	2.000	Yes
1171	11.71	0.70	0.12	0.58	0.98	0.562	1.06	0.532	1.00	1.30	2.000	Yes
1172	11.72	0.70	0.12	0.58	0.98	0.563	1.06	0.533	1.00	1.30	2.000	Yes
1173	11.73	0.70	0.12	0.58	0.98	0.563	1.06	0.533	1.00	1.30	2.000	Yes
1174	11.74	0.70	0.12	0.58	0.98	0.563	1.06	0.533	1.00	1.30	0.693	No
1175	11.75	0.70	0.12	0.58	0.98	0.563	1.06	0.533	1.00	1.30	0.693	No
1176	11.76	0.70	0.12	0.58	0.98	0.563	1.06	0.533	1.00	1.30	0.693	No
1177	11.77	0.70	0.12	0.58	0.98	0.564	1.06	0.533	1.00	1.30	0.693	No
1178	11.78	0.70	0.12	0.59	0.98	0.564	1.06	0.534	1.00	1.30	0.694	No
1179	11.79	0.70	0.12	0.59	0.98	0.564	1.06	0.534	1.00	1.30	0.694	No
1180	11.80	0.70	0.12	0.59	0.98	0.564	1.06	0.534	1.00	1.30	0.694	No
1181	11.81	0.70	0.12	0.59	0.98	0.564	1.06	0.534	1.00	1.30	0.694	No
1182	11.82	0.71	0.12	0.59	0.98	0.564	1.06	0.534	1.00	1.30	0.695	No
1183	11.83	0.71	0.12	0.59	0.98	0.565	1.06	0.535	1.00	1.30	0.695	No
1184	11.84	0.71	0.12	0.59	0.98	0.565	1.06	0.535	1.00	1.30	0.695	No
1185	11.85	0.71	0.12	0.59	0.98	0.565	1.06	0.535	1.00	1.30	0.695	No
1186	11.86	0.71	0.12	0.59	0.98	0.565	1.06	0.535	1.00	1.30	0.696	No
1187	11.87	0.71	0.12	0.59	0.98	0.565	1.06	0.535	1.00	1.30	0.696	No
1188	11.88	0.71	0.12	0.59	0.98	0.566	1.06	0.535	1.00	1.30	0.696	No
1189	11.89	0.71	0.12	0.59	0.98	0.566	1.06	0.536	1.00	1.30	0.696	No
1190	11.90	0.71	0.12	0.59	0.98	0.566	1.06	0.536	1.00	1.30	0.697	No
1191	11.91	0.71	0.12	0.59	0.98	0.566	1.06	0.536	1.00	1.30	0.697	No
1192	11.92	0.71	0.12	0.59	0.98	0.566	1.06	0.536	1.00	1.30	0.697	No
1193	11.93	0.71	0.12	0.59	0.98	0.567	1.06	0.536	1.00	1.30	0.697	No
1194	11.94	0.71	0.12	0.59	0.98	0.567	1.06	0.537	1.00	1.30	0.697	No
1195	11.95	0.71	0.12	0.59	0.98	0.567	1.06	0.537	1.00	1.30	0.698	No
1196	11.96	0.71	0.12	0.59	0.98	0.567	1.06	0.537	1.00	1.30	0.698	No
1197	11.97	0.71	0.12	0.59	0.97	0.567	1.06	0.537	1.00	1.30	0.698	No
1198	11.98	0.71	0.12	0.59	0.97	0.568	1.06	0.537	1.00	1.30	0.698	No
1199	11.99	0.72	0.12	0.59	0.97	0.568	1.06	0.537	1.00	1.30	0.699	No
1200	12.00	0.72	0.12	0.59	0.97	0.568	1.06	0.538	1.00	1.30	0.699	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1201	12.01	0.72	0.13	0.59	0.97	0.568	1.06	0.538	1.00	1.30	0.699	No
1202	12.02	0.72	0.13	0.59	0.97	0.568	1.06	0.538	1.00	1.30	0.699	No
1203	12.03	0.72	0.13	0.59	0.97	0.568	1.06	0.538	1.00	1.30	0.700	No
1204	12.04	0.72	0.13	0.59	0.97	0.569	1.06	0.538	1.00	1.30	0.700	No
1205	12.05	0.72	0.13	0.59	0.97	0.569	1.06	0.539	1.00	1.30	0.700	No
1206	12.06	0.72	0.13	0.59	0.97	0.569	1.06	0.539	1.00	1.30	0.700	No
1207	12.07	0.72	0.13	0.59	0.97	0.569	1.06	0.539	1.00	1.30	0.701	No
1208	12.08	0.72	0.13	0.59	0.97	0.569	1.06	0.539	1.00	1.30	0.701	No
1209	12.09	0.72	0.13	0.59	0.97	0.570	1.06	0.539	1.00	1.30	0.701	No
1210	12.10	0.72	0.13	0.59	0.97	0.570	1.06	0.539	1.00	1.30	0.701	No
1211	12.11	0.72	0.13	0.59	0.97	0.570	1.06	0.540	1.00	1.30	0.701	No
1212	12.12	0.72	0.13	0.59	0.97	0.570	1.06	0.540	1.00	1.30	0.702	No
1213	12.13	0.72	0.13	0.59	0.97	0.570	1.06	0.540	1.00	1.30	0.702	No
1214	12.14	0.72	0.13	0.59	0.97	0.571	1.06	0.540	1.00	1.30	0.702	No
1215	12.15	0.72	0.13	0.60	0.97	0.571	1.06	0.540	1.00	1.30	0.702	No
1216	12.16	0.73	0.13	0.60	0.97	0.571	1.06	0.541	1.00	1.30	0.703	No
1217	12.17	0.73	0.13	0.60	0.97	0.571	1.06	0.541	1.00	1.30	0.703	No
1218	12.18	0.73	0.13	0.60	0.97	0.571	1.06	0.541	1.00	1.30	0.703	No
1219	12.19	0.73	0.13	0.60	0.97	0.572	1.06	0.541	1.00	1.30	0.703	No
1220	12.20	0.73	0.13	0.60	0.97	0.572	1.06	0.541	1.00	1.30	0.704	No
1221	12.21	0.73	0.13	0.60	0.97	0.572	1.06	0.541	1.00	1.30	0.704	No
1222	12.22	0.73	0.13	0.60	0.97	0.572	1.06	0.542	1.00	1.30	0.704	No
1223	12.23	0.73	0.13	0.60	0.97	0.572	1.06	0.542	1.00	1.30	0.704	No
1224	12.24	0.73	0.13	0.60	0.97	0.573	1.06	0.542	1.00	1.30	0.705	No
1225	12.25	0.73	0.13	0.60	0.97	0.573	1.06	0.542	1.00	1.30	0.705	No
1226	12.26	0.73	0.13	0.60	0.97	0.573	1.06	0.542	1.00	1.30	0.705	No
1227	12.27	0.73	0.13	0.60	0.97	0.573	1.06	0.543	1.00	1.30	0.705	No
1228	12.28	0.73	0.13	0.60	0.97	0.573	1.06	0.543	1.00	1.30	0.705	No
1229	12.29	0.73	0.13	0.60	0.97	0.573	1.06	0.543	1.00	1.30	0.706	No
1230	12.30	0.73	0.13	0.60	0.97	0.574	1.06	0.543	1.00	1.30	0.706	No
1231	12.31	0.73	0.13	0.60	0.97	0.574	1.06	0.543	1.00	1.30	0.706	No
1232	12.32	0.73	0.13	0.60	0.97	0.574	1.06	0.543	1.00	1.30	0.706	No
1233	12.33	0.73	0.14	0.60	0.97	0.574	1.06	0.544	1.00	1.30	0.707	No
1234	12.34	0.73	0.14	0.60	0.97	0.574	1.06	0.544	1.00	1.30	0.707	No
1235	12.35	0.74	0.14	0.60	0.97	0.575	1.06	0.544	1.00	1.30	0.707	No
1236	12.36	0.74	0.14	0.60	0.97	0.575	1.06	0.544	1.00	1.30	0.707	No
1237	12.37	0.74	0.14	0.60	0.97	0.575	1.06	0.544	1.00	1.30	0.708	No
1238	12.38	0.74	0.14	0.60	0.97	0.575	1.06	0.544	1.00	1.30	0.708	No
1239	12.39	0.74	0.14	0.60	0.97	0.575	1.06	0.545	1.00	1.30	0.708	No
1240	12.40	0.74	0.14	0.60	0.97	0.576	1.06	0.545	1.00	1.30	0.708	No
1241	12.41	0.74	0.14	0.60	0.97	0.576	1.06	0.545	1.00	1.30	0.709	No
1242	12.42	0.74	0.14	0.60	0.97	0.576	1.06	0.545	1.00	1.30	0.709	No
1243	12.43	0.74	0.14	0.60	0.97	0.576	1.06	0.545	1.00	1.30	0.709	No
1244	12.44	0.74	0.14	0.60	0.97	0.576	1.06	0.546	1.00	1.30	0.709	No
1245	12.45	0.74	0.14	0.60	0.97	0.577	1.06	0.546	1.00	1.30	0.709	No
1246	12.46	0.74	0.14	0.60	0.97	0.577	1.06	0.546	1.00	1.30	0.710	No
1247	12.47	0.74	0.14	0.60	0.97	0.577	1.06	0.546	1.00	1.30	0.710	No
1248	12.48	0.74	0.14	0.60	0.97	0.577	1.06	0.546	1.00	1.30	0.710	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1249	12.49	0.74	0.14	0.60	0.97	0.577	1.06	0.546	1.00	1.30	0.710	No
1250	12.50	0.74	0.14	0.60	0.97	0.577	1.06	0.547	1.00	1.30	0.711	No
1251	12.51	0.74	0.14	0.60	0.97	0.578	1.06	0.547	1.00	1.30	0.711	No
1252	12.52	0.74	0.14	0.60	0.97	0.578	1.06	0.547	1.00	1.30	0.711	No
1253	12.53	0.75	0.14	0.60	0.97	0.578	1.06	0.547	1.00	1.30	0.711	No
1254	12.54	0.75	0.14	0.60	0.97	0.578	1.06	0.547	1.00	1.30	0.712	No
1255	12.55	0.75	0.14	0.60	0.97	0.578	1.06	0.548	1.00	1.30	0.712	No
1256	12.56	0.75	0.14	0.60	0.97	0.579	1.06	0.548	1.00	1.30	0.712	No
1257	12.57	0.75	0.14	0.60	0.97	0.579	1.06	0.548	1.00	1.30	0.712	No
1258	12.58	0.75	0.14	0.60	0.97	0.579	1.06	0.548	1.00	1.30	0.713	No
1259	12.59	0.75	0.14	0.61	0.97	0.579	1.06	0.548	1.00	1.30	0.713	No
1260	12.60	0.75	0.14	0.61	0.97	0.579	1.06	0.548	1.00	1.30	0.713	No
1261	12.61	0.75	0.14	0.61	0.97	0.580	1.06	0.549	1.00	1.30	0.713	No
1262	12.62	0.75	0.14	0.61	0.97	0.580	1.06	0.549	1.00	1.30	0.713	No
1263	12.63	0.75	0.14	0.61	0.97	0.580	1.06	0.549	1.00	1.30	0.714	No
1264	12.64	0.75	0.14	0.61	0.97	0.580	1.06	0.549	1.00	1.30	0.714	No
1265	12.65	0.75	0.15	0.61	0.97	0.580	1.06	0.549	1.00	1.30	0.714	No
1266	12.66	0.75	0.15	0.61	0.97	0.581	1.06	0.550	1.00	1.30	0.714	No
1267	12.67	0.75	0.15	0.61	0.97	0.581	1.06	0.550	1.00	1.30	0.715	No
1268	12.68	0.75	0.15	0.61	0.97	0.581	1.06	0.550	1.00	1.30	0.715	No
1269	12.69	0.75	0.15	0.61	0.97	0.581	1.06	0.550	1.00	1.30	0.715	No
1270	12.70	0.75	0.15	0.61	0.97	0.581	1.06	0.550	1.00	1.30	0.715	No
1271	12.71	0.75	0.15	0.61	0.97	0.581	1.06	0.550	1.00	1.30	0.716	No
1272	12.72	0.76	0.15	0.61	0.97	0.582	1.06	0.551	1.00	1.30	0.716	No
1273	12.73	0.76	0.15	0.61	0.97	0.582	1.06	0.551	1.00	1.30	0.716	No
1274	12.74	0.76	0.15	0.61	0.97	0.582	1.06	0.551	1.00	1.30	0.716	No
1275	12.75	0.76	0.15	0.61	0.97	0.582	1.06	0.551	1.00	1.30	0.716	No
1276	12.76	0.76	0.15	0.61	0.97	0.582	1.06	0.551	1.00	1.30	0.717	No
1277	12.77	0.76	0.15	0.61	0.97	0.583	1.06	0.551	1.00	1.30	0.717	No
1278	12.78	0.76	0.15	0.61	0.97	0.583	1.06	0.552	1.00	1.30	0.717	No
1279	12.79	0.76	0.15	0.61	0.97	0.583	1.06	0.552	1.00	1.30	0.717	No
1280	12.80	0.76	0.15	0.61	0.97	0.583	1.06	0.552	1.00	1.30	0.718	No
1281	12.81	0.76	0.15	0.61	0.97	0.583	1.06	0.552	1.00	1.30	0.718	No
1282	12.82	0.76	0.15	0.61	0.97	0.584	1.06	0.552	1.00	1.30	0.718	No
1283	12.83	0.76	0.15	0.61	0.97	0.584	1.06	0.553	1.00	1.30	0.718	No
1284	12.84	0.76	0.15	0.61	0.97	0.584	1.06	0.553	1.00	1.30	0.719	No
1285	12.85	0.76	0.15	0.61	0.97	0.584	1.06	0.553	1.00	1.30	0.719	No
1286	12.86	0.76	0.15	0.61	0.97	0.584	1.06	0.553	1.00	1.30	0.719	No
1287	12.87	0.76	0.15	0.61	0.97	0.584	1.06	0.553	1.00	1.30	0.719	No
1288	12.88	0.76	0.15	0.61	0.97	0.585	1.06	0.553	1.00	1.30	0.719	No
1289	12.89	0.76	0.15	0.61	0.97	0.585	1.06	0.554	1.00	1.30	0.720	No
1290	12.90	0.76	0.15	0.61	0.97	0.585	1.06	0.554	1.00	1.30	0.720	No
1291	12.91	0.76	0.15	0.61	0.97	0.585	1.06	0.554	1.00	1.30	0.720	No
1292	12.92	0.77	0.15	0.61	0.97	0.585	1.06	0.554	1.00	1.30	0.720	No
1293	12.93	0.77	0.15	0.61	0.97	0.586	1.06	0.554	1.00	1.30	0.721	No
1294	12.94	0.77	0.15	0.61	0.97	0.586	1.06	0.555	1.00	1.30	0.721	No
1295	12.95	0.77	0.15	0.61	0.97	0.586	1.06	0.555	1.00	1.30	0.721	No
1296	12.96	0.77	0.15	0.61	0.97	0.586	1.06	0.555	1.00	1.30	0.721	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1297	12.97	0.77	0.16	0.61	0.97	0.586	1.06	0.555	1.00	1.30	0.722	No
1298	12.98	0.77	0.16	0.61	0.97	0.587	1.06	0.555	1.00	1.30	0.722	No
1299	12.99	0.77	0.16	0.61	0.97	0.587	1.06	0.555	1.00	1.30	0.722	No
1300	13.00	0.77	0.16	0.61	0.97	0.587	1.06	0.556	1.00	1.30	0.722	No
1301	13.01	0.77	0.16	0.61	0.97	0.587	1.06	0.556	1.00	1.30	0.722	No
1302	13.02	0.77	0.16	0.61	0.97	0.587	1.06	0.556	1.00	1.30	0.723	No
1303	13.03	0.77	0.16	0.61	0.97	0.587	1.06	0.556	1.00	1.30	0.723	No
1304	13.04	0.77	0.16	0.61	0.97	0.588	1.06	0.556	1.00	1.30	0.723	No
1305	13.05	0.77	0.16	0.61	0.97	0.588	1.06	0.556	1.00	1.30	0.723	No
1306	13.06	0.77	0.16	0.61	0.97	0.588	1.06	0.557	1.00	1.30	0.724	No
1307	13.07	0.77	0.16	0.62	0.97	0.588	1.06	0.557	1.00	1.30	0.724	No
1308	13.08	0.77	0.16	0.62	0.97	0.588	1.06	0.557	1.00	1.30	0.724	No
1309	13.09	0.77	0.16	0.62	0.97	0.589	1.06	0.557	1.00	1.30	0.724	No
1310	13.10	0.77	0.16	0.62	0.97	0.589	1.06	0.557	1.00	1.30	0.725	No
1311	13.11	0.78	0.16	0.62	0.97	0.589	1.06	0.558	1.00	1.30	0.725	No
1312	13.12	0.78	0.16	0.62	0.97	0.589	1.06	0.558	1.00	1.30	0.725	No
1313	13.13	0.78	0.16	0.62	0.97	0.589	1.06	0.558	1.00	1.30	0.725	No
1314	13.14	0.78	0.16	0.62	0.97	0.590	1.06	0.558	1.00	1.30	0.725	No
1315	13.15	0.78	0.16	0.62	0.97	0.590	1.06	0.558	1.00	1.30	0.726	No
1316	13.16	0.78	0.16	0.62	0.97	0.590	1.06	0.558	1.00	1.30	0.726	No
1317	13.17	0.78	0.16	0.62	0.97	0.590	1.06	0.559	1.00	1.30	0.726	No
1318	13.18	0.78	0.16	0.62	0.97	0.590	1.06	0.559	1.00	1.30	0.726	No
1319	13.19	0.78	0.16	0.62	0.97	0.590	1.06	0.559	1.00	1.30	0.727	No
1320	13.20	0.78	0.16	0.62	0.97	0.591	1.06	0.559	1.00	1.30	0.727	No
1321	13.21	0.78	0.16	0.62	0.97	0.591	1.06	0.559	1.00	1.30	0.727	No
1322	13.22	0.78	0.16	0.62	0.97	0.591	1.06	0.559	1.00	1.30	0.727	No
1323	13.23	0.78	0.16	0.62	0.97	0.591	1.06	0.560	1.00	1.30	0.728	No
1324	13.24	0.78	0.16	0.62	0.97	0.591	1.06	0.560	1.00	1.30	0.728	No
1325	13.25	0.78	0.16	0.62	0.97	0.592	1.06	0.560	1.00	1.30	0.728	No
1326	13.26	0.78	0.16	0.62	0.97	0.592	1.06	0.560	1.00	1.30	0.728	No
1327	13.27	0.78	0.16	0.62	0.97	0.592	1.06	0.560	1.00	1.30	0.729	No
1328	13.28	0.78	0.16	0.62	0.97	0.592	1.06	0.561	1.00	1.30	0.729	No
1329	13.29	0.78	0.17	0.62	0.97	0.592	1.06	0.561	1.00	1.30	0.729	No
1330	13.30	0.78	0.17	0.62	0.97	0.593	1.06	0.561	1.00	1.30	0.729	No
1331	13.31	0.78	0.17	0.62	0.97	0.593	1.06	0.561	1.00	1.30	0.729	No
1332	13.32	0.79	0.17	0.62	0.97	0.593	1.06	0.561	1.00	1.30	0.730	No
1333	13.33	0.79	0.17	0.62	0.97	0.593	1.06	0.562	1.00	1.30	0.730	No
1334	13.34	0.79	0.17	0.62	0.97	0.593	1.06	0.562	1.00	1.30	0.730	No
1335	13.35	0.79	0.17	0.62	0.97	0.594	1.06	0.562	1.00	1.30	0.730	No
1336	13.36	0.79	0.17	0.62	0.97	0.594	1.06	0.562	1.00	1.30	0.731	No
1337	13.37	0.79	0.17	0.62	0.97	0.594	1.06	0.562	1.00	1.30	0.731	No
1338	13.38	0.79	0.17	0.62	0.97	0.594	1.06	0.562	1.00	1.30	0.731	No
1339	13.39	0.79	0.17	0.62	0.97	0.594	1.06	0.563	1.00	1.30	0.731	No
1340	13.40	0.79	0.17	0.62	0.97	0.595	1.06	0.563	1.00	1.30	0.732	No
1341	13.41	0.79	0.17	0.62	0.97	0.595	1.06	0.563	1.00	1.30	0.732	No
1342	13.42	0.79	0.17	0.62	0.97	0.595	1.06	0.563	1.00	1.30	0.732	No
1343	13.43	0.79	0.17	0.62	0.97	0.595	1.06	0.563	1.00	1.30	0.732	No
1344	13.44	0.79	0.17	0.62	0.97	0.595	1.06	0.564	1.00	1.30	0.733	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1345	13.45	0.79	0.17	0.62	0.97	0.595	1.06	0.564	1.00	1.30	0.733	No
1346	13.46	0.79	0.17	0.62	0.97	0.596	1.06	0.564	1.00	1.30	0.733	No
1347	13.47	0.79	0.17	0.62	0.97	0.596	1.06	0.564	1.00	1.30	0.733	No
1348	13.48	0.79	0.17	0.62	0.97	0.596	1.06	0.564	1.00	1.30	0.733	No
1349	13.49	0.79	0.17	0.62	0.97	0.596	1.06	0.564	1.00	1.30	0.734	No
1350	13.50	0.79	0.17	0.62	0.97	0.596	1.06	0.565	1.00	1.30	0.734	No
1351	13.51	0.79	0.17	0.62	0.97	0.597	1.06	0.565	1.00	1.30	0.734	No
1352	13.52	0.79	0.17	0.62	0.97	0.597	1.06	0.565	1.00	1.30	0.734	No
1353	13.53	0.79	0.17	0.62	0.97	0.597	1.06	0.565	1.00	1.30	0.735	No
1354	13.54	0.80	0.17	0.62	0.97	0.597	1.06	0.565	1.00	1.30	0.735	No
1355	13.55	0.80	0.17	0.62	0.97	0.597	1.06	0.565	1.00	1.30	0.735	No
1356	13.56	0.80	0.17	0.62	0.97	0.597	1.06	0.566	1.00	1.30	0.735	No
1357	13.57	0.80	0.17	0.62	0.97	0.598	1.06	0.566	1.00	1.30	0.736	No
1358	13.58	0.80	0.17	0.62	0.97	0.598	1.06	0.566	1.00	1.30	0.736	No
1359	13.59	0.80	0.17	0.62	0.97	0.598	1.06	0.566	1.00	1.30	0.736	No
1360	13.60	0.80	0.17	0.62	0.97	0.598	1.06	0.566	1.00	1.30	0.736	No
1361	13.61	0.80	0.18	0.62	0.97	0.598	1.06	0.566	1.00	1.30	0.736	No
1362	13.62	0.80	0.18	0.62	0.97	0.599	1.06	0.567	1.00	1.30	0.737	No
1363	13.63	0.80	0.18	0.62	0.97	0.599	1.06	0.567	1.00	1.30	0.737	No
1364	13.64	0.80	0.18	0.62	0.97	0.599	1.06	0.567	1.00	1.30	0.737	No
1365	13.65	0.80	0.18	0.62	0.97	0.599	1.06	0.567	1.00	1.30	0.737	No
1366	13.66	0.80	0.18	0.62	0.97	0.599	1.06	0.567	1.00	1.30	0.738	No
1367	13.67	0.80	0.18	0.63	0.97	0.599	1.06	0.567	1.00	1.30	0.738	No
1368	13.68	0.80	0.18	0.63	0.97	0.600	1.06	0.568	1.00	1.30	0.738	No
1369	13.69	0.80	0.18	0.63	0.97	0.600	1.06	0.568	1.00	1.30	0.738	No
1370	13.70	0.80	0.18	0.63	0.97	0.600	1.06	0.568	1.00	1.30	0.738	No
1371	13.71	0.80	0.18	0.63	0.97	0.600	1.06	0.568	1.00	1.30	0.739	No
1372	13.72	0.80	0.18	0.63	0.97	0.600	1.06	0.568	1.00	1.30	0.739	No
1373	13.73	0.81	0.18	0.63	0.97	0.601	1.06	0.568	1.00	1.30	0.739	No
1374	13.74	0.81	0.18	0.63	0.97	0.601	1.06	0.569	1.00	1.30	0.739	No
1375	13.75	0.81	0.18	0.63	0.97	0.601	1.06	0.569	1.00	1.30	0.739	No
1376	13.76	0.81	0.18	0.63	0.97	0.601	1.06	0.569	1.00	1.30	0.740	No
1377	13.77	0.81	0.18	0.63	0.97	0.601	1.06	0.569	1.00	1.30	0.740	No
1378	13.78	0.81	0.18	0.63	0.97	0.601	1.06	0.569	1.00	1.30	0.740	No
1379	13.79	0.81	0.18	0.63	0.97	0.602	1.06	0.570	1.00	1.30	0.740	No
1380	13.80	0.81	0.18	0.63	0.97	0.602	1.06	0.570	1.00	1.30	0.741	No
1381	13.81	0.81	0.18	0.63	0.97	0.602	1.06	0.570	1.00	1.30	0.741	No
1382	13.82	0.81	0.18	0.63	0.97	0.602	1.06	0.570	1.00	1.30	0.741	No
1383	13.83	0.81	0.18	0.63	0.97	0.602	1.06	0.570	1.00	1.30	0.741	No
1384	13.84	0.81	0.18	0.63	0.97	0.602	1.06	0.570	1.00	1.30	0.741	No
1385	13.85	0.81	0.18	0.63	0.97	0.603	1.06	0.570	1.00	1.30	0.742	No
1386	13.86	0.81	0.18	0.63	0.97	0.603	1.06	0.571	1.00	1.30	0.742	No
1387	13.87	0.81	0.18	0.63	0.97	0.603	1.06	0.571	1.00	1.30	0.742	No
1388	13.88	0.81	0.18	0.63	0.97	0.603	1.06	0.571	1.00	1.30	0.742	No
1389	13.89	0.81	0.18	0.63	0.97	0.603	1.06	0.571	1.00	1.30	0.743	No
1390	13.90	0.81	0.18	0.63	0.97	0.604	1.06	0.571	1.00	1.30	0.743	No
1391	13.91	0.81	0.18	0.63	0.97	0.604	1.06	0.571	1.00	1.30	0.743	No
1392	13.92	0.81	0.18	0.63	0.97	0.604	1.06	0.572	1.00	1.30	0.743	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1393	13.93	0.82	0.19	0.63	0.97	0.604	1.06	0.572	1.00	1.30	0.743	No
1394	13.94	0.82	0.19	0.63	0.97	0.604	1.06	0.572	1.00	1.30	0.744	No
1395	13.95	0.82	0.19	0.63	0.97	0.604	1.06	0.572	1.00	1.30	0.744	No
1396	13.96	0.82	0.19	0.63	0.97	0.605	1.06	0.572	1.00	1.30	0.744	No
1397	13.97	0.82	0.19	0.63	0.97	0.605	1.06	0.573	1.00	1.30	0.744	No
1398	13.98	0.82	0.19	0.63	0.97	0.605	1.06	0.573	1.00	1.30	0.744	No
1399	13.99	0.82	0.19	0.63	0.97	0.605	1.06	0.573	1.00	1.30	0.745	No
1400	14.00	0.82	0.19	0.63	0.97	0.605	1.06	0.573	1.00	1.30	0.745	No
1401	14.01	0.82	0.19	0.63	0.97	0.605	1.06	0.573	1.00	1.30	0.745	No
1402	14.02	0.82	0.19	0.63	0.97	0.606	1.06	0.573	1.00	1.30	0.745	No
1403	14.03	0.82	0.19	0.63	0.97	0.606	1.06	0.574	1.00	1.30	0.746	No
1404	14.04	0.82	0.19	0.63	0.97	0.606	1.06	0.574	1.00	1.30	0.746	No
1405	14.05	0.82	0.19	0.63	0.97	0.606	1.06	0.574	1.00	1.30	0.746	No
1406	14.06	0.82	0.19	0.63	0.97	0.606	1.06	0.574	1.00	1.30	0.746	No
1407	14.07	0.82	0.19	0.63	0.97	0.607	1.06	0.574	1.00	1.30	0.746	No
1408	14.08	0.82	0.19	0.63	0.97	0.607	1.06	0.574	1.00	1.30	0.747	No
1409	14.09	0.82	0.19	0.63	0.97	0.607	1.06	0.575	1.00	1.30	0.747	No
1410	14.10	0.82	0.19	0.63	0.97	0.607	1.06	0.575	1.00	1.30	0.747	No
1411	14.11	0.82	0.19	0.63	0.97	0.607	1.06	0.575	1.00	1.30	0.747	No
1412	14.12	0.82	0.19	0.63	0.97	0.607	1.06	0.575	1.00	1.30	0.748	No
1413	14.13	0.83	0.19	0.63	0.97	0.608	1.06	0.575	1.00	1.30	0.748	No
1414	14.14	0.83	0.19	0.63	0.97	0.608	1.06	0.575	1.00	1.30	0.748	No
1415	14.15	0.83	0.19	0.63	0.97	0.608	1.06	0.575	1.00	1.30	0.748	No
1416	14.16	0.83	0.19	0.63	0.97	0.608	1.06	0.576	1.00	1.30	0.748	No
1417	14.17	0.83	0.19	0.63	0.97	0.608	1.06	0.576	1.00	1.30	0.749	No
1418	14.18	0.83	0.19	0.63	0.97	0.608	1.06	0.576	1.00	1.30	0.749	No
1419	14.19	0.83	0.19	0.64	0.97	0.609	1.06	0.576	1.00	1.30	0.749	No
1420	14.20	0.83	0.19	0.64	0.97	0.609	1.06	0.576	1.00	1.30	0.749	No
1421	14.21	0.83	0.19	0.64	0.97	0.609	1.06	0.576	1.00	1.30	0.749	No
1422	14.22	0.83	0.19	0.64	0.97	0.609	1.06	0.577	1.00	1.30	0.750	No
1423	14.23	0.83	0.19	0.64	0.97	0.609	1.06	0.577	1.00	1.30	0.750	No
1424	14.24	0.83	0.19	0.64	0.97	0.609	1.06	0.577	1.00	1.30	0.750	No
1425	14.25	0.83	0.20	0.64	0.97	0.610	1.06	0.577	1.00	1.30	0.750	No
1426	14.26	0.83	0.20	0.64	0.97	0.610	1.06	0.577	1.00	1.30	0.750	No
1427	14.27	0.83	0.20	0.64	0.97	0.610	1.06	0.577	1.00	1.30	0.751	No
1428	14.28	0.83	0.20	0.64	0.97	0.610	1.06	0.578	1.00	1.30	0.751	No
1429	14.29	0.83	0.20	0.64	0.97	0.610	1.06	0.578	1.00	1.30	0.751	No
1430	14.30	0.83	0.20	0.64	0.97	0.610	1.06	0.578	1.00	1.30	0.751	No
1431	14.31	0.83	0.20	0.64	0.97	0.611	1.06	0.578	1.00	1.30	0.751	No
1432	14.32	0.84	0.20	0.64	0.97	0.611	1.06	0.578	1.00	1.30	0.752	No
1433	14.33	0.84	0.20	0.64	0.97	0.611	1.06	0.578	1.00	1.30	0.752	No
1434	14.34	0.84	0.20	0.64	0.97	0.611	1.06	0.578	1.00	1.30	0.752	No
1435	14.35	0.84	0.20	0.64	0.97	0.611	1.06	0.579	1.00	1.30	0.752	No
1436	14.36	0.84	0.20	0.64	0.97	0.611	1.06	0.579	1.00	1.30	0.752	No
1437	14.37	0.84	0.20	0.64	0.97	0.612	1.06	0.579	1.00	1.30	0.753	No
1438	14.38	0.84	0.20	0.64	0.97	0.612	1.06	0.579	1.00	1.30	0.753	No
1439	14.39	0.84	0.20	0.64	0.97	0.612	1.06	0.579	1.00	1.30	0.753	No
1440	14.40	0.84	0.20	0.64	0.97	0.612	1.06	0.579	1.00	1.30	0.753	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1441	14.41	0.84	0.20	0.64	0.97	0.612	1.06	0.580	1.00	1.30	0.753	No
1442	14.42	0.84	0.20	0.64	0.97	0.612	1.06	0.580	1.00	1.30	0.754	No
1443	14.43	0.84	0.20	0.64	0.97	0.613	1.06	0.580	1.00	1.30	0.754	No
1444	14.44	0.84	0.20	0.64	0.97	0.613	1.06	0.580	1.00	1.30	0.754	No
1445	14.45	0.84	0.20	0.64	0.97	0.613	1.06	0.580	1.00	1.30	0.754	No
1446	14.46	0.84	0.20	0.64	0.97	0.613	1.06	0.580	1.00	1.30	0.754	No
1447	14.47	0.84	0.20	0.64	0.97	0.613	1.06	0.580	1.00	1.30	0.755	No
1448	14.48	0.84	0.20	0.64	0.97	0.613	1.06	0.581	1.00	1.30	0.755	No
1449	14.49	0.84	0.20	0.64	0.97	0.613	1.06	0.581	1.00	1.30	0.755	No
1450	14.50	0.85	0.20	0.64	0.97	0.614	1.06	0.581	1.00	1.30	0.755	No
1451	14.51	0.85	0.20	0.64	0.97	0.614	1.06	0.581	1.00	1.30	0.755	No
1452	14.52	0.85	0.20	0.64	0.97	0.614	1.06	0.581	1.00	1.30	0.756	No
1453	14.53	0.85	0.20	0.64	0.97	0.614	1.06	0.581	1.00	1.30	0.756	No
1454	14.54	0.85	0.20	0.64	0.97	0.614	1.06	0.581	1.00	1.30	0.756	No
1455	14.55	0.85	0.20	0.64	0.97	0.614	1.06	0.582	1.00	1.30	0.756	No
1456	14.56	0.85	0.20	0.64	0.97	0.615	1.06	0.582	1.00	1.30	0.756	No
1457	14.57	0.85	0.20	0.64	0.97	0.615	1.06	0.582	1.00	1.30	0.756	No
1458	14.58	0.85	0.21	0.64	0.97	0.615	1.06	0.582	1.00	1.30	0.757	No
1459	14.59	0.85	0.21	0.64	0.97	0.615	1.06	0.582	1.00	1.30	0.757	No
1460	14.60	0.85	0.21	0.64	0.97	0.615	1.06	0.582	1.00	1.30	0.757	No
1461	14.61	0.85	0.21	0.65	0.97	0.615	1.06	0.583	1.00	1.30	0.757	No
1462	14.62	0.85	0.21	0.65	0.97	0.616	1.06	0.583	1.00	1.30	0.757	No
1463	14.63	0.85	0.21	0.65	0.97	0.616	1.06	0.583	1.00	1.30	0.758	No
1464	14.64	0.85	0.21	0.65	0.97	0.616	1.06	0.583	1.00	1.30	0.758	No
1465	14.65	0.85	0.21	0.65	0.97	0.616	1.06	0.583	1.00	1.30	0.758	No
1466	14.66	0.85	0.21	0.65	0.97	0.616	1.06	0.583	1.00	1.30	0.758	No
1467	14.67	0.85	0.21	0.65	0.97	0.616	1.06	0.583	1.00	1.30	0.758	No
1468	14.68	0.86	0.21	0.65	0.97	0.616	1.06	0.584	1.00	1.30	0.759	No
1469	14.69	0.86	0.21	0.65	0.97	0.617	1.06	0.584	1.00	1.30	0.759	No
1470	14.70	0.86	0.21	0.65	0.97	0.617	1.06	0.584	1.00	1.30	0.759	No
1471	14.71	0.86	0.21	0.65	0.97	0.617	1.06	0.584	1.00	1.30	0.759	No
1472	14.72	0.86	0.21	0.65	0.97	0.617	1.06	0.584	1.00	1.30	0.759	No
1473	14.73	0.86	0.21	0.65	0.97	0.617	1.06	0.584	1.00	1.30	0.760	No
1474	14.74	0.86	0.21	0.65	0.97	0.617	1.06	0.584	1.00	1.30	0.760	No
1475	14.75	0.86	0.21	0.65	0.97	0.618	1.06	0.585	1.00	1.30	0.760	No
1476	14.76	0.86	0.21	0.65	0.97	0.618	1.06	0.585	1.00	1.30	0.760	No
1477	14.77	0.86	0.21	0.65	0.97	0.618	1.06	0.585	1.00	1.30	0.760	No
1478	14.78	0.86	0.21	0.65	0.97	0.618	1.06	0.585	1.00	1.30	0.761	No
1479	14.79	0.86	0.21	0.65	0.97	0.618	1.06	0.585	1.00	1.30	0.761	No
1480	14.80	0.86	0.21	0.65	0.97	0.618	1.06	0.585	1.00	1.30	0.761	No
1481	14.81	0.86	0.21	0.65	0.97	0.619	1.06	0.586	1.00	1.30	0.761	No
1482	14.82	0.86	0.21	0.65	0.97	0.619	1.06	0.586	1.00	1.30	0.761	No
1483	14.83	0.86	0.21	0.65	0.97	0.619	1.06	0.586	1.00	1.30	0.762	No
1484	14.84	0.86	0.21	0.65	0.97	0.619	1.06	0.586	1.00	1.30	0.762	No
1485	14.85	0.86	0.21	0.65	0.97	0.619	1.06	0.586	1.00	1.30	0.762	No
1486	14.86	0.86	0.21	0.65	0.97	0.619	1.06	0.586	1.00	1.30	0.762	No
1487	14.87	0.87	0.21	0.65	0.97	0.619	1.06	0.586	1.00	1.30	0.762	No
1488	14.88	0.87	0.21	0.65	0.97	0.620	1.06	0.587	1.00	1.30	0.763	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1489	14.89	0.87	0.21	0.65	0.97	0.620	1.06	0.587	1.00	1.30	0.763	No
1490	14.90	0.87	0.22	0.65	0.97	0.620	1.06	0.587	1.00	1.30	0.763	No
1491	14.91	0.87	0.22	0.65	0.97	0.620	1.06	0.587	1.00	1.30	0.763	No
1492	14.92	0.87	0.22	0.65	0.97	0.620	1.06	0.587	1.00	1.30	0.763	No
1493	14.93	0.87	0.22	0.65	0.97	0.620	1.06	0.587	1.00	1.30	0.763	No
1494	14.94	0.87	0.22	0.65	0.97	0.621	1.06	0.587	1.00	1.30	0.764	No
1495	14.95	0.87	0.22	0.65	0.97	0.621	1.06	0.588	1.00	1.30	0.764	No
1496	14.96	0.87	0.22	0.65	0.97	0.621	1.06	0.588	1.00	1.30	0.764	No
1497	14.97	0.87	0.22	0.65	0.97	0.621	1.06	0.588	1.00	1.30	0.764	No
1498	14.98	0.87	0.22	0.65	0.97	0.621	1.06	0.588	1.00	1.30	0.764	No
1499	14.99	0.87	0.22	0.65	0.97	0.621	1.06	0.588	1.00	1.30	0.765	No
1500	15.00	0.87	0.22	0.65	0.97	0.621	1.06	0.588	1.00	1.30	0.765	No
1501	15.01	0.87	0.22	0.65	0.97	0.622	1.06	0.588	1.00	1.30	0.765	No
1502	15.02	0.87	0.22	0.65	0.97	0.622	1.06	0.589	1.00	1.30	0.765	No
1503	15.03	0.87	0.22	0.65	0.97	0.622	1.06	0.589	1.00	1.30	0.765	No
1504	15.04	0.87	0.22	0.65	0.97	0.622	1.06	0.589	1.00	1.30	0.766	No
1505	15.05	0.88	0.22	0.66	0.97	0.622	1.06	0.589	1.00	1.30	0.766	No
1506	15.06	0.88	0.22	0.66	0.97	0.622	1.06	0.589	1.00	1.30	0.766	No
1507	15.07	0.88	0.22	0.66	0.97	0.623	1.06	0.589	1.00	1.30	0.766	No
1508	15.08	0.88	0.22	0.66	0.97	0.623	1.06	0.589	1.00	1.30	0.766	No
1509	15.09	0.88	0.22	0.66	0.97	0.623	1.06	0.590	1.00	1.30	0.766	No
1510	15.10	0.88	0.22	0.66	0.97	0.623	1.06	0.590	1.00	1.30	0.767	No
1511	15.11	0.88	0.22	0.66	0.97	0.623	1.06	0.590	1.00	1.30	0.767	No
1512	15.12	0.88	0.22	0.66	0.97	0.623	1.06	0.590	1.00	1.30	0.767	No
1513	15.13	0.88	0.22	0.66	0.97	0.623	1.06	0.590	1.00	1.30	0.767	No
1514	15.14	0.88	0.22	0.66	0.97	0.624	1.06	0.590	1.00	1.30	0.767	No
1515	15.15	0.88	0.22	0.66	0.97	0.624	1.06	0.590	1.00	1.30	0.768	No
1516	15.16	0.88	0.22	0.66	0.97	0.624	1.06	0.591	1.00	1.30	0.768	No
1517	15.17	0.88	0.22	0.66	0.97	0.624	1.06	0.591	1.00	1.30	0.768	No
1518	15.18	0.88	0.22	0.66	0.97	0.624	1.06	0.591	1.00	1.30	0.768	No
1519	15.19	0.88	0.22	0.66	0.97	0.624	1.06	0.591	1.00	1.30	0.768	No
1520	15.20	0.88	0.22	0.66	0.97	0.624	1.06	0.591	1.00	1.30	0.769	No
1521	15.21	0.88	0.22	0.66	0.97	0.625	1.06	0.591	1.00	1.30	0.769	No
1522	15.22	0.88	0.23	0.66	0.97	0.625	1.06	0.591	1.00	1.30	0.769	No
1523	15.23	0.88	0.23	0.66	0.97	0.625	1.06	0.592	1.00	1.30	0.769	No
1524	15.24	0.89	0.23	0.66	0.97	0.625	1.06	0.592	1.00	1.30	0.769	No
1525	15.25	0.89	0.23	0.66	0.97	0.625	1.06	0.592	1.00	1.30	0.769	No
1526	15.26	0.89	0.23	0.66	0.97	0.625	1.06	0.592	1.00	1.30	0.770	No
1527	15.27	0.89	0.23	0.66	0.97	0.626	1.06	0.592	1.00	1.30	0.770	No
1528	15.28	0.89	0.23	0.66	0.97	0.626	1.06	0.592	1.00	1.30	0.770	No
1529	15.29	0.89	0.23	0.66	0.97	0.626	1.06	0.592	1.00	1.30	0.770	No
1530	15.30	0.89	0.23	0.66	0.97	0.626	1.06	0.593	1.00	1.30	0.770	No
1531	15.31	0.89	0.23	0.66	0.97	0.626	1.06	0.593	1.00	1.30	0.770	No
1532	15.32	0.89	0.23	0.66	0.97	0.626	1.06	0.593	1.00	1.30	0.771	No
1533	15.33	0.89	0.23	0.66	0.97	0.626	1.06	0.593	1.00	1.30	0.771	No
1534	15.34	0.89	0.23	0.66	0.97	0.627	1.06	0.593	1.00	1.30	0.771	No
1535	15.35	0.89	0.23	0.66	0.97	0.627	1.06	0.593	1.00	1.30	0.771	No
1536	15.36	0.89	0.23	0.66	0.97	0.627	1.06	0.593	1.00	1.30	0.771	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1537	15.37	0.89	0.23	0.66	0.97	0.627	1.06	0.593	1.00	1.30	0.772	No
1538	15.38	0.89	0.23	0.66	0.97	0.627	1.06	0.594	1.00	1.30	0.772	No
1539	15.39	0.89	0.23	0.66	0.97	0.627	1.06	0.594	1.00	1.30	0.772	No
1540	15.40	0.89	0.23	0.66	0.97	0.627	1.06	0.594	1.00	1.30	0.772	No
1541	15.41	0.90	0.23	0.66	0.97	0.628	1.06	0.594	1.00	1.30	0.772	No
1542	15.42	0.90	0.23	0.66	0.97	0.628	1.06	0.594	1.00	1.30	0.772	No
1543	15.43	0.90	0.23	0.66	0.97	0.628	1.06	0.594	1.00	1.30	0.773	No
1544	15.44	0.90	0.23	0.66	0.97	0.628	1.06	0.594	1.00	1.30	0.773	No
1545	15.45	0.90	0.23	0.67	0.97	0.628	1.06	0.595	1.00	1.30	0.773	No
1546	15.46	0.90	0.23	0.67	0.97	0.628	1.06	0.595	1.00	1.30	0.773	No
1547	15.47	0.90	0.23	0.67	0.97	0.628	1.06	0.595	1.00	1.30	0.773	No
1548	15.48	0.90	0.23	0.67	0.97	0.628	1.06	0.595	1.00	1.30	0.773	No
1549	15.49	0.90	0.23	0.67	0.97	0.629	1.06	0.595	1.00	1.30	0.774	No
1550	15.50	0.90	0.23	0.67	0.97	0.629	1.06	0.595	1.00	1.30	0.774	No
1551	15.51	0.90	0.23	0.67	0.97	0.629	1.06	0.595	1.00	1.30	0.774	No
1552	15.52	0.90	0.23	0.67	0.97	0.629	1.06	0.595	1.00	1.30	0.774	No
1553	15.53	0.90	0.23	0.67	0.97	0.629	1.06	0.596	1.00	1.30	0.774	No
1554	15.54	0.90	0.24	0.67	0.97	0.629	1.06	0.596	1.00	1.30	0.774	No
1555	15.55	0.90	0.24	0.67	0.97	0.629	1.06	0.596	1.00	1.30	0.775	No
1556	15.56	0.90	0.24	0.67	0.97	0.630	1.06	0.596	1.00	1.30	0.775	No
1557	15.57	0.90	0.24	0.67	0.97	0.630	1.06	0.596	1.00	1.30	0.775	No
1558	15.58	0.90	0.24	0.67	0.97	0.630	1.06	0.596	1.00	1.30	0.775	No
1559	15.59	0.91	0.24	0.67	0.97	0.630	1.06	0.596	1.00	1.30	0.775	No
1560	15.60	0.91	0.24	0.67	0.97	0.630	1.06	0.597	1.00	1.30	0.776	No
1561	15.61	0.91	0.24	0.67	0.97	0.630	1.06	0.597	1.00	1.30	0.776	No
1562	15.62	0.91	0.24	0.67	0.97	0.630	1.06	0.597	1.00	1.30	0.776	No
1563	15.63	0.91	0.24	0.67	0.97	0.631	1.06	0.597	1.00	1.30	0.776	No
1564	15.64	0.91	0.24	0.67	0.97	0.631	1.06	0.597	1.00	1.30	0.776	No
1565	15.65	0.91	0.24	0.67	0.97	0.631	1.06	0.597	1.00	1.30	0.776	No
1566	15.66	0.91	0.24	0.67	0.97	0.631	1.06	0.597	1.00	1.30	0.777	No
1567	15.67	0.91	0.24	0.67	0.97	0.631	1.06	0.597	1.00	1.30	0.777	No
1568	15.68	0.91	0.24	0.67	0.97	0.631	1.06	0.598	1.00	1.30	0.777	No
1569	15.69	0.91	0.24	0.67	0.97	0.631	1.06	0.598	1.00	1.30	0.777	No
1570	15.70	0.91	0.24	0.67	0.97	0.632	1.06	0.598	1.00	1.30	0.777	No
1571	15.71	0.91	0.24	0.67	0.97	0.632	1.06	0.598	1.00	1.30	0.777	No
1572	15.72	0.91	0.24	0.67	0.97	0.632	1.06	0.598	1.00	1.30	0.778	No
1573	15.73	0.91	0.24	0.67	0.97	0.632	1.06	0.598	1.00	1.30	0.778	No
1574	15.74	0.91	0.24	0.67	0.97	0.632	1.06	0.598	1.00	1.30	0.778	No
1575	15.75	0.91	0.24	0.67	0.97	0.632	1.06	0.599	1.00	1.30	0.778	No
1576	15.76	0.91	0.24	0.67	0.97	0.632	1.06	0.599	1.00	1.30	0.778	No
1577	15.77	0.92	0.24	0.67	0.97	0.633	1.06	0.599	1.00	1.30	0.778	No
1578	15.78	0.92	0.24	0.67	0.97	0.633	1.06	0.599	1.00	1.30	0.779	No
1579	15.79	0.92	0.24	0.67	0.97	0.633	1.06	0.599	1.00	1.30	0.779	No
1580	15.80	0.92	0.24	0.67	0.97	0.633	1.06	0.599	1.00	1.30	0.779	No
1581	15.81	0.92	0.24	0.67	0.97	0.633	1.06	0.599	1.00	1.30	0.779	No
1582	15.82	0.92	0.24	0.67	0.97	0.633	1.06	0.600	1.00	1.30	0.779	No
1583	15.83	0.92	0.24	0.67	0.97	0.633	1.06	0.600	1.00	1.30	0.780	No
1584	15.84	0.92	0.24	0.67	0.97	0.634	1.06	0.600	1.00	1.30	0.780	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1585	15.85	0.92	0.24	0.67	0.97	0.634	1.06	0.600	1.00	1.30	0.780	No
1586	15.86	0.92	0.25	0.68	0.97	0.634	1.06	0.600	1.00	1.30	0.780	No
1587	15.87	0.92	0.25	0.68	0.97	0.634	1.06	0.600	1.00	1.30	0.780	No
1588	15.88	0.92	0.25	0.68	0.97	0.634	1.06	0.600	1.00	1.30	0.780	No
1589	15.89	0.92	0.25	0.68	0.97	0.634	1.06	0.600	1.00	1.30	0.781	No
1590	15.90	0.92	0.25	0.68	0.97	0.634	1.06	0.601	1.00	1.30	0.781	No
1591	15.91	0.92	0.25	0.68	0.97	0.635	1.06	0.601	1.00	1.30	0.781	No
1592	15.92	0.92	0.25	0.68	0.97	0.635	1.06	0.601	1.00	1.30	0.781	No
1593	15.93	0.92	0.25	0.68	0.97	0.635	1.06	0.601	1.00	1.30	0.781	No
1594	15.94	0.92	0.25	0.68	0.97	0.635	1.06	0.601	1.00	1.30	0.781	No
1595	15.95	0.93	0.25	0.68	0.97	0.635	1.06	0.601	1.00	1.30	0.782	No
1596	15.96	0.93	0.25	0.68	0.97	0.635	1.06	0.601	1.00	1.30	0.782	No
1597	15.97	0.93	0.25	0.68	0.97	0.635	1.06	0.602	1.00	1.30	0.782	No
1598	15.98	0.93	0.25	0.68	0.97	0.636	1.06	0.602	1.00	1.30	0.782	No
1599	15.99	0.93	0.25	0.68	0.97	0.636	1.06	0.602	1.00	1.30	0.782	No
1600	16.00	0.93	0.25	0.68	0.97	0.636	1.06	0.602	1.00	1.30	0.782	No
1601	16.01	0.93	0.25	0.68	0.97	0.636	1.06	0.602	1.00	1.30	0.783	No
1602	16.02	0.93	0.25	0.68	0.97	0.636	1.06	0.602	1.00	1.30	0.783	No
1603	16.03	0.93	0.25	0.68	0.97	0.636	1.06	0.602	1.00	1.30	0.783	No
1604	16.04	0.93	0.25	0.68	0.97	0.636	1.06	0.602	1.00	1.30	0.783	No
1605	16.05	0.93	0.25	0.68	0.97	0.637	1.06	0.603	1.00	1.30	0.783	No
1606	16.06	0.93	0.25	0.68	0.97	0.637	1.06	0.603	1.00	1.30	0.784	No
1607	16.07	0.93	0.25	0.68	0.97	0.637	1.06	0.603	1.00	1.30	0.784	No
1608	16.08	0.93	0.25	0.68	0.97	0.637	1.06	0.603	1.00	1.30	0.784	No
1609	16.09	0.93	0.25	0.68	0.97	0.637	1.06	0.603	1.00	1.30	0.784	No
1610	16.10	0.93	0.25	0.68	0.97	0.637	1.06	0.603	1.00	1.30	0.784	No
1611	16.11	0.93	0.25	0.68	0.97	0.637	1.06	0.603	1.00	1.30	0.784	No
1612	16.12	0.93	0.25	0.68	0.97	0.638	1.06	0.604	1.00	1.30	0.785	No
1613	16.13	0.94	0.25	0.68	0.97	0.638	1.06	0.604	1.00	1.30	0.785	No
1614	16.14	0.94	0.25	0.68	0.97	0.638	1.06	0.604	1.00	1.30	0.785	No
1615	16.15	0.94	0.25	0.68	0.97	0.638	1.06	0.604	1.00	1.30	0.785	No
1616	16.16	0.94	0.25	0.68	0.97	0.638	1.06	0.604	1.00	1.30	0.785	No
1617	16.17	0.94	0.25	0.68	0.97	0.638	1.06	0.604	1.00	1.30	0.785	No
1618	16.18	0.94	0.26	0.68	0.97	0.638	1.06	0.604	1.00	1.30	0.786	No
1619	16.19	0.94	0.26	0.68	0.97	0.639	1.06	0.604	1.00	1.30	0.786	No
1620	16.20	0.94	0.26	0.68	0.97	0.639	1.06	0.605	1.00	1.30	0.786	No
1621	16.21	0.94	0.26	0.68	0.97	0.639	1.06	0.605	1.00	1.30	0.786	No
1622	16.22	0.94	0.26	0.68	0.97	0.639	1.06	0.605	1.00	1.30	0.786	No
1623	16.23	0.94	0.26	0.68	0.97	0.639	1.06	0.605	1.00	1.30	0.786	No
1624	16.24	0.94	0.26	0.68	0.97	0.639	1.06	0.605	1.00	1.30	0.787	No
1625	16.25	0.94	0.26	0.68	0.97	0.639	1.06	0.605	1.00	1.30	0.787	No
1626	16.26	0.94	0.26	0.68	0.97	0.639	1.06	0.605	1.00	1.30	0.787	No
1627	16.27	0.94	0.26	0.68	0.97	0.640	1.06	0.605	1.00	1.30	0.787	No
1628	16.28	0.94	0.26	0.68	0.97	0.640	1.06	0.606	1.00	1.30	0.787	No
1629	16.29	0.94	0.26	0.69	0.97	0.640	1.06	0.606	1.00	1.30	0.787	No
1630	16.30	0.94	0.26	0.69	0.97	0.640	1.06	0.606	1.00	1.30	0.788	No
1631	16.31	0.94	0.26	0.69	0.97	0.640	1.06	0.606	1.00	1.30	0.788	No
1632	16.32	0.95	0.26	0.69	0.97	0.640	1.06	0.606	1.00	1.30	0.788	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1633	16.33	0.95	0.26	0.69	0.97	0.640	1.06	0.606	1.00	1.30	0.788	No
1634	16.34	0.95	0.26	0.69	0.97	0.641	1.06	0.606	1.00	1.30	0.788	No
1635	16.35	0.95	0.26	0.69	0.97	0.641	1.06	0.606	1.00	1.30	0.788	No
1636	16.36	0.95	0.26	0.69	0.97	0.641	1.06	0.607	1.00	1.30	0.789	No
1637	16.37	0.95	0.26	0.69	0.97	0.641	1.06	0.607	1.00	1.30	0.789	No
1638	16.38	0.95	0.26	0.69	0.97	0.641	1.06	0.607	1.00	1.30	0.789	No
1639	16.39	0.95	0.26	0.69	0.97	0.641	1.06	0.607	1.00	1.30	0.789	No
1640	16.40	0.95	0.26	0.69	0.97	0.641	1.06	0.607	1.00	1.30	0.789	No
1641	16.41	0.95	0.26	0.69	0.97	0.641	1.06	0.607	1.00	1.30	0.789	No
1642	16.42	0.95	0.26	0.69	0.97	0.642	1.06	0.607	1.00	1.30	0.790	No
1643	16.43	0.95	0.26	0.69	0.97	0.642	1.06	0.607	1.00	1.30	0.790	No
1644	16.44	0.95	0.26	0.69	0.97	0.642	1.06	0.608	1.00	1.30	0.790	No
1645	16.45	0.95	0.26	0.69	0.97	0.642	1.06	0.608	1.00	1.30	0.790	No
1646	16.46	0.95	0.26	0.69	0.97	0.642	1.06	0.608	1.00	1.30	0.790	No
1647	16.47	0.95	0.26	0.69	0.97	0.642	1.06	0.608	1.00	1.30	0.790	No
1648	16.48	0.95	0.26	0.69	0.97	0.642	1.06	0.608	1.00	1.30	0.790	No
1649	16.49	0.96	0.26	0.69	0.97	0.642	1.06	0.608	1.00	1.30	0.791	No
1650	16.50	0.96	0.27	0.69	0.97	0.643	1.06	0.608	1.00	1.30	0.791	No
1651	16.51	0.96	0.27	0.69	0.97	0.643	1.06	0.608	1.00	1.30	0.791	No
1652	16.52	0.96	0.27	0.69	0.97	0.643	1.06	0.609	1.00	1.30	0.791	No
1653	16.53	0.96	0.27	0.69	0.97	0.643	1.06	0.609	1.00	1.30	0.791	No
1654	16.54	0.96	0.27	0.69	0.97	0.643	1.06	0.609	1.00	1.30	0.791	No
1655	16.55	0.96	0.27	0.69	0.97	0.643	1.06	0.609	1.00	1.30	0.792	No
1656	16.56	0.96	0.27	0.69	0.97	0.643	1.06	0.609	1.00	1.30	0.792	No
1657	16.57	0.96	0.27	0.69	0.97	0.643	1.06	0.609	1.00	1.30	0.792	No
1658	16.58	0.96	0.27	0.69	0.97	0.644	1.06	0.609	1.00	1.30	0.792	No
1659	16.59	0.96	0.27	0.69	0.97	0.644	1.06	0.609	1.00	1.30	0.792	No
1660	16.60	0.96	0.27	0.69	0.97	0.644	1.06	0.609	1.00	1.30	0.792	No
1661	16.61	0.96	0.27	0.69	0.97	0.644	1.06	0.610	1.00	1.30	0.792	No
1662	16.62	0.96	0.27	0.69	0.96	0.644	1.06	0.610	1.00	1.30	0.793	No
1663	16.63	0.96	0.27	0.69	0.96	0.644	1.06	0.610	1.00	1.30	0.793	No
1664	16.64	0.96	0.27	0.69	0.96	0.644	1.06	0.610	1.00	1.30	0.793	No
1665	16.65	0.96	0.27	0.69	0.96	0.644	1.06	0.610	1.00	1.30	0.793	No
1666	16.66	0.97	0.27	0.69	0.96	0.645	1.06	0.610	1.00	1.30	0.793	No
1667	16.67	0.97	0.27	0.70	0.96	0.645	1.06	0.610	1.00	1.30	0.793	No
1668	16.68	0.97	0.27	0.70	0.96	0.645	1.06	0.610	1.00	1.30	0.794	No
1669	16.69	0.97	0.27	0.70	0.96	0.645	1.06	0.611	1.00	1.30	0.794	No
1670	16.70	0.97	0.27	0.70	0.96	0.645	1.06	0.611	1.00	1.30	0.794	No
1671	16.71	0.97	0.27	0.70	0.96	0.645	1.06	0.611	1.00	1.30	0.794	No
1672	16.72	0.97	0.27	0.70	0.96	0.645	1.06	0.611	1.00	1.30	0.794	No
1673	16.73	0.97	0.27	0.70	0.96	0.645	1.06	0.611	1.00	1.30	0.794	No
1674	16.74	0.97	0.27	0.70	0.96	0.646	1.06	0.611	1.00	1.30	0.794	No
1675	16.75	0.97	0.27	0.70	0.96	0.646	1.06	0.611	1.00	1.30	0.795	No
1676	16.76	0.97	0.27	0.70	0.96	0.646	1.06	0.611	1.00	1.30	0.795	No
1677	16.77	0.97	0.27	0.70	0.96	0.646	1.06	0.611	1.00	1.30	0.795	No
1678	16.78	0.97	0.27	0.70	0.96	0.646	1.06	0.612	1.00	1.30	0.795	No
1679	16.79	0.97	0.27	0.70	0.96	0.646	1.06	0.612	1.00	1.30	0.795	No
1680	16.80	0.97	0.27	0.70	0.96	0.646	1.06	0.612	1.00	1.30	0.795	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1681	16.81	0.97	0.27	0.70	0.96	0.646	1.06	0.612	1.00	1.30	0.796	No
1682	16.82	0.97	0.28	0.70	0.96	0.647	1.06	0.612	1.00	1.30	0.796	No
1683	16.83	0.97	0.28	0.70	0.96	0.647	1.06	0.612	1.00	1.30	0.796	No
1684	16.84	0.98	0.28	0.70	0.96	0.647	1.06	0.612	1.00	1.30	0.796	No
1685	16.85	0.98	0.28	0.70	0.96	0.647	1.06	0.612	1.00	1.30	0.796	No
1686	16.86	0.98	0.28	0.70	0.96	0.647	1.06	0.613	1.00	1.30	0.796	No
1687	16.87	0.98	0.28	0.70	0.96	0.647	1.06	0.613	1.00	1.30	0.796	No
1688	16.88	0.98	0.28	0.70	0.96	0.647	1.06	0.613	1.00	1.30	0.797	No
1689	16.89	0.98	0.28	0.70	0.96	0.647	1.06	0.613	1.00	1.30	0.797	No
1690	16.90	0.98	0.28	0.70	0.96	0.648	1.06	0.613	1.00	1.30	0.797	No
1691	16.91	0.98	0.28	0.70	0.96	0.648	1.06	0.613	1.00	1.30	0.797	No
1692	16.92	0.98	0.28	0.70	0.96	0.648	1.06	0.613	1.00	1.30	0.797	No
1693	16.93	0.98	0.28	0.70	0.96	0.648	1.06	0.613	1.00	1.30	0.797	No
1694	16.94	0.98	0.28	0.70	0.96	0.648	1.06	0.613	1.00	1.30	0.798	No
1695	16.95	0.98	0.28	0.70	0.96	0.648	1.06	0.614	1.00	1.30	0.798	No
1696	16.96	0.98	0.28	0.70	0.96	0.648	1.06	0.614	1.00	1.30	0.798	No
1697	16.97	0.98	0.28	0.70	0.96	0.648	1.06	0.614	1.00	1.30	0.798	No
1698	16.98	0.98	0.28	0.70	0.96	0.649	1.06	0.614	1.00	1.30	0.798	No
1699	16.99	0.98	0.28	0.70	0.96	0.649	1.06	0.614	1.00	1.30	0.798	No
1700	17.00	0.98	0.28	0.70	0.96	0.649	1.06	0.614	1.00	1.30	0.798	No
1701	17.01	0.98	0.28	0.70	0.96	0.649	1.06	0.614	1.00	1.30	0.799	No
1702	17.02	0.99	0.28	0.70	0.96	0.649	1.06	0.614	1.00	1.30	0.799	No
1703	17.03	0.99	0.28	0.70	0.96	0.649	1.06	0.615	1.00	1.30	0.799	No
1704	17.04	0.99	0.28	0.70	0.96	0.649	1.06	0.615	1.00	1.30	0.799	No
1705	17.05	0.99	0.28	0.70	0.96	0.649	1.06	0.615	1.00	1.30	0.799	No
1706	17.06	0.99	0.28	0.71	0.96	0.650	1.06	0.615	1.00	1.30	0.799	No
1707	17.07	0.99	0.28	0.71	0.96	0.650	1.06	0.615	1.00	1.30	0.800	No
1708	17.08	0.99	0.28	0.71	0.96	0.650	1.06	0.615	1.00	1.30	0.800	No
1709	17.09	0.99	0.28	0.71	0.96	0.650	1.06	0.615	1.00	1.30	0.800	No
1710	17.10	0.99	0.28	0.71	0.96	0.650	1.06	0.615	1.00	1.30	0.800	No
1711	17.11	0.99	0.28	0.71	0.96	0.650	1.06	0.615	1.00	1.30	0.800	No
1712	17.12	0.99	0.28	0.71	0.96	0.650	1.06	0.616	1.00	1.30	0.800	No
1713	17.13	0.99	0.28	0.71	0.96	0.650	1.06	0.616	1.00	1.30	0.800	No
1714	17.14	0.99	0.29	0.71	0.96	0.651	1.06	0.616	1.00	1.30	0.801	No
1715	17.15	0.99	0.29	0.71	0.96	0.651	1.06	0.616	1.00	1.30	0.801	No
1716	17.16	0.99	0.29	0.71	0.96	0.651	1.06	0.616	1.00	1.30	0.801	No
1717	17.17	0.99	0.29	0.71	0.96	0.651	1.06	0.616	1.00	1.30	0.801	No
1718	17.18	0.99	0.29	0.71	0.96	0.651	1.06	0.616	1.00	1.30	0.801	No
1719	17.19	1.00	0.29	0.71	0.96	0.651	1.06	0.616	1.00	1.30	0.801	No
1720	17.20	1.00	0.29	0.71	0.96	0.651	1.06	0.617	1.00	1.30	0.802	No
1721	17.21	1.00	0.29	0.71	0.96	0.651	1.06	0.617	1.00	1.30	0.802	No
1722	17.22	1.00	0.29	0.71	0.96	0.652	1.06	0.617	1.00	1.30	0.802	No
1723	17.23	1.00	0.29	0.71	0.96	0.652	1.06	0.617	1.00	1.30	0.802	No
1724	17.24	1.00	0.29	0.71	0.96	0.652	1.06	0.617	1.00	1.30	0.802	No
1725	17.25	1.00	0.29	0.71	0.96	0.652	1.06	0.617	1.00	1.30	0.802	No
1726	17.26	1.00	0.29	0.71	0.96	0.652	1.06	0.617	1.00	1.30	0.802	No
1727	17.27	1.00	0.29	0.71	0.96	0.652	1.06	0.617	1.00	1.30	0.803	No
1728	17.28	1.00	0.29	0.71	0.96	0.652	1.06	0.617	1.00	1.30	0.803	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1729	17.29	1.00	0.29	0.71	0.96	0.652	1.06	0.618	1.00	1.30	0.803	No
1730	17.30	1.00	0.29	0.71	0.96	0.653	1.06	0.618	1.00	1.30	0.803	No
1731	17.31	1.00	0.29	0.71	0.96	0.653	1.06	0.618	1.00	1.30	0.803	No
1732	17.32	1.00	0.29	0.71	0.96	0.653	1.06	0.618	1.00	1.30	0.803	No
1733	17.33	1.00	0.29	0.71	0.96	0.653	1.06	0.618	1.00	1.30	0.804	No
1734	17.34	1.00	0.29	0.71	0.96	0.653	1.06	0.618	1.00	1.30	0.804	No
1735	17.35	1.00	0.29	0.71	0.96	0.653	1.06	0.618	1.00	1.30	0.804	No
1736	17.36	1.00	0.29	0.71	0.96	0.653	1.06	0.618	1.00	1.30	0.804	No
1737	17.37	1.00	0.29	0.71	0.96	0.653	1.06	0.619	1.00	1.30	0.804	No
1738	17.38	1.01	0.29	0.71	0.96	0.654	1.06	0.619	1.00	1.30	0.804	No
1739	17.39	1.01	0.29	0.71	0.96	0.654	1.06	0.619	1.00	1.30	0.804	No
1740	17.40	1.01	0.29	0.71	0.96	0.654	1.06	0.619	1.00	1.30	0.805	No
1741	17.41	1.01	0.29	0.71	0.96	0.654	1.06	0.619	1.00	1.30	0.805	No
1742	17.42	1.01	0.29	0.71	0.96	0.654	1.06	0.619	1.00	1.30	0.805	No
1743	17.43	1.01	0.29	0.71	0.96	0.654	1.06	0.619	1.00	1.30	0.805	No
1744	17.44	1.01	0.29	0.71	0.96	0.654	1.06	0.619	1.00	1.30	0.805	No
1745	17.45	1.01	0.29	0.71	0.96	0.654	1.06	0.620	1.00	1.30	0.805	No
1746	17.46	1.01	0.30	0.71	0.96	0.655	1.06	0.620	1.00	1.30	0.806	No
1747	17.47	1.01	0.30	0.71	0.96	0.655	1.06	0.620	1.00	1.30	0.806	No
1748	17.48	1.01	0.30	0.71	0.96	0.655	1.06	0.620	1.00	1.30	0.806	No
1749	17.49	1.01	0.30	0.72	0.96	0.655	1.06	0.620	1.00	1.30	0.806	No
1750	17.50	1.01	0.30	0.72	0.96	0.655	1.06	0.620	1.00	1.30	0.806	No
1751	17.51	1.01	0.30	0.72	0.96	0.655	1.06	0.620	1.00	1.30	0.806	No
1752	17.52	1.01	0.30	0.72	0.96	0.655	1.06	0.620	1.00	1.30	0.807	No
1753	17.53	1.01	0.30	0.72	0.96	0.656	1.06	0.621	1.00	1.30	0.807	No
1754	17.54	1.01	0.30	0.72	0.96	0.656	1.06	0.621	1.00	1.30	0.807	No
1755	17.55	1.01	0.30	0.72	0.96	0.656	1.06	0.621	1.00	1.30	0.807	No
1756	17.56	1.01	0.30	0.72	0.96	0.656	1.06	0.621	1.00	1.30	0.807	No
1757	17.57	1.02	0.30	0.72	0.96	0.656	1.06	0.621	1.00	1.30	0.807	No
1758	17.58	1.02	0.30	0.72	0.96	0.656	1.06	0.621	1.00	1.30	0.807	No
1759	17.59	1.02	0.30	0.72	0.96	0.656	1.06	0.621	1.00	1.30	0.808	No
1760	17.60	1.02	0.30	0.72	0.96	0.656	1.06	0.621	1.00	1.30	0.808	No
1761	17.61	1.02	0.30	0.72	0.96	0.657	1.06	0.621	1.00	1.30	0.808	No
1762	17.62	1.02	0.30	0.72	0.96	0.657	1.06	0.622	1.00	1.30	0.808	No
1763	17.63	1.02	0.30	0.72	0.96	0.657	1.06	0.622	1.00	1.30	0.808	No
1764	17.64	1.02	0.30	0.72	0.96	0.657	1.06	0.622	1.00	1.30	0.808	No
1765	17.65	1.02	0.30	0.72	0.96	0.657	1.06	0.622	1.00	1.30	0.809	No
1766	17.66	1.02	0.30	0.72	0.96	0.657	1.06	0.622	1.00	1.30	0.809	No
1767	17.67	1.02	0.30	0.72	0.96	0.657	1.06	0.622	1.00	1.30	0.809	No
1768	17.68	1.02	0.30	0.72	0.96	0.657	1.06	0.622	1.00	1.30	0.809	No
1769	17.69	1.02	0.30	0.72	0.96	0.657	1.06	0.622	1.00	1.30	0.809	No
1770	17.70	1.02	0.30	0.72	0.96	0.658	1.06	0.623	1.00	1.30	0.809	No
1771	17.71	1.02	0.30	0.72	0.96	0.658	1.06	0.623	1.00	1.30	0.809	No
1772	17.72	1.02	0.30	0.72	0.96	0.658	1.06	0.623	1.00	1.30	0.810	No
1773	17.73	1.02	0.30	0.72	0.96	0.658	1.06	0.623	1.00	1.30	0.810	No
1774	17.74	1.02	0.30	0.72	0.96	0.658	1.06	0.623	1.00	1.30	0.810	No
1775	17.75	1.03	0.30	0.72	0.96	0.658	1.06	0.623	1.00	1.30	0.810	No
1776	17.76	1.03	0.30	0.72	0.96	0.658	1.06	0.623	1.00	1.30	0.810	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1777	17.77	1.03	0.30	0.72	0.96	0.658	1.06	0.623	1.00	1.30	0.810	No
1778	17.78	1.03	0.31	0.72	0.96	0.659	1.06	0.623	1.00	1.30	0.810	No
1779	17.79	1.03	0.31	0.72	0.96	0.659	1.06	0.624	1.00	1.30	0.811	No
1780	17.80	1.03	0.31	0.72	0.96	0.659	1.06	0.624	1.00	1.30	0.811	No
1781	17.81	1.03	0.31	0.72	0.96	0.659	1.06	0.624	1.00	1.30	0.811	No
1782	17.82	1.03	0.31	0.72	0.96	0.659	1.06	0.624	1.00	1.30	0.811	No
1783	17.83	1.03	0.31	0.72	0.96	0.659	1.06	0.624	1.00	1.30	0.811	No
1784	17.84	1.03	0.31	0.72	0.96	0.659	1.06	0.624	1.00	1.30	0.811	No
1785	17.85	1.03	0.31	0.72	0.96	0.659	1.06	0.624	1.00	1.30	0.811	No
1786	17.86	1.03	0.31	0.72	0.96	0.660	1.06	0.624	1.00	1.30	0.812	No
1787	17.87	1.03	0.31	0.72	0.96	0.660	1.06	0.624	1.00	1.30	0.812	No
1788	17.88	1.03	0.31	0.72	0.96	0.660	1.06	0.625	1.00	1.30	0.812	No
1789	17.89	1.03	0.31	0.72	0.96	0.660	1.06	0.625	1.00	1.30	0.812	No
1790	17.90	1.03	0.31	0.72	0.96	0.660	1.06	0.625	1.00	1.30	0.812	No
1791	17.91	1.03	0.31	0.72	0.96	0.660	1.06	0.625	1.00	1.30	0.812	No
1792	17.92	1.03	0.31	0.73	0.96	0.660	1.06	0.625	1.00	1.30	0.813	No
1793	17.93	1.04	0.31	0.73	0.96	0.660	1.06	0.625	1.00	1.30	0.813	No
1794	17.94	1.04	0.31	0.73	0.96	0.660	1.06	0.625	1.00	1.30	0.813	No
1795	17.95	1.04	0.31	0.73	0.96	0.661	1.06	0.625	1.00	1.30	0.813	No
1796	17.96	1.04	0.31	0.73	0.96	0.661	1.06	0.625	1.00	1.30	0.813	No
1797	17.97	1.04	0.31	0.73	0.96	0.661	1.06	0.626	1.00	1.30	0.813	No
1798	17.98	1.04	0.31	0.73	0.96	0.661	1.06	0.626	1.00	1.30	0.813	No
1799	17.99	1.04	0.31	0.73	0.96	0.661	1.06	0.626	1.00	1.30	0.814	No
1800	18.00	1.04	0.31	0.73	0.96	0.661	1.06	0.626	1.00	1.30	0.814	No
1801	18.01	1.04	0.31	0.73	0.96	0.661	1.06	0.626	1.00	1.30	0.814	No
1802	18.02	1.04	0.31	0.73	0.96	0.661	1.06	0.626	1.00	1.30	0.814	No
1803	18.03	1.04	0.31	0.73	0.96	0.662	1.06	0.626	1.00	1.30	0.814	No
1804	18.04	1.04	0.31	0.73	0.96	0.662	1.06	0.626	1.00	1.30	0.814	No
1805	18.05	1.04	0.31	0.73	0.96	0.662	1.06	0.626	1.00	1.30	0.814	No
1806	18.06	1.04	0.31	0.73	0.96	0.662	1.06	0.627	1.00	1.30	0.815	No
1807	18.07	1.04	0.31	0.73	0.96	0.662	1.06	0.627	1.00	1.30	0.815	No
1808	18.08	1.04	0.31	0.73	0.96	0.662	1.06	0.627	1.00	1.30	0.815	No
1809	18.09	1.04	0.31	0.73	0.96	0.662	1.06	0.627	1.00	1.30	0.815	No
1810	18.10	1.04	0.32	0.73	0.96	0.662	1.06	0.627	1.00	1.30	0.815	No
1811	18.11	1.05	0.32	0.73	0.96	0.662	1.06	0.627	1.00	1.30	0.815	No
1812	18.12	1.05	0.32	0.73	0.96	0.663	1.06	0.627	1.00	1.30	0.815	No
1813	18.13	1.05	0.32	0.73	0.96	0.663	1.06	0.627	1.00	1.30	0.815	No
1814	18.14	1.05	0.32	0.73	0.96	0.663	1.06	0.627	1.00	1.30	0.816	No
1815	18.15	1.05	0.32	0.73	0.96	0.663	1.06	0.628	1.00	1.30	0.816	No
1816	18.16	1.05	0.32	0.73	0.96	0.663	1.06	0.628	1.00	1.30	0.816	No
1817	18.17	1.05	0.32	0.73	0.96	0.663	1.06	0.628	1.00	1.30	0.816	No
1818	18.18	1.05	0.32	0.73	0.96	0.663	1.06	0.628	1.00	1.30	0.816	No
1819	18.19	1.05	0.32	0.73	0.96	0.663	1.06	0.628	1.00	1.30	0.816	No
1820	18.20	1.05	0.32	0.73	0.96	0.663	1.06	0.628	1.00	1.30	0.816	No
1821	18.21	1.05	0.32	0.73	0.96	0.664	1.06	0.628	1.00	1.30	0.817	No
1822	18.22	1.05	0.32	0.73	0.96	0.664	1.06	0.628	1.00	1.30	0.817	No
1823	18.23	1.05	0.32	0.73	0.96	0.664	1.06	0.628	1.00	1.30	0.817	No
1824	18.24	1.05	0.32	0.73	0.96	0.664	1.06	0.628	1.00	1.30	0.817	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1825	18.25	1.05	0.32	0.73	0.96	0.664	1.06	0.629	1.00	1.30	0.817	No
1826	18.26	1.05	0.32	0.73	0.96	0.664	1.06	0.629	1.00	1.30	0.817	No
1827	18.27	1.05	0.32	0.73	0.96	0.664	1.06	0.629	1.00	1.30	0.817	No
1828	18.28	1.05	0.32	0.73	0.96	0.664	1.06	0.629	1.00	1.30	0.817	No
1829	18.29	1.06	0.32	0.73	0.96	0.664	1.06	0.629	1.00	1.30	0.818	No
1830	18.30	1.06	0.32	0.73	0.96	0.664	1.06	0.629	1.00	1.30	0.818	No
1831	18.31	1.06	0.32	0.74	0.96	0.665	1.06	0.629	1.00	1.30	0.818	No
1832	18.32	1.06	0.32	0.74	0.96	0.665	1.06	0.629	1.00	1.30	0.818	No
1833	18.33	1.06	0.32	0.74	0.96	0.665	1.06	0.629	1.00	1.30	0.818	No
1834	18.34	1.06	0.32	0.74	0.96	0.665	1.06	0.629	1.00	1.30	0.818	No
1835	18.35	1.06	0.32	0.74	0.96	0.665	1.06	0.630	1.00	1.30	0.818	No
1836	18.36	1.06	0.32	0.74	0.96	0.665	1.06	0.630	1.00	1.30	0.819	No
1837	18.37	1.06	0.32	0.74	0.96	0.665	1.06	0.630	1.00	1.30	0.819	No
1838	18.38	1.06	0.32	0.74	0.96	0.665	1.06	0.630	1.00	1.30	0.819	No
1839	18.39	1.06	0.32	0.74	0.96	0.665	1.06	0.630	1.00	1.30	0.819	No
1840	18.40	1.06	0.32	0.74	0.96	0.666	1.06	0.630	1.00	1.30	0.819	No
1841	18.41	1.06	0.32	0.74	0.96	0.666	1.06	0.630	1.00	1.30	0.819	No
1842	18.42	1.06	0.33	0.74	0.96	0.666	1.06	0.630	1.00	1.30	0.819	No
1843	18.43	1.06	0.33	0.74	0.96	0.666	1.06	0.630	1.00	1.30	0.819	No
1844	18.44	1.06	0.33	0.74	0.96	0.666	1.06	0.630	1.00	1.30	0.820	No
1845	18.45	1.06	0.33	0.74	0.96	0.666	1.06	0.631	1.00	1.30	0.820	No
1846	18.46	1.07	0.33	0.74	0.96	0.666	1.06	0.631	1.00	1.30	0.820	No
1847	18.47	1.07	0.33	0.74	0.96	0.666	1.06	0.631	1.00	1.30	0.820	No
1848	18.48	1.07	0.33	0.74	0.96	0.666	1.06	0.631	1.00	1.30	0.820	No
1849	18.49	1.07	0.33	0.74	0.96	0.667	1.06	0.631	1.00	1.30	0.820	No
1850	18.50	1.07	0.33	0.74	0.96	0.667	1.06	0.631	1.00	1.30	0.820	No
1851	18.51	1.07	0.33	0.74	0.96	0.667	1.06	0.631	1.00	1.30	0.821	No
1852	18.52	1.07	0.33	0.74	0.96	0.667	1.06	0.631	1.00	1.30	0.821	No
1853	18.53	1.07	0.33	0.74	0.96	0.667	1.06	0.631	1.00	1.30	0.821	No
1854	18.54	1.07	0.33	0.74	0.96	0.667	1.06	0.631	1.00	1.30	0.821	No
1855	18.55	1.07	0.33	0.74	0.96	0.667	1.06	0.632	1.00	1.30	0.821	No
1856	18.56	1.07	0.33	0.74	0.96	0.667	1.06	0.632	1.00	1.30	0.821	No
1857	18.57	1.07	0.33	0.74	0.96	0.667	1.06	0.632	1.00	1.30	0.821	No
1858	18.58	1.07	0.33	0.74	0.96	0.668	1.06	0.632	1.00	1.30	0.821	No
1859	18.59	1.07	0.33	0.74	0.96	0.668	1.06	0.632	1.00	1.30	0.822	No
1860	18.60	1.07	0.33	0.74	0.96	0.668	1.06	0.632	1.00	1.30	0.822	No
1861	18.61	1.07	0.33	0.74	0.96	0.668	1.06	0.632	1.00	1.30	0.822	No
1862	18.62	1.07	0.33	0.74	0.96	0.668	1.06	0.632	1.00	1.30	0.822	No
1863	18.63	1.07	0.33	0.74	0.96	0.668	1.06	0.632	1.00	1.30	0.822	No
1864	18.64	1.08	0.33	0.74	0.96	0.668	1.06	0.633	1.00	1.30	0.822	No
1865	18.65	1.08	0.33	0.74	0.96	0.668	1.06	0.633	1.00	1.30	0.822	No
1866	18.66	1.08	0.33	0.74	0.96	0.668	1.06	0.633	1.00	1.30	0.823	No
1867	18.67	1.08	0.33	0.74	0.96	0.669	1.06	0.633	1.00	1.30	0.823	No
1868	18.68	1.08	0.33	0.74	0.96	0.669	1.06	0.633	1.00	1.30	0.823	No
1869	18.69	1.08	0.33	0.74	0.96	0.669	1.06	0.633	1.00	1.30	0.823	No
1870	18.70	1.08	0.33	0.74	0.96	0.669	1.06	0.633	1.00	1.30	0.823	No
1871	18.71	1.08	0.33	0.74	0.96	0.669	1.06	0.633	1.00	1.30	0.823	No
1872	18.72	1.08	0.33	0.75	0.96	0.669	1.06	0.633	1.00	1.30	0.823	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1873	18.73	1.08	0.33	0.75	0.96	0.669	1.06	0.633	1.00	1.30	0.824	No
1874	18.74	1.08	0.34	0.75	0.96	0.669	1.06	0.634	1.00	1.30	0.824	No
1875	18.75	1.08	0.34	0.75	0.96	0.669	1.06	0.634	1.00	1.30	0.824	No
1876	18.76	1.08	0.34	0.75	0.96	0.670	1.06	0.634	1.00	1.30	0.824	No
1877	18.77	1.08	0.34	0.75	0.96	0.670	1.06	0.634	1.00	1.30	0.824	No
1878	18.78	1.08	0.34	0.75	0.96	0.670	1.06	0.634	1.00	1.30	0.824	No
1879	18.79	1.08	0.34	0.75	0.96	0.670	1.06	0.634	1.00	1.30	0.824	No
1880	18.80	1.08	0.34	0.75	0.96	0.670	1.06	0.634	1.00	1.30	0.825	No
1881	18.81	1.08	0.34	0.75	0.96	0.670	1.06	0.634	1.00	1.30	0.825	No
1882	18.82	1.08	0.34	0.75	0.96	0.670	1.06	0.634	1.00	1.30	0.825	No
1883	18.83	1.09	0.34	0.75	0.96	0.670	1.06	0.635	1.00	1.30	0.825	No
1884	18.84	1.09	0.34	0.75	0.96	0.670	1.06	0.635	1.00	1.30	0.825	No
1885	18.85	1.09	0.34	0.75	0.96	0.671	1.06	0.635	1.00	1.30	0.825	No
1886	18.86	1.09	0.34	0.75	0.96	0.671	1.06	0.635	1.00	1.30	0.825	No
1887	18.87	1.09	0.34	0.75	0.96	0.671	1.06	0.635	1.00	1.30	0.826	No
1888	18.88	1.09	0.34	0.75	0.96	0.671	1.06	0.635	1.00	1.30	0.826	No
1889	18.89	1.09	0.34	0.75	0.96	0.671	1.06	0.635	1.00	1.30	0.826	No
1890	18.90	1.09	0.34	0.75	0.96	0.671	1.06	0.635	1.00	1.30	0.826	No
1891	18.91	1.09	0.34	0.75	0.96	0.671	1.06	0.635	1.00	1.30	0.826	No
1892	18.92	1.09	0.34	0.75	0.96	0.671	1.06	0.636	1.00	1.30	0.826	No
1893	18.93	1.09	0.34	0.75	0.96	0.671	1.06	0.636	1.00	1.30	0.826	No
1894	18.94	1.09	0.34	0.75	0.96	0.672	1.06	0.636	1.00	1.30	0.826	No
1895	18.95	1.09	0.34	0.75	0.96	0.672	1.06	0.636	1.00	1.30	0.827	No
1896	18.96	1.09	0.34	0.75	0.96	0.672	1.06	0.636	1.00	1.30	0.827	No
1897	18.97	1.09	0.34	0.75	0.96	0.672	1.06	0.636	1.00	1.30	0.827	No
1898	18.98	1.09	0.34	0.75	0.96	0.672	1.06	0.636	1.00	1.30	0.827	No
1899	18.99	1.09	0.34	0.75	0.96	0.672	1.06	0.636	1.00	1.30	0.827	No
1900	19.00	1.09	0.34	0.75	0.96	0.672	1.06	0.636	1.00	1.30	0.827	No
1901	19.01	1.10	0.34	0.75	0.96	0.672	1.06	0.637	1.00	1.30	0.827	No
1902	19.02	1.10	0.34	0.75	0.96	0.672	1.06	0.637	1.00	1.30	0.828	No
1903	19.03	1.10	0.34	0.75	0.96	0.673	1.06	0.637	1.00	1.30	0.828	No
1904	19.04	1.10	0.34	0.75	0.96	0.673	1.06	0.637	1.00	1.30	0.828	No
1905	19.05	1.10	0.34	0.75	0.96	0.673	1.06	0.637	1.00	1.30	0.828	No
1906	19.06	1.10	0.35	0.75	0.96	0.673	1.06	0.637	1.00	1.30	0.828	No
1907	19.07	1.10	0.35	0.75	0.96	0.673	1.06	0.637	1.00	1.30	0.828	No
1908	19.08	1.10	0.35	0.75	0.96	0.673	1.06	0.637	1.00	1.30	0.828	No
1909	19.09	1.10	0.35	0.75	0.96	0.673	1.06	0.637	1.00	1.30	0.829	No
1910	19.10	1.10	0.35	0.75	0.96	0.673	1.06	0.637	1.00	1.30	0.829	No
1911	19.11	1.10	0.35	0.75	0.96	0.673	1.06	0.638	1.00	1.30	0.829	No
1912	19.12	1.10	0.35	0.75	0.96	0.674	1.06	0.638	1.00	1.30	0.829	No
1913	19.13	1.10	0.35	0.75	0.96	0.674	1.06	0.638	1.00	1.30	0.829	No
1914	19.14	1.10	0.35	0.75	0.96	0.674	1.06	0.638	1.00	1.30	0.829	No
1915	19.15	1.10	0.35	0.75	0.96	0.674	1.06	0.638	1.00	1.30	0.829	No
1916	19.16	1.10	0.35	0.76	0.96	0.674	1.06	0.638	1.00	1.30	0.829	No
1917	19.17	1.10	0.35	0.76	0.96	0.674	1.06	0.638	1.00	1.30	0.830	No
1918	19.18	1.10	0.35	0.76	0.96	0.674	1.06	0.638	1.00	1.30	0.830	No
1919	19.19	1.10	0.35	0.76	0.96	0.674	1.06	0.638	1.00	1.30	0.830	No
1920	19.20	1.11	0.35	0.76	0.96	0.674	1.06	0.638	1.00	1.30	0.830	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1921	19.21	1.11	0.35	0.76	0.96	0.675	1.06	0.639	1.00	1.30	0.830	No
1922	19.22	1.11	0.35	0.76	0.96	0.675	1.06	0.639	1.00	1.30	0.830	No
1923	19.23	1.11	0.35	0.76	0.96	0.675	1.06	0.639	1.00	1.30	0.830	No
1924	19.24	1.11	0.35	0.76	0.96	0.675	1.06	0.639	1.00	1.30	0.831	No
1925	19.25	1.11	0.35	0.76	0.96	0.675	1.06	0.639	1.00	1.30	0.831	No
1926	19.26	1.11	0.35	0.76	0.96	0.675	1.06	0.639	1.00	1.30	0.831	No
1927	19.27	1.11	0.35	0.76	0.96	0.675	1.06	0.639	1.00	1.30	0.831	No
1928	19.28	1.11	0.35	0.76	0.96	0.675	1.06	0.639	1.00	1.30	0.831	No
1929	19.29	1.11	0.35	0.76	0.96	0.675	1.06	0.639	1.00	1.30	0.831	No
1930	19.30	1.11	0.35	0.76	0.96	0.676	1.06	0.639	1.00	1.30	0.831	No
1931	19.31	1.11	0.35	0.76	0.96	0.676	1.06	0.640	1.00	1.30	0.831	No
1932	19.32	1.11	0.35	0.76	0.96	0.676	1.06	0.640	1.00	1.30	0.832	No
1933	19.33	1.11	0.35	0.76	0.96	0.676	1.06	0.640	1.00	1.30	0.832	No
1934	19.34	1.11	0.35	0.76	0.96	0.676	1.06	0.640	1.00	1.30	0.832	No
1935	19.35	1.11	0.35	0.76	0.96	0.676	1.06	0.640	1.00	1.30	0.832	No
1936	19.36	1.11	0.35	0.76	0.96	0.676	1.06	0.640	1.00	1.30	0.832	No
1937	19.37	1.11	0.35	0.76	0.96	0.676	1.06	0.640	1.00	1.30	0.832	No
1938	19.38	1.11	0.36	0.76	0.96	0.676	1.06	0.640	1.00	1.30	0.832	No
1939	19.39	1.12	0.36	0.76	0.96	0.677	1.06	0.640	1.00	1.30	0.833	No
1940	19.40	1.12	0.36	0.76	0.96	0.677	1.06	0.641	1.00	1.30	0.833	No
1941	19.41	1.12	0.36	0.76	0.96	0.677	1.06	0.641	1.00	1.30	0.833	No
1942	19.42	1.12	0.36	0.76	0.96	0.677	1.06	0.641	1.00	1.30	0.833	No
1943	19.43	1.12	0.36	0.76	0.96	0.677	1.06	0.641	1.00	1.30	0.833	No
1944	19.44	1.12	0.36	0.76	0.96	0.677	1.06	0.641	1.00	1.30	0.833	No
1945	19.45	1.12	0.36	0.76	0.96	0.677	1.06	0.641	1.00	1.30	0.833	No
1946	19.46	1.12	0.36	0.76	0.96	0.677	1.06	0.641	1.00	1.30	0.834	No
1947	19.47	1.12	0.36	0.76	0.96	0.677	1.06	0.641	1.00	1.30	0.834	No
1948	19.48	1.12	0.36	0.76	0.96	0.678	1.06	0.641	1.00	1.30	0.834	No
1949	19.49	1.12	0.36	0.76	0.96	0.678	1.06	0.641	1.00	1.30	0.834	No
1950	19.50	1.12	0.36	0.76	0.96	0.678	1.06	0.642	1.00	1.30	0.834	No
1951	19.51	1.12	0.36	0.76	0.96	0.678	1.06	0.642	1.00	1.30	0.834	No
1952	19.52	1.12	0.36	0.76	0.96	0.678	1.06	0.642	1.00	1.30	0.834	No
1953	19.53	1.12	0.36	0.76	0.96	0.678	1.06	0.642	1.00	1.30	0.834	No
1954	19.54	1.12	0.36	0.76	0.96	0.678	1.06	0.642	1.00	1.30	0.835	No
1955	19.55	1.12	0.36	0.76	0.96	0.678	1.06	0.642	1.00	1.30	0.835	No
1956	19.56	1.12	0.36	0.76	0.96	0.678	1.06	0.642	1.00	1.30	0.835	No
1957	19.57	1.12	0.36	0.76	0.96	0.679	1.06	0.642	1.00	1.30	0.835	No
1958	19.58	1.13	0.36	0.76	0.96	0.679	1.06	0.642	1.00	1.30	0.835	No
1959	19.59	1.13	0.36	0.76	0.96	0.679	1.06	0.643	1.00	1.30	0.835	No
1960	19.60	1.13	0.36	0.76	0.96	0.679	1.06	0.643	1.00	1.30	0.835	No
1961	19.61	1.13	0.36	0.76	0.96	0.679	1.06	0.643	1.00	1.30	0.836	No
1962	19.62	1.13	0.36	0.76	0.96	0.679	1.06	0.643	1.00	1.30	0.836	No
1963	19.63	1.13	0.36	0.77	0.96	0.679	1.06	0.643	1.00	1.30	0.836	No
1964	19.64	1.13	0.36	0.77	0.96	0.679	1.06	0.643	1.00	1.30	0.836	No
1965	19.65	1.13	0.36	0.77	0.96	0.679	1.06	0.643	1.00	1.30	0.836	No
1966	19.66	1.13	0.36	0.77	0.96	0.680	1.06	0.643	1.00	1.30	0.836	No
1967	19.67	1.13	0.36	0.77	0.96	0.680	1.06	0.643	1.00	1.30	0.836	No
1968	19.68	1.13	0.36	0.77	0.96	0.680	1.06	0.643	1.00	1.30	0.837	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1969	19.69	1.13	0.36	0.77	0.96	0.680	1.06	0.644	1.00	1.30	0.837	No
1970	19.70	1.13	0.37	0.77	0.96	0.680	1.06	0.644	1.00	1.30	0.837	No
1971	19.71	1.13	0.37	0.77	0.96	0.680	1.06	0.644	1.00	1.30	0.837	No
1972	19.72	1.13	0.37	0.77	0.96	0.680	1.06	0.644	1.00	1.30	0.837	No
1973	19.73	1.13	0.37	0.77	0.96	0.680	1.06	0.644	1.00	1.30	0.837	No
1974	19.74	1.13	0.37	0.77	0.96	0.680	1.06	0.644	1.00	1.30	0.837	No
1975	19.75	1.13	0.37	0.77	0.96	0.681	1.06	0.644	1.00	1.30	0.837	No
1976	19.76	1.13	0.37	0.77	0.96	0.681	1.06	0.644	1.00	1.30	0.838	No
1977	19.77	1.14	0.37	0.77	0.96	0.681	1.06	0.644	1.00	1.30	0.838	No
1978	19.78	1.14	0.37	0.77	0.96	0.681	1.06	0.645	1.00	1.30	0.838	No
1979	19.79	1.14	0.37	0.77	0.96	0.681	1.06	0.645	1.00	1.30	0.838	No
1980	19.80	1.14	0.37	0.77	0.96	0.681	1.06	0.645	1.00	1.30	0.838	No
1981	19.81	1.14	0.37	0.77	0.96	0.681	1.06	0.645	1.00	1.30	0.838	No
1982	19.82	1.14	0.37	0.77	0.96	0.681	1.06	0.645	1.00	1.30	0.838	No
1983	19.83	1.14	0.37	0.77	0.96	0.681	1.06	0.645	1.00	1.30	0.839	No
1984	19.84	1.14	0.37	0.77	0.96	0.682	1.06	0.645	1.00	1.30	0.839	No
1985	19.85	1.14	0.37	0.77	0.96	0.682	1.06	0.645	1.00	1.30	0.839	No
1986	19.86	1.14	0.37	0.77	0.96	0.682	1.06	0.645	1.00	1.30	0.839	No
1987	19.87	1.14	0.37	0.77	0.96	0.682	1.06	0.645	1.00	1.30	0.839	No
1988	19.88	1.14	0.37	0.77	0.96	0.682	1.06	0.646	1.00	1.30	0.839	No
1989	19.89	1.14	0.37	0.77	0.96	0.682	1.06	0.646	1.00	1.30	0.839	No
1990	19.90	1.14	0.37	0.77	0.96	0.682	1.06	0.646	1.00	1.30	0.839	No
1991	19.91	1.14	0.37	0.77	0.96	0.682	1.06	0.646	1.00	1.30	0.840	No
1992	19.92	1.14	0.37	0.77	0.96	0.682	1.06	0.646	1.00	1.30	0.840	No
1993	19.93	1.14	0.37	0.77	0.96	0.682	1.06	0.646	1.00	1.30	0.840	No
1994	19.94	1.14	0.37	0.77	0.96	0.683	1.06	0.646	1.00	1.30	0.840	No
1995	19.95	1.15	0.37	0.77	0.96	0.683	1.06	0.646	1.00	1.30	0.840	No
1996	19.96	1.15	0.37	0.77	0.96	0.683	1.06	0.646	1.00	1.30	0.840	No
1997	19.97	1.15	0.37	0.77	0.96	0.683	1.06	0.646	1.00	1.30	0.840	No
1998	19.98	1.15	0.37	0.77	0.96	0.683	1.06	0.646	1.00	1.30	0.840	No
1999	19.99	1.15	0.37	0.77	0.96	0.683	1.06	0.647	1.00	1.30	0.840	No
2000	20.00	1.15	0.37	0.77	0.96	0.683	1.06	0.647	1.00	1.30	0.841	No
2001	20.01	1.15	0.37	0.77	0.96	0.683	1.06	0.647	1.00	1.30	0.841	No
2002	20.02	1.15	0.38	0.77	0.96	0.683	1.06	0.647	1.00	1.30	0.841	No
2003	20.03	1.15	0.38	0.77	0.96	0.683	1.06	0.647	1.00	1.30	0.841	No
2004	20.04	1.15	0.38	0.77	0.96	0.683	1.06	0.647	1.00	1.30	0.841	No
2005	20.05	1.15	0.38	0.77	0.96	0.684	1.06	0.647	1.00	1.30	0.841	No
2006	20.06	1.15	0.38	0.77	0.96	0.684	1.06	0.647	1.00	1.30	0.841	No
2007	20.07	1.15	0.38	0.78	0.96	0.684	1.06	0.647	1.00	1.30	0.841	No
2008	20.08	1.15	0.38	0.78	0.96	0.684	1.06	0.647	1.00	1.30	0.842	No
2009	20.09	1.15	0.38	0.78	0.96	0.684	1.06	0.647	1.00	1.30	0.842	No
2010	20.10	1.15	0.38	0.78	0.96	0.684	1.06	0.648	1.00	1.30	0.842	No
2011	20.11	1.15	0.38	0.78	0.96	0.684	1.06	0.648	1.00	1.30	0.842	No
2012	20.12	1.15	0.38	0.78	0.96	0.684	1.06	0.648	1.00	1.30	0.842	No
2013	20.13	1.15	0.38	0.78	0.96	0.684	1.06	0.648	1.00	1.30	0.842	No
2014	20.14	1.16	0.38	0.78	0.96	0.684	1.06	0.648	1.00	1.30	0.842	No
2015	20.15	1.16	0.38	0.78	0.96	0.685	1.06	0.648	1.00	1.30	0.842	No
2016	20.16	1.16	0.38	0.78	0.96	0.685	1.06	0.648	1.00	1.30	0.843	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
2017	20.17	1.16	0.38	0.78	0.96	0.685	1.06	0.648	1.00	1.30	0.843	No
2018	20.18	1.16	0.38	0.78	0.96	0.685	1.06	0.648	1.00	1.30	0.843	No
2019	20.19	1.16	0.38	0.78	0.96	0.685	1.06	0.648	1.00	1.30	0.843	No
2020	20.20	1.16	0.38	0.78	0.96	0.685	1.06	0.649	1.00	1.30	0.843	No
2021	20.21	1.16	0.38	0.78	0.96	0.685	1.06	0.649	1.00	1.30	0.843	No
2022	20.22	1.16	0.38	0.78	0.96	0.685	1.06	0.649	1.00	1.30	0.843	No
2023	20.23	1.16	0.38	0.78	0.96	0.685	1.06	0.649	1.00	1.30	0.843	No
2024	20.24	1.16	0.38	0.78	0.96	0.686	1.06	0.649	1.00	1.30	0.844	No
2025	20.25	1.16	0.38	0.78	0.96	0.686	1.06	0.649	1.00	1.30	0.844	No
2026	20.26	1.16	0.38	0.78	0.96	0.686	1.06	0.649	1.00	1.30	0.844	No
2027	20.27	1.16	0.38	0.78	0.96	0.686	1.06	0.649	1.00	1.30	0.844	No
2028	20.28	1.16	0.38	0.78	0.96	0.686	1.06	0.649	1.00	1.30	0.844	No
2029	20.29	1.16	0.38	0.78	0.96	0.686	1.06	0.649	1.00	1.30	0.844	No
2030	20.30	1.16	0.38	0.78	0.96	0.686	1.06	0.650	1.00	1.30	0.844	No
2031	20.31	1.16	0.38	0.78	0.96	0.686	1.06	0.650	1.00	1.30	0.845	No
2032	20.32	1.16	0.38	0.78	0.96	0.686	1.06	0.650	1.00	1.30	0.845	No
2033	20.33	1.17	0.38	0.78	0.96	0.686	1.06	0.650	1.00	1.30	0.845	No
2034	20.34	1.17	0.39	0.78	0.96	0.687	1.06	0.650	1.00	1.30	0.845	No
2035	20.35	1.17	0.39	0.78	0.96	0.687	1.06	0.650	1.00	1.30	0.845	No
2036	20.36	1.17	0.39	0.78	0.96	0.687	1.06	0.650	1.00	1.30	0.845	No
2037	20.37	1.17	0.39	0.78	0.96	0.687	1.06	0.650	1.00	1.30	0.845	No
2038	20.38	1.17	0.39	0.78	0.96	0.687	1.06	0.650	1.00	1.30	0.845	No
2039	20.39	1.17	0.39	0.78	0.96	0.687	1.06	0.650	1.00	1.30	0.846	No
2040	20.40	1.17	0.39	0.78	0.96	0.687	1.06	0.650	1.00	1.30	0.846	No
2041	20.41	1.17	0.39	0.78	0.96	0.687	1.06	0.651	1.00	1.30	0.846	No
2042	20.42	1.17	0.39	0.78	0.96	0.687	1.06	0.651	1.00	1.30	0.846	No
2043	20.43	1.17	0.39	0.78	0.96	0.687	1.06	0.651	1.00	1.30	0.846	No
2044	20.44	1.17	0.39	0.78	0.96	0.688	1.06	0.651	1.00	1.30	0.846	No
2045	20.45	1.17	0.39	0.78	0.96	0.688	1.06	0.651	1.00	1.30	0.846	No
2046	20.46	1.17	0.39	0.78	0.96	0.688	1.06	0.651	1.00	1.30	0.846	No
2047	20.47	1.17	0.39	0.78	0.96	0.688	1.06	0.651	1.00	1.30	0.846	No
2048	20.48	1.17	0.39	0.78	0.96	0.688	1.06	0.651	1.00	1.30	0.847	No
2049	20.49	1.17	0.39	0.78	0.96	0.688	1.06	0.651	1.00	1.30	0.847	No
2050	20.50	1.17	0.39	0.78	0.96	0.688	1.06	0.651	1.00	1.30	0.847	No
2051	20.51	1.18	0.39	0.78	0.96	0.688	1.06	0.651	1.00	1.30	0.847	No
2052	20.52	1.18	0.39	0.79	0.96	0.688	1.06	0.652	1.00	1.30	0.847	No
2053	20.53	1.18	0.39	0.79	0.96	0.688	1.06	0.652	1.00	1.30	0.847	No
2054	20.54	1.18	0.39	0.79	0.96	0.688	1.06	0.652	1.00	1.30	0.847	No
2055	20.55	1.18	0.39	0.79	0.96	0.689	1.06	0.652	1.00	1.30	0.847	No
2056	20.56	1.18	0.39	0.79	0.96	0.689	1.06	0.652	1.00	1.30	0.847	No
2057	20.57	1.18	0.39	0.79	0.96	0.689	1.06	0.652	1.00	1.30	0.848	No
2058	20.58	1.18	0.39	0.79	0.96	0.689	1.06	0.652	1.00	1.30	0.848	No
2059	20.59	1.18	0.39	0.79	0.96	0.689	1.06	0.652	1.00	1.30	0.848	No
2060	20.60	1.18	0.39	0.79	0.96	0.689	1.06	0.652	1.00	1.30	0.848	No
2061	20.61	1.18	0.39	0.79	0.96	0.689	1.06	0.652	1.00	1.30	0.848	No
2062	20.62	1.18	0.39	0.79	0.96	0.689	1.06	0.652	1.00	1.30	0.848	No
2063	20.63	1.18	0.39	0.79	0.96	0.689	1.06	0.652	1.00	1.30	0.848	No
2064	20.64	1.18	0.39	0.79	0.96	0.689	1.06	0.653	1.00	1.30	0.848	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
2065	20.65	1.18	0.39	0.79	0.96	0.689	1.06	0.653	1.00	1.30	0.848	No
2066	20.66	1.18	0.39	0.79	0.96	0.689	1.06	0.653	1.00	1.30	0.848	No
2067	20.67	1.18	0.40	0.79	0.96	0.690	1.06	0.653	1.00	1.30	0.849	No
2068	20.68	1.19	0.40	0.79	0.96	0.690	1.06	0.653	1.00	1.30	0.849	No
2069	20.69	1.19	0.40	0.79	0.96	0.690	1.06	0.653	1.00	1.30	0.849	No
2070	20.70	1.19	0.40	0.79	0.96	0.690	1.06	0.653	1.00	1.30	0.849	No
2071	20.71	1.19	0.40	0.79	0.96	0.690	1.06	0.653	1.00	1.30	0.849	No
2072	20.72	1.19	0.40	0.79	0.95	0.690	1.06	0.653	1.00	1.30	0.849	No
2073	20.73	1.19	0.40	0.79	0.95	0.690	1.06	0.653	1.00	1.30	0.849	No
2074	20.74	1.19	0.40	0.79	0.95	0.690	1.06	0.653	1.00	1.30	0.849	No
2075	20.75	1.19	0.40	0.79	0.95	0.690	1.06	0.653	1.00	1.30	0.849	No
2076	20.76	1.19	0.40	0.79	0.95	0.690	1.06	0.653	1.00	1.30	0.850	No
2077	20.77	1.19	0.40	0.79	0.95	0.690	1.06	0.654	1.00	1.30	0.850	No
2078	20.78	1.19	0.40	0.79	0.95	0.690	1.06	0.654	1.00	1.30	0.850	No
2079	20.79	1.19	0.40	0.79	0.95	0.691	1.06	0.654	1.00	1.30	0.850	No
2080	20.80	1.19	0.40	0.79	0.95	0.691	1.06	0.654	1.00	1.30	0.850	No
2081	20.81	1.19	0.40	0.79	0.95	0.691	1.06	0.654	1.00	1.30	0.850	No
2082	20.82	1.19	0.40	0.79	0.95	0.691	1.06	0.654	1.00	1.30	0.850	No
2083	20.83	1.19	0.40	0.79	0.95	0.691	1.06	0.654	1.00	1.30	0.850	No
2084	20.84	1.19	0.40	0.79	0.95	0.691	1.06	0.654	1.00	1.30	0.850	No
2085	20.85	1.19	0.40	0.79	0.95	0.691	1.06	0.654	1.00	1.30	0.850	No
2086	20.86	1.20	0.40	0.79	0.95	0.691	1.06	0.654	1.00	1.30	0.851	No
2087	20.87	1.20	0.40	0.79	0.95	0.691	1.06	0.654	1.00	1.30	0.851	No
2088	20.88	1.20	0.40	0.79	0.95	0.691	1.06	0.654	1.00	1.30	0.851	No
2089	20.89	1.20	0.40	0.79	0.95	0.691	1.06	0.655	1.00	1.30	0.851	No
2090	20.90	1.20	0.40	0.80	0.95	0.692	1.06	0.655	1.00	1.30	0.851	No
2091	20.91	1.20	0.40	0.80	0.95	0.692	1.06	0.655	1.00	1.30	0.851	No
2092	20.92	1.20	0.40	0.80	0.95	0.692	1.06	0.655	1.00	1.30	0.851	No
2093	20.93	1.20	0.40	0.80	0.95	0.692	1.06	0.655	1.00	1.30	0.851	No
2094	20.94	1.20	0.40	0.80	0.95	0.692	1.06	0.655	1.00	1.30	0.851	No
2095	20.95	1.20	0.40	0.80	0.95	0.692	1.06	0.655	1.00	1.30	0.852	No
2096	20.96	1.20	0.40	0.80	0.95	0.692	1.06	0.655	1.00	1.30	0.852	No
2097	20.97	1.20	0.40	0.80	0.95	0.692	1.06	0.655	1.00	1.30	0.852	No
2098	20.98	1.20	0.40	0.80	0.95	0.692	1.06	0.655	1.00	1.30	0.852	No
2099	20.99	1.20	0.41	0.80	0.95	0.692	1.06	0.655	1.00	1.30	0.852	No
2100	21.00	1.20	0.41	0.80	0.95	0.692	1.06	0.655	1.00	1.30	0.852	No
2101	21.01	1.20	0.41	0.80	0.95	0.692	1.06	0.656	1.00	1.30	0.852	No
2102	21.02	1.20	0.41	0.80	0.95	0.693	1.06	0.656	1.00	1.30	0.852	No
2103	21.03	1.20	0.41	0.80	0.95	0.693	1.06	0.656	1.00	1.30	0.852	No
2104	21.04	1.21	0.41	0.80	0.95	0.693	1.06	0.656	1.00	1.30	0.853	No
2105	21.05	1.21	0.41	0.80	0.95	0.693	1.06	0.656	1.00	1.30	0.853	No
2106	21.06	1.21	0.41	0.80	0.95	0.693	1.06	0.656	1.00	1.30	0.853	No
2107	21.07	1.21	0.41	0.80	0.95	0.693	1.06	0.656	1.00	1.30	0.853	No
2108	21.08	1.21	0.41	0.80	0.95	0.693	1.06	0.656	1.00	1.30	0.853	No
2109	21.09	1.21	0.41	0.80	0.95	0.693	1.06	0.656	1.00	1.30	0.853	No
2110	21.10	1.21	0.41	0.80	0.95	0.693	1.06	0.656	1.00	1.30	0.853	No
2111	21.11	1.21	0.41	0.80	0.95	0.693	1.06	0.656	1.00	1.30	0.853	No
2112	21.12	1.21	0.41	0.80	0.95	0.693	1.06	0.656	1.00	1.30	0.853	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
2113	21.13	1.21	0.41	0.80	0.95	0.694	1.06	0.657	1.00	1.30	0.854	No
2114	21.14	1.21	0.41	0.80	0.95	0.694	1.06	0.657	1.00	1.30	0.854	No
2115	21.15	1.21	0.41	0.80	0.95	0.694	1.06	0.657	1.00	1.30	0.854	No
2116	21.16	1.21	0.41	0.80	0.95	0.694	1.06	0.657	1.00	1.30	0.854	No
2117	21.17	1.21	0.41	0.80	0.95	0.694	1.06	0.657	1.00	1.30	0.854	No
2118	21.18	1.21	0.41	0.80	0.95	0.694	1.06	0.657	1.00	1.30	0.854	No
2119	21.19	1.21	0.41	0.80	0.95	0.694	1.06	0.657	1.00	1.30	0.854	No
2120	21.20	1.21	0.41	0.80	0.95	0.694	1.06	0.657	1.00	1.30	0.854	No
2121	21.21	1.21	0.41	0.80	0.95	0.694	1.06	0.657	1.00	1.30	0.854	No
2122	21.22	1.22	0.41	0.80	0.95	0.694	1.06	0.657	1.00	1.30	0.854	No
2123	21.23	1.22	0.41	0.80	0.95	0.694	1.06	0.657	1.00	1.30	0.855	No
2124	21.24	1.22	0.41	0.80	0.95	0.695	1.06	0.657	1.00	1.30	0.855	No
2125	21.25	1.22	0.41	0.80	0.95	0.695	1.06	0.658	1.00	1.30	0.855	No
2126	21.26	1.22	0.41	0.80	0.95	0.695	1.06	0.658	1.00	1.30	0.855	No
2127	21.27	1.22	0.41	0.80	0.95	0.695	1.06	0.658	1.00	1.30	0.855	No
2128	21.28	1.22	0.41	0.80	0.95	0.695	1.06	0.658	1.00	1.30	0.855	No
2129	21.29	1.22	0.41	0.80	0.95	0.695	1.06	0.658	1.00	1.30	0.855	No
2130	21.30	1.22	0.41	0.80	0.95	0.695	1.06	0.658	1.00	1.30	0.855	No
2131	21.31	1.22	0.42	0.81	0.95	0.695	1.06	0.658	1.00	1.30	0.855	No
2132	21.32	1.22	0.42	0.81	0.95	0.695	1.06	0.658	1.00	1.30	0.856	No
2133	21.33	1.22	0.42	0.81	0.95	0.695	1.06	0.658	1.00	1.30	0.856	No
2134	21.34	1.22	0.42	0.81	0.95	0.695	1.06	0.658	1.00	1.30	0.856	No
2135	21.35	1.22	0.42	0.81	0.95	0.695	1.06	0.658	1.00	1.30	0.856	No
2136	21.36	1.22	0.42	0.81	0.95	0.696	1.06	0.658	1.00	1.30	0.856	No
2137	21.37	1.22	0.42	0.81	0.95	0.696	1.06	0.658	1.00	1.30	0.856	No
2138	21.38	1.22	0.42	0.81	0.95	0.696	1.06	0.659	1.00	1.30	0.856	No
2139	21.39	1.22	0.42	0.81	0.95	0.696	1.06	0.659	1.00	1.30	0.856	No
2140	21.40	1.23	0.42	0.81	0.95	0.696	1.06	0.659	1.00	1.30	0.856	No
2141	21.41	1.23	0.42	0.81	0.95	0.696	1.06	0.659	1.00	1.30	0.856	No
2142	21.42	1.23	0.42	0.81	0.95	0.696	1.06	0.659	1.00	1.30	0.857	No
2143	21.43	1.23	0.42	0.81	0.95	0.696	1.06	0.659	1.00	1.30	0.857	No
2144	21.44	1.23	0.42	0.81	0.95	0.696	1.06	0.659	1.00	1.30	0.857	No
2145	21.45	1.23	0.42	0.81	0.95	0.696	1.06	0.659	1.00	1.30	0.857	No
2146	21.46	1.23	0.42	0.81	0.95	0.696	1.06	0.659	1.00	1.30	0.857	No
2147	21.47	1.23	0.42	0.81	0.95	0.696	1.06	0.659	1.00	1.30	0.857	No
2148	21.48	1.23	0.42	0.81	0.95	0.696	1.06	0.659	1.00	1.30	0.857	No
2149	21.49	1.23	0.42	0.81	0.95	0.697	1.06	0.659	1.00	1.30	0.857	No
2150	21.50	1.23	0.42	0.81	0.95	0.697	1.06	0.659	1.00	1.30	0.857	No
2151	21.51	1.23	0.42	0.81	0.95	0.697	1.06	0.660	1.00	1.30	0.857	No
2152	21.52	1.23	0.42	0.81	0.95	0.697	1.06	0.660	1.00	1.30	0.857	No
2153	21.53	1.23	0.42	0.81	0.95	0.697	1.06	0.660	1.00	1.30	0.858	No
2154	21.54	1.23	0.42	0.81	0.95	0.697	1.06	0.660	1.00	1.30	0.858	No
2155	21.55	1.23	0.42	0.81	0.95	0.697	1.06	0.660	1.00	1.30	0.858	No
2156	21.56	1.23	0.42	0.81	0.95	0.697	1.06	0.660	1.00	1.30	0.858	No
2157	21.57	1.24	0.42	0.81	0.95	0.697	1.06	0.660	1.00	1.30	0.858	No
2158	21.58	1.24	0.42	0.81	0.95	0.697	1.06	0.660	1.00	1.30	0.858	No
2159	21.59	1.24	0.42	0.81	0.95	0.697	1.06	0.660	1.00	1.30	0.858	No
2160	21.60	1.24	0.42	0.81	0.95	0.697	1.06	0.660	1.00	1.30	0.858	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
2161	21.61	1.24	0.42	0.81	0.95	0.697	1.06	0.660	1.00	1.30	0.858	No
2162	21.62	1.24	0.42	0.81	0.95	0.698	1.06	0.660	1.00	1.30	0.858	No
2163	21.63	1.24	0.43	0.81	0.95	0.698	1.06	0.660	1.00	1.30	0.858	No
2164	21.64	1.24	0.43	0.81	0.95	0.698	1.06	0.660	1.00	1.30	0.859	No
2165	21.65	1.24	0.43	0.81	0.95	0.698	1.06	0.661	1.00	1.30	0.859	No
2166	21.66	1.24	0.43	0.81	0.95	0.698	1.06	0.661	1.00	1.30	0.859	No
2167	21.67	1.24	0.43	0.81	0.95	0.698	1.06	0.661	1.00	1.30	0.859	No
2168	21.68	1.24	0.43	0.81	0.95	0.698	1.06	0.661	1.00	1.30	0.859	No
2169	21.69	1.24	0.43	0.82	0.95	0.698	1.06	0.661	1.00	1.30	0.859	No
2170	21.70	1.24	0.43	0.82	0.95	0.698	1.06	0.661	1.00	1.30	0.859	No
2171	21.71	1.24	0.43	0.82	0.95	0.698	1.06	0.661	1.00	1.30	0.859	No
2172	21.72	1.24	0.43	0.82	0.95	0.698	1.06	0.661	1.00	1.30	0.859	No
2173	21.73	1.24	0.43	0.82	0.95	0.698	1.06	0.661	1.00	1.30	0.859	No
2174	21.74	1.25	0.43	0.82	0.95	0.698	1.06	0.661	1.00	1.30	0.860	No
2175	21.75	1.25	0.43	0.82	0.95	0.699	1.06	0.661	1.00	1.30	0.860	No
2176	21.76	1.25	0.43	0.82	0.95	0.699	1.06	0.661	1.00	1.30	0.860	No
2177	21.77	1.25	0.43	0.82	0.95	0.699	1.06	0.661	1.00	1.30	0.860	No
2178	21.78	1.25	0.43	0.82	0.95	0.699	1.06	0.662	1.00	1.30	0.860	No
2179	21.79	1.25	0.43	0.82	0.95	0.699	1.06	0.662	1.00	1.30	0.860	No
2180	21.80	1.25	0.43	0.82	0.95	0.699	1.06	0.662	1.00	1.30	0.860	No
2181	21.81	1.25	0.43	0.82	0.95	0.699	1.06	0.662	1.00	1.30	0.860	No
2182	21.82	1.25	0.43	0.82	0.95	0.699	1.06	0.662	1.00	1.30	0.860	No
2183	21.83	1.25	0.43	0.82	0.95	0.699	1.06	0.662	1.00	1.30	0.860	No
2184	21.84	1.25	0.43	0.82	0.95	0.699	1.06	0.662	1.00	1.30	0.861	No
2185	21.85	1.25	0.43	0.82	0.95	0.699	1.06	0.662	1.00	1.30	0.861	No
2186	21.86	1.25	0.43	0.82	0.95	0.699	1.06	0.662	1.00	1.30	0.861	No
2187	21.87	1.25	0.43	0.82	0.95	0.700	1.06	0.662	1.00	1.30	0.861	No
2188	21.88	1.25	0.43	0.82	0.95	0.700	1.06	0.662	1.00	1.30	0.861	No
2189	21.89	1.25	0.43	0.82	0.95	0.700	1.06	0.662	1.00	1.30	0.861	No
2190	21.90	1.25	0.43	0.82	0.95	0.700	1.06	0.662	1.00	1.30	0.861	No
2191	21.91	1.25	0.43	0.82	0.95	0.700	1.06	0.663	1.00	1.30	0.861	No
2192	21.92	1.26	0.43	0.82	0.95	0.700	1.06	0.663	1.00	1.30	0.861	No
2193	21.93	1.26	0.43	0.82	0.95	0.700	1.06	0.663	1.00	1.30	0.861	No
2194	21.94	1.26	0.43	0.82	0.95	0.700	1.06	0.663	1.00	1.30	0.862	No
2195	21.95	1.26	0.44	0.82	0.95	0.700	1.06	0.663	1.00	1.30	0.862	No
2196	21.96	1.26	0.44	0.82	0.95	0.700	1.06	0.663	1.00	1.30	0.862	No
2197	21.97	1.26	0.44	0.82	0.95	0.700	1.06	0.663	1.00	1.30	0.862	No
2198	21.98	1.26	0.44	0.82	0.95	0.700	1.06	0.663	1.00	1.30	0.862	No
2199	21.99	1.26	0.44	0.82	0.95	0.701	1.06	0.663	1.00	1.30	0.862	No
2200	22.00	1.26	0.44	0.82	0.95	0.701	1.06	0.663	1.00	1.30	0.862	No
2201	22.01	1.26	0.44	0.82	0.95	0.701	1.06	0.663	1.00	1.30	0.862	No
2202	22.02	1.26	0.44	0.82	0.95	0.701	1.06	0.663	1.00	1.30	0.862	No
2203	22.03	1.26	0.44	0.82	0.95	0.701	1.06	0.664	1.00	1.30	0.863	No
2204	22.04	1.26	0.44	0.82	0.95	0.701	1.06	0.664	1.00	1.30	0.863	No
2205	22.05	1.26	0.44	0.82	0.95	0.701	1.06	0.664	1.00	1.30	0.863	No
2206	22.06	1.26	0.44	0.82	0.95	0.701	1.06	0.664	1.00	1.30	0.863	No
2207	22.07	1.26	0.44	0.82	0.95	0.701	1.06	0.664	1.00	1.30	0.863	No
2208	22.08	1.26	0.44	0.82	0.95	0.701	1.06	0.664	1.00	1.30	0.863	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
2209	22.09	1.26	0.44	0.82	0.95	0.701	1.06	0.664	1.00	1.30	0.863	No
2210	22.10	1.26	0.44	0.82	0.95	0.702	1.06	0.664	1.00	1.30	0.863	No
2211	22.11	1.27	0.44	0.82	0.95	0.702	1.06	0.664	1.00	1.30	0.863	No
2212	22.12	1.27	0.44	0.83	0.95	0.702	1.06	0.664	1.00	1.30	0.864	No
2213	22.13	1.27	0.44	0.83	0.95	0.702	1.06	0.664	1.00	1.30	0.864	No
2214	22.14	1.27	0.44	0.83	0.95	0.702	1.06	0.664	1.00	1.30	0.864	No
2215	22.15	1.27	0.44	0.83	0.95	0.702	1.06	0.665	1.00	1.30	0.864	No
2216	22.16	1.27	0.44	0.83	0.95	0.702	1.06	0.665	1.00	1.30	0.864	No
2217	22.17	1.27	0.44	0.83	0.95	0.702	1.06	0.665	1.00	1.30	0.864	No
2218	22.18	1.27	0.44	0.83	0.95	0.702	1.06	0.665	1.00	1.30	0.864	No
2219	22.19	1.27	0.44	0.83	0.95	0.702	1.06	0.665	1.00	1.30	0.864	No
2220	22.20	1.27	0.44	0.83	0.95	0.702	1.06	0.665	1.00	1.30	0.864	No
2221	22.21	1.27	0.44	0.83	0.95	0.703	1.06	0.665	1.00	1.30	0.865	No
2222	22.22	1.27	0.44	0.83	0.95	0.703	1.06	0.665	1.00	1.30	0.865	No
2223	22.23	1.27	0.44	0.83	0.95	0.703	1.06	0.665	1.00	1.30	0.865	No
2224	22.24	1.27	0.44	0.83	0.95	0.703	1.06	0.665	1.00	1.30	0.865	No
2225	22.25	1.27	0.44	0.83	0.95	0.703	1.06	0.665	1.00	1.30	0.865	No
2226	22.26	1.27	0.44	0.83	0.95	0.703	1.06	0.665	1.00	1.30	0.865	No
2227	22.27	1.27	0.45	0.83	0.95	0.703	1.06	0.666	1.00	1.30	0.865	No
2228	22.28	1.27	0.45	0.83	0.95	0.703	1.06	0.666	1.00	1.30	0.865	No
2229	22.29	1.27	0.45	0.83	0.95	0.703	1.06	0.666	1.00	1.30	0.865	No
2230	22.30	1.28	0.45	0.83	0.95	0.703	1.06	0.666	1.00	1.30	0.866	No
2231	22.31	1.28	0.45	0.83	0.95	0.703	1.06	0.666	1.00	1.30	0.866	No
2232	22.32	1.28	0.45	0.83	0.95	0.704	1.06	0.666	1.00	1.30	0.866	No
2233	22.33	1.28	0.45	0.83	0.95	0.704	1.06	0.666	1.00	1.30	0.866	No
2234	22.34	1.28	0.45	0.83	0.95	0.704	1.06	0.666	1.00	1.30	0.866	No
2235	22.35	1.28	0.45	0.83	0.95	0.704	1.06	0.666	1.00	1.30	0.866	No
2236	22.36	1.28	0.45	0.83	0.95	0.704	1.06	0.666	1.00	1.30	0.866	No
2237	22.37	1.28	0.45	0.83	0.95	0.704	1.06	0.666	1.00	1.30	0.866	No
2238	22.38	1.28	0.45	0.83	0.95	0.704	1.06	0.666	1.00	1.30	0.866	No
2239	22.39	1.28	0.45	0.83	0.95	0.704	1.06	0.667	1.00	1.30	0.867	No
2240	22.40	1.28	0.45	0.83	0.95	0.704	1.06	0.667	1.00	1.30	0.867	No
2241	22.41	1.28	0.45	0.83	0.95	0.704	1.06	0.667	1.00	1.30	0.867	No
2242	22.42	1.28	0.45	0.83	0.95	0.704	1.06	0.667	1.00	1.30	0.867	No
2243	22.43	1.28	0.45	0.83	0.95	0.704	1.06	0.667	1.00	1.30	0.867	No
2244	22.44	1.28	0.45	0.83	0.95	0.705	1.06	0.667	1.00	1.30	0.867	No
2245	22.45	1.28	0.45	0.83	0.95	0.705	1.06	0.667	1.00	1.30	0.867	No
2246	22.46	1.28	0.45	0.83	0.95	0.705	1.06	0.667	1.00	1.30	0.867	No
2247	22.47	1.28	0.45	0.83	0.95	0.705	1.06	0.667	1.00	1.30	0.867	No
2248	22.48	1.28	0.45	0.83	0.95	0.705	1.06	0.667	1.00	1.30	0.867	No
2249	22.49	1.28	0.45	0.83	0.95	0.705	1.06	0.667	1.00	1.30	0.868	No
2250	22.50	1.29	0.45	0.83	0.95	0.705	1.06	0.667	1.00	1.30	0.868	No
2251	22.51	1.29	0.45	0.83	0.95	0.705	1.06	0.668	1.00	1.30	0.868	No
2252	22.52	1.29	0.45	0.83	0.95	0.705	1.06	0.668	1.00	1.30	0.868	No
2253	22.53	1.29	0.45	0.83	0.95	0.705	1.06	0.668	1.00	1.30	0.868	No
2254	22.54	1.29	0.45	0.83	0.95	0.705	1.06	0.668	1.00	1.30	0.868	No
2255	22.55	1.29	0.45	0.83	0.95	0.706	1.06	0.668	1.00	1.30	0.868	No
2256	22.56	1.29	0.45	0.83	0.95	0.706	1.06	0.668	1.00	1.30	0.868	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
2257	22.57	1.29	0.45	0.83	0.95	0.706	1.06	0.668	1.00	1.30	0.868	No
2258	22.58	1.29	0.45	0.83	0.95	0.706	1.06	0.668	1.00	1.30	0.869	No
2259	22.59	1.29	0.46	0.83	0.95	0.706	1.06	0.668	1.00	1.30	0.869	No
2260	22.60	1.29	0.46	0.84	0.95	0.706	1.06	0.668	1.00	1.30	0.869	No
2261	22.61	1.29	0.46	0.84	0.95	0.706	1.06	0.668	1.00	1.30	0.869	No
2262	22.62	1.29	0.46	0.84	0.95	0.706	1.06	0.668	1.00	1.30	0.869	No
2263	22.63	1.29	0.46	0.84	0.95	0.706	1.06	0.668	1.00	1.30	0.869	No
2264	22.64	1.29	0.46	0.84	0.95	0.706	1.06	0.669	1.00	1.30	0.869	No
2265	22.65	1.29	0.46	0.84	0.95	0.706	1.06	0.669	1.00	1.30	0.869	No
2266	22.66	1.29	0.46	0.84	0.95	0.706	1.06	0.669	1.00	1.30	0.869	No
2267	22.67	1.29	0.46	0.84	0.95	0.707	1.06	0.669	1.00	1.30	0.869	No
2268	22.68	1.29	0.46	0.84	0.95	0.707	1.06	0.669	1.00	1.30	0.870	No
2269	22.69	1.30	0.46	0.84	0.95	0.707	1.06	0.669	1.00	1.30	0.870	No
2270	22.70	1.30	0.46	0.84	0.95	0.707	1.06	0.669	1.00	1.30	0.870	No
2271	22.71	1.30	0.46	0.84	0.95	0.707	1.06	0.669	1.00	1.30	0.870	No
2272	22.72	1.30	0.46	0.84	0.95	0.707	1.06	0.669	1.00	1.30	0.870	No
2273	22.73	1.30	0.46	0.84	0.95	0.707	1.06	0.669	1.00	1.30	0.870	No
2274	22.74	1.30	0.46	0.84	0.95	0.707	1.06	0.669	1.00	1.30	0.870	No
2275	22.75	1.30	0.46	0.84	0.95	0.707	1.06	0.669	1.00	1.30	0.870	No
2276	22.76	1.30	0.46	0.84	0.95	0.707	1.06	0.670	1.00	1.30	0.870	No
2277	22.77	1.30	0.46	0.84	0.95	0.707	1.06	0.670	1.00	1.30	0.870	No
2278	22.78	1.30	0.46	0.84	0.95	0.707	1.06	0.670	1.00	1.30	0.871	No
2279	22.79	1.30	0.46	0.84	0.95	0.708	1.06	0.670	1.00	1.30	0.871	No
2280	22.80	1.30	0.46	0.84	0.95	0.708	1.06	0.670	1.00	1.30	0.871	No
2281	22.81	1.30	0.46	0.84	0.95	0.708	1.06	0.670	1.00	1.30	0.871	No
2282	22.82	1.30	0.46	0.84	0.95	0.708	1.06	0.670	1.00	1.30	0.871	No
2283	22.83	1.30	0.46	0.84	0.95	0.708	1.06	0.670	1.00	1.30	0.871	No
2284	22.84	1.30	0.46	0.84	0.95	0.708	1.06	0.670	1.00	1.30	0.871	No
2285	22.85	1.30	0.46	0.84	0.95	0.708	1.06	0.670	1.00	1.30	0.871	No
2286	22.86	1.30	0.46	0.84	0.95	0.708	1.06	0.670	1.00	1.30	0.871	No
2287	22.87	1.30	0.46	0.84	0.95	0.708	1.06	0.670	1.00	1.30	0.872	No
2288	22.88	1.31	0.46	0.84	0.95	0.708	1.06	0.670	1.00	1.30	0.872	No
2289	22.89	1.31	0.46	0.84	0.95	0.708	1.06	0.671	1.00	1.30	0.872	No
2290	22.90	1.31	0.46	0.84	0.95	0.708	1.06	0.671	1.00	1.30	0.872	No
2291	22.91	1.31	0.47	0.84	0.95	0.709	1.06	0.671	1.00	1.30	0.872	No
2292	22.92	1.31	0.47	0.84	0.95	0.709	1.06	0.671	1.00	1.30	0.872	No
2293	22.93	1.31	0.47	0.84	0.95	0.709	1.06	0.671	1.00	1.30	0.872	No
2294	22.94	1.31	0.47	0.84	0.95	0.709	1.06	0.671	1.00	1.30	0.872	No
2295	22.95	1.31	0.47	0.84	0.95	0.709	1.06	0.671	1.00	1.30	0.872	No
2296	22.96	1.31	0.47	0.84	0.95	0.709	1.06	0.671	1.00	1.30	0.872	No
2297	22.97	1.31	0.47	0.84	0.95	0.709	1.06	0.671	1.00	1.30	0.873	No
2298	22.98	1.31	0.47	0.84	0.95	0.709	1.06	0.671	1.00	1.30	0.873	No
2299	22.99	1.31	0.47	0.84	0.95	0.709	1.06	0.671	1.00	1.30	0.873	No
2300	23.00	1.31	0.47	0.84	0.95	0.709	1.06	0.671	1.00	1.30	0.873	No
2301	23.01	1.31	0.47	0.84	0.95	0.709	1.06	0.672	1.00	1.30	0.873	No
2302	23.02	1.31	0.47	0.84	0.95	0.709	1.06	0.672	1.00	1.30	0.873	No
2303	23.03	1.31	0.47	0.84	0.95	0.710	1.06	0.672	1.00	1.30	0.873	No
2304	23.04	1.31	0.47	0.84	0.95	0.710	1.06	0.672	1.00	1.30	0.873	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
2305	23.05	1.31	0.47	0.84	0.95	0.710	1.06	0.672	1.00	1.30	0.873	No
2306	23.06	1.31	0.47	0.84	0.95	0.710	1.06	0.672	1.00	1.30	0.873	No
2307	23.07	1.32	0.47	0.85	0.95	0.710	1.06	0.672	1.00	1.30	0.874	No
2308	23.08	1.32	0.47	0.85	0.95	0.710	1.06	0.672	1.00	1.30	0.874	No
2309	23.09	1.32	0.47	0.85	0.95	0.710	1.06	0.672	1.00	1.30	0.874	No
2310	23.10	1.32	0.47	0.85	0.95	0.710	1.06	0.672	1.00	1.30	0.874	No
2311	23.11	1.32	0.47	0.85	0.95	0.710	1.06	0.672	1.00	1.30	0.874	No
2312	23.12	1.32	0.47	0.85	0.95	0.710	1.06	0.672	1.00	1.30	0.874	No
2313	23.13	1.32	0.47	0.85	0.95	0.710	1.06	0.672	1.00	1.30	0.874	No
2314	23.14	1.32	0.47	0.85	0.95	0.710	1.06	0.673	1.00	1.30	0.874	No
2315	23.15	1.32	0.47	0.85	0.95	0.710	1.06	0.673	1.00	1.30	0.874	No
2316	23.16	1.32	0.47	0.85	0.95	0.711	1.06	0.673	1.00	1.30	0.874	No
2317	23.17	1.32	0.47	0.85	0.95	0.711	1.06	0.673	1.00	1.30	0.875	No
2318	23.18	1.32	0.47	0.85	0.95	0.711	1.06	0.673	1.00	1.30	0.875	No
2319	23.19	1.32	0.47	0.85	0.95	0.711	1.06	0.673	1.00	1.30	0.875	No
2320	23.20	1.32	0.47	0.85	0.95	0.711	1.06	0.673	1.00	1.30	0.875	No
2321	23.21	1.32	0.47	0.85	0.95	0.711	1.06	0.673	1.00	1.30	0.875	No
2322	23.22	1.32	0.47	0.85	0.95	0.711	1.06	0.673	1.00	1.30	0.875	No
2323	23.23	1.32	0.48	0.85	0.95	0.711	1.06	0.673	1.00	1.30	0.875	No
2324	23.24	1.32	0.48	0.85	0.95	0.711	1.06	0.673	1.00	1.30	0.875	No
2325	23.25	1.32	0.48	0.85	0.95	0.711	1.06	0.673	1.00	1.30	0.875	No
2326	23.26	1.33	0.48	0.85	0.95	0.711	1.06	0.673	1.00	1.30	0.875	No
2327	23.27	1.33	0.48	0.85	0.95	0.711	1.06	0.673	1.00	1.30	0.875	No
2328	23.28	1.33	0.48	0.85	0.95	0.711	1.06	0.674	1.00	1.30	0.876	No
2329	23.29	1.33	0.48	0.85	0.95	0.712	1.06	0.674	1.00	1.30	0.876	No
2330	23.30	1.33	0.48	0.85	0.95	0.712	1.06	0.674	1.00	1.30	0.876	No
2331	23.31	1.33	0.48	0.85	0.95	0.712	1.06	0.674	1.00	1.30	0.876	No
2332	23.32	1.33	0.48	0.85	0.95	0.712	1.06	0.674	1.00	1.30	0.876	No
2333	23.33	1.33	0.48	0.85	0.95	0.712	1.06	0.674	1.00	1.30	0.876	No
2334	23.34	1.33	0.48	0.85	0.95	0.712	1.06	0.674	1.00	1.30	0.876	No
2335	23.35	1.33	0.48	0.85	0.95	0.712	1.06	0.674	1.00	1.30	0.876	No
2336	23.36	1.33	0.48	0.85	0.95	0.712	1.06	0.674	1.00	1.30	0.876	No
2337	23.37	1.33	0.48	0.85	0.95	0.712	1.06	0.674	1.00	1.30	0.876	No
2338	23.38	1.33	0.48	0.85	0.95	0.712	1.06	0.674	1.00	1.30	0.876	No
2339	23.39	1.33	0.48	0.85	0.95	0.712	1.06	0.674	1.00	1.30	0.877	No
2340	23.40	1.33	0.48	0.85	0.95	0.712	1.06	0.674	1.00	1.30	0.877	No
2341	23.41	1.33	0.48	0.85	0.95	0.712	1.06	0.674	1.00	1.30	0.877	No
2342	23.42	1.33	0.48	0.85	0.95	0.712	1.06	0.674	1.00	1.30	0.877	No
2343	23.43	1.33	0.48	0.85	0.95	0.713	1.06	0.675	1.00	1.30	0.877	No
2344	23.44	1.34	0.48	0.85	0.95	0.713	1.06	0.675	1.00	1.30	0.877	No
2345	23.45	1.34	0.48	0.85	0.95	0.713	1.06	0.675	1.00	1.30	0.877	No
2346	23.46	1.34	0.48	0.85	0.95	0.713	1.06	0.675	1.00	1.30	0.877	No
2347	23.47	1.34	0.48	0.85	0.95	0.713	1.06	0.675	1.00	1.30	0.877	No
2348	23.48	1.34	0.48	0.85	0.95	0.713	1.06	0.675	1.00	1.30	0.877	No
2349	23.49	1.34	0.48	0.85	0.95	0.713	1.06	0.675	1.00	1.30	0.877	No
2350	23.50	1.34	0.48	0.86	0.95	0.713	1.06	0.675	1.00	1.30	0.877	No
2351	23.51	1.34	0.48	0.86	0.95	0.713	1.06	0.675	1.00	1.30	0.878	No
2352	23.52	1.34	0.48	0.86	0.95	0.713	1.06	0.675	1.00	1.30	0.878	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
2353	23.53	1.34	0.48	0.86	0.95	0.713	1.06	0.675	1.00	1.30	0.878	No
2354	23.54	1.34	0.48	0.86	0.95	0.713	1.06	0.675	1.00	1.30	0.878	No
2355	23.55	1.34	0.49	0.86	0.95	0.713	1.06	0.675	1.00	1.30	0.878	No
2356	23.56	1.34	0.49	0.86	0.95	0.713	1.06	0.675	1.00	1.30	0.878	No
2357	23.57	1.34	0.49	0.86	0.95	0.714	1.06	0.675	1.00	1.30	0.878	No
2358	23.58	1.34	0.49	0.86	0.95	0.714	1.06	0.675	1.00	1.30	0.878	No
2359	23.59	1.34	0.49	0.86	0.95	0.714	1.06	0.676	1.00	1.30	0.878	No
2360	23.60	1.34	0.49	0.86	0.95	0.714	1.06	0.676	1.00	1.30	0.878	No
2361	23.61	1.34	0.49	0.86	0.95	0.714	1.06	0.676	1.00	1.30	0.878	No
2362	23.62	1.35	0.49	0.86	0.95	0.714	1.06	0.676	1.00	1.30	0.878	No
2363	23.63	1.35	0.49	0.86	0.95	0.714	1.06	0.676	1.00	1.30	0.879	No
2364	23.64	1.35	0.49	0.86	0.95	0.714	1.06	0.676	1.00	1.30	0.879	No
2365	23.65	1.35	0.49	0.86	0.95	0.714	1.06	0.676	1.00	1.30	0.879	No
2366	23.66	1.35	0.49	0.86	0.95	0.714	1.06	0.676	1.00	1.30	0.879	No
2367	23.67	1.35	0.49	0.86	0.95	0.714	1.06	0.676	1.00	1.30	0.879	No
2368	23.68	1.35	0.49	0.86	0.95	0.714	1.06	0.676	1.00	1.30	0.879	No
2369	23.69	1.35	0.49	0.86	0.95	0.714	1.06	0.676	1.00	1.30	0.879	No
2370	23.70	1.35	0.49	0.86	0.95	0.714	1.06	0.676	1.00	1.30	0.879	No
2371	23.71	1.35	0.49	0.86	0.95	0.714	1.06	0.676	1.00	1.30	0.879	No
2372	23.72	1.35	0.49	0.86	0.95	0.714	1.06	0.676	1.00	1.30	0.879	No
2373	23.73	1.35	0.49	0.86	0.95	0.715	1.06	0.676	1.00	1.30	0.879	No
2374	23.74	1.35	0.49	0.86	0.95	0.715	1.06	0.676	1.00	1.30	0.879	No
2375	23.75	1.35	0.49	0.86	0.95	0.715	1.06	0.677	1.00	1.30	0.880	No
2376	23.76	1.35	0.49	0.86	0.95	0.715	1.06	0.677	1.00	1.30	0.880	No
2377	23.77	1.35	0.49	0.86	0.95	0.715	1.06	0.677	1.00	1.30	0.880	No
2378	23.78	1.35	0.49	0.86	0.95	0.715	1.06	0.677	1.00	1.30	0.880	No
2379	23.79	1.35	0.49	0.86	0.95	0.715	1.06	0.677	1.00	1.30	0.880	No
2380	23.80	1.36	0.49	0.86	0.95	0.715	1.06	0.677	1.00	1.30	0.880	No
2381	23.81	1.36	0.49	0.86	0.95	0.715	1.06	0.677	1.00	1.30	0.880	No
2382	23.82	1.36	0.49	0.86	0.95	0.715	1.06	0.677	1.00	1.30	0.880	No
2383	23.83	1.36	0.49	0.86	0.95	0.715	1.06	0.677	1.00	1.30	0.880	No
2384	23.84	1.36	0.49	0.86	0.95	0.715	1.06	0.677	1.00	1.30	0.880	No
2385	23.85	1.36	0.49	0.86	0.95	0.715	1.06	0.677	1.00	1.30	0.880	No
2386	23.86	1.36	0.49	0.86	0.95	0.715	1.06	0.677	1.00	1.30	0.880	No
2387	23.87	1.36	0.50	0.86	0.95	0.715	1.06	0.677	1.00	1.30	0.880	No
2388	23.88	1.36	0.50	0.86	0.95	0.715	1.06	0.677	1.00	1.30	0.880	No
2389	23.89	1.36	0.50	0.86	0.95	0.716	1.06	0.677	1.00	1.30	0.881	No
2390	23.90	1.36	0.50	0.87	0.95	0.716	1.06	0.677	1.00	1.30	0.881	No
2391	23.91	1.36	0.50	0.87	0.95	0.716	1.06	0.677	1.00	1.30	0.881	No
2392	23.92	1.36	0.50	0.87	0.95	0.716	1.06	0.678	1.00	1.30	0.881	No
2393	23.93	1.36	0.50	0.87	0.95	0.716	1.06	0.678	1.00	1.30	0.881	No
2394	23.94	1.36	0.50	0.87	0.95	0.716	1.06	0.678	1.00	1.30	0.881	No
2395	23.95	1.36	0.50	0.87	0.95	0.716	1.06	0.678	1.00	1.30	0.881	No
2396	23.96	1.36	0.50	0.87	0.95	0.716	1.06	0.678	1.00	1.30	0.881	No
2397	23.97	1.37	0.50	0.87	0.95	0.716	1.06	0.678	1.00	1.30	0.881	No
2398	23.98	1.37	0.50	0.87	0.95	0.716	1.06	0.678	1.00	1.30	0.881	No
2399	23.99	1.37	0.50	0.87	0.95	0.716	1.06	0.678	1.00	1.30	0.881	No
2400	24.00	1.37	0.50	0.87	0.95	0.716	1.06	0.678	1.00	1.30	0.881	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
2401	24.01	1.37	0.50	0.87	0.95	0.716	1.06	0.678	1.00	1.30	0.881	No
2402	24.02	1.37	0.50	0.87	0.95	0.716	1.06	0.678	1.00	1.30	0.881	No
2403	24.03	1.37	0.50	0.87	0.95	0.716	1.06	0.678	1.00	1.30	0.882	No
2404	24.04	1.37	0.50	0.87	0.95	0.716	1.06	0.678	1.00	1.30	0.882	No
2405	24.05	1.37	0.50	0.87	0.95	0.716	1.06	0.678	1.00	1.30	0.882	No
2406	24.06	1.37	0.50	0.87	0.95	0.717	1.06	0.678	1.00	1.30	0.882	No
2407	24.07	1.37	0.50	0.87	0.95	0.717	1.06	0.678	1.00	1.30	0.882	No
2408	24.08	1.37	0.50	0.87	0.94	0.717	1.06	0.678	1.00	1.30	0.882	No
2409	24.09	1.37	0.50	0.87	0.94	0.717	1.06	0.678	1.00	1.30	0.882	No
2410	24.10	1.37	0.50	0.87	0.94	0.717	1.06	0.679	1.00	1.30	0.882	No
2411	24.11	1.37	0.50	0.87	0.94	0.717	1.06	0.679	1.00	1.30	0.882	No
2412	24.12	1.37	0.50	0.87	0.94	0.717	1.06	0.679	1.00	1.30	0.882	No
2413	24.13	1.37	0.50	0.87	0.94	0.717	1.06	0.679	1.00	1.30	0.882	No
2414	24.14	1.38	0.50	0.87	0.94	0.717	1.06	0.679	1.00	1.30	0.882	No
2415	24.15	1.38	0.50	0.87	0.94	0.717	1.06	0.679	1.00	1.30	0.882	No
2416	24.16	1.38	0.50	0.87	0.94	0.717	1.06	0.679	1.00	1.30	0.882	No
2417	24.17	1.38	0.50	0.87	0.94	0.717	1.06	0.679	1.00	1.30	0.883	No
2418	24.18	1.38	0.50	0.87	0.94	0.717	1.06	0.679	1.00	1.30	0.883	No
2419	24.19	1.38	0.51	0.87	0.94	0.717	1.06	0.679	1.00	1.30	0.883	No
2420	24.20	1.38	0.51	0.87	0.94	0.717	1.06	0.679	1.00	1.30	0.883	No
2421	24.21	1.38	0.51	0.87	0.94	0.717	1.06	0.679	1.00	1.30	0.883	No
2422	24.22	1.38	0.51	0.87	0.94	0.717	1.06	0.679	1.00	1.30	0.883	No
2423	24.23	1.38	0.51	0.87	0.94	0.718	1.06	0.679	1.00	1.30	0.883	No
2424	24.24	1.38	0.51	0.87	0.94	0.718	1.06	0.679	1.00	1.30	0.883	No
2425	24.25	1.38	0.51	0.87	0.94	0.718	1.06	0.679	1.00	1.30	0.883	No
2426	24.26	1.38	0.51	0.87	0.94	0.718	1.06	0.679	1.00	1.30	0.883	No
2427	24.27	1.38	0.51	0.87	0.94	0.718	1.06	0.679	1.00	1.30	0.883	No
2428	24.28	1.38	0.51	0.88	0.94	0.718	1.06	0.680	1.00	1.30	0.883	No
2429	24.29	1.38	0.51	0.88	0.94	0.718	1.06	0.680	1.00	1.30	0.883	No
2430	24.30	1.38	0.51	0.88	0.94	0.718	1.06	0.680	1.00	1.30	0.884	No
2431	24.31	1.38	0.51	0.88	0.94	0.718	1.06	0.680	1.00	1.30	0.884	No
2432	24.32	1.39	0.51	0.88	0.94	0.718	1.06	0.680	1.00	1.30	0.884	No
2433	24.33	1.39	0.51	0.88	0.94	0.718	1.06	0.680	1.00	1.30	0.884	No
2434	24.34	1.39	0.51	0.88	0.94	0.718	1.06	0.680	1.00	1.30	0.884	No
2435	24.35	1.39	0.51	0.88	0.94	0.718	1.06	0.680	1.00	1.30	0.884	No
2436	24.36	1.39	0.51	0.88	0.94	0.718	1.06	0.680	1.00	1.30	0.884	No
2437	24.37	1.39	0.51	0.88	0.94	0.718	1.06	0.680	1.00	1.30	0.884	No
2438	24.38	1.39	0.51	0.88	0.94	0.718	1.06	0.680	1.00	1.30	0.884	No
2439	24.39	1.39	0.51	0.88	0.94	0.718	1.06	0.680	1.00	1.30	0.884	No
2440	24.40	1.39	0.51	0.88	0.94	0.719	1.06	0.680	1.00	1.30	0.884	No
2441	24.41	1.39	0.51	0.88	0.94	0.719	1.06	0.680	1.00	1.30	0.884	No
2442	24.42	1.39	0.51	0.88	0.94	0.719	1.06	0.680	1.00	1.30	0.884	No
2443	24.43	1.39	0.51	0.88	0.94	0.719	1.06	0.680	1.00	1.30	0.884	No
2444	24.44	1.39	0.51	0.88	0.94	0.719	1.06	0.680	1.00	1.30	0.885	No
2445	24.45	1.39	0.51	0.88	0.94	0.719	1.06	0.680	1.00	1.30	0.885	No
2446	24.46	1.39	0.51	0.88	0.94	0.719	1.06	0.680	1.00	1.30	0.885	No
2447	24.47	1.39	0.51	0.88	0.94	0.719	1.06	0.681	1.00	1.30	0.885	No
2448	24.48	1.39	0.51	0.88	0.94	0.719	1.06	0.681	1.00	1.30	0.885	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
2449	24.49	1.40	0.51	0.88	0.94	0.719	1.06	0.681	1.00	1.30	0.885	No
2450	24.50	1.40	0.51	0.88	0.94	0.719	1.06	0.681	1.00	1.30	0.885	No
2451	24.51	1.40	0.52	0.88	0.94	0.719	1.06	0.681	1.00	1.30	0.885	No
2452	24.52	1.40	0.52	0.88	0.94	0.719	1.06	0.681	1.00	1.30	0.885	No
2453	24.53	1.40	0.52	0.88	0.94	0.719	1.06	0.681	1.00	1.30	0.885	No
2454	24.54	1.40	0.52	0.88	0.94	0.719	1.06	0.681	1.00	1.30	0.885	No
2455	24.55	1.40	0.52	0.88	0.94	0.719	1.06	0.681	1.00	1.30	0.885	No
2456	24.56	1.40	0.52	0.88	0.94	0.719	1.06	0.681	1.00	1.30	0.885	No
2457	24.57	1.40	0.52	0.88	0.94	0.719	1.06	0.681	1.00	1.30	0.885	No
2458	24.58	1.40	0.52	0.88	0.94	0.720	1.06	0.681	1.00	1.30	0.885	No
2459	24.59	1.40	0.52	0.88	0.94	0.720	1.06	0.681	1.00	1.30	0.886	No
2460	24.60	1.40	0.52	0.88	0.94	0.720	1.06	0.681	1.00	1.30	0.886	No
2461	24.61	1.40	0.52	0.88	0.94	0.720	1.06	0.681	1.00	1.30	0.886	No
2462	24.62	1.40	0.52	0.88	0.94	0.720	1.06	0.681	1.00	1.30	0.886	No
2463	24.63	1.40	0.52	0.88	0.94	0.720	1.06	0.681	1.00	1.30	0.886	No
2464	24.64	1.40	0.52	0.88	0.94	0.720	1.06	0.681	1.00	1.30	0.886	No
2465	24.65	1.40	0.52	0.88	0.94	0.720	1.06	0.681	1.00	1.30	0.886	No
2466	24.66	1.40	0.52	0.89	0.94	0.720	1.06	0.682	1.00	1.30	0.886	No
2467	24.67	1.41	0.52	0.89	0.94	0.720	1.06	0.682	1.00	1.30	0.886	No
2468	24.68	1.41	0.52	0.89	0.94	0.720	1.06	0.682	1.00	1.30	0.886	No
2469	24.69	1.41	0.52	0.89	0.94	0.720	1.06	0.682	1.00	1.30	0.886	No
2470	24.70	1.41	0.52	0.89	0.94	0.720	1.06	0.682	1.00	1.30	0.886	No
2471	24.71	1.41	0.52	0.89	0.94	0.720	1.06	0.682	1.00	1.30	0.886	No
2472	24.72	1.41	0.52	0.89	0.94	0.720	1.06	0.682	1.00	1.30	0.886	No
2473	24.73	1.41	0.52	0.89	0.94	0.720	1.06	0.682	1.00	1.30	0.886	No
2474	24.74	1.41	0.52	0.89	0.94	0.720	1.06	0.682	1.00	1.30	0.887	No
2475	24.75	1.41	0.52	0.89	0.94	0.720	1.06	0.682	1.00	1.30	0.887	No
2476	24.76	1.41	0.52	0.89	0.94	0.721	1.06	0.682	1.00	1.30	0.887	No
2477	24.77	1.41	0.52	0.89	0.94	0.721	1.06	0.682	1.00	1.30	0.887	No
2478	24.78	1.41	0.52	0.89	0.94	0.721	1.06	0.682	1.00	1.30	0.887	No
2479	24.79	1.41	0.52	0.89	0.94	0.721	1.06	0.682	1.00	1.30	0.887	No
2480	24.80	1.41	0.52	0.89	0.94	0.721	1.06	0.682	1.00	1.30	0.887	No
2481	24.81	1.41	0.52	0.89	0.94	0.721	1.06	0.682	1.00	1.30	0.887	No
2482	24.82	1.41	0.52	0.89	0.94	0.721	1.06	0.682	1.00	1.30	0.887	No
2483	24.83	1.41	0.53	0.89	0.94	0.721	1.06	0.682	1.00	1.30	0.887	No
2484	24.84	1.42	0.53	0.89	0.94	0.721	1.06	0.682	1.00	1.30	0.887	No
2485	24.85	1.42	0.53	0.89	0.94	0.721	1.06	0.683	1.00	1.30	0.887	No
2486	24.86	1.42	0.53	0.89	0.94	0.721	1.06	0.683	1.00	1.30	0.887	No
2487	24.87	1.42	0.53	0.89	0.94	0.721	1.06	0.683	1.00	1.30	0.887	No
2488	24.88	1.42	0.53	0.89	0.94	0.721	1.06	0.683	1.00	1.30	0.888	No
2489	24.89	1.42	0.53	0.89	0.94	0.721	1.06	0.683	1.00	1.30	0.888	No
2490	24.90	1.42	0.53	0.89	0.94	0.721	1.06	0.683	1.00	1.30	0.888	No
2491	24.91	1.42	0.53	0.89	0.94	0.721	1.06	0.683	1.00	1.30	0.888	No
2492	24.92	1.42	0.53	0.89	0.94	0.721	1.06	0.683	1.00	1.30	0.888	No
2493	24.93	1.42	0.53	0.89	0.94	0.721	1.06	0.683	1.00	1.30	0.888	No
2494	24.94	1.42	0.53	0.89	0.94	0.722	1.06	0.683	1.00	1.30	0.888	No
2495	24.95	1.42	0.53	0.89	0.94	0.722	1.06	0.683	1.00	1.30	0.888	No
2496	24.96	1.42	0.53	0.89	0.94	0.722	1.06	0.683	1.00	1.30	0.888	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
2497	24.97	1.42	0.53	0.89	0.94	0.722	1.06	0.683	1.00	1.30	0.888	No
2498	24.98	1.42	0.53	0.89	0.94	0.722	1.06	0.683	1.00	1.30	0.888	No
2499	24.99	1.42	0.53	0.89	0.94	0.722	1.06	0.683	1.00	1.30	0.888	No
2500	25.00	1.42	0.53	0.89	0.94	0.722	1.06	0.683	1.00	1.30	0.888	No
2501	25.01	1.42	0.53	0.89	0.94	0.722	1.06	0.683	1.00	1.30	0.888	No
2502	25.02	1.43	0.53	0.89	0.94	0.722	1.06	0.683	1.00	1.30	0.889	No
2503	25.03	1.43	0.53	0.89	0.94	0.722	1.06	0.684	1.00	1.30	0.889	No
2504	25.04	1.43	0.53	0.89	0.94	0.722	1.06	0.684	1.00	1.30	0.889	No
2505	25.05	1.43	0.53	0.89	0.94	0.722	1.06	0.684	1.00	1.30	0.889	No
2506	25.06	1.43	0.53	0.90	0.94	0.722	1.06	0.684	1.00	1.30	0.889	No
2507	25.07	1.43	0.53	0.90	0.94	0.722	1.06	0.684	1.00	1.30	0.889	No
2508	25.08	1.43	0.53	0.90	0.94	0.722	1.06	0.684	1.00	1.30	0.889	No
2509	25.09	1.43	0.53	0.90	0.94	0.722	1.06	0.684	1.00	1.30	0.889	No
2510	25.10	1.43	0.53	0.90	0.94	0.722	1.06	0.684	1.00	1.30	0.889	No
2511	25.11	1.43	0.53	0.90	0.94	0.723	1.06	0.684	1.00	1.30	0.889	No
2512	25.12	1.43	0.53	0.90	0.94	0.723	1.06	0.684	1.00	1.30	0.889	No
2513	25.13	1.43	0.53	0.90	0.94	0.723	1.06	0.684	1.00	1.30	0.889	No
2514	25.14	1.43	0.53	0.90	0.94	0.723	1.06	0.684	1.00	1.30	0.889	No
2515	25.15	1.43	0.54	0.90	0.94	0.723	1.06	0.684	1.00	1.30	0.889	No
2516	25.16	1.43	0.54	0.90	0.94	0.723	1.06	0.684	1.00	1.30	0.890	No
2517	25.17	1.43	0.54	0.90	0.94	0.723	1.06	0.684	1.00	1.30	0.890	No
2518	25.18	1.43	0.54	0.90	0.94	0.723	1.06	0.684	1.00	1.30	0.890	No
2519	25.19	1.43	0.54	0.90	0.94	0.723	1.06	0.684	1.00	1.30	0.890	No
2520	25.20	1.43	0.54	0.90	0.94	0.723	1.06	0.685	1.00	1.30	0.890	No
2521	25.21	1.44	0.54	0.90	0.94	0.723	1.06	0.685	1.00	1.30	0.890	No
2522	25.22	1.44	0.54	0.90	0.94	0.723	1.06	0.685	1.00	1.30	0.890	No
2523	25.23	1.44	0.54	0.90	0.94	0.723	1.06	0.685	1.00	1.30	0.890	No
2524	25.24	1.44	0.54	0.90	0.94	0.723	1.06	0.685	1.00	1.30	0.890	No
2525	25.25	1.44	0.54	0.90	0.94	0.723	1.06	0.685	1.00	1.30	0.890	No
2526	25.26	1.44	0.54	0.90	0.94	0.723	1.06	0.685	1.00	1.30	0.890	No
2527	25.27	1.44	0.54	0.90	0.94	0.724	1.06	0.685	1.00	1.30	0.890	No
2528	25.28	1.44	0.54	0.90	0.94	0.724	1.06	0.685	1.00	1.30	0.890	No
2529	25.29	1.44	0.54	0.90	0.94	0.724	1.06	0.685	1.00	1.30	0.891	No
2530	25.30	1.44	0.54	0.90	0.94	0.724	1.06	0.685	1.00	1.30	0.891	No
2531	25.31	1.44	0.54	0.90	0.94	0.724	1.06	0.685	1.00	1.30	0.891	No
2532	25.32	1.44	0.54	0.90	0.94	0.724	1.06	0.685	1.00	1.30	0.891	No
2533	25.33	1.44	0.54	0.90	0.94	0.724	1.06	0.685	1.00	1.30	0.891	No
2534	25.34	1.44	0.54	0.90	0.94	0.724	1.06	0.685	1.00	1.30	0.891	No
2535	25.35	1.44	0.54	0.90	0.94	0.724	1.06	0.685	1.00	1.30	0.891	No
2536	25.36	1.44	0.54	0.90	0.94	0.724	1.06	0.685	1.00	1.30	0.891	No
2537	25.37	1.44	0.54	0.90	0.94	0.724	1.06	0.686	1.00	1.30	0.891	No
2538	25.38	1.44	0.54	0.90	0.94	0.724	1.06	0.686	1.00	1.30	0.891	No
2539	25.39	1.45	0.54	0.90	0.94	0.724	1.06	0.686	1.00	1.30	0.891	No
2540	25.40	1.45	0.54	0.90	0.94	0.724	1.06	0.686	1.00	1.30	0.891	No
2541	25.41	1.45	0.54	0.90	0.94	0.724	1.06	0.686	1.00	1.30	0.891	No
2542	25.42	1.45	0.54	0.90	0.94	0.724	1.06	0.686	1.00	1.30	0.892	No
2543	25.43	1.45	0.54	0.90	0.94	0.725	1.06	0.686	1.00	1.30	0.892	No
2544	25.44	1.45	0.54	0.90	0.94	0.725	1.06	0.686	1.00	1.30	0.892	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
2545	25.45	1.45	0.54	0.90	0.94	0.725	1.06	0.686	1.00	1.30	0.892	No
2546	25.46	1.45	0.54	0.90	0.94	0.725	1.06	0.686	1.00	1.30	0.892	No
2547	25.47	1.45	0.55	0.90	0.94	0.725	1.06	0.686	1.00	1.30	0.892	No
2548	25.48	1.45	0.55	0.90	0.94	0.725	1.06	0.686	1.00	1.30	0.892	No
2549	25.49	1.45	0.55	0.90	0.94	0.725	1.06	0.686	1.00	1.30	0.892	No
2550	25.50	1.45	0.55	0.91	0.94	0.725	1.06	0.686	1.00	1.30	0.892	No
2551	25.51	1.45	0.55	0.91	0.94	0.725	1.06	0.686	1.00	1.30	0.892	No
2552	25.52	1.45	0.55	0.91	0.94	0.725	1.06	0.686	1.00	1.30	0.892	No
2553	25.53	1.45	0.55	0.91	0.94	0.725	1.06	0.686	1.00	1.30	0.892	No
2554	25.54	1.45	0.55	0.91	0.94	0.725	1.06	0.686	1.00	1.30	0.892	No
2555	25.55	1.45	0.55	0.91	0.94	0.725	1.06	0.687	1.00	1.30	0.892	No
2556	25.56	1.45	0.55	0.91	0.94	0.725	1.06	0.687	1.00	1.30	0.893	No
2557	25.57	1.45	0.55	0.91	0.94	0.725	1.06	0.687	1.00	1.30	0.893	No
2558	25.58	1.46	0.55	0.91	0.94	0.725	1.06	0.687	1.00	1.30	0.893	No
2559	25.59	1.46	0.55	0.91	0.94	0.725	1.06	0.687	1.00	1.30	0.893	No
2560	25.60	1.46	0.55	0.91	0.94	0.726	1.06	0.687	1.00	1.30	0.893	No
2561	25.61	1.46	0.55	0.91	0.94	0.726	1.06	0.687	1.00	1.30	0.893	No
2562	25.62	1.46	0.55	0.91	0.94	0.726	1.06	0.687	1.00	1.30	0.893	No
2563	25.63	1.46	0.55	0.91	0.94	0.726	1.06	0.687	1.00	1.30	0.893	No
2564	25.64	1.46	0.55	0.91	0.94	0.726	1.06	0.687	1.00	1.30	0.893	No
2565	25.65	1.46	0.55	0.91	0.94	0.726	1.06	0.687	1.00	1.30	0.893	No
2566	25.66	1.46	0.55	0.91	0.94	0.726	1.06	0.687	1.00	1.30	0.893	No
2567	25.67	1.46	0.55	0.91	0.94	0.726	1.06	0.687	1.00	1.30	0.893	No
2568	25.68	1.46	0.55	0.91	0.94	0.726	1.06	0.687	1.00	1.30	0.893	No
2569	25.69	1.46	0.55	0.91	0.94	0.726	1.06	0.687	1.00	1.30	0.893	No
2570	25.70	1.46	0.55	0.91	0.94	0.726	1.06	0.687	1.00	1.30	0.894	No
2571	25.71	1.46	0.55	0.91	0.94	0.726	1.06	0.687	1.00	1.30	0.894	No
2572	25.72	1.46	0.55	0.91	0.94	0.726	1.06	0.687	1.00	1.30	0.894	No
2573	25.73	1.46	0.55	0.91	0.94	0.726	1.06	0.687	1.00	1.30	0.894	No
2574	25.74	1.46	0.55	0.91	0.94	0.726	1.06	0.688	1.00	1.30	0.894	No
2575	25.75	1.46	0.55	0.91	0.94	0.726	1.06	0.688	1.00	1.30	0.894	No
2576	25.76	1.47	0.55	0.91	0.94	0.726	1.06	0.688	1.00	1.30	0.894	No
2577	25.77	1.47	0.55	0.91	0.94	0.726	1.06	0.688	1.00	1.30	0.894	No
2578	25.78	1.47	0.55	0.91	0.94	0.727	1.06	0.688	1.00	1.30	0.894	No
2579	25.79	1.47	0.56	0.91	0.94	0.727	1.06	0.688	1.00	1.30	0.894	No
2580	25.80	1.47	0.56	0.91	0.94	0.727	1.06	0.688	1.00	1.30	0.894	No
2581	25.81	1.47	0.56	0.91	0.94	0.727	1.06	0.688	1.00	1.30	0.894	No
2582	25.82	1.47	0.56	0.91	0.94	0.727	1.06	0.688	1.00	1.30	0.894	No
2583	25.83	1.47	0.56	0.91	0.94	0.727	1.06	0.688	1.00	1.30	0.894	No
2584	25.84	1.47	0.56	0.91	0.94	0.727	1.06	0.688	1.00	1.30	0.894	No
2585	25.85	1.47	0.56	0.91	0.94	0.727	1.06	0.688	1.00	1.30	0.895	No
2586	25.86	1.47	0.56	0.91	0.94	0.727	1.06	0.688	1.00	1.30	0.895	No
2587	25.87	1.47	0.56	0.91	0.94	0.727	1.06	0.688	1.00	1.30	0.895	No
2588	25.88	1.47	0.56	0.91	0.94	0.727	1.06	0.688	1.00	1.30	0.895	No
2589	25.89	1.47	0.56	0.91	0.94	0.727	1.06	0.688	1.00	1.30	0.895	No
2590	25.90	1.47	0.56	0.91	0.94	0.727	1.06	0.688	1.00	1.30	0.895	No
2591	25.91	1.47	0.56	0.91	0.94	0.727	1.06	0.688	1.00	1.30	0.895	No
2592	25.92	1.47	0.56	0.92	0.94	0.727	1.06	0.688	1.00	1.30	0.895	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
2593	25.93	1.47	0.56	0.92	0.94	0.727	1.06	0.688	1.00	1.30	0.895	No
2594	25.94	1.48	0.56	0.92	0.94	0.727	1.06	0.689	1.00	1.30	0.895	No
2595	25.95	1.48	0.56	0.92	0.94	0.727	1.06	0.689	1.00	1.30	0.895	No
2596	25.96	1.48	0.56	0.92	0.94	0.727	1.06	0.689	1.00	1.30	0.895	No
2597	25.97	1.48	0.56	0.92	0.94	0.727	1.06	0.689	1.00	1.30	0.895	No
2598	25.98	1.48	0.56	0.92	0.94	0.728	1.06	0.689	1.00	1.30	0.895	No
2599	25.99	1.48	0.56	0.92	0.94	0.728	1.06	0.689	1.00	1.30	0.895	No
2600	26.00	1.48	0.56	0.92	0.94	0.728	1.06	0.689	1.00	1.30	0.895	No
2601	26.01	1.48	0.56	0.92	0.94	0.728	1.06	0.689	1.00	1.30	0.895	No
2602	26.02	1.48	0.56	0.92	0.94	0.728	1.06	0.689	1.00	1.30	0.896	No
2603	26.03	1.48	0.56	0.92	0.94	0.728	1.06	0.689	1.00	1.30	0.896	No
2604	26.04	1.48	0.56	0.92	0.94	0.728	1.06	0.689	1.00	1.30	0.896	No
2605	26.05	1.48	0.56	0.92	0.94	0.728	1.06	0.689	1.00	1.30	0.896	No
2606	26.06	1.48	0.56	0.92	0.94	0.728	1.06	0.689	1.00	1.30	0.896	No
2607	26.07	1.48	0.56	0.92	0.94	0.728	1.06	0.689	1.00	1.30	0.896	No
2608	26.08	1.48	0.56	0.92	0.94	0.728	1.06	0.689	1.00	1.30	0.896	No
2609	26.09	1.48	0.56	0.92	0.94	0.728	1.06	0.689	1.00	1.30	0.896	No
2610	26.10	1.48	0.56	0.92	0.94	0.728	1.06	0.689	1.00	1.30	0.896	No
2611	26.11	1.48	0.57	0.92	0.94	0.728	1.06	0.689	1.00	1.30	0.896	No
2612	26.12	1.49	0.57	0.92	0.94	0.728	1.06	0.689	1.00	1.30	0.896	No
2613	26.13	1.49	0.57	0.92	0.94	0.728	1.06	0.689	1.00	1.30	0.896	No
2614	26.14	1.49	0.57	0.92	0.94	0.728	1.06	0.689	1.00	1.30	0.896	No
2615	26.15	1.49	0.57	0.92	0.94	0.728	1.06	0.689	1.00	1.30	0.896	No
2616	26.16	1.49	0.57	0.92	0.94	0.728	1.06	0.689	1.00	1.30	0.896	No
2617	26.17	1.49	0.57	0.92	0.94	0.728	1.06	0.690	1.00	1.30	0.896	No
2618	26.18	1.49	0.57	0.92	0.94	0.728	1.06	0.690	1.00	1.30	0.896	No
2619	26.19	1.49	0.57	0.92	0.94	0.728	1.06	0.690	1.00	1.30	0.896	No
2620	26.20	1.49	0.57	0.92	0.94	0.729	1.06	0.690	1.00	1.30	0.897	No
2621	26.21	1.49	0.57	0.92	0.94	0.729	1.06	0.690	1.00	1.30	0.897	No
2622	26.22	1.49	0.57	0.92	0.94	0.729	1.06	0.690	1.00	1.30	0.897	No
2623	26.23	1.49	0.57	0.92	0.94	0.729	1.06	0.690	1.00	1.30	0.897	No
2624	26.24	1.49	0.57	0.92	0.94	0.729	1.06	0.690	1.00	1.30	0.897	No
2625	26.25	1.49	0.57	0.92	0.94	0.729	1.06	0.690	1.00	1.30	0.897	No
2626	26.26	1.49	0.57	0.92	0.94	0.729	1.06	0.690	1.00	1.30	0.897	No
2627	26.27	1.49	0.57	0.92	0.94	0.729	1.06	0.690	1.00	1.30	0.897	No
2628	26.28	1.49	0.57	0.92	0.94	0.729	1.06	0.690	1.00	1.30	0.897	No
2629	26.29	1.50	0.57	0.92	0.94	0.729	1.06	0.690	1.00	1.30	0.897	No
2630	26.30	1.50	0.57	0.92	0.94	0.729	1.06	0.690	1.00	1.30	0.897	No
2631	26.31	1.50	0.57	0.93	0.94	0.729	1.06	0.690	1.00	1.30	0.897	No
2632	26.32	1.50	0.57	0.93	0.94	0.729	1.06	0.690	1.00	1.30	0.897	No
2633	26.33	1.50	0.57	0.93	0.94	0.729	1.06	0.690	1.00	1.30	0.897	No
2634	26.34	1.50	0.57	0.93	0.94	0.729	1.06	0.690	1.00	1.30	0.897	No
2635	26.35	1.50	0.57	0.93	0.94	0.729	1.06	0.690	1.00	1.30	0.897	No
2636	26.36	1.50	0.57	0.93	0.94	0.729	1.06	0.690	1.00	1.30	0.897	No
2637	26.37	1.50	0.57	0.93	0.94	0.729	1.06	0.690	1.00	1.30	0.897	No
2638	26.38	1.50	0.57	0.93	0.94	0.729	1.06	0.690	1.00	1.30	0.898	No
2639	26.39	1.50	0.57	0.93	0.94	0.729	1.06	0.690	1.00	1.30	0.898	No
2640	26.40	1.50	0.57	0.93	0.94	0.729	1.06	0.690	1.00	1.30	0.898	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
2641	26.41	1.50	0.57	0.93	0.94	0.729	1.06	0.691	1.00	1.30	0.898	No
2642	26.42	1.50	0.57	0.93	0.94	0.729	1.06	0.691	1.00	1.30	0.898	No
2643	26.43	1.50	0.58	0.93	0.94	0.730	1.06	0.691	1.00	1.30	0.898	No
2644	26.44	1.50	0.58	0.93	0.94	0.730	1.06	0.691	1.00	1.30	0.898	No
2645	26.45	1.50	0.58	0.93	0.94	0.730	1.06	0.691	1.00	1.30	0.898	No
2646	26.46	1.50	0.58	0.93	0.94	0.730	1.06	0.691	1.00	1.30	0.898	No
2647	26.47	1.51	0.58	0.93	0.94	0.730	1.06	0.691	1.00	1.30	0.898	No
2648	26.48	1.51	0.58	0.93	0.94	0.730	1.06	0.691	1.00	1.30	0.898	No
2649	26.49	1.51	0.58	0.93	0.94	0.730	1.06	0.691	1.00	1.30	0.898	No
2650	26.50	1.51	0.58	0.93	0.94	0.730	1.06	0.691	1.00	1.30	0.898	No
2651	26.51	1.51	0.58	0.93	0.94	0.730	1.06	0.691	1.00	1.30	0.898	No
2652	26.52	1.51	0.58	0.93	0.94	0.730	1.06	0.691	1.00	1.30	0.898	No
2653	26.53	1.51	0.58	0.93	0.94	0.730	1.06	0.691	1.00	1.30	0.898	No
2654	26.54	1.51	0.58	0.93	0.94	0.730	1.06	0.691	1.00	1.30	0.898	No
2655	26.55	1.51	0.58	0.93	0.94	0.730	1.06	0.691	1.00	1.30	0.898	No
2656	26.56	1.51	0.58	0.93	0.94	0.730	1.06	0.691	1.00	1.30	0.898	No
2657	26.57	1.51	0.58	0.93	0.94	0.730	1.06	0.691	1.00	1.30	0.898	No
2658	26.58	1.51	0.58	0.93	0.94	0.730	1.06	0.691	1.00	1.30	0.899	No
2659	26.59	1.51	0.58	0.93	0.94	0.730	1.06	0.691	1.00	1.30	0.899	No
2660	26.60	1.51	0.58	0.93	0.94	0.730	1.06	0.691	1.00	1.30	0.899	No
2661	26.61	1.51	0.58	0.93	0.94	0.730	1.06	0.691	1.00	1.30	0.899	No
2662	26.62	1.51	0.58	0.93	0.94	0.730	1.06	0.691	1.00	1.30	0.899	No
2663	26.63	1.51	0.58	0.93	0.94	0.730	1.06	0.691	1.00	1.30	0.899	No
2664	26.64	1.52	0.58	0.93	0.94	0.730	1.06	0.691	1.00	1.30	0.899	No
2665	26.65	1.52	0.58	0.93	0.94	0.730	1.06	0.691	1.00	1.30	0.899	No
2666	26.66	1.52	0.58	0.93	0.94	0.730	1.06	0.691	1.00	1.30	0.899	No
2667	26.67	1.52	0.58	0.93	0.94	0.730	1.06	0.692	1.00	1.30	0.899	No
2668	26.68	1.52	0.58	0.93	0.94	0.731	1.06	0.692	1.00	1.30	0.899	No
2669	26.69	1.52	0.58	0.94	0.94	0.731	1.06	0.692	1.00	1.30	0.899	No
2670	26.70	1.52	0.58	0.94	0.94	0.731	1.06	0.692	1.00	1.30	0.899	No
2671	26.71	1.52	0.58	0.94	0.94	0.731	1.06	0.692	1.00	1.30	0.899	No
2672	26.72	1.52	0.58	0.94	0.94	0.731	1.06	0.692	1.00	1.30	0.899	No
2673	26.73	1.52	0.58	0.94	0.94	0.731	1.06	0.692	1.00	1.30	0.899	No
2674	26.74	1.52	0.58	0.94	0.94	0.731	1.06	0.692	1.00	1.30	0.899	No
2675	26.75	1.52	0.59	0.94	0.94	0.731	1.06	0.692	1.00	1.30	0.899	No
2676	26.76	1.52	0.59	0.94	0.94	0.731	1.06	0.692	1.00	1.30	0.899	No
2677	26.77	1.52	0.59	0.94	0.94	0.731	1.06	0.692	1.00	1.30	0.899	No
2678	26.78	1.52	0.59	0.94	0.94	0.731	1.06	0.692	1.00	1.30	0.900	No
2679	26.79	1.52	0.59	0.94	0.94	0.731	1.06	0.692	1.00	1.30	0.900	No
2680	26.80	1.52	0.59	0.94	0.94	0.731	1.06	0.692	1.00	1.30	0.900	No
2681	26.81	1.53	0.59	0.94	0.94	0.731	1.06	0.692	1.00	1.30	0.900	No
2682	26.82	1.53	0.59	0.94	0.93	0.731	1.06	0.692	1.00	1.30	0.900	No
2683	26.83	1.53	0.59	0.94	0.93	0.731	1.06	0.692	1.00	1.30	0.900	No
2684	26.84	1.53	0.59	0.94	0.93	0.731	1.06	0.692	1.00	1.30	0.900	No
2685	26.85	1.53	0.59	0.94	0.93	0.731	1.06	0.692	1.00	1.30	0.900	No
2686	26.86	1.53	0.59	0.94	0.93	0.731	1.06	0.692	1.00	1.30	0.900	No
2687	26.87	1.53	0.59	0.94	0.93	0.731	1.06	0.692	1.00	1.30	0.900	No
2688	26.88	1.53	0.59	0.94	0.93	0.731	1.06	0.692	1.00	1.30	0.900	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
2689	26.89	1.53	0.59	0.94	0.93	0.731	1.06	0.692	1.00	1.30	0.900	No
2690	26.90	1.53	0.59	0.94	0.93	0.731	1.06	0.692	1.00	1.30	0.900	No
2691	26.91	1.53	0.59	0.94	0.93	0.731	1.06	0.692	1.00	1.30	0.900	No
2692	26.92	1.53	0.59	0.94	0.93	0.732	1.06	0.692	1.00	1.30	0.900	No
2693	26.93	1.53	0.59	0.94	0.93	0.732	1.06	0.693	1.00	1.30	0.900	No
2694	26.94	1.53	0.59	0.94	0.93	0.732	1.06	0.693	1.00	1.30	0.900	No
2695	26.95	1.53	0.59	0.94	0.93	0.732	1.06	0.693	1.00	1.30	0.900	No
2696	26.96	1.53	0.59	0.94	0.93	0.732	1.06	0.693	1.00	1.30	0.900	No
2697	26.97	1.53	0.59	0.94	0.93	0.732	1.06	0.693	1.00	1.30	0.900	No
2698	26.98	1.53	0.59	0.94	0.93	0.732	1.06	0.693	1.00	1.30	0.901	No
2699	26.99	1.54	0.59	0.94	0.93	0.732	1.06	0.693	1.00	1.30	0.901	No
2700	27.00	1.54	0.59	0.94	0.93	0.732	1.06	0.693	1.00	1.30	0.901	No
2701	27.01	1.54	0.59	0.94	0.93	0.732	1.06	0.693	1.00	1.30	0.901	No
2702	27.02	1.54	0.59	0.94	0.93	0.732	1.06	0.693	1.00	1.30	0.901	No
2703	27.03	1.54	0.59	0.94	0.93	0.732	1.06	0.693	1.00	1.30	0.901	No
2704	27.04	1.54	0.59	0.94	0.93	0.732	1.06	0.693	1.00	1.30	0.901	No
2705	27.05	1.54	0.59	0.94	0.93	0.732	1.06	0.693	1.00	1.30	0.901	No
2706	27.06	1.54	0.59	0.94	0.93	0.732	1.06	0.693	1.00	1.30	0.901	No
2707	27.07	1.54	0.59	0.94	0.93	0.732	1.06	0.693	1.00	1.30	0.901	No
2708	27.08	1.54	0.60	0.95	0.93	0.732	1.06	0.693	1.00	1.30	0.901	No
2709	27.09	1.54	0.60	0.95	0.93	0.732	1.06	0.693	1.00	1.30	0.901	No
2710	27.10	1.54	0.60	0.95	0.93	0.732	1.06	0.693	1.00	1.30	0.901	No
2711	27.11	1.54	0.60	0.95	0.93	0.732	1.06	0.693	1.00	1.30	0.901	No
2712	27.12	1.54	0.60	0.95	0.93	0.732	1.06	0.693	1.00	1.30	0.901	No
2713	27.13	1.54	0.60	0.95	0.93	0.732	1.06	0.693	1.00	1.30	0.901	No
2714	27.14	1.54	0.60	0.95	0.93	0.732	1.06	0.693	1.00	1.30	0.901	No
2715	27.15	1.54	0.60	0.95	0.93	0.732	1.06	0.693	1.00	1.30	0.901	No
2716	27.16	1.54	0.60	0.95	0.93	0.732	1.06	0.693	1.00	1.30	0.901	No
2717	27.17	1.55	0.60	0.95	0.93	0.733	1.06	0.693	1.00	1.30	0.901	No
2718	27.18	1.55	0.60	0.95	0.93	0.733	1.06	0.693	1.00	1.30	0.902	No
2719	27.19	1.55	0.60	0.95	0.93	0.733	1.06	0.694	1.00	1.30	0.902	No
2720	27.20	1.55	0.60	0.95	0.93	0.733	1.06	0.694	1.00	1.30	0.902	No
2721	27.21	1.55	0.60	0.95	0.93	0.733	1.06	0.694	1.00	1.30	0.902	No
2722	27.22	1.55	0.60	0.95	0.93	0.733	1.06	0.694	1.00	1.30	0.902	No
2723	27.23	1.55	0.60	0.95	0.93	0.733	1.06	0.694	1.00	1.30	0.902	No
2724	27.24	1.55	0.60	0.95	0.93	0.733	1.06	0.694	1.00	1.30	0.902	No
2725	27.25	1.55	0.60	0.95	0.93	0.733	1.06	0.694	1.00	1.30	0.902	No
2726	27.26	1.55	0.60	0.95	0.93	0.733	1.06	0.694	1.00	1.30	0.902	No
2727	27.27	1.55	0.60	0.95	0.93	0.733	1.06	0.694	1.00	1.30	0.902	No
2728	27.28	1.55	0.60	0.95	0.93	0.733	1.06	0.694	1.00	1.30	0.902	No
2729	27.29	1.55	0.60	0.95	0.93	0.733	1.06	0.694	1.00	1.30	0.902	No
2730	27.30	1.55	0.60	0.95	0.93	0.733	1.06	0.694	1.00	1.30	0.902	No
2731	27.31	1.55	0.60	0.95	0.93	0.733	1.06	0.694	1.00	1.30	0.902	No
2732	27.32	1.55	0.60	0.95	0.93	0.733	1.06	0.694	1.00	1.30	0.902	No
2733	27.33	1.55	0.60	0.95	0.93	0.733	1.06	0.694	1.00	1.30	0.902	No
2734	27.34	1.55	0.60	0.95	0.93	0.733	1.06	0.694	1.00	1.30	0.902	No
2735	27.35	1.56	0.60	0.95	0.93	0.733	1.06	0.694	1.00	1.30	0.902	No
2736	27.36	1.56	0.60	0.95	0.93	0.733	1.06	0.694	1.00	1.30	0.902	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
2737	27.37	1.56	0.60	0.95	0.93	0.733	1.06	0.694	1.00	1.30	0.902	No
2738	27.38	1.56	0.60	0.95	0.93	0.733	1.06	0.694	1.00	1.30	0.903	No
2739	27.39	1.56	0.60	0.95	0.93	0.733	1.06	0.694	1.00	1.30	0.903	No
2740	27.40	1.56	0.61	0.95	0.93	0.733	1.06	0.694	1.00	1.30	0.903	No
2741	27.41	1.56	0.61	0.95	0.93	0.733	1.06	0.694	1.00	1.30	0.903	No
2742	27.42	1.56	0.61	0.95	0.93	0.734	1.06	0.694	1.00	1.30	0.903	No
2743	27.43	1.56	0.61	0.95	0.93	0.734	1.06	0.694	1.00	1.30	0.903	No
2744	27.44	1.56	0.61	0.95	0.93	0.734	1.06	0.694	1.00	1.30	0.903	No
2745	27.45	1.56	0.61	0.95	0.93	0.734	1.06	0.694	1.00	1.30	0.903	No
2746	27.46	1.56	0.61	0.95	0.93	0.734	1.06	0.695	1.00	1.30	0.903	No
2747	27.47	1.56	0.61	0.95	0.93	0.734	1.06	0.695	1.00	1.30	0.903	No
2748	27.48	1.56	0.61	0.96	0.93	0.734	1.06	0.695	1.00	1.30	0.903	No
2749	27.49	1.56	0.61	0.96	0.93	0.734	1.06	0.695	1.00	1.30	0.903	No
2750	27.50	1.56	0.61	0.96	0.93	0.734	1.06	0.695	1.00	1.30	0.903	No
2751	27.51	1.56	0.61	0.96	0.93	0.734	1.06	0.695	1.00	1.30	0.903	No
2752	27.52	1.57	0.61	0.96	0.93	0.734	1.06	0.695	1.00	1.30	0.903	No
2753	27.53	1.57	0.61	0.96	0.93	0.734	1.06	0.695	1.00	1.30	0.903	No
2754	27.54	1.57	0.61	0.96	0.93	0.734	1.06	0.695	1.00	1.30	0.903	No
2755	27.55	1.57	0.61	0.96	0.93	0.734	1.06	0.695	1.00	1.30	0.903	No
2756	27.56	1.57	0.61	0.96	0.93	0.734	1.06	0.695	1.00	1.30	0.903	No
2757	27.57	1.57	0.61	0.96	0.93	0.734	1.06	0.695	1.00	1.30	0.903	No
2758	27.58	1.57	0.61	0.96	0.93	0.734	1.06	0.695	1.00	1.30	0.903	No
2759	27.59	1.57	0.61	0.96	0.93	0.734	1.06	0.695	1.00	1.30	0.903	No
2760	27.60	1.57	0.61	0.96	0.93	0.734	1.06	0.695	1.00	1.30	0.903	No
2761	27.61	1.57	0.61	0.96	0.93	0.734	1.06	0.695	1.00	1.30	0.904	No
2762	27.62	1.57	0.61	0.96	0.93	0.734	1.06	0.695	1.00	1.30	0.904	No
2763	27.63	1.57	0.61	0.96	0.93	0.734	1.06	0.695	1.00	1.30	0.904	No
2764	27.64	1.57	0.61	0.96	0.93	0.734	1.06	0.695	1.00	1.30	0.904	No
2765	27.65	1.57	0.61	0.96	0.93	0.734	1.06	0.695	1.00	1.30	0.904	No
2766	27.66	1.57	0.61	0.96	0.93	0.734	1.06	0.695	1.00	1.30	0.904	No
2767	27.67	1.57	0.61	0.96	0.93	0.734	1.06	0.695	1.00	1.30	0.904	No
2768	27.68	1.57	0.61	0.96	0.93	0.734	1.06	0.695	1.00	1.30	0.904	No
2769	27.69	1.57	0.61	0.96	0.93	0.734	1.06	0.695	1.00	1.30	0.904	No
2770	27.70	1.58	0.61	0.96	0.93	0.735	1.06	0.695	1.00	1.30	0.904	No
2771	27.71	1.58	0.61	0.96	0.93	0.735	1.06	0.695	1.00	1.30	0.904	No
2772	27.72	1.58	0.62	0.96	0.93	0.735	1.06	0.695	1.00	1.30	0.904	No
2773	27.73	1.58	0.62	0.96	0.93	0.735	1.06	0.695	1.00	1.30	0.904	No
2774	27.74	1.58	0.62	0.96	0.93	0.735	1.06	0.695	1.00	1.30	0.904	No
2775	27.75	1.58	0.62	0.96	0.93	0.735	1.06	0.695	1.00	1.30	0.904	No
2776	27.76	1.58	0.62	0.96	0.93	0.735	1.06	0.696	1.00	1.30	0.904	No
2777	27.77	1.58	0.62	0.96	0.93	0.735	1.06	0.696	1.00	1.30	0.904	No
2778	27.78	1.58	0.62	0.96	0.93	0.735	1.06	0.696	1.00	1.30	0.904	No
2779	27.79	1.58	0.62	0.96	0.93	0.735	1.06	0.696	1.00	1.30	0.904	No
2780	27.80	1.58	0.62	0.96	0.93	0.735	1.06	0.696	1.00	1.30	0.904	No
2781	27.81	1.58	0.62	0.96	0.93	0.735	1.06	0.696	1.00	1.30	0.904	No
2782	27.82	1.58	0.62	0.96	0.93	0.735	1.06	0.696	1.00	1.30	0.904	No
2783	27.83	1.58	0.62	0.96	0.93	0.735	1.06	0.696	1.00	1.30	0.904	No
2784	27.84	1.58	0.62	0.96	0.93	0.735	1.06	0.696	1.00	1.30	0.905	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
2785	27.85	1.58	0.62	0.96	0.93	0.735	1.06	0.696	1.00	1.30	0.905	No
2786	27.86	1.58	0.62	0.96	0.93	0.735	1.06	0.696	1.00	1.30	0.905	No
2787	27.87	1.59	0.62	0.97	0.93	0.735	1.06	0.696	1.00	1.30	0.905	No
2788	27.88	1.59	0.62	0.97	0.93	0.735	1.06	0.696	1.00	1.30	0.905	No
2789	27.89	1.59	0.62	0.97	0.93	0.735	1.06	0.696	1.00	1.30	0.905	No
2790	27.90	1.59	0.62	0.97	0.93	0.735	1.06	0.696	1.00	1.30	0.905	No
2791	27.91	1.59	0.62	0.97	0.93	0.735	1.06	0.696	1.00	1.30	0.905	No
2792	27.92	1.59	0.62	0.97	0.93	0.735	1.06	0.696	1.00	1.30	0.905	No
2793	27.93	1.59	0.62	0.97	0.93	0.735	1.06	0.696	1.00	1.30	0.905	No
2794	27.94	1.59	0.62	0.97	0.93	0.735	1.06	0.696	1.00	1.30	0.905	No
2795	27.95	1.59	0.62	0.97	0.93	0.735	1.06	0.696	1.00	1.30	0.905	No
2796	27.96	1.59	0.62	0.97	0.93	0.735	1.06	0.696	1.00	1.30	0.905	No
2797	27.97	1.59	0.62	0.97	0.93	0.735	1.06	0.696	1.00	1.30	0.905	No
2798	27.98	1.59	0.62	0.97	0.93	0.735	1.06	0.696	1.00	1.30	0.905	No
2799	27.99	1.59	0.62	0.97	0.93	0.736	1.06	0.696	1.00	1.30	0.905	No
2800	28.00	1.59	0.62	0.97	0.93	0.736	1.06	0.696	1.00	1.30	0.905	No
2801	28.01	1.59	0.62	0.97	0.93	0.736	1.06	0.696	1.00	1.30	0.905	No
2802	28.02	1.59	0.62	0.97	0.93	0.736	1.06	0.696	1.00	1.30	0.905	No
2803	28.03	1.59	0.62	0.97	0.93	0.736	1.06	0.696	1.00	1.30	0.905	No
2804	28.04	1.59	0.63	0.97	0.93	0.736	1.06	0.696	1.00	1.30	0.905	No
2805	28.05	1.60	0.63	0.97	0.93	0.736	1.06	0.696	1.00	1.30	0.905	No
2806	28.06	1.60	0.63	0.97	0.93	0.736	1.06	0.696	1.00	1.30	0.905	No
2807	28.07	1.60	0.63	0.97	0.93	0.736	1.06	0.697	1.00	1.30	0.905	No
2808	28.08	1.60	0.63	0.97	0.93	0.736	1.06	0.697	1.00	1.30	0.906	No
2809	28.09	1.60	0.63	0.97	0.93	0.736	1.06	0.697	1.00	1.30	0.906	No
2810	28.10	1.60	0.63	0.97	0.93	0.736	1.06	0.697	1.00	1.30	0.906	No
2811	28.11	1.60	0.63	0.97	0.93	0.736	1.06	0.697	1.00	1.30	0.906	No
2812	28.12	1.60	0.63	0.97	0.93	0.736	1.06	0.697	1.00	1.30	0.906	No
2813	28.13	1.60	0.63	0.97	0.93	0.736	1.06	0.697	1.00	1.30	0.906	No
2814	28.14	1.60	0.63	0.97	0.93	0.736	1.06	0.697	1.00	1.30	0.906	No
2815	28.15	1.60	0.63	0.97	0.93	0.736	1.06	0.697	1.00	1.30	0.906	No
2816	28.16	1.60	0.63	0.97	0.93	0.736	1.06	0.697	1.00	1.30	0.906	No
2817	28.17	1.60	0.63	0.97	0.93	0.736	1.06	0.697	1.00	1.30	0.906	No
2818	28.18	1.60	0.63	0.97	0.93	0.736	1.06	0.697	1.00	1.30	0.906	No
2819	28.19	1.60	0.63	0.97	0.93	0.736	1.06	0.697	1.00	1.30	0.906	No
2820	28.20	1.60	0.63	0.97	0.93	0.736	1.06	0.697	1.00	1.30	0.906	No
2821	28.21	1.60	0.63	0.97	0.93	0.736	1.06	0.697	1.00	1.30	0.906	No
2822	28.22	1.60	0.63	0.97	0.93	0.736	1.06	0.697	1.00	1.30	0.906	No
2823	28.23	1.61	0.63	0.97	0.93	0.736	1.06	0.697	1.00	1.30	0.906	No
2824	28.24	1.61	0.63	0.97	0.93	0.736	1.06	0.697	1.00	1.30	0.906	No
2825	28.25	1.61	0.63	0.97	0.93	0.736	1.06	0.697	1.00	1.30	0.906	No
2826	28.26	1.61	0.63	0.98	0.93	0.736	1.06	0.697	1.00	1.30	0.906	No
2827	28.27	1.61	0.63	0.98	0.93	0.736	1.06	0.697	1.00	1.30	0.906	No
2828	28.28	1.61	0.63	0.98	0.93	0.736	1.06	0.697	1.00	1.30	0.906	No
2829	28.29	1.61	0.63	0.98	0.93	0.736	1.06	0.697	1.00	1.30	0.906	No
2830	28.30	1.61	0.63	0.98	0.93	0.737	1.06	0.697	1.00	1.30	0.906	No
2831	28.31	1.61	0.63	0.98	0.93	0.737	1.06	0.697	1.00	1.30	0.906	No
2832	28.32	1.61	0.63	0.98	0.93	0.737	1.06	0.697	1.00	1.30	0.906	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
2833	28.33	1.61	0.63	0.98	0.93	0.737	1.06	0.697	1.00	1.30	0.906	No
2834	28.34	1.61	0.63	0.98	0.93	0.737	1.06	0.697	1.00	1.30	0.907	No
2835	28.35	1.61	0.63	0.98	0.93	0.737	1.06	0.697	1.00	1.30	0.907	No
2836	28.36	1.61	0.64	0.98	0.93	0.737	1.06	0.697	1.00	1.30	0.907	No
2837	28.37	1.61	0.64	0.98	0.93	0.737	1.06	0.697	1.00	1.30	0.907	No
2838	28.38	1.61	0.64	0.98	0.93	0.737	1.06	0.697	1.00	1.30	0.907	No
2839	28.39	1.61	0.64	0.98	0.93	0.737	1.06	0.697	1.00	1.30	0.907	No
2840	28.40	1.62	0.64	0.98	0.93	0.737	1.06	0.698	1.00	1.30	0.907	No
2841	28.41	1.62	0.64	0.98	0.93	0.737	1.06	0.698	1.00	1.30	0.907	No
2842	28.42	1.62	0.64	0.98	0.93	0.737	1.06	0.698	1.00	1.30	0.907	No
2843	28.43	1.62	0.64	0.98	0.93	0.737	1.06	0.698	1.00	1.30	0.907	No
2844	28.44	1.62	0.64	0.98	0.93	0.737	1.06	0.698	1.00	1.30	0.907	No
2845	28.45	1.62	0.64	0.98	0.93	0.737	1.06	0.698	1.00	1.30	0.907	No
2846	28.46	1.62	0.64	0.98	0.93	0.737	1.06	0.698	1.00	1.30	0.907	No
2847	28.47	1.62	0.64	0.98	0.93	0.737	1.06	0.698	1.00	1.30	0.907	No
2848	28.48	1.62	0.64	0.98	0.93	0.737	1.06	0.698	1.00	1.30	0.907	No
2849	28.49	1.62	0.64	0.98	0.93	0.737	1.06	0.698	1.00	1.30	0.907	No
2850	28.50	1.62	0.64	0.98	0.93	0.737	1.06	0.698	1.00	1.30	0.907	No
2851	28.51	1.62	0.64	0.98	0.93	0.737	1.06	0.698	1.00	1.30	0.907	No
2852	28.52	1.62	0.64	0.98	0.93	0.737	1.06	0.698	1.00	1.30	0.907	No
2853	28.53	1.62	0.64	0.98	0.93	0.737	1.06	0.698	1.00	1.30	0.907	No
2854	28.54	1.62	0.64	0.98	0.93	0.737	1.06	0.698	1.00	1.30	0.907	No
2855	28.55	1.62	0.64	0.98	0.93	0.737	1.06	0.698	1.00	1.30	0.907	No
2856	28.56	1.62	0.64	0.98	0.93	0.737	1.06	0.698	1.00	1.30	0.907	No
2857	28.57	1.62	0.64	0.98	0.93	0.737	1.06	0.698	1.00	1.30	0.907	No
2858	28.58	1.63	0.64	0.98	0.93	0.737	1.06	0.698	1.00	1.30	0.908	No
2859	28.59	1.63	0.64	0.98	0.93	0.737	1.06	0.698	1.00	1.30	0.908	No
2860	28.60	1.63	0.64	0.98	0.93	0.738	1.06	0.698	1.00	1.30	0.908	No
2861	28.61	1.63	0.64	0.98	0.93	0.738	1.06	0.698	1.00	1.30	0.908	No
2862	28.62	1.63	0.64	0.98	0.93	0.738	1.06	0.698	1.00	1.30	0.908	No
2863	28.63	1.63	0.64	0.98	0.93	0.738	1.06	0.698	1.00	1.30	0.908	No
2864	28.64	1.63	0.64	0.98	0.93	0.738	1.06	0.698	1.00	1.30	0.908	No
2865	28.65	1.63	0.64	0.98	0.93	0.738	1.06	0.698	1.00	1.30	0.908	No
2866	28.66	1.63	0.64	0.98	0.93	0.738	1.06	0.698	1.00	1.30	0.908	No
2867	28.67	1.63	0.64	0.99	0.93	0.738	1.06	0.698	1.00	1.30	0.908	No
2868	28.68	1.63	0.65	0.99	0.93	0.738	1.06	0.698	1.00	1.30	0.908	No
2869	28.69	1.63	0.65	0.99	0.93	0.738	1.06	0.698	1.00	1.30	0.908	No
2870	28.70	1.63	0.65	0.99	0.93	0.738	1.06	0.698	1.00	1.30	0.908	No
2871	28.71	1.63	0.65	0.99	0.93	0.738	1.06	0.699	1.00	1.30	0.908	No
2872	28.72	1.63	0.65	0.99	0.93	0.738	1.06	0.699	1.00	1.30	0.908	No
2873	28.73	1.63	0.65	0.99	0.93	0.738	1.06	0.699	1.00	1.30	0.908	No
2874	28.74	1.63	0.65	0.99	0.93	0.738	1.06	0.699	1.00	1.30	0.908	No
2875	28.75	1.63	0.65	0.99	0.93	0.738	1.06	0.699	1.00	1.30	0.908	No
2876	28.76	1.64	0.65	0.99	0.93	0.738	1.06	0.699	1.00	1.30	0.908	No
2877	28.77	1.64	0.65	0.99	0.93	0.738	1.06	0.699	1.00	1.30	0.908	No
2878	28.78	1.64	0.65	0.99	0.93	0.738	1.06	0.699	1.00	1.30	0.908	No
2879	28.79	1.64	0.65	0.99	0.93	0.738	1.06	0.699	1.00	1.30	0.908	No
2880	28.80	1.64	0.65	0.99	0.93	0.738	1.06	0.699	1.00	1.30	0.908	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
2881	28.81	1.64	0.65	0.99	0.93	0.738	1.06	0.699	1.00	1.30	0.908	No
2882	28.82	1.64	0.65	0.99	0.93	0.738	1.06	0.699	1.00	1.30	0.909	No
2883	28.83	1.64	0.65	0.99	0.93	0.738	1.06	0.699	1.00	1.30	0.909	No
2884	28.84	1.64	0.65	0.99	0.93	0.738	1.06	0.699	1.00	1.30	0.909	No
2885	28.85	1.64	0.65	0.99	0.93	0.738	1.06	0.699	1.00	1.30	0.909	No
2886	28.86	1.64	0.65	0.99	0.93	0.738	1.06	0.699	1.00	1.30	0.909	No
2887	28.87	1.64	0.65	0.99	0.93	0.738	1.06	0.699	1.00	1.30	0.909	No
2888	28.88	1.64	0.65	0.99	0.93	0.738	1.06	0.699	1.00	1.30	0.909	No
2889	28.89	1.64	0.65	0.99	0.93	0.738	1.06	0.699	1.00	1.30	0.909	No
2890	28.90	1.64	0.65	0.99	0.93	0.738	1.06	0.699	1.00	1.30	0.909	No
2891	28.91	1.64	0.65	0.99	0.93	0.739	1.06	0.699	1.00	1.30	0.909	No
2892	28.92	1.64	0.65	0.99	0.93	0.739	1.06	0.699	1.00	1.30	0.909	No
2893	28.93	1.64	0.65	0.99	0.93	0.739	1.06	0.699	1.00	1.30	0.909	No
2894	28.94	1.65	0.65	0.99	0.93	0.739	1.06	0.699	1.00	1.30	0.909	No
2895	28.95	1.65	0.65	0.99	0.93	0.739	1.06	0.699	1.00	1.30	0.909	No
2896	28.96	1.65	0.65	0.99	0.93	0.739	1.06	0.699	1.00	1.30	0.909	No
2897	28.97	1.65	0.65	0.99	0.93	0.739	1.06	0.699	1.00	1.30	0.909	No
2898	28.98	1.65	0.65	0.99	0.93	0.739	1.06	0.699	1.00	1.30	0.909	No
2899	28.99	1.65	0.65	0.99	0.93	0.739	1.06	0.699	1.00	1.30	0.909	No
2900	29.00	1.65	0.66	0.99	0.93	0.739	1.06	0.699	1.00	1.30	0.909	No
2901	29.01	1.65	0.66	0.99	0.93	0.739	1.06	0.699	1.00	1.30	0.909	No
2902	29.02	1.65	0.66	0.99	0.93	0.739	1.06	0.699	1.00	1.30	0.909	No
2903	29.03	1.65	0.66	0.99	0.93	0.739	1.06	0.699	1.00	1.30	0.909	No
2904	29.04	1.65	0.66	0.99	0.93	0.739	1.06	0.699	1.00	1.30	0.909	No
2905	29.05	1.65	0.66	0.99	0.93	0.739	1.06	0.699	1.00	1.30	0.909	No
2906	29.06	1.65	0.66	0.99	0.93	0.739	1.06	0.699	1.00	1.30	0.909	No
2907	29.07	1.65	0.66	1.00	0.93	0.739	1.06	0.699	1.00	1.30	0.909	No
2908	29.08	1.65	0.66	1.00	0.93	0.739	1.06	0.700	1.00	1.30	0.909	No
2909	29.09	1.65	0.66	1.00	0.93	0.739	1.06	0.700	1.00	1.30	0.909	No
2910	29.10	1.65	0.66	1.00	0.92	0.739	1.06	0.700	1.00	1.30	0.909	No
2911	29.11	1.65	0.66	1.00	0.92	0.739	1.06	0.700	1.00	1.30	0.909	No
2912	29.12	1.66	0.66	1.00	0.92	0.739	1.06	0.700	1.00	1.30	0.909	No
2913	29.13	1.66	0.66	1.00	0.92	0.739	1.06	0.700	1.00	1.30	0.909	No
2914	29.14	1.66	0.66	1.00	0.92	0.739	1.06	0.700	1.00	1.30	0.910	No
2915	29.15	1.66	0.66	1.00	0.92	0.739	1.06	0.700	1.00	1.30	0.910	No
2916	29.16	1.66	0.66	1.00	0.92	0.739	1.06	0.700	1.00	1.30	0.910	No
2917	29.17	1.66	0.66	1.00	0.92	0.739	1.06	0.700	1.00	1.30	0.910	No
2918	29.18	1.66	0.66	1.00	0.92	0.739	1.06	0.700	1.00	1.30	0.910	No
2919	29.19	1.66	0.66	1.00	0.92	0.739	1.06	0.700	1.00	1.30	0.910	No
2920	29.20	1.66	0.66	1.00	0.92	0.739	1.06	0.700	1.00	1.30	0.910	No
2921	29.21	1.66	0.66	1.00	0.92	0.739	1.06	0.700	1.00	1.30	0.910	No
2922	29.22	1.66	0.66	1.00	0.92	0.739	1.06	0.700	1.00	1.30	0.910	No
2923	29.23	1.66	0.66	1.00	0.92	0.739	1.06	0.700	1.00	1.30	0.910	No
2924	29.24	1.66	0.66	1.00	0.92	0.739	1.06	0.700	1.00	1.30	0.910	No
2925	29.25	1.66	0.66	1.00	0.92	0.739	1.06	0.700	1.00	1.30	0.910	No
2926	29.26	1.66	0.66	1.00	0.92	0.739	1.06	0.700	1.00	1.30	0.910	No
2927	29.27	1.66	0.66	1.00	0.92	0.739	1.06	0.700	1.00	1.30	0.910	No
2928	29.28	1.66	0.66	1.00	0.92	0.739	1.06	0.700	1.00	1.30	0.910	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
2929	29.29	1.67	0.66	1.00	0.92	0.739	1.06	0.700	1.00	1.30	0.910	No
2930	29.30	1.67	0.66	1.00	0.92	0.739	1.06	0.700	1.00	1.30	0.910	No
2931	29.31	1.67	0.66	1.00	0.92	0.739	1.06	0.700	1.00	1.30	0.910	No
2932	29.32	1.67	0.67	1.00	0.92	0.739	1.06	0.700	1.00	1.30	0.910	No
2933	29.33	1.67	0.67	1.00	0.92	0.739	1.06	0.700	1.00	1.30	0.910	No
2934	29.34	1.67	0.67	1.00	0.92	0.739	1.06	0.700	1.00	1.30	0.910	No
2935	29.35	1.67	0.67	1.00	0.92	0.739	1.06	0.700	1.00	1.30	0.910	No
2936	29.36	1.67	0.67	1.00	0.92	0.739	1.06	0.700	1.00	1.30	0.910	No
2937	29.37	1.67	0.67	1.00	0.92	0.739	1.06	0.700	1.00	1.30	0.910	No
2938	29.38	1.67	0.67	1.00	0.92	0.740	1.06	0.700	1.00	1.30	0.910	No
2939	29.39	1.67	0.67	1.00	0.92	0.740	1.06	0.700	1.00	1.30	0.910	No
2940	29.40	1.67	0.67	1.00	0.92	0.740	1.06	0.700	1.00	1.30	0.910	No
2941	29.41	1.67	0.67	1.00	0.92	0.740	1.06	0.700	1.00	1.30	0.910	No
2942	29.42	1.67	0.67	1.00	0.92	0.740	1.06	0.700	1.00	1.30	0.910	No
2943	29.43	1.67	0.67	1.01	0.92	0.740	1.06	0.700	1.00	1.30	0.910	No
2944	29.44	1.67	0.67	1.01	0.92	0.740	1.06	0.700	1.00	1.30	0.910	No
2945	29.45	1.67	0.67	1.01	0.92	0.740	1.06	0.700	1.00	1.30	0.910	No
2946	29.46	1.68	0.67	1.01	0.92	0.740	1.06	0.700	1.00	1.30	0.910	No
2947	29.47	1.68	0.67	1.01	0.92	0.740	1.06	0.700	1.00	1.30	0.910	No
2948	29.48	1.68	0.67	1.01	0.92	0.740	1.06	0.700	1.00	1.30	0.910	No
2949	29.49	1.68	0.67	1.01	0.92	0.740	1.06	0.700	1.00	1.30	0.910	No
2950	29.50	1.68	0.67	1.01	0.92	0.740	1.06	0.700	1.00	1.30	0.910	No
2951	29.51	1.68	0.67	1.01	0.92	0.740	1.06	0.700	1.00	1.30	0.910	No
2952	29.52	1.68	0.67	1.01	0.92	0.740	1.06	0.700	1.00	1.30	0.910	No
2953	29.53	1.68	0.67	1.01	0.92	0.740	1.06	0.700	1.00	1.30	0.910	No
2954	29.54	1.68	0.67	1.01	0.92	0.740	1.06	0.700	1.00	1.30	0.910	No
2955	29.55	1.68	0.67	1.01	0.92	0.740	1.06	0.700	1.00	1.30	0.910	No
2956	29.56	1.68	0.67	1.01	0.92	0.740	1.06	0.700	1.00	1.30	0.910	No
2957	29.57	1.68	0.67	1.01	0.92	0.740	1.06	0.700	1.00	1.30	0.910	No
2958	29.58	1.68	0.67	1.01	0.92	0.740	1.06	0.700	1.00	1.30	0.910	No
2959	29.59	1.68	0.67	1.01	0.92	0.740	1.06	0.700	1.00	1.30	0.910	No
2960	29.60	1.68	0.67	1.01	0.92	0.740	1.06	0.700	1.00	1.30	0.910	No
2961	29.61	1.68	0.67	1.01	0.92	0.740	1.06	0.700	1.00	1.30	0.911	No
2962	29.62	1.69	0.67	1.01	0.92	0.740	1.06	0.700	1.00	1.30	0.911	No
2963	29.63	1.69	0.67	1.01	0.92	0.740	1.06	0.700	1.00	1.30	0.911	No
2964	29.64	1.69	0.68	1.01	0.92	0.740	1.06	0.700	1.00	1.30	0.911	No
2965	29.65	1.69	0.68	1.01	0.92	0.740	1.06	0.700	1.00	1.30	0.911	No
2966	29.66	1.69	0.68	1.01	0.92	0.740	1.06	0.700	1.00	1.30	0.911	No
2967	29.67	1.69	0.68	1.01	0.92	0.740	1.06	0.700	1.00	1.30	0.911	No
2968	29.68	1.69	0.68	1.01	0.92	0.740	1.06	0.700	1.00	1.30	0.911	No
2969	29.69	1.69	0.68	1.01	0.92	0.740	1.06	0.700	1.00	1.30	0.911	No
2970	29.70	1.69	0.68	1.01	0.92	0.740	1.06	0.700	1.00	1.30	0.911	No
2971	29.71	1.69	0.68	1.01	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
2972	29.72	1.69	0.68	1.01	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
2973	29.73	1.69	0.68	1.01	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
2974	29.74	1.69	0.68	1.01	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
2975	29.75	1.69	0.68	1.01	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
2976	29.76	1.69	0.68	1.01	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
2977	29.77	1.69	0.68	1.01	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
2978	29.78	1.69	0.68	1.02	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
2979	29.79	1.70	0.68	1.02	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
2980	29.80	1.70	0.68	1.02	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
2981	29.81	1.70	0.68	1.02	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
2982	29.82	1.70	0.68	1.02	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
2983	29.83	1.70	0.68	1.02	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
2984	29.84	1.70	0.68	1.02	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
2985	29.85	1.70	0.68	1.02	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
2986	29.86	1.70	0.68	1.02	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
2987	29.87	1.70	0.68	1.02	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
2988	29.88	1.70	0.68	1.02	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
2989	29.89	1.70	0.68	1.02	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
2990	29.90	1.70	0.68	1.02	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
2991	29.91	1.70	0.68	1.02	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
2992	29.92	1.70	0.68	1.02	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
2993	29.93	1.70	0.68	1.02	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
2994	29.94	1.70	0.68	1.02	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
2995	29.95	1.70	0.68	1.02	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
2996	29.96	1.71	0.69	1.02	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
2997	29.97	1.71	0.69	1.02	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
2998	29.98	1.71	0.69	1.02	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
2999	29.99	1.71	0.69	1.02	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3000	30.00	1.71	0.69	1.02	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3001	30.01	1.71	0.69	1.02	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3002	30.02	1.71	0.69	1.02	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3003	30.03	1.71	0.69	1.02	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3004	30.04	1.71	0.69	1.02	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3005	30.05	1.71	0.69	1.02	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3006	30.06	1.71	0.69	1.02	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3007	30.07	1.71	0.69	1.02	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3008	30.08	1.71	0.69	1.02	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3009	30.09	1.71	0.69	1.02	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3010	30.10	1.71	0.69	1.02	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3011	30.11	1.71	0.69	1.02	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3012	30.12	1.72	0.69	1.03	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3013	30.13	1.72	0.69	1.03	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3014	30.14	1.72	0.69	1.03	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3015	30.15	1.72	0.69	1.03	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3016	30.16	1.72	0.69	1.03	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3017	30.17	1.72	0.69	1.03	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3018	30.18	1.72	0.69	1.03	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3019	30.19	1.72	0.69	1.03	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3020	30.20	1.72	0.69	1.03	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3021	30.21	1.72	0.69	1.03	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3022	30.22	1.72	0.69	1.03	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3023	30.23	1.72	0.69	1.03	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3024	30.24	1.72	0.69	1.03	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
3025	30.25	1.72	0.69	1.03	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3026	30.26	1.72	0.69	1.03	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3027	30.27	1.72	0.69	1.03	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3028	30.28	1.73	0.70	1.03	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3029	30.29	1.73	0.70	1.03	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3030	30.30	1.73	0.70	1.03	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3031	30.31	1.73	0.70	1.03	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3032	30.32	1.73	0.70	1.03	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3033	30.33	1.73	0.70	1.03	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3034	30.34	1.73	0.70	1.03	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3035	30.35	1.73	0.70	1.03	0.92	0.741	1.06	0.701	1.00	1.30	0.911	No
3036	30.36	1.73	0.70	1.03	0.92	0.741	1.06	0.701	1.00	1.30	0.911	No
3037	30.37	1.73	0.70	1.03	0.92	0.741	1.06	0.701	1.00	1.30	0.911	No
3038	30.38	1.73	0.70	1.03	0.92	0.741	1.06	0.701	1.00	1.30	0.911	No
3039	30.39	1.73	0.70	1.03	0.92	0.741	1.06	0.701	1.00	1.30	0.911	No
3040	30.40	1.73	0.70	1.03	0.92	0.741	1.06	0.701	1.00	1.30	0.911	No
3041	30.41	1.73	0.70	1.03	0.92	0.741	1.06	0.701	1.00	1.30	0.911	No
3042	30.42	1.73	0.70	1.03	0.92	0.741	1.06	0.701	1.00	1.30	0.911	No
3043	30.43	1.73	0.70	1.03	0.92	0.741	1.06	0.701	1.00	1.30	0.911	No
3044	30.44	1.74	0.70	1.03	0.92	0.741	1.06	0.701	1.00	1.30	0.911	No
3045	30.45	1.74	0.70	1.04	0.92	0.741	1.06	0.701	1.00	1.30	0.911	No
3046	30.46	1.74	0.70	1.04	0.92	0.741	1.06	0.701	1.00	1.30	0.911	No
3047	30.47	1.74	0.70	1.04	0.92	0.741	1.06	0.701	1.00	1.30	0.911	No
3048	30.48	1.74	0.70	1.04	0.92	0.741	1.06	0.701	1.00	1.30	0.911	No
3049	30.49	1.74	0.70	1.04	0.92	0.741	1.06	0.701	1.00	1.30	0.911	No
3050	30.50	1.74	0.70	1.04	0.92	0.741	1.06	0.701	1.00	1.30	0.911	No
3051	30.51	1.74	0.70	1.04	0.92	0.741	1.06	0.701	1.00	1.30	0.911	No
3052	30.52	1.74	0.70	1.04	0.92	0.741	1.06	0.701	1.00	1.30	0.911	No
3053	30.53	1.74	0.70	1.04	0.92	0.741	1.06	0.701	1.00	1.30	2.000	Yes
3054	30.54	1.74	0.70	1.04	0.92	0.741	1.06	0.701	1.00	1.30	2.000	Yes
3055	30.55	1.74	0.70	1.04	0.92	0.741	1.06	0.701	1.00	1.30	2.000	Yes
3056	30.56	1.74	0.70	1.04	0.92	0.741	1.06	0.701	1.00	1.30	2.000	Yes
3057	30.57	1.74	0.70	1.04	0.92	0.741	1.06	0.701	1.00	1.30	2.000	Yes
3058	30.58	1.74	0.70	1.04	0.92	0.741	1.06	0.701	1.00	1.30	2.000	Yes
3059	30.59	1.74	0.70	1.04	0.92	0.741	1.06	0.701	1.00	1.30	2.000	Yes
3060	30.60	1.74	0.71	1.04	0.92	0.741	1.06	0.701	1.00	1.30	2.000	Yes
3061	30.61	1.75	0.71	1.04	0.92	0.741	1.06	0.701	1.00	1.30	2.000	Yes
3062	30.62	1.75	0.71	1.04	0.92	0.741	1.06	0.701	1.00	1.30	2.000	Yes
3063	30.63	1.75	0.71	1.04	0.92	0.741	1.06	0.701	1.00	1.30	2.000	Yes
3064	30.64	1.75	0.71	1.04	0.92	0.741	1.06	0.701	1.00	1.30	2.000	Yes
3065	30.65	1.75	0.71	1.04	0.92	0.741	1.06	0.701	1.00	1.30	2.000	Yes
3066	30.66	1.75	0.71	1.04	0.92	0.741	1.06	0.701	1.00	1.30	2.000	Yes
3067	30.67	1.75	0.71	1.04	0.92	0.741	1.06	0.701	1.00	1.30	2.000	Yes
3068	30.68	1.75	0.71	1.04	0.92	0.741	1.06	0.701	1.00	1.30	2.000	Yes
3069	30.69	1.75	0.71	1.04	0.92	0.741	1.06	0.701	1.00	1.30	2.000	Yes
3070	30.70	1.75	0.71	1.04	0.92	0.741	1.06	0.701	1.00	1.30	2.000	Yes
3071	30.71	1.75	0.71	1.04	0.92	0.741	1.06	0.701	1.00	1.30	2.000	Yes
3072	30.72	1.75	0.71	1.04	0.92	0.741	1.06	0.701	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
3073	30.73	1.75	0.71	1.04	0.92	0.741	1.06	0.701	1.00	1.30	2.000	Yes
3074	30.74	1.75	0.71	1.04	0.92	0.741	1.06	0.701	1.00	1.30	2.000	Yes
3075	30.75	1.75	0.71	1.04	0.92	0.741	1.06	0.701	1.00	1.30	2.000	Yes
3076	30.76	1.76	0.71	1.04	0.92	0.741	1.06	0.701	1.00	1.30	2.000	Yes
3077	30.77	1.76	0.71	1.05	0.92	0.741	1.06	0.701	1.00	1.30	2.000	Yes
3078	30.78	1.76	0.71	1.05	0.92	0.741	1.06	0.701	1.00	1.30	2.000	Yes
3079	30.79	1.76	0.71	1.05	0.92	0.741	1.06	0.701	1.00	1.30	2.000	Yes
3080	30.80	1.76	0.71	1.05	0.92	0.741	1.06	0.701	1.00	1.30	2.000	Yes
3081	30.81	1.76	0.71	1.05	0.92	0.741	1.06	0.701	1.00	1.30	2.000	Yes
3082	30.82	1.76	0.71	1.05	0.92	0.741	1.06	0.701	1.00	1.30	2.000	Yes
3083	30.83	1.76	0.71	1.05	0.92	0.741	1.06	0.701	1.00	1.30	2.000	Yes
3084	30.84	1.76	0.71	1.05	0.92	0.741	1.06	0.701	1.00	1.30	2.000	Yes
3085	30.85	1.76	0.71	1.05	0.92	0.740	1.06	0.701	1.00	1.30	2.000	Yes
3086	30.86	1.76	0.71	1.05	0.92	0.740	1.06	0.701	1.00	1.30	2.000	Yes
3087	30.87	1.76	0.71	1.05	0.92	0.740	1.06	0.701	1.00	1.30	2.000	Yes
3088	30.88	1.76	0.71	1.05	0.92	0.740	1.06	0.701	1.00	1.30	2.000	Yes
3089	30.89	1.76	0.71	1.05	0.92	0.740	1.06	0.701	1.00	1.30	2.000	Yes
3090	30.90	1.76	0.71	1.05	0.92	0.740	1.06	0.701	1.00	1.30	2.000	Yes
3091	30.91	1.76	0.71	1.05	0.92	0.740	1.06	0.701	1.00	1.30	2.000	Yes
3092	30.92	1.77	0.72	1.05	0.92	0.740	1.06	0.701	1.00	1.30	2.000	Yes
3093	30.93	1.77	0.72	1.05	0.92	0.740	1.06	0.701	1.00	1.30	2.000	Yes
3094	30.94	1.77	0.72	1.05	0.92	0.740	1.06	0.701	1.00	1.30	2.000	Yes
3095	30.95	1.77	0.72	1.05	0.92	0.740	1.06	0.701	1.00	1.30	2.000	Yes
3096	30.96	1.77	0.72	1.05	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3097	30.97	1.77	0.72	1.05	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3098	30.98	1.77	0.72	1.05	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3099	30.99	1.77	0.72	1.05	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3100	31.00	1.77	0.72	1.05	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3101	31.01	1.77	0.72	1.05	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3102	31.02	1.77	0.72	1.05	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3103	31.03	1.77	0.72	1.05	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3104	31.04	1.77	0.72	1.05	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3105	31.05	1.77	0.72	1.05	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3106	31.06	1.77	0.72	1.05	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
3107	31.07	1.77	0.72	1.05	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No
3108	31.08	1.78	0.72	1.06	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No
3109	31.09	1.78	0.72	1.06	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No
3110	31.10	1.78	0.72	1.06	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No
3111	31.11	1.78	0.72	1.06	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No
3112	31.12	1.78	0.72	1.06	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No
3113	31.13	1.78	0.72	1.06	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No
3114	31.14	1.78	0.72	1.06	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No
3115	31.15	1.78	0.72	1.06	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No
3116	31.16	1.78	0.72	1.06	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No
3117	31.17	1.78	0.72	1.06	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No
3118	31.18	1.78	0.72	1.06	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No
3119	31.19	1.78	0.72	1.06	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No
3120	31.20	1.78	0.72	1.06	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
3121	31.21	1.78	0.72	1.06	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No
3122	31.22	1.78	0.72	1.06	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No
3123	31.23	1.79	0.72	1.06	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No
3124	31.24	1.79	0.73	1.06	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No
3125	31.25	1.79	0.73	1.06	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No
3126	31.26	1.79	0.73	1.06	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No
3127	31.27	1.79	0.73	1.06	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No
3128	31.28	1.79	0.73	1.06	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No
3129	31.29	1.79	0.73	1.06	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No
3130	31.30	1.79	0.73	1.06	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No
3131	31.31	1.79	0.73	1.06	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No
3132	31.32	1.79	0.73	1.06	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No
3133	31.33	1.79	0.73	1.06	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No
3134	31.34	1.79	0.73	1.06	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No
3135	31.35	1.79	0.73	1.06	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No
3136	31.36	1.79	0.73	1.06	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No
3137	31.37	1.79	0.73	1.07	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No
3138	31.38	1.79	0.73	1.07	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No
3139	31.39	1.80	0.73	1.07	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No
3140	31.40	1.80	0.73	1.07	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No
3141	31.41	1.80	0.73	1.07	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No
3142	31.42	1.80	0.73	1.07	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No
3143	31.43	1.80	0.73	1.07	0.91	0.740	1.06	0.701	1.00	1.30	0.911	No
3144	31.44	1.80	0.73	1.07	0.91	0.740	1.06	0.700	1.00	1.30	0.911	No
3145	31.45	1.80	0.73	1.07	0.91	0.740	1.06	0.700	1.00	1.30	0.911	No
3146	31.46	1.80	0.73	1.07	0.91	0.740	1.06	0.700	1.00	1.30	0.911	No
3147	31.47	1.80	0.73	1.07	0.91	0.740	1.06	0.700	1.00	1.30	0.911	No
3148	31.48	1.80	0.73	1.07	0.91	0.740	1.06	0.700	1.00	1.30	0.911	No
3149	31.49	1.80	0.73	1.07	0.91	0.740	1.06	0.700	1.00	1.30	0.911	No
3150	31.50	1.80	0.73	1.07	0.91	0.740	1.06	0.700	1.00	1.30	0.911	No
3151	31.51	1.80	0.73	1.07	0.91	0.740	1.06	0.700	1.00	1.30	0.911	No
3152	31.52	1.80	0.73	1.07	0.91	0.740	1.06	0.700	1.00	1.30	0.911	No
3153	31.53	1.80	0.73	1.07	0.91	0.740	1.06	0.700	1.00	1.30	0.911	No
3154	31.54	1.81	0.73	1.07	0.91	0.740	1.06	0.700	1.00	1.30	0.910	No
3155	31.55	1.81	0.73	1.07	0.91	0.740	1.06	0.700	1.00	1.30	0.910	No
3156	31.56	1.81	0.74	1.07	0.91	0.740	1.06	0.700	1.00	1.30	0.910	No
3157	31.57	1.81	0.74	1.07	0.91	0.740	1.06	0.700	1.00	1.30	0.910	No
3158	31.58	1.81	0.74	1.07	0.91	0.740	1.06	0.700	1.00	1.30	0.910	No
3159	31.59	1.81	0.74	1.07	0.91	0.740	1.06	0.700	1.00	1.30	0.910	No
3160	31.60	1.81	0.74	1.07	0.91	0.740	1.06	0.700	1.00	1.30	0.910	No
3161	31.61	1.81	0.74	1.07	0.91	0.740	1.06	0.700	1.00	1.30	0.910	No
3162	31.62	1.81	0.74	1.07	0.91	0.740	1.06	0.700	1.00	1.30	0.910	No
3163	31.63	1.81	0.74	1.07	0.91	0.740	1.06	0.700	1.00	1.30	0.910	No
3164	31.64	1.81	0.74	1.07	0.91	0.740	1.06	0.700	1.00	1.30	0.910	No
3165	31.65	1.81	0.74	1.07	0.91	0.740	1.06	0.700	1.00	1.30	0.910	No
3166	31.66	1.81	0.74	1.07	0.91	0.740	1.06	0.700	1.00	1.30	0.910	No
3167	31.67	1.81	0.74	1.08	0.91	0.740	1.06	0.700	1.00	1.30	0.910	No
3168	31.68	1.81	0.74	1.08	0.91	0.740	1.06	0.700	1.00	1.30	0.910	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
3169	31.69	1.82	0.74	1.08	0.91	0.740	1.06	0.700	1.00	1.30	0.910	No
3170	31.70	1.82	0.74	1.08	0.91	0.740	1.06	0.700	1.00	1.30	0.910	No
3171	31.71	1.82	0.74	1.08	0.91	0.740	1.06	0.700	1.00	1.30	0.910	No
3172	31.72	1.82	0.74	1.08	0.91	0.740	1.06	0.700	1.00	1.30	0.910	No
3173	31.73	1.82	0.74	1.08	0.91	0.740	1.06	0.700	1.00	1.30	0.910	No
3174	31.74	1.82	0.74	1.08	0.91	0.740	1.06	0.700	1.00	1.30	0.910	No
3175	31.75	1.82	0.74	1.08	0.91	0.740	1.06	0.700	1.00	1.30	0.910	No
3176	31.76	1.82	0.74	1.08	0.91	0.740	1.06	0.700	1.00	1.30	0.910	No
3177	31.77	1.82	0.74	1.08	0.91	0.740	1.06	0.700	1.00	1.30	0.910	No
3178	31.78	1.82	0.74	1.08	0.91	0.740	1.06	0.700	1.00	1.30	0.910	No
3179	31.79	1.82	0.74	1.08	0.91	0.739	1.06	0.700	1.00	1.30	0.910	No
3180	31.80	1.82	0.74	1.08	0.91	0.739	1.06	0.700	1.00	1.30	0.910	No
3181	31.81	1.82	0.74	1.08	0.91	0.739	1.06	0.700	1.00	1.30	0.910	No
3182	31.82	1.82	0.74	1.08	0.91	0.739	1.06	0.700	1.00	1.30	0.910	No
3183	31.83	1.82	0.74	1.08	0.91	0.739	1.06	0.700	1.00	1.30	0.910	No
3184	31.84	1.82	0.74	1.08	0.91	0.739	1.06	0.700	1.00	1.30	0.910	No
3185	31.85	1.83	0.74	1.08	0.91	0.739	1.06	0.700	1.00	1.30	0.910	No
3186	31.86	1.83	0.74	1.08	0.91	0.739	1.06	0.700	1.00	1.30	0.910	No
3187	31.87	1.83	0.74	1.08	0.91	0.739	1.06	0.700	1.00	1.30	0.910	No
3188	31.88	1.83	0.75	1.08	0.91	0.739	1.06	0.700	1.00	1.30	0.910	No
3189	31.89	1.83	0.75	1.08	0.91	0.739	1.06	0.700	1.00	1.30	0.910	No
3190	31.90	1.83	0.75	1.08	0.91	0.739	1.06	0.700	1.00	1.30	0.910	No
3191	31.91	1.83	0.75	1.08	0.91	0.739	1.06	0.700	1.00	1.30	0.910	No
3192	31.92	1.83	0.75	1.08	0.91	0.739	1.06	0.700	1.00	1.30	0.910	No
3193	31.93	1.83	0.75	1.08	0.91	0.739	1.06	0.700	1.00	1.30	0.910	No
3194	31.94	1.83	0.75	1.08	0.91	0.739	1.06	0.700	1.00	1.30	0.910	No
3195	31.95	1.83	0.75	1.08	0.91	0.739	1.06	0.700	1.00	1.30	0.910	No
3196	31.96	1.83	0.75	1.09	0.91	0.739	1.06	0.700	1.00	1.30	0.910	No
3197	31.97	1.83	0.75	1.09	0.91	0.739	1.06	0.700	1.00	1.30	0.910	No
3198	31.98	1.83	0.75	1.09	0.91	0.739	1.06	0.700	1.00	1.30	0.910	No
3199	31.99	1.83	0.75	1.09	0.91	0.739	1.06	0.700	1.00	1.30	0.910	No
3200	32.00	1.84	0.75	1.09	0.91	0.739	1.06	0.700	1.00	1.30	0.910	No
3201	32.01	1.84	0.75	1.09	0.91	0.739	1.06	0.700	1.00	1.30	0.910	No
3202	32.02	1.84	0.75	1.09	0.91	0.739	1.06	0.700	1.00	1.30	0.910	No
3203	32.03	1.84	0.75	1.09	0.91	0.739	1.06	0.700	1.00	1.30	0.910	No
3204	32.04	1.84	0.75	1.09	0.91	0.739	1.06	0.700	1.00	1.30	0.910	No
3205	32.05	1.84	0.75	1.09	0.91	0.739	1.06	0.700	1.00	1.30	0.910	No
3206	32.06	1.84	0.75	1.09	0.91	0.739	1.06	0.700	1.00	1.30	0.909	No
3207	32.07	1.84	0.75	1.09	0.91	0.739	1.06	0.700	1.00	1.30	0.909	No
3208	32.08	1.84	0.75	1.09	0.91	0.739	1.06	0.700	1.00	1.30	0.909	No
3209	32.09	1.84	0.75	1.09	0.91	0.739	1.06	0.700	1.00	1.30	0.909	No
3210	32.10	1.84	0.75	1.09	0.91	0.739	1.06	0.700	1.00	1.30	0.909	No
3211	32.11	1.84	0.75	1.09	0.91	0.739	1.06	0.700	1.00	1.30	0.909	No
3212	32.12	1.84	0.75	1.09	0.91	0.739	1.06	0.700	1.00	1.30	0.909	No
3213	32.13	1.84	0.75	1.09	0.91	0.739	1.06	0.699	1.00	1.30	0.909	No
3214	32.14	1.84	0.75	1.09	0.91	0.739	1.06	0.699	1.00	1.30	0.909	No
3215	32.15	1.85	0.75	1.09	0.91	0.739	1.06	0.699	1.00	1.30	0.909	No
3216	32.16	1.85	0.75	1.09	0.91	0.739	1.06	0.699	1.00	1.30	0.909	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
3217	32.17	1.85	0.75	1.09	0.91	0.739	1.06	0.699	1.00	1.30	0.909	No
3218	32.18	1.85	0.75	1.09	0.91	0.739	1.06	0.699	1.00	1.30	0.909	No
3219	32.19	1.85	0.75	1.09	0.91	0.739	1.06	0.699	1.00	1.30	0.909	No
3220	32.20	1.85	0.76	1.09	0.91	0.739	1.06	0.699	1.00	1.30	0.909	No
3221	32.21	1.85	0.76	1.09	0.91	0.739	1.06	0.699	1.00	1.30	0.909	No
3222	32.22	1.85	0.76	1.09	0.91	0.739	1.06	0.699	1.00	1.30	0.909	No
3223	32.23	1.85	0.76	1.09	0.91	0.739	1.06	0.699	1.00	1.30	0.909	No
3224	32.24	1.85	0.76	1.09	0.91	0.739	1.06	0.699	1.00	1.30	0.909	No
3225	32.25	1.85	0.76	1.10	0.91	0.739	1.06	0.699	1.00	1.30	0.909	No
3226	32.26	1.85	0.76	1.10	0.91	0.739	1.06	0.699	1.00	1.30	0.909	No
3227	32.27	1.85	0.76	1.10	0.91	0.739	1.06	0.699	1.00	1.30	0.909	No
3228	32.28	1.85	0.76	1.10	0.91	0.739	1.06	0.699	1.00	1.30	0.909	No
3229	32.29	1.85	0.76	1.10	0.91	0.739	1.06	0.699	1.00	1.30	0.909	No
3230	32.30	1.86	0.76	1.10	0.91	0.739	1.06	0.699	1.00	1.30	0.909	No
3231	32.31	1.86	0.76	1.10	0.91	0.739	1.06	0.699	1.00	1.30	0.909	No
3232	32.32	1.86	0.76	1.10	0.91	0.739	1.06	0.699	1.00	1.30	0.909	No
3233	32.33	1.86	0.76	1.10	0.91	0.739	1.06	0.699	1.00	1.30	0.909	No
3234	32.34	1.86	0.76	1.10	0.91	0.739	1.06	0.699	1.00	1.30	0.909	No
3235	32.35	1.86	0.76	1.10	0.91	0.739	1.06	0.699	1.00	1.30	0.909	No
3236	32.36	1.86	0.76	1.10	0.91	0.738	1.06	0.699	1.00	1.30	0.909	No
3237	32.37	1.86	0.76	1.10	0.91	0.738	1.06	0.699	1.00	1.30	0.909	No
3238	32.38	1.86	0.76	1.10	0.91	0.738	1.06	0.699	1.00	1.30	0.909	No
3239	32.39	1.86	0.76	1.10	0.91	0.738	1.06	0.699	1.00	1.30	0.909	No
3240	32.40	1.86	0.76	1.10	0.91	0.738	1.06	0.699	1.00	1.30	0.909	No
3241	32.41	1.86	0.76	1.10	0.91	0.738	1.06	0.699	1.00	1.30	0.909	No
3242	32.42	1.86	0.76	1.10	0.91	0.738	1.06	0.699	1.00	1.30	0.909	No
3243	32.43	1.86	0.76	1.10	0.91	0.738	1.06	0.699	1.00	1.30	0.909	No
3244	32.44	1.86	0.76	1.10	0.91	0.738	1.06	0.699	1.00	1.30	0.909	No
3245	32.45	1.86	0.76	1.10	0.91	0.738	1.06	0.699	1.00	1.30	0.909	No
3246	32.46	1.87	0.76	1.10	0.91	0.738	1.06	0.699	1.00	1.30	0.909	No
3247	32.47	1.87	0.76	1.10	0.91	0.738	1.06	0.699	1.00	1.30	0.909	No
3248	32.48	1.87	0.76	1.10	0.91	0.738	1.06	0.699	1.00	1.30	0.909	No
3249	32.49	1.87	0.76	1.10	0.91	0.738	1.06	0.699	1.00	1.30	0.908	No
3250	32.50	1.87	0.76	1.10	0.91	0.738	1.06	0.699	1.00	1.30	0.908	No
3251	32.51	1.87	0.76	1.10	0.91	0.738	1.06	0.699	1.00	1.30	0.908	No
3252	32.52	1.87	0.77	1.10	0.91	0.738	1.06	0.699	1.00	1.30	0.908	No
3253	32.53	1.87	0.77	1.10	0.91	0.738	1.06	0.699	1.00	1.30	0.908	No
3254	32.54	1.87	0.77	1.11	0.91	0.738	1.06	0.699	1.00	1.30	0.908	No
3255	32.55	1.87	0.77	1.11	0.91	0.738	1.06	0.699	1.00	1.30	0.908	No
3256	32.56	1.87	0.77	1.11	0.91	0.738	1.06	0.699	1.00	1.30	0.908	No
3257	32.57	1.87	0.77	1.11	0.91	0.738	1.06	0.699	1.00	1.30	0.908	No
3258	32.58	1.87	0.77	1.11	0.91	0.738	1.06	0.699	1.00	1.30	0.908	No
3259	32.59	1.87	0.77	1.11	0.91	0.738	1.06	0.699	1.00	1.30	0.908	No
3260	32.60	1.87	0.77	1.11	0.91	0.738	1.06	0.699	1.00	1.30	0.908	No
3261	32.61	1.88	0.77	1.11	0.91	0.738	1.06	0.699	1.00	1.30	0.908	No
3262	32.62	1.88	0.77	1.11	0.91	0.738	1.06	0.699	1.00	1.30	0.908	No
3263	32.63	1.88	0.77	1.11	0.91	0.738	1.06	0.699	1.00	1.30	0.908	No
3264	32.64	1.88	0.77	1.11	0.91	0.738	1.06	0.699	1.00	1.30	0.908	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
3265	32.65	1.88	0.77	1.11	0.91	0.738	1.06	0.699	1.00	1.30	0.908	No
3266	32.66	1.88	0.77	1.11	0.91	0.738	1.06	0.698	1.00	1.30	0.908	No
3267	32.67	1.88	0.77	1.11	0.91	0.738	1.06	0.698	1.00	1.30	0.908	No
3268	32.68	1.88	0.77	1.11	0.91	0.738	1.06	0.698	1.00	1.30	0.908	No
3269	32.69	1.88	0.77	1.11	0.91	0.738	1.06	0.698	1.00	1.30	0.908	No
3270	32.70	1.88	0.77	1.11	0.91	0.738	1.06	0.698	1.00	1.30	0.908	No
3271	32.71	1.88	0.77	1.11	0.91	0.738	1.06	0.698	1.00	1.30	0.908	No
3272	32.72	1.88	0.77	1.11	0.91	0.738	1.06	0.698	1.00	1.30	0.908	No
3273	32.73	1.88	0.77	1.11	0.91	0.738	1.06	0.698	1.00	1.30	0.908	No
3274	32.74	1.88	0.77	1.11	0.91	0.738	1.06	0.698	1.00	1.30	0.908	No
3275	32.75	1.88	0.77	1.11	0.91	0.738	1.06	0.698	1.00	1.30	0.908	No
3276	32.76	1.89	0.77	1.11	0.91	0.738	1.06	0.698	1.00	1.30	0.908	No
3277	32.77	1.89	0.77	1.11	0.91	0.738	1.06	0.698	1.00	1.30	0.908	No
3278	32.78	1.89	0.77	1.11	0.91	0.738	1.06	0.698	1.00	1.30	0.908	No
3279	32.79	1.89	0.77	1.11	0.91	0.738	1.06	0.698	1.00	1.30	0.908	No
3280	32.80	1.89	0.77	1.11	0.90	0.738	1.06	0.698	1.00	1.30	0.908	No
3281	32.81	1.89	0.77	1.11	0.90	0.738	1.06	0.698	1.00	1.30	0.908	No
3282	32.82	1.89	0.77	1.12	0.90	0.737	1.06	0.698	1.00	1.30	0.908	No
3283	32.83	1.89	0.77	1.12	0.90	0.737	1.06	0.698	1.00	1.30	0.908	No
3284	32.84	1.89	0.78	1.12	0.90	0.737	1.06	0.698	1.00	1.30	0.908	No
3285	32.85	1.89	0.78	1.12	0.90	0.737	1.06	0.698	1.00	1.30	0.907	No
3286	32.86	1.89	0.78	1.12	0.90	0.737	1.06	0.698	1.00	1.30	0.907	No
3287	32.87	1.89	0.78	1.12	0.90	0.737	1.06	0.698	1.00	1.30	0.907	No
3288	32.88	1.89	0.78	1.12	0.90	0.737	1.06	0.698	1.00	1.30	0.907	No
3289	32.89	1.89	0.78	1.12	0.90	0.737	1.06	0.698	1.00	1.30	0.907	No
3290	32.90	1.89	0.78	1.12	0.90	0.737	1.06	0.698	1.00	1.30	0.907	No
3291	32.91	1.90	0.78	1.12	0.90	0.737	1.06	0.698	1.00	1.30	0.907	No
3292	32.92	1.90	0.78	1.12	0.90	0.737	1.06	0.698	1.00	1.30	0.907	No
3293	32.93	1.90	0.78	1.12	0.90	0.737	1.06	0.698	1.00	1.30	0.907	No
3294	32.94	1.90	0.78	1.12	0.90	0.737	1.06	0.698	1.00	1.30	0.907	No
3295	32.95	1.90	0.78	1.12	0.90	0.737	1.06	0.698	1.00	1.30	0.907	No
3296	32.96	1.90	0.78	1.12	0.90	0.737	1.06	0.698	1.00	1.30	0.907	No
3297	32.97	1.90	0.78	1.12	0.90	0.737	1.06	0.698	1.00	1.30	0.907	No
3298	32.98	1.90	0.78	1.12	0.90	0.737	1.06	0.698	1.00	1.30	0.907	No
3299	32.99	1.90	0.78	1.12	0.90	0.737	1.06	0.698	1.00	1.30	0.907	No
3300	33.00	1.90	0.78	1.12	0.90	0.737	1.06	0.698	1.00	1.30	0.907	No
3301	33.01	1.90	0.78	1.12	0.90	0.737	1.06	0.698	1.00	1.30	0.907	No
3302	33.02	1.90	0.78	1.12	0.90	0.737	1.06	0.698	1.00	1.30	0.907	No
3303	33.03	1.90	0.78	1.12	0.90	0.737	1.06	0.698	1.00	1.30	0.907	No
3304	33.04	1.90	0.78	1.12	0.90	0.737	1.06	0.698	1.00	1.30	0.907	No
3305	33.05	1.90	0.78	1.12	0.90	0.737	1.06	0.698	1.00	1.30	0.907	No
3306	33.06	1.91	0.78	1.12	0.90	0.737	1.06	0.698	1.00	1.30	0.907	No
3307	33.07	1.91	0.78	1.12	0.90	0.737	1.06	0.698	1.00	1.30	0.907	No
3308	33.08	1.91	0.78	1.12	0.90	0.737	1.06	0.697	1.00	1.30	0.907	No
3309	33.09	1.91	0.78	1.12	0.90	0.737	1.06	0.697	1.00	1.30	0.907	No
3310	33.10	1.91	0.78	1.13	0.90	0.737	1.06	0.697	1.00	1.30	0.907	No
3311	33.11	1.91	0.78	1.13	0.90	0.737	1.06	0.697	1.00	1.30	0.907	No
3312	33.12	1.91	0.78	1.13	0.90	0.737	1.06	0.697	1.00	1.30	0.907	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
3313	33.13	1.91	0.78	1.13	0.90	0.737	1.06	0.697	1.00	1.30	0.907	No
3314	33.14	1.91	0.78	1.13	0.90	0.737	1.06	0.697	1.00	1.30	0.907	No
3315	33.15	1.91	0.78	1.13	0.90	0.737	1.06	0.697	1.00	1.30	0.907	No
3316	33.16	1.91	0.78	1.13	0.90	0.737	1.06	0.697	1.00	1.30	0.906	No
3317	33.17	1.91	0.79	1.13	0.90	0.737	1.06	0.697	1.00	1.30	0.906	No
3318	33.18	1.91	0.79	1.13	0.90	0.737	1.06	0.697	1.00	1.30	0.906	No
3319	33.19	1.91	0.79	1.13	0.90	0.737	1.06	0.697	1.00	1.30	0.906	No
3320	33.20	1.91	0.79	1.13	0.90	0.736	1.06	0.697	1.00	1.30	0.906	No
3321	33.21	1.92	0.79	1.13	0.90	0.736	1.06	0.697	1.00	1.30	0.906	No
3322	33.22	1.92	0.79	1.13	0.90	0.736	1.06	0.697	1.00	1.30	0.906	No
3323	33.23	1.92	0.79	1.13	0.90	0.736	1.06	0.697	1.00	1.30	0.906	No
3324	33.24	1.92	0.79	1.13	0.90	0.736	1.06	0.697	1.00	1.30	0.906	No
3325	33.25	1.92	0.79	1.13	0.90	0.736	1.06	0.697	1.00	1.30	0.906	No
3326	33.26	1.92	0.79	1.13	0.90	0.736	1.06	0.697	1.00	1.30	0.906	No
3327	33.27	1.92	0.79	1.13	0.90	0.736	1.06	0.697	1.00	1.30	0.906	No
3328	33.28	1.92	0.79	1.13	0.90	0.736	1.06	0.697	1.00	1.30	0.906	No
3329	33.29	1.92	0.79	1.13	0.90	0.736	1.06	0.697	1.00	1.30	0.906	No
3330	33.30	1.92	0.79	1.13	0.90	0.736	1.06	0.697	1.00	1.30	0.906	No
3331	33.31	1.92	0.79	1.13	0.90	0.736	1.06	0.697	1.00	1.30	0.906	No
3332	33.32	1.92	0.79	1.13	0.90	0.736	1.06	0.697	1.00	1.30	0.906	No
3333	33.33	1.92	0.79	1.13	0.90	0.736	1.06	0.697	1.00	1.30	0.906	No
3334	33.34	1.92	0.79	1.13	0.90	0.736	1.06	0.697	1.00	1.30	0.906	No
3335	33.35	1.93	0.79	1.13	0.90	0.736	1.06	0.697	1.00	1.30	0.906	No
3336	33.36	1.93	0.79	1.13	0.90	0.736	1.06	0.697	1.00	1.30	0.906	No
3337	33.37	1.93	0.79	1.13	0.90	0.736	1.06	0.697	1.00	1.30	0.906	No
3338	33.38	1.93	0.79	1.14	0.90	0.736	1.06	0.697	1.00	1.30	0.906	No
3339	33.39	1.93	0.79	1.14	0.90	0.736	1.06	0.697	1.00	1.30	0.906	No
3340	33.40	1.93	0.79	1.14	0.90	0.736	1.06	0.697	1.00	1.30	0.906	No
3341	33.41	1.93	0.79	1.14	0.90	0.736	1.06	0.697	1.00	1.30	0.906	No
3342	33.42	1.93	0.79	1.14	0.90	0.736	1.06	0.697	1.00	1.30	0.906	No
3343	33.43	1.93	0.79	1.14	0.90	0.736	1.06	0.697	1.00	1.30	0.906	No
3344	33.44	1.93	0.79	1.14	0.90	0.736	1.06	0.697	1.00	1.30	0.906	No
3345	33.45	1.93	0.79	1.14	0.90	0.736	1.06	0.697	1.00	1.30	0.905	No
3346	33.46	1.93	0.79	1.14	0.90	0.736	1.06	0.696	1.00	1.30	0.905	No
3347	33.47	1.93	0.79	1.14	0.90	0.736	1.06	0.696	1.00	1.30	0.905	No
3348	33.48	1.93	0.79	1.14	0.90	0.736	1.06	0.696	1.00	1.30	0.905	No
3349	33.49	1.93	0.80	1.14	0.90	0.736	1.06	0.696	1.00	1.30	0.905	No
3350	33.50	1.94	0.80	1.14	0.90	0.736	1.06	0.696	1.00	1.30	0.905	No
3351	33.51	1.94	0.80	1.14	0.90	0.736	1.06	0.696	1.00	1.30	0.905	No
3352	33.52	1.94	0.80	1.14	0.90	0.736	1.06	0.696	1.00	1.30	0.905	No
3353	33.53	1.94	0.80	1.14	0.90	0.736	1.06	0.696	1.00	1.30	0.905	No
3354	33.54	1.94	0.80	1.14	0.90	0.736	1.06	0.696	1.00	1.30	0.905	No
3355	33.55	1.94	0.80	1.14	0.90	0.736	1.06	0.696	1.00	1.30	0.905	No
3356	33.56	1.94	0.80	1.14	0.90	0.735	1.06	0.696	1.00	1.30	0.905	No
3357	33.57	1.94	0.80	1.14	0.90	0.735	1.06	0.696	1.00	1.30	0.905	No
3358	33.58	1.94	0.80	1.14	0.90	0.735	1.06	0.696	1.00	1.30	0.905	No
3359	33.59	1.94	0.80	1.14	0.90	0.735	1.06	0.696	1.00	1.30	0.905	No
3360	33.60	1.94	0.80	1.14	0.90	0.735	1.06	0.696	1.00	1.30	0.905	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
3361	33.61	1.94	0.80	1.14	0.90	0.735	1.06	0.696	1.00	1.30	0.905	No
3362	33.62	1.94	0.80	1.14	0.90	0.735	1.06	0.696	1.00	1.30	0.905	No
3363	33.63	1.94	0.80	1.14	0.90	0.735	1.06	0.696	1.00	1.30	0.905	No
3364	33.64	1.94	0.80	1.14	0.90	0.735	1.06	0.696	1.00	1.30	0.905	No
3365	33.65	1.95	0.80	1.14	0.90	0.735	1.06	0.696	1.00	1.30	0.905	No
3366	33.66	1.95	0.80	1.15	0.90	0.735	1.06	0.696	1.00	1.30	0.905	No
3367	33.67	1.95	0.80	1.15	0.90	0.735	1.06	0.696	1.00	1.30	0.905	No
3368	33.68	1.95	0.80	1.15	0.90	0.735	1.06	0.696	1.00	1.30	0.905	No
3369	33.69	1.95	0.80	1.15	0.90	0.735	1.06	0.696	1.00	1.30	0.905	No
3370	33.70	1.95	0.80	1.15	0.90	0.735	1.06	0.696	1.00	1.30	0.905	No
3371	33.71	1.95	0.80	1.15	0.90	0.735	1.06	0.696	1.00	1.30	0.905	No
3372	33.72	1.95	0.80	1.15	0.90	0.735	1.06	0.696	1.00	1.30	0.905	No
3373	33.73	1.95	0.80	1.15	0.90	0.735	1.06	0.696	1.00	1.30	0.905	No
3374	33.74	1.95	0.80	1.15	0.90	0.735	1.06	0.696	1.00	1.30	0.904	No
3375	33.75	1.95	0.80	1.15	0.90	0.735	1.06	0.696	1.00	1.30	0.904	No
3376	33.76	1.95	0.80	1.15	0.90	0.735	1.06	0.696	1.00	1.30	0.904	No
3377	33.77	1.95	0.80	1.15	0.90	0.735	1.06	0.696	1.00	1.30	0.904	No
3378	33.78	1.95	0.80	1.15	0.90	0.735	1.06	0.696	1.00	1.30	0.904	No
3379	33.79	1.95	0.80	1.15	0.90	0.735	1.06	0.696	1.00	1.30	0.904	No
3380	33.80	1.96	0.80	1.15	0.90	0.735	1.06	0.696	1.00	1.30	0.904	No
3381	33.81	1.96	0.81	1.15	0.90	0.735	1.06	0.696	1.00	1.30	0.904	No
3382	33.82	1.96	0.81	1.15	0.90	0.735	1.06	0.696	1.00	1.30	0.904	No
3383	33.83	1.96	0.81	1.15	0.90	0.735	1.06	0.696	1.00	1.30	0.904	No
3384	33.84	1.96	0.81	1.15	0.90	0.735	1.06	0.695	1.00	1.30	0.904	No
3385	33.85	1.96	0.81	1.15	0.90	0.735	1.06	0.695	1.00	1.30	0.904	No
3386	33.86	1.96	0.81	1.15	0.90	0.735	1.06	0.695	1.00	1.30	0.904	No
3387	33.87	1.96	0.81	1.15	0.90	0.735	1.06	0.695	1.00	1.30	0.904	No
3388	33.88	1.96	0.81	1.15	0.90	0.735	1.06	0.695	1.00	1.30	0.904	No
3389	33.89	1.96	0.81	1.15	0.90	0.735	1.06	0.695	1.00	1.30	0.904	No
3390	33.90	1.96	0.81	1.15	0.90	0.735	1.06	0.695	1.00	1.30	0.904	No
3391	33.91	1.96	0.81	1.15	0.90	0.734	1.06	0.695	1.00	1.30	0.904	No
3392	33.92	1.96	0.81	1.15	0.90	0.734	1.06	0.695	1.00	1.30	0.904	No
3393	33.93	1.96	0.81	1.15	0.90	0.734	1.06	0.695	1.00	1.30	0.904	No
3394	33.94	1.96	0.81	1.16	0.90	0.734	1.06	0.695	1.00	1.30	0.904	No
3395	33.95	1.97	0.81	1.16	0.90	0.734	1.06	0.695	1.00	1.30	0.904	No
3396	33.96	1.97	0.81	1.16	0.90	0.734	1.06	0.695	1.00	1.30	0.904	No
3397	33.97	1.97	0.81	1.16	0.90	0.734	1.06	0.695	1.00	1.30	0.904	No
3398	33.98	1.97	0.81	1.16	0.90	0.734	1.06	0.695	1.00	1.30	0.904	No
3399	33.99	1.97	0.81	1.16	0.90	0.734	1.06	0.695	1.00	1.30	0.904	No
3400	34.00	1.97	0.81	1.16	0.90	0.734	1.06	0.695	1.00	1.30	0.904	No
3401	34.01	1.97	0.81	1.16	0.90	0.734	1.06	0.695	1.00	1.30	0.904	No
3402	34.02	1.97	0.81	1.16	0.90	0.734	1.06	0.695	1.00	1.30	0.903	No
3403	34.03	1.97	0.81	1.16	0.90	0.734	1.06	0.695	1.00	1.30	0.903	No
3404	34.04	1.97	0.81	1.16	0.90	0.734	1.06	0.695	1.00	1.30	0.903	No
3405	34.05	1.97	0.81	1.16	0.90	0.734	1.06	0.695	1.00	1.30	0.903	No
3406	34.06	1.97	0.81	1.16	0.90	0.734	1.06	0.695	1.00	1.30	0.903	No
3407	34.07	1.97	0.81	1.16	0.90	0.734	1.06	0.695	1.00	1.30	0.903	No
3408	34.08	1.97	0.81	1.16	0.90	0.734	1.06	0.695	1.00	1.30	0.903	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
3409	34.09	1.97	0.81	1.16	0.90	0.734	1.06	0.695	1.00	1.30	0.903	No
3410	34.10	1.98	0.81	1.16	0.90	0.734	1.06	0.695	1.00	1.30	0.903	No
3411	34.11	1.98	0.81	1.16	0.90	0.734	1.06	0.695	1.00	1.30	0.903	No
3412	34.12	1.98	0.81	1.16	0.90	0.734	1.06	0.695	1.00	1.30	0.903	No
3413	34.13	1.98	0.82	1.16	0.90	0.734	1.06	0.695	1.00	1.30	0.903	No
3414	34.14	1.98	0.82	1.16	0.90	0.734	1.06	0.695	1.00	1.30	0.903	No
3415	34.15	1.98	0.82	1.16	0.90	0.734	1.06	0.695	1.00	1.30	0.903	No
3416	34.16	1.98	0.82	1.16	0.90	0.734	1.06	0.695	1.00	1.30	0.903	No
3417	34.17	1.98	0.82	1.16	0.90	0.734	1.06	0.695	1.00	1.30	0.903	No
3418	34.18	1.98	0.82	1.16	0.90	0.734	1.06	0.695	1.00	1.30	0.903	No
3419	34.19	1.98	0.82	1.16	0.90	0.734	1.06	0.695	1.00	1.30	0.903	No
3420	34.20	1.98	0.82	1.16	0.90	0.734	1.06	0.694	1.00	1.30	0.903	No
3421	34.21	1.98	0.82	1.16	0.90	0.734	1.06	0.694	1.00	1.30	0.903	No
3422	34.22	1.98	0.82	1.16	0.90	0.734	1.06	0.694	1.00	1.30	0.903	No
3423	34.23	1.98	0.82	1.17	0.90	0.734	1.06	0.694	1.00	1.30	0.903	No
3424	34.24	1.98	0.82	1.17	0.90	0.734	1.06	0.694	1.00	1.30	0.903	No
3425	34.25	1.99	0.82	1.17	0.90	0.733	1.06	0.694	1.00	1.30	0.903	No
3426	34.26	1.99	0.82	1.17	0.90	0.733	1.06	0.694	1.00	1.30	0.903	No
3427	34.27	1.99	0.82	1.17	0.90	0.733	1.06	0.694	1.00	1.30	0.903	No
3428	34.28	1.99	0.82	1.17	0.90	0.733	1.06	0.694	1.00	1.30	0.903	No
3429	34.29	1.99	0.82	1.17	0.90	0.733	1.06	0.694	1.00	1.30	0.902	No
3430	34.30	1.99	0.82	1.17	0.90	0.733	1.06	0.694	1.00	1.30	0.902	No
3431	34.31	1.99	0.82	1.17	0.90	0.733	1.06	0.694	1.00	1.30	0.902	No
3432	34.32	1.99	0.82	1.17	0.90	0.733	1.06	0.694	1.00	1.30	0.902	No
3433	34.33	1.99	0.82	1.17	0.90	0.733	1.06	0.694	1.00	1.30	0.902	No
3434	34.34	1.99	0.82	1.17	0.90	0.733	1.06	0.694	1.00	1.30	0.902	No
3435	34.35	1.99	0.82	1.17	0.90	0.733	1.06	0.694	1.00	1.30	0.902	No
3436	34.36	1.99	0.82	1.17	0.89	0.733	1.06	0.694	1.00	1.30	0.902	No
3437	34.37	1.99	0.82	1.17	0.89	0.733	1.06	0.694	1.00	1.30	0.902	No
3438	34.38	1.99	0.82	1.17	0.89	0.733	1.06	0.694	1.00	1.30	0.902	No
3439	34.39	1.99	0.82	1.17	0.89	0.733	1.06	0.694	1.00	1.30	0.902	No
3440	34.40	1.99	0.82	1.17	0.89	0.733	1.06	0.694	1.00	1.30	0.902	No
3441	34.41	2.00	0.82	1.17	0.89	0.733	1.06	0.694	1.00	1.30	0.902	No
3442	34.42	2.00	0.82	1.17	0.89	0.733	1.06	0.694	1.00	1.30	0.902	No
3443	34.43	2.00	0.82	1.17	0.89	0.733	1.06	0.694	1.00	1.30	0.902	No
3444	34.44	2.00	0.82	1.17	0.89	0.733	1.06	0.694	1.00	1.30	0.902	No
3445	34.45	2.00	0.83	1.17	0.89	0.733	1.06	0.694	1.00	1.30	0.902	No
3446	34.46	2.00	0.83	1.17	0.89	0.733	1.06	0.694	1.00	1.30	0.902	No
3447	34.47	2.00	0.83	1.17	0.89	0.733	1.06	0.694	1.00	1.30	0.902	No
3448	34.48	2.00	0.83	1.17	0.89	0.733	1.06	0.694	1.00	1.30	0.902	No
3449	34.49	2.00	0.83	1.17	0.89	0.733	1.06	0.694	1.00	1.30	0.902	No
3450	34.50	2.00	0.83	1.17	0.89	0.733	1.06	0.694	1.00	1.30	0.902	No
3451	34.51	2.00	0.83	1.18	0.89	0.733	1.06	0.694	1.00	1.30	0.902	No
3452	34.52	2.00	0.83	1.18	0.89	0.733	1.06	0.694	1.00	1.30	0.902	No
3453	34.53	2.00	0.83	1.18	0.89	0.733	1.06	0.693	1.00	1.30	0.902	No
3454	34.54	2.00	0.83	1.18	0.89	0.733	1.06	0.693	1.00	1.30	0.901	No
3455	34.55	2.01	0.83	1.18	0.89	0.733	1.06	0.693	1.00	1.30	0.901	No
3456	34.56	2.01	0.83	1.18	0.89	0.732	1.06	0.693	1.00	1.30	0.901	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
3457	34.57	2.01	0.83	1.18	0.89	0.732	1.06	0.693	1.00	1.30	0.901	No
3458	34.58	2.01	0.83	1.18	0.89	0.732	1.06	0.693	1.00	1.30	0.901	No
3459	34.59	2.01	0.83	1.18	0.89	0.732	1.06	0.693	1.00	1.30	0.901	No
3460	34.60	2.01	0.83	1.18	0.89	0.732	1.06	0.693	1.00	1.30	0.901	No
3461	34.61	2.01	0.83	1.18	0.89	0.732	1.06	0.693	1.00	1.30	0.901	No
3462	34.62	2.01	0.83	1.18	0.89	0.732	1.06	0.693	1.00	1.30	0.901	No
3463	34.63	2.01	0.83	1.18	0.89	0.732	1.06	0.693	1.00	1.30	0.901	No
3464	34.64	2.01	0.83	1.18	0.89	0.732	1.06	0.693	1.00	1.30	0.901	No
3465	34.65	2.01	0.83	1.18	0.89	0.732	1.06	0.693	1.00	1.30	0.901	No
3466	34.66	2.01	0.83	1.18	0.89	0.732	1.06	0.693	1.00	1.30	0.901	No
3467	34.67	2.01	0.83	1.18	0.89	0.732	1.06	0.693	1.00	1.30	0.901	No
3468	34.68	2.01	0.83	1.18	0.89	0.732	1.06	0.693	1.00	1.30	0.901	No
3469	34.69	2.01	0.83	1.18	0.89	0.732	1.06	0.693	1.00	1.30	0.901	No
3470	34.70	2.02	0.83	1.18	0.89	0.732	1.06	0.693	1.00	1.30	0.901	No
3471	34.71	2.02	0.83	1.18	0.89	0.732	1.06	0.693	1.00	1.30	0.901	No
3472	34.72	2.02	0.83	1.18	0.89	0.732	1.06	0.693	1.00	1.30	0.901	No
3473	34.73	2.02	0.83	1.18	0.89	0.732	1.06	0.693	1.00	1.30	0.901	No
3474	34.74	2.02	0.83	1.18	0.89	0.732	1.06	0.693	1.00	1.30	0.901	No
3475	34.75	2.02	0.83	1.18	0.89	0.732	1.06	0.693	1.00	1.30	0.901	No
3476	34.76	2.02	0.83	1.18	0.89	0.732	1.06	0.693	1.00	1.30	0.901	No
3477	34.77	2.02	0.84	1.18	0.89	0.732	1.06	0.693	1.00	1.30	0.901	No
3478	34.78	2.02	0.84	1.18	0.89	0.732	1.06	0.693	1.00	1.30	0.900	No
3479	34.79	2.02	0.84	1.19	0.89	0.732	1.06	0.693	1.00	1.30	0.900	No
3480	34.80	2.02	0.84	1.19	0.89	0.732	1.06	0.693	1.00	1.30	0.900	No
3481	34.81	2.02	0.84	1.19	0.89	0.732	1.06	0.693	1.00	1.30	0.900	No
3482	34.82	2.02	0.84	1.19	0.89	0.732	1.06	0.693	1.00	1.30	0.900	No
3483	34.83	2.02	0.84	1.19	0.89	0.732	1.06	0.693	1.00	1.30	0.900	No
3484	34.84	2.02	0.84	1.19	0.89	0.732	1.06	0.692	1.00	1.30	0.900	No
3485	34.85	2.03	0.84	1.19	0.89	0.731	1.06	0.692	1.00	1.30	0.900	No
3486	34.86	2.03	0.84	1.19	0.89	0.731	1.06	0.692	1.00	1.30	0.900	No
3487	34.87	2.03	0.84	1.19	0.89	0.731	1.06	0.692	1.00	1.30	0.900	No
3488	34.88	2.03	0.84	1.19	0.89	0.731	1.06	0.692	1.00	1.30	0.900	No
3489	34.89	2.03	0.84	1.19	0.89	0.731	1.06	0.692	1.00	1.30	0.900	No
3490	34.90	2.03	0.84	1.19	0.89	0.731	1.06	0.692	1.00	1.30	0.900	No
3491	34.91	2.03	0.84	1.19	0.89	0.731	1.06	0.692	1.00	1.30	0.900	No
3492	34.92	2.03	0.84	1.19	0.89	0.731	1.06	0.692	1.00	1.30	0.900	No
3493	34.93	2.03	0.84	1.19	0.89	0.731	1.06	0.692	1.00	1.30	0.900	No
3494	34.94	2.03	0.84	1.19	0.89	0.731	1.06	0.692	1.00	1.30	0.900	No
3495	34.95	2.03	0.84	1.19	0.89	0.731	1.06	0.692	1.00	1.30	0.900	No
3496	34.96	2.03	0.84	1.19	0.89	0.731	1.06	0.692	1.00	1.30	0.900	No
3497	34.97	2.03	0.84	1.19	0.89	0.731	1.06	0.692	1.00	1.30	0.900	No
3498	34.98	2.03	0.84	1.19	0.89	0.731	1.06	0.692	1.00	1.30	0.900	No
3499	34.99	2.03	0.84	1.19	0.89	0.731	1.06	0.692	1.00	1.30	0.900	No
3500	35.00	2.04	0.84	1.19	0.89	0.731	1.06	0.692	1.00	1.30	0.900	No
3501	35.01	2.04	0.84	1.19	0.89	0.731	1.06	0.692	1.00	1.30	0.900	No
3502	35.02	2.04	0.84	1.19	0.89	0.731	1.06	0.692	1.00	1.30	0.899	No
3503	35.03	2.04	0.84	1.19	0.89	0.731	1.06	0.692	1.00	1.30	0.899	No
3504	35.04	2.04	0.84	1.19	0.89	0.731	1.06	0.692	1.00	1.30	0.899	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
3505	35.05	2.04	0.84	1.19	0.89	0.731	1.06	0.692	1.00	1.30	0.899	No
3506	35.06	2.04	0.84	1.19	0.89	0.731	1.06	0.692	1.00	1.30	0.899	No
3507	35.07	2.04	0.84	1.20	0.89	0.731	1.06	0.692	1.00	1.30	0.899	No
3508	35.08	2.04	0.84	1.20	0.89	0.731	1.06	0.692	1.00	1.30	0.899	No
3509	35.09	2.04	0.85	1.20	0.89	0.731	1.06	0.692	1.00	1.30	0.899	No
3510	35.10	2.04	0.85	1.20	0.89	0.731	1.06	0.692	1.00	1.30	0.899	No
3511	35.11	2.04	0.85	1.20	0.89	0.731	1.06	0.692	1.00	1.30	0.899	No
3512	35.12	2.04	0.85	1.20	0.89	0.731	1.06	0.692	1.00	1.30	0.899	No
3513	35.13	2.04	0.85	1.20	0.89	0.731	1.06	0.692	1.00	1.30	0.899	No
3514	35.14	2.04	0.85	1.20	0.89	0.731	1.06	0.692	1.00	1.30	0.899	No
3515	35.15	2.04	0.85	1.20	0.89	0.730	1.06	0.691	1.00	1.30	0.899	No
3516	35.16	2.05	0.85	1.20	0.89	0.730	1.06	0.691	1.00	1.30	0.899	No
3517	35.17	2.05	0.85	1.20	0.89	0.730	1.06	0.691	1.00	1.30	0.899	No
3518	35.18	2.05	0.85	1.20	0.89	0.730	1.06	0.691	1.00	1.30	0.899	No
3519	35.19	2.05	0.85	1.20	0.89	0.730	1.06	0.691	1.00	1.30	0.899	No
3520	35.20	2.05	0.85	1.20	0.89	0.730	1.06	0.691	1.00	1.30	0.899	No
3521	35.21	2.05	0.85	1.20	0.89	0.730	1.06	0.691	1.00	1.30	0.899	No
3522	35.22	2.05	0.85	1.20	0.89	0.730	1.06	0.691	1.00	1.30	0.899	No
3523	35.23	2.05	0.85	1.20	0.89	0.730	1.06	0.691	1.00	1.30	0.899	No
3524	35.24	2.05	0.85	1.20	0.89	0.730	1.06	0.691	1.00	1.30	0.899	No
3525	35.25	2.05	0.85	1.20	0.89	0.730	1.06	0.691	1.00	1.30	0.899	No
3526	35.26	2.05	0.85	1.20	0.89	0.730	1.06	0.691	1.00	1.30	0.898	No
3527	35.27	2.05	0.85	1.20	0.89	0.730	1.06	0.691	1.00	1.30	0.898	No
3528	35.28	2.05	0.85	1.20	0.89	0.730	1.06	0.691	1.00	1.30	0.898	No
3529	35.29	2.05	0.85	1.20	0.89	0.730	1.06	0.691	1.00	1.30	0.898	No
3530	35.30	2.05	0.85	1.20	0.89	0.730	1.06	0.691	1.00	1.30	0.898	No
3531	35.31	2.06	0.85	1.20	0.89	0.730	1.06	0.691	1.00	1.30	0.898	No
3532	35.32	2.06	0.85	1.20	0.89	0.730	1.06	0.691	1.00	1.30	0.898	No
3533	35.33	2.06	0.85	1.20	0.89	0.730	1.06	0.691	1.00	1.30	0.898	No
3534	35.34	2.06	0.85	1.20	0.89	0.730	1.06	0.691	1.00	1.30	0.898	No
3535	35.35	2.06	0.85	1.20	0.89	0.730	1.06	0.691	1.00	1.30	0.898	No
3536	35.36	2.06	0.85	1.20	0.89	0.730	1.06	0.691	1.00	1.30	0.898	No
3537	35.37	2.06	0.85	1.21	0.89	0.730	1.06	0.691	1.00	1.30	0.898	No
3538	35.38	2.06	0.85	1.21	0.89	0.730	1.06	0.691	1.00	1.30	0.898	No
3539	35.39	2.06	0.85	1.21	0.89	0.730	1.06	0.691	1.00	1.30	0.898	No
3540	35.40	2.06	0.85	1.21	0.89	0.730	1.06	0.691	1.00	1.30	0.898	No
3541	35.41	2.06	0.86	1.21	0.89	0.730	1.06	0.691	1.00	1.30	0.898	No
3542	35.42	2.06	0.86	1.21	0.89	0.730	1.06	0.691	1.00	1.30	0.898	No
3543	35.43	2.06	0.86	1.21	0.89	0.730	1.06	0.691	1.00	1.30	0.898	No
3544	35.44	2.06	0.86	1.21	0.89	0.730	1.06	0.691	1.00	1.30	0.898	No
3545	35.45	2.06	0.86	1.21	0.89	0.730	1.06	0.691	1.00	1.30	0.898	No
3546	35.46	2.07	0.86	1.21	0.89	0.729	1.06	0.691	1.00	1.30	0.898	No
3547	35.47	2.07	0.86	1.21	0.89	0.729	1.06	0.691	1.00	1.30	0.898	No
3548	35.48	2.07	0.86	1.21	0.89	0.729	1.06	0.690	1.00	1.30	0.898	No
3549	35.49	2.07	0.86	1.21	0.89	0.729	1.06	0.690	1.00	1.30	0.898	No
3550	35.50	2.07	0.86	1.21	0.89	0.729	1.06	0.690	1.00	1.30	0.898	No
3551	35.51	2.07	0.86	1.21	0.89	0.729	1.06	0.690	1.00	1.30	0.898	No
3552	35.52	2.07	0.86	1.21	0.89	0.729	1.06	0.690	1.00	1.30	0.897	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
3553	35.53	2.07	0.86	1.21	0.89	0.729	1.06	0.690	1.00	1.30	0.897	No
3554	35.54	2.07	0.86	1.21	0.89	0.729	1.06	0.690	1.00	1.30	0.897	No
3555	35.55	2.07	0.86	1.21	0.89	0.729	1.06	0.690	1.00	1.30	0.897	No
3556	35.56	2.07	0.86	1.21	0.89	0.729	1.06	0.690	1.00	1.30	0.897	No
3557	35.57	2.07	0.86	1.21	0.89	0.729	1.06	0.690	1.00	1.30	0.897	No
3558	35.58	2.07	0.86	1.21	0.89	0.729	1.06	0.690	1.00	1.30	0.897	No
3559	35.59	2.07	0.86	1.21	0.89	0.729	1.06	0.690	1.00	1.30	0.897	No
3560	35.60	2.07	0.86	1.21	0.89	0.729	1.06	0.690	1.00	1.30	0.897	No
3561	35.61	2.07	0.86	1.21	0.89	0.729	1.06	0.690	1.00	1.30	0.897	No
3562	35.62	2.08	0.86	1.21	0.89	0.729	1.06	0.690	1.00	1.30	0.897	No
3563	35.63	2.08	0.86	1.21	0.89	0.729	1.06	0.690	1.00	1.30	0.897	No
3564	35.64	2.08	0.86	1.21	0.89	0.729	1.06	0.690	1.00	1.30	0.897	No
3565	35.65	2.08	0.86	1.21	0.89	0.729	1.06	0.690	1.00	1.30	0.897	No
3566	35.66	2.08	0.86	1.21	0.89	0.729	1.06	0.690	1.00	1.30	0.897	No
3567	35.67	2.08	0.86	1.22	0.89	0.729	1.06	0.690	1.00	1.30	0.897	No
3568	35.68	2.08	0.86	1.22	0.89	0.729	1.06	0.690	1.00	1.30	0.897	No
3569	35.69	2.08	0.86	1.22	0.89	0.729	1.06	0.690	1.00	1.30	0.897	No
3570	35.70	2.08	0.86	1.22	0.89	0.729	1.06	0.690	1.00	1.30	0.897	No
3571	35.71	2.08	0.86	1.22	0.89	0.729	1.06	0.690	1.00	1.30	0.897	No
3572	35.72	2.08	0.86	1.22	0.89	0.729	1.06	0.690	1.00	1.30	0.897	No
3573	35.73	2.08	0.87	1.22	0.89	0.729	1.06	0.690	1.00	1.30	0.897	No
3574	35.74	2.08	0.87	1.22	0.89	0.729	1.06	0.690	1.00	1.30	0.897	No
3575	35.75	2.08	0.87	1.22	0.89	0.729	1.06	0.690	1.00	1.30	0.897	No
3576	35.76	2.08	0.87	1.22	0.89	0.729	1.06	0.690	1.00	1.30	0.897	No
3577	35.77	2.08	0.87	1.22	0.89	0.729	1.06	0.690	1.00	1.30	0.897	No
3578	35.78	2.09	0.87	1.22	0.89	0.729	1.06	0.690	1.00	1.30	0.897	No
3579	35.79	2.09	0.87	1.22	0.88	0.728	1.06	0.690	1.00	1.30	0.896	No
3580	35.80	2.09	0.87	1.22	0.88	0.728	1.06	0.690	1.00	1.30	0.896	No
3581	35.81	2.09	0.87	1.22	0.88	0.728	1.06	0.690	1.00	1.30	0.896	No
3582	35.82	2.09	0.87	1.22	0.88	0.728	1.06	0.690	1.00	1.30	0.896	No
3583	35.83	2.09	0.87	1.22	0.88	0.728	1.06	0.689	1.00	1.30	0.896	No
3584	35.84	2.09	0.87	1.22	0.88	0.728	1.06	0.689	1.00	1.30	0.896	No
3585	35.85	2.09	0.87	1.22	0.88	0.728	1.06	0.689	1.00	1.30	0.896	No
3586	35.86	2.09	0.87	1.22	0.88	0.728	1.06	0.689	1.00	1.30	0.896	No
3587	35.87	2.09	0.87	1.22	0.88	0.728	1.06	0.689	1.00	1.30	0.896	No
3588	35.88	2.09	0.87	1.22	0.88	0.728	1.06	0.689	1.00	1.30	0.896	No
3589	35.89	2.09	0.87	1.22	0.88	0.728	1.06	0.689	1.00	1.30	0.896	No
3590	35.90	2.09	0.87	1.22	0.88	0.728	1.06	0.689	1.00	1.30	0.896	No
3591	35.91	2.09	0.87	1.22	0.88	0.728	1.06	0.689	1.00	1.30	0.896	No
3592	35.92	2.09	0.87	1.22	0.88	0.728	1.06	0.689	1.00	1.30	0.896	No
3593	35.93	2.09	0.87	1.22	0.88	0.728	1.06	0.689	1.00	1.30	0.896	No
3594	35.94	2.10	0.87	1.22	0.88	0.728	1.06	0.689	1.00	1.30	0.896	No
3595	35.95	2.10	0.87	1.22	0.88	0.728	1.06	0.689	1.00	1.30	0.896	No
3596	35.96	2.10	0.87	1.22	0.88	0.728	1.06	0.689	1.00	1.30	0.896	No
3597	35.97	2.10	0.87	1.22	0.88	0.728	1.06	0.689	1.00	1.30	0.896	No
3598	35.98	2.10	0.87	1.23	0.88	0.728	1.06	0.689	1.00	1.30	0.896	No
3599	35.99	2.10	0.87	1.23	0.88	0.728	1.06	0.689	1.00	1.30	0.896	No
3600	36.00	2.10	0.87	1.23	0.88	0.728	1.06	0.689	1.00	1.30	0.896	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
3601	36.01	2.10	0.87	1.23	0.88	0.728	1.06	0.689	1.00	1.30	0.896	No
3602	36.02	2.10	0.87	1.23	0.88	0.728	1.06	0.689	1.00	1.30	0.896	No
3603	36.03	2.10	0.87	1.23	0.88	0.728	1.06	0.689	1.00	1.30	0.896	No
3604	36.04	2.10	0.87	1.23	0.88	0.728	1.06	0.689	1.00	1.30	0.896	No
3605	36.05	2.10	0.88	1.23	0.88	0.728	1.06	0.689	1.00	1.30	0.895	No
3606	36.06	2.10	0.88	1.23	0.88	0.728	1.06	0.689	1.00	1.30	0.895	No
3607	36.07	2.10	0.88	1.23	0.88	0.728	1.06	0.689	1.00	1.30	0.895	No
3608	36.08	2.10	0.88	1.23	0.88	0.728	1.06	0.689	1.00	1.30	0.895	No
3609	36.09	2.11	0.88	1.23	0.88	0.728	1.06	0.689	1.00	1.30	0.895	No
3610	36.10	2.11	0.88	1.23	0.88	0.727	1.06	0.689	1.00	1.30	0.895	No
3611	36.11	2.11	0.88	1.23	0.88	0.727	1.06	0.689	1.00	1.30	0.895	No
3612	36.12	2.11	0.88	1.23	0.88	0.727	1.06	0.689	1.00	1.30	0.895	No
3613	36.13	2.11	0.88	1.23	0.88	0.727	1.06	0.689	1.00	1.30	0.895	No
3614	36.14	2.11	0.88	1.23	0.88	0.727	1.06	0.689	1.00	1.30	0.895	No
3615	36.15	2.11	0.88	1.23	0.88	0.727	1.06	0.689	1.00	1.30	0.895	No
3616	36.16	2.11	0.88	1.23	0.88	0.727	1.06	0.688	1.00	1.30	0.895	No
3617	36.17	2.11	0.88	1.23	0.88	0.727	1.06	0.688	1.00	1.30	0.895	No
3618	36.18	2.11	0.88	1.23	0.88	0.727	1.06	0.688	1.00	1.30	0.895	No
3619	36.19	2.11	0.88	1.23	0.88	0.727	1.06	0.688	1.00	1.30	0.895	No
3620	36.20	2.11	0.88	1.23	0.88	0.727	1.06	0.688	1.00	1.30	0.895	No
3621	36.21	2.11	0.88	1.23	0.88	0.727	1.06	0.688	1.00	1.30	0.895	No
3622	36.22	2.11	0.88	1.23	0.88	0.727	1.06	0.688	1.00	1.30	0.895	No
3623	36.23	2.11	0.88	1.23	0.88	0.727	1.06	0.688	1.00	1.30	0.895	No
3624	36.24	2.11	0.88	1.23	0.88	0.727	1.06	0.688	1.00	1.30	0.895	No
3625	36.25	2.12	0.88	1.23	0.88	0.727	1.06	0.688	1.00	1.30	0.895	No
3626	36.26	2.12	0.88	1.23	0.88	0.727	1.06	0.688	1.00	1.30	0.895	No
3627	36.27	2.12	0.88	1.23	0.88	0.727	1.06	0.688	1.00	1.30	0.895	No
3628	36.28	2.12	0.88	1.23	0.88	0.727	1.06	0.688	1.00	1.30	0.895	No
3629	36.29	2.12	0.88	1.24	0.88	0.727	1.06	0.688	1.00	1.30	0.895	No
3630	36.30	2.12	0.88	1.24	0.88	0.727	1.06	0.688	1.00	1.30	0.894	No
3631	36.31	2.12	0.88	1.24	0.88	0.727	1.06	0.688	1.00	1.30	0.894	No
3632	36.32	2.12	0.88	1.24	0.88	0.727	1.06	0.688	1.00	1.30	0.894	No
3633	36.33	2.12	0.88	1.24	0.88	0.727	1.06	0.688	1.00	1.30	0.894	No
3634	36.34	2.12	0.88	1.24	0.88	0.727	1.06	0.688	1.00	1.30	0.894	No
3635	36.35	2.12	0.88	1.24	0.88	0.727	1.06	0.688	1.00	1.30	0.894	No
3636	36.36	2.12	0.88	1.24	0.88	0.727	1.06	0.688	1.00	1.30	0.894	No
3637	36.37	2.12	0.89	1.24	0.88	0.727	1.06	0.688	1.00	1.30	0.894	No
3638	36.38	2.12	0.89	1.24	0.88	0.727	1.06	0.688	1.00	1.30	0.894	No
3639	36.39	2.12	0.89	1.24	0.88	0.727	1.06	0.688	1.00	1.30	0.894	No
3640	36.40	2.12	0.89	1.24	0.88	0.726	1.06	0.688	1.00	1.30	0.894	No
3641	36.41	2.13	0.89	1.24	0.88	0.726	1.06	0.688	1.00	1.30	0.894	No
3642	36.42	2.13	0.89	1.24	0.88	0.726	1.06	0.688	1.00	1.30	0.894	No
3643	36.43	2.13	0.89	1.24	0.88	0.726	1.06	0.688	1.00	1.30	0.894	No
3644	36.44	2.13	0.89	1.24	0.88	0.726	1.06	0.688	1.00	1.30	0.894	No
3645	36.45	2.13	0.89	1.24	0.88	0.726	1.06	0.688	1.00	1.30	0.894	No
3646	36.46	2.13	0.89	1.24	0.88	0.726	1.06	0.688	1.00	1.30	0.894	No
3647	36.47	2.13	0.89	1.24	0.88	0.726	1.06	0.687	1.00	1.30	0.894	No
3648	36.48	2.13	0.89	1.24	0.88	0.726	1.06	0.687	1.00	1.30	0.894	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
3649	36.49	2.13	0.89	1.24	0.88	0.726	1.06	0.687	1.00	1.30	0.894	No
3650	36.50	2.13	0.89	1.24	0.88	0.726	1.06	0.687	1.00	1.30	0.894	No
3651	36.51	2.13	0.89	1.24	0.88	0.726	1.06	0.687	1.00	1.30	0.894	No
3652	36.52	2.13	0.89	1.24	0.88	0.726	1.06	0.687	1.00	1.30	0.894	No
3653	36.53	2.13	0.89	1.24	0.88	0.726	1.06	0.687	1.00	1.30	0.893	No
3654	36.54	2.13	0.89	1.24	0.88	0.726	1.06	0.687	1.00	1.30	0.893	No
3655	36.55	2.13	0.89	1.24	0.88	0.726	1.06	0.687	1.00	1.30	0.893	No
3656	36.56	2.13	0.89	1.24	0.88	0.726	1.06	0.687	1.00	1.30	0.893	No
3657	36.57	2.14	0.89	1.24	0.88	0.726	1.06	0.687	1.00	1.30	0.893	No
3658	36.58	2.14	0.89	1.24	0.88	0.726	1.06	0.687	1.00	1.30	0.893	No
3659	36.59	2.14	0.89	1.24	0.88	0.726	1.06	0.687	1.00	1.30	0.893	No
3660	36.60	2.14	0.89	1.25	0.88	0.726	1.06	0.687	1.00	1.30	0.893	No
3661	36.61	2.14	0.89	1.25	0.88	0.726	1.06	0.687	1.00	1.30	0.893	No
3662	36.62	2.14	0.89	1.25	0.88	0.726	1.06	0.687	1.00	1.30	0.893	No
3663	36.63	2.14	0.89	1.25	0.88	0.726	1.06	0.687	1.00	1.30	0.893	No
3664	36.64	2.14	0.89	1.25	0.88	0.726	1.06	0.687	1.00	1.30	0.893	No
3665	36.65	2.14	0.89	1.25	0.88	0.726	1.06	0.687	1.00	1.30	0.893	No
3666	36.66	2.14	0.89	1.25	0.88	0.726	1.06	0.687	1.00	1.30	0.893	No
3667	36.67	2.14	0.89	1.25	0.88	0.726	1.06	0.687	1.00	1.30	0.893	No
3668	36.68	2.14	0.89	1.25	0.88	0.725	1.06	0.687	1.00	1.30	0.893	No
3669	36.69	2.14	0.90	1.25	0.88	0.725	1.06	0.687	1.00	1.30	0.893	No
3670	36.70	2.14	0.90	1.25	0.88	0.725	1.06	0.687	1.00	1.30	0.893	No
3671	36.71	2.14	0.90	1.25	0.88	0.725	1.06	0.687	1.00	1.30	0.893	No
3672	36.72	2.15	0.90	1.25	0.88	0.725	1.06	0.687	1.00	1.30	0.893	No
3673	36.73	2.15	0.90	1.25	0.88	0.725	1.06	0.687	1.00	1.30	0.893	No
3674	36.74	2.15	0.90	1.25	0.88	0.725	1.06	0.687	1.00	1.30	0.893	No
3675	36.75	2.15	0.90	1.25	0.88	0.725	1.06	0.687	1.00	1.30	0.892	No
3676	36.76	2.15	0.90	1.25	0.88	0.725	1.06	0.686	1.00	1.30	0.892	No
3677	36.77	2.15	0.90	1.25	0.88	0.725	1.06	0.686	1.00	1.30	0.892	No
3678	36.78	2.15	0.90	1.25	0.88	0.725	1.06	0.686	1.00	1.30	0.892	No
3679	36.79	2.15	0.90	1.25	0.88	0.725	1.06	0.686	1.00	1.30	0.892	No
3680	36.80	2.15	0.90	1.25	0.88	0.725	1.06	0.686	1.00	1.30	0.892	No
3681	36.81	2.15	0.90	1.25	0.88	0.725	1.06	0.686	1.00	1.30	0.892	No
3682	36.82	2.15	0.90	1.25	0.88	0.725	1.06	0.686	1.00	1.30	0.892	No
3683	36.83	2.15	0.90	1.25	0.88	0.725	1.06	0.686	1.00	1.30	0.892	No
3684	36.84	2.15	0.90	1.25	0.88	0.725	1.06	0.686	1.00	1.30	0.892	No
3685	36.85	2.15	0.90	1.25	0.88	0.725	1.06	0.686	1.00	1.30	0.892	No
3686	36.86	2.15	0.90	1.25	0.88	0.725	1.06	0.686	1.00	1.30	0.892	No
3687	36.87	2.15	0.90	1.25	0.88	0.725	1.06	0.686	1.00	1.30	0.892	No
3688	36.88	2.16	0.90	1.25	0.88	0.725	1.06	0.686	1.00	1.30	0.892	No
3689	36.89	2.16	0.90	1.25	0.88	0.725	1.06	0.686	1.00	1.30	0.892	No
3690	36.90	2.16	0.90	1.26	0.88	0.725	1.06	0.686	1.00	1.30	0.892	No
3691	36.91	2.16	0.90	1.26	0.88	0.725	1.06	0.686	1.00	1.30	0.892	No
3692	36.92	2.16	0.90	1.26	0.88	0.725	1.06	0.686	1.00	1.30	0.892	No
3693	36.93	2.16	0.90	1.26	0.88	0.725	1.06	0.686	1.00	1.30	0.892	No
3694	36.94	2.16	0.90	1.26	0.88	0.724	1.06	0.686	1.00	1.30	0.892	No
3695	36.95	2.16	0.90	1.26	0.88	0.724	1.06	0.686	1.00	1.30	0.892	No
3696	36.96	2.16	0.90	1.26	0.88	0.724	1.06	0.686	1.00	1.30	0.891	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
3697	36.97	2.16	0.90	1.26	0.88	0.724	1.06	0.686	1.00	1.30	0.891	No
3698	36.98	2.16	0.90	1.26	0.88	0.724	1.06	0.686	1.00	1.30	0.891	No
3699	36.99	2.16	0.90	1.26	0.88	0.724	1.06	0.686	1.00	1.30	0.891	No
3700	37.00	2.16	0.90	1.26	0.88	0.724	1.06	0.686	1.00	1.30	0.891	No
3701	37.01	2.16	0.91	1.26	0.88	0.724	1.06	0.686	1.00	1.30	0.891	No
3702	37.02	2.16	0.91	1.26	0.88	0.724	1.06	0.686	1.00	1.30	0.891	No
3703	37.03	2.17	0.91	1.26	0.88	0.724	1.06	0.685	1.00	1.30	0.891	No
3704	37.04	2.17	0.91	1.26	0.88	0.724	1.06	0.685	1.00	1.30	0.891	No
3705	37.05	2.17	0.91	1.26	0.88	0.724	1.06	0.685	1.00	1.30	0.891	No
3706	37.06	2.17	0.91	1.26	0.88	0.724	1.06	0.685	1.00	1.30	0.891	No
3707	37.07	2.17	0.91	1.26	0.88	0.724	1.06	0.685	1.00	1.30	0.891	No
3708	37.08	2.17	0.91	1.26	0.88	0.724	1.06	0.685	1.00	1.30	0.891	No
3709	37.09	2.17	0.91	1.26	0.88	0.724	1.06	0.685	1.00	1.30	0.891	No
3710	37.10	2.17	0.91	1.26	0.88	0.724	1.06	0.685	1.00	1.30	0.891	No
3711	37.11	2.17	0.91	1.26	0.88	0.724	1.06	0.685	1.00	1.30	0.891	No
3712	37.12	2.17	0.91	1.26	0.87	0.724	1.06	0.685	1.00	1.30	0.891	No
3713	37.13	2.17	0.91	1.26	0.87	0.724	1.06	0.685	1.00	1.30	0.891	No
3714	37.14	2.17	0.91	1.26	0.87	0.724	1.06	0.685	1.00	1.30	0.891	No
3715	37.15	2.17	0.91	1.26	0.87	0.724	1.06	0.685	1.00	1.30	0.891	No
3716	37.16	2.17	0.91	1.26	0.87	0.724	1.06	0.685	1.00	1.30	0.891	No
3717	37.17	2.17	0.91	1.26	0.87	0.724	1.06	0.685	1.00	1.30	0.890	No
3718	37.18	2.17	0.91	1.26	0.87	0.724	1.06	0.685	1.00	1.30	0.890	No
3719	37.19	2.18	0.91	1.26	0.87	0.723	1.06	0.685	1.00	1.30	0.890	No
3720	37.20	2.18	0.91	1.26	0.87	0.723	1.06	0.685	1.00	1.30	0.890	No
3721	37.21	2.18	0.91	1.27	0.87	0.723	1.06	0.685	1.00	1.30	0.890	No
3722	37.22	2.18	0.91	1.27	0.87	0.723	1.06	0.685	1.00	1.30	0.890	No
3723	37.23	2.18	0.91	1.27	0.87	0.723	1.06	0.685	1.00	1.30	0.890	No
3724	37.24	2.18	0.91	1.27	0.87	0.723	1.06	0.685	1.00	1.30	0.890	No
3725	37.25	2.18	0.91	1.27	0.87	0.723	1.06	0.685	1.00	1.30	0.890	No
3726	37.26	2.18	0.91	1.27	0.87	0.723	1.06	0.685	1.00	1.30	0.890	No
3727	37.27	2.18	0.91	1.27	0.87	0.723	1.06	0.685	1.00	1.30	0.890	No
3728	37.28	2.18	0.91	1.27	0.87	0.723	1.06	0.685	1.00	1.30	0.890	No
3729	37.29	2.18	0.91	1.27	0.87	0.723	1.06	0.685	1.00	1.30	0.890	No
3730	37.30	2.18	0.91	1.27	0.87	0.723	1.06	0.684	1.00	1.30	0.890	No
3731	37.31	2.18	0.91	1.27	0.87	0.723	1.06	0.684	1.00	1.30	0.890	No
3732	37.32	2.18	0.91	1.27	0.87	0.723	1.06	0.684	1.00	1.30	0.890	No
3733	37.33	2.18	0.92	1.27	0.87	0.723	1.06	0.684	1.00	1.30	0.890	No
3734	37.34	2.18	0.92	1.27	0.87	0.723	1.06	0.684	1.00	1.30	0.890	No
3735	37.35	2.19	0.92	1.27	0.87	0.723	1.06	0.684	1.00	1.30	0.890	No
3736	37.36	2.19	0.92	1.27	0.87	0.723	1.06	0.684	1.00	1.30	0.890	No
3737	37.37	2.19	0.92	1.27	0.87	0.723	1.06	0.684	1.00	1.30	0.889	No
3738	37.38	2.19	0.92	1.27	0.87	0.723	1.06	0.684	1.00	1.30	0.889	No
3739	37.39	2.19	0.92	1.27	0.87	0.723	1.06	0.684	1.00	1.30	0.889	No
3740	37.40	2.19	0.92	1.27	0.87	0.723	1.06	0.684	1.00	1.30	0.889	No
3741	37.41	2.19	0.92	1.27	0.87	0.723	1.06	0.684	1.00	1.30	0.889	No
3742	37.42	2.19	0.92	1.27	0.87	0.723	1.06	0.684	1.00	1.30	0.889	No
3743	37.43	2.19	0.92	1.27	0.87	0.723	1.06	0.684	1.00	1.30	0.889	No
3744	37.44	2.19	0.92	1.27	0.87	0.723	1.06	0.684	1.00	1.30	0.889	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
3745	37.45	2.19	0.92	1.27	0.87	0.722	1.06	0.684	1.00	1.30	0.889	No
3746	37.46	2.19	0.92	1.27	0.87	0.722	1.06	0.684	1.00	1.30	0.889	No
3747	37.47	2.19	0.92	1.27	0.87	0.722	1.06	0.684	1.00	1.30	0.889	No
3748	37.48	2.19	0.92	1.27	0.87	0.722	1.06	0.684	1.00	1.30	0.889	No
3749	37.49	2.19	0.92	1.27	0.87	0.722	1.06	0.684	1.00	1.30	0.889	No
3750	37.50	2.20	0.92	1.27	0.87	0.722	1.06	0.684	1.00	1.30	0.889	No
3751	37.51	2.20	0.92	1.28	0.87	0.722	1.06	0.684	1.00	1.30	0.889	No
3752	37.52	2.20	0.92	1.28	0.87	0.722	1.06	0.684	1.00	1.30	0.889	No
3753	37.53	2.20	0.92	1.28	0.87	0.722	1.06	0.684	1.00	1.30	0.889	No
3754	37.54	2.20	0.92	1.28	0.87	0.722	1.06	0.684	1.00	1.30	0.889	No
3755	37.55	2.20	0.92	1.28	0.87	0.722	1.06	0.684	1.00	1.30	0.889	No
3756	37.56	2.20	0.92	1.28	0.87	0.722	1.06	0.683	1.00	1.30	0.889	No
3757	37.57	2.20	0.92	1.28	0.87	0.722	1.06	0.683	1.00	1.30	0.888	No
3758	37.58	2.20	0.92	1.28	0.87	0.722	1.06	0.683	1.00	1.30	0.888	No
3759	37.59	2.20	0.92	1.28	0.87	0.722	1.06	0.683	1.00	1.30	0.888	No
3760	37.60	2.20	0.92	1.28	0.87	0.722	1.06	0.683	1.00	1.30	0.888	No
3761	37.61	2.20	0.92	1.28	0.87	0.722	1.06	0.683	1.00	1.30	0.888	No
3762	37.62	2.20	0.92	1.28	0.87	0.722	1.06	0.683	1.00	1.30	0.888	No
3763	37.63	2.20	0.92	1.28	0.87	0.722	1.06	0.683	1.00	1.30	0.888	No
3764	37.64	2.20	0.92	1.28	0.87	0.722	1.06	0.683	1.00	1.30	0.888	No
3765	37.65	2.20	0.93	1.28	0.87	0.722	1.06	0.683	1.00	1.30	0.888	No
3766	37.66	2.21	0.93	1.28	0.87	0.722	1.06	0.683	1.00	1.30	0.888	No
3767	37.67	2.21	0.93	1.28	0.87	0.722	1.06	0.683	1.00	1.30	0.888	No
3768	37.68	2.21	0.93	1.28	0.87	0.722	1.06	0.683	1.00	1.30	0.888	No
3769	37.69	2.21	0.93	1.28	0.87	0.721	1.06	0.683	1.00	1.30	0.888	No
3770	37.70	2.21	0.93	1.28	0.87	0.721	1.06	0.683	1.00	1.30	0.888	No
3771	37.71	2.21	0.93	1.28	0.87	0.721	1.06	0.683	1.00	1.30	2.000	Yes
3772	37.72	2.21	0.93	1.28	0.87	0.721	1.06	0.683	1.00	1.30	2.000	Yes
3773	37.73	2.21	0.93	1.28	0.87	0.721	1.06	0.683	1.00	1.30	2.000	Yes
3774	37.74	2.21	0.93	1.28	0.87	0.721	1.06	0.683	1.00	1.30	2.000	Yes
3775	37.75	2.21	0.93	1.28	0.87	0.721	1.06	0.683	1.00	1.30	2.000	Yes
3776	37.76	2.21	0.93	1.28	0.87	0.721	1.06	0.683	1.00	1.30	2.000	Yes
3777	37.77	2.21	0.93	1.28	0.87	0.721	1.06	0.683	1.00	1.30	2.000	Yes
3778	37.78	2.21	0.93	1.28	0.87	0.721	1.06	0.683	1.00	1.30	2.000	Yes
3779	37.79	2.21	0.93	1.28	0.87	0.721	1.06	0.683	1.00	1.30	2.000	Yes
3780	37.80	2.21	0.93	1.28	0.87	0.721	1.06	0.683	1.00	1.30	2.000	Yes
3781	37.81	2.22	0.93	1.28	0.87	0.721	1.06	0.682	1.00	1.30	2.000	Yes
3782	37.82	2.22	0.93	1.29	0.87	0.721	1.06	0.682	1.00	1.30	2.000	Yes
3783	37.83	2.22	0.93	1.29	0.87	0.721	1.06	0.682	1.00	1.30	2.000	Yes
3784	37.84	2.22	0.93	1.29	0.87	0.721	1.06	0.682	1.00	1.30	2.000	Yes
3785	37.85	2.22	0.93	1.29	0.87	0.721	1.06	0.682	1.00	1.30	2.000	Yes
3786	37.86	2.22	0.93	1.29	0.87	0.721	1.06	0.682	1.00	1.30	2.000	Yes
3787	37.87	2.22	0.93	1.29	0.87	0.721	1.06	0.682	1.00	1.30	2.000	Yes
3788	37.88	2.22	0.93	1.29	0.87	0.721	1.06	0.682	1.00	1.30	2.000	Yes
3789	37.89	2.22	0.93	1.29	0.87	0.721	1.06	0.682	1.00	1.30	2.000	Yes
3790	37.90	2.22	0.93	1.29	0.87	0.721	1.06	0.682	1.00	1.30	2.000	Yes
3791	37.91	2.22	0.93	1.29	0.87	0.721	1.06	0.682	1.00	1.30	2.000	Yes
3792	37.92	2.22	0.93	1.29	0.87	0.720	1.06	0.682	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
3793	37.93	2.22	0.93	1.29	0.87	0.720	1.06	0.682	1.00	1.30	2.000	Yes
3794	37.94	2.22	0.93	1.29	0.87	0.720	1.06	0.682	1.00	1.30	2.000	Yes
3795	37.95	2.22	0.93	1.29	0.87	0.720	1.06	0.682	1.00	1.30	2.000	Yes
3796	37.96	2.22	0.93	1.29	0.87	0.720	1.06	0.682	1.00	1.30	2.000	Yes
3797	37.97	2.23	0.94	1.29	0.87	0.720	1.06	0.682	1.00	1.30	2.000	Yes
3798	37.98	2.23	0.94	1.29	0.87	0.720	1.06	0.682	1.00	1.30	2.000	Yes
3799	37.99	2.23	0.94	1.29	0.87	0.720	1.06	0.682	1.00	1.30	2.000	Yes
3800	38.00	2.23	0.94	1.29	0.87	0.720	1.06	0.682	1.00	1.30	2.000	Yes
3801	38.01	2.23	0.94	1.29	0.87	0.720	1.06	0.682	1.00	1.30	2.000	Yes
3802	38.02	2.23	0.94	1.29	0.87	0.720	1.06	0.682	1.00	1.30	2.000	Yes
3803	38.03	2.23	0.94	1.29	0.87	0.720	1.06	0.682	1.00	1.30	2.000	Yes
3804	38.04	2.23	0.94	1.29	0.87	0.720	1.06	0.681	1.00	1.30	2.000	Yes
3805	38.05	2.23	0.94	1.29	0.87	0.720	1.06	0.681	1.00	1.30	2.000	Yes
3806	38.06	2.23	0.94	1.29	0.87	0.720	1.06	0.681	1.00	1.30	2.000	Yes
3807	38.07	2.23	0.94	1.29	0.87	0.720	1.06	0.681	1.00	1.30	0.886	No
3808	38.08	2.23	0.94	1.29	0.87	0.720	1.06	0.681	1.00	1.30	0.886	No
3809	38.09	2.23	0.94	1.29	0.87	0.720	1.06	0.681	1.00	1.30	0.886	No
3810	38.10	2.23	0.94	1.29	0.87	0.720	1.06	0.681	1.00	1.30	0.886	No
3811	38.11	2.23	0.94	1.30	0.87	0.720	1.06	0.681	1.00	1.30	0.886	No
3812	38.12	2.24	0.94	1.30	0.87	0.720	1.06	0.681	1.00	1.30	0.885	No
3813	38.13	2.24	0.94	1.30	0.87	0.719	1.06	0.681	1.00	1.30	0.885	No
3814	38.14	2.24	0.94	1.30	0.87	0.719	1.06	0.681	1.00	1.30	0.885	No
3815	38.15	2.24	0.94	1.30	0.87	0.719	1.06	0.681	1.00	1.30	2.000	Yes
3816	38.16	2.24	0.94	1.30	0.87	0.719	1.06	0.681	1.00	1.30	2.000	Yes
3817	38.17	2.24	0.94	1.30	0.87	0.719	1.06	0.681	1.00	1.30	2.000	Yes
3818	38.18	2.24	0.94	1.30	0.87	0.719	1.06	0.681	1.00	1.30	2.000	Yes
3819	38.19	2.24	0.94	1.30	0.87	0.719	1.06	0.681	1.00	1.30	2.000	Yes
3820	38.20	2.24	0.94	1.30	0.87	0.719	1.06	0.681	1.00	1.30	2.000	Yes
3821	38.21	2.24	0.94	1.30	0.87	0.719	1.06	0.681	1.00	1.30	2.000	Yes
3822	38.22	2.24	0.94	1.30	0.87	0.719	1.06	0.681	1.00	1.30	2.000	Yes
3823	38.23	2.24	0.94	1.30	0.87	0.719	1.06	0.681	1.00	1.30	2.000	Yes
3824	38.24	2.24	0.94	1.30	0.87	0.719	1.06	0.681	1.00	1.30	2.000	Yes
3825	38.25	2.24	0.94	1.30	0.87	0.719	1.06	0.681	1.00	1.30	2.000	Yes
3826	38.26	2.24	0.94	1.30	0.87	0.719	1.06	0.681	1.00	1.30	2.000	Yes
3827	38.27	2.25	0.94	1.30	0.87	0.719	1.06	0.680	1.00	1.30	2.000	Yes
3828	38.28	2.25	0.94	1.30	0.87	0.719	1.06	0.680	1.00	1.30	2.000	Yes
3829	38.29	2.25	0.95	1.30	0.87	0.719	1.06	0.680	1.00	1.30	2.000	Yes
3830	38.30	2.25	0.95	1.30	0.87	0.719	1.06	0.680	1.00	1.30	2.000	Yes
3831	38.31	2.25	0.95	1.30	0.87	0.719	1.06	0.680	1.00	1.30	2.000	Yes
3832	38.32	2.25	0.95	1.30	0.87	0.719	1.06	0.680	1.00	1.30	2.000	Yes
3833	38.33	2.25	0.95	1.30	0.87	0.719	1.06	0.680	1.00	1.30	2.000	Yes
3834	38.34	2.25	0.95	1.30	0.87	0.718	1.06	0.680	1.00	1.30	2.000	Yes
3835	38.35	2.25	0.95	1.30	0.87	0.718	1.06	0.680	1.00	1.30	2.000	Yes
3836	38.36	2.25	0.95	1.30	0.87	0.718	1.06	0.680	1.00	1.30	2.000	Yes
3837	38.37	2.25	0.95	1.30	0.86	0.718	1.06	0.680	1.00	1.30	2.000	Yes
3838	38.38	2.25	0.95	1.30	0.86	0.718	1.06	0.680	1.00	1.30	2.000	Yes
3839	38.39	2.25	0.95	1.30	0.86	0.718	1.06	0.680	1.00	1.30	2.000	Yes
3840	38.40	2.25	0.95	1.31	0.86	0.718	1.06	0.680	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
3841	38.41	2.25	0.95	1.31	0.86	0.718	1.06	0.680	1.00	1.30	2.000	Yes
3842	38.42	2.25	0.95	1.31	0.86	0.718	1.06	0.680	1.00	1.30	2.000	Yes
3843	38.43	2.26	0.95	1.31	0.86	0.718	1.06	0.680	1.00	1.30	2.000	Yes
3844	38.44	2.26	0.95	1.31	0.86	0.718	1.06	0.680	1.00	1.30	2.000	Yes
3845	38.45	2.26	0.95	1.31	0.86	0.718	1.06	0.680	1.00	1.30	2.000	Yes
3846	38.46	2.26	0.95	1.31	0.86	0.718	1.06	0.680	1.00	1.30	2.000	Yes
3847	38.47	2.26	0.95	1.31	0.86	0.718	1.06	0.680	1.00	1.30	2.000	Yes
3848	38.48	2.26	0.95	1.31	0.86	0.718	1.06	0.679	1.00	1.30	0.883	No
3849	38.49	2.26	0.95	1.31	0.86	0.718	1.06	0.679	1.00	1.30	0.883	No
3850	38.50	2.26	0.95	1.31	0.86	0.718	1.06	0.679	1.00	1.30	0.883	No
3851	38.51	2.26	0.95	1.31	0.86	0.718	1.06	0.679	1.00	1.30	0.883	No
3852	38.52	2.26	0.95	1.31	0.86	0.718	1.06	0.679	1.00	1.30	0.883	No
3853	38.53	2.26	0.95	1.31	0.86	0.718	1.06	0.679	1.00	1.30	0.883	No
3854	38.54	2.26	0.95	1.31	0.86	0.717	1.06	0.679	1.00	1.30	0.883	No
3855	38.55	2.26	0.95	1.31	0.86	0.717	1.06	0.679	1.00	1.30	0.883	No
3856	38.56	2.26	0.95	1.31	0.86	0.717	1.06	0.679	1.00	1.30	0.883	No
3857	38.57	2.26	0.95	1.31	0.86	0.717	1.06	0.679	1.00	1.30	0.883	No
3858	38.58	2.27	0.95	1.31	0.86	0.717	1.06	0.679	1.00	1.30	0.883	No
3859	38.59	2.27	0.95	1.31	0.86	0.717	1.06	0.679	1.00	1.30	0.883	No
3860	38.60	2.27	0.95	1.31	0.86	0.717	1.06	0.679	1.00	1.30	0.883	No
3861	38.61	2.27	0.96	1.31	0.86	0.717	1.06	0.679	1.00	1.30	0.882	No
3862	38.62	2.27	0.96	1.31	0.86	0.717	1.06	0.679	1.00	1.30	0.882	No
3863	38.63	2.27	0.96	1.31	0.86	0.717	1.06	0.679	1.00	1.30	0.882	No
3864	38.64	2.27	0.96	1.31	0.86	0.717	1.06	0.679	1.00	1.30	0.882	No
3865	38.65	2.27	0.96	1.31	0.86	0.717	1.06	0.679	1.00	1.30	0.882	No
3866	38.66	2.27	0.96	1.31	0.86	0.717	1.06	0.679	1.00	1.30	0.882	No
3867	38.67	2.27	0.96	1.31	0.86	0.717	1.06	0.679	1.00	1.30	0.882	No
3868	38.68	2.27	0.96	1.32	0.86	0.717	1.06	0.678	1.00	1.30	0.882	No
3869	38.69	2.27	0.96	1.32	0.86	0.717	1.06	0.678	1.00	1.30	0.882	No
3870	38.70	2.27	0.96	1.32	0.86	0.717	1.06	0.678	1.00	1.30	0.882	No
3871	38.71	2.27	0.96	1.32	0.86	0.717	1.06	0.678	1.00	1.30	0.882	No
3872	38.72	2.27	0.96	1.32	0.86	0.717	1.06	0.678	1.00	1.30	0.882	No
3873	38.73	2.28	0.96	1.32	0.86	0.716	1.06	0.678	1.00	1.30	0.882	No
3874	38.74	2.28	0.96	1.32	0.86	0.716	1.06	0.678	1.00	1.30	0.882	No
3875	38.75	2.28	0.96	1.32	0.86	0.716	1.06	0.678	1.00	1.30	0.882	No
3876	38.76	2.28	0.96	1.32	0.86	0.716	1.06	0.678	1.00	1.30	0.881	No
3877	38.77	2.28	0.96	1.32	0.86	0.716	1.06	0.678	1.00	1.30	0.881	No
3878	38.78	2.28	0.96	1.32	0.86	0.716	1.06	0.678	1.00	1.30	0.881	No
3879	38.79	2.28	0.96	1.32	0.86	0.716	1.06	0.678	1.00	1.30	0.881	No
3880	38.80	2.28	0.96	1.32	0.86	0.716	1.06	0.678	1.00	1.30	0.881	No
3881	38.81	2.28	0.96	1.32	0.86	0.716	1.06	0.678	1.00	1.30	0.881	No
3882	38.82	2.28	0.96	1.32	0.86	0.716	1.06	0.678	1.00	1.30	0.881	No
3883	38.83	2.28	0.96	1.32	0.86	0.716	1.06	0.678	1.00	1.30	0.881	No
3884	38.84	2.28	0.96	1.32	0.86	0.716	1.06	0.678	1.00	1.30	0.881	No
3885	38.85	2.28	0.96	1.32	0.86	0.716	1.06	0.678	1.00	1.30	0.881	No
3886	38.86	2.28	0.96	1.32	0.86	0.716	1.06	0.678	1.00	1.30	0.881	No
3887	38.87	2.29	0.96	1.32	0.86	0.716	1.06	0.678	1.00	1.30	0.881	No
3888	38.88	2.29	0.96	1.32	0.86	0.716	1.06	0.677	1.00	1.30	0.881	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
3889	38.89	2.29	0.96	1.32	0.86	0.716	1.06	0.677	1.00	1.30	0.881	No
3890	38.90	2.29	0.96	1.32	0.86	0.716	1.06	0.677	1.00	1.30	0.881	No
3891	38.91	2.29	0.96	1.32	0.86	0.715	1.06	0.677	1.00	1.30	0.880	No
3892	38.92	2.29	0.96	1.32	0.86	0.715	1.06	0.677	1.00	1.30	0.880	No
3893	38.93	2.29	0.97	1.32	0.86	0.715	1.06	0.677	1.00	1.30	0.880	No
3894	38.94	2.29	0.97	1.32	0.86	0.715	1.06	0.677	1.00	1.30	0.880	No
3895	38.95	2.29	0.97	1.32	0.86	0.715	1.06	0.677	1.00	1.30	0.880	No
3896	38.96	2.29	0.97	1.33	0.86	0.715	1.06	0.677	1.00	1.30	0.880	No
3897	38.97	2.29	0.97	1.33	0.86	0.715	1.06	0.677	1.00	1.30	0.880	No
3898	38.98	2.29	0.97	1.33	0.86	0.715	1.06	0.677	1.00	1.30	0.880	No
3899	38.99	2.29	0.97	1.33	0.86	0.715	1.06	0.677	1.00	1.30	0.880	No
3900	39.00	2.29	0.97	1.33	0.86	0.715	1.06	0.677	1.00	1.30	0.880	No
3901	39.01	2.29	0.97	1.33	0.86	0.715	1.06	0.677	1.00	1.30	0.880	No
3902	39.02	2.30	0.97	1.33	0.86	0.715	1.06	0.677	1.00	1.30	0.880	No
3903	39.03	2.30	0.97	1.33	0.86	0.715	1.06	0.677	1.00	1.30	0.880	No
3904	39.04	2.30	0.97	1.33	0.86	0.715	1.06	0.677	1.00	1.30	0.880	No
3905	39.05	2.30	0.97	1.33	0.86	0.715	1.06	0.677	1.00	1.30	0.880	No
3906	39.06	2.30	0.97	1.33	0.86	0.715	1.06	0.677	1.00	1.30	0.879	No
3907	39.07	2.30	0.97	1.33	0.86	0.715	1.06	0.676	1.00	1.30	0.879	No
3908	39.08	2.30	0.97	1.33	0.86	0.715	1.06	0.676	1.00	1.30	0.879	No
3909	39.09	2.30	0.97	1.33	0.86	0.714	1.06	0.676	1.00	1.30	0.879	No
3910	39.10	2.30	0.97	1.33	0.86	0.714	1.06	0.676	1.00	1.30	0.879	No
3911	39.11	2.30	0.97	1.33	0.86	0.714	1.06	0.676	1.00	1.30	0.879	No
3912	39.12	2.30	0.97	1.33	0.86	0.714	1.06	0.676	1.00	1.30	0.879	No
3913	39.13	2.30	0.97	1.33	0.86	0.714	1.06	0.676	1.00	1.30	0.879	No
3914	39.14	2.30	0.97	1.33	0.86	0.714	1.06	0.676	1.00	1.30	0.879	No
3915	39.15	2.30	0.97	1.33	0.86	0.714	1.06	0.676	1.00	1.30	0.879	No
3916	39.16	2.30	0.97	1.33	0.86	0.714	1.06	0.676	1.00	1.30	0.879	No
3917	39.17	2.31	0.97	1.33	0.86	0.714	1.06	0.676	1.00	1.30	0.879	No
3918	39.18	2.31	0.97	1.33	0.86	0.714	1.06	0.676	1.00	1.30	0.879	No
3919	39.19	2.31	0.97	1.33	0.86	0.714	1.06	0.676	1.00	1.30	0.879	No
3920	39.20	2.31	0.97	1.33	0.86	0.714	1.06	0.676	1.00	1.30	0.879	No
3921	39.21	2.31	0.97	1.33	0.86	0.714	1.06	0.676	1.00	1.30	0.878	No
3922	39.22	2.31	0.97	1.33	0.86	0.714	1.06	0.676	1.00	1.30	0.878	No
3923	39.23	2.31	0.97	1.33	0.86	0.714	1.06	0.676	1.00	1.30	0.878	No
3924	39.24	2.31	0.97	1.34	0.86	0.714	1.06	0.676	1.00	1.30	0.878	No
3925	39.25	2.31	0.98	1.34	0.86	0.714	1.06	0.676	1.00	1.30	0.878	No
3926	39.26	2.31	0.98	1.34	0.86	0.714	1.06	0.675	1.00	1.30	0.878	No
3927	39.27	2.31	0.98	1.34	0.86	0.714	1.06	0.675	1.00	1.30	0.878	No
3928	39.28	2.31	0.98	1.34	0.86	0.713	1.06	0.675	1.00	1.30	0.878	No
3929	39.29	2.31	0.98	1.34	0.86	0.713	1.06	0.675	1.00	1.30	0.878	No
3930	39.30	2.31	0.98	1.34	0.86	0.713	1.06	0.675	1.00	1.30	0.878	No
3931	39.31	2.31	0.98	1.34	0.86	0.713	1.06	0.675	1.00	1.30	0.878	No
3932	39.32	2.32	0.98	1.34	0.86	0.713	1.06	0.675	1.00	1.30	0.878	No
3933	39.33	2.32	0.98	1.34	0.86	0.713	1.06	0.675	1.00	1.30	0.878	No
3934	39.34	2.32	0.98	1.34	0.86	0.713	1.06	0.675	1.00	1.30	0.878	No
3935	39.35	2.32	0.98	1.34	0.86	0.713	1.06	0.675	1.00	1.30	0.878	No
3936	39.36	2.32	0.98	1.34	0.86	0.713	1.06	0.675	1.00	1.30	0.877	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
3937	39.37	2.32	0.98	1.34	0.86	0.713	1.06	0.675	1.00	1.30	0.877	No
3938	39.38	2.32	0.98	1.34	0.86	0.713	1.06	0.675	1.00	1.30	0.877	No
3939	39.39	2.32	0.98	1.34	0.86	0.713	1.06	0.675	1.00	1.30	0.877	No
3940	39.40	2.32	0.98	1.34	0.86	0.713	1.06	0.675	1.00	1.30	0.877	No
3941	39.41	2.32	0.98	1.34	0.86	0.713	1.06	0.675	1.00	1.30	0.877	No
3942	39.42	2.32	0.98	1.34	0.86	0.713	1.06	0.675	1.00	1.30	0.877	No
3943	39.43	2.32	0.98	1.34	0.86	0.713	1.06	0.675	1.00	1.30	0.877	No
3944	39.44	2.32	0.98	1.34	0.86	0.713	1.06	0.675	1.00	1.30	0.877	No
3945	39.45	2.32	0.98	1.34	0.86	0.712	1.06	0.674	1.00	1.30	0.877	No
3946	39.46	2.32	0.98	1.34	0.86	0.712	1.06	0.674	1.00	1.30	0.877	No
3947	39.47	2.33	0.98	1.34	0.86	0.712	1.06	0.674	1.00	1.30	0.877	No
3948	39.48	2.33	0.98	1.34	0.86	0.712	1.06	0.674	1.00	1.30	0.877	No
3949	39.49	2.33	0.98	1.34	0.86	0.712	1.06	0.674	1.00	1.30	0.877	No
3950	39.50	2.33	0.98	1.34	0.86	0.712	1.06	0.674	1.00	1.30	0.876	No
3951	39.51	2.33	0.98	1.34	0.86	0.712	1.06	0.674	1.00	1.30	0.876	No
3952	39.52	2.33	0.98	1.35	0.86	0.712	1.06	0.674	1.00	1.30	0.876	No
3953	39.53	2.33	0.98	1.35	0.86	0.712	1.06	0.674	1.00	1.30	0.876	No
3954	39.54	2.33	0.98	1.35	0.86	0.712	1.06	0.674	1.00	1.30	0.876	No
3955	39.55	2.33	0.98	1.35	0.85	0.712	1.06	0.674	1.00	1.30	0.876	No
3956	39.56	2.33	0.98	1.35	0.85	0.712	1.06	0.674	1.00	1.30	0.876	No
3957	39.57	2.33	0.98	1.35	0.85	0.712	1.06	0.674	1.00	1.30	0.876	No
3958	39.58	2.33	0.99	1.35	0.85	0.712	1.06	0.674	1.00	1.30	0.876	No
3959	39.59	2.33	0.99	1.35	0.85	0.712	1.06	0.674	1.00	1.30	0.876	No
3960	39.60	2.33	0.99	1.35	0.85	0.712	1.06	0.674	1.00	1.30	0.876	No
3961	39.61	2.33	0.99	1.35	0.85	0.712	1.06	0.674	1.00	1.30	0.876	No
3962	39.62	2.34	0.99	1.35	0.85	0.712	1.06	0.674	1.00	1.30	0.876	No
3963	39.63	2.34	0.99	1.35	0.85	0.711	1.06	0.673	1.00	1.30	0.876	No
3964	39.64	2.34	0.99	1.35	0.85	0.711	1.06	0.673	1.00	1.30	0.875	No
3965	39.65	2.34	0.99	1.35	0.85	0.711	1.06	0.673	1.00	1.30	0.875	No
3966	39.66	2.34	0.99	1.35	0.85	0.711	1.06	0.673	1.00	1.30	0.875	No
3967	39.67	2.34	0.99	1.35	0.85	0.711	1.06	0.673	1.00	1.30	0.875	No
3968	39.68	2.34	0.99	1.35	0.85	0.711	1.06	0.673	1.00	1.30	0.875	No
3969	39.69	2.34	0.99	1.35	0.85	0.711	1.06	0.673	1.00	1.30	0.875	No
3970	39.70	2.34	0.99	1.35	0.85	0.711	1.06	0.673	1.00	1.30	0.875	No
3971	39.71	2.34	0.99	1.35	0.85	0.711	1.06	0.673	1.00	1.30	0.875	No
3972	39.72	2.34	0.99	1.35	0.85	0.711	1.06	0.673	1.00	1.30	0.875	No
3973	39.73	2.34	0.99	1.35	0.85	0.711	1.06	0.673	1.00	1.30	0.875	No
3974	39.74	2.34	0.99	1.35	0.85	0.711	1.06	0.673	1.00	1.30	0.875	No
3975	39.75	2.34	0.99	1.35	0.85	0.711	1.06	0.673	1.00	1.30	0.875	No
3976	39.76	2.34	0.99	1.35	0.85	0.711	1.06	0.673	1.00	1.30	0.875	No
3977	39.77	2.35	0.99	1.35	0.85	0.711	1.06	0.673	1.00	1.30	0.875	No
3978	39.78	2.35	0.99	1.35	0.85	0.711	1.06	0.673	1.00	1.30	0.874	No
3979	39.79	2.35	0.99	1.36	0.85	0.711	1.06	0.673	1.00	1.30	0.874	No
3980	39.80	2.35	0.99	1.36	0.85	0.710	1.06	0.673	1.00	1.30	0.874	No
3981	39.81	2.35	0.99	1.36	0.85	0.710	1.06	0.672	1.00	1.30	0.874	No
3982	39.82	2.35	0.99	1.36	0.85	0.710	1.06	0.672	1.00	1.30	0.874	No
3983	39.83	2.35	0.99	1.36	0.85	0.710	1.06	0.672	1.00	1.30	0.874	No
3984	39.84	2.35	0.99	1.36	0.85	0.710	1.06	0.672	1.00	1.30	0.874	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
3985	39.85	2.35	0.99	1.36	0.85	0.710	1.06	0.672	1.00	1.30	0.874	No
3986	39.86	2.35	0.99	1.36	0.85	0.710	1.06	0.672	1.00	1.30	0.874	No
3987	39.87	2.35	0.99	1.36	0.85	0.710	1.06	0.672	1.00	1.30	0.874	No
3988	39.88	2.35	0.99	1.36	0.85	0.710	1.06	0.672	1.00	1.30	0.874	No
3989	39.89	2.35	0.99	1.36	0.85	0.710	1.06	0.672	1.00	1.30	0.874	No
3990	39.90	2.35	1.00	1.36	0.85	0.710	1.06	0.672	1.00	1.30	0.874	No
3991	39.91	2.35	1.00	1.36	0.85	0.710	1.06	0.672	1.00	1.30	0.874	No
3992	39.92	2.36	1.00	1.36	0.85	0.710	1.06	0.672	1.00	1.30	0.873	No
3993	39.93	2.36	1.00	1.36	0.85	0.710	1.06	0.672	1.00	1.30	0.873	No
3994	39.94	2.36	1.00	1.36	0.85	0.710	1.06	0.672	1.00	1.30	0.873	No
3995	39.95	2.36	1.00	1.36	0.85	0.710	1.06	0.672	1.00	1.30	0.873	No
3996	39.96	2.36	1.00	1.36	0.85	0.710	1.06	0.672	1.00	1.30	0.873	No
3997	39.97	2.36	1.00	1.36	0.85	0.709	1.06	0.672	1.00	1.30	0.873	No
3998	39.98	2.36	1.00	1.36	0.85	0.709	1.06	0.672	1.00	1.30	0.873	No
3999	39.99	2.36	1.00	1.36	0.85	0.709	1.06	0.671	1.00	1.30	0.873	No
4000	40.00	2.36	1.00	1.36	0.85	0.709	1.06	0.671	1.00	1.30	0.873	No
4001	40.01	2.36	1.00	1.36	0.85	0.709	1.06	0.671	1.00	1.30	0.873	No
4002	40.02	2.36	1.00	1.36	0.85	0.709	1.06	0.671	1.00	1.30	0.873	No
4003	40.03	2.36	1.00	1.36	0.85	0.709	1.06	0.671	1.00	1.30	0.873	No
4004	40.04	2.36	1.00	1.36	0.85	0.709	1.06	0.671	1.00	1.30	0.873	No
4005	40.05	2.36	1.00	1.36	0.85	0.709	1.06	0.671	1.00	1.30	0.873	No
4006	40.06	2.37	1.00	1.36	0.85	0.709	1.06	0.671	1.00	1.30	0.872	No
4007	40.07	2.37	1.00	1.37	0.85	0.709	1.06	0.671	1.00	1.30	0.872	No
4008	40.08	2.37	1.00	1.37	0.85	0.709	1.06	0.671	1.00	1.30	0.872	No
4009	40.09	2.37	1.00	1.37	0.85	0.709	1.06	0.671	1.00	1.30	0.872	No
4010	40.10	2.37	1.00	1.37	0.85	0.709	1.06	0.671	1.00	1.30	0.872	No
4011	40.11	2.37	1.00	1.37	0.85	0.709	1.06	0.671	1.00	1.30	0.872	No
4012	40.12	2.37	1.00	1.37	0.85	0.709	1.06	0.671	1.00	1.30	0.872	No
4013	40.13	2.37	1.00	1.37	0.85	0.709	1.06	0.671	1.00	1.30	0.872	No
4014	40.14	2.37	1.00	1.37	0.85	0.708	1.06	0.671	1.00	1.30	0.872	No
4015	40.15	2.37	1.00	1.37	0.85	0.708	1.06	0.671	1.00	1.30	0.872	No
4016	40.16	2.37	1.00	1.37	0.85	0.708	1.06	0.671	1.00	1.30	0.872	No
4017	40.17	2.37	1.00	1.37	0.85	0.708	1.06	0.670	1.00	1.30	0.872	No
4018	40.18	2.37	1.00	1.37	0.85	0.708	1.06	0.670	1.00	1.30	0.872	No
4019	40.19	2.37	1.00	1.37	0.85	0.708	1.06	0.670	1.00	1.30	0.871	No
4020	40.20	2.37	1.00	1.37	0.85	0.708	1.06	0.670	1.00	1.30	0.871	No
4021	40.21	2.38	1.00	1.37	0.85	0.708	1.06	0.670	1.00	1.30	0.871	No
4022	40.22	2.38	1.01	1.37	0.85	0.708	1.06	0.670	1.00	1.30	0.871	No
4023	40.23	2.38	1.01	1.37	0.85	0.708	1.06	0.670	1.00	1.30	0.871	No
4024	40.24	2.38	1.01	1.37	0.85	0.708	1.06	0.670	1.00	1.30	0.871	No
4025	40.25	2.38	1.01	1.37	0.85	0.708	1.06	0.670	1.00	1.30	0.871	No
4026	40.26	2.38	1.01	1.37	0.85	0.708	1.06	0.670	1.00	1.30	0.871	No
4027	40.27	2.38	1.01	1.37	0.85	0.708	1.06	0.670	1.00	1.30	0.871	No
4028	40.28	2.38	1.01	1.37	0.85	0.708	1.06	0.670	1.00	1.30	0.871	No
4029	40.29	2.38	1.01	1.37	0.85	0.708	1.06	0.670	1.00	1.30	0.871	No
4030	40.30	2.38	1.01	1.37	0.85	0.707	1.06	0.670	1.00	1.30	0.871	No
4031	40.31	2.38	1.01	1.37	0.85	0.707	1.06	0.670	1.00	1.30	0.871	No
4032	40.32	2.38	1.01	1.37	0.85	0.707	1.06	0.670	1.00	1.30	0.871	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
4033	40.33	2.38	1.01	1.37	0.85	0.707	1.06	0.670	1.00	1.30	0.870	No
4034	40.34	2.38	1.01	1.37	0.85	0.707	1.06	0.670	1.00	1.30	0.870	No
4035	40.35	2.38	1.01	1.38	0.85	0.707	1.06	0.669	1.00	1.30	0.870	No
4036	40.36	2.39	1.01	1.38	0.85	0.707	1.06	0.669	1.00	1.30	0.870	No
4037	40.37	2.39	1.01	1.38	0.85	0.707	1.06	0.669	1.00	1.30	0.870	No
4038	40.38	2.39	1.01	1.38	0.85	0.707	1.06	0.669	1.00	1.30	0.870	No
4039	40.39	2.39	1.01	1.38	0.85	0.707	1.06	0.669	1.00	1.30	0.870	No
4040	40.40	2.39	1.01	1.38	0.85	0.707	1.06	0.669	1.00	1.30	0.870	No
4041	40.41	2.39	1.01	1.38	0.85	0.707	1.06	0.669	1.00	1.30	0.870	No
4042	40.42	2.39	1.01	1.38	0.85	0.707	1.06	0.669	1.00	1.30	0.870	No
4043	40.43	2.39	1.01	1.38	0.85	0.707	1.06	0.669	1.00	1.30	0.870	No
4044	40.44	2.39	1.01	1.38	0.85	0.707	1.06	0.669	1.00	1.30	0.870	No
4045	40.45	2.39	1.01	1.38	0.85	0.707	1.06	0.669	1.00	1.30	0.870	No
4046	40.46	2.39	1.01	1.38	0.85	0.707	1.06	0.669	1.00	1.30	0.869	No
4047	40.47	2.39	1.01	1.38	0.85	0.706	1.06	0.669	1.00	1.30	0.869	No
4048	40.48	2.39	1.01	1.38	0.85	0.706	1.06	0.669	1.00	1.30	0.869	No
4049	40.49	2.39	1.01	1.38	0.85	0.706	1.06	0.669	1.00	1.30	0.869	No
4050	40.50	2.39	1.01	1.38	0.85	0.706	1.06	0.669	1.00	1.30	0.869	No
4051	40.51	2.40	1.01	1.38	0.85	0.706	1.06	0.669	1.00	1.30	0.869	No
4052	40.52	2.40	1.01	1.38	0.85	0.706	1.06	0.668	1.00	1.30	0.869	No
4053	40.53	2.40	1.01	1.38	0.85	0.706	1.06	0.668	1.00	1.30	0.869	No
4054	40.54	2.40	1.02	1.38	0.85	0.706	1.06	0.668	1.00	1.30	0.869	No
4055	40.55	2.40	1.02	1.38	0.85	0.706	1.06	0.668	1.00	1.30	0.869	No
4056	40.56	2.40	1.02	1.38	0.85	0.706	1.06	0.668	1.00	1.30	0.869	No
4057	40.57	2.40	1.02	1.38	0.85	0.706	1.06	0.668	1.00	1.30	0.869	No
4058	40.58	2.40	1.02	1.38	0.85	0.706	1.06	0.668	1.00	1.30	0.869	No
4059	40.59	2.40	1.02	1.38	0.85	0.706	1.06	0.668	1.00	1.30	0.869	No
4060	40.60	2.40	1.02	1.38	0.85	0.706	1.06	0.668	1.00	1.30	0.868	No
4061	40.61	2.40	1.02	1.38	0.85	0.706	1.06	0.668	1.00	1.30	0.868	No
4062	40.62	2.40	1.02	1.38	0.85	0.706	1.06	0.668	1.00	1.30	0.868	No
4063	40.63	2.40	1.02	1.39	0.85	0.706	1.06	0.668	1.00	1.30	0.868	No
4064	40.64	2.40	1.02	1.39	0.85	0.705	1.06	0.668	1.00	1.30	0.868	No
4065	40.65	2.40	1.02	1.39	0.85	0.705	1.06	0.668	1.00	1.30	0.868	No
4066	40.66	2.41	1.02	1.39	0.85	0.705	1.06	0.668	1.00	1.30	0.868	No
4067	40.67	2.41	1.02	1.39	0.85	0.705	1.06	0.668	1.00	1.30	0.868	No
4068	40.68	2.41	1.02	1.39	0.84	0.705	1.06	0.668	1.00	1.30	0.868	No
4069	40.69	2.41	1.02	1.39	0.84	0.705	1.06	0.668	1.00	1.30	0.868	No
4070	40.70	2.41	1.02	1.39	0.84	0.705	1.06	0.667	1.00	1.30	0.868	No
4071	40.71	2.41	1.02	1.39	0.84	0.705	1.06	0.667	1.00	1.30	0.868	No
4072	40.72	2.41	1.02	1.39	0.84	0.705	1.06	0.667	1.00	1.30	0.868	No
4073	40.73	2.41	1.02	1.39	0.84	0.705	1.06	0.667	1.00	1.30	0.867	No
4074	40.74	2.41	1.02	1.39	0.84	0.705	1.06	0.667	1.00	1.30	0.867	No
4075	40.75	2.41	1.02	1.39	0.84	0.705	1.06	0.667	1.00	1.30	0.867	No
4076	40.76	2.41	1.02	1.39	0.84	0.705	1.06	0.667	1.00	1.30	0.867	No
4077	40.77	2.41	1.02	1.39	0.84	0.705	1.06	0.667	1.00	1.30	0.867	No
4078	40.78	2.41	1.02	1.39	0.84	0.705	1.06	0.667	1.00	1.30	0.867	No
4079	40.79	2.41	1.02	1.39	0.84	0.705	1.06	0.667	1.00	1.30	0.867	No
4080	40.80	2.41	1.02	1.39	0.84	0.704	1.06	0.667	1.00	1.30	0.867	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
4081	40.81	2.42	1.02	1.39	0.84	0.704	1.06	0.667	1.00	1.30	0.867	No
4082	40.82	2.42	1.02	1.39	0.84	0.704	1.06	0.667	1.00	1.30	0.867	No
4083	40.83	2.42	1.02	1.39	0.84	0.704	1.06	0.667	1.00	1.30	0.867	No
4084	40.84	2.42	1.02	1.39	0.84	0.704	1.06	0.667	1.00	1.30	0.867	No
4085	40.85	2.42	1.02	1.39	0.84	0.704	1.06	0.667	1.00	1.30	0.867	No
4086	40.86	2.42	1.03	1.39	0.84	0.704	1.06	0.667	1.00	1.30	0.867	No
4087	40.87	2.42	1.03	1.39	0.84	0.704	1.06	0.666	1.00	1.30	0.866	No
4088	40.88	2.42	1.03	1.39	0.84	0.704	1.06	0.666	1.00	1.30	0.866	No
4089	40.89	2.42	1.03	1.39	0.84	0.704	1.06	0.666	1.00	1.30	0.866	No
4090	40.90	2.42	1.03	1.39	0.84	0.704	1.06	0.666	1.00	1.30	0.866	No
4091	40.91	2.42	1.03	1.40	0.84	0.704	1.06	0.666	1.00	1.30	0.866	No
4092	40.92	2.42	1.03	1.40	0.84	0.704	1.06	0.666	1.00	1.30	0.866	No
4093	40.93	2.42	1.03	1.40	0.84	0.704	1.06	0.666	1.00	1.30	0.866	No
4094	40.94	2.42	1.03	1.40	0.84	0.704	1.06	0.666	1.00	1.30	0.866	No
4095	40.95	2.42	1.03	1.40	0.84	0.704	1.06	0.666	1.00	1.30	0.866	No
4096	40.96	2.43	1.03	1.40	0.84	0.704	1.06	0.666	1.00	1.30	0.866	No
4097	40.97	2.43	1.03	1.40	0.84	0.703	1.06	0.666	1.00	1.30	0.866	No
4098	40.98	2.43	1.03	1.40	0.84	0.703	1.06	0.666	1.00	1.30	0.866	No
4099	40.99	2.43	1.03	1.40	0.84	0.703	1.06	0.666	1.00	1.30	0.866	No
4100	41.00	2.43	1.03	1.40	0.84	0.703	1.06	0.666	1.00	1.30	0.865	No
4101	41.01	2.43	1.03	1.40	0.84	0.703	1.06	0.666	1.00	1.30	0.865	No
4102	41.02	2.43	1.03	1.40	0.84	0.703	1.06	0.666	1.00	1.30	2.000	Yes
4103	41.03	2.43	1.03	1.40	0.84	0.703	1.06	0.666	1.00	1.30	2.000	Yes
4104	41.04	2.43	1.03	1.40	0.84	0.703	1.06	0.666	1.00	1.30	2.000	Yes
4105	41.05	2.43	1.03	1.40	0.84	0.703	1.06	0.665	1.00	1.30	2.000	Yes
4106	41.06	2.43	1.03	1.40	0.84	0.703	1.06	0.665	1.00	1.30	2.000	Yes
4107	41.07	2.43	1.03	1.40	0.84	0.703	1.06	0.665	1.00	1.30	2.000	Yes
4108	41.08	2.43	1.03	1.40	0.84	0.703	1.06	0.665	1.00	1.30	2.000	Yes
4109	41.09	2.43	1.03	1.40	0.84	0.703	1.06	0.665	1.00	1.30	2.000	Yes
4110	41.10	2.43	1.03	1.40	0.84	0.703	1.06	0.665	1.00	1.30	2.000	Yes
4111	41.11	2.44	1.03	1.40	0.84	0.703	1.06	0.665	1.00	1.30	2.000	Yes
4112	41.12	2.44	1.03	1.40	0.84	0.703	1.06	0.665	1.00	1.30	2.000	Yes
4113	41.13	2.44	1.03	1.40	0.84	0.703	1.06	0.665	1.00	1.30	2.000	Yes
4114	41.14	2.44	1.03	1.40	0.84	0.702	1.06	0.665	1.00	1.30	2.000	Yes
4115	41.15	2.44	1.03	1.40	0.84	0.702	1.06	0.665	1.00	1.30	2.000	Yes
4116	41.16	2.44	1.03	1.40	0.84	0.702	1.06	0.665	1.00	1.30	2.000	Yes
4117	41.17	2.44	1.03	1.40	0.84	0.702	1.06	0.665	1.00	1.30	2.000	Yes
4118	41.18	2.44	1.04	1.40	0.84	0.702	1.06	0.665	1.00	1.30	2.000	Yes
4119	41.19	2.44	1.04	1.40	0.84	0.702	1.06	0.665	1.00	1.30	2.000	Yes
4120	41.20	2.44	1.04	1.40	0.84	0.702	1.06	0.665	1.00	1.30	2.000	Yes
4121	41.21	2.44	1.04	1.41	0.84	0.702	1.06	0.665	1.00	1.30	2.000	Yes
4122	41.22	2.44	1.04	1.41	0.84	0.702	1.06	0.665	1.00	1.30	2.000	Yes
4123	41.23	2.44	1.04	1.41	0.84	0.702	1.06	0.664	1.00	1.30	2.000	Yes
4124	41.24	2.44	1.04	1.41	0.84	0.702	1.06	0.664	1.00	1.30	2.000	Yes
4125	41.25	2.44	1.04	1.41	0.84	0.702	1.06	0.664	1.00	1.30	2.000	Yes
4126	41.26	2.44	1.04	1.41	0.84	0.702	1.06	0.664	1.00	1.30	2.000	Yes
4127	41.27	2.45	1.04	1.41	0.84	0.702	1.06	0.664	1.00	1.30	2.000	Yes
4128	41.28	2.45	1.04	1.41	0.84	0.702	1.06	0.664	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
4129	41.29	2.45	1.04	1.41	0.84	0.702	1.06	0.664	1.00	1.30	2.000	Yes
4130	41.30	2.45	1.04	1.41	0.84	0.702	1.06	0.664	1.00	1.30	2.000	Yes
4131	41.31	2.45	1.04	1.41	0.84	0.702	1.06	0.664	1.00	1.30	2.000	Yes
4132	41.32	2.45	1.04	1.41	0.84	0.701	1.06	0.664	1.00	1.30	2.000	Yes
4133	41.33	2.45	1.04	1.41	0.84	0.701	1.06	0.664	1.00	1.30	2.000	Yes
4134	41.34	2.45	1.04	1.41	0.84	0.701	1.06	0.664	1.00	1.30	2.000	Yes
4135	41.35	2.45	1.04	1.41	0.84	0.701	1.06	0.664	1.00	1.30	2.000	Yes
4136	41.36	2.45	1.04	1.41	0.84	0.701	1.06	0.664	1.00	1.30	2.000	Yes
4137	41.37	2.45	1.04	1.41	0.84	0.701	1.06	0.664	1.00	1.30	2.000	Yes
4138	41.38	2.45	1.04	1.41	0.84	0.701	1.06	0.664	1.00	1.30	2.000	Yes
4139	41.39	2.45	1.04	1.41	0.84	0.701	1.06	0.664	1.00	1.30	2.000	Yes
4140	41.40	2.45	1.04	1.41	0.84	0.701	1.06	0.664	1.00	1.30	2.000	Yes
4141	41.41	2.45	1.04	1.41	0.84	0.701	1.06	0.664	1.00	1.30	2.000	Yes
4142	41.42	2.45	1.04	1.41	0.84	0.701	1.06	0.663	1.00	1.30	2.000	Yes
4143	41.43	2.46	1.04	1.41	0.84	0.701	1.06	0.663	1.00	1.30	2.000	Yes
4144	41.44	2.46	1.04	1.41	0.84	0.701	1.06	0.663	1.00	1.30	2.000	Yes
4145	41.45	2.46	1.04	1.41	0.84	0.701	1.06	0.663	1.00	1.30	2.000	Yes
4146	41.46	2.46	1.04	1.41	0.84	0.701	1.06	0.663	1.00	1.30	2.000	Yes
4147	41.47	2.46	1.04	1.41	0.84	0.701	1.06	0.663	1.00	1.30	2.000	Yes
4148	41.48	2.46	1.04	1.41	0.84	0.701	1.06	0.663	1.00	1.30	2.000	Yes
4149	41.49	2.46	1.04	1.41	0.84	0.700	1.06	0.663	1.00	1.30	2.000	Yes
4150	41.50	2.46	1.05	1.41	0.84	0.700	1.06	0.663	1.00	1.30	2.000	Yes
4151	41.51	2.46	1.05	1.42	0.84	0.700	1.06	0.663	1.00	1.30	2.000	Yes
4152	41.52	2.46	1.05	1.42	0.84	0.700	1.06	0.663	1.00	1.30	2.000	Yes
4153	41.53	2.46	1.05	1.42	0.84	0.700	1.06	0.663	1.00	1.30	2.000	Yes
4154	41.54	2.46	1.05	1.42	0.84	0.700	1.06	0.663	1.00	1.30	2.000	Yes
4155	41.55	2.46	1.05	1.42	0.84	0.700	1.06	0.663	1.00	1.30	2.000	Yes
4156	41.56	2.46	1.05	1.42	0.84	0.700	1.06	0.663	1.00	1.30	2.000	Yes
4157	41.57	2.46	1.05	1.42	0.84	0.700	1.06	0.663	1.00	1.30	2.000	Yes
4158	41.58	2.46	1.05	1.42	0.84	0.700	1.06	0.663	1.00	1.30	2.000	Yes
4159	41.59	2.47	1.05	1.42	0.84	0.700	1.06	0.663	1.00	1.30	2.000	Yes
4160	41.60	2.47	1.05	1.42	0.84	0.700	1.06	0.663	1.00	1.30	2.000	Yes
4161	41.61	2.47	1.05	1.42	0.84	0.700	1.06	0.662	1.00	1.30	2.000	Yes
4162	41.62	2.47	1.05	1.42	0.84	0.700	1.06	0.662	1.00	1.30	2.000	Yes
4163	41.63	2.47	1.05	1.42	0.84	0.700	1.06	0.662	1.00	1.30	2.000	Yes
4164	41.64	2.47	1.05	1.42	0.84	0.700	1.06	0.662	1.00	1.30	2.000	Yes
4165	41.65	2.47	1.05	1.42	0.84	0.700	1.06	0.662	1.00	1.30	2.000	Yes
4166	41.66	2.47	1.05	1.42	0.84	0.700	1.06	0.662	1.00	1.30	2.000	Yes
4167	41.67	2.47	1.05	1.42	0.84	0.699	1.06	0.662	1.00	1.30	2.000	Yes
4168	41.68	2.47	1.05	1.42	0.84	0.699	1.06	0.662	1.00	1.30	2.000	Yes
4169	41.69	2.47	1.05	1.42	0.84	0.699	1.06	0.662	1.00	1.30	2.000	Yes
4170	41.70	2.47	1.05	1.42	0.84	0.699	1.06	0.662	1.00	1.30	2.000	Yes
4171	41.71	2.47	1.05	1.42	0.84	0.699	1.06	0.662	1.00	1.30	2.000	Yes
4172	41.72	2.47	1.05	1.42	0.84	0.699	1.06	0.662	1.00	1.30	2.000	Yes
4173	41.73	2.47	1.05	1.42	0.84	0.699	1.06	0.662	1.00	1.30	2.000	Yes
4174	41.74	2.48	1.05	1.42	0.84	0.699	1.06	0.662	1.00	1.30	2.000	Yes
4175	41.75	2.48	1.05	1.42	0.84	0.699	1.06	0.662	1.00	1.30	2.000	Yes
4176	41.76	2.48	1.05	1.42	0.84	0.699	1.06	0.662	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
4177	41.77	2.48	1.05	1.42	0.83	0.699	1.06	0.662	1.00	1.30	2.000	Yes
4178	41.78	2.48	1.05	1.42	0.83	0.699	1.06	0.662	1.00	1.30	2.000	Yes
4179	41.79	2.48	1.05	1.42	0.83	0.699	1.06	0.662	1.00	1.30	2.000	Yes
4180	41.80	2.48	1.05	1.42	0.83	0.699	1.06	0.661	1.00	1.30	2.000	Yes
4181	41.81	2.48	1.05	1.42	0.83	0.699	1.06	0.661	1.00	1.30	2.000	Yes
4182	41.82	2.48	1.06	1.42	0.83	0.699	1.06	0.661	1.00	1.30	2.000	Yes
4183	41.83	2.48	1.06	1.43	0.83	0.699	1.06	0.661	1.00	1.30	2.000	Yes
4184	41.84	2.48	1.06	1.43	0.83	0.699	1.06	0.661	1.00	1.30	2.000	Yes
4185	41.85	2.48	1.06	1.43	0.83	0.698	1.06	0.661	1.00	1.30	2.000	Yes
4186	41.86	2.48	1.06	1.43	0.83	0.698	1.06	0.661	1.00	1.30	2.000	Yes
4187	41.87	2.48	1.06	1.43	0.83	0.698	1.06	0.661	1.00	1.30	2.000	Yes
4188	41.88	2.48	1.06	1.43	0.83	0.698	1.06	0.661	1.00	1.30	2.000	Yes
4189	41.89	2.48	1.06	1.43	0.83	0.698	1.06	0.661	1.00	1.30	2.000	Yes
4190	41.90	2.49	1.06	1.43	0.83	0.698	1.06	0.661	1.00	1.30	2.000	Yes
4191	41.91	2.49	1.06	1.43	0.83	0.698	1.06	0.661	1.00	1.30	2.000	Yes
4192	41.92	2.49	1.06	1.43	0.83	0.698	1.06	0.661	1.00	1.30	2.000	Yes
4193	41.93	2.49	1.06	1.43	0.83	0.698	1.06	0.661	1.00	1.30	2.000	Yes
4194	41.94	2.49	1.06	1.43	0.83	0.698	1.06	0.661	1.00	1.30	2.000	Yes
4195	41.95	2.49	1.06	1.43	0.83	0.698	1.06	0.661	1.00	1.30	2.000	Yes
4196	41.96	2.49	1.06	1.43	0.83	0.698	1.06	0.661	1.00	1.30	0.859	No
4197	41.97	2.49	1.06	1.43	0.83	0.698	1.06	0.661	1.00	1.30	0.859	No
4198	41.98	2.49	1.06	1.43	0.83	0.698	1.06	0.660	1.00	1.30	0.859	No
4199	41.99	2.49	1.06	1.43	0.83	0.698	1.06	0.660	1.00	1.30	0.859	No
4200	42.00	2.49	1.06	1.43	0.83	0.698	1.06	0.660	1.00	1.30	0.858	No
4201	42.01	2.49	1.06	1.43	0.83	0.698	1.06	0.660	1.00	1.30	0.858	No
4202	42.02	2.49	1.06	1.43	0.83	0.697	1.06	0.660	1.00	1.30	0.858	No
4203	42.03	2.49	1.06	1.43	0.83	0.697	1.06	0.660	1.00	1.30	0.858	No
4204	42.04	2.49	1.06	1.43	0.83	0.697	1.06	0.660	1.00	1.30	0.858	No
4205	42.05	2.49	1.06	1.43	0.83	0.697	1.06	0.660	1.00	1.30	0.858	No
4206	42.06	2.50	1.06	1.43	0.83	0.697	1.06	0.660	1.00	1.30	0.858	No
4207	42.07	2.50	1.06	1.43	0.83	0.697	1.06	0.660	1.00	1.30	0.858	No
4208	42.08	2.50	1.06	1.43	0.83	0.697	1.06	0.660	1.00	1.30	0.858	No
4209	42.09	2.50	1.06	1.43	0.83	0.697	1.06	0.660	1.00	1.30	0.858	No
4210	42.10	2.50	1.06	1.43	0.83	0.697	1.06	0.660	1.00	1.30	0.858	No
4211	42.11	2.50	1.06	1.43	0.83	0.697	1.06	0.660	1.00	1.30	0.858	No
4212	42.12	2.50	1.06	1.43	0.83	0.697	1.06	0.660	1.00	1.30	0.858	No
4213	42.13	2.50	1.06	1.43	0.83	0.697	1.06	0.660	1.00	1.30	0.858	No
4214	42.14	2.50	1.07	1.44	0.83	0.697	1.06	0.660	1.00	1.30	0.857	No
4215	42.15	2.50	1.07	1.44	0.83	0.697	1.06	0.660	1.00	1.30	0.857	No
4216	42.16	2.50	1.07	1.44	0.83	0.697	1.06	0.659	1.00	1.30	0.857	No
4217	42.17	2.50	1.07	1.44	0.83	0.697	1.06	0.659	1.00	1.30	0.857	No
4218	42.18	2.50	1.07	1.44	0.83	0.697	1.06	0.659	1.00	1.30	0.857	No
4219	42.19	2.50	1.07	1.44	0.83	0.696	1.06	0.659	1.00	1.30	0.857	No
4220	42.20	2.50	1.07	1.44	0.83	0.696	1.06	0.659	1.00	1.30	0.857	No
4221	42.21	2.50	1.07	1.44	0.83	0.696	1.06	0.659	1.00	1.30	0.857	No
4222	42.22	2.51	1.07	1.44	0.83	0.696	1.06	0.659	1.00	1.30	0.857	No
4223	42.23	2.51	1.07	1.44	0.83	0.696	1.06	0.659	1.00	1.30	0.857	No
4224	42.24	2.51	1.07	1.44	0.83	0.696	1.06	0.659	1.00	1.30	0.857	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
4225	42.25	2.51	1.07	1.44	0.83	0.696	1.06	0.659	1.00	1.30	0.857	No
4226	42.26	2.51	1.07	1.44	0.83	0.696	1.06	0.659	1.00	1.30	0.857	No
4227	42.27	2.51	1.07	1.44	0.83	0.696	1.06	0.659	1.00	1.30	0.857	No
4228	42.28	2.51	1.07	1.44	0.83	0.696	1.06	0.659	1.00	1.30	0.856	No
4229	42.29	2.51	1.07	1.44	0.83	0.696	1.06	0.659	1.00	1.30	0.856	No
4230	42.30	2.51	1.07	1.44	0.83	0.696	1.06	0.659	1.00	1.30	0.856	No
4231	42.31	2.51	1.07	1.44	0.83	0.696	1.06	0.659	1.00	1.30	0.856	No
4232	42.32	2.51	1.07	1.44	0.83	0.696	1.06	0.659	1.00	1.30	0.856	No
4233	42.33	2.51	1.07	1.44	0.83	0.696	1.06	0.659	1.00	1.30	0.856	No
4234	42.34	2.51	1.07	1.44	0.83	0.696	1.06	0.658	1.00	1.30	0.856	No
4235	42.35	2.51	1.07	1.44	0.83	0.696	1.06	0.658	1.00	1.30	0.856	No
4236	42.36	2.51	1.07	1.44	0.83	0.695	1.06	0.658	1.00	1.30	0.856	No
4237	42.37	2.52	1.07	1.44	0.83	0.695	1.06	0.658	1.00	1.30	0.856	No
4238	42.38	2.52	1.07	1.44	0.83	0.695	1.06	0.658	1.00	1.30	0.856	No
4239	42.39	2.52	1.07	1.44	0.83	0.695	1.06	0.658	1.00	1.30	0.856	No
4240	42.40	2.52	1.07	1.44	0.83	0.695	1.06	0.658	1.00	1.30	0.856	No
4241	42.41	2.52	1.07	1.44	0.83	0.695	1.06	0.658	1.00	1.30	0.855	No
4242	42.42	2.52	1.07	1.44	0.83	0.695	1.06	0.658	1.00	1.30	0.855	No
4243	42.43	2.52	1.07	1.44	0.83	0.695	1.06	0.658	1.00	1.30	0.855	No
4244	42.44	2.52	1.07	1.44	0.83	0.695	1.06	0.658	1.00	1.30	0.855	No
4245	42.45	2.52	1.07	1.45	0.83	0.695	1.06	0.658	1.00	1.30	0.855	No
4246	42.46	2.52	1.08	1.45	0.83	0.695	1.06	0.658	1.00	1.30	0.855	No
4247	42.47	2.52	1.08	1.45	0.83	0.695	1.06	0.658	1.00	1.30	0.855	No
4248	42.48	2.52	1.08	1.45	0.83	0.695	1.06	0.658	1.00	1.30	0.855	No
4249	42.49	2.52	1.08	1.45	0.83	0.695	1.06	0.658	1.00	1.30	0.855	No
4250	42.50	2.52	1.08	1.45	0.83	0.695	1.06	0.658	1.00	1.30	0.855	No
4251	42.51	2.52	1.08	1.45	0.83	0.695	1.06	0.658	1.00	1.30	0.855	No
4252	42.52	2.52	1.08	1.45	0.83	0.695	1.06	0.657	1.00	1.30	0.855	No
4253	42.53	2.53	1.08	1.45	0.83	0.694	1.06	0.657	1.00	1.30	0.855	No
4254	42.54	2.53	1.08	1.45	0.83	0.694	1.06	0.657	1.00	1.30	0.855	No
4255	42.55	2.53	1.08	1.45	0.83	0.694	1.06	0.657	1.00	1.30	0.854	No
4256	42.56	2.53	1.08	1.45	0.83	0.694	1.06	0.657	1.00	1.30	0.854	No
4257	42.57	2.53	1.08	1.45	0.83	0.694	1.06	0.657	1.00	1.30	0.854	No
4258	42.58	2.53	1.08	1.45	0.83	0.694	1.06	0.657	1.00	1.30	0.854	No
4259	42.59	2.53	1.08	1.45	0.83	0.694	1.06	0.657	1.00	1.30	0.854	No
4260	42.60	2.53	1.08	1.45	0.83	0.694	1.06	0.657	1.00	1.30	0.854	No
4261	42.61	2.53	1.08	1.45	0.83	0.694	1.06	0.657	1.00	1.30	0.854	No
4262	42.62	2.53	1.08	1.45	0.83	0.694	1.06	0.657	1.00	1.30	0.854	No
4263	42.63	2.53	1.08	1.45	0.83	0.694	1.06	0.657	1.00	1.30	0.854	No
4264	42.64	2.53	1.08	1.45	0.83	0.694	1.06	0.657	1.00	1.30	0.854	No
4265	42.65	2.53	1.08	1.45	0.83	0.694	1.06	0.657	1.00	1.30	0.854	No
4266	42.66	2.53	1.08	1.45	0.83	0.694	1.06	0.657	1.00	1.30	0.854	No
4267	42.67	2.53	1.08	1.45	0.83	0.694	1.06	0.657	1.00	1.30	0.854	No
4268	42.68	2.53	1.08	1.45	0.83	0.694	1.06	0.657	1.00	1.30	0.854	No
4269	42.69	2.54	1.08	1.45	0.83	0.694	1.06	0.657	1.00	1.30	0.853	No
4270	42.70	2.54	1.08	1.45	0.83	0.693	1.06	0.656	1.00	1.30	0.853	No
4271	42.71	2.54	1.08	1.45	0.83	0.693	1.06	0.656	1.00	1.30	0.853	No
4272	42.72	2.54	1.08	1.45	0.83	0.693	1.06	0.656	1.00	1.30	0.853	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
4273	42.73	2.54	1.08	1.45	0.83	0.693	1.06	0.656	1.00	1.30	0.853	No
4274	42.74	2.54	1.08	1.45	0.83	0.693	1.06	0.656	1.00	1.30	0.853	No
4275	42.75	2.54	1.08	1.45	0.83	0.693	1.06	0.656	1.00	1.30	0.853	No
4276	42.76	2.54	1.08	1.46	0.83	0.693	1.06	0.656	1.00	1.30	0.853	No
4277	42.77	2.54	1.08	1.46	0.83	0.693	1.06	0.656	1.00	1.30	0.853	No
4278	42.78	2.54	1.09	1.46	0.83	0.693	1.06	0.656	1.00	1.30	0.853	No
4279	42.79	2.54	1.09	1.46	0.83	0.693	1.06	0.656	1.00	1.30	0.853	No
4280	42.80	2.54	1.09	1.46	0.83	0.693	1.06	0.656	1.00	1.30	0.853	No
4281	42.81	2.54	1.09	1.46	0.83	0.693	1.06	0.656	1.00	1.30	0.853	No
4282	42.82	2.54	1.09	1.46	0.83	0.693	1.06	0.656	1.00	1.30	0.853	No
4283	42.83	2.54	1.09	1.46	0.82	0.693	1.06	0.656	1.00	1.30	0.852	No
4284	42.84	2.54	1.09	1.46	0.82	0.693	1.06	0.656	1.00	1.30	0.852	No
4285	42.85	2.55	1.09	1.46	0.82	0.693	1.06	0.656	1.00	1.30	0.852	No
4286	42.86	2.55	1.09	1.46	0.82	0.693	1.06	0.656	1.00	1.30	0.852	No
4287	42.87	2.55	1.09	1.46	0.82	0.692	1.06	0.656	1.00	1.30	0.852	No
4288	42.88	2.55	1.09	1.46	0.82	0.692	1.06	0.655	1.00	1.30	0.852	No
4289	42.89	2.55	1.09	1.46	0.82	0.692	1.06	0.655	1.00	1.30	0.852	No
4290	42.90	2.55	1.09	1.46	0.82	0.692	1.06	0.655	1.00	1.30	0.852	No
4291	42.91	2.55	1.09	1.46	0.82	0.692	1.06	0.655	1.00	1.30	0.852	No
4292	42.92	2.55	1.09	1.46	0.82	0.692	1.06	0.655	1.00	1.30	0.852	No
4293	42.93	2.55	1.09	1.46	0.82	0.692	1.06	0.655	1.00	1.30	0.852	No
4294	42.94	2.55	1.09	1.46	0.82	0.692	1.06	0.655	1.00	1.30	0.852	No
4295	42.95	2.55	1.09	1.46	0.82	0.692	1.06	0.655	1.00	1.30	0.852	No
4296	42.96	2.55	1.09	1.46	0.82	0.692	1.06	0.655	1.00	1.30	0.852	No
4297	42.97	2.55	1.09	1.46	0.82	0.692	1.06	0.655	1.00	1.30	0.851	No
4298	42.98	2.55	1.09	1.46	0.82	0.692	1.06	0.655	1.00	1.30	0.851	No
4299	42.99	2.55	1.09	1.46	0.82	0.692	1.06	0.655	1.00	1.30	0.851	No
4300	43.00	2.55	1.09	1.46	0.82	0.692	1.06	0.655	1.00	1.30	0.851	No
4301	43.01	2.56	1.09	1.46	0.82	0.692	1.06	0.655	1.00	1.30	0.851	No
4302	43.02	2.56	1.09	1.46	0.82	0.692	1.06	0.655	1.00	1.30	0.851	No
4303	43.03	2.56	1.09	1.46	0.82	0.692	1.06	0.655	1.00	1.30	0.851	No
4304	43.04	2.56	1.09	1.46	0.82	0.691	1.06	0.655	1.00	1.30	0.851	No
4305	43.05	2.56	1.09	1.46	0.82	0.691	1.06	0.655	1.00	1.30	0.851	No
4306	43.06	2.56	1.09	1.46	0.82	0.691	1.06	0.654	1.00	1.30	0.851	No
4307	43.07	2.56	1.09	1.46	0.82	0.691	1.06	0.654	1.00	1.30	0.851	No
4308	43.08	2.56	1.09	1.46	0.82	0.691	1.06	0.654	1.00	1.30	0.851	No
4309	43.09	2.56	1.09	1.47	0.82	0.691	1.06	0.654	1.00	1.30	0.851	No
4310	43.10	2.56	1.10	1.47	0.82	0.691	1.06	0.654	1.00	1.30	0.850	No
4311	43.11	2.56	1.10	1.47	0.82	0.691	1.06	0.654	1.00	1.30	0.850	No
4312	43.12	2.56	1.10	1.47	0.82	0.691	1.06	0.654	1.00	1.30	0.850	No
4313	43.13	2.56	1.10	1.47	0.82	0.691	1.06	0.654	1.00	1.30	0.850	No
4314	43.14	2.56	1.10	1.47	0.82	0.691	1.06	0.654	1.00	1.30	0.850	No
4315	43.15	2.56	1.10	1.47	0.82	0.691	1.06	0.654	1.00	1.30	0.850	No
4316	43.16	2.56	1.10	1.47	0.82	0.691	1.06	0.654	1.00	1.30	0.850	No
4317	43.17	2.57	1.10	1.47	0.82	0.691	1.06	0.654	1.00	1.30	0.850	No
4318	43.18	2.57	1.10	1.47	0.82	0.691	1.06	0.654	1.00	1.30	0.850	No
4319	43.19	2.57	1.10	1.47	0.82	0.691	1.06	0.654	1.00	1.30	0.850	No
4320	43.20	2.57	1.10	1.47	0.82	0.690	1.06	0.654	1.00	1.30	0.850	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
4321	43.21	2.57	1.10	1.47	0.82	0.690	1.06	0.654	1.00	1.30	0.850	No
4322	43.22	2.57	1.10	1.47	0.82	0.690	1.06	0.654	1.00	1.30	0.850	No
4323	43.23	2.57	1.10	1.47	0.82	0.690	1.06	0.653	1.00	1.30	0.849	No
4324	43.24	2.57	1.10	1.47	0.82	0.690	1.06	0.653	1.00	1.30	0.849	No
4325	43.25	2.57	1.10	1.47	0.82	0.690	1.06	0.653	1.00	1.30	0.849	No
4326	43.26	2.57	1.10	1.47	0.82	0.690	1.06	0.653	1.00	1.30	0.849	No
4327	43.27	2.57	1.10	1.47	0.82	0.690	1.06	0.653	1.00	1.30	0.849	No
4328	43.28	2.57	1.10	1.47	0.82	0.690	1.06	0.653	1.00	1.30	0.849	No
4329	43.29	2.57	1.10	1.47	0.82	0.690	1.06	0.653	1.00	1.30	0.849	No
4330	43.30	2.57	1.10	1.47	0.82	0.690	1.06	0.653	1.00	1.30	0.849	No
4331	43.31	2.57	1.10	1.47	0.82	0.690	1.06	0.653	1.00	1.30	0.849	No
4332	43.32	2.57	1.10	1.47	0.82	0.690	1.06	0.653	1.00	1.30	0.849	No
4333	43.33	2.58	1.10	1.47	0.82	0.690	1.06	0.653	1.00	1.30	0.849	No
4334	43.34	2.58	1.10	1.47	0.82	0.690	1.06	0.653	1.00	1.30	2.000	Yes
4335	43.35	2.58	1.10	1.47	0.82	0.690	1.06	0.653	1.00	1.30	2.000	Yes
4336	43.36	2.58	1.10	1.47	0.82	0.689	1.06	0.653	1.00	1.30	2.000	Yes
4337	43.37	2.58	1.10	1.47	0.82	0.689	1.06	0.653	1.00	1.30	2.000	Yes
4338	43.38	2.58	1.10	1.47	0.82	0.689	1.06	0.653	1.00	1.30	2.000	Yes
4339	43.39	2.58	1.10	1.47	0.82	0.689	1.06	0.653	1.00	1.30	2.000	Yes
4340	43.40	2.58	1.10	1.48	0.82	0.689	1.06	0.652	1.00	1.30	2.000	Yes
4341	43.41	2.58	1.10	1.48	0.82	0.689	1.06	0.652	1.00	1.30	2.000	Yes
4342	43.42	2.58	1.11	1.48	0.82	0.689	1.06	0.652	1.00	1.30	2.000	Yes
4343	43.43	2.58	1.11	1.48	0.82	0.689	1.06	0.652	1.00	1.30	2.000	Yes
4344	43.44	2.58	1.11	1.48	0.82	0.689	1.06	0.652	1.00	1.30	2.000	Yes
4345	43.45	2.58	1.11	1.48	0.82	0.689	1.06	0.652	1.00	1.30	2.000	Yes
4346	43.46	2.58	1.11	1.48	0.82	0.689	1.06	0.652	1.00	1.30	2.000	Yes
4347	43.47	2.58	1.11	1.48	0.82	0.689	1.06	0.652	1.00	1.30	2.000	Yes
4348	43.48	2.58	1.11	1.48	0.82	0.689	1.06	0.652	1.00	1.30	2.000	Yes
4349	43.49	2.59	1.11	1.48	0.82	0.689	1.06	0.652	1.00	1.30	2.000	Yes
4350	43.50	2.59	1.11	1.48	0.82	0.689	1.06	0.652	1.00	1.30	2.000	Yes
4351	43.51	2.59	1.11	1.48	0.82	0.689	1.06	0.652	1.00	1.30	2.000	Yes
4352	43.52	2.59	1.11	1.48	0.82	0.688	1.06	0.652	1.00	1.30	2.000	Yes
4353	43.53	2.59	1.11	1.48	0.82	0.688	1.06	0.652	1.00	1.30	2.000	Yes
4354	43.54	2.59	1.11	1.48	0.82	0.688	1.06	0.652	1.00	1.30	2.000	Yes
4355	43.55	2.59	1.11	1.48	0.82	0.688	1.06	0.652	1.00	1.30	2.000	Yes
4356	43.56	2.59	1.11	1.48	0.82	0.688	1.06	0.651	1.00	1.30	2.000	Yes
4357	43.57	2.59	1.11	1.48	0.82	0.688	1.06	0.651	1.00	1.30	2.000	Yes
4358	43.58	2.59	1.11	1.48	0.82	0.688	1.06	0.651	1.00	1.30	2.000	Yes
4359	43.59	2.59	1.11	1.48	0.82	0.688	1.06	0.651	1.00	1.30	2.000	Yes
4360	43.60	2.59	1.11	1.48	0.82	0.688	1.06	0.651	1.00	1.30	2.000	Yes
4361	43.61	2.59	1.11	1.48	0.82	0.688	1.06	0.651	1.00	1.30	0.847	No
4362	43.62	2.59	1.11	1.48	0.82	0.688	1.06	0.651	1.00	1.30	0.846	No
4363	43.63	2.59	1.11	1.48	0.82	0.688	1.06	0.651	1.00	1.30	0.846	No
4364	43.64	2.59	1.11	1.48	0.82	0.688	1.06	0.651	1.00	1.30	0.846	No
4365	43.65	2.60	1.11	1.48	0.82	0.688	1.06	0.651	1.00	1.30	0.846	No
4366	43.66	2.60	1.11	1.48	0.82	0.688	1.06	0.651	1.00	1.30	0.846	No
4367	43.67	2.60	1.11	1.48	0.82	0.688	1.06	0.651	1.00	1.30	0.846	No
4368	43.68	2.60	1.11	1.48	0.82	0.687	1.06	0.651	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
4369	43.69	2.60	1.11	1.48	0.82	0.687	1.06	0.651	1.00	1.30	2.000	Yes
4370	43.70	2.60	1.11	1.48	0.82	0.687	1.06	0.651	1.00	1.30	2.000	Yes
4371	43.71	2.60	1.11	1.49	0.82	0.687	1.06	0.651	1.00	1.30	2.000	Yes
4372	43.72	2.60	1.11	1.49	0.82	0.687	1.06	0.651	1.00	1.30	2.000	Yes
4373	43.73	2.60	1.11	1.49	0.82	0.687	1.06	0.650	1.00	1.30	2.000	Yes
4374	43.74	2.60	1.12	1.49	0.82	0.687	1.06	0.650	1.00	1.30	2.000	Yes
4375	43.75	2.60	1.12	1.49	0.82	0.687	1.06	0.650	1.00	1.30	2.000	Yes
4376	43.76	2.60	1.12	1.49	0.82	0.687	1.06	0.650	1.00	1.30	2.000	Yes
4377	43.77	2.60	1.12	1.49	0.82	0.687	1.06	0.650	1.00	1.30	2.000	Yes
4378	43.78	2.60	1.12	1.49	0.82	0.687	1.06	0.650	1.00	1.30	2.000	Yes
4379	43.79	2.60	1.12	1.49	0.82	0.687	1.06	0.650	1.00	1.30	2.000	Yes
4380	43.80	2.61	1.12	1.49	0.82	0.687	1.06	0.650	1.00	1.30	2.000	Yes
4381	43.81	2.61	1.12	1.49	0.82	0.687	1.06	0.650	1.00	1.30	2.000	Yes
4382	43.82	2.61	1.12	1.49	0.82	0.687	1.06	0.650	1.00	1.30	2.000	Yes
4383	43.83	2.61	1.12	1.49	0.82	0.687	1.06	0.650	1.00	1.30	2.000	Yes
4384	43.84	2.61	1.12	1.49	0.82	0.686	1.06	0.650	1.00	1.30	2.000	Yes
4385	43.85	2.61	1.12	1.49	0.82	0.686	1.06	0.650	1.00	1.30	2.000	Yes
4386	43.86	2.61	1.12	1.49	0.81	0.686	1.06	0.650	1.00	1.30	2.000	Yes
4387	43.87	2.61	1.12	1.49	0.81	0.686	1.06	0.650	1.00	1.30	2.000	Yes
4388	43.88	2.61	1.12	1.49	0.81	0.686	1.06	0.650	1.00	1.30	2.000	Yes
4389	43.89	2.61	1.12	1.49	0.81	0.686	1.06	0.650	1.00	1.30	2.000	Yes
4390	43.90	2.61	1.12	1.49	0.81	0.686	1.06	0.649	1.00	1.30	2.000	Yes
4391	43.91	2.61	1.12	1.49	0.81	0.686	1.06	0.649	1.00	1.30	2.000	Yes
4392	43.92	2.61	1.12	1.49	0.81	0.686	1.06	0.649	1.00	1.30	2.000	Yes
4393	43.93	2.61	1.12	1.49	0.81	0.686	1.06	0.649	1.00	1.30	2.000	Yes
4394	43.94	2.61	1.12	1.49	0.81	0.686	1.06	0.649	1.00	1.30	2.000	Yes
4395	43.95	2.61	1.12	1.49	0.81	0.686	1.06	0.649	1.00	1.30	2.000	Yes
4396	43.96	2.62	1.12	1.49	0.81	0.686	1.06	0.649	1.00	1.30	2.000	Yes
4397	43.97	2.62	1.12	1.49	0.81	0.686	1.06	0.649	1.00	1.30	2.000	Yes
4398	43.98	2.62	1.12	1.49	0.81	0.686	1.06	0.649	1.00	1.30	2.000	Yes
4399	43.99	2.62	1.12	1.49	0.81	0.685	1.06	0.649	1.00	1.30	2.000	Yes
4400	44.00	2.62	1.12	1.49	0.81	0.685	1.06	0.649	1.00	1.30	2.000	Yes
4401	44.01	2.62	1.12	1.49	0.81	0.685	1.06	0.649	1.00	1.30	2.000	Yes
4402	44.02	2.62	1.12	1.50	0.81	0.685	1.06	0.649	1.00	1.30	2.000	Yes
4403	44.03	2.62	1.12	1.50	0.81	0.685	1.06	0.649	1.00	1.30	2.000	Yes
4404	44.04	2.62	1.12	1.50	0.81	0.685	1.06	0.649	1.00	1.30	2.000	Yes
4405	44.05	2.62	1.12	1.50	0.81	0.685	1.06	0.649	1.00	1.30	0.843	No
4406	44.06	2.62	1.13	1.50	0.81	0.685	1.06	0.648	1.00	1.30	0.843	No
4407	44.07	2.62	1.13	1.50	0.81	0.685	1.06	0.648	1.00	1.30	0.843	No
4408	44.08	2.62	1.13	1.50	0.81	0.685	1.06	0.648	1.00	1.30	0.843	No
4409	44.09	2.62	1.13	1.50	0.81	0.685	1.06	0.648	1.00	1.30	0.843	No
4410	44.10	2.62	1.13	1.50	0.81	0.685	1.06	0.648	1.00	1.30	0.843	No
4411	44.11	2.62	1.13	1.50	0.81	0.685	1.06	0.648	1.00	1.30	0.843	No
4412	44.12	2.63	1.13	1.50	0.81	0.685	1.06	0.648	1.00	1.30	0.843	No
4413	44.13	2.63	1.13	1.50	0.81	0.685	1.06	0.648	1.00	1.30	2.000	Yes
4414	44.14	2.63	1.13	1.50	0.81	0.684	1.06	0.648	1.00	1.30	2.000	Yes
4415	44.15	2.63	1.13	1.50	0.81	0.684	1.06	0.648	1.00	1.30	2.000	Yes
4416	44.16	2.63	1.13	1.50	0.81	0.684	1.06	0.648	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
4417	44.17	2.63	1.13	1.50	0.81	0.684	1.06	0.648	1.00	1.30	2.000	Yes
4418	44.18	2.63	1.13	1.50	0.81	0.684	1.06	0.648	1.00	1.30	2.000	Yes
4419	44.19	2.63	1.13	1.50	0.81	0.684	1.06	0.648	1.00	1.30	2.000	Yes
4420	44.20	2.63	1.13	1.50	0.81	0.684	1.06	0.648	1.00	1.30	2.000	Yes
4421	44.21	2.63	1.13	1.50	0.81	0.684	1.06	0.648	1.00	1.30	2.000	Yes
4422	44.22	2.63	1.13	1.50	0.81	0.684	1.06	0.647	1.00	1.30	2.000	Yes
4423	44.23	2.63	1.13	1.50	0.81	0.684	1.06	0.647	1.00	1.30	2.000	Yes
4424	44.24	2.63	1.13	1.50	0.81	0.684	1.06	0.647	1.00	1.30	2.000	Yes
4425	44.25	2.63	1.13	1.50	0.81	0.684	1.06	0.647	1.00	1.30	2.000	Yes
4426	44.26	2.63	1.13	1.50	0.81	0.684	1.06	0.647	1.00	1.30	2.000	Yes
4427	44.27	2.64	1.13	1.50	0.81	0.684	1.06	0.647	1.00	1.30	2.000	Yes
4428	44.28	2.64	1.13	1.50	0.81	0.684	1.06	0.647	1.00	1.30	2.000	Yes
4429	44.29	2.64	1.13	1.50	0.81	0.683	1.06	0.647	1.00	1.30	2.000	Yes
4430	44.30	2.64	1.13	1.50	0.81	0.683	1.06	0.647	1.00	1.30	2.000	Yes
4431	44.31	2.64	1.13	1.50	0.81	0.683	1.06	0.647	1.00	1.30	2.000	Yes
4432	44.32	2.64	1.13	1.51	0.81	0.683	1.06	0.647	1.00	1.30	2.000	Yes
4433	44.33	2.64	1.13	1.51	0.81	0.683	1.06	0.647	1.00	1.30	2.000	Yes
4434	44.34	2.64	1.13	1.51	0.81	0.683	1.06	0.647	1.00	1.30	2.000	Yes
4435	44.35	2.64	1.13	1.51	0.81	0.683	1.06	0.647	1.00	1.30	2.000	Yes
4436	44.36	2.64	1.13	1.51	0.81	0.683	1.06	0.647	1.00	1.30	2.000	Yes
4437	44.37	2.64	1.13	1.51	0.81	0.683	1.06	0.646	1.00	1.30	2.000	Yes
4438	44.38	2.64	1.14	1.51	0.81	0.683	1.06	0.646	1.00	1.30	2.000	Yes
4439	44.39	2.64	1.14	1.51	0.81	0.683	1.06	0.646	1.00	1.30	2.000	Yes
4440	44.40	2.64	1.14	1.51	0.81	0.683	1.06	0.646	1.00	1.30	2.000	Yes
4441	44.41	2.64	1.14	1.51	0.81	0.683	1.06	0.646	1.00	1.30	2.000	Yes
4442	44.42	2.64	1.14	1.51	0.81	0.683	1.06	0.646	1.00	1.30	2.000	Yes
4443	44.43	2.65	1.14	1.51	0.81	0.683	1.06	0.646	1.00	1.30	2.000	Yes
4444	44.44	2.65	1.14	1.51	0.81	0.682	1.06	0.646	1.00	1.30	2.000	Yes
4445	44.45	2.65	1.14	1.51	0.81	0.682	1.06	0.646	1.00	1.30	2.000	Yes
4446	44.46	2.65	1.14	1.51	0.81	0.682	1.06	0.646	1.00	1.30	2.000	Yes
4447	44.47	2.65	1.14	1.51	0.81	0.682	1.06	0.646	1.00	1.30	2.000	Yes
4448	44.48	2.65	1.14	1.51	0.81	0.682	1.06	0.646	1.00	1.30	2.000	Yes
4449	44.49	2.65	1.14	1.51	0.81	0.682	1.06	0.646	1.00	1.30	2.000	Yes
4450	44.50	2.65	1.14	1.51	0.81	0.682	1.06	0.646	1.00	1.30	2.000	Yes
4451	44.51	2.65	1.14	1.51	0.81	0.682	1.06	0.646	1.00	1.30	2.000	Yes
4452	44.52	2.65	1.14	1.51	0.81	0.682	1.06	0.646	1.00	1.30	2.000	Yes
4453	44.53	2.65	1.14	1.51	0.81	0.682	1.06	0.645	1.00	1.30	2.000	Yes
4454	44.54	2.65	1.14	1.51	0.81	0.682	1.06	0.645	1.00	1.30	2.000	Yes
4455	44.55	2.65	1.14	1.51	0.81	0.682	1.06	0.645	1.00	1.30	2.000	Yes
4456	44.56	2.65	1.14	1.51	0.81	0.682	1.06	0.645	1.00	1.30	2.000	Yes
4457	44.57	2.65	1.14	1.51	0.81	0.682	1.06	0.645	1.00	1.30	2.000	Yes
4458	44.58	2.66	1.14	1.51	0.81	0.681	1.06	0.645	1.00	1.30	2.000	Yes
4459	44.59	2.66	1.14	1.51	0.81	0.681	1.06	0.645	1.00	1.30	2.000	Yes
4460	44.60	2.66	1.14	1.51	0.81	0.681	1.06	0.645	1.00	1.30	2.000	Yes
4461	44.61	2.66	1.14	1.51	0.81	0.681	1.06	0.645	1.00	1.30	2.000	Yes
4462	44.62	2.66	1.14	1.52	0.81	0.681	1.06	0.645	1.00	1.30	2.000	Yes
4463	44.63	2.66	1.14	1.52	0.81	0.681	1.06	0.645	1.00	1.30	2.000	Yes
4464	44.64	2.66	1.14	1.52	0.81	0.681	1.06	0.645	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
4465	44.65	2.66	1.14	1.52	0.81	0.681	1.06	0.645	1.00	1.30	2.000	Yes
4466	44.66	2.66	1.14	1.52	0.81	0.681	1.06	0.645	1.00	1.30	2.000	Yes
4467	44.67	2.66	1.14	1.52	0.81	0.681	1.06	0.645	1.00	1.30	2.000	Yes
4468	44.68	2.66	1.14	1.52	0.81	0.681	1.06	0.644	1.00	1.30	2.000	Yes
4469	44.69	2.66	1.14	1.52	0.81	0.681	1.06	0.644	1.00	1.30	2.000	Yes
4470	44.70	2.66	1.15	1.52	0.81	0.681	1.06	0.644	1.00	1.30	2.000	Yes
4471	44.71	2.66	1.15	1.52	0.81	0.681	1.06	0.644	1.00	1.30	2.000	Yes
4472	44.72	2.66	1.15	1.52	0.81	0.681	1.06	0.644	1.00	1.30	2.000	Yes
4473	44.73	2.66	1.15	1.52	0.81	0.680	1.06	0.644	1.00	1.30	2.000	Yes
4474	44.74	2.67	1.15	1.52	0.81	0.680	1.06	0.644	1.00	1.30	2.000	Yes
4475	44.75	2.67	1.15	1.52	0.81	0.680	1.06	0.644	1.00	1.30	2.000	Yes
4476	44.76	2.67	1.15	1.52	0.81	0.680	1.06	0.644	1.00	1.30	2.000	Yes
4477	44.77	2.67	1.15	1.52	0.81	0.680	1.06	0.644	1.00	1.30	2.000	Yes
4478	44.78	2.67	1.15	1.52	0.81	0.680	1.06	0.644	1.00	1.30	2.000	Yes
4479	44.79	2.67	1.15	1.52	0.81	0.680	1.06	0.644	1.00	1.30	2.000	Yes
4480	44.80	2.67	1.15	1.52	0.81	0.680	1.06	0.644	1.00	1.30	2.000	Yes
4481	44.81	2.67	1.15	1.52	0.81	0.680	1.06	0.644	1.00	1.30	0.837	No
4482	44.82	2.67	1.15	1.52	0.81	0.680	1.06	0.644	1.00	1.30	0.837	No
4483	44.83	2.67	1.15	1.52	0.81	0.680	1.06	0.643	1.00	1.30	0.837	No
4484	44.84	2.67	1.15	1.52	0.81	0.680	1.06	0.643	1.00	1.30	0.836	No
4485	44.85	2.67	1.15	1.52	0.81	0.680	1.06	0.643	1.00	1.30	0.836	No
4486	44.86	2.67	1.15	1.52	0.81	0.680	1.06	0.643	1.00	1.30	0.836	No
4487	44.87	2.67	1.15	1.52	0.80	0.679	1.06	0.643	1.00	1.30	0.836	No
4488	44.88	2.67	1.15	1.52	0.80	0.679	1.06	0.643	1.00	1.30	0.836	No
4489	44.89	2.68	1.15	1.52	0.80	0.679	1.06	0.643	1.00	1.30	0.836	No
4490	44.90	2.68	1.15	1.52	0.80	0.679	1.06	0.643	1.00	1.30	0.836	No
4491	44.91	2.68	1.15	1.53	0.80	0.679	1.06	0.643	1.00	1.30	0.836	No
4492	44.92	2.68	1.15	1.53	0.80	0.679	1.06	0.643	1.00	1.30	0.836	No
4493	44.93	2.68	1.15	1.53	0.80	0.679	1.06	0.643	1.00	1.30	0.836	No
4494	44.94	2.68	1.15	1.53	0.80	0.679	1.06	0.643	1.00	1.30	0.836	No
4495	44.95	2.68	1.15	1.53	0.80	0.679	1.06	0.643	1.00	1.30	0.835	No
4496	44.96	2.68	1.15	1.53	0.80	0.679	1.06	0.643	1.00	1.30	0.835	No
4497	44.97	2.68	1.15	1.53	0.80	0.679	1.06	0.643	1.00	1.30	0.835	No
4498	44.98	2.68	1.15	1.53	0.80	0.679	1.06	0.642	1.00	1.30	0.835	No
4499	44.99	2.68	1.15	1.53	0.80	0.679	1.06	0.642	1.00	1.30	0.835	No
4500	45.00	2.68	1.15	1.53	0.80	0.679	1.06	0.642	1.00	1.30	0.835	No
4501	45.01	2.68	1.15	1.53	0.80	0.679	1.06	0.642	1.00	1.30	0.835	No
4502	45.02	2.68	1.16	1.53	0.80	0.678	1.06	0.642	1.00	1.30	0.835	No
4503	45.03	2.68	1.16	1.53	0.80	0.678	1.06	0.642	1.00	1.30	0.835	No
4504	45.04	2.69	1.16	1.53	0.80	0.678	1.06	0.642	1.00	1.30	0.835	No
4505	45.05	2.69	1.16	1.53	0.80	0.678	1.06	0.642	1.00	1.30	0.835	No
4506	45.06	2.69	1.16	1.53	0.80	0.678	1.06	0.642	1.00	1.30	0.835	No
4507	45.07	2.69	1.16	1.53	0.80	0.678	1.06	0.642	1.00	1.30	0.834	No
4508	45.08	2.69	1.16	1.53	0.80	0.678	1.06	0.642	1.00	1.30	2.000	Yes
4509	45.09	2.69	1.16	1.53	0.80	0.678	1.06	0.642	1.00	1.30	2.000	Yes
4510	45.10	2.69	1.16	1.53	0.80	0.678	1.06	0.642	1.00	1.30	2.000	Yes
4511	45.11	2.69	1.16	1.53	0.80	0.678	1.06	0.642	1.00	1.30	2.000	Yes
4512	45.12	2.69	1.16	1.53	0.80	0.678	1.06	0.642	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
4513	45.13	2.69	1.16	1.53	0.80	0.678	1.06	0.641	1.00	1.30	2.000	Yes
4514	45.14	2.69	1.16	1.53	0.80	0.678	1.06	0.641	1.00	1.30	2.000	Yes
4515	45.15	2.69	1.16	1.53	0.80	0.678	1.06	0.641	1.00	1.30	2.000	Yes
4516	45.16	2.69	1.16	1.53	0.80	0.677	1.06	0.641	1.00	1.30	2.000	Yes
4517	45.17	2.69	1.16	1.53	0.80	0.677	1.06	0.641	1.00	1.30	2.000	Yes
4518	45.18	2.69	1.16	1.53	0.80	0.677	1.06	0.641	1.00	1.30	2.000	Yes
4519	45.19	2.69	1.16	1.53	0.80	0.677	1.06	0.641	1.00	1.30	2.000	Yes
4520	45.20	2.70	1.16	1.53	0.80	0.677	1.06	0.641	1.00	1.30	2.000	Yes
4521	45.21	2.70	1.16	1.54	0.80	0.677	1.06	0.641	1.00	1.30	2.000	Yes
4522	45.22	2.70	1.16	1.54	0.80	0.677	1.06	0.641	1.00	1.30	2.000	Yes
4523	45.23	2.70	1.16	1.54	0.80	0.677	1.06	0.641	1.00	1.30	2.000	Yes
4524	45.24	2.70	1.16	1.54	0.80	0.677	1.06	0.641	1.00	1.30	2.000	Yes
4525	45.25	2.70	1.16	1.54	0.80	0.677	1.06	0.641	1.00	1.30	2.000	Yes
4526	45.26	2.70	1.16	1.54	0.80	0.677	1.06	0.641	1.00	1.30	2.000	Yes
4527	45.27	2.70	1.16	1.54	0.80	0.677	1.06	0.641	1.00	1.30	2.000	Yes
4528	45.28	2.70	1.16	1.54	0.80	0.677	1.06	0.640	1.00	1.30	2.000	Yes
4529	45.29	2.70	1.16	1.54	0.80	0.677	1.06	0.640	1.00	1.30	2.000	Yes
4530	45.30	2.70	1.16	1.54	0.80	0.676	1.06	0.640	1.00	1.30	2.000	Yes
4531	45.31	2.70	1.16	1.54	0.80	0.676	1.06	0.640	1.00	1.30	2.000	Yes
4532	45.32	2.70	1.16	1.54	0.80	0.676	1.06	0.640	1.00	1.30	2.000	Yes
4533	45.33	2.70	1.16	1.54	0.80	0.676	1.06	0.640	1.00	1.30	2.000	Yes
4534	45.34	2.70	1.17	1.54	0.80	0.676	1.06	0.640	1.00	1.30	0.832	No
4535	45.35	2.71	1.17	1.54	0.80	0.676	1.06	0.640	1.00	1.30	0.832	No
4536	45.36	2.71	1.17	1.54	0.80	0.676	1.06	0.640	1.00	1.30	0.832	No
4537	45.37	2.71	1.17	1.54	0.80	0.676	1.06	0.640	1.00	1.30	0.832	No
4538	45.38	2.71	1.17	1.54	0.80	0.676	1.06	0.640	1.00	1.30	0.832	No
4539	45.39	2.71	1.17	1.54	0.80	0.676	1.06	0.640	1.00	1.30	0.832	No
4540	45.40	2.71	1.17	1.54	0.80	0.676	1.06	0.640	1.00	1.30	0.832	No
4541	45.41	2.71	1.17	1.54	0.80	0.676	1.06	0.640	1.00	1.30	0.832	No
4542	45.42	2.71	1.17	1.54	0.80	0.676	1.06	0.640	1.00	1.30	0.831	No
4543	45.43	2.71	1.17	1.54	0.80	0.676	1.06	0.639	1.00	1.30	0.831	No
4544	45.44	2.71	1.17	1.54	0.80	0.675	1.06	0.639	1.00	1.30	0.831	No
4545	45.45	2.71	1.17	1.54	0.80	0.675	1.06	0.639	1.00	1.30	0.831	No
4546	45.46	2.71	1.17	1.54	0.80	0.675	1.06	0.639	1.00	1.30	0.831	No
4547	45.47	2.71	1.17	1.54	0.80	0.675	1.06	0.639	1.00	1.30	0.831	No
4548	45.48	2.71	1.17	1.54	0.80	0.675	1.06	0.639	1.00	1.30	0.831	No
4549	45.49	2.71	1.17	1.54	0.80	0.675	1.06	0.639	1.00	1.30	0.831	No
4550	45.50	2.71	1.17	1.54	0.80	0.675	1.06	0.639	1.00	1.30	2.000	Yes
4551	45.51	2.72	1.17	1.55	0.80	0.675	1.06	0.639	1.00	1.30	2.000	Yes
4552	45.52	2.72	1.17	1.55	0.80	0.675	1.06	0.639	1.00	1.30	2.000	Yes
4553	45.53	2.72	1.17	1.55	0.80	0.675	1.06	0.639	1.00	1.30	2.000	Yes
4554	45.54	2.72	1.17	1.55	0.80	0.675	1.06	0.639	1.00	1.30	2.000	Yes
4555	45.55	2.72	1.17	1.55	0.80	0.675	1.06	0.639	1.00	1.30	2.000	Yes
4556	45.56	2.72	1.17	1.55	0.80	0.675	1.06	0.639	1.00	1.30	2.000	Yes
4557	45.57	2.72	1.17	1.55	0.80	0.675	1.06	0.639	1.00	1.30	2.000	Yes
4558	45.58	2.72	1.17	1.55	0.80	0.674	1.06	0.638	1.00	1.30	2.000	Yes
4559	45.59	2.72	1.17	1.55	0.80	0.674	1.06	0.638	1.00	1.30	2.000	Yes
4560	45.60	2.72	1.17	1.55	0.80	0.674	1.06	0.638	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
4561	45.61	2.72	1.17	1.55	0.80	0.674	1.06	0.638	1.00	1.30	2.000	Yes
4562	45.62	2.72	1.17	1.55	0.80	0.674	1.06	0.638	1.00	1.30	2.000	Yes
4563	45.63	2.72	1.17	1.55	0.80	0.674	1.06	0.638	1.00	1.30	2.000	Yes
4564	45.64	2.72	1.17	1.55	0.80	0.674	1.06	0.638	1.00	1.30	2.000	Yes
4565	45.65	2.72	1.17	1.55	0.80	0.674	1.06	0.638	1.00	1.30	2.000	Yes
4566	45.66	2.73	1.17	1.55	0.80	0.674	1.06	0.638	1.00	1.30	2.000	Yes
4567	45.67	2.73	1.18	1.55	0.80	0.674	1.06	0.638	1.00	1.30	2.000	Yes
4568	45.68	2.73	1.18	1.55	0.80	0.674	1.06	0.638	1.00	1.30	2.000	Yes
4569	45.69	2.73	1.18	1.55	0.80	0.674	1.06	0.638	1.00	1.30	2.000	Yes
4570	45.70	2.73	1.18	1.55	0.80	0.674	1.06	0.638	1.00	1.30	2.000	Yes
4571	45.71	2.73	1.18	1.55	0.80	0.674	1.06	0.638	1.00	1.30	2.000	Yes
4572	45.72	2.73	1.18	1.55	0.80	0.673	1.06	0.638	1.00	1.30	2.000	Yes
4573	45.73	2.73	1.18	1.55	0.80	0.673	1.06	0.637	1.00	1.30	2.000	Yes
4574	45.74	2.73	1.18	1.55	0.80	0.673	1.06	0.637	1.00	1.30	2.000	Yes
4575	45.75	2.73	1.18	1.55	0.80	0.673	1.06	0.637	1.00	1.30	2.000	Yes
4576	45.76	2.73	1.18	1.55	0.80	0.673	1.06	0.637	1.00	1.30	2.000	Yes
4577	45.77	2.73	1.18	1.55	0.80	0.673	1.06	0.637	1.00	1.30	0.828	No
4578	45.78	2.73	1.18	1.55	0.80	0.673	1.06	0.637	1.00	1.30	0.828	No
4579	45.79	2.73	1.18	1.55	0.80	0.673	1.06	0.637	1.00	1.30	0.828	No
4580	45.80	2.73	1.18	1.56	0.80	0.673	1.06	0.637	1.00	1.30	0.828	No
4581	45.81	2.74	1.18	1.56	0.80	0.673	1.06	0.637	1.00	1.30	0.828	No
4582	45.82	2.74	1.18	1.56	0.80	0.673	1.06	0.637	1.00	1.30	0.828	No
4583	45.83	2.74	1.18	1.56	0.80	0.673	1.06	0.637	1.00	1.30	0.828	No
4584	45.84	2.74	1.18	1.56	0.80	0.673	1.06	0.637	1.00	1.30	0.828	No
4585	45.85	2.74	1.18	1.56	0.80	0.673	1.06	0.637	1.00	1.30	0.828	No
4586	45.86	2.74	1.18	1.56	0.79	0.672	1.06	0.637	1.00	1.30	0.828	No
4587	45.87	2.74	1.18	1.56	0.79	0.672	1.06	0.637	1.00	1.30	0.827	No
4588	45.88	2.74	1.18	1.56	0.79	0.672	1.06	0.636	1.00	1.30	0.827	No
4589	45.89	2.74	1.18	1.56	0.79	0.672	1.06	0.636	1.00	1.30	0.827	No
4590	45.90	2.74	1.18	1.56	0.79	0.672	1.06	0.636	1.00	1.30	0.827	No
4591	45.91	2.74	1.18	1.56	0.79	0.672	1.06	0.636	1.00	1.30	0.827	No
4592	45.92	2.74	1.18	1.56	0.79	0.672	1.06	0.636	1.00	1.30	0.827	No
4593	45.93	2.74	1.18	1.56	0.79	0.672	1.06	0.636	1.00	1.30	0.827	No
4594	45.94	2.74	1.18	1.56	0.79	0.672	1.06	0.636	1.00	1.30	0.827	No
4595	45.95	2.74	1.18	1.56	0.79	0.672	1.06	0.636	1.00	1.30	0.827	No
4596	45.96	2.74	1.18	1.56	0.79	0.672	1.06	0.636	1.00	1.30	0.827	No
4597	45.97	2.75	1.18	1.56	0.79	0.672	1.06	0.636	1.00	1.30	0.827	No
4598	45.98	2.75	1.18	1.56	0.79	0.672	1.06	0.636	1.00	1.30	0.827	No
4599	45.99	2.75	1.19	1.56	0.79	0.672	1.06	0.636	1.00	1.30	0.826	No
4600	46.00	2.75	1.19	1.56	0.79	0.671	1.06	0.636	1.00	1.30	0.826	No
4601	46.01	2.75	1.19	1.56	0.79	0.671	1.06	0.636	1.00	1.30	0.826	No
4602	46.02	2.75	1.19	1.56	0.79	0.671	1.06	0.636	1.00	1.30	0.826	No
4603	46.03	2.75	1.19	1.56	0.79	0.671	1.06	0.635	1.00	1.30	0.826	No
4604	46.04	2.75	1.19	1.56	0.79	0.671	1.06	0.635	1.00	1.30	0.826	No
4605	46.05	2.75	1.19	1.56	0.79	0.671	1.06	0.635	1.00	1.30	0.826	No
4606	46.06	2.75	1.19	1.56	0.79	0.671	1.06	0.635	1.00	1.30	0.826	No
4607	46.07	2.75	1.19	1.56	0.79	0.671	1.06	0.635	1.00	1.30	0.826	No
4608	46.08	2.75	1.19	1.56	0.79	0.671	1.06	0.635	1.00	1.30	0.826	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
4609	46.09	2.75	1.19	1.56	0.79	0.671	1.06	0.635	1.00	1.30	0.826	No
4610	46.10	2.75	1.19	1.57	0.79	0.671	1.06	0.635	1.00	1.30	0.825	No
4611	46.11	2.75	1.19	1.57	0.79	0.671	1.06	0.635	1.00	1.30	0.825	No
4612	46.12	2.76	1.19	1.57	0.79	0.671	1.06	0.635	1.00	1.30	0.825	No
4613	46.13	2.76	1.19	1.57	0.79	0.671	1.06	0.635	1.00	1.30	0.825	No
4614	46.14	2.76	1.19	1.57	0.79	0.670	1.06	0.635	1.00	1.30	0.825	No
4615	46.15	2.76	1.19	1.57	0.79	0.670	1.06	0.635	1.00	1.30	0.825	No
4616	46.16	2.76	1.19	1.57	0.79	0.670	1.06	0.635	1.00	1.30	0.825	No
4617	46.17	2.76	1.19	1.57	0.79	0.670	1.06	0.634	1.00	1.30	0.825	No
4618	46.18	2.76	1.19	1.57	0.79	0.670	1.06	0.634	1.00	1.30	0.825	No
4619	46.19	2.76	1.19	1.57	0.79	0.670	1.06	0.634	1.00	1.30	0.825	No
4620	46.20	2.76	1.19	1.57	0.79	0.670	1.06	0.634	1.00	1.30	0.825	No
4621	46.21	2.76	1.19	1.57	0.79	0.670	1.06	0.634	1.00	1.30	0.824	No
4622	46.22	2.76	1.19	1.57	0.79	0.670	1.06	0.634	1.00	1.30	0.824	No
4623	46.23	2.76	1.19	1.57	0.79	0.670	1.06	0.634	1.00	1.30	0.824	No
4624	46.24	2.76	1.19	1.57	0.79	0.670	1.06	0.634	1.00	1.30	0.824	No
4625	46.25	2.76	1.19	1.57	0.79	0.670	1.06	0.634	1.00	1.30	0.824	No
4626	46.26	2.76	1.19	1.57	0.79	0.670	1.06	0.634	1.00	1.30	0.824	No
4627	46.27	2.76	1.19	1.57	0.79	0.670	1.06	0.634	1.00	1.30	0.824	No
4628	46.28	2.77	1.19	1.57	0.79	0.669	1.06	0.634	1.00	1.30	0.824	No
4629	46.29	2.77	1.19	1.57	0.79	0.669	1.06	0.634	1.00	1.30	0.824	No
4630	46.30	2.77	1.19	1.57	0.79	0.669	1.06	0.634	1.00	1.30	0.824	No
4631	46.31	2.77	1.20	1.57	0.79	0.669	1.06	0.634	1.00	1.30	0.824	No
4632	46.32	2.77	1.20	1.57	0.79	0.669	1.06	0.633	1.00	1.30	0.823	No
4633	46.33	2.77	1.20	1.57	0.79	0.669	1.06	0.633	1.00	1.30	0.823	No
4634	46.34	2.77	1.20	1.57	0.79	0.669	1.06	0.633	1.00	1.30	0.823	No
4635	46.35	2.77	1.20	1.57	0.79	0.669	1.06	0.633	1.00	1.30	0.823	No
4636	46.36	2.77	1.20	1.57	0.79	0.669	1.06	0.633	1.00	1.30	0.823	No
4637	46.37	2.77	1.20	1.57	0.79	0.669	1.06	0.633	1.00	1.30	0.823	No
4638	46.38	2.77	1.20	1.57	0.79	0.669	1.06	0.633	1.00	1.30	0.823	No
4639	46.39	2.77	1.20	1.57	0.79	0.669	1.06	0.633	1.00	1.30	0.823	No
4640	46.40	2.77	1.20	1.58	0.79	0.669	1.06	0.633	1.00	1.30	0.823	No
4641	46.41	2.77	1.20	1.58	0.79	0.668	1.06	0.633	1.00	1.30	0.823	No
4642	46.42	2.77	1.20	1.58	0.79	0.668	1.06	0.633	1.00	1.30	0.823	No
4643	46.43	2.78	1.20	1.58	0.79	0.668	1.06	0.633	1.00	1.30	0.822	No
4644	46.44	2.78	1.20	1.58	0.79	0.668	1.06	0.633	1.00	1.30	0.822	No
4645	46.45	2.78	1.20	1.58	0.79	0.668	1.06	0.633	1.00	1.30	2.000	Yes
4646	46.46	2.78	1.20	1.58	0.79	0.668	1.06	0.632	1.00	1.30	2.000	Yes
4647	46.47	2.78	1.20	1.58	0.79	0.668	1.06	0.632	1.00	1.30	2.000	Yes
4648	46.48	2.78	1.20	1.58	0.79	0.668	1.06	0.632	1.00	1.30	2.000	Yes
4649	46.49	2.78	1.20	1.58	0.79	0.668	1.06	0.632	1.00	1.30	2.000	Yes
4650	46.50	2.78	1.20	1.58	0.79	0.668	1.06	0.632	1.00	1.30	2.000	Yes
4651	46.51	2.78	1.20	1.58	0.79	0.668	1.06	0.632	1.00	1.30	2.000	Yes
4652	46.52	2.78	1.20	1.58	0.79	0.668	1.06	0.632	1.00	1.30	2.000	Yes
4653	46.53	2.78	1.20	1.58	0.79	0.668	1.06	0.632	1.00	1.30	2.000	Yes
4654	46.54	2.78	1.20	1.58	0.79	0.668	1.06	0.632	1.00	1.30	2.000	Yes
4655	46.55	2.78	1.20	1.58	0.79	0.667	1.06	0.632	1.00	1.30	2.000	Yes
4656	46.56	2.78	1.20	1.58	0.79	0.667	1.06	0.632	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
4657	46.57	2.78	1.20	1.58	0.79	0.667	1.06	0.632	1.00	1.30	2.000	Yes
4658	46.58	2.79	1.20	1.58	0.79	0.667	1.06	0.632	1.00	1.30	2.000	Yes
4659	46.59	2.79	1.20	1.58	0.79	0.667	1.06	0.632	1.00	1.30	2.000	Yes
4660	46.60	2.79	1.20	1.58	0.79	0.667	1.06	0.632	1.00	1.30	2.000	Yes
4661	46.61	2.79	1.20	1.58	0.79	0.667	1.06	0.631	1.00	1.30	2.000	Yes
4662	46.62	2.79	1.20	1.58	0.79	0.667	1.06	0.631	1.00	1.30	2.000	Yes
4663	46.63	2.79	1.21	1.58	0.79	0.667	1.06	0.631	1.00	1.30	2.000	Yes
4664	46.64	2.79	1.21	1.58	0.79	0.667	1.06	0.631	1.00	1.30	2.000	Yes
4665	46.65	2.79	1.21	1.58	0.79	0.667	1.06	0.631	1.00	1.30	2.000	Yes
4666	46.66	2.79	1.21	1.58	0.79	0.667	1.06	0.631	1.00	1.30	2.000	Yes
4667	46.67	2.79	1.21	1.58	0.79	0.667	1.06	0.631	1.00	1.30	2.000	Yes
4668	46.68	2.79	1.21	1.58	0.79	0.667	1.06	0.631	1.00	1.30	2.000	Yes
4669	46.69	2.79	1.21	1.59	0.79	0.666	1.06	0.631	1.00	1.30	2.000	Yes
4670	46.70	2.79	1.21	1.59	0.79	0.666	1.06	0.631	1.00	1.30	2.000	Yes
4671	46.71	2.79	1.21	1.59	0.79	0.666	1.06	0.631	1.00	1.30	2.000	Yes
4672	46.72	2.79	1.21	1.59	0.79	0.666	1.06	0.631	1.00	1.30	2.000	Yes
4673	46.73	2.79	1.21	1.59	0.79	0.666	1.06	0.631	1.00	1.30	2.000	Yes
4674	46.74	2.80	1.21	1.59	0.79	0.666	1.06	0.631	1.00	1.30	2.000	Yes
4675	46.75	2.80	1.21	1.59	0.79	0.666	1.06	0.630	1.00	1.30	2.000	Yes
4676	46.76	2.80	1.21	1.59	0.79	0.666	1.06	0.630	1.00	1.30	2.000	Yes
4677	46.77	2.80	1.21	1.59	0.79	0.666	1.06	0.630	1.00	1.30	2.000	Yes
4678	46.78	2.80	1.21	1.59	0.79	0.666	1.06	0.630	1.00	1.30	2.000	Yes
4679	46.79	2.80	1.21	1.59	0.79	0.666	1.06	0.630	1.00	1.30	2.000	Yes
4680	46.80	2.80	1.21	1.59	0.79	0.666	1.06	0.630	1.00	1.30	2.000	Yes
4681	46.81	2.80	1.21	1.59	0.79	0.666	1.06	0.630	1.00	1.30	2.000	Yes
4682	46.82	2.80	1.21	1.59	0.79	0.665	1.06	0.630	1.00	1.30	2.000	Yes
4683	46.83	2.80	1.21	1.59	0.79	0.665	1.06	0.630	1.00	1.30	2.000	Yes
4684	46.84	2.80	1.21	1.59	0.79	0.665	1.06	0.630	1.00	1.30	2.000	Yes
4685	46.85	2.80	1.21	1.59	0.78	0.665	1.06	0.630	1.00	1.30	2.000	Yes
4686	46.86	2.80	1.21	1.59	0.78	0.665	1.06	0.630	1.00	1.30	2.000	Yes
4687	46.87	2.80	1.21	1.59	0.78	0.665	1.06	0.630	1.00	1.30	2.000	Yes
4688	46.88	2.80	1.21	1.59	0.78	0.665	1.06	0.630	1.00	1.30	2.000	Yes
4689	46.89	2.81	1.21	1.59	0.78	0.665	1.06	0.629	1.00	1.30	2.000	Yes
4690	46.90	2.81	1.21	1.59	0.78	0.665	1.06	0.629	1.00	1.30	2.000	Yes
4691	46.91	2.81	1.21	1.59	0.78	0.665	1.06	0.629	1.00	1.30	2.000	Yes
4692	46.92	2.81	1.21	1.59	0.78	0.665	1.06	0.629	1.00	1.30	2.000	Yes
4693	46.93	2.81	1.21	1.59	0.78	0.665	1.06	0.629	1.00	1.30	2.000	Yes
4694	46.94	2.81	1.21	1.59	0.78	0.665	1.06	0.629	1.00	1.30	2.000	Yes
4695	46.95	2.81	1.22	1.59	0.78	0.665	1.06	0.629	1.00	1.30	2.000	Yes
4696	46.96	2.81	1.22	1.59	0.78	0.664	1.06	0.629	1.00	1.30	2.000	Yes
4697	46.97	2.81	1.22	1.59	0.78	0.664	1.06	0.629	1.00	1.30	2.000	Yes
4698	46.98	2.81	1.22	1.59	0.78	0.664	1.06	0.629	1.00	1.30	2.000	Yes
4699	46.99	2.81	1.22	1.60	0.78	0.664	1.06	0.629	1.00	1.30	2.000	Yes
4700	47.00	2.81	1.22	1.60	0.78	0.664	1.06	0.629	1.00	1.30	2.000	Yes
4701	47.01	2.81	1.22	1.60	0.78	0.664	1.06	0.629	1.00	1.30	2.000	Yes
4702	47.02	2.81	1.22	1.60	0.78	0.664	1.06	0.629	1.00	1.30	2.000	Yes
4703	47.03	2.81	1.22	1.60	0.78	0.664	1.06	0.629	1.00	1.30	2.000	Yes
4704	47.04	2.81	1.22	1.60	0.78	0.664	1.06	0.628	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
4705	47.05	2.82	1.22	1.60	0.78	0.664	1.06	0.628	1.00	1.30	2.000	Yes
4706	47.06	2.82	1.22	1.60	0.78	0.664	1.06	0.628	1.00	1.30	2.000	Yes
4707	47.07	2.82	1.22	1.60	0.78	0.664	1.06	0.628	1.00	1.30	0.817	No
4708	47.08	2.82	1.22	1.60	0.78	0.664	1.06	0.628	1.00	1.30	0.817	No
4709	47.09	2.82	1.22	1.60	0.78	0.664	1.06	0.628	1.00	1.30	0.817	No
4710	47.10	2.82	1.22	1.60	0.78	0.663	1.06	0.628	1.00	1.30	0.816	No
4711	47.11	2.82	1.22	1.60	0.78	0.663	1.06	0.628	1.00	1.30	0.816	No
4712	47.12	2.82	1.22	1.60	0.78	0.663	1.06	0.628	1.00	1.30	0.816	No
4713	47.13	2.82	1.22	1.60	0.78	0.663	1.06	0.628	1.00	1.30	0.816	No
4714	47.14	2.82	1.22	1.60	0.78	0.663	1.06	0.628	1.00	1.30	0.816	No
4715	47.15	2.82	1.22	1.60	0.78	0.663	1.06	0.628	1.00	1.30	0.816	No
4716	47.16	2.82	1.22	1.60	0.78	0.663	1.06	0.628	1.00	1.30	0.816	No
4717	47.17	2.82	1.22	1.60	0.78	0.663	1.06	0.628	1.00	1.30	0.816	No
4718	47.18	2.82	1.22	1.60	0.78	0.663	1.06	0.627	1.00	1.30	0.816	No
4719	47.19	2.82	1.22	1.60	0.78	0.663	1.06	0.627	1.00	1.30	0.816	No
4720	47.20	2.83	1.22	1.60	0.78	0.663	1.06	0.627	1.00	1.30	0.816	No
4721	47.21	2.83	1.22	1.60	0.78	0.663	1.06	0.627	1.00	1.30	0.815	No
4722	47.22	2.83	1.22	1.60	0.78	0.663	1.06	0.627	1.00	1.30	0.815	No
4723	47.23	2.83	1.22	1.60	0.78	0.663	1.06	0.627	1.00	1.30	0.815	No
4724	47.24	2.83	1.22	1.60	0.78	0.662	1.06	0.627	1.00	1.30	0.815	No
4725	47.25	2.83	1.22	1.60	0.78	0.662	1.06	0.627	1.00	1.30	0.815	No
4726	47.26	2.83	1.22	1.60	0.78	0.662	1.06	0.627	1.00	1.30	0.815	No
4727	47.27	2.83	1.23	1.60	0.78	0.662	1.06	0.627	1.00	1.30	0.815	No
4728	47.28	2.83	1.23	1.60	0.78	0.662	1.06	0.627	1.00	1.30	0.815	No
4729	47.29	2.83	1.23	1.61	0.78	0.662	1.06	0.627	1.00	1.30	0.815	No
4730	47.30	2.83	1.23	1.61	0.78	0.662	1.06	0.627	1.00	1.30	0.815	No
4731	47.31	2.83	1.23	1.61	0.78	0.662	1.06	0.627	1.00	1.30	0.815	No
4732	47.32	2.83	1.23	1.61	0.78	0.662	1.06	0.627	1.00	1.30	0.814	No
4733	47.33	2.83	1.23	1.61	0.78	0.662	1.06	0.626	1.00	1.30	0.814	No
4734	47.34	2.83	1.23	1.61	0.78	0.662	1.06	0.626	1.00	1.30	0.814	No
4735	47.35	2.83	1.23	1.61	0.78	0.662	1.06	0.626	1.00	1.30	0.814	No
4736	47.36	2.84	1.23	1.61	0.78	0.662	1.06	0.626	1.00	1.30	0.814	No
4737	47.37	2.84	1.23	1.61	0.78	0.661	1.06	0.626	1.00	1.30	0.814	No
4738	47.38	2.84	1.23	1.61	0.78	0.661	1.06	0.626	1.00	1.30	0.814	No
4739	47.39	2.84	1.23	1.61	0.78	0.661	1.06	0.626	1.00	1.30	0.814	No
4740	47.40	2.84	1.23	1.61	0.78	0.661	1.06	0.626	1.00	1.30	0.814	No
4741	47.41	2.84	1.23	1.61	0.78	0.661	1.06	0.626	1.00	1.30	0.814	No
4742	47.42	2.84	1.23	1.61	0.78	0.661	1.06	0.626	1.00	1.30	0.814	No
4743	47.43	2.84	1.23	1.61	0.78	0.661	1.06	0.626	1.00	1.30	0.814	No
4744	47.44	2.84	1.23	1.61	0.78	0.661	1.06	0.626	1.00	1.30	0.813	No
4745	47.45	2.84	1.23	1.61	0.78	0.661	1.06	0.626	1.00	1.30	0.813	No
4746	47.46	2.84	1.23	1.61	0.78	0.661	1.06	0.626	1.00	1.30	0.813	No
4747	47.47	2.84	1.23	1.61	0.78	0.661	1.06	0.626	1.00	1.30	0.813	No
4748	47.48	2.84	1.23	1.61	0.78	0.661	1.06	0.625	1.00	1.30	0.813	No
4749	47.49	2.84	1.23	1.61	0.78	0.661	1.06	0.625	1.00	1.30	0.813	No
4750	47.50	2.84	1.23	1.61	0.78	0.661	1.06	0.625	1.00	1.30	0.813	No
4751	47.51	2.85	1.23	1.61	0.78	0.660	1.06	0.625	1.00	1.30	0.813	No
4752	47.52	2.85	1.23	1.61	0.78	0.660	1.06	0.625	1.00	1.30	0.813	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
4753	47.53	2.85	1.23	1.61	0.78	0.660	1.06	0.625	1.00	1.30	0.813	No
4754	47.54	2.85	1.23	1.61	0.78	0.660	1.06	0.625	1.00	1.30	0.813	No
4755	47.55	2.85	1.23	1.61	0.78	0.660	1.06	0.625	1.00	1.30	0.812	No
4756	47.56	2.85	1.23	1.61	0.78	0.660	1.06	0.625	1.00	1.30	0.812	No
4757	47.57	2.85	1.23	1.61	0.78	0.660	1.06	0.625	1.00	1.30	0.812	No
4758	47.58	2.85	1.23	1.61	0.78	0.660	1.06	0.625	1.00	1.30	0.812	No
4759	47.59	2.85	1.24	1.61	0.78	0.660	1.06	0.625	1.00	1.30	0.812	No
4760	47.60	2.85	1.24	1.62	0.78	0.660	1.06	0.625	1.00	1.30	0.812	No
4761	47.61	2.85	1.24	1.62	0.78	0.660	1.06	0.625	1.00	1.30	0.812	No
4762	47.62	2.85	1.24	1.62	0.78	0.660	1.06	0.624	1.00	1.30	0.812	No
4763	47.63	2.85	1.24	1.62	0.78	0.660	1.06	0.624	1.00	1.30	0.812	No
4764	47.64	2.85	1.24	1.62	0.78	0.660	1.06	0.624	1.00	1.30	0.812	No
4765	47.65	2.85	1.24	1.62	0.78	0.659	1.06	0.624	1.00	1.30	0.812	No
4766	47.66	2.85	1.24	1.62	0.78	0.659	1.06	0.624	1.00	1.30	0.811	No
4767	47.67	2.86	1.24	1.62	0.78	0.659	1.06	0.624	1.00	1.30	0.811	No
4768	47.68	2.86	1.24	1.62	0.78	0.659	1.06	0.624	1.00	1.30	0.811	No
4769	47.69	2.86	1.24	1.62	0.78	0.659	1.06	0.624	1.00	1.30	0.811	No
4770	47.70	2.86	1.24	1.62	0.78	0.659	1.06	0.624	1.00	1.30	0.811	No
4771	47.71	2.86	1.24	1.62	0.78	0.659	1.06	0.624	1.00	1.30	0.811	No
4772	47.72	2.86	1.24	1.62	0.78	0.659	1.06	0.624	1.00	1.30	0.811	No
4773	47.73	2.86	1.24	1.62	0.78	0.659	1.06	0.624	1.00	1.30	0.811	No
4774	47.74	2.86	1.24	1.62	0.78	0.659	1.06	0.624	1.00	1.30	0.811	No
4775	47.75	2.86	1.24	1.62	0.78	0.659	1.06	0.624	1.00	1.30	0.811	No
4776	47.76	2.86	1.24	1.62	0.78	0.659	1.06	0.624	1.00	1.30	0.811	No
4777	47.77	2.86	1.24	1.62	0.78	0.659	1.06	0.623	1.00	1.30	0.810	No
4778	47.78	2.86	1.24	1.62	0.78	0.659	1.06	0.623	1.00	1.30	0.810	No
4779	47.79	2.86	1.24	1.62	0.78	0.658	1.06	0.623	1.00	1.30	0.810	No
4780	47.80	2.86	1.24	1.62	0.78	0.658	1.06	0.623	1.00	1.30	0.810	No
4781	47.81	2.86	1.24	1.62	0.78	0.658	1.06	0.623	1.00	1.30	0.810	No
4782	47.82	2.86	1.24	1.62	0.78	0.658	1.06	0.623	1.00	1.30	0.810	No
4783	47.83	2.87	1.24	1.62	0.77	0.658	1.06	0.623	1.00	1.30	0.810	No
4784	47.84	2.87	1.24	1.62	0.77	0.658	1.06	0.623	1.00	1.30	0.810	No
4785	47.85	2.87	1.24	1.62	0.77	0.658	1.06	0.623	1.00	1.30	0.810	No
4786	47.86	2.87	1.24	1.62	0.77	0.658	1.06	0.623	1.00	1.30	0.810	No
4787	47.87	2.87	1.24	1.62	0.77	0.658	1.06	0.623	1.00	1.30	0.810	No
4788	47.88	2.87	1.24	1.62	0.77	0.658	1.06	0.623	1.00	1.30	0.810	No
4789	47.89	2.87	1.24	1.62	0.77	0.658	1.06	0.623	1.00	1.30	0.809	No
4790	47.90	2.87	1.24	1.62	0.77	0.658	1.06	0.623	1.00	1.30	0.809	No
4791	47.91	2.87	1.25	1.63	0.77	0.658	1.06	0.623	1.00	1.30	0.809	No
4792	47.92	2.87	1.25	1.63	0.77	0.658	1.06	0.622	1.00	1.30	0.809	No
4793	47.93	2.87	1.25	1.63	0.77	0.657	1.06	0.622	1.00	1.30	0.809	No
4794	47.94	2.87	1.25	1.63	0.77	0.657	1.06	0.622	1.00	1.30	0.809	No
4795	47.95	2.87	1.25	1.63	0.77	0.657	1.06	0.622	1.00	1.30	0.809	No
4796	47.96	2.87	1.25	1.63	0.77	0.657	1.06	0.622	1.00	1.30	0.809	No
4797	47.97	2.87	1.25	1.63	0.77	0.657	1.06	0.622	1.00	1.30	0.809	No
4798	47.98	2.87	1.25	1.63	0.77	0.657	1.06	0.622	1.00	1.30	0.809	No
4799	47.99	2.88	1.25	1.63	0.77	0.657	1.06	0.622	1.00	1.30	0.809	No
4800	48.00	2.88	1.25	1.63	0.77	0.657	1.06	0.622	1.00	1.30	0.808	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
4801	48.01	2.88	1.25	1.63	0.77	0.657	1.06	0.622	1.00	1.30	0.808	No
4802	48.02	2.88	1.25	1.63	0.77	0.657	1.06	0.622	1.00	1.30	0.808	No
4803	48.03	2.88	1.25	1.63	0.77	0.657	1.06	0.622	1.00	1.30	0.808	No
4804	48.04	2.88	1.25	1.63	0.77	0.657	1.06	0.622	1.00	1.30	0.808	No
4805	48.05	2.88	1.25	1.63	0.77	0.657	1.06	0.622	1.00	1.30	0.808	No
4806	48.06	2.88	1.25	1.63	0.77	0.657	1.06	0.622	1.00	1.30	0.808	No
4807	48.07	2.88	1.25	1.63	0.77	0.656	1.06	0.621	1.00	1.30	0.808	No
4808	48.08	2.88	1.25	1.63	0.77	0.656	1.06	0.621	1.00	1.30	0.808	No
4809	48.09	2.88	1.25	1.63	0.77	0.656	1.06	0.621	1.00	1.30	0.808	No
4810	48.10	2.88	1.25	1.63	0.77	0.656	1.06	0.621	1.00	1.30	0.808	No
4811	48.11	2.88	1.25	1.63	0.77	0.656	1.06	0.621	1.00	1.30	0.808	No
4812	48.12	2.88	1.25	1.63	0.77	0.656	1.06	0.621	1.00	1.30	0.807	No
4813	48.13	2.88	1.25	1.63	0.77	0.656	1.06	0.621	1.00	1.30	0.807	No
4814	48.14	2.88	1.25	1.63	0.77	0.656	1.06	0.621	1.00	1.30	0.807	No
4815	48.15	2.89	1.25	1.63	0.77	0.656	1.06	0.621	1.00	1.30	0.807	No
4816	48.16	2.89	1.25	1.63	0.77	0.656	1.06	0.621	1.00	1.30	0.807	No
4817	48.17	2.89	1.25	1.63	0.77	0.656	1.06	0.621	1.00	1.30	0.807	No
4818	48.18	2.89	1.25	1.63	0.77	0.656	1.06	0.621	1.00	1.30	0.807	No
4819	48.19	2.89	1.25	1.63	0.77	0.656	1.06	0.621	1.00	1.30	0.807	No
4820	48.20	2.89	1.25	1.63	0.77	0.656	1.06	0.621	1.00	1.30	0.807	No
4821	48.21	2.89	1.25	1.63	0.77	0.655	1.06	0.620	1.00	1.30	0.807	No
4822	48.22	2.89	1.25	1.64	0.77	0.655	1.06	0.620	1.00	1.30	0.807	No
4823	48.23	2.89	1.26	1.64	0.77	0.655	1.06	0.620	1.00	1.30	0.806	No
4824	48.24	2.89	1.26	1.64	0.77	0.655	1.06	0.620	1.00	1.30	0.806	No
4825	48.25	2.89	1.26	1.64	0.77	0.655	1.06	0.620	1.00	1.30	0.806	No
4826	48.26	2.89	1.26	1.64	0.77	0.655	1.06	0.620	1.00	1.30	0.806	No
4827	48.27	2.89	1.26	1.64	0.77	0.655	1.06	0.620	1.00	1.30	2.000	Yes
4828	48.28	2.89	1.26	1.64	0.77	0.655	1.06	0.620	1.00	1.30	2.000	Yes
4829	48.29	2.89	1.26	1.64	0.77	0.655	1.06	0.620	1.00	1.30	2.000	Yes
4830	48.30	2.89	1.26	1.64	0.77	0.655	1.06	0.620	1.00	1.30	2.000	Yes
4831	48.31	2.90	1.26	1.64	0.77	0.655	1.06	0.620	1.00	1.30	2.000	Yes
4832	48.32	2.90	1.26	1.64	0.77	0.655	1.06	0.620	1.00	1.30	2.000	Yes
4833	48.33	2.90	1.26	1.64	0.77	0.655	1.06	0.620	1.00	1.30	2.000	Yes
4834	48.34	2.90	1.26	1.64	0.77	0.655	1.06	0.620	1.00	1.30	2.000	Yes
4835	48.35	2.90	1.26	1.64	0.77	0.654	1.06	0.620	1.00	1.30	2.000	Yes
4836	48.36	2.90	1.26	1.64	0.77	0.654	1.06	0.619	1.00	1.30	2.000	Yes
4837	48.37	2.90	1.26	1.64	0.77	0.654	1.06	0.619	1.00	1.30	2.000	Yes
4838	48.38	2.90	1.26	1.64	0.77	0.654	1.06	0.619	1.00	1.30	2.000	Yes
4839	48.39	2.90	1.26	1.64	0.77	0.654	1.06	0.619	1.00	1.30	2.000	Yes
4840	48.40	2.90	1.26	1.64	0.77	0.654	1.06	0.619	1.00	1.30	2.000	Yes
4841	48.41	2.90	1.26	1.64	0.77	0.654	1.06	0.619	1.00	1.30	2.000	Yes
4842	48.42	2.90	1.26	1.64	0.77	0.654	1.06	0.619	1.00	1.30	2.000	Yes
4843	48.43	2.90	1.26	1.64	0.77	0.654	1.06	0.619	1.00	1.30	2.000	Yes
4844	48.44	2.90	1.26	1.64	0.77	0.654	1.06	0.619	1.00	1.30	2.000	Yes
4845	48.45	2.90	1.26	1.64	0.77	0.654	1.06	0.619	1.00	1.30	2.000	Yes
4846	48.46	2.90	1.26	1.64	0.77	0.654	1.06	0.619	1.00	1.30	2.000	Yes
4847	48.47	2.91	1.26	1.64	0.77	0.654	1.06	0.619	1.00	1.30	2.000	Yes
4848	48.48	2.91	1.26	1.64	0.77	0.654	1.06	0.619	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
4849	48.49	2.91	1.26	1.64	0.77	0.653	1.06	0.619	1.00	1.30	2.000	Yes
4850	48.50	2.91	1.26	1.64	0.77	0.653	1.06	0.619	1.00	1.30	2.000	Yes
4851	48.51	2.91	1.26	1.64	0.77	0.653	1.06	0.618	1.00	1.30	2.000	Yes
4852	48.52	2.91	1.26	1.64	0.77	0.653	1.06	0.618	1.00	1.30	2.000	Yes
4853	48.53	2.91	1.26	1.64	0.77	0.653	1.06	0.618	1.00	1.30	2.000	Yes
4854	48.54	2.91	1.26	1.65	0.77	0.653	1.06	0.618	1.00	1.30	0.804	No
4855	48.55	2.91	1.27	1.65	0.77	0.653	1.06	0.618	1.00	1.30	0.804	No
4856	48.56	2.91	1.27	1.65	0.77	0.653	1.06	0.618	1.00	1.30	0.804	No
4857	48.57	2.91	1.27	1.65	0.77	0.653	1.06	0.618	1.00	1.30	0.803	No
4858	48.58	2.91	1.27	1.65	0.77	0.653	1.06	0.618	1.00	1.30	0.803	No
4859	48.59	2.91	1.27	1.65	0.77	0.653	1.06	0.618	1.00	1.30	0.803	No
4860	48.60	2.91	1.27	1.65	0.77	0.653	1.06	0.618	1.00	1.30	0.803	No
4861	48.61	2.91	1.27	1.65	0.77	0.653	1.06	0.618	1.00	1.30	0.803	No
4862	48.62	2.91	1.27	1.65	0.77	0.653	1.06	0.618	1.00	1.30	2.000	Yes
4863	48.63	2.92	1.27	1.65	0.77	0.652	1.06	0.618	1.00	1.30	2.000	Yes
4864	48.64	2.92	1.27	1.65	0.77	0.652	1.06	0.618	1.00	1.30	2.000	Yes
4865	48.65	2.92	1.27	1.65	0.77	0.652	1.06	0.618	1.00	1.30	2.000	Yes
4866	48.66	2.92	1.27	1.65	0.77	0.652	1.06	0.617	1.00	1.30	2.000	Yes
4867	48.67	2.92	1.27	1.65	0.77	0.652	1.06	0.617	1.00	1.30	2.000	Yes
4868	48.68	2.92	1.27	1.65	0.77	0.652	1.06	0.617	1.00	1.30	2.000	Yes
4869	48.69	2.92	1.27	1.65	0.77	0.652	1.06	0.617	1.00	1.30	2.000	Yes
4870	48.70	2.92	1.27	1.65	0.77	0.652	1.06	0.617	1.00	1.30	2.000	Yes
4871	48.71	2.92	1.27	1.65	0.77	0.652	1.06	0.617	1.00	1.30	2.000	Yes
4872	48.72	2.92	1.27	1.65	0.77	0.652	1.06	0.617	1.00	1.30	2.000	Yes
4873	48.73	2.92	1.27	1.65	0.77	0.652	1.06	0.617	1.00	1.30	2.000	Yes
4874	48.74	2.92	1.27	1.65	0.77	0.652	1.06	0.617	1.00	1.30	2.000	Yes
4875	48.75	2.92	1.27	1.65	0.77	0.652	1.06	0.617	1.00	1.30	2.000	Yes
4876	48.76	2.92	1.27	1.65	0.77	0.652	1.06	0.617	1.00	1.30	2.000	Yes
4877	48.77	2.92	1.27	1.65	0.77	0.651	1.06	0.617	1.00	1.30	2.000	Yes
4878	48.78	2.93	1.27	1.65	0.77	0.651	1.06	0.617	1.00	1.30	2.000	Yes
4879	48.79	2.93	1.27	1.65	0.77	0.651	1.06	0.617	1.00	1.30	2.000	Yes
4880	48.80	2.93	1.27	1.65	0.76	0.651	1.06	0.616	1.00	1.30	2.000	Yes
4881	48.81	2.93	1.27	1.65	0.76	0.651	1.06	0.616	1.00	1.30	2.000	Yes
4882	48.82	2.93	1.27	1.65	0.76	0.651	1.06	0.616	1.00	1.30	2.000	Yes
4883	48.83	2.93	1.27	1.65	0.76	0.651	1.06	0.616	1.00	1.30	2.000	Yes
4884	48.84	2.93	1.27	1.65	0.76	0.651	1.06	0.616	1.00	1.30	2.000	Yes
4885	48.85	2.93	1.27	1.65	0.76	0.651	1.06	0.616	1.00	1.30	2.000	Yes
4886	48.86	2.93	1.27	1.66	0.76	0.651	1.06	0.616	1.00	1.30	2.000	Yes
4887	48.87	2.93	1.28	1.66	0.76	0.651	1.06	0.616	1.00	1.30	2.000	Yes
4888	48.88	2.93	1.28	1.66	0.76	0.651	1.06	0.616	1.00	1.30	2.000	Yes
4889	48.89	2.93	1.28	1.66	0.76	0.651	1.06	0.616	1.00	1.30	2.000	Yes
4890	48.90	2.93	1.28	1.66	0.76	0.651	1.06	0.616	1.00	1.30	0.801	No
4891	48.91	2.93	1.28	1.66	0.76	0.650	1.06	0.616	1.00	1.30	0.800	No
4892	48.92	2.93	1.28	1.66	0.76	0.650	1.06	0.616	1.00	1.30	0.800	No
4893	48.93	2.93	1.28	1.66	0.76	0.650	1.06	0.616	1.00	1.30	0.800	No
4894	48.94	2.94	1.28	1.66	0.76	0.650	1.06	0.616	1.00	1.30	0.800	No
4895	48.95	2.94	1.28	1.66	0.76	0.650	1.06	0.615	1.00	1.30	0.800	No
4896	48.96	2.94	1.28	1.66	0.76	0.650	1.06	0.615	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
4897	48.97	2.94	1.28	1.66	0.76	0.650	1.06	0.615	1.00	1.30	2.000	Yes
4898	48.98	2.94	1.28	1.66	0.76	0.650	1.06	0.615	1.00	1.30	2.000	Yes
4899	48.99	2.94	1.28	1.66	0.76	0.650	1.06	0.615	1.00	1.30	2.000	Yes
4900	49.00	2.94	1.28	1.66	0.76	0.650	1.06	0.615	1.00	1.30	2.000	Yes
4901	49.01	2.94	1.28	1.66	0.76	0.650	1.06	0.615	1.00	1.30	2.000	Yes
4902	49.02	2.94	1.28	1.66	0.76	0.650	1.06	0.615	1.00	1.30	2.000	Yes
4903	49.03	2.94	1.28	1.66	0.76	0.650	1.06	0.615	1.00	1.30	2.000	Yes
4904	49.04	2.94	1.28	1.66	0.76	0.649	1.06	0.615	1.00	1.30	2.000	Yes
4905	49.05	2.94	1.28	1.66	0.76	0.649	1.06	0.615	1.00	1.30	2.000	Yes
4906	49.06	2.94	1.28	1.66	0.76	0.649	1.06	0.615	1.00	1.30	2.000	Yes
4907	49.07	2.94	1.28	1.66	0.76	0.649	1.06	0.615	1.00	1.30	2.000	Yes
4908	49.08	2.94	1.28	1.66	0.76	0.649	1.06	0.615	1.00	1.30	2.000	Yes
4909	49.09	2.94	1.28	1.66	0.76	0.649	1.06	0.614	1.00	1.30	2.000	Yes
4910	49.10	2.95	1.28	1.66	0.76	0.649	1.06	0.614	1.00	1.30	2.000	Yes
4911	49.11	2.95	1.28	1.66	0.76	0.649	1.06	0.614	1.00	1.30	2.000	Yes
4912	49.12	2.95	1.28	1.66	0.76	0.649	1.06	0.614	1.00	1.30	2.000	Yes
4913	49.13	2.95	1.28	1.66	0.76	0.649	1.06	0.614	1.00	1.30	2.000	Yes
4914	49.14	2.95	1.28	1.66	0.76	0.649	1.06	0.614	1.00	1.30	2.000	Yes
4915	49.15	2.95	1.28	1.67	0.76	0.649	1.06	0.614	1.00	1.30	2.000	Yes
4916	49.16	2.95	1.28	1.67	0.76	0.649	1.06	0.614	1.00	1.30	2.000	Yes
4917	49.17	2.95	1.28	1.67	0.76	0.648	1.06	0.614	1.00	1.30	2.000	Yes
4918	49.18	2.95	1.28	1.67	0.76	0.648	1.06	0.614	1.00	1.30	2.000	Yes
4919	49.19	2.95	1.29	1.67	0.76	0.648	1.06	0.614	1.00	1.30	2.000	Yes
4920	49.20	2.95	1.29	1.67	0.76	0.648	1.06	0.614	1.00	1.30	2.000	Yes
4921	49.21	2.95	1.29	1.67	0.76	0.648	1.06	0.614	1.00	1.30	2.000	Yes
4922	49.22	2.95	1.29	1.67	0.76	0.648	1.06	0.614	1.00	1.30	2.000	Yes
4923	49.23	2.95	1.29	1.67	0.76	0.648	1.06	0.613	1.00	1.30	2.000	Yes
4924	49.24	2.95	1.29	1.67	0.76	0.648	1.06	0.613	1.00	1.30	2.000	Yes
4925	49.25	2.96	1.29	1.67	0.76	0.648	1.06	0.613	1.00	1.30	2.000	Yes
4926	49.26	2.96	1.29	1.67	0.76	0.648	1.06	0.613	1.00	1.30	2.000	Yes
4927	49.27	2.96	1.29	1.67	0.76	0.648	1.06	0.613	1.00	1.30	2.000	Yes
4928	49.28	2.96	1.29	1.67	0.76	0.648	1.06	0.613	1.00	1.30	2.000	Yes
4929	49.29	2.96	1.29	1.67	0.76	0.648	1.06	0.613	1.00	1.30	2.000	Yes
4930	49.30	2.96	1.29	1.67	0.76	0.647	1.06	0.613	1.00	1.30	2.000	Yes
4931	49.31	2.96	1.29	1.67	0.76	0.647	1.06	0.613	1.00	1.30	2.000	Yes
4932	49.32	2.96	1.29	1.67	0.76	0.647	1.06	0.613	1.00	1.30	2.000	Yes
4933	49.33	2.96	1.29	1.67	0.76	0.647	1.06	0.613	1.00	1.30	2.000	Yes
4934	49.34	2.96	1.29	1.67	0.76	0.647	1.06	0.613	1.00	1.30	2.000	Yes
4935	49.35	2.96	1.29	1.67	0.76	0.647	1.06	0.613	1.00	1.30	2.000	Yes
4936	49.36	2.96	1.29	1.67	0.76	0.647	1.06	0.612	1.00	1.30	2.000	Yes
4937	49.37	2.96	1.29	1.67	0.76	0.647	1.06	0.612	1.00	1.30	2.000	Yes
4938	49.38	2.96	1.29	1.67	0.76	0.647	1.06	0.612	1.00	1.30	2.000	Yes
4939	49.39	2.96	1.29	1.67	0.76	0.647	1.06	0.612	1.00	1.30	2.000	Yes
4940	49.40	2.97	1.29	1.67	0.76	0.647	1.06	0.612	1.00	1.30	2.000	Yes
4941	49.41	2.97	1.29	1.67	0.76	0.647	1.06	0.612	1.00	1.30	0.796	No
4942	49.42	2.97	1.29	1.67	0.76	0.647	1.06	0.612	1.00	1.30	0.796	No
4943	49.43	2.97	1.29	1.67	0.76	0.646	1.06	0.612	1.00	1.30	0.796	No
4944	49.44	2.97	1.29	1.68	0.76	0.646	1.06	0.612	1.00	1.30	0.795	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
4945	49.45	2.97	1.29	1.68	0.76	0.646	1.06	0.612	1.00	1.30	0.795	No
4946	49.46	2.97	1.29	1.68	0.76	0.646	1.06	0.612	1.00	1.30	0.795	No
4947	49.47	2.97	1.29	1.68	0.76	0.646	1.06	0.612	1.00	1.30	0.795	No
4948	49.48	2.97	1.29	1.68	0.76	0.646	1.06	0.612	1.00	1.30	0.795	No
4949	49.49	2.97	1.29	1.68	0.76	0.646	1.06	0.612	1.00	1.30	0.795	No
4950	49.50	2.97	1.29	1.68	0.76	0.646	1.06	0.611	1.00	1.30	0.795	No
4951	49.51	2.97	1.30	1.68	0.76	0.646	1.06	0.611	1.00	1.30	0.795	No
4952	49.52	2.97	1.30	1.68	0.76	0.646	1.06	0.611	1.00	1.30	0.795	No
4953	49.53	2.97	1.30	1.68	0.76	0.646	1.06	0.611	1.00	1.30	0.795	No
4954	49.54	2.97	1.30	1.68	0.76	0.646	1.06	0.611	1.00	1.30	0.794	No
4955	49.55	2.98	1.30	1.68	0.76	0.646	1.06	0.611	1.00	1.30	0.794	No
4956	49.56	2.98	1.30	1.68	0.76	0.645	1.06	0.611	1.00	1.30	0.794	No
4957	49.57	2.98	1.30	1.68	0.76	0.645	1.06	0.611	1.00	1.30	0.794	No
4958	49.58	2.98	1.30	1.68	0.76	0.645	1.06	0.611	1.00	1.30	0.794	No
4959	49.59	2.98	1.30	1.68	0.76	0.645	1.06	0.611	1.00	1.30	0.794	No
4960	49.60	2.98	1.30	1.68	0.76	0.645	1.06	0.611	1.00	1.30	0.794	No
4961	49.61	2.98	1.30	1.68	0.76	0.645	1.06	0.611	1.00	1.30	0.794	No
4962	49.62	2.98	1.30	1.68	0.76	0.645	1.06	0.611	1.00	1.30	0.794	No
4963	49.63	2.98	1.30	1.68	0.76	0.645	1.06	0.610	1.00	1.30	0.794	No
4964	49.64	2.98	1.30	1.68	0.76	0.645	1.06	0.610	1.00	1.30	0.794	No
4965	49.65	2.98	1.30	1.68	0.76	0.645	1.06	0.610	1.00	1.30	0.793	No
4966	49.66	2.98	1.30	1.68	0.76	0.645	1.06	0.610	1.00	1.30	0.793	No
4967	49.67	2.98	1.30	1.68	0.76	0.645	1.06	0.610	1.00	1.30	0.793	No
4968	49.68	2.98	1.30	1.68	0.76	0.645	1.06	0.610	1.00	1.30	0.793	No
4969	49.69	2.98	1.30	1.68	0.76	0.644	1.06	0.610	1.00	1.30	0.793	No
4970	49.70	2.99	1.30	1.68	0.76	0.644	1.06	0.610	1.00	1.30	0.793	No
4971	49.71	2.99	1.30	1.68	0.76	0.644	1.06	0.610	1.00	1.30	0.793	No
4972	49.72	2.99	1.30	1.68	0.76	0.644	1.06	0.610	1.00	1.30	0.793	No
4973	49.73	2.99	1.30	1.69	0.76	0.644	1.06	0.610	1.00	1.30	0.793	No
4974	49.74	2.99	1.30	1.69	0.76	0.644	1.06	0.610	1.00	1.30	0.793	No
4975	49.75	2.99	1.30	1.69	0.76	0.644	1.06	0.610	1.00	1.30	0.793	No
4976	49.76	2.99	1.30	1.69	0.76	0.644	1.06	0.610	1.00	1.30	0.792	No
4977	49.77	2.99	1.30	1.69	0.76	0.644	1.06	0.609	1.00	1.30	0.792	No
4978	49.78	2.99	1.30	1.69	0.75	0.644	1.06	0.609	1.00	1.30	0.792	No
4979	49.79	2.99	1.30	1.69	0.75	0.644	1.06	0.609	1.00	1.30	0.792	No
4980	49.80	2.99	1.30	1.69	0.75	0.644	1.06	0.609	1.00	1.30	0.792	No
4981	49.81	2.99	1.30	1.69	0.75	0.644	1.06	0.609	1.00	1.30	0.792	No
4982	49.82	2.99	1.30	1.69	0.75	0.643	1.06	0.609	1.00	1.30	0.792	No
4983	49.83	2.99	1.31	1.69	0.75	0.643	1.06	0.609	1.00	1.30	0.792	No
4984	49.84	2.99	1.31	1.69	0.75	0.643	1.06	0.609	1.00	1.30	0.792	No
4985	49.85	2.99	1.31	1.69	0.75	0.643	1.06	0.609	1.00	1.30	0.792	No
4986	49.86	3.00	1.31	1.69	0.75	0.643	1.06	0.609	1.00	1.30	0.791	No
4987	49.87	3.00	1.31	1.69	0.75	0.643	1.06	0.609	1.00	1.30	0.791	No
4988	49.88	3.00	1.31	1.69	0.75	0.643	1.06	0.609	1.00	1.30	0.791	No
4989	49.89	3.00	1.31	1.69	0.75	0.643	1.06	0.609	1.00	1.30	0.791	No
4990	49.90	3.00	1.31	1.69	0.75	0.643	1.06	0.609	1.00	1.30	0.791	No
4991	49.91	3.00	1.31	1.69	0.75	0.643	1.06	0.608	1.00	1.30	0.791	No
4992	49.92	3.00	1.31	1.69	0.75	0.643	1.06	0.608	1.00	1.30	0.791	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
4993	49.93	3.00	1.31	1.69	0.75	0.643	1.06	0.608	1.00	1.30	0.791	No
4994	49.94	3.00	1.31	1.69	0.75	0.643	1.06	0.608	1.00	1.30	0.791	No
4995	49.95	3.00	1.31	1.69	0.75	0.642	1.06	0.608	1.00	1.30	0.791	No
4996	49.96	3.00	1.31	1.69	0.75	0.642	1.06	0.608	1.00	1.30	0.791	No
4997	49.97	3.00	1.31	1.69	0.75	0.642	1.06	0.608	1.00	1.30	0.790	No
4998	49.98	3.00	1.31	1.69	0.75	0.642	1.06	0.608	1.00	1.30	0.790	No
4999	49.99	3.00	1.31	1.69	0.75	0.642	1.06	0.608	1.00	1.30	0.790	No
5000	50.00	3.00	1.31	1.69	0.75	0.642	1.06	0.608	1.00	1.30	0.790	No

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
 σ_v : Total overburden pressure at test point (tsf)
 u_0 : Water pressure at test point (tsf)
 σ_v' : Effective overburden pressure based on GWT during earthquake (tsf)
 r_d : Nonlinear shear mass factor
 CSR: Cyclic Stress Ratio
 MSF: Magnitude Scaling Factor
 CSR_{eq} : CSR adjusted for M=7.5
 K_σ : Effective overburden stress factor
 CSR*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::												
Point ID	Depth (ft)	q _k (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1	0.01	30.91	2.20	1.47	0.69	58.42	1.61	93.96	4.000	No	No	2.00
2	0.02	30.75	2.19	1.45	0.69	58.11	1.60	93.07	4.000	No	No	2.00
3	0.03	30.52	2.19	1.42	0.68	57.69	1.59	91.83	4.000	No	No	2.00
4	0.04	30.24	2.19	1.39	0.68	57.15	1.59	90.71	4.000	No	No	2.00
5	0.05	29.79	2.19	1.37	0.68	56.30	1.59	89.54	4.000	No	No	2.00
6	0.06	29.13	2.19	1.35	0.69	55.05	1.60	88.15	4.000	No	No	2.00
7	0.07	28.30	2.20	1.34	0.69	53.49	1.62	86.52	4.000	No	No	2.00
8	0.08	27.40	2.21	1.32	0.69	51.78	1.64	84.76	4.000	No	No	2.00
9	0.09	26.46	2.22	1.30	0.70	50.01	1.66	82.96	4.000	No	No	2.00
10	0.10	25.55	2.23	1.28	0.70	48.28	1.68	81.21	4.000	No	No	2.00
11	0.11	24.69	2.23	1.27	0.70	46.66	1.71	79.61	4.000	No	No	2.00
12	0.12	23.95	2.24	1.25	0.70	45.26	1.73	78.24	4.000	No	No	2.00
13	0.13	23.54	2.25	1.25	0.71	44.48	1.75	77.73	4.000	No	No	2.00
14	0.14	23.44	2.25	1.27	0.71	44.29	1.76	78.09	4.000	No	No	2.00
15	0.15	23.59	2.26	1.30	0.71	44.58	1.78	79.27	4.000	No	No	2.00
16	0.16	23.77	2.26	1.34	0.71	44.92	1.79	80.62	4.000	No	No	2.00
17	0.17	23.97	2.27	1.39	0.71	45.28	1.81	82.08	4.000	No	No	2.00
18	0.18	24.16	2.27	1.43	0.72	45.65	1.83	83.57	4.000	No	No	2.00
19	0.19	24.35	2.28	1.47	0.72	46.01	1.85	85.01	4.000	No	No	2.00
20	0.20	24.52	2.28	1.51	0.72	46.33	1.86	86.33	4.000	No	No	2.00
21	0.21	24.72	2.29	1.54	0.72	46.70	1.87	87.52	4.000	No	No	2.00
22	0.22	25.06	2.29	1.57	0.72	47.34	1.88	88.80	4.000	No	No	2.00
23	0.23	25.60	2.28	1.60	0.72	48.37	1.87	90.35	4.000	No	No	2.00
24	0.24	26.34	2.28	1.64	0.72	49.76	1.85	92.28	4.000	No	No	2.00
25	0.25	27.16	2.28	1.68	0.72	51.31	1.84	94.45	4.000	No	No	2.00
26	0.26	28.03	2.27	1.72	0.72	52.95	1.83	96.76	4.000	No	No	2.00
27	0.27	28.89	2.27	1.76	0.72	54.58	1.82	99.07	4.000	No	No	2.00
28	0.28	29.71	2.27	1.80	0.71	56.13	1.80	101.29	4.000	No	No	2.00
29	0.29	30.44	2.26	1.83	0.71	57.51	1.80	103.27	4.000	No	No	2.00
30	0.30	31.08	2.26	1.86	0.71	58.72	1.79	104.90	4.000	No	No	2.00
31	0.31	31.72	2.26	1.87	0.71	59.92	1.77	106.31	4.000	No	No	2.00
32	0.32	32.43	2.25	1.89	0.71	61.27	1.76	107.71	4.000	No	No	2.00
33	0.33	33.28	2.25	1.90	0.71	62.86	1.74	109.31	4.000	No	No	2.00
34	0.34	34.20	2.24	1.92	0.70	64.61	1.72	111.08	4.000	No	No	2.00
35	0.35	35.15	2.23	1.93	0.70	66.40	1.70	112.92	4.000	No	No	2.00
36	0.36	36.09	2.23	1.95	0.70	68.17	1.68	114.75	4.000	No	No	2.00
37	0.37	36.95	2.22	1.96	0.70	69.81	1.67	116.47	4.000	No	No	2.00
38	0.38	37.71	2.22	1.97	0.70	71.24	1.66	117.97	4.000	No	No	2.00
39	0.39	38.38	2.21	1.98	0.69	72.50	1.64	119.18	4.000	No	No	2.00
40	0.40	39.04	2.21	1.98	0.69	73.76	1.63	120.26	4.000	No	No	2.00
41	0.41	39.80	2.20	1.98	0.69	75.19	1.61	121.37	4.000	No	No	2.00
42	0.42	40.67	2.19	1.98	0.69	76.83	1.60	122.67	4.000	No	No	2.00
43	0.43	41.60	2.19	1.97	0.68	78.59	1.58	124.07	4.000	No	No	2.00
44	0.44	42.55	2.18	1.97	0.68	80.37	1.56	125.52	4.000	No	No	2.00
45	0.45	43.46	2.17	1.97	0.68	82.09	1.55	126.93	4.000	No	No	2.00
46	0.46	44.29	2.16	1.96	0.68	83.66	1.53	128.24	4.000	No	No	2.00
47	0.47	44.98	2.16	1.96	0.67	84.98	1.52	129.36	4.000	No	No	2.00
48	0.48	45.59	2.16	1.96	0.67	86.13	1.51	130.41	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
49	0.49	46.19	2.15	1.97	0.67	87.26	1.51	131.53	4.000	No	No	2.00
50	0.50	46.87	2.15	1.97	0.67	88.55	1.50	132.83	4.000	No	No	2.00
51	0.51	47.63	2.14	1.98	0.67	89.98	1.49	134.29	4.000	No	No	2.00
52	0.52	48.43	2.14	1.98	0.67	91.48	1.48	135.84	4.000	No	No	2.00
53	0.53	49.22	2.14	1.99	0.67	92.99	1.48	137.39	4.000	No	No	2.00
54	0.54	49.98	2.13	2.00	0.66	94.41	1.47	138.87	4.000	No	No	2.00
55	0.55	50.65	2.13	2.00	0.66	95.67	1.47	140.19	4.000	No	No	2.00
56	0.56	51.19	2.13	2.01	0.66	96.70	1.46	141.28	4.000	No	No	2.00
57	0.57	51.66	2.12	2.01	0.66	97.59	1.46	142.26	4.000	No	No	2.00
58	0.58	52.12	2.12	2.02	0.66	98.45	1.46	143.26	4.000	No	No	2.00
59	0.59	52.64	2.12	2.03	0.66	99.44	1.45	144.41	4.000	No	No	2.00
60	0.60	53.21	2.12	2.04	0.66	100.51	1.45	145.66	4.000	No	No	2.00
61	0.61	53.80	2.12	2.05	0.66	101.62	1.45	146.96	4.000	No	No	2.00
62	0.62	54.37	2.12	2.06	0.66	102.71	1.44	148.24	4.000	No	No	2.00
63	0.63	54.91	2.11	2.06	0.66	103.72	1.44	149.43	4.000	No	No	2.00
64	0.64	55.37	2.11	2.07	0.66	104.59	1.44	150.45	4.000	No	No	2.00
65	0.65	55.71	2.11	2.08	0.66	105.24	1.44	151.21	4.000	No	No	2.00
66	0.66	55.98	2.11	2.08	0.66	105.74	1.44	151.78	4.000	No	No	2.00
67	0.67	56.22	2.11	2.08	0.66	106.19	1.43	152.28	4.000	No	No	2.00
68	0.68	56.49	2.11	2.09	0.66	106.70	1.43	152.85	4.000	No	No	2.00
69	0.69	56.78	2.11	2.09	0.66	107.24	1.43	153.46	4.000	No	No	2.00
70	0.70	57.07	2.11	2.09	0.65	107.80	1.43	154.08	4.000	No	No	2.00
71	0.71	57.35	2.11	2.10	0.65	108.33	1.43	154.67	4.000	No	No	2.00
72	0.72	57.61	2.11	2.10	0.65	108.81	1.43	155.21	4.000	No	No	2.00
73	0.73	57.82	2.10	2.10	0.65	109.20	1.43	155.64	4.000	No	No	2.00
74	0.74	57.97	2.10	2.10	0.65	109.49	1.42	155.93	4.000	No	No	2.00
75	0.75	58.09	2.10	2.10	0.65	109.71	1.42	156.11	4.000	No	No	2.00
76	0.76	58.20	2.10	2.10	0.65	109.92	1.42	156.25	4.000	No	No	2.00
77	0.77	58.33	2.10	2.09	0.65	110.16	1.42	156.41	4.000	No	No	2.00
78	0.78	58.46	2.10	2.09	0.65	110.41	1.42	156.58	4.000	No	No	2.00
79	0.79	58.59	2.10	2.09	0.65	110.66	1.42	156.75	4.000	No	No	2.00
80	0.80	58.72	2.10	2.08	0.65	110.90	1.41	156.91	4.000	No	No	2.00
81	0.81	58.83	2.10	2.08	0.65	111.11	1.41	157.05	4.000	No	No	2.00
82	0.82	58.92	2.10	2.08	0.65	111.28	1.41	157.16	4.000	No	No	2.00
83	0.83	59.00	2.09	2.07	0.65	111.43	1.41	157.22	4.000	No	No	2.00
84	0.84	59.08	2.09	2.07	0.65	111.59	1.41	157.27	4.000	No	No	2.00
85	0.85	59.18	2.09	2.06	0.65	111.77	1.41	157.31	4.000	No	No	2.00
86	0.86	59.28	2.09	2.06	0.65	111.96	1.41	157.35	4.000	No	No	2.00
87	0.87	59.39	2.09	2.05	0.65	112.16	1.40	157.40	4.000	No	No	2.00
88	0.88	59.49	2.09	2.05	0.65	112.36	1.40	157.45	4.000	No	No	2.00
89	0.89	59.59	2.09	2.04	0.65	112.54	1.40	157.50	4.000	No	No	2.00
90	0.90	59.68	2.09	2.04	0.65	112.70	1.40	157.54	4.000	No	No	2.00
91	0.91	59.76	2.08	2.03	0.65	112.86	1.40	157.60	4.000	No	No	2.00
92	0.92	59.87	2.08	2.03	0.65	113.06	1.39	157.69	4.000	No	No	2.00
93	0.93	60.00	2.08	2.02	0.65	113.30	1.39	157.81	4.000	No	No	2.00
94	0.94	60.14	2.08	2.02	0.65	113.58	1.39	157.96	4.000	No	No	2.00
95	0.95	60.30	2.08	2.01	0.64	113.87	1.39	158.11	4.000	No	No	2.00
96	0.96	60.46	2.08	2.00	0.64	114.18	1.39	158.27	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _k (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
97	0.97	60.62	2.07	2.00	0.64	114.47	1.38	158.42	4.000	No	No	2.00
98	0.98	60.76	2.07	1.99	0.64	114.73	1.38	158.56	4.000	No	No	2.00
99	0.99	60.90	2.07	1.99	0.64	114.99	1.38	158.71	4.000	No	No	2.00
100	1.00	61.09	2.07	1.98	0.64	115.36	1.38	158.93	4.000	No	No	2.00
101	1.01	61.36	2.07	1.97	0.64	115.88	1.37	159.26	4.000	No	No	2.00
102	1.02	61.72	2.06	1.96	0.64	116.55	1.37	159.71	4.000	No	No	2.00
103	1.03	62.12	2.06	1.95	0.64	117.29	1.37	160.20	4.000	No	No	2.00
104	1.04	62.53	2.06	1.94	0.64	118.08	1.36	160.73	4.000	No	No	2.00
105	1.05	62.94	2.05	1.92	0.63	118.86	1.36	161.26	4.000	No	No	2.00
106	1.06	63.33	2.05	1.91	0.63	119.59	1.35	161.76	4.000	No	No	2.00
107	1.07	63.68	2.04	1.90	0.63	120.24	1.35	162.21	4.000	No	No	2.00
108	1.08	63.97	2.04	1.89	0.63	120.79	1.35	162.56	4.000	No	No	2.00
109	1.09	64.23	2.04	1.88	0.63	121.29	1.34	162.85	4.000	No	No	2.00
110	1.10	64.51	2.03	1.87	0.63	121.82	1.34	163.10	4.000	No	No	2.00
111	1.11	64.83	2.03	1.85	0.63	122.42	1.33	163.38	4.000	No	No	2.00
112	1.12	65.18	2.03	1.83	0.62	123.08	1.33	163.70	4.000	No	No	2.00
113	1.13	65.54	2.02	1.81	0.62	123.76	1.33	164.03	4.000	No	No	2.00
114	1.14	65.90	2.02	1.80	0.62	124.43	1.32	164.37	4.000	No	No	2.00
115	1.15	66.22	2.01	1.78	0.62	125.04	1.32	164.68	4.000	No	No	2.00
116	1.16	66.50	2.01	1.76	0.62	125.57	1.31	164.95	4.000	No	No	2.00
117	1.17	66.72	2.00	1.75	0.62	125.98	1.31	165.12	4.000	No	No	2.00
118	1.18	66.91	2.00	1.73	0.62	126.33	1.31	165.20	4.000	No	No	2.00
119	1.19	67.09	2.00	1.72	0.61	126.68	1.30	165.22	4.000	No	No	2.00
120	1.20	67.30	1.99	1.70	0.61	127.07	1.30	165.25	4.000	No	No	2.00
121	1.21	67.52	1.99	1.68	0.61	127.48	1.30	165.29	4.000	No	No	2.00
122	1.22	67.74	1.98	1.65	0.61	127.90	1.29	165.33	4.000	No	No	2.00
123	1.23	67.96	1.98	1.63	0.61	128.31	1.29	165.38	4.000	No	No	2.00
124	1.24	68.15	1.97	1.61	0.60	128.68	1.29	165.42	4.000	No	No	2.00
125	1.25	68.30	1.97	1.60	0.60	128.96	1.28	165.45	4.000	No	No	2.00
126	1.26	68.38	1.97	1.59	0.60	129.12	1.28	165.43	4.000	No	No	2.00
127	1.27	68.42	1.96	1.58	0.60	129.18	1.28	165.39	4.000	No	No	2.00
128	1.28	68.43	1.96	1.58	0.60	129.20	1.28	165.31	4.000	No	No	2.00
129	1.29	68.44	1.96	1.57	0.60	129.22	1.28	165.23	4.000	No	No	2.00
130	1.30	68.45	1.96	1.56	0.60	129.24	1.28	165.14	4.000	No	No	2.00
131	1.31	68.47	1.96	1.56	0.60	129.27	1.28	165.05	4.000	No	No	2.00
132	1.32	68.48	1.96	1.55	0.60	129.29	1.28	164.97	4.000	No	No	2.00
133	1.33	68.49	1.96	1.55	0.60	129.31	1.28	164.90	4.000	No	No	2.00
134	1.34	68.46	1.96	1.55	0.60	129.26	1.28	164.81	4.000	No	No	2.00
135	1.35	68.38	1.96	1.55	0.60	129.09	1.28	164.70	4.000	No	No	2.00
136	1.36	68.22	1.96	1.56	0.60	128.80	1.28	164.55	4.000	No	No	2.00
137	1.37	68.03	1.96	1.57	0.60	128.43	1.28	164.37	4.000	No	No	2.00
138	1.38	67.82	1.97	1.58	0.60	128.04	1.28	164.17	4.000	No	No	2.00
139	1.39	67.61	1.97	1.59	0.60	127.64	1.28	163.97	4.000	No	No	2.00
140	1.40	67.40	1.97	1.61	0.61	127.24	1.29	163.77	4.000	No	No	2.00
141	1.41	67.21	1.98	1.62	0.61	126.88	1.29	163.59	4.000	No	No	2.00
142	1.42	67.05	1.98	1.63	0.61	126.57	1.29	163.44	4.000	No	No	2.00
143	1.43	66.95	1.98	1.64	0.61	126.38	1.29	163.40	4.000	No	No	2.00
144	1.44	66.90	1.98	1.65	0.61	126.29	1.29	163.47	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _t (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
145	1.45	66.89	1.99	1.66	0.61	126.27	1.30	163.64	4.000	No	No	2.00
146	1.46	66.88	1.99	1.67	0.61	126.24	1.30	163.83	4.000	No	No	2.00
147	1.47	66.86	1.99	1.68	0.61	126.22	1.30	164.03	4.000	No	No	2.00
148	1.48	66.85	1.99	1.69	0.61	126.19	1.30	164.24	4.000	No	No	2.00
149	1.49	66.84	2.00	1.70	0.61	126.17	1.30	164.44	4.000	No	No	2.00
150	1.50	66.83	2.00	1.72	0.62	126.14	1.31	164.62	4.000	No	No	2.00
151	1.51	66.82	2.00	1.72	0.62	126.12	1.31	164.77	4.000	No	No	2.00
152	1.52	66.80	2.00	1.73	0.62	126.09	1.31	164.89	4.000	No	No	2.00
153	1.53	66.78	2.00	1.74	0.62	126.06	1.31	164.99	4.000	No	No	2.00
154	1.54	66.76	2.00	1.75	0.62	126.02	1.31	165.10	4.000	No	No	2.00
155	1.55	66.73	2.01	1.76	0.62	125.97	1.31	165.22	4.000	No	No	2.00
156	1.56	66.71	2.01	1.77	0.62	125.91	1.31	165.35	4.000	No	No	2.00
157	1.57	66.68	2.01	1.77	0.62	125.86	1.31	165.48	4.000	No	No	2.00
158	1.58	66.66	2.01	1.78	0.62	125.82	1.32	165.60	4.000	No	No	2.00
159	1.59	66.64	2.01	1.79	0.62	125.77	1.32	165.70	4.000	No	No	2.00
160	1.60	66.58	2.01	1.80	0.62	125.67	1.32	165.71	4.000	No	No	2.00
161	1.61	66.47	2.01	1.80	0.62	125.46	1.32	165.56	4.000	No	No	2.00
162	1.62	66.29	2.02	1.80	0.62	125.12	1.32	165.26	4.000	No	No	2.00
163	1.63	66.08	2.02	1.81	0.62	124.71	1.32	164.88	4.000	No	No	2.00
164	1.64	65.84	2.02	1.81	0.62	124.27	1.32	164.48	4.000	No	No	2.00
165	1.65	65.60	2.02	1.81	0.62	123.81	1.33	164.06	4.000	No	No	2.00
166	1.66	65.37	2.02	1.82	0.63	123.37	1.33	163.66	4.000	No	No	2.00
167	1.67	65.15	2.02	1.82	0.63	122.96	1.33	163.28	4.000	No	No	2.00
168	1.68	64.96	2.02	1.82	0.63	122.60	1.33	162.96	4.000	No	No	2.00
169	1.69	64.80	2.03	1.82	0.63	122.29	1.33	162.66	4.000	No	No	2.00
170	1.70	64.63	2.03	1.82	0.63	121.96	1.33	162.33	4.000	No	No	2.00
171	1.71	64.43	2.03	1.82	0.63	121.59	1.33	161.94	4.000	No	No	2.00
172	1.72	64.21	2.03	1.82	0.63	121.17	1.33	161.50	4.000	No	No	2.00
173	1.73	63.97	2.03	1.82	0.63	120.72	1.33	161.03	4.000	No	No	2.00
174	1.74	63.73	2.03	1.82	0.63	120.26	1.34	160.56	4.000	No	No	2.00
175	1.75	63.50	2.03	1.82	0.63	119.83	1.34	160.10	4.000	No	No	2.00
176	1.76	63.29	2.03	1.82	0.63	119.43	1.34	159.69	4.000	No	No	2.00
177	1.77	63.11	2.03	1.82	0.63	119.08	1.34	159.31	4.000	No	No	2.00
178	1.78	62.91	2.03	1.82	0.63	118.71	1.34	158.88	4.000	No	No	2.00
179	1.79	62.68	2.03	1.82	0.63	118.27	1.34	158.35	4.000	No	No	2.00
180	1.80	62.40	2.04	1.81	0.63	117.74	1.34	157.68	4.000	No	No	2.00
181	1.81	62.09	2.04	1.81	0.63	117.15	1.34	156.95	4.000	No	No	2.00
182	1.82	61.76	2.04	1.80	0.63	116.53	1.34	156.18	4.000	No	No	2.00
183	1.83	61.44	2.04	1.79	0.63	115.92	1.34	155.42	4.000	No	No	2.00
184	1.84	61.13	2.04	1.79	0.63	115.35	1.34	154.70	4.000	No	No	2.00
185	1.85	60.87	2.04	1.78	0.63	114.84	1.34	154.07	4.000	No	No	2.00
186	1.86	60.62	2.04	1.78	0.63	114.36	1.34	153.49	4.000	No	No	2.00
187	1.87	60.34	2.04	1.77	0.63	113.85	1.34	152.87	4.000	No	No	2.00
188	1.88	60.02	2.04	1.77	0.63	113.23	1.34	152.13	4.000	No	No	2.00
189	1.89	59.63	2.04	1.76	0.63	112.50	1.34	151.26	4.000	No	No	2.00
190	1.90	59.22	2.04	1.76	0.63	111.71	1.35	150.32	4.000	No	No	2.00
191	1.91	58.79	2.04	1.75	0.63	110.90	1.35	149.36	4.000	No	No	2.00
192	1.92	58.37	2.04	1.74	0.63	110.12	1.35	148.43	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _t (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
193	1.93	57.99	2.04	1.74	0.63	109.39	1.35	147.57	4.000	No	No	2.00
194	1.94	57.65	2.05	1.73	0.63	108.76	1.35	146.82	4.000	No	No	2.00
195	1.95	57.33	2.05	1.73	0.64	108.15	1.35	146.14	4.000	No	No	2.00
196	1.96	56.98	2.05	1.73	0.64	107.48	1.35	145.44	4.000	No	No	2.00
197	1.97	56.56	2.05	1.73	0.64	106.68	1.36	144.63	4.000	No	No	2.00
198	1.98	56.08	2.05	1.73	0.64	105.78	1.36	143.70	4.000	No	No	2.00
199	1.99	55.57	2.06	1.73	0.64	104.81	1.36	142.73	4.000	No	No	2.00
200	2.00	55.06	2.06	1.73	0.64	103.84	1.37	141.74	4.000	No	No	2.00
201	2.01	54.57	2.06	1.73	0.64	102.91	1.37	140.81	4.000	No	No	2.00
202	2.02	54.12	2.06	1.73	0.64	102.07	1.37	139.96	4.000	No	No	2.00
203	2.03	53.73	2.07	1.73	0.64	101.33	1.37	139.23	4.000	No	No	2.00
204	2.04	53.34	2.07	1.73	0.64	100.59	1.38	138.49	4.000	No	No	2.00
205	2.05	52.90	2.07	1.73	0.64	99.75	1.38	137.65	4.000	No	No	2.00
206	2.06	52.37	2.07	1.73	0.65	98.75	1.38	136.65	4.000	No	No	2.00
207	2.07	51.78	2.08	1.73	0.65	97.64	1.39	135.56	4.000	No	No	2.00
208	2.08	51.17	2.08	1.73	0.65	96.48	1.39	134.42	4.000	No	No	2.00
209	2.09	50.56	2.09	1.73	0.65	95.33	1.40	133.29	4.000	No	No	2.00
210	2.10	49.99	2.09	1.73	0.65	94.25	1.40	132.24	4.000	No	No	2.00
211	2.11	49.49	2.09	1.73	0.65	93.30	1.41	131.32	4.000	No	No	2.00
212	2.12	49.07	2.09	1.73	0.65	92.52	1.41	130.54	4.000	No	No	2.00
213	2.13	48.71	2.10	1.73	0.65	91.82	1.41	129.80	4.000	No	No	2.00
214	2.14	48.33	2.10	1.72	0.66	91.11	1.42	129.01	4.000	No	No	2.00
215	2.15	47.89	2.10	1.72	0.66	90.29	1.42	128.09	4.000	No	No	2.00
216	2.16	47.43	2.10	1.71	0.66	89.40	1.42	127.10	4.000	No	No	2.00
217	2.17	46.94	2.10	1.70	0.66	88.49	1.42	126.09	4.000	No	No	2.00
218	2.18	46.48	2.11	1.70	0.66	87.60	1.43	125.11	4.000	No	No	2.00
219	2.19	46.05	2.11	1.69	0.66	86.79	1.43	124.20	4.000	No	No	2.00
220	2.20	45.68	2.11	1.69	0.66	86.09	1.43	123.44	4.000	No	No	2.00
221	2.21	45.37	2.11	1.68	0.66	85.51	1.44	122.79	4.000	No	No	2.00
222	2.22	45.09	2.11	1.68	0.66	84.98	1.44	122.18	4.000	No	No	2.00
223	2.23	44.79	2.11	1.67	0.66	84.40	1.44	121.52	4.000	No	No	2.00
224	2.24	44.44	2.12	1.67	0.66	83.75	1.44	120.78	4.000	No	No	2.00
225	2.25	44.08	2.12	1.66	0.66	83.06	1.44	119.99	4.000	No	No	2.00
226	2.26	43.71	2.12	1.66	0.66	82.37	1.45	119.20	4.000	No	No	2.00
227	2.27	43.36	2.12	1.65	0.66	81.70	1.45	118.44	4.000	No	No	2.00
228	2.28	43.04	2.12	1.65	0.66	81.10	1.45	117.76	4.000	No	No	2.00
229	2.29	42.78	2.12	1.64	0.67	80.60	1.45	117.18	4.000	No	No	2.00
230	2.30	42.53	2.12	1.64	0.67	80.14	1.46	116.65	4.000	No	No	2.00
231	2.31	42.28	2.12	1.63	0.67	79.66	1.46	116.10	4.000	No	No	2.00
232	2.32	41.99	2.13	1.63	0.67	79.11	1.46	115.47	4.000	No	No	2.00
233	2.33	41.67	2.13	1.62	0.67	78.49	1.46	114.77	4.000	No	No	2.00
234	2.34	41.33	2.13	1.61	0.67	77.86	1.46	114.04	4.000	No	No	2.00
235	2.35	41.00	2.13	1.61	0.67	77.23	1.47	113.32	4.000	No	No	2.00
236	2.36	40.69	2.13	1.60	0.67	76.64	1.47	112.65	4.000	No	No	2.00
237	2.37	40.41	2.13	1.60	0.67	76.12	1.47	112.06	4.000	No	No	2.00
238	2.38	40.19	2.13	1.59	0.67	75.69	1.47	111.56	4.000	No	No	2.00
239	2.39	39.98	2.13	1.59	0.67	75.30	1.48	111.11	4.000	No	No	2.00
240	2.40	39.77	2.14	1.58	0.67	74.89	1.48	110.62	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _k (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
241	2.41	39.52	2.14	1.58	0.67	74.43	1.48	110.07	4.000	No	No	2.00
242	2.42	39.25	2.14	1.57	0.67	73.92	1.48	109.47	4.000	No	No	2.00
243	2.43	38.98	2.14	1.57	0.67	73.41	1.48	108.86	4.000	No	No	2.00
244	2.44	38.72	2.14	1.56	0.67	72.91	1.49	108.27	4.000	No	No	2.00
245	2.45	38.47	2.14	1.55	0.67	72.44	1.49	107.72	4.000	No	No	2.00
246	2.46	38.26	2.14	1.55	0.67	72.05	1.49	107.26	4.000	No	No	2.00
247	2.47	38.08	2.14	1.55	0.67	71.69	1.49	106.88	4.000	No	No	2.00
248	2.48	37.89	2.14	1.55	0.67	71.33	1.49	106.54	4.000	No	No	2.00
249	2.49	37.67	2.15	1.55	0.67	70.92	1.50	106.18	4.000	No	No	2.00
250	2.50	37.42	2.15	1.55	0.68	70.45	1.50	105.77	4.000	No	No	2.00
251	2.51	37.16	2.15	1.55	0.68	69.95	1.51	105.35	4.000	No	No	2.00
252	2.52	36.90	2.15	1.55	0.68	69.45	1.51	104.92	4.000	No	No	2.00
253	2.53	36.64	2.16	1.55	0.68	68.98	1.52	104.51	4.000	No	No	2.00
254	2.54	36.42	2.16	1.55	0.68	68.55	1.52	104.14	4.000	No	No	2.00
255	2.55	36.21	2.16	1.55	0.68	68.16	1.52	103.80	4.000	No	No	2.00
256	2.56	35.99	2.16	1.55	0.68	67.74	1.53	103.42	4.000	No	No	2.00
257	2.57	35.73	2.16	1.54	0.68	67.24	1.53	102.94	4.000	No	No	2.00
258	2.58	35.41	2.17	1.54	0.68	66.63	1.54	102.36	4.000	No	No	2.00
259	2.59	35.05	2.17	1.54	0.68	65.96	1.54	101.73	4.000	No	No	2.00
260	2.60	34.68	2.17	1.53	0.68	65.27	1.55	101.07	4.000	No	No	2.00
261	2.61	34.32	2.17	1.53	0.69	64.58	1.56	100.42	4.000	No	No	2.00
262	2.62	33.98	2.18	1.53	0.69	63.93	1.56	99.82	4.000	No	No	2.00
263	2.63	33.68	2.18	1.53	0.69	63.37	1.57	99.29	4.000	No	No	2.00
264	2.64	33.42	2.18	1.52	0.69	62.88	1.57	98.82	4.000	No	No	2.00
265	2.65	33.17	2.18	1.52	0.69	62.40	1.58	98.33	4.000	No	No	2.00
266	2.66	32.89	2.19	1.52	0.69	61.86	1.58	97.77	4.000	No	No	2.00
267	2.67	32.56	2.19	1.51	0.69	61.24	1.59	97.13	4.000	No	No	2.00
268	2.68	32.21	2.19	1.50	0.69	60.57	1.59	96.44	4.000	No	No	2.00
269	2.69	31.85	2.19	1.50	0.69	59.89	1.60	95.73	4.000	No	No	2.00
270	2.70	31.50	2.20	1.49	0.69	59.23	1.60	95.05	4.000	No	No	2.00
271	2.71	31.17	2.20	1.49	0.70	58.62	1.61	94.42	4.000	No	No	2.00
272	2.72	30.91	2.20	1.48	0.70	58.12	1.62	93.91	4.000	No	No	2.00
273	2.73	30.75	2.20	1.48	0.70	57.82	1.62	93.56	4.000	No	No	2.00
274	2.74	30.68	2.20	1.47	0.70	57.68	1.62	93.33	4.000	No	No	2.00
275	2.75	30.65	2.20	1.47	0.70	57.63	1.62	93.15	4.000	No	No	2.00
276	2.76	30.62	2.20	1.46	0.70	57.57	1.61	92.95	4.000	No	No	2.00
277	2.77	30.59	2.20	1.46	0.70	57.51	1.61	92.74	4.000	No	No	2.00
278	2.78	30.56	2.20	1.45	0.70	57.45	1.61	92.52	4.000	No	No	2.00
279	2.79	30.53	2.20	1.44	0.70	57.39	1.61	92.32	4.000	No	No	2.00
280	2.80	30.50	2.20	1.44	0.69	57.34	1.61	92.14	4.000	No	No	2.00
281	2.81	30.48	2.20	1.43	0.69	57.29	1.61	91.98	4.000	No	No	2.00
282	2.82	30.46	2.20	1.43	0.69	57.25	1.60	91.83	4.000	No	No	2.00
283	2.83	30.44	2.20	1.42	0.69	57.21	1.60	91.68	4.000	No	No	2.00
284	2.84	30.41	2.19	1.42	0.69	57.17	1.60	91.50	4.000	No	No	2.00
285	2.85	30.39	2.19	1.41	0.69	57.12	1.60	91.30	4.000	No	No	2.00
286	2.86	30.36	2.19	1.41	0.69	57.07	1.60	91.10	4.000	No	No	2.00
287	2.87	30.33	2.19	1.40	0.69	57.02	1.59	90.89	4.000	No	No	2.00
288	2.88	30.31	2.19	1.39	0.69	56.97	1.59	90.71	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
289	2.89	30.29	2.19	1.39	0.69	56.93	1.59	90.54	4.000	No	No	2.00
290	2.90	30.25	2.19	1.38	0.69	56.86	1.59	90.34	4.000	No	No	2.00
291	2.91	30.20	2.19	1.38	0.69	56.75	1.59	90.07	4.000	No	No	2.00
292	2.92	30.11	2.19	1.37	0.69	56.60	1.58	89.69	4.000	No	No	2.00
293	2.93	30.02	2.19	1.36	0.69	56.41	1.58	89.24	4.000	No	No	2.00
294	2.94	29.91	2.19	1.34	0.69	56.21	1.58	88.77	4.000	No	No	2.00
295	2.95	29.81	2.18	1.33	0.69	56.01	1.58	88.28	4.000	No	No	2.00
296	2.96	29.70	2.18	1.32	0.69	55.81	1.57	87.81	4.000	No	No	2.00
297	2.97	29.61	2.18	1.31	0.69	55.63	1.57	87.38	4.000	No	No	2.00
298	2.98	29.50	2.18	1.30	0.69	55.43	1.57	86.98	4.000	No	No	2.00
299	2.99	29.28	2.18	1.29	0.69	55.02	1.57	86.43	4.000	No	No	2.00
300	3.00	28.92	2.18	1.28	0.69	54.33	1.58	85.66	4.000	No	No	2.00
301	3.01	28.41	2.19	1.27	0.69	53.36	1.59	84.64	4.000	No	No	2.00
302	3.02	27.83	2.19	1.26	0.69	52.27	1.60	83.50	4.000	No	No	2.00
303	3.03	27.22	2.20	1.25	0.70	51.12	1.61	82.31	4.000	No	No	2.00
304	3.04	26.61	2.20	1.23	0.70	49.96	1.62	81.12	4.000	No	No	2.00
305	3.05	26.03	2.21	1.22	0.70	48.86	1.64	80.00	4.000	No	No	2.00
306	3.06	25.51	2.21	1.21	0.70	47.87	1.65	79.00	4.000	No	No	2.00
307	3.07	25.05	2.22	1.20	0.70	47.00	1.66	78.18	4.000	No	No	2.00
308	3.08	24.59	2.22	1.20	0.71	46.14	1.68	77.47	4.000	No	No	2.00
309	3.09	24.08	2.23	1.20	0.71	45.17	1.70	76.77	4.000	No	No	2.00
310	3.10	23.47	2.24	1.20	0.71	44.02	1.73	76.00	4.000	No	No	2.00
311	3.11	22.80	2.25	1.20	0.72	42.76	1.76	75.17	4.000	No	No	2.00
312	3.12	22.11	2.26	1.20	0.72	41.45	1.79	74.34	4.000	No	No	2.00
313	3.13	21.43	2.27	1.20	0.73	40.15	1.83	73.54	4.000	No	No	2.00
314	3.14	20.79	2.29	1.20	0.73	38.95	1.87	72.81	4.000	No	No	2.00
315	3.15	20.23	2.29	1.20	0.73	37.89	1.91	72.20	4.000	No	No	2.00
316	3.16	19.88	2.30	1.20	0.74	37.22	1.93	71.82	4.000	No	No	2.00
317	3.17	19.72	2.30	1.20	0.74	36.92	1.94	71.65	4.000	No	No	2.00
318	3.18	19.71	2.30	1.20	0.74	36.91	1.94	71.65	4.000	No	No	2.00
319	3.19	19.71	2.30	1.20	0.74	36.91	1.94	71.65	4.000	No	No	2.00
320	3.20	19.71	2.30	1.20	0.74	36.91	1.94	71.65	4.000	No	No	2.00
321	3.21	19.71	2.30	1.20	0.74	36.91	1.94	71.65	4.000	No	No	2.00
322	3.22	19.71	2.30	1.20	0.74	36.90	1.94	71.65	4.000	No	No	2.00
323	3.23	19.71	2.30	1.20	0.74	36.90	1.94	71.65	4.000	No	No	2.00
324	3.24	19.72	2.30	1.20	0.74	36.91	1.94	71.64	4.000	No	No	2.00
325	3.25	19.74	2.30	1.20	0.74	36.95	1.94	71.58	4.000	No	No	2.00
326	3.26	19.79	2.30	1.19	0.74	37.04	1.93	71.48	4.000	No	No	2.00
327	3.27	19.85	2.30	1.19	0.73	37.16	1.92	71.32	4.000	No	No	2.00
328	3.28	19.93	2.30	1.18	0.73	37.31	1.91	71.15	4.000	No	No	2.00
329	3.29	20.01	2.29	1.17	0.73	37.46	1.89	70.96	4.000	No	No	2.00
330	3.30	20.09	2.29	1.16	0.73	37.60	1.88	70.78	4.000	No	No	2.00
331	3.31	20.16	2.29	1.15	0.73	37.75	1.87	70.61	4.000	No	No	2.00
332	3.32	20.23	2.28	1.14	0.73	37.87	1.86	70.46	4.000	No	No	2.00
333	3.33	20.28	2.28	1.13	0.73	37.96	1.85	70.31	4.000	No	No	2.00
334	3.34	20.30	2.28	1.13	0.73	38.01	1.85	70.16	4.000	No	No	2.00
335	3.35	20.31	2.28	1.12	0.73	38.02	1.84	69.96	4.000	No	No	2.00
336	3.36	20.31	2.27	1.11	0.73	38.02	1.83	69.72	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _k (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
337	3.37	20.31	2.27	1.10	0.73	38.02	1.83	69.47	4.000	No	No	2.00
338	3.38	20.31	2.27	1.09	0.72	38.02	1.82	69.20	4.000	No	No	2.00
339	3.39	20.31	2.27	1.08	0.72	38.02	1.81	68.94	4.000	No	No	2.00
340	3.40	20.31	2.27	1.07	0.72	38.01	1.81	68.69	4.000	No	No	2.00
341	3.41	20.31	2.27	1.07	0.72	38.01	1.80	68.48	4.000	No	No	2.00
342	3.42	20.31	2.26	1.06	0.72	38.01	1.80	68.37	4.000	No	No	2.00
343	3.43	20.31	2.26	1.06	0.72	38.01	1.80	68.35	4.000	No	No	2.00
344	3.44	20.31	2.26	1.07	0.72	38.01	1.80	68.42	4.000	No	No	2.00
345	3.45	20.31	2.27	1.07	0.72	38.01	1.80	68.50	4.000	No	No	2.00
346	3.46	20.31	2.27	1.07	0.72	38.01	1.80	68.59	4.000	No	No	2.00
347	3.47	20.31	2.27	1.07	0.72	38.01	1.81	68.67	4.000	No	No	2.00
348	3.48	20.31	2.27	1.08	0.72	38.01	1.81	68.76	4.000	No	No	2.00
349	3.49	20.31	2.27	1.08	0.72	38.01	1.81	68.84	4.000	No	No	2.00
350	3.50	20.32	2.27	1.08	0.72	38.02	1.81	68.92	4.000	No	No	2.00
351	3.51	20.37	2.27	1.09	0.72	38.11	1.81	69.06	4.000	No	No	2.00
352	3.52	20.46	2.27	1.09	0.72	38.29	1.81	69.29	4.000	No	No	2.00
353	3.53	20.59	2.27	1.10	0.72	38.54	1.81	69.59	4.000	No	No	2.00
354	3.54	20.75	2.27	1.10	0.72	38.82	1.80	69.93	4.000	No	No	2.00
355	3.55	20.90	2.26	1.11	0.72	39.12	1.80	70.29	4.000	No	No	2.00
356	3.56	21.06	2.26	1.11	0.72	39.42	1.79	70.65	4.000	No	No	2.00
357	3.57	21.22	2.26	1.12	0.72	39.71	1.79	70.99	4.000	No	No	2.00
358	3.58	21.35	2.26	1.13	0.72	39.96	1.78	71.30	4.000	No	No	2.00
359	3.59	21.48	2.26	1.13	0.72	40.20	1.78	71.53	4.000	No	No	2.00
360	3.60	21.62	2.26	1.13	0.72	40.47	1.77	71.68	4.000	No	No	2.00
361	3.61	21.79	2.25	1.12	0.72	40.80	1.76	71.78	4.000	No	No	2.00
362	3.62	22.01	2.25	1.12	0.72	41.20	1.74	71.88	4.000	No	No	2.00
363	3.63	22.24	2.24	1.11	0.71	41.64	1.73	72.00	4.000	No	No	2.00
364	3.64	22.48	2.24	1.11	0.71	42.09	1.71	72.12	4.000	No	No	2.00
365	3.65	22.71	2.23	1.10	0.71	42.53	1.70	72.25	4.000	No	No	2.00
366	3.66	22.93	2.23	1.09	0.71	42.95	1.68	72.37	4.000	No	No	2.00
367	3.67	23.13	2.22	1.09	0.71	43.31	1.67	72.48	4.000	No	No	2.00
368	3.68	23.28	2.22	1.08	0.71	43.60	1.66	72.55	4.000	No	No	2.00
369	3.69	23.41	2.22	1.08	0.70	43.84	1.66	72.61	4.000	No	No	2.00
370	3.70	23.54	2.21	1.07	0.70	44.08	1.65	72.64	4.000	No	No	2.00
371	3.71	23.68	2.21	1.07	0.70	44.36	1.64	72.68	4.000	No	No	2.00
372	3.72	23.84	2.21	1.06	0.70	44.65	1.63	72.72	4.000	No	No	2.00
373	3.73	24.00	2.20	1.06	0.70	44.96	1.62	72.77	4.000	No	No	2.00
374	3.74	24.15	2.20	1.05	0.70	45.25	1.61	72.83	4.000	No	No	2.00
375	3.75	24.30	2.19	1.04	0.70	45.51	1.60	72.87	4.000	No	No	2.00
376	3.76	24.42	2.19	1.04	0.70	45.75	1.59	72.95	4.000	No	No	2.00
377	3.77	24.56	2.19	1.04	0.69	46.00	1.59	73.12	4.000	No	No	2.00
378	3.78	24.72	2.19	1.04	0.69	46.31	1.59	73.42	4.000	No	No	2.00
379	3.79	24.92	2.19	1.05	0.69	46.69	1.58	73.84	4.000	No	No	2.00
380	3.80	25.15	2.18	1.05	0.69	47.12	1.58	74.31	4.000	No	No	2.00
381	3.81	25.39	2.18	1.06	0.69	47.57	1.57	74.81	4.000	No	No	2.00
382	3.82	25.63	2.18	1.07	0.69	48.02	1.57	75.31	4.000	No	No	2.00
383	3.83	25.85	2.18	1.07	0.69	48.45	1.56	75.78	4.000	No	No	2.00
384	3.84	26.06	2.18	1.08	0.69	48.83	1.56	76.21	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
385	3.85	26.28	2.18	1.08	0.69	49.26	1.56	76.65	4.000	No	No	2.00
386	3.86	26.59	2.17	1.09	0.69	49.85	1.55	77.22	4.000	No	No	2.00
387	3.87	27.04	2.17	1.09	0.69	50.68	1.54	77.99	4.000	No	No	2.00
388	3.88	27.58	2.16	1.10	0.68	51.70	1.53	78.93	4.000	No	No	2.00
389	3.89	28.17	2.16	1.10	0.68	52.82	1.51	79.98	4.000	No	No	2.00
390	3.90	28.78	2.15	1.11	0.68	53.98	1.50	81.08	4.000	No	No	2.00
391	3.91	29.39	2.14	1.11	0.68	55.12	1.49	82.17	4.000	No	No	2.00
392	3.92	29.95	2.14	1.12	0.68	56.18	1.48	83.19	4.000	No	No	2.00
393	3.93	30.44	2.13	1.12	0.67	57.10	1.47	84.09	4.000	No	No	2.00
394	3.94	30.83	2.13	1.13	0.67	57.85	1.47	84.78	4.000	No	No	2.00
395	3.95	31.19	2.13	1.13	0.67	58.52	1.46	85.35	4.000	No	No	2.00
396	3.96	31.55	2.12	1.12	0.67	59.20	1.45	85.89	4.000	No	No	2.00
397	3.97	31.97	2.12	1.12	0.67	59.99	1.44	86.51	4.000	No	No	2.00
398	3.98	32.41	2.11	1.12	0.66	60.83	1.43	87.19	4.000	No	No	2.00
399	3.99	32.87	2.10	1.11	0.66	61.69	1.42	87.89	4.000	No	No	2.00
400	4.00	33.30	2.10	1.11	0.66	62.51	1.42	88.57	4.000	No	No	2.00
401	4.01	33.70	2.09	1.11	0.66	63.27	1.41	89.20	4.000	No	No	2.00
402	4.02	34.01	2.09	1.11	0.66	63.85	1.40	89.69	4.000	No	No	2.00
403	4.03	34.19	2.09	1.10	0.66	64.18	1.40	89.95	4.000	No	No	2.00
404	4.04	34.25	2.09	1.10	0.66	64.30	1.40	90.00	4.000	No	No	2.00
405	4.05	34.25	2.09	1.10	0.66	64.29	1.40	89.95	4.000	No	No	2.00
406	4.06	34.25	2.09	1.10	0.66	64.29	1.40	89.88	4.000	No	No	2.00
407	4.07	34.25	2.08	1.09	0.66	64.29	1.40	89.82	4.000	No	No	2.00
408	4.08	34.25	2.08	1.09	0.66	64.29	1.40	89.75	4.000	No	No	2.00
409	4.09	34.25	2.08	1.09	0.65	64.29	1.40	89.69	4.000	No	No	2.00
410	4.10	34.25	2.08	1.08	0.65	64.29	1.39	89.64	4.000	No	No	2.00
411	4.11	34.25	2.08	1.08	0.65	64.29	1.39	89.61	4.000	No	No	2.00
412	4.12	34.25	2.08	1.08	0.65	64.29	1.39	89.61	4.000	No	No	2.00
413	4.13	34.25	2.08	1.08	0.65	64.29	1.39	89.65	4.000	No	No	2.00
414	4.14	34.25	2.08	1.09	0.66	64.28	1.40	89.71	4.000	No	No	2.00
415	4.15	34.25	2.08	1.09	0.66	64.28	1.40	89.77	4.000	No	No	2.00
416	4.16	34.25	2.08	1.09	0.66	64.28	1.40	89.84	4.000	No	No	2.00
417	4.17	34.25	2.09	1.10	0.66	64.28	1.40	89.90	4.000	No	No	2.00
418	4.18	34.25	2.09	1.10	0.66	64.28	1.40	89.96	4.000	No	No	2.00
419	4.19	34.25	2.09	1.10	0.66	64.28	1.40	90.01	4.000	No	No	2.00
420	4.20	34.25	2.09	1.11	0.66	64.28	1.40	90.09	4.000	No	No	2.00
421	4.21	34.25	2.09	1.11	0.66	64.28	1.40	90.20	4.000	No	No	2.00
422	4.22	34.25	2.09	1.12	0.66	64.28	1.41	90.36	4.000	No	No	2.00
423	4.23	34.25	2.09	1.13	0.66	64.28	1.41	90.55	4.000	No	No	2.00
424	4.24	34.25	2.10	1.14	0.66	64.27	1.41	90.74	4.000	No	No	2.00
425	4.25	34.25	2.10	1.15	0.66	64.27	1.41	90.95	4.000	No	No	2.00
426	4.26	34.25	2.10	1.16	0.66	64.27	1.42	91.14	4.000	No	No	2.00
427	4.27	34.25	2.10	1.16	0.66	64.27	1.42	91.32	4.000	No	No	2.00
428	4.28	34.25	2.10	1.17	0.66	64.26	1.42	91.47	4.000	No	No	2.00
429	4.29	34.23	2.10	1.18	0.66	64.23	1.43	91.58	4.000	No	No	2.00
430	4.30	34.20	2.11	1.18	0.66	64.17	1.43	91.68	4.000	No	No	2.00
431	4.31	34.15	2.11	1.19	0.67	64.08	1.43	91.78	4.000	No	No	2.00
432	4.32	34.10	2.11	1.20	0.67	63.99	1.44	91.89	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
433	4.33	34.05	2.11	1.21	0.67	63.88	1.44	92.02	4.000	No	No	2.00
434	4.34	33.99	2.12	1.22	0.67	63.78	1.44	92.14	4.000	No	No	2.00
435	4.35	33.94	2.12	1.23	0.67	63.69	1.45	92.26	4.000	No	No	2.00
436	4.36	33.90	2.12	1.24	0.67	63.60	1.45	92.36	4.000	No	No	2.00
437	4.37	33.88	2.12	1.24	0.67	63.56	1.45	92.46	4.000	No	No	2.00
438	4.38	33.89	2.12	1.25	0.67	63.58	1.46	92.57	4.000	No	No	2.00
439	4.39	33.94	2.12	1.25	0.67	63.67	1.46	92.71	4.000	No	No	2.00
440	4.40	33.99	2.12	1.25	0.67	63.78	1.46	92.87	4.000	No	No	2.00
441	4.41	34.06	2.12	1.26	0.67	63.90	1.46	93.05	4.000	No	No	2.00
442	4.42	34.13	2.12	1.26	0.67	64.02	1.46	93.23	4.000	No	No	2.00
443	4.43	34.19	2.12	1.26	0.67	64.15	1.46	93.41	4.000	No	No	2.00
444	4.44	34.25	2.12	1.27	0.67	64.26	1.46	93.58	4.000	No	No	2.00
445	4.45	34.31	2.12	1.27	0.67	64.36	1.46	93.73	4.000	No	No	2.00
446	4.46	34.39	2.12	1.27	0.67	64.52	1.46	93.91	4.000	No	No	2.00
447	4.47	34.53	2.12	1.27	0.67	64.78	1.45	94.14	4.000	No	No	2.00
448	4.48	34.72	2.12	1.27	0.67	65.14	1.45	94.47	4.000	No	No	2.00
449	4.49	34.94	2.12	1.27	0.67	65.56	1.45	94.84	4.000	No	No	2.00
450	4.50	35.18	2.12	1.27	0.67	66.01	1.44	95.24	4.000	No	No	2.00
451	4.51	35.42	2.11	1.27	0.67	66.46	1.44	95.64	4.000	No	No	2.00
452	4.52	35.65	2.11	1.27	0.67	66.90	1.44	96.04	4.000	No	No	2.00
453	4.53	35.86	2.11	1.27	0.67	67.29	1.43	96.40	4.000	No	No	2.00
454	4.54	36.04	2.11	1.27	0.67	67.63	1.43	96.71	4.000	No	No	2.00
455	4.55	36.22	2.11	1.27	0.66	67.96	1.43	97.00	4.000	No	No	2.00
456	4.56	36.41	2.10	1.27	0.66	68.32	1.42	97.33	4.000	No	No	2.00
457	4.57	36.63	2.10	1.27	0.66	68.74	1.42	97.72	4.000	No	No	2.00
458	4.58	36.88	2.10	1.27	0.66	69.22	1.42	98.15	4.000	No	No	2.00
459	4.59	37.15	2.10	1.27	0.66	69.71	1.41	98.61	4.000	No	No	2.00
460	4.60	37.41	2.09	1.27	0.66	70.21	1.41	99.07	4.000	No	No	2.00
461	4.61	37.66	2.09	1.27	0.66	70.67	1.41	99.50	4.000	No	No	2.00
462	4.62	37.88	2.09	1.27	0.66	71.09	1.41	99.89	4.000	No	No	2.00
463	4.63	38.09	2.09	1.27	0.66	71.49	1.40	100.24	4.000	No	No	2.00
464	4.64	38.33	2.09	1.27	0.66	71.94	1.40	100.61	4.000	No	No	2.00
465	4.65	38.63	2.08	1.26	0.66	72.50	1.39	101.05	4.000	No	No	2.00
466	4.66	38.98	2.08	1.26	0.65	73.18	1.39	101.57	4.000	No	No	2.00
467	4.67	39.37	2.07	1.25	0.65	73.91	1.38	102.14	4.000	No	No	2.00
468	4.68	39.77	2.07	1.24	0.65	74.66	1.38	102.74	4.000	No	No	2.00
469	4.69	40.16	2.06	1.24	0.65	75.40	1.37	103.33	4.000	No	No	2.00
470	4.70	40.53	2.06	1.23	0.65	76.09	1.37	103.89	4.000	No	No	2.00
471	4.71	40.84	2.06	1.23	0.65	76.69	1.36	104.37	4.000	No	No	2.00
472	4.72	41.13	2.05	1.22	0.64	77.22	1.36	104.81	4.000	No	No	2.00
473	4.73	41.42	2.05	1.22	0.64	77.77	1.35	105.26	4.000	No	No	2.00
474	4.74	41.75	2.04	1.21	0.64	78.41	1.35	105.80	4.000	No	No	2.00
475	4.75	42.14	2.04	1.21	0.64	79.13	1.34	106.41	4.000	No	No	2.00
476	4.76	42.55	2.04	1.20	0.64	79.91	1.34	107.06	4.000	No	No	2.00
477	4.77	42.96	2.03	1.19	0.64	80.69	1.34	107.73	4.000	No	No	2.00
478	4.78	43.36	2.03	1.19	0.64	81.45	1.33	108.38	4.000	No	No	2.00
479	4.79	43.73	2.02	1.18	0.63	82.13	1.33	108.98	4.000	No	No	2.00
480	4.80	44.04	2.02	1.18	0.63	82.73	1.32	109.51	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _k (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
481	4.81	44.35	2.02	1.17	0.63	83.31	1.32	110.06	4.000	No	No	2.00
482	4.82	44.70	2.01	1.17	0.63	83.96	1.32	110.71	4.000	No	No	2.00
483	4.83	45.11	2.01	1.17	0.63	84.73	1.32	111.50	4.000	No	No	2.00
484	4.84	45.56	2.01	1.17	0.63	85.60	1.31	112.38	4.000	No	No	2.00
485	4.85	46.04	2.00	1.17	0.63	86.50	1.31	113.31	4.000	No	No	2.00
486	4.86	46.52	2.00	1.17	0.63	87.40	1.31	114.24	4.000	No	No	2.00
487	4.87	46.97	2.00	1.17	0.62	88.25	1.30	115.11	4.000	No	No	2.00
488	4.88	47.37	1.99	1.17	0.62	89.00	1.30	115.89	4.000	No	No	2.00
489	4.89	47.73	1.99	1.17	0.62	89.69	1.30	116.61	4.000	No	No	2.00
490	4.90	48.12	1.99	1.17	0.62	90.42	1.30	117.36	4.000	No	No	2.00
491	4.91	48.58	1.99	1.17	0.62	91.29	1.30	118.27	4.000	No	No	2.00
492	4.92	49.12	1.98	1.17	0.62	92.32	1.29	119.33	4.000	No	No	2.00
493	4.93	49.72	1.98	1.17	0.62	93.43	1.29	120.50	4.000	No	No	2.00
494	4.94	50.32	1.97	1.17	0.62	94.58	1.29	121.70	4.000	No	No	2.00
495	4.95	50.92	1.97	1.17	0.61	95.71	1.28	122.87	4.000	No	No	2.00
496	4.96	51.47	1.97	1.17	0.61	96.75	1.28	123.96	4.000	No	No	2.00
497	4.97	51.94	1.96	1.17	0.61	97.64	1.28	124.90	4.000	No	No	2.00
498	4.98	52.33	1.96	1.17	0.61	98.37	1.28	125.66	4.000	No	No	2.00
499	4.99	52.67	1.96	1.17	0.61	99.02	1.28	126.34	4.000	No	No	2.00
500	5.00	53.03	1.96	1.17	0.61	99.69	1.27	127.05	4.000	No	No	2.00
501	5.01	53.44	1.95	1.17	0.61	100.46	1.27	127.85	4.000	No	No	2.00
502	5.02	53.87	1.95	1.17	0.61	101.28	1.27	128.71	4.000	No	No	2.00
503	5.03	54.31	1.95	1.17	0.61	102.11	1.27	129.58	4.000	No	No	2.00
504	5.04	54.74	1.95	1.17	0.61	102.91	1.27	130.42	4.000	No	No	2.00
505	5.05	55.12	1.94	1.17	0.60	103.63	1.27	131.17	4.000	No	No	2.00
506	5.06	55.42	1.94	1.17	0.60	104.20	1.26	131.76	4.000	No	No	2.00
507	5.07	55.62	1.94	1.17	0.60	104.59	1.26	132.13	4.000	No	No	2.00
508	5.08	55.76	1.94	1.17	0.60	104.84	1.26	132.33	4.000	No	No	2.00
509	5.09	55.88	1.94	1.16	0.60	105.07	1.26	132.47	4.000	No	No	2.00
510	5.10	56.01	1.93	1.15	0.60	105.31	1.26	132.62	4.000	No	No	2.00
511	5.11	56.15	1.93	1.15	0.60	105.57	1.26	132.79	4.000	No	No	2.00
512	5.12	56.29	1.93	1.14	0.60	105.83	1.26	132.95	4.000	No	No	2.00
513	5.13	56.42	1.93	1.14	0.60	106.08	1.25	133.10	4.000	No	No	2.00
514	5.14	56.53	1.93	1.13	0.60	106.29	1.25	133.23	4.000	No	No	2.00
515	5.15	56.62	1.92	1.13	0.60	106.47	1.25	133.34	4.000	No	No	2.00
516	5.16	56.70	1.92	1.12	0.60	106.61	1.25	133.44	4.000	No	No	2.00
517	5.17	56.77	1.92	1.12	0.60	106.75	1.25	133.53	4.000	No	No	2.00
518	5.18	56.86	1.92	1.12	0.60	106.91	1.25	133.65	4.000	No	No	2.00
519	5.19	56.95	1.92	1.12	0.60	107.08	1.25	133.77	4.000	No	No	2.00
520	5.20	57.04	1.92	1.11	0.59	107.25	1.25	133.89	4.000	No	No	2.00
521	5.21	57.13	1.92	1.11	0.59	107.42	1.25	134.01	4.000	No	No	2.00
522	5.22	57.22	1.91	1.11	0.59	107.58	1.25	134.13	4.000	No	No	2.00
523	5.23	57.29	1.91	1.10	0.59	107.72	1.25	134.23	4.000	No	No	2.00
524	5.24	57.37	1.91	1.10	0.59	107.86	1.25	134.38	4.000	No	No	2.00
525	5.25	57.45	1.91	1.11	0.59	108.03	1.25	134.60	4.000	No	No	2.00
526	5.26	57.56	1.91	1.11	0.59	108.23	1.25	134.90	4.000	No	No	2.00
527	5.27	57.69	1.92	1.12	0.59	108.46	1.25	135.25	4.000	No	No	2.00
528	5.28	57.82	1.92	1.12	0.59	108.71	1.25	135.62	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
529	5.29	57.95	1.92	1.13	0.59	108.96	1.25	135.99	4.000	No	No	2.00
530	5.30	58.08	1.92	1.14	0.60	109.20	1.25	136.35	4.000	No	No	2.00
531	5.31	58.19	1.92	1.14	0.60	109.42	1.25	136.68	4.000	No	No	2.00
532	5.32	58.27	1.92	1.15	0.60	109.56	1.25	136.92	4.000	No	No	2.00
533	5.33	58.28	1.92	1.15	0.60	109.58	1.25	137.03	4.000	No	No	2.00
534	5.34	58.23	1.92	1.16	0.60	109.48	1.25	137.05	4.000	No	No	2.00
535	5.35	58.14	1.93	1.17	0.60	109.31	1.25	137.01	4.000	No	No	2.00
536	5.36	58.04	1.93	1.18	0.60	109.12	1.26	136.97	4.000	No	No	2.00
537	5.37	57.93	1.93	1.19	0.60	108.91	1.26	136.93	4.000	No	No	2.00
538	5.38	57.82	1.93	1.20	0.60	108.71	1.26	136.88	4.000	No	No	2.00
539	5.39	57.73	1.94	1.20	0.60	108.52	1.26	136.84	4.000	No	No	2.00
540	5.40	57.64	1.94	1.21	0.60	108.36	1.26	136.80	4.000	No	No	2.00
541	5.41	57.56	1.94	1.22	0.60	108.20	1.26	136.74	4.000	No	No	2.00
542	5.42	57.47	1.94	1.22	0.60	108.04	1.26	136.66	4.000	No	No	2.00
543	5.43	57.37	1.94	1.23	0.61	107.85	1.27	136.54	4.000	No	No	2.00
544	5.44	57.25	1.95	1.23	0.61	107.62	1.27	136.40	4.000	No	No	2.00
545	5.45	57.12	1.95	1.24	0.61	107.37	1.27	136.25	4.000	No	No	2.00
546	5.46	56.99	1.95	1.25	0.61	107.12	1.27	136.09	4.000	No	No	2.00
547	5.47	56.86	1.95	1.25	0.61	106.87	1.27	135.94	4.000	No	No	2.00
548	5.48	56.74	1.95	1.26	0.61	106.64	1.27	135.79	4.000	No	No	2.00
549	5.49	56.64	1.96	1.26	0.61	106.45	1.27	135.67	4.000	No	No	2.00
550	5.50	56.58	1.96	1.27	0.61	106.34	1.28	135.60	4.000	No	No	2.00
551	5.51	56.55	1.96	1.27	0.61	106.29	1.28	135.57	4.000	No	No	2.00
552	5.52	56.55	1.96	1.27	0.61	106.29	1.28	135.57	4.000	No	No	2.00
553	5.53	56.55	1.96	1.27	0.61	106.29	1.28	135.57	4.000	No	No	2.00
554	5.54	56.55	1.96	1.27	0.61	106.29	1.28	135.57	4.000	No	No	2.00
555	5.55	56.55	1.96	1.27	0.61	106.29	1.28	135.57	4.000	No	No	2.00
556	5.56	56.55	1.96	1.27	0.61	106.29	1.28	135.57	4.000	No	No	2.00
557	5.57	56.55	1.96	1.27	0.61	106.29	1.28	135.57	4.000	No	No	2.00
558	5.58	56.54	1.96	1.27	0.61	106.26	1.28	135.55	4.000	No	No	2.00
559	5.59	56.50	1.96	1.27	0.61	106.19	1.28	135.47	4.000	No	No	2.00
560	5.60	56.44	1.96	1.27	0.61	106.07	1.28	135.34	4.000	No	No	2.00
561	5.61	56.34	1.96	1.27	0.61	105.89	1.28	135.15	4.000	No	No	2.00
562	5.62	56.24	1.96	1.27	0.61	105.70	1.28	134.95	4.000	No	No	2.00
563	5.63	56.14	1.96	1.27	0.61	105.49	1.28	134.74	4.000	No	No	2.00
564	5.64	56.03	1.96	1.27	0.61	105.29	1.28	134.53	4.000	No	No	2.00
565	5.65	55.93	1.96	1.27	0.61	105.10	1.28	134.33	4.000	No	No	2.00
566	5.66	55.84	1.96	1.27	0.61	104.94	1.28	134.15	4.000	No	No	2.00
567	5.67	55.77	1.96	1.27	0.61	104.79	1.28	134.01	4.000	No	No	2.00
568	5.68	55.69	1.96	1.27	0.61	104.65	1.28	133.88	4.000	No	No	2.00
569	5.69	55.61	1.96	1.27	0.61	104.49	1.28	133.76	4.000	No	No	2.00
570	5.70	55.51	1.97	1.27	0.61	104.31	1.28	133.62	4.000	No	No	2.00
571	5.71	55.41	1.97	1.28	0.61	104.11	1.28	133.46	4.000	No	No	2.00
572	5.72	55.30	1.97	1.28	0.62	103.91	1.28	133.30	4.000	No	No	2.00
573	5.73	55.20	1.97	1.28	0.62	103.71	1.28	133.15	4.000	No	No	2.00
574	5.74	55.10	1.97	1.29	0.62	103.53	1.28	133.00	4.000	No	No	2.00
575	5.75	55.02	1.97	1.29	0.62	103.38	1.29	132.89	4.000	No	No	2.00
576	5.76	54.98	1.97	1.29	0.62	103.29	1.29	132.83	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
577	5.77	54.96	1.97	1.29	0.62	103.25	1.29	132.83	4.000	No	No	2.00
578	5.78	54.96	1.97	1.30	0.62	103.25	1.29	132.87	4.000	No	No	2.00
579	5.79	54.96	1.97	1.30	0.62	103.25	1.29	132.92	4.000	No	No	2.00
580	5.80	54.96	1.98	1.30	0.62	103.25	1.29	132.98	4.000	No	No	2.00
581	5.81	54.96	1.98	1.31	0.62	103.25	1.29	133.03	4.000	No	No	2.00
582	5.82	54.96	1.98	1.31	0.62	103.25	1.29	133.08	4.000	No	No	2.00
583	5.83	54.96	1.98	1.31	0.62	103.25	1.29	133.13	4.000	No	No	2.00
584	5.84	54.96	1.98	1.31	0.62	103.25	1.29	133.15	4.000	No	No	2.00
585	5.85	54.96	1.98	1.31	0.62	103.24	1.29	133.15	4.000	No	No	2.00
586	5.86	54.96	1.98	1.31	0.62	103.24	1.29	133.12	4.000	No	No	2.00
587	5.87	54.96	1.98	1.31	0.62	103.24	1.29	133.07	4.000	No	No	2.00
588	5.88	54.96	1.98	1.31	0.62	103.24	1.29	133.02	4.000	No	No	2.00
589	5.89	54.96	1.98	1.30	0.62	103.24	1.29	132.97	4.000	No	No	2.00
590	5.90	54.96	1.97	1.30	0.62	103.24	1.29	132.91	4.000	No	No	2.00
591	5.91	54.96	1.97	1.30	0.62	103.24	1.29	132.86	4.000	No	No	2.00
592	5.92	54.96	1.97	1.29	0.62	103.24	1.29	132.82	4.000	No	No	2.00
593	5.93	54.96	1.97	1.29	0.62	103.24	1.29	132.80	4.000	No	No	2.00
594	5.94	54.96	1.97	1.29	0.62	103.23	1.29	132.81	4.000	No	No	2.00
595	5.95	54.96	1.97	1.30	0.62	103.23	1.29	132.84	4.000	No	No	2.00
596	5.96	54.96	1.97	1.30	0.62	103.23	1.29	132.89	4.000	No	No	2.00
597	5.97	54.96	1.98	1.30	0.62	103.23	1.29	132.94	4.000	No	No	2.00
598	5.98	54.96	1.98	1.30	0.62	103.23	1.29	133.00	4.000	No	No	2.00
599	5.99	54.96	1.98	1.31	0.62	103.22	1.29	133.04	4.000	No	No	2.00
600	6.00	54.96	1.98	1.31	0.62	103.15	1.29	133.01	4.000	No	No	2.00
601	6.01	54.96	1.98	1.31	0.62	103.08	1.29	132.98	4.000	No	No	2.00
602	6.02	54.96	1.98	1.32	0.62	103.01	1.29	132.97	4.000	No	No	2.00
603	6.03	54.96	1.98	1.32	0.62	102.95	1.29	132.97	4.000	No	No	2.00
604	6.04	54.96	1.98	1.33	0.62	102.90	1.29	133.01	4.000	No	No	2.00
605	6.05	54.96	1.98	1.33	0.62	102.86	1.29	133.07	4.000	No	No	2.00
606	6.06	54.96	1.98	1.34	0.62	102.82	1.29	133.14	4.000	No	No	2.00
607	6.07	54.96	1.99	1.34	0.62	102.78	1.30	133.21	4.000	No	No	2.00
608	6.08	54.96	1.99	1.35	0.62	102.74	1.30	133.27	4.000	No	No	2.00
609	6.09	54.96	1.99	1.36	0.62	102.69	1.30	133.31	4.000	No	No	2.00
610	6.10	54.97	1.99	1.36	0.62	102.66	1.30	133.34	4.000	No	No	2.00
611	6.11	55.02	1.99	1.36	0.63	102.65	1.30	133.38	4.000	No	No	2.00
612	6.12	55.09	1.99	1.36	0.63	102.70	1.30	133.43	4.000	No	No	2.00
613	6.13	55.20	1.99	1.36	0.63	102.78	1.30	133.52	4.000	No	No	2.00
614	6.14	55.31	1.99	1.36	0.62	102.88	1.30	133.62	4.000	No	No	2.00
615	6.15	55.43	1.99	1.36	0.62	102.99	1.30	133.74	4.000	No	No	2.00
616	6.16	55.55	1.99	1.36	0.62	103.09	1.30	133.85	4.000	No	No	2.00
617	6.17	55.66	1.99	1.36	0.62	103.18	1.30	133.94	4.000	No	No	2.00
618	6.18	55.76	1.99	1.36	0.62	103.25	1.30	134.02	4.000	No	No	2.00
619	6.19	55.89	1.99	1.36	0.62	103.37	1.30	134.11	4.000	No	No	2.00
620	6.20	56.08	1.99	1.36	0.62	103.56	1.30	134.27	4.000	No	No	2.00
621	6.21	56.35	1.98	1.35	0.62	103.88	1.29	134.52	4.000	No	No	2.00
622	6.22	56.67	1.98	1.35	0.62	104.26	1.29	134.82	4.000	No	No	2.00
623	6.23	57.01	1.98	1.34	0.62	104.68	1.29	135.16	4.000	No	No	2.00
624	6.24	57.36	1.98	1.34	0.62	105.12	1.29	135.50	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
625	6.25	57.71	1.97	1.33	0.62	105.53	1.29	135.83	4.000	No	No	2.00
626	6.26	58.02	1.97	1.32	0.62	105.91	1.29	136.13	4.000	No	No	2.00
627	6.27	58.31	1.97	1.32	0.62	106.25	1.28	136.40	4.000	No	No	2.00
628	6.28	58.66	1.97	1.31	0.62	106.69	1.28	136.80	4.000	No	No	2.00
629	6.29	59.14	1.96	1.31	0.62	107.34	1.28	137.40	4.000	No	No	2.00
630	6.30	59.77	1.96	1.30	0.61	108.22	1.28	138.24	4.000	No	No	2.00
631	6.31	60.48	1.96	1.30	0.61	109.22	1.27	139.19	4.000	No	No	2.00
632	6.32	61.24	1.95	1.29	0.61	110.29	1.27	140.20	4.000	No	No	2.00
633	6.33	61.99	1.95	1.29	0.61	111.35	1.27	141.22	4.000	No	No	2.00
634	6.34	62.72	1.94	1.28	0.61	112.36	1.27	142.18	4.000	No	No	2.00
635	6.35	63.37	1.94	1.27	0.61	113.26	1.26	143.03	4.000	No	No	2.00
636	6.36	63.96	1.94	1.27	0.61	114.06	1.26	143.80	4.000	No	No	2.00
637	6.37	64.57	1.93	1.27	0.60	114.93	1.26	144.67	4.000	No	No	2.00
638	6.38	65.30	1.93	1.27	0.60	115.98	1.26	145.77	4.000	No	No	2.00
639	6.39	66.18	1.93	1.27	0.60	117.28	1.25	147.12	4.000	No	No	2.00
640	6.40	67.15	1.92	1.27	0.60	118.71	1.25	148.62	4.000	No	No	2.00
641	6.41	68.15	1.92	1.27	0.60	120.20	1.25	150.18	4.000	No	No	2.00
642	6.42	69.15	1.92	1.27	0.60	121.67	1.25	151.71	4.000	No	No	2.00
643	6.43	70.08	1.91	1.27	0.60	123.04	1.24	153.12	4.000	No	No	2.00
644	6.44	70.90	1.91	1.27	0.60	124.22	1.24	154.35	4.000	No	No	2.00
645	6.45	71.61	1.91	1.27	0.60	125.22	1.24	155.39	4.000	No	No	2.00
646	6.46	72.29	1.90	1.27	0.59	126.02	1.24	156.21	4.000	No	No	2.00
647	6.47	73.05	1.90	1.27	0.59	127.09	1.24	157.32	4.000	No	No	2.00
648	6.48	73.92	1.90	1.27	0.59	128.34	1.24	158.60	4.000	No	No	2.00
649	6.49	74.86	1.89	1.27	0.59	129.69	1.23	159.98	4.000	No	No	2.00
650	6.50	75.82	1.89	1.27	0.59	131.07	1.23	161.39	4.000	No	No	2.00
651	6.51	76.75	1.89	1.27	0.59	132.41	1.23	162.75	4.000	No	No	2.00
652	6.52	77.61	1.89	1.27	0.59	133.62	1.23	163.98	4.000	No	No	2.00
653	6.53	78.34	1.88	1.27	0.59	134.64	1.23	165.00	4.000	No	No	2.00
654	6.54	78.96	1.88	1.27	0.58	135.48	1.22	165.86	4.000	No	No	2.00
655	6.55	79.56	1.88	1.27	0.58	136.29	1.22	166.67	4.000	No	No	2.00
656	6.56	80.23	1.88	1.27	0.58	137.20	1.22	167.58	4.000	No	No	2.00
657	6.57	80.98	1.88	1.27	0.58	138.24	1.22	168.62	4.000	No	No	2.00
658	6.58	81.77	1.87	1.27	0.58	139.34	1.22	169.72	4.000	No	No	2.00
659	6.59	82.57	1.87	1.27	0.58	140.45	1.22	170.81	4.000	No	No	2.00
660	6.60	83.33	1.87	1.27	0.58	141.49	1.21	171.85	4.000	No	No	2.00
661	6.61	84.01	1.87	1.27	0.58	142.42	1.21	172.76	4.000	No	No	2.00
662	6.62	84.56	1.86	1.27	0.58	143.14	1.21	173.47	4.000	No	No	2.00
663	6.63	85.00	1.86	1.27	0.58	143.69	1.21	174.00	4.000	No	No	2.00
664	6.64	85.38	1.86	1.27	0.58	144.15	1.21	174.46	4.000	No	No	2.00
665	6.65	85.80	1.86	1.27	0.58	144.68	1.21	174.97	4.000	No	No	2.00
666	6.66	86.26	1.86	1.27	0.58	145.26	1.21	175.54	4.000	No	No	2.00
667	6.67	86.74	1.86	1.27	0.58	145.87	1.21	176.13	4.000	No	No	2.00
668	6.68	87.22	1.86	1.27	0.58	146.47	1.21	176.71	4.000	No	No	2.00
669	6.69	87.66	1.86	1.27	0.58	147.02	1.21	177.24	4.000	No	No	2.00
670	6.70	88.05	1.86	1.27	0.57	147.49	1.20	177.70	4.000	No	No	2.00
671	6.71	88.31	1.85	1.27	0.57	147.77	1.20	177.99	4.000	No	No	2.00
672	6.72	88.46	1.85	1.27	0.57	147.90	1.20	178.15	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
673	6.73	88.53	1.86	1.27	0.58	147.92	1.20	178.24	4.000	No	No	2.00
674	6.74	88.60	1.86	1.27	0.58	147.95	1.21	178.35	4.000	No	No	2.00
675	6.75	88.68	1.86	1.28	0.58	147.99	1.21	178.47	4.000	No	No	2.00
676	6.76	88.76	1.86	1.28	0.58	148.03	1.21	178.60	4.000	No	No	2.00
677	6.77	88.84	1.86	1.28	0.58	148.07	1.21	178.72	4.000	No	No	2.00
678	6.78	88.91	1.86	1.29	0.58	148.09	1.21	178.82	4.000	No	No	2.00
679	6.79	88.95	1.86	1.29	0.58	148.07	1.21	178.88	4.000	No	No	2.00
680	6.80	88.92	1.86	1.29	0.58	147.94	1.21	178.83	4.000	No	No	2.00
681	6.81	88.79	1.86	1.29	0.58	147.69	1.21	178.70	4.000	No	No	2.00
682	6.82	88.59	1.86	1.30	0.58	147.34	1.21	178.49	4.000	No	No	2.00
683	6.83	88.37	1.87	1.31	0.58	146.95	1.21	178.27	4.000	No	No	2.00
684	6.84	88.13	1.87	1.31	0.58	146.55	1.21	178.04	4.000	No	No	2.00
685	6.85	87.89	1.87	1.32	0.58	146.15	1.22	177.80	4.000	No	No	2.00
686	6.86	87.66	1.87	1.32	0.58	145.76	1.22	177.56	4.000	No	No	2.00
687	6.87	87.46	1.87	1.33	0.58	145.41	1.22	177.34	4.000	No	No	2.00
688	6.88	87.26	1.88	1.33	0.58	145.06	1.22	177.11	4.000	No	No	2.00
689	6.89	87.04	1.88	1.34	0.58	144.67	1.22	176.85	4.000	No	No	2.00
690	6.90	86.75	1.88	1.35	0.59	144.20	1.22	176.53	4.000	No	No	2.00
691	6.91	86.40	1.88	1.36	0.59	143.65	1.23	176.17	4.000	No	No	2.00
692	6.92	86.01	1.89	1.36	0.59	143.06	1.23	175.77	4.000	No	No	2.00
693	6.93	85.61	1.89	1.37	0.59	142.45	1.23	175.36	4.000	No	No	2.00
694	6.94	85.22	1.89	1.38	0.59	141.84	1.23	174.94	4.000	No	No	2.00
695	6.95	84.85	1.90	1.39	0.59	141.27	1.24	174.53	4.000	No	No	2.00
696	6.96	84.53	1.90	1.40	0.59	140.75	1.24	174.16	4.000	No	No	2.00
697	6.97	84.25	1.90	1.41	0.59	140.27	1.24	173.80	4.000	No	No	2.00
698	6.98	83.97	1.91	1.41	0.59	139.79	1.24	173.40	4.000	No	No	2.00
699	6.99	83.65	1.91	1.42	0.60	139.26	1.24	172.95	4.000	No	No	2.00
700	7.00	83.29	1.91	1.42	0.60	138.66	1.24	172.43	4.000	No	No	2.00
701	7.01	82.89	1.91	1.43	0.60	138.02	1.25	171.89	4.000	No	No	2.00
702	7.02	82.49	1.92	1.43	0.60	137.37	1.25	171.33	4.000	No	No	2.00
703	7.03	82.10	1.92	1.44	0.60	136.73	1.25	170.79	4.000	No	No	2.00
704	7.04	81.75	1.92	1.45	0.60	136.14	1.25	170.28	4.000	No	No	2.00
705	7.05	81.46	1.92	1.45	0.60	135.64	1.25	169.84	4.000	No	No	2.00
706	7.06	81.25	1.92	1.46	0.60	135.26	1.25	169.52	4.000	No	No	2.00
707	7.07	81.10	1.93	1.46	0.60	134.97	1.25	169.30	4.000	No	No	2.00
708	7.08	80.96	1.93	1.47	0.60	134.71	1.26	169.13	4.000	No	No	2.00
709	7.09	80.81	1.93	1.47	0.60	134.43	1.26	168.95	4.000	No	No	2.00
710	7.10	80.66	1.93	1.48	0.61	134.15	1.26	168.76	4.000	No	No	2.00
711	7.11	80.50	1.93	1.48	0.61	133.86	1.26	168.57	4.000	No	No	2.00
712	7.12	80.34	1.94	1.49	0.61	133.58	1.26	168.38	4.000	No	No	2.00
713	7.13	80.21	1.94	1.49	0.61	133.31	1.26	168.20	4.000	No	No	2.00
714	7.14	80.14	1.94	1.50	0.61	133.15	1.26	168.09	4.000	No	No	2.00
715	7.15	80.19	1.94	1.50	0.61	133.12	1.26	168.10	4.000	No	No	2.00
716	7.16	80.34	1.94	1.50	0.61	133.25	1.26	168.25	4.000	No	No	2.00
717	7.17	80.55	1.94	1.50	0.61	133.46	1.26	168.47	4.000	No	No	2.00
718	7.18	80.78	1.94	1.50	0.61	133.70	1.26	168.73	4.000	No	No	2.00
719	7.19	81.02	1.94	1.50	0.61	133.96	1.26	169.00	4.000	No	No	2.00
720	7.20	81.26	1.94	1.50	0.61	134.21	1.26	169.26	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _k (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
721	7.21	81.48	1.94	1.50	0.61	134.43	1.26	169.50	4.000	No	No	2.00
722	7.22	81.67	1.94	1.50	0.61	134.62	1.26	169.70	4.000	No	No	2.00
723	7.23	81.89	1.94	1.50	0.61	134.83	1.26	169.90	4.000	No	No	2.00
724	7.24	82.17	1.93	1.50	0.61	135.12	1.26	170.15	4.000	No	No	2.00
725	7.25	82.55	1.93	1.49	0.61	135.53	1.26	170.50	4.000	No	No	2.00
726	7.26	82.99	1.93	1.49	0.60	136.03	1.26	170.92	4.000	No	No	2.00
727	7.27	83.46	1.93	1.48	0.60	136.57	1.25	171.37	4.000	No	No	2.00
728	7.28	83.94	1.92	1.47	0.60	137.12	1.25	171.83	4.000	No	No	2.00
729	7.29	84.41	1.92	1.47	0.60	137.65	1.25	172.27	4.000	No	No	2.00
730	7.30	84.83	1.92	1.46	0.60	138.12	1.25	172.66	4.000	No	No	2.00
731	7.31	85.21	1.92	1.46	0.60	138.52	1.25	172.99	4.000	No	No	2.00
732	7.32	85.59	1.92	1.45	0.60	138.94	1.25	173.34	4.000	No	No	2.00
733	7.33	86.03	1.91	1.45	0.60	139.44	1.25	173.77	4.000	No	No	2.00
734	7.34	86.56	1.91	1.44	0.60	140.07	1.24	174.33	4.000	No	No	2.00
735	7.35	87.17	1.91	1.44	0.60	140.80	1.24	174.97	4.000	No	No	2.00
736	7.36	87.80	1.91	1.43	0.60	141.56	1.24	175.64	4.000	No	No	2.00
737	7.37	88.44	1.90	1.42	0.60	142.33	1.24	176.31	4.000	No	No	2.00
738	7.38	89.05	1.90	1.42	0.59	143.05	1.24	176.93	4.000	No	No	2.00
739	7.39	89.59	1.90	1.41	0.59	143.68	1.24	177.47	4.000	No	No	2.00
740	7.40	90.06	1.90	1.41	0.59	144.22	1.23	177.93	4.000	No	No	2.00
741	7.41	90.54	1.89	1.40	0.59	144.76	1.23	178.39	4.000	No	No	2.00
742	7.42	91.08	1.89	1.40	0.59	145.39	1.23	178.93	4.000	No	No	2.00
743	7.43	91.71	1.89	1.39	0.59	146.14	1.23	179.58	4.000	No	No	2.00
744	7.44	92.41	1.88	1.39	0.59	146.98	1.23	180.30	4.000	No	No	2.00
745	7.45	93.13	1.88	1.38	0.59	147.85	1.22	181.03	4.000	No	No	2.00
746	7.46	93.83	1.88	1.37	0.59	148.70	1.22	181.74	4.000	No	No	2.00
747	7.47	94.49	1.88	1.37	0.58	149.49	1.22	182.39	4.000	No	No	2.00
748	7.48	95.07	1.87	1.36	0.58	150.15	1.22	182.94	4.000	No	No	2.00
749	7.49	95.56	1.87	1.36	0.58	150.71	1.22	183.42	4.000	No	No	2.00
750	7.50	96.03	1.87	1.36	0.58	151.26	1.22	183.93	4.000	No	No	2.00
751	7.51	96.54	1.87	1.36	0.58	151.88	1.22	184.55	4.000	No	No	2.00
752	7.52	97.13	1.87	1.36	0.58	152.62	1.21	185.27	4.000	No	No	2.00
753	7.53	97.75	1.87	1.36	0.58	153.41	1.21	186.06	4.000	No	No	2.00
754	7.54	98.39	1.86	1.36	0.58	154.21	1.21	186.85	4.000	No	No	2.00
755	7.55	99.01	1.86	1.36	0.58	154.98	1.21	187.61	4.000	No	No	2.00
756	7.56	99.58	1.86	1.36	0.58	155.68	1.21	188.29	4.000	No	No	2.00
757	7.57	100.07	1.86	1.36	0.58	156.27	1.21	188.87	4.000	No	No	2.00
758	7.58	100.54	1.86	1.36	0.58	156.82	1.21	189.41	4.000	No	No	2.00
759	7.59	101.05	1.86	1.36	0.58	157.43	1.21	190.01	4.000	No	No	2.00
760	7.60	101.65	1.86	1.36	0.58	158.18	1.21	190.74	4.000	No	No	2.00
761	7.61	102.33	1.85	1.36	0.58	159.04	1.20	191.57	4.000	No	No	2.00
762	7.62	103.05	1.85	1.36	0.58	159.94	1.20	192.44	4.000	No	No	2.00
763	7.63	103.77	1.85	1.36	0.58	160.84	1.20	193.31	4.000	No	No	2.00
764	7.64	104.45	1.85	1.36	0.58	161.69	1.20	194.13	4.000	No	No	2.00
765	7.65	105.05	1.85	1.36	0.58	162.43	1.20	194.84	4.000	No	No	2.00
766	7.66	105.55	1.85	1.36	0.57	163.03	1.20	195.44	4.000	No	No	2.00
767	7.67	105.99	1.85	1.36	0.57	163.56	1.20	196.02	4.000	No	No	2.00
768	7.68	106.42	1.85	1.37	0.57	164.11	1.20	196.68	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
769	7.69	106.92	1.85	1.37	0.57	164.75	1.20	197.47	4.000	No	No	2.00
770	7.70	107.46	1.85	1.38	0.57	165.47	1.20	198.35	4.000	No	No	2.00
771	7.71	108.02	1.85	1.38	0.58	166.22	1.20	199.26	4.000	No	No	2.00
772	7.72	108.57	1.85	1.39	0.58	166.95	1.20	200.15	4.000	No	No	2.00
773	7.73	109.09	1.85	1.40	0.58	167.61	1.20	200.97	4.000	No	No	2.00
774	7.74	109.53	1.85	1.40	0.58	168.18	1.20	201.67	4.000	No	No	2.00
775	7.75	109.89	1.85	1.41	0.58	168.62	1.20	202.23	4.000	No	No	2.00
776	7.76	110.21	1.85	1.41	0.58	168.99	1.20	202.73	4.000	No	No	2.00
777	7.77	110.53	1.85	1.42	0.58	169.38	1.20	203.26	4.000	No	No	2.00
778	7.78	110.89	1.85	1.42	0.58	169.84	1.20	203.89	4.000	No	No	2.00
779	7.79	111.29	1.85	1.43	0.58	170.35	1.20	204.57	4.000	No	No	2.00
780	7.80	111.69	1.85	1.43	0.58	170.86	1.20	205.26	4.000	No	No	2.00
781	7.81	112.07	1.85	1.44	0.58	171.35	1.20	205.92	4.000	No	No	2.00
782	7.82	112.43	1.85	1.45	0.58	171.78	1.20	206.51	4.000	No	No	2.00
783	7.83	112.72	1.85	1.45	0.58	172.13	1.20	206.98	4.000	No	No	2.00
784	7.84	112.98	1.85	1.45	0.58	172.39	1.20	207.30	4.000	No	No	2.00
785	7.85	113.22	1.85	1.45	0.58	172.62	1.20	207.55	4.000	No	No	2.00
786	7.86	113.49	1.85	1.45	0.58	172.87	1.20	207.80	4.000	No	No	2.00
787	7.87	113.79	1.85	1.45	0.58	173.18	1.20	208.09	4.000	No	No	2.00
788	7.88	114.11	1.85	1.45	0.58	173.50	1.20	208.41	4.000	No	No	2.00
789	7.89	114.43	1.85	1.45	0.58	173.82	1.20	208.72	4.000	No	No	2.00
790	7.90	114.73	1.85	1.45	0.58	174.12	1.20	209.01	4.000	No	No	2.00
791	7.91	115.00	1.85	1.45	0.58	174.38	1.20	209.25	4.000	No	No	2.00
792	7.92	115.18	1.85	1.45	0.58	174.52	1.20	209.40	4.000	No	No	2.00
793	7.93	115.28	1.85	1.45	0.58	174.54	1.20	209.46	4.000	No	No	2.00
794	7.94	115.30	1.85	1.46	0.58	174.47	1.20	209.47	4.000	No	No	2.00
795	7.95	115.30	1.85	1.46	0.58	174.38	1.20	209.47	4.000	No	No	2.00
796	7.96	115.30	1.85	1.46	0.58	174.29	1.20	209.48	4.000	No	No	2.00
797	7.97	115.30	1.85	1.47	0.58	174.21	1.20	209.49	4.000	No	No	2.00
798	7.98	115.30	1.85	1.47	0.58	174.12	1.20	209.50	4.000	No	No	2.00
799	7.99	115.30	1.85	1.47	0.58	174.03	1.20	209.50	4.000	No	No	2.00
800	8.00	115.30	1.85	1.47	0.58	173.94	1.20	209.49	4.000	No	No	2.00
801	8.01	115.30	1.86	1.48	0.58	173.91	1.20	209.55	4.000	No	No	2.00
802	8.02	115.30	1.86	1.48	0.58	173.89	1.21	209.64	4.000	No	No	2.00
803	8.03	115.30	1.86	1.49	0.58	173.88	1.21	209.79	4.000	No	No	2.00
804	8.04	115.30	1.86	1.49	0.58	173.88	1.21	209.96	4.000	No	No	2.00
805	8.05	115.30	1.86	1.50	0.58	173.89	1.21	210.14	4.000	No	No	2.00
806	8.06	115.30	1.86	1.50	0.58	173.89	1.21	210.33	4.000	No	No	2.00
807	8.07	115.30	1.86	1.51	0.58	173.90	1.21	210.51	4.000	No	No	2.00
808	8.08	115.30	1.86	1.52	0.58	173.89	1.21	210.66	4.000	No	No	2.00
809	8.09	115.32	1.86	1.52	0.58	173.91	1.21	210.79	4.000	No	No	2.00
810	8.10	115.42	1.86	1.52	0.58	174.00	1.21	210.92	4.000	No	No	2.00
811	8.11	115.61	1.86	1.52	0.58	174.19	1.21	211.08	4.000	No	No	2.00
812	8.12	115.89	1.86	1.52	0.58	174.48	1.21	211.29	4.000	No	No	2.00
813	8.13	116.19	1.86	1.51	0.58	174.81	1.21	211.54	4.000	No	No	2.00
814	8.14	116.51	1.86	1.51	0.58	175.16	1.21	211.79	4.000	No	No	2.00
815	8.15	116.83	1.86	1.51	0.58	175.50	1.21	212.04	4.000	No	No	2.00
816	8.16	117.13	1.86	1.51	0.58	175.83	1.21	212.27	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
817	8.17	117.40	1.86	1.50	0.58	176.11	1.21	212.47	4.000	No	No	2.00
818	8.18	117.66	1.86	1.50	0.58	176.38	1.21	212.64	4.000	No	No	2.00
819	8.19	117.98	1.85	1.49	0.58	176.71	1.20	212.82	4.000	No	No	2.00
820	8.20	118.40	1.85	1.49	0.58	177.14	1.20	213.03	4.000	No	No	2.00
821	8.21	118.89	1.85	1.48	0.58	177.68	1.20	213.29	4.000	No	No	2.00
822	8.22	119.44	1.85	1.47	0.58	178.26	1.20	213.56	4.000	No	No	2.00
823	8.23	120.00	1.84	1.46	0.57	178.87	1.20	213.82	4.000	No	No	2.00
824	8.24	120.55	1.84	1.45	0.57	179.45	1.19	214.07	4.000	No	No	2.00
825	8.25	121.06	1.84	1.44	0.57	180.00	1.19	214.28	4.000	No	No	2.00
826	8.26	121.50	1.84	1.44	0.57	180.46	1.19	214.45	4.000	No	No	2.00
827	8.27	121.93	1.83	1.43	0.57	180.92	1.19	214.66	4.000	No	No	2.00
828	8.28	122.41	1.83	1.42	0.57	181.45	1.18	214.96	4.000	No	No	2.00
829	8.29	122.99	1.83	1.42	0.57	182.12	1.18	215.39	4.000	No	No	2.00
830	8.30	123.65	1.83	1.41	0.57	182.90	1.18	215.87	4.000	No	No	2.00
831	8.31	124.36	1.82	1.41	0.57	183.73	1.18	216.38	4.000	No	No	2.00
832	8.32	125.08	1.82	1.40	0.57	184.58	1.18	216.88	4.000	No	No	2.00
833	8.33	125.77	1.82	1.39	0.57	185.39	1.17	217.34	4.000	No	No	2.00
834	8.34	126.40	1.82	1.39	0.56	186.11	1.17	217.75	4.000	No	No	2.00
835	8.35	126.94	1.81	1.38	0.56	186.72	1.17	218.08	4.000	No	No	2.00
836	8.36	127.41	1.81	1.38	0.56	187.26	1.17	218.40	4.000	No	No	2.00
837	8.37	127.89	1.81	1.38	0.56	187.81	1.16	218.76	4.000	No	No	2.00
838	8.38	128.43	1.81	1.38	0.56	188.45	1.16	219.19	4.000	No	No	2.00
839	8.39	129.04	1.81	1.37	0.56	189.18	1.16	219.66	4.000	No	No	2.00
840	8.40	129.68	1.81	1.37	0.56	189.94	1.16	220.16	4.000	No	No	2.00
841	8.41	130.31	1.80	1.37	0.56	190.69	1.16	220.64	4.000	No	No	2.00
842	8.42	130.92	1.80	1.36	0.56	191.40	1.16	221.09	4.000	No	No	2.00
843	8.43	131.45	1.80	1.36	0.56	192.03	1.15	221.48	4.000	No	No	2.00
844	8.44	131.87	1.80	1.36	0.56	192.51	1.15	221.78	4.000	No	No	2.00
845	8.45	132.22	1.80	1.36	0.56	192.90	1.15	222.06	4.000	No	No	2.00
846	8.46	132.54	1.80	1.36	0.56	193.27	1.15	222.35	4.000	No	No	2.00
847	8.47	132.89	1.80	1.36	0.56	193.68	1.15	222.69	4.000	No	No	2.00
848	8.48	133.28	1.80	1.36	0.56	194.14	1.15	223.07	4.000	No	No	2.00
849	8.49	133.68	1.80	1.36	0.56	194.61	1.15	223.45	4.000	No	No	2.00
850	8.50	134.07	1.80	1.36	0.56	195.08	1.15	223.83	4.000	No	No	2.00
851	8.51	134.44	1.79	1.36	0.56	195.50	1.15	224.17	4.000	No	No	2.00
852	8.52	134.75	1.79	1.36	0.56	195.86	1.15	224.46	4.000	No	No	2.00
853	8.53	134.99	1.79	1.36	0.56	196.12	1.15	224.67	4.000	No	No	2.00
854	8.54	135.19	1.79	1.36	0.56	196.32	1.15	224.84	4.000	No	No	2.00
855	8.55	135.39	1.79	1.36	0.56	196.52	1.14	225.00	4.000	No	No	2.00
856	8.56	135.61	1.79	1.36	0.56	196.75	1.14	225.18	4.000	No	No	2.00
857	8.57	135.85	1.79	1.36	0.56	197.00	1.14	225.39	4.000	No	No	2.00
858	8.58	136.09	1.79	1.36	0.56	197.26	1.14	225.59	4.000	No	No	2.00
859	8.59	136.32	1.79	1.36	0.56	197.50	1.14	225.79	4.000	No	No	2.00
860	8.60	136.53	1.79	1.36	0.56	197.72	1.14	225.96	4.000	No	No	2.00
861	8.61	136.69	1.79	1.36	0.56	197.88	1.14	226.09	4.000	No	No	2.00
862	8.62	136.81	1.79	1.36	0.56	197.96	1.14	226.16	4.000	No	No	2.00
863	8.63	136.88	1.79	1.36	0.56	198.00	1.14	226.19	4.000	No	No	2.00
864	8.64	136.95	1.79	1.36	0.56	198.03	1.14	226.21	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
865	8.65	137.03	1.79	1.36	0.56	198.06	1.14	226.24	4.000	No	No	2.00
866	8.66	137.11	1.79	1.36	0.56	198.11	1.14	226.27	4.000	No	No	2.00
867	8.67	137.19	1.79	1.36	0.56	198.15	1.14	226.30	4.000	No	No	2.00
868	8.68	137.26	1.79	1.36	0.56	198.18	1.14	226.33	4.000	No	No	2.00
869	8.69	137.33	1.79	1.36	0.56	198.20	1.14	226.35	4.000	No	No	2.00
870	8.70	137.37	1.79	1.36	0.56	198.19	1.14	226.28	4.000	No	No	2.00
871	8.71	137.40	1.79	1.35	0.55	198.12	1.14	226.07	4.000	No	No	2.00
872	8.72	137.40	1.79	1.35	0.55	198.00	1.14	225.71	4.000	No	No	2.00
873	8.73	137.40	1.79	1.34	0.55	197.86	1.14	225.27	4.000	No	No	2.00
874	8.74	137.40	1.79	1.34	0.55	197.71	1.14	224.79	4.000	No	No	2.00
875	8.75	137.40	1.79	1.33	0.55	197.57	1.14	224.30	4.000	No	No	2.00
876	8.76	137.40	1.78	1.33	0.55	197.42	1.13	223.81	4.000	No	No	2.00
877	8.77	137.40	1.78	1.32	0.55	197.28	1.13	223.35	4.000	No	No	2.00
878	8.78	137.39	1.78	1.32	0.55	197.15	1.13	222.94	4.000	No	No	2.00
879	8.79	137.36	1.78	1.31	0.55	196.99	1.13	222.59	4.000	No	No	2.00
880	8.80	137.27	1.78	1.31	0.55	196.78	1.13	222.25	4.000	No	No	2.00
881	8.81	137.14	1.78	1.31	0.55	196.51	1.13	221.88	4.000	No	No	2.00
882	8.82	136.99	1.78	1.30	0.55	196.21	1.13	221.47	4.000	No	No	2.00
883	8.83	136.84	1.78	1.30	0.55	195.89	1.13	221.04	4.000	No	No	2.00
884	8.84	136.68	1.78	1.30	0.55	195.58	1.13	220.60	4.000	No	No	2.00
885	8.85	136.52	1.78	1.29	0.55	195.27	1.13	220.18	4.000	No	No	2.00
886	8.86	136.38	1.78	1.29	0.55	194.99	1.13	219.79	4.000	No	No	2.00
887	8.87	136.25	1.78	1.29	0.55	194.73	1.13	219.50	4.000	No	No	2.00
888	8.88	136.09	1.78	1.29	0.55	194.46	1.13	219.36	4.000	No	No	2.00
889	8.89	135.87	1.78	1.29	0.55	194.16	1.13	219.36	4.000	No	No	2.00
890	8.90	135.59	1.78	1.30	0.55	193.80	1.13	219.43	4.000	No	No	2.00
891	8.91	135.29	1.78	1.31	0.55	193.41	1.13	219.50	4.000	No	No	2.00
892	8.92	134.97	1.79	1.31	0.55	193.01	1.14	219.56	4.000	No	No	2.00
893	8.93	134.65	1.79	1.32	0.55	192.60	1.14	219.61	4.000	No	No	2.00
894	8.94	134.35	1.79	1.32	0.56	192.22	1.14	219.64	4.000	No	No	2.00
895	8.95	134.09	1.79	1.33	0.56	191.87	1.14	219.66	4.000	No	No	2.00
896	8.96	133.85	1.79	1.33	0.56	191.54	1.15	219.61	4.000	No	No	2.00
897	8.97	133.59	1.80	1.34	0.56	191.17	1.15	219.48	4.000	No	No	2.00
898	8.98	133.29	1.80	1.34	0.56	190.74	1.15	219.26	4.000	No	No	2.00
899	8.99	132.93	1.80	1.34	0.56	190.23	1.15	219.00	4.000	No	No	2.00
900	9.00	132.54	1.80	1.35	0.56	189.69	1.15	218.71	4.000	No	No	2.00
901	9.01	132.14	1.80	1.35	0.56	189.14	1.15	218.41	4.000	No	No	2.00
902	9.02	131.75	1.80	1.35	0.56	188.59	1.16	218.12	4.000	No	No	2.00
903	9.03	131.38	1.80	1.35	0.56	188.09	1.16	217.83	4.000	No	No	2.00
904	9.04	131.07	1.81	1.36	0.56	187.64	1.16	217.58	4.000	No	No	2.00
905	9.05	130.81	1.81	1.36	0.56	187.27	1.16	217.41	4.000	No	No	2.00
906	9.06	130.57	1.81	1.36	0.56	186.93	1.16	217.31	4.000	No	No	2.00
907	9.07	130.31	1.81	1.37	0.56	186.59	1.16	217.25	4.000	No	No	2.00
908	9.08	130.01	1.81	1.37	0.56	186.20	1.17	217.18	4.000	No	No	2.00
909	9.09	129.70	1.81	1.38	0.56	185.79	1.17	217.10	4.000	No	No	2.00
910	9.10	129.38	1.82	1.39	0.57	185.38	1.17	217.02	4.000	No	No	2.00
911	9.11	129.07	1.82	1.39	0.57	184.98	1.17	216.92	4.000	No	No	2.00
912	9.12	128.79	1.82	1.40	0.57	184.61	1.17	216.82	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
913	9.13	128.58	1.82	1.40	0.57	184.31	1.18	216.75	4.000	No	No	2.00
914	9.14	128.44	1.82	1.41	0.57	184.11	1.18	216.75	4.000	No	No	2.00
915	9.15	128.35	1.82	1.41	0.57	183.99	1.18	216.83	4.000	No	No	2.00
916	9.16	128.29	1.83	1.42	0.57	183.90	1.18	216.97	4.000	No	No	2.00
917	9.17	128.21	1.83	1.42	0.57	183.81	1.18	217.12	4.000	No	No	2.00
918	9.18	128.13	1.83	1.43	0.57	183.71	1.18	217.27	4.000	No	No	2.00
919	9.19	128.05	1.83	1.44	0.57	183.61	1.18	217.42	4.000	No	No	2.00
920	9.20	127.98	1.83	1.44	0.57	183.51	1.19	217.55	4.000	No	No	2.00
921	9.21	127.91	1.83	1.45	0.57	183.42	1.19	217.66	4.000	No	No	2.00
922	9.22	127.89	1.83	1.45	0.57	183.38	1.19	217.74	4.000	No	No	2.00
923	9.23	127.94	1.83	1.45	0.57	183.40	1.19	217.82	4.000	No	No	2.00
924	9.24	128.06	1.83	1.45	0.57	183.49	1.19	217.92	4.000	No	No	2.00
925	9.25	128.20	1.83	1.45	0.57	183.62	1.19	218.04	4.000	No	No	2.00
926	9.26	128.36	1.83	1.45	0.57	183.77	1.19	218.18	4.000	No	No	2.00
927	9.27	128.52	1.83	1.45	0.57	183.92	1.19	218.32	4.000	No	No	2.00
928	9.28	128.67	1.83	1.45	0.57	184.07	1.19	218.46	4.000	No	No	2.00
929	9.29	128.82	1.83	1.45	0.57	184.20	1.19	218.58	4.000	No	No	2.00
930	9.30	128.95	1.83	1.45	0.57	184.32	1.19	218.69	4.000	No	No	2.00
931	9.31	129.17	1.83	1.45	0.57	184.53	1.19	218.82	4.000	No	No	2.00
932	9.32	129.49	1.83	1.45	0.57	184.86	1.18	219.01	4.000	No	No	2.00
933	9.33	129.95	1.83	1.44	0.57	185.36	1.18	219.26	4.000	No	No	2.00
934	9.34	130.47	1.83	1.44	0.57	185.92	1.18	219.55	4.000	No	No	2.00
935	9.35	131.03	1.82	1.43	0.57	186.53	1.18	219.86	4.000	No	No	2.00
936	9.36	131.59	1.82	1.42	0.57	187.14	1.18	220.15	4.000	No	No	2.00
937	9.37	132.12	1.82	1.42	0.57	187.72	1.17	220.42	4.000	No	No	2.00
938	9.38	132.61	1.82	1.41	0.57	188.24	1.17	220.65	4.000	No	No	2.00
939	9.39	133.04	1.82	1.41	0.57	188.70	1.17	220.84	4.000	No	No	2.00
940	9.40	133.51	1.81	1.40	0.57	189.20	1.17	221.04	4.000	No	No	2.00
941	9.41	134.08	1.81	1.40	0.56	189.81	1.17	221.27	4.000	No	No	2.00
942	9.42	134.77	1.81	1.39	0.56	190.57	1.16	221.54	4.000	No	No	2.00
943	9.43	135.54	1.81	1.38	0.56	191.41	1.16	221.82	4.000	No	No	2.00
944	9.44	136.33	1.80	1.37	0.56	192.28	1.16	222.09	4.000	No	No	2.00
945	9.45	137.13	1.80	1.36	0.56	193.15	1.15	222.32	4.000	No	No	2.00
946	9.46	137.87	1.80	1.35	0.56	193.96	1.15	222.51	4.000	No	No	2.00
947	9.47	138.53	1.79	1.34	0.56	194.67	1.14	222.65	4.000	No	No	2.00
948	9.48	139.09	1.79	1.34	0.56	195.26	1.14	222.77	4.000	No	No	2.00
949	9.49	139.61	1.79	1.33	0.56	195.82	1.14	222.90	4.000	No	No	2.00
950	9.50	140.17	1.79	1.33	0.55	196.43	1.14	223.08	4.000	No	No	2.00
951	9.51	140.82	1.78	1.32	0.55	197.14	1.13	223.28	4.000	No	No	2.00
952	9.52	141.52	1.78	1.32	0.55	197.92	1.13	223.48	4.000	No	No	2.00
953	9.53	142.24	1.78	1.31	0.55	198.72	1.13	223.67	4.000	No	No	2.00
954	9.54	142.94	1.78	1.30	0.55	199.49	1.12	223.83	4.000	No	No	2.00
955	9.55	143.59	1.77	1.30	0.55	200.20	1.12	223.96	4.000	No	No	2.00
956	9.56	144.09	1.77	1.29	0.55	200.72	1.12	223.98	4.000	No	No	2.00
957	9.57	144.10	1.77	1.29	0.55	200.60	1.11	223.53	4.000	No	No	2.00
958	9.58	143.60	1.77	1.28	0.55	199.81	1.11	222.53	4.000	No	No	2.00
959	9.59	142.65	1.77	1.27	0.55	198.42	1.11	220.99	4.000	No	No	2.00
960	9.60	141.56	1.77	1.26	0.55	196.84	1.11	219.25	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
961	9.61	140.42	1.77	1.26	0.55	195.18	1.11	217.42	4.000	No	No	2.00
962	9.62	139.26	1.77	1.25	0.55	193.50	1.11	215.57	4.000	No	No	2.00
963	9.63	138.15	1.77	1.24	0.55	191.90	1.11	213.81	4.000	No	No	2.00
964	9.64	137.15	1.77	1.23	0.55	190.44	1.11	212.22	4.000	No	No	2.00
965	9.65	136.42	1.77	1.22	0.55	189.36	1.11	211.00	4.000	No	No	2.00
966	9.66	136.05	1.77	1.22	0.55	188.76	1.11	210.20	4.000	No	No	2.00
967	9.67	135.99	1.77	1.21	0.55	188.56	1.11	209.71	4.000	No	No	2.00
968	9.68	136.06	1.77	1.21	0.55	188.53	1.11	209.29	4.000	No	No	2.00
969	9.69	136.14	1.77	1.20	0.55	188.49	1.11	208.83	4.000	No	No	2.00
970	9.70	136.22	1.76	1.19	0.55	188.46	1.11	208.35	4.000	No	No	2.00
971	9.71	136.29	1.76	1.19	0.55	188.43	1.10	207.86	4.000	No	No	2.00
972	9.72	136.37	1.76	1.18	0.55	188.39	1.10	207.39	4.000	No	No	2.00
973	9.73	136.43	1.76	1.18	0.54	188.36	1.10	206.96	4.000	No	No	2.00
974	9.74	136.04	1.76	1.17	0.54	187.75	1.10	206.36	4.000	No	No	2.00
975	9.75	134.97	1.76	1.17	0.55	186.32	1.10	205.42	4.000	No	No	2.00
976	9.76	133.13	1.77	1.18	0.55	183.94	1.11	203.99	4.000	No	No	2.00
977	9.77	130.93	1.77	1.18	0.55	181.09	1.12	202.23	4.000	No	No	2.00
978	9.78	128.55	1.78	1.18	0.55	178.00	1.12	200.24	4.000	No	No	2.00
979	9.79	126.10	1.78	1.19	0.55	174.83	1.13	198.10	0.803	No	No	1.25
980	9.80	123.73	1.79	1.19	0.56	171.75	1.14	195.92	0.779	No	No	1.21
981	9.81	121.54	1.80	1.19	0.56	168.90	1.15	193.84	0.757	No	No	1.18
982	9.82	119.59	1.80	1.20	0.56	166.39	1.15	192.08	0.739	No	No	1.15
983	9.83	117.46	1.81	1.22	0.56	163.81	1.17	190.98	0.728	No	No	1.13
984	9.84	114.82	1.83	1.26	0.57	160.78	1.18	190.09	0.719	No	No	1.12
985	9.85	111.45	1.85	1.33	0.58	156.96	1.20	188.75	0.705	No	No	1.10
986	9.86	107.64	1.88	1.41	0.59	152.57	1.22	186.45	0.683	No	No	1.06
987	9.87	103.59	1.91	1.49	0.60	147.82	1.24	183.37	0.653	No	No	1.01
988	9.88	99.52	1.93	1.57	0.61	142.94	1.26	179.86	0.621	No	No	0.96
989	9.89	95.63	1.96	1.65	0.62	138.20	1.28	176.27	0.589	No	No	0.91
990	9.90	92.13	1.98	1.72	0.63	133.86	1.29	172.94	0.561	No	No	0.87
991	9.91	89.61	2.00	1.78	0.64	130.76	1.31	170.80	0.543	No	No	0.84
992	9.92	88.39	2.01	1.84	0.64	129.37	1.32	170.45	0.541	No	No	0.84
993	9.93	88.29	2.02	1.90	0.65	129.52	1.33	171.85	0.552	No	No	0.86
994	9.94	88.65	2.03	1.97	0.65	130.35	1.34	174.20	0.572	No	No	0.89
995	9.95	89.05	2.04	2.05	0.65	131.26	1.35	176.85	0.594	No	No	0.92
996	9.96	89.47	2.05	2.13	0.66	132.20	1.36	179.66	0.619	No	No	0.96
997	9.97	89.89	2.06	2.21	0.66	133.12	1.37	182.49	0.645	No	No	1.00
998	9.98	90.28	2.07	2.29	0.66	133.98	1.38	185.19	0.671	No	No	1.04
999	9.99	90.62	2.08	2.35	0.67	134.72	1.39	187.59	0.694	No	No	1.07
1000	10.00	90.70	2.09	2.39	0.67	134.97	1.40	188.87	0.707	No	No	1.09
1001	10.01	90.47	2.09	2.41	0.67	134.66	1.40	188.93	0.707	No	No	1.09
1002	10.02	89.92	2.09	2.40	0.67	133.81	1.40	187.87	0.697	No	No	1.07
1003	10.03	89.25	2.09	2.39	0.67	132.78	1.40	186.54	0.684	No	No	1.05
1004	10.04	88.54	2.09	2.38	0.67	131.67	1.41	185.10	0.670	No	No	1.03
1005	10.05	87.80	2.09	2.37	0.67	130.54	1.41	183.63	0.656	No	No	1.01
1006	10.06	87.08	2.09	2.35	0.67	129.44	1.41	182.21	0.643	No	No	0.99
1007	10.07	86.42	2.09	2.34	0.67	128.43	1.41	180.90	0.631	No	No	0.97
1008	10.08	85.78	2.09	2.33	0.67	127.45	1.41	179.71	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1009	10.09	84.79	2.10	2.33	0.67	126.02	1.41	178.27	4.000	Yes	No	2.00
1010	10.10	83.29	2.10	2.34	0.68	123.92	1.42	176.39	4.000	Yes	No	2.00
1011	10.11	81.22	2.11	2.36	0.68	121.05	1.44	173.96	4.000	Yes	No	2.00
1012	10.12	78.88	2.12	2.38	0.68	117.80	1.45	171.26	4.000	Yes	No	2.00
1013	10.13	76.41	2.13	2.40	0.69	114.36	1.47	168.45	4.000	Yes	No	2.00
1014	10.14	73.91	2.14	2.42	0.69	110.89	1.49	165.67	4.000	Yes	No	2.00
1015	10.15	71.54	2.16	2.43	0.70	107.56	1.52	163.07	4.000	Yes	No	2.00
1016	10.16	69.39	2.17	2.45	0.70	104.55	1.54	160.76	4.000	Yes	No	2.00
1017	10.17	67.57	2.18	2.47	0.70	102.01	1.56	159.07	4.000	Yes	No	2.00
1018	10.18	65.89	2.19	2.51	0.71	99.69	1.59	158.08	4.000	Yes	No	2.00
1019	10.19	64.10	2.20	2.57	0.71	97.29	1.62	157.68	4.000	Yes	No	2.00
1020	10.20	62.02	2.22	2.64	0.72	94.50	1.67	157.54	4.000	Yes	No	2.00
1021	10.21	59.73	2.24	2.73	0.73	91.39	1.72	157.48	4.000	Yes	No	2.00
1022	10.22	57.35	2.26	2.81	0.74	88.14	1.79	157.50	4.000	Yes	No	2.00
1023	10.23	54.99	2.28	2.90	0.74	84.89	1.86	157.60	4.000	Yes	No	2.00
1024	10.24	52.79	2.30	2.98	0.75	81.82	1.93	157.74	4.000	Yes	No	2.00
1025	10.25	50.85	2.32	3.05	0.76	79.11	2.00	157.90	4.000	Yes	No	2.00
1026	10.26	49.28	2.33	3.11	0.76	76.90	2.06	158.30	4.000	Yes	No	2.00
1027	10.27	47.90	2.35	3.18	0.77	74.96	2.12	159.06	4.000	Yes	No	2.00
1028	10.28	46.50	2.36	3.27	0.78	73.02	2.19	160.24	4.000	Yes	No	2.00
1029	10.29	44.91	2.38	3.36	0.78	70.78	2.28	161.62	4.000	Yes	No	2.00
1030	10.30	43.18	2.40	3.47	0.79	68.34	2.39	163.08	4.000	Yes	No	2.00
1031	10.31	41.42	2.42	3.57	0.80	65.83	2.50	164.52	4.000	Yes	No	2.00
1032	10.32	39.71	2.44	3.68	0.81	63.37	2.62	165.84	4.000	Yes	No	2.00
1033	10.33	38.14	2.46	3.77	0.81	61.09	2.73	166.98	4.000	Yes	No	2.00
1034	10.34	36.84	2.48	3.86	0.82	59.19	2.84	167.91	4.000	Yes	No	2.00
1035	10.35	35.90	2.49	3.92	0.82	57.82	2.92	168.82	4.000	Yes	No	2.00
1036	10.36	35.22	2.50	3.99	0.83	56.83	2.83	160.86	4.000	Yes	No	2.00
1037	10.37	34.62	2.51	4.05	0.83	55.96	3.02	169.16	4.000	Yes	No	2.00
1038	10.38	33.95	2.52	4.13	0.84	54.98	3.25	178.93	4.000	Yes	No	2.00
1039	10.39	33.23	2.53	4.21	0.84	53.93	3.52	189.78	4.000	Yes	No	2.00
1040	10.40	32.51	2.55	4.29	0.85	52.88	3.81	201.22	4.000	Yes	No	2.00
1041	10.41	31.83	2.56	4.37	0.85	51.87	4.10	212.69	4.000	Yes	No	2.00
1042	10.42	31.21	2.57	4.44	0.85	50.96	4.39	223.48	4.000	Yes	No	2.00
1043	10.43	30.76	2.58	4.49	0.86	50.28	4.62	232.30	4.000	Yes	No	2.00
1044	10.44	30.50	2.58	4.54	0.86	49.89	4.79	239.02	4.000	Yes	No	2.00
1045	10.45	30.39	2.59	4.58	0.86	49.73	4.91	244.43	4.000	Yes	No	2.00
1046	10.46	30.32	2.59	4.63	0.86	49.64	5.04	250.09	4.000	Yes	No	2.00
1047	10.47	30.24	2.59	4.68	0.86	49.54	5.18	256.40	4.000	Yes	No	2.00
1048	10.48	30.16	2.60	4.74	0.87	49.44	5.32	263.05	4.000	Yes	No	2.00
1049	10.49	30.08	2.60	4.79	0.87	49.33	5.47	269.71	4.000	Yes	No	2.00
1050	10.50	30.01	2.61	4.84	0.87	49.23	5.61	276.05	4.000	Yes	No	2.00
1051	10.51	29.94	2.61	4.89	0.87	49.14	5.73	281.68	4.000	Yes	No	2.00
1052	10.52	29.90	2.61	4.92	0.87	49.08	5.82	285.76	3.600	No	No	2.00
1053	10.53	29.89	2.61	4.94	0.87	49.05	5.88	288.57	3.600	No	No	2.00
1054	10.54	29.88	2.61	4.96	0.87	49.04	5.93	290.57	3.600	No	No	2.00
1055	10.55	29.88	2.62	4.97	0.87	49.03	5.97	292.78	3.600	No	No	2.00
1056	10.56	29.88	2.62	4.99	0.87	49.02	6.02	295.16	3.600	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1057	10.57	29.88	2.62	5.01	0.87	49.04	6.07	297.48	3.600	No	No	2.00
1058	10.58	29.88	2.62	5.03	0.87	49.03	6.12	299.86	3.600	No	No	2.00
1059	10.59	29.88	2.62	5.05	0.88	49.02	6.16	302.07	3.600	No	No	2.00
1060	10.60	29.90	2.62	5.06	0.88	49.03	6.19	303.50	3.600	No	No	2.00
1061	10.61	29.99	2.62	5.06	0.88	49.14	6.16	302.52	3.600	No	No	2.00
1062	10.62	30.16	2.62	5.04	0.87	49.38	6.05	298.89	4.000	Yes	No	2.00
1063	10.63	30.42	2.61	5.01	0.87	49.71	5.90	293.18	4.000	Yes	No	2.00
1064	10.64	30.71	2.61	4.97	0.87	50.11	5.72	286.71	4.000	Yes	No	2.00
1065	10.65	31.02	2.60	4.93	0.87	50.54	5.54	280.01	4.000	Yes	No	2.00
1066	10.66	31.32	2.60	4.89	0.87	50.96	5.37	273.41	4.000	Yes	No	2.00
1067	10.67	31.62	2.59	4.85	0.86	51.36	5.20	267.26	4.000	Yes	No	2.00
1068	10.68	31.88	2.59	4.82	0.86	51.72	5.06	261.86	4.000	Yes	No	2.00
1069	10.69	32.16	2.59	4.79	0.86	52.09	4.92	256.43	4.000	Yes	No	2.00
1070	10.70	32.52	2.58	4.75	0.86	52.60	4.74	249.57	4.000	Yes	No	2.00
1071	10.71	33.03	2.57	4.69	0.86	53.31	4.51	240.51	4.000	Yes	No	2.00
1072	10.72	33.66	2.56	4.62	0.85	54.20	4.24	229.71	4.000	Yes	No	2.00
1073	10.73	34.36	2.55	4.55	0.85	55.17	3.96	218.31	4.000	Yes	No	2.00
1074	10.74	35.08	2.54	4.47	0.84	56.17	3.68	206.99	4.000	Yes	No	2.00
1075	10.75	35.79	2.53	4.39	0.84	57.15	3.44	196.32	4.000	Yes	No	2.00
1076	10.76	36.45	2.52	4.32	0.84	58.06	3.22	186.78	4.000	Yes	No	2.00
1077	10.77	37.03	2.51	4.26	0.83	58.85	3.04	178.75	4.000	Yes	No	2.00
1078	10.78	37.61	2.50	4.20	0.83	59.64	2.88	171.49	4.000	Yes	No	2.00
1079	10.79	38.27	2.49	4.14	0.83	60.54	2.94	178.19	4.000	Yes	No	2.00
1080	10.80	39.10	2.48	4.07	0.82	61.68	2.87	177.05	4.000	Yes	No	2.00
1081	10.81	40.06	2.47	3.99	0.82	63.00	2.79	175.69	4.000	Yes	No	2.00
1082	10.82	41.09	2.46	3.91	0.81	64.41	2.70	174.18	4.000	Yes	No	2.00
1083	10.83	42.14	2.44	3.82	0.81	65.83	2.62	172.59	4.000	Yes	No	2.00
1084	10.84	43.16	2.43	3.73	0.80	67.20	2.54	171.01	4.000	Yes	No	2.00
1085	10.85	44.09	2.42	3.66	0.80	68.45	2.48	169.52	4.000	Yes	No	2.00
1086	10.86	44.92	2.41	3.59	0.79	69.54	2.42	168.26	4.000	Yes	No	2.00
1087	10.87	45.76	2.40	3.53	0.79	70.66	2.37	167.21	4.000	Yes	No	2.00
1088	10.88	46.74	2.39	3.47	0.79	71.97	2.31	166.25	4.000	Yes	No	2.00
1089	10.89	47.95	2.37	3.40	0.78	73.59	2.25	165.22	4.000	Yes	No	2.00
1090	10.90	49.30	2.36	3.32	0.78	75.39	2.18	164.04	4.000	Yes	No	2.00
1091	10.91	50.73	2.34	3.24	0.77	77.29	2.11	162.80	4.000	Yes	No	2.00
1092	10.92	52.17	2.33	3.16	0.76	79.17	2.04	161.54	4.000	Yes	No	2.00
1093	10.93	53.53	2.31	3.08	0.76	80.95	1.98	160.36	4.000	Yes	No	2.00
1094	10.94	54.75	2.30	3.01	0.75	82.52	1.93	159.30	4.000	Yes	No	2.00
1095	10.95	55.78	2.29	2.95	0.75	83.83	1.89	158.42	4.000	Yes	No	2.00
1096	10.96	56.72	2.28	2.89	0.75	85.02	1.85	157.62	4.000	Yes	No	2.00
1097	10.97	57.69	2.27	2.84	0.74	86.24	1.82	156.80	4.000	Yes	No	2.00
1098	10.98	58.81	2.26	2.77	0.74	87.65	1.78	155.88	4.000	Yes	No	2.00
1099	10.99	60.05	2.24	2.70	0.73	89.19	1.74	154.90	4.000	Yes	No	2.00
1100	11.00	61.33	2.23	2.63	0.73	90.77	1.70	153.92	4.000	Yes	No	2.00
1101	11.01	62.59	2.22	2.56	0.72	92.31	1.66	153.01	4.000	Yes	No	2.00
1102	11.02	63.77	2.20	2.49	0.72	93.73	1.62	152.20	4.000	Yes	No	2.00
1103	11.03	64.79	2.19	2.43	0.71	94.96	1.60	151.53	4.000	Yes	No	2.00
1104	11.04	65.56	2.18	2.39	0.71	95.86	1.57	150.97	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1105	11.05	66.15	2.18	2.35	0.71	96.52	1.56	150.43	4.000	Yes	No	2.00
1106	11.06	66.67	2.17	2.31	0.70	97.08	1.54	149.85	4.000	Yes	No	2.00
1107	11.07	67.25	2.16	2.27	0.70	97.72	1.53	149.19	4.000	Yes	No	2.00
1108	11.08	67.88	2.15	2.22	0.70	98.40	1.51	148.52	4.000	Yes	No	2.00
1109	11.09	68.52	2.14	2.17	0.69	99.09	1.49	147.86	4.000	Yes	No	2.00
1110	11.10	69.14	2.14	2.13	0.69	99.75	1.48	147.25	4.000	Yes	No	2.00
1111	11.11	69.71	2.13	2.08	0.69	100.34	1.46	146.71	4.000	Yes	No	2.00
1112	11.12	70.14	2.12	2.05	0.68	100.78	1.45	146.24	4.000	Yes	No	2.00
1113	11.13	70.34	2.12	2.02	0.68	100.93	1.44	145.71	4.000	Yes	No	2.00
1114	11.14	70.33	2.11	2.00	0.68	100.80	1.44	145.05	0.364	No	No	0.54
1115	11.15	70.18	2.11	1.98	0.68	100.49	1.44	144.23	0.359	No	No	0.53
1116	11.16	70.01	2.11	1.96	0.68	100.14	1.43	143.31	0.354	No	No	0.52
1117	11.17	69.83	2.11	1.93	0.68	99.78	1.43	142.34	0.348	No	No	0.51
1118	11.18	69.65	2.10	1.91	0.68	99.41	1.42	141.38	0.343	No	No	0.50
1119	11.19	69.48	2.10	1.88	0.68	99.06	1.42	140.47	0.338	No	No	0.50
1120	11.20	69.33	2.10	1.86	0.68	98.75	1.41	139.66	0.333	No	No	0.49
1121	11.21	69.12	2.10	1.85	0.68	98.39	1.41	138.99	0.330	No	No	0.48
1122	11.22	68.78	2.10	1.84	0.68	97.89	1.41	138.41	4.000	Yes	No	2.00
1123	11.23	68.26	2.10	1.85	0.68	97.18	1.42	137.84	4.000	Yes	No	2.00
1124	11.24	67.61	2.10	1.86	0.68	96.31	1.42	137.20	4.000	Yes	No	2.00
1125	11.25	66.90	2.11	1.87	0.68	95.35	1.43	136.51	4.000	Yes	No	2.00
1126	11.26	66.17	2.11	1.88	0.68	94.37	1.44	135.81	4.000	Yes	No	2.00
1127	11.27	65.44	2.12	1.89	0.68	93.39	1.45	135.12	4.000	Yes	No	2.00
1128	11.28	64.77	2.12	1.90	0.69	92.49	1.45	134.49	4.000	Yes	No	2.00
1129	11.29	64.18	2.13	1.90	0.69	91.69	1.46	133.93	4.000	Yes	No	2.00
1130	11.30	63.58	2.13	1.92	0.69	90.90	1.47	133.52	4.000	Yes	No	2.00
1131	11.31	62.89	2.14	1.94	0.69	89.99	1.48	133.22	4.000	Yes	No	2.00
1132	11.32	62.01	2.15	1.97	0.69	88.87	1.50	132.98	4.000	Yes	No	2.00
1133	11.33	61.00	2.16	2.00	0.70	87.58	1.52	132.75	4.000	Yes	No	2.00
1134	11.34	59.92	2.17	2.04	0.70	86.20	1.54	132.53	4.000	Yes	No	2.00
1135	11.35	58.82	2.18	2.08	0.71	84.78	1.56	132.34	4.000	Yes	No	2.00
1136	11.36	57.76	2.19	2.12	0.71	83.40	1.58	132.19	4.000	Yes	No	2.00
1137	11.37	56.79	2.20	2.15	0.71	82.14	1.61	132.07	4.000	Yes	No	2.00
1138	11.38	55.93	2.21	2.18	0.72	81.01	1.63	132.01	4.000	Yes	No	2.00
1139	11.39	55.04	2.22	2.21	0.72	79.85	1.65	132.01	4.000	Yes	No	2.00
1140	11.40	54.01	2.23	2.25	0.73	78.50	1.68	132.10	4.000	Yes	No	2.00
1141	11.41	52.74	2.24	2.31	0.73	76.85	1.72	132.29	4.000	Yes	No	2.00
1142	11.42	51.32	2.25	2.36	0.74	74.98	1.77	132.54	4.000	Yes	No	2.00
1143	11.43	49.82	2.27	2.42	0.74	73.01	1.82	132.86	4.000	Yes	No	2.00
1144	11.44	48.33	2.29	2.48	0.75	71.03	1.88	133.22	4.000	Yes	No	2.00
1145	11.45	46.91	2.30	2.54	0.75	69.13	1.93	133.59	4.000	Yes	No	2.00
1146	11.46	45.64	2.32	2.59	0.76	67.43	1.99	133.94	4.000	Yes	No	2.00
1147	11.47	44.59	2.33	2.64	0.76	66.01	2.04	134.34	4.000	Yes	No	2.00
1148	11.48	43.66	2.34	2.69	0.77	64.75	2.08	134.87	4.000	Yes	No	2.00
1149	11.49	42.71	2.35	2.74	0.77	63.47	2.14	135.61	4.000	Yes	No	2.00
1150	11.50	41.62	2.37	2.80	0.78	62.01	2.20	136.52	4.000	Yes	No	2.00
1151	11.51	40.44	2.38	2.87	0.78	60.41	2.28	137.51	4.000	Yes	No	2.00
1152	11.52	39.21	2.40	2.94	0.79	58.74	2.36	138.53	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1153	11.53	38.00	2.41	3.01	0.80	57.09	2.44	139.51	4.000	Yes	No	2.00
1154	11.54	36.88	2.43	3.08	0.80	55.54	2.53	140.40	4.000	Yes	No	2.00
1155	11.55	35.91	2.44	3.14	0.81	54.18	2.61	141.16	4.000	Yes	No	2.00
1156	11.56	35.13	2.45	3.19	0.81	53.11	2.67	141.89	4.000	Yes	No	2.00
1157	11.57	34.46	2.46	3.24	0.82	52.17	2.74	142.71	4.000	Yes	No	2.00
1158	11.58	33.79	2.47	3.30	0.82	51.25	2.80	143.72	4.000	Yes	No	2.00
1159	11.59	33.03	2.49	3.36	0.82	50.19	2.89	144.85	4.000	Yes	No	2.00
1160	11.60	32.21	2.50	3.43	0.83	49.05	2.98	146.02	4.000	Yes	No	2.00
1161	11.61	31.38	2.51	3.51	0.84	47.89	3.07	146.94	4.000	Yes	No	2.00
1162	11.62	30.58	2.53	3.58	0.84	46.76	3.36	156.87	4.000	Yes	No	2.00
1163	11.63	29.84	2.54	3.64	0.84	45.72	3.64	166.47	4.000	Yes	No	2.00
1164	11.64	29.25	2.55	3.69	0.85	44.87	3.90	174.84	4.000	Yes	No	2.00
1165	11.65	28.81	2.56	3.74	0.85	44.25	4.11	181.77	4.000	Yes	No	2.00
1166	11.66	28.48	2.56	3.78	0.85	43.78	4.29	188.01	4.000	Yes	No	2.00
1167	11.67	28.16	2.57	3.83	0.86	43.33	4.49	194.72	4.000	Yes	No	2.00
1168	11.68	27.81	2.58	3.88	0.86	42.83	4.73	202.45	4.000	Yes	No	2.00
1169	11.69	27.44	2.59	3.94	0.86	42.30	4.98	210.83	4.000	Yes	No	2.00
1170	11.70	27.07	2.60	3.99	0.87	41.78	5.25	219.49	4.000	Yes	No	2.00
1171	11.71	26.72	2.60	4.05	0.87	41.29	5.52	227.88	4.000	Yes	No	2.00
1172	11.72	26.40	2.61	4.09	0.87	40.84	5.77	235.67	4.000	Yes	No	2.00
1173	11.73	26.21	2.61	4.13	0.87	40.55	5.95	241.14	4.000	Yes	No	2.00
1174	11.74	26.15	2.62	4.15	0.88	40.47	6.02	243.81	3.600	No	No	2.00
1175	11.75	26.23	2.62	4.15	0.88	40.57	6.02	244.07	3.600	No	No	2.00
1176	11.76	26.35	2.62	4.16	0.87	40.74	5.98	243.68	3.600	No	No	2.00
1177	11.77	26.49	2.61	4.17	0.87	40.92	5.94	243.25	3.600	No	No	2.00
1178	11.78	26.63	2.61	4.17	0.87	41.12	5.91	242.81	3.600	No	No	2.00
1179	11.79	26.76	2.61	4.18	0.87	41.31	5.87	242.38	3.600	No	No	2.00
1180	11.80	26.89	2.61	4.18	0.87	41.48	5.83	242.00	3.600	No	No	2.00
1181	11.81	26.99	2.61	4.19	0.87	41.62	5.81	241.70	3.600	No	No	2.00
1182	11.82	26.96	2.61	4.18	0.87	41.55	5.82	241.66	3.600	No	No	2.00
1183	11.83	26.76	2.61	4.17	0.87	41.24	5.87	241.91	3.600	No	No	2.00
1184	11.84	26.40	2.62	4.15	0.87	40.67	5.96	242.43	3.600	No	No	2.00
1185	11.85	25.99	2.62	4.12	0.88	40.03	6.07	243.08	3.600	No	No	2.00
1186	11.86	25.55	2.62	4.09	0.88	39.34	6.20	243.83	3.600	No	No	2.00
1187	11.87	25.10	2.62	4.06	0.88	38.64	6.33	244.68	3.600	No	No	2.00
1188	11.88	24.67	2.63	4.03	0.88	37.97	6.47	245.57	3.600	No	No	2.00
1189	11.89	24.27	2.63	4.00	0.88	37.35	6.60	246.47	3.600	No	No	2.00
1190	11.90	23.96	2.63	3.98	0.88	36.86	6.70	246.85	3.600	No	No	2.00
1191	11.91	23.76	2.63	3.95	0.88	36.53	6.73	245.73	3.600	No	No	2.00
1192	11.92	23.64	2.63	3.91	0.88	36.32	6.69	242.87	3.600	No	No	2.00
1193	11.93	23.55	2.63	3.87	0.88	36.14	6.60	238.65	3.600	No	No	2.00
1194	11.94	23.45	2.63	3.82	0.88	35.95	6.51	233.95	3.600	No	No	2.00
1195	11.95	23.34	2.63	3.76	0.88	35.74	6.41	229.04	3.600	No	No	2.00
1196	11.96	23.23	2.62	3.71	0.88	35.54	6.31	224.19	3.600	No	No	2.00
1197	11.97	23.13	2.62	3.66	0.88	35.35	6.21	219.63	3.600	No	No	2.00
1198	11.98	23.04	2.62	3.61	0.88	35.18	6.13	215.61	3.600	No	No	2.00
1199	11.99	22.93	2.62	3.58	0.88	34.97	6.08	212.66	3.600	No	No	2.00
1200	12.00	22.76	2.62	3.54	0.88	34.69	6.07	210.66	3.600	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1201	12.01	22.50	2.62	3.51	0.88	34.28	6.11	209.29	3.600	No	No	2.00
1202	12.02	22.19	2.62	3.46	0.88	33.78	6.15	207.90	3.600	No	No	2.00
1203	12.03	21.85	2.62	3.42	0.88	33.24	6.21	206.41	3.600	No	No	2.00
1204	12.04	21.49	2.62	3.37	0.88	32.68	6.27	204.89	3.600	No	No	2.00
1205	12.05	21.15	2.62	3.33	0.88	32.13	6.33	203.45	3.600	No	No	2.00
1206	12.06	20.83	2.63	3.28	0.88	31.63	6.39	202.15	3.600	No	No	2.00
1207	12.07	20.54	2.63	3.25	0.88	31.18	6.45	201.19	3.600	No	No	2.00
1208	12.08	20.15	2.63	3.23	0.88	30.58	6.63	202.89	3.600	No	No	2.00
1209	12.09	19.60	2.64	3.22	0.88	29.75	6.99	207.94	3.600	No	No	2.00
1210	12.10	18.82	2.65	3.22	0.89	28.60	7.59	217.03	3.600	No	No	2.00
1211	12.11	17.94	2.67	3.22	0.90	27.28	8.37	228.44	3.600	No	No	2.00
1212	12.12	16.99	2.69	3.22	0.90	25.87	9.36	242.06	3.600	No	No	2.00
1213	12.13	16.03	2.71	3.22	0.91	24.43	4.77	116.45	1.165	No	Yes	1.66
1214	12.14	15.10	2.73	3.22	0.92	23.05	4.98	114.77	1.099	No	Yes	1.57
1215	12.15	14.26	2.74	3.23	0.92	21.78	5.20	113.17	1.039	No	Yes	1.48
1216	12.16	13.60	2.76	3.23	0.93	20.78	5.39	111.91	0.991	No	Yes	1.41
1217	12.17	13.17	2.77	3.25	0.94	20.13	5.53	111.26	0.960	No	Yes	1.37
1218	12.18	12.90	2.78	3.27	0.94	19.73	5.63	111.17	0.941	No	Yes	1.34
1219	12.19	12.70	2.79	3.31	0.94	19.43	5.73	111.37	0.927	No	Yes	1.32
1220	12.20	12.47	2.80	3.35	0.95	19.09	5.85	111.58	0.910	No	Yes	1.29
1221	12.21	12.23	2.81	3.39	0.95	18.73	5.97	111.76	0.893	No	Yes	1.27
1222	12.22	11.99	2.82	3.43	0.95	18.37	6.09	111.92	0.876	No	Yes	1.24
1223	12.23	11.77	2.83	3.47	0.96	18.03	6.21	112.05	0.860	No	Yes	1.22
1224	12.24	11.57	2.84	3.50	0.96	17.73	6.32	112.14	0.846	No	Yes	1.20
1225	12.25	11.40	2.84	3.54	0.96	17.47	6.43	112.26	0.833	No	Yes	1.18
1226	12.26	11.23	2.85	3.57	0.97	17.22	6.53	112.45	0.821	No	Yes	1.16
1227	12.27	11.05	2.86	3.62	0.97	16.94	6.65	112.73	0.808	No	Yes	1.15
1228	12.28	10.83	2.87	3.68	0.97	16.62	6.80	113.05	0.793	No	Yes	1.12
1229	12.29	10.60	2.88	3.74	0.98	16.27	6.97	113.36	0.776	No	Yes	1.10
1230	12.30	10.36	2.90	3.80	0.98	15.91	7.14	113.64	0.759	No	Yes	1.08
1231	12.31	10.12	2.91	3.86	0.99	15.56	7.32	113.87	0.742	No	Yes	1.05
1232	12.32	9.90	2.92	3.92	0.99	15.23	7.49	114.04	0.726	No	Yes	1.03
1233	12.33	9.72	2.93	3.97	0.99	14.94	7.64	114.15	0.712	No	Yes	1.01
1234	12.34	9.55	2.94	4.02	1.00	14.68	7.78	114.23	0.700	No	Yes	0.99
1235	12.35	9.38	2.95	4.07	1.00	14.41	7.93	114.25	0.687	No	Yes	0.97
1236	12.36	9.18	2.96	4.12	1.00	14.08	8.11	114.19	0.672	No	Yes	0.95
1237	12.37	8.96	2.97	4.18	1.00	13.70	8.33	114.08	0.654	No	Yes	0.92
1238	12.38	8.72	2.99	4.25	1.00	13.30	8.56	113.91	0.635	No	Yes	0.90
1239	12.39	8.48	3.00	4.32	1.00	12.90	8.81	113.68	0.615	No	Yes	0.87
1240	12.40	8.25	3.02	4.39	1.00	12.51	9.07	113.41	0.597	No	Yes	0.84
1241	12.41	8.04	3.03	4.45	1.00	12.15	9.31	113.11	0.580	No	Yes	0.82
1242	12.42	7.87	3.04	4.51	1.00	11.86	9.51	112.83	0.566	No	Yes	0.80
1243	12.43	7.73	3.05	4.55	1.00	11.62	9.69	112.61	0.554	No	Yes	0.78
1244	12.44	7.60	3.06	4.60	1.00	11.41	9.86	112.43	0.544	No	Yes	0.77
1245	12.45	7.47	3.07	4.65	1.00	11.18	10.04	112.22	0.533	No	Yes	0.75
1246	12.46	7.32	3.08	4.71	1.00	10.92	10.26	111.97	0.521	No	Yes	0.73
1247	12.47	7.16	3.09	4.77	1.00	10.65	10.49	111.67	0.508	No	Yes	0.72
1248	12.48	7.00	3.11	4.83	1.00	10.38	10.73	111.34	0.495	No	Yes	0.70

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1249	12.49	6.85	3.12	4.89	1.00	10.13	10.96	111.00	0.483	No	Yes	0.68
1250	12.50	6.71	3.13	4.94	1.00	9.90	11.18	110.67	0.472	No	Yes	0.66
1251	12.51	6.61	3.14	4.98	1.00	9.73	11.35	110.40	0.464	No	Yes	0.65
1252	12.52	6.53	3.14	5.02	1.00	9.59	11.48	110.19	0.458	No	Yes	0.64
1253	12.53	6.47	3.15	5.05	1.00	9.48	11.60	110.02	0.452	No	Yes	0.64
1254	12.54	6.40	3.15	5.08	1.00	9.36	11.73	109.83	0.446	No	Yes	0.63
1255	12.55	6.32	3.16	5.11	1.00	9.23	11.88	109.61	0.440	No	Yes	0.62
1256	12.56	6.24	3.17	5.15	1.00	9.09	12.03	109.38	0.434	No	Yes	0.61
1257	12.57	6.16	3.18	5.19	1.00	8.96	12.19	109.14	0.427	No	Yes	0.60
1258	12.58	6.09	3.18	5.22	1.00	8.83	12.33	108.91	0.421	No	Yes	0.59
1259	12.59	6.03	3.19	5.25	1.00	8.73	12.46	108.71	0.416	No	Yes	0.58
1260	12.60	5.99	3.19	5.27	1.00	8.66	12.53	108.58	0.413	No	Yes	0.58
1261	12.61	5.98	3.19	5.28	1.00	8.63	12.57	108.52	0.412	No	Yes	0.58
1262	12.62	5.98	3.19	5.28	1.00	8.63	12.57	108.51	0.412	No	Yes	0.58
1263	12.63	5.98	3.19	5.28	1.00	8.63	12.58	108.49	0.411	No	Yes	0.58
1264	12.64	5.98	3.19	5.28	1.00	8.62	12.58	108.48	0.411	No	Yes	0.58
1265	12.65	5.98	3.19	5.28	1.00	8.62	12.59	108.47	0.411	No	Yes	0.58
1266	12.66	5.98	3.19	5.28	1.00	8.61	12.59	108.45	0.411	No	Yes	0.58
1267	12.67	5.98	3.19	5.28	1.00	8.61	12.59	108.44	0.411	No	Yes	0.57
1268	12.68	5.98	3.19	5.28	1.00	8.61	12.59	108.39	0.411	No	Yes	0.57
1269	12.69	5.98	3.19	5.27	1.00	8.60	12.58	108.25	0.410	No	Yes	0.57
1270	12.70	5.98	3.19	5.24	1.00	8.60	12.56	108.00	0.410	No	Yes	0.57
1271	12.71	5.98	3.19	5.21	1.00	8.59	12.53	107.66	0.410	No	Yes	0.57
1272	12.72	5.98	3.19	5.17	1.00	8.59	12.49	107.28	0.410	No	Yes	0.57
1273	12.73	5.98	3.19	5.14	1.00	8.59	12.45	106.88	0.410	No	Yes	0.57
1274	12.74	5.98	3.19	5.10	1.00	8.58	12.41	106.48	0.409	No	Yes	0.57
1275	12.75	5.98	3.18	5.06	1.00	8.58	12.37	106.11	0.409	No	Yes	0.57
1276	12.76	5.98	3.18	5.03	1.00	8.58	12.33	105.77	0.409	No	Yes	0.57
1277	12.77	5.98	3.18	5.00	1.00	8.57	12.30	105.44	0.409	No	Yes	0.57
1278	12.78	5.98	3.18	4.96	1.00	8.57	12.26	105.07	0.409	No	Yes	0.57
1279	12.79	5.98	3.18	4.92	1.00	8.56	12.21	104.59	0.408	No	Yes	0.57
1280	12.80	5.98	3.17	4.86	1.00	8.56	12.15	104.03	0.408	No	Yes	0.57
1281	12.81	5.98	3.17	4.80	1.00	8.56	12.09	103.42	0.408	No	Yes	0.57
1282	12.82	5.98	3.17	4.74	1.00	8.55	12.02	102.79	0.408	No	Yes	0.57
1283	12.83	5.98	3.16	4.68	1.00	8.55	11.95	102.17	0.408	No	Yes	0.57
1284	12.84	5.98	3.16	4.63	1.00	8.54	11.89	101.60	0.408	No	Yes	0.57
1285	12.85	5.98	3.16	4.58	1.00	8.54	11.84	101.09	0.407	No	Yes	0.57
1286	12.86	5.98	3.16	4.54	1.00	8.54	11.79	100.62	0.407	No	Yes	0.57
1287	12.87	5.98	3.15	4.49	1.00	8.53	11.73	100.12	0.407	No	Yes	0.57
1288	12.88	5.98	3.15	4.44	1.00	8.53	11.67	99.53	0.407	No	Yes	0.57
1289	12.89	5.98	3.15	4.37	1.00	8.52	11.60	98.85	0.407	No	Yes	0.57
1290	12.90	5.98	3.14	4.31	1.00	8.52	11.52	98.13	0.406	No	Yes	0.56
1291	12.91	5.98	3.14	4.24	1.00	8.52	11.43	97.39	0.406	No	Yes	0.56
1292	12.92	5.98	3.14	4.17	1.00	8.51	11.36	96.68	0.406	No	Yes	0.56
1293	12.93	5.98	3.13	4.12	1.00	8.51	11.28	96.03	0.406	No	Yes	0.56
1294	12.94	5.98	3.13	4.06	1.00	8.51	11.22	95.46	0.406	No	Yes	0.56
1295	12.95	5.98	3.13	4.01	1.00	8.50	11.16	94.89	0.406	No	Yes	0.56
1296	12.96	5.98	3.12	3.96	1.00	8.50	11.09	94.26	0.405	No	Yes	0.56

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _t (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1297	12.97	5.98	3.12	3.89	1.00	8.49	11.01	93.49	0.405	No	Yes	0.56
1298	12.98	5.98	3.11	3.82	1.00	8.49	10.91	92.64	0.405	No	Yes	0.56
1299	12.99	5.98	3.11	3.74	1.00	8.49	10.81	91.74	0.405	No	Yes	0.56
1300	13.00	5.98	3.10	3.66	1.00	8.48	10.71	90.84	0.405	No	Yes	0.56
1301	13.01	5.98	3.10	3.59	1.00	8.48	10.61	89.99	0.404	No	Yes	0.56
1302	13.02	5.98	3.10	3.52	1.00	8.48	10.53	89.22	0.404	No	Yes	0.56
1303	13.03	5.95	3.09	3.47	1.00	8.43	10.49	88.46	0.402	No	Yes	0.56
1304	13.04	5.88	3.10	3.43	1.00	8.31	10.53	87.55	0.396	No	Yes	0.55
1305	13.05	5.76	3.10	3.39	1.00	8.12	10.65	86.40	0.387	No	Yes	0.54
1306	13.06	5.62	3.11	3.34	1.00	7.88	10.79	85.03	0.376	No	Yes	0.52
1307	13.07	5.46	3.12	3.30	1.00	7.62	10.96	83.55	0.364	No	Yes	0.50
1308	13.08	5.30	3.13	3.25	1.00	7.36	11.15	82.02	0.351	No	Yes	0.48
1309	13.09	5.14	3.14	3.20	1.00	7.10	11.34	80.52	0.339	No	Yes	0.47
1310	13.10	5.00	3.14	3.16	1.00	6.86	11.53	79.13	0.327	No	Yes	0.45
1311	13.11	4.87	3.15	3.12	1.00	6.65	11.71	77.92	0.317	No	Yes	0.44
1312	13.12	4.74	3.16	3.10	1.00	6.44	11.93	76.78	0.307	No	Yes	0.42
1313	13.13	4.58	3.18	3.08	1.00	6.18	12.22	75.56	0.295	No	Yes	0.41
1314	13.14	4.39	3.20	3.07	1.00	5.86	12.64	74.07	0.279	No	Yes	0.39
1315	13.15	4.16	3.22	3.06	1.00	5.49	13.17	72.36	0.262	No	Yes	0.36
1316	13.16	3.93	3.25	3.05	1.00	5.11	13.80	70.49	0.244	No	Yes	0.34
1317	13.17	3.69	3.27	3.05	1.00	4.72	14.54	68.54	0.225	No	Yes	0.31
1318	13.18	3.46	3.31	3.06	1.00	4.34	15.35	66.61	0.207	No	Yes	0.29
1319	13.19	3.25	3.34	3.07	1.00	4.00	16.19	64.82	0.191	No	Yes	0.26
1320	13.20	3.09	3.36	3.08	1.00	3.74	16.95	63.36	0.178	No	Yes	0.25
1321	13.21	2.98	3.38	3.09	1.00	3.56	17.52	62.32	0.170	No	Yes	0.23
1322	13.22	2.90	3.40	3.10	1.00	3.43	17.94	61.59	0.164	No	Yes	0.23
1323	13.23	2.83	3.41	3.11	1.00	3.32	18.34	60.89	0.158	No	Yes	0.22
1324	13.24	2.76	3.43	3.12	1.00	3.19	18.82	60.12	0.152	No	Yes	0.21
1325	13.25	2.68	3.44	3.13	1.00	3.06	19.35	59.29	0.146	No	Yes	0.20
1326	13.26	2.60	3.46	3.14	1.00	2.93	19.92	58.46	0.140	No	Yes	0.19
1327	13.27	2.52	3.48	3.16	1.00	2.81	20.51	57.67	0.134	No	Yes	0.18
1328	13.28	2.46	3.49	3.17	1.00	2.70	21.06	56.96	0.129	No	Yes	0.18
1329	13.29	2.41	3.50	3.19	1.00	2.63	21.46	56.52	0.126	No	Yes	0.17
1330	13.30	2.39	3.51	3.21	1.00	2.60	21.69	56.37	0.124	No	Yes	0.17
1331	13.31	2.39	3.51	3.23	1.00	2.59	21.77	56.47	0.124	No	Yes	0.17
1332	13.32	2.39	3.51	3.26	1.00	2.59	21.84	56.62	0.124	No	Yes	0.17
1333	13.33	2.39	3.52	3.29	1.00	2.59	21.92	56.79	0.124	No	Yes	0.17
1334	13.34	2.39	3.52	3.32	1.00	2.59	21.99	56.96	0.124	No	Yes	0.17
1335	13.35	2.39	3.52	3.34	1.00	2.59	22.07	57.12	0.123	No	Yes	0.17
1336	13.36	2.39	3.52	3.37	1.00	2.59	22.14	57.27	0.123	No	Yes	0.17
1337	13.37	2.40	3.52	3.39	1.00	2.59	22.15	57.45	0.124	No	Yes	0.17
1338	13.38	2.44	3.51	3.39	1.00	2.66	21.81	58.01	0.127	No	Yes	0.17
1339	13.39	2.52	3.49	3.38	1.00	2.80	21.09	59.03	0.133	No	Yes	0.18
1340	13.40	2.65	3.46	3.37	1.00	3.01	20.11	60.51	0.144	No	Yes	0.20
1341	13.41	2.80	3.43	3.35	1.00	3.25	19.13	62.15	0.155	No	Yes	0.21
1342	13.42	2.96	3.41	3.35	1.00	3.50	18.23	63.85	0.167	No	Yes	0.23
1343	13.43	3.12	3.38	3.35	1.00	3.76	17.44	65.53	0.179	No	Yes	0.24
1344	13.44	3.28	3.36	3.36	1.00	4.00	16.77	67.11	0.191	No	Yes	0.26

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _k (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1345	13.45	3.41	3.34	3.37	1.00	4.22	16.22	68.51	0.201	No	Yes	0.27
1346	13.46	3.54	3.32	3.38	1.00	4.42	15.76	69.74	0.211	No	Yes	0.29
1347	13.47	3.68	3.30	3.38	1.00	4.65	15.28	71.00	0.222	No	Yes	0.30
1348	13.48	3.85	3.28	3.38	1.00	4.92	14.73	72.46	0.235	No	Yes	0.32
1349	13.49	4.06	3.26	3.38	1.00	5.25	14.13	74.17	0.250	No	Yes	0.34
1350	13.50	4.29	3.23	3.38	1.00	5.62	13.53	76.02	0.268	No	Yes	0.37
1351	13.51	4.53	3.21	3.39	1.00	6.00	12.98	77.90	0.286	No	Yes	0.39
1352	13.52	4.76	3.19	3.40	1.00	6.38	12.50	79.72	0.304	No	Yes	0.41
1353	13.53	4.99	3.17	3.42	1.00	6.74	12.08	81.39	0.321	No	Yes	0.44
1354	13.54	5.18	3.16	3.43	1.00	7.05	11.75	82.84	0.336	No	Yes	0.46
1355	13.55	5.30	3.15	3.45	1.00	7.23	11.58	83.75	0.345	No	Yes	0.47
1356	13.56	5.34	3.15	3.47	1.00	7.29	11.54	84.16	0.348	No	Yes	0.47
1357	13.57	5.30	3.15	3.49	1.00	7.23	11.64	84.17	0.345	No	Yes	0.47
1358	13.58	5.26	3.16	3.52	1.00	7.15	11.76	84.12	0.341	No	Yes	0.46
1359	13.59	5.20	3.16	3.54	1.00	7.07	11.90	84.06	0.337	No	Yes	0.46
1360	13.60	5.15	3.17	3.57	1.00	6.98	12.04	83.99	0.333	No	Yes	0.45
1361	13.61	5.10	3.18	3.60	1.00	6.89	12.18	83.92	0.329	No	Yes	0.45
1362	13.62	5.05	3.18	3.63	1.00	6.81	12.31	83.85	0.325	No	Yes	0.44
1363	13.63	5.01	3.19	3.65	1.00	6.75	12.43	83.82	0.322	No	Yes	0.44
1364	13.64	4.99	3.19	3.69	1.00	6.71	12.53	84.00	0.320	No	Yes	0.43
1365	13.65	4.98	3.20	3.74	1.00	6.69	12.62	84.44	0.319	No	Yes	0.43
1366	13.66	4.98	3.20	3.81	1.00	6.69	12.73	85.13	0.319	No	Yes	0.43
1367	13.67	4.98	3.21	3.89	1.00	6.68	12.85	85.90	0.319	No	Yes	0.43
1368	13.68	4.98	3.21	3.98	1.00	6.68	12.98	86.70	0.319	No	Yes	0.43
1369	13.69	4.98	3.22	4.07	1.00	6.68	13.10	87.51	0.319	No	Yes	0.43
1370	13.70	4.98	3.22	4.15	1.00	6.67	13.22	88.27	0.318	No	Yes	0.43
1371	13.71	4.98	3.23	4.22	1.00	6.67	13.33	88.94	0.318	No	Yes	0.43
1372	13.72	4.99	3.23	4.27	1.00	6.69	13.38	89.53	0.319	No	Yes	0.43
1373	13.73	5.04	3.23	4.30	1.00	6.77	13.32	90.10	0.323	No	Yes	0.44
1374	13.74	5.13	3.22	4.29	1.00	6.90	13.15	90.73	0.329	No	Yes	0.45
1375	13.75	5.24	3.21	4.28	1.00	7.08	12.91	91.47	0.338	No	Yes	0.46
1376	13.76	5.37	3.20	4.27	1.00	7.28	12.67	92.28	0.347	No	Yes	0.47
1377	13.77	5.51	3.19	4.25	1.00	7.49	12.42	93.10	0.357	No	Yes	0.48
1378	13.78	5.64	3.18	4.24	1.00	7.70	12.19	93.90	0.367	No	Yes	0.50
1379	13.79	5.76	3.17	4.23	1.00	7.89	11.99	94.63	0.377	No	Yes	0.51
1380	13.80	5.87	3.16	4.22	1.00	8.06	11.81	95.27	0.385	No	Yes	0.52
1381	13.81	5.91	3.15	4.20	1.00	8.12	11.74	95.39	0.388	No	Yes	0.52
1382	13.82	5.87	3.16	4.18	1.00	8.06	11.78	94.90	0.384	No	Yes	0.52
1383	13.83	5.75	3.16	4.16	1.00	7.87	11.92	93.77	0.375	No	Yes	0.51
1384	13.84	5.61	3.17	4.12	1.00	7.63	12.11	92.40	0.364	No	Yes	0.49
1385	13.85	5.45	3.18	4.08	1.00	7.38	12.32	90.92	0.352	No	Yes	0.47
1386	13.86	5.29	3.19	4.05	1.00	7.12	12.55	89.39	0.340	No	Yes	0.46
1387	13.87	5.13	3.20	4.01	1.00	6.87	12.79	87.90	0.328	No	Yes	0.44
1388	13.88	4.99	3.21	3.98	1.00	6.64	13.03	86.52	0.317	No	Yes	0.43
1389	13.89	4.87	3.22	3.96	1.00	6.44	13.25	85.37	0.307	No	Yes	0.41
1390	13.90	4.76	3.23	3.96	1.00	6.26	13.50	84.53	0.299	No	Yes	0.40
1391	13.91	4.64	3.25	4.00	1.00	6.08	13.81	83.92	0.290	No	Yes	0.39
1392	13.92	4.51	3.26	4.06	1.00	5.86	14.22	83.35	0.280	No	Yes	0.38

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1393	13.93	4.36	3.28	4.13	1.00	5.62	14.70	82.68	0.268	No	Yes	0.36
1394	13.94	4.20	3.30	4.21	1.00	5.37	15.26	81.92	0.256	No	Yes	0.34
1395	13.95	4.04	3.33	4.29	1.00	5.11	15.86	81.10	0.244	No	Yes	0.33
1396	13.96	3.89	3.35	4.38	1.00	4.87	16.48	80.27	0.232	No	Yes	0.31
1397	13.97	3.75	3.37	4.46	1.00	4.65	17.09	79.48	0.222	No	Yes	0.30
1398	13.98	3.65	3.39	4.53	1.00	4.49	17.58	78.97	0.214	No	Yes	0.29
1399	13.99	3.60	3.40	4.61	1.00	4.41	17.91	78.91	0.210	No	Yes	0.28
1400	14.00	3.59	3.40	4.69	1.00	4.38	18.10	79.31	0.209	No	Yes	0.28
1401	14.01	3.59	3.41	4.78	1.00	4.38	18.25	79.94	0.209	No	Yes	0.28
1402	14.02	3.59	3.41	4.88	1.00	4.38	18.42	80.64	0.209	No	Yes	0.28
1403	14.03	3.59	3.42	4.99	1.00	4.38	18.59	81.35	0.209	No	Yes	0.28
1404	14.04	3.59	3.42	5.10	1.00	4.37	18.76	82.05	0.209	No	Yes	0.28
1405	14.05	3.59	3.43	5.20	1.00	4.37	18.92	82.70	0.209	No	Yes	0.28
1406	14.06	3.59	3.43	5.29	1.00	4.37	19.06	83.27	0.208	No	Yes	0.28
1407	14.07	3.62	3.43	5.36	1.00	4.42	19.04	84.08	0.211	No	Yes	0.28
1408	14.08	3.69	3.43	5.42	1.00	4.53	18.84	85.34	0.216	No	Yes	0.29
1409	14.09	3.81	3.41	5.48	1.00	4.72	18.46	87.16	0.225	No	Yes	0.30
1410	14.10	3.96	3.40	5.55	1.00	4.95	18.04	89.29	0.236	No	Yes	0.32
1411	14.11	4.12	3.39	5.63	1.00	5.19	17.63	91.58	0.248	No	Yes	0.33
1412	14.12	4.28	3.37	5.71	1.00	5.45	17.25	93.91	0.260	No	Yes	0.35
1413	14.13	4.43	3.36	5.80	1.00	5.69	16.91	96.17	0.271	No	Yes	0.36
1414	14.14	4.57	3.35	5.88	1.00	5.91	16.62	98.23	0.282	No	Yes	0.38
1415	14.15	4.70	3.34	5.94	1.00	6.11	16.37	100.02	0.291	No	Yes	0.39
1416	14.16	4.83	3.33	5.99	1.00	6.32	16.11	101.74	0.301	No	Yes	0.40
1417	14.17	4.99	3.32	6.03	1.00	6.56	15.78	103.62	0.313	No	Yes	0.42
1418	14.18	5.19	3.31	6.07	1.00	6.88	15.39	105.86	0.328	No	Yes	0.44
1419	14.19	5.42	3.29	6.11	1.00	7.23	14.99	108.37	0.345	No	Yes	0.46
1420	14.20	5.66	3.28	6.16	1.00	7.60	14.60	110.99	0.363	No	Yes	0.48
1421	14.21	5.90	3.26	6.22	1.00	7.97	14.25	113.61	0.380	No	Yes	0.51
1422	14.22	6.13	3.25	6.27	1.00	8.33	13.94	116.08	0.397	No	Yes	0.53
1423	14.23	6.33	3.24	6.32	1.00	8.65	13.68	118.29	0.412	No	Yes	0.55
1424	14.24	6.51	3.23	6.35	1.00	8.92	13.46	120.06	0.425	No	Yes	0.57
1425	14.25	6.67	3.22	6.36	1.00	9.18	13.24	121.52	0.438	No	Yes	0.58
1426	14.26	6.85	3.21	6.35	1.00	9.46	12.99	122.85	0.451	No	Yes	0.60
1427	14.27	7.06	3.20	6.33	1.00	9.78	12.71	124.30	0.467	No	Yes	0.62
1428	14.28	7.29	3.19	6.30	1.00	10.14	12.41	125.87	0.484	No	Yes	0.64
1429	14.29	7.53	3.17	6.28	1.00	10.51	12.13	127.46	0.501	No	Yes	0.67
1430	14.30	7.77	3.16	6.26	1.00	10.88	11.86	128.99	0.519	No	Yes	0.69
1431	14.31	7.99	3.15	6.24	1.00	11.22	11.62	130.40	0.535	No	Yes	0.71
1432	14.32	8.19	3.14	6.23	1.00	11.52	11.42	131.60	0.550	No	Yes	0.73
1433	14.33	8.34	3.13	6.22	1.00	11.76	11.27	132.50	0.561	No	Yes	0.75
1434	14.34	8.47	3.13	6.20	1.00	11.96	11.14	133.18	0.570	No	Yes	0.76
1435	14.35	8.60	3.12	6.18	1.00	12.15	11.01	133.76	0.580	No	Yes	0.77
1436	14.36	8.74	3.11	6.15	1.00	12.37	10.86	134.41	0.590	No	Yes	0.78
1437	14.37	8.90	3.10	6.12	1.00	12.61	10.71	135.10	0.602	No	Yes	0.80
1438	14.38	9.06	3.10	6.09	1.00	12.86	10.56	135.78	0.613	No	Yes	0.81
1439	14.39	9.22	3.09	6.07	1.00	13.09	10.42	136.42	0.625	No	Yes	0.83
1440	14.40	9.36	3.08	6.04	1.00	13.31	10.29	137.00	0.635	No	Yes	0.84

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1441	14.41	9.47	3.08	6.03	1.00	13.48	10.20	137.48	0.643	No	Yes	0.85
1442	14.42	9.51	3.08	6.04	1.00	13.54	10.18	137.87	0.646	No	Yes	0.86
1443	14.43	9.49	3.08	6.08	1.00	13.50	10.24	138.25	0.644	No	Yes	0.85
1444	14.44	9.42	3.09	6.15	1.00	13.39	10.35	138.65	0.639	No	Yes	0.85
1445	14.45	9.35	3.09	6.23	1.00	13.27	10.48	139.09	0.633	No	Yes	0.84
1446	14.46	9.27	3.10	6.32	1.00	13.14	10.62	139.54	0.627	No	Yes	0.83
1447	14.47	9.19	3.11	6.40	1.00	13.01	10.76	139.97	0.620	No	Yes	0.82
1448	14.48	9.11	3.11	6.48	1.00	12.88	10.90	140.36	0.615	No	Yes	0.81
1449	14.49	9.05	3.12	6.56	1.00	12.77	11.02	140.70	0.609	No	Yes	0.81
1450	14.50	8.95	3.13	6.63	1.00	12.62	11.16	140.80	0.602	No	Yes	0.80
1451	14.51	8.79	3.14	6.71	1.00	12.35	11.37	140.49	0.589	No	Yes	0.78
1452	14.52	8.53	3.15	6.81	1.00	11.95	11.69	139.70	0.570	No	Yes	0.75
1453	14.53	8.20	3.17	6.93	1.00	11.43	12.12	138.56	0.545	No	Yes	0.72
1454	14.54	7.84	3.20	7.08	1.00	10.87	12.62	137.17	0.518	No	Yes	0.69
1455	14.55	7.47	3.22	7.24	1.00	10.28	13.18	135.57	0.491	No	Yes	0.65
1456	14.56	7.10	3.24	7.40	1.00	9.71	13.79	133.84	0.463	No	Yes	0.61
1457	14.57	6.76	3.27	7.55	1.00	9.17	14.40	132.06	0.437	No	Yes	0.58
1458	14.58	6.45	3.29	7.70	1.00	8.70	14.99	130.38	0.415	No	Yes	0.55
1459	14.59	6.23	3.31	7.81	1.00	8.35	15.45	129.06	0.398	No	Yes	0.53
1460	14.60	6.07	3.32	7.89	1.00	8.10	15.81	128.02	0.386	No	Yes	0.51
1461	14.61	5.94	3.33	7.95	1.00	7.90	16.10	127.12	0.377	No	Yes	0.50
1462	14.62	5.80	3.35	8.02	1.00	7.67	16.45	126.07	0.366	No	Yes	0.48
1463	14.63	5.64	3.36	8.10	1.00	7.42	16.84	124.92	0.354	No	Yes	0.47
1464	14.64	5.48	3.37	8.18	1.00	7.17	17.26	123.70	0.342	No	Yes	0.45
1465	14.65	5.33	3.39	8.27	1.00	6.92	17.69	122.49	0.330	No	Yes	0.44
1466	14.66	5.18	3.40	8.35	1.00	6.70	18.11	121.34	0.320	No	Yes	0.42
1467	14.67	5.08	3.41	8.41	1.00	6.53	18.44	120.47	0.312	No	Yes	0.41
1468	14.68	5.05	3.42	8.43	1.00	6.49	18.53	120.25	0.310	No	Yes	0.41
1469	14.69	5.11	3.41	8.41	1.00	6.57	18.37	120.70	0.313	No	Yes	0.41
1470	14.70	5.22	3.40	8.35	1.00	6.74	18.05	121.64	0.321	No	Yes	0.42
1471	14.71	5.34	3.39	8.29	1.00	6.93	17.70	122.67	0.331	No	Yes	0.44
1472	14.72	5.48	3.38	8.22	1.00	7.13	17.35	123.73	0.340	No	Yes	0.45
1473	14.73	5.61	3.37	8.16	1.00	7.33	17.01	124.77	0.350	No	Yes	0.46
1474	14.74	5.73	3.36	8.11	1.00	7.53	16.71	125.73	0.359	No	Yes	0.47
1475	14.75	5.85	3.35	8.06	1.00	7.70	16.45	126.58	0.367	No	Yes	0.48
1476	14.76	5.93	3.34	8.02	1.00	7.82	16.26	127.12	0.373	No	Yes	0.49
1477	14.77	5.97	3.34	7.99	1.00	7.88	16.16	127.28	0.376	No	Yes	0.49
1478	14.78	5.98	3.33	7.96	1.00	7.89	16.11	127.11	0.376	No	Yes	0.49
1479	14.79	5.98	3.33	7.92	1.00	7.88	16.08	126.80	0.376	No	Yes	0.49
1480	14.80	5.98	3.33	7.88	1.00	7.88	16.05	126.45	0.376	No	Yes	0.49
1481	14.81	5.98	3.33	7.83	1.00	7.88	16.01	126.10	0.376	No	Yes	0.49
1482	14.82	5.98	3.33	7.79	1.00	7.87	15.97	125.75	0.376	No	Yes	0.49
1483	14.83	5.98	3.33	7.75	1.00	7.87	15.94	125.43	0.375	No	Yes	0.49
1484	14.84	5.98	3.33	7.72	1.00	7.87	15.91	125.14	0.375	No	Yes	0.49
1485	14.85	6.01	3.32	7.67	1.00	7.91	15.81	125.13	0.377	No	Yes	0.50
1486	14.86	6.09	3.32	7.62	1.00	8.03	15.62	125.42	0.383	No	Yes	0.50
1487	14.87	6.21	3.31	7.54	1.00	8.22	15.33	126.02	0.392	No	Yes	0.51
1488	14.88	6.36	3.29	7.45	1.00	8.44	15.01	126.69	0.403	No	Yes	0.53

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1489	14.89	6.52	3.28	7.35	1.00	8.68	14.68	127.37	0.414	No	Yes	0.54
1490	14.90	6.68	3.27	7.26	1.00	8.92	14.35	128.03	0.425	No	Yes	0.56
1491	14.91	6.83	3.26	7.17	1.00	9.15	14.05	128.63	0.437	No	Yes	0.57
1492	14.92	6.98	3.24	7.09	1.00	9.37	13.79	129.14	0.447	No	Yes	0.59
1493	14.93	7.10	3.24	7.02	1.00	9.55	13.57	129.55	0.455	No	Yes	0.60
1494	14.94	7.21	3.23	6.96	1.00	9.71	13.37	129.90	0.463	No	Yes	0.61
1495	14.95	7.32	3.22	6.89	1.00	9.89	13.17	130.23	0.472	No	Yes	0.62
1496	14.96	7.46	3.21	6.82	1.00	10.09	12.94	130.58	0.481	No	Yes	0.63
1497	14.97	7.61	3.20	6.73	1.00	10.32	12.70	130.95	0.492	No	Yes	0.64
1498	14.98	7.77	3.19	6.65	1.00	10.55	12.44	131.31	0.503	No	Yes	0.66
1499	14.99	7.93	3.18	6.56	1.00	10.79	12.20	131.63	0.515	No	Yes	0.67
1500	15.00	8.08	3.17	6.48	1.00	11.02	11.97	131.90	0.526	No	Yes	0.69
1501	15.01	8.21	3.16	6.41	1.00	11.22	11.77	132.12	0.535	No	Yes	0.70
1502	15.02	8.28	3.15	6.36	1.00	11.32	11.67	132.11	0.540	No	Yes	0.71
1503	15.03	8.26	3.15	6.35	1.00	11.28	11.68	131.77	0.538	No	Yes	0.70
1504	15.04	8.14	3.16	6.36	1.00	11.10	11.81	131.06	0.529	No	Yes	0.69
1505	15.05	7.98	3.17	6.39	1.00	10.84	12.00	130.11	0.517	No	Yes	0.68
1506	15.06	7.80	3.18	6.42	1.00	10.56	12.22	129.06	0.504	No	Yes	0.66
1507	15.07	7.61	3.19	6.45	1.00	10.27	12.46	127.95	0.490	No	Yes	0.64
1508	15.08	7.43	3.20	6.48	1.00	9.99	12.70	126.83	0.476	No	Yes	0.62
1509	15.09	7.26	3.21	6.51	1.00	9.72	12.94	125.76	0.464	No	Yes	0.61
1510	15.10	7.11	3.22	6.54	1.00	9.49	13.15	124.81	0.453	No	Yes	0.59
1511	15.11	7.03	3.22	6.57	1.00	9.37	13.29	124.51	0.447	No	Yes	0.58
1512	15.12	7.03	3.23	6.62	1.00	9.37	13.34	124.93	0.447	No	Yes	0.58
1513	15.13	7.09	3.23	6.69	1.00	9.46	13.32	126.03	0.451	No	Yes	0.59
1514	15.14	7.17	3.22	6.76	1.00	9.57	13.31	127.31	0.456	No	Yes	0.59
1515	15.15	7.25	3.22	6.84	1.00	9.68	13.29	128.69	0.462	No	Yes	0.60
1516	15.16	7.33	3.22	6.93	1.00	9.80	13.27	130.08	0.467	No	Yes	0.61
1517	15.17	7.40	3.22	7.01	1.00	9.91	13.26	131.43	0.473	No	Yes	0.62
1518	15.18	7.47	3.22	7.08	1.00	10.02	13.25	132.67	0.478	No	Yes	0.62
1519	15.19	7.55	3.22	7.14	1.00	10.13	13.21	133.79	0.483	No	Yes	0.63
1520	15.20	7.68	3.22	7.16	1.00	10.32	13.09	135.08	0.492	No	Yes	0.64
1521	15.21	7.89	3.21	7.16	1.00	10.63	12.86	136.71	0.507	No	Yes	0.66
1522	15.22	8.17	3.19	7.14	1.00	11.05	12.56	138.73	0.527	No	Yes	0.69
1523	15.23	8.48	3.18	7.13	1.00	11.52	12.24	140.96	0.549	No	Yes	0.71
1524	15.24	8.81	3.16	7.12	1.00	12.01	11.92	143.25	0.573	No	Yes	0.74
1525	15.25	9.14	3.15	7.11	1.00	12.51	11.63	145.49	0.597	No	Yes	0.78
1526	15.26	9.45	3.14	7.10	1.00	12.97	11.37	147.58	0.619	No	Yes	0.80
1527	15.27	9.73	3.13	7.09	1.00	13.39	11.16	149.40	0.639	No	Yes	0.83
1528	15.28	9.98	3.12	7.07	1.00	13.76	10.96	150.84	0.656	No	Yes	0.85
1529	15.29	10.24	3.11	7.03	1.00	14.14	10.75	151.99	0.675	No	Yes	0.88
1530	15.30	10.54	3.09	6.95	1.00	14.59	10.49	153.01	0.696	No	Yes	0.90
1531	15.31	10.89	3.08	6.86	1.00	15.12	10.19	154.06	0.721	No	Yes	0.94
1532	15.32	11.28	3.06	6.76	1.00	15.70	9.88	155.12	0.749	No	Yes	0.97
1533	15.33	11.68	3.05	6.66	1.00	16.30	9.58	156.11	0.777	No	Yes	1.01
1534	15.34	12.07	3.03	6.56	1.00	16.88	9.30	156.99	0.805	No	Yes	1.04
1535	15.35	12.44	3.02	6.47	1.00	17.43	9.05	157.72	0.831	No	Yes	1.08
1536	15.36	12.75	3.00	6.40	1.00	17.90	8.84	158.29	0.854	No	Yes	1.11

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1537	15.37	13.02	2.99	6.33	1.00	18.30	8.67	158.66	0.873	No	Yes	1.13
1538	15.38	13.27	2.98	6.27	1.00	18.67	8.51	158.89	0.890	No	Yes	1.15
1539	15.39	13.54	2.97	6.19	1.00	19.06	8.34	159.04	0.909	No	Yes	1.18
1540	15.40	13.85	2.96	6.10	1.00	19.52	8.15	159.15	0.931	No	Yes	1.21
1541	15.41	14.18	2.95	6.01	1.00	20.01	7.96	159.21	0.954	No	Yes	1.24
1542	15.42	14.52	2.94	5.92	1.00	20.51	7.76	159.20	0.978	No	Yes	1.27
1543	15.43	14.84	2.93	5.83	1.00	20.95	7.59	159.01	0.999	No	Yes	1.29
1544	15.44	15.14	2.92	5.75	0.99	21.34	7.44	158.78	1.018	No	Yes	1.32
1545	15.45	15.34	2.91	5.69	0.99	21.61	7.33	158.46	1.031	No	Yes	1.33
1546	15.46	15.33	2.91	5.65	0.99	21.58	7.31	157.78	1.030	No	Yes	1.33
1547	15.47	15.11	2.91	5.63	0.99	21.26	7.37	156.64	1.014	No	Yes	1.31
1548	15.48	14.74	2.92	5.63	0.99	20.72	7.49	155.11	0.988	No	Yes	1.28
1549	15.49	14.32	2.93	5.62	1.00	20.12	7.62	153.37	0.960	No	Yes	1.24
1550	15.50	13.88	2.94	5.61	1.00	19.49	7.77	151.49	0.929	No	Yes	1.20
1551	15.51	13.45	2.95	5.60	1.00	18.82	7.94	149.51	0.898	No	Yes	1.16
1552	15.52	13.03	2.96	5.60	1.00	18.19	8.11	147.60	0.868	No	Yes	1.12
1553	15.53	12.66	2.97	5.59	1.00	17.63	8.27	145.87	0.841	No	Yes	1.09
1554	15.54	12.35	2.98	5.60	1.00	17.15	8.42	144.50	0.818	No	Yes	1.06
1555	15.55	12.06	2.99	5.62	1.00	16.71	8.58	143.44	0.797	No	Yes	1.03
1556	15.56	11.75	3.00	5.66	1.00	16.25	8.77	142.51	0.775	No	Yes	1.00
1557	15.57	11.40	3.01	5.71	1.00	15.71	9.01	141.45	0.749	No	Yes	0.97
1558	15.58	11.01	3.03	5.77	1.00	15.12	9.27	140.22	0.721	No	Yes	0.93
1559	15.59	10.61	3.04	5.83	1.00	14.52	9.57	138.88	0.692	No	Yes	0.89
1560	15.60	10.22	3.06	5.89	1.00	13.92	9.88	137.48	0.664	No	Yes	0.86
1561	15.61	9.85	3.08	5.95	1.00	13.37	10.18	136.11	0.638	No	Yes	0.82
1562	15.62	9.54	3.09	6.00	1.00	12.89	10.46	134.86	0.615	No	Yes	0.79
1563	15.63	9.34	3.10	6.05	1.00	12.59	10.66	134.15	0.601	No	Yes	0.77
1564	15.64	9.24	3.11	6.09	1.00	12.43	10.78	133.96	0.593	No	Yes	0.76
1565	15.65	9.20	3.11	6.13	1.00	12.38	10.84	134.21	0.590	No	Yes	0.76
1566	15.66	9.17	3.12	6.18	1.00	12.32	10.92	134.50	0.588	No	Yes	0.76
1567	15.67	9.13	3.12	6.23	1.00	12.25	11.00	134.80	0.585	No	Yes	0.75
1568	15.68	9.09	3.12	6.28	1.00	12.19	11.08	135.10	0.581	No	Yes	0.75
1569	15.69	9.05	3.13	6.33	1.00	12.13	11.16	135.38	0.578	No	Yes	0.74
1570	15.70	9.01	3.13	6.38	1.00	12.07	11.24	135.63	0.576	No	Yes	0.74
1571	15.71	8.98	3.13	6.42	1.00	12.02	11.30	135.82	0.573	No	Yes	0.74
1572	15.72	8.94	3.14	6.45	1.00	11.95	11.37	135.92	0.570	No	Yes	0.73
1573	15.73	8.89	3.14	6.49	1.00	11.87	11.46	135.95	0.566	No	Yes	0.73
1574	15.74	8.82	3.15	6.53	1.00	11.76	11.56	135.95	0.561	No	Yes	0.72
1575	15.75	8.74	3.15	6.58	1.00	11.64	11.68	135.93	0.555	No	Yes	0.71
1576	15.76	8.66	3.16	6.64	1.00	11.52	11.80	135.90	0.549	No	Yes	0.71
1577	15.77	8.58	3.16	6.69	1.00	11.40	11.92	135.87	0.544	No	Yes	0.70
1578	15.78	8.51	3.17	6.74	1.00	11.28	12.04	135.83	0.538	No	Yes	0.69
1579	15.79	8.44	3.17	6.79	1.00	11.17	12.15	135.78	0.533	No	Yes	0.68
1580	15.80	8.38	3.18	6.82	1.00	11.08	12.24	135.67	0.529	No	Yes	0.68
1581	15.81	8.33	3.18	6.84	1.00	11.00	12.32	135.46	0.525	No	Yes	0.67
1582	15.82	8.27	3.19	6.86	1.00	10.90	12.40	135.13	0.520	No	Yes	0.67
1583	15.83	8.20	3.19	6.87	1.00	10.79	12.48	134.71	0.515	No	Yes	0.66
1584	15.84	8.12	3.19	6.89	1.00	10.67	12.58	134.26	0.509	No	Yes	0.65

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1585	15.85	8.04	3.20	6.90	1.00	10.55	12.68	133.79	0.503	No	Yes	0.65
1586	15.86	7.96	3.20	6.92	1.00	10.43	12.79	133.32	0.497	No	Yes	0.64
1587	15.87	7.89	3.21	6.93	1.00	10.31	12.88	132.88	0.492	No	Yes	0.63
1588	15.88	7.82	3.21	6.95	1.00	10.22	12.97	132.49	0.487	No	Yes	0.62
1589	15.89	7.77	3.21	6.94	1.00	10.13	13.03	132.01	0.483	No	Yes	0.62
1590	15.90	7.71	3.22	6.93	1.00	10.04	13.08	131.37	0.479	No	Yes	0.61
1591	15.91	7.65	3.22	6.89	1.00	9.94	13.13	130.52	0.474	No	Yes	0.61
1592	15.92	7.57	3.22	6.85	1.00	9.83	13.18	129.54	0.469	No	Yes	0.60
1593	15.93	7.49	3.22	6.81	1.00	9.71	13.24	128.51	0.463	No	Yes	0.59
1594	15.94	7.41	3.22	6.77	1.00	9.58	13.30	127.45	0.457	No	Yes	0.59
1595	15.95	7.34	3.23	6.73	1.00	9.47	13.36	126.44	0.452	No	Yes	0.58
1596	15.96	7.27	3.23	6.69	1.00	9.36	13.41	125.52	0.446	No	Yes	0.57
1597	15.97	7.21	3.23	6.66	1.00	9.28	13.45	124.78	0.442	No	Yes	0.57
1598	15.98	7.18	3.23	6.63	1.00	9.23	13.47	124.26	0.440	No	Yes	0.56
1599	15.99	7.17	3.23	6.60	1.00	9.21	13.45	123.90	0.439	No	Yes	0.56
1600	16.00	7.17	3.23	6.57	1.00	9.21	13.42	123.58	0.439	No	Yes	0.56
1601	16.01	7.17	3.23	6.53	1.00	9.20	13.39	123.22	0.439	No	Yes	0.56
1602	16.02	7.17	3.23	6.49	1.00	9.20	13.36	122.84	0.439	No	Yes	0.56
1603	16.03	7.17	3.23	6.46	1.00	9.19	13.32	122.47	0.439	No	Yes	0.56
1604	16.04	7.17	3.22	6.42	1.00	9.19	13.29	122.11	0.438	No	Yes	0.56
1605	16.05	7.17	3.22	6.39	1.00	9.19	13.26	121.79	0.438	No	Yes	0.56
1606	16.06	7.17	3.22	6.37	1.00	9.18	13.25	121.62	0.438	No	Yes	0.56
1607	16.07	7.17	3.22	6.37	1.00	9.18	13.25	121.64	0.438	No	Yes	0.56
1608	16.08	7.17	3.22	6.40	1.00	9.17	13.28	121.85	0.438	No	Yes	0.56
1609	16.09	7.17	3.23	6.43	1.00	9.17	13.32	122.13	0.437	No	Yes	0.56
1610	16.10	7.17	3.23	6.47	1.00	9.17	13.36	122.43	0.437	No	Yes	0.56
1611	16.11	7.17	3.23	6.50	1.00	9.16	13.40	122.74	0.437	No	Yes	0.56
1612	16.12	7.17	3.23	6.54	1.00	9.16	13.44	123.05	0.437	No	Yes	0.56
1613	16.13	7.17	3.23	6.57	1.00	9.15	13.47	123.33	0.437	No	Yes	0.56
1614	16.14	7.17	3.23	6.60	1.00	9.15	13.50	123.58	0.436	No	Yes	0.56
1615	16.15	7.17	3.23	6.63	1.00	9.15	13.54	123.86	0.436	No	Yes	0.56
1616	16.16	7.17	3.24	6.68	1.00	9.14	13.59	124.22	0.436	No	Yes	0.56
1617	16.17	7.17	3.24	6.73	1.00	9.14	13.64	124.70	0.436	No	Yes	0.56
1618	16.18	7.17	3.24	6.80	1.00	9.14	13.71	125.25	0.436	No	Yes	0.55
1619	16.19	7.17	3.24	6.86	1.00	9.13	13.78	125.84	0.436	No	Yes	0.55
1620	16.20	7.17	3.25	6.93	1.00	9.13	13.85	126.43	0.435	No	Yes	0.55
1621	16.21	7.17	3.25	7.00	1.00	9.12	13.92	126.99	0.435	No	Yes	0.55
1622	16.22	7.17	3.25	7.06	1.00	9.12	13.98	127.50	0.435	No	Yes	0.55
1623	16.23	7.20	3.25	7.10	1.00	9.16	13.99	128.08	0.437	No	Yes	0.56
1624	16.24	7.31	3.25	7.12	1.00	9.30	13.87	129.09	0.444	No	Yes	0.56
1625	16.25	7.50	3.24	7.12	1.00	9.59	13.62	130.64	0.457	No	Yes	0.58
1626	16.26	7.78	3.22	7.10	1.00	9.99	13.29	132.67	0.476	No	Yes	0.61
1627	16.27	8.08	3.21	7.08	1.00	10.43	12.94	134.89	0.497	No	Yes	0.63
1628	16.28	8.40	3.19	7.07	1.00	10.89	12.60	137.16	0.519	No	Yes	0.66
1629	16.29	8.72	3.18	7.06	1.00	11.35	12.28	139.37	0.541	No	Yes	0.69
1630	16.30	9.02	3.17	7.05	1.00	11.78	12.01	141.42	0.562	No	Yes	0.71
1631	16.31	9.28	3.16	7.04	1.00	12.16	11.77	143.20	0.580	No	Yes	0.74
1632	16.32	9.53	3.15	7.02	1.00	12.51	11.56	144.64	0.597	No	Yes	0.76

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1633	16.33	9.78	3.14	6.98	1.00	12.88	11.33	145.88	0.614	No	Yes	0.78
1634	16.34	10.09	3.12	6.91	1.00	13.32	11.04	147.08	0.635	No	Yes	0.81
1635	16.35	10.44	3.11	6.83	1.00	13.83	10.73	148.37	0.660	No	Yes	0.84
1636	16.36	10.83	3.09	6.74	1.00	14.39	10.40	149.69	0.687	No	Yes	0.87
1637	16.37	11.23	3.07	6.65	1.00	14.97	10.08	150.96	0.714	No	Yes	0.91
1638	16.38	11.63	3.06	6.57	1.00	15.53	9.79	152.10	0.741	No	Yes	0.94
1639	16.39	11.99	3.04	6.50	1.00	16.05	9.54	153.09	0.766	No	Yes	0.97
1640	16.40	12.30	3.03	6.43	1.00	16.51	9.32	153.87	0.787	No	Yes	1.00
1641	16.41	12.60	3.02	6.36	1.00	16.93	9.12	154.42	0.808	No	Yes	1.02
1642	16.42	12.93	3.01	6.27	1.00	17.40	8.90	154.78	0.830	No	Yes	1.05
1643	16.43	13.32	2.99	6.15	1.00	17.96	8.63	155.01	0.857	No	Yes	1.08
1644	16.44	13.76	2.97	6.02	1.00	18.60	8.34	155.16	0.887	No	Yes	1.12
1645	16.45	14.24	2.96	5.89	1.00	19.28	8.05	155.18	0.919	No	Yes	1.16
1646	16.46	14.72	2.94	5.75	1.00	19.96	7.77	155.07	0.952	No	Yes	1.21
1647	16.47	15.18	2.92	5.63	1.00	20.58	7.52	154.71	0.982	No	Yes	1.24
1648	16.48	15.60	2.91	5.51	0.99	21.13	7.30	154.26	1.008	No	Yes	1.28
1649	16.49	15.98	2.89	5.41	0.99	21.62	7.12	153.86	1.031	No	Yes	1.30
1650	16.50	16.39	2.88	5.32	0.98	22.16	6.93	153.57	1.057	No	Yes	1.34
1651	16.51	16.89	2.87	5.22	0.97	22.82	6.72	153.35	1.088	No	Yes	1.38
1652	16.52	17.51	2.85	5.10	0.97	23.62	6.48	153.05	1.127	No	Yes	1.42
1653	16.53	18.19	2.83	4.98	0.96	24.52	6.22	152.57	1.169	No	Yes	1.48
1654	16.54	18.91	2.81	4.85	0.95	25.45	5.97	151.89	1.214	No	Yes	1.53
1655	16.55	19.63	2.79	4.72	0.95	26.37	5.73	151.05	1.258	No	Yes	1.59
1656	16.56	20.30	2.77	4.60	0.94	27.23	5.51	150.11	1.299	No	Yes	1.64
1657	16.57	20.90	2.76	4.49	0.93	27.99	5.33	149.16	1.335	No	Yes	1.69
1658	16.58	21.30	2.75	4.41	0.93	28.49	5.20	148.14	1.359	No	Yes	1.72
1659	16.59	21.52	2.74	4.33	0.93	28.75	5.11	146.91	1.372	No	Yes	1.73
1660	16.60	21.60	2.73	4.25	0.92	28.82	5.04	145.35	1.375	No	Yes	1.74
1661	16.61	21.66	2.72	4.17	0.92	28.86	4.97	143.49	1.377	No	Yes	1.74
1662	16.62	21.72	2.72	4.07	0.92	28.90	4.89	141.45	1.379	No	Yes	1.74
1663	16.63	21.78	2.71	3.98	0.92	28.95	4.81	139.33	1.381	No	Yes	1.74
1664	16.64	21.84	2.70	3.88	0.91	28.99	4.73	137.23	1.383	No	Yes	1.74
1665	16.65	21.90	2.70	3.80	0.91	29.02	9.91	287.62	3.600	No	No	2.00
1666	16.66	21.94	2.69	3.72	0.91	29.04	9.56	277.58	3.600	No	No	2.00
1667	16.67	21.87	2.69	3.68	0.91	28.92	9.43	272.83	3.600	No	No	2.00
1668	16.68	21.67	2.69	3.66	0.91	28.64	9.53	272.91	3.600	No	No	2.00
1669	16.69	21.34	2.69	3.66	0.91	28.20	9.82	276.91	3.600	No	No	2.00
1670	16.70	20.97	2.70	3.65	0.91	27.70	10.17	281.60	3.600	No	No	2.00
1671	16.71	20.58	2.71	3.65	0.91	27.17	4.77	129.54	1.296	No	Yes	1.63
1672	16.72	20.18	2.71	3.65	0.92	26.63	4.83	128.76	1.270	No	Yes	1.60
1673	16.73	19.79	2.72	3.64	0.92	26.12	4.90	128.01	1.246	No	Yes	1.57
1674	16.74	19.45	2.72	3.64	0.92	25.65	4.96	127.32	1.223	No	Yes	1.54
1675	16.75	19.15	2.73	3.65	0.92	25.25	5.03	126.92	1.204	No	Yes	1.52
1676	16.76	18.88	2.74	3.68	0.93	24.89	5.10	127.07	1.187	No	Yes	1.49
1677	16.77	18.59	2.75	3.74	0.93	24.52	5.21	127.78	1.170	No	Yes	1.47
1678	16.78	18.26	2.76	3.82	0.93	24.10	5.35	128.83	1.150	No	Yes	1.45
1679	16.79	17.90	2.77	3.91	0.94	23.63	5.50	129.93	1.127	No	Yes	1.42
1680	16.80	17.51	2.78	4.00	0.94	23.14	5.66	131.02	1.104	No	Yes	1.39

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1681	16.81	17.13	2.80	4.09	0.95	22.64	5.83	132.04	1.080	No	Yes	1.36
1682	16.82	16.78	2.81	4.18	0.95	22.18	5.99	132.93	1.058	No	Yes	1.33
1683	16.83	16.46	2.82	4.26	0.96	21.76	6.14	133.67	1.038	No	Yes	1.30
1684	16.84	16.15	2.83	4.34	0.96	21.36	6.29	134.32	1.019	No	Yes	1.28
1685	16.85	15.79	2.85	4.43	0.97	20.88	6.46	134.99	0.996	No	Yes	1.25
1686	16.86	15.33	2.86	4.54	0.97	20.28	6.69	135.72	0.968	No	Yes	1.22
1687	16.87	14.79	2.88	4.67	0.98	19.58	6.97	136.46	0.934	No	Yes	1.17
1688	16.88	14.21	2.91	4.82	0.99	18.80	7.29	137.09	0.897	No	Yes	1.13
1689	16.89	13.61	2.93	4.98	1.00	18.01	7.64	137.54	0.859	No	Yes	1.08
1690	16.90	13.02	2.95	5.13	1.00	17.17	8.01	137.62	0.819	No	Yes	1.03
1691	16.91	12.48	2.98	5.27	1.00	16.39	8.39	137.50	0.782	No	Yes	0.98
1692	16.92	12.02	3.00	5.40	1.00	15.74	8.72	137.27	0.751	No	Yes	0.94
1693	16.93	11.69	3.01	5.50	1.00	15.26	8.99	137.19	0.728	No	Yes	0.91
1694	16.94	11.46	3.02	5.60	1.00	14.92	9.20	137.31	0.712	No	Yes	0.89
1695	16.95	11.26	3.04	5.70	1.00	14.64	9.40	137.62	0.698	No	Yes	0.88
1696	16.96	11.04	3.05	5.81	1.00	14.31	9.64	137.92	0.683	No	Yes	0.86
1697	16.97	10.80	3.06	5.93	1.00	13.97	9.89	138.18	0.666	No	Yes	0.84
1698	16.98	10.56	3.08	6.05	1.00	13.62	10.16	138.37	0.650	No	Yes	0.81
1699	16.99	10.33	3.09	6.17	1.00	13.29	10.42	138.49	0.634	No	Yes	0.79
1700	17.00	10.12	3.10	6.28	1.00	12.99	10.67	138.54	0.620	No	Yes	0.78
1701	17.01	9.98	3.11	6.37	1.00	12.78	10.84	138.59	0.610	No	Yes	0.76
1702	17.02	9.94	3.11	6.40	1.00	12.72	10.91	138.74	0.607	No	Yes	0.76
1703	17.03	9.99	3.11	6.40	1.00	12.79	10.87	139.03	0.610	No	Yes	0.76
1704	17.04	10.10	3.11	6.38	1.00	12.93	10.78	139.42	0.617	No	Yes	0.77
1705	17.05	10.21	3.10	6.36	1.00	13.09	10.69	139.85	0.624	No	Yes	0.78
1706	17.06	10.33	3.10	6.34	1.00	13.25	10.59	140.29	0.632	No	Yes	0.79
1707	17.07	10.45	3.09	6.32	1.00	13.41	10.49	140.71	0.640	No	Yes	0.80
1708	17.08	10.56	3.09	6.30	1.00	13.57	10.40	141.11	0.647	No	Yes	0.81
1709	17.09	10.66	3.09	6.29	1.00	13.70	10.32	141.45	0.654	No	Yes	0.82
1710	17.10	10.73	3.08	6.26	1.00	13.79	10.26	141.47	0.658	No	Yes	0.82
1711	17.11	10.76	3.08	6.21	1.00	13.82	10.20	141.07	0.659	No	Yes	0.82
1712	17.12	10.76	3.08	6.14	1.00	13.82	10.14	140.23	0.659	No	Yes	0.82
1713	17.13	10.76	3.07	6.06	1.00	13.82	10.07	139.19	0.659	No	Yes	0.82
1714	17.14	10.76	3.07	5.97	1.00	13.81	10.00	138.07	0.659	No	Yes	0.82
1715	17.15	10.76	3.06	5.88	1.00	13.81	9.92	136.90	0.659	No	Yes	0.82
1716	17.16	10.76	3.06	5.79	1.00	13.80	9.84	135.76	0.658	No	Yes	0.82
1717	17.17	10.76	3.06	5.70	1.00	13.79	9.76	134.70	0.658	No	Yes	0.82
1718	17.18	10.75	3.05	5.63	1.00	13.77	9.71	133.75	0.657	No	Yes	0.82
1719	17.19	10.66	3.05	5.59	1.00	13.64	9.73	132.69	0.651	No	Yes	0.81
1720	17.20	10.47	3.06	5.56	1.00	13.37	9.82	131.34	0.638	No	Yes	0.80
1721	17.21	10.18	3.07	5.54	1.00	12.96	10.00	129.60	0.618	No	Yes	0.77
1722	17.22	9.86	3.08	5.52	1.00	12.50	10.21	127.61	0.596	No	Yes	0.74
1723	17.23	9.52	3.09	5.50	1.00	12.01	10.45	125.47	0.573	No	Yes	0.71
1724	17.24	9.17	3.10	5.48	1.00	11.52	10.70	123.28	0.549	No	Yes	0.68
1725	17.25	8.84	3.12	5.46	1.00	11.05	10.97	121.16	0.527	No	Yes	0.66
1726	17.26	8.54	3.13	5.45	1.00	10.62	11.23	119.22	0.507	No	Yes	0.63
1727	17.27	8.28	3.14	5.44	1.00	10.26	11.47	117.62	0.489	No	Yes	0.61
1728	17.28	8.04	3.15	5.46	1.00	9.91	11.73	116.28	0.473	No	Yes	0.59

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1729	17.29	7.79	3.17	5.50	1.00	9.55	12.05	115.02	0.455	No	Yes	0.57
1730	17.30	7.49	3.19	5.56	1.00	9.12	12.45	113.58	0.435	No	Yes	0.54
1731	17.31	7.15	3.21	5.62	1.00	8.65	12.93	111.90	0.413	No	Yes	0.51
1732	17.32	6.81	3.23	5.70	1.00	8.16	13.49	110.07	0.389	No	Yes	0.48
1733	17.33	6.46	3.26	5.78	1.00	7.68	14.09	108.16	0.366	No	Yes	0.46
1734	17.34	6.14	3.28	5.86	1.00	7.22	14.72	106.27	0.344	No	Yes	0.43
1735	17.35	5.86	3.31	5.94	1.00	6.82	15.33	104.53	0.325	No	Yes	0.40
1736	17.36	5.68	3.32	6.01	1.00	6.56	15.76	103.44	0.313	No	Yes	0.39
1737	17.37	5.60	3.33	6.05	1.00	6.46	15.97	103.09	0.308	No	Yes	0.38
1738	17.38	5.62	3.33	6.08	1.00	6.47	15.98	103.40	0.309	No	Yes	0.38
1739	17.39	5.64	3.33	6.11	1.00	6.50	15.98	103.84	0.310	No	Yes	0.39
1740	17.40	5.67	3.33	6.14	1.00	6.53	15.97	104.31	0.312	No	Yes	0.39
1741	17.41	5.69	3.33	6.18	1.00	6.57	15.96	104.80	0.313	No	Yes	0.39
1742	17.42	5.72	3.33	6.21	1.00	6.60	15.95	105.28	0.315	No	Yes	0.39
1743	17.43	5.74	3.33	6.24	1.00	6.63	15.94	105.72	0.316	No	Yes	0.39
1744	17.44	5.76	3.33	6.27	1.00	6.66	15.93	106.09	0.318	No	Yes	0.39
1745	17.45	5.78	3.33	6.30	1.00	6.68	15.93	106.44	0.319	No	Yes	0.40
1746	17.46	5.80	3.33	6.32	1.00	6.71	15.93	106.82	0.320	No	Yes	0.40
1747	17.47	5.82	3.33	6.36	1.00	6.73	15.93	107.26	0.321	No	Yes	0.40
1748	17.48	5.85	3.33	6.40	1.00	6.77	15.93	107.77	0.323	No	Yes	0.40
1749	17.49	5.87	3.33	6.44	1.00	6.80	15.93	108.31	0.324	No	Yes	0.40
1750	17.50	5.90	3.33	6.48	1.00	6.84	15.92	108.85	0.326	No	Yes	0.40
1751	17.51	5.93	3.33	6.52	1.00	6.87	15.92	109.36	0.328	No	Yes	0.41
1752	17.52	5.95	3.33	6.56	1.00	6.90	15.92	109.83	0.329	No	Yes	0.41
1753	17.53	5.98	3.33	6.58	1.00	6.94	15.89	110.34	0.331	No	Yes	0.41
1754	17.54	6.05	3.32	6.61	1.00	7.03	15.80	111.10	0.335	No	Yes	0.42
1755	17.55	6.16	3.32	6.63	1.00	7.18	15.63	112.20	0.342	No	Yes	0.42
1756	17.56	6.30	3.31	6.65	1.00	7.37	15.42	113.60	0.352	No	Yes	0.44
1757	17.57	6.45	3.30	6.68	1.00	7.58	15.19	115.13	0.362	No	Yes	0.45
1758	17.58	6.61	3.29	6.71	1.00	7.80	14.96	116.72	0.372	No	Yes	0.46
1759	17.59	6.77	3.28	6.74	1.00	8.02	14.75	118.29	0.382	No	Yes	0.47
1760	17.60	6.92	3.28	6.77	1.00	8.22	14.57	119.75	0.392	No	Yes	0.49
1761	17.61	7.05	3.27	6.80	1.00	8.40	14.41	121.03	0.401	No	Yes	0.50
1762	17.62	7.16	3.26	6.82	1.00	8.55	14.28	122.12	0.408	No	Yes	0.50
1763	17.63	7.27	3.26	6.84	1.00	8.71	14.15	123.18	0.415	No	Yes	0.51
1764	17.64	7.40	3.25	6.86	1.00	8.88	14.00	124.34	0.423	No	Yes	0.52
1765	17.65	7.54	3.25	6.88	1.00	9.08	13.85	125.67	0.433	No	Yes	0.54
1766	17.66	7.70	3.24	6.91	1.00	9.29	13.68	127.11	0.443	No	Yes	0.55
1767	17.67	7.86	3.23	6.94	1.00	9.51	13.52	128.57	0.454	No	Yes	0.56
1768	17.68	8.02	3.23	6.96	1.00	9.72	13.37	129.99	0.464	No	Yes	0.57
1769	17.69	8.16	3.22	6.99	1.00	9.92	13.24	131.29	0.473	No	Yes	0.58
1770	17.70	8.27	3.22	7.01	1.00	10.07	13.14	132.32	0.480	No	Yes	0.59
1771	17.71	8.32	3.22	7.04	1.00	10.13	13.12	132.88	0.483	No	Yes	0.60
1772	17.72	8.30	3.22	7.07	1.00	10.10	13.17	133.00	0.482	No	Yes	0.60
1773	17.73	8.23	3.22	7.10	1.00	10.00	13.28	132.83	0.477	No	Yes	0.59
1774	17.74	8.16	3.23	7.15	1.00	9.90	13.40	132.64	0.472	No	Yes	0.58
1775	17.75	8.08	3.23	7.19	1.00	9.78	13.54	132.43	0.467	No	Yes	0.58
1776	17.76	8.00	3.24	7.24	1.00	9.67	13.68	132.21	0.461	No	Yes	0.57

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1777	17.77	7.92	3.25	7.29	1.00	9.56	13.81	131.99	0.456	No	Yes	0.56
1778	17.78	7.85	3.25	7.33	1.00	9.46	13.93	131.79	0.451	No	Yes	0.56
1779	17.79	7.80	3.26	7.36	1.00	9.37	14.04	131.62	0.447	No	Yes	0.55
1780	17.80	7.74	3.26	7.40	1.00	9.29	14.15	131.49	0.443	No	Yes	0.55
1781	17.81	7.68	3.26	7.45	1.00	9.21	14.27	131.39	0.439	No	Yes	0.54
1782	17.82	7.61	3.27	7.51	1.00	9.11	14.42	131.28	0.434	No	Yes	0.54
1783	17.83	7.53	3.28	7.57	1.00	9.00	14.58	131.15	0.429	No	Yes	0.53
1784	17.84	7.45	3.28	7.64	1.00	8.88	14.75	131.00	0.424	No	Yes	0.52
1785	17.85	7.38	3.29	7.70	1.00	8.77	14.92	130.84	0.418	No	Yes	0.52
1786	17.86	7.30	3.30	7.76	1.00	8.66	15.08	130.69	0.413	No	Yes	0.51
1787	17.87	7.24	3.30	7.82	1.00	8.57	15.23	130.54	0.409	No	Yes	0.50
1788	17.88	7.19	3.31	7.86	1.00	8.51	15.34	130.51	0.406	No	Yes	0.50
1789	17.89	7.18	3.31	7.90	1.00	8.48	15.41	130.64	0.404	No	Yes	0.50
1790	17.90	7.17	3.31	7.95	1.00	8.47	15.45	130.93	0.404	No	Yes	0.50
1791	17.91	7.17	3.31	7.99	1.00	8.47	15.50	131.28	0.404	No	Yes	0.50
1792	17.92	7.17	3.31	8.04	1.00	8.47	15.55	131.66	0.404	No	Yes	0.50
1793	17.93	7.17	3.32	8.09	1.00	8.46	15.60	132.05	0.404	No	Yes	0.50
1794	17.94	7.17	3.32	8.15	1.00	8.46	15.65	132.42	0.404	No	Yes	0.50
1795	17.95	7.17	3.32	8.19	1.00	8.46	15.70	132.76	0.403	No	Yes	0.50
1796	17.96	7.18	3.32	8.23	1.00	8.46	15.73	133.06	0.404	No	Yes	0.50
1797	17.97	7.21	3.32	8.24	1.00	8.50	15.70	133.39	0.405	No	Yes	0.50
1798	17.98	7.27	3.32	8.22	1.00	8.58	15.60	133.79	0.409	No	Yes	0.50
1799	17.99	7.36	3.31	8.19	1.00	8.70	15.45	134.31	0.415	No	Yes	0.51
1800	18.00	7.46	3.30	8.15	1.00	8.83	15.28	134.88	0.421	No	Yes	0.52
1801	18.01	7.56	3.30	8.11	1.00	8.97	15.10	135.47	0.428	No	Yes	0.53
1802	18.02	7.67	3.29	8.07	1.00	9.11	14.93	136.06	0.435	No	Yes	0.53
1803	18.03	7.77	3.28	8.04	1.00	9.25	14.77	136.61	0.441	No	Yes	0.54
1804	18.04	7.86	3.28	8.00	1.00	9.37	14.63	137.10	0.447	No	Yes	0.55
1805	18.05	7.98	3.27	7.96	1.00	9.53	14.45	137.69	0.455	No	Yes	0.56
1806	18.06	8.18	3.26	7.87	1.00	9.80	14.14	138.61	0.468	No	Yes	0.57
1807	18.07	8.50	3.24	7.75	1.00	10.23	13.68	139.95	0.488	No	Yes	0.60
1808	18.08	8.89	3.22	7.59	1.00	10.77	13.14	141.52	0.514	No	Yes	0.63
1809	18.09	9.33	3.19	7.43	1.00	11.36	12.60	143.10	0.542	No	Yes	0.66
1810	18.10	9.78	3.17	7.26	1.00	11.98	12.07	144.56	0.571	No	Yes	0.70
1811	18.11	10.23	3.15	7.10	1.00	12.59	11.59	145.85	0.600	No	Yes	0.74
1812	18.12	10.65	3.13	6.96	1.00	13.15	11.17	146.90	0.627	No	Yes	0.77
1813	18.13	11.01	3.11	6.84	1.00	13.65	10.82	147.72	0.651	No	Yes	0.80
1814	18.14	11.42	3.09	6.72	1.00	14.19	10.47	148.65	0.677	No	Yes	0.83
1815	18.15	11.92	3.07	6.59	1.00	14.88	10.07	149.86	0.710	No	Yes	0.87
1816	18.16	12.59	3.05	6.44	1.00	15.79	9.59	151.38	0.753	No	Yes	0.92
1817	18.17	13.36	3.02	6.27	1.00	16.84	9.08	152.88	0.803	No	Yes	0.98
1818	18.18	14.20	2.99	6.09	1.00	17.98	8.57	154.16	0.858	No	Yes	1.05
1819	18.19	15.06	2.96	5.91	1.00	19.14	8.11	155.13	0.913	No	Yes	1.12
1820	18.20	15.88	2.93	5.75	1.00	20.26	7.69	155.77	0.967	No	Yes	1.18
1821	18.21	16.64	2.91	5.60	0.99	21.24	7.34	155.96	1.013	No	Yes	1.24
1822	18.22	17.27	2.89	5.47	0.99	22.03	7.08	155.87	1.051	No	Yes	1.29
1823	18.23	17.74	2.88	5.36	0.98	22.61	6.87	155.38	1.078	No	Yes	1.32
1824	18.24	18.09	2.86	5.25	0.98	23.04	6.70	154.49	1.099	No	Yes	1.35

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1825	18.25	18.43	2.85	5.13	0.97	23.44	6.53	153.18	1.118	No	Yes	1.37
1826	18.26	18.80	2.84	5.00	0.97	23.89	6.35	151.63	1.140	No	Yes	1.39
1827	18.27	19.20	2.82	4.85	0.96	24.37	6.15	149.89	1.162	No	Yes	1.42
1828	18.28	19.60	2.81	4.71	0.95	24.84	5.96	148.05	1.185	No	Yes	1.45
1829	18.29	19.98	2.79	4.57	0.95	25.29	5.78	146.19	1.206	No	Yes	1.48
1830	18.30	20.32	2.78	4.45	0.94	25.69	5.62	144.46	1.225	No	Yes	1.50
1831	18.31	20.53	2.77	4.36	0.94	25.92	5.51	142.91	1.237	No	Yes	1.51
1832	18.32	20.55	2.77	4.28	0.94	25.93	5.45	141.43	1.237	No	Yes	1.51
1833	18.33	20.40	2.77	4.22	0.94	25.71	5.44	139.82	1.226	No	Yes	1.50
1834	18.34	20.15	2.77	4.16	0.94	25.38	5.44	137.95	1.211	No	Yes	1.48
1835	18.35	19.89	2.77	4.09	0.94	25.02	5.43	135.90	1.193	No	Yes	1.46
1836	18.36	19.62	2.76	4.01	0.94	24.64	5.43	133.77	1.175	No	Yes	1.44
1837	18.37	19.34	2.76	3.94	0.94	24.27	5.43	131.69	1.158	No	Yes	1.41
1838	18.38	19.09	2.76	3.87	0.94	23.93	5.42	129.75	1.141	No	Yes	1.39
1839	18.39	18.87	2.76	3.81	0.94	23.62	5.42	128.05	1.127	No	Yes	1.38
1840	18.40	18.63	2.77	3.78	0.94	23.30	5.45	126.92	1.112	No	Yes	1.36
1841	18.41	18.33	2.77	3.78	0.94	22.92	5.51	126.28	1.093	No	Yes	1.33
1842	18.42	17.94	2.78	3.81	0.94	22.41	5.62	125.98	1.069	No	Yes	1.30
1843	18.43	17.48	2.79	3.84	0.95	21.83	5.75	125.63	1.041	No	Yes	1.27
1844	18.44	16.99	2.80	3.87	0.95	21.20	5.91	125.21	1.011	No	Yes	1.23
1845	18.45	16.48	2.82	3.91	0.96	20.56	6.07	124.73	0.981	No	Yes	1.20
1846	18.46	16.00	2.83	3.94	0.96	19.94	6.23	124.23	0.951	No	Yes	1.16
1847	18.47	15.55	2.84	3.97	0.97	19.37	6.39	123.73	0.924	No	Yes	1.13
1848	18.48	15.17	2.85	4.00	0.97	18.88	6.53	123.32	0.900	No	Yes	1.10
1849	18.49	14.80	2.86	4.05	0.98	18.41	6.69	123.09	0.878	No	Yes	1.07
1850	18.50	14.40	2.88	4.10	0.98	17.90	6.87	123.02	0.854	No	Yes	1.04
1851	18.51	13.93	2.89	4.18	0.99	17.29	7.11	123.01	0.825	No	Yes	1.01
1852	18.52	13.39	2.91	4.27	0.99	16.61	7.40	122.88	0.792	No	Yes	0.97
1853	18.53	12.83	2.93	4.37	1.00	15.88	7.72	122.59	0.758	No	Yes	0.92
1854	18.54	12.27	2.96	4.47	1.00	15.11	8.08	122.08	0.721	No	Yes	0.88
1855	18.55	11.73	2.98	4.57	1.00	14.39	8.44	121.46	0.686	No	Yes	0.84
1856	18.56	11.25	3.00	4.66	1.00	13.73	8.79	120.78	0.655	No	Yes	0.80
1857	18.57	10.87	3.02	4.73	1.00	13.21	9.10	120.18	0.630	No	Yes	0.77
1858	18.58	10.56	3.03	4.80	1.00	12.79	9.36	119.69	0.610	No	Yes	0.74
1859	18.59	10.28	3.05	4.87	1.00	12.40	9.62	119.27	0.592	No	Yes	0.72
1860	18.60	9.97	3.06	4.95	1.00	11.98	9.91	118.77	0.572	No	Yes	0.70
1861	18.61	9.63	3.08	5.04	1.00	11.52	10.26	118.15	0.549	No	Yes	0.67
1862	18.62	9.28	3.10	5.13	1.00	11.04	10.64	117.43	0.527	No	Yes	0.64
1863	18.63	8.93	3.12	5.23	1.00	10.57	11.03	116.62	0.504	No	Yes	0.61
1864	18.64	8.61	3.14	5.32	1.00	10.13	11.43	115.78	0.483	No	Yes	0.59
1865	18.65	8.32	3.16	5.41	1.00	9.75	11.80	114.98	0.465	No	Yes	0.57
1866	18.66	8.10	3.17	5.48	1.00	9.44	12.10	114.31	0.451	No	Yes	0.55
1867	18.67	7.91	3.18	5.54	1.00	9.19	12.38	113.74	0.438	No	Yes	0.53
1868	18.68	7.73	3.20	5.61	1.00	8.94	12.66	113.18	0.427	No	Yes	0.52
1869	18.69	7.53	3.21	5.68	1.00	8.66	12.99	112.50	0.413	No	Yes	0.50
1870	18.70	7.30	3.23	5.77	1.00	8.36	13.37	111.72	0.399	No	Yes	0.48
1871	18.71	7.08	3.24	5.85	1.00	8.05	13.77	110.88	0.384	No	Yes	0.47
1872	18.72	6.86	3.26	5.94	1.00	7.75	14.19	110.01	0.370	No	Yes	0.45

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1873	18.73	6.66	3.28	6.03	1.00	7.48	14.59	109.18	0.357	No	Yes	0.43
1874	18.74	6.49	3.29	6.10	1.00	7.26	14.95	108.48	0.346	No	Yes	0.42
1875	18.75	6.37	3.30	6.17	1.00	7.09	15.24	108.03	0.338	No	Yes	0.41
1876	18.76	6.28	3.31	6.24	1.00	6.96	15.49	107.80	0.332	No	Yes	0.40
1877	18.77	6.19	3.32	6.33	1.00	6.84	15.75	107.68	0.326	No	Yes	0.40
1878	18.78	6.09	3.33	6.42	1.00	6.70	16.04	107.52	0.320	No	Yes	0.39
1879	18.79	5.98	3.34	6.52	1.00	6.56	16.37	107.33	0.313	No	Yes	0.38
1880	18.80	5.87	3.36	6.62	1.00	6.41	16.71	107.11	0.306	No	Yes	0.37
1881	18.81	5.77	3.37	6.72	1.00	6.27	17.04	106.89	0.299	No	Yes	0.36
1882	18.82	5.68	3.38	6.81	1.00	6.15	17.34	106.66	0.293	No	Yes	0.36
1883	18.83	5.62	3.38	6.89	1.00	6.06	17.57	106.56	0.289	No	Yes	0.35
1884	18.84	5.59	3.39	6.95	1.00	6.02	17.72	106.67	0.287	No	Yes	0.35
1885	18.85	5.58	3.39	7.01	1.00	6.01	17.81	106.98	0.286	No	Yes	0.35
1886	18.86	5.58	3.40	7.08	1.00	6.00	17.89	107.42	0.286	No	Yes	0.35
1887	18.87	5.58	3.40	7.15	1.00	6.00	17.98	107.89	0.286	No	Yes	0.35
1888	18.88	5.58	3.40	7.22	1.00	6.00	18.07	108.38	0.286	No	Yes	0.35
1889	18.89	5.58	3.40	7.30	1.00	6.00	18.15	108.86	0.286	No	Yes	0.35
1890	18.90	5.58	3.41	7.36	1.00	5.99	18.23	109.30	0.286	No	Yes	0.35
1891	18.91	5.58	3.41	7.42	1.00	5.99	18.31	109.68	0.286	No	Yes	0.35
1892	18.92	5.60	3.41	7.46	1.00	6.02	18.29	110.12	0.287	No	Yes	0.35
1893	18.93	5.65	3.41	7.47	1.00	6.09	18.19	110.70	0.290	No	Yes	0.35
1894	18.94	5.74	3.40	7.46	1.00	6.20	17.99	111.47	0.296	No	Yes	0.36
1895	18.95	5.84	3.39	7.45	1.00	6.33	17.76	112.35	0.302	No	Yes	0.36
1896	18.96	5.94	3.38	7.44	1.00	6.46	17.53	113.28	0.308	No	Yes	0.37
1897	18.97	6.05	3.38	7.43	1.00	6.60	17.30	114.23	0.315	No	Yes	0.38
1898	18.98	6.15	3.37	7.42	1.00	6.74	17.09	115.14	0.321	No	Yes	0.39
1899	18.99	6.25	3.36	7.41	1.00	6.86	16.90	115.96	0.327	No	Yes	0.40
1900	19.00	6.33	3.36	7.40	1.00	6.96	16.75	116.63	0.332	No	Yes	0.40
1901	19.01	6.40	3.35	7.38	1.00	7.06	16.59	117.15	0.337	No	Yes	0.41
1902	19.02	6.48	3.35	7.35	1.00	7.16	16.42	117.58	0.342	No	Yes	0.41
1903	19.03	6.57	3.34	7.30	1.00	7.28	16.22	118.01	0.347	No	Yes	0.42
1904	19.04	6.67	3.33	7.25	1.00	7.41	15.99	118.48	0.353	No	Yes	0.43
1905	19.05	6.78	3.32	7.19	1.00	7.55	15.76	118.97	0.360	No	Yes	0.43
1906	19.06	6.88	3.31	7.14	1.00	7.68	15.54	119.44	0.367	No	Yes	0.44
1907	19.07	6.98	3.31	7.09	1.00	7.82	15.34	119.87	0.373	No	Yes	0.45
1908	19.08	7.07	3.30	7.04	1.00	7.93	15.16	120.25	0.378	No	Yes	0.46
1909	19.09	7.13	3.29	7.01	1.00	8.01	15.03	120.44	0.382	No	Yes	0.46
1910	19.10	7.17	3.29	6.97	1.00	8.05	14.95	120.38	0.384	No	Yes	0.46
1911	19.11	7.17	3.29	6.93	1.00	8.06	14.91	120.08	0.384	No	Yes	0.46
1912	19.12	7.17	3.29	6.88	1.00	8.05	14.86	119.66	0.384	No	Yes	0.46
1913	19.13	7.17	3.29	6.83	1.00	8.05	14.81	119.20	0.384	No	Yes	0.46
1914	19.14	7.17	3.28	6.77	1.00	8.05	14.76	118.73	0.384	No	Yes	0.46
1915	19.15	7.17	3.28	6.72	1.00	8.04	14.71	118.27	0.384	No	Yes	0.46
1916	19.16	7.17	3.28	6.67	1.00	8.04	14.66	117.83	0.383	No	Yes	0.46
1917	19.17	7.17	3.28	6.63	1.00	8.04	14.62	117.44	0.383	No	Yes	0.46
1918	19.18	7.15	3.28	6.60	1.00	8.00	14.62	116.99	0.382	No	Yes	0.46
1919	19.19	7.10	3.28	6.58	1.00	7.93	14.68	116.40	0.378	No	Yes	0.46
1920	19.20	7.01	3.29	6.57	1.00	7.81	14.80	115.61	0.373	No	Yes	0.45

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _k (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1921	19.21	6.91	3.29	6.55	1.00	7.68	14.94	114.70	0.366	No	Yes	0.44
1922	19.22	6.81	3.30	6.54	1.00	7.54	15.09	113.72	0.360	No	Yes	0.43
1923	19.23	6.70	3.30	6.52	1.00	7.39	15.25	112.73	0.353	No	Yes	0.42
1924	19.24	6.60	3.31	6.51	1.00	7.25	15.41	111.76	0.346	No	Yes	0.42
1925	19.25	6.50	3.31	6.50	1.00	7.13	15.56	110.88	0.340	No	Yes	0.41
1926	19.26	6.42	3.32	6.49	1.00	7.02	15.69	110.12	0.335	No	Yes	0.40
1927	19.27	6.35	3.32	6.49	1.00	6.92	15.82	109.42	0.330	No	Yes	0.40
1928	19.28	6.27	3.33	6.48	1.00	6.81	15.95	108.68	0.325	No	Yes	0.39
1929	19.29	6.18	3.33	6.47	1.00	6.69	16.12	107.83	0.319	No	Yes	0.38
1930	19.30	6.08	3.34	6.46	1.00	6.55	16.31	106.87	0.313	No	Yes	0.38
1931	19.31	5.97	3.35	6.45	1.00	6.41	16.51	105.86	0.306	No	Yes	0.37
1932	19.32	5.87	3.36	6.45	1.00	6.27	16.72	104.85	0.299	No	Yes	0.36
1933	19.33	5.77	3.36	6.44	1.00	6.13	16.93	103.89	0.293	No	Yes	0.35
1934	19.34	5.68	3.37	6.44	1.00	6.01	17.13	103.02	0.287	No	Yes	0.34
1935	19.35	5.62	3.37	6.43	1.00	5.93	17.26	102.35	0.283	No	Yes	0.34
1936	19.36	5.58	3.38	6.40	1.00	5.89	17.30	101.84	0.281	No	Yes	0.34
1937	19.37	5.58	3.37	6.35	1.00	5.88	17.26	101.42	0.280	No	Yes	0.34
1938	19.38	5.58	3.37	6.29	1.00	5.87	17.19	100.97	0.280	No	Yes	0.34
1939	19.39	5.58	3.37	6.22	1.00	5.87	17.11	100.48	0.280	No	Yes	0.34
1940	19.40	5.58	3.37	6.15	1.00	5.87	17.03	99.97	0.280	No	Yes	0.34
1941	19.41	5.58	3.36	6.08	1.00	5.87	16.95	99.46	0.280	No	Yes	0.34
1942	19.42	5.58	3.36	6.02	1.00	5.86	16.88	98.99	0.280	No	Yes	0.34
1943	19.43	5.58	3.36	5.97	1.00	5.86	16.82	98.58	0.280	No	Yes	0.34
1944	19.44	5.58	3.36	5.92	1.00	5.86	16.76	98.22	0.280	No	Yes	0.34
1945	19.45	5.58	3.36	5.87	1.00	5.86	16.71	97.86	0.279	No	Yes	0.34
1946	19.46	5.58	3.35	5.82	1.00	5.85	16.64	97.45	0.279	No	Yes	0.34
1947	19.47	5.58	3.35	5.76	1.00	5.85	16.57	96.99	0.279	No	Yes	0.33
1948	19.48	5.58	3.35	5.70	1.00	5.85	16.49	96.49	0.279	No	Yes	0.33
1949	19.49	5.58	3.35	5.63	1.00	5.85	16.41	95.98	0.279	No	Yes	0.33
1950	19.50	5.58	3.34	5.57	1.00	5.85	16.34	95.49	0.279	No	Yes	0.33
1951	19.51	5.58	3.34	5.51	1.00	5.84	16.27	95.04	0.279	No	Yes	0.33
1952	19.52	5.58	3.34	5.46	1.00	5.84	16.21	94.66	0.279	No	Yes	0.33
1953	19.53	5.58	3.34	5.42	1.00	5.84	16.16	94.35	0.278	No	Yes	0.33
1954	19.54	5.58	3.33	5.39	1.00	5.84	16.12	94.06	0.278	No	Yes	0.33
1955	19.55	5.58	3.33	5.35	1.00	5.83	16.07	93.75	0.278	No	Yes	0.33
1956	19.56	5.58	3.33	5.30	1.00	5.83	16.02	93.39	0.278	No	Yes	0.33
1957	19.57	5.58	3.33	5.26	1.00	5.83	15.96	93.02	0.278	No	Yes	0.33
1958	19.58	5.58	3.33	5.21	1.00	5.83	15.90	92.65	0.278	No	Yes	0.33
1959	19.59	5.58	3.32	5.17	1.00	5.82	15.85	92.30	0.278	No	Yes	0.33
1960	19.60	5.58	3.32	5.13	1.00	5.82	15.80	91.98	0.278	No	Yes	0.33
1961	19.61	5.58	3.32	5.10	1.00	5.82	15.77	91.74	0.277	No	Yes	0.33
1962	19.62	5.57	3.32	5.09	1.00	5.81	15.77	91.57	0.277	No	Yes	0.33
1963	19.63	5.56	3.32	5.08	1.00	5.79	15.78	91.44	0.276	No	Yes	0.33
1964	19.64	5.55	3.32	5.08	1.00	5.78	15.81	91.30	0.276	No	Yes	0.33
1965	19.65	5.54	3.32	5.07	1.00	5.76	15.83	91.15	0.275	No	Yes	0.33
1966	19.66	5.52	3.33	5.07	1.00	5.74	15.86	91.00	0.274	No	Yes	0.33
1967	19.67	5.51	3.33	5.07	1.00	5.72	15.89	90.85	0.273	No	Yes	0.33
1968	19.68	5.50	3.33	5.06	1.00	5.70	15.92	90.71	0.272	No	Yes	0.32

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1969	19.69	5.49	3.33	5.06	1.00	5.68	15.94	90.59	0.271	No	Yes	0.32
1970	19.70	5.45	3.33	5.07	1.00	5.64	16.04	90.44	0.269	No	Yes	0.32
1971	19.71	5.40	3.34	5.11	1.00	5.56	16.22	90.24	0.265	No	Yes	0.32
1972	19.72	5.31	3.35	5.17	1.00	5.45	16.51	89.96	0.260	No	Yes	0.31
1973	19.73	5.21	3.36	5.24	1.00	5.32	16.85	89.63	0.254	No	Yes	0.30
1974	19.74	5.11	3.37	5.32	1.00	5.18	17.23	89.26	0.247	No	Yes	0.30
1975	19.75	5.00	3.39	5.40	1.00	5.04	17.64	88.86	0.240	No	Yes	0.29
1976	19.76	4.90	3.40	5.48	1.00	4.90	18.04	88.46	0.234	No	Yes	0.28
1977	19.77	4.81	3.41	5.55	1.00	4.78	18.43	88.07	0.228	No	Yes	0.27
1978	19.78	4.78	3.42	5.61	1.00	4.75	18.58	88.19	0.226	No	Yes	0.27
1979	19.79	4.93	3.40	5.62	1.00	4.94	18.15	89.69	0.236	No	Yes	0.28
1980	19.80	5.29	3.37	5.60	1.00	5.40	17.17	92.76	0.258	No	Yes	0.31
1981	19.81	5.80	3.33	5.58	1.00	6.06	15.99	96.96	0.289	No	Yes	0.35
1982	19.82	6.37	3.29	5.58	1.00	6.80	14.91	101.47	0.325	No	Yes	0.39
1983	19.83	6.97	3.25	5.60	1.00	7.58	13.99	106.03	0.362	No	Yes	0.43
1984	19.84	7.56	3.22	5.63	1.00	8.35	13.23	110.45	0.398	No	Yes	0.47
1985	19.85	8.13	3.19	5.68	1.00	9.08	12.61	114.52	0.433	No	Yes	0.52
1986	19.86	8.63	3.17	5.72	1.00	9.73	12.14	118.07	0.464	No	Yes	0.55
1987	19.87	9.07	3.16	5.76	1.00	10.30	11.75	121.09	0.491	No	Yes	0.59
1988	19.88	9.53	3.14	5.78	1.00	10.89	11.39	123.99	0.519	No	Yes	0.62
1989	19.89	10.06	3.12	5.80	1.00	11.57	10.99	127.15	0.552	No	Yes	0.66
1990	19.90	10.68	3.10	5.83	1.00	12.37	10.57	130.76	0.590	No	Yes	0.70
1991	19.91	11.35	3.08	5.87	1.00	13.24	10.17	134.60	0.631	No	Yes	0.75
1992	19.92	12.04	3.06	5.91	1.00	14.13	9.80	138.47	0.674	No	Yes	0.80
1993	19.93	12.72	3.04	5.95	1.00	15.01	9.47	142.19	0.716	No	Yes	0.85
1994	19.94	13.36	3.02	5.99	1.00	15.82	9.20	145.59	0.755	No	Yes	0.90
1995	19.95	13.88	3.01	6.03	1.00	16.49	9.00	148.37	0.787	No	Yes	0.94
1996	19.96	14.03	3.01	6.04	1.00	16.69	8.94	149.20	0.796	No	Yes	0.95
1997	19.97	13.81	3.01	6.03	1.00	16.39	9.03	148.08	0.782	No	Yes	0.93
1998	19.98	13.25	3.03	6.00	1.00	15.66	9.27	145.14	0.747	No	Yes	0.89
1999	19.99	12.61	3.04	5.96	1.00	14.82	9.56	141.75	0.707	No	Yes	0.84
2000	20.00	11.92	3.06	5.93	1.00	13.93	9.91	138.06	0.665	No	Yes	0.79
2001	20.01	11.23	3.08	5.90	1.00	13.03	10.30	134.24	0.622	No	Yes	0.74
2002	20.02	10.56	3.11	5.88	1.00	12.16	10.73	130.49	0.580	No	Yes	0.69
2003	20.03	9.96	3.13	5.86	1.00	11.38	11.16	126.99	0.543	No	Yes	0.65
2004	20.04	9.45	3.15	5.86	1.00	10.72	11.57	124.02	0.511	No	Yes	0.61
2005	20.05	9.01	3.17	5.86	1.00	10.15	11.97	121.46	0.484	No	Yes	0.58
2006	20.06	8.59	3.19	5.87	1.00	9.60	12.40	118.99	0.458	No	Yes	0.54
2007	20.07	8.11	3.21	5.90	1.00	8.98	12.94	116.18	0.428	No	Yes	0.51
2008	20.08	7.58	3.24	5.94	1.00	8.28	13.63	112.93	0.395	No	Yes	0.47
2009	20.09	7.02	3.27	6.00	1.00	7.56	14.46	109.37	0.361	No	Yes	0.43
2010	20.10	6.46	3.31	6.07	1.00	6.84	15.44	105.66	0.326	No	Yes	0.39
2011	20.11	5.94	3.35	6.15	1.00	6.16	16.55	101.97	0.294	No	Yes	0.35
2012	20.12	5.47	3.39	6.25	1.00	5.56	17.72	98.53	0.265	No	Yes	0.32
2013	20.13	5.15	3.42	6.35	1.00	5.15	18.67	96.18	0.246	No	Yes	0.29
2014	20.14	4.99	3.44	6.44	1.00	4.94	19.26	95.10	0.235	No	Yes	0.28
2015	20.15	4.95	3.45	6.52	1.00	4.88	19.51	95.15	0.233	No	Yes	0.28
2016	20.16	4.92	3.45	6.61	1.00	4.85	19.70	95.46	0.231	No	Yes	0.27

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _t (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
2017	20.17	4.90	3.46	6.71	1.00	4.81	19.91	95.78	0.229	No	Yes	0.27
2018	20.18	4.87	3.46	6.81	1.00	4.77	20.13	96.11	0.228	No	Yes	0.27
2019	20.19	4.84	3.47	6.91	1.00	4.74	20.35	96.42	0.226	No	Yes	0.27
2020	20.20	4.82	3.48	7.00	1.00	4.71	20.55	96.70	0.224	No	Yes	0.27
2021	20.21	4.80	3.48	7.09	1.00	4.68	20.73	96.94	0.223	No	Yes	0.26
2022	20.22	4.78	3.49	7.17	1.00	4.65	20.90	97.19	0.222	No	Yes	0.26
2023	20.23	4.76	3.49	7.25	1.00	4.63	21.08	97.48	0.221	No	Yes	0.26
2024	20.24	4.74	3.50	7.36	1.00	4.60	21.29	97.85	0.219	No	Yes	0.26
2025	20.25	4.71	3.51	7.49	1.00	4.56	21.54	98.27	0.218	No	Yes	0.26
2026	20.26	4.69	3.51	7.62	1.00	4.53	21.81	98.70	0.216	No	Yes	0.26
2027	20.27	4.66	3.52	7.75	1.00	4.49	22.08	99.13	0.214	No	Yes	0.25
2028	20.28	4.64	3.53	7.88	1.00	4.46	22.34	99.53	0.213	No	Yes	0.25
2029	20.29	4.61	3.53	8.00	1.00	4.42	22.58	99.88	0.211	No	Yes	0.25
2030	20.30	4.62	3.54	8.09	1.00	4.43	22.68	100.39	0.211	No	Yes	0.25
2031	20.31	4.69	3.53	8.13	1.00	4.52	22.47	101.47	0.215	No	Yes	0.26
2032	20.32	4.83	3.52	8.14	1.00	4.70	21.96	103.24	0.224	No	Yes	0.27
2033	20.33	5.04	3.50	8.14	1.00	4.96	21.27	105.60	0.237	No	Yes	0.28
2034	20.34	5.27	3.48	8.14	1.00	5.26	20.59	108.19	0.251	No	Yes	0.30
2035	20.35	5.51	3.46	8.15	1.00	5.56	19.94	110.87	0.265	No	Yes	0.31
2036	20.36	5.75	3.44	8.17	1.00	5.86	19.36	113.51	0.280	No	Yes	0.33
2037	20.37	5.97	3.43	8.20	1.00	6.15	18.87	115.97	0.293	No	Yes	0.35
2038	20.38	6.17	3.41	8.22	1.00	6.40	18.46	118.14	0.305	No	Yes	0.36
2039	20.39	6.36	3.40	8.23	1.00	6.64	18.08	120.04	0.317	No	Yes	0.37
2040	20.40	6.57	3.39	8.20	1.00	6.91	17.65	121.93	0.330	No	Yes	0.39
2041	20.41	6.84	3.37	8.16	1.00	7.24	17.13	124.06	0.345	No	Yes	0.41
2042	20.42	7.15	3.35	8.10	1.00	7.64	16.56	126.48	0.364	No	Yes	0.43
2043	20.43	7.49	3.33	8.05	1.00	8.07	16.00	129.05	0.385	No	Yes	0.45
2044	20.44	7.83	3.31	8.01	1.00	8.51	15.48	131.63	0.406	No	Yes	0.48
2045	20.45	8.17	3.29	7.97	1.00	8.94	15.01	134.09	0.426	No	Yes	0.50
2046	20.46	8.49	3.28	7.94	1.00	9.33	14.61	136.30	0.445	No	Yes	0.53
2047	20.47	8.76	3.26	7.91	1.00	9.68	14.28	138.17	0.462	No	Yes	0.55
2048	20.48	9.01	3.25	7.87	1.00	10.00	13.98	139.74	0.477	No	Yes	0.56
2049	20.49	9.29	3.24	7.81	1.00	10.34	13.65	141.19	0.493	No	Yes	0.58
2050	20.50	9.62	3.22	7.73	1.00	10.76	13.27	142.74	0.513	No	Yes	0.61
2051	20.51	9.99	3.21	7.63	1.00	11.23	12.86	144.42	0.535	No	Yes	0.63
2052	20.52	10.38	3.19	7.54	1.00	11.73	12.46	146.12	0.559	No	Yes	0.66
2053	20.53	10.78	3.17	7.45	1.00	12.23	12.08	147.75	0.583	No	Yes	0.69
2054	20.54	11.17	3.15	7.37	1.00	12.71	11.74	149.23	0.606	No	Yes	0.72
2055	20.55	11.51	3.14	7.29	1.00	13.15	11.44	150.51	0.627	No	Yes	0.74
2056	20.56	11.80	3.13	7.23	1.00	13.50	11.21	151.44	0.644	No	Yes	0.76
2057	20.57	12.02	3.12	7.17	1.00	13.78	11.03	151.99	0.657	No	Yes	0.78
2058	20.58	12.21	3.11	7.10	1.00	14.02	10.86	152.25	0.669	No	Yes	0.79
2059	20.59	12.42	3.10	7.01	1.00	14.28	10.67	152.38	0.681	No	Yes	0.80
2060	20.60	12.65	3.09	6.92	1.00	14.57	10.47	152.49	0.695	No	Yes	0.82
2061	20.61	12.89	3.08	6.82	1.00	14.86	10.26	152.56	0.709	No	Yes	0.84
2062	20.62	13.13	3.07	6.73	1.00	15.16	10.06	152.59	0.723	No	Yes	0.85
2063	20.63	13.35	3.06	6.64	1.00	15.44	9.88	152.57	0.736	No	Yes	0.87
2064	20.64	13.55	3.05	6.56	1.00	15.68	9.73	152.53	0.748	No	Yes	0.88

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
2065	20.65	13.72	3.05	6.49	1.00	15.90	9.59	152.43	0.758	No	Yes	0.89
2066	20.66	13.89	3.04	6.42	1.00	16.10	9.46	152.25	0.768	No	Yes	0.91
2067	20.67	14.07	3.03	6.33	1.00	16.33	9.31	151.97	0.779	No	Yes	0.92
2068	20.68	14.29	3.02	6.24	1.00	16.60	9.13	151.61	0.792	No	Yes	0.93
2069	20.69	14.52	3.01	6.13	1.00	16.89	8.95	151.17	0.806	No	Yes	0.95
2070	20.70	14.76	3.00	6.02	1.00	17.19	8.77	150.67	0.820	No	Yes	0.97
2071	20.71	15.00	2.99	5.92	1.00	17.48	8.59	150.14	0.834	No	Yes	0.98
2072	20.72	15.21	2.98	5.83	1.00	17.74	8.43	149.60	0.846	No	Yes	1.00
2073	20.73	15.39	2.97	5.75	1.00	17.96	8.30	149.09	0.857	No	Yes	1.01
2074	20.74	15.46	2.97	5.68	1.00	18.05	8.23	148.46	0.861	No	Yes	1.01
2075	20.75	15.44	2.96	5.64	1.00	18.01	8.20	147.64	0.859	No	Yes	1.01
2076	20.76	15.34	2.96	5.59	1.00	17.88	8.20	146.55	0.853	No	Yes	1.00
2077	20.77	15.23	2.96	5.54	1.00	17.73	8.19	145.33	0.846	No	Yes	1.00
2078	20.78	15.11	2.96	5.48	1.00	17.58	8.19	144.03	0.838	No	Yes	0.99
2079	20.79	14.99	2.96	5.42	1.00	17.42	8.19	142.72	0.831	No	Yes	0.98
2080	20.80	14.88	2.96	5.37	1.00	17.27	8.19	141.47	0.824	No	Yes	0.97
2081	20.81	14.77	2.96	5.32	1.00	17.13	8.19	140.34	0.817	No	Yes	0.96
2082	20.82	14.66	2.97	5.29	1.00	16.98	8.21	139.41	0.810	No	Yes	0.95
2083	20.83	14.48	2.97	5.28	1.00	16.74	8.28	138.66	0.799	No	Yes	0.94
2084	20.84	14.21	2.98	5.30	1.00	16.40	8.41	137.97	0.782	No	Yes	0.92
2085	20.85	13.86	2.99	5.34	1.00	15.96	8.60	137.19	0.761	No	Yes	0.90
2086	20.86	13.48	3.00	5.39	1.00	15.47	8.81	136.27	0.738	No	Yes	0.87
2087	20.87	13.08	3.01	5.44	1.00	14.96	9.04	135.27	0.714	No	Yes	0.84
2088	20.88	12.69	3.03	5.48	1.00	14.46	9.28	134.23	0.690	No	Yes	0.81
2089	20.89	12.31	3.04	5.53	1.00	13.99	9.52	133.20	0.667	No	Yes	0.78
2090	20.90	11.98	3.05	5.57	1.00	13.57	9.75	132.24	0.647	No	Yes	0.76
2091	20.91	11.73	3.06	5.62	1.00	13.24	9.94	131.61	0.631	No	Yes	0.74
2092	20.92	11.52	3.07	5.68	1.00	12.97	10.12	131.32	0.619	No	Yes	0.73
2093	20.93	11.33	3.08	5.76	1.00	12.73	10.32	131.30	0.607	No	Yes	0.71
2094	20.94	11.11	3.10	5.85	1.00	12.45	10.54	131.28	0.594	No	Yes	0.70
2095	20.95	10.88	3.11	5.95	1.00	12.15	10.80	131.22	0.580	No	Yes	0.68
2096	20.96	10.64	3.12	6.05	1.00	11.85	11.07	131.11	0.565	No	Yes	0.66
2097	20.97	10.40	3.14	6.16	1.00	11.55	11.34	130.94	0.551	No	Yes	0.65
2098	20.98	10.19	3.15	6.26	1.00	11.27	11.60	130.75	0.538	No	Yes	0.63
2099	20.99	10.00	3.16	6.34	1.00	11.03	11.83	130.54	0.526	No	Yes	0.62
2100	21.00	9.83	3.17	6.41	1.00	10.82	12.04	130.28	0.516	No	Yes	0.61
2101	21.01	9.66	3.18	6.49	1.00	10.60	12.26	129.95	0.506	No	Yes	0.59
2102	21.02	9.46	3.19	6.57	1.00	10.35	12.51	129.51	0.494	No	Yes	0.58
2103	21.03	9.24	3.20	6.66	1.00	10.07	12.81	128.97	0.480	No	Yes	0.56
2104	21.04	9.00	3.22	6.76	1.00	9.76	13.14	128.35	0.466	No	Yes	0.55
2105	21.05	8.76	3.23	6.87	1.00	9.46	13.49	127.67	0.451	No	Yes	0.53
2106	21.06	8.53	3.25	6.97	1.00	9.17	13.85	126.97	0.437	No	Yes	0.51
2107	21.07	8.33	3.26	7.06	1.00	8.91	14.18	126.29	0.425	No	Yes	0.50
2108	21.08	8.16	3.27	7.14	1.00	8.70	14.45	125.71	0.415	No	Yes	0.49
2109	21.09	8.04	3.28	7.19	1.00	8.54	14.66	125.20	0.407	No	Yes	0.48
2110	21.10	7.94	3.29	7.23	1.00	8.41	14.83	124.72	0.401	No	Yes	0.47
2111	21.11	7.83	3.29	7.26	1.00	8.28	15.00	124.17	0.395	No	Yes	0.46
2112	21.12	7.72	3.30	7.30	1.00	8.13	15.20	123.56	0.388	No	Yes	0.45

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
2113	21.13	7.60	3.31	7.34	1.00	7.98	15.41	122.92	0.381	No	Yes	0.45
2114	21.14	7.48	3.32	7.38	1.00	7.83	15.62	122.27	0.373	No	Yes	0.44
2115	21.15	7.37	3.32	7.42	1.00	7.69	15.83	121.65	0.367	No	Yes	0.43
2116	21.16	7.27	3.33	7.46	1.00	7.56	16.02	121.09	0.361	No	Yes	0.42
2117	21.17	7.27	3.33	7.46	1.00	7.55	16.03	121.02	0.360	No	Yes	0.42
2118	21.18	7.38	3.32	7.41	1.00	7.69	15.81	121.55	0.367	No	Yes	0.43
2119	21.19	7.62	3.31	7.31	1.00	7.98	15.37	122.68	0.381	No	Yes	0.45
2120	21.20	7.91	3.29	7.19	1.00	8.34	14.87	124.00	0.398	No	Yes	0.47
2121	21.21	8.22	3.27	7.08	1.00	8.73	14.36	125.35	0.416	No	Yes	0.49
2122	21.22	8.54	3.25	6.96	1.00	9.12	13.88	126.65	0.435	No	Yes	0.51
2123	21.23	8.85	3.23	6.86	1.00	9.51	13.45	127.84	0.453	No	Yes	0.53
2124	21.24	9.14	3.21	6.76	1.00	9.86	13.07	128.86	0.470	No	Yes	0.55
2125	21.25	9.40	3.20	6.68	1.00	10.18	12.74	129.75	0.486	No	Yes	0.57
2126	21.26	9.72	3.18	6.59	1.00	10.58	12.37	130.84	0.505	No	Yes	0.59
2127	21.27	10.15	3.16	6.47	1.00	11.11	11.91	132.25	0.530	No	Yes	0.62
2128	21.28	10.72	3.14	6.33	1.00	11.81	11.35	133.99	0.563	No	Yes	0.66
2129	21.29	11.36	3.11	6.18	1.00	12.60	10.77	135.74	0.601	No	Yes	0.70
2130	21.30	12.04	3.08	6.03	1.00	13.44	10.22	137.37	0.641	No	Yes	0.75
2131	21.31	12.72	3.05	5.88	1.00	14.29	9.71	138.77	0.681	No	Yes	0.80
2132	21.32	13.38	3.03	5.75	1.00	15.09	9.27	139.91	0.720	No	Yes	0.84
2133	21.33	13.97	3.01	5.63	1.00	15.82	8.90	140.77	0.755	No	Yes	0.88
2134	21.34	14.44	2.99	5.54	1.00	16.40	8.62	141.29	0.782	No	Yes	0.91
2135	21.35	14.81	2.98	5.45	1.00	16.86	8.39	141.46	0.804	No	Yes	0.94
2136	21.36	15.13	2.96	5.36	1.00	17.25	8.19	141.33	0.823	No	Yes	0.96
2137	21.37	15.48	2.95	5.26	1.00	17.68	7.98	141.01	0.843	No	Yes	0.98
2138	21.38	15.87	2.94	5.15	1.00	18.14	7.75	140.59	0.865	No	Yes	1.01
2139	21.39	16.27	2.92	5.03	1.00	18.63	7.52	140.07	0.889	No	Yes	1.04
2140	21.40	16.66	2.91	4.92	1.00	19.09	7.30	139.41	0.911	No	Yes	1.06
2141	21.41	17.03	2.89	4.82	0.99	19.52	7.11	138.70	0.931	No	Yes	1.09
2142	21.42	17.36	2.88	4.72	0.99	19.89	6.94	138.03	0.949	No	Yes	1.11
2143	21.43	17.66	2.87	4.65	0.98	20.24	6.80	137.61	0.965	No	Yes	1.13
2144	21.44	17.99	2.86	4.60	0.98	20.62	6.67	137.48	0.984	No	Yes	1.15
2145	21.45	18.39	2.85	4.55	0.97	21.08	6.53	137.58	1.006	No	Yes	1.17
2146	21.46	18.86	2.84	4.49	0.97	21.62	6.37	137.69	1.031	No	Yes	1.20
2147	21.47	19.36	2.83	4.44	0.97	22.20	6.20	137.75	1.059	No	Yes	1.24
2148	21.48	19.88	2.82	4.38	0.96	22.79	6.04	137.76	1.087	No	Yes	1.27
2149	21.49	20.38	2.80	4.32	0.96	23.37	5.89	137.72	1.115	No	Yes	1.30
2150	21.50	20.84	2.79	4.27	0.95	23.90	5.76	137.64	1.140	No	Yes	1.33
2151	21.51	21.21	2.78	4.22	0.95	24.32	5.65	137.52	1.160	No	Yes	1.35
2152	21.52	21.44	2.78	4.20	0.95	24.57	5.59	137.36	1.172	No	Yes	1.37
2153	21.53	21.53	2.78	4.18	0.95	24.67	5.56	137.15	1.177	No	Yes	1.37
2154	21.54	21.54	2.77	4.16	0.95	24.68	5.55	136.88	1.177	No	Yes	1.37
2155	21.55	21.56	2.77	4.15	0.95	24.68	5.53	136.57	1.177	No	Yes	1.37
2156	21.56	21.57	2.77	4.13	0.94	24.69	5.52	136.25	1.178	No	Yes	1.37
2157	21.57	21.59	2.77	4.11	0.94	24.70	5.50	135.92	1.178	No	Yes	1.37
2158	21.58	21.60	2.77	4.10	0.94	24.70	5.49	135.61	1.178	No	Yes	1.37
2159	21.59	21.62	2.77	4.08	0.94	24.71	5.48	135.32	1.179	No	Yes	1.37
2160	21.60	21.54	2.77	4.08	0.94	24.61	5.49	135.05	1.174	No	Yes	1.37

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _k (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
2161	21.61	21.27	2.77	4.09	0.95	24.29	5.54	134.69	1.159	No	Yes	1.35
2162	21.62	20.78	2.78	4.11	0.95	23.71	5.66	134.21	1.131	No	Yes	1.32
2163	21.63	20.13	2.80	4.15	0.95	22.94	5.82	133.56	1.094	No	Yes	1.27
2164	21.64	19.41	2.81	4.18	0.96	22.10	6.01	132.79	1.054	No	Yes	1.23
2165	21.65	18.67	2.83	4.23	0.97	21.22	6.22	131.92	1.012	No	Yes	1.18
2166	21.66	17.93	2.85	4.27	0.97	20.35	6.44	130.98	0.971	No	Yes	1.13
2167	21.67	17.24	2.86	4.31	0.98	19.53	6.66	130.02	0.932	No	Yes	1.08
2168	21.68	16.63	2.88	4.34	0.98	18.81	6.86	129.12	0.897	No	Yes	1.04
2169	21.69	16.15	2.89	4.38	0.99	18.24	7.05	128.50	0.870	No	Yes	1.01
2170	21.70	15.73	2.90	4.43	0.99	17.74	7.22	128.15	0.846	No	Yes	0.99
2171	21.71	15.33	2.91	4.49	1.00	17.26	7.42	128.01	0.823	No	Yes	0.96
2172	21.72	14.86	2.93	4.57	1.00	16.69	7.65	127.76	0.796	No	Yes	0.93
2173	21.73	14.36	2.95	4.65	1.00	16.07	7.93	127.38	0.767	No	Yes	0.89
2174	21.74	13.85	2.97	4.74	1.00	15.44	8.22	126.91	0.736	No	Yes	0.86
2175	21.75	13.35	2.98	4.82	1.00	14.82	8.52	126.35	0.707	No	Yes	0.82
2176	21.76	12.89	3.00	4.90	1.00	14.26	8.82	125.74	0.680	No	Yes	0.79
2177	21.77	12.50	3.02	4.97	1.00	13.78	9.09	125.16	0.657	No	Yes	0.76
2178	21.78	12.16	3.03	5.03	1.00	13.36	9.33	124.62	0.637	No	Yes	0.74
2179	21.79	11.83	3.05	5.10	1.00	12.94	9.59	124.05	0.617	No	Yes	0.72
2180	21.80	11.45	3.06	5.18	1.00	12.47	9.89	123.36	0.595	No	Yes	0.69
2181	21.81	11.03	3.08	5.27	1.00	11.95	10.25	122.50	0.570	No	Yes	0.66
2182	21.82	10.58	3.10	5.37	1.00	11.40	10.66	121.49	0.544	No	Yes	0.63
2183	21.83	10.12	3.12	5.47	1.00	10.84	11.10	120.36	0.517	No	Yes	0.60
2184	21.84	9.69	3.15	5.57	1.00	10.31	11.56	119.18	0.492	No	Yes	0.57
2185	21.85	9.31	3.17	5.67	1.00	9.83	12.00	118.02	0.469	No	Yes	0.54
2186	21.86	8.99	3.18	5.75	1.00	9.44	12.39	117.00	0.450	No	Yes	0.52
2187	21.87	8.72	3.20	5.82	1.00	9.11	12.74	116.07	0.435	No	Yes	0.50
2188	21.88	8.46	3.22	5.89	1.00	8.79	13.09	115.12	0.420	No	Yes	0.49
2189	21.89	8.17	3.23	5.97	1.00	8.44	13.51	114.00	0.403	No	Yes	0.47
2190	21.90	7.86	3.25	6.06	1.00	8.05	14.00	112.71	0.384	No	Yes	0.45
2191	21.91	7.53	3.28	6.17	1.00	7.64	14.56	111.28	0.365	No	Yes	0.42
2192	21.92	7.20	3.30	6.27	1.00	7.24	15.16	109.78	0.345	No	Yes	0.40
2193	21.93	6.89	3.32	6.38	1.00	6.87	15.77	108.30	0.328	No	Yes	0.38
2194	21.94	6.63	3.34	6.49	1.00	6.54	16.36	106.94	0.312	No	Yes	0.36
2195	21.95	6.44	3.36	6.55	1.00	6.31	16.79	105.86	0.301	No	Yes	0.35
2196	21.96	6.31	3.37	6.58	1.00	6.15	17.08	104.99	0.293	No	Yes	0.34
2197	21.97	6.22	3.37	6.58	1.00	6.04	17.25	104.21	0.288	No	Yes	0.33
2198	21.98	6.12	3.38	6.57	1.00	5.92	17.46	103.32	0.282	No	Yes	0.33
2199	21.99	6.02	3.39	6.57	1.00	5.79	17.68	102.36	0.276	No	Yes	0.32
2200	22.00	5.91	3.40	6.57	1.00	5.66	17.92	101.38	0.270	No	Yes	0.31
2201	22.01	5.81	3.40	6.56	1.00	5.53	18.16	100.42	0.264	No	Yes	0.31
2202	22.02	5.71	3.41	6.56	1.00	5.41	18.39	99.54	0.258	No	Yes	0.30
2203	22.03	5.64	3.42	6.56	1.00	5.32	18.58	98.80	0.254	No	Yes	0.29
2204	22.04	5.59	3.42	6.54	1.00	5.26	18.67	98.23	0.251	No	Yes	0.29
2205	22.05	5.58	3.42	6.49	1.00	5.24	18.66	97.78	0.250	No	Yes	0.29
2206	22.06	5.58	3.42	6.43	1.00	5.24	18.58	97.32	0.250	No	Yes	0.29
2207	22.07	5.58	3.41	6.35	1.00	5.24	18.49	96.82	0.250	No	Yes	0.29
2208	22.08	5.58	3.41	6.27	1.00	5.23	18.39	96.28	0.250	No	Yes	0.29

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
2209	22.09	5.58	3.41	6.19	1.00	5.23	18.29	95.73	0.250	No	Yes	0.29
2210	22.10	5.58	3.41	6.12	1.00	5.23	18.20	95.21	0.250	No	Yes	0.29
2211	22.11	5.58	3.40	6.05	1.00	5.23	18.12	94.74	0.249	No	Yes	0.29
2212	22.12	5.58	3.40	6.00	1.00	5.23	18.05	94.34	0.249	No	Yes	0.29
2213	22.13	5.58	3.40	5.95	1.00	5.22	17.99	93.99	0.249	No	Yes	0.29
2214	22.14	5.58	3.40	5.90	1.00	5.22	17.93	93.64	0.249	No	Yes	0.29
2215	22.15	5.58	3.39	5.84	1.00	5.22	17.86	93.24	0.249	No	Yes	0.29
2216	22.16	5.58	3.39	5.78	1.00	5.22	17.78	92.80	0.249	No	Yes	0.29
2217	22.17	5.58	3.39	5.72	1.00	5.22	17.70	92.34	0.249	No	Yes	0.29
2218	22.18	5.58	3.39	5.65	1.00	5.21	17.62	91.89	0.249	No	Yes	0.29
2219	22.19	5.58	3.38	5.60	1.00	5.21	17.55	91.46	0.249	No	Yes	0.29
2220	22.20	5.58	3.38	5.54	1.00	5.21	17.48	91.08	0.249	No	Yes	0.29
2221	22.21	5.57	3.38	5.51	1.00	5.20	17.46	90.74	0.248	No	Yes	0.29
2222	22.22	5.54	3.38	5.49	1.00	5.16	17.50	90.37	0.246	No	Yes	0.28
2223	22.23	5.50	3.39	5.48	1.00	5.11	17.60	89.94	0.244	No	Yes	0.28
2224	22.24	5.45	3.39	5.47	1.00	5.05	17.71	89.44	0.241	No	Yes	0.28
2225	22.25	5.40	3.39	5.46	1.00	4.98	17.84	88.90	0.238	No	Yes	0.27
2226	22.26	5.35	3.40	5.45	1.00	4.92	17.96	88.36	0.235	No	Yes	0.27
2227	22.27	5.29	3.40	5.44	1.00	4.85	18.09	87.83	0.232	No	Yes	0.27
2228	22.28	5.25	3.41	5.43	1.00	4.80	18.21	87.34	0.229	No	Yes	0.26
2229	22.29	5.21	3.41	5.42	1.00	4.76	18.29	86.98	0.227	No	Yes	0.26
2230	22.30	5.22	3.41	5.40	1.00	4.76	18.24	86.93	0.227	No	Yes	0.26
2231	22.31	5.28	3.40	5.37	1.00	4.83	18.06	87.19	0.230	No	Yes	0.27
2232	22.32	5.37	3.39	5.33	1.00	4.93	17.77	87.67	0.235	No	Yes	0.27
2233	22.33	5.47	3.38	5.29	1.00	5.05	17.46	88.21	0.241	No	Yes	0.28
2234	22.34	5.57	3.37	5.25	1.00	5.18	17.14	88.76	0.247	No	Yes	0.29
2235	22.35	5.68	3.36	5.21	1.00	5.31	16.83	89.31	0.253	No	Yes	0.29
2236	22.36	5.78	3.35	5.17	1.00	5.42	16.56	89.82	0.259	No	Yes	0.30
2237	22.37	5.87	3.34	5.14	1.00	5.53	16.32	90.26	0.264	No	Yes	0.30
2238	22.38	5.94	3.34	5.12	1.00	5.62	16.14	90.61	0.268	No	Yes	0.31
2239	22.39	6.00	3.33	5.10	1.00	5.68	16.01	90.88	0.271	No	Yes	0.31
2240	22.40	6.04	3.33	5.09	1.00	5.73	15.91	91.11	0.273	No	Yes	0.32
2241	22.41	6.09	3.32	5.08	1.00	5.78	15.80	91.37	0.276	No	Yes	0.32
2242	22.42	6.14	3.32	5.07	1.00	5.84	15.69	91.65	0.279	No	Yes	0.32
2243	22.43	6.19	3.31	5.06	1.00	5.90	15.57	91.94	0.282	No	Yes	0.32
2244	22.44	6.24	3.31	5.05	1.00	5.97	15.46	92.22	0.285	No	Yes	0.33
2245	22.45	6.29	3.31	5.04	1.00	6.02	15.36	92.49	0.287	No	Yes	0.33
2246	22.46	6.34	3.30	5.03	1.00	6.07	15.27	92.71	0.290	No	Yes	0.33
2247	22.47	6.38	3.30	5.02	1.00	6.12	15.18	92.95	0.292	No	Yes	0.34
2248	22.48	6.43	3.30	5.02	1.00	6.18	15.09	93.25	0.295	No	Yes	0.34
2249	22.49	6.49	3.29	5.01	1.00	6.25	14.97	93.63	0.298	No	Yes	0.34
2250	22.50	6.57	3.29	5.01	1.00	6.34	14.84	94.07	0.302	No	Yes	0.35
2251	22.51	6.64	3.28	5.00	1.00	6.43	14.70	94.54	0.307	No	Yes	0.35
2252	22.52	6.73	3.28	4.99	1.00	6.53	14.56	95.02	0.311	No	Yes	0.36
2253	22.53	6.80	3.27	4.99	1.00	6.62	14.43	95.48	0.316	No	Yes	0.36
2254	22.54	6.87	3.27	4.98	1.00	6.70	14.32	95.89	0.320	No	Yes	0.37
2255	22.55	6.93	3.26	4.98	1.00	6.76	14.23	96.22	0.323	No	Yes	0.37
2256	22.56	6.96	3.26	4.98	1.00	6.80	14.18	96.42	0.324	No	Yes	0.37

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
2257	22.57	6.97	3.26	4.99	1.00	6.81	14.17	96.52	0.325	No	Yes	0.37
2258	22.58	6.97	3.26	4.99	1.00	6.81	14.18	96.56	0.325	No	Yes	0.37
2259	22.59	6.97	3.26	5.00	1.00	6.81	14.20	96.62	0.325	No	Yes	0.37
2260	22.60	6.97	3.26	5.01	1.00	6.80	14.21	96.68	0.324	No	Yes	0.37
2261	22.61	6.97	3.26	5.02	1.00	6.80	14.22	96.73	0.324	No	Yes	0.37
2262	22.62	6.97	3.26	5.03	1.00	6.80	14.24	96.79	0.324	No	Yes	0.37
2263	22.63	6.97	3.26	5.03	1.00	6.80	14.25	96.83	0.324	No	Yes	0.37
2264	22.64	6.95	3.27	5.04	1.00	6.76	14.30	96.74	0.323	No	Yes	0.37
2265	22.65	6.87	3.27	5.06	1.00	6.67	14.44	96.39	0.318	No	Yes	0.37
2266	22.66	6.75	3.28	5.08	1.00	6.52	14.69	95.73	0.311	No	Yes	0.36
2267	22.67	6.58	3.29	5.12	1.00	6.32	15.01	94.87	0.301	No	Yes	0.35
2268	22.68	6.40	3.31	5.16	1.00	6.10	15.39	93.91	0.291	No	Yes	0.33
2269	22.69	6.21	3.32	5.20	1.00	5.88	15.81	92.89	0.280	No	Yes	0.32
2270	22.70	6.03	3.34	5.25	1.00	5.65	16.25	91.86	0.270	No	Yes	0.31
2271	22.71	5.86	3.35	5.30	1.00	5.45	16.68	90.88	0.260	No	Yes	0.30
2272	22.72	5.71	3.37	5.34	1.00	5.27	17.09	90.00	0.251	No	Yes	0.29
2273	22.73	5.62	3.38	5.36	1.00	5.16	17.34	89.43	0.246	No	Yes	0.28
2274	22.74	5.58	3.38	5.37	1.00	5.11	17.45	89.12	0.244	No	Yes	0.28
2275	22.75	5.58	3.38	5.36	1.00	5.10	17.44	89.02	0.243	No	Yes	0.28
2276	22.76	5.58	3.38	5.34	1.00	5.10	17.43	88.91	0.243	No	Yes	0.28
2277	22.77	5.58	3.38	5.33	1.00	5.10	17.41	88.79	0.243	No	Yes	0.28
2278	22.78	5.58	3.38	5.31	1.00	5.10	17.39	88.66	0.243	No	Yes	0.28
2279	22.79	5.58	3.38	5.30	1.00	5.10	17.37	88.54	0.243	No	Yes	0.28
2280	22.80	5.58	3.38	5.28	1.00	5.09	17.36	88.43	0.243	No	Yes	0.28
2281	22.81	5.58	3.38	5.27	1.00	5.09	17.34	88.33	0.243	No	Yes	0.28
2282	22.82	5.58	3.38	5.26	1.00	5.09	17.33	88.22	0.243	No	Yes	0.28
2283	22.83	5.58	3.38	5.24	1.00	5.09	17.31	88.10	0.243	No	Yes	0.28
2284	22.84	5.58	3.38	5.22	1.00	5.09	17.29	87.94	0.243	No	Yes	0.28
2285	22.85	5.58	3.37	5.20	1.00	5.09	17.26	87.77	0.243	No	Yes	0.28
2286	22.86	5.58	3.37	5.18	1.00	5.08	17.23	87.58	0.242	No	Yes	0.28
2287	22.87	5.58	3.37	5.15	1.00	5.08	17.20	87.40	0.242	No	Yes	0.28
2288	22.88	5.58	3.37	5.13	1.00	5.08	17.17	87.22	0.242	No	Yes	0.28
2289	22.89	5.58	3.37	5.11	1.00	5.08	17.15	87.07	0.242	No	Yes	0.28
2290	22.90	5.58	3.37	5.10	1.00	5.08	17.13	86.96	0.242	No	Yes	0.28
2291	22.91	5.58	3.37	5.09	1.00	5.07	17.12	86.90	0.242	No	Yes	0.28
2292	22.92	5.58	3.37	5.09	1.00	5.07	17.13	86.88	0.242	No	Yes	0.28
2293	22.93	5.58	3.37	5.09	1.00	5.07	17.13	86.87	0.242	No	Yes	0.28
2294	22.94	5.58	3.37	5.09	1.00	5.07	17.14	86.86	0.242	No	Yes	0.28
2295	22.95	5.58	3.37	5.09	1.00	5.07	17.14	86.85	0.242	No	Yes	0.28
2296	22.96	5.58	3.37	5.09	1.00	5.07	17.15	86.84	0.242	No	Yes	0.28
2297	22.97	5.58	3.37	5.09	1.00	5.06	17.15	86.84	0.242	No	Yes	0.28
2298	22.98	5.58	3.37	5.09	1.00	5.06	17.15	86.84	0.241	No	Yes	0.28
2299	22.99	5.64	3.37	5.08	1.00	5.13	17.00	87.24	0.245	No	Yes	0.28
2300	23.00	5.77	3.35	5.07	1.00	5.28	16.68	88.13	0.252	No	Yes	0.29
2301	23.01	5.98	3.34	5.05	1.00	5.54	16.18	89.56	0.264	No	Yes	0.30
2302	23.02	6.23	3.32	5.02	1.00	5.82	15.65	91.17	0.278	No	Yes	0.32
2303	23.03	6.49	3.30	5.00	1.00	6.13	15.14	92.86	0.293	No	Yes	0.34
2304	23.04	6.76	3.28	4.99	1.00	6.45	14.66	94.55	0.308	No	Yes	0.35

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
2305	23.05	7.02	3.26	4.98	1.00	6.75	14.24	96.14	0.322	No	Yes	0.37
2306	23.06	7.25	3.25	4.97	1.00	7.03	13.89	97.57	0.335	No	Yes	0.38
2307	23.07	7.44	3.24	4.97	1.00	7.25	13.62	98.73	0.346	No	Yes	0.40
2308	23.08	7.58	3.23	4.98	1.00	7.41	13.45	99.63	0.353	No	Yes	0.40
2309	23.09	7.67	3.23	5.00	1.00	7.52	13.35	100.40	0.359	No	Yes	0.41
2310	23.10	7.76	3.22	5.03	1.00	7.62	13.27	101.20	0.364	No	Yes	0.42
2311	23.11	7.87	3.22	5.07	1.00	7.74	13.19	102.10	0.369	No	Yes	0.42
2312	23.12	7.97	3.22	5.10	1.00	7.86	13.10	103.05	0.375	No	Yes	0.43
2313	23.13	8.08	3.21	5.14	1.00	7.99	13.02	103.99	0.381	No	Yes	0.44
2314	23.14	8.18	3.21	5.17	1.00	8.10	12.94	104.88	0.387	No	Yes	0.44
2315	23.15	8.27	3.21	5.20	1.00	8.21	12.88	105.68	0.391	No	Yes	0.45
2316	23.16	8.32	3.21	5.23	1.00	8.27	12.85	106.25	0.394	No	Yes	0.45
2317	23.17	8.33	3.21	5.26	1.00	8.28	12.88	106.58	0.395	No	Yes	0.45
2318	23.18	8.30	3.21	5.30	1.00	8.24	12.96	106.75	0.393	No	Yes	0.45
2319	23.19	8.25	3.21	5.34	1.00	8.18	13.07	106.88	0.390	No	Yes	0.45
2320	23.20	8.20	3.22	5.39	1.00	8.11	13.19	107.03	0.387	No	Yes	0.44
2321	23.21	8.15	3.23	5.45	1.00	8.05	13.32	107.17	0.384	No	Yes	0.44
2322	23.22	8.10	3.23	5.50	1.00	7.98	13.44	107.30	0.381	No	Yes	0.44
2323	23.23	8.05	3.24	5.55	1.00	7.92	13.56	107.42	0.378	No	Yes	0.43
2324	23.24	8.01	3.24	5.59	1.00	7.87	13.66	107.53	0.375	No	Yes	0.43
2325	23.25	8.00	3.24	5.62	1.00	7.87	13.70	107.79	0.375	No	Yes	0.43
2326	23.26	8.05	3.24	5.64	1.00	7.91	13.68	108.26	0.378	No	Yes	0.43
2327	23.27	8.13	3.24	5.66	1.00	8.01	13.60	108.98	0.382	No	Yes	0.44
2328	23.28	8.23	3.23	5.69	1.00	8.13	13.51	109.80	0.388	No	Yes	0.44
2329	23.29	8.34	3.23	5.72	1.00	8.25	13.42	110.69	0.393	No	Yes	0.45
2330	23.30	8.44	3.23	5.74	1.00	8.37	13.33	111.58	0.399	No	Yes	0.46
2331	23.31	8.55	3.22	5.77	1.00	8.49	13.25	112.44	0.405	No	Yes	0.46
2332	23.32	8.64	3.22	5.80	1.00	8.59	13.17	113.22	0.410	No	Yes	0.47
2333	23.33	8.72	3.22	5.82	1.00	8.69	13.11	113.89	0.414	No	Yes	0.47
2334	23.34	8.79	3.21	5.83	1.00	8.77	13.06	114.49	0.418	No	Yes	0.48
2335	23.35	8.87	3.21	5.85	1.00	8.86	13.00	115.12	0.423	No	Yes	0.48
2336	23.36	8.96	3.21	5.87	1.00	8.96	12.93	115.84	0.427	No	Yes	0.49
2337	23.37	9.06	3.21	5.90	1.00	9.08	12.85	116.65	0.433	No	Yes	0.49
2338	23.38	9.17	3.20	5.92	1.00	9.20	12.77	117.51	0.439	No	Yes	0.50
2339	23.39	9.28	3.20	5.95	1.00	9.32	12.70	118.35	0.445	No	Yes	0.51
2340	23.40	9.38	3.20	5.97	1.00	9.43	12.63	119.15	0.450	No	Yes	0.51
2341	23.41	9.47	3.19	5.99	1.00	9.54	12.57	119.86	0.455	No	Yes	0.52
2342	23.42	9.54	3.19	6.01	1.00	9.62	12.52	120.43	0.459	No	Yes	0.52
2343	23.43	9.62	3.19	6.01	1.00	9.71	12.46	120.90	0.463	No	Yes	0.53
2344	23.44	9.70	3.18	6.01	1.00	9.80	12.38	121.34	0.467	No	Yes	0.53
2345	23.45	9.79	3.18	6.01	1.00	9.91	12.30	121.84	0.473	No	Yes	0.54
2346	23.46	9.90	3.18	6.01	1.00	10.02	12.21	122.38	0.478	No	Yes	0.55
2347	23.47	10.00	3.17	6.01	1.00	10.15	12.12	122.93	0.484	No	Yes	0.55
2348	23.48	10.11	3.17	6.00	1.00	10.26	12.03	123.47	0.490	No	Yes	0.56
2349	23.49	10.21	3.16	6.00	1.00	10.37	11.95	123.97	0.495	No	Yes	0.56
2350	23.50	10.29	3.16	6.00	1.00	10.47	11.88	124.40	0.499	No	Yes	0.57
2351	23.51	10.38	3.16	5.99	1.00	10.56	11.81	124.76	0.504	No	Yes	0.57
2352	23.52	10.47	3.15	5.98	1.00	10.67	11.72	125.09	0.509	No	Yes	0.58

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
2353	23.53	10.59	3.15	5.95	1.00	10.81	11.61	125.45	0.516	No	Yes	0.59
2354	23.54	10.72	3.14	5.93	1.00	10.96	11.48	125.86	0.523	No	Yes	0.60
2355	23.55	10.87	3.14	5.90	1.00	11.13	11.35	126.28	0.531	No	Yes	0.60
2356	23.56	11.02	3.13	5.87	1.00	11.29	11.22	126.70	0.539	No	Yes	0.61
2357	23.57	11.16	3.12	5.84	1.00	11.46	11.09	127.10	0.546	No	Yes	0.62
2358	23.58	11.29	3.12	5.82	1.00	11.60	10.99	127.45	0.553	No	Yes	0.63
2359	23.59	11.39	3.11	5.80	1.00	11.72	10.90	127.74	0.559	No	Yes	0.64
2360	23.60	11.48	3.11	5.79	1.00	11.82	10.83	128.00	0.564	No	Yes	0.64
2361	23.61	11.56	3.11	5.78	1.00	11.91	10.77	128.27	0.568	No	Yes	0.65
2362	23.62	11.66	3.10	5.77	1.00	12.02	10.70	128.59	0.573	No	Yes	0.65
2363	23.63	11.76	3.10	5.76	1.00	12.13	10.63	128.95	0.579	No	Yes	0.66
2364	23.64	11.86	3.10	5.75	1.00	12.25	10.56	129.32	0.584	No	Yes	0.67
2365	23.65	11.97	3.09	5.74	1.00	12.37	10.48	129.68	0.590	No	Yes	0.67
2366	23.66	12.07	3.09	5.73	1.00	12.48	10.42	130.02	0.595	No	Yes	0.68
2367	23.67	12.16	3.09	5.72	1.00	12.58	10.36	130.32	0.600	No	Yes	0.68
2368	23.68	12.21	3.09	5.72	1.00	12.64	10.33	130.55	0.603	No	Yes	0.69
2369	23.69	12.23	3.09	5.73	1.00	12.65	10.34	130.74	0.603	No	Yes	0.69
2370	23.70	12.20	3.09	5.76	1.00	12.62	10.38	130.91	0.602	No	Yes	0.68
2371	23.71	12.17	3.09	5.79	1.00	12.57	10.43	131.10	0.600	No	Yes	0.68
2372	23.72	12.13	3.09	5.83	1.00	12.52	10.49	131.31	0.597	No	Yes	0.68
2373	23.73	12.09	3.10	5.86	1.00	12.47	10.55	131.53	0.595	No	Yes	0.68
2374	23.74	12.05	3.10	5.90	1.00	12.42	10.60	131.73	0.593	No	Yes	0.67
2375	23.75	12.01	3.10	5.93	1.00	12.38	10.66	131.92	0.590	No	Yes	0.67
2376	23.76	11.99	3.10	5.96	1.00	12.34	10.70	132.11	0.589	No	Yes	0.67
2377	23.77	12.06	3.10	5.98	1.00	12.43	10.68	132.73	0.593	No	Yes	0.67
2378	23.78	12.26	3.10	6.00	1.00	12.65	10.58	133.90	0.604	No	Yes	0.69
2379	23.79	12.59	3.09	6.03	1.00	13.03	10.42	135.68	0.621	No	Yes	0.71
2380	23.80	12.96	3.08	6.05	1.00	13.45	10.24	137.70	0.642	No	Yes	0.73
2381	23.81	13.35	3.07	6.09	1.00	13.90	10.06	139.83	0.663	No	Yes	0.75
2382	23.82	13.75	3.06	6.12	1.00	14.36	9.89	141.98	0.685	No	Yes	0.78
2383	23.83	14.14	3.05	6.15	1.00	14.80	9.73	144.03	0.706	No	Yes	0.80
2384	23.84	14.49	3.05	6.18	1.00	15.20	9.60	145.88	0.725	No	Yes	0.82
2385	23.85	14.77	3.04	6.20	1.00	15.52	9.50	147.36	0.740	No	Yes	0.84
2386	23.86	14.96	3.04	6.23	1.00	15.74	9.43	148.48	0.751	No	Yes	0.85
2387	23.87	15.11	3.03	6.25	1.00	15.91	9.39	149.39	0.759	No	Yes	0.86
2388	23.88	15.25	3.03	6.28	1.00	16.06	9.36	150.31	0.766	No	Yes	0.87
2389	23.89	15.40	3.03	6.31	1.00	16.23	9.33	151.34	0.774	No	Yes	0.88
2390	23.90	15.56	3.03	6.35	1.00	16.41	9.29	152.43	0.783	No	Yes	0.89
2391	23.91	15.72	3.03	6.38	1.00	16.59	9.25	153.50	0.791	No	Yes	0.90
2392	23.92	15.87	3.03	6.41	1.00	16.75	9.22	154.52	0.799	No	Yes	0.91
2393	23.93	16.00	3.02	6.44	1.00	16.90	9.20	155.42	0.806	No	Yes	0.92
2394	23.94	16.04	3.02	6.46	1.00	16.94	9.20	155.86	0.808	No	Yes	0.92
2395	23.95	15.96	3.03	6.48	1.00	16.85	9.24	155.74	0.804	No	Yes	0.91
2396	23.96	15.76	3.03	6.49	1.00	16.60	9.34	155.06	0.792	No	Yes	0.90
2397	23.97	15.49	3.04	6.51	1.00	16.29	9.46	154.17	0.777	No	Yes	0.88
2398	23.98	15.21	3.05	6.53	1.00	15.96	9.60	153.18	0.761	No	Yes	0.86
2399	23.99	14.91	3.05	6.55	1.00	15.61	9.74	152.14	0.745	No	Yes	0.85
2400	24.00	14.63	3.06	6.57	1.00	15.28	9.89	151.11	0.729	No	Yes	0.83

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
2401	24.01	14.36	3.07	6.59	1.00	14.97	10.03	150.13	0.714	No	Yes	0.81
2402	24.02	14.14	3.08	6.60	1.00	14.70	10.15	149.29	0.701	No	Yes	0.80
2403	24.03	13.99	3.08	6.61	1.00	14.53	10.24	148.71	0.693	No	Yes	0.79
2404	24.04	13.91	3.08	6.62	1.00	14.43	10.28	148.33	0.688	No	Yes	0.78
2405	24.05	13.86	3.08	6.61	1.00	14.37	10.30	148.07	0.686	No	Yes	0.78
2406	24.06	13.81	3.09	6.61	1.00	14.31	10.33	147.78	0.683	No	Yes	0.77
2407	24.07	13.76	3.09	6.61	1.00	14.24	10.35	147.47	0.679	No	Yes	0.77
2408	24.08	13.71	3.09	6.60	1.00	14.18	10.38	147.15	0.676	No	Yes	0.77
2409	24.09	13.66	3.09	6.60	1.00	14.11	10.40	146.85	0.673	No	Yes	0.76
2410	24.10	13.61	3.09	6.60	1.00	14.06	10.43	146.57	0.670	No	Yes	0.76
2411	24.11	13.56	3.09	6.60	1.00	13.99	10.46	146.31	0.667	No	Yes	0.76
2412	24.12	13.48	3.09	6.60	1.00	13.89	10.51	145.98	0.663	No	Yes	0.75
2413	24.13	13.35	3.10	6.62	1.00	13.75	10.59	145.56	0.656	No	Yes	0.74
2414	24.14	13.19	3.10	6.64	1.00	13.56	10.69	145.01	0.647	No	Yes	0.73
2415	24.15	13.02	3.11	6.66	1.00	13.35	10.82	144.40	0.637	No	Yes	0.72
2416	24.16	12.83	3.12	6.69	1.00	13.13	10.95	143.75	0.626	No	Yes	0.71
2417	24.17	12.64	3.12	6.71	1.00	12.92	11.08	143.10	0.616	No	Yes	0.70
2418	24.18	12.47	3.13	6.74	1.00	12.71	11.21	142.47	0.606	No	Yes	0.69
2419	24.19	12.32	3.14	6.76	1.00	12.53	11.33	141.90	0.598	No	Yes	0.68
2420	24.20	12.18	3.14	6.78	1.00	12.37	11.43	141.43	0.590	No	Yes	0.67
2421	24.21	12.05	3.15	6.81	1.00	12.22	11.54	141.01	0.583	No	Yes	0.66
2422	24.22	11.91	3.15	6.84	1.00	12.05	11.67	140.58	0.575	No	Yes	0.65
2423	24.23	11.74	3.16	6.89	1.00	11.85	11.82	140.08	0.565	No	Yes	0.64
2424	24.24	11.56	3.17	6.93	1.00	11.64	11.98	139.52	0.555	No	Yes	0.63
2425	24.25	11.37	3.17	6.98	1.00	11.42	12.16	138.93	0.545	No	Yes	0.62
2426	24.26	11.19	3.18	7.02	1.00	11.21	12.34	138.34	0.535	No	Yes	0.61
2427	24.27	11.02	3.19	7.07	1.00	11.01	12.51	137.78	0.525	No	Yes	0.59
2428	24.28	10.88	3.20	7.10	1.00	10.85	12.65	137.32	0.518	No	Yes	0.59
2429	24.29	10.85	3.20	7.13	1.00	10.81	12.70	137.31	0.516	No	Yes	0.58
2430	24.30	10.91	3.20	7.14	1.00	10.88	12.67	137.79	0.519	No	Yes	0.59
2431	24.31	11.06	3.19	7.14	1.00	11.05	12.56	138.72	0.527	No	Yes	0.60
2432	24.32	11.24	3.19	7.15	1.00	11.24	12.43	139.77	0.536	No	Yes	0.61
2433	24.33	11.42	3.18	7.16	1.00	11.45	12.30	140.89	0.546	No	Yes	0.62
2434	24.34	11.61	3.18	7.16	1.00	11.66	12.18	142.00	0.556	No	Yes	0.63
2435	24.35	11.79	3.17	7.17	1.00	11.86	12.06	143.07	0.566	No	Yes	0.64
2436	24.36	11.95	3.17	7.18	1.00	12.04	11.96	144.03	0.574	No	Yes	0.65
2437	24.37	12.09	3.16	7.19	1.00	12.19	11.88	144.83	0.582	No	Yes	0.66
2438	24.38	12.22	3.16	7.19	1.00	12.34	11.80	145.56	0.588	No	Yes	0.67
2439	24.39	12.35	3.15	7.19	1.00	12.49	11.72	146.32	0.596	No	Yes	0.67
2440	24.40	12.52	3.15	7.19	1.00	12.67	11.62	147.18	0.604	No	Yes	0.68
2441	24.41	12.69	3.14	7.20	1.00	12.87	11.51	148.14	0.614	No	Yes	0.69
2442	24.42	12.88	3.14	7.20	1.00	13.07	11.41	149.14	0.624	No	Yes	0.71
2443	24.43	13.07	3.13	7.20	1.00	13.28	11.31	150.12	0.633	No	Yes	0.72
2444	24.44	13.24	3.13	7.21	1.00	13.47	11.21	151.04	0.643	No	Yes	0.73
2445	24.45	13.39	3.13	7.21	1.00	13.64	11.13	151.85	0.651	No	Yes	0.74
2446	24.46	13.50	3.12	7.21	1.00	13.75	11.08	152.35	0.656	No	Yes	0.74
2447	24.47	13.54	3.12	7.21	1.00	13.80	11.05	152.55	0.658	No	Yes	0.74
2448	24.48	13.55	3.12	7.20	1.00	13.81	11.05	152.50	0.659	No	Yes	0.74

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
2449	24.49	13.55	3.12	7.19	1.00	13.80	11.04	152.39	0.658	No	Yes	0.74
2450	24.50	13.55	3.12	7.19	1.00	13.80	11.04	152.28	0.658	No	Yes	0.74
2451	24.51	13.55	3.12	7.18	1.00	13.79	11.03	152.16	0.658	No	Yes	0.74
2452	24.52	13.55	3.12	7.17	1.00	13.79	11.03	152.05	0.658	No	Yes	0.74
2453	24.53	13.55	3.12	7.16	1.00	13.78	11.02	151.94	0.657	No	Yes	0.74
2454	24.54	13.55	3.12	7.15	1.00	13.77	11.02	151.83	0.657	No	Yes	0.74
2455	24.55	13.52	3.12	7.14	1.00	13.74	11.03	151.55	0.655	No	Yes	0.74
2456	24.56	13.46	3.12	7.13	1.00	13.67	11.05	151.06	0.652	No	Yes	0.74
2457	24.57	13.38	3.12	7.10	1.00	13.57	11.08	150.34	0.647	No	Yes	0.73
2458	24.58	13.28	3.13	7.08	1.00	13.45	11.12	149.52	0.641	No	Yes	0.72
2459	24.59	13.17	3.13	7.05	1.00	13.32	11.16	148.66	0.636	No	Yes	0.72
2460	24.60	13.06	3.13	7.02	1.00	13.20	11.20	147.79	0.630	No	Yes	0.71
2461	24.61	12.96	3.13	7.00	1.00	13.08	11.24	146.96	0.624	No	Yes	0.70
2462	24.62	12.87	3.13	6.97	1.00	12.97	11.27	146.20	0.619	No	Yes	0.70
2463	24.63	12.79	3.13	6.95	1.00	12.88	11.30	145.55	0.614	No	Yes	0.69
2464	24.64	12.72	3.14	6.93	1.00	12.79	11.33	144.93	0.610	No	Yes	0.69
2465	24.65	12.64	3.14	6.91	1.00	12.69	11.36	144.26	0.605	No	Yes	0.68
2466	24.66	12.55	3.14	6.88	1.00	12.58	11.40	143.47	0.600	No	Yes	0.68
2467	24.67	12.44	3.14	6.85	1.00	12.47	11.44	142.60	0.595	No	Yes	0.67
2468	24.68	12.34	3.14	6.82	1.00	12.34	11.48	141.70	0.589	No	Yes	0.66
2469	24.69	12.23	3.14	6.79	1.00	12.22	11.53	140.80	0.583	No	Yes	0.66
2470	24.70	12.13	3.15	6.76	1.00	12.10	11.57	139.96	0.577	No	Yes	0.65
2471	24.71	12.04	3.15	6.74	1.00	12.00	11.60	139.22	0.572	No	Yes	0.65
2472	24.72	11.97	3.15	6.72	1.00	11.91	11.64	138.58	0.568	No	Yes	0.64
2473	24.73	11.89	3.15	6.70	1.00	11.82	11.67	137.98	0.564	No	Yes	0.64
2474	24.74	11.81	3.15	6.68	1.00	11.72	11.72	137.33	0.559	No	Yes	0.63
2475	24.75	11.71	3.16	6.66	1.00	11.61	11.77	136.59	0.554	No	Yes	0.62
2476	24.76	11.61	3.16	6.64	1.00	11.49	11.82	135.78	0.548	No	Yes	0.62
2477	24.77	11.50	3.16	6.62	1.00	11.36	11.88	134.95	0.542	No	Yes	0.61
2478	24.78	11.40	3.16	6.59	1.00	11.24	11.93	134.14	0.536	No	Yes	0.60
2479	24.79	11.30	3.17	6.57	1.00	11.13	11.98	133.40	0.531	No	Yes	0.60
2480	24.80	11.22	3.17	6.56	1.00	11.03	12.03	132.74	0.526	No	Yes	0.59
2481	24.81	11.11	3.17	6.55	1.00	10.91	12.10	132.06	0.520	No	Yes	0.59
2482	24.82	10.98	3.18	6.54	1.00	10.76	12.20	131.26	0.513	No	Yes	0.58
2483	24.83	10.80	3.18	6.54	1.00	10.56	12.34	130.26	0.503	No	Yes	0.57
2484	24.84	10.60	3.19	6.54	1.00	10.33	12.50	129.12	0.493	No	Yes	0.56
2485	24.85	10.39	3.20	6.54	1.00	10.09	12.68	127.90	0.481	No	Yes	0.54
2486	24.86	10.18	3.21	6.54	1.00	9.84	12.87	126.66	0.470	No	Yes	0.53
2487	24.87	9.98	3.21	6.54	1.00	9.61	13.05	125.46	0.458	No	Yes	0.52
2488	24.88	9.79	3.22	6.54	1.00	9.40	13.23	124.37	0.448	No	Yes	0.51
2489	24.89	9.65	3.23	6.54	1.00	9.23	13.37	123.49	0.440	No	Yes	0.50
2490	24.90	9.54	3.23	6.54	1.00	9.11	13.48	122.80	0.434	No	Yes	0.49
2491	24.91	9.45	3.24	6.54	1.00	9.00	13.57	122.23	0.430	No	Yes	0.48
2492	24.92	9.35	3.24	6.54	1.00	8.90	13.67	121.62	0.424	No	Yes	0.48
2493	24.93	9.25	3.24	6.54	1.00	8.78	13.78	120.95	0.419	No	Yes	0.47
2494	24.94	9.14	3.25	6.53	1.00	8.66	13.89	120.24	0.413	No	Yes	0.47
2495	24.95	9.04	3.25	6.53	1.00	8.54	14.00	119.54	0.407	No	Yes	0.46
2496	24.96	8.94	3.26	6.53	1.00	8.42	14.12	118.88	0.402	No	Yes	0.45

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
2497	24.97	8.85	3.26	6.53	1.00	8.32	14.22	118.29	0.397	No	Yes	0.45
2498	24.98	8.78	3.27	6.53	1.00	8.23	14.31	117.79	0.393	No	Yes	0.44
2499	24.99	8.70	3.27	6.53	1.00	8.15	14.40	117.31	0.389	No	Yes	0.44
2500	25.00	8.62	3.27	6.54	1.00	8.05	14.50	116.78	0.384	No	Yes	0.43
2501	25.01	8.52	3.28	6.54	1.00	7.94	14.63	116.17	0.379	No	Yes	0.43
2502	25.02	8.42	3.28	6.55	1.00	7.82	14.77	115.51	0.373	No	Yes	0.42
2503	25.03	8.31	3.29	6.55	1.00	7.70	14.91	114.83	0.367	No	Yes	0.41
2504	25.04	8.21	3.30	6.56	1.00	7.58	15.06	114.16	0.362	No	Yes	0.41
2505	25.05	8.11	3.30	6.57	1.00	7.47	15.20	113.54	0.356	No	Yes	0.40
2506	25.06	8.03	3.31	6.57	1.00	7.38	15.32	113.00	0.352	No	Yes	0.40
2507	25.07	7.96	3.31	6.58	1.00	7.29	15.44	112.54	0.348	No	Yes	0.39
2508	25.08	7.88	3.31	6.59	1.00	7.20	15.56	112.08	0.344	No	Yes	0.39
2509	25.09	7.79	3.32	6.61	1.00	7.10	15.71	111.57	0.339	No	Yes	0.38
2510	25.10	7.69	3.33	6.63	1.00	6.99	15.88	110.99	0.333	No	Yes	0.37
2511	25.11	7.58	3.33	6.65	1.00	6.87	16.07	110.37	0.328	No	Yes	0.37
2512	25.12	7.48	3.34	6.67	1.00	6.75	16.27	109.74	0.322	No	Yes	0.36
2513	25.13	7.38	3.35	6.70	1.00	6.63	16.46	109.13	0.316	No	Yes	0.36
2514	25.14	7.28	3.35	6.72	1.00	6.53	16.64	108.57	0.311	No	Yes	0.35
2515	25.15	7.22	3.36	6.73	1.00	6.45	16.77	108.17	0.308	No	Yes	0.35
2516	25.16	7.18	3.36	6.75	1.00	6.41	16.85	107.98	0.306	No	Yes	0.34
2517	25.17	7.17	3.36	6.76	1.00	6.39	16.88	107.96	0.305	No	Yes	0.34
2518	25.18	7.17	3.36	6.77	1.00	6.39	16.90	108.03	0.305	No	Yes	0.34
2519	25.19	7.17	3.36	6.78	1.00	6.39	16.92	108.10	0.305	No	Yes	0.34
2520	25.20	7.17	3.36	6.79	1.00	6.39	16.93	108.17	0.305	No	Yes	0.34
2521	25.21	7.17	3.36	6.80	1.00	6.39	16.95	108.24	0.305	No	Yes	0.34
2522	25.22	7.17	3.36	6.82	1.00	6.38	16.97	108.31	0.304	No	Yes	0.34
2523	25.23	7.17	3.36	6.83	1.00	6.38	16.98	108.37	0.304	No	Yes	0.34
2524	25.24	7.15	3.37	6.83	1.00	6.36	17.03	108.26	0.303	No	Yes	0.34
2525	25.25	7.10	3.37	6.84	1.00	6.30	17.13	107.92	0.301	No	Yes	0.34
2526	25.26	7.02	3.38	6.85	1.00	6.21	17.29	107.32	0.296	No	Yes	0.33
2527	25.27	6.93	3.38	6.86	1.00	6.10	17.48	106.61	0.291	No	Yes	0.33
2528	25.28	6.82	3.39	6.87	1.00	5.98	17.70	105.83	0.285	No	Yes	0.32
2529	25.29	6.72	3.40	6.88	1.00	5.86	17.93	105.03	0.279	No	Yes	0.31
2530	25.30	6.61	3.40	6.90	1.00	5.74	18.16	104.25	0.274	No	Yes	0.31
2531	25.31	6.52	3.41	6.91	1.00	5.63	18.38	103.52	0.269	No	Yes	0.30
2532	25.32	6.44	3.42	6.92	1.00	5.55	18.56	102.92	0.265	No	Yes	0.30
2533	25.33	6.39	3.42	6.92	1.00	5.49	18.66	102.51	0.262	No	Yes	0.29
2534	25.34	6.38	3.42	6.90	1.00	5.47	18.68	102.23	0.261	No	Yes	0.29
2535	25.35	6.38	3.42	6.87	1.00	5.47	18.65	102.02	0.261	No	Yes	0.29
2536	25.36	6.38	3.42	6.84	1.00	5.47	18.61	101.79	0.261	No	Yes	0.29
2537	25.37	6.38	3.42	6.80	1.00	5.47	18.58	101.54	0.261	No	Yes	0.29
2538	25.38	6.38	3.42	6.77	1.00	5.46	18.54	101.29	0.261	No	Yes	0.29
2539	25.39	6.38	3.42	6.73	1.00	5.46	18.50	101.05	0.261	No	Yes	0.29
2540	25.40	6.38	3.41	6.70	1.00	5.46	18.47	100.84	0.260	No	Yes	0.29
2541	25.41	6.39	3.41	6.67	1.00	5.47	18.41	100.73	0.261	No	Yes	0.29
2542	25.42	6.43	3.41	6.64	1.00	5.51	18.29	100.82	0.263	No	Yes	0.29
2543	25.43	6.50	3.40	6.60	1.00	5.59	18.09	101.10	0.267	No	Yes	0.30
2544	25.44	6.59	3.39	6.55	1.00	5.69	17.84	101.50	0.271	No	Yes	0.30

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
2545	25.45	6.69	3.38	6.49	1.00	5.80	17.57	101.93	0.277	No	Yes	0.31
2546	25.46	6.80	3.38	6.44	1.00	5.92	17.30	102.36	0.282	No	Yes	0.32
2547	25.47	6.90	3.37	6.39	1.00	6.03	17.04	102.78	0.288	No	Yes	0.32
2548	25.48	7.00	3.36	6.34	1.00	6.14	16.80	103.16	0.293	No	Yes	0.33
2549	25.49	7.09	3.35	6.30	1.00	6.23	16.60	103.49	0.297	No	Yes	0.33
2550	25.50	7.17	3.35	6.26	1.00	6.31	16.44	103.79	0.301	No	Yes	0.34
2551	25.51	7.24	3.34	6.24	1.00	6.39	16.28	104.11	0.305	No	Yes	0.34
2552	25.52	7.32	3.33	6.21	1.00	6.49	16.11	104.50	0.309	No	Yes	0.35
2553	25.53	7.42	3.33	6.18	1.00	6.59	15.93	104.94	0.314	No	Yes	0.35
2554	25.54	7.53	3.32	6.15	1.00	6.70	15.73	105.42	0.320	No	Yes	0.36
2555	25.55	7.63	3.31	6.12	1.00	6.82	15.53	105.90	0.325	No	Yes	0.36
2556	25.56	7.74	3.31	6.09	1.00	6.93	15.35	106.35	0.331	No	Yes	0.37
2557	25.57	7.83	3.30	6.06	1.00	7.03	15.18	106.77	0.335	No	Yes	0.38
2558	25.58	7.91	3.29	6.04	1.00	7.12	15.04	107.13	0.340	No	Yes	0.38
2559	25.59	7.99	3.29	6.03	1.00	7.20	14.94	107.56	0.343	No	Yes	0.38
2560	25.60	8.06	3.29	6.04	1.00	7.28	14.84	108.11	0.347	No	Yes	0.39
2561	25.61	8.15	3.28	6.06	1.00	7.38	14.75	108.81	0.352	No	Yes	0.39
2562	25.62	8.25	3.28	6.08	1.00	7.49	14.64	109.61	0.357	No	Yes	0.40
2563	25.63	8.36	3.27	6.10	1.00	7.60	14.53	110.45	0.363	No	Yes	0.41
2564	25.64	8.47	3.27	6.12	1.00	7.71	14.43	111.30	0.368	No	Yes	0.41
2565	25.65	8.57	3.27	6.14	1.00	7.82	14.33	112.10	0.373	No	Yes	0.42
2566	25.66	8.66	3.26	6.16	1.00	7.92	14.24	112.82	0.378	No	Yes	0.42
2567	25.67	8.72	3.26	6.18	1.00	7.99	14.19	113.38	0.381	No	Yes	0.43
2568	25.68	8.76	3.26	6.20	1.00	8.03	14.18	113.79	0.383	No	Yes	0.43
2569	25.69	8.77	3.26	6.23	1.00	8.03	14.20	114.10	0.383	No	Yes	0.43
2570	25.70	8.77	3.26	6.27	1.00	8.03	14.25	114.43	0.383	No	Yes	0.43
2571	25.71	8.77	3.27	6.32	1.00	8.03	14.30	114.79	0.383	No	Yes	0.43
2572	25.72	8.77	3.27	6.36	1.00	8.02	14.35	115.16	0.383	No	Yes	0.43
2573	25.73	8.77	3.27	6.41	1.00	8.02	14.40	115.53	0.383	No	Yes	0.43
2574	25.74	8.77	3.27	6.45	1.00	8.02	14.45	115.87	0.383	No	Yes	0.43
2575	25.75	8.77	3.27	6.49	1.00	8.02	14.49	116.16	0.382	No	Yes	0.43
2576	25.76	8.79	3.27	6.51	1.00	8.04	14.49	116.48	0.383	No	Yes	0.43
2577	25.77	8.84	3.27	6.52	1.00	8.09	14.45	116.88	0.386	No	Yes	0.43
2578	25.78	8.92	3.27	6.52	1.00	8.18	14.36	117.40	0.390	No	Yes	0.44
2579	25.79	9.02	3.26	6.52	1.00	8.28	14.25	118.01	0.395	No	Yes	0.44
2580	25.80	9.12	3.26	6.52	1.00	8.39	14.14	118.66	0.400	No	Yes	0.45
2581	25.81	9.23	3.25	6.52	1.00	8.51	14.03	119.32	0.406	No	Yes	0.45
2582	25.82	9.33	3.25	6.53	1.00	8.62	13.92	119.96	0.411	No	Yes	0.46
2583	25.83	9.43	3.25	6.53	1.00	8.72	13.82	120.54	0.416	No	Yes	0.47
2584	25.84	9.51	3.24	6.53	1.00	8.81	13.74	121.03	0.420	No	Yes	0.47
2585	25.85	9.58	3.24	6.53	1.00	8.88	13.67	121.47	0.424	No	Yes	0.47
2586	25.86	9.66	3.24	6.53	1.00	8.97	13.60	121.91	0.428	No	Yes	0.48
2587	25.87	9.75	3.23	6.53	1.00	9.06	13.51	122.42	0.432	No	Yes	0.48
2588	25.88	9.85	3.23	6.53	1.00	9.17	13.42	122.99	0.437	No	Yes	0.49
2589	25.89	9.96	3.23	6.53	1.00	9.28	13.32	123.59	0.443	No	Yes	0.49
2590	25.90	10.06	3.22	6.53	1.00	9.39	13.22	124.19	0.448	No	Yes	0.50
2591	25.91	10.16	3.22	6.53	1.00	9.50	13.13	124.75	0.453	No	Yes	0.51
2592	25.92	10.25	3.21	6.53	1.00	9.60	13.05	125.26	0.458	No	Yes	0.51

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
2593	25.93	10.36	3.21	6.52	1.00	9.71	12.96	125.83	0.463	No	Yes	0.52
2594	25.94	10.53	3.20	6.52	1.00	9.89	12.81	126.67	0.472	No	Yes	0.53
2595	25.95	10.77	3.19	6.50	1.00	10.15	12.60	127.88	0.484	No	Yes	0.54
2596	25.96	11.07	3.18	6.49	1.00	10.48	12.35	129.37	0.500	No	Yes	0.56
2597	25.97	11.41	3.17	6.47	1.00	10.84	12.08	130.97	0.517	No	Yes	0.58
2598	25.98	11.75	3.16	6.46	1.00	11.21	11.83	132.62	0.535	No	Yes	0.60
2599	25.99	12.10	3.15	6.45	1.00	11.58	11.59	134.20	0.552	No	Yes	0.62
2600	26.00	12.42	3.14	6.44	1.00	11.93	11.37	135.66	0.569	No	Yes	0.64
2601	26.01	12.70	3.13	6.43	1.00	12.23	11.20	136.92	0.583	No	Yes	0.65
2602	26.02	12.89	3.12	6.43	1.00	12.44	11.08	137.82	0.593	No	Yes	0.66
2603	26.03	13.02	3.12	6.43	1.00	12.57	11.01	138.45	0.600	No	Yes	0.67
2604	26.04	13.11	3.12	6.44	1.00	12.66	10.97	138.94	0.604	No	Yes	0.67
2605	26.05	13.20	3.12	6.45	1.00	12.77	10.93	139.49	0.609	No	Yes	0.68
2606	26.06	13.31	3.11	6.46	1.00	12.88	10.88	140.09	0.614	No	Yes	0.69
2607	26.07	13.42	3.11	6.47	1.00	12.99	10.83	140.70	0.620	No	Yes	0.69
2608	26.08	13.52	3.11	6.48	1.00	13.10	10.79	141.28	0.625	No	Yes	0.70
2609	26.09	13.61	3.11	6.50	1.00	13.20	10.75	141.82	0.629	No	Yes	0.70
2610	26.10	13.68	3.11	6.51	1.00	13.26	10.73	142.20	0.632	No	Yes	0.71
2611	26.11	13.65	3.11	6.52	1.00	13.22	10.76	142.23	0.631	No	Yes	0.70
2612	26.12	13.53	3.11	6.54	1.00	13.09	10.84	141.90	0.624	No	Yes	0.70
2613	26.13	13.33	3.12	6.57	1.00	12.86	10.98	141.28	0.614	No	Yes	0.68
2614	26.14	13.10	3.13	6.61	1.00	12.61	11.14	140.57	0.602	No	Yes	0.67
2615	26.15	12.86	3.13	6.64	1.00	12.35	11.32	139.80	0.589	No	Yes	0.66
2616	26.16	12.62	3.14	6.68	1.00	12.09	11.50	139.01	0.577	No	Yes	0.64
2617	26.17	12.39	3.15	6.72	1.00	11.84	11.68	138.25	0.565	No	Yes	0.63
2618	26.18	12.19	3.16	6.75	1.00	11.61	11.85	137.54	0.554	No	Yes	0.62
2619	26.19	12.05	3.17	6.78	1.00	11.45	11.97	137.08	0.546	No	Yes	0.61
2620	26.20	11.97	3.17	6.81	1.00	11.37	12.05	136.93	0.542	No	Yes	0.60
2621	26.21	11.96	3.17	6.83	1.00	11.34	12.08	137.08	0.541	No	Yes	0.60
2622	26.22	11.96	3.17	6.86	1.00	11.34	12.11	137.35	0.541	No	Yes	0.60
2623	26.23	11.96	3.17	6.89	1.00	11.34	12.14	137.65	0.541	No	Yes	0.60
2624	26.24	11.96	3.17	6.92	1.00	11.33	12.17	137.96	0.541	No	Yes	0.60
2625	26.25	11.96	3.18	6.96	1.00	11.33	12.20	138.26	0.540	No	Yes	0.60
2626	26.26	11.96	3.18	6.99	1.00	11.33	12.23	138.55	0.540	No	Yes	0.60
2627	26.27	11.96	3.18	7.01	1.00	11.32	12.26	138.79	0.540	No	Yes	0.60
2628	26.28	11.98	3.18	7.03	1.00	11.34	12.26	139.09	0.541	No	Yes	0.60
2629	26.29	12.03	3.18	7.05	1.00	11.39	12.24	139.50	0.544	No	Yes	0.61
2630	26.30	12.11	3.18	7.06	1.00	11.48	12.20	140.07	0.548	No	Yes	0.61
2631	26.31	12.21	3.17	7.08	1.00	11.58	12.15	140.73	0.553	No	Yes	0.62
2632	26.32	12.32	3.17	7.09	1.00	11.69	12.10	141.43	0.558	No	Yes	0.62
2633	26.33	12.42	3.17	7.11	1.00	11.80	12.04	142.15	0.563	No	Yes	0.63
2634	26.34	12.53	3.17	7.13	1.00	11.91	11.99	142.85	0.568	No	Yes	0.63
2635	26.35	12.62	3.16	7.14	1.00	12.01	11.95	143.48	0.573	No	Yes	0.64
2636	26.36	12.70	3.16	7.15	1.00	12.09	11.91	143.99	0.577	No	Yes	0.64
2637	26.37	12.78	3.16	7.15	1.00	12.17	11.86	144.35	0.580	No	Yes	0.65
2638	26.38	12.85	3.16	7.14	1.00	12.25	11.81	144.60	0.584	No	Yes	0.65
2639	26.39	12.94	3.15	7.12	1.00	12.34	11.73	144.83	0.589	No	Yes	0.66
2640	26.40	13.04	3.15	7.09	1.00	12.45	11.66	145.07	0.594	No	Yes	0.66

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
2641	26.41	13.15	3.15	7.07	1.00	12.56	11.57	145.33	0.599	No	Yes	0.67
2642	26.42	13.26	3.14	7.04	1.00	12.67	11.49	145.58	0.604	No	Yes	0.67
2643	26.43	13.36	3.14	7.02	1.00	12.77	11.42	145.81	0.609	No	Yes	0.68
2644	26.44	13.45	3.14	7.00	1.00	12.86	11.35	146.02	0.614	No	Yes	0.68
2645	26.45	13.51	3.13	6.98	1.00	12.93	11.30	146.09	0.617	No	Yes	0.69
2646	26.46	13.54	3.13	6.96	1.00	12.96	11.26	145.97	0.618	No	Yes	0.69
2647	26.47	13.55	3.13	6.93	1.00	12.96	11.24	145.65	0.618	No	Yes	0.69
2648	26.48	13.55	3.13	6.89	1.00	12.96	11.21	145.23	0.618	No	Yes	0.69
2649	26.49	13.55	3.13	6.85	1.00	12.95	11.18	144.76	0.618	No	Yes	0.69
2650	26.50	13.55	3.13	6.81	1.00	12.95	11.14	144.28	0.618	No	Yes	0.69
2651	26.51	13.55	3.12	6.77	1.00	12.94	11.11	143.80	0.617	No	Yes	0.69
2652	26.52	13.55	3.12	6.73	1.00	12.94	11.08	143.36	0.617	No	Yes	0.69
2653	26.53	13.55	3.12	6.70	1.00	12.94	11.05	142.97	0.617	No	Yes	0.69
2654	26.54	13.56	3.12	6.67	1.00	12.94	11.03	142.70	0.617	No	Yes	0.69
2655	26.55	13.59	3.12	6.65	1.00	12.97	10.99	142.55	0.619	No	Yes	0.69
2656	26.56	13.63	3.12	6.62	1.00	13.01	10.95	142.46	0.620	No	Yes	0.69
2657	26.57	13.68	3.11	6.60	1.00	13.06	10.90	142.37	0.623	No	Yes	0.69
2658	26.58	13.73	3.11	6.57	1.00	13.11	10.85	142.27	0.625	No	Yes	0.70
2659	26.59	13.78	3.11	6.54	1.00	13.16	10.80	142.16	0.628	No	Yes	0.70
2660	26.60	13.84	3.11	6.51	1.00	13.21	10.75	142.06	0.630	No	Yes	0.70
2661	26.61	13.88	3.10	6.48	1.00	13.26	10.71	141.96	0.632	No	Yes	0.70
2662	26.62	13.91	3.10	6.46	1.00	13.29	10.68	141.84	0.634	No	Yes	0.71
2663	26.63	13.90	3.10	6.45	1.00	13.27	10.68	141.65	0.633	No	Yes	0.70
2664	26.64	13.85	3.10	6.45	1.00	13.20	10.70	141.35	0.630	No	Yes	0.70
2665	26.65	13.76	3.11	6.45	1.00	13.10	10.76	140.95	0.625	No	Yes	0.70
2666	26.66	13.65	3.11	6.46	1.00	12.99	10.81	140.50	0.620	No	Yes	0.69
2667	26.67	13.55	3.11	6.46	1.00	12.87	10.88	140.03	0.614	No	Yes	0.68
2668	26.68	13.44	3.12	6.46	1.00	12.76	10.94	139.55	0.608	No	Yes	0.68
2669	26.69	13.34	3.12	6.46	1.00	12.64	11.00	139.10	0.603	No	Yes	0.67
2670	26.70	13.25	3.12	6.46	1.00	12.54	11.06	138.69	0.598	No	Yes	0.67
2671	26.71	13.17	3.12	6.47	1.00	12.45	11.11	138.29	0.594	No	Yes	0.66
2672	26.72	13.07	3.13	6.47	1.00	12.34	11.17	137.83	0.589	No	Yes	0.65
2673	26.73	12.95	3.13	6.47	1.00	12.21	11.24	137.24	0.583	No	Yes	0.65
2674	26.74	12.81	3.14	6.46	1.00	12.06	11.32	136.53	0.575	No	Yes	0.64
2675	26.75	12.66	3.14	6.46	1.00	11.89	11.42	135.76	0.567	No	Yes	0.63
2676	26.76	12.50	3.14	6.46	1.00	11.71	11.52	134.95	0.559	No	Yes	0.62
2677	26.77	12.34	3.15	6.46	1.00	11.54	11.62	134.15	0.551	No	Yes	0.61
2678	26.78	12.19	3.15	6.46	1.00	11.38	11.72	133.41	0.543	No	Yes	0.60
2679	26.79	12.07	3.16	6.46	1.00	11.24	11.81	132.75	0.536	No	Yes	0.60
2680	26.80	11.99	3.16	6.45	1.00	11.16	11.86	132.30	0.532	No	Yes	0.59
2681	26.81	11.96	3.16	6.44	1.00	11.12	11.87	132.00	0.530	No	Yes	0.59
2682	26.82	11.96	3.16	6.43	1.00	11.11	11.86	131.79	0.530	No	Yes	0.59
2683	26.83	11.96	3.16	6.40	1.00	11.11	11.84	131.56	0.530	No	Yes	0.59
2684	26.84	11.95	3.16	6.38	1.00	11.11	11.82	131.32	0.530	No	Yes	0.59
2685	26.85	11.95	3.16	6.36	1.00	11.10	11.80	131.06	0.530	No	Yes	0.59
2686	26.86	11.95	3.16	6.34	1.00	11.10	11.79	130.82	0.529	No	Yes	0.59
2687	26.87	11.95	3.16	6.32	1.00	11.10	11.77	130.60	0.529	No	Yes	0.59
2688	26.88	11.98	3.15	6.30	1.00	11.12	11.74	130.53	0.531	No	Yes	0.59

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
2689	26.89	12.11	3.15	6.28	1.00	11.25	11.64	130.92	0.537	No	Yes	0.60
2690	26.90	12.35	3.14	6.26	1.00	11.50	11.46	131.80	0.549	No	Yes	0.61
2691	26.91	12.68	3.13	6.23	1.00	11.86	11.22	133.09	0.566	No	Yes	0.63
2692	26.92	13.06	3.12	6.20	1.00	12.26	10.97	134.49	0.585	No	Yes	0.65
2693	26.93	13.46	3.11	6.17	1.00	12.68	10.72	135.92	0.605	No	Yes	0.67
2694	26.94	13.86	3.09	6.14	1.00	13.09	10.49	137.32	0.625	No	Yes	0.69
2695	26.95	14.24	3.08	6.12	1.00	13.49	10.28	138.61	0.643	No	Yes	0.71
2696	26.96	14.57	3.07	6.10	1.00	13.84	10.09	139.73	0.660	No	Yes	0.73
2697	26.97	14.77	3.07	6.08	1.00	14.05	9.99	140.34	0.670	No	Yes	0.74
2698	26.98	14.79	3.07	6.07	1.00	14.06	9.98	140.30	0.671	No	Yes	0.74
2699	26.99	14.64	3.07	6.07	1.00	13.90	10.04	139.64	0.663	No	Yes	0.74
2700	27.00	14.43	3.08	6.07	1.00	13.67	10.15	138.72	0.652	No	Yes	0.72
2701	27.01	14.20	3.08	6.06	1.00	13.42	10.26	137.70	0.640	No	Yes	0.71
2702	27.02	13.96	3.09	6.06	1.00	13.16	10.38	136.65	0.628	No	Yes	0.70
2703	27.03	13.72	3.09	6.06	1.00	12.91	10.51	135.60	0.616	No	Yes	0.68
2704	27.04	13.50	3.10	6.06	1.00	12.67	10.62	134.62	0.604	No	Yes	0.67
2705	27.05	13.31	3.11	6.06	1.00	12.46	10.73	133.76	0.595	No	Yes	0.66
2706	27.06	13.08	3.11	6.07	1.00	12.22	10.87	132.81	0.583	No	Yes	0.65
2707	27.07	12.78	3.12	6.08	1.00	11.89	11.07	131.63	0.567	No	Yes	0.63
2708	27.08	12.37	3.14	6.11	1.00	11.46	11.35	130.06	0.546	No	Yes	0.61
2709	27.09	11.90	3.15	6.15	1.00	10.96	11.70	128.21	0.523	No	Yes	0.58
2710	27.10	11.40	3.17	6.19	1.00	10.43	12.10	126.17	0.497	No	Yes	0.55
2711	27.11	10.90	3.19	6.24	1.00	9.89	12.54	124.02	0.472	No	Yes	0.52
2712	27.12	10.41	3.21	6.29	1.00	9.37	13.01	121.88	0.447	No	Yes	0.50
2713	27.13	9.96	3.23	6.34	1.00	8.90	13.47	119.86	0.424	No	Yes	0.47
2714	27.14	9.63	3.25	6.39	1.00	8.54	13.85	118.32	0.407	No	Yes	0.45
2715	27.15	9.48	3.26	6.42	1.00	8.38	14.04	117.69	0.400	No	Yes	0.44
2716	27.16	9.50	3.26	6.44	1.00	8.40	14.05	117.95	0.401	No	Yes	0.44
2717	27.17	9.61	3.25	6.45	1.00	8.51	13.95	118.73	0.406	No	Yes	0.45
2718	27.18	9.74	3.25	6.47	1.00	8.64	13.84	119.60	0.412	No	Yes	0.46
2719	27.19	9.87	3.24	6.49	1.00	8.78	13.72	120.52	0.419	No	Yes	0.46
2720	27.20	10.00	3.24	6.50	1.00	8.92	13.62	121.43	0.425	No	Yes	0.47
2721	27.21	10.13	3.23	6.52	1.00	9.05	13.52	122.29	0.432	No	Yes	0.48
2722	27.22	10.24	3.23	6.54	1.00	9.16	13.43	123.05	0.437	No	Yes	0.48
2723	27.23	10.32	3.23	6.55	1.00	9.24	13.37	123.57	0.441	No	Yes	0.49
2724	27.24	10.35	3.23	6.55	1.00	9.28	13.35	123.83	0.443	No	Yes	0.49
2725	27.25	10.36	3.23	6.56	1.00	9.28	13.35	123.89	0.443	No	Yes	0.49
2726	27.26	10.36	3.23	6.56	1.00	9.28	13.35	123.91	0.443	No	Yes	0.49
2727	27.27	10.36	3.23	6.57	1.00	9.28	13.36	123.93	0.442	No	Yes	0.49
2728	27.28	10.36	3.23	6.57	1.00	9.27	13.37	123.95	0.442	No	Yes	0.49
2729	27.29	10.36	3.23	6.57	1.00	9.27	13.37	123.97	0.442	No	Yes	0.49
2730	27.30	10.36	3.23	6.58	1.00	9.27	13.38	123.99	0.442	No	Yes	0.49
2731	27.31	10.36	3.23	6.58	1.00	9.26	13.39	124.00	0.442	No	Yes	0.49
2732	27.32	10.36	3.23	6.58	1.00	9.26	13.39	123.99	0.442	No	Yes	0.49
2733	27.33	10.36	3.23	6.58	1.00	9.26	13.39	123.95	0.442	No	Yes	0.49
2734	27.34	10.36	3.23	6.57	1.00	9.25	13.39	123.89	0.441	No	Yes	0.49
2735	27.35	10.36	3.23	6.57	1.00	9.25	13.38	123.81	0.441	No	Yes	0.49
2736	27.36	10.36	3.23	6.56	1.00	9.25	13.38	123.73	0.441	No	Yes	0.49

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _t (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
2737	27.37	10.36	3.23	6.55	1.00	9.25	13.37	123.65	0.441	No	Yes	0.49
2738	27.38	10.36	3.23	6.55	1.00	9.24	13.37	123.58	0.441	No	Yes	0.49
2739	27.39	10.36	3.23	6.54	1.00	9.24	13.37	123.50	0.441	No	Yes	0.49
2740	27.40	10.39	3.23	6.53	1.00	9.27	13.34	123.58	0.442	No	Yes	0.49
2741	27.41	10.50	3.22	6.52	1.00	9.38	13.23	124.08	0.447	No	Yes	0.50
2742	27.42	10.71	3.21	6.50	1.00	9.60	13.03	125.06	0.458	No	Yes	0.51
2743	27.43	11.01	3.20	6.48	1.00	9.91	12.76	126.43	0.473	No	Yes	0.52
2744	27.44	11.34	3.19	6.46	1.00	10.25	12.48	127.93	0.489	No	Yes	0.54
2745	27.45	11.68	3.18	6.43	1.00	10.61	12.21	129.46	0.506	No	Yes	0.56
2746	27.46	12.03	3.16	6.41	1.00	10.96	11.94	130.97	0.523	No	Yes	0.58
2747	27.47	12.35	3.15	6.40	1.00	11.30	11.71	132.36	0.539	No	Yes	0.60
2748	27.48	12.64	3.14	6.38	1.00	11.60	11.51	133.57	0.553	No	Yes	0.61
2749	27.49	12.89	3.14	6.37	1.00	11.86	11.35	134.63	0.566	No	Yes	0.63
2750	27.50	13.13	3.13	6.37	1.00	12.11	11.21	135.70	0.577	No	Yes	0.64
2751	27.51	13.40	3.12	6.37	1.00	12.38	11.06	136.91	0.591	No	Yes	0.65
2752	27.52	13.71	3.11	6.37	1.00	12.70	10.89	138.33	0.606	No	Yes	0.67
2753	27.53	14.05	3.11	6.38	1.00	13.05	10.72	139.85	0.622	No	Yes	0.69
2754	27.54	14.39	3.10	6.38	1.00	13.41	10.55	141.40	0.640	No	Yes	0.71
2755	27.55	14.73	3.09	6.39	1.00	13.76	10.39	142.91	0.656	No	Yes	0.73
2756	27.56	15.05	3.08	6.40	1.00	14.08	10.25	144.29	0.672	No	Yes	0.74
2757	27.57	15.31	3.08	6.40	1.00	14.35	10.13	145.44	0.685	No	Yes	0.76
2758	27.58	15.39	3.07	6.42	1.00	14.43	10.12	145.96	0.688	No	Yes	0.76
2759	27.59	15.28	3.08	6.45	1.00	14.31	10.20	145.89	0.682	No	Yes	0.76
2760	27.60	14.99	3.09	6.50	1.00	14.01	10.37	145.30	0.668	No	Yes	0.74
2761	27.61	14.67	3.10	6.56	1.00	13.67	10.58	144.60	0.652	No	Yes	0.72
2762	27.62	14.33	3.11	6.63	1.00	13.31	10.81	143.82	0.635	No	Yes	0.70
2763	27.63	13.98	3.12	6.69	1.00	12.94	11.05	142.98	0.617	No	Yes	0.68
2764	27.64	13.65	3.13	6.76	1.00	12.59	11.29	142.14	0.601	No	Yes	0.66
2765	27.65	13.35	3.14	6.82	1.00	12.27	11.52	141.34	0.585	No	Yes	0.65
2766	27.66	13.08	3.15	6.87	1.00	11.99	11.73	140.58	0.572	No	Yes	0.63
2767	27.67	12.79	3.16	6.93	1.00	11.69	11.95	139.71	0.557	No	Yes	0.62
2768	27.68	12.46	3.18	6.99	1.00	11.33	12.23	138.59	0.541	No	Yes	0.60
2769	27.69	12.05	3.19	7.06	1.00	10.90	12.58	137.16	0.520	No	Yes	0.58
2770	27.70	11.59	3.21	7.15	1.00	10.42	13.00	135.49	0.497	No	Yes	0.55
2771	27.71	11.11	3.23	7.25	1.00	9.92	13.47	133.66	0.473	No	Yes	0.52
2772	27.72	10.63	3.25	7.35	1.00	9.42	13.98	131.75	0.449	No	Yes	0.50
2773	27.73	10.18	3.27	7.45	1.00	8.95	14.51	129.85	0.427	No	Yes	0.47
2774	27.74	9.79	3.29	7.55	1.00	8.53	15.01	128.09	0.407	No	Yes	0.45
2775	27.75	9.52	3.31	7.62	1.00	8.25	15.38	126.91	0.394	No	Yes	0.44
2776	27.76	9.39	3.31	7.67	1.00	8.11	15.58	126.37	0.387	No	Yes	0.43
2777	27.77	9.37	3.32	7.69	1.00	8.09	15.63	126.41	0.386	No	Yes	0.43
2778	27.78	9.37	3.32	7.72	1.00	8.09	15.65	126.58	0.386	No	Yes	0.43
2779	27.79	9.37	3.32	7.74	1.00	8.08	15.68	126.77	0.386	No	Yes	0.43
2780	27.80	9.37	3.32	7.77	1.00	8.08	15.71	126.96	0.385	No	Yes	0.43
2781	27.81	9.37	3.32	7.79	1.00	8.08	15.74	127.15	0.385	No	Yes	0.43
2782	27.82	9.37	3.32	7.82	1.00	8.08	15.77	127.32	0.385	No	Yes	0.43
2783	27.83	9.37	3.32	7.84	1.00	8.08	15.78	127.50	0.385	No	Yes	0.43
2784	27.84	9.44	3.32	7.84	1.00	8.15	15.71	127.96	0.389	No	Yes	0.43

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _t (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
2785	27.85	9.59	3.31	7.82	1.00	8.30	15.52	128.79	0.396	No	Yes	0.44
2786	27.86	9.81	3.30	7.79	1.00	8.53	15.24	130.02	0.407	No	Yes	0.45
2787	27.87	10.07	3.29	7.75	1.00	8.80	14.94	131.40	0.420	No	Yes	0.46
2788	27.88	10.35	3.28	7.71	1.00	9.08	14.63	132.84	0.433	No	Yes	0.48
2789	27.89	10.63	3.27	7.67	1.00	9.37	14.33	134.27	0.447	No	Yes	0.49
2790	27.90	10.90	3.26	7.64	1.00	9.64	14.06	135.62	0.460	No	Yes	0.51
2791	27.91	11.14	3.25	7.61	1.00	9.89	13.83	136.82	0.472	No	Yes	0.52
2792	27.92	11.34	3.24	7.59	1.00	10.09	13.65	137.75	0.481	No	Yes	0.53
2793	27.93	11.49	3.23	7.57	1.00	10.24	13.51	138.39	0.489	No	Yes	0.54
2794	27.94	11.61	3.23	7.54	1.00	10.37	13.39	138.82	0.494	No	Yes	0.55
2795	27.95	11.74	3.22	7.50	1.00	10.49	13.27	139.21	0.501	No	Yes	0.55
2796	27.96	11.88	3.22	7.47	1.00	10.63	13.13	139.63	0.507	No	Yes	0.56
2797	27.97	12.02	3.21	7.43	1.00	10.78	12.99	140.06	0.514	No	Yes	0.57
2798	27.98	12.17	3.21	7.39	1.00	10.93	12.85	140.48	0.521	No	Yes	0.58
2799	27.99	12.31	3.20	7.35	1.00	11.07	12.73	140.86	0.528	No	Yes	0.58
2800	28.00	12.43	3.20	7.32	1.00	11.19	12.62	141.20	0.534	No	Yes	0.59
2801	28.01	12.48	3.19	7.30	1.00	11.24	12.56	141.24	0.536	No	Yes	0.59
2802	28.02	12.46	3.19	7.28	1.00	11.22	12.56	140.88	0.535	No	Yes	0.59
2803	28.03	12.36	3.19	7.26	1.00	11.11	12.62	140.12	0.530	No	Yes	0.59
2804	28.04	12.23	3.20	7.23	1.00	10.97	12.69	139.17	0.523	No	Yes	0.58
2805	28.05	12.08	3.20	7.21	1.00	10.82	12.77	138.14	0.516	No	Yes	0.57
2806	28.06	11.94	3.21	7.18	1.00	10.66	12.86	137.08	0.509	No	Yes	0.56
2807	28.07	11.79	3.21	7.16	1.00	10.51	12.94	136.04	0.501	No	Yes	0.55
2808	28.08	11.66	3.21	7.13	1.00	10.37	13.03	135.08	0.495	No	Yes	0.55
2809	28.09	11.55	3.22	7.11	1.00	10.25	13.10	134.25	0.489	No	Yes	0.54
2810	28.10	11.44	3.22	7.10	1.00	10.14	13.17	133.50	0.484	No	Yes	0.53
2811	28.11	11.34	3.22	7.08	1.00	10.03	13.24	132.74	0.478	No	Yes	0.53
2812	28.12	11.22	3.23	7.06	1.00	9.90	13.32	131.87	0.472	No	Yes	0.52
2813	28.13	11.08	3.23	7.04	1.00	9.76	13.41	130.88	0.465	No	Yes	0.51
2814	28.14	10.94	3.23	7.01	1.00	9.61	13.52	129.83	0.458	No	Yes	0.51
2815	28.15	10.79	3.24	6.99	1.00	9.45	13.62	128.76	0.451	No	Yes	0.50
2816	28.16	10.65	3.24	6.97	1.00	9.30	13.73	127.74	0.444	No	Yes	0.49
2817	28.17	10.52	3.25	6.95	1.00	9.17	13.83	126.81	0.437	No	Yes	0.48
2818	28.18	10.46	3.25	6.93	1.00	9.10	13.87	126.23	0.434	No	Yes	0.48
2819	28.19	10.53	3.24	6.89	1.00	9.17	13.77	126.27	0.437	No	Yes	0.48
2820	28.20	10.73	3.23	6.83	1.00	9.38	13.54	126.92	0.447	No	Yes	0.49
2821	28.21	11.03	3.22	6.76	1.00	9.68	13.22	127.92	0.462	No	Yes	0.51
2822	28.22	11.36	3.21	6.69	1.00	10.02	12.88	129.00	0.478	No	Yes	0.53
2823	28.23	11.71	3.19	6.61	1.00	10.37	12.55	130.07	0.495	No	Yes	0.55
2824	28.24	12.05	3.18	6.54	1.00	10.72	12.23	131.09	0.511	No	Yes	0.56
2825	28.25	12.37	3.16	6.48	1.00	11.05	11.95	132.00	0.527	No	Yes	0.58
2826	28.26	12.66	3.15	6.42	1.00	11.34	11.71	132.77	0.541	No	Yes	0.60
2827	28.27	12.85	3.15	6.38	1.00	11.52	11.56	133.20	0.550	No	Yes	0.61
2828	28.28	12.94	3.14	6.35	1.00	11.61	11.47	133.27	0.554	No	Yes	0.61
2829	28.29	12.95	3.14	6.32	1.00	11.62	11.45	133.02	0.554	No	Yes	0.61
2830	28.30	12.95	3.14	6.29	1.00	11.62	11.42	132.69	0.554	No	Yes	0.61
2831	28.31	12.95	3.14	6.26	1.00	11.62	11.39	132.33	0.554	No	Yes	0.61
2832	28.32	12.95	3.14	6.23	1.00	11.61	11.36	131.96	0.554	No	Yes	0.61

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
2833	28.33	12.95	3.14	6.19	1.00	11.61	11.34	131.60	0.554	No	Yes	0.61
2834	28.34	12.95	3.13	6.16	1.00	11.60	11.31	131.26	0.554	No	Yes	0.61
2835	28.35	12.94	3.13	6.14	1.00	11.59	11.30	130.93	0.553	No	Yes	0.61
2836	28.36	12.82	3.14	6.14	1.00	11.46	11.37	130.34	0.547	No	Yes	0.60
2837	28.37	12.58	3.15	6.15	1.00	11.21	11.54	129.37	0.535	No	Yes	0.59
2838	28.38	12.21	3.16	6.18	1.00	10.83	11.82	127.96	0.517	No	Yes	0.57
2839	28.39	11.78	3.17	6.22	1.00	10.39	12.15	126.32	0.496	No	Yes	0.55
2840	28.40	11.34	3.19	6.27	1.00	9.93	12.54	124.52	0.474	No	Yes	0.52
2841	28.41	10.88	3.21	6.32	1.00	9.47	12.96	122.64	0.452	No	Yes	0.50
2842	28.42	10.45	3.23	6.37	1.00	9.02	13.39	120.79	0.430	No	Yes	0.47
2843	28.43	10.06	3.25	6.43	1.00	8.62	13.82	119.05	0.411	No	Yes	0.45
2844	28.44	9.76	3.26	6.47	1.00	8.31	14.17	117.71	0.396	No	Yes	0.44
2845	28.45	9.56	3.27	6.51	1.00	8.11	14.42	116.89	0.387	No	Yes	0.43
2846	28.46	9.45	3.28	6.55	1.00	7.99	14.58	116.50	0.381	No	Yes	0.42
2847	28.47	9.36	3.28	6.59	1.00	7.89	14.73	116.25	0.376	No	Yes	0.41
2848	28.48	9.25	3.29	6.63	1.00	7.78	14.90	115.98	0.371	No	Yes	0.41
2849	28.49	9.15	3.30	6.68	1.00	7.67	15.08	115.69	0.366	No	Yes	0.40
2850	28.50	9.04	3.30	6.72	1.00	7.56	15.26	115.39	0.361	No	Yes	0.40
2851	28.51	8.94	3.31	6.77	1.00	7.46	15.43	115.10	0.356	No	Yes	0.39
2852	28.52	8.85	3.31	6.81	1.00	7.37	15.59	114.83	0.351	No	Yes	0.39
2853	28.53	8.80	3.32	6.84	1.00	7.31	15.69	114.65	0.349	No	Yes	0.38
2854	28.54	8.77	3.32	6.85	1.00	7.28	15.74	114.55	0.347	No	Yes	0.38
2855	28.55	8.77	3.32	6.85	1.00	7.27	15.75	114.51	0.347	No	Yes	0.38
2856	28.56	8.77	3.32	6.85	1.00	7.27	15.75	114.48	0.347	No	Yes	0.38
2857	28.57	8.77	3.32	6.84	1.00	7.27	15.75	114.45	0.347	No	Yes	0.38
2858	28.58	8.77	3.32	6.84	1.00	7.26	15.75	114.42	0.347	No	Yes	0.38
2859	28.59	8.77	3.32	6.84	1.00	7.26	15.75	114.38	0.346	No	Yes	0.38
2860	28.60	8.77	3.32	6.84	1.00	7.26	15.75	114.35	0.346	No	Yes	0.38
2861	28.61	8.76	3.32	6.84	1.00	7.25	15.76	114.31	0.346	No	Yes	0.38
2862	28.62	8.74	3.32	6.84	1.00	7.22	15.80	114.13	0.345	No	Yes	0.38
2863	28.63	8.68	3.33	6.85	1.00	7.16	15.89	113.80	0.342	No	Yes	0.38
2864	28.64	8.59	3.33	6.86	1.00	7.07	16.02	113.30	0.337	No	Yes	0.37
2865	28.65	8.49	3.34	6.88	1.00	6.97	16.18	112.73	0.332	No	Yes	0.37
2866	28.66	8.38	3.34	6.89	1.00	6.86	16.35	112.13	0.327	No	Yes	0.36
2867	28.67	8.28	3.35	6.91	1.00	6.75	16.53	111.52	0.322	No	Yes	0.35
2868	28.68	8.18	3.36	6.93	1.00	6.64	16.70	110.92	0.317	No	Yes	0.35
2869	28.69	8.08	3.36	6.95	1.00	6.55	16.86	110.39	0.312	No	Yes	0.34
2870	28.70	8.03	3.36	6.96	1.00	6.49	16.96	110.09	0.310	No	Yes	0.34
2871	28.71	8.04	3.36	6.97	1.00	6.50	16.96	110.20	0.310	No	Yes	0.34
2872	28.72	8.12	3.36	6.97	1.00	6.57	16.85	110.76	0.314	No	Yes	0.35
2873	28.73	8.23	3.35	6.97	1.00	6.69	16.68	111.57	0.319	No	Yes	0.35
2874	28.74	8.36	3.35	6.98	1.00	6.82	16.50	112.47	0.325	No	Yes	0.36
2875	28.75	8.49	3.34	6.98	1.00	6.95	16.32	113.41	0.331	No	Yes	0.36
2876	28.76	8.63	3.34	6.99	1.00	7.08	16.15	114.33	0.338	No	Yes	0.37
2877	28.77	8.75	3.33	6.99	1.00	7.20	15.99	115.19	0.344	No	Yes	0.38
2878	28.78	8.86	3.32	7.00	1.00	7.31	15.86	115.95	0.349	No	Yes	0.38
2879	28.79	8.99	3.32	6.99	1.00	7.44	15.69	116.73	0.355	No	Yes	0.39
2880	28.80	9.16	3.31	6.97	1.00	7.62	15.45	117.70	0.363	No	Yes	0.40

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
2881	28.81	9.41	3.30	6.94	1.00	7.86	15.13	118.95	0.375	No	Yes	0.41
2882	28.82	9.70	3.28	6.89	1.00	8.15	14.77	120.39	0.389	No	Yes	0.43
2883	28.83	10.01	3.27	6.85	1.00	8.47	14.40	121.91	0.404	No	Yes	0.44
2884	28.84	10.33	3.26	6.81	1.00	8.79	14.05	123.44	0.419	No	Yes	0.46
2885	28.85	10.64	3.24	6.78	1.00	9.10	13.72	124.89	0.434	No	Yes	0.48
2886	28.86	10.93	3.23	6.75	1.00	9.39	13.44	126.20	0.448	No	Yes	0.49
2887	28.87	11.18	3.22	6.72	1.00	9.63	13.21	127.27	0.459	No	Yes	0.51
2888	28.88	11.38	3.21	6.69	1.00	9.83	13.02	128.03	0.469	No	Yes	0.52
2889	28.89	11.56	3.20	6.65	1.00	10.02	12.84	128.59	0.478	No	Yes	0.53
2890	28.90	11.76	3.20	6.59	1.00	10.21	12.64	129.06	0.487	No	Yes	0.54
2891	28.91	11.99	3.19	6.53	1.00	10.44	12.42	129.57	0.498	No	Yes	0.55
2892	28.92	12.22	3.18	6.46	1.00	10.67	12.19	130.09	0.509	No	Yes	0.56
2893	28.93	12.46	3.17	6.40	1.00	10.91	11.97	130.58	0.520	No	Yes	0.57
2894	28.94	12.69	3.16	6.34	1.00	11.14	11.76	131.03	0.531	No	Yes	0.58
2895	28.95	12.90	3.15	6.29	1.00	11.34	11.59	131.41	0.541	No	Yes	0.60
2896	28.96	13.09	3.14	6.24	1.00	11.53	11.42	131.77	0.550	No	Yes	0.61
2897	28.97	13.32	3.13	6.19	1.00	11.76	11.25	132.22	0.561	No	Yes	0.62
2898	28.98	13.60	3.12	6.13	1.00	12.04	11.03	132.80	0.574	No	Yes	0.63
2899	28.99	13.95	3.11	6.06	1.00	12.38	10.78	133.50	0.591	No	Yes	0.65
2900	29.00	14.33	3.09	5.99	1.00	12.77	10.51	134.21	0.609	No	Yes	0.67
2901	29.01	14.73	3.08	5.91	1.00	13.17	10.25	134.90	0.628	No	Yes	0.69
2902	29.02	15.13	3.07	5.84	1.00	13.56	10.00	135.54	0.647	No	Yes	0.71
2903	29.03	15.50	3.06	5.78	1.00	13.93	9.77	136.08	0.664	No	Yes	0.73
2904	29.04	15.82	3.05	5.72	1.00	14.25	9.58	136.53	0.680	No	Yes	0.75
2905	29.05	16.12	3.04	5.67	1.00	14.55	9.42	136.97	0.694	No	Yes	0.76
2906	29.06	16.44	3.03	5.63	1.00	14.86	9.25	137.50	0.709	No	Yes	0.78
2907	29.07	16.81	3.02	5.58	1.00	15.23	9.07	138.17	0.727	No	Yes	0.80
2908	29.08	17.25	3.00	5.54	1.00	15.66	8.87	138.93	0.747	No	Yes	0.82
2909	29.09	17.72	2.99	5.48	1.00	16.13	8.66	139.70	0.769	No	Yes	0.85
2910	29.10	18.20	2.98	5.43	1.00	16.61	8.46	140.44	0.792	No	Yes	0.87
2911	29.11	18.67	2.97	5.38	1.00	17.07	8.27	141.12	0.814	No	Yes	0.90
2912	29.12	19.09	2.96	5.34	1.00	17.50	8.10	141.70	0.835	No	Yes	0.92
2913	29.13	19.45	2.95	5.30	1.00	17.85	7.96	142.15	0.852	No	Yes	0.94
2914	29.14	19.72	2.94	5.27	1.00	18.12	7.86	142.44	0.864	No	Yes	0.95
2915	29.15	19.93	2.94	5.25	1.00	18.32	7.78	142.62	0.874	No	Yes	0.96
2916	29.16	20.13	2.93	5.22	1.00	18.52	7.71	142.75	0.883	No	Yes	0.97
2917	29.17	20.36	2.93	5.19	1.00	18.74	7.63	142.88	0.894	No	Yes	0.98
2918	29.18	20.60	2.92	5.16	1.00	18.97	7.54	143.01	0.905	No	Yes	0.99
2919	29.19	20.83	2.92	5.13	1.00	19.20	7.45	143.13	0.916	No	Yes	1.01
2920	29.20	21.06	2.91	5.10	1.00	19.43	7.37	143.23	0.927	No	Yes	1.02
2921	29.21	21.27	2.91	5.08	1.00	19.63	7.30	143.31	0.936	No	Yes	1.03
2922	29.22	21.41	2.90	5.06	1.00	19.76	7.26	143.36	0.943	No	Yes	1.04
2923	29.23	21.46	2.90	5.06	1.00	19.80	7.24	143.39	0.945	No	Yes	1.04
2924	29.24	21.42	2.90	5.06	1.00	19.76	7.26	143.40	0.943	No	Yes	1.04
2925	29.25	21.36	2.91	5.07	1.00	19.69	7.28	143.41	0.939	No	Yes	1.03
2926	29.26	21.28	2.91	5.09	1.00	19.61	7.31	143.41	0.935	No	Yes	1.03
2927	29.27	21.20	2.91	5.10	1.00	19.52	7.35	143.42	0.931	No	Yes	1.02
2928	29.28	21.12	2.91	5.11	1.00	19.43	7.38	143.42	0.927	No	Yes	1.02

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _k (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
2929	29.29	21.05	2.91	5.13	1.00	19.35	7.41	143.42	0.923	No	Yes	1.01
2930	29.30	20.98	2.92	5.14	1.00	19.28	7.44	143.42	0.920	No	Yes	1.01
2931	29.31	20.95	2.92	5.14	1.00	19.25	7.45	143.42	0.918	No	Yes	1.01
2932	29.32	20.97	2.92	5.14	1.00	19.26	7.44	143.42	0.919	No	Yes	1.01
2933	29.33	21.03	2.91	5.13	1.00	19.32	7.42	143.41	0.922	No	Yes	1.01
2934	29.34	21.11	2.91	5.12	1.00	19.39	7.40	143.41	0.925	No	Yes	1.02
2935	29.35	21.18	2.91	5.11	1.00	19.46	7.37	143.41	0.928	No	Yes	1.02
2936	29.36	21.26	2.91	5.10	1.00	19.53	7.34	143.41	0.932	No	Yes	1.02
2937	29.37	21.34	2.91	5.09	1.00	19.60	7.32	143.40	0.935	No	Yes	1.03
2938	29.38	21.41	2.91	5.08	1.00	19.67	7.29	143.39	0.938	No	Yes	1.03
2939	29.39	21.49	2.90	5.06	1.00	19.74	7.26	143.38	0.942	No	Yes	1.03
2940	29.40	21.66	2.90	5.04	1.00	19.90	7.20	143.37	0.949	No	Yes	1.04
2941	29.41	21.94	2.89	5.00	1.00	20.18	7.10	143.34	0.962	No	Yes	1.06
2942	29.42	22.34	2.88	4.94	1.00	20.57	6.97	143.27	0.981	No	Yes	1.08
2943	29.43	22.79	2.87	4.87	0.99	21.00	6.82	143.15	1.002	No	Yes	1.10
2944	29.44	23.27	2.86	4.81	0.99	21.47	6.66	142.98	1.024	No	Yes	1.12
2945	29.45	23.75	2.85	4.74	0.98	21.93	6.51	142.76	1.046	No	Yes	1.15
2946	29.46	24.20	2.84	4.67	0.98	22.37	6.37	142.51	1.067	No	Yes	1.17
2947	29.47	24.61	2.83	4.62	0.98	22.77	6.25	142.25	1.086	No	Yes	1.19
2948	29.48	24.97	2.82	4.57	0.97	23.11	6.15	142.09	1.102	No	Yes	1.21
2949	29.49	25.30	2.82	4.54	0.97	23.43	6.07	142.09	1.117	No	Yes	1.23
2950	29.50	25.66	2.81	4.51	0.97	23.77	5.98	142.27	1.134	No	Yes	1.25
2951	29.51	26.08	2.80	4.49	0.97	24.18	5.89	142.53	1.153	No	Yes	1.27
2952	29.52	26.54	2.80	4.46	0.96	24.63	5.80	142.80	1.175	No	Yes	1.29
2953	29.53	27.02	2.79	4.43	0.96	25.09	5.70	143.05	1.197	No	Yes	1.31
2954	29.54	27.49	2.78	4.41	0.96	25.55	5.61	143.29	1.219	No	Yes	1.34
2955	29.55	27.94	2.77	4.38	0.95	25.98	5.52	143.49	1.239	No	Yes	1.36
2956	29.56	28.32	2.77	4.36	0.95	26.35	5.45	143.65	1.257	No	Yes	1.38
2957	29.57	28.60	2.76	4.35	0.95	26.61	5.41	143.85	1.269	No	Yes	1.39
2958	29.58	28.79	2.76	4.35	0.95	26.79	5.38	144.14	1.278	No	Yes	1.40
2959	29.59	28.92	2.76	4.36	0.95	26.91	5.37	144.57	1.284	No	Yes	1.41
2960	29.60	29.06	2.76	4.37	0.95	27.04	5.36	145.06	1.290	No	Yes	1.42
2961	29.61	29.22	2.76	4.38	0.95	27.19	5.35	145.60	1.297	No	Yes	1.42
2962	29.62	29.38	2.76	4.40	0.95	27.34	5.35	146.14	1.304	No	Yes	1.43
2963	29.63	29.54	2.76	4.41	0.95	27.49	5.34	146.67	1.311	No	Yes	1.44
2964	29.64	29.68	2.76	4.43	0.95	27.62	5.33	147.16	1.317	No	Yes	1.45
2965	29.65	29.78	2.76	4.44	0.95	27.71	5.33	147.58	1.322	No	Yes	1.45
2966	29.66	29.78	2.76	4.46	0.95	27.70	5.34	147.98	1.321	No	Yes	1.45
2967	29.67	29.66	2.76	4.49	0.95	27.58	5.38	148.42	1.316	No	Yes	1.44
2968	29.68	29.46	2.77	4.53	0.95	27.38	5.44	148.94	1.306	No	Yes	1.43
2969	29.69	29.24	2.77	4.57	0.95	27.15	5.51	149.52	1.295	No	Yes	1.42
2970	29.70	29.00	2.78	4.62	0.96	26.91	5.58	150.11	1.284	No	Yes	1.41
2971	29.71	28.76	2.78	4.67	0.96	26.67	5.65	150.69	1.272	No	Yes	1.40
2972	29.72	28.53	2.79	4.72	0.96	26.44	5.72	151.23	1.261	No	Yes	1.38
2973	29.73	28.33	2.79	4.76	0.96	26.23	5.78	151.70	1.251	No	Yes	1.37
2974	29.74	28.12	2.80	4.80	0.96	26.03	5.85	152.18	1.241	No	Yes	1.36
2975	29.75	27.87	2.81	4.86	0.97	25.77	5.93	152.81	1.229	No	Yes	1.35
2976	29.76	27.53	2.82	4.94	0.97	25.43	6.04	153.67	1.213	No	Yes	1.33

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _t (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
2977	29.77	27.10	2.83	5.03	0.97	25.01	6.18	154.68	1.193	No	Yes	1.31
2978	29.78	26.64	2.84	5.14	0.98	24.55	6.34	155.74	1.171	No	Yes	1.29
2979	29.79	26.16	2.85	5.25	0.98	24.08	6.51	156.76	1.149	No	Yes	1.26
2980	29.80	25.69	2.86	5.36	0.99	23.61	6.68	157.71	1.126	No	Yes	1.24
2981	29.81	25.25	2.87	5.46	0.99	23.17	6.84	158.53	1.105	No	Yes	1.21
2982	29.82	24.86	2.88	5.56	1.00	22.79	6.99	159.19	1.087	No	Yes	1.19
2983	29.83	24.69	2.89	5.62	1.00	22.61	7.07	159.85	1.079	No	Yes	1.18
2984	29.84	24.73	2.89	5.66	1.00	22.65	7.09	160.64	1.080	No	Yes	1.19
2985	29.85	24.98	2.89	5.69	1.00	22.88	7.07	161.67	1.091	No	Yes	1.20
2986	29.86	25.27	2.89	5.71	1.00	23.16	7.03	162.86	1.105	No	Yes	1.21
2987	29.87	25.58	2.89	5.75	1.00	23.46	7.00	164.15	1.119	No	Yes	1.23
2988	29.88	25.90	2.88	5.78	1.00	23.77	6.96	165.46	1.134	No	Yes	1.24
2989	29.89	26.21	2.88	5.81	1.00	24.07	6.93	166.72	1.148	No	Yes	1.26
2990	29.90	26.50	2.88	5.84	0.99	24.34	6.90	167.88	1.161	No	Yes	1.27
2991	29.91	26.75	2.88	5.86	0.99	24.58	6.87	168.83	1.173	No	Yes	1.29
2992	29.92	27.05	2.87	5.86	0.99	24.86	6.82	169.50	1.186	No	Yes	1.30
2993	29.93	27.42	2.87	5.83	0.99	25.21	6.74	169.97	1.203	No	Yes	1.32
2994	29.94	27.89	2.86	5.80	0.99	25.66	6.64	170.36	1.224	No	Yes	1.34
2995	29.95	28.41	2.85	5.76	0.98	26.17	6.53	170.77	1.248	No	Yes	1.37
2996	29.96	28.97	2.84	5.71	0.98	26.70	6.41	171.17	1.274	No	Yes	1.40
2997	29.97	29.53	2.83	5.67	0.98	27.24	6.30	171.53	1.299	No	Yes	1.43
2998	29.98	30.06	2.83	5.63	0.98	27.74	6.19	171.85	1.323	No	Yes	1.45
2999	29.99	30.53	2.82	5.59	0.97	28.20	6.10	172.11	1.345	No	Yes	1.48
3000	30.00	30.85	2.82	5.57	0.97	28.49	6.05	172.36	1.359	No	Yes	1.49
3001	30.01	30.96	2.81	5.58	0.97	28.59	6.04	172.67	1.364	No	Yes	1.50
3002	30.02	30.89	2.82	5.61	0.97	28.52	6.07	173.11	1.360	No	Yes	1.49
3003	30.03	30.75	2.82	5.65	0.97	28.37	6.12	173.64	1.353	No	Yes	1.49
3004	30.04	30.60	2.83	5.70	0.97	28.22	6.17	174.21	1.346	No	Yes	1.48
3005	30.05	30.44	2.83	5.75	0.98	28.05	6.23	174.80	1.338	No	Yes	1.47
3006	30.06	30.28	2.83	5.79	0.98	27.89	6.29	175.37	1.330	No	Yes	1.46
3007	30.07	30.13	2.84	5.84	0.98	27.74	6.34	175.89	1.323	No	Yes	1.45
3008	30.08	30.00	2.84	5.88	0.98	27.61	6.39	176.33	1.317	No	Yes	1.45
3009	30.09	29.94	2.84	5.91	0.98	27.54	6.42	176.70	1.314	No	Yes	1.44
3010	30.10	29.94	2.84	5.92	0.98	27.54	6.43	177.04	1.313	No	Yes	1.44
3011	30.11	30.01	2.84	5.94	0.98	27.59	6.43	177.41	1.316	No	Yes	1.44
3012	30.12	30.08	2.84	5.95	0.98	27.65	6.43	177.84	1.319	No	Yes	1.45
3013	30.13	30.16	2.84	5.97	0.98	27.72	6.43	178.29	1.322	No	Yes	1.45
3014	30.14	30.24	2.84	5.98	0.98	27.79	6.43	178.76	1.326	No	Yes	1.45
3015	30.15	30.32	2.84	6.00	0.98	27.86	6.43	179.21	1.329	No	Yes	1.46
3016	30.16	30.39	2.84	6.01	0.98	27.92	6.43	179.63	1.332	No	Yes	1.46
3017	30.17	30.47	2.84	6.02	0.98	27.99	6.43	179.94	1.335	No	Yes	1.47
3018	30.18	30.65	2.84	6.01	0.98	28.15	6.40	180.05	1.343	No	Yes	1.47
3019	30.19	30.94	2.84	5.97	0.98	28.42	6.33	179.98	1.356	No	Yes	1.49
3020	30.20	31.34	2.83	5.92	0.98	28.81	6.24	179.78	1.374	No	Yes	1.51
3021	30.21	31.80	2.82	5.86	0.97	29.24	6.14	179.51	1.395	No	Yes	1.53
3022	30.22	32.27	2.81	5.79	0.97	29.69	6.04	179.21	1.416	No	Yes	1.55
3023	30.23	32.75	2.81	5.73	0.97	30.14	5.93	178.86	1.438	No	Yes	1.58
3024	30.24	33.20	2.80	5.67	0.97	30.57	5.84	178.51	1.458	No	Yes	1.60

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _p (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3025	30.25	33.61	2.79	5.62	0.96	30.95	5.76	178.16	1.476	No	Yes	1.62
3026	30.26	33.93	2.79	5.58	0.96	31.25	5.69	177.94	1.490	No	Yes	1.64
3027	30.27	34.16	2.78	5.56	0.96	31.47	5.65	177.92	1.501	No	Yes	1.65
3028	30.28	34.36	2.78	5.55	0.96	31.65	5.63	178.10	1.510	No	Yes	1.66
3029	30.29	34.57	2.78	5.54	0.96	31.84	5.60	178.36	1.519	No	Yes	1.67
3030	30.30	34.81	2.78	5.54	0.96	32.06	5.57	178.65	1.529	No	Yes	1.68
3031	30.31	35.05	2.77	5.53	0.96	32.28	5.54	178.95	1.540	No	Yes	1.69
3032	30.32	35.28	2.77	5.53	0.95	32.50	5.51	179.24	1.550	No	Yes	1.70
3033	30.33	35.50	2.77	5.52	0.95	32.70	5.49	179.50	1.560	No	Yes	1.71
3034	30.34	35.69	2.77	5.52	0.95	32.88	5.47	179.73	1.568	No	Yes	1.72
3035	30.35	35.78	2.77	5.52	0.95	32.95	5.46	180.02	1.572	No	Yes	1.72
3036	30.36	35.75	2.77	5.55	0.95	32.91	5.48	180.43	1.570	No	Yes	1.72
3037	30.37	35.62	2.77	5.58	0.96	32.78	5.52	181.00	1.564	No	Yes	1.72
3038	30.38	35.48	2.78	5.63	0.96	32.63	5.57	181.65	1.556	No	Yes	1.71
3039	30.39	35.32	2.78	5.67	0.96	32.47	5.62	182.33	1.549	No	Yes	1.70
3040	30.40	35.16	2.78	5.72	0.96	32.31	5.67	183.02	1.541	No	Yes	1.69
3041	30.41	35.00	2.79	5.77	0.96	32.15	5.71	183.68	1.533	No	Yes	1.68
3042	30.42	34.86	2.79	5.81	0.96	32.00	5.76	184.27	1.527	No	Yes	1.68
3043	30.43	34.74	2.80	5.84	0.96	31.87	5.80	184.73	1.520	No	Yes	1.67
3044	30.44	34.60	2.80	5.87	0.96	31.73	5.83	184.99	1.514	No	Yes	1.66
3045	30.45	34.44	2.80	5.89	0.97	31.57	5.86	185.10	1.506	No	Yes	1.65
3046	30.46	34.24	2.80	5.91	0.97	31.36	5.90	185.12	1.496	No	Yes	1.64
3047	30.47	34.01	2.81	5.94	0.97	31.13	5.95	185.13	1.485	No	Yes	1.63
3048	30.48	33.77	2.81	5.96	0.97	30.90	5.99	185.15	1.474	No	Yes	1.62
3049	30.49	33.53	2.81	5.99	0.97	30.66	6.04	185.15	1.462	No	Yes	1.60
3050	30.50	33.31	2.82	6.01	0.97	30.43	6.08	185.15	1.452	No	Yes	1.59
3051	30.51	33.10	2.82	6.03	0.97	30.23	6.13	185.14	1.442	No	Yes	1.58
3052	30.52	33.05	2.82	6.04	0.97	30.17	6.14	185.15	1.439	No	Yes	1.58
3053	30.53	33.24	2.82	6.02	0.97	30.34	6.10	185.19	4.000	Yes	Yes	2.00
3054	30.54	33.67	2.81	5.98	0.97	30.74	6.03	185.26	4.000	Yes	Yes	2.00
3055	30.55	34.23	2.81	5.93	0.97	31.27	5.93	185.32	4.000	Yes	Yes	2.00
3056	30.56	34.85	2.80	5.87	0.96	31.86	5.82	185.34	4.000	Yes	Yes	2.00
3057	30.57	35.49	2.79	5.82	0.96	32.46	5.71	185.33	4.000	Yes	Yes	2.00
3058	30.58	36.12	2.78	5.76	0.96	33.06	5.60	185.28	4.000	Yes	Yes	2.00
3059	30.59	36.71	2.77	5.71	0.96	33.61	5.51	185.20	4.000	Yes	Yes	2.00
3060	30.60	37.22	2.77	5.66	0.95	34.09	5.43	185.10	4.000	Yes	Yes	2.00
3061	30.61	37.88	2.76	5.61	0.95	34.71	5.33	185.05	4.000	Yes	Yes	2.00
3062	30.62	38.81	2.75	5.54	0.95	35.59	5.20	185.03	4.000	Yes	Yes	2.00
3063	30.63	40.09	2.73	5.44	0.94	36.81	5.03	184.98	4.000	Yes	Yes	2.00
3064	30.64	41.56	2.71	5.34	0.93	38.20	4.84	184.77	4.000	Yes	Yes	2.00
3065	30.65	43.14	2.69	5.23	0.93	39.70	9.81	389.55	4.000	Yes	No	2.00
3066	30.66	44.74	2.68	5.11	0.92	41.22	8.76	361.22	4.000	Yes	No	2.00
3067	30.67	46.29	2.66	5.01	0.91	42.68	7.87	335.85	4.000	Yes	No	2.00
3068	30.68	47.69	2.64	4.91	0.91	44.02	7.14	314.26	4.000	Yes	No	2.00
3069	30.69	48.92	2.63	4.83	0.90	45.18	6.57	296.66	4.000	Yes	No	2.00
3070	30.70	50.13	2.62	4.75	0.90	46.32	6.06	280.63	4.000	Yes	No	2.00
3071	30.71	51.48	2.60	4.66	0.89	47.60	5.55	263.98	4.000	Yes	No	2.00
3072	30.72	53.11	2.59	4.57	0.89	49.13	4.99	245.43	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _t (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3073	30.73	54.93	2.57	4.46	0.88	50.86	4.45	226.15	4.000	Yes	No	2.00
3074	30.74	56.84	2.55	4.34	0.87	52.66	3.94	207.38	4.000	Yes	No	2.00
3075	30.75	58.75	2.53	4.23	0.86	54.47	3.49	190.07	4.000	Yes	No	2.00
3076	30.76	60.56	2.52	4.12	0.86	56.18	3.11	174.86	4.000	Yes	No	2.00
3077	30.77	62.17	2.50	4.03	0.85	57.69	2.81	162.21	4.000	Yes	No	2.00
3078	30.78	63.55	2.49	3.95	0.85	59.00	2.89	170.72	4.000	Yes	No	2.00
3079	30.79	64.89	2.48	3.87	0.84	60.25	2.81	169.44	4.000	Yes	No	2.00
3080	30.80	66.35	2.46	3.79	0.84	61.62	2.73	168.00	4.000	Yes	No	2.00
3081	30.81	68.05	2.45	3.70	0.83	63.23	2.63	166.29	4.000	Yes	No	2.00
3082	30.82	69.91	2.43	3.59	0.82	64.98	2.53	164.38	4.000	Yes	No	2.00
3083	30.83	71.83	2.41	3.48	0.82	66.79	2.43	162.36	4.000	Yes	No	2.00
3084	30.84	73.72	2.39	3.38	0.81	68.56	2.34	160.34	4.000	Yes	No	2.00
3085	30.85	75.47	2.38	3.28	0.81	70.21	2.26	158.46	4.000	Yes	No	2.00
3086	30.86	76.98	2.36	3.20	0.80	71.63	2.19	156.82	4.000	Yes	No	2.00
3087	30.87	78.15	2.35	3.14	0.80	72.72	2.14	155.76	4.000	Yes	No	2.00
3088	30.88	79.10	2.34	3.10	0.79	73.61	2.11	155.15	4.000	Yes	No	2.00
3089	30.89	80.00	2.34	3.07	0.79	74.45	2.08	154.86	4.000	Yes	No	2.00
3090	30.90	81.04	2.33	3.04	0.79	75.41	2.05	154.52	4.000	Yes	No	2.00
3091	30.91	82.14	2.32	3.00	0.78	76.44	2.02	154.17	4.000	Yes	No	2.00
3092	30.92	83.26	2.32	2.97	0.78	77.48	1.99	153.82	4.000	Yes	No	2.00
3093	30.93	84.34	2.31	2.93	0.78	78.48	1.96	153.49	4.000	Yes	No	2.00
3094	30.94	85.32	2.30	2.90	0.78	79.40	1.93	153.19	4.000	Yes	No	2.00
3095	30.95	86.09	2.30	2.88	0.77	80.11	1.91	153.04	4.000	Yes	No	2.00
3096	30.96	86.56	2.29	2.87	0.77	80.53	1.90	153.25	0.415	No	No	0.46
3097	30.97	86.80	2.29	2.89	0.77	80.74	1.91	153.83	0.419	No	No	0.46
3098	30.98	86.94	2.30	2.91	0.77	80.85	1.91	154.72	0.424	No	No	0.47
3099	30.99	87.09	2.30	2.94	0.78	80.97	1.92	155.72	0.431	No	No	0.47
3100	31.00	87.25	2.30	2.97	0.78	81.11	1.93	156.77	0.438	No	No	0.48
3101	31.01	87.41	2.30	2.99	0.78	81.24	1.94	157.82	0.446	No	No	0.49
3102	31.02	87.56	2.31	3.02	0.78	81.36	1.95	158.82	0.453	No	No	0.50
3103	31.03	87.69	2.31	3.05	0.78	81.47	1.96	159.70	0.459	No	No	0.50
3104	31.04	87.77	2.31	3.07	0.78	81.52	1.97	160.42	0.464	No	No	0.51
3105	31.05	87.78	2.31	3.08	0.78	81.51	1.98	161.03	0.468	No	No	0.51
3106	31.06	87.74	2.32	3.10	0.78	81.45	1.98	161.64	0.473	No	No	0.52
3107	31.07	87.66	2.32	3.13	0.78	81.36	2.00	162.33	0.478	No	No	0.52
3108	31.08	87.59	2.32	3.15	0.78	81.27	2.01	163.09	0.483	No	No	0.53
3109	31.09	87.51	2.32	3.18	0.79	81.17	2.02	163.88	0.489	No	No	0.54
3110	31.10	87.43	2.33	3.20	0.79	81.08	2.03	164.65	0.495	No	No	0.54
3111	31.11	87.36	2.33	3.23	0.79	80.99	2.04	165.36	0.501	No	No	0.55
3112	31.12	87.30	2.33	3.25	0.79	80.91	2.05	165.98	0.505	No	No	0.55
3113	31.13	87.30	2.33	3.26	0.79	80.89	2.06	166.52	0.509	No	No	0.56
3114	31.14	87.36	2.33	3.28	0.79	80.93	2.06	167.06	0.514	No	No	0.56
3115	31.15	87.49	2.34	3.29	0.79	81.03	2.07	167.66	0.518	No	No	0.57
3116	31.16	87.64	2.34	3.31	0.79	81.15	2.07	168.36	0.524	No	No	0.57
3117	31.17	87.80	2.34	3.33	0.79	81.28	2.08	169.11	0.530	No	No	0.58
3118	31.18	87.96	2.34	3.35	0.79	81.41	2.09	169.86	0.536	No	No	0.59
3119	31.19	88.11	2.34	3.37	0.79	81.54	2.09	170.59	0.542	No	No	0.59
3120	31.20	88.25	2.34	3.38	0.79	81.65	2.10	171.26	0.547	No	No	0.60

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
3121	31.21	88.39	2.34	3.40	0.79	81.76	2.10	171.80	0.552	No	No	0.61
3122	31.22	88.58	2.34	3.40	0.79	81.91	2.10	172.24	0.555	No	No	0.61
3123	31.23	88.84	2.34	3.41	0.79	82.14	2.10	172.64	0.558	No	No	0.61
3124	31.24	89.19	2.34	3.42	0.79	82.44	2.10	173.07	0.562	No	No	0.62
3125	31.25	89.57	2.34	3.42	0.79	82.78	2.10	173.55	0.566	No	No	0.62
3126	31.26	89.96	2.34	3.43	0.79	83.14	2.09	174.06	0.570	No	No	0.63
3127	31.27	90.36	2.34	3.43	0.79	83.49	2.09	174.56	0.575	No	No	0.63
3128	31.28	90.74	2.34	3.44	0.79	83.82	2.09	175.04	0.579	No	No	0.64
3129	31.29	91.07	2.34	3.44	0.79	84.11	2.09	175.46	0.582	No	No	0.64
3130	31.30	91.38	2.34	3.45	0.79	84.39	2.08	175.75	0.585	No	No	0.64
3131	31.31	91.73	2.34	3.44	0.79	84.69	2.08	175.92	0.586	No	No	0.64
3132	31.32	92.15	2.34	3.44	0.79	85.07	2.07	176.00	0.587	No	No	0.64
3133	31.33	92.65	2.33	3.43	0.79	85.51	2.06	176.08	0.588	No	No	0.65
3134	31.34	93.19	2.33	3.42	0.79	86.00	2.05	176.16	0.588	No	No	0.65
3135	31.35	93.75	2.33	3.41	0.79	86.51	2.04	176.24	0.589	No	No	0.65
3136	31.36	94.30	2.33	3.40	0.79	87.00	2.03	176.32	0.590	No	No	0.65
3137	31.37	94.81	2.32	3.39	0.79	87.46	2.02	176.40	0.590	No	No	0.65
3138	31.38	95.26	2.32	3.38	0.78	87.86	2.01	176.46	0.591	No	No	0.65
3139	31.39	95.77	2.32	3.37	0.78	88.32	2.00	176.52	0.592	No	No	0.65
3140	31.40	96.41	2.32	3.36	0.78	88.90	1.99	176.60	0.592	No	No	0.65
3141	31.41	97.25	2.31	3.34	0.78	89.67	1.97	176.70	0.593	No	No	0.65
3142	31.42	98.22	2.31	3.33	0.78	90.55	1.95	176.82	0.594	No	No	0.65
3143	31.43	99.24	2.30	3.31	0.78	91.49	1.93	176.95	0.595	No	No	0.65
3144	31.44	100.28	2.30	3.29	0.78	92.45	1.92	177.09	0.596	No	No	0.65
3145	31.45	101.28	2.29	3.27	0.77	93.36	1.90	177.22	0.598	No	No	0.66
3146	31.46	102.19	2.29	3.25	0.77	94.19	1.88	177.34	0.599	No	No	0.66
3147	31.47	102.98	2.28	3.24	0.77	94.91	1.87	177.45	0.600	No	No	0.66
3148	31.48	103.75	2.28	3.22	0.77	95.61	1.86	177.55	0.601	No	No	0.66
3149	31.49	104.61	2.28	3.21	0.77	96.40	1.84	177.66	0.602	No	No	0.66
3150	31.50	105.64	2.27	3.19	0.77	97.34	1.83	177.81	0.603	No	No	0.66
3151	31.51	106.78	2.27	3.16	0.76	98.39	1.81	177.97	0.604	No	No	0.66
3152	31.52	107.98	2.26	3.14	0.76	99.49	1.79	178.16	0.606	No	No	0.67
3153	31.53	109.17	2.26	3.12	0.76	100.58	1.77	178.35	0.608	No	No	0.67
3154	31.54	110.29	2.25	3.10	0.76	101.61	1.76	178.53	0.609	No	No	0.67
3155	31.55	111.29	2.25	3.08	0.76	102.52	1.74	178.70	0.611	No	No	0.67
3156	31.56	112.15	2.24	3.06	0.76	103.30	1.73	178.83	0.612	No	No	0.67
3157	31.57	112.98	2.24	3.04	0.75	104.06	1.72	178.92	0.613	No	No	0.67
3158	31.58	113.91	2.23	3.02	0.75	104.90	1.71	179.01	0.613	No	No	0.67
3159	31.59	114.98	2.23	3.00	0.75	105.88	1.69	179.12	0.614	No	No	0.67
3160	31.60	116.15	2.22	2.98	0.75	106.95	1.68	179.25	0.616	No	No	0.68
3161	31.61	117.35	2.22	2.95	0.75	108.05	1.66	179.39	0.617	No	No	0.68
3162	31.62	118.52	2.21	2.93	0.74	109.12	1.65	179.54	0.618	No	No	0.68
3163	31.63	119.61	2.21	2.90	0.74	110.12	1.63	179.69	0.620	No	No	0.68
3164	31.64	120.55	2.20	2.88	0.74	110.97	1.62	179.81	0.621	No	No	0.68
3165	31.65	121.35	2.20	2.86	0.74	111.69	1.61	179.88	0.621	No	No	0.68
3166	31.66	122.11	2.19	2.84	0.74	112.38	1.60	179.88	0.621	No	No	0.68
3167	31.67	122.96	2.19	2.82	0.74	113.15	1.59	179.84	0.621	No	No	0.68
3168	31.68	123.93	2.18	2.79	0.73	114.03	1.58	179.82	0.621	No	No	0.68

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3169	31.69	124.95	2.18	2.76	0.73	114.96	1.56	179.80	0.621	No	No	0.68
3170	31.70	125.99	2.17	2.74	0.73	115.91	1.55	179.80	0.621	No	No	0.68
3171	31.71	126.99	2.17	2.71	0.73	116.82	1.54	179.81	0.621	No	No	0.68
3172	31.72	127.89	2.16	2.68	0.72	117.64	1.53	179.83	0.621	No	No	0.68
3173	31.73	128.63	2.16	2.66	0.72	118.30	1.52	179.86	0.621	No	No	0.68
3174	31.74	129.22	2.16	2.65	0.72	118.82	1.51	179.89	0.621	No	No	0.68
3175	31.75	129.73	2.15	2.63	0.72	119.28	1.51	179.94	0.622	No	No	0.68
3176	31.76	130.28	2.15	2.62	0.72	119.76	1.50	180.00	0.622	No	No	0.68
3177	31.77	130.89	2.15	2.60	0.72	120.31	1.50	180.07	0.623	No	No	0.68
3178	31.78	131.53	2.14	2.59	0.72	120.88	1.49	180.16	0.624	No	No	0.69
3179	31.79	132.16	2.14	2.57	0.72	121.44	1.48	180.25	0.625	No	No	0.69
3180	31.80	132.76	2.14	2.56	0.72	121.97	1.48	180.34	0.625	No	No	0.69
3181	31.81	133.29	2.13	2.54	0.71	122.44	1.47	180.42	0.626	No	No	0.69
3182	31.82	133.71	2.13	2.54	0.71	122.80	1.47	180.51	0.627	No	No	0.69
3183	31.83	134.05	2.13	2.53	0.71	123.10	1.47	180.63	0.628	No	No	0.69
3184	31.84	134.37	2.13	2.53	0.71	123.36	1.47	180.81	0.630	No	No	0.69
3185	31.85	134.73	2.13	2.52	0.71	123.67	1.46	181.03	0.632	No	No	0.69
3186	31.86	135.12	2.13	2.52	0.71	124.01	1.46	181.27	0.634	No	No	0.70
3187	31.87	135.52	2.13	2.52	0.71	124.35	1.46	181.52	0.636	No	No	0.70
3188	31.88	135.91	2.12	2.51	0.71	124.69	1.46	181.76	0.638	No	No	0.70
3189	31.89	136.27	2.12	2.51	0.71	125.00	1.46	181.98	0.640	No	No	0.70
3190	31.90	136.57	2.12	2.51	0.71	125.25	1.45	182.16	0.642	No	No	0.71
3191	31.91	136.75	2.12	2.51	0.71	125.39	1.45	182.28	0.643	No	No	0.71
3192	31.92	136.82	2.12	2.51	0.71	125.43	1.45	182.35	0.644	No	No	0.71
3193	31.93	136.82	2.12	2.51	0.71	125.40	1.45	182.39	0.644	No	No	0.71
3194	31.94	136.82	2.12	2.51	0.71	125.37	1.46	182.45	0.645	No	No	0.71
3195	31.95	136.82	2.12	2.52	0.71	125.34	1.46	182.50	0.645	No	No	0.71
3196	31.96	136.82	2.12	2.52	0.71	125.31	1.46	182.56	0.646	No	No	0.71
3197	31.97	136.82	2.12	2.52	0.71	125.28	1.46	182.62	0.646	No	No	0.71
3198	31.98	136.82	2.13	2.53	0.71	125.25	1.46	182.67	0.647	No	No	0.71
3199	31.99	136.81	2.13	2.53	0.71	125.21	1.46	182.71	0.647	No	No	0.71
3200	32.00	136.75	2.13	2.53	0.71	125.13	1.46	182.75	0.648	No	No	0.71
3201	32.01	136.65	2.13	2.54	0.71	125.00	1.46	182.81	0.648	No	No	0.71
3202	32.02	136.52	2.13	2.55	0.71	124.84	1.46	182.88	0.649	No	No	0.71
3203	32.03	136.36	2.13	2.56	0.71	124.67	1.47	182.97	0.650	No	No	0.71
3204	32.04	136.20	2.13	2.57	0.71	124.49	1.47	183.07	0.651	No	No	0.72
3205	32.05	136.05	2.13	2.58	0.71	124.31	1.47	183.16	0.651	No	No	0.72
3206	32.06	135.90	2.14	2.59	0.71	124.15	1.48	183.25	0.652	No	No	0.72
3207	32.07	135.76	2.14	2.59	0.72	123.99	1.48	183.33	0.653	No	No	0.72
3208	32.08	135.65	2.14	2.60	0.72	123.86	1.48	183.39	0.654	No	No	0.72
3209	32.09	135.54	2.14	2.61	0.72	123.72	1.48	183.45	0.654	No	No	0.72
3210	32.10	135.42	2.14	2.61	0.72	123.58	1.49	183.53	0.655	No	No	0.72
3211	32.11	135.27	2.14	2.62	0.72	123.41	1.49	183.62	0.656	No	No	0.72
3212	32.12	135.12	2.14	2.63	0.72	123.24	1.49	183.72	0.657	No	No	0.72
3213	32.13	134.96	2.14	2.64	0.72	123.06	1.49	183.82	0.658	No	No	0.72
3214	32.14	134.80	2.15	2.65	0.72	122.89	1.50	183.93	0.659	No	No	0.72
3215	32.15	134.66	2.15	2.66	0.72	122.72	1.50	184.02	0.660	No	No	0.73
3216	32.16	134.53	2.15	2.67	0.72	122.58	1.50	184.10	0.660	No	No	0.73

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3217	32.17	134.42	2.15	2.67	0.72	122.44	1.50	184.17	0.661	No	No	0.73
3218	32.18	134.31	2.15	2.68	0.72	122.31	1.51	184.24	0.662	No	No	0.73
3219	32.19	134.17	2.15	2.69	0.72	122.16	1.51	184.33	0.662	No	No	0.73
3220	32.20	134.03	2.15	2.70	0.72	121.99	1.51	184.43	0.663	No	No	0.73
3221	32.21	133.87	2.16	2.71	0.72	121.81	1.52	184.54	0.665	No	No	0.73
3222	32.22	133.71	2.16	2.72	0.72	121.63	1.52	184.66	0.666	No	No	0.73
3223	32.23	133.55	2.16	2.73	0.72	121.46	1.52	184.77	0.667	No	No	0.73
3224	32.24	133.42	2.16	2.73	0.72	121.30	1.52	184.87	0.668	No	No	0.73
3225	32.25	133.31	2.16	2.74	0.73	121.17	1.53	184.95	0.668	No	No	0.74
3226	32.26	133.22	2.16	2.75	0.73	121.06	1.53	185.01	0.669	No	No	0.74
3227	32.27	133.16	2.16	2.75	0.73	120.97	1.53	185.08	0.670	No	No	0.74
3228	32.28	133.09	2.16	2.76	0.73	120.88	1.53	185.16	0.670	No	No	0.74
3229	32.29	133.01	2.16	2.76	0.73	120.78	1.53	185.25	0.671	No	No	0.74
3230	32.30	132.93	2.17	2.77	0.73	120.68	1.54	185.34	0.672	No	No	0.74
3231	32.31	132.85	2.17	2.78	0.73	120.57	1.54	185.44	0.673	No	No	0.74
3232	32.32	132.78	2.17	2.78	0.73	120.47	1.54	185.53	0.674	No	No	0.74
3233	32.33	132.71	2.17	2.79	0.73	120.38	1.54	185.60	0.675	No	No	0.74
3234	32.34	132.67	2.17	2.79	0.73	120.32	1.54	185.68	0.675	No	No	0.74
3235	32.35	132.65	2.17	2.80	0.73	120.27	1.54	185.77	0.676	No	No	0.74
3236	32.36	132.65	2.17	2.80	0.73	120.24	1.55	185.89	0.677	No	No	0.75
3237	32.37	132.65	2.17	2.81	0.73	120.21	1.55	186.04	0.679	No	No	0.75
3238	32.38	132.65	2.17	2.81	0.73	120.18	1.55	186.20	0.680	No	No	0.75
3239	32.39	132.65	2.17	2.82	0.73	120.15	1.55	186.37	0.682	No	No	0.75
3240	32.40	132.65	2.17	2.83	0.73	120.12	1.55	186.54	0.684	No	No	0.75
3241	32.41	132.65	2.17	2.83	0.73	120.09	1.55	186.69	0.685	No	No	0.75
3242	32.42	132.65	2.18	2.84	0.73	120.06	1.56	186.81	0.686	No	No	0.76
3243	32.43	132.65	2.18	2.84	0.73	120.03	1.56	186.92	0.687	No	No	0.76
3244	32.44	132.65	2.18	2.84	0.73	120.00	1.56	187.04	0.689	No	No	0.76
3245	32.45	132.65	2.18	2.85	0.73	119.97	1.56	187.17	0.690	No	No	0.76
3246	32.46	132.65	2.18	2.86	0.73	119.94	1.56	187.33	0.691	No	No	0.76
3247	32.47	132.65	2.18	2.86	0.73	119.91	1.56	187.50	0.693	No	No	0.76
3248	32.48	132.65	2.18	2.87	0.73	119.88	1.57	187.67	0.695	No	No	0.76
3249	32.49	132.65	2.18	2.87	0.73	119.85	1.57	187.83	0.696	No	No	0.77
3250	32.50	132.65	2.18	2.88	0.73	119.82	1.57	187.98	0.698	No	No	0.77
3251	32.51	132.66	2.18	2.88	0.73	119.80	1.57	188.11	0.699	No	No	0.77
3252	32.52	132.69	2.18	2.89	0.73	119.80	1.57	188.24	0.700	No	No	0.77
3253	32.53	132.74	2.18	2.89	0.73	119.81	1.57	188.41	0.702	No	No	0.77
3254	32.54	132.81	2.18	2.90	0.73	119.85	1.57	188.61	0.704	No	No	0.78
3255	32.55	132.88	2.18	2.91	0.73	119.89	1.58	188.84	0.706	No	No	0.78
3256	32.56	132.96	2.18	2.91	0.73	119.93	1.58	189.09	0.709	No	No	0.78
3257	32.57	133.04	2.18	2.92	0.73	119.98	1.58	189.32	0.711	No	No	0.78
3258	32.58	133.12	2.19	2.92	0.74	120.01	1.58	189.55	0.713	No	No	0.79
3259	32.59	133.18	2.19	2.93	0.74	120.04	1.58	189.74	0.715	No	No	0.79
3260	32.60	133.47	2.19	2.93	0.74	120.28	1.58	190.10	0.719	No	No	0.79
3261	32.61	134.08	2.19	2.94	0.73	120.81	1.58	190.74	0.725	No	No	0.80
3262	32.62	135.08	2.18	2.94	0.73	121.70	1.58	191.72	0.735	No	No	0.81
3263	32.63	136.27	2.18	2.95	0.73	122.76	1.57	192.90	0.748	No	No	0.82
3264	32.64	137.56	2.18	2.95	0.73	123.91	1.57	194.17	0.761	No	No	0.84

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3265	32.65	138.88	2.18	2.96	0.73	125.10	1.56	195.49	0.775	No	No	0.85
3266	32.66	140.17	2.18	2.97	0.73	126.25	1.56	196.76	0.788	No	No	0.87
3267	32.67	141.35	2.17	2.97	0.73	127.30	1.55	197.94	0.801	No	No	0.88
3268	32.68	142.37	2.17	2.98	0.73	128.20	1.55	198.95	0.812	No	No	0.89
3269	32.69	143.26	2.17	2.98	0.73	128.98	1.55	199.83	0.822	No	No	0.91
3270	32.70	144.15	2.17	2.98	0.73	129.77	1.55	200.72	4.000	No	No	2.00
3271	32.71	145.15	2.17	2.99	0.73	130.66	1.54	201.73	4.000	No	No	2.00
3272	32.72	146.29	2.17	2.99	0.73	131.67	1.54	202.89	4.000	No	No	2.00
3273	32.73	147.50	2.17	3.00	0.73	132.74	1.54	204.11	4.000	No	No	2.00
3274	32.74	148.71	2.17	3.01	0.73	133.82	1.53	205.35	4.000	No	No	2.00
3275	32.75	149.87	2.16	3.01	0.73	134.84	1.53	206.53	4.000	No	No	2.00
3276	32.76	150.92	2.16	3.02	0.73	135.77	1.53	207.59	4.000	No	No	2.00
3277	32.77	151.69	2.16	3.02	0.73	136.45	1.53	208.40	4.000	No	No	2.00
3278	32.78	152.16	2.16	3.03	0.73	136.84	1.53	208.96	4.000	No	No	2.00
3279	32.79	152.39	2.16	3.03	0.73	137.01	1.53	209.34	4.000	No	No	2.00
3280	32.80	152.54	2.16	3.04	0.73	137.11	1.53	209.70	4.000	No	No	2.00
3281	32.81	152.70	2.16	3.05	0.73	137.23	1.53	210.11	4.000	No	No	2.00
3282	32.82	152.88	2.16	3.06	0.73	137.35	1.53	210.53	4.000	No	No	2.00
3283	32.83	153.05	2.17	3.07	0.73	137.47	1.53	210.95	4.000	No	No	2.00
3284	32.84	153.21	2.17	3.08	0.73	137.58	1.54	211.34	4.000	No	No	2.00
3285	32.85	153.35	2.17	3.09	0.73	137.68	1.54	211.68	4.000	No	No	2.00
3286	32.86	153.53	2.17	3.09	0.73	137.81	1.54	211.98	4.000	No	No	2.00
3287	32.87	153.78	2.17	3.10	0.73	138.00	1.54	212.29	4.000	No	No	2.00
3288	32.88	154.14	2.17	3.10	0.73	138.30	1.54	212.66	4.000	No	No	2.00
3289	32.89	154.56	2.17	3.10	0.73	138.65	1.54	213.09	4.000	No	No	2.00
3290	32.90	155.01	2.17	3.10	0.73	139.03	1.54	213.56	4.000	No	No	2.00
3291	32.91	155.48	2.17	3.11	0.73	139.42	1.54	214.04	4.000	No	No	2.00
3292	32.92	155.93	2.17	3.11	0.73	139.79	1.53	214.50	4.000	No	No	2.00
3293	32.93	156.35	2.16	3.11	0.73	140.14	1.53	214.93	4.000	No	No	2.00
3294	32.94	156.71	2.16	3.12	0.73	140.44	1.53	215.28	4.000	No	No	2.00
3295	32.95	157.07	2.16	3.11	0.73	140.74	1.53	215.56	4.000	No	No	2.00
3296	32.96	157.49	2.16	3.11	0.73	141.09	1.53	215.80	4.000	No	No	2.00
3297	32.97	158.01	2.16	3.11	0.73	141.52	1.53	216.06	4.000	No	No	2.00
3298	32.98	158.59	2.16	3.10	0.73	142.02	1.52	216.35	4.000	No	No	2.00
3299	32.99	159.20	2.16	3.09	0.73	142.55	1.52	216.66	4.000	No	No	2.00
3300	33.00	159.82	2.16	3.09	0.72	143.08	1.52	216.98	4.000	No	No	2.00
3301	33.01	160.41	2.15	3.08	0.72	143.58	1.51	217.28	4.000	No	No	2.00
3302	33.02	160.94	2.15	3.08	0.72	144.03	1.51	217.55	4.000	No	No	2.00
3303	33.03	161.39	2.15	3.07	0.72	144.41	1.51	217.75	4.000	No	No	2.00
3304	33.04	161.83	2.15	3.06	0.72	144.78	1.51	217.90	4.000	No	No	2.00
3305	33.05	162.30	2.15	3.05	0.72	145.18	1.50	218.02	4.000	No	No	2.00
3306	33.06	162.86	2.15	3.04	0.72	145.66	1.50	218.14	4.000	No	No	2.00
3307	33.07	163.48	2.14	3.03	0.72	146.19	1.49	218.28	4.000	No	No	2.00
3308	33.08	164.12	2.14	3.02	0.72	146.74	1.49	218.43	4.000	No	No	2.00
3309	33.09	164.75	2.14	3.01	0.72	147.29	1.48	218.59	4.000	No	No	2.00
3310	33.10	165.34	2.14	2.99	0.72	147.80	1.48	218.73	4.000	No	No	2.00
3311	33.11	165.86	2.14	2.98	0.72	148.24	1.48	218.85	4.000	No	No	2.00
3312	33.12	166.34	2.13	2.97	0.72	148.64	1.47	218.98	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
3313	33.13	166.84	2.13	2.97	0.72	149.07	1.47	219.14	4.000	No	No	2.00
3314	33.14	167.45	2.13	2.96	0.71	149.59	1.47	219.35	4.000	No	No	2.00
3315	33.15	168.14	2.13	2.94	0.71	150.19	1.46	219.61	4.000	No	No	2.00
3316	33.16	168.89	2.12	2.93	0.71	150.85	1.46	219.89	4.000	No	No	2.00
3317	33.17	169.66	2.12	2.92	0.71	151.51	1.45	220.19	4.000	No	No	2.00
3318	33.18	170.41	2.12	2.91	0.71	152.16	1.45	220.48	4.000	No	No	2.00
3319	33.19	171.09	2.12	2.89	0.71	152.75	1.45	220.74	4.000	No	No	2.00
3320	33.20	171.68	2.11	2.88	0.71	153.25	1.44	220.96	4.000	No	No	2.00
3321	33.21	172.17	2.11	2.88	0.71	153.67	1.44	221.13	4.000	No	No	2.00
3322	33.22	172.65	2.11	2.87	0.71	154.08	1.44	221.27	4.000	No	No	2.00
3323	33.23	173.19	2.11	2.86	0.71	154.53	1.43	221.43	4.000	No	No	2.00
3324	33.24	173.79	2.11	2.84	0.71	155.05	1.43	221.61	4.000	No	No	2.00
3325	33.25	174.42	2.10	2.83	0.71	155.59	1.43	221.81	4.000	No	No	2.00
3326	33.26	175.06	2.10	2.82	0.70	156.14	1.42	222.01	4.000	No	No	2.00
3327	33.27	175.67	2.10	2.81	0.70	156.66	1.42	222.20	4.000	No	No	2.00
3328	33.28	176.21	2.10	2.80	0.70	157.13	1.42	222.38	4.000	No	No	2.00
3329	33.29	176.62	2.10	2.79	0.70	157.46	1.41	222.47	4.000	No	No	2.00
3330	33.30	176.85	2.09	2.78	0.70	157.64	1.41	222.44	4.000	No	No	2.00
3331	33.31	176.95	2.09	2.77	0.70	157.70	1.41	222.30	4.000	No	No	2.00
3332	33.32	177.02	2.09	2.76	0.70	157.73	1.41	222.10	4.000	No	No	2.00
3333	33.33	177.10	2.09	2.75	0.70	157.77	1.41	221.89	4.000	No	No	2.00
3334	33.34	177.18	2.09	2.75	0.70	157.81	1.40	221.67	4.000	No	No	2.00
3335	33.35	177.26	2.09	2.74	0.70	157.85	1.40	221.46	4.000	No	No	2.00
3336	33.36	177.33	2.09	2.73	0.70	157.89	1.40	221.25	4.000	No	No	2.00
3337	33.37	177.40	2.09	2.72	0.70	157.92	1.40	221.07	4.000	No	No	2.00
3338	33.38	177.36	2.09	2.71	0.70	157.85	1.40	220.85	4.000	No	No	2.00
3339	33.39	177.19	2.09	2.71	0.70	157.66	1.40	220.56	4.000	No	No	2.00
3340	33.40	176.88	2.09	2.71	0.70	157.34	1.40	220.16	4.000	No	No	2.00
3341	33.41	176.52	2.09	2.71	0.70	156.98	1.40	219.71	4.000	No	No	2.00
3342	33.42	176.12	2.09	2.70	0.70	156.59	1.40	219.22	4.000	No	No	2.00
3343	33.43	175.72	2.09	2.70	0.70	156.19	1.40	218.73	4.000	No	No	2.00
3344	33.44	175.33	2.09	2.70	0.70	155.81	1.40	218.25	4.000	No	No	2.00
3345	33.45	174.98	2.09	2.69	0.70	155.45	1.40	217.80	4.000	No	No	2.00
3346	33.46	174.65	2.09	2.69	0.70	155.12	1.40	217.40	4.000	No	No	2.00
3347	33.47	174.26	2.09	2.69	0.70	154.73	1.40	216.97	4.000	No	No	2.00
3348	33.48	173.74	2.09	2.69	0.70	154.23	1.40	216.44	4.000	No	No	2.00
3349	33.49	173.07	2.09	2.69	0.70	153.59	1.40	215.78	4.000	No	No	2.00
3350	33.50	172.32	2.09	2.69	0.70	152.88	1.41	215.04	4.000	No	No	2.00
3351	33.51	171.53	2.09	2.69	0.70	152.12	1.41	214.27	4.000	No	No	2.00
3352	33.52	170.73	2.09	2.69	0.70	151.37	1.41	213.50	4.000	No	No	2.00
3353	33.53	169.97	2.10	2.69	0.70	150.65	1.41	212.76	4.000	No	No	2.00
3354	33.54	169.29	2.10	2.69	0.70	150.00	1.41	212.10	4.000	No	No	2.00
3355	33.55	168.67	2.10	2.69	0.70	149.40	1.42	211.52	4.000	No	No	2.00
3356	33.56	167.99	2.10	2.70	0.70	148.76	1.42	210.96	4.000	No	No	2.00
3357	33.57	167.18	2.10	2.70	0.70	147.98	1.42	210.35	4.000	No	No	2.00
3358	33.58	166.19	2.10	2.71	0.71	147.06	1.43	209.65	4.000	No	No	2.00
3359	33.59	165.11	2.11	2.72	0.71	146.05	1.43	208.88	4.000	No	No	2.00
3360	33.60	163.99	2.11	2.73	0.71	145.00	1.44	208.09	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
3361	33.61	162.89	2.11	2.74	0.71	143.96	1.44	207.31	4.000	No	No	2.00
3362	33.62	161.86	2.12	2.75	0.71	143.00	1.44	206.59	4.000	No	No	2.00
3363	33.63	160.96	2.12	2.76	0.71	142.15	1.45	205.96	4.000	No	No	2.00
3364	33.64	160.15	2.12	2.76	0.71	141.38	1.45	205.43	4.000	No	No	2.00
3365	33.65	159.32	2.12	2.77	0.71	140.60	1.46	204.94	4.000	No	No	2.00
3366	33.66	158.37	2.13	2.79	0.71	139.71	1.46	204.42	4.000	No	No	2.00
3367	33.67	157.28	2.13	2.80	0.72	138.68	1.47	203.83	4.000	No	No	2.00
3368	33.68	156.10	2.14	2.82	0.72	137.58	1.48	203.20	4.000	No	No	2.00
3369	33.69	154.90	2.14	2.83	0.72	136.46	1.48	202.58	4.000	No	No	2.00
3370	33.70	153.74	2.14	2.85	0.72	135.38	1.49	201.98	4.000	No	No	2.00
3371	33.71	152.67	2.15	2.86	0.72	134.38	1.50	201.44	4.000	No	No	2.00
3372	33.72	151.76	2.15	2.88	0.72	133.53	1.51	200.97	4.000	No	No	2.00
3373	33.73	150.96	2.15	2.89	0.72	132.77	1.51	200.54	4.000	No	No	2.00
3374	33.74	150.13	2.16	2.90	0.73	131.99	1.52	200.10	4.000	No	No	2.00
3375	33.75	149.19	2.16	2.91	0.73	131.11	1.52	199.58	0.819	No	No	0.91
3376	33.76	148.14	2.16	2.92	0.73	130.13	1.53	199.01	0.813	No	No	0.90
3377	33.77	147.03	2.17	2.93	0.73	129.09	1.54	198.41	0.806	No	No	0.89
3378	33.78	145.91	2.17	2.94	0.73	128.06	1.54	197.83	0.800	No	No	0.88
3379	33.79	144.85	2.17	2.96	0.73	127.07	1.55	197.27	0.794	No	No	0.88
3380	33.80	143.90	2.18	2.97	0.73	126.18	1.56	196.78	0.789	No	No	0.87
3381	33.81	143.10	2.18	2.98	0.73	125.43	1.57	196.36	0.784	No	No	0.87
3382	33.82	142.35	2.18	2.99	0.74	124.73	1.57	195.98	0.780	No	No	0.86
3383	33.83	141.56	2.18	3.00	0.74	123.99	1.58	195.60	0.776	No	No	0.86
3384	33.84	140.65	2.19	3.01	0.74	123.13	1.58	195.16	0.771	No	No	0.85
3385	33.85	139.64	2.19	3.02	0.74	122.20	1.59	194.69	0.766	No	No	0.85
3386	33.86	138.60	2.20	3.03	0.74	121.23	1.60	194.21	0.761	No	No	0.84
3387	33.87	137.58	2.20	3.05	0.74	120.28	1.61	193.74	0.756	No	No	0.84
3388	33.88	136.62	2.20	3.06	0.74	119.40	1.62	193.30	0.752	No	No	0.83
3389	33.89	135.79	2.20	3.07	0.74	118.62	1.63	192.93	0.748	No	No	0.83
3390	33.90	135.25	2.21	3.08	0.75	118.11	1.63	192.73	0.746	No	No	0.83
3391	33.91	134.97	2.21	3.08	0.75	117.82	1.64	192.72	0.746	No	No	0.82
3392	33.92	134.88	2.21	3.09	0.75	117.71	1.64	192.87	0.747	No	No	0.83
3393	33.93	134.79	2.21	3.10	0.75	117.60	1.64	193.05	0.749	No	No	0.83
3394	33.94	134.68	2.21	3.11	0.75	117.47	1.65	193.25	0.751	No	No	0.83
3395	33.95	134.58	2.21	3.12	0.75	117.34	1.65	193.45	0.753	No	No	0.83
3396	33.96	134.47	2.21	3.13	0.75	117.22	1.65	193.65	0.755	No	No	0.84
3397	33.97	134.38	2.22	3.14	0.75	117.10	1.66	193.83	0.757	No	No	0.84
3398	33.98	134.30	2.22	3.14	0.75	117.00	1.66	193.98	0.759	No	No	0.84
3399	33.99	134.23	2.22	3.15	0.75	116.91	1.66	194.12	0.760	No	No	0.84
3400	34.00	134.17	2.22	3.16	0.75	116.83	1.66	194.27	0.762	No	No	0.84
3401	34.01	134.10	2.22	3.17	0.75	116.74	1.67	194.46	0.764	No	No	0.85
3402	34.02	134.03	2.22	3.17	0.75	116.64	1.67	194.67	0.766	No	No	0.85
3403	34.03	133.95	2.22	3.18	0.75	116.54	1.67	194.90	0.769	No	No	0.85
3404	34.04	133.87	2.22	3.19	0.75	116.43	1.68	195.13	0.771	No	No	0.85
3405	34.05	133.79	2.22	3.20	0.75	116.33	1.68	195.34	0.773	No	No	0.86
3406	34.06	133.73	2.23	3.21	0.75	116.24	1.68	195.54	0.775	No	No	0.86
3407	34.07	133.62	2.23	3.22	0.75	116.12	1.68	195.64	0.776	No	No	0.86
3408	34.08	133.42	2.23	3.22	0.75	115.91	1.69	195.64	0.776	No	No	0.86

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3409	34.09	133.10	2.23	3.23	0.75	115.59	1.69	195.52	0.775	No	No	0.86
3410	34.10	132.70	2.23	3.23	0.75	115.21	1.70	195.37	0.773	No	No	0.86
3411	34.11	132.26	2.23	3.24	0.76	114.79	1.70	195.20	0.772	No	No	0.85
3412	34.12	131.81	2.23	3.25	0.76	114.35	1.71	195.03	0.770	No	No	0.85
3413	34.13	131.36	2.24	3.25	0.76	113.93	1.71	194.86	0.768	No	No	0.85
3414	34.14	130.95	2.24	3.26	0.76	113.53	1.72	194.70	0.766	No	No	0.85
3415	34.15	130.58	2.24	3.26	0.76	113.18	1.72	194.56	0.765	No	No	0.85
3416	34.16	130.38	2.24	3.27	0.76	112.97	1.72	194.53	0.765	No	No	0.85
3417	34.17	130.32	2.24	3.27	0.76	112.89	1.72	194.61	0.765	No	No	0.85
3418	34.18	130.39	2.24	3.28	0.76	112.92	1.73	194.81	0.768	No	No	0.85
3419	34.19	130.46	2.24	3.28	0.76	112.95	1.73	195.05	0.770	No	No	0.85
3420	34.20	130.54	2.24	3.29	0.76	112.99	1.73	195.30	0.773	No	No	0.86
3421	34.21	130.62	2.24	3.30	0.76	113.03	1.73	195.55	0.775	No	No	0.86
3422	34.22	130.70	2.24	3.30	0.76	113.07	1.73	195.80	0.778	No	No	0.86
3423	34.23	130.77	2.24	3.31	0.76	113.11	1.73	196.03	0.781	No	No	0.86
3424	34.24	130.85	2.24	3.31	0.76	113.15	1.73	196.23	0.783	No	No	0.87
3425	34.25	131.00	2.24	3.32	0.76	113.26	1.73	196.48	0.785	No	No	0.87
3426	34.26	131.25	2.24	3.32	0.76	113.45	1.73	196.81	0.789	No	No	0.87
3427	34.27	131.59	2.24	3.33	0.76	113.72	1.73	197.24	0.794	No	No	0.88
3428	34.28	131.96	2.24	3.33	0.76	114.02	1.73	197.72	0.799	No	No	0.89
3429	34.29	132.36	2.24	3.34	0.76	114.35	1.73	198.23	0.804	No	No	0.89
3430	34.30	132.76	2.24	3.35	0.76	114.67	1.73	198.74	0.810	No	No	0.90
3431	34.31	133.14	2.24	3.35	0.76	114.97	1.73	199.22	0.815	No	No	0.90
3432	34.32	133.48	2.24	3.36	0.76	115.24	1.73	199.64	0.820	No	No	0.91
3433	34.33	133.82	2.24	3.36	0.76	115.52	1.73	200.01	4.000	No	No	2.00
3434	34.34	134.26	2.24	3.36	0.76	115.88	1.73	200.35	4.000	No	No	2.00
3435	34.35	134.84	2.24	3.36	0.76	116.37	1.72	200.73	4.000	No	No	2.00
3436	34.36	135.55	2.24	3.36	0.76	116.97	1.72	201.17	4.000	No	No	2.00
3437	34.37	136.32	2.24	3.35	0.76	117.62	1.71	201.66	4.000	No	No	2.00
3438	34.38	137.12	2.24	3.35	0.76	118.31	1.71	202.16	4.000	No	No	2.00
3439	34.39	137.91	2.23	3.35	0.76	118.98	1.70	202.66	4.000	No	No	2.00
3440	34.40	138.64	2.23	3.34	0.76	119.60	1.70	203.12	4.000	No	No	2.00
3441	34.41	139.28	2.23	3.34	0.76	120.13	1.69	203.52	4.000	No	No	2.00
3442	34.42	139.88	2.23	3.34	0.75	120.63	1.69	203.86	4.000	No	No	2.00
3443	34.43	140.52	2.23	3.33	0.75	121.18	1.68	204.16	4.000	No	No	2.00
3444	34.44	141.29	2.22	3.32	0.75	121.83	1.68	204.50	4.000	No	No	2.00
3445	34.45	142.17	2.22	3.31	0.75	122.59	1.67	204.89	4.000	No	No	2.00
3446	34.46	143.12	2.22	3.30	0.75	123.40	1.66	205.31	4.000	No	No	2.00
3447	34.47	144.08	2.22	3.29	0.75	124.22	1.66	205.74	4.000	No	No	2.00
3448	34.48	145.01	2.21	3.28	0.75	125.02	1.65	206.16	4.000	No	No	2.00
3449	34.49	145.85	2.21	3.28	0.75	125.74	1.64	206.54	4.000	No	No	2.00
3450	34.50	146.58	2.21	3.27	0.75	126.36	1.64	206.85	4.000	No	No	2.00
3451	34.51	147.30	2.21	3.26	0.75	126.97	1.63	207.05	4.000	No	No	2.00
3452	34.52	148.09	2.20	3.24	0.75	127.65	1.62	207.19	4.000	No	No	2.00
3453	34.53	149.04	2.20	3.22	0.74	128.47	1.61	207.32	4.000	No	No	2.00
3454	34.54	150.10	2.20	3.20	0.74	129.39	1.60	207.48	4.000	No	No	2.00
3455	34.55	151.22	2.19	3.18	0.74	130.35	1.59	207.65	4.000	No	No	2.00
3456	34.56	152.33	2.19	3.16	0.74	131.32	1.58	207.83	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3457	34.57	153.39	2.18	3.14	0.74	132.23	1.57	208.00	4.000	No	No	2.00
3458	34.58	154.32	2.18	3.12	0.74	133.04	1.56	208.16	4.000	No	No	2.00
3459	34.59	155.17	2.18	3.10	0.73	133.77	1.56	208.29	4.000	No	No	2.00
3460	34.60	156.04	2.17	3.08	0.73	134.52	1.55	208.38	4.000	No	No	2.00
3461	34.61	157.06	2.17	3.06	0.73	135.40	1.54	208.47	4.000	No	No	2.00
3462	34.62	158.27	2.16	3.03	0.73	136.46	1.53	208.59	4.000	No	No	2.00
3463	34.63	159.59	2.16	3.00	0.73	137.61	1.52	208.73	4.000	No	No	2.00
3464	34.64	160.95	2.15	2.96	0.73	138.80	1.51	208.90	4.000	No	No	2.00
3465	34.65	162.28	2.14	2.93	0.72	139.97	1.49	209.08	4.000	No	No	2.00
3466	34.66	163.52	2.14	2.90	0.72	141.05	1.48	209.26	4.000	No	No	2.00
3467	34.67	164.60	2.13	2.88	0.72	141.99	1.47	209.43	4.000	No	No	2.00
3468	34.68	165.50	2.13	2.86	0.72	142.77	1.47	209.49	4.000	No	No	2.00
3469	34.69	166.34	2.13	2.83	0.72	143.49	1.46	209.46	4.000	No	No	2.00
3470	34.70	167.24	2.12	2.80	0.71	144.28	1.45	209.35	4.000	No	No	2.00
3471	34.71	168.27	2.11	2.76	0.71	145.19	1.44	209.25	4.000	No	No	2.00
3472	34.72	169.37	2.11	2.73	0.71	146.16	1.43	209.16	4.000	No	No	2.00
3473	34.73	170.49	2.10	2.69	0.71	147.14	1.42	209.10	4.000	No	No	2.00
3474	34.74	171.57	2.10	2.65	0.70	148.09	1.41	209.06	4.000	No	No	2.00
3475	34.75	172.55	2.09	2.62	0.70	148.96	1.40	209.05	4.000	No	No	2.00
3476	34.76	173.37	2.08	2.59	0.70	149.67	1.40	209.03	4.000	No	No	2.00
3477	34.77	174.04	2.08	2.56	0.70	150.25	1.39	208.97	4.000	No	No	2.00
3478	34.78	174.67	2.08	2.54	0.70	150.79	1.39	208.86	4.000	No	No	2.00
3479	34.79	175.35	2.07	2.51	0.69	151.39	1.38	208.71	4.000	No	No	2.00
3480	34.80	176.10	2.06	2.48	0.69	152.06	1.37	208.58	4.000	No	No	2.00
3481	34.81	176.90	2.06	2.44	0.69	152.76	1.36	208.46	4.000	No	No	2.00
3482	34.82	177.69	2.05	2.41	0.69	153.46	1.36	208.35	4.000	No	No	2.00
3483	34.83	178.45	2.05	2.37	0.69	154.12	1.35	208.27	4.000	No	No	2.00
3484	34.84	179.11	2.04	2.34	0.68	154.71	1.35	208.21	4.000	No	No	2.00
3485	34.85	179.64	2.04	2.32	0.68	155.17	1.34	208.14	4.000	No	No	2.00
3486	34.86	180.06	2.03	2.30	0.68	155.53	1.34	208.07	4.000	No	No	2.00
3487	34.87	180.45	2.03	2.28	0.68	155.85	1.33	207.96	4.000	No	No	2.00
3488	34.88	180.87	2.03	2.26	0.68	156.22	1.33	207.85	4.000	No	No	2.00
3489	34.89	181.34	2.02	2.23	0.68	156.63	1.33	207.74	4.000	No	No	2.00
3490	34.90	181.82	2.02	2.21	0.67	157.05	1.32	207.63	4.000	No	No	2.00
3491	34.91	182.29	2.01	2.18	0.67	157.46	1.32	207.53	4.000	No	No	2.00
3492	34.92	182.73	2.01	2.16	0.67	157.83	1.31	207.45	4.000	No	No	2.00
3493	34.93	183.09	2.00	2.14	0.67	158.15	1.31	207.36	4.000	No	No	2.00
3494	34.94	183.24	2.00	2.12	0.67	158.27	1.31	207.14	4.000	No	No	2.00
3495	34.95	183.18	2.00	2.11	0.67	158.19	1.31	206.72	4.000	No	No	2.00
3496	34.96	182.92	2.00	2.09	0.67	157.95	1.30	206.09	4.000	No	No	2.00
3497	34.97	182.62	1.99	2.07	0.67	157.68	1.30	205.38	4.000	No	No	2.00
3498	34.98	182.30	1.99	2.05	0.67	157.40	1.30	204.62	4.000	No	No	2.00
3499	34.99	181.98	1.99	2.02	0.66	157.11	1.30	203.86	4.000	No	No	2.00
3500	35.00	181.67	1.99	2.00	0.66	156.83	1.30	203.13	4.000	No	No	2.00
3501	35.01	181.39	1.98	1.98	0.66	156.57	1.29	202.47	4.000	No	No	2.00
3502	35.02	181.10	1.98	1.97	0.66	156.30	1.29	201.86	4.000	No	No	2.00
3503	35.03	180.67	1.98	1.96	0.66	155.91	1.29	201.19	4.000	No	No	2.00
3504	35.04	180.05	1.98	1.95	0.66	155.33	1.29	200.37	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3505	35.05	179.23	1.98	1.94	0.66	154.59	1.29	199.36	0.817	No	No	0.91
3506	35.06	178.32	1.98	1.92	0.66	153.77	1.29	198.24	0.804	No	No	0.89
3507	35.07	177.36	1.98	1.91	0.66	152.91	1.29	197.06	0.792	No	No	0.88
3508	35.08	176.41	1.98	1.90	0.66	152.05	1.29	195.89	0.779	No	No	0.87
3509	35.09	175.50	1.98	1.89	0.66	151.24	1.29	194.79	0.767	No	No	0.85
3510	35.10	174.70	1.97	1.88	0.66	150.51	1.29	193.81	0.757	No	No	0.84
3511	35.11	173.94	1.97	1.87	0.66	149.82	1.29	192.91	0.748	No	No	0.83
3512	35.12	173.07	1.98	1.86	0.66	149.03	1.29	191.97	0.738	No	No	0.82
3513	35.13	171.99	1.98	1.86	0.66	148.05	1.29	190.86	0.727	No	No	0.81
3514	35.14	170.71	1.98	1.86	0.66	146.89	1.29	189.56	0.713	No	No	0.79
3515	35.15	169.31	1.98	1.86	0.66	145.63	1.29	188.15	0.699	No	No	0.78
3516	35.16	167.87	1.98	1.85	0.66	144.33	1.29	186.69	0.685	No	No	0.76
3517	35.17	166.45	1.98	1.85	0.66	143.06	1.30	185.27	0.671	No	No	0.75
3518	35.18	165.15	1.99	1.85	0.66	141.88	1.30	183.96	0.659	No	No	0.73
3519	35.19	164.00	1.99	1.85	0.66	140.85	1.30	182.81	0.648	No	No	0.72
3520	35.20	162.86	1.99	1.85	0.67	139.81	1.30	181.70	0.638	No	No	0.71
3521	35.21	161.55	1.99	1.85	0.67	138.63	1.30	180.49	0.627	No	No	0.70
3522	35.22	159.93	2.00	1.85	0.67	137.16	1.31	179.03	0.614	No	No	0.68
3523	35.23	158.08	2.00	1.86	0.67	135.50	1.31	177.38	0.599	No	No	0.67
3524	35.24	156.11	2.01	1.87	0.67	133.73	1.31	175.62	0.584	No	No	0.65
3525	35.25	154.11	2.01	1.87	0.67	131.93	1.32	173.85	0.569	No	No	0.63
3526	35.26	152.18	2.02	1.88	0.68	130.21	1.32	172.15	0.554	No	No	0.62
3527	35.27	150.44	2.02	1.89	0.68	128.64	1.33	170.62	0.542	No	No	0.60
3528	35.28	148.95	2.03	1.89	0.68	127.30	1.33	169.31	0.531	No	No	0.59
3529	35.29	147.56	2.03	1.89	0.68	126.05	1.33	168.10	0.522	No	No	0.58
3530	35.30	146.10	2.03	1.90	0.68	124.73	1.34	166.82	0.512	No	No	0.57
3531	35.31	144.39	2.04	1.91	0.68	123.20	1.34	165.34	0.500	No	No	0.56
3532	35.32	142.48	2.04	1.91	0.69	121.50	1.35	163.70	0.488	No	No	0.54
3533	35.33	140.49	2.05	1.92	0.69	119.72	1.35	162.00	0.475	No	No	0.53
3534	35.34	138.50	2.05	1.93	0.69	117.94	1.36	160.33	0.463	No	No	0.52
3535	35.35	136.63	2.06	1.93	0.69	116.27	1.37	158.76	0.452	No	No	0.50
3536	35.36	134.97	2.06	1.94	0.69	114.79	1.37	157.37	0.442	No	No	0.49
3537	35.37	133.57	2.07	1.94	0.69	113.54	1.38	156.18	0.434	No	No	0.48
3538	35.38	132.29	2.07	1.94	0.70	112.39	1.38	155.03	0.427	No	No	0.47
3539	35.39	130.92	2.07	1.94	0.70	111.17	1.38	153.76	0.418	No	No	0.47
3540	35.40	129.35	2.08	1.94	0.70	109.77	1.39	152.30	0.409	No	No	0.45
3541	35.41	127.63	2.08	1.93	0.70	108.25	1.39	150.72	0.398	No	No	0.44
3542	35.42	125.87	2.08	1.93	0.70	106.69	1.40	149.11	0.388	No	No	0.43
3543	35.43	124.15	2.09	1.93	0.70	105.16	1.40	147.54	0.379	No	No	0.42
3544	35.44	122.55	2.09	1.93	0.70	103.75	1.41	146.09	0.370	No	No	0.41
3545	35.45	121.19	2.10	1.92	0.71	102.54	1.41	144.84	0.363	No	No	0.40
3546	35.46	120.09	2.10	1.92	0.71	101.56	1.42	143.83	0.357	No	No	0.40
3547	35.47	119.14	2.10	1.92	0.71	100.71	1.42	142.91	0.351	No	No	0.39
3548	35.48	118.16	2.10	1.91	0.71	99.84	1.42	141.95	0.346	No	No	0.39
3549	35.49	117.05	2.10	1.91	0.71	98.85	1.42	140.86	0.340	No	No	0.38
3550	35.50	115.86	2.11	1.90	0.71	97.80	1.43	139.70	0.334	No	No	0.37
3551	35.51	114.66	2.11	1.90	0.71	96.74	1.43	138.54	0.327	No	No	0.36
3552	35.52	113.51	2.11	1.89	0.71	95.72	1.44	137.42	0.321	No	No	0.36

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3553	35.53	112.47	2.11	1.89	0.71	94.80	1.44	136.41	0.316	No	No	0.35
3554	35.54	111.62	2.12	1.88	0.71	94.04	1.44	135.61	0.312	No	No	0.35
3555	35.55	110.98	2.12	1.88	0.71	93.47	1.44	135.04	0.309	No	No	0.34
3556	35.56	110.45	2.12	1.88	0.71	92.98	1.45	134.62	0.307	No	No	0.34
3557	35.57	109.90	2.12	1.88	0.72	92.48	1.45	134.22	0.305	No	No	0.34
3558	35.58	109.29	2.12	1.89	0.72	91.93	1.46	133.78	0.303	No	No	0.34
3559	35.59	108.65	2.13	1.89	0.72	91.35	1.46	133.32	0.300	No	No	0.33
3560	35.60	108.02	2.13	1.89	0.72	90.78	1.46	132.87	0.298	No	No	0.33
3561	35.61	107.42	2.13	1.90	0.72	90.24	1.47	132.45	0.296	No	No	0.33
3562	35.62	106.89	2.13	1.90	0.72	89.76	1.47	132.08	0.294	No	No	0.33
3563	35.63	106.46	2.13	1.90	0.72	89.36	1.48	131.81	0.293	No	No	0.33
3564	35.64	106.08	2.14	1.91	0.72	89.01	1.48	131.66	0.292	No	No	0.33
3565	35.65	105.70	2.14	1.92	0.72	88.66	1.48	131.58	0.292	No	No	0.33
3566	35.66	105.27	2.14	1.93	0.72	88.25	1.49	131.51	0.292	No	No	0.33
3567	35.67	104.81	2.15	1.95	0.73	87.82	1.50	131.45	0.291	No	No	0.32
3568	35.68	104.33	2.15	1.96	0.73	87.38	1.50	131.39	0.291	No	No	0.32
3569	35.69	103.86	2.15	1.97	0.73	86.94	1.51	131.33	0.291	No	No	0.32
3570	35.70	103.42	2.16	1.98	0.73	86.54	1.52	131.28	0.290	No	No	0.32
3571	35.71	103.06	2.16	1.99	0.73	86.19	1.52	131.24	0.290	No	No	0.32
3572	35.72	102.78	2.16	2.00	0.73	85.93	1.53	131.25	0.290	No	No	0.32
3573	35.73	102.57	2.16	2.01	0.73	85.72	1.53	131.31	0.291	No	No	0.32
3574	35.74	102.37	2.17	2.02	0.73	85.53	1.54	131.43	0.291	No	No	0.32
3575	35.75	102.15	2.17	2.03	0.73	85.31	1.54	131.56	0.292	No	No	0.33
3576	35.76	101.91	2.17	2.05	0.74	85.08	1.55	131.71	0.292	No	No	0.33
3577	35.77	101.67	2.17	2.06	0.74	84.84	1.55	131.85	0.293	No	No	0.33
3578	35.78	101.44	2.18	2.07	0.74	84.62	1.56	132.00	0.294	No	No	0.33
3579	35.79	101.23	2.18	2.08	0.74	84.41	1.57	132.13	0.295	No	No	0.33
3580	35.80	101.09	2.18	2.09	0.74	84.26	1.57	132.24	0.295	No	No	0.33
3581	35.81	101.03	2.18	2.10	0.74	84.19	1.57	132.34	0.296	No	No	0.33
3582	35.82	101.05	2.18	2.10	0.74	84.19	1.57	132.44	0.296	No	No	0.33
3583	35.83	101.12	2.18	2.10	0.74	84.23	1.57	132.55	0.297	No	No	0.33
3584	35.84	101.20	2.18	2.11	0.74	84.28	1.57	132.67	0.297	No	No	0.33
3585	35.85	101.28	2.18	2.11	0.74	84.33	1.57	132.81	0.298	No	No	0.33
3586	35.86	101.36	2.18	2.11	0.74	84.38	1.58	132.94	0.298	No	No	0.33
3587	35.87	101.43	2.18	2.12	0.74	84.42	1.58	133.06	0.299	No	No	0.33
3588	35.88	101.50	2.18	2.12	0.74	84.46	1.58	133.17	0.300	No	No	0.33
3589	35.89	101.60	2.18	2.12	0.74	84.53	1.58	133.24	0.300	No	No	0.33
3590	35.90	101.76	2.18	2.12	0.74	84.65	1.57	133.29	0.300	No	No	0.34
3591	35.91	102.00	2.18	2.11	0.74	84.84	1.57	133.33	0.300	No	No	0.34
3592	35.92	102.29	2.18	2.11	0.74	85.08	1.57	133.37	0.301	No	No	0.34
3593	35.93	102.60	2.18	2.10	0.74	85.33	1.56	133.41	0.301	No	No	0.34
3594	35.94	102.92	2.18	2.09	0.74	85.60	1.56	133.46	0.301	No	No	0.34
3595	35.95	103.23	2.17	2.09	0.74	85.85	1.56	133.51	0.301	No	No	0.34
3596	35.96	103.52	2.17	2.08	0.74	86.09	1.55	133.55	0.302	No	No	0.34
3597	35.97	103.77	2.17	2.08	0.74	86.29	1.55	133.59	0.302	No	No	0.34
3598	35.98	103.99	2.17	2.07	0.73	86.47	1.54	133.58	0.302	No	No	0.34
3599	35.99	104.22	2.17	2.06	0.73	86.66	1.54	133.52	0.301	No	No	0.34
3600	36.00	104.48	2.17	2.05	0.73	86.87	1.54	133.42	0.301	No	No	0.34

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3601	36.01	104.78	2.16	2.04	0.73	87.12	1.53	133.31	0.300	No	No	0.34
3602	36.02	105.10	2.16	2.03	0.73	87.39	1.52	133.21	0.300	No	No	0.33
3603	36.03	105.42	2.16	2.01	0.73	87.65	1.52	133.10	0.299	No	No	0.33
3604	36.04	105.72	2.15	2.00	0.73	87.91	1.51	133.00	0.299	No	No	0.33
3605	36.05	106.00	2.15	1.99	0.73	88.14	1.51	132.91	0.298	No	No	0.33
3606	36.06	106.23	2.15	1.98	0.73	88.32	1.50	132.81	0.298	No	No	0.33
3607	36.07	106.42	2.15	1.97	0.73	88.48	1.50	132.66	0.297	No	No	0.33
3608	36.08	106.60	2.15	1.95	0.73	88.64	1.49	132.44	0.296	No	No	0.33
3609	36.09	106.81	2.14	1.94	0.72	88.81	1.49	132.17	0.295	No	No	0.33
3610	36.10	107.04	2.14	1.92	0.72	89.01	1.48	131.87	0.293	No	No	0.33
3611	36.11	107.28	2.13	1.90	0.72	89.21	1.47	131.57	0.292	No	No	0.33
3612	36.12	107.52	2.13	1.88	0.72	89.41	1.47	131.27	0.290	No	No	0.32
3613	36.13	107.74	2.13	1.86	0.72	89.60	1.46	131.00	0.289	No	No	0.32
3614	36.14	107.94	2.12	1.85	0.72	89.77	1.46	130.76	0.288	No	No	0.32
3615	36.15	108.08	2.12	1.84	0.72	89.88	1.45	130.58	0.287	No	No	0.32
3616	36.16	108.18	2.12	1.83	0.72	89.96	1.45	130.46	0.287	No	No	0.32
3617	36.17	108.24	2.12	1.82	0.72	90.00	1.45	130.37	0.286	No	No	0.32
3618	36.18	108.32	2.12	1.82	0.72	90.05	1.45	130.28	0.286	No	No	0.32
3619	36.19	108.39	2.12	1.81	0.71	90.10	1.44	130.18	0.285	No	No	0.32
3620	36.20	108.47	2.12	1.81	0.71	90.16	1.44	130.07	0.285	No	No	0.32
3621	36.21	108.55	2.11	1.80	0.71	90.22	1.44	129.97	0.284	No	No	0.32
3622	36.22	108.62	2.11	1.79	0.71	90.27	1.44	129.88	0.284	No	No	0.32
3623	36.23	108.68	2.11	1.79	0.71	90.30	1.44	129.81	0.283	No	No	0.32
3624	36.24	108.72	2.11	1.79	0.71	90.31	1.44	129.84	0.284	No	No	0.32
3625	36.25	108.73	2.11	1.80	0.71	90.30	1.44	129.97	0.284	No	No	0.32
3626	36.26	108.73	2.12	1.81	0.71	90.28	1.44	130.20	0.285	No	No	0.32
3627	36.27	108.73	2.12	1.82	0.72	90.25	1.45	130.46	0.287	No	No	0.32
3628	36.28	108.73	2.12	1.83	0.72	90.22	1.45	130.75	0.288	No	No	0.32
3629	36.29	108.73	2.12	1.84	0.72	90.19	1.45	131.03	0.289	No	No	0.32
3630	36.30	108.73	2.12	1.86	0.72	90.16	1.46	131.31	0.291	No	No	0.32
3631	36.31	108.73	2.13	1.87	0.72	90.13	1.46	131.56	0.292	No	No	0.33
3632	36.32	108.72	2.13	1.88	0.72	90.10	1.46	131.79	0.293	No	No	0.33
3633	36.33	108.70	2.13	1.89	0.72	90.04	1.47	132.08	0.294	No	No	0.33
3634	36.34	108.64	2.13	1.91	0.72	89.97	1.47	132.46	0.296	No	No	0.33
3635	36.35	108.58	2.14	1.93	0.72	89.87	1.48	132.94	0.298	No	No	0.33
3636	36.36	108.50	2.14	1.95	0.72	89.77	1.49	133.48	0.301	No	No	0.34
3637	36.37	108.42	2.15	1.98	0.73	89.66	1.50	134.04	0.304	No	No	0.34
3638	36.38	108.34	2.15	2.01	0.73	89.55	1.50	134.61	0.307	No	No	0.34
3639	36.39	108.27	2.15	2.03	0.73	89.45	1.51	135.16	0.310	No	No	0.35
3640	36.40	108.20	2.16	2.05	0.73	89.36	1.52	135.64	0.312	No	No	0.35
3641	36.41	108.12	2.16	2.07	0.73	89.25	1.52	136.05	0.314	No	No	0.35
3642	36.42	107.99	2.16	2.09	0.73	89.11	1.53	136.45	0.316	No	No	0.35
3643	36.43	107.81	2.17	2.11	0.73	88.91	1.54	136.89	0.319	No	No	0.36
3644	36.44	107.59	2.17	2.14	0.74	88.69	1.55	137.41	0.321	No	No	0.36
3645	36.45	107.35	2.18	2.16	0.74	88.45	1.56	137.99	0.324	No	No	0.36
3646	36.46	107.11	2.18	2.19	0.74	88.20	1.57	138.59	0.328	No	No	0.37
3647	36.47	106.88	2.19	2.22	0.74	87.96	1.58	139.18	0.331	No	No	0.37
3648	36.48	106.67	2.19	2.25	0.74	87.74	1.59	139.74	0.334	No	No	0.37

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
3649	36.49	106.48	2.19	2.27	0.74	87.55	1.60	140.20	0.336	No	No	0.38
3650	36.50	106.31	2.20	2.29	0.75	87.38	1.61	140.56	0.338	No	No	0.38
3651	36.51	106.14	2.20	2.30	0.75	87.20	1.62	140.86	0.340	No	No	0.38
3652	36.52	105.94	2.20	2.32	0.75	87.00	1.62	141.16	0.342	No	No	0.38
3653	36.53	105.72	2.21	2.34	0.75	86.78	1.63	141.50	0.344	No	No	0.38
3654	36.54	105.48	2.21	2.36	0.75	86.54	1.64	141.87	0.346	No	No	0.39
3655	36.55	105.24	2.21	2.37	0.75	86.31	1.65	142.25	0.348	No	No	0.39
3656	36.56	105.02	2.22	2.39	0.75	86.08	1.66	142.61	0.350	No	No	0.39
3657	36.57	104.81	2.22	2.41	0.75	85.87	1.66	142.93	0.352	No	No	0.39
3658	36.58	104.65	2.22	2.42	0.76	85.71	1.67	143.19	0.353	No	No	0.40
3659	36.59	104.54	2.22	2.43	0.76	85.59	1.68	143.39	0.354	No	No	0.40
3660	36.60	104.47	2.22	2.44	0.76	85.51	1.68	143.56	0.355	No	No	0.40
3661	36.61	104.40	2.23	2.45	0.76	85.42	1.68	143.75	0.356	No	No	0.40
3662	36.62	104.32	2.23	2.46	0.76	85.33	1.69	143.96	0.357	No	No	0.40
3663	36.63	104.24	2.23	2.47	0.76	85.24	1.69	144.17	0.359	No	No	0.40
3664	36.64	104.16	2.23	2.48	0.76	85.15	1.70	144.39	0.360	No	No	0.40
3665	36.65	104.09	2.23	2.49	0.76	85.06	1.70	144.59	0.361	No	No	0.40
3666	36.66	104.02	2.23	2.49	0.76	84.98	1.70	144.77	0.362	No	No	0.41
3667	36.67	103.98	2.23	2.50	0.76	84.93	1.71	144.89	0.363	No	No	0.41
3668	36.68	103.96	2.23	2.50	0.76	84.89	1.71	144.98	0.363	No	No	0.41
3669	36.69	103.96	2.24	2.51	0.76	84.87	1.71	145.04	0.364	No	No	0.41
3670	36.70	103.96	2.24	2.51	0.76	84.85	1.71	145.12	0.364	No	No	0.41
3671	36.71	103.96	2.24	2.51	0.76	84.83	1.71	145.20	0.365	No	No	0.41
3672	36.72	103.96	2.24	2.52	0.76	84.81	1.71	145.28	0.365	No	No	0.41
3673	36.73	103.96	2.24	2.52	0.76	84.79	1.71	145.36	0.366	No	No	0.41
3674	36.74	103.96	2.24	2.52	0.76	84.77	1.72	145.43	0.366	No	No	0.41
3675	36.75	103.96	2.24	2.52	0.76	84.74	1.72	145.49	0.366	No	No	0.41
3676	36.76	103.94	2.24	2.53	0.76	84.70	1.72	145.56	0.367	No	No	0.41
3677	36.77	103.89	2.24	2.53	0.76	84.65	1.72	145.64	0.367	No	No	0.41
3678	36.78	103.83	2.24	2.54	0.76	84.57	1.72	145.74	0.368	No	No	0.41
3679	36.79	103.75	2.24	2.54	0.76	84.48	1.73	145.86	0.369	No	No	0.41
3680	36.80	103.67	2.24	2.55	0.76	84.39	1.73	145.98	0.369	No	No	0.41
3681	36.81	103.59	2.24	2.56	0.76	84.30	1.73	146.11	0.370	No	No	0.41
3682	36.82	103.52	2.24	2.56	0.76	84.22	1.74	146.23	0.371	No	No	0.42
3683	36.83	103.45	2.25	2.57	0.76	84.14	1.74	146.33	0.371	No	No	0.42
3684	36.84	103.38	2.25	2.57	0.77	84.06	1.74	146.44	0.372	No	No	0.42
3685	36.85	103.30	2.25	2.58	0.77	83.96	1.75	146.57	0.373	No	No	0.42
3686	36.86	103.18	2.25	2.59	0.77	83.84	1.75	146.76	0.374	No	No	0.42
3687	36.87	103.04	2.25	2.60	0.77	83.70	1.76	146.99	0.375	No	No	0.42
3688	36.88	102.89	2.25	2.61	0.77	83.54	1.76	147.26	0.377	No	No	0.42
3689	36.89	102.73	2.26	2.62	0.77	83.38	1.77	147.53	0.379	No	No	0.42
3690	36.90	102.57	2.26	2.64	0.77	83.22	1.78	147.80	0.380	No	No	0.43
3691	36.91	102.42	2.26	2.65	0.77	83.07	1.78	148.05	0.382	No	No	0.43
3692	36.92	102.29	2.26	2.66	0.77	82.94	1.79	148.28	0.383	No	No	0.43
3693	36.93	102.15	2.26	2.67	0.77	82.79	1.79	148.41	0.384	No	No	0.43
3694	36.94	101.96	2.26	2.67	0.77	82.61	1.80	148.46	0.384	No	No	0.43
3695	36.95	101.72	2.27	2.68	0.77	82.38	1.80	148.44	0.384	No	No	0.43
3696	36.96	101.42	2.27	2.68	0.77	82.11	1.81	148.41	0.384	No	No	0.43

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _t (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3697	36.97	101.11	2.27	2.69	0.77	81.83	1.81	148.38	0.384	No	No	0.43
3698	36.98	100.79	2.27	2.70	0.77	81.54	1.82	148.35	0.384	No	No	0.43
3699	36.99	100.48	2.27	2.70	0.78	81.25	1.83	148.33	0.383	No	No	0.43
3700	37.00	100.19	2.27	2.71	0.78	80.99	1.83	148.30	0.383	No	No	0.43
3701	37.01	99.96	2.28	2.71	0.78	80.77	1.84	148.27	0.383	No	No	0.43
3702	37.02	99.78	2.28	2.72	0.78	80.60	1.84	148.16	0.382	No	No	0.43
3703	37.03	99.64	2.28	2.71	0.78	80.47	1.84	147.97	0.381	No	No	0.43
3704	37.04	99.51	2.28	2.71	0.78	80.34	1.84	147.70	0.380	No	No	0.43
3705	37.05	99.36	2.28	2.70	0.78	80.20	1.84	147.40	0.378	No	No	0.42
3706	37.06	99.20	2.28	2.70	0.78	80.05	1.84	147.08	0.376	No	No	0.42
3707	37.07	99.04	2.28	2.69	0.78	79.91	1.84	146.76	0.374	No	No	0.42
3708	37.08	98.89	2.28	2.68	0.78	79.76	1.84	146.45	0.372	No	No	0.42
3709	37.09	98.75	2.28	2.68	0.78	79.64	1.84	146.18	0.370	No	No	0.42
3710	37.10	98.66	2.27	2.67	0.78	79.55	1.83	145.91	0.369	No	No	0.41
3711	37.11	98.64	2.27	2.66	0.78	79.52	1.83	145.59	0.367	No	No	0.41
3712	37.12	98.68	2.27	2.65	0.78	79.54	1.83	145.19	0.365	No	No	0.41
3713	37.13	98.75	2.27	2.63	0.77	79.60	1.82	144.70	0.362	No	No	0.41
3714	37.14	98.83	2.27	2.61	0.77	79.66	1.81	144.16	0.359	No	No	0.40
3715	37.15	98.91	2.27	2.60	0.77	79.72	1.80	143.60	0.355	No	No	0.40
3716	37.16	98.98	2.26	2.58	0.77	79.78	1.79	143.05	0.352	No	No	0.40
3717	37.17	99.06	2.26	2.56	0.77	79.84	1.79	142.54	0.349	No	No	0.39
3718	37.18	99.12	2.26	2.54	0.77	79.88	1.78	142.09	0.347	No	No	0.39
3719	37.19	99.16	2.26	2.53	0.77	79.91	1.77	141.81	0.345	No	No	0.39
3720	37.20	99.18	2.26	2.53	0.77	79.91	1.77	141.68	0.344	No	No	0.39
3721	37.21	99.18	2.26	2.53	0.77	79.89	1.77	141.67	0.344	No	No	0.39
3722	37.22	99.18	2.26	2.53	0.77	79.88	1.77	141.68	0.344	No	No	0.39
3723	37.23	99.18	2.26	2.53	0.77	79.86	1.77	141.68	0.345	No	No	0.39
3724	37.24	99.18	2.26	2.53	0.77	79.84	1.77	141.69	0.345	No	No	0.39
3725	37.25	99.18	2.26	2.53	0.77	79.82	1.78	141.69	0.345	No	No	0.39
3726	37.26	99.18	2.26	2.53	0.77	79.81	1.78	141.70	0.345	No	No	0.39
3727	37.27	99.19	2.26	2.53	0.77	79.80	1.78	141.67	0.344	No	No	0.39
3728	37.28	99.24	2.26	2.53	0.77	79.82	1.77	141.50	0.343	No	No	0.39
3729	37.29	99.33	2.25	2.51	0.77	79.89	1.77	141.16	0.342	No	No	0.38
3730	37.30	99.46	2.25	2.49	0.77	80.00	1.76	140.66	0.339	No	No	0.38
3731	37.31	99.61	2.25	2.47	0.77	80.12	1.75	140.10	0.336	No	No	0.38
3732	37.32	99.77	2.25	2.45	0.77	80.25	1.74	139.52	0.333	No	No	0.37
3733	37.33	99.93	2.24	2.43	0.76	80.39	1.73	138.94	0.329	No	No	0.37
3734	37.34	100.08	2.24	2.41	0.76	80.51	1.72	138.39	0.326	No	No	0.37
3735	37.35	100.22	2.24	2.39	0.76	80.62	1.71	137.90	0.324	No	No	0.36
3736	37.36	100.32	2.23	2.37	0.76	80.71	1.70	137.43	0.321	No	No	0.36
3737	37.37	100.40	2.23	2.35	0.76	80.78	1.69	136.90	0.319	No	No	0.36
3738	37.38	100.47	2.23	2.33	0.76	80.83	1.69	136.23	0.315	No	No	0.35
3739	37.39	100.54	2.22	2.30	0.76	80.90	1.67	135.42	0.311	No	No	0.35
3740	37.40	100.62	2.22	2.27	0.76	80.97	1.66	134.54	0.307	No	No	0.34
3741	37.41	100.69	2.21	2.23	0.75	81.04	1.65	133.64	0.302	No	No	0.34
3742	37.42	100.77	2.21	2.20	0.75	81.12	1.64	132.76	0.298	No	No	0.33
3743	37.43	100.85	2.20	2.17	0.75	81.19	1.63	131.94	0.294	No	No	0.33
3744	37.44	100.91	2.20	2.15	0.75	81.25	1.62	131.23	0.290	No	No	0.33

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _k (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3745	37.45	100.92	2.20	2.14	0.75	81.24	1.61	130.97	0.289	No	No	0.32
3746	37.46	100.86	2.20	2.15	0.75	81.17	1.62	131.19	0.290	No	No	0.33
3747	37.47	100.74	2.21	2.18	0.75	81.03	1.63	131.87	0.293	No	No	0.33
3748	37.48	100.59	2.21	2.21	0.75	80.86	1.64	132.69	0.297	No	No	0.33
3749	37.49	100.43	2.22	2.24	0.75	80.68	1.66	133.58	0.302	No	No	0.34
3750	37.50	100.27	2.22	2.28	0.76	80.51	1.67	134.50	0.306	No	No	0.34
3751	37.51	100.12	2.23	2.31	0.76	80.33	1.69	135.40	0.311	No	No	0.35
3752	37.52	99.98	2.23	2.35	0.76	80.17	1.70	136.23	0.315	No	No	0.35
3753	37.53	99.86	2.24	2.37	0.76	80.03	1.71	136.92	0.319	No	No	0.36
3754	37.54	99.75	2.24	2.39	0.76	79.91	1.72	137.46	0.322	No	No	0.36
3755	37.55	99.63	2.24	2.41	0.76	79.78	1.73	137.91	0.324	No	No	0.36
3756	37.56	99.50	2.24	2.43	0.77	79.64	1.74	138.37	0.326	No	No	0.37
3757	37.57	99.35	2.25	2.45	0.77	79.48	1.75	138.90	0.329	No	No	0.37
3758	37.58	99.19	2.25	2.47	0.77	79.31	1.76	139.46	0.332	No	No	0.37
3759	37.59	99.03	2.26	2.50	0.77	79.15	1.77	140.02	0.335	No	No	0.38
3760	37.60	98.88	2.26	2.52	0.77	78.99	1.78	140.55	0.338	No	No	0.38
3761	37.61	98.74	2.26	2.54	0.77	78.85	1.79	141.04	0.341	No	No	0.38
3762	37.62	98.62	2.26	2.55	0.77	78.72	1.80	141.45	0.343	No	No	0.39
3763	37.63	98.51	2.27	2.57	0.77	78.60	1.80	141.84	0.345	No	No	0.39
3764	37.64	98.39	2.27	2.59	0.77	78.47	1.81	142.28	0.348	No	No	0.39
3765	37.65	98.25	2.27	2.61	0.78	78.32	1.82	142.79	0.351	No	No	0.39
3766	37.66	98.10	2.27	2.63	0.78	78.16	1.83	143.35	0.354	No	No	0.40
3767	37.67	97.94	2.28	2.65	0.78	78.00	1.85	143.94	0.357	No	No	0.40
3768	37.68	97.78	2.28	2.67	0.78	77.83	1.86	144.52	0.361	No	No	0.41
3769	37.69	97.64	2.28	2.69	0.78	77.68	1.87	145.06	0.364	No	No	0.41
3770	37.70	97.51	2.29	2.71	0.78	77.55	1.88	145.54	0.367	No	No	0.41
3771	37.71	97.39	2.29	2.73	0.78	77.42	1.89	146.12	4.000	Yes	No	2.00
3772	37.72	97.28	2.29	2.76	0.78	77.29	1.90	146.93	4.000	Yes	No	2.00
3773	37.73	97.16	2.30	2.80	0.79	77.15	1.92	148.05	4.000	Yes	No	2.00
3774	37.74	97.01	2.30	2.84	0.79	76.98	1.94	149.35	4.000	Yes	No	2.00
3775	37.75	96.85	2.31	2.89	0.79	76.80	1.96	150.76	4.000	Yes	No	2.00
3776	37.76	96.69	2.32	2.94	0.79	76.62	1.99	152.19	4.000	Yes	No	2.00
3777	37.77	96.54	2.32	2.98	0.80	76.45	2.01	153.59	4.000	Yes	No	2.00
3778	37.78	96.40	2.33	3.03	0.80	76.29	2.03	154.87	4.000	Yes	No	2.00
3779	37.79	96.27	2.33	3.06	0.80	76.14	2.05	155.97	4.000	Yes	No	2.00
3780	37.80	96.11	2.34	3.10	0.80	75.98	2.07	156.97	4.000	Yes	No	2.00
3781	37.81	95.90	2.34	3.13	0.80	75.76	2.09	158.01	4.000	Yes	No	2.00
3782	37.82	95.63	2.35	3.18	0.80	75.50	2.11	159.22	4.000	Yes	No	2.00
3783	37.83	95.33	2.35	3.22	0.81	75.21	2.14	160.59	4.000	Yes	No	2.00
3784	37.84	95.01	2.36	3.27	0.81	74.90	2.16	162.03	4.000	Yes	No	2.00
3785	37.85	94.69	2.36	3.32	0.81	74.59	2.19	163.48	4.000	Yes	No	2.00
3786	37.86	94.39	2.37	3.37	0.81	74.30	2.22	164.85	4.000	Yes	No	2.00
3787	37.87	94.12	2.37	3.42	0.82	74.04	2.24	166.08	4.000	Yes	No	2.00
3788	37.88	93.88	2.38	3.45	0.82	73.80	2.27	167.19	4.000	Yes	No	2.00
3789	37.89	93.63	2.38	3.50	0.82	73.56	2.29	168.35	4.000	Yes	No	2.00
3790	37.90	93.33	2.39	3.54	0.82	73.27	2.32	169.72	4.000	Yes	No	2.00
3791	37.91	92.98	2.40	3.60	0.82	72.94	2.35	171.36	4.000	Yes	No	2.00
3792	37.92	92.59	2.40	3.66	0.83	72.57	2.39	173.15	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3793	37.93	92.19	2.41	3.73	0.83	72.20	2.42	175.01	4.000	Yes	No	2.00
3794	37.94	91.80	2.42	3.79	0.83	71.83	2.46	176.83	4.000	Yes	No	2.00
3795	37.95	91.43	2.42	3.85	0.83	71.48	2.50	178.52	4.000	Yes	No	2.00
3796	37.96	91.12	2.43	3.90	0.84	71.18	2.53	179.99	4.000	Yes	No	2.00
3797	37.97	90.82	2.43	3.94	0.84	70.90	2.56	181.19	4.000	Yes	No	2.00
3798	37.98	90.50	2.44	3.98	0.84	70.60	2.58	182.28	4.000	Yes	No	2.00
3799	37.99	90.11	2.44	4.03	0.84	70.25	2.61	183.41	4.000	Yes	No	2.00
3800	38.00	89.67	2.45	4.08	0.84	69.86	2.64	184.70	4.000	Yes	No	2.00
3801	38.01	89.20	2.45	4.13	0.85	69.43	2.68	186.09	4.000	Yes	No	2.00
3802	38.02	88.72	2.46	4.18	0.85	69.00	2.72	187.49	4.000	Yes	No	2.00
3803	38.03	88.26	2.47	4.24	0.85	68.59	2.75	188.84	4.000	Yes	No	2.00
3804	38.04	87.84	2.47	4.28	0.85	68.20	2.79	190.06	4.000	Yes	No	2.00
3805	38.05	87.48	2.48	4.32	0.85	67.89	2.81	191.05	4.000	Yes	No	2.00
3806	38.06	87.20	2.48	4.35	0.86	67.63	2.84	191.76	4.000	Yes	No	2.00
3807	38.07	86.95	2.48	4.37	0.86	67.40	2.85	192.30	0.741	No	No	0.84
3808	38.08	86.68	2.48	4.40	0.86	67.15	2.87	192.80	0.747	No	No	0.84
3809	38.09	86.37	2.49	4.42	0.86	66.88	2.89	193.37	0.752	No	No	0.85
3810	38.10	86.06	2.49	4.45	0.86	66.59	2.91	193.96	0.759	No	No	0.86
3811	38.11	85.74	2.49	4.48	0.86	66.31	2.93	194.55	0.765	No	No	0.86
3812	38.12	85.44	2.50	4.50	0.86	66.04	2.95	195.10	0.771	No	No	0.87
3813	38.13	85.17	2.50	4.52	0.86	65.80	2.97	195.59	0.776	No	No	0.88
3814	38.14	85.10	2.50	4.54	0.86	65.72	2.81	184.63	0.665	No	No	0.75
3815	38.15	85.36	2.50	4.53	0.86	65.92	2.97	196.03	4.000	Yes	No	2.00
3816	38.16	85.95	2.50	4.52	0.86	66.39	2.95	195.97	4.000	Yes	No	2.00
3817	38.17	86.73	2.49	4.49	0.86	67.01	2.92	195.84	4.000	Yes	No	2.00
3818	38.18	87.59	2.49	4.47	0.86	67.70	2.89	195.70	4.000	Yes	No	2.00
3819	38.19	88.47	2.48	4.44	0.86	68.40	2.86	195.55	4.000	Yes	No	2.00
3820	38.20	89.33	2.48	4.42	0.86	69.10	2.83	195.39	4.000	Yes	No	2.00
3821	38.21	90.14	2.47	4.39	0.85	69.75	2.80	195.24	4.000	Yes	No	2.00
3822	38.22	90.84	2.47	4.37	0.85	70.31	2.77	195.09	4.000	Yes	No	2.00
3823	38.23	91.74	2.46	4.34	0.85	71.04	2.74	194.78	4.000	Yes	No	2.00
3824	38.24	93.00	2.46	4.30	0.85	72.06	2.70	194.22	4.000	Yes	No	2.00
3825	38.25	94.73	2.45	4.23	0.84	73.48	2.63	193.37	4.000	Yes	No	2.00
3826	38.26	96.72	2.43	4.16	0.84	75.11	2.56	192.37	4.000	Yes	No	2.00
3827	38.27	98.84	2.42	4.08	0.83	76.86	2.49	191.26	4.000	Yes	No	2.00
3828	38.28	101.01	2.41	4.00	0.83	78.64	2.42	190.12	4.000	Yes	No	2.00
3829	38.29	103.09	2.40	3.93	0.82	80.36	2.35	188.99	4.000	Yes	No	2.00
3830	38.30	104.99	2.38	3.86	0.82	81.93	2.29	187.95	4.000	Yes	No	2.00
3831	38.31	106.63	2.37	3.80	0.82	83.28	2.25	187.06	4.000	Yes	No	2.00
3832	38.32	108.17	2.37	3.74	0.81	84.55	2.20	186.22	4.000	Yes	No	2.00
3833	38.33	109.84	2.36	3.68	0.81	85.93	2.16	185.34	4.000	Yes	No	2.00
3834	38.34	111.81	2.34	3.61	0.80	87.56	2.10	184.32	4.000	Yes	No	2.00
3835	38.35	114.00	2.33	3.54	0.80	89.39	2.05	183.19	4.000	Yes	No	2.00
3836	38.36	116.31	2.32	3.46	0.79	91.32	1.99	182.02	4.000	Yes	No	2.00
3837	38.37	118.62	2.30	3.38	0.79	93.24	1.94	180.87	4.000	Yes	No	2.00
3838	38.38	120.80	2.29	3.30	0.78	95.07	1.89	179.81	4.000	Yes	No	2.00
3839	38.39	122.75	2.28	3.23	0.78	96.70	1.85	178.89	4.000	Yes	No	2.00
3840	38.40	124.30	2.27	3.19	0.78	98.00	1.82	178.43	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3841	38.41	125.59	2.27	3.16	0.77	99.05	1.80	178.53	4.000	Yes	No	2.00
3842	38.42	126.79	2.26	3.16	0.77	100.02	1.79	179.19	4.000	Yes	No	2.00
3843	38.43	128.14	2.26	3.16	0.77	101.11	1.78	180.10	4.000	Yes	No	2.00
3844	38.44	129.62	2.26	3.16	0.77	102.30	1.77	181.09	4.000	Yes	No	2.00
3845	38.45	131.14	2.25	3.15	0.77	103.53	1.76	182.13	4.000	Yes	No	2.00
3846	38.46	132.63	2.25	3.15	0.77	104.73	1.75	183.14	4.000	Yes	No	2.00
3847	38.47	134.02	2.25	3.15	0.77	105.85	1.74	184.09	4.000	Yes	No	2.00
3848	38.48	135.21	2.24	3.15	0.77	106.81	1.73	184.93	0.668	No	No	0.76
3849	38.49	135.93	2.24	3.16	0.77	107.36	1.73	185.92	0.678	No	No	0.77
3850	38.50	136.24	2.25	3.20	0.77	107.56	1.74	187.22	0.690	No	No	0.78
3851	38.51	136.24	2.25	3.25	0.77	107.49	1.76	189.00	0.708	No	No	0.80
3852	38.52	136.24	2.26	3.31	0.77	107.41	1.78	191.06	0.729	No	No	0.83
3853	38.53	136.24	2.26	3.38	0.77	107.33	1.80	193.28	0.751	No	No	0.85
3854	38.54	136.24	2.27	3.45	0.78	107.25	1.82	195.55	0.775	No	No	0.88
3855	38.55	136.25	2.28	3.51	0.78	107.17	1.85	197.76	0.799	No	No	0.91
3856	38.56	136.25	2.28	3.57	0.78	107.10	1.87	199.79	0.822	No	No	0.93
3857	38.57	136.17	2.29	3.62	0.78	106.97	1.88	201.49	4.000	No	No	2.00
3858	38.58	135.87	2.29	3.67	0.79	106.66	1.90	202.97	4.000	No	No	2.00
3859	38.59	135.29	2.30	3.72	0.79	106.12	1.93	204.41	4.000	No	No	2.00
3860	38.60	134.48	2.31	3.78	0.79	105.38	1.96	206.05	4.000	No	No	2.00
3861	38.61	133.57	2.32	3.85	0.79	104.56	1.99	207.89	4.000	No	No	2.00
3862	38.62	132.61	2.33	3.93	0.80	103.70	2.02	209.85	4.000	No	No	2.00
3863	38.63	131.66	2.33	4.00	0.80	102.85	2.06	211.80	4.000	No	No	2.00
3864	38.64	130.76	2.34	4.07	0.80	102.04	2.09	213.67	4.000	No	No	2.00
3865	38.65	129.95	2.35	4.13	0.81	101.32	2.13	215.32	4.000	No	No	2.00
3866	38.66	129.23	2.36	4.19	0.81	100.67	2.15	216.77	4.000	No	No	2.00
3867	38.67	128.46	2.36	4.25	0.81	99.99	2.18	218.20	4.000	No	No	2.00
3868	38.68	127.56	2.37	4.31	0.81	99.19	2.22	219.82	4.000	No	No	2.00
3869	38.69	126.49	2.38	4.38	0.82	98.25	2.26	221.71	4.000	No	No	2.00
3870	38.70	125.33	2.39	4.46	0.82	97.24	2.30	223.77	4.000	No	No	2.00
3871	38.71	124.13	2.40	4.55	0.82	96.19	2.35	225.89	4.000	No	No	2.00
3872	38.72	122.95	2.40	4.63	0.83	95.17	2.40	227.96	4.000	No	No	2.00
3873	38.73	121.86	2.41	4.71	0.83	94.22	2.44	229.87	4.000	No	No	2.00
3874	38.74	120.92	2.42	4.77	0.83	93.40	2.48	231.50	4.000	No	No	2.00
3875	38.75	120.17	2.42	4.82	0.84	92.75	2.51	232.64	4.000	No	No	2.00
3876	38.76	119.53	2.43	4.86	0.84	92.19	2.53	233.43	4.000	No	No	2.00
3877	38.77	118.88	2.43	4.89	0.84	91.63	2.55	234.03	4.000	No	No	2.00
3878	38.78	118.14	2.44	4.92	0.84	91.00	2.58	234.71	4.000	No	No	2.00
3879	38.79	117.35	2.44	4.96	0.84	90.32	2.61	235.43	4.000	No	No	2.00
3880	38.80	116.55	2.45	5.00	0.84	89.63	2.63	236.16	4.000	No	No	2.00
3881	38.81	115.79	2.45	5.04	0.85	88.97	2.66	236.85	4.000	No	No	2.00
3882	38.82	115.09	2.46	5.07	0.85	88.37	2.69	237.47	4.000	No	No	2.00
3883	38.83	114.58	2.46	5.09	0.85	87.94	2.70	237.85	4.000	No	No	2.00
3884	38.84	114.42	2.46	5.10	0.85	87.78	2.71	237.76	4.000	No	No	2.00
3885	38.85	114.57	2.46	5.08	0.85	87.89	2.70	237.19	4.000	No	No	2.00
3886	38.86	114.91	2.45	5.04	0.85	88.16	2.68	236.27	4.000	No	No	2.00
3887	38.87	115.29	2.45	5.01	0.85	88.46	2.66	235.25	4.000	No	No	2.00
3888	38.88	115.69	2.45	4.97	0.84	88.78	2.64	234.17	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3889	38.89	116.08	2.44	4.93	0.84	89.09	2.62	233.10	4.000	No	No	2.00
3890	38.90	116.46	2.44	4.90	0.84	89.39	2.60	232.08	4.000	No	No	2.00
3891	38.91	116.79	2.44	4.86	0.84	89.65	2.58	231.18	4.000	No	No	2.00
3892	38.92	117.22	2.43	4.83	0.84	89.99	2.56	230.20	4.000	No	No	2.00
3893	38.93	117.86	2.43	4.78	0.84	90.51	2.53	228.95	4.000	No	No	2.00
3894	38.94	118.80	2.42	4.71	0.84	91.28	2.49	227.25	4.000	No	No	2.00
3895	38.95	119.94	2.41	4.63	0.83	92.22	2.44	225.21	4.000	No	No	2.00
3896	38.96	121.18	2.40	4.54	0.83	93.25	2.39	222.97	4.000	No	No	2.00
3897	38.97	122.46	2.39	4.45	0.82	94.31	2.34	220.65	4.000	No	No	2.00
3898	38.98	123.72	2.38	4.37	0.82	95.35	2.29	218.38	4.000	No	No	2.00
3899	38.99	124.88	2.37	4.28	0.82	96.32	2.25	216.27	4.000	No	No	2.00
3900	39.00	125.89	2.37	4.21	0.81	97.16	2.21	214.43	4.000	No	No	2.00
3901	39.01	126.86	2.36	4.15	0.81	97.96	2.17	212.76	4.000	No	No	2.00
3902	39.02	127.93	2.35	4.08	0.81	98.85	2.13	211.04	4.000	No	No	2.00
3903	39.03	129.23	2.34	4.00	0.80	99.94	2.09	209.04	4.000	No	No	2.00
3904	39.04	130.71	2.33	3.91	0.80	101.18	2.04	206.78	4.000	No	No	2.00
3905	39.05	132.29	2.32	3.81	0.80	102.50	1.99	204.38	4.000	No	No	2.00
3906	39.06	133.89	2.31	3.71	0.79	103.85	1.94	201.98	4.000	No	No	2.00
3907	39.07	135.42	2.29	3.61	0.79	105.15	1.90	199.70	0.821	No	No	0.93
3908	39.08	136.82	2.28	3.53	0.78	106.33	1.86	197.67	0.798	No	No	0.91
3909	39.09	137.99	2.27	3.46	0.78	107.32	1.83	196.07	0.781	No	No	0.89
3910	39.10	139.01	2.27	3.41	0.78	108.18	1.80	194.96	0.769	No	No	0.87
3911	39.11	140.04	2.26	3.36	0.77	109.03	1.78	194.17	0.761	No	No	0.87
3912	39.12	141.20	2.25	3.32	0.77	110.00	1.76	193.45	0.753	No	No	0.86
3913	39.13	142.50	2.24	3.26	0.77	111.07	1.73	192.67	0.745	No	No	0.85
3914	39.14	143.85	2.24	3.21	0.76	112.21	1.71	191.87	0.737	No	No	0.84
3915	39.15	145.20	2.23	3.16	0.76	113.33	1.69	191.11	0.729	No	No	0.83
3916	39.16	146.47	2.22	3.11	0.76	114.40	1.66	190.41	0.722	No	No	0.82
3917	39.17	147.60	2.21	3.07	0.76	115.34	1.65	189.82	0.716	No	No	0.81
3918	39.18	148.54	2.21	3.04	0.75	116.11	1.63	189.53	0.713	No	No	0.81
3919	39.19	149.38	2.20	3.02	0.75	116.79	1.62	189.63	0.714	No	No	0.81
3920	39.20	150.25	2.20	3.01	0.75	117.48	1.62	190.08	0.719	No	No	0.82
3921	39.21	151.26	2.20	3.01	0.75	118.28	1.61	190.69	0.725	No	No	0.83
3922	39.22	152.35	2.20	3.01	0.75	119.15	1.61	191.35	0.732	No	No	0.83
3923	39.23	153.47	2.19	3.00	0.75	120.04	1.60	192.04	0.739	No	No	0.84
3924	39.24	154.56	2.19	3.00	0.75	120.91	1.59	192.71	0.746	No	No	0.85
3925	39.25	155.58	2.19	2.99	0.75	121.71	1.59	193.33	0.752	No	No	0.86
3926	39.26	156.45	2.19	2.99	0.75	122.40	1.58	193.87	0.758	No	No	0.86
3927	39.27	157.15	2.19	2.99	0.75	122.95	1.58	194.40	0.763	No	No	0.87
3928	39.28	157.78	2.19	2.99	0.75	123.43	1.58	195.00	0.770	No	No	0.88
3929	39.29	158.43	2.19	3.00	0.75	123.92	1.58	195.73	0.777	No	No	0.89
3930	39.30	159.18	2.19	3.01	0.75	124.49	1.58	196.56	0.786	No	No	0.90
3931	39.31	159.97	2.19	3.02	0.75	125.09	1.58	197.46	0.796	No	No	0.91
3932	39.32	160.77	2.18	3.03	0.75	125.70	1.58	198.36	0.806	No	No	0.92
3933	39.33	161.53	2.18	3.04	0.75	126.29	1.58	199.23	0.815	No	No	0.93
3934	39.34	162.23	2.18	3.05	0.75	126.81	1.58	200.01	4.000	No	No	2.00
3935	39.35	162.80	2.18	3.06	0.75	127.24	1.58	200.63	4.000	No	No	2.00
3936	39.36	163.28	2.18	3.06	0.75	127.60	1.58	201.06	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3937	39.37	163.71	2.18	3.06	0.75	127.93	1.57	201.36	4.000	No	No	2.00
3938	39.38	164.20	2.18	3.06	0.74	128.29	1.57	201.65	4.000	No	No	2.00
3939	39.39	164.73	2.18	3.05	0.74	128.70	1.57	201.97	4.000	No	No	2.00
3940	39.40	165.29	2.18	3.05	0.74	129.13	1.57	202.30	4.000	No	No	2.00
3941	39.41	165.84	2.18	3.05	0.74	129.56	1.56	202.64	4.000	No	No	2.00
3942	39.42	166.37	2.18	3.05	0.74	129.96	1.56	202.96	4.000	No	No	2.00
3943	39.43	166.83	2.18	3.05	0.74	130.31	1.56	203.23	4.000	No	No	2.00
3944	39.44	167.20	2.18	3.05	0.74	130.58	1.56	203.50	4.000	No	No	2.00
3945	39.45	167.53	2.18	3.05	0.74	130.81	1.56	203.82	4.000	No	No	2.00
3946	39.46	167.84	2.18	3.06	0.74	131.03	1.56	204.22	4.000	No	No	2.00
3947	39.47	168.20	2.18	3.06	0.74	131.29	1.56	204.71	4.000	No	No	2.00
3948	39.48	168.59	2.18	3.07	0.74	131.56	1.56	205.24	4.000	No	No	2.00
3949	39.49	168.99	2.18	3.08	0.74	131.85	1.56	205.79	4.000	No	No	2.00
3950	39.50	169.38	2.18	3.09	0.74	132.13	1.56	206.32	4.000	No	No	2.00
3951	39.51	169.74	2.18	3.09	0.74	132.38	1.56	206.81	4.000	No	No	2.00
3952	39.52	170.05	2.18	3.10	0.74	132.59	1.56	207.23	4.000	No	No	2.00
3953	39.53	170.25	2.18	3.11	0.74	132.71	1.56	207.59	4.000	No	No	2.00
3954	39.54	170.36	2.18	3.12	0.74	132.77	1.57	207.95	4.000	No	No	2.00
3955	39.55	170.43	2.18	3.13	0.74	132.77	1.57	208.35	4.000	No	No	2.00
3956	39.56	170.50	2.18	3.14	0.75	132.79	1.57	208.82	4.000	No	No	2.00
3957	39.57	170.58	2.18	3.16	0.75	132.80	1.58	209.32	4.000	No	No	2.00
3958	39.58	170.66	2.19	3.17	0.75	132.82	1.58	209.82	4.000	No	No	2.00
3959	39.59	170.74	2.19	3.19	0.75	132.83	1.58	210.30	4.000	No	No	2.00
3960	39.60	170.81	2.19	3.20	0.75	132.85	1.59	210.74	4.000	No	No	2.00
3961	39.61	170.88	2.19	3.21	0.75	132.86	1.59	210.99	4.000	No	No	2.00
3962	39.62	170.96	2.19	3.20	0.75	132.90	1.59	210.91	4.000	No	No	2.00
3963	39.63	171.07	2.19	3.19	0.75	132.99	1.58	210.48	4.000	No	No	2.00
3964	39.64	171.21	2.18	3.17	0.75	133.10	1.58	209.83	4.000	No	No	2.00
3965	39.65	171.36	2.18	3.14	0.75	133.23	1.57	209.12	4.000	No	No	2.00
3966	39.66	171.52	2.18	3.11	0.74	133.36	1.56	208.38	4.000	No	No	2.00
3967	39.67	171.67	2.18	3.09	0.74	133.50	1.56	207.66	4.000	No	No	2.00
3968	39.68	171.82	2.17	3.06	0.74	133.63	1.55	206.99	4.000	No	No	2.00
3969	39.69	171.95	2.17	3.04	0.74	133.74	1.54	206.39	4.000	No	No	2.00
3970	39.70	172.07	2.17	3.02	0.74	133.83	1.54	205.89	4.000	No	No	2.00
3971	39.71	172.18	2.16	3.01	0.74	133.91	1.53	205.41	4.000	No	No	2.00
3972	39.72	172.30	2.16	2.99	0.74	134.01	1.53	204.91	4.000	No	No	2.00
3973	39.73	172.45	2.16	2.96	0.74	134.13	1.52	204.34	4.000	No	No	2.00
3974	39.74	172.60	2.16	2.94	0.74	134.26	1.52	203.73	4.000	No	No	2.00
3975	39.75	172.76	2.15	2.92	0.73	134.40	1.51	203.10	4.000	No	No	2.00
3976	39.76	172.92	2.15	2.89	0.73	134.54	1.51	202.50	4.000	No	No	2.00
3977	39.77	173.06	2.15	2.87	0.73	134.66	1.50	201.95	4.000	No	No	2.00
3978	39.78	173.17	2.15	2.85	0.73	134.74	1.50	201.49	4.000	No	No	2.00
3979	39.79	173.13	2.14	2.84	0.73	134.70	1.49	201.17	4.000	No	No	2.00
3980	39.80	172.93	2.14	2.84	0.73	134.51	1.49	200.96	4.000	No	No	2.00
3981	39.81	172.58	2.15	2.85	0.73	134.19	1.50	200.81	4.000	No	No	2.00
3982	39.82	172.18	2.15	2.85	0.73	133.83	1.50	200.64	4.000	No	No	2.00
3983	39.83	171.76	2.15	2.86	0.73	133.45	1.50	200.46	4.000	No	No	2.00
3984	39.84	171.33	2.15	2.87	0.73	133.07	1.51	200.28	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3985	39.85	170.92	2.15	2.87	0.73	132.70	1.51	200.11	4.000	No	No	2.00
3986	39.86	170.55	2.15	2.88	0.73	132.37	1.51	199.96	0.824	No	No	0.94
3987	39.87	170.19	2.16	2.89	0.74	132.03	1.51	199.85	0.822	No	No	0.94
3988	39.88	169.71	2.16	2.90	0.74	131.60	1.52	199.80	0.822	No	No	0.94
3989	39.89	169.05	2.16	2.92	0.74	131.01	1.53	199.83	0.822	No	No	0.94
3990	39.90	168.22	2.17	2.94	0.74	130.28	1.53	199.90	0.823	No	No	0.94
3991	39.91	167.30	2.17	2.97	0.74	129.47	1.54	199.99	0.824	No	No	0.94
3992	39.92	166.34	2.18	3.00	0.74	128.63	1.56	200.10	4.000	No	No	2.00
3993	39.93	165.39	2.18	3.03	0.75	127.80	1.57	200.22	4.000	No	No	2.00
3994	39.94	164.50	2.18	3.05	0.75	127.02	1.58	200.34	4.000	No	No	2.00
3995	39.95	163.71	2.19	3.08	0.75	126.32	1.59	200.46	4.000	No	No	2.00
3996	39.96	163.15	2.19	3.10	0.75	125.82	1.59	200.67	4.000	No	No	2.00
3997	39.97	162.77	2.20	3.12	0.75	125.46	1.60	201.04	4.000	No	No	2.00
3998	39.98	162.53	2.20	3.14	0.75	125.20	1.61	201.62	4.000	No	No	2.00
3999	39.99	162.26	2.20	3.17	0.75	124.92	1.62	202.31	4.000	No	No	2.00
4000	40.00	161.98	2.21	3.20	0.76	124.63	1.63	203.08	4.000	No	No	2.00
4001	40.01	161.68	2.21	3.24	0.76	124.33	1.64	203.87	4.000	No	No	2.00
4002	40.02	161.40	2.21	3.27	0.76	124.03	1.65	204.66	4.000	No	No	2.00
4003	40.03	161.14	2.22	3.30	0.76	123.76	1.66	205.38	4.000	No	No	2.00
4004	40.04	160.96	2.22	3.32	0.76	123.56	1.67	205.98	4.000	No	No	2.00
4005	40.05	161.13	2.22	3.33	0.76	123.66	1.67	206.34	4.000	No	No	2.00
4006	40.06	161.68	2.22	3.32	0.76	124.08	1.66	206.51	4.000	No	No	2.00
4007	40.07	162.61	2.22	3.30	0.76	124.82	1.65	206.55	4.000	No	No	2.00
4008	40.08	163.65	2.21	3.28	0.76	125.66	1.64	206.62	4.000	No	No	2.00
4009	40.09	164.76	2.21	3.26	0.76	126.55	1.63	206.69	4.000	No	No	2.00
4010	40.10	165.88	2.20	3.24	0.75	127.44	1.62	206.77	4.000	No	No	2.00
4011	40.11	166.95	2.20	3.21	0.75	128.30	1.61	206.86	4.000	No	No	2.00
4012	40.12	167.91	2.20	3.19	0.75	129.07	1.60	206.94	4.000	No	No	2.00
4013	40.13	168.71	2.19	3.18	0.75	129.71	1.60	206.96	4.000	No	No	2.00
4014	40.14	169.40	2.19	3.16	0.75	130.26	1.59	206.86	4.000	No	No	2.00
4015	40.15	170.08	2.19	3.14	0.75	130.80	1.58	206.62	4.000	No	No	2.00
4016	40.16	170.84	2.18	3.11	0.75	131.43	1.57	206.31	4.000	No	No	2.00
4017	40.17	171.68	2.18	3.08	0.74	132.12	1.56	205.98	4.000	No	No	2.00
4018	40.18	172.56	2.17	3.05	0.74	132.84	1.55	205.64	4.000	No	No	2.00
4019	40.19	173.43	2.17	3.01	0.74	133.56	1.54	205.33	4.000	No	No	2.00
4020	40.20	174.25	2.16	2.98	0.74	134.23	1.53	205.04	4.000	No	No	2.00
4021	40.21	174.97	2.16	2.96	0.74	134.82	1.52	204.80	4.000	No	No	2.00
4022	40.22	175.43	2.15	2.94	0.74	135.19	1.51	204.58	4.000	No	No	2.00
4023	40.23	175.65	2.15	2.93	0.74	135.36	1.51	204.37	4.000	No	No	2.00
4024	40.24	175.67	2.15	2.92	0.73	135.36	1.51	204.12	4.000	No	No	2.00
4025	40.25	175.67	2.15	2.91	0.73	135.35	1.51	203.84	4.000	No	No	2.00
4026	40.26	175.67	2.15	2.90	0.73	135.34	1.50	203.55	4.000	No	No	2.00
4027	40.27	175.67	2.15	2.89	0.73	135.32	1.50	203.24	4.000	No	No	2.00
4028	40.28	175.67	2.15	2.88	0.73	135.31	1.50	202.95	4.000	No	No	2.00
4029	40.29	175.67	2.15	2.87	0.73	135.30	1.50	202.67	4.000	No	No	2.00
4030	40.30	175.66	2.15	2.87	0.73	135.27	1.50	202.43	4.000	No	No	2.00
4031	40.31	175.62	2.15	2.86	0.73	135.22	1.50	202.18	4.000	No	No	2.00
4032	40.32	175.53	2.14	2.85	0.73	135.13	1.49	201.89	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
4033	40.33	175.40	2.14	2.85	0.73	135.01	1.49	201.53	4.000	No	No	2.00
4034	40.34	175.25	2.14	2.84	0.73	134.88	1.49	201.13	4.000	No	No	2.00
4035	40.35	175.09	2.14	2.83	0.73	134.74	1.49	200.71	4.000	No	No	2.00
4036	40.36	174.93	2.14	2.82	0.73	134.60	1.49	200.29	4.000	No	No	2.00
4037	40.37	174.78	2.14	2.81	0.73	134.46	1.49	199.89	0.823	No	No	0.95
4038	40.38	174.64	2.14	2.80	0.73	134.34	1.49	199.52	0.819	No	No	0.94
4039	40.39	174.50	2.14	2.79	0.73	134.22	1.48	199.19	0.815	No	No	0.94
4040	40.40	174.34	2.14	2.79	0.73	134.06	1.48	198.85	0.811	No	No	0.93
4041	40.41	174.11	2.14	2.78	0.73	133.87	1.48	198.45	0.807	No	No	0.93
4042	40.42	173.83	2.14	2.77	0.73	133.63	1.48	197.97	0.802	No	No	0.92
4043	40.43	173.53	2.14	2.76	0.73	133.37	1.48	197.45	0.796	No	No	0.92
4044	40.44	173.21	2.14	2.75	0.73	133.11	1.48	196.91	0.790	No	No	0.91
4045	40.45	172.89	2.14	2.74	0.73	132.84	1.48	196.37	0.784	No	No	0.90
4046	40.46	172.59	2.14	2.74	0.73	132.59	1.48	195.87	0.779	No	No	0.90
4047	40.47	172.33	2.14	2.73	0.73	132.37	1.48	195.43	0.774	No	No	0.89
4048	40.48	172.09	2.14	2.72	0.73	132.16	1.48	195.06	0.770	No	No	0.89
4049	40.49	171.83	2.14	2.72	0.73	131.93	1.48	194.72	0.767	No	No	0.88
4050	40.50	171.52	2.14	2.72	0.73	131.65	1.48	194.38	0.763	No	No	0.88
4051	40.51	171.15	2.14	2.71	0.73	131.34	1.48	193.99	0.759	No	No	0.87
4052	40.52	170.76	2.14	2.71	0.73	131.01	1.48	193.58	0.755	No	No	0.87
4053	40.53	170.36	2.14	2.71	0.73	130.67	1.48	193.15	0.750	No	No	0.86
4054	40.54	169.97	2.14	2.70	0.73	130.33	1.48	192.74	0.746	No	No	0.86
4055	40.55	169.61	2.14	2.70	0.73	130.02	1.48	192.35	0.742	No	No	0.85
4056	40.56	169.29	2.14	2.70	0.73	129.74	1.48	192.01	0.738	No	No	0.85
4057	40.57	168.90	2.14	2.70	0.73	129.41	1.48	191.65	0.735	No	No	0.85
4058	40.58	168.39	2.14	2.70	0.73	128.97	1.48	191.21	0.730	No	No	0.84
4059	40.59	167.73	2.14	2.70	0.73	128.42	1.48	190.67	0.725	No	No	0.83
4060	40.60	166.98	2.14	2.70	0.73	127.79	1.49	190.07	0.719	No	No	0.83
4061	40.61	166.18	2.14	2.70	0.73	127.13	1.49	189.43	0.712	No	No	0.82
4062	40.62	165.39	2.14	2.70	0.73	126.47	1.49	188.79	0.706	No	No	0.81
4063	40.63	164.62	2.15	2.70	0.73	125.83	1.50	188.18	0.700	No	No	0.81
4064	40.64	163.94	2.15	2.70	0.73	125.26	1.50	187.63	0.694	No	No	0.80
4065	40.65	163.33	2.15	2.70	0.73	124.75	1.50	187.14	0.690	No	No	0.79
4066	40.66	162.68	2.15	2.70	0.73	124.21	1.50	186.63	0.684	No	No	0.79
4067	40.67	161.93	2.15	2.70	0.74	123.58	1.51	186.02	0.679	No	No	0.78
4068	40.68	161.02	2.15	2.70	0.74	122.83	1.51	185.31	0.672	No	No	0.77
4069	40.69	160.02	2.15	2.70	0.74	122.01	1.51	184.53	0.664	No	No	0.77
4070	40.70	158.98	2.16	2.70	0.74	121.15	1.52	183.72	0.657	No	No	0.76
4071	40.71	157.95	2.16	2.70	0.74	120.31	1.52	182.92	0.649	No	No	0.75
4072	40.72	156.99	2.16	2.70	0.74	119.52	1.52	182.18	0.642	No	No	0.74
4073	40.73	156.15	2.16	2.70	0.74	118.82	1.53	181.52	0.636	No	No	0.73
4074	40.74	155.38	2.16	2.70	0.74	118.18	1.53	181.01	0.632	No	No	0.73
4075	40.75	154.58	2.17	2.71	0.74	117.51	1.54	180.58	0.628	No	No	0.72
4076	40.76	153.64	2.17	2.72	0.74	116.72	1.54	180.19	0.624	No	No	0.72
4077	40.77	152.55	2.17	2.74	0.74	115.81	1.55	179.74	0.620	No	No	0.72
4078	40.78	151.37	2.18	2.75	0.75	114.83	1.56	179.28	0.616	No	No	0.71
4079	40.79	150.17	2.18	2.77	0.75	113.83	1.57	178.81	0.612	No	No	0.71
4080	40.80	149.00	2.19	2.78	0.75	112.86	1.58	178.36	0.608	No	No	0.70

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4081	40.81	147.93	2.19	2.79	0.75	111.97	1.59	177.96	0.604	No	No	0.70
4082	40.82	147.00	2.19	2.81	0.75	111.20	1.60	177.60	0.601	No	No	0.69
4083	40.83	146.10	2.20	2.81	0.75	110.45	1.60	177.19	0.597	No	No	0.69
4084	40.84	145.10	2.20	2.82	0.75	109.62	1.61	176.69	0.593	No	No	0.68
4085	40.85	143.90	2.20	2.83	0.76	108.64	1.62	176.06	0.588	No	No	0.68
4086	40.86	142.55	2.21	2.84	0.76	107.53	1.63	175.36	0.581	No	No	0.67
4087	40.87	141.12	2.21	2.85	0.76	106.37	1.64	174.62	0.575	No	No	0.66
4088	40.88	139.69	2.22	2.86	0.76	105.20	1.65	173.89	0.569	No	No	0.66
4089	40.89	138.32	2.22	2.87	0.76	104.08	1.66	173.21	0.563	No	No	0.65
4090	40.90	137.09	2.22	2.88	0.76	103.08	1.67	172.59	0.558	No	No	0.64
4091	40.91	136.02	2.23	2.88	0.76	102.21	1.68	171.99	0.553	No	No	0.64
4092	40.92	134.96	2.23	2.88	0.77	101.35	1.69	171.27	0.547	No	No	0.63
4093	40.93	133.78	2.23	2.88	0.77	100.40	1.70	170.33	0.540	No	No	0.62
4094	40.94	132.38	2.23	2.88	0.77	99.28	1.70	169.17	0.530	No	No	0.61
4095	40.95	130.83	2.24	2.87	0.77	98.06	1.71	167.91	0.520	No	No	0.60
4096	40.96	129.23	2.24	2.86	0.77	96.78	1.72	166.61	0.510	No	No	0.59
4097	40.97	127.66	2.24	2.86	0.77	95.53	1.73	165.33	0.500	No	No	0.58
4098	40.98	126.18	2.25	2.85	0.77	94.35	1.74	164.13	0.491	No	No	0.57
4099	40.99	124.89	2.25	2.85	0.77	93.32	1.75	163.09	0.483	No	No	0.56
4100	41.00	123.77	2.25	2.85	0.77	92.43	1.76	162.22	0.477	No	No	0.55
4101	41.01	122.69	2.25	2.84	0.77	91.56	1.76	161.42	0.471	No	No	0.54
4102	41.02	121.48	2.26	2.84	0.78	90.60	1.77	160.58	4.000	Yes	No	2.00
4103	41.03	120.10	2.26	2.84	0.78	89.50	1.78	159.62	4.000	Yes	No	2.00
4104	41.04	118.61	2.26	2.84	0.78	88.31	1.80	158.60	4.000	Yes	No	2.00
4105	41.05	117.09	2.27	2.84	0.78	87.10	1.81	157.56	4.000	Yes	No	2.00
4106	41.06	115.61	2.27	2.84	0.78	85.92	1.82	156.55	4.000	Yes	No	2.00
4107	41.07	114.26	2.27	2.84	0.78	84.85	1.83	155.64	4.000	Yes	No	2.00
4108	41.08	113.09	2.28	2.84	0.78	83.91	1.85	154.86	4.000	Yes	No	2.00
4109	41.09	111.98	2.28	2.84	0.79	83.03	1.86	154.18	4.000	Yes	No	2.00
4110	41.10	110.78	2.29	2.84	0.79	82.07	1.87	153.50	4.000	Yes	No	2.00
4111	41.11	109.36	2.29	2.85	0.79	80.94	1.89	152.73	4.000	Yes	No	2.00
4112	41.12	107.76	2.30	2.85	0.79	79.67	1.91	151.88	4.000	Yes	No	2.00
4113	41.13	106.07	2.30	2.86	0.79	78.32	1.93	150.99	4.000	Yes	No	2.00
4114	41.14	104.38	2.31	2.87	0.80	76.98	1.95	150.10	4.000	Yes	No	2.00
4115	41.15	102.77	2.31	2.87	0.80	75.70	1.97	149.27	4.000	Yes	No	2.00
4116	41.16	101.32	2.32	2.88	0.80	74.56	1.99	148.53	4.000	Yes	No	2.00
4117	41.17	100.10	2.32	2.88	0.80	73.58	2.01	147.84	4.000	Yes	No	2.00
4118	41.18	98.96	2.33	2.88	0.80	72.68	2.02	147.07	4.000	Yes	No	2.00
4119	41.19	97.75	2.33	2.87	0.80	71.73	2.04	146.12	4.000	Yes	No	2.00
4120	41.20	96.34	2.33	2.86	0.81	70.63	2.05	144.97	4.000	Yes	No	2.00
4121	41.21	94.80	2.34	2.85	0.81	69.42	2.07	143.73	4.000	Yes	No	2.00
4122	41.22	93.20	2.34	2.84	0.81	68.18	2.09	142.44	4.000	Yes	No	2.00
4123	41.23	91.62	2.35	2.83	0.81	66.94	2.11	141.18	4.000	Yes	No	2.00
4124	41.24	90.15	2.35	2.82	0.81	65.79	2.13	140.01	4.000	Yes	No	2.00
4125	41.25	88.86	2.35	2.82	0.81	64.79	2.15	138.99	4.000	Yes	No	2.00
4126	41.26	87.86	2.36	2.81	0.81	64.01	2.16	138.33	4.000	Yes	No	2.00
4127	41.27	87.06	2.36	2.82	0.82	63.36	2.18	137.96	4.000	Yes	No	2.00
4128	41.28	86.30	2.36	2.83	0.82	62.76	2.20	137.83	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4129	41.29	85.45	2.37	2.84	0.82	62.08	2.22	137.68	4.000	Yes	No	2.00
4130	41.30	84.52	2.37	2.85	0.82	61.34	2.24	137.53	4.000	Yes	No	2.00
4131	41.31	83.58	2.38	2.86	0.82	60.59	2.27	137.37	4.000	Yes	No	2.00
4132	41.32	82.67	2.38	2.88	0.83	59.86	2.29	137.22	4.000	Yes	No	2.00
4133	41.33	81.84	2.39	2.89	0.83	59.20	2.32	137.09	4.000	Yes	No	2.00
4134	41.34	81.13	2.39	2.90	0.83	58.63	2.34	137.01	4.000	Yes	No	2.00
4135	41.35	80.52	2.40	2.91	0.83	58.14	2.36	137.11	4.000	Yes	No	2.00
4136	41.36	79.92	2.40	2.93	0.83	57.65	2.38	137.41	4.000	Yes	No	2.00
4137	41.37	79.25	2.41	2.96	0.83	57.11	2.41	137.87	4.000	Yes	No	2.00
4138	41.38	78.50	2.41	2.99	0.84	56.49	2.45	138.40	4.000	Yes	No	2.00
4139	41.39	77.70	2.42	3.03	0.84	55.85	2.49	138.94	4.000	Yes	No	2.00
4140	41.40	76.91	2.43	3.06	0.84	55.21	2.53	139.49	4.000	Yes	No	2.00
4141	41.41	76.15	2.43	3.09	0.84	54.59	2.56	140.01	4.000	Yes	No	2.00
4142	41.42	75.47	2.44	3.12	0.85	54.05	2.60	140.47	4.000	Yes	No	2.00
4143	41.43	74.90	2.45	3.14	0.85	53.58	2.63	140.88	4.000	Yes	No	2.00
4144	41.44	74.37	2.45	3.17	0.85	53.15	2.66	141.31	4.000	Yes	No	2.00
4145	41.45	73.80	2.46	3.20	0.85	52.69	2.69	141.81	4.000	Yes	No	2.00
4146	41.46	73.15	2.46	3.23	0.86	52.16	2.73	142.41	4.000	Yes	No	2.00
4147	41.47	72.44	2.47	3.27	0.86	51.59	2.77	143.07	4.000	Yes	No	2.00
4148	41.48	71.70	2.48	3.30	0.86	50.99	2.82	143.74	4.000	Yes	No	2.00
4149	41.49	70.97	2.48	3.34	0.86	50.40	2.86	144.39	4.000	Yes	No	2.00
4150	41.50	70.29	2.49	3.38	0.87	49.86	2.91	144.99	4.000	Yes	No	2.00
4151	41.51	69.70	2.50	3.41	0.87	49.38	2.95	145.51	4.000	Yes	No	2.00
4152	41.52	69.17	2.50	3.44	0.87	48.95	2.82	138.15	4.000	Yes	No	2.00
4153	41.53	68.64	2.51	3.48	0.87	48.52	2.95	142.95	4.000	Yes	No	2.00
4154	41.54	68.04	2.52	3.54	0.88	48.02	3.11	149.22	4.000	Yes	No	2.00
4155	41.55	67.34	2.52	3.60	0.88	47.46	3.30	156.67	4.000	Yes	No	2.00
4156	41.56	66.60	2.53	3.67	0.88	46.85	3.52	164.96	4.000	Yes	No	2.00
4157	41.57	65.84	2.54	3.74	0.89	46.23	3.76	173.73	4.000	Yes	No	2.00
4158	41.58	65.10	2.55	3.81	0.89	45.64	4.00	182.52	4.000	Yes	No	2.00
4159	41.59	64.43	2.56	3.87	0.89	45.10	4.23	190.84	4.000	Yes	No	2.00
4160	41.60	63.85	2.57	3.92	0.90	44.63	4.44	198.20	4.000	Yes	No	2.00
4161	41.61	63.29	2.58	3.97	0.90	44.18	4.64	205.11	4.000	Yes	No	2.00
4162	41.62	62.68	2.58	4.02	0.90	43.69	4.86	212.52	4.000	Yes	No	2.00
4163	41.63	61.96	2.59	4.08	0.90	43.12	5.14	221.40	4.000	Yes	No	2.00
4164	41.64	61.15	2.60	4.14	0.91	42.47	5.45	231.69	4.000	Yes	No	2.00
4165	41.65	60.29	2.61	4.21	0.91	41.80	5.81	242.95	4.000	Yes	No	2.00
4166	41.66	59.44	2.62	4.27	0.92	41.13	6.19	254.64	4.000	Yes	No	2.00
4167	41.67	58.62	2.63	4.34	0.92	40.49	6.57	266.17	4.000	Yes	No	2.00
4168	41.68	57.90	2.64	4.40	0.92	39.92	6.94	276.84	4.000	Yes	No	2.00
4169	41.69	57.29	2.65	4.45	0.93	39.44	7.26	286.28	4.000	Yes	No	2.00
4170	41.70	56.73	2.65	4.49	0.93	39.00	7.58	295.52	4.000	Yes	No	2.00
4171	41.71	56.15	2.66	4.55	0.93	38.54	7.93	305.81	4.000	Yes	No	2.00
4172	41.72	55.48	2.67	4.61	0.93	38.01	8.37	318.16	4.000	Yes	No	2.00
4173	41.73	54.74	2.68	4.68	0.94	37.44	8.87	332.14	4.000	Yes	No	2.00
4174	41.74	53.98	2.69	4.75	0.94	36.85	9.42	347.12	4.000	Yes	No	2.00
4175	41.75	53.24	2.70	4.83	0.94	36.27	9.99	362.39	4.000	Yes	No	2.00
4176	41.76	52.54	2.71	4.89	0.95	35.72	4.77	170.33	4.000	Yes	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _k (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4177	41.77	51.93	2.71	4.95	0.95	35.25	4.85	170.99	4.000	Yes	Yes	2.00
4178	41.78	51.42	2.72	5.01	0.95	34.85	4.92	171.65	4.000	Yes	Yes	2.00
4179	41.79	50.95	2.73	5.07	0.96	34.48	5.00	172.42	4.000	Yes	Yes	2.00
4180	41.80	50.44	2.74	5.14	0.96	34.08	5.09	173.39	4.000	Yes	Yes	2.00
4181	41.81	49.85	2.74	5.22	0.96	33.62	5.19	174.47	4.000	Yes	Yes	2.00
4182	41.82	49.22	2.75	5.31	0.97	33.13	5.30	175.58	4.000	Yes	Yes	2.00
4183	41.83	48.58	2.76	5.40	0.97	32.63	5.41	176.67	4.000	Yes	Yes	2.00
4184	41.84	47.96	2.77	5.48	0.97	32.15	5.53	177.67	4.000	Yes	Yes	2.00
4185	41.85	47.40	2.78	5.56	0.98	31.71	5.63	178.55	4.000	Yes	Yes	2.00
4186	41.86	46.94	2.79	5.63	0.98	31.35	5.72	179.29	4.000	Yes	Yes	2.00
4187	41.87	46.59	2.80	5.69	0.98	31.08	5.79	180.05	4.000	Yes	Yes	2.00
4188	41.88	46.32	2.80	5.76	0.98	30.86	5.86	180.93	4.000	Yes	Yes	2.00
4189	41.89	46.05	2.81	5.83	0.99	30.64	5.94	182.00	4.000	Yes	Yes	2.00
4190	41.90	45.74	2.81	5.92	0.99	30.40	6.03	183.18	4.000	Yes	Yes	2.00
4191	41.91	45.42	2.82	6.00	0.99	30.14	6.12	184.38	4.000	Yes	Yes	2.00
4192	41.92	45.11	2.83	6.09	1.00	29.89	6.21	185.57	4.000	Yes	Yes	2.00
4193	41.93	44.81	2.83	6.18	1.00	29.65	6.30	186.66	4.000	Yes	Yes	2.00
4194	41.94	44.54	2.84	6.25	1.00	29.43	6.37	187.62	4.000	Yes	Yes	2.00
4195	41.95	44.36	2.84	6.30	1.00	29.30	6.43	188.36	4.000	Yes	Yes	2.00
4196	41.96	44.30	2.85	6.34	1.00	29.25	6.46	188.87	1.395	No	Yes	1.62
4197	41.97	44.34	2.85	6.35	1.00	29.27	6.47	189.23	1.396	No	Yes	1.63
4198	41.98	44.41	2.85	6.37	1.00	29.31	6.47	189.60	1.398	No	Yes	1.63
4199	41.99	44.48	2.85	6.38	1.00	29.36	6.47	190.01	1.400	No	Yes	1.63
4200	42.00	44.56	2.85	6.40	1.00	29.41	6.48	190.43	1.403	No	Yes	1.63
4201	42.01	44.64	2.85	6.41	1.00	29.45	6.48	190.84	1.405	No	Yes	1.64
4202	42.02	44.72	2.85	6.43	1.00	29.50	6.48	191.23	1.407	No	Yes	1.64
4203	42.03	44.78	2.85	6.44	1.00	29.54	6.49	191.55	1.409	No	Yes	1.64
4204	42.04	44.98	2.85	6.43	1.00	29.67	6.46	191.60	1.415	No	Yes	1.65
4205	42.05	45.36	2.84	6.38	1.00	29.92	6.39	191.34	1.427	No	Yes	1.66
4206	42.06	45.93	2.83	6.31	1.00	30.34	6.29	190.81	1.447	No	Yes	1.69
4207	42.07	46.60	2.82	6.22	0.99	30.83	6.17	190.18	1.471	No	Yes	1.71
4208	42.08	47.30	2.82	6.13	0.99	31.35	6.04	189.44	1.495	No	Yes	1.74
4209	42.09	48.02	2.81	6.03	0.99	31.89	5.92	188.65	1.521	No	Yes	1.77
4210	42.10	48.72	2.80	5.94	0.98	32.40	5.80	187.83	1.546	No	Yes	1.80
4211	42.11	49.35	2.79	5.86	0.98	32.87	5.69	187.04	1.568	No	Yes	1.83
4212	42.12	49.92	2.78	5.78	0.98	33.29	5.60	186.28	1.588	No	Yes	1.85
4213	42.13	50.55	2.77	5.70	0.97	33.76	5.49	185.34	1.610	No	Yes	1.88
4214	42.14	51.31	2.76	5.60	0.97	34.33	5.36	184.09	1.637	No	Yes	1.91
4215	42.15	52.26	2.75	5.46	0.96	35.04	5.21	182.43	1.672	No	Yes	1.95
4216	42.16	53.32	2.73	5.32	0.96	35.84	5.03	180.46	1.710	No	Yes	1.99
4217	42.17	54.43	2.71	5.17	0.95	36.69	4.86	178.27	1.750	No	Yes	2.00
4218	42.18	55.55	2.70	5.01	0.95	37.54	10.06	377.82	3.600	No	No	2.00
4219	42.19	56.60	2.68	4.87	0.94	38.34	9.14	350.57	3.600	No	No	2.00
4220	42.20	57.54	2.67	4.74	0.93	39.06	8.38	327.52	3.600	No	No	2.00
4221	42.21	58.32	2.66	4.64	0.93	39.67	7.79	309.19	3.600	No	No	2.00
4222	42.22	59.04	2.65	4.54	0.93	40.21	7.29	293.30	3.600	No	No	2.00
4223	42.23	59.77	2.64	4.45	0.92	40.78	6.81	277.52	3.600	No	No	2.00
4224	42.24	60.63	2.62	4.34	0.92	41.44	6.28	260.11	3.600	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
4225	42.25	61.56	2.61	4.22	0.91	42.16	5.74	241.98	3.600	No	No	2.00
4226	42.26	62.52	2.59	4.09	0.91	42.91	5.22	224.19	4.000	No	No	2.00
4227	42.27	63.46	2.58	3.97	0.90	43.65	4.76	207.62	4.000	No	No	2.00
4228	42.28	64.33	2.57	3.86	0.90	44.34	4.35	192.99	0.748	No	No	0.87
4229	42.29	65.09	2.55	3.76	0.89	44.93	4.03	180.95	0.631	No	No	0.74
4230	42.30	65.65	2.55	3.69	0.89	45.37	3.80	172.52	0.558	No	No	0.65
4231	42.31	66.09	2.54	3.64	0.89	45.71	3.64	166.47	0.509	No	No	0.59
4232	42.32	66.47	2.53	3.60	0.88	46.01	3.51	161.54	0.472	No	No	0.55
4233	42.33	66.92	2.53	3.55	0.88	46.35	3.37	156.03	0.433	No	No	0.51
4234	42.34	67.39	2.52	3.50	0.88	46.72	3.22	150.27	0.396	No	No	0.46
4235	42.35	67.87	2.51	3.45	0.88	47.10	3.07	144.57	0.361	No	No	0.42
4236	42.36	68.33	2.51	3.40	0.87	47.46	2.93	139.23	0.331	No	No	0.39
4237	42.37	68.75	2.50	3.35	0.87	47.78	2.81	134.48	0.306	No	No	0.36
4238	42.38	69.04	2.50	3.32	0.87	48.00	2.95	141.71	0.345	No	No	0.40
4239	42.39	69.05	2.49	3.30	0.87	48.02	2.94	141.26	0.342	No	No	0.40
4240	42.40	68.80	2.50	3.31	0.87	47.81	2.95	141.14	0.341	No	No	0.40
4241	42.41	68.36	2.50	3.32	0.87	47.47	2.97	141.18	0.342	No	No	0.40
4242	42.42	67.87	2.50	3.33	0.87	47.09	2.86	134.64	0.307	No	No	0.36
4243	42.43	67.36	2.51	3.34	0.87	46.69	2.93	136.96	0.319	No	No	0.37
4244	42.44	66.85	2.51	3.35	0.87	46.29	3.01	139.32	0.331	No	No	0.39
4245	42.45	66.36	2.51	3.37	0.88	45.91	3.08	141.59	0.344	No	No	0.40
4246	42.46	65.93	2.52	3.38	0.88	45.57	3.15	143.65	0.356	No	No	0.42
4247	42.47	65.49	2.52	3.40	0.88	45.23	3.24	146.41	0.372	No	No	0.43
4248	42.48	64.95	2.53	3.43	0.88	44.80	3.37	150.84	0.399	No	No	0.47
4249	42.49	64.24	2.54	3.48	0.88	44.23	3.56	157.57	0.444	No	No	0.52
4250	42.50	63.39	2.55	3.55	0.89	43.56	3.81	166.12	0.506	No	No	0.59
4251	42.51	62.46	2.56	3.62	0.89	42.82	4.11	175.85	0.586	No	No	0.69
4252	42.52	61.49	2.57	3.69	0.90	42.07	4.43	186.35	0.682	No	No	0.80
4253	42.53	60.55	2.58	3.76	0.90	41.34	4.77	197.10	0.792	No	No	0.93
4254	42.54	59.68	2.59	3.83	0.91	40.65	5.10	207.51	4.000	No	No	2.00
4255	42.55	58.92	2.60	3.89	0.91	40.06	5.41	216.92	3.600	No	No	2.00
4256	42.56	58.24	2.61	3.94	0.91	39.53	5.71	225.75	3.600	No	No	2.00
4257	42.57	57.54	2.62	3.99	0.92	38.98	6.03	235.21	3.600	No	No	2.00
4258	42.58	56.73	2.63	4.06	0.92	38.35	6.43	246.63	3.600	No	No	2.00
4259	42.59	55.80	2.64	4.13	0.92	37.64	6.91	260.19	3.600	No	No	2.00
4260	42.60	54.81	2.65	4.21	0.93	36.88	7.47	275.36	3.600	No	No	2.00
4261	42.61	53.80	2.66	4.30	0.93	36.11	8.07	291.48	3.600	No	No	2.00
4262	42.62	52.84	2.67	4.37	0.94	35.37	8.70	307.74	3.600	No	No	2.00
4263	42.63	51.96	2.69	4.45	0.94	34.70	9.31	323.19	3.600	No	No	2.00
4264	42.64	51.22	2.69	4.50	0.95	34.13	9.85	336.21	3.600	No	No	2.00
4265	42.65	50.56	2.70	4.54	0.95	33.64	4.73	158.95	1.604	No	Yes	1.88
4266	42.66	49.90	2.71	4.57	0.95	33.14	4.79	158.80	1.581	No	Yes	1.85
4267	42.67	49.15	2.71	4.59	0.95	32.58	4.86	158.45	1.554	No	Yes	1.82
4268	42.68	48.32	2.72	4.61	0.96	31.96	4.94	158.05	1.525	No	Yes	1.79
4269	42.69	47.44	2.73	4.63	0.96	31.31	5.03	157.60	1.494	No	Yes	1.75
4270	42.70	46.56	2.74	4.66	0.96	30.67	5.12	157.13	1.463	No	Yes	1.71
4271	42.71	45.74	2.75	4.68	0.97	30.06	5.21	156.67	1.434	No	Yes	1.68
4272	42.72	45.01	2.75	4.70	0.97	29.51	5.29	156.23	1.408	No	Yes	1.65

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _k (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4273	42.73	44.50	2.76	4.71	0.97	29.14	5.34	155.73	1.390	No	Yes	1.63
4274	42.74	44.22	2.76	4.69	0.97	28.94	5.36	155.05	1.380	No	Yes	1.62
4275	42.75	44.12	2.76	4.65	0.97	28.87	5.34	154.10	1.377	No	Yes	1.61
4276	42.76	44.05	2.75	4.60	0.97	28.82	5.31	152.96	1.375	No	Yes	1.61
4277	42.77	43.97	2.75	4.55	0.97	28.77	5.27	151.71	1.372	No	Yes	1.61
4278	42.78	43.89	2.75	4.49	0.97	28.72	5.24	150.42	1.370	No	Yes	1.61
4279	42.79	43.81	2.75	4.44	0.96	28.67	5.20	149.16	1.367	No	Yes	1.60
4280	42.80	43.74	2.74	4.39	0.96	28.62	5.17	147.99	1.365	No	Yes	1.60
4281	42.81	43.70	2.74	4.34	0.96	28.59	5.14	146.98	1.364	No	Yes	1.60
4282	42.82	43.91	2.73	4.30	0.96	28.75	5.08	146.19	1.371	No	Yes	1.61
4283	42.83	44.43	2.73	4.24	0.96	29.14	4.99	145.52	1.390	No	Yes	1.63
4284	42.84	45.28	2.72	4.17	0.95	29.76	4.87	144.82	1.420	No	Yes	1.67
4285	42.85	46.24	2.70	4.09	0.95	30.47	4.72	143.96	1.454	No	Yes	1.71
4286	42.86	47.26	2.69	4.00	0.94	31.24	9.42	294.34	3.600	No	No	2.00
4287	42.87	48.30	2.67	3.92	0.94	32.01	8.62	275.95	3.600	No	No	2.00
4288	42.88	49.30	2.66	3.83	0.93	32.76	7.91	259.21	3.600	No	No	2.00
4289	42.89	50.21	2.65	3.76	0.93	33.43	7.32	244.78	3.600	No	No	2.00
4290	42.90	50.99	2.64	3.70	0.92	34.02	6.86	233.31	3.600	No	No	2.00
4291	42.91	51.74	2.63	3.65	0.92	34.57	6.48	223.98	3.600	No	No	2.00
4292	42.92	52.55	2.62	3.61	0.92	35.17	6.12	215.42	3.600	No	No	2.00
4293	42.93	53.51	2.61	3.57	0.91	35.89	5.75	206.27	3.600	No	No	2.00
4294	42.94	54.58	2.60	3.52	0.91	36.68	5.36	196.56	0.786	No	No	0.92
4295	42.95	55.69	2.59	3.47	0.90	37.51	4.98	186.88	0.687	No	No	0.81
4296	42.96	56.80	2.58	3.42	0.90	38.34	4.64	177.71	0.602	No	No	0.71
4297	42.97	57.85	2.57	3.38	0.90	39.12	4.33	169.46	0.533	No	No	0.63
4298	42.98	58.78	2.56	3.34	0.89	39.81	4.08	162.46	0.479	No	No	0.56
4299	42.99	59.45	2.55	3.31	0.89	40.31	3.92	157.99	0.447	No	No	0.52
4300	43.00	59.89	2.55	3.31	0.89	40.63	3.84	155.90	0.432	No	No	0.51
4301	43.01	60.17	2.55	3.31	0.89	40.83	3.81	155.70	0.431	No	No	0.51
4302	43.02	60.46	2.55	3.32	0.89	41.02	3.80	155.87	0.432	No	No	0.51
4303	43.03	60.77	2.55	3.33	0.89	41.24	3.78	156.05	0.433	No	No	0.51
4304	43.04	61.09	2.54	3.35	0.89	41.46	3.77	156.24	0.435	No	No	0.51
4305	43.05	61.41	2.54	3.36	0.89	41.68	3.75	156.43	0.436	No	No	0.51
4306	43.06	61.70	2.54	3.37	0.89	41.88	3.74	156.61	0.437	No	No	0.51
4307	43.07	61.94	2.54	3.38	0.89	42.04	3.73	156.90	0.439	No	No	0.52
4308	43.08	62.06	2.54	3.40	0.89	42.12	3.76	158.42	0.450	No	No	0.53
4309	43.09	62.08	2.55	3.43	0.89	42.10	3.84	161.51	0.472	No	No	0.55
4310	43.10	62.02	2.55	3.48	0.89	42.02	3.96	166.33	0.508	No	No	0.60
4311	43.11	61.94	2.56	3.53	0.89	41.94	4.10	171.88	0.552	No	No	0.65
4312	43.12	61.87	2.56	3.59	0.90	41.84	4.25	177.91	0.604	No	No	0.71
4313	43.13	61.79	2.57	3.65	0.90	41.75	4.41	184.12	0.660	No	No	0.78
4314	43.14	61.71	2.57	3.71	0.90	41.66	4.57	190.19	0.720	No	No	0.85
4315	43.15	61.64	2.58	3.76	0.90	41.58	4.71	195.78	0.778	No	No	0.92
4316	43.16	61.58	2.58	3.80	0.90	41.51	4.83	200.66	4.000	No	No	2.00
4317	43.17	61.53	2.59	3.84	0.90	41.44	4.96	205.35	4.000	No	No	2.00
4318	43.18	61.47	2.59	3.89	0.91	41.37	5.09	210.47	4.000	No	No	2.00
4319	43.19	61.40	2.60	3.94	0.91	41.29	5.25	216.56	4.000	No	No	2.00
4320	43.20	61.32	2.60	4.00	0.91	41.20	5.42	223.43	3.600	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4321	43.21	61.24	2.61	4.06	0.91	41.11	5.61	230.73	3.600	No	No	2.00
4322	43.22	61.17	2.61	4.12	0.91	41.02	5.81	238.11	3.600	No	No	2.00
4323	43.23	61.09	2.62	4.18	0.92	40.93	5.99	245.18	3.600	No	No	2.00
4324	43.24	61.03	2.62	4.23	0.92	40.85	6.16	251.53	3.600	No	No	2.00
4325	43.25	60.99	2.62	4.27	0.92	40.80	6.27	255.90	3.600	No	No	2.00
4326	43.26	60.99	2.62	4.29	0.92	40.79	6.33	258.25	3.600	No	No	2.00
4327	43.27	61.03	2.62	4.29	0.92	40.80	6.35	259.00	3.600	No	No	2.00
4328	43.28	61.08	2.63	4.30	0.92	40.83	6.36	259.53	3.600	No	No	2.00
4329	43.29	61.13	2.63	4.31	0.92	40.85	6.37	260.11	3.600	No	No	2.00
4330	43.30	61.18	2.63	4.31	0.92	40.88	6.38	260.70	3.600	No	No	2.00
4331	43.31	61.23	2.63	4.32	0.92	40.91	6.39	261.28	3.600	No	No	2.00
4332	43.32	61.28	2.63	4.33	0.92	40.93	6.40	261.82	3.600	No	No	2.00
4333	43.33	61.33	2.63	4.33	0.92	40.96	6.40	262.05	3.600	No	No	2.00
4334	43.34	61.46	2.62	4.32	0.92	41.05	6.34	260.16	4.000	Yes	No	2.00
4335	43.35	61.70	2.62	4.29	0.92	41.22	6.20	255.72	4.000	Yes	No	2.00
4336	43.36	62.04	2.62	4.24	0.92	41.48	6.00	248.80	4.000	Yes	No	2.00
4337	43.37	62.44	2.61	4.19	0.91	41.77	5.77	241.09	4.000	Yes	No	2.00
4338	43.38	62.85	2.60	4.13	0.91	42.09	5.54	233.07	4.000	Yes	No	2.00
4339	43.39	63.28	2.60	4.08	0.91	42.41	5.31	225.14	4.000	Yes	No	2.00
4340	43.40	63.68	2.59	4.02	0.91	42.72	5.10	217.72	4.000	Yes	No	2.00
4341	43.41	64.05	2.59	3.97	0.90	43.00	4.91	211.15	4.000	Yes	No	2.00
4342	43.42	64.40	2.58	3.93	0.90	43.27	4.75	205.31	4.000	Yes	No	2.00
4343	43.43	64.86	2.57	3.89	0.90	43.61	4.57	199.12	4.000	Yes	No	2.00
4344	43.44	65.46	2.57	3.83	0.90	44.06	4.35	191.78	4.000	Yes	No	2.00
4345	43.45	66.23	2.56	3.77	0.89	44.64	4.10	183.08	4.000	Yes	No	2.00
4346	43.46	67.07	2.55	3.70	0.89	45.28	3.84	173.79	4.000	Yes	No	2.00
4347	43.47	67.96	2.54	3.63	0.89	45.95	3.58	164.46	4.000	Yes	No	2.00
4348	43.48	68.83	2.53	3.56	0.88	46.62	3.34	155.57	4.000	Yes	No	2.00
4349	43.49	69.66	2.52	3.49	0.88	47.26	3.12	147.53	4.000	Yes	No	2.00
4350	43.50	70.39	2.51	3.43	0.88	47.81	2.94	140.69	4.000	Yes	No	2.00
4351	43.51	70.99	2.50	3.38	0.87	48.27	2.98	143.78	4.000	Yes	No	2.00
4352	43.52	71.52	2.49	3.34	0.87	48.67	2.93	142.85	4.000	Yes	No	2.00
4353	43.53	72.06	2.49	3.30	0.87	49.09	2.89	141.91	4.000	Yes	No	2.00
4354	43.54	72.67	2.48	3.25	0.86	49.56	2.84	140.83	4.000	Yes	No	2.00
4355	43.55	73.34	2.47	3.19	0.86	50.07	2.79	139.65	4.000	Yes	No	2.00
4356	43.56	74.03	2.46	3.14	0.86	50.60	2.74	138.43	4.000	Yes	No	2.00
4357	43.57	74.70	2.45	3.09	0.86	51.12	2.68	137.22	4.000	Yes	No	2.00
4358	43.58	75.31	2.45	3.04	0.85	51.60	2.64	136.11	4.000	Yes	No	2.00
4359	43.59	75.83	2.44	3.00	0.85	51.99	2.60	135.17	4.000	Yes	No	2.00
4360	43.60	76.13	2.44	2.97	0.85	52.22	2.58	134.56	4.000	Yes	No	2.00
4361	43.61	76.25	2.43	2.96	0.85	52.31	2.57	134.22	0.305	No	No	0.36
4362	43.62	76.24	2.43	2.96	0.85	52.30	2.56	134.04	0.304	No	No	0.36
4363	43.63	76.24	2.43	2.95	0.85	52.30	2.56	133.83	0.303	No	No	0.36
4364	43.64	76.24	2.43	2.94	0.85	52.29	2.56	133.61	0.302	No	No	0.36
4365	43.65	76.24	2.43	2.93	0.85	52.28	2.55	133.39	0.301	No	No	0.36
4366	43.66	76.24	2.43	2.93	0.85	52.27	2.55	133.18	0.300	No	No	0.35
4367	43.67	76.24	2.43	2.92	0.85	52.27	2.54	132.99	0.299	No	No	0.35
4368	43.68	76.16	2.43	2.92	0.85	52.20	2.55	132.99	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _k (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4369	43.69	75.90	2.43	2.94	0.85	51.98	2.57	133.40	4.000	Yes	No	2.00
4370	43.70	75.41	2.44	2.98	0.85	51.59	2.60	134.27	4.000	Yes	No	2.00
4371	43.71	74.76	2.45	3.03	0.85	51.06	2.65	135.47	4.000	Yes	No	2.00
4372	43.72	74.04	2.46	3.09	0.86	50.48	2.71	136.79	4.000	Yes	No	2.00
4373	43.73	73.29	2.47	3.15	0.86	49.88	2.77	138.16	4.000	Yes	No	2.00
4374	43.74	72.55	2.48	3.21	0.86	49.28	2.83	139.50	4.000	Yes	No	2.00
4375	43.75	71.85	2.49	3.27	0.87	48.73	2.89	140.75	4.000	Yes	No	2.00
4376	43.76	71.23	2.49	3.32	0.87	48.23	2.94	141.84	4.000	Yes	No	2.00
4377	43.77	70.59	2.50	3.37	0.87	47.72	2.85	136.13	4.000	Yes	No	2.00
4378	43.78	69.81	2.51	3.44	0.88	47.10	3.05	143.77	4.000	Yes	No	2.00
4379	43.79	68.79	2.53	3.53	0.88	46.29	3.33	154.37	4.000	Yes	No	2.00
4380	43.80	67.58	2.54	3.64	0.89	45.35	3.70	167.58	4.000	Yes	No	2.00
4381	43.81	66.27	2.56	3.75	0.90	44.33	4.12	182.79	4.000	Yes	No	2.00
4382	43.82	64.93	2.58	3.87	0.90	43.30	4.61	199.40	4.000	Yes	No	2.00
4383	43.83	63.63	2.59	3.99	0.91	42.29	5.12	216.63	4.000	Yes	No	2.00
4384	43.84	62.43	2.61	4.10	0.91	41.37	5.64	233.48	4.000	Yes	No	2.00
4385	43.85	61.40	2.62	4.20	0.92	40.58	6.13	248.80	4.000	Yes	No	2.00
4386	43.86	60.52	2.63	4.28	0.92	39.90	6.60	263.27	4.000	Yes	No	2.00
4387	43.87	59.66	2.64	4.37	0.93	39.24	7.10	278.77	4.000	Yes	No	2.00
4388	43.88	58.71	2.66	4.48	0.93	38.51	7.73	297.51	4.000	Yes	No	2.00
4389	43.89	57.63	2.67	4.61	0.94	37.69	8.49	319.80	4.000	Yes	No	2.00
4390	43.90	56.48	2.69	4.74	0.94	36.82	9.36	344.80	4.000	Yes	No	2.00
4391	43.91	55.33	2.70	4.87	0.95	35.95	4.73	170.09	4.000	Yes	Yes	2.00
4392	43.92	54.22	2.72	5.00	0.96	35.12	4.89	171.83	4.000	Yes	Yes	2.00
4393	43.93	53.23	2.73	5.11	0.96	34.37	5.04	173.30	4.000	Yes	Yes	2.00
4394	43.94	52.45	2.74	5.21	0.97	33.79	5.17	174.52	4.000	Yes	Yes	2.00
4395	43.95	51.89	2.75	5.29	0.97	33.36	5.27	175.69	4.000	Yes	Yes	2.00
4396	43.96	51.47	2.76	5.38	0.97	33.04	5.36	176.99	4.000	Yes	Yes	2.00
4397	43.97	51.05	2.77	5.48	0.98	32.71	5.46	178.52	4.000	Yes	Yes	2.00
4398	43.98	50.59	2.78	5.58	0.98	32.35	5.57	180.17	4.000	Yes	Yes	2.00
4399	43.99	50.11	2.79	5.70	0.98	31.98	5.69	181.83	4.000	Yes	Yes	2.00
4400	44.00	49.64	2.80	5.81	0.99	31.62	5.80	183.44	4.000	Yes	Yes	2.00
4401	44.01	49.19	2.80	5.91	0.99	31.27	5.91	184.90	4.000	Yes	Yes	2.00
4402	44.02	48.80	2.81	6.00	0.99	30.97	6.01	186.14	4.000	Yes	Yes	2.00
4403	44.03	48.58	2.82	6.07	0.99	30.79	6.08	187.20	4.000	Yes	Yes	2.00
4404	44.04	48.53	2.82	6.13	1.00	30.74	6.12	188.21	4.000	Yes	Yes	2.00
4405	44.05	48.64	2.82	6.18	1.00	30.80	6.15	189.32	1.469	No	Yes	1.74
4406	44.06	48.79	2.83	6.24	1.00	30.88	6.17	190.62	1.473	No	Yes	1.75
4407	44.07	48.94	2.83	6.30	1.00	30.97	6.20	192.01	1.477	No	Yes	1.75
4408	44.08	49.11	2.83	6.36	1.00	31.06	6.23	193.44	1.482	No	Yes	1.76
4409	44.09	49.26	2.83	6.42	1.00	31.15	6.25	194.83	1.486	No	Yes	1.76
4410	44.10	49.41	2.83	6.47	1.00	31.23	6.28	196.12	1.490	No	Yes	1.77
4411	44.11	49.55	2.83	6.52	1.00	31.32	6.30	197.19	1.494	No	Yes	1.77
4412	44.12	49.79	2.83	6.54	1.00	31.47	6.29	197.93	1.501	No	Yes	1.78
4413	44.13	50.17	2.83	6.53	1.00	31.72	6.25	198.43	4.000	Yes	Yes	2.00
4414	44.14	50.70	2.83	6.51	1.00	32.09	6.20	198.85	4.000	Yes	Yes	2.00
4415	44.15	51.30	2.82	6.49	1.00	32.50	6.13	199.31	4.000	Yes	Yes	2.00
4416	44.16	51.93	2.82	6.46	0.99	32.94	6.07	199.79	4.000	Yes	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4417	44.17	52.57	2.81	6.44	0.99	33.38	6.00	200.25	4.000	Yes	Yes	2.00
4418	44.18	53.18	2.81	6.42	0.99	33.80	5.94	200.68	4.000	Yes	Yes	2.00
4419	44.19	53.73	2.80	6.40	0.99	34.18	5.88	201.07	4.000	Yes	Yes	2.00
4420	44.20	54.29	2.80	6.37	0.99	34.58	5.82	201.31	4.000	Yes	Yes	2.00
4421	44.21	55.04	2.79	6.32	0.98	35.10	5.74	201.35	4.000	Yes	Yes	2.00
4422	44.22	56.06	2.78	6.24	0.98	35.82	5.62	201.16	4.000	Yes	Yes	2.00
4423	44.23	57.35	2.77	6.14	0.98	36.74	5.47	200.80	4.000	Yes	Yes	2.00
4424	44.24	58.77	2.75	6.04	0.97	37.75	5.31	200.30	4.000	Yes	Yes	2.00
4425	44.25	60.24	2.74	5.93	0.97	38.81	5.14	199.66	4.000	Yes	Yes	2.00
4426	44.26	61.70	2.73	5.82	0.96	39.85	4.99	198.92	4.000	Yes	Yes	2.00
4427	44.27	63.07	2.71	5.71	0.96	40.84	4.85	198.13	4.000	Yes	Yes	2.00
4428	44.28	64.27	2.70	5.63	0.95	41.70	4.73	197.36	4.000	Yes	Yes	2.00
4429	44.29	65.42	2.69	5.54	0.95	42.53	9.68	411.66	4.000	Yes	No	2.00
4430	44.30	66.69	2.68	5.45	0.94	43.45	9.00	391.02	4.000	Yes	No	2.00
4431	44.31	68.24	2.67	5.34	0.94	44.58	8.23	367.02	4.000	Yes	No	2.00
4432	44.32	70.05	2.65	5.21	0.93	45.90	7.42	340.68	4.000	Yes	No	2.00
4433	44.33	72.01	2.63	5.07	0.92	47.33	6.63	314.02	4.000	Yes	No	2.00
4434	44.34	74.00	2.61	4.93	0.92	48.80	5.91	288.54	4.000	Yes	No	2.00
4435	44.35	75.94	2.60	4.79	0.91	50.23	5.28	265.40	4.000	Yes	No	2.00
4436	44.36	77.73	2.58	4.67	0.90	51.55	4.76	245.46	4.000	Yes	No	2.00
4437	44.37	79.25	2.57	4.56	0.90	52.69	4.36	229.47	4.000	Yes	No	2.00
4438	44.38	80.58	2.55	4.47	0.89	53.67	4.04	216.61	4.000	Yes	No	2.00
4439	44.39	81.91	2.54	4.39	0.89	54.66	3.75	204.93	4.000	Yes	No	2.00
4440	44.40	83.41	2.53	4.30	0.89	55.77	3.45	192.67	4.000	Yes	No	2.00
4441	44.41	85.09	2.52	4.21	0.88	57.03	3.15	179.55	4.000	Yes	No	2.00
4442	44.42	86.88	2.50	4.10	0.87	58.37	2.85	166.43	4.000	Yes	No	2.00
4443	44.43	88.68	2.49	4.00	0.87	59.73	2.89	172.88	4.000	Yes	No	2.00
4444	44.44	90.39	2.47	3.90	0.86	61.02	2.80	170.90	4.000	Yes	No	2.00
4445	44.45	91.93	2.46	3.81	0.86	62.19	2.72	169.09	4.000	Yes	No	2.00
4446	44.46	93.21	2.45	3.74	0.85	63.16	2.65	167.59	4.000	Yes	No	2.00
4447	44.47	94.32	2.44	3.68	0.85	64.00	2.60	166.31	4.000	Yes	No	2.00
4448	44.48	95.42	2.43	3.62	0.85	64.83	2.55	165.10	4.000	Yes	No	2.00
4449	44.49	96.66	2.42	3.55	0.84	65.77	2.49	163.74	4.000	Yes	No	2.00
4450	44.50	98.03	2.41	3.48	0.84	66.82	2.43	162.22	4.000	Yes	No	2.00
4451	44.51	99.45	2.40	3.40	0.84	67.91	2.37	160.64	4.000	Yes	No	2.00
4452	44.52	100.86	2.39	3.33	0.83	68.99	2.31	159.07	4.000	Yes	No	2.00
4453	44.53	102.17	2.38	3.26	0.83	70.01	2.25	157.60	4.000	Yes	No	2.00
4454	44.54	103.33	2.37	3.20	0.82	70.90	2.20	156.30	4.000	Yes	No	2.00
4455	44.55	104.13	2.36	3.15	0.82	71.52	2.17	155.32	4.000	Yes	No	2.00
4456	44.56	104.65	2.35	3.12	0.82	71.92	2.15	154.54	4.000	Yes	No	2.00
4457	44.57	104.97	2.35	3.10	0.82	72.17	2.13	153.85	4.000	Yes	No	2.00
4458	44.58	105.32	2.35	3.06	0.82	72.44	2.11	153.07	4.000	Yes	No	2.00
4459	44.59	105.69	2.34	3.03	0.81	72.74	2.09	152.23	4.000	Yes	No	2.00
4460	44.60	106.08	2.34	3.00	0.81	73.04	2.07	151.38	4.000	Yes	No	2.00
4461	44.61	106.45	2.33	2.97	0.81	73.33	2.05	150.55	4.000	Yes	No	2.00
4462	44.62	106.79	2.33	2.94	0.81	73.61	2.04	149.79	4.000	Yes	No	2.00
4463	44.63	107.10	2.32	2.91	0.81	73.85	2.02	149.15	4.000	Yes	No	2.00
4464	44.64	107.47	2.32	2.89	0.81	74.13	2.01	148.66	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
4465	44.65	107.94	2.32	2.87	0.80	74.49	1.99	148.23	4.000	Yes	No	2.00
4466	44.66	108.56	2.31	2.84	0.80	74.96	1.97	147.81	4.000	Yes	No	2.00
4467	44.67	109.26	2.31	2.82	0.80	75.49	1.95	147.33	4.000	Yes	No	2.00
4468	44.68	109.99	2.30	2.79	0.80	76.05	1.93	146.83	4.000	Yes	No	2.00
4469	44.69	110.73	2.30	2.76	0.80	76.62	1.91	146.34	4.000	Yes	No	2.00
4470	44.70	111.43	2.29	2.73	0.79	77.16	1.89	145.87	4.000	Yes	No	2.00
4471	44.71	112.06	2.29	2.71	0.79	77.64	1.87	145.46	4.000	Yes	No	2.00
4472	44.72	112.60	2.28	2.68	0.79	78.05	1.86	145.10	4.000	Yes	No	2.00
4473	44.73	113.11	2.28	2.66	0.79	78.44	1.85	144.77	4.000	Yes	No	2.00
4474	44.74	113.66	2.27	2.64	0.79	78.87	1.83	144.41	4.000	Yes	No	2.00
4475	44.75	114.31	2.27	2.62	0.79	79.36	1.81	143.99	4.000	Yes	No	2.00
4476	44.76	115.02	2.26	2.59	0.78	79.91	1.80	143.55	4.000	Yes	No	2.00
4477	44.77	115.75	2.26	2.56	0.78	80.48	1.78	143.09	4.000	Yes	No	2.00
4478	44.78	116.48	2.25	2.53	0.78	81.05	1.76	142.65	4.000	Yes	No	2.00
4479	44.79	117.15	2.25	2.50	0.78	81.58	1.74	142.25	4.000	Yes	No	2.00
4480	44.80	117.75	2.24	2.48	0.78	82.04	1.73	141.90	4.000	Yes	No	2.00
4481	44.81	118.04	2.24	2.47	0.78	82.26	1.72	141.67	0.344	No	No	0.41
4482	44.82	118.02	2.24	2.46	0.78	82.23	1.72	141.54	0.344	No	No	0.41
4483	44.83	117.72	2.24	2.47	0.78	81.99	1.73	141.48	0.343	No	No	0.41
4484	44.84	117.36	2.24	2.47	0.78	81.69	1.73	141.42	0.343	No	No	0.41
4485	44.85	116.96	2.24	2.48	0.78	81.37	1.74	141.36	0.343	No	No	0.41
4486	44.86	116.56	2.25	2.49	0.78	81.05	1.74	141.30	0.342	No	No	0.41
4487	44.87	116.18	2.25	2.49	0.78	80.74	1.75	141.24	0.342	No	No	0.41
4488	44.88	115.82	2.25	2.50	0.78	80.45	1.76	141.19	0.342	No	No	0.41
4489	44.89	115.52	2.25	2.50	0.78	80.20	1.76	141.16	0.342	No	No	0.41
4490	44.90	115.24	2.25	2.51	0.78	79.97	1.77	141.17	0.342	No	No	0.41
4491	44.91	114.95	2.26	2.52	0.78	79.73	1.77	141.24	0.342	No	No	0.41
4492	44.92	114.61	2.26	2.53	0.78	79.45	1.78	141.35	0.343	No	No	0.41
4493	44.93	114.24	2.26	2.54	0.78	79.14	1.79	141.48	0.343	No	No	0.41
4494	44.94	113.84	2.26	2.56	0.78	78.81	1.80	141.62	0.344	No	No	0.41
4495	44.95	113.44	2.27	2.57	0.79	78.48	1.81	141.77	0.345	No	No	0.41
4496	44.96	113.06	2.27	2.58	0.79	78.17	1.82	141.91	0.346	No	No	0.41
4497	44.97	112.72	2.27	2.59	0.79	77.89	1.82	142.03	0.346	No	No	0.41
4498	44.98	112.44	2.27	2.60	0.79	77.65	1.83	142.18	0.347	No	No	0.42
4499	44.99	112.20	2.28	2.62	0.79	77.44	1.84	142.41	0.349	No	No	0.42
4500	45.00	111.95	2.28	2.63	0.79	77.22	1.85	142.76	0.351	No	No	0.42
4501	45.01	111.67	2.28	2.65	0.79	76.97	1.86	143.19	0.353	No	No	0.42
4502	45.02	111.36	2.29	2.67	0.79	76.70	1.87	143.67	0.356	No	No	0.43
4503	45.03	111.04	2.29	2.70	0.79	76.42	1.89	144.18	0.359	No	No	0.43
4504	45.04	110.73	2.29	2.72	0.80	76.15	1.90	144.68	0.362	No	No	0.43
4505	45.05	110.43	2.30	2.74	0.80	75.89	1.91	145.14	0.364	No	No	0.44
4506	45.06	110.17	2.30	2.76	0.80	75.66	1.92	145.55	0.367	No	No	0.44
4507	45.07	109.95	2.30	2.77	0.80	75.46	1.93	145.93	0.369	No	No	0.44
4508	45.08	109.72	2.31	2.79	0.80	75.26	1.94	146.34	4.000	Yes	No	2.00
4509	45.09	109.47	2.31	2.81	0.80	75.03	1.96	146.82	4.000	Yes	No	2.00
4510	45.10	109.18	2.31	2.84	0.80	74.77	1.97	147.39	4.000	Yes	No	2.00
4511	45.11	108.87	2.32	2.86	0.81	74.50	1.99	148.00	4.000	Yes	No	2.00
4512	45.12	108.55	2.32	2.89	0.81	74.22	2.00	148.62	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4513	45.13	108.24	2.32	2.91	0.81	73.95	2.02	149.23	4.000	Yes	No	2.00
4514	45.14	107.95	2.33	2.93	0.81	73.70	2.03	149.78	4.000	Yes	No	2.00
4515	45.15	107.70	2.33	2.95	0.81	73.48	2.05	150.27	4.000	Yes	No	2.00
4516	45.16	107.43	2.33	2.97	0.81	73.24	2.06	150.74	4.000	Yes	No	2.00
4517	45.17	107.11	2.34	3.00	0.81	72.97	2.07	151.26	4.000	Yes	No	2.00
4518	45.18	106.71	2.34	3.02	0.81	72.63	2.09	151.88	4.000	Yes	No	2.00
4519	45.19	106.25	2.35	3.05	0.82	72.25	2.11	152.59	4.000	Yes	No	2.00
4520	45.20	105.78	2.35	3.09	0.82	71.85	2.13	153.34	4.000	Yes	No	2.00
4521	45.21	105.30	2.36	3.12	0.82	71.46	2.16	154.09	4.000	Yes	No	2.00
4522	45.22	104.84	2.36	3.15	0.82	71.08	2.18	154.81	4.000	Yes	No	2.00
4523	45.23	104.44	2.36	3.18	0.82	70.74	2.20	155.45	4.000	Yes	No	2.00
4524	45.24	104.09	2.37	3.20	0.83	70.45	2.21	156.01	4.000	Yes	No	2.00
4525	45.25	103.76	2.37	3.23	0.83	70.17	2.23	156.58	4.000	Yes	No	2.00
4526	45.26	103.40	2.38	3.25	0.83	69.87	2.25	157.22	4.000	Yes	No	2.00
4527	45.27	102.97	2.38	3.28	0.83	69.51	2.27	157.98	4.000	Yes	No	2.00
4528	45.28	102.51	2.39	3.32	0.83	69.13	2.30	158.81	4.000	Yes	No	2.00
4529	45.29	102.03	2.39	3.35	0.83	68.74	2.32	159.67	4.000	Yes	No	2.00
4530	45.30	101.56	2.40	3.39	0.84	68.35	2.35	160.52	4.000	Yes	No	2.00
4531	45.31	101.12	2.40	3.42	0.84	67.98	2.37	161.31	4.000	Yes	No	2.00
4532	45.32	100.73	2.40	3.45	0.84	67.67	2.39	162.00	4.000	Yes	No	2.00
4533	45.33	100.43	2.41	3.47	0.84	67.41	2.41	162.49	4.000	Yes	No	2.00
4534	45.34	100.17	2.41	3.49	0.84	67.20	2.42	162.83	0.482	No	No	0.58
4535	45.35	99.91	2.41	3.50	0.84	66.99	2.43	163.09	0.483	No	No	0.58
4536	45.36	99.62	2.41	3.52	0.84	66.75	2.45	163.39	0.486	No	No	0.58
4537	45.37	99.31	2.42	3.53	0.84	66.50	2.46	163.71	0.488	No	No	0.59
4538	45.38	98.99	2.42	3.55	0.84	66.24	2.48	164.03	0.490	No	No	0.59
4539	45.39	98.68	2.42	3.56	0.85	65.99	2.49	164.34	0.493	No	No	0.59
4540	45.40	98.39	2.42	3.58	0.85	65.76	2.50	164.63	0.495	No	No	0.60
4541	45.41	98.18	2.43	3.59	0.85	65.58	2.51	164.80	0.496	No	No	0.60
4542	45.42	98.10	2.43	3.59	0.85	65.51	2.51	164.70	0.496	No	No	0.60
4543	45.43	98.15	2.42	3.57	0.85	65.55	2.51	164.31	0.493	No	No	0.59
4544	45.44	98.29	2.42	3.55	0.85	65.65	2.49	163.68	0.488	No	No	0.59
4545	45.45	98.44	2.42	3.53	0.84	65.77	2.48	162.98	0.483	No	No	0.58
4546	45.46	98.60	2.42	3.50	0.84	65.89	2.46	162.24	0.477	No	No	0.57
4547	45.47	98.76	2.41	3.48	0.84	66.01	2.45	161.50	0.472	No	No	0.57
4548	45.48	98.91	2.41	3.45	0.84	66.13	2.43	160.79	0.467	No	No	0.56
4549	45.49	99.04	2.41	3.43	0.84	66.23	2.42	160.16	0.462	No	No	0.56
4550	45.50	99.23	2.41	3.41	0.84	66.38	2.40	159.54	4.000	Yes	No	2.00
4551	45.51	99.56	2.40	3.38	0.84	66.63	2.38	158.82	4.000	Yes	No	2.00
4552	45.52	100.07	2.40	3.34	0.84	67.01	2.36	157.89	4.000	Yes	No	2.00
4553	45.53	100.71	2.39	3.30	0.83	67.50	2.32	156.77	4.000	Yes	No	2.00
4554	45.54	101.40	2.38	3.25	0.83	68.04	2.29	155.55	4.000	Yes	No	2.00
4555	45.55	102.12	2.38	3.19	0.83	68.60	2.25	154.28	4.000	Yes	No	2.00
4556	45.56	102.83	2.37	3.14	0.83	69.14	2.21	153.04	4.000	Yes	No	2.00
4557	45.57	103.49	2.36	3.10	0.82	69.66	2.18	151.88	4.000	Yes	No	2.00
4558	45.58	104.06	2.35	3.05	0.82	70.10	2.15	150.87	4.000	Yes	No	2.00
4559	45.59	104.60	2.35	3.02	0.82	70.52	2.13	150.02	4.000	Yes	No	2.00
4560	45.60	105.19	2.34	2.98	0.82	70.97	2.10	149.23	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4561	45.61	105.89	2.34	2.94	0.81	71.51	2.07	148.37	4.000	Yes	No	2.00
4562	45.62	106.70	2.33	2.90	0.81	72.13	2.04	147.40	4.000	Yes	No	2.00
4563	45.63	107.56	2.32	2.85	0.81	72.80	2.01	146.36	4.000	Yes	No	2.00
4564	45.64	108.44	2.31	2.80	0.81	73.49	1.98	145.31	4.000	Yes	No	2.00
4565	45.65	109.29	2.31	2.76	0.80	74.15	1.95	144.31	4.000	Yes	No	2.00
4566	45.66	110.07	2.30	2.71	0.80	74.75	1.92	143.41	4.000	Yes	No	2.00
4567	45.67	110.72	2.29	2.68	0.80	75.26	1.90	142.67	4.000	Yes	No	2.00
4568	45.68	111.25	2.29	2.65	0.80	75.67	1.88	142.11	4.000	Yes	No	2.00
4569	45.69	111.75	2.28	2.63	0.79	76.05	1.86	141.66	4.000	Yes	No	2.00
4570	45.70	112.29	2.28	2.60	0.79	76.47	1.85	141.20	4.000	Yes	No	2.00
4571	45.71	112.90	2.27	2.57	0.79	76.93	1.83	140.70	4.000	Yes	No	2.00
4572	45.72	113.53	2.27	2.55	0.79	77.42	1.81	140.17	4.000	Yes	No	2.00
4573	45.73	114.17	2.26	2.52	0.79	77.92	1.79	139.66	4.000	Yes	No	2.00
4574	45.74	114.77	2.26	2.49	0.78	78.38	1.78	139.18	4.000	Yes	No	2.00
4575	45.75	115.31	2.25	2.46	0.78	78.80	1.76	138.75	4.000	Yes	No	2.00
4576	45.76	115.73	2.25	2.45	0.78	79.12	1.75	138.43	4.000	Yes	No	2.00
4577	45.77	116.04	2.25	2.43	0.78	79.36	1.74	138.20	0.325	No	No	0.39
4578	45.78	116.31	2.24	2.42	0.78	79.55	1.74	138.03	0.325	No	No	0.39
4579	45.79	116.59	2.24	2.41	0.78	79.76	1.73	137.85	0.324	No	No	0.39
4580	45.80	116.90	2.24	2.40	0.78	79.99	1.72	137.65	0.323	No	No	0.39
4581	45.81	117.22	2.24	2.38	0.78	80.23	1.71	137.46	0.322	No	No	0.39
4582	45.82	117.53	2.23	2.37	0.78	80.47	1.71	137.26	0.321	No	No	0.39
4583	45.83	117.83	2.23	2.36	0.77	80.69	1.70	137.08	0.320	No	No	0.39
4584	45.84	118.08	2.23	2.35	0.77	80.88	1.69	136.93	0.319	No	No	0.39
4585	45.85	118.36	2.23	2.34	0.77	81.09	1.69	136.78	0.318	No	No	0.38
4586	45.86	118.70	2.22	2.33	0.77	81.34	1.68	136.62	0.317	No	No	0.38
4587	45.87	119.15	2.22	2.31	0.77	81.68	1.67	136.44	0.316	No	No	0.38
4588	45.88	119.67	2.22	2.29	0.77	82.08	1.66	136.23	0.315	No	No	0.38
4589	45.89	120.22	2.21	2.27	0.77	82.52	1.65	136.03	0.314	No	No	0.38
4590	45.90	120.78	2.21	2.25	0.77	82.95	1.64	135.82	0.313	No	No	0.38
4591	45.91	121.32	2.21	2.24	0.76	83.36	1.63	135.62	0.312	No	No	0.38
4592	45.92	121.81	2.20	2.22	0.76	83.74	1.62	135.45	0.311	No	No	0.38
4593	45.93	122.26	2.20	2.20	0.76	84.08	1.61	135.31	0.310	No	No	0.38
4594	45.94	122.74	2.19	2.19	0.76	84.45	1.60	135.21	0.310	No	No	0.37
4595	45.95	123.34	2.19	2.17	0.76	84.90	1.59	135.14	0.310	No	No	0.37
4596	45.96	124.09	2.19	2.15	0.76	85.48	1.58	135.08	0.309	No	No	0.37
4597	45.97	124.92	2.18	2.13	0.75	86.12	1.57	135.03	0.309	No	No	0.37
4598	45.98	125.80	2.17	2.11	0.75	86.79	1.56	134.99	0.309	No	No	0.37
4599	45.99	126.67	2.17	2.09	0.75	87.47	1.54	134.96	0.309	No	No	0.37
4600	46.00	127.50	2.16	2.07	0.75	88.11	1.53	134.95	0.309	No	No	0.37
4601	46.01	128.24	2.16	2.05	0.75	88.68	1.52	134.94	0.309	No	No	0.37
4602	46.02	128.87	2.15	2.03	0.74	89.16	1.51	134.93	0.308	No	No	0.37
4603	46.03	129.48	2.15	2.01	0.74	89.64	1.50	134.90	0.308	No	No	0.37
4604	46.04	130.15	2.15	1.99	0.74	90.16	1.50	134.86	0.308	No	No	0.37
4605	46.05	130.93	2.14	1.97	0.74	90.77	1.49	134.82	0.308	No	No	0.37
4606	46.06	131.79	2.13	1.95	0.74	91.45	1.47	134.80	0.308	No	No	0.37
4607	46.07	132.67	2.13	1.92	0.73	92.14	1.46	134.79	0.308	No	No	0.37
4608	46.08	133.53	2.12	1.89	0.73	92.83	1.45	134.79	0.308	No	No	0.37

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4609	46.09	134.33	2.12	1.87	0.73	93.46	1.44	134.81	0.308	No	No	0.37
4610	46.10	135.03	2.11	1.85	0.73	94.01	1.43	134.85	0.308	No	No	0.37
4611	46.11	135.61	2.11	1.85	0.73	94.43	1.43	135.19	0.310	No	No	0.38
4612	46.12	136.15	2.11	1.86	0.73	94.78	1.43	135.90	0.313	No	No	0.38
4613	46.13	136.73	2.11	1.90	0.73	95.12	1.44	137.04	0.319	No	No	0.39
4614	46.14	137.40	2.12	1.94	0.73	95.50	1.45	138.35	0.326	No	No	0.40
4615	46.15	138.11	2.12	1.98	0.73	95.92	1.46	139.76	0.334	No	No	0.40
4616	46.16	138.83	2.13	2.02	0.74	96.34	1.47	141.22	0.342	No	No	0.41
4617	46.17	139.52	2.13	2.06	0.74	96.75	1.47	142.63	0.350	No	No	0.42
4618	46.18	140.15	2.14	2.09	0.74	97.11	1.48	143.92	0.357	No	No	0.43
4619	46.19	140.68	2.14	2.12	0.74	97.42	1.49	145.03	0.364	No	No	0.44
4620	46.20	141.13	2.15	2.15	0.74	97.66	1.50	146.07	0.370	No	No	0.45
4621	46.21	141.56	2.15	2.19	0.74	97.89	1.50	147.18	0.376	No	No	0.46
4622	46.22	142.04	2.15	2.23	0.75	98.14	1.51	148.49	0.384	No	No	0.47
4623	46.23	142.57	2.16	2.27	0.75	98.42	1.52	149.96	0.394	No	No	0.48
4624	46.24	143.13	2.17	2.32	0.75	98.71	1.54	151.53	0.404	No	No	0.49
4625	46.25	143.69	2.17	2.36	0.75	99.01	1.55	153.10	0.414	No	No	0.50
4626	46.26	144.21	2.18	2.41	0.75	99.29	1.56	154.61	0.424	No	No	0.51
4627	46.27	144.68	2.18	2.44	0.75	99.53	1.57	155.96	0.433	No	No	0.53
4628	46.28	144.99	2.18	2.46	0.76	99.70	1.57	156.70	0.438	No	No	0.53
4629	46.29	145.11	2.18	2.46	0.76	99.78	1.57	156.70	0.438	No	No	0.53
4630	46.30	145.08	2.18	2.44	0.75	99.79	1.56	155.97	0.433	No	No	0.53
4631	46.31	145.01	2.17	2.40	0.75	99.79	1.55	154.98	0.426	No	No	0.52
4632	46.32	144.93	2.17	2.37	0.75	99.79	1.54	153.91	0.419	No	No	0.51
4633	46.33	144.85	2.16	2.33	0.75	99.79	1.53	152.82	0.412	No	No	0.50
4634	46.34	144.77	2.16	2.29	0.75	99.80	1.52	151.77	0.405	No	No	0.49
4635	46.35	144.70	2.15	2.26	0.74	99.80	1.51	150.80	0.399	No	No	0.48
4636	46.36	144.63	2.15	2.23	0.74	99.80	1.50	149.98	0.394	No	No	0.48
4637	46.37	144.40	2.15	2.21	0.74	99.65	1.50	149.41	0.390	No	No	0.47
4638	46.38	143.98	2.15	2.21	0.74	99.33	1.50	149.01	0.388	No	No	0.47
4639	46.39	143.33	2.15	2.21	0.74	98.82	1.50	148.71	0.386	No	No	0.47
4640	46.40	142.59	2.15	2.22	0.74	98.24	1.51	148.37	0.384	No	No	0.47
4641	46.41	141.80	2.16	2.23	0.75	97.63	1.52	148.02	0.382	No	No	0.46
4642	46.42	141.00	2.16	2.24	0.75	97.00	1.52	147.67	0.379	No	No	0.46
4643	46.43	140.23	2.16	2.24	0.75	96.40	1.53	147.33	0.377	No	No	0.46
4644	46.44	139.53	2.16	2.25	0.75	95.86	1.53	147.02	0.376	No	No	0.46
4645	46.45	138.90	2.17	2.26	0.75	95.36	1.54	146.79	4.000	Yes	No	2.00
4646	46.46	138.19	2.17	2.27	0.75	94.79	1.55	146.69	4.000	Yes	No	2.00
4647	46.47	137.31	2.18	2.29	0.75	94.08	1.56	146.70	4.000	Yes	No	2.00
4648	46.48	136.22	2.18	2.32	0.76	93.20	1.57	146.79	4.000	Yes	No	2.00
4649	46.49	135.00	2.19	2.36	0.76	92.23	1.59	146.91	4.000	Yes	No	2.00
4650	46.50	133.72	2.20	2.39	0.76	91.21	1.61	147.07	4.000	Yes	No	2.00
4651	46.51	132.45	2.21	2.43	0.77	90.20	1.63	147.25	4.000	Yes	No	2.00
4652	46.52	131.25	2.21	2.46	0.77	89.25	1.65	147.44	4.000	Yes	No	2.00
4653	46.53	130.19	2.22	2.49	0.77	88.40	1.67	147.62	4.000	Yes	No	2.00
4654	46.54	129.18	2.23	2.52	0.77	87.59	1.69	147.72	4.000	Yes	No	2.00
4655	46.55	128.04	2.23	2.54	0.78	86.70	1.70	147.75	4.000	Yes	No	2.00
4656	46.56	126.62	2.24	2.57	0.78	85.61	1.73	147.70	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4657	46.57	124.94	2.25	2.60	0.78	84.33	1.75	147.65	4.000	Yes	No	2.00
4658	46.58	123.12	2.26	2.64	0.79	82.94	1.78	147.62	4.000	Yes	No	2.00
4659	46.59	121.23	2.27	2.68	0.79	81.50	1.81	147.62	4.000	Yes	No	2.00
4660	46.60	119.39	2.28	2.71	0.79	80.11	1.84	147.64	4.000	Yes	No	2.00
4661	46.61	117.69	2.29	2.74	0.80	78.82	1.87	147.67	4.000	Yes	No	2.00
4662	46.62	116.21	2.29	2.77	0.80	77.70	1.90	147.73	4.000	Yes	No	2.00
4663	46.63	114.90	2.30	2.81	0.80	76.70	1.93	148.04	4.000	Yes	No	2.00
4664	46.64	113.58	2.31	2.85	0.81	75.67	1.96	148.66	4.000	Yes	No	2.00
4665	46.65	112.06	2.32	2.91	0.81	74.50	2.01	149.65	4.000	Yes	No	2.00
4666	46.66	110.34	2.33	2.98	0.81	73.17	2.06	150.79	4.000	Yes	No	2.00
4667	46.67	108.49	2.35	3.05	0.82	71.75	2.12	152.02	4.000	Yes	No	2.00
4668	46.68	106.63	2.36	3.12	0.82	70.33	2.18	153.29	4.000	Yes	No	2.00
4669	46.69	104.84	2.37	3.19	0.83	68.97	2.24	154.51	4.000	Yes	No	2.00
4670	46.70	103.22	2.39	3.26	0.83	67.74	2.30	155.62	4.000	Yes	No	2.00
4671	46.71	101.83	2.40	3.31	0.84	66.69	2.35	156.64	4.000	Yes	No	2.00
4672	46.72	100.57	2.41	3.37	0.84	65.73	2.40	157.79	4.000	Yes	No	2.00
4673	46.73	99.26	2.42	3.44	0.85	64.72	2.46	159.23	4.000	Yes	No	2.00
4674	46.74	97.74	2.43	3.52	0.85	63.56	2.53	161.00	4.000	Yes	No	2.00
4675	46.75	96.05	2.44	3.62	0.86	62.28	2.62	162.96	4.000	Yes	No	2.00
4676	46.76	94.28	2.46	3.72	0.86	60.94	2.71	164.98	4.000	Yes	No	2.00
4677	46.77	92.52	2.47	3.81	0.87	59.62	2.80	166.95	4.000	Yes	No	2.00
4678	46.78	90.85	2.49	3.91	0.87	58.38	2.89	168.76	4.000	Yes	No	2.00
4679	46.79	89.38	2.50	3.99	0.88	57.28	2.97	170.34	4.000	Yes	No	2.00
4680	46.80	88.14	2.51	4.06	0.88	56.36	2.99	168.57	4.000	Yes	No	2.00
4681	46.81	87.00	2.52	4.13	0.89	55.51	3.19	177.27	4.000	Yes	No	2.00
4682	46.82	85.79	2.53	4.20	0.89	54.61	3.43	187.10	4.000	Yes	No	2.00
4683	46.83	84.39	2.54	4.29	0.89	53.58	3.71	199.02	4.000	Yes	No	2.00
4684	46.84	82.87	2.56	4.39	0.90	52.46	4.05	212.64	4.000	Yes	No	2.00
4685	46.85	81.31	2.57	4.49	0.90	51.32	4.43	227.39	4.000	Yes	No	2.00
4686	46.86	79.78	2.58	4.58	0.91	50.21	4.83	242.58	4.000	Yes	No	2.00
4687	46.87	78.37	2.59	4.68	0.91	49.18	5.23	257.34	4.000	Yes	No	2.00
4688	46.88	77.15	2.61	4.75	0.92	48.30	5.60	270.57	4.000	Yes	No	2.00
4689	46.89	76.07	2.61	4.81	0.92	47.53	5.92	281.52	4.000	Yes	No	2.00
4690	46.90	75.01	2.62	4.86	0.92	46.77	6.23	291.36	4.000	Yes	No	2.00
4691	46.91	73.80	2.63	4.90	0.93	45.92	6.57	301.73	4.000	Yes	No	2.00
4692	46.92	72.43	2.64	4.95	0.93	44.95	6.98	313.96	4.000	Yes	No	2.00
4693	46.93	70.97	2.65	5.01	0.94	43.93	7.46	327.58	4.000	Yes	No	2.00
4694	46.94	69.49	2.66	5.06	0.94	42.90	7.97	341.98	4.000	Yes	No	2.00
4695	46.95	68.07	2.67	5.12	0.94	41.91	8.51	356.45	4.000	Yes	No	2.00
4696	46.96	66.78	2.68	5.17	0.95	41.01	9.03	370.13	4.000	Yes	No	2.00
4697	46.97	65.71	2.69	5.20	0.95	40.27	9.47	381.50	4.000	Yes	No	2.00
4698	46.98	64.81	2.69	5.23	0.95	39.64	9.84	390.12	4.000	Yes	No	2.00
4699	46.99	63.93	2.70	5.24	0.95	39.04	10.17	397.00	4.000	Yes	No	2.00
4700	47.00	62.96	2.71	5.24	0.96	38.38	4.76	182.81	4.000	Yes	Yes	2.00
4701	47.01	61.88	2.71	5.25	0.96	37.64	4.83	181.84	4.000	Yes	Yes	2.00
4702	47.02	60.75	2.72	5.26	0.96	36.87	4.90	180.82	4.000	Yes	Yes	2.00
4703	47.03	59.62	2.73	5.27	0.96	36.11	4.98	179.78	4.000	Yes	Yes	2.00
4704	47.04	58.56	2.73	5.28	0.97	35.40	5.05	178.79	4.000	Yes	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _k (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4705	47.05	57.63	2.74	5.29	0.97	34.76	5.12	177.90	4.000	Yes	Yes	2.00
4706	47.06	56.97	2.74	5.29	0.97	34.31	5.17	177.30	4.000	Yes	Yes	2.00
4707	47.07	56.57	2.75	5.30	0.97	34.04	5.20	177.00	1.624	No	Yes	1.99
4708	47.08	56.36	2.75	5.31	0.97	33.89	5.22	176.95	1.616	No	Yes	1.98
4709	47.09	56.16	2.75	5.32	0.97	33.74	5.24	176.94	1.610	No	Yes	1.97
4710	47.10	55.94	2.75	5.33	0.97	33.59	5.27	176.93	1.602	No	Yes	1.96
4711	47.11	55.72	2.75	5.34	0.97	33.43	5.29	176.92	1.594	No	Yes	1.95
4712	47.12	55.50	2.76	5.36	0.98	33.27	5.32	176.91	1.587	No	Yes	1.94
4713	47.13	55.30	2.76	5.37	0.98	33.12	5.34	176.90	1.580	No	Yes	1.94
4714	47.14	55.14	2.76	5.38	0.98	33.01	5.36	176.90	1.574	No	Yes	1.93
4715	47.15	55.12	2.76	5.38	0.98	32.99	5.37	177.04	1.573	No	Yes	1.93
4716	47.16	55.25	2.76	5.39	0.98	33.06	5.36	177.36	1.577	No	Yes	1.93
4717	47.17	55.51	2.76	5.40	0.98	33.22	5.35	177.86	1.585	No	Yes	1.94
4718	47.18	55.81	2.76	5.41	0.98	33.41	5.34	178.43	1.594	No	Yes	1.95
4719	47.19	56.13	2.76	5.42	0.98	33.61	5.33	179.03	1.603	No	Yes	1.97
4720	47.20	56.45	2.76	5.44	0.98	33.81	5.31	179.65	1.613	No	Yes	1.98
4721	47.21	56.75	2.75	5.45	0.98	34.00	5.30	180.23	1.622	No	Yes	1.99
4722	47.22	57.03	2.75	5.46	0.97	34.17	5.29	180.76	1.630	No	Yes	2.00
4723	47.23	57.29	2.75	5.46	0.97	34.34	5.28	181.13	1.638	No	Yes	2.00
4724	47.24	57.59	2.75	5.45	0.97	34.53	5.25	181.27	1.647	No	Yes	2.00
4725	47.25	57.97	2.75	5.43	0.97	34.78	5.21	181.18	1.659	No	Yes	2.00
4726	47.26	58.44	2.74	5.40	0.97	35.10	5.16	180.98	1.674	No	Yes	2.00
4727	47.27	58.97	2.74	5.36	0.97	35.45	5.10	180.74	1.691	No	Yes	2.00
4728	47.28	59.51	2.73	5.32	0.97	35.82	5.04	180.47	1.709	No	Yes	2.00
4729	47.29	60.06	2.73	5.28	0.96	36.19	4.98	180.19	1.726	No	Yes	2.00
4730	47.30	60.57	2.72	5.25	0.96	36.53	4.93	179.92	1.742	No	Yes	2.00
4731	47.31	61.02	2.72	5.21	0.96	36.83	4.88	179.67	1.757	No	Yes	2.00
4732	47.32	61.41	2.71	5.18	0.96	37.10	4.83	179.32	1.769	No	Yes	2.00
4733	47.33	61.78	2.71	5.14	0.96	37.35	4.79	178.78	1.782	No	Yes	2.00
4734	47.34	62.20	2.70	5.09	0.96	37.64	4.73	177.98	1.795	No	Yes	2.00
4735	47.35	62.68	2.70	5.03	0.95	37.97	9.91	376.45	3.600	No	No	2.00
4736	47.36	63.20	2.69	4.97	0.95	38.34	9.49	363.91	3.600	No	No	2.00
4737	47.37	63.73	2.68	4.90	0.95	38.71	9.08	351.34	3.600	No	No	2.00
4738	47.38	64.25	2.67	4.83	0.95	39.08	8.68	339.39	3.600	No	No	2.00
4739	47.39	64.73	2.67	4.77	0.94	39.42	8.34	328.62	3.600	No	No	2.00
4740	47.40	65.15	2.66	4.72	0.94	39.71	8.05	319.49	3.600	No	No	2.00
4741	47.41	65.53	2.66	4.67	0.94	39.98	7.78	311.10	3.600	No	No	2.00
4742	47.42	65.93	2.65	4.62	0.94	40.26	7.51	302.25	3.600	No	No	2.00
4743	47.43	66.40	2.64	4.55	0.93	40.60	7.19	291.96	3.600	No	No	2.00
4744	47.44	66.93	2.64	4.48	0.93	40.98	6.85	280.58	3.600	No	No	2.00
4745	47.45	67.50	2.63	4.41	0.93	41.38	6.50	268.81	3.600	No	No	2.00
4746	47.46	68.07	2.62	4.33	0.92	41.80	6.16	257.27	3.600	No	No	2.00
4747	47.47	68.61	2.61	4.26	0.92	42.19	5.84	246.54	3.600	No	No	2.00
4748	47.48	69.10	2.60	4.19	0.92	42.55	5.57	237.12	3.600	No	No	2.00
4749	47.49	69.48	2.60	4.14	0.92	42.82	5.36	229.58	4.000	No	No	2.00
4750	47.50	69.71	2.59	4.09	0.91	43.00	5.20	223.47	4.000	No	No	2.00
4751	47.51	69.84	2.59	4.04	0.91	43.10	5.06	217.87	4.000	No	No	2.00
4752	47.52	69.93	2.58	3.99	0.91	43.18	4.90	211.77	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
4753	47.53	70.03	2.58	3.93	0.91	43.27	4.74	205.11	4.000	No	No	2.00
4754	47.54	70.14	2.57	3.87	0.91	43.37	4.57	198.29	0.805	No	No	0.99
4755	47.55	70.24	2.57	3.81	0.91	43.47	4.41	191.64	0.735	No	No	0.90
4756	47.56	70.34	2.56	3.75	0.90	43.56	4.26	185.51	0.674	No	No	0.83
4757	47.57	70.43	2.56	3.70	0.90	43.64	4.13	180.20	0.624	No	No	0.77
4758	47.58	70.45	2.55	3.66	0.90	43.68	4.03	176.10	0.588	No	No	0.72
4759	47.59	70.41	2.55	3.62	0.90	43.66	3.96	172.80	0.560	No	No	0.69
4760	47.60	70.29	2.55	3.59	0.90	43.59	3.89	169.77	0.535	No	No	0.66
4761	47.61	70.15	2.55	3.55	0.90	43.51	3.82	166.36	0.508	No	No	0.63
4762	47.62	69.99	2.54	3.50	0.90	43.42	3.75	162.69	0.480	No	No	0.59
4763	47.63	69.83	2.54	3.46	0.89	43.33	3.67	158.97	0.454	No	No	0.56
4764	47.64	69.67	2.54	3.41	0.89	43.25	3.59	155.39	0.429	No	No	0.53
4765	47.65	69.53	2.53	3.37	0.89	43.16	3.52	152.12	0.407	No	No	0.50
4766	47.66	69.44	2.53	3.34	0.89	43.11	3.46	149.29	0.389	No	No	0.48
4767	47.67	69.56	2.53	3.31	0.89	43.21	3.39	146.49	0.372	No	No	0.46
4768	47.68	69.92	2.52	3.29	0.89	43.46	3.30	143.35	0.354	No	No	0.44
4769	47.69	70.52	2.52	3.26	0.89	43.88	3.18	139.57	0.333	No	No	0.41
4770	47.70	71.19	2.51	3.23	0.88	44.35	3.05	135.39	0.311	No	No	0.38
4771	47.71	71.90	2.51	3.20	0.88	44.85	2.92	131.08	0.289	No	No	0.36
4772	47.72	72.62	2.50	3.17	0.88	45.36	2.98	134.99	0.309	No	No	0.38
4773	47.73	73.31	2.49	3.13	0.88	45.84	2.93	134.48	0.306	No	No	0.38
4774	47.74	73.93	2.49	3.11	0.87	46.28	2.90	134.00	0.304	No	No	0.37
4775	47.75	74.39	2.48	3.08	0.87	46.61	2.87	133.57	0.302	No	No	0.37
4776	47.76	74.68	2.48	3.06	0.87	46.81	2.84	133.10	0.299	No	No	0.37
4777	47.77	74.82	2.48	3.04	0.87	46.92	2.82	132.52	0.296	No	No	0.37
4778	47.78	74.93	2.47	3.02	0.87	47.00	2.80	131.83	0.293	No	No	0.36
4779	47.79	75.04	2.47	2.99	0.87	47.09	2.78	131.06	0.289	No	No	0.36
4780	47.80	75.16	2.47	2.96	0.87	47.19	2.76	130.25	0.286	No	No	0.35
4781	47.81	75.28	2.46	2.93	0.87	47.28	2.74	129.46	0.282	No	No	0.35
4782	47.82	75.39	2.46	2.90	0.86	47.37	2.72	128.71	0.278	No	No	0.34
4783	47.83	75.49	2.46	2.88	0.86	47.45	2.70	128.05	0.275	No	No	0.34
4784	47.84	75.42	2.46	2.86	0.86	47.41	2.69	127.54	0.273	No	No	0.34
4785	47.85	75.14	2.46	2.85	0.86	47.22	2.69	127.13	0.271	No	No	0.33
4786	47.86	74.62	2.46	2.85	0.86	46.85	2.71	126.77	0.269	No	No	0.33
4787	47.87	73.99	2.46	2.85	0.86	46.41	2.72	126.36	0.268	No	No	0.33
4788	47.88	73.31	2.46	2.84	0.87	45.94	2.74	125.92	0.266	No	No	0.33
4789	47.89	72.62	2.47	2.84	0.87	45.45	2.76	125.47	0.264	No	No	0.33
4790	47.90	71.94	2.47	2.84	0.87	44.98	2.78	125.03	0.262	No	No	0.32
4791	47.91	71.32	2.47	2.84	0.87	44.55	2.80	124.63	0.260	No	No	0.32
4792	47.92	70.80	2.48	2.84	0.87	44.18	2.81	124.34	0.259	No	No	0.32
4793	47.93	70.40	2.48	2.85	0.87	43.89	2.84	124.45	0.259	No	No	0.32
4794	47.94	70.07	2.48	2.87	0.87	43.63	2.86	124.99	0.262	No	No	0.32
4795	47.95	69.74	2.49	2.91	0.88	43.37	2.90	125.92	0.266	No	No	0.33
4796	47.96	69.37	2.50	2.95	0.88	43.08	2.95	126.96	0.270	No	No	0.33
4797	47.97	68.98	2.50	3.00	0.88	42.77	2.84	121.68	0.248	No	No	0.31
4798	47.98	68.59	2.51	3.05	0.88	42.46	2.98	126.44	0.268	No	No	0.33
4799	47.99	68.21	2.52	3.09	0.89	42.17	3.11	131.11	0.290	No	No	0.36
4800	48.00	67.88	2.52	3.13	0.89	41.90	3.23	135.41	0.311	No	No	0.38

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _k (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4801	48.01	67.55	2.53	3.17	0.89	41.65	3.35	139.55	0.333	No	No	0.41
4802	48.02	67.16	2.53	3.21	0.89	41.35	3.49	144.41	0.360	No	No	0.45
4803	48.03	66.66	2.54	3.26	0.90	40.96	3.68	150.73	0.398	No	No	0.49
4804	48.04	66.04	2.55	3.33	0.90	40.49	3.92	158.74	0.452	No	No	0.56
4805	48.05	65.36	2.56	3.40	0.90	39.98	4.20	167.91	0.520	No	No	0.64
4806	48.06	64.65	2.57	3.48	0.91	39.45	4.51	177.84	0.603	No	No	0.75
4807	48.07	63.94	2.58	3.55	0.91	38.92	4.83	188.05	0.698	No	No	0.86
4808	48.08	63.28	2.59	3.63	0.91	38.43	5.15	197.99	0.802	No	No	0.99
4809	48.09	62.70	2.60	3.69	0.92	38.00	5.45	207.03	3.600	No	No	2.00
4810	48.10	62.22	2.61	3.74	0.92	37.64	5.70	214.70	3.600	No	No	2.00
4811	48.11	61.77	2.61	3.79	0.92	37.31	5.94	221.80	3.600	No	No	2.00
4812	48.12	61.29	2.62	3.83	0.93	36.96	6.20	229.32	3.600	No	No	2.00
4813	48.13	60.75	2.63	3.89	0.93	36.56	6.52	238.18	3.600	No	No	2.00
4814	48.14	60.15	2.64	3.95	0.93	36.13	6.87	248.02	3.600	No	No	2.00
4815	48.15	59.55	2.65	4.01	0.94	35.69	7.24	258.40	3.600	No	No	2.00
4816	48.16	58.96	2.65	4.07	0.94	35.26	7.62	268.79	3.600	No	No	2.00
4817	48.17	58.42	2.66	4.12	0.94	34.87	7.99	278.62	3.600	No	No	2.00
4818	48.18	57.97	2.67	4.16	0.94	34.55	8.30	286.73	3.600	No	No	2.00
4819	48.19	57.65	2.67	4.18	0.94	34.33	8.48	291.23	3.600	No	No	2.00
4820	48.20	57.43	2.67	4.18	0.95	34.17	8.56	292.40	3.600	No	No	2.00
4821	48.21	57.25	2.67	4.17	0.95	34.05	8.56	291.37	3.600	No	No	2.00
4822	48.22	57.04	2.67	4.15	0.95	33.91	8.56	290.20	3.600	No	No	2.00
4823	48.23	56.82	2.67	4.13	0.95	33.77	8.56	288.96	3.600	No	No	2.00
4824	48.24	56.60	2.67	4.11	0.95	33.62	8.56	287.72	3.600	No	No	2.00
4825	48.25	56.39	2.67	4.09	0.95	33.49	8.56	286.54	3.600	No	No	2.00
4826	48.26	56.20	2.67	4.08	0.95	33.36	8.56	285.49	3.600	No	No	2.00
4827	48.27	56.11	2.67	4.06	0.95	33.31	8.50	283.02	4.000	Yes	No	2.00
4828	48.28	56.20	2.67	4.01	0.94	33.37	8.31	277.22	4.000	Yes	No	2.00
4829	48.29	56.46	2.66	3.95	0.94	33.56	7.97	267.51	4.000	Yes	No	2.00
4830	48.30	56.82	2.65	3.87	0.94	33.83	7.54	255.18	4.000	Yes	No	2.00
4831	48.31	57.23	2.64	3.78	0.93	34.14	7.09	241.99	4.000	Yes	No	2.00
4832	48.32	57.64	2.63	3.69	0.93	34.45	6.64	228.72	4.000	Yes	No	2.00
4833	48.33	58.06	2.62	3.59	0.93	34.77	6.21	216.05	4.000	Yes	No	2.00
4834	48.34	58.45	2.61	3.51	0.92	35.06	5.84	204.59	4.000	Yes	No	2.00
4835	48.35	58.79	2.60	3.43	0.92	35.32	5.52	194.85	4.000	Yes	No	2.00
4836	48.36	59.16	2.60	3.37	0.92	35.60	5.24	186.45	4.000	Yes	No	2.00
4837	48.37	59.64	2.59	3.31	0.91	35.94	4.96	178.22	4.000	Yes	No	2.00
4838	48.38	60.28	2.58	3.24	0.91	36.40	4.65	169.13	4.000	Yes	No	2.00
4839	48.39	61.02	2.56	3.16	0.90	36.94	4.31	159.04	4.000	Yes	No	2.00
4840	48.40	61.82	2.55	3.08	0.90	37.52	3.96	148.64	4.000	Yes	No	2.00
4841	48.41	62.64	2.54	3.00	0.90	38.11	3.63	138.51	4.000	Yes	No	2.00
4842	48.42	63.43	2.53	2.92	0.89	38.70	3.34	129.15	4.000	Yes	No	2.00
4843	48.43	64.16	2.51	2.84	0.89	39.23	3.08	120.95	4.000	Yes	No	2.00
4844	48.44	64.78	2.50	2.78	0.88	39.69	2.88	114.39	4.000	Yes	No	2.00
4845	48.45	65.33	2.50	2.73	0.88	40.09	2.95	118.35	4.000	Yes	No	2.00
4846	48.46	65.88	2.49	2.70	0.88	40.48	2.90	117.60	4.000	Yes	No	2.00
4847	48.47	66.51	2.48	2.66	0.87	40.93	2.86	116.94	4.000	Yes	No	2.00
4848	48.48	67.22	2.47	2.63	0.87	41.43	2.80	116.20	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4849	48.49	67.97	2.47	2.59	0.87	41.97	2.75	115.40	4.000	Yes	No	2.00
4850	48.50	68.72	2.46	2.55	0.86	42.51	2.70	114.59	4.000	Yes	No	2.00
4851	48.51	69.43	2.45	2.51	0.86	43.02	2.65	113.81	4.000	Yes	No	2.00
4852	48.52	70.07	2.44	2.47	0.86	43.48	2.60	113.11	4.000	Yes	No	2.00
4853	48.53	70.56	2.44	2.45	0.86	43.83	2.57	112.65	4.000	Yes	No	2.00
4854	48.54	70.90	2.43	2.44	0.86	44.06	2.55	112.53	0.213	No	No	0.26
4855	48.55	71.12	2.43	2.44	0.85	44.20	2.55	112.72	0.213	No	No	0.27
4856	48.56	71.34	2.43	2.45	0.85	44.34	2.55	113.06	0.214	No	No	0.27
4857	48.57	71.58	2.43	2.46	0.85	44.48	2.55	113.43	0.216	No	No	0.27
4858	48.58	71.83	2.43	2.47	0.85	44.64	2.55	113.82	0.217	No	No	0.27
4859	48.59	72.08	2.43	2.48	0.85	44.79	2.55	114.20	0.219	No	No	0.27
4860	48.60	72.31	2.43	2.49	0.85	44.93	2.55	114.55	0.220	No	No	0.27
4861	48.61	72.51	2.43	2.50	0.85	45.05	2.55	114.87	0.221	No	No	0.28
4862	48.62	72.55	2.43	2.52	0.86	45.05	2.57	115.56	4.000	Yes	No	2.00
4863	48.63	72.40	2.44	2.56	0.86	44.90	2.60	116.81	4.000	Yes	No	2.00
4864	48.64	72.07	2.45	2.64	0.86	44.60	2.66	118.74	4.000	Yes	No	2.00
4865	48.65	71.68	2.46	2.72	0.87	44.25	2.73	120.98	4.000	Yes	No	2.00
4866	48.66	71.26	2.47	2.81	0.87	43.88	2.81	123.37	4.000	Yes	No	2.00
4867	48.67	70.83	2.49	2.90	0.88	43.51	2.89	125.80	4.000	Yes	No	2.00
4868	48.68	70.41	2.50	2.99	0.88	43.15	2.97	128.13	4.000	Yes	No	2.00
4869	48.69	70.03	2.51	3.07	0.88	42.82	2.98	127.53	4.000	Yes	No	2.00
4870	48.70	69.69	2.52	3.15	0.89	42.54	3.17	134.68	4.000	Yes	No	2.00
4871	48.71	69.36	2.53	3.23	0.89	42.24	3.38	142.90	4.000	Yes	No	2.00
4872	48.72	68.97	2.54	3.34	0.90	41.91	3.66	153.58	4.000	Yes	No	2.00
4873	48.73	68.51	2.56	3.47	0.90	41.50	4.04	167.75	4.000	Yes	No	2.00
4874	48.74	67.98	2.57	3.62	0.91	41.04	4.50	184.52	4.000	Yes	No	2.00
4875	48.75	67.43	2.59	3.78	0.91	40.57	5.01	203.24	4.000	Yes	No	2.00
4876	48.76	66.87	2.60	3.94	0.92	40.10	5.56	223.05	4.000	Yes	No	2.00
4877	48.77	66.34	2.62	4.10	0.93	39.66	6.12	242.90	4.000	Yes	No	2.00
4878	48.78	65.87	2.63	4.23	0.93	39.27	6.66	261.52	4.000	Yes	No	2.00
4879	48.79	65.46	2.64	4.35	0.94	38.93	7.13	277.77	4.000	Yes	No	2.00
4880	48.80	65.06	2.65	4.45	0.94	38.62	7.59	292.98	4.000	Yes	No	2.00
4881	48.81	64.62	2.66	4.56	0.94	38.27	8.08	309.21	4.000	Yes	No	2.00
4882	48.82	64.11	2.67	4.68	0.95	37.88	8.67	328.56	4.000	Yes	No	2.00
4883	48.83	63.55	2.69	4.82	0.95	37.44	9.36	350.61	4.000	Yes	No	2.00
4884	48.84	62.97	2.70	4.96	0.96	37.00	10.12	374.40	4.000	Yes	No	2.00
4885	48.85	62.40	2.71	5.09	0.96	36.56	4.82	176.37	4.000	Yes	Yes	2.00
4886	48.86	61.86	2.72	5.22	0.97	36.16	4.94	178.76	4.000	Yes	Yes	2.00
4887	48.87	61.39	2.73	5.34	0.97	35.80	5.05	180.80	4.000	Yes	Yes	2.00
4888	48.88	61.10	2.74	5.41	0.97	35.58	5.12	182.16	4.000	Yes	Yes	2.00
4889	48.89	60.97	2.74	5.46	0.97	35.47	5.16	182.98	4.000	Yes	Yes	2.00
4890	48.90	60.97	2.74	5.48	0.97	35.45	5.17	183.44	1.691	No	Yes	2.00
4891	48.91	60.97	2.74	5.50	0.97	35.44	5.19	183.94	1.690	No	Yes	2.00
4892	48.92	60.97	2.75	5.53	0.97	35.42	5.21	184.48	1.689	No	Yes	2.00
4893	48.93	60.97	2.75	5.55	0.98	35.40	5.23	185.04	1.689	No	Yes	2.00
4894	48.94	60.97	2.75	5.58	0.98	35.38	5.24	185.57	1.688	No	Yes	2.00
4895	48.95	60.97	2.75	5.60	0.98	35.37	5.26	186.06	1.687	No	Yes	2.00
4896	48.96	61.06	2.75	5.61	0.98	35.41	5.26	186.42	4.000	Yes	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4897	48.97	61.50	2.75	5.59	0.98	35.70	5.23	186.54	4.000	Yes	Yes	2.00
4898	48.98	62.38	2.74	5.54	0.97	36.27	5.14	186.41	4.000	Yes	Yes	2.00
4899	48.99	63.66	2.73	5.47	0.97	37.12	5.01	186.06	4.000	Yes	Yes	2.00
4900	49.00	65.09	2.72	5.38	0.96	38.07	4.88	185.60	4.000	Yes	Yes	2.00
4901	49.01	66.60	2.70	5.29	0.96	39.07	4.74	185.02	4.000	Yes	Yes	2.00
4902	49.02	68.12	2.69	5.20	0.95	40.08	9.55	382.82	4.000	Yes	No	2.00
4903	49.03	69.55	2.68	5.12	0.95	41.04	8.85	363.05	4.000	Yes	No	2.00
4904	49.04	70.84	2.67	5.04	0.94	41.91	8.26	346.16	4.000	Yes	No	2.00
4905	49.05	72.07	2.66	4.97	0.94	42.73	7.74	330.89	4.000	Yes	No	2.00
4906	49.06	73.50	2.64	4.89	0.94	43.69	7.20	314.35	4.000	Yes	No	2.00
4907	49.07	75.30	2.63	4.80	0.93	44.91	6.56	294.77	4.000	Yes	No	2.00
4908	49.08	77.48	2.61	4.68	0.92	46.39	5.88	272.62	4.000	Yes	No	2.00
4909	49.09	79.88	2.59	4.56	0.92	48.03	5.21	250.02	4.000	Yes	No	2.00
4910	49.10	82.36	2.57	4.43	0.91	49.73	4.59	228.32	4.000	Yes	No	2.00
4911	49.11	84.80	2.56	4.31	0.90	51.42	4.06	208.54	4.000	Yes	No	2.00
4912	49.12	87.08	2.54	4.19	0.90	53.00	3.61	191.40	4.000	Yes	No	2.00
4913	49.13	89.06	2.52	4.09	0.89	54.38	3.26	177.41	4.000	Yes	No	2.00
4914	49.14	90.94	2.51	4.01	0.88	55.69	2.98	165.76	4.000	Yes	No	2.00
4915	49.15	92.99	2.49	3.92	0.88	57.11	2.94	168.13	4.000	Yes	No	2.00
4916	49.16	95.46	2.48	3.83	0.87	58.83	2.84	166.88	4.000	Yes	No	2.00
4917	49.17	98.30	2.46	3.73	0.87	60.82	2.72	165.39	4.000	Yes	No	2.00
4918	49.18	101.35	2.44	3.62	0.86	62.97	2.60	163.72	4.000	Yes	No	2.00
4919	49.19	104.46	2.42	3.51	0.85	65.17	2.49	161.97	4.000	Yes	No	2.00
4920	49.20	107.46	2.40	3.41	0.84	67.30	2.38	160.25	4.000	Yes	No	2.00
4921	49.21	110.20	2.38	3.31	0.84	69.27	2.29	158.65	4.000	Yes	No	2.00
4922	49.22	112.54	2.37	3.23	0.83	70.95	2.22	157.36	4.000	Yes	No	2.00
4923	49.23	114.65	2.36	3.17	0.83	72.46	2.16	156.48	4.000	Yes	No	2.00
4924	49.24	116.81	2.34	3.11	0.82	74.00	2.11	155.90	4.000	Yes	No	2.00
4925	49.25	119.31	2.33	3.06	0.82	75.77	2.05	155.43	4.000	Yes	No	2.00
4926	49.26	122.10	2.32	2.99	0.81	77.77	1.99	154.93	4.000	Yes	No	2.00
4927	49.27	125.05	2.30	2.93	0.81	79.89	1.93	154.43	4.000	Yes	No	2.00
4928	49.28	127.99	2.29	2.86	0.80	82.02	1.88	153.98	4.000	Yes	No	2.00
4929	49.29	130.79	2.27	2.80	0.79	84.06	1.83	153.61	4.000	Yes	No	2.00
4930	49.30	133.29	2.26	2.74	0.79	85.88	1.79	153.30	4.000	Yes	No	2.00
4931	49.31	135.27	2.25	2.70	0.79	87.32	1.75	153.19	4.000	Yes	No	2.00
4932	49.32	136.86	2.24	2.67	0.78	88.46	1.73	153.30	4.000	Yes	No	2.00
4933	49.33	138.28	2.24	2.66	0.78	89.46	1.72	153.64	4.000	Yes	No	2.00
4934	49.34	139.85	2.23	2.64	0.78	90.57	1.70	154.10	4.000	Yes	No	2.00
4935	49.35	141.56	2.23	2.62	0.78	91.79	1.68	154.62	4.000	Yes	No	2.00
4936	49.36	143.34	2.22	2.61	0.78	93.05	1.67	155.17	4.000	Yes	No	2.00
4937	49.37	145.09	2.21	2.59	0.77	94.29	1.65	155.72	4.000	Yes	No	2.00
4938	49.38	146.71	2.21	2.57	0.77	95.44	1.64	156.25	4.000	Yes	No	2.00
4939	49.39	148.13	2.20	2.56	0.77	96.44	1.62	156.72	4.000	Yes	No	2.00
4940	49.40	149.24	2.20	2.56	0.77	97.21	1.62	157.21	4.000	Yes	No	2.00
4941	49.41	150.17	2.20	2.56	0.77	97.85	1.61	157.80	0.445	No	No	0.56
4942	49.42	151.06	2.20	2.56	0.77	98.44	1.61	158.56	0.451	No	No	0.57
4943	49.43	152.09	2.20	2.57	0.77	99.12	1.61	159.43	0.457	No	No	0.57
4944	49.44	153.19	2.20	2.58	0.77	99.85	1.61	160.37	0.464	No	No	0.58

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4945	49.45	154.31	2.20	2.59	0.77	100.60	1.60	161.32	0.470	No	No	0.59
4946	49.46	155.40	2.19	2.60	0.77	101.32	1.60	162.25	0.477	No	No	0.60
4947	49.47	156.38	2.19	2.61	0.77	101.97	1.60	163.09	0.483	No	No	0.61
4948	49.48	157.18	2.19	2.61	0.76	102.50	1.60	163.67	0.488	No	No	0.61
4949	49.49	157.71	2.19	2.60	0.76	102.88	1.59	163.72	0.488	No	No	0.61
4950	49.50	158.05	2.19	2.58	0.76	103.15	1.58	163.24	0.485	No	No	0.61
4951	49.51	158.32	2.18	2.54	0.76	103.41	1.57	162.37	0.478	No	No	0.60
4952	49.52	158.62	2.18	2.50	0.76	103.70	1.56	161.43	0.471	No	No	0.59
4953	49.53	158.94	2.17	2.46	0.76	104.01	1.54	160.46	0.464	No	No	0.58
4954	49.54	159.25	2.16	2.42	0.75	104.33	1.53	159.51	0.457	No	No	0.58
4955	49.55	159.55	2.16	2.37	0.75	104.63	1.52	158.62	0.451	No	No	0.57
4956	49.56	159.82	2.15	2.34	0.75	104.89	1.50	157.85	0.446	No	No	0.56
4957	49.57	159.94	2.15	2.31	0.75	105.04	1.50	157.10	0.441	No	No	0.55
4958	49.58	159.84	2.14	2.27	0.75	105.05	1.49	156.21	0.434	No	No	0.55
4959	49.59	159.52	2.14	2.24	0.74	104.91	1.48	155.07	0.427	No	No	0.54
4960	49.60	159.10	2.13	2.19	0.74	104.71	1.47	153.70	0.418	No	No	0.53
4961	49.61	158.63	2.12	2.14	0.74	104.50	1.46	152.23	0.408	No	No	0.51
4962	49.62	158.15	2.12	2.09	0.74	104.28	1.45	150.74	0.399	No	No	0.50
4963	49.63	157.68	2.11	2.05	0.73	104.08	1.43	149.30	0.390	No	No	0.49
4964	49.64	157.24	2.10	2.00	0.73	103.88	1.42	147.99	0.381	No	No	0.48
4965	49.65	156.86	2.10	1.96	0.73	103.71	1.42	146.87	0.375	No	No	0.47
4966	49.66	156.50	2.10	1.94	0.73	103.51	1.41	146.12	0.370	No	No	0.47
4967	49.67	156.12	2.09	1.93	0.73	103.25	1.41	145.65	0.367	No	No	0.46
4968	49.68	155.67	2.10	1.93	0.73	102.91	1.41	145.38	0.366	No	No	0.46
4969	49.69	155.16	2.10	1.93	0.73	102.52	1.42	145.07	0.364	No	No	0.46
4970	49.70	154.60	2.10	1.94	0.73	102.10	1.42	144.74	0.362	No	No	0.46
4971	49.71	154.04	2.10	1.94	0.73	101.67	1.42	144.40	0.360	No	No	0.45
4972	49.72	153.50	2.10	1.94	0.73	101.26	1.42	144.08	0.358	No	No	0.45
4973	49.73	153.01	2.10	1.95	0.73	100.88	1.43	143.79	0.356	No	No	0.45
4974	49.74	152.60	2.11	1.95	0.73	100.56	1.43	143.53	0.355	No	No	0.45
4975	49.75	152.23	2.11	1.95	0.73	100.29	1.43	143.30	0.354	No	No	0.45
4976	49.76	151.87	2.11	1.95	0.73	100.01	1.43	143.05	0.352	No	No	0.44
4977	49.77	151.47	2.11	1.95	0.73	99.71	1.43	142.75	0.351	No	No	0.44
4978	49.78	151.01	2.11	1.95	0.73	99.37	1.43	142.43	0.349	No	No	0.44
4979	49.79	150.53	2.11	1.95	0.73	99.01	1.44	142.09	0.347	No	No	0.44
4980	49.80	150.06	2.11	1.95	0.73	98.65	1.44	141.75	0.345	No	No	0.44
4981	49.81	149.60	2.11	1.95	0.73	98.32	1.44	141.43	0.343	No	No	0.43
4982	49.82	149.20	2.11	1.95	0.74	98.01	1.44	141.15	0.342	No	No	0.43
4983	49.83	148.77	2.12	1.96	0.74	97.68	1.44	140.92	0.340	No	No	0.43
4984	49.84	148.21	2.12	1.97	0.74	97.24	1.45	140.73	0.339	No	No	0.43
4985	49.85	147.45	2.12	1.98	0.74	96.64	1.45	140.57	0.338	No	No	0.43
4986	49.86	146.53	2.13	2.00	0.74	95.92	1.46	140.41	0.337	No	No	0.43
4987	49.87	145.52	2.13	2.02	0.74	95.13	1.47	140.25	0.337	No	No	0.43
4988	49.88	144.48	2.14	2.05	0.75	94.31	1.49	140.10	0.336	No	No	0.42
4989	49.89	143.46	2.15	2.07	0.75	93.52	1.50	139.97	0.335	No	No	0.42
4990	49.90	142.51	2.15	2.09	0.75	92.78	1.51	139.86	0.334	No	No	0.42
4991	49.91	141.69	2.16	2.11	0.75	92.14	1.52	139.77	0.334	No	No	0.42
4992	49.92	141.02	2.16	2.12	0.75	91.61	1.52	139.67	0.333	No	No	0.42

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4993	49.93	140.40	2.16	2.13	0.75	91.14	1.53	139.56	0.333	No	No	0.42
4994	49.94	139.76	2.17	2.15	0.76	90.65	1.54	139.40	0.332	No	No	0.42
4995	49.95	139.02	2.17	2.16	0.76	90.08	1.55	139.24	0.331	No	No	0.42
4996	49.96	138.23	2.17	2.17	0.76	89.48	1.55	139.06	0.330	No	No	0.42
4997	49.97	137.43	2.18	2.18	0.76	88.88	1.56	138.89	0.329	No	No	0.42
4998	49.98	136.66	2.18	2.20	0.76	88.29	1.57	138.74	0.328	No	No	0.42
4999	49.99	135.96	2.19	2.21	0.76	87.76	1.58	138.60	0.328	No	No	0.41
5000	50.00	135.52	2.19	2.21	0.76	87.42	1.58	138.51	0.327	No	No	0.41

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q_t :	Total cone resistance
I_c :	Soil behavior type index
Fr:	Normalized friction ratio (%)
n:	Stress exponent
Q_{tn} :	Normalized cone resistance
K_c :	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Normalized and adjusted cone resistance
CRR _{7.5} :	Cyclic resistance ratio for $M_w=7.5$
FS:	Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
0.01	2.00	0.00	0.00	0.01	0.00	0.02	2.00	0.00	0.00	0.01	0.00
0.03	2.00	0.00	0.00	0.01	0.00	0.04	2.00	0.00	0.00	0.01	0.00
0.05	2.00	0.00	0.00	0.01	0.00	0.06	2.00	0.00	0.00	0.01	0.00
0.07	2.00	0.00	0.00	0.01	0.00	0.08	2.00	0.00	0.00	0.01	0.00
0.09	2.00	0.00	0.00	0.01	0.00	0.10	2.00	0.00	0.00	0.01	0.00
0.11	2.00	0.00	0.00	0.01	0.00	0.12	2.00	0.00	0.00	0.01	0.00
0.13	2.00	0.00	0.00	0.01	0.00	0.14	2.00	0.00	0.00	0.01	0.00
0.15	2.00	0.00	0.00	0.01	0.00	0.16	2.00	0.00	0.00	0.01	0.00
0.17	2.00	0.00	0.00	0.01	0.00	0.18	2.00	0.00	0.00	0.01	0.00
0.19	2.00	0.00	0.00	0.01	0.00	0.20	2.00	0.00	0.00	0.01	0.00
0.21	2.00	0.00	0.00	0.01	0.00	0.22	2.00	0.00	0.00	0.01	0.00
0.23	2.00	0.00	0.00	0.01	0.00	0.24	2.00	0.00	0.00	0.01	0.00
0.25	2.00	0.00	0.00	0.01	0.00	0.26	2.00	0.00	0.00	0.01	0.00
0.27	2.00	0.00	0.00	0.01	0.00	0.28	2.00	0.00	0.00	0.01	0.00
0.29	2.00	0.00	0.00	0.01	0.00	0.30	2.00	0.00	0.00	0.01	0.00
0.31	2.00	0.00	0.00	0.01	0.00	0.32	2.00	0.00	0.00	0.01	0.00
0.33	2.00	0.00	0.00	0.01	0.00	0.34	2.00	0.00	0.00	0.01	0.00
0.35	2.00	0.00	0.00	0.01	0.00	0.36	2.00	0.00	0.00	0.01	0.00
0.37	2.00	0.00	0.00	0.01	0.00	0.38	2.00	0.00	0.00	0.01	0.00
0.39	2.00	0.00	0.00	0.01	0.00	0.40	2.00	0.00	0.00	0.01	0.00
0.41	2.00	0.00	0.00	0.01	0.00	0.42	2.00	0.00	0.00	0.01	0.00
0.43	2.00	0.00	0.00	0.01	0.00	0.44	2.00	0.00	0.00	0.01	0.00
0.45	2.00	0.00	0.00	0.01	0.00	0.46	2.00	0.00	0.00	0.01	0.00
0.47	2.00	0.00	0.00	0.01	0.00	0.48	2.00	0.00	0.00	0.01	0.00
0.49	2.00	0.00	0.00	0.01	0.00	0.50	2.00	0.00	0.00	0.01	0.00
0.51	2.00	0.00	0.00	0.01	0.00	0.52	2.00	0.00	0.00	0.01	0.00
0.53	2.00	0.00	0.00	0.01	0.00	0.54	2.00	0.00	0.00	0.01	0.00
0.55	2.00	0.00	0.00	0.01	0.00	0.56	2.00	0.00	0.00	0.01	0.00
0.57	2.00	0.00	0.00	0.01	0.00	0.58	2.00	0.00	0.00	0.01	0.00
0.59	2.00	0.00	0.00	0.01	0.00	0.60	2.00	0.00	0.00	0.01	0.00
0.61	2.00	0.00	0.00	0.01	0.00	0.62	2.00	0.00	0.00	0.01	0.00
0.63	2.00	0.00	0.00	0.01	0.00	0.64	2.00	0.00	0.00	0.01	0.00
0.65	2.00	0.00	0.00	0.01	0.00	0.66	2.00	0.00	0.00	0.01	0.00
0.67	2.00	0.00	0.00	0.01	0.00	0.68	2.00	0.00	0.00	0.01	0.00
0.69	2.00	0.00	0.00	0.01	0.00	0.70	2.00	0.00	0.00	0.01	0.00
0.71	2.00	0.00	0.00	0.01	0.00	0.72	2.00	0.00	0.00	0.01	0.00
0.73	2.00	0.00	0.00	0.01	0.00	0.74	2.00	0.00	0.00	0.01	0.00
0.75	2.00	0.00	0.00	0.01	0.00	0.76	2.00	0.00	0.00	0.01	0.00
0.77	2.00	0.00	0.00	0.01	0.00	0.78	2.00	0.00	0.00	0.01	0.00
0.79	2.00	0.00	0.00	0.01	0.00	0.80	2.00	0.00	0.00	0.01	0.00
0.81	2.00	0.00	0.00	0.01	0.00	0.82	2.00	0.00	0.00	0.01	0.00
0.83	2.00	0.00	0.00	0.01	0.00	0.84	2.00	0.00	0.00	0.01	0.00
0.85	2.00	0.00	0.00	0.01	0.00	0.86	2.00	0.00	0.00	0.01	0.00
0.87	2.00	0.00	0.00	0.01	0.00	0.88	2.00	0.00	0.00	0.01	0.00
0.89	2.00	0.00	0.00	0.01	0.00	0.90	2.00	0.00	0.00	0.01	0.00
0.91	2.00	0.00	0.00	0.01	0.00	0.92	2.00	0.00	0.00	0.01	0.00
0.93	2.00	0.00	0.00	0.01	0.00	0.94	2.00	0.00	0.00	0.01	0.00
0.95	2.00	0.00	0.00	0.01	0.00	0.96	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
0.97	2.00	0.00	0.00	0.01	0.00	0.98	2.00	0.00	0.00	0.01	0.00
0.99	2.00	0.00	0.00	0.01	0.00	1.00	2.00	0.00	0.00	0.01	0.00
1.01	2.00	0.00	0.00	0.01	0.00	1.02	2.00	0.00	0.00	0.01	0.00
1.03	2.00	0.00	0.00	0.01	0.00	1.04	2.00	0.00	0.00	0.01	0.00
1.05	2.00	0.00	0.00	0.01	0.00	1.06	2.00	0.00	0.00	0.01	0.00
1.07	2.00	0.00	0.00	0.01	0.00	1.08	2.00	0.00	0.00	0.01	0.00
1.09	2.00	0.00	0.00	0.01	0.00	1.10	2.00	0.00	0.00	0.01	0.00
1.11	2.00	0.00	0.00	0.01	0.00	1.12	2.00	0.00	0.00	0.01	0.00
1.13	2.00	0.00	0.00	0.01	0.00	1.14	2.00	0.00	0.00	0.01	0.00
1.15	2.00	0.00	0.00	0.01	0.00	1.16	2.00	0.00	0.00	0.01	0.00
1.17	2.00	0.00	0.00	0.01	0.00	1.18	2.00	0.00	0.00	0.01	0.00
1.19	2.00	0.00	0.00	0.01	0.00	1.20	2.00	0.00	0.00	0.01	0.00
1.21	2.00	0.00	0.00	0.01	0.00	1.22	2.00	0.00	0.00	0.01	0.00
1.23	2.00	0.00	0.00	0.01	0.00	1.24	2.00	0.00	0.00	0.01	0.00
1.25	2.00	0.00	0.00	0.01	0.00	1.26	2.00	0.00	0.00	0.01	0.00
1.27	2.00	0.00	0.00	0.01	0.00	1.28	2.00	0.00	0.00	0.01	0.00
1.29	2.00	0.00	0.00	0.01	0.00	1.30	2.00	0.00	0.00	0.01	0.00
1.31	2.00	0.00	0.00	0.01	0.00	1.32	2.00	0.00	0.00	0.01	0.00
1.33	2.00	0.00	0.00	0.01	0.00	1.34	2.00	0.00	0.00	0.01	0.00
1.35	2.00	0.00	0.00	0.01	0.00	1.36	2.00	0.00	0.00	0.01	0.00
1.37	2.00	0.00	0.00	0.01	0.00	1.38	2.00	0.00	0.00	0.01	0.00
1.39	2.00	0.00	0.00	0.01	0.00	1.40	2.00	0.00	0.00	0.01	0.00
1.41	2.00	0.00	0.00	0.01	0.00	1.42	2.00	0.00	0.00	0.01	0.00
1.43	2.00	0.00	0.00	0.01	0.00	1.44	2.00	0.00	0.00	0.01	0.00
1.45	2.00	0.00	0.00	0.01	0.00	1.46	2.00	0.00	0.00	0.01	0.00
1.47	2.00	0.00	0.00	0.01	0.00	1.48	2.00	0.00	0.00	0.01	0.00
1.49	2.00	0.00	0.00	0.01	0.00	1.50	2.00	0.00	0.00	0.01	0.00
1.51	2.00	0.00	0.00	0.01	0.00	1.52	2.00	0.00	0.00	0.01	0.00
1.53	2.00	0.00	0.00	0.01	0.00	1.54	2.00	0.00	0.00	0.01	0.00
1.55	2.00	0.00	0.00	0.01	0.00	1.56	2.00	0.00	0.00	0.01	0.00
1.57	2.00	0.00	0.00	0.01	0.00	1.58	2.00	0.00	0.00	0.01	0.00
1.59	2.00	0.00	0.00	0.01	0.00	1.60	2.00	0.00	0.00	0.01	0.00
1.61	2.00	0.00	0.00	0.01	0.00	1.62	2.00	0.00	0.00	0.01	0.00
1.63	2.00	0.00	0.00	0.01	0.00	1.64	2.00	0.00	0.00	0.01	0.00
1.65	2.00	0.00	0.00	0.01	0.00	1.66	2.00	0.00	0.00	0.01	0.00
1.67	2.00	0.00	0.00	0.01	0.00	1.68	2.00	0.00	0.00	0.01	0.00
1.69	2.00	0.00	0.00	0.01	0.00	1.70	2.00	0.00	0.00	0.01	0.00
1.71	2.00	0.00	0.00	0.01	0.00	1.72	2.00	0.00	0.00	0.01	0.00
1.73	2.00	0.00	0.00	0.01	0.00	1.74	2.00	0.00	0.00	0.01	0.00
1.75	2.00	0.00	0.00	0.01	0.00	1.76	2.00	0.00	0.00	0.01	0.00
1.77	2.00	0.00	0.00	0.01	0.00	1.78	2.00	0.00	0.00	0.01	0.00
1.79	2.00	0.00	0.00	0.01	0.00	1.80	2.00	0.00	0.00	0.01	0.00
1.81	2.00	0.00	0.00	0.01	0.00	1.82	2.00	0.00	0.00	0.01	0.00
1.83	2.00	0.00	0.00	0.01	0.00	1.84	2.00	0.00	0.00	0.01	0.00
1.85	2.00	0.00	0.00	0.01	0.00	1.86	2.00	0.00	0.00	0.01	0.00
1.87	2.00	0.00	0.00	0.01	0.00	1.88	2.00	0.00	0.00	0.01	0.00
1.89	2.00	0.00	0.00	0.01	0.00	1.90	2.00	0.00	0.00	0.01	0.00
1.91	2.00	0.00	0.00	0.01	0.00	1.92	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
1.93	2.00	0.00	0.00	0.01	0.00	1.94	2.00	0.00	0.00	0.01	0.00
1.95	2.00	0.00	0.00	0.01	0.00	1.96	2.00	0.00	0.00	0.01	0.00
1.97	2.00	0.00	0.00	0.01	0.00	1.98	2.00	0.00	0.00	0.01	0.00
1.99	2.00	0.00	0.00	0.01	0.00	2.00	2.00	0.00	0.00	0.01	0.00
2.01	2.00	0.00	0.00	0.01	0.00	2.02	2.00	0.00	0.00	0.01	0.00
2.03	2.00	0.00	0.00	0.01	0.00	2.04	2.00	0.00	0.00	0.01	0.00
2.05	2.00	0.00	0.00	0.01	0.00	2.06	2.00	0.00	0.00	0.01	0.00
2.07	2.00	0.00	0.00	0.01	0.00	2.08	2.00	0.00	0.00	0.01	0.00
2.09	2.00	0.00	0.00	0.01	0.00	2.10	2.00	0.00	0.00	0.01	0.00
2.11	2.00	0.00	0.00	0.01	0.00	2.12	2.00	0.00	0.00	0.01	0.00
2.13	2.00	0.00	0.00	0.01	0.00	2.14	2.00	0.00	0.00	0.01	0.00
2.15	2.00	0.00	0.00	0.01	0.00	2.16	2.00	0.00	0.00	0.01	0.00
2.17	2.00	0.00	0.00	0.01	0.00	2.18	2.00	0.00	0.00	0.01	0.00
2.19	2.00	0.00	0.00	0.01	0.00	2.20	2.00	0.00	0.00	0.01	0.00
2.21	2.00	0.00	0.00	0.01	0.00	2.22	2.00	0.00	0.00	0.01	0.00
2.23	2.00	0.00	0.00	0.01	0.00	2.24	2.00	0.00	0.00	0.01	0.00
2.25	2.00	0.00	0.00	0.01	0.00	2.26	2.00	0.00	0.00	0.01	0.00
2.27	2.00	0.00	0.00	0.01	0.00	2.28	2.00	0.00	0.00	0.01	0.00
2.29	2.00	0.00	0.00	0.01	0.00	2.30	2.00	0.00	0.00	0.01	0.00
2.31	2.00	0.00	0.00	0.01	0.00	2.32	2.00	0.00	0.00	0.01	0.00
2.33	2.00	0.00	0.00	0.01	0.00	2.34	2.00	0.00	0.00	0.01	0.00
2.35	2.00	0.00	0.00	0.01	0.00	2.36	2.00	0.00	0.00	0.01	0.00
2.37	2.00	0.00	0.00	0.01	0.00	2.38	2.00	0.00	0.00	0.01	0.00
2.39	2.00	0.00	0.00	0.01	0.00	2.40	2.00	0.00	0.00	0.01	0.00
2.41	2.00	0.00	0.00	0.01	0.00	2.42	2.00	0.00	0.00	0.01	0.00
2.43	2.00	0.00	0.00	0.01	0.00	2.44	2.00	0.00	0.00	0.01	0.00
2.45	2.00	0.00	0.00	0.01	0.00	2.46	2.00	0.00	0.00	0.01	0.00
2.47	2.00	0.00	0.00	0.01	0.00	2.48	2.00	0.00	0.00	0.01	0.00
2.49	2.00	0.00	0.00	0.01	0.00	2.50	2.00	0.00	0.00	0.01	0.00
2.51	2.00	0.00	0.00	0.01	0.00	2.52	2.00	0.00	0.00	0.01	0.00
2.53	2.00	0.00	0.00	0.01	0.00	2.54	2.00	0.00	0.00	0.01	0.00
2.55	2.00	0.00	0.00	0.01	0.00	2.56	2.00	0.00	0.00	0.01	0.00
2.57	2.00	0.00	0.00	0.01	0.00	2.58	2.00	0.00	0.00	0.01	0.00
2.59	2.00	0.00	0.00	0.01	0.00	2.60	2.00	0.00	0.00	0.01	0.00
2.61	2.00	0.00	0.00	0.01	0.00	2.62	2.00	0.00	0.00	0.01	0.00
2.63	2.00	0.00	0.00	0.01	0.00	2.64	2.00	0.00	0.00	0.01	0.00
2.65	2.00	0.00	0.00	0.01	0.00	2.66	2.00	0.00	0.00	0.01	0.00
2.67	2.00	0.00	0.00	0.01	0.00	2.68	2.00	0.00	0.00	0.01	0.00
2.69	2.00	0.00	0.00	0.01	0.00	2.70	2.00	0.00	0.00	0.01	0.00
2.71	2.00	0.00	0.00	0.01	0.00	2.72	2.00	0.00	0.00	0.01	0.00
2.73	2.00	0.00	0.00	0.01	0.00	2.74	2.00	0.00	0.00	0.01	0.00
2.75	2.00	0.00	0.00	0.01	0.00	2.76	2.00	0.00	0.00	0.01	0.00
2.77	2.00	0.00	0.00	0.01	0.00	2.78	2.00	0.00	0.00	0.01	0.00
2.79	2.00	0.00	0.00	0.01	0.00	2.80	2.00	0.00	0.00	0.01	0.00
2.81	2.00	0.00	0.00	0.01	0.00	2.82	2.00	0.00	0.00	0.01	0.00
2.83	2.00	0.00	0.00	0.01	0.00	2.84	2.00	0.00	0.00	0.01	0.00
2.85	2.00	0.00	0.00	0.01	0.00	2.86	2.00	0.00	0.00	0.01	0.00
2.87	2.00	0.00	0.00	0.01	0.00	2.88	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
2.89	2.00	0.00	0.00	0.01	0.00	2.90	2.00	0.00	0.00	0.01	0.00
2.91	2.00	0.00	0.00	0.01	0.00	2.92	2.00	0.00	0.00	0.01	0.00
2.93	2.00	0.00	0.00	0.01	0.00	2.94	2.00	0.00	0.00	0.01	0.00
2.95	2.00	0.00	0.00	0.01	0.00	2.96	2.00	0.00	0.00	0.01	0.00
2.97	2.00	0.00	0.00	0.01	0.00	2.98	2.00	0.00	0.00	0.01	0.00
2.99	2.00	0.00	0.00	0.01	0.00	3.00	2.00	0.00	0.00	0.01	0.00
3.01	2.00	0.00	0.00	0.01	0.00	3.02	2.00	0.00	0.00	0.01	0.00
3.03	2.00	0.00	0.00	0.01	0.00	3.04	2.00	0.00	0.00	0.01	0.00
3.05	2.00	0.00	0.00	0.01	0.00	3.06	2.00	0.00	0.00	0.01	0.00
3.07	2.00	0.00	0.00	0.01	0.00	3.08	2.00	0.00	0.00	0.01	0.00
3.09	2.00	0.00	0.00	0.01	0.00	3.10	2.00	0.00	0.00	0.01	0.00
3.11	2.00	0.00	0.00	0.01	0.00	3.12	2.00	0.00	0.00	0.01	0.00
3.13	2.00	0.00	0.00	0.01	0.00	3.14	2.00	0.00	0.00	0.01	0.00
3.15	2.00	0.00	0.00	0.01	0.00	3.16	2.00	0.00	0.00	0.01	0.00
3.17	2.00	0.00	0.00	0.01	0.00	3.18	2.00	0.00	0.00	0.01	0.00
3.19	2.00	0.00	0.00	0.01	0.00	3.20	2.00	0.00	0.00	0.01	0.00
3.21	2.00	0.00	0.00	0.01	0.00	3.22	2.00	0.00	0.00	0.01	0.00
3.23	2.00	0.00	0.00	0.01	0.00	3.24	2.00	0.00	0.00	0.01	0.00
3.25	2.00	0.00	0.00	0.01	0.00	3.26	2.00	0.00	0.00	0.01	0.00
3.27	2.00	0.00	0.00	0.01	0.00	3.28	2.00	0.00	0.00	0.01	0.00
3.29	2.00	0.00	0.00	0.01	0.00	3.30	2.00	0.00	0.00	0.01	0.00
3.31	2.00	0.00	0.00	0.01	0.00	3.32	2.00	0.00	0.00	0.01	0.00
3.33	2.00	0.00	0.00	0.01	0.00	3.34	2.00	0.00	0.00	0.01	0.00
3.35	2.00	0.00	0.00	0.01	0.00	3.36	2.00	0.00	0.00	0.01	0.00
3.37	2.00	0.00	0.00	0.01	0.00	3.38	2.00	0.00	0.00	0.01	0.00
3.39	2.00	0.00	0.00	0.01	0.00	3.40	2.00	0.00	0.00	0.01	0.00
3.41	2.00	0.00	0.00	0.01	0.00	3.42	2.00	0.00	0.00	0.01	0.00
3.43	2.00	0.00	0.00	0.01	0.00	3.44	2.00	0.00	0.00	0.01	0.00
3.45	2.00	0.00	0.00	0.01	0.00	3.46	2.00	0.00	0.00	0.01	0.00
3.47	2.00	0.00	0.00	0.01	0.00	3.48	2.00	0.00	0.00	0.01	0.00
3.49	2.00	0.00	0.00	0.01	0.00	3.50	2.00	0.00	0.00	0.01	0.00
3.51	2.00	0.00	0.00	0.01	0.00	3.52	2.00	0.00	0.00	0.01	0.00
3.53	2.00	0.00	0.00	0.01	0.00	3.54	2.00	0.00	0.00	0.01	0.00
3.55	2.00	0.00	0.00	0.01	0.00	3.56	2.00	0.00	0.00	0.01	0.00
3.57	2.00	0.00	0.00	0.01	0.00	3.58	2.00	0.00	0.00	0.01	0.00
3.59	2.00	0.00	0.00	0.01	0.00	3.60	2.00	0.00	0.00	0.01	0.00
3.61	2.00	0.00	0.00	0.01	0.00	3.62	2.00	0.00	0.00	0.01	0.00
3.63	2.00	0.00	0.00	0.01	0.00	3.64	2.00	0.00	0.00	0.01	0.00
3.65	2.00	0.00	0.00	0.01	0.00	3.66	2.00	0.00	0.00	0.01	0.00
3.67	2.00	0.00	0.00	0.01	0.00	3.68	2.00	0.00	0.00	0.01	0.00
3.69	2.00	0.00	0.00	0.01	0.00	3.70	2.00	0.00	0.00	0.01	0.00
3.71	2.00	0.00	0.00	0.01	0.00	3.72	2.00	0.00	0.00	0.01	0.00
3.73	2.00	0.00	0.00	0.01	0.00	3.74	2.00	0.00	0.00	0.01	0.00
3.75	2.00	0.00	0.00	0.01	0.00	3.76	2.00	0.00	0.00	0.01	0.00
3.77	2.00	0.00	0.00	0.01	0.00	3.78	2.00	0.00	0.00	0.01	0.00
3.79	2.00	0.00	0.00	0.01	0.00	3.80	2.00	0.00	0.00	0.01	0.00
3.81	2.00	0.00	0.00	0.01	0.00	3.82	2.00	0.00	0.00	0.01	0.00
3.83	2.00	0.00	0.00	0.01	0.00	3.84	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
3.85	2.00	0.00	0.00	0.01	0.00	3.86	2.00	0.00	0.00	0.01	0.00
3.87	2.00	0.00	0.00	0.01	0.00	3.88	2.00	0.00	0.00	0.01	0.00
3.89	2.00	0.00	0.00	0.01	0.00	3.90	2.00	0.00	0.00	0.01	0.00
3.91	2.00	0.00	0.00	0.01	0.00	3.92	2.00	0.00	0.00	0.01	0.00
3.93	2.00	0.00	0.00	0.01	0.00	3.94	2.00	0.00	0.00	0.01	0.00
3.95	2.00	0.00	0.00	0.01	0.00	3.96	2.00	0.00	0.00	0.01	0.00
3.97	2.00	0.00	0.00	0.01	0.00	3.98	2.00	0.00	0.00	0.01	0.00
3.99	2.00	0.00	0.00	0.01	0.00	4.00	2.00	0.00	0.00	0.01	0.00
4.01	2.00	0.00	0.00	0.01	0.00	4.02	2.00	0.00	0.00	0.01	0.00
4.03	2.00	0.00	0.00	0.01	0.00	4.04	2.00	0.00	0.00	0.01	0.00
4.05	2.00	0.00	0.00	0.01	0.00	4.06	2.00	0.00	0.00	0.01	0.00
4.07	2.00	0.00	0.00	0.01	0.00	4.08	2.00	0.00	0.00	0.01	0.00
4.09	2.00	0.00	0.00	0.01	0.00	4.10	2.00	0.00	0.00	0.01	0.00
4.11	2.00	0.00	0.00	0.01	0.00	4.12	2.00	0.00	0.00	0.01	0.00
4.13	2.00	0.00	0.00	0.01	0.00	4.14	2.00	0.00	0.00	0.01	0.00
4.15	2.00	0.00	0.00	0.01	0.00	4.16	2.00	0.00	0.00	0.01	0.00
4.17	2.00	0.00	0.00	0.01	0.00	4.18	2.00	0.00	0.00	0.01	0.00
4.19	2.00	0.00	0.00	0.01	0.00	4.20	2.00	0.00	0.00	0.01	0.00
4.21	2.00	0.00	0.00	0.01	0.00	4.22	2.00	0.00	0.00	0.01	0.00
4.23	2.00	0.00	0.00	0.01	0.00	4.24	2.00	0.00	0.00	0.01	0.00
4.25	2.00	0.00	0.00	0.01	0.00	4.26	2.00	0.00	0.00	0.01	0.00
4.27	2.00	0.00	0.00	0.01	0.00	4.28	2.00	0.00	0.00	0.01	0.00
4.29	2.00	0.00	0.00	0.01	0.00	4.30	2.00	0.00	0.00	0.01	0.00
4.31	2.00	0.00	0.00	0.01	0.00	4.32	2.00	0.00	0.00	0.01	0.00
4.33	2.00	0.00	0.00	0.01	0.00	4.34	2.00	0.00	0.00	0.01	0.00
4.35	2.00	0.00	0.00	0.01	0.00	4.36	2.00	0.00	0.00	0.01	0.00
4.37	2.00	0.00	0.00	0.01	0.00	4.38	2.00	0.00	0.00	0.01	0.00
4.39	2.00	0.00	0.00	0.01	0.00	4.40	2.00	0.00	0.00	0.01	0.00
4.41	2.00	0.00	0.00	0.01	0.00	4.42	2.00	0.00	0.00	0.01	0.00
4.43	2.00	0.00	0.00	0.01	0.00	4.44	2.00	0.00	0.00	0.01	0.00
4.45	2.00	0.00	0.00	0.01	0.00	4.46	2.00	0.00	0.00	0.01	0.00
4.47	2.00	0.00	0.00	0.01	0.00	4.48	2.00	0.00	0.00	0.01	0.00
4.49	2.00	0.00	0.00	0.01	0.00	4.50	2.00	0.00	0.00	0.01	0.00
4.51	2.00	0.00	0.00	0.01	0.00	4.52	2.00	0.00	0.00	0.01	0.00
4.53	2.00	0.00	0.00	0.01	0.00	4.54	2.00	0.00	0.00	0.01	0.00
4.55	2.00	0.00	0.00	0.01	0.00	4.56	2.00	0.00	0.00	0.01	0.00
4.57	2.00	0.00	0.00	0.01	0.00	4.58	2.00	0.00	0.00	0.01	0.00
4.59	2.00	0.00	0.00	0.01	0.00	4.60	2.00	0.00	0.00	0.01	0.00
4.61	2.00	0.00	0.00	0.01	0.00	4.62	2.00	0.00	0.00	0.01	0.00
4.63	2.00	0.00	0.00	0.01	0.00	4.64	2.00	0.00	0.00	0.01	0.00
4.65	2.00	0.00	0.00	0.01	0.00	4.66	2.00	0.00	0.00	0.01	0.00
4.67	2.00	0.00	0.00	0.01	0.00	4.68	2.00	0.00	0.00	0.01	0.00
4.69	2.00	0.00	0.00	0.01	0.00	4.70	2.00	0.00	0.00	0.01	0.00
4.71	2.00	0.00	0.00	0.01	0.00	4.72	2.00	0.00	0.00	0.01	0.00
4.73	2.00	0.00	0.00	0.01	0.00	4.74	2.00	0.00	0.00	0.01	0.00
4.75	2.00	0.00	0.00	0.01	0.00	4.76	2.00	0.00	0.00	0.01	0.00
4.77	2.00	0.00	0.00	0.01	0.00	4.78	2.00	0.00	0.00	0.01	0.00
4.79	2.00	0.00	0.00	0.01	0.00	4.80	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
4.81	2.00	0.00	0.00	0.01	0.00	4.82	2.00	0.00	0.00	0.01	0.00
4.83	2.00	0.00	0.00	0.01	0.00	4.84	2.00	0.00	0.00	0.01	0.00
4.85	2.00	0.00	0.00	0.01	0.00	4.86	2.00	0.00	0.00	0.01	0.00
4.87	2.00	0.00	0.00	0.01	0.00	4.88	2.00	0.00	0.00	0.01	0.00
4.89	2.00	0.00	0.00	0.01	0.00	4.90	2.00	0.00	0.00	0.01	0.00
4.91	2.00	0.00	0.00	0.01	0.00	4.92	2.00	0.00	0.00	0.01	0.00
4.93	2.00	0.00	0.00	0.01	0.00	4.94	2.00	0.00	0.00	0.01	0.00
4.95	2.00	0.00	0.00	0.01	0.00	4.96	2.00	0.00	0.00	0.01	0.00
4.97	2.00	0.00	0.00	0.01	0.00	4.98	2.00	0.00	0.00	0.01	0.00
4.99	2.00	0.00	0.00	0.01	0.00	5.00	2.00	0.00	0.00	0.01	0.00
5.01	2.00	0.00	0.00	0.01	0.00	5.02	2.00	0.00	0.00	0.01	0.00
5.03	2.00	0.00	0.00	0.01	0.00	5.04	2.00	0.00	0.00	0.01	0.00
5.05	2.00	0.00	0.00	0.01	0.00	5.06	2.00	0.00	0.00	0.01	0.00
5.07	2.00	0.00	0.00	0.01	0.00	5.08	2.00	0.00	0.00	0.01	0.00
5.09	2.00	0.00	0.00	0.01	0.00	5.10	2.00	0.00	0.00	0.01	0.00
5.11	2.00	0.00	0.00	0.01	0.00	5.12	2.00	0.00	0.00	0.01	0.00
5.13	2.00	0.00	0.00	0.01	0.00	5.14	2.00	0.00	0.00	0.01	0.00
5.15	2.00	0.00	0.00	0.01	0.00	5.16	2.00	0.00	0.00	0.01	0.00
5.17	2.00	0.00	0.00	0.01	0.00	5.18	2.00	0.00	0.00	0.01	0.00
5.19	2.00	0.00	0.00	0.01	0.00	5.20	2.00	0.00	0.00	0.01	0.00
5.21	2.00	0.00	0.00	0.01	0.00	5.22	2.00	0.00	0.00	0.01	0.00
5.23	2.00	0.00	0.00	0.01	0.00	5.24	2.00	0.00	0.00	0.01	0.00
5.25	2.00	0.00	0.00	0.01	0.00	5.26	2.00	0.00	0.00	0.01	0.00
5.27	2.00	0.00	0.00	0.01	0.00	5.28	2.00	0.00	0.00	0.01	0.00
5.29	2.00	0.00	0.00	0.01	0.00	5.30	2.00	0.00	0.00	0.01	0.00
5.31	2.00	0.00	0.00	0.01	0.00	5.32	2.00	0.00	0.00	0.01	0.00
5.33	2.00	0.00	0.00	0.01	0.00	5.34	2.00	0.00	0.00	0.01	0.00
5.35	2.00	0.00	0.00	0.01	0.00	5.36	2.00	0.00	0.00	0.01	0.00
5.37	2.00	0.00	0.00	0.01	0.00	5.38	2.00	0.00	0.00	0.01	0.00
5.39	2.00	0.00	0.00	0.01	0.00	5.40	2.00	0.00	0.00	0.01	0.00
5.41	2.00	0.00	0.00	0.01	0.00	5.42	2.00	0.00	0.00	0.01	0.00
5.43	2.00	0.00	0.00	0.01	0.00	5.44	2.00	0.00	0.00	0.01	0.00
5.45	2.00	0.00	0.00	0.01	0.00	5.46	2.00	0.00	0.00	0.01	0.00
5.47	2.00	0.00	0.00	0.01	0.00	5.48	2.00	0.00	0.00	0.01	0.00
5.49	2.00	0.00	0.00	0.01	0.00	5.50	2.00	0.00	0.00	0.01	0.00
5.51	2.00	0.00	0.00	0.01	0.00	5.52	2.00	0.00	0.00	0.01	0.00
5.53	2.00	0.00	0.00	0.01	0.00	5.54	2.00	0.00	0.00	0.01	0.00
5.55	2.00	0.00	0.00	0.01	0.00	5.56	2.00	0.00	0.00	0.01	0.00
5.57	2.00	0.00	0.00	0.01	0.00	5.58	2.00	0.00	0.00	0.01	0.00
5.59	2.00	0.00	0.00	0.01	0.00	5.60	2.00	0.00	0.00	0.01	0.00
5.61	2.00	0.00	0.00	0.01	0.00	5.62	2.00	0.00	0.00	0.01	0.00
5.63	2.00	0.00	0.00	0.01	0.00	5.64	2.00	0.00	0.00	0.01	0.00
5.65	2.00	0.00	0.00	0.01	0.00	5.66	2.00	0.00	0.00	0.01	0.00
5.67	2.00	0.00	0.00	0.01	0.00	5.68	2.00	0.00	0.00	0.01	0.00
5.69	2.00	0.00	0.00	0.01	0.00	5.70	2.00	0.00	0.00	0.01	0.00
5.71	2.00	0.00	0.00	0.01	0.00	5.72	2.00	0.00	0.00	0.01	0.00
5.73	2.00	0.00	0.00	0.01	0.00	5.74	2.00	0.00	0.00	0.01	0.00
5.75	2.00	0.00	0.00	0.01	0.00	5.76	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
5.77	2.00	0.00	0.00	0.01	0.00	5.78	2.00	0.00	0.00	0.01	0.00
5.79	2.00	0.00	0.00	0.01	0.00	5.80	2.00	0.00	0.00	0.01	0.00
5.81	2.00	0.00	0.00	0.01	0.00	5.82	2.00	0.00	0.00	0.01	0.00
5.83	2.00	0.00	0.00	0.01	0.00	5.84	2.00	0.00	0.00	0.01	0.00
5.85	2.00	0.00	0.00	0.01	0.00	5.86	2.00	0.00	0.00	0.01	0.00
5.87	2.00	0.00	0.00	0.01	0.00	5.88	2.00	0.00	0.00	0.01	0.00
5.89	2.00	0.00	0.00	0.01	0.00	5.90	2.00	0.00	0.00	0.01	0.00
5.91	2.00	0.00	0.00	0.01	0.00	5.92	2.00	0.00	0.00	0.01	0.00
5.93	2.00	0.00	0.00	0.01	0.00	5.94	2.00	0.00	0.00	0.01	0.00
5.95	2.00	0.00	0.00	0.01	0.00	5.96	2.00	0.00	0.00	0.01	0.00
5.97	2.00	0.00	0.00	0.01	0.00	5.98	2.00	0.00	0.00	0.01	0.00
5.99	2.00	0.00	0.00	0.01	0.00	6.00	2.00	0.00	0.00	0.01	0.00
6.01	2.00	0.00	0.00	0.01	0.00	6.02	2.00	0.00	0.00	0.01	0.00
6.03	2.00	0.00	0.00	0.01	0.00	6.04	2.00	0.00	0.00	0.01	0.00
6.05	2.00	0.00	0.00	0.01	0.00	6.06	2.00	0.00	0.00	0.01	0.00
6.07	2.00	0.00	0.00	0.01	0.00	6.08	2.00	0.00	0.00	0.01	0.00
6.09	2.00	0.00	0.00	0.01	0.00	6.10	2.00	0.00	0.00	0.01	0.00
6.11	2.00	0.00	0.00	0.01	0.00	6.12	2.00	0.00	0.00	0.01	0.00
6.13	2.00	0.00	0.00	0.01	0.00	6.14	2.00	0.00	0.00	0.01	0.00
6.15	2.00	0.00	0.00	0.01	0.00	6.16	2.00	0.00	0.00	0.01	0.00
6.17	2.00	0.00	0.00	0.01	0.00	6.18	2.00	0.00	0.00	0.01	0.00
6.19	2.00	0.00	0.00	0.01	0.00	6.20	2.00	0.00	0.00	0.01	0.00
6.21	2.00	0.00	0.00	0.01	0.00	6.22	2.00	0.00	0.00	0.01	0.00
6.23	2.00	0.00	0.00	0.01	0.00	6.24	2.00	0.00	0.00	0.01	0.00
6.25	2.00	0.00	0.00	0.01	0.00	6.26	2.00	0.00	0.00	0.01	0.00
6.27	2.00	0.00	0.00	0.01	0.00	6.28	2.00	0.00	0.00	0.01	0.00
6.29	2.00	0.00	0.00	0.01	0.00	6.30	2.00	0.00	0.00	0.01	0.00
6.31	2.00	0.00	0.00	0.01	0.00	6.32	2.00	0.00	0.00	0.01	0.00
6.33	2.00	0.00	0.00	0.01	0.00	6.34	2.00	0.00	0.00	0.01	0.00
6.35	2.00	0.00	0.00	0.01	0.00	6.36	2.00	0.00	0.00	0.01	0.00
6.37	2.00	0.00	0.00	0.01	0.00	6.38	2.00	0.00	0.00	0.01	0.00
6.39	2.00	0.00	0.00	0.01	0.00	6.40	2.00	0.00	0.00	0.01	0.00
6.41	2.00	0.00	0.00	0.01	0.00	6.42	2.00	0.00	0.00	0.01	0.00
6.43	2.00	0.00	0.00	0.01	0.00	6.44	2.00	0.00	0.00	0.01	0.00
6.45	2.00	0.00	0.00	0.01	0.00	6.46	2.00	0.00	0.00	0.01	0.00
6.47	2.00	0.00	0.00	0.01	0.00	6.48	2.00	0.00	0.00	0.01	0.00
6.49	2.00	0.00	0.00	0.01	0.00	6.50	2.00	0.00	0.00	0.01	0.00
6.51	2.00	0.00	0.00	0.01	0.00	6.52	2.00	0.00	0.00	0.01	0.00
6.53	2.00	0.00	0.00	0.01	0.00	6.54	2.00	0.00	0.00	0.01	0.00
6.55	2.00	0.00	0.00	0.01	0.00	6.56	2.00	0.00	0.00	0.01	0.00
6.57	2.00	0.00	0.00	0.01	0.00	6.58	2.00	0.00	0.00	0.01	0.00
6.59	2.00	0.00	0.00	0.01	0.00	6.60	2.00	0.00	0.00	0.01	0.00
6.61	2.00	0.00	0.00	0.01	0.00	6.62	2.00	0.00	0.00	0.01	0.00
6.63	2.00	0.00	0.00	0.01	0.00	6.64	2.00	0.00	0.00	0.01	0.00
6.65	2.00	0.00	0.00	0.01	0.00	6.66	2.00	0.00	0.00	0.01	0.00
6.67	2.00	0.00	0.00	0.01	0.00	6.68	2.00	0.00	0.00	0.01	0.00
6.69	2.00	0.00	0.00	0.01	0.00	6.70	2.00	0.00	0.00	0.01	0.00
6.71	2.00	0.00	0.00	0.01	0.00	6.72	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
6.73	2.00	0.00	0.00	0.01	0.00	6.74	2.00	0.00	0.00	0.01	0.00
6.75	2.00	0.00	0.00	0.01	0.00	6.76	2.00	0.00	0.00	0.01	0.00
6.77	2.00	0.00	0.00	0.01	0.00	6.78	2.00	0.00	0.00	0.01	0.00
6.79	2.00	0.00	0.00	0.01	0.00	6.80	2.00	0.00	0.00	0.01	0.00
6.81	2.00	0.00	0.00	0.01	0.00	6.82	2.00	0.00	0.00	0.01	0.00
6.83	2.00	0.00	0.00	0.01	0.00	6.84	2.00	0.00	0.00	0.01	0.00
6.85	2.00	0.00	0.00	0.01	0.00	6.86	2.00	0.00	0.00	0.01	0.00
6.87	2.00	0.00	0.00	0.01	0.00	6.88	2.00	0.00	0.00	0.01	0.00
6.89	2.00	0.00	0.00	0.01	0.00	6.90	2.00	0.00	0.00	0.01	0.00
6.91	2.00	0.00	0.00	0.01	0.00	6.92	2.00	0.00	0.00	0.01	0.00
6.93	2.00	0.00	0.00	0.01	0.00	6.94	2.00	0.00	0.00	0.01	0.00
6.95	2.00	0.00	0.00	0.01	0.00	6.96	2.00	0.00	0.00	0.01	0.00
6.97	2.00	0.00	0.00	0.01	0.00	6.98	2.00	0.00	0.00	0.01	0.00
6.99	2.00	0.00	0.00	0.01	0.00	7.00	2.00	0.00	0.00	0.01	0.00
7.01	2.00	0.00	0.00	0.01	0.00	7.02	2.00	0.00	0.00	0.01	0.00
7.03	2.00	0.00	0.00	0.01	0.00	7.04	2.00	0.00	0.00	0.01	0.00
7.05	2.00	0.00	0.00	0.01	0.00	7.06	2.00	0.00	0.00	0.01	0.00
7.07	2.00	0.00	0.00	0.01	0.00	7.08	2.00	0.00	0.00	0.01	0.00
7.09	2.00	0.00	0.00	0.01	0.00	7.10	2.00	0.00	0.00	0.01	0.00
7.11	2.00	0.00	0.00	0.01	0.00	7.12	2.00	0.00	0.00	0.01	0.00
7.13	2.00	0.00	0.00	0.01	0.00	7.14	2.00	0.00	0.00	0.01	0.00
7.15	2.00	0.00	0.00	0.01	0.00	7.16	2.00	0.00	0.00	0.01	0.00
7.17	2.00	0.00	0.00	0.01	0.00	7.18	2.00	0.00	0.00	0.01	0.00
7.19	2.00	0.00	0.00	0.01	0.00	7.20	2.00	0.00	0.00	0.01	0.00
7.21	2.00	0.00	0.00	0.01	0.00	7.22	2.00	0.00	0.00	0.01	0.00
7.23	2.00	0.00	0.00	0.01	0.00	7.24	2.00	0.00	0.00	0.01	0.00
7.25	2.00	0.00	0.00	0.01	0.00	7.26	2.00	0.00	0.00	0.01	0.00
7.27	2.00	0.00	0.00	0.01	0.00	7.28	2.00	0.00	0.00	0.01	0.00
7.29	2.00	0.00	0.00	0.01	0.00	7.30	2.00	0.00	0.00	0.01	0.00
7.31	2.00	0.00	0.00	0.01	0.00	7.32	2.00	0.00	0.00	0.01	0.00
7.33	2.00	0.00	0.00	0.01	0.00	7.34	2.00	0.00	0.00	0.01	0.00
7.35	2.00	0.00	0.00	0.01	0.00	7.36	2.00	0.00	0.00	0.01	0.00
7.37	2.00	0.00	0.00	0.01	0.00	7.38	2.00	0.00	0.00	0.01	0.00
7.39	2.00	0.00	0.00	0.01	0.00	7.40	2.00	0.00	0.00	0.01	0.00
7.41	2.00	0.00	0.00	0.01	0.00	7.42	2.00	0.00	0.00	0.01	0.00
7.43	2.00	0.00	0.00	0.01	0.00	7.44	2.00	0.00	0.00	0.01	0.00
7.45	2.00	0.00	0.00	0.01	0.00	7.46	2.00	0.00	0.00	0.01	0.00
7.47	2.00	0.00	0.00	0.01	0.00	7.48	2.00	0.00	0.00	0.01	0.00
7.49	2.00	0.00	0.00	0.01	0.00	7.50	2.00	0.00	0.00	0.01	0.00
7.51	2.00	0.00	0.00	0.01	0.00	7.52	2.00	0.00	0.00	0.01	0.00
7.53	2.00	0.00	0.00	0.01	0.00	7.54	2.00	0.00	0.00	0.01	0.00
7.55	2.00	0.00	0.00	0.01	0.00	7.56	2.00	0.00	0.00	0.01	0.00
7.57	2.00	0.00	0.00	0.01	0.00	7.58	2.00	0.00	0.00	0.01	0.00
7.59	2.00	0.00	0.00	0.01	0.00	7.60	2.00	0.00	0.00	0.01	0.00
7.61	2.00	0.00	0.00	0.01	0.00	7.62	2.00	0.00	0.00	0.01	0.00
7.63	2.00	0.00	0.00	0.01	0.00	7.64	2.00	0.00	0.00	0.01	0.00
7.65	2.00	0.00	0.00	0.01	0.00	7.66	2.00	0.00	0.00	0.01	0.00
7.67	2.00	0.00	0.00	0.01	0.00	7.68	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
7.69	2.00	0.00	0.00	0.01	0.00	7.70	2.00	0.00	0.00	0.01	0.00
7.71	2.00	0.00	0.00	0.01	0.00	7.72	2.00	0.00	0.00	0.01	0.00
7.73	2.00	0.00	0.00	0.01	0.00	7.74	2.00	0.00	0.00	0.01	0.00
7.75	2.00	0.00	0.00	0.01	0.00	7.76	2.00	0.00	0.00	0.01	0.00
7.77	2.00	0.00	0.00	0.01	0.00	7.78	2.00	0.00	0.00	0.01	0.00
7.79	2.00	0.00	0.00	0.01	0.00	7.80	2.00	0.00	0.00	0.01	0.00
7.81	2.00	0.00	0.00	0.01	0.00	7.82	2.00	0.00	0.00	0.01	0.00
7.83	2.00	0.00	0.00	0.01	0.00	7.84	2.00	0.00	0.00	0.01	0.00
7.85	2.00	0.00	0.00	0.01	0.00	7.86	2.00	0.00	0.00	0.01	0.00
7.87	2.00	0.00	0.00	0.01	0.00	7.88	2.00	0.00	0.00	0.01	0.00
7.89	2.00	0.00	0.00	0.01	0.00	7.90	2.00	0.00	0.00	0.01	0.00
7.91	2.00	0.00	0.00	0.01	0.00	7.92	2.00	0.00	0.00	0.01	0.00
7.93	2.00	0.00	0.00	0.01	0.00	7.94	2.00	0.00	0.00	0.01	0.00
7.95	2.00	0.00	0.00	0.01	0.00	7.96	2.00	0.00	0.00	0.01	0.00
7.97	2.00	0.00	0.00	0.01	0.00	7.98	2.00	0.00	0.00	0.01	0.00
7.99	2.00	0.00	0.00	0.01	0.00	8.00	2.00	0.00	0.00	0.01	0.00
8.01	2.00	0.00	0.00	0.01	0.00	8.02	2.00	0.00	0.00	0.01	0.00
8.03	2.00	0.00	0.00	0.01	0.00	8.04	2.00	0.00	0.00	0.01	0.00
8.05	2.00	0.00	0.00	0.01	0.00	8.06	2.00	0.00	0.00	0.01	0.00
8.07	2.00	0.00	0.00	0.01	0.00	8.08	2.00	0.00	0.00	0.01	0.00
8.09	2.00	0.00	0.00	0.01	0.00	8.10	2.00	0.00	0.00	0.01	0.00
8.11	2.00	0.00	0.00	0.01	0.00	8.12	2.00	0.00	0.00	0.01	0.00
8.13	2.00	0.00	0.00	0.01	0.00	8.14	2.00	0.00	0.00	0.01	0.00
8.15	2.00	0.00	0.00	0.01	0.00	8.16	2.00	0.00	0.00	0.01	0.00
8.17	2.00	0.00	0.00	0.01	0.00	8.18	2.00	0.00	0.00	0.01	0.00
8.19	2.00	0.00	0.00	0.01	0.00	8.20	2.00	0.00	0.00	0.01	0.00
8.21	2.00	0.00	0.00	0.01	0.00	8.22	2.00	0.00	0.00	0.01	0.00
8.23	2.00	0.00	0.00	0.01	0.00	8.24	2.00	0.00	0.00	0.01	0.00
8.25	2.00	0.00	0.00	0.01	0.00	8.26	2.00	0.00	0.00	0.01	0.00
8.27	2.00	0.00	0.00	0.01	0.00	8.28	2.00	0.00	0.00	0.01	0.00
8.29	2.00	0.00	0.00	0.01	0.00	8.30	2.00	0.00	0.00	0.01	0.00
8.31	2.00	0.00	0.00	0.01	0.00	8.32	2.00	0.00	0.00	0.01	0.00
8.33	2.00	0.00	0.00	0.01	0.00	8.34	2.00	0.00	0.00	0.01	0.00
8.35	2.00	0.00	0.00	0.01	0.00	8.36	2.00	0.00	0.00	0.01	0.00
8.37	2.00	0.00	0.00	0.01	0.00	8.38	2.00	0.00	0.00	0.01	0.00
8.39	2.00	0.00	0.00	0.01	0.00	8.40	2.00	0.00	0.00	0.01	0.00
8.41	2.00	0.00	0.00	0.01	0.00	8.42	2.00	0.00	0.00	0.01	0.00
8.43	2.00	0.00	0.00	0.01	0.00	8.44	2.00	0.00	0.00	0.01	0.00
8.45	2.00	0.00	0.00	0.01	0.00	8.46	2.00	0.00	0.00	0.01	0.00
8.47	2.00	0.00	0.00	0.01	0.00	8.48	2.00	0.00	0.00	0.01	0.00
8.49	2.00	0.00	0.00	0.01	0.00	8.50	2.00	0.00	0.00	0.01	0.00
8.51	2.00	0.00	0.00	0.01	0.00	8.52	2.00	0.00	0.00	0.01	0.00
8.53	2.00	0.00	0.00	0.01	0.00	8.54	2.00	0.00	0.00	0.01	0.00
8.55	2.00	0.00	0.00	0.01	0.00	8.56	2.00	0.00	0.00	0.01	0.00
8.57	2.00	0.00	0.00	0.01	0.00	8.58	2.00	0.00	0.00	0.01	0.00
8.59	2.00	0.00	0.00	0.01	0.00	8.60	2.00	0.00	0.00	0.01	0.00
8.61	2.00	0.00	0.00	0.01	0.00	8.62	2.00	0.00	0.00	0.01	0.00
8.63	2.00	0.00	0.00	0.01	0.00	8.64	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
8.65	2.00	0.00	0.00	0.01	0.00	8.66	2.00	0.00	0.00	0.01	0.00
8.67	2.00	0.00	0.00	0.01	0.00	8.68	2.00	0.00	0.00	0.01	0.00
8.69	2.00	0.00	0.00	0.01	0.00	8.70	2.00	0.00	0.00	0.01	0.00
8.71	2.00	0.00	0.00	0.01	0.00	8.72	2.00	0.00	0.00	0.01	0.00
8.73	2.00	0.00	0.00	0.01	0.00	8.74	2.00	0.00	0.00	0.01	0.00
8.75	2.00	0.00	0.00	0.01	0.00	8.76	2.00	0.00	0.00	0.01	0.00
8.77	2.00	0.00	0.00	0.01	0.00	8.78	2.00	0.00	0.00	0.01	0.00
8.79	2.00	0.00	0.00	0.01	0.00	8.80	2.00	0.00	0.00	0.01	0.00
8.81	2.00	0.00	0.00	0.01	0.00	8.82	2.00	0.00	0.00	0.01	0.00
8.83	2.00	0.00	0.00	0.01	0.00	8.84	2.00	0.00	0.00	0.01	0.00
8.85	2.00	0.00	0.00	0.01	0.00	8.86	2.00	0.00	0.00	0.01	0.00
8.87	2.00	0.00	0.00	0.01	0.00	8.88	2.00	0.00	0.00	0.01	0.00
8.89	2.00	0.00	0.00	0.01	0.00	8.90	2.00	0.00	0.00	0.01	0.00
8.91	2.00	0.00	0.00	0.01	0.00	8.92	2.00	0.00	0.00	0.01	0.00
8.93	2.00	0.00	0.00	0.01	0.00	8.94	2.00	0.00	0.00	0.01	0.00
8.95	2.00	0.00	0.00	0.01	0.00	8.96	2.00	0.00	0.00	0.01	0.00
8.97	2.00	0.00	0.00	0.01	0.00	8.98	2.00	0.00	0.00	0.01	0.00
8.99	2.00	0.00	0.00	0.01	0.00	9.00	2.00	0.00	0.00	0.01	0.00
9.01	2.00	0.00	0.00	0.01	0.00	9.02	2.00	0.00	0.00	0.01	0.00
9.03	2.00	0.00	0.00	0.01	0.00	9.04	2.00	0.00	0.00	0.01	0.00
9.05	2.00	0.00	0.00	0.01	0.00	9.06	2.00	0.00	0.00	0.01	0.00
9.07	2.00	0.00	0.00	0.01	0.00	9.08	2.00	0.00	0.00	0.01	0.00
9.09	2.00	0.00	0.00	0.01	0.00	9.10	2.00	0.00	0.00	0.01	0.00
9.11	2.00	0.00	0.00	0.01	0.00	9.12	2.00	0.00	0.00	0.01	0.00
9.13	2.00	0.00	0.00	0.01	0.00	9.14	2.00	0.00	0.00	0.01	0.00
9.15	2.00	0.00	0.00	0.01	0.00	9.16	2.00	0.00	0.00	0.01	0.00
9.17	2.00	0.00	0.00	0.01	0.00	9.18	2.00	0.00	0.00	0.01	0.00
9.19	2.00	0.00	0.00	0.01	0.00	9.20	2.00	0.00	0.00	0.01	0.00
9.21	2.00	0.00	0.00	0.01	0.00	9.22	2.00	0.00	0.00	0.01	0.00
9.23	2.00	0.00	0.00	0.01	0.00	9.24	2.00	0.00	0.00	0.01	0.00
9.25	2.00	0.00	0.00	0.01	0.00	9.26	2.00	0.00	0.00	0.01	0.00
9.27	2.00	0.00	0.00	0.01	0.00	9.28	2.00	0.00	0.00	0.01	0.00
9.29	2.00	0.00	0.00	0.01	0.00	9.30	2.00	0.00	0.00	0.01	0.00
9.31	2.00	0.00	0.00	0.01	0.00	9.32	2.00	0.00	0.00	0.01	0.00
9.33	2.00	0.00	0.00	0.01	0.00	9.34	2.00	0.00	0.00	0.01	0.00
9.35	2.00	0.00	0.00	0.01	0.00	9.36	2.00	0.00	0.00	0.01	0.00
9.37	2.00	0.00	0.00	0.01	0.00	9.38	2.00	0.00	0.00	0.01	0.00
9.39	2.00	0.00	0.00	0.01	0.00	9.40	2.00	0.00	0.00	0.01	0.00
9.41	2.00	0.00	0.00	0.01	0.00	9.42	2.00	0.00	0.00	0.01	0.00
9.43	2.00	0.00	0.00	0.01	0.00	9.44	2.00	0.00	0.00	0.01	0.00
9.45	2.00	0.00	0.00	0.01	0.00	9.46	2.00	0.00	0.00	0.01	0.00
9.47	2.00	0.00	0.00	0.01	0.00	9.48	2.00	0.00	0.00	0.01	0.00
9.49	2.00	0.00	0.00	0.01	0.00	9.50	2.00	0.00	0.00	0.01	0.00
9.51	2.00	0.00	0.00	0.01	0.00	9.52	2.00	0.00	0.00	0.01	0.00
9.53	2.00	0.00	0.00	0.01	0.00	9.54	2.00	0.00	0.00	0.01	0.00
9.55	2.00	0.00	0.00	0.01	0.00	9.56	2.00	0.00	0.00	0.01	0.00
9.57	2.00	0.00	0.00	0.01	0.00	9.58	2.00	0.00	0.00	0.01	0.00
9.59	2.00	0.00	0.00	0.01	0.00	9.60	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
9.61	2.00	0.00	0.00	0.01	0.00	9.62	2.00	0.00	0.00	0.01	0.00
9.63	2.00	0.00	0.00	0.01	0.00	9.64	2.00	0.00	0.00	0.01	0.00
9.65	2.00	0.00	0.00	0.01	0.00	9.66	2.00	0.00	0.00	0.01	0.00
9.67	2.00	0.00	0.00	0.01	0.00	9.68	2.00	0.00	0.00	0.01	0.00
9.69	2.00	0.00	0.00	0.01	0.00	9.70	2.00	0.00	0.00	0.01	0.00
9.71	2.00	0.00	0.00	0.01	0.00	9.72	2.00	0.00	0.00	0.01	0.00
9.73	2.00	0.00	0.00	0.01	0.00	9.74	2.00	0.00	0.00	0.01	0.00
9.75	2.00	0.00	0.00	0.01	0.00	9.76	2.00	0.00	0.00	0.01	0.00
9.77	2.00	0.00	0.00	0.01	0.00	9.78	2.00	0.00	0.00	0.01	0.00
9.79	1.25	0.00	0.00	0.01	0.00	9.80	1.21	0.00	0.00	0.01	0.00
9.81	1.18	0.00	0.00	0.01	0.00	9.82	1.15	0.00	0.00	0.01	0.00
9.83	1.13	0.00	0.00	0.01	0.00	9.84	1.12	0.00	0.00	0.01	0.00
9.85	1.10	0.00	0.00	0.01	0.00	9.86	1.06	0.00	0.00	0.01	0.00
9.87	1.01	0.00	0.00	0.01	0.00	9.88	0.96	0.00	0.00	0.01	0.00
9.89	0.91	0.00	0.00	0.01	0.00	9.90	0.87	0.00	0.00	0.01	0.00
9.91	0.84	0.00	0.00	0.01	0.00	9.92	0.84	0.00	0.00	0.01	0.00
9.93	0.86	0.00	0.00	0.01	0.00	9.94	0.89	0.00	0.00	0.01	0.00
9.95	0.92	0.00	0.00	0.01	0.00	9.96	0.96	0.00	0.00	0.01	0.00
9.97	1.00	0.00	0.00	0.01	0.00	9.98	1.04	0.00	0.00	0.01	0.00
9.99	1.07	0.00	0.00	0.01	0.00	10.00	1.09	0.00	0.00	0.01	0.00
10.01	1.09	0.00	0.00	0.01	0.00	10.02	1.07	0.00	0.00	0.01	0.00
10.03	1.05	0.00	0.00	0.01	0.00	10.04	1.03	0.00	0.00	0.01	0.00
10.05	1.01	0.00	0.00	0.01	0.00	10.06	0.99	0.00	0.00	0.01	0.00
10.07	0.97	0.00	0.00	0.01	0.00	10.08	2.00	0.00	0.00	0.01	0.00
10.09	2.00	0.00	0.00	0.01	0.00	10.10	2.00	0.00	0.00	0.01	0.00
10.11	2.00	0.00	0.00	0.01	0.00	10.12	2.00	0.00	0.00	0.01	0.00
10.13	2.00	0.00	0.00	0.01	0.00	10.14	2.00	0.00	0.00	0.01	0.00
10.15	2.00	0.00	0.00	0.01	0.00	10.16	2.00	0.00	0.00	0.01	0.00
10.17	2.00	0.00	0.00	0.01	0.00	10.18	2.00	0.00	0.00	0.01	0.00
10.19	2.00	0.00	0.00	0.01	0.00	10.20	2.00	0.00	0.00	0.01	0.00
10.21	2.00	0.00	0.00	0.01	0.00	10.22	2.00	0.00	0.00	0.01	0.00
10.23	2.00	0.00	0.00	0.01	0.00	10.24	2.00	0.00	0.00	0.01	0.00
10.25	2.00	0.00	0.00	0.01	0.00	10.26	2.00	0.00	0.00	0.01	0.00
10.27	2.00	0.00	0.00	0.01	0.00	10.28	2.00	0.00	0.00	0.01	0.00
10.29	2.00	0.00	0.00	0.01	0.00	10.30	2.00	0.00	0.00	0.01	0.00
10.31	2.00	0.00	0.00	0.01	0.00	10.32	2.00	0.00	0.00	0.01	0.00
10.33	2.00	0.00	0.00	0.01	0.00	10.34	2.00	0.00	0.00	0.01	0.00
10.35	2.00	0.00	0.00	0.01	0.00	10.36	2.00	0.00	0.00	0.01	0.00
10.37	2.00	0.00	0.00	0.01	0.00	10.38	2.00	0.00	0.00	0.01	0.00
10.39	2.00	0.00	0.00	0.01	0.00	10.40	2.00	0.00	0.00	0.01	0.00
10.41	2.00	0.00	0.00	0.01	0.00	10.42	2.00	0.00	0.00	0.01	0.00
10.43	2.00	0.00	0.00	0.01	0.00	10.44	2.00	0.00	0.00	0.01	0.00
10.45	2.00	0.00	0.00	0.01	0.00	10.46	2.00	0.00	0.00	0.01	0.00
10.47	2.00	0.00	0.00	0.01	0.00	10.48	2.00	0.00	0.00	0.01	0.00
10.49	2.00	0.00	0.00	0.01	0.00	10.50	2.00	0.00	0.00	0.01	0.00
10.51	2.00	0.00	0.00	0.01	0.00	10.52	2.00	0.00	0.00	0.01	0.00
10.53	2.00	0.00	0.00	0.01	0.00	10.54	2.00	0.00	0.00	0.01	0.00
10.55	2.00	0.00	0.00	0.01	0.00	10.56	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
10.57	2.00	0.00	0.00	0.01	0.00	10.58	2.00	0.00	0.00	0.01	0.00
10.59	2.00	0.00	0.00	0.01	0.00	10.60	2.00	0.00	0.00	0.01	0.00
10.61	2.00	0.00	0.00	0.01	0.00	10.62	2.00	0.00	0.00	0.01	0.00
10.63	2.00	0.00	0.00	0.01	0.00	10.64	2.00	0.00	0.00	0.01	0.00
10.65	2.00	0.00	0.00	0.01	0.00	10.66	2.00	0.00	0.00	0.01	0.00
10.67	2.00	0.00	0.00	0.01	0.00	10.68	2.00	0.00	0.00	0.01	0.00
10.69	2.00	0.00	0.00	0.01	0.00	10.70	2.00	0.00	0.00	0.01	0.00
10.71	2.00	0.00	0.00	0.01	0.00	10.72	2.00	0.00	0.00	0.01	0.00
10.73	2.00	0.00	0.00	0.01	0.00	10.74	2.00	0.00	0.00	0.01	0.00
10.75	2.00	0.00	0.00	0.01	0.00	10.76	2.00	0.00	0.00	0.01	0.00
10.77	2.00	0.00	0.00	0.01	0.00	10.78	2.00	0.00	0.00	0.01	0.00
10.79	2.00	0.00	0.00	0.01	0.00	10.80	2.00	0.00	0.00	0.01	0.00
10.81	2.00	0.00	0.00	0.01	0.00	10.82	2.00	0.00	0.00	0.01	0.00
10.83	2.00	0.00	0.00	0.01	0.00	10.84	2.00	0.00	0.00	0.01	0.00
10.85	2.00	0.00	0.00	0.01	0.00	10.86	2.00	0.00	0.00	0.01	0.00
10.87	2.00	0.00	0.00	0.01	0.00	10.88	2.00	0.00	0.00	0.01	0.00
10.89	2.00	0.00	0.00	0.01	0.00	10.90	2.00	0.00	0.00	0.01	0.00
10.91	2.00	0.00	0.00	0.01	0.00	10.92	2.00	0.00	0.00	0.01	0.00
10.93	2.00	0.00	0.00	0.01	0.00	10.94	2.00	0.00	0.00	0.01	0.00
10.95	2.00	0.00	0.00	0.01	0.00	10.96	2.00	0.00	0.00	0.01	0.00
10.97	2.00	0.00	0.00	0.01	0.00	10.98	2.00	0.00	0.00	0.01	0.00
10.99	2.00	0.00	0.00	0.01	0.00	11.00	2.00	0.00	0.00	0.01	0.00
11.01	2.00	0.00	0.00	0.01	0.00	11.02	2.00	0.00	0.00	0.01	0.00
11.03	2.00	0.00	0.00	0.01	0.00	11.04	2.00	0.00	0.00	0.01	0.00
11.05	2.00	0.00	0.00	0.01	0.00	11.06	2.00	0.00	0.00	0.01	0.00
11.07	2.00	0.00	0.00	0.01	0.00	11.08	2.00	0.00	0.00	0.01	0.00
11.09	2.00	0.00	0.00	0.01	0.00	11.10	2.00	0.00	0.00	0.01	0.00
11.11	2.00	0.00	0.00	0.01	0.00	11.12	2.00	0.00	0.00	0.01	0.00
11.13	2.00	0.00	0.00	0.01	0.00	11.14	0.54	0.00	0.00	0.01	0.01
11.15	0.53	0.00	0.00	0.01	0.01	11.16	0.52	0.00	0.00	0.01	0.01
11.17	0.51	0.00	0.00	0.01	0.01	11.18	0.50	0.00	0.00	0.01	0.01
11.19	0.50	0.00	0.00	0.01	0.01	11.20	0.49	0.00	0.00	0.01	0.01
11.21	0.48	0.00	0.00	0.01	0.01	11.22	2.00	0.00	0.00	0.01	0.00
11.23	2.00	0.00	0.00	0.01	0.00	11.24	2.00	0.00	0.00	0.01	0.00
11.25	2.00	0.00	0.00	0.01	0.00	11.26	2.00	0.00	0.00	0.01	0.00
11.27	2.00	0.00	0.00	0.01	0.00	11.28	2.00	0.00	0.00	0.01	0.00
11.29	2.00	0.00	0.00	0.01	0.00	11.30	2.00	0.00	0.00	0.01	0.00
11.31	2.00	0.00	0.00	0.01	0.00	11.32	2.00	0.00	0.00	0.01	0.00
11.33	2.00	0.00	0.00	0.01	0.00	11.34	2.00	0.00	0.00	0.01	0.00
11.35	2.00	0.00	0.00	0.01	0.00	11.36	2.00	0.00	0.00	0.01	0.00
11.37	2.00	0.00	0.00	0.01	0.00	11.38	2.00	0.00	0.00	0.01	0.00
11.39	2.00	0.00	0.00	0.01	0.00	11.40	2.00	0.00	0.00	0.01	0.00
11.41	2.00	0.00	0.00	0.01	0.00	11.42	2.00	0.00	0.00	0.01	0.00
11.43	2.00	0.00	0.00	0.01	0.00	11.44	2.00	0.00	0.00	0.01	0.00
11.45	2.00	0.00	0.00	0.01	0.00	11.46	2.00	0.00	0.00	0.01	0.00
11.47	2.00	0.00	0.00	0.01	0.00	11.48	2.00	0.00	0.00	0.01	0.00
11.49	2.00	0.00	0.00	0.01	0.00	11.50	2.00	0.00	0.00	0.01	0.00
11.51	2.00	0.00	0.00	0.01	0.00	11.52	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
11.53	2.00	0.00	0.00	0.01	0.00	11.54	2.00	0.00	0.00	0.01	0.00
11.55	2.00	0.00	0.00	0.01	0.00	11.56	2.00	0.00	0.00	0.01	0.00
11.57	2.00	0.00	0.00	0.01	0.00	11.58	2.00	0.00	0.00	0.01	0.00
11.59	2.00	0.00	0.00	0.01	0.00	11.60	2.00	0.00	0.00	0.01	0.00
11.61	2.00	0.00	0.00	0.01	0.00	11.62	2.00	0.00	0.00	0.01	0.00
11.63	2.00	0.00	0.00	0.01	0.00	11.64	2.00	0.00	0.00	0.01	0.00
11.65	2.00	0.00	0.00	0.01	0.00	11.66	2.00	0.00	0.00	0.01	0.00
11.67	2.00	0.00	0.00	0.01	0.00	11.68	2.00	0.00	0.00	0.01	0.00
11.69	2.00	0.00	0.00	0.01	0.00	11.70	2.00	0.00	0.00	0.01	0.00
11.71	2.00	0.00	0.00	0.01	0.00	11.72	2.00	0.00	0.00	0.01	0.00
11.73	2.00	0.00	0.00	0.01	0.00	11.74	2.00	0.00	0.00	0.01	0.00
11.75	2.00	0.00	0.00	0.01	0.00	11.76	2.00	0.00	0.00	0.01	0.00
11.77	2.00	0.00	0.00	0.01	0.00	11.78	2.00	0.00	0.00	0.01	0.00
11.79	2.00	0.00	0.00	0.01	0.00	11.80	2.00	0.00	0.00	0.01	0.00
11.81	2.00	0.00	0.00	0.01	0.00	11.82	2.00	0.00	0.00	0.01	0.00
11.83	2.00	0.00	0.00	0.01	0.00	11.84	2.00	0.00	0.00	0.01	0.00
11.85	2.00	0.00	0.00	0.01	0.00	11.86	2.00	0.00	0.00	0.01	0.00
11.87	2.00	0.00	0.00	0.01	0.00	11.88	2.00	0.00	0.00	0.01	0.00
11.89	2.00	0.00	0.00	0.01	0.00	11.90	2.00	0.00	0.00	0.01	0.00
11.91	2.00	0.00	0.00	0.01	0.00	11.92	2.00	0.00	0.00	0.01	0.00
11.93	2.00	0.00	0.00	0.01	0.00	11.94	2.00	0.00	0.00	0.01	0.00
11.95	2.00	0.00	0.00	0.01	0.00	11.96	2.00	0.00	0.00	0.01	0.00
11.97	2.00	0.00	0.00	0.01	0.00	11.98	2.00	0.00	0.00	0.01	0.00
11.99	2.00	0.00	0.00	0.01	0.00	12.00	2.00	0.00	0.00	0.01	0.00
12.01	2.00	0.00	0.00	0.01	0.00	12.02	2.00	0.00	0.00	0.01	0.00
12.03	2.00	0.00	0.00	0.01	0.00	12.04	2.00	0.00	0.00	0.01	0.00
12.05	2.00	0.00	0.00	0.01	0.00	12.06	2.00	0.00	0.00	0.01	0.00
12.07	2.00	0.00	0.00	0.01	0.00	12.08	2.00	0.00	0.00	0.01	0.00
12.09	2.00	0.00	0.00	0.01	0.00	12.10	2.00	0.00	0.00	0.01	0.00
12.11	2.00	0.00	0.00	0.01	0.00	12.12	2.00	0.00	0.00	0.01	0.00
12.13	1.66	0.00	0.00	0.01	0.00	12.14	1.57	0.00	0.00	0.01	0.00
12.15	1.48	0.00	0.00	0.01	0.00	12.16	1.41	0.00	0.00	0.01	0.00
12.17	1.37	0.00	0.00	0.01	0.00	12.18	1.34	0.00	0.00	0.01	0.00
12.19	1.32	0.00	0.00	0.01	0.00	12.20	1.29	0.00	0.00	0.01	0.00
12.21	1.27	0.00	0.00	0.01	0.00	12.22	1.24	0.00	0.00	0.01	0.00
12.23	1.22	0.00	0.00	0.01	0.00	12.24	1.20	0.00	0.00	0.01	0.00
12.25	1.18	0.00	0.00	0.01	0.00	12.26	1.16	0.00	0.00	0.01	0.00
12.27	1.15	0.00	0.00	0.01	0.00	12.28	1.12	0.00	0.00	0.01	0.00
12.29	1.10	0.00	0.00	0.01	0.00	12.30	1.08	0.00	0.00	0.01	0.00
12.31	1.05	0.00	0.00	0.01	0.00	12.32	1.03	0.00	0.00	0.01	0.00
12.33	1.01	0.00	0.00	0.01	0.00	12.34	0.99	0.00	0.00	0.01	0.00
12.35	0.97	0.00	0.00	0.01	0.00	12.36	0.95	0.00	0.00	0.01	0.00
12.37	0.92	0.00	0.00	0.01	0.00	12.38	0.90	0.00	0.00	0.01	0.00
12.39	0.87	0.00	0.00	0.01	0.00	12.40	0.84	0.00	0.00	0.01	0.00
12.41	0.82	0.00	0.00	0.01	0.00	12.42	0.80	0.00	0.00	0.01	0.00
12.43	0.78	0.00	0.00	0.01	0.01	12.44	0.77	0.00	0.00	0.01	0.01
12.45	0.75	0.00	0.00	0.01	0.01	12.46	0.73	0.00	0.00	0.01	0.01
12.47	0.72	0.00	0.00	0.01	0.01	12.48	0.70	0.00	0.00	0.01	0.01

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
12.49	0.68	0.00	0.00	0.01	0.01	12.50	0.66	0.00	0.00	0.01	0.01
12.51	0.65	0.00	0.00	0.01	0.01	12.52	0.64	0.00	0.00	0.01	0.01
12.53	0.64	0.00	0.00	0.01	0.01	12.54	0.63	0.00	0.00	0.01	0.01
12.55	0.62	0.00	0.00	0.01	0.01	12.56	0.61	0.00	0.00	0.01	0.01
12.57	0.60	0.00	0.00	0.01	0.01	12.58	0.59	0.00	0.00	0.01	0.01
12.59	0.58	0.00	0.00	0.01	0.01	12.60	0.58	0.00	0.00	0.01	0.01
12.61	0.58	0.00	0.00	0.01	0.01	12.62	0.58	0.00	0.00	0.01	0.01
12.63	0.58	0.00	0.00	0.01	0.01	12.64	0.58	0.00	0.00	0.01	0.01
12.65	0.58	0.00	0.00	0.01	0.01	12.66	0.58	0.00	0.00	0.01	0.01
12.67	0.57	0.00	0.00	0.01	0.01	12.68	0.57	0.00	0.00	0.01	0.01
12.69	0.57	0.00	0.00	0.01	0.01	12.70	0.57	0.00	0.00	0.01	0.01
12.71	0.57	0.00	0.00	0.01	0.01	12.72	0.57	0.00	0.00	0.01	0.01
12.73	0.57	0.00	0.00	0.01	0.01	12.74	0.57	0.00	0.00	0.01	0.01
12.75	0.57	0.00	0.00	0.01	0.01	12.76	0.57	0.00	0.00	0.01	0.01
12.77	0.57	0.00	0.00	0.01	0.01	12.78	0.57	0.00	0.00	0.01	0.01
12.79	0.57	0.00	0.00	0.01	0.01	12.80	0.57	0.00	0.00	0.01	0.01
12.81	0.57	0.00	0.00	0.01	0.01	12.82	0.57	0.00	0.00	0.01	0.01
12.83	0.57	0.00	0.00	0.01	0.01	12.84	0.57	0.00	0.00	0.01	0.01
12.85	0.57	0.00	0.00	0.01	0.01	12.86	0.57	0.00	0.00	0.01	0.01
12.87	0.57	0.00	0.00	0.01	0.01	12.88	0.57	0.00	0.00	0.01	0.01
12.89	0.57	0.00	0.00	0.01	0.01	12.90	0.56	0.00	0.00	0.01	0.01
12.91	0.56	0.00	0.00	0.01	0.01	12.92	0.56	0.00	0.00	0.01	0.01
12.93	0.56	0.00	0.00	0.01	0.01	12.94	0.56	0.00	0.00	0.01	0.01
12.95	0.56	0.00	0.00	0.01	0.01	12.96	0.56	0.00	0.00	0.01	0.01
12.97	0.56	0.00	0.00	0.01	0.01	12.98	0.56	0.00	0.00	0.01	0.01
12.99	0.56	0.00	0.00	0.01	0.01	13.00	0.56	0.00	0.00	0.01	0.01
13.01	0.56	0.00	0.00	0.01	0.01	13.02	0.56	0.00	0.00	0.01	0.01
13.03	0.56	0.00	0.00	0.01	0.01	13.04	0.55	0.00	0.00	0.01	0.01
13.05	0.54	0.00	0.00	0.01	0.01	13.06	0.52	0.00	0.00	0.01	0.01
13.07	0.50	0.00	0.00	0.01	0.01	13.08	0.48	0.00	0.00	0.01	0.01
13.09	0.47	0.00	0.00	0.01	0.01	13.10	0.45	0.00	0.00	0.01	0.01
13.11	0.44	0.00	0.00	0.01	0.01	13.12	0.42	0.00	0.00	0.01	0.01
13.13	0.41	0.00	0.00	0.01	0.01	13.14	0.39	0.00	0.00	0.01	0.01
13.15	0.36	0.00	0.00	0.01	0.02	13.16	0.34	0.00	0.00	0.01	0.02
13.17	0.31	0.00	0.00	0.01	0.02	13.18	0.29	0.00	0.00	0.01	0.02
13.19	0.26	0.00	0.00	0.01	0.02	13.20	0.25	0.00	0.00	0.01	0.02
13.21	0.23	0.00	0.00	0.01	0.02	13.22	0.23	0.00	0.00	0.01	0.02
13.23	0.22	0.00	0.00	0.01	0.02	13.24	0.21	0.00	0.00	0.01	0.02
13.25	0.20	0.00	0.00	0.01	0.02	13.26	0.19	0.00	0.00	0.01	0.02
13.27	0.18	0.00	0.00	0.01	0.02	13.28	0.18	0.00	0.00	0.01	0.02
13.29	0.17	0.00	0.00	0.01	0.02	13.30	0.17	0.00	0.00	0.01	0.02
13.31	0.17	0.00	0.00	0.01	0.02	13.32	0.17	0.00	0.00	0.01	0.02
13.33	0.17	0.00	0.00	0.01	0.02	13.34	0.17	0.00	0.00	0.01	0.02
13.35	0.17	0.00	0.00	0.01	0.02	13.36	0.17	0.00	0.00	0.01	0.02
13.37	0.17	0.00	0.00	0.01	0.02	13.38	0.17	0.00	0.00	0.01	0.02
13.39	0.18	0.00	0.00	0.01	0.02	13.40	0.20	0.00	0.00	0.01	0.02
13.41	0.21	0.00	0.00	0.01	0.02	13.42	0.23	0.00	0.00	0.01	0.02
13.43	0.24	0.00	0.00	0.01	0.02	13.44	0.26	0.00	0.00	0.01	0.02

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
13.45	0.27	0.00	0.00	0.01	0.02	13.46	0.29	0.00	0.00	0.01	0.02
13.47	0.30	0.00	0.00	0.01	0.02	13.48	0.32	0.00	0.00	0.01	0.02
13.49	0.34	0.00	0.00	0.01	0.02	13.50	0.37	0.00	0.00	0.01	0.02
13.51	0.39	0.00	0.00	0.01	0.01	13.52	0.41	0.00	0.00	0.01	0.01
13.53	0.44	0.00	0.00	0.01	0.01	13.54	0.46	0.00	0.00	0.01	0.01
13.55	0.47	0.00	0.00	0.01	0.01	13.56	0.47	0.00	0.00	0.01	0.01
13.57	0.47	0.00	0.00	0.01	0.01	13.58	0.46	0.00	0.00	0.01	0.01
13.59	0.46	0.00	0.00	0.01	0.01	13.60	0.45	0.00	0.00	0.01	0.01
13.61	0.45	0.00	0.00	0.01	0.01	13.62	0.44	0.00	0.00	0.01	0.01
13.63	0.44	0.00	0.00	0.01	0.01	13.64	0.43	0.00	0.00	0.01	0.01
13.65	0.43	0.00	0.00	0.01	0.01	13.66	0.43	0.00	0.00	0.01	0.01
13.67	0.43	0.00	0.00	0.01	0.01	13.68	0.43	0.00	0.00	0.01	0.01
13.69	0.43	0.00	0.00	0.01	0.01	13.70	0.43	0.00	0.00	0.01	0.01
13.71	0.43	0.00	0.00	0.01	0.01	13.72	0.43	0.00	0.00	0.01	0.01
13.73	0.44	0.00	0.00	0.01	0.01	13.74	0.45	0.00	0.00	0.01	0.01
13.75	0.46	0.00	0.00	0.01	0.01	13.76	0.47	0.00	0.00	0.01	0.01
13.77	0.48	0.00	0.00	0.01	0.01	13.78	0.50	0.00	0.00	0.01	0.01
13.79	0.51	0.00	0.00	0.01	0.01	13.80	0.52	0.00	0.00	0.01	0.01
13.81	0.52	0.00	0.00	0.01	0.01	13.82	0.52	0.00	0.00	0.01	0.01
13.83	0.51	0.00	0.00	0.01	0.01	13.84	0.49	0.00	0.00	0.01	0.01
13.85	0.47	0.00	0.00	0.01	0.01	13.86	0.46	0.00	0.00	0.01	0.01
13.87	0.44	0.00	0.00	0.01	0.01	13.88	0.43	0.00	0.00	0.01	0.01
13.89	0.41	0.00	0.00	0.01	0.01	13.90	0.40	0.00	0.00	0.01	0.01
13.91	0.39	0.00	0.00	0.01	0.01	13.92	0.38	0.00	0.00	0.01	0.01
13.93	0.36	0.00	0.00	0.01	0.02	13.94	0.34	0.00	0.00	0.01	0.02
13.95	0.33	0.00	0.00	0.01	0.02	13.96	0.31	0.00	0.00	0.01	0.02
13.97	0.30	0.00	0.00	0.01	0.02	13.98	0.29	0.00	0.00	0.01	0.02
13.99	0.28	0.00	0.00	0.01	0.02	14.00	0.28	0.00	0.00	0.01	0.02
14.01	0.28	0.00	0.00	0.01	0.02	14.02	0.28	0.00	0.00	0.01	0.02
14.03	0.28	0.00	0.00	0.01	0.02	14.04	0.28	0.00	0.00	0.01	0.02
14.05	0.28	0.00	0.00	0.01	0.02	14.06	0.28	0.00	0.00	0.01	0.02
14.07	0.28	0.00	0.00	0.01	0.02	14.08	0.29	0.00	0.00	0.01	0.02
14.09	0.30	0.00	0.00	0.01	0.02	14.10	0.32	0.00	0.00	0.01	0.02
14.11	0.33	0.00	0.00	0.01	0.02	14.12	0.35	0.00	0.00	0.01	0.02
14.13	0.36	0.00	0.00	0.01	0.02	14.14	0.38	0.00	0.00	0.01	0.01
14.15	0.39	0.00	0.00	0.01	0.01	14.16	0.40	0.00	0.00	0.01	0.01
14.17	0.42	0.00	0.00	0.01	0.01	14.18	0.44	0.00	0.00	0.01	0.01
14.19	0.46	0.00	0.00	0.01	0.01	14.20	0.48	0.00	0.00	0.01	0.01
14.21	0.51	0.00	0.00	0.01	0.01	14.22	0.53	0.00	0.00	0.01	0.01
14.23	0.55	0.00	0.00	0.01	0.01	14.24	0.57	0.00	0.00	0.01	0.01
14.25	0.58	0.00	0.00	0.01	0.01	14.26	0.60	0.00	0.00	0.01	0.01
14.27	0.62	0.00	0.00	0.01	0.01	14.28	0.64	0.00	0.00	0.01	0.01
14.29	0.67	0.00	0.00	0.01	0.01	14.30	0.69	0.00	0.00	0.01	0.01
14.31	0.71	0.00	0.00	0.01	0.01	14.32	0.73	0.00	0.00	0.01	0.01
14.33	0.75	0.00	0.00	0.01	0.01	14.34	0.76	0.00	0.00	0.01	0.01
14.35	0.77	0.00	0.00	0.01	0.01	14.36	0.78	0.00	0.00	0.01	0.01
14.37	0.80	0.00	0.00	0.01	0.00	14.38	0.81	0.00	0.00	0.01	0.00
14.39	0.83	0.00	0.00	0.01	0.00	14.40	0.84	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
14.41	0.85	0.00	0.00	0.01	0.00	14.42	0.86	0.00	0.00	0.01	0.00
14.43	0.85	0.00	0.00	0.01	0.00	14.44	0.85	0.00	0.00	0.01	0.00
14.45	0.84	0.00	0.00	0.01	0.00	14.46	0.83	0.00	0.00	0.01	0.00
14.47	0.82	0.00	0.00	0.01	0.00	14.48	0.81	0.00	0.00	0.01	0.00
14.49	0.81	0.00	0.00	0.01	0.00	14.50	0.80	0.00	0.00	0.01	0.00
14.51	0.78	0.00	0.00	0.01	0.01	14.52	0.75	0.00	0.00	0.01	0.01
14.53	0.72	0.00	0.00	0.01	0.01	14.54	0.69	0.00	0.00	0.01	0.01
14.55	0.65	0.00	0.00	0.01	0.01	14.56	0.61	0.00	0.00	0.01	0.01
14.57	0.58	0.00	0.00	0.01	0.01	14.58	0.55	0.00	0.00	0.01	0.01
14.59	0.53	0.00	0.00	0.01	0.01	14.60	0.51	0.00	0.00	0.01	0.01
14.61	0.50	0.00	0.00	0.01	0.01	14.62	0.48	0.00	0.00	0.01	0.01
14.63	0.47	0.00	0.00	0.01	0.01	14.64	0.45	0.00	0.00	0.01	0.01
14.65	0.44	0.00	0.00	0.01	0.01	14.66	0.42	0.00	0.00	0.01	0.01
14.67	0.41	0.00	0.00	0.01	0.01	14.68	0.41	0.00	0.00	0.01	0.01
14.69	0.41	0.00	0.00	0.01	0.01	14.70	0.42	0.00	0.00	0.01	0.01
14.71	0.44	0.00	0.00	0.01	0.01	14.72	0.45	0.00	0.00	0.01	0.01
14.73	0.46	0.00	0.00	0.01	0.01	14.74	0.47	0.00	0.00	0.01	0.01
14.75	0.48	0.00	0.00	0.01	0.01	14.76	0.49	0.00	0.00	0.01	0.01
14.77	0.49	0.00	0.00	0.01	0.01	14.78	0.49	0.00	0.00	0.01	0.01
14.79	0.49	0.00	0.00	0.01	0.01	14.80	0.49	0.00	0.00	0.01	0.01
14.81	0.49	0.00	0.00	0.01	0.01	14.82	0.49	0.00	0.00	0.01	0.01
14.83	0.49	0.00	0.00	0.01	0.01	14.84	0.49	0.00	0.00	0.01	0.01
14.85	0.50	0.00	0.00	0.01	0.01	14.86	0.50	0.00	0.00	0.01	0.01
14.87	0.51	0.00	0.00	0.01	0.01	14.88	0.53	0.00	0.00	0.01	0.01
14.89	0.54	0.00	0.00	0.01	0.01	14.90	0.56	0.00	0.00	0.01	0.01
14.91	0.57	0.00	0.00	0.01	0.01	14.92	0.59	0.00	0.00	0.01	0.01
14.93	0.60	0.00	0.00	0.01	0.01	14.94	0.61	0.00	0.00	0.01	0.01
14.95	0.62	0.00	0.00	0.01	0.01	14.96	0.63	0.00	0.00	0.01	0.01
14.97	0.64	0.00	0.00	0.01	0.01	14.98	0.66	0.00	0.00	0.01	0.01
14.99	0.67	0.00	0.00	0.01	0.01	15.00	0.69	0.00	0.00	0.01	0.01
15.01	0.70	0.00	0.00	0.01	0.01	15.02	0.71	0.00	0.00	0.01	0.01
15.03	0.70	0.00	0.00	0.01	0.01	15.04	0.69	0.00	0.00	0.01	0.01
15.05	0.68	0.00	0.00	0.01	0.01	15.06	0.66	0.00	0.00	0.01	0.01
15.07	0.64	0.00	0.00	0.01	0.01	15.08	0.62	0.00	0.00	0.01	0.01
15.09	0.61	0.00	0.00	0.01	0.01	15.10	0.59	0.00	0.00	0.01	0.01
15.11	0.58	0.00	0.00	0.01	0.01	15.12	0.58	0.00	0.00	0.01	0.01
15.13	0.59	0.00	0.00	0.01	0.01	15.14	0.59	0.00	0.00	0.01	0.01
15.15	0.60	0.00	0.00	0.01	0.01	15.16	0.61	0.00	0.00	0.01	0.01
15.17	0.62	0.00	0.00	0.01	0.01	15.18	0.62	0.00	0.00	0.01	0.01
15.19	0.63	0.00	0.00	0.01	0.01	15.20	0.64	0.00	0.00	0.01	0.01
15.21	0.66	0.00	0.00	0.01	0.01	15.22	0.69	0.00	0.00	0.01	0.01
15.23	0.71	0.00	0.00	0.01	0.01	15.24	0.74	0.00	0.00	0.01	0.01
15.25	0.78	0.00	0.00	0.01	0.01	15.26	0.80	0.00	0.00	0.01	0.00
15.27	0.83	0.00	0.00	0.01	0.00	15.28	0.85	0.00	0.00	0.01	0.00
15.29	0.88	0.00	0.00	0.01	0.00	15.30	0.90	0.00	0.00	0.01	0.00
15.31	0.94	0.00	0.00	0.01	0.00	15.32	0.97	0.00	0.00	0.01	0.00
15.33	1.01	0.00	0.00	0.01	0.00	15.34	1.04	0.00	0.00	0.01	0.00
15.35	1.08	0.00	0.00	0.01	0.00	15.36	1.11	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
15.37	1.13	0.00	0.00	0.01	0.00	15.38	1.15	0.00	0.00	0.01	0.00
15.39	1.18	0.00	0.00	0.01	0.00	15.40	1.21	0.00	0.00	0.01	0.00
15.41	1.24	0.00	0.00	0.01	0.00	15.42	1.27	0.00	0.00	0.01	0.00
15.43	1.29	0.00	0.00	0.01	0.00	15.44	1.32	0.00	0.00	0.01	0.00
15.45	1.33	0.00	0.00	0.01	0.00	15.46	1.33	0.00	0.00	0.01	0.00
15.47	1.31	0.00	0.00	0.01	0.00	15.48	1.28	0.00	0.00	0.01	0.00
15.49	1.24	0.00	0.00	0.01	0.00	15.50	1.20	0.00	0.00	0.01	0.00
15.51	1.16	0.00	0.00	0.01	0.00	15.52	1.12	0.00	0.00	0.01	0.00
15.53	1.09	0.00	0.00	0.01	0.00	15.54	1.06	0.00	0.00	0.01	0.00
15.55	1.03	0.00	0.00	0.01	0.00	15.56	1.00	0.00	0.00	0.01	0.00
15.57	0.97	0.00	0.00	0.01	0.00	15.58	0.93	0.00	0.00	0.01	0.00
15.59	0.89	0.00	0.00	0.01	0.00	15.60	0.86	0.00	0.00	0.01	0.00
15.61	0.82	0.00	0.00	0.01	0.00	15.62	0.79	0.00	0.00	0.01	0.00
15.63	0.77	0.00	0.00	0.01	0.01	15.64	0.76	0.00	0.00	0.01	0.01
15.65	0.76	0.00	0.00	0.01	0.01	15.66	0.76	0.00	0.00	0.01	0.01
15.67	0.75	0.00	0.00	0.01	0.01	15.68	0.75	0.00	0.00	0.01	0.01
15.69	0.74	0.00	0.00	0.01	0.01	15.70	0.74	0.00	0.00	0.01	0.01
15.71	0.74	0.00	0.00	0.01	0.01	15.72	0.73	0.00	0.00	0.01	0.01
15.73	0.73	0.00	0.00	0.01	0.01	15.74	0.72	0.00	0.00	0.01	0.01
15.75	0.71	0.00	0.00	0.01	0.01	15.76	0.71	0.00	0.00	0.01	0.01
15.77	0.70	0.00	0.00	0.01	0.01	15.78	0.69	0.00	0.00	0.01	0.01
15.79	0.68	0.00	0.00	0.01	0.01	15.80	0.68	0.00	0.00	0.01	0.01
15.81	0.67	0.00	0.00	0.01	0.01	15.82	0.67	0.00	0.00	0.01	0.01
15.83	0.66	0.00	0.00	0.01	0.01	15.84	0.65	0.00	0.00	0.01	0.01
15.85	0.65	0.00	0.00	0.01	0.01	15.86	0.64	0.00	0.00	0.01	0.01
15.87	0.63	0.00	0.00	0.01	0.01	15.88	0.62	0.00	0.00	0.01	0.01
15.89	0.62	0.00	0.00	0.01	0.01	15.90	0.61	0.00	0.00	0.01	0.01
15.91	0.61	0.00	0.00	0.01	0.01	15.92	0.60	0.00	0.00	0.01	0.01
15.93	0.59	0.00	0.00	0.01	0.01	15.94	0.59	0.00	0.00	0.01	0.01
15.95	0.58	0.00	0.00	0.01	0.01	15.96	0.57	0.00	0.00	0.01	0.01
15.97	0.57	0.00	0.00	0.01	0.01	15.98	0.56	0.00	0.00	0.01	0.01
15.99	0.56	0.00	0.00	0.01	0.01	16.00	0.56	0.00	0.00	0.01	0.01
16.01	0.56	0.00	0.00	0.01	0.01	16.02	0.56	0.00	0.00	0.01	0.01
16.03	0.56	0.00	0.00	0.01	0.01	16.04	0.56	0.00	0.00	0.01	0.01
16.05	0.56	0.00	0.00	0.01	0.01	16.06	0.56	0.00	0.00	0.01	0.01
16.07	0.56	0.00	0.00	0.01	0.01	16.08	0.56	0.00	0.00	0.01	0.01
16.09	0.56	0.00	0.00	0.01	0.01	16.10	0.56	0.00	0.00	0.01	0.01
16.11	0.56	0.00	0.00	0.01	0.01	16.12	0.56	0.00	0.00	0.01	0.01
16.13	0.56	0.00	0.00	0.01	0.01	16.14	0.56	0.00	0.00	0.01	0.01
16.15	0.56	0.00	0.00	0.01	0.01	16.16	0.56	0.00	0.00	0.01	0.01
16.17	0.56	0.00	0.00	0.01	0.01	16.18	0.55	0.00	0.00	0.01	0.01
16.19	0.55	0.00	0.00	0.01	0.01	16.20	0.55	0.00	0.00	0.01	0.01
16.21	0.55	0.00	0.00	0.01	0.01	16.22	0.55	0.00	0.00	0.01	0.01
16.23	0.56	0.00	0.00	0.01	0.01	16.24	0.56	0.00	0.00	0.01	0.01
16.25	0.58	0.00	0.00	0.01	0.01	16.26	0.61	0.00	0.00	0.01	0.01
16.27	0.63	0.00	0.00	0.01	0.01	16.28	0.66	0.00	0.00	0.01	0.01
16.29	0.69	0.00	0.00	0.01	0.01	16.30	0.71	0.00	0.00	0.01	0.01
16.31	0.74	0.00	0.00	0.01	0.01	16.32	0.76	0.00	0.00	0.01	0.01

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
16.33	0.78	0.00	0.00	0.01	0.01	16.34	0.81	0.00	0.00	0.01	0.00
16.35	0.84	0.00	0.00	0.01	0.00	16.36	0.87	0.00	0.00	0.01	0.00
16.37	0.91	0.00	0.00	0.01	0.00	16.38	0.94	0.00	0.00	0.01	0.00
16.39	0.97	0.00	0.00	0.01	0.00	16.40	1.00	0.00	0.00	0.01	0.00
16.41	1.02	0.00	0.00	0.01	0.00	16.42	1.05	0.00	0.00	0.01	0.00
16.43	1.08	0.00	0.00	0.01	0.00	16.44	1.12	0.00	0.00	0.01	0.00
16.45	1.16	0.00	0.00	0.01	0.00	16.46	1.21	0.00	0.00	0.01	0.00
16.47	1.24	0.00	0.00	0.01	0.00	16.48	1.28	0.00	0.00	0.01	0.00
16.49	1.30	0.00	0.00	0.01	0.00	16.50	1.34	0.00	0.00	0.01	0.00
16.51	1.38	0.00	0.00	0.01	0.00	16.52	1.42	0.00	0.00	0.01	0.00
16.53	1.48	0.00	0.00	0.01	0.00	16.54	1.53	0.00	0.00	0.01	0.00
16.55	1.59	0.00	0.00	0.01	0.00	16.56	1.64	0.00	0.00	0.01	0.00
16.57	1.69	0.00	0.00	0.01	0.00	16.58	1.72	0.00	0.00	0.01	0.00
16.59	1.73	0.00	0.00	0.01	0.00	16.60	1.74	0.00	0.00	0.01	0.00
16.61	1.74	0.00	0.00	0.01	0.00	16.62	1.74	0.00	0.00	0.01	0.00
16.63	1.74	0.00	0.00	0.01	0.00	16.64	1.74	0.00	0.00	0.01	0.00
16.65	2.00	0.00	0.00	0.01	0.00	16.66	2.00	0.00	0.00	0.01	0.00
16.67	2.00	0.00	0.00	0.01	0.00	16.68	2.00	0.00	0.00	0.01	0.00
16.69	2.00	0.00	0.00	0.01	0.00	16.70	2.00	0.00	0.00	0.01	0.00
16.71	1.63	0.00	0.00	0.01	0.00	16.72	1.60	0.00	0.00	0.01	0.00
16.73	1.57	0.00	0.00	0.01	0.00	16.74	1.54	0.00	0.00	0.01	0.00
16.75	1.52	0.00	0.00	0.01	0.00	16.76	1.49	0.00	0.00	0.01	0.00
16.77	1.47	0.00	0.00	0.01	0.00	16.78	1.45	0.00	0.00	0.01	0.00
16.79	1.42	0.00	0.00	0.01	0.00	16.80	1.39	0.00	0.00	0.01	0.00
16.81	1.36	0.00	0.00	0.01	0.00	16.82	1.33	0.00	0.00	0.01	0.00
16.83	1.30	0.00	0.00	0.01	0.00	16.84	1.28	0.00	0.00	0.01	0.00
16.85	1.25	0.00	0.00	0.01	0.00	16.86	1.22	0.00	0.00	0.01	0.00
16.87	1.17	0.00	0.00	0.01	0.00	16.88	1.13	0.00	0.00	0.01	0.00
16.89	1.08	0.00	0.00	0.01	0.00	16.90	1.03	0.00	0.00	0.01	0.00
16.91	0.98	0.00	0.00	0.01	0.00	16.92	0.94	0.00	0.00	0.01	0.00
16.93	0.91	0.00	0.00	0.01	0.00	16.94	0.89	0.00	0.00	0.01	0.00
16.95	0.88	0.00	0.00	0.01	0.00	16.96	0.86	0.00	0.00	0.01	0.00
16.97	0.84	0.00	0.00	0.01	0.00	16.98	0.81	0.00	0.00	0.01	0.00
16.99	0.79	0.00	0.00	0.01	0.00	17.00	0.78	0.00	0.00	0.01	0.01
17.01	0.76	0.00	0.00	0.01	0.01	17.02	0.76	0.00	0.00	0.01	0.01
17.03	0.76	0.00	0.00	0.01	0.01	17.04	0.77	0.00	0.00	0.01	0.01
17.05	0.78	0.00	0.00	0.01	0.00	17.06	0.79	0.00	0.00	0.01	0.00
17.07	0.80	0.00	0.00	0.01	0.00	17.08	0.81	0.00	0.00	0.01	0.00
17.09	0.82	0.00	0.00	0.01	0.00	17.10	0.82	0.00	0.00	0.01	0.00
17.11	0.82	0.00	0.00	0.01	0.00	17.12	0.82	0.00	0.00	0.01	0.00
17.13	0.82	0.00	0.00	0.01	0.00	17.14	0.82	0.00	0.00	0.01	0.00
17.15	0.82	0.00	0.00	0.01	0.00	17.16	0.82	0.00	0.00	0.01	0.00
17.17	0.82	0.00	0.00	0.01	0.00	17.18	0.82	0.00	0.00	0.01	0.00
17.19	0.81	0.00	0.00	0.01	0.00	17.20	0.80	0.00	0.00	0.01	0.00
17.21	0.77	0.00	0.00	0.01	0.01	17.22	0.74	0.00	0.00	0.01	0.01
17.23	0.71	0.00	0.00	0.01	0.01	17.24	0.68	0.00	0.00	0.01	0.01
17.25	0.66	0.00	0.00	0.01	0.01	17.26	0.63	0.00	0.00	0.01	0.01
17.27	0.61	0.00	0.00	0.01	0.01	17.28	0.59	0.00	0.00	0.01	0.01

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
17.29	0.57	0.00	0.00	0.01	0.01	17.30	0.54	0.00	0.00	0.01	0.01
17.31	0.51	0.00	0.00	0.01	0.01	17.32	0.48	0.00	0.00	0.01	0.01
17.33	0.46	0.00	0.00	0.01	0.01	17.34	0.43	0.00	0.00	0.01	0.01
17.35	0.40	0.00	0.00	0.01	0.01	17.36	0.39	0.00	0.00	0.01	0.01
17.37	0.38	0.00	0.00	0.01	0.01	17.38	0.38	0.00	0.00	0.01	0.01
17.39	0.39	0.00	0.00	0.01	0.01	17.40	0.39	0.00	0.00	0.01	0.01
17.41	0.39	0.00	0.00	0.01	0.01	17.42	0.39	0.00	0.00	0.01	0.01
17.43	0.39	0.00	0.00	0.01	0.01	17.44	0.39	0.00	0.00	0.01	0.01
17.45	0.40	0.00	0.00	0.01	0.01	17.46	0.40	0.00	0.00	0.01	0.01
17.47	0.40	0.00	0.00	0.01	0.01	17.48	0.40	0.00	0.00	0.01	0.01
17.49	0.40	0.00	0.00	0.01	0.01	17.50	0.40	0.00	0.00	0.01	0.01
17.51	0.41	0.00	0.00	0.01	0.01	17.52	0.41	0.00	0.00	0.01	0.01
17.53	0.41	0.00	0.00	0.01	0.01	17.54	0.42	0.00	0.00	0.01	0.01
17.55	0.42	0.00	0.00	0.01	0.01	17.56	0.44	0.00	0.00	0.01	0.01
17.57	0.45	0.00	0.00	0.01	0.01	17.58	0.46	0.00	0.00	0.01	0.01
17.59	0.47	0.00	0.00	0.01	0.01	17.60	0.49	0.00	0.00	0.01	0.01
17.61	0.50	0.00	0.00	0.01	0.01	17.62	0.50	0.00	0.00	0.01	0.01
17.63	0.51	0.00	0.00	0.01	0.01	17.64	0.52	0.00	0.00	0.01	0.01
17.65	0.54	0.00	0.00	0.01	0.01	17.66	0.55	0.00	0.00	0.01	0.01
17.67	0.56	0.00	0.00	0.01	0.01	17.68	0.57	0.00	0.00	0.01	0.01
17.69	0.58	0.00	0.00	0.01	0.01	17.70	0.59	0.00	0.00	0.01	0.01
17.71	0.60	0.00	0.00	0.01	0.01	17.72	0.60	0.00	0.00	0.01	0.01
17.73	0.59	0.00	0.00	0.01	0.01	17.74	0.58	0.00	0.00	0.01	0.01
17.75	0.58	0.00	0.00	0.01	0.01	17.76	0.57	0.00	0.00	0.01	0.01
17.77	0.56	0.00	0.00	0.01	0.01	17.78	0.56	0.00	0.00	0.01	0.01
17.79	0.55	0.00	0.00	0.01	0.01	17.80	0.55	0.00	0.00	0.01	0.01
17.81	0.54	0.00	0.00	0.01	0.01	17.82	0.54	0.00	0.00	0.01	0.01
17.83	0.53	0.00	0.00	0.01	0.01	17.84	0.52	0.00	0.00	0.01	0.01
17.85	0.52	0.00	0.00	0.01	0.01	17.86	0.51	0.00	0.00	0.01	0.01
17.87	0.50	0.00	0.00	0.01	0.01	17.88	0.50	0.00	0.00	0.01	0.01
17.89	0.50	0.00	0.00	0.01	0.01	17.90	0.50	0.00	0.00	0.01	0.01
17.91	0.50	0.00	0.00	0.01	0.01	17.92	0.50	0.00	0.00	0.01	0.01
17.93	0.50	0.00	0.00	0.01	0.01	17.94	0.50	0.00	0.00	0.01	0.01
17.95	0.50	0.00	0.00	0.01	0.01	17.96	0.50	0.00	0.00	0.01	0.01
17.97	0.50	0.00	0.00	0.01	0.01	17.98	0.50	0.00	0.00	0.01	0.01
17.99	0.51	0.00	0.00	0.01	0.01	18.00	0.52	0.00	0.00	0.01	0.01
18.01	0.53	0.00	0.00	0.01	0.01	18.02	0.53	0.00	0.00	0.01	0.01
18.03	0.54	0.00	0.00	0.01	0.01	18.04	0.55	0.00	0.00	0.01	0.01
18.05	0.56	0.00	0.00	0.01	0.01	18.06	0.57	0.00	0.00	0.01	0.01
18.07	0.60	0.00	0.00	0.01	0.01	18.08	0.63	0.00	0.00	0.01	0.01
18.09	0.66	0.00	0.00	0.01	0.01	18.10	0.70	0.00	0.00	0.01	0.01
18.11	0.74	0.00	0.00	0.01	0.01	18.12	0.77	0.00	0.00	0.01	0.01
18.13	0.80	0.00	0.00	0.01	0.00	18.14	0.83	0.00	0.00	0.01	0.00
18.15	0.87	0.00	0.00	0.01	0.00	18.16	0.92	0.00	0.00	0.01	0.00
18.17	0.98	0.00	0.00	0.01	0.00	18.18	1.05	0.00	0.00	0.01	0.00
18.19	1.12	0.00	0.00	0.01	0.00	18.20	1.18	0.00	0.00	0.01	0.00
18.21	1.24	0.00	0.00	0.01	0.00	18.22	1.29	0.00	0.00	0.01	0.00
18.23	1.32	0.00	0.00	0.01	0.00	18.24	1.35	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
18.25	1.37	0.00	0.00	0.01	0.00	18.26	1.39	0.00	0.00	0.01	0.00
18.27	1.42	0.00	0.00	0.01	0.00	18.28	1.45	0.00	0.00	0.01	0.00
18.29	1.48	0.00	0.00	0.01	0.00	18.30	1.50	0.00	0.00	0.01	0.00
18.31	1.51	0.00	0.00	0.01	0.00	18.32	1.51	0.00	0.00	0.01	0.00
18.33	1.50	0.00	0.00	0.01	0.00	18.34	1.48	0.00	0.00	0.01	0.00
18.35	1.46	0.00	0.00	0.01	0.00	18.36	1.44	0.00	0.00	0.01	0.00
18.37	1.41	0.00	0.00	0.01	0.00	18.38	1.39	0.00	0.00	0.01	0.00
18.39	1.38	0.00	0.00	0.01	0.00	18.40	1.36	0.00	0.00	0.01	0.00
18.41	1.33	0.00	0.00	0.01	0.00	18.42	1.30	0.00	0.00	0.01	0.00
18.43	1.27	0.00	0.00	0.01	0.00	18.44	1.23	0.00	0.00	0.01	0.00
18.45	1.20	0.00	0.00	0.01	0.00	18.46	1.16	0.00	0.00	0.01	0.00
18.47	1.13	0.00	0.00	0.01	0.00	18.48	1.10	0.00	0.00	0.01	0.00
18.49	1.07	0.00	0.00	0.01	0.00	18.50	1.04	0.00	0.00	0.01	0.00
18.51	1.01	0.00	0.00	0.01	0.00	18.52	0.97	0.00	0.00	0.01	0.00
18.53	0.92	0.00	0.00	0.01	0.00	18.54	0.88	0.00	0.00	0.01	0.00
18.55	0.84	0.00	0.00	0.01	0.00	18.56	0.80	0.00	0.00	0.01	0.00
18.57	0.77	0.00	0.00	0.01	0.01	18.58	0.74	0.00	0.00	0.01	0.01
18.59	0.72	0.00	0.00	0.01	0.01	18.60	0.70	0.00	0.00	0.01	0.01
18.61	0.67	0.00	0.00	0.01	0.01	18.62	0.64	0.00	0.00	0.01	0.01
18.63	0.61	0.00	0.00	0.01	0.01	18.64	0.59	0.00	0.00	0.01	0.01
18.65	0.57	0.00	0.00	0.01	0.01	18.66	0.55	0.00	0.00	0.01	0.01
18.67	0.53	0.00	0.00	0.01	0.01	18.68	0.52	0.00	0.00	0.01	0.01
18.69	0.50	0.00	0.00	0.01	0.01	18.70	0.48	0.00	0.00	0.01	0.01
18.71	0.47	0.00	0.00	0.01	0.01	18.72	0.45	0.00	0.00	0.01	0.01
18.73	0.43	0.00	0.00	0.01	0.01	18.74	0.42	0.00	0.00	0.01	0.01
18.75	0.41	0.00	0.00	0.01	0.01	18.76	0.40	0.00	0.00	0.01	0.01
18.77	0.40	0.00	0.00	0.01	0.01	18.78	0.39	0.00	0.00	0.01	0.01
18.79	0.38	0.00	0.00	0.01	0.01	18.80	0.37	0.00	0.00	0.01	0.01
18.81	0.36	0.00	0.00	0.01	0.01	18.82	0.36	0.00	0.00	0.01	0.01
18.83	0.35	0.00	0.00	0.01	0.01	18.84	0.35	0.00	0.00	0.01	0.01
18.85	0.35	0.00	0.00	0.01	0.01	18.86	0.35	0.00	0.00	0.01	0.01
18.87	0.35	0.00	0.00	0.01	0.01	18.88	0.35	0.00	0.00	0.01	0.01
18.89	0.35	0.00	0.00	0.01	0.01	18.90	0.35	0.00	0.00	0.01	0.01
18.91	0.35	0.00	0.00	0.01	0.01	18.92	0.35	0.00	0.00	0.01	0.01
18.93	0.35	0.00	0.00	0.01	0.01	18.94	0.36	0.00	0.00	0.01	0.01
18.95	0.36	0.00	0.00	0.01	0.01	18.96	0.37	0.00	0.00	0.01	0.01
18.97	0.38	0.00	0.00	0.01	0.01	18.98	0.39	0.00	0.00	0.01	0.01
18.99	0.40	0.00	0.00	0.01	0.01	19.00	0.40	0.00	0.00	0.01	0.01
19.01	0.41	0.00	0.00	0.01	0.01	19.02	0.41	0.00	0.00	0.01	0.01
19.03	0.42	0.00	0.00	0.01	0.01	19.04	0.43	0.00	0.00	0.01	0.01
19.05	0.43	0.00	0.00	0.01	0.01	19.06	0.44	0.00	0.00	0.01	0.01
19.07	0.45	0.00	0.00	0.01	0.01	19.08	0.46	0.00	0.00	0.01	0.01
19.09	0.46	0.00	0.00	0.01	0.01	19.10	0.46	0.00	0.00	0.01	0.01
19.11	0.46	0.00	0.00	0.01	0.01	19.12	0.46	0.00	0.00	0.01	0.01
19.13	0.46	0.00	0.00	0.01	0.01	19.14	0.46	0.00	0.00	0.01	0.01
19.15	0.46	0.00	0.00	0.01	0.01	19.16	0.46	0.00	0.00	0.01	0.01
19.17	0.46	0.00	0.00	0.01	0.01	19.18	0.46	0.00	0.00	0.01	0.01
19.19	0.46	0.00	0.00	0.01	0.01	19.20	0.45	0.00	0.00	0.01	0.01

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
19.21	0.44	0.00	0.00	0.01	0.01	19.22	0.43	0.00	0.00	0.01	0.01
19.23	0.42	0.00	0.00	0.01	0.01	19.24	0.42	0.00	0.00	0.01	0.01
19.25	0.41	0.00	0.00	0.01	0.01	19.26	0.40	0.00	0.00	0.01	0.01
19.27	0.40	0.00	0.00	0.01	0.01	19.28	0.39	0.00	0.00	0.01	0.01
19.29	0.38	0.00	0.00	0.01	0.01	19.30	0.38	0.00	0.00	0.01	0.01
19.31	0.37	0.00	0.00	0.01	0.01	19.32	0.36	0.00	0.00	0.01	0.01
19.33	0.35	0.00	0.00	0.01	0.01	19.34	0.34	0.00	0.00	0.01	0.01
19.35	0.34	0.00	0.00	0.01	0.01	19.36	0.34	0.00	0.00	0.01	0.01
19.37	0.34	0.00	0.00	0.01	0.01	19.38	0.34	0.00	0.00	0.01	0.01
19.39	0.34	0.00	0.00	0.01	0.01	19.40	0.34	0.00	0.00	0.01	0.01
19.41	0.34	0.00	0.00	0.01	0.01	19.42	0.34	0.00	0.00	0.01	0.01
19.43	0.34	0.00	0.00	0.01	0.01	19.44	0.34	0.00	0.00	0.01	0.01
19.45	0.34	0.00	0.00	0.01	0.01	19.46	0.34	0.00	0.00	0.01	0.01
19.47	0.33	0.00	0.00	0.01	0.01	19.48	0.33	0.00	0.00	0.01	0.01
19.49	0.33	0.00	0.00	0.01	0.01	19.50	0.33	0.00	0.00	0.01	0.01
19.51	0.33	0.00	0.00	0.01	0.01	19.52	0.33	0.00	0.00	0.01	0.01
19.53	0.33	0.00	0.00	0.01	0.01	19.54	0.33	0.00	0.00	0.01	0.01
19.55	0.33	0.00	0.00	0.01	0.01	19.56	0.33	0.00	0.00	0.01	0.01
19.57	0.33	0.00	0.00	0.01	0.01	19.58	0.33	0.00	0.00	0.01	0.01
19.59	0.33	0.00	0.00	0.01	0.01	19.60	0.33	0.00	0.00	0.01	0.01
19.61	0.33	0.00	0.00	0.01	0.01	19.62	0.33	0.00	0.00	0.01	0.01
19.63	0.33	0.00	0.00	0.01	0.01	19.64	0.33	0.00	0.00	0.01	0.01
19.65	0.33	0.00	0.00	0.01	0.01	19.66	0.33	0.00	0.00	0.01	0.01
19.67	0.33	0.00	0.00	0.01	0.01	19.68	0.32	0.00	0.00	0.01	0.01
19.69	0.32	0.00	0.00	0.01	0.01	19.70	0.32	0.00	0.00	0.01	0.01
19.71	0.32	0.00	0.00	0.01	0.01	19.72	0.31	0.00	0.00	0.01	0.01
19.73	0.30	0.00	0.00	0.01	0.01	19.74	0.30	0.00	0.00	0.01	0.02
19.75	0.29	0.00	0.00	0.01	0.02	19.76	0.28	0.00	0.00	0.01	0.02
19.77	0.27	0.00	0.00	0.01	0.02	19.78	0.27	0.00	0.00	0.01	0.02
19.79	0.28	0.00	0.00	0.01	0.02	19.80	0.31	0.00	0.00	0.01	0.01
19.81	0.35	0.00	0.00	0.01	0.01	19.82	0.39	0.00	0.00	0.01	0.01
19.83	0.43	0.00	0.00	0.01	0.01	19.84	0.47	0.00	0.00	0.01	0.01
19.85	0.52	0.00	0.00	0.01	0.01	19.86	0.55	0.00	0.00	0.01	0.01
19.87	0.59	0.00	0.00	0.01	0.01	19.88	0.62	0.00	0.00	0.01	0.01
19.89	0.66	0.00	0.00	0.01	0.01	19.90	0.70	0.00	0.00	0.01	0.01
19.91	0.75	0.00	0.00	0.01	0.01	19.92	0.80	0.00	0.00	0.01	0.00
19.93	0.85	0.00	0.00	0.01	0.00	19.94	0.90	0.00	0.00	0.01	0.00
19.95	0.94	0.00	0.00	0.01	0.00	19.96	0.95	0.00	0.00	0.01	0.00
19.97	0.93	0.00	0.00	0.01	0.00	19.98	0.89	0.00	0.00	0.01	0.00
19.99	0.84	0.00	0.00	0.01	0.00	20.00	0.79	0.00	0.00	0.01	0.00
20.01	0.74	0.00	0.00	0.01	0.01	20.02	0.69	0.00	0.00	0.01	0.01
20.03	0.65	0.00	0.00	0.01	0.01	20.04	0.61	0.00	0.00	0.01	0.01
20.05	0.58	0.00	0.00	0.01	0.01	20.06	0.54	0.00	0.00	0.01	0.01
20.07	0.51	0.00	0.00	0.01	0.01	20.08	0.47	0.00	0.00	0.01	0.01
20.09	0.43	0.00	0.00	0.01	0.01	20.10	0.39	0.00	0.00	0.01	0.01
20.11	0.35	0.00	0.00	0.01	0.01	20.12	0.32	0.00	0.00	0.01	0.01
20.13	0.29	0.00	0.00	0.01	0.01	20.14	0.28	0.00	0.00	0.01	0.02
20.15	0.28	0.00	0.00	0.01	0.02	20.16	0.27	0.00	0.00	0.01	0.02

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
20.17	0.27	0.00	0.00	0.01	0.02	20.18	0.27	0.00	0.00	0.01	0.02
20.19	0.27	0.00	0.00	0.01	0.02	20.20	0.27	0.00	0.00	0.01	0.02
20.21	0.26	0.00	0.00	0.01	0.02	20.22	0.26	0.00	0.00	0.01	0.02
20.23	0.26	0.00	0.00	0.01	0.02	20.24	0.26	0.00	0.00	0.01	0.02
20.25	0.26	0.00	0.00	0.01	0.02	20.26	0.26	0.00	0.00	0.01	0.02
20.27	0.25	0.00	0.00	0.01	0.02	20.28	0.25	0.00	0.00	0.01	0.02
20.29	0.25	0.00	0.00	0.01	0.02	20.30	0.25	0.00	0.00	0.01	0.02
20.31	0.26	0.00	0.00	0.01	0.02	20.32	0.27	0.00	0.00	0.01	0.02
20.33	0.28	0.00	0.00	0.01	0.02	20.34	0.30	0.00	0.00	0.01	0.01
20.35	0.31	0.00	0.00	0.01	0.01	20.36	0.33	0.00	0.00	0.01	0.01
20.37	0.35	0.00	0.00	0.01	0.01	20.38	0.36	0.00	0.00	0.01	0.01
20.39	0.37	0.00	0.00	0.01	0.01	20.40	0.39	0.00	0.00	0.01	0.01
20.41	0.41	0.00	0.00	0.01	0.01	20.42	0.43	0.00	0.00	0.01	0.01
20.43	0.45	0.00	0.00	0.01	0.01	20.44	0.48	0.00	0.00	0.01	0.01
20.45	0.50	0.00	0.00	0.01	0.01	20.46	0.53	0.00	0.00	0.01	0.01
20.47	0.55	0.00	0.00	0.01	0.01	20.48	0.56	0.00	0.00	0.01	0.01
20.49	0.58	0.00	0.00	0.01	0.01	20.50	0.61	0.00	0.00	0.01	0.01
20.51	0.63	0.00	0.00	0.01	0.01	20.52	0.66	0.00	0.00	0.01	0.01
20.53	0.69	0.00	0.00	0.01	0.01	20.54	0.72	0.00	0.00	0.01	0.01
20.55	0.74	0.00	0.00	0.01	0.01	20.56	0.76	0.00	0.00	0.01	0.01
20.57	0.78	0.00	0.00	0.01	0.00	20.58	0.79	0.00	0.00	0.01	0.00
20.59	0.80	0.00	0.00	0.01	0.00	20.60	0.82	0.00	0.00	0.01	0.00
20.61	0.84	0.00	0.00	0.01	0.00	20.62	0.85	0.00	0.00	0.01	0.00
20.63	0.87	0.00	0.00	0.01	0.00	20.64	0.88	0.00	0.00	0.01	0.00
20.65	0.89	0.00	0.00	0.01	0.00	20.66	0.91	0.00	0.00	0.01	0.00
20.67	0.92	0.00	0.00	0.01	0.00	20.68	0.93	0.00	0.00	0.01	0.00
20.69	0.95	0.00	0.00	0.01	0.00	20.70	0.97	0.00	0.00	0.01	0.00
20.71	0.98	0.00	0.00	0.01	0.00	20.72	1.00	0.00	0.00	0.01	0.00
20.73	1.01	0.00	0.00	0.01	0.00	20.74	1.01	0.00	0.00	0.01	0.00
20.75	1.01	0.00	0.00	0.01	0.00	20.76	1.00	0.00	0.00	0.01	0.00
20.77	1.00	0.00	0.00	0.01	0.00	20.78	0.99	0.00	0.00	0.01	0.00
20.79	0.98	0.00	0.00	0.01	0.00	20.80	0.97	0.00	0.00	0.01	0.00
20.81	0.96	0.00	0.00	0.01	0.00	20.82	0.95	0.00	0.00	0.01	0.00
20.83	0.94	0.00	0.00	0.01	0.00	20.84	0.92	0.00	0.00	0.01	0.00
20.85	0.90	0.00	0.00	0.01	0.00	20.86	0.87	0.00	0.00	0.01	0.00
20.87	0.84	0.00	0.00	0.01	0.00	20.88	0.81	0.00	0.00	0.01	0.00
20.89	0.78	0.00	0.00	0.01	0.00	20.90	0.76	0.00	0.00	0.01	0.00
20.91	0.74	0.00	0.00	0.01	0.01	20.92	0.73	0.00	0.00	0.01	0.01
20.93	0.71	0.00	0.00	0.01	0.01	20.94	0.70	0.00	0.00	0.01	0.01
20.95	0.68	0.00	0.00	0.01	0.01	20.96	0.66	0.00	0.00	0.01	0.01
20.97	0.65	0.00	0.00	0.01	0.01	20.98	0.63	0.00	0.00	0.01	0.01
20.99	0.62	0.00	0.00	0.01	0.01	21.00	0.61	0.00	0.00	0.01	0.01
21.01	0.59	0.00	0.00	0.01	0.01	21.02	0.58	0.00	0.00	0.01	0.01
21.03	0.56	0.00	0.00	0.01	0.01	21.04	0.55	0.00	0.00	0.01	0.01
21.05	0.53	0.00	0.00	0.01	0.01	21.06	0.51	0.00	0.00	0.01	0.01
21.07	0.50	0.00	0.00	0.01	0.01	21.08	0.49	0.00	0.00	0.01	0.01
21.09	0.48	0.00	0.00	0.01	0.01	21.10	0.47	0.00	0.00	0.01	0.01
21.11	0.46	0.00	0.00	0.01	0.01	21.12	0.45	0.00	0.00	0.01	0.01

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
21.13	0.45	0.00	0.00	0.01	0.01	21.14	0.44	0.00	0.00	0.01	0.01
21.15	0.43	0.00	0.00	0.01	0.01	21.16	0.42	0.00	0.00	0.01	0.01
21.17	0.42	0.00	0.00	0.01	0.01	21.18	0.43	0.00	0.00	0.01	0.01
21.19	0.45	0.00	0.00	0.01	0.01	21.20	0.47	0.00	0.00	0.01	0.01
21.21	0.49	0.00	0.00	0.01	0.01	21.22	0.51	0.00	0.00	0.01	0.01
21.23	0.53	0.00	0.00	0.01	0.01	21.24	0.55	0.00	0.00	0.01	0.01
21.25	0.57	0.00	0.00	0.01	0.01	21.26	0.59	0.00	0.00	0.01	0.01
21.27	0.62	0.00	0.00	0.01	0.01	21.28	0.66	0.00	0.00	0.01	0.01
21.29	0.70	0.00	0.00	0.01	0.01	21.30	0.75	0.00	0.00	0.01	0.01
21.31	0.80	0.00	0.00	0.01	0.00	21.32	0.84	0.00	0.00	0.01	0.00
21.33	0.88	0.00	0.00	0.01	0.00	21.34	0.91	0.00	0.00	0.01	0.00
21.35	0.94	0.00	0.00	0.01	0.00	21.36	0.96	0.00	0.00	0.01	0.00
21.37	0.98	0.00	0.00	0.01	0.00	21.38	1.01	0.00	0.00	0.01	0.00
21.39	1.04	0.00	0.00	0.01	0.00	21.40	1.06	0.00	0.00	0.01	0.00
21.41	1.09	0.00	0.00	0.01	0.00	21.42	1.11	0.00	0.00	0.01	0.00
21.43	1.13	0.00	0.00	0.01	0.00	21.44	1.15	0.00	0.00	0.01	0.00
21.45	1.17	0.00	0.00	0.01	0.00	21.46	1.20	0.00	0.00	0.01	0.00
21.47	1.24	0.00	0.00	0.01	0.00	21.48	1.27	0.00	0.00	0.01	0.00
21.49	1.30	0.00	0.00	0.01	0.00	21.50	1.33	0.00	0.00	0.01	0.00
21.51	1.35	0.00	0.00	0.01	0.00	21.52	1.37	0.00	0.00	0.01	0.00
21.53	1.37	0.00	0.00	0.01	0.00	21.54	1.37	0.00	0.00	0.01	0.00
21.55	1.37	0.00	0.00	0.01	0.00	21.56	1.37	0.00	0.00	0.01	0.00
21.57	1.37	0.00	0.00	0.01	0.00	21.58	1.37	0.00	0.00	0.01	0.00
21.59	1.37	0.00	0.00	0.01	0.00	21.60	1.37	0.00	0.00	0.01	0.00
21.61	1.35	0.00	0.00	0.01	0.00	21.62	1.32	0.00	0.00	0.01	0.00
21.63	1.27	0.00	0.00	0.01	0.00	21.64	1.23	0.00	0.00	0.01	0.00
21.65	1.18	0.00	0.00	0.01	0.00	21.66	1.13	0.00	0.00	0.01	0.00
21.67	1.08	0.00	0.00	0.01	0.00	21.68	1.04	0.00	0.00	0.01	0.00
21.69	1.01	0.00	0.00	0.01	0.00	21.70	0.99	0.00	0.00	0.01	0.00
21.71	0.96	0.00	0.00	0.01	0.00	21.72	0.93	0.00	0.00	0.01	0.00
21.73	0.89	0.00	0.00	0.01	0.00	21.74	0.86	0.00	0.00	0.01	0.00
21.75	0.82	0.00	0.00	0.01	0.00	21.76	0.79	0.00	0.00	0.01	0.00
21.77	0.76	0.00	0.00	0.01	0.00	21.78	0.74	0.00	0.00	0.01	0.01
21.79	0.72	0.00	0.00	0.01	0.01	21.80	0.69	0.00	0.00	0.01	0.01
21.81	0.66	0.00	0.00	0.01	0.01	21.82	0.63	0.00	0.00	0.01	0.01
21.83	0.60	0.00	0.00	0.01	0.01	21.84	0.57	0.00	0.00	0.01	0.01
21.85	0.54	0.00	0.00	0.01	0.01	21.86	0.52	0.00	0.00	0.01	0.01
21.87	0.50	0.00	0.00	0.01	0.01	21.88	0.49	0.00	0.00	0.01	0.01
21.89	0.47	0.00	0.00	0.01	0.01	21.90	0.45	0.00	0.00	0.01	0.01
21.91	0.42	0.00	0.00	0.01	0.01	21.92	0.40	0.00	0.00	0.01	0.01
21.93	0.38	0.00	0.00	0.01	0.01	21.94	0.36	0.00	0.00	0.01	0.01
21.95	0.35	0.00	0.00	0.01	0.01	21.96	0.34	0.00	0.00	0.01	0.01
21.97	0.33	0.00	0.00	0.01	0.01	21.98	0.33	0.00	0.00	0.01	0.01
21.99	0.32	0.00	0.00	0.01	0.01	22.00	0.31	0.00	0.00	0.01	0.01
22.01	0.31	0.00	0.00	0.01	0.01	22.02	0.30	0.00	0.00	0.01	0.01
22.03	0.29	0.00	0.00	0.01	0.01	22.04	0.29	0.00	0.00	0.01	0.01
22.05	0.29	0.00	0.00	0.01	0.01	22.06	0.29	0.00	0.00	0.01	0.01
22.07	0.29	0.00	0.00	0.01	0.01	22.08	0.29	0.00	0.00	0.01	0.01

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
22.09	0.29	0.00	0.00	0.01	0.01	22.10	0.29	0.00	0.00	0.01	0.01
22.11	0.29	0.00	0.00	0.01	0.01	22.12	0.29	0.00	0.00	0.01	0.01
22.13	0.29	0.00	0.00	0.01	0.01	22.14	0.29	0.00	0.00	0.01	0.01
22.15	0.29	0.00	0.00	0.01	0.01	22.16	0.29	0.00	0.00	0.01	0.01
22.17	0.29	0.00	0.00	0.01	0.01	22.18	0.29	0.00	0.00	0.01	0.01
22.19	0.29	0.00	0.00	0.01	0.01	22.20	0.29	0.00	0.00	0.01	0.01
22.21	0.29	0.00	0.00	0.01	0.01	22.22	0.28	0.00	0.00	0.01	0.01
22.23	0.28	0.00	0.00	0.01	0.01	22.24	0.28	0.00	0.00	0.01	0.01
22.25	0.27	0.00	0.00	0.01	0.01	22.26	0.27	0.00	0.00	0.01	0.01
22.27	0.27	0.00	0.00	0.01	0.01	22.28	0.26	0.00	0.00	0.01	0.01
22.29	0.26	0.00	0.00	0.01	0.01	22.30	0.26	0.00	0.00	0.01	0.01
22.31	0.27	0.00	0.00	0.01	0.01	22.32	0.27	0.00	0.00	0.01	0.01
22.33	0.28	0.00	0.00	0.01	0.01	22.34	0.29	0.00	0.00	0.01	0.01
22.35	0.29	0.00	0.00	0.01	0.01	22.36	0.30	0.00	0.00	0.01	0.01
22.37	0.30	0.00	0.00	0.01	0.01	22.38	0.31	0.00	0.00	0.01	0.01
22.39	0.31	0.00	0.00	0.01	0.01	22.40	0.32	0.00	0.00	0.01	0.01
22.41	0.32	0.00	0.00	0.01	0.01	22.42	0.32	0.00	0.00	0.01	0.01
22.43	0.32	0.00	0.00	0.01	0.01	22.44	0.33	0.00	0.00	0.01	0.01
22.45	0.33	0.00	0.00	0.01	0.01	22.46	0.33	0.00	0.00	0.01	0.01
22.47	0.34	0.00	0.00	0.01	0.01	22.48	0.34	0.00	0.00	0.01	0.01
22.49	0.34	0.00	0.00	0.01	0.01	22.50	0.35	0.00	0.00	0.01	0.01
22.51	0.35	0.00	0.00	0.01	0.01	22.52	0.36	0.00	0.00	0.01	0.01
22.53	0.36	0.00	0.00	0.01	0.01	22.54	0.37	0.00	0.00	0.01	0.01
22.55	0.37	0.00	0.00	0.01	0.01	22.56	0.37	0.00	0.00	0.01	0.01
22.57	0.37	0.00	0.00	0.01	0.01	22.58	0.37	0.00	0.00	0.01	0.01
22.59	0.37	0.00	0.00	0.01	0.01	22.60	0.37	0.00	0.00	0.01	0.01
22.61	0.37	0.00	0.00	0.01	0.01	22.62	0.37	0.00	0.00	0.01	0.01
22.63	0.37	0.00	0.00	0.01	0.01	22.64	0.37	0.00	0.00	0.01	0.01
22.65	0.37	0.00	0.00	0.01	0.01	22.66	0.36	0.00	0.00	0.01	0.01
22.67	0.35	0.00	0.00	0.01	0.01	22.68	0.33	0.00	0.00	0.01	0.01
22.69	0.32	0.00	0.00	0.01	0.01	22.70	0.31	0.00	0.00	0.01	0.01
22.71	0.30	0.00	0.00	0.01	0.01	22.72	0.29	0.00	0.00	0.01	0.01
22.73	0.28	0.00	0.00	0.01	0.01	22.74	0.28	0.00	0.00	0.01	0.01
22.75	0.28	0.00	0.00	0.01	0.01	22.76	0.28	0.00	0.00	0.01	0.01
22.77	0.28	0.00	0.00	0.01	0.01	22.78	0.28	0.00	0.00	0.01	0.01
22.79	0.28	0.00	0.00	0.01	0.01	22.80	0.28	0.00	0.00	0.01	0.01
22.81	0.28	0.00	0.00	0.01	0.01	22.82	0.28	0.00	0.00	0.01	0.01
22.83	0.28	0.00	0.00	0.01	0.01	22.84	0.28	0.00	0.00	0.01	0.01
22.85	0.28	0.00	0.00	0.01	0.01	22.86	0.28	0.00	0.00	0.01	0.01
22.87	0.28	0.00	0.00	0.01	0.01	22.88	0.28	0.00	0.00	0.01	0.01
22.89	0.28	0.00	0.00	0.01	0.01	22.90	0.28	0.00	0.00	0.01	0.01
22.91	0.28	0.00	0.00	0.01	0.01	22.92	0.28	0.00	0.00	0.01	0.01
22.93	0.28	0.00	0.00	0.01	0.01	22.94	0.28	0.00	0.00	0.01	0.01
22.95	0.28	0.00	0.00	0.01	0.01	22.96	0.28	0.00	0.00	0.01	0.01
22.97	0.28	0.00	0.00	0.01	0.01	22.98	0.28	0.00	0.00	0.01	0.01
22.99	0.28	0.00	0.00	0.01	0.01	23.00	0.29	0.00	0.00	0.01	0.01
23.01	0.30	0.00	0.00	0.01	0.01	23.02	0.32	0.00	0.00	0.01	0.01
23.03	0.34	0.00	0.00	0.01	0.01	23.04	0.35	0.00	0.00	0.01	0.01

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
23.05	0.37	0.00	0.00	0.01	0.01	23.06	0.38	0.00	0.00	0.01	0.01
23.07	0.40	0.00	0.00	0.01	0.01	23.08	0.40	0.00	0.00	0.01	0.01
23.09	0.41	0.00	0.00	0.01	0.01	23.10	0.42	0.00	0.00	0.01	0.01
23.11	0.42	0.00	0.00	0.01	0.01	23.12	0.43	0.00	0.00	0.01	0.01
23.13	0.44	0.00	0.00	0.01	0.01	23.14	0.44	0.00	0.00	0.01	0.01
23.15	0.45	0.00	0.00	0.01	0.01	23.16	0.45	0.00	0.00	0.01	0.01
23.17	0.45	0.00	0.00	0.01	0.01	23.18	0.45	0.00	0.00	0.01	0.01
23.19	0.45	0.00	0.00	0.01	0.01	23.20	0.44	0.00	0.00	0.01	0.01
23.21	0.44	0.00	0.00	0.01	0.01	23.22	0.44	0.00	0.00	0.01	0.01
23.23	0.43	0.00	0.00	0.01	0.01	23.24	0.43	0.00	0.00	0.01	0.01
23.25	0.43	0.00	0.00	0.01	0.01	23.26	0.43	0.00	0.00	0.01	0.01
23.27	0.44	0.00	0.00	0.01	0.01	23.28	0.44	0.00	0.00	0.01	0.01
23.29	0.45	0.00	0.00	0.01	0.01	23.30	0.46	0.00	0.00	0.01	0.01
23.31	0.46	0.00	0.00	0.01	0.01	23.32	0.47	0.00	0.00	0.01	0.01
23.33	0.47	0.00	0.00	0.01	0.01	23.34	0.48	0.00	0.00	0.01	0.01
23.35	0.48	0.00	0.00	0.01	0.01	23.36	0.49	0.00	0.00	0.01	0.01
23.37	0.49	0.00	0.00	0.01	0.01	23.38	0.50	0.00	0.00	0.01	0.01
23.39	0.51	0.00	0.00	0.01	0.01	23.40	0.51	0.00	0.00	0.01	0.01
23.41	0.52	0.00	0.00	0.01	0.01	23.42	0.52	0.00	0.00	0.01	0.01
23.43	0.53	0.00	0.00	0.01	0.01	23.44	0.53	0.00	0.00	0.01	0.01
23.45	0.54	0.00	0.00	0.01	0.01	23.46	0.55	0.00	0.00	0.01	0.01
23.47	0.55	0.00	0.00	0.01	0.01	23.48	0.56	0.00	0.00	0.01	0.01
23.49	0.56	0.00	0.00	0.01	0.01	23.50	0.57	0.00	0.00	0.01	0.01
23.51	0.57	0.00	0.00	0.01	0.01	23.52	0.58	0.00	0.00	0.01	0.01
23.53	0.59	0.00	0.00	0.01	0.01	23.54	0.60	0.00	0.00	0.01	0.01
23.55	0.60	0.00	0.00	0.01	0.01	23.56	0.61	0.00	0.00	0.01	0.01
23.57	0.62	0.00	0.00	0.01	0.01	23.58	0.63	0.00	0.00	0.01	0.01
23.59	0.64	0.00	0.00	0.01	0.01	23.60	0.64	0.00	0.00	0.01	0.01
23.61	0.65	0.00	0.00	0.01	0.01	23.62	0.65	0.00	0.00	0.01	0.01
23.63	0.66	0.00	0.00	0.01	0.01	23.64	0.67	0.00	0.00	0.01	0.01
23.65	0.67	0.00	0.00	0.01	0.01	23.66	0.68	0.00	0.00	0.01	0.01
23.67	0.68	0.00	0.00	0.01	0.01	23.68	0.69	0.00	0.00	0.01	0.01
23.69	0.69	0.00	0.00	0.01	0.01	23.70	0.68	0.00	0.00	0.01	0.01
23.71	0.68	0.00	0.00	0.01	0.01	23.72	0.68	0.00	0.00	0.01	0.01
23.73	0.68	0.00	0.00	0.01	0.01	23.74	0.67	0.00	0.00	0.01	0.01
23.75	0.67	0.00	0.00	0.01	0.01	23.76	0.67	0.00	0.00	0.01	0.01
23.77	0.67	0.00	0.00	0.01	0.01	23.78	0.69	0.00	0.00	0.01	0.01
23.79	0.71	0.00	0.00	0.01	0.01	23.80	0.73	0.00	0.00	0.01	0.01
23.81	0.75	0.00	0.00	0.01	0.00	23.82	0.78	0.00	0.00	0.01	0.00
23.83	0.80	0.00	0.00	0.01	0.00	23.84	0.82	0.00	0.00	0.01	0.00
23.85	0.84	0.00	0.00	0.01	0.00	23.86	0.85	0.00	0.00	0.01	0.00
23.87	0.86	0.00	0.00	0.01	0.00	23.88	0.87	0.00	0.00	0.01	0.00
23.89	0.88	0.00	0.00	0.01	0.00	23.90	0.89	0.00	0.00	0.01	0.00
23.91	0.90	0.00	0.00	0.01	0.00	23.92	0.91	0.00	0.00	0.01	0.00
23.93	0.92	0.00	0.00	0.01	0.00	23.94	0.92	0.00	0.00	0.01	0.00
23.95	0.91	0.00	0.00	0.01	0.00	23.96	0.90	0.00	0.00	0.01	0.00
23.97	0.88	0.00	0.00	0.01	0.00	23.98	0.86	0.00	0.00	0.01	0.00
23.99	0.85	0.00	0.00	0.01	0.00	24.00	0.83	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
24.01	0.81	0.00	0.00	0.01	0.00	24.02	0.80	0.00	0.00	0.01	0.00
24.03	0.79	0.00	0.00	0.01	0.00	24.04	0.78	0.00	0.00	0.01	0.00
24.05	0.78	0.00	0.00	0.01	0.00	24.06	0.77	0.00	0.00	0.01	0.00
24.07	0.77	0.00	0.00	0.01	0.00	24.08	0.77	0.00	0.00	0.01	0.00
24.09	0.76	0.00	0.00	0.01	0.00	24.10	0.76	0.00	0.00	0.01	0.00
24.11	0.76	0.00	0.00	0.01	0.00	24.12	0.75	0.00	0.00	0.01	0.00
24.13	0.74	0.00	0.00	0.01	0.00	24.14	0.73	0.00	0.00	0.01	0.01
24.15	0.72	0.00	0.00	0.01	0.01	24.16	0.71	0.00	0.00	0.01	0.01
24.17	0.70	0.00	0.00	0.01	0.01	24.18	0.69	0.00	0.00	0.01	0.01
24.19	0.68	0.00	0.00	0.01	0.01	24.20	0.67	0.00	0.00	0.01	0.01
24.21	0.66	0.00	0.00	0.01	0.01	24.22	0.65	0.00	0.00	0.01	0.01
24.23	0.64	0.00	0.00	0.01	0.01	24.24	0.63	0.00	0.00	0.01	0.01
24.25	0.62	0.00	0.00	0.01	0.01	24.26	0.61	0.00	0.00	0.01	0.01
24.27	0.59	0.00	0.00	0.01	0.01	24.28	0.59	0.00	0.00	0.01	0.01
24.29	0.58	0.00	0.00	0.01	0.01	24.30	0.59	0.00	0.00	0.01	0.01
24.31	0.60	0.00	0.00	0.01	0.01	24.32	0.61	0.00	0.00	0.01	0.01
24.33	0.62	0.00	0.00	0.01	0.01	24.34	0.63	0.00	0.00	0.01	0.01
24.35	0.64	0.00	0.00	0.01	0.01	24.36	0.65	0.00	0.00	0.01	0.01
24.37	0.66	0.00	0.00	0.01	0.01	24.38	0.67	0.00	0.00	0.01	0.01
24.39	0.67	0.00	0.00	0.01	0.01	24.40	0.68	0.00	0.00	0.01	0.01
24.41	0.69	0.00	0.00	0.01	0.01	24.42	0.71	0.00	0.00	0.01	0.01
24.43	0.72	0.00	0.00	0.01	0.01	24.44	0.73	0.00	0.00	0.01	0.01
24.45	0.74	0.00	0.00	0.01	0.01	24.46	0.74	0.00	0.00	0.01	0.00
24.47	0.74	0.00	0.00	0.01	0.00	24.48	0.74	0.00	0.00	0.01	0.00
24.49	0.74	0.00	0.00	0.01	0.00	24.50	0.74	0.00	0.00	0.01	0.00
24.51	0.74	0.00	0.00	0.01	0.00	24.52	0.74	0.00	0.00	0.01	0.00
24.53	0.74	0.00	0.00	0.01	0.00	24.54	0.74	0.00	0.00	0.01	0.00
24.55	0.74	0.00	0.00	0.01	0.00	24.56	0.74	0.00	0.00	0.01	0.01
24.57	0.73	0.00	0.00	0.01	0.01	24.58	0.72	0.00	0.00	0.01	0.01
24.59	0.72	0.00	0.00	0.01	0.01	24.60	0.71	0.00	0.00	0.01	0.01
24.61	0.70	0.00	0.00	0.01	0.01	24.62	0.70	0.00	0.00	0.01	0.01
24.63	0.69	0.00	0.00	0.01	0.01	24.64	0.69	0.00	0.00	0.01	0.01
24.65	0.68	0.00	0.00	0.01	0.01	24.66	0.68	0.00	0.00	0.01	0.01
24.67	0.67	0.00	0.00	0.01	0.01	24.68	0.66	0.00	0.00	0.01	0.01
24.69	0.66	0.00	0.00	0.01	0.01	24.70	0.65	0.00	0.00	0.01	0.01
24.71	0.65	0.00	0.00	0.01	0.01	24.72	0.64	0.00	0.00	0.01	0.01
24.73	0.64	0.00	0.00	0.01	0.01	24.74	0.63	0.00	0.00	0.01	0.01
24.75	0.62	0.00	0.00	0.01	0.01	24.76	0.62	0.00	0.00	0.01	0.01
24.77	0.61	0.00	0.00	0.01	0.01	24.78	0.60	0.00	0.00	0.01	0.01
24.79	0.60	0.00	0.00	0.01	0.01	24.80	0.59	0.00	0.00	0.01	0.01
24.81	0.59	0.00	0.00	0.01	0.01	24.82	0.58	0.00	0.00	0.01	0.01
24.83	0.57	0.00	0.00	0.01	0.01	24.84	0.56	0.00	0.00	0.01	0.01
24.85	0.54	0.00	0.00	0.01	0.01	24.86	0.53	0.00	0.00	0.01	0.01
24.87	0.52	0.00	0.00	0.01	0.01	24.88	0.51	0.00	0.00	0.01	0.01
24.89	0.50	0.00	0.00	0.01	0.01	24.90	0.49	0.00	0.00	0.01	0.01
24.91	0.48	0.00	0.00	0.01	0.01	24.92	0.48	0.00	0.00	0.01	0.01
24.93	0.47	0.00	0.00	0.01	0.01	24.94	0.47	0.00	0.00	0.01	0.01
24.95	0.46	0.00	0.00	0.01	0.01	24.96	0.45	0.00	0.00	0.01	0.01

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
24.97	0.45	0.00	0.00	0.01	0.01	24.98	0.44	0.00	0.00	0.01	0.01
24.99	0.44	0.00	0.00	0.01	0.01	25.00	0.43	0.00	0.00	0.01	0.01
25.01	0.43	0.00	0.00	0.01	0.01	25.02	0.42	0.00	0.00	0.01	0.01
25.03	0.41	0.00	0.00	0.01	0.01	25.04	0.41	0.00	0.00	0.01	0.01
25.05	0.40	0.00	0.00	0.01	0.01	25.06	0.40	0.00	0.00	0.01	0.01
25.07	0.39	0.00	0.00	0.01	0.01	25.08	0.39	0.00	0.00	0.01	0.01
25.09	0.38	0.00	0.00	0.01	0.01	25.10	0.37	0.00	0.00	0.01	0.01
25.11	0.37	0.00	0.00	0.01	0.01	25.12	0.36	0.00	0.00	0.01	0.01
25.13	0.36	0.00	0.00	0.01	0.01	25.14	0.35	0.00	0.00	0.01	0.01
25.15	0.35	0.00	0.00	0.01	0.01	25.16	0.34	0.00	0.00	0.01	0.01
25.17	0.34	0.00	0.00	0.01	0.01	25.18	0.34	0.00	0.00	0.01	0.01
25.19	0.34	0.00	0.00	0.01	0.01	25.20	0.34	0.00	0.00	0.01	0.01
25.21	0.34	0.00	0.00	0.01	0.01	25.22	0.34	0.00	0.00	0.01	0.01
25.23	0.34	0.00	0.00	0.01	0.01	25.24	0.34	0.00	0.00	0.01	0.01
25.25	0.34	0.00	0.00	0.01	0.01	25.26	0.33	0.00	0.00	0.01	0.01
25.27	0.33	0.00	0.00	0.01	0.01	25.28	0.32	0.00	0.00	0.01	0.01
25.29	0.31	0.00	0.00	0.01	0.01	25.30	0.31	0.00	0.00	0.01	0.01
25.31	0.30	0.00	0.00	0.01	0.01	25.32	0.30	0.00	0.00	0.01	0.01
25.33	0.29	0.00	0.00	0.01	0.01	25.34	0.29	0.00	0.00	0.01	0.01
25.35	0.29	0.00	0.00	0.01	0.01	25.36	0.29	0.00	0.00	0.01	0.01
25.37	0.29	0.00	0.00	0.01	0.01	25.38	0.29	0.00	0.00	0.01	0.01
25.39	0.29	0.00	0.00	0.01	0.01	25.40	0.29	0.00	0.00	0.01	0.01
25.41	0.29	0.00	0.00	0.01	0.01	25.42	0.29	0.00	0.00	0.01	0.01
25.43	0.30	0.00	0.00	0.01	0.01	25.44	0.30	0.00	0.00	0.01	0.01
25.45	0.31	0.00	0.00	0.01	0.01	25.46	0.32	0.00	0.00	0.01	0.01
25.47	0.32	0.00	0.00	0.01	0.01	25.48	0.33	0.00	0.00	0.01	0.01
25.49	0.33	0.00	0.00	0.01	0.01	25.50	0.34	0.00	0.00	0.01	0.01
25.51	0.34	0.00	0.00	0.01	0.01	25.52	0.35	0.00	0.00	0.01	0.01
25.53	0.35	0.00	0.00	0.01	0.01	25.54	0.36	0.00	0.00	0.01	0.01
25.55	0.36	0.00	0.00	0.01	0.01	25.56	0.37	0.00	0.00	0.01	0.01
25.57	0.38	0.00	0.00	0.01	0.01	25.58	0.38	0.00	0.00	0.01	0.01
25.59	0.38	0.00	0.00	0.01	0.01	25.60	0.39	0.00	0.00	0.01	0.01
25.61	0.39	0.00	0.00	0.01	0.01	25.62	0.40	0.00	0.00	0.01	0.01
25.63	0.41	0.00	0.00	0.01	0.01	25.64	0.41	0.00	0.00	0.01	0.01
25.65	0.42	0.00	0.00	0.01	0.01	25.66	0.42	0.00	0.00	0.01	0.01
25.67	0.43	0.00	0.00	0.01	0.01	25.68	0.43	0.00	0.00	0.01	0.01
25.69	0.43	0.00	0.00	0.01	0.01	25.70	0.43	0.00	0.00	0.01	0.01
25.71	0.43	0.00	0.00	0.01	0.01	25.72	0.43	0.00	0.00	0.01	0.01
25.73	0.43	0.00	0.00	0.01	0.01	25.74	0.43	0.00	0.00	0.01	0.01
25.75	0.43	0.00	0.00	0.01	0.01	25.76	0.43	0.00	0.00	0.01	0.01
25.77	0.43	0.00	0.00	0.01	0.01	25.78	0.44	0.00	0.00	0.01	0.01
25.79	0.44	0.00	0.00	0.01	0.01	25.80	0.45	0.00	0.00	0.01	0.01
25.81	0.45	0.00	0.00	0.01	0.01	25.82	0.46	0.00	0.00	0.01	0.01
25.83	0.47	0.00	0.00	0.01	0.01	25.84	0.47	0.00	0.00	0.01	0.01
25.85	0.47	0.00	0.00	0.01	0.01	25.86	0.48	0.00	0.00	0.01	0.01
25.87	0.48	0.00	0.00	0.01	0.01	25.88	0.49	0.00	0.00	0.01	0.01
25.89	0.49	0.00	0.00	0.01	0.01	25.90	0.50	0.00	0.00	0.01	0.01
25.91	0.51	0.00	0.00	0.01	0.01	25.92	0.51	0.00	0.00	0.01	0.01

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
25.93	0.52	0.00	0.00	0.01	0.01	25.94	0.53	0.00	0.00	0.01	0.01
25.95	0.54	0.00	0.00	0.01	0.01	25.96	0.56	0.00	0.00	0.01	0.01
25.97	0.58	0.00	0.00	0.01	0.01	25.98	0.60	0.00	0.00	0.01	0.01
25.99	0.62	0.00	0.00	0.01	0.01	26.00	0.64	0.00	0.00	0.01	0.01
26.01	0.65	0.00	0.00	0.01	0.01	26.02	0.66	0.00	0.00	0.01	0.01
26.03	0.67	0.00	0.00	0.01	0.01	26.04	0.67	0.00	0.00	0.01	0.01
26.05	0.68	0.00	0.00	0.01	0.01	26.06	0.69	0.00	0.00	0.01	0.01
26.07	0.69	0.00	0.00	0.01	0.01	26.08	0.70	0.00	0.00	0.01	0.01
26.09	0.70	0.00	0.00	0.01	0.01	26.10	0.71	0.00	0.00	0.01	0.01
26.11	0.70	0.00	0.00	0.01	0.01	26.12	0.70	0.00	0.00	0.01	0.01
26.13	0.68	0.00	0.00	0.01	0.01	26.14	0.67	0.00	0.00	0.01	0.01
26.15	0.66	0.00	0.00	0.01	0.01	26.16	0.64	0.00	0.00	0.01	0.01
26.17	0.63	0.00	0.00	0.01	0.01	26.18	0.62	0.00	0.00	0.01	0.01
26.19	0.61	0.00	0.00	0.01	0.01	26.20	0.60	0.00	0.00	0.01	0.01
26.21	0.60	0.00	0.00	0.01	0.01	26.22	0.60	0.00	0.00	0.01	0.01
26.23	0.60	0.00	0.00	0.01	0.01	26.24	0.60	0.00	0.00	0.01	0.01
26.25	0.60	0.00	0.00	0.01	0.01	26.26	0.60	0.00	0.00	0.01	0.01
26.27	0.60	0.00	0.00	0.01	0.01	26.28	0.60	0.00	0.00	0.01	0.01
26.29	0.61	0.00	0.00	0.01	0.01	26.30	0.61	0.00	0.00	0.01	0.01
26.31	0.62	0.00	0.00	0.01	0.01	26.32	0.62	0.00	0.00	0.01	0.01
26.33	0.63	0.00	0.00	0.01	0.01	26.34	0.63	0.00	0.00	0.01	0.01
26.35	0.64	0.00	0.00	0.01	0.01	26.36	0.64	0.00	0.00	0.01	0.01
26.37	0.65	0.00	0.00	0.01	0.01	26.38	0.65	0.00	0.00	0.01	0.01
26.39	0.66	0.00	0.00	0.01	0.01	26.40	0.66	0.00	0.00	0.01	0.01
26.41	0.67	0.00	0.00	0.01	0.01	26.42	0.67	0.00	0.00	0.01	0.01
26.43	0.68	0.00	0.00	0.01	0.01	26.44	0.68	0.00	0.00	0.01	0.01
26.45	0.69	0.00	0.00	0.01	0.01	26.46	0.69	0.00	0.00	0.01	0.01
26.47	0.69	0.00	0.00	0.01	0.01	26.48	0.69	0.00	0.00	0.01	0.01
26.49	0.69	0.00	0.00	0.01	0.01	26.50	0.69	0.00	0.00	0.01	0.01
26.51	0.69	0.00	0.00	0.01	0.01	26.52	0.69	0.00	0.00	0.01	0.01
26.53	0.69	0.00	0.00	0.01	0.01	26.54	0.69	0.00	0.00	0.01	0.01
26.55	0.69	0.00	0.00	0.01	0.01	26.56	0.69	0.00	0.00	0.01	0.01
26.57	0.69	0.00	0.00	0.01	0.01	26.58	0.70	0.00	0.00	0.01	0.01
26.59	0.70	0.00	0.00	0.01	0.01	26.60	0.70	0.00	0.00	0.01	0.01
26.61	0.70	0.00	0.00	0.01	0.01	26.62	0.71	0.00	0.00	0.01	0.01
26.63	0.70	0.00	0.00	0.01	0.01	26.64	0.70	0.00	0.00	0.01	0.01
26.65	0.70	0.00	0.00	0.01	0.01	26.66	0.69	0.00	0.00	0.01	0.01
26.67	0.68	0.00	0.00	0.01	0.01	26.68	0.68	0.00	0.00	0.01	0.01
26.69	0.67	0.00	0.00	0.01	0.01	26.70	0.67	0.00	0.00	0.01	0.01
26.71	0.66	0.00	0.00	0.01	0.01	26.72	0.65	0.00	0.00	0.01	0.01
26.73	0.65	0.00	0.00	0.01	0.01	26.74	0.64	0.00	0.00	0.01	0.01
26.75	0.63	0.00	0.00	0.01	0.01	26.76	0.62	0.00	0.00	0.01	0.01
26.77	0.61	0.00	0.00	0.01	0.01	26.78	0.60	0.00	0.00	0.01	0.01
26.79	0.60	0.00	0.00	0.01	0.01	26.80	0.59	0.00	0.00	0.01	0.01
26.81	0.59	0.00	0.00	0.01	0.01	26.82	0.59	0.00	0.00	0.01	0.01
26.83	0.59	0.00	0.00	0.01	0.01	26.84	0.59	0.00	0.00	0.01	0.01
26.85	0.59	0.00	0.00	0.01	0.01	26.86	0.59	0.00	0.00	0.01	0.01
26.87	0.59	0.00	0.00	0.01	0.01	26.88	0.59	0.00	0.00	0.01	0.01

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
26.89	0.60	0.00	0.00	0.01	0.01	26.90	0.61	0.00	0.00	0.01	0.01
26.91	0.63	0.00	0.00	0.01	0.01	26.92	0.65	0.00	0.00	0.01	0.01
26.93	0.67	0.00	0.00	0.01	0.01	26.94	0.69	0.00	0.00	0.01	0.01
26.95	0.71	0.00	0.00	0.01	0.01	26.96	0.73	0.00	0.00	0.01	0.00
26.97	0.74	0.00	0.00	0.01	0.00	26.98	0.74	0.00	0.00	0.01	0.00
26.99	0.74	0.00	0.00	0.01	0.00	27.00	0.72	0.00	0.00	0.01	0.00
27.01	0.71	0.00	0.00	0.01	0.01	27.02	0.70	0.00	0.00	0.01	0.01
27.03	0.68	0.00	0.00	0.01	0.01	27.04	0.67	0.00	0.00	0.01	0.01
27.05	0.66	0.00	0.00	0.01	0.01	27.06	0.65	0.00	0.00	0.01	0.01
27.07	0.63	0.00	0.00	0.01	0.01	27.08	0.61	0.00	0.00	0.01	0.01
27.09	0.58	0.00	0.00	0.01	0.01	27.10	0.55	0.00	0.00	0.01	0.01
27.11	0.52	0.00	0.00	0.01	0.01	27.12	0.50	0.00	0.00	0.01	0.01
27.13	0.47	0.00	0.00	0.01	0.01	27.14	0.45	0.00	0.00	0.01	0.01
27.15	0.44	0.00	0.00	0.01	0.01	27.16	0.44	0.00	0.00	0.01	0.01
27.17	0.45	0.00	0.00	0.01	0.01	27.18	0.46	0.00	0.00	0.01	0.01
27.19	0.46	0.00	0.00	0.01	0.01	27.20	0.47	0.00	0.00	0.01	0.01
27.21	0.48	0.00	0.00	0.01	0.01	27.22	0.48	0.00	0.00	0.01	0.01
27.23	0.49	0.00	0.00	0.01	0.01	27.24	0.49	0.00	0.00	0.01	0.01
27.25	0.49	0.00	0.00	0.01	0.01	27.26	0.49	0.00	0.00	0.01	0.01
27.27	0.49	0.00	0.00	0.01	0.01	27.28	0.49	0.00	0.00	0.01	0.01
27.29	0.49	0.00	0.00	0.01	0.01	27.30	0.49	0.00	0.00	0.01	0.01
27.31	0.49	0.00	0.00	0.01	0.01	27.32	0.49	0.00	0.00	0.01	0.01
27.33	0.49	0.00	0.00	0.01	0.01	27.34	0.49	0.00	0.00	0.01	0.01
27.35	0.49	0.00	0.00	0.01	0.01	27.36	0.49	0.00	0.00	0.01	0.01
27.37	0.49	0.00	0.00	0.01	0.01	27.38	0.49	0.00	0.00	0.01	0.01
27.39	0.49	0.00	0.00	0.01	0.01	27.40	0.49	0.00	0.00	0.01	0.01
27.41	0.50	0.00	0.00	0.01	0.01	27.42	0.51	0.00	0.00	0.01	0.01
27.43	0.52	0.00	0.00	0.01	0.01	27.44	0.54	0.00	0.00	0.01	0.01
27.45	0.56	0.00	0.00	0.01	0.01	27.46	0.58	0.00	0.00	0.01	0.01
27.47	0.60	0.00	0.00	0.01	0.01	27.48	0.61	0.00	0.00	0.01	0.01
27.49	0.63	0.00	0.00	0.01	0.01	27.50	0.64	0.00	0.00	0.01	0.01
27.51	0.65	0.00	0.00	0.01	0.01	27.52	0.67	0.00	0.00	0.01	0.01
27.53	0.69	0.00	0.00	0.01	0.01	27.54	0.71	0.00	0.00	0.01	0.01
27.55	0.73	0.00	0.00	0.01	0.00	27.56	0.74	0.00	0.00	0.01	0.00
27.57	0.76	0.00	0.00	0.01	0.00	27.58	0.76	0.00	0.00	0.01	0.00
27.59	0.76	0.00	0.00	0.01	0.00	27.60	0.74	0.00	0.00	0.01	0.00
27.61	0.72	0.00	0.00	0.01	0.00	27.62	0.70	0.00	0.00	0.01	0.01
27.63	0.68	0.00	0.00	0.01	0.01	27.64	0.66	0.00	0.00	0.01	0.01
27.65	0.65	0.00	0.00	0.01	0.01	27.66	0.63	0.00	0.00	0.01	0.01
27.67	0.62	0.00	0.00	0.01	0.01	27.68	0.60	0.00	0.00	0.01	0.01
27.69	0.58	0.00	0.00	0.01	0.01	27.70	0.55	0.00	0.00	0.01	0.01
27.71	0.52	0.00	0.00	0.01	0.01	27.72	0.50	0.00	0.00	0.01	0.01
27.73	0.47	0.00	0.00	0.01	0.01	27.74	0.45	0.00	0.00	0.01	0.01
27.75	0.44	0.00	0.00	0.01	0.01	27.76	0.43	0.00	0.00	0.01	0.01
27.77	0.43	0.00	0.00	0.01	0.01	27.78	0.43	0.00	0.00	0.01	0.01
27.79	0.43	0.00	0.00	0.01	0.01	27.80	0.43	0.00	0.00	0.01	0.01
27.81	0.43	0.00	0.00	0.01	0.01	27.82	0.43	0.00	0.00	0.01	0.01
27.83	0.43	0.00	0.00	0.01	0.01	27.84	0.43	0.00	0.00	0.01	0.01

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
27.85	0.44	0.00	0.00	0.01	0.01	27.86	0.45	0.00	0.00	0.01	0.01
27.87	0.46	0.00	0.00	0.01	0.01	27.88	0.48	0.00	0.00	0.01	0.01
27.89	0.49	0.00	0.00	0.01	0.01	27.90	0.51	0.00	0.00	0.01	0.01
27.91	0.52	0.00	0.00	0.01	0.01	27.92	0.53	0.00	0.00	0.01	0.01
27.93	0.54	0.00	0.00	0.01	0.01	27.94	0.55	0.00	0.00	0.01	0.01
27.95	0.55	0.00	0.00	0.01	0.01	27.96	0.56	0.00	0.00	0.01	0.01
27.97	0.57	0.00	0.00	0.01	0.01	27.98	0.58	0.00	0.00	0.01	0.01
27.99	0.58	0.00	0.00	0.01	0.01	28.00	0.59	0.00	0.00	0.01	0.01
28.01	0.59	0.00	0.00	0.01	0.01	28.02	0.59	0.00	0.00	0.01	0.01
28.03	0.59	0.00	0.00	0.01	0.01	28.04	0.58	0.00	0.00	0.01	0.01
28.05	0.57	0.00	0.00	0.01	0.01	28.06	0.56	0.00	0.00	0.01	0.01
28.07	0.55	0.00	0.00	0.01	0.01	28.08	0.55	0.00	0.00	0.01	0.01
28.09	0.54	0.00	0.00	0.01	0.01	28.10	0.53	0.00	0.00	0.01	0.01
28.11	0.53	0.00	0.00	0.01	0.01	28.12	0.52	0.00	0.00	0.01	0.01
28.13	0.51	0.00	0.00	0.01	0.01	28.14	0.51	0.00	0.00	0.01	0.01
28.15	0.50	0.00	0.00	0.01	0.01	28.16	0.49	0.00	0.00	0.01	0.01
28.17	0.48	0.00	0.00	0.01	0.01	28.18	0.48	0.00	0.00	0.01	0.01
28.19	0.48	0.00	0.00	0.01	0.01	28.20	0.49	0.00	0.00	0.01	0.01
28.21	0.51	0.00	0.00	0.01	0.01	28.22	0.53	0.00	0.00	0.01	0.01
28.23	0.55	0.00	0.00	0.01	0.01	28.24	0.56	0.00	0.00	0.01	0.01
28.25	0.58	0.00	0.00	0.01	0.01	28.26	0.60	0.00	0.00	0.01	0.01
28.27	0.61	0.00	0.00	0.01	0.01	28.28	0.61	0.00	0.00	0.01	0.01
28.29	0.61	0.00	0.00	0.01	0.01	28.30	0.61	0.00	0.00	0.01	0.01
28.31	0.61	0.00	0.00	0.01	0.01	28.32	0.61	0.00	0.00	0.01	0.01
28.33	0.61	0.00	0.00	0.01	0.01	28.34	0.61	0.00	0.00	0.01	0.01
28.35	0.61	0.00	0.00	0.01	0.01	28.36	0.60	0.00	0.00	0.01	0.01
28.37	0.59	0.00	0.00	0.01	0.01	28.38	0.57	0.00	0.00	0.01	0.01
28.39	0.55	0.00	0.00	0.01	0.01	28.40	0.52	0.00	0.00	0.01	0.01
28.41	0.50	0.00	0.00	0.01	0.01	28.42	0.47	0.00	0.00	0.01	0.01
28.43	0.45	0.00	0.00	0.01	0.01	28.44	0.44	0.00	0.00	0.01	0.01
28.45	0.43	0.00	0.00	0.01	0.01	28.46	0.42	0.00	0.00	0.01	0.01
28.47	0.41	0.00	0.00	0.01	0.01	28.48	0.41	0.00	0.00	0.01	0.01
28.49	0.40	0.00	0.00	0.01	0.01	28.50	0.40	0.00	0.00	0.01	0.01
28.51	0.39	0.00	0.00	0.01	0.01	28.52	0.39	0.00	0.00	0.01	0.01
28.53	0.38	0.00	0.00	0.01	0.01	28.54	0.38	0.00	0.00	0.01	0.01
28.55	0.38	0.00	0.00	0.01	0.01	28.56	0.38	0.00	0.00	0.01	0.01
28.57	0.38	0.00	0.00	0.01	0.01	28.58	0.38	0.00	0.00	0.01	0.01
28.59	0.38	0.00	0.00	0.01	0.01	28.60	0.38	0.00	0.00	0.01	0.01
28.61	0.38	0.00	0.00	0.01	0.01	28.62	0.38	0.00	0.00	0.01	0.01
28.63	0.38	0.00	0.00	0.01	0.01	28.64	0.37	0.00	0.00	0.01	0.01
28.65	0.37	0.00	0.00	0.01	0.01	28.66	0.36	0.00	0.00	0.01	0.01
28.67	0.35	0.00	0.00	0.01	0.01	28.68	0.35	0.00	0.00	0.01	0.01
28.69	0.34	0.00	0.00	0.01	0.01	28.70	0.34	0.00	0.00	0.01	0.01
28.71	0.34	0.00	0.00	0.01	0.01	28.72	0.35	0.00	0.00	0.01	0.01
28.73	0.35	0.00	0.00	0.01	0.01	28.74	0.36	0.00	0.00	0.01	0.01
28.75	0.36	0.00	0.00	0.01	0.01	28.76	0.37	0.00	0.00	0.01	0.01
28.77	0.38	0.00	0.00	0.01	0.01	28.78	0.38	0.00	0.00	0.01	0.01
28.79	0.39	0.00	0.00	0.01	0.01	28.80	0.40	0.00	0.00	0.01	0.01

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
28.81	0.41	0.00	0.00	0.01	0.01	28.82	0.43	0.00	0.00	0.01	0.01
28.83	0.44	0.00	0.00	0.01	0.01	28.84	0.46	0.00	0.00	0.01	0.01
28.85	0.48	0.00	0.00	0.01	0.01	28.86	0.49	0.00	0.00	0.01	0.01
28.87	0.51	0.00	0.00	0.01	0.01	28.88	0.52	0.00	0.00	0.01	0.01
28.89	0.53	0.00	0.00	0.01	0.01	28.90	0.54	0.00	0.00	0.01	0.01
28.91	0.55	0.00	0.00	0.01	0.01	28.92	0.56	0.00	0.00	0.01	0.01
28.93	0.57	0.00	0.00	0.01	0.01	28.94	0.58	0.00	0.00	0.01	0.01
28.95	0.60	0.00	0.00	0.01	0.01	28.96	0.61	0.00	0.00	0.01	0.01
28.97	0.62	0.00	0.00	0.01	0.01	28.98	0.63	0.00	0.00	0.01	0.01
28.99	0.65	0.00	0.00	0.01	0.01	29.00	0.67	0.00	0.00	0.01	0.01
29.01	0.69	0.00	0.00	0.01	0.01	29.02	0.71	0.00	0.00	0.01	0.00
29.03	0.73	0.00	0.00	0.01	0.00	29.04	0.75	0.00	0.00	0.01	0.00
29.05	0.76	0.00	0.00	0.01	0.00	29.06	0.78	0.00	0.00	0.01	0.00
29.07	0.80	0.00	0.00	0.01	0.00	29.08	0.82	0.00	0.00	0.01	0.00
29.09	0.85	0.00	0.00	0.01	0.00	29.10	0.87	0.00	0.00	0.01	0.00
29.11	0.90	0.00	0.00	0.01	0.00	29.12	0.92	0.00	0.00	0.01	0.00
29.13	0.94	0.00	0.00	0.01	0.00	29.14	0.95	0.00	0.00	0.01	0.00
29.15	0.96	0.00	0.00	0.01	0.00	29.16	0.97	0.00	0.00	0.01	0.00
29.17	0.98	0.00	0.00	0.01	0.00	29.18	0.99	0.00	0.00	0.01	0.00
29.19	1.01	0.00	0.00	0.01	0.00	29.20	1.02	0.00	0.00	0.01	0.00
29.21	1.03	0.00	0.00	0.01	0.00	29.22	1.04	0.00	0.00	0.01	0.00
29.23	1.04	0.00	0.00	0.01	0.00	29.24	1.04	0.00	0.00	0.01	0.00
29.25	1.03	0.00	0.00	0.01	0.00	29.26	1.03	0.00	0.00	0.01	0.00
29.27	1.02	0.00	0.00	0.01	0.00	29.28	1.02	0.00	0.00	0.01	0.00
29.29	1.01	0.00	0.00	0.01	0.00	29.30	1.01	0.00	0.00	0.01	0.00
29.31	1.01	0.00	0.00	0.01	0.00	29.32	1.01	0.00	0.00	0.01	0.00
29.33	1.01	0.00	0.00	0.01	0.00	29.34	1.02	0.00	0.00	0.01	0.00
29.35	1.02	0.00	0.00	0.01	0.00	29.36	1.02	0.00	0.00	0.01	0.00
29.37	1.03	0.00	0.00	0.01	0.00	29.38	1.03	0.00	0.00	0.01	0.00
29.39	1.03	0.00	0.00	0.01	0.00	29.40	1.04	0.00	0.00	0.01	0.00
29.41	1.06	0.00	0.00	0.01	0.00	29.42	1.08	0.00	0.00	0.01	0.00
29.43	1.10	0.00	0.00	0.01	0.00	29.44	1.12	0.00	0.00	0.01	0.00
29.45	1.15	0.00	0.00	0.01	0.00	29.46	1.17	0.00	0.00	0.01	0.00
29.47	1.19	0.00	0.00	0.01	0.00	29.48	1.21	0.00	0.00	0.01	0.00
29.49	1.23	0.00	0.00	0.01	0.00	29.50	1.25	0.00	0.00	0.01	0.00
29.51	1.27	0.00	0.00	0.01	0.00	29.52	1.29	0.00	0.00	0.01	0.00
29.53	1.31	0.00	0.00	0.01	0.00	29.54	1.34	0.00	0.00	0.01	0.00
29.55	1.36	0.00	0.00	0.01	0.00	29.56	1.38	0.00	0.00	0.01	0.00
29.57	1.39	0.00	0.00	0.01	0.00	29.58	1.40	0.00	0.00	0.01	0.00
29.59	1.41	0.00	0.00	0.01	0.00	29.60	1.42	0.00	0.00	0.01	0.00
29.61	1.42	0.00	0.00	0.01	0.00	29.62	1.43	0.00	0.00	0.01	0.00
29.63	1.44	0.00	0.00	0.01	0.00	29.64	1.45	0.00	0.00	0.01	0.00
29.65	1.45	0.00	0.00	0.01	0.00	29.66	1.45	0.00	0.00	0.01	0.00
29.67	1.44	0.00	0.00	0.01	0.00	29.68	1.43	0.00	0.00	0.01	0.00
29.69	1.42	0.00	0.00	0.01	0.00	29.70	1.41	0.00	0.00	0.01	0.00
29.71	1.40	0.00	0.00	0.01	0.00	29.72	1.38	0.00	0.00	0.01	0.00
29.73	1.37	0.00	0.00	0.01	0.00	29.74	1.36	0.00	0.00	0.01	0.00
29.75	1.35	0.00	0.00	0.01	0.00	29.76	1.33	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
29.77	1.31	0.00	0.00	0.01	0.00	29.78	1.29	0.00	0.00	0.01	0.00
29.79	1.26	0.00	0.00	0.01	0.00	29.80	1.24	0.00	0.00	0.01	0.00
29.81	1.21	0.00	0.00	0.01	0.00	29.82	1.19	0.00	0.00	0.01	0.00
29.83	1.18	0.00	0.00	0.01	0.00	29.84	1.19	0.00	0.00	0.01	0.00
29.85	1.20	0.00	0.00	0.01	0.00	29.86	1.21	0.00	0.00	0.01	0.00
29.87	1.23	0.00	0.00	0.01	0.00	29.88	1.24	0.00	0.00	0.01	0.00
29.89	1.26	0.00	0.00	0.01	0.00	29.90	1.27	0.00	0.00	0.01	0.00
29.91	1.29	0.00	0.00	0.01	0.00	29.92	1.30	0.00	0.00	0.01	0.00
29.93	1.32	0.00	0.00	0.01	0.00	29.94	1.34	0.00	0.00	0.01	0.00
29.95	1.37	0.00	0.00	0.01	0.00	29.96	1.40	0.00	0.00	0.01	0.00
29.97	1.43	0.00	0.00	0.01	0.00	29.98	1.45	0.00	0.00	0.01	0.00
29.99	1.48	0.00	0.00	0.01	0.00	30.00	1.49	0.00	0.00	0.01	0.00
30.01	1.50	0.00	0.00	0.01	0.00	30.02	1.49	0.00	0.00	0.01	0.00
30.03	1.49	0.00	0.00	0.01	0.00	30.04	1.48	0.00	0.00	0.01	0.00
30.05	1.47	0.00	0.00	0.01	0.00	30.06	1.46	0.00	0.00	0.01	0.00
30.07	1.45	0.00	0.00	0.01	0.00	30.08	1.45	0.00	0.00	0.01	0.00
30.09	1.44	0.00	0.00	0.01	0.00	30.10	1.44	0.00	0.00	0.01	0.00
30.11	1.44	0.00	0.00	0.01	0.00	30.12	1.45	0.00	0.00	0.01	0.00
30.13	1.45	0.00	0.00	0.01	0.00	30.14	1.45	0.00	0.00	0.01	0.00
30.15	1.46	0.00	0.00	0.01	0.00	30.16	1.46	0.00	0.00	0.01	0.00
30.17	1.47	0.00	0.00	0.01	0.00	30.18	1.47	0.00	0.00	0.01	0.00
30.19	1.49	0.00	0.00	0.01	0.00	30.20	1.51	0.00	0.00	0.01	0.00
30.21	1.53	0.00	0.00	0.01	0.00	30.22	1.55	0.00	0.00	0.01	0.00
30.23	1.58	0.00	0.00	0.01	0.00	30.24	1.60	0.00	0.00	0.01	0.00
30.25	1.62	0.00	0.00	0.01	0.00	30.26	1.64	0.00	0.00	0.01	0.00
30.27	1.65	0.00	0.00	0.01	0.00	30.28	1.66	0.00	0.00	0.01	0.00
30.29	1.67	0.00	0.00	0.01	0.00	30.30	1.68	0.00	0.00	0.01	0.00
30.31	1.69	0.00	0.00	0.01	0.00	30.32	1.70	0.00	0.00	0.01	0.00
30.33	1.71	0.00	0.00	0.01	0.00	30.34	1.72	0.00	0.00	0.01	0.00
30.35	1.72	0.00	0.00	0.01	0.00	30.36	1.72	0.00	0.00	0.01	0.00
30.37	1.72	0.00	0.00	0.01	0.00	30.38	1.71	0.00	0.00	0.01	0.00
30.39	1.70	0.00	0.00	0.01	0.00	30.40	1.69	0.00	0.00	0.01	0.00
30.41	1.68	0.00	0.00	0.01	0.00	30.42	1.68	0.00	0.00	0.01	0.00
30.43	1.67	0.00	0.00	0.01	0.00	30.44	1.66	0.00	0.00	0.01	0.00
30.45	1.65	0.00	0.00	0.01	0.00	30.46	1.64	0.00	0.00	0.01	0.00
30.47	1.63	0.00	0.00	0.01	0.00	30.48	1.62	0.00	0.00	0.01	0.00
30.49	1.60	0.00	0.00	0.01	0.00	30.50	1.59	0.00	0.00	0.01	0.00
30.51	1.58	0.00	0.00	0.01	0.00	30.52	1.58	0.00	0.00	0.01	0.00
30.53	2.00	0.00	0.00	0.01	0.00	30.54	2.00	0.00	0.00	0.01	0.00
30.55	2.00	0.00	0.00	0.01	0.00	30.56	2.00	0.00	0.00	0.01	0.00
30.57	2.00	0.00	0.00	0.01	0.00	30.58	2.00	0.00	0.00	0.01	0.00
30.59	2.00	0.00	0.00	0.01	0.00	30.60	2.00	0.00	0.00	0.01	0.00
30.61	2.00	0.00	0.00	0.01	0.00	30.62	2.00	0.00	0.00	0.01	0.00
30.63	2.00	0.00	0.00	0.01	0.00	30.64	2.00	0.00	0.00	0.01	0.00
30.65	2.00	0.00	0.00	0.01	0.00	30.66	2.00	0.00	0.00	0.01	0.00
30.67	2.00	0.00	0.00	0.01	0.00	30.68	2.00	0.00	0.00	0.01	0.00
30.69	2.00	0.00	0.00	0.01	0.00	30.70	2.00	0.00	0.00	0.01	0.00
30.71	2.00	0.00	0.00	0.01	0.00	30.72	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
30.73	2.00	0.00	0.00	0.01	0.00	30.74	2.00	0.00	0.00	0.01	0.00
30.75	2.00	0.00	0.00	0.01	0.00	30.76	2.00	0.00	0.00	0.01	0.00
30.77	2.00	0.00	0.00	0.01	0.00	30.78	2.00	0.00	0.00	0.01	0.00
30.79	2.00	0.00	0.00	0.01	0.00	30.80	2.00	0.00	0.00	0.01	0.00
30.81	2.00	0.00	0.00	0.01	0.00	30.82	2.00	0.00	0.00	0.01	0.00
30.83	2.00	0.00	0.00	0.01	0.00	30.84	2.00	0.00	0.00	0.01	0.00
30.85	2.00	0.00	0.00	0.01	0.00	30.86	2.00	0.00	0.00	0.01	0.00
30.87	2.00	0.00	0.00	0.01	0.00	30.88	2.00	0.00	0.00	0.01	0.00
30.89	2.00	0.00	0.00	0.01	0.00	30.90	2.00	0.00	0.00	0.01	0.00
30.91	2.00	0.00	0.00	0.01	0.00	30.92	2.00	0.00	0.00	0.01	0.00
30.93	2.00	0.00	0.00	0.01	0.00	30.94	2.00	0.00	0.00	0.01	0.00
30.95	2.00	0.00	0.00	0.01	0.00	30.96	0.46	0.00	0.00	0.01	0.01
30.97	0.46	0.00	0.00	0.01	0.01	30.98	0.47	0.00	0.00	0.01	0.01
30.99	0.47	0.00	0.00	0.01	0.01	31.00	0.48	0.00	0.00	0.01	0.01
31.01	0.49	0.00	0.00	0.01	0.01	31.02	0.50	0.00	0.00	0.01	0.01
31.03	0.50	0.00	0.00	0.01	0.01	31.04	0.51	0.00	0.00	0.01	0.01
31.05	0.51	0.00	0.00	0.01	0.01	31.06	0.52	0.00	0.00	0.01	0.01
31.07	0.52	0.00	0.00	0.01	0.01	31.08	0.53	0.00	0.00	0.01	0.01
31.09	0.54	0.00	0.00	0.01	0.01	31.10	0.54	0.00	0.00	0.01	0.01
31.11	0.55	0.00	0.00	0.01	0.01	31.12	0.55	0.00	0.00	0.01	0.01
31.13	0.56	0.00	0.00	0.01	0.01	31.14	0.56	0.00	0.00	0.01	0.01
31.15	0.57	0.00	0.00	0.01	0.01	31.16	0.57	0.00	0.00	0.01	0.01
31.17	0.58	0.00	0.00	0.01	0.01	31.18	0.59	0.00	0.00	0.01	0.01
31.19	0.59	0.00	0.00	0.01	0.01	31.20	0.60	0.00	0.00	0.01	0.01
31.21	0.61	0.00	0.00	0.01	0.01	31.22	0.61	0.00	0.00	0.01	0.01
31.23	0.61	0.00	0.00	0.01	0.01	31.24	0.62	0.00	0.00	0.01	0.01
31.25	0.62	0.00	0.00	0.01	0.01	31.26	0.63	0.00	0.00	0.01	0.01
31.27	0.63	0.00	0.00	0.01	0.01	31.28	0.64	0.00	0.00	0.01	0.01
31.29	0.64	0.00	0.00	0.01	0.01	31.30	0.64	0.00	0.00	0.01	0.01
31.31	0.64	0.00	0.00	0.01	0.01	31.32	0.64	0.00	0.00	0.01	0.01
31.33	0.65	0.00	0.00	0.01	0.01	31.34	0.65	0.00	0.00	0.01	0.01
31.35	0.65	0.00	0.00	0.01	0.01	31.36	0.65	0.00	0.00	0.01	0.01
31.37	0.65	0.00	0.00	0.01	0.01	31.38	0.65	0.00	0.00	0.01	0.01
31.39	0.65	0.00	0.00	0.01	0.01	31.40	0.65	0.00	0.00	0.01	0.01
31.41	0.65	0.00	0.00	0.01	0.01	31.42	0.65	0.00	0.00	0.01	0.01
31.43	0.65	0.00	0.00	0.01	0.01	31.44	0.65	0.00	0.00	0.01	0.01
31.45	0.66	0.00	0.00	0.01	0.01	31.46	0.66	0.00	0.00	0.01	0.01
31.47	0.66	0.00	0.00	0.01	0.01	31.48	0.66	0.00	0.00	0.01	0.01
31.49	0.66	0.00	0.00	0.01	0.01	31.50	0.66	0.00	0.00	0.01	0.01
31.51	0.66	0.00	0.00	0.01	0.01	31.52	0.67	0.00	0.00	0.01	0.01
31.53	0.67	0.00	0.00	0.01	0.01	31.54	0.67	0.00	0.00	0.01	0.01
31.55	0.67	0.00	0.00	0.01	0.01	31.56	0.67	0.00	0.00	0.01	0.01
31.57	0.67	0.00	0.00	0.01	0.01	31.58	0.67	0.00	0.00	0.01	0.01
31.59	0.67	0.00	0.00	0.01	0.01	31.60	0.68	0.00	0.00	0.01	0.01
31.61	0.68	0.00	0.00	0.01	0.01	31.62	0.68	0.00	0.00	0.01	0.01
31.63	0.68	0.00	0.00	0.01	0.01	31.64	0.68	0.00	0.00	0.01	0.01
31.65	0.68	0.00	0.00	0.01	0.01	31.66	0.68	0.00	0.00	0.01	0.01
31.67	0.68	0.00	0.00	0.01	0.01	31.68	0.68	0.00	0.00	0.01	0.01

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
31.69	0.68	0.00	0.00	0.01	0.01	31.70	0.68	0.00	0.00	0.01	0.01
31.71	0.68	0.00	0.00	0.01	0.01	31.72	0.68	0.00	0.00	0.01	0.01
31.73	0.68	0.00	0.00	0.01	0.00	31.74	0.68	0.00	0.00	0.01	0.00
31.75	0.68	0.00	0.00	0.01	0.00	31.76	0.68	0.00	0.00	0.01	0.00
31.77	0.68	0.00	0.00	0.01	0.00	31.78	0.69	0.00	0.00	0.01	0.00
31.79	0.69	0.00	0.00	0.01	0.00	31.80	0.69	0.00	0.00	0.01	0.00
31.81	0.69	0.00	0.00	0.01	0.00	31.82	0.69	0.00	0.00	0.01	0.00
31.83	0.69	0.00	0.00	0.01	0.00	31.84	0.69	0.00	0.00	0.01	0.00
31.85	0.69	0.00	0.00	0.01	0.00	31.86	0.70	0.00	0.00	0.01	0.00
31.87	0.70	0.00	0.00	0.01	0.00	31.88	0.70	0.00	0.00	0.01	0.00
31.89	0.70	0.00	0.00	0.01	0.00	31.90	0.71	0.00	0.00	0.01	0.00
31.91	0.71	0.00	0.00	0.01	0.00	31.92	0.71	0.00	0.00	0.01	0.00
31.93	0.71	0.00	0.00	0.01	0.00	31.94	0.71	0.00	0.00	0.01	0.00
31.95	0.71	0.00	0.00	0.01	0.00	31.96	0.71	0.00	0.00	0.01	0.00
31.97	0.71	0.00	0.00	0.01	0.00	31.98	0.71	0.00	0.00	0.01	0.00
31.99	0.71	0.00	0.00	0.01	0.00	32.00	0.71	0.00	0.00	0.01	0.00
32.01	0.71	0.00	0.00	0.01	0.00	32.02	0.71	0.00	0.00	0.01	0.00
32.03	0.71	0.00	0.00	0.01	0.00	32.04	0.72	0.00	0.00	0.01	0.00
32.05	0.72	0.00	0.00	0.01	0.00	32.06	0.72	0.00	0.00	0.01	0.00
32.07	0.72	0.00	0.00	0.01	0.00	32.08	0.72	0.00	0.00	0.01	0.00
32.09	0.72	0.00	0.00	0.01	0.00	32.10	0.72	0.00	0.00	0.01	0.00
32.11	0.72	0.00	0.00	0.01	0.00	32.12	0.72	0.00	0.00	0.01	0.00
32.13	0.72	0.00	0.00	0.01	0.00	32.14	0.72	0.00	0.00	0.01	0.00
32.15	0.73	0.00	0.00	0.01	0.00	32.16	0.73	0.00	0.00	0.01	0.00
32.17	0.73	0.00	0.00	0.01	0.00	32.18	0.73	0.00	0.00	0.01	0.00
32.19	0.73	0.00	0.00	0.01	0.00	32.20	0.73	0.00	0.00	0.01	0.00
32.21	0.73	0.00	0.00	0.01	0.00	32.22	0.73	0.00	0.00	0.01	0.00
32.23	0.73	0.00	0.00	0.01	0.00	32.24	0.73	0.00	0.00	0.01	0.00
32.25	0.74	0.00	0.00	0.01	0.00	32.26	0.74	0.00	0.00	0.01	0.00
32.27	0.74	0.00	0.00	0.01	0.00	32.28	0.74	0.00	0.00	0.01	0.00
32.29	0.74	0.00	0.00	0.01	0.00	32.30	0.74	0.00	0.00	0.01	0.00
32.31	0.74	0.00	0.00	0.01	0.00	32.32	0.74	0.00	0.00	0.01	0.00
32.33	0.74	0.00	0.00	0.01	0.00	32.34	0.74	0.00	0.00	0.01	0.00
32.35	0.74	0.00	0.00	0.01	0.00	32.36	0.75	0.00	0.00	0.01	0.00
32.37	0.75	0.00	0.00	0.01	0.00	32.38	0.75	0.00	0.00	0.01	0.00
32.39	0.75	0.00	0.00	0.01	0.00	32.40	0.75	0.00	0.00	0.01	0.00
32.41	0.75	0.00	0.00	0.01	0.00	32.42	0.76	0.00	0.00	0.01	0.00
32.43	0.76	0.00	0.00	0.01	0.00	32.44	0.76	0.00	0.00	0.01	0.00
32.45	0.76	0.00	0.00	0.01	0.00	32.46	0.76	0.00	0.00	0.01	0.00
32.47	0.76	0.00	0.00	0.01	0.00	32.48	0.76	0.00	0.00	0.01	0.00
32.49	0.77	0.00	0.00	0.01	0.00	32.50	0.77	0.00	0.00	0.01	0.00
32.51	0.77	0.00	0.00	0.01	0.00	32.52	0.77	0.00	0.00	0.01	0.00
32.53	0.77	0.00	0.00	0.01	0.00	32.54	0.78	0.00	0.00	0.01	0.00
32.55	0.78	0.00	0.00	0.01	0.00	32.56	0.78	0.00	0.00	0.01	0.00
32.57	0.78	0.00	0.00	0.01	0.00	32.58	0.79	0.00	0.00	0.01	0.00
32.59	0.79	0.00	0.00	0.01	0.00	32.60	0.79	0.00	0.00	0.01	0.00
32.61	0.80	0.00	0.00	0.01	0.00	32.62	0.81	0.00	0.00	0.01	0.00
32.63	0.82	0.00	0.00	0.01	0.00	32.64	0.84	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
32.65	0.85	0.00	0.00	0.01	0.00	32.66	0.87	0.00	0.00	0.01	0.00
32.67	0.88	0.00	0.00	0.01	0.00	32.68	0.89	0.00	0.00	0.01	0.00
32.69	0.91	0.00	0.00	0.01	0.00	32.70	2.00	0.00	0.00	0.01	0.00
32.71	2.00	0.00	0.00	0.01	0.00	32.72	2.00	0.00	0.00	0.01	0.00
32.73	2.00	0.00	0.00	0.01	0.00	32.74	2.00	0.00	0.00	0.01	0.00
32.75	2.00	0.00	0.00	0.01	0.00	32.76	2.00	0.00	0.00	0.01	0.00
32.77	2.00	0.00	0.00	0.01	0.00	32.78	2.00	0.00	0.00	0.01	0.00
32.79	2.00	0.00	0.00	0.01	0.00	32.80	2.00	0.00	0.00	0.01	0.00
32.81	2.00	0.00	0.00	0.01	0.00	32.82	2.00	0.00	0.00	0.01	0.00
32.83	2.00	0.00	0.00	0.01	0.00	32.84	2.00	0.00	0.00	0.01	0.00
32.85	2.00	0.00	0.00	0.01	0.00	32.86	2.00	0.00	0.00	0.01	0.00
32.87	2.00	0.00	0.00	0.01	0.00	32.88	2.00	0.00	0.00	0.01	0.00
32.89	2.00	0.00	0.00	0.01	0.00	32.90	2.00	0.00	0.00	0.01	0.00
32.91	2.00	0.00	0.00	0.01	0.00	32.92	2.00	0.00	0.00	0.01	0.00
32.93	2.00	0.00	0.00	0.01	0.00	32.94	2.00	0.00	0.00	0.01	0.00
32.95	2.00	0.00	0.00	0.01	0.00	32.96	2.00	0.00	0.00	0.01	0.00
32.97	2.00	0.00	0.00	0.01	0.00	32.98	2.00	0.00	0.00	0.01	0.00
32.99	2.00	0.00	0.00	0.01	0.00	33.00	2.00	0.00	0.00	0.01	0.00
33.01	2.00	0.00	0.00	0.01	0.00	33.02	2.00	0.00	0.00	0.01	0.00
33.03	2.00	0.00	0.00	0.01	0.00	33.04	2.00	0.00	0.00	0.01	0.00
33.05	2.00	0.00	0.00	0.01	0.00	33.06	2.00	0.00	0.00	0.01	0.00
33.07	2.00	0.00	0.00	0.01	0.00	33.08	2.00	0.00	0.00	0.01	0.00
33.09	2.00	0.00	0.00	0.01	0.00	33.10	2.00	0.00	0.00	0.01	0.00
33.11	2.00	0.00	0.00	0.01	0.00	33.12	2.00	0.00	0.00	0.01	0.00
33.13	2.00	0.00	0.00	0.01	0.00	33.14	2.00	0.00	0.00	0.01	0.00
33.15	2.00	0.00	0.00	0.01	0.00	33.16	2.00	0.00	0.00	0.01	0.00
33.17	2.00	0.00	0.00	0.01	0.00	33.18	2.00	0.00	0.00	0.01	0.00
33.19	2.00	0.00	0.00	0.01	0.00	33.20	2.00	0.00	0.00	0.01	0.00
33.21	2.00	0.00	0.00	0.01	0.00	33.22	2.00	0.00	0.00	0.01	0.00
33.23	2.00	0.00	0.00	0.01	0.00	33.24	2.00	0.00	0.00	0.01	0.00
33.25	2.00	0.00	0.00	0.01	0.00	33.26	2.00	0.00	0.00	0.01	0.00
33.27	2.00	0.00	0.00	0.01	0.00	33.28	2.00	0.00	0.00	0.01	0.00
33.29	2.00	0.00	0.00	0.01	0.00	33.30	2.00	0.00	0.00	0.01	0.00
33.31	2.00	0.00	0.00	0.01	0.00	33.32	2.00	0.00	0.00	0.01	0.00
33.33	2.00	0.00	0.00	0.01	0.00	33.34	2.00	0.00	0.00	0.01	0.00
33.35	2.00	0.00	0.00	0.01	0.00	33.36	2.00	0.00	0.00	0.01	0.00
33.37	2.00	0.00	0.00	0.01	0.00	33.38	2.00	0.00	0.00	0.01	0.00
33.39	2.00	0.00	0.00	0.01	0.00	33.40	2.00	0.00	0.00	0.01	0.00
33.41	2.00	0.00	0.00	0.01	0.00	33.42	2.00	0.00	0.00	0.01	0.00
33.43	2.00	0.00	0.00	0.01	0.00	33.44	2.00	0.00	0.00	0.01	0.00
33.45	2.00	0.00	0.00	0.01	0.00	33.46	2.00	0.00	0.00	0.01	0.00
33.47	2.00	0.00	0.00	0.01	0.00	33.48	2.00	0.00	0.00	0.01	0.00
33.49	2.00	0.00	0.00	0.01	0.00	33.50	2.00	0.00	0.00	0.01	0.00
33.51	2.00	0.00	0.00	0.01	0.00	33.52	2.00	0.00	0.00	0.01	0.00
33.53	2.00	0.00	0.00	0.01	0.00	33.54	2.00	0.00	0.00	0.01	0.00
33.55	2.00	0.00	0.00	0.01	0.00	33.56	2.00	0.00	0.00	0.01	0.00
33.57	2.00	0.00	0.00	0.01	0.00	33.58	2.00	0.00	0.00	0.01	0.00
33.59	2.00	0.00	0.00	0.01	0.00	33.60	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
33.61	2.00	0.00	0.00	0.01	0.00	33.62	2.00	0.00	0.00	0.01	0.00
33.63	2.00	0.00	0.00	0.01	0.00	33.64	2.00	0.00	0.00	0.01	0.00
33.65	2.00	0.00	0.00	0.01	0.00	33.66	2.00	0.00	0.00	0.01	0.00
33.67	2.00	0.00	0.00	0.01	0.00	33.68	2.00	0.00	0.00	0.01	0.00
33.69	2.00	0.00	0.00	0.01	0.00	33.70	2.00	0.00	0.00	0.01	0.00
33.71	2.00	0.00	0.00	0.01	0.00	33.72	2.00	0.00	0.00	0.01	0.00
33.73	2.00	0.00	0.00	0.01	0.00	33.74	2.00	0.00	0.00	0.01	0.00
33.75	0.91	0.00	0.00	0.01	0.00	33.76	0.90	0.00	0.00	0.01	0.00
33.77	0.89	0.00	0.00	0.01	0.00	33.78	0.88	0.00	0.00	0.01	0.00
33.79	0.88	0.00	0.00	0.01	0.00	33.80	0.87	0.00	0.00	0.01	0.00
33.81	0.87	0.00	0.00	0.01	0.00	33.82	0.86	0.00	0.00	0.01	0.00
33.83	0.86	0.00	0.00	0.01	0.00	33.84	0.85	0.00	0.00	0.01	0.00
33.85	0.85	0.00	0.00	0.01	0.00	33.86	0.84	0.00	0.00	0.01	0.00
33.87	0.84	0.00	0.00	0.01	0.00	33.88	0.83	0.00	0.00	0.01	0.00
33.89	0.83	0.00	0.00	0.01	0.00	33.90	0.83	0.00	0.00	0.01	0.00
33.91	0.82	0.00	0.00	0.01	0.00	33.92	0.83	0.00	0.00	0.01	0.00
33.93	0.83	0.00	0.00	0.01	0.00	33.94	0.83	0.00	0.00	0.01	0.00
33.95	0.83	0.00	0.00	0.01	0.00	33.96	0.84	0.00	0.00	0.01	0.00
33.97	0.84	0.00	0.00	0.01	0.00	33.98	0.84	0.00	0.00	0.01	0.00
33.99	0.84	0.00	0.00	0.01	0.00	34.00	0.84	0.00	0.00	0.01	0.00
34.01	0.85	0.00	0.00	0.01	0.00	34.02	0.85	0.00	0.00	0.01	0.00
34.03	0.85	0.00	0.00	0.01	0.00	34.04	0.85	0.00	0.00	0.01	0.00
34.05	0.86	0.00	0.00	0.01	0.00	34.06	0.86	0.00	0.00	0.01	0.00
34.07	0.86	0.00	0.00	0.01	0.00	34.08	0.86	0.00	0.00	0.01	0.00
34.09	0.86	0.00	0.00	0.01	0.00	34.10	0.86	0.00	0.00	0.01	0.00
34.11	0.85	0.00	0.00	0.01	0.00	34.12	0.85	0.00	0.00	0.01	0.00
34.13	0.85	0.00	0.00	0.01	0.00	34.14	0.85	0.00	0.00	0.01	0.00
34.15	0.85	0.00	0.00	0.01	0.00	34.16	0.85	0.00	0.00	0.01	0.00
34.17	0.85	0.00	0.00	0.01	0.00	34.18	0.85	0.00	0.00	0.01	0.00
34.19	0.85	0.00	0.00	0.01	0.00	34.20	0.86	0.00	0.00	0.01	0.00
34.21	0.86	0.00	0.00	0.01	0.00	34.22	0.86	0.00	0.00	0.01	0.00
34.23	0.86	0.00	0.00	0.01	0.00	34.24	0.87	0.00	0.00	0.01	0.00
34.25	0.87	0.00	0.00	0.01	0.00	34.26	0.87	0.00	0.00	0.01	0.00
34.27	0.88	0.00	0.00	0.01	0.00	34.28	0.89	0.00	0.00	0.01	0.00
34.29	0.89	0.00	0.00	0.01	0.00	34.30	0.90	0.00	0.00	0.01	0.00
34.31	0.90	0.00	0.00	0.01	0.00	34.32	0.91	0.00	0.00	0.01	0.00
34.33	2.00	0.00	0.00	0.01	0.00	34.34	2.00	0.00	0.00	0.01	0.00
34.35	2.00	0.00	0.00	0.01	0.00	34.36	2.00	0.00	0.00	0.01	0.00
34.37	2.00	0.00	0.00	0.01	0.00	34.38	2.00	0.00	0.00	0.01	0.00
34.39	2.00	0.00	0.00	0.01	0.00	34.40	2.00	0.00	0.00	0.01	0.00
34.41	2.00	0.00	0.00	0.01	0.00	34.42	2.00	0.00	0.00	0.01	0.00
34.43	2.00	0.00	0.00	0.01	0.00	34.44	2.00	0.00	0.00	0.01	0.00
34.45	2.00	0.00	0.00	0.01	0.00	34.46	2.00	0.00	0.00	0.01	0.00
34.47	2.00	0.00	0.00	0.01	0.00	34.48	2.00	0.00	0.00	0.01	0.00
34.49	2.00	0.00	0.00	0.01	0.00	34.50	2.00	0.00	0.00	0.01	0.00
34.51	2.00	0.00	0.00	0.01	0.00	34.52	2.00	0.00	0.00	0.01	0.00
34.53	2.00	0.00	0.00	0.01	0.00	34.54	2.00	0.00	0.00	0.01	0.00
34.55	2.00	0.00	0.00	0.01	0.00	34.56	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
34.57	2.00	0.00	0.00	0.01	0.00	34.58	2.00	0.00	0.00	0.01	0.00
34.59	2.00	0.00	0.00	0.01	0.00	34.60	2.00	0.00	0.00	0.01	0.00
34.61	2.00	0.00	0.00	0.01	0.00	34.62	2.00	0.00	0.00	0.01	0.00
34.63	2.00	0.00	0.00	0.01	0.00	34.64	2.00	0.00	0.00	0.01	0.00
34.65	2.00	0.00	0.00	0.01	0.00	34.66	2.00	0.00	0.00	0.01	0.00
34.67	2.00	0.00	0.00	0.01	0.00	34.68	2.00	0.00	0.00	0.01	0.00
34.69	2.00	0.00	0.00	0.01	0.00	34.70	2.00	0.00	0.00	0.01	0.00
34.71	2.00	0.00	0.00	0.01	0.00	34.72	2.00	0.00	0.00	0.01	0.00
34.73	2.00	0.00	0.00	0.01	0.00	34.74	2.00	0.00	0.00	0.01	0.00
34.75	2.00	0.00	0.00	0.01	0.00	34.76	2.00	0.00	0.00	0.01	0.00
34.77	2.00	0.00	0.00	0.01	0.00	34.78	2.00	0.00	0.00	0.01	0.00
34.79	2.00	0.00	0.00	0.01	0.00	34.80	2.00	0.00	0.00	0.01	0.00
34.81	2.00	0.00	0.00	0.01	0.00	34.82	2.00	0.00	0.00	0.01	0.00
34.83	2.00	0.00	0.00	0.01	0.00	34.84	2.00	0.00	0.00	0.01	0.00
34.85	2.00	0.00	0.00	0.01	0.00	34.86	2.00	0.00	0.00	0.01	0.00
34.87	2.00	0.00	0.00	0.01	0.00	34.88	2.00	0.00	0.00	0.01	0.00
34.89	2.00	0.00	0.00	0.01	0.00	34.90	2.00	0.00	0.00	0.01	0.00
34.91	2.00	0.00	0.00	0.01	0.00	34.92	2.00	0.00	0.00	0.01	0.00
34.93	2.00	0.00	0.00	0.01	0.00	34.94	2.00	0.00	0.00	0.01	0.00
34.95	2.00	0.00	0.00	0.01	0.00	34.96	2.00	0.00	0.00	0.01	0.00
34.97	2.00	0.00	0.00	0.01	0.00	34.98	2.00	0.00	0.00	0.01	0.00
34.99	2.00	0.00	0.00	0.01	0.00	35.00	2.00	0.00	0.00	0.01	0.00
35.01	2.00	0.00	0.00	0.01	0.00	35.02	2.00	0.00	0.00	0.01	0.00
35.03	2.00	0.00	0.00	0.01	0.00	35.04	2.00	0.00	0.00	0.01	0.00
35.05	0.91	0.00	0.00	0.01	0.00	35.06	0.89	0.00	0.00	0.01	0.00
35.07	0.88	0.00	0.00	0.01	0.00	35.08	0.87	0.00	0.00	0.01	0.00
35.09	0.85	0.00	0.00	0.01	0.00	35.10	0.84	0.00	0.00	0.01	0.00
35.11	0.83	0.00	0.00	0.01	0.00	35.12	0.82	0.00	0.00	0.01	0.00
35.13	0.81	0.00	0.00	0.01	0.00	35.14	0.79	0.00	0.00	0.01	0.00
35.15	0.78	0.00	0.00	0.01	0.00	35.16	0.76	0.00	0.00	0.01	0.00
35.17	0.75	0.00	0.00	0.01	0.00	35.18	0.73	0.00	0.00	0.01	0.00
35.19	0.72	0.00	0.00	0.01	0.00	35.20	0.71	0.00	0.00	0.01	0.00
35.21	0.70	0.00	0.00	0.01	0.00	35.22	0.68	0.00	0.00	0.01	0.00
35.23	0.67	0.00	0.00	0.01	0.00	35.24	0.65	0.00	0.00	0.01	0.00
35.25	0.63	0.00	0.00	0.01	0.01	35.26	0.62	0.00	0.00	0.01	0.01
35.27	0.60	0.00	0.00	0.01	0.01	35.28	0.59	0.00	0.00	0.01	0.01
35.29	0.58	0.00	0.00	0.01	0.01	35.30	0.57	0.00	0.00	0.01	0.01
35.31	0.56	0.00	0.00	0.01	0.01	35.32	0.54	0.00	0.00	0.01	0.01
35.33	0.53	0.00	0.00	0.01	0.01	35.34	0.52	0.00	0.00	0.01	0.01
35.35	0.50	0.00	0.00	0.01	0.01	35.36	0.49	0.00	0.00	0.01	0.01
35.37	0.48	0.00	0.00	0.01	0.01	35.38	0.47	0.00	0.00	0.01	0.01
35.39	0.47	0.00	0.00	0.01	0.01	35.40	0.45	0.00	0.00	0.01	0.01
35.41	0.44	0.00	0.00	0.01	0.01	35.42	0.43	0.00	0.00	0.01	0.01
35.43	0.42	0.00	0.00	0.01	0.01	35.44	0.41	0.00	0.00	0.01	0.01
35.45	0.40	0.00	0.00	0.01	0.01	35.46	0.40	0.00	0.00	0.01	0.01
35.47	0.39	0.00	0.00	0.01	0.01	35.48	0.39	0.00	0.00	0.01	0.01
35.49	0.38	0.00	0.00	0.01	0.01	35.50	0.37	0.00	0.00	0.01	0.01
35.51	0.36	0.00	0.00	0.01	0.01	35.52	0.36	0.00	0.00	0.01	0.01

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
35.53	0.35	0.00	0.00	0.01	0.01	35.54	0.35	0.00	0.00	0.01	0.01
35.55	0.34	0.00	0.00	0.01	0.01	35.56	0.34	0.00	0.00	0.01	0.01
35.57	0.34	0.00	0.00	0.01	0.01	35.58	0.34	0.00	0.00	0.01	0.01
35.59	0.33	0.00	0.00	0.01	0.01	35.60	0.33	0.00	0.00	0.01	0.01
35.61	0.33	0.00	0.00	0.01	0.01	35.62	0.33	0.00	0.00	0.01	0.01
35.63	0.33	0.00	0.00	0.01	0.01	35.64	0.33	0.00	0.00	0.01	0.01
35.65	0.33	0.00	0.00	0.01	0.01	35.66	0.33	0.00	0.00	0.01	0.01
35.67	0.32	0.00	0.00	0.01	0.01	35.68	0.32	0.00	0.00	0.01	0.01
35.69	0.32	0.00	0.00	0.01	0.01	35.70	0.32	0.00	0.00	0.01	0.01
35.71	0.32	0.00	0.00	0.01	0.01	35.72	0.32	0.00	0.00	0.01	0.01
35.73	0.32	0.00	0.00	0.01	0.01	35.74	0.32	0.00	0.00	0.01	0.01
35.75	0.33	0.00	0.00	0.01	0.01	35.76	0.33	0.00	0.00	0.01	0.01
35.77	0.33	0.00	0.00	0.01	0.01	35.78	0.33	0.00	0.00	0.01	0.01
35.79	0.33	0.00	0.00	0.01	0.01	35.80	0.33	0.00	0.00	0.01	0.01
35.81	0.33	0.00	0.00	0.01	0.01	35.82	0.33	0.00	0.00	0.01	0.01
35.83	0.33	0.00	0.00	0.01	0.01	35.84	0.33	0.00	0.00	0.01	0.01
35.85	0.33	0.00	0.00	0.01	0.01	35.86	0.33	0.00	0.00	0.01	0.01
35.87	0.33	0.00	0.00	0.01	0.01	35.88	0.33	0.00	0.00	0.01	0.01
35.89	0.33	0.00	0.00	0.01	0.01	35.90	0.34	0.00	0.00	0.01	0.01
35.91	0.34	0.00	0.00	0.01	0.01	35.92	0.34	0.00	0.00	0.01	0.01
35.93	0.34	0.00	0.00	0.01	0.01	35.94	0.34	0.00	0.00	0.01	0.01
35.95	0.34	0.00	0.00	0.01	0.01	35.96	0.34	0.00	0.00	0.01	0.01
35.97	0.34	0.00	0.00	0.01	0.01	35.98	0.34	0.00	0.00	0.01	0.01
35.99	0.34	0.00	0.00	0.01	0.01	36.00	0.34	0.00	0.00	0.01	0.01
36.01	0.34	0.00	0.00	0.01	0.01	36.02	0.33	0.00	0.00	0.01	0.01
36.03	0.33	0.00	0.00	0.01	0.01	36.04	0.33	0.00	0.00	0.01	0.01
36.05	0.33	0.00	0.00	0.01	0.01	36.06	0.33	0.00	0.00	0.01	0.01
36.07	0.33	0.00	0.00	0.01	0.01	36.08	0.33	0.00	0.00	0.01	0.01
36.09	0.33	0.00	0.00	0.01	0.01	36.10	0.33	0.00	0.00	0.01	0.01
36.11	0.33	0.00	0.00	0.01	0.01	36.12	0.32	0.00	0.00	0.01	0.01
36.13	0.32	0.00	0.00	0.01	0.01	36.14	0.32	0.00	0.00	0.01	0.01
36.15	0.32	0.00	0.00	0.01	0.01	36.16	0.32	0.00	0.00	0.01	0.01
36.17	0.32	0.00	0.00	0.01	0.01	36.18	0.32	0.00	0.00	0.01	0.01
36.19	0.32	0.00	0.00	0.01	0.01	36.20	0.32	0.00	0.00	0.01	0.01
36.21	0.32	0.00	0.00	0.01	0.01	36.22	0.32	0.00	0.00	0.01	0.01
36.23	0.32	0.00	0.00	0.01	0.01	36.24	0.32	0.00	0.00	0.01	0.01
36.25	0.32	0.00	0.00	0.01	0.01	36.26	0.32	0.00	0.00	0.01	0.01
36.27	0.32	0.00	0.00	0.01	0.01	36.28	0.32	0.00	0.00	0.01	0.01
36.29	0.32	0.00	0.00	0.01	0.01	36.30	0.32	0.00	0.00	0.01	0.01
36.31	0.33	0.00	0.00	0.01	0.01	36.32	0.33	0.00	0.00	0.01	0.01
36.33	0.33	0.00	0.00	0.01	0.01	36.34	0.33	0.00	0.00	0.01	0.01
36.35	0.33	0.00	0.00	0.01	0.01	36.36	0.34	0.00	0.00	0.01	0.01
36.37	0.34	0.00	0.00	0.01	0.01	36.38	0.34	0.00	0.00	0.01	0.01
36.39	0.35	0.00	0.00	0.01	0.01	36.40	0.35	0.00	0.00	0.01	0.01
36.41	0.35	0.00	0.00	0.01	0.01	36.42	0.35	0.00	0.00	0.01	0.01
36.43	0.36	0.00	0.00	0.01	0.01	36.44	0.36	0.00	0.00	0.01	0.01
36.45	0.36	0.00	0.00	0.01	0.01	36.46	0.37	0.00	0.00	0.01	0.01
36.47	0.37	0.00	0.00	0.01	0.01	36.48	0.37	0.00	0.00	0.01	0.01

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
36.49	0.38	0.00	0.00	0.01	0.01	36.50	0.38	0.00	0.00	0.01	0.01
36.51	0.38	0.00	0.00	0.01	0.01	36.52	0.38	0.00	0.00	0.01	0.01
36.53	0.38	0.00	0.00	0.01	0.01	36.54	0.39	0.00	0.00	0.01	0.01
36.55	0.39	0.00	0.00	0.01	0.01	36.56	0.39	0.00	0.00	0.01	0.01
36.57	0.39	0.00	0.00	0.01	0.01	36.58	0.40	0.00	0.00	0.01	0.01
36.59	0.40	0.00	0.00	0.01	0.01	36.60	0.40	0.00	0.00	0.01	0.01
36.61	0.40	0.00	0.00	0.01	0.01	36.62	0.40	0.00	0.00	0.01	0.01
36.63	0.40	0.00	0.00	0.01	0.01	36.64	0.40	0.00	0.00	0.01	0.01
36.65	0.40	0.00	0.00	0.01	0.01	36.66	0.41	0.00	0.00	0.01	0.01
36.67	0.41	0.00	0.00	0.01	0.01	36.68	0.41	0.00	0.00	0.01	0.01
36.69	0.41	0.00	0.00	0.01	0.01	36.70	0.41	0.00	0.00	0.01	0.01
36.71	0.41	0.00	0.00	0.01	0.01	36.72	0.41	0.00	0.00	0.01	0.01
36.73	0.41	0.00	0.00	0.01	0.01	36.74	0.41	0.00	0.00	0.01	0.01
36.75	0.41	0.00	0.00	0.01	0.01	36.76	0.41	0.00	0.00	0.01	0.01
36.77	0.41	0.00	0.00	0.01	0.01	36.78	0.41	0.00	0.00	0.01	0.01
36.79	0.41	0.00	0.00	0.01	0.01	36.80	0.41	0.00	0.00	0.01	0.01
36.81	0.41	0.00	0.00	0.01	0.01	36.82	0.42	0.00	0.00	0.01	0.01
36.83	0.42	0.00	0.00	0.01	0.01	36.84	0.42	0.00	0.00	0.01	0.01
36.85	0.42	0.00	0.00	0.01	0.01	36.86	0.42	0.00	0.00	0.01	0.01
36.87	0.42	0.00	0.00	0.01	0.01	36.88	0.42	0.00	0.00	0.01	0.01
36.89	0.42	0.00	0.00	0.01	0.01	36.90	0.43	0.00	0.00	0.01	0.01
36.91	0.43	0.00	0.00	0.01	0.01	36.92	0.43	0.00	0.00	0.01	0.01
36.93	0.43	0.00	0.00	0.01	0.01	36.94	0.43	0.00	0.00	0.01	0.01
36.95	0.43	0.00	0.00	0.01	0.01	36.96	0.43	0.00	0.00	0.01	0.01
36.97	0.43	0.00	0.00	0.01	0.01	36.98	0.43	0.00	0.00	0.01	0.01
36.99	0.43	0.00	0.00	0.01	0.01	37.00	0.43	0.00	0.00	0.01	0.01
37.01	0.43	0.00	0.00	0.01	0.01	37.02	0.43	0.00	0.00	0.01	0.01
37.03	0.43	0.00	0.00	0.01	0.01	37.04	0.43	0.00	0.00	0.01	0.01
37.05	0.42	0.00	0.00	0.01	0.01	37.06	0.42	0.00	0.00	0.01	0.01
37.07	0.42	0.00	0.00	0.01	0.01	37.08	0.42	0.00	0.00	0.01	0.01
37.09	0.42	0.00	0.00	0.01	0.01	37.10	0.41	0.00	0.00	0.01	0.01
37.11	0.41	0.00	0.00	0.01	0.01	37.12	0.41	0.00	0.00	0.01	0.01
37.13	0.41	0.00	0.00	0.01	0.01	37.14	0.40	0.00	0.00	0.01	0.01
37.15	0.40	0.00	0.00	0.01	0.01	37.16	0.40	0.00	0.00	0.01	0.01
37.17	0.39	0.00	0.00	0.01	0.01	37.18	0.39	0.00	0.00	0.01	0.01
37.19	0.39	0.00	0.00	0.01	0.01	37.20	0.39	0.00	0.00	0.01	0.01
37.21	0.39	0.00	0.00	0.01	0.01	37.22	0.39	0.00	0.00	0.01	0.01
37.23	0.39	0.00	0.00	0.01	0.01	37.24	0.39	0.00	0.00	0.01	0.01
37.25	0.39	0.00	0.00	0.01	0.01	37.26	0.39	0.00	0.00	0.01	0.01
37.27	0.39	0.00	0.00	0.01	0.01	37.28	0.39	0.00	0.00	0.01	0.01
37.29	0.38	0.00	0.00	0.01	0.01	37.30	0.38	0.00	0.00	0.01	0.01
37.31	0.38	0.00	0.00	0.01	0.01	37.32	0.37	0.00	0.00	0.01	0.01
37.33	0.37	0.00	0.00	0.01	0.01	37.34	0.37	0.00	0.00	0.01	0.01
37.35	0.36	0.00	0.00	0.01	0.01	37.36	0.36	0.00	0.00	0.01	0.01
37.37	0.36	0.00	0.00	0.01	0.01	37.38	0.35	0.00	0.00	0.01	0.01
37.39	0.35	0.00	0.00	0.01	0.01	37.40	0.34	0.00	0.00	0.01	0.01
37.41	0.34	0.00	0.00	0.01	0.01	37.42	0.33	0.00	0.00	0.01	0.01
37.43	0.33	0.00	0.00	0.01	0.01	37.44	0.33	0.00	0.00	0.01	0.01

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
37.45	0.32	0.00	0.00	0.01	0.01	37.46	0.33	0.00	0.00	0.01	0.01
37.47	0.33	0.00	0.00	0.01	0.01	37.48	0.33	0.00	0.00	0.01	0.01
37.49	0.34	0.00	0.00	0.01	0.01	37.50	0.34	0.00	0.00	0.01	0.01
37.51	0.35	0.00	0.00	0.01	0.01	37.52	0.35	0.00	0.00	0.01	0.01
37.53	0.36	0.00	0.00	0.01	0.01	37.54	0.36	0.00	0.00	0.01	0.01
37.55	0.36	0.00	0.00	0.01	0.01	37.56	0.37	0.00	0.00	0.01	0.01
37.57	0.37	0.00	0.00	0.01	0.01	37.58	0.37	0.00	0.00	0.01	0.01
37.59	0.38	0.00	0.00	0.01	0.01	37.60	0.38	0.00	0.00	0.01	0.01
37.61	0.38	0.00	0.00	0.01	0.01	37.62	0.39	0.00	0.00	0.01	0.01
37.63	0.39	0.00	0.00	0.01	0.01	37.64	0.39	0.00	0.00	0.01	0.01
37.65	0.39	0.00	0.00	0.01	0.01	37.66	0.40	0.00	0.00	0.01	0.01
37.67	0.40	0.00	0.00	0.01	0.01	37.68	0.41	0.00	0.00	0.01	0.01
37.69	0.41	0.00	0.00	0.01	0.01	37.70	0.41	0.00	0.00	0.01	0.01
37.71	2.00	0.00	0.00	0.01	0.00	37.72	2.00	0.00	0.00	0.01	0.00
37.73	2.00	0.00	0.00	0.01	0.00	37.74	2.00	0.00	0.00	0.01	0.00
37.75	2.00	0.00	0.00	0.01	0.00	37.76	2.00	0.00	0.00	0.01	0.00
37.77	2.00	0.00	0.00	0.01	0.00	37.78	2.00	0.00	0.00	0.01	0.00
37.79	2.00	0.00	0.00	0.01	0.00	37.80	2.00	0.00	0.00	0.01	0.00
37.81	2.00	0.00	0.00	0.01	0.00	37.82	2.00	0.00	0.00	0.01	0.00
37.83	2.00	0.00	0.00	0.01	0.00	37.84	2.00	0.00	0.00	0.01	0.00
37.85	2.00	0.00	0.00	0.01	0.00	37.86	2.00	0.00	0.00	0.01	0.00
37.87	2.00	0.00	0.00	0.01	0.00	37.88	2.00	0.00	0.00	0.01	0.00
37.89	2.00	0.00	0.00	0.01	0.00	37.90	2.00	0.00	0.00	0.01	0.00
37.91	2.00	0.00	0.00	0.01	0.00	37.92	2.00	0.00	0.00	0.01	0.00
37.93	2.00	0.00	0.00	0.01	0.00	37.94	2.00	0.00	0.00	0.01	0.00
37.95	2.00	0.00	0.00	0.01	0.00	37.96	2.00	0.00	0.00	0.01	0.00
37.97	2.00	0.00	0.00	0.01	0.00	37.98	2.00	0.00	0.00	0.01	0.00
37.99	2.00	0.00	0.00	0.01	0.00	38.00	2.00	0.00	0.00	0.01	0.00
38.01	2.00	0.00	0.00	0.01	0.00	38.02	2.00	0.00	0.00	0.01	0.00
38.03	2.00	0.00	0.00	0.01	0.00	38.04	2.00	0.00	0.00	0.01	0.00
38.05	2.00	0.00	0.00	0.01	0.00	38.06	2.00	0.00	0.00	0.01	0.00
38.07	0.84	0.00	0.00	0.01	0.00	38.08	0.84	0.00	0.00	0.01	0.00
38.09	0.85	0.00	0.00	0.01	0.00	38.10	0.86	0.00	0.00	0.01	0.00
38.11	0.86	0.00	0.00	0.01	0.00	38.12	0.87	0.00	0.00	0.01	0.00
38.13	0.88	0.00	0.00	0.01	0.00	38.14	0.75	0.00	0.00	0.01	0.00
38.15	2.00	0.00	0.00	0.01	0.00	38.16	2.00	0.00	0.00	0.01	0.00
38.17	2.00	0.00	0.00	0.01	0.00	38.18	2.00	0.00	0.00	0.01	0.00
38.19	2.00	0.00	0.00	0.01	0.00	38.20	2.00	0.00	0.00	0.01	0.00
38.21	2.00	0.00	0.00	0.01	0.00	38.22	2.00	0.00	0.00	0.01	0.00
38.23	2.00	0.00	0.00	0.01	0.00	38.24	2.00	0.00	0.00	0.01	0.00
38.25	2.00	0.00	0.00	0.01	0.00	38.26	2.00	0.00	0.00	0.01	0.00
38.27	2.00	0.00	0.00	0.01	0.00	38.28	2.00	0.00	0.00	0.01	0.00
38.29	2.00	0.00	0.00	0.01	0.00	38.30	2.00	0.00	0.00	0.01	0.00
38.31	2.00	0.00	0.00	0.01	0.00	38.32	2.00	0.00	0.00	0.01	0.00
38.33	2.00	0.00	0.00	0.01	0.00	38.34	2.00	0.00	0.00	0.01	0.00
38.35	2.00	0.00	0.00	0.01	0.00	38.36	2.00	0.00	0.00	0.01	0.00
38.37	2.00	0.00	0.00	0.01	0.00	38.38	2.00	0.00	0.00	0.01	0.00
38.39	2.00	0.00	0.00	0.01	0.00	38.40	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
38.41	2.00	0.00	0.00	0.01	0.00	38.42	2.00	0.00	0.00	0.01	0.00
38.43	2.00	0.00	0.00	0.01	0.00	38.44	2.00	0.00	0.00	0.01	0.00
38.45	2.00	0.00	0.00	0.01	0.00	38.46	2.00	0.00	0.00	0.01	0.00
38.47	2.00	0.00	0.00	0.01	0.00	38.48	0.76	0.00	0.00	0.01	0.00
38.49	0.77	0.00	0.00	0.01	0.00	38.50	0.78	0.00	0.00	0.01	0.00
38.51	0.80	0.00	0.00	0.01	0.00	38.52	0.83	0.00	0.00	0.01	0.00
38.53	0.85	0.00	0.00	0.01	0.00	38.54	0.88	0.00	0.00	0.01	0.00
38.55	0.91	0.00	0.00	0.01	0.00	38.56	0.93	0.00	0.00	0.01	0.00
38.57	2.00	0.00	0.00	0.01	0.00	38.58	2.00	0.00	0.00	0.01	0.00
38.59	2.00	0.00	0.00	0.01	0.00	38.60	2.00	0.00	0.00	0.01	0.00
38.61	2.00	0.00	0.00	0.01	0.00	38.62	2.00	0.00	0.00	0.01	0.00
38.63	2.00	0.00	0.00	0.01	0.00	38.64	2.00	0.00	0.00	0.01	0.00
38.65	2.00	0.00	0.00	0.01	0.00	38.66	2.00	0.00	0.00	0.01	0.00
38.67	2.00	0.00	0.00	0.01	0.00	38.68	2.00	0.00	0.00	0.01	0.00
38.69	2.00	0.00	0.00	0.01	0.00	38.70	2.00	0.00	0.00	0.01	0.00
38.71	2.00	0.00	0.00	0.01	0.00	38.72	2.00	0.00	0.00	0.01	0.00
38.73	2.00	0.00	0.00	0.01	0.00	38.74	2.00	0.00	0.00	0.01	0.00
38.75	2.00	0.00	0.00	0.01	0.00	38.76	2.00	0.00	0.00	0.01	0.00
38.77	2.00	0.00	0.00	0.01	0.00	38.78	2.00	0.00	0.00	0.01	0.00
38.79	2.00	0.00	0.00	0.01	0.00	38.80	2.00	0.00	0.00	0.01	0.00
38.81	2.00	0.00	0.00	0.01	0.00	38.82	2.00	0.00	0.00	0.01	0.00
38.83	2.00	0.00	0.00	0.01	0.00	38.84	2.00	0.00	0.00	0.01	0.00
38.85	2.00	0.00	0.00	0.01	0.00	38.86	2.00	0.00	0.00	0.01	0.00
38.87	2.00	0.00	0.00	0.01	0.00	38.88	2.00	0.00	0.00	0.01	0.00
38.89	2.00	0.00	0.00	0.01	0.00	38.90	2.00	0.00	0.00	0.01	0.00
38.91	2.00	0.00	0.00	0.01	0.00	38.92	2.00	0.00	0.00	0.01	0.00
38.93	2.00	0.00	0.00	0.01	0.00	38.94	2.00	0.00	0.00	0.01	0.00
38.95	2.00	0.00	0.00	0.01	0.00	38.96	2.00	0.00	0.00	0.01	0.00
38.97	2.00	0.00	0.00	0.01	0.00	38.98	2.00	0.00	0.00	0.01	0.00
38.99	2.00	0.00	0.00	0.01	0.00	39.00	2.00	0.00	0.00	0.01	0.00
39.01	2.00	0.00	0.00	0.01	0.00	39.02	2.00	0.00	0.00	0.01	0.00
39.03	2.00	0.00	0.00	0.01	0.00	39.04	2.00	0.00	0.00	0.01	0.00
39.05	2.00	0.00	0.00	0.01	0.00	39.06	2.00	0.00	0.00	0.01	0.00
39.07	0.93	0.00	0.00	0.01	0.00	39.08	0.91	0.00	0.00	0.01	0.00
39.09	0.89	0.00	0.00	0.01	0.00	39.10	0.87	0.00	0.00	0.01	0.00
39.11	0.87	0.00	0.00	0.01	0.00	39.12	0.86	0.00	0.00	0.01	0.00
39.13	0.85	0.00	0.00	0.01	0.00	39.14	0.84	0.00	0.00	0.01	0.00
39.15	0.83	0.00	0.00	0.01	0.00	39.16	0.82	0.00	0.00	0.01	0.00
39.17	0.81	0.00	0.00	0.01	0.00	39.18	0.81	0.00	0.00	0.01	0.00
39.19	0.81	0.00	0.00	0.01	0.00	39.20	0.82	0.00	0.00	0.01	0.00
39.21	0.83	0.00	0.00	0.01	0.00	39.22	0.83	0.00	0.00	0.01	0.00
39.23	0.84	0.00	0.00	0.01	0.00	39.24	0.85	0.00	0.00	0.01	0.00
39.25	0.86	0.00	0.00	0.01	0.00	39.26	0.86	0.00	0.00	0.01	0.00
39.27	0.87	0.00	0.00	0.01	0.00	39.28	0.88	0.00	0.00	0.01	0.00
39.29	0.89	0.00	0.00	0.01	0.00	39.30	0.90	0.00	0.00	0.01	0.00
39.31	0.91	0.00	0.00	0.01	0.00	39.32	0.92	0.00	0.00	0.01	0.00
39.33	0.93	0.00	0.00	0.01	0.00	39.34	2.00	0.00	0.00	0.01	0.00
39.35	2.00	0.00	0.00	0.01	0.00	39.36	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
39.37	2.00	0.00	0.00	0.01	0.00	39.38	2.00	0.00	0.00	0.01	0.00
39.39	2.00	0.00	0.00	0.01	0.00	39.40	2.00	0.00	0.00	0.01	0.00
39.41	2.00	0.00	0.00	0.01	0.00	39.42	2.00	0.00	0.00	0.01	0.00
39.43	2.00	0.00	0.00	0.01	0.00	39.44	2.00	0.00	0.00	0.01	0.00
39.45	2.00	0.00	0.00	0.01	0.00	39.46	2.00	0.00	0.00	0.01	0.00
39.47	2.00	0.00	0.00	0.01	0.00	39.48	2.00	0.00	0.00	0.01	0.00
39.49	2.00	0.00	0.00	0.01	0.00	39.50	2.00	0.00	0.00	0.01	0.00
39.51	2.00	0.00	0.00	0.01	0.00	39.52	2.00	0.00	0.00	0.01	0.00
39.53	2.00	0.00	0.00	0.01	0.00	39.54	2.00	0.00	0.00	0.01	0.00
39.55	2.00	0.00	0.00	0.01	0.00	39.56	2.00	0.00	0.00	0.01	0.00
39.57	2.00	0.00	0.00	0.01	0.00	39.58	2.00	0.00	0.00	0.01	0.00
39.59	2.00	0.00	0.00	0.01	0.00	39.60	2.00	0.00	0.00	0.01	0.00
39.61	2.00	0.00	0.00	0.01	0.00	39.62	2.00	0.00	0.00	0.01	0.00
39.63	2.00	0.00	0.00	0.01	0.00	39.64	2.00	0.00	0.00	0.01	0.00
39.65	2.00	0.00	0.00	0.01	0.00	39.66	2.00	0.00	0.00	0.01	0.00
39.67	2.00	0.00	0.00	0.01	0.00	39.68	2.00	0.00	0.00	0.01	0.00
39.69	2.00	0.00	0.00	0.01	0.00	39.70	2.00	0.00	0.00	0.01	0.00
39.71	2.00	0.00	0.00	0.01	0.00	39.72	2.00	0.00	0.00	0.01	0.00
39.73	2.00	0.00	0.00	0.01	0.00	39.74	2.00	0.00	0.00	0.01	0.00
39.75	2.00	0.00	0.00	0.01	0.00	39.76	2.00	0.00	0.00	0.01	0.00
39.77	2.00	0.00	0.00	0.01	0.00	39.78	2.00	0.00	0.00	0.01	0.00
39.79	2.00	0.00	0.00	0.01	0.00	39.80	2.00	0.00	0.00	0.01	0.00
39.81	2.00	0.00	0.00	0.01	0.00	39.82	2.00	0.00	0.00	0.01	0.00
39.83	2.00	0.00	0.00	0.01	0.00	39.84	2.00	0.00	0.00	0.01	0.00
39.85	2.00	0.00	0.00	0.01	0.00	39.86	0.94	0.00	0.00	0.01	0.00
39.87	0.94	0.00	0.00	0.01	0.00	39.88	0.94	0.00	0.00	0.01	0.00
39.89	0.94	0.00	0.00	0.01	0.00	39.90	0.94	0.00	0.00	0.01	0.00
39.91	0.94	0.00	0.00	0.01	0.00	39.92	2.00	0.00	0.00	0.01	0.00
39.93	2.00	0.00	0.00	0.01	0.00	39.94	2.00	0.00	0.00	0.01	0.00
39.95	2.00	0.00	0.00	0.01	0.00	39.96	2.00	0.00	0.00	0.01	0.00
39.97	2.00	0.00	0.00	0.01	0.00	39.98	2.00	0.00	0.00	0.01	0.00
39.99	2.00	0.00	0.00	0.01	0.00	40.00	2.00	0.00	0.00	0.01	0.00
40.01	2.00	0.00	0.00	0.01	0.00	40.02	2.00	0.00	0.00	0.01	0.00
40.03	2.00	0.00	0.00	0.01	0.00	40.04	2.00	0.00	0.00	0.01	0.00
40.05	2.00	0.00	0.00	0.01	0.00	40.06	2.00	0.00	0.00	0.01	0.00
40.07	2.00	0.00	0.00	0.01	0.00	40.08	2.00	0.00	0.00	0.01	0.00
40.09	2.00	0.00	0.00	0.01	0.00	40.10	2.00	0.00	0.00	0.01	0.00
40.11	2.00	0.00	0.00	0.01	0.00	40.12	2.00	0.00	0.00	0.01	0.00
40.13	2.00	0.00	0.00	0.01	0.00	40.14	2.00	0.00	0.00	0.01	0.00
40.15	2.00	0.00	0.00	0.01	0.00	40.16	2.00	0.00	0.00	0.01	0.00
40.17	2.00	0.00	0.00	0.01	0.00	40.18	2.00	0.00	0.00	0.01	0.00
40.19	2.00	0.00	0.00	0.01	0.00	40.20	2.00	0.00	0.00	0.01	0.00
40.21	2.00	0.00	0.00	0.01	0.00	40.22	2.00	0.00	0.00	0.01	0.00
40.23	2.00	0.00	0.00	0.01	0.00	40.24	2.00	0.00	0.00	0.01	0.00
40.25	2.00	0.00	0.00	0.01	0.00	40.26	2.00	0.00	0.00	0.01	0.00
40.27	2.00	0.00	0.00	0.01	0.00	40.28	2.00	0.00	0.00	0.01	0.00
40.29	2.00	0.00	0.00	0.01	0.00	40.30	2.00	0.00	0.00	0.01	0.00
40.31	2.00	0.00	0.00	0.01	0.00	40.32	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
40.33	2.00	0.00	0.00	0.01	0.00	40.34	2.00	0.00	0.00	0.01	0.00
40.35	2.00	0.00	0.00	0.01	0.00	40.36	2.00	0.00	0.00	0.01	0.00
40.37	0.95	0.00	0.00	0.01	0.00	40.38	0.94	0.00	0.00	0.01	0.00
40.39	0.94	0.00	0.00	0.01	0.00	40.40	0.93	0.00	0.00	0.01	0.00
40.41	0.93	0.00	0.00	0.01	0.00	40.42	0.92	0.00	0.00	0.01	0.00
40.43	0.92	0.00	0.00	0.01	0.00	40.44	0.91	0.00	0.00	0.01	0.00
40.45	0.90	0.00	0.00	0.01	0.00	40.46	0.90	0.00	0.00	0.01	0.00
40.47	0.89	0.00	0.00	0.01	0.00	40.48	0.89	0.00	0.00	0.01	0.00
40.49	0.88	0.00	0.00	0.01	0.00	40.50	0.88	0.00	0.00	0.01	0.00
40.51	0.87	0.00	0.00	0.01	0.00	40.52	0.87	0.00	0.00	0.01	0.00
40.53	0.86	0.00	0.00	0.01	0.00	40.54	0.86	0.00	0.00	0.01	0.00
40.55	0.85	0.00	0.00	0.01	0.00	40.56	0.85	0.00	0.00	0.01	0.00
40.57	0.85	0.00	0.00	0.01	0.00	40.58	0.84	0.00	0.00	0.01	0.00
40.59	0.83	0.00	0.00	0.01	0.00	40.60	0.83	0.00	0.00	0.01	0.00
40.61	0.82	0.00	0.00	0.01	0.00	40.62	0.81	0.00	0.00	0.01	0.00
40.63	0.81	0.00	0.00	0.01	0.00	40.64	0.80	0.00	0.00	0.01	0.00
40.65	0.79	0.00	0.00	0.01	0.00	40.66	0.79	0.00	0.00	0.01	0.00
40.67	0.78	0.00	0.00	0.01	0.00	40.68	0.77	0.00	0.00	0.01	0.00
40.69	0.77	0.00	0.00	0.01	0.00	40.70	0.76	0.00	0.00	0.01	0.00
40.71	0.75	0.00	0.00	0.01	0.00	40.72	0.74	0.00	0.00	0.01	0.00
40.73	0.73	0.00	0.00	0.01	0.00	40.74	0.73	0.00	0.00	0.01	0.00
40.75	0.72	0.00	0.00	0.01	0.00	40.76	0.72	0.00	0.00	0.01	0.00
40.77	0.72	0.00	0.00	0.01	0.00	40.78	0.71	0.00	0.00	0.01	0.00
40.79	0.71	0.00	0.00	0.01	0.00	40.80	0.70	0.00	0.00	0.01	0.00
40.81	0.70	0.00	0.00	0.01	0.00	40.82	0.69	0.00	0.00	0.01	0.00
40.83	0.69	0.00	0.00	0.01	0.00	40.84	0.68	0.00	0.00	0.01	0.00
40.85	0.68	0.00	0.00	0.01	0.00	40.86	0.67	0.00	0.00	0.01	0.00
40.87	0.66	0.00	0.00	0.01	0.00	40.88	0.66	0.00	0.00	0.01	0.00
40.89	0.65	0.00	0.00	0.01	0.00	40.90	0.64	0.00	0.00	0.01	0.00
40.91	0.64	0.00	0.00	0.01	0.00	40.92	0.63	0.00	0.00	0.01	0.00
40.93	0.62	0.00	0.00	0.01	0.00	40.94	0.61	0.00	0.00	0.01	0.00
40.95	0.60	0.00	0.00	0.01	0.00	40.96	0.59	0.00	0.00	0.01	0.00
40.97	0.58	0.00	0.00	0.01	0.00	40.98	0.57	0.00	0.00	0.01	0.00
40.99	0.56	0.00	0.00	0.01	0.01	41.00	0.55	0.00	0.00	0.01	0.01
41.01	0.54	0.00	0.00	0.01	0.01	41.02	2.00	0.00	0.00	0.01	0.00
41.03	2.00	0.00	0.00	0.01	0.00	41.04	2.00	0.00	0.00	0.01	0.00
41.05	2.00	0.00	0.00	0.01	0.00	41.06	2.00	0.00	0.00	0.01	0.00
41.07	2.00	0.00	0.00	0.01	0.00	41.08	2.00	0.00	0.00	0.01	0.00
41.09	2.00	0.00	0.00	0.01	0.00	41.10	2.00	0.00	0.00	0.01	0.00
41.11	2.00	0.00	0.00	0.01	0.00	41.12	2.00	0.00	0.00	0.01	0.00
41.13	2.00	0.00	0.00	0.01	0.00	41.14	2.00	0.00	0.00	0.01	0.00
41.15	2.00	0.00	0.00	0.01	0.00	41.16	2.00	0.00	0.00	0.01	0.00
41.17	2.00	0.00	0.00	0.01	0.00	41.18	2.00	0.00	0.00	0.01	0.00
41.19	2.00	0.00	0.00	0.01	0.00	41.20	2.00	0.00	0.00	0.01	0.00
41.21	2.00	0.00	0.00	0.01	0.00	41.22	2.00	0.00	0.00	0.01	0.00
41.23	2.00	0.00	0.00	0.01	0.00	41.24	2.00	0.00	0.00	0.01	0.00
41.25	2.00	0.00	0.00	0.01	0.00	41.26	2.00	0.00	0.00	0.01	0.00
41.27	2.00	0.00	0.00	0.01	0.00	41.28	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
41.29	2.00	0.00	0.00	0.01	0.00	41.30	2.00	0.00	0.00	0.01	0.00
41.31	2.00	0.00	0.00	0.01	0.00	41.32	2.00	0.00	0.00	0.01	0.00
41.33	2.00	0.00	0.00	0.01	0.00	41.34	2.00	0.00	0.00	0.01	0.00
41.35	2.00	0.00	0.00	0.01	0.00	41.36	2.00	0.00	0.00	0.01	0.00
41.37	2.00	0.00	0.00	0.01	0.00	41.38	2.00	0.00	0.00	0.01	0.00
41.39	2.00	0.00	0.00	0.01	0.00	41.40	2.00	0.00	0.00	0.01	0.00
41.41	2.00	0.00	0.00	0.01	0.00	41.42	2.00	0.00	0.00	0.01	0.00
41.43	2.00	0.00	0.00	0.01	0.00	41.44	2.00	0.00	0.00	0.01	0.00
41.45	2.00	0.00	0.00	0.01	0.00	41.46	2.00	0.00	0.00	0.01	0.00
41.47	2.00	0.00	0.00	0.01	0.00	41.48	2.00	0.00	0.00	0.01	0.00
41.49	2.00	0.00	0.00	0.01	0.00	41.50	2.00	0.00	0.00	0.01	0.00
41.51	2.00	0.00	0.00	0.01	0.00	41.52	2.00	0.00	0.00	0.01	0.00
41.53	2.00	0.00	0.00	0.01	0.00	41.54	2.00	0.00	0.00	0.01	0.00
41.55	2.00	0.00	0.00	0.01	0.00	41.56	2.00	0.00	0.00	0.01	0.00
41.57	2.00	0.00	0.00	0.01	0.00	41.58	2.00	0.00	0.00	0.01	0.00
41.59	2.00	0.00	0.00	0.01	0.00	41.60	2.00	0.00	0.00	0.01	0.00
41.61	2.00	0.00	0.00	0.01	0.00	41.62	2.00	0.00	0.00	0.01	0.00
41.63	2.00	0.00	0.00	0.01	0.00	41.64	2.00	0.00	0.00	0.01	0.00
41.65	2.00	0.00	0.00	0.01	0.00	41.66	2.00	0.00	0.00	0.01	0.00
41.67	2.00	0.00	0.00	0.01	0.00	41.68	2.00	0.00	0.00	0.01	0.00
41.69	2.00	0.00	0.00	0.01	0.00	41.70	2.00	0.00	0.00	0.01	0.00
41.71	2.00	0.00	0.00	0.01	0.00	41.72	2.00	0.00	0.00	0.01	0.00
41.73	2.00	0.00	0.00	0.01	0.00	41.74	2.00	0.00	0.00	0.01	0.00
41.75	2.00	0.00	0.00	0.01	0.00	41.76	2.00	0.00	0.00	0.01	0.00
41.77	2.00	0.00	0.00	0.01	0.00	41.78	2.00	0.00	0.00	0.01	0.00
41.79	2.00	0.00	0.00	0.01	0.00	41.80	2.00	0.00	0.00	0.01	0.00
41.81	2.00	0.00	0.00	0.01	0.00	41.82	2.00	0.00	0.00	0.01	0.00
41.83	2.00	0.00	0.00	0.01	0.00	41.84	2.00	0.00	0.00	0.01	0.00
41.85	2.00	0.00	0.00	0.01	0.00	41.86	2.00	0.00	0.00	0.01	0.00
41.87	2.00	0.00	0.00	0.01	0.00	41.88	2.00	0.00	0.00	0.01	0.00
41.89	2.00	0.00	0.00	0.01	0.00	41.90	2.00	0.00	0.00	0.01	0.00
41.91	2.00	0.00	0.00	0.01	0.00	41.92	2.00	0.00	0.00	0.01	0.00
41.93	2.00	0.00	0.00	0.01	0.00	41.94	2.00	0.00	0.00	0.01	0.00
41.95	2.00	0.00	0.00	0.01	0.00	41.96	1.62	0.00	0.00	0.01	0.00
41.97	1.63	0.00	0.00	0.01	0.00	41.98	1.63	0.00	0.00	0.01	0.00
41.99	1.63	0.00	0.00	0.01	0.00	42.00	1.63	0.00	0.00	0.01	0.00
42.01	1.64	0.00	0.00	0.01	0.00	42.02	1.64	0.00	0.00	0.01	0.00
42.03	1.64	0.00	0.00	0.01	0.00	42.04	1.65	0.00	0.00	0.01	0.00
42.05	1.66	0.00	0.00	0.01	0.00	42.06	1.69	0.00	0.00	0.01	0.00
42.07	1.71	0.00	0.00	0.01	0.00	42.08	1.74	0.00	0.00	0.01	0.00
42.09	1.77	0.00	0.00	0.01	0.00	42.10	1.80	0.00	0.00	0.01	0.00
42.11	1.83	0.00	0.00	0.01	0.00	42.12	1.85	0.00	0.00	0.01	0.00
42.13	1.88	0.00	0.00	0.01	0.00	42.14	1.91	0.00	0.00	0.01	0.00
42.15	1.95	0.00	0.00	0.01	0.00	42.16	1.99	0.00	0.00	0.01	0.00
42.17	2.00	0.00	0.00	0.01	0.00	42.18	2.00	0.00	0.00	0.01	0.00
42.19	2.00	0.00	0.00	0.01	0.00	42.20	2.00	0.00	0.00	0.01	0.00
42.21	2.00	0.00	0.00	0.01	0.00	42.22	2.00	0.00	0.00	0.01	0.00
42.23	2.00	0.00	0.00	0.01	0.00	42.24	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
42.25	2.00	0.00	0.00	0.01	0.00	42.26	2.00	0.00	0.00	0.01	0.00
42.27	2.00	0.00	0.00	0.01	0.00	42.28	0.87	0.00	0.00	0.01	0.00
42.29	0.74	0.00	0.00	0.01	0.00	42.30	0.65	0.00	0.00	0.01	0.00
42.31	0.59	0.00	0.00	0.01	0.00	42.32	0.55	0.00	0.00	0.01	0.00
42.33	0.51	0.00	0.00	0.01	0.01	42.34	0.46	0.00	0.00	0.01	0.01
42.35	0.42	0.00	0.00	0.01	0.01	42.36	0.39	0.00	0.00	0.01	0.01
42.37	0.36	0.00	0.00	0.01	0.01	42.38	0.40	0.00	0.00	0.01	0.01
42.39	0.40	0.00	0.00	0.01	0.01	42.40	0.40	0.00	0.00	0.01	0.01
42.41	0.40	0.00	0.00	0.01	0.01	42.42	0.36	0.00	0.00	0.01	0.01
42.43	0.37	0.00	0.00	0.01	0.01	42.44	0.39	0.00	0.00	0.01	0.01
42.45	0.40	0.00	0.00	0.01	0.01	42.46	0.42	0.00	0.00	0.01	0.01
42.47	0.43	0.00	0.00	0.01	0.01	42.48	0.47	0.00	0.00	0.01	0.01
42.49	0.52	0.00	0.00	0.01	0.01	42.50	0.59	0.00	0.00	0.01	0.00
42.51	0.69	0.00	0.00	0.01	0.00	42.52	0.80	0.00	0.00	0.01	0.00
42.53	0.93	0.00	0.00	0.01	0.00	42.54	2.00	0.00	0.00	0.01	0.00
42.55	2.00	0.00	0.00	0.01	0.00	42.56	2.00	0.00	0.00	0.01	0.00
42.57	2.00	0.00	0.00	0.01	0.00	42.58	2.00	0.00	0.00	0.01	0.00
42.59	2.00	0.00	0.00	0.01	0.00	42.60	2.00	0.00	0.00	0.01	0.00
42.61	2.00	0.00	0.00	0.01	0.00	42.62	2.00	0.00	0.00	0.01	0.00
42.63	2.00	0.00	0.00	0.01	0.00	42.64	2.00	0.00	0.00	0.01	0.00
42.65	1.88	0.00	0.00	0.01	0.00	42.66	1.85	0.00	0.00	0.01	0.00
42.67	1.82	0.00	0.00	0.01	0.00	42.68	1.79	0.00	0.00	0.01	0.00
42.69	1.75	0.00	0.00	0.01	0.00	42.70	1.71	0.00	0.00	0.01	0.00
42.71	1.68	0.00	0.00	0.01	0.00	42.72	1.65	0.00	0.00	0.01	0.00
42.73	1.63	0.00	0.00	0.01	0.00	42.74	1.62	0.00	0.00	0.01	0.00
42.75	1.61	0.00	0.00	0.01	0.00	42.76	1.61	0.00	0.00	0.01	0.00
42.77	1.61	0.00	0.00	0.01	0.00	42.78	1.61	0.00	0.00	0.01	0.00
42.79	1.60	0.00	0.00	0.01	0.00	42.80	1.60	0.00	0.00	0.01	0.00
42.81	1.60	0.00	0.00	0.01	0.00	42.82	1.61	0.00	0.00	0.01	0.00
42.83	1.63	0.00	0.00	0.01	0.00	42.84	1.67	0.00	0.00	0.01	0.00
42.85	1.71	0.00	0.00	0.01	0.00	42.86	2.00	0.00	0.00	0.01	0.00
42.87	2.00	0.00	0.00	0.01	0.00	42.88	2.00	0.00	0.00	0.01	0.00
42.89	2.00	0.00	0.00	0.01	0.00	42.90	2.00	0.00	0.00	0.01	0.00
42.91	2.00	0.00	0.00	0.01	0.00	42.92	2.00	0.00	0.00	0.01	0.00
42.93	2.00	0.00	0.00	0.01	0.00	42.94	0.92	0.00	0.00	0.01	0.00
42.95	0.81	0.00	0.00	0.01	0.00	42.96	0.71	0.00	0.00	0.01	0.00
42.97	0.63	0.00	0.00	0.01	0.00	42.98	0.56	0.00	0.00	0.01	0.00
42.99	0.52	0.00	0.00	0.01	0.00	43.00	0.51	0.00	0.00	0.01	0.01
43.01	0.51	0.00	0.00	0.01	0.01	43.02	0.51	0.00	0.00	0.01	0.01
43.03	0.51	0.00	0.00	0.01	0.01	43.04	0.51	0.00	0.00	0.01	0.01
43.05	0.51	0.00	0.00	0.01	0.01	43.06	0.51	0.00	0.00	0.01	0.01
43.07	0.52	0.00	0.00	0.01	0.01	43.08	0.53	0.00	0.00	0.01	0.00
43.09	0.55	0.00	0.00	0.01	0.00	43.10	0.60	0.00	0.00	0.01	0.00
43.11	0.65	0.00	0.00	0.01	0.00	43.12	0.71	0.00	0.00	0.01	0.00
43.13	0.78	0.00	0.00	0.01	0.00	43.14	0.85	0.00	0.00	0.01	0.00
43.15	0.92	0.00	0.00	0.01	0.00	43.16	2.00	0.00	0.00	0.01	0.00
43.17	2.00	0.00	0.00	0.01	0.00	43.18	2.00	0.00	0.00	0.01	0.00
43.19	2.00	0.00	0.00	0.01	0.00	43.20	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
43.21	2.00	0.00	0.00	0.01	0.00	43.22	2.00	0.00	0.00	0.01	0.00
43.23	2.00	0.00	0.00	0.01	0.00	43.24	2.00	0.00	0.00	0.01	0.00
43.25	2.00	0.00	0.00	0.01	0.00	43.26	2.00	0.00	0.00	0.01	0.00
43.27	2.00	0.00	0.00	0.01	0.00	43.28	2.00	0.00	0.00	0.01	0.00
43.29	2.00	0.00	0.00	0.01	0.00	43.30	2.00	0.00	0.00	0.01	0.00
43.31	2.00	0.00	0.00	0.01	0.00	43.32	2.00	0.00	0.00	0.01	0.00
43.33	2.00	0.00	0.00	0.01	0.00	43.34	2.00	0.00	0.00	0.01	0.00
43.35	2.00	0.00	0.00	0.01	0.00	43.36	2.00	0.00	0.00	0.01	0.00
43.37	2.00	0.00	0.00	0.01	0.00	43.38	2.00	0.00	0.00	0.01	0.00
43.39	2.00	0.00	0.00	0.01	0.00	43.40	2.00	0.00	0.00	0.01	0.00
43.41	2.00	0.00	0.00	0.01	0.00	43.42	2.00	0.00	0.00	0.01	0.00
43.43	2.00	0.00	0.00	0.01	0.00	43.44	2.00	0.00	0.00	0.01	0.00
43.45	2.00	0.00	0.00	0.01	0.00	43.46	2.00	0.00	0.00	0.01	0.00
43.47	2.00	0.00	0.00	0.01	0.00	43.48	2.00	0.00	0.00	0.01	0.00
43.49	2.00	0.00	0.00	0.01	0.00	43.50	2.00	0.00	0.00	0.01	0.00
43.51	2.00	0.00	0.00	0.01	0.00	43.52	2.00	0.00	0.00	0.01	0.00
43.53	2.00	0.00	0.00	0.01	0.00	43.54	2.00	0.00	0.00	0.01	0.00
43.55	2.00	0.00	0.00	0.01	0.00	43.56	2.00	0.00	0.00	0.01	0.00
43.57	2.00	0.00	0.00	0.01	0.00	43.58	2.00	0.00	0.00	0.01	0.00
43.59	2.00	0.00	0.00	0.01	0.00	43.60	2.00	0.00	0.00	0.01	0.00
43.61	0.36	0.00	0.00	0.01	0.01	43.62	0.36	0.00	0.00	0.01	0.01
43.63	0.36	0.00	0.00	0.01	0.01	43.64	0.36	0.00	0.00	0.01	0.01
43.65	0.36	0.00	0.00	0.01	0.01	43.66	0.35	0.00	0.00	0.01	0.01
43.67	0.35	0.00	0.00	0.01	0.01	43.68	2.00	0.00	0.00	0.01	0.00
43.69	2.00	0.00	0.00	0.01	0.00	43.70	2.00	0.00	0.00	0.01	0.00
43.71	2.00	0.00	0.00	0.01	0.00	43.72	2.00	0.00	0.00	0.01	0.00
43.73	2.00	0.00	0.00	0.01	0.00	43.74	2.00	0.00	0.00	0.01	0.00
43.75	2.00	0.00	0.00	0.01	0.00	43.76	2.00	0.00	0.00	0.01	0.00
43.77	2.00	0.00	0.00	0.01	0.00	43.78	2.00	0.00	0.00	0.01	0.00
43.79	2.00	0.00	0.00	0.01	0.00	43.80	2.00	0.00	0.00	0.01	0.00
43.81	2.00	0.00	0.00	0.01	0.00	43.82	2.00	0.00	0.00	0.01	0.00
43.83	2.00	0.00	0.00	0.01	0.00	43.84	2.00	0.00	0.00	0.01	0.00
43.85	2.00	0.00	0.00	0.01	0.00	43.86	2.00	0.00	0.00	0.01	0.00
43.87	2.00	0.00	0.00	0.01	0.00	43.88	2.00	0.00	0.00	0.01	0.00
43.89	2.00	0.00	0.00	0.01	0.00	43.90	2.00	0.00	0.00	0.01	0.00
43.91	2.00	0.00	0.00	0.01	0.00	43.92	2.00	0.00	0.00	0.01	0.00
43.93	2.00	0.00	0.00	0.01	0.00	43.94	2.00	0.00	0.00	0.01	0.00
43.95	2.00	0.00	0.00	0.01	0.00	43.96	2.00	0.00	0.00	0.01	0.00
43.97	2.00	0.00	0.00	0.01	0.00	43.98	2.00	0.00	0.00	0.01	0.00
43.99	2.00	0.00	0.00	0.01	0.00	44.00	2.00	0.00	0.00	0.01	0.00
44.01	2.00	0.00	0.00	0.01	0.00	44.02	2.00	0.00	0.00	0.01	0.00
44.03	2.00	0.00	0.00	0.01	0.00	44.04	2.00	0.00	0.00	0.01	0.00
44.05	1.74	0.00	0.00	0.01	0.00	44.06	1.75	0.00	0.00	0.01	0.00
44.07	1.75	0.00	0.00	0.01	0.00	44.08	1.76	0.00	0.00	0.01	0.00
44.09	1.76	0.00	0.00	0.01	0.00	44.10	1.77	0.00	0.00	0.01	0.00
44.11	1.77	0.00	0.00	0.01	0.00	44.12	1.78	0.00	0.00	0.01	0.00
44.13	2.00	0.00	0.00	0.01	0.00	44.14	2.00	0.00	0.00	0.01	0.00
44.15	2.00	0.00	0.00	0.01	0.00	44.16	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
44.17	2.00	0.00	0.00	0.01	0.00	44.18	2.00	0.00	0.00	0.01	0.00
44.19	2.00	0.00	0.00	0.01	0.00	44.20	2.00	0.00	0.00	0.01	0.00
44.21	2.00	0.00	0.00	0.01	0.00	44.22	2.00	0.00	0.00	0.01	0.00
44.23	2.00	0.00	0.00	0.01	0.00	44.24	2.00	0.00	0.00	0.01	0.00
44.25	2.00	0.00	0.00	0.01	0.00	44.26	2.00	0.00	0.00	0.01	0.00
44.27	2.00	0.00	0.00	0.01	0.00	44.28	2.00	0.00	0.00	0.01	0.00
44.29	2.00	0.00	0.00	0.01	0.00	44.30	2.00	0.00	0.00	0.01	0.00
44.31	2.00	0.00	0.00	0.01	0.00	44.32	2.00	0.00	0.00	0.01	0.00
44.33	2.00	0.00	0.00	0.01	0.00	44.34	2.00	0.00	0.00	0.01	0.00
44.35	2.00	0.00	0.00	0.01	0.00	44.36	2.00	0.00	0.00	0.01	0.00
44.37	2.00	0.00	0.00	0.01	0.00	44.38	2.00	0.00	0.00	0.01	0.00
44.39	2.00	0.00	0.00	0.01	0.00	44.40	2.00	0.00	0.00	0.01	0.00
44.41	2.00	0.00	0.00	0.01	0.00	44.42	2.00	0.00	0.00	0.01	0.00
44.43	2.00	0.00	0.00	0.01	0.00	44.44	2.00	0.00	0.00	0.01	0.00
44.45	2.00	0.00	0.00	0.01	0.00	44.46	2.00	0.00	0.00	0.01	0.00
44.47	2.00	0.00	0.00	0.01	0.00	44.48	2.00	0.00	0.00	0.01	0.00
44.49	2.00	0.00	0.00	0.01	0.00	44.50	2.00	0.00	0.00	0.01	0.00
44.51	2.00	0.00	0.00	0.01	0.00	44.52	2.00	0.00	0.00	0.01	0.00
44.53	2.00	0.00	0.00	0.01	0.00	44.54	2.00	0.00	0.00	0.01	0.00
44.55	2.00	0.00	0.00	0.01	0.00	44.56	2.00	0.00	0.00	0.01	0.00
44.57	2.00	0.00	0.00	0.01	0.00	44.58	2.00	0.00	0.00	0.01	0.00
44.59	2.00	0.00	0.00	0.01	0.00	44.60	2.00	0.00	0.00	0.01	0.00
44.61	2.00	0.00	0.00	0.01	0.00	44.62	2.00	0.00	0.00	0.01	0.00
44.63	2.00	0.00	0.00	0.01	0.00	44.64	2.00	0.00	0.00	0.01	0.00
44.65	2.00	0.00	0.00	0.01	0.00	44.66	2.00	0.00	0.00	0.01	0.00
44.67	2.00	0.00	0.00	0.01	0.00	44.68	2.00	0.00	0.00	0.01	0.00
44.69	2.00	0.00	0.00	0.01	0.00	44.70	2.00	0.00	0.00	0.01	0.00
44.71	2.00	0.00	0.00	0.01	0.00	44.72	2.00	0.00	0.00	0.01	0.00
44.73	2.00	0.00	0.00	0.01	0.00	44.74	2.00	0.00	0.00	0.01	0.00
44.75	2.00	0.00	0.00	0.01	0.00	44.76	2.00	0.00	0.00	0.01	0.00
44.77	2.00	0.00	0.00	0.01	0.00	44.78	2.00	0.00	0.00	0.01	0.00
44.79	2.00	0.00	0.00	0.01	0.00	44.80	2.00	0.00	0.00	0.01	0.00
44.81	0.41	0.00	0.00	0.01	0.01	44.82	0.41	0.00	0.00	0.01	0.01
44.83	0.41	0.00	0.00	0.01	0.01	44.84	0.41	0.00	0.00	0.01	0.01
44.85	0.41	0.00	0.00	0.01	0.01	44.86	0.41	0.00	0.00	0.01	0.01
44.87	0.41	0.00	0.00	0.01	0.01	44.88	0.41	0.00	0.00	0.01	0.01
44.89	0.41	0.00	0.00	0.01	0.01	44.90	0.41	0.00	0.00	0.01	0.01
44.91	0.41	0.00	0.00	0.01	0.01	44.92	0.41	0.00	0.00	0.01	0.01
44.93	0.41	0.00	0.00	0.01	0.01	44.94	0.41	0.00	0.00	0.01	0.01
44.95	0.41	0.00	0.00	0.01	0.01	44.96	0.41	0.00	0.00	0.01	0.01
44.97	0.41	0.00	0.00	0.01	0.01	44.98	0.42	0.00	0.00	0.01	0.01
44.99	0.42	0.00	0.00	0.01	0.01	45.00	0.42	0.00	0.00	0.01	0.01
45.01	0.42	0.00	0.00	0.01	0.01	45.02	0.43	0.00	0.00	0.01	0.01
45.03	0.43	0.00	0.00	0.01	0.01	45.04	0.43	0.00	0.00	0.01	0.01
45.05	0.44	0.00	0.00	0.01	0.01	45.06	0.44	0.00	0.00	0.01	0.01
45.07	0.44	0.00	0.00	0.01	0.01	45.08	2.00	0.00	0.00	0.01	0.00
45.09	2.00	0.00	0.00	0.01	0.00	45.10	2.00	0.00	0.00	0.01	0.00
45.11	2.00	0.00	0.00	0.01	0.00	45.12	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
45.13	2.00	0.00	0.00	0.01	0.00	45.14	2.00	0.00	0.00	0.01	0.00
45.15	2.00	0.00	0.00	0.01	0.00	45.16	2.00	0.00	0.00	0.01	0.00
45.17	2.00	0.00	0.00	0.01	0.00	45.18	2.00	0.00	0.00	0.01	0.00
45.19	2.00	0.00	0.00	0.01	0.00	45.20	2.00	0.00	0.00	0.01	0.00
45.21	2.00	0.00	0.00	0.01	0.00	45.22	2.00	0.00	0.00	0.01	0.00
45.23	2.00	0.00	0.00	0.01	0.00	45.24	2.00	0.00	0.00	0.01	0.00
45.25	2.00	0.00	0.00	0.01	0.00	45.26	2.00	0.00	0.00	0.01	0.00
45.27	2.00	0.00	0.00	0.01	0.00	45.28	2.00	0.00	0.00	0.01	0.00
45.29	2.00	0.00	0.00	0.01	0.00	45.30	2.00	0.00	0.00	0.01	0.00
45.31	2.00	0.00	0.00	0.01	0.00	45.32	2.00	0.00	0.00	0.01	0.00
45.33	2.00	0.00	0.00	0.01	0.00	45.34	0.58	0.00	0.00	0.01	0.00
45.35	0.58	0.00	0.00	0.01	0.00	45.36	0.58	0.00	0.00	0.01	0.00
45.37	0.59	0.00	0.00	0.01	0.00	45.38	0.59	0.00	0.00	0.01	0.00
45.39	0.59	0.00	0.00	0.01	0.00	45.40	0.60	0.00	0.00	0.01	0.00
45.41	0.60	0.00	0.00	0.01	0.00	45.42	0.60	0.00	0.00	0.01	0.00
45.43	0.59	0.00	0.00	0.01	0.00	45.44	0.59	0.00	0.00	0.01	0.00
45.45	0.58	0.00	0.00	0.01	0.00	45.46	0.57	0.00	0.00	0.01	0.00
45.47	0.57	0.00	0.00	0.01	0.00	45.48	0.56	0.00	0.00	0.01	0.00
45.49	0.56	0.00	0.00	0.01	0.00	45.50	2.00	0.00	0.00	0.01	0.00
45.51	2.00	0.00	0.00	0.01	0.00	45.52	2.00	0.00	0.00	0.01	0.00
45.53	2.00	0.00	0.00	0.01	0.00	45.54	2.00	0.00	0.00	0.01	0.00
45.55	2.00	0.00	0.00	0.01	0.00	45.56	2.00	0.00	0.00	0.01	0.00
45.57	2.00	0.00	0.00	0.01	0.00	45.58	2.00	0.00	0.00	0.01	0.00
45.59	2.00	0.00	0.00	0.01	0.00	45.60	2.00	0.00	0.00	0.01	0.00
45.61	2.00	0.00	0.00	0.01	0.00	45.62	2.00	0.00	0.00	0.01	0.00
45.63	2.00	0.00	0.00	0.01	0.00	45.64	2.00	0.00	0.00	0.01	0.00
45.65	2.00	0.00	0.00	0.01	0.00	45.66	2.00	0.00	0.00	0.01	0.00
45.67	2.00	0.00	0.00	0.01	0.00	45.68	2.00	0.00	0.00	0.01	0.00
45.69	2.00	0.00	0.00	0.01	0.00	45.70	2.00	0.00	0.00	0.01	0.00
45.71	2.00	0.00	0.00	0.01	0.00	45.72	2.00	0.00	0.00	0.01	0.00
45.73	2.00	0.00	0.00	0.01	0.00	45.74	2.00	0.00	0.00	0.01	0.00
45.75	2.00	0.00	0.00	0.01	0.00	45.76	2.00	0.00	0.00	0.01	0.00
45.77	0.39	0.00	0.00	0.01	0.01	45.78	0.39	0.00	0.00	0.01	0.01
45.79	0.39	0.00	0.00	0.01	0.01	45.80	0.39	0.00	0.00	0.01	0.01
45.81	0.39	0.00	0.00	0.01	0.01	45.82	0.39	0.00	0.00	0.01	0.01
45.83	0.39	0.00	0.00	0.01	0.01	45.84	0.39	0.00	0.00	0.01	0.01
45.85	0.38	0.00	0.00	0.01	0.01	45.86	0.38	0.00	0.00	0.01	0.01
45.87	0.38	0.00	0.00	0.01	0.01	45.88	0.38	0.00	0.00	0.01	0.01
45.89	0.38	0.00	0.00	0.01	0.01	45.90	0.38	0.00	0.00	0.01	0.01
45.91	0.38	0.00	0.00	0.01	0.01	45.92	0.38	0.00	0.00	0.01	0.01
45.93	0.38	0.00	0.00	0.01	0.01	45.94	0.37	0.00	0.00	0.01	0.01
45.95	0.37	0.00	0.00	0.01	0.01	45.96	0.37	0.00	0.00	0.01	0.01
45.97	0.37	0.00	0.00	0.01	0.01	45.98	0.37	0.00	0.00	0.01	0.01
45.99	0.37	0.00	0.00	0.01	0.01	46.00	0.37	0.00	0.00	0.01	0.01
46.01	0.37	0.00	0.00	0.01	0.01	46.02	0.37	0.00	0.00	0.01	0.01
46.03	0.37	0.00	0.00	0.01	0.01	46.04	0.37	0.00	0.00	0.01	0.01
46.05	0.37	0.00	0.00	0.01	0.01	46.06	0.37	0.00	0.00	0.01	0.01
46.07	0.37	0.00	0.00	0.01	0.01	46.08	0.37	0.00	0.00	0.01	0.01

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
46.09	0.37	0.00	0.00	0.01	0.01	46.10	0.37	0.00	0.00	0.01	0.01
46.11	0.38	0.00	0.00	0.01	0.01	46.12	0.38	0.00	0.00	0.01	0.01
46.13	0.39	0.00	0.00	0.01	0.01	46.14	0.40	0.00	0.00	0.01	0.01
46.15	0.40	0.00	0.00	0.01	0.01	46.16	0.41	0.00	0.00	0.01	0.01
46.17	0.42	0.00	0.00	0.01	0.01	46.18	0.43	0.00	0.00	0.01	0.01
46.19	0.44	0.00	0.00	0.01	0.01	46.20	0.45	0.00	0.00	0.01	0.00
46.21	0.46	0.00	0.00	0.01	0.00	46.22	0.47	0.00	0.00	0.01	0.00
46.23	0.48	0.00	0.00	0.01	0.00	46.24	0.49	0.00	0.00	0.01	0.00
46.25	0.50	0.00	0.00	0.01	0.00	46.26	0.51	0.00	0.00	0.01	0.00
46.27	0.53	0.00	0.00	0.01	0.00	46.28	0.53	0.00	0.00	0.01	0.00
46.29	0.53	0.00	0.00	0.01	0.00	46.30	0.53	0.00	0.00	0.01	0.00
46.31	0.52	0.00	0.00	0.01	0.00	46.32	0.51	0.00	0.00	0.01	0.00
46.33	0.50	0.00	0.00	0.01	0.00	46.34	0.49	0.00	0.00	0.01	0.00
46.35	0.48	0.00	0.00	0.01	0.00	46.36	0.48	0.00	0.00	0.01	0.00
46.37	0.47	0.00	0.00	0.01	0.00	46.38	0.47	0.00	0.00	0.01	0.00
46.39	0.47	0.00	0.00	0.01	0.00	46.40	0.47	0.00	0.00	0.01	0.00
46.41	0.46	0.00	0.00	0.01	0.00	46.42	0.46	0.00	0.00	0.01	0.00
46.43	0.46	0.00	0.00	0.01	0.00	46.44	0.46	0.00	0.00	0.01	0.00
46.45	2.00	0.00	0.00	0.01	0.00	46.46	2.00	0.00	0.00	0.01	0.00
46.47	2.00	0.00	0.00	0.01	0.00	46.48	2.00	0.00	0.00	0.01	0.00
46.49	2.00	0.00	0.00	0.01	0.00	46.50	2.00	0.00	0.00	0.01	0.00
46.51	2.00	0.00	0.00	0.01	0.00	46.52	2.00	0.00	0.00	0.01	0.00
46.53	2.00	0.00	0.00	0.01	0.00	46.54	2.00	0.00	0.00	0.01	0.00
46.55	2.00	0.00	0.00	0.01	0.00	46.56	2.00	0.00	0.00	0.01	0.00
46.57	2.00	0.00	0.00	0.01	0.00	46.58	2.00	0.00	0.00	0.01	0.00
46.59	2.00	0.00	0.00	0.01	0.00	46.60	2.00	0.00	0.00	0.01	0.00
46.61	2.00	0.00	0.00	0.01	0.00	46.62	2.00	0.00	0.00	0.01	0.00
46.63	2.00	0.00	0.00	0.01	0.00	46.64	2.00	0.00	0.00	0.01	0.00
46.65	2.00	0.00	0.00	0.01	0.00	46.66	2.00	0.00	0.00	0.01	0.00
46.67	2.00	0.00	0.00	0.01	0.00	46.68	2.00	0.00	0.00	0.01	0.00
46.69	2.00	0.00	0.00	0.01	0.00	46.70	2.00	0.00	0.00	0.01	0.00
46.71	2.00	0.00	0.00	0.01	0.00	46.72	2.00	0.00	0.00	0.01	0.00
46.73	2.00	0.00	0.00	0.01	0.00	46.74	2.00	0.00	0.00	0.01	0.00
46.75	2.00	0.00	0.00	0.01	0.00	46.76	2.00	0.00	0.00	0.01	0.00
46.77	2.00	0.00	0.00	0.01	0.00	46.78	2.00	0.00	0.00	0.01	0.00
46.79	2.00	0.00	0.00	0.01	0.00	46.80	2.00	0.00	0.00	0.01	0.00
46.81	2.00	0.00	0.00	0.01	0.00	46.82	2.00	0.00	0.00	0.01	0.00
46.83	2.00	0.00	0.00	0.01	0.00	46.84	2.00	0.00	0.00	0.01	0.00
46.85	2.00	0.00	0.00	0.01	0.00	46.86	2.00	0.00	0.00	0.01	0.00
46.87	2.00	0.00	0.00	0.01	0.00	46.88	2.00	0.00	0.00	0.01	0.00
46.89	2.00	0.00	0.00	0.01	0.00	46.90	2.00	0.00	0.00	0.01	0.00
46.91	2.00	0.00	0.00	0.01	0.00	46.92	2.00	0.00	0.00	0.01	0.00
46.93	2.00	0.00	0.00	0.01	0.00	46.94	2.00	0.00	0.00	0.01	0.00
46.95	2.00	0.00	0.00	0.01	0.00	46.96	2.00	0.00	0.00	0.01	0.00
46.97	2.00	0.00	0.00	0.01	0.00	46.98	2.00	0.00	0.00	0.01	0.00
46.99	2.00	0.00	0.00	0.01	0.00	47.00	2.00	0.00	0.00	0.01	0.00
47.01	2.00	0.00	0.00	0.01	0.00	47.02	2.00	0.00	0.00	0.01	0.00
47.03	2.00	0.00	0.00	0.01	0.00	47.04	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
47.05	2.00	0.00	0.00	0.01	0.00	47.06	2.00	0.00	0.00	0.01	0.00
47.07	1.99	0.00	0.00	0.01	0.00	47.08	1.98	0.00	0.00	0.01	0.00
47.09	1.97	0.00	0.00	0.01	0.00	47.10	1.96	0.00	0.00	0.01	0.00
47.11	1.95	0.00	0.00	0.01	0.00	47.12	1.94	0.00	0.00	0.01	0.00
47.13	1.94	0.00	0.00	0.01	0.00	47.14	1.93	0.00	0.00	0.01	0.00
47.15	1.93	0.00	0.00	0.01	0.00	47.16	1.93	0.00	0.00	0.01	0.00
47.17	1.94	0.00	0.00	0.01	0.00	47.18	1.95	0.00	0.00	0.01	0.00
47.19	1.97	0.00	0.00	0.01	0.00	47.20	1.98	0.00	0.00	0.01	0.00
47.21	1.99	0.00	0.00	0.01	0.00	47.22	2.00	0.00	0.00	0.01	0.00
47.23	2.00	0.00	0.00	0.01	0.00	47.24	2.00	0.00	0.00	0.01	0.00
47.25	2.00	0.00	0.00	0.01	0.00	47.26	2.00	0.00	0.00	0.01	0.00
47.27	2.00	0.00	0.00	0.01	0.00	47.28	2.00	0.00	0.00	0.01	0.00
47.29	2.00	0.00	0.00	0.01	0.00	47.30	2.00	0.00	0.00	0.01	0.00
47.31	2.00	0.00	0.00	0.01	0.00	47.32	2.00	0.00	0.00	0.01	0.00
47.33	2.00	0.00	0.00	0.01	0.00	47.34	2.00	0.00	0.00	0.01	0.00
47.35	2.00	0.00	0.00	0.01	0.00	47.36	2.00	0.00	0.00	0.01	0.00
47.37	2.00	0.00	0.00	0.01	0.00	47.38	2.00	0.00	0.00	0.01	0.00
47.39	2.00	0.00	0.00	0.01	0.00	47.40	2.00	0.00	0.00	0.01	0.00
47.41	2.00	0.00	0.00	0.01	0.00	47.42	2.00	0.00	0.00	0.01	0.00
47.43	2.00	0.00	0.00	0.01	0.00	47.44	2.00	0.00	0.00	0.01	0.00
47.45	2.00	0.00	0.00	0.01	0.00	47.46	2.00	0.00	0.00	0.01	0.00
47.47	2.00	0.00	0.00	0.01	0.00	47.48	2.00	0.00	0.00	0.01	0.00
47.49	2.00	0.00	0.00	0.01	0.00	47.50	2.00	0.00	0.00	0.01	0.00
47.51	2.00	0.00	0.00	0.01	0.00	47.52	2.00	0.00	0.00	0.01	0.00
47.53	2.00	0.00	0.00	0.01	0.00	47.54	0.99	0.00	0.00	0.01	0.00
47.55	0.90	0.00	0.00	0.01	0.00	47.56	0.83	0.00	0.00	0.01	0.00
47.57	0.77	0.00	0.00	0.01	0.00	47.58	0.72	0.00	0.00	0.01	0.00
47.59	0.69	0.00	0.00	0.01	0.00	47.60	0.66	0.00	0.00	0.01	0.00
47.61	0.63	0.00	0.00	0.01	0.00	47.62	0.59	0.00	0.00	0.01	0.00
47.63	0.56	0.00	0.00	0.01	0.00	47.64	0.53	0.00	0.00	0.01	0.00
47.65	0.50	0.00	0.00	0.01	0.00	47.66	0.48	0.00	0.00	0.01	0.00
47.67	0.46	0.00	0.00	0.01	0.00	47.68	0.44	0.00	0.00	0.01	0.00
47.69	0.41	0.00	0.00	0.01	0.00	47.70	0.38	0.00	0.00	0.01	0.01
47.71	0.36	0.00	0.00	0.01	0.01	47.72	0.38	0.00	0.00	0.01	0.01
47.73	0.38	0.00	0.00	0.01	0.01	47.74	0.37	0.00	0.00	0.01	0.01
47.75	0.37	0.00	0.00	0.01	0.01	47.76	0.37	0.00	0.00	0.01	0.01
47.77	0.37	0.00	0.00	0.01	0.01	47.78	0.36	0.00	0.00	0.01	0.01
47.79	0.36	0.00	0.00	0.01	0.01	47.80	0.35	0.00	0.00	0.01	0.01
47.81	0.35	0.00	0.00	0.01	0.01	47.82	0.34	0.00	0.00	0.01	0.01
47.83	0.34	0.00	0.00	0.01	0.01	47.84	0.34	0.00	0.00	0.01	0.01
47.85	0.33	0.00	0.00	0.01	0.01	47.86	0.33	0.00	0.00	0.01	0.01
47.87	0.33	0.00	0.00	0.01	0.01	47.88	0.33	0.00	0.00	0.01	0.01
47.89	0.33	0.00	0.00	0.01	0.01	47.90	0.32	0.00	0.00	0.01	0.01
47.91	0.32	0.00	0.00	0.01	0.01	47.92	0.32	0.00	0.00	0.01	0.01
47.93	0.32	0.00	0.00	0.01	0.01	47.94	0.32	0.00	0.00	0.01	0.01
47.95	0.33	0.00	0.00	0.01	0.01	47.96	0.33	0.00	0.00	0.01	0.01
47.97	0.31	0.00	0.00	0.01	0.01	47.98	0.33	0.00	0.00	0.01	0.01
47.99	0.36	0.00	0.00	0.01	0.01	48.00	0.38	0.00	0.00	0.01	0.01

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
48.01	0.41	0.00	0.00	0.01	0.00	48.02	0.45	0.00	0.00	0.01	0.00
48.03	0.49	0.00	0.00	0.01	0.00	48.04	0.56	0.00	0.00	0.01	0.00
48.05	0.64	0.00	0.00	0.01	0.00	48.06	0.75	0.00	0.00	0.01	0.00
48.07	0.86	0.00	0.00	0.01	0.00	48.08	0.99	0.00	0.00	0.01	0.00
48.09	2.00	0.00	0.00	0.01	0.00	48.10	2.00	0.00	0.00	0.01	0.00
48.11	2.00	0.00	0.00	0.01	0.00	48.12	2.00	0.00	0.00	0.01	0.00
48.13	2.00	0.00	0.00	0.01	0.00	48.14	2.00	0.00	0.00	0.01	0.00
48.15	2.00	0.00	0.00	0.01	0.00	48.16	2.00	0.00	0.00	0.01	0.00
48.17	2.00	0.00	0.00	0.01	0.00	48.18	2.00	0.00	0.00	0.01	0.00
48.19	2.00	0.00	0.00	0.01	0.00	48.20	2.00	0.00	0.00	0.01	0.00
48.21	2.00	0.00	0.00	0.01	0.00	48.22	2.00	0.00	0.00	0.01	0.00
48.23	2.00	0.00	0.00	0.01	0.00	48.24	2.00	0.00	0.00	0.01	0.00
48.25	2.00	0.00	0.00	0.01	0.00	48.26	2.00	0.00	0.00	0.01	0.00
48.27	2.00	0.00	0.00	0.01	0.00	48.28	2.00	0.00	0.00	0.01	0.00
48.29	2.00	0.00	0.00	0.01	0.00	48.30	2.00	0.00	0.00	0.01	0.00
48.31	2.00	0.00	0.00	0.01	0.00	48.32	2.00	0.00	0.00	0.01	0.00
48.33	2.00	0.00	0.00	0.01	0.00	48.34	2.00	0.00	0.00	0.01	0.00
48.35	2.00	0.00	0.00	0.01	0.00	48.36	2.00	0.00	0.00	0.01	0.00
48.37	2.00	0.00	0.00	0.01	0.00	48.38	2.00	0.00	0.00	0.01	0.00
48.39	2.00	0.00	0.00	0.01	0.00	48.40	2.00	0.00	0.00	0.01	0.00
48.41	2.00	0.00	0.00	0.01	0.00	48.42	2.00	0.00	0.00	0.01	0.00
48.43	2.00	0.00	0.00	0.01	0.00	48.44	2.00	0.00	0.00	0.01	0.00
48.45	2.00	0.00	0.00	0.01	0.00	48.46	2.00	0.00	0.00	0.01	0.00
48.47	2.00	0.00	0.00	0.01	0.00	48.48	2.00	0.00	0.00	0.01	0.00
48.49	2.00	0.00	0.00	0.01	0.00	48.50	2.00	0.00	0.00	0.01	0.00
48.51	2.00	0.00	0.00	0.01	0.00	48.52	2.00	0.00	0.00	0.01	0.00
48.53	2.00	0.00	0.00	0.01	0.00	48.54	0.26	0.74	0.30	0.01	0.01
48.55	0.27	0.73	0.31	0.01	0.01	48.56	0.27	0.73	0.31	0.01	0.01
48.57	0.27	0.73	0.31	0.01	0.01	48.58	0.27	0.73	0.31	0.01	0.01
48.59	0.27	0.73	0.31	0.01	0.01	48.60	0.27	0.73	0.31	0.01	0.01
48.61	0.28	0.72	0.31	0.01	0.01	48.62	2.00	0.00	0.00	0.01	0.00
48.63	2.00	0.00	0.00	0.01	0.00	48.64	2.00	0.00	0.00	0.01	0.00
48.65	2.00	0.00	0.00	0.01	0.00	48.66	2.00	0.00	0.00	0.01	0.00
48.67	2.00	0.00	0.00	0.01	0.00	48.68	2.00	0.00	0.00	0.01	0.00
48.69	2.00	0.00	0.00	0.01	0.00	48.70	2.00	0.00	0.00	0.01	0.00
48.71	2.00	0.00	0.00	0.01	0.00	48.72	2.00	0.00	0.00	0.01	0.00
48.73	2.00	0.00	0.00	0.01	0.00	48.74	2.00	0.00	0.00	0.01	0.00
48.75	2.00	0.00	0.00	0.01	0.00	48.76	2.00	0.00	0.00	0.01	0.00
48.77	2.00	0.00	0.00	0.01	0.00	48.78	2.00	0.00	0.00	0.01	0.00
48.79	2.00	0.00	0.00	0.01	0.00	48.80	2.00	0.00	0.00	0.01	0.00
48.81	2.00	0.00	0.00	0.01	0.00	48.82	2.00	0.00	0.00	0.01	0.00
48.83	2.00	0.00	0.00	0.01	0.00	48.84	2.00	0.00	0.00	0.01	0.00
48.85	2.00	0.00	0.00	0.01	0.00	48.86	2.00	0.00	0.00	0.01	0.00
48.87	2.00	0.00	0.00	0.01	0.00	48.88	2.00	0.00	0.00	0.01	0.00
48.89	2.00	0.00	0.00	0.01	0.00	48.90	2.00	0.00	0.00	0.01	0.00
48.91	2.00	0.00	0.00	0.01	0.00	48.92	2.00	0.00	0.00	0.01	0.00
48.93	2.00	0.00	0.00	0.01	0.00	48.94	2.00	0.00	0.00	0.01	0.00
48.95	2.00	0.00	0.00	0.01	0.00	48.96	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
48.97	2.00	0.00	0.00	0.01	0.00	48.98	2.00	0.00	0.00	0.01	0.00
48.99	2.00	0.00	0.00	0.01	0.00	49.00	2.00	0.00	0.00	0.01	0.00
49.01	2.00	0.00	0.00	0.01	0.00	49.02	2.00	0.00	0.00	0.01	0.00
49.03	2.00	0.00	0.00	0.01	0.00	49.04	2.00	0.00	0.00	0.01	0.00
49.05	2.00	0.00	0.00	0.01	0.00	49.06	2.00	0.00	0.00	0.01	0.00
49.07	2.00	0.00	0.00	0.01	0.00	49.08	2.00	0.00	0.00	0.01	0.00
49.09	2.00	0.00	0.00	0.01	0.00	49.10	2.00	0.00	0.00	0.01	0.00
49.11	2.00	0.00	0.00	0.01	0.00	49.12	2.00	0.00	0.00	0.01	0.00
49.13	2.00	0.00	0.00	0.01	0.00	49.14	2.00	0.00	0.00	0.01	0.00
49.15	2.00	0.00	0.00	0.01	0.00	49.16	2.00	0.00	0.00	0.01	0.00
49.17	2.00	0.00	0.00	0.01	0.00	49.18	2.00	0.00	0.00	0.01	0.00
49.19	2.00	0.00	0.00	0.01	0.00	49.20	2.00	0.00	0.00	0.01	0.00
49.21	2.00	0.00	0.00	0.01	0.00	49.22	2.00	0.00	0.00	0.01	0.00
49.23	2.00	0.00	0.00	0.01	0.00	49.24	2.00	0.00	0.00	0.01	0.00
49.25	2.00	0.00	0.00	0.01	0.00	49.26	2.00	0.00	0.00	0.01	0.00
49.27	2.00	0.00	0.00	0.01	0.00	49.28	2.00	0.00	0.00	0.01	0.00
49.29	2.00	0.00	0.00	0.01	0.00	49.30	2.00	0.00	0.00	0.01	0.00
49.31	2.00	0.00	0.00	0.01	0.00	49.32	2.00	0.00	0.00	0.01	0.00
49.33	2.00	0.00	0.00	0.01	0.00	49.34	2.00	0.00	0.00	0.01	0.00
49.35	2.00	0.00	0.00	0.01	0.00	49.36	2.00	0.00	0.00	0.01	0.00
49.37	2.00	0.00	0.00	0.01	0.00	49.38	2.00	0.00	0.00	0.01	0.00
49.39	2.00	0.00	0.00	0.01	0.00	49.40	2.00	0.00	0.00	0.01	0.00
49.41	0.56	0.00	0.00	0.01	0.00	49.42	0.57	0.00	0.00	0.01	0.00
49.43	0.57	0.00	0.00	0.01	0.00	49.44	0.58	0.00	0.00	0.01	0.00
49.45	0.59	0.00	0.00	0.01	0.00	49.46	0.60	0.00	0.00	0.01	0.00
49.47	0.61	0.00	0.00	0.01	0.00	49.48	0.61	0.00	0.00	0.01	0.00
49.49	0.61	0.00	0.00	0.01	0.00	49.50	0.61	0.00	0.00	0.01	0.00
49.51	0.60	0.00	0.00	0.01	0.00	49.52	0.59	0.00	0.00	0.01	0.00
49.53	0.58	0.00	0.00	0.01	0.00	49.54	0.58	0.00	0.00	0.01	0.00
49.55	0.57	0.00	0.00	0.01	0.00	49.56	0.56	0.00	0.00	0.01	0.00
49.57	0.55	0.00	0.00	0.01	0.00	49.58	0.55	0.00	0.00	0.01	0.00
49.59	0.54	0.00	0.00	0.01	0.00	49.60	0.53	0.00	0.00	0.01	0.00
49.61	0.51	0.00	0.00	0.01	0.00	49.62	0.50	0.00	0.00	0.01	0.00
49.63	0.49	0.00	0.00	0.01	0.00	49.64	0.48	0.00	0.00	0.01	0.00
49.65	0.47	0.00	0.00	0.01	0.00	49.66	0.47	0.00	0.00	0.01	0.00
49.67	0.46	0.00	0.00	0.01	0.00	49.68	0.46	0.00	0.00	0.01	0.00
49.69	0.46	0.00	0.00	0.01	0.00	49.70	0.46	0.00	0.00	0.01	0.00
49.71	0.45	0.00	0.00	0.01	0.00	49.72	0.45	0.00	0.00	0.01	0.00
49.73	0.45	0.00	0.00	0.01	0.00	49.74	0.45	0.00	0.00	0.01	0.00
49.75	0.45	0.00	0.00	0.01	0.00	49.76	0.44	0.00	0.00	0.01	0.00
49.77	0.44	0.00	0.00	0.01	0.00	49.78	0.44	0.00	0.00	0.01	0.00
49.79	0.44	0.00	0.00	0.01	0.00	49.80	0.44	0.00	0.00	0.01	0.00
49.81	0.43	0.00	0.00	0.01	0.00	49.82	0.43	0.00	0.00	0.01	0.00
49.83	0.43	0.00	0.00	0.01	0.00	49.84	0.43	0.00	0.00	0.01	0.00
49.85	0.43	0.00	0.00	0.01	0.00	49.86	0.43	0.00	0.00	0.01	0.00
49.87	0.43	0.00	0.00	0.01	0.00	49.88	0.42	0.00	0.00	0.01	0.00
49.89	0.42	0.00	0.00	0.01	0.00	49.90	0.42	0.00	0.00	0.01	0.00
49.91	0.42	0.00	0.00	0.01	0.00	49.92	0.42	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
49.93	0.42	0.00	0.00	0.01	0.00	49.94	0.42	0.00	0.00	0.01	0.00
49.95	0.42	0.00	0.00	0.01	0.00	49.96	0.42	0.00	0.00	0.01	0.00
49.97	0.42	0.00	0.00	0.01	0.00	49.98	0.42	0.00	0.00	0.01	0.00
49.99	0.41	0.00	0.00	0.01	0.00	50.00	0.41	0.00	0.00	0.01	0.00

Overall liquefaction potential: 19.48

LPI = 0.00 - Liquefaction risk very low

LPI between 0.00 and 5.00 - Liquefaction risk low

LPI between 5.00 and 15.00 - Liquefaction risk high

LPI > 15.00 - Liquefaction risk very high

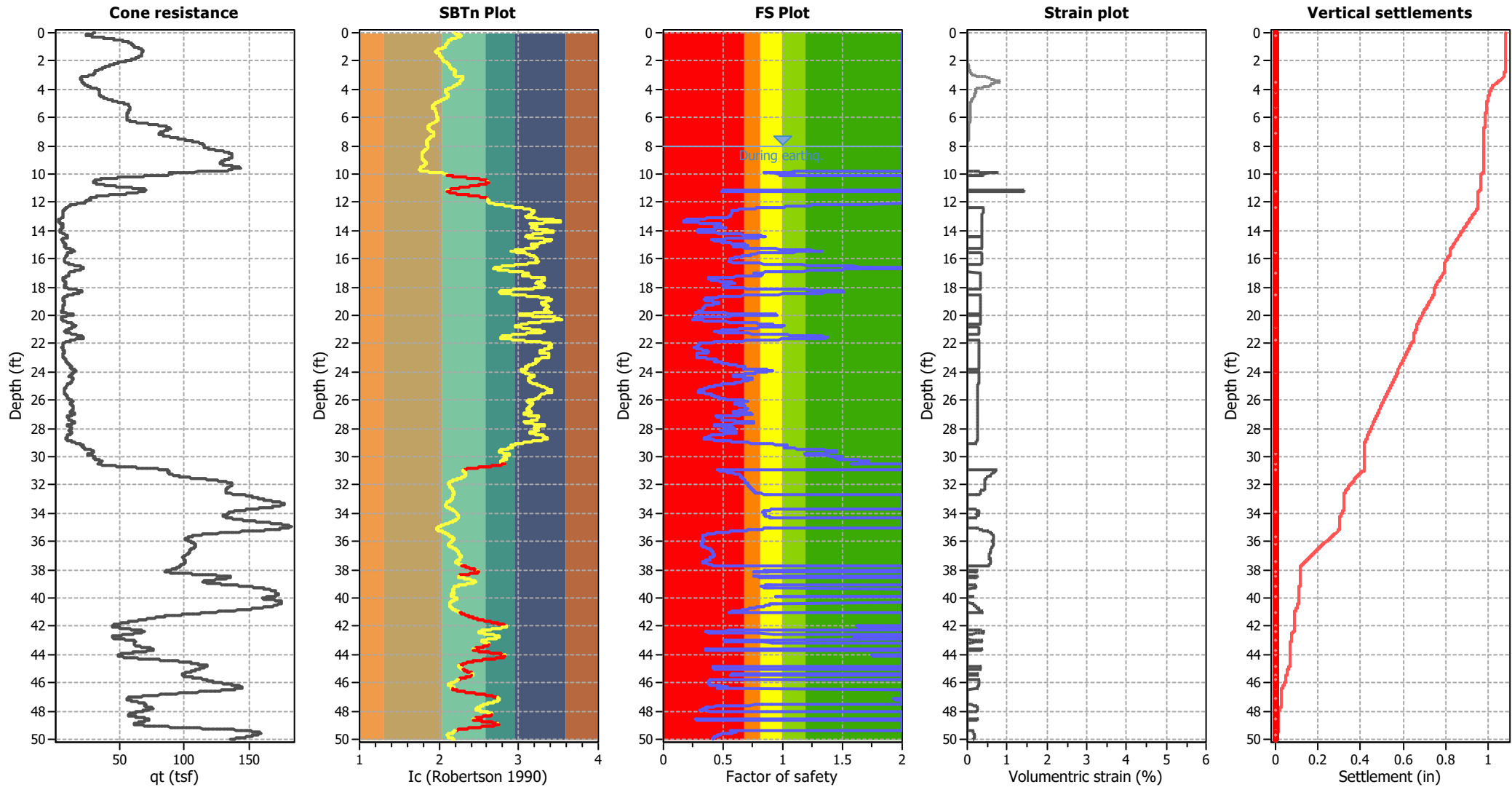
Abbreviations

FS: Calculated factor of safety for test point

F_L: 1 - FSw_z: Function value of the extend of soil liquefaction according to depthd_z: Layer thickness (ft)

LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

- q_c : Total cone resistance (cone resistance q_c corrected for pore water effects)
- I_c : Soil Behaviour Type Index
- FS: Calculated Factor of Safety against liquefaction
- Volumetric strain: Post-liquefaction volumetric strain

:: Post-earthquake settlement of dry sands ::												
Depth (ft)	Ic	Q _{tn}	Kc	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _r (%)	Settle. (in)
0.01	2.20	58.42	1.61	93.96	21	450	0.59	0.000	0.00	13.69	0.00	0.000
0.02	2.19	58.11	1.60	93.07	21	446	0.59	0.000	0.00	13.69	0.00	0.000
0.03	2.19	57.69	1.59	91.83	21	440	0.59	0.000	0.00	13.69	0.00	0.000
0.04	2.19	57.15	1.59	90.71	20	435	0.59	0.000	0.00	13.69	0.00	0.000
0.05	2.19	56.30	1.59	89.54	20	429	0.59	0.000	0.00	13.69	0.00	0.000
0.06	2.19	55.05	1.60	88.15	20	422	0.59	0.000	0.00	13.69	0.00	0.000
0.07	2.20	53.49	1.62	86.52	20	414	0.59	0.001	0.00	13.69	0.00	0.000
0.08	2.21	51.78	1.64	84.76	19	404	0.59	0.001	0.00	13.69	0.00	0.000
0.09	2.22	50.01	1.66	82.96	19	395	0.59	0.001	0.00	13.69	0.00	0.000
0.10	2.23	48.28	1.68	81.21	19	385	0.59	0.001	0.00	13.69	0.00	0.000
0.11	2.23	46.66	1.71	79.61	18	376	0.59	0.001	0.00	13.69	0.00	0.000
0.12	2.24	45.26	1.73	78.24	18	368	0.59	0.001	0.00	13.69	0.00	0.000
0.13	2.25	44.48	1.75	77.73	18	365	0.59	0.001	0.00	13.69	0.00	0.000
0.14	2.25	44.29	1.76	78.09	18	366	0.59	0.001	0.00	13.69	0.00	0.000
0.15	2.26	44.58	1.78	79.27	18	370	0.59	0.001	0.00	13.69	0.00	0.000
0.16	2.26	44.92	1.79	80.62	19	376	0.59	0.001	0.00	13.69	0.00	0.000
0.17	2.27	45.28	1.81	82.08	19	381	0.59	0.002	0.00	13.69	0.00	0.000
0.18	2.27	45.65	1.83	83.57	19	387	0.59	0.002	0.00	13.69	0.00	0.000
0.19	2.28	46.01	1.85	85.01	20	392	0.59	0.002	0.00	13.69	0.00	0.000
0.20	2.28	46.33	1.86	86.33	20	397	0.59	0.002	0.00	13.69	0.00	0.000
0.21	2.29	46.70	1.87	87.52	20	402	0.59	0.002	0.00	13.69	0.00	0.000
0.22	2.29	47.34	1.88	88.80	21	408	0.59	0.002	0.00	13.69	0.00	0.000
0.23	2.28	48.37	1.87	90.35	21	416	0.59	0.002	0.00	13.69	0.00	0.000
0.24	2.28	49.76	1.85	92.28	22	426	0.59	0.002	0.00	13.69	0.00	0.000
0.25	2.28	51.31	1.84	94.45	22	437	0.59	0.002	0.00	13.69	0.00	0.000
0.26	2.27	52.95	1.83	96.76	23	448	0.59	0.002	0.00	13.69	0.00	0.000
0.27	2.27	54.58	1.82	99.07	23	460	0.59	0.002	0.00	13.69	0.00	0.000
0.28	2.27	56.13	1.80	101.29	23	471	0.59	0.002	0.00	13.69	0.00	0.000
0.29	2.26	57.51	1.80	103.27	24	481	0.59	0.002	0.00	13.69	0.00	0.000
0.30	2.26	58.72	1.79	104.90	24	489	0.59	0.002	0.00	13.69	0.00	0.000
0.31	2.26	59.92	1.77	106.31	25	497	0.59	0.002	0.00	13.69	0.00	0.000
0.32	2.25	61.27	1.76	107.71	25	505	0.59	0.002	0.00	13.69	0.00	0.000
0.33	2.25	62.86	1.74	109.31	25	514	0.59	0.002	0.00	13.69	0.00	0.000
0.34	2.24	64.61	1.72	111.08	25	524	0.59	0.002	0.00	13.69	0.00	0.000
0.35	2.23	66.40	1.70	112.92	26	534	0.59	0.002	0.00	13.69	0.00	0.000
0.36	2.23	68.17	1.68	114.75	26	544	0.59	0.002	0.00	13.69	0.00	0.000
0.37	2.22	69.81	1.67	116.47	26	553	0.59	0.002	0.00	13.69	0.00	0.000
0.38	2.22	71.24	1.66	117.97	27	561	0.59	0.002	0.00	13.69	0.00	0.000
0.39	2.21	72.50	1.64	119.18	27	568	0.59	0.002	0.00	13.69	0.00	0.000
0.40	2.21	73.76	1.63	120.26	27	574	0.59	0.002	0.00	13.69	0.00	0.000
0.41	2.20	75.19	1.61	121.37	27	581	0.59	0.002	0.00	13.69	0.00	0.000
0.42	2.19	76.83	1.60	122.67	28	588	0.59	0.002	0.00	13.69	0.00	0.000
0.43	2.19	78.59	1.58	124.07	28	596	0.59	0.002	0.00	13.69	0.00	0.000
0.44	2.18	80.37	1.56	125.52	28	603	0.59	0.002	0.00	13.69	0.00	0.000
0.45	2.17	82.09	1.55	126.93	28	611	0.59	0.003	0.00	13.69	0.00	0.000
0.46	2.16	83.66	1.53	128.24	28	617	0.59	0.003	0.00	13.69	0.00	0.000
0.47	2.16	84.98	1.52	129.36	29	623	0.59	0.003	0.00	13.69	0.00	0.000
0.48	2.16	86.13	1.51	130.41	29	628	0.59	0.003	0.00	13.69	0.00	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	Ic	Q _{tn}	Kc	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _r (%)	Settle. (in)
0.49	2.15	87.26	1.51	131.53	29	634	0.59	0.003	0.00	13.69	0.00	0.000
0.50	2.15	88.55	1.50	132.83	29	640	0.59	0.003	0.00	13.69	0.00	0.000
0.51	2.14	89.98	1.49	134.29	30	647	0.59	0.003	0.00	13.69	0.00	0.000
0.52	2.14	91.48	1.48	135.84	30	655	0.59	0.003	0.00	13.69	0.00	0.000
0.53	2.14	92.99	1.48	137.39	30	662	0.59	0.003	0.00	13.69	0.00	0.000
0.54	2.13	94.41	1.47	138.87	30	669	0.59	0.003	0.00	13.69	0.00	0.000
0.55	2.13	95.67	1.47	140.19	31	675	0.59	0.003	0.00	13.69	0.00	0.000
0.56	2.13	96.70	1.46	141.28	31	680	0.59	0.003	0.00	13.69	0.00	0.000
0.57	2.12	97.59	1.46	142.26	31	685	0.59	0.003	0.00	13.69	0.00	0.000
0.58	2.12	98.45	1.46	143.26	31	690	0.59	0.003	0.00	13.69	0.00	0.000
0.59	2.12	99.44	1.45	144.41	32	695	0.59	0.003	0.00	13.69	0.00	0.000
0.60	2.12	100.51	1.45	145.66	32	701	0.59	0.003	0.00	13.69	0.00	0.000
0.61	2.12	101.62	1.45	146.96	32	707	0.59	0.003	0.00	13.69	0.00	0.000
0.62	2.12	102.71	1.44	148.24	32	713	0.59	0.003	0.00	13.69	0.00	0.000
0.63	2.11	103.72	1.44	149.43	33	718	0.59	0.003	0.00	13.69	0.00	0.000
0.64	2.11	104.59	1.44	150.45	33	723	0.59	0.003	0.00	13.69	0.00	0.000
0.65	2.11	105.24	1.44	151.21	33	727	0.59	0.003	0.00	13.69	0.00	0.000
0.66	2.11	105.74	1.44	151.78	33	729	0.59	0.003	0.00	13.69	0.00	0.000
0.67	2.11	106.19	1.43	152.28	33	732	0.59	0.003	0.00	13.69	0.00	0.000
0.68	2.11	106.70	1.43	152.85	33	734	0.59	0.003	0.00	13.69	0.00	0.000
0.69	2.11	107.24	1.43	153.46	33	737	0.59	0.003	0.00	13.69	0.00	0.000
0.70	2.11	107.80	1.43	154.08	33	740	0.59	0.003	0.00	13.69	0.00	0.000
0.71	2.11	108.33	1.43	154.67	34	743	0.59	0.003	0.00	13.69	0.00	0.000
0.72	2.11	108.81	1.43	155.21	34	745	0.59	0.003	0.00	13.69	0.00	0.000
0.73	2.10	109.20	1.43	155.64	34	747	0.59	0.003	0.00	13.69	0.00	0.000
0.74	2.10	109.49	1.42	155.93	34	748	0.59	0.003	0.00	13.69	0.00	0.000
0.75	2.10	109.71	1.42	156.11	34	749	0.59	0.004	0.00	13.69	0.00	0.000
0.76	2.10	109.92	1.42	156.25	34	749	0.59	0.004	0.00	13.69	0.00	0.000
0.77	2.10	110.16	1.42	156.41	34	750	0.59	0.004	0.00	13.69	0.00	0.000
0.78	2.10	110.41	1.42	156.58	34	751	0.59	0.004	0.00	13.69	0.00	0.000
0.79	2.10	110.66	1.42	156.75	34	751	0.59	0.004	0.00	13.69	0.00	0.000
0.80	2.10	110.90	1.41	156.91	34	752	0.59	0.004	0.00	13.69	0.00	0.000
0.81	2.10	111.11	1.41	157.05	34	752	0.59	0.004	0.00	13.69	0.00	0.000
0.82	2.10	111.28	1.41	157.16	34	753	0.59	0.004	0.00	13.69	0.00	0.000
0.83	2.09	111.43	1.41	157.22	34	753	0.59	0.004	0.00	13.69	0.00	0.000
0.84	2.09	111.59	1.41	157.27	34	753	0.59	0.004	0.00	13.69	0.00	0.000
0.85	2.09	111.77	1.41	157.31	34	753	0.59	0.004	0.00	13.69	0.00	0.000
0.86	2.09	111.96	1.41	157.35	34	753	0.59	0.004	0.00	13.69	0.00	0.000
0.87	2.09	112.16	1.40	157.40	34	753	0.59	0.004	0.00	13.69	0.00	0.000
0.88	2.09	112.36	1.40	157.45	34	753	0.59	0.004	0.00	13.69	0.00	0.000
0.89	2.09	112.54	1.40	157.50	34	752	0.59	0.004	0.00	13.69	0.00	0.000
0.90	2.09	112.70	1.40	157.54	34	752	0.59	0.004	0.00	13.69	0.00	0.000
0.91	2.08	112.86	1.40	157.60	34	752	0.59	0.004	0.00	13.69	0.00	0.000
0.92	2.08	113.06	1.39	157.69	34	753	0.59	0.004	0.00	13.69	0.00	0.000
0.93	2.08	113.30	1.39	157.81	34	753	0.59	0.005	0.00	13.69	0.00	0.000
0.94	2.08	113.58	1.39	157.96	34	753	0.59	0.005	0.00	13.69	0.00	0.000
0.95	2.08	113.87	1.39	158.11	34	753	0.59	0.005	0.00	13.69	0.00	0.000
0.96	2.08	114.18	1.39	158.27	34	754	0.59	0.005	0.00	13.69	0.00	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	Ic	Q _{tn}	Kc	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _r (%)	Settle. (in)
0.97	2.07	114.47	1.38	158.42	34	754	0.59	0.005	0.00	13.69	0.00	0.000
0.98	2.07	114.73	1.38	158.56	34	754	0.59	0.005	0.00	13.69	0.00	0.000
0.99	2.07	114.99	1.38	158.71	34	755	0.59	0.005	0.00	13.69	0.00	0.000
1.00	2.07	115.36	1.38	158.93	34	755	0.59	0.005	0.00	13.69	0.00	0.000
1.01	2.07	115.88	1.37	159.26	34	756	0.59	0.005	0.00	13.69	0.00	0.000
1.02	2.06	116.55	1.37	159.71	34	757	0.59	0.005	0.00	13.69	0.00	0.000
1.03	2.06	117.29	1.37	160.20	34	758	0.59	0.005	0.00	13.69	0.00	0.000
1.04	2.06	118.08	1.36	160.73	34	759	0.59	0.005	0.00	13.69	0.00	0.000
1.05	2.05	118.86	1.36	161.26	34	760	0.59	0.005	0.00	13.69	0.00	0.000
1.06	2.05	119.59	1.35	161.76	34	762	0.59	0.005	0.00	13.69	0.00	0.000
1.07	2.04	120.24	1.35	162.21	34	762	0.59	0.005	0.00	13.69	0.00	0.000
1.08	2.04	120.79	1.35	162.56	34	763	0.59	0.005	0.00	13.69	0.00	0.000
1.09	2.04	121.29	1.34	162.85	34	763	0.59	0.005	0.00	13.69	0.00	0.000
1.10	2.03	121.82	1.34	163.10	34	763	0.59	0.005	0.00	13.69	0.00	0.000
1.11	2.03	122.42	1.33	163.38	34	762	0.59	0.006	0.00	13.69	0.00	0.000
1.12	2.03	123.08	1.33	163.70	34	762	0.59	0.006	0.00	13.69	0.00	0.000
1.13	2.02	123.76	1.33	164.03	34	761	0.59	0.006	0.00	13.69	0.00	0.000
1.14	2.02	124.43	1.32	164.37	34	761	0.59	0.006	0.00	13.69	0.00	0.000
1.15	2.01	125.04	1.32	164.68	34	760	0.59	0.006	0.00	13.69	0.00	0.000
1.16	2.01	125.57	1.31	164.95	34	760	0.59	0.006	0.00	13.69	0.00	0.000
1.17	2.00	125.98	1.31	165.12	34	759	0.59	0.006	0.00	13.69	0.00	0.000
1.18	2.00	126.33	1.31	165.20	34	758	0.59	0.006	0.00	13.69	0.00	0.000
1.19	2.00	126.68	1.30	165.22	34	756	0.59	0.006	0.00	13.69	0.00	0.000
1.20	1.99	127.07	1.30	165.25	34	754	0.59	0.006	0.00	13.69	0.00	0.000
1.21	1.99	127.48	1.30	165.29	34	751	0.59	0.006	0.00	13.69	0.00	0.000
1.22	1.98	127.90	1.29	165.33	34	749	0.59	0.006	0.00	13.69	0.00	0.000
1.23	1.98	128.31	1.29	165.38	34	747	0.59	0.006	0.00	13.69	0.00	0.000
1.24	1.97	128.68	1.29	165.42	34	744	0.59	0.007	0.00	13.69	0.00	0.000
1.25	1.97	128.96	1.28	165.45	34	743	0.59	0.007	0.00	13.69	0.00	0.000
1.26	1.97	129.12	1.28	165.43	34	741	0.59	0.007	0.00	13.69	0.00	0.000
1.27	1.96	129.18	1.28	165.39	34	740	0.59	0.007	0.00	13.69	0.00	0.000
1.28	1.96	129.20	1.28	165.31	34	740	0.59	0.007	0.00	13.69	0.00	0.000
1.29	1.96	129.22	1.28	165.23	34	738	0.59	0.007	0.00	13.69	0.00	0.000
1.30	1.96	129.24	1.28	165.14	34	737	0.59	0.007	0.00	13.69	0.00	0.000
1.31	1.96	129.27	1.28	165.05	34	736	0.59	0.007	0.00	13.69	0.00	0.000
1.32	1.96	129.29	1.28	164.97	34	735	0.59	0.007	0.00	13.69	0.00	0.000
1.33	1.96	129.31	1.28	164.90	34	734	0.59	0.007	0.00	13.69	0.00	0.000
1.34	1.96	129.26	1.28	164.81	34	734	0.59	0.007	0.00	13.69	0.00	0.000
1.35	1.96	129.09	1.28	164.70	34	734	0.59	0.008	0.00	13.69	0.00	0.000
1.36	1.96	128.80	1.28	164.55	34	735	0.59	0.008	0.00	13.69	0.00	0.000
1.37	1.96	128.43	1.28	164.37	34	736	0.59	0.008	0.00	13.69	0.00	0.000
1.38	1.97	128.04	1.28	164.17	34	736	0.59	0.008	0.00	13.69	0.00	0.000
1.39	1.97	127.64	1.28	163.97	34	737	0.59	0.008	0.00	13.69	0.00	0.000
1.40	1.97	127.24	1.29	163.77	34	738	0.59	0.008	0.00	13.69	0.00	0.000
1.41	1.98	126.88	1.29	163.59	34	739	0.59	0.008	0.00	13.69	0.00	0.000
1.42	1.98	126.57	1.29	163.44	34	739	0.59	0.008	0.00	13.69	0.00	0.000
1.43	1.98	126.38	1.29	163.40	34	740	0.59	0.008	0.00	13.69	0.00	0.000
1.44	1.98	126.29	1.29	163.47	34	742	0.59	0.008	0.00	13.69	0.00	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	Ic	Q _{tn}	Kc	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _r (%)	Settle. (in)
1.45	1.99	126.27	1.30	163.64	34	743	0.59	0.008	0.00	13.69	0.00	0.000
1.46	1.99	126.24	1.30	163.83	34	745	0.59	0.008	0.00	13.69	0.00	0.000
1.47	1.99	126.22	1.30	164.03	34	747	0.59	0.008	0.00	13.69	0.00	0.000
1.48	1.99	126.19	1.30	164.24	34	750	0.59	0.008	0.00	13.69	0.00	0.000
1.49	2.00	126.17	1.30	164.44	34	752	0.59	0.008	0.00	13.69	0.00	0.000
1.50	2.00	126.14	1.31	164.62	34	753	0.59	0.008	0.00	13.69	0.00	0.000
1.51	2.00	126.12	1.31	164.77	34	755	0.59	0.008	0.00	13.69	0.00	0.000
1.52	2.00	126.09	1.31	164.89	34	756	0.59	0.008	0.00	13.69	0.00	0.000
1.53	2.00	126.06	1.31	164.99	34	757	0.59	0.008	0.00	13.69	0.00	0.000
1.54	2.00	126.02	1.31	165.10	34	759	0.59	0.008	0.00	13.69	0.00	0.000
1.55	2.01	125.97	1.31	165.22	34	760	0.59	0.008	0.00	13.69	0.00	0.000
1.56	2.01	125.91	1.31	165.35	35	761	0.59	0.009	0.00	13.69	0.00	0.000
1.57	2.01	125.86	1.31	165.48	35	763	0.59	0.009	0.00	13.69	0.00	0.000
1.58	2.01	125.82	1.32	165.60	35	764	0.59	0.009	0.00	13.69	0.00	0.000
1.59	2.01	125.77	1.32	165.70	35	765	0.59	0.009	0.00	13.69	0.00	0.000
1.60	2.01	125.67	1.32	165.71	35	766	0.59	0.009	0.00	13.69	0.00	0.000
1.61	2.01	125.46	1.32	165.56	35	766	0.59	0.009	0.00	13.69	0.00	0.000
1.62	2.02	125.12	1.32	165.26	35	765	0.59	0.009	0.00	13.69	0.00	0.000
1.63	2.02	124.71	1.32	164.88	35	764	0.59	0.009	0.00	13.69	0.00	0.000
1.64	2.02	124.27	1.32	164.48	34	763	0.59	0.009	0.00	13.69	0.00	0.000
1.65	2.02	123.81	1.33	164.06	34	761	0.59	0.009	0.00	13.69	0.00	0.000
1.66	2.02	123.37	1.33	163.66	34	760	0.59	0.009	0.00	13.69	0.00	0.000
1.67	2.02	122.96	1.33	163.28	34	759	0.59	0.009	0.00	13.69	0.00	0.000
1.68	2.02	122.60	1.33	162.96	34	758	0.59	0.009	0.00	13.69	0.00	0.000
1.69	2.03	122.29	1.33	162.66	34	757	0.59	0.010	0.01	13.69	0.00	0.000
1.70	2.03	121.96	1.33	162.33	34	756	0.59	0.010	0.01	13.69	0.00	0.000
1.71	2.03	121.59	1.33	161.94	34	755	0.59	0.010	0.01	13.69	0.00	0.000
1.72	2.03	121.17	1.33	161.50	34	753	0.59	0.010	0.01	13.69	0.00	0.000
1.73	2.03	120.72	1.33	161.03	34	751	0.59	0.010	0.01	13.69	0.00	0.000
1.74	2.03	120.26	1.34	160.56	34	749	0.59	0.010	0.01	13.69	0.00	0.000
1.75	2.03	119.83	1.34	160.10	34	748	0.59	0.010	0.01	13.69	0.01	0.000
1.76	2.03	119.43	1.34	159.69	34	746	0.59	0.010	0.01	13.69	0.01	0.000
1.77	2.03	119.08	1.34	159.31	34	745	0.59	0.010	0.01	13.69	0.01	0.000
1.78	2.03	118.71	1.34	158.88	34	743	0.59	0.011	0.01	13.69	0.01	0.000
1.79	2.03	118.27	1.34	158.35	33	741	0.59	0.011	0.01	13.69	0.01	0.000
1.80	2.04	117.74	1.34	157.68	33	738	0.59	0.011	0.01	13.69	0.01	0.000
1.81	2.04	117.15	1.34	156.95	33	734	0.59	0.011	0.01	13.69	0.01	0.000
1.82	2.04	116.53	1.34	156.18	33	731	0.59	0.011	0.01	13.69	0.01	0.000
1.83	2.04	115.92	1.34	155.42	33	728	0.59	0.011	0.01	13.69	0.01	0.000
1.84	2.04	115.35	1.34	154.70	33	724	0.59	0.011	0.01	13.69	0.01	0.000
1.85	2.04	114.84	1.34	154.07	33	722	0.59	0.012	0.01	13.69	0.01	0.000
1.86	2.04	114.36	1.34	153.49	32	719	0.59	0.012	0.01	13.69	0.01	0.000
1.87	2.04	113.85	1.34	152.87	32	716	0.59	0.012	0.01	13.69	0.01	0.000
1.88	2.04	113.23	1.34	152.13	32	713	0.59	0.012	0.01	13.69	0.01	0.000
1.89	2.04	112.50	1.34	151.26	32	710	0.59	0.012	0.01	13.69	0.01	0.000
1.90	2.04	111.71	1.35	150.32	32	705	0.59	0.013	0.01	13.69	0.01	0.000
1.91	2.04	110.90	1.35	149.36	32	701	0.59	0.013	0.01	13.69	0.01	0.000
1.92	2.04	110.12	1.35	148.43	31	697	0.59	0.013	0.01	13.69	0.01	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	Ic	Q _{tn}	Kc	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _r (%)	Settle. (in)
1.93	2.04	109.39	1.35	147.57	31	694	0.59	0.013	0.01	13.69	0.01	0.000
1.94	2.05	108.76	1.35	146.82	31	690	0.59	0.014	0.01	13.69	0.01	0.000
1.95	2.05	108.15	1.35	146.14	31	688	0.59	0.014	0.01	13.69	0.01	0.000
1.96	2.05	107.48	1.35	145.44	31	685	0.59	0.014	0.01	13.69	0.01	0.000
1.97	2.05	106.68	1.36	144.63	31	682	0.59	0.014	0.01	13.69	0.01	0.000
1.98	2.05	105.78	1.36	143.70	31	678	0.59	0.014	0.01	13.69	0.01	0.000
1.99	2.06	104.81	1.36	142.73	30	674	0.59	0.015	0.01	13.69	0.01	0.000
2.00	2.06	103.84	1.37	141.74	30	671	0.59	0.015	0.01	13.69	0.01	0.000
2.01	2.06	102.91	1.37	140.81	30	667	0.59	0.015	0.01	13.69	0.01	0.000
2.02	2.06	102.07	1.37	139.96	30	664	0.59	0.015	0.01	13.69	0.01	0.000
2.03	2.07	101.33	1.37	139.23	30	661	0.59	0.016	0.01	13.69	0.01	0.000
2.04	2.07	100.59	1.38	138.49	30	658	0.59	0.016	0.01	13.69	0.01	0.000
2.05	2.07	99.75	1.38	137.65	29	654	0.59	0.016	0.01	13.69	0.01	0.000
2.06	2.07	98.75	1.38	136.65	29	650	0.59	0.017	0.01	13.69	0.01	0.000
2.07	2.08	97.64	1.39	135.56	29	646	0.59	0.017	0.01	13.69	0.01	0.000
2.08	2.08	96.48	1.39	134.42	29	641	0.59	0.017	0.01	13.69	0.01	0.000
2.09	2.09	95.33	1.40	133.29	29	637	0.59	0.018	0.01	13.69	0.01	0.000
2.10	2.09	94.25	1.40	132.24	29	632	0.59	0.018	0.01	13.69	0.01	0.000
2.11	2.09	93.30	1.41	131.32	28	628	0.59	0.018	0.01	13.69	0.01	0.000
2.12	2.09	92.52	1.41	130.54	28	625	0.59	0.019	0.01	13.69	0.01	0.000
2.13	2.10	91.82	1.41	129.80	28	622	0.59	0.019	0.01	13.69	0.01	0.000
2.14	2.10	91.11	1.42	129.01	28	618	0.59	0.020	0.01	13.69	0.01	0.000
2.15	2.10	90.29	1.42	128.09	28	614	0.59	0.020	0.01	13.69	0.01	0.000
2.16	2.10	89.40	1.42	127.10	28	610	0.59	0.020	0.01	13.69	0.01	0.000
2.17	2.10	88.49	1.42	126.09	27	605	0.59	0.021	0.01	13.69	0.01	0.000
2.18	2.11	87.60	1.43	125.11	27	601	0.59	0.021	0.01	13.69	0.01	0.000
2.19	2.11	86.79	1.43	124.20	27	596	0.59	0.022	0.02	13.69	0.01	0.000
2.20	2.11	86.09	1.43	123.44	27	593	0.59	0.022	0.02	13.69	0.01	0.000
2.21	2.11	85.51	1.44	122.79	27	590	0.59	0.023	0.02	13.69	0.01	0.000
2.22	2.11	84.98	1.44	122.18	27	587	0.59	0.023	0.02	13.69	0.02	0.000
2.23	2.11	84.40	1.44	121.52	26	584	0.59	0.024	0.02	13.69	0.02	0.000
2.24	2.12	83.75	1.44	120.78	26	581	0.59	0.024	0.02	13.69	0.02	0.000
2.25	2.12	83.06	1.44	119.99	26	577	0.59	0.025	0.02	13.69	0.02	0.000
2.26	2.12	82.37	1.45	119.20	26	573	0.59	0.025	0.02	13.69	0.02	0.000
2.27	2.12	81.70	1.45	118.44	26	570	0.59	0.026	0.02	13.69	0.02	0.000
2.28	2.12	81.10	1.45	117.76	26	567	0.59	0.027	0.02	13.69	0.02	0.000
2.29	2.12	80.60	1.45	117.18	26	564	0.59	0.027	0.02	13.69	0.02	0.000
2.30	2.12	80.14	1.46	116.65	25	562	0.59	0.028	0.02	13.69	0.02	0.000
2.31	2.12	79.66	1.46	116.10	25	559	0.59	0.028	0.02	13.69	0.02	0.000
2.32	2.13	79.11	1.46	115.47	25	556	0.59	0.029	0.02	13.69	0.02	0.000
2.33	2.13	78.49	1.46	114.77	25	553	0.59	0.029	0.02	13.69	0.02	0.000
2.34	2.13	77.86	1.46	114.04	25	549	0.59	0.030	0.02	13.69	0.02	0.000
2.35	2.13	77.23	1.47	113.32	25	546	0.59	0.031	0.02	13.69	0.02	0.000
2.36	2.13	76.64	1.47	112.65	25	543	0.59	0.031	0.02	13.69	0.02	0.000
2.37	2.13	76.12	1.47	112.06	25	540	0.59	0.032	0.03	13.69	0.02	0.000
2.38	2.13	75.69	1.47	111.56	24	537	0.59	0.033	0.03	13.69	0.02	0.000
2.39	2.13	75.30	1.48	111.11	24	535	0.59	0.033	0.03	13.69	0.02	0.000
2.40	2.14	74.89	1.48	110.62	24	533	0.59	0.034	0.03	13.69	0.02	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	Ic	Q _{tn}	Kc	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _r (%)	Settle. (in)
2.41	2.14	74.43	1.48	110.07	24	530	0.59	0.035	0.03	13.69	0.03	0.000
2.42	2.14	73.92	1.48	109.47	24	528	0.59	0.036	0.03	13.69	0.03	0.000
2.43	2.14	73.41	1.48	108.86	24	525	0.59	0.036	0.03	13.69	0.03	0.000
2.44	2.14	72.91	1.49	108.27	24	522	0.59	0.037	0.03	13.69	0.03	0.000
2.45	2.14	72.44	1.49	107.72	24	519	0.59	0.038	0.03	13.69	0.03	0.000
2.46	2.14	72.05	1.49	107.26	24	517	0.59	0.039	0.03	13.69	0.03	0.000
2.47	2.14	71.69	1.49	106.88	24	515	0.59	0.039	0.03	13.69	0.03	0.000
2.48	2.14	71.33	1.49	106.54	23	513	0.59	0.040	0.03	13.69	0.03	0.000
2.49	2.15	70.92	1.50	106.18	23	512	0.59	0.041	0.03	13.69	0.03	0.000
2.50	2.15	70.45	1.50	105.77	23	510	0.59	0.042	0.03	13.69	0.03	0.000
2.51	2.15	69.95	1.51	105.35	23	508	0.59	0.042	0.04	13.69	0.03	0.000
2.52	2.15	69.45	1.51	104.92	23	506	0.59	0.043	0.04	13.69	0.03	0.000
2.53	2.16	68.98	1.52	104.51	23	504	0.59	0.044	0.04	13.69	0.03	0.000
2.54	2.16	68.55	1.52	104.14	23	502	0.59	0.045	0.04	13.69	0.03	0.000
2.55	2.16	68.16	1.52	103.80	23	500	0.59	0.046	0.04	13.69	0.04	0.000
2.56	2.16	67.74	1.53	103.42	23	498	0.59	0.047	0.04	13.69	0.04	0.000
2.57	2.16	67.24	1.53	102.94	23	496	0.59	0.048	0.04	13.69	0.04	0.000
2.58	2.17	66.63	1.54	102.36	23	493	0.59	0.049	0.04	13.69	0.04	0.000
2.59	2.17	65.96	1.54	101.73	23	490	0.59	0.050	0.04	13.69	0.04	0.000
2.60	2.17	65.27	1.55	101.07	23	486	0.59	0.052	0.04	13.69	0.04	0.000
2.61	2.17	64.58	1.56	100.42	22	483	0.59	0.053	0.05	13.69	0.04	0.000
2.62	2.18	63.93	1.56	99.82	22	480	0.59	0.055	0.05	13.69	0.04	0.000
2.63	2.18	63.37	1.57	99.29	22	477	0.59	0.056	0.05	13.69	0.05	0.000
2.64	2.18	62.88	1.57	98.82	22	475	0.59	0.058	0.05	13.69	0.05	0.000
2.65	2.18	62.40	1.58	98.33	22	472	0.59	0.059	0.05	13.69	0.05	0.000
2.66	2.19	61.86	1.58	97.77	22	469	0.59	0.061	0.05	13.69	0.05	0.000
2.67	2.19	61.24	1.59	97.13	22	466	0.59	0.063	0.06	13.69	0.05	0.000
2.68	2.19	60.57	1.59	96.44	22	462	0.59	0.065	0.06	13.69	0.05	0.000
2.69	2.19	59.89	1.60	95.73	22	459	0.59	0.068	0.06	13.69	0.06	0.000
2.70	2.20	59.23	1.60	95.05	21	455	0.59	0.070	0.06	13.69	0.06	0.000
2.71	2.20	58.62	1.61	94.42	21	452	0.59	0.072	0.07	13.69	0.06	0.000
2.72	2.20	58.12	1.62	93.91	21	449	0.59	0.075	0.07	13.69	0.06	0.000
2.73	2.20	57.82	1.62	93.56	21	447	0.59	0.076	0.07	13.69	0.07	0.000
2.74	2.20	57.68	1.62	93.33	21	446	0.59	0.078	0.07	13.69	0.07	0.000
2.75	2.20	57.63	1.62	93.15	21	445	0.59	0.079	0.07	13.69	0.07	0.000
2.76	2.20	57.57	1.61	92.95	21	445	0.59	0.080	0.08	13.69	0.07	0.000
2.77	2.20	57.51	1.61	92.74	21	444	0.59	0.081	0.08	13.69	0.07	0.000
2.78	2.20	57.45	1.61	92.52	21	443	0.59	0.082	0.08	13.69	0.07	0.000
2.79	2.20	57.39	1.61	92.32	21	442	0.59	0.083	0.08	13.69	0.07	0.000
2.80	2.20	57.34	1.61	92.14	21	441	0.59	0.085	0.08	13.69	0.07	0.000
2.81	2.20	57.29	1.61	91.98	21	440	0.59	0.086	0.08	13.69	0.07	0.000
2.82	2.20	57.25	1.60	91.83	21	440	0.59	0.087	0.08	13.69	0.08	0.000
2.83	2.20	57.21	1.60	91.68	21	439	0.59	0.088	0.08	13.69	0.08	0.000
2.84	2.19	57.17	1.60	91.50	21	438	0.59	0.089	0.09	13.69	0.08	0.000
2.85	2.19	57.12	1.60	91.30	21	437	0.59	0.091	0.09	13.69	0.08	0.000
2.86	2.19	57.07	1.60	91.10	20	437	0.59	0.092	0.09	13.69	0.08	0.000
2.87	2.19	57.02	1.59	90.89	20	436	0.59	0.093	0.09	13.69	0.08	0.000
2.88	2.19	56.97	1.59	90.71	20	435	0.59	0.095	0.09	13.69	0.08	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	Ic	Q _{tn}	Kc	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _r (%)	Settle. (in)
2.89	2.19	56.93	1.59	90.54	20	434	0.59	0.096	0.09	13.69	0.09	0.000
2.90	2.19	56.86	1.59	90.34	20	433	0.59	0.098	0.10	13.69	0.09	0.000
2.91	2.19	56.75	1.59	90.07	20	432	0.59	0.099	0.10	13.69	0.09	0.000
2.92	2.19	56.60	1.58	89.69	20	430	0.59	0.102	0.10	13.69	0.09	0.000
2.93	2.19	56.41	1.58	89.24	20	428	0.59	0.105	0.10	13.69	0.09	0.000
2.94	2.19	56.21	1.58	88.77	20	426	0.59	0.107	0.11	13.69	0.10	0.000
2.95	2.18	56.01	1.58	88.28	20	424	0.59	0.111	0.11	13.69	0.10	0.000
2.96	2.18	55.81	1.57	87.81	20	422	0.59	0.114	0.12	13.69	0.11	0.000
2.97	2.18	55.63	1.57	87.38	20	420	0.59	0.117	0.12	13.69	0.11	0.000
2.98	2.18	55.43	1.57	86.98	19	418	0.59	0.120	0.12	13.69	0.11	0.000
2.99	2.18	55.02	1.57	86.43	19	415	0.59	0.124	0.13	13.69	0.12	0.000
3.00	2.18	54.33	1.58	85.66	19	411	0.59	0.130	0.14	13.69	0.12	0.000
3.01	2.19	53.36	1.59	84.64	19	406	0.59	0.139	0.15	13.69	0.13	0.000
3.02	2.19	52.27	1.60	83.50	19	400	0.59	0.149	0.16	13.69	0.15	0.000
3.03	2.20	51.12	1.61	82.31	19	394	0.59	0.161	0.18	13.69	0.16	0.000
3.04	2.20	49.96	1.62	81.12	18	388	0.59	0.175	0.19	13.69	0.18	0.000
3.05	2.21	48.86	1.64	80.00	18	382	0.59	0.190	0.21	13.69	0.19	0.000
3.06	2.21	47.87	1.65	79.00	18	376	0.59	0.205	0.23	13.69	0.21	0.000
3.07	2.22	47.00	1.66	78.18	18	372	0.59	0.219	0.25	13.69	0.23	0.000
3.08	2.22	46.14	1.68	77.47	18	368	0.59	0.233	0.27	13.69	0.25	0.000
3.09	2.23	45.17	1.70	76.77	18	363	0.59	0.249	0.29	13.69	0.26	0.000
3.10	2.24	44.02	1.73	76.00	17	358	0.59	0.270	0.32	13.69	0.29	0.000
3.11	2.25	42.76	1.76	75.17	17	352	0.59	0.296	0.35	13.69	0.32	0.000
3.12	2.26	41.45	1.79	74.34	17	346	0.59	0.326	0.39	13.69	0.35	0.000
3.13	2.27	40.15	1.83	73.54	17	340	0.59	0.361	0.43	13.69	0.39	0.000
3.14	2.29	38.95	1.87	72.81	17	335	0.59	0.398	0.48	13.69	0.44	0.001
3.15	2.29	37.89	1.91	72.20	17	330	0.59	0.437	0.53	13.69	0.48	0.001
3.16	2.30	37.22	1.93	71.82	17	327	0.59	0.465	0.57	13.69	0.51	0.001
3.17	2.30	36.92	1.94	71.65	17	325	0.59	0.481	0.59	13.69	0.53	0.001
3.18	2.30	36.91	1.94	71.65	17	325	0.59	0.485	0.59	13.69	0.54	0.001
3.19	2.30	36.91	1.94	71.65	17	325	0.59	0.489	0.60	13.69	0.54	0.001
3.20	2.30	36.91	1.94	71.65	17	325	0.59	0.493	0.60	13.69	0.55	0.001
3.21	2.30	36.91	1.94	71.65	17	325	0.59	0.497	0.61	13.69	0.55	0.001
3.22	2.30	36.90	1.94	71.65	17	325	0.59	0.501	0.61	13.69	0.55	0.001
3.23	2.30	36.90	1.94	71.65	17	325	0.59	0.506	0.62	13.69	0.56	0.001
3.24	2.30	36.91	1.94	71.64	17	325	0.59	0.510	0.62	13.69	0.56	0.001
3.25	2.30	36.95	1.94	71.58	17	325	0.59	0.514	0.63	13.69	0.57	0.001
3.26	2.30	37.04	1.93	71.48	17	325	0.59	0.519	0.64	13.69	0.58	0.001
3.27	2.30	37.16	1.92	71.32	17	325	0.59	0.524	0.65	13.69	0.58	0.001
3.28	2.30	37.31	1.91	71.15	17	325	0.59	0.529	0.66	13.69	0.59	0.001
3.29	2.29	37.46	1.89	70.96	17	325	0.59	0.534	0.67	13.69	0.60	0.001
3.30	2.29	37.60	1.88	70.78	17	325	0.59	0.539	0.68	13.69	0.61	0.001
3.31	2.29	37.75	1.87	70.61	17	325	0.59	0.545	0.69	13.69	0.62	0.001
3.32	2.28	37.87	1.86	70.46	16	325	0.59	0.550	0.70	13.69	0.63	0.001
3.33	2.28	37.96	1.85	70.31	16	324	0.59	0.557	0.71	13.69	0.64	0.001
3.34	2.28	38.01	1.85	70.16	16	324	0.59	0.565	0.72	13.69	0.65	0.001
3.35	2.28	38.02	1.84	69.96	16	323	0.59	0.575	0.74	13.69	0.66	0.001
3.36	2.27	38.02	1.83	69.72	16	323	0.59	0.588	0.76	13.69	0.68	0.001

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	Ic	Q _{tn}	Kc	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _r (%)	Settle. (in)
3.37	2.27	38.02	1.83	69.47	16	322	0.59	0.602	0.78	13.69	0.70	0.001
3.38	2.27	38.02	1.82	69.20	16	321	0.59	0.616	0.80	13.69	0.72	0.001
3.39	2.27	38.02	1.81	68.94	16	320	0.59	0.631	0.82	13.69	0.74	0.001
3.40	2.27	38.01	1.81	68.69	16	319	0.59	0.645	0.85	13.69	0.76	0.001
3.41	2.27	38.01	1.80	68.48	16	319	0.59	0.659	0.87	13.69	0.78	0.001
3.42	2.26	38.01	1.80	68.37	16	318	0.59	0.669	0.88	13.69	0.80	0.001
3.43	2.26	38.01	1.80	68.35	16	318	0.59	0.675	0.89	13.69	0.80	0.001
3.44	2.26	38.01	1.80	68.42	16	319	0.59	0.677	0.90	13.69	0.81	0.001
3.45	2.27	38.01	1.80	68.50	16	319	0.59	0.679	0.90	13.69	0.81	0.001
3.46	2.27	38.01	1.80	68.59	16	319	0.59	0.681	0.90	13.69	0.81	0.001
3.47	2.27	38.01	1.81	68.67	16	319	0.59	0.683	0.90	13.69	0.81	0.001
3.48	2.27	38.01	1.81	68.76	16	320	0.59	0.685	0.90	13.69	0.81	0.001
3.49	2.27	38.01	1.81	68.84	16	320	0.59	0.687	0.90	13.69	0.81	0.001
3.50	2.27	38.02	1.81	68.92	16	320	0.59	0.688	0.90	13.69	0.81	0.001
3.51	2.27	38.11	1.81	69.06	16	321	0.59	0.685	0.89	13.69	0.80	0.001
3.52	2.27	38.29	1.81	69.29	16	322	0.59	0.675	0.88	13.69	0.79	0.001
3.53	2.27	38.54	1.81	69.59	16	324	0.59	0.660	0.85	13.69	0.77	0.001
3.54	2.27	38.82	1.80	69.93	16	325	0.59	0.644	0.83	13.69	0.74	0.001
3.55	2.26	39.12	1.80	70.29	16	327	0.59	0.626	0.80	13.69	0.72	0.001
3.56	2.26	39.42	1.79	70.65	16	329	0.59	0.609	0.78	13.69	0.70	0.001
3.57	2.26	39.71	1.79	70.99	16	331	0.59	0.594	0.75	13.69	0.68	0.001
3.58	2.26	39.96	1.78	71.30	16	333	0.59	0.582	0.73	13.69	0.66	0.001
3.59	2.26	40.20	1.78	71.53	17	334	0.59	0.573	0.72	13.69	0.65	0.001
3.60	2.26	40.47	1.77	71.68	17	335	0.59	0.565	0.71	13.69	0.64	0.001
3.61	2.25	40.80	1.76	71.78	17	336	0.59	0.559	0.70	13.69	0.63	0.001
3.62	2.25	41.20	1.74	71.88	17	338	0.59	0.551	0.69	13.69	0.62	0.001
3.63	2.24	41.64	1.73	72.00	17	339	0.59	0.542	0.68	13.69	0.61	0.001
3.64	2.24	42.09	1.71	72.12	17	340	0.59	0.533	0.67	13.69	0.60	0.001
3.65	2.23	42.53	1.70	72.25	17	342	0.59	0.525	0.66	13.69	0.59	0.001
3.66	2.23	42.95	1.68	72.37	17	343	0.59	0.518	0.65	13.69	0.58	0.001
3.67	2.22	43.31	1.67	72.48	16	344	0.59	0.513	0.65	13.69	0.58	0.001
3.68	2.22	43.60	1.66	72.55	16	345	0.59	0.510	0.64	13.69	0.58	0.001
3.69	2.22	43.84	1.66	72.61	16	346	0.59	0.508	0.64	13.69	0.57	0.001
3.70	2.21	44.08	1.65	72.64	16	346	0.59	0.507	0.64	13.69	0.57	0.001
3.71	2.21	44.36	1.64	72.68	16	347	0.59	0.506	0.64	13.69	0.57	0.001
3.72	2.21	44.65	1.63	72.72	16	347	0.59	0.505	0.64	13.69	0.57	0.001
3.73	2.20	44.96	1.62	72.77	16	348	0.59	0.503	0.64	13.69	0.57	0.001
3.74	2.20	45.25	1.61	72.83	16	349	0.59	0.502	0.64	13.69	0.57	0.001
3.75	2.19	45.51	1.60	72.87	16	349	0.59	0.501	0.64	13.69	0.57	0.001
3.76	2.19	45.75	1.59	72.95	16	350	0.59	0.500	0.63	13.69	0.57	0.001
3.77	2.19	46.00	1.59	73.12	16	351	0.59	0.495	0.63	13.69	0.56	0.001
3.78	2.19	46.31	1.59	73.42	16	352	0.59	0.486	0.61	13.69	0.55	0.001
3.79	2.19	46.69	1.58	73.84	17	354	0.59	0.473	0.59	13.69	0.53	0.001
3.80	2.18	47.12	1.58	74.31	17	357	0.59	0.459	0.57	13.69	0.51	0.001
3.81	2.18	47.57	1.57	74.81	17	359	0.59	0.445	0.55	13.69	0.49	0.001
3.82	2.18	48.02	1.57	75.31	17	362	0.59	0.431	0.53	13.69	0.47	0.001
3.83	2.18	48.45	1.56	75.78	17	364	0.59	0.418	0.51	13.69	0.46	0.001
3.84	2.18	48.83	1.56	76.21	17	366	0.59	0.408	0.49	13.69	0.44	0.001

:: Post-earthquake settlement of dry sands :: (continued)												
Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _r (%)	Settle. (in)
3.85	2.18	49.26	1.56	76.65	17	369	0.59	0.397	0.48	13.69	0.43	0.001
3.86	2.17	49.85	1.55	77.22	17	371	0.59	0.383	0.46	13.69	0.41	0.000
3.87	2.17	50.68	1.54	77.99	17	375	0.59	0.365	0.43	13.69	0.39	0.000
3.88	2.16	51.70	1.53	78.93	18	380	0.59	0.344	0.40	13.69	0.36	0.000
3.89	2.16	52.82	1.51	79.98	18	385	0.59	0.322	0.37	13.69	0.33	0.000
3.90	2.15	53.98	1.50	81.08	18	391	0.59	0.302	0.35	13.69	0.31	0.000
3.91	2.14	55.12	1.49	82.17	18	396	0.59	0.284	0.32	13.69	0.29	0.000
3.92	2.14	56.18	1.48	83.19	18	401	0.59	0.269	0.30	13.69	0.27	0.000
3.93	2.13	57.10	1.47	84.09	18	405	0.59	0.257	0.28	13.69	0.25	0.000
3.94	2.13	57.85	1.47	84.78	19	408	0.59	0.249	0.27	13.69	0.24	0.000
3.95	2.13	58.52	1.46	85.35	19	411	0.59	0.243	0.26	13.69	0.24	0.000
3.96	2.12	59.20	1.45	85.89	19	413	0.59	0.238	0.26	13.69	0.23	0.000
3.97	2.12	59.99	1.44	86.51	19	416	0.59	0.232	0.25	13.69	0.22	0.000
3.98	2.11	60.83	1.43	87.19	19	419	0.59	0.226	0.24	13.69	0.21	0.000
3.99	2.10	61.69	1.42	87.89	19	422	0.59	0.220	0.23	13.69	0.21	0.000
4.00	2.10	62.51	1.42	88.57	19	425	0.59	0.214	0.23	13.69	0.20	0.000
4.01	2.09	63.27	1.41	89.20	19	427	0.59	0.210	0.22	13.69	0.20	0.000
4.02	2.09	63.85	1.40	89.69	19	429	0.59	0.207	0.22	13.69	0.19	0.000
4.03	2.09	64.18	1.40	89.95	19	430	0.59	0.206	0.21	13.69	0.19	0.000
4.04	2.09	64.30	1.40	90.00	19	430	0.59	0.207	0.21	13.69	0.19	0.000
4.05	2.09	64.29	1.40	89.95	19	430	0.59	0.209	0.22	13.69	0.19	0.000
4.06	2.09	64.29	1.40	89.88	19	429	0.59	0.211	0.22	13.69	0.20	0.000
4.07	2.08	64.29	1.40	89.82	19	429	0.59	0.213	0.22	13.69	0.20	0.000
4.08	2.08	64.29	1.40	89.75	19	428	0.59	0.215	0.22	13.69	0.20	0.000
4.09	2.08	64.29	1.40	89.69	19	428	0.59	0.217	0.23	13.69	0.20	0.000
4.10	2.08	64.29	1.39	89.64	19	428	0.59	0.220	0.23	13.69	0.20	0.000
4.11	2.08	64.29	1.39	89.61	19	428	0.59	0.221	0.23	13.69	0.21	0.000
4.12	2.08	64.29	1.39	89.61	19	428	0.59	0.222	0.23	13.69	0.21	0.000
4.13	2.08	64.29	1.39	89.65	19	428	0.59	0.223	0.23	13.69	0.21	0.000
4.14	2.08	64.28	1.40	89.71	19	428	0.59	0.224	0.23	13.69	0.21	0.000
4.15	2.08	64.28	1.40	89.77	19	429	0.59	0.224	0.23	13.69	0.21	0.000
4.16	2.08	64.28	1.40	89.84	19	429	0.59	0.224	0.23	13.69	0.21	0.000
4.17	2.09	64.28	1.40	89.90	19	429	0.59	0.224	0.23	13.69	0.21	0.000
4.18	2.09	64.28	1.40	89.96	19	430	0.59	0.225	0.23	13.69	0.21	0.000
4.19	2.09	64.28	1.40	90.01	19	430	0.59	0.225	0.23	13.69	0.21	0.000
4.20	2.09	64.28	1.40	90.09	19	431	0.59	0.225	0.23	13.69	0.21	0.000
4.21	2.09	64.28	1.40	90.20	19	431	0.59	0.225	0.23	13.69	0.21	0.000
4.22	2.09	64.28	1.41	90.36	19	432	0.59	0.224	0.23	13.69	0.20	0.000
4.23	2.09	64.28	1.41	90.55	20	433	0.59	0.222	0.23	13.69	0.20	0.000
4.24	2.10	64.27	1.41	90.74	20	435	0.59	0.221	0.23	13.69	0.20	0.000
4.25	2.10	64.27	1.41	90.95	20	436	0.59	0.219	0.22	13.69	0.20	0.000
4.26	2.10	64.27	1.42	91.14	20	437	0.59	0.218	0.22	13.69	0.20	0.000
4.27	2.10	64.27	1.42	91.32	20	438	0.59	0.217	0.22	13.69	0.19	0.000
4.28	2.10	64.26	1.42	91.47	20	439	0.59	0.216	0.22	13.69	0.19	0.000
4.29	2.10	64.23	1.43	91.58	20	440	0.59	0.215	0.22	13.69	0.19	0.000
4.30	2.11	64.17	1.43	91.68	20	440	0.59	0.215	0.22	13.69	0.19	0.000
4.31	2.11	64.08	1.43	91.78	20	441	0.59	0.215	0.22	13.69	0.19	0.000
4.32	2.11	63.99	1.44	91.89	20	442	0.59	0.214	0.21	13.69	0.19	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	Ic	Q _{tn}	Kc	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _r (%)	Settle. (in)
4.33	2.11	63.88	1.44	92.02	20	442	0.59	0.214	0.21	13.69	0.19	0.000
4.34	2.12	63.78	1.44	92.14	20	443	0.59	0.213	0.21	13.69	0.19	0.000
4.35	2.12	63.69	1.45	92.26	20	444	0.59	0.213	0.21	13.69	0.19	0.000
4.36	2.12	63.60	1.45	92.36	20	444	0.59	0.213	0.21	13.69	0.19	0.000
4.37	2.12	63.56	1.45	92.46	20	445	0.59	0.213	0.21	13.69	0.19	0.000
4.38	2.12	63.58	1.46	92.57	20	446	0.59	0.212	0.21	13.69	0.19	0.000
4.39	2.12	63.67	1.46	92.71	20	446	0.59	0.212	0.21	13.69	0.18	0.000
4.40	2.12	63.78	1.46	92.87	20	447	0.59	0.212	0.21	13.69	0.18	0.000
4.41	2.12	63.90	1.46	93.05	20	448	0.59	0.211	0.21	13.69	0.18	0.000
4.42	2.12	64.02	1.46	93.23	20	449	0.59	0.210	0.21	13.69	0.18	0.000
4.43	2.12	64.15	1.46	93.41	20	450	0.59	0.209	0.20	13.69	0.18	0.000
4.44	2.12	64.26	1.46	93.58	20	450	0.59	0.209	0.20	13.69	0.18	0.000
4.45	2.12	64.36	1.46	93.73	20	451	0.59	0.208	0.20	13.69	0.18	0.000
4.46	2.12	64.52	1.46	93.91	21	452	0.59	0.208	0.20	13.69	0.18	0.000
4.47	2.12	64.78	1.45	94.14	21	453	0.59	0.207	0.20	13.69	0.18	0.000
4.48	2.12	65.14	1.45	94.47	21	455	0.59	0.205	0.20	13.69	0.17	0.000
4.49	2.12	65.56	1.45	94.84	21	456	0.59	0.202	0.19	13.69	0.17	0.000
4.50	2.12	66.01	1.44	95.24	21	458	0.59	0.200	0.19	13.69	0.17	0.000
4.51	2.11	66.46	1.44	95.64	21	460	0.59	0.197	0.19	13.69	0.17	0.000
4.52	2.11	66.90	1.44	96.04	21	461	0.59	0.195	0.19	13.69	0.16	0.000
4.53	2.11	67.29	1.43	96.40	21	463	0.59	0.193	0.18	13.69	0.16	0.000
4.54	2.11	67.63	1.43	96.71	21	464	0.59	0.192	0.18	13.69	0.16	0.000
4.55	2.11	67.96	1.43	97.00	21	466	0.59	0.190	0.18	13.69	0.16	0.000
4.56	2.10	68.32	1.42	97.33	21	467	0.59	0.189	0.18	13.69	0.16	0.000
4.57	2.10	68.74	1.42	97.72	21	469	0.59	0.187	0.17	13.69	0.15	0.000
4.58	2.10	69.22	1.42	98.15	21	471	0.59	0.185	0.17	13.69	0.15	0.000
4.59	2.10	69.71	1.41	98.61	21	472	0.59	0.182	0.17	13.69	0.15	0.000
4.60	2.09	70.21	1.41	99.07	21	474	0.59	0.180	0.17	13.69	0.15	0.000
4.61	2.09	70.67	1.41	99.50	21	476	0.59	0.178	0.16	13.69	0.14	0.000
4.62	2.09	71.09	1.41	99.89	22	478	0.59	0.176	0.16	13.69	0.14	0.000
4.63	2.09	71.49	1.40	100.24	22	479	0.59	0.175	0.16	13.69	0.14	0.000
4.64	2.09	71.94	1.40	100.61	22	481	0.59	0.173	0.16	13.69	0.14	0.000
4.65	2.08	72.50	1.39	101.05	22	482	0.59	0.172	0.16	13.69	0.14	0.000
4.66	2.08	73.18	1.39	101.57	22	484	0.59	0.170	0.15	13.69	0.13	0.000
4.67	2.07	73.91	1.38	102.14	22	486	0.59	0.168	0.15	13.69	0.13	0.000
4.68	2.07	74.66	1.38	102.74	22	488	0.59	0.166	0.15	13.69	0.13	0.000
4.69	2.06	75.40	1.37	103.33	22	490	0.59	0.164	0.15	13.69	0.13	0.000
4.70	2.06	76.09	1.37	103.89	22	492	0.59	0.162	0.14	13.69	0.13	0.000
4.71	2.06	76.69	1.36	104.37	22	493	0.59	0.161	0.14	13.69	0.12	0.000
4.72	2.05	77.22	1.36	104.81	22	494	0.59	0.160	0.14	13.69	0.12	0.000
4.73	2.05	77.77	1.35	105.26	22	496	0.59	0.159	0.14	13.69	0.12	0.000
4.74	2.04	78.41	1.35	105.80	22	497	0.59	0.157	0.14	13.69	0.12	0.000
4.75	2.04	79.13	1.34	106.41	22	499	0.59	0.156	0.14	13.69	0.12	0.000
4.76	2.04	79.91	1.34	107.06	23	501	0.59	0.154	0.13	13.69	0.12	0.000
4.77	2.03	80.69	1.34	107.73	23	503	0.59	0.152	0.13	13.69	0.11	0.000
4.78	2.03	81.45	1.33	108.38	23	505	0.59	0.151	0.13	13.69	0.11	0.000
4.79	2.02	82.13	1.33	108.98	23	506	0.59	0.149	0.13	13.69	0.11	0.000
4.80	2.02	82.73	1.32	109.51	23	508	0.59	0.148	0.13	13.69	0.11	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _r (%)	Settle. (in)
4.81	2.02	83.31	1.32	110.06	23	510	0.59	0.147	0.12	13.69	0.11	0.000
4.82	2.01	83.96	1.32	110.71	23	512	0.59	0.145	0.12	13.69	0.11	0.000
4.83	2.01	84.73	1.32	111.50	23	514	0.59	0.143	0.12	13.69	0.10	0.000
4.84	2.01	85.60	1.31	112.38	23	517	0.59	0.140	0.12	13.69	0.10	0.000
4.85	2.00	86.50	1.31	113.31	24	521	0.59	0.137	0.11	13.69	0.10	0.000
4.86	2.00	87.40	1.31	114.24	24	524	0.59	0.135	0.11	13.69	0.10	0.000
4.87	2.00	88.25	1.30	115.11	24	527	0.59	0.132	0.11	13.69	0.09	0.000
4.88	1.99	89.00	1.30	115.89	24	529	0.59	0.130	0.10	13.69	0.09	0.000
4.89	1.99	89.69	1.30	116.61	24	532	0.59	0.128	0.10	13.69	0.09	0.000
4.90	1.99	90.42	1.30	117.36	24	534	0.59	0.127	0.10	13.69	0.09	0.000
4.91	1.99	91.29	1.30	118.27	24	537	0.59	0.124	0.10	13.69	0.09	0.000
4.92	1.98	92.32	1.29	119.33	25	541	0.59	0.122	0.09	13.69	0.08	0.000
4.93	1.98	93.43	1.29	120.50	25	544	0.59	0.119	0.09	13.69	0.08	0.000
4.94	1.97	94.58	1.29	121.70	25	548	0.59	0.116	0.09	13.69	0.08	0.000
4.95	1.97	95.71	1.28	122.87	25	552	0.59	0.114	0.09	13.69	0.08	0.000
4.96	1.97	96.75	1.28	123.96	25	556	0.59	0.112	0.08	13.69	0.07	0.000
4.97	1.96	97.64	1.28	124.90	26	559	0.59	0.110	0.08	13.69	0.07	0.000
4.98	1.96	98.37	1.28	125.66	26	561	0.59	0.109	0.08	13.69	0.07	0.000
4.99	1.96	99.02	1.28	126.34	26	563	0.59	0.108	0.08	13.69	0.07	0.000
5.00	1.96	99.69	1.27	127.05	26	565	0.59	0.106	0.08	13.69	0.07	0.000
5.01	1.95	100.46	1.27	127.85	26	568	0.59	0.105	0.08	13.69	0.07	0.000
5.02	1.95	101.28	1.27	128.71	26	571	0.59	0.104	0.07	13.69	0.07	0.000
5.03	1.95	102.11	1.27	129.58	26	573	0.59	0.102	0.07	13.69	0.06	0.000
5.04	1.95	102.91	1.27	130.42	27	576	0.59	0.101	0.07	13.69	0.06	0.000
5.05	1.94	103.63	1.27	131.17	27	578	0.59	0.100	0.07	13.69	0.06	0.000
5.06	1.94	104.20	1.26	131.76	27	580	0.59	0.099	0.07	13.69	0.06	0.000
5.07	1.94	104.59	1.26	132.13	27	581	0.59	0.099	0.07	13.69	0.06	0.000
5.08	1.94	104.84	1.26	132.33	27	581	0.59	0.100	0.07	13.69	0.06	0.000
5.09	1.94	105.07	1.26	132.47	27	581	0.59	0.100	0.07	13.69	0.06	0.000
5.10	1.93	105.31	1.26	132.62	27	581	0.59	0.101	0.07	13.69	0.06	0.000
5.11	1.93	105.57	1.26	132.79	27	580	0.59	0.101	0.07	13.69	0.06	0.000
5.12	1.93	105.83	1.26	132.95	27	580	0.59	0.102	0.07	13.69	0.06	0.000
5.13	1.93	106.08	1.25	133.10	27	580	0.59	0.103	0.07	13.69	0.06	0.000
5.14	1.93	106.29	1.25	133.23	27	579	0.59	0.103	0.07	13.69	0.06	0.000
5.15	1.92	106.47	1.25	133.34	27	579	0.59	0.104	0.07	13.69	0.06	0.000
5.16	1.92	106.61	1.25	133.44	27	579	0.59	0.104	0.07	13.69	0.06	0.000
5.17	1.92	106.75	1.25	133.53	27	579	0.59	0.105	0.07	13.69	0.06	0.000
5.18	1.92	106.91	1.25	133.65	27	579	0.59	0.105	0.07	13.69	0.06	0.000
5.19	1.92	107.08	1.25	133.77	27	579	0.59	0.106	0.07	13.69	0.06	0.000
5.20	1.92	107.25	1.25	133.89	27	579	0.59	0.106	0.07	13.69	0.06	0.000
5.21	1.92	107.42	1.25	134.01	27	579	0.59	0.106	0.07	13.69	0.06	0.000
5.22	1.91	107.58	1.25	134.13	27	579	0.59	0.107	0.07	13.69	0.06	0.000
5.23	1.91	107.72	1.25	134.23	27	579	0.59	0.107	0.07	13.69	0.06	0.000
5.24	1.91	107.86	1.25	134.38	27	579	0.59	0.107	0.07	13.69	0.06	0.000
5.25	1.91	108.03	1.25	134.60	27	580	0.59	0.107	0.07	13.69	0.06	0.000
5.26	1.91	108.23	1.25	134.90	27	582	0.59	0.107	0.07	13.69	0.06	0.000
5.27	1.92	108.46	1.25	135.25	27	584	0.59	0.106	0.07	13.69	0.06	0.000
5.28	1.92	108.71	1.25	135.62	27	586	0.59	0.105	0.07	13.69	0.06	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _r (%)	Settle. (in)
5.29	1.92	108.96	1.25	135.99	27	588	0.59	0.104	0.07	13.69	0.06	0.000
5.30	1.92	109.20	1.25	136.35	28	590	0.59	0.103	0.07	13.69	0.06	0.000
5.31	1.92	109.42	1.25	136.68	28	591	0.59	0.102	0.07	13.69	0.06	0.000
5.32	1.92	109.56	1.25	136.92	28	593	0.59	0.102	0.07	13.69	0.06	0.000
5.33	1.92	109.58	1.25	137.03	28	594	0.59	0.102	0.07	13.69	0.06	0.000
5.34	1.92	109.48	1.25	137.05	28	595	0.59	0.102	0.07	13.69	0.06	0.000
5.35	1.93	109.31	1.25	137.01	28	596	0.59	0.101	0.07	13.69	0.06	0.000
5.36	1.93	109.12	1.26	136.97	28	597	0.59	0.101	0.07	13.69	0.06	0.000
5.37	1.93	108.91	1.26	136.93	28	598	0.59	0.101	0.07	13.69	0.06	0.000
5.38	1.93	108.71	1.26	136.88	28	599	0.59	0.101	0.07	13.69	0.06	0.000
5.39	1.94	108.52	1.26	136.84	28	600	0.59	0.100	0.07	13.69	0.06	0.000
5.40	1.94	108.36	1.26	136.80	28	601	0.59	0.100	0.07	13.69	0.06	0.000
5.41	1.94	108.20	1.26	136.74	28	602	0.59	0.100	0.07	13.69	0.06	0.000
5.42	1.94	108.04	1.26	136.66	28	602	0.59	0.100	0.07	13.69	0.06	0.000
5.43	1.94	107.85	1.27	136.54	28	602	0.59	0.101	0.07	13.69	0.06	0.000
5.44	1.95	107.62	1.27	136.40	28	603	0.59	0.101	0.07	13.69	0.06	0.000
5.45	1.95	107.37	1.27	136.25	28	603	0.59	0.101	0.07	13.69	0.06	0.000
5.46	1.95	107.12	1.27	136.09	28	603	0.59	0.101	0.07	13.69	0.06	0.000
5.47	1.95	106.87	1.27	135.94	28	603	0.59	0.101	0.07	13.69	0.06	0.000
5.48	1.95	106.64	1.27	135.79	28	604	0.59	0.102	0.07	13.69	0.06	0.000
5.49	1.96	106.45	1.27	135.67	28	604	0.59	0.102	0.07	13.69	0.06	0.000
5.50	1.96	106.34	1.28	135.60	28	604	0.59	0.102	0.07	13.69	0.06	0.000
5.51	1.96	106.29	1.28	135.57	28	604	0.59	0.103	0.07	13.69	0.06	0.000
5.52	1.96	106.29	1.28	135.57	28	604	0.59	0.103	0.07	13.69	0.06	0.000
5.53	1.96	106.29	1.28	135.57	28	604	0.59	0.103	0.07	13.69	0.06	0.000
5.54	1.96	106.29	1.28	135.57	28	604	0.59	0.104	0.07	13.69	0.06	0.000
5.55	1.96	106.29	1.28	135.57	28	604	0.59	0.104	0.07	13.69	0.06	0.000
5.56	1.96	106.29	1.28	135.57	28	604	0.59	0.105	0.07	13.69	0.06	0.000
5.57	1.96	106.29	1.28	135.57	28	604	0.59	0.105	0.07	13.69	0.06	0.000
5.58	1.96	106.26	1.28	135.55	28	604	0.59	0.105	0.07	13.69	0.06	0.000
5.59	1.96	106.19	1.28	135.47	28	604	0.59	0.106	0.07	13.69	0.06	0.000
5.60	1.96	106.07	1.28	135.34	28	603	0.59	0.107	0.07	13.69	0.06	0.000
5.61	1.96	105.89	1.28	135.15	28	603	0.59	0.107	0.07	13.69	0.06	0.000
5.62	1.96	105.70	1.28	134.95	28	602	0.59	0.108	0.07	13.69	0.06	0.000
5.63	1.96	105.49	1.28	134.74	28	601	0.59	0.109	0.07	13.69	0.06	0.000
5.64	1.96	105.29	1.28	134.53	28	601	0.59	0.110	0.07	13.69	0.06	0.000
5.65	1.96	105.10	1.28	134.33	28	600	0.59	0.111	0.08	13.69	0.06	0.000
5.66	1.96	104.94	1.28	134.15	28	599	0.59	0.112	0.08	13.69	0.07	0.000
5.67	1.96	104.79	1.28	134.01	27	599	0.59	0.112	0.08	13.69	0.07	0.000
5.68	1.96	104.65	1.28	133.88	27	599	0.59	0.113	0.08	13.69	0.07	0.000
5.69	1.96	104.49	1.28	133.76	27	599	0.59	0.113	0.08	13.69	0.07	0.000
5.70	1.97	104.31	1.28	133.62	27	599	0.59	0.114	0.08	13.69	0.07	0.000
5.71	1.97	104.11	1.28	133.46	27	598	0.59	0.114	0.08	13.69	0.07	0.000
5.72	1.97	103.91	1.28	133.30	27	598	0.59	0.115	0.08	13.69	0.07	0.000
5.73	1.97	103.71	1.28	133.15	27	598	0.59	0.115	0.08	13.69	0.07	0.000
5.74	1.97	103.53	1.28	133.00	27	598	0.59	0.116	0.08	13.69	0.07	0.000
5.75	1.97	103.38	1.29	132.89	27	598	0.59	0.117	0.08	13.69	0.07	0.000
5.76	1.97	103.29	1.29	132.83	27	598	0.59	0.117	0.08	13.69	0.07	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	Ic	Q _{tn}	Kc	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _r (%)	Settle. (in)
5.77	1.97	103.25	1.29	132.83	27	598	0.59	0.117	0.08	13.69	0.07	0.000
5.78	1.97	103.25	1.29	132.87	27	599	0.59	0.117	0.08	13.69	0.07	0.000
5.79	1.97	103.25	1.29	132.92	27	599	0.59	0.117	0.08	13.69	0.07	0.000
5.80	1.98	103.25	1.29	132.98	27	600	0.59	0.117	0.08	13.69	0.07	0.000
5.81	1.98	103.25	1.29	133.03	27	600	0.59	0.117	0.08	13.69	0.07	0.000
5.82	1.98	103.25	1.29	133.08	27	601	0.59	0.117	0.08	13.69	0.07	0.000
5.83	1.98	103.25	1.29	133.13	27	601	0.59	0.118	0.08	13.69	0.07	0.000
5.84	1.98	103.25	1.29	133.15	27	602	0.59	0.118	0.08	13.69	0.07	0.000
5.85	1.98	103.24	1.29	133.15	27	602	0.58	0.118	0.08	13.69	0.07	0.000
5.86	1.98	103.24	1.29	133.12	27	601	0.58	0.119	0.08	13.69	0.07	0.000
5.87	1.98	103.24	1.29	133.07	27	601	0.58	0.120	0.08	13.69	0.07	0.000
5.88	1.98	103.24	1.29	133.02	27	600	0.58	0.120	0.08	13.69	0.07	0.000
5.89	1.98	103.24	1.29	132.97	27	600	0.58	0.121	0.08	13.69	0.07	0.000
5.90	1.97	103.24	1.29	132.91	27	599	0.58	0.122	0.08	13.69	0.07	0.000
5.91	1.97	103.24	1.29	132.86	27	599	0.58	0.123	0.08	13.69	0.07	0.000
5.92	1.97	103.24	1.29	132.82	27	598	0.58	0.124	0.08	13.69	0.07	0.000
5.93	1.97	103.24	1.29	132.80	27	598	0.58	0.124	0.09	13.69	0.07	0.000
5.94	1.97	103.23	1.29	132.81	27	598	0.58	0.125	0.09	13.69	0.07	0.000
5.95	1.97	103.23	1.29	132.84	27	599	0.58	0.125	0.09	13.69	0.07	0.000
5.96	1.97	103.23	1.29	132.89	27	599	0.58	0.125	0.09	13.69	0.07	0.000
5.97	1.98	103.23	1.29	132.94	27	600	0.58	0.125	0.09	13.69	0.07	0.000
5.98	1.98	103.23	1.29	133.00	27	600	0.58	0.125	0.09	13.69	0.07	0.000
5.99	1.98	103.22	1.29	133.04	27	601	0.58	0.125	0.09	13.69	0.07	0.000
6.00	1.98	103.15	1.29	133.01	27	601	0.58	0.125	0.09	13.69	0.07	0.000
6.01	1.98	103.08	1.29	132.98	27	602	0.58	0.125	0.09	13.69	0.07	0.000
6.02	1.98	103.01	1.29	132.97	27	603	0.58	0.125	0.09	13.69	0.07	0.000
6.03	1.98	102.95	1.29	132.97	27	603	0.58	0.125	0.09	13.69	0.07	0.000
6.04	1.98	102.90	1.29	133.01	27	604	0.58	0.124	0.08	13.69	0.07	0.000
6.05	1.98	102.86	1.29	133.07	28	605	0.58	0.124	0.08	13.69	0.07	0.000
6.06	1.98	102.82	1.29	133.14	28	607	0.58	0.124	0.08	13.69	0.07	0.000
6.07	1.99	102.78	1.30	133.21	28	608	0.58	0.123	0.08	13.69	0.07	0.000
6.08	1.99	102.74	1.30	133.27	28	609	0.58	0.123	0.08	13.69	0.07	0.000
6.09	1.99	102.69	1.30	133.31	28	610	0.58	0.122	0.08	13.69	0.07	0.000
6.10	1.99	102.66	1.30	133.34	28	611	0.58	0.122	0.08	13.69	0.07	0.000
6.11	1.99	102.65	1.30	133.38	28	612	0.58	0.122	0.08	13.69	0.07	0.000
6.12	1.99	102.70	1.30	133.43	28	612	0.58	0.122	0.08	13.69	0.07	0.000
6.13	1.99	102.78	1.30	133.52	28	613	0.58	0.121	0.08	13.69	0.07	0.000
6.14	1.99	102.88	1.30	133.62	28	614	0.58	0.121	0.08	13.69	0.07	0.000
6.15	1.99	102.99	1.30	133.74	28	616	0.58	0.121	0.08	13.69	0.07	0.000
6.16	1.99	103.09	1.30	133.85	28	617	0.58	0.120	0.08	13.69	0.07	0.000
6.17	1.99	103.18	1.30	133.94	28	618	0.58	0.120	0.08	13.69	0.07	0.000
6.18	1.99	103.25	1.30	134.02	28	619	0.58	0.120	0.08	13.69	0.07	0.000
6.19	1.99	103.37	1.30	134.11	28	619	0.58	0.120	0.08	13.69	0.07	0.000
6.20	1.99	103.56	1.30	134.27	28	621	0.58	0.119	0.08	13.69	0.07	0.000
6.21	1.98	103.88	1.29	134.52	28	622	0.58	0.119	0.08	13.69	0.07	0.000
6.22	1.98	104.26	1.29	134.82	28	624	0.58	0.118	0.08	13.69	0.07	0.000
6.23	1.98	104.68	1.29	135.16	28	625	0.58	0.117	0.08	13.69	0.07	0.000
6.24	1.98	105.12	1.29	135.50	28	627	0.58	0.116	0.08	13.69	0.07	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	Ic	Q _{tn}	Kc	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _r (%)	Settle. (in)
6.25	1.97	105.53	1.29	135.83	28	629	0.58	0.116	0.08	13.69	0.07	0.000
6.26	1.97	105.91	1.29	136.13	28	630	0.58	0.115	0.08	13.69	0.07	0.000
6.27	1.97	106.25	1.28	136.40	28	632	0.58	0.114	0.08	13.69	0.06	0.000
6.28	1.97	106.69	1.28	136.80	28	634	0.58	0.114	0.08	13.69	0.06	0.000
6.29	1.96	107.34	1.28	137.40	28	637	0.58	0.112	0.07	13.69	0.06	0.000
6.30	1.96	108.22	1.28	138.24	28	640	0.58	0.110	0.07	13.69	0.06	0.000
6.31	1.96	109.22	1.27	139.19	28	644	0.58	0.108	0.07	13.69	0.06	0.000
6.32	1.95	110.29	1.27	140.20	29	649	0.58	0.106	0.07	13.69	0.06	0.000
6.33	1.95	111.35	1.27	141.22	29	653	0.58	0.104	0.07	13.69	0.06	0.000
6.34	1.94	112.36	1.27	142.18	29	657	0.58	0.102	0.07	13.69	0.06	0.000
6.35	1.94	113.26	1.26	143.03	29	661	0.58	0.100	0.06	13.69	0.05	0.000
6.36	1.94	114.06	1.26	143.80	29	664	0.58	0.099	0.06	13.69	0.05	0.000
6.37	1.93	114.93	1.26	144.67	29	668	0.58	0.097	0.06	13.69	0.05	0.000
6.38	1.93	115.98	1.26	145.77	30	673	0.58	0.095	0.06	13.69	0.05	0.000
6.39	1.93	117.28	1.25	147.12	30	679	0.58	0.092	0.06	13.69	0.05	0.000
6.40	1.92	118.71	1.25	148.62	30	686	0.58	0.090	0.06	13.69	0.05	0.000
6.41	1.92	120.20	1.25	150.18	30	693	0.58	0.087	0.05	13.69	0.04	0.000
6.42	1.92	121.67	1.25	151.71	31	700	0.58	0.085	0.05	13.69	0.04	0.000
6.43	1.91	123.04	1.24	153.12	31	706	0.58	0.083	0.05	13.69	0.04	0.000
6.44	1.91	124.22	1.24	154.35	31	712	0.58	0.081	0.05	13.69	0.04	0.000
6.45	1.91	125.22	1.24	155.39	31	716	0.58	0.079	0.05	13.69	0.04	0.000
6.46	1.90	126.02	1.24	156.21	31	721	0.58	0.078	0.05	13.69	0.04	0.000
6.47	1.90	127.09	1.24	157.32	32	727	0.58	0.076	0.04	13.69	0.04	0.000
6.48	1.90	128.34	1.24	158.60	32	732	0.58	0.075	0.04	13.69	0.04	0.000
6.49	1.89	129.69	1.23	159.98	32	739	0.58	0.073	0.04	13.69	0.04	0.000
6.50	1.89	131.07	1.23	161.39	32	745	0.58	0.071	0.04	13.69	0.03	0.000
6.51	1.89	132.41	1.23	162.75	32	751	0.58	0.070	0.04	13.69	0.03	0.000
6.52	1.89	133.62	1.23	163.98	33	757	0.58	0.068	0.04	13.69	0.03	0.000
6.53	1.88	134.64	1.23	165.00	33	762	0.58	0.067	0.04	13.69	0.03	0.000
6.54	1.88	135.48	1.22	165.86	33	766	0.58	0.066	0.04	13.69	0.03	0.000
6.55	1.88	136.29	1.22	166.67	33	770	0.58	0.066	0.04	13.69	0.03	0.000
6.56	1.88	137.20	1.22	167.58	33	774	0.58	0.065	0.04	13.69	0.03	0.000
6.57	1.88	138.24	1.22	168.62	33	779	0.58	0.064	0.03	13.69	0.03	0.000
6.58	1.87	139.34	1.22	169.72	34	785	0.58	0.063	0.03	13.69	0.03	0.000
6.59	1.87	140.45	1.22	170.81	34	790	0.58	0.062	0.03	13.69	0.03	0.000
6.60	1.87	141.49	1.21	171.85	34	795	0.58	0.061	0.03	13.69	0.03	0.000
6.61	1.87	142.42	1.21	172.76	34	799	0.58	0.060	0.03	13.69	0.03	0.000
6.62	1.86	143.14	1.21	173.47	34	803	0.58	0.059	0.03	13.69	0.03	0.000
6.63	1.86	143.69	1.21	174.00	34	806	0.58	0.059	0.03	13.69	0.03	0.000
6.64	1.86	144.15	1.21	174.46	34	809	0.58	0.059	0.03	13.69	0.03	0.000
6.65	1.86	144.68	1.21	174.97	35	812	0.58	0.058	0.03	13.69	0.03	0.000
6.66	1.86	145.26	1.21	175.54	35	815	0.58	0.058	0.03	13.69	0.03	0.000
6.67	1.86	145.87	1.21	176.13	35	818	0.58	0.057	0.03	13.69	0.02	0.000
6.68	1.86	146.47	1.21	176.71	35	821	0.58	0.057	0.03	13.69	0.02	0.000
6.69	1.86	147.02	1.21	177.24	35	824	0.58	0.056	0.03	13.69	0.02	0.000
6.70	1.86	147.49	1.20	177.70	35	827	0.58	0.056	0.03	13.69	0.02	0.000
6.71	1.85	147.77	1.20	177.99	35	829	0.58	0.056	0.03	13.69	0.02	0.000
6.72	1.85	147.90	1.20	178.15	35	830	0.58	0.056	0.03	13.69	0.02	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	Ic	Q _{tn}	Kc	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _r (%)	Settle. (in)
6.73	1.86	147.92	1.20	178.24	35	831	0.58	0.056	0.03	13.69	0.02	0.000
6.74	1.86	147.95	1.21	178.35	35	833	0.58	0.056	0.03	13.69	0.02	0.000
6.75	1.86	147.99	1.21	178.47	35	834	0.58	0.055	0.03	13.69	0.02	0.000
6.76	1.86	148.03	1.21	178.60	35	836	0.58	0.055	0.03	13.69	0.02	0.000
6.77	1.86	148.07	1.21	178.72	35	837	0.58	0.055	0.03	13.69	0.02	0.000
6.78	1.86	148.09	1.21	178.82	35	838	0.58	0.055	0.03	13.69	0.02	0.000
6.79	1.86	148.07	1.21	178.88	35	840	0.58	0.055	0.03	13.69	0.02	0.000
6.80	1.86	147.94	1.21	178.83	35	840	0.58	0.055	0.03	13.69	0.02	0.000
6.81	1.86	147.69	1.21	178.70	35	841	0.58	0.055	0.03	13.69	0.02	0.000
6.82	1.86	147.34	1.21	178.49	35	841	0.58	0.055	0.03	13.69	0.02	0.000
6.83	1.87	146.95	1.21	178.27	35	841	0.58	0.055	0.03	13.69	0.02	0.000
6.84	1.87	146.55	1.21	178.04	35	841	0.58	0.055	0.03	13.69	0.02	0.000
6.85	1.87	146.15	1.22	177.80	35	841	0.58	0.056	0.03	13.69	0.02	0.000
6.86	1.87	145.76	1.22	177.56	35	842	0.58	0.056	0.03	13.69	0.02	0.000
6.87	1.87	145.41	1.22	177.34	35	842	0.58	0.056	0.03	13.69	0.02	0.000
6.88	1.88	145.06	1.22	177.11	35	842	0.58	0.056	0.03	13.69	0.02	0.000
6.89	1.88	144.67	1.22	176.85	35	842	0.58	0.056	0.03	13.69	0.02	0.000
6.90	1.88	144.20	1.22	176.53	35	842	0.58	0.056	0.03	13.69	0.02	0.000
6.91	1.88	143.65	1.23	176.17	35	842	0.58	0.056	0.03	13.69	0.02	0.000
6.92	1.89	143.06	1.23	175.77	35	841	0.58	0.057	0.03	13.69	0.02	0.000
6.93	1.89	142.45	1.23	175.36	35	841	0.58	0.057	0.03	13.69	0.02	0.000
6.94	1.89	141.84	1.23	174.94	35	841	0.58	0.057	0.03	13.69	0.02	0.000
6.95	1.90	141.27	1.24	174.53	35	841	0.58	0.057	0.03	13.69	0.02	0.000
6.96	1.90	140.75	1.24	174.16	35	840	0.58	0.057	0.03	13.69	0.02	0.000
6.97	1.90	140.27	1.24	173.80	35	840	0.58	0.058	0.03	13.69	0.02	0.000
6.98	1.91	139.79	1.24	173.40	35	840	0.58	0.058	0.03	13.69	0.02	0.000
6.99	1.91	139.26	1.24	172.95	35	839	0.58	0.058	0.03	13.69	0.03	0.000
7.00	1.91	138.66	1.24	172.43	35	838	0.58	0.058	0.03	13.69	0.03	0.000
7.01	1.91	138.02	1.25	171.89	35	837	0.58	0.059	0.03	13.69	0.03	0.000
7.02	1.92	137.37	1.25	171.33	35	836	0.58	0.059	0.03	13.69	0.03	0.000
7.03	1.92	136.73	1.25	170.79	34	835	0.58	0.060	0.03	13.69	0.03	0.000
7.04	1.92	136.14	1.25	170.28	34	834	0.58	0.060	0.03	13.69	0.03	0.000
7.05	1.92	135.64	1.25	169.84	34	833	0.58	0.060	0.03	13.69	0.03	0.000
7.06	1.92	135.26	1.25	169.52	34	833	0.58	0.060	0.03	13.69	0.03	0.000
7.07	1.93	134.97	1.25	169.30	34	833	0.58	0.061	0.03	13.69	0.03	0.000
7.08	1.93	134.71	1.26	169.13	34	833	0.58	0.061	0.03	13.69	0.03	0.000
7.09	1.93	134.43	1.26	168.95	34	834	0.58	0.061	0.03	13.69	0.03	0.000
7.10	1.93	134.15	1.26	168.76	34	834	0.58	0.061	0.03	13.69	0.03	0.000
7.11	1.93	133.86	1.26	168.57	34	834	0.58	0.061	0.03	13.69	0.03	0.000
7.12	1.94	133.58	1.26	168.38	34	835	0.58	0.061	0.03	13.69	0.03	0.000
7.13	1.94	133.31	1.26	168.20	34	835	0.58	0.061	0.03	13.69	0.03	0.000
7.14	1.94	133.15	1.26	168.09	34	836	0.58	0.061	0.03	13.69	0.03	0.000
7.15	1.94	133.12	1.26	168.10	34	837	0.58	0.061	0.03	13.69	0.03	0.000
7.16	1.94	133.25	1.26	168.25	34	838	0.58	0.061	0.03	13.69	0.03	0.000
7.17	1.94	133.46	1.26	168.47	34	840	0.58	0.061	0.03	13.69	0.03	0.000
7.18	1.94	133.70	1.26	168.73	34	842	0.58	0.060	0.03	13.69	0.03	0.000
7.19	1.94	133.96	1.26	169.00	34	844	0.58	0.060	0.03	13.69	0.03	0.000
7.20	1.94	134.21	1.26	169.26	34	845	0.58	0.060	0.03	13.69	0.03	0.000

:: Post-earthquake settlement of dry sands :: (continued)												
Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _r (%)	Settle. (in)
7.21	1.94	134.43	1.26	169.50	34	847	0.58	0.060	0.03	13.69	0.03	0.000
7.22	1.94	134.62	1.26	169.70	34	849	0.58	0.060	0.03	13.69	0.03	0.000
7.23	1.94	134.83	1.26	169.90	35	850	0.58	0.060	0.03	13.69	0.03	0.000
7.24	1.93	135.12	1.26	170.15	35	852	0.58	0.059	0.03	13.69	0.03	0.000
7.25	1.93	135.53	1.26	170.50	35	854	0.58	0.059	0.03	13.69	0.03	0.000
7.26	1.93	136.03	1.26	170.92	35	856	0.58	0.059	0.03	13.69	0.03	0.000
7.27	1.93	136.57	1.25	171.37	35	858	0.58	0.059	0.03	13.69	0.03	0.000
7.28	1.92	137.12	1.25	171.83	35	860	0.58	0.058	0.03	13.69	0.03	0.000
7.29	1.92	137.65	1.25	172.27	35	862	0.58	0.058	0.03	13.69	0.02	0.000
7.30	1.92	138.12	1.25	172.66	35	864	0.58	0.058	0.03	13.69	0.02	0.000
7.31	1.92	138.52	1.25	172.99	35	866	0.58	0.058	0.03	13.69	0.02	0.000
7.32	1.92	138.94	1.25	173.34	35	868	0.58	0.058	0.03	13.69	0.02	0.000
7.33	1.91	139.44	1.25	173.77	35	870	0.58	0.057	0.03	13.69	0.02	0.000
7.34	1.91	140.07	1.24	174.33	35	872	0.58	0.057	0.03	13.69	0.02	0.000
7.35	1.91	140.80	1.24	174.97	35	875	0.58	0.057	0.03	13.69	0.02	0.000
7.36	1.91	141.56	1.24	175.64	35	878	0.58	0.056	0.03	13.69	0.02	0.000
7.37	1.90	142.33	1.24	176.31	35	881	0.58	0.056	0.03	13.69	0.02	0.000
7.38	1.90	143.05	1.24	176.93	35	884	0.58	0.056	0.03	13.69	0.02	0.000
7.39	1.90	143.68	1.24	177.47	36	887	0.58	0.055	0.03	13.69	0.02	0.000
7.40	1.90	144.22	1.23	177.93	36	889	0.58	0.055	0.03	13.69	0.02	0.000
7.41	1.89	144.76	1.23	178.39	36	892	0.58	0.055	0.03	13.69	0.02	0.000
7.42	1.89	145.39	1.23	178.93	36	894	0.58	0.055	0.03	13.69	0.02	0.000
7.43	1.89	146.14	1.23	179.58	36	897	0.58	0.054	0.03	13.69	0.02	0.000
7.44	1.88	146.98	1.23	180.30	36	901	0.58	0.054	0.03	13.69	0.02	0.000
7.45	1.88	147.85	1.22	181.03	36	904	0.58	0.053	0.03	13.69	0.02	0.000
7.46	1.88	148.70	1.22	181.74	36	907	0.58	0.053	0.03	13.69	0.02	0.000
7.47	1.88	149.49	1.22	182.39	36	910	0.58	0.053	0.03	13.69	0.02	0.000
7.48	1.87	150.15	1.22	182.94	36	913	0.58	0.052	0.03	13.69	0.02	0.000
7.49	1.87	150.71	1.22	183.42	36	916	0.58	0.052	0.03	13.69	0.02	0.000
7.50	1.87	151.26	1.22	183.93	36	918	0.58	0.052	0.03	13.69	0.02	0.000
7.51	1.87	151.88	1.22	184.55	37	922	0.58	0.052	0.02	13.69	0.02	0.000
7.52	1.87	152.62	1.21	185.27	37	926	0.58	0.051	0.02	13.69	0.02	0.000
7.53	1.87	153.41	1.21	186.06	37	930	0.58	0.051	0.02	13.69	0.02	0.000
7.54	1.86	154.21	1.21	186.85	37	934	0.58	0.050	0.02	13.69	0.02	0.000
7.55	1.86	154.98	1.21	187.61	37	938	0.58	0.050	0.02	13.69	0.02	0.000
7.56	1.86	155.68	1.21	188.29	37	942	0.58	0.049	0.02	13.69	0.02	0.000
7.57	1.86	156.27	1.21	188.87	37	945	0.58	0.049	0.02	13.69	0.02	0.000
7.58	1.86	156.82	1.21	189.41	37	949	0.58	0.049	0.02	13.69	0.02	0.000
7.59	1.86	157.43	1.21	190.01	38	952	0.58	0.048	0.02	13.69	0.02	0.000
7.60	1.86	158.18	1.21	190.74	38	956	0.58	0.048	0.02	13.69	0.02	0.000
7.61	1.85	159.04	1.20	191.57	38	960	0.58	0.048	0.02	13.69	0.02	0.000
7.62	1.85	159.94	1.20	192.44	38	965	0.58	0.047	0.02	13.69	0.02	0.000
7.63	1.85	160.84	1.20	193.31	38	970	0.58	0.047	0.02	13.69	0.02	0.000
7.64	1.85	161.69	1.20	194.13	38	974	0.58	0.046	0.02	13.69	0.02	0.000
7.65	1.85	162.43	1.20	194.84	38	978	0.58	0.046	0.02	13.69	0.02	0.000
7.66	1.85	163.03	1.20	195.44	38	982	0.58	0.046	0.02	13.69	0.02	0.000
7.67	1.85	163.56	1.20	196.02	39	985	0.58	0.045	0.02	13.69	0.02	0.000
7.68	1.85	164.11	1.20	196.68	39	989	0.58	0.045	0.02	13.69	0.02	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
7.69	1.85	164.75	1.20	197.47	39	994	0.58	0.045	0.02	13.69	0.02	0.000
7.70	1.85	165.47	1.20	198.35	39	999	0.58	0.044	0.02	13.69	0.02	0.000
7.71	1.85	166.22	1.20	199.26	39	1005	0.58	0.044	0.02	13.69	0.02	0.000
7.72	1.85	166.95	1.20	200.15	39	1010	0.58	0.043	0.02	13.69	0.02	0.000
7.73	1.85	167.61	1.20	200.97	40	1015	0.58	0.043	0.02	13.69	0.02	0.000
7.74	1.85	168.18	1.20	201.67	40	1020	0.58	0.043	0.02	13.69	0.02	0.000
7.75	1.85	168.62	1.20	202.23	40	1023	0.58	0.042	0.02	13.69	0.02	0.000
7.76	1.85	168.99	1.20	202.73	40	1027	0.58	0.042	0.02	13.69	0.02	0.000
7.77	1.85	169.38	1.20	203.26	40	1030	0.58	0.042	0.02	13.69	0.02	0.000
7.78	1.85	169.84	1.20	203.89	40	1034	0.58	0.042	0.02	13.69	0.01	0.000
7.79	1.85	170.35	1.20	204.57	40	1039	0.58	0.041	0.02	13.69	0.01	0.000
7.80	1.85	170.86	1.20	205.26	40	1043	0.58	0.041	0.02	13.69	0.01	0.000
7.81	1.85	171.35	1.20	205.92	41	1047	0.58	0.041	0.02	13.69	0.01	0.000
7.82	1.85	171.78	1.20	206.51	41	1051	0.58	0.040	0.02	13.69	0.01	0.000
7.83	1.85	172.13	1.20	206.98	41	1055	0.58	0.040	0.02	13.69	0.01	0.000
7.84	1.85	172.39	1.20	207.30	41	1057	0.58	0.040	0.02	13.69	0.01	0.000
7.85	1.85	172.62	1.20	207.55	41	1059	0.58	0.040	0.02	13.69	0.01	0.000
7.86	1.85	172.87	1.20	207.80	41	1061	0.58	0.040	0.02	13.69	0.01	0.000
7.87	1.85	173.18	1.20	208.09	41	1063	0.58	0.040	0.02	13.69	0.01	0.000
7.88	1.85	173.50	1.20	208.41	41	1066	0.58	0.040	0.02	13.69	0.01	0.000
7.89	1.85	173.82	1.20	208.72	41	1068	0.58	0.040	0.02	13.69	0.01	0.000
7.90	1.85	174.12	1.20	209.01	41	1070	0.58	0.040	0.02	13.69	0.01	0.000
7.91	1.85	174.38	1.20	209.25	41	1072	0.58	0.039	0.02	13.69	0.01	0.000
7.92	1.85	174.52	1.20	209.40	41	1073	0.58	0.039	0.02	13.69	0.01	0.000
7.93	1.85	174.54	1.20	209.46	41	1075	0.58	0.039	0.02	13.69	0.01	0.000
7.94	1.85	174.47	1.20	209.47	41	1076	0.58	0.039	0.02	13.69	0.01	0.000
7.95	1.85	174.38	1.20	209.47	41	1077	0.58	0.039	0.02	13.69	0.01	0.000
7.96	1.85	174.29	1.20	209.48	41	1078	0.58	0.039	0.02	13.69	0.01	0.000
7.97	1.85	174.21	1.20	209.49	41	1079	0.58	0.039	0.02	13.69	0.01	0.000
7.98	1.85	174.12	1.20	209.50	41	1080	0.58	0.039	0.02	13.69	0.01	0.000
7.99	1.85	174.03	1.20	209.50	41	1081	0.58	0.039	0.02	13.69	0.01	0.000

Total estimated settlement: 0.10**Abbreviations**

Q_{tn}: Equivalent clean sand normalized cone resistance
 K_c: Fines correction factor
 Q_{tn,cs}: Post-liquefaction volumetric strain
 G_{max}: Small strain shear modulus
 CSR: Soil cyclic stress ratio
 γ: Cyclic shear strain
 e_{vol(15)}: Volumetric strain after 15 cycles
 N_c: Equivalent number of cycles
 e_v: Volumetric strain
 Settle.: Calculated settlement

:: Post-earthquake settlement due to soil liquefaction ::

Depth (ft)	Q _{tn,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	Q _{tn,cs}	FS	e _v (%)	DF	Settlement (in)
8.00	209.49	2.00	0.00	0.85	0.00	8.01	209.55	2.00	0.00	0.85	0.00
8.02	209.64	2.00	0.00	0.85	0.00	8.03	209.79	2.00	0.00	0.85	0.00
8.04	209.96	2.00	0.00	0.85	0.00	8.05	210.14	2.00	0.00	0.85	0.00
8.06	210.33	2.00	0.00	0.85	0.00	8.07	210.51	2.00	0.00	0.85	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
8.08	210.66	2.00	0.00	0.85	0.00	8.09	210.79	2.00	0.00	0.85	0.00
8.10	210.92	2.00	0.00	0.85	0.00	8.11	211.08	2.00	0.00	0.85	0.00
8.12	211.29	2.00	0.00	0.85	0.00	8.13	211.54	2.00	0.00	0.85	0.00
8.14	211.79	2.00	0.00	0.85	0.00	8.15	212.04	2.00	0.00	0.85	0.00
8.16	212.27	2.00	0.00	0.85	0.00	8.17	212.47	2.00	0.00	0.85	0.00
8.18	212.64	2.00	0.00	0.85	0.00	8.19	212.82	2.00	0.00	0.85	0.00
8.20	213.03	2.00	0.00	0.85	0.00	8.21	213.29	2.00	0.00	0.85	0.00
8.22	213.56	2.00	0.00	0.85	0.00	8.23	213.82	2.00	0.00	0.85	0.00
8.24	214.07	2.00	0.00	0.85	0.00	8.25	214.28	2.00	0.00	0.85	0.00
8.26	214.45	2.00	0.00	0.85	0.00	8.27	214.66	2.00	0.00	0.85	0.00
8.28	214.96	2.00	0.00	0.85	0.00	8.29	215.39	2.00	0.00	0.85	0.00
8.30	215.87	2.00	0.00	0.85	0.00	8.31	216.38	2.00	0.00	0.85	0.00
8.32	216.88	2.00	0.00	0.85	0.00	8.33	217.34	2.00	0.00	0.85	0.00
8.34	217.75	2.00	0.00	0.85	0.00	8.35	218.08	2.00	0.00	0.85	0.00
8.36	218.40	2.00	0.00	0.85	0.00	8.37	218.76	2.00	0.00	0.85	0.00
8.38	219.19	2.00	0.00	0.85	0.00	8.39	219.66	2.00	0.00	0.85	0.00
8.40	220.16	2.00	0.00	0.85	0.00	8.41	220.64	2.00	0.00	0.85	0.00
8.42	221.09	2.00	0.00	0.85	0.00	8.43	221.48	2.00	0.00	0.85	0.00
8.44	221.78	2.00	0.00	0.85	0.00	8.45	222.06	2.00	0.00	0.85	0.00
8.46	222.35	2.00	0.00	0.85	0.00	8.47	222.69	2.00	0.00	0.85	0.00
8.48	223.07	2.00	0.00	0.85	0.00	8.49	223.45	2.00	0.00	0.85	0.00
8.50	223.83	2.00	0.00	0.85	0.00	8.51	224.17	2.00	0.00	0.85	0.00
8.52	224.46	2.00	0.00	0.85	0.00	8.53	224.67	2.00	0.00	0.84	0.00
8.54	224.84	2.00	0.00	0.84	0.00	8.55	225.00	2.00	0.00	0.84	0.00
8.56	225.18	2.00	0.00	0.84	0.00	8.57	225.39	2.00	0.00	0.84	0.00
8.58	225.59	2.00	0.00	0.84	0.00	8.59	225.79	2.00	0.00	0.84	0.00
8.60	225.96	2.00	0.00	0.84	0.00	8.61	226.09	2.00	0.00	0.84	0.00
8.62	226.16	2.00	0.00	0.84	0.00	8.63	226.19	2.00	0.00	0.84	0.00
8.64	226.21	2.00	0.00	0.84	0.00	8.65	226.24	2.00	0.00	0.84	0.00
8.66	226.27	2.00	0.00	0.84	0.00	8.67	226.30	2.00	0.00	0.84	0.00
8.68	226.33	2.00	0.00	0.84	0.00	8.69	226.35	2.00	0.00	0.84	0.00
8.70	226.28	2.00	0.00	0.84	0.00	8.71	226.07	2.00	0.00	0.84	0.00
8.72	225.71	2.00	0.00	0.84	0.00	8.73	225.27	2.00	0.00	0.84	0.00
8.74	224.79	2.00	0.00	0.84	0.00	8.75	224.30	2.00	0.00	0.84	0.00
8.76	223.81	2.00	0.00	0.84	0.00	8.77	223.35	2.00	0.00	0.84	0.00
8.78	222.94	2.00	0.00	0.84	0.00	8.79	222.59	2.00	0.00	0.84	0.00
8.80	222.25	2.00	0.00	0.84	0.00	8.81	221.88	2.00	0.00	0.84	0.00
8.82	221.47	2.00	0.00	0.84	0.00	8.83	221.04	2.00	0.00	0.84	0.00
8.84	220.60	2.00	0.00	0.84	0.00	8.85	220.18	2.00	0.00	0.84	0.00
8.86	219.79	2.00	0.00	0.84	0.00	8.87	219.50	2.00	0.00	0.84	0.00
8.88	219.36	2.00	0.00	0.84	0.00	8.89	219.36	2.00	0.00	0.84	0.00
8.90	219.43	2.00	0.00	0.84	0.00	8.91	219.50	2.00	0.00	0.84	0.00
8.92	219.56	2.00	0.00	0.84	0.00	8.93	219.61	2.00	0.00	0.84	0.00
8.94	219.64	2.00	0.00	0.84	0.00	8.95	219.66	2.00	0.00	0.84	0.00
8.96	219.61	2.00	0.00	0.84	0.00	8.97	219.48	2.00	0.00	0.84	0.00
8.98	219.26	2.00	0.00	0.84	0.00	8.99	219.00	2.00	0.00	0.84	0.00
9.00	218.71	2.00	0.00	0.84	0.00	9.01	218.41	2.00	0.00	0.84	0.00
9.02	218.12	2.00	0.00	0.84	0.00	9.03	217.83	2.00	0.00	0.84	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
9.04	217.58	2.00	0.00	0.84	0.00	9.05	217.41	2.00	0.00	0.84	0.00
9.06	217.31	2.00	0.00	0.84	0.00	9.07	217.25	2.00	0.00	0.84	0.00
9.08	217.18	2.00	0.00	0.83	0.00	9.09	217.10	2.00	0.00	0.83	0.00
9.10	217.02	2.00	0.00	0.83	0.00	9.11	216.92	2.00	0.00	0.83	0.00
9.12	216.82	2.00	0.00	0.83	0.00	9.13	216.75	2.00	0.00	0.83	0.00
9.14	216.75	2.00	0.00	0.83	0.00	9.15	216.83	2.00	0.00	0.83	0.00
9.16	216.97	2.00	0.00	0.83	0.00	9.17	217.12	2.00	0.00	0.83	0.00
9.18	217.27	2.00	0.00	0.83	0.00	9.19	217.42	2.00	0.00	0.83	0.00
9.20	217.55	2.00	0.00	0.83	0.00	9.21	217.66	2.00	0.00	0.83	0.00
9.22	217.74	2.00	0.00	0.83	0.00	9.23	217.82	2.00	0.00	0.83	0.00
9.24	217.92	2.00	0.00	0.83	0.00	9.25	218.04	2.00	0.00	0.83	0.00
9.26	218.18	2.00	0.00	0.83	0.00	9.27	218.32	2.00	0.00	0.83	0.00
9.28	218.46	2.00	0.00	0.83	0.00	9.29	218.58	2.00	0.00	0.83	0.00
9.30	218.69	2.00	0.00	0.83	0.00	9.31	218.82	2.00	0.00	0.83	0.00
9.32	219.01	2.00	0.00	0.83	0.00	9.33	219.26	2.00	0.00	0.83	0.00
9.34	219.55	2.00	0.00	0.83	0.00	9.35	219.86	2.00	0.00	0.83	0.00
9.36	220.15	2.00	0.00	0.83	0.00	9.37	220.42	2.00	0.00	0.83	0.00
9.38	220.65	2.00	0.00	0.83	0.00	9.39	220.84	2.00	0.00	0.83	0.00
9.40	221.04	2.00	0.00	0.83	0.00	9.41	221.27	2.00	0.00	0.83	0.00
9.42	221.54	2.00	0.00	0.83	0.00	9.43	221.82	2.00	0.00	0.83	0.00
9.44	222.09	2.00	0.00	0.83	0.00	9.45	222.32	2.00	0.00	0.83	0.00
9.46	222.51	2.00	0.00	0.83	0.00	9.47	222.65	2.00	0.00	0.83	0.00
9.48	222.77	2.00	0.00	0.83	0.00	9.49	222.90	2.00	0.00	0.83	0.00
9.50	223.08	2.00	0.00	0.83	0.00	9.51	223.28	2.00	0.00	0.83	0.00
9.52	223.48	2.00	0.00	0.83	0.00	9.53	223.67	2.00	0.00	0.83	0.00
9.54	223.83	2.00	0.00	0.83	0.00	9.55	223.96	2.00	0.00	0.83	0.00
9.56	223.98	2.00	0.00	0.83	0.00	9.57	223.53	2.00	0.00	0.83	0.00
9.58	222.53	2.00	0.00	0.83	0.00	9.59	220.99	2.00	0.00	0.83	0.00
9.60	219.25	2.00	0.00	0.83	0.00	9.61	217.42	2.00	0.00	0.83	0.00
9.62	215.57	2.00	0.00	0.83	0.00	9.63	213.81	2.00	0.00	0.82	0.00
9.64	212.22	2.00	0.00	0.82	0.00	9.65	211.00	2.00	0.00	0.82	0.00
9.66	210.20	2.00	0.00	0.82	0.00	9.67	209.71	2.00	0.00	0.82	0.00
9.68	209.29	2.00	0.00	0.82	0.00	9.69	208.83	2.00	0.00	0.82	0.00
9.70	208.35	2.00	0.00	0.82	0.00	9.71	207.86	2.00	0.00	0.82	0.00
9.72	207.39	2.00	0.00	0.82	0.00	9.73	206.96	2.00	0.00	0.82	0.00
9.74	206.36	2.00	0.00	0.82	0.00	9.75	205.42	2.00	0.00	0.82	0.00
9.76	203.99	2.00	0.00	0.82	0.00	9.77	202.23	2.00	0.00	0.82	0.00
9.78	200.24	2.00	0.00	0.82	0.00	9.79	198.10	1.25	0.15	0.82	0.00
9.80	195.92	1.21	0.21	0.82	0.00	9.81	193.84	1.18	0.21	0.82	0.00
9.82	192.08	1.15	0.21	0.82	0.00	9.83	190.98	1.13	0.30	0.82	0.00
9.84	190.09	1.12	0.30	0.82	0.00	9.85	188.75	1.10	0.30	0.82	0.00
9.86	186.45	1.06	0.30	0.82	0.00	9.87	183.37	1.01	0.41	0.82	0.00
9.88	179.86	0.96	0.42	0.82	0.00	9.89	176.27	0.91	0.56	0.82	0.00
9.90	172.94	0.87	0.57	0.82	0.00	9.91	170.80	0.84	0.76	0.82	0.00
9.92	170.45	0.84	0.76	0.82	0.00	9.93	171.85	0.86	0.58	0.82	0.00
9.94	174.20	0.89	0.56	0.82	0.00	9.95	176.85	0.92	0.55	0.82	0.00
9.96	179.66	0.96	0.42	0.82	0.00	9.97	182.49	1.00	0.41	0.82	0.00
9.98	185.19	1.04	0.41	0.82	0.00	9.99	187.59	1.07	0.30	0.82	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
10.00	188.87	1.09	0.30	0.82	0.00	10.01	188.93	1.09	0.30	0.82	0.00
10.02	187.87	1.07	0.30	0.82	0.00	10.03	186.54	1.05	0.30	0.82	0.00
10.04	185.10	1.03	0.41	0.82	0.00	10.05	183.63	1.01	0.41	0.82	0.00
10.06	182.21	0.99	0.41	0.82	0.00	10.07	180.90	0.97	0.42	0.82	0.00
10.08	179.71	2.00	0.00	0.82	0.00	10.09	178.27	2.00	0.00	0.82	0.00
10.10	176.39	2.00	0.00	0.82	0.00	10.11	173.96	2.00	0.00	0.82	0.00
10.12	171.26	2.00	0.00	0.82	0.00	10.13	168.45	2.00	0.00	0.82	0.00
10.14	165.67	2.00	0.00	0.82	0.00	10.15	163.07	2.00	0.00	0.82	0.00
10.16	160.76	2.00	0.00	0.82	0.00	10.17	159.07	2.00	0.00	0.82	0.00
10.18	158.08	2.00	0.00	0.81	0.00	10.19	157.68	2.00	0.00	0.81	0.00
10.20	157.54	2.00	0.00	0.81	0.00	10.21	157.48	2.00	0.00	0.81	0.00
10.22	157.50	2.00	0.00	0.81	0.00	10.23	157.60	2.00	0.00	0.81	0.00
10.24	157.74	2.00	0.00	0.81	0.00	10.25	157.90	2.00	0.00	0.81	0.00
10.26	158.30	2.00	0.00	0.81	0.00	10.27	159.06	2.00	0.00	0.81	0.00
10.28	160.24	2.00	0.00	0.81	0.00	10.29	161.62	2.00	0.00	0.81	0.00
10.30	163.08	2.00	0.00	0.81	0.00	10.31	164.52	2.00	0.00	0.81	0.00
10.32	165.84	2.00	0.00	0.81	0.00	10.33	166.98	2.00	0.00	0.81	0.00
10.34	167.91	2.00	0.00	0.81	0.00	10.35	168.82	2.00	0.00	0.81	0.00
10.36	160.86	2.00	0.00	0.81	0.00	10.37	169.16	2.00	0.00	0.81	0.00
10.38	178.93	2.00	0.00	0.81	0.00	10.39	189.78	2.00	0.00	0.81	0.00
10.40	201.22	2.00	0.00	0.81	0.00	10.41	212.69	2.00	0.00	0.81	0.00
10.42	223.48	2.00	0.00	0.81	0.00	10.43	232.30	2.00	0.00	0.81	0.00
10.44	239.02	2.00	0.00	0.81	0.00	10.45	244.43	2.00	0.00	0.81	0.00
10.46	250.09	2.00	0.00	0.81	0.00	10.47	256.40	2.00	0.00	0.81	0.00
10.48	263.05	2.00	0.00	0.81	0.00	10.49	269.71	2.00	0.00	0.81	0.00
10.50	276.05	2.00	0.00	0.81	0.00	10.51	281.68	2.00	0.00	0.81	0.00
10.52	285.76	2.00	0.00	0.81	0.00	10.53	288.57	2.00	0.00	0.81	0.00
10.54	290.57	2.00	0.00	0.81	0.00	10.55	292.78	2.00	0.00	0.81	0.00
10.56	295.16	2.00	0.00	0.81	0.00	10.57	297.48	2.00	0.00	0.81	0.00
10.58	299.86	2.00	0.00	0.81	0.00	10.59	302.07	2.00	0.00	0.81	0.00
10.60	303.50	2.00	0.00	0.81	0.00	10.61	302.52	2.00	0.00	0.81	0.00
10.62	298.89	2.00	0.00	0.81	0.00	10.63	293.18	2.00	0.00	0.81	0.00
10.64	286.71	2.00	0.00	0.81	0.00	10.65	280.01	2.00	0.00	0.81	0.00
10.66	273.41	2.00	0.00	0.81	0.00	10.67	267.26	2.00	0.00	0.81	0.00
10.68	261.86	2.00	0.00	0.81	0.00	10.69	256.43	2.00	0.00	0.81	0.00
10.70	249.57	2.00	0.00	0.81	0.00	10.71	240.51	2.00	0.00	0.81	0.00
10.72	229.71	2.00	0.00	0.81	0.00	10.73	218.31	2.00	0.00	0.80	0.00
10.74	206.99	2.00	0.00	0.80	0.00	10.75	196.32	2.00	0.00	0.80	0.00
10.76	186.78	2.00	0.00	0.80	0.00	10.77	178.75	2.00	0.00	0.80	0.00
10.78	171.49	2.00	0.00	0.80	0.00	10.79	178.19	2.00	0.00	0.80	0.00
10.80	177.05	2.00	0.00	0.80	0.00	10.81	175.69	2.00	0.00	0.80	0.00
10.82	174.18	2.00	0.00	0.80	0.00	10.83	172.59	2.00	0.00	0.80	0.00
10.84	171.01	2.00	0.00	0.80	0.00	10.85	169.52	2.00	0.00	0.80	0.00
10.86	168.26	2.00	0.00	0.80	0.00	10.87	167.21	2.00	0.00	0.80	0.00
10.88	166.25	2.00	0.00	0.80	0.00	10.89	165.22	2.00	0.00	0.80	0.00
10.90	164.04	2.00	0.00	0.80	0.00	10.91	162.80	2.00	0.00	0.80	0.00
10.92	161.54	2.00	0.00	0.80	0.00	10.93	160.36	2.00	0.00	0.80	0.00
10.94	159.30	2.00	0.00	0.80	0.00	10.95	158.42	2.00	0.00	0.80	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
10.96	157.62	2.00	0.00	0.80	0.00	10.97	156.80	2.00	0.00	0.80	0.00
10.98	155.88	2.00	0.00	0.80	0.00	10.99	154.90	2.00	0.00	0.80	0.00
11.00	153.92	2.00	0.00	0.80	0.00	11.01	153.01	2.00	0.00	0.80	0.00
11.02	152.20	2.00	0.00	0.80	0.00	11.03	151.53	2.00	0.00	0.80	0.00
11.04	150.97	2.00	0.00	0.80	0.00	11.05	150.43	2.00	0.00	0.80	0.00
11.06	149.85	2.00	0.00	0.80	0.00	11.07	149.19	2.00	0.00	0.80	0.00
11.08	148.52	2.00	0.00	0.80	0.00	11.09	147.86	2.00	0.00	0.80	0.00
11.10	147.25	2.00	0.00	0.80	0.00	11.11	146.71	2.00	0.00	0.80	0.00
11.12	146.24	2.00	0.00	0.80	0.00	11.13	145.71	2.00	0.00	0.80	0.00
11.14	145.05	0.54	1.37	0.80	0.00	11.15	144.23	0.53	1.38	0.80	0.00
11.16	143.31	0.52	1.39	0.80	0.00	11.17	142.34	0.51	1.39	0.80	0.00
11.18	141.38	0.50	1.40	0.80	0.00	11.19	140.47	0.50	1.41	0.80	0.00
11.20	139.66	0.49	1.41	0.80	0.00	11.21	138.99	0.48	1.42	0.80	0.00
11.22	138.41	2.00	0.00	0.80	0.00	11.23	137.84	2.00	0.00	0.80	0.00
11.24	137.20	2.00	0.00	0.80	0.00	11.25	136.51	2.00	0.00	0.80	0.00
11.26	135.81	2.00	0.00	0.80	0.00	11.27	135.12	2.00	0.00	0.80	0.00
11.28	134.49	2.00	0.00	0.79	0.00	11.29	133.93	2.00	0.00	0.79	0.00
11.30	133.52	2.00	0.00	0.79	0.00	11.31	133.22	2.00	0.00	0.79	0.00
11.32	132.98	2.00	0.00	0.79	0.00	11.33	132.75	2.00	0.00	0.79	0.00
11.34	132.53	2.00	0.00	0.79	0.00	11.35	132.34	2.00	0.00	0.79	0.00
11.36	132.19	2.00	0.00	0.79	0.00	11.37	132.07	2.00	0.00	0.79	0.00
11.38	132.01	2.00	0.00	0.79	0.00	11.39	132.01	2.00	0.00	0.79	0.00
11.40	132.10	2.00	0.00	0.79	0.00	11.41	132.29	2.00	0.00	0.79	0.00
11.42	132.54	2.00	0.00	0.79	0.00	11.43	132.86	2.00	0.00	0.79	0.00
11.44	133.22	2.00	0.00	0.79	0.00	11.45	133.59	2.00	0.00	0.79	0.00
11.46	133.94	2.00	0.00	0.79	0.00	11.47	134.34	2.00	0.00	0.79	0.00
11.48	134.87	2.00	0.00	0.79	0.00	11.49	135.61	2.00	0.00	0.79	0.00
11.50	136.52	2.00	0.00	0.79	0.00	11.51	137.51	2.00	0.00	0.79	0.00
11.52	138.53	2.00	0.00	0.79	0.00	11.53	139.51	2.00	0.00	0.79	0.00
11.54	140.40	2.00	0.00	0.79	0.00	11.55	141.16	2.00	0.00	0.79	0.00
11.56	141.89	2.00	0.00	0.79	0.00	11.57	142.71	2.00	0.00	0.79	0.00
11.58	143.72	2.00	0.00	0.79	0.00	11.59	144.85	2.00	0.00	0.79	0.00
11.60	146.02	2.00	0.00	0.79	0.00	11.61	146.94	2.00	0.00	0.79	0.00
11.62	156.87	2.00	0.00	0.79	0.00	11.63	166.47	2.00	0.00	0.79	0.00
11.64	174.84	2.00	0.00	0.79	0.00	11.65	181.77	2.00	0.00	0.79	0.00
11.66	188.01	2.00	0.00	0.79	0.00	11.67	194.72	2.00	0.00	0.79	0.00
11.68	202.45	2.00	0.00	0.79	0.00	11.69	210.83	2.00	0.00	0.79	0.00
11.70	219.49	2.00	0.00	0.79	0.00	11.71	227.88	2.00	0.00	0.79	0.00
11.72	235.67	2.00	0.00	0.79	0.00	11.73	241.14	2.00	0.00	0.79	0.00
11.74	243.81	2.00	0.00	0.79	0.00	11.75	244.07	2.00	0.00	0.79	0.00
11.76	243.68	2.00	0.00	0.79	0.00	11.77	243.25	2.00	0.00	0.79	0.00
11.78	242.81	2.00	0.00	0.79	0.00	11.79	242.38	2.00	0.00	0.79	0.00
11.80	242.00	2.00	0.00	0.79	0.00	11.81	241.70	2.00	0.00	0.79	0.00
11.82	241.66	2.00	0.00	0.79	0.00	11.83	241.91	2.00	0.00	0.78	0.00
11.84	242.43	2.00	0.00	0.78	0.00	11.85	243.08	2.00	0.00	0.78	0.00
11.86	243.83	2.00	0.00	0.78	0.00	11.87	244.68	2.00	0.00	0.78	0.00
11.88	245.57	2.00	0.00	0.78	0.00	11.89	246.47	2.00	0.00	0.78	0.00
11.90	246.85	2.00	0.00	0.78	0.00	11.91	245.73	2.00	0.00	0.78	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
11.92	242.87	2.00	0.00	0.78	0.00	11.93	238.65	2.00	0.00	0.78	0.00
11.94	233.95	2.00	0.00	0.78	0.00	11.95	229.04	2.00	0.00	0.78	0.00
11.96	224.19	2.00	0.00	0.78	0.00	11.97	219.63	2.00	0.00	0.78	0.00
11.98	215.61	2.00	0.00	0.78	0.00	11.99	212.66	2.00	0.00	0.78	0.00
12.00	210.66	2.00	0.00	0.78	0.00	12.01	209.29	2.00	0.00	0.78	0.00
12.02	207.90	2.00	0.00	0.78	0.00	12.03	206.41	2.00	0.00	0.78	0.00
12.04	204.89	2.00	0.00	0.78	0.00	12.05	203.45	2.00	0.00	0.78	0.00
12.06	202.15	2.00	0.00	0.78	0.00	12.07	201.19	2.00	0.00	0.78	0.00
12.08	202.89	2.00	0.00	0.78	0.00	12.09	207.94	2.00	0.00	0.78	0.00
12.10	217.03	2.00	0.00	0.78	0.00	12.11	228.44	2.00	0.00	0.78	0.00
12.12	242.06	2.00	0.00	0.78	0.00	12.13	116.45	1.66	0.00	0.78	0.00
12.14	114.77	1.57	0.00	0.78	0.00	12.15	113.17	1.48	0.00	0.78	0.00
12.16	111.91	1.41	0.00	0.78	0.00	12.17	111.26	1.37	0.00	0.78	0.00
12.18	111.17	1.34	0.01	0.78	0.00	12.19	111.37	1.32	0.01	0.78	0.00
12.20	111.58	1.29	0.01	0.78	0.00	12.21	111.76	1.27	0.01	0.78	0.00
12.22	111.92	1.24	0.01	0.78	0.00	12.23	112.05	1.22	0.01	0.78	0.00
12.24	112.14	1.20	0.01	0.78	0.00	12.25	112.26	1.18	0.01	0.78	0.00
12.26	112.45	1.16	0.01	0.78	0.00	12.27	112.73	1.15	0.01	0.78	0.00
12.28	113.05	1.12	0.01	0.78	0.00	12.29	113.36	1.10	0.01	0.78	0.00
12.30	113.64	1.08	0.01	0.78	0.00	12.31	113.87	1.05	0.01	0.78	0.00
12.32	114.04	1.03	0.01	0.78	0.00	12.33	114.15	1.01	0.01	0.78	0.00
12.34	114.23	0.99	0.02	0.78	0.00	12.35	114.25	0.97	0.02	0.78	0.00
12.36	114.19	0.95	0.02	0.78	0.00	12.37	114.08	0.92	0.02	0.78	0.00
12.38	113.91	0.90	0.02	0.77	0.00	12.39	113.68	0.87	0.02	0.77	0.00
12.40	113.41	0.84	0.03	0.77	0.00	12.41	113.11	0.82	0.39	0.77	0.00
12.42	112.83	0.80	0.39	0.77	0.00	12.43	112.61	0.78	0.39	0.77	0.00
12.44	112.43	0.77	0.39	0.77	0.00	12.45	112.22	0.75	0.39	0.77	0.00
12.46	111.97	0.73	0.39	0.77	0.00	12.47	111.67	0.72	0.39	0.77	0.00
12.48	111.34	0.70	0.39	0.77	0.00	12.49	111.00	0.68	0.39	0.77	0.00
12.50	110.67	0.66	0.39	0.77	0.00	12.51	110.40	0.65	0.39	0.77	0.00
12.52	110.19	0.64	0.39	0.77	0.00	12.53	110.02	0.64	0.39	0.77	0.00
12.54	109.83	0.63	0.39	0.77	0.00	12.55	109.61	0.62	0.39	0.77	0.00
12.56	109.38	0.61	0.39	0.77	0.00	12.57	109.14	0.60	0.39	0.77	0.00
12.58	108.91	0.59	0.39	0.77	0.00	12.59	108.71	0.58	0.39	0.77	0.00
12.60	108.58	0.58	0.39	0.77	0.00	12.61	108.52	0.58	0.39	0.77	0.00
12.62	108.51	0.58	0.39	0.77	0.00	12.63	108.49	0.58	0.39	0.77	0.00
12.64	108.48	0.58	0.39	0.77	0.00	12.65	108.47	0.58	0.39	0.77	0.00
12.66	108.45	0.58	0.38	0.77	0.00	12.67	108.44	0.57	0.38	0.77	0.00
12.68	108.39	0.57	0.38	0.77	0.00	12.69	108.25	0.57	0.38	0.77	0.00
12.70	108.00	0.57	0.38	0.77	0.00	12.71	107.66	0.57	0.38	0.77	0.00
12.72	107.28	0.57	0.38	0.77	0.00	12.73	106.88	0.57	0.38	0.77	0.00
12.74	106.48	0.57	0.38	0.77	0.00	12.75	106.11	0.57	0.38	0.77	0.00
12.76	105.77	0.57	0.38	0.77	0.00	12.77	105.44	0.57	0.38	0.77	0.00
12.78	105.07	0.57	0.38	0.77	0.00	12.79	104.59	0.57	0.38	0.77	0.00
12.80	104.03	0.57	0.38	0.77	0.00	12.81	103.42	0.57	0.38	0.77	0.00
12.82	102.79	0.57	0.38	0.77	0.00	12.83	102.17	0.57	0.38	0.77	0.00
12.84	101.60	0.57	0.38	0.77	0.00	12.85	101.09	0.57	0.38	0.77	0.00
12.86	100.62	0.57	0.38	0.77	0.00	12.87	100.12	0.57	0.38	0.77	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
12.88	99.53	0.57	0.38	0.77	0.00	12.89	98.85	0.57	0.38	0.77	0.00
12.90	98.13	0.56	0.38	0.77	0.00	12.91	97.39	0.56	0.38	0.77	0.00
12.92	96.68	0.56	0.38	0.77	0.00	12.93	96.03	0.56	0.38	0.76	0.00
12.94	95.46	0.56	0.38	0.76	0.00	12.95	94.89	0.56	0.38	0.76	0.00
12.96	94.26	0.56	0.38	0.76	0.00	12.97	93.49	0.56	0.38	0.76	0.00
12.98	92.64	0.56	0.38	0.76	0.00	12.99	91.74	0.56	0.38	0.76	0.00
13.00	90.84	0.56	0.38	0.76	0.00	13.01	89.99	0.56	0.38	0.76	0.00
13.02	89.22	0.56	0.38	0.76	0.00	13.03	88.46	0.56	0.38	0.76	0.00
13.04	87.55	0.55	0.38	0.76	0.00	13.05	86.40	0.54	0.38	0.76	0.00
13.06	85.03	0.52	0.38	0.76	0.00	13.07	83.55	0.50	0.38	0.76	0.00
13.08	82.02	0.48	0.38	0.76	0.00	13.09	80.52	0.47	0.38	0.76	0.00
13.10	79.13	0.45	0.38	0.76	0.00	13.11	77.92	0.44	0.38	0.76	0.00
13.12	76.78	0.42	0.38	0.76	0.00	13.13	75.56	0.41	0.38	0.76	0.00
13.14	74.07	0.39	0.38	0.76	0.00	13.15	72.36	0.36	0.38	0.76	0.00
13.16	70.49	0.34	0.38	0.76	0.00	13.17	68.54	0.31	0.38	0.76	0.00
13.18	66.61	0.29	0.38	0.76	0.00	13.19	64.82	0.26	0.38	0.76	0.00
13.20	63.36	0.25	0.38	0.76	0.00	13.21	62.32	0.23	0.38	0.76	0.00
13.22	61.59	0.23	0.38	0.76	0.00	13.23	60.89	0.22	0.38	0.76	0.00
13.24	60.12	0.21	0.38	0.76	0.00	13.25	59.29	0.20	0.38	0.76	0.00
13.26	58.46	0.19	0.38	0.76	0.00	13.27	57.67	0.18	0.38	0.76	0.00
13.28	56.96	0.18	0.38	0.76	0.00	13.29	56.52	0.17	0.38	0.76	0.00
13.30	56.37	0.17	0.38	0.76	0.00	13.31	56.47	0.17	0.38	0.76	0.00
13.32	56.62	0.17	0.38	0.76	0.00	13.33	56.79	0.17	0.38	0.76	0.00
13.34	56.96	0.17	0.38	0.76	0.00	13.35	57.12	0.17	0.38	0.76	0.00
13.36	57.27	0.17	0.38	0.76	0.00	13.37	57.45	0.17	0.38	0.76	0.00
13.38	58.01	0.17	0.38	0.76	0.00	13.39	59.03	0.18	0.38	0.76	0.00
13.40	60.51	0.20	0.38	0.76	0.00	13.41	62.15	0.21	0.38	0.76	0.00
13.42	63.85	0.23	0.38	0.76	0.00	13.43	65.53	0.24	0.38	0.76	0.00
13.44	67.11	0.26	0.38	0.76	0.00	13.45	68.51	0.27	0.38	0.76	0.00
13.46	69.74	0.29	0.38	0.76	0.00	13.47	71.00	0.30	0.38	0.76	0.00
13.48	72.46	0.32	0.38	0.75	0.00	13.49	74.17	0.34	0.38	0.75	0.00
13.50	76.02	0.37	0.38	0.75	0.00	13.51	77.90	0.39	0.38	0.75	0.00
13.52	79.72	0.41	0.38	0.75	0.00	13.53	81.39	0.44	0.38	0.75	0.00
13.54	82.84	0.46	0.38	0.75	0.00	13.55	83.75	0.47	0.38	0.75	0.00
13.56	84.16	0.47	0.38	0.75	0.00	13.57	84.17	0.47	0.38	0.75	0.00
13.58	84.12	0.46	0.38	0.75	0.00	13.59	84.06	0.46	0.38	0.75	0.00
13.60	83.99	0.45	0.38	0.75	0.00	13.61	83.92	0.45	0.38	0.75	0.00
13.62	83.85	0.44	0.38	0.75	0.00	13.63	83.82	0.44	0.38	0.75	0.00
13.64	84.00	0.43	0.38	0.75	0.00	13.65	84.44	0.43	0.38	0.75	0.00
13.66	85.13	0.43	0.38	0.75	0.00	13.67	85.90	0.43	0.38	0.75	0.00
13.68	86.70	0.43	0.38	0.75	0.00	13.69	87.51	0.43	0.38	0.75	0.00
13.70	88.27	0.43	0.38	0.75	0.00	13.71	88.94	0.43	0.38	0.75	0.00
13.72	89.53	0.43	0.38	0.75	0.00	13.73	90.10	0.44	0.38	0.75	0.00
13.74	90.73	0.45	0.38	0.75	0.00	13.75	91.47	0.46	0.38	0.75	0.00
13.76	92.28	0.47	0.37	0.75	0.00	13.77	93.10	0.48	0.37	0.75	0.00
13.78	93.90	0.50	0.37	0.75	0.00	13.79	94.63	0.51	0.37	0.75	0.00
13.80	95.27	0.52	0.37	0.75	0.00	13.81	95.39	0.52	0.37	0.75	0.00
13.82	94.90	0.52	0.37	0.75	0.00	13.83	93.77	0.51	0.37	0.75	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
13.84	92.40	0.49	0.37	0.75	0.00	13.85	90.92	0.47	0.37	0.75	0.00
13.86	89.39	0.46	0.37	0.75	0.00	13.87	87.90	0.44	0.37	0.75	0.00
13.88	86.52	0.43	0.37	0.75	0.00	13.89	85.37	0.41	0.37	0.75	0.00
13.90	84.53	0.40	0.37	0.75	0.00	13.91	83.92	0.39	0.37	0.75	0.00
13.92	83.35	0.38	0.37	0.75	0.00	13.93	82.68	0.36	0.37	0.75	0.00
13.94	81.92	0.34	0.37	0.75	0.00	13.95	81.10	0.33	0.37	0.75	0.00
13.96	80.27	0.31	0.37	0.75	0.00	13.97	79.48	0.30	0.37	0.75	0.00
13.98	78.97	0.29	0.37	0.75	0.00	13.99	78.91	0.28	0.37	0.75	0.00
14.00	79.31	0.28	0.37	0.75	0.00	14.01	79.94	0.28	0.37	0.75	0.00
14.02	80.64	0.28	0.37	0.75	0.00	14.03	81.35	0.28	0.37	0.74	0.00
14.04	82.05	0.28	0.37	0.74	0.00	14.05	82.70	0.28	0.37	0.74	0.00
14.06	83.27	0.28	0.37	0.74	0.00	14.07	84.08	0.28	0.37	0.74	0.00
14.08	85.34	0.29	0.37	0.74	0.00	14.09	87.16	0.30	0.37	0.74	0.00
14.10	89.29	0.32	0.37	0.74	0.00	14.11	91.58	0.33	0.37	0.74	0.00
14.12	93.91	0.35	0.37	0.74	0.00	14.13	96.17	0.36	0.37	0.74	0.00
14.14	98.23	0.38	0.37	0.74	0.00	14.15	100.02	0.39	0.37	0.74	0.00
14.16	101.74	0.40	0.37	0.74	0.00	14.17	103.62	0.42	0.37	0.74	0.00
14.18	105.86	0.44	0.37	0.74	0.00	14.19	108.37	0.46	0.37	0.74	0.00
14.20	110.99	0.48	0.37	0.74	0.00	14.21	113.61	0.51	0.37	0.74	0.00
14.22	116.08	0.53	0.37	0.74	0.00	14.23	118.29	0.55	0.37	0.74	0.00
14.24	120.06	0.57	0.37	0.74	0.00	14.25	121.52	0.58	0.37	0.74	0.00
14.26	122.85	0.60	0.37	0.74	0.00	14.27	124.30	0.62	0.37	0.74	0.00
14.28	125.87	0.64	0.37	0.74	0.00	14.29	127.46	0.67	0.37	0.74	0.00
14.30	128.99	0.69	0.37	0.74	0.00	14.31	130.40	0.71	0.37	0.74	0.00
14.32	131.60	0.73	0.37	0.74	0.00	14.33	132.50	0.75	0.37	0.74	0.00
14.34	133.18	0.76	0.37	0.74	0.00	14.35	133.76	0.77	0.37	0.74	0.00
14.36	134.41	0.78	0.37	0.74	0.00	14.37	135.10	0.80	0.37	0.74	0.00
14.38	135.78	0.81	0.37	0.74	0.00	14.39	136.42	0.83	0.37	0.74	0.00
14.40	137.00	0.84	0.02	0.74	0.00	14.41	137.48	0.85	0.02	0.74	0.00
14.42	137.87	0.86	0.02	0.74	0.00	14.43	138.25	0.85	0.02	0.74	0.00
14.44	138.65	0.85	0.02	0.74	0.00	14.45	139.09	0.84	0.37	0.74	0.00
14.46	139.54	0.83	0.37	0.74	0.00	14.47	139.97	0.82	0.37	0.74	0.00
14.48	140.36	0.81	0.37	0.74	0.00	14.49	140.70	0.81	0.37	0.74	0.00
14.50	140.80	0.80	0.37	0.74	0.00	14.51	140.49	0.78	0.37	0.74	0.00
14.52	139.70	0.75	0.37	0.74	0.00	14.53	138.56	0.72	0.37	0.74	0.00
14.54	137.17	0.69	0.37	0.74	0.00	14.55	135.57	0.65	0.37	0.74	0.00
14.56	133.84	0.61	0.37	0.74	0.00	14.57	132.06	0.58	0.37	0.74	0.00
14.58	130.38	0.55	0.37	0.73	0.00	14.59	129.06	0.53	0.37	0.73	0.00
14.60	128.02	0.51	0.37	0.73	0.00	14.61	127.12	0.50	0.37	0.73	0.00
14.62	126.07	0.48	0.37	0.73	0.00	14.63	124.92	0.47	0.37	0.73	0.00
14.64	123.70	0.45	0.37	0.73	0.00	14.65	122.49	0.44	0.37	0.73	0.00
14.66	121.34	0.42	0.37	0.73	0.00	14.67	120.47	0.41	0.37	0.73	0.00
14.68	120.25	0.41	0.37	0.73	0.00	14.69	120.70	0.41	0.37	0.73	0.00
14.70	121.64	0.42	0.37	0.73	0.00	14.71	122.67	0.44	0.37	0.73	0.00
14.72	123.73	0.45	0.37	0.73	0.00	14.73	124.77	0.46	0.37	0.73	0.00
14.74	125.73	0.47	0.37	0.73	0.00	14.75	126.58	0.48	0.37	0.73	0.00
14.76	127.12	0.49	0.37	0.73	0.00	14.77	127.28	0.49	0.37	0.73	0.00
14.78	127.11	0.49	0.37	0.73	0.00	14.79	126.80	0.49	0.37	0.73	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
14.80	126.45	0.49	0.37	0.73	0.00	14.81	126.10	0.49	0.37	0.73	0.00
14.82	125.75	0.49	0.37	0.73	0.00	14.83	125.43	0.49	0.37	0.73	0.00
14.84	125.14	0.49	0.37	0.73	0.00	14.85	125.13	0.50	0.36	0.73	0.00
14.86	125.42	0.50	0.36	0.73	0.00	14.87	126.02	0.51	0.36	0.73	0.00
14.88	126.69	0.53	0.36	0.73	0.00	14.89	127.37	0.54	0.36	0.73	0.00
14.90	128.03	0.56	0.36	0.73	0.00	14.91	128.63	0.57	0.36	0.73	0.00
14.92	129.14	0.59	0.36	0.73	0.00	14.93	129.55	0.60	0.36	0.73	0.00
14.94	129.90	0.61	0.36	0.73	0.00	14.95	130.23	0.62	0.36	0.73	0.00
14.96	130.58	0.63	0.36	0.73	0.00	14.97	130.95	0.64	0.36	0.73	0.00
14.98	131.31	0.66	0.36	0.73	0.00	14.99	131.63	0.67	0.36	0.73	0.00
15.00	131.90	0.69	0.36	0.73	0.00	15.01	132.12	0.70	0.36	0.73	0.00
15.02	132.11	0.71	0.36	0.73	0.00	15.03	131.77	0.70	0.36	0.73	0.00
15.04	131.06	0.69	0.36	0.73	0.00	15.05	130.11	0.68	0.36	0.73	0.00
15.06	129.06	0.66	0.36	0.73	0.00	15.07	127.95	0.64	0.36	0.73	0.00
15.08	126.83	0.62	0.36	0.73	0.00	15.09	125.76	0.61	0.36	0.73	0.00
15.10	124.81	0.59	0.36	0.73	0.00	15.11	124.51	0.58	0.36	0.73	0.00
15.12	124.93	0.58	0.36	0.73	0.00	15.13	126.03	0.59	0.36	0.72	0.00
15.14	127.31	0.59	0.36	0.72	0.00	15.15	128.69	0.60	0.36	0.72	0.00
15.16	130.08	0.61	0.36	0.72	0.00	15.17	131.43	0.62	0.36	0.72	0.00
15.18	132.67	0.62	0.36	0.72	0.00	15.19	133.79	0.63	0.36	0.72	0.00
15.20	135.08	0.64	0.36	0.72	0.00	15.21	136.71	0.66	0.36	0.72	0.00
15.22	138.73	0.69	0.36	0.72	0.00	15.23	140.96	0.71	0.36	0.72	0.00
15.24	143.25	0.74	0.36	0.72	0.00	15.25	145.49	0.78	0.36	0.72	0.00
15.26	147.58	0.80	0.36	0.72	0.00	15.27	149.40	0.83	0.36	0.72	0.00
15.28	150.84	0.85	0.02	0.72	0.00	15.29	151.99	0.88	0.02	0.72	0.00
15.30	153.01	0.90	0.02	0.72	0.00	15.31	154.06	0.94	0.01	0.72	0.00
15.32	155.12	0.97	0.01	0.72	0.00	15.33	156.11	1.01	0.01	0.72	0.00
15.34	156.99	1.04	0.01	0.72	0.00	15.35	157.72	1.08	0.01	0.72	0.00
15.36	158.29	1.11	0.01	0.72	0.00	15.37	158.66	1.13	0.01	0.72	0.00
15.38	158.89	1.15	0.01	0.72	0.00	15.39	159.04	1.18	0.01	0.72	0.00
15.40	159.15	1.21	0.01	0.72	0.00	15.41	159.21	1.24	0.01	0.72	0.00
15.42	159.20	1.27	0.01	0.72	0.00	15.43	159.01	1.29	0.00	0.72	0.00
15.44	158.78	1.32	0.00	0.72	0.00	15.45	158.46	1.33	0.00	0.72	0.00
15.46	157.78	1.33	0.00	0.72	0.00	15.47	156.64	1.31	0.00	0.72	0.00
15.48	155.11	1.28	0.01	0.72	0.00	15.49	153.37	1.24	0.01	0.72	0.00
15.50	151.49	1.20	0.01	0.72	0.00	15.51	149.51	1.16	0.01	0.72	0.00
15.52	147.60	1.12	0.01	0.72	0.00	15.53	145.87	1.09	0.01	0.72	0.00
15.54	144.50	1.06	0.01	0.72	0.00	15.55	143.44	1.03	0.01	0.72	0.00
15.56	142.51	1.00	0.01	0.72	0.00	15.57	141.45	0.97	0.01	0.72	0.00
15.58	140.22	0.93	0.01	0.72	0.00	15.59	138.88	0.89	0.02	0.72	0.00
15.60	137.48	0.86	0.02	0.72	0.00	15.61	136.11	0.82	0.36	0.72	0.00
15.62	134.86	0.79	0.36	0.72	0.00	15.63	134.15	0.77	0.36	0.72	0.00
15.64	133.96	0.76	0.36	0.72	0.00	15.65	134.21	0.76	0.36	0.72	0.00
15.66	134.50	0.76	0.36	0.72	0.00	15.67	134.80	0.75	0.36	0.72	0.00
15.68	135.10	0.75	0.36	0.71	0.00	15.69	135.38	0.74	0.36	0.71	0.00
15.70	135.63	0.74	0.36	0.71	0.00	15.71	135.82	0.74	0.36	0.71	0.00
15.72	135.92	0.73	0.36	0.71	0.00	15.73	135.95	0.73	0.36	0.71	0.00
15.74	135.95	0.72	0.36	0.71	0.00	15.75	135.93	0.71	0.36	0.71	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
15.76	135.90	0.71	0.36	0.71	0.00	15.77	135.87	0.70	0.36	0.71	0.00
15.78	135.83	0.69	0.36	0.71	0.00	15.79	135.78	0.68	0.36	0.71	0.00
15.80	135.67	0.68	0.36	0.71	0.00	15.81	135.46	0.67	0.36	0.71	0.00
15.82	135.13	0.67	0.36	0.71	0.00	15.83	134.71	0.66	0.36	0.71	0.00
15.84	134.26	0.65	0.36	0.71	0.00	15.85	133.79	0.65	0.36	0.71	0.00
15.86	133.32	0.64	0.36	0.71	0.00	15.87	132.88	0.63	0.36	0.71	0.00
15.88	132.49	0.62	0.36	0.71	0.00	15.89	132.01	0.62	0.36	0.71	0.00
15.90	131.37	0.61	0.36	0.71	0.00	15.91	130.52	0.61	0.36	0.71	0.00
15.92	129.54	0.60	0.36	0.71	0.00	15.93	128.51	0.59	0.36	0.71	0.00
15.94	127.45	0.59	0.36	0.71	0.00	15.95	126.44	0.58	0.35	0.71	0.00
15.96	125.52	0.57	0.35	0.71	0.00	15.97	124.78	0.57	0.35	0.71	0.00
15.98	124.26	0.56	0.35	0.71	0.00	15.99	123.90	0.56	0.35	0.71	0.00
16.00	123.58	0.56	0.35	0.71	0.00	16.01	123.22	0.56	0.35	0.71	0.00
16.02	122.84	0.56	0.35	0.71	0.00	16.03	122.47	0.56	0.35	0.71	0.00
16.04	122.11	0.56	0.35	0.71	0.00	16.05	121.79	0.56	0.35	0.71	0.00
16.06	121.62	0.56	0.35	0.71	0.00	16.07	121.64	0.56	0.35	0.71	0.00
16.08	121.85	0.56	0.35	0.71	0.00	16.09	122.13	0.56	0.35	0.71	0.00
16.10	122.43	0.56	0.35	0.71	0.00	16.11	122.74	0.56	0.35	0.71	0.00
16.12	123.05	0.56	0.35	0.71	0.00	16.13	123.33	0.56	0.35	0.71	0.00
16.14	123.58	0.56	0.35	0.71	0.00	16.15	123.86	0.56	0.35	0.71	0.00
16.16	124.22	0.56	0.35	0.71	0.00	16.17	124.70	0.56	0.35	0.71	0.00
16.18	125.25	0.55	0.35	0.71	0.00	16.19	125.84	0.55	0.35	0.71	0.00
16.20	126.43	0.55	0.35	0.71	0.00	16.21	126.99	0.55	0.35	0.71	0.00
16.22	127.50	0.55	0.35	0.71	0.00	16.23	128.08	0.56	0.35	0.70	0.00
16.24	129.09	0.56	0.35	0.70	0.00	16.25	130.64	0.58	0.35	0.70	0.00
16.26	132.67	0.61	0.35	0.70	0.00	16.27	134.89	0.63	0.35	0.70	0.00
16.28	137.16	0.66	0.35	0.70	0.00	16.29	139.37	0.69	0.35	0.70	0.00
16.30	141.42	0.71	0.35	0.70	0.00	16.31	143.20	0.74	0.35	0.70	0.00
16.32	144.64	0.76	0.35	0.70	0.00	16.33	145.88	0.78	0.35	0.70	0.00
16.34	147.08	0.81	0.35	0.70	0.00	16.35	148.37	0.84	0.35	0.70	0.00
16.36	149.69	0.87	0.02	0.70	0.00	16.37	150.96	0.91	0.02	0.70	0.00
16.38	152.10	0.94	0.01	0.70	0.00	16.39	153.09	0.97	0.01	0.70	0.00
16.40	153.87	1.00	0.01	0.70	0.00	16.41	154.42	1.02	0.01	0.70	0.00
16.42	154.78	1.05	0.01	0.70	0.00	16.43	155.01	1.08	0.01	0.70	0.00
16.44	155.16	1.12	0.01	0.70	0.00	16.45	155.18	1.16	0.01	0.70	0.00
16.46	155.07	1.21	0.01	0.70	0.00	16.47	154.71	1.24	0.01	0.70	0.00
16.48	154.26	1.28	0.00	0.70	0.00	16.49	153.86	1.30	0.00	0.70	0.00
16.50	153.57	1.34	0.00	0.70	0.00	16.51	153.35	1.38	0.00	0.70	0.00
16.52	153.05	1.42	0.00	0.70	0.00	16.53	152.57	1.48	0.00	0.70	0.00
16.54	151.89	1.53	0.00	0.70	0.00	16.55	151.05	1.59	0.00	0.70	0.00
16.56	150.11	1.64	0.00	0.70	0.00	16.57	149.16	1.69	0.00	0.70	0.00
16.58	148.14	1.72	0.00	0.70	0.00	16.59	146.91	1.73	0.00	0.70	0.00
16.60	145.35	1.74	0.00	0.70	0.00	16.61	143.49	1.74	0.00	0.70	0.00
16.62	141.45	1.74	0.00	0.70	0.00	16.63	139.33	1.74	0.00	0.70	0.00
16.64	137.23	1.74	0.00	0.70	0.00	16.65	287.62	2.00	0.00	0.70	0.00
16.66	277.58	2.00	0.00	0.70	0.00	16.67	272.83	2.00	0.00	0.70	0.00
16.68	272.91	2.00	0.00	0.70	0.00	16.69	276.91	2.00	0.00	0.70	0.00
16.70	281.60	2.00	0.00	0.70	0.00	16.71	129.54	1.63	0.00	0.70	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
16.72	128.76	1.60	0.00	0.70	0.00	16.73	128.01	1.57	0.00	0.70	0.00
16.74	127.32	1.54	0.00	0.70	0.00	16.75	126.92	1.52	0.00	0.70	0.00
16.76	127.07	1.49	0.00	0.70	0.00	16.77	127.78	1.47	0.00	0.70	0.00
16.78	128.83	1.45	0.00	0.69	0.00	16.79	129.93	1.42	0.00	0.69	0.00
16.80	131.02	1.39	0.00	0.69	0.00	16.81	132.04	1.36	0.00	0.69	0.00
16.82	132.93	1.33	0.00	0.69	0.00	16.83	133.67	1.30	0.00	0.69	0.00
16.84	134.32	1.28	0.00	0.69	0.00	16.85	134.99	1.25	0.01	0.69	0.00
16.86	135.72	1.22	0.01	0.69	0.00	16.87	136.46	1.17	0.01	0.69	0.00
16.88	137.09	1.13	0.01	0.69	0.00	16.89	137.54	1.08	0.01	0.69	0.00
16.90	137.62	1.03	0.01	0.69	0.00	16.91	137.50	0.98	0.01	0.69	0.00
16.92	137.27	0.94	0.01	0.69	0.00	16.93	137.19	0.91	0.01	0.69	0.00
16.94	137.31	0.89	0.02	0.69	0.00	16.95	137.62	0.88	0.02	0.69	0.00
16.96	137.92	0.86	0.02	0.69	0.00	16.97	138.18	0.84	0.35	0.69	0.00
16.98	138.37	0.81	0.35	0.69	0.00	16.99	138.49	0.79	0.35	0.69	0.00
17.00	138.54	0.78	0.35	0.69	0.00	17.01	138.59	0.76	0.35	0.69	0.00
17.02	138.74	0.76	0.35	0.69	0.00	17.03	139.03	0.76	0.35	0.69	0.00
17.04	139.42	0.77	0.35	0.69	0.00	17.05	139.85	0.78	0.34	0.69	0.00
17.06	140.29	0.79	0.34	0.69	0.00	17.07	140.71	0.80	0.34	0.69	0.00
17.08	141.11	0.81	0.34	0.69	0.00	17.09	141.45	0.82	0.34	0.69	0.00
17.10	141.47	0.82	0.34	0.69	0.00	17.11	141.07	0.82	0.34	0.69	0.00
17.12	140.23	0.82	0.34	0.69	0.00	17.13	139.19	0.82	0.34	0.69	0.00
17.14	138.07	0.82	0.34	0.69	0.00	17.15	136.90	0.82	0.34	0.69	0.00
17.16	135.76	0.82	0.34	0.69	0.00	17.17	134.70	0.82	0.34	0.69	0.00
17.18	133.75	0.82	0.34	0.69	0.00	17.19	132.69	0.81	0.34	0.69	0.00
17.20	131.34	0.80	0.34	0.69	0.00	17.21	129.60	0.77	0.34	0.69	0.00
17.22	127.61	0.74	0.34	0.69	0.00	17.23	125.47	0.71	0.34	0.69	0.00
17.24	123.28	0.68	0.34	0.69	0.00	17.25	121.16	0.66	0.34	0.69	0.00
17.26	119.22	0.63	0.34	0.69	0.00	17.27	117.62	0.61	0.34	0.69	0.00
17.28	116.28	0.59	0.34	0.69	0.00	17.29	115.02	0.57	0.34	0.69	0.00
17.30	113.58	0.54	0.34	0.69	0.00	17.31	111.90	0.51	0.34	0.69	0.00
17.32	110.07	0.48	0.34	0.69	0.00	17.33	108.16	0.46	0.34	0.68	0.00
17.34	106.27	0.43	0.34	0.68	0.00	17.35	104.53	0.40	0.34	0.68	0.00
17.36	103.44	0.39	0.34	0.68	0.00	17.37	103.09	0.38	0.34	0.68	0.00
17.38	103.40	0.38	0.34	0.68	0.00	17.39	103.84	0.39	0.34	0.68	0.00
17.40	104.31	0.39	0.34	0.68	0.00	17.41	104.80	0.39	0.34	0.68	0.00
17.42	105.28	0.39	0.34	0.68	0.00	17.43	105.72	0.39	0.34	0.68	0.00
17.44	106.09	0.39	0.34	0.68	0.00	17.45	106.44	0.40	0.34	0.68	0.00
17.46	106.82	0.40	0.34	0.68	0.00	17.47	107.26	0.40	0.34	0.68	0.00
17.48	107.77	0.40	0.34	0.68	0.00	17.49	108.31	0.40	0.34	0.68	0.00
17.50	108.85	0.40	0.34	0.68	0.00	17.51	109.36	0.41	0.34	0.68	0.00
17.52	109.83	0.41	0.34	0.68	0.00	17.53	110.34	0.41	0.34	0.68	0.00
17.54	111.10	0.42	0.34	0.68	0.00	17.55	112.20	0.42	0.34	0.68	0.00
17.56	113.60	0.44	0.34	0.68	0.00	17.57	115.13	0.45	0.34	0.68	0.00
17.58	116.72	0.46	0.34	0.68	0.00	17.59	118.29	0.47	0.34	0.68	0.00
17.60	119.75	0.49	0.34	0.68	0.00	17.61	121.03	0.50	0.34	0.68	0.00
17.62	122.12	0.50	0.34	0.68	0.00	17.63	123.18	0.51	0.34	0.68	0.00
17.64	124.34	0.52	0.34	0.68	0.00	17.65	125.67	0.54	0.34	0.68	0.00
17.66	127.11	0.55	0.34	0.68	0.00	17.67	128.57	0.56	0.34	0.68	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
17.68	129.99	0.57	0.34	0.68	0.00	17.69	131.29	0.58	0.34	0.68	0.00
17.70	132.32	0.59	0.34	0.68	0.00	17.71	132.88	0.60	0.34	0.68	0.00
17.72	133.00	0.60	0.34	0.68	0.00	17.73	132.83	0.59	0.34	0.68	0.00
17.74	132.64	0.58	0.34	0.68	0.00	17.75	132.43	0.58	0.34	0.68	0.00
17.76	132.21	0.57	0.34	0.68	0.00	17.77	131.99	0.56	0.34	0.68	0.00
17.78	131.79	0.56	0.34	0.68	0.00	17.79	131.62	0.55	0.34	0.68	0.00
17.80	131.49	0.55	0.34	0.68	0.00	17.81	131.39	0.54	0.34	0.68	0.00
17.82	131.28	0.54	0.34	0.68	0.00	17.83	131.15	0.53	0.34	0.68	0.00
17.84	131.00	0.52	0.34	0.68	0.00	17.85	130.84	0.52	0.34	0.68	0.00
17.86	130.69	0.51	0.34	0.68	0.00	17.87	130.54	0.50	0.34	0.68	0.00
17.88	130.51	0.50	0.34	0.67	0.00	17.89	130.64	0.50	0.34	0.67	0.00
17.90	130.93	0.50	0.34	0.67	0.00	17.91	131.28	0.50	0.34	0.67	0.00
17.92	131.66	0.50	0.34	0.67	0.00	17.93	132.05	0.50	0.34	0.67	0.00
17.94	132.42	0.50	0.34	0.67	0.00	17.95	132.76	0.50	0.34	0.67	0.00
17.96	133.06	0.50	0.34	0.67	0.00	17.97	133.39	0.50	0.34	0.67	0.00
17.98	133.79	0.50	0.34	0.67	0.00	17.99	134.31	0.51	0.34	0.67	0.00
18.00	134.88	0.52	0.34	0.67	0.00	18.01	135.47	0.53	0.34	0.67	0.00
18.02	136.06	0.53	0.34	0.67	0.00	18.03	136.61	0.54	0.34	0.67	0.00
18.04	137.10	0.55	0.34	0.67	0.00	18.05	137.69	0.56	0.34	0.67	0.00
18.06	138.61	0.57	0.34	0.67	0.00	18.07	139.95	0.60	0.34	0.67	0.00
18.08	141.52	0.63	0.34	0.67	0.00	18.09	143.10	0.66	0.34	0.67	0.00
18.10	144.56	0.70	0.34	0.67	0.00	18.11	145.85	0.74	0.34	0.67	0.00
18.12	146.90	0.77	0.34	0.67	0.00	18.13	147.72	0.80	0.34	0.67	0.00
18.14	148.65	0.83	0.34	0.67	0.00	18.15	149.86	0.87	0.02	0.67	0.00
18.16	151.38	0.92	0.01	0.67	0.00	18.17	152.88	0.98	0.01	0.67	0.00
18.18	154.16	1.05	0.01	0.67	0.00	18.19	155.13	1.12	0.01	0.67	0.00
18.20	155.77	1.18	0.01	0.67	0.00	18.21	155.96	1.24	0.00	0.67	0.00
18.22	155.87	1.29	0.00	0.67	0.00	18.23	155.38	1.32	0.00	0.67	0.00
18.24	154.49	1.35	0.00	0.67	0.00	18.25	153.18	1.37	0.00	0.67	0.00
18.26	151.63	1.39	0.00	0.67	0.00	18.27	149.89	1.42	0.00	0.67	0.00
18.28	148.05	1.45	0.00	0.67	0.00	18.29	146.19	1.48	0.00	0.67	0.00
18.30	144.46	1.50	0.00	0.67	0.00	18.31	142.91	1.51	0.00	0.67	0.00
18.32	141.43	1.51	0.00	0.67	0.00	18.33	139.82	1.50	0.00	0.67	0.00
18.34	137.95	1.48	0.00	0.67	0.00	18.35	135.90	1.46	0.00	0.67	0.00
18.36	133.77	1.44	0.00	0.67	0.00	18.37	131.69	1.41	0.00	0.67	0.00
18.38	129.75	1.39	0.00	0.67	0.00	18.39	128.05	1.38	0.00	0.67	0.00
18.40	126.92	1.36	0.00	0.67	0.00	18.41	126.28	1.33	0.00	0.67	0.00
18.42	125.98	1.30	0.00	0.67	0.00	18.43	125.63	1.27	0.00	0.66	0.00
18.44	125.21	1.23	0.00	0.66	0.00	18.45	124.73	1.20	0.01	0.66	0.00
18.46	124.23	1.16	0.01	0.66	0.00	18.47	123.73	1.13	0.01	0.66	0.00
18.48	123.32	1.10	0.01	0.66	0.00	18.49	123.09	1.07	0.01	0.66	0.00
18.50	123.02	1.04	0.01	0.66	0.00	18.51	123.01	1.01	0.01	0.66	0.00
18.52	122.88	0.97	0.01	0.66	0.00	18.53	122.59	0.92	0.01	0.66	0.00
18.54	122.08	0.88	0.01	0.66	0.00	18.55	121.46	0.84	0.33	0.66	0.00
18.56	120.78	0.80	0.33	0.66	0.00	18.57	120.18	0.77	0.33	0.66	0.00
18.58	119.69	0.74	0.33	0.66	0.00	18.59	119.27	0.72	0.33	0.66	0.00
18.60	118.77	0.70	0.33	0.66	0.00	18.61	118.15	0.67	0.33	0.66	0.00
18.62	117.43	0.64	0.33	0.66	0.00	18.63	116.62	0.61	0.33	0.66	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
18.64	115.78	0.59	0.33	0.66	0.00	18.65	114.98	0.57	0.33	0.66	0.00
18.66	114.31	0.55	0.33	0.66	0.00	18.67	113.74	0.53	0.33	0.66	0.00
18.68	113.18	0.52	0.33	0.66	0.00	18.69	112.50	0.50	0.33	0.66	0.00
18.70	111.72	0.48	0.33	0.66	0.00	18.71	110.88	0.47	0.33	0.66	0.00
18.72	110.01	0.45	0.33	0.66	0.00	18.73	109.18	0.43	0.33	0.66	0.00
18.74	108.48	0.42	0.33	0.66	0.00	18.75	108.03	0.41	0.33	0.66	0.00
18.76	107.80	0.40	0.33	0.66	0.00	18.77	107.68	0.40	0.33	0.66	0.00
18.78	107.52	0.39	0.33	0.66	0.00	18.79	107.33	0.38	0.33	0.66	0.00
18.80	107.11	0.37	0.33	0.66	0.00	18.81	106.89	0.36	0.33	0.66	0.00
18.82	106.66	0.36	0.33	0.66	0.00	18.83	106.56	0.35	0.33	0.66	0.00
18.84	106.67	0.35	0.33	0.66	0.00	18.85	106.98	0.35	0.33	0.66	0.00
18.86	107.42	0.35	0.33	0.66	0.00	18.87	107.89	0.35	0.33	0.66	0.00
18.88	108.38	0.35	0.33	0.66	0.00	18.89	108.86	0.35	0.33	0.66	0.00
18.90	109.30	0.35	0.33	0.66	0.00	18.91	109.68	0.35	0.33	0.66	0.00
18.92	110.12	0.35	0.33	0.66	0.00	18.93	110.70	0.35	0.33	0.66	0.00
18.94	111.47	0.36	0.33	0.66	0.00	18.95	112.35	0.36	0.33	0.66	0.00
18.96	113.28	0.37	0.33	0.66	0.00	18.97	114.23	0.38	0.33	0.66	0.00
18.98	115.14	0.39	0.33	0.65	0.00	18.99	115.96	0.40	0.33	0.65	0.00
19.00	116.63	0.40	0.33	0.65	0.00	19.01	117.15	0.41	0.33	0.65	0.00
19.02	117.58	0.41	0.33	0.65	0.00	19.03	118.01	0.42	0.33	0.65	0.00
19.04	118.48	0.43	0.33	0.65	0.00	19.05	118.97	0.43	0.33	0.65	0.00
19.06	119.44	0.44	0.33	0.65	0.00	19.07	119.87	0.45	0.33	0.65	0.00
19.08	120.25	0.46	0.33	0.65	0.00	19.09	120.44	0.46	0.33	0.65	0.00
19.10	120.38	0.46	0.33	0.65	0.00	19.11	120.08	0.46	0.33	0.65	0.00
19.12	119.66	0.46	0.33	0.65	0.00	19.13	119.20	0.46	0.33	0.65	0.00
19.14	118.73	0.46	0.33	0.65	0.00	19.15	118.27	0.46	0.33	0.65	0.00
19.16	117.83	0.46	0.33	0.65	0.00	19.17	117.44	0.46	0.33	0.65	0.00
19.18	116.99	0.46	0.33	0.65	0.00	19.19	116.40	0.46	0.33	0.65	0.00
19.20	115.61	0.45	0.33	0.65	0.00	19.21	114.70	0.44	0.33	0.65	0.00
19.22	113.72	0.43	0.33	0.65	0.00	19.23	112.73	0.42	0.33	0.65	0.00
19.24	111.76	0.42	0.33	0.65	0.00	19.25	110.88	0.41	0.33	0.65	0.00
19.26	110.12	0.40	0.32	0.65	0.00	19.27	109.42	0.40	0.32	0.65	0.00
19.28	108.68	0.39	0.32	0.65	0.00	19.29	107.83	0.38	0.32	0.65	0.00
19.30	106.87	0.38	0.32	0.65	0.00	19.31	105.86	0.37	0.32	0.65	0.00
19.32	104.85	0.36	0.32	0.65	0.00	19.33	103.89	0.35	0.32	0.65	0.00
19.34	103.02	0.34	0.32	0.65	0.00	19.35	102.35	0.34	0.32	0.65	0.00
19.36	101.84	0.34	0.32	0.65	0.00	19.37	101.42	0.34	0.32	0.65	0.00
19.38	100.97	0.34	0.32	0.65	0.00	19.39	100.48	0.34	0.32	0.65	0.00
19.40	99.97	0.34	0.32	0.65	0.00	19.41	99.46	0.34	0.32	0.65	0.00
19.42	98.99	0.34	0.32	0.65	0.00	19.43	98.58	0.34	0.32	0.65	0.00
19.44	98.22	0.34	0.32	0.65	0.00	19.45	97.86	0.34	0.32	0.65	0.00
19.46	97.45	0.34	0.32	0.65	0.00	19.47	96.99	0.33	0.32	0.65	0.00
19.48	96.49	0.33	0.32	0.65	0.00	19.49	95.98	0.33	0.32	0.65	0.00
19.50	95.49	0.33	0.32	0.65	0.00	19.51	95.04	0.33	0.32	0.65	0.00
19.52	94.66	0.33	0.32	0.65	0.00	19.53	94.35	0.33	0.32	0.64	0.00
19.54	94.06	0.33	0.32	0.64	0.00	19.55	93.75	0.33	0.32	0.64	0.00
19.56	93.39	0.33	0.32	0.64	0.00	19.57	93.02	0.33	0.32	0.64	0.00
19.58	92.65	0.33	0.32	0.64	0.00	19.59	92.30	0.33	0.32	0.64	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
19.60	91.98	0.33	0.32	0.64	0.00	19.61	91.74	0.33	0.32	0.64	0.00
19.62	91.57	0.33	0.32	0.64	0.00	19.63	91.44	0.33	0.32	0.64	0.00
19.64	91.30	0.33	0.32	0.64	0.00	19.65	91.15	0.33	0.32	0.64	0.00
19.66	91.00	0.33	0.32	0.64	0.00	19.67	90.85	0.33	0.32	0.64	0.00
19.68	90.71	0.32	0.32	0.64	0.00	19.69	90.59	0.32	0.32	0.64	0.00
19.70	90.44	0.32	0.32	0.64	0.00	19.71	90.24	0.32	0.32	0.64	0.00
19.72	89.96	0.31	0.32	0.64	0.00	19.73	89.63	0.30	0.32	0.64	0.00
19.74	89.26	0.30	0.32	0.64	0.00	19.75	88.86	0.29	0.32	0.64	0.00
19.76	88.46	0.28	0.32	0.64	0.00	19.77	88.07	0.27	0.32	0.64	0.00
19.78	88.19	0.27	0.32	0.64	0.00	19.79	89.69	0.28	0.32	0.64	0.00
19.80	92.76	0.31	0.32	0.64	0.00	19.81	96.96	0.35	0.32	0.64	0.00
19.82	101.47	0.39	0.32	0.64	0.00	19.83	106.03	0.43	0.32	0.64	0.00
19.84	110.45	0.47	0.32	0.64	0.00	19.85	114.52	0.52	0.32	0.64	0.00
19.86	118.07	0.55	0.32	0.64	0.00	19.87	121.09	0.59	0.32	0.64	0.00
19.88	123.99	0.62	0.32	0.64	0.00	19.89	127.15	0.66	0.32	0.64	0.00
19.90	130.76	0.70	0.32	0.64	0.00	19.91	134.60	0.75	0.32	0.64	0.00
19.92	138.47	0.80	0.32	0.64	0.00	19.93	142.19	0.85	0.02	0.64	0.00
19.94	145.59	0.90	0.01	0.64	0.00	19.95	148.37	0.94	0.01	0.64	0.00
19.96	149.20	0.95	0.01	0.64	0.00	19.97	148.08	0.93	0.01	0.64	0.00
19.98	145.14	0.89	0.01	0.64	0.00	19.99	141.75	0.84	0.02	0.64	0.00
20.00	138.06	0.79	0.32	0.64	0.00	20.01	134.24	0.74	0.32	0.64	0.00
20.02	130.49	0.69	0.32	0.64	0.00	20.03	126.99	0.65	0.32	0.64	0.00
20.04	124.02	0.61	0.32	0.64	0.00	20.05	121.46	0.58	0.32	0.64	0.00
20.06	118.99	0.54	0.32	0.64	0.00	20.07	116.18	0.51	0.32	0.64	0.00
20.08	112.93	0.47	0.32	0.63	0.00	20.09	109.37	0.43	0.32	0.63	0.00
20.10	105.66	0.39	0.32	0.63	0.00	20.11	101.97	0.35	0.32	0.63	0.00
20.12	98.53	0.32	0.32	0.63	0.00	20.13	96.18	0.29	0.32	0.63	0.00
20.14	95.10	0.28	0.32	0.63	0.00	20.15	95.15	0.28	0.32	0.63	0.00
20.16	95.46	0.27	0.32	0.63	0.00	20.17	95.78	0.27	0.32	0.63	0.00
20.18	96.11	0.27	0.32	0.63	0.00	20.19	96.42	0.27	0.32	0.63	0.00
20.20	96.70	0.27	0.32	0.63	0.00	20.21	96.94	0.26	0.32	0.63	0.00
20.22	97.19	0.26	0.32	0.63	0.00	20.23	97.48	0.26	0.32	0.63	0.00
20.24	97.85	0.26	0.32	0.63	0.00	20.25	98.27	0.26	0.32	0.63	0.00
20.26	98.70	0.26	0.32	0.63	0.00	20.27	99.13	0.25	0.32	0.63	0.00
20.28	99.53	0.25	0.32	0.63	0.00	20.29	99.88	0.25	0.32	0.63	0.00
20.30	100.39	0.25	0.32	0.63	0.00	20.31	101.47	0.26	0.32	0.63	0.00
20.32	103.24	0.27	0.32	0.63	0.00	20.33	105.60	0.28	0.32	0.63	0.00
20.34	108.19	0.30	0.32	0.63	0.00	20.35	110.87	0.31	0.32	0.63	0.00
20.36	113.51	0.33	0.31	0.63	0.00	20.37	115.97	0.35	0.31	0.63	0.00
20.38	118.14	0.36	0.31	0.63	0.00	20.39	120.04	0.37	0.31	0.63	0.00
20.40	121.93	0.39	0.31	0.63	0.00	20.41	124.06	0.41	0.31	0.63	0.00
20.42	126.48	0.43	0.31	0.63	0.00	20.43	129.05	0.45	0.31	0.63	0.00
20.44	131.63	0.48	0.31	0.63	0.00	20.45	134.09	0.50	0.31	0.63	0.00
20.46	136.30	0.53	0.31	0.63	0.00	20.47	138.17	0.55	0.31	0.63	0.00
20.48	139.74	0.56	0.31	0.63	0.00	20.49	141.19	0.58	0.31	0.63	0.00
20.50	142.74	0.61	0.31	0.63	0.00	20.51	144.42	0.63	0.31	0.63	0.00
20.52	146.12	0.66	0.31	0.63	0.00	20.53	147.75	0.69	0.31	0.63	0.00
20.54	149.23	0.72	0.31	0.63	0.00	20.55	150.51	0.74	0.31	0.63	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
20.56	151.44	0.76	0.31	0.63	0.00	20.57	151.99	0.78	0.31	0.63	0.00
20.58	152.25	0.79	0.31	0.63	0.00	20.59	152.38	0.80	0.31	0.63	0.00
20.60	152.49	0.82	0.31	0.63	0.00	20.61	152.56	0.84	0.31	0.63	0.00
20.62	152.59	0.85	0.01	0.63	0.00	20.63	152.57	0.87	0.01	0.62	0.00
20.64	152.53	0.88	0.01	0.62	0.00	20.65	152.43	0.89	0.01	0.62	0.00
20.66	152.25	0.91	0.01	0.62	0.00	20.67	151.97	0.92	0.01	0.62	0.00
20.68	151.61	0.93	0.01	0.62	0.00	20.69	151.17	0.95	0.01	0.62	0.00
20.70	150.67	0.97	0.01	0.62	0.00	20.71	150.14	0.98	0.01	0.62	0.00
20.72	149.60	1.00	0.01	0.62	0.00	20.73	149.09	1.01	0.01	0.62	0.00
20.74	148.46	1.01	0.01	0.62	0.00	20.75	147.64	1.01	0.01	0.62	0.00
20.76	146.55	1.00	0.01	0.62	0.00	20.77	145.33	1.00	0.01	0.62	0.00
20.78	144.03	0.99	0.01	0.62	0.00	20.79	142.72	0.98	0.01	0.62	0.00
20.80	141.47	0.97	0.01	0.62	0.00	20.81	140.34	0.96	0.01	0.62	0.00
20.82	139.41	0.95	0.01	0.62	0.00	20.83	138.66	0.94	0.01	0.62	0.00
20.84	137.97	0.92	0.01	0.62	0.00	20.85	137.19	0.90	0.01	0.62	0.00
20.86	136.27	0.87	0.01	0.62	0.00	20.87	135.27	0.84	0.31	0.62	0.00
20.88	134.23	0.81	0.31	0.62	0.00	20.89	133.20	0.78	0.31	0.62	0.00
20.90	132.24	0.76	0.31	0.62	0.00	20.91	131.61	0.74	0.31	0.62	0.00
20.92	131.32	0.73	0.31	0.62	0.00	20.93	131.30	0.71	0.31	0.62	0.00
20.94	131.28	0.70	0.31	0.62	0.00	20.95	131.22	0.68	0.31	0.62	0.00
20.96	131.11	0.66	0.31	0.62	0.00	20.97	130.94	0.65	0.31	0.62	0.00
20.98	130.75	0.63	0.31	0.62	0.00	20.99	130.54	0.62	0.31	0.62	0.00
21.00	130.28	0.61	0.31	0.62	0.00	21.01	129.95	0.59	0.31	0.62	0.00
21.02	129.51	0.58	0.31	0.62	0.00	21.03	128.97	0.56	0.31	0.62	0.00
21.04	128.35	0.55	0.31	0.62	0.00	21.05	127.67	0.53	0.31	0.62	0.00
21.06	126.97	0.51	0.31	0.62	0.00	21.07	126.29	0.50	0.31	0.62	0.00
21.08	125.71	0.49	0.31	0.62	0.00	21.09	125.20	0.48	0.31	0.62	0.00
21.10	124.72	0.47	0.31	0.62	0.00	21.11	124.17	0.46	0.31	0.62	0.00
21.12	123.56	0.45	0.31	0.62	0.00	21.13	122.92	0.45	0.31	0.62	0.00
21.14	122.27	0.44	0.31	0.62	0.00	21.15	121.65	0.43	0.31	0.62	0.00
21.16	121.09	0.42	0.31	0.62	0.00	21.17	121.02	0.42	0.31	0.62	0.00
21.18	121.55	0.43	0.31	0.61	0.00	21.19	122.68	0.45	0.31	0.61	0.00
21.20	124.00	0.47	0.31	0.61	0.00	21.21	125.35	0.49	0.31	0.61	0.00
21.22	126.65	0.51	0.31	0.61	0.00	21.23	127.84	0.53	0.31	0.61	0.00
21.24	128.86	0.55	0.31	0.61	0.00	21.25	129.75	0.57	0.31	0.61	0.00
21.26	130.84	0.59	0.31	0.61	0.00	21.27	132.25	0.62	0.31	0.61	0.00
21.28	133.99	0.66	0.31	0.61	0.00	21.29	135.74	0.70	0.31	0.61	0.00
21.30	137.37	0.75	0.31	0.61	0.00	21.31	138.77	0.80	0.31	0.61	0.00
21.32	139.91	0.84	0.01	0.61	0.00	21.33	140.77	0.88	0.01	0.61	0.00
21.34	141.29	0.91	0.01	0.61	0.00	21.35	141.46	0.94	0.01	0.61	0.00
21.36	141.33	0.96	0.01	0.61	0.00	21.37	141.01	0.98	0.01	0.61	0.00
21.38	140.59	1.01	0.01	0.61	0.00	21.39	140.07	1.04	0.01	0.61	0.00
21.40	139.41	1.06	0.01	0.61	0.00	21.41	138.70	1.09	0.01	0.61	0.00
21.42	138.03	1.11	0.01	0.61	0.00	21.43	137.61	1.13	0.01	0.61	0.00
21.44	137.48	1.15	0.01	0.61	0.00	21.45	137.58	1.17	0.01	0.61	0.00
21.46	137.69	1.20	0.00	0.61	0.00	21.47	137.75	1.24	0.00	0.61	0.00
21.48	137.76	1.27	0.00	0.61	0.00	21.49	137.72	1.30	0.00	0.61	0.00
21.50	137.64	1.33	0.00	0.61	0.00	21.51	137.52	1.35	0.00	0.61	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
21.52	137.36	1.37	0.00	0.61	0.00	21.53	137.15	1.37	0.00	0.61	0.00
21.54	136.88	1.37	0.00	0.61	0.00	21.55	136.57	1.37	0.00	0.61	0.00
21.56	136.25	1.37	0.00	0.61	0.00	21.57	135.92	1.37	0.00	0.61	0.00
21.58	135.61	1.37	0.00	0.61	0.00	21.59	135.32	1.37	0.00	0.61	0.00
21.60	135.05	1.37	0.00	0.61	0.00	21.61	134.69	1.35	0.00	0.61	0.00
21.62	134.21	1.32	0.00	0.61	0.00	21.63	133.56	1.27	0.00	0.61	0.00
21.64	132.79	1.23	0.00	0.61	0.00	21.65	131.92	1.18	0.00	0.61	0.00
21.66	130.98	1.13	0.01	0.61	0.00	21.67	130.02	1.08	0.01	0.61	0.00
21.68	129.12	1.04	0.01	0.61	0.00	21.69	128.50	1.01	0.01	0.61	0.00
21.70	128.15	0.99	0.01	0.61	0.00	21.71	128.01	0.96	0.01	0.61	0.00
21.72	127.76	0.93	0.01	0.61	0.00	21.73	127.38	0.89	0.01	0.60	0.00
21.74	126.91	0.86	0.01	0.60	0.00	21.75	126.35	0.82	0.30	0.60	0.00
21.76	125.74	0.79	0.30	0.60	0.00	21.77	125.16	0.76	0.30	0.60	0.00
21.78	124.62	0.74	0.30	0.60	0.00	21.79	124.05	0.72	0.30	0.60	0.00
21.80	123.36	0.69	0.30	0.60	0.00	21.81	122.50	0.66	0.30	0.60	0.00
21.82	121.49	0.63	0.30	0.60	0.00	21.83	120.36	0.60	0.30	0.60	0.00
21.84	119.18	0.57	0.30	0.60	0.00	21.85	118.02	0.54	0.30	0.60	0.00
21.86	117.00	0.52	0.30	0.60	0.00	21.87	116.07	0.50	0.30	0.60	0.00
21.88	115.12	0.49	0.30	0.60	0.00	21.89	114.00	0.47	0.30	0.60	0.00
21.90	112.71	0.45	0.30	0.60	0.00	21.91	111.28	0.42	0.30	0.60	0.00
21.92	109.78	0.40	0.30	0.60	0.00	21.93	108.30	0.38	0.30	0.60	0.00
21.94	106.94	0.36	0.30	0.60	0.00	21.95	105.86	0.35	0.30	0.60	0.00
21.96	104.99	0.34	0.30	0.60	0.00	21.97	104.21	0.33	0.30	0.60	0.00
21.98	103.32	0.33	0.30	0.60	0.00	21.99	102.36	0.32	0.30	0.60	0.00
22.00	101.38	0.31	0.30	0.60	0.00	22.01	100.42	0.31	0.30	0.60	0.00
22.02	99.54	0.30	0.30	0.60	0.00	22.03	98.80	0.29	0.30	0.60	0.00
22.04	98.23	0.29	0.30	0.60	0.00	22.05	97.78	0.29	0.30	0.60	0.00
22.06	97.32	0.29	0.30	0.60	0.00	22.07	96.82	0.29	0.30	0.60	0.00
22.08	96.28	0.29	0.30	0.60	0.00	22.09	95.73	0.29	0.30	0.60	0.00
22.10	95.21	0.29	0.30	0.60	0.00	22.11	94.74	0.29	0.30	0.60	0.00
22.12	94.34	0.29	0.30	0.60	0.00	22.13	93.99	0.29	0.30	0.60	0.00
22.14	93.64	0.29	0.30	0.60	0.00	22.15	93.24	0.29	0.30	0.60	0.00
22.16	92.80	0.29	0.30	0.60	0.00	22.17	92.34	0.29	0.30	0.60	0.00
22.18	91.89	0.29	0.30	0.60	0.00	22.19	91.46	0.29	0.30	0.60	0.00
22.20	91.08	0.29	0.30	0.60	0.00	22.21	90.74	0.29	0.30	0.60	0.00
22.22	90.37	0.28	0.30	0.60	0.00	22.23	89.94	0.28	0.30	0.60	0.00
22.24	89.44	0.28	0.30	0.60	0.00	22.25	88.90	0.27	0.30	0.60	0.00
22.26	88.36	0.27	0.30	0.60	0.00	22.27	87.83	0.27	0.30	0.60	0.00
22.28	87.34	0.26	0.30	0.59	0.00	22.29	86.98	0.26	0.30	0.59	0.00
22.30	86.93	0.26	0.30	0.59	0.00	22.31	87.19	0.27	0.30	0.59	0.00
22.32	87.67	0.27	0.30	0.59	0.00	22.33	88.21	0.28	0.30	0.59	0.00
22.34	88.76	0.29	0.30	0.59	0.00	22.35	89.31	0.29	0.30	0.59	0.00
22.36	89.82	0.30	0.30	0.59	0.00	22.37	90.26	0.30	0.30	0.59	0.00
22.38	90.61	0.31	0.30	0.59	0.00	22.39	90.88	0.31	0.30	0.59	0.00
22.40	91.11	0.32	0.30	0.59	0.00	22.41	91.37	0.32	0.30	0.59	0.00
22.42	91.65	0.32	0.30	0.59	0.00	22.43	91.94	0.32	0.30	0.59	0.00
22.44	92.22	0.33	0.30	0.59	0.00	22.45	92.49	0.33	0.30	0.59	0.00
22.46	92.71	0.33	0.30	0.59	0.00	22.47	92.95	0.34	0.30	0.59	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
22.48	93.25	0.34	0.30	0.59	0.00	22.49	93.63	0.34	0.30	0.59	0.00
22.50	94.07	0.35	0.30	0.59	0.00	22.51	94.54	0.35	0.30	0.59	0.00
22.52	95.02	0.36	0.30	0.59	0.00	22.53	95.48	0.36	0.30	0.59	0.00
22.54	95.89	0.37	0.30	0.59	0.00	22.55	96.22	0.37	0.29	0.59	0.00
22.56	96.42	0.37	0.29	0.59	0.00	22.57	96.52	0.37	0.29	0.59	0.00
22.58	96.56	0.37	0.29	0.59	0.00	22.59	96.62	0.37	0.29	0.59	0.00
22.60	96.68	0.37	0.29	0.59	0.00	22.61	96.73	0.37	0.29	0.59	0.00
22.62	96.79	0.37	0.29	0.59	0.00	22.63	96.83	0.37	0.29	0.59	0.00
22.64	96.74	0.37	0.29	0.59	0.00	22.65	96.39	0.37	0.29	0.59	0.00
22.66	95.73	0.36	0.29	0.59	0.00	22.67	94.87	0.35	0.29	0.59	0.00
22.68	93.91	0.33	0.29	0.59	0.00	22.69	92.89	0.32	0.29	0.59	0.00
22.70	91.86	0.31	0.29	0.59	0.00	22.71	90.88	0.30	0.29	0.59	0.00
22.72	90.00	0.29	0.29	0.59	0.00	22.73	89.43	0.28	0.29	0.59	0.00
22.74	89.12	0.28	0.29	0.59	0.00	22.75	89.02	0.28	0.29	0.59	0.00
22.76	88.91	0.28	0.29	0.59	0.00	22.77	88.79	0.28	0.29	0.59	0.00
22.78	88.66	0.28	0.29	0.59	0.00	22.79	88.54	0.28	0.29	0.59	0.00
22.80	88.43	0.28	0.29	0.59	0.00	22.81	88.33	0.28	0.29	0.59	0.00
22.82	88.22	0.28	0.29	0.59	0.00	22.83	88.10	0.28	0.29	0.58	0.00
22.84	87.94	0.28	0.29	0.58	0.00	22.85	87.77	0.28	0.29	0.58	0.00
22.86	87.58	0.28	0.29	0.58	0.00	22.87	87.40	0.28	0.29	0.58	0.00
22.88	87.22	0.28	0.29	0.58	0.00	22.89	87.07	0.28	0.29	0.58	0.00
22.90	86.96	0.28	0.29	0.58	0.00	22.91	86.90	0.28	0.29	0.58	0.00
22.92	86.88	0.28	0.29	0.58	0.00	22.93	86.87	0.28	0.29	0.58	0.00
22.94	86.86	0.28	0.29	0.58	0.00	22.95	86.85	0.28	0.29	0.58	0.00
22.96	86.84	0.28	0.29	0.58	0.00	22.97	86.84	0.28	0.29	0.58	0.00
22.98	86.84	0.28	0.29	0.58	0.00	22.99	87.24	0.28	0.29	0.58	0.00
23.00	88.13	0.29	0.29	0.58	0.00	23.01	89.56	0.30	0.29	0.58	0.00
23.02	91.17	0.32	0.29	0.58	0.00	23.03	92.86	0.34	0.29	0.58	0.00
23.04	94.55	0.35	0.29	0.58	0.00	23.05	96.14	0.37	0.29	0.58	0.00
23.06	97.57	0.38	0.29	0.58	0.00	23.07	98.73	0.40	0.29	0.58	0.00
23.08	99.63	0.40	0.29	0.58	0.00	23.09	100.40	0.41	0.29	0.58	0.00
23.10	101.20	0.42	0.29	0.58	0.00	23.11	102.10	0.42	0.29	0.58	0.00
23.12	103.05	0.43	0.29	0.58	0.00	23.13	103.99	0.44	0.29	0.58	0.00
23.14	104.88	0.44	0.29	0.58	0.00	23.15	105.68	0.45	0.29	0.58	0.00
23.16	106.25	0.45	0.29	0.58	0.00	23.17	106.58	0.45	0.29	0.58	0.00
23.18	106.75	0.45	0.29	0.58	0.00	23.19	106.88	0.45	0.29	0.58	0.00
23.20	107.03	0.44	0.29	0.58	0.00	23.21	107.17	0.44	0.29	0.58	0.00
23.22	107.30	0.44	0.29	0.58	0.00	23.23	107.42	0.43	0.29	0.58	0.00
23.24	107.53	0.43	0.29	0.58	0.00	23.25	107.79	0.43	0.29	0.58	0.00
23.26	108.26	0.43	0.29	0.58	0.00	23.27	108.98	0.44	0.29	0.58	0.00
23.28	109.80	0.44	0.29	0.58	0.00	23.29	110.69	0.45	0.29	0.58	0.00
23.30	111.58	0.46	0.29	0.58	0.00	23.31	112.44	0.46	0.29	0.58	0.00
23.32	113.22	0.47	0.29	0.58	0.00	23.33	113.89	0.47	0.29	0.58	0.00
23.34	114.49	0.48	0.29	0.58	0.00	23.35	115.12	0.48	0.29	0.58	0.00
23.36	115.84	0.49	0.29	0.58	0.00	23.37	116.65	0.49	0.29	0.58	0.00
23.38	117.51	0.50	0.29	0.57	0.00	23.39	118.35	0.51	0.29	0.57	0.00
23.40	119.15	0.51	0.29	0.57	0.00	23.41	119.86	0.52	0.29	0.57	0.00
23.42	120.43	0.52	0.29	0.57	0.00	23.43	120.90	0.53	0.29	0.57	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
23.44	121.34	0.53	0.29	0.57	0.00	23.45	121.84	0.54	0.29	0.57	0.00
23.46	122.38	0.55	0.29	0.57	0.00	23.47	122.93	0.55	0.29	0.57	0.00
23.48	123.47	0.56	0.29	0.57	0.00	23.49	123.97	0.56	0.29	0.57	0.00
23.50	124.40	0.57	0.29	0.57	0.00	23.51	124.76	0.57	0.29	0.57	0.00
23.52	125.09	0.58	0.29	0.57	0.00	23.53	125.45	0.59	0.29	0.57	0.00
23.54	125.86	0.60	0.29	0.57	0.00	23.55	126.28	0.60	0.29	0.57	0.00
23.56	126.70	0.61	0.29	0.57	0.00	23.57	127.10	0.62	0.29	0.57	0.00
23.58	127.45	0.63	0.29	0.57	0.00	23.59	127.74	0.64	0.29	0.57	0.00
23.60	128.00	0.64	0.29	0.57	0.00	23.61	128.27	0.65	0.29	0.57	0.00
23.62	128.59	0.65	0.29	0.57	0.00	23.63	128.95	0.66	0.29	0.57	0.00
23.64	129.32	0.67	0.29	0.57	0.00	23.65	129.68	0.67	0.28	0.57	0.00
23.66	130.02	0.68	0.28	0.57	0.00	23.67	130.32	0.68	0.28	0.57	0.00
23.68	130.55	0.69	0.28	0.57	0.00	23.69	130.74	0.69	0.28	0.57	0.00
23.70	130.91	0.68	0.28	0.57	0.00	23.71	131.10	0.68	0.28	0.57	0.00
23.72	131.31	0.68	0.28	0.57	0.00	23.73	131.53	0.68	0.28	0.57	0.00
23.74	131.73	0.67	0.28	0.57	0.00	23.75	131.92	0.67	0.28	0.57	0.00
23.76	132.11	0.67	0.28	0.57	0.00	23.77	132.73	0.67	0.28	0.57	0.00
23.78	133.90	0.69	0.28	0.57	0.00	23.79	135.68	0.71	0.28	0.57	0.00
23.80	137.70	0.73	0.28	0.57	0.00	23.81	139.83	0.75	0.28	0.57	0.00
23.82	141.98	0.78	0.28	0.57	0.00	23.83	144.03	0.80	0.28	0.57	0.00
23.84	145.88	0.82	0.28	0.57	0.00	23.85	147.36	0.84	0.01	0.57	0.00
23.86	148.48	0.85	0.01	0.57	0.00	23.87	149.39	0.86	0.01	0.57	0.00
23.88	150.31	0.87	0.01	0.57	0.00	23.89	151.34	0.88	0.01	0.57	0.00
23.90	152.43	0.89	0.01	0.57	0.00	23.91	153.50	0.90	0.01	0.57	0.00
23.92	154.52	0.91	0.01	0.57	0.00	23.93	155.42	0.92	0.01	0.56	0.00
23.94	155.86	0.92	0.01	0.56	0.00	23.95	155.74	0.91	0.01	0.56	0.00
23.96	155.06	0.90	0.01	0.56	0.00	23.97	154.17	0.88	0.01	0.56	0.00
23.98	153.18	0.86	0.01	0.56	0.00	23.99	152.14	0.85	0.01	0.56	0.00
24.00	151.11	0.83	0.28	0.56	0.00	24.01	150.13	0.81	0.28	0.56	0.00
24.02	149.29	0.80	0.28	0.56	0.00	24.03	148.71	0.79	0.28	0.56	0.00
24.04	148.33	0.78	0.28	0.56	0.00	24.05	148.07	0.78	0.28	0.56	0.00
24.06	147.78	0.77	0.28	0.56	0.00	24.07	147.47	0.77	0.28	0.56	0.00
24.08	147.15	0.77	0.28	0.56	0.00	24.09	146.85	0.76	0.28	0.56	0.00
24.10	146.57	0.76	0.28	0.56	0.00	24.11	146.31	0.76	0.28	0.56	0.00
24.12	145.98	0.75	0.28	0.56	0.00	24.13	145.56	0.74	0.28	0.56	0.00
24.14	145.01	0.73	0.28	0.56	0.00	24.15	144.40	0.72	0.28	0.56	0.00
24.16	143.75	0.71	0.28	0.56	0.00	24.17	143.10	0.70	0.28	0.56	0.00
24.18	142.47	0.69	0.28	0.56	0.00	24.19	141.90	0.68	0.28	0.56	0.00
24.20	141.43	0.67	0.28	0.56	0.00	24.21	141.01	0.66	0.28	0.56	0.00
24.22	140.58	0.65	0.28	0.56	0.00	24.23	140.08	0.64	0.28	0.56	0.00
24.24	139.52	0.63	0.28	0.56	0.00	24.25	138.93	0.62	0.28	0.56	0.00
24.26	138.34	0.61	0.28	0.56	0.00	24.27	137.78	0.59	0.28	0.56	0.00
24.28	137.32	0.59	0.28	0.56	0.00	24.29	137.31	0.58	0.28	0.56	0.00
24.30	137.79	0.59	0.28	0.56	0.00	24.31	138.72	0.60	0.28	0.56	0.00
24.32	139.77	0.61	0.28	0.56	0.00	24.33	140.89	0.62	0.28	0.56	0.00
24.34	142.00	0.63	0.28	0.56	0.00	24.35	143.07	0.64	0.28	0.56	0.00
24.36	144.03	0.65	0.28	0.56	0.00	24.37	144.83	0.66	0.28	0.56	0.00
24.38	145.56	0.67	0.28	0.56	0.00	24.39	146.32	0.67	0.28	0.56	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
24.40	147.18	0.68	0.28	0.56	0.00	24.41	148.14	0.69	0.28	0.56	0.00
24.42	149.14	0.71	0.28	0.56	0.00	24.43	150.12	0.72	0.28	0.56	0.00
24.44	151.04	0.73	0.28	0.56	0.00	24.45	151.85	0.74	0.28	0.56	0.00
24.46	152.35	0.74	0.28	0.56	0.00	24.47	152.55	0.74	0.28	0.56	0.00
24.48	152.50	0.74	0.28	0.55	0.00	24.49	152.39	0.74	0.28	0.55	0.00
24.50	152.28	0.74	0.28	0.55	0.00	24.51	152.16	0.74	0.28	0.55	0.00
24.52	152.05	0.74	0.28	0.55	0.00	24.53	151.94	0.74	0.28	0.55	0.00
24.54	151.83	0.74	0.28	0.55	0.00	24.55	151.55	0.74	0.28	0.55	0.00
24.56	151.06	0.74	0.28	0.55	0.00	24.57	150.34	0.73	0.28	0.55	0.00
24.58	149.52	0.72	0.28	0.55	0.00	24.59	148.66	0.72	0.28	0.55	0.00
24.60	147.79	0.71	0.28	0.55	0.00	24.61	146.96	0.70	0.28	0.55	0.00
24.62	146.20	0.70	0.28	0.55	0.00	24.63	145.55	0.69	0.28	0.55	0.00
24.64	144.93	0.69	0.28	0.55	0.00	24.65	144.26	0.68	0.28	0.55	0.00
24.66	143.47	0.68	0.28	0.55	0.00	24.67	142.60	0.67	0.28	0.55	0.00
24.68	141.70	0.66	0.28	0.55	0.00	24.69	140.80	0.66	0.28	0.55	0.00
24.70	139.96	0.65	0.28	0.55	0.00	24.71	139.22	0.65	0.28	0.55	0.00
24.72	138.58	0.64	0.28	0.55	0.00	24.73	137.98	0.64	0.28	0.55	0.00
24.74	137.33	0.63	0.28	0.55	0.00	24.75	136.59	0.62	0.28	0.55	0.00
24.76	135.78	0.62	0.27	0.55	0.00	24.77	134.95	0.61	0.27	0.55	0.00
24.78	134.14	0.60	0.27	0.55	0.00	24.79	133.40	0.60	0.27	0.55	0.00
24.80	132.74	0.59	0.27	0.55	0.00	24.81	132.06	0.59	0.27	0.55	0.00
24.82	131.26	0.58	0.27	0.55	0.00	24.83	130.26	0.57	0.27	0.55	0.00
24.84	129.12	0.56	0.27	0.55	0.00	24.85	127.90	0.54	0.27	0.55	0.00
24.86	126.66	0.53	0.27	0.55	0.00	24.87	125.46	0.52	0.27	0.55	0.00
24.88	124.37	0.51	0.27	0.55	0.00	24.89	123.49	0.50	0.27	0.55	0.00
24.90	122.80	0.49	0.27	0.55	0.00	24.91	122.23	0.48	0.27	0.55	0.00
24.92	121.62	0.48	0.27	0.55	0.00	24.93	120.95	0.47	0.27	0.55	0.00
24.94	120.24	0.47	0.27	0.55	0.00	24.95	119.54	0.46	0.27	0.55	0.00
24.96	118.88	0.45	0.27	0.55	0.00	24.97	118.29	0.45	0.27	0.55	0.00
24.98	117.79	0.44	0.27	0.55	0.00	24.99	117.31	0.44	0.27	0.55	0.00
25.00	116.78	0.43	0.27	0.55	0.00	25.01	116.17	0.43	0.27	0.55	0.00
25.02	115.51	0.42	0.27	0.55	0.00	25.03	114.83	0.41	0.27	0.54	0.00
25.04	114.16	0.41	0.27	0.54	0.00	25.05	113.54	0.40	0.27	0.54	0.00
25.06	113.00	0.40	0.27	0.54	0.00	25.07	112.54	0.39	0.27	0.54	0.00
25.08	112.08	0.39	0.27	0.54	0.00	25.09	111.57	0.38	0.27	0.54	0.00
25.10	110.99	0.37	0.27	0.54	0.00	25.11	110.37	0.37	0.27	0.54	0.00
25.12	109.74	0.36	0.27	0.54	0.00	25.13	109.13	0.36	0.27	0.54	0.00
25.14	108.57	0.35	0.27	0.54	0.00	25.15	108.17	0.35	0.27	0.54	0.00
25.16	107.98	0.34	0.27	0.54	0.00	25.17	107.96	0.34	0.27	0.54	0.00
25.18	108.03	0.34	0.27	0.54	0.00	25.19	108.10	0.34	0.27	0.54	0.00
25.20	108.17	0.34	0.27	0.54	0.00	25.21	108.24	0.34	0.27	0.54	0.00
25.22	108.31	0.34	0.27	0.54	0.00	25.23	108.37	0.34	0.27	0.54	0.00
25.24	108.26	0.34	0.27	0.54	0.00	25.25	107.92	0.34	0.27	0.54	0.00
25.26	107.32	0.33	0.27	0.54	0.00	25.27	106.61	0.33	0.27	0.54	0.00
25.28	105.83	0.32	0.27	0.54	0.00	25.29	105.03	0.31	0.27	0.54	0.00
25.30	104.25	0.31	0.27	0.54	0.00	25.31	103.52	0.30	0.27	0.54	0.00
25.32	102.92	0.30	0.27	0.54	0.00	25.33	102.51	0.29	0.27	0.54	0.00
25.34	102.23	0.29	0.27	0.54	0.00	25.35	102.02	0.29	0.27	0.54	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
25.36	101.79	0.29	0.27	0.54	0.00	25.37	101.54	0.29	0.27	0.54	0.00
25.38	101.29	0.29	0.27	0.54	0.00	25.39	101.05	0.29	0.27	0.54	0.00
25.40	100.84	0.29	0.27	0.54	0.00	25.41	100.73	0.29	0.27	0.54	0.00
25.42	100.82	0.29	0.27	0.54	0.00	25.43	101.10	0.30	0.27	0.54	0.00
25.44	101.50	0.30	0.27	0.54	0.00	25.45	101.93	0.31	0.27	0.54	0.00
25.46	102.36	0.32	0.27	0.54	0.00	25.47	102.78	0.32	0.27	0.54	0.00
25.48	103.16	0.33	0.27	0.54	0.00	25.49	103.49	0.33	0.27	0.54	0.00
25.50	103.79	0.34	0.27	0.54	0.00	25.51	104.11	0.34	0.27	0.54	0.00
25.52	104.50	0.35	0.27	0.54	0.00	25.53	104.94	0.35	0.27	0.54	0.00
25.54	105.42	0.36	0.27	0.54	0.00	25.55	105.90	0.36	0.27	0.54	0.00
25.56	106.35	0.37	0.27	0.54	0.00	25.57	106.77	0.38	0.27	0.54	0.00
25.58	107.13	0.38	0.27	0.53	0.00	25.59	107.56	0.38	0.27	0.53	0.00
25.60	108.11	0.39	0.27	0.53	0.00	25.61	108.81	0.39	0.27	0.53	0.00
25.62	109.61	0.40	0.27	0.53	0.00	25.63	110.45	0.41	0.27	0.53	0.00
25.64	111.30	0.41	0.27	0.53	0.00	25.65	112.10	0.42	0.27	0.53	0.00
25.66	112.82	0.42	0.27	0.53	0.00	25.67	113.38	0.43	0.27	0.53	0.00
25.68	113.79	0.43	0.27	0.53	0.00	25.69	114.10	0.43	0.27	0.53	0.00
25.70	114.43	0.43	0.27	0.53	0.00	25.71	114.79	0.43	0.27	0.53	0.00
25.72	115.16	0.43	0.27	0.53	0.00	25.73	115.53	0.43	0.27	0.53	0.00
25.74	115.87	0.43	0.27	0.53	0.00	25.75	116.16	0.43	0.27	0.53	0.00
25.76	116.48	0.43	0.27	0.53	0.00	25.77	116.88	0.43	0.27	0.53	0.00
25.78	117.40	0.44	0.27	0.53	0.00	25.79	118.01	0.44	0.27	0.53	0.00
25.80	118.66	0.45	0.27	0.53	0.00	25.81	119.32	0.45	0.27	0.53	0.00
25.82	119.96	0.46	0.27	0.53	0.00	25.83	120.54	0.47	0.27	0.53	0.00
25.84	121.03	0.47	0.27	0.53	0.00	25.85	121.47	0.47	0.27	0.53	0.00
25.86	121.91	0.48	0.26	0.53	0.00	25.87	122.42	0.48	0.26	0.53	0.00
25.88	122.99	0.49	0.26	0.53	0.00	25.89	123.59	0.49	0.26	0.53	0.00
25.90	124.19	0.50	0.26	0.53	0.00	25.91	124.75	0.51	0.26	0.53	0.00
25.92	125.26	0.51	0.26	0.53	0.00	25.93	125.83	0.52	0.26	0.53	0.00
25.94	126.67	0.53	0.26	0.53	0.00	25.95	127.88	0.54	0.26	0.53	0.00
25.96	129.37	0.56	0.26	0.53	0.00	25.97	130.97	0.58	0.26	0.53	0.00
25.98	132.62	0.60	0.26	0.53	0.00	25.99	134.20	0.62	0.26	0.53	0.00
26.00	135.66	0.64	0.26	0.53	0.00	26.01	136.92	0.65	0.26	0.53	0.00
26.02	137.82	0.66	0.26	0.53	0.00	26.03	138.45	0.67	0.26	0.53	0.00
26.04	138.94	0.67	0.26	0.53	0.00	26.05	139.49	0.68	0.26	0.53	0.00
26.06	140.09	0.69	0.26	0.53	0.00	26.07	140.70	0.69	0.26	0.53	0.00
26.08	141.28	0.70	0.26	0.53	0.00	26.09	141.82	0.70	0.26	0.53	0.00
26.10	142.20	0.71	0.26	0.53	0.00	26.11	142.23	0.70	0.26	0.53	0.00
26.12	141.90	0.70	0.26	0.53	0.00	26.13	141.28	0.68	0.26	0.52	0.00
26.14	140.57	0.67	0.26	0.52	0.00	26.15	139.80	0.66	0.26	0.52	0.00
26.16	139.01	0.64	0.26	0.52	0.00	26.17	138.25	0.63	0.26	0.52	0.00
26.18	137.54	0.62	0.26	0.52	0.00	26.19	137.08	0.61	0.26	0.52	0.00
26.20	136.93	0.60	0.26	0.52	0.00	26.21	137.08	0.60	0.26	0.52	0.00
26.22	137.35	0.60	0.26	0.52	0.00	26.23	137.65	0.60	0.26	0.52	0.00
26.24	137.96	0.60	0.26	0.52	0.00	26.25	138.26	0.60	0.26	0.52	0.00
26.26	138.55	0.60	0.26	0.52	0.00	26.27	138.79	0.60	0.26	0.52	0.00
26.28	139.09	0.60	0.26	0.52	0.00	26.29	139.50	0.61	0.26	0.52	0.00
26.30	140.07	0.61	0.26	0.52	0.00	26.31	140.73	0.62	0.26	0.52	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
26.32	141.43	0.62	0.26	0.52	0.00	26.33	142.15	0.63	0.26	0.52	0.00
26.34	142.85	0.63	0.26	0.52	0.00	26.35	143.48	0.64	0.26	0.52	0.00
26.36	143.99	0.64	0.26	0.52	0.00	26.37	144.35	0.65	0.26	0.52	0.00
26.38	144.60	0.65	0.26	0.52	0.00	26.39	144.83	0.66	0.26	0.52	0.00
26.40	145.07	0.66	0.26	0.52	0.00	26.41	145.33	0.67	0.26	0.52	0.00
26.42	145.58	0.67	0.26	0.52	0.00	26.43	145.81	0.68	0.26	0.52	0.00
26.44	146.02	0.68	0.26	0.52	0.00	26.45	146.09	0.69	0.26	0.52	0.00
26.46	145.97	0.69	0.26	0.52	0.00	26.47	145.65	0.69	0.26	0.52	0.00
26.48	145.23	0.69	0.26	0.52	0.00	26.49	144.76	0.69	0.26	0.52	0.00
26.50	144.28	0.69	0.26	0.52	0.00	26.51	143.80	0.69	0.26	0.52	0.00
26.52	143.36	0.69	0.26	0.52	0.00	26.53	142.97	0.69	0.26	0.52	0.00
26.54	142.70	0.69	0.26	0.52	0.00	26.55	142.55	0.69	0.26	0.52	0.00
26.56	142.46	0.69	0.26	0.52	0.00	26.57	142.37	0.69	0.26	0.52	0.00
26.58	142.27	0.70	0.26	0.52	0.00	26.59	142.16	0.70	0.26	0.52	0.00
26.60	142.06	0.70	0.26	0.52	0.00	26.61	141.96	0.70	0.26	0.52	0.00
26.62	141.84	0.71	0.26	0.52	0.00	26.63	141.65	0.70	0.26	0.52	0.00
26.64	141.35	0.70	0.26	0.52	0.00	26.65	140.95	0.70	0.26	0.52	0.00
26.66	140.50	0.69	0.26	0.52	0.00	26.67	140.03	0.68	0.26	0.52	0.00
26.68	139.55	0.68	0.26	0.51	0.00	26.69	139.10	0.67	0.26	0.51	0.00
26.70	138.69	0.67	0.26	0.51	0.00	26.71	138.29	0.66	0.26	0.51	0.00
26.72	137.83	0.65	0.26	0.51	0.00	26.73	137.24	0.65	0.26	0.51	0.00
26.74	136.53	0.64	0.26	0.51	0.00	26.75	135.76	0.63	0.26	0.51	0.00
26.76	134.95	0.62	0.26	0.51	0.00	26.77	134.15	0.61	0.26	0.51	0.00
26.78	133.41	0.60	0.26	0.51	0.00	26.79	132.75	0.60	0.26	0.51	0.00
26.80	132.30	0.59	0.26	0.51	0.00	26.81	132.00	0.59	0.26	0.51	0.00
26.82	131.79	0.59	0.26	0.51	0.00	26.83	131.56	0.59	0.26	0.51	0.00
26.84	131.32	0.59	0.26	0.51	0.00	26.85	131.06	0.59	0.26	0.51	0.00
26.86	130.82	0.59	0.26	0.51	0.00	26.87	130.60	0.59	0.26	0.51	0.00
26.88	130.53	0.59	0.26	0.51	0.00	26.89	130.92	0.60	0.26	0.51	0.00
26.90	131.80	0.61	0.26	0.51	0.00	26.91	133.09	0.63	0.26	0.51	0.00
26.92	134.49	0.65	0.26	0.51	0.00	26.93	135.92	0.67	0.26	0.51	0.00
26.94	137.32	0.69	0.26	0.51	0.00	26.95	138.61	0.71	0.26	0.51	0.00
26.96	139.73	0.73	0.25	0.51	0.00	26.97	140.34	0.74	0.25	0.51	0.00
26.98	140.30	0.74	0.25	0.51	0.00	26.99	139.64	0.74	0.25	0.51	0.00
27.00	138.72	0.72	0.25	0.51	0.00	27.01	137.70	0.71	0.25	0.51	0.00
27.02	136.65	0.70	0.25	0.51	0.00	27.03	135.60	0.68	0.25	0.51	0.00
27.04	134.62	0.67	0.25	0.51	0.00	27.05	133.76	0.66	0.25	0.51	0.00
27.06	132.81	0.65	0.25	0.51	0.00	27.07	131.63	0.63	0.25	0.51	0.00
27.08	130.06	0.61	0.25	0.51	0.00	27.09	128.21	0.58	0.25	0.51	0.00
27.10	126.17	0.55	0.25	0.51	0.00	27.11	124.02	0.52	0.25	0.51	0.00
27.12	121.88	0.50	0.25	0.51	0.00	27.13	119.86	0.47	0.25	0.51	0.00
27.14	118.32	0.45	0.25	0.51	0.00	27.15	117.69	0.44	0.25	0.51	0.00
27.16	117.95	0.44	0.25	0.51	0.00	27.17	118.73	0.45	0.25	0.51	0.00
27.18	119.60	0.46	0.25	0.51	0.00	27.19	120.52	0.46	0.25	0.51	0.00
27.20	121.43	0.47	0.25	0.51	0.00	27.21	122.29	0.48	0.25	0.51	0.00
27.22	123.05	0.48	0.25	0.51	0.00	27.23	123.57	0.49	0.25	0.50	0.00
27.24	123.83	0.49	0.25	0.50	0.00	27.25	123.89	0.49	0.25	0.50	0.00
27.26	123.91	0.49	0.25	0.50	0.00	27.27	123.93	0.49	0.25	0.50	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
27.28	123.95	0.49	0.25	0.50	0.00	27.29	123.97	0.49	0.25	0.50	0.00
27.30	123.99	0.49	0.25	0.50	0.00	27.31	124.00	0.49	0.25	0.50	0.00
27.32	123.99	0.49	0.25	0.50	0.00	27.33	123.95	0.49	0.25	0.50	0.00
27.34	123.89	0.49	0.25	0.50	0.00	27.35	123.81	0.49	0.25	0.50	0.00
27.36	123.73	0.49	0.25	0.50	0.00	27.37	123.65	0.49	0.25	0.50	0.00
27.38	123.58	0.49	0.25	0.50	0.00	27.39	123.50	0.49	0.25	0.50	0.00
27.40	123.58	0.49	0.25	0.50	0.00	27.41	124.08	0.50	0.25	0.50	0.00
27.42	125.06	0.51	0.25	0.50	0.00	27.43	126.43	0.52	0.25	0.50	0.00
27.44	127.93	0.54	0.25	0.50	0.00	27.45	129.46	0.56	0.25	0.50	0.00
27.46	130.97	0.58	0.25	0.50	0.00	27.47	132.36	0.60	0.25	0.50	0.00
27.48	133.57	0.61	0.25	0.50	0.00	27.49	134.63	0.63	0.25	0.50	0.00
27.50	135.70	0.64	0.25	0.50	0.00	27.51	136.91	0.65	0.25	0.50	0.00
27.52	138.33	0.67	0.25	0.50	0.00	27.53	139.85	0.69	0.25	0.50	0.00
27.54	141.40	0.71	0.25	0.50	0.00	27.55	142.91	0.73	0.25	0.50	0.00
27.56	144.29	0.74	0.25	0.50	0.00	27.57	145.44	0.76	0.25	0.50	0.00
27.58	145.96	0.76	0.25	0.50	0.00	27.59	145.89	0.76	0.25	0.50	0.00
27.60	145.30	0.74	0.25	0.50	0.00	27.61	144.60	0.72	0.25	0.50	0.00
27.62	143.82	0.70	0.25	0.50	0.00	27.63	142.98	0.68	0.25	0.50	0.00
27.64	142.14	0.66	0.25	0.50	0.00	27.65	141.34	0.65	0.25	0.50	0.00
27.66	140.58	0.63	0.25	0.50	0.00	27.67	139.71	0.62	0.25	0.50	0.00
27.68	138.59	0.60	0.25	0.50	0.00	27.69	137.16	0.58	0.25	0.50	0.00
27.70	135.49	0.55	0.25	0.50	0.00	27.71	133.66	0.52	0.25	0.50	0.00
27.72	131.75	0.50	0.25	0.50	0.00	27.73	129.85	0.47	0.25	0.50	0.00
27.74	128.09	0.45	0.25	0.50	0.00	27.75	126.91	0.44	0.25	0.50	0.00
27.76	126.37	0.43	0.25	0.50	0.00	27.77	126.41	0.43	0.25	0.50	0.00
27.78	126.58	0.43	0.25	0.49	0.00	27.79	126.77	0.43	0.25	0.49	0.00
27.80	126.96	0.43	0.25	0.49	0.00	27.81	127.15	0.43	0.25	0.49	0.00
27.82	127.32	0.43	0.25	0.49	0.00	27.83	127.50	0.43	0.25	0.49	0.00
27.84	127.96	0.43	0.25	0.49	0.00	27.85	128.79	0.44	0.25	0.49	0.00
27.86	130.02	0.45	0.25	0.49	0.00	27.87	131.40	0.46	0.25	0.49	0.00
27.88	132.84	0.48	0.25	0.49	0.00	27.89	134.27	0.49	0.25	0.49	0.00
27.90	135.62	0.51	0.25	0.49	0.00	27.91	136.82	0.52	0.25	0.49	0.00
27.92	137.75	0.53	0.25	0.49	0.00	27.93	138.39	0.54	0.25	0.49	0.00
27.94	138.82	0.55	0.25	0.49	0.00	27.95	139.21	0.55	0.25	0.49	0.00
27.96	139.63	0.56	0.25	0.49	0.00	27.97	140.06	0.57	0.25	0.49	0.00
27.98	140.48	0.58	0.25	0.49	0.00	27.99	140.86	0.58	0.25	0.49	0.00
28.00	141.20	0.59	0.25	0.49	0.00	28.01	141.24	0.59	0.25	0.49	0.00
28.02	140.88	0.59	0.25	0.49	0.00	28.03	140.12	0.59	0.25	0.49	0.00
28.04	139.17	0.58	0.25	0.49	0.00	28.05	138.14	0.57	0.24	0.49	0.00
28.06	137.08	0.56	0.24	0.49	0.00	28.07	136.04	0.55	0.24	0.49	0.00
28.08	135.08	0.55	0.24	0.49	0.00	28.09	134.25	0.54	0.24	0.49	0.00
28.10	133.50	0.53	0.24	0.49	0.00	28.11	132.74	0.53	0.24	0.49	0.00
28.12	131.87	0.52	0.24	0.49	0.00	28.13	130.88	0.51	0.24	0.49	0.00
28.14	129.83	0.51	0.24	0.49	0.00	28.15	128.76	0.50	0.24	0.49	0.00
28.16	127.74	0.49	0.24	0.49	0.00	28.17	126.81	0.48	0.24	0.49	0.00
28.18	126.23	0.48	0.24	0.49	0.00	28.19	126.27	0.48	0.24	0.49	0.00
28.20	126.92	0.49	0.24	0.49	0.00	28.21	127.92	0.51	0.24	0.49	0.00
28.22	129.00	0.53	0.24	0.49	0.00	28.23	130.07	0.55	0.24	0.49	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
28.24	131.09	0.56	0.24	0.49	0.00	28.25	132.00	0.58	0.24	0.49	0.00
28.26	132.77	0.60	0.24	0.49	0.00	28.27	133.20	0.61	0.24	0.49	0.00
28.28	133.27	0.61	0.24	0.49	0.00	28.29	133.02	0.61	0.24	0.49	0.00
28.30	132.69	0.61	0.24	0.49	0.00	28.31	132.33	0.61	0.24	0.49	0.00
28.32	131.96	0.61	0.24	0.49	0.00	28.33	131.60	0.61	0.24	0.48	0.00
28.34	131.26	0.61	0.24	0.48	0.00	28.35	130.93	0.61	0.24	0.48	0.00
28.36	130.34	0.60	0.24	0.48	0.00	28.37	129.37	0.59	0.24	0.48	0.00
28.38	127.96	0.57	0.24	0.48	0.00	28.39	126.32	0.55	0.24	0.48	0.00
28.40	124.52	0.52	0.24	0.48	0.00	28.41	122.64	0.50	0.24	0.48	0.00
28.42	120.79	0.47	0.24	0.48	0.00	28.43	119.05	0.45	0.24	0.48	0.00
28.44	117.71	0.44	0.24	0.48	0.00	28.45	116.89	0.43	0.24	0.48	0.00
28.46	116.50	0.42	0.24	0.48	0.00	28.47	116.25	0.41	0.24	0.48	0.00
28.48	115.98	0.41	0.24	0.48	0.00	28.49	115.69	0.40	0.24	0.48	0.00
28.50	115.39	0.40	0.24	0.48	0.00	28.51	115.10	0.39	0.24	0.48	0.00
28.52	114.83	0.39	0.24	0.48	0.00	28.53	114.65	0.38	0.24	0.48	0.00
28.54	114.55	0.38	0.24	0.48	0.00	28.55	114.51	0.38	0.24	0.48	0.00
28.56	114.48	0.38	0.24	0.48	0.00	28.57	114.45	0.38	0.24	0.48	0.00
28.58	114.42	0.38	0.24	0.48	0.00	28.59	114.38	0.38	0.24	0.48	0.00
28.60	114.35	0.38	0.24	0.48	0.00	28.61	114.31	0.38	0.24	0.48	0.00
28.62	114.13	0.38	0.24	0.48	0.00	28.63	113.80	0.38	0.24	0.48	0.00
28.64	113.30	0.37	0.24	0.48	0.00	28.65	112.73	0.37	0.24	0.48	0.00
28.66	112.13	0.36	0.24	0.48	0.00	28.67	111.52	0.35	0.24	0.48	0.00
28.68	110.92	0.35	0.24	0.48	0.00	28.69	110.39	0.34	0.24	0.48	0.00
28.70	110.09	0.34	0.24	0.48	0.00	28.71	110.20	0.34	0.24	0.48	0.00
28.72	110.76	0.35	0.24	0.48	0.00	28.73	111.57	0.35	0.24	0.48	0.00
28.74	112.47	0.36	0.24	0.48	0.00	28.75	113.41	0.36	0.24	0.48	0.00
28.76	114.33	0.37	0.24	0.48	0.00	28.77	115.19	0.38	0.24	0.48	0.00
28.78	115.95	0.38	0.24	0.48	0.00	28.79	116.73	0.39	0.24	0.48	0.00
28.80	117.70	0.40	0.24	0.48	0.00	28.81	118.95	0.41	0.24	0.48	0.00
28.82	120.39	0.43	0.24	0.48	0.00	28.83	121.91	0.44	0.24	0.48	0.00
28.84	123.44	0.46	0.24	0.48	0.00	28.85	124.89	0.48	0.24	0.48	0.00
28.86	126.20	0.49	0.24	0.48	0.00	28.87	127.27	0.51	0.24	0.48	0.00
28.88	128.03	0.52	0.24	0.47	0.00	28.89	128.59	0.53	0.24	0.47	0.00
28.90	129.06	0.54	0.24	0.47	0.00	28.91	129.57	0.55	0.24	0.47	0.00
28.92	130.09	0.56	0.24	0.47	0.00	28.93	130.58	0.57	0.24	0.47	0.00
28.94	131.03	0.58	0.24	0.47	0.00	28.95	131.41	0.60	0.24	0.47	0.00
28.96	131.77	0.61	0.24	0.47	0.00	28.97	132.22	0.62	0.24	0.47	0.00
28.98	132.80	0.63	0.24	0.47	0.00	28.99	133.50	0.65	0.24	0.47	0.00
29.00	134.21	0.67	0.24	0.47	0.00	29.01	134.90	0.69	0.24	0.47	0.00
29.02	135.54	0.71	0.24	0.47	0.00	29.03	136.08	0.73	0.24	0.47	0.00
29.04	136.53	0.75	0.24	0.47	0.00	29.05	136.97	0.76	0.24	0.47	0.00
29.06	137.50	0.78	0.24	0.47	0.00	29.07	138.17	0.80	0.24	0.47	0.00
29.08	138.93	0.82	0.24	0.47	0.00	29.09	139.70	0.85	0.01	0.47	0.00
29.10	140.44	0.87	0.01	0.47	0.00	29.11	141.12	0.90	0.01	0.47	0.00
29.12	141.70	0.92	0.01	0.47	0.00	29.13	142.15	0.94	0.01	0.47	0.00
29.14	142.44	0.95	0.01	0.47	0.00	29.15	142.62	0.96	0.01	0.47	0.00
29.16	142.75	0.97	0.01	0.47	0.00	29.17	142.88	0.98	0.01	0.47	0.00
29.18	143.01	0.99	0.01	0.47	0.00	29.19	143.13	1.01	0.01	0.47	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
29.20	143.23	1.02	0.01	0.47	0.00	29.21	143.31	1.03	0.01	0.47	0.00
29.22	143.36	1.04	0.01	0.47	0.00	29.23	143.39	1.04	0.01	0.47	0.00
29.24	143.40	1.04	0.01	0.47	0.00	29.25	143.41	1.03	0.01	0.47	0.00
29.26	143.41	1.03	0.01	0.47	0.00	29.27	143.42	1.02	0.01	0.47	0.00
29.28	143.42	1.02	0.01	0.47	0.00	29.29	143.42	1.01	0.01	0.47	0.00
29.30	143.42	1.01	0.01	0.47	0.00	29.31	143.42	1.01	0.01	0.47	0.00
29.32	143.42	1.01	0.01	0.47	0.00	29.33	143.41	1.01	0.01	0.47	0.00
29.34	143.41	1.02	0.01	0.47	0.00	29.35	143.41	1.02	0.01	0.47	0.00
29.36	143.41	1.02	0.01	0.47	0.00	29.37	143.40	1.03	0.01	0.47	0.00
29.38	143.39	1.03	0.01	0.47	0.00	29.39	143.38	1.03	0.01	0.47	0.00
29.40	143.37	1.04	0.01	0.47	0.00	29.41	143.34	1.06	0.00	0.47	0.00
29.42	143.27	1.08	0.00	0.47	0.00	29.43	143.15	1.10	0.00	0.46	0.00
29.44	142.98	1.12	0.00	0.46	0.00	29.45	142.76	1.15	0.00	0.46	0.00
29.46	142.51	1.17	0.00	0.46	0.00	29.47	142.25	1.19	0.00	0.46	0.00
29.48	142.09	1.21	0.00	0.46	0.00	29.49	142.09	1.23	0.00	0.46	0.00
29.50	142.27	1.25	0.00	0.46	0.00	29.51	142.53	1.27	0.00	0.46	0.00
29.52	142.80	1.29	0.00	0.46	0.00	29.53	143.05	1.31	0.00	0.46	0.00
29.54	143.29	1.34	0.00	0.46	0.00	29.55	143.49	1.36	0.00	0.46	0.00
29.56	143.65	1.38	0.00	0.46	0.00	29.57	143.85	1.39	0.00	0.46	0.00
29.58	144.14	1.40	0.00	0.46	0.00	29.59	144.57	1.41	0.00	0.46	0.00
29.60	145.06	1.42	0.00	0.46	0.00	29.61	145.60	1.42	0.00	0.46	0.00
29.62	146.14	1.43	0.00	0.46	0.00	29.63	146.67	1.44	0.00	0.46	0.00
29.64	147.16	1.45	0.00	0.46	0.00	29.65	147.58	1.45	0.00	0.46	0.00
29.66	147.98	1.45	0.00	0.46	0.00	29.67	148.42	1.44	0.00	0.46	0.00
29.68	148.94	1.43	0.00	0.46	0.00	29.69	149.52	1.42	0.00	0.46	0.00
29.70	150.11	1.41	0.00	0.46	0.00	29.71	150.69	1.40	0.00	0.46	0.00
29.72	151.23	1.38	0.00	0.46	0.00	29.73	151.70	1.37	0.00	0.46	0.00
29.74	152.18	1.36	0.00	0.46	0.00	29.75	152.81	1.35	0.00	0.46	0.00
29.76	153.67	1.33	0.00	0.46	0.00	29.77	154.68	1.31	0.00	0.46	0.00
29.78	155.74	1.29	0.00	0.46	0.00	29.79	156.76	1.26	0.00	0.46	0.00
29.80	157.71	1.24	0.00	0.46	0.00	29.81	158.53	1.21	0.00	0.46	0.00
29.82	159.19	1.19	0.00	0.46	0.00	29.83	159.85	1.18	0.00	0.46	0.00
29.84	160.64	1.19	0.00	0.46	0.00	29.85	161.67	1.20	0.00	0.46	0.00
29.86	162.86	1.21	0.00	0.46	0.00	29.87	164.15	1.23	0.00	0.46	0.00
29.88	165.46	1.24	0.00	0.46	0.00	29.89	166.72	1.26	0.00	0.46	0.00
29.90	167.88	1.27	0.00	0.46	0.00	29.91	168.83	1.29	0.00	0.46	0.00
29.92	169.50	1.30	0.00	0.46	0.00	29.93	169.97	1.32	0.00	0.46	0.00
29.94	170.36	1.34	0.00	0.46	0.00	29.95	170.77	1.37	0.00	0.46	0.00
29.96	171.17	1.40	0.00	0.46	0.00	29.97	171.53	1.43	0.00	0.46	0.00
29.98	171.85	1.45	0.00	0.45	0.00	29.99	172.11	1.48	0.00	0.45	0.00
30.00	172.36	1.49	0.00	0.45	0.00	30.01	172.67	1.50	0.00	0.45	0.00
30.02	173.11	1.49	0.00	0.45	0.00	30.03	173.64	1.49	0.00	0.45	0.00
30.04	174.21	1.48	0.00	0.45	0.00	30.05	174.80	1.47	0.00	0.45	0.00
30.06	175.37	1.46	0.00	0.45	0.00	30.07	175.89	1.45	0.00	0.45	0.00
30.08	176.33	1.45	0.00	0.45	0.00	30.09	176.70	1.44	0.00	0.45	0.00
30.10	177.04	1.44	0.00	0.45	0.00	30.11	177.41	1.44	0.00	0.45	0.00
30.12	177.84	1.45	0.00	0.45	0.00	30.13	178.29	1.45	0.00	0.45	0.00
30.14	178.76	1.45	0.00	0.45	0.00	30.15	179.21	1.46	0.00	0.45	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
30.16	179.63	1.46	0.00	0.45	0.00	30.17	179.94	1.47	0.00	0.45	0.00
30.18	180.05	1.47	0.00	0.45	0.00	30.19	179.98	1.49	0.00	0.45	0.00
30.20	179.78	1.51	0.00	0.45	0.00	30.21	179.51	1.53	0.00	0.45	0.00
30.22	179.21	1.55	0.00	0.45	0.00	30.23	178.86	1.58	0.00	0.45	0.00
30.24	178.51	1.60	0.00	0.45	0.00	30.25	178.16	1.62	0.00	0.45	0.00
30.26	177.94	1.64	0.00	0.45	0.00	30.27	177.92	1.65	0.00	0.45	0.00
30.28	178.10	1.66	0.00	0.45	0.00	30.29	178.36	1.67	0.00	0.45	0.00
30.30	178.65	1.68	0.00	0.45	0.00	30.31	178.95	1.69	0.00	0.45	0.00
30.32	179.24	1.70	0.00	0.45	0.00	30.33	179.50	1.71	0.00	0.45	0.00
30.34	179.73	1.72	0.00	0.45	0.00	30.35	180.02	1.72	0.00	0.45	0.00
30.36	180.43	1.72	0.00	0.45	0.00	30.37	181.00	1.72	0.00	0.45	0.00
30.38	181.65	1.71	0.00	0.45	0.00	30.39	182.33	1.70	0.00	0.45	0.00
30.40	183.02	1.69	0.00	0.45	0.00	30.41	183.68	1.68	0.00	0.45	0.00
30.42	184.27	1.68	0.00	0.45	0.00	30.43	184.73	1.67	0.00	0.45	0.00
30.44	184.99	1.66	0.00	0.45	0.00	30.45	185.10	1.65	0.00	0.45	0.00
30.46	185.12	1.64	0.00	0.45	0.00	30.47	185.13	1.63	0.00	0.45	0.00
30.48	185.15	1.62	0.00	0.45	0.00	30.49	185.15	1.60	0.00	0.45	0.00
30.50	185.15	1.59	0.00	0.45	0.00	30.51	185.14	1.58	0.00	0.45	0.00
30.52	185.15	1.58	0.00	0.45	0.00	30.53	185.19	2.00	0.00	0.44	0.00
30.54	185.26	2.00	0.00	0.44	0.00	30.55	185.32	2.00	0.00	0.44	0.00
30.56	185.34	2.00	0.00	0.44	0.00	30.57	185.33	2.00	0.00	0.44	0.00
30.58	185.28	2.00	0.00	0.44	0.00	30.59	185.20	2.00	0.00	0.44	0.00
30.60	185.10	2.00	0.00	0.44	0.00	30.61	185.05	2.00	0.00	0.44	0.00
30.62	185.03	2.00	0.00	0.44	0.00	30.63	184.98	2.00	0.00	0.44	0.00
30.64	184.77	2.00	0.00	0.44	0.00	30.65	389.55	2.00	0.00	0.44	0.00
30.66	361.22	2.00	0.00	0.44	0.00	30.67	335.85	2.00	0.00	0.44	0.00
30.68	314.26	2.00	0.00	0.44	0.00	30.69	296.66	2.00	0.00	0.44	0.00
30.70	280.63	2.00	0.00	0.44	0.00	30.71	263.98	2.00	0.00	0.44	0.00
30.72	245.43	2.00	0.00	0.44	0.00	30.73	226.15	2.00	0.00	0.44	0.00
30.74	207.38	2.00	0.00	0.44	0.00	30.75	190.07	2.00	0.00	0.44	0.00
30.76	174.86	2.00	0.00	0.44	0.00	30.77	162.21	2.00	0.00	0.44	0.00
30.78	170.72	2.00	0.00	0.44	0.00	30.79	169.44	2.00	0.00	0.44	0.00
30.80	168.00	2.00	0.00	0.44	0.00	30.81	166.29	2.00	0.00	0.44	0.00
30.82	164.38	2.00	0.00	0.44	0.00	30.83	162.36	2.00	0.00	0.44	0.00
30.84	160.34	2.00	0.00	0.44	0.00	30.85	158.46	2.00	0.00	0.44	0.00
30.86	156.82	2.00	0.00	0.44	0.00	30.87	155.76	2.00	0.00	0.44	0.00
30.88	155.15	2.00	0.00	0.44	0.00	30.89	154.86	2.00	0.00	0.44	0.00
30.90	154.52	2.00	0.00	0.44	0.00	30.91	154.17	2.00	0.00	0.44	0.00
30.92	153.82	2.00	0.00	0.44	0.00	30.93	153.49	2.00	0.00	0.44	0.00
30.94	153.19	2.00	0.00	0.44	0.00	30.95	153.04	2.00	0.00	0.44	0.00
30.96	153.25	0.46	0.72	0.44	0.00	30.97	153.83	0.46	0.72	0.44	0.00
30.98	154.72	0.47	0.71	0.44	0.00	30.99	155.72	0.47	0.71	0.44	0.00
31.00	156.77	0.48	0.71	0.44	0.00	31.01	157.82	0.49	0.70	0.44	0.00
31.02	158.82	0.50	0.70	0.44	0.00	31.03	159.70	0.50	0.69	0.44	0.00
31.04	160.42	0.51	0.69	0.44	0.00	31.05	161.03	0.51	0.69	0.44	0.00
31.06	161.64	0.52	0.69	0.44	0.00	31.07	162.33	0.52	0.68	0.44	0.00
31.08	163.09	0.53	0.68	0.43	0.00	31.09	163.88	0.54	0.68	0.43	0.00
31.10	164.65	0.54	0.67	0.43	0.00	31.11	165.36	0.55	0.67	0.43	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
31.12	165.98	0.55	0.63	0.43	0.00	31.13	166.52	0.56	0.63	0.43	0.00
31.14	167.06	0.56	0.63	0.43	0.00	31.15	167.66	0.57	0.62	0.43	0.00
31.16	168.36	0.57	0.62	0.43	0.00	31.17	169.11	0.58	0.61	0.43	0.00
31.18	169.86	0.59	0.61	0.43	0.00	31.19	170.59	0.59	0.61	0.43	0.00
31.20	171.26	0.60	0.60	0.43	0.00	31.21	171.80	0.61	0.60	0.43	0.00
31.22	172.24	0.61	0.60	0.43	0.00	31.23	172.64	0.61	0.59	0.43	0.00
31.24	173.07	0.62	0.59	0.43	0.00	31.25	173.55	0.62	0.59	0.43	0.00
31.26	174.06	0.63	0.59	0.43	0.00	31.27	174.56	0.63	0.58	0.43	0.00
31.28	175.04	0.64	0.58	0.43	0.00	31.29	175.46	0.64	0.58	0.43	0.00
31.30	175.75	0.64	0.58	0.43	0.00	31.31	175.92	0.64	0.58	0.43	0.00
31.32	176.00	0.64	0.58	0.43	0.00	31.33	176.08	0.65	0.58	0.43	0.00
31.34	176.16	0.65	0.57	0.43	0.00	31.35	176.24	0.65	0.57	0.43	0.00
31.36	176.32	0.65	0.57	0.43	0.00	31.37	176.40	0.65	0.57	0.43	0.00
31.38	176.46	0.65	0.57	0.43	0.00	31.39	176.52	0.65	0.57	0.43	0.00
31.40	176.60	0.65	0.47	0.43	0.00	31.41	176.70	0.65	0.47	0.43	0.00
31.42	176.82	0.65	0.47	0.43	0.00	31.43	176.95	0.65	0.47	0.43	0.00
31.44	177.09	0.65	0.47	0.43	0.00	31.45	177.22	0.66	0.47	0.43	0.00
31.46	177.34	0.66	0.47	0.43	0.00	31.47	177.45	0.66	0.47	0.43	0.00
31.48	177.55	0.66	0.47	0.43	0.00	31.49	177.66	0.66	0.46	0.43	0.00
31.50	177.81	0.66	0.46	0.43	0.00	31.51	177.97	0.66	0.46	0.43	0.00
31.52	178.16	0.67	0.46	0.43	0.00	31.53	178.35	0.67	0.46	0.43	0.00
31.54	178.53	0.67	0.46	0.43	0.00	31.55	178.70	0.67	0.46	0.43	0.00
31.56	178.83	0.67	0.46	0.43	0.00	31.57	178.92	0.67	0.46	0.43	0.00
31.58	179.01	0.67	0.46	0.43	0.00	31.59	179.12	0.67	0.46	0.43	0.00
31.60	179.25	0.68	0.46	0.43	0.00	31.61	179.39	0.68	0.46	0.43	0.00
31.62	179.54	0.68	0.46	0.43	0.00	31.63	179.69	0.68	0.45	0.42	0.00
31.64	179.81	0.68	0.45	0.42	0.00	31.65	179.88	0.68	0.45	0.42	0.00
31.66	179.88	0.68	0.45	0.42	0.00	31.67	179.84	0.68	0.45	0.42	0.00
31.68	179.82	0.68	0.45	0.42	0.00	31.69	179.80	0.68	0.45	0.42	0.00
31.70	179.80	0.68	0.45	0.42	0.00	31.71	179.81	0.68	0.45	0.42	0.00
31.72	179.83	0.68	0.45	0.42	0.00	31.73	179.86	0.68	0.45	0.42	0.00
31.74	179.89	0.68	0.45	0.42	0.00	31.75	179.94	0.68	0.45	0.42	0.00
31.76	180.00	0.68	0.45	0.42	0.00	31.77	180.07	0.68	0.45	0.42	0.00
31.78	180.16	0.69	0.45	0.42	0.00	31.79	180.25	0.69	0.45	0.42	0.00
31.80	180.34	0.69	0.45	0.42	0.00	31.81	180.42	0.69	0.45	0.42	0.00
31.82	180.51	0.69	0.45	0.42	0.00	31.83	180.63	0.69	0.45	0.42	0.00
31.84	180.81	0.69	0.45	0.42	0.00	31.85	181.03	0.69	0.45	0.42	0.00
31.86	181.27	0.70	0.44	0.42	0.00	31.87	181.52	0.70	0.44	0.42	0.00
31.88	181.76	0.70	0.44	0.42	0.00	31.89	181.98	0.70	0.44	0.42	0.00
31.90	182.16	0.71	0.44	0.42	0.00	31.91	182.28	0.71	0.44	0.42	0.00
31.92	182.35	0.71	0.44	0.42	0.00	31.93	182.39	0.71	0.44	0.42	0.00
31.94	182.45	0.71	0.44	0.42	0.00	31.95	182.50	0.71	0.44	0.42	0.00
31.96	182.56	0.71	0.44	0.42	0.00	31.97	182.62	0.71	0.44	0.42	0.00
31.98	182.67	0.71	0.44	0.42	0.00	31.99	182.71	0.71	0.44	0.42	0.00
32.00	182.75	0.71	0.44	0.42	0.00	32.01	182.81	0.71	0.44	0.42	0.00
32.02	182.88	0.71	0.44	0.42	0.00	32.03	182.97	0.71	0.44	0.42	0.00
32.04	183.07	0.72	0.43	0.42	0.00	32.05	183.16	0.72	0.43	0.42	0.00
32.06	183.25	0.72	0.43	0.42	0.00	32.07	183.33	0.72	0.43	0.42	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
32.08	183.39	0.72	0.43	0.42	0.00	32.09	183.45	0.72	0.43	0.42	0.00
32.10	183.53	0.72	0.43	0.42	0.00	32.11	183.62	0.72	0.43	0.42	0.00
32.12	183.72	0.72	0.43	0.42	0.00	32.13	183.82	0.72	0.43	0.42	0.00
32.14	183.93	0.72	0.43	0.42	0.00	32.15	184.02	0.73	0.43	0.42	0.00
32.16	184.10	0.73	0.43	0.42	0.00	32.17	184.17	0.73	0.43	0.42	0.00
32.18	184.24	0.73	0.43	0.41	0.00	32.19	184.33	0.73	0.43	0.41	0.00
32.20	184.43	0.73	0.43	0.41	0.00	32.21	184.54	0.73	0.43	0.41	0.00
32.22	184.66	0.73	0.43	0.41	0.00	32.23	184.77	0.73	0.43	0.41	0.00
32.24	184.87	0.73	0.43	0.41	0.00	32.25	184.95	0.74	0.42	0.41	0.00
32.26	185.01	0.74	0.42	0.41	0.00	32.27	185.08	0.74	0.42	0.41	0.00
32.28	185.16	0.74	0.42	0.41	0.00	32.29	185.25	0.74	0.42	0.41	0.00
32.30	185.34	0.74	0.42	0.41	0.00	32.31	185.44	0.74	0.42	0.41	0.00
32.32	185.53	0.74	0.42	0.41	0.00	32.33	185.60	0.74	0.42	0.41	0.00
32.34	185.68	0.74	0.42	0.41	0.00	32.35	185.77	0.74	0.42	0.41	0.00
32.36	185.89	0.75	0.42	0.41	0.00	32.37	186.04	0.75	0.42	0.41	0.00
32.38	186.20	0.75	0.42	0.41	0.00	32.39	186.37	0.75	0.34	0.41	0.00
32.40	186.54	0.75	0.34	0.41	0.00	32.41	186.69	0.75	0.34	0.41	0.00
32.42	186.81	0.76	0.33	0.41	0.00	32.43	186.92	0.76	0.33	0.41	0.00
32.44	187.04	0.76	0.33	0.41	0.00	32.45	187.17	0.76	0.33	0.41	0.00
32.46	187.33	0.76	0.33	0.41	0.00	32.47	187.50	0.76	0.33	0.41	0.00
32.48	187.67	0.76	0.33	0.41	0.00	32.49	187.83	0.77	0.33	0.41	0.00
32.50	187.98	0.77	0.33	0.41	0.00	32.51	188.11	0.77	0.33	0.41	0.00
32.52	188.24	0.77	0.33	0.41	0.00	32.53	188.41	0.77	0.33	0.41	0.00
32.54	188.61	0.78	0.33	0.41	0.00	32.55	188.84	0.78	0.33	0.41	0.00
32.56	189.09	0.78	0.33	0.41	0.00	32.57	189.32	0.78	0.33	0.41	0.00
32.58	189.55	0.79	0.33	0.41	0.00	32.59	189.74	0.79	0.32	0.41	0.00
32.60	190.10	0.79	0.32	0.41	0.00	32.61	190.74	0.80	0.32	0.41	0.00
32.62	191.72	0.81	0.32	0.41	0.00	32.63	192.90	0.82	0.32	0.41	0.00
32.64	194.17	0.84	0.31	0.41	0.00	32.65	195.49	0.85	0.24	0.41	0.00
32.66	196.76	0.87	0.23	0.41	0.00	32.67	197.94	0.88	0.23	0.41	0.00
32.68	198.95	0.89	0.23	0.41	0.00	32.69	199.83	0.91	0.23	0.41	0.00
32.70	200.72	2.00	0.00	0.41	0.00	32.71	201.73	2.00	0.00	0.41	0.00
32.72	202.89	2.00	0.00	0.41	0.00	32.73	204.11	2.00	0.00	0.40	0.00
32.74	205.35	2.00	0.00	0.40	0.00	32.75	206.53	2.00	0.00	0.40	0.00
32.76	207.59	2.00	0.00	0.40	0.00	32.77	208.40	2.00	0.00	0.40	0.00
32.78	208.96	2.00	0.00	0.40	0.00	32.79	209.34	2.00	0.00	0.40	0.00
32.80	209.70	2.00	0.00	0.40	0.00	32.81	210.11	2.00	0.00	0.40	0.00
32.82	210.53	2.00	0.00	0.40	0.00	32.83	210.95	2.00	0.00	0.40	0.00
32.84	211.34	2.00	0.00	0.40	0.00	32.85	211.68	2.00	0.00	0.40	0.00
32.86	211.98	2.00	0.00	0.40	0.00	32.87	212.29	2.00	0.00	0.40	0.00
32.88	212.66	2.00	0.00	0.40	0.00	32.89	213.09	2.00	0.00	0.40	0.00
32.90	213.56	2.00	0.00	0.40	0.00	32.91	214.04	2.00	0.00	0.40	0.00
32.92	214.50	2.00	0.00	0.40	0.00	32.93	214.93	2.00	0.00	0.40	0.00
32.94	215.28	2.00	0.00	0.40	0.00	32.95	215.56	2.00	0.00	0.40	0.00
32.96	215.80	2.00	0.00	0.40	0.00	32.97	216.06	2.00	0.00	0.40	0.00
32.98	216.35	2.00	0.00	0.40	0.00	32.99	216.66	2.00	0.00	0.40	0.00
33.00	216.98	2.00	0.00	0.40	0.00	33.01	217.28	2.00	0.00	0.40	0.00
33.02	217.55	2.00	0.00	0.40	0.00	33.03	217.75	2.00	0.00	0.40	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
33.04	217.90	2.00	0.00	0.40	0.00	33.05	218.02	2.00	0.00	0.40	0.00
33.06	218.14	2.00	0.00	0.40	0.00	33.07	218.28	2.00	0.00	0.40	0.00
33.08	218.43	2.00	0.00	0.40	0.00	33.09	218.59	2.00	0.00	0.40	0.00
33.10	218.73	2.00	0.00	0.40	0.00	33.11	218.85	2.00	0.00	0.40	0.00
33.12	218.98	2.00	0.00	0.40	0.00	33.13	219.14	2.00	0.00	0.40	0.00
33.14	219.35	2.00	0.00	0.40	0.00	33.15	219.61	2.00	0.00	0.40	0.00
33.16	219.89	2.00	0.00	0.40	0.00	33.17	220.19	2.00	0.00	0.40	0.00
33.18	220.48	2.00	0.00	0.40	0.00	33.19	220.74	2.00	0.00	0.40	0.00
33.20	220.96	2.00	0.00	0.40	0.00	33.21	221.13	2.00	0.00	0.40	0.00
33.22	221.27	2.00	0.00	0.40	0.00	33.23	221.43	2.00	0.00	0.40	0.00
33.24	221.61	2.00	0.00	0.40	0.00	33.25	221.81	2.00	0.00	0.40	0.00
33.26	222.01	2.00	0.00	0.40	0.00	33.27	222.20	2.00	0.00	0.40	0.00
33.28	222.38	2.00	0.00	0.39	0.00	33.29	222.47	2.00	0.00	0.39	0.00
33.30	222.44	2.00	0.00	0.39	0.00	33.31	222.30	2.00	0.00	0.39	0.00
33.32	222.10	2.00	0.00	0.39	0.00	33.33	221.89	2.00	0.00	0.39	0.00
33.34	221.67	2.00	0.00	0.39	0.00	33.35	221.46	2.00	0.00	0.39	0.00
33.36	221.25	2.00	0.00	0.39	0.00	33.37	221.07	2.00	0.00	0.39	0.00
33.38	220.85	2.00	0.00	0.39	0.00	33.39	220.56	2.00	0.00	0.39	0.00
33.40	220.16	2.00	0.00	0.39	0.00	33.41	219.71	2.00	0.00	0.39	0.00
33.42	219.22	2.00	0.00	0.39	0.00	33.43	218.73	2.00	0.00	0.39	0.00
33.44	218.25	2.00	0.00	0.39	0.00	33.45	217.80	2.00	0.00	0.39	0.00
33.46	217.40	2.00	0.00	0.39	0.00	33.47	216.97	2.00	0.00	0.39	0.00
33.48	216.44	2.00	0.00	0.39	0.00	33.49	215.78	2.00	0.00	0.39	0.00
33.50	215.04	2.00	0.00	0.39	0.00	33.51	214.27	2.00	0.00	0.39	0.00
33.52	213.50	2.00	0.00	0.39	0.00	33.53	212.76	2.00	0.00	0.39	0.00
33.54	212.10	2.00	0.00	0.39	0.00	33.55	211.52	2.00	0.00	0.39	0.00
33.56	210.96	2.00	0.00	0.39	0.00	33.57	210.35	2.00	0.00	0.39	0.00
33.58	209.65	2.00	0.00	0.39	0.00	33.59	208.88	2.00	0.00	0.39	0.00
33.60	208.09	2.00	0.00	0.39	0.00	33.61	207.31	2.00	0.00	0.39	0.00
33.62	206.59	2.00	0.00	0.39	0.00	33.63	205.96	2.00	0.00	0.39	0.00
33.64	205.43	2.00	0.00	0.39	0.00	33.65	204.94	2.00	0.00	0.39	0.00
33.66	204.42	2.00	0.00	0.39	0.00	33.67	203.83	2.00	0.00	0.39	0.00
33.68	203.20	2.00	0.00	0.39	0.00	33.69	202.58	2.00	0.00	0.39	0.00
33.70	201.98	2.00	0.00	0.39	0.00	33.71	201.44	2.00	0.00	0.39	0.00
33.72	200.97	2.00	0.00	0.39	0.00	33.73	200.54	2.00	0.00	0.39	0.00
33.74	200.10	2.00	0.00	0.39	0.00	33.75	199.58	0.91	0.22	0.39	0.00
33.76	199.01	0.90	0.22	0.39	0.00	33.77	198.41	0.89	0.22	0.39	0.00
33.78	197.83	0.88	0.22	0.39	0.00	33.79	197.27	0.88	0.22	0.39	0.00
33.80	196.78	0.87	0.22	0.39	0.00	33.81	196.36	0.87	0.22	0.39	0.00
33.82	195.98	0.86	0.22	0.39	0.00	33.83	195.60	0.86	0.22	0.38	0.00
33.84	195.16	0.85	0.22	0.38	0.00	33.85	194.69	0.85	0.30	0.38	0.00
33.86	194.21	0.84	0.30	0.38	0.00	33.87	193.74	0.84	0.30	0.38	0.00
33.88	193.30	0.83	0.30	0.38	0.00	33.89	192.93	0.83	0.30	0.38	0.00
33.90	192.73	0.83	0.30	0.38	0.00	33.91	192.72	0.82	0.30	0.38	0.00
33.92	192.87	0.83	0.30	0.38	0.00	33.93	193.05	0.83	0.30	0.38	0.00
33.94	193.25	0.83	0.30	0.38	0.00	33.95	193.45	0.83	0.30	0.38	0.00
33.96	193.65	0.84	0.30	0.38	0.00	33.97	193.83	0.84	0.30	0.38	0.00
33.98	193.98	0.84	0.30	0.38	0.00	33.99	194.12	0.84	0.29	0.38	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
34.00	194.27	0.84	0.29	0.38	0.00	34.01	194.46	0.85	0.29	0.38	0.00
34.02	194.67	0.85	0.29	0.38	0.00	34.03	194.90	0.85	0.22	0.38	0.00
34.04	195.13	0.85	0.22	0.38	0.00	34.05	195.34	0.86	0.22	0.38	0.00
34.06	195.54	0.86	0.22	0.38	0.00	34.07	195.64	0.86	0.22	0.38	0.00
34.08	195.64	0.86	0.22	0.38	0.00	34.09	195.52	0.86	0.22	0.38	0.00
34.10	195.37	0.86	0.22	0.38	0.00	34.11	195.20	0.85	0.22	0.38	0.00
34.12	195.03	0.85	0.22	0.38	0.00	34.13	194.86	0.85	0.22	0.38	0.00
34.14	194.70	0.85	0.29	0.38	0.00	34.15	194.56	0.85	0.29	0.38	0.00
34.16	194.53	0.85	0.29	0.38	0.00	34.17	194.61	0.85	0.29	0.38	0.00
34.18	194.81	0.85	0.22	0.38	0.00	34.19	195.05	0.85	0.22	0.38	0.00
34.20	195.30	0.86	0.22	0.38	0.00	34.21	195.55	0.86	0.22	0.38	0.00
34.22	195.80	0.86	0.22	0.38	0.00	34.23	196.03	0.86	0.22	0.38	0.00
34.24	196.23	0.87	0.22	0.38	0.00	34.25	196.48	0.87	0.22	0.38	0.00
34.26	196.81	0.87	0.22	0.38	0.00	34.27	197.24	0.88	0.22	0.38	0.00
34.28	197.72	0.89	0.22	0.38	0.00	34.29	198.23	0.89	0.21	0.38	0.00
34.30	198.74	0.90	0.21	0.38	0.00	34.31	199.22	0.90	0.21	0.38	0.00
34.32	199.64	0.91	0.21	0.38	0.00	34.33	200.01	2.00	0.00	0.38	0.00
34.34	200.35	2.00	0.00	0.38	0.00	34.35	200.73	2.00	0.00	0.38	0.00
34.36	201.17	2.00	0.00	0.38	0.00	34.37	201.66	2.00	0.00	0.38	0.00
34.38	202.16	2.00	0.00	0.37	0.00	34.39	202.66	2.00	0.00	0.37	0.00
34.40	203.12	2.00	0.00	0.37	0.00	34.41	203.52	2.00	0.00	0.37	0.00
34.42	203.86	2.00	0.00	0.37	0.00	34.43	204.16	2.00	0.00	0.37	0.00
34.44	204.50	2.00	0.00	0.37	0.00	34.45	204.89	2.00	0.00	0.37	0.00
34.46	205.31	2.00	0.00	0.37	0.00	34.47	205.74	2.00	0.00	0.37	0.00
34.48	206.16	2.00	0.00	0.37	0.00	34.49	206.54	2.00	0.00	0.37	0.00
34.50	206.85	2.00	0.00	0.37	0.00	34.51	207.05	2.00	0.00	0.37	0.00
34.52	207.19	2.00	0.00	0.37	0.00	34.53	207.32	2.00	0.00	0.37	0.00
34.54	207.48	2.00	0.00	0.37	0.00	34.55	207.65	2.00	0.00	0.37	0.00
34.56	207.83	2.00	0.00	0.37	0.00	34.57	208.00	2.00	0.00	0.37	0.00
34.58	208.16	2.00	0.00	0.37	0.00	34.59	208.29	2.00	0.00	0.37	0.00
34.60	208.38	2.00	0.00	0.37	0.00	34.61	208.47	2.00	0.00	0.37	0.00
34.62	208.59	2.00	0.00	0.37	0.00	34.63	208.73	2.00	0.00	0.37	0.00
34.64	208.90	2.00	0.00	0.37	0.00	34.65	209.08	2.00	0.00	0.37	0.00
34.66	209.26	2.00	0.00	0.37	0.00	34.67	209.43	2.00	0.00	0.37	0.00
34.68	209.49	2.00	0.00	0.37	0.00	34.69	209.46	2.00	0.00	0.37	0.00
34.70	209.35	2.00	0.00	0.37	0.00	34.71	209.25	2.00	0.00	0.37	0.00
34.72	209.16	2.00	0.00	0.37	0.00	34.73	209.10	2.00	0.00	0.37	0.00
34.74	209.06	2.00	0.00	0.37	0.00	34.75	209.05	2.00	0.00	0.37	0.00
34.76	209.03	2.00	0.00	0.37	0.00	34.77	208.97	2.00	0.00	0.37	0.00
34.78	208.86	2.00	0.00	0.37	0.00	34.79	208.71	2.00	0.00	0.37	0.00
34.80	208.58	2.00	0.00	0.37	0.00	34.81	208.46	2.00	0.00	0.37	0.00
34.82	208.35	2.00	0.00	0.37	0.00	34.83	208.27	2.00	0.00	0.37	0.00
34.84	208.21	2.00	0.00	0.37	0.00	34.85	208.14	2.00	0.00	0.37	0.00
34.86	208.07	2.00	0.00	0.37	0.00	34.87	207.96	2.00	0.00	0.37	0.00
34.88	207.85	2.00	0.00	0.37	0.00	34.89	207.74	2.00	0.00	0.37	0.00
34.90	207.63	2.00	0.00	0.37	0.00	34.91	207.53	2.00	0.00	0.37	0.00
34.92	207.45	2.00	0.00	0.37	0.00	34.93	207.36	2.00	0.00	0.36	0.00
34.94	207.14	2.00	0.00	0.36	0.00	34.95	206.72	2.00	0.00	0.36	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
34.96	206.09	2.00	0.00	0.36	0.00	34.97	205.38	2.00	0.00	0.36	0.00
34.98	204.62	2.00	0.00	0.36	0.00	34.99	203.86	2.00	0.00	0.36	0.00
35.00	203.13	2.00	0.00	0.36	0.00	35.01	202.47	2.00	0.00	0.36	0.00
35.02	201.86	2.00	0.00	0.36	0.00	35.03	201.19	2.00	0.00	0.36	0.00
35.04	200.37	2.00	0.00	0.36	0.00	35.05	199.36	0.91	0.20	0.36	0.00
35.06	198.24	0.89	0.21	0.36	0.00	35.07	197.06	0.88	0.21	0.36	0.00
35.08	195.89	0.87	0.21	0.36	0.00	35.09	194.79	0.85	0.21	0.36	0.00
35.10	193.81	0.84	0.28	0.36	0.00	35.11	192.91	0.83	0.28	0.36	0.00
35.12	191.97	0.82	0.28	0.36	0.00	35.13	190.86	0.81	0.29	0.36	0.00
35.14	189.56	0.79	0.29	0.36	0.00	35.15	188.15	0.78	0.29	0.36	0.00
35.16	186.69	0.76	0.29	0.36	0.00	35.17	185.27	0.75	0.37	0.36	0.00
35.18	183.96	0.73	0.37	0.36	0.00	35.19	182.81	0.72	0.38	0.36	0.00
35.20	181.70	0.71	0.38	0.36	0.00	35.21	180.49	0.70	0.38	0.36	0.00
35.22	179.03	0.68	0.39	0.36	0.00	35.23	177.38	0.67	0.39	0.36	0.00
35.24	175.62	0.65	0.48	0.36	0.00	35.25	173.85	0.63	0.49	0.36	0.00
35.26	172.15	0.62	0.50	0.36	0.00	35.27	170.62	0.60	0.50	0.36	0.00
35.28	169.31	0.59	0.51	0.36	0.00	35.29	168.10	0.58	0.51	0.36	0.00
35.30	166.82	0.57	0.52	0.36	0.00	35.31	165.34	0.56	0.52	0.36	0.00
35.32	163.70	0.54	0.56	0.36	0.00	35.33	162.00	0.53	0.56	0.36	0.00
35.34	160.33	0.52	0.57	0.36	0.00	35.35	158.76	0.50	0.57	0.36	0.00
35.36	157.37	0.49	0.58	0.36	0.00	35.37	156.18	0.48	0.58	0.36	0.00
35.38	155.03	0.47	0.58	0.36	0.00	35.39	153.76	0.47	0.59	0.36	0.00
35.40	152.30	0.45	0.59	0.36	0.00	35.41	150.72	0.44	0.59	0.36	0.00
35.42	149.11	0.43	0.60	0.36	0.00	35.43	147.54	0.42	0.60	0.36	0.00
35.44	146.09	0.41	0.61	0.36	0.00	35.45	144.84	0.40	0.61	0.36	0.00
35.46	143.83	0.40	0.62	0.36	0.00	35.47	142.91	0.39	0.62	0.36	0.00
35.48	141.95	0.39	0.62	0.35	0.00	35.49	140.86	0.38	0.63	0.35	0.00
35.50	139.70	0.37	0.63	0.35	0.00	35.51	138.54	0.36	0.63	0.35	0.00
35.52	137.42	0.36	0.64	0.35	0.00	35.53	136.41	0.35	0.64	0.35	0.00
35.54	135.61	0.35	0.64	0.35	0.00	35.55	135.04	0.34	0.65	0.35	0.00
35.56	134.62	0.34	0.65	0.35	0.00	35.57	134.22	0.34	0.65	0.35	0.00
35.58	133.78	0.34	0.65	0.35	0.00	35.59	133.32	0.33	0.65	0.35	0.00
35.60	132.87	0.33	0.65	0.35	0.00	35.61	132.45	0.33	0.65	0.35	0.00
35.62	132.08	0.33	0.66	0.35	0.00	35.63	131.81	0.33	0.66	0.35	0.00
35.64	131.66	0.33	0.66	0.35	0.00	35.65	131.58	0.33	0.66	0.35	0.00
35.66	131.51	0.33	0.66	0.35	0.00	35.67	131.45	0.32	0.66	0.35	0.00
35.68	131.39	0.32	0.66	0.35	0.00	35.69	131.33	0.32	0.66	0.35	0.00
35.70	131.28	0.32	0.66	0.35	0.00	35.71	131.24	0.32	0.66	0.35	0.00
35.72	131.25	0.32	0.66	0.35	0.00	35.73	131.31	0.32	0.65	0.35	0.00
35.74	131.43	0.32	0.65	0.35	0.00	35.75	131.56	0.33	0.65	0.35	0.00
35.76	131.71	0.33	0.65	0.35	0.00	35.77	131.85	0.33	0.65	0.35	0.00
35.78	132.00	0.33	0.65	0.35	0.00	35.79	132.13	0.33	0.65	0.35	0.00
35.80	132.24	0.33	0.65	0.35	0.00	35.81	132.34	0.33	0.65	0.35	0.00
35.82	132.44	0.33	0.65	0.35	0.00	35.83	132.55	0.33	0.65	0.35	0.00
35.84	132.67	0.33	0.65	0.35	0.00	35.85	132.81	0.33	0.64	0.35	0.00
35.86	132.94	0.33	0.64	0.35	0.00	35.87	133.06	0.33	0.64	0.35	0.00
35.88	133.17	0.33	0.64	0.35	0.00	35.89	133.24	0.33	0.64	0.35	0.00
35.90	133.29	0.34	0.64	0.35	0.00	35.91	133.33	0.34	0.64	0.35	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
35.92	133.37	0.34	0.64	0.35	0.00	35.93	133.41	0.34	0.64	0.35	0.00
35.94	133.46	0.34	0.64	0.35	0.00	35.95	133.51	0.34	0.64	0.35	0.00
35.96	133.55	0.34	0.64	0.35	0.00	35.97	133.59	0.34	0.64	0.35	0.00
35.98	133.58	0.34	0.64	0.35	0.00	35.99	133.52	0.34	0.64	0.35	0.00
36.00	133.42	0.34	0.64	0.35	0.00	36.01	133.31	0.34	0.64	0.35	0.00
36.02	133.21	0.33	0.64	0.35	0.00	36.03	133.10	0.33	0.64	0.34	0.00
36.04	133.00	0.33	0.64	0.34	0.00	36.05	132.91	0.33	0.64	0.34	0.00
36.06	132.81	0.33	0.64	0.34	0.00	36.07	132.66	0.33	0.64	0.34	0.00
36.08	132.44	0.33	0.64	0.34	0.00	36.09	132.17	0.33	0.64	0.34	0.00
36.10	131.87	0.33	0.64	0.34	0.00	36.11	131.57	0.33	0.64	0.34	0.00
36.12	131.27	0.32	0.64	0.34	0.00	36.13	131.00	0.32	0.64	0.34	0.00
36.14	130.76	0.32	0.64	0.34	0.00	36.15	130.58	0.32	0.64	0.34	0.00
36.16	130.46	0.32	0.64	0.34	0.00	36.17	130.37	0.32	0.64	0.34	0.00
36.18	130.28	0.32	0.64	0.34	0.00	36.19	130.18	0.32	0.64	0.34	0.00
36.20	130.07	0.32	0.64	0.34	0.00	36.21	129.97	0.32	0.64	0.34	0.00
36.22	129.88	0.32	0.64	0.34	0.00	36.23	129.81	0.32	0.64	0.34	0.00
36.24	129.84	0.32	0.64	0.34	0.00	36.25	129.97	0.32	0.64	0.34	0.00
36.26	130.20	0.32	0.64	0.34	0.00	36.27	130.46	0.32	0.64	0.34	0.00
36.28	130.75	0.32	0.64	0.34	0.00	36.29	131.03	0.32	0.64	0.34	0.00
36.30	131.31	0.32	0.64	0.34	0.00	36.31	131.56	0.33	0.63	0.34	0.00
36.32	131.79	0.33	0.63	0.34	0.00	36.33	132.08	0.33	0.63	0.34	0.00
36.34	132.46	0.33	0.63	0.34	0.00	36.35	132.94	0.33	0.63	0.34	0.00
36.36	133.48	0.34	0.62	0.34	0.00	36.37	134.04	0.34	0.62	0.34	0.00
36.38	134.61	0.34	0.62	0.34	0.00	36.39	135.16	0.35	0.62	0.34	0.00
36.40	135.64	0.35	0.62	0.34	0.00	36.41	136.05	0.35	0.61	0.34	0.00
36.42	136.45	0.35	0.61	0.34	0.00	36.43	136.89	0.36	0.61	0.34	0.00
36.44	137.41	0.36	0.61	0.34	0.00	36.45	137.99	0.36	0.61	0.34	0.00
36.46	138.59	0.37	0.60	0.34	0.00	36.47	139.18	0.37	0.60	0.34	0.00
36.48	139.74	0.37	0.60	0.34	0.00	36.49	140.20	0.38	0.60	0.34	0.00
36.50	140.56	0.38	0.59	0.34	0.00	36.51	140.86	0.38	0.59	0.34	0.00
36.52	141.16	0.38	0.59	0.34	0.00	36.53	141.50	0.38	0.59	0.34	0.00
36.54	141.87	0.39	0.59	0.34	0.00	36.55	142.25	0.39	0.59	0.34	0.00
36.56	142.61	0.39	0.59	0.34	0.00	36.57	142.93	0.39	0.58	0.34	0.00
36.58	143.19	0.40	0.58	0.33	0.00	36.59	143.39	0.40	0.58	0.33	0.00
36.60	143.56	0.40	0.58	0.33	0.00	36.61	143.75	0.40	0.58	0.33	0.00
36.62	143.96	0.40	0.58	0.33	0.00	36.63	144.17	0.40	0.58	0.33	0.00
36.64	144.39	0.40	0.58	0.33	0.00	36.65	144.59	0.40	0.58	0.33	0.00
36.66	144.77	0.41	0.58	0.33	0.00	36.67	144.89	0.41	0.57	0.33	0.00
36.68	144.98	0.41	0.57	0.33	0.00	36.69	145.04	0.41	0.57	0.33	0.00
36.70	145.12	0.41	0.57	0.33	0.00	36.71	145.20	0.41	0.57	0.33	0.00
36.72	145.28	0.41	0.57	0.33	0.00	36.73	145.36	0.41	0.57	0.33	0.00
36.74	145.43	0.41	0.57	0.33	0.00	36.75	145.49	0.41	0.57	0.33	0.00
36.76	145.56	0.41	0.57	0.33	0.00	36.77	145.64	0.41	0.57	0.33	0.00
36.78	145.74	0.41	0.57	0.33	0.00	36.79	145.86	0.41	0.57	0.33	0.00
36.80	145.98	0.41	0.57	0.33	0.00	36.81	146.11	0.41	0.57	0.33	0.00
36.82	146.23	0.42	0.57	0.33	0.00	36.83	146.33	0.42	0.56	0.33	0.00
36.84	146.44	0.42	0.56	0.33	0.00	36.85	146.57	0.42	0.56	0.33	0.00
36.86	146.76	0.42	0.56	0.33	0.00	36.87	146.99	0.42	0.56	0.33	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
36.88	147.26	0.42	0.56	0.33	0.00	36.89	147.53	0.42	0.56	0.33	0.00
36.90	147.80	0.43	0.56	0.33	0.00	36.91	148.05	0.43	0.56	0.33	0.00
36.92	148.28	0.43	0.56	0.33	0.00	36.93	148.41	0.43	0.56	0.33	0.00
36.94	148.46	0.43	0.55	0.33	0.00	36.95	148.44	0.43	0.55	0.33	0.00
36.96	148.41	0.43	0.55	0.33	0.00	36.97	148.38	0.43	0.55	0.33	0.00
36.98	148.35	0.43	0.55	0.33	0.00	36.99	148.33	0.43	0.55	0.33	0.00
37.00	148.30	0.43	0.55	0.33	0.00	37.01	148.27	0.43	0.55	0.33	0.00
37.02	148.16	0.43	0.55	0.33	0.00	37.03	147.97	0.43	0.55	0.33	0.00
37.04	147.70	0.43	0.55	0.33	0.00	37.05	147.40	0.42	0.55	0.33	0.00
37.06	147.08	0.42	0.56	0.33	0.00	37.07	146.76	0.42	0.56	0.33	0.00
37.08	146.45	0.42	0.56	0.33	0.00	37.09	146.18	0.42	0.56	0.33	0.00
37.10	145.91	0.41	0.56	0.33	0.00	37.11	145.59	0.41	0.56	0.33	0.00
37.12	145.19	0.41	0.56	0.33	0.00	37.13	144.70	0.41	0.56	0.32	0.00
37.14	144.16	0.40	0.56	0.32	0.00	37.15	143.60	0.40	0.56	0.32	0.00
37.16	143.05	0.40	0.57	0.32	0.00	37.17	142.54	0.39	0.57	0.32	0.00
37.18	142.09	0.39	0.57	0.32	0.00	37.19	141.81	0.39	0.57	0.32	0.00
37.20	141.68	0.39	0.57	0.32	0.00	37.21	141.67	0.39	0.57	0.32	0.00
37.22	141.68	0.39	0.57	0.32	0.00	37.23	141.68	0.39	0.57	0.32	0.00
37.24	141.69	0.39	0.57	0.32	0.00	37.25	141.69	0.39	0.57	0.32	0.00
37.26	141.70	0.39	0.57	0.32	0.00	37.27	141.67	0.39	0.57	0.32	0.00
37.28	141.50	0.39	0.57	0.32	0.00	37.29	141.16	0.38	0.57	0.32	0.00
37.30	140.66	0.38	0.57	0.32	0.00	37.31	140.10	0.38	0.57	0.32	0.00
37.32	139.52	0.37	0.57	0.32	0.00	37.33	138.94	0.37	0.57	0.32	0.00
37.34	138.39	0.37	0.57	0.32	0.00	37.35	137.90	0.36	0.58	0.32	0.00
37.36	137.43	0.36	0.58	0.32	0.00	37.37	136.90	0.36	0.58	0.32	0.00
37.38	136.23	0.35	0.58	0.32	0.00	37.39	135.42	0.35	0.58	0.32	0.00
37.40	134.54	0.34	0.59	0.32	0.00	37.41	133.64	0.34	0.59	0.32	0.00
37.42	132.76	0.33	0.59	0.32	0.00	37.43	131.94	0.33	0.59	0.32	0.00
37.44	131.23	0.33	0.60	0.32	0.00	37.45	130.97	0.32	0.60	0.32	0.00
37.46	131.19	0.33	0.60	0.32	0.00	37.47	131.87	0.33	0.59	0.32	0.00
37.48	132.69	0.33	0.59	0.32	0.00	37.49	133.58	0.34	0.59	0.32	0.00
37.50	134.50	0.34	0.58	0.32	0.00	37.51	135.40	0.35	0.58	0.32	0.00
37.52	136.23	0.35	0.58	0.32	0.00	37.53	136.92	0.36	0.57	0.32	0.00
37.54	137.46	0.36	0.57	0.32	0.00	37.55	137.91	0.36	0.57	0.32	0.00
37.56	138.37	0.37	0.57	0.32	0.00	37.57	138.90	0.37	0.57	0.32	0.00
37.58	139.46	0.37	0.56	0.32	0.00	37.59	140.02	0.38	0.56	0.32	0.00
37.60	140.55	0.38	0.56	0.32	0.00	37.61	141.04	0.38	0.56	0.32	0.00
37.62	141.45	0.39	0.56	0.32	0.00	37.63	141.84	0.39	0.55	0.32	0.00
37.64	142.28	0.39	0.55	0.32	0.00	37.65	142.79	0.39	0.55	0.32	0.00
37.66	143.35	0.40	0.55	0.32	0.00	37.67	143.94	0.40	0.55	0.32	0.00
37.68	144.52	0.41	0.54	0.31	0.00	37.69	145.06	0.41	0.54	0.31	0.00
37.70	145.54	0.41	0.54	0.31	0.00	37.71	146.12	2.00	0.00	0.31	0.00
37.72	146.93	2.00	0.00	0.31	0.00	37.73	148.05	2.00	0.00	0.31	0.00
37.74	149.35	2.00	0.00	0.31	0.00	37.75	150.76	2.00	0.00	0.31	0.00
37.76	152.19	2.00	0.00	0.31	0.00	37.77	153.59	2.00	0.00	0.31	0.00
37.78	154.87	2.00	0.00	0.31	0.00	37.79	155.97	2.00	0.00	0.31	0.00
37.80	156.97	2.00	0.00	0.31	0.00	37.81	158.01	2.00	0.00	0.31	0.00
37.82	159.22	2.00	0.00	0.31	0.00	37.83	160.59	2.00	0.00	0.31	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
37.84	162.03	2.00	0.00	0.31	0.00	37.85	163.48	2.00	0.00	0.31	0.00
37.86	164.85	2.00	0.00	0.31	0.00	37.87	166.08	2.00	0.00	0.31	0.00
37.88	167.19	2.00	0.00	0.31	0.00	37.89	168.35	2.00	0.00	0.31	0.00
37.90	169.72	2.00	0.00	0.31	0.00	37.91	171.36	2.00	0.00	0.31	0.00
37.92	173.15	2.00	0.00	0.31	0.00	37.93	175.01	2.00	0.00	0.31	0.00
37.94	176.83	2.00	0.00	0.31	0.00	37.95	178.52	2.00	0.00	0.31	0.00
37.96	179.99	2.00	0.00	0.31	0.00	37.97	181.19	2.00	0.00	0.31	0.00
37.98	182.28	2.00	0.00	0.31	0.00	37.99	183.41	2.00	0.00	0.31	0.00
38.00	184.70	2.00	0.00	0.31	0.00	38.01	186.09	2.00	0.00	0.31	0.00
38.02	187.49	2.00	0.00	0.31	0.00	38.03	188.84	2.00	0.00	0.31	0.00
38.04	190.06	2.00	0.00	0.31	0.00	38.05	191.05	2.00	0.00	0.31	0.00
38.06	191.76	2.00	0.00	0.31	0.00	38.07	192.30	0.84	0.24	0.31	0.00
38.08	192.80	0.84	0.24	0.31	0.00	38.09	193.37	0.85	0.24	0.31	0.00
38.10	193.96	0.86	0.18	0.31	0.00	38.11	194.55	0.86	0.18	0.31	0.00
38.12	195.10	0.87	0.18	0.31	0.00	38.13	195.59	0.88	0.18	0.31	0.00
38.14	184.63	0.75	0.25	0.31	0.00	38.15	196.03	2.00	0.00	0.31	0.00
38.16	195.97	2.00	0.00	0.31	0.00	38.17	195.84	2.00	0.00	0.31	0.00
38.18	195.70	2.00	0.00	0.31	0.00	38.19	195.55	2.00	0.00	0.31	0.00
38.20	195.39	2.00	0.00	0.31	0.00	38.21	195.24	2.00	0.00	0.31	0.00
38.22	195.09	2.00	0.00	0.31	0.00	38.23	194.78	2.00	0.00	0.30	0.00
38.24	194.22	2.00	0.00	0.30	0.00	38.25	193.37	2.00	0.00	0.30	0.00
38.26	192.37	2.00	0.00	0.30	0.00	38.27	191.26	2.00	0.00	0.30	0.00
38.28	190.12	2.00	0.00	0.30	0.00	38.29	188.99	2.00	0.00	0.30	0.00
38.30	187.95	2.00	0.00	0.30	0.00	38.31	187.06	2.00	0.00	0.30	0.00
38.32	186.22	2.00	0.00	0.30	0.00	38.33	185.34	2.00	0.00	0.30	0.00
38.34	184.32	2.00	0.00	0.30	0.00	38.35	183.19	2.00	0.00	0.30	0.00
38.36	182.02	2.00	0.00	0.30	0.00	38.37	180.87	2.00	0.00	0.30	0.00
38.38	179.81	2.00	0.00	0.30	0.00	38.39	178.89	2.00	0.00	0.30	0.00
38.40	178.43	2.00	0.00	0.30	0.00	38.41	178.53	2.00	0.00	0.30	0.00
38.42	179.19	2.00	0.00	0.30	0.00	38.43	180.10	2.00	0.00	0.30	0.00
38.44	181.09	2.00	0.00	0.30	0.00	38.45	182.13	2.00	0.00	0.30	0.00
38.46	183.14	2.00	0.00	0.30	0.00	38.47	184.09	2.00	0.00	0.30	0.00
38.48	184.93	0.76	0.25	0.30	0.00	38.49	185.92	0.77	0.25	0.30	0.00
38.50	187.22	0.78	0.24	0.30	0.00	38.51	189.00	0.80	0.24	0.30	0.00
38.52	191.06	0.83	0.24	0.30	0.00	38.53	193.28	0.85	0.18	0.30	0.00
38.54	195.55	0.88	0.17	0.30	0.00	38.55	197.76	0.91	0.17	0.30	0.00
38.56	199.79	0.93	0.17	0.30	0.00	38.57	201.49	2.00	0.00	0.30	0.00
38.58	202.97	2.00	0.00	0.30	0.00	38.59	204.41	2.00	0.00	0.30	0.00
38.60	206.05	2.00	0.00	0.30	0.00	38.61	207.89	2.00	0.00	0.30	0.00
38.62	209.85	2.00	0.00	0.30	0.00	38.63	211.80	2.00	0.00	0.30	0.00
38.64	213.67	2.00	0.00	0.30	0.00	38.65	215.32	2.00	0.00	0.30	0.00
38.66	216.77	2.00	0.00	0.30	0.00	38.67	218.20	2.00	0.00	0.30	0.00
38.68	219.82	2.00	0.00	0.30	0.00	38.69	221.71	2.00	0.00	0.30	0.00
38.70	223.77	2.00	0.00	0.30	0.00	38.71	225.89	2.00	0.00	0.30	0.00
38.72	227.96	2.00	0.00	0.30	0.00	38.73	229.87	2.00	0.00	0.30	0.00
38.74	231.50	2.00	0.00	0.30	0.00	38.75	232.64	2.00	0.00	0.30	0.00
38.76	233.43	2.00	0.00	0.30	0.00	38.77	234.03	2.00	0.00	0.30	0.00
38.78	234.71	2.00	0.00	0.29	0.00	38.79	235.43	2.00	0.00	0.29	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
38.80	236.16	2.00	0.00	0.29	0.00	38.81	236.85	2.00	0.00	0.29	0.00
38.82	237.47	2.00	0.00	0.29	0.00	38.83	237.85	2.00	0.00	0.29	0.00
38.84	237.76	2.00	0.00	0.29	0.00	38.85	237.19	2.00	0.00	0.29	0.00
38.86	236.27	2.00	0.00	0.29	0.00	38.87	235.25	2.00	0.00	0.29	0.00
38.88	234.17	2.00	0.00	0.29	0.00	38.89	233.10	2.00	0.00	0.29	0.00
38.90	232.08	2.00	0.00	0.29	0.00	38.91	231.18	2.00	0.00	0.29	0.00
38.92	230.20	2.00	0.00	0.29	0.00	38.93	228.95	2.00	0.00	0.29	0.00
38.94	227.25	2.00	0.00	0.29	0.00	38.95	225.21	2.00	0.00	0.29	0.00
38.96	222.97	2.00	0.00	0.29	0.00	38.97	220.65	2.00	0.00	0.29	0.00
38.98	218.38	2.00	0.00	0.29	0.00	38.99	216.27	2.00	0.00	0.29	0.00
39.00	214.43	2.00	0.00	0.29	0.00	39.01	212.76	2.00	0.00	0.29	0.00
39.02	211.04	2.00	0.00	0.29	0.00	39.03	209.04	2.00	0.00	0.29	0.00
39.04	206.78	2.00	0.00	0.29	0.00	39.05	204.38	2.00	0.00	0.29	0.00
39.06	201.98	2.00	0.00	0.29	0.00	39.07	199.70	0.93	0.16	0.29	0.00
39.08	197.67	0.91	0.17	0.29	0.00	39.09	196.07	0.89	0.17	0.29	0.00
39.10	194.96	0.87	0.17	0.29	0.00	39.11	194.17	0.87	0.17	0.29	0.00
39.12	193.45	0.86	0.17	0.29	0.00	39.13	192.67	0.85	0.23	0.29	0.00
39.14	191.87	0.84	0.23	0.29	0.00	39.15	191.11	0.83	0.23	0.29	0.00
39.16	190.41	0.82	0.23	0.29	0.00	39.17	189.82	0.81	0.23	0.29	0.00
39.18	189.53	0.81	0.23	0.29	0.00	39.19	189.63	0.81	0.23	0.29	0.00
39.20	190.08	0.82	0.23	0.29	0.00	39.21	190.69	0.83	0.23	0.29	0.00
39.22	191.35	0.83	0.23	0.29	0.00	39.23	192.04	0.84	0.22	0.29	0.00
39.24	192.71	0.85	0.22	0.29	0.00	39.25	193.33	0.86	0.17	0.29	0.00
39.26	193.87	0.86	0.17	0.29	0.00	39.27	194.40	0.87	0.17	0.29	0.00
39.28	195.00	0.88	0.17	0.29	0.00	39.29	195.73	0.89	0.17	0.29	0.00
39.30	196.56	0.90	0.16	0.29	0.00	39.31	197.46	0.91	0.16	0.29	0.00
39.32	198.36	0.92	0.16	0.29	0.00	39.33	199.23	0.93	0.16	0.28	0.00
39.34	200.01	2.00	0.00	0.28	0.00	39.35	200.63	2.00	0.00	0.28	0.00
39.36	201.06	2.00	0.00	0.28	0.00	39.37	201.36	2.00	0.00	0.28	0.00
39.38	201.65	2.00	0.00	0.28	0.00	39.39	201.97	2.00	0.00	0.28	0.00
39.40	202.30	2.00	0.00	0.28	0.00	39.41	202.64	2.00	0.00	0.28	0.00
39.42	202.96	2.00	0.00	0.28	0.00	39.43	203.23	2.00	0.00	0.28	0.00
39.44	203.50	2.00	0.00	0.28	0.00	39.45	203.82	2.00	0.00	0.28	0.00
39.46	204.22	2.00	0.00	0.28	0.00	39.47	204.71	2.00	0.00	0.28	0.00
39.48	205.24	2.00	0.00	0.28	0.00	39.49	205.79	2.00	0.00	0.28	0.00
39.50	206.32	2.00	0.00	0.28	0.00	39.51	206.81	2.00	0.00	0.28	0.00
39.52	207.23	2.00	0.00	0.28	0.00	39.53	207.59	2.00	0.00	0.28	0.00
39.54	207.95	2.00	0.00	0.28	0.00	39.55	208.35	2.00	0.00	0.28	0.00
39.56	208.82	2.00	0.00	0.28	0.00	39.57	209.32	2.00	0.00	0.28	0.00
39.58	209.82	2.00	0.00	0.28	0.00	39.59	210.30	2.00	0.00	0.28	0.00
39.60	210.74	2.00	0.00	0.28	0.00	39.61	210.99	2.00	0.00	0.28	0.00
39.62	210.91	2.00	0.00	0.28	0.00	39.63	210.48	2.00	0.00	0.28	0.00
39.64	209.83	2.00	0.00	0.28	0.00	39.65	209.12	2.00	0.00	0.28	0.00
39.66	208.38	2.00	0.00	0.28	0.00	39.67	207.66	2.00	0.00	0.28	0.00
39.68	206.99	2.00	0.00	0.28	0.00	39.69	206.39	2.00	0.00	0.28	0.00
39.70	205.89	2.00	0.00	0.28	0.00	39.71	205.41	2.00	0.00	0.28	0.00
39.72	204.91	2.00	0.00	0.28	0.00	39.73	204.34	2.00	0.00	0.28	0.00
39.74	203.73	2.00	0.00	0.28	0.00	39.75	203.10	2.00	0.00	0.28	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
39.76	202.50	2.00	0.00	0.28	0.00	39.77	201.95	2.00	0.00	0.28	0.00
39.78	201.49	2.00	0.00	0.28	0.00	39.79	201.17	2.00	0.00	0.28	0.00
39.80	200.96	2.00	0.00	0.28	0.00	39.81	200.81	2.00	0.00	0.28	0.00
39.82	200.64	2.00	0.00	0.28	0.00	39.83	200.46	2.00	0.00	0.28	0.00
39.84	200.28	2.00	0.00	0.28	0.00	39.85	200.11	2.00	0.00	0.28	0.00
39.86	199.96	0.94	0.15	0.28	0.00	39.87	199.85	0.94	0.15	0.28	0.00
39.88	199.80	0.94	0.15	0.27	0.00	39.89	199.83	0.94	0.15	0.27	0.00
39.90	199.90	0.94	0.15	0.27	0.00	39.91	199.99	0.94	0.15	0.27	0.00
39.92	200.10	2.00	0.00	0.27	0.00	39.93	200.22	2.00	0.00	0.27	0.00
39.94	200.34	2.00	0.00	0.27	0.00	39.95	200.46	2.00	0.00	0.27	0.00
39.96	200.67	2.00	0.00	0.27	0.00	39.97	201.04	2.00	0.00	0.27	0.00
39.98	201.62	2.00	0.00	0.27	0.00	39.99	202.31	2.00	0.00	0.27	0.00
40.00	203.08	2.00	0.00	0.27	0.00	40.01	203.87	2.00	0.00	0.27	0.00
40.02	204.66	2.00	0.00	0.27	0.00	40.03	205.38	2.00	0.00	0.27	0.00
40.04	205.98	2.00	0.00	0.27	0.00	40.05	206.34	2.00	0.00	0.27	0.00
40.06	206.51	2.00	0.00	0.27	0.00	40.07	206.55	2.00	0.00	0.27	0.00
40.08	206.62	2.00	0.00	0.27	0.00	40.09	206.69	2.00	0.00	0.27	0.00
40.10	206.77	2.00	0.00	0.27	0.00	40.11	206.86	2.00	0.00	0.27	0.00
40.12	206.94	2.00	0.00	0.27	0.00	40.13	206.96	2.00	0.00	0.27	0.00
40.14	206.86	2.00	0.00	0.27	0.00	40.15	206.62	2.00	0.00	0.27	0.00
40.16	206.31	2.00	0.00	0.27	0.00	40.17	205.98	2.00	0.00	0.27	0.00
40.18	205.64	2.00	0.00	0.27	0.00	40.19	205.33	2.00	0.00	0.27	0.00
40.20	205.04	2.00	0.00	0.27	0.00	40.21	204.80	2.00	0.00	0.27	0.00
40.22	204.58	2.00	0.00	0.27	0.00	40.23	204.37	2.00	0.00	0.27	0.00
40.24	204.12	2.00	0.00	0.27	0.00	40.25	203.84	2.00	0.00	0.27	0.00
40.26	203.55	2.00	0.00	0.27	0.00	40.27	203.24	2.00	0.00	0.27	0.00
40.28	202.95	2.00	0.00	0.27	0.00	40.29	202.67	2.00	0.00	0.27	0.00
40.30	202.43	2.00	0.00	0.27	0.00	40.31	202.18	2.00	0.00	0.27	0.00
40.32	201.89	2.00	0.00	0.27	0.00	40.33	201.53	2.00	0.00	0.27	0.00
40.34	201.13	2.00	0.00	0.27	0.00	40.35	200.71	2.00	0.00	0.27	0.00
40.36	200.29	2.00	0.00	0.27	0.00	40.37	199.89	0.95	0.15	0.27	0.00
40.38	199.52	0.94	0.15	0.27	0.00	40.39	199.19	0.94	0.15	0.27	0.00
40.40	198.85	0.93	0.15	0.27	0.00	40.41	198.45	0.93	0.15	0.27	0.00
40.42	197.97	0.92	0.15	0.27	0.00	40.43	197.45	0.92	0.15	0.26	0.00
40.44	196.91	0.91	0.15	0.26	0.00	40.45	196.37	0.90	0.15	0.26	0.00
40.46	195.87	0.90	0.15	0.26	0.00	40.47	195.43	0.89	0.15	0.26	0.00
40.48	195.06	0.89	0.15	0.26	0.00	40.49	194.72	0.88	0.15	0.26	0.00
40.50	194.38	0.88	0.15	0.26	0.00	40.51	193.99	0.87	0.15	0.26	0.00
40.52	193.58	0.87	0.16	0.26	0.00	40.53	193.15	0.86	0.16	0.26	0.00
40.54	192.74	0.86	0.16	0.26	0.00	40.55	192.35	0.85	0.16	0.26	0.00
40.56	192.01	0.85	0.21	0.26	0.00	40.57	191.65	0.85	0.21	0.26	0.00
40.58	191.21	0.84	0.21	0.26	0.00	40.59	190.67	0.83	0.21	0.26	0.00
40.60	190.07	0.83	0.21	0.26	0.00	40.61	189.43	0.82	0.21	0.26	0.00
40.62	188.79	0.81	0.21	0.26	0.00	40.63	188.18	0.81	0.21	0.26	0.00
40.64	187.63	0.80	0.21	0.26	0.00	40.65	187.14	0.79	0.21	0.26	0.00
40.66	186.63	0.79	0.21	0.26	0.00	40.67	186.02	0.78	0.21	0.26	0.00
40.68	185.31	0.77	0.21	0.26	0.00	40.69	184.53	0.77	0.22	0.26	0.00
40.70	183.72	0.76	0.22	0.26	0.00	40.71	182.92	0.75	0.27	0.26	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
40.72	182.18	0.74	0.27	0.26	0.00	40.73	181.52	0.73	0.27	0.26	0.00
40.74	181.01	0.73	0.27	0.26	0.00	40.75	180.58	0.72	0.28	0.26	0.00
40.76	180.19	0.72	0.28	0.26	0.00	40.77	179.74	0.72	0.28	0.26	0.00
40.78	179.28	0.71	0.28	0.26	0.00	40.79	178.81	0.71	0.28	0.26	0.00
40.80	178.36	0.70	0.28	0.26	0.00	40.81	177.96	0.70	0.28	0.26	0.00
40.82	177.60	0.69	0.28	0.26	0.00	40.83	177.19	0.69	0.28	0.26	0.00
40.84	176.69	0.68	0.28	0.26	0.00	40.85	176.06	0.68	0.28	0.26	0.00
40.86	175.36	0.67	0.28	0.26	0.00	40.87	174.62	0.66	0.29	0.26	0.00
40.88	173.89	0.66	0.29	0.26	0.00	40.89	173.21	0.65	0.29	0.26	0.00
40.90	172.59	0.64	0.35	0.26	0.00	40.91	171.99	0.64	0.35	0.26	0.00
40.92	171.27	0.63	0.36	0.26	0.00	40.93	170.33	0.62	0.36	0.26	0.00
40.94	169.17	0.61	0.36	0.26	0.00	40.95	167.91	0.60	0.37	0.26	0.00
40.96	166.61	0.59	0.37	0.26	0.00	40.97	165.33	0.58	0.37	0.26	0.00
40.98	164.13	0.57	0.38	0.25	0.00	40.99	163.09	0.56	0.38	0.25	0.00
41.00	162.22	0.55	0.38	0.25	0.00	41.01	161.42	0.54	0.40	0.25	0.00
41.02	160.58	2.00	0.00	0.25	0.00	41.03	159.62	2.00	0.00	0.25	0.00
41.04	158.60	2.00	0.00	0.25	0.00	41.05	157.56	2.00	0.00	0.25	0.00
41.06	156.55	2.00	0.00	0.25	0.00	41.07	155.64	2.00	0.00	0.25	0.00
41.08	154.86	2.00	0.00	0.25	0.00	41.09	154.18	2.00	0.00	0.25	0.00
41.10	153.50	2.00	0.00	0.25	0.00	41.11	152.73	2.00	0.00	0.25	0.00
41.12	151.88	2.00	0.00	0.25	0.00	41.13	150.99	2.00	0.00	0.25	0.00
41.14	150.10	2.00	0.00	0.25	0.00	41.15	149.27	2.00	0.00	0.25	0.00
41.16	148.53	2.00	0.00	0.25	0.00	41.17	147.84	2.00	0.00	0.25	0.00
41.18	147.07	2.00	0.00	0.25	0.00	41.19	146.12	2.00	0.00	0.25	0.00
41.20	144.97	2.00	0.00	0.25	0.00	41.21	143.73	2.00	0.00	0.25	0.00
41.22	142.44	2.00	0.00	0.25	0.00	41.23	141.18	2.00	0.00	0.25	0.00
41.24	140.01	2.00	0.00	0.25	0.00	41.25	138.99	2.00	0.00	0.25	0.00
41.26	138.33	2.00	0.00	0.25	0.00	41.27	137.96	2.00	0.00	0.25	0.00
41.28	137.83	2.00	0.00	0.25	0.00	41.29	137.68	2.00	0.00	0.25	0.00
41.30	137.53	2.00	0.00	0.25	0.00	41.31	137.37	2.00	0.00	0.25	0.00
41.32	137.22	2.00	0.00	0.25	0.00	41.33	137.09	2.00	0.00	0.25	0.00
41.34	137.01	2.00	0.00	0.25	0.00	41.35	137.11	2.00	0.00	0.25	0.00
41.36	137.41	2.00	0.00	0.25	0.00	41.37	137.87	2.00	0.00	0.25	0.00
41.38	138.40	2.00	0.00	0.25	0.00	41.39	138.94	2.00	0.00	0.25	0.00
41.40	139.49	2.00	0.00	0.25	0.00	41.41	140.01	2.00	0.00	0.25	0.00
41.42	140.47	2.00	0.00	0.25	0.00	41.43	140.88	2.00	0.00	0.25	0.00
41.44	141.31	2.00	0.00	0.25	0.00	41.45	141.81	2.00	0.00	0.25	0.00
41.46	142.41	2.00	0.00	0.25	0.00	41.47	143.07	2.00	0.00	0.25	0.00
41.48	143.74	2.00	0.00	0.25	0.00	41.49	144.39	2.00	0.00	0.25	0.00
41.50	144.99	2.00	0.00	0.25	0.00	41.51	145.51	2.00	0.00	0.25	0.00
41.52	138.15	2.00	0.00	0.25	0.00	41.53	142.95	2.00	0.00	0.24	0.00
41.54	149.22	2.00	0.00	0.24	0.00	41.55	156.67	2.00	0.00	0.24	0.00
41.56	164.96	2.00	0.00	0.24	0.00	41.57	173.73	2.00	0.00	0.24	0.00
41.58	182.52	2.00	0.00	0.24	0.00	41.59	190.84	2.00	0.00	0.24	0.00
41.60	198.20	2.00	0.00	0.24	0.00	41.61	205.11	2.00	0.00	0.24	0.00
41.62	212.52	2.00	0.00	0.24	0.00	41.63	221.40	2.00	0.00	0.24	0.00
41.64	231.69	2.00	0.00	0.24	0.00	41.65	242.95	2.00	0.00	0.24	0.00
41.66	254.64	2.00	0.00	0.24	0.00	41.67	266.17	2.00	0.00	0.24	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
41.68	276.84	2.00	0.00	0.24	0.00	41.69	286.28	2.00	0.00	0.24	0.00
41.70	295.52	2.00	0.00	0.24	0.00	41.71	305.81	2.00	0.00	0.24	0.00
41.72	318.16	2.00	0.00	0.24	0.00	41.73	332.14	2.00	0.00	0.24	0.00
41.74	347.12	2.00	0.00	0.24	0.00	41.75	362.39	2.00	0.00	0.24	0.00
41.76	170.33	2.00	0.00	0.24	0.00	41.77	170.99	2.00	0.00	0.24	0.00
41.78	171.65	2.00	0.00	0.24	0.00	41.79	172.42	2.00	0.00	0.24	0.00
41.80	173.39	2.00	0.00	0.24	0.00	41.81	174.47	2.00	0.00	0.24	0.00
41.82	175.58	2.00	0.00	0.24	0.00	41.83	176.67	2.00	0.00	0.24	0.00
41.84	177.67	2.00	0.00	0.24	0.00	41.85	178.55	2.00	0.00	0.24	0.00
41.86	179.29	2.00	0.00	0.24	0.00	41.87	180.05	2.00	0.00	0.24	0.00
41.88	180.93	2.00	0.00	0.24	0.00	41.89	182.00	2.00	0.00	0.24	0.00
41.90	183.18	2.00	0.00	0.24	0.00	41.91	184.38	2.00	0.00	0.24	0.00
41.92	185.57	2.00	0.00	0.24	0.00	41.93	186.66	2.00	0.00	0.24	0.00
41.94	187.62	2.00	0.00	0.24	0.00	41.95	188.36	2.00	0.00	0.24	0.00
41.96	188.87	1.62	0.00	0.24	0.00	41.97	189.23	1.63	0.00	0.24	0.00
41.98	189.60	1.63	0.00	0.24	0.00	41.99	190.01	1.63	0.00	0.24	0.00
42.00	190.43	1.63	0.00	0.24	0.00	42.01	190.84	1.64	0.00	0.24	0.00
42.02	191.23	1.64	0.00	0.24	0.00	42.03	191.55	1.64	0.00	0.24	0.00
42.04	191.60	1.65	0.00	0.24	0.00	42.05	191.34	1.66	0.00	0.24	0.00
42.06	190.81	1.69	0.00	0.24	0.00	42.07	190.18	1.71	0.00	0.24	0.00
42.08	189.44	1.74	0.00	0.23	0.00	42.09	188.65	1.77	0.00	0.23	0.00
42.10	187.83	1.80	0.00	0.23	0.00	42.11	187.04	1.83	0.00	0.23	0.00
42.12	186.28	1.85	0.00	0.23	0.00	42.13	185.34	1.88	0.00	0.23	0.00
42.14	184.09	1.91	0.00	0.23	0.00	42.15	182.43	1.95	0.00	0.23	0.00
42.16	180.46	1.99	0.00	0.23	0.00	42.17	178.27	2.00	0.00	0.23	0.00
42.18	377.82	2.00	0.00	0.23	0.00	42.19	350.57	2.00	0.00	0.23	0.00
42.20	327.52	2.00	0.00	0.23	0.00	42.21	309.19	2.00	0.00	0.23	0.00
42.22	293.30	2.00	0.00	0.23	0.00	42.23	277.52	2.00	0.00	0.23	0.00
42.24	260.11	2.00	0.00	0.23	0.00	42.25	241.98	2.00	0.00	0.23	0.00
42.26	224.19	2.00	0.00	0.23	0.00	42.27	207.62	2.00	0.00	0.23	0.00
42.28	192.99	0.87	0.14	0.23	0.00	42.29	180.95	0.74	0.24	0.23	0.00
42.30	172.52	0.65	0.26	0.23	0.00	42.31	166.47	0.59	0.33	0.23	0.00
42.32	161.54	0.55	0.35	0.23	0.00	42.33	156.03	0.51	0.37	0.23	0.00
42.34	150.27	0.46	0.39	0.23	0.00	42.35	144.57	0.42	0.40	0.23	0.00
42.36	139.23	0.39	0.41	0.23	0.00	42.37	134.48	0.36	0.42	0.23	0.00
42.38	141.71	0.40	0.40	0.23	0.00	42.39	141.26	0.40	0.40	0.23	0.00
42.40	141.14	0.40	0.40	0.23	0.00	42.41	141.18	0.40	0.40	0.23	0.00
42.42	134.64	0.36	0.42	0.23	0.00	42.43	136.96	0.37	0.41	0.23	0.00
42.44	139.32	0.39	0.41	0.23	0.00	42.45	141.59	0.40	0.40	0.23	0.00
42.46	143.65	0.42	0.40	0.23	0.00	42.47	146.41	0.43	0.39	0.23	0.00
42.48	150.84	0.47	0.38	0.23	0.00	42.49	157.57	0.52	0.37	0.23	0.00
42.50	166.12	0.59	0.33	0.23	0.00	42.51	175.85	0.69	0.25	0.23	0.00
42.52	186.35	0.80	0.19	0.23	0.00	42.53	197.10	0.93	0.13	0.23	0.00
42.54	207.51	2.00	0.00	0.23	0.00	42.55	216.92	2.00	0.00	0.23	0.00
42.56	225.75	2.00	0.00	0.23	0.00	42.57	235.21	2.00	0.00	0.23	0.00
42.58	246.63	2.00	0.00	0.23	0.00	42.59	260.19	2.00	0.00	0.23	0.00
42.60	275.36	2.00	0.00	0.23	0.00	42.61	291.48	2.00	0.00	0.23	0.00
42.62	307.74	2.00	0.00	0.23	0.00	42.63	323.19	2.00	0.00	0.22	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
42.64	336.21	2.00	0.00	0.22	0.00	42.65	158.95	1.88	0.00	0.22	0.00
42.66	158.80	1.85	0.00	0.22	0.00	42.67	158.45	1.82	0.00	0.22	0.00
42.68	158.05	1.79	0.00	0.22	0.00	42.69	157.60	1.75	0.00	0.22	0.00
42.70	157.13	1.71	0.00	0.22	0.00	42.71	156.67	1.68	0.00	0.22	0.00
42.72	156.23	1.65	0.00	0.22	0.00	42.73	155.73	1.63	0.00	0.22	0.00
42.74	155.05	1.62	0.00	0.22	0.00	42.75	154.10	1.61	0.00	0.22	0.00
42.76	152.96	1.61	0.00	0.22	0.00	42.77	151.71	1.61	0.00	0.22	0.00
42.78	150.42	1.61	0.00	0.22	0.00	42.79	149.16	1.60	0.00	0.22	0.00
42.80	147.99	1.60	0.00	0.22	0.00	42.81	146.98	1.60	0.00	0.22	0.00
42.82	146.19	1.61	0.00	0.22	0.00	42.83	145.52	1.63	0.00	0.22	0.00
42.84	144.82	1.67	0.00	0.22	0.00	42.85	143.96	1.71	0.00	0.22	0.00
42.86	294.34	2.00	0.00	0.22	0.00	42.87	275.95	2.00	0.00	0.22	0.00
42.88	259.21	2.00	0.00	0.22	0.00	42.89	244.78	2.00	0.00	0.22	0.00
42.90	233.31	2.00	0.00	0.22	0.00	42.91	223.98	2.00	0.00	0.22	0.00
42.92	215.42	2.00	0.00	0.22	0.00	42.93	206.27	2.00	0.00	0.22	0.00
42.94	196.56	0.92	0.13	0.22	0.00	42.95	186.88	0.81	0.18	0.22	0.00
42.96	177.71	0.71	0.24	0.22	0.00	42.97	169.46	0.63	0.31	0.22	0.00
42.98	162.46	0.56	0.33	0.22	0.00	42.99	157.99	0.52	0.35	0.22	0.00
43.00	155.90	0.51	0.35	0.22	0.00	43.01	155.70	0.51	0.35	0.22	0.00
43.02	155.87	0.51	0.35	0.22	0.00	43.03	156.05	0.51	0.35	0.22	0.00
43.04	156.24	0.51	0.35	0.22	0.00	43.05	156.43	0.51	0.35	0.22	0.00
43.06	156.61	0.51	0.35	0.22	0.00	43.07	156.90	0.52	0.35	0.22	0.00
43.08	158.42	0.53	0.35	0.22	0.00	43.09	161.51	0.55	0.33	0.22	0.00
43.10	166.33	0.60	0.31	0.22	0.00	43.11	171.88	0.65	0.30	0.22	0.00
43.12	177.91	0.71	0.23	0.22	0.00	43.13	184.12	0.78	0.18	0.22	0.00
43.14	190.19	0.85	0.17	0.22	0.00	43.15	195.78	0.92	0.12	0.22	0.00
43.16	200.66	2.00	0.00	0.22	0.00	43.17	205.35	2.00	0.00	0.22	0.00
43.18	210.47	2.00	0.00	0.21	0.00	43.19	216.56	2.00	0.00	0.21	0.00
43.20	223.43	2.00	0.00	0.21	0.00	43.21	230.73	2.00	0.00	0.21	0.00
43.22	238.11	2.00	0.00	0.21	0.00	43.23	245.18	2.00	0.00	0.21	0.00
43.24	251.53	2.00	0.00	0.21	0.00	43.25	255.90	2.00	0.00	0.21	0.00
43.26	258.25	2.00	0.00	0.21	0.00	43.27	259.00	2.00	0.00	0.21	0.00
43.28	259.53	2.00	0.00	0.21	0.00	43.29	260.11	2.00	0.00	0.21	0.00
43.30	260.70	2.00	0.00	0.21	0.00	43.31	261.28	2.00	0.00	0.21	0.00
43.32	261.82	2.00	0.00	0.21	0.00	43.33	262.05	2.00	0.00	0.21	0.00
43.34	260.16	2.00	0.00	0.21	0.00	43.35	255.72	2.00	0.00	0.21	0.00
43.36	248.80	2.00	0.00	0.21	0.00	43.37	241.09	2.00	0.00	0.21	0.00
43.38	233.07	2.00	0.00	0.21	0.00	43.39	225.14	2.00	0.00	0.21	0.00
43.40	217.72	2.00	0.00	0.21	0.00	43.41	211.15	2.00	0.00	0.21	0.00
43.42	205.31	2.00	0.00	0.21	0.00	43.43	199.12	2.00	0.00	0.21	0.00
43.44	191.78	2.00	0.00	0.21	0.00	43.45	183.08	2.00	0.00	0.21	0.00
43.46	173.79	2.00	0.00	0.21	0.00	43.47	164.46	2.00	0.00	0.21	0.00
43.48	155.57	2.00	0.00	0.21	0.00	43.49	147.53	2.00	0.00	0.21	0.00
43.50	140.69	2.00	0.00	0.21	0.00	43.51	143.78	2.00	0.00	0.21	0.00
43.52	142.85	2.00	0.00	0.21	0.00	43.53	141.91	2.00	0.00	0.21	0.00
43.54	140.83	2.00	0.00	0.21	0.00	43.55	139.65	2.00	0.00	0.21	0.00
43.56	138.43	2.00	0.00	0.21	0.00	43.57	137.22	2.00	0.00	0.21	0.00
43.58	136.11	2.00	0.00	0.21	0.00	43.59	135.17	2.00	0.00	0.21	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
43.60	134.56	2.00	0.00	0.21	0.00	43.61	134.22	0.36	0.38	0.21	0.00
43.62	134.04	0.36	0.38	0.21	0.00	43.63	133.83	0.36	0.38	0.21	0.00
43.64	133.61	0.36	0.38	0.21	0.00	43.65	133.39	0.36	0.38	0.21	0.00
43.66	133.18	0.35	0.38	0.21	0.00	43.67	132.99	0.35	0.38	0.21	0.00
43.68	132.99	2.00	0.00	0.21	0.00	43.69	133.40	2.00	0.00	0.21	0.00
43.70	134.27	2.00	0.00	0.21	0.00	43.71	135.47	2.00	0.00	0.21	0.00
43.72	136.79	2.00	0.00	0.21	0.00	43.73	138.16	2.00	0.00	0.20	0.00
43.74	139.50	2.00	0.00	0.20	0.00	43.75	140.75	2.00	0.00	0.20	0.00
43.76	141.84	2.00	0.00	0.20	0.00	43.77	136.13	2.00	0.00	0.20	0.00
43.78	143.77	2.00	0.00	0.20	0.00	43.79	154.37	2.00	0.00	0.20	0.00
43.80	167.58	2.00	0.00	0.20	0.00	43.81	182.79	2.00	0.00	0.20	0.00
43.82	199.40	2.00	0.00	0.20	0.00	43.83	216.63	2.00	0.00	0.20	0.00
43.84	233.48	2.00	0.00	0.20	0.00	43.85	248.80	2.00	0.00	0.20	0.00
43.86	263.27	2.00	0.00	0.20	0.00	43.87	278.77	2.00	0.00	0.20	0.00
43.88	297.51	2.00	0.00	0.20	0.00	43.89	319.80	2.00	0.00	0.20	0.00
43.90	344.80	2.00	0.00	0.20	0.00	43.91	170.09	2.00	0.00	0.20	0.00
43.92	171.83	2.00	0.00	0.20	0.00	43.93	173.30	2.00	0.00	0.20	0.00
43.94	174.52	2.00	0.00	0.20	0.00	43.95	175.69	2.00	0.00	0.20	0.00
43.96	176.99	2.00	0.00	0.20	0.00	43.97	178.52	2.00	0.00	0.20	0.00
43.98	180.17	2.00	0.00	0.20	0.00	43.99	181.83	2.00	0.00	0.20	0.00
44.00	183.44	2.00	0.00	0.20	0.00	44.01	184.90	2.00	0.00	0.20	0.00
44.02	186.14	2.00	0.00	0.20	0.00	44.03	187.20	2.00	0.00	0.20	0.00
44.04	188.21	2.00	0.00	0.20	0.00	44.05	189.32	1.74	0.00	0.20	0.00
44.06	190.62	1.75	0.00	0.20	0.00	44.07	192.01	1.75	0.00	0.20	0.00
44.08	193.44	1.76	0.00	0.20	0.00	44.09	194.83	1.76	0.00	0.20	0.00
44.10	196.12	1.77	0.00	0.20	0.00	44.11	197.19	1.77	0.00	0.20	0.00
44.12	197.93	1.78	0.00	0.20	0.00	44.13	198.43	2.00	0.00	0.20	0.00
44.14	198.85	2.00	0.00	0.20	0.00	44.15	199.31	2.00	0.00	0.20	0.00
44.16	199.79	2.00	0.00	0.20	0.00	44.17	200.25	2.00	0.00	0.20	0.00
44.18	200.68	2.00	0.00	0.20	0.00	44.19	201.07	2.00	0.00	0.20	0.00
44.20	201.31	2.00	0.00	0.20	0.00	44.21	201.35	2.00	0.00	0.20	0.00
44.22	201.16	2.00	0.00	0.20	0.00	44.23	200.80	2.00	0.00	0.20	0.00
44.24	200.30	2.00	0.00	0.20	0.00	44.25	199.66	2.00	0.00	0.20	0.00
44.26	198.92	2.00	0.00	0.20	0.00	44.27	198.13	2.00	0.00	0.20	0.00
44.28	197.36	2.00	0.00	0.19	0.00	44.29	411.66	2.00	0.00	0.19	0.00
44.30	391.02	2.00	0.00	0.19	0.00	44.31	367.02	2.00	0.00	0.19	0.00
44.32	340.68	2.00	0.00	0.19	0.00	44.33	314.02	2.00	0.00	0.19	0.00
44.34	288.54	2.00	0.00	0.19	0.00	44.35	265.40	2.00	0.00	0.19	0.00
44.36	245.46	2.00	0.00	0.19	0.00	44.37	229.47	2.00	0.00	0.19	0.00
44.38	216.61	2.00	0.00	0.19	0.00	44.39	204.93	2.00	0.00	0.19	0.00
44.40	192.67	2.00	0.00	0.19	0.00	44.41	179.55	2.00	0.00	0.19	0.00
44.42	166.43	2.00	0.00	0.19	0.00	44.43	172.88	2.00	0.00	0.19	0.00
44.44	170.90	2.00	0.00	0.19	0.00	44.45	169.09	2.00	0.00	0.19	0.00
44.46	167.59	2.00	0.00	0.19	0.00	44.47	166.31	2.00	0.00	0.19	0.00
44.48	165.10	2.00	0.00	0.19	0.00	44.49	163.74	2.00	0.00	0.19	0.00
44.50	162.22	2.00	0.00	0.19	0.00	44.51	160.64	2.00	0.00	0.19	0.00
44.52	159.07	2.00	0.00	0.19	0.00	44.53	157.60	2.00	0.00	0.19	0.00
44.54	156.30	2.00	0.00	0.19	0.00	44.55	155.32	2.00	0.00	0.19	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
44.56	154.54	2.00	0.00	0.19	0.00	44.57	153.85	2.00	0.00	0.19	0.00
44.58	153.07	2.00	0.00	0.19	0.00	44.59	152.23	2.00	0.00	0.19	0.00
44.60	151.38	2.00	0.00	0.19	0.00	44.61	150.55	2.00	0.00	0.19	0.00
44.62	149.79	2.00	0.00	0.19	0.00	44.63	149.15	2.00	0.00	0.19	0.00
44.64	148.66	2.00	0.00	0.19	0.00	44.65	148.23	2.00	0.00	0.19	0.00
44.66	147.81	2.00	0.00	0.19	0.00	44.67	147.33	2.00	0.00	0.19	0.00
44.68	146.83	2.00	0.00	0.19	0.00	44.69	146.34	2.00	0.00	0.19	0.00
44.70	145.87	2.00	0.00	0.19	0.00	44.71	145.46	2.00	0.00	0.19	0.00
44.72	145.10	2.00	0.00	0.19	0.00	44.73	144.77	2.00	0.00	0.19	0.00
44.74	144.41	2.00	0.00	0.19	0.00	44.75	143.99	2.00	0.00	0.19	0.00
44.76	143.55	2.00	0.00	0.19	0.00	44.77	143.09	2.00	0.00	0.19	0.00
44.78	142.65	2.00	0.00	0.19	0.00	44.79	142.25	2.00	0.00	0.19	0.00
44.80	141.90	2.00	0.00	0.19	0.00	44.81	141.67	0.41	0.33	0.19	0.00
44.82	141.54	0.41	0.33	0.19	0.00	44.83	141.48	0.41	0.33	0.18	0.00
44.84	141.42	0.41	0.32	0.18	0.00	44.85	141.36	0.41	0.32	0.18	0.00
44.86	141.30	0.41	0.32	0.18	0.00	44.87	141.24	0.41	0.32	0.18	0.00
44.88	141.19	0.41	0.32	0.18	0.00	44.89	141.16	0.41	0.32	0.18	0.00
44.90	141.17	0.41	0.32	0.18	0.00	44.91	141.24	0.41	0.32	0.18	0.00
44.92	141.35	0.41	0.32	0.18	0.00	44.93	141.48	0.41	0.32	0.18	0.00
44.94	141.62	0.41	0.32	0.18	0.00	44.95	141.77	0.41	0.32	0.18	0.00
44.96	141.91	0.41	0.32	0.18	0.00	44.97	142.03	0.41	0.32	0.18	0.00
44.98	142.18	0.42	0.32	0.18	0.00	44.99	142.41	0.42	0.32	0.18	0.00
45.00	142.76	0.42	0.32	0.18	0.00	45.01	143.19	0.42	0.32	0.18	0.00
45.02	143.67	0.43	0.32	0.18	0.00	45.03	144.18	0.43	0.31	0.18	0.00
45.04	144.68	0.43	0.31	0.18	0.00	45.05	145.14	0.44	0.31	0.18	0.00
45.06	145.55	0.44	0.31	0.18	0.00	45.07	145.93	0.44	0.31	0.18	0.00
45.08	146.34	2.00	0.00	0.18	0.00	45.09	146.82	2.00	0.00	0.18	0.00
45.10	147.39	2.00	0.00	0.18	0.00	45.11	148.00	2.00	0.00	0.18	0.00
45.12	148.62	2.00	0.00	0.18	0.00	45.13	149.23	2.00	0.00	0.18	0.00
45.14	149.78	2.00	0.00	0.18	0.00	45.15	150.27	2.00	0.00	0.18	0.00
45.16	150.74	2.00	0.00	0.18	0.00	45.17	151.26	2.00	0.00	0.18	0.00
45.18	151.88	2.00	0.00	0.18	0.00	45.19	152.59	2.00	0.00	0.18	0.00
45.20	153.34	2.00	0.00	0.18	0.00	45.21	154.09	2.00	0.00	0.18	0.00
45.22	154.81	2.00	0.00	0.18	0.00	45.23	155.45	2.00	0.00	0.18	0.00
45.24	156.01	2.00	0.00	0.18	0.00	45.25	156.58	2.00	0.00	0.18	0.00
45.26	157.22	2.00	0.00	0.18	0.00	45.27	157.98	2.00	0.00	0.18	0.00
45.28	158.81	2.00	0.00	0.18	0.00	45.29	159.67	2.00	0.00	0.18	0.00
45.30	160.52	2.00	0.00	0.18	0.00	45.31	161.31	2.00	0.00	0.18	0.00
45.32	162.00	2.00	0.00	0.18	0.00	45.33	162.49	2.00	0.00	0.18	0.00
45.34	162.83	0.58	0.26	0.18	0.00	45.35	163.09	0.58	0.26	0.18	0.00
45.36	163.39	0.58	0.26	0.18	0.00	45.37	163.71	0.59	0.26	0.18	0.00
45.38	164.03	0.59	0.26	0.17	0.00	45.39	164.34	0.59	0.26	0.17	0.00
45.40	164.63	0.60	0.26	0.17	0.00	45.41	164.80	0.60	0.26	0.17	0.00
45.42	164.70	0.60	0.26	0.17	0.00	45.43	164.31	0.59	0.26	0.17	0.00
45.44	163.68	0.59	0.26	0.17	0.00	45.45	162.98	0.58	0.26	0.17	0.00
45.46	162.24	0.57	0.26	0.17	0.00	45.47	161.50	0.57	0.26	0.17	0.00
45.48	160.79	0.56	0.26	0.17	0.00	45.49	160.16	0.56	0.27	0.17	0.00
45.50	159.54	2.00	0.00	0.17	0.00	45.51	158.82	2.00	0.00	0.17	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
45.52	157.89	2.00	0.00	0.17	0.00	45.53	156.77	2.00	0.00	0.17	0.00
45.54	155.55	2.00	0.00	0.17	0.00	45.55	154.28	2.00	0.00	0.17	0.00
45.56	153.04	2.00	0.00	0.17	0.00	45.57	151.88	2.00	0.00	0.17	0.00
45.58	150.87	2.00	0.00	0.17	0.00	45.59	150.02	2.00	0.00	0.17	0.00
45.60	149.23	2.00	0.00	0.17	0.00	45.61	148.37	2.00	0.00	0.17	0.00
45.62	147.40	2.00	0.00	0.17	0.00	45.63	146.36	2.00	0.00	0.17	0.00
45.64	145.31	2.00	0.00	0.17	0.00	45.65	144.31	2.00	0.00	0.17	0.00
45.66	143.41	2.00	0.00	0.17	0.00	45.67	142.67	2.00	0.00	0.17	0.00
45.68	142.11	2.00	0.00	0.17	0.00	45.69	141.66	2.00	0.00	0.17	0.00
45.70	141.20	2.00	0.00	0.17	0.00	45.71	140.70	2.00	0.00	0.17	0.00
45.72	140.17	2.00	0.00	0.17	0.00	45.73	139.66	2.00	0.00	0.17	0.00
45.74	139.18	2.00	0.00	0.17	0.00	45.75	138.75	2.00	0.00	0.17	0.00
45.76	138.43	2.00	0.00	0.17	0.00	45.77	138.20	0.39	0.30	0.17	0.00
45.78	138.03	0.39	0.30	0.17	0.00	45.79	137.85	0.39	0.30	0.17	0.00
45.80	137.65	0.39	0.30	0.17	0.00	45.81	137.46	0.39	0.30	0.17	0.00
45.82	137.26	0.39	0.30	0.17	0.00	45.83	137.08	0.39	0.30	0.17	0.00
45.84	136.93	0.39	0.30	0.17	0.00	45.85	136.78	0.38	0.30	0.17	0.00
45.86	136.62	0.38	0.30	0.17	0.00	45.87	136.44	0.38	0.30	0.17	0.00
45.88	136.23	0.38	0.30	0.17	0.00	45.89	136.03	0.38	0.30	0.17	0.00
45.90	135.82	0.38	0.30	0.17	0.00	45.91	135.62	0.38	0.30	0.17	0.00
45.92	135.45	0.38	0.30	0.17	0.00	45.93	135.31	0.38	0.30	0.16	0.00
45.94	135.21	0.37	0.30	0.16	0.00	45.95	135.14	0.37	0.30	0.16	0.00
45.96	135.08	0.37	0.30	0.16	0.00	45.97	135.03	0.37	0.30	0.16	0.00
45.98	134.99	0.37	0.30	0.16	0.00	45.99	134.96	0.37	0.30	0.16	0.00
46.00	134.95	0.37	0.30	0.16	0.00	46.01	134.94	0.37	0.30	0.16	0.00
46.02	134.93	0.37	0.30	0.16	0.00	46.03	134.90	0.37	0.30	0.16	0.00
46.04	134.86	0.37	0.30	0.16	0.00	46.05	134.82	0.37	0.30	0.16	0.00
46.06	134.80	0.37	0.30	0.16	0.00	46.07	134.79	0.37	0.30	0.16	0.00
46.08	134.79	0.37	0.30	0.16	0.00	46.09	134.81	0.37	0.30	0.16	0.00
46.10	134.85	0.37	0.30	0.16	0.00	46.11	135.19	0.38	0.29	0.16	0.00
46.12	135.90	0.38	0.29	0.16	0.00	46.13	137.04	0.39	0.29	0.16	0.00
46.14	138.35	0.40	0.29	0.16	0.00	46.15	139.76	0.40	0.29	0.16	0.00
46.16	141.22	0.41	0.28	0.16	0.00	46.17	142.63	0.42	0.28	0.16	0.00
46.18	143.92	0.43	0.28	0.16	0.00	46.19	145.03	0.44	0.28	0.16	0.00
46.20	146.07	0.45	0.27	0.16	0.00	46.21	147.18	0.46	0.27	0.16	0.00
46.22	148.49	0.47	0.27	0.16	0.00	46.23	149.96	0.48	0.27	0.16	0.00
46.24	151.53	0.49	0.26	0.16	0.00	46.25	153.10	0.50	0.26	0.16	0.00
46.26	154.61	0.51	0.26	0.16	0.00	46.27	155.96	0.53	0.26	0.16	0.00
46.28	156.70	0.53	0.26	0.16	0.00	46.29	156.70	0.53	0.26	0.16	0.00
46.30	155.97	0.53	0.26	0.16	0.00	46.31	154.98	0.52	0.26	0.16	0.00
46.32	153.91	0.51	0.26	0.16	0.00	46.33	152.82	0.50	0.26	0.16	0.00
46.34	151.77	0.49	0.26	0.16	0.00	46.35	150.80	0.48	0.26	0.16	0.00
46.36	149.98	0.48	0.26	0.16	0.00	46.37	149.41	0.47	0.26	0.16	0.00
46.38	149.01	0.47	0.26	0.16	0.00	46.39	148.71	0.47	0.26	0.16	0.00
46.40	148.37	0.47	0.26	0.16	0.00	46.41	148.02	0.46	0.26	0.16	0.00
46.42	147.67	0.46	0.26	0.16	0.00	46.43	147.33	0.46	0.26	0.16	0.00
46.44	147.02	0.46	0.27	0.16	0.00	46.45	146.79	2.00	0.00	0.16	0.00
46.46	146.69	2.00	0.00	0.16	0.00	46.47	146.70	2.00	0.00	0.16	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
46.48	146.79	2.00	0.00	0.15	0.00	46.49	146.91	2.00	0.00	0.15	0.00
46.50	147.07	2.00	0.00	0.15	0.00	46.51	147.25	2.00	0.00	0.15	0.00
46.52	147.44	2.00	0.00	0.15	0.00	46.53	147.62	2.00	0.00	0.15	0.00
46.54	147.72	2.00	0.00	0.15	0.00	46.55	147.75	2.00	0.00	0.15	0.00
46.56	147.70	2.00	0.00	0.15	0.00	46.57	147.65	2.00	0.00	0.15	0.00
46.58	147.62	2.00	0.00	0.15	0.00	46.59	147.62	2.00	0.00	0.15	0.00
46.60	147.64	2.00	0.00	0.15	0.00	46.61	147.67	2.00	0.00	0.15	0.00
46.62	147.73	2.00	0.00	0.15	0.00	46.63	148.04	2.00	0.00	0.15	0.00
46.64	148.66	2.00	0.00	0.15	0.00	46.65	149.65	2.00	0.00	0.15	0.00
46.66	150.79	2.00	0.00	0.15	0.00	46.67	152.02	2.00	0.00	0.15	0.00
46.68	153.29	2.00	0.00	0.15	0.00	46.69	154.51	2.00	0.00	0.15	0.00
46.70	155.62	2.00	0.00	0.15	0.00	46.71	156.64	2.00	0.00	0.15	0.00
46.72	157.79	2.00	0.00	0.15	0.00	46.73	159.23	2.00	0.00	0.15	0.00
46.74	161.00	2.00	0.00	0.15	0.00	46.75	162.96	2.00	0.00	0.15	0.00
46.76	164.98	2.00	0.00	0.15	0.00	46.77	166.95	2.00	0.00	0.15	0.00
46.78	168.76	2.00	0.00	0.15	0.00	46.79	170.34	2.00	0.00	0.15	0.00
46.80	168.57	2.00	0.00	0.15	0.00	46.81	177.27	2.00	0.00	0.15	0.00
46.82	187.10	2.00	0.00	0.15	0.00	46.83	199.02	2.00	0.00	0.15	0.00
46.84	212.64	2.00	0.00	0.15	0.00	46.85	227.39	2.00	0.00	0.15	0.00
46.86	242.58	2.00	0.00	0.15	0.00	46.87	257.34	2.00	0.00	0.15	0.00
46.88	270.57	2.00	0.00	0.15	0.00	46.89	281.52	2.00	0.00	0.15	0.00
46.90	291.36	2.00	0.00	0.15	0.00	46.91	301.73	2.00	0.00	0.15	0.00
46.92	313.96	2.00	0.00	0.15	0.00	46.93	327.58	2.00	0.00	0.15	0.00
46.94	341.98	2.00	0.00	0.15	0.00	46.95	356.45	2.00	0.00	0.15	0.00
46.96	370.13	2.00	0.00	0.15	0.00	46.97	381.50	2.00	0.00	0.15	0.00
46.98	390.12	2.00	0.00	0.15	0.00	46.99	397.00	2.00	0.00	0.15	0.00
47.00	182.81	2.00	0.00	0.15	0.00	47.01	181.84	2.00	0.00	0.15	0.00
47.02	180.82	2.00	0.00	0.15	0.00	47.03	179.78	2.00	0.00	0.14	0.00
47.04	178.79	2.00	0.00	0.14	0.00	47.05	177.90	2.00	0.00	0.14	0.00
47.06	177.30	2.00	0.00	0.14	0.00	47.07	177.00	1.99	0.00	0.14	0.00
47.08	176.95	1.98	0.00	0.14	0.00	47.09	176.94	1.97	0.00	0.14	0.00
47.10	176.93	1.96	0.00	0.14	0.00	47.11	176.92	1.95	0.00	0.14	0.00
47.12	176.91	1.94	0.00	0.14	0.00	47.13	176.90	1.94	0.00	0.14	0.00
47.14	176.90	1.93	0.00	0.14	0.00	47.15	177.04	1.93	0.00	0.14	0.00
47.16	177.36	1.93	0.00	0.14	0.00	47.17	177.86	1.94	0.00	0.14	0.00
47.18	178.43	1.95	0.00	0.14	0.00	47.19	179.03	1.97	0.00	0.14	0.00
47.20	179.65	1.98	0.00	0.14	0.00	47.21	180.23	1.99	0.00	0.14	0.00
47.22	180.76	2.00	0.00	0.14	0.00	47.23	181.13	2.00	0.00	0.14	0.00
47.24	181.27	2.00	0.00	0.14	0.00	47.25	181.18	2.00	0.00	0.14	0.00
47.26	180.98	2.00	0.00	0.14	0.00	47.27	180.74	2.00	0.00	0.14	0.00
47.28	180.47	2.00	0.00	0.14	0.00	47.29	180.19	2.00	0.00	0.14	0.00
47.30	179.92	2.00	0.00	0.14	0.00	47.31	179.67	2.00	0.00	0.14	0.00
47.32	179.32	2.00	0.00	0.14	0.00	47.33	178.78	2.00	0.00	0.14	0.00
47.34	177.98	2.00	0.00	0.14	0.00	47.35	376.45	2.00	0.00	0.14	0.00
47.36	363.91	2.00	0.00	0.14	0.00	47.37	351.34	2.00	0.00	0.14	0.00
47.38	339.39	2.00	0.00	0.14	0.00	47.39	328.62	2.00	0.00	0.14	0.00
47.40	319.49	2.00	0.00	0.14	0.00	47.41	311.10	2.00	0.00	0.14	0.00
47.42	302.25	2.00	0.00	0.14	0.00	47.43	291.96	2.00	0.00	0.14	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
47.44	280.58	2.00	0.00	0.14	0.00	47.45	268.81	2.00	0.00	0.14	0.00
47.46	257.27	2.00	0.00	0.14	0.00	47.47	246.54	2.00	0.00	0.14	0.00
47.48	237.12	2.00	0.00	0.14	0.00	47.49	229.58	2.00	0.00	0.14	0.00
47.50	223.47	2.00	0.00	0.14	0.00	47.51	217.87	2.00	0.00	0.14	0.00
47.52	211.77	2.00	0.00	0.14	0.00	47.53	205.11	2.00	0.00	0.14	0.00
47.54	198.29	0.99	0.06	0.14	0.00	47.55	191.64	0.90	0.08	0.14	0.00
47.56	185.51	0.83	0.11	0.14	0.00	47.57	180.20	0.77	0.12	0.14	0.00
47.58	176.10	0.72	0.15	0.13	0.00	47.59	172.80	0.69	0.15	0.13	0.00
47.60	169.77	0.66	0.16	0.13	0.00	47.61	166.36	0.63	0.19	0.13	0.00
47.62	162.69	0.59	0.20	0.13	0.00	47.63	158.97	0.56	0.21	0.13	0.00
47.64	155.39	0.53	0.22	0.13	0.00	47.65	152.12	0.50	0.22	0.13	0.00
47.66	149.29	0.48	0.22	0.13	0.00	47.67	146.49	0.46	0.23	0.13	0.00
47.68	143.35	0.44	0.23	0.13	0.00	47.69	139.57	0.41	0.24	0.13	0.00
47.70	135.39	0.38	0.24	0.13	0.00	47.71	131.08	0.36	0.25	0.13	0.00
47.72	134.99	0.38	0.24	0.13	0.00	47.73	134.48	0.38	0.24	0.13	0.00
47.74	134.00	0.37	0.24	0.13	0.00	47.75	133.57	0.37	0.24	0.13	0.00
47.76	133.10	0.37	0.24	0.13	0.00	47.77	132.52	0.37	0.24	0.13	0.00
47.78	131.83	0.36	0.24	0.13	0.00	47.79	131.06	0.36	0.25	0.13	0.00
47.80	130.25	0.35	0.25	0.13	0.00	47.81	129.46	0.35	0.25	0.13	0.00
47.82	128.71	0.34	0.25	0.13	0.00	47.83	128.05	0.34	0.25	0.13	0.00
47.84	127.54	0.34	0.25	0.13	0.00	47.85	127.13	0.33	0.25	0.13	0.00
47.86	126.77	0.33	0.25	0.13	0.00	47.87	126.36	0.33	0.25	0.13	0.00
47.88	125.92	0.33	0.25	0.13	0.00	47.89	125.47	0.33	0.25	0.13	0.00
47.90	125.03	0.32	0.25	0.13	0.00	47.91	124.63	0.32	0.25	0.13	0.00
47.92	124.34	0.32	0.25	0.13	0.00	47.93	124.45	0.32	0.25	0.13	0.00
47.94	124.99	0.32	0.25	0.13	0.00	47.95	125.92	0.33	0.25	0.13	0.00
47.96	126.96	0.33	0.25	0.13	0.00	47.97	121.68	0.31	0.25	0.13	0.00
47.98	126.44	0.33	0.25	0.13	0.00	47.99	131.11	0.36	0.24	0.13	0.00
48.00	135.41	0.38	0.23	0.13	0.00	48.01	139.55	0.41	0.23	0.13	0.00
48.02	144.41	0.45	0.22	0.13	0.00	48.03	150.73	0.49	0.21	0.13	0.00
48.04	158.74	0.56	0.20	0.13	0.00	48.05	167.91	0.64	0.18	0.13	0.00
48.06	177.84	0.75	0.14	0.13	0.00	48.07	188.05	0.86	0.08	0.13	0.00
48.08	197.99	0.99	0.06	0.13	0.00	48.09	207.03	2.00	0.00	0.13	0.00
48.10	214.70	2.00	0.00	0.13	0.00	48.11	221.80	2.00	0.00	0.13	0.00
48.12	229.32	2.00	0.00	0.13	0.00	48.13	238.18	2.00	0.00	0.12	0.00
48.14	248.02	2.00	0.00	0.12	0.00	48.15	258.40	2.00	0.00	0.12	0.00
48.16	268.79	2.00	0.00	0.12	0.00	48.17	278.62	2.00	0.00	0.12	0.00
48.18	286.73	2.00	0.00	0.12	0.00	48.19	291.23	2.00	0.00	0.12	0.00
48.20	292.40	2.00	0.00	0.12	0.00	48.21	291.37	2.00	0.00	0.12	0.00
48.22	290.20	2.00	0.00	0.12	0.00	48.23	288.96	2.00	0.00	0.12	0.00
48.24	287.72	2.00	0.00	0.12	0.00	48.25	286.54	2.00	0.00	0.12	0.00
48.26	285.49	2.00	0.00	0.12	0.00	48.27	283.02	2.00	0.00	0.12	0.00
48.28	277.22	2.00	0.00	0.12	0.00	48.29	267.51	2.00	0.00	0.12	0.00
48.30	255.18	2.00	0.00	0.12	0.00	48.31	241.99	2.00	0.00	0.12	0.00
48.32	228.72	2.00	0.00	0.12	0.00	48.33	216.05	2.00	0.00	0.12	0.00
48.34	204.59	2.00	0.00	0.12	0.00	48.35	194.85	2.00	0.00	0.12	0.00
48.36	186.45	2.00	0.00	0.12	0.00	48.37	178.22	2.00	0.00	0.12	0.00
48.38	169.13	2.00	0.00	0.12	0.00	48.39	159.04	2.00	0.00	0.12	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
48.40	148.64	2.00	0.00	0.12	0.00	48.41	138.51	2.00	0.00	0.12	0.00
48.42	129.15	2.00	0.00	0.12	0.00	48.43	120.95	2.00	0.00	0.12	0.00
48.44	114.39	2.00	0.00	0.12	0.00	48.45	118.35	2.00	0.00	0.12	0.00
48.46	117.60	2.00	0.00	0.12	0.00	48.47	116.94	2.00	0.00	0.12	0.00
48.48	116.20	2.00	0.00	0.12	0.00	48.49	115.40	2.00	0.00	0.12	0.00
48.50	114.59	2.00	0.00	0.12	0.00	48.51	113.81	2.00	0.00	0.12	0.00
48.52	113.11	2.00	0.00	0.12	0.00	48.53	112.65	2.00	0.00	0.12	0.00
48.54	112.53	0.26	0.25	0.12	0.00	48.55	112.72	0.27	0.25	0.12	0.00
48.56	113.06	0.27	0.25	0.12	0.00	48.57	113.43	0.27	0.25	0.12	0.00
48.58	113.82	0.27	0.25	0.12	0.00	48.59	114.20	0.27	0.24	0.12	0.00
48.60	114.55	0.27	0.24	0.12	0.00	48.61	114.87	0.28	0.24	0.12	0.00
48.62	115.56	2.00	0.00	0.12	0.00	48.63	116.81	2.00	0.00	0.12	0.00
48.64	118.74	2.00	0.00	0.12	0.00	48.65	120.98	2.00	0.00	0.12	0.00
48.66	123.37	2.00	0.00	0.12	0.00	48.67	125.80	2.00	0.00	0.12	0.00
48.68	128.13	2.00	0.00	0.11	0.00	48.69	127.53	2.00	0.00	0.11	0.00
48.70	134.68	2.00	0.00	0.11	0.00	48.71	142.90	2.00	0.00	0.11	0.00
48.72	153.58	2.00	0.00	0.11	0.00	48.73	167.75	2.00	0.00	0.11	0.00
48.74	184.52	2.00	0.00	0.11	0.00	48.75	203.24	2.00	0.00	0.11	0.00
48.76	223.05	2.00	0.00	0.11	0.00	48.77	242.90	2.00	0.00	0.11	0.00
48.78	261.52	2.00	0.00	0.11	0.00	48.79	277.77	2.00	0.00	0.11	0.00
48.80	292.98	2.00	0.00	0.11	0.00	48.81	309.21	2.00	0.00	0.11	0.00
48.82	328.56	2.00	0.00	0.11	0.00	48.83	350.61	2.00	0.00	0.11	0.00
48.84	374.40	2.00	0.00	0.11	0.00	48.85	176.37	2.00	0.00	0.11	0.00
48.86	178.76	2.00	0.00	0.11	0.00	48.87	180.80	2.00	0.00	0.11	0.00
48.88	182.16	2.00	0.00	0.11	0.00	48.89	182.98	2.00	0.00	0.11	0.00
48.90	183.44	2.00	0.00	0.11	0.00	48.91	183.94	2.00	0.00	0.11	0.00
48.92	184.48	2.00	0.00	0.11	0.00	48.93	185.04	2.00	0.00	0.11	0.00
48.94	185.57	2.00	0.00	0.11	0.00	48.95	186.06	2.00	0.00	0.11	0.00
48.96	186.42	2.00	0.00	0.11	0.00	48.97	186.54	2.00	0.00	0.11	0.00
48.98	186.41	2.00	0.00	0.11	0.00	48.99	186.06	2.00	0.00	0.11	0.00
49.00	185.60	2.00	0.00	0.11	0.00	49.01	185.02	2.00	0.00	0.11	0.00
49.02	382.82	2.00	0.00	0.11	0.00	49.03	363.05	2.00	0.00	0.11	0.00
49.04	346.16	2.00	0.00	0.11	0.00	49.05	330.89	2.00	0.00	0.11	0.00
49.06	314.35	2.00	0.00	0.11	0.00	49.07	294.77	2.00	0.00	0.11	0.00
49.08	272.62	2.00	0.00	0.11	0.00	49.09	250.02	2.00	0.00	0.11	0.00
49.10	228.32	2.00	0.00	0.11	0.00	49.11	208.54	2.00	0.00	0.11	0.00
49.12	191.40	2.00	0.00	0.11	0.00	49.13	177.41	2.00	0.00	0.11	0.00
49.14	165.76	2.00	0.00	0.11	0.00	49.15	168.13	2.00	0.00	0.11	0.00
49.16	166.88	2.00	0.00	0.11	0.00	49.17	165.39	2.00	0.00	0.11	0.00
49.18	163.72	2.00	0.00	0.11	0.00	49.19	161.97	2.00	0.00	0.11	0.00
49.20	160.25	2.00	0.00	0.11	0.00	49.21	158.65	2.00	0.00	0.11	0.00
49.22	157.36	2.00	0.00	0.11	0.00	49.23	156.48	2.00	0.00	0.10	0.00
49.24	155.90	2.00	0.00	0.10	0.00	49.25	155.43	2.00	0.00	0.10	0.00
49.26	154.93	2.00	0.00	0.10	0.00	49.27	154.43	2.00	0.00	0.10	0.00
49.28	153.98	2.00	0.00	0.10	0.00	49.29	153.61	2.00	0.00	0.10	0.00
49.30	153.30	2.00	0.00	0.10	0.00	49.31	153.19	2.00	0.00	0.10	0.00
49.32	153.30	2.00	0.00	0.10	0.00	49.33	153.64	2.00	0.00	0.10	0.00
49.34	154.10	2.00	0.00	0.10	0.00	49.35	154.62	2.00	0.00	0.10	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
49.36	155.17	2.00	0.00	0.10	0.00	49.37	155.72	2.00	0.00	0.10	0.00
49.38	156.25	2.00	0.00	0.10	0.00	49.39	156.72	2.00	0.00	0.10	0.00
49.40	157.21	2.00	0.00	0.10	0.00	49.41	157.80	0.56	0.16	0.10	0.00
49.42	158.56	0.57	0.16	0.10	0.00	49.43	159.43	0.57	0.16	0.10	0.00
49.44	160.37	0.58	0.15	0.10	0.00	49.45	161.32	0.59	0.15	0.10	0.00
49.46	162.25	0.60	0.15	0.10	0.00	49.47	163.09	0.61	0.15	0.10	0.00
49.48	163.67	0.61	0.15	0.10	0.00	49.49	163.72	0.61	0.15	0.10	0.00
49.50	163.24	0.61	0.15	0.10	0.00	49.51	162.37	0.60	0.15	0.10	0.00
49.52	161.43	0.59	0.15	0.10	0.00	49.53	160.46	0.58	0.15	0.10	0.00
49.54	159.51	0.58	0.15	0.10	0.00	49.55	158.62	0.57	0.15	0.10	0.00
49.56	157.85	0.56	0.15	0.10	0.00	49.57	157.10	0.55	0.16	0.10	0.00
49.58	156.21	0.55	0.16	0.10	0.00	49.59	155.07	0.54	0.16	0.10	0.00
49.60	153.70	0.53	0.16	0.10	0.00	49.61	152.23	0.51	0.16	0.10	0.00
49.62	150.74	0.50	0.16	0.10	0.00	49.63	149.30	0.49	0.16	0.10	0.00
49.64	147.99	0.48	0.17	0.10	0.00	49.65	146.87	0.47	0.17	0.10	0.00
49.66	146.12	0.47	0.17	0.10	0.00	49.67	145.65	0.46	0.17	0.10	0.00
49.68	145.38	0.46	0.17	0.10	0.00	49.69	145.07	0.46	0.17	0.10	0.00
49.70	144.74	0.46	0.17	0.10	0.00	49.71	144.40	0.45	0.17	0.10	0.00
49.72	144.08	0.45	0.17	0.10	0.00	49.73	143.79	0.45	0.17	0.10	0.00
49.74	143.53	0.45	0.17	0.10	0.00	49.75	143.30	0.45	0.17	0.10	0.00
49.76	143.05	0.44	0.17	0.10	0.00	49.77	142.75	0.44	0.17	0.10	0.00
49.78	142.43	0.44	0.17	0.09	0.00	49.79	142.09	0.44	0.17	0.09	0.00
49.80	141.75	0.44	0.17	0.09	0.00	49.81	141.43	0.43	0.17	0.09	0.00
49.82	141.15	0.43	0.17	0.09	0.00	49.83	140.92	0.43	0.17	0.09	0.00
49.84	140.73	0.43	0.17	0.09	0.00	49.85	140.57	0.43	0.17	0.09	0.00
49.86	140.41	0.43	0.17	0.09	0.00	49.87	140.25	0.43	0.17	0.09	0.00
49.88	140.10	0.42	0.16	0.09	0.00	49.89	139.97	0.42	0.16	0.09	0.00
49.90	139.86	0.42	0.16	0.09	0.00	49.91	139.77	0.42	0.16	0.09	0.00
49.92	139.67	0.42	0.16	0.09	0.00	49.93	139.56	0.42	0.16	0.09	0.00
49.94	139.40	0.42	0.16	0.09	0.00	49.95	139.24	0.42	0.16	0.09	0.00
49.96	139.06	0.42	0.16	0.09	0.00	49.97	138.89	0.42	0.16	0.09	0.00
49.98	138.74	0.42	0.16	0.09	0.00	49.99	138.60	0.41	0.16	0.09	0.00
50.00	138.51	0.41	0.16	0.09	0.00						

Total estimated settlement: 0.98**Abbreviations**

$Q_{tn,cs}$: Equivalent clean sand normalized cone resistance
 FS: Factor of safety against liquefaction
 e_v (%): Post-liquefaction volumetric strain
 DF: e_v depth weighting factor
 Settlement: Calculated settlement

:: Strength loss calculation (Robertson (2009)) ::

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.01	30.91	58.42	1.61	93.96	2.20	0.74	0.74
0.02	30.75	58.11	1.60	93.07	2.19	0.73	0.73
0.03	30.52	57.69	1.59	91.83	2.19	0.73	0.73
0.04	30.24	57.15	1.59	90.71	2.19	0.73	0.73
0.05	29.79	56.30	1.59	89.54	2.19	0.73	0.73
0.06	29.13	55.05	1.60	88.15	2.19	0.72	0.72
0.07	28.30	53.49	1.62	86.52	2.20	0.72	0.72
0.08	27.40	51.78	1.64	84.76	2.21	0.72	0.72
0.09	26.46	50.01	1.66	82.96	2.22	0.71	0.71
0.10	25.55	48.28	1.68	81.21	2.23	0.65	0.71
0.11	24.69	46.66	1.71	79.61	2.23	0.57	0.71
0.12	23.95	45.26	1.73	78.24	2.24	0.50	0.70
0.13	23.54	44.48	1.75	77.73	2.25	0.48	0.70
0.14	23.44	44.29	1.76	78.09	2.25	0.50	0.70
0.15	23.59	44.58	1.78	79.27	2.26	0.55	0.71
0.16	23.77	44.92	1.79	80.62	2.26	0.62	0.71
0.17	23.97	45.28	1.81	82.08	2.27	0.69	0.71
0.18	24.16	45.65	1.83	83.57	2.27	0.72	0.72
0.19	24.35	46.01	1.85	85.01	2.28	0.72	0.72
0.20	24.52	46.33	1.86	86.33	2.28	0.72	0.72
0.21	24.72	46.70	1.87	87.52	2.29	0.72	0.72
0.22	25.06	47.34	1.88	88.80	2.29	0.73	0.73
0.23	25.60	48.37	1.87	90.35	2.28	0.73	0.73
0.24	26.34	49.76	1.85	92.28	2.28	0.73	0.73
0.25	27.16	51.31	1.84	94.45	2.28	0.74	0.74
0.26	28.03	52.95	1.83	96.76	2.27	0.74	0.74
0.27	28.89	54.58	1.82	99.07	2.27	0.75	0.75
0.28	29.71	56.13	1.80	101.29	2.27	0.75	0.75
0.29	30.44	57.51	1.80	103.27	2.26	0.75	0.75
0.30	31.08	58.72	1.79	104.90	2.26	0.76	0.76
0.31	31.72	59.92	1.77	106.31	2.26	0.76	0.76
0.32	32.43	61.27	1.76	107.71	2.25	0.76	0.76
0.33	33.28	62.86	1.74	109.31	2.25	0.76	0.76
0.34	34.20	64.61	1.72	111.08	2.24	0.77	0.77
0.35	35.15	66.40	1.70	112.92	2.23	0.77	0.77
0.36	36.09	68.17	1.68	114.75	2.23	0.77	0.77
0.37	36.95	69.81	1.67	116.47	2.22	0.78	0.78
0.38	37.71	71.24	1.66	117.97	2.22	0.78	0.78
0.39	38.38	72.50	1.64	119.18	2.21	0.78	0.78
0.40	39.04	73.76	1.63	120.26	2.21	0.78	0.78
0.41	39.80	75.19	1.61	121.37	2.20	0.79	0.79
0.42	40.67	76.83	1.60	122.67	2.19	0.79	0.79
0.43	41.60	78.59	1.58	124.07	2.19	0.79	0.79
0.44	42.55	80.37	1.56	125.52	2.18	0.79	0.79
0.45	43.46	82.09	1.55	126.93	2.17	0.79	0.79
0.46	44.29	83.66	1.53	128.24	2.16	0.80	0.80
0.47	44.98	84.98	1.52	129.36	2.16	0.80	0.80
0.48	45.59	86.13	1.51	130.41	2.16	0.80	0.80

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.49	46.19	87.26	1.51	131.53	2.15	0.80	0.80
0.50	46.87	88.55	1.50	132.83	2.15	0.80	0.80
0.51	47.63	89.98	1.49	134.29	2.14	0.80	0.80
0.52	48.43	91.48	1.48	135.84	2.14	0.81	0.81
0.53	49.22	92.99	1.48	137.39	2.14	0.81	0.81
0.54	49.98	94.41	1.47	138.87	2.13	0.81	0.81
0.55	50.65	95.67	1.47	140.19	2.13	0.81	0.81
0.56	51.19	96.70	1.46	141.28	2.13	0.81	0.81
0.57	51.66	97.59	1.46	142.26	2.12	0.82	0.82
0.58	52.12	98.45	1.46	143.26	2.12	0.82	0.82
0.59	52.64	99.44	1.45	144.41	2.12	0.82	0.82
0.60	53.21	100.51	1.45	145.66	2.12	0.82	0.82
0.61	53.80	101.62	1.45	146.96	2.12	0.82	0.82
0.62	54.37	102.71	1.44	148.24	2.12	0.82	0.82
0.63	54.91	103.72	1.44	149.43	2.11	0.83	0.83
0.64	55.37	104.59	1.44	150.45	2.11	0.83	0.83
0.65	55.71	105.24	1.44	151.21	2.11	0.83	0.83
0.66	55.98	105.74	1.44	151.78	2.11	0.83	0.83
0.67	56.22	106.19	1.43	152.28	2.11	0.83	0.83
0.68	56.49	106.70	1.43	152.85	2.11	0.83	0.83
0.69	56.78	107.24	1.43	153.46	2.11	0.83	0.83
0.70	57.07	107.80	1.43	154.08	2.11	0.83	0.83
0.71	57.35	108.33	1.43	154.67	2.11	0.83	0.83
0.72	57.61	108.81	1.43	155.21	2.11	0.83	0.83
0.73	57.82	109.20	1.43	155.64	2.10	0.83	0.83
0.74	57.97	109.49	1.42	155.93	2.10	0.83	0.83
0.75	58.09	109.71	1.42	156.11	2.10	0.84	0.84
0.76	58.20	109.92	1.42	156.25	2.10	0.84	0.84
0.77	58.33	110.16	1.42	156.41	2.10	0.84	0.84
0.78	58.46	110.41	1.42	156.58	2.10	0.84	0.84
0.79	58.59	110.66	1.42	156.75	2.10	0.84	0.84
0.80	58.72	110.90	1.41	156.91	2.10	0.84	0.84
0.81	58.83	111.11	1.41	157.05	2.10	0.84	0.84
0.82	58.92	111.28	1.41	157.16	2.10	0.84	0.84
0.83	59.00	111.43	1.41	157.22	2.09	0.84	0.84
0.84	59.08	111.59	1.41	157.27	2.09	0.84	0.84
0.85	59.18	111.77	1.41	157.31	2.09	0.84	0.84
0.86	59.28	111.96	1.41	157.35	2.09	0.84	0.84
0.87	59.39	112.16	1.40	157.40	2.09	0.84	0.84
0.88	59.49	112.36	1.40	157.45	2.09	0.84	0.84
0.89	59.59	112.54	1.40	157.50	2.09	0.84	0.84
0.90	59.68	112.70	1.40	157.54	2.09	0.84	0.84
0.91	59.76	112.86	1.40	157.60	2.08	0.84	0.84
0.92	59.87	113.06	1.39	157.69	2.08	0.84	0.84
0.93	60.00	113.30	1.39	157.81	2.08	0.84	0.84
0.94	60.14	113.58	1.39	157.96	2.08	0.84	0.84
0.95	60.30	113.87	1.39	158.11	2.08	0.84	0.84
0.96	60.46	114.18	1.39	158.27	2.08	0.84	0.84

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.97	60.62	114.47	1.38	158.42	2.07	0.84	0.84
0.98	60.76	114.73	1.38	158.56	2.07	0.84	0.84
0.99	60.90	114.99	1.38	158.71	2.07	0.84	0.84
1.00	61.09	115.36	1.38	158.93	2.07	0.84	0.84
1.01	61.36	115.88	1.37	159.26	2.07	0.84	0.84
1.02	61.72	116.55	1.37	159.71	2.06	0.84	0.84
1.03	62.12	117.29	1.37	160.20	2.06	0.84	0.84
1.04	62.53	118.08	1.36	160.73	2.06	0.84	0.84
1.05	62.94	118.86	1.36	161.26	2.05	0.84	0.84
1.06	63.33	119.59	1.35	161.76	2.05	0.84	0.84
1.07	63.68	120.24	1.35	162.21	2.04	0.84	0.84
1.08	63.97	120.79	1.35	162.56	2.04	0.84	0.84
1.09	64.23	121.29	1.34	162.85	2.04	0.84	0.84
1.10	64.51	121.82	1.34	163.10	2.03	0.84	0.84
1.11	64.83	122.42	1.33	163.38	2.03	0.84	0.84
1.12	65.18	123.08	1.33	163.70	2.03	0.84	0.84
1.13	65.54	123.76	1.33	164.03	2.02	0.85	0.85
1.14	65.90	124.43	1.32	164.37	2.02	0.85	0.85
1.15	66.22	125.04	1.32	164.68	2.01	0.85	0.85
1.16	66.50	125.57	1.31	164.95	2.01	0.85	0.85
1.17	66.72	125.98	1.31	165.12	2.00	0.85	0.85
1.18	66.91	126.33	1.31	165.20	2.00	0.85	0.85
1.19	67.09	126.68	1.30	165.22	2.00	0.85	0.85
1.20	67.30	127.07	1.30	165.25	1.99	0.85	0.85
1.21	67.52	127.48	1.30	165.29	1.99	0.85	0.85
1.22	67.74	127.90	1.29	165.33	1.98	0.85	0.85
1.23	67.96	128.31	1.29	165.38	1.98	0.85	0.85
1.24	68.15	128.68	1.29	165.42	1.97	0.85	0.85
1.25	68.30	128.96	1.28	165.45	1.97	0.85	0.85
1.26	68.38	129.12	1.28	165.43	1.97	0.85	0.85
1.27	68.42	129.18	1.28	165.39	1.96	0.85	0.85
1.28	68.43	129.20	1.28	165.31	1.96	0.85	0.85
1.29	68.44	129.22	1.28	165.23	1.96	0.85	0.85
1.30	68.45	129.24	1.28	165.14	1.96	0.85	0.85
1.31	68.47	129.27	1.28	165.05	1.96	0.85	0.85
1.32	68.48	129.29	1.28	164.97	1.96	0.85	0.85
1.33	68.49	129.31	1.28	164.90	1.96	0.85	0.85
1.34	68.46	129.26	1.28	164.81	1.96	0.85	0.85
1.35	68.38	129.09	1.28	164.70	1.96	0.85	0.85
1.36	68.22	128.80	1.28	164.55	1.96	0.85	0.85
1.37	68.03	128.43	1.28	164.37	1.96	0.85	0.85
1.38	67.82	128.04	1.28	164.17	1.97	0.85	0.85
1.39	67.61	127.64	1.28	163.97	1.97	0.85	0.85
1.40	67.40	127.24	1.29	163.77	1.97	0.84	0.84
1.41	67.21	126.88	1.29	163.59	1.98	0.84	0.84
1.42	67.05	126.57	1.29	163.44	1.98	0.84	0.84
1.43	66.95	126.38	1.29	163.40	1.98	0.84	0.84
1.44	66.90	126.29	1.29	163.47	1.98	0.84	0.84

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
1.45	66.89	126.27	1.30	163.64	1.99	0.84	0.84
1.46	66.88	126.24	1.30	163.83	1.99	0.84	0.84
1.47	66.86	126.22	1.30	164.03	1.99	0.85	0.85
1.48	66.85	126.19	1.30	164.24	1.99	0.85	0.85
1.49	66.84	126.17	1.30	164.44	2.00	0.85	0.85
1.50	66.83	126.14	1.31	164.62	2.00	0.85	0.85
1.51	66.82	126.12	1.31	164.77	2.00	0.85	0.85
1.52	66.80	126.09	1.31	164.89	2.00	0.85	0.85
1.53	66.78	126.06	1.31	164.99	2.00	0.85	0.85
1.54	66.76	126.02	1.31	165.10	2.00	0.85	0.85
1.55	66.73	125.97	1.31	165.22	2.01	0.85	0.85
1.56	66.71	125.91	1.31	165.35	2.01	0.85	0.85
1.57	66.68	125.86	1.31	165.48	2.01	0.85	0.85
1.58	66.66	125.82	1.32	165.60	2.01	0.85	0.85
1.59	66.64	125.77	1.32	165.70	2.01	0.85	0.85
1.60	66.58	125.67	1.32	165.71	2.01	0.85	0.85
1.61	66.47	125.46	1.32	165.56	2.01	0.85	0.85
1.62	66.29	125.12	1.32	165.26	2.02	0.85	0.85
1.63	66.08	124.71	1.32	164.88	2.02	0.85	0.85
1.64	65.84	124.27	1.32	164.48	2.02	0.85	0.85
1.65	65.60	123.81	1.33	164.06	2.02	0.85	0.85
1.66	65.37	123.37	1.33	163.66	2.02	0.84	0.84
1.67	65.15	122.96	1.33	163.28	2.02	0.84	0.84
1.68	64.96	122.60	1.33	162.96	2.02	0.84	0.84
1.69	64.80	122.29	1.33	162.66	2.03	0.84	0.84
1.70	64.63	121.96	1.33	162.33	2.03	0.84	0.84
1.71	64.43	121.59	1.33	161.94	2.03	0.84	0.84
1.72	64.21	121.17	1.33	161.50	2.03	0.84	0.84
1.73	63.97	120.72	1.33	161.03	2.03	0.84	0.84
1.74	63.73	120.26	1.34	160.56	2.03	0.84	0.84
1.75	63.50	119.83	1.34	160.10	2.03	0.84	0.84
1.76	63.29	119.43	1.34	159.69	2.03	0.84	0.84
1.77	63.11	119.08	1.34	159.31	2.03	0.84	0.84
1.78	62.91	118.71	1.34	158.88	2.03	0.84	0.84
1.79	62.68	118.27	1.34	158.35	2.03	0.84	0.84
1.80	62.40	117.74	1.34	157.68	2.04	0.84	0.84
1.81	62.09	117.15	1.34	156.95	2.04	0.84	0.84
1.82	61.76	116.53	1.34	156.18	2.04	0.84	0.84
1.83	61.44	115.92	1.34	155.42	2.04	0.83	0.83
1.84	61.13	115.35	1.34	154.70	2.04	0.83	0.83
1.85	60.87	114.84	1.34	154.07	2.04	0.83	0.83
1.86	60.62	114.36	1.34	153.49	2.04	0.83	0.83
1.87	60.34	113.85	1.34	152.87	2.04	0.83	0.83
1.88	60.02	113.23	1.34	152.13	2.04	0.83	0.83
1.89	59.63	112.50	1.34	151.26	2.04	0.83	0.83
1.90	59.22	111.71	1.35	150.32	2.04	0.83	0.83
1.91	58.79	110.90	1.35	149.36	2.04	0.83	0.83
1.92	58.37	110.12	1.35	148.43	2.04	0.82	0.82

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
1.93	57.99	109.39	1.35	147.57	2.04	0.82	0.82
1.94	57.65	108.76	1.35	146.82	2.05	0.82	0.82
1.95	57.33	108.15	1.35	146.14	2.05	0.82	0.82
1.96	56.98	107.48	1.35	145.44	2.05	0.82	0.82
1.97	56.56	106.68	1.36	144.63	2.05	0.82	0.82
1.98	56.08	105.78	1.36	143.70	2.05	0.82	0.82
1.99	55.57	104.81	1.36	142.73	2.06	0.82	0.82
2.00	55.06	103.84	1.37	141.74	2.06	0.82	0.82
2.01	54.57	102.91	1.37	140.81	2.06	0.81	0.81
2.02	54.12	102.07	1.37	139.96	2.06	0.81	0.81
2.03	53.73	101.33	1.37	139.23	2.07	0.81	0.81
2.04	53.34	100.59	1.38	138.49	2.07	0.81	0.81
2.05	52.90	99.75	1.38	137.65	2.07	0.81	0.81
2.06	52.37	98.75	1.38	136.65	2.07	0.81	0.81
2.07	51.78	97.64	1.39	135.56	2.08	0.81	0.81
2.08	51.17	96.48	1.39	134.42	2.08	0.81	0.81
2.09	50.56	95.33	1.40	133.29	2.09	0.80	0.80
2.10	49.99	94.25	1.40	132.24	2.09	0.80	0.80
2.11	49.49	93.30	1.41	131.32	2.09	0.80	0.80
2.12	49.07	92.52	1.41	130.54	2.09	0.80	0.80
2.13	48.71	91.82	1.41	129.80	2.10	0.80	0.80
2.14	48.33	91.11	1.42	129.01	2.10	0.80	0.80
2.15	47.89	90.29	1.42	128.09	2.10	0.80	0.80
2.16	47.43	89.40	1.42	127.10	2.10	0.79	0.79
2.17	46.94	88.49	1.42	126.09	2.10	0.79	0.79
2.18	46.48	87.60	1.43	125.11	2.11	0.79	0.79
2.19	46.05	86.79	1.43	124.20	2.11	0.79	0.79
2.20	45.68	86.09	1.43	123.44	2.11	0.79	0.79
2.21	45.37	85.51	1.44	122.79	2.11	0.79	0.79
2.22	45.09	84.98	1.44	122.18	2.11	0.79	0.79
2.23	44.79	84.40	1.44	121.52	2.11	0.79	0.79
2.24	44.44	83.75	1.44	120.78	2.12	0.78	0.78
2.25	44.08	83.06	1.44	119.99	2.12	0.78	0.78
2.26	43.71	82.37	1.45	119.20	2.12	0.78	0.78
2.27	43.36	81.70	1.45	118.44	2.12	0.78	0.78
2.28	43.04	81.10	1.45	117.76	2.12	0.78	0.78
2.29	42.78	80.60	1.45	117.18	2.12	0.78	0.78
2.30	42.53	80.14	1.46	116.65	2.12	0.78	0.78
2.31	42.28	79.66	1.46	116.10	2.12	0.78	0.78
2.32	41.99	79.11	1.46	115.47	2.13	0.78	0.78
2.33	41.67	78.49	1.46	114.77	2.13	0.77	0.77
2.34	41.33	77.86	1.46	114.04	2.13	0.77	0.77
2.35	41.00	77.23	1.47	113.32	2.13	0.77	0.77
2.36	40.69	76.64	1.47	112.65	2.13	0.77	0.77
2.37	40.41	76.12	1.47	112.06	2.13	0.77	0.77
2.38	40.19	75.69	1.47	111.56	2.13	0.77	0.77
2.39	39.98	75.30	1.48	111.11	2.13	0.77	0.77
2.40	39.77	74.89	1.48	110.62	2.14	0.77	0.77

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
2.41	39.52	74.43	1.48	110.07	2.14	0.77	0.77
2.42	39.25	73.92	1.48	109.47	2.14	0.77	0.77
2.43	38.98	73.41	1.48	108.86	2.14	0.76	0.76
2.44	38.72	72.91	1.49	108.27	2.14	0.76	0.76
2.45	38.47	72.44	1.49	107.72	2.14	0.76	0.76
2.46	38.26	72.05	1.49	107.26	2.14	0.76	0.76
2.47	38.08	71.69	1.49	106.88	2.14	0.76	0.76
2.48	37.89	71.33	1.49	106.54	2.14	0.76	0.76
2.49	37.67	70.92	1.50	106.18	2.15	0.76	0.76
2.50	37.42	70.45	1.50	105.77	2.15	0.76	0.76
2.51	37.16	69.95	1.51	105.35	2.15	0.76	0.76
2.52	36.90	69.45	1.51	104.92	2.15	0.76	0.76
2.53	36.64	68.98	1.52	104.51	2.16	0.76	0.76
2.54	36.42	68.55	1.52	104.14	2.16	0.76	0.76
2.55	36.21	68.16	1.52	103.80	2.16	0.76	0.76
2.56	35.99	67.74	1.53	103.42	2.16	0.75	0.75
2.57	35.73	67.24	1.53	102.94	2.16	0.75	0.75
2.58	35.41	66.63	1.54	102.36	2.17	0.75	0.75
2.59	35.05	65.96	1.54	101.73	2.17	0.75	0.75
2.60	34.68	65.27	1.55	101.07	2.17	0.75	0.75
2.61	34.32	64.58	1.56	100.42	2.17	0.75	0.75
2.62	33.98	63.93	1.56	99.82	2.18	0.75	0.75
2.63	33.68	63.37	1.57	99.29	2.18	0.75	0.75
2.64	33.42	62.88	1.57	98.82	2.18	0.75	0.75
2.65	33.17	62.40	1.58	98.33	2.18	0.74	0.74
2.66	32.89	61.86	1.58	97.77	2.19	0.74	0.74
2.67	32.56	61.24	1.59	97.13	2.19	0.74	0.74
2.68	32.21	60.57	1.59	96.44	2.19	0.74	0.74
2.69	31.85	59.89	1.60	95.73	2.19	0.74	0.74
2.70	31.50	59.23	1.60	95.05	2.20	0.74	0.74
2.71	31.17	58.62	1.61	94.42	2.20	0.74	0.74
2.72	30.91	58.12	1.62	93.91	2.20	0.74	0.74
2.73	30.75	57.82	1.62	93.56	2.20	0.74	0.74
2.74	30.68	57.68	1.62	93.33	2.20	0.74	0.74
2.75	30.65	57.63	1.62	93.15	2.20	0.73	0.73
2.76	30.62	57.57	1.61	92.95	2.20	0.73	0.73
2.77	30.59	57.51	1.61	92.74	2.20	0.73	0.73
2.78	30.56	57.45	1.61	92.52	2.20	0.73	0.73
2.79	30.53	57.39	1.61	92.32	2.20	0.73	0.73
2.80	30.50	57.34	1.61	92.14	2.20	0.73	0.73
2.81	30.48	57.29	1.61	91.98	2.20	0.73	0.73
2.82	30.46	57.25	1.60	91.83	2.20	0.73	0.73
2.83	30.44	57.21	1.60	91.68	2.20	0.73	0.73
2.84	30.41	57.17	1.60	91.50	2.19	0.73	0.73
2.85	30.39	57.12	1.60	91.30	2.19	0.73	0.73
2.86	30.36	57.07	1.60	91.10	2.19	0.73	0.73
2.87	30.33	57.02	1.59	90.89	2.19	0.73	0.73
2.88	30.31	56.97	1.59	90.71	2.19	0.73	0.73

:: Strength loss calculation (Robertson (2009)) :: (continued)							
Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
2.89	30.29	56.93	1.59	90.54	2.19	0.73	0.73
2.90	30.25	56.86	1.59	90.34	2.19	0.73	0.73
2.91	30.20	56.75	1.59	90.07	2.19	0.73	0.73
2.92	30.11	56.60	1.58	89.69	2.19	0.73	0.73
2.93	30.02	56.41	1.58	89.24	2.19	0.73	0.73
2.94	29.91	56.21	1.58	88.77	2.19	0.73	0.73
2.95	29.81	56.01	1.58	88.28	2.18	0.73	0.73
2.96	29.70	55.81	1.57	87.81	2.18	0.72	0.72
2.97	29.61	55.63	1.57	87.38	2.18	0.72	0.72
2.98	29.50	55.43	1.57	86.98	2.18	0.72	0.72
2.99	29.28	55.02	1.57	86.43	2.18	0.72	0.72
3.00	28.92	54.33	1.58	85.66	2.18	0.72	0.72
3.01	28.41	53.36	1.59	84.64	2.19	0.72	0.72
3.02	27.83	52.27	1.60	83.50	2.19	0.71	0.71
3.03	27.22	51.12	1.61	82.31	2.20	0.71	0.71
3.04	26.61	49.96	1.62	81.12	2.20	0.64	0.71
3.05	26.03	48.86	1.64	80.00	2.21	0.58	0.71
3.06	25.51	47.87	1.65	79.00	2.21	0.54	0.70
3.07	25.05	47.00	1.66	78.18	2.22	0.50	0.70
3.08	24.59	46.14	1.68	77.47	2.22	0.47	0.70
3.09	24.08	45.17	1.70	76.77	2.23	0.45	0.70
3.10	23.47	44.02	1.73	76.00	2.24	0.42	0.70
3.11	22.80	42.76	1.76	75.17	2.25	0.39	0.70
3.12	22.11	41.45	1.79	74.34	2.26	0.36	0.69
3.13	21.43	40.15	1.83	73.54	2.27	0.34	0.69
3.14	20.79	38.95	1.87	72.81	2.29	0.32	0.69
3.15	20.23	37.89	1.91	72.20	2.29	0.31	0.69
3.16	19.88	37.22	1.93	71.82	2.30	0.30	0.69
3.17	19.72	36.92	1.94	71.65	2.30	0.29	0.69
3.18	19.71	36.91	1.94	71.65	2.30	0.29	0.69
3.19	19.71	36.91	1.94	71.65	2.30	0.29	0.69
3.20	19.71	36.91	1.94	71.65	2.30	0.29	0.69
3.21	19.71	36.91	1.94	71.65	2.30	0.29	0.69
3.22	19.71	36.90	1.94	71.65	2.30	0.29	0.69
3.23	19.71	36.90	1.94	71.65	2.30	0.29	0.69
3.24	19.72	36.91	1.94	71.64	2.30	0.29	0.69
3.25	19.74	36.95	1.94	71.58	2.30	0.29	0.69
3.26	19.79	37.04	1.93	71.48	2.30	0.29	0.69
3.27	19.85	37.16	1.92	71.32	2.30	0.28	0.69
3.28	19.93	37.31	1.91	71.15	2.30	0.28	0.69
3.29	20.01	37.46	1.89	70.96	2.29	0.28	0.69
3.30	20.09	37.60	1.88	70.78	2.29	0.27	0.69
3.31	20.16	37.75	1.87	70.61	2.29	0.27	0.68
3.32	20.23	37.87	1.86	70.46	2.28	0.26	0.68
3.33	20.28	37.96	1.85	70.31	2.28	0.26	0.68
3.34	20.30	38.01	1.85	70.16	2.28	0.26	0.68
3.35	20.31	38.02	1.84	69.96	2.28	0.25	0.68
3.36	20.31	38.02	1.83	69.72	2.27	0.25	0.68

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
3.37	20.31	38.02	1.83	69.47	2.27	0.24	0.68
3.38	20.31	38.02	1.82	69.20	2.27	0.24	0.68
3.39	20.31	38.02	1.81	68.94	2.27	0.23	0.68
3.40	20.31	38.01	1.81	68.69	2.27	0.23	0.68
3.41	20.31	38.01	1.80	68.48	2.27	0.22	0.68
3.42	20.31	38.01	1.80	68.37	2.26	0.22	0.68
3.43	20.31	38.01	1.80	68.35	2.26	0.22	0.68
3.44	20.31	38.01	1.80	68.42	2.26	0.22	0.68
3.45	20.31	38.01	1.80	68.50	2.27	0.23	0.68
3.46	20.31	38.01	1.80	68.59	2.27	0.23	0.68
3.47	20.31	38.01	1.81	68.67	2.27	0.23	0.68
3.48	20.31	38.01	1.81	68.76	2.27	0.23	0.68
3.49	20.31	38.01	1.81	68.84	2.27	0.23	0.68
3.50	20.32	38.02	1.81	68.92	2.27	0.23	0.68
3.51	20.37	38.11	1.81	69.06	2.27	0.24	0.68
3.52	20.46	38.29	1.81	69.29	2.27	0.24	0.68
3.53	20.59	38.54	1.81	69.59	2.27	0.25	0.68
3.54	20.75	38.82	1.80	69.93	2.27	0.25	0.68
3.55	20.90	39.12	1.80	70.29	2.26	0.26	0.68
3.56	21.06	39.42	1.79	70.65	2.26	0.27	0.68
3.57	21.22	39.71	1.79	70.99	2.26	0.28	0.69
3.58	21.35	39.96	1.78	71.30	2.26	0.28	0.69
3.59	21.48	40.20	1.78	71.53	2.26	0.29	0.69
3.60	21.62	40.47	1.77	71.68	2.26	0.29	0.69
3.61	21.79	40.80	1.76	71.78	2.25	0.30	0.69
3.62	22.01	41.20	1.74	71.88	2.25	0.30	0.69
3.63	22.24	41.64	1.73	72.00	2.24	0.30	0.69
3.64	22.48	42.09	1.71	72.12	2.24	0.30	0.69
3.65	22.71	42.53	1.70	72.25	2.23	0.31	0.69
3.66	22.93	42.95	1.68	72.37	2.23	0.31	0.69
3.67	23.13	43.31	1.67	72.48	2.22	0.31	0.69
3.68	23.28	43.60	1.66	72.55	2.22	0.31	0.69
3.69	23.41	43.84	1.66	72.61	2.22	0.32	0.69
3.70	23.54	44.08	1.65	72.64	2.21	0.32	0.69
3.71	23.68	44.36	1.64	72.68	2.21	0.32	0.69
3.72	23.84	44.65	1.63	72.72	2.21	0.32	0.69
3.73	24.00	44.96	1.62	72.77	2.20	0.32	0.69
3.74	24.15	45.25	1.61	72.83	2.20	0.32	0.69
3.75	24.30	45.51	1.60	72.87	2.19	0.32	0.69
3.76	24.42	45.75	1.59	72.95	2.19	0.32	0.69
3.77	24.56	46.00	1.59	73.12	2.19	0.33	0.69
3.78	24.72	46.31	1.59	73.42	2.19	0.34	0.69
3.79	24.92	46.69	1.58	73.84	2.19	0.35	0.69
3.80	25.15	47.12	1.58	74.31	2.18	0.36	0.69
3.81	25.39	47.57	1.57	74.81	2.18	0.38	0.70
3.82	25.63	48.02	1.57	75.31	2.18	0.40	0.70
3.83	25.85	48.45	1.56	75.78	2.18	0.41	0.70
3.84	26.06	48.83	1.56	76.21	2.18	0.43	0.70

:: Strength loss calculation (Robertson (2009)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
3.85	26.28	49.26	1.56	76.65	2.18	0.44	0.70
3.86	26.59	49.85	1.55	77.22	2.17	0.46	0.70
3.87	27.04	50.68	1.54	77.99	2.17	0.49	0.70
3.88	27.58	51.70	1.53	78.93	2.16	0.53	0.70
3.89	28.17	52.82	1.51	79.98	2.16	0.58	0.71
3.90	28.78	53.98	1.50	81.08	2.15	0.64	0.71
3.91	29.39	55.12	1.49	82.17	2.14	0.70	0.71
3.92	29.95	56.18	1.48	83.19	2.14	0.71	0.71
3.93	30.44	57.10	1.47	84.09	2.13	0.72	0.72
3.94	30.83	57.85	1.47	84.78	2.13	0.72	0.72
3.95	31.19	58.52	1.46	85.35	2.13	0.72	0.72
3.96	31.55	59.20	1.45	85.89	2.12	0.72	0.72
3.97	31.97	59.99	1.44	86.51	2.12	0.72	0.72
3.98	32.41	60.83	1.43	87.19	2.11	0.72	0.72
3.99	32.87	61.69	1.42	87.89	2.10	0.72	0.72
4.00	33.30	62.51	1.42	88.57	2.10	0.73	0.73
4.01	33.70	63.27	1.41	89.20	2.09	0.73	0.73
4.02	34.01	63.85	1.40	89.69	2.09	0.73	0.73
4.03	34.19	64.18	1.40	89.95	2.09	0.73	0.73
4.04	34.25	64.30	1.40	90.00	2.09	0.73	0.73
4.05	34.25	64.29	1.40	89.95	2.09	0.73	0.73
4.06	34.25	64.29	1.40	89.88	2.09	0.73	0.73
4.07	34.25	64.29	1.40	89.82	2.08	0.73	0.73
4.08	34.25	64.29	1.40	89.75	2.08	0.73	0.73
4.09	34.25	64.29	1.40	89.69	2.08	0.73	0.73
4.10	34.25	64.29	1.39	89.64	2.08	0.73	0.73
4.11	34.25	64.29	1.39	89.61	2.08	0.73	0.73
4.12	34.25	64.29	1.39	89.61	2.08	0.73	0.73
4.13	34.25	64.29	1.39	89.65	2.08	0.73	0.73
4.14	34.25	64.28	1.40	89.71	2.08	0.73	0.73
4.15	34.25	64.28	1.40	89.77	2.08	0.73	0.73
4.16	34.25	64.28	1.40	89.84	2.08	0.73	0.73
4.17	34.25	64.28	1.40	89.90	2.09	0.73	0.73
4.18	34.25	64.28	1.40	89.96	2.09	0.73	0.73
4.19	34.25	64.28	1.40	90.01	2.09	0.73	0.73
4.20	34.25	64.28	1.40	90.09	2.09	0.73	0.73
4.21	34.25	64.28	1.40	90.20	2.09	0.73	0.73
4.22	34.25	64.28	1.41	90.36	2.09	0.73	0.73
4.23	34.25	64.28	1.41	90.55	2.09	0.73	0.73
4.24	34.25	64.27	1.41	90.74	2.10	0.73	0.73
4.25	34.25	64.27	1.41	90.95	2.10	0.73	0.73
4.26	34.25	64.27	1.42	91.14	2.10	0.73	0.73
4.27	34.25	64.27	1.42	91.32	2.10	0.73	0.73
4.28	34.25	64.26	1.42	91.47	2.10	0.73	0.73
4.29	34.23	64.23	1.43	91.58	2.10	0.73	0.73
4.30	34.20	64.17	1.43	91.68	2.11	0.73	0.73
4.31	34.15	64.08	1.43	91.78	2.11	0.73	0.73
4.32	34.10	63.99	1.44	91.89	2.11	0.73	0.73

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
4.33	34.05	63.88	1.44	92.02	2.11	0.73	0.73
4.34	33.99	63.78	1.44	92.14	2.12	0.73	0.73
4.35	33.94	63.69	1.45	92.26	2.12	0.73	0.73
4.36	33.90	63.60	1.45	92.36	2.12	0.73	0.73
4.37	33.88	63.56	1.45	92.46	2.12	0.73	0.73
4.38	33.89	63.58	1.46	92.57	2.12	0.73	0.73
4.39	33.94	63.67	1.46	92.71	2.12	0.73	0.73
4.40	33.99	63.78	1.46	92.87	2.12	0.73	0.73
4.41	34.06	63.90	1.46	93.05	2.12	0.73	0.73
4.42	34.13	64.02	1.46	93.23	2.12	0.74	0.74
4.43	34.19	64.15	1.46	93.41	2.12	0.74	0.74
4.44	34.25	64.26	1.46	93.58	2.12	0.74	0.74
4.45	34.31	64.36	1.46	93.73	2.12	0.74	0.74
4.46	34.39	64.52	1.46	93.91	2.12	0.74	0.74
4.47	34.53	64.78	1.45	94.14	2.12	0.74	0.74
4.48	34.72	65.14	1.45	94.47	2.12	0.74	0.74
4.49	34.94	65.56	1.45	94.84	2.12	0.74	0.74
4.50	35.18	66.01	1.44	95.24	2.12	0.74	0.74
4.51	35.42	66.46	1.44	95.64	2.11	0.74	0.74
4.52	35.65	66.90	1.44	96.04	2.11	0.74	0.74
4.53	35.86	67.29	1.43	96.40	2.11	0.74	0.74
4.54	36.04	67.63	1.43	96.71	2.11	0.74	0.74
4.55	36.22	67.96	1.43	97.00	2.11	0.74	0.74
4.56	36.41	68.32	1.42	97.33	2.10	0.74	0.74
4.57	36.63	68.74	1.42	97.72	2.10	0.74	0.74
4.58	36.88	69.22	1.42	98.15	2.10	0.74	0.74
4.59	37.15	69.71	1.41	98.61	2.10	0.75	0.75
4.60	37.41	70.21	1.41	99.07	2.09	0.75	0.75
4.61	37.66	70.67	1.41	99.50	2.09	0.75	0.75
4.62	37.88	71.09	1.41	99.89	2.09	0.75	0.75
4.63	38.09	71.49	1.40	100.24	2.09	0.75	0.75
4.64	38.33	71.94	1.40	100.61	2.09	0.75	0.75
4.65	38.63	72.50	1.39	101.05	2.08	0.75	0.75
4.66	38.98	73.18	1.39	101.57	2.08	0.75	0.75
4.67	39.37	73.91	1.38	102.14	2.07	0.75	0.75
4.68	39.77	74.66	1.38	102.74	2.07	0.75	0.75
4.69	40.16	75.40	1.37	103.33	2.06	0.75	0.75
4.70	40.53	76.09	1.37	103.89	2.06	0.76	0.76
4.71	40.84	76.69	1.36	104.37	2.06	0.76	0.76
4.72	41.13	77.22	1.36	104.81	2.05	0.76	0.76
4.73	41.42	77.77	1.35	105.26	2.05	0.76	0.76
4.74	41.75	78.41	1.35	105.80	2.04	0.76	0.76
4.75	42.14	79.13	1.34	106.41	2.04	0.76	0.76
4.76	42.55	79.91	1.34	107.06	2.04	0.76	0.76
4.77	42.96	80.69	1.34	107.73	2.03	0.76	0.76
4.78	43.36	81.45	1.33	108.38	2.03	0.76	0.76
4.79	43.73	82.13	1.33	108.98	2.02	0.76	0.76
4.80	44.04	82.73	1.32	109.51	2.02	0.77	0.77

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
4.81	44.35	83.31	1.32	110.06	2.02	0.77	0.77
4.82	44.70	83.96	1.32	110.71	2.01	0.77	0.77
4.83	45.11	84.73	1.32	111.50	2.01	0.77	0.77
4.84	45.56	85.60	1.31	112.38	2.01	0.77	0.77
4.85	46.04	86.50	1.31	113.31	2.00	0.77	0.77
4.86	46.52	87.40	1.31	114.24	2.00	0.77	0.77
4.87	46.97	88.25	1.30	115.11	2.00	0.77	0.77
4.88	47.37	89.00	1.30	115.89	1.99	0.78	0.78
4.89	47.73	89.69	1.30	116.61	1.99	0.78	0.78
4.90	48.12	90.42	1.30	117.36	1.99	0.78	0.78
4.91	48.58	91.29	1.30	118.27	1.99	0.78	0.78
4.92	49.12	92.32	1.29	119.33	1.98	0.78	0.78
4.93	49.72	93.43	1.29	120.50	1.98	0.78	0.78
4.94	50.32	94.58	1.29	121.70	1.97	0.79	0.79
4.95	50.92	95.71	1.28	122.87	1.97	0.79	0.79
4.96	51.47	96.75	1.28	123.96	1.97	0.79	0.79
4.97	51.94	97.64	1.28	124.90	1.96	0.79	0.79
4.98	52.33	98.37	1.28	125.66	1.96	0.79	0.79
4.99	52.67	99.02	1.28	126.34	1.96	0.79	0.79
5.00	53.03	99.69	1.27	127.05	1.96	0.79	0.79
5.01	53.44	100.46	1.27	127.85	1.95	0.80	0.80
5.02	53.87	101.28	1.27	128.71	1.95	0.80	0.80
5.03	54.31	102.11	1.27	129.58	1.95	0.80	0.80
5.04	54.74	102.91	1.27	130.42	1.95	0.80	0.80
5.05	55.12	103.63	1.27	131.17	1.94	0.80	0.80
5.06	55.42	104.20	1.26	131.76	1.94	0.80	0.80
5.07	55.62	104.59	1.26	132.13	1.94	0.80	0.80
5.08	55.76	104.84	1.26	132.33	1.94	0.80	0.80
5.09	55.88	105.07	1.26	132.47	1.94	0.80	0.80
5.10	56.01	105.31	1.26	132.62	1.93	0.80	0.80
5.11	56.15	105.57	1.26	132.79	1.93	0.80	0.80
5.12	56.29	105.83	1.26	132.95	1.93	0.80	0.80
5.13	56.42	106.08	1.25	133.10	1.93	0.80	0.80
5.14	56.53	106.29	1.25	133.23	1.93	0.80	0.80
5.15	56.62	106.47	1.25	133.34	1.92	0.80	0.80
5.16	56.70	106.61	1.25	133.44	1.92	0.80	0.80
5.17	56.77	106.75	1.25	133.53	1.92	0.80	0.80
5.18	56.86	106.91	1.25	133.65	1.92	0.80	0.80
5.19	56.95	107.08	1.25	133.77	1.92	0.80	0.80
5.20	57.04	107.25	1.25	133.89	1.92	0.80	0.80
5.21	57.13	107.42	1.25	134.01	1.92	0.80	0.80
5.22	57.22	107.58	1.25	134.13	1.91	0.80	0.80
5.23	57.29	107.72	1.25	134.23	1.91	0.80	0.80
5.24	57.37	107.86	1.25	134.38	1.91	0.80	0.80
5.25	57.45	108.03	1.25	134.60	1.91	0.81	0.81
5.26	57.56	108.23	1.25	134.90	1.91	0.81	0.81
5.27	57.69	108.46	1.25	135.25	1.92	0.81	0.81
5.28	57.82	108.71	1.25	135.62	1.92	0.81	0.81

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
5.29	57.95	108.96	1.25	135.99	1.92	0.81	0.81
5.30	58.08	109.20	1.25	136.35	1.92	0.81	0.81
5.31	58.19	109.42	1.25	136.68	1.92	0.81	0.81
5.32	58.27	109.56	1.25	136.92	1.92	0.81	0.81
5.33	58.28	109.58	1.25	137.03	1.92	0.81	0.81
5.34	58.23	109.48	1.25	137.05	1.92	0.81	0.81
5.35	58.14	109.31	1.25	137.01	1.93	0.81	0.81
5.36	58.04	109.12	1.26	136.97	1.93	0.81	0.81
5.37	57.93	108.91	1.26	136.93	1.93	0.81	0.81
5.38	57.82	108.71	1.26	136.88	1.93	0.81	0.81
5.39	57.73	108.52	1.26	136.84	1.94	0.81	0.81
5.40	57.64	108.36	1.26	136.80	1.94	0.81	0.81
5.41	57.56	108.20	1.26	136.74	1.94	0.81	0.81
5.42	57.47	108.04	1.26	136.66	1.94	0.81	0.81
5.43	57.37	107.85	1.27	136.54	1.94	0.81	0.81
5.44	57.25	107.62	1.27	136.40	1.95	0.81	0.81
5.45	57.12	107.37	1.27	136.25	1.95	0.81	0.81
5.46	56.99	107.12	1.27	136.09	1.95	0.81	0.81
5.47	56.86	106.87	1.27	135.94	1.95	0.81	0.81
5.48	56.74	106.64	1.27	135.79	1.95	0.81	0.81
5.49	56.64	106.45	1.27	135.67	1.96	0.81	0.81
5.50	56.58	106.34	1.28	135.60	1.96	0.81	0.81
5.51	56.55	106.29	1.28	135.57	1.96	0.81	0.81
5.52	56.55	106.29	1.28	135.57	1.96	0.81	0.81
5.53	56.55	106.29	1.28	135.57	1.96	0.81	0.81
5.54	56.55	106.29	1.28	135.57	1.96	0.81	0.81
5.55	56.55	106.29	1.28	135.57	1.96	0.81	0.81
5.56	56.55	106.29	1.28	135.57	1.96	0.81	0.81
5.57	56.55	106.29	1.28	135.57	1.96	0.81	0.81
5.58	56.54	106.26	1.28	135.55	1.96	0.81	0.81
5.59	56.50	106.19	1.28	135.47	1.96	0.81	0.81
5.60	56.44	106.07	1.28	135.34	1.96	0.81	0.81
5.61	56.34	105.89	1.28	135.15	1.96	0.81	0.81
5.62	56.24	105.70	1.28	134.95	1.96	0.81	0.81
5.63	56.14	105.49	1.28	134.74	1.96	0.81	0.81
5.64	56.03	105.29	1.28	134.53	1.96	0.81	0.81
5.65	55.93	105.10	1.28	134.33	1.96	0.80	0.80
5.66	55.84	104.94	1.28	134.15	1.96	0.80	0.80
5.67	55.77	104.79	1.28	134.01	1.96	0.80	0.80
5.68	55.69	104.65	1.28	133.88	1.96	0.80	0.80
5.69	55.61	104.49	1.28	133.76	1.96	0.80	0.80
5.70	55.51	104.31	1.28	133.62	1.97	0.80	0.80
5.71	55.41	104.11	1.28	133.46	1.97	0.80	0.80
5.72	55.30	103.91	1.28	133.30	1.97	0.80	0.80
5.73	55.20	103.71	1.28	133.15	1.97	0.80	0.80
5.74	55.10	103.53	1.28	133.00	1.97	0.80	0.80
5.75	55.02	103.38	1.29	132.89	1.97	0.80	0.80
5.76	54.98	103.29	1.29	132.83	1.97	0.80	0.80

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
5.77	54.96	103.25	1.29	132.83	1.97	0.80	0.80
5.78	54.96	103.25	1.29	132.87	1.97	0.80	0.80
5.79	54.96	103.25	1.29	132.92	1.97	0.80	0.80
5.80	54.96	103.25	1.29	132.98	1.98	0.80	0.80
5.81	54.96	103.25	1.29	133.03	1.98	0.80	0.80
5.82	54.96	103.25	1.29	133.08	1.98	0.80	0.80
5.83	54.96	103.25	1.29	133.13	1.98	0.80	0.80
5.84	54.96	103.25	1.29	133.15	1.98	0.80	0.80
5.85	54.96	103.24	1.29	133.15	1.98	0.80	0.80
5.86	54.96	103.24	1.29	133.12	1.98	0.80	0.80
5.87	54.96	103.24	1.29	133.07	1.98	0.80	0.80
5.88	54.96	103.24	1.29	133.02	1.98	0.80	0.80
5.89	54.96	103.24	1.29	132.97	1.98	0.80	0.80
5.90	54.96	103.24	1.29	132.91	1.97	0.80	0.80
5.91	54.96	103.24	1.29	132.86	1.97	0.80	0.80
5.92	54.96	103.24	1.29	132.82	1.97	0.80	0.80
5.93	54.96	103.24	1.29	132.80	1.97	0.80	0.80
5.94	54.96	103.23	1.29	132.81	1.97	0.80	0.80
5.95	54.96	103.23	1.29	132.84	1.97	0.80	0.80
5.96	54.96	103.23	1.29	132.89	1.97	0.80	0.80
5.97	54.96	103.23	1.29	132.94	1.98	0.80	0.80
5.98	54.96	103.23	1.29	133.00	1.98	0.80	0.80
5.99	54.96	103.22	1.29	133.04	1.98	0.80	0.80
6.00	54.96	103.15	1.29	133.01	1.98	0.80	0.80
6.01	54.96	103.08	1.29	132.98	1.98	0.80	0.80
6.02	54.96	103.01	1.29	132.97	1.98	0.80	0.80
6.03	54.96	102.95	1.29	132.97	1.98	0.80	0.80
6.04	54.96	102.90	1.29	133.01	1.98	0.80	0.80
6.05	54.96	102.86	1.29	133.07	1.98	0.80	0.80
6.06	54.96	102.82	1.29	133.14	1.98	0.80	0.80
6.07	54.96	102.78	1.30	133.21	1.99	0.80	0.80
6.08	54.96	102.74	1.30	133.27	1.99	0.80	0.80
6.09	54.96	102.69	1.30	133.31	1.99	0.80	0.80
6.10	54.97	102.66	1.30	133.34	1.99	0.80	0.80
6.11	55.02	102.65	1.30	133.38	1.99	0.80	0.80
6.12	55.09	102.70	1.30	133.43	1.99	0.80	0.80
6.13	55.20	102.78	1.30	133.52	1.99	0.80	0.80
6.14	55.31	102.88	1.30	133.62	1.99	0.80	0.80
6.15	55.43	102.99	1.30	133.74	1.99	0.80	0.80
6.16	55.55	103.09	1.30	133.85	1.99	0.80	0.80
6.17	55.66	103.18	1.30	133.94	1.99	0.80	0.80
6.18	55.76	103.25	1.30	134.02	1.99	0.80	0.80
6.19	55.89	103.37	1.30	134.11	1.99	0.80	0.80
6.20	56.08	103.56	1.30	134.27	1.99	0.80	0.80
6.21	56.35	103.88	1.29	134.52	1.98	0.81	0.81
6.22	56.67	104.26	1.29	134.82	1.98	0.81	0.81
6.23	57.01	104.68	1.29	135.16	1.98	0.81	0.81
6.24	57.36	105.12	1.29	135.50	1.98	0.81	0.81

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
6.25	57.71	105.53	1.29	135.83	1.97	0.81	0.81
6.26	58.02	105.91	1.29	136.13	1.97	0.81	0.81
6.27	58.31	106.25	1.28	136.40	1.97	0.81	0.81
6.28	58.66	106.69	1.28	136.80	1.97	0.81	0.81
6.29	59.14	107.34	1.28	137.40	1.96	0.81	0.81
6.30	59.77	108.22	1.28	138.24	1.96	0.81	0.81
6.31	60.48	109.22	1.27	139.19	1.96	0.81	0.81
6.32	61.24	110.29	1.27	140.20	1.95	0.81	0.81
6.33	61.99	111.35	1.27	141.22	1.95	0.81	0.81
6.34	62.72	112.36	1.27	142.18	1.94	0.82	0.82
6.35	63.37	113.26	1.26	143.03	1.94	0.82	0.82
6.36	63.96	114.06	1.26	143.80	1.94	0.82	0.82
6.37	64.57	114.93	1.26	144.67	1.93	0.82	0.82
6.38	65.30	115.98	1.26	145.77	1.93	0.82	0.82
6.39	66.18	117.28	1.25	147.12	1.93	0.82	0.82
6.40	67.15	118.71	1.25	148.62	1.92	0.83	0.83
6.41	68.15	120.20	1.25	150.18	1.92	0.83	0.83
6.42	69.15	121.67	1.25	151.71	1.92	0.83	0.83
6.43	70.08	123.04	1.24	153.12	1.91	0.83	0.83
6.44	70.90	124.22	1.24	154.35	1.91	0.83	0.83
6.45	71.61	125.22	1.24	155.39	1.91	0.83	0.83
6.46	72.29	126.02	1.24	156.21	1.90	0.84	0.84
6.47	73.05	127.09	1.24	157.32	1.90	0.84	0.84
6.48	73.92	128.34	1.24	158.60	1.90	0.84	0.84
6.49	74.86	129.69	1.23	159.98	1.89	0.84	0.84
6.50	75.82	131.07	1.23	161.39	1.89	0.84	0.84
6.51	76.75	132.41	1.23	162.75	1.89	0.84	0.84
6.52	77.61	133.62	1.23	163.98	1.89	0.85	0.85
6.53	78.34	134.64	1.23	165.00	1.88	0.85	0.85
6.54	78.96	135.48	1.22	165.86	1.88	0.85	0.85
6.55	79.56	136.29	1.22	166.67	1.88	0.85	0.85
6.56	80.23	137.20	1.22	167.58	1.88	0.85	0.85
6.57	80.98	138.24	1.22	168.62	1.88	0.85	0.85
6.58	81.77	139.34	1.22	169.72	1.87	0.85	0.85
6.59	82.57	140.45	1.22	170.81	1.87	0.85	0.85
6.60	83.33	141.49	1.21	171.85	1.87	0.85	0.85
6.61	84.01	142.42	1.21	172.76	1.87	0.86	0.86
6.62	84.56	143.14	1.21	173.47	1.86	0.86	0.86
6.63	85.00	143.69	1.21	174.00	1.86	0.86	0.86
6.64	85.38	144.15	1.21	174.46	1.86	0.86	0.86
6.65	85.80	144.68	1.21	174.97	1.86	0.86	0.86
6.66	86.26	145.26	1.21	175.54	1.86	0.86	0.86
6.67	86.74	145.87	1.21	176.13	1.86	0.86	0.86
6.68	87.22	146.47	1.21	176.71	1.86	0.86	0.86
6.69	87.66	147.02	1.21	177.24	1.86	0.86	0.86
6.70	88.05	147.49	1.20	177.70	1.86	0.86	0.86
6.71	88.31	147.77	1.20	177.99	1.85	0.86	0.86
6.72	88.46	147.90	1.20	178.15	1.85	0.86	0.86

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
6.73	88.53	147.92	1.20	178.24	1.86	0.86	0.86
6.74	88.60	147.95	1.21	178.35	1.86	0.86	0.86
6.75	88.68	147.99	1.21	178.47	1.86	0.86	0.86
6.76	88.76	148.03	1.21	178.60	1.86	0.86	0.86
6.77	88.84	148.07	1.21	178.72	1.86	0.86	0.86
6.78	88.91	148.09	1.21	178.82	1.86	0.86	0.86
6.79	88.95	148.07	1.21	178.88	1.86	0.86	0.86
6.80	88.92	147.94	1.21	178.83	1.86	0.86	0.86
6.81	88.79	147.69	1.21	178.70	1.86	0.86	0.86
6.82	88.59	147.34	1.21	178.49	1.86	0.86	0.86
6.83	88.37	146.95	1.21	178.27	1.87	0.86	0.86
6.84	88.13	146.55	1.21	178.04	1.87	0.86	0.86
6.85	87.89	146.15	1.22	177.80	1.87	0.86	0.86
6.86	87.66	145.76	1.22	177.56	1.87	0.86	0.86
6.87	87.46	145.41	1.22	177.34	1.87	0.86	0.86
6.88	87.26	145.06	1.22	177.11	1.88	0.86	0.86
6.89	87.04	144.67	1.22	176.85	1.88	0.86	0.86
6.90	86.75	144.20	1.22	176.53	1.88	0.86	0.86
6.91	86.40	143.65	1.23	176.17	1.88	0.86	0.86
6.92	86.01	143.06	1.23	175.77	1.89	0.86	0.86
6.93	85.61	142.45	1.23	175.36	1.89	0.86	0.86
6.94	85.22	141.84	1.23	174.94	1.89	0.86	0.86
6.95	84.85	141.27	1.24	174.53	1.90	0.86	0.86
6.96	84.53	140.75	1.24	174.16	1.90	0.86	0.86
6.97	84.25	140.27	1.24	173.80	1.90	0.86	0.86
6.98	83.97	139.79	1.24	173.40	1.91	0.86	0.86
6.99	83.65	139.26	1.24	172.95	1.91	0.86	0.86
7.00	83.29	138.66	1.24	172.43	1.91	0.86	0.86
7.01	82.89	138.02	1.25	171.89	1.91	0.85	0.85
7.02	82.49	137.37	1.25	171.33	1.92	0.85	0.85
7.03	82.10	136.73	1.25	170.79	1.92	0.85	0.85
7.04	81.75	136.14	1.25	170.28	1.92	0.85	0.85
7.05	81.46	135.64	1.25	169.84	1.92	0.85	0.85
7.06	81.25	135.26	1.25	169.52	1.92	0.85	0.85
7.07	81.10	134.97	1.25	169.30	1.93	0.85	0.85
7.08	80.96	134.71	1.26	169.13	1.93	0.85	0.85
7.09	80.81	134.43	1.26	168.95	1.93	0.85	0.85
7.10	80.66	134.15	1.26	168.76	1.93	0.85	0.85
7.11	80.50	133.86	1.26	168.57	1.93	0.85	0.85
7.12	80.34	133.58	1.26	168.38	1.94	0.85	0.85
7.13	80.21	133.31	1.26	168.20	1.94	0.85	0.85
7.14	80.14	133.15	1.26	168.09	1.94	0.85	0.85
7.15	80.19	133.12	1.26	168.10	1.94	0.85	0.85
7.16	80.34	133.25	1.26	168.25	1.94	0.85	0.85
7.17	80.55	133.46	1.26	168.47	1.94	0.85	0.85
7.18	80.78	133.70	1.26	168.73	1.94	0.85	0.85
7.19	81.02	133.96	1.26	169.00	1.94	0.85	0.85
7.20	81.26	134.21	1.26	169.26	1.94	0.85	0.85

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
7.21	81.48	134.43	1.26	169.50	1.94	0.85	0.85
7.22	81.67	134.62	1.26	169.70	1.94	0.85	0.85
7.23	81.89	134.83	1.26	169.90	1.94	0.85	0.85
7.24	82.17	135.12	1.26	170.15	1.93	0.85	0.85
7.25	82.55	135.53	1.26	170.50	1.93	0.85	0.85
7.26	82.99	136.03	1.26	170.92	1.93	0.85	0.85
7.27	83.46	136.57	1.25	171.37	1.93	0.85	0.85
7.28	83.94	137.12	1.25	171.83	1.92	0.85	0.85
7.29	84.41	137.65	1.25	172.27	1.92	0.86	0.86
7.30	84.83	138.12	1.25	172.66	1.92	0.86	0.86
7.31	85.21	138.52	1.25	172.99	1.92	0.86	0.86
7.32	85.59	138.94	1.25	173.34	1.92	0.86	0.86
7.33	86.03	139.44	1.25	173.77	1.91	0.86	0.86
7.34	86.56	140.07	1.24	174.33	1.91	0.86	0.86
7.35	87.17	140.80	1.24	174.97	1.91	0.86	0.86
7.36	87.80	141.56	1.24	175.64	1.91	0.86	0.86
7.37	88.44	142.33	1.24	176.31	1.90	0.86	0.86
7.38	89.05	143.05	1.24	176.93	1.90	0.86	0.86
7.39	89.59	143.68	1.24	177.47	1.90	0.86	0.86
7.40	90.06	144.22	1.23	177.93	1.90	0.86	0.86
7.41	90.54	144.76	1.23	178.39	1.89	0.86	0.86
7.42	91.08	145.39	1.23	178.93	1.89	0.86	0.86
7.43	91.71	146.14	1.23	179.58	1.89	0.86	0.86
7.44	92.41	146.98	1.23	180.30	1.88	0.86	0.86
7.45	93.13	147.85	1.22	181.03	1.88	0.87	0.87
7.46	93.83	148.70	1.22	181.74	1.88	0.87	0.87
7.47	94.49	149.49	1.22	182.39	1.88	0.87	0.87
7.48	95.07	150.15	1.22	182.94	1.87	0.87	0.87
7.49	95.56	150.71	1.22	183.42	1.87	0.87	0.87
7.50	96.03	151.26	1.22	183.93	1.87	0.87	0.87
7.51	96.54	151.88	1.22	184.55	1.87	0.87	0.87
7.52	97.13	152.62	1.21	185.27	1.87	0.87	0.87
7.53	97.75	153.41	1.21	186.06	1.87	0.87	0.87
7.54	98.39	154.21	1.21	186.85	1.86	0.87	0.87
7.55	99.01	154.98	1.21	187.61	1.86	0.87	0.87
7.56	99.58	155.68	1.21	188.29	1.86	0.87	0.87
7.57	100.07	156.27	1.21	188.87	1.86	0.87	0.87
7.58	100.54	156.82	1.21	189.41	1.86	0.88	0.88
7.59	101.05	157.43	1.21	190.01	1.86	0.88	0.88
7.60	101.65	158.18	1.21	190.74	1.86	0.88	0.88
7.61	102.33	159.04	1.20	191.57	1.85	0.88	0.88
7.62	103.05	159.94	1.20	192.44	1.85	0.88	0.88
7.63	103.77	160.84	1.20	193.31	1.85	0.88	0.88
7.64	104.45	161.69	1.20	194.13	1.85	0.88	0.88
7.65	105.05	162.43	1.20	194.84	1.85	0.88	0.88
7.66	105.55	163.03	1.20	195.44	1.85	0.88	0.88
7.67	105.99	163.56	1.20	196.02	1.85	0.88	0.88
7.68	106.42	164.11	1.20	196.68	1.85	0.88	0.88

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
7.69	106.92	164.75	1.20	197.47	1.85	0.88	0.88
7.70	107.46	165.47	1.20	198.35	1.85	0.89	0.89
7.71	108.02	166.22	1.20	199.26	1.85	0.89	0.89
7.72	108.57	166.95	1.20	200.15	1.85	0.89	0.89
7.73	109.09	167.61	1.20	200.97	1.85	0.89	0.89
7.74	109.53	168.18	1.20	201.67	1.85	0.89	0.89
7.75	109.89	168.62	1.20	202.23	1.85	0.89	0.89
7.76	110.21	168.99	1.20	202.73	1.85	0.89	0.89
7.77	110.53	169.38	1.20	203.26	1.85	0.89	0.89
7.78	110.89	169.84	1.20	203.89	1.85	0.89	0.89
7.79	111.29	170.35	1.20	204.57	1.85	0.89	0.89
7.80	111.69	170.86	1.20	205.26	1.85	0.89	0.89
7.81	112.07	171.35	1.20	205.92	1.85	0.89	0.89
7.82	112.43	171.78	1.20	206.51	1.85	0.89	0.89
7.83	112.72	172.13	1.20	206.98	1.85	0.89	0.89
7.84	112.98	172.39	1.20	207.30	1.85	0.89	0.89
7.85	113.22	172.62	1.20	207.55	1.85	0.89	0.89
7.86	113.49	172.87	1.20	207.80	1.85	0.90	0.90
7.87	113.79	173.18	1.20	208.09	1.85	0.90	0.90
7.88	114.11	173.50	1.20	208.41	1.85	0.90	0.90
7.89	114.43	173.82	1.20	208.72	1.85	0.90	0.90
7.90	114.73	174.12	1.20	209.01	1.85	0.90	0.90
7.91	115.00	174.38	1.20	209.25	1.85	0.90	0.90
7.92	115.18	174.52	1.20	209.40	1.85	0.90	0.90
7.93	115.28	174.54	1.20	209.46	1.85	0.90	0.90
7.94	115.30	174.47	1.20	209.47	1.85	0.90	0.90
7.95	115.30	174.38	1.20	209.47	1.85	0.90	0.90
7.96	115.30	174.29	1.20	209.48	1.85	0.90	0.90
7.97	115.30	174.21	1.20	209.49	1.85	0.90	0.90
7.98	115.30	174.12	1.20	209.50	1.85	0.90	0.90
7.99	115.30	174.03	1.20	209.50	1.85	0.90	0.90
8.00	115.30	173.94	1.20	209.49	1.85	0.90	0.90
8.01	115.30	173.91	1.20	209.55	1.86	0.90	0.90
8.02	115.30	173.89	1.21	209.64	1.86	0.90	0.90
8.03	115.30	173.88	1.21	209.79	1.86	0.90	0.90
8.04	115.30	173.88	1.21	209.96	1.86	0.90	0.90
8.05	115.30	173.89	1.21	210.14	1.86	0.90	0.90
8.06	115.30	173.89	1.21	210.33	1.86	0.90	0.90
8.07	115.30	173.90	1.21	210.51	1.86	0.90	0.90
8.08	115.30	173.89	1.21	210.66	1.86	0.90	0.90
8.09	115.32	173.91	1.21	210.79	1.86	0.90	0.90
8.10	115.42	174.00	1.21	210.92	1.86	0.90	0.90
8.11	115.61	174.19	1.21	211.08	1.86	0.90	0.90
8.12	115.89	174.48	1.21	211.29	1.86	0.90	0.90
8.13	116.19	174.81	1.21	211.54	1.86	0.90	0.90
8.14	116.51	175.16	1.21	211.79	1.86	0.90	0.90
8.15	116.83	175.50	1.21	212.04	1.86	0.90	0.90
8.16	117.13	175.83	1.21	212.27	1.86	0.90	0.90

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)'/σ'_v}	S _{u(peak)'/σ'_v}
8.17	117.40	176.11	1.21	212.47	1.86	0.90	0.90
8.18	117.66	176.38	1.21	212.64	1.86	0.90	0.90
8.19	117.98	176.71	1.20	212.82	1.85	0.90	0.90
8.20	118.40	177.14	1.20	213.03	1.85	0.90	0.90
8.21	118.89	177.68	1.20	213.29	1.85	0.90	0.90
8.22	119.44	178.26	1.20	213.56	1.85	0.90	0.90
8.23	120.00	178.87	1.20	213.82	1.84	0.90	0.90
8.24	120.55	179.45	1.19	214.07	1.84	0.90	0.90
8.25	121.06	180.00	1.19	214.28	1.84	0.90	0.90
8.26	121.50	180.46	1.19	214.45	1.84	0.90	0.90
8.27	121.93	180.92	1.19	214.66	1.83	0.90	0.90
8.28	122.41	181.45	1.18	214.96	1.83	0.90	0.90
8.29	122.99	182.12	1.18	215.39	1.83	0.90	0.90
8.30	123.65	182.90	1.18	215.87	1.83	0.90	0.90
8.31	124.36	183.73	1.18	216.38	1.82	0.90	0.90
8.32	125.08	184.58	1.18	216.88	1.82	0.90	0.90
8.33	125.77	185.39	1.17	217.34	1.82	0.90	0.90
8.34	126.40	186.11	1.17	217.75	1.82	0.91	0.91
8.35	126.94	186.72	1.17	218.08	1.81	0.91	0.91
8.36	127.41	187.26	1.17	218.40	1.81	0.91	0.91
8.37	127.89	187.81	1.16	218.76	1.81	0.91	0.91
8.38	128.43	188.45	1.16	219.19	1.81	0.91	0.91
8.39	129.04	189.18	1.16	219.66	1.81	0.91	0.91
8.40	129.68	189.94	1.16	220.16	1.81	0.91	0.91
8.41	130.31	190.69	1.16	220.64	1.80	0.91	0.91
8.42	130.92	191.40	1.16	221.09	1.80	0.91	0.91
8.43	131.45	192.03	1.15	221.48	1.80	0.91	0.91
8.44	131.87	192.51	1.15	221.78	1.80	0.91	0.91
8.45	132.22	192.90	1.15	222.06	1.80	0.91	0.91
8.46	132.54	193.27	1.15	222.35	1.80	0.91	0.91
8.47	132.89	193.68	1.15	222.69	1.80	0.91	0.91
8.48	133.28	194.14	1.15	223.07	1.80	0.91	0.91
8.49	133.68	194.61	1.15	223.45	1.80	0.91	0.91
8.50	134.07	195.08	1.15	223.83	1.80	0.91	0.91
8.51	134.44	195.50	1.15	224.17	1.79	0.91	0.91
8.52	134.75	195.86	1.15	224.46	1.79	0.91	0.91
8.53	134.99	196.12	1.15	224.67	1.79	0.91	0.91
8.54	135.19	196.32	1.15	224.84	1.79	0.91	0.91
8.55	135.39	196.52	1.14	225.00	1.79	0.91	0.91
8.56	135.61	196.75	1.14	225.18	1.79	0.91	0.91
8.57	135.85	197.00	1.14	225.39	1.79	0.91	0.91
8.58	136.09	197.26	1.14	225.59	1.79	0.91	0.91
8.59	136.32	197.50	1.14	225.79	1.79	0.91	0.91
8.60	136.53	197.72	1.14	225.96	1.79	0.91	0.91
8.61	136.69	197.88	1.14	226.09	1.79	0.91	0.91
8.62	136.81	197.96	1.14	226.16	1.79	0.91	0.91
8.63	136.88	198.00	1.14	226.19	1.79	0.91	0.91
8.64	136.95	198.03	1.14	226.21	1.79	0.91	0.91

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
8.65	137.03	198.06	1.14	226.24	1.79	0.91	0.91
8.66	137.11	198.11	1.14	226.27	1.79	0.91	0.91
8.67	137.19	198.15	1.14	226.30	1.79	0.91	0.91
8.68	137.26	198.18	1.14	226.33	1.79	0.91	0.91
8.69	137.33	198.20	1.14	226.35	1.79	0.91	0.91
8.70	137.37	198.19	1.14	226.28	1.79	0.91	0.91
8.71	137.40	198.12	1.14	226.07	1.79	0.91	0.91
8.72	137.40	198.00	1.14	225.71	1.79	0.91	0.91
8.73	137.40	197.86	1.14	225.27	1.79	0.91	0.91
8.74	137.40	197.71	1.14	224.79	1.79	0.91	0.91
8.75	137.40	197.57	1.14	224.30	1.79	0.91	0.91
8.76	137.40	197.42	1.13	223.81	1.78	0.91	0.91
8.77	137.40	197.28	1.13	223.35	1.78	0.91	0.91
8.78	137.39	197.15	1.13	222.94	1.78	0.91	0.91
8.79	137.36	196.99	1.13	222.59	1.78	0.91	0.91
8.80	137.27	196.78	1.13	222.25	1.78	0.91	0.91
8.81	137.14	196.51	1.13	221.88	1.78	0.91	0.91
8.82	136.99	196.21	1.13	221.47	1.78	0.91	0.91
8.83	136.84	195.89	1.13	221.04	1.78	0.91	0.91
8.84	136.68	195.58	1.13	220.60	1.78	0.91	0.91
8.85	136.52	195.27	1.13	220.18	1.78	0.91	0.91
8.86	136.38	194.99	1.13	219.79	1.78	0.91	0.91
8.87	136.25	194.73	1.13	219.50	1.78	0.91	0.91
8.88	136.09	194.46	1.13	219.36	1.78	0.91	0.91
8.89	135.87	194.16	1.13	219.36	1.78	0.91	0.91
8.90	135.59	193.80	1.13	219.43	1.78	0.91	0.91
8.91	135.29	193.41	1.13	219.50	1.78	0.91	0.91
8.92	134.97	193.01	1.14	219.56	1.79	0.91	0.91
8.93	134.65	192.60	1.14	219.61	1.79	0.91	0.91
8.94	134.35	192.22	1.14	219.64	1.79	0.91	0.91
8.95	134.09	191.87	1.14	219.66	1.79	0.91	0.91
8.96	133.85	191.54	1.15	219.61	1.79	0.91	0.91
8.97	133.59	191.17	1.15	219.48	1.80	0.91	0.91
8.98	133.29	190.74	1.15	219.26	1.80	0.91	0.91
8.99	132.93	190.23	1.15	219.00	1.80	0.91	0.91
9.00	132.54	189.69	1.15	218.71	1.80	0.91	0.91
9.01	132.14	189.14	1.15	218.41	1.80	0.91	0.91
9.02	131.75	188.59	1.16	218.12	1.80	0.91	0.91
9.03	131.38	188.09	1.16	217.83	1.80	0.91	0.91
9.04	131.07	187.64	1.16	217.58	1.81	0.91	0.91
9.05	130.81	187.27	1.16	217.41	1.81	0.90	0.90
9.06	130.57	186.93	1.16	217.31	1.81	0.90	0.90
9.07	130.31	186.59	1.16	217.25	1.81	0.90	0.90
9.08	130.01	186.20	1.17	217.18	1.81	0.90	0.90
9.09	129.70	185.79	1.17	217.10	1.81	0.90	0.90
9.10	129.38	185.38	1.17	217.02	1.82	0.90	0.90
9.11	129.07	184.98	1.17	216.92	1.82	0.90	0.90
9.12	128.79	184.61	1.17	216.82	1.82	0.90	0.90

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.13	128.58	184.31	1.18	216.75	1.82	0.90	0.90
9.14	128.44	184.11	1.18	216.75	1.82	0.90	0.90
9.15	128.35	183.99	1.18	216.83	1.82	0.90	0.90
9.16	128.29	183.90	1.18	216.97	1.83	0.90	0.90
9.17	128.21	183.81	1.18	217.12	1.83	0.90	0.90
9.18	128.13	183.71	1.18	217.27	1.83	0.90	0.90
9.19	128.05	183.61	1.18	217.42	1.83	0.90	0.90
9.20	127.98	183.51	1.19	217.55	1.83	0.91	0.91
9.21	127.91	183.42	1.19	217.66	1.83	0.91	0.91
9.22	127.89	183.38	1.19	217.74	1.83	0.91	0.91
9.23	127.94	183.40	1.19	217.82	1.83	0.91	0.91
9.24	128.06	183.49	1.19	217.92	1.83	0.91	0.91
9.25	128.20	183.62	1.19	218.04	1.83	0.91	0.91
9.26	128.36	183.77	1.19	218.18	1.83	0.91	0.91
9.27	128.52	183.92	1.19	218.32	1.83	0.91	0.91
9.28	128.67	184.07	1.19	218.46	1.83	0.91	0.91
9.29	128.82	184.20	1.19	218.58	1.83	0.91	0.91
9.30	128.95	184.32	1.19	218.69	1.83	0.91	0.91
9.31	129.17	184.53	1.19	218.82	1.83	0.91	0.91
9.32	129.49	184.86	1.18	219.01	1.83	0.91	0.91
9.33	129.95	185.36	1.18	219.26	1.83	0.91	0.91
9.34	130.47	185.92	1.18	219.55	1.83	0.91	0.91
9.35	131.03	186.53	1.18	219.86	1.82	0.91	0.91
9.36	131.59	187.14	1.18	220.15	1.82	0.91	0.91
9.37	132.12	187.72	1.17	220.42	1.82	0.91	0.91
9.38	132.61	188.24	1.17	220.65	1.82	0.91	0.91
9.39	133.04	188.70	1.17	220.84	1.82	0.91	0.91
9.40	133.51	189.20	1.17	221.04	1.81	0.91	0.91
9.41	134.08	189.81	1.17	221.27	1.81	0.91	0.91
9.42	134.77	190.57	1.16	221.54	1.81	0.91	0.91
9.43	135.54	191.41	1.16	221.82	1.81	0.91	0.91
9.44	136.33	192.28	1.16	222.09	1.80	0.91	0.91
9.45	137.13	193.15	1.15	222.32	1.80	0.91	0.91
9.46	137.87	193.96	1.15	222.51	1.80	0.91	0.91
9.47	138.53	194.67	1.14	222.65	1.79	0.91	0.91
9.48	139.09	195.26	1.14	222.77	1.79	0.91	0.91
9.49	139.61	195.82	1.14	222.90	1.79	0.91	0.91
9.50	140.17	196.43	1.14	223.08	1.79	0.91	0.91
9.51	140.82	197.14	1.13	223.28	1.78	0.91	0.91
9.52	141.52	197.92	1.13	223.48	1.78	0.91	0.91
9.53	142.24	198.72	1.13	223.67	1.78	0.91	0.91
9.54	142.94	199.49	1.12	223.83	1.78	0.91	0.91
9.55	143.59	200.20	1.12	223.96	1.77	0.91	0.91
9.56	144.09	200.72	1.12	223.98	1.77	0.91	0.91
9.57	144.10	200.60	1.11	223.53	1.77	0.91	0.91
9.58	143.60	199.81	1.11	222.53	1.77	0.91	0.91
9.59	142.65	198.42	1.11	220.99	1.77	0.91	0.91
9.60	141.56	196.84	1.11	219.25	1.77	0.91	0.91

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.61	140.42	195.18	1.11	217.42	1.77	0.90	0.90
9.62	139.26	193.50	1.11	215.57	1.77	0.90	0.90
9.63	138.15	191.90	1.11	213.81	1.77	0.90	0.90
9.64	137.15	190.44	1.11	212.22	1.77	0.90	0.90
9.65	136.42	189.36	1.11	211.00	1.77	0.90	0.90
9.66	136.05	188.76	1.11	210.20	1.77	0.90	0.90
9.67	135.99	188.56	1.11	209.71	1.77	0.90	0.90
9.68	136.06	188.53	1.11	209.29	1.77	0.90	0.90
9.69	136.14	188.49	1.11	208.83	1.77	0.90	0.90
9.70	136.22	188.46	1.11	208.35	1.76	0.90	0.90
9.71	136.29	188.43	1.10	207.86	1.76	0.90	0.90
9.72	136.37	188.39	1.10	207.39	1.76	0.89	0.89
9.73	136.43	188.36	1.10	206.96	1.76	0.89	0.89
9.74	136.04	187.75	1.10	206.36	1.76	0.89	0.89
9.75	134.97	186.32	1.10	205.42	1.76	0.89	0.89
9.76	133.13	183.94	1.11	203.99	1.77	0.89	0.89
9.77	130.93	181.09	1.12	202.23	1.77	0.89	0.89
9.78	128.55	178.00	1.12	200.24	1.78	0.89	0.89
9.79	126.10	174.83	1.13	198.10	1.78	0.88	0.88
9.80	123.73	171.75	1.14	195.92	1.79	0.88	0.88
9.81	121.54	168.90	1.15	193.84	1.80	0.88	0.88
9.82	119.59	166.39	1.15	192.08	1.80	0.88	0.88
9.83	117.46	163.81	1.17	190.98	1.81	0.88	0.88
9.84	114.82	160.78	1.18	190.09	1.83	0.88	0.88
9.85	111.45	156.96	1.20	188.75	1.85	0.87	0.87
9.86	107.64	152.57	1.22	186.45	1.88	0.87	0.87
9.87	103.59	147.82	1.24	183.37	1.91	0.87	0.87
9.88	99.52	142.94	1.26	179.86	1.93	0.86	0.86
9.89	95.63	138.20	1.28	176.27	1.96	0.86	0.86
9.90	92.13	133.86	1.29	172.94	1.98	0.86	0.86
9.91	89.61	130.76	1.31	170.80	2.00	0.85	0.85
9.92	88.39	129.37	1.32	170.45	2.01	0.85	0.85
9.93	88.29	129.52	1.33	171.85	2.02	0.85	0.85
9.94	88.65	130.35	1.34	174.20	2.03	0.86	0.86
9.95	89.05	131.26	1.35	176.85	2.04	0.86	0.86
9.96	89.47	132.20	1.36	179.66	2.05	0.86	0.86
9.97	89.89	133.12	1.37	182.49	2.06	0.87	0.87
9.98	90.28	133.98	1.38	185.19	2.07	0.87	0.87
9.99	90.62	134.72	1.39	187.59	2.08	0.87	0.87
10.00	90.70	134.97	1.40	188.87	2.09	0.87	0.87
10.01	90.47	134.66	1.40	188.93	2.09	0.87	0.87
10.02	89.92	133.81	1.40	187.87	2.09	0.87	0.87
10.03	89.25	132.78	1.40	186.54	2.09	0.87	0.87
10.04	88.54	131.67	1.41	185.10	2.09	0.87	0.87
10.05	87.80	130.54	1.41	183.63	2.09	0.87	0.87
10.06	87.08	129.44	1.41	182.21	2.09	0.87	0.87
10.07	86.42	128.43	1.41	180.90	2.09	0.87	0.87
10.08	85.78	127.45	1.41	179.71	2.09	0.86	0.86

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
10.09	84.79	126.02	1.41	178.27	2.10	0.86	0.86
10.10	83.29	123.92	1.42	176.39	2.10	0.86	0.86
10.11	81.22	121.05	1.44	173.96	2.11	0.86	0.86
10.12	78.88	117.80	1.45	171.26	2.12	0.85	0.85
10.13	76.41	114.36	1.47	168.45	2.13	0.85	0.85
10.14	73.91	110.89	1.49	165.67	2.14	0.85	0.85
10.15	71.54	107.56	1.52	163.07	2.16	0.84	0.84
10.16	69.39	104.55	1.54	160.76	2.17	0.84	0.84
10.17	67.57	102.01	1.56	159.07	2.18	0.84	0.84
10.18	65.89	99.69	1.59	158.08	2.19	0.84	0.84
10.19	64.10	97.29	1.62	157.68	2.20	0.84	0.84
10.20	62.02	94.50	1.67	157.54	2.22	0.84	0.84
10.21	59.73	91.39	1.72	157.48	2.24	0.84	0.84
10.22	57.35	88.14	1.79	157.50	2.26	0.84	0.84
10.23	54.99	84.89	1.86	157.60	2.28	0.84	0.84
10.24	52.79	81.82	1.93	157.74	2.30	0.84	0.84
10.25	50.85	79.11	2.00	157.90	2.32	0.84	0.84
10.26	49.28	76.90	2.06	158.30	2.33	0.84	0.84
10.27	47.90	74.96	2.12	159.06	2.35	0.84	0.84
10.28	46.50	73.02	2.19	160.24	2.36	0.84	0.84
10.29	44.91	70.78	2.28	161.62	2.38	0.84	0.84
10.30	43.18	68.34	2.39	163.08	2.40	0.84	0.84
10.31	41.42	65.83	2.50	164.52	2.42	0.85	0.85
10.32	39.71	63.37	2.62	165.84	2.44	0.85	0.85
10.33	38.14	61.09	2.73	166.98	2.46	0.85	0.85
10.34	36.84	59.19	2.84	167.91	2.48	0.85	0.85
10.35	35.90	57.82	2.92	168.82	2.49	0.85	0.85
10.36	35.22	56.83	2.99	169.84	2.50	0.84	0.84
10.37	34.62	55.96	3.06	171.08	2.51	0.85	0.85
10.38	33.95	54.98	3.14	172.44	2.52	0.86	0.86
10.39	33.23	53.93	3.22	173.84	2.53	0.88	0.88
10.40	32.51	52.88	3.31	175.19	2.55	0.89	0.89
10.41	31.83	51.87	3.40	176.42	2.56	0.90	0.90
10.42	31.21	50.96	3.48	177.49	2.57	0.91	0.91
10.43	30.76	50.28	3.55	178.39	2.58	0.92	0.92
10.44	30.50	49.89	3.59	179.31	2.58	0.93	0.93
10.45	30.39	49.73	3.63	180.36	2.59	0.93	0.93
10.46	30.32	49.64	3.66	181.62	2.59	0.94	0.94
10.47	30.24	49.54	3.69	183.00	2.59	0.94	0.94
10.48	30.16	49.44	3.73	184.42	2.60	0.95	0.95
10.49	30.08	49.33	3.77	185.83	2.60	0.95	0.95
10.50	30.01	49.23	3.80	187.13	2.61	0.96	0.96
10.51	29.94	49.14	3.83	188.26	2.61	0.96	0.96
10.52	29.90	49.08	3.85	189.08	2.61	0.97	0.97
10.53	29.89	49.05	3.87	189.65	2.61	0.97	0.97
10.54	29.88	49.04	3.88	190.09	2.61	0.97	0.97
10.55	29.88	49.03	3.89	190.59	2.62	0.97	0.97
10.56	29.88	49.02	3.90	191.12	2.62	0.97	0.97

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
10.57	29.88	49.04	3.91	191.70	2.62	0.98	0.98
10.58	29.88	49.03	3.92	192.22	2.62	0.98	0.98
10.59	29.88	49.02	3.93	192.71	2.62	0.98	0.98
10.60	29.90	49.03	3.94	193.06	2.62	0.98	0.98
10.61	29.99	49.14	3.93	193.12	2.62	0.98	0.98
10.62	30.16	49.38	3.91	192.88	2.62	0.98	0.98
10.63	30.42	49.71	3.87	192.38	2.61	0.97	0.97
10.64	30.71	50.11	3.83	191.85	2.61	0.97	0.97
10.65	31.02	50.54	3.78	191.27	2.60	0.96	0.96
10.66	31.32	50.96	3.74	190.67	2.60	0.96	0.96
10.67	31.62	51.36	3.70	190.09	2.59	0.95	0.95
10.68	31.88	51.72	3.67	189.56	2.59	0.95	0.95
10.69	32.16	52.09	3.63	189.03	2.59	0.94	0.94
10.70	32.52	52.60	3.58	188.40	2.58	0.94	0.94
10.71	33.03	53.31	3.52	187.56	2.57	0.93	0.93
10.72	33.66	54.20	3.44	186.51	2.56	0.92	0.92
10.73	34.36	55.17	3.36	185.31	2.55	0.91	0.91
10.74	35.08	56.17	3.28	184.01	2.54	0.89	0.89
10.75	35.79	57.15	3.20	182.68	2.53	0.88	0.88
10.76	36.45	58.06	3.12	181.39	2.52	0.87	0.87
10.77	37.03	58.85	3.06	180.23	2.51	0.86	0.86
10.78	37.61	59.64	3.00	179.21	2.50	0.85	0.85
10.79	38.27	60.54	2.94	178.19	2.49	0.86	0.86
10.80	39.10	61.68	2.87	177.05	2.48	0.86	0.86
10.81	40.06	63.00	2.79	175.69	2.47	0.86	0.86
10.82	41.09	64.41	2.70	174.18	2.46	0.86	0.86
10.83	42.14	65.83	2.62	172.59	2.44	0.86	0.86
10.84	43.16	67.20	2.54	171.01	2.43	0.85	0.85
10.85	44.09	68.45	2.48	169.52	2.42	0.85	0.85
10.86	44.92	69.54	2.42	168.26	2.41	0.85	0.85
10.87	45.76	70.66	2.37	167.21	2.40	0.85	0.85
10.88	46.74	71.97	2.31	166.25	2.39	0.85	0.85
10.89	47.95	73.59	2.25	165.22	2.37	0.85	0.85
10.90	49.30	75.39	2.18	164.04	2.36	0.85	0.85
10.91	50.73	77.29	2.11	162.80	2.34	0.84	0.84
10.92	52.17	79.17	2.04	161.54	2.33	0.84	0.84
10.93	53.53	80.95	1.98	160.36	2.31	0.84	0.84
10.94	54.75	82.52	1.93	159.30	2.30	0.84	0.84
10.95	55.78	83.83	1.89	158.42	2.29	0.84	0.84
10.96	56.72	85.02	1.85	157.62	2.28	0.84	0.84
10.97	57.69	86.24	1.82	156.80	2.27	0.84	0.84
10.98	58.81	87.65	1.78	155.88	2.26	0.83	0.83
10.99	60.05	89.19	1.74	154.90	2.24	0.83	0.83
11.00	61.33	90.77	1.70	153.92	2.23	0.83	0.83
11.01	62.59	92.31	1.66	153.01	2.22	0.83	0.83
11.02	63.77	93.73	1.62	152.20	2.20	0.83	0.83
11.03	64.79	94.96	1.60	151.53	2.19	0.83	0.83
11.04	65.56	95.86	1.57	150.97	2.18	0.83	0.83

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
11.05	66.15	96.52	1.56	150.43	2.18	0.83	0.83
11.06	66.67	97.08	1.54	149.85	2.17	0.83	0.83
11.07	67.25	97.72	1.53	149.19	2.16	0.83	0.83
11.08	67.88	98.40	1.51	148.52	2.15	0.82	0.82
11.09	68.52	99.09	1.49	147.86	2.14	0.82	0.82
11.10	69.14	99.75	1.48	147.25	2.14	0.82	0.82
11.11	69.71	100.34	1.46	146.71	2.13	0.82	0.82
11.12	70.14	100.78	1.45	146.24	2.12	0.82	0.82
11.13	70.34	100.93	1.44	145.71	2.12	0.82	0.82
11.14	70.33	100.80	1.44	145.05	2.11	0.82	0.82
11.15	70.18	100.49	1.44	144.23	2.11	0.82	0.82
11.16	70.01	100.14	1.43	143.31	2.11	0.82	0.82
11.17	69.83	99.78	1.43	142.34	2.11	0.82	0.82
11.18	69.65	99.41	1.42	141.38	2.10	0.82	0.82
11.19	69.48	99.06	1.42	140.47	2.10	0.81	0.81
11.20	69.33	98.75	1.41	139.66	2.10	0.81	0.81
11.21	69.12	98.39	1.41	138.99	2.10	0.81	0.81
11.22	68.78	97.89	1.41	138.41	2.10	0.81	0.81
11.23	68.26	97.18	1.42	137.84	2.10	0.81	0.81
11.24	67.61	96.31	1.42	137.20	2.10	0.81	0.81
11.25	66.90	95.35	1.43	136.51	2.11	0.81	0.81
11.26	66.17	94.37	1.44	135.81	2.11	0.81	0.81
11.27	65.44	93.39	1.45	135.12	2.12	0.81	0.81
11.28	64.77	92.49	1.45	134.49	2.12	0.81	0.81
11.29	64.18	91.69	1.46	133.93	2.13	0.80	0.80
11.30	63.58	90.90	1.47	133.52	2.13	0.80	0.80
11.31	62.89	89.99	1.48	133.22	2.14	0.80	0.80
11.32	62.01	88.87	1.50	132.98	2.15	0.80	0.80
11.33	61.00	87.58	1.52	132.75	2.16	0.80	0.80
11.34	59.92	86.20	1.54	132.53	2.17	0.80	0.80
11.35	58.82	84.78	1.56	132.34	2.18	0.80	0.80
11.36	57.76	83.40	1.58	132.19	2.19	0.80	0.80
11.37	56.79	82.14	1.61	132.07	2.20	0.80	0.80
11.38	55.93	81.01	1.63	132.01	2.21	0.80	0.80
11.39	55.04	79.85	1.65	132.01	2.22	0.80	0.80
11.40	54.01	78.50	1.68	132.10	2.23	0.80	0.80
11.41	52.74	76.85	1.72	132.29	2.24	0.80	0.80
11.42	51.32	74.98	1.77	132.54	2.25	0.80	0.80
11.43	49.82	73.01	1.82	132.86	2.27	0.80	0.80
11.44	48.33	71.03	1.88	133.22	2.29	0.80	0.80
11.45	46.91	69.13	1.93	133.59	2.30	0.80	0.80
11.46	45.64	67.43	1.99	133.94	2.32	0.80	0.80
11.47	44.59	66.01	2.04	134.34	2.33	0.80	0.80
11.48	43.66	64.75	2.08	134.87	2.34	0.81	0.81
11.49	42.71	63.47	2.14	135.61	2.35	0.81	0.81
11.50	41.62	62.01	2.20	136.52	2.37	0.81	0.81
11.51	40.44	60.41	2.28	137.51	2.38	0.81	0.81
11.52	39.21	58.74	2.36	138.53	2.40	0.81	0.81

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
11.53	38.00	57.09	2.44	139.51	2.41	0.81	0.81
11.54	36.88	55.54	2.53	140.40	2.43	0.81	0.81
11.55	35.91	54.18	2.61	141.16	2.44	0.81	0.81
11.56	35.13	53.11	2.67	141.89	2.45	0.82	0.82
11.57	34.46	52.17	2.74	142.71	2.46	0.82	0.82
11.58	33.79	51.25	2.80	143.72	2.47	0.82	0.82
11.59	33.03	50.19	2.89	144.85	2.49	0.82	0.82
11.60	32.21	49.05	2.98	146.02	2.50	0.82	0.82
11.61	31.38	47.89	3.07	147.16	2.51	0.82	0.82
11.62	30.58	46.76	3.17	148.22	2.53	0.84	0.84
11.63	29.84	45.72	3.26	149.14	2.54	0.85	0.85
11.64	29.25	44.87	3.34	149.90	2.55	0.86	0.86
11.65	28.81	44.25	3.40	150.60	2.56	0.87	0.87
11.66	28.48	43.78	3.46	151.35	2.56	0.87	0.87
11.67	28.16	43.33	3.51	152.23	2.57	0.88	0.88
11.68	27.81	42.83	3.58	153.19	2.58	0.89	0.89
11.69	27.44	42.30	3.64	154.18	2.59	0.90	0.90
11.70	27.07	41.78	3.71	155.15	2.60	0.91	0.91
11.71	26.72	41.29	3.78	156.05	2.60	0.92	0.92
11.72	26.40	40.84	3.84	156.83	2.61	0.92	0.92
11.73	26.21	40.55	3.88	157.40	2.61	0.93	0.93
11.74	26.15	40.47	3.90	157.81	2.62	0.93	0.93
11.75	26.23	40.57	3.90	158.12	2.62	0.93	0.93
11.76	26.35	40.74	3.89	158.45	2.62	0.93	0.93
11.77	26.49	40.92	3.88	158.82	2.61	0.93	0.93
11.78	26.63	41.12	3.87	159.20	2.61	0.93	0.93
11.79	26.76	41.31	3.86	159.57	2.61	0.93	0.93
11.80	26.89	41.48	3.86	159.91	2.61	0.93	0.93
11.81	26.99	41.62	3.85	160.19	2.61	0.93	0.93
11.82	26.96	41.55	3.85	160.01	2.61	0.93	0.93
11.83	26.76	41.24	3.86	159.29	2.61	0.93	0.93
11.84	26.40	40.67	3.88	158.00	2.62	0.93	0.93
11.85	25.99	40.03	3.91	156.54	2.62	0.93	0.93
11.86	25.55	39.34	3.94	154.97	2.62	0.93	0.93
11.87	25.10	38.64	3.97	153.39	2.62	0.93	0.93
11.88	24.67	37.97	4.00	151.87	2.63	0.93	0.93
11.89	24.27	37.35	4.03	150.48	2.63	0.93	0.93
11.90	23.96	36.86	4.05	149.29	2.63	0.93	0.93
11.91	23.76	36.53	4.06	148.18	2.63	0.93	0.93
11.92	23.64	36.32	4.05	147.01	2.63	0.93	0.93
11.93	23.55	36.14	4.03	145.64	2.63	0.93	0.93
11.94	23.45	35.95	4.01	144.10	2.63	0.92	0.92
11.95	23.34	35.74	3.99	142.50	2.63	0.92	0.92
11.96	23.23	35.54	3.96	140.89	2.62	0.91	0.91
11.97	23.13	35.35	3.94	139.38	2.62	0.91	0.91
11.98	23.04	35.18	3.92	138.03	2.62	0.90	0.90
11.99	22.93	34.97	3.91	136.84	2.62	0.90	0.90
12.00	22.76	34.69	3.91	135.65	2.62	0.90	0.90

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
12.01	22.50	34.28	3.92	134.30	2.62	0.90	0.90
12.02	22.19	33.78	3.93	132.73	2.62	0.90	0.90
12.03	21.85	33.24	3.94	131.02	2.62	0.89	0.89
12.04	21.49	32.68	3.96	129.27	2.62	0.89	0.89
12.05	21.15	32.13	3.97	127.55	2.62	0.89	0.89
12.06	20.83	31.63	3.98	125.97	2.63	0.89	0.89
12.07	20.54	31.18	4.00	124.60	2.63	0.89	0.89
12.08	20.15	30.58	4.04	123.44	2.63	0.89	0.89
12.09	19.60	29.75	4.11	122.34	2.64	0.90	0.90
12.10	18.82	28.60	4.24	121.12	2.65	0.90	0.90
12.11	17.94	27.28	4.39	119.69	2.67	0.92	0.92
12.12	16.99	25.87	4.57	118.11	2.69	0.93	0.93
12.13	16.03	24.43	4.77	116.45	2.71	0.78	0.78
12.14	15.10	23.05	4.98	114.77	2.73	0.77	0.77
12.15	14.26	21.78	5.20	113.17	2.74	0.77	0.77
12.16	13.60	20.78	5.39	111.91	2.76	0.77	0.77
12.17	13.17	20.13	5.53	111.26	2.77	0.77	0.77
12.18	12.90	19.73	5.63	111.17	2.78	0.77	0.77
12.19	12.70	19.43	5.73	111.37	2.79	0.77	0.77
12.20	12.47	19.09	5.85	111.58	2.80	0.77	0.77
12.21	12.23	18.73	5.97	111.76	2.81	0.77	0.77
12.22	11.99	18.37	6.09	111.92	2.82	0.77	0.77
12.23	11.77	18.03	6.21	112.05	2.83	0.77	0.77
12.24	11.57	17.73	6.32	112.14	2.84	0.77	0.77
12.25	11.40	17.47	6.43	112.26	2.84	0.77	0.77
12.26	11.23	17.22	6.53	112.45	2.85	0.77	0.77
12.27	11.05	16.94	6.65	112.73	2.86	0.77	0.77
12.28	10.83	16.62	6.80	113.05	2.87	0.77	0.77
12.29	10.60	16.27	6.97	113.36	2.88	0.77	0.77
12.30	10.36	15.91	7.14	113.64	2.90	0.77	0.77
12.31	10.12	15.56	7.32	113.87	2.91	0.77	0.77
12.32	9.90	15.23	7.49	114.04	2.92	0.77	0.77
12.33	9.72	14.94	7.64	114.15	2.93	0.77	0.77
12.34	9.55	14.68	7.78	114.23	2.94	0.77	0.77
12.35	9.38	14.41	7.93	114.25	2.95	0.77	0.77
12.36	9.18	14.08	8.11	114.19	2.96	0.77	0.77
12.37	8.96	13.70	8.33	114.08	2.97	0.77	0.77
12.38	8.72	13.30	8.56	113.91	2.99	0.77	0.77
12.39	8.48	12.90	8.81	113.68	3.00	0.56	0.92
12.40	8.25	12.51	9.07	113.41	3.02	0.55	0.89
12.41	8.04	12.15	9.31	113.11	3.03	0.54	0.87
12.42	7.87	11.86	9.51	112.83	3.04	0.53	0.85
12.43	7.73	11.62	9.69	112.61	3.05	0.53	0.83
12.44	7.60	11.41	9.86	112.43	3.06	0.52	0.81
12.45	7.47	11.18	10.04	112.22	3.07	0.52	0.80
12.46	7.32	10.92	10.26	111.97	3.08	0.51	0.78
12.47	7.16	10.65	10.49	111.67	3.09	0.51	0.76
12.48	7.00	10.38	10.73	111.34	3.11	0.50	0.74

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
12.49	6.85	10.13	10.96	111.00	3.12	0.49	0.72
12.50	6.71	9.90	11.18	110.67	3.13	0.49	0.71
12.51	6.61	9.73	11.35	110.40	3.14	0.48	0.69
12.52	6.53	9.59	11.48	110.19	3.14	0.48	0.69
12.53	6.47	9.48	11.60	110.02	3.15	0.48	0.68
12.54	6.40	9.36	11.73	109.83	3.15	0.48	0.67
12.55	6.32	9.23	11.88	109.61	3.16	0.47	0.66
12.56	6.24	9.09	12.03	109.38	3.17	0.47	0.65
12.57	6.16	8.96	12.19	109.14	3.18	0.46	0.64
12.58	6.09	8.83	12.33	108.91	3.18	0.46	0.63
12.59	6.03	8.73	12.46	108.71	3.19	0.46	0.62
12.60	5.99	8.66	12.53	108.58	3.19	0.46	0.62
12.61	5.98	8.63	12.57	108.52	3.19	0.46	0.62
12.62	5.98	8.63	12.57	108.51	3.19	0.46	0.62
12.63	5.98	8.63	12.58	108.49	3.19	0.46	0.62
12.64	5.98	8.62	12.58	108.48	3.19	0.46	0.62
12.65	5.98	8.62	12.59	108.47	3.19	0.46	0.62
12.66	5.98	8.61	12.59	108.45	3.19	0.46	0.62
12.67	5.98	8.61	12.59	108.44	3.19	0.45	0.62
12.68	5.98	8.61	12.59	108.39	3.19	0.45	0.61
12.69	5.98	8.60	12.58	108.25	3.19	0.45	0.61
12.70	5.98	8.60	12.56	108.00	3.19	0.45	0.61
12.71	5.98	8.59	12.53	107.66	3.19	0.45	0.61
12.72	5.98	8.59	12.49	107.28	3.19	0.44	0.61
12.73	5.98	8.59	12.45	106.88	3.19	0.44	0.61
12.74	5.98	8.58	12.41	106.48	3.19	0.44	0.61
12.75	5.98	8.58	12.37	106.11	3.18	0.43	0.61
12.76	5.98	8.58	12.33	105.77	3.18	0.43	0.61
12.77	5.98	8.57	12.30	105.44	3.18	0.43	0.61
12.78	5.98	8.57	12.26	105.07	3.18	0.43	0.61
12.79	5.98	8.56	12.21	104.59	3.18	0.42	0.61
12.80	5.98	8.56	12.15	104.03	3.17	0.42	0.61
12.81	5.98	8.56	12.09	103.42	3.17	0.41	0.61
12.82	5.98	8.55	12.02	102.79	3.17	0.41	0.61
12.83	5.98	8.55	11.95	102.17	3.16	0.40	0.61
12.84	5.98	8.54	11.89	101.60	3.16	0.40	0.61
12.85	5.98	8.54	11.84	101.09	3.16	0.39	0.61
12.86	5.98	8.54	11.79	100.62	3.16	0.39	0.61
12.87	5.98	8.53	11.73	100.12	3.15	0.38	0.61
12.88	5.98	8.53	11.67	99.53	3.15	0.38	0.61
12.89	5.98	8.52	11.60	98.85	3.15	0.37	0.61
12.90	5.98	8.52	11.52	98.13	3.14	0.37	0.61
12.91	5.98	8.52	11.43	97.39	3.14	0.36	0.61
12.92	5.98	8.51	11.36	96.68	3.14	0.36	0.61
12.93	5.98	8.51	11.28	96.03	3.13	0.35	0.61
12.94	5.98	8.51	11.22	95.46	3.13	0.35	0.61
12.95	5.98	8.50	11.16	94.89	3.13	0.34	0.61
12.96	5.98	8.50	11.09	94.26	3.12	0.34	0.61

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
12.97	5.98	8.49	11.01	93.49	3.12	0.33	0.61
12.98	5.98	8.49	10.91	92.64	3.11	0.32	0.61
12.99	5.98	8.49	10.81	91.74	3.11	0.32	0.61
13.00	5.98	8.48	10.71	90.84	3.10	0.31	0.61
13.01	5.98	8.48	10.61	89.99	3.10	0.30	0.61
13.02	5.98	8.48	10.53	89.22	3.10	0.30	0.61
13.03	5.95	8.43	10.49	88.46	3.09	0.29	0.60
13.04	5.88	8.31	10.53	87.55	3.10	0.29	0.59
13.05	5.76	8.12	10.65	86.40	3.10	0.28	0.58
13.06	5.62	7.88	10.79	85.03	3.11	0.26	0.56
13.07	5.46	7.62	10.96	83.55	3.12	0.25	0.54
13.08	5.30	7.36	11.15	82.02	3.13	0.24	0.53
13.09	5.14	7.10	11.34	80.52	3.14	0.23	0.51
13.10	5.00	6.86	11.53	79.13	3.14	0.22	0.49
13.11	4.87	6.65	11.71	77.92	3.15	0.21	0.48
13.12	4.74	6.44	11.93	76.78	3.16	0.20	0.46
13.13	4.58	6.18	12.22	75.56	3.18	0.19	0.44
13.14	4.39	5.86	12.64	74.07	3.20	0.18	0.42
13.15	4.16	5.49	13.17	72.36	3.22	0.17	0.39
13.16	3.93	5.11	13.80	70.49	3.25	0.16	0.36
13.17	3.69	4.72	14.54	68.54	3.27	0.14	0.34
13.18	3.46	4.34	15.35	66.61	3.31	0.13	0.31
13.19	3.25	4.00	16.19	64.82	3.34	0.12	0.29
13.20	3.09	3.74	16.95	63.36	3.36	0.11	0.27
13.21	2.98	3.56	17.52	62.32	3.38	0.11	0.25
13.22	2.90	3.43	17.94	61.59	3.40	0.11	0.25
13.23	2.83	3.32	18.34	60.89	3.41	0.10	0.24
13.24	2.76	3.19	18.82	60.12	3.43	0.10	0.23
13.25	2.68	3.06	19.35	59.29	3.44	0.10	0.22
13.26	2.60	2.93	19.92	58.46	3.46	0.09	0.21
13.27	2.52	2.81	20.51	57.67	3.48	0.09	0.20
13.28	2.46	2.70	21.06	56.96	3.49	0.09	0.19
13.29	2.41	2.63	21.46	56.52	3.50	0.08	0.19
13.30	2.39	2.60	21.69	56.37	3.51	0.08	0.19
13.31	2.39	2.59	21.77	56.47	3.51	0.08	0.19
13.32	2.39	2.59	21.84	56.62	3.51	0.08	0.19
13.33	2.39	2.59	21.92	56.79	3.52	0.09	0.19
13.34	2.39	2.59	21.99	56.96	3.52	0.09	0.18
13.35	2.39	2.59	22.07	57.12	3.52	0.09	0.18
13.36	2.39	2.59	22.14	57.27	3.52	0.09	0.18
13.37	2.40	2.59	22.15	57.45	3.52	0.09	0.19
13.38	2.44	2.66	21.81	58.01	3.51	0.09	0.19
13.39	2.52	2.80	21.09	59.03	3.49	0.09	0.20
13.40	2.65	3.01	20.11	60.51	3.46	0.10	0.21
13.41	2.80	3.25	19.13	62.15	3.43	0.11	0.23
13.42	2.96	3.50	18.23	63.85	3.41	0.12	0.25
13.43	3.12	3.76	17.44	65.53	3.38	0.13	0.27
13.44	3.28	4.00	16.77	67.11	3.36	0.13	0.29

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
13.45	3.41	4.22	16.22	68.51	3.34	0.14	0.30
13.46	3.54	4.42	15.76	69.74	3.32	0.15	0.32
13.47	3.68	4.65	15.28	71.00	3.30	0.16	0.33
13.48	3.85	4.92	14.73	72.46	3.28	0.17	0.35
13.49	4.06	5.25	14.13	74.17	3.26	0.18	0.37
13.50	4.29	5.62	13.53	76.02	3.23	0.19	0.40
13.51	4.53	6.00	12.98	77.90	3.21	0.20	0.43
13.52	4.76	6.38	12.50	79.72	3.19	0.22	0.46
13.53	4.99	6.74	12.08	81.39	3.17	0.23	0.48
13.54	5.18	7.05	11.75	82.84	3.16	0.24	0.50
13.55	5.30	7.23	11.58	83.75	3.15	0.25	0.52
13.56	5.34	7.29	11.54	84.16	3.15	0.25	0.52
13.57	5.30	7.23	11.64	84.17	3.15	0.25	0.52
13.58	5.26	7.15	11.76	84.12	3.16	0.25	0.51
13.59	5.20	7.07	11.90	84.06	3.16	0.25	0.50
13.60	5.15	6.98	12.04	83.99	3.17	0.25	0.50
13.61	5.10	6.89	12.18	83.92	3.18	0.25	0.49
13.62	5.05	6.81	12.31	83.85	3.18	0.25	0.49
13.63	5.01	6.75	12.43	83.82	3.19	0.25	0.48
13.64	4.99	6.71	12.53	84.00	3.19	0.25	0.48
13.65	4.98	6.69	12.62	84.44	3.20	0.25	0.48
13.66	4.98	6.69	12.73	85.13	3.20	0.25	0.48
13.67	4.98	6.68	12.85	85.90	3.21	0.26	0.48
13.68	4.98	6.68	12.98	86.70	3.21	0.27	0.48
13.69	4.98	6.68	13.10	87.51	3.22	0.27	0.48
13.70	4.98	6.67	13.22	88.27	3.22	0.28	0.48
13.71	4.98	6.67	13.33	88.94	3.23	0.28	0.48
13.72	4.99	6.69	13.38	89.53	3.23	0.29	0.48
13.73	5.04	6.77	13.32	90.10	3.23	0.29	0.48
13.74	5.13	6.90	13.15	90.73	3.22	0.30	0.49
13.75	5.24	7.08	12.91	91.47	3.21	0.30	0.51
13.76	5.37	7.28	12.67	92.28	3.20	0.31	0.52
13.77	5.51	7.49	12.42	93.10	3.19	0.32	0.54
13.78	5.64	7.70	12.19	93.90	3.18	0.33	0.55
13.79	5.76	7.89	11.99	94.63	3.17	0.33	0.56
13.80	5.87	8.06	11.81	95.27	3.16	0.34	0.58
13.81	5.91	8.12	11.74	95.39	3.15	0.35	0.58
13.82	5.87	8.06	11.78	94.90	3.16	0.34	0.58
13.83	5.75	7.87	11.92	93.77	3.16	0.33	0.56
13.84	5.61	7.63	12.11	92.40	3.17	0.31	0.55
13.85	5.45	7.38	12.32	90.92	3.18	0.30	0.53
13.86	5.29	7.12	12.55	89.39	3.19	0.29	0.51
13.87	5.13	6.87	12.79	87.90	3.20	0.28	0.49
13.88	4.99	6.64	13.03	86.52	3.21	0.26	0.47
13.89	4.87	6.44	13.25	85.37	3.22	0.25	0.46
13.90	4.76	6.26	13.50	84.53	3.23	0.25	0.45
13.91	4.64	6.08	13.81	83.92	3.25	0.24	0.43
13.92	4.51	5.86	14.22	83.35	3.26	0.24	0.42

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
13.93	4.36	5.62	14.70	82.68	3.28	0.23	0.40
13.94	4.20	5.37	15.26	81.92	3.30	0.23	0.38
13.95	4.04	5.11	15.86	81.10	3.33	0.22	0.37
13.96	3.89	4.87	16.48	80.27	3.35	0.21	0.35
13.97	3.75	4.65	17.09	79.48	3.37	0.21	0.33
13.98	3.65	4.49	17.58	78.97	3.39	0.20	0.32
13.99	3.60	4.41	17.91	78.91	3.40	0.20	0.31
14.00	3.59	4.38	18.10	79.31	3.40	0.21	0.31
14.01	3.59	4.38	18.25	79.94	3.41	0.21	0.31
14.02	3.59	4.38	18.42	80.64	3.41	0.21	0.31
14.03	3.59	4.38	18.59	81.35	3.42	0.22	0.31
14.04	3.59	4.37	18.76	82.05	3.42	0.22	0.31
14.05	3.59	4.37	18.92	82.70	3.43	0.23	0.31
14.06	3.59	4.37	19.06	83.27	3.43	0.23	0.31
14.07	3.62	4.42	19.04	84.08	3.43	0.23	0.32
14.08	3.69	4.53	18.84	85.34	3.43	0.24	0.32
14.09	3.81	4.72	18.46	87.16	3.41	0.26	0.34
14.10	3.96	4.95	18.04	89.29	3.40	0.27	0.35
14.11	4.12	5.19	17.63	91.58	3.39	0.29	0.37
14.12	4.28	5.45	17.25	93.91	3.37	0.31	0.39
14.13	4.43	5.69	16.91	96.17	3.36	0.33	0.41
14.14	4.57	5.91	16.62	98.23	3.35	0.35	0.42
14.15	4.70	6.11	16.37	100.02	3.34	0.36	0.44
14.16	4.83	6.32	16.11	101.74	3.33	0.38	0.45
14.17	4.99	6.56	15.78	103.62	3.32	0.39	0.47
14.18	5.19	6.88	15.39	105.86	3.31	0.42	0.49
14.19	5.42	7.23	14.99	108.37	3.29	0.44	0.52
14.20	5.66	7.60	14.60	110.99	3.28	0.47	0.54
14.21	5.90	7.97	14.25	113.61	3.26	0.50	0.57
14.22	6.13	8.33	13.94	116.08	3.25	0.52	0.59
14.23	6.33	8.65	13.68	118.29	3.24	0.55	0.62
14.24	6.51	8.92	13.46	120.06	3.23	0.57	0.64
14.25	6.67	9.18	13.24	121.52	3.22	0.58	0.66
14.26	6.85	9.46	12.99	122.85	3.21	0.60	0.68
14.27	7.06	9.78	12.71	124.30	3.20	0.62	0.70
14.28	7.29	10.14	12.41	125.87	3.19	0.64	0.72
14.29	7.53	10.51	12.13	127.46	3.17	0.66	0.75
14.30	7.77	10.88	11.86	128.99	3.16	0.68	0.78
14.31	7.99	11.22	11.62	130.40	3.15	0.70	0.80
14.32	8.19	11.52	11.42	131.60	3.14	0.72	0.82
14.33	8.34	11.76	11.27	132.50	3.13	0.73	0.84
14.34	8.47	11.96	11.14	133.18	3.13	0.74	0.85
14.35	8.60	12.15	11.01	133.76	3.12	0.75	0.87
14.36	8.74	12.37	10.86	134.41	3.11	0.76	0.88
14.37	8.90	12.61	10.71	135.10	3.10	0.77	0.90
14.38	9.06	12.86	10.56	135.78	3.10	0.78	0.92
14.39	9.22	13.09	10.42	136.42	3.09	0.79	0.94
14.40	9.36	13.31	10.29	137.00	3.08	0.80	0.95

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
14.41	9.47	13.48	10.20	137.48	3.08	0.81	0.96
14.42	9.51	13.54	10.18	137.87	3.08	0.82	0.97
14.43	9.49	13.50	10.24	138.25	3.08	0.82	0.96
14.44	9.42	13.39	10.35	138.65	3.09	0.82	0.96
14.45	9.35	13.27	10.48	139.09	3.09	0.83	0.95
14.46	9.27	13.14	10.62	139.54	3.10	0.83	0.94
14.47	9.19	13.01	10.76	139.97	3.11	0.83	0.93
14.48	9.11	12.88	10.90	140.36	3.11	0.84	0.92
14.49	9.05	12.77	11.02	140.70	3.12	0.84	0.91
14.50	8.95	12.62	11.16	140.80	3.13	0.84	0.90
14.51	8.79	12.35	11.37	140.49	3.14	0.83	0.88
14.52	8.53	11.95	11.69	139.70	3.15	0.81	0.85
14.53	8.20	11.43	12.12	138.56	3.17	0.79	0.82
14.54	7.84	10.87	12.62	137.17	3.20	0.77	0.78
14.55	7.47	10.28	13.18	135.57	3.22	0.74	0.73
14.56	7.10	9.71	13.79	133.84	3.24	0.72	0.69
14.57	6.76	9.17	14.40	132.06	3.27	0.69	0.65
14.58	6.45	8.70	14.99	130.38	3.29	0.67	0.62
14.59	6.23	8.35	15.45	129.06	3.31	0.65	0.60
14.60	6.07	8.10	15.81	128.02	3.32	0.64	0.58
14.61	5.94	7.90	16.10	127.12	3.33	0.63	0.56
14.62	5.80	7.67	16.45	126.07	3.35	0.62	0.55
14.63	5.64	7.42	16.84	124.92	3.36	0.60	0.53
14.64	5.48	7.17	17.26	123.70	3.37	0.59	0.51
14.65	5.33	6.92	17.69	122.49	3.39	0.57	0.49
14.66	5.18	6.70	18.11	121.34	3.40	0.56	0.48
14.67	5.08	6.53	18.44	120.47	3.41	0.55	0.47
14.68	5.05	6.49	18.53	120.25	3.42	0.54	0.46
14.69	5.11	6.57	18.37	120.70	3.41	0.55	0.47
14.70	5.22	6.74	18.05	121.64	3.40	0.56	0.48
14.71	5.34	6.93	17.70	122.67	3.39	0.57	0.50
14.72	5.48	7.13	17.35	123.73	3.38	0.59	0.51
14.73	5.61	7.33	17.01	124.77	3.37	0.60	0.52
14.74	5.73	7.53	16.71	125.73	3.36	0.61	0.54
14.75	5.85	7.70	16.45	126.58	3.35	0.62	0.55
14.76	5.93	7.82	16.26	127.12	3.34	0.63	0.56
14.77	5.97	7.88	16.16	127.28	3.34	0.63	0.56
14.78	5.98	7.89	16.11	127.11	3.33	0.63	0.56
14.79	5.98	7.88	16.08	126.80	3.33	0.62	0.56
14.80	5.98	7.88	16.05	126.45	3.33	0.62	0.56
14.81	5.98	7.88	16.01	126.10	3.33	0.62	0.56
14.82	5.98	7.87	15.97	125.75	3.33	0.61	0.56
14.83	5.98	7.87	15.94	125.43	3.33	0.61	0.56
14.84	5.98	7.87	15.91	125.14	3.33	0.61	0.56
14.85	6.01	7.91	15.81	125.13	3.32	0.60	0.57
14.86	6.09	8.03	15.62	125.42	3.32	0.61	0.57
14.87	6.21	8.22	15.33	126.02	3.31	0.62	0.59
14.88	6.36	8.44	15.01	126.69	3.29	0.63	0.60

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
14.89	6.52	8.68	14.68	127.37	3.28	0.64	0.62
14.90	6.68	8.92	14.35	128.03	3.27	0.65	0.64
14.91	6.83	9.15	14.05	128.63	3.26	0.66	0.65
14.92	6.98	9.37	13.79	129.14	3.24	0.66	0.67
14.93	7.10	9.55	13.57	129.55	3.24	0.67	0.68
14.94	7.21	9.71	13.37	129.90	3.23	0.68	0.69
14.95	7.32	9.89	13.17	130.23	3.22	0.68	0.71
14.96	7.46	10.09	12.94	130.58	3.21	0.69	0.72
14.97	7.61	10.32	12.70	130.95	3.20	0.69	0.74
14.98	7.77	10.55	12.44	131.31	3.19	0.70	0.75
14.99	7.93	10.79	12.20	131.63	3.18	0.71	0.77
15.00	8.08	11.02	11.97	131.90	3.17	0.71	0.79
15.01	8.21	11.22	11.77	132.12	3.16	0.72	0.80
15.02	8.28	11.32	11.67	132.11	3.15	0.72	0.81
15.03	8.26	11.28	11.68	131.77	3.15	0.72	0.81
15.04	8.14	11.10	11.81	131.06	3.16	0.71	0.79
15.05	7.98	10.84	12.00	130.11	3.17	0.69	0.77
15.06	7.80	10.56	12.22	129.06	3.18	0.68	0.75
15.07	7.61	10.27	12.46	127.95	3.19	0.66	0.73
15.08	7.43	9.99	12.70	126.83	3.20	0.65	0.71
15.09	7.26	9.72	12.94	125.76	3.21	0.63	0.69
15.10	7.11	9.49	13.15	124.81	3.22	0.62	0.68
15.11	7.03	9.37	13.29	124.51	3.22	0.61	0.67
15.12	7.03	9.37	13.34	124.93	3.23	0.62	0.67
15.13	7.09	9.46	13.32	126.03	3.23	0.63	0.68
15.14	7.17	9.57	13.31	127.31	3.22	0.65	0.68
15.15	7.25	9.68	13.29	128.69	3.22	0.66	0.69
15.16	7.33	9.80	13.27	130.08	3.22	0.68	0.70
15.17	7.40	9.91	13.26	131.43	3.22	0.70	0.71
15.18	7.47	10.02	13.25	132.67	3.22	0.71	0.72
15.19	7.55	10.13	13.21	133.79	3.22	0.72	0.72
15.20	7.68	10.32	13.09	135.08	3.22	0.74	0.74
15.21	7.89	10.63	12.86	136.71	3.21	0.76	0.76
15.22	8.17	11.05	12.56	138.73	3.19	0.79	0.79
15.23	8.48	11.52	12.24	140.96	3.18	0.82	0.82
15.24	8.81	12.01	11.92	143.25	3.16	0.85	0.86
15.25	9.14	12.51	11.63	145.49	3.15	0.89	0.89
15.26	9.45	12.97	11.37	147.58	3.14	0.92	0.93
15.27	9.73	13.39	11.16	149.40	3.13	0.95	0.96
15.28	9.98	13.76	10.96	150.84	3.12	0.98	0.98
15.29	10.24	14.14	10.75	151.99	3.11	0.99	1.01
15.30	10.54	14.59	10.49	153.01	3.09	1.01	1.04
15.31	10.89	15.12	10.19	154.06	3.08	1.04	1.08
15.32	11.28	15.70	9.88	155.12	3.06	1.06	1.12
15.33	11.68	16.30	9.58	156.11	3.05	1.09	1.16
15.34	12.07	16.88	9.30	156.99	3.03	1.11	1.21
15.35	12.44	17.43	9.05	157.72	3.02	1.13	1.24
15.36	12.75	17.90	8.84	158.29	3.00	1.15	1.28

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
15.37	13.02	18.30	8.67	158.66	2.99	0.84	0.84
15.38	13.27	18.67	8.51	158.89	2.98	0.84	0.84
15.39	13.54	19.06	8.34	159.04	2.97	0.84	0.84
15.40	13.85	19.52	8.15	159.15	2.96	0.84	0.84
15.41	14.18	20.01	7.96	159.21	2.95	0.84	0.84
15.42	14.52	20.51	7.76	159.20	2.94	0.84	0.84
15.43	14.84	20.95	7.59	159.01	2.93	0.84	0.84
15.44	15.14	21.34	7.44	158.78	2.92	0.84	0.84
15.45	15.34	21.61	7.33	158.46	2.91	0.84	0.84
15.46	15.33	21.58	7.31	157.78	2.91	0.84	0.84
15.47	15.11	21.26	7.37	156.64	2.91	0.84	0.84
15.48	14.74	20.72	7.49	155.11	2.92	0.83	0.83
15.49	14.32	20.12	7.62	153.37	2.93	0.83	0.83
15.50	13.88	19.49	7.77	151.49	2.94	0.83	0.83
15.51	13.45	18.82	7.94	149.51	2.95	0.83	0.83
15.52	13.03	18.19	8.11	147.60	2.96	0.82	0.82
15.53	12.66	17.63	8.27	145.87	2.97	0.82	0.82
15.54	12.35	17.15	8.42	144.50	2.98	0.82	0.82
15.55	12.06	16.71	8.58	143.44	2.99	0.82	0.82
15.56	11.75	16.25	8.77	142.51	3.00	0.82	0.82
15.57	11.40	15.71	9.01	141.45	3.01	0.90	1.12
15.58	11.01	15.12	9.27	140.22	3.03	0.87	1.08
15.59	10.61	14.52	9.57	138.88	3.04	0.85	1.04
15.60	10.22	13.92	9.88	137.48	3.06	0.82	0.99
15.61	9.85	13.37	10.18	136.11	3.08	0.79	0.95
15.62	9.54	12.89	10.46	134.86	3.09	0.77	0.92
15.63	9.34	12.59	10.66	134.15	3.10	0.76	0.90
15.64	9.24	12.43	10.78	133.96	3.11	0.76	0.89
15.65	9.20	12.38	10.84	134.21	3.11	0.76	0.88
15.66	9.17	12.32	10.92	134.50	3.12	0.76	0.88
15.67	9.13	12.25	11.00	134.80	3.12	0.76	0.88
15.68	9.09	12.19	11.08	135.10	3.12	0.77	0.87
15.69	9.05	12.13	11.16	135.38	3.13	0.77	0.87
15.70	9.01	12.07	11.24	135.63	3.13	0.77	0.86
15.71	8.98	12.02	11.30	135.82	3.13	0.77	0.86
15.72	8.94	11.95	11.37	135.92	3.14	0.77	0.85
15.73	8.89	11.87	11.46	135.95	3.14	0.77	0.85
15.74	8.82	11.76	11.56	135.95	3.15	0.77	0.84
15.75	8.74	11.64	11.68	135.93	3.15	0.77	0.83
15.76	8.66	11.52	11.80	135.90	3.16	0.76	0.82
15.77	8.58	11.40	11.92	135.87	3.16	0.76	0.81
15.78	8.51	11.28	12.04	135.83	3.17	0.76	0.81
15.79	8.44	11.17	12.15	135.78	3.17	0.76	0.80
15.80	8.38	11.08	12.24	135.67	3.18	0.76	0.79
15.81	8.33	11.00	12.32	135.46	3.18	0.75	0.79
15.82	8.27	10.90	12.40	135.13	3.19	0.75	0.78
15.83	8.20	10.79	12.48	134.71	3.19	0.74	0.77
15.84	8.12	10.67	12.58	134.26	3.19	0.73	0.76

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
15.85	8.04	10.55	12.68	133.79	3.20	0.73	0.75
15.86	7.96	10.43	12.79	133.32	3.20	0.72	0.74
15.87	7.89	10.31	12.88	132.88	3.21	0.71	0.74
15.88	7.82	10.22	12.97	132.49	3.21	0.71	0.73
15.89	7.77	10.13	13.03	132.01	3.21	0.70	0.72
15.90	7.71	10.04	13.08	131.37	3.22	0.70	0.72
15.91	7.65	9.94	13.13	130.52	3.22	0.69	0.71
15.92	7.57	9.83	13.18	129.54	3.22	0.67	0.70
15.93	7.49	9.71	13.24	128.51	3.22	0.66	0.69
15.94	7.41	9.58	13.30	127.45	3.22	0.65	0.68
15.95	7.34	9.47	13.36	126.44	3.23	0.64	0.68
15.96	7.27	9.36	13.41	125.52	3.23	0.63	0.67
15.97	7.21	9.28	13.45	124.78	3.23	0.62	0.66
15.98	7.18	9.23	13.47	124.26	3.23	0.61	0.66
15.99	7.17	9.21	13.45	123.90	3.23	0.61	0.66
16.00	7.17	9.21	13.42	123.58	3.23	0.60	0.66
16.01	7.17	9.20	13.39	123.22	3.23	0.60	0.66
16.02	7.17	9.20	13.36	122.84	3.23	0.60	0.66
16.03	7.17	9.19	13.32	122.47	3.23	0.59	0.66
16.04	7.17	9.19	13.29	122.11	3.22	0.59	0.66
16.05	7.17	9.19	13.26	121.79	3.22	0.59	0.66
16.06	7.17	9.18	13.25	121.62	3.22	0.58	0.66
16.07	7.17	9.18	13.25	121.64	3.22	0.58	0.66
16.08	7.17	9.17	13.28	121.85	3.22	0.59	0.66
16.09	7.17	9.17	13.32	122.13	3.23	0.59	0.65
16.10	7.17	9.17	13.36	122.43	3.23	0.59	0.65
16.11	7.17	9.16	13.40	122.74	3.23	0.60	0.65
16.12	7.17	9.16	13.44	123.05	3.23	0.60	0.65
16.13	7.17	9.15	13.47	123.33	3.23	0.60	0.65
16.14	7.17	9.15	13.50	123.58	3.23	0.60	0.65
16.15	7.17	9.15	13.54	123.86	3.23	0.61	0.65
16.16	7.17	9.14	13.59	124.22	3.24	0.61	0.65
16.17	7.17	9.14	13.64	124.70	3.24	0.62	0.65
16.18	7.17	9.14	13.71	125.25	3.24	0.62	0.65
16.19	7.17	9.13	13.78	125.84	3.24	0.63	0.65
16.20	7.17	9.13	13.85	126.43	3.25	0.63	0.65
16.21	7.17	9.12	13.92	126.99	3.25	0.64	0.65
16.22	7.17	9.12	13.98	127.50	3.25	0.64	0.65
16.23	7.20	9.16	13.99	128.08	3.25	0.65	0.65
16.24	7.31	9.30	13.87	129.09	3.25	0.66	0.66
16.25	7.50	9.59	13.62	130.64	3.24	0.68	0.68
16.26	7.78	9.99	13.29	132.67	3.22	0.71	0.71
16.27	8.08	10.43	12.94	134.89	3.21	0.74	0.74
16.28	8.40	10.89	12.60	137.16	3.19	0.77	0.78
16.29	8.72	11.35	12.28	139.37	3.18	0.80	0.81
16.30	9.02	11.78	12.01	141.42	3.17	0.83	0.84
16.31	9.28	12.16	11.77	143.20	3.16	0.86	0.87
16.32	9.53	12.51	11.56	144.64	3.15	0.88	0.89

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
16.33	9.78	12.88	11.33	145.88	3.14	0.90	0.92
16.34	10.09	13.32	11.04	147.08	3.12	0.92	0.95
16.35	10.44	13.83	10.73	148.37	3.11	0.94	0.99
16.36	10.83	14.39	10.40	149.69	3.09	0.97	1.03
16.37	11.23	14.97	10.08	150.96	3.07	1.00	1.07
16.38	11.63	15.53	9.79	152.10	3.06	1.02	1.11
16.39	11.99	16.05	9.54	153.09	3.04	1.04	1.15
16.40	12.30	16.51	9.32	153.87	3.03	1.06	1.18
16.41	12.60	16.93	9.12	154.42	3.02	1.08	1.21
16.42	12.93	17.40	8.90	154.78	3.01	1.09	1.24
16.43	13.32	17.96	8.63	155.01	2.99	0.83	0.83
16.44	13.76	18.60	8.34	155.16	2.97	0.83	0.83
16.45	14.24	19.28	8.05	155.18	2.96	0.83	0.83
16.46	14.72	19.96	7.77	155.07	2.94	0.83	0.83
16.47	15.18	20.58	7.52	154.71	2.92	0.83	0.83
16.48	15.60	21.13	7.30	154.26	2.91	0.83	0.83
16.49	15.98	21.62	7.12	153.86	2.89	0.83	0.83
16.50	16.39	22.16	6.93	153.57	2.88	0.83	0.83
16.51	16.89	22.82	6.72	153.35	2.87	0.83	0.83
16.52	17.51	23.62	6.48	153.05	2.85	0.83	0.83
16.53	18.19	24.52	6.22	152.57	2.83	0.83	0.83
16.54	18.91	25.45	5.97	151.89	2.81	0.83	0.83
16.55	19.63	26.37	5.73	151.05	2.79	0.83	0.83
16.56	20.30	27.23	5.51	150.11	2.77	0.83	0.83
16.57	20.90	27.99	5.33	149.16	2.76	0.83	0.83
16.58	21.30	28.49	5.20	148.14	2.75	0.82	0.82
16.59	21.52	28.75	5.11	146.91	2.74	0.82	0.82
16.60	21.60	28.82	5.04	145.35	2.73	0.82	0.82
16.61	21.66	28.86	4.97	143.49	2.72	0.82	0.82
16.62	21.72	28.90	4.89	141.45	2.72	0.82	0.82
16.63	21.78	28.95	4.81	139.33	2.71	0.81	0.81
16.64	21.84	28.99	4.73	137.23	2.70	0.81	0.81
16.65	21.90	29.02	4.66	135.28	2.70	0.97	0.97
16.66	21.94	29.04	4.60	133.61	2.69	0.96	0.96
16.67	21.87	28.92	4.58	132.44	2.69	0.96	0.96
16.68	21.67	28.64	4.60	131.63	2.69	0.96	0.96
16.69	21.34	28.20	4.65	131.01	2.69	0.96	0.96
16.70	20.97	27.70	4.70	130.30	2.70	0.96	0.96
16.71	20.58	27.17	4.77	129.54	2.71	0.80	0.80
16.72	20.18	26.63	4.83	128.76	2.71	0.80	0.80
16.73	19.79	26.12	4.90	128.01	2.72	0.80	0.80
16.74	19.45	25.65	4.96	127.32	2.72	0.79	0.79
16.75	19.15	25.25	5.03	126.92	2.73	0.79	0.79
16.76	18.88	24.89	5.10	127.07	2.74	0.79	0.79
16.77	18.59	24.52	5.21	127.78	2.75	0.80	0.80
16.78	18.26	24.10	5.35	128.83	2.76	0.80	0.80
16.79	17.90	23.63	5.50	129.93	2.77	0.80	0.80
16.80	17.51	23.14	5.66	131.02	2.78	0.80	0.80

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
16.81	17.13	22.64	5.83	132.04	2.80	0.80	0.80
16.82	16.78	22.18	5.99	132.93	2.81	0.80	0.80
16.83	16.46	21.76	6.14	133.67	2.82	0.80	0.80
16.84	16.15	21.36	6.29	134.32	2.83	0.80	0.80
16.85	15.79	20.88	6.46	134.99	2.85	0.81	0.81
16.86	15.33	20.28	6.69	135.72	2.86	0.81	0.81
16.87	14.79	19.58	6.97	136.46	2.88	0.81	0.81
16.88	14.21	18.80	7.29	137.09	2.91	0.81	0.81
16.89	13.61	18.01	7.64	137.54	2.93	0.81	0.81
16.90	13.02	17.17	8.01	137.62	2.95	0.81	0.81
16.91	12.48	16.39	8.39	137.50	2.98	0.81	0.81
16.92	12.02	15.74	8.72	137.27	3.00	0.81	0.81
16.93	11.69	15.26	8.99	137.19	3.01	0.84	1.09
16.94	11.46	14.92	9.20	137.31	3.02	0.84	1.07
16.95	11.26	14.64	9.40	137.62	3.04	0.83	1.05
16.96	11.04	14.31	9.64	137.92	3.05	0.83	1.02
16.97	10.80	13.97	9.89	138.18	3.06	0.83	1.00
16.98	10.56	13.62	10.16	138.37	3.08	0.83	0.97
16.99	10.33	13.29	10.42	138.49	3.09	0.82	0.95
17.00	10.12	12.99	10.67	138.54	3.10	0.82	0.93
17.01	9.98	12.78	10.84	138.59	3.11	0.81	0.91
17.02	9.94	12.72	10.91	138.74	3.11	0.81	0.91
17.03	9.99	12.79	10.87	139.03	3.11	0.82	0.91
17.04	10.10	12.93	10.78	139.42	3.11	0.83	0.92
17.05	10.21	13.09	10.69	139.85	3.10	0.83	0.93
17.06	10.33	13.25	10.59	140.29	3.10	0.84	0.95
17.07	10.45	13.41	10.49	140.71	3.09	0.85	0.96
17.08	10.56	13.57	10.40	141.11	3.09	0.86	0.97
17.09	10.66	13.70	10.32	141.45	3.09	0.86	0.98
17.10	10.73	13.79	10.26	141.47	3.08	0.87	0.98
17.11	10.76	13.82	10.20	141.07	3.08	0.86	0.99
17.12	10.76	13.82	10.14	140.23	3.08	0.85	0.99
17.13	10.76	13.82	10.07	139.19	3.07	0.84	0.99
17.14	10.76	13.81	10.00	138.07	3.07	0.82	0.99
17.15	10.76	13.81	9.92	136.90	3.06	0.81	0.99
17.16	10.76	13.80	9.84	135.76	3.06	0.80	0.99
17.17	10.76	13.79	9.76	134.70	3.06	0.79	0.99
17.18	10.75	13.77	9.71	133.75	3.05	0.78	0.98
17.19	10.66	13.64	9.73	132.69	3.05	0.77	0.97
17.20	10.47	13.37	9.82	131.34	3.06	0.74	0.95
17.21	10.18	12.96	10.00	129.60	3.07	0.72	0.93
17.22	9.86	12.50	10.21	127.61	3.08	0.69	0.89
17.23	9.52	12.01	10.45	125.47	3.09	0.66	0.86
17.24	9.17	11.52	10.70	123.28	3.10	0.63	0.82
17.25	8.84	11.05	10.97	121.16	3.12	0.60	0.79
17.26	8.54	10.62	11.23	119.22	3.13	0.58	0.76
17.27	8.28	10.26	11.47	117.62	3.14	0.56	0.73
17.28	8.04	9.91	11.73	116.28	3.15	0.54	0.71

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
17.29	7.79	9.55	12.05	115.02	3.17	0.53	0.68
17.30	7.49	9.12	12.45	113.58	3.19	0.51	0.65
17.31	7.15	8.65	12.93	111.90	3.21	0.49	0.62
17.32	6.81	8.16	13.49	110.07	3.23	0.47	0.58
17.33	6.46	7.68	14.09	108.16	3.26	0.44	0.55
17.34	6.14	7.22	14.72	106.27	3.28	0.42	0.52
17.35	5.86	6.82	15.33	104.53	3.31	0.40	0.49
17.36	5.68	6.56	15.76	103.44	3.32	0.39	0.47
17.37	5.60	6.46	15.97	103.09	3.33	0.39	0.46
17.38	5.62	6.47	15.98	103.40	3.33	0.39	0.46
17.39	5.64	6.50	15.98	103.84	3.33	0.40	0.46
17.40	5.67	6.53	15.97	104.31	3.33	0.40	0.47
17.41	5.69	6.57	15.96	104.80	3.33	0.41	0.47
17.42	5.72	6.60	15.95	105.28	3.33	0.41	0.47
17.43	5.74	6.63	15.94	105.72	3.33	0.41	0.47
17.44	5.76	6.66	15.93	106.09	3.33	0.42	0.48
17.45	5.78	6.68	15.93	106.44	3.33	0.42	0.48
17.46	5.80	6.71	15.93	106.82	3.33	0.42	0.48
17.47	5.82	6.73	15.93	107.26	3.33	0.43	0.48
17.48	5.85	6.77	15.93	107.77	3.33	0.43	0.48
17.49	5.87	6.80	15.93	108.31	3.33	0.44	0.49
17.50	5.90	6.84	15.92	108.85	3.33	0.44	0.49
17.51	5.93	6.87	15.92	109.36	3.33	0.45	0.49
17.52	5.95	6.90	15.92	109.83	3.33	0.45	0.49
17.53	5.98	6.94	15.89	110.34	3.33	0.46	0.50
17.54	6.05	7.03	15.80	111.10	3.32	0.46	0.50
17.55	6.16	7.18	15.63	112.20	3.32	0.47	0.51
17.56	6.30	7.37	15.42	113.60	3.31	0.49	0.53
17.57	6.45	7.58	15.19	115.13	3.30	0.51	0.54
17.58	6.61	7.80	14.96	116.72	3.29	0.52	0.56
17.59	6.77	8.02	14.75	118.29	3.28	0.54	0.57
17.60	6.92	8.22	14.57	119.75	3.28	0.56	0.59
17.61	7.05	8.40	14.41	121.03	3.27	0.57	0.60
17.62	7.16	8.55	14.28	122.12	3.26	0.58	0.61
17.63	7.27	8.71	14.15	123.18	3.26	0.59	0.62
17.64	7.40	8.88	14.00	124.34	3.25	0.61	0.63
17.65	7.54	9.08	13.85	125.67	3.25	0.62	0.65
17.66	7.70	9.29	13.68	127.11	3.24	0.64	0.66
17.67	7.86	9.51	13.52	128.57	3.23	0.66	0.68
17.68	8.02	9.72	13.37	129.99	3.23	0.68	0.69
17.69	8.16	9.92	13.24	131.29	3.22	0.69	0.71
17.70	8.27	10.07	13.14	132.32	3.22	0.71	0.72
17.71	8.32	10.13	13.12	132.88	3.22	0.72	0.72
17.72	8.30	10.10	13.17	133.00	3.22	0.71	0.72
17.73	8.23	10.00	13.28	132.83	3.22	0.71	0.71
17.74	8.16	9.90	13.40	132.64	3.23	0.71	0.71
17.75	8.08	9.78	13.54	132.43	3.23	0.70	0.70
17.76	8.00	9.67	13.68	132.21	3.24	0.70	0.69

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
17.77	7.92	9.56	13.81	131.99	3.25	0.70	0.68
17.78	7.85	9.46	13.93	131.79	3.25	0.69	0.68
17.79	7.80	9.37	14.04	131.62	3.26	0.69	0.67
17.80	7.74	9.29	14.15	131.49	3.26	0.69	0.66
17.81	7.68	9.21	14.27	131.39	3.26	0.69	0.66
17.82	7.61	9.11	14.42	131.28	3.27	0.68	0.65
17.83	7.53	9.00	14.58	131.15	3.28	0.68	0.64
17.84	7.45	8.88	14.75	131.00	3.28	0.68	0.63
17.85	7.38	8.77	14.92	130.84	3.29	0.68	0.63
17.86	7.30	8.66	15.08	130.69	3.30	0.67	0.62
17.87	7.24	8.57	15.23	130.54	3.30	0.67	0.61
17.88	7.19	8.51	15.34	130.51	3.31	0.67	0.61
17.89	7.18	8.48	15.41	130.64	3.31	0.67	0.61
17.90	7.17	8.47	15.45	130.93	3.31	0.67	0.61
17.91	7.17	8.47	15.50	131.28	3.31	0.68	0.61
17.92	7.17	8.47	15.55	131.66	3.31	0.68	0.60
17.93	7.17	8.46	15.60	132.05	3.32	0.69	0.60
17.94	7.17	8.46	15.65	132.42	3.32	0.69	0.60
17.95	7.17	8.46	15.70	132.76	3.32	0.69	0.60
17.96	7.18	8.46	15.73	133.06	3.32	0.70	0.60
17.97	7.21	8.50	15.70	133.39	3.32	0.70	0.61
17.98	7.27	8.58	15.60	133.79	3.32	0.70	0.61
17.99	7.36	8.70	15.45	134.31	3.31	0.71	0.62
18.00	7.46	8.83	15.28	134.88	3.30	0.72	0.63
18.01	7.56	8.97	15.10	135.47	3.30	0.73	0.64
18.02	7.67	9.11	14.93	136.06	3.29	0.74	0.65
18.03	7.77	9.25	14.77	136.61	3.28	0.74	0.66
18.04	7.86	9.37	14.63	137.10	3.28	0.75	0.67
18.05	7.98	9.53	14.45	137.69	3.27	0.76	0.68
18.06	8.18	9.80	14.14	138.61	3.26	0.77	0.70
18.07	8.50	10.23	13.68	139.95	3.24	0.79	0.73
18.08	8.89	10.77	13.14	141.52	3.22	0.82	0.77
18.09	9.33	11.36	12.60	143.10	3.19	0.84	0.81
18.10	9.78	11.98	12.07	144.56	3.17	0.87	0.86
18.11	10.23	12.59	11.59	145.85	3.15	0.90	0.90
18.12	10.65	13.15	11.17	146.90	3.13	0.92	0.94
18.13	11.01	13.65	10.82	147.72	3.11	0.94	0.98
18.14	11.42	14.19	10.47	148.65	3.09	0.95	1.01
18.15	11.92	14.88	10.07	149.86	3.07	0.98	1.06
18.16	12.59	15.79	9.59	151.38	3.05	1.02	1.13
18.17	13.36	16.84	9.08	152.88	3.02	1.06	1.20
18.18	14.20	17.98	8.57	154.16	2.99	0.83	0.83
18.19	15.06	19.14	8.11	155.13	2.96	0.83	0.83
18.20	15.88	20.26	7.69	155.77	2.93	0.83	0.83
18.21	16.64	21.24	7.34	155.96	2.91	0.83	0.83
18.22	17.27	22.03	7.08	155.87	2.89	0.83	0.83
18.23	17.74	22.61	6.87	155.38	2.88	0.83	0.83
18.24	18.09	23.04	6.70	154.49	2.86	0.83	0.83

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
18.25	18.43	23.44	6.53	153.18	2.85	0.83	0.83
18.26	18.80	23.89	6.35	151.63	2.84	0.83	0.83
18.27	19.20	24.37	6.15	149.89	2.82	0.83	0.83
18.28	19.60	24.84	5.96	148.05	2.81	0.82	0.82
18.29	19.98	25.29	5.78	146.19	2.79	0.82	0.82
18.30	20.32	25.69	5.62	144.46	2.78	0.82	0.82
18.31	20.53	25.92	5.51	142.91	2.77	0.82	0.82
18.32	20.55	25.93	5.45	141.43	2.77	0.82	0.82
18.33	20.40	25.71	5.44	139.82	2.77	0.81	0.81
18.34	20.15	25.38	5.44	137.95	2.77	0.81	0.81
18.35	19.89	25.02	5.43	135.90	2.77	0.81	0.81
18.36	19.62	24.64	5.43	133.77	2.76	0.80	0.80
18.37	19.34	24.27	5.43	131.69	2.76	0.80	0.80
18.38	19.09	23.93	5.42	129.75	2.76	0.80	0.80
18.39	18.87	23.62	5.42	128.05	2.76	0.80	0.80
18.40	18.63	23.30	5.45	126.92	2.77	0.79	0.79
18.41	18.33	22.92	5.51	126.28	2.77	0.79	0.79
18.42	17.94	22.41	5.62	125.98	2.78	0.79	0.79
18.43	17.48	21.83	5.75	125.63	2.79	0.79	0.79
18.44	16.99	21.20	5.91	125.21	2.80	0.79	0.79
18.45	16.48	20.56	6.07	124.73	2.82	0.79	0.79
18.46	16.00	19.94	6.23	124.23	2.83	0.79	0.79
18.47	15.55	19.37	6.39	123.73	2.84	0.79	0.79
18.48	15.17	18.88	6.53	123.32	2.85	0.79	0.79
18.49	14.80	18.41	6.69	123.09	2.86	0.79	0.79
18.50	14.40	17.90	6.87	123.02	2.88	0.79	0.79
18.51	13.93	17.29	7.11	123.01	2.89	0.79	0.79
18.52	13.39	16.61	7.40	122.88	2.91	0.79	0.79
18.53	12.83	15.88	7.72	122.59	2.93	0.79	0.79
18.54	12.27	15.11	8.08	122.08	2.96	0.79	0.79
18.55	11.73	14.39	8.44	121.46	2.98	0.79	0.79
18.56	11.25	13.73	8.79	120.78	3.00	0.64	0.98
18.57	10.87	13.21	9.10	120.18	3.02	0.62	0.94
18.58	10.56	12.79	9.36	119.69	3.03	0.61	0.91
18.59	10.28	12.40	9.62	119.27	3.05	0.60	0.89
18.60	9.97	11.98	9.91	118.77	3.06	0.59	0.86
18.61	9.63	11.52	10.26	118.15	3.08	0.58	0.82
18.62	9.28	11.04	10.64	117.43	3.10	0.57	0.79
18.63	8.93	10.57	11.03	116.62	3.12	0.55	0.76
18.64	8.61	10.13	11.43	115.78	3.14	0.54	0.72
18.65	8.32	9.75	11.80	114.98	3.16	0.53	0.70
18.66	8.10	9.44	12.10	114.31	3.17	0.52	0.67
18.67	7.91	9.19	12.38	113.74	3.18	0.51	0.66
18.68	7.73	8.94	12.66	113.18	3.20	0.50	0.64
18.69	7.53	8.66	12.99	112.50	3.21	0.49	0.62
18.70	7.30	8.36	13.37	111.72	3.23	0.48	0.60
18.71	7.08	8.05	13.77	110.88	3.24	0.47	0.58
18.72	6.86	7.75	14.19	110.01	3.26	0.46	0.55

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
18.73	6.66	7.48	14.59	109.18	3.28	0.45	0.53
18.74	6.49	7.26	14.95	108.48	3.29	0.44	0.52
18.75	6.37	7.09	15.24	108.03	3.30	0.44	0.51
18.76	6.28	6.96	15.49	107.80	3.31	0.43	0.50
18.77	6.19	6.84	15.75	107.68	3.32	0.43	0.49
18.78	6.09	6.70	16.04	107.52	3.33	0.43	0.48
18.79	5.98	6.56	16.37	107.33	3.34	0.43	0.47
18.80	5.87	6.41	16.71	107.11	3.36	0.42	0.46
18.81	5.77	6.27	17.04	106.89	3.37	0.42	0.45
18.82	5.68	6.15	17.34	106.66	3.38	0.42	0.44
18.83	5.62	6.06	17.57	106.56	3.38	0.42	0.43
18.84	5.59	6.02	17.72	106.67	3.39	0.42	0.43
18.85	5.58	6.01	17.81	106.98	3.39	0.42	0.43
18.86	5.58	6.00	17.89	107.42	3.40	0.42	0.43
18.87	5.58	6.00	17.98	107.89	3.40	0.43	0.43
18.88	5.58	6.00	18.07	108.38	3.40	0.43	0.43
18.89	5.58	6.00	18.15	108.86	3.40	0.44	0.43
18.90	5.58	5.99	18.23	109.30	3.41	0.44	0.43
18.91	5.58	5.99	18.31	109.68	3.41	0.45	0.43
18.92	5.60	6.02	18.29	110.12	3.41	0.45	0.43
18.93	5.65	6.09	18.19	110.70	3.41	0.45	0.43
18.94	5.74	6.20	17.99	111.47	3.40	0.46	0.44
18.95	5.84	6.33	17.76	112.35	3.39	0.47	0.45
18.96	5.94	6.46	17.53	113.28	3.38	0.48	0.46
18.97	6.05	6.60	17.30	114.23	3.38	0.49	0.47
18.98	6.15	6.74	17.09	115.14	3.37	0.50	0.48
18.99	6.25	6.86	16.90	115.96	3.36	0.51	0.49
19.00	6.33	6.96	16.75	116.63	3.36	0.52	0.50
19.01	6.40	7.06	16.59	117.15	3.35	0.52	0.50
19.02	6.48	7.16	16.42	117.58	3.35	0.53	0.51
19.03	6.57	7.28	16.22	118.01	3.34	0.53	0.52
19.04	6.67	7.41	15.99	118.48	3.33	0.54	0.53
19.05	6.78	7.55	15.76	118.97	3.32	0.54	0.54
19.06	6.88	7.68	15.54	119.44	3.31	0.55	0.55
19.07	6.98	7.82	15.34	119.87	3.31	0.55	0.56
19.08	7.07	7.93	15.16	120.25	3.30	0.56	0.57
19.09	7.13	8.01	15.03	120.44	3.29	0.56	0.57
19.10	7.17	8.05	14.95	120.38	3.29	0.56	0.57
19.11	7.17	8.06	14.91	120.08	3.29	0.56	0.58
19.12	7.17	8.05	14.86	119.66	3.29	0.55	0.58
19.13	7.17	8.05	14.81	119.20	3.29	0.55	0.57
19.14	7.17	8.05	14.76	118.73	3.28	0.54	0.57
19.15	7.17	8.04	14.71	118.27	3.28	0.54	0.57
19.16	7.17	8.04	14.66	117.83	3.28	0.54	0.57
19.17	7.17	8.04	14.62	117.44	3.28	0.53	0.57
19.18	7.15	8.00	14.62	116.99	3.28	0.53	0.57
19.19	7.10	7.93	14.68	116.40	3.28	0.52	0.57
19.20	7.01	7.81	14.80	115.61	3.29	0.51	0.56

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
19.21	6.91	7.68	14.94	114.70	3.29	0.50	0.55
19.22	6.81	7.54	15.09	113.72	3.30	0.49	0.54
19.23	6.70	7.39	15.25	112.73	3.30	0.48	0.53
19.24	6.60	7.25	15.41	111.76	3.31	0.47	0.52
19.25	6.50	7.13	15.56	110.88	3.31	0.46	0.51
19.26	6.42	7.02	15.69	110.12	3.32	0.46	0.50
19.27	6.35	6.92	15.82	109.42	3.32	0.45	0.49
19.28	6.27	6.81	15.95	108.68	3.33	0.44	0.49
19.29	6.18	6.69	16.12	107.83	3.33	0.43	0.48
19.30	6.08	6.55	16.31	106.87	3.34	0.42	0.47
19.31	5.97	6.41	16.51	105.86	3.35	0.41	0.46
19.32	5.87	6.27	16.72	104.85	3.36	0.40	0.45
19.33	5.77	6.13	16.93	103.89	3.36	0.39	0.44
19.34	5.68	6.01	17.13	103.02	3.37	0.39	0.43
19.35	5.62	5.93	17.26	102.35	3.37	0.38	0.42
19.36	5.58	5.89	17.30	101.84	3.38	0.38	0.42
19.37	5.58	5.88	17.26	101.42	3.37	0.37	0.42
19.38	5.58	5.87	17.19	100.97	3.37	0.37	0.42
19.39	5.58	5.87	17.11	100.48	3.37	0.37	0.42
19.40	5.58	5.87	17.03	99.97	3.37	0.36	0.42
19.41	5.58	5.87	16.95	99.46	3.36	0.36	0.42
19.42	5.58	5.86	16.88	98.99	3.36	0.35	0.42
19.43	5.58	5.86	16.82	98.58	3.36	0.35	0.42
19.44	5.58	5.86	16.76	98.22	3.36	0.35	0.42
19.45	5.58	5.86	16.71	97.86	3.36	0.34	0.42
19.46	5.58	5.85	16.64	97.45	3.35	0.34	0.42
19.47	5.58	5.85	16.57	96.99	3.35	0.34	0.42
19.48	5.58	5.85	16.49	96.49	3.35	0.33	0.42
19.49	5.58	5.85	16.41	95.98	3.35	0.33	0.42
19.50	5.58	5.85	16.34	95.49	3.34	0.33	0.42
19.51	5.58	5.84	16.27	95.04	3.34	0.32	0.42
19.52	5.58	5.84	16.21	94.66	3.34	0.32	0.42
19.53	5.58	5.84	16.16	94.35	3.34	0.32	0.42
19.54	5.58	5.84	16.12	94.06	3.33	0.31	0.42
19.55	5.58	5.83	16.07	93.75	3.33	0.31	0.42
19.56	5.58	5.83	16.02	93.39	3.33	0.31	0.42
19.57	5.58	5.83	15.96	93.02	3.33	0.31	0.42
19.58	5.58	5.83	15.90	92.65	3.33	0.30	0.42
19.59	5.58	5.82	15.85	92.30	3.32	0.30	0.42
19.60	5.58	5.82	15.80	91.98	3.32	0.30	0.42
19.61	5.58	5.82	15.77	91.74	3.32	0.30	0.42
19.62	5.57	5.81	15.77	91.57	3.32	0.30	0.41
19.63	5.56	5.79	15.78	91.44	3.32	0.29	0.41
19.64	5.55	5.78	15.81	91.30	3.32	0.29	0.41
19.65	5.54	5.76	15.83	91.15	3.32	0.29	0.41
19.66	5.52	5.74	15.86	91.00	3.33	0.29	0.41
19.67	5.51	5.72	15.89	90.85	3.33	0.29	0.41
19.68	5.50	5.70	15.92	90.71	3.33	0.29	0.41

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
19.69	5.49	5.68	15.94	90.59	3.33	0.29	0.41
19.70	5.45	5.64	16.04	90.44	3.33	0.29	0.40
19.71	5.40	5.56	16.22	90.24	3.34	0.28	0.40
19.72	5.31	5.45	16.51	89.96	3.35	0.28	0.39
19.73	5.21	5.32	16.85	89.63	3.36	0.28	0.38
19.74	5.11	5.18	17.23	89.26	3.37	0.28	0.37
19.75	5.00	5.04	17.64	88.86	3.39	0.27	0.36
19.76	4.90	4.90	18.04	88.46	3.40	0.27	0.35
19.77	4.81	4.78	18.43	88.07	3.41	0.27	0.34
19.78	4.78	4.75	18.58	88.19	3.42	0.26	0.34
19.79	4.93	4.94	18.15	89.69	3.40	0.27	0.35
19.80	5.29	5.40	17.17	92.76	3.37	0.30	0.39
19.81	5.80	6.06	15.99	96.96	3.33	0.34	0.43
19.82	6.37	6.80	14.91	101.47	3.29	0.38	0.49
19.83	6.97	7.58	13.99	106.03	3.25	0.42	0.54
19.84	7.56	8.35	13.23	110.45	3.22	0.47	0.60
19.85	8.13	9.08	12.61	114.52	3.19	0.52	0.65
19.86	8.63	9.73	12.14	118.07	3.17	0.56	0.69
19.87	9.07	10.30	11.75	121.09	3.16	0.59	0.74
19.88	9.53	10.89	11.39	123.99	3.14	0.63	0.78
19.89	10.06	11.57	10.99	127.15	3.12	0.67	0.83
19.90	10.68	12.37	10.57	130.76	3.10	0.72	0.88
19.91	11.35	13.24	10.17	134.60	3.08	0.78	0.95
19.92	12.04	14.13	9.80	138.47	3.06	0.83	1.01
19.93	12.72	15.01	9.47	142.19	3.04	0.89	1.07
19.94	13.36	15.82	9.20	145.59	3.02	0.95	1.13
19.95	13.88	16.49	9.00	148.37	3.01	1.00	1.18
19.96	14.03	16.69	8.94	149.20	3.01	1.03	1.19
19.97	13.81	16.39	9.03	148.08	3.01	0.99	1.17
19.98	13.25	15.66	9.27	145.14	3.03	0.94	1.12
19.99	12.61	14.82	9.56	141.75	3.04	0.89	1.06
20.00	11.92	13.93	9.91	138.06	3.06	0.83	1.00
20.01	11.23	13.03	10.30	134.24	3.08	0.77	0.93
20.02	10.56	12.16	10.73	130.49	3.11	0.71	0.87
20.03	9.96	11.38	11.16	126.99	3.13	0.66	0.81
20.04	9.45	10.72	11.57	124.02	3.15	0.62	0.77
20.05	9.01	10.15	11.97	121.46	3.17	0.59	0.73
20.06	8.59	9.60	12.40	118.99	3.19	0.57	0.69
20.07	8.11	8.98	12.94	116.18	3.21	0.53	0.64
20.08	7.58	8.28	13.63	112.93	3.24	0.49	0.59
20.09	7.02	7.56	14.46	109.37	3.27	0.45	0.54
20.10	6.46	6.84	15.44	105.66	3.31	0.41	0.49
20.11	5.94	6.16	16.55	101.97	3.35	0.38	0.44
20.12	5.47	5.56	17.72	98.53	3.39	0.35	0.40
20.13	5.15	5.15	18.67	96.18	3.42	0.32	0.37
20.14	4.99	4.94	19.26	95.10	3.44	0.32	0.35
20.15	4.95	4.88	19.51	95.15	3.45	0.32	0.35
20.16	4.92	4.85	19.70	95.46	3.45	0.32	0.35

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
20.17	4.90	4.81	19.91	95.78	3.46	0.32	0.34
20.18	4.87	4.77	20.13	96.11	3.46	0.33	0.34
20.19	4.84	4.74	20.35	96.42	3.47	0.33	0.34
20.20	4.82	4.71	20.55	96.70	3.48	0.33	0.34
20.21	4.80	4.68	20.73	96.94	3.48	0.33	0.33
20.22	4.78	4.65	20.90	97.19	3.49	0.33	0.33
20.23	4.76	4.63	21.08	97.48	3.49	0.34	0.33
20.24	4.74	4.60	21.29	97.85	3.50	0.34	0.33
20.25	4.71	4.56	21.54	98.27	3.51	0.34	0.33
20.26	4.69	4.53	21.81	98.70	3.51	0.34	0.32
20.27	4.66	4.49	22.08	99.13	3.52	0.35	0.32
20.28	4.64	4.46	22.34	99.53	3.53	0.35	0.32
20.29	4.61	4.42	22.58	99.88	3.53	0.35	0.32
20.30	4.62	4.43	22.68	100.39	3.54	0.36	0.32
20.31	4.69	4.52	22.47	101.47	3.53	0.36	0.32
20.32	4.83	4.70	21.96	103.24	3.52	0.38	0.34
20.33	5.04	4.96	21.27	105.60	3.50	0.40	0.35
20.34	5.27	5.26	20.59	108.19	3.48	0.43	0.38
20.35	5.51	5.56	19.94	110.87	3.46	0.45	0.40
20.36	5.75	5.86	19.36	113.51	3.44	0.48	0.42
20.37	5.97	6.15	18.87	115.97	3.43	0.50	0.44
20.38	6.17	6.40	18.46	118.14	3.41	0.53	0.46
20.39	6.36	6.64	18.08	120.04	3.40	0.55	0.47
20.40	6.57	6.91	17.65	121.93	3.39	0.56	0.49
20.41	6.84	7.24	17.13	124.06	3.37	0.59	0.52
20.42	7.15	7.64	16.56	126.48	3.35	0.62	0.55
20.43	7.49	8.07	16.00	129.05	3.33	0.65	0.58
20.44	7.83	8.51	15.48	131.63	3.31	0.68	0.61
20.45	8.17	8.94	15.01	134.09	3.29	0.71	0.64
20.46	8.49	9.33	14.61	136.30	3.28	0.74	0.67
20.47	8.76	9.68	14.28	138.17	3.26	0.77	0.69
20.48	9.01	10.00	13.98	139.74	3.25	0.79	0.71
20.49	9.29	10.34	13.65	141.19	3.24	0.81	0.74
20.50	9.62	10.76	13.27	142.74	3.22	0.83	0.77
20.51	9.99	11.23	12.86	144.42	3.21	0.86	0.80
20.52	10.38	11.73	12.46	146.12	3.19	0.88	0.84
20.53	10.78	12.23	12.08	147.75	3.17	0.91	0.87
20.54	11.17	12.71	11.74	149.23	3.15	0.94	0.91
20.55	11.51	13.15	11.44	150.51	3.14	0.96	0.94
20.56	11.80	13.50	11.21	151.44	3.13	0.98	0.96
20.57	12.02	13.78	11.03	151.99	3.12	0.99	0.98
20.58	12.21	14.02	10.86	152.25	3.11	0.99	1.00
20.59	12.42	14.28	10.67	152.38	3.10	1.00	1.02
20.60	12.65	14.57	10.47	152.49	3.09	1.01	1.04
20.61	12.89	14.86	10.26	152.56	3.08	1.01	1.06
20.62	13.13	15.16	10.06	152.59	3.07	1.02	1.08
20.63	13.35	15.44	9.88	152.57	3.06	1.03	1.10
20.64	13.55	15.68	9.73	152.53	3.05	1.03	1.12

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
20.65	13.72	15.90	9.59	152.43	3.05	1.03	1.14
20.66	13.89	16.10	9.46	152.25	3.04	1.03	1.15
20.67	14.07	16.33	9.31	151.97	3.03	1.03	1.17
20.68	14.29	16.60	9.13	151.61	3.02	1.04	1.19
20.69	14.52	16.89	8.95	151.17	3.01	1.04	1.21
20.70	14.76	17.19	8.77	150.67	3.00	0.83	0.83
20.71	15.00	17.48	8.59	150.14	2.99	0.83	0.83
20.72	15.21	17.74	8.43	149.60	2.98	0.83	0.83
20.73	15.39	17.96	8.30	149.09	2.97	0.83	0.83
20.74	15.46	18.05	8.23	148.46	2.97	0.82	0.82
20.75	15.44	18.01	8.20	147.64	2.96	0.82	0.82
20.76	15.34	17.88	8.20	146.55	2.96	0.82	0.82
20.77	15.23	17.73	8.19	145.33	2.96	0.82	0.82
20.78	15.11	17.58	8.19	144.03	2.96	0.82	0.82
20.79	14.99	17.42	8.19	142.72	2.96	0.82	0.82
20.80	14.88	17.27	8.19	141.47	2.96	0.82	0.82
20.81	14.77	17.13	8.19	140.34	2.96	0.81	0.81
20.82	14.66	16.98	8.21	139.41	2.97	0.81	0.81
20.83	14.48	16.74	8.28	138.66	2.97	0.81	0.81
20.84	14.21	16.40	8.41	137.97	2.98	0.81	0.81
20.85	13.86	15.96	8.60	137.19	2.99	0.81	0.81
20.86	13.48	15.47	8.81	136.27	3.00	0.83	1.11
20.87	13.08	14.96	9.04	135.27	3.01	0.81	1.07
20.88	12.69	14.46	9.28	134.23	3.03	0.79	1.03
20.89	12.31	13.99	9.52	133.20	3.04	0.77	1.00
20.90	11.98	13.57	9.75	132.24	3.05	0.76	0.97
20.91	11.73	13.24	9.94	131.61	3.06	0.74	0.95
20.92	11.52	12.97	10.12	131.32	3.07	0.74	0.93
20.93	11.33	12.73	10.32	131.30	3.08	0.73	0.91
20.94	11.11	12.45	10.54	131.28	3.10	0.73	0.89
20.95	10.88	12.15	10.80	131.22	3.11	0.72	0.87
20.96	10.64	11.85	11.07	131.11	3.12	0.72	0.85
20.97	10.40	11.55	11.34	130.94	3.14	0.71	0.82
20.98	10.19	11.27	11.60	130.75	3.15	0.70	0.81
20.99	10.00	11.03	11.83	130.54	3.16	0.70	0.79
21.00	9.83	10.82	12.04	130.28	3.17	0.69	0.77
21.01	9.66	10.60	12.26	129.95	3.18	0.69	0.76
21.02	9.46	10.35	12.51	129.51	3.19	0.68	0.74
21.03	9.24	10.07	12.81	128.97	3.20	0.67	0.72
21.04	9.00	9.76	13.14	128.35	3.22	0.66	0.70
21.05	8.76	9.46	13.49	127.67	3.23	0.65	0.68
21.06	8.53	9.17	13.85	126.97	3.25	0.64	0.66
21.07	8.33	8.91	14.18	126.29	3.26	0.63	0.64
21.08	8.16	8.70	14.45	125.71	3.27	0.62	0.62
21.09	8.04	8.54	14.66	125.20	3.28	0.61	0.61
21.10	7.94	8.41	14.83	124.72	3.29	0.61	0.60
21.11	7.83	8.28	15.00	124.17	3.29	0.60	0.59
21.12	7.72	8.13	15.20	123.56	3.30	0.59	0.58

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
21.13	7.60	7.98	15.41	122.92	3.31	0.59	0.57
21.14	7.48	7.83	15.62	122.27	3.32	0.58	0.56
21.15	7.37	7.69	15.83	121.65	3.32	0.57	0.55
21.16	7.27	7.56	16.02	121.09	3.33	0.56	0.54
21.17	7.27	7.55	16.03	121.02	3.33	0.56	0.54
21.18	7.38	7.69	15.81	121.55	3.32	0.57	0.55
21.19	7.62	7.98	15.37	122.68	3.31	0.58	0.57
21.20	7.91	8.34	14.87	124.00	3.29	0.60	0.60
21.21	8.22	8.73	14.36	125.35	3.27	0.62	0.62
21.22	8.54	9.12	13.88	126.65	3.25	0.64	0.65
21.23	8.85	9.51	13.45	127.84	3.23	0.65	0.68
21.24	9.14	9.86	13.07	128.86	3.21	0.67	0.70
21.25	9.40	10.18	12.74	129.75	3.20	0.68	0.73
21.26	9.72	10.58	12.37	130.84	3.18	0.69	0.76
21.27	10.15	11.11	11.91	132.25	3.16	0.72	0.79
21.28	10.72	11.81	11.35	133.99	3.14	0.75	0.84
21.29	11.36	12.60	10.77	135.74	3.11	0.78	0.90
21.30	12.04	13.44	10.22	137.37	3.08	0.81	0.96
21.31	12.72	14.29	9.71	138.77	3.05	0.84	1.02
21.32	13.38	15.09	9.27	139.91	3.03	0.87	1.08
21.33	13.97	15.82	8.90	140.77	3.01	0.89	1.13
21.34	14.44	16.40	8.62	141.29	2.99	0.81	0.81
21.35	14.81	16.86	8.39	141.46	2.98	0.82	0.82
21.36	15.13	17.25	8.19	141.33	2.96	0.81	0.81
21.37	15.48	17.68	7.98	141.01	2.95	0.81	0.81
21.38	15.87	18.14	7.75	140.59	2.94	0.81	0.81
21.39	16.27	18.63	7.52	140.07	2.92	0.81	0.81
21.40	16.66	19.09	7.30	139.41	2.91	0.81	0.81
21.41	17.03	19.52	7.11	138.70	2.89	0.81	0.81
21.42	17.36	19.89	6.94	138.03	2.88	0.81	0.81
21.43	17.66	20.24	6.80	137.61	2.87	0.81	0.81
21.44	17.99	20.62	6.67	137.48	2.86	0.81	0.81
21.45	18.39	21.08	6.53	137.58	2.85	0.81	0.81
21.46	18.86	21.62	6.37	137.69	2.84	0.81	0.81
21.47	19.36	22.20	6.20	137.75	2.83	0.81	0.81
21.48	19.88	22.79	6.04	137.76	2.82	0.81	0.81
21.49	20.38	23.37	5.89	137.72	2.80	0.81	0.81
21.50	20.84	23.90	5.76	137.64	2.79	0.81	0.81
21.51	21.21	24.32	5.65	137.52	2.78	0.81	0.81
21.52	21.44	24.57	5.59	137.36	2.78	0.81	0.81
21.53	21.53	24.67	5.56	137.15	2.78	0.81	0.81
21.54	21.54	24.68	5.55	136.88	2.77	0.81	0.81
21.55	21.56	24.68	5.53	136.57	2.77	0.81	0.81
21.56	21.57	24.69	5.52	136.25	2.77	0.81	0.81
21.57	21.59	24.70	5.50	135.92	2.77	0.81	0.81
21.58	21.60	24.70	5.49	135.61	2.77	0.81	0.81
21.59	21.62	24.71	5.48	135.32	2.77	0.81	0.81
21.60	21.54	24.61	5.49	135.05	2.77	0.81	0.81

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
21.61	21.27	24.29	5.54	134.69	2.77	0.81	0.81
21.62	20.78	23.71	5.66	134.21	2.78	0.80	0.80
21.63	20.13	22.94	5.82	133.56	2.80	0.80	0.80
21.64	19.41	22.10	6.01	132.79	2.81	0.80	0.80
21.65	18.67	21.22	6.22	131.92	2.83	0.80	0.80
21.66	17.93	20.35	6.44	130.98	2.85	0.80	0.80
21.67	17.24	19.53	6.66	130.02	2.86	0.80	0.80
21.68	16.63	18.81	6.86	129.12	2.88	0.80	0.80
21.69	16.15	18.24	7.05	128.50	2.89	0.80	0.80
21.70	15.73	17.74	7.22	128.15	2.90	0.80	0.80
21.71	15.33	17.26	7.42	128.01	2.91	0.80	0.80
21.72	14.86	16.69	7.65	127.76	2.93	0.80	0.80
21.73	14.36	16.07	7.93	127.38	2.95	0.79	0.79
21.74	13.85	15.44	8.22	126.91	2.97	0.79	0.79
21.75	13.35	14.82	8.52	126.35	2.98	0.79	0.79
21.76	12.89	14.26	8.82	125.74	3.00	0.70	1.02
21.77	12.50	13.78	9.09	125.16	3.02	0.68	0.98
21.78	12.16	13.36	9.33	124.62	3.03	0.67	0.95
21.79	11.83	12.94	9.59	124.05	3.05	0.66	0.92
21.80	11.45	12.47	9.89	123.36	3.06	0.65	0.89
21.81	11.03	11.95	10.25	122.50	3.08	0.63	0.85
21.82	10.58	11.40	10.66	121.49	3.10	0.61	0.81
21.83	10.12	10.84	11.10	120.36	3.12	0.59	0.77
21.84	9.69	10.31	11.56	119.18	3.15	0.57	0.74
21.85	9.31	9.83	12.00	118.02	3.17	0.56	0.70
21.86	8.99	9.44	12.39	117.00	3.18	0.54	0.67
21.87	8.72	9.11	12.74	116.07	3.20	0.53	0.65
21.88	8.46	8.79	13.09	115.12	3.22	0.52	0.63
21.89	8.17	8.44	13.51	114.00	3.23	0.50	0.60
21.90	7.86	8.05	14.00	112.71	3.25	0.49	0.57
21.91	7.53	7.64	14.56	111.28	3.28	0.47	0.55
21.92	7.20	7.24	15.16	109.78	3.30	0.45	0.52
21.93	6.89	6.87	15.77	108.30	3.32	0.44	0.49
21.94	6.63	6.54	16.36	106.94	3.34	0.42	0.47
21.95	6.44	6.31	16.79	105.86	3.36	0.41	0.45
21.96	6.31	6.15	17.08	104.99	3.37	0.41	0.44
21.97	6.22	6.04	17.25	104.21	3.37	0.40	0.43
21.98	6.12	5.92	17.46	103.32	3.38	0.39	0.42
21.99	6.02	5.79	17.68	102.36	3.39	0.38	0.41
22.00	5.91	5.66	17.92	101.38	3.40	0.37	0.40
22.01	5.81	5.53	18.16	100.42	3.40	0.36	0.39
22.02	5.71	5.41	18.39	99.54	3.41	0.35	0.39
22.03	5.64	5.32	18.58	98.80	3.42	0.35	0.38
22.04	5.59	5.26	18.67	98.23	3.42	0.34	0.38
22.05	5.58	5.24	18.66	97.78	3.42	0.34	0.37
22.06	5.58	5.24	18.58	97.32	3.42	0.34	0.37
22.07	5.58	5.24	18.49	96.82	3.41	0.33	0.37
22.08	5.58	5.23	18.39	96.28	3.41	0.33	0.37

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
22.09	5.58	5.23	18.29	95.73	3.41	0.32	0.37
22.10	5.58	5.23	18.20	95.21	3.41	0.32	0.37
22.11	5.58	5.23	18.12	94.74	3.40	0.32	0.37
22.12	5.58	5.23	18.05	94.34	3.40	0.31	0.37
22.13	5.58	5.22	17.99	93.99	3.40	0.31	0.37
22.14	5.58	5.22	17.93	93.64	3.40	0.31	0.37
22.15	5.58	5.22	17.86	93.24	3.39	0.31	0.37
22.16	5.58	5.22	17.78	92.80	3.39	0.30	0.37
22.17	5.58	5.22	17.70	92.34	3.39	0.30	0.37
22.18	5.58	5.21	17.62	91.89	3.39	0.29	0.37
22.19	5.58	5.21	17.55	91.46	3.38	0.29	0.37
22.20	5.58	5.21	17.48	91.08	3.38	0.29	0.37
22.21	5.57	5.20	17.46	90.74	3.38	0.29	0.37
22.22	5.54	5.16	17.50	90.37	3.38	0.28	0.37
22.23	5.50	5.11	17.60	89.94	3.39	0.28	0.37
22.24	5.45	5.05	17.71	89.44	3.39	0.28	0.36
22.25	5.40	4.98	17.84	88.90	3.39	0.27	0.36
22.26	5.35	4.92	17.96	88.36	3.40	0.27	0.35
22.27	5.29	4.85	18.09	87.83	3.40	0.26	0.35
22.28	5.25	4.80	18.21	87.34	3.41	0.26	0.34
22.29	5.21	4.76	18.29	86.98	3.41	0.26	0.34
22.30	5.22	4.76	18.24	86.93	3.41	0.26	0.34
22.31	5.28	4.83	18.06	87.19	3.40	0.26	0.34
22.32	5.37	4.93	17.77	87.67	3.39	0.26	0.35
22.33	5.47	5.05	17.46	88.21	3.38	0.27	0.36
22.34	5.57	5.18	17.14	88.76	3.37	0.27	0.37
22.35	5.68	5.31	16.83	89.31	3.36	0.28	0.38
22.36	5.78	5.42	16.56	89.82	3.35	0.28	0.39
22.37	5.87	5.53	16.32	90.26	3.34	0.28	0.40
22.38	5.94	5.62	16.14	90.61	3.34	0.29	0.40
22.39	6.00	5.68	16.01	90.88	3.33	0.29	0.41
22.40	6.04	5.73	15.91	91.11	3.33	0.29	0.41
22.41	6.09	5.78	15.80	91.37	3.32	0.29	0.41
22.42	6.14	5.84	15.69	91.65	3.32	0.30	0.42
22.43	6.19	5.90	15.57	91.94	3.31	0.30	0.42
22.44	6.24	5.97	15.46	92.22	3.31	0.30	0.43
22.45	6.29	6.02	15.36	92.49	3.31	0.30	0.43
22.46	6.34	6.07	15.27	92.71	3.30	0.31	0.43
22.47	6.38	6.12	15.18	92.95	3.30	0.31	0.44
22.48	6.43	6.18	15.09	93.25	3.30	0.31	0.44
22.49	6.49	6.25	14.97	93.63	3.29	0.31	0.45
22.50	6.57	6.34	14.84	94.07	3.29	0.32	0.45
22.51	6.64	6.43	14.70	94.54	3.28	0.32	0.46
22.52	6.73	6.53	14.56	95.02	3.28	0.33	0.47
22.53	6.80	6.62	14.43	95.48	3.27	0.33	0.47
22.54	6.87	6.70	14.32	95.89	3.27	0.33	0.48
22.55	6.93	6.76	14.23	96.22	3.26	0.34	0.48
22.56	6.96	6.80	14.18	96.42	3.26	0.34	0.49

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
22.57	6.97	6.81	14.17	96.52	3.26	0.34	0.49
22.58	6.97	6.81	14.18	96.56	3.26	0.34	0.49
22.59	6.97	6.81	14.20	96.62	3.26	0.34	0.49
22.60	6.97	6.80	14.21	96.68	3.26	0.34	0.49
22.61	6.97	6.80	14.22	96.73	3.26	0.34	0.49
22.62	6.97	6.80	14.24	96.79	3.26	0.34	0.49
22.63	6.97	6.80	14.25	96.83	3.26	0.34	0.49
22.64	6.95	6.76	14.30	96.74	3.27	0.34	0.48
22.65	6.87	6.67	14.44	96.39	3.27	0.34	0.48
22.66	6.75	6.52	14.69	95.73	3.28	0.33	0.47
22.67	6.58	6.32	15.01	94.87	3.29	0.32	0.45
22.68	6.40	6.10	15.39	93.91	3.31	0.31	0.44
22.69	6.21	5.88	15.81	92.89	3.32	0.31	0.42
22.70	6.03	5.65	16.25	91.86	3.34	0.30	0.40
22.71	5.86	5.45	16.68	90.88	3.35	0.29	0.39
22.72	5.71	5.27	17.09	90.00	3.37	0.28	0.38
22.73	5.62	5.16	17.34	89.43	3.38	0.27	0.37
22.74	5.58	5.11	17.45	89.12	3.38	0.27	0.36
22.75	5.58	5.10	17.44	89.02	3.38	0.27	0.36
22.76	5.58	5.10	17.43	88.91	3.38	0.27	0.36
22.77	5.58	5.10	17.41	88.79	3.38	0.27	0.36
22.78	5.58	5.10	17.39	88.66	3.38	0.27	0.36
22.79	5.58	5.10	17.37	88.54	3.38	0.27	0.36
22.80	5.58	5.09	17.36	88.43	3.38	0.27	0.36
22.81	5.58	5.09	17.34	88.33	3.38	0.27	0.36
22.82	5.58	5.09	17.33	88.22	3.38	0.27	0.36
22.83	5.58	5.09	17.31	88.10	3.38	0.27	0.36
22.84	5.58	5.09	17.29	87.94	3.38	0.27	0.36
22.85	5.58	5.09	17.26	87.77	3.37	0.26	0.36
22.86	5.58	5.08	17.23	87.58	3.37	0.26	0.36
22.87	5.58	5.08	17.20	87.40	3.37	0.26	0.36
22.88	5.58	5.08	17.17	87.22	3.37	0.26	0.36
22.89	5.58	5.08	17.15	87.07	3.37	0.26	0.36
22.90	5.58	5.08	17.13	86.96	3.37	0.26	0.36
22.91	5.58	5.07	17.12	86.90	3.37	0.26	0.36
22.92	5.58	5.07	17.13	86.88	3.37	0.26	0.36
22.93	5.58	5.07	17.13	86.87	3.37	0.26	0.36
22.94	5.58	5.07	17.14	86.86	3.37	0.26	0.36
22.95	5.58	5.07	17.14	86.85	3.37	0.26	0.36
22.96	5.58	5.07	17.15	86.84	3.37	0.26	0.36
22.97	5.58	5.06	17.15	86.84	3.37	0.26	0.36
22.98	5.58	5.06	17.15	86.84	3.37	0.26	0.36
22.99	5.64	5.13	17.00	87.24	3.37	0.26	0.37
23.00	5.77	5.28	16.68	88.13	3.35	0.27	0.38
23.01	5.98	5.54	16.18	89.56	3.34	0.28	0.40
23.02	6.23	5.82	15.65	91.17	3.32	0.29	0.42
23.03	6.49	6.13	15.14	92.86	3.30	0.31	0.44
23.04	6.76	6.45	14.66	94.55	3.28	0.32	0.46

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
23.05	7.02	6.75	14.24	96.14	3.26	0.34	0.48
23.06	7.25	7.03	13.89	97.57	3.25	0.35	0.50
23.07	7.44	7.25	13.62	98.73	3.24	0.36	0.52
23.08	7.58	7.41	13.45	99.63	3.23	0.37	0.53
23.09	7.67	7.52	13.35	100.40	3.23	0.38	0.54
23.10	7.76	7.62	13.27	101.20	3.22	0.38	0.54
23.11	7.87	7.74	13.19	102.10	3.22	0.39	0.55
23.12	7.97	7.86	13.10	103.05	3.22	0.40	0.56
23.13	8.08	7.99	13.02	103.99	3.21	0.41	0.57
23.14	8.18	8.10	12.94	104.88	3.21	0.42	0.58
23.15	8.27	8.21	12.88	105.68	3.21	0.43	0.59
23.16	8.32	8.27	12.85	106.25	3.21	0.43	0.59
23.17	8.33	8.28	12.88	106.58	3.21	0.44	0.59
23.18	8.30	8.24	12.96	106.75	3.21	0.44	0.59
23.19	8.25	8.18	13.07	106.88	3.21	0.44	0.58
23.20	8.20	8.11	13.19	107.03	3.22	0.44	0.58
23.21	8.15	8.05	13.32	107.17	3.23	0.44	0.57
23.22	8.10	7.98	13.44	107.30	3.23	0.44	0.57
23.23	8.05	7.92	13.56	107.42	3.24	0.44	0.57
23.24	8.01	7.87	13.66	107.53	3.24	0.44	0.56
23.25	8.00	7.87	13.70	107.79	3.24	0.44	0.56
23.26	8.05	7.91	13.68	108.26	3.24	0.45	0.57
23.27	8.13	8.01	13.60	108.98	3.24	0.45	0.57
23.28	8.23	8.13	13.51	109.80	3.23	0.46	0.58
23.29	8.34	8.25	13.42	110.69	3.23	0.47	0.59
23.30	8.44	8.37	13.33	111.58	3.23	0.48	0.60
23.31	8.55	8.49	13.25	112.44	3.22	0.49	0.61
23.32	8.64	8.59	13.17	113.22	3.22	0.50	0.61
23.33	8.72	8.69	13.11	113.89	3.22	0.51	0.62
23.34	8.79	8.77	13.06	114.49	3.21	0.51	0.63
23.35	8.87	8.86	13.00	115.12	3.21	0.52	0.63
23.36	8.96	8.96	12.93	115.84	3.21	0.53	0.64
23.37	9.06	9.08	12.85	116.65	3.21	0.54	0.65
23.38	9.17	9.20	12.77	117.51	3.20	0.54	0.66
23.39	9.28	9.32	12.70	118.35	3.20	0.55	0.67
23.40	9.38	9.43	12.63	119.15	3.20	0.56	0.67
23.41	9.47	9.54	12.57	119.86	3.19	0.57	0.68
23.42	9.54	9.62	12.52	120.43	3.19	0.58	0.69
23.43	9.62	9.71	12.46	120.90	3.19	0.58	0.69
23.44	9.70	9.80	12.38	121.34	3.18	0.59	0.70
23.45	9.79	9.91	12.30	121.84	3.18	0.60	0.71
23.46	9.90	10.02	12.21	122.38	3.18	0.60	0.72
23.47	10.00	10.15	12.12	122.93	3.17	0.61	0.72
23.48	10.11	10.26	12.03	123.47	3.17	0.62	0.73
23.49	10.21	10.37	11.95	123.97	3.16	0.62	0.74
23.50	10.29	10.47	11.88	124.40	3.16	0.63	0.75
23.51	10.38	10.56	11.81	124.76	3.16	0.63	0.75
23.52	10.47	10.67	11.72	125.09	3.15	0.64	0.76

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
23.53	10.59	10.81	11.61	125.45	3.15	0.64	0.77
23.54	10.72	10.96	11.48	125.86	3.14	0.65	0.78
23.55	10.87	11.13	11.35	126.28	3.14	0.66	0.79
23.56	11.02	11.29	11.22	126.70	3.13	0.66	0.81
23.57	11.16	11.46	11.09	127.10	3.12	0.67	0.82
23.58	11.29	11.60	10.99	127.45	3.12	0.68	0.83
23.59	11.39	11.72	10.90	127.74	3.11	0.68	0.84
23.60	11.48	11.82	10.83	128.00	3.11	0.68	0.84
23.61	11.56	11.91	10.77	128.27	3.11	0.69	0.85
23.62	11.66	12.02	10.70	128.59	3.10	0.69	0.86
23.63	11.76	12.13	10.63	128.95	3.10	0.70	0.87
23.64	11.86	12.25	10.56	129.32	3.10	0.70	0.87
23.65	11.97	12.37	10.48	129.68	3.09	0.71	0.88
23.66	12.07	12.48	10.42	130.02	3.09	0.72	0.89
23.67	12.16	12.58	10.36	130.32	3.09	0.72	0.90
23.68	12.21	12.64	10.33	130.55	3.09	0.72	0.90
23.69	12.23	12.65	10.34	130.74	3.09	0.73	0.90
23.70	12.20	12.62	10.38	130.91	3.09	0.73	0.90
23.71	12.17	12.57	10.43	131.10	3.09	0.73	0.90
23.72	12.13	12.52	10.49	131.31	3.09	0.73	0.89
23.73	12.09	12.47	10.55	131.53	3.10	0.73	0.89
23.74	12.05	12.42	10.60	131.73	3.10	0.73	0.89
23.75	12.01	12.38	10.66	131.92	3.10	0.73	0.88
23.76	11.99	12.34	10.70	132.11	3.10	0.73	0.88
23.77	12.06	12.43	10.68	132.73	3.10	0.74	0.89
23.78	12.26	12.65	10.58	133.90	3.10	0.76	0.90
23.79	12.59	13.03	10.42	135.68	3.09	0.78	0.93
23.80	12.96	13.45	10.24	137.70	3.08	0.81	0.96
23.81	13.35	13.90	10.06	139.83	3.07	0.85	0.99
23.82	13.75	14.36	9.89	141.98	3.06	0.88	1.03
23.83	14.14	14.80	9.73	144.03	3.05	0.91	1.06
23.84	14.49	15.20	9.60	145.88	3.05	0.94	1.09
23.85	14.77	15.52	9.50	147.36	3.04	0.97	1.11
23.86	14.96	15.74	9.43	148.48	3.04	0.98	1.12
23.87	15.11	15.91	9.39	149.39	3.03	0.99	1.14
23.88	15.25	16.06	9.36	150.31	3.03	1.01	1.15
23.89	15.40	16.23	9.33	151.34	3.03	1.02	1.16
23.90	15.56	16.41	9.29	152.43	3.03	1.04	1.17
23.91	15.72	16.59	9.25	153.50	3.03	1.06	1.18
23.92	15.87	16.75	9.22	154.52	3.03	1.07	1.20
23.93	16.00	16.90	9.20	155.42	3.02	1.09	1.21
23.94	16.04	16.94	9.20	155.86	3.02	1.10	1.21
23.95	15.96	16.85	9.24	155.74	3.03	1.09	1.20
23.96	15.76	16.60	9.34	155.06	3.03	1.08	1.19
23.97	15.49	16.29	9.46	154.17	3.04	1.06	1.16
23.98	15.21	15.96	9.60	153.18	3.05	1.04	1.14
23.99	14.91	15.61	9.74	152.14	3.05	1.02	1.12
24.00	14.63	15.28	9.89	151.11	3.06	1.00	1.09

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
24.01	14.36	14.97	10.03	150.13	3.07	0.99	1.07
24.02	14.14	14.70	10.15	149.29	3.08	0.97	1.05
24.03	13.99	14.53	10.24	148.71	3.08	0.96	1.04
24.04	13.91	14.43	10.28	148.33	3.08	0.95	1.03
24.05	13.86	14.37	10.30	148.07	3.08	0.95	1.03
24.06	13.81	14.31	10.33	147.78	3.09	0.95	1.02
24.07	13.76	14.24	10.35	147.47	3.09	0.94	1.02
24.08	13.71	14.18	10.38	147.15	3.09	0.94	1.01
24.09	13.66	14.11	10.40	146.85	3.09	0.93	1.01
24.10	13.61	14.06	10.43	146.57	3.09	0.93	1.00
24.11	13.56	13.99	10.46	146.31	3.09	0.92	1.00
24.12	13.48	13.89	10.51	145.98	3.09	0.92	0.99
24.13	13.35	13.75	10.59	145.56	3.10	0.91	0.98
24.14	13.19	13.56	10.69	145.01	3.10	0.90	0.97
24.15	13.02	13.35	10.82	144.40	3.11	0.89	0.95
24.16	12.83	13.13	10.95	143.75	3.12	0.88	0.94
24.17	12.64	12.92	11.08	143.10	3.12	0.87	0.92
24.18	12.47	12.71	11.21	142.47	3.13	0.86	0.91
24.19	12.32	12.53	11.33	141.90	3.14	0.85	0.89
24.20	12.18	12.37	11.43	141.43	3.14	0.84	0.88
24.21	12.05	12.22	11.54	141.01	3.15	0.83	0.87
24.22	11.91	12.05	11.67	140.58	3.15	0.83	0.86
24.23	11.74	11.85	11.82	140.08	3.16	0.82	0.85
24.24	11.56	11.64	11.98	139.52	3.17	0.81	0.83
24.25	11.37	11.42	12.16	138.93	3.17	0.80	0.82
24.26	11.19	11.21	12.34	138.34	3.18	0.79	0.80
24.27	11.02	11.01	12.51	137.78	3.19	0.78	0.79
24.28	10.88	10.85	12.65	137.32	3.20	0.77	0.78
24.29	10.85	10.81	12.70	137.31	3.20	0.77	0.77
24.30	10.91	10.88	12.67	137.79	3.20	0.78	0.78
24.31	11.06	11.05	12.56	138.72	3.19	0.79	0.79
24.32	11.24	11.24	12.43	139.77	3.19	0.80	0.80
24.33	11.42	11.45	12.30	140.89	3.18	0.82	0.82
24.34	11.61	11.66	12.18	142.00	3.18	0.84	0.83
24.35	11.79	11.86	12.06	143.07	3.17	0.85	0.85
24.36	11.95	12.04	11.96	144.03	3.17	0.87	0.86
24.37	12.09	12.19	11.88	144.83	3.16	0.88	0.87
24.38	12.22	12.34	11.80	145.56	3.16	0.89	0.88
24.39	12.35	12.49	11.72	146.32	3.15	0.90	0.89
24.40	12.52	12.67	11.62	147.18	3.15	0.91	0.90
24.41	12.69	12.87	11.51	148.14	3.14	0.93	0.92
24.42	12.88	13.07	11.41	149.14	3.14	0.94	0.93
24.43	13.07	13.28	11.31	150.12	3.13	0.96	0.95
24.44	13.24	13.47	11.21	151.04	3.13	0.97	0.96
24.45	13.39	13.64	11.13	151.85	3.13	0.98	0.97
24.46	13.50	13.75	11.08	152.35	3.12	0.99	0.98
24.47	13.54	13.80	11.05	152.55	3.12	1.00	0.99
24.48	13.55	13.81	11.05	152.50	3.12	0.99	0.99

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
24.49	13.55	13.80	11.04	152.39	3.12	0.99	0.99
24.50	13.55	13.80	11.04	152.28	3.12	0.99	0.99
24.51	13.55	13.79	11.03	152.16	3.12	0.99	0.99
24.52	13.55	13.79	11.03	152.05	3.12	0.99	0.98
24.53	13.55	13.78	11.02	151.94	3.12	0.99	0.98
24.54	13.55	13.77	11.02	151.83	3.12	0.99	0.98
24.55	13.52	13.74	11.03	151.55	3.12	0.98	0.98
24.56	13.46	13.67	11.05	151.06	3.12	0.97	0.98
24.57	13.38	13.57	11.08	150.34	3.12	0.96	0.97
24.58	13.28	13.45	11.12	149.52	3.13	0.95	0.96
24.59	13.17	13.32	11.16	148.66	3.13	0.94	0.95
24.60	13.06	13.20	11.20	147.79	3.13	0.93	0.94
24.61	12.96	13.08	11.24	146.96	3.13	0.91	0.93
24.62	12.87	12.97	11.27	146.20	3.13	0.90	0.93
24.63	12.79	12.88	11.30	145.55	3.13	0.89	0.92
24.64	12.72	12.79	11.33	144.93	3.14	0.89	0.91
24.65	12.64	12.69	11.36	144.26	3.14	0.88	0.91
24.66	12.55	12.58	11.40	143.47	3.14	0.87	0.90
24.67	12.44	12.47	11.44	142.60	3.14	0.85	0.89
24.68	12.34	12.34	11.48	141.70	3.14	0.84	0.88
24.69	12.23	12.22	11.53	140.80	3.14	0.83	0.87
24.70	12.13	12.10	11.57	139.96	3.15	0.82	0.86
24.71	12.04	12.00	11.60	139.22	3.15	0.81	0.86
24.72	11.97	11.91	11.64	138.58	3.15	0.80	0.85
24.73	11.89	11.82	11.67	137.98	3.15	0.79	0.84
24.74	11.81	11.72	11.72	137.33	3.15	0.78	0.84
24.75	11.71	11.61	11.77	136.59	3.16	0.77	0.83
24.76	11.61	11.49	11.82	135.78	3.16	0.76	0.82
24.77	11.50	11.36	11.88	134.95	3.16	0.75	0.81
24.78	11.40	11.24	11.93	134.14	3.16	0.74	0.80
24.79	11.30	11.13	11.98	133.40	3.17	0.73	0.80
24.80	11.22	11.03	12.03	132.74	3.17	0.72	0.79
24.81	11.11	10.91	12.10	132.06	3.17	0.72	0.78
24.82	10.98	10.76	12.20	131.26	3.18	0.70	0.77
24.83	10.80	10.56	12.34	130.26	3.18	0.69	0.75
24.84	10.60	10.33	12.50	129.12	3.19	0.68	0.74
24.85	10.39	10.09	12.68	127.90	3.20	0.66	0.72
24.86	10.18	9.84	12.87	126.66	3.21	0.64	0.70
24.87	9.98	9.61	13.05	125.46	3.21	0.63	0.69
24.88	9.79	9.40	13.23	124.37	3.22	0.61	0.67
24.89	9.65	9.23	13.37	123.49	3.23	0.60	0.66
24.90	9.54	9.11	13.48	122.80	3.23	0.60	0.65
24.91	9.45	9.00	13.57	122.23	3.24	0.59	0.64
24.92	9.35	8.90	13.67	121.62	3.24	0.58	0.64
24.93	9.25	8.78	13.78	120.95	3.24	0.57	0.63
24.94	9.14	8.66	13.89	120.24	3.25	0.57	0.62
24.95	9.04	8.54	14.00	119.54	3.25	0.56	0.61
24.96	8.94	8.42	14.12	118.88	3.26	0.55	0.60

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
24.97	8.85	8.32	14.22	118.29	3.26	0.54	0.59
24.98	8.78	8.23	14.31	117.79	3.27	0.54	0.59
24.99	8.70	8.15	14.40	117.31	3.27	0.53	0.58
25.00	8.62	8.05	14.50	116.78	3.27	0.53	0.58
25.01	8.52	7.94	14.63	116.17	3.28	0.52	0.57
25.02	8.42	7.82	14.77	115.51	3.28	0.51	0.56
25.03	8.31	7.70	14.91	114.83	3.29	0.50	0.55
25.04	8.21	7.58	15.06	114.16	3.30	0.50	0.54
25.05	8.11	7.47	15.20	113.54	3.30	0.49	0.53
25.06	8.03	7.38	15.32	113.00	3.31	0.48	0.53
25.07	7.96	7.29	15.44	112.54	3.31	0.48	0.52
25.08	7.88	7.20	15.56	112.08	3.31	0.48	0.51
25.09	7.79	7.10	15.71	111.57	3.32	0.47	0.51
25.10	7.69	6.99	15.88	110.99	3.33	0.46	0.50
25.11	7.58	6.87	16.07	110.37	3.33	0.46	0.49
25.12	7.48	6.75	16.27	109.74	3.34	0.45	0.48
25.13	7.38	6.63	16.46	109.13	3.35	0.44	0.47
25.14	7.28	6.53	16.64	108.57	3.35	0.44	0.47
25.15	7.22	6.45	16.77	108.17	3.36	0.43	0.46
25.16	7.18	6.41	16.85	107.98	3.36	0.43	0.46
25.17	7.17	6.39	16.88	107.96	3.36	0.43	0.46
25.18	7.17	6.39	16.90	108.03	3.36	0.43	0.46
25.19	7.17	6.39	16.92	108.10	3.36	0.43	0.46
25.20	7.17	6.39	16.93	108.17	3.36	0.43	0.46
25.21	7.17	6.39	16.95	108.24	3.36	0.43	0.46
25.22	7.17	6.38	16.97	108.31	3.36	0.44	0.46
25.23	7.17	6.38	16.98	108.37	3.36	0.44	0.46
25.24	7.15	6.36	17.03	108.26	3.37	0.44	0.45
25.25	7.10	6.30	17.13	107.92	3.37	0.43	0.45
25.26	7.02	6.21	17.29	107.32	3.38	0.43	0.44
25.27	6.93	6.10	17.48	106.61	3.38	0.42	0.44
25.28	6.82	5.98	17.70	105.83	3.39	0.41	0.43
25.29	6.72	5.86	17.93	105.03	3.40	0.40	0.42
25.30	6.61	5.74	18.16	104.25	3.40	0.40	0.41
25.31	6.52	5.63	18.38	103.52	3.41	0.39	0.40
25.32	6.44	5.55	18.56	102.92	3.42	0.38	0.40
25.33	6.39	5.49	18.66	102.51	3.42	0.38	0.39
25.34	6.38	5.47	18.68	102.23	3.42	0.38	0.39
25.35	6.38	5.47	18.65	102.02	3.42	0.38	0.39
25.36	6.38	5.47	18.61	101.79	3.42	0.37	0.39
25.37	6.38	5.47	18.58	101.54	3.42	0.37	0.39
25.38	6.38	5.46	18.54	101.29	3.42	0.37	0.39
25.39	6.38	5.46	18.50	101.05	3.42	0.37	0.39
25.40	6.38	5.46	18.47	100.84	3.41	0.37	0.39
25.41	6.39	5.47	18.41	100.73	3.41	0.36	0.39
25.42	6.43	5.51	18.29	100.82	3.41	0.37	0.39
25.43	6.50	5.59	18.09	101.10	3.40	0.37	0.40
25.44	6.59	5.69	17.84	101.50	3.39	0.37	0.41

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
25.45	6.69	5.80	17.57	101.93	3.38	0.38	0.41
25.46	6.80	5.92	17.30	102.36	3.38	0.38	0.42
25.47	6.90	6.03	17.04	102.78	3.37	0.39	0.43
25.48	7.00	6.14	16.80	103.16	3.36	0.39	0.44
25.49	7.09	6.23	16.60	103.49	3.35	0.39	0.45
25.50	7.17	6.31	16.44	103.79	3.35	0.40	0.45
25.51	7.24	6.39	16.28	104.11	3.34	0.40	0.46
25.52	7.32	6.49	16.11	104.50	3.33	0.40	0.46
25.53	7.42	6.59	15.93	104.94	3.33	0.41	0.47
25.54	7.53	6.70	15.73	105.42	3.32	0.41	0.48
25.55	7.63	6.82	15.53	105.90	3.31	0.42	0.49
25.56	7.74	6.93	15.35	106.35	3.31	0.42	0.50
25.57	7.83	7.03	15.18	106.77	3.30	0.43	0.50
25.58	7.91	7.12	15.04	107.13	3.29	0.43	0.51
25.59	7.99	7.20	14.94	107.56	3.29	0.43	0.51
25.60	8.06	7.28	14.84	108.11	3.29	0.44	0.52
25.61	8.15	7.38	14.75	108.81	3.28	0.45	0.53
25.62	8.25	7.49	14.64	109.61	3.28	0.45	0.53
25.63	8.36	7.60	14.53	110.45	3.27	0.46	0.54
25.64	8.47	7.71	14.43	111.30	3.27	0.47	0.55
25.65	8.57	7.82	14.33	112.10	3.27	0.48	0.56
25.66	8.66	7.92	14.24	112.82	3.26	0.49	0.57
25.67	8.72	7.99	14.19	113.38	3.26	0.49	0.57
25.68	8.76	8.03	14.18	113.79	3.26	0.50	0.57
25.69	8.77	8.03	14.20	114.10	3.26	0.50	0.57
25.70	8.77	8.03	14.25	114.43	3.26	0.50	0.57
25.71	8.77	8.03	14.30	114.79	3.27	0.51	0.57
25.72	8.77	8.02	14.35	115.16	3.27	0.51	0.57
25.73	8.77	8.02	14.40	115.53	3.27	0.51	0.57
25.74	8.77	8.02	14.45	115.87	3.27	0.52	0.57
25.75	8.77	8.02	14.49	116.16	3.27	0.52	0.57
25.76	8.79	8.04	14.49	116.48	3.27	0.52	0.57
25.77	8.84	8.09	14.45	116.88	3.27	0.53	0.58
25.78	8.92	8.18	14.36	117.40	3.27	0.53	0.58
25.79	9.02	8.28	14.25	118.01	3.26	0.54	0.59
25.80	9.12	8.39	14.14	118.66	3.26	0.55	0.60
25.81	9.23	8.51	14.03	119.32	3.25	0.56	0.61
25.82	9.33	8.62	13.92	119.96	3.25	0.56	0.62
25.83	9.43	8.72	13.82	120.54	3.25	0.57	0.62
25.84	9.51	8.81	13.74	121.03	3.24	0.58	0.63
25.85	9.58	8.88	13.67	121.47	3.24	0.58	0.63
25.86	9.66	8.97	13.60	121.91	3.24	0.59	0.64
25.87	9.75	9.06	13.51	122.42	3.23	0.59	0.65
25.88	9.85	9.17	13.42	122.99	3.23	0.60	0.65
25.89	9.96	9.28	13.32	123.59	3.23	0.61	0.66
25.90	10.06	9.39	13.22	124.19	3.22	0.61	0.67
25.91	10.16	9.50	13.13	124.75	3.22	0.62	0.68
25.92	10.25	9.60	13.05	125.26	3.21	0.63	0.69

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
25.93	10.36	9.71	12.96	125.83	3.21	0.63	0.69
25.94	10.53	9.89	12.81	126.67	3.20	0.64	0.71
25.95	10.77	10.15	12.60	127.88	3.19	0.66	0.72
25.96	11.07	10.48	12.35	129.37	3.18	0.68	0.75
25.97	11.41	10.84	12.08	130.97	3.17	0.70	0.77
25.98	11.75	11.21	11.83	132.62	3.16	0.72	0.80
25.99	12.10	11.58	11.59	134.20	3.15	0.75	0.83
26.00	12.42	11.93	11.37	135.66	3.14	0.77	0.85
26.01	12.70	12.23	11.20	136.92	3.13	0.79	0.87
26.02	12.89	12.44	11.08	137.82	3.12	0.80	0.89
26.03	13.02	12.57	11.01	138.45	3.12	0.81	0.90
26.04	13.11	12.66	10.97	138.94	3.12	0.82	0.90
26.05	13.20	12.77	10.93	139.49	3.12	0.82	0.91
26.06	13.31	12.88	10.88	140.09	3.11	0.83	0.92
26.07	13.42	12.99	10.83	140.70	3.11	0.84	0.93
26.08	13.52	13.10	10.79	141.28	3.11	0.85	0.94
26.09	13.61	13.20	10.75	141.82	3.11	0.86	0.94
26.10	13.68	13.26	10.73	142.20	3.11	0.86	0.95
26.11	13.65	13.22	10.76	142.23	3.11	0.87	0.94
26.12	13.53	13.09	10.84	141.90	3.11	0.86	0.93
26.13	13.33	12.86	10.98	141.28	3.12	0.85	0.92
26.14	13.10	12.61	11.14	140.57	3.13	0.83	0.90
26.15	12.86	12.35	11.32	139.80	3.13	0.82	0.88
26.16	12.62	12.09	11.50	139.01	3.14	0.81	0.86
26.17	12.39	11.84	11.68	138.25	3.15	0.79	0.85
26.18	12.19	11.61	11.85	137.54	3.16	0.78	0.83
26.19	12.05	11.45	11.97	137.08	3.17	0.77	0.82
26.20	11.97	11.37	12.05	136.93	3.17	0.77	0.81
26.21	11.96	11.34	12.08	137.08	3.17	0.77	0.81
26.22	11.96	11.34	12.11	137.35	3.17	0.78	0.81
26.23	11.96	11.34	12.14	137.65	3.17	0.78	0.81
26.24	11.96	11.33	12.17	137.96	3.17	0.78	0.81
26.25	11.96	11.33	12.20	138.26	3.18	0.79	0.81
26.26	11.96	11.33	12.23	138.55	3.18	0.79	0.81
26.27	11.96	11.32	12.26	138.79	3.18	0.79	0.81
26.28	11.98	11.34	12.26	139.09	3.18	0.80	0.81
26.29	12.03	11.39	12.24	139.50	3.18	0.80	0.81
26.30	12.11	11.48	12.20	140.07	3.18	0.81	0.82
26.31	12.21	11.58	12.15	140.73	3.17	0.82	0.83
26.32	12.32	11.69	12.10	141.43	3.17	0.83	0.84
26.33	12.42	11.80	12.04	142.15	3.17	0.84	0.84
26.34	12.53	11.91	11.99	142.85	3.17	0.85	0.85
26.35	12.62	12.01	11.95	143.48	3.16	0.86	0.86
26.36	12.70	12.09	11.91	143.99	3.16	0.87	0.86
26.37	12.78	12.17	11.86	144.35	3.16	0.87	0.87
26.38	12.85	12.25	11.81	144.60	3.16	0.87	0.87
26.39	12.94	12.34	11.73	144.83	3.15	0.88	0.88
26.40	13.04	12.45	11.66	145.07	3.15	0.88	0.89

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
26.41	13.15	12.56	11.57	145.33	3.15	0.89	0.90
26.42	13.26	12.67	11.49	145.58	3.14	0.89	0.90
26.43	13.36	12.77	11.42	145.81	3.14	0.90	0.91
26.44	13.45	12.86	11.35	146.02	3.14	0.90	0.92
26.45	13.51	12.93	11.30	146.09	3.13	0.90	0.92
26.46	13.54	12.96	11.26	145.97	3.13	0.90	0.93
26.47	13.55	12.96	11.24	145.65	3.13	0.90	0.93
26.48	13.55	12.96	11.21	145.23	3.13	0.89	0.93
26.49	13.55	12.95	11.18	144.76	3.13	0.89	0.93
26.50	13.55	12.95	11.14	144.28	3.13	0.88	0.92
26.51	13.55	12.94	11.11	143.80	3.12	0.88	0.92
26.52	13.55	12.94	11.08	143.36	3.12	0.87	0.92
26.53	13.55	12.94	11.05	142.97	3.12	0.87	0.92
26.54	13.56	12.94	11.03	142.70	3.12	0.86	0.92
26.55	13.59	12.97	10.99	142.55	3.12	0.86	0.93
26.56	13.63	13.01	10.95	142.46	3.12	0.86	0.93
26.57	13.68	13.06	10.90	142.37	3.11	0.86	0.93
26.58	13.73	13.11	10.85	142.27	3.11	0.86	0.94
26.59	13.78	13.16	10.80	142.16	3.11	0.86	0.94
26.60	13.84	13.21	10.75	142.06	3.11	0.86	0.94
26.61	13.88	13.26	10.71	141.96	3.10	0.86	0.95
26.62	13.91	13.29	10.68	141.84	3.10	0.86	0.95
26.63	13.90	13.27	10.68	141.65	3.10	0.86	0.95
26.64	13.85	13.20	10.70	141.35	3.10	0.85	0.94
26.65	13.76	13.10	10.76	140.95	3.11	0.85	0.94
26.66	13.65	12.99	10.81	140.50	3.11	0.84	0.93
26.67	13.55	12.87	10.88	140.03	3.11	0.83	0.92
26.68	13.44	12.76	10.94	139.55	3.12	0.82	0.91
26.69	13.34	12.64	11.00	139.10	3.12	0.82	0.90
26.70	13.25	12.54	11.06	138.69	3.12	0.81	0.90
26.71	13.17	12.45	11.11	138.29	3.12	0.81	0.89
26.72	13.07	12.34	11.17	137.83	3.13	0.80	0.88
26.73	12.95	12.21	11.24	137.24	3.13	0.79	0.87
26.74	12.81	12.06	11.32	136.53	3.14	0.78	0.86
26.75	12.66	11.89	11.42	135.76	3.14	0.77	0.85
26.76	12.50	11.71	11.52	134.95	3.14	0.76	0.84
26.77	12.34	11.54	11.62	134.15	3.15	0.75	0.82
26.78	12.19	11.38	11.72	133.41	3.15	0.73	0.81
26.79	12.07	11.24	11.81	132.75	3.16	0.73	0.80
26.80	11.99	11.16	11.86	132.30	3.16	0.72	0.80
26.81	11.96	11.12	11.87	132.00	3.16	0.72	0.79
26.82	11.96	11.11	11.86	131.79	3.16	0.71	0.79
26.83	11.96	11.11	11.84	131.56	3.16	0.71	0.79
26.84	11.95	11.11	11.82	131.32	3.16	0.71	0.79
26.85	11.95	11.10	11.80	131.06	3.16	0.71	0.79
26.86	11.95	11.10	11.79	130.82	3.16	0.70	0.79
26.87	11.95	11.10	11.77	130.60	3.16	0.70	0.79
26.88	11.98	11.12	11.74	130.53	3.15	0.70	0.79

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
26.89	12.11	11.25	11.64	130.92	3.15	0.70	0.80
26.90	12.35	11.50	11.46	131.80	3.14	0.72	0.82
26.91	12.68	11.86	11.22	133.09	3.13	0.74	0.85
26.92	13.06	12.26	10.97	134.49	3.12	0.76	0.88
26.93	13.46	12.68	10.72	135.92	3.11	0.78	0.91
26.94	13.86	13.09	10.49	137.32	3.09	0.80	0.94
26.95	14.24	13.49	10.28	138.61	3.08	0.83	0.96
26.96	14.57	13.84	10.09	139.73	3.07	0.85	0.99
26.97	14.77	14.05	9.99	140.34	3.07	0.86	1.00
26.98	14.79	14.06	9.98	140.30	3.07	0.86	1.00
26.99	14.64	13.90	10.04	139.64	3.07	0.84	0.99
27.00	14.43	13.67	10.15	138.72	3.08	0.83	0.98
27.01	14.20	13.42	10.26	137.70	3.08	0.81	0.96
27.02	13.96	13.16	10.38	136.65	3.09	0.80	0.94
27.03	13.72	12.91	10.51	135.60	3.09	0.78	0.92
27.04	13.50	12.67	10.62	134.62	3.10	0.77	0.91
27.05	13.31	12.46	10.73	133.76	3.11	0.75	0.89
27.06	13.08	12.22	10.87	132.81	3.11	0.74	0.87
27.07	12.78	11.89	11.07	131.63	3.12	0.73	0.85
27.08	12.37	11.46	11.35	130.06	3.14	0.70	0.82
27.09	11.90	10.96	11.70	128.21	3.15	0.67	0.78
27.10	11.40	10.43	12.10	126.17	3.17	0.65	0.74
27.11	10.90	9.89	12.54	124.02	3.19	0.62	0.71
27.12	10.41	9.37	13.01	121.88	3.21	0.59	0.67
27.13	9.96	8.90	13.47	119.86	3.23	0.56	0.64
27.14	9.63	8.54	13.85	118.32	3.25	0.54	0.61
27.15	9.48	8.38	14.04	117.69	3.26	0.53	0.60
27.16	9.50	8.40	14.05	117.95	3.26	0.54	0.60
27.17	9.61	8.51	13.95	118.73	3.25	0.55	0.61
27.18	9.74	8.64	13.84	119.60	3.25	0.56	0.62
27.19	9.87	8.78	13.72	120.52	3.24	0.57	0.63
27.20	10.00	8.92	13.62	121.43	3.24	0.58	0.64
27.21	10.13	9.05	13.52	122.29	3.23	0.59	0.65
27.22	10.24	9.16	13.43	123.05	3.23	0.60	0.65
27.23	10.32	9.24	13.37	123.57	3.23	0.61	0.66
27.24	10.35	9.28	13.35	123.83	3.23	0.61	0.66
27.25	10.36	9.28	13.35	123.89	3.23	0.61	0.66
27.26	10.36	9.28	13.35	123.91	3.23	0.61	0.66
27.27	10.36	9.28	13.36	123.93	3.23	0.61	0.66
27.28	10.36	9.27	13.37	123.95	3.23	0.61	0.66
27.29	10.36	9.27	13.37	123.97	3.23	0.61	0.66
27.30	10.36	9.27	13.38	123.99	3.23	0.61	0.66
27.31	10.36	9.26	13.39	124.00	3.23	0.61	0.66
27.32	10.36	9.26	13.39	123.99	3.23	0.61	0.66
27.33	10.36	9.26	13.39	123.95	3.23	0.61	0.66
27.34	10.36	9.25	13.39	123.89	3.23	0.61	0.66
27.35	10.36	9.25	13.38	123.81	3.23	0.61	0.66
27.36	10.36	9.25	13.38	123.73	3.23	0.61	0.66

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
27.37	10.36	9.25	13.37	123.65	3.23	0.61	0.66
27.38	10.36	9.24	13.37	123.58	3.23	0.61	0.66
27.39	10.36	9.24	13.37	123.50	3.23	0.60	0.66
27.40	10.39	9.27	13.34	123.58	3.23	0.60	0.66
27.41	10.50	9.38	13.23	124.08	3.22	0.61	0.67
27.42	10.71	9.60	13.03	125.06	3.21	0.62	0.69
27.43	11.01	9.91	12.76	126.43	3.20	0.64	0.71
27.44	11.34	10.25	12.48	127.93	3.19	0.66	0.73
27.45	11.68	10.61	12.21	129.46	3.18	0.68	0.76
27.46	12.03	10.96	11.94	130.97	3.16	0.70	0.78
27.47	12.35	11.30	11.71	132.36	3.15	0.72	0.81
27.48	12.64	11.60	11.51	133.57	3.14	0.74	0.83
27.49	12.89	11.86	11.35	134.63	3.14	0.76	0.85
27.50	13.13	12.11	11.21	135.70	3.13	0.77	0.86
27.51	13.40	12.38	11.06	136.91	3.12	0.79	0.88
27.52	13.71	12.70	10.89	138.33	3.11	0.81	0.91
27.53	14.05	13.05	10.72	139.85	3.11	0.83	0.93
27.54	14.39	13.41	10.55	141.40	3.10	0.86	0.96
27.55	14.73	13.76	10.39	142.91	3.09	0.88	0.98
27.56	15.05	14.08	10.25	144.29	3.08	0.90	1.01
27.57	15.31	14.35	10.13	145.44	3.08	0.92	1.03
27.58	15.39	14.43	10.12	145.96	3.07	0.93	1.03
27.59	15.28	14.31	10.20	145.89	3.08	0.92	1.02
27.60	14.99	14.01	10.37	145.30	3.09	0.91	1.00
27.61	14.67	13.67	10.58	144.60	3.10	0.90	0.98
27.62	14.33	13.31	10.81	143.82	3.11	0.88	0.95
27.63	13.98	12.94	11.05	142.98	3.12	0.87	0.92
27.64	13.65	12.59	11.29	142.14	3.13	0.85	0.90
27.65	13.35	12.27	11.52	141.34	3.14	0.84	0.88
27.66	13.08	11.99	11.73	140.58	3.15	0.82	0.86
27.67	12.79	11.69	11.95	139.71	3.16	0.81	0.83
27.68	12.46	11.33	12.23	138.59	3.18	0.79	0.81
27.69	12.05	10.90	12.58	137.16	3.19	0.77	0.78
27.70	11.59	10.42	13.00	135.49	3.21	0.75	0.74
27.71	11.11	9.92	13.47	133.66	3.23	0.72	0.71
27.72	10.63	9.42	13.98	131.75	3.25	0.69	0.67
27.73	10.18	8.95	14.51	129.85	3.27	0.67	0.64
27.74	9.79	8.53	15.01	128.09	3.29	0.64	0.61
27.75	9.52	8.25	15.38	126.91	3.31	0.62	0.59
27.76	9.39	8.11	15.58	126.37	3.31	0.62	0.58
27.77	9.37	8.09	15.63	126.41	3.32	0.62	0.58
27.78	9.37	8.09	15.65	126.58	3.32	0.62	0.58
27.79	9.37	8.08	15.68	126.77	3.32	0.63	0.58
27.80	9.37	8.08	15.71	126.96	3.32	0.63	0.58
27.81	9.37	8.08	15.74	127.15	3.32	0.63	0.58
27.82	9.37	8.08	15.77	127.32	3.32	0.63	0.58
27.83	9.37	8.08	15.78	127.50	3.32	0.63	0.58
27.84	9.44	8.15	15.71	127.96	3.32	0.64	0.58

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
27.85	9.59	8.30	15.52	128.79	3.31	0.65	0.59
27.86	9.81	8.53	15.24	130.02	3.30	0.66	0.61
27.87	10.07	8.80	14.94	131.40	3.29	0.68	0.63
27.88	10.35	9.08	14.63	132.84	3.28	0.70	0.65
27.89	10.63	9.37	14.33	134.27	3.27	0.72	0.67
27.90	10.90	9.64	14.06	135.62	3.26	0.74	0.69
27.91	11.14	9.89	13.83	136.82	3.25	0.75	0.71
27.92	11.34	10.09	13.65	137.75	3.24	0.77	0.72
27.93	11.49	10.24	13.51	138.39	3.23	0.78	0.73
27.94	11.61	10.37	13.39	138.82	3.23	0.78	0.74
27.95	11.74	10.49	13.27	139.21	3.22	0.79	0.75
27.96	11.88	10.63	13.13	139.63	3.22	0.79	0.76
27.97	12.02	10.78	12.99	140.06	3.21	0.80	0.77
27.98	12.17	10.93	12.85	140.48	3.21	0.81	0.78
27.99	12.31	11.07	12.73	140.86	3.20	0.81	0.79
28.00	12.43	11.19	12.62	141.20	3.20	0.82	0.80
28.01	12.48	11.24	12.56	141.24	3.19	0.82	0.80
28.02	12.46	11.22	12.56	140.88	3.19	0.82	0.80
28.03	12.36	11.11	12.62	140.12	3.19	0.81	0.79
28.04	12.23	10.97	12.69	139.17	3.20	0.79	0.78
28.05	12.08	10.82	12.77	138.14	3.20	0.78	0.77
28.06	11.94	10.66	12.86	137.08	3.21	0.77	0.76
28.07	11.79	10.51	12.94	136.04	3.21	0.75	0.75
28.08	11.66	10.37	13.03	135.08	3.21	0.74	0.74
28.09	11.55	10.25	13.10	134.25	3.22	0.73	0.73
28.10	11.44	10.14	13.17	133.50	3.22	0.72	0.72
28.11	11.34	10.03	13.24	132.74	3.22	0.71	0.72
28.12	11.22	9.90	13.32	131.87	3.23	0.70	0.71
28.13	11.08	9.76	13.41	130.88	3.23	0.69	0.70
28.14	10.94	9.61	13.52	129.83	3.23	0.67	0.69
28.15	10.79	9.45	13.62	128.76	3.24	0.66	0.68
28.16	10.65	9.30	13.73	127.74	3.24	0.65	0.66
28.17	10.52	9.17	13.83	126.81	3.25	0.64	0.66
28.18	10.46	9.10	13.87	126.23	3.25	0.63	0.65
28.19	10.53	9.17	13.77	126.27	3.24	0.63	0.65
28.20	10.73	9.38	13.54	126.92	3.23	0.64	0.67
28.21	11.03	9.68	13.22	127.92	3.22	0.65	0.69
28.22	11.36	10.02	12.88	129.00	3.21	0.67	0.72
28.23	11.71	10.37	12.55	130.07	3.19	0.69	0.74
28.24	12.05	10.72	12.23	131.09	3.18	0.70	0.77
28.25	12.37	11.05	11.95	132.00	3.16	0.72	0.79
28.26	12.66	11.34	11.71	132.77	3.15	0.73	0.81
28.27	12.85	11.52	11.56	133.20	3.15	0.74	0.82
28.28	12.94	11.61	11.47	133.27	3.14	0.74	0.83
28.29	12.95	11.62	11.45	133.02	3.14	0.73	0.83
28.30	12.95	11.62	11.42	132.69	3.14	0.73	0.83
28.31	12.95	11.62	11.39	132.33	3.14	0.73	0.83
28.32	12.95	11.61	11.36	131.96	3.14	0.72	0.83

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
28.33	12.95	11.61	11.34	131.60	3.14	0.72	0.83
28.34	12.95	11.60	11.31	131.26	3.13	0.72	0.83
28.35	12.94	11.59	11.30	130.93	3.13	0.71	0.83
28.36	12.82	11.46	11.37	130.34	3.14	0.71	0.82
28.37	12.58	11.21	11.54	129.37	3.15	0.69	0.80
28.38	12.21	10.83	11.82	127.96	3.16	0.67	0.77
28.39	11.78	10.39	12.15	126.32	3.17	0.65	0.74
28.40	11.34	9.93	12.54	124.52	3.19	0.62	0.71
28.41	10.88	9.47	12.96	122.64	3.21	0.60	0.68
28.42	10.45	9.02	13.39	120.79	3.23	0.57	0.64
28.43	10.06	8.62	13.82	119.05	3.25	0.55	0.62
28.44	9.76	8.31	14.17	117.71	3.26	0.53	0.59
28.45	9.56	8.11	14.42	116.89	3.27	0.53	0.58
28.46	9.45	7.99	14.58	116.50	3.28	0.52	0.57
28.47	9.36	7.89	14.73	116.25	3.28	0.52	0.56
28.48	9.25	7.78	14.90	115.98	3.29	0.52	0.56
28.49	9.15	7.67	15.08	115.69	3.30	0.51	0.55
28.50	9.04	7.56	15.26	115.39	3.30	0.51	0.54
28.51	8.94	7.46	15.43	115.10	3.31	0.50	0.53
28.52	8.85	7.37	15.59	114.83	3.31	0.50	0.53
28.53	8.80	7.31	15.69	114.65	3.32	0.50	0.52
28.54	8.77	7.28	15.74	114.55	3.32	0.50	0.52
28.55	8.77	7.27	15.75	114.51	3.32	0.50	0.52
28.56	8.77	7.27	15.75	114.48	3.32	0.50	0.52
28.57	8.77	7.27	15.75	114.45	3.32	0.50	0.52
28.58	8.77	7.26	15.75	114.42	3.32	0.50	0.52
28.59	8.77	7.26	15.75	114.38	3.32	0.50	0.52
28.60	8.77	7.26	15.75	114.35	3.32	0.50	0.52
28.61	8.76	7.25	15.76	114.31	3.32	0.50	0.52
28.62	8.74	7.22	15.80	114.13	3.32	0.50	0.52
28.63	8.68	7.16	15.89	113.80	3.33	0.49	0.51
28.64	8.59	7.07	16.02	113.30	3.33	0.49	0.51
28.65	8.49	6.97	16.18	112.73	3.34	0.48	0.50
28.66	8.38	6.86	16.35	112.13	3.34	0.47	0.49
28.67	8.28	6.75	16.53	111.52	3.35	0.47	0.48
28.68	8.18	6.64	16.70	110.92	3.36	0.46	0.47
28.69	8.08	6.55	16.86	110.39	3.36	0.45	0.47
28.70	8.03	6.49	16.96	110.09	3.36	0.45	0.46
28.71	8.04	6.50	16.96	110.20	3.36	0.45	0.46
28.72	8.12	6.57	16.85	110.76	3.36	0.46	0.47
28.73	8.23	6.69	16.68	111.57	3.35	0.47	0.48
28.74	8.36	6.82	16.50	112.47	3.35	0.48	0.49
28.75	8.49	6.95	16.32	113.41	3.34	0.49	0.50
28.76	8.63	7.08	16.15	114.33	3.34	0.49	0.51
28.77	8.75	7.20	15.99	115.19	3.33	0.50	0.51
28.78	8.86	7.31	15.86	115.95	3.32	0.51	0.52
28.79	8.99	7.44	15.69	116.73	3.32	0.52	0.53
28.80	9.16	7.62	15.45	117.70	3.31	0.53	0.54

:: Strength loss calculation (Robertson (2009)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
28.81	9.41	7.86	15.13	118.95	3.30	0.54	0.56
28.82	9.70	8.15	14.77	120.39	3.28	0.56	0.58
28.83	10.01	8.47	14.40	121.91	3.27	0.58	0.60
28.84	10.33	8.79	14.05	123.44	3.26	0.60	0.63
28.85	10.64	9.10	13.72	124.89	3.24	0.62	0.65
28.86	10.93	9.39	13.44	126.20	3.23	0.63	0.67
28.87	11.18	9.63	13.21	127.27	3.22	0.65	0.69
28.88	11.38	9.83	13.02	128.03	3.21	0.66	0.70
28.89	11.56	10.02	12.84	128.59	3.20	0.67	0.72
28.90	11.76	10.21	12.64	129.06	3.20	0.67	0.73
28.91	11.99	10.44	12.42	129.57	3.19	0.68	0.75
28.92	12.22	10.67	12.19	130.09	3.18	0.69	0.76
28.93	12.46	10.91	11.97	130.58	3.17	0.70	0.78
28.94	12.69	11.14	11.76	131.03	3.16	0.71	0.80
28.95	12.90	11.34	11.59	131.41	3.15	0.71	0.81
28.96	13.09	11.53	11.42	131.77	3.14	0.72	0.82
28.97	13.32	11.76	11.25	132.22	3.13	0.73	0.84
28.98	13.60	12.04	11.03	132.80	3.12	0.74	0.86
28.99	13.95	12.38	10.78	133.50	3.11	0.75	0.88
29.00	14.33	12.77	10.51	134.21	3.09	0.76	0.91
29.01	14.73	13.17	10.25	134.90	3.08	0.78	0.94
29.02	15.13	13.56	10.00	135.54	3.07	0.79	0.97
29.03	15.50	13.93	9.77	136.08	3.06	0.80	0.99
29.04	15.82	14.25	9.58	136.53	3.05	0.82	1.02
29.05	16.12	14.55	9.42	136.97	3.04	0.82	1.04
29.06	16.44	14.86	9.25	137.50	3.03	0.84	1.06
29.07	16.81	15.23	9.07	138.17	3.02	0.85	1.09
29.08	17.25	15.66	8.87	138.93	3.00	0.87	1.12
29.09	17.72	16.13	8.66	139.70	2.99	0.81	0.81
29.10	18.20	16.61	8.46	140.44	2.98	0.81	0.81
29.11	18.67	17.07	8.27	141.12	2.97	0.81	0.81
29.12	19.09	17.50	8.10	141.70	2.96	0.82	0.82
29.13	19.45	17.85	7.96	142.15	2.95	0.82	0.82
29.14	19.72	18.12	7.86	142.44	2.94	0.82	0.82
29.15	19.93	18.32	7.78	142.62	2.94	0.82	0.82
29.16	20.13	18.52	7.71	142.75	2.93	0.82	0.82
29.17	20.36	18.74	7.63	142.88	2.93	0.82	0.82
29.18	20.60	18.97	7.54	143.01	2.92	0.82	0.82
29.19	20.83	19.20	7.45	143.13	2.92	0.82	0.82
29.20	21.06	19.43	7.37	143.23	2.91	0.82	0.82
29.21	21.27	19.63	7.30	143.31	2.91	0.82	0.82
29.22	21.41	19.76	7.26	143.36	2.90	0.82	0.82
29.23	21.46	19.80	7.24	143.39	2.90	0.82	0.82
29.24	21.42	19.76	7.26	143.40	2.90	0.82	0.82
29.25	21.36	19.69	7.28	143.41	2.91	0.82	0.82
29.26	21.28	19.61	7.31	143.41	2.91	0.82	0.82
29.27	21.20	19.52	7.35	143.42	2.91	0.82	0.82
29.28	21.12	19.43	7.38	143.42	2.91	0.82	0.82

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
29.29	21.05	19.35	7.41	143.42	2.91	0.82	0.82
29.30	20.98	19.28	7.44	143.42	2.92	0.82	0.82
29.31	20.95	19.25	7.45	143.42	2.92	0.82	0.82
29.32	20.97	19.26	7.44	143.42	2.92	0.82	0.82
29.33	21.03	19.32	7.42	143.41	2.91	0.82	0.82
29.34	21.11	19.39	7.40	143.41	2.91	0.82	0.82
29.35	21.18	19.46	7.37	143.41	2.91	0.82	0.82
29.36	21.26	19.53	7.34	143.41	2.91	0.82	0.82
29.37	21.34	19.60	7.32	143.40	2.91	0.82	0.82
29.38	21.41	19.67	7.29	143.39	2.91	0.82	0.82
29.39	21.49	19.74	7.26	143.38	2.90	0.82	0.82
29.40	21.66	19.90	7.20	143.37	2.90	0.82	0.82
29.41	21.94	20.18	7.10	143.34	2.89	0.82	0.82
29.42	22.34	20.57	6.97	143.27	2.88	0.82	0.82
29.43	22.79	21.00	6.82	143.15	2.87	0.82	0.82
29.44	23.27	21.47	6.66	142.98	2.86	0.82	0.82
29.45	23.75	21.93	6.51	142.76	2.85	0.82	0.82
29.46	24.20	22.37	6.37	142.51	2.84	0.82	0.82
29.47	24.61	22.77	6.25	142.25	2.83	0.82	0.82
29.48	24.97	23.11	6.15	142.09	2.82	0.82	0.82
29.49	25.30	23.43	6.07	142.09	2.82	0.82	0.82
29.50	25.66	23.77	5.98	142.27	2.81	0.82	0.82
29.51	26.08	24.18	5.89	142.53	2.80	0.82	0.82
29.52	26.54	24.63	5.80	142.80	2.80	0.82	0.82
29.53	27.02	25.09	5.70	143.05	2.79	0.82	0.82
29.54	27.49	25.55	5.61	143.29	2.78	0.82	0.82
29.55	27.94	25.98	5.52	143.49	2.77	0.82	0.82
29.56	28.32	26.35	5.45	143.65	2.77	0.82	0.82
29.57	28.60	26.61	5.41	143.85	2.76	0.82	0.82
29.58	28.79	26.79	5.38	144.14	2.76	0.82	0.82
29.59	28.92	26.91	5.37	144.57	2.76	0.82	0.82
29.60	29.06	27.04	5.36	145.06	2.76	0.82	0.82
29.61	29.22	27.19	5.35	145.60	2.76	0.82	0.82
29.62	29.38	27.34	5.35	146.14	2.76	0.82	0.82
29.63	29.54	27.49	5.34	146.67	2.76	0.82	0.82
29.64	29.68	27.62	5.33	147.16	2.76	0.82	0.82
29.65	29.78	27.71	5.33	147.58	2.76	0.82	0.82
29.66	29.78	27.70	5.34	147.98	2.76	0.82	0.82
29.67	29.66	27.58	5.38	148.42	2.76	0.82	0.82
29.68	29.46	27.38	5.44	148.94	2.77	0.83	0.83
29.69	29.24	27.15	5.51	149.52	2.77	0.83	0.83
29.70	29.00	26.91	5.58	150.11	2.78	0.83	0.83
29.71	28.76	26.67	5.65	150.69	2.78	0.83	0.83
29.72	28.53	26.44	5.72	151.23	2.79	0.83	0.83
29.73	28.33	26.23	5.78	151.70	2.79	0.83	0.83
29.74	28.12	26.03	5.85	152.18	2.80	0.83	0.83
29.75	27.87	25.77	5.93	152.81	2.81	0.83	0.83
29.76	27.53	25.43	6.04	153.67	2.82	0.83	0.83

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
29.77	27.10	25.01	6.18	154.68	2.83	0.83	0.83
29.78	26.64	24.55	6.34	155.74	2.84	0.83	0.83
29.79	26.16	24.08	6.51	156.76	2.85	0.84	0.84
29.80	25.69	23.61	6.68	157.71	2.86	0.84	0.84
29.81	25.25	23.17	6.84	158.53	2.87	0.84	0.84
29.82	24.86	22.79	6.99	159.19	2.88	0.84	0.84
29.83	24.69	22.61	7.07	159.85	2.89	0.84	0.84
29.84	24.73	22.65	7.09	160.64	2.89	0.84	0.84
29.85	24.98	22.88	7.07	161.67	2.89	0.84	0.84
29.86	25.27	23.16	7.03	162.86	2.89	0.84	0.84
29.87	25.58	23.46	7.00	164.15	2.89	0.85	0.85
29.88	25.90	23.77	6.96	165.46	2.88	0.85	0.85
29.89	26.21	24.07	6.93	166.72	2.88	0.85	0.85
29.90	26.50	24.34	6.90	167.88	2.88	0.85	0.85
29.91	26.75	24.58	6.87	168.83	2.88	0.85	0.85
29.92	27.05	24.86	6.82	169.50	2.87	0.85	0.85
29.93	27.42	25.21	6.74	169.97	2.87	0.85	0.85
29.94	27.89	25.66	6.64	170.36	2.86	0.85	0.85
29.95	28.41	26.17	6.53	170.77	2.85	0.85	0.85
29.96	28.97	26.70	6.41	171.17	2.84	0.85	0.85
29.97	29.53	27.24	6.30	171.53	2.83	0.85	0.85
29.98	30.06	27.74	6.19	171.85	2.83	0.85	0.85
29.99	30.53	28.20	6.10	172.11	2.82	0.86	0.86
30.00	30.85	28.49	6.05	172.36	2.82	0.86	0.86
30.01	30.96	28.59	6.04	172.67	2.81	0.86	0.86
30.02	30.89	28.52	6.07	173.11	2.82	0.86	0.86
30.03	30.75	28.37	6.12	173.64	2.82	0.86	0.86
30.04	30.60	28.22	6.17	174.21	2.83	0.86	0.86
30.05	30.44	28.05	6.23	174.80	2.83	0.86	0.86
30.06	30.28	27.89	6.29	175.37	2.83	0.86	0.86
30.07	30.13	27.74	6.34	175.89	2.84	0.86	0.86
30.08	30.00	27.61	6.39	176.33	2.84	0.86	0.86
30.09	29.94	27.54	6.42	176.70	2.84	0.86	0.86
30.10	29.94	27.54	6.43	177.04	2.84	0.86	0.86
30.11	30.01	27.59	6.43	177.41	2.84	0.86	0.86
30.12	30.08	27.65	6.43	177.84	2.84	0.86	0.86
30.13	30.16	27.72	6.43	178.29	2.84	0.86	0.86
30.14	30.24	27.79	6.43	178.76	2.84	0.86	0.86
30.15	30.32	27.86	6.43	179.21	2.84	0.86	0.86
30.16	30.39	27.92	6.43	179.63	2.84	0.86	0.86
30.17	30.47	27.99	6.43	179.94	2.84	0.86	0.86
30.18	30.65	28.15	6.40	180.05	2.84	0.86	0.86
30.19	30.94	28.42	6.33	179.98	2.84	0.86	0.86
30.20	31.34	28.81	6.24	179.78	2.83	0.86	0.86
30.21	31.80	29.24	6.14	179.51	2.82	0.86	0.86
30.22	32.27	29.69	6.04	179.21	2.81	0.86	0.86
30.23	32.75	30.14	5.93	178.86	2.81	0.86	0.86
30.24	33.20	30.57	5.84	178.51	2.80	0.86	0.86

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
30.25	33.61	30.95	5.76	178.16	2.79	0.86	0.86
30.26	33.93	31.25	5.69	177.94	2.79	0.86	0.86
30.27	34.16	31.47	5.65	177.92	2.78	0.86	0.86
30.28	34.36	31.65	5.63	178.10	2.78	0.86	0.86
30.29	34.57	31.84	5.60	178.36	2.78	0.86	0.86
30.30	34.81	32.06	5.57	178.65	2.78	0.86	0.86
30.31	35.05	32.28	5.54	178.95	2.77	0.86	0.86
30.32	35.28	32.50	5.51	179.24	2.77	0.86	0.86
30.33	35.50	32.70	5.49	179.50	2.77	0.86	0.86
30.34	35.69	32.88	5.47	179.73	2.77	0.86	0.86
30.35	35.78	32.95	5.46	180.02	2.77	0.86	0.86
30.36	35.75	32.91	5.48	180.43	2.77	0.87	0.87
30.37	35.62	32.78	5.52	181.00	2.77	0.87	0.87
30.38	35.48	32.63	5.57	181.65	2.78	0.87	0.87
30.39	35.32	32.47	5.62	182.33	2.78	0.87	0.87
30.40	35.16	32.31	5.67	183.02	2.78	0.87	0.87
30.41	35.00	32.15	5.71	183.68	2.79	0.87	0.87
30.42	34.86	32.00	5.76	184.27	2.79	0.87	0.87
30.43	34.74	31.87	5.80	184.73	2.80	0.87	0.87
30.44	34.60	31.73	5.83	184.99	2.80	0.87	0.87
30.45	34.44	31.57	5.86	185.10	2.80	0.87	0.87
30.46	34.24	31.36	5.90	185.12	2.80	0.87	0.87
30.47	34.01	31.13	5.95	185.13	2.81	0.87	0.87
30.48	33.77	30.90	5.99	185.15	2.81	0.87	0.87
30.49	33.53	30.66	6.04	185.15	2.81	0.87	0.87
30.50	33.31	30.43	6.08	185.15	2.82	0.87	0.87
30.51	33.10	30.23	6.13	185.14	2.82	0.87	0.87
30.52	33.05	30.17	6.14	185.15	2.82	0.87	0.87
30.53	33.24	30.34	6.10	185.19	2.82	0.87	0.87
30.54	33.67	30.74	6.03	185.26	2.81	0.87	0.87
30.55	34.23	31.27	5.93	185.32	2.81	0.87	0.87
30.56	34.85	31.86	5.82	185.34	2.80	0.87	0.87
30.57	35.49	32.46	5.71	185.33	2.79	0.87	0.87
30.58	36.12	33.06	5.60	185.28	2.78	0.87	0.87
30.59	36.71	33.61	5.51	185.20	2.77	0.87	0.87
30.60	37.22	34.09	5.43	185.10	2.77	0.87	0.87
30.61	37.88	34.71	5.33	185.05	2.76	0.87	0.87
30.62	38.81	35.59	5.20	185.03	2.75	0.87	0.87
30.63	40.09	36.81	5.03	184.98	2.73	0.87	0.87
30.64	41.56	38.20	4.84	184.77	2.71	0.87	0.87
30.65	43.14	39.70	4.64	184.39	2.69	1.04	1.04
30.66	44.74	41.22	4.46	183.83	2.68	1.02	1.02
30.67	46.29	42.68	4.29	183.15	2.66	1.00	1.00
30.68	47.69	44.02	4.14	182.40	2.64	0.99	0.99
30.69	48.92	45.18	4.02	181.68	2.63	0.98	0.98
30.70	50.13	46.32	3.91	180.98	2.62	0.96	0.96
30.71	51.48	47.60	3.79	180.20	2.60	0.95	0.95
30.72	53.11	49.13	3.65	179.22	2.59	0.93	0.93

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)'/σ'_v}	S _{u(peak)'/σ'_v}
30.73	54.93	50.86	3.50	178.00	2.57	0.91	0.91
30.74	56.84	52.66	3.35	176.59	2.55	0.89	0.89
30.75	58.75	54.47	3.21	175.06	2.53	0.88	0.88
30.76	60.56	56.18	3.09	173.50	2.52	0.86	0.86
30.77	62.17	57.69	2.98	172.03	2.50	0.84	0.84
30.78	63.55	59.00	2.89	170.72	2.49	0.85	0.85
30.79	64.89	60.25	2.81	169.44	2.48	0.85	0.85
30.80	66.35	61.62	2.73	168.00	2.46	0.85	0.85
30.81	68.05	63.23	2.63	166.29	2.45	0.85	0.85
30.82	69.91	64.98	2.53	164.38	2.43	0.85	0.85
30.83	71.83	66.79	2.43	162.36	2.41	0.84	0.84
30.84	73.72	68.56	2.34	160.34	2.39	0.84	0.84
30.85	75.47	70.21	2.26	158.46	2.38	0.84	0.84
30.86	76.98	71.63	2.19	156.82	2.36	0.84	0.84
30.87	78.15	72.72	2.14	155.76	2.35	0.83	0.83
30.88	79.10	73.61	2.11	155.15	2.34	0.83	0.83
30.89	80.00	74.45	2.08	154.86	2.34	0.83	0.83
30.90	81.04	75.41	2.05	154.52	2.33	0.83	0.83
30.91	82.14	76.44	2.02	154.17	2.32	0.83	0.83
30.92	83.26	77.48	1.99	153.82	2.32	0.83	0.83
30.93	84.34	78.48	1.96	153.49	2.31	0.83	0.83
30.94	85.32	79.40	1.93	153.19	2.30	0.83	0.83
30.95	86.09	80.11	1.91	153.04	2.30	0.83	0.83
30.96	86.56	80.53	1.90	153.25	2.29	0.83	0.83
30.97	86.80	80.74	1.91	153.83	2.29	0.83	0.83
30.98	86.94	80.85	1.91	154.72	2.30	0.83	0.83
30.99	87.09	80.97	1.92	155.72	2.30	0.83	0.83
31.00	87.25	81.11	1.93	156.77	2.30	0.84	0.84
31.01	87.41	81.24	1.94	157.82	2.30	0.84	0.84
31.02	87.56	81.36	1.95	158.82	2.31	0.84	0.84
31.03	87.69	81.47	1.96	159.70	2.31	0.84	0.84
31.04	87.77	81.52	1.97	160.42	2.31	0.84	0.84
31.05	87.78	81.51	1.98	161.03	2.31	0.84	0.84
31.06	87.74	81.45	1.98	161.64	2.32	0.84	0.84
31.07	87.66	81.36	2.00	162.33	2.32	0.84	0.84
31.08	87.59	81.27	2.01	163.09	2.32	0.84	0.84
31.09	87.51	81.17	2.02	163.88	2.32	0.85	0.85
31.10	87.43	81.08	2.03	164.65	2.33	0.85	0.85
31.11	87.36	80.99	2.04	165.36	2.33	0.85	0.85
31.12	87.30	80.91	2.05	165.98	2.33	0.85	0.85
31.13	87.30	80.89	2.06	166.52	2.33	0.85	0.85
31.14	87.36	80.93	2.06	167.06	2.33	0.85	0.85
31.15	87.49	81.03	2.07	167.66	2.34	0.85	0.85
31.16	87.64	81.15	2.07	168.36	2.34	0.85	0.85
31.17	87.80	81.28	2.08	169.11	2.34	0.85	0.85
31.18	87.96	81.41	2.09	169.86	2.34	0.85	0.85
31.19	88.11	81.54	2.09	170.59	2.34	0.85	0.85
31.20	88.25	81.65	2.10	171.26	2.34	0.85	0.85

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
31.21	88.39	81.76	2.10	171.80	2.34	0.85	0.85
31.22	88.58	81.91	2.10	172.24	2.34	0.86	0.86
31.23	88.84	82.14	2.10	172.64	2.34	0.86	0.86
31.24	89.19	82.44	2.10	173.07	2.34	0.86	0.86
31.25	89.57	82.78	2.10	173.55	2.34	0.86	0.86
31.26	89.96	83.14	2.09	174.06	2.34	0.86	0.86
31.27	90.36	83.49	2.09	174.56	2.34	0.86	0.86
31.28	90.74	83.82	2.09	175.04	2.34	0.86	0.86
31.29	91.07	84.11	2.09	175.46	2.34	0.86	0.86
31.30	91.38	84.39	2.08	175.75	2.34	0.86	0.86
31.31	91.73	84.69	2.08	175.92	2.34	0.86	0.86
31.32	92.15	85.07	2.07	176.00	2.34	0.86	0.86
31.33	92.65	85.51	2.06	176.08	2.33	0.86	0.86
31.34	93.19	86.00	2.05	176.16	2.33	0.86	0.86
31.35	93.75	86.51	2.04	176.24	2.33	0.86	0.86
31.36	94.30	87.00	2.03	176.32	2.33	0.86	0.86
31.37	94.81	87.46	2.02	176.40	2.32	0.86	0.86
31.38	95.26	87.86	2.01	176.46	2.32	0.86	0.86
31.39	95.77	88.32	2.00	176.52	2.32	0.86	0.86
31.40	96.41	88.90	1.99	176.60	2.32	0.86	0.86
31.41	97.25	89.67	1.97	176.70	2.31	0.86	0.86
31.42	98.22	90.55	1.95	176.82	2.31	0.86	0.86
31.43	99.24	91.49	1.93	176.95	2.30	0.86	0.86
31.44	100.28	92.45	1.92	177.09	2.30	0.86	0.86
31.45	101.28	93.36	1.90	177.22	2.29	0.86	0.86
31.46	102.19	94.19	1.88	177.34	2.29	0.86	0.86
31.47	102.98	94.91	1.87	177.45	2.28	0.86	0.86
31.48	103.75	95.61	1.86	177.55	2.28	0.86	0.86
31.49	104.61	96.40	1.84	177.66	2.28	0.86	0.86
31.50	105.64	97.34	1.83	177.81	2.27	0.86	0.86
31.51	106.78	98.39	1.81	177.97	2.27	0.86	0.86
31.52	107.98	99.49	1.79	178.16	2.26	0.86	0.86
31.53	109.17	100.58	1.77	178.35	2.26	0.86	0.86
31.54	110.29	101.61	1.76	178.53	2.25	0.86	0.86
31.55	111.29	102.52	1.74	178.70	2.25	0.86	0.86
31.56	112.15	103.30	1.73	178.83	2.24	0.86	0.86
31.57	112.98	104.06	1.72	178.92	2.24	0.86	0.86
31.58	113.91	104.90	1.71	179.01	2.23	0.86	0.86
31.59	114.98	105.88	1.69	179.12	2.23	0.86	0.86
31.60	116.15	106.95	1.68	179.25	2.22	0.86	0.86
31.61	117.35	108.05	1.66	179.39	2.22	0.86	0.86
31.62	118.52	109.12	1.65	179.54	2.21	0.86	0.86
31.63	119.61	110.12	1.63	179.69	2.21	0.86	0.86
31.64	120.55	110.97	1.62	179.81	2.20	0.86	0.86
31.65	121.35	111.69	1.61	179.88	2.20	0.86	0.86
31.66	122.11	112.38	1.60	179.88	2.19	0.86	0.86
31.67	122.96	113.15	1.59	179.84	2.19	0.86	0.86
31.68	123.93	114.03	1.58	179.82	2.18	0.86	0.86

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
31.69	124.95	114.96	1.56	179.80	2.18	0.86	0.86
31.70	125.99	115.91	1.55	179.80	2.17	0.86	0.86
31.71	126.99	116.82	1.54	179.81	2.17	0.86	0.86
31.72	127.89	117.64	1.53	179.83	2.16	0.86	0.86
31.73	128.63	118.30	1.52	179.86	2.16	0.86	0.86
31.74	129.22	118.82	1.51	179.89	2.16	0.86	0.86
31.75	129.73	119.28	1.51	179.94	2.15	0.86	0.86
31.76	130.28	119.76	1.50	180.00	2.15	0.86	0.86
31.77	130.89	120.31	1.50	180.07	2.15	0.86	0.86
31.78	131.53	120.88	1.49	180.16	2.14	0.86	0.86
31.79	132.16	121.44	1.48	180.25	2.14	0.86	0.86
31.80	132.76	121.97	1.48	180.34	2.14	0.86	0.86
31.81	133.29	122.44	1.47	180.42	2.13	0.86	0.86
31.82	133.71	122.80	1.47	180.51	2.13	0.87	0.87
31.83	134.05	123.10	1.47	180.63	2.13	0.87	0.87
31.84	134.37	123.36	1.47	180.81	2.13	0.87	0.87
31.85	134.73	123.67	1.46	181.03	2.13	0.87	0.87
31.86	135.12	124.01	1.46	181.27	2.13	0.87	0.87
31.87	135.52	124.35	1.46	181.52	2.13	0.87	0.87
31.88	135.91	124.69	1.46	181.76	2.12	0.87	0.87
31.89	136.27	125.00	1.46	181.98	2.12	0.87	0.87
31.90	136.57	125.25	1.45	182.16	2.12	0.87	0.87
31.91	136.75	125.39	1.45	182.28	2.12	0.87	0.87
31.92	136.82	125.43	1.45	182.35	2.12	0.87	0.87
31.93	136.82	125.40	1.45	182.39	2.12	0.87	0.87
31.94	136.82	125.37	1.46	182.45	2.12	0.87	0.87
31.95	136.82	125.34	1.46	182.50	2.12	0.87	0.87
31.96	136.82	125.31	1.46	182.56	2.12	0.87	0.87
31.97	136.82	125.28	1.46	182.62	2.12	0.87	0.87
31.98	136.82	125.25	1.46	182.67	2.13	0.87	0.87
31.99	136.81	125.21	1.46	182.71	2.13	0.87	0.87
32.00	136.75	125.13	1.46	182.75	2.13	0.87	0.87
32.01	136.65	125.00	1.46	182.81	2.13	0.87	0.87
32.02	136.52	124.84	1.46	182.88	2.13	0.87	0.87
32.03	136.36	124.67	1.47	182.97	2.13	0.87	0.87
32.04	136.20	124.49	1.47	183.07	2.13	0.87	0.87
32.05	136.05	124.31	1.47	183.16	2.13	0.87	0.87
32.06	135.90	124.15	1.48	183.25	2.14	0.87	0.87
32.07	135.76	123.99	1.48	183.33	2.14	0.87	0.87
32.08	135.65	123.86	1.48	183.39	2.14	0.87	0.87
32.09	135.54	123.72	1.48	183.45	2.14	0.87	0.87
32.10	135.42	123.58	1.49	183.53	2.14	0.87	0.87
32.11	135.27	123.41	1.49	183.62	2.14	0.87	0.87
32.12	135.12	123.24	1.49	183.72	2.14	0.87	0.87
32.13	134.96	123.06	1.49	183.82	2.14	0.87	0.87
32.14	134.80	122.89	1.50	183.93	2.15	0.87	0.87
32.15	134.66	122.72	1.50	184.02	2.15	0.87	0.87
32.16	134.53	122.58	1.50	184.10	2.15	0.87	0.87

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
32.17	134.42	122.44	1.50	184.17	2.15	0.87	0.87
32.18	134.31	122.31	1.51	184.24	2.15	0.87	0.87
32.19	134.17	122.16	1.51	184.33	2.15	0.87	0.87
32.20	134.03	121.99	1.51	184.43	2.15	0.87	0.87
32.21	133.87	121.81	1.52	184.54	2.16	0.87	0.87
32.22	133.71	121.63	1.52	184.66	2.16	0.87	0.87
32.23	133.55	121.46	1.52	184.77	2.16	0.87	0.87
32.24	133.42	121.30	1.52	184.87	2.16	0.87	0.87
32.25	133.31	121.17	1.53	184.95	2.16	0.87	0.87
32.26	133.22	121.06	1.53	185.01	2.16	0.87	0.87
32.27	133.16	120.97	1.53	185.08	2.16	0.87	0.87
32.28	133.09	120.88	1.53	185.16	2.16	0.87	0.87
32.29	133.01	120.78	1.53	185.25	2.16	0.87	0.87
32.30	132.93	120.68	1.54	185.34	2.17	0.87	0.87
32.31	132.85	120.57	1.54	185.44	2.17	0.87	0.87
32.32	132.78	120.47	1.54	185.53	2.17	0.87	0.87
32.33	132.71	120.38	1.54	185.60	2.17	0.87	0.87
32.34	132.67	120.32	1.54	185.68	2.17	0.87	0.87
32.35	132.65	120.27	1.54	185.77	2.17	0.87	0.87
32.36	132.65	120.24	1.55	185.89	2.17	0.87	0.87
32.37	132.65	120.21	1.55	186.04	2.17	0.87	0.87
32.38	132.65	120.18	1.55	186.20	2.17	0.87	0.87
32.39	132.65	120.15	1.55	186.37	2.17	0.87	0.87
32.40	132.65	120.12	1.55	186.54	2.17	0.87	0.87
32.41	132.65	120.09	1.55	186.69	2.17	0.87	0.87
32.42	132.65	120.06	1.56	186.81	2.18	0.87	0.87
32.43	132.65	120.03	1.56	186.92	2.18	0.87	0.87
32.44	132.65	120.00	1.56	187.04	2.18	0.87	0.87
32.45	132.65	119.97	1.56	187.17	2.18	0.87	0.87
32.46	132.65	119.94	1.56	187.33	2.18	0.87	0.87
32.47	132.65	119.91	1.56	187.50	2.18	0.87	0.87
32.48	132.65	119.88	1.57	187.67	2.18	0.87	0.87
32.49	132.65	119.85	1.57	187.83	2.18	0.87	0.87
32.50	132.65	119.82	1.57	187.98	2.18	0.87	0.87
32.51	132.66	119.80	1.57	188.11	2.18	0.87	0.87
32.52	132.69	119.80	1.57	188.24	2.18	0.87	0.87
32.53	132.74	119.81	1.57	188.41	2.18	0.87	0.87
32.54	132.81	119.85	1.57	188.61	2.18	0.87	0.87
32.55	132.88	119.89	1.58	188.84	2.18	0.87	0.87
32.56	132.96	119.93	1.58	189.09	2.18	0.87	0.87
32.57	133.04	119.98	1.58	189.32	2.18	0.88	0.88
32.58	133.12	120.01	1.58	189.55	2.19	0.88	0.88
32.59	133.18	120.04	1.58	189.74	2.19	0.88	0.88
32.60	133.47	120.28	1.58	190.10	2.19	0.88	0.88
32.61	134.08	120.81	1.58	190.74	2.19	0.88	0.88
32.62	135.08	121.70	1.58	191.72	2.18	0.88	0.88
32.63	136.27	122.76	1.57	192.90	2.18	0.88	0.88
32.64	137.56	123.91	1.57	194.17	2.18	0.88	0.88

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
32.65	138.88	125.10	1.56	195.49	2.18	0.88	0.88
32.66	140.17	126.25	1.56	196.76	2.18	0.88	0.88
32.67	141.35	127.30	1.55	197.94	2.17	0.88	0.88
32.68	142.37	128.20	1.55	198.95	2.17	0.89	0.89
32.69	143.26	128.98	1.55	199.83	2.17	0.89	0.89
32.70	144.15	129.77	1.55	200.72	2.17	0.89	0.89
32.71	145.15	130.66	1.54	201.73	2.17	0.89	0.89
32.72	146.29	131.67	1.54	202.89	2.17	0.89	0.89
32.73	147.50	132.74	1.54	204.11	2.17	0.89	0.89
32.74	148.71	133.82	1.53	205.35	2.17	0.89	0.89
32.75	149.87	134.84	1.53	206.53	2.16	0.89	0.89
32.76	150.92	135.77	1.53	207.59	2.16	0.89	0.89
32.77	151.69	136.45	1.53	208.40	2.16	0.90	0.90
32.78	152.16	136.84	1.53	208.96	2.16	0.90	0.90
32.79	152.39	137.01	1.53	209.34	2.16	0.90	0.90
32.80	152.54	137.11	1.53	209.70	2.16	0.90	0.90
32.81	152.70	137.23	1.53	210.11	2.16	0.90	0.90
32.82	152.88	137.35	1.53	210.53	2.16	0.90	0.90
32.83	153.05	137.47	1.53	210.95	2.17	0.90	0.90
32.84	153.21	137.58	1.54	211.34	2.17	0.90	0.90
32.85	153.35	137.68	1.54	211.68	2.17	0.90	0.90
32.86	153.53	137.81	1.54	211.98	2.17	0.90	0.90
32.87	153.78	138.00	1.54	212.29	2.17	0.90	0.90
32.88	154.14	138.30	1.54	212.66	2.17	0.90	0.90
32.89	154.56	138.65	1.54	213.09	2.17	0.90	0.90
32.90	155.01	139.03	1.54	213.56	2.17	0.90	0.90
32.91	155.48	139.42	1.54	214.04	2.17	0.90	0.90
32.92	155.93	139.79	1.53	214.50	2.17	0.90	0.90
32.93	156.35	140.14	1.53	214.93	2.16	0.90	0.90
32.94	156.71	140.44	1.53	215.28	2.16	0.90	0.90
32.95	157.07	140.74	1.53	215.56	2.16	0.90	0.90
32.96	157.49	141.09	1.53	215.80	2.16	0.90	0.90
32.97	158.01	141.52	1.53	216.06	2.16	0.90	0.90
32.98	158.59	142.02	1.52	216.35	2.16	0.90	0.90
32.99	159.20	142.55	1.52	216.66	2.16	0.90	0.90
33.00	159.82	143.08	1.52	216.98	2.16	0.90	0.90
33.01	160.41	143.58	1.51	217.28	2.15	0.90	0.90
33.02	160.94	144.03	1.51	217.55	2.15	0.91	0.91
33.03	161.39	144.41	1.51	217.75	2.15	0.91	0.91
33.04	161.83	144.78	1.51	217.90	2.15	0.91	0.91
33.05	162.30	145.18	1.50	218.02	2.15	0.91	0.91
33.06	162.86	145.66	1.50	218.14	2.15	0.91	0.91
33.07	163.48	146.19	1.49	218.28	2.14	0.91	0.91
33.08	164.12	146.74	1.49	218.43	2.14	0.91	0.91
33.09	164.75	147.29	1.48	218.59	2.14	0.91	0.91
33.10	165.34	147.80	1.48	218.73	2.14	0.91	0.91
33.11	165.86	148.24	1.48	218.85	2.14	0.91	0.91
33.12	166.34	148.64	1.47	218.98	2.13	0.91	0.91

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
33.13	166.84	149.07	1.47	219.14	2.13	0.91	0.91
33.14	167.45	149.59	1.47	219.35	2.13	0.91	0.91
33.15	168.14	150.19	1.46	219.61	2.13	0.91	0.91
33.16	168.89	150.85	1.46	219.89	2.12	0.91	0.91
33.17	169.66	151.51	1.45	220.19	2.12	0.91	0.91
33.18	170.41	152.16	1.45	220.48	2.12	0.91	0.91
33.19	171.09	152.75	1.45	220.74	2.12	0.91	0.91
33.20	171.68	153.25	1.44	220.96	2.11	0.91	0.91
33.21	172.17	153.67	1.44	221.13	2.11	0.91	0.91
33.22	172.65	154.08	1.44	221.27	2.11	0.91	0.91
33.23	173.19	154.53	1.43	221.43	2.11	0.91	0.91
33.24	173.79	155.05	1.43	221.61	2.11	0.91	0.91
33.25	174.42	155.59	1.43	221.81	2.10	0.91	0.91
33.26	175.06	156.14	1.42	222.01	2.10	0.91	0.91
33.27	175.67	156.66	1.42	222.20	2.10	0.91	0.91
33.28	176.21	157.13	1.42	222.38	2.10	0.91	0.91
33.29	176.62	157.46	1.41	222.47	2.10	0.91	0.91
33.30	176.85	157.64	1.41	222.44	2.09	0.91	0.91
33.31	176.95	157.70	1.41	222.30	2.09	0.91	0.91
33.32	177.02	157.73	1.41	222.10	2.09	0.91	0.91
33.33	177.10	157.77	1.41	221.89	2.09	0.91	0.91
33.34	177.18	157.81	1.40	221.67	2.09	0.91	0.91
33.35	177.26	157.85	1.40	221.46	2.09	0.91	0.91
33.36	177.33	157.89	1.40	221.25	2.09	0.91	0.91
33.37	177.40	157.92	1.40	221.07	2.09	0.91	0.91
33.38	177.36	157.85	1.40	220.85	2.09	0.91	0.91
33.39	177.19	157.66	1.40	220.56	2.09	0.91	0.91
33.40	176.88	157.34	1.40	220.16	2.09	0.91	0.91
33.41	176.52	156.98	1.40	219.71	2.09	0.91	0.91
33.42	176.12	156.59	1.40	219.22	2.09	0.91	0.91
33.43	175.72	156.19	1.40	218.73	2.09	0.91	0.91
33.44	175.33	155.81	1.40	218.25	2.09	0.91	0.91
33.45	174.98	155.45	1.40	217.80	2.09	0.91	0.91
33.46	174.65	155.12	1.40	217.40	2.09	0.90	0.90
33.47	174.26	154.73	1.40	216.97	2.09	0.90	0.90
33.48	173.74	154.23	1.40	216.44	2.09	0.90	0.90
33.49	173.07	153.59	1.40	215.78	2.09	0.90	0.90
33.50	172.32	152.88	1.41	215.04	2.09	0.90	0.90
33.51	171.53	152.12	1.41	214.27	2.09	0.90	0.90
33.52	170.73	151.37	1.41	213.50	2.09	0.90	0.90
33.53	169.97	150.65	1.41	212.76	2.10	0.90	0.90
33.54	169.29	150.00	1.41	212.10	2.10	0.90	0.90
33.55	168.67	149.40	1.42	211.52	2.10	0.90	0.90
33.56	167.99	148.76	1.42	210.96	2.10	0.90	0.90
33.57	167.18	147.98	1.42	210.35	2.10	0.90	0.90
33.58	166.19	147.06	1.43	209.65	2.10	0.90	0.90
33.59	165.11	146.05	1.43	208.88	2.11	0.90	0.90
33.60	163.99	145.00	1.44	208.09	2.11	0.90	0.90

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
33.61	162.89	143.96	1.44	207.31	2.11	0.89	0.89
33.62	161.86	143.00	1.44	206.59	2.12	0.89	0.89
33.63	160.96	142.15	1.45	205.96	2.12	0.89	0.89
33.64	160.15	141.38	1.45	205.43	2.12	0.89	0.89
33.65	159.32	140.60	1.46	204.94	2.12	0.89	0.89
33.66	158.37	139.71	1.46	204.42	2.13	0.89	0.89
33.67	157.28	138.68	1.47	203.83	2.13	0.89	0.89
33.68	156.10	137.58	1.48	203.20	2.14	0.89	0.89
33.69	154.90	136.46	1.48	202.58	2.14	0.89	0.89
33.70	153.74	135.38	1.49	201.98	2.14	0.89	0.89
33.71	152.67	134.38	1.50	201.44	2.15	0.89	0.89
33.72	151.76	133.53	1.51	200.97	2.15	0.89	0.89
33.73	150.96	132.77	1.51	200.54	2.15	0.89	0.89
33.74	150.13	131.99	1.52	200.10	2.16	0.89	0.89
33.75	149.19	131.11	1.52	199.58	2.16	0.89	0.89
33.76	148.14	130.13	1.53	199.01	2.16	0.89	0.89
33.77	147.03	129.09	1.54	198.41	2.17	0.89	0.89
33.78	145.91	128.06	1.54	197.83	2.17	0.88	0.88
33.79	144.85	127.07	1.55	197.27	2.17	0.88	0.88
33.80	143.90	126.18	1.56	196.78	2.18	0.88	0.88
33.81	143.10	125.43	1.57	196.36	2.18	0.88	0.88
33.82	142.35	124.73	1.57	195.98	2.18	0.88	0.88
33.83	141.56	123.99	1.58	195.60	2.18	0.88	0.88
33.84	140.65	123.13	1.58	195.16	2.19	0.88	0.88
33.85	139.64	122.20	1.59	194.69	2.19	0.88	0.88
33.86	138.60	121.23	1.60	194.21	2.20	0.88	0.88
33.87	137.58	120.28	1.61	193.74	2.20	0.88	0.88
33.88	136.62	119.40	1.62	193.30	2.20	0.88	0.88
33.89	135.79	118.62	1.63	192.93	2.20	0.88	0.88
33.90	135.25	118.11	1.63	192.73	2.21	0.88	0.88
33.91	134.97	117.82	1.64	192.72	2.21	0.88	0.88
33.92	134.88	117.71	1.64	192.87	2.21	0.88	0.88
33.93	134.79	117.60	1.64	193.05	2.21	0.88	0.88
33.94	134.68	117.47	1.65	193.25	2.21	0.88	0.88
33.95	134.58	117.34	1.65	193.45	2.21	0.88	0.88
33.96	134.47	117.22	1.65	193.65	2.21	0.88	0.88
33.97	134.38	117.10	1.66	193.83	2.22	0.88	0.88
33.98	134.30	117.00	1.66	193.98	2.22	0.88	0.88
33.99	134.23	116.91	1.66	194.12	2.22	0.88	0.88
34.00	134.17	116.83	1.66	194.27	2.22	0.88	0.88
34.01	134.10	116.74	1.67	194.46	2.22	0.88	0.88
34.02	134.03	116.64	1.67	194.67	2.22	0.88	0.88
34.03	133.95	116.54	1.67	194.90	2.22	0.88	0.88
34.04	133.87	116.43	1.68	195.13	2.22	0.88	0.88
34.05	133.79	116.33	1.68	195.34	2.22	0.88	0.88
34.06	133.73	116.24	1.68	195.54	2.23	0.88	0.88
34.07	133.62	116.12	1.68	195.64	2.23	0.88	0.88
34.08	133.42	115.91	1.69	195.64	2.23	0.88	0.88

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
34.09	133.10	115.59	1.69	195.52	2.23	0.88	0.88
34.10	132.70	115.21	1.70	195.37	2.23	0.88	0.88
34.11	132.26	114.79	1.70	195.20	2.23	0.88	0.88
34.12	131.81	114.35	1.71	195.03	2.23	0.88	0.88
34.13	131.36	113.93	1.71	194.86	2.24	0.88	0.88
34.14	130.95	113.53	1.72	194.70	2.24	0.88	0.88
34.15	130.58	113.18	1.72	194.56	2.24	0.88	0.88
34.16	130.38	112.97	1.72	194.53	2.24	0.88	0.88
34.17	130.32	112.89	1.72	194.61	2.24	0.88	0.88
34.18	130.39	112.92	1.73	194.81	2.24	0.88	0.88
34.19	130.46	112.95	1.73	195.05	2.24	0.88	0.88
34.20	130.54	112.99	1.73	195.30	2.24	0.88	0.88
34.21	130.62	113.03	1.73	195.55	2.24	0.88	0.88
34.22	130.70	113.07	1.73	195.80	2.24	0.88	0.88
34.23	130.77	113.11	1.73	196.03	2.24	0.88	0.88
34.24	130.85	113.15	1.73	196.23	2.24	0.88	0.88
34.25	131.00	113.26	1.73	196.48	2.24	0.88	0.88
34.26	131.25	113.45	1.73	196.81	2.24	0.88	0.88
34.27	131.59	113.72	1.73	197.24	2.24	0.88	0.88
34.28	131.96	114.02	1.73	197.72	2.24	0.88	0.88
34.29	132.36	114.35	1.73	198.23	2.24	0.88	0.88
34.30	132.76	114.67	1.73	198.74	2.24	0.89	0.89
34.31	133.14	114.97	1.73	199.22	2.24	0.89	0.89
34.32	133.48	115.24	1.73	199.64	2.24	0.89	0.89
34.33	133.82	115.52	1.73	200.01	2.24	0.89	0.89
34.34	134.26	115.88	1.73	200.35	2.24	0.89	0.89
34.35	134.84	116.37	1.72	200.73	2.24	0.89	0.89
34.36	135.55	116.97	1.72	201.17	2.24	0.89	0.89
34.37	136.32	117.62	1.71	201.66	2.24	0.89	0.89
34.38	137.12	118.31	1.71	202.16	2.24	0.89	0.89
34.39	137.91	118.98	1.70	202.66	2.23	0.89	0.89
34.40	138.64	119.60	1.70	203.12	2.23	0.89	0.89
34.41	139.28	120.13	1.69	203.52	2.23	0.89	0.89
34.42	139.88	120.63	1.69	203.86	2.23	0.89	0.89
34.43	140.52	121.18	1.68	204.16	2.23	0.89	0.89
34.44	141.29	121.83	1.68	204.50	2.22	0.89	0.89
34.45	142.17	122.59	1.67	204.89	2.22	0.89	0.89
34.46	143.12	123.40	1.66	205.31	2.22	0.89	0.89
34.47	144.08	124.22	1.66	205.74	2.22	0.89	0.89
34.48	145.01	125.02	1.65	206.16	2.21	0.89	0.89
34.49	145.85	125.74	1.64	206.54	2.21	0.89	0.89
34.50	146.58	126.36	1.64	206.85	2.21	0.89	0.89
34.51	147.30	126.97	1.63	207.05	2.21	0.89	0.89
34.52	148.09	127.65	1.62	207.19	2.20	0.89	0.89
34.53	149.04	128.47	1.61	207.32	2.20	0.89	0.89
34.54	150.10	129.39	1.60	207.48	2.20	0.89	0.89
34.55	151.22	130.35	1.59	207.65	2.19	0.89	0.89
34.56	152.33	131.32	1.58	207.83	2.19	0.90	0.90

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
34.57	153.39	132.23	1.57	208.00	2.18	0.90	0.90
34.58	154.32	133.04	1.56	208.16	2.18	0.90	0.90
34.59	155.17	133.77	1.56	208.29	2.18	0.90	0.90
34.60	156.04	134.52	1.55	208.38	2.17	0.90	0.90
34.61	157.06	135.40	1.54	208.47	2.17	0.90	0.90
34.62	158.27	136.46	1.53	208.59	2.16	0.90	0.90
34.63	159.59	137.61	1.52	208.73	2.16	0.90	0.90
34.64	160.95	138.80	1.51	208.90	2.15	0.90	0.90
34.65	162.28	139.97	1.49	209.08	2.14	0.90	0.90
34.66	163.52	141.05	1.48	209.26	2.14	0.90	0.90
34.67	164.60	141.99	1.47	209.43	2.13	0.90	0.90
34.68	165.50	142.77	1.47	209.49	2.13	0.90	0.90
34.69	166.34	143.49	1.46	209.46	2.13	0.90	0.90
34.70	167.24	144.28	1.45	209.35	2.12	0.90	0.90
34.71	168.27	145.19	1.44	209.25	2.11	0.90	0.90
34.72	169.37	146.16	1.43	209.16	2.11	0.90	0.90
34.73	170.49	147.14	1.42	209.10	2.10	0.90	0.90
34.74	171.57	148.09	1.41	209.06	2.10	0.90	0.90
34.75	172.55	148.96	1.40	209.05	2.09	0.90	0.90
34.76	173.37	149.67	1.40	209.03	2.08	0.90	0.90
34.77	174.04	150.25	1.39	208.97	2.08	0.90	0.90
34.78	174.67	150.79	1.39	208.86	2.08	0.90	0.90
34.79	175.35	151.39	1.38	208.71	2.07	0.90	0.90
34.80	176.10	152.06	1.37	208.58	2.06	0.90	0.90
34.81	176.90	152.76	1.36	208.46	2.06	0.90	0.90
34.82	177.69	153.46	1.36	208.35	2.05	0.90	0.90
34.83	178.45	154.12	1.35	208.27	2.05	0.90	0.90
34.84	179.11	154.71	1.35	208.21	2.04	0.90	0.90
34.85	179.64	155.17	1.34	208.14	2.04	0.90	0.90
34.86	180.06	155.53	1.34	208.07	2.03	0.90	0.90
34.87	180.45	155.85	1.33	207.96	2.03	0.90	0.90
34.88	180.87	156.22	1.33	207.85	2.03	0.90	0.90
34.89	181.34	156.63	1.33	207.74	2.02	0.90	0.90
34.90	181.82	157.05	1.32	207.63	2.02	0.89	0.89
34.91	182.29	157.46	1.32	207.53	2.01	0.89	0.89
34.92	182.73	157.83	1.31	207.45	2.01	0.89	0.89
34.93	183.09	158.15	1.31	207.36	2.00	0.89	0.89
34.94	183.24	158.27	1.31	207.14	2.00	0.89	0.89
34.95	183.18	158.19	1.31	206.72	2.00	0.89	0.89
34.96	182.92	157.95	1.30	206.09	2.00	0.89	0.89
34.97	182.62	157.68	1.30	205.38	1.99	0.89	0.89
34.98	182.30	157.40	1.30	204.62	1.99	0.89	0.89
34.99	181.98	157.11	1.30	203.86	1.99	0.89	0.89
35.00	181.67	156.83	1.30	203.13	1.99	0.89	0.89
35.01	181.39	156.57	1.29	202.47	1.98	0.89	0.89
35.02	181.10	156.30	1.29	201.86	1.98	0.89	0.89
35.03	180.67	155.91	1.29	201.19	1.98	0.89	0.89
35.04	180.05	155.33	1.29	200.37	1.98	0.89	0.89

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
35.05	179.23	154.59	1.29	199.36	1.98	0.89	0.89
35.06	178.32	153.77	1.29	198.24	1.98	0.88	0.88
35.07	177.36	152.91	1.29	197.06	1.98	0.88	0.88
35.08	176.41	152.05	1.29	195.89	1.98	0.88	0.88
35.09	175.50	151.24	1.29	194.79	1.98	0.88	0.88
35.10	174.70	150.51	1.29	193.81	1.97	0.88	0.88
35.11	173.94	149.82	1.29	192.91	1.97	0.88	0.88
35.12	173.07	149.03	1.29	191.97	1.98	0.88	0.88
35.13	171.99	148.05	1.29	190.86	1.98	0.88	0.88
35.14	170.71	146.89	1.29	189.56	1.98	0.88	0.88
35.15	169.31	145.63	1.29	188.15	1.98	0.87	0.87
35.16	167.87	144.33	1.29	186.69	1.98	0.87	0.87
35.17	166.45	143.06	1.30	185.27	1.98	0.87	0.87
35.18	165.15	141.88	1.30	183.96	1.99	0.87	0.87
35.19	164.00	140.85	1.30	182.81	1.99	0.87	0.87
35.20	162.86	139.81	1.30	181.70	1.99	0.87	0.87
35.21	161.55	138.63	1.30	180.49	1.99	0.87	0.87
35.22	159.93	137.16	1.31	179.03	2.00	0.86	0.86
35.23	158.08	135.50	1.31	177.38	2.00	0.86	0.86
35.24	156.11	133.73	1.31	175.62	2.01	0.86	0.86
35.25	154.11	131.93	1.32	173.85	2.01	0.86	0.86
35.26	152.18	130.21	1.32	172.15	2.02	0.86	0.86
35.27	150.44	128.64	1.33	170.62	2.02	0.85	0.85
35.28	148.95	127.30	1.33	169.31	2.03	0.85	0.85
35.29	147.56	126.05	1.33	168.10	2.03	0.85	0.85
35.30	146.10	124.73	1.34	166.82	2.03	0.85	0.85
35.31	144.39	123.20	1.34	165.34	2.04	0.85	0.85
35.32	142.48	121.50	1.35	163.70	2.04	0.84	0.84
35.33	140.49	119.72	1.35	162.00	2.05	0.84	0.84
35.34	138.50	117.94	1.36	160.33	2.05	0.84	0.84
35.35	136.63	116.27	1.37	158.76	2.06	0.84	0.84
35.36	134.97	114.79	1.37	157.37	2.06	0.84	0.84
35.37	133.57	113.54	1.38	156.18	2.07	0.84	0.84
35.38	132.29	112.39	1.38	155.03	2.07	0.83	0.83
35.39	130.92	111.17	1.38	153.76	2.07	0.83	0.83
35.40	129.35	109.77	1.39	152.30	2.08	0.83	0.83
35.41	127.63	108.25	1.39	150.72	2.08	0.83	0.83
35.42	125.87	106.69	1.40	149.11	2.08	0.83	0.83
35.43	124.15	105.16	1.40	147.54	2.09	0.82	0.82
35.44	122.55	103.75	1.41	146.09	2.09	0.82	0.82
35.45	121.19	102.54	1.41	144.84	2.10	0.82	0.82
35.46	120.09	101.56	1.42	143.83	2.10	0.82	0.82
35.47	119.14	100.71	1.42	142.91	2.10	0.82	0.82
35.48	118.16	99.84	1.42	141.95	2.10	0.82	0.82
35.49	117.05	98.85	1.42	140.86	2.10	0.81	0.81
35.50	115.86	97.80	1.43	139.70	2.11	0.81	0.81
35.51	114.66	96.74	1.43	138.54	2.11	0.81	0.81
35.52	113.51	95.72	1.44	137.42	2.11	0.81	0.81

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
35.53	112.47	94.80	1.44	136.41	2.11	0.81	0.81
35.54	111.62	94.04	1.44	135.61	2.12	0.81	0.81
35.55	110.98	93.47	1.44	135.04	2.12	0.81	0.81
35.56	110.45	92.98	1.45	134.62	2.12	0.81	0.81
35.57	109.90	92.48	1.45	134.22	2.12	0.80	0.80
35.58	109.29	91.93	1.46	133.78	2.12	0.80	0.80
35.59	108.65	91.35	1.46	133.32	2.13	0.80	0.80
35.60	108.02	90.78	1.46	132.87	2.13	0.80	0.80
35.61	107.42	90.24	1.47	132.45	2.13	0.80	0.80
35.62	106.89	89.76	1.47	132.08	2.13	0.80	0.80
35.63	106.46	89.36	1.48	131.81	2.13	0.80	0.80
35.64	106.08	89.01	1.48	131.66	2.14	0.80	0.80
35.65	105.70	88.66	1.48	131.58	2.14	0.80	0.80
35.66	105.27	88.25	1.49	131.51	2.14	0.80	0.80
35.67	104.81	87.82	1.50	131.45	2.15	0.80	0.80
35.68	104.33	87.38	1.50	131.39	2.15	0.80	0.80
35.69	103.86	86.94	1.51	131.33	2.15	0.80	0.80
35.70	103.42	86.54	1.52	131.28	2.16	0.80	0.80
35.71	103.06	86.19	1.52	131.24	2.16	0.80	0.80
35.72	102.78	85.93	1.53	131.25	2.16	0.80	0.80
35.73	102.57	85.72	1.53	131.31	2.16	0.80	0.80
35.74	102.37	85.53	1.54	131.43	2.17	0.80	0.80
35.75	102.15	85.31	1.54	131.56	2.17	0.80	0.80
35.76	101.91	85.08	1.55	131.71	2.17	0.80	0.80
35.77	101.67	84.84	1.55	131.85	2.17	0.80	0.80
35.78	101.44	84.62	1.56	132.00	2.18	0.80	0.80
35.79	101.23	84.41	1.57	132.13	2.18	0.80	0.80
35.80	101.09	84.26	1.57	132.24	2.18	0.80	0.80
35.81	101.03	84.19	1.57	132.34	2.18	0.80	0.80
35.82	101.05	84.19	1.57	132.44	2.18	0.80	0.80
35.83	101.12	84.23	1.57	132.55	2.18	0.80	0.80
35.84	101.20	84.28	1.57	132.67	2.18	0.80	0.80
35.85	101.28	84.33	1.57	132.81	2.18	0.80	0.80
35.86	101.36	84.38	1.58	132.94	2.18	0.80	0.80
35.87	101.43	84.42	1.58	133.06	2.18	0.80	0.80
35.88	101.50	84.46	1.58	133.17	2.18	0.80	0.80
35.89	101.60	84.53	1.58	133.24	2.18	0.80	0.80
35.90	101.76	84.65	1.57	133.29	2.18	0.80	0.80
35.91	102.00	84.84	1.57	133.33	2.18	0.80	0.80
35.92	102.29	85.08	1.57	133.37	2.18	0.80	0.80
35.93	102.60	85.33	1.56	133.41	2.18	0.80	0.80
35.94	102.92	85.60	1.56	133.46	2.18	0.80	0.80
35.95	103.23	85.85	1.56	133.51	2.17	0.80	0.80
35.96	103.52	86.09	1.55	133.55	2.17	0.80	0.80
35.97	103.77	86.29	1.55	133.59	2.17	0.80	0.80
35.98	103.99	86.47	1.54	133.58	2.17	0.80	0.80
35.99	104.22	86.66	1.54	133.52	2.17	0.80	0.80
36.00	104.48	86.87	1.54	133.42	2.17	0.80	0.80

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)'/σ'_v}	S _{u(peak)'/σ'_v}
36.01	104.78	87.12	1.53	133.31	2.16	0.80	0.80
36.02	105.10	87.39	1.52	133.21	2.16	0.80	0.80
36.03	105.42	87.65	1.52	133.10	2.16	0.80	0.80
36.04	105.72	87.91	1.51	133.00	2.15	0.80	0.80
36.05	106.00	88.14	1.51	132.91	2.15	0.80	0.80
36.06	106.23	88.32	1.50	132.81	2.15	0.80	0.80
36.07	106.42	88.48	1.50	132.66	2.15	0.80	0.80
36.08	106.60	88.64	1.49	132.44	2.15	0.80	0.80
36.09	106.81	88.81	1.49	132.17	2.14	0.80	0.80
36.10	107.04	89.01	1.48	131.87	2.14	0.80	0.80
36.11	107.28	89.21	1.47	131.57	2.13	0.80	0.80
36.12	107.52	89.41	1.47	131.27	2.13	0.80	0.80
36.13	107.74	89.60	1.46	131.00	2.13	0.80	0.80
36.14	107.94	89.77	1.46	130.76	2.12	0.80	0.80
36.15	108.08	89.88	1.45	130.58	2.12	0.80	0.80
36.16	108.18	89.96	1.45	130.46	2.12	0.80	0.80
36.17	108.24	90.00	1.45	130.37	2.12	0.80	0.80
36.18	108.32	90.05	1.45	130.28	2.12	0.80	0.80
36.19	108.39	90.10	1.44	130.18	2.12	0.80	0.80
36.20	108.47	90.16	1.44	130.07	2.12	0.80	0.80
36.21	108.55	90.22	1.44	129.97	2.11	0.80	0.80
36.22	108.62	90.27	1.44	129.88	2.11	0.80	0.80
36.23	108.68	90.30	1.44	129.81	2.11	0.80	0.80
36.24	108.72	90.31	1.44	129.84	2.11	0.80	0.80
36.25	108.73	90.30	1.44	129.97	2.11	0.80	0.80
36.26	108.73	90.28	1.44	130.20	2.12	0.80	0.80
36.27	108.73	90.25	1.45	130.46	2.12	0.80	0.80
36.28	108.73	90.22	1.45	130.75	2.12	0.80	0.80
36.29	108.73	90.19	1.45	131.03	2.12	0.80	0.80
36.30	108.73	90.16	1.46	131.31	2.12	0.80	0.80
36.31	108.73	90.13	1.46	131.56	2.13	0.80	0.80
36.32	108.72	90.10	1.46	131.79	2.13	0.80	0.80
36.33	108.70	90.04	1.47	132.08	2.13	0.80	0.80
36.34	108.64	89.97	1.47	132.46	2.13	0.80	0.80
36.35	108.58	89.87	1.48	132.94	2.14	0.80	0.80
36.36	108.50	89.77	1.49	133.48	2.14	0.80	0.80
36.37	108.42	89.66	1.50	134.04	2.15	0.80	0.80
36.38	108.34	89.55	1.50	134.61	2.15	0.81	0.81
36.39	108.27	89.45	1.51	135.16	2.15	0.81	0.81
36.40	108.20	89.36	1.52	135.64	2.16	0.81	0.81
36.41	108.12	89.25	1.52	136.05	2.16	0.81	0.81
36.42	107.99	89.11	1.53	136.45	2.16	0.81	0.81
36.43	107.81	88.91	1.54	136.89	2.17	0.81	0.81
36.44	107.59	88.69	1.55	137.41	2.17	0.81	0.81
36.45	107.35	88.45	1.56	137.99	2.18	0.81	0.81
36.46	107.11	88.20	1.57	138.59	2.18	0.81	0.81
36.47	106.88	87.96	1.58	139.18	2.19	0.81	0.81
36.48	106.67	87.74	1.59	139.74	2.19	0.81	0.81

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
36.49	106.48	87.55	1.60	140.20	2.19	0.81	0.81
36.50	106.31	87.38	1.61	140.56	2.20	0.81	0.81
36.51	106.14	87.20	1.62	140.86	2.20	0.81	0.81
36.52	105.94	87.00	1.62	141.16	2.20	0.81	0.81
36.53	105.72	86.78	1.63	141.50	2.21	0.82	0.82
36.54	105.48	86.54	1.64	141.87	2.21	0.82	0.82
36.55	105.24	86.31	1.65	142.25	2.21	0.82	0.82
36.56	105.02	86.08	1.66	142.61	2.22	0.82	0.82
36.57	104.81	85.87	1.66	142.93	2.22	0.82	0.82
36.58	104.65	85.71	1.67	143.19	2.22	0.82	0.82
36.59	104.54	85.59	1.68	143.39	2.22	0.82	0.82
36.60	104.47	85.51	1.68	143.56	2.22	0.82	0.82
36.61	104.40	85.42	1.68	143.75	2.23	0.82	0.82
36.62	104.32	85.33	1.69	143.96	2.23	0.82	0.82
36.63	104.24	85.24	1.69	144.17	2.23	0.82	0.82
36.64	104.16	85.15	1.70	144.39	2.23	0.82	0.82
36.65	104.09	85.06	1.70	144.59	2.23	0.82	0.82
36.66	104.02	84.98	1.70	144.77	2.23	0.82	0.82
36.67	103.98	84.93	1.71	144.89	2.23	0.82	0.82
36.68	103.96	84.89	1.71	144.98	2.23	0.82	0.82
36.69	103.96	84.87	1.71	145.04	2.24	0.82	0.82
36.70	103.96	84.85	1.71	145.12	2.24	0.82	0.82
36.71	103.96	84.83	1.71	145.20	2.24	0.82	0.82
36.72	103.96	84.81	1.71	145.28	2.24	0.82	0.82
36.73	103.96	84.79	1.71	145.36	2.24	0.82	0.82
36.74	103.96	84.77	1.72	145.43	2.24	0.82	0.82
36.75	103.96	84.74	1.72	145.49	2.24	0.82	0.82
36.76	103.94	84.70	1.72	145.56	2.24	0.82	0.82
36.77	103.89	84.65	1.72	145.64	2.24	0.82	0.82
36.78	103.83	84.57	1.72	145.74	2.24	0.82	0.82
36.79	103.75	84.48	1.73	145.86	2.24	0.82	0.82
36.80	103.67	84.39	1.73	145.98	2.24	0.82	0.82
36.81	103.59	84.30	1.73	146.11	2.24	0.82	0.82
36.82	103.52	84.22	1.74	146.23	2.24	0.82	0.82
36.83	103.45	84.14	1.74	146.33	2.25	0.82	0.82
36.84	103.38	84.06	1.74	146.44	2.25	0.82	0.82
36.85	103.30	83.96	1.75	146.57	2.25	0.82	0.82
36.86	103.18	83.84	1.75	146.76	2.25	0.82	0.82
36.87	103.04	83.70	1.76	146.99	2.25	0.82	0.82
36.88	102.89	83.54	1.76	147.26	2.25	0.82	0.82
36.89	102.73	83.38	1.77	147.53	2.26	0.82	0.82
36.90	102.57	83.22	1.78	147.80	2.26	0.82	0.82
36.91	102.42	83.07	1.78	148.05	2.26	0.82	0.82
36.92	102.29	82.94	1.79	148.28	2.26	0.82	0.82
36.93	102.15	82.79	1.79	148.41	2.26	0.82	0.82
36.94	101.96	82.61	1.80	148.46	2.26	0.82	0.82
36.95	101.72	82.38	1.80	148.44	2.27	0.82	0.82
36.96	101.42	82.11	1.81	148.41	2.27	0.82	0.82

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)'/σ'_v}	S _{u(peak)'/σ'_v}
36.97	101.11	81.83	1.81	148.38	2.27	0.82	0.82
36.98	100.79	81.54	1.82	148.35	2.27	0.82	0.82
36.99	100.48	81.25	1.83	148.33	2.27	0.82	0.82
37.00	100.19	80.99	1.83	148.30	2.27	0.82	0.82
37.01	99.96	80.77	1.84	148.27	2.28	0.82	0.82
37.02	99.78	80.60	1.84	148.16	2.28	0.82	0.82
37.03	99.64	80.47	1.84	147.97	2.28	0.82	0.82
37.04	99.51	80.34	1.84	147.70	2.28	0.82	0.82
37.05	99.36	80.20	1.84	147.40	2.28	0.82	0.82
37.06	99.20	80.05	1.84	147.08	2.28	0.82	0.82
37.07	99.04	79.91	1.84	146.76	2.28	0.82	0.82
37.08	98.89	79.76	1.84	146.45	2.28	0.82	0.82
37.09	98.75	79.64	1.84	146.18	2.28	0.82	0.82
37.10	98.66	79.55	1.83	145.91	2.27	0.82	0.82
37.11	98.64	79.52	1.83	145.59	2.27	0.82	0.82
37.12	98.68	79.54	1.83	145.19	2.27	0.82	0.82
37.13	98.75	79.60	1.82	144.70	2.27	0.82	0.82
37.14	98.83	79.66	1.81	144.16	2.27	0.82	0.82
37.15	98.91	79.72	1.80	143.60	2.27	0.82	0.82
37.16	98.98	79.78	1.79	143.05	2.26	0.82	0.82
37.17	99.06	79.84	1.79	142.54	2.26	0.82	0.82
37.18	99.12	79.88	1.78	142.09	2.26	0.82	0.82
37.19	99.16	79.91	1.77	141.81	2.26	0.82	0.82
37.20	99.18	79.91	1.77	141.68	2.26	0.82	0.82
37.21	99.18	79.89	1.77	141.67	2.26	0.82	0.82
37.22	99.18	79.88	1.77	141.68	2.26	0.82	0.82
37.23	99.18	79.86	1.77	141.68	2.26	0.82	0.82
37.24	99.18	79.84	1.77	141.69	2.26	0.82	0.82
37.25	99.18	79.82	1.78	141.69	2.26	0.82	0.82
37.26	99.18	79.81	1.78	141.70	2.26	0.82	0.82
37.27	99.19	79.80	1.78	141.67	2.26	0.82	0.82
37.28	99.24	79.82	1.77	141.50	2.26	0.82	0.82
37.29	99.33	79.89	1.77	141.16	2.25	0.81	0.81
37.30	99.46	80.00	1.76	140.66	2.25	0.81	0.81
37.31	99.61	80.12	1.75	140.10	2.25	0.81	0.81
37.32	99.77	80.25	1.74	139.52	2.25	0.81	0.81
37.33	99.93	80.39	1.73	138.94	2.24	0.81	0.81
37.34	100.08	80.51	1.72	138.39	2.24	0.81	0.81
37.35	100.22	80.62	1.71	137.90	2.24	0.81	0.81
37.36	100.32	80.71	1.70	137.43	2.23	0.81	0.81
37.37	100.40	80.78	1.69	136.90	2.23	0.81	0.81
37.38	100.47	80.83	1.69	136.23	2.23	0.81	0.81
37.39	100.54	80.90	1.67	135.42	2.22	0.81	0.81
37.40	100.62	80.97	1.66	134.54	2.22	0.81	0.81
37.41	100.69	81.04	1.65	133.64	2.21	0.80	0.80
37.42	100.77	81.12	1.64	132.76	2.21	0.80	0.80
37.43	100.85	81.19	1.63	131.94	2.20	0.80	0.80
37.44	100.91	81.25	1.62	131.23	2.20	0.80	0.80

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
37.45	100.92	81.24	1.61	130.97	2.20	0.80	0.80
37.46	100.86	81.17	1.62	131.19	2.20	0.80	0.80
37.47	100.74	81.03	1.63	131.87	2.21	0.80	0.80
37.48	100.59	80.86	1.64	132.69	2.21	0.80	0.80
37.49	100.43	80.68	1.66	133.58	2.22	0.80	0.80
37.50	100.27	80.51	1.67	134.50	2.22	0.81	0.81
37.51	100.12	80.33	1.69	135.40	2.23	0.81	0.81
37.52	99.98	80.17	1.70	136.23	2.23	0.81	0.81
37.53	99.86	80.03	1.71	136.92	2.24	0.81	0.81
37.54	99.75	79.91	1.72	137.46	2.24	0.81	0.81
37.55	99.63	79.78	1.73	137.91	2.24	0.81	0.81
37.56	99.50	79.64	1.74	138.37	2.24	0.81	0.81
37.57	99.35	79.48	1.75	138.90	2.25	0.81	0.81
37.58	99.19	79.31	1.76	139.46	2.25	0.81	0.81
37.59	99.03	79.15	1.77	140.02	2.26	0.81	0.81
37.60	98.88	78.99	1.78	140.55	2.26	0.81	0.81
37.61	98.74	78.85	1.79	141.04	2.26	0.81	0.81
37.62	98.62	78.72	1.80	141.45	2.26	0.82	0.82
37.63	98.51	78.60	1.80	141.84	2.27	0.82	0.82
37.64	98.39	78.47	1.81	142.28	2.27	0.82	0.82
37.65	98.25	78.32	1.82	142.79	2.27	0.82	0.82
37.66	98.10	78.16	1.83	143.35	2.27	0.82	0.82
37.67	97.94	78.00	1.85	143.94	2.28	0.82	0.82
37.68	97.78	77.83	1.86	144.52	2.28	0.82	0.82
37.69	97.64	77.68	1.87	145.06	2.28	0.82	0.82
37.70	97.51	77.55	1.88	145.54	2.29	0.82	0.82
37.71	97.39	77.42	1.89	146.12	2.29	0.82	0.82
37.72	97.28	77.29	1.90	146.93	2.29	0.82	0.82
37.73	97.16	77.15	1.92	148.05	2.30	0.82	0.82
37.74	97.01	76.98	1.94	149.35	2.30	0.83	0.83
37.75	96.85	76.80	1.96	150.76	2.31	0.83	0.83
37.76	96.69	76.62	1.99	152.19	2.32	0.83	0.83
37.77	96.54	76.45	2.01	153.59	2.32	0.83	0.83
37.78	96.40	76.29	2.03	154.87	2.33	0.83	0.83
37.79	96.27	76.14	2.05	155.97	2.33	0.83	0.83
37.80	96.11	75.98	2.07	156.97	2.34	0.84	0.84
37.81	95.90	75.76	2.09	158.01	2.34	0.84	0.84
37.82	95.63	75.50	2.11	159.22	2.35	0.84	0.84
37.83	95.33	75.21	2.14	160.59	2.35	0.84	0.84
37.84	95.01	74.90	2.16	162.03	2.36	0.84	0.84
37.85	94.69	74.59	2.19	163.48	2.36	0.84	0.84
37.86	94.39	74.30	2.22	164.85	2.37	0.85	0.85
37.87	94.12	74.04	2.24	166.08	2.37	0.85	0.85
37.88	93.88	73.80	2.27	167.19	2.38	0.85	0.85
37.89	93.63	73.56	2.29	168.35	2.38	0.85	0.85
37.90	93.33	73.27	2.32	169.72	2.39	0.85	0.85
37.91	92.98	72.94	2.35	171.36	2.40	0.85	0.85
37.92	92.59	72.57	2.39	173.15	2.40	0.86	0.86

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
37.93	92.19	72.20	2.42	175.01	2.41	0.86	0.86
37.94	91.80	71.83	2.46	176.83	2.42	0.86	0.86
37.95	91.43	71.48	2.50	178.52	2.42	0.86	0.86
37.96	91.12	71.18	2.53	179.99	2.43	0.86	0.86
37.97	90.82	70.90	2.56	181.19	2.43	0.87	0.87
37.98	90.50	70.60	2.58	182.28	2.44	0.87	0.87
37.99	90.11	70.25	2.61	183.41	2.44	0.87	0.87
38.00	89.67	69.86	2.64	184.70	2.45	0.87	0.87
38.01	89.20	69.43	2.68	186.09	2.45	0.87	0.87
38.02	88.72	69.00	2.72	187.49	2.46	0.87	0.87
38.03	88.26	68.59	2.75	188.84	2.47	0.87	0.87
38.04	87.84	68.20	2.79	190.06	2.47	0.88	0.88
38.05	87.48	67.89	2.81	191.05	2.48	0.88	0.88
38.06	87.20	67.63	2.84	191.76	2.48	0.88	0.88
38.07	86.95	67.40	2.85	192.30	2.48	0.88	0.88
38.08	86.68	67.15	2.87	192.80	2.48	0.88	0.88
38.09	86.37	66.88	2.89	193.37	2.49	0.88	0.88
38.10	86.06	66.59	2.91	193.96	2.49	0.88	0.88
38.11	85.74	66.31	2.93	194.55	2.49	0.88	0.88
38.12	85.44	66.04	2.95	195.10	2.50	0.88	0.88
38.13	85.17	65.80	2.97	195.59	2.50	0.88	0.88
38.14	85.10	65.72	2.98	195.91	2.50	0.87	0.87
38.15	85.36	65.92	2.97	196.03	2.50	0.88	0.88
38.16	85.95	66.39	2.95	195.97	2.50	0.88	0.88
38.17	86.73	67.01	2.92	195.84	2.49	0.88	0.88
38.18	87.59	67.70	2.89	195.70	2.49	0.88	0.88
38.19	88.47	68.40	2.86	195.55	2.48	0.88	0.88
38.20	89.33	69.10	2.83	195.39	2.48	0.88	0.88
38.21	90.14	69.75	2.80	195.24	2.47	0.88	0.88
38.22	90.84	70.31	2.77	195.09	2.47	0.88	0.88
38.23	91.74	71.04	2.74	194.78	2.46	0.88	0.88
38.24	93.00	72.06	2.70	194.22	2.46	0.88	0.88
38.25	94.73	73.48	2.63	193.37	2.45	0.88	0.88
38.26	96.72	75.11	2.56	192.37	2.43	0.88	0.88
38.27	98.84	76.86	2.49	191.26	2.42	0.88	0.88
38.28	101.01	78.64	2.42	190.12	2.41	0.88	0.88
38.29	103.09	80.36	2.35	188.99	2.40	0.87	0.87
38.30	104.99	81.93	2.29	187.95	2.38	0.87	0.87
38.31	106.63	83.28	2.25	187.06	2.37	0.87	0.87
38.32	108.17	84.55	2.20	186.22	2.37	0.87	0.87
38.33	109.84	85.93	2.16	185.34	2.36	0.87	0.87
38.34	111.81	87.56	2.10	184.32	2.34	0.87	0.87
38.35	114.00	89.39	2.05	183.19	2.33	0.87	0.87
38.36	116.31	91.32	1.99	182.02	2.32	0.87	0.87
38.37	118.62	93.24	1.94	180.87	2.30	0.87	0.87
38.38	120.80	95.07	1.89	179.81	2.29	0.86	0.86
38.39	122.75	96.70	1.85	178.89	2.28	0.86	0.86
38.40	124.30	98.00	1.82	178.43	2.27	0.86	0.86

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
38.41	125.59	99.05	1.80	178.53	2.27	0.86	0.86
38.42	126.79	100.02	1.79	179.19	2.26	0.86	0.86
38.43	128.14	101.11	1.78	180.10	2.26	0.86	0.86
38.44	129.62	102.30	1.77	181.09	2.26	0.87	0.87
38.45	131.14	103.53	1.76	182.13	2.25	0.87	0.87
38.46	132.63	104.73	1.75	183.14	2.25	0.87	0.87
38.47	134.02	105.85	1.74	184.09	2.25	0.87	0.87
38.48	135.21	106.81	1.73	184.93	2.24	0.87	0.87
38.49	135.93	107.36	1.73	185.92	2.24	0.87	0.87
38.50	136.24	107.56	1.74	187.22	2.25	0.87	0.87
38.51	136.24	107.49	1.76	189.00	2.25	0.87	0.87
38.52	136.24	107.41	1.78	191.06	2.26	0.88	0.88
38.53	136.24	107.33	1.80	193.28	2.26	0.88	0.88
38.54	136.24	107.25	1.82	195.55	2.27	0.88	0.88
38.55	136.25	107.17	1.85	197.76	2.28	0.88	0.88
38.56	136.25	107.10	1.87	199.79	2.28	0.89	0.89
38.57	136.17	106.97	1.88	201.49	2.29	0.89	0.89
38.58	135.87	106.66	1.90	202.97	2.29	0.89	0.89
38.59	135.29	106.12	1.93	204.41	2.30	0.89	0.89
38.60	134.48	105.38	1.96	206.05	2.31	0.89	0.89
38.61	133.57	104.56	1.99	207.89	2.32	0.90	0.90
38.62	132.61	103.70	2.02	209.85	2.33	0.90	0.90
38.63	131.66	102.85	2.06	211.80	2.33	0.90	0.90
38.64	130.76	102.04	2.09	213.67	2.34	0.90	0.90
38.65	129.95	101.32	2.13	215.32	2.35	0.90	0.90
38.66	129.23	100.67	2.15	216.77	2.36	0.90	0.90
38.67	128.46	99.99	2.18	218.20	2.36	0.91	0.91
38.68	127.56	99.19	2.22	219.82	2.37	0.91	0.91
38.69	126.49	98.25	2.26	221.71	2.38	0.91	0.91
38.70	125.33	97.24	2.30	223.77	2.39	0.91	0.91
38.71	124.13	96.19	2.35	225.89	2.40	0.91	0.91
38.72	122.95	95.17	2.40	227.96	2.40	0.92	0.92
38.73	121.86	94.22	2.44	229.87	2.41	0.92	0.92
38.74	120.92	93.40	2.48	231.50	2.42	0.92	0.92
38.75	120.17	92.75	2.51	232.64	2.42	0.92	0.92
38.76	119.53	92.19	2.53	233.43	2.43	0.92	0.92
38.77	118.88	91.63	2.55	234.03	2.43	0.92	0.92
38.78	118.14	91.00	2.58	234.71	2.44	0.92	0.92
38.79	117.35	90.32	2.61	235.43	2.44	0.92	0.92
38.80	116.55	89.63	2.63	236.16	2.45	0.92	0.92
38.81	115.79	88.97	2.66	236.85	2.45	0.92	0.92
38.82	115.09	88.37	2.69	237.47	2.46	0.92	0.92
38.83	114.58	87.94	2.70	237.85	2.46	0.92	0.92
38.84	114.42	87.78	2.71	237.76	2.46	0.92	0.92
38.85	114.57	87.89	2.70	237.19	2.46	0.92	0.92
38.86	114.91	88.16	2.68	236.27	2.45	0.92	0.92
38.87	115.29	88.46	2.66	235.25	2.45	0.92	0.92
38.88	115.69	88.78	2.64	234.17	2.45	0.92	0.92

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
38.89	116.08	89.09	2.62	233.10	2.44	0.92	0.92
38.90	116.46	89.39	2.60	232.08	2.44	0.92	0.92
38.91	116.79	89.65	2.58	231.18	2.44	0.92	0.92
38.92	117.22	89.99	2.56	230.20	2.43	0.92	0.92
38.93	117.86	90.51	2.53	228.95	2.43	0.92	0.92
38.94	118.80	91.28	2.49	227.25	2.42	0.91	0.91
38.95	119.94	92.22	2.44	225.21	2.41	0.91	0.91
38.96	121.18	93.25	2.39	222.97	2.40	0.91	0.91
38.97	122.46	94.31	2.34	220.65	2.39	0.91	0.91
38.98	123.72	95.35	2.29	218.38	2.38	0.91	0.91
38.99	124.88	96.32	2.25	216.27	2.37	0.90	0.90
39.00	125.89	97.16	2.21	214.43	2.37	0.90	0.90
39.01	126.86	97.96	2.17	212.76	2.36	0.90	0.90
39.02	127.93	98.85	2.13	211.04	2.35	0.90	0.90
39.03	129.23	99.94	2.09	209.04	2.34	0.90	0.90
39.04	130.71	101.18	2.04	206.78	2.33	0.89	0.89
39.05	132.29	102.50	1.99	204.38	2.32	0.89	0.89
39.06	133.89	103.85	1.94	201.98	2.31	0.89	0.89
39.07	135.42	105.15	1.90	199.70	2.29	0.89	0.89
39.08	136.82	106.33	1.86	197.67	2.28	0.88	0.88
39.09	137.99	107.32	1.83	196.07	2.27	0.88	0.88
39.10	139.01	108.18	1.80	194.96	2.27	0.88	0.88
39.11	140.04	109.03	1.78	194.17	2.26	0.88	0.88
39.12	141.20	110.00	1.76	193.45	2.25	0.88	0.88
39.13	142.50	111.07	1.73	192.67	2.24	0.88	0.88
39.14	143.85	112.21	1.71	191.87	2.24	0.88	0.88
39.15	145.20	113.33	1.69	191.11	2.23	0.88	0.88
39.16	146.47	114.40	1.66	190.41	2.22	0.88	0.88
39.17	147.60	115.34	1.65	189.82	2.21	0.88	0.88
39.18	148.54	116.11	1.63	189.53	2.21	0.88	0.88
39.19	149.38	116.79	1.62	189.63	2.20	0.88	0.88
39.20	150.25	117.48	1.62	190.08	2.20	0.88	0.88
39.21	151.26	118.28	1.61	190.69	2.20	0.88	0.88
39.22	152.35	119.15	1.61	191.35	2.20	0.88	0.88
39.23	153.47	120.04	1.60	192.04	2.19	0.88	0.88
39.24	154.56	120.91	1.59	192.71	2.19	0.88	0.88
39.25	155.58	121.71	1.59	193.33	2.19	0.88	0.88
39.26	156.45	122.40	1.58	193.87	2.19	0.88	0.88
39.27	157.15	122.95	1.58	194.40	2.19	0.88	0.88
39.28	157.78	123.43	1.58	195.00	2.19	0.88	0.88
39.29	158.43	123.92	1.58	195.73	2.19	0.88	0.88
39.30	159.18	124.49	1.58	196.56	2.19	0.88	0.88
39.31	159.97	125.09	1.58	197.46	2.19	0.88	0.88
39.32	160.77	125.70	1.58	198.36	2.18	0.89	0.89
39.33	161.53	126.29	1.58	199.23	2.18	0.89	0.89
39.34	162.23	126.81	1.58	200.01	2.18	0.89	0.89
39.35	162.80	127.24	1.58	200.63	2.18	0.89	0.89
39.36	163.28	127.60	1.58	201.06	2.18	0.89	0.89

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
39.37	163.71	127.93	1.57	201.36	2.18	0.89	0.89
39.38	164.20	128.29	1.57	201.65	2.18	0.89	0.89
39.39	164.73	128.70	1.57	201.97	2.18	0.89	0.89
39.40	165.29	129.13	1.57	202.30	2.18	0.89	0.89
39.41	165.84	129.56	1.56	202.64	2.18	0.89	0.89
39.42	166.37	129.96	1.56	202.96	2.18	0.89	0.89
39.43	166.83	130.31	1.56	203.23	2.18	0.89	0.89
39.44	167.20	130.58	1.56	203.50	2.18	0.89	0.89
39.45	167.53	130.81	1.56	203.82	2.18	0.89	0.89
39.46	167.84	131.03	1.56	204.22	2.18	0.89	0.89
39.47	168.20	131.29	1.56	204.71	2.18	0.89	0.89
39.48	168.59	131.56	1.56	205.24	2.18	0.89	0.89
39.49	168.99	131.85	1.56	205.79	2.18	0.89	0.89
39.50	169.38	132.13	1.56	206.32	2.18	0.89	0.89
39.51	169.74	132.38	1.56	206.81	2.18	0.89	0.89
39.52	170.05	132.59	1.56	207.23	2.18	0.89	0.89
39.53	170.25	132.71	1.56	207.59	2.18	0.89	0.89
39.54	170.36	132.77	1.57	207.95	2.18	0.90	0.90
39.55	170.43	132.77	1.57	208.35	2.18	0.90	0.90
39.56	170.50	132.79	1.57	208.82	2.18	0.90	0.90
39.57	170.58	132.80	1.58	209.32	2.18	0.90	0.90
39.58	170.66	132.82	1.58	209.82	2.19	0.90	0.90
39.59	170.74	132.83	1.58	210.30	2.19	0.90	0.90
39.60	170.81	132.85	1.59	210.74	2.19	0.90	0.90
39.61	170.88	132.86	1.59	210.99	2.19	0.90	0.90
39.62	170.96	132.90	1.59	210.91	2.19	0.90	0.90
39.63	171.07	132.99	1.58	210.48	2.19	0.90	0.90
39.64	171.21	133.10	1.58	209.83	2.18	0.90	0.90
39.65	171.36	133.23	1.57	209.12	2.18	0.90	0.90
39.66	171.52	133.36	1.56	208.38	2.18	0.90	0.90
39.67	171.67	133.50	1.56	207.66	2.18	0.89	0.89
39.68	171.82	133.63	1.55	206.99	2.17	0.89	0.89
39.69	171.95	133.74	1.54	206.39	2.17	0.89	0.89
39.70	172.07	133.83	1.54	205.89	2.17	0.89	0.89
39.71	172.18	133.91	1.53	205.41	2.16	0.89	0.89
39.72	172.30	134.01	1.53	204.91	2.16	0.89	0.89
39.73	172.45	134.13	1.52	204.34	2.16	0.89	0.89
39.74	172.60	134.26	1.52	203.73	2.16	0.89	0.89
39.75	172.76	134.40	1.51	203.10	2.15	0.89	0.89
39.76	172.92	134.54	1.51	202.50	2.15	0.89	0.89
39.77	173.06	134.66	1.50	201.95	2.15	0.89	0.89
39.78	173.17	134.74	1.50	201.49	2.15	0.89	0.89
39.79	173.13	134.70	1.49	201.17	2.14	0.89	0.89
39.80	172.93	134.51	1.49	200.96	2.14	0.89	0.89
39.81	172.58	134.19	1.50	200.81	2.15	0.89	0.89
39.82	172.18	133.83	1.50	200.64	2.15	0.89	0.89
39.83	171.76	133.45	1.50	200.46	2.15	0.89	0.89
39.84	171.33	133.07	1.51	200.28	2.15	0.89	0.89

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
39.85	170.92	132.70	1.51	200.11	2.15	0.89	0.89
39.86	170.55	132.37	1.51	199.96	2.15	0.89	0.89
39.87	170.19	132.03	1.51	199.85	2.16	0.89	0.89
39.88	169.71	131.60	1.52	199.80	2.16	0.89	0.89
39.89	169.05	131.01	1.53	199.83	2.16	0.89	0.89
39.90	168.22	130.28	1.53	199.90	2.17	0.89	0.89
39.91	167.30	129.47	1.54	199.99	2.17	0.89	0.89
39.92	166.34	128.63	1.56	200.10	2.18	0.89	0.89
39.93	165.39	127.80	1.57	200.22	2.18	0.89	0.89
39.94	164.50	127.02	1.58	200.34	2.18	0.89	0.89
39.95	163.71	126.32	1.59	200.46	2.19	0.89	0.89
39.96	163.15	125.82	1.59	200.67	2.19	0.89	0.89
39.97	162.77	125.46	1.60	201.04	2.20	0.89	0.89
39.98	162.53	125.20	1.61	201.62	2.20	0.89	0.89
39.99	162.26	124.92	1.62	202.31	2.20	0.89	0.89
40.00	161.98	124.63	1.63	203.08	2.21	0.89	0.89
40.01	161.68	124.33	1.64	203.87	2.21	0.89	0.89
40.02	161.40	124.03	1.65	204.66	2.21	0.89	0.89
40.03	161.14	123.76	1.66	205.38	2.22	0.89	0.89
40.04	160.96	123.56	1.67	205.98	2.22	0.89	0.89
40.05	161.13	123.66	1.67	206.34	2.22	0.89	0.89
40.06	161.68	124.08	1.66	206.51	2.22	0.89	0.89
40.07	162.61	124.82	1.65	206.55	2.22	0.89	0.89
40.08	163.65	125.66	1.64	206.62	2.21	0.89	0.89
40.09	164.76	126.55	1.63	206.69	2.21	0.89	0.89
40.10	165.88	127.44	1.62	206.77	2.20	0.89	0.89
40.11	166.95	128.30	1.61	206.86	2.20	0.89	0.89
40.12	167.91	129.07	1.60	206.94	2.20	0.89	0.89
40.13	168.71	129.71	1.60	206.96	2.19	0.89	0.89
40.14	169.40	130.26	1.59	206.86	2.19	0.89	0.89
40.15	170.08	130.80	1.58	206.62	2.19	0.89	0.89
40.16	170.84	131.43	1.57	206.31	2.18	0.89	0.89
40.17	171.68	132.12	1.56	205.98	2.18	0.89	0.89
40.18	172.56	132.84	1.55	205.64	2.17	0.89	0.89
40.19	173.43	133.56	1.54	205.33	2.17	0.89	0.89
40.20	174.25	134.23	1.53	205.04	2.16	0.89	0.89
40.21	174.97	134.82	1.52	204.80	2.16	0.89	0.89
40.22	175.43	135.19	1.51	204.58	2.15	0.89	0.89
40.23	175.65	135.36	1.51	204.37	2.15	0.89	0.89
40.24	175.67	135.36	1.51	204.12	2.15	0.89	0.89
40.25	175.67	135.35	1.51	203.84	2.15	0.89	0.89
40.26	175.67	135.34	1.50	203.55	2.15	0.89	0.89
40.27	175.67	135.32	1.50	203.24	2.15	0.89	0.89
40.28	175.67	135.31	1.50	202.95	2.15	0.89	0.89
40.29	175.67	135.30	1.50	202.67	2.15	0.89	0.89
40.30	175.66	135.27	1.50	202.43	2.15	0.89	0.89
40.31	175.62	135.22	1.50	202.18	2.15	0.89	0.89
40.32	175.53	135.13	1.49	201.89	2.14	0.89	0.89

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
40.33	175.40	135.01	1.49	201.53	2.14	0.89	0.89
40.34	175.25	134.88	1.49	201.13	2.14	0.89	0.89
40.35	175.09	134.74	1.49	200.71	2.14	0.89	0.89
40.36	174.93	134.60	1.49	200.29	2.14	0.89	0.89
40.37	174.78	134.46	1.49	199.89	2.14	0.89	0.89
40.38	174.64	134.34	1.49	199.52	2.14	0.89	0.89
40.39	174.50	134.22	1.48	199.19	2.14	0.89	0.89
40.40	174.34	134.06	1.48	198.85	2.14	0.89	0.89
40.41	174.11	133.87	1.48	198.45	2.14	0.89	0.89
40.42	173.83	133.63	1.48	197.97	2.14	0.88	0.88
40.43	173.53	133.37	1.48	197.45	2.14	0.88	0.88
40.44	173.21	133.11	1.48	196.91	2.14	0.88	0.88
40.45	172.89	132.84	1.48	196.37	2.14	0.88	0.88
40.46	172.59	132.59	1.48	195.87	2.14	0.88	0.88
40.47	172.33	132.37	1.48	195.43	2.14	0.88	0.88
40.48	172.09	132.16	1.48	195.06	2.14	0.88	0.88
40.49	171.83	131.93	1.48	194.72	2.14	0.88	0.88
40.50	171.52	131.65	1.48	194.38	2.14	0.88	0.88
40.51	171.15	131.34	1.48	193.99	2.14	0.88	0.88
40.52	170.76	131.01	1.48	193.58	2.14	0.88	0.88
40.53	170.36	130.67	1.48	193.15	2.14	0.88	0.88
40.54	169.97	130.33	1.48	192.74	2.14	0.88	0.88
40.55	169.61	130.02	1.48	192.35	2.14	0.88	0.88
40.56	169.29	129.74	1.48	192.01	2.14	0.88	0.88
40.57	168.90	129.41	1.48	191.65	2.14	0.88	0.88
40.58	168.39	128.97	1.48	191.21	2.14	0.88	0.88
40.59	167.73	128.42	1.48	190.67	2.14	0.88	0.88
40.60	166.98	127.79	1.49	190.07	2.14	0.88	0.88
40.61	166.18	127.13	1.49	189.43	2.14	0.88	0.88
40.62	165.39	126.47	1.49	188.79	2.14	0.87	0.87
40.63	164.62	125.83	1.50	188.18	2.15	0.87	0.87
40.64	163.94	125.26	1.50	187.63	2.15	0.87	0.87
40.65	163.33	124.75	1.50	187.14	2.15	0.87	0.87
40.66	162.68	124.21	1.50	186.63	2.15	0.87	0.87
40.67	161.93	123.58	1.51	186.02	2.15	0.87	0.87
40.68	161.02	122.83	1.51	185.31	2.15	0.87	0.87
40.69	160.02	122.01	1.51	184.53	2.15	0.87	0.87
40.70	158.98	121.15	1.52	183.72	2.16	0.87	0.87
40.71	157.95	120.31	1.52	182.92	2.16	0.87	0.87
40.72	156.99	119.52	1.52	182.18	2.16	0.87	0.87
40.73	156.15	118.82	1.53	181.52	2.16	0.87	0.87
40.74	155.38	118.18	1.53	181.01	2.16	0.87	0.87
40.75	154.58	117.51	1.54	180.58	2.17	0.87	0.87
40.76	153.64	116.72	1.54	180.19	2.17	0.86	0.86
40.77	152.55	115.81	1.55	179.74	2.17	0.86	0.86
40.78	151.37	114.83	1.56	179.28	2.18	0.86	0.86
40.79	150.17	113.83	1.57	178.81	2.18	0.86	0.86
40.80	149.00	112.86	1.58	178.36	2.19	0.86	0.86

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
40.81	147.93	111.97	1.59	177.96	2.19	0.86	0.86
40.82	147.00	111.20	1.60	177.60	2.19	0.86	0.86
40.83	146.10	110.45	1.60	177.19	2.20	0.86	0.86
40.84	145.10	109.62	1.61	176.69	2.20	0.86	0.86
40.85	143.90	108.64	1.62	176.06	2.20	0.86	0.86
40.86	142.55	107.53	1.63	175.36	2.21	0.86	0.86
40.87	141.12	106.37	1.64	174.62	2.21	0.86	0.86
40.88	139.69	105.20	1.65	173.89	2.22	0.86	0.86
40.89	138.32	104.08	1.66	173.21	2.22	0.86	0.86
40.90	137.09	103.08	1.67	172.59	2.22	0.86	0.86
40.91	136.02	102.21	1.68	171.99	2.23	0.86	0.86
40.92	134.96	101.35	1.69	171.27	2.23	0.85	0.85
40.93	133.78	100.40	1.70	170.33	2.23	0.85	0.85
40.94	132.38	99.28	1.70	169.17	2.23	0.85	0.85
40.95	130.83	98.06	1.71	167.91	2.24	0.85	0.85
40.96	129.23	96.78	1.72	166.61	2.24	0.85	0.85
40.97	127.66	95.53	1.73	165.33	2.24	0.85	0.85
40.98	126.18	94.35	1.74	164.13	2.25	0.85	0.85
40.99	124.89	93.32	1.75	163.09	2.25	0.84	0.84
41.00	123.77	92.43	1.76	162.22	2.25	0.84	0.84
41.01	122.69	91.56	1.76	161.42	2.25	0.84	0.84
41.02	121.48	90.60	1.77	160.58	2.26	0.84	0.84
41.03	120.10	89.50	1.78	159.62	2.26	0.84	0.84
41.04	118.61	88.31	1.80	158.60	2.26	0.84	0.84
41.05	117.09	87.10	1.81	157.56	2.27	0.84	0.84
41.06	115.61	85.92	1.82	156.55	2.27	0.84	0.84
41.07	114.26	84.85	1.83	155.64	2.27	0.83	0.83
41.08	113.09	83.91	1.85	154.86	2.28	0.83	0.83
41.09	111.98	83.03	1.86	154.18	2.28	0.83	0.83
41.10	110.78	82.07	1.87	153.50	2.29	0.83	0.83
41.11	109.36	80.94	1.89	152.73	2.29	0.83	0.83
41.12	107.76	79.67	1.91	151.88	2.30	0.83	0.83
41.13	106.07	78.32	1.93	150.99	2.30	0.83	0.83
41.14	104.38	76.98	1.95	150.10	2.31	0.83	0.83
41.15	102.77	75.70	1.97	149.27	2.31	0.83	0.83
41.16	101.32	74.56	1.99	148.53	2.32	0.82	0.82
41.17	100.10	73.58	2.01	147.84	2.32	0.82	0.82
41.18	98.96	72.68	2.02	147.07	2.33	0.82	0.82
41.19	97.75	71.73	2.04	146.12	2.33	0.82	0.82
41.20	96.34	70.63	2.05	144.97	2.33	0.82	0.82
41.21	94.80	69.42	2.07	143.73	2.34	0.82	0.82
41.22	93.20	68.18	2.09	142.44	2.34	0.82	0.82
41.23	91.62	66.94	2.11	141.18	2.35	0.81	0.81
41.24	90.15	65.79	2.13	140.01	2.35	0.81	0.81
41.25	88.86	64.79	2.15	138.99	2.35	0.81	0.81
41.26	87.86	64.01	2.16	138.33	2.36	0.81	0.81
41.27	87.06	63.36	2.18	137.96	2.36	0.81	0.81
41.28	86.30	62.76	2.20	137.83	2.36	0.81	0.81

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
41.29	85.45	62.08	2.22	137.68	2.37	0.81	0.81
41.30	84.52	61.34	2.24	137.53	2.37	0.81	0.81
41.31	83.58	60.59	2.27	137.37	2.38	0.81	0.81
41.32	82.67	59.86	2.29	137.22	2.38	0.81	0.81
41.33	81.84	59.20	2.32	137.09	2.39	0.81	0.81
41.34	81.13	58.63	2.34	137.01	2.39	0.81	0.81
41.35	80.52	58.14	2.36	137.11	2.40	0.81	0.81
41.36	79.92	57.65	2.38	137.41	2.40	0.81	0.81
41.37	79.25	57.11	2.41	137.87	2.41	0.81	0.81
41.38	78.50	56.49	2.45	138.40	2.41	0.81	0.81
41.39	77.70	55.85	2.49	138.94	2.42	0.81	0.81
41.40	76.91	55.21	2.53	139.49	2.43	0.81	0.81
41.41	76.15	54.59	2.56	140.01	2.43	0.81	0.81
41.42	75.47	54.05	2.60	140.47	2.44	0.81	0.81
41.43	74.90	53.58	2.63	140.88	2.45	0.81	0.81
41.44	74.37	53.15	2.66	141.31	2.45	0.81	0.81
41.45	73.80	52.69	2.69	141.81	2.46	0.82	0.82
41.46	73.15	52.16	2.73	142.41	2.46	0.82	0.82
41.47	72.44	51.59	2.77	143.07	2.47	0.82	0.82
41.48	71.70	50.99	2.82	143.74	2.48	0.82	0.82
41.49	70.97	50.40	2.86	144.39	2.48	0.82	0.82
41.50	70.29	49.86	2.91	144.99	2.49	0.82	0.82
41.51	69.70	49.38	2.95	145.51	2.50	0.82	0.82
41.52	69.17	48.95	2.99	146.15	2.50	0.81	0.81
41.53	68.64	48.52	3.03	147.02	2.51	0.82	0.82
41.54	68.04	48.02	3.09	148.23	2.52	0.83	0.83
41.55	67.34	47.46	3.15	149.59	2.52	0.84	0.84
41.56	66.60	46.85	3.22	151.04	2.53	0.85	0.85
41.57	65.84	46.23	3.30	152.49	2.54	0.86	0.86
41.58	65.10	45.64	3.37	153.87	2.55	0.87	0.87
41.59	64.43	45.10	3.44	155.10	2.56	0.88	0.88
41.60	63.85	44.63	3.50	156.13	2.57	0.88	0.88
41.61	63.29	44.18	3.55	157.01	2.58	0.89	0.89
41.62	62.68	43.69	3.61	157.87	2.58	0.90	0.90
41.63	61.96	43.12	3.68	158.82	2.59	0.91	0.91
41.64	61.15	42.47	3.76	159.86	2.60	0.92	0.92
41.65	60.29	41.80	3.85	160.92	2.61	0.93	0.93
41.66	59.44	41.13	3.94	161.95	2.62	0.94	0.94
41.67	58.62	40.49	4.02	162.89	2.63	0.95	0.95
41.68	57.90	39.92	4.10	163.71	2.64	0.96	0.96
41.69	57.29	39.44	4.17	164.40	2.65	0.97	0.97
41.70	56.73	39.00	4.23	165.09	2.65	0.97	0.97
41.71	56.15	38.54	4.30	165.87	2.66	0.98	0.98
41.72	55.48	38.01	4.39	166.77	2.67	0.99	0.99
41.73	54.74	37.44	4.48	167.71	2.68	1.00	1.00
41.74	53.98	36.85	4.58	168.65	2.69	1.01	1.01
41.75	53.24	36.27	4.68	169.54	2.70	1.02	1.02
41.76	52.54	35.72	4.77	170.33	2.71	0.85	0.85

:: Strength loss calculation (Robertson (2009)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
41.77	51.93	35.25	4.85	170.99	2.71	0.85	0.85
41.78	51.42	34.85	4.92	171.65	2.72	0.85	0.85
41.79	50.95	34.48	5.00	172.42	2.73	0.86	0.86
41.80	50.44	34.08	5.09	173.39	2.74	0.86	0.86
41.81	49.85	33.62	5.19	174.47	2.74	0.86	0.86
41.82	49.22	33.13	5.30	175.58	2.75	0.86	0.86
41.83	48.58	32.63	5.41	176.67	2.76	0.86	0.86
41.84	47.96	32.15	5.53	177.67	2.77	0.86	0.86
41.85	47.40	31.71	5.63	178.55	2.78	0.86	0.86
41.86	46.94	31.35	5.72	179.29	2.79	0.86	0.86
41.87	46.59	31.08	5.79	180.05	2.80	0.86	0.86
41.88	46.32	30.86	5.86	180.93	2.80	0.87	0.87
41.89	46.05	30.64	5.94	182.00	2.81	0.87	0.87
41.90	45.74	30.40	6.03	183.18	2.81	0.87	0.87
41.91	45.42	30.14	6.12	184.38	2.82	0.87	0.87
41.92	45.11	29.89	6.21	185.57	2.83	0.87	0.87
41.93	44.81	29.65	6.30	186.66	2.83	0.87	0.87
41.94	44.54	29.43	6.37	187.62	2.84	0.87	0.87
41.95	44.36	29.30	6.43	188.36	2.84	0.87	0.87
41.96	44.30	29.25	6.46	188.87	2.85	0.87	0.87
41.97	44.34	29.27	6.47	189.23	2.85	0.88	0.88
41.98	44.41	29.31	6.47	189.60	2.85	0.88	0.88
41.99	44.48	29.36	6.47	190.01	2.85	0.88	0.88
42.00	44.56	29.41	6.48	190.43	2.85	0.88	0.88
42.01	44.64	29.45	6.48	190.84	2.85	0.88	0.88
42.02	44.72	29.50	6.48	191.23	2.85	0.88	0.88
42.03	44.78	29.54	6.49	191.55	2.85	0.88	0.88
42.04	44.98	29.67	6.46	191.60	2.85	0.88	0.88
42.05	45.36	29.92	6.39	191.34	2.84	0.88	0.88
42.06	45.93	30.34	6.29	190.81	2.83	0.88	0.88
42.07	46.60	30.83	6.17	190.18	2.82	0.88	0.88
42.08	47.30	31.35	6.04	189.44	2.82	0.88	0.88
42.09	48.02	31.89	5.92	188.65	2.81	0.87	0.87
42.10	48.72	32.40	5.80	187.83	2.80	0.87	0.87
42.11	49.35	32.87	5.69	187.04	2.79	0.87	0.87
42.12	49.92	33.29	5.60	186.28	2.78	0.87	0.87
42.13	50.55	33.76	5.49	185.34	2.77	0.87	0.87
42.14	51.31	34.33	5.36	184.09	2.76	0.87	0.87
42.15	52.26	35.04	5.21	182.43	2.75	0.87	0.87
42.16	53.32	35.84	5.03	180.46	2.73	0.87	0.87
42.17	54.43	36.69	4.86	178.27	2.71	0.86	0.86
42.18	55.55	37.54	4.69	175.95	2.70	1.03	1.03
42.19	56.60	38.34	4.53	173.63	2.68	1.02	1.02
42.20	57.54	39.06	4.39	171.48	2.67	1.00	1.00
42.21	58.32	39.67	4.28	169.63	2.66	0.98	0.98
42.22	59.04	40.21	4.18	167.91	2.65	0.97	0.97
42.23	59.77	40.78	4.07	166.11	2.64	0.96	0.96
42.24	60.63	41.44	3.96	163.98	2.62	0.94	0.94

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
42.25	61.56	42.16	3.83	161.59	2.61	0.93	0.93
42.26	62.52	42.91	3.71	159.04	2.59	0.91	0.91
42.27	63.46	43.65	3.58	156.47	2.58	0.89	0.89
42.28	64.33	44.34	3.47	154.02	2.57	0.88	0.88
42.29	65.09	44.93	3.38	151.86	2.55	0.87	0.87
42.30	65.65	45.37	3.31	150.28	2.55	0.86	0.86
42.31	66.09	45.71	3.26	149.13	2.54	0.85	0.85
42.32	66.47	46.01	3.22	148.19	2.53	0.84	0.84
42.33	66.92	46.35	3.17	147.11	2.53	0.83	0.83
42.34	67.39	46.72	3.12	145.95	2.52	0.83	0.83
42.35	67.87	47.10	3.07	144.75	2.51	0.82	0.82
42.36	68.33	47.46	3.03	143.59	2.51	0.81	0.81
42.37	68.75	47.78	2.98	142.53	2.50	0.81	0.81
42.38	69.04	48.00	2.95	141.71	2.50	0.82	0.82
42.39	69.05	48.02	2.94	141.26	2.49	0.81	0.81
42.40	68.80	47.81	2.95	141.14	2.50	0.81	0.81
42.41	68.36	47.47	2.97	141.18	2.50	0.81	0.81
42.42	67.87	47.09	3.00	141.22	2.50	0.81	0.81
42.43	67.36	46.69	3.03	141.26	2.51	0.81	0.81
42.44	66.85	46.29	3.05	141.30	2.51	0.81	0.81
42.45	66.36	45.91	3.08	141.33	2.51	0.82	0.82
42.46	65.93	45.57	3.10	141.36	2.52	0.82	0.82
42.47	65.49	45.23	3.13	141.60	2.52	0.82	0.82
42.48	64.95	44.80	3.17	142.19	2.53	0.83	0.83
42.49	64.24	44.23	3.24	143.19	2.54	0.84	0.84
42.50	63.39	43.56	3.32	144.42	2.55	0.85	0.85
42.51	62.46	42.82	3.40	145.73	2.56	0.86	0.86
42.52	61.49	42.07	3.50	147.05	2.57	0.87	0.87
42.53	60.55	41.34	3.59	148.30	2.58	0.88	0.88
42.54	59.68	40.65	3.68	149.43	2.59	0.89	0.89
42.55	58.92	40.06	3.75	150.39	2.60	0.90	0.90
42.56	58.24	39.53	3.83	151.23	2.61	0.91	0.91
42.57	57.54	38.98	3.90	152.10	2.62	0.92	0.92
42.58	56.73	38.35	3.99	153.09	2.63	0.93	0.93
42.59	55.80	37.64	4.10	154.18	2.64	0.94	0.94
42.60	54.81	36.88	4.21	155.29	2.65	0.96	0.96
42.61	53.80	36.11	4.33	156.36	2.66	0.97	0.97
42.62	52.84	35.37	4.45	157.33	2.67	0.98	0.98
42.63	51.96	34.70	4.56	158.17	2.69	1.00	1.00
42.64	51.22	34.13	4.65	158.75	2.69	1.00	1.00
42.65	50.56	33.64	4.73	158.95	2.70	0.84	0.84
42.66	49.90	33.14	4.79	158.80	2.71	0.84	0.84
42.67	49.15	32.58	4.86	158.45	2.71	0.84	0.84
42.68	48.32	31.96	4.94	158.05	2.72	0.84	0.84
42.69	47.44	31.31	5.03	157.60	2.73	0.84	0.84
42.70	46.56	30.67	5.12	157.13	2.74	0.84	0.84
42.71	45.74	30.06	5.21	156.67	2.75	0.84	0.84
42.72	45.01	29.51	5.29	156.23	2.75	0.84	0.84

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
42.73	44.50	29.14	5.34	155.73	2.76	0.83	0.83
42.74	44.22	28.94	5.36	155.05	2.76	0.83	0.83
42.75	44.12	28.87	5.34	154.10	2.76	0.83	0.83
42.76	44.05	28.82	5.31	152.96	2.75	0.83	0.83
42.77	43.97	28.77	5.27	151.71	2.75	0.83	0.83
42.78	43.89	28.72	5.24	150.42	2.75	0.83	0.83
42.79	43.81	28.67	5.20	149.16	2.75	0.83	0.83
42.80	43.74	28.62	5.17	147.99	2.74	0.82	0.82
42.81	43.70	28.59	5.14	146.98	2.74	0.82	0.82
42.82	43.91	28.75	5.08	146.19	2.73	0.82	0.82
42.83	44.43	29.14	4.99	145.52	2.73	0.82	0.82
42.84	45.28	29.76	4.87	144.82	2.72	0.82	0.82
42.85	46.24	30.47	4.72	143.96	2.70	0.82	0.82
42.86	47.26	31.24	4.58	142.99	2.69	0.97	0.97
42.87	48.30	32.01	4.43	141.92	2.67	0.96	0.96
42.88	49.30	32.76	4.30	140.84	2.66	0.94	0.94
42.89	50.21	33.43	4.18	139.80	2.65	0.93	0.93
42.90	50.99	34.02	4.08	138.96	2.64	0.92	0.92
42.91	51.74	34.57	4.00	138.37	2.63	0.91	0.91
42.92	52.55	35.17	3.92	137.97	2.62	0.90	0.90
42.93	53.51	35.89	3.83	137.61	2.61	0.89	0.89
42.94	54.58	36.68	3.74	137.18	2.60	0.88	0.88
42.95	55.69	37.51	3.64	136.69	2.59	0.87	0.87
42.96	56.80	38.34	3.55	136.18	2.58	0.86	0.86
42.97	57.85	39.12	3.47	135.66	2.57	0.85	0.85
42.98	58.78	39.81	3.40	135.19	2.56	0.84	0.84
42.99	59.45	40.31	3.35	134.95	2.55	0.84	0.84
43.00	59.89	40.63	3.32	135.01	2.55	0.83	0.83
43.01	60.17	40.83	3.32	135.37	2.55	0.83	0.83
43.02	60.46	41.02	3.31	135.84	2.55	0.83	0.83
43.03	60.77	41.24	3.31	136.36	2.55	0.83	0.83
43.04	61.09	41.46	3.30	136.89	2.54	0.84	0.84
43.05	61.41	41.68	3.30	137.41	2.54	0.84	0.84
43.06	61.70	41.88	3.29	137.90	2.54	0.84	0.84
43.07	61.94	42.04	3.29	138.34	2.54	0.84	0.84
43.08	62.06	42.12	3.30	138.96	2.54	0.84	0.84
43.09	62.08	42.10	3.32	139.89	2.55	0.84	0.84
43.10	62.02	42.02	3.36	141.17	2.55	0.85	0.85
43.11	61.94	41.94	3.40	142.62	2.56	0.85	0.85
43.12	61.87	41.84	3.45	144.15	2.56	0.86	0.86
43.13	61.79	41.75	3.49	145.70	2.57	0.87	0.87
43.14	61.71	41.66	3.53	147.18	2.57	0.88	0.88
43.15	61.64	41.58	3.57	148.51	2.58	0.88	0.88
43.16	61.58	41.51	3.61	149.65	2.58	0.89	0.89
43.17	61.53	41.44	3.64	150.72	2.59	0.89	0.89
43.18	61.47	41.37	3.67	151.88	2.59	0.90	0.90
43.19	61.40	41.29	3.71	153.24	2.60	0.90	0.90
43.20	61.32	41.20	3.76	154.74	2.60	0.91	0.91

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
43.21	61.24	41.11	3.80	156.30	2.61	0.92	0.92
43.22	61.17	41.02	3.85	157.84	2.61	0.92	0.92
43.23	61.09	40.93	3.89	159.28	2.62	0.93	0.93
43.24	61.03	40.85	3.93	160.55	2.62	0.94	0.94
43.25	60.99	40.80	3.96	161.42	2.62	0.94	0.94
43.26	60.99	40.79	3.97	161.91	2.62	0.94	0.94
43.27	61.03	40.80	3.97	162.12	2.62	0.94	0.94
43.28	61.08	40.83	3.98	162.30	2.63	0.94	0.94
43.29	61.13	40.85	3.98	162.49	2.63	0.94	0.94
43.30	61.18	40.88	3.98	162.69	2.63	0.95	0.95
43.31	61.23	40.91	3.98	162.89	2.63	0.95	0.95
43.32	61.28	40.93	3.98	163.07	2.63	0.95	0.95
43.33	61.33	40.96	3.98	163.19	2.63	0.95	0.95
43.34	61.46	41.05	3.97	162.99	2.62	0.94	0.94
43.35	61.70	41.22	3.94	162.43	2.62	0.94	0.94
43.36	62.04	41.48	3.89	161.49	2.62	0.93	0.93
43.37	62.44	41.77	3.84	160.42	2.61	0.93	0.93
43.38	62.85	42.09	3.78	159.27	2.60	0.92	0.92
43.39	63.28	42.41	3.73	158.09	2.60	0.91	0.91
43.40	63.68	42.72	3.67	156.94	2.59	0.91	0.91
43.41	64.05	43.00	3.63	155.89	2.59	0.90	0.90
43.42	64.40	43.27	3.58	154.97	2.58	0.89	0.89
43.43	64.86	43.61	3.53	154.07	2.57	0.89	0.89
43.44	65.46	44.06	3.47	153.06	2.57	0.88	0.88
43.45	66.23	44.64	3.40	151.84	2.56	0.87	0.87
43.46	67.07	45.28	3.32	150.47	2.55	0.86	0.86
43.47	67.96	45.95	3.24	149.00	2.54	0.85	0.85
43.48	68.83	46.62	3.16	147.52	2.53	0.83	0.83
43.49	69.66	47.26	3.09	146.10	2.52	0.82	0.82
43.50	70.39	47.81	3.03	144.83	2.51	0.81	0.81
43.51	70.99	48.27	2.98	143.78	2.50	0.82	0.82
43.52	71.52	48.67	2.93	142.85	2.49	0.82	0.82
43.53	72.06	49.09	2.89	141.91	2.49	0.82	0.82
43.54	72.67	49.56	2.84	140.83	2.48	0.81	0.81
43.55	73.34	50.07	2.79	139.65	2.47	0.81	0.81
43.56	74.03	50.60	2.74	138.43	2.46	0.81	0.81
43.57	74.70	51.12	2.68	137.22	2.45	0.81	0.81
43.58	75.31	51.60	2.64	136.11	2.45	0.81	0.81
43.59	75.83	51.99	2.60	135.17	2.44	0.81	0.81
43.60	76.13	52.22	2.58	134.56	2.44	0.81	0.81
43.61	76.25	52.31	2.57	134.22	2.43	0.80	0.80
43.62	76.24	52.30	2.56	134.04	2.43	0.80	0.80
43.63	76.24	52.30	2.56	133.83	2.43	0.80	0.80
43.64	76.24	52.29	2.56	133.61	2.43	0.80	0.80
43.65	76.24	52.28	2.55	133.39	2.43	0.80	0.80
43.66	76.24	52.27	2.55	133.18	2.43	0.80	0.80
43.67	76.24	52.27	2.54	132.99	2.43	0.80	0.80
43.68	76.16	52.20	2.55	132.99	2.43	0.80	0.80

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)'/σ'_v}	S _{u(peak)'/σ'_v}
43.69	75.90	51.98	2.57	133.40	2.43	0.80	0.80
43.70	75.41	51.59	2.60	134.27	2.44	0.80	0.80
43.71	74.76	51.06	2.65	135.47	2.45	0.81	0.81
43.72	74.04	50.48	2.71	136.79	2.46	0.81	0.81
43.73	73.29	49.88	2.77	138.16	2.47	0.81	0.81
43.74	72.55	49.28	2.83	139.50	2.48	0.81	0.81
43.75	71.85	48.73	2.89	140.75	2.49	0.81	0.81
43.76	71.23	48.23	2.94	141.84	2.49	0.82	0.82
43.77	70.59	47.72	3.00	143.01	2.50	0.81	0.81
43.78	69.81	47.10	3.07	144.49	2.51	0.82	0.82
43.79	68.79	46.29	3.16	146.44	2.53	0.83	0.83
43.80	67.58	45.35	3.28	148.70	2.54	0.85	0.85
43.81	66.27	44.33	3.41	151.08	2.56	0.87	0.87
43.82	64.93	43.30	3.54	153.44	2.58	0.89	0.89
43.83	63.63	42.29	3.68	155.65	2.59	0.90	0.90
43.84	62.43	41.37	3.81	157.60	2.61	0.92	0.92
43.85	61.40	40.58	3.92	159.24	2.62	0.93	0.93
43.86	60.52	39.90	4.03	160.74	2.63	0.95	0.95
43.87	59.66	39.24	4.14	162.33	2.64	0.96	0.96
43.88	58.71	38.51	4.26	164.16	2.66	0.98	0.98
43.89	57.63	37.69	4.41	166.16	2.67	0.99	0.99
43.90	56.48	36.82	4.57	168.17	2.69	1.01	1.01
43.91	55.33	35.95	4.73	170.09	2.70	0.85	0.85
43.92	54.22	35.12	4.89	171.83	2.72	0.85	0.85
43.93	53.23	34.37	5.04	173.30	2.73	0.86	0.86
43.94	52.45	33.79	5.17	174.52	2.74	0.86	0.86
43.95	51.89	33.36	5.27	175.69	2.75	0.86	0.86
43.96	51.47	33.04	5.36	176.99	2.76	0.86	0.86
43.97	51.05	32.71	5.46	178.52	2.77	0.86	0.86
43.98	50.59	32.35	5.57	180.17	2.78	0.86	0.86
43.99	50.11	31.98	5.69	181.83	2.79	0.87	0.87
44.00	49.64	31.62	5.80	183.44	2.80	0.87	0.87
44.01	49.19	31.27	5.91	184.90	2.80	0.87	0.87
44.02	48.80	30.97	6.01	186.14	2.81	0.87	0.87
44.03	48.58	30.79	6.08	187.20	2.82	0.87	0.87
44.04	48.53	30.74	6.12	188.21	2.82	0.87	0.87
44.05	48.64	30.80	6.15	189.32	2.82	0.88	0.88
44.06	48.79	30.88	6.17	190.62	2.83	0.88	0.88
44.07	48.94	30.97	6.20	192.01	2.83	0.88	0.88
44.08	49.11	31.06	6.23	193.44	2.83	0.88	0.88
44.09	49.26	31.15	6.25	194.83	2.83	0.88	0.88
44.10	49.41	31.23	6.28	196.12	2.83	0.88	0.88
44.11	49.55	31.32	6.30	197.19	2.83	0.88	0.88
44.12	49.79	31.47	6.29	197.93	2.83	0.88	0.88
44.13	50.17	31.72	6.25	198.43	2.83	0.89	0.89
44.14	50.70	32.09	6.20	198.85	2.83	0.89	0.89
44.15	51.30	32.50	6.13	199.31	2.82	0.89	0.89
44.16	51.93	32.94	6.07	199.79	2.82	0.89	0.89

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
44.17	52.57	33.38	6.00	200.25	2.81	0.89	0.89
44.18	53.18	33.80	5.94	200.68	2.81	0.89	0.89
44.19	53.73	34.18	5.88	201.07	2.80	0.89	0.89
44.20	54.29	34.58	5.82	201.31	2.80	0.89	0.89
44.21	55.04	35.10	5.74	201.35	2.79	0.89	0.89
44.22	56.06	35.82	5.62	201.16	2.78	0.89	0.89
44.23	57.35	36.74	5.47	200.80	2.77	0.89	0.89
44.24	58.77	37.75	5.31	200.30	2.75	0.89	0.89
44.25	60.24	38.81	5.14	199.66	2.74	0.89	0.89
44.26	61.70	39.85	4.99	198.92	2.73	0.89	0.89
44.27	63.07	40.84	4.85	198.13	2.71	0.88	0.88
44.28	64.27	41.70	4.73	197.36	2.70	0.88	0.88
44.29	65.42	42.53	4.62	196.57	2.69	1.06	1.06
44.30	66.69	43.45	4.50	195.63	2.68	1.04	1.04
44.31	68.24	44.58	4.36	194.41	2.67	1.03	1.03
44.32	70.05	45.90	4.20	192.86	2.65	1.01	1.01
44.33	72.01	47.33	4.04	191.04	2.63	0.99	0.99
44.34	74.00	48.80	3.87	189.02	2.61	0.97	0.97
44.35	75.94	50.23	3.72	186.92	2.60	0.95	0.95
44.36	77.73	51.55	3.59	184.87	2.58	0.93	0.93
44.37	79.25	52.69	3.47	183.06	2.57	0.92	0.92
44.38	80.58	53.67	3.38	181.54	2.55	0.90	0.90
44.39	81.91	54.66	3.30	180.14	2.54	0.89	0.89
44.40	83.41	55.77	3.20	178.61	2.53	0.88	0.88
44.41	85.09	57.03	3.10	176.84	2.52	0.86	0.86
44.42	86.88	58.37	3.00	174.89	2.50	0.85	0.85
44.43	88.68	59.73	2.89	172.88	2.49	0.86	0.86
44.44	90.39	61.02	2.80	170.90	2.47	0.85	0.85
44.45	91.93	62.19	2.72	169.09	2.46	0.85	0.85
44.46	93.21	63.16	2.65	167.59	2.45	0.85	0.85
44.47	94.32	64.00	2.60	166.31	2.44	0.85	0.85
44.48	95.42	64.83	2.55	165.10	2.43	0.85	0.85
44.49	96.66	65.77	2.49	163.74	2.42	0.84	0.84
44.50	98.03	66.82	2.43	162.22	2.41	0.84	0.84
44.51	99.45	67.91	2.37	160.64	2.40	0.84	0.84
44.52	100.86	68.99	2.31	159.07	2.39	0.84	0.84
44.53	102.17	70.01	2.25	157.60	2.38	0.84	0.84
44.54	103.33	70.90	2.20	156.30	2.37	0.84	0.84
44.55	104.13	71.52	2.17	155.32	2.36	0.83	0.83
44.56	104.65	71.92	2.15	154.54	2.35	0.83	0.83
44.57	104.97	72.17	2.13	153.85	2.35	0.83	0.83
44.58	105.32	72.44	2.11	153.07	2.35	0.83	0.83
44.59	105.69	72.74	2.09	152.23	2.34	0.83	0.83
44.60	106.08	73.04	2.07	151.38	2.34	0.83	0.83
44.61	106.45	73.33	2.05	150.55	2.33	0.83	0.83
44.62	106.79	73.61	2.04	149.79	2.33	0.83	0.83
44.63	107.10	73.85	2.02	149.15	2.32	0.83	0.83
44.64	107.47	74.13	2.01	148.66	2.32	0.83	0.83

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
44.65	107.94	74.49	1.99	148.23	2.32	0.82	0.82
44.66	108.56	74.96	1.97	147.81	2.31	0.82	0.82
44.67	109.26	75.49	1.95	147.33	2.31	0.82	0.82
44.68	109.99	76.05	1.93	146.83	2.30	0.82	0.82
44.69	110.73	76.62	1.91	146.34	2.30	0.82	0.82
44.70	111.43	77.16	1.89	145.87	2.29	0.82	0.82
44.71	112.06	77.64	1.87	145.46	2.29	0.82	0.82
44.72	112.60	78.05	1.86	145.10	2.28	0.82	0.82
44.73	113.11	78.44	1.85	144.77	2.28	0.82	0.82
44.74	113.66	78.87	1.83	144.41	2.27	0.82	0.82
44.75	114.31	79.36	1.81	143.99	2.27	0.82	0.82
44.76	115.02	79.91	1.80	143.55	2.26	0.82	0.82
44.77	115.75	80.48	1.78	143.09	2.26	0.82	0.82
44.78	116.48	81.05	1.76	142.65	2.25	0.82	0.82
44.79	117.15	81.58	1.74	142.25	2.25	0.82	0.82
44.80	117.75	82.04	1.73	141.90	2.24	0.82	0.82
44.81	118.04	82.26	1.72	141.67	2.24	0.82	0.82
44.82	118.02	82.23	1.72	141.54	2.24	0.82	0.82
44.83	117.72	81.99	1.73	141.48	2.24	0.82	0.82
44.84	117.36	81.69	1.73	141.42	2.24	0.82	0.82
44.85	116.96	81.37	1.74	141.36	2.24	0.82	0.82
44.86	116.56	81.05	1.74	141.30	2.25	0.81	0.81
44.87	116.18	80.74	1.75	141.24	2.25	0.81	0.81
44.88	115.82	80.45	1.76	141.19	2.25	0.81	0.81
44.89	115.52	80.20	1.76	141.16	2.25	0.81	0.81
44.90	115.24	79.97	1.77	141.17	2.25	0.81	0.81
44.91	114.95	79.73	1.77	141.24	2.26	0.81	0.81
44.92	114.61	79.45	1.78	141.35	2.26	0.82	0.82
44.93	114.24	79.14	1.79	141.48	2.26	0.82	0.82
44.94	113.84	78.81	1.80	141.62	2.26	0.82	0.82
44.95	113.44	78.48	1.81	141.77	2.27	0.82	0.82
44.96	113.06	78.17	1.82	141.91	2.27	0.82	0.82
44.97	112.72	77.89	1.82	142.03	2.27	0.82	0.82
44.98	112.44	77.65	1.83	142.18	2.27	0.82	0.82
44.99	112.20	77.44	1.84	142.41	2.28	0.82	0.82
45.00	111.95	77.22	1.85	142.76	2.28	0.82	0.82
45.01	111.67	76.97	1.86	143.19	2.28	0.82	0.82
45.02	111.36	76.70	1.87	143.67	2.29	0.82	0.82
45.03	111.04	76.42	1.89	144.18	2.29	0.82	0.82
45.04	110.73	76.15	1.90	144.68	2.29	0.82	0.82
45.05	110.43	75.89	1.91	145.14	2.30	0.82	0.82
45.06	110.17	75.66	1.92	145.55	2.30	0.82	0.82
45.07	109.95	75.46	1.93	145.93	2.30	0.82	0.82
45.08	109.72	75.26	1.94	146.34	2.31	0.82	0.82
45.09	109.47	75.03	1.96	146.82	2.31	0.82	0.82
45.10	109.18	74.77	1.97	147.39	2.31	0.82	0.82
45.11	108.87	74.50	1.99	148.00	2.32	0.82	0.82
45.12	108.55	74.22	2.00	148.62	2.32	0.83	0.83

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
45.13	108.24	73.95	2.02	149.23	2.32	0.83	0.83
45.14	107.95	73.70	2.03	149.78	2.33	0.83	0.83
45.15	107.70	73.48	2.05	150.27	2.33	0.83	0.83
45.16	107.43	73.24	2.06	150.74	2.33	0.83	0.83
45.17	107.11	72.97	2.07	151.26	2.34	0.83	0.83
45.18	106.71	72.63	2.09	151.88	2.34	0.83	0.83
45.19	106.25	72.25	2.11	152.59	2.35	0.83	0.83
45.20	105.78	71.85	2.13	153.34	2.35	0.83	0.83
45.21	105.30	71.46	2.16	154.09	2.36	0.83	0.83
45.22	104.84	71.08	2.18	154.81	2.36	0.83	0.83
45.23	104.44	70.74	2.20	155.45	2.36	0.83	0.83
45.24	104.09	70.45	2.21	156.01	2.37	0.83	0.83
45.25	103.76	70.17	2.23	156.58	2.37	0.84	0.84
45.26	103.40	69.87	2.25	157.22	2.38	0.84	0.84
45.27	102.97	69.51	2.27	157.98	2.38	0.84	0.84
45.28	102.51	69.13	2.30	158.81	2.39	0.84	0.84
45.29	102.03	68.74	2.32	159.67	2.39	0.84	0.84
45.30	101.56	68.35	2.35	160.52	2.40	0.84	0.84
45.31	101.12	67.98	2.37	161.31	2.40	0.84	0.84
45.32	100.73	67.67	2.39	162.00	2.40	0.84	0.84
45.33	100.43	67.41	2.41	162.49	2.41	0.84	0.84
45.34	100.17	67.20	2.42	162.83	2.41	0.84	0.84
45.35	99.91	66.99	2.43	163.09	2.41	0.84	0.84
45.36	99.62	66.75	2.45	163.39	2.41	0.84	0.84
45.37	99.31	66.50	2.46	163.71	2.42	0.84	0.84
45.38	98.99	66.24	2.48	164.03	2.42	0.85	0.85
45.39	98.68	65.99	2.49	164.34	2.42	0.85	0.85
45.40	98.39	65.76	2.50	164.63	2.42	0.85	0.85
45.41	98.18	65.58	2.51	164.80	2.43	0.85	0.85
45.42	98.10	65.51	2.51	164.70	2.43	0.85	0.85
45.43	98.15	65.55	2.51	164.31	2.42	0.85	0.85
45.44	98.29	65.65	2.49	163.68	2.42	0.84	0.84
45.45	98.44	65.77	2.48	162.98	2.42	0.84	0.84
45.46	98.60	65.89	2.46	162.24	2.42	0.84	0.84
45.47	98.76	66.01	2.45	161.50	2.41	0.84	0.84
45.48	98.91	66.13	2.43	160.79	2.41	0.84	0.84
45.49	99.04	66.23	2.42	160.16	2.41	0.84	0.84
45.50	99.23	66.38	2.40	159.54	2.41	0.84	0.84
45.51	99.56	66.63	2.38	158.82	2.40	0.84	0.84
45.52	100.07	67.01	2.36	157.89	2.40	0.84	0.84
45.53	100.71	67.50	2.32	156.77	2.39	0.84	0.84
45.54	101.40	68.04	2.29	155.55	2.38	0.83	0.83
45.55	102.12	68.60	2.25	154.28	2.38	0.83	0.83
45.56	102.83	69.14	2.21	153.04	2.37	0.83	0.83
45.57	103.49	69.66	2.18	151.88	2.36	0.83	0.83
45.58	104.06	70.10	2.15	150.87	2.35	0.83	0.83
45.59	104.60	70.52	2.13	150.02	2.35	0.83	0.83
45.60	105.19	70.97	2.10	149.23	2.34	0.83	0.83

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
45.61	105.89	71.51	2.07	148.37	2.34	0.82	0.82
45.62	106.70	72.13	2.04	147.40	2.33	0.82	0.82
45.63	107.56	72.80	2.01	146.36	2.32	0.82	0.82
45.64	108.44	73.49	1.98	145.31	2.31	0.82	0.82
45.65	109.29	74.15	1.95	144.31	2.31	0.82	0.82
45.66	110.07	74.75	1.92	143.41	2.30	0.82	0.82
45.67	110.72	75.26	1.90	142.67	2.29	0.82	0.82
45.68	111.25	75.67	1.88	142.11	2.29	0.82	0.82
45.69	111.75	76.05	1.86	141.66	2.28	0.82	0.82
45.70	112.29	76.47	1.85	141.20	2.28	0.81	0.81
45.71	112.90	76.93	1.83	140.70	2.27	0.81	0.81
45.72	113.53	77.42	1.81	140.17	2.27	0.81	0.81
45.73	114.17	77.92	1.79	139.66	2.26	0.81	0.81
45.74	114.77	78.38	1.78	139.18	2.26	0.81	0.81
45.75	115.31	78.80	1.76	138.75	2.25	0.81	0.81
45.76	115.73	79.12	1.75	138.43	2.25	0.81	0.81
45.77	116.04	79.36	1.74	138.20	2.25	0.81	0.81
45.78	116.31	79.55	1.74	138.03	2.24	0.81	0.81
45.79	116.59	79.76	1.73	137.85	2.24	0.81	0.81
45.80	116.90	79.99	1.72	137.65	2.24	0.81	0.81
45.81	117.22	80.23	1.71	137.46	2.24	0.81	0.81
45.82	117.53	80.47	1.71	137.26	2.23	0.81	0.81
45.83	117.83	80.69	1.70	137.08	2.23	0.81	0.81
45.84	118.08	80.88	1.69	136.93	2.23	0.81	0.81
45.85	118.36	81.09	1.69	136.78	2.23	0.81	0.81
45.86	118.70	81.34	1.68	136.62	2.22	0.81	0.81
45.87	119.15	81.68	1.67	136.44	2.22	0.81	0.81
45.88	119.67	82.08	1.66	136.23	2.22	0.81	0.81
45.89	120.22	82.52	1.65	136.03	2.21	0.81	0.81
45.90	120.78	82.95	1.64	135.82	2.21	0.81	0.81
45.91	121.32	83.36	1.63	135.62	2.21	0.81	0.81
45.92	121.81	83.74	1.62	135.45	2.20	0.81	0.81
45.93	122.26	84.08	1.61	135.31	2.20	0.81	0.81
45.94	122.74	84.45	1.60	135.21	2.19	0.81	0.81
45.95	123.34	84.90	1.59	135.14	2.19	0.81	0.81
45.96	124.09	85.48	1.58	135.08	2.19	0.81	0.81
45.97	124.92	86.12	1.57	135.03	2.18	0.81	0.81
45.98	125.80	86.79	1.56	134.99	2.17	0.81	0.81
45.99	126.67	87.47	1.54	134.96	2.17	0.81	0.81
46.00	127.50	88.11	1.53	134.95	2.16	0.81	0.81
46.01	128.24	88.68	1.52	134.94	2.16	0.81	0.81
46.02	128.87	89.16	1.51	134.93	2.15	0.81	0.81
46.03	129.48	89.64	1.50	134.90	2.15	0.81	0.81
46.04	130.15	90.16	1.50	134.86	2.15	0.81	0.81
46.05	130.93	90.77	1.49	134.82	2.14	0.81	0.81
46.06	131.79	91.45	1.47	134.80	2.13	0.81	0.81
46.07	132.67	92.14	1.46	134.79	2.13	0.81	0.81
46.08	133.53	92.83	1.45	134.79	2.12	0.81	0.81

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
46.09	134.33	93.46	1.44	134.81	2.12	0.81	0.81
46.10	135.03	94.01	1.43	134.85	2.11	0.81	0.81
46.11	135.61	94.43	1.43	135.19	2.11	0.81	0.81
46.12	136.15	94.78	1.43	135.90	2.11	0.81	0.81
46.13	136.73	95.12	1.44	137.04	2.11	0.81	0.81
46.14	137.40	95.50	1.45	138.35	2.12	0.81	0.81
46.15	138.11	95.92	1.46	139.76	2.12	0.81	0.81
46.16	138.83	96.34	1.47	141.22	2.13	0.81	0.81
46.17	139.52	96.75	1.47	142.63	2.13	0.82	0.82
46.18	140.15	97.11	1.48	143.92	2.14	0.82	0.82
46.19	140.68	97.42	1.49	145.03	2.14	0.82	0.82
46.20	141.13	97.66	1.50	146.07	2.15	0.82	0.82
46.21	141.56	97.89	1.50	147.18	2.15	0.82	0.82
46.22	142.04	98.14	1.51	148.49	2.15	0.82	0.82
46.23	142.57	98.42	1.52	149.96	2.16	0.83	0.83
46.24	143.13	98.71	1.54	151.53	2.17	0.83	0.83
46.25	143.69	99.01	1.55	153.10	2.17	0.83	0.83
46.26	144.21	99.29	1.56	154.61	2.18	0.83	0.83
46.27	144.68	99.53	1.57	155.96	2.18	0.83	0.83
46.28	144.99	99.70	1.57	156.70	2.18	0.84	0.84
46.29	145.11	99.78	1.57	156.70	2.18	0.84	0.84
46.30	145.08	99.79	1.56	155.97	2.18	0.83	0.83
46.31	145.01	99.79	1.55	154.98	2.17	0.83	0.83
46.32	144.93	99.79	1.54	153.91	2.17	0.83	0.83
46.33	144.85	99.79	1.53	152.82	2.16	0.83	0.83
46.34	144.77	99.80	1.52	151.77	2.16	0.83	0.83
46.35	144.70	99.80	1.51	150.80	2.15	0.83	0.83
46.36	144.63	99.80	1.50	149.98	2.15	0.83	0.83
46.37	144.40	99.65	1.50	149.41	2.15	0.83	0.83
46.38	143.98	99.33	1.50	149.01	2.15	0.83	0.83
46.39	143.33	98.82	1.50	148.71	2.15	0.83	0.83
46.40	142.59	98.24	1.51	148.37	2.15	0.82	0.82
46.41	141.80	97.63	1.52	148.02	2.16	0.82	0.82
46.42	141.00	97.00	1.52	147.67	2.16	0.82	0.82
46.43	140.23	96.40	1.53	147.33	2.16	0.82	0.82
46.44	139.53	95.86	1.53	147.02	2.16	0.82	0.82
46.45	138.90	95.36	1.54	146.79	2.17	0.82	0.82
46.46	138.19	94.79	1.55	146.69	2.17	0.82	0.82
46.47	137.31	94.08	1.56	146.70	2.18	0.82	0.82
46.48	136.22	93.20	1.57	146.79	2.18	0.82	0.82
46.49	135.00	92.23	1.59	146.91	2.19	0.82	0.82
46.50	133.72	91.21	1.61	147.07	2.20	0.82	0.82
46.51	132.45	90.20	1.63	147.25	2.21	0.82	0.82
46.52	131.25	89.25	1.65	147.44	2.21	0.82	0.82
46.53	130.19	88.40	1.67	147.62	2.22	0.82	0.82
46.54	129.18	87.59	1.69	147.72	2.23	0.82	0.82
46.55	128.04	86.70	1.70	147.75	2.23	0.82	0.82
46.56	126.62	85.61	1.73	147.70	2.24	0.82	0.82

:: Strength loss calculation (Robertson (2009)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
46.57	124.94	84.33	1.75	147.65	2.25	0.82	0.82
46.58	123.12	82.94	1.78	147.62	2.26	0.82	0.82
46.59	121.23	81.50	1.81	147.62	2.27	0.82	0.82
46.60	119.39	80.11	1.84	147.64	2.28	0.82	0.82
46.61	117.69	78.82	1.87	147.67	2.29	0.82	0.82
46.62	116.21	77.70	1.90	147.73	2.29	0.82	0.82
46.63	114.90	76.70	1.93	148.04	2.30	0.82	0.82
46.64	113.58	75.67	1.96	148.66	2.31	0.83	0.83
46.65	112.06	74.50	2.01	149.65	2.32	0.83	0.83
46.66	110.34	73.17	2.06	150.79	2.33	0.83	0.83
46.67	108.49	71.75	2.12	152.02	2.35	0.83	0.83
46.68	106.63	70.33	2.18	153.29	2.36	0.83	0.83
46.69	104.84	68.97	2.24	154.51	2.37	0.83	0.83
46.70	103.22	67.74	2.30	155.62	2.39	0.83	0.83
46.71	101.83	66.69	2.35	156.64	2.40	0.84	0.84
46.72	100.57	65.73	2.40	157.79	2.41	0.84	0.84
46.73	99.26	64.72	2.46	159.23	2.42	0.84	0.84
46.74	97.74	63.56	2.53	161.00	2.43	0.84	0.84
46.75	96.05	62.28	2.62	162.96	2.44	0.84	0.84
46.76	94.28	60.94	2.71	164.98	2.46	0.85	0.85
46.77	92.52	59.62	2.80	166.95	2.47	0.85	0.85
46.78	90.85	58.38	2.89	168.76	2.49	0.85	0.85
46.79	89.38	57.28	2.97	170.34	2.50	0.85	0.85
46.80	88.14	56.36	3.05	171.68	2.51	0.85	0.85
46.81	87.00	55.51	3.12	172.98	2.52	0.86	0.86
46.82	85.79	54.61	3.19	174.40	2.53	0.87	0.87
46.83	84.39	53.58	3.29	176.01	2.54	0.89	0.89
46.84	82.87	52.46	3.39	177.71	2.56	0.90	0.90
46.85	81.31	51.32	3.50	179.40	2.57	0.91	0.91
46.86	79.78	50.21	3.60	180.98	2.58	0.93	0.93
46.87	78.37	49.18	3.71	182.38	2.59	0.94	0.94
46.88	77.15	48.30	3.80	183.51	2.61	0.95	0.95
46.89	76.07	47.53	3.88	184.22	2.61	0.96	0.96
46.90	75.01	46.77	3.95	184.58	2.62	0.97	0.97
46.91	73.80	45.92	4.02	184.71	2.63	0.98	0.98
46.92	72.43	44.95	4.11	184.82	2.64	0.99	0.99
46.93	70.97	43.93	4.21	184.90	2.65	1.00	1.00
46.94	69.49	42.90	4.31	184.93	2.66	1.01	1.01
46.95	68.07	41.91	4.41	184.91	2.67	1.02	1.02
46.96	66.78	41.01	4.51	184.85	2.68	1.03	1.03
46.97	65.71	40.27	4.59	184.69	2.69	1.04	1.04
46.98	64.81	39.64	4.65	184.31	2.69	1.04	1.04
46.99	63.93	39.04	4.70	183.67	2.70	1.05	1.05
47.00	62.96	38.38	4.76	182.81	2.71	0.87	0.87
47.01	61.88	37.64	4.83	181.84	2.71	0.87	0.87
47.02	60.75	36.87	4.90	180.82	2.72	0.87	0.87
47.03	59.62	36.11	4.98	179.78	2.73	0.86	0.86
47.04	58.56	35.40	5.05	178.79	2.73	0.86	0.86

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
47.05	57.63	34.76	5.12	177.90	2.74	0.86	0.86
47.06	56.97	34.31	5.17	177.30	2.74	0.86	0.86
47.07	56.57	34.04	5.20	177.00	2.75	0.86	0.86
47.08	56.36	33.89	5.22	176.95	2.75	0.86	0.86
47.09	56.16	33.74	5.24	176.94	2.75	0.86	0.86
47.10	55.94	33.59	5.27	176.93	2.75	0.86	0.86
47.11	55.72	33.43	5.29	176.92	2.75	0.86	0.86
47.12	55.50	33.27	5.32	176.91	2.76	0.86	0.86
47.13	55.30	33.12	5.34	176.90	2.76	0.86	0.86
47.14	55.14	33.01	5.36	176.90	2.76	0.86	0.86
47.15	55.12	32.99	5.37	177.04	2.76	0.86	0.86
47.16	55.25	33.06	5.36	177.36	2.76	0.86	0.86
47.17	55.51	33.22	5.35	177.86	2.76	0.86	0.86
47.18	55.81	33.41	5.34	178.43	2.76	0.86	0.86
47.19	56.13	33.61	5.33	179.03	2.76	0.86	0.86
47.20	56.45	33.81	5.31	179.65	2.76	0.86	0.86
47.21	56.75	34.00	5.30	180.23	2.75	0.86	0.86
47.22	57.03	34.17	5.29	180.76	2.75	0.87	0.87
47.23	57.29	34.34	5.28	181.13	2.75	0.87	0.87
47.24	57.59	34.53	5.25	181.27	2.75	0.87	0.87
47.25	57.97	34.78	5.21	181.18	2.75	0.87	0.87
47.26	58.44	35.10	5.16	180.98	2.74	0.87	0.87
47.27	58.97	35.45	5.10	180.74	2.74	0.87	0.87
47.28	59.51	35.82	5.04	180.47	2.73	0.87	0.87
47.29	60.06	36.19	4.98	180.19	2.73	0.86	0.86
47.30	60.57	36.53	4.93	179.92	2.72	0.86	0.86
47.31	61.02	36.83	4.88	179.67	2.72	0.86	0.86
47.32	61.41	37.10	4.83	179.32	2.71	0.86	0.86
47.33	61.78	37.35	4.79	178.78	2.71	0.86	0.86
47.34	62.20	37.64	4.73	177.98	2.70	0.86	0.86
47.35	62.68	37.97	4.66	177.02	2.70	1.03	1.03
47.36	63.20	38.34	4.59	175.95	2.69	1.02	1.02
47.37	63.73	38.71	4.52	174.84	2.68	1.02	1.02
47.38	64.25	39.08	4.45	173.73	2.67	1.01	1.01
47.39	64.73	39.42	4.38	172.68	2.67	1.00	1.00
47.40	65.15	39.71	4.33	171.75	2.66	0.99	0.99
47.41	65.53	39.98	4.27	170.86	2.66	0.99	0.99
47.42	65.93	40.26	4.22	169.87	2.65	0.98	0.98
47.43	66.40	40.60	4.15	168.66	2.64	0.97	0.97
47.44	66.93	40.98	4.08	167.28	2.64	0.96	0.96
47.45	67.50	41.38	4.01	165.78	2.63	0.95	0.95
47.46	68.07	41.80	3.93	164.25	2.62	0.94	0.94
47.47	68.61	42.19	3.86	162.75	2.61	0.93	0.93
47.48	69.10	42.55	3.79	161.37	2.60	0.92	0.92
47.49	69.48	42.82	3.74	160.19	2.60	0.92	0.92
47.50	69.71	43.00	3.70	159.07	2.59	0.91	0.91
47.51	69.84	43.10	3.66	157.88	2.59	0.91	0.91
47.52	69.93	43.18	3.62	156.48	2.58	0.90	0.90

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
47.53	70.03	43.27	3.58	154.93	2.58	0.89	0.89
47.54	70.14	43.37	3.53	153.31	2.57	0.89	0.89
47.55	70.24	43.47	3.49	151.69	2.57	0.88	0.88
47.56	70.34	43.56	3.45	150.16	2.56	0.87	0.87
47.57	70.43	43.64	3.41	148.81	2.56	0.86	0.86
47.58	70.45	43.68	3.38	147.68	2.55	0.86	0.86
47.59	70.41	43.66	3.36	146.66	2.55	0.86	0.86
47.60	70.29	43.59	3.34	145.61	2.55	0.85	0.85
47.61	70.15	43.51	3.32	144.39	2.55	0.85	0.85
47.62	69.99	43.42	3.29	143.08	2.54	0.84	0.84
47.63	69.83	43.33	3.27	141.73	2.54	0.84	0.84
47.64	69.67	43.25	3.25	140.42	2.54	0.83	0.83
47.65	69.53	43.16	3.23	139.21	2.53	0.83	0.83
47.66	69.44	43.11	3.21	138.19	2.53	0.83	0.83
47.67	69.56	43.21	3.18	137.47	2.53	0.82	0.82
47.68	69.92	43.46	3.15	136.96	2.52	0.82	0.82
47.69	70.52	43.88	3.11	136.54	2.52	0.81	0.81
47.70	71.19	44.35	3.07	136.05	2.51	0.81	0.81
47.71	71.90	44.85	3.02	135.53	2.51	0.80	0.80
47.72	72.62	45.36	2.98	134.99	2.50	0.81	0.81
47.73	73.31	45.84	2.93	134.48	2.49	0.81	0.81
47.74	73.93	46.28	2.90	134.00	2.49	0.80	0.80
47.75	74.39	46.61	2.87	133.57	2.48	0.80	0.80
47.76	74.68	46.81	2.84	133.10	2.48	0.80	0.80
47.77	74.82	46.92	2.82	132.52	2.48	0.80	0.80
47.78	74.93	47.00	2.80	131.83	2.47	0.80	0.80
47.79	75.04	47.09	2.78	131.06	2.47	0.80	0.80
47.80	75.16	47.19	2.76	130.25	2.47	0.80	0.80
47.81	75.28	47.28	2.74	129.46	2.46	0.80	0.80
47.82	75.39	47.37	2.72	128.71	2.46	0.80	0.80
47.83	75.49	47.45	2.70	128.05	2.46	0.80	0.80
47.84	75.42	47.41	2.69	127.54	2.46	0.79	0.79
47.85	75.14	47.22	2.69	127.13	2.46	0.79	0.79
47.86	74.62	46.85	2.71	126.77	2.46	0.79	0.79
47.87	73.99	46.41	2.72	126.36	2.46	0.79	0.79
47.88	73.31	45.94	2.74	125.92	2.46	0.79	0.79
47.89	72.62	45.45	2.76	125.47	2.47	0.79	0.79
47.90	71.94	44.98	2.78	125.03	2.47	0.79	0.79
47.91	71.32	44.55	2.80	124.63	2.47	0.79	0.79
47.92	70.80	44.18	2.81	124.34	2.48	0.79	0.79
47.93	70.40	43.89	2.84	124.45	2.48	0.79	0.79
47.94	70.07	43.63	2.86	124.99	2.48	0.79	0.79
47.95	69.74	43.37	2.90	125.92	2.49	0.79	0.79
47.96	69.37	43.08	2.95	126.96	2.50	0.79	0.79
47.97	68.98	42.77	2.99	128.05	2.50	0.79	0.79
47.98	68.59	42.46	3.04	129.14	2.51	0.79	0.79
47.99	68.21	42.17	3.09	130.18	2.52	0.80	0.80
48.00	67.88	41.90	3.13	131.11	2.52	0.81	0.81

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
48.01	67.55	41.65	3.17	131.96	2.53	0.81	0.81
48.02	67.16	41.35	3.21	132.93	2.53	0.82	0.82
48.03	66.66	40.96	3.27	134.12	2.54	0.83	0.83
48.04	66.04	40.49	3.35	135.57	2.55	0.84	0.84
48.05	65.36	39.98	3.43	137.14	2.56	0.85	0.85
48.06	64.65	39.45	3.52	138.74	2.57	0.86	0.86
48.07	63.94	38.92	3.60	140.30	2.58	0.87	0.87
48.08	63.28	38.43	3.69	141.73	2.59	0.88	0.88
48.09	62.70	38.00	3.76	142.96	2.60	0.89	0.89
48.10	62.22	37.64	3.82	143.94	2.61	0.90	0.90
48.11	61.77	37.31	3.88	144.80	2.61	0.91	0.91
48.12	61.29	36.96	3.94	145.65	2.62	0.92	0.92
48.13	60.75	36.56	4.01	146.61	2.63	0.93	0.93
48.14	60.15	36.13	4.09	147.62	2.64	0.93	0.93
48.15	59.55	35.69	4.16	148.63	2.65	0.94	0.94
48.16	58.96	35.26	4.24	149.60	2.65	0.95	0.95
48.17	58.42	34.87	4.31	150.46	2.66	0.96	0.96
48.18	57.97	34.55	4.37	151.11	2.67	0.97	0.97
48.19	57.65	34.33	4.41	151.32	2.67	0.97	0.97
48.20	57.43	34.17	4.42	151.11	2.67	0.97	0.97
48.21	57.25	34.05	4.42	150.57	2.67	0.97	0.97
48.22	57.04	33.91	4.42	149.97	2.67	0.97	0.97
48.23	56.82	33.77	4.42	149.33	2.67	0.97	0.97
48.24	56.60	33.62	4.42	148.69	2.67	0.97	0.97
48.25	56.39	33.49	4.42	148.07	2.67	0.97	0.97
48.26	56.20	33.36	4.42	147.52	2.67	0.97	0.97
48.27	56.11	33.31	4.41	146.91	2.67	0.96	0.96
48.28	56.20	33.37	4.38	146.00	2.67	0.96	0.96
48.29	56.46	33.56	4.31	144.68	2.66	0.95	0.95
48.30	56.82	33.83	4.23	142.99	2.65	0.94	0.94
48.31	57.23	34.14	4.13	141.10	2.64	0.93	0.93
48.32	57.64	34.45	4.04	139.09	2.63	0.92	0.92
48.33	58.06	34.77	3.94	137.08	2.62	0.90	0.90
48.34	58.45	35.06	3.86	135.17	2.61	0.89	0.89
48.35	58.79	35.32	3.78	133.47	2.60	0.88	0.88
48.36	59.16	35.60	3.71	132.05	2.60	0.87	0.87
48.37	59.64	35.94	3.64	130.76	2.59	0.86	0.86
48.38	60.28	36.40	3.56	129.40	2.58	0.85	0.85
48.39	61.02	36.94	3.46	127.82	2.56	0.84	0.84
48.40	61.82	37.52	3.36	126.07	2.55	0.83	0.83
48.41	62.64	38.11	3.26	124.25	2.54	0.81	0.81
48.42	63.43	38.70	3.16	122.45	2.53	0.80	0.80
48.43	64.16	39.23	3.08	120.77	2.51	0.78	0.78
48.44	64.78	39.69	3.01	119.36	2.50	0.77	0.77
48.45	65.33	40.09	2.95	118.35	2.50	0.78	0.78
48.46	65.88	40.48	2.90	117.60	2.49	0.78	0.78
48.47	66.51	40.93	2.86	116.94	2.48	0.78	0.78
48.48	67.22	41.43	2.80	116.20	2.47	0.78	0.78

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
48.49	67.97	41.97	2.75	115.40	2.47	0.78	0.78
48.50	68.72	42.51	2.70	114.59	2.46	0.77	0.77
48.51	69.43	43.02	2.65	113.81	2.45	0.77	0.77
48.52	70.07	43.48	2.60	113.11	2.44	0.77	0.77
48.53	70.56	43.83	2.57	112.65	2.44	0.77	0.77
48.54	70.90	44.06	2.55	112.53	2.43	0.77	0.77
48.55	71.12	44.20	2.55	112.72	2.43	0.77	0.77
48.56	71.34	44.34	2.55	113.06	2.43	0.77	0.77
48.57	71.58	44.48	2.55	113.43	2.43	0.77	0.77
48.58	71.83	44.64	2.55	113.82	2.43	0.77	0.77
48.59	72.08	44.79	2.55	114.20	2.43	0.77	0.77
48.60	72.31	44.93	2.55	114.55	2.43	0.77	0.77
48.61	72.51	45.05	2.55	114.87	2.43	0.77	0.77
48.62	72.55	45.05	2.57	115.56	2.43	0.78	0.78
48.63	72.40	44.90	2.60	116.81	2.44	0.78	0.78
48.64	72.07	44.60	2.66	118.74	2.45	0.78	0.78
48.65	71.68	44.25	2.73	120.98	2.46	0.78	0.78
48.66	71.26	43.88	2.81	123.37	2.47	0.79	0.79
48.67	70.83	43.51	2.89	125.80	2.49	0.79	0.79
48.68	70.41	43.15	2.97	128.13	2.50	0.80	0.80
48.69	70.03	42.82	3.04	130.25	2.51	0.79	0.79
48.70	69.69	42.54	3.11	132.15	2.52	0.81	0.81
48.71	69.36	42.24	3.18	134.30	2.53	0.82	0.82
48.72	68.97	41.91	3.27	137.01	2.54	0.83	0.83
48.73	68.51	41.50	3.38	140.44	2.56	0.85	0.85
48.74	67.98	41.04	3.51	144.22	2.57	0.87	0.87
48.75	67.43	40.57	3.65	148.14	2.59	0.89	0.89
48.76	66.87	40.10	3.79	151.99	2.60	0.91	0.91
48.77	66.34	39.66	3.92	155.57	2.62	0.93	0.93
48.78	65.87	39.27	4.04	158.72	2.63	0.95	0.95
48.79	65.46	38.93	4.14	161.30	2.64	0.96	0.96
48.80	65.06	38.62	4.24	163.55	2.65	0.97	0.97
48.81	64.62	38.27	4.33	165.79	2.66	0.98	0.98
48.82	64.11	37.88	4.44	168.31	2.67	1.00	1.00
48.83	63.55	37.44	4.57	171.01	2.69	1.02	1.02
48.84	62.97	37.00	4.70	173.75	2.70	1.03	1.03
48.85	62.40	36.56	4.82	176.37	2.71	0.86	0.86
48.86	61.86	36.16	4.94	178.76	2.72	0.86	0.86
48.87	61.39	35.80	5.05	180.80	2.73	0.87	0.87
48.88	61.10	35.58	5.12	182.16	2.74	0.87	0.87
48.89	60.97	35.47	5.16	182.98	2.74	0.87	0.87
48.90	60.97	35.45	5.17	183.44	2.74	0.87	0.87
48.91	60.97	35.44	5.19	183.94	2.74	0.87	0.87
48.92	60.97	35.42	5.21	184.48	2.75	0.87	0.87
48.93	60.97	35.40	5.23	185.04	2.75	0.87	0.87
48.94	60.97	35.38	5.24	185.57	2.75	0.87	0.87
48.95	60.97	35.37	5.26	186.06	2.75	0.87	0.87
48.96	61.06	35.41	5.26	186.42	2.75	0.87	0.87

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
48.97	61.50	35.70	5.23	186.54	2.75	0.87	0.87
48.98	62.38	36.27	5.14	186.41	2.74	0.87	0.87
48.99	63.66	37.12	5.01	186.06	2.73	0.87	0.87
49.00	65.09	38.07	4.88	185.60	2.72	0.87	0.87
49.01	66.60	39.07	4.74	185.02	2.70	0.87	0.87
49.02	68.12	40.08	4.60	184.37	2.69	1.04	1.04
49.03	69.55	41.04	4.47	183.67	2.68	1.02	1.02
49.04	70.84	41.91	4.37	182.98	2.67	1.01	1.01
49.05	72.07	42.73	4.27	182.31	2.66	1.00	1.00
49.06	73.50	43.69	4.16	181.55	2.64	0.99	0.99
49.07	75.30	44.91	4.02	180.58	2.63	0.97	0.97
49.08	77.48	46.39	3.87	179.31	2.61	0.96	0.96
49.09	79.88	48.03	3.70	177.78	2.59	0.94	0.94
49.10	82.36	49.73	3.54	176.05	2.57	0.92	0.92
49.11	84.80	51.42	3.39	174.21	2.56	0.90	0.90
49.12	87.08	53.00	3.25	172.39	2.54	0.88	0.88
49.13	89.06	54.38	3.14	170.72	2.52	0.86	0.86
49.14	90.94	55.69	3.04	169.35	2.51	0.85	0.85
49.15	92.99	57.11	2.94	168.13	2.49	0.85	0.85
49.16	95.46	58.83	2.84	166.88	2.48	0.85	0.85
49.17	98.30	60.82	2.72	165.39	2.46	0.85	0.85
49.18	101.35	62.97	2.60	163.72	2.44	0.84	0.84
49.19	104.46	65.17	2.49	161.97	2.42	0.84	0.84
49.20	107.46	67.30	2.38	160.25	2.40	0.84	0.84
49.21	110.20	69.27	2.29	158.65	2.38	0.84	0.84
49.22	112.54	70.95	2.22	157.36	2.37	0.84	0.84
49.23	114.65	72.46	2.16	156.48	2.36	0.84	0.84
49.24	116.81	74.00	2.11	155.90	2.34	0.83	0.83
49.25	119.31	75.77	2.05	155.43	2.33	0.83	0.83
49.26	122.10	77.77	1.99	154.93	2.32	0.83	0.83
49.27	125.05	79.89	1.93	154.43	2.30	0.83	0.83
49.28	127.99	82.02	1.88	153.98	2.29	0.83	0.83
49.29	130.79	84.06	1.83	153.61	2.27	0.83	0.83
49.30	133.29	85.88	1.79	153.30	2.26	0.83	0.83
49.31	135.27	87.32	1.75	153.19	2.25	0.83	0.83
49.32	136.86	88.46	1.73	153.30	2.24	0.83	0.83
49.33	138.28	89.46	1.72	153.64	2.24	0.83	0.83
49.34	139.85	90.57	1.70	154.10	2.23	0.83	0.83
49.35	141.56	91.79	1.68	154.62	2.23	0.83	0.83
49.36	143.34	93.05	1.67	155.17	2.22	0.83	0.83
49.37	145.09	94.29	1.65	155.72	2.21	0.83	0.83
49.38	146.71	95.44	1.64	156.25	2.21	0.84	0.84
49.39	148.13	96.44	1.62	156.72	2.20	0.84	0.84
49.40	149.24	97.21	1.62	157.21	2.20	0.84	0.84
49.41	150.17	97.85	1.61	157.80	2.20	0.84	0.84
49.42	151.06	98.44	1.61	158.56	2.20	0.84	0.84
49.43	152.09	99.12	1.61	159.43	2.20	0.84	0.84
49.44	153.19	99.85	1.61	160.37	2.20	0.84	0.84

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
49.45	154.31	100.60	1.60	161.32	2.20	0.84	0.84
49.46	155.40	101.32	1.60	162.25	2.19	0.84	0.84
49.47	156.38	101.97	1.60	163.09	2.19	0.84	0.84
49.48	157.18	102.50	1.60	163.67	2.19	0.84	0.84
49.49	157.71	102.88	1.59	163.72	2.19	0.84	0.84
49.50	158.05	103.15	1.58	163.24	2.19	0.84	0.84
49.51	158.32	103.41	1.57	162.37	2.18	0.84	0.84
49.52	158.62	103.70	1.56	161.43	2.18	0.84	0.84
49.53	158.94	104.01	1.54	160.46	2.17	0.84	0.84
49.54	159.25	104.33	1.53	159.51	2.16	0.84	0.84
49.55	159.55	104.63	1.52	158.62	2.16	0.84	0.84
49.56	159.82	104.89	1.50	157.85	2.15	0.84	0.84
49.57	159.94	105.04	1.50	157.10	2.15	0.84	0.84
49.58	159.84	105.05	1.49	156.21	2.14	0.84	0.84
49.59	159.52	104.91	1.48	155.07	2.14	0.83	0.83
49.60	159.10	104.71	1.47	153.70	2.13	0.83	0.83
49.61	158.63	104.50	1.46	152.23	2.12	0.83	0.83
49.62	158.15	104.28	1.45	150.74	2.12	0.83	0.83
49.63	157.68	104.08	1.43	149.30	2.11	0.83	0.83
49.64	157.24	103.88	1.42	147.99	2.10	0.82	0.82
49.65	156.86	103.71	1.42	146.87	2.10	0.82	0.82
49.66	156.50	103.51	1.41	146.12	2.10	0.82	0.82
49.67	156.12	103.25	1.41	145.65	2.09	0.82	0.82
49.68	155.67	102.91	1.41	145.38	2.10	0.82	0.82
49.69	155.16	102.52	1.42	145.07	2.10	0.82	0.82
49.70	154.60	102.10	1.42	144.74	2.10	0.82	0.82
49.71	154.04	101.67	1.42	144.40	2.10	0.82	0.82
49.72	153.50	101.26	1.42	144.08	2.10	0.82	0.82
49.73	153.01	100.88	1.43	143.79	2.10	0.82	0.82
49.74	152.60	100.56	1.43	143.53	2.11	0.82	0.82
49.75	152.23	100.29	1.43	143.30	2.11	0.82	0.82
49.76	151.87	100.01	1.43	143.05	2.11	0.82	0.82
49.77	151.47	99.71	1.43	142.75	2.11	0.82	0.82
49.78	151.01	99.37	1.43	142.43	2.11	0.82	0.82
49.79	150.53	99.01	1.44	142.09	2.11	0.82	0.82
49.80	150.06	98.65	1.44	141.75	2.11	0.82	0.82
49.81	149.60	98.32	1.44	141.43	2.11	0.82	0.82
49.82	149.20	98.01	1.44	141.15	2.11	0.81	0.81
49.83	148.77	97.68	1.44	140.92	2.12	0.81	0.81
49.84	148.21	97.24	1.45	140.73	2.12	0.81	0.81
49.85	147.45	96.64	1.45	140.57	2.12	0.81	0.81
49.86	146.53	95.92	1.46	140.41	2.13	0.81	0.81
49.87	145.52	95.13	1.47	140.25	2.13	0.81	0.81
49.88	144.48	94.31	1.49	140.10	2.14	0.81	0.81
49.89	143.46	93.52	1.50	139.97	2.15	0.81	0.81
49.90	142.51	92.78	1.51	139.86	2.15	0.81	0.81
49.91	141.69	92.14	1.52	139.77	2.16	0.81	0.81
49.92	141.02	91.61	1.52	139.67	2.16	0.81	0.81

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
49.93	140.40	91.14	1.53	139.56	2.16	0.81	0.81
49.94	139.76	90.65	1.54	139.40	2.17	0.81	0.81
49.95	139.02	90.08	1.55	139.24	2.17	0.81	0.81
49.96	138.23	89.48	1.55	139.06	2.17	0.81	0.81
49.97	137.43	88.88	1.56	138.89	2.18	0.81	0.81
49.98	136.66	88.29	1.57	138.74	2.18	0.81	0.81
49.99	135.96	87.76	1.58	138.60	2.19	0.81	0.81
50.00	135.52	87.42	1.58	138.51	2.19	0.81	0.81

Abbreviations

q_t :	Total cone resistance
K_c :	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c :	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

LIQUEFACTION ANALYSIS REPORT

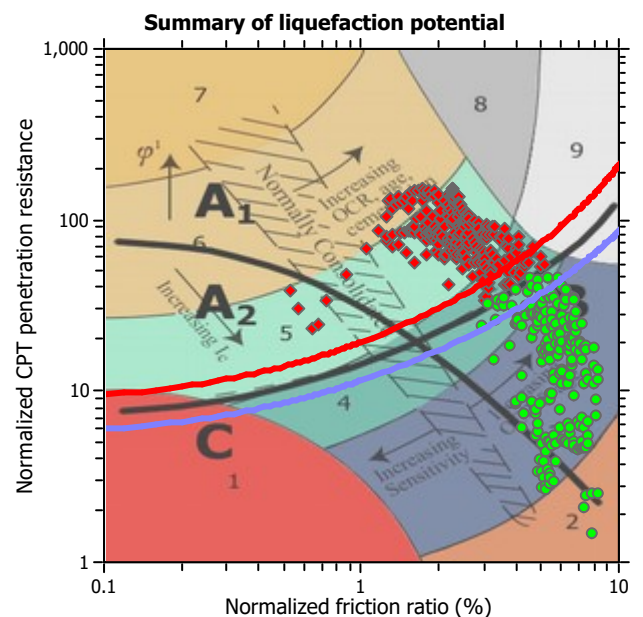
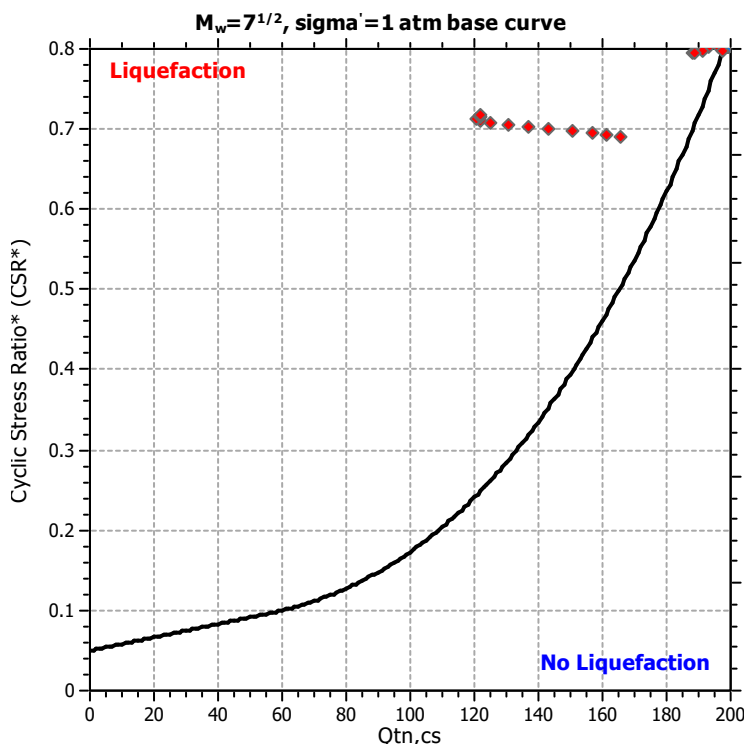
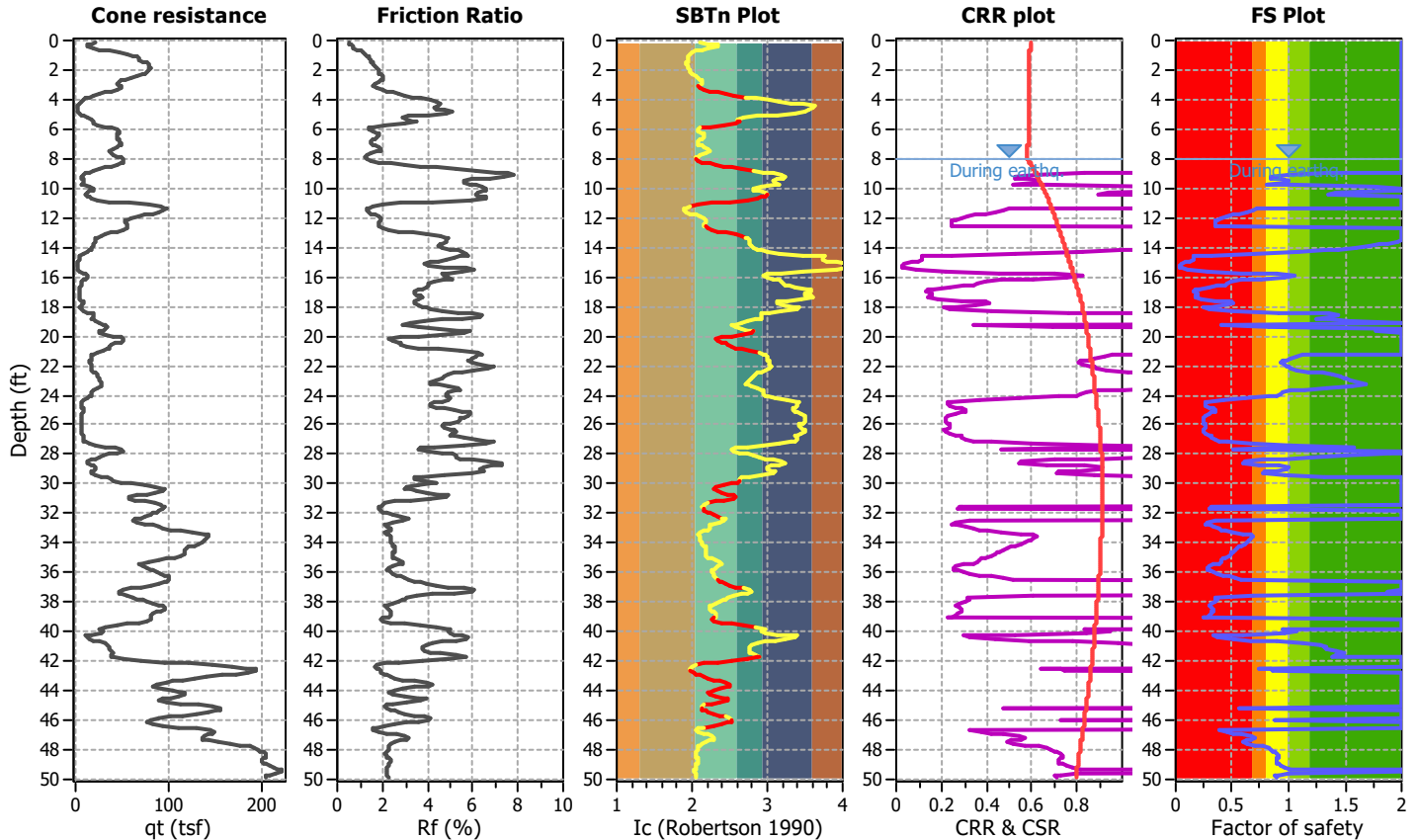
Project title : 21-483 Equestrian Estates

Location : Avenue 64 at Harrison Street, Thermal California

CPT file : CPT-3 Robt 2009

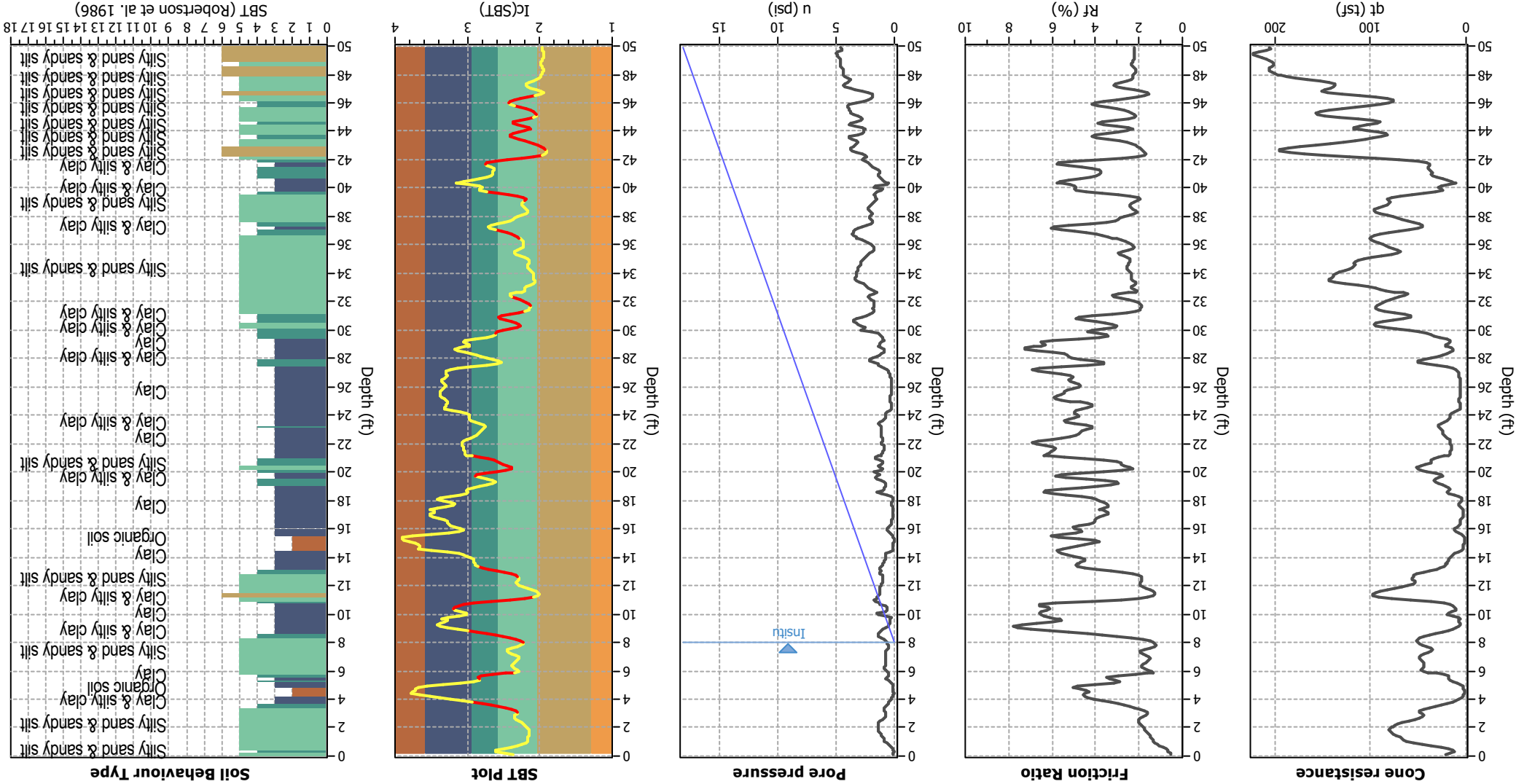
Input parameters and analysis data

Analysis method:	Robertson (2009)	G.W.T. (in-situ):	8.00 ft	Use fill:	No	Clay like behavior	
Fines correction method:	Robertson (2009)	G.W.T. (earthq.):	8.00 ft	Fill height:	N/A	applied:	All soils
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude M_w :	7.34	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.74	Unit weight calculation:	Based on SBT	K_o applied:	No	MSF method:	Method based



Zone A₁: Cyclic liquefaction likely depending on size and duration of cyclic loading
 Zone A₂: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
 Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
 Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



Input parameters and analysis data

Analysis method:	Robertson (2009)	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Limit depth applied:	No
Points to test:	Based on Ic value	Clay like behavior applied:	All soils
Earthquake magnitude M_w :	7.34	K_0 applied:	No
Peak ground acceleration:	0.74	Transition detect. applied:	Yes
Depth to water table (instu):	8.00 ft	Limit depth:	N/A
Fill height:	N/A	Unit weight calculation:	Based on SBT
Use fill:	No	Unit weight:	2.60
Depth to water table (earthq.):	8.00 ft	Ic cut-off value:	3
Average results interval:	3	Based on SBT:	N/A

SBT legend	1. Sensitive fine grained	2. Organic material	3. Clay to silty clay	4. Clayey silt to silty	5. Silty sand to sandy silt	6. Clean sand to silty sand	7. Gravely sand to sand	8. Very stiff sand to	9. Very stiff fine grained
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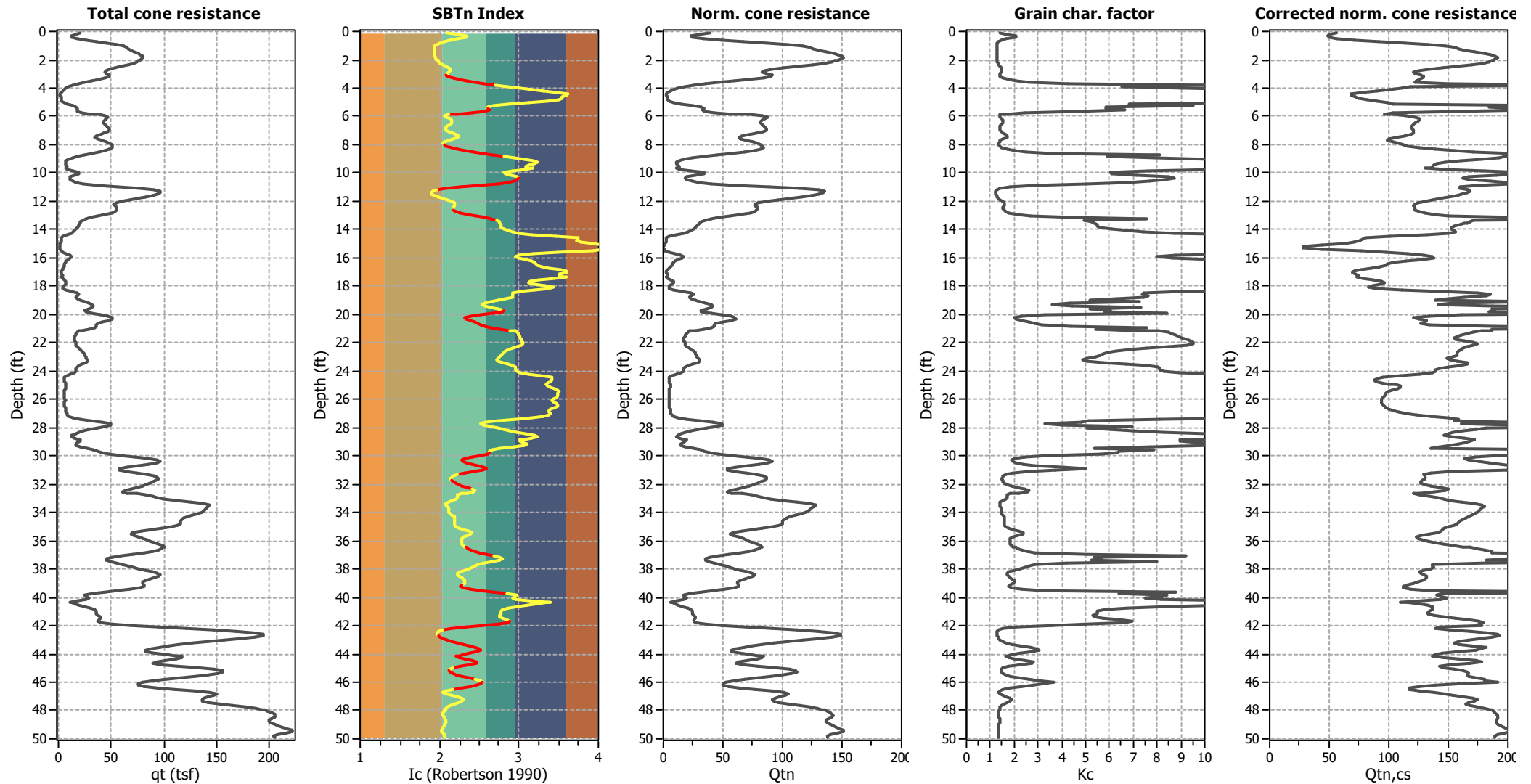
The figure displays five vertical plots showing geotechnical data versus depth (0 to 50 ft).

- Norm. cone resistance:** The y-axis is Depth (ft) from 0 to 50. The x-axis is Qtn (0 to 200). The plot shows a highly variable line representing normalized cone resistance.
- Norm. friction ratio:** The y-axis is Depth (ft) from 0 to 50. The x-axis is Fr (%) from 0 to 10. The plot shows a highly variable line representing normalized friction ratio.
- Nom. pore pressure ratio:** The y-axis is Depth (ft) from 0 to 50. The x-axis is Bq (-0.2 to 1). The plot shows a line representing normalized pore pressure ratio, mostly near zero.
- SBTn Plot:** The y-axis is Depth (ft) from 0 to 50. The x-axis is Ic (Robertson 1990) from 1 to 4. The plot shows a line representing the Soil Behaviour Type Number (SBTn) plotted against the normalized cone resistance (Qtn) and normalized friction ratio (Fr) using the Robertson (1990) method.
- Norm. Soil Behaviour Type:** The y-axis is Depth (ft) from 0 to 50. The x-axis is SBTn (Robertson 1990) from 0 to 18. The plot shows a line representing the Soil Behaviour Type Number (SBTn) plotted against the normalized cone resistance (Qtn) and normalized friction ratio (Fr) using the Robertson (1990) method.

Analysis method:	Robertson (2009)	Depth to water table (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	No
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

	1. Sensitive fine grained		4. Clayey silt to silty		7. Gravely sand to sand
	2. Organic material		5. Silty sand to sandy silt		8. Very stiff sand to
	3. Clay to silty clay		6. Clean sand to silty sand		9. Very stiff fine grained

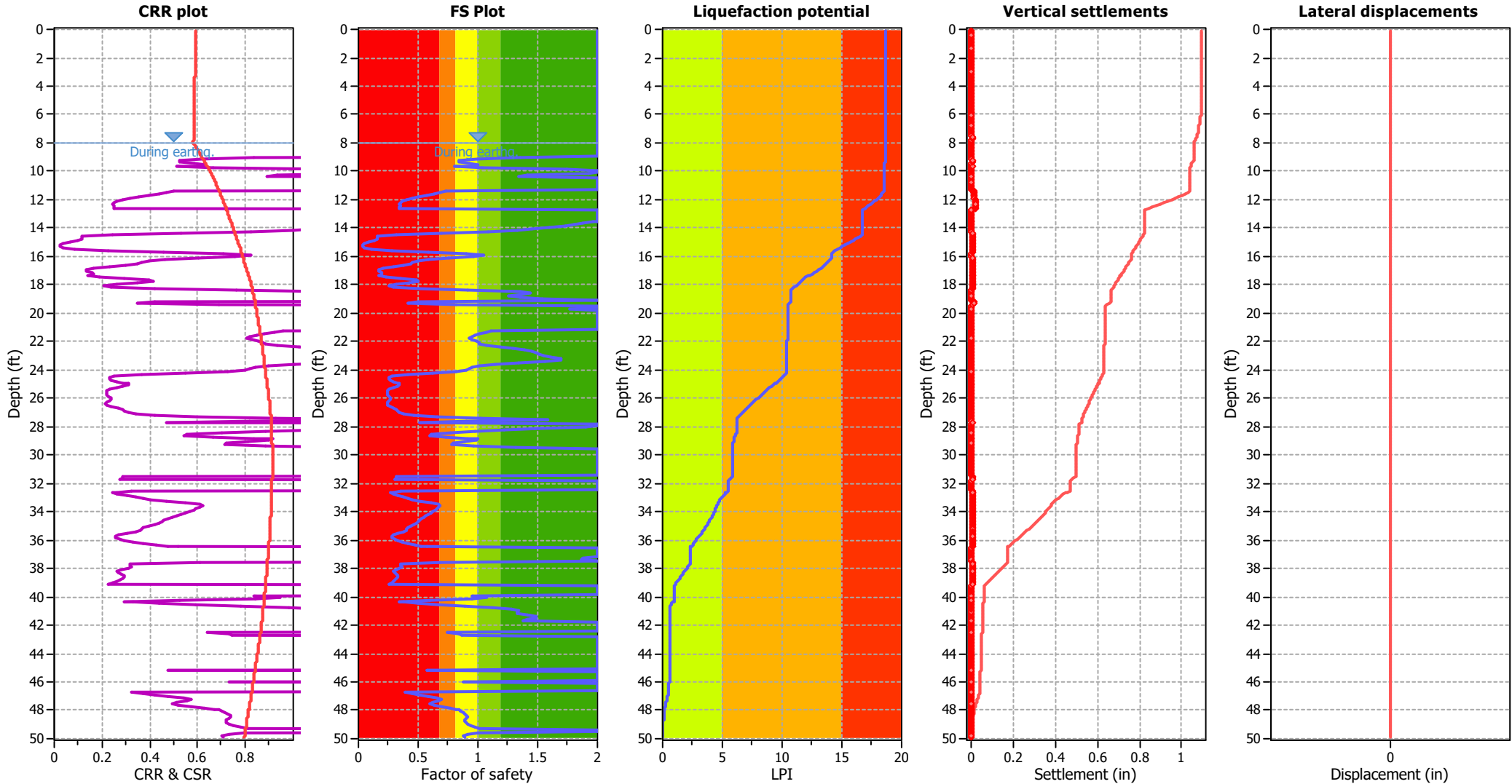
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on I_c value	I_c cut-off value:	2.60	K_o applied:	No
Earthquake magnitude M_w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (earthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	No
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

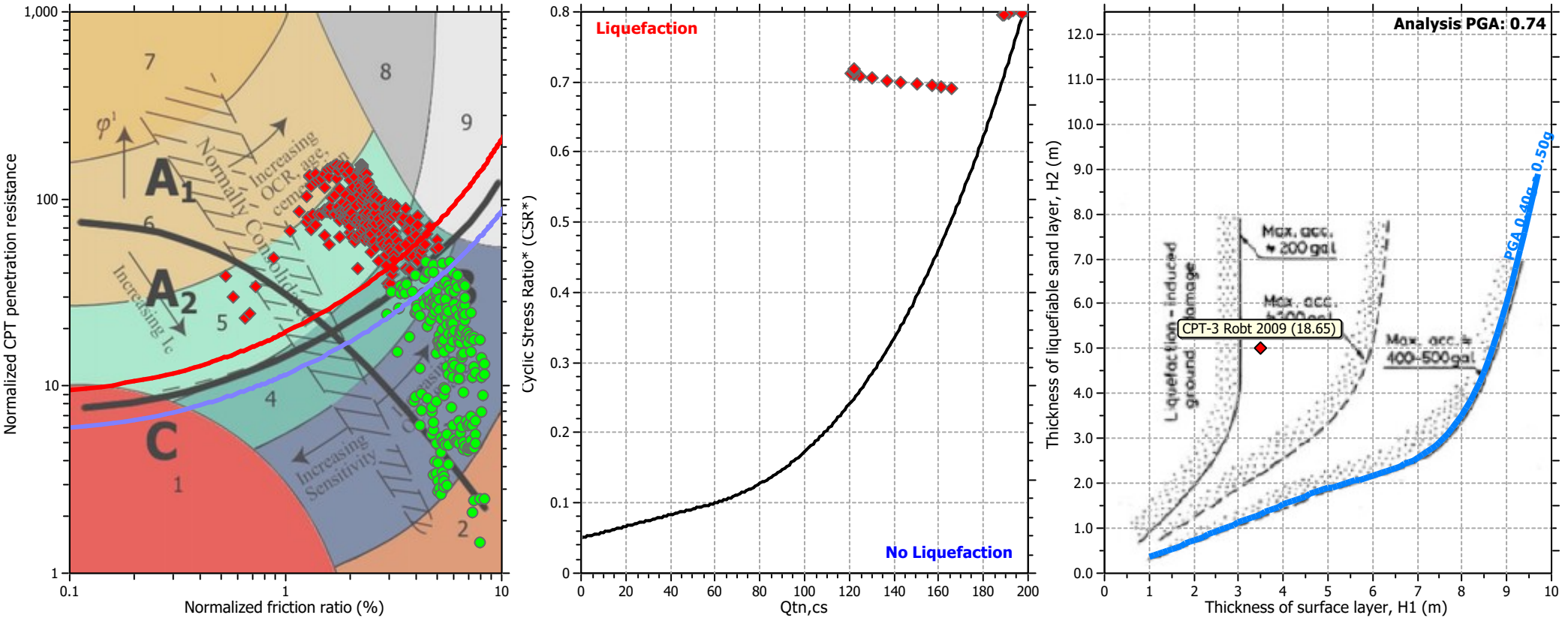
F.S. color scheme

- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

LPI color scheme

- Very high risk
- High risk
- Low risk

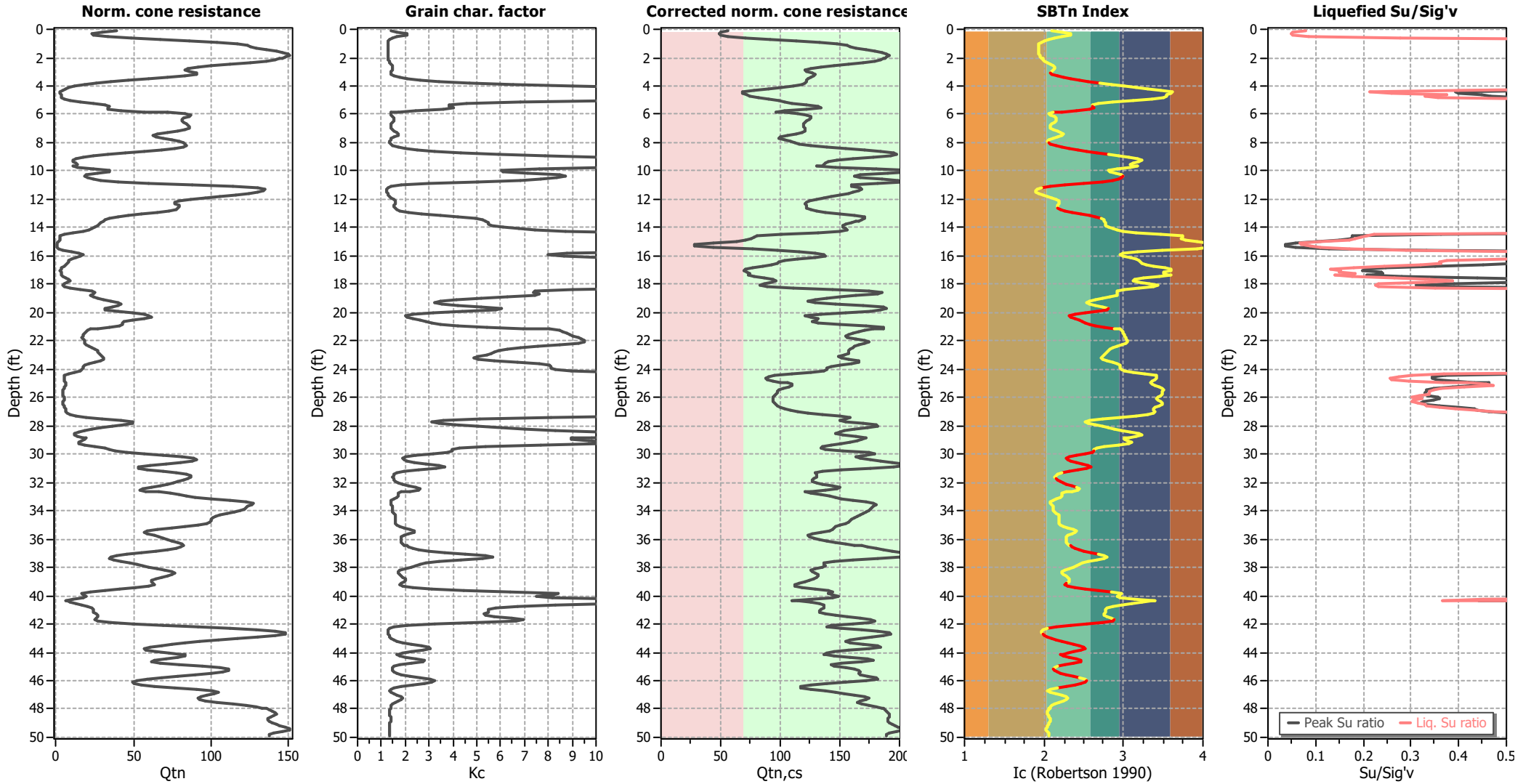
Liquefaction analysis summary plots



Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_0 applied:	No
Earthquake magnitude M_w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

Check for strength loss plots (Robertson (2010))



Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on I_c value	I_c cut-off value:	2.60	K_o applied:	No
Earthquake magnitude M_w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

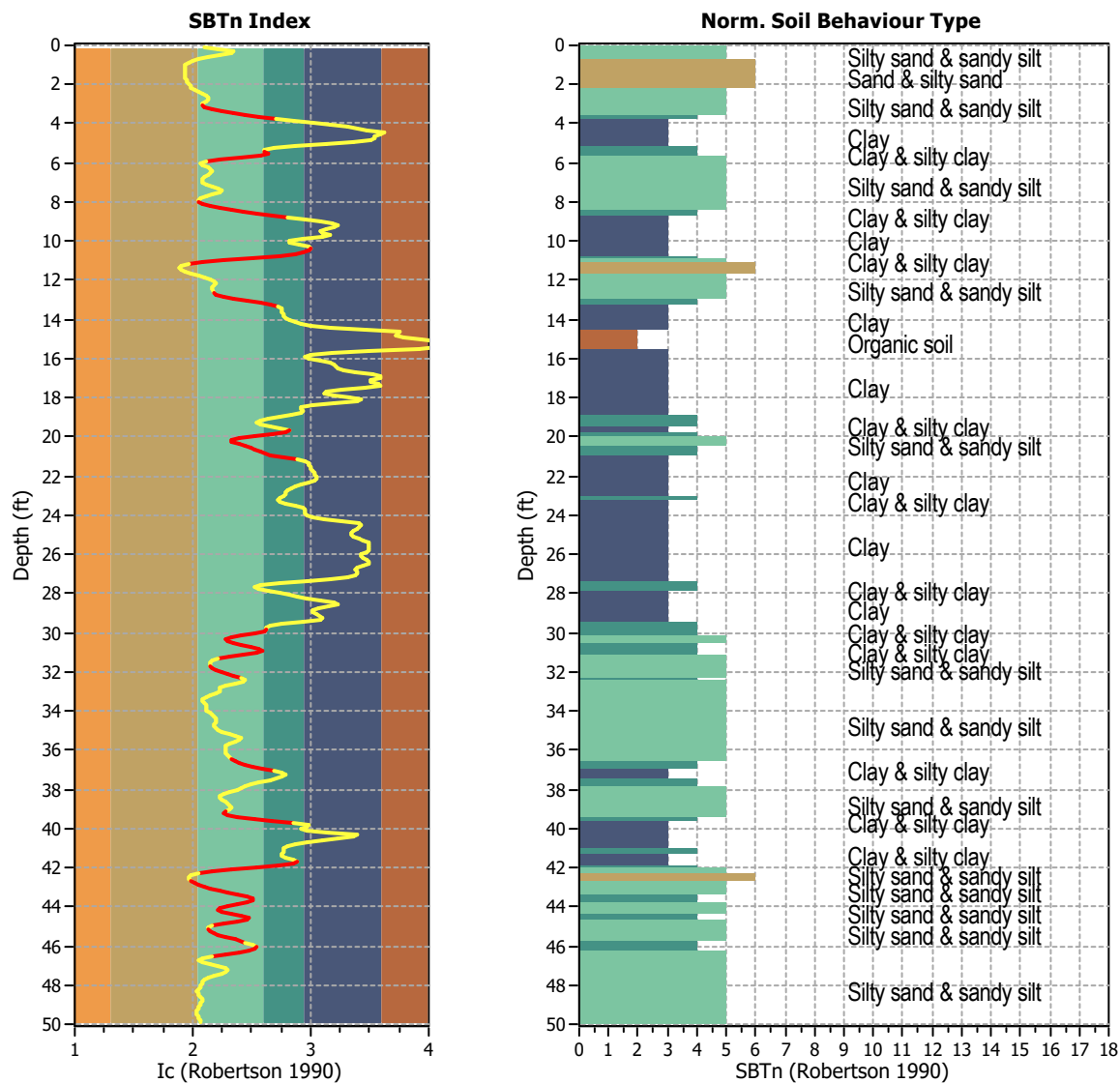
TRANSITION LAYER DETECTION ALGORITHM REPORT

Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vise-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between $1.80 < I_c < 3.0$) and a rate of change of I_c . Transitions typically occur when the rate of change of I_c is fast (i.e. ΔI_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties

I_c minimum check value: 1.70
 I_c maximum check value: 3.00
 I_c change ratio value: 0.0250
Minimum number of points in layer: 4

General statistics

Total points in CPT file: 499
Total points excluded: 137
Exclusion percentage: 27.45%
Number of layers detected: 20

Transition layer No	Number of points	Depth	SBT _n number	SBT _n description
Transition layer 1	8	Start depth: 3.20 (ft)	5	Silty sand & sandy silt
		End depth: 3.90 (ft)	3	Clay
Transition layer 2	6	Start depth: 5.50 (ft)	4	Clay & silty clay
		End depth: 6.00 (ft)	5	Silty sand & sandy silt
Transition layer 3	9	Start depth: 8.10 (ft)	5	Silty sand & sandy silt
		End depth: 8.90 (ft)	3	Clay
Transition layer 4	9	Start depth: 10.50 (ft)	3	Clay
		End depth: 11.30 (ft)	6	Sand & silty sand
Transition layer 5	8	Start depth: 12.70 (ft)	5	Silty sand & sandy silt
		End depth: 13.40 (ft)	3	Clay
Transition layer 6	5	Start depth: 19.80 (ft)	3	Clay
		End depth: 20.20 (ft)	5	Silty sand & sandy silt
Transition layer 7	10	Start depth: 20.30 (ft)	5	Silty sand & sandy silt
		End depth: 21.20 (ft)	3	Clay
Transition layer 8	5	Start depth: 29.90 (ft)	4	Clay & silty clay
		End depth: 30.30 (ft)	5	Silty sand & sandy silt
Transition layer 9	6	Start depth: 30.40 (ft)	5	Silty sand & sandy silt
		End depth: 30.90 (ft)	4	Clay & silty clay
Transition layer 10	6	Start depth: 30.90 (ft)	4	Clay & silty clay
		End depth: 31.40 (ft)	5	Silty sand & sandy silt
Transition layer 11	7	Start depth: 31.80 (ft)	5	Silty sand & sandy silt
		End depth: 32.40 (ft)	4	Clay & silty clay
Transition layer 12	7	Start depth: 36.60 (ft)	5	Silty sand & sandy silt
		End depth: 37.20 (ft)	3	Clay
Transition layer 13	7	Start depth: 39.20 (ft)	5	Silty sand & sandy silt
		End depth: 39.80 (ft)	3	Clay
Transition layer 14	7	Start depth: 41.80 (ft)	3	Clay
		End depth: 42.40 (ft)	6	Sand & silty sand
Transition layer 15	9	Start depth: 42.80 (ft)	5	Silty sand & sandy silt
		End depth: 43.60 (ft)	4	Clay & silty clay
Transition layer 16	5	Start depth: 43.70 (ft)	4	Clay & silty clay
		End depth: 44.10 (ft)	5	Silty sand & sandy silt
Transition layer 17	5	Start depth: 44.20 (ft)	5	Silty sand & sandy silt
		End depth: 44.60 (ft)	4	Clay & silty clay
Transition layer 18	5	Start depth: 44.70 (ft)	4	Clay & silty clay
		End depth: 45.10 (ft)	5	Silty sand & sandy silt
Transition layer 19	7	Start depth: 45.30 (ft)	5	Silty sand & sandy silt
		End depth: 45.90 (ft)	4	Clay & silty clay
Transition layer 20	6	Start depth: 46.10 (ft)	4	Clay & silty clay
		End depth: 46.60 (ft)	5	Silty sand & sandy silt

Start depth: Depth where the transition layer begins
End depth: Depth where the transition layer ends

:: Field input data ::						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1	0.10	23.36	0.12	0.12	15.85	101.47
2	0.20	15.35	0.09	0.09	19.55	99.44
3	0.30	9.12	0.06	0.06	24.14	97.83
4	0.40	12.40	0.08	0.08	23.84	98.63
5	0.50	17.04	0.11	0.11	19.72	102.39
6	0.60	24.34	0.19	0.19	16.80	107.27
7	0.70	35.40	0.37	0.37	14.54	111.74
8	0.80	47.10	0.55	0.55	12.97	114.99
9	0.90	54.87	0.67	0.67	11.93	117.32
10	1.00	63.20	0.84	0.84	11.36	118.85
11	1.10	67.85	0.94	0.94	11.26	119.69
12	1.20	65.14	0.92	0.92	11.34	120.11
13	1.30	67.16	0.98	0.98	11.34	120.62
14	1.40	74.04	1.11	1.11	11.24	121.31
15	1.50	75.01	1.17	1.17	11.15	122.00
16	1.60	77.31	1.25	1.25	11.21	122.55
17	1.70	80.96	1.35	1.35	11.31	122.99
18	1.80	80.02	1.38	1.38	11.51	123.26
19	1.90	78.73	1.39	1.39	11.85	123.32
20	2.00	77.42	1.40	1.40	12.17	123.34
21	2.10	76.40	1.41	1.41	12.41	123.32
22	2.20	75.47	1.40	1.40	12.71	123.24
23	2.30	72.92	1.39	1.39	13.26	123.05
24	2.40	67.65	1.36	1.36	14.21	122.55
25	2.50	59.20	1.22	1.22	15.35	121.67
26	2.60	52.57	1.06	1.06	16.28	120.48
27	2.70	48.33	0.93	0.93	16.78	119.25
28	2.80	44.75	0.81	0.81	16.88	118.13
29	2.90	42.83	0.72	0.72	16.38	117.34
30	3.00	45.35	0.70	0.70	15.50	117.26
31	3.10	49.63	0.76	0.76	15.17	117.86
32	3.20	49.85	0.87	0.87	15.99	118.47
33	3.30	44.82	0.90	0.90	17.92	118.56
34	3.40	38.54	0.86	0.86	20.64	117.98
35	3.50	31.85	0.79	0.79	23.98	116.81
36	3.60	24.55	0.67	0.67	28.16	115.19
37	3.70	18.60	0.55	0.55	33.56	113.20
38	3.80	13.62	0.46	0.46	40.35	110.98
39	3.90	9.43	0.36	0.36	48.94	108.44
40	4.00	6.42	0.27	0.27	59.41	105.43
41	4.10	4.27	0.19	0.19	70.08	102.53
42	4.20	3.51	0.16	0.16	82.18	99.28
43	4.30	2.12	0.10	0.10	96.27	95.74
44	4.40	1.20	0.05	0.05	100.00	92.31
45	4.50	1.57	0.07	0.07	100.00	92.34
46	4.60	2.27	0.10	0.10	100.00	93.69
47	4.70	1.85	0.09	0.09	100.00	94.63
48	4.80	1.86	0.10	0.10	100.00	96.45

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
49	4.90	3.12	0.16	0.16	86.53	99.04
50	5.00	4.25	0.19	0.19	67.21	102.50
51	5.10	7.69	0.26	0.26	50.30	105.75
52	5.20	13.10	0.35	0.35	39.89	109.38
53	5.30	18.16	0.52	0.52	35.93	112.46
54	5.40	19.86	0.70	0.70	35.96	113.89
55	5.50	17.23	0.64	0.64	36.95	113.78
56	5.60	16.35	0.51	0.51	34.37	112.89
57	5.70	21.19	0.47	0.47	26.99	112.56
58	5.80	30.23	0.46	0.46	20.00	113.21
59	5.90	39.59	0.50	0.50	16.04	114.53
60	6.00	46.17	0.62	0.62	14.89	116.08
61	6.10	47.46	0.75	0.75	15.44	117.39
62	6.20	45.94	0.83	0.83	16.62	118.03
63	6.30	43.81	0.84	0.84	17.53	118.12
64	6.40	42.74	0.81	0.81	17.73	117.90
65	6.50	43.21	0.78	0.78	17.30	117.59
66	6.60	43.90	0.74	0.74	16.58	117.35
67	6.70	45.19	0.72	0.72	15.87	117.18
68	6.80	46.56	0.71	0.71	15.35	117.15
69	6.90	47.97	0.71	0.71	15.10	117.28
70	7.00	48.76	0.74	0.74	15.39	117.54
71	7.10	47.05	0.78	0.78	16.38	117.77
72	7.20	43.20	0.80	0.80	17.92	117.76
73	7.30	39.14	0.80	0.80	19.53	117.31
74	7.40	35.23	0.71	0.71	20.43	116.41
75	7.50	33.45	0.60	0.60	19.89	115.36
76	7.60	35.99	0.53	0.53	18.06	114.64
77	7.70	40.66	0.51	0.51	16.09	114.68
78	7.80	45.60	0.55	0.55	14.82	115.28
79	7.90	49.24	0.61	0.61	14.37	116.07
80	8.00	50.61	0.66	0.66	14.50	116.83
81	8.10	51.17	0.72	0.72	15.23	117.70
82	8.20	50.93	0.86	0.86	17.17	119.23
83	8.30	49.16	1.18	1.18	19.99	120.65
84	8.40	44.49	1.36	1.36	23.47	121.54
85	8.50	38.38	1.42	1.42	27.49	121.57
86	8.60	31.10	1.40	1.40	32.29	120.92
87	8.70	23.78	1.27	1.27	38.57	119.79
88	8.80	17.85	1.13	1.13	46.15	118.19
89	8.90	13.17	0.96	0.96	54.78	116.18
90	9.00	9.32	0.74	0.74	63.76	113.66
91	9.10	6.86	0.53	0.53	71.69	111.11
92	9.20	6.02	0.45	0.45	75.29	109.24
93	9.30	6.09	0.42	0.42	73.08	108.59
94	9.40	6.95	0.41	0.41	67.63	108.75
95	9.50	8.10	0.44	0.44	64.23	108.92
96	9.60	7.66	0.42	0.42	65.18	108.64

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
97	9.70	6.25	0.38	0.38	70.73	107.42
98	9.80	4.87	0.31	0.31	64.98	110.04
99	9.90	12.65	0.78	0.78	53.66	115.26
100	10.00	21.85	1.43	1.43	46.94	118.94
101	10.10	21.86	1.48	1.48	47.23	118.92
102	10.20	12.25	0.78	0.78	51.79	116.47
103	10.30	9.79	0.61	0.61	57.34	113.31
104	10.40	10.78	0.66	0.66	58.12	112.77
105	10.50	10.84	0.66	0.66	56.88	113.47
106	10.60	11.83	0.75	0.75	53.90	115.64
107	10.70	17.45	1.22	1.22	50.29	117.59
108	10.80	19.39	1.25	1.25	42.23	120.15
109	10.90	32.59	1.60	1.60	30.89	122.14
110	11.00	57.58	1.73	1.73	21.31	123.67
111	11.10	80.88	1.54	1.54	15.27	124.21
112	11.20	94.33	1.46	1.46	12.00	123.96
113	11.30	98.49	1.33	1.33	10.61	123.48
114	11.40	96.60	1.19	1.19	10.12	122.98
115	11.50	95.04	1.19	1.19	10.33	122.66
116	11.60	89.85	1.21	1.21	11.17	122.64
117	11.70	82.57	1.24	1.24	12.52	122.62
118	11.80	74.95	1.27	1.27	14.18	122.36
119	11.90	65.44	1.21	1.21	15.84	121.96
120	12.00	60.20	1.17	1.17	17.35	121.28
121	12.10	54.00	1.07	1.07	18.45	120.51
122	12.20	49.56	0.96	0.96	18.71	120.08
123	12.30	54.68	1.02	1.02	18.39	120.02
124	12.40	55.98	1.03	1.03	17.93	120.26
125	12.50	55.38	1.02	1.02	17.90	120.27
126	12.60	55.38	1.02	1.02	18.19	120.31
127	12.70	54.30	1.06	1.06	19.05	120.67
128	12.80	52.80	1.20	1.20	21.01	121.07
129	12.90	46.00	1.28	1.28	24.35	120.97
130	13.00	34.79	1.18	1.18	28.83	120.69
131	13.10	31.32	1.27	1.27	33.91	120.12
132	13.20	26.15	1.23	1.23	38.00	119.58
133	13.30	21.95	1.09	1.09	41.51	118.57
134	13.40	20.08	0.97	0.97	43.16	117.83
135	13.50	20.69	0.99	0.99	43.62	117.47
136	13.60	20.11	0.98	0.98	43.83	117.28
137	13.70	19.22	0.91	0.91	44.19	116.73
138	13.80	18.46	0.82	0.82	44.26	116.20
139	13.90	18.46	0.81	0.81	44.97	115.81
140	14.00	17.17	0.81	0.81	47.14	115.35
141	14.10	14.45	0.73	0.73	50.20	114.88
142	14.20	13.85	0.74	0.74	52.99	114.58
143	14.30	13.76	0.78	0.78	58.23	113.08
144	14.40	7.30	0.43	0.43	69.93	109.42

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
145	14.50	2.41	0.14	0.14	95.36	103.06
146	14.60	2.41	0.13	0.13	100.00	97.61
147	14.70	2.41	0.12	0.12	100.00	97.15
148	14.80	2.41	0.12	0.12	100.00	96.67
149	14.90	2.41	0.11	0.11	100.00	95.24
150	15.00	1.75	0.07	0.07	100.00	92.65
151	15.10	1.20	0.04	0.04	100.00	89.56
152	15.20	1.20	0.05	0.05	100.00	88.55
153	15.30	1.20	0.06	0.06	100.00	89.83
154	15.40	1.20	0.07	0.07	100.00	92.56
155	15.50	1.77	0.11	0.11	100.00	96.70
156	15.60	3.16	0.19	0.19	97.54	102.42
157	15.70	6.83	0.35	0.35	70.95	107.31
158	15.80	11.33	0.50	0.50	58.36	110.80
159	15.90	13.58	0.62	0.62	55.16	112.33
160	16.00	11.74	0.61	0.61	57.92	111.99
161	16.10	8.82	0.46	0.46	64.07	110.14
162	16.20	7.21	0.33	0.33	69.92	107.42
163	16.30	6.02	0.25	0.25	72.58	105.37
164	16.40	6.02	0.24	0.24	73.94	104.36
165	16.50	6.02	0.24	0.24	75.28	103.93
166	16.60	5.35	0.22	0.22	79.64	102.79
167	16.70	4.18	0.16	0.16	87.94	100.72
168	16.80	3.23	0.12	0.12	100.00	97.98
169	16.90	2.46	0.09	0.09	100.00	96.40
170	17.00	3.01	0.10	0.10	100.00	95.88
171	17.10	3.09	0.10	0.10	100.00	97.00
172	17.20	3.58	0.12	0.12	100.00	97.44
173	17.30	3.19	0.12	0.12	100.00	97.13
174	17.40	2.45	0.10	0.10	100.00	96.99
175	17.50	3.29	0.12	0.12	94.68	98.71
176	17.60	5.31	0.18	0.18	77.57	101.73
177	17.70	7.05	0.23	0.23	67.97	104.11
178	17.80	7.83	0.27	0.27	66.97	104.70
179	17.90	6.23	0.23	0.23	72.97	103.59
180	18.00	4.20	0.16	0.16	83.57	101.67
181	18.10	4.01	0.16	0.16	92.49	100.34
182	18.20	4.01	0.16	0.16	88.41	101.80
183	18.30	5.63	0.25	0.25	72.28	107.19
184	18.40	12.16	0.60	0.60	59.39	113.37
185	18.50	19.22	1.13	1.13	53.00	117.76
186	18.60	21.87	1.46	1.46	52.73	118.89
187	18.70	16.04	1.05	1.05	53.75	118.30
188	18.80	16.26	0.91	0.91	52.97	116.65
189	18.90	18.16	0.84	0.84	48.03	116.20
190	19.00	20.82	0.81	0.81	42.67	116.19
191	19.10	24.12	0.79	0.79	37.63	116.44
192	19.20	28.37	0.80	0.80	33.73	117.05

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
193	19.30	32.47	0.90	0.90	32.34	118.37
194	19.40	34.48	1.17	1.17	33.96	120.08
195	19.50	33.01	1.49	1.49	37.75	121.31
196	19.60	28.76	1.60	1.60	42.68	121.60
197	19.70	24.19	1.51	1.51	46.85	120.84
198	19.80	21.41	1.24	1.24	45.63	120.72
199	19.90	30.61	1.50	1.50	38.88	121.69
200	20.00	43.94	1.76	1.76	31.72	122.04
201	20.10	46.11	1.11	1.11	26.18	121.66
202	20.20	51.95	1.06	1.06	23.28	120.89
203	20.30	53.23	1.29	1.29	23.72	121.48
204	20.40	48.90	1.38	1.38	25.93	121.54
205	20.50	40.77	1.19	1.19	28.31	120.60
206	20.60	35.38	0.98	0.98	30.07	119.44
207	20.70	34.67	0.99	0.99	31.50	119.58
208	20.80	36.88	1.29	1.29	33.84	120.92
209	20.90	35.91	1.63	1.63	37.95	121.92
210	21.00	28.52	1.65	1.65	43.95	121.67
211	21.10	21.10	1.39	1.39	50.91	120.26
212	21.20	17.53	1.13	1.13	55.48	118.73
213	21.30	17.43	1.07	1.07	57.17	117.67
214	21.40	16.33	1.00	1.00	57.67	117.18
215	21.50	15.77	0.96	0.96	58.51	116.64
216	21.60	15.34	0.89	0.89	58.89	116.22
217	21.70	15.05	0.87	0.87	59.43	115.89
218	21.80	14.58	0.86	0.86	60.35	115.92
219	21.90	14.69	0.91	0.91	60.88	116.66
220	22.00	16.43	1.13	1.13	61.38	117.45
221	22.10	16.15	1.15	1.15	61.39	117.84
222	22.20	15.74	1.06	1.06	60.31	117.66
223	22.30	17.06	1.03	1.03	57.33	117.52
224	22.40	18.76	1.03	1.03	53.48	117.82
225	22.50	20.92	1.09	1.09	50.34	118.22
226	22.60	22.52	1.11	1.11	47.94	118.56
227	22.70	23.58	1.10	1.10	46.32	118.79
228	22.80	24.50	1.14	1.14	45.56	118.98
229	22.90	24.68	1.16	1.16	44.98	119.08
230	23.00	25.14	1.13	1.13	43.88	119.01
231	23.10	26.33	1.07	1.07	42.10	119.03
232	23.20	28.36	1.12	1.12	41.18	119.47
233	23.30	29.17	1.28	1.28	42.32	120.00
234	23.40	26.46	1.33	1.33	45.52	120.03
235	23.50	22.23	1.23	1.23	49.95	119.18
236	23.60	18.49	1.03	1.03	53.67	117.90
237	23.70	17.23	0.91	0.91	55.47	116.57
238	23.80	16.44	0.80	0.80	55.67	115.63
239	23.90	15.88	0.74	0.74	55.75	115.17
240	24.00	16.09	0.78	0.78	56.57	115.03

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
241	24.10	15.38	0.77	0.77	59.26	114.37
242	24.20	12.06	0.60	0.60	66.68	112.02
243	24.30	6.53	0.32	0.32	78.06	108.59
244	24.40	5.62	0.26	0.26	90.22	105.18
245	24.50	5.62	0.24	0.24	91.33	104.14
246	24.60	5.62	0.23	0.23	90.40	103.80
247	24.70	5.62	0.23	0.23	89.26	104.07
248	24.80	6.08	0.26	0.26	86.90	105.23
249	24.90	7.02	0.33	0.33	85.05	106.60
250	25.00	7.22	0.37	0.37	84.72	107.76
251	25.10	7.22	0.41	0.41	86.49	108.37
252	25.20	7.10	0.42	0.42	89.99	108.24
253	25.30	6.16	0.37	0.37	94.22	107.53
254	25.40	5.62	0.33	0.33	97.90	106.57
255	25.50	5.62	0.31	0.31	98.85	106.00
256	25.60	5.62	0.30	0.30	98.47	105.84
257	25.70	5.62	0.31	0.31	98.47	105.79
258	25.80	5.62	0.31	0.31	98.15	105.65
259	25.90	5.62	0.29	0.29	95.89	105.46
260	26.00	5.97	0.28	0.28	92.30	105.46
261	26.10	6.42	0.29	0.29	91.60	105.43
262	26.20	5.78	0.28	0.28	93.20	105.38
263	26.30	5.62	0.28	0.28	96.71	105.24
264	26.40	5.62	0.29	0.29	98.25	105.41
265	26.50	5.62	0.30	0.30	97.84	105.70
266	26.60	5.92	0.31	0.31	93.73	106.21
267	26.70	6.87	0.33	0.33	89.37	106.88
268	26.80	7.22	0.37	0.37	87.33	107.72
269	26.90	7.22	0.40	0.40	88.50	108.46
270	27.00	7.24	0.44	0.44	88.76	109.58
271	27.10	8.25	0.54	0.54	87.31	110.96
272	27.20	9.15	0.65	0.65	81.76	112.94
273	27.30	11.79	0.83	0.83	70.15	115.65
274	27.40	19.00	1.16	1.16	55.80	118.33
275	27.50	28.88	1.34	1.34	42.53	120.58
276	27.60	42.78	1.44	1.44	34.45	122.41
277	27.70	52.84	1.77	1.77	31.71	123.98
278	27.80	52.02	2.12	2.12	33.23	124.94
279	27.90	44.52	2.16	2.16	37.28	124.84
280	28.00	36.12	1.93	1.93	42.08	123.62
281	28.10	28.71	1.51	1.51	46.73	121.69
282	28.20	23.10	1.19	1.19	51.05	119.72
283	28.30	20.01	1.08	1.08	56.64	117.99
284	28.40	15.37	0.92	0.92	63.94	116.59
285	28.50	12.11	0.83	0.83	72.57	115.44
286	28.60	11.28	0.84	0.84	75.03	115.92
287	28.70	14.81	1.11	1.11	69.42	117.68
288	28.80	19.73	1.38	1.38	62.52	119.31

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
289	28.90	21.85	1.39	1.39	59.21	119.75
290	29.00	19.95	1.23	1.23	59.09	119.44
291	29.10	18.95	1.23	1.23	61.96	118.66
292	29.20	16.41	1.11	1.11	65.18	117.71
293	29.30	14.40	0.91	0.91	63.65	117.04
294	29.40	18.69	0.95	0.95	54.12	117.31
295	29.50	27.27	1.03	1.03	43.72	118.55
296	29.60	35.26	1.12	1.12	38.29	119.76
297	29.70	36.90	1.27	1.27	36.67	120.81
298	29.80	37.86	1.42	1.42	36.57	122.67
299	29.90	47.57	2.06	2.06	35.63	125.18
300	30.00	59.43	2.84	2.84	31.90	126.96
301	30.10	72.06	2.61	2.61	27.13	127.87
302	30.20	88.24	2.49	2.49	23.36	128.27
303	30.30	96.28	2.86	2.86	21.90	128.96
304	30.40	98.08	3.12	3.12	22.50	129.68
305	30.50	94.63	3.30	3.30	24.07	130.09
306	30.60	87.48	3.49	3.49	26.65	130.14
307	30.70	75.37	3.48	3.48	29.99	129.78
308	30.80	63.77	3.24	3.24	33.28	128.88
309	30.90	55.59	2.77	2.77	34.73	127.66
310	31.00	54.58	2.33	2.33	32.64	126.55
311	31.10	63.00	2.08	2.08	27.79	125.82
312	31.20	75.21	1.86	1.86	22.84	125.45
313	31.30	85.87	1.74	1.74	19.60	125.39
314	31.40	91.96	1.81	1.81	18.03	125.57
315	31.50	95.17	1.85	1.85	17.40	125.68
316	31.60	95.44	1.76	1.76	17.13	125.56
317	31.70	93.52	1.71	1.71	17.30	125.35
318	31.80	89.94	1.73	1.73	17.99	125.26
319	31.90	86.16	1.75	1.75	19.00	125.29
320	32.00	83.26	1.80	1.80	20.32	125.51
321	32.10	79.93	1.96	1.96	22.12	125.94
322	32.20	75.59	2.16	2.16	24.40	126.32
323	32.30	69.54	2.25	2.25	26.71	126.25
324	32.40	62.40	2.08	2.08	28.20	125.53
325	32.50	57.88	1.73	1.73	27.69	124.55
326	32.60	62.47	1.56	1.56	24.72	123.92
327	32.70	74.66	1.53	1.53	21.60	124.21
328	32.80	84.96	1.71	1.71	19.95	125.15
329	32.90	90.22	2.01	2.01	19.83	126.27
330	33.00	92.64	2.26	2.26	19.92	127.22
331	33.10	99.42	2.42	2.42	19.15	127.90
332	33.20	111.27	2.49	2.49	17.53	128.54
333	33.30	126.51	2.64	2.64	16.04	129.37
334	33.40	140.69	3.00	3.00	15.34	130.27
335	33.50	145.55	3.29	3.29	15.40	130.94
336	33.60	143.14	3.38	3.38	15.86	131.19

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
337	33.70	138.85	3.35	3.35	16.19	131.15
338	33.80	138.32	3.29	3.29	16.25	131.01
339	33.90	139.02	3.23	3.23	16.26	130.93
340	34.00	137.10	3.26	3.26	16.50	130.83
341	34.10	131.72	3.20	3.20	17.05	130.71
342	34.20	126.79	3.17	3.17	17.71	130.51
343	34.30	121.80	3.13	3.13	18.33	130.32
344	34.40	118.10	3.07	3.07	18.74	130.11
345	34.50	116.34	2.98	2.98	18.86	129.88
346	34.60	115.59	2.90	2.90	18.72	129.69
347	34.70	116.33	2.86	2.86	18.51	129.57
348	34.80	117.22	2.83	2.83	18.43	129.45
349	34.90	114.57	2.77	2.77	18.67	129.19
350	35.00	107.70	2.62	2.62	19.39	128.73
351	35.10	98.96	2.48	2.48	20.74	128.16
352	35.20	88.31	2.39	2.39	22.75	127.59
353	35.30	77.62	2.31	2.31	25.09	126.86
354	35.40	68.31	2.07	2.07	26.62	125.99
355	35.50	65.97	1.83	1.83	26.31	125.20
356	35.60	70.57	1.74	1.74	24.53	124.81
357	35.70	76.50	1.71	1.71	22.78	124.90
358	35.80	80.96	1.78	1.78	21.81	125.25
359	35.90	83.75	1.89	1.89	21.57	125.80
360	36.00	86.58	2.05	2.05	21.60	126.46
361	36.10	90.50	2.24	2.24	21.67	127.25
362	36.20	95.49	2.50	2.50	21.83	128.14
363	36.30	99.63	2.81	2.81	22.21	129.01
364	36.40	101.57	3.09	3.09	22.85	129.63
365	36.50	99.95	3.20	3.20	23.67	130.01
366	36.60	97.99	3.31	3.31	24.68	130.27
367	36.70	96.11	3.50	3.50	26.05	130.50
368	36.80	90.93	3.63	3.63	28.02	130.53
369	36.90	81.16	3.56	3.56	30.87	130.25
370	37.00	69.87	3.46	3.46	34.83	129.70
371	37.10	58.29	3.34	3.34	39.61	128.94
372	37.20	48.52	3.08	3.08	43.73	128.03
373	37.30	44.82	2.76	2.76	45.21	126.97
374	37.40	44.66	2.36	2.36	43.04	125.94
375	37.50	47.56	2.02	2.02	38.39	125.08
376	37.60	54.34	1.82	1.82	33.54	124.67
377	37.70	61.44	1.82	1.82	30.07	124.86
378	37.80	66.90	1.95	1.95	28.27	125.41
379	37.90	71.00	2.09	2.09	27.04	125.94
380	38.00	75.80	2.11	2.11	25.38	126.18
381	38.10	82.21	2.02	2.02	23.14	126.14
382	38.20	89.04	1.90	1.90	21.04	126.13
383	38.30	95.54	1.95	1.95	19.96	126.37
384	38.40	97.51	2.10	2.10	19.95	126.78

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
385	38.50	96.01	2.19	2.19	20.66	127.03
386	38.60	92.05	2.19	2.19	21.58	126.91
387	38.70	86.37	2.09	2.09	22.47	126.54
388	38.80	81.79	1.98	1.98	23.16	126.06
389	38.90	79.22	1.90	1.90	23.37	125.63
390	39.00	78.86	1.80	1.80	22.83	125.20
391	39.10	80.81	1.66	1.66	21.69	124.73
392	39.20	83.20	1.54	1.54	21.08	124.40
393	39.30	80.09	1.57	1.57	22.26	124.18
394	39.40	67.79	1.60	1.60	25.80	124.11
395	39.50	56.06	1.70	1.70	31.67	123.72
396	39.60	42.81	1.63	1.63	39.21	122.92
397	39.70	31.60	1.47	1.47	48.62	121.25
398	39.80	21.76	1.13	1.13	57.06	119.38
399	39.90	20.05	0.99	0.99	56.18	119.96
400	40.00	35.20	1.71	1.71	53.24	121.06
401	40.10	31.33	1.58	1.58	56.06	120.12
402	40.20	11.47	0.61	0.61	68.69	116.38
403	40.30	8.83	0.49	0.49	88.64	112.26
404	40.40	11.74	0.69	0.69	85.88	113.34
405	40.50	14.26	0.83	0.83	75.88	115.57
406	40.60	18.46	1.00	1.00	65.83	117.48
407	40.70	24.66	1.17	1.17	56.61	119.14
408	40.80	30.75	1.29	1.29	49.72	120.42
409	40.90	35.57	1.38	1.38	45.74	121.13
410	41.00	36.72	1.39	1.39	44.37	121.20
411	41.10	34.52	1.28	1.28	44.31	121.01
412	41.20	34.77	1.29	1.29	44.25	121.05
413	41.30	37.22	1.41	1.41	43.46	121.86
414	41.40	41.26	1.66	1.66	43.78	122.83
415	41.50	39.99	1.83	1.83	45.54	123.67
416	41.60	37.91	1.99	1.99	48.74	124.23
417	41.70	36.72	2.17	2.17	50.98	124.69
418	41.80	37.46	2.28	2.28	49.47	125.39
419	41.90	46.22	2.46	2.46	42.02	126.55
420	42.00	68.41	2.76	2.76	32.44	127.63
421	42.10	92.84	2.62	2.62	23.73	128.36
422	42.20	122.77	2.42	2.42	17.65	128.75
423	42.30	149.87	2.52	2.52	14.21	129.40
424	42.40	169.09	2.82	2.82	12.71	130.45
425	42.50	186.52	3.22	3.22	12.20	131.52
426	42.60	197.52	3.58	3.58	12.18	132.32
427	42.70	197.98	3.75	3.75	12.56	132.66
428	42.80	187.91	3.72	3.72	13.31	132.54
429	42.90	172.76	3.56	3.56	14.39	132.13
430	43.00	157.50	3.41	3.41	15.79	131.61
431	43.10	141.29	3.29	3.29	17.53	131.08
432	43.20	125.70	3.18	3.18	19.72	130.71

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
433	43.30	113.88	3.28	3.28	22.40	130.68
434	43.40	104.92	3.57	3.57	25.54	130.98
435	43.50	96.55	3.92	3.92	28.57	131.22
436	43.60	89.34	3.94	3.94	30.91	130.72
437	43.70	77.67	3.18	3.18	31.27	129.73
438	43.80	79.25	2.75	2.75	29.06	128.74
439	43.90	91.29	2.66	2.66	25.45	128.50
440	44.00	104.05	2.63	2.63	22.25	128.66
441	44.10	114.13	2.61	2.61	20.19	128.75
442	44.20	117.55	2.54	2.54	19.46	128.99
443	44.30	118.63	2.78	2.78	20.57	129.67
444	44.40	113.54	3.38	3.38	23.32	130.60
445	44.50	102.81	3.86	3.86	26.83	131.11
446	44.60	91.24	3.80	3.80	29.42	130.81
447	44.70	85.19	3.29	3.29	29.13	130.03
448	44.80	92.79	2.88	2.88	25.57	129.41
449	44.90	112.45	2.76	2.76	21.11	129.40
450	45.00	133.95	2.84	2.84	17.96	129.99
451	45.10	150.30	3.12	3.12	16.60	130.87
452	45.20	157.91	3.52	3.52	16.52	131.67
453	45.30	157.87	3.76	3.76	17.11	132.16
454	45.40	152.89	3.82	3.82	18.08	132.30
455	45.50	143.70	3.84	3.84	19.53	132.21
456	45.60	130.56	3.85	3.85	21.82	132.09
457	45.70	115.53	3.98	3.98	24.98	131.94
458	45.80	100.63	4.07	4.07	28.47	131.61
459	45.90	88.36	3.83	3.83	31.26	130.84
460	46.00	79.14	3.26	3.26	32.45	129.58
461	46.10	73.45	2.64	2.64	31.70	128.15
462	46.20	74.28	2.26	2.26	29.33	126.98
463	46.30	80.05	2.05	2.05	25.82	126.39
464	46.40	91.55	1.94	1.94	21.76	126.28
465	46.50	109.27	1.90	1.90	17.79	126.53
466	46.60	130.77	1.93	1.93	15.07	127.27
467	46.70	148.04	2.23	2.23	14.30	128.53
468	46.80	153.23	2.79	2.79	15.28	129.97
469	46.90	148.15	3.32	3.32	17.36	131.18
470	47.00	140.81	3.78	3.78	19.70	132.11
471	47.10	137.41	4.26	4.26	21.50	132.72
472	47.20	135.96	4.43	4.43	22.28	132.94
473	47.30	135.33	4.23	4.23	21.86	132.80
474	47.40	140.26	3.98	3.98	20.40	132.54
475	47.50	151.98	3.84	3.84	18.46	132.45
476	47.60	166.12	3.80	3.80	16.78	132.65
477	47.70	179.12	3.99	3.99	15.75	133.07
478	47.80	188.27	4.24	4.24	15.32	133.57
479	47.90	193.48	4.44	4.44	15.10	133.89
480	48.00	196.13	4.43	4.43	14.88	134.02

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
481	48.10	198.96	4.39	4.39	14.56	134.01
482	48.20	202.27	4.36	4.36	14.25	134.03
483	48.30	205.66	4.39	4.39	14.06	134.08
484	48.40	206.79	4.43	4.43	14.12	134.20
485	48.50	205.41	4.55	4.55	14.44	134.35
486	48.60	202.79	4.68	4.68	14.86	134.46
487	48.70	199.77	4.69	4.69	15.15	134.50
488	48.80	199.67	4.68	4.68	15.19	134.49
489	48.90	201.72	4.67	4.67	14.99	134.48
490	49.00	204.99	4.63	4.63	14.71	134.50
491	49.10	208.60	4.65	4.65	14.44	134.58
492	49.20	212.60	4.74	4.74	14.25	134.73
493	49.30	216.89	4.83	4.83	14.04	134.91
494	49.40	222.43	4.90	4.90	13.86	135.08
495	49.50	225.67	4.98	4.98	13.86	135.10
496	49.60	218.36	4.87	4.87	14.13	134.86
497	49.70	204.49	4.56	4.56	14.47	134.51
498	49.80	202.28	4.48	4.48	14.70	134.37
499	49.90	206.77	4.68	4.68	14.74	134.44

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q _c :	Measured cone resistance (tsf)
f _s :	Sleeve friction resistance (tsf)
u:	Pore pressure (tsf)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (pcf)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1	0.10	0.01	0.00	0.01	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
2	0.20	0.01	0.00	0.01	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
3	0.30	0.01	0.00	0.01	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
4	0.40	0.02	0.00	0.02	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
5	0.50	0.02	0.00	0.02	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
6	0.60	0.03	0.00	0.03	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
7	0.70	0.04	0.00	0.04	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
8	0.80	0.04	0.00	0.04	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
9	0.90	0.05	0.00	0.05	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
10	1.00	0.05	0.00	0.05	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
11	1.10	0.06	0.00	0.06	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
12	1.20	0.07	0.00	0.07	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
13	1.30	0.07	0.00	0.07	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
14	1.40	0.08	0.00	0.08	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
15	1.50	0.08	0.00	0.08	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
16	1.60	0.09	0.00	0.09	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
17	1.70	0.10	0.00	0.10	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
18	1.80	0.10	0.00	0.10	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
19	1.90	0.11	0.00	0.11	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
20	2.00	0.11	0.00	0.11	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
21	2.10	0.12	0.00	0.12	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
22	2.20	0.13	0.00	0.13	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
23	2.30	0.13	0.00	0.13	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
24	2.40	0.14	0.00	0.14	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
25	2.50	0.15	0.00	0.15	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
26	2.60	0.15	0.00	0.15	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
27	2.70	0.16	0.00	0.16	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
28	2.80	0.16	0.00	0.16	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
29	2.90	0.17	0.00	0.17	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
30	3.00	0.17	0.00	0.17	0.99	0.479	1.06	0.453	1.00	1.30	2.000	No
31	3.10	0.18	0.00	0.18	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
32	3.20	0.19	0.00	0.19	0.99	0.478	1.06	0.453	1.00	1.30	2.000	Yes
33	3.30	0.19	0.00	0.19	0.99	0.478	1.06	0.453	1.00	1.30	2.000	Yes
34	3.40	0.20	0.00	0.20	0.99	0.478	1.06	0.453	1.00	1.30	2.000	Yes
35	3.50	0.20	0.00	0.20	0.99	0.478	1.06	0.452	1.00	1.30	2.000	Yes
36	3.60	0.21	0.00	0.21	0.99	0.478	1.06	0.452	1.00	1.30	2.000	Yes
37	3.70	0.22	0.00	0.22	0.99	0.478	1.06	0.452	1.00	1.30	2.000	Yes
38	3.80	0.22	0.00	0.22	0.99	0.478	1.06	0.452	1.00	1.30	2.000	Yes
39	3.90	0.23	0.00	0.23	0.99	0.478	1.06	0.452	1.00	1.30	2.000	Yes
40	4.00	0.23	0.00	0.23	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
41	4.10	0.24	0.00	0.24	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
42	4.20	0.24	0.00	0.24	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
43	4.30	0.25	0.00	0.25	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
44	4.40	0.25	0.00	0.25	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
45	4.50	0.26	0.00	0.26	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
46	4.60	0.26	0.00	0.26	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
47	4.70	0.27	0.00	0.27	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
48	4.80	0.27	0.00	0.27	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
49	4.90	0.28	0.00	0.28	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
50	5.00	0.28	0.00	0.28	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
51	5.10	0.29	0.00	0.29	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
52	5.20	0.29	0.00	0.29	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
53	5.30	0.30	0.00	0.30	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
54	5.40	0.30	0.00	0.30	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
55	5.50	0.31	0.00	0.31	0.99	0.476	1.06	0.450	1.00	1.30	2.000	Yes
56	5.60	0.31	0.00	0.31	0.99	0.476	1.06	0.450	1.00	1.30	2.000	Yes
57	5.70	0.32	0.00	0.32	0.99	0.476	1.06	0.450	1.00	1.30	2.000	Yes
58	5.80	0.33	0.00	0.33	0.99	0.475	1.06	0.450	1.00	1.30	2.000	Yes
59	5.90	0.33	0.00	0.33	0.99	0.475	1.06	0.450	1.00	1.30	2.000	Yes
60	6.00	0.34	0.00	0.34	0.99	0.475	1.06	0.450	1.00	1.30	2.000	Yes
61	6.10	0.34	0.00	0.34	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
62	6.20	0.35	0.00	0.35	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
63	6.30	0.35	0.00	0.35	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
64	6.40	0.36	0.00	0.36	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
65	6.50	0.37	0.00	0.37	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
66	6.60	0.37	0.00	0.37	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
67	6.70	0.38	0.00	0.38	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
68	6.80	0.38	0.00	0.38	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
69	6.90	0.39	0.00	0.39	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
70	7.00	0.40	0.00	0.40	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
71	7.10	0.40	0.00	0.40	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
72	7.20	0.41	0.00	0.41	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
73	7.30	0.41	0.00	0.41	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
74	7.40	0.42	0.00	0.42	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
75	7.50	0.42	0.00	0.42	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
76	7.60	0.43	0.00	0.43	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
77	7.70	0.44	0.00	0.44	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
78	7.80	0.44	0.00	0.44	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
79	7.90	0.45	0.00	0.45	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
80	8.00	0.45	0.00	0.45	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
81	8.10	0.46	0.00	0.46	0.98	0.476	1.06	0.451	1.00	1.30	2.000	Yes
82	8.20	0.47	0.01	0.46	0.98	0.479	1.06	0.454	1.00	1.30	2.000	Yes
83	8.30	0.47	0.01	0.46	0.98	0.482	1.06	0.457	1.00	1.30	2.000	Yes
84	8.40	0.48	0.01	0.46	0.98	0.485	1.06	0.459	1.00	1.30	2.000	Yes
85	8.50	0.48	0.02	0.47	0.98	0.488	1.06	0.462	1.00	1.30	2.000	Yes
86	8.60	0.49	0.02	0.47	0.98	0.491	1.06	0.465	1.00	1.30	2.000	Yes
87	8.70	0.50	0.02	0.47	0.98	0.494	1.06	0.468	1.00	1.30	2.000	Yes
88	8.80	0.50	0.02	0.48	0.98	0.497	1.06	0.470	1.00	1.30	2.000	Yes
89	8.90	0.51	0.03	0.48	0.98	0.500	1.06	0.473	1.00	1.30	2.000	Yes
90	9.00	0.51	0.03	0.48	0.98	0.503	1.06	0.476	1.00	1.30	0.618	No
91	9.10	0.52	0.03	0.48	0.98	0.505	1.06	0.478	1.00	1.30	0.622	No
92	9.20	0.52	0.04	0.49	0.98	0.508	1.06	0.481	1.00	1.30	0.625	No
93	9.30	0.53	0.04	0.49	0.98	0.511	1.06	0.484	1.00	1.30	0.629	No
94	9.40	0.53	0.04	0.49	0.98	0.514	1.06	0.486	1.00	1.30	0.632	No
95	9.50	0.54	0.05	0.49	0.98	0.516	1.06	0.489	1.00	1.30	0.635	No
96	9.60	0.55	0.05	0.50	0.98	0.519	1.06	0.491	1.00	1.30	0.638	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
97	9.70	0.55	0.05	0.50	0.98	0.521	1.06	0.494	1.00	1.30	0.642	No
98	9.80	0.56	0.06	0.50	0.98	0.524	1.06	0.496	1.00	1.30	0.645	No
99	9.90	0.56	0.06	0.50	0.98	0.527	1.06	0.498	1.00	1.30	0.648	No
100	10.00	0.57	0.06	0.51	0.98	0.529	1.06	0.501	1.00	1.30	0.651	No
101	10.10	0.57	0.07	0.51	0.98	0.532	1.06	0.503	1.00	1.30	0.654	No
102	10.20	0.58	0.07	0.51	0.98	0.534	1.06	0.505	1.00	1.30	0.657	No
103	10.30	0.59	0.07	0.51	0.98	0.536	1.06	0.508	1.00	1.30	0.660	No
104	10.40	0.59	0.07	0.52	0.98	0.539	1.06	0.510	1.00	1.30	0.663	No
105	10.50	0.60	0.08	0.52	0.98	0.541	1.06	0.512	1.00	1.30	2.000	Yes
106	10.60	0.60	0.08	0.52	0.98	0.543	1.06	0.514	1.00	1.30	2.000	Yes
107	10.70	0.61	0.08	0.52	0.98	0.546	1.06	0.517	1.00	1.30	2.000	Yes
108	10.80	0.61	0.09	0.53	0.98	0.548	1.06	0.519	1.00	1.30	2.000	Yes
109	10.90	0.62	0.09	0.53	0.98	0.550	1.06	0.521	1.00	1.30	2.000	Yes
110	11.00	0.63	0.09	0.53	0.98	0.552	1.06	0.523	1.00	1.30	2.000	Yes
111	11.10	0.63	0.10	0.54	0.98	0.555	1.06	0.525	1.00	1.30	2.000	Yes
112	11.20	0.64	0.10	0.54	0.98	0.557	1.06	0.527	1.00	1.30	2.000	Yes
113	11.30	0.65	0.10	0.54	0.98	0.559	1.06	0.529	1.00	1.30	2.000	Yes
114	11.40	0.65	0.11	0.55	0.98	0.561	1.06	0.531	1.00	1.30	0.690	No
115	11.50	0.66	0.11	0.55	0.98	0.563	1.06	0.533	1.00	1.30	0.693	No
116	11.60	0.66	0.11	0.55	0.98	0.565	1.06	0.535	1.00	1.30	0.695	No
117	11.70	0.67	0.12	0.55	0.98	0.567	1.06	0.537	1.00	1.30	0.698	No
118	11.80	0.68	0.12	0.56	0.98	0.569	1.06	0.539	1.00	1.30	0.700	No
119	11.90	0.68	0.12	0.56	0.98	0.571	1.06	0.540	1.00	1.30	0.702	No
120	12.00	0.69	0.12	0.56	0.97	0.573	1.06	0.542	1.00	1.30	0.705	No
121	12.10	0.69	0.13	0.57	0.97	0.575	1.06	0.544	1.00	1.30	0.707	No
122	12.20	0.70	0.13	0.57	0.97	0.577	1.06	0.546	1.00	1.30	0.710	No
123	12.30	0.71	0.13	0.57	0.97	0.578	1.06	0.548	1.00	1.30	0.712	No
124	12.40	0.71	0.14	0.58	0.97	0.580	1.06	0.549	1.00	1.30	0.714	No
125	12.50	0.72	0.14	0.58	0.97	0.582	1.06	0.551	1.00	1.30	0.716	No
126	12.60	0.72	0.14	0.58	0.97	0.584	1.06	0.553	1.00	1.30	0.719	No
127	12.70	0.73	0.15	0.58	0.97	0.586	1.06	0.555	1.00	1.30	2.000	Yes
128	12.80	0.74	0.15	0.59	0.97	0.588	1.06	0.556	1.00	1.30	2.000	Yes
129	12.90	0.74	0.15	0.59	0.97	0.589	1.06	0.558	1.00	1.30	2.000	Yes
130	13.00	0.75	0.16	0.59	0.97	0.591	1.06	0.560	1.00	1.30	2.000	Yes
131	13.10	0.75	0.16	0.60	0.97	0.593	1.06	0.561	1.00	1.30	2.000	Yes
132	13.20	0.76	0.16	0.60	0.97	0.595	1.06	0.563	1.00	1.30	2.000	Yes
133	13.30	0.77	0.17	0.60	0.97	0.596	1.06	0.564	1.00	1.30	2.000	Yes
134	13.40	0.77	0.17	0.60	0.97	0.598	1.06	0.566	1.00	1.30	2.000	Yes
135	13.50	0.78	0.17	0.61	0.97	0.600	1.06	0.568	1.00	1.30	0.738	No
136	13.60	0.78	0.17	0.61	0.97	0.601	1.06	0.569	1.00	1.30	0.740	No
137	13.70	0.79	0.18	0.61	0.97	0.603	1.06	0.571	1.00	1.30	0.742	No
138	13.80	0.80	0.18	0.61	0.97	0.605	1.06	0.572	1.00	1.30	0.744	No
139	13.90	0.80	0.18	0.62	0.97	0.606	1.06	0.574	1.00	1.30	0.746	No
140	14.00	0.81	0.19	0.62	0.97	0.608	1.06	0.575	1.00	1.30	0.748	No
141	14.10	0.81	0.19	0.62	0.97	0.609	1.06	0.577	1.00	1.30	0.750	No
142	14.20	0.82	0.19	0.63	0.97	0.611	1.06	0.578	1.00	1.30	0.752	No
143	14.30	0.82	0.20	0.63	0.97	0.613	1.06	0.580	1.00	1.30	0.754	No
144	14.40	0.83	0.20	0.63	0.97	0.614	1.06	0.582	1.00	1.30	0.756	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
145	14.50	0.84	0.20	0.63	0.97	0.616	1.06	0.583	1.00	1.30	0.758	No
146	14.60	0.84	0.21	0.63	0.97	0.618	1.06	0.585	1.00	1.30	0.760	No
147	14.70	0.84	0.21	0.64	0.97	0.619	1.06	0.586	1.00	1.30	0.762	No
148	14.80	0.85	0.21	0.64	0.97	0.621	1.06	0.588	1.00	1.30	0.764	No
149	14.90	0.85	0.22	0.64	0.97	0.623	1.06	0.590	1.00	1.30	0.767	No
150	15.00	0.86	0.22	0.64	0.97	0.625	1.06	0.591	1.00	1.30	0.769	No
151	15.10	0.86	0.22	0.64	0.97	0.626	1.06	0.593	1.00	1.30	0.771	No
152	15.20	0.87	0.22	0.64	0.97	0.628	1.06	0.595	1.00	1.30	0.773	No
153	15.30	0.87	0.23	0.64	0.97	0.630	1.06	0.596	1.00	1.30	0.775	No
154	15.40	0.88	0.23	0.65	0.97	0.632	1.06	0.598	1.00	1.30	0.777	No
155	15.50	0.88	0.23	0.65	0.97	0.633	1.06	0.600	1.00	1.30	0.779	No
156	15.60	0.89	0.24	0.65	0.97	0.635	1.06	0.601	1.00	1.30	0.781	No
157	15.70	0.89	0.24	0.65	0.97	0.636	1.06	0.603	1.00	1.30	0.783	No
158	15.80	0.90	0.24	0.65	0.97	0.638	1.06	0.604	1.00	1.30	0.785	No
159	15.90	0.90	0.25	0.66	0.97	0.639	1.06	0.605	1.00	1.30	0.787	No
160	16.00	0.91	0.25	0.66	0.97	0.641	1.06	0.607	1.00	1.30	0.788	No
161	16.10	0.91	0.25	0.66	0.97	0.642	1.06	0.608	1.00	1.30	0.790	No
162	16.20	0.92	0.26	0.66	0.97	0.644	1.06	0.609	1.00	1.30	0.792	No
163	16.30	0.93	0.26	0.67	0.97	0.645	1.06	0.611	1.00	1.30	0.794	No
164	16.40	0.93	0.26	0.67	0.97	0.646	1.06	0.612	1.00	1.30	0.796	No
165	16.50	0.94	0.27	0.67	0.97	0.648	1.06	0.613	1.00	1.30	0.797	No
166	16.60	0.94	0.27	0.67	0.97	0.649	1.06	0.615	1.00	1.30	0.799	No
167	16.70	0.95	0.27	0.67	0.96	0.651	1.06	0.616	1.00	1.30	0.801	No
168	16.80	0.95	0.27	0.68	0.96	0.652	1.06	0.618	1.00	1.30	0.803	No
169	16.90	0.96	0.28	0.68	0.96	0.654	1.06	0.619	1.00	1.30	0.805	No
170	17.00	0.96	0.28	0.68	0.96	0.655	1.06	0.620	1.00	1.30	0.806	No
171	17.10	0.97	0.28	0.68	0.96	0.657	1.06	0.622	1.00	1.30	0.808	No
172	17.20	0.97	0.29	0.68	0.96	0.658	1.06	0.623	1.00	1.30	0.810	No
173	17.30	0.98	0.29	0.68	0.96	0.660	1.06	0.625	1.00	1.30	0.812	No
174	17.40	0.98	0.29	0.69	0.96	0.661	1.06	0.626	1.00	1.30	0.814	No
175	17.50	0.98	0.30	0.69	0.96	0.663	1.06	0.627	1.00	1.30	0.815	No
176	17.60	0.99	0.30	0.69	0.96	0.664	1.06	0.629	1.00	1.30	0.817	No
177	17.70	1.00	0.30	0.69	0.96	0.665	1.06	0.630	1.00	1.30	0.819	No
178	17.80	1.00	0.31	0.69	0.96	0.667	1.06	0.631	1.00	1.30	0.820	No
179	17.90	1.01	0.31	0.70	0.96	0.668	1.06	0.632	1.00	1.30	0.822	No
180	18.00	1.01	0.31	0.70	0.96	0.669	1.06	0.634	1.00	1.30	0.824	No
181	18.10	1.02	0.32	0.70	0.96	0.671	1.06	0.635	1.00	1.30	0.825	No
182	18.20	1.02	0.32	0.70	0.96	0.672	1.06	0.636	1.00	1.30	0.827	No
183	18.30	1.03	0.32	0.70	0.96	0.673	1.06	0.637	1.00	1.30	0.828	No
184	18.40	1.03	0.32	0.71	0.96	0.674	1.06	0.638	1.00	1.30	0.830	No
185	18.50	1.04	0.33	0.71	0.96	0.675	1.06	0.639	1.00	1.30	0.831	No
186	18.60	1.04	0.33	0.71	0.96	0.676	1.06	0.640	1.00	1.30	0.832	No
187	18.70	1.05	0.33	0.72	0.96	0.677	1.06	0.641	1.00	1.30	0.833	No
188	18.80	1.06	0.34	0.72	0.96	0.678	1.06	0.642	1.00	1.30	0.835	No
189	18.90	1.06	0.34	0.72	0.96	0.679	1.06	0.643	1.00	1.30	0.836	No
190	19.00	1.07	0.34	0.72	0.96	0.680	1.06	0.644	1.00	1.30	0.837	No
191	19.10	1.07	0.35	0.73	0.96	0.681	1.06	0.645	1.00	1.30	0.838	No
192	19.20	1.08	0.35	0.73	0.96	0.682	1.06	0.646	1.00	1.30	0.840	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
193	19.30	1.08	0.35	0.73	0.96	0.683	1.06	0.647	1.00	1.30	0.841	No
194	19.40	1.09	0.36	0.73	0.96	0.684	1.06	0.648	1.00	1.30	0.842	No
195	19.50	1.10	0.36	0.74	0.96	0.685	1.06	0.648	1.00	1.30	0.843	No
196	19.60	1.10	0.36	0.74	0.96	0.686	1.06	0.649	1.00	1.30	0.844	No
197	19.70	1.11	0.37	0.74	0.96	0.687	1.06	0.650	1.00	1.30	0.845	No
198	19.80	1.11	0.37	0.75	0.96	0.688	1.06	0.651	1.00	1.30	2.000	Yes
199	19.90	1.12	0.37	0.75	0.96	0.688	1.06	0.652	1.00	1.30	2.000	Yes
200	20.00	1.13	0.37	0.75	0.96	0.689	1.06	0.652	1.00	1.30	2.000	Yes
201	20.10	1.13	0.38	0.76	0.96	0.690	1.06	0.653	1.00	1.30	2.000	Yes
202	20.20	1.14	0.38	0.76	0.96	0.691	1.06	0.654	1.00	1.30	2.000	Yes
203	20.30	1.15	0.38	0.76	0.96	0.692	1.06	0.655	1.00	1.30	2.000	Yes
204	20.40	1.15	0.39	0.76	0.96	0.692	1.06	0.656	1.00	1.30	2.000	Yes
205	20.50	1.16	0.39	0.77	0.96	0.693	1.06	0.656	1.00	1.30	2.000	Yes
206	20.60	1.16	0.39	0.77	0.96	0.694	1.06	0.657	1.00	1.30	2.000	Yes
207	20.70	1.17	0.40	0.77	0.96	0.695	1.06	0.658	1.00	1.30	2.000	Yes
208	20.80	1.18	0.40	0.78	0.95	0.696	1.06	0.659	1.00	1.30	2.000	Yes
209	20.90	1.18	0.40	0.78	0.95	0.696	1.06	0.659	1.00	1.30	2.000	Yes
210	21.00	1.19	0.41	0.78	0.95	0.697	1.06	0.660	1.00	1.30	2.000	Yes
211	21.10	1.19	0.41	0.78	0.95	0.698	1.06	0.661	1.00	1.30	2.000	Yes
212	21.20	1.20	0.41	0.79	0.95	0.699	1.06	0.661	1.00	1.30	2.000	Yes
213	21.30	1.21	0.41	0.79	0.95	0.699	1.06	0.662	1.00	1.30	0.861	No
214	21.40	1.21	0.42	0.79	0.95	0.700	1.06	0.663	1.00	1.30	0.862	No
215	21.50	1.22	0.42	0.80	0.95	0.701	1.06	0.664	1.00	1.30	0.863	No
216	21.60	1.22	0.42	0.80	0.95	0.702	1.06	0.664	1.00	1.30	0.864	No
217	21.70	1.23	0.43	0.80	0.95	0.702	1.06	0.665	1.00	1.30	0.864	No
218	21.80	1.23	0.43	0.80	0.95	0.703	1.06	0.666	1.00	1.30	0.865	No
219	21.90	1.24	0.43	0.81	0.95	0.704	1.06	0.666	1.00	1.30	0.866	No
220	22.00	1.25	0.44	0.81	0.95	0.705	1.06	0.667	1.00	1.30	0.867	No
221	22.10	1.25	0.44	0.81	0.95	0.705	1.06	0.668	1.00	1.30	0.868	No
222	22.20	1.26	0.44	0.81	0.95	0.706	1.06	0.668	1.00	1.30	0.869	No
223	22.30	1.26	0.45	0.82	0.95	0.707	1.06	0.669	1.00	1.30	0.870	No
224	22.40	1.27	0.45	0.82	0.95	0.707	1.06	0.670	1.00	1.30	0.871	No
225	22.50	1.28	0.45	0.82	0.95	0.708	1.06	0.670	1.00	1.30	0.871	No
226	22.60	1.28	0.46	0.83	0.95	0.709	1.06	0.671	1.00	1.30	0.872	No
227	22.70	1.29	0.46	0.83	0.95	0.709	1.06	0.672	1.00	1.30	0.873	No
228	22.80	1.29	0.46	0.83	0.95	0.710	1.06	0.672	1.00	1.30	0.874	No
229	22.90	1.30	0.46	0.83	0.95	0.711	1.06	0.673	1.00	1.30	0.874	No
230	23.00	1.31	0.47	0.84	0.95	0.711	1.06	0.673	1.00	1.30	0.875	No
231	23.10	1.31	0.47	0.84	0.95	0.712	1.06	0.674	1.00	1.30	0.876	No
232	23.20	1.32	0.47	0.84	0.95	0.712	1.06	0.674	1.00	1.30	0.877	No
233	23.30	1.32	0.48	0.85	0.95	0.713	1.06	0.675	1.00	1.30	0.877	No
234	23.40	1.33	0.48	0.85	0.95	0.714	1.06	0.675	1.00	1.30	0.878	No
235	23.50	1.34	0.48	0.85	0.95	0.714	1.06	0.676	1.00	1.30	0.879	No
236	23.60	1.34	0.49	0.85	0.95	0.715	1.06	0.677	1.00	1.30	0.880	No
237	23.70	1.35	0.49	0.86	0.95	0.715	1.06	0.677	1.00	1.30	0.880	No
238	23.80	1.35	0.49	0.86	0.95	0.716	1.06	0.678	1.00	1.30	0.881	No
239	23.90	1.36	0.50	0.86	0.95	0.716	1.06	0.678	1.00	1.30	0.882	No
240	24.00	1.36	0.50	0.86	0.95	0.717	1.06	0.679	1.00	1.30	0.882	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
241	24.10	1.37	0.50	0.87	0.94	0.718	1.06	0.679	1.00	1.30	0.883	No
242	24.20	1.38	0.51	0.87	0.94	0.718	1.06	0.680	1.00	1.30	0.884	No
243	24.30	1.38	0.51	0.87	0.94	0.719	1.06	0.681	1.00	1.30	0.885	No
244	24.40	1.39	0.51	0.87	0.94	0.720	1.06	0.681	1.00	1.30	0.886	No
245	24.50	1.39	0.51	0.88	0.94	0.720	1.06	0.682	1.00	1.30	0.887	No
246	24.60	1.40	0.52	0.88	0.94	0.721	1.06	0.683	1.00	1.30	0.887	No
247	24.70	1.40	0.52	0.88	0.94	0.722	1.06	0.683	1.00	1.30	0.888	No
248	24.80	1.41	0.52	0.88	0.94	0.723	1.06	0.684	1.00	1.30	0.889	No
249	24.90	1.41	0.53	0.89	0.94	0.723	1.06	0.685	1.00	1.30	0.890	No
250	25.00	1.42	0.53	0.89	0.94	0.724	1.06	0.685	1.00	1.30	0.891	No
251	25.10	1.42	0.53	0.89	0.94	0.724	1.06	0.686	1.00	1.30	0.892	No
252	25.20	1.43	0.54	0.89	0.94	0.725	1.06	0.686	1.00	1.30	0.892	No
253	25.30	1.43	0.54	0.89	0.94	0.726	1.06	0.687	1.00	1.30	0.893	No
254	25.40	1.44	0.54	0.90	0.94	0.726	1.06	0.688	1.00	1.30	0.894	No
255	25.50	1.44	0.55	0.90	0.94	0.727	1.06	0.688	1.00	1.30	0.895	No
256	25.60	1.45	0.55	0.90	0.94	0.728	1.06	0.689	1.00	1.30	0.895	No
257	25.70	1.46	0.55	0.90	0.94	0.728	1.06	0.689	1.00	1.30	0.896	No
258	25.80	1.46	0.56	0.91	0.94	0.729	1.06	0.690	1.00	1.30	0.897	No
259	25.90	1.47	0.56	0.91	0.94	0.729	1.06	0.690	1.00	1.30	0.898	No
260	26.00	1.47	0.56	0.91	0.94	0.730	1.06	0.691	1.00	1.30	0.898	No
261	26.10	1.48	0.56	0.91	0.94	0.731	1.06	0.692	1.00	1.30	0.899	No
262	26.20	1.48	0.57	0.91	0.94	0.731	1.06	0.692	1.00	1.30	0.900	No
263	26.30	1.49	0.57	0.92	0.94	0.732	1.06	0.693	1.00	1.30	0.900	No
264	26.40	1.49	0.57	0.92	0.94	0.732	1.06	0.693	1.00	1.30	0.901	No
265	26.50	1.50	0.58	0.92	0.94	0.733	1.06	0.694	1.00	1.30	0.902	No
266	26.60	1.50	0.58	0.92	0.94	0.733	1.06	0.694	1.00	1.30	0.903	No
267	26.70	1.51	0.58	0.92	0.94	0.734	1.06	0.695	1.00	1.30	0.903	No
268	26.80	1.51	0.59	0.93	0.94	0.734	1.06	0.695	1.00	1.30	0.904	No
269	26.90	1.52	0.59	0.93	0.93	0.735	1.06	0.696	1.00	1.30	0.904	No
270	27.00	1.52	0.59	0.93	0.93	0.735	1.06	0.696	1.00	1.30	0.905	No
271	27.10	1.53	0.60	0.93	0.93	0.736	1.06	0.697	1.00	1.30	0.905	No
272	27.20	1.54	0.60	0.94	0.93	0.736	1.06	0.697	1.00	1.30	0.906	No
273	27.30	1.54	0.60	0.94	0.93	0.737	1.06	0.697	1.00	1.30	0.906	No
274	27.40	1.55	0.61	0.94	0.93	0.737	1.06	0.698	1.00	1.30	0.907	No
275	27.50	1.55	0.61	0.94	0.93	0.737	1.06	0.698	1.00	1.30	0.907	No
276	27.60	1.56	0.61	0.95	0.93	0.737	1.06	0.698	1.00	1.30	0.907	No
277	27.70	1.57	0.61	0.95	0.93	0.738	1.06	0.698	1.00	1.30	0.908	No
278	27.80	1.57	0.62	0.95	0.93	0.738	1.06	0.698	1.00	1.30	0.908	No
279	27.90	1.58	0.62	0.96	0.93	0.738	1.06	0.698	1.00	1.30	0.908	No
280	28.00	1.58	0.62	0.96	0.93	0.738	1.06	0.699	1.00	1.30	0.908	No
281	28.10	1.59	0.63	0.96	0.93	0.738	1.06	0.699	1.00	1.30	0.909	No
282	28.20	1.60	0.63	0.97	0.93	0.738	1.06	0.699	1.00	1.30	0.909	No
283	28.30	1.60	0.63	0.97	0.93	0.739	1.06	0.699	1.00	1.30	0.909	No
284	28.40	1.61	0.64	0.97	0.93	0.739	1.06	0.700	1.00	1.30	0.909	No
285	28.50	1.61	0.64	0.97	0.93	0.739	1.06	0.700	1.00	1.30	0.910	No
286	28.60	1.62	0.64	0.98	0.93	0.740	1.06	0.700	1.00	1.30	0.910	No
287	28.70	1.63	0.65	0.98	0.93	0.740	1.06	0.700	1.00	1.30	0.910	No
288	28.80	1.63	0.65	0.98	0.93	0.740	1.06	0.700	1.00	1.30	0.911	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
289	28.90	1.64	0.65	0.99	0.93	0.740	1.06	0.701	1.00	1.30	0.911	No
290	29.00	1.64	0.66	0.99	0.93	0.740	1.06	0.701	1.00	1.30	0.911	No
291	29.10	1.65	0.66	0.99	0.92	0.740	1.06	0.701	1.00	1.30	0.911	No
292	29.20	1.66	0.66	0.99	0.92	0.741	1.06	0.701	1.00	1.30	0.911	No
293	29.30	1.66	0.66	1.00	0.92	0.741	1.06	0.701	1.00	1.30	0.912	No
294	29.40	1.67	0.67	1.00	0.92	0.741	1.06	0.702	1.00	1.30	0.912	No
295	29.50	1.67	0.67	1.00	0.92	0.741	1.06	0.702	1.00	1.30	0.912	No
296	29.60	1.68	0.67	1.00	0.92	0.741	1.06	0.702	1.00	1.30	0.912	No
297	29.70	1.68	0.68	1.01	0.92	0.741	1.06	0.702	1.00	1.30	0.912	No
298	29.80	1.69	0.68	1.01	0.92	0.742	1.06	0.702	1.00	1.30	0.913	No
299	29.90	1.70	0.68	1.01	0.92	0.742	1.06	0.702	1.00	1.30	2.000	Yes
300	30.00	1.70	0.69	1.02	0.92	0.742	1.06	0.702	1.00	1.30	2.000	Yes
301	30.10	1.71	0.69	1.02	0.92	0.742	1.06	0.702	1.00	1.30	2.000	Yes
302	30.20	1.72	0.69	1.02	0.92	0.742	1.06	0.702	1.00	1.30	2.000	Yes
303	30.30	1.72	0.70	1.03	0.92	0.742	1.06	0.702	1.00	1.30	2.000	Yes
304	30.40	1.73	0.70	1.03	0.92	0.741	1.06	0.702	1.00	1.30	2.000	Yes
305	30.50	1.74	0.70	1.03	0.92	0.741	1.06	0.702	1.00	1.30	2.000	Yes
306	30.60	1.74	0.71	1.04	0.92	0.741	1.06	0.702	1.00	1.30	2.000	Yes
307	30.70	1.75	0.71	1.04	0.92	0.741	1.06	0.702	1.00	1.30	2.000	Yes
308	30.80	1.76	0.71	1.04	0.92	0.741	1.06	0.702	1.00	1.30	2.000	Yes
309	30.90	1.76	0.71	1.05	0.92	0.741	1.06	0.702	1.00	1.30	2.000	Yes
310	31.00	1.77	0.72	1.05	0.92	0.741	1.06	0.702	1.00	1.30	2.000	Yes
311	31.10	1.77	0.72	1.05	0.91	0.741	1.06	0.701	1.00	1.30	2.000	Yes
312	31.20	1.78	0.72	1.06	0.91	0.741	1.06	0.701	1.00	1.30	2.000	Yes
313	31.30	1.79	0.73	1.06	0.91	0.741	1.06	0.701	1.00	1.30	2.000	Yes
314	31.40	1.79	0.73	1.06	0.91	0.741	1.06	0.701	1.00	1.30	2.000	Yes
315	31.50	1.80	0.73	1.07	0.91	0.741	1.06	0.701	1.00	1.30	0.912	No
316	31.60	1.81	0.74	1.07	0.91	0.741	1.06	0.701	1.00	1.30	0.912	No
317	31.70	1.81	0.74	1.07	0.91	0.741	1.06	0.701	1.00	1.30	0.912	No
318	31.80	1.82	0.74	1.08	0.91	0.741	1.06	0.701	1.00	1.30	2.000	Yes
319	31.90	1.82	0.75	1.08	0.91	0.741	1.06	0.701	1.00	1.30	2.000	Yes
320	32.00	1.83	0.75	1.08	0.91	0.740	1.06	0.701	1.00	1.30	2.000	Yes
321	32.10	1.84	0.75	1.09	0.91	0.740	1.06	0.701	1.00	1.30	2.000	Yes
322	32.20	1.84	0.76	1.09	0.91	0.740	1.06	0.701	1.00	1.30	2.000	Yes
323	32.30	1.85	0.76	1.09	0.91	0.740	1.06	0.701	1.00	1.30	2.000	Yes
324	32.40	1.86	0.76	1.09	0.91	0.740	1.06	0.701	1.00	1.30	2.000	Yes
325	32.50	1.86	0.76	1.10	0.91	0.740	1.06	0.700	1.00	1.30	0.911	No
326	32.60	1.87	0.77	1.10	0.91	0.740	1.06	0.700	1.00	1.30	0.910	No
327	32.70	1.87	0.77	1.10	0.91	0.740	1.06	0.700	1.00	1.30	0.910	No
328	32.80	1.88	0.77	1.11	0.90	0.740	1.06	0.700	1.00	1.30	0.910	No
329	32.90	1.89	0.78	1.11	0.90	0.739	1.06	0.700	1.00	1.30	0.910	No
330	33.00	1.89	0.78	1.11	0.90	0.739	1.06	0.700	1.00	1.30	0.910	No
331	33.10	1.90	0.78	1.12	0.90	0.739	1.06	0.700	1.00	1.30	0.909	No
332	33.20	1.91	0.79	1.12	0.90	0.739	1.06	0.699	1.00	1.30	0.909	No
333	33.30	1.91	0.79	1.12	0.90	0.739	1.06	0.699	1.00	1.30	0.909	No
334	33.40	1.92	0.79	1.13	0.90	0.738	1.06	0.699	1.00	1.30	0.909	No
335	33.50	1.93	0.80	1.13	0.90	0.738	1.06	0.699	1.00	1.30	0.908	No
336	33.60	1.93	0.80	1.13	0.90	0.738	1.06	0.699	1.00	1.30	0.908	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
337	33.70	1.94	0.80	1.14	0.90	0.738	1.06	0.698	1.00	1.30	0.908	No
338	33.80	1.95	0.80	1.14	0.90	0.737	1.06	0.698	1.00	1.30	0.907	No
339	33.90	1.95	0.81	1.14	0.90	0.737	1.06	0.698	1.00	1.30	0.907	No
340	34.00	1.96	0.81	1.15	0.90	0.737	1.06	0.697	1.00	1.30	0.907	No
341	34.10	1.97	0.81	1.15	0.90	0.737	1.06	0.697	1.00	1.30	0.906	No
342	34.20	1.97	0.82	1.15	0.90	0.736	1.06	0.697	1.00	1.30	0.906	No
343	34.30	1.98	0.82	1.16	0.90	0.736	1.06	0.697	1.00	1.30	0.906	No
344	34.40	1.98	0.82	1.16	0.89	0.736	1.06	0.696	1.00	1.30	0.905	No
345	34.50	1.99	0.83	1.16	0.89	0.735	1.06	0.696	1.00	1.30	0.905	No
346	34.60	2.00	0.83	1.17	0.89	0.735	1.06	0.696	1.00	1.30	0.905	No
347	34.70	2.00	0.83	1.17	0.89	0.735	1.06	0.696	1.00	1.30	0.904	No
348	34.80	2.01	0.84	1.17	0.89	0.735	1.06	0.695	1.00	1.30	0.904	No
349	34.90	2.02	0.84	1.18	0.89	0.734	1.06	0.695	1.00	1.30	0.904	No
350	35.00	2.02	0.84	1.18	0.89	0.734	1.06	0.695	1.00	1.30	0.903	No
351	35.10	2.03	0.85	1.18	0.89	0.734	1.06	0.694	1.00	1.30	0.903	No
352	35.20	2.04	0.85	1.19	0.89	0.733	1.06	0.694	1.00	1.30	0.902	No
353	35.30	2.04	0.85	1.19	0.89	0.733	1.06	0.694	1.00	1.30	0.902	No
354	35.40	2.05	0.85	1.19	0.89	0.733	1.06	0.694	1.00	1.30	0.902	No
355	35.50	2.06	0.86	1.20	0.89	0.732	1.06	0.693	1.00	1.30	0.901	No
356	35.60	2.06	0.86	1.20	0.89	0.732	1.06	0.693	1.00	1.30	0.901	No
357	35.70	2.07	0.86	1.20	0.89	0.732	1.06	0.693	1.00	1.30	0.901	No
358	35.80	2.07	0.87	1.21	0.88	0.732	1.06	0.693	1.00	1.30	0.900	No
359	35.90	2.08	0.87	1.21	0.88	0.731	1.06	0.692	1.00	1.30	0.900	No
360	36.00	2.09	0.87	1.21	0.88	0.731	1.06	0.692	1.00	1.30	0.900	No
361	36.10	2.09	0.88	1.22	0.88	0.731	1.06	0.692	1.00	1.30	0.899	No
362	36.20	2.10	0.88	1.22	0.88	0.730	1.06	0.691	1.00	1.30	0.899	No
363	36.30	2.11	0.88	1.22	0.88	0.730	1.06	0.691	1.00	1.30	0.898	No
364	36.40	2.11	0.89	1.23	0.88	0.730	1.06	0.691	1.00	1.30	0.898	No
365	36.50	2.12	0.89	1.23	0.88	0.729	1.06	0.690	1.00	1.30	0.897	No
366	36.60	2.13	0.89	1.23	0.88	0.729	1.06	0.690	1.00	1.30	2.000	Yes
367	36.70	2.13	0.90	1.24	0.88	0.728	1.06	0.689	1.00	1.30	2.000	Yes
368	36.80	2.14	0.90	1.24	0.88	0.728	1.06	0.689	1.00	1.30	2.000	Yes
369	36.90	2.14	0.90	1.24	0.88	0.728	1.06	0.689	1.00	1.30	2.000	Yes
370	37.00	2.15	0.90	1.25	0.88	0.727	1.06	0.688	1.00	1.30	2.000	Yes
371	37.10	2.16	0.91	1.25	0.88	0.727	1.06	0.688	1.00	1.30	2.000	Yes
372	37.20	2.16	0.91	1.25	0.87	0.726	1.06	0.688	1.00	1.30	2.000	Yes
373	37.30	2.17	0.91	1.26	0.87	0.726	1.06	0.687	1.00	1.30	0.893	No
374	37.40	2.18	0.92	1.26	0.87	0.726	1.06	0.687	1.00	1.30	0.893	No
375	37.50	2.18	0.92	1.26	0.87	0.725	1.06	0.686	1.00	1.30	0.892	No
376	37.60	2.19	0.92	1.27	0.87	0.725	1.06	0.686	1.00	1.30	0.892	No
377	37.70	2.20	0.93	1.27	0.87	0.724	1.06	0.686	1.00	1.30	0.891	No
378	37.80	2.20	0.93	1.27	0.87	0.724	1.06	0.685	1.00	1.30	0.891	No
379	37.90	2.21	0.93	1.28	0.87	0.724	1.06	0.685	1.00	1.30	0.890	No
380	38.00	2.21	0.94	1.28	0.87	0.723	1.06	0.685	1.00	1.30	0.890	No
381	38.10	2.22	0.94	1.28	0.87	0.723	1.06	0.684	1.00	1.30	0.889	No
382	38.20	2.23	0.94	1.28	0.87	0.722	1.06	0.684	1.00	1.30	0.889	No
383	38.30	2.23	0.95	1.29	0.87	0.722	1.06	0.683	1.00	1.30	0.888	No
384	38.40	2.24	0.95	1.29	0.86	0.721	1.06	0.683	1.00	1.30	0.888	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
385	38.50	2.25	0.95	1.29	0.86	0.721	1.06	0.683	1.00	1.30	0.887	No
386	38.60	2.25	0.95	1.30	0.86	0.721	1.06	0.682	1.00	1.30	0.887	No
387	38.70	2.26	0.96	1.30	0.86	0.720	1.06	0.682	1.00	1.30	0.886	No
388	38.80	2.27	0.96	1.30	0.86	0.720	1.06	0.681	1.00	1.30	0.886	No
389	38.90	2.27	0.96	1.31	0.86	0.719	1.06	0.681	1.00	1.30	0.885	No
390	39.00	2.28	0.97	1.31	0.86	0.719	1.06	0.680	1.00	1.30	0.884	No
391	39.10	2.28	0.97	1.31	0.86	0.718	1.06	0.680	1.00	1.30	0.884	No
392	39.20	2.29	0.97	1.32	0.86	0.718	1.06	0.680	1.00	1.30	2.000	Yes
393	39.30	2.30	0.98	1.32	0.86	0.717	1.06	0.679	1.00	1.30	2.000	Yes
394	39.40	2.30	0.98	1.32	0.86	0.717	1.06	0.679	1.00	1.30	2.000	Yes
395	39.50	2.31	0.98	1.33	0.86	0.716	1.06	0.678	1.00	1.30	2.000	Yes
396	39.60	2.31	0.99	1.33	0.85	0.716	1.06	0.678	1.00	1.30	2.000	Yes
397	39.70	2.32	0.99	1.33	0.85	0.716	1.06	0.677	1.00	1.30	2.000	Yes
398	39.80	2.33	0.99	1.33	0.85	0.715	1.06	0.677	1.00	1.30	2.000	Yes
399	39.90	2.33	1.00	1.34	0.85	0.715	1.06	0.677	1.00	1.30	0.880	No
400	40.00	2.34	1.00	1.34	0.85	0.714	1.06	0.676	1.00	1.30	0.879	No
401	40.10	2.34	1.00	1.34	0.85	0.714	1.06	0.676	1.00	1.30	0.878	No
402	40.20	2.35	1.00	1.35	0.85	0.713	1.06	0.675	1.00	1.30	0.878	No
403	40.30	2.36	1.01	1.35	0.85	0.713	1.06	0.675	1.00	1.30	0.877	No
404	40.40	2.36	1.01	1.35	0.85	0.713	1.06	0.675	1.00	1.30	0.877	No
405	40.50	2.37	1.01	1.35	0.85	0.712	1.06	0.674	1.00	1.30	0.876	No
406	40.60	2.37	1.02	1.36	0.85	0.712	1.06	0.674	1.00	1.30	0.876	No
407	40.70	2.38	1.02	1.36	0.84	0.711	1.06	0.673	1.00	1.30	0.875	No
408	40.80	2.39	1.02	1.36	0.84	0.711	1.06	0.673	1.00	1.30	0.875	No
409	40.90	2.39	1.03	1.37	0.84	0.710	1.06	0.672	1.00	1.30	0.874	No
410	41.00	2.40	1.03	1.37	0.84	0.710	1.06	0.672	1.00	1.30	0.874	No
411	41.10	2.40	1.03	1.37	0.84	0.709	1.06	0.672	1.00	1.30	0.873	No
412	41.20	2.41	1.04	1.37	0.84	0.709	1.06	0.671	1.00	1.30	0.872	No
413	41.30	2.42	1.04	1.38	0.84	0.708	1.06	0.671	1.00	1.30	0.872	No
414	41.40	2.42	1.04	1.38	0.84	0.708	1.06	0.670	1.00	1.30	0.871	No
415	41.50	2.43	1.05	1.38	0.84	0.707	1.06	0.670	1.00	1.30	0.870	No
416	41.60	2.43	1.05	1.39	0.84	0.707	1.06	0.669	1.00	1.30	0.870	No
417	41.70	2.44	1.05	1.39	0.84	0.706	1.06	0.668	1.00	1.30	0.869	No
418	41.80	2.45	1.05	1.39	0.83	0.706	1.06	0.668	1.00	1.30	2.000	Yes
419	41.90	2.45	1.06	1.40	0.83	0.705	1.06	0.667	1.00	1.30	2.000	Yes
420	42.00	2.46	1.06	1.40	0.83	0.704	1.06	0.667	1.00	1.30	2.000	Yes
421	42.10	2.47	1.06	1.40	0.83	0.704	1.06	0.666	1.00	1.30	2.000	Yes
422	42.20	2.47	1.07	1.41	0.83	0.703	1.06	0.666	1.00	1.30	2.000	Yes
423	42.30	2.48	1.07	1.41	0.83	0.702	1.06	0.665	1.00	1.30	2.000	Yes
424	42.40	2.49	1.07	1.41	0.83	0.702	1.06	0.664	1.00	1.30	2.000	Yes
425	42.50	2.49	1.08	1.42	0.83	0.701	1.06	0.664	1.00	1.30	0.863	No
426	42.60	2.50	1.08	1.42	0.83	0.700	1.06	0.663	1.00	1.30	0.862	No
427	42.70	2.51	1.08	1.42	0.83	0.700	1.06	0.662	1.00	1.30	0.861	No
428	42.80	2.51	1.09	1.43	0.83	0.699	1.06	0.662	1.00	1.30	2.000	Yes
429	42.90	2.52	1.09	1.43	0.82	0.698	1.06	0.661	1.00	1.30	2.000	Yes
430	43.00	2.53	1.09	1.43	0.82	0.698	1.06	0.661	1.00	1.30	2.000	Yes
431	43.10	2.53	1.10	1.44	0.82	0.697	1.06	0.660	1.00	1.30	2.000	Yes
432	43.20	2.54	1.10	1.44	0.82	0.696	1.06	0.659	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
433	43.30	2.54	1.10	1.44	0.82	0.696	1.06	0.659	1.00	1.30	2.000	Yes
434	43.40	2.55	1.10	1.45	0.82	0.695	1.06	0.658	1.00	1.30	2.000	Yes
435	43.50	2.56	1.11	1.45	0.82	0.694	1.06	0.657	1.00	1.30	2.000	Yes
436	43.60	2.56	1.11	1.45	0.82	0.694	1.06	0.657	1.00	1.30	2.000	Yes
437	43.70	2.57	1.11	1.46	0.82	0.693	1.06	0.656	1.00	1.30	2.000	Yes
438	43.80	2.58	1.12	1.46	0.82	0.692	1.06	0.655	1.00	1.30	2.000	Yes
439	43.90	2.58	1.12	1.46	0.81	0.692	1.06	0.655	1.00	1.30	2.000	Yes
440	44.00	2.59	1.12	1.47	0.81	0.691	1.06	0.654	1.00	1.30	2.000	Yes
441	44.10	2.60	1.13	1.47	0.81	0.690	1.06	0.653	1.00	1.30	2.000	Yes
442	44.20	2.60	1.13	1.47	0.81	0.690	1.06	0.653	1.00	1.30	2.000	Yes
443	44.30	2.61	1.13	1.48	0.81	0.689	1.06	0.652	1.00	1.30	2.000	Yes
444	44.40	2.62	1.14	1.48	0.81	0.688	1.06	0.651	1.00	1.30	2.000	Yes
445	44.50	2.62	1.14	1.48	0.81	0.687	1.06	0.651	1.00	1.30	2.000	Yes
446	44.60	2.63	1.14	1.49	0.81	0.687	1.06	0.650	1.00	1.30	2.000	Yes
447	44.70	2.64	1.15	1.49	0.81	0.686	1.06	0.649	1.00	1.30	2.000	Yes
448	44.80	2.64	1.15	1.49	0.81	0.685	1.06	0.649	1.00	1.30	2.000	Yes
449	44.90	2.65	1.15	1.50	0.80	0.685	1.06	0.648	1.00	1.30	2.000	Yes
450	45.00	2.66	1.15	1.50	0.80	0.684	1.06	0.647	1.00	1.30	2.000	Yes
451	45.10	2.66	1.16	1.50	0.80	0.683	1.06	0.647	1.00	1.30	2.000	Yes
452	45.20	2.67	1.16	1.51	0.80	0.682	1.06	0.646	1.00	1.30	0.840	No
453	45.30	2.67	1.16	1.51	0.80	0.682	1.06	0.645	1.00	1.30	2.000	Yes
454	45.40	2.68	1.17	1.51	0.80	0.681	1.06	0.645	1.00	1.30	2.000	Yes
455	45.50	2.69	1.17	1.52	0.80	0.680	1.06	0.644	1.00	1.30	2.000	Yes
456	45.60	2.69	1.17	1.52	0.80	0.679	1.06	0.643	1.00	1.30	2.000	Yes
457	45.70	2.70	1.18	1.53	0.80	0.679	1.06	0.642	1.00	1.30	2.000	Yes
458	45.80	2.71	1.18	1.53	0.80	0.678	1.06	0.642	1.00	1.30	2.000	Yes
459	45.90	2.71	1.18	1.53	0.79	0.677	1.06	0.641	1.00	1.30	2.000	Yes
460	46.00	2.72	1.19	1.54	0.79	0.676	1.06	0.640	1.00	1.30	0.832	No
461	46.10	2.73	1.19	1.54	0.79	0.676	1.06	0.640	1.00	1.30	2.000	Yes
462	46.20	2.73	1.19	1.54	0.79	0.675	1.06	0.639	1.00	1.30	2.000	Yes
463	46.30	2.74	1.19	1.54	0.79	0.674	1.06	0.638	1.00	1.30	2.000	Yes
464	46.40	2.75	1.20	1.55	0.79	0.674	1.06	0.638	1.00	1.30	2.000	Yes
465	46.50	2.75	1.20	1.55	0.79	0.673	1.06	0.637	1.00	1.30	2.000	Yes
466	46.60	2.76	1.20	1.55	0.79	0.672	1.06	0.636	1.00	1.30	2.000	Yes
467	46.70	2.77	1.21	1.56	0.79	0.671	1.06	0.636	1.00	1.30	0.826	No
468	46.80	2.77	1.21	1.56	0.79	0.671	1.06	0.635	1.00	1.30	0.825	No
469	46.90	2.78	1.21	1.56	0.78	0.670	1.06	0.634	1.00	1.30	0.824	No
470	47.00	2.79	1.22	1.57	0.78	0.669	1.06	0.633	1.00	1.30	0.824	No
471	47.10	2.79	1.22	1.57	0.78	0.668	1.06	0.633	1.00	1.30	0.823	No
472	47.20	2.80	1.22	1.58	0.78	0.668	1.06	0.632	1.00	1.30	0.822	No
473	47.30	2.80	1.23	1.58	0.78	0.667	1.06	0.631	1.00	1.30	0.821	No
474	47.40	2.81	1.23	1.58	0.78	0.666	1.06	0.631	1.00	1.30	0.820	No
475	47.50	2.82	1.23	1.59	0.78	0.665	1.06	0.630	1.00	1.30	0.819	No
476	47.60	2.82	1.24	1.59	0.78	0.664	1.06	0.629	1.00	1.30	0.818	No
477	47.70	2.83	1.24	1.59	0.78	0.664	1.06	0.628	1.00	1.30	0.817	No
478	47.80	2.84	1.24	1.60	0.78	0.663	1.06	0.628	1.00	1.30	0.816	No
479	47.90	2.84	1.24	1.60	0.77	0.662	1.06	0.627	1.00	1.30	0.815	No
480	48.00	2.85	1.25	1.60	0.77	0.661	1.06	0.626	1.00	1.30	0.814	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
481	48.10	2.86	1.25	1.61	0.77	0.661	1.06	0.625	1.00	1.30	0.813	No
482	48.20	2.86	1.25	1.61	0.77	0.660	1.06	0.625	1.00	1.30	0.812	No
483	48.30	2.87	1.26	1.61	0.77	0.659	1.06	0.624	1.00	1.30	0.811	No
484	48.40	2.88	1.26	1.62	0.77	0.658	1.06	0.623	1.00	1.30	0.810	No
485	48.50	2.89	1.26	1.62	0.77	0.657	1.06	0.622	1.00	1.30	0.809	No
486	48.60	2.89	1.27	1.63	0.77	0.657	1.06	0.621	1.00	1.30	0.808	No
487	48.70	2.90	1.27	1.63	0.77	0.656	1.06	0.621	1.00	1.30	0.807	No
488	48.80	2.91	1.27	1.63	0.76	0.655	1.06	0.620	1.00	1.30	0.806	No
489	48.90	2.91	1.28	1.64	0.76	0.654	1.06	0.619	1.00	1.30	0.805	No
490	49.00	2.92	1.28	1.64	0.76	0.653	1.06	0.618	1.00	1.30	0.804	No
491	49.10	2.93	1.28	1.64	0.76	0.652	1.06	0.618	1.00	1.30	0.803	No
492	49.20	2.93	1.29	1.65	0.76	0.652	1.06	0.617	1.00	1.30	0.802	No
493	49.30	2.94	1.29	1.65	0.76	0.651	1.06	0.616	1.00	1.30	0.801	No
494	49.40	2.95	1.29	1.65	0.76	0.650	1.06	0.615	1.00	1.30	0.800	No
495	49.50	2.95	1.29	1.66	0.76	0.649	1.06	0.615	1.00	1.30	0.799	No
496	49.60	2.96	1.30	1.66	0.76	0.648	1.06	0.614	1.00	1.30	0.798	No
497	49.70	2.97	1.30	1.66	0.76	0.648	1.06	0.613	1.00	1.30	0.797	No
498	49.80	2.97	1.30	1.67	0.75	0.647	1.06	0.612	1.00	1.30	0.796	No
499	49.90	2.98	1.31	1.67	0.75	0.646	1.06	0.612	1.00	1.30	0.795	No

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
 σ_v : Total overburden pressure at test point (tsf)
 u_0 : Water pressure at test point (tsf)
 σ_v' : Effective overburden pressure based on GWT during earthquake (tsf)
 r_d : Nonlinear shear mass factor
 CSR: Cyclic Stress Ratio
 MSF: Magnitude Scaling Factor
 CSR_{eq} : CSR adjusted for M=7.5
 K_σ : Effective overburden stress factor
 CSR*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::												
Point ID	Depth (ft)	q _t (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1	0.10	20.69	2.10	0.53	0.65	39.10	1.42	55.57	4.000	No	No	2.00
2	0.20	15.95	2.22	0.57	0.69	30.12	1.66	49.90	4.000	No	No	2.00
3	0.30	12.29	2.34	0.64	0.74	23.21	2.10	48.70	4.000	No	No	2.00
4	0.40	12.85	2.33	0.68	0.74	24.26	2.06	50.09	4.000	No	No	2.00
5	0.50	17.93	2.22	0.73	0.70	33.84	1.67	56.52	4.000	No	No	2.00
6	0.60	25.60	2.13	0.88	0.66	48.33	1.47	71.07	4.000	No	No	2.00
7	0.70	35.62	2.06	1.04	0.64	67.26	1.36	91.66	4.000	No	No	2.00
8	0.80	45.80	2.00	1.16	0.61	86.49	1.31	113.12	4.000	No	No	2.00
9	0.90	55.07	1.96	1.25	0.60	103.99	1.28	132.90	4.000	No	No	2.00
10	1.00	61.98	1.94	1.32	0.59	117.06	1.26	147.81	4.000	No	No	2.00
11	1.10	65.41	1.94	1.38	0.59	123.52	1.26	155.65	4.000	No	No	2.00
12	1.20	66.73	1.94	1.42	0.59	126.01	1.26	159.05	4.000	No	No	2.00
13	1.30	68.80	1.94	1.46	0.59	129.90	1.26	163.96	4.000	No	No	2.00
14	1.40	72.09	1.93	1.51	0.59	136.11	1.26	171.44	4.000	No	No	2.00
15	1.50	75.47	1.93	1.56	0.59	142.50	1.26	179.17	4.000	No	No	2.00
16	1.60	77.78	1.93	1.61	0.59	146.84	1.26	184.84	4.000	No	No	2.00
17	1.70	79.45	1.94	1.67	0.59	149.99	1.26	189.22	4.000	No	No	2.00
18	1.80	79.92	1.95	1.72	0.60	150.87	1.27	191.13	4.000	No	No	2.00
19	1.90	78.74	1.96	1.76	0.60	148.63	1.28	189.63	4.000	No	No	2.00
20	2.00	77.53	1.97	1.81	0.61	146.34	1.28	187.97	4.000	No	No	2.00
21	2.10	76.45	1.98	1.84	0.61	144.27	1.29	186.30	4.000	No	No	2.00
22	2.20	74.95	1.99	1.87	0.61	141.43	1.30	183.85	4.000	No	No	2.00
23	2.30	72.03	2.01	1.92	0.62	135.91	1.32	178.97	4.000	No	No	2.00
24	2.40	66.61	2.05	1.99	0.64	125.64	1.35	169.63	4.000	No	No	2.00
25	2.50	59.83	2.08	2.03	0.65	112.81	1.40	157.60	4.000	No	No	2.00
26	2.60	53.38	2.12	2.01	0.66	100.62	1.44	145.16	4.000	No	No	2.00
27	2.70	48.56	2.13	1.93	0.67	91.49	1.47	134.49	4.000	No	No	2.00
28	2.80	45.31	2.13	1.82	0.67	85.34	1.48	125.91	4.000	No	No	2.00
29	2.90	44.32	2.12	1.68	0.67	83.45	1.45	120.83	4.000	No	No	2.00
30	3.00	45.95	2.09	1.59	0.65	86.52	1.40	121.48	4.000	No	No	2.00
31	3.10	48.29	2.08	1.61	0.65	90.93	1.39	126.32	4.000	No	No	2.00
32	3.20	48.11	2.11	1.76	0.66	90.59	1.43	129.35	4.000	Yes	No	2.00
33	3.30	44.42	2.17	1.98	0.68	83.59	1.54	128.66	4.000	Yes	No	2.00
34	3.40	38.42	2.25	2.22	0.72	72.24	1.75	126.16	4.000	Yes	No	2.00
35	3.50	31.66	2.34	2.46	0.75	59.45	2.08	123.67	4.000	Yes	No	2.00
36	3.60	25.01	2.44	2.70	0.79	46.88	2.61	122.26	4.000	Yes	No	2.00
37	3.70	18.93	2.56	2.99	0.84	35.38	4.24	150.03	4.000	Yes	No	2.00
38	3.80	13.89	2.70	3.35	0.89	25.84	10.06	260.02	4.000	Yes	No	2.00
39	3.90	9.83	2.85	3.79	0.95	18.15	6.50	118.04	4.000	Yes	Yes	2.00
40	4.00	6.71	3.01	4.23	1.00	12.24	9.02	110.41	4.000	No	Yes	2.00
41	4.10	4.73	3.16	4.60	1.00	8.50	11.89	101.07	4.000	No	Yes	2.00
42	4.20	3.30	3.31	4.89	1.00	5.78	15.54	89.83	4.000	No	Yes	2.00
43	4.30	2.28	3.47	5.14	1.00	3.84	20.36	78.22	4.000	No	Yes	2.00
44	4.40	1.63	3.62	5.28	1.00	2.61	26.07	67.99	4.000	No	Yes	2.00
45	4.50	1.68	3.60	5.08	1.00	2.70	25.15	67.85	4.000	No	Yes	2.00
46	4.60	1.90	3.55	5.11	1.00	3.10	23.18	71.75	4.000	No	Yes	2.00
47	4.70	1.99	3.54	5.42	1.00	3.27	22.94	75.00	4.000	No	Yes	2.00
48	4.80	2.28	3.50	5.73	1.00	3.79	21.46	81.39	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _t (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
49	4.90	3.08	3.36	5.29	1.00	5.30	16.96	89.83	4.000	No	Yes	2.00
50	5.00	5.02	3.12	4.26	1.00	8.96	11.09	99.38	4.000	No	Yes	2.00
51	5.10	8.35	2.87	3.30	0.96	15.24	6.81	103.82	4.000	No	Yes	2.00
52	5.20	12.99	2.69	2.97	0.89	24.00	9.52	228.52	4.000	No	No	2.00
53	5.30	17.05	2.61	3.13	0.86	31.66	5.83	184.55	4.000	No	No	2.00
54	5.40	18.42	2.61	3.43	0.86	34.25	5.86	200.60	4.000	No	No	2.00
55	5.50	17.82	2.63	3.53	0.87	33.10	6.65	220.00	4.000	Yes	No	2.00
56	5.60	18.27	2.58	3.03	0.85	33.93	4.74	160.76	4.000	Yes	No	2.00
57	5.70	22.60	2.41	2.17	0.78	42.11	2.45	103.16	4.000	Yes	No	2.00
58	5.80	30.34	2.23	1.60	0.71	56.74	1.69	96.02	4.000	Yes	No	2.00
59	5.90	38.67	2.11	1.38	0.67	72.46	1.43	103.65	4.000	Yes	No	2.00
60	6.00	44.41	2.07	1.42	0.65	83.32	1.38	114.74	4.000	Yes	No	2.00
61	6.10	46.53	2.09	1.59	0.66	87.31	1.40	122.36	4.000	No	No	2.00
62	6.20	45.75	2.13	1.78	0.68	85.81	1.46	125.37	4.000	No	No	2.00
63	6.30	44.18	2.16	1.89	0.69	82.83	1.51	125.44	4.000	No	No	2.00
64	6.40	43.27	2.16	1.88	0.69	81.10	1.53	123.81	4.000	No	No	2.00
65	6.50	43.29	2.15	1.80	0.69	81.14	1.50	121.74	4.000	No	No	2.00
66	6.60	44.11	2.13	1.70	0.68	82.67	1.46	120.61	4.000	No	No	2.00
67	6.70	45.23	2.10	1.61	0.67	84.41	1.42	120.00	4.000	No	No	2.00
68	6.80	46.59	2.08	1.54	0.66	85.54	1.40	119.50	4.000	No	No	2.00
69	6.90	47.78	2.08	1.52	0.66	86.62	1.39	120.05	4.000	No	No	2.00
70	7.00	47.94	2.09	1.56	0.66	86.40	1.40	120.86	4.000	No	No	2.00
71	7.10	46.35	2.12	1.69	0.68	83.70	1.45	121.17	4.000	No	No	2.00
72	7.20	43.14	2.17	1.86	0.70	78.48	1.54	120.81	4.000	No	No	2.00
73	7.30	39.20	2.22	1.99	0.71	71.76	1.65	118.75	4.000	No	No	2.00
74	7.40	35.95	2.24	1.97	0.72	65.71	1.73	113.59	4.000	No	No	2.00
75	7.50	34.90	2.23	1.78	0.72	62.81	1.68	105.75	4.000	No	No	2.00
76	7.60	36.71	2.17	1.51	0.70	64.29	1.55	99.54	4.000	No	No	2.00
77	7.70	40.76	2.11	1.32	0.67	69.26	1.43	99.23	4.000	No	No	2.00
78	7.80	45.18	2.07	1.24	0.66	75.11	1.37	103.22	4.000	No	No	2.00
79	7.90	48.49	2.05	1.26	0.65	79.59	1.36	107.93	4.000	No	No	2.00
80	8.00	50.35	2.06	1.33	0.65	82.10	1.36	111.75	4.000	No	No	2.00
81	8.10	50.92	2.08	1.48	0.66	83.37	1.39	116.05	4.000	Yes	No	2.00
82	8.20	50.43	2.14	1.84	0.69	83.91	1.49	125.21	4.000	Yes	No	2.00
83	8.30	48.21	2.23	2.38	0.72	82.00	1.69	138.70	4.000	Yes	No	2.00
84	8.40	44.03	2.33	3.03	0.76	76.81	2.02	155.46	4.000	Yes	No	2.00
85	8.50	38.01	2.43	3.71	0.80	67.96	2.52	170.95	4.000	Yes	No	2.00
86	8.60	31.11	2.54	4.45	0.84	57.06	3.55	202.51	4.000	Yes	No	2.00
87	8.70	24.26	2.66	5.34	0.89	44.92	8.13	365.20	4.000	Yes	No	2.00
88	8.80	18.28	2.80	6.30	0.94	33.61	5.89	197.84	4.000	Yes	Yes	2.00
89	8.90	13.46	2.94	7.28	0.99	24.48	7.87	192.66	4.000	Yes	Yes	2.00
90	9.00	9.80	3.08	8.00	1.00	17.55	10.15	178.13	0.837	No	Yes	1.35
91	9.10	7.41	3.18	8.35	1.00	13.03	12.35	160.97	0.622	No	Yes	1.00
92	9.20	6.33	3.23	8.08	1.00	10.98	13.41	147.24	0.524	No	Yes	0.84
93	9.30	6.36	3.20	7.35	1.00	11.02	12.76	140.62	0.526	No	Yes	0.84
94	9.40	7.05	3.13	6.50	1.00	12.32	11.21	138.06	0.588	No	Yes	0.93
95	9.50	7.58	3.08	6.02	1.00	13.30	10.28	136.69	0.634	No	Yes	1.00
96	9.60	7.34	3.10	6.06	1.00	12.84	10.53	135.30	0.613	No	Yes	0.96

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
97	9.70	6.26	3.17	6.44	1.00	10.80	12.08	130.39	0.515	No	Yes	0.80
98	9.80	7.93	3.09	6.59	1.00	13.93	10.48	146.02	0.665	No	Yes	1.03
99	9.90	13.13	2.93	6.67	0.99	23.76	7.60	180.56	1.133	No	Yes	1.75
100	10.00	18.80	2.82	6.74	0.95	34.47	6.06	208.85	1.644	No	Yes	2.00
101	10.10	18.67	2.82	6.80	0.95	34.21	6.12	209.42	1.632	No	Yes	2.00
102	10.20	14.65	2.90	6.78	0.98	26.59	7.16	190.32	1.268	No	Yes	1.93
103	10.30	10.95	2.98	6.58	1.00	19.59	8.50	166.51	0.935	No	Yes	1.42
104	10.40	10.48	2.99	6.51	1.00	18.69	8.69	162.44	0.891	No	Yes	1.34
105	10.50	11.16	2.98	6.56	1.00	19.96	8.38	167.34	4.000	Yes	Yes	2.00
106	10.60	13.38	2.93	6.87	0.99	24.16	7.66	184.96	4.000	Yes	Yes	2.00
107	10.70	16.24	2.87	6.87	0.97	29.17	6.81	198.61	4.000	Yes	Yes	2.00
108	10.80	23.16	2.73	6.00	0.92	40.35	5.06	204.26	4.000	Yes	Yes	2.00
109	10.90	36.54	2.50	4.25	0.83	60.20	2.89	173.93	4.000	Yes	No	2.00
110	11.00	57.04	2.27	2.88	0.74	88.44	1.81	159.82	4.000	Yes	No	2.00
111	11.10	77.62	2.08	2.05	0.67	114.57	1.39	159.68	4.000	Yes	No	2.00
112	11.20	91.25	1.96	1.59	0.62	130.34	1.28	166.80	4.000	Yes	No	2.00
113	11.30	96.49	1.91	1.38	0.60	135.47	1.24	168.36	4.000	Yes	No	2.00
114	11.40	96.73	1.89	1.29	0.60	134.66	1.23	165.51	0.502	No	No	0.73
115	11.50	93.84	1.90	1.28	0.60	130.49	1.24	161.18	0.469	No	No	0.68
116	11.60	89.17	1.93	1.37	0.61	124.60	1.26	156.72	0.438	No	No	0.63
117	11.70	82.47	1.98	1.52	0.63	116.28	1.29	150.52	0.397	No	No	0.57
118	11.80	74.34	2.04	1.68	0.66	105.91	1.35	142.88	0.351	No	No	0.50
119	11.90	66.88	2.10	1.84	0.68	96.17	1.42	136.60	0.317	No	No	0.45
120	12.00	59.90	2.15	1.94	0.70	86.72	1.50	130.39	0.286	No	No	0.41
121	12.10	54.60	2.18	1.98	0.71	79.32	1.58	124.95	0.261	No	No	0.37
122	12.20	52.76	2.19	1.96	0.71	76.47	1.59	121.82	0.248	No	No	0.35
123	12.30	53.42	2.18	1.91	0.71	76.99	1.57	120.93	0.244	No	No	0.34
124	12.40	55.36	2.17	1.88	0.70	79.28	1.54	122.10	0.249	No	No	0.35
125	12.50	55.60	2.17	1.87	0.70	79.32	1.54	121.95	0.249	No	No	0.35
126	12.60	55.04	2.18	1.91	0.71	78.40	1.56	122.09	0.249	No	No	0.35
127	12.70	54.18	2.20	2.05	0.72	77.33	1.62	125.14	4.000	Yes	No	2.00
128	12.80	51.05	2.26	2.34	0.74	73.48	1.78	130.74	4.000	Yes	No	2.00
129	12.90	44.55	2.35	2.78	0.77	65.03	2.12	138.07	4.000	Yes	No	2.00
130	13.00	37.39	2.46	3.39	0.81	55.52	2.70	150.09	4.000	Yes	No	2.00
131	13.10	30.77	2.57	4.08	0.86	46.43	4.45	206.70	4.000	Yes	No	2.00
132	13.20	26.49	2.65	4.65	0.89	40.37	7.58	306.09	4.000	Yes	No	2.00
133	13.30	22.74	2.72	4.99	0.92	34.84	4.92	171.29	4.000	Yes	Yes	2.00
134	13.40	20.92	2.75	5.06	0.93	32.02	5.25	168.19	4.000	Yes	Yes	2.00
135	13.50	20.31	2.76	5.02	0.93	30.96	5.35	165.57	1.477	No	Yes	2.00
136	13.60	20.02	2.76	4.99	0.93	30.39	5.39	163.90	1.450	No	Yes	1.96
137	13.70	19.28	2.77	4.88	0.93	29.13	5.47	159.27	1.389	No	Yes	1.87
138	13.80	18.73	2.77	4.72	0.93	28.14	5.48	154.30	1.343	No	Yes	1.80
139	13.90	18.04	2.78	4.72	0.94	27.03	5.63	152.22	1.289	No	Yes	1.73
140	14.00	16.71	2.82	4.93	0.95	25.01	6.10	152.62	1.193	No	Yes	1.59
141	14.10	15.17	2.87	5.29	0.97	22.72	6.79	154.31	1.084	No	Yes	1.45
142	14.20	14.03	2.92	5.66	0.99	21.02	7.44	156.38	1.003	No	Yes	1.33
143	14.30	11.65	3.00	5.98	1.00	17.23	8.72	150.24	0.822	No	Yes	1.09
144	14.40	7.83	3.16	6.41	1.00	11.11	11.85	131.58	0.530	No	Yes	0.70

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
145	14.50	4.04	3.46	7.30	1.00	5.07	20.03	101.58	0.242	No	Yes	0.32
146	14.60	2.41	3.75	8.41	1.00	2.48	32.40	80.21	0.118	No	Yes	0.16
147	14.70	2.41	3.74	7.94	1.00	2.46	31.74	78.12	0.117	No	Yes	0.15
148	14.80	2.41	3.72	7.46	1.00	2.45	31.05	75.98	0.117	No	Yes	0.15
149	14.90	2.19	3.78	7.39	1.00	2.09	34.01	71.06	0.100	No	Yes	0.13
150	15.00	1.79	3.93	7.98	1.00	1.45	43.72	63.39	0.069	No	Yes	0.09
151	15.10	1.39	4.06	10.12	1.00	0.81	54.25	44.18	0.039	No	Yes	0.05
152	15.20	1.20	4.06	14.35	1.00	0.52	54.25	28.39	0.025	No	Yes	0.03
153	15.30	1.20	4.06	17.30	1.00	0.52	54.25	27.97	0.025	No	Yes	0.03
154	15.40	1.39	4.06	15.42	1.00	0.80	54.25	43.31	0.038	No	Yes	0.05
155	15.50	2.04	3.92	10.59	1.00	1.79	43.11	77.37	0.086	No	Yes	0.11
156	15.60	3.92	3.49	7.15	1.00	4.67	20.83	97.25	0.223	No	Yes	0.28
157	15.70	7.11	3.17	5.58	1.00	9.53	12.14	115.74	0.455	No	Yes	0.58
158	15.80	10.59	3.00	5.05	1.00	14.80	8.75	129.53	0.706	No	Yes	0.90
159	15.90	12.22	2.95	5.08	1.00	17.23	7.96	137.10	0.822	No	Yes	1.04
160	16.00	11.38	2.99	5.37	1.00	15.88	8.64	137.25	0.757	No	Yes	0.96
161	16.10	9.26	3.08	5.61	1.00	12.61	10.24	129.07	0.601	No	Yes	0.76
162	16.20	7.35	3.16	5.41	1.00	9.69	11.85	114.76	0.462	No	Yes	0.58
163	16.30	6.42	3.19	5.01	1.00	8.25	12.61	104.02	0.393	No	Yes	0.50
164	16.40	6.02	3.21	4.81	1.00	7.62	13.01	99.12	0.363	No	Yes	0.46
165	16.50	5.80	3.23	4.81	1.00	7.25	13.41	97.25	0.346	No	Yes	0.43
166	16.60	5.19	3.28	4.90	1.00	6.31	14.74	92.99	0.301	No	Yes	0.38
167	16.70	4.26	3.38	5.06	1.00	4.91	17.43	85.54	0.234	No	Yes	0.29
168	16.80	3.29	3.52	5.35	1.00	3.46	22.06	76.36	0.165	No	Yes	0.21
169	16.90	2.90	3.59	5.41	1.00	2.87	24.80	71.23	0.137	No	Yes	0.17
170	17.00	2.86	3.59	5.20	1.00	2.79	24.87	69.38	0.133	No	Yes	0.17
171	17.10	3.23	3.51	4.88	1.00	3.32	21.80	72.39	0.158	No	Yes	0.20
172	17.20	3.29	3.51	5.03	1.00	3.39	21.78	73.85	0.162	No	Yes	0.20
173	17.30	3.07	3.57	5.44	1.00	3.06	23.92	73.25	0.146	No	Yes	0.18
174	17.40	2.98	3.60	5.67	1.00	2.91	25.07	72.92	0.139	No	Yes	0.17
175	17.50	3.69	3.45	4.94	1.00	3.92	19.79	77.63	0.187	No	Yes	0.23
176	17.60	5.22	3.26	4.24	1.00	6.13	14.10	86.38	0.292	No	Yes	0.36
177	17.70	6.73	3.13	3.98	1.00	8.29	11.30	93.63	0.395	No	Yes	0.48
178	17.80	7.04	3.12	4.03	1.00	8.70	11.02	95.85	0.415	No	Yes	0.51
179	17.90	6.09	3.20	4.32	1.00	7.30	12.72	92.87	0.348	No	Yes	0.42
180	18.00	4.82	3.33	4.80	1.00	5.45	15.99	87.15	0.260	No	Yes	0.32
181	18.10	4.08	3.43	5.26	1.00	4.37	19.01	83.11	0.209	No	Yes	0.25
182	18.20	4.56	3.39	5.36	1.00	5.03	17.59	88.54	0.240	No	Yes	0.29
183	18.30	7.27	3.19	5.42	1.00	8.86	12.52	111.00	0.423	No	Yes	0.51
184	18.40	12.35	3.01	5.84	1.00	16.00	9.01	144.21	0.763	No	Yes	0.92
185	18.50	17.77	2.92	6.37	0.99	23.51	7.44	174.91	1.121	No	Yes	1.35
186	18.60	19.06	2.91	6.75	0.99	25.20	7.38	185.92	1.202	No	Yes	1.44
187	18.70	18.07	2.93	6.70	1.00	23.78	7.62	181.17	1.134	No	Yes	1.36
188	18.80	16.83	2.92	5.91	0.99	21.92	7.43	162.95	1.045	No	Yes	1.25
189	18.90	18.43	2.83	4.90	0.96	23.75	6.30	149.63	1.133	No	Yes	1.36
190	19.00	21.05	2.74	4.07	0.93	26.87	5.15	138.46	1.282	No	Yes	1.53
191	19.10	24.45	2.65	3.42	0.89	30.90	7.24	223.64	3.600	No	No	2.00
192	19.20	28.33	2.57	3.04	0.86	35.51	4.34	154.24	0.421	No	No	0.50

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
193	19.30	31.79	2.54	3.11	0.85	39.71	3.57	141.96	0.346	No	No	0.41
194	19.40	33.34	2.57	3.68	0.86	41.77	4.48	187.11	0.689	No	No	0.82
195	19.50	32.10	2.65	4.59	0.89	40.45	7.35	297.13	3.600	No	No	2.00
196	19.60	28.67	2.74	5.57	0.93	36.30	5.15	187.09	1.731	No	Yes	2.00
197	19.70	24.81	2.81	6.13	0.96	31.39	6.04	189.60	1.498	No	Yes	1.77
198	19.80	25.42	2.79	5.83	0.95	31.99	5.77	184.75	4.000	Yes	Yes	2.00
199	19.90	32.01	2.67	4.86	0.90	39.85	8.44	336.45	4.000	Yes	No	2.00
200	20.00	40.24	2.52	3.72	0.85	49.34	3.27	161.15	4.000	Yes	No	2.00
201	20.10	47.35	2.39	2.84	0.80	57.16	2.34	133.96	4.000	Yes	No	2.00
202	20.20	50.45	2.32	2.34	0.77	60.22	2.00	120.70	4.000	Yes	No	2.00
203	20.30	51.38	2.33	2.48	0.77	61.26	2.05	125.66	4.000	Yes	No	2.00
204	20.40	47.65	2.39	2.77	0.80	56.93	2.31	131.65	4.000	Yes	No	2.00
205	20.50	41.70	2.45	2.92	0.82	49.84	2.63	131.07	4.000	Yes	No	2.00
206	20.60	36.95	2.49	2.94	0.83	44.08	2.89	127.22	4.000	Yes	No	2.00
207	20.70	35.66	2.52	3.14	0.85	42.51	3.16	134.45	4.000	Yes	No	2.00
208	20.80	35.84	2.57	3.75	0.87	42.85	4.41	188.86	4.000	Yes	No	2.00
209	20.90	33.79	2.65	4.66	0.90	40.57	7.53	305.62	4.000	Yes	No	2.00
210	21.00	28.53	2.76	5.68	0.94	34.35	5.42	186.05	4.000	Yes	Yes	2.00
211	21.10	22.40	2.88	6.55	0.99	26.91	6.95	187.10	4.000	Yes	Yes	2.00
212	21.20	18.70	2.95	6.83	1.00	22.22	8.04	178.64	4.000	Yes	Yes	2.00
213	21.30	17.11	2.98	6.71	1.00	20.13	8.45	170.13	0.960	No	Yes	1.12
214	21.40	16.52	2.99	6.59	1.00	19.31	8.58	165.68	0.921	No	Yes	1.07
215	21.50	15.83	3.00	6.51	1.00	18.36	8.79	161.39	0.876	No	Yes	1.02
216	21.60	15.40	3.01	6.40	1.00	17.76	8.89	157.77	0.847	No	Yes	0.98
217	21.70	15.00	3.01	6.35	1.00	17.19	9.02	155.16	0.820	No	Yes	0.95
218	21.80	14.79	3.03	6.50	1.00	16.86	9.26	156.12	0.804	No	Yes	0.93
219	21.90	15.25	3.04	6.90	1.00	17.37	9.40	163.21	0.828	No	Yes	0.96
220	22.00	15.77	3.04	7.32	1.00	17.95	9.52	170.98	0.856	No	Yes	0.99
221	22.10	16.13	3.04	7.48	1.00	18.32	9.53	174.52	0.874	No	Yes	1.01
222	22.20	16.33	3.03	7.18	1.00	18.50	9.25	171.13	0.883	No	Yes	1.02
223	22.30	17.20	2.98	6.54	1.00	19.49	8.49	165.61	0.930	No	Yes	1.07
224	22.40	18.93	2.92	5.96	1.00	21.53	7.56	162.66	1.027	No	Yes	1.18
225	22.50	20.75	2.87	5.53	0.98	23.56	6.82	160.68	1.124	No	Yes	1.29
226	22.60	22.36	2.83	5.23	0.97	25.32	6.28	158.98	1.208	No	Yes	1.38
227	22.70	23.55	2.81	5.02	0.96	26.59	5.92	157.52	1.268	No	Yes	1.45
228	22.80	24.27	2.79	4.94	0.95	27.32	5.76	157.34	1.303	No	Yes	1.49
229	22.90	24.79	2.78	4.87	0.95	27.82	5.64	156.78	1.327	No	Yes	1.52
230	23.00	25.40	2.76	4.66	0.94	28.39	5.40	153.41	1.354	No	Yes	1.55
231	23.10	26.63	2.73	4.38	0.93	29.65	5.04	149.33	1.414	No	Yes	1.61
232	23.20	27.97	2.71	4.35	0.92	31.08	4.85	150.73	1.482	No	Yes	1.69
233	23.30	28.02	2.73	4.66	0.93	31.08	5.08	157.89	1.483	No	Yes	1.69
234	23.40	25.97	2.79	5.20	0.95	28.74	5.75	165.31	1.371	No	Yes	1.56
235	23.50	22.41	2.87	5.69	0.98	24.66	6.73	166.04	1.176	No	Yes	1.34
236	23.60	19.33	2.93	5.88	1.00	21.06	7.60	160.07	1.005	No	Yes	1.14
237	23.70	17.40	2.95	5.69	1.00	18.73	8.04	150.55	0.894	No	Yes	1.02
238	23.80	16.53	2.96	5.38	1.00	17.65	8.09	142.73	0.842	No	Yes	0.96
239	23.90	16.15	2.96	5.23	1.00	17.15	8.10	139.01	0.818	No	Yes	0.93
240	24.00	15.80	2.97	5.29	1.00	16.69	8.31	138.60	0.796	No	Yes	0.90

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
241	24.10	14.52	3.01	5.45	1.00	15.16	8.98	136.16	0.723	No	Yes	0.82
242	24.20	11.33	3.12	5.68	1.00	11.44	10.94	125.22	0.546	No	Yes	0.62
243	24.30	8.08	3.26	5.92	1.00	7.67	14.25	109.35	0.366	No	Yes	0.41
244	24.40	5.93	3.41	6.07	1.00	5.19	18.21	94.56	0.248	No	Yes	0.28
245	24.50	5.62	3.42	5.75	1.00	4.83	18.60	89.77	0.230	No	Yes	0.26
246	24.60	5.62	3.41	5.49	1.00	4.81	18.27	87.89	0.229	No	Yes	0.26
247	24.70	5.77	3.40	5.46	1.00	4.97	17.88	88.79	0.237	No	Yes	0.27
248	24.80	6.24	3.37	5.64	1.00	5.48	17.08	93.57	0.261	No	Yes	0.29
249	24.90	6.78	3.35	5.96	1.00	6.06	16.47	99.86	0.289	No	Yes	0.32
250	25.00	7.16	3.34	6.41	1.00	6.47	16.36	105.93	0.309	No	Yes	0.35
251	25.10	7.19	3.36	6.93	1.00	6.48	16.95	109.82	0.309	No	Yes	0.35
252	25.20	6.84	3.40	7.38	1.00	6.06	18.13	109.92	0.289	No	Yes	0.32
253	25.30	6.30	3.45	7.65	1.00	5.44	19.62	106.76	0.260	No	Yes	0.29
254	25.40	5.81	3.49	7.68	1.00	4.87	20.97	102.13	0.232	No	Yes	0.26
255	25.50	5.62	3.50	7.50	1.00	4.65	21.32	99.16	0.222	No	Yes	0.25
256	25.60	5.62	3.50	7.35	1.00	4.63	21.18	98.13	0.221	No	Yes	0.25
257	25.70	5.62	3.50	7.32	1.00	4.62	21.18	97.77	0.220	No	Yes	0.25
258	25.80	5.62	3.49	7.19	1.00	4.60	21.06	96.87	0.219	No	Yes	0.24
259	25.90	5.74	3.47	6.77	1.00	4.71	20.23	95.31	0.225	No	Yes	0.25
260	26.00	6.01	3.43	6.28	1.00	4.99	18.94	94.48	0.238	No	Yes	0.26
261	26.10	6.06	3.42	6.17	1.00	5.03	18.69	94.04	0.240	No	Yes	0.27
262	26.20	5.94	3.44	6.34	1.00	4.88	19.26	94.06	0.233	No	Yes	0.26
263	26.30	5.68	3.48	6.72	1.00	4.58	20.53	93.92	0.218	No	Yes	0.24
264	26.40	5.62	3.49	7.01	1.00	4.50	21.10	94.95	0.215	No	Yes	0.24
265	26.50	5.72	3.49	7.08	1.00	4.59	20.94	96.20	0.219	No	Yes	0.24
266	26.60	6.14	3.44	6.75	1.00	5.03	19.45	97.81	0.240	No	Yes	0.27
267	26.70	6.68	3.40	6.46	1.00	5.59	17.92	100.18	0.267	No	Yes	0.30
268	26.80	7.11	3.37	6.56	1.00	6.04	17.23	104.06	0.288	No	Yes	0.32
269	26.90	7.23	3.39	7.06	1.00	6.15	17.62	108.41	0.293	No	Yes	0.32
270	27.00	7.58	3.39	7.66	1.00	6.50	17.71	115.06	0.310	No	Yes	0.34
271	27.10	8.22	3.37	8.14	1.00	7.16	17.22	123.35	0.342	No	Yes	0.38
272	27.20	9.74	3.31	8.22	1.00	8.76	15.41	134.97	0.418	No	Yes	0.46
273	27.30	13.33	3.16	7.47	1.00	12.55	11.91	149.50	0.599	No	Yes	0.66
274	27.40	19.91	2.96	6.05	1.00	19.49	8.12	158.22	0.930	No	Yes	1.03
275	27.50	30.24	2.74	4.58	0.94	30.15	5.12	154.48	1.438	No	Yes	1.59
276	27.60	41.52	2.58	3.80	0.88	41.60	4.79	199.46	0.818	No	No	0.90
277	27.70	49.24	2.52	3.73	0.86	49.37	3.26	161.12	0.469	No	No	0.52
278	27.80	49.82	2.56	4.18	0.87	49.90	4.05	202.19	4.000	No	No	2.00
279	27.90	44.25	2.64	4.85	0.90	44.15	6.93	305.96	3.600	No	No	2.00
280	28.00	36.48	2.73	5.35	0.94	36.12	5.03	181.72	1.723	No	Yes	1.90
281	28.10	29.33	2.81	5.57	0.97	28.72	6.01	172.64	1.370	No	Yes	1.51
282	28.20	23.96	2.88	5.65	0.99	23.14	6.98	161.61	1.104	No	Yes	1.21
283	28.30	19.51	2.97	5.96	1.00	18.48	8.32	153.82	0.882	No	Yes	0.97
284	28.40	15.84	3.08	6.63	1.00	14.65	10.20	149.43	0.699	No	Yes	0.77
285	28.50	12.93	3.19	7.63	1.00	11.62	12.61	146.47	0.554	No	Yes	0.61
286	28.60	12.75	3.23	8.32	1.00	11.39	13.33	151.86	0.543	No	Yes	0.60
287	28.70	15.29	3.15	8.12	1.00	13.95	11.70	163.26	0.665	No	Yes	0.73
288	28.80	18.82	3.06	7.52	1.00	17.49	9.82	171.85	0.834	No	Yes	0.92

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
289	28.90	20.53	3.01	7.06	1.00	19.18	8.97	171.95	0.915	No	Yes	1.00
290	29.00	20.27	3.01	6.89	1.00	18.85	8.94	168.48	0.899	No	Yes	0.99
291	29.10	18.46	3.05	7.08	1.00	16.96	9.68	164.12	0.809	No	Yes	0.89
292	29.20	16.60	3.10	7.25	1.00	15.04	10.53	158.43	0.717	No	Yes	0.79
293	29.30	16.51	3.07	6.67	1.00	14.91	10.12	150.91	0.711	No	Yes	0.78
294	29.40	20.13	2.93	5.21	1.00	18.48	7.71	142.45	0.881	No	Yes	0.97
295	29.50	27.09	2.76	4.06	0.95	25.29	5.37	135.82	1.206	No	Yes	1.32
296	29.60	33.16	2.66	3.62	0.91	31.18	7.86	245.01	3.600	No	No	2.00
297	29.70	36.69	2.63	3.63	0.90	34.57	6.41	221.64	3.600	No	No	2.00
298	29.80	40.80	2.62	4.04	0.90	38.51	6.33	243.95	3.600	No	No	2.00
299	29.90	48.32	2.61	4.52	0.89	45.76	5.61	256.68	4.000	Yes	No	2.00
300	30.00	59.72	2.53	4.31	0.86	56.73	3.35	190.27	4.000	Yes	No	2.00
301	30.10	73.28	2.42	3.70	0.82	69.68	2.47	171.93	4.000	Yes	No	2.00
302	30.20	85.57	2.32	3.17	0.78	81.32	2.01	163.64	4.000	Yes	No	2.00
303	30.30	94.24	2.28	3.05	0.77	89.46	1.86	166.65	4.000	Yes	No	2.00
304	30.40	96.38	2.30	3.27	0.77	91.31	1.92	175.56	4.000	Yes	No	2.00
305	30.50	93.45	2.34	3.60	0.79	88.28	2.09	184.55	4.000	Yes	No	2.00
306	30.60	85.88	2.41	4.07	0.82	80.82	2.40	194.35	4.000	Yes	No	2.00
307	30.70	75.59	2.48	4.61	0.85	70.78	2.87	203.41	4.000	Yes	No	2.00
308	30.80	64.96	2.56	5.01	0.87	60.44	4.08	246.52	4.000	Yes	No	2.00
309	30.90	58.02	2.59	4.95	0.89	53.66	4.98	267.00	4.000	Yes	No	2.00
310	31.00	57.76	2.54	4.28	0.87	53.25	3.73	198.66	4.000	Yes	No	2.00
311	31.10	64.29	2.43	3.34	0.83	59.30	2.56	151.63	4.000	Yes	No	2.00
312	31.20	74.72	2.31	2.59	0.78	69.01	1.96	135.05	4.000	Yes	No	2.00
313	31.30	84.37	2.22	2.18	0.75	77.95	1.66	129.45	4.000	Yes	No	2.00
314	31.40	91.02	2.17	2.02	0.73	84.05	1.55	129.96	4.000	Yes	No	2.00
315	31.50	94.21	2.15	1.95	0.72	86.86	1.51	130.81	0.288	No	No	0.32
316	31.60	94.73	2.14	1.91	0.72	87.16	1.49	129.89	0.284	No	No	0.31
317	31.70	92.99	2.15	1.90	0.72	85.34	1.50	128.04	0.275	No	No	0.30
318	31.80	89.90	2.17	1.96	0.73	82.26	1.54	127.00	4.000	Yes	No	2.00
319	31.90	86.48	2.20	2.08	0.74	78.87	1.61	127.32	4.000	Yes	No	2.00
320	32.00	83.14	2.24	2.26	0.75	75.57	1.72	129.94	4.000	Yes	No	2.00
321	32.10	79.62	2.29	2.54	0.77	72.09	1.88	135.85	4.000	Yes	No	2.00
322	32.20	75.05	2.35	2.90	0.80	67.65	2.13	144.01	4.000	Yes	No	2.00
323	32.30	69.21	2.41	3.21	0.82	62.06	2.41	149.69	4.000	Yes	No	2.00
324	32.40	63.30	2.44	3.29	0.83	56.45	2.61	147.58	4.000	Yes	No	2.00
325	32.50	60.94	2.43	3.03	0.83	54.16	2.54	137.73	0.323	No	No	0.35
326	32.60	65.02	2.36	2.54	0.80	57.83	2.17	125.25	0.263	No	No	0.29
327	32.70	74.05	2.27	2.22	0.77	66.03	1.83	121.08	0.245	No	No	0.27
328	32.80	83.30	2.23	2.15	0.75	74.38	1.69	125.62	0.264	No	No	0.29
329	32.90	89.30	2.22	2.28	0.75	79.69	1.68	133.79	0.303	No	No	0.33
330	33.00	94.12	2.23	2.42	0.75	83.89	1.69	141.45	0.343	No	No	0.38
331	33.10	101.14	2.20	2.41	0.74	90.11	1.63	146.50	0.372	No	No	0.41
332	33.20	112.44	2.16	2.28	0.72	100.24	1.51	151.82	0.405	No	No	0.45
333	33.30	126.20	2.11	2.18	0.71	112.59	1.43	161.02	0.468	No	No	0.52
334	33.40	137.62	2.08	2.19	0.70	122.75	1.40	171.45	0.549	No	No	0.60
335	33.50	143.17	2.09	2.28	0.70	127.48	1.40	178.43	0.608	No	No	0.67
336	33.60	142.56	2.10	2.38	0.70	126.60	1.42	179.91	0.622	No	No	0.68

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
337	33.70	140.15	2.11	2.42	0.71	124.12	1.44	178.51	0.609	No	No	0.67
338	33.80	138.78	2.11	2.40	0.71	122.61	1.44	176.68	0.593	No	No	0.65
339	33.90	138.19	2.11	2.39	0.71	121.82	1.44	175.59	0.583	No	No	0.64
340	34.00	135.99	2.12	2.41	0.71	119.56	1.45	173.87	0.569	No	No	0.63
341	34.10	131.92	2.14	2.47	0.72	115.61	1.49	171.69	0.551	No	No	0.61
342	34.20	126.82	2.16	2.54	0.73	110.75	1.53	168.98	0.529	No	No	0.58
343	34.30	122.27	2.18	2.60	0.74	106.42	1.57	166.75	0.511	No	No	0.56
344	34.40	118.79	2.19	2.62	0.74	103.06	1.60	164.44	0.494	No	No	0.55
345	34.50	116.72	2.20	2.60	0.74	101.00	1.60	162.03	0.476	No	No	0.53
346	34.60	116.13	2.19	2.55	0.74	100.27	1.59	159.86	0.460	No	No	0.51
347	34.70	116.42	2.19	2.50	0.74	100.33	1.58	158.43	0.450	No	No	0.50
348	34.80	116.08	2.18	2.47	0.74	99.83	1.57	157.06	0.440	No	No	0.49
349	34.90	113.21	2.19	2.47	0.74	97.07	1.59	154.41	0.422	No	No	0.47
350	35.00	107.12	2.21	2.50	0.75	91.47	1.64	150.40	0.396	No	No	0.44
351	35.10	98.36	2.25	2.59	0.76	83.53	1.76	146.61	0.373	No	No	0.41
352	35.20	88.33	2.31	2.77	0.78	74.49	1.95	145.13	0.364	No	No	0.40
353	35.30	78.11	2.37	2.97	0.81	65.34	2.21	144.33	0.360	No	No	0.40
354	35.40	70.66	2.41	3.02	0.82	58.71	2.40	140.97	0.341	No	No	0.38
355	35.50	68.31	2.40	2.84	0.82	56.59	2.36	133.62	0.302	No	No	0.33
356	35.60	71.04	2.35	2.55	0.80	58.91	2.14	126.28	0.267	No	No	0.30
357	35.70	76.04	2.31	2.36	0.79	63.18	1.95	123.30	0.254	No	No	0.28
358	35.80	80.43	2.28	2.29	0.78	66.88	1.85	124.02	0.257	No	No	0.29
359	35.90	83.79	2.27	2.34	0.77	69.62	1.83	127.50	0.273	No	No	0.30
360	36.00	86.97	2.27	2.43	0.77	72.18	1.83	132.35	0.296	No	No	0.33
361	36.10	90.89	2.28	2.55	0.77	75.33	1.84	138.64	0.328	No	No	0.36
362	36.20	95.24	2.28	2.70	0.78	78.84	1.86	146.32	0.371	No	No	0.41
363	36.30	98.94	2.29	2.89	0.78	81.74	1.89	154.77	0.425	No	No	0.47
364	36.40	100.43	2.31	3.08	0.79	82.73	1.96	162.04	0.476	No	No	0.53
365	36.50	99.89	2.33	3.27	0.80	81.99	2.05	167.72	0.519	No	No	0.58
366	36.60	98.07	2.36	3.48	0.81	80.15	2.16	173.25	4.000	Yes	No	2.00
367	36.70	95.06	2.39	3.74	0.82	77.30	2.33	179.97	4.000	Yes	No	2.00
368	36.80	89.45	2.44	4.08	0.84	72.26	2.59	187.05	4.000	Yes	No	2.00
369	36.90	80.70	2.50	4.52	0.86	64.60	2.88	186.22	4.000	Yes	No	2.00
370	37.00	69.82	2.59	5.11	0.90	55.23	5.04	278.40	4.000	Yes	No	2.00
371	37.10	58.94	2.68	5.81	0.93	45.95	9.21	423.28	4.000	Yes	No	2.00
372	37.20	50.59	2.76	6.32	0.96	38.90	5.37	208.94	4.000	Yes	Yes	2.00
373	37.30	46.04	2.79	6.23	0.97	35.09	5.68	199.45	1.674	No	Yes	1.87
374	37.40	45.72	2.75	5.47	0.96	34.83	5.23	182.11	1.661	No	Yes	1.86
375	37.50	48.88	2.66	4.43	0.92	37.49	7.96	298.35	3.600	No	No	2.00
376	37.60	54.47	2.56	3.61	0.89	42.16	4.23	178.25	0.607	No	No	0.68
377	37.70	60.92	2.49	3.18	0.86	47.50	2.89	137.04	0.319	No	No	0.36
378	37.80	66.48	2.44	3.04	0.84	52.02	2.62	136.49	0.316	No	No	0.36
379	37.90	71.26	2.42	2.97	0.83	55.89	2.46	137.24	0.320	No	No	0.36
380	38.00	76.37	2.37	2.80	0.82	60.07	2.24	134.83	0.308	No	No	0.35
381	38.10	82.38	2.32	2.51	0.79	65.07	1.99	129.40	0.282	No	No	0.32
382	38.20	88.96	2.26	2.26	0.77	70.57	1.78	125.79	0.265	No	No	0.30
383	38.30	94.06	2.23	2.16	0.76	74.74	1.69	126.27	0.267	No	No	0.30
384	38.40	96.38	2.23	2.21	0.76	76.48	1.69	129.16	0.280	No	No	0.32

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
385	38.50	95.22	2.25	2.33	0.77	75.26	1.75	131.62	0.292	No	No	0.33
386	38.60	91.50	2.27	2.42	0.78	71.97	1.83	131.86	0.293	No	No	0.33
387	38.70	86.76	2.30	2.47	0.79	67.88	1.92	130.30	0.286	No	No	0.32
388	38.80	82.49	2.32	2.48	0.79	64.22	1.99	127.88	0.274	No	No	0.31
389	38.90	79.99	2.32	2.44	0.80	62.06	2.01	124.95	0.261	No	No	0.30
390	39.00	79.66	2.31	2.31	0.79	61.74	1.96	120.80	0.244	No	No	0.28
391	39.10	80.98	2.28	2.12	0.78	62.84	1.84	115.76	0.224	No	No	0.25
392	39.20	81.39	2.26	2.01	0.77	63.13	1.79	112.74	4.000	Yes	No	2.00
393	39.30	77.05	2.29	2.10	0.79	59.38	1.90	112.75	4.000	Yes	No	2.00
394	39.40	68.00	2.38	2.47	0.82	51.69	2.30	118.71	4.000	Yes	No	2.00
395	39.50	55.58	2.52	3.09	0.87	41.34	3.24	134.05	4.000	Yes	No	2.00
396	39.60	43.51	2.68	3.89	0.93	31.48	8.79	276.77	4.000	Yes	No	2.00
397	39.70	32.08	2.84	4.74	1.00	22.36	6.43	143.78	4.000	Yes	Yes	2.00
398	39.80	24.49	2.98	5.40	1.00	16.60	8.43	139.94	4.000	Yes	Yes	2.00
399	39.90	25.69	2.97	5.46	1.00	17.46	8.21	143.33	0.833	No	Yes	0.95
400	40.00	28.88	2.92	5.37	1.00	19.80	7.50	148.45	0.944	No	Yes	1.07
401	40.10	26.02	2.96	5.48	1.00	17.62	8.18	144.17	0.841	No	Yes	0.96
402	40.20	17.22	3.14	6.00	1.00	11.05	11.50	127.06	0.527	No	Yes	0.60
403	40.30	10.69	3.39	7.15	1.00	6.18	17.67	109.18	0.295	No	Yes	0.34
404	40.40	11.62	3.36	7.25	1.00	6.85	16.74	114.73	0.327	No	Yes	0.37
405	40.50	14.83	3.24	6.74	1.00	9.21	13.59	125.12	0.439	No	Yes	0.50
406	40.60	19.14	3.10	5.97	1.00	12.36	10.71	132.38	0.590	No	Yes	0.67
407	40.70	24.64	2.97	5.19	1.00	16.37	8.32	136.17	0.781	No	Yes	0.89
408	40.80	30.34	2.86	4.59	1.00	20.52	6.68	137.08	0.979	No	Yes	1.12
409	40.90	34.36	2.80	4.24	0.98	23.54	5.80	136.50	1.123	No	Yes	1.28
410	41.00	35.62	2.77	4.07	0.97	24.47	5.51	134.71	1.167	No	Yes	1.34
411	41.10	35.36	2.77	4.01	0.97	24.22	5.49	133.05	1.155	No	Yes	1.32
412	41.20	35.52	2.77	4.01	0.97	24.29	5.48	133.12	1.159	No	Yes	1.33
413	41.30	37.77	2.76	4.11	0.96	25.92	5.32	137.77	1.236	No	Yes	1.42
414	41.40	39.51	2.76	4.40	0.97	27.12	5.38	145.91	1.293	No	Yes	1.48
415	41.50	39.75	2.79	4.90	0.98	27.14	5.75	156.14	1.294	No	Yes	1.49
416	41.60	38.24	2.85	5.58	1.00	25.83	6.46	166.81	1.232	No	Yes	1.42
417	41.70	37.40	2.88	6.14	1.00	25.16	6.97	175.34	1.200	No	Yes	1.38
418	41.80	40.17	2.86	6.11	1.00	27.09	6.62	179.45	4.000	Yes	Yes	2.00
419	41.90	50.73	2.73	5.18	0.96	35.02	5.02	175.81	4.000	Yes	Yes	2.00
420	42.00	69.20	2.54	3.91	0.88	49.29	3.62	178.59	4.000	Yes	No	2.00
421	42.10	94.71	2.33	2.82	0.80	69.50	2.05	142.66	4.000	Yes	No	2.00
422	42.20	121.87	2.16	2.11	0.74	91.48	1.52	139.20	4.000	Yes	No	2.00
423	42.30	147.28	2.05	1.79	0.70	112.12	1.35	151.37	4.000	Yes	No	2.00
424	42.40	168.54	1.99	1.72	0.68	129.14	1.30	167.86	4.000	Yes	No	2.00
425	42.50	184.42	1.97	1.76	0.67	141.54	1.29	181.95	0.640	No	No	0.74
426	42.60	194.06	1.97	1.84	0.67	148.80	1.28	191.17	0.730	No	No	0.85
427	42.70	194.52	1.99	1.92	0.67	148.65	1.30	192.61	0.745	No	No	0.86
428	42.80	186.27	2.01	2.00	0.68	141.56	1.32	186.66	4.000	Yes	No	2.00
429	42.90	172.77	2.05	2.09	0.70	130.36	1.36	176.86	4.000	Yes	No	2.00
430	43.00	157.23	2.10	2.21	0.72	117.60	1.42	166.71	4.000	Yes	No	2.00
431	43.10	141.54	2.16	2.37	0.74	104.80	1.51	158.67	4.000	Yes	No	2.00
432	43.20	127.00	2.22	2.61	0.76	92.93	1.67	155.22	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
433	43.30	114.88	2.30	2.98	0.79	82.98	1.91	158.67	4.000	Yes	No	2.00
434	43.40	105.17	2.38	3.50	0.82	74.92	2.26	169.64	4.000	Yes	No	2.00
435	43.50	96.99	2.45	4.03	0.85	68.21	2.67	181.83	4.000	Yes	No	2.00
436	43.60	87.91	2.51	4.31	0.87	61.12	2.90	177.17	4.000	Yes	No	2.00
437	43.70	82.13	2.51	4.13	0.88	56.81	3.06	173.72	4.000	Yes	No	2.00
438	43.80	82.78	2.46	3.57	0.86	57.50	2.74	157.36	4.000	Yes	No	2.00
439	43.90	91.57	2.38	3.01	0.82	64.35	2.25	144.98	4.000	Yes	No	2.00
440	44.00	103.19	2.29	2.62	0.79	73.37	1.90	139.21	4.000	Yes	No	2.00
441	44.10	111.95	2.24	2.37	0.77	80.18	1.71	137.01	4.000	Yes	No	2.00
442	44.20	116.80	2.21	2.31	0.76	83.81	1.65	138.27	4.000	Yes	No	2.00
443	44.30	116.61	2.25	2.54	0.78	83.18	1.74	144.81	4.000	Yes	No	2.00
444	44.40	111.71	2.32	3.06	0.80	78.69	2.01	158.02	4.000	Yes	No	2.00
445	44.50	102.58	2.41	3.69	0.84	71.14	2.43	172.75	4.000	Yes	No	2.00
446	44.60	93.13	2.47	4.04	0.86	63.78	2.79	177.83	4.000	Yes	No	2.00
447	44.70	89.79	2.46	3.81	0.86	61.35	2.75	168.46	4.000	Yes	No	2.00
448	44.80	96.85	2.38	3.16	0.83	66.93	2.27	151.81	4.000	Yes	No	2.00
449	44.90	113.10	2.26	2.56	0.78	79.55	1.79	142.30	4.000	Yes	No	2.00
450	45.00	132.27	2.17	2.24	0.75	94.33	1.54	145.46	4.000	Yes	No	2.00
451	45.10	147.43	2.13	2.18	0.73	105.80	1.46	154.46	4.000	Yes	No	2.00
452	45.20	155.41	2.12	2.27	0.73	111.47	1.46	162.21	0.477	No	No	0.57
453	45.30	156.28	2.14	2.41	0.74	111.60	1.49	166.12	4.000	Yes	No	2.00
454	45.40	151.54	2.17	2.56	0.75	107.52	1.55	166.61	4.000	Yes	No	2.00
455	45.50	142.44	2.22	2.75	0.77	100.16	1.66	165.78	4.000	Yes	No	2.00
456	45.60	129.99	2.28	3.06	0.79	90.25	1.86	167.45	4.000	Yes	No	2.00
457	45.70	115.63	2.36	3.51	0.82	78.99	2.20	173.53	4.000	Yes	No	2.00
458	45.80	101.57	2.45	4.01	0.86	68.20	2.65	180.86	4.000	Yes	No	2.00
459	45.90	89.43	2.51	4.29	0.88	59.18	3.05	180.65	4.000	Yes	No	2.00
460	46.00	80.36	2.54	4.18	0.89	52.68	3.63	191.30	0.731	No	No	0.88
461	46.10	75.66	2.52	3.73	0.88	49.51	3.26	161.23	4.000	Yes	No	2.00
462	46.20	75.96	2.47	3.17	0.86	49.99	2.77	138.71	4.000	Yes	No	2.00
463	46.30	81.99	2.39	2.63	0.83	54.66	2.30	125.66	4.000	Yes	No	2.00
464	46.40	93.65	2.28	2.16	0.79	63.56	1.85	117.53	4.000	Yes	No	2.00
465	46.50	110.56	2.16	1.78	0.75	76.54	1.53	117.13	4.000	Yes	No	2.00
466	46.60	129.39	2.08	1.59	0.71	90.92	1.38	125.92	4.000	Yes	No	2.00
467	46.70	144.05	2.05	1.64	0.70	101.68	1.35	137.61	0.322	No	No	0.39
468	46.80	149.85	2.08	1.89	0.72	105.16	1.39	146.60	0.373	No	No	0.45
469	46.90	147.45	2.15	2.28	0.74	102.23	1.50	153.73	0.418	No	No	0.51
470	47.00	142.18	2.22	2.72	0.77	97.28	1.67	162.30	0.478	No	No	0.58
471	47.10	138.12	2.27	3.07	0.79	93.55	1.82	170.72	0.543	No	No	0.66
472	47.20	136.30	2.29	3.23	0.80	91.82	1.90	174.43	0.574	No	No	0.70
473	47.30	137.24	2.28	3.13	0.79	92.45	1.86	171.87	0.552	No	No	0.67
474	47.40	142.58	2.24	2.87	0.78	96.55	1.73	166.68	0.511	No	No	0.62
475	47.50	152.84	2.18	2.58	0.76	104.38	1.58	164.46	0.494	No	No	0.60
476	47.60	165.80	2.13	2.38	0.74	114.11	1.47	167.72	0.519	No	No	0.63
477	47.70	177.89	2.10	2.29	0.72	123.01	1.42	174.14	0.571	No	No	0.70
478	47.80	187.02	2.08	2.29	0.72	129.49	1.40	180.72	0.629	No	No	0.77
479	47.90	192.69	2.08	2.30	0.72	133.40	1.39	184.92	0.668	No	No	0.82
480	48.00	196.25	2.07	2.28	0.71	135.83	1.38	187.00	0.688	No	No	0.85

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
481	48.10	199.18	2.06	2.24	0.71	137.90	1.36	188.02	0.698	No	No	0.86
482	48.20	202.36	2.05	2.19	0.71	140.14	1.35	189.38	0.712	No	No	0.88
483	48.30	204.97	2.04	2.17	0.70	141.89	1.34	190.75	0.726	No	No	0.89
484	48.40	206.02	2.04	2.19	0.70	142.34	1.35	191.69	0.735	No	No	0.91
485	48.50	205.06	2.05	2.25	0.71	141.17	1.36	191.83	0.737	No	No	0.91
486	48.60	202.72	2.07	2.32	0.71	138.98	1.38	191.18	0.730	No	No	0.90
487	48.70	200.81	2.08	2.37	0.72	137.19	1.39	190.43	0.722	No	No	0.90
488	48.80	200.45	2.08	2.37	0.72	136.68	1.39	189.96	0.717	No	No	0.89
489	48.90	202.19	2.07	2.34	0.72	137.80	1.38	190.37	0.722	No	No	0.90
490	49.00	205.17	2.06	2.30	0.71	139.85	1.37	191.52	0.733	No	No	0.91
491	49.10	208.80	2.05	2.27	0.71	142.34	1.36	193.42	0.753	No	No	0.94
492	49.20	212.77	2.05	2.26	0.71	145.01	1.35	195.97	0.780	No	No	0.97
493	49.30	217.38	2.04	2.25	0.71	148.13	1.34	199.07	0.814	No	No	1.02
494	49.40	221.74	2.03	2.24	0.70	151.06	1.34	202.00	4.000	No	No	2.00
495	49.50	222.23	2.03	2.24	0.70	151.15	1.34	202.10	4.000	No	No	2.00
496	49.60	216.25	2.04	2.25	0.71	146.54	1.35	197.41	0.795	No	No	1.00
497	49.70	208.44	2.05	2.25	0.71	140.66	1.36	191.32	0.731	No	No	0.92
498	49.80	204.58	2.06	2.27	0.71	137.59	1.37	188.42	0.702	No	No	0.88
499	49.90	205.34	2.06	2.28	0.72	137.86	1.37	188.96	0.708	No	No	0.89

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q_t :	Total cone resistance
I_c :	Soil behavior type index
Fr:	Normalized friction ratio (%)
n:	Stress exponent
Q_{tn} :	Normalized cone resistance
K_c :	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Normalized and adjusted cone resistance
CRR _{7.5} :	Cyclic resistance ratio for $M_w=7.5$
FS:	Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
0.10	2.00	0.00	0.00	0.10	0.00	0.20	2.00	0.00	0.00	0.10	0.00
0.30	2.00	0.00	0.00	0.10	0.00	0.40	2.00	0.00	0.00	0.10	0.00
0.50	2.00	0.00	0.00	0.10	0.00	0.60	2.00	0.00	0.00	0.10	0.00
0.70	2.00	0.00	0.00	0.10	0.00	0.80	2.00	0.00	0.00	0.10	0.00
0.90	2.00	0.00	0.00	0.10	0.00	1.00	2.00	0.00	0.00	0.10	0.00
1.10	2.00	0.00	0.00	0.10	0.00	1.20	2.00	0.00	0.00	0.10	0.00
1.30	2.00	0.00	0.00	0.10	0.00	1.40	2.00	0.00	0.00	0.10	0.00
1.50	2.00	0.00	0.00	0.10	0.00	1.60	2.00	0.00	0.00	0.10	0.00
1.70	2.00	0.00	0.00	0.10	0.00	1.80	2.00	0.00	0.00	0.10	0.00
1.90	2.00	0.00	0.00	0.10	0.00	2.00	2.00	0.00	0.00	0.10	0.00
2.10	2.00	0.00	0.00	0.10	0.00	2.20	2.00	0.00	0.00	0.10	0.00
2.30	2.00	0.00	0.00	0.10	0.00	2.40	2.00	0.00	0.00	0.10	0.00
2.50	2.00	0.00	0.00	0.10	0.00	2.60	2.00	0.00	0.00	0.10	0.00
2.70	2.00	0.00	0.00	0.10	0.00	2.80	2.00	0.00	0.00	0.10	0.00
2.90	2.00	0.00	0.00	0.10	0.00	3.00	2.00	0.00	0.00	0.10	0.00
3.10	2.00	0.00	0.00	0.10	0.00	3.20	2.00	0.00	0.00	0.10	0.00
3.30	2.00	0.00	0.00	0.10	0.00	3.40	2.00	0.00	0.00	0.10	0.00
3.50	2.00	0.00	0.00	0.10	0.00	3.60	2.00	0.00	0.00	0.10	0.00
3.70	2.00	0.00	0.00	0.10	0.00	3.80	2.00	0.00	0.00	0.10	0.00
3.90	2.00	0.00	0.00	0.10	0.00	4.00	2.00	0.00	0.00	0.10	0.00
4.10	2.00	0.00	0.00	0.10	0.00	4.20	2.00	0.00	0.00	0.10	0.00
4.30	2.00	0.00	0.00	0.10	0.00	4.40	2.00	0.00	0.00	0.10	0.00
4.50	2.00	0.00	0.00	0.10	0.00	4.60	2.00	0.00	0.00	0.10	0.00
4.70	2.00	0.00	0.00	0.10	0.00	4.80	2.00	0.00	0.00	0.10	0.00
4.90	2.00	0.00	0.00	0.10	0.00	5.00	2.00	0.00	0.00	0.10	0.00
5.10	2.00	0.00	0.00	0.10	0.00	5.20	2.00	0.00	0.00	0.10	0.00
5.30	2.00	0.00	0.00	0.10	0.00	5.40	2.00	0.00	0.00	0.10	0.00
5.50	2.00	0.00	0.00	0.10	0.00	5.60	2.00	0.00	0.00	0.10	0.00
5.70	2.00	0.00	0.00	0.10	0.00	5.80	2.00	0.00	0.00	0.10	0.00
5.90	2.00	0.00	0.00	0.10	0.00	6.00	2.00	0.00	0.00	0.10	0.00
6.10	2.00	0.00	0.00	0.10	0.00	6.20	2.00	0.00	0.00	0.10	0.00
6.30	2.00	0.00	0.00	0.10	0.00	6.40	2.00	0.00	0.00	0.10	0.00
6.50	2.00	0.00	0.00	0.10	0.00	6.60	2.00	0.00	0.00	0.10	0.00
6.70	2.00	0.00	0.00	0.10	0.00	6.80	2.00	0.00	0.00	0.10	0.00
6.90	2.00	0.00	0.00	0.10	0.00	7.00	2.00	0.00	0.00	0.10	0.00
7.10	2.00	0.00	0.00	0.10	0.00	7.20	2.00	0.00	0.00	0.10	0.00
7.30	2.00	0.00	0.00	0.10	0.00	7.40	2.00	0.00	0.00	0.10	0.00
7.50	2.00	0.00	0.00	0.10	0.00	7.60	2.00	0.00	0.00	0.10	0.00
7.70	2.00	0.00	0.00	0.10	0.00	7.80	2.00	0.00	0.00	0.10	0.00
7.90	2.00	0.00	0.00	0.10	0.00	8.00	2.00	0.00	0.00	0.10	0.00
8.10	2.00	0.00	0.00	0.10	0.00	8.20	2.00	0.00	0.00	0.10	0.00
8.30	2.00	0.00	0.00	0.10	0.00	8.40	2.00	0.00	0.00	0.10	0.00
8.50	2.00	0.00	0.00	0.10	0.00	8.60	2.00	0.00	0.00	0.10	0.00
8.70	2.00	0.00	0.00	0.10	0.00	8.80	2.00	0.00	0.00	0.10	0.00
8.90	2.00	0.00	0.00	0.10	0.00	9.00	1.35	0.00	0.00	0.10	0.00
9.10	1.00	0.00	0.00	0.10	0.00	9.20	0.84	0.00	0.00	0.10	0.04
9.30	0.84	0.00	0.00	0.10	0.04	9.40	0.93	0.00	0.00	0.10	0.02
9.50	1.00	0.00	0.00	0.10	0.00	9.60	0.96	0.00	0.00	0.10	0.01

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
9.70	0.80	0.00	0.00	0.10	0.05	9.80	1.03	0.00	0.00	0.10	0.00
9.90	1.75	0.00	0.00	0.10	0.00	10.00	2.00	0.00	0.00	0.10	0.00
10.10	2.00	0.00	0.00	0.10	0.00	10.20	1.93	0.00	0.00	0.10	0.00
10.30	1.42	0.00	0.00	0.10	0.00	10.40	1.34	0.00	0.00	0.10	0.00
10.50	2.00	0.00	0.00	0.10	0.00	10.60	2.00	0.00	0.00	0.10	0.00
10.70	2.00	0.00	0.00	0.10	0.00	10.80	2.00	0.00	0.00	0.10	0.00
10.90	2.00	0.00	0.00	0.10	0.00	11.00	2.00	0.00	0.00	0.10	0.00
11.10	2.00	0.00	0.00	0.10	0.00	11.20	2.00	0.00	0.00	0.10	0.00
11.30	2.00	0.00	0.00	0.10	0.00	11.40	0.73	0.00	0.00	0.10	0.07
11.50	0.68	0.32	0.83	0.10	0.08	11.60	0.63	0.37	0.70	0.10	0.09
11.70	0.57	0.43	0.57	0.10	0.11	11.80	0.50	0.50	0.48	0.10	0.12
11.90	0.45	0.55	0.43	0.10	0.14	12.00	0.41	0.59	0.39	0.10	0.15
12.10	0.37	0.63	0.36	0.10	0.16	12.20	0.35	0.65	0.35	0.10	0.16
12.30	0.34	0.66	0.35	0.10	0.16	12.40	0.35	0.65	0.35	0.10	0.16
12.50	0.35	0.65	0.35	0.10	0.16	12.60	0.35	0.65	0.35	0.10	0.16
12.70	2.00	0.00	0.00	0.10	0.00	12.80	2.00	0.00	0.00	0.10	0.00
12.90	2.00	0.00	0.00	0.10	0.00	13.00	2.00	0.00	0.00	0.10	0.00
13.10	2.00	0.00	0.00	0.10	0.00	13.20	2.00	0.00	0.00	0.10	0.00
13.30	2.00	0.00	0.00	0.10	0.00	13.40	2.00	0.00	0.00	0.10	0.00
13.50	2.00	0.00	0.00	0.10	0.00	13.60	1.96	0.00	0.00	0.10	0.00
13.70	1.87	0.00	0.00	0.10	0.00	13.80	1.80	0.00	0.00	0.10	0.00
13.90	1.73	0.00	0.00	0.10	0.00	14.00	1.59	0.00	0.00	0.10	0.00
14.10	1.45	0.00	0.00	0.10	0.00	14.20	1.33	0.00	0.00	0.10	0.00
14.30	1.09	0.00	0.00	0.10	0.00	14.40	0.70	0.00	0.00	0.10	0.07
14.50	0.32	0.68	0.33	0.10	0.16	14.60	0.16	0.84	0.26	0.10	0.20
14.70	0.15	0.85	0.26	0.10	0.20	14.80	0.15	0.85	0.26	0.10	0.20
14.90	0.13	0.87	0.25	0.10	0.20	15.00	0.09	0.91	0.24	0.10	0.21
15.10	0.05	0.95	0.23	0.10	0.22	15.20	0.03	0.97	0.22	0.10	0.23
15.30	0.03	0.97	0.22	0.10	0.23	15.40	0.05	0.95	0.23	0.10	0.22
15.50	0.11	0.89	0.25	0.10	0.21	15.60	0.28	0.72	0.31	0.10	0.17
15.70	0.58	0.42	0.59	0.10	0.10	15.80	0.90	0.00	0.00	0.10	0.02
15.90	1.04	0.00	0.00	0.10	0.00	16.00	0.96	0.00	0.00	0.10	0.01
16.10	0.76	0.00	0.00	0.10	0.05	16.20	0.58	0.42	0.60	0.10	0.10
16.30	0.50	0.50	0.47	0.10	0.12	16.40	0.46	0.54	0.43	0.10	0.12
16.50	0.43	0.57	0.41	0.10	0.13	16.60	0.38	0.62	0.37	0.10	0.14
16.70	0.29	0.71	0.32	0.10	0.16	16.80	0.21	0.79	0.28	0.10	0.18
16.90	0.17	0.83	0.27	0.10	0.19	17.00	0.17	0.83	0.26	0.10	0.19
17.10	0.20	0.80	0.28	0.10	0.18	17.20	0.20	0.80	0.28	0.10	0.18
17.30	0.18	0.82	0.27	0.10	0.18	17.40	0.17	0.83	0.27	0.10	0.19
17.50	0.23	0.77	0.29	0.10	0.17	17.60	0.36	0.64	0.36	0.10	0.14
17.70	0.48	0.52	0.46	0.10	0.12	17.80	0.51	0.49	0.49	0.10	0.11
17.90	0.42	0.58	0.40	0.10	0.13	18.00	0.32	0.68	0.33	0.10	0.15
18.10	0.25	0.75	0.30	0.10	0.16	18.20	0.29	0.71	0.32	0.10	0.16
18.30	0.51	0.49	0.49	0.10	0.11	18.40	0.92	0.00	0.00	0.10	0.02
18.50	1.35	0.00	0.00	0.10	0.00	18.60	1.44	0.00	0.00	0.10	0.00
18.70	1.36	0.00	0.00	0.10	0.00	18.80	1.25	0.00	0.00	0.10	0.00
18.90	1.36	0.00	0.00	0.10	0.00	19.00	1.53	0.00	0.00	0.10	0.00
19.10	2.00	0.00	0.00	0.10	0.00	19.20	0.50	0.50	0.48	0.10	0.11

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
19.30	0.41	0.59	0.39	0.10	0.13	19.40	0.82	0.00	0.00	0.10	0.04
19.50	2.00	0.00	0.00	0.10	0.00	19.60	2.00	0.00	0.00	0.10	0.00
19.70	1.77	0.00	0.00	0.10	0.00	19.80	2.00	0.00	0.00	0.10	0.00
19.90	2.00	0.00	0.00	0.10	0.00	20.00	2.00	0.00	0.00	0.10	0.00
20.10	2.00	0.00	0.00	0.10	0.00	20.20	2.00	0.00	0.00	0.10	0.00
20.30	2.00	0.00	0.00	0.10	0.00	20.40	2.00	0.00	0.00	0.10	0.00
20.50	2.00	0.00	0.00	0.10	0.00	20.60	2.00	0.00	0.00	0.10	0.00
20.70	2.00	0.00	0.00	0.10	0.00	20.80	2.00	0.00	0.00	0.10	0.00
20.90	2.00	0.00	0.00	0.10	0.00	21.00	2.00	0.00	0.00	0.10	0.00
21.10	2.00	0.00	0.00	0.10	0.00	21.20	2.00	0.00	0.00	0.10	0.00
21.30	1.12	0.00	0.00	0.10	0.00	21.40	1.07	0.00	0.00	0.10	0.00
21.50	1.02	0.00	0.00	0.10	0.00	21.60	0.98	0.00	0.00	0.10	0.00
21.70	0.95	0.00	0.00	0.10	0.01	21.80	0.93	0.00	0.00	0.10	0.01
21.90	0.96	0.00	0.00	0.10	0.01	22.00	0.99	0.00	0.00	0.10	0.00
22.10	1.01	0.00	0.00	0.10	0.00	22.20	1.02	0.00	0.00	0.10	0.00
22.30	1.07	0.00	0.00	0.10	0.00	22.40	1.18	0.00	0.00	0.10	0.00
22.50	1.29	0.00	0.00	0.10	0.00	22.60	1.38	0.00	0.00	0.10	0.00
22.70	1.45	0.00	0.00	0.10	0.00	22.80	1.49	0.00	0.00	0.10	0.00
22.90	1.52	0.00	0.00	0.10	0.00	23.00	1.55	0.00	0.00	0.10	0.00
23.10	1.61	0.00	0.00	0.10	0.00	23.20	1.69	0.00	0.00	0.10	0.00
23.30	1.69	0.00	0.00	0.10	0.00	23.40	1.56	0.00	0.00	0.10	0.00
23.50	1.34	0.00	0.00	0.10	0.00	23.60	1.14	0.00	0.00	0.10	0.00
23.70	1.02	0.00	0.00	0.10	0.00	23.80	0.96	0.00	0.00	0.10	0.01
23.90	0.93	0.00	0.00	0.10	0.01	24.00	0.90	0.00	0.00	0.10	0.02
24.10	0.82	0.00	0.00	0.10	0.03	24.20	0.62	0.38	0.67	0.10	0.07
24.30	0.41	0.59	0.40	0.10	0.11	24.40	0.28	0.72	0.31	0.10	0.14
24.50	0.26	0.74	0.30	0.10	0.14	24.60	0.26	0.74	0.30	0.10	0.14
24.70	0.27	0.73	0.31	0.10	0.14	24.80	0.29	0.71	0.32	0.10	0.13
24.90	0.32	0.68	0.34	0.10	0.13	25.00	0.35	0.65	0.35	0.10	0.12
25.10	0.35	0.65	0.35	0.10	0.12	25.20	0.32	0.68	0.34	0.10	0.13
25.30	0.29	0.71	0.32	0.10	0.13	25.40	0.26	0.74	0.30	0.10	0.14
25.50	0.25	0.75	0.30	0.10	0.14	25.60	0.25	0.75	0.30	0.10	0.14
25.70	0.25	0.75	0.30	0.10	0.14	25.80	0.24	0.76	0.30	0.10	0.14
25.90	0.25	0.75	0.30	0.10	0.14	26.00	0.26	0.74	0.30	0.10	0.14
26.10	0.27	0.73	0.31	0.10	0.13	26.20	0.26	0.74	0.30	0.10	0.14
26.30	0.24	0.76	0.29	0.10	0.14	26.40	0.24	0.76	0.29	0.10	0.14
26.50	0.24	0.76	0.29	0.10	0.14	26.60	0.27	0.73	0.31	0.10	0.13
26.70	0.30	0.70	0.32	0.10	0.13	26.80	0.32	0.68	0.33	0.10	0.12
26.90	0.32	0.68	0.34	0.10	0.12	27.00	0.34	0.66	0.35	0.10	0.12
27.10	0.38	0.62	0.37	0.10	0.11	27.20	0.46	0.54	0.44	0.10	0.10
27.30	0.66	0.34	0.78	0.10	0.06	27.40	1.03	0.00	0.00	0.10	0.00
27.50	1.59	0.00	0.00	0.10	0.00	27.60	0.90	0.00	0.00	0.10	0.02
27.70	0.52	0.48	0.50	0.10	0.09	27.80	2.00	0.00	0.00	0.10	0.00
27.90	2.00	0.00	0.00	0.10	0.00	28.00	1.90	0.00	0.00	0.10	0.00
28.10	1.51	0.00	0.00	0.10	0.00	28.20	1.21	0.00	0.00	0.10	0.00
28.30	0.97	0.00	0.00	0.10	0.01	28.40	0.77	0.00	0.00	0.10	0.04
28.50	0.61	0.39	0.65	0.10	0.07	28.60	0.60	0.40	0.62	0.10	0.07
28.70	0.73	0.00	0.00	0.10	0.05	28.80	0.92	0.00	0.00	0.10	0.01

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
28.90	1.00	0.00	0.00	0.10	0.00	29.00	0.99	0.00	0.00	0.10	0.00
29.10	0.89	0.00	0.00	0.10	0.02	29.20	0.79	0.00	0.00	0.10	0.04
29.30	0.78	0.00	0.00	0.10	0.04	29.40	0.97	0.00	0.00	0.10	0.01
29.50	1.32	0.00	0.00	0.10	0.00	29.60	2.00	0.00	0.00	0.10	0.00
29.70	2.00	0.00	0.00	0.10	0.00	29.80	2.00	0.00	0.00	0.10	0.00
29.90	2.00	0.00	0.00	0.10	0.00	30.00	2.00	0.00	0.00	0.10	0.00
30.10	2.00	0.00	0.00	0.10	0.00	30.20	2.00	0.00	0.00	0.10	0.00
30.30	2.00	0.00	0.00	0.10	0.00	30.40	2.00	0.00	0.00	0.10	0.00
30.50	2.00	0.00	0.00	0.10	0.00	30.60	2.00	0.00	0.00	0.10	0.00
30.70	2.00	0.00	0.00	0.10	0.00	30.80	2.00	0.00	0.00	0.10	0.00
30.90	2.00	0.00	0.00	0.10	0.00	31.00	2.00	0.00	0.00	0.10	0.00
31.10	2.00	0.00	0.00	0.10	0.00	31.20	2.00	0.00	0.00	0.10	0.00
31.30	2.00	0.00	0.00	0.10	0.00	31.40	2.00	0.00	0.00	0.10	0.00
31.50	0.32	0.68	0.33	0.10	0.11	31.60	0.31	0.69	0.33	0.10	0.11
31.70	0.30	0.70	0.32	0.10	0.11	31.80	2.00	0.00	0.00	0.10	0.00
31.90	2.00	0.00	0.00	0.10	0.00	32.00	2.00	0.00	0.00	0.10	0.00
32.10	2.00	0.00	0.00	0.10	0.00	32.20	2.00	0.00	0.00	0.10	0.00
32.30	2.00	0.00	0.00	0.10	0.00	32.40	2.00	0.00	0.00	0.10	0.00
32.50	0.35	0.65	0.35	0.10	0.10	32.60	0.29	0.71	0.32	0.10	0.11
32.70	0.27	0.73	0.31	0.10	0.11	32.80	0.29	0.71	0.32	0.10	0.11
32.90	0.33	0.67	0.34	0.10	0.10	33.00	0.38	0.62	0.37	0.10	0.09
33.10	0.41	0.59	0.39	0.10	0.09	33.20	0.45	0.55	0.42	0.10	0.08
33.30	0.52	0.48	0.50	0.10	0.07	33.40	0.60	0.40	0.64	0.10	0.06
33.50	0.67	0.33	0.81	0.10	0.05	33.60	0.68	0.32	0.86	0.10	0.05
33.70	0.67	0.33	0.81	0.10	0.05	33.80	0.65	0.35	0.76	0.10	0.05
33.90	0.64	0.36	0.73	0.10	0.05	34.00	0.63	0.37	0.69	0.10	0.05
34.10	0.61	0.39	0.65	0.10	0.06	34.20	0.58	0.42	0.60	0.10	0.06
34.30	0.56	0.44	0.57	0.10	0.06	34.40	0.55	0.45	0.54	0.10	0.07
34.50	0.53	0.47	0.51	0.10	0.07	34.60	0.51	0.49	0.49	0.10	0.07
34.70	0.50	0.50	0.48	0.10	0.07	34.80	0.49	0.51	0.46	0.10	0.07
34.90	0.47	0.53	0.44	0.10	0.08	35.00	0.44	0.56	0.42	0.10	0.08
35.10	0.41	0.59	0.40	0.10	0.08	35.20	0.40	0.60	0.39	0.10	0.08
35.30	0.40	0.60	0.38	0.10	0.08	35.40	0.38	0.62	0.37	0.10	0.09
35.50	0.33	0.67	0.34	0.10	0.09	35.60	0.30	0.70	0.32	0.10	0.10
35.70	0.28	0.72	0.31	0.10	0.10	35.80	0.29	0.71	0.32	0.10	0.10
35.90	0.30	0.70	0.32	0.10	0.10	36.00	0.33	0.67	0.34	0.10	0.09
36.10	0.36	0.64	0.36	0.10	0.09	36.20	0.41	0.59	0.40	0.10	0.08
36.30	0.47	0.53	0.45	0.10	0.07	36.40	0.53	0.47	0.52	0.10	0.06
36.50	0.58	0.42	0.59	0.10	0.06	36.60	2.00	0.00	0.00	0.10	0.00
36.70	2.00	0.00	0.00	0.10	0.00	36.80	2.00	0.00	0.00	0.10	0.00
36.90	2.00	0.00	0.00	0.10	0.00	37.00	2.00	0.00	0.00	0.10	0.00
37.10	2.00	0.00	0.00	0.10	0.00	37.20	2.00	0.00	0.00	0.10	0.00
37.30	1.87	0.00	0.00	0.10	0.00	37.40	1.86	0.00	0.00	0.10	0.00
37.50	2.00	0.00	0.00	0.10	0.00	37.60	0.68	0.32	0.84	0.10	0.04
37.70	0.36	0.64	0.36	0.10	0.08	37.80	0.36	0.64	0.35	0.10	0.08
37.90	0.36	0.64	0.36	0.10	0.08	38.00	0.35	0.65	0.35	0.10	0.08
38.10	0.32	0.68	0.33	0.10	0.09	38.20	0.30	0.70	0.32	0.10	0.09
38.30	0.30	0.70	0.32	0.10	0.09	38.40	0.32	0.68	0.33	0.10	0.09

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
38.50	0.33	0.67	0.34	0.10	0.08	38.60	0.33	0.67	0.34	0.10	0.08
38.70	0.32	0.68	0.33	0.10	0.08	38.80	0.31	0.69	0.33	0.10	0.09
38.90	0.30	0.70	0.32	0.10	0.09	39.00	0.28	0.72	0.31	0.10	0.09
39.10	0.25	0.75	0.30	0.10	0.09	39.20	2.00	0.00	0.00	0.10	0.00
39.30	2.00	0.00	0.00	0.10	0.00	39.40	2.00	0.00	0.00	0.10	0.00
39.50	2.00	0.00	0.00	0.10	0.00	39.60	2.00	0.00	0.00	0.10	0.00
39.70	2.00	0.00	0.00	0.10	0.00	39.80	2.00	0.00	0.00	0.10	0.00
39.90	0.95	0.00	0.00	0.10	0.01	40.00	1.07	0.00	0.00	0.10	0.00
40.10	0.96	0.00	0.00	0.10	0.01	40.20	0.60	0.40	0.63	0.10	0.05
40.30	0.34	0.66	0.34	0.10	0.08	40.40	0.37	0.63	0.37	0.10	0.07
40.50	0.50	0.50	0.48	0.10	0.06	40.60	0.67	0.33	0.82	0.10	0.04
40.70	0.89	0.00	0.00	0.10	0.01	40.80	1.12	0.00	0.00	0.10	0.00
40.90	1.28	0.00	0.00	0.10	0.00	41.00	1.34	0.00	0.00	0.10	0.00
41.10	1.32	0.00	0.00	0.10	0.00	41.20	1.33	0.00	0.00	0.10	0.00
41.30	1.42	0.00	0.00	0.10	0.00	41.40	1.48	0.00	0.00	0.10	0.00
41.50	1.49	0.00	0.00	0.10	0.00	41.60	1.42	0.00	0.00	0.10	0.00
41.70	1.38	0.00	0.00	0.10	0.00	41.80	2.00	0.00	0.00	0.10	0.00
41.90	2.00	0.00	0.00	0.10	0.00	42.00	2.00	0.00	0.00	0.10	0.00
42.10	2.00	0.00	0.00	0.10	0.00	42.20	2.00	0.00	0.00	0.10	0.00
42.30	2.00	0.00	0.00	0.10	0.00	42.40	2.00	0.00	0.00	0.10	0.00
42.50	0.74	0.00	0.00	0.10	0.03	42.60	0.85	0.00	0.00	0.10	0.02
42.70	0.86	0.00	0.00	0.10	0.01	42.80	2.00	0.00	0.00	0.10	0.00
42.90	2.00	0.00	0.00	0.10	0.00	43.00	2.00	0.00	0.00	0.10	0.00
43.10	2.00	0.00	0.00	0.10	0.00	43.20	2.00	0.00	0.00	0.10	0.00
43.30	2.00	0.00	0.00	0.10	0.00	43.40	2.00	0.00	0.00	0.10	0.00
43.50	2.00	0.00	0.00	0.10	0.00	43.60	2.00	0.00	0.00	0.10	0.00
43.70	2.00	0.00	0.00	0.10	0.00	43.80	2.00	0.00	0.00	0.10	0.00
43.90	2.00	0.00	0.00	0.10	0.00	44.00	2.00	0.00	0.00	0.10	0.00
44.10	2.00	0.00	0.00	0.10	0.00	44.20	2.00	0.00	0.00	0.10	0.00
44.30	2.00	0.00	0.00	0.10	0.00	44.40	2.00	0.00	0.00	0.10	0.00
44.50	2.00	0.00	0.00	0.10	0.00	44.60	2.00	0.00	0.00	0.10	0.00
44.70	2.00	0.00	0.00	0.10	0.00	44.80	2.00	0.00	0.00	0.10	0.00
44.90	2.00	0.00	0.00	0.10	0.00	45.00	2.00	0.00	0.00	0.10	0.00
45.10	2.00	0.00	0.00	0.10	0.00	45.20	0.57	0.43	0.57	0.10	0.04
45.30	2.00	0.00	0.00	0.10	0.00	45.40	2.00	0.00	0.00	0.10	0.00
45.50	2.00	0.00	0.00	0.10	0.00	45.60	2.00	0.00	0.00	0.10	0.00
45.70	2.00	0.00	0.00	0.10	0.00	45.80	2.00	0.00	0.00	0.10	0.00
45.90	2.00	0.00	0.00	0.10	0.00	46.00	0.88	0.00	0.00	0.10	0.01
46.10	2.00	0.00	0.00	0.10	0.00	46.20	2.00	0.00	0.00	0.10	0.00
46.30	2.00	0.00	0.00	0.10	0.00	46.40	2.00	0.00	0.00	0.10	0.00
46.50	2.00	0.00	0.00	0.10	0.00	46.60	2.00	0.00	0.00	0.10	0.00
46.70	0.39	0.61	0.38	0.10	0.05	46.80	0.45	0.55	0.43	0.10	0.05
46.90	0.51	0.49	0.49	0.10	0.04	47.00	0.58	0.42	0.59	0.10	0.04
47.10	0.66	0.34	0.78	0.10	0.03	47.20	0.70	0.00	0.00	0.10	0.03
47.30	0.67	0.33	0.82	0.10	0.03	47.40	0.62	0.38	0.68	0.10	0.03
47.50	0.60	0.40	0.64	0.10	0.03	47.60	0.63	0.37	0.71	0.10	0.03
47.70	0.70	0.00	0.00	0.10	0.03	47.80	0.77	0.00	0.00	0.10	0.02
47.90	0.82	0.00	0.00	0.10	0.01	48.00	0.85	0.00	0.00	0.10	0.01

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
48.10	0.86	0.00	0.00	0.10	0.01	48.20	0.88	0.00	0.00	0.10	0.01
48.30	0.89	0.00	0.00	0.10	0.01	48.40	0.91	0.00	0.00	0.10	0.01
48.50	0.91	0.00	0.00	0.10	0.01	48.60	0.90	0.00	0.00	0.10	0.01
48.70	0.90	0.00	0.00	0.10	0.01	48.80	0.89	0.00	0.00	0.10	0.01
48.90	0.90	0.00	0.00	0.10	0.01	49.00	0.91	0.00	0.00	0.10	0.01
49.10	0.94	0.00	0.00	0.10	0.00	49.20	0.97	0.00	0.00	0.10	0.00
49.30	1.02	0.00	0.00	0.10	0.00	49.40	2.00	0.00	0.00	0.10	0.00
49.50	2.00	0.00	0.00	0.10	0.00	49.60	1.00	0.00	0.00	0.10	0.00
49.70	0.92	0.00	0.00	0.10	0.01	49.80	0.88	0.00	0.00	0.10	0.01
49.90	0.89	0.00	0.00	0.10	0.01						

Overall liquefaction potential: 18.65

LPI = 0.00 - Liquefaction risk very low

LPI between 0.00 and 5.00 - Liquefaction risk low

LPI between 5.00 and 15.00 - Liquefaction risk high

LPI > 15.00 - Liquefaction risk very high

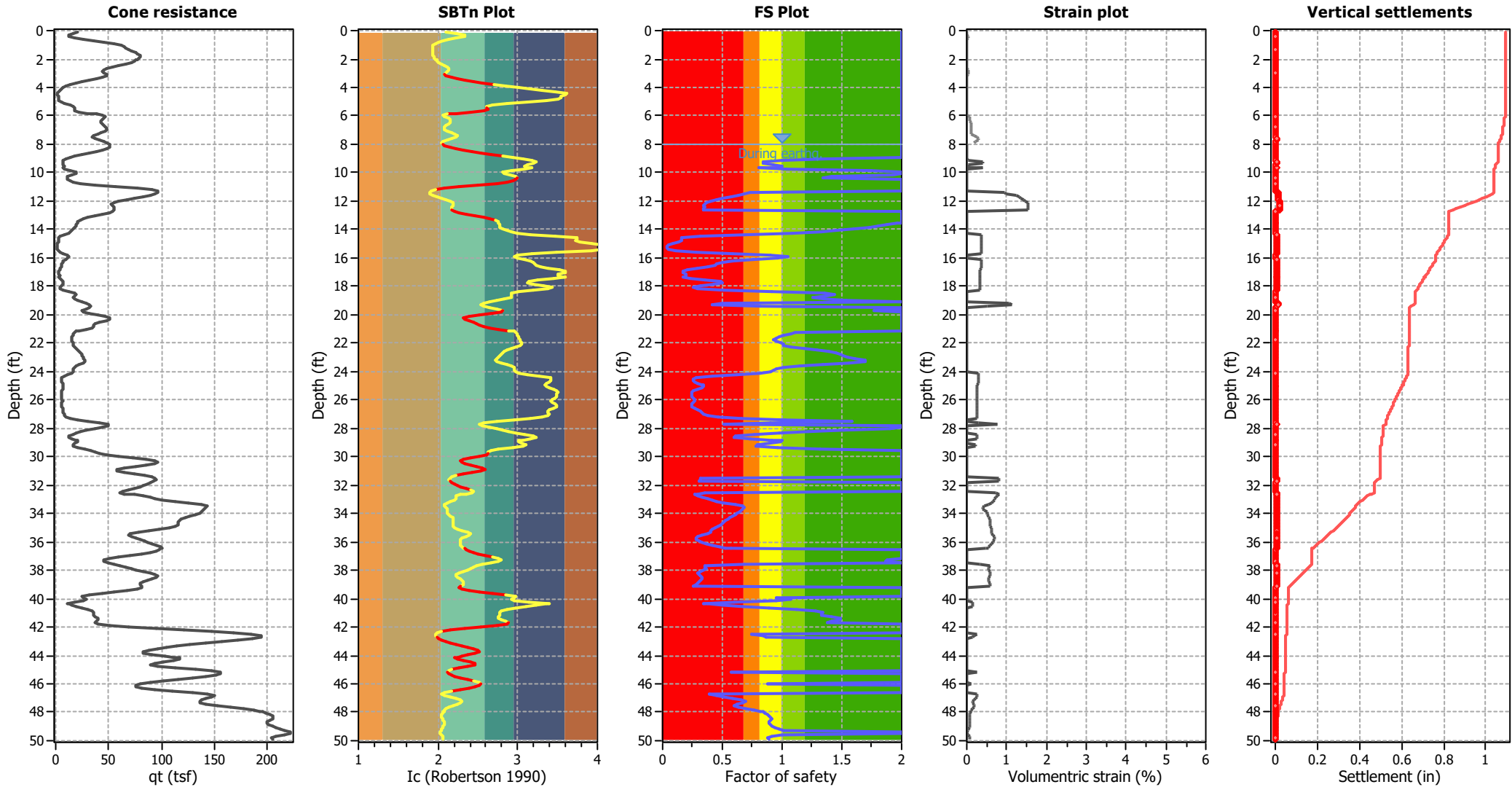
Abbreviations

FS: Calculated factor of safety for test point

F_L: 1 - FSw_z: Function value of the extend of soil liquefaction according to depthd_z: Layer thickness (ft)

LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

- q_c : Total cone resistance (cone resistance q_c corrected for pore water effects)
- I_c : Soil Behaviour Type Index
- FS: Calculated Factor of Safety against liquefaction
- Volumetric strain: Post-liquefaction volumetric strain

:: Post-earthquake settlement of dry sands ::												
Depth (ft)	Ic	Q _{tn}	Kc	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _r (%)	Settle. (in)
0.10	2.10	39.10	1.42	55.57	12	266	0.59	0.001	0.00	13.69	0.00	0.000
0.20	2.22	30.12	1.66	49.90	11	237	0.59	0.004	0.01	13.69	0.01	0.000
0.30	2.34	23.21	2.10	48.70	12	215	0.59	0.009	0.02	13.69	0.02	0.000
0.40	2.33	24.26	2.06	50.09	12	222	0.59	0.013	0.02	13.69	0.02	0.000
0.50	2.22	33.84	1.67	56.52	13	268	0.59	0.011	0.02	13.69	0.02	0.000
0.60	2.13	48.33	1.47	71.07	16	342	0.59	0.009	0.01	13.69	0.01	0.000
0.70	2.06	67.26	1.36	91.66	20	433	0.59	0.007	0.01	13.69	0.01	0.000
0.80	2.00	86.49	1.31	113.12	24	519	0.59	0.006	0.00	13.69	0.00	0.000
0.90	1.96	103.99	1.28	132.90	27	594	0.59	0.006	0.00	13.69	0.00	0.000
1.00	1.94	117.06	1.26	147.81	30	650	0.59	0.006	0.00	13.69	0.00	0.000
1.10	1.94	123.52	1.26	155.65	32	682	0.59	0.006	0.00	13.69	0.00	0.000
1.20	1.94	126.01	1.26	159.05	32	699	0.59	0.006	0.00	13.69	0.00	0.000
1.30	1.94	129.90	1.26	163.96	33	720	0.59	0.007	0.00	13.69	0.00	0.000
1.40	1.93	136.11	1.26	171.44	35	751	0.59	0.007	0.00	13.69	0.00	0.000
1.50	1.93	142.50	1.26	179.17	36	783	0.59	0.007	0.00	13.69	0.00	0.000
1.60	1.93	146.84	1.26	184.84	38	809	0.59	0.007	0.00	13.69	0.00	0.000
1.70	1.94	149.99	1.26	189.22	38	830	0.59	0.008	0.00	13.69	0.00	0.000
1.80	1.95	150.87	1.27	191.13	39	844	0.59	0.008	0.00	13.69	0.00	0.000
1.90	1.96	148.63	1.28	189.63	39	845	0.59	0.009	0.00	13.69	0.00	0.000
2.00	1.97	146.34	1.28	187.97	39	845	0.59	0.009	0.00	13.69	0.00	0.000
2.10	1.98	144.27	1.29	186.30	38	843	0.59	0.010	0.00	13.69	0.00	0.000
2.20	1.99	141.43	1.30	183.85	38	838	0.59	0.011	0.00	13.69	0.00	0.000
2.30	2.01	135.91	1.32	178.97	37	826	0.59	0.012	0.01	13.69	0.01	0.000
2.40	2.05	125.64	1.35	169.63	36	798	0.59	0.013	0.01	13.69	0.01	0.000
2.50	2.08	112.81	1.40	157.60	34	753	0.59	0.016	0.01	13.69	0.01	0.000
2.60	2.12	100.62	1.44	145.16	32	698	0.59	0.019	0.01	13.69	0.01	0.000
2.70	2.13	91.49	1.47	134.49	29	648	0.59	0.024	0.02	13.69	0.01	0.000
2.80	2.13	85.34	1.48	125.91	28	607	0.59	0.030	0.02	13.69	0.02	0.000
2.90	2.12	83.45	1.45	120.83	26	581	0.59	0.036	0.03	13.69	0.02	0.000
3.00	2.09	86.52	1.40	121.48	26	581	0.59	0.038	0.03	13.69	0.02	0.000
3.10	2.08	90.93	1.39	126.32	27	602	0.59	0.036	0.03	13.69	0.02	0.000
3.20	2.11	90.59	1.43	129.35	0	0	0.59	0.000	0.00	13.69	0.00	0.000
3.30	2.17	83.59	1.54	128.66	0	0	0.59	0.000	0.00	13.69	0.00	0.000
3.40	2.25	72.24	1.75	126.16	0	0	0.59	0.000	0.00	13.69	0.00	0.000
3.50	2.34	59.45	2.08	123.67	0	0	0.59	0.000	0.00	13.69	0.00	0.000
3.60	2.44	46.88	2.61	122.26	0	0	0.59	0.000	0.00	13.69	0.00	0.000
3.70	2.56	35.38	3.44	121.77	0	0	0.59	0.000	0.00	0.00	0.00	0.000
3.80	2.70	25.84	4.69	121.11	0	0	0.59	0.000	0.00	0.00	0.00	0.000
3.90	2.85	18.15	6.50	118.04	0	0	0.59	0.000	0.00	0.00	0.00	0.000
4.00	3.01	12.24	9.02	110.41	0	0	0.59	0.000	0.00	0.00	0.00	0.000
4.10	3.16	8.50	11.89	101.07	0	0	0.59	0.000	0.00	0.00	0.00	0.000
4.20	3.31	5.78	15.54	89.83	0	0	0.59	0.000	0.00	0.00	0.00	0.000
4.30	3.47	3.84	20.36	78.22	0	0	0.59	0.000	0.00	0.00	0.00	0.000
4.40	3.62	2.61	26.07	67.99	0	0	0.59	0.000	0.00	0.00	0.00	0.000
4.50	3.60	2.70	25.15	67.85	0	0	0.59	0.000	0.00	0.00	0.00	0.000
4.60	3.55	3.10	23.18	71.75	0	0	0.59	0.000	0.00	0.00	0.00	0.000
4.70	3.54	3.27	22.94	75.00	0	0	0.59	0.000	0.00	0.00	0.00	0.000
4.80	3.50	3.79	21.46	81.39	0	0	0.59	0.000	0.00	0.00	0.00	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
4.90	3.36	5.30	16.96	89.83	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.00	3.12	8.96	11.09	99.38	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.10	2.87	15.24	6.81	103.82	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.20	2.69	24.00	4.60	110.26	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.30	2.61	31.66	3.85	122.01	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.40	2.61	34.25	3.86	132.22	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.50	2.63	33.10	4.04	133.70	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.60	2.58	33.93	3.58	121.46	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.70	2.41	42.11	2.45	103.16	0	0	0.59	0.000	0.00	13.69	0.00	0.000
5.80	2.23	56.74	1.69	96.02	0	0	0.59	0.000	0.00	13.69	0.00	0.000
5.90	2.11	72.46	1.43	103.65	0	0	0.58	0.000	0.00	13.69	0.00	0.000
6.00	2.07	83.32	1.38	114.74	0	0	0.58	0.000	0.00	13.69	0.00	0.000
6.10	2.09	87.31	1.40	122.36	26	585	0.58	0.136	0.10	13.69	0.08	0.001
6.20	2.13	85.81	1.46	125.37	27	604	0.58	0.125	0.09	13.69	0.07	0.001
6.30	2.16	82.83	1.51	125.44	28	604	0.58	0.129	0.09	13.69	0.07	0.001
6.40	2.16	81.10	1.53	123.81	27	596	0.58	0.140	0.10	13.69	0.08	0.001
6.50	2.15	81.14	1.50	121.74	27	587	0.58	0.155	0.11	13.69	0.09	0.001
6.60	2.13	82.67	1.46	120.61	26	581	0.58	0.167	0.12	13.69	0.10	0.001
6.70	2.10	84.41	1.42	120.00	26	578	0.58	0.176	0.13	13.69	0.11	0.001
6.80	2.08	85.54	1.40	119.50	26	583	0.58	0.177	0.13	13.69	0.11	0.001
6.90	2.08	86.62	1.39	120.05	26	591	0.58	0.172	0.13	13.69	0.11	0.001
7.00	2.09	86.40	1.40	120.86	26	601	0.58	0.167	0.12	13.69	0.10	0.001
7.10	2.12	83.70	1.45	121.17	26	605	0.58	0.168	0.12	13.69	0.10	0.001
7.20	2.17	78.48	1.54	120.81	27	599	0.58	0.181	0.13	13.69	0.11	0.001
7.30	2.22	71.76	1.65	118.75	27	577	0.58	0.217	0.15	13.69	0.13	0.002
7.40	2.24	65.71	1.73	113.59	26	547	0.58	0.286	0.21	13.69	0.17	0.002
7.50	2.23	62.81	1.68	105.75	24	520	0.58	0.376	0.30	13.69	0.25	0.003
7.60	2.17	64.29	1.55	99.54	22	511	0.58	0.426	0.38	13.69	0.31	0.004
7.70	2.11	69.26	1.43	99.23	22	524	0.58	0.386	0.35	13.69	0.29	0.003
7.80	2.07	75.11	1.37	103.22	22	551	0.58	0.314	0.28	13.69	0.23	0.003
7.90	2.05	79.59	1.36	107.93	23	581	0.58	0.257	0.22	13.69	0.18	0.002

Total estimated settlement: 0.04**Abbreviations**

Q_{tn}: Equivalent clean sand normalized cone resistance
 K_c: Fines correction factor
 Q_{tn,cs}: Post-liquefaction volumetric strain
 G_{max}: Small strain shear modulus
 CSR: Soil cyclic stress ratio
 γ: Cyclic shear strain
 e_{vol(15)}: Volumetric strain after 15 cycles
 N_c: Equivalent number of cycles
 e_v: Volumetric strain
 Settle.: Calculated settlement

:: Post-earthquake settlement due to soil liquefaction ::

Depth (ft)	Q _{tn,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	Q _{tn,cs}	FS	e _v (%)	DF	Settlement (in)
8.00	111.75	2.00	0.00	0.85	0.00	8.10	116.05	2.00	0.00	0.85	0.00
8.20	125.21	2.00	0.00	0.85	0.00	8.30	138.70	2.00	0.00	0.85	0.00
8.40	155.46	2.00	0.00	0.85	0.00	8.50	170.95	2.00	0.00	0.85	0.00
8.60	202.51	2.00	0.00	0.84	0.00	8.70	365.20	2.00	0.00	0.84	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
8.80	197.84	2.00	0.00	0.84	0.00	8.90	192.66	2.00	0.00	0.84	0.00
9.00	178.13	1.35	0.01	0.84	0.00	9.10	160.97	1.00	0.02	0.83	0.00
9.20	147.24	0.84	0.42	0.83	0.00	9.30	140.62	0.84	0.42	0.83	0.00
9.40	138.06	0.93	0.03	0.83	0.00	9.50	136.69	1.00	0.02	0.83	0.00
9.60	135.30	0.96	0.02	0.83	0.00	9.70	130.39	0.80	0.41	0.82	0.00
9.80	146.02	1.03	0.02	0.82	0.00	9.90	180.56	1.75	0.00	0.82	0.00
10.00	208.85	2.00	0.00	0.82	0.00	10.10	209.42	2.00	0.00	0.82	0.00
10.20	190.32	1.93	0.00	0.81	0.00	10.30	166.51	1.42	0.00	0.81	0.00
10.40	162.44	1.34	0.01	0.81	0.00	10.50	167.34	2.00	0.00	0.81	0.00
10.60	184.96	2.00	0.00	0.81	0.00	10.70	198.61	2.00	0.00	0.81	0.00
10.80	204.26	2.00	0.00	0.80	0.00	10.90	173.93	2.00	0.00	0.80	0.00
11.00	159.82	2.00	0.00	0.80	0.00	11.10	159.68	2.00	0.00	0.80	0.00
11.20	166.80	2.00	0.00	0.80	0.00	11.30	168.36	2.00	0.00	0.79	0.00
11.40	165.51	0.73	0.95	0.79	0.01	11.50	161.18	0.68	0.99	0.79	0.01
11.60	156.72	0.63	1.25	0.79	0.01	11.70	150.52	0.57	1.32	0.79	0.02
11.80	142.88	0.50	1.37	0.79	0.02	11.90	136.60	0.45	1.42	0.78	0.02
12.00	130.39	0.41	1.47	0.78	0.02	12.10	124.95	0.37	1.52	0.78	0.02
12.20	121.82	0.35	1.55	0.78	0.02	12.30	120.93	0.34	1.55	0.78	0.02
12.40	122.10	0.35	1.54	0.77	0.02	12.50	121.95	0.35	1.53	0.77	0.02
12.60	122.09	0.35	1.53	0.77	0.02	12.70	125.14	2.00	0.00	0.77	0.00
12.80	130.74	2.00	0.00	0.77	0.00	12.90	138.07	2.00	0.00	0.77	0.00
13.00	150.09	2.00	0.00	0.76	0.00	13.10	206.70	2.00	0.00	0.76	0.00
13.20	306.09	2.00	0.00	0.76	0.00	13.30	171.29	2.00	0.00	0.76	0.00
13.40	168.19	2.00	0.00	0.76	0.00	13.50	165.57	2.00	0.00	0.75	0.00
13.60	163.90	1.96	0.00	0.75	0.00	13.70	159.27	1.87	0.00	0.75	0.00
13.80	154.30	1.80	0.00	0.75	0.00	13.90	152.22	1.73	0.00	0.75	0.00
14.00	152.62	1.59	0.00	0.75	0.00	14.10	154.31	1.45	0.00	0.74	0.00
14.20	156.38	1.33	0.00	0.74	0.00	14.30	150.24	1.09	0.01	0.74	0.00
14.40	131.58	0.70	0.37	0.74	0.00	14.50	101.58	0.32	0.37	0.74	0.00
14.60	80.21	0.16	0.37	0.73	0.00	14.70	78.12	0.15	0.37	0.73	0.00
14.80	75.98	0.15	0.37	0.73	0.00	14.90	71.06	0.13	0.36	0.73	0.00
15.00	63.39	0.09	0.36	0.73	0.00	15.10	44.18	0.05	0.36	0.73	0.00
15.20	28.39	0.03	0.36	0.72	0.00	15.30	27.97	0.03	0.36	0.72	0.00
15.40	43.31	0.05	0.36	0.72	0.00	15.50	77.37	0.11	0.36	0.72	0.00
15.60	97.25	0.28	0.36	0.72	0.00	15.70	115.74	0.58	0.36	0.71	0.00
15.80	129.53	0.90	0.02	0.71	0.00	15.90	137.10	1.04	0.01	0.71	0.00
16.00	137.25	0.96	0.01	0.71	0.00	16.10	129.07	0.76	0.35	0.71	0.00
16.20	114.76	0.58	0.35	0.71	0.00	16.30	104.02	0.50	0.35	0.70	0.00
16.40	99.12	0.46	0.35	0.70	0.00	16.50	97.25	0.43	0.35	0.70	0.00
16.60	92.99	0.38	0.35	0.70	0.00	16.70	85.54	0.29	0.35	0.70	0.00
16.80	76.36	0.21	0.35	0.69	0.00	16.90	71.23	0.17	0.35	0.69	0.00
17.00	69.38	0.17	0.35	0.69	0.00	17.10	72.39	0.20	0.34	0.69	0.00
17.20	73.85	0.20	0.34	0.69	0.00	17.30	73.25	0.18	0.34	0.69	0.00
17.40	72.92	0.17	0.34	0.68	0.00	17.50	77.63	0.23	0.34	0.68	0.00
17.60	86.38	0.36	0.34	0.68	0.00	17.70	93.63	0.48	0.34	0.68	0.00
17.80	95.85	0.51	0.34	0.68	0.00	17.90	92.87	0.42	0.34	0.67	0.00
18.00	87.15	0.32	0.34	0.67	0.00	18.10	83.11	0.25	0.34	0.67	0.00
18.20	88.54	0.29	0.33	0.67	0.00	18.30	111.00	0.51	0.33	0.67	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
18.40	144.21	0.92	0.01	0.67	0.00	18.50	174.91	1.35	0.00	0.66	0.00
18.60	185.92	1.44	0.00	0.66	0.00	18.70	181.17	1.36	0.00	0.66	0.00
18.80	162.95	1.25	0.00	0.66	0.00	18.90	149.63	1.36	0.00	0.66	0.00
19.00	138.46	1.53	0.00	0.65	0.00	19.10	223.64	2.00	0.00	0.65	0.00
19.20	154.24	0.50	1.07	0.65	0.01	19.30	141.96	0.41	1.14	0.65	0.01
19.40	187.11	0.82	0.53	0.65	0.01	19.50	297.13	2.00	0.00	0.65	0.00
19.60	187.09	2.00	0.00	0.64	0.00	19.70	189.60	1.77	0.00	0.64	0.00
19.80	184.75	2.00	0.00	0.64	0.00	19.90	336.45	2.00	0.00	0.64	0.00
20.00	161.15	2.00	0.00	0.64	0.00	20.10	133.96	2.00	0.00	0.63	0.00
20.20	120.70	2.00	0.00	0.63	0.00	20.30	125.66	2.00	0.00	0.63	0.00
20.40	131.65	2.00	0.00	0.63	0.00	20.50	131.07	2.00	0.00	0.63	0.00
20.60	127.22	2.00	0.00	0.63	0.00	20.70	134.45	2.00	0.00	0.62	0.00
20.80	188.86	2.00	0.00	0.62	0.00	20.90	305.62	2.00	0.00	0.62	0.00
21.00	186.05	2.00	0.00	0.62	0.00	21.10	187.10	2.00	0.00	0.62	0.00
21.20	178.64	2.00	0.00	0.61	0.00	21.30	170.13	1.12	0.01	0.61	0.00
21.40	165.68	1.07	0.01	0.61	0.00	21.50	161.39	1.02	0.01	0.61	0.00
21.60	157.77	0.98	0.01	0.61	0.00	21.70	155.16	0.95	0.01	0.61	0.00
21.80	156.12	0.93	0.01	0.60	0.00	21.90	163.21	0.96	0.01	0.60	0.00
22.00	170.98	0.99	0.01	0.60	0.00	22.10	174.52	1.01	0.01	0.60	0.00
22.20	171.13	1.02	0.01	0.60	0.00	22.30	165.61	1.07	0.01	0.59	0.00
22.40	162.66	1.18	0.00	0.59	0.00	22.50	160.68	1.29	0.00	0.59	0.00
22.60	158.98	1.38	0.00	0.59	0.00	22.70	157.52	1.45	0.00	0.59	0.00
22.80	157.34	1.49	0.00	0.59	0.00	22.90	156.78	1.52	0.00	0.58	0.00
23.00	153.41	1.55	0.00	0.58	0.00	23.10	149.33	1.61	0.00	0.58	0.00
23.20	150.73	1.69	0.00	0.58	0.00	23.30	157.89	1.69	0.00	0.58	0.00
23.40	165.31	1.56	0.00	0.57	0.00	23.50	166.04	1.34	0.00	0.57	0.00
23.60	160.07	1.14	0.00	0.57	0.00	23.70	150.55	1.02	0.01	0.57	0.00
23.80	142.73	0.96	0.01	0.57	0.00	23.90	139.01	0.93	0.01	0.57	0.00
24.00	138.60	0.90	0.01	0.56	0.00	24.10	136.16	0.82	0.28	0.56	0.00
24.20	125.22	0.62	0.28	0.56	0.00	24.30	109.35	0.41	0.28	0.56	0.00
24.40	94.56	0.28	0.28	0.56	0.00	24.50	89.77	0.26	0.28	0.55	0.00
24.60	87.89	0.26	0.28	0.55	0.00	24.70	88.79	0.27	0.28	0.55	0.00
24.80	93.57	0.29	0.27	0.55	0.00	24.90	99.86	0.32	0.27	0.55	0.00
25.00	105.93	0.35	0.27	0.55	0.00	25.10	109.82	0.35	0.27	0.54	0.00
25.20	109.92	0.32	0.27	0.54	0.00	25.30	106.76	0.29	0.27	0.54	0.00
25.40	102.13	0.26	0.27	0.54	0.00	25.50	99.16	0.25	0.27	0.54	0.00
25.60	98.13	0.25	0.27	0.53	0.00	25.70	97.77	0.25	0.27	0.53	0.00
25.80	96.87	0.24	0.27	0.53	0.00	25.90	95.31	0.25	0.26	0.53	0.00
26.00	94.48	0.26	0.26	0.53	0.00	26.10	94.04	0.27	0.26	0.53	0.00
26.20	94.06	0.26	0.26	0.52	0.00	26.30	93.92	0.24	0.26	0.52	0.00
26.40	94.95	0.24	0.26	0.52	0.00	26.50	96.20	0.24	0.26	0.52	0.00
26.60	97.81	0.27	0.26	0.52	0.00	26.70	100.18	0.30	0.26	0.51	0.00
26.80	104.06	0.32	0.26	0.51	0.00	26.90	108.41	0.32	0.26	0.51	0.00
27.00	115.06	0.34	0.25	0.51	0.00	27.10	123.35	0.38	0.25	0.51	0.00
27.20	134.97	0.46	0.25	0.51	0.00	27.30	149.50	0.66	0.25	0.50	0.00
27.40	158.22	1.03	0.01	0.50	0.00	27.50	154.48	1.59	0.00	0.50	0.00
27.60	199.46	0.90	0.28	0.50	0.00	27.70	161.12	0.52	0.78	0.50	0.01
27.80	202.19	2.00	0.00	0.49	0.00	27.90	305.96	2.00	0.00	0.49	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
28.00	181.72	1.90	0.00	0.49	0.00	28.10	172.64	1.51	0.00	0.49	0.00
28.20	161.61	1.21	0.00	0.49	0.00	28.30	153.82	0.97	0.01	0.49	0.00
28.40	149.43	0.77	0.24	0.48	0.00	28.50	146.47	0.61	0.24	0.48	0.00
28.60	151.86	0.60	0.24	0.48	0.00	28.70	163.26	0.73	0.24	0.48	0.00
28.80	171.85	0.92	0.01	0.48	0.00	28.90	171.95	1.00	0.01	0.47	0.00
29.00	168.48	0.99	0.01	0.47	0.00	29.10	164.12	0.89	0.01	0.47	0.00
29.20	158.43	0.79	0.23	0.47	0.00	29.30	150.91	0.78	0.23	0.47	0.00
29.40	142.45	0.97	0.01	0.47	0.00	29.50	135.82	1.32	0.00	0.46	0.00
29.60	245.01	2.00	0.00	0.46	0.00	29.70	221.64	2.00	0.00	0.46	0.00
29.80	243.95	2.00	0.00	0.46	0.00	29.90	256.68	2.00	0.00	0.46	0.00
30.00	190.27	2.00	0.00	0.45	0.00	30.10	171.93	2.00	0.00	0.45	0.00
30.20	163.64	2.00	0.00	0.45	0.00	30.30	166.65	2.00	0.00	0.45	0.00
30.40	175.56	2.00	0.00	0.45	0.00	30.50	184.55	2.00	0.00	0.45	0.00
30.60	194.35	2.00	0.00	0.44	0.00	30.70	203.41	2.00	0.00	0.44	0.00
30.80	246.52	2.00	0.00	0.44	0.00	30.90	267.00	2.00	0.00	0.44	0.00
31.00	198.66	2.00	0.00	0.44	0.00	31.10	151.63	2.00	0.00	0.43	0.00
31.20	135.05	2.00	0.00	0.43	0.00	31.30	129.45	2.00	0.00	0.43	0.00
31.40	129.96	2.00	0.00	0.43	0.00	31.50	130.81	0.32	0.80	0.43	0.01
31.60	129.89	0.31	0.80	0.43	0.01	31.70	128.04	0.30	0.81	0.42	0.01
31.80	127.00	2.00	0.00	0.42	0.00	31.90	127.32	2.00	0.00	0.42	0.00
32.00	129.94	2.00	0.00	0.42	0.00	32.10	135.85	2.00	0.00	0.42	0.00
32.20	144.01	2.00	0.00	0.41	0.00	32.30	149.69	2.00	0.00	0.41	0.00
32.40	147.58	2.00	0.00	0.41	0.00	32.50	137.73	0.35	0.74	0.41	0.01
32.60	125.25	0.29	0.79	0.41	0.01	32.70	121.08	0.27	0.81	0.41	0.01
32.80	125.62	0.29	0.78	0.40	0.01	32.90	133.79	0.33	0.74	0.40	0.01
33.00	141.45	0.38	0.70	0.40	0.01	33.10	146.50	0.41	0.68	0.40	0.01
33.20	151.82	0.45	0.66	0.40	0.01	33.30	161.02	0.52	0.62	0.39	0.01
33.40	171.45	0.60	0.55	0.39	0.01	33.50	178.43	0.67	0.42	0.39	0.01
33.60	179.91	0.68	0.42	0.39	0.00	33.70	178.51	0.67	0.42	0.39	0.01
33.80	176.68	0.65	0.42	0.39	0.01	33.90	175.59	0.64	0.51	0.38	0.01
34.00	173.87	0.63	0.52	0.38	0.01	34.10	171.69	0.61	0.53	0.38	0.01
34.20	168.98	0.58	0.54	0.38	0.01	34.30	166.75	0.56	0.54	0.38	0.01
34.40	164.44	0.55	0.58	0.37	0.01	34.50	162.03	0.53	0.59	0.37	0.01
34.60	159.86	0.51	0.59	0.37	0.01	34.70	158.43	0.50	0.59	0.37	0.01
34.80	157.06	0.49	0.59	0.37	0.01	34.90	154.41	0.47	0.60	0.37	0.01
35.00	150.40	0.44	0.61	0.36	0.01	35.10	146.61	0.41	0.62	0.36	0.01
35.20	145.13	0.40	0.62	0.36	0.01	35.30	144.33	0.40	0.62	0.36	0.01
35.40	140.97	0.38	0.63	0.36	0.01	35.50	133.62	0.33	0.65	0.35	0.01
35.60	126.28	0.30	0.68	0.35	0.01	35.70	123.30	0.28	0.69	0.35	0.01
35.80	124.02	0.29	0.68	0.35	0.01	35.90	127.50	0.30	0.66	0.35	0.01
36.00	132.35	0.33	0.64	0.35	0.01	36.10	138.64	0.36	0.61	0.34	0.01
36.20	146.32	0.41	0.58	0.34	0.01	36.30	154.77	0.47	0.56	0.34	0.01
36.40	162.04	0.53	0.53	0.34	0.01	36.50	167.72	0.58	0.48	0.34	0.01
36.60	173.25	2.00	0.00	0.33	0.00	36.70	179.97	2.00	0.00	0.33	0.00
36.80	187.05	2.00	0.00	0.33	0.00	36.90	186.22	2.00	0.00	0.33	0.00
37.00	278.40	2.00	0.00	0.33	0.00	37.10	423.28	2.00	0.00	0.33	0.00
37.20	208.94	2.00	0.00	0.32	0.00	37.30	199.45	1.87	0.00	0.32	0.00
37.40	182.11	1.86	0.00	0.32	0.00	37.50	298.35	2.00	0.00	0.32	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
37.60	178.25	0.68	0.34	0.32	0.00	37.70	137.04	0.36	0.57	0.31	0.01
37.80	136.49	0.36	0.57	0.31	0.01	37.90	137.24	0.36	0.56	0.31	0.01
38.00	134.83	0.35	0.57	0.31	0.01	38.10	129.40	0.32	0.58	0.31	0.01
38.20	125.79	0.30	0.59	0.31	0.01	38.30	126.27	0.30	0.59	0.30	0.01
38.40	129.16	0.32	0.57	0.30	0.01	38.50	131.62	0.33	0.56	0.30	0.01
38.60	131.86	0.33	0.56	0.30	0.01	38.70	130.30	0.32	0.56	0.30	0.01
38.80	127.88	0.31	0.56	0.29	0.01	38.90	124.95	0.30	0.57	0.29	0.01
39.00	120.80	0.28	0.58	0.29	0.01	39.10	115.76	0.25	0.60	0.29	0.01
39.20	112.74	2.00	0.00	0.29	0.00	39.30	112.75	2.00	0.00	0.29	0.00
39.40	118.71	2.00	0.00	0.28	0.00	39.50	134.05	2.00	0.00	0.28	0.00
39.60	276.77	2.00	0.00	0.28	0.00	39.70	143.78	2.00	0.00	0.28	0.00
39.80	139.94	2.00	0.00	0.28	0.00	39.90	143.33	0.95	0.00	0.27	0.00
40.00	148.45	1.07	0.00	0.27	0.00	40.10	144.17	0.96	0.00	0.27	0.00
40.20	127.06	0.60	0.13	0.27	0.00	40.30	109.18	0.34	0.13	0.27	0.00
40.40	114.73	0.37	0.13	0.27	0.00	40.50	125.12	0.50	0.13	0.26	0.00
40.60	132.38	0.67	0.13	0.26	0.00	40.70	136.17	0.89	0.00	0.26	0.00
40.80	137.08	1.12	0.00	0.26	0.00	40.90	136.50	1.28	0.00	0.26	0.00
41.00	134.71	1.34	0.00	0.25	0.00	41.10	133.05	1.32	0.00	0.25	0.00
41.20	133.12	1.33	0.00	0.25	0.00	41.30	137.77	1.42	0.00	0.25	0.00
41.40	145.91	1.48	0.00	0.25	0.00	41.50	156.14	1.49	0.00	0.25	0.00
41.60	166.81	1.42	0.00	0.24	0.00	41.70	175.34	1.38	0.00	0.24	0.00
41.80	179.45	2.00	0.00	0.24	0.00	41.90	175.81	2.00	0.00	0.24	0.00
42.00	178.59	2.00	0.00	0.24	0.00	42.10	142.66	2.00	0.00	0.23	0.00
42.20	139.20	2.00	0.00	0.23	0.00	42.30	151.37	2.00	0.00	0.23	0.00
42.40	167.86	2.00	0.00	0.23	0.00	42.50	181.95	0.74	0.24	0.23	0.00
42.60	191.17	0.85	0.18	0.23	0.00	42.70	192.61	0.86	0.13	0.22	0.00
42.80	186.66	2.00	0.00	0.22	0.00	42.90	176.86	2.00	0.00	0.22	0.00
43.00	166.71	2.00	0.00	0.22	0.00	43.10	158.67	2.00	0.00	0.22	0.00
43.20	155.22	2.00	0.00	0.21	0.00	43.30	158.67	2.00	0.00	0.21	0.00
43.40	169.64	2.00	0.00	0.21	0.00	43.50	181.83	2.00	0.00	0.21	0.00
43.60	177.17	2.00	0.00	0.21	0.00	43.70	173.72	2.00	0.00	0.21	0.00
43.80	157.36	2.00	0.00	0.20	0.00	43.90	144.98	2.00	0.00	0.20	0.00
44.00	139.21	2.00	0.00	0.20	0.00	44.10	137.01	2.00	0.00	0.20	0.00
44.20	138.27	2.00	0.00	0.20	0.00	44.30	144.81	2.00	0.00	0.19	0.00
44.40	158.02	2.00	0.00	0.19	0.00	44.50	172.75	2.00	0.00	0.19	0.00
44.60	177.83	2.00	0.00	0.19	0.00	44.70	168.46	2.00	0.00	0.19	0.00
44.80	151.81	2.00	0.00	0.19	0.00	44.90	142.30	2.00	0.00	0.18	0.00
45.00	145.46	2.00	0.00	0.18	0.00	45.10	154.46	2.00	0.00	0.18	0.00
45.20	162.21	0.57	0.27	0.18	0.00	45.30	166.12	2.00	0.00	0.18	0.00
45.40	166.61	2.00	0.00	0.17	0.00	45.50	165.78	2.00	0.00	0.17	0.00
45.60	167.45	2.00	0.00	0.17	0.00	45.70	173.53	2.00	0.00	0.17	0.00
45.80	180.86	2.00	0.00	0.17	0.00	45.90	180.65	2.00	0.00	0.17	0.00
46.00	191.30	0.88	0.10	0.16	0.00	46.10	161.23	2.00	0.00	0.16	0.00
46.20	138.71	2.00	0.00	0.16	0.00	46.30	125.66	2.00	0.00	0.16	0.00
46.40	117.53	2.00	0.00	0.16	0.00	46.50	117.13	2.00	0.00	0.15	0.00
46.60	125.92	2.00	0.00	0.15	0.00	46.70	137.61	0.39	0.27	0.15	0.00
46.80	146.60	0.45	0.25	0.15	0.00	46.90	153.73	0.51	0.24	0.15	0.00
47.00	162.30	0.58	0.22	0.15	0.00	47.10	170.72	0.66	0.17	0.14	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
47.20	174.43	0.70	0.16	0.14	0.00	47.30	171.87	0.67	0.16	0.14	0.00
47.40	166.68	0.62	0.20	0.14	0.00	47.50	164.46	0.60	0.20	0.14	0.00
47.60	167.72	0.63	0.19	0.13	0.00	47.70	174.14	0.70	0.15	0.13	0.00
47.80	180.72	0.77	0.11	0.13	0.00	47.90	184.92	0.82	0.11	0.13	0.00
48.00	187.00	0.85	0.10	0.13	0.00	48.10	188.02	0.86	0.08	0.13	0.00
48.20	189.38	0.88	0.08	0.12	0.00	48.30	190.75	0.89	0.07	0.12	0.00
48.40	191.69	0.91	0.07	0.12	0.00	48.50	191.83	0.91	0.07	0.12	0.00
48.60	191.18	0.90	0.07	0.12	0.00	48.70	190.43	0.90	0.07	0.11	0.00
48.80	189.96	0.89	0.07	0.11	0.00	48.90	190.37	0.90	0.07	0.11	0.00
49.00	191.52	0.91	0.07	0.11	0.00	49.10	193.42	0.94	0.06	0.11	0.00
49.20	195.97	0.97	0.05	0.11	0.00	49.30	199.07	1.02	0.05	0.10	0.00
49.40	202.00	2.00	0.00	0.10	0.00	49.50	202.10	2.00	0.00	0.10	0.00
49.60	197.41	1.00	0.05	0.10	0.00	49.70	191.32	0.92	0.06	0.10	0.00
49.80	188.42	0.88	0.06	0.09	0.00	49.90	188.96	0.89	0.06	0.09	0.00

Total estimated settlement: 1.06**Abbreviations**

$Q_{tn,cs}$:	Equivalent clean sand normalized cone resistance
FS:	Factor of safety against liquefaction
e_v (%):	Post-liquefaction volumetric strain
DF:	e_v depth weighting factor
Settlement:	Calculated settlement

:: Strength loss calculation (Robertson (2009)) ::

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.10	20.69	39.10	1.42	55.57	2.10	0.08	0.64
0.20	15.95	30.12	1.66	49.90	2.22	0.05	0.63
0.30	12.29	23.21	2.10	48.70	2.34	0.05	0.62
0.40	12.85	24.26	2.06	50.09	2.33	0.05	0.63
0.50	17.93	33.84	1.67	56.52	2.22	0.09	0.65
0.60	25.60	48.33	1.47	71.07	2.13	0.28	0.69
0.70	35.62	67.26	1.36	91.66	2.06	0.73	0.73
0.80	45.80	86.49	1.31	113.12	2.00	0.77	0.77
0.90	55.07	103.99	1.28	132.90	1.96	0.80	0.80
1.00	61.98	117.06	1.26	147.81	1.94	0.82	0.82
1.10	65.41	123.52	1.26	155.65	1.94	0.83	0.83
1.20	66.73	126.01	1.26	159.05	1.94	0.84	0.84
1.30	68.80	129.90	1.26	163.96	1.94	0.85	0.85
1.40	72.09	136.11	1.26	171.44	1.93	0.85	0.85
1.50	75.47	142.50	1.26	179.17	1.93	0.86	0.86
1.60	77.78	146.84	1.26	184.84	1.93	0.87	0.87
1.70	79.45	149.99	1.26	189.22	1.94	0.88	0.88
1.80	79.92	150.87	1.27	191.13	1.95	0.88	0.88
1.90	78.74	148.63	1.28	189.63	1.96	0.88	0.88
2.00	77.53	146.34	1.28	187.97	1.97	0.87	0.87
2.10	76.45	144.27	1.29	186.30	1.98	0.87	0.87
2.20	74.95	141.43	1.30	183.85	1.99	0.87	0.87
2.30	72.03	135.91	1.32	178.97	2.01	0.86	0.86
2.40	66.61	125.64	1.35	169.63	2.05	0.85	0.85
2.50	59.83	112.81	1.40	157.60	2.08	0.84	0.84
2.60	53.38	100.62	1.44	145.16	2.12	0.82	0.82
2.70	48.56	91.49	1.47	134.49	2.13	0.81	0.81
2.80	45.31	85.34	1.48	125.91	2.13	0.79	0.79
2.90	44.32	83.45	1.45	120.83	2.12	0.78	0.78
3.00	45.95	86.52	1.40	121.48	2.09	0.79	0.79
3.10	48.29	90.93	1.39	126.32	2.08	0.79	0.79
3.20	48.11	90.59	1.43	129.35	2.11	0.80	0.80
3.30	44.42	83.59	1.54	128.66	2.17	0.80	0.80
3.40	38.42	72.24	1.75	126.16	2.25	0.79	0.79
3.50	31.66	59.45	2.08	123.67	2.34	0.79	0.79
3.60	25.01	46.88	2.61	122.26	2.44	0.79	0.79
3.70	18.93	35.38	3.44	121.77	2.56	0.83	0.83
3.80	13.89	25.84	4.69	121.11	2.70	0.94	0.94
3.90	9.83	18.15	6.50	118.04	2.85	0.78	0.78
4.00	6.71	12.24	9.02	110.41	3.01	1.17	2.00
4.10	4.73	8.50	11.89	101.07	3.16	0.80	1.35
4.20	3.30	5.78	15.54	89.83	3.31	0.66	0.90
4.30	2.28	3.84	20.36	78.22	3.47	0.40	0.59
4.40	1.63	2.61	26.07	67.99	3.62	0.21	0.39
4.50	1.68	2.70	25.15	67.85	3.60	0.26	0.40
4.60	1.90	3.10	23.18	71.75	3.55	0.37	0.45
4.70	1.99	3.27	22.94	75.00	3.54	0.33	0.47
4.80	2.28	3.79	21.46	81.39	3.50	0.36	0.53

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
4.90	3.08	5.30	16.96	89.83	3.36	0.59	0.73
5.00	5.02	8.96	11.09	99.38	3.12	0.67	1.21
5.10	8.35	15.24	6.81	103.82	2.87	0.76	0.76
5.20	12.99	24.00	4.60	110.26	2.69	0.92	0.92
5.30	17.05	31.66	3.85	122.01	2.61	0.87	0.87
5.40	18.42	34.25	3.86	132.22	2.61	0.89	0.89
5.50	17.82	33.10	4.04	133.70	2.63	0.91	0.91
5.60	18.27	33.93	3.58	121.46	2.58	0.84	0.84
5.70	22.60	42.11	2.45	103.16	2.41	0.75	0.75
5.80	30.34	56.74	1.69	96.02	2.23	0.74	0.74
5.90	38.67	72.46	1.43	103.65	2.11	0.75	0.75
6.00	44.41	83.32	1.38	114.74	2.07	0.77	0.77
6.10	46.53	87.31	1.40	122.36	2.09	0.79	0.79
6.20	45.75	85.81	1.46	125.37	2.13	0.79	0.79
6.30	44.18	82.83	1.51	125.44	2.16	0.79	0.79
6.40	43.27	81.10	1.53	123.81	2.16	0.79	0.79
6.50	43.29	81.14	1.50	121.74	2.15	0.79	0.79
6.60	44.11	82.67	1.46	120.61	2.13	0.78	0.78
6.70	45.23	84.41	1.42	120.00	2.10	0.78	0.78
6.80	46.59	85.54	1.40	119.50	2.08	0.78	0.78
6.90	47.78	86.62	1.39	120.05	2.08	0.78	0.78
7.00	47.94	86.40	1.40	120.86	2.09	0.78	0.78
7.10	46.35	83.70	1.45	121.17	2.12	0.78	0.78
7.20	43.14	78.48	1.54	120.81	2.17	0.78	0.78
7.30	39.20	71.76	1.65	118.75	2.22	0.78	0.78
7.40	35.95	65.71	1.73	113.59	2.24	0.77	0.77
7.50	34.90	62.81	1.68	105.75	2.23	0.76	0.76
7.60	36.71	64.29	1.55	99.54	2.17	0.75	0.75
7.70	40.76	69.26	1.43	99.23	2.11	0.75	0.75
7.80	45.18	75.11	1.37	103.22	2.07	0.75	0.75
7.90	48.49	79.59	1.36	107.93	2.05	0.76	0.76
8.00	50.35	82.10	1.36	111.75	2.06	0.77	0.77
8.10	50.92	83.37	1.39	116.05	2.08	0.78	0.78
8.20	50.43	83.91	1.49	125.21	2.14	0.79	0.79
8.30	48.21	82.00	1.69	138.70	2.23	0.81	0.81
8.40	44.03	76.81	2.02	155.46	2.33	0.83	0.83
8.50	38.01	67.96	2.52	170.95	2.43	0.85	0.85
8.60	31.11	57.06	3.23	184.47	2.54	0.89	0.89
8.70	24.26	44.92	4.34	195.02	2.66	1.03	1.03
8.80	18.28	33.61	5.89	197.84	2.80	0.88	0.88
8.90	13.46	24.48	7.87	192.66	2.94	0.88	0.88
9.00	9.80	17.55	10.15	178.13	3.08	1.54	1.38
9.10	7.41	13.03	12.35	160.97	3.18	1.10	1.02
9.20	6.33	10.98	13.41	147.24	3.23	0.93	0.85
9.30	6.36	11.02	12.76	140.62	3.20	0.86	0.85
9.40	7.05	12.32	11.21	138.06	3.13	0.84	0.95
9.50	7.58	13.30	10.28	136.69	3.08	0.89	1.02
9.60	7.34	12.84	10.53	135.30	3.10	0.85	0.98

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.70	6.26	10.80	12.08	130.39	3.17	0.76	0.82
9.80	7.93	13.93	10.48	146.02	3.09	0.61	1.05
9.90	13.13	23.76	7.60	180.56	2.93	0.87	0.87
10.00	18.80	34.47	6.06	208.85	2.82	0.90	0.90
10.10	18.67	34.21	6.12	209.42	2.82	0.90	0.90
10.20	14.65	26.59	7.16	190.32	2.90	0.88	0.88
10.30	10.95	19.59	8.50	166.51	2.98	0.85	0.85
10.40	10.48	18.69	8.69	162.44	2.99	0.84	0.84
10.50	11.16	19.96	8.38	167.34	2.98	0.85	0.85
10.60	13.38	24.16	7.66	184.96	2.93	0.87	0.87
10.70	16.24	29.17	6.81	198.61	2.87	0.89	0.89
10.80	23.16	40.35	5.06	204.26	2.73	0.89	0.89
10.90	36.54	60.20	3.01	181.19	2.50	0.86	0.86
11.00	57.04	88.44	1.81	159.82	2.27	0.84	0.84
11.10	77.62	114.57	1.39	159.68	2.08	0.84	0.84
11.20	91.25	130.34	1.28	166.80	1.96	0.85	0.85
11.30	96.49	135.47	1.24	168.36	1.91	0.85	0.85
11.40	96.73	134.66	1.23	165.51	1.89	0.85	0.85
11.50	93.84	130.49	1.24	161.18	1.90	0.84	0.84
11.60	89.17	124.60	1.26	156.72	1.93	0.84	0.84
11.70	82.47	116.28	1.29	150.52	1.98	0.83	0.83
11.80	74.34	105.91	1.35	142.88	2.04	0.82	0.82
11.90	66.88	96.17	1.42	136.60	2.10	0.81	0.81
12.00	59.90	86.72	1.50	130.39	2.15	0.80	0.80
12.10	54.60	79.32	1.58	124.95	2.18	0.79	0.79
12.20	52.76	76.47	1.59	121.82	2.19	0.79	0.79
12.30	53.42	76.99	1.57	120.93	2.18	0.78	0.78
12.40	55.36	79.28	1.54	122.10	2.17	0.79	0.79
12.50	55.60	79.32	1.54	121.95	2.17	0.79	0.79
12.60	55.04	78.40	1.56	122.09	2.18	0.79	0.79
12.70	54.18	77.33	1.62	125.14	2.20	0.79	0.79
12.80	51.05	73.48	1.78	130.74	2.26	0.80	0.80
12.90	44.55	65.03	2.12	138.07	2.35	0.81	0.81
13.00	37.39	55.52	2.70	150.09	2.46	0.83	0.83
13.10	30.77	46.43	3.50	162.58	2.57	0.89	0.89
13.20	26.49	40.37	4.23	170.94	2.65	0.98	0.98
13.30	22.74	34.84	4.92	171.29	2.72	0.85	0.85
13.40	20.92	32.02	5.25	168.19	2.75	0.85	0.85
13.50	20.31	30.96	5.35	165.57	2.76	0.85	0.85
13.60	20.02	30.39	5.39	163.90	2.76	0.85	0.85
13.70	19.28	29.13	5.47	159.27	2.77	0.84	0.84
13.80	18.73	28.14	5.48	154.30	2.77	0.83	0.83
13.90	18.04	27.03	5.63	152.22	2.78	0.83	0.83
14.00	16.71	25.01	6.10	152.62	2.82	0.83	0.83
14.10	15.17	22.72	6.79	154.31	2.87	0.83	0.83
14.20	14.03	21.02	7.44	156.38	2.92	0.84	0.84
14.30	11.65	17.23	8.72	150.24	3.00	0.83	0.83
14.40	7.83	11.11	11.85	131.58	3.16	0.68	0.79

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
14.50	4.04	5.07	20.03	101.58	3.46	0.22	0.36
14.60	2.41	2.48	32.40	80.21	3.75	0.21	0.18
14.70	2.41	2.46	31.74	78.12	3.74	0.20	0.18
14.80	2.41	2.45	31.05	75.98	3.72	0.18	0.17
14.90	2.19	2.09	34.01	71.06	3.78	0.17	0.15
15.00	1.79	1.45	43.72	63.39	3.93	0.11	0.10
15.10	1.39	0.81	54.25	44.18	4.06	0.07	0.06
15.20	1.20	0.52	54.25	28.39	4.06	0.07	0.04
15.30	1.20	0.52	54.25	27.97	4.06	0.09	0.04
15.40	1.39	0.80	54.25	43.31	4.06	0.11	0.06
15.50	2.04	1.79	43.11	77.37	3.92	0.17	0.13
15.60	3.92	4.67	20.83	97.25	3.49	0.29	0.33
15.70	7.11	9.53	12.14	115.74	3.17	0.54	0.68
15.80	10.59	14.80	8.75	129.53	3.00	0.80	0.80
15.90	12.22	17.23	7.96	137.10	2.95	0.81	0.81
16.00	11.38	15.88	8.64	137.25	2.99	0.81	0.81
16.10	9.26	12.61	10.24	129.07	3.08	0.70	0.90
16.20	7.35	9.69	11.85	114.76	3.16	0.50	0.69
16.30	6.42	8.25	12.61	104.02	3.19	0.38	0.59
16.40	6.02	7.62	13.01	99.12	3.21	0.36	0.54
16.50	5.80	7.25	13.41	97.25	3.23	0.36	0.52
16.60	5.19	6.31	14.74	92.99	3.28	0.32	0.45
16.70	4.26	4.91	17.43	85.54	3.38	0.24	0.35
16.80	3.29	3.46	22.06	76.36	3.52	0.18	0.25
16.90	2.90	2.87	24.80	71.23	3.59	0.13	0.21
17.00	2.86	2.79	24.87	69.38	3.59	0.15	0.20
17.10	3.23	3.32	21.80	72.39	3.51	0.15	0.24
17.20	3.29	3.39	21.78	73.85	3.51	0.18	0.24
17.30	3.07	3.06	23.92	73.25	3.57	0.18	0.22
17.40	2.98	2.91	25.07	72.92	3.60	0.14	0.21
17.50	3.69	3.92	19.79	77.63	3.45	0.18	0.28
17.60	5.22	6.13	14.10	86.38	3.26	0.26	0.44
17.70	6.73	8.29	11.30	93.63	3.13	0.34	0.59
17.80	7.04	8.70	11.02	95.85	3.12	0.39	0.62
17.90	6.09	7.30	12.72	92.87	3.20	0.33	0.52
18.00	4.82	5.45	15.99	87.15	3.33	0.23	0.39
18.10	4.08	4.37	19.01	83.11	3.43	0.22	0.31
18.20	4.56	5.03	17.59	88.54	3.39	0.23	0.36
18.30	7.27	8.86	12.52	111.00	3.19	0.35	0.63
18.40	12.35	16.00	9.01	144.21	3.01	0.86	1.14
18.50	17.77	23.51	7.44	174.91	2.92	0.86	0.86
18.60	19.06	25.20	7.38	185.92	2.91	0.87	0.87
18.70	18.07	23.78	7.62	181.17	2.93	0.87	0.87
18.80	16.83	21.92	7.43	162.95	2.92	0.84	0.84
18.90	18.43	23.75	6.30	149.63	2.83	0.83	0.83
19.00	21.05	26.87	5.15	138.46	2.74	0.81	0.81
19.10	24.45	30.90	4.16	128.68	2.65	0.91	0.91
19.20	28.33	35.51	3.47	123.26	2.57	0.83	0.83

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
19.30	31.79	39.71	3.24	128.71	2.54	0.82	0.82
19.40	33.34	41.77	3.51	146.58	2.57	0.87	0.87
19.50	32.10	40.45	4.19	169.34	2.65	0.98	0.98
19.60	28.67	36.30	5.15	187.09	2.74	0.87	0.87
19.70	24.81	31.39	6.04	189.60	2.81	0.88	0.88
19.80	25.42	31.99	5.77	184.75	2.79	0.87	0.87
19.90	32.01	39.85	4.40	175.37	2.67	1.01	1.01
20.00	40.24	49.34	3.14	154.94	2.52	0.84	0.84
20.10	47.35	57.16	2.34	133.96	2.39	0.80	0.80
20.20	50.45	60.22	2.00	120.70	2.32	0.78	0.78
20.30	51.38	61.26	2.05	125.66	2.33	0.79	0.79
20.40	47.65	56.93	2.31	131.65	2.39	0.80	0.80
20.50	41.70	49.84	2.63	131.07	2.45	0.80	0.80
20.60	36.95	44.08	2.89	127.22	2.49	0.79	0.79
20.70	35.66	42.51	3.11	132.03	2.52	0.81	0.81
20.80	35.84	42.85	3.49	149.51	2.57	0.87	0.87
20.90	33.79	40.57	4.22	171.40	2.65	0.98	0.98
21.00	28.53	34.35	5.42	186.05	2.76	0.87	0.87
21.10	22.40	26.91	6.95	187.10	2.88	0.87	0.87
21.20	18.70	22.22	8.04	178.64	2.95	0.86	0.86
21.30	17.11	20.13	8.45	170.13	2.98	0.85	0.85
21.40	16.52	19.31	8.58	165.68	2.99	0.85	0.85
21.50	15.83	18.36	8.79	161.39	3.00	1.20	1.31
21.60	15.40	17.76	8.89	157.77	3.01	1.12	1.27
21.70	15.00	17.19	9.02	155.16	3.01	1.09	1.23
21.80	14.79	16.86	9.26	156.12	3.03	1.07	1.20
21.90	15.25	17.37	9.40	163.21	3.04	1.13	1.24
22.00	15.77	17.95	9.52	170.98	3.04	1.39	1.28
22.10	16.13	18.32	9.53	174.52	3.04	1.42	1.31
22.20	16.33	18.50	9.25	171.13	3.03	1.30	1.32
22.30	17.20	19.49	8.49	165.61	2.98	0.85	0.85
22.40	18.93	21.53	7.56	162.66	2.92	0.84	0.84
22.50	20.75	23.56	6.82	160.68	2.87	0.84	0.84
22.60	22.36	25.32	6.28	158.98	2.83	0.84	0.84
22.70	23.55	26.59	5.92	157.52	2.81	0.84	0.84
22.80	24.27	27.32	5.76	157.34	2.79	0.84	0.84
22.90	24.79	27.82	5.64	156.78	2.78	0.84	0.84
23.00	25.40	28.39	5.40	153.41	2.76	0.83	0.83
23.10	26.63	29.65	5.04	149.33	2.73	0.83	0.83
23.20	27.97	31.08	4.85	150.73	2.71	0.83	0.83
23.30	28.02	31.08	5.08	157.89	2.73	0.84	0.84
23.40	25.97	28.74	5.75	165.31	2.79	0.85	0.85
23.50	22.41	24.66	6.73	166.04	2.87	0.85	0.85
23.60	19.33	21.06	7.60	160.07	2.93	0.84	0.84
23.70	17.40	18.73	8.04	150.55	2.95	0.83	0.83
23.80	16.53	17.65	8.09	142.73	2.96	0.82	0.82
23.90	16.15	17.15	8.10	139.01	2.96	0.81	0.81
24.00	15.80	16.69	8.31	138.60	2.97	0.81	0.81

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
24.10	14.52	15.16	8.98	136.16	3.01	0.89	1.08
24.20	11.33	11.44	10.94	125.22	3.12	0.69	0.82
24.30	8.08	7.67	14.25	109.35	3.26	0.37	0.55
24.40	5.93	5.19	18.21	94.56	3.41	0.30	0.37
24.50	5.62	4.83	18.60	89.77	3.42	0.27	0.34
24.60	5.62	4.81	18.27	87.89	3.41	0.26	0.34
24.70	5.77	4.97	17.88	88.79	3.40	0.26	0.35
24.80	6.24	5.48	17.08	93.57	3.37	0.30	0.39
24.90	6.78	6.06	16.47	99.86	3.35	0.37	0.43
25.00	7.16	6.47	16.36	105.93	3.34	0.42	0.46
25.10	7.19	6.48	16.95	109.82	3.36	0.46	0.46
25.20	6.84	6.06	18.13	109.92	3.40	0.47	0.43
25.30	6.30	5.44	19.62	106.76	3.45	0.41	0.39
25.40	5.81	4.87	20.97	102.13	3.49	0.36	0.35
25.50	5.62	4.65	21.32	99.16	3.50	0.35	0.33
25.60	5.62	4.63	21.18	98.13	3.50	0.34	0.33
25.70	5.62	4.62	21.18	97.77	3.50	0.34	0.33
25.80	5.62	4.60	21.06	96.87	3.49	0.34	0.33
25.90	5.74	4.71	20.23	95.31	3.47	0.32	0.34
26.00	6.01	4.99	18.94	94.48	3.43	0.30	0.36
26.10	6.06	5.03	18.69	94.04	3.42	0.32	0.36
26.20	5.94	4.88	19.26	94.06	3.44	0.31	0.35
26.30	5.68	4.58	20.53	93.92	3.48	0.30	0.33
26.40	5.62	4.50	21.10	94.95	3.49	0.32	0.32
26.50	5.72	4.59	20.94	96.20	3.49	0.33	0.33
26.60	6.14	5.03	19.45	97.81	3.44	0.33	0.36
26.70	6.68	5.59	17.92	100.18	3.40	0.36	0.40
26.80	7.11	6.04	17.23	104.06	3.37	0.39	0.43
26.90	7.23	6.15	17.62	108.41	3.39	0.44	0.44
27.00	7.58	6.50	17.71	115.06	3.39	0.47	0.46
27.10	8.22	7.16	17.22	123.35	3.37	0.58	0.51
27.20	9.74	8.76	15.41	134.97	3.31	0.69	0.63
27.30	13.33	12.55	11.91	149.50	3.16	0.88	0.90
27.40	19.91	19.49	8.12	158.22	2.96	0.84	0.84
27.50	30.24	30.15	5.12	154.48	2.74	0.83	0.83
27.60	41.52	41.60	3.59	149.55	2.58	0.89	0.89
27.70	49.24	49.37	3.14	155.01	2.52	0.84	0.84
27.80	49.82	49.90	3.39	169.00	2.56	0.89	0.89
27.90	44.25	44.15	4.10	181.00	2.64	0.98	0.98
28.00	36.48	36.12	5.03	181.72	2.73	0.87	0.87
28.10	29.33	28.72	6.01	172.64	2.81	0.86	0.86
28.20	23.96	23.14	6.98	161.61	2.88	0.84	0.84
28.30	19.51	18.48	8.32	153.82	2.97	0.83	0.83
28.40	15.84	14.65	10.20	149.43	3.08	0.95	1.05
28.50	12.93	11.62	12.61	146.47	3.19	0.85	0.83
28.60	12.75	11.39	13.33	151.86	3.23	0.86	0.81
28.70	15.29	13.95	11.70	163.26	3.15	1.13	1.00
28.80	18.82	17.49	9.82	171.85	3.06	1.40	1.25

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
28.90	20.53	19.18	8.97	171.95	3.01	1.41	1.37
29.00	20.27	18.85	8.94	168.48	3.01	1.25	1.35
29.10	18.46	16.96	9.68	164.12	3.05	1.24	1.21
29.20	16.60	15.04	10.53	158.43	3.10	1.12	1.07
29.30	16.51	14.91	10.12	150.91	3.07	0.92	1.06
29.40	20.13	18.48	7.71	142.45	2.93	0.82	0.82
29.50	27.09	25.29	5.37	135.82	2.76	0.81	0.81
29.60	33.16	31.18	4.29	133.73	2.66	0.93	0.93
29.70	36.69	34.57	3.99	137.83	2.63	0.91	0.91
29.80	40.80	38.51	3.97	152.89	2.62	0.93	0.93
29.90	48.32	45.76	3.80	173.96	2.61	0.94	0.94
30.00	59.72	56.73	3.17	179.81	2.53	0.88	0.88
30.10	73.28	69.68	2.47	171.93	2.42	0.85	0.85
30.20	85.57	81.32	2.01	163.64	2.32	0.84	0.84
30.30	94.24	89.46	1.86	166.65	2.28	0.85	0.85
30.40	96.38	91.31	1.92	175.56	2.30	0.86	0.86
30.50	93.45	88.28	2.09	184.55	2.34	0.87	0.87
30.60	85.88	80.82	2.40	194.35	2.41	0.88	0.88
30.70	75.59	70.78	2.87	203.41	2.48	0.89	0.89
30.80	64.96	60.44	3.39	205.19	2.56	0.93	0.93
30.90	58.02	53.66	3.64	195.46	2.59	0.95	0.95
31.00	57.76	53.25	3.29	175.20	2.54	0.89	0.89
31.10	64.29	59.30	2.56	151.63	2.43	0.83	0.83
31.20	74.72	69.01	1.96	135.05	2.31	0.81	0.81
31.30	84.37	77.95	1.66	129.45	2.22	0.80	0.80
31.40	91.02	84.05	1.55	129.96	2.17	0.80	0.80
31.50	94.21	86.86	1.51	130.81	2.15	0.80	0.80
31.60	94.73	87.16	1.49	129.89	2.14	0.80	0.80
31.70	92.99	85.34	1.50	128.04	2.15	0.80	0.80
31.80	89.90	82.26	1.54	127.00	2.17	0.79	0.79
31.90	86.48	78.87	1.61	127.32	2.20	0.79	0.79
32.00	83.14	75.57	1.72	129.94	2.24	0.80	0.80
32.10	79.62	72.09	1.88	135.85	2.29	0.81	0.81
32.20	75.05	67.65	2.13	144.01	2.35	0.82	0.82
32.30	69.21	62.06	2.41	149.69	2.41	0.83	0.83
32.40	63.30	56.45	2.61	147.58	2.44	0.82	0.82
32.50	60.94	54.16	2.54	137.73	2.43	0.81	0.81
32.60	65.02	57.83	2.17	125.25	2.36	0.79	0.79
32.70	74.05	66.03	1.83	121.08	2.27	0.78	0.78
32.80	83.30	74.38	1.69	125.62	2.23	0.79	0.79
32.90	89.30	79.69	1.68	133.79	2.22	0.80	0.80
33.00	94.12	83.89	1.69	141.45	2.23	0.82	0.82
33.10	101.14	90.11	1.63	146.50	2.20	0.82	0.82
33.20	112.44	100.24	1.51	151.82	2.16	0.83	0.83
33.30	126.20	112.59	1.43	161.02	2.11	0.84	0.84
33.40	137.62	122.75	1.40	171.45	2.08	0.85	0.85
33.50	143.17	127.48	1.40	178.43	2.09	0.86	0.86
33.60	142.56	126.60	1.42	179.91	2.10	0.86	0.86

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
33.70	140.15	124.12	1.44	178.51	2.11	0.86	0.86
33.80	138.78	122.61	1.44	176.68	2.11	0.86	0.86
33.90	138.19	121.82	1.44	175.59	2.11	0.86	0.86
34.00	135.99	119.56	1.45	173.87	2.12	0.86	0.86
34.10	131.92	115.61	1.49	171.69	2.14	0.85	0.85
34.20	126.82	110.75	1.53	168.98	2.16	0.85	0.85
34.30	122.27	106.42	1.57	166.75	2.18	0.85	0.85
34.40	118.79	103.06	1.60	164.44	2.19	0.85	0.85
34.50	116.72	101.00	1.60	162.03	2.20	0.84	0.84
34.60	116.13	100.27	1.59	159.86	2.19	0.84	0.84
34.70	116.42	100.33	1.58	158.43	2.19	0.84	0.84
34.80	116.08	99.83	1.57	157.06	2.18	0.84	0.84
34.90	113.21	97.07	1.59	154.41	2.19	0.83	0.83
35.00	107.12	91.47	1.64	150.40	2.21	0.83	0.83
35.10	98.36	83.53	1.76	146.61	2.25	0.82	0.82
35.20	88.33	74.49	1.95	145.13	2.31	0.82	0.82
35.30	78.11	65.34	2.21	144.33	2.37	0.82	0.82
35.40	70.66	58.71	2.40	140.97	2.41	0.81	0.81
35.50	68.31	56.59	2.36	133.62	2.40	0.80	0.80
35.60	71.04	58.91	2.14	126.28	2.35	0.79	0.79
35.70	76.04	63.18	1.95	123.30	2.31	0.79	0.79
35.80	80.43	66.88	1.85	124.02	2.28	0.79	0.79
35.90	83.79	69.62	1.83	127.50	2.27	0.79	0.79
36.00	86.97	72.18	1.83	132.35	2.27	0.80	0.80
36.10	90.89	75.33	1.84	138.64	2.28	0.81	0.81
36.20	95.24	78.84	1.86	146.32	2.28	0.82	0.82
36.30	98.94	81.74	1.89	154.77	2.29	0.83	0.83
36.40	100.43	82.73	1.96	162.04	2.31	0.84	0.84
36.50	99.89	81.99	2.05	167.72	2.33	0.85	0.85
36.60	98.07	80.15	2.16	173.25	2.36	0.86	0.86
36.70	95.06	77.30	2.33	179.97	2.39	0.86	0.86
36.80	89.45	72.26	2.59	187.05	2.44	0.87	0.87
36.90	80.70	64.60	3.01	194.29	2.50	0.87	0.87
37.00	69.82	55.23	3.66	202.10	2.59	0.96	0.96
37.10	58.94	45.95	4.54	208.64	2.68	1.06	1.06
37.20	50.59	38.90	5.37	208.94	2.76	0.90	0.90
37.30	46.04	35.09	5.68	199.45	2.79	0.89	0.89
37.40	45.72	34.83	5.23	182.11	2.75	0.87	0.87
37.50	48.88	37.49	4.31	161.52	2.66	0.98	0.98
37.60	54.47	42.16	3.44	144.96	2.56	0.86	0.86
37.70	60.92	47.50	2.89	137.04	2.49	0.81	0.81
37.80	66.48	52.02	2.62	136.49	2.44	0.81	0.81
37.90	71.26	55.89	2.46	137.24	2.42	0.81	0.81
38.00	76.37	60.07	2.24	134.83	2.37	0.81	0.81
38.10	82.38	65.07	1.99	129.40	2.32	0.80	0.80
38.20	88.96	70.57	1.78	125.79	2.26	0.79	0.79
38.30	94.06	74.74	1.69	126.27	2.23	0.79	0.79
38.40	96.38	76.48	1.69	129.16	2.23	0.80	0.80

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
38.50	95.22	75.26	1.75	131.62	2.25	0.80	0.80
38.60	91.50	71.97	1.83	131.86	2.27	0.80	0.80
38.70	86.76	67.88	1.92	130.30	2.30	0.80	0.80
38.80	82.49	64.22	1.99	127.88	2.32	0.80	0.80
38.90	79.99	62.06	2.01	124.95	2.32	0.79	0.79
39.00	79.66	61.74	1.96	120.80	2.31	0.78	0.78
39.10	80.98	62.84	1.84	115.76	2.28	0.78	0.78
39.20	81.39	63.13	1.79	112.74	2.26	0.77	0.77
39.30	77.05	59.38	1.90	112.75	2.29	0.77	0.77
39.40	68.00	51.69	2.30	118.71	2.38	0.78	0.78
39.50	55.58	41.34	3.13	129.50	2.52	0.80	0.80
39.60	43.51	31.48	4.46	140.57	2.68	0.96	0.96
39.70	32.08	22.36	6.43	143.78	2.84	0.82	0.82
39.80	24.49	16.60	8.43	139.94	2.98	0.81	0.81
39.90	25.69	17.46	8.21	143.33	2.97	0.82	0.82
40.00	28.88	19.80	7.50	148.45	2.92	0.82	0.82
40.10	26.02	17.62	8.18	144.17	2.96	0.82	0.82
40.20	17.22	11.05	11.50	127.06	3.14	0.45	0.79
40.30	10.69	6.18	17.67	109.18	3.39	0.37	0.44
40.40	11.62	6.85	16.74	114.73	3.36	0.51	0.49
40.50	14.83	9.21	13.59	125.12	3.24	0.62	0.66
40.60	19.14	12.36	10.71	132.38	3.10	0.74	0.88
40.70	24.64	16.37	8.32	136.17	2.97	0.81	0.81
40.80	30.34	20.52	6.68	137.08	2.86	0.81	0.81
40.90	34.36	23.54	5.80	136.50	2.80	0.81	0.81
41.00	35.62	24.47	5.51	134.71	2.77	0.81	0.81
41.10	35.36	24.22	5.49	133.05	2.77	0.80	0.80
41.20	35.52	24.29	5.48	133.12	2.77	0.80	0.80
41.30	37.77	25.92	5.32	137.77	2.76	0.81	0.81
41.40	39.51	27.12	5.38	145.91	2.76	0.82	0.82
41.50	39.75	27.14	5.75	156.14	2.79	0.84	0.84
41.60	38.24	25.83	6.46	166.81	2.85	0.85	0.85
41.70	37.40	25.16	6.97	175.34	2.88	0.86	0.86
41.80	40.17	27.09	6.62	179.45	2.86	0.86	0.86
41.90	50.73	35.02	5.02	175.81	2.73	0.86	0.86
42.00	69.20	49.29	3.26	160.50	2.54	0.86	0.86
42.10	94.71	69.50	2.05	142.66	2.33	0.82	0.82
42.20	121.87	91.48	1.52	139.20	2.16	0.81	0.81
42.30	147.28	112.12	1.35	151.37	2.05	0.83	0.83
42.40	168.54	129.14	1.30	167.86	1.99	0.85	0.85
42.50	184.42	141.54	1.29	181.95	1.97	0.87	0.87
42.60	194.06	148.80	1.28	191.17	1.97	0.88	0.88
42.70	194.52	148.65	1.30	192.61	1.99	0.88	0.88
42.80	186.27	141.56	1.32	186.66	2.01	0.87	0.87
42.90	172.77	130.36	1.36	176.86	2.05	0.86	0.86
43.00	157.23	117.60	1.42	166.71	2.10	0.85	0.85
43.10	141.54	104.80	1.51	158.67	2.16	0.84	0.84
43.20	127.00	92.93	1.67	155.22	2.22	0.83	0.83

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
43.30	114.88	82.98	1.91	158.67	2.30	0.84	0.84
43.40	105.17	74.92	2.26	169.64	2.38	0.85	0.85
43.50	96.99	68.21	2.67	181.83	2.45	0.87	0.87
43.60	87.91	61.12	3.01	184.17	2.51	0.86	0.86
43.70	82.13	56.81	3.07	174.37	2.51	0.86	0.86
43.80	82.78	57.50	2.74	157.36	2.46	0.84	0.84
43.90	91.57	64.35	2.25	144.98	2.38	0.82	0.82
44.00	103.19	73.37	1.90	139.21	2.29	0.81	0.81
44.10	111.95	80.18	1.71	137.01	2.24	0.81	0.81
44.20	116.80	83.81	1.65	138.27	2.21	0.81	0.81
44.30	116.61	83.18	1.74	144.81	2.25	0.82	0.82
44.40	111.71	78.69	2.01	158.02	2.32	0.84	0.84
44.50	102.58	71.14	2.43	172.75	2.41	0.86	0.86
44.60	93.13	63.78	2.79	177.83	2.47	0.86	0.86
44.70	89.79	61.35	2.75	168.46	2.46	0.85	0.85
44.80	96.85	66.93	2.27	151.81	2.38	0.83	0.83
44.90	113.10	79.55	1.79	142.30	2.26	0.82	0.82
45.00	132.27	94.33	1.54	145.46	2.17	0.82	0.82
45.10	147.43	105.80	1.46	154.46	2.13	0.83	0.83
45.20	155.41	111.47	1.46	162.21	2.12	0.84	0.84
45.30	156.28	111.60	1.49	166.12	2.14	0.85	0.85
45.40	151.54	107.52	1.55	166.61	2.17	0.85	0.85
45.50	142.44	100.16	1.66	165.78	2.22	0.85	0.85
45.60	129.99	90.25	1.86	167.45	2.28	0.85	0.85
45.70	115.63	78.99	2.20	173.53	2.36	0.86	0.86
45.80	101.57	68.20	2.65	180.86	2.45	0.87	0.87
45.90	89.43	59.18	3.07	181.54	2.51	0.87	0.87
46.00	80.36	52.68	3.26	171.70	2.54	0.88	0.88
46.10	75.66	49.51	3.14	155.32	2.52	0.84	0.84
46.20	75.96	49.99	2.77	138.71	2.47	0.81	0.81
46.30	81.99	54.66	2.30	125.66	2.39	0.79	0.79
46.40	93.65	63.56	1.85	117.53	2.28	0.78	0.78
46.50	110.56	76.54	1.53	117.13	2.16	0.78	0.78
46.60	129.39	90.92	1.38	125.92	2.08	0.79	0.79
46.70	144.05	101.68	1.35	137.61	2.05	0.81	0.81
46.80	149.85	105.16	1.39	146.60	2.08	0.82	0.82
46.90	147.45	102.23	1.50	153.73	2.15	0.83	0.83
47.00	142.18	97.28	1.67	162.30	2.22	0.84	0.84
47.10	138.12	93.55	1.82	170.72	2.27	0.85	0.85
47.20	136.30	91.82	1.90	174.43	2.29	0.86	0.86
47.30	137.24	92.45	1.86	171.87	2.28	0.85	0.85
47.40	142.58	96.55	1.73	166.68	2.24	0.85	0.85
47.50	152.84	104.38	1.58	164.46	2.18	0.85	0.85
47.60	165.80	114.11	1.47	167.72	2.13	0.85	0.85
47.70	177.89	123.01	1.42	174.14	2.10	0.86	0.86
47.80	187.02	129.49	1.40	180.72	2.08	0.87	0.87
47.90	192.69	133.40	1.39	184.92	2.08	0.87	0.87
48.00	196.25	135.83	1.38	187.00	2.07	0.87	0.87

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
48.10	199.18	137.90	1.36	188.02	2.06	0.87	0.87
48.20	202.36	140.14	1.35	189.38	2.05	0.88	0.88
48.30	204.97	141.89	1.34	190.75	2.04	0.88	0.88
48.40	206.02	142.34	1.35	191.69	2.04	0.88	0.88
48.50	205.06	141.17	1.36	191.83	2.05	0.88	0.88
48.60	202.72	138.98	1.38	191.18	2.07	0.88	0.88
48.70	200.81	137.19	1.39	190.43	2.08	0.88	0.88
48.80	200.45	136.68	1.39	189.96	2.08	0.88	0.88
48.90	202.19	137.80	1.38	190.37	2.07	0.88	0.88
49.00	205.17	139.85	1.37	191.52	2.06	0.88	0.88
49.10	208.80	142.34	1.36	193.42	2.05	0.88	0.88
49.20	212.77	145.01	1.35	195.97	2.05	0.88	0.88
49.30	217.38	148.13	1.34	199.07	2.04	0.89	0.89
49.40	221.74	151.06	1.34	202.00	2.03	0.89	0.89
49.50	222.23	151.15	1.34	202.10	2.03	0.89	0.89
49.60	216.25	146.54	1.35	197.41	2.04	0.88	0.88
49.70	208.44	140.66	1.36	191.32	2.05	0.88	0.88
49.80	204.58	137.59	1.37	188.42	2.06	0.87	0.87
49.90	205.34	137.86	1.37	188.96	2.06	0.87	0.87

Abbreviations

q_t :	Total cone resistance
K_c :	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c :	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

LIQUEFACTION ANALYSIS REPORT

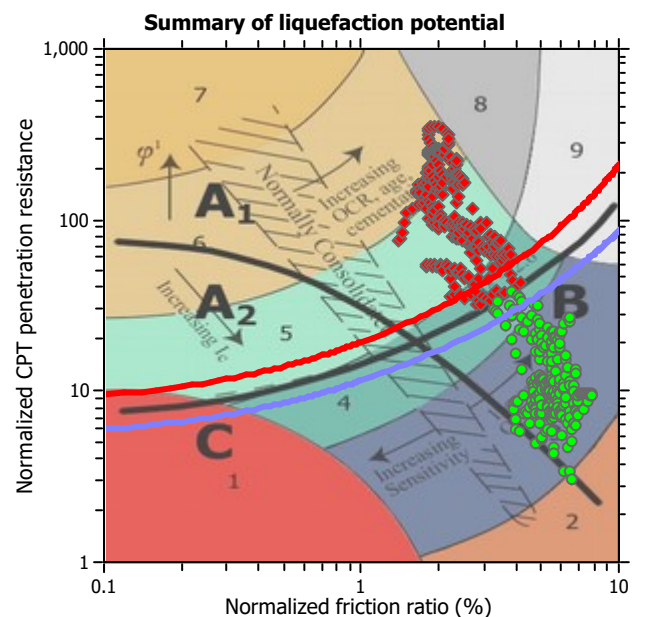
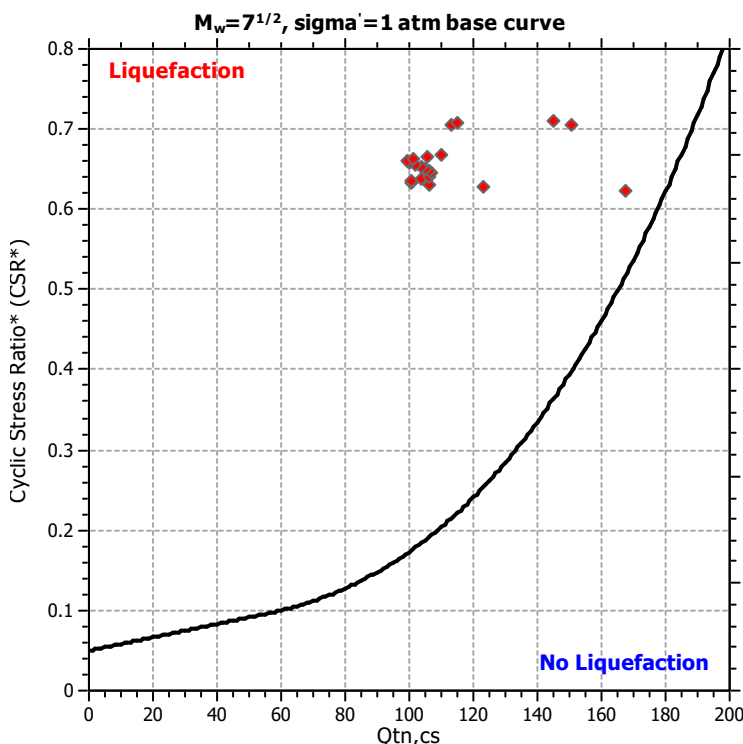
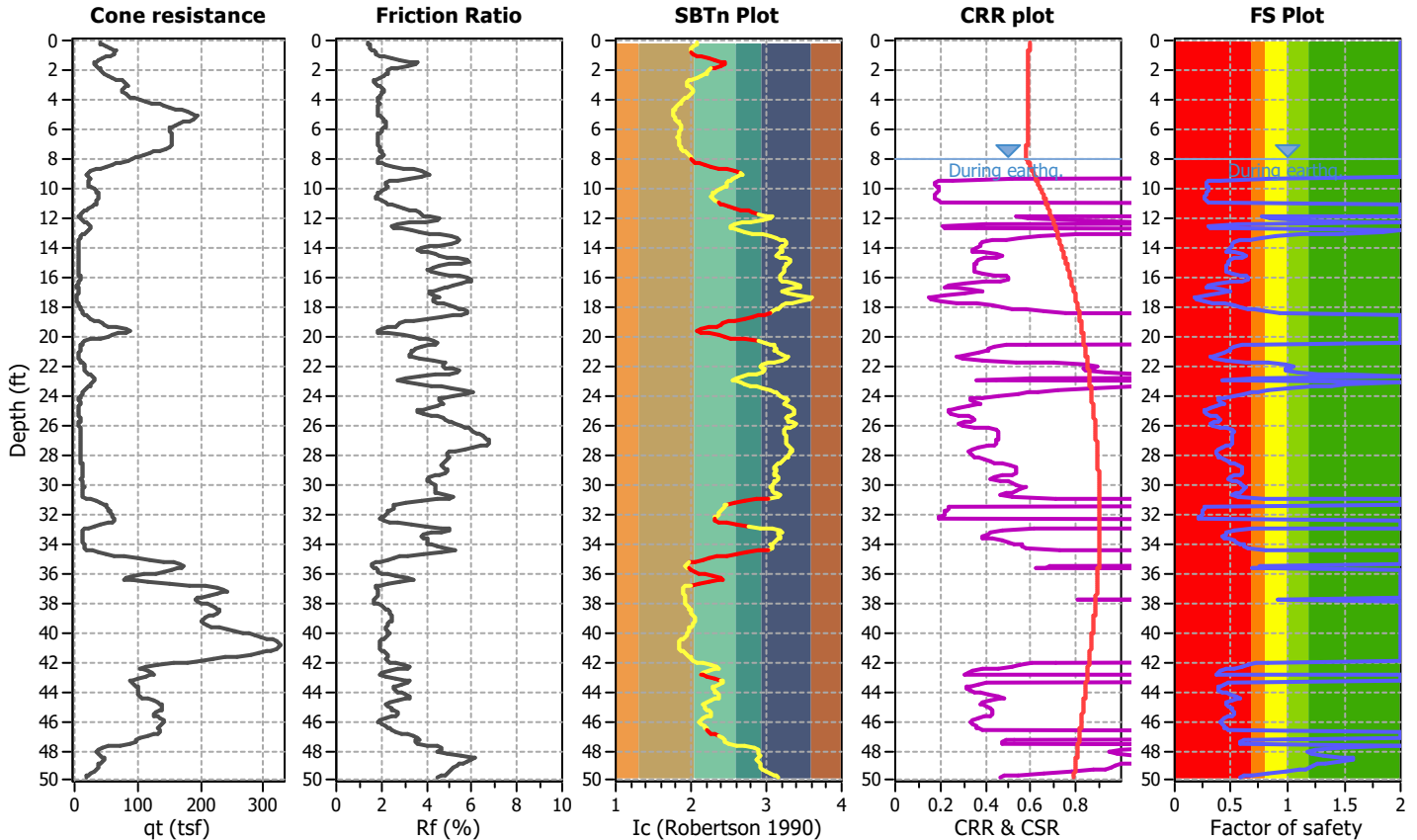
Project title : 21-483 Equestrian Estates

Location : Avenue 64 at Harrison Street, Thermal California

CPT file : CPT-4 Robt 2009

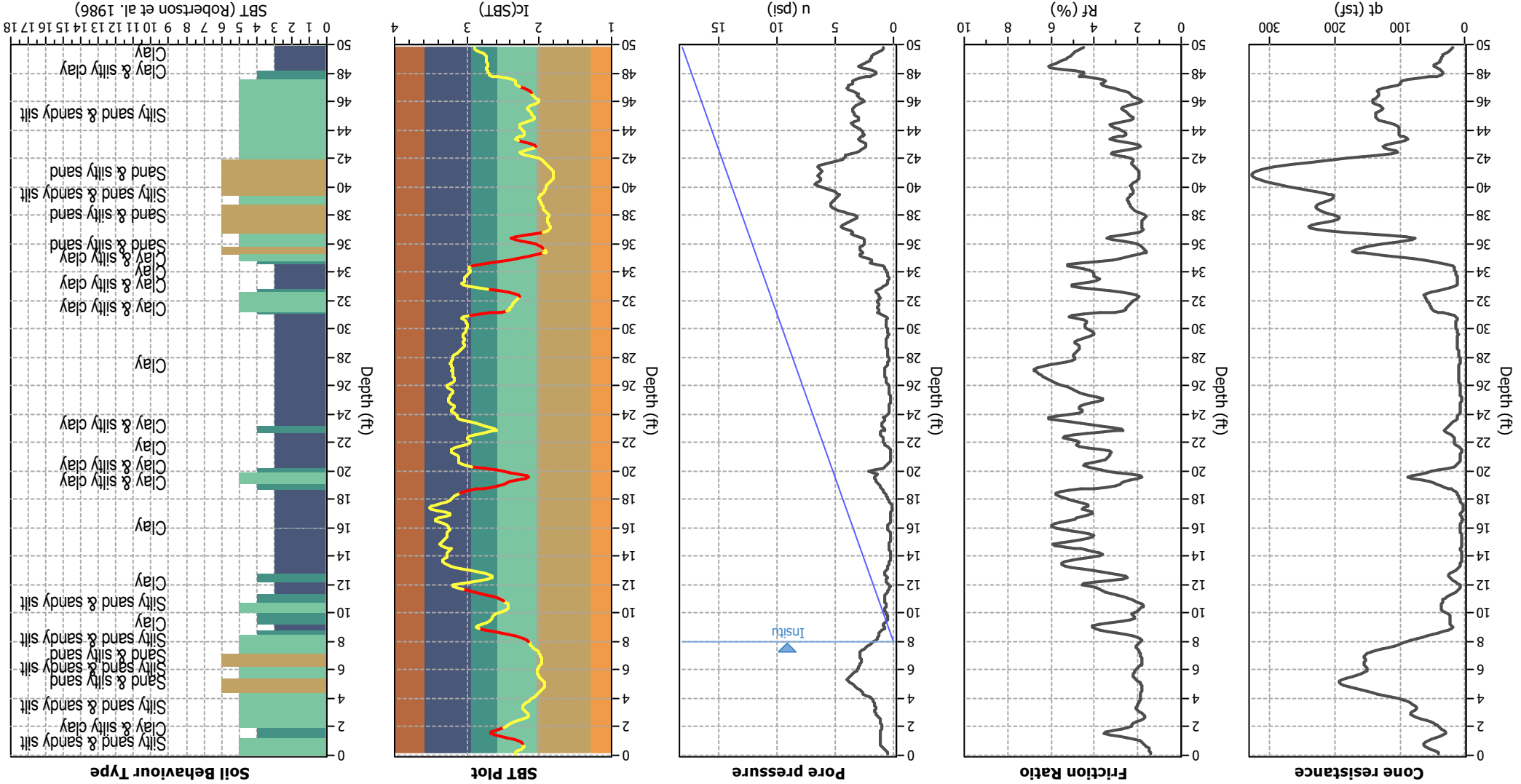
Input parameters and analysis data

Analysis method:	Robertson (2009)	G.W.T. (in-situ):	8.00 ft	Use fill:	No	Clay like behavior	
Fines correction method:	Robertson (2009)	G.W.T. (earthq.):	8.00 ft	Fill height:	N/A	applied:	All soils
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude M_w :	7.34	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.74	Unit weight calculation:	Based on SBT	K_o applied:	No	MSF method:	Method based



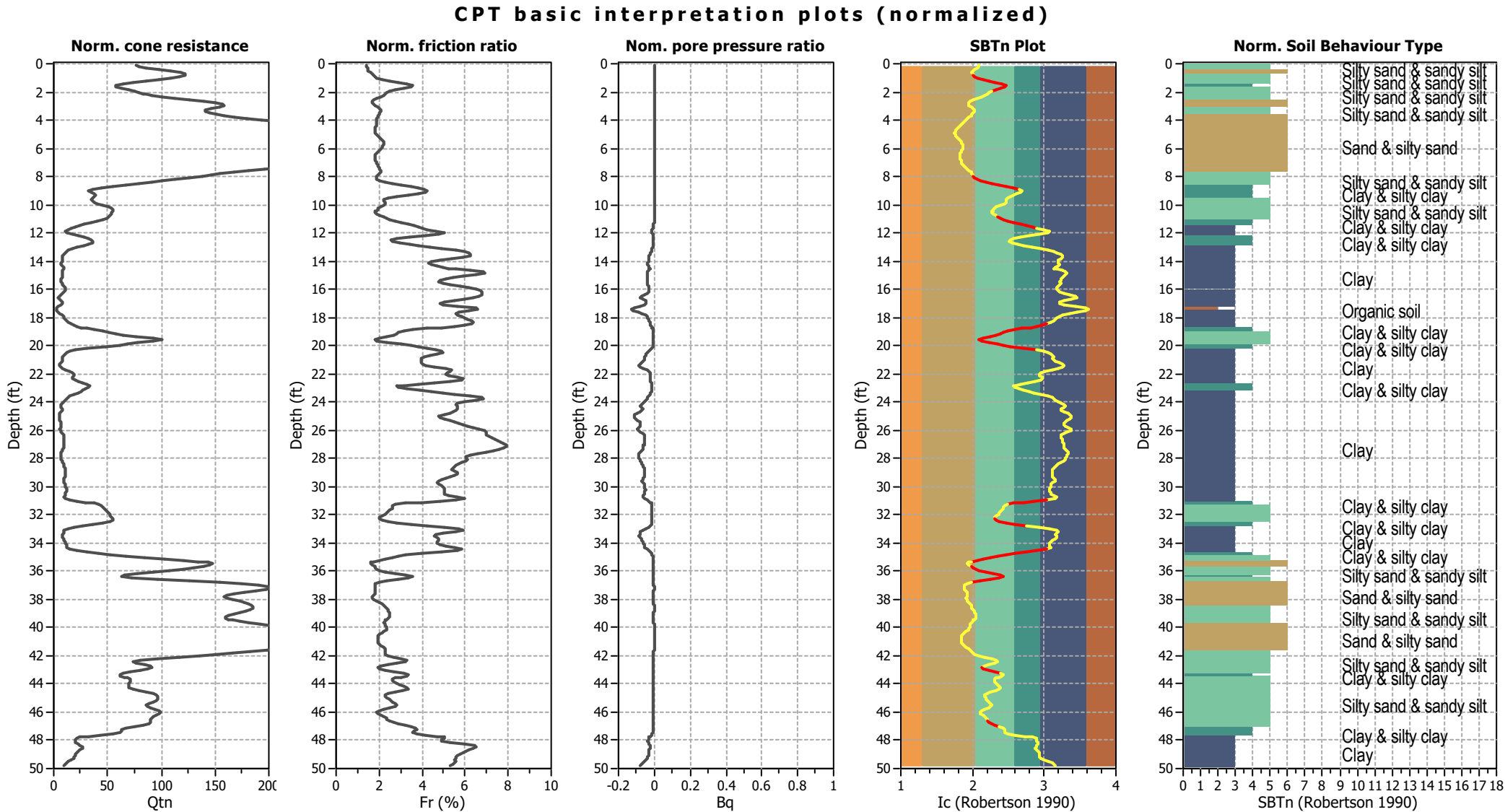
Zone A1: Cyclic liquefaction likely depending on size and duration of cyclic loading
 Zone A2: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
 Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
 Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



Input parameters and analysis data

Analysis method:	Robertson (2009)	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Transition detect. applied:	Yes
Points to test:	Based on Ic value	K _g applied:	No
Earthquake magnitude M _w :	7.34	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Limit depth applied:	No
Depth to water table (instu):	8.00 ft	Limit depth:	N/A
Depth to water table (earthq.):	8.00 ft	Unit weight calculation:	Based on SBT
		Use fill:	No
		Fill height:	N/A



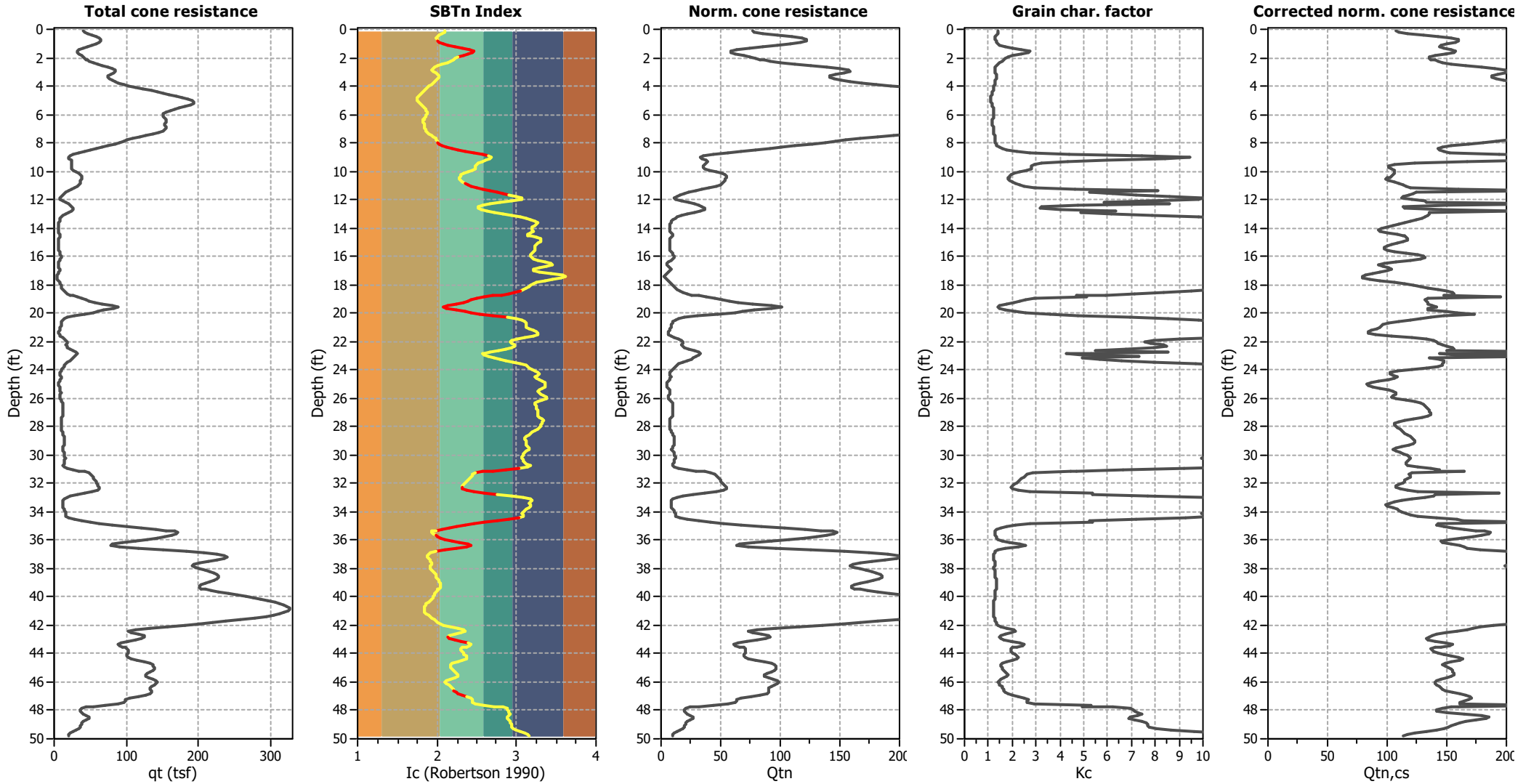
Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	No
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

SBTn legend

1. Sensitive fine grained	4. Clayey silt to silty	7. Gravely sand to sand
2. Organic material	5. Silty sand to sandy silt	8. Very stiff sand to
3. Clay to silty clay	6. Clean sand to silty sand	9. Very stiff fine grained

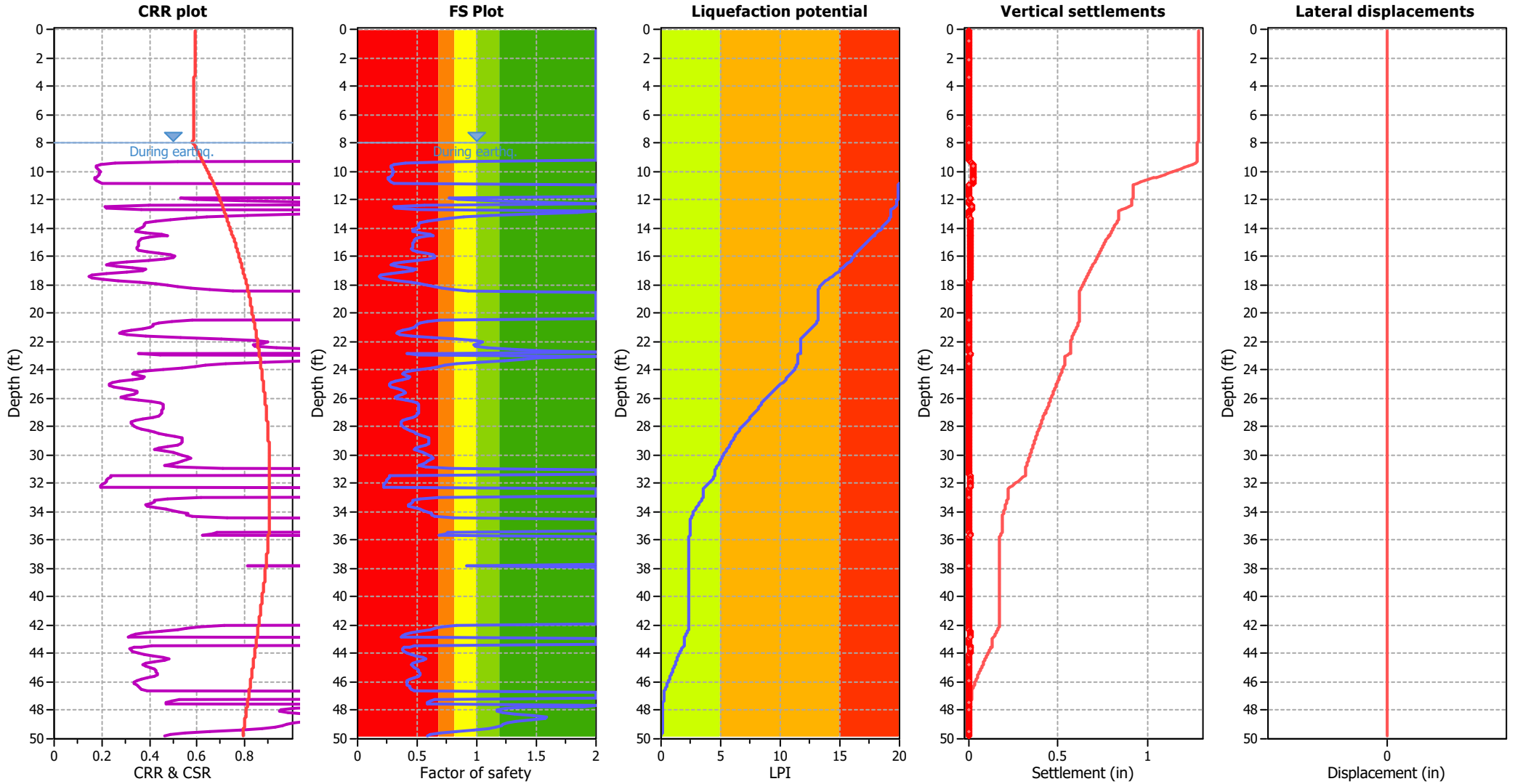
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	No
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (earthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	No
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

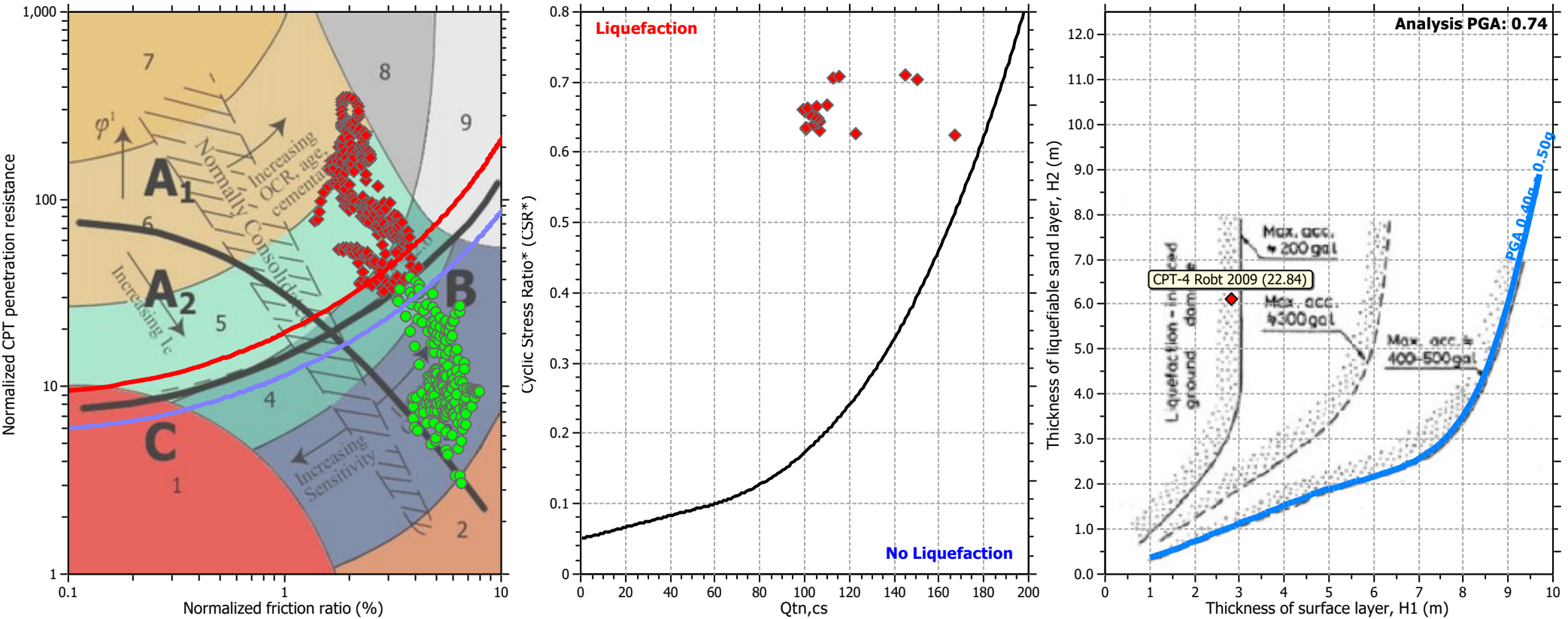
F.S. color scheme

Red	Almost certain it will liquefy
Orange	Very likely to liquefy
Yellow	Liquefaction and no liq. are equally likely
Light Green	Unlike to liquefy
Dark Green	Almost certain it will not liquefy

LPI color scheme

Red	Very high risk
Orange	High risk
Yellow	Low risk

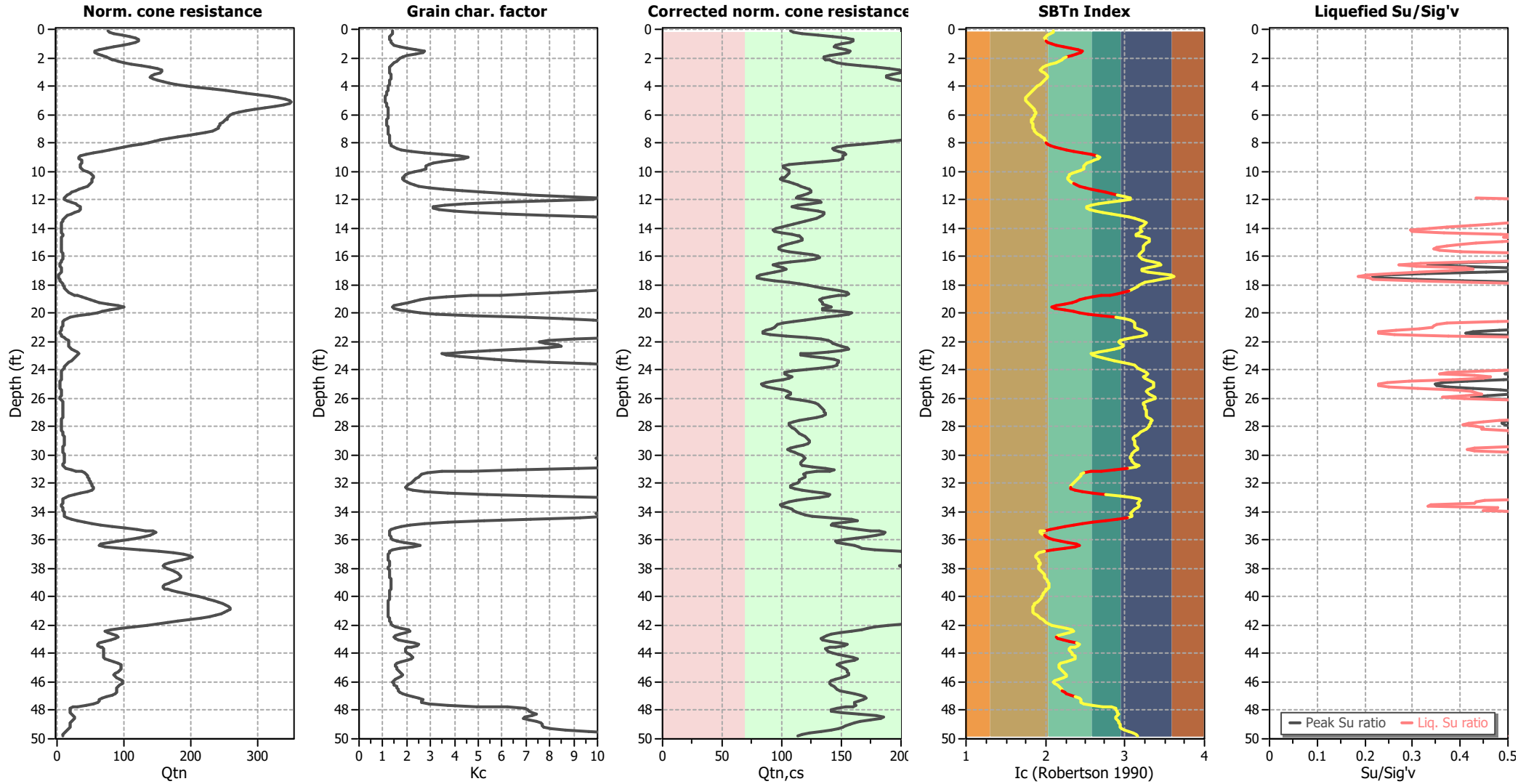
Liquefaction analysis summary plots



Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_0 applied:	No
Earthquake magnitude M_w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

Check for strength loss plots (Robertson (2010))



Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	No
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

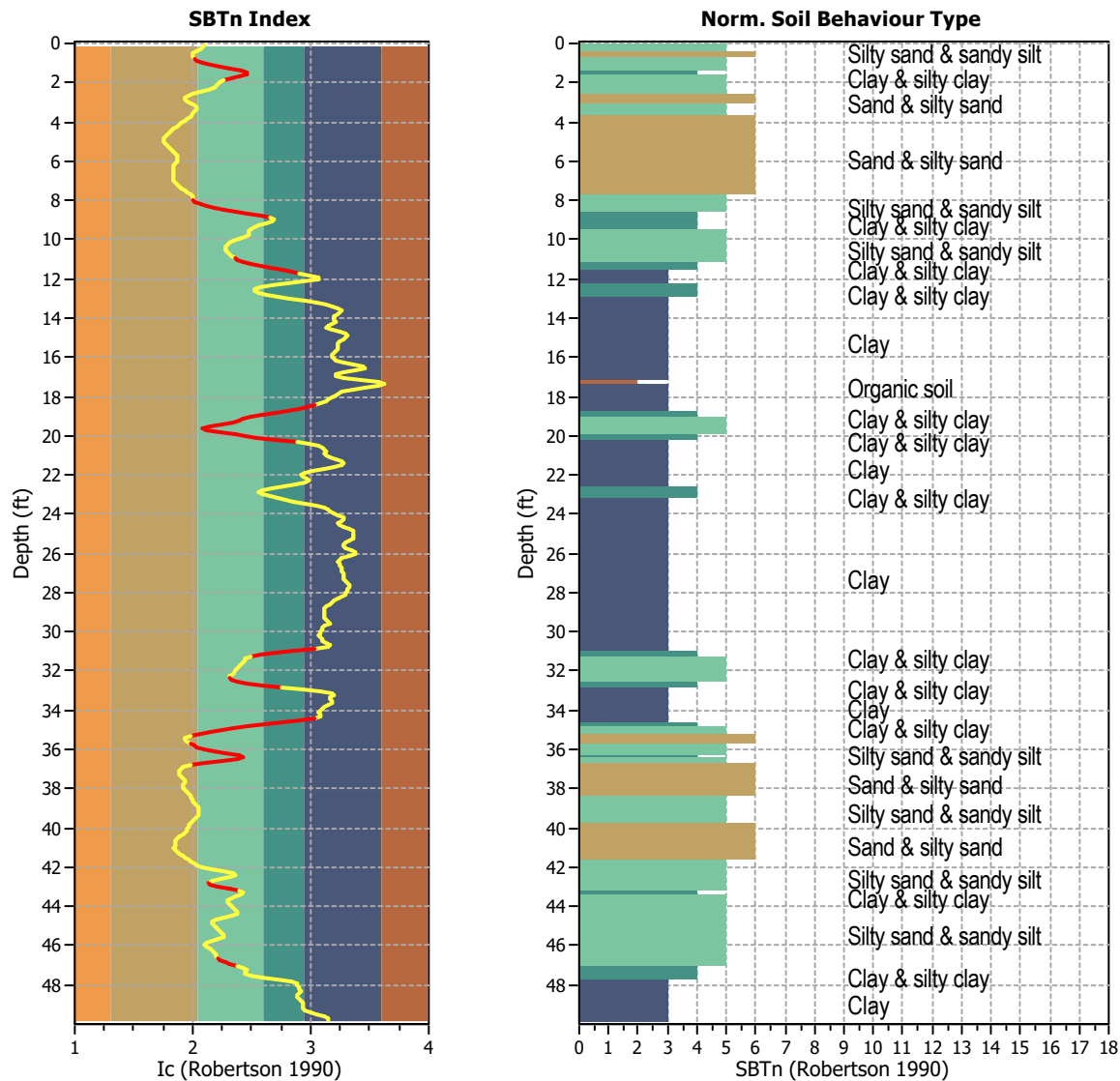
TRANSITION LAYER DETECTION ALGORITHM REPORT

Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vise-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between $1.80 < I_c < 3.0$) and a rate of change of I_c . Transitions typically occur when the rate of change of I_c is fast (i.e. ΔI_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties

I_c minimum check value: 1.70
 I_c maximum check value: 3.00
 I_c change ratio value: 0.0250
Minimum number of points in layer: 4

General statistics

Total points in CPT file: 498
Total points excluded: 96
Exclusion percentage: 19.28%
Number of layers detected: 13

Transition layer No	Number of points	Depth	SBT _n number	SBT _n description
Transition layer 1	7	Start depth: 0.90 (ft)	5	Silty sand & sandy silt
		End depth: 1.50 (ft)	4	Clay & silty clay
Transition layer 2	5	Start depth: 1.60 (ft)	4	Clay & silty clay
		End depth: 2.00 (ft)	5	Silty sand & sandy silt
Transition layer 3	10	Start depth: 8.10 (ft)	5	Silty sand & sandy silt
		End depth: 9.00 (ft)	4	Clay & silty clay
Transition layer 4	9	Start depth: 11.00 (ft)	5	Silty sand & sandy silt
		End depth: 11.80 (ft)	3	Clay
Transition layer 5	12	Start depth: 18.50 (ft)	3	Clay
		End depth: 19.60 (ft)	5	Silty sand & sandy silt
Transition layer 6	9	Start depth: 19.60 (ft)	5	Silty sand & sandy silt
		End depth: 20.40 (ft)	3	Clay
Transition layer 7	5	Start depth: 31.00 (ft)	3	Clay
		End depth: 31.40 (ft)	5	Silty sand & sandy silt
Transition layer 8	6	Start depth: 32.40 (ft)	5	Silty sand & sandy silt
		End depth: 32.90 (ft)	3	Clay
Transition layer 9	10	Start depth: 34.50 (ft)	3	Clay
		End depth: 35.40 (ft)	6	Sand & silty sand
Transition layer 10	7	Start depth: 35.80 (ft)	5	Silty sand & sandy silt
		End depth: 36.40 (ft)	4	Clay & silty clay
Transition layer 11	6	Start depth: 36.40 (ft)	4	Clay & silty clay
		End depth: 36.90 (ft)	6	Sand & silty sand
Transition layer 12	5	Start depth: 42.90 (ft)	5	Silty sand & sandy silt
		End depth: 43.30 (ft)	4	Clay & silty clay
Transition layer 13	5	Start depth: 46.70 (ft)	5	Silty sand & sandy silt
		End depth: 47.10 (ft)	4	Clay & silty clay

Start depth: Depth where the transition layer begins

End depth: Depth where the transition layer ends

:: Field input data ::						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1	0.10	41.00	0.56	0.56	15.55	115.03
2	0.20	39.03	0.56	0.56	15.49	115.52
3	0.30	44.69	0.66	0.66	14.86	116.49
4	0.40	51.96	0.75	0.75	13.73	117.89
5	0.50	58.56	0.87	0.87	12.98	119.18
6	0.60	63.15	1.00	1.00	12.80	120.28
7	0.70	65.24	1.10	1.10	12.94	120.99
8	0.80	65.22	1.14	1.14	13.23	121.22
9	0.90	62.85	1.10	1.10	13.84	121.10
10	1.00	58.21	1.09	1.09	15.06	120.82
11	1.10	51.50	1.09	1.09	17.09	120.59
12	1.20	45.48	1.11	1.11	19.87	120.37
13	1.30	39.28	1.13	1.13	23.16	120.04
14	1.40	32.97	1.11	1.11	26.60	119.64
15	1.50	29.52	1.09	1.09	28.93	119.30
16	1.60	29.90	1.09	1.09	28.67	119.21
17	1.70	33.28	1.06	1.06	26.38	119.20
18	1.80	36.76	1.00	1.00	23.59	119.15
19	1.90	40.00	0.97	0.97	21.36	119.08
20	2.00	42.42	0.96	0.96	20.06	119.22
21	2.10	44.01	1.00	1.00	19.49	119.53
22	2.20	45.36	1.06	1.06	19.10	119.97
23	2.30	48.11	1.10	1.10	18.23	120.37
24	2.40	52.55	1.11	1.11	16.68	120.73
25	2.50	58.94	1.12	1.12	14.81	121.17
26	2.60	67.10	1.17	1.17	13.14	121.73
27	2.70	74.58	1.25	1.25	12.01	122.43
28	2.80	80.32	1.35	1.35	11.43	123.14
29	2.90	84.27	1.46	1.46	11.35	123.77
30	3.00	85.07	1.54	1.54	11.73	124.22
31	3.10	82.32	1.62	1.62	12.40	124.38
32	3.20	77.74	1.59	1.59	13.19	124.26
33	3.30	73.68	1.54	1.54	13.68	124.03
34	3.40	73.39	1.53	1.53	13.68	123.98
35	3.50	77.07	1.57	1.57	13.32	124.16
36	3.60	80.36	1.61	1.61	12.83	124.45
37	3.70	83.50	1.65	1.65	12.33	124.78
38	3.80	88.60	1.71	1.71	11.73	125.19
39	3.90	95.36	1.80	1.80	11.04	125.67
40	4.00	102.34	1.88	1.88	10.48	126.28
41	4.10	109.71	2.04	2.04	9.95	127.21
42	4.20	124.22	2.38	2.38	9.48	128.23
43	4.30	135.70	2.59	2.59	9.01	129.05
44	4.40	141.94	2.66	2.66	8.55	129.55
45	4.50	149.87	2.75	2.75	8.14	129.94
46	4.60	158.76	2.89	2.89	7.77	130.43
47	4.70	168.42	3.07	3.07	7.47	130.97
48	4.80	177.89	3.24	3.24	7.26	131.50

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
49	4.90	186.95	3.41	3.41	7.17	131.97
50	5.00	191.99	3.56	3.56	7.20	132.37
51	5.10	194.46	3.71	3.71	7.37	132.69
52	5.20	194.11	3.84	3.84	7.70	132.93
53	5.30	189.61	3.94	3.94	8.14	133.01
54	5.40	181.39	3.92	3.92	8.61	132.89
55	5.50	173.21	3.80	3.80	9.01	132.59
56	5.60	165.67	3.63	3.63	9.29	132.22
57	5.70	160.44	3.52	3.52	9.52	131.83
58	5.80	154.26	3.37	3.37	9.67	131.41
59	5.90	148.77	3.16	3.16	9.66	131.02
60	6.00	150.43	3.07	3.07	9.50	130.73
61	6.10	151.75	3.01	3.01	9.28	130.58
62	6.20	152.44	2.95	2.95	9.09	130.45
63	6.30	153.63	2.89	2.89	8.90	130.34
64	6.40	155.75	2.86	2.86	8.77	130.26
65	6.50	155.56	2.83	2.83	8.73	130.19
66	6.60	154.18	2.81	2.81	8.78	130.13
67	6.70	153.47	2.79	2.79	8.85	130.07
68	6.80	153.11	2.79	2.79	8.89	130.09
69	6.90	154.71	2.82	2.82	8.93	130.15
70	7.00	155.67	2.86	2.86	9.05	130.27
71	7.10	154.21	2.91	2.91	9.26	130.32
72	7.20	151.43	2.90	2.90	9.55	130.23
73	7.30	145.74	2.82	2.82	9.93	129.97
74	7.40	136.94	2.71	2.71	10.44	129.52
75	7.50	127.06	2.56	2.56	11.09	128.98
76	7.60	117.34	2.42	2.42	11.75	128.39
77	7.70	109.86	2.30	2.30	12.39	127.66
78	7.80	99.48	2.04	2.04	12.82	126.82
79	7.90	94.17	1.84	1.84	12.88	126.06
80	8.00	95.88	1.78	1.78	13.02	125.22
81	8.10	83.51	1.52	1.52	13.52	124.26
82	8.20	72.14	1.34	1.34	14.72	123.19
83	8.30	66.13	1.32	1.32	16.32	122.51
84	8.40	58.66	1.30	1.30	18.36	122.13
85	8.50	50.47	1.29	1.29	21.20	121.71
86	8.60	42.14	1.28	1.28	24.87	121.00
87	8.70	33.04	1.17	1.17	29.13	119.90
88	8.80	26.06	1.01	1.01	33.83	118.14
89	8.90	19.45	0.78	0.78	37.86	116.46
90	9.00	17.86	0.74	0.74	39.83	115.80
91	9.10	20.55	0.87	0.87	38.87	116.25
92	9.20	22.68	0.88	0.88	36.12	116.73
93	9.30	24.95	0.81	0.81	33.68	116.11
94	9.40	23.48	0.63	0.63	31.65	114.81
95	9.50	22.40	0.51	0.51	30.43	113.31
96	9.60	22.33	0.47	0.47	29.73	112.62

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
97	9.70	22.78	0.49	0.49	29.54	112.72
98	9.80	23.33	0.52	0.52	29.48	113.34
99	9.90	24.87	0.58	0.58	28.20	114.36
100	10.00	30.30	0.67	0.67	26.00	115.37
101	10.10	34.75	0.69	0.69	23.92	116.13
102	10.20	36.53	0.71	0.71	22.74	116.41
103	10.30	37.03	0.70	0.70	22.24	116.40
104	10.40	37.03	0.68	0.68	21.90	116.19
105	10.50	37.03	0.64	0.64	21.61	115.93
106	10.60	37.03	0.63	0.63	21.66	115.88
107	10.70	36.64	0.66	0.66	22.37	116.08
108	10.80	35.22	0.71	0.71	23.48	116.46
109	10.90	34.64	0.76	0.76	24.63	116.81
110	11.00	34.13	0.78	0.78	25.76	116.92
111	11.10	31.68	0.77	0.77	27.54	116.63
112	11.20	27.08	0.73	0.73	30.36	116.02
113	11.30	22.93	0.69	0.69	34.19	115.06
114	11.40	18.70	0.62	0.62	38.52	113.88
115	11.50	15.21	0.54	0.54	43.21	112.39
116	11.60	12.41	0.46	0.46	47.64	110.92
117	11.70	10.81	0.41	0.41	52.05	109.34
118	11.80	8.80	0.34	0.34	57.77	107.54
119	11.90	6.37	0.26	0.26	63.26	106.67
120	12.00	7.32	0.34	0.34	62.58	108.20
121	12.10	10.88	0.52	0.52	54.40	111.06
122	12.20	15.19	0.64	0.64	45.91	113.18
123	12.30	19.58	0.65	0.65	39.01	114.02
124	12.40	22.65	0.59	0.59	34.35	114.02
125	12.50	23.71	0.55	0.55	31.69	114.28
126	12.60	26.46	0.65	0.65	31.51	115.05
127	12.70	26.27	0.76	0.76	33.16	115.83
128	12.80	23.03	0.78	0.78	36.57	115.79
129	12.90	19.04	0.71	0.71	41.35	114.89
130	13.00	14.99	0.62	0.62	47.44	113.37
131	13.10	11.10	0.52	0.52	54.87	111.67
132	13.20	8.80	0.46	0.46	62.41	110.39
133	13.30	8.36	0.46	0.46	67.36	109.50
134	13.40	7.62	0.41	0.41	71.21	108.55
135	13.50	6.21	0.34	0.34	75.05	107.44
136	13.60	5.97	0.33	0.33	77.77	106.45
137	13.70	5.97	0.30	0.30	77.12	105.89
138	13.80	5.97	0.28	0.28	75.24	105.19
139	13.90	5.97	0.24	0.24	73.16	104.39
140	14.00	5.97	0.22	0.22	72.36	103.48
141	14.10	5.53	0.19	0.19	72.96	102.86
142	14.20	5.38	0.20	0.20	73.75	103.13
143	14.30	5.99	0.24	0.24	71.91	104.72
144	14.40	7.34	0.32	0.32	68.79	106.59

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
145	14.50	8.17	0.38	0.38	68.26	107.49
146	14.60	7.17	0.35	0.35	71.34	107.42
147	14.70	6.16	0.33	0.33	77.10	107.05
148	14.80	5.97	0.36	0.36	81.34	107.01
149	14.90	5.97	0.36	0.36	82.13	106.98
150	15.00	5.97	0.33	0.33	80.88	106.53
151	15.10	5.97	0.30	0.30	78.94	105.83
152	15.20	5.97	0.27	0.27	77.19	105.19
153	15.30	5.97	0.26	0.26	75.89	104.68
154	15.40	5.97	0.24	0.24	75.01	104.32
155	15.50	5.97	0.24	0.24	74.91	104.23
156	15.60	5.97	0.25	0.25	75.38	104.65
157	15.70	6.20	0.28	0.28	74.12	106.09
158	15.80	7.60	0.38	0.38	72.35	107.91
159	15.90	8.36	0.46	0.46	71.19	109.42
160	16.00	8.36	0.49	0.49	71.61	110.16
161	16.10	8.36	0.50	0.50	72.34	110.35
162	16.20	8.35	0.50	0.50	74.55	109.70
163	16.30	6.77	0.40	0.40	78.96	108.19
164	16.40	5.33	0.30	0.30	86.39	105.76
165	16.50	4.39	0.22	0.22	93.21	103.48
166	16.60	3.98	0.19	0.19	94.87	102.52
167	16.70	4.57	0.22	0.22	88.21	103.62
168	16.80	6.23	0.30	0.30	79.31	105.19
169	16.90	7.17	0.31	0.31	73.45	105.95
170	17.00	6.97	0.27	0.27	73.43	105.30
171	17.10	5.70	0.23	0.23	79.77	103.71
172	17.20	4.17	0.19	0.19	92.59	101.63
173	17.30	3.16	0.15	0.15	100.00	99.76
174	17.40	2.99	0.14	0.14	100.00	99.09
175	17.50	3.58	0.15	0.15	100.00	99.40
176	17.60	3.81	0.16	0.16	94.74	101.22
177	17.70	5.21	0.23	0.23	85.66	103.64
178	17.80	6.62	0.31	0.31	77.56	106.45
179	17.90	8.03	0.41	0.41	73.55	108.28
180	18.00	8.36	0.44	0.44	71.22	109.50
181	18.10	8.97	0.48	0.48	69.42	110.57
182	18.20	10.23	0.57	0.57	67.42	111.77
183	18.30	11.10	0.65	0.65	64.67	113.15
184	18.40	12.80	0.75	0.75	61.23	114.40
185	18.50	14.92	0.84	0.84	56.69	115.60
186	18.60	17.52	0.92	0.92	51.67	116.65
187	18.70	20.81	0.99	0.99	46.19	117.62
188	18.80	25.48	1.05	1.05	40.47	118.49
189	18.90	31.13	1.08	1.08	34.94	119.31
190	19.00	37.95	1.13	1.13	30.53	120.13
191	19.10	44.31	1.22	1.22	27.80	120.97
192	19.20	47.84	1.33	1.33	26.03	121.84

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
193	19.30	53.35	1.45	1.45	23.96	122.73
194	19.40	63.92	1.55	1.55	20.58	123.67
195	19.50	81.62	1.63	1.63	17.02	124.43
196	19.60	96.87	1.63	1.63	15.35	124.67
197	19.70	87.68	1.56	1.56	16.45	124.04
198	19.80	59.40	1.36	1.36	20.23	123.82
199	19.90	57.64	1.76	1.76	24.67	124.33
200	20.00	60.92	2.13	2.13	27.85	124.36
201	20.10	41.31	1.57	1.57	32.42	122.48
202	20.20	21.92	0.90	0.90	40.77	118.75
203	20.30	16.55	0.73	0.73	50.92	114.99
204	20.40	12.77	0.59	0.59	57.49	112.91
205	20.50	10.96	0.49	0.49	62.48	110.93
206	20.60	9.60	0.39	0.39	65.47	109.02
207	20.70	8.36	0.31	0.31	66.79	107.41
208	20.80	8.36	0.29	0.29	67.25	106.46
209	20.90	8.36	0.28	0.28	66.82	106.25
210	21.00	8.36	0.28	0.28	67.28	105.97
211	21.10	7.90	0.26	0.26	69.64	105.19
212	21.20	6.67	0.22	0.22	73.52	104.00
213	21.30	5.97	0.19	0.19	77.33	102.94
214	21.40	5.97	0.19	0.19	79.15	102.89
215	21.50	6.18	0.22	0.22	78.04	104.47
216	21.60	7.51	0.32	0.32	73.34	107.58
217	21.70	10.48	0.50	0.50	66.09	111.00
218	21.80	13.95	0.69	0.69	59.39	113.65
219	21.90	16.71	0.80	0.80	54.99	115.15
220	22.00	17.85	0.82	0.82	53.44	115.68
221	22.10	16.99	0.81	0.81	54.43	115.72
222	22.20	15.85	0.82	0.82	56.64	115.80
223	22.30	15.91	0.88	0.88	57.36	116.28
224	22.40	17.59	0.97	0.97	54.99	117.16
225	22.50	20.78	1.07	1.07	50.01	118.16
226	22.60	25.38	1.13	1.13	44.22	118.86
227	22.70	29.79	1.10	1.10	39.00	118.90
228	22.80	31.89	0.94	0.94	35.22	118.27
229	22.90	31.90	0.81	0.81	33.64	117.48
230	23.00	30.29	0.80	0.80	34.67	117.16
231	23.10	27.68	0.87	0.87	37.74	117.40
232	23.20	25.65	0.95	0.95	41.54	117.83
233	23.30	24.19	1.03	1.03	45.20	117.99
234	23.40	21.70	1.01	1.01	49.37	117.62
235	23.50	17.86	0.91	0.91	55.09	116.61
236	23.60	14.04	0.81	0.81	61.96	115.56
237	23.70	12.62	0.80	0.80	66.78	115.03
238	23.80	13.13	0.83	0.83	68.62	114.45
239	23.90	11.74	0.66	0.66	69.72	113.21
240	24.00	9.83	0.49	0.49	72.13	111.12

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
241	24.10	8.69	0.40	0.40	75.61	109.05
242	24.20	7.60	0.34	0.34	79.05	107.74
243	24.30	7.17	0.33	0.33	79.90	107.61
244	24.40	8.30	0.39	0.39	78.21	108.32
245	24.50	8.96	0.42	0.42	75.93	109.00
246	24.60	8.83	0.41	0.41	76.27	108.72
247	24.70	7.90	0.35	0.35	79.48	107.45
248	24.80	6.48	0.27	0.27	83.74	105.69
249	24.90	5.97	0.23	0.23	86.64	104.12
250	25.00	5.97	0.21	0.21	86.93	103.45
251	25.10	5.97	0.21	0.21	86.87	103.52
252	25.20	6.07	0.23	0.23	85.79	104.49
253	25.30	6.96	0.29	0.29	82.95	106.10
254	25.40	8.07	0.36	0.36	80.16	107.60
255	25.50	8.36	0.40	0.40	78.94	108.51
256	25.60	8.36	0.41	0.41	79.33	108.87
257	25.70	8.36	0.42	0.42	81.12	108.76
258	25.80	7.64	0.39	0.39	84.92	108.19
259	25.90	6.57	0.34	0.34	88.29	107.85
260	26.00	7.10	0.39	0.39	87.60	108.56
261	26.10	8.52	0.49	0.49	82.76	110.23
262	26.20	9.92	0.59	0.59	78.38	111.71
263	26.30	10.72	0.64	0.64	76.22	112.56
264	26.40	10.75	0.65	0.65	75.81	112.95
265	26.50	10.75	0.67	0.67	76.39	113.13
266	26.60	10.75	0.69	0.69	76.96	113.28
267	26.70	10.75	0.69	0.69	77.43	113.40
268	26.80	10.75	0.71	0.71	77.87	113.51
269	26.90	10.75	0.72	0.72	78.34	113.63
270	27.00	10.75	0.73	0.73	78.72	113.72
271	27.10	10.75	0.73	0.73	78.96	113.76
272	27.20	10.75	0.73	0.73	78.97	113.73
273	27.30	10.75	0.72	0.72	79.11	113.47
274	27.40	10.34	0.66	0.66	80.31	112.71
275	27.50	9.14	0.55	0.55	82.35	111.53
276	27.60	8.37	0.48	0.48	83.87	110.32
277	27.70	8.36	0.44	0.44	83.66	109.51
278	27.80	8.36	0.41	0.41	82.58	109.11
279	27.90	8.36	0.40	0.40	81.56	109.08
280	28.00	8.73	0.43	0.43	80.78	109.33
281	28.10	8.96	0.45	0.45	80.20	109.62
282	28.20	8.96	0.45	0.45	78.19	110.13
283	28.30	10.19	0.50	0.50	75.68	110.64
284	28.40	10.75	0.52	0.52	73.32	111.08
285	28.50	10.75	0.51	0.51	71.78	111.35
286	28.60	11.41	0.54	0.54	69.63	111.88
287	28.70	12.82	0.60	0.60	67.47	112.50
288	28.80	13.14	0.61	0.61	66.22	112.97

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
289	28.90	13.14	0.63	0.63	66.40	113.17
290	29.00	13.14	0.65	0.65	66.89	113.32
291	29.10	13.14	0.65	0.65	67.04	113.35
292	29.20	13.14	0.63	0.63	66.65	113.18
293	29.30	13.14	0.60	0.60	66.69	112.61
294	29.40	12.13	0.53	0.53	67.81	111.61
295	29.50	10.78	0.44	0.44	69.23	110.59
296	29.60	10.75	0.43	0.43	69.68	110.09
297	29.70	11.19	0.45	0.45	67.13	110.77
298	29.80	13.31	0.54	0.54	65.39	111.59
299	29.90	13.24	0.56	0.56	65.02	112.18
300	30.00	12.54	0.56	0.56	64.49	112.74
301	30.10	14.78	0.65	0.65	63.60	113.22
302	30.20	14.87	0.66	0.66	62.95	113.48
303	30.30	13.62	0.61	0.61	64.02	113.15
304	30.40	13.36	0.58	0.58	64.78	112.81
305	30.50	13.74	0.59	0.59	65.43	112.63
306	30.60	12.87	0.57	0.57	67.66	112.39
307	30.70	11.48	0.56	0.56	70.78	112.45
308	30.80	11.97	0.63	0.63	69.07	113.82
309	30.90	16.42	0.87	0.87	60.16	116.40
310	31.00	24.61	1.16	1.16	49.49	118.96
311	31.10	34.03	1.33	1.33	40.54	120.56
312	31.20	42.25	1.30	1.30	33.92	121.16
313	31.30	48.23	1.21	1.21	29.98	121.31
314	31.40	50.71	1.25	1.25	28.34	121.58
315	31.50	52.01	1.35	1.35	28.01	121.91
316	31.60	52.84	1.35	1.35	27.52	122.05
317	31.70	54.50	1.29	1.29	26.67	121.96
318	31.80	55.90	1.27	1.27	26.01	121.95
319	31.90	56.61	1.31	1.31	25.56	122.07
320	32.00	58.40	1.33	1.33	24.90	122.10
321	32.10	60.32	1.25	1.25	23.98	121.89
322	32.20	60.43	1.18	1.18	23.15	121.66
323	32.30	61.77	1.19	1.19	22.86	121.81
324	32.40	63.95	1.30	1.30	23.38	122.28
325	32.50	61.78	1.41	1.41	25.33	122.67
326	32.60	53.36	1.47	1.47	29.14	122.64
327	32.70	42.96	1.46	1.46	35.28	121.86
328	32.80	30.42	1.27	1.27	43.68	120.29
329	32.90	20.70	1.01	1.01	53.99	118.10
330	33.00	15.91	0.83	0.83	63.92	115.74
331	33.10	12.76	0.65	0.65	70.90	113.58
332	33.20	10.96	0.51	0.51	73.06	111.97
333	33.30	11.90	0.49	0.49	70.70	111.22
334	33.40	12.96	0.49	0.49	69.83	110.54
335	33.50	10.44	0.39	0.39	71.50	109.77
336	33.60	9.90	0.38	0.38	71.52	110.16

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
337	33.70	13.56	0.55	0.55	69.27	111.22
338	33.80	13.40	0.55	0.55	66.83	112.05
339	33.90	12.94	0.52	0.52	65.28	112.50
340	34.00	15.53	0.63	0.63	63.96	113.05
341	34.10	15.53	0.65	0.65	62.95	113.87
342	34.20	15.53	0.69	0.69	64.12	114.29
343	34.30	15.53	0.74	0.74	64.60	115.20
344	34.40	17.23	0.90	0.90	60.48	117.84
345	34.50	26.55	1.48	1.48	51.94	121.12
346	34.60	39.58	1.98	1.98	43.12	123.40
347	34.70	48.83	1.89	1.89	35.29	124.53
348	34.80	61.25	1.85	1.85	29.06	125.32
349	34.90	77.74	2.17	2.17	24.41	126.73
350	35.00	98.31	2.60	2.60	20.63	128.28
351	35.10	122.27	2.81	2.81	17.39	129.35
352	35.20	142.08	2.82	2.82	14.63	129.77
353	35.30	156.41	2.66	2.66	12.57	129.84
354	35.40	169.29	2.61	2.61	11.41	129.99
355	35.50	175.83	2.79	2.79	11.21	130.26
356	35.60	170.89	2.90	2.90	11.74	130.46
357	35.70	161.21	2.88	2.88	12.47	130.40
358	35.80	155.63	2.83	2.83	13.18	130.01
359	35.90	143.20	2.61	2.61	14.07	129.47
360	36.00	128.06	2.48	2.48	15.67	128.92
361	36.10	112.58	2.52	2.52	18.34	128.51
362	36.20	93.81	2.54	2.54	22.01	128.14
363	36.30	77.77	2.51	2.51	25.97	127.82
364	36.40	71.60	2.59	2.59	27.81	128.10
365	36.50	83.66	2.94	2.94	25.42	129.19
366	36.60	113.82	3.37	3.37	20.52	130.63
367	36.70	152.43	3.61	3.61	15.82	131.70
368	36.80	187.23	3.55	3.55	12.62	132.37
369	36.90	210.72	3.66	3.66	10.92	132.91
370	37.00	225.38	3.98	3.98	10.26	133.65
371	37.10	241.24	4.39	4.39	10.08	134.23
372	37.20	243.91	4.44	4.44	10.06	134.46
373	37.30	237.09	4.32	4.32	10.22	134.26
374	37.40	226.32	4.12	4.12	10.54	133.81
375	37.50	212.54	3.87	3.87	10.91	133.25
376	37.60	200.47	3.61	3.61	11.19	132.60
377	37.70	192.31	3.33	3.33	11.18	131.97
378	37.80	190.02	3.10	3.10	10.92	131.56
379	37.90	194.57	3.10	3.10	10.71	131.64
380	38.00	202.44	3.38	3.38	10.79	132.26
381	38.10	210.31	3.83	3.83	11.17	133.16
382	38.20	216.96	4.31	4.31	11.68	134.07
383	38.30	222.19	4.78	4.78	12.13	134.79
384	38.40	225.73	5.05	5.05	12.42	135.27

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
385	38.50	228.35	5.18	5.18	12.62	135.59
386	38.60	229.78	5.39	5.39	12.81	135.76
387	38.70	227.47	5.42	5.42	13.08	135.81
388	38.80	221.38	5.33	5.33	13.42	135.71
389	38.90	214.86	5.29	5.29	13.78	135.52
390	39.00	208.71	5.16	5.16	14.12	135.30
391	39.10	202.88	5.02	5.02	14.30	135.05
392	39.20	199.95	4.88	4.88	14.30	134.82
393	39.30	199.94	4.76	4.76	14.09	134.65
394	39.40	202.72	4.68	4.68	13.75	134.61
395	39.50	208.73	4.74	4.74	13.32	134.71
396	39.60	217.25	4.83	4.83	12.87	134.97
397	39.70	227.80	5.00	5.00	12.46	135.39
398	39.80	241.02	5.36	5.36	12.16	135.96
399	39.90	254.53	5.78	5.78	11.96	136.60
400	40.00	267.01	6.16	6.16	11.85	137.18
401	40.10	276.08	6.52	6.52	11.69	137.28
402	40.20	286.98	6.73	6.73	11.34	137.28
403	40.30	297.29	6.61	6.61	10.77	137.28
404	40.40	306.47	6.42	6.42	10.12	137.28
405	40.50	313.76	6.26	6.26	9.59	137.28
406	40.60	319.57	6.19	6.19	9.30	137.28
407	40.70	324.16	6.36	6.36	9.22	137.28
408	40.80	327.41	6.50	6.50	9.19	137.28
409	40.90	327.89	6.37	6.37	9.12	137.28
410	41.00	325.27	6.23	6.23	9.08	137.28
411	41.10	320.12	6.14	6.14	9.24	137.28
412	41.20	312.89	6.19	6.19	9.60	137.28
413	41.30	305.10	6.32	6.32	10.14	137.28
414	41.40	295.58	6.45	6.45	10.76	137.28
415	41.50	279.85	6.31	6.31	11.42	137.28
416	41.60	259.50	5.93	5.93	12.08	136.80
417	41.70	237.21	5.42	5.42	12.68	135.95
418	41.80	216.87	4.83	4.83	13.19	135.03
419	41.90	202.63	4.43	4.43	13.92	134.19
420	42.00	182.14	4.20	4.20	15.34	133.55
421	42.10	157.40	4.15	4.15	17.85	133.01
422	42.20	131.87	4.09	4.09	21.06	132.27
423	42.30	108.58	3.65	3.65	23.91	131.21
424	42.40	96.91	3.12	3.12	24.63	130.16
425	42.50	104.19	2.92	2.92	22.72	129.54
426	42.60	117.86	2.77	2.77	19.82	129.22
427	42.70	126.64	2.51	2.51	17.66	128.84
428	42.80	127.25	2.33	2.33	16.83	128.45
429	42.90	122.61	2.34	2.34	17.51	128.26
430	43.00	112.59	2.42	2.42	19.63	128.38
431	43.10	100.42	2.64	2.64	22.75	128.65
432	43.20	91.07	2.87	2.87	25.88	128.92

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
433	43.30	86.64	2.97	2.97	27.47	129.03
434	43.40	88.66	2.89	2.89	26.92	128.97
435	43.50	95.01	2.76	2.76	25.15	128.77
436	43.60	99.48	2.60	2.60	23.47	128.56
437	43.70	101.90	2.54	2.54	22.61	128.44
438	43.80	102.15	2.57	2.57	22.57	128.50
439	43.90	101.13	2.64	2.64	22.96	128.70
440	44.00	101.44	2.76	2.76	23.52	128.98
441	44.10	101.53	2.89	2.89	24.20	129.35
442	44.20	100.88	3.08	3.08	25.04	129.80
443	44.30	101.07	3.31	3.31	25.60	130.34
444	44.40	105.84	3.56	3.56	25.19	130.82
445	44.50	114.38	3.60	3.60	23.43	131.03
446	44.60	125.14	3.36	3.36	21.00	130.85
447	44.70	133.34	3.05	3.05	18.93	130.50
448	44.80	136.80	2.95	2.95	17.89	130.30
449	44.90	137.37	3.02	3.02	17.87	130.45
450	45.00	137.80	3.21	3.21	18.29	130.81
451	45.10	138.89	3.39	3.39	18.74	131.12
452	45.20	137.86	3.43	3.43	19.20	131.27
453	45.30	134.20	3.44	3.44	19.88	131.28
454	45.40	128.98	3.49	3.49	20.73	131.24
455	45.50	124.75	3.49	3.49	21.28	131.19
456	45.60	125.46	3.43	3.43	20.92	131.05
457	45.70	131.26	3.28	3.28	19.62	130.76
458	45.80	137.15	2.99	2.99	17.90	130.28
459	45.90	141.54	2.70	2.70	16.40	129.72
460	46.00	143.88	2.54	2.54	15.77	129.41
461	46.10	141.25	2.62	2.62	16.14	129.51
462	46.20	137.40	2.83	2.83	17.18	129.88
463	46.30	134.84	3.01	3.01	18.18	130.20
464	46.40	132.71	3.07	3.07	18.73	130.33
465	46.50	131.99	3.03	3.03	19.03	130.46
466	46.60	133.65	3.19	3.19	19.44	130.84
467	46.70	135.55	3.53	3.53	20.21	131.43
468	46.80	134.44	3.82	3.82	21.45	131.94
469	46.90	128.23	4.01	4.01	23.19	132.07
470	47.00	114.82	3.93	3.93	25.35	131.89
471	47.10	104.67	3.86	3.86	27.57	131.34
472	47.20	94.36	3.54	3.54	28.61	130.88
473	47.30	97.16	3.45	3.45	28.21	130.61
474	47.40	103.73	3.47	3.47	28.21	130.33
475	47.50	89.80	3.20	3.20	30.20	129.72
476	47.60	71.11	2.93	2.93	35.19	128.31
477	47.70	51.94	2.39	2.39	41.72	126.51
478	47.80	40.84	1.95	1.95	47.70	124.59
479	47.90	36.45	1.71	1.71	50.92	123.14
480	48.00	34.41	1.55	1.55	51.49	122.40

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
481	48.10	35.44	1.53	1.53	51.65	122.39
482	48.20	36.19	1.71	1.71	52.29	123.32
483	48.30	38.22	2.13	2.13	52.94	124.99
484	48.40	44.04	2.74	2.74	52.16	126.60
485	48.50	49.23	3.06	3.06	50.93	127.37
486	48.60	47.66	2.81	2.81	50.58	127.15
487	48.70	43.48	2.49	2.49	51.65	126.17
488	48.80	39.06	2.20	2.20	53.10	125.19
489	48.90	37.33	2.04	2.04	53.87	124.49
490	49.00	37.43	1.98	1.98	53.93	124.06
491	49.10	36.47	1.89	1.89	53.95	123.74
492	49.20	35.54	1.82	1.82	54.37	123.35
493	49.30	34.39	1.74	1.74	55.43	122.76
494	49.40	31.21	1.56	1.56	57.95	121.65
495	49.50	25.43	1.25	1.25	61.87	120.04
496	49.60	21.54	1.03	1.03	66.07	118.32
497	49.70	19.93	0.92	0.92	68.60	117.09
498	49.80	19.14	0.85	0.85	69.49	116.50

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q _c :	Measured cone resistance (tsf)
f _s :	Sleeve friction resistance (tsf)
u:	Pore pressure (tsf)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (pcf)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1	0.10	0.01	0.00	0.01	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
2	0.20	0.01	0.00	0.01	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
3	0.30	0.02	0.00	0.02	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
4	0.40	0.02	0.00	0.02	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
5	0.50	0.03	0.00	0.03	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
6	0.60	0.04	0.00	0.04	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
7	0.70	0.04	0.00	0.04	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
8	0.80	0.05	0.00	0.05	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
9	0.90	0.05	0.00	0.05	1.00	0.481	1.06	0.455	1.00	1.30	2.000	Yes
10	1.00	0.06	0.00	0.06	1.00	0.481	1.06	0.455	1.00	1.30	2.000	Yes
11	1.10	0.07	0.00	0.07	1.00	0.481	1.06	0.455	1.00	1.30	2.000	Yes
12	1.20	0.07	0.00	0.07	1.00	0.481	1.06	0.455	1.00	1.30	2.000	Yes
13	1.30	0.08	0.00	0.08	1.00	0.480	1.06	0.455	1.00	1.30	2.000	Yes
14	1.40	0.08	0.00	0.08	1.00	0.480	1.06	0.455	1.00	1.30	2.000	Yes
15	1.50	0.09	0.00	0.09	1.00	0.480	1.06	0.455	1.00	1.30	2.000	Yes
16	1.60	0.10	0.00	0.10	1.00	0.480	1.06	0.455	1.00	1.30	2.000	Yes
17	1.70	0.10	0.00	0.10	1.00	0.480	1.06	0.454	1.00	1.30	2.000	Yes
18	1.80	0.11	0.00	0.11	1.00	0.480	1.06	0.454	1.00	1.30	2.000	Yes
19	1.90	0.11	0.00	0.11	1.00	0.480	1.06	0.454	1.00	1.30	2.000	Yes
20	2.00	0.12	0.00	0.12	1.00	0.480	1.06	0.454	1.00	1.30	2.000	Yes
21	2.10	0.13	0.00	0.13	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
22	2.20	0.13	0.00	0.13	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
23	2.30	0.14	0.00	0.14	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
24	2.40	0.14	0.00	0.14	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
25	2.50	0.15	0.00	0.15	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
26	2.60	0.16	0.00	0.16	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
27	2.70	0.16	0.00	0.16	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
28	2.80	0.17	0.00	0.17	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
29	2.90	0.17	0.00	0.17	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
30	3.00	0.18	0.00	0.18	0.99	0.479	1.06	0.453	1.00	1.30	2.000	No
31	3.10	0.19	0.00	0.19	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
32	3.20	0.19	0.00	0.19	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
33	3.30	0.20	0.00	0.20	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
34	3.40	0.20	0.00	0.20	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
35	3.50	0.21	0.00	0.21	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
36	3.60	0.22	0.00	0.22	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
37	3.70	0.22	0.00	0.22	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
38	3.80	0.23	0.00	0.23	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
39	3.90	0.24	0.00	0.24	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
40	4.00	0.24	0.00	0.24	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
41	4.10	0.25	0.00	0.25	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
42	4.20	0.26	0.00	0.26	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
43	4.30	0.26	0.00	0.26	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
44	4.40	0.27	0.00	0.27	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
45	4.50	0.27	0.00	0.27	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
46	4.60	0.28	0.00	0.28	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
47	4.70	0.29	0.00	0.29	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
48	4.80	0.29	0.00	0.29	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
49	4.90	0.30	0.00	0.30	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
50	5.00	0.31	0.00	0.31	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
51	5.10	0.31	0.00	0.31	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
52	5.20	0.32	0.00	0.32	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
53	5.30	0.33	0.00	0.33	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
54	5.40	0.33	0.00	0.33	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
55	5.50	0.34	0.00	0.34	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
56	5.60	0.35	0.00	0.35	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
57	5.70	0.35	0.00	0.35	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
58	5.80	0.36	0.00	0.36	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
59	5.90	0.37	0.00	0.37	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
60	6.00	0.37	0.00	0.37	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
61	6.10	0.38	0.00	0.38	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
62	6.20	0.39	0.00	0.39	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
63	6.30	0.39	0.00	0.39	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
64	6.40	0.40	0.00	0.40	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
65	6.50	0.41	0.00	0.41	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
66	6.60	0.41	0.00	0.41	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
67	6.70	0.42	0.00	0.42	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
68	6.80	0.43	0.00	0.43	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
69	6.90	0.43	0.00	0.43	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
70	7.00	0.44	0.00	0.44	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
71	7.10	0.45	0.00	0.45	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
72	7.20	0.45	0.00	0.45	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
73	7.30	0.46	0.00	0.46	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
74	7.40	0.46	0.00	0.46	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
75	7.50	0.47	0.00	0.47	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
76	7.60	0.48	0.00	0.48	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
77	7.70	0.48	0.00	0.48	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
78	7.80	0.49	0.00	0.49	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
79	7.90	0.50	0.00	0.50	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
80	8.00	0.50	0.00	0.50	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
81	8.10	0.51	0.00	0.51	0.98	0.476	1.06	0.450	1.00	1.30	2.000	Yes
82	8.20	0.52	0.01	0.51	0.98	0.479	1.06	0.453	1.00	1.30	2.000	Yes
83	8.30	0.52	0.01	0.51	0.98	0.481	1.06	0.456	1.00	1.30	2.000	Yes
84	8.40	0.53	0.01	0.51	0.98	0.484	1.06	0.458	1.00	1.30	2.000	Yes
85	8.50	0.53	0.02	0.52	0.98	0.487	1.06	0.461	1.00	1.30	2.000	Yes
86	8.60	0.54	0.02	0.52	0.98	0.489	1.06	0.463	1.00	1.30	2.000	Yes
87	8.70	0.55	0.02	0.52	0.98	0.492	1.06	0.466	1.00	1.30	2.000	Yes
88	8.80	0.55	0.02	0.53	0.98	0.495	1.06	0.468	1.00	1.30	2.000	Yes
89	8.90	0.56	0.03	0.53	0.98	0.497	1.06	0.471	1.00	1.30	2.000	Yes
90	9.00	0.56	0.03	0.53	0.98	0.500	1.06	0.473	1.00	1.30	2.000	Yes
91	9.10	0.57	0.03	0.53	0.98	0.502	1.06	0.475	1.00	1.30	0.618	No
92	9.20	0.57	0.04	0.54	0.98	0.505	1.06	0.478	1.00	1.30	0.621	No
93	9.30	0.58	0.04	0.54	0.98	0.507	1.06	0.480	1.00	1.30	0.624	No
94	9.40	0.59	0.04	0.54	0.98	0.510	1.06	0.482	1.00	1.30	0.627	No
95	9.50	0.59	0.05	0.55	0.98	0.512	1.06	0.485	1.00	1.30	0.630	No
96	9.60	0.60	0.05	0.55	0.98	0.514	1.06	0.487	1.00	1.30	0.633	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
97	9.70	0.60	0.05	0.55	0.98	0.517	1.06	0.489	1.00	1.30	0.636	No
98	9.80	0.61	0.06	0.55	0.98	0.519	1.06	0.491	1.00	1.30	0.639	No
99	9.90	0.61	0.06	0.56	0.98	0.521	1.06	0.494	1.00	1.30	0.642	No
100	10.00	0.62	0.06	0.56	0.98	0.524	1.06	0.496	1.00	1.30	0.644	No
101	10.10	0.63	0.07	0.56	0.98	0.526	1.06	0.498	1.00	1.30	0.647	No
102	10.20	0.63	0.07	0.56	0.98	0.528	1.06	0.500	1.00	1.30	0.650	No
103	10.30	0.64	0.07	0.57	0.98	0.530	1.06	0.502	1.00	1.30	0.653	No
104	10.40	0.64	0.07	0.57	0.98	0.533	1.06	0.504	1.00	1.30	0.655	No
105	10.50	0.65	0.08	0.57	0.98	0.535	1.06	0.506	1.00	1.30	0.658	No
106	10.60	0.66	0.08	0.57	0.98	0.537	1.06	0.508	1.00	1.30	0.661	No
107	10.70	0.66	0.08	0.58	0.98	0.539	1.06	0.510	1.00	1.30	0.663	No
108	10.80	0.67	0.09	0.58	0.98	0.541	1.06	0.512	1.00	1.30	0.666	No
109	10.90	0.67	0.09	0.58	0.98	0.543	1.06	0.514	1.00	1.30	0.668	No
110	11.00	0.68	0.09	0.58	0.98	0.545	1.06	0.516	1.00	1.30	2.000	Yes
111	11.10	0.68	0.10	0.59	0.98	0.547	1.06	0.518	1.00	1.30	2.000	Yes
112	11.20	0.69	0.10	0.59	0.98	0.549	1.06	0.520	1.00	1.30	2.000	Yes
113	11.30	0.70	0.10	0.59	0.98	0.551	1.06	0.522	1.00	1.30	2.000	Yes
114	11.40	0.70	0.11	0.60	0.98	0.553	1.06	0.524	1.00	1.30	2.000	Yes
115	11.50	0.71	0.11	0.60	0.98	0.555	1.06	0.526	1.00	1.30	2.000	Yes
116	11.60	0.71	0.11	0.60	0.98	0.557	1.06	0.527	1.00	1.30	2.000	Yes
117	11.70	0.72	0.12	0.60	0.98	0.559	1.06	0.529	1.00	1.30	2.000	Yes
118	11.80	0.72	0.12	0.61	0.98	0.561	1.06	0.531	1.00	1.30	2.000	Yes
119	11.90	0.73	0.12	0.61	0.98	0.563	1.06	0.533	1.00	1.30	0.693	No
120	12.00	0.73	0.12	0.61	0.97	0.565	1.06	0.535	1.00	1.30	0.695	No
121	12.10	0.74	0.13	0.61	0.97	0.567	1.06	0.537	1.00	1.30	0.698	No
122	12.20	0.75	0.13	0.61	0.97	0.569	1.06	0.538	1.00	1.30	0.700	No
123	12.30	0.75	0.13	0.62	0.97	0.571	1.06	0.540	1.00	1.30	0.702	No
124	12.40	0.76	0.14	0.62	0.97	0.572	1.06	0.542	1.00	1.30	0.704	No
125	12.50	0.76	0.14	0.62	0.97	0.574	1.06	0.543	1.00	1.30	0.707	No
126	12.60	0.77	0.14	0.62	0.97	0.576	1.06	0.545	1.00	1.30	0.709	No
127	12.70	0.77	0.15	0.63	0.97	0.578	1.06	0.547	1.00	1.30	0.711	No
128	12.80	0.78	0.15	0.63	0.97	0.579	1.06	0.548	1.00	1.30	0.713	No
129	12.90	0.79	0.15	0.63	0.97	0.581	1.06	0.550	1.00	1.30	0.715	No
130	13.00	0.79	0.16	0.64	0.97	0.583	1.06	0.552	1.00	1.30	0.717	No
131	13.10	0.80	0.16	0.64	0.97	0.585	1.06	0.553	1.00	1.30	0.719	No
132	13.20	0.80	0.16	0.64	0.97	0.586	1.06	0.555	1.00	1.30	0.721	No
133	13.30	0.81	0.17	0.64	0.97	0.588	1.06	0.557	1.00	1.30	0.724	No
134	13.40	0.81	0.17	0.64	0.97	0.590	1.06	0.558	1.00	1.30	0.726	No
135	13.50	0.82	0.17	0.65	0.97	0.591	1.06	0.560	1.00	1.30	0.728	No
136	13.60	0.82	0.17	0.65	0.97	0.593	1.06	0.561	1.00	1.30	0.730	No
137	13.70	0.83	0.18	0.65	0.97	0.595	1.06	0.563	1.00	1.30	0.732	No
138	13.80	0.83	0.18	0.65	0.97	0.596	1.06	0.565	1.00	1.30	0.734	No
139	13.90	0.84	0.18	0.66	0.97	0.598	1.06	0.566	1.00	1.30	0.736	No
140	14.00	0.85	0.19	0.66	0.97	0.600	1.06	0.568	1.00	1.30	0.738	No
141	14.10	0.85	0.19	0.66	0.97	0.601	1.06	0.569	1.00	1.30	0.740	No
142	14.20	0.86	0.19	0.66	0.97	0.603	1.06	0.571	1.00	1.30	0.742	No
143	14.30	0.86	0.20	0.66	0.97	0.605	1.06	0.572	1.00	1.30	0.744	No
144	14.40	0.87	0.20	0.67	0.97	0.606	1.06	0.574	1.00	1.30	0.746	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
145	14.50	0.87	0.20	0.67	0.97	0.608	1.06	0.575	1.00	1.30	0.748	No
146	14.60	0.88	0.21	0.67	0.97	0.609	1.06	0.577	1.00	1.30	0.750	No
147	14.70	0.88	0.21	0.67	0.97	0.611	1.06	0.578	1.00	1.30	0.752	No
148	14.80	0.89	0.21	0.68	0.97	0.613	1.06	0.580	1.00	1.30	0.754	No
149	14.90	0.89	0.22	0.68	0.97	0.614	1.06	0.581	1.00	1.30	0.756	No
150	15.00	0.90	0.22	0.68	0.97	0.616	1.06	0.583	1.00	1.30	0.758	No
151	15.10	0.90	0.22	0.68	0.97	0.617	1.06	0.584	1.00	1.30	0.759	No
152	15.20	0.91	0.22	0.68	0.97	0.619	1.06	0.586	1.00	1.30	0.761	No
153	15.30	0.91	0.23	0.69	0.97	0.620	1.06	0.587	1.00	1.30	0.763	No
154	15.40	0.92	0.23	0.69	0.97	0.622	1.06	0.588	1.00	1.30	0.765	No
155	15.50	0.92	0.23	0.69	0.97	0.623	1.06	0.590	1.00	1.30	0.767	No
156	15.60	0.93	0.24	0.69	0.97	0.625	1.06	0.591	1.00	1.30	0.769	No
157	15.70	0.93	0.24	0.69	0.97	0.626	1.06	0.593	1.00	1.30	0.770	No
158	15.80	0.94	0.24	0.70	0.97	0.627	1.06	0.594	1.00	1.30	0.772	No
159	15.90	0.95	0.25	0.70	0.97	0.629	1.06	0.595	1.00	1.30	0.774	No
160	16.00	0.95	0.25	0.70	0.97	0.630	1.06	0.597	1.00	1.30	0.776	No
161	16.10	0.96	0.25	0.70	0.97	0.632	1.06	0.598	1.00	1.30	0.777	No
162	16.20	0.96	0.26	0.71	0.97	0.633	1.06	0.599	1.00	1.30	0.779	No
163	16.30	0.97	0.26	0.71	0.97	0.634	1.06	0.600	1.00	1.30	0.781	No
164	16.40	0.97	0.26	0.71	0.97	0.636	1.06	0.602	1.00	1.30	0.782	No
165	16.50	0.98	0.27	0.71	0.97	0.637	1.06	0.603	1.00	1.30	0.784	No
166	16.60	0.98	0.27	0.71	0.97	0.638	1.06	0.604	1.00	1.30	0.786	No
167	16.70	0.99	0.27	0.72	0.96	0.640	1.06	0.606	1.00	1.30	0.787	No
168	16.80	0.99	0.27	0.72	0.96	0.641	1.06	0.607	1.00	1.30	0.789	No
169	16.90	1.00	0.28	0.72	0.96	0.642	1.06	0.608	1.00	1.30	0.791	No
170	17.00	1.00	0.28	0.72	0.96	0.644	1.06	0.609	1.00	1.30	0.792	No
171	17.10	1.01	0.28	0.73	0.96	0.645	1.06	0.611	1.00	1.30	0.794	No
172	17.20	1.01	0.29	0.73	0.96	0.646	1.06	0.612	1.00	1.30	0.796	No
173	17.30	1.02	0.29	0.73	0.96	0.648	1.06	0.613	1.00	1.30	0.797	No
174	17.40	1.02	0.29	0.73	0.96	0.649	1.06	0.615	1.00	1.30	0.799	No
175	17.50	1.03	0.30	0.73	0.96	0.651	1.06	0.616	1.00	1.30	0.801	No
176	17.60	1.03	0.30	0.73	0.96	0.652	1.06	0.617	1.00	1.30	0.802	No
177	17.70	1.04	0.30	0.74	0.96	0.653	1.06	0.618	1.00	1.30	0.804	No
178	17.80	1.04	0.31	0.74	0.96	0.654	1.06	0.619	1.00	1.30	0.805	No
179	17.90	1.05	0.31	0.74	0.96	0.656	1.06	0.621	1.00	1.30	0.807	No
180	18.00	1.06	0.31	0.74	0.96	0.657	1.06	0.622	1.00	1.30	0.808	No
181	18.10	1.06	0.32	0.75	0.96	0.658	1.06	0.623	1.00	1.30	0.810	No
182	18.20	1.07	0.32	0.75	0.96	0.659	1.06	0.624	1.00	1.30	0.811	No
183	18.30	1.07	0.32	0.75	0.96	0.660	1.06	0.625	1.00	1.30	0.812	No
184	18.40	1.08	0.32	0.75	0.96	0.661	1.06	0.626	1.00	1.30	0.814	No
185	18.50	1.08	0.33	0.76	0.96	0.662	1.06	0.627	1.00	1.30	2.000	Yes
186	18.60	1.09	0.33	0.76	0.96	0.663	1.06	0.628	1.00	1.30	2.000	Yes
187	18.70	1.10	0.33	0.76	0.96	0.664	1.06	0.629	1.00	1.30	2.000	Yes
188	18.80	1.10	0.34	0.76	0.96	0.665	1.06	0.630	1.00	1.30	2.000	Yes
189	18.90	1.11	0.34	0.77	0.96	0.666	1.06	0.631	1.00	1.30	2.000	Yes
190	19.00	1.11	0.34	0.77	0.96	0.667	1.06	0.631	1.00	1.30	2.000	Yes
191	19.10	1.12	0.35	0.77	0.96	0.668	1.06	0.632	1.00	1.30	2.000	Yes
192	19.20	1.13	0.35	0.78	0.96	0.669	1.06	0.633	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
193	19.30	1.13	0.35	0.78	0.96	0.670	1.06	0.634	1.00	1.30	2.000	Yes
194	19.40	1.14	0.36	0.78	0.96	0.671	1.06	0.635	1.00	1.30	2.000	Yes
195	19.50	1.14	0.36	0.79	0.96	0.671	1.06	0.636	1.00	1.30	2.000	Yes
196	19.60	1.15	0.36	0.79	0.96	0.672	1.06	0.636	1.00	1.30	2.000	Yes
197	19.70	1.16	0.37	0.79	0.96	0.673	1.06	0.637	1.00	1.30	2.000	Yes
198	19.80	1.16	0.37	0.79	0.96	0.674	1.06	0.638	1.00	1.30	2.000	Yes
199	19.90	1.17	0.37	0.80	0.96	0.675	1.06	0.639	1.00	1.30	2.000	Yes
200	20.00	1.18	0.37	0.80	0.96	0.675	1.06	0.639	1.00	1.30	2.000	Yes
201	20.10	1.18	0.38	0.80	0.96	0.676	1.06	0.640	1.00	1.30	2.000	Yes
202	20.20	1.19	0.38	0.81	0.96	0.677	1.06	0.641	1.00	1.30	2.000	Yes
203	20.30	1.19	0.38	0.81	0.96	0.678	1.06	0.642	1.00	1.30	2.000	Yes
204	20.40	1.20	0.39	0.81	0.96	0.679	1.06	0.643	1.00	1.30	2.000	Yes
205	20.50	1.20	0.39	0.81	0.96	0.680	1.06	0.643	1.00	1.30	0.836	No
206	20.60	1.21	0.39	0.82	0.96	0.681	1.06	0.644	1.00	1.30	0.838	No
207	20.70	1.22	0.40	0.82	0.96	0.682	1.06	0.645	1.00	1.30	0.839	No
208	20.80	1.22	0.40	0.82	0.95	0.683	1.06	0.646	1.00	1.30	0.840	No
209	20.90	1.23	0.40	0.82	0.95	0.684	1.06	0.647	1.00	1.30	0.841	No
210	21.00	1.23	0.41	0.83	0.95	0.684	1.06	0.648	1.00	1.30	0.842	No
211	21.10	1.24	0.41	0.83	0.95	0.685	1.06	0.649	1.00	1.30	0.844	No
212	21.20	1.24	0.41	0.83	0.95	0.686	1.06	0.650	1.00	1.30	0.845	No
213	21.30	1.25	0.41	0.83	0.95	0.687	1.06	0.651	1.00	1.30	0.846	No
214	21.40	1.25	0.42	0.83	0.95	0.688	1.06	0.652	1.00	1.30	0.847	No
215	21.50	1.26	0.42	0.84	0.95	0.689	1.06	0.652	1.00	1.30	0.848	No
216	21.60	1.26	0.42	0.84	0.95	0.690	1.06	0.653	1.00	1.30	0.849	No
217	21.70	1.27	0.43	0.84	0.95	0.691	1.06	0.654	1.00	1.30	0.850	No
218	21.80	1.27	0.43	0.84	0.95	0.692	1.06	0.655	1.00	1.30	0.851	No
219	21.90	1.28	0.43	0.85	0.95	0.692	1.06	0.656	1.00	1.30	0.852	No
220	22.00	1.29	0.44	0.85	0.95	0.693	1.06	0.656	1.00	1.30	0.853	No
221	22.10	1.29	0.44	0.85	0.95	0.694	1.06	0.657	1.00	1.30	0.854	No
222	22.20	1.30	0.44	0.85	0.95	0.695	1.06	0.658	1.00	1.30	0.855	No
223	22.30	1.30	0.45	0.86	0.95	0.695	1.06	0.658	1.00	1.30	0.856	No
224	22.40	1.31	0.45	0.86	0.95	0.696	1.06	0.659	1.00	1.30	0.857	No
225	22.50	1.31	0.45	0.86	0.95	0.697	1.06	0.660	1.00	1.30	0.857	No
226	22.60	1.32	0.46	0.86	0.95	0.697	1.06	0.660	1.00	1.30	0.858	No
227	22.70	1.33	0.46	0.87	0.95	0.698	1.06	0.661	1.00	1.30	0.859	No
228	22.80	1.33	0.46	0.87	0.95	0.699	1.06	0.661	1.00	1.30	0.860	No
229	22.90	1.34	0.46	0.87	0.95	0.699	1.06	0.662	1.00	1.30	0.861	No
230	23.00	1.34	0.47	0.88	0.95	0.700	1.06	0.663	1.00	1.30	0.861	No
231	23.10	1.35	0.47	0.88	0.95	0.701	1.06	0.663	1.00	1.30	0.862	No
232	23.20	1.36	0.47	0.88	0.95	0.701	1.06	0.664	1.00	1.30	0.863	No
233	23.30	1.36	0.48	0.88	0.95	0.702	1.06	0.664	1.00	1.30	0.864	No
234	23.40	1.37	0.48	0.89	0.95	0.702	1.06	0.665	1.00	1.30	0.864	No
235	23.50	1.37	0.48	0.89	0.95	0.703	1.06	0.665	1.00	1.30	0.865	No
236	23.60	1.38	0.49	0.89	0.95	0.704	1.06	0.666	1.00	1.30	0.866	No
237	23.70	1.38	0.49	0.90	0.95	0.704	1.06	0.667	1.00	1.30	0.867	No
238	23.80	1.39	0.49	0.90	0.95	0.705	1.06	0.667	1.00	1.30	0.867	No
239	23.90	1.40	0.50	0.90	0.95	0.705	1.06	0.668	1.00	1.30	0.868	No
240	24.00	1.40	0.50	0.90	0.95	0.706	1.06	0.668	1.00	1.30	0.869	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
241	24.10	1.41	0.50	0.91	0.94	0.707	1.06	0.669	1.00	1.30	0.870	No
242	24.20	1.41	0.51	0.91	0.94	0.707	1.06	0.670	1.00	1.30	0.871	No
243	24.30	1.42	0.51	0.91	0.94	0.708	1.06	0.670	1.00	1.30	0.871	No
244	24.40	1.42	0.51	0.91	0.94	0.709	1.06	0.671	1.00	1.30	0.872	No
245	24.50	1.43	0.51	0.91	0.94	0.709	1.06	0.672	1.00	1.30	0.873	No
246	24.60	1.43	0.52	0.92	0.94	0.710	1.06	0.672	1.00	1.30	0.874	No
247	24.70	1.44	0.52	0.92	0.94	0.711	1.06	0.673	1.00	1.30	0.875	No
248	24.80	1.45	0.52	0.92	0.94	0.711	1.06	0.673	1.00	1.30	0.875	No
249	24.90	1.45	0.53	0.92	0.94	0.712	1.06	0.674	1.00	1.30	0.876	No
250	25.00	1.46	0.53	0.93	0.94	0.713	1.06	0.675	1.00	1.30	0.877	No
251	25.10	1.46	0.53	0.93	0.94	0.713	1.06	0.675	1.00	1.30	0.878	No
252	25.20	1.47	0.54	0.93	0.94	0.714	1.06	0.676	1.00	1.30	0.879	No
253	25.30	1.47	0.54	0.93	0.94	0.715	1.06	0.677	1.00	1.30	0.880	No
254	25.40	1.48	0.54	0.93	0.94	0.715	1.06	0.677	1.00	1.30	0.880	No
255	25.50	1.48	0.55	0.94	0.94	0.716	1.06	0.678	1.00	1.30	0.881	No
256	25.60	1.49	0.55	0.94	0.94	0.716	1.06	0.678	1.00	1.30	0.882	No
257	25.70	1.49	0.55	0.94	0.94	0.717	1.06	0.679	1.00	1.30	0.882	No
258	25.80	1.50	0.56	0.94	0.94	0.718	1.06	0.679	1.00	1.30	0.883	No
259	25.90	1.50	0.56	0.95	0.94	0.718	1.06	0.680	1.00	1.30	0.884	No
260	26.00	1.51	0.56	0.95	0.94	0.719	1.06	0.680	1.00	1.30	0.884	No
261	26.10	1.51	0.56	0.95	0.94	0.719	1.06	0.681	1.00	1.30	0.885	No
262	26.20	1.52	0.57	0.95	0.94	0.720	1.06	0.681	1.00	1.30	0.886	No
263	26.30	1.53	0.57	0.95	0.94	0.720	1.06	0.682	1.00	1.30	0.886	No
264	26.40	1.53	0.57	0.96	0.94	0.721	1.06	0.682	1.00	1.30	0.887	No
265	26.50	1.54	0.58	0.96	0.94	0.721	1.06	0.683	1.00	1.30	0.887	No
266	26.60	1.54	0.58	0.96	0.94	0.722	1.06	0.683	1.00	1.30	0.888	No
267	26.70	1.55	0.58	0.96	0.94	0.722	1.06	0.683	1.00	1.30	0.888	No
268	26.80	1.55	0.59	0.97	0.94	0.722	1.06	0.684	1.00	1.30	0.889	No
269	26.90	1.56	0.59	0.97	0.93	0.723	1.06	0.684	1.00	1.30	0.890	No
270	27.00	1.57	0.59	0.97	0.93	0.723	1.06	0.685	1.00	1.30	0.890	No
271	27.10	1.57	0.60	0.98	0.93	0.724	1.06	0.685	1.00	1.30	0.891	No
272	27.20	1.58	0.60	0.98	0.93	0.724	1.06	0.685	1.00	1.30	0.891	No
273	27.30	1.58	0.60	0.98	0.93	0.724	1.06	0.686	1.00	1.30	0.891	No
274	27.40	1.59	0.61	0.98	0.93	0.725	1.06	0.686	1.00	1.30	0.892	No
275	27.50	1.59	0.61	0.99	0.93	0.725	1.06	0.687	1.00	1.30	0.892	No
276	27.60	1.60	0.61	0.99	0.93	0.726	1.06	0.687	1.00	1.30	0.893	No
277	27.70	1.60	0.61	0.99	0.93	0.726	1.06	0.687	1.00	1.30	0.893	No
278	27.80	1.61	0.62	0.99	0.93	0.726	1.06	0.688	1.00	1.30	0.894	No
279	27.90	1.62	0.62	0.99	0.93	0.727	1.06	0.688	1.00	1.30	0.895	No
280	28.00	1.62	0.62	1.00	0.93	0.727	1.06	0.688	1.00	1.30	0.895	No
281	28.10	1.63	0.63	1.00	0.93	0.728	1.06	0.689	1.00	1.30	0.895	No
282	28.20	1.63	0.63	1.00	0.93	0.728	1.06	0.689	1.00	1.30	0.896	No
283	28.30	1.64	0.63	1.00	0.93	0.728	1.06	0.690	1.00	1.30	0.896	No
284	28.40	1.64	0.64	1.01	0.93	0.729	1.06	0.690	1.00	1.30	0.897	No
285	28.50	1.65	0.64	1.01	0.93	0.729	1.06	0.690	1.00	1.30	0.897	No
286	28.60	1.65	0.64	1.01	0.93	0.729	1.06	0.690	1.00	1.30	0.898	No
287	28.70	1.66	0.65	1.01	0.93	0.730	1.06	0.691	1.00	1.30	0.898	No
288	28.80	1.67	0.65	1.02	0.93	0.730	1.06	0.691	1.00	1.30	0.898	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
289	28.90	1.67	0.65	1.02	0.93	0.730	1.06	0.691	1.00	1.30	0.899	No
290	29.00	1.68	0.66	1.02	0.93	0.731	1.06	0.692	1.00	1.30	0.899	No
291	29.10	1.68	0.66	1.02	0.92	0.731	1.06	0.692	1.00	1.30	0.899	No
292	29.20	1.69	0.66	1.03	0.92	0.731	1.06	0.692	1.00	1.30	0.900	No
293	29.30	1.69	0.66	1.03	0.92	0.731	1.06	0.692	1.00	1.30	0.900	No
294	29.40	1.70	0.67	1.03	0.92	0.732	1.06	0.693	1.00	1.30	0.900	No
295	29.50	1.71	0.67	1.03	0.92	0.732	1.06	0.693	1.00	1.30	0.901	No
296	29.60	1.71	0.67	1.04	0.92	0.732	1.06	0.693	1.00	1.30	0.901	No
297	29.70	1.72	0.68	1.04	0.92	0.733	1.06	0.693	1.00	1.30	0.901	No
298	29.80	1.72	0.68	1.04	0.92	0.733	1.06	0.694	1.00	1.30	0.902	No
299	29.90	1.73	0.68	1.04	0.92	0.733	1.06	0.694	1.00	1.30	0.902	No
300	30.00	1.73	0.69	1.05	0.92	0.733	1.06	0.694	1.00	1.30	0.902	No
301	30.10	1.74	0.69	1.05	0.92	0.733	1.06	0.694	1.00	1.30	0.903	No
302	30.20	1.74	0.69	1.05	0.92	0.734	1.06	0.694	1.00	1.30	0.903	No
303	30.30	1.75	0.70	1.05	0.92	0.734	1.06	0.695	1.00	1.30	0.903	No
304	30.40	1.76	0.70	1.06	0.92	0.734	1.06	0.695	1.00	1.30	0.903	No
305	30.50	1.76	0.70	1.06	0.92	0.734	1.06	0.695	1.00	1.30	0.904	No
306	30.60	1.77	0.71	1.06	0.92	0.734	1.06	0.695	1.00	1.30	0.904	No
307	30.70	1.77	0.71	1.06	0.92	0.735	1.06	0.695	1.00	1.30	0.904	No
308	30.80	1.78	0.71	1.07	0.92	0.735	1.06	0.696	1.00	1.30	0.904	No
309	30.90	1.78	0.71	1.07	0.92	0.735	1.06	0.696	1.00	1.30	0.904	No
310	31.00	1.79	0.72	1.07	0.92	0.735	1.06	0.696	1.00	1.30	2.000	Yes
311	31.10	1.80	0.72	1.08	0.91	0.735	1.06	0.696	1.00	1.30	2.000	Yes
312	31.20	1.80	0.72	1.08	0.91	0.735	1.06	0.696	1.00	1.30	2.000	Yes
313	31.30	1.81	0.73	1.08	0.91	0.735	1.06	0.696	1.00	1.30	2.000	Yes
314	31.40	1.81	0.73	1.08	0.91	0.735	1.06	0.696	1.00	1.30	2.000	Yes
315	31.50	1.82	0.73	1.09	0.91	0.735	1.06	0.696	1.00	1.30	0.905	No
316	31.60	1.83	0.74	1.09	0.91	0.735	1.06	0.696	1.00	1.30	0.905	No
317	31.70	1.83	0.74	1.09	0.91	0.735	1.06	0.696	1.00	1.30	0.905	No
318	31.80	1.84	0.74	1.10	0.91	0.735	1.06	0.696	1.00	1.30	0.905	No
319	31.90	1.84	0.75	1.10	0.91	0.735	1.06	0.696	1.00	1.30	0.904	No
320	32.00	1.85	0.75	1.10	0.91	0.735	1.06	0.696	1.00	1.30	0.904	No
321	32.10	1.86	0.75	1.10	0.91	0.735	1.06	0.696	1.00	1.30	0.904	No
322	32.20	1.86	0.76	1.11	0.91	0.735	1.06	0.696	1.00	1.30	0.904	No
323	32.30	1.87	0.76	1.11	0.91	0.735	1.06	0.696	1.00	1.30	0.904	No
324	32.40	1.88	0.76	1.11	0.91	0.735	1.06	0.696	1.00	1.30	2.000	Yes
325	32.50	1.88	0.76	1.12	0.91	0.735	1.06	0.696	1.00	1.30	2.000	Yes
326	32.60	1.89	0.77	1.12	0.91	0.735	1.06	0.695	1.00	1.30	2.000	Yes
327	32.70	1.89	0.77	1.12	0.91	0.735	1.06	0.695	1.00	1.30	2.000	Yes
328	32.80	1.90	0.77	1.13	0.90	0.735	1.06	0.695	1.00	1.30	2.000	Yes
329	32.90	1.91	0.78	1.13	0.90	0.734	1.06	0.695	1.00	1.30	2.000	Yes
330	33.00	1.91	0.78	1.13	0.90	0.734	1.06	0.695	1.00	1.30	0.904	No
331	33.10	1.92	0.78	1.13	0.90	0.734	1.06	0.695	1.00	1.30	0.904	No
332	33.20	1.92	0.79	1.14	0.90	0.735	1.06	0.695	1.00	1.30	0.904	No
333	33.30	1.93	0.79	1.14	0.90	0.735	1.06	0.695	1.00	1.30	0.904	No
334	33.40	1.93	0.79	1.14	0.90	0.735	1.06	0.695	1.00	1.30	0.904	No
335	33.50	1.94	0.80	1.14	0.90	0.735	1.06	0.695	1.00	1.30	0.904	No
336	33.60	1.94	0.80	1.15	0.90	0.735	1.06	0.695	1.00	1.30	0.904	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
337	33.70	1.95	0.80	1.15	0.90	0.735	1.06	0.695	1.00	1.30	0.904	No
338	33.80	1.96	0.80	1.15	0.90	0.735	1.06	0.695	1.00	1.30	0.904	No
339	33.90	1.96	0.81	1.15	0.90	0.735	1.06	0.695	1.00	1.30	0.904	No
340	34.00	1.97	0.81	1.16	0.90	0.735	1.06	0.695	1.00	1.30	0.904	No
341	34.10	1.97	0.81	1.16	0.90	0.735	1.06	0.695	1.00	1.30	0.904	No
342	34.20	1.98	0.82	1.16	0.90	0.735	1.06	0.695	1.00	1.30	0.904	No
343	34.30	1.98	0.82	1.16	0.90	0.734	1.06	0.695	1.00	1.30	0.904	No
344	34.40	1.99	0.82	1.17	0.89	0.734	1.06	0.695	1.00	1.30	0.904	No
345	34.50	2.00	0.83	1.17	0.89	0.734	1.06	0.695	1.00	1.30	2.000	Yes
346	34.60	2.00	0.83	1.17	0.89	0.734	1.06	0.695	1.00	1.30	2.000	Yes
347	34.70	2.01	0.83	1.18	0.89	0.734	1.06	0.695	1.00	1.30	2.000	Yes
348	34.80	2.01	0.84	1.18	0.89	0.733	1.06	0.694	1.00	1.30	2.000	Yes
349	34.90	2.02	0.84	1.18	0.89	0.733	1.06	0.694	1.00	1.30	2.000	Yes
350	35.00	2.03	0.84	1.19	0.89	0.733	1.06	0.694	1.00	1.30	2.000	Yes
351	35.10	2.03	0.85	1.19	0.89	0.733	1.06	0.694	1.00	1.30	2.000	Yes
352	35.20	2.04	0.85	1.19	0.89	0.732	1.06	0.693	1.00	1.30	2.000	Yes
353	35.30	2.05	0.85	1.20	0.89	0.732	1.06	0.693	1.00	1.30	2.000	Yes
354	35.40	2.05	0.85	1.20	0.89	0.732	1.06	0.693	1.00	1.30	2.000	Yes
355	35.50	2.06	0.86	1.20	0.89	0.731	1.06	0.692	1.00	1.30	0.900	No
356	35.60	2.07	0.86	1.21	0.89	0.731	1.06	0.692	1.00	1.30	0.900	No
357	35.70	2.07	0.86	1.21	0.89	0.731	1.06	0.692	1.00	1.30	0.899	No
358	35.80	2.08	0.87	1.21	0.88	0.730	1.06	0.691	1.00	1.30	2.000	Yes
359	35.90	2.09	0.87	1.22	0.88	0.730	1.06	0.691	1.00	1.30	2.000	Yes
360	36.00	2.09	0.87	1.22	0.88	0.730	1.06	0.691	1.00	1.30	2.000	Yes
361	36.10	2.10	0.88	1.22	0.88	0.729	1.06	0.690	1.00	1.30	2.000	Yes
362	36.20	2.11	0.88	1.23	0.88	0.729	1.06	0.690	1.00	1.30	2.000	Yes
363	36.30	2.11	0.88	1.23	0.88	0.728	1.06	0.690	1.00	1.30	2.000	Yes
364	36.40	2.12	0.89	1.23	0.88	0.728	1.06	0.689	1.00	1.30	2.000	Yes
365	36.50	2.12	0.89	1.24	0.88	0.728	1.06	0.689	1.00	1.30	2.000	Yes
366	36.60	2.13	0.89	1.24	0.88	0.727	1.06	0.689	1.00	1.30	2.000	Yes
367	36.70	2.14	0.90	1.24	0.88	0.727	1.06	0.688	1.00	1.30	2.000	Yes
368	36.80	2.14	0.90	1.25	0.88	0.727	1.06	0.688	1.00	1.30	2.000	Yes
369	36.90	2.15	0.90	1.25	0.88	0.726	1.06	0.687	1.00	1.30	2.000	Yes
370	37.00	2.16	0.90	1.25	0.88	0.726	1.06	0.687	1.00	1.30	0.893	No
371	37.10	2.16	0.91	1.26	0.88	0.725	1.06	0.686	1.00	1.30	0.892	No
372	37.20	2.17	0.91	1.26	0.87	0.725	1.06	0.686	1.00	1.30	0.892	No
373	37.30	2.18	0.91	1.26	0.87	0.724	1.06	0.686	1.00	1.30	0.891	No
374	37.40	2.18	0.92	1.27	0.87	0.724	1.06	0.685	1.00	1.30	0.891	No
375	37.50	2.19	0.92	1.27	0.87	0.723	1.06	0.685	1.00	1.30	0.890	No
376	37.60	2.20	0.92	1.27	0.87	0.723	1.06	0.684	1.00	1.30	0.889	No
377	37.70	2.20	0.93	1.28	0.87	0.722	1.06	0.684	1.00	1.30	0.889	No
378	37.80	2.21	0.93	1.28	0.87	0.722	1.06	0.683	1.00	1.30	0.888	No
379	37.90	2.22	0.93	1.28	0.87	0.721	1.06	0.683	1.00	1.30	0.888	No
380	38.00	2.22	0.94	1.29	0.87	0.721	1.06	0.682	1.00	1.30	0.887	No
381	38.10	2.23	0.94	1.29	0.87	0.720	1.06	0.682	1.00	1.30	0.887	No
382	38.20	2.24	0.94	1.30	0.87	0.720	1.06	0.681	1.00	1.30	0.886	No
383	38.30	2.24	0.95	1.30	0.87	0.719	1.06	0.681	1.00	1.30	0.885	No
384	38.40	2.25	0.95	1.30	0.86	0.719	1.06	0.680	1.00	1.30	0.885	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
385	38.50	2.26	0.95	1.31	0.86	0.718	1.06	0.680	1.00	1.30	0.884	No
386	38.60	2.26	0.95	1.31	0.86	0.718	1.06	0.679	1.00	1.30	0.883	No
387	38.70	2.27	0.96	1.31	0.86	0.717	1.06	0.679	1.00	1.30	0.883	No
388	38.80	2.28	0.96	1.32	0.86	0.717	1.06	0.678	1.00	1.30	0.882	No
389	38.90	2.28	0.96	1.32	0.86	0.716	1.06	0.678	1.00	1.30	0.881	No
390	39.00	2.29	0.97	1.32	0.86	0.715	1.06	0.677	1.00	1.30	0.881	No
391	39.10	2.30	0.97	1.33	0.86	0.715	1.06	0.677	1.00	1.30	0.880	No
392	39.20	2.31	0.97	1.33	0.86	0.714	1.06	0.676	1.00	1.30	0.879	No
393	39.30	2.31	0.98	1.34	0.86	0.714	1.06	0.676	1.00	1.30	0.878	No
394	39.40	2.32	0.98	1.34	0.86	0.713	1.06	0.675	1.00	1.30	0.878	No
395	39.50	2.33	0.98	1.34	0.86	0.713	1.06	0.675	1.00	1.30	0.877	No
396	39.60	2.33	0.99	1.35	0.85	0.712	1.06	0.674	1.00	1.30	0.876	No
397	39.70	2.34	0.99	1.35	0.85	0.711	1.06	0.674	1.00	1.30	0.876	No
398	39.80	2.35	0.99	1.35	0.85	0.711	1.06	0.673	1.00	1.30	0.875	No
399	39.90	2.35	1.00	1.36	0.85	0.710	1.06	0.672	1.00	1.30	0.874	No
400	40.00	2.36	1.00	1.36	0.85	0.710	1.06	0.672	1.00	1.30	0.873	No
401	40.10	2.37	1.00	1.36	0.85	0.709	1.06	0.671	1.00	1.30	0.873	No
402	40.20	2.37	1.00	1.37	0.85	0.708	1.06	0.671	1.00	1.30	0.872	No
403	40.30	2.38	1.01	1.37	0.85	0.708	1.06	0.670	1.00	1.30	0.871	No
404	40.40	2.39	1.01	1.38	0.85	0.707	1.06	0.669	1.00	1.30	0.870	No
405	40.50	2.39	1.01	1.38	0.85	0.707	1.06	0.669	1.00	1.30	0.869	No
406	40.60	2.40	1.02	1.38	0.85	0.706	1.06	0.668	1.00	1.30	0.869	No
407	40.70	2.41	1.02	1.39	0.84	0.705	1.06	0.668	1.00	1.30	0.868	No
408	40.80	2.41	1.02	1.39	0.84	0.705	1.06	0.667	1.00	1.30	0.867	No
409	40.90	2.42	1.03	1.39	0.84	0.704	1.06	0.666	1.00	1.30	0.866	No
410	41.00	2.43	1.03	1.40	0.84	0.703	1.06	0.666	1.00	1.30	0.865	No
411	41.10	2.43	1.03	1.40	0.84	0.703	1.06	0.665	1.00	1.30	0.865	No
412	41.20	2.44	1.04	1.41	0.84	0.702	1.06	0.664	1.00	1.30	0.864	No
413	41.30	2.45	1.04	1.41	0.84	0.701	1.06	0.664	1.00	1.30	0.863	No
414	41.40	2.46	1.04	1.41	0.84	0.701	1.06	0.663	1.00	1.30	0.862	No
415	41.50	2.46	1.05	1.42	0.84	0.700	1.06	0.663	1.00	1.30	0.861	No
416	41.60	2.47	1.05	1.42	0.84	0.699	1.06	0.662	1.00	1.30	0.861	No
417	41.70	2.48	1.05	1.42	0.84	0.699	1.06	0.661	1.00	1.30	0.860	No
418	41.80	2.48	1.05	1.43	0.83	0.698	1.06	0.661	1.00	1.30	0.859	No
419	41.90	2.49	1.06	1.43	0.83	0.697	1.06	0.660	1.00	1.30	0.858	No
420	42.00	2.50	1.06	1.44	0.83	0.697	1.06	0.659	1.00	1.30	0.857	No
421	42.10	2.50	1.06	1.44	0.83	0.696	1.06	0.659	1.00	1.30	0.857	No
422	42.20	2.51	1.07	1.44	0.83	0.695	1.06	0.658	1.00	1.30	0.856	No
423	42.30	2.52	1.07	1.45	0.83	0.695	1.06	0.658	1.00	1.30	0.855	No
424	42.40	2.52	1.07	1.45	0.83	0.694	1.06	0.657	1.00	1.30	0.854	No
425	42.50	2.53	1.08	1.45	0.83	0.693	1.06	0.656	1.00	1.30	0.853	No
426	42.60	2.54	1.08	1.46	0.83	0.693	1.06	0.656	1.00	1.30	0.853	No
427	42.70	2.54	1.08	1.46	0.83	0.692	1.06	0.655	1.00	1.30	0.852	No
428	42.80	2.55	1.09	1.46	0.83	0.692	1.06	0.655	1.00	1.30	0.851	No
429	42.90	2.55	1.09	1.47	0.82	0.691	1.06	0.654	1.00	1.30	2.000	Yes
430	43.00	2.56	1.09	1.47	0.82	0.690	1.06	0.654	1.00	1.30	2.000	Yes
431	43.10	2.57	1.10	1.47	0.82	0.690	1.06	0.653	1.00	1.30	2.000	Yes
432	43.20	2.57	1.10	1.48	0.82	0.689	1.06	0.652	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
433	43.30	2.58	1.10	1.48	0.82	0.688	1.06	0.652	1.00	1.30	2.000	Yes
434	43.40	2.59	1.10	1.48	0.82	0.688	1.06	0.651	1.00	1.30	0.846	No
435	43.50	2.59	1.11	1.49	0.82	0.687	1.06	0.651	1.00	1.30	0.846	No
436	43.60	2.60	1.11	1.49	0.82	0.687	1.06	0.650	1.00	1.30	0.845	No
437	43.70	2.61	1.11	1.49	0.82	0.686	1.06	0.649	1.00	1.30	0.844	No
438	43.80	2.61	1.12	1.50	0.82	0.685	1.06	0.649	1.00	1.30	0.843	No
439	43.90	2.62	1.12	1.50	0.81	0.685	1.06	0.648	1.00	1.30	0.842	No
440	44.00	2.63	1.12	1.50	0.81	0.684	1.06	0.647	1.00	1.30	0.842	No
441	44.10	2.63	1.13	1.51	0.81	0.683	1.06	0.647	1.00	1.30	0.841	No
442	44.20	2.64	1.13	1.51	0.81	0.683	1.06	0.646	1.00	1.30	0.840	No
443	44.30	2.64	1.13	1.51	0.81	0.682	1.06	0.646	1.00	1.30	0.839	No
444	44.40	2.65	1.14	1.52	0.81	0.681	1.06	0.645	1.00	1.30	0.838	No
445	44.50	2.66	1.14	1.52	0.81	0.681	1.06	0.644	1.00	1.30	0.837	No
446	44.60	2.66	1.14	1.52	0.81	0.680	1.06	0.644	1.00	1.30	0.837	No
447	44.70	2.67	1.15	1.53	0.81	0.679	1.06	0.643	1.00	1.30	0.836	No
448	44.80	2.68	1.15	1.53	0.81	0.678	1.06	0.642	1.00	1.30	0.835	No
449	44.90	2.68	1.15	1.53	0.80	0.678	1.06	0.642	1.00	1.30	0.834	No
450	45.00	2.69	1.15	1.54	0.80	0.677	1.06	0.641	1.00	1.30	0.833	No
451	45.10	2.70	1.16	1.54	0.80	0.676	1.06	0.640	1.00	1.30	0.832	No
452	45.20	2.70	1.16	1.54	0.80	0.676	1.06	0.640	1.00	1.30	0.831	No
453	45.30	2.71	1.16	1.55	0.80	0.675	1.06	0.639	1.00	1.30	0.831	No
454	45.40	2.72	1.17	1.55	0.80	0.674	1.06	0.638	1.00	1.30	0.830	No
455	45.50	2.72	1.17	1.55	0.80	0.673	1.06	0.638	1.00	1.30	0.829	No
456	45.60	2.73	1.17	1.56	0.80	0.673	1.06	0.637	1.00	1.30	0.828	No
457	45.70	2.74	1.18	1.56	0.80	0.672	1.06	0.636	1.00	1.30	0.827	No
458	45.80	2.74	1.18	1.56	0.80	0.671	1.06	0.635	1.00	1.30	0.826	No
459	45.90	2.75	1.18	1.57	0.79	0.671	1.06	0.635	1.00	1.30	0.825	No
460	46.00	2.76	1.19	1.57	0.79	0.670	1.06	0.634	1.00	1.30	0.824	No
461	46.10	2.76	1.19	1.57	0.79	0.669	1.06	0.633	1.00	1.30	0.824	No
462	46.20	2.77	1.19	1.58	0.79	0.668	1.06	0.633	1.00	1.30	0.823	No
463	46.30	2.78	1.19	1.58	0.79	0.668	1.06	0.632	1.00	1.30	0.822	No
464	46.40	2.78	1.20	1.58	0.79	0.667	1.06	0.631	1.00	1.30	0.821	No
465	46.50	2.79	1.20	1.59	0.79	0.666	1.06	0.631	1.00	1.30	0.820	No
466	46.60	2.79	1.20	1.59	0.79	0.666	1.06	0.630	1.00	1.30	0.819	No
467	46.70	2.80	1.21	1.59	0.79	0.665	1.06	0.629	1.00	1.30	2.000	Yes
468	46.80	2.81	1.21	1.60	0.79	0.664	1.06	0.629	1.00	1.30	2.000	Yes
469	46.90	2.81	1.21	1.60	0.78	0.663	1.06	0.628	1.00	1.30	2.000	Yes
470	47.00	2.82	1.22	1.60	0.78	0.663	1.06	0.627	1.00	1.30	2.000	Yes
471	47.10	2.83	1.22	1.61	0.78	0.662	1.06	0.627	1.00	1.30	2.000	Yes
472	47.20	2.83	1.22	1.61	0.78	0.661	1.06	0.626	1.00	1.30	0.814	No
473	47.30	2.84	1.23	1.61	0.78	0.660	1.06	0.625	1.00	1.30	0.813	No
474	47.40	2.85	1.23	1.62	0.78	0.660	1.06	0.624	1.00	1.30	0.812	No
475	47.50	2.85	1.23	1.62	0.78	0.659	1.06	0.624	1.00	1.30	0.811	No
476	47.60	2.86	1.24	1.62	0.78	0.658	1.06	0.623	1.00	1.30	0.810	No
477	47.70	2.87	1.24	1.63	0.78	0.657	1.06	0.622	1.00	1.30	0.809	No
478	47.80	2.87	1.24	1.63	0.78	0.657	1.06	0.622	1.00	1.30	0.808	No
479	47.90	2.88	1.24	1.63	0.77	0.656	1.06	0.621	1.00	1.30	0.807	No
480	48.00	2.89	1.25	1.64	0.77	0.655	1.06	0.620	1.00	1.30	0.807	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
481	48.10	2.89	1.25	1.64	0.77	0.655	1.06	0.620	1.00	1.30	0.806	No
482	48.20	2.90	1.25	1.64	0.77	0.654	1.06	0.619	1.00	1.30	0.805	No
483	48.30	2.90	1.26	1.65	0.77	0.653	1.06	0.618	1.00	1.30	0.804	No
484	48.40	2.91	1.26	1.65	0.77	0.653	1.06	0.618	1.00	1.30	0.803	No
485	48.50	2.92	1.26	1.65	0.77	0.652	1.06	0.617	1.00	1.30	0.802	No
486	48.60	2.92	1.27	1.66	0.77	0.651	1.06	0.616	1.00	1.30	0.801	No
487	48.70	2.93	1.27	1.66	0.77	0.650	1.06	0.616	1.00	1.30	0.800	No
488	48.80	2.94	1.27	1.66	0.76	0.650	1.06	0.615	1.00	1.30	0.800	No
489	48.90	2.94	1.28	1.67	0.76	0.649	1.06	0.614	1.00	1.30	0.799	No
490	49.00	2.95	1.28	1.67	0.76	0.648	1.06	0.614	1.00	1.30	0.798	No
491	49.10	2.95	1.28	1.67	0.76	0.648	1.06	0.613	1.00	1.30	0.797	No
492	49.20	2.96	1.29	1.67	0.76	0.647	1.06	0.612	1.00	1.30	0.796	No
493	49.30	2.97	1.29	1.68	0.76	0.646	1.06	0.612	1.00	1.30	0.795	No
494	49.40	2.97	1.29	1.68	0.76	0.646	1.06	0.611	1.00	1.30	0.794	No
495	49.50	2.98	1.29	1.68	0.76	0.645	1.06	0.610	1.00	1.30	0.794	No
496	49.60	2.98	1.30	1.69	0.76	0.644	1.06	0.610	1.00	1.30	0.793	No
497	49.70	2.99	1.30	1.69	0.76	0.644	1.06	0.609	1.00	1.30	0.792	No
498	49.80	3.00	1.30	1.69	0.75	0.643	1.06	0.609	1.00	1.30	0.791	No

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
 σ_v : Total overburden pressure at test point (tsf)
 u_0 : Water pressure at test point (tsf)
 σ_v' : Effective overburden pressure based on GWT during earthquake (tsf)
 r_d : Nonlinear shear mass factor
 CSR: Cyclic Stress Ratio
 MSF: Magnitude Scaling Factor
 CSR_{eq} : CSR adjusted for M=7.5
 K_σ : Effective overburden stress factor
 CSR*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::												
Point ID	Depth (ft)	q _p (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1	0.10	40.35	2.09	1.38	0.65	76.26	1.41	107.26	4.000	No	No	2.00
2	0.20	41.58	2.09	1.42	0.65	78.57	1.40	110.29	4.000	No	No	2.00
3	0.30	45.23	2.07	1.45	0.64	85.47	1.38	117.58	4.000	No	No	2.00
4	0.40	51.74	2.03	1.47	0.62	97.76	1.33	130.28	4.000	No	No	2.00
5	0.50	57.90	2.00	1.51	0.61	109.39	1.31	143.10	4.000	No	No	2.00
6	0.60	62.33	1.99	1.59	0.61	117.75	1.30	153.38	4.000	No	No	2.00
7	0.70	64.56	2.00	1.67	0.61	121.94	1.31	159.37	4.000	No	No	2.00
8	0.80	64.46	2.01	1.73	0.62	121.74	1.32	160.23	4.000	No	No	2.00
9	0.90	62.11	2.03	1.79	0.63	117.30	1.34	156.76	4.000	Yes	No	2.00
10	1.00	57.54	2.07	1.90	0.64	108.64	1.38	150.41	4.000	Yes	No	2.00
11	1.10	51.75	2.14	2.13	0.67	97.69	1.49	145.34	4.000	Yes	No	2.00
12	1.20	45.44	2.23	2.46	0.70	85.75	1.68	144.23	4.000	Yes	No	2.00
13	1.30	39.26	2.32	2.86	0.74	74.06	1.99	147.46	4.000	Yes	No	2.00
14	1.40	33.94	2.40	3.28	0.77	63.99	2.40	153.47	4.000	Yes	No	2.00
15	1.50	30.81	2.46	3.57	0.79	58.07	2.72	157.77	4.000	Yes	No	2.00
16	1.60	30.91	2.45	3.51	0.79	58.25	2.68	156.13	4.000	Yes	No	2.00
17	1.70	33.33	2.40	3.17	0.77	62.80	2.37	148.82	4.000	Yes	No	2.00
18	1.80	36.69	2.33	2.77	0.74	69.15	2.04	140.85	4.000	Yes	No	2.00
19	1.90	39.74	2.27	2.47	0.72	74.90	1.81	135.65	4.000	Yes	No	2.00
20	2.00	42.16	2.23	2.32	0.71	79.46	1.70	134.91	4.000	Yes	No	2.00
21	2.10	43.95	2.21	2.29	0.70	82.83	1.65	136.83	4.000	No	No	2.00
22	2.20	45.84	2.20	2.30	0.70	86.40	1.62	140.13	4.000	No	No	2.00
23	2.30	48.69	2.18	2.24	0.69	91.77	1.56	143.13	4.000	No	No	2.00
24	2.40	53.22	2.13	2.09	0.67	100.32	1.46	146.87	4.000	No	No	2.00
25	2.50	59.55	2.07	1.91	0.64	112.27	1.37	154.22	4.000	No	No	2.00
26	2.60	66.89	2.01	1.77	0.62	126.14	1.31	165.65	4.000	No	No	2.00
27	2.70	74.02	1.96	1.70	0.61	139.60	1.28	178.70	4.000	No	No	2.00
28	2.80	79.74	1.94	1.70	0.60	150.41	1.26	190.22	4.000	No	No	2.00
29	2.90	83.24	1.94	1.74	0.60	157.01	1.26	198.22	4.000	No	No	2.00
30	3.00	83.91	1.95	1.84	0.60	158.26	1.27	201.38	4.000	No	No	2.00
31	3.10	81.73	1.98	1.94	0.61	154.13	1.29	199.01	4.000	No	No	2.00
32	3.20	77.93	2.01	2.04	0.62	146.95	1.31	193.19	4.000	No	No	2.00
33	3.30	74.96	2.03	2.08	0.63	141.31	1.33	188.08	4.000	No	No	2.00
34	3.40	74.74	2.03	2.07	0.63	140.88	1.33	187.49	4.000	No	No	2.00
35	3.50	76.96	2.01	2.04	0.63	145.07	1.32	191.33	4.000	No	No	2.00
36	3.60	80.33	2.00	2.01	0.62	151.43	1.30	197.41	4.000	No	No	2.00
37	3.70	84.17	1.98	1.97	0.61	158.68	1.29	204.53	4.000	No	No	2.00
38	3.80	89.18	1.95	1.93	0.61	168.13	1.27	213.96	4.000	No	No	2.00
39	3.90	95.46	1.93	1.89	0.60	179.99	1.25	225.79	4.000	No	No	2.00
40	4.00	102.50	1.90	1.86	0.59	193.28	1.24	239.52	4.000	No	No	2.00
41	4.10	112.12	1.88	1.88	0.58	211.45	1.22	258.89	4.000	No	No	2.00
42	4.20	123.24	1.86	1.90	0.57	232.46	1.21	281.19	4.000	No	No	2.00
43	4.30	133.99	1.84	1.90	0.56	252.77	1.19	301.48	4.000	No	No	2.00
44	4.40	142.54	1.82	1.88	0.56	268.92	1.17	315.65	4.000	No	No	2.00
45	4.50	150.23	1.80	1.85	0.55	283.44	1.15	327.13	4.000	No	No	2.00
46	4.60	159.06	1.78	1.83	0.54	300.11	1.13	340.10	4.000	No	No	2.00
47	4.70	168.40	1.77	1.82	0.54	317.76	1.11	353.89	4.000	No	No	2.00
48	4.80	177.80	1.76	1.82	0.53	332.27	1.10	364.92	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
49	4.90	185.66	1.75	1.83	0.53	342.32	1.09	373.45	4.000	No	No	2.00
50	5.00	191.18	1.76	1.86	0.53	348.87	1.09	381.42	4.000	No	No	2.00
51	5.10	193.58	1.76	1.92	0.54	350.80	1.11	388.21	4.000	No	No	2.00
52	5.20	192.78	1.78	1.99	0.54	348.06	1.13	392.78	4.000	No	No	2.00
53	5.30	188.43	1.80	2.07	0.55	339.67	1.15	391.90	4.000	No	No	2.00
54	5.40	181.46	1.82	2.15	0.56	326.69	1.18	384.28	4.000	No	No	2.00
55	5.50	173.48	1.84	2.19	0.57	311.38	1.19	371.36	4.000	No	No	2.00
56	5.60	166.49	1.85	2.20	0.57	297.27	1.20	357.63	4.000	No	No	2.00
57	5.70	160.17	1.86	2.19	0.58	284.19	1.21	344.11	4.000	No	No	2.00
58	5.80	154.54	1.87	2.17	0.58	272.12	1.22	330.85	4.000	No	No	2.00
59	5.90	151.20	1.87	2.12	0.58	263.49	1.22	320.22	4.000	No	No	2.00
60	6.00	150.36	1.86	2.05	0.58	258.74	1.21	313.09	4.000	No	No	2.00
61	6.10	151.58	1.85	1.99	0.57	257.09	1.20	309.17	4.000	No	No	2.00
62	6.20	152.65	1.84	1.94	0.57	255.63	1.20	305.65	4.000	No	No	2.00
63	6.30	153.98	1.84	1.89	0.57	254.68	1.19	302.66	4.000	No	No	2.00
64	6.40	155.02	1.83	1.85	0.57	253.52	1.18	299.93	4.000	No	No	2.00
65	6.50	155.21	1.83	1.83	0.57	251.42	1.18	297.06	4.000	No	No	2.00
66	6.60	154.44	1.83	1.82	0.57	248.22	1.18	293.82	4.000	No	No	2.00
67	6.70	153.63	1.83	1.82	0.57	245.07	1.19	290.81	4.000	No	No	2.00
68	6.80	153.80	1.84	1.83	0.57	243.41	1.19	289.23	4.000	No	No	2.00
69	6.90	154.54	1.84	1.83	0.57	242.67	1.19	288.73	4.000	No	No	2.00
70	7.00	154.90	1.84	1.85	0.57	241.69	1.19	288.69	4.000	No	No	2.00
71	7.10	153.81	1.85	1.88	0.58	238.72	1.20	286.92	4.000	No	No	2.00
72	7.20	150.50	1.86	1.92	0.58	232.63	1.21	281.89	4.000	No	No	2.00
73	7.30	144.74	1.88	1.95	0.59	223.06	1.22	272.94	4.000	No	No	2.00
74	7.40	136.62	1.90	1.98	0.60	210.20	1.24	260.26	4.000	No	No	2.00
75	7.50	127.15	1.93	2.02	0.61	195.62	1.26	245.62	4.000	No	No	2.00
76	7.60	118.12	1.95	2.06	0.62	181.65	1.27	231.24	4.000	No	No	2.00
77	7.70	108.93	1.98	2.08	0.63	167.35	1.29	216.02	4.000	No	No	2.00
78	7.80	101.20	2.00	2.05	0.63	154.92	1.30	201.92	4.000	No	No	2.00
79	7.90	96.54	2.00	1.96	0.63	146.66	1.30	191.39	4.000	No	No	2.00
80	8.00	91.21	2.00	1.89	0.64	137.66	1.31	180.26	4.000	No	No	2.00
81	8.10	83.87	2.02	1.85	0.64	126.67	1.33	167.92	4.000	Yes	No	2.00
82	8.20	73.95	2.06	1.90	0.66	112.49	1.37	154.13	4.000	Yes	No	2.00
83	8.30	65.66	2.12	2.03	0.68	100.90	1.44	145.75	4.000	Yes	No	2.00
84	8.40	58.44	2.18	2.25	0.71	90.94	1.57	142.64	4.000	Yes	No	2.00
85	8.50	50.44	2.26	2.59	0.74	79.84	1.80	143.46	4.000	Yes	No	2.00
86	8.60	41.90	2.36	3.02	0.77	67.67	2.18	147.70	4.000	Yes	No	2.00
87	8.70	33.76	2.46	3.47	0.81	55.64	2.75	152.84	4.000	Yes	No	2.00
88	8.80	26.20	2.57	3.85	0.85	43.97	4.40	193.67	4.000	Yes	No	2.00
89	8.90	21.14	2.65	4.09	0.88	35.90	7.45	267.42	4.000	Yes	No	2.00
90	9.00	19.30	2.69	4.24	0.90	32.88	9.46	311.07	4.000	Yes	No	2.00
91	9.10	20.38	2.67	4.19	0.89	34.45	8.43	290.51	3.600	No	No	2.00
92	9.20	22.74	2.62	3.85	0.87	37.82	5.98	225.96	3.600	No	No	2.00
93	9.30	23.71	2.57	3.34	0.85	38.80	4.31	167.41	0.516	No	No	0.83
94	9.40	23.62	2.52	2.81	0.84	38.05	3.23	123.06	0.253	No	No	0.40
95	9.50	22.74	2.49	2.42	0.83	36.21	2.94	106.47	0.192	No	No	0.31
96	9.60	22.51	2.48	2.23	0.82	35.54	2.83	100.72	0.175	No	No	0.28

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _t (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
97	9.70	22.82	2.47	2.22	0.82	35.87	2.81	100.65	0.175	No	No	0.27
98	9.80	23.67	2.47	2.30	0.82	37.07	2.80	103.70	0.184	No	No	0.29
99	9.90	26.17	2.44	2.31	0.81	40.64	2.61	106.25	0.192	No	No	0.30
100	10.00	29.98	2.39	2.20	0.79	45.91	2.32	106.58	0.193	No	No	0.30
101	10.10	33.87	2.34	2.07	0.77	51.13	2.07	106.04	0.191	No	No	0.29
102	10.20	36.11	2.31	1.97	0.75	53.96	1.95	105.04	0.188	No	No	0.29
103	10.30	36.87	2.29	1.91	0.75	54.74	1.90	103.81	0.184	No	No	0.28
104	10.40	37.04	2.28	1.85	0.75	54.68	1.86	101.87	0.178	No	No	0.27
105	10.50	37.04	2.28	1.79	0.74	54.38	1.84	99.80	0.172	No	No	0.26
106	10.60	36.91	2.28	1.78	0.74	54.01	1.84	99.38	0.171	No	No	0.26
107	10.70	36.31	2.30	1.87	0.75	53.16	1.91	101.47	0.177	No	No	0.27
108	10.80	35.51	2.33	2.03	0.76	52.14	2.03	105.63	0.190	No	No	0.28
109	10.90	34.67	2.36	2.20	0.77	51.05	2.15	110.00	0.204	No	No	0.30
110	11.00	33.49	2.38	2.35	0.79	49.41	2.29	113.24	4.000	Yes	No	2.00
111	11.10	30.97	2.43	2.51	0.80	45.89	2.52	115.78	4.000	Yes	No	2.00
112	11.20	27.24	2.49	2.75	0.83	40.67	2.93	119.12	4.000	Yes	No	2.00
113	11.30	22.91	2.58	3.05	0.86	34.54	4.63	159.79	4.000	Yes	No	2.00
114	11.40	18.96	2.66	3.36	0.89	28.83	8.08	233.07	4.000	Yes	No	2.00
115	11.50	15.45	2.75	3.64	0.93	23.64	5.26	124.40	4.000	Yes	Yes	2.00
116	11.60	12.82	2.83	3.86	0.96	19.66	6.21	122.14	4.000	Yes	Yes	2.00
117	11.70	10.68	2.90	4.02	0.98	16.37	7.22	118.19	4.000	Yes	Yes	2.00
118	11.80	8.66	2.99	4.22	1.00	13.12	8.60	112.93	4.000	Yes	Yes	2.00
119	11.90	7.50	3.07	4.61	1.00	11.15	10.02	111.73	0.532	No	Yes	0.77
120	12.00	8.19	3.06	5.01	1.00	12.24	9.84	120.43	0.584	No	Yes	0.84
121	12.10	11.14	2.94	4.79	1.00	16.97	7.78	131.99	0.810	No	Yes	1.16
122	12.20	15.23	2.80	4.15	0.95	22.88	5.83	133.48	1.091	No	Yes	1.56
123	12.30	19.15	2.67	3.39	0.90	28.22	8.57	241.94	3.600	No	No	2.00
124	12.40	21.99	2.58	2.81	0.86	31.83	4.73	150.46	0.397	No	No	0.56
125	12.50	24.28	2.52	2.54	0.84	34.72	3.25	112.94	0.214	No	No	0.30
126	12.60	25.49	2.52	2.64	0.84	36.34	3.17	115.16	0.222	No	No	0.31
127	12.70	25.26	2.55	2.97	0.85	36.13	4.01	144.97	0.363	No	No	0.51
128	12.80	22.79	2.62	3.41	0.88	32.82	6.33	207.78	3.600	No	No	2.00
129	12.90	19.03	2.72	3.86	0.92	27.60	4.88	134.79	1.316	No	Yes	1.84
130	13.00	15.05	2.82	4.34	0.96	21.95	6.17	135.39	1.047	No	Yes	1.46
131	13.10	11.64	2.95	4.93	1.00	17.00	7.89	134.12	0.811	No	Yes	1.13
132	13.20	9.43	3.06	5.58	1.00	13.47	9.79	131.96	0.643	No	Yes	0.89
133	13.30	8.27	3.13	5.97	1.00	11.61	11.13	129.16	0.554	No	Yes	0.77
134	13.40	7.40	3.18	6.16	1.00	10.22	12.22	124.80	0.487	No	Yes	0.67
135	13.50	6.61	3.23	6.25	1.00	8.94	13.34	119.25	0.426	No	Yes	0.59
136	13.60	6.06	3.26	6.22	1.00	8.06	14.16	114.12	0.384	No	Yes	0.53
137	13.70	5.98	3.25	5.88	1.00	7.90	13.96	110.30	0.377	No	Yes	0.51
138	13.80	5.98	3.23	5.35	1.00	7.87	13.39	105.35	0.375	No	Yes	0.51
139	13.90	5.98	3.20	4.81	1.00	7.83	12.78	100.08	0.374	No	Yes	0.51
140	14.00	5.83	3.19	4.41	1.00	7.57	12.55	95.03	0.361	No	Yes	0.49
141	14.10	5.63	3.20	4.27	1.00	7.24	12.72	92.13	0.345	No	Yes	0.47
142	14.20	5.64	3.21	4.43	1.00	7.22	12.95	93.54	0.344	No	Yes	0.46
143	14.30	6.24	3.19	4.73	1.00	8.10	12.42	100.58	0.386	No	Yes	0.52
144	14.40	7.17	3.14	4.97	1.00	9.47	11.53	109.14	0.452	No	Yes	0.61

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _t (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
145	14.50	7.57	3.14	5.20	1.00	10.02	11.38	113.98	0.478	No	Yes	0.64
146	14.60	7.18	3.18	5.58	1.00	9.39	12.25	115.06	0.448	No	Yes	0.60
147	14.70	6.44	3.25	6.22	1.00	8.26	13.95	115.27	0.394	No	Yes	0.52
148	14.80	6.04	3.30	6.82	1.00	7.63	15.27	116.57	0.364	No	Yes	0.48
149	14.90	5.98	3.31	6.91	1.00	7.51	15.52	116.52	0.358	No	Yes	0.47
150	15.00	5.98	3.30	6.50	1.00	7.47	15.13	113.05	0.356	No	Yes	0.47
151	15.10	5.98	3.27	5.92	1.00	7.44	14.52	108.04	0.355	No	Yes	0.47
152	15.20	5.98	3.25	5.43	1.00	7.41	13.98	103.61	0.353	No	Yes	0.46
153	15.30	5.98	3.24	5.07	1.00	7.38	13.59	100.27	0.352	No	Yes	0.46
154	15.40	5.98	3.23	4.83	1.00	7.35	13.33	97.93	0.351	No	Yes	0.46
155	15.50	5.98	3.22	4.78	1.00	7.32	13.30	97.31	0.349	No	Yes	0.46
156	15.60	6.05	3.23	4.96	1.00	7.40	13.44	99.43	0.353	No	Yes	0.46
157	15.70	6.60	3.21	5.32	1.00	8.15	13.06	106.52	0.389	No	Yes	0.50
158	15.80	7.40	3.19	5.75	1.00	9.26	12.54	116.20	0.442	No	Yes	0.57
159	15.90	8.12	3.18	6.18	1.00	10.25	12.21	125.19	0.489	No	Yes	0.63
160	16.00	8.37	3.18	6.54	1.00	10.57	12.33	130.36	0.504	No	Yes	0.65
161	16.10	8.36	3.19	6.73	1.00	10.52	12.54	131.94	0.502	No	Yes	0.65
162	16.20	7.83	3.22	6.78	1.00	9.73	13.19	128.33	0.464	No	Yes	0.60
163	16.30	6.82	3.27	6.77	1.00	8.26	14.53	120.04	0.394	No	Yes	0.50
164	16.40	5.50	3.36	6.75	1.00	6.37	16.91	107.79	0.304	No	Yes	0.39
165	16.50	4.57	3.44	6.62	1.00	5.04	19.26	97.08	0.240	No	Yes	0.31
166	16.60	4.32	3.46	6.39	1.00	4.66	19.86	92.57	0.222	No	Yes	0.28
167	16.70	4.93	3.38	6.00	1.00	5.50	17.52	96.33	0.262	No	Yes	0.33
168	16.80	5.99	3.28	5.50	1.00	6.95	14.63	101.72	0.332	No	Yes	0.42
169	16.90	6.79	3.21	5.05	1.00	8.03	12.87	103.38	0.383	No	Yes	0.48
170	17.00	6.62	3.21	4.81	1.00	7.76	12.86	99.77	0.370	No	Yes	0.47
171	17.10	5.62	3.28	4.98	1.00	6.35	14.78	93.88	0.303	No	Yes	0.38
172	17.20	4.35	3.43	5.65	1.00	4.58	19.04	87.21	0.218	No	Yes	0.27
173	17.30	3.44	3.58	6.50	1.00	3.32	24.47	81.29	0.158	No	Yes	0.20
174	17.40	3.24	3.62	6.60	1.00	3.04	25.98	78.90	0.145	No	Yes	0.18
175	17.50	3.46	3.57	6.16	1.00	3.32	23.95	79.45	0.158	No	Yes	0.20
176	17.60	4.20	3.46	5.68	1.00	4.31	19.81	85.35	0.206	No	Yes	0.26
177	17.70	5.21	3.35	5.58	1.00	5.66	16.67	94.43	0.270	No	Yes	0.34
178	17.80	6.62	3.26	5.66	1.00	7.55	14.10	106.39	0.360	No	Yes	0.45
179	17.90	7.68	3.21	5.82	1.00	8.94	12.89	115.24	0.426	No	Yes	0.53
180	18.00	8.46	3.18	5.96	1.00	9.95	12.22	121.60	0.475	No	Yes	0.59
181	18.10	9.19	3.15	6.11	1.00	10.90	11.71	127.56	0.520	No	Yes	0.64
182	18.20	10.11	3.13	6.28	1.00	12.08	11.15	134.61	0.576	No	Yes	0.71
183	18.30	11.39	3.09	6.39	1.00	13.73	10.40	142.78	0.655	No	Yes	0.81
184	18.40	12.95	3.04	6.30	1.00	15.75	9.49	149.44	0.751	No	Yes	0.92
185	18.50	15.09	2.97	5.99	1.00	18.52	8.33	154.33	4.000	Yes	Yes	2.00
186	18.60	17.76	2.89	5.50	0.99	21.88	7.13	155.98	4.000	Yes	Yes	2.00
187	18.70	21.28	2.80	4.88	0.95	26.10	5.90	153.88	4.000	Yes	Yes	2.00
188	18.80	25.82	2.70	4.21	0.92	31.44	4.71	148.07	4.000	Yes	Yes	2.00
189	18.90	31.54	2.59	3.58	0.87	38.07	5.12	194.85	4.000	Yes	No	2.00
190	19.00	37.82	2.50	3.12	0.84	45.24	2.95	133.67	4.000	Yes	No	2.00
191	19.10	43.39	2.43	2.90	0.81	51.55	2.56	131.93	4.000	Yes	No	2.00
192	19.20	48.52	2.39	2.81	0.80	57.34	2.33	133.34	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _t (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
193	19.30	55.06	2.34	2.67	0.78	64.65	2.08	134.36	4.000	Yes	No	2.00
194	19.40	66.32	2.25	2.36	0.74	77.08	1.74	134.27	4.000	Yes	No	2.00
195	19.50	80.83	2.14	2.01	0.70	92.82	1.48	137.72	4.000	Yes	No	2.00
196	19.60	88.75	2.08	1.83	0.68	101.14	1.40	141.30	4.000	Yes	No	2.00
197	19.70	81.34	2.12	1.89	0.70	92.71	1.45	134.56	4.000	Yes	No	2.00
198	19.80	68.26	2.24	2.32	0.74	78.36	1.71	134.09	4.000	Yes	No	2.00
199	19.90	59.34	2.36	3.01	0.79	68.63	2.16	148.22	4.000	Yes	No	2.00
200	20.00	53.32	2.43	3.49	0.82	61.83	2.56	158.59	4.000	Yes	No	2.00
201	20.10	41.41	2.54	3.81	0.86	48.08	3.61	173.72	4.000	Yes	No	2.00
202	20.20	26.61	2.71	4.20	0.92	30.82	4.77	146.98	4.000	Yes	Yes	2.00
203	20.30	17.09	2.88	4.65	0.99	19.57	6.95	136.07	4.000	Yes	Yes	2.00
204	20.40	13.44	2.99	4.93	1.00	15.07	8.53	128.60	4.000	Yes	Yes	2.00
205	20.50	11.12	3.06	4.95	1.00	12.17	9.81	119.45	0.581	No	Yes	0.69
206	20.60	9.65	3.10	4.69	1.00	10.33	10.61	109.61	0.493	No	Yes	0.59
207	20.70	8.78	3.12	4.34	1.00	9.23	10.97	101.33	0.440	No	Yes	0.53
208	20.80	8.37	3.12	4.10	1.00	8.70	11.10	96.57	0.415	No	Yes	0.49
209	20.90	8.37	3.12	3.98	1.00	8.67	10.98	95.21	0.414	No	Yes	0.49
210	21.00	8.21	3.12	3.94	1.00	8.46	11.11	93.93	0.403	No	Yes	0.48
211	21.10	7.65	3.16	3.95	1.00	7.74	11.77	91.14	0.369	No	Yes	0.44
212	21.20	6.85	3.21	3.98	1.00	6.76	12.89	87.10	0.322	No	Yes	0.38
213	21.30	6.21	3.25	4.03	1.00	5.96	14.03	83.63	0.284	No	Yes	0.34
214	21.40	6.04	3.28	4.18	1.00	5.75	14.58	83.80	0.274	No	Yes	0.32
215	21.50	6.56	3.26	4.56	1.00	6.34	14.24	90.29	0.302	No	Yes	0.36
216	21.60	8.06	3.20	5.08	1.00	8.11	12.83	104.05	0.387	No	Yes	0.46
217	21.70	10.65	3.11	5.35	1.00	11.16	10.78	120.34	0.532	No	Yes	0.63
218	21.80	13.72	3.01	5.32	1.00	14.76	9.01	133.07	0.704	No	Yes	0.83
219	21.90	16.18	2.95	5.17	1.00	17.62	7.92	139.48	0.840	No	Yes	0.99
220	22.00	17.19	2.92	5.10	1.00	18.75	7.55	141.48	0.894	No	Yes	1.05
221	22.10	16.91	2.94	5.25	1.00	18.34	7.78	142.78	0.875	No	Yes	1.02
222	22.20	16.26	2.97	5.62	1.00	17.53	8.32	145.89	0.836	No	Yes	0.98
223	22.30	16.46	2.98	5.90	1.00	17.70	8.50	150.49	0.844	No	Yes	0.99
224	22.40	18.11	2.95	5.81	1.00	19.55	7.92	154.82	0.933	No	Yes	1.09
225	22.50	21.27	2.87	5.31	0.98	23.06	6.75	155.60	1.100	No	Yes	1.28
226	22.60	25.33	2.77	4.59	0.95	27.46	5.47	150.32	1.310	No	Yes	1.53
227	22.70	29.04	2.67	3.82	0.91	31.36	8.56	268.56	3.600	No	No	2.00
228	22.80	31.21	2.60	3.17	0.88	33.53	5.31	178.05	0.605	No	No	0.70
229	22.90	31.37	2.56	2.83	0.87	33.54	4.29	143.79	0.356	No	No	0.41
230	23.00	29.97	2.59	2.88	0.88	31.93	4.93	157.50	0.443	No	No	0.51
231	23.10	27.89	2.65	3.29	0.90	29.64	7.34	217.72	3.600	No	No	2.00
232	23.20	25.85	2.72	3.88	0.93	27.43	4.92	135.01	1.308	No	Yes	1.52
233	23.30	23.86	2.79	4.44	0.95	25.23	5.68	143.34	1.203	No	Yes	1.39
234	23.40	21.26	2.86	4.95	0.98	22.35	6.60	147.53	1.066	No	Yes	1.23
235	23.50	17.88	2.95	5.51	1.00	18.55	7.94	147.32	0.885	No	Yes	1.02
236	23.60	14.85	3.05	6.23	1.00	15.09	9.68	146.07	0.720	No	Yes	0.83
237	23.70	13.28	3.12	6.81	1.00	13.28	10.97	145.74	0.634	No	Yes	0.73
238	23.80	12.51	3.14	6.85	1.00	12.39	11.48	142.23	0.591	No	Yes	0.68
239	23.90	11.58	3.16	6.49	1.00	11.31	11.79	133.35	0.540	No	Yes	0.62
240	24.00	10.09	3.19	5.98	1.00	9.63	12.48	120.18	0.459	No	Yes	0.53

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
241	24.10	8.71	3.23	5.63	1.00	8.07	13.51	109.01	0.385	No	Yes	0.44
242	24.20	7.82	3.28	5.56	1.00	7.07	14.55	102.84	0.337	No	Yes	0.39
243	24.30	7.70	3.29	5.61	1.00	6.90	14.82	102.28	0.329	No	Yes	0.38
244	24.40	8.15	3.27	5.66	1.00	7.38	14.29	105.43	0.352	No	Yes	0.40
245	24.50	8.70	3.24	5.62	1.00	7.96	13.60	108.26	0.380	No	Yes	0.43
246	24.60	8.57	3.24	5.54	1.00	7.78	13.70	106.67	0.371	No	Yes	0.42
247	24.70	7.74	3.28	5.45	1.00	6.86	14.69	100.75	0.327	No	Yes	0.37
248	24.80	6.79	3.33	5.28	1.00	5.80	16.04	93.07	0.277	No	Yes	0.32
249	24.90	6.15	3.37	5.02	1.00	5.09	17.00	86.47	0.243	No	Yes	0.28
250	25.00	5.98	3.37	4.80	1.00	4.89	17.09	83.52	0.233	No	Yes	0.27
251	25.10	6.01	3.37	4.81	1.00	4.90	17.07	83.73	0.234	No	Yes	0.27
252	25.20	6.34	3.36	5.03	1.00	5.24	16.71	87.60	0.250	No	Yes	0.28
253	25.30	7.03	3.32	5.31	1.00	5.97	15.79	94.30	0.285	No	Yes	0.32
254	25.40	7.80	3.29	5.53	1.00	6.77	14.90	100.93	0.323	No	Yes	0.37
255	25.50	8.27	3.27	5.72	1.00	7.25	14.52	105.30	0.346	No	Yes	0.39
256	25.60	8.37	3.28	5.91	1.00	7.33	14.64	107.36	0.350	No	Yes	0.40
257	25.70	8.13	3.30	6.10	1.00	7.05	15.20	107.22	0.336	No	Yes	0.38
258	25.80	7.53	3.35	6.36	1.00	6.40	16.43	105.07	0.305	No	Yes	0.35
259	25.90	7.11	3.38	6.67	1.00	5.93	17.55	104.06	0.283	No	Yes	0.32
260	26.00	7.40	3.38	6.89	1.00	6.22	17.32	107.69	0.297	No	Yes	0.34
261	26.10	8.52	3.32	6.95	1.00	7.37	15.73	115.94	0.352	No	Yes	0.40
262	26.20	9.73	3.27	6.95	1.00	8.62	14.35	123.61	0.411	No	Yes	0.46
263	26.30	10.47	3.24	6.99	1.00	9.37	13.69	128.26	0.447	No	Yes	0.50
264	26.40	10.75	3.24	7.09	1.00	9.63	13.57	130.62	0.459	No	Yes	0.52
265	26.50	10.76	3.24	7.26	1.00	9.61	13.74	132.04	0.458	No	Yes	0.52
266	26.60	10.76	3.25	7.41	1.00	9.58	13.91	133.25	0.457	No	Yes	0.51
267	26.70	10.76	3.26	7.54	1.00	9.55	14.06	134.20	0.455	No	Yes	0.51
268	26.80	10.76	3.26	7.66	1.00	9.52	14.19	135.04	0.454	No	Yes	0.51
269	26.90	10.76	3.27	7.79	1.00	9.48	14.34	135.97	0.452	No	Yes	0.51
270	27.00	10.76	3.27	7.89	1.00	9.45	14.45	136.64	0.451	No	Yes	0.51
271	27.10	10.76	3.27	7.94	1.00	9.42	14.53	136.88	0.449	No	Yes	0.50
272	27.20	10.76	3.27	7.91	1.00	9.39	14.53	136.47	0.448	No	Yes	0.50
273	27.30	10.62	3.28	7.79	1.00	9.22	14.57	134.41	0.440	No	Yes	0.49
274	27.40	10.09	3.29	7.60	1.00	8.65	14.95	129.24	0.412	No	Yes	0.46
275	27.50	9.29	3.32	7.34	1.00	7.81	15.59	121.84	0.373	No	Yes	0.42
276	27.60	8.63	3.33	6.98	1.00	7.12	16.08	114.51	0.340	No	Yes	0.38
277	27.70	8.37	3.33	6.56	1.00	6.83	16.02	109.46	0.326	No	Yes	0.36
278	27.80	8.37	3.32	6.22	1.00	6.81	15.67	106.68	0.325	No	Yes	0.36
279	27.90	8.49	3.31	6.06	1.00	6.91	15.34	106.03	0.330	No	Yes	0.37
280	28.00	8.69	3.30	6.05	1.00	7.09	15.10	107.03	0.338	No	Yes	0.38
281	28.10	8.89	3.29	6.08	1.00	7.27	14.91	108.37	0.347	No	Yes	0.39
282	28.20	9.37	3.27	6.01	1.00	7.73	14.29	110.43	0.369	No	Yes	0.41
283	28.30	9.97	3.23	5.86	1.00	8.30	13.53	112.26	0.396	No	Yes	0.44
284	28.40	10.57	3.20	5.70	1.00	8.87	12.83	113.72	0.423	No	Yes	0.47
285	28.50	10.98	3.18	5.59	1.00	9.25	12.38	114.46	0.441	No	Yes	0.49
286	28.60	11.67	3.16	5.49	1.00	9.90	11.76	116.48	0.472	No	Yes	0.53
287	28.70	12.47	3.13	5.41	1.00	10.66	11.16	118.95	0.508	No	Yes	0.57
288	28.80	13.04	3.11	5.40	1.00	11.19	10.82	121.06	0.534	No	Yes	0.59

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
289	28.90	13.15	3.11	5.49	1.00	11.26	10.87	122.36	0.537	No	Yes	0.60
290	29.00	13.15	3.12	5.60	1.00	11.23	11.00	123.50	0.536	No	Yes	0.60
291	29.10	13.15	3.12	5.63	1.00	11.19	11.04	123.61	0.534	No	Yes	0.59
292	29.20	13.15	3.12	5.50	1.00	11.16	10.93	122.04	0.532	No	Yes	0.59
293	29.30	12.81	3.12	5.29	1.00	10.80	10.94	118.22	0.515	No	Yes	0.57
294	29.40	12.02	3.13	5.08	1.00	10.01	11.25	112.62	0.477	No	Yes	0.53
295	29.50	11.23	3.15	4.90	1.00	9.21	11.65	107.30	0.439	No	Yes	0.49
296	29.60	10.91	3.16	4.78	1.00	8.88	11.78	104.58	0.424	No	Yes	0.47
297	29.70	11.76	3.12	4.69	1.00	9.66	11.07	106.96	0.461	No	Yes	0.51
298	29.80	12.59	3.10	4.74	1.00	10.43	10.59	110.50	0.498	No	Yes	0.55
299	29.90	13.04	3.09	4.87	1.00	10.83	10.49	113.64	0.517	No	Yes	0.57
300	30.00	13.53	3.09	4.99	1.00	11.27	10.35	116.63	0.538	No	Yes	0.60
301	30.10	14.07	3.07	5.02	1.00	11.76	10.11	118.88	0.561	No	Yes	0.62
302	30.20	14.43	3.06	5.02	1.00	12.07	9.94	119.91	0.576	No	Yes	0.64
303	30.30	13.96	3.08	5.04	1.00	11.58	10.22	118.41	0.553	No	Yes	0.61
304	30.40	13.58	3.09	5.02	1.00	11.19	10.42	116.67	0.534	No	Yes	0.59
305	30.50	13.33	3.10	5.03	1.00	10.92	10.60	115.77	0.521	No	Yes	0.58
306	30.60	12.70	3.13	5.23	1.00	10.30	11.21	115.52	0.491	No	Yes	0.54
307	30.70	12.12	3.17	5.67	1.00	9.72	12.09	117.55	0.464	No	Yes	0.51
308	30.80	13.30	3.15	5.95	1.00	10.80	11.61	125.41	0.515	No	Yes	0.57
309	30.90	17.68	3.02	5.58	1.00	14.86	9.21	136.92	0.709	No	Yes	0.78
310	31.00	25.04	2.86	4.82	0.99	21.68	6.63	143.72	4.000	Yes	Yes	2.00
311	31.10	33.65	2.70	3.97	0.93	29.66	4.72	140.06	4.000	Yes	Yes	2.00
312	31.20	41.52	2.57	3.22	0.88	36.92	4.46	164.65	4.000	Yes	No	2.00
313	31.30	47.08	2.48	2.77	0.85	42.02	2.87	120.67	4.000	Yes	No	2.00
314	31.40	50.34	2.45	2.62	0.83	44.94	2.63	118.39	4.000	Yes	No	2.00
315	31.50	51.88	2.44	2.63	0.83	46.26	2.59	119.70	0.239	No	No	0.26
316	31.60	53.14	2.43	2.59	0.83	47.32	2.52	119.29	0.238	No	No	0.26
317	31.70	54.44	2.41	2.48	0.82	48.41	2.41	116.57	0.227	No	No	0.25
318	31.80	55.69	2.39	2.40	0.81	49.46	2.32	114.90	0.221	No	No	0.24
319	31.90	56.99	2.38	2.36	0.81	50.55	2.27	114.60	0.220	No	No	0.24
320	32.00	58.46	2.36	2.29	0.80	51.79	2.19	113.24	0.215	No	No	0.24
321	32.10	59.74	2.34	2.16	0.79	52.86	2.08	109.98	0.204	No	No	0.23
322	32.20	60.86	2.32	2.04	0.79	53.78	1.99	107.01	0.194	No	No	0.21
323	32.30	62.07	2.31	2.03	0.78	54.77	1.96	107.29	0.195	No	No	0.22
324	32.40	62.52	2.32	2.14	0.79	55.04	2.01	110.91	4.000	Yes	No	2.00
325	32.50	59.72	2.37	2.41	0.81	52.33	2.24	117.14	4.000	Yes	No	2.00
326	32.60	52.72	2.46	2.85	0.84	45.80	2.75	125.85	4.000	Yes	No	2.00
327	32.70	42.27	2.60	3.47	0.89	36.19	5.35	193.64	4.000	Yes	No	2.00
328	32.80	31.38	2.76	4.23	0.95	26.26	5.36	140.82	4.000	Yes	Yes	2.00
329	32.90	22.36	2.93	5.06	1.00	18.12	7.68	139.16	4.000	Yes	Yes	2.00
330	33.00	16.47	3.08	5.70	1.00	12.87	10.19	131.21	0.614	No	Yes	0.68
331	33.10	13.22	3.17	5.89	1.00	9.97	12.13	120.88	0.475	No	Yes	0.53
332	33.20	11.88	3.20	5.55	1.00	8.77	12.75	111.78	0.418	No	Yes	0.46
333	33.30	11.95	3.17	4.97	1.00	8.80	12.07	106.22	0.420	No	Yes	0.46
334	33.40	11.78	3.16	4.63	1.00	8.63	11.82	101.98	0.411	No	Yes	0.46
335	33.50	11.11	3.18	4.57	1.00	8.02	12.30	98.61	0.383	No	Yes	0.42
336	33.60	11.31	3.18	4.69	1.00	8.17	12.30	100.53	0.390	No	Yes	0.43

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
337	33.70	12.29	3.15	4.77	1.00	9.01	11.66	105.05	0.430	No	Yes	0.48
338	33.80	13.31	3.12	4.74	1.00	9.86	10.98	108.34	0.471	No	Yes	0.52
339	33.90	13.96	3.10	4.69	1.00	10.41	10.56	109.90	0.496	No	Yes	0.55
340	34.00	14.67	3.08	4.70	1.00	11.00	10.21	112.22	0.524	No	Yes	0.58
341	34.10	15.54	3.06	4.83	1.00	11.71	9.94	116.39	0.559	No	Yes	0.62
342	34.20	15.54	3.08	5.12	1.00	11.68	10.25	119.70	0.557	No	Yes	0.62
343	34.30	16.11	3.09	5.50	1.00	12.14	10.38	125.97	0.579	No	Yes	0.64
344	34.40	19.78	3.03	5.85	1.00	15.26	9.29	141.78	0.728	No	Yes	0.81
345	34.50	27.81	2.90	5.63	1.00	22.07	7.19	158.74	4.000	Yes	Yes	2.00
346	34.60	38.35	2.75	4.91	0.95	31.15	5.24	163.38	4.000	Yes	Yes	2.00
347	34.70	49.92	2.60	3.98	0.90	41.21	5.36	220.98	4.000	Yes	No	2.00
348	34.80	62.64	2.46	3.25	0.84	52.31	2.74	143.11	4.000	Yes	No	2.00
349	34.90	79.13	2.35	2.86	0.80	66.70	2.13	142.02	4.000	Yes	No	2.00
350	35.00	99.48	2.25	2.59	0.76	84.48	1.75	147.48	4.000	Yes	No	2.00
351	35.10	120.93	2.15	2.31	0.73	103.28	1.51	155.49	4.000	Yes	No	2.00
352	35.20	140.29	2.06	2.00	0.69	120.35	1.37	164.43	4.000	Yes	No	2.00
353	35.30	155.97	1.99	1.75	0.66	134.18	1.30	173.87	4.000	Yes	No	2.00
354	35.40	167.22	1.94	1.63	0.65	144.01	1.26	182.05	4.000	Yes	No	2.00
355	35.50	172.04	1.93	1.63	0.64	148.00	1.26	186.30	0.681	No	No	0.76
356	35.60	169.35	1.95	1.71	0.65	145.24	1.27	184.86	0.667	No	No	0.74
357	35.70	162.62	1.98	1.79	0.66	138.93	1.29	179.62	0.619	No	No	0.69
358	35.80	153.39	2.01	1.83	0.67	130.51	1.31	171.55	4.000	Yes	No	2.00
359	35.90	142.33	2.04	1.88	0.68	120.54	1.34	162.10	4.000	Yes	No	2.00
360	36.00	127.98	2.10	2.02	0.71	107.67	1.41	152.06	4.000	Yes	No	2.00
361	36.10	111.52	2.18	2.30	0.74	92.97	1.57	145.72	4.000	Yes	No	2.00
362	36.20	94.75	2.29	2.72	0.78	78.10	1.87	146.32	4.000	Yes	No	2.00
363	36.30	81.09	2.39	3.22	0.82	66.05	2.32	153.12	4.000	Yes	No	2.00
364	36.40	77.71	2.43	3.54	0.84	62.92	2.56	161.10	4.000	Yes	No	2.00
365	36.50	89.74	2.38	3.38	0.81	73.00	2.25	164.17	4.000	Yes	No	2.00
366	36.60	116.69	2.24	2.89	0.76	95.99	1.74	166.66	4.000	Yes	No	2.00
367	36.70	151.21	2.10	2.35	0.71	125.75	1.42	178.50	4.000	Yes	No	2.00
368	36.80	183.51	1.99	1.99	0.67	153.75	1.30	199.49	4.000	Yes	No	2.00
369	36.90	207.83	1.92	1.81	0.64	174.76	1.25	218.63	4.000	Yes	No	2.00
370	37.00	225.84	1.89	1.79	0.63	190.03	1.23	234.36	4.000	No	No	2.00
371	37.10	236.91	1.89	1.82	0.63	199.16	1.23	244.58	4.000	No	No	2.00
372	37.20	240.81	1.89	1.84	0.63	202.11	1.23	248.10	4.000	No	No	2.00
373	37.30	235.84	1.89	1.84	0.63	197.44	1.23	243.25	4.000	No	No	2.00
374	37.40	225.38	1.91	1.84	0.64	188.09	1.24	233.40	4.000	No	No	2.00
375	37.50	213.17	1.92	1.83	0.64	177.28	1.25	221.78	4.000	No	No	2.00
376	37.60	201.83	1.93	1.81	0.65	167.31	1.26	210.53	4.000	No	No	2.00
377	37.70	194.32	1.93	1.74	0.65	160.72	1.26	202.21	4.000	No	No	2.00
378	37.80	192.34	1.92	1.67	0.64	158.91	1.25	198.83	0.811	No	No	0.91
379	37.90	195.72	1.91	1.65	0.64	161.54	1.25	201.20	4.000	No	No	2.00
380	38.00	202.49	1.92	1.72	0.64	166.84	1.25	208.20	4.000	No	No	2.00
381	38.10	209.96	1.93	1.85	0.65	172.55	1.26	217.04	4.000	No	No	2.00
382	38.20	216.55	1.95	2.01	0.66	177.42	1.27	225.56	4.000	No	No	2.00
383	38.30	221.69	1.97	2.15	0.66	181.09	1.28	232.42	4.000	No	No	2.00
384	38.40	225.49	1.98	2.24	0.67	183.72	1.29	237.27	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _k (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
385	38.50	228.03	1.99	2.31	0.67	185.33	1.30	240.44	4.000	No	No	2.00
386	38.60	228.61	1.99	2.35	0.67	185.34	1.30	241.49	4.000	No	No	2.00
387	38.70	226.29	2.00	2.40	0.68	182.93	1.31	239.89	4.000	No	No	2.00
388	38.80	221.32	2.02	2.44	0.68	178.34	1.32	235.81	4.000	No	No	2.00
389	38.90	215.06	2.03	2.47	0.69	172.72	1.33	230.49	4.000	No	No	2.00
390	39.00	208.89	2.04	2.50	0.69	167.21	1.35	225.14	4.000	No	No	2.00
391	39.10	203.92	2.05	2.49	0.69	162.78	1.35	220.27	4.000	No	No	2.00
392	39.20	201.00	2.05	2.46	0.69	160.10	1.35	216.67	4.000	No	No	2.00
393	39.30	200.94	2.04	2.40	0.69	159.85	1.35	215.07	4.000	No	No	2.00
394	39.40	203.86	2.03	2.35	0.69	162.06	1.33	216.08	4.000	No	No	2.00
395	39.50	209.63	2.01	2.29	0.68	166.61	1.32	219.76	4.000	No	No	2.00
396	39.60	217.99	2.00	2.25	0.67	173.26	1.30	226.10	4.000	No	No	2.00
397	39.70	228.76	1.98	2.24	0.67	181.83	1.29	235.07	4.000	No	No	2.00
398	39.80	241.19	1.97	2.25	0.66	191.65	1.28	246.15	4.000	No	No	2.00
399	39.90	254.27	1.96	2.29	0.66	201.91	1.28	258.19	4.000	No	No	2.00
400	40.00	265.96	1.96	2.33	0.66	210.97	1.28	269.15	4.000	No	No	2.00
401	40.10	276.78	1.95	2.36	0.66	219.35	1.27	278.88	4.000	No	No	2.00
402	40.20	286.88	1.94	2.33	0.65	227.30	1.26	286.91	4.000	No	No	2.00
403	40.30	297.01	1.92	2.24	0.64	235.49	1.25	293.69	4.000	No	No	2.00
404	40.40	305.93	1.89	2.12	0.63	242.83	1.23	298.50	4.000	No	No	2.00
405	40.50	313.36	1.87	2.02	0.63	248.89	1.21	301.93	4.000	No	No	2.00
406	40.60	319.25	1.85	1.98	0.62	253.48	1.20	305.08	4.000	No	No	2.00
407	40.70	323.81	1.85	1.98	0.62	256.78	1.20	308.25	4.000	No	No	2.00
408	40.80	326.58	1.85	1.98	0.62	258.58	1.20	310.12	4.000	No	No	2.00
409	40.90	326.95	1.85	1.96	0.62	258.50	1.20	309.42	4.000	No	No	2.00
410	41.00	324.52	1.84	1.94	0.62	256.18	1.20	306.29	4.000	No	No	2.00
411	41.10	319.51	1.85	1.95	0.62	251.59	1.20	302.19	4.000	No	No	2.00
412	41.20	312.79	1.87	2.00	0.63	245.39	1.21	297.74	4.000	No	No	2.00
413	41.30	304.61	1.89	2.09	0.64	237.91	1.23	292.57	4.000	No	No	2.00
414	41.40	293.60	1.92	2.19	0.65	228.19	1.25	284.54	4.000	No	No	2.00
415	41.50	278.40	1.94	2.26	0.66	215.25	1.26	272.15	4.000	No	No	2.00
416	41.60	258.94	1.97	2.30	0.67	199.13	1.28	255.30	4.000	No	No	2.00
417	41.70	237.94	1.99	2.29	0.68	182.03	1.30	236.47	4.000	No	No	2.00
418	41.80	218.97	2.01	2.26	0.68	166.71	1.31	219.18	4.000	No	No	2.00
419	41.90	200.61	2.04	2.27	0.69	151.83	1.34	203.34	4.000	No	No	2.00
420	42.00	180.78	2.08	2.39	0.71	135.61	1.40	189.41	0.712	No	No	0.83
421	42.10	157.20	2.17	2.68	0.74	116.35	1.53	178.56	0.609	No	No	0.71
422	42.20	132.67	2.26	3.04	0.78	96.63	1.78	172.42	0.557	No	No	0.65
423	42.30	112.50	2.34	3.29	0.81	80.76	2.07	167.43	0.516	No	No	0.60
424	42.40	103.27	2.36	3.21	0.82	73.67	2.16	158.76	0.452	No	No	0.53
425	42.50	106.36	2.31	2.83	0.80	76.23	1.95	148.30	0.383	No	No	0.45
426	42.60	116.27	2.22	2.40	0.77	84.17	1.68	141.26	0.342	No	No	0.40
427	42.70	123.96	2.16	2.09	0.74	90.41	1.52	137.62	0.322	No	No	0.38
428	42.80	125.54	2.13	1.95	0.73	91.71	1.47	135.07	0.309	No	No	0.36
429	42.90	120.85	2.15	2.00	0.74	87.83	1.51	132.89	4.000	Yes	No	2.00
430	43.00	111.91	2.22	2.26	0.77	80.40	1.66	133.70	4.000	Yes	No	2.00
431	43.10	101.40	2.31	2.67	0.80	71.75	1.95	139.79	4.000	Yes	No	2.00
432	43.20	92.75	2.39	3.13	0.83	64.68	2.31	149.17	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
433	43.30	88.83	2.43	3.37	0.84	61.44	2.51	154.44	4.000	Yes	No	2.00
434	43.40	90.15	2.41	3.28	0.84	62.36	2.44	152.17	0.408	No	No	0.48
435	43.50	94.42	2.37	3.00	0.82	65.64	2.22	145.47	0.366	No	No	0.43
436	43.60	98.83	2.33	2.74	0.81	69.05	2.02	139.74	0.334	No	No	0.40
437	43.70	101.21	2.30	2.61	0.80	70.83	1.93	136.98	0.319	No	No	0.38
438	43.80	101.76	2.30	2.61	0.80	71.10	1.93	137.20	0.320	No	No	0.38
439	43.90	101.61	2.31	2.69	0.80	70.76	1.97	139.40	0.332	No	No	0.39
440	44.00	101.41	2.33	2.80	0.81	70.34	2.03	142.77	0.351	No	No	0.42
441	44.10	101.33	2.34	2.95	0.81	69.98	2.11	147.36	0.378	No	No	0.45
442	44.20	101.20	2.37	3.14	0.82	69.56	2.20	153.26	0.415	No	No	0.49
443	44.30	102.65	2.38	3.32	0.83	70.30	2.27	159.70	0.459	No	No	0.55
444	44.40	107.15	2.37	3.34	0.82	73.43	2.22	163.08	0.483	No	No	0.58
445	44.50	115.17	2.32	3.12	0.81	79.40	2.02	160.41	0.464	No	No	0.55
446	44.60	124.33	2.26	2.74	0.78	86.49	1.78	153.87	0.419	No	No	0.50
447	44.70	131.80	2.20	2.41	0.76	92.40	1.61	148.70	0.386	No	No	0.46
448	44.80	135.88	2.17	2.25	0.75	95.58	1.54	146.92	0.375	No	No	0.45
449	44.90	137.36	2.17	2.27	0.75	96.48	1.54	148.17	0.383	No	No	0.46
450	45.00	138.06	2.18	2.37	0.75	96.63	1.56	151.12	0.401	No	No	0.48
451	45.10	138.23	2.19	2.47	0.76	96.38	1.60	153.78	0.418	No	No	0.50
452	45.20	137.03	2.21	2.54	0.76	95.17	1.63	155.09	0.427	No	No	0.51
453	45.30	133.73	2.23	2.63	0.77	92.39	1.68	155.47	0.429	No	No	0.52
454	45.40	129.36	2.25	2.74	0.78	88.83	1.75	155.87	0.432	No	No	0.52
455	45.50	126.45	2.27	2.81	0.79	86.43	1.80	155.93	0.433	No	No	0.52
456	45.60	127.21	2.26	2.73	0.78	86.93	1.77	153.97	0.419	No	No	0.51
457	45.70	131.34	2.22	2.52	0.77	90.15	1.66	149.85	0.393	No	No	0.48
458	45.80	136.70	2.17	2.23	0.75	94.47	1.54	145.28	0.365	No	No	0.44
459	45.90	140.90	2.12	1.99	0.73	97.96	1.45	141.93	0.346	No	No	0.42
460	46.00	142.26	2.10	1.88	0.72	99.07	1.42	140.37	0.337	No	No	0.41
461	46.10	140.88	2.11	1.93	0.73	97.75	1.44	140.33	0.337	No	No	0.41
462	46.20	137.87	2.14	2.09	0.74	94.97	1.49	141.79	0.345	No	No	0.42
463	46.30	135.03	2.18	2.24	0.75	92.38	1.56	143.75	0.356	No	No	0.43
464	46.40	133.22	2.19	2.33	0.76	90.73	1.59	144.70	0.362	No	No	0.44
465	46.50	132.83	2.20	2.38	0.76	90.17	1.62	145.76	0.368	No	No	0.45
466	46.60	133.78	2.21	2.48	0.77	90.50	1.65	149.12	0.388	No	No	0.47
467	46.70	134.60	2.24	2.67	0.78	90.57	1.71	154.91	4.000	Yes	No	2.00
468	46.80	132.80	2.27	2.92	0.79	88.68	1.82	161.37	4.000	Yes	No	2.00
469	46.90	125.89	2.32	3.19	0.81	83.19	1.99	165.91	4.000	Yes	No	2.00
470	47.00	115.97	2.37	3.48	0.83	75.67	2.24	169.55	4.000	Yes	No	2.00
471	47.10	104.67	2.43	3.71	0.85	67.40	2.53	170.35	4.000	Yes	No	2.00
472	47.20	98.78	2.45	3.77	0.86	63.13	2.67	168.63	0.526	No	No	0.65
473	47.30	98.47	2.44	3.65	0.86	62.90	2.62	164.47	0.494	No	No	0.61
474	47.40	96.95	2.44	3.59	0.86	61.77	2.62	161.58	0.472	No	No	0.58
475	47.50	88.26	2.49	3.75	0.88	55.55	2.90	161.33	0.471	No	No	0.58
476	47.60	70.99	2.60	4.17	0.92	43.46	5.29	229.98	4.000	No	No	2.00
477	47.70	54.66	2.72	4.68	0.96	32.30	4.96	160.21	1.541	No	Yes	1.90
478	47.80	43.11	2.83	5.01	1.00	24.66	6.23	153.58	1.177	No	Yes	1.46
479	47.90	37.26	2.88	5.05	1.00	21.04	6.95	146.31	1.004	No	Yes	1.24
480	48.00	35.46	2.89	4.90	1.00	19.90	7.09	141.01	0.949	No	Yes	1.18

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
481	48.10	35.37	2.89	4.92	1.00	19.80	7.12	141.08	0.945	No	Yes	1.17
482	48.20	36.65	2.90	5.31	1.00	20.54	7.28	149.41	0.980	No	Yes	1.22
483	48.30	39.52	2.91	5.99	1.00	22.24	7.43	165.15	1.061	No	Yes	1.32
484	48.40	43.87	2.90	6.45	1.00	24.83	7.24	179.87	1.184	No	Yes	1.47
485	48.50	47.02	2.88	6.50	1.00	26.68	6.96	185.63	1.273	No	Yes	1.59
486	48.60	46.83	2.88	6.34	1.00	26.51	6.88	182.33	1.265	No	Yes	1.58
487	48.70	43.44	2.89	6.17	1.00	24.41	7.13	173.95	1.164	No	Yes	1.45
488	48.80	39.99	2.92	6.06	1.00	22.29	7.47	166.43	1.063	No	Yes	1.33
489	48.90	37.97	2.93	5.93	1.00	21.03	7.65	160.86	1.003	No	Yes	1.26
490	49.00	37.11	2.93	5.78	1.00	20.47	7.66	156.88	0.976	No	Yes	1.22
491	49.10	36.51	2.93	5.66	1.00	20.07	7.67	153.90	0.957	No	Yes	1.20
492	49.20	35.49	2.94	5.58	1.00	19.43	7.77	150.91	0.927	No	Yes	1.16
493	49.30	33.74	2.95	5.54	1.00	18.34	8.03	147.20	0.875	No	Yes	1.10
494	49.40	30.37	2.99	5.54	1.00	16.30	8.65	140.97	0.778	No	Yes	0.98
495	49.50	26.08	3.05	5.55	1.00	13.72	9.65	132.46	0.655	No	Yes	0.82
496	49.60	22.32	3.11	5.52	1.00	11.46	10.77	123.51	0.547	No	Yes	0.69
497	49.70	20.21	3.14	5.41	1.00	10.20	11.47	117.01	0.486	No	Yes	0.61
498	49.80	19.41	3.15	5.31	1.00	9.70	11.73	113.79	0.463	No	Yes	0.59

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q_t :	Total cone resistance
I_c :	Soil behavior type index
Fr:	Normalized friction ratio (%)
n:	Stress exponent
Q_{tn} :	Normalized cone resistance
K_c :	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Normalized and adjusted cone resistance
CRR _{7.5} :	Cyclic resistance ratio for $M_w=7.5$
FS:	Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
0.10	2.00	0.00	0.00	0.10	0.00	0.20	2.00	0.00	0.00	0.10	0.00
0.30	2.00	0.00	0.00	0.10	0.00	0.40	2.00	0.00	0.00	0.10	0.00
0.50	2.00	0.00	0.00	0.10	0.00	0.60	2.00	0.00	0.00	0.10	0.00
0.70	2.00	0.00	0.00	0.10	0.00	0.80	2.00	0.00	0.00	0.10	0.00
0.90	2.00	0.00	0.00	0.10	0.00	1.00	2.00	0.00	0.00	0.10	0.00
1.10	2.00	0.00	0.00	0.10	0.00	1.20	2.00	0.00	0.00	0.10	0.00
1.30	2.00	0.00	0.00	0.10	0.00	1.40	2.00	0.00	0.00	0.10	0.00
1.50	2.00	0.00	0.00	0.10	0.00	1.60	2.00	0.00	0.00	0.10	0.00
1.70	2.00	0.00	0.00	0.10	0.00	1.80	2.00	0.00	0.00	0.10	0.00
1.90	2.00	0.00	0.00	0.10	0.00	2.00	2.00	0.00	0.00	0.10	0.00
2.10	2.00	0.00	0.00	0.10	0.00	2.20	2.00	0.00	0.00	0.10	0.00
2.30	2.00	0.00	0.00	0.10	0.00	2.40	2.00	0.00	0.00	0.10	0.00
2.50	2.00	0.00	0.00	0.10	0.00	2.60	2.00	0.00	0.00	0.10	0.00
2.70	2.00	0.00	0.00	0.10	0.00	2.80	2.00	0.00	0.00	0.10	0.00
2.90	2.00	0.00	0.00	0.10	0.00	3.00	2.00	0.00	0.00	0.10	0.00
3.10	2.00	0.00	0.00	0.10	0.00	3.20	2.00	0.00	0.00	0.10	0.00
3.30	2.00	0.00	0.00	0.10	0.00	3.40	2.00	0.00	0.00	0.10	0.00
3.50	2.00	0.00	0.00	0.10	0.00	3.60	2.00	0.00	0.00	0.10	0.00
3.70	2.00	0.00	0.00	0.10	0.00	3.80	2.00	0.00	0.00	0.10	0.00
3.90	2.00	0.00	0.00	0.10	0.00	4.00	2.00	0.00	0.00	0.10	0.00
4.10	2.00	0.00	0.00	0.10	0.00	4.20	2.00	0.00	0.00	0.10	0.00
4.30	2.00	0.00	0.00	0.10	0.00	4.40	2.00	0.00	0.00	0.10	0.00
4.50	2.00	0.00	0.00	0.10	0.00	4.60	2.00	0.00	0.00	0.10	0.00
4.70	2.00	0.00	0.00	0.10	0.00	4.80	2.00	0.00	0.00	0.10	0.00
4.90	2.00	0.00	0.00	0.10	0.00	5.00	2.00	0.00	0.00	0.10	0.00
5.10	2.00	0.00	0.00	0.10	0.00	5.20	2.00	0.00	0.00	0.10	0.00
5.30	2.00	0.00	0.00	0.10	0.00	5.40	2.00	0.00	0.00	0.10	0.00
5.50	2.00	0.00	0.00	0.10	0.00	5.60	2.00	0.00	0.00	0.10	0.00
5.70	2.00	0.00	0.00	0.10	0.00	5.80	2.00	0.00	0.00	0.10	0.00
5.90	2.00	0.00	0.00	0.10	0.00	6.00	2.00	0.00	0.00	0.10	0.00
6.10	2.00	0.00	0.00	0.10	0.00	6.20	2.00	0.00	0.00	0.10	0.00
6.30	2.00	0.00	0.00	0.10	0.00	6.40	2.00	0.00	0.00	0.10	0.00
6.50	2.00	0.00	0.00	0.10	0.00	6.60	2.00	0.00	0.00	0.10	0.00
6.70	2.00	0.00	0.00	0.10	0.00	6.80	2.00	0.00	0.00	0.10	0.00
6.90	2.00	0.00	0.00	0.10	0.00	7.00	2.00	0.00	0.00	0.10	0.00
7.10	2.00	0.00	0.00	0.10	0.00	7.20	2.00	0.00	0.00	0.10	0.00
7.30	2.00	0.00	0.00	0.10	0.00	7.40	2.00	0.00	0.00	0.10	0.00
7.50	2.00	0.00	0.00	0.10	0.00	7.60	2.00	0.00	0.00	0.10	0.00
7.70	2.00	0.00	0.00	0.10	0.00	7.80	2.00	0.00	0.00	0.10	0.00
7.90	2.00	0.00	0.00	0.10	0.00	8.00	2.00	0.00	0.00	0.10	0.00
8.10	2.00	0.00	0.00	0.10	0.00	8.20	2.00	0.00	0.00	0.10	0.00
8.30	2.00	0.00	0.00	0.10	0.00	8.40	2.00	0.00	0.00	0.10	0.00
8.50	2.00	0.00	0.00	0.10	0.00	8.60	2.00	0.00	0.00	0.10	0.00
8.70	2.00	0.00	0.00	0.10	0.00	8.80	2.00	0.00	0.00	0.10	0.00
8.90	2.00	0.00	0.00	0.10	0.00	9.00	2.00	0.00	0.00	0.10	0.00
9.10	2.00	0.00	0.00	0.10	0.00	9.20	2.00	0.00	0.00	0.10	0.00
9.30	0.83	0.00	0.00	0.10	0.05	9.40	0.40	0.00	0.00	0.10	0.16
9.50	0.31	0.00	0.00	0.10	0.18	9.60	0.28	0.00	0.00	0.10	0.19

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
9.70	0.27	0.00	0.00	0.10	0.19	9.80	0.29	0.00	0.00	0.10	0.18
9.90	0.30	0.00	0.00	0.10	0.18	10.00	0.30	0.00	0.00	0.10	0.18
10.10	0.29	0.00	0.00	0.10	0.18	10.20	0.29	0.00	0.00	0.10	0.18
10.30	0.28	0.00	0.00	0.10	0.18	10.40	0.27	0.00	0.00	0.10	0.19
10.50	0.26	0.00	0.00	0.10	0.19	10.60	0.26	0.00	0.00	0.10	0.19
10.70	0.27	0.00	0.00	0.10	0.19	10.80	0.28	0.00	0.00	0.10	0.18
10.90	0.30	0.00	0.00	0.10	0.18	11.00	2.00	0.00	0.00	0.10	0.00
11.10	2.00	0.00	0.00	0.10	0.00	11.20	2.00	0.00	0.00	0.10	0.00
11.30	2.00	0.00	0.00	0.10	0.00	11.40	2.00	0.00	0.00	0.10	0.00
11.50	2.00	0.00	0.00	0.10	0.00	11.60	2.00	0.00	0.00	0.10	0.00
11.70	2.00	0.00	0.00	0.10	0.00	11.80	2.00	0.00	0.00	0.10	0.00
11.90	0.77	0.00	0.00	0.10	0.06	12.00	0.84	0.00	0.00	0.10	0.04
12.10	1.16	0.00	0.00	0.10	0.00	12.20	1.56	0.00	0.00	0.10	0.00
12.30	2.00	0.00	0.00	0.10	0.00	12.40	0.56	0.00	0.00	0.10	0.11
12.50	0.30	0.00	0.00	0.10	0.17	12.60	0.31	0.00	0.00	0.10	0.17
12.70	0.51	0.00	0.00	0.10	0.12	12.80	2.00	0.00	0.00	0.10	0.00
12.90	1.84	0.00	0.00	0.10	0.00	13.00	1.46	0.00	0.00	0.10	0.00
13.10	1.13	0.00	0.00	0.10	0.00	13.20	0.89	0.00	0.00	0.10	0.03
13.30	0.77	0.00	0.00	0.10	0.06	13.40	0.67	0.00	0.00	0.10	0.08
13.50	0.59	0.00	0.00	0.10	0.10	13.60	0.53	0.00	0.00	0.10	0.11
13.70	0.51	0.00	0.00	0.10	0.12	13.80	0.51	0.00	0.00	0.10	0.12
13.90	0.51	0.00	0.00	0.10	0.12	14.00	0.49	0.00	0.00	0.10	0.12
14.10	0.47	0.00	0.00	0.10	0.13	14.20	0.46	0.00	0.00	0.10	0.13
14.30	0.52	0.00	0.00	0.10	0.11	14.40	0.61	0.00	0.00	0.10	0.09
14.50	0.64	0.00	0.00	0.10	0.09	14.60	0.60	0.00	0.00	0.10	0.10
14.70	0.52	0.00	0.00	0.10	0.11	14.80	0.48	0.00	0.00	0.10	0.12
14.90	0.47	0.00	0.00	0.10	0.12	15.00	0.47	0.00	0.00	0.10	0.12
15.10	0.47	0.00	0.00	0.10	0.12	15.20	0.46	0.00	0.00	0.10	0.13
15.30	0.46	0.00	0.00	0.10	0.13	15.40	0.46	0.00	0.00	0.10	0.13
15.50	0.46	0.00	0.00	0.10	0.13	15.60	0.46	0.00	0.00	0.10	0.13
15.70	0.50	0.00	0.00	0.10	0.11	15.80	0.57	0.00	0.00	0.10	0.10
15.90	0.63	0.00	0.00	0.10	0.08	16.00	0.65	0.00	0.00	0.10	0.08
16.10	0.65	0.00	0.00	0.10	0.08	16.20	0.60	0.00	0.00	0.10	0.09
16.30	0.50	0.00	0.00	0.10	0.11	16.40	0.39	0.00	0.00	0.10	0.14
16.50	0.31	0.00	0.00	0.10	0.16	16.60	0.28	0.00	0.00	0.10	0.16
16.70	0.33	0.00	0.00	0.10	0.15	16.80	0.42	0.00	0.00	0.10	0.13
16.90	0.48	0.00	0.00	0.10	0.12	17.00	0.47	0.00	0.00	0.10	0.12
17.10	0.38	0.00	0.00	0.10	0.14	17.20	0.27	0.00	0.00	0.10	0.16
17.30	0.20	0.00	0.00	0.10	0.18	17.40	0.18	0.00	0.00	0.10	0.18
17.50	0.20	0.00	0.00	0.10	0.18	17.60	0.26	0.00	0.00	0.10	0.17
17.70	0.34	0.00	0.00	0.10	0.15	17.80	0.45	0.00	0.00	0.10	0.12
17.90	0.53	0.00	0.00	0.10	0.10	18.00	0.59	0.00	0.00	0.10	0.09
18.10	0.64	0.00	0.00	0.10	0.08	18.20	0.71	0.00	0.00	0.10	0.06
18.30	0.81	0.00	0.00	0.10	0.04	18.40	0.92	0.00	0.00	0.10	0.02
18.50	2.00	0.00	0.00	0.10	0.00	18.60	2.00	0.00	0.00	0.10	0.00
18.70	2.00	0.00	0.00	0.10	0.00	18.80	2.00	0.00	0.00	0.10	0.00
18.90	2.00	0.00	0.00	0.10	0.00	19.00	2.00	0.00	0.00	0.10	0.00
19.10	2.00	0.00	0.00	0.10	0.00	19.20	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
19.30	2.00	0.00	0.00	0.10	0.00	19.40	2.00	0.00	0.00	0.10	0.00
19.50	2.00	0.00	0.00	0.10	0.00	19.60	2.00	0.00	0.00	0.10	0.00
19.70	2.00	0.00	0.00	0.10	0.00	19.80	2.00	0.00	0.00	0.10	0.00
19.90	2.00	0.00	0.00	0.10	0.00	20.00	2.00	0.00	0.00	0.10	0.00
20.10	2.00	0.00	0.00	0.10	0.00	20.20	2.00	0.00	0.00	0.10	0.00
20.30	2.00	0.00	0.00	0.10	0.00	20.40	2.00	0.00	0.00	0.10	0.00
20.50	0.69	0.00	0.00	0.10	0.06	20.60	0.59	0.00	0.00	0.10	0.09
20.70	0.53	0.00	0.00	0.10	0.10	20.80	0.49	0.00	0.00	0.10	0.11
20.90	0.49	0.00	0.00	0.10	0.11	21.00	0.48	0.00	0.00	0.10	0.11
21.10	0.44	0.00	0.00	0.10	0.12	21.20	0.38	0.00	0.00	0.10	0.13
21.30	0.34	0.00	0.00	0.10	0.14	21.40	0.32	0.00	0.00	0.10	0.14
21.50	0.36	0.00	0.00	0.10	0.13	21.60	0.46	0.00	0.00	0.10	0.11
21.70	0.63	0.00	0.00	0.10	0.08	21.80	0.83	0.00	0.00	0.10	0.04
21.90	0.99	0.00	0.00	0.10	0.00	22.00	1.05	0.00	0.00	0.10	0.00
22.10	1.02	0.00	0.00	0.10	0.00	22.20	0.98	0.00	0.00	0.10	0.00
22.30	0.99	0.00	0.00	0.10	0.00	22.40	1.09	0.00	0.00	0.10	0.00
22.50	1.28	0.00	0.00	0.10	0.00	22.60	1.53	0.00	0.00	0.10	0.00
22.70	2.00	0.00	0.00	0.10	0.00	22.80	0.70	0.00	0.00	0.10	0.06
22.90	0.41	0.00	0.00	0.10	0.12	23.00	0.51	0.00	0.00	0.10	0.10
23.10	2.00	0.00	0.00	0.10	0.00	23.20	1.52	0.00	0.00	0.10	0.00
23.30	1.39	0.00	0.00	0.10	0.00	23.40	1.23	0.00	0.00	0.10	0.00
23.50	1.02	0.00	0.00	0.10	0.00	23.60	0.83	0.00	0.00	0.10	0.03
23.70	0.73	0.00	0.00	0.10	0.05	23.80	0.68	0.00	0.00	0.10	0.06
23.90	0.62	0.00	0.00	0.10	0.07	24.00	0.53	0.00	0.00	0.10	0.09
24.10	0.44	0.00	0.00	0.10	0.11	24.20	0.39	0.00	0.00	0.10	0.12
24.30	0.38	0.00	0.00	0.10	0.12	24.40	0.40	0.00	0.00	0.10	0.11
24.50	0.43	0.00	0.00	0.10	0.11	24.60	0.42	0.00	0.00	0.10	0.11
24.70	0.37	0.00	0.00	0.10	0.12	24.80	0.32	0.00	0.00	0.10	0.13
24.90	0.28	0.00	0.00	0.10	0.14	25.00	0.27	0.00	0.00	0.10	0.14
25.10	0.27	0.00	0.00	0.10	0.14	25.20	0.28	0.00	0.00	0.10	0.13
25.30	0.32	0.00	0.00	0.10	0.13	25.40	0.37	0.00	0.00	0.10	0.12
25.50	0.39	0.00	0.00	0.10	0.11	25.60	0.40	0.00	0.00	0.10	0.11
25.70	0.38	0.00	0.00	0.10	0.11	25.80	0.35	0.00	0.00	0.10	0.12
25.90	0.32	0.00	0.00	0.10	0.13	26.00	0.34	0.00	0.00	0.10	0.12
26.10	0.40	0.00	0.00	0.10	0.11	26.20	0.46	0.00	0.00	0.10	0.10
26.30	0.50	0.00	0.00	0.10	0.09	26.40	0.52	0.00	0.00	0.10	0.09
26.50	0.52	0.00	0.00	0.10	0.09	26.60	0.51	0.00	0.00	0.10	0.09
26.70	0.51	0.00	0.00	0.10	0.09	26.80	0.51	0.00	0.00	0.10	0.09
26.90	0.51	0.00	0.00	0.10	0.09	27.00	0.51	0.00	0.00	0.10	0.09
27.10	0.50	0.00	0.00	0.10	0.09	27.20	0.50	0.00	0.00	0.10	0.09
27.30	0.49	0.00	0.00	0.10	0.09	27.40	0.46	0.00	0.00	0.10	0.10
27.50	0.42	0.00	0.00	0.10	0.10	27.60	0.38	0.00	0.00	0.10	0.11
27.70	0.36	0.00	0.00	0.10	0.11	27.80	0.36	0.00	0.00	0.10	0.11
27.90	0.37	0.00	0.00	0.10	0.11	28.00	0.38	0.00	0.00	0.10	0.11
28.10	0.39	0.00	0.00	0.10	0.11	28.20	0.41	0.00	0.00	0.10	0.10
28.30	0.44	0.00	0.00	0.10	0.10	28.40	0.47	0.00	0.00	0.10	0.09
28.50	0.49	0.00	0.00	0.10	0.09	28.60	0.53	0.00	0.00	0.10	0.08
28.70	0.57	0.00	0.00	0.10	0.07	28.80	0.59	0.00	0.00	0.10	0.07

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
28.90	0.60	0.00	0.00	0.10	0.07	29.00	0.60	0.00	0.00	0.10	0.07
29.10	0.59	0.00	0.00	0.10	0.07	29.20	0.59	0.00	0.00	0.10	0.07
29.30	0.57	0.00	0.00	0.10	0.07	29.40	0.53	0.00	0.00	0.10	0.08
29.50	0.49	0.00	0.00	0.10	0.09	29.60	0.47	0.00	0.00	0.10	0.09
29.70	0.51	0.00	0.00	0.10	0.08	29.80	0.55	0.00	0.00	0.10	0.07
29.90	0.57	0.00	0.00	0.10	0.07	30.00	0.60	0.00	0.00	0.10	0.07
30.10	0.62	0.00	0.00	0.10	0.06	30.20	0.64	0.00	0.00	0.10	0.06
30.30	0.61	0.00	0.00	0.10	0.06	30.40	0.59	0.00	0.00	0.10	0.07
30.50	0.58	0.00	0.00	0.10	0.07	30.60	0.54	0.00	0.00	0.10	0.07
30.70	0.51	0.00	0.00	0.10	0.08	30.80	0.57	0.00	0.00	0.10	0.07
30.90	0.78	0.00	0.00	0.10	0.03	31.00	2.00	0.00	0.00	0.10	0.00
31.10	2.00	0.00	0.00	0.10	0.00	31.20	2.00	0.00	0.00	0.10	0.00
31.30	2.00	0.00	0.00	0.10	0.00	31.40	2.00	0.00	0.00	0.10	0.00
31.50	0.26	0.00	0.00	0.10	0.12	31.60	0.26	0.00	0.00	0.10	0.12
31.70	0.25	0.00	0.00	0.10	0.12	31.80	0.24	0.00	0.00	0.10	0.12
31.90	0.24	0.00	0.00	0.10	0.12	32.00	0.24	0.00	0.00	0.10	0.12
32.10	0.23	0.00	0.00	0.10	0.12	32.20	0.21	0.00	0.00	0.10	0.12
32.30	0.22	0.00	0.00	0.10	0.12	32.40	2.00	0.00	0.00	0.10	0.00
32.50	2.00	0.00	0.00	0.10	0.00	32.60	2.00	0.00	0.00	0.10	0.00
32.70	2.00	0.00	0.00	0.10	0.00	32.80	2.00	0.00	0.00	0.10	0.00
32.90	2.00	0.00	0.00	0.10	0.00	33.00	0.68	0.00	0.00	0.10	0.05
33.10	0.53	0.00	0.00	0.10	0.07	33.20	0.46	0.00	0.00	0.10	0.08
33.30	0.46	0.00	0.00	0.10	0.08	33.40	0.46	0.00	0.00	0.10	0.08
33.50	0.42	0.00	0.00	0.10	0.09	33.60	0.43	0.00	0.00	0.10	0.08
33.70	0.48	0.00	0.00	0.10	0.08	33.80	0.52	0.00	0.00	0.10	0.07
33.90	0.55	0.00	0.00	0.10	0.07	34.00	0.58	0.00	0.00	0.10	0.06
34.10	0.62	0.00	0.00	0.10	0.06	34.20	0.62	0.00	0.00	0.10	0.06
34.30	0.64	0.00	0.00	0.10	0.05	34.40	0.81	0.00	0.00	0.10	0.03
34.50	2.00	0.00	0.00	0.10	0.00	34.60	2.00	0.00	0.00	0.10	0.00
34.70	2.00	0.00	0.00	0.10	0.00	34.80	2.00	0.00	0.00	0.10	0.00
34.90	2.00	0.00	0.00	0.10	0.00	35.00	2.00	0.00	0.00	0.10	0.00
35.10	2.00	0.00	0.00	0.10	0.00	35.20	2.00	0.00	0.00	0.10	0.00
35.30	2.00	0.00	0.00	0.10	0.00	35.40	2.00	0.00	0.00	0.10	0.00
35.50	0.76	0.00	0.00	0.10	0.03	35.60	0.74	0.00	0.00	0.10	0.04
35.70	0.69	0.00	0.00	0.10	0.04	35.80	2.00	0.00	0.00	0.10	0.00
35.90	2.00	0.00	0.00	0.10	0.00	36.00	2.00	0.00	0.00	0.10	0.00
36.10	2.00	0.00	0.00	0.10	0.00	36.20	2.00	0.00	0.00	0.10	0.00
36.30	2.00	0.00	0.00	0.10	0.00	36.40	2.00	0.00	0.00	0.10	0.00
36.50	2.00	0.00	0.00	0.10	0.00	36.60	2.00	0.00	0.00	0.10	0.00
36.70	2.00	0.00	0.00	0.10	0.00	36.80	2.00	0.00	0.00	0.10	0.00
36.90	2.00	0.00	0.00	0.10	0.00	37.00	2.00	0.00	0.00	0.10	0.00
37.10	2.00	0.00	0.00	0.10	0.00	37.20	2.00	0.00	0.00	0.10	0.00
37.30	2.00	0.00	0.00	0.10	0.00	37.40	2.00	0.00	0.00	0.10	0.00
37.50	2.00	0.00	0.00	0.10	0.00	37.60	2.00	0.00	0.00	0.10	0.00
37.70	2.00	0.00	0.00	0.10	0.00	37.80	0.91	0.00	0.00	0.10	0.01
37.90	2.00	0.00	0.00	0.10	0.00	38.00	2.00	0.00	0.00	0.10	0.00
38.10	2.00	0.00	0.00	0.10	0.00	38.20	2.00	0.00	0.00	0.10	0.00
38.30	2.00	0.00	0.00	0.10	0.00	38.40	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
38.50	2.00	0.00	0.00	0.10	0.00	38.60	2.00	0.00	0.00	0.10	0.00
38.70	2.00	0.00	0.00	0.10	0.00	38.80	2.00	0.00	0.00	0.10	0.00
38.90	2.00	0.00	0.00	0.10	0.00	39.00	2.00	0.00	0.00	0.10	0.00
39.10	2.00	0.00	0.00	0.10	0.00	39.20	2.00	0.00	0.00	0.10	0.00
39.30	2.00	0.00	0.00	0.10	0.00	39.40	2.00	0.00	0.00	0.10	0.00
39.50	2.00	0.00	0.00	0.10	0.00	39.60	2.00	0.00	0.00	0.10	0.00
39.70	2.00	0.00	0.00	0.10	0.00	39.80	2.00	0.00	0.00	0.10	0.00
39.90	2.00	0.00	0.00	0.10	0.00	40.00	2.00	0.00	0.00	0.10	0.00
40.10	2.00	0.00	0.00	0.10	0.00	40.20	2.00	0.00	0.00	0.10	0.00
40.30	2.00	0.00	0.00	0.10	0.00	40.40	2.00	0.00	0.00	0.10	0.00
40.50	2.00	0.00	0.00	0.10	0.00	40.60	2.00	0.00	0.00	0.10	0.00
40.70	2.00	0.00	0.00	0.10	0.00	40.80	2.00	0.00	0.00	0.10	0.00
40.90	2.00	0.00	0.00	0.10	0.00	41.00	2.00	0.00	0.00	0.10	0.00
41.10	2.00	0.00	0.00	0.10	0.00	41.20	2.00	0.00	0.00	0.10	0.00
41.30	2.00	0.00	0.00	0.10	0.00	41.40	2.00	0.00	0.00	0.10	0.00
41.50	2.00	0.00	0.00	0.10	0.00	41.60	2.00	0.00	0.00	0.10	0.00
41.70	2.00	0.00	0.00	0.10	0.00	41.80	2.00	0.00	0.00	0.10	0.00
41.90	2.00	0.00	0.00	0.10	0.00	42.00	0.83	0.00	0.00	0.10	0.02
42.10	0.71	0.00	0.00	0.10	0.03	42.20	0.65	0.00	0.00	0.10	0.04
42.30	0.60	0.00	0.00	0.10	0.04	42.40	0.53	0.00	0.00	0.10	0.05
42.50	0.45	0.00	0.00	0.10	0.06	42.60	0.40	0.00	0.00	0.10	0.06
42.70	0.38	0.00	0.00	0.10	0.07	42.80	0.36	0.00	0.00	0.10	0.07
42.90	2.00	0.00	0.00	0.10	0.00	43.00	2.00	0.00	0.00	0.10	0.00
43.10	2.00	0.00	0.00	0.10	0.00	43.20	2.00	0.00	0.00	0.10	0.00
43.30	2.00	0.00	0.00	0.10	0.00	43.40	0.48	0.00	0.00	0.10	0.05
43.50	0.43	0.00	0.00	0.10	0.06	43.60	0.40	0.00	0.00	0.10	0.06
43.70	0.38	0.00	0.00	0.10	0.06	43.80	0.38	0.00	0.00	0.10	0.06
43.90	0.39	0.00	0.00	0.10	0.06	44.00	0.42	0.00	0.00	0.10	0.06
44.10	0.45	0.00	0.00	0.10	0.06	44.20	0.49	0.00	0.00	0.10	0.05
44.30	0.55	0.00	0.00	0.10	0.04	44.40	0.58	0.00	0.00	0.10	0.04
44.50	0.55	0.00	0.00	0.10	0.04	44.60	0.50	0.00	0.00	0.10	0.05
44.70	0.46	0.00	0.00	0.10	0.05	44.80	0.45	0.00	0.00	0.10	0.05
44.90	0.46	0.00	0.00	0.10	0.05	45.00	0.48	0.00	0.00	0.10	0.05
45.10	0.50	0.00	0.00	0.10	0.05	45.20	0.51	0.00	0.00	0.10	0.05
45.30	0.52	0.00	0.00	0.10	0.05	45.40	0.52	0.00	0.00	0.10	0.04
45.50	0.52	0.00	0.00	0.10	0.04	45.60	0.51	0.00	0.00	0.10	0.05
45.70	0.48	0.00	0.00	0.10	0.05	45.80	0.44	0.00	0.00	0.10	0.05
45.90	0.42	0.00	0.00	0.10	0.05	46.00	0.41	0.00	0.00	0.10	0.05
46.10	0.41	0.00	0.00	0.10	0.05	46.20	0.42	0.00	0.00	0.10	0.05
46.30	0.43	0.00	0.00	0.10	0.05	46.40	0.44	0.00	0.00	0.10	0.05
46.50	0.45	0.00	0.00	0.10	0.05	46.60	0.47	0.00	0.00	0.10	0.05
46.70	2.00	0.00	0.00	0.10	0.00	46.80	2.00	0.00	0.00	0.10	0.00
46.90	2.00	0.00	0.00	0.10	0.00	47.00	2.00	0.00	0.00	0.10	0.00
47.10	2.00	0.00	0.00	0.10	0.00	47.20	0.65	0.00	0.00	0.10	0.03
47.30	0.61	0.00	0.00	0.10	0.03	47.40	0.58	0.00	0.00	0.10	0.04
47.50	0.58	0.00	0.00	0.10	0.04	47.60	2.00	0.00	0.00	0.10	0.00
47.70	1.90	0.00	0.00	0.10	0.00	47.80	1.46	0.00	0.00	0.10	0.00
47.90	1.24	0.00	0.00	0.10	0.00	48.00	1.18	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
48.10	1.17	0.00	0.00	0.10	0.00	48.20	1.22	0.00	0.00	0.10	0.00
48.30	1.32	0.00	0.00	0.10	0.00	48.40	1.47	0.00	0.00	0.10	0.00
48.50	1.59	0.00	0.00	0.10	0.00	48.60	1.58	0.00	0.00	0.10	0.00
48.70	1.45	0.00	0.00	0.10	0.00	48.80	1.33	0.00	0.00	0.10	0.00
48.90	1.26	0.00	0.00	0.10	0.00	49.00	1.22	0.00	0.00	0.10	0.00
49.10	1.20	0.00	0.00	0.10	0.00	49.20	1.16	0.00	0.00	0.10	0.00
49.30	1.10	0.00	0.00	0.10	0.00	49.40	0.98	0.00	0.00	0.10	0.00
49.50	0.82	0.00	0.00	0.10	0.01	49.60	0.69	0.00	0.00	0.10	0.02
49.70	0.61	0.00	0.00	0.10	0.03	49.80	0.59	0.00	0.00	0.10	0.03

Overall liquefaction potential: 22.84

LPI = 0.00 - Liquefaction risk very low

LPI between 0.00 and 5.00 - Liquefaction risk low

LPI between 5.00 and 15.00 - Liquefaction risk high

LPI > 15.00 - Liquefaction risk very high

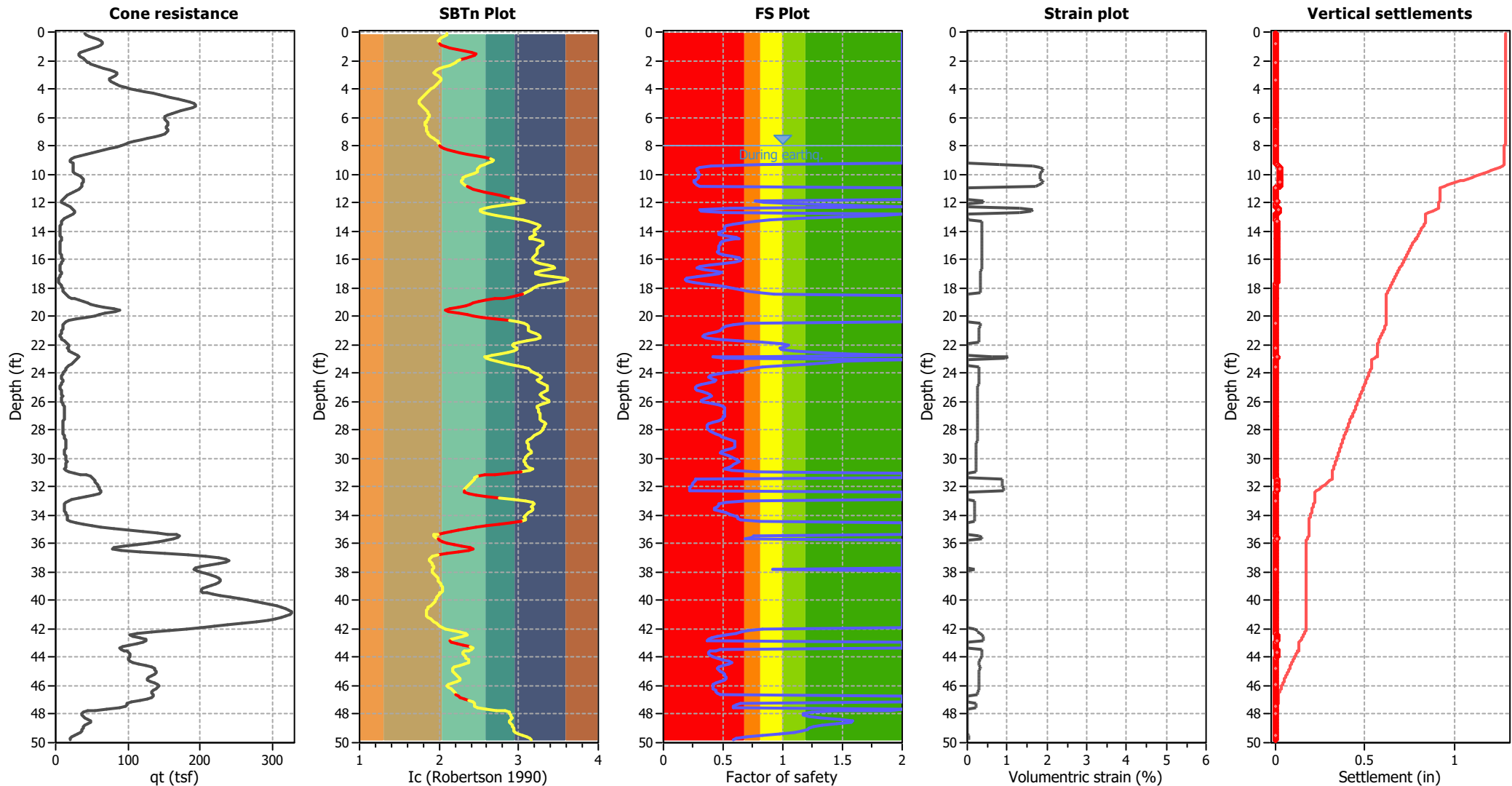
Abbreviations

FS: Calculated factor of safety for test point

F_L: 1 - FSw_z: Function value of the extend of soil liquefaction according to depthd_z: Layer thickness (ft)

LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

- q_c : Total cone resistance (cone resistance q_c corrected for pore water effects)
- I_c : Soil Behaviour Type Index
- FS: Calculated Factor of Safety against liquefaction
- Volumetric strain: Post-liquefaction volumetric strain

:: Post-earthquake settlement of dry sands ::												
Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _r (%)	Settle. (in)
0.10	2.09	76.26	1.41	107.26	23	513	0.59	0.001	0.00	13.69	0.00	0.000
0.20	2.09	78.57	1.40	110.29	24	527	0.59	0.001	0.00	13.69	0.00	0.000
0.30	2.07	85.47	1.38	117.58	25	558	0.59	0.002	0.00	13.69	0.00	0.000
0.40	2.03	97.76	1.33	130.28	27	607	0.59	0.002	0.00	13.69	0.00	0.000
0.50	2.00	109.39	1.31	143.10	30	657	0.59	0.003	0.00	13.69	0.00	0.000
0.60	1.99	117.75	1.30	153.38	32	701	0.59	0.003	0.00	13.69	0.00	0.000
0.70	2.00	121.94	1.31	159.37	33	731	0.59	0.003	0.00	13.69	0.00	0.000
0.80	2.01	121.74	1.32	160.23	33	739	0.59	0.004	0.00	13.69	0.00	0.000
0.90	2.03	117.30	1.34	156.76	0	0	0.59	0.000	0.00	13.69	0.00	0.000
1.00	2.07	108.64	1.38	150.41	0	0	0.59	0.000	0.00	13.69	0.00	0.000
1.10	2.14	97.69	1.49	145.34	0	0	0.59	0.000	0.00	13.69	0.00	0.000
1.20	2.23	85.75	1.68	144.23	0	0	0.59	0.000	0.00	13.69	0.00	0.000
1.30	2.32	74.06	1.99	147.46	0	0	0.59	0.000	0.00	13.69	0.00	0.000
1.40	2.40	63.99	2.40	153.47	0	0	0.59	0.000	0.00	13.69	0.00	0.000
1.50	2.46	58.07	2.72	157.77	0	0	0.59	0.000	0.00	13.69	0.00	0.000
1.60	2.45	58.25	2.68	156.13	0	0	0.59	0.000	0.00	13.69	0.00	0.000
1.70	2.40	62.80	2.37	148.82	0	0	0.59	0.000	0.00	13.69	0.00	0.000
1.80	2.33	69.15	2.04	140.85	0	0	0.59	0.000	0.00	13.69	0.00	0.000
1.90	2.27	74.90	1.81	135.65	0	0	0.59	0.000	0.00	13.69	0.00	0.000
2.00	2.23	79.46	1.70	134.91	0	0	0.59	0.000	0.00	13.69	0.00	0.000
2.10	2.21	82.83	1.65	136.83	31	652	0.59	0.017	0.01	13.69	0.01	0.000
2.20	2.20	86.40	1.62	140.13	32	670	0.59	0.017	0.01	13.69	0.01	0.000
2.30	2.18	91.77	1.56	143.13	32	688	0.59	0.017	0.01	13.69	0.01	0.000
2.40	2.13	100.32	1.46	146.87	32	707	0.59	0.017	0.01	13.69	0.01	0.000
2.50	2.07	112.27	1.37	154.22	33	732	0.59	0.017	0.01	13.69	0.01	0.000
2.60	2.01	126.14	1.31	165.65	35	763	0.59	0.017	0.01	13.69	0.01	0.000
2.70	1.96	139.60	1.28	178.70	37	800	0.59	0.016	0.01	13.69	0.01	0.000
2.80	1.94	150.41	1.26	190.22	39	838	0.59	0.016	0.01	13.69	0.01	0.000
2.90	1.94	157.01	1.26	198.22	40	871	0.59	0.015	0.01	13.69	0.01	0.000
3.00	1.95	158.26	1.27	201.38	41	894	0.59	0.015	0.01	13.69	0.01	0.000
3.10	1.98	154.13	1.29	199.01	41	900	0.59	0.016	0.01	13.69	0.01	0.000
3.20	2.01	146.95	1.31	193.19	40	891	0.59	0.017	0.01	13.69	0.01	0.000
3.30	2.03	141.31	1.33	188.08	40	876	0.59	0.018	0.01	13.69	0.01	0.000
3.40	2.03	140.88	1.33	187.49	39	873	0.59	0.019	0.01	13.69	0.01	0.000
3.50	2.01	145.07	1.32	191.33	40	885	0.59	0.019	0.01	13.69	0.01	0.000
3.60	2.00	151.43	1.30	197.41	41	903	0.59	0.019	0.01	13.69	0.01	0.000
3.70	1.98	158.68	1.29	204.53	42	923	0.59	0.019	0.01	13.69	0.01	0.000
3.80	1.95	168.13	1.27	213.96	44	950	0.59	0.019	0.01	13.69	0.01	0.000
3.90	1.93	179.99	1.25	225.79	46	983	0.59	0.018	0.01	13.69	0.01	0.000
4.00	1.90	193.28	1.24	239.52	48	1025	0.59	0.018	0.01	13.69	0.01	0.000
4.10	1.88	211.45	1.22	258.89	52	1091	0.59	0.016	0.01	13.69	0.00	0.000
4.20	1.86	232.46	1.21	281.19	56	1169	0.59	0.015	0.00	13.69	0.00	0.000
4.30	1.84	252.77	1.19	301.48	59	1238	0.59	0.014	0.00	13.69	0.00	0.000
4.40	1.82	268.92	1.17	315.65	61	1283	0.59	0.014	0.00	13.69	0.00	0.000
4.50	1.80	283.44	1.15	327.13	63	1320	0.59	0.014	0.00	13.69	0.00	0.000
4.60	1.78	300.11	1.13	340.10	65	1367	0.59	0.013	0.00	13.69	0.00	0.000
4.70	1.77	317.76	1.11	353.89	68	1422	0.59	0.013	0.00	13.69	0.00	0.000
4.80	1.76	332.27	1.10	364.92	70	1481	0.59	0.012	0.00	13.69	0.00	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
4.90	1.75	342.32	1.09	373.45	71	1538	0.59	0.012	0.00	13.69	0.00	0.000
5.00	1.76	348.87	1.09	381.42	73	1586	0.59	0.012	0.00	13.69	0.00	0.000
5.10	1.76	350.80	1.11	388.21	74	1624	0.59	0.012	0.00	13.69	0.00	0.000
5.20	1.78	348.06	1.13	392.78	75	1650	0.59	0.012	0.00	13.69	0.00	0.000
5.30	1.80	339.67	1.15	391.90	76	1656	0.59	0.012	0.00	13.69	0.00	0.000
5.40	1.82	326.69	1.18	384.28	75	1639	0.59	0.013	0.00	13.69	0.00	0.000
5.50	1.84	311.38	1.19	371.36	73	1602	0.59	0.013	0.00	13.69	0.00	0.000
5.60	1.85	297.27	1.20	357.63	70	1562	0.59	0.014	0.00	13.69	0.00	0.000
5.70	1.86	284.19	1.21	344.11	68	1522	0.59	0.015	0.00	13.69	0.00	0.000
5.80	1.87	272.12	1.22	330.85	66	1481	0.59	0.016	0.00	13.69	0.00	0.000
5.90	1.87	263.49	1.22	320.22	63	1447	0.58	0.017	0.00	13.69	0.00	0.000
6.00	1.86	258.74	1.21	313.09	62	1427	0.58	0.018	0.00	13.69	0.00	0.000
6.10	1.85	257.09	1.20	309.17	61	1421	0.58	0.018	0.00	13.69	0.00	0.000
6.20	1.84	255.63	1.20	305.65	60	1416	0.58	0.019	0.00	13.69	0.00	0.000
6.30	1.84	254.68	1.19	302.66	59	1413	0.58	0.019	0.01	13.69	0.00	0.000
6.40	1.83	253.52	1.18	299.93	59	1412	0.58	0.019	0.01	13.69	0.00	0.000
6.50	1.83	251.42	1.18	297.06	58	1410	0.58	0.020	0.01	13.69	0.00	0.000
6.60	1.83	248.22	1.18	293.82	57	1407	0.58	0.020	0.01	13.69	0.00	0.000
6.70	1.83	245.07	1.19	290.81	57	1406	0.58	0.021	0.01	13.69	0.01	0.000
6.80	1.84	243.41	1.19	289.23	57	1410	0.58	0.021	0.01	13.69	0.01	0.000
6.90	1.84	242.67	1.19	288.73	57	1420	0.58	0.021	0.01	13.69	0.01	0.000
7.00	1.84	241.69	1.19	288.69	57	1433	0.58	0.021	0.01	13.69	0.01	0.000
7.10	1.85	238.72	1.20	286.92	56	1440	0.58	0.022	0.01	13.69	0.01	0.000
7.20	1.86	232.63	1.21	281.89	56	1431	0.58	0.022	0.01	13.69	0.01	0.000
7.30	1.88	223.06	1.22	272.94	54	1405	0.58	0.023	0.01	13.69	0.01	0.000
7.40	1.90	210.20	1.24	260.26	52	1362	0.58	0.025	0.01	13.69	0.01	0.000
7.50	1.93	195.62	1.26	245.62	50	1311	0.58	0.027	0.01	13.69	0.01	0.000
7.60	1.95	181.65	1.27	231.24	47	1258	0.58	0.030	0.01	13.69	0.01	0.000
7.70	1.98	167.35	1.29	216.02	45	1197	0.58	0.034	0.01	13.69	0.01	0.000
7.80	2.00	154.92	1.30	201.92	42	1134	0.58	0.038	0.02	13.69	0.01	0.000
7.90	2.00	146.66	1.30	191.39	40	1084	0.58	0.043	0.02	13.69	0.02	0.000

Total estimated settlement: 0.00**Abbreviations**

Q_{tn}: Equivalent clean sand normalized cone resistance
 K_c: Fines correction factor
 Q_{tn,cs}: Post-liquefaction volumetric strain
 G_{max}: Small strain shear modulus
 CSR: Soil cyclic stress ratio
 γ: Cyclic shear strain
 e_{vol(15)}: Volumetric strain after 15 cycles
 N_c: Equivalent number of cycles
 e_v: Volumetric strain
 Settle.: Calculated settlement

:: Post-earthquake settlement due to soil liquefaction ::

Depth (ft)	Q _{tn,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	Q _{tn,cs}	FS	e _v (%)	DF	Settlement (in)
8.00	180.26	2.00	0.00	0.85	0.00	8.10	167.92	2.00	0.00	0.85	0.00
8.20	154.13	2.00	0.00	0.85	0.00	8.30	145.75	2.00	0.00	0.85	0.00
8.40	142.64	2.00	0.00	0.85	0.00	8.50	143.46	2.00	0.00	0.85	0.00
8.60	147.70	2.00	0.00	0.84	0.00	8.70	152.84	2.00	0.00	0.84	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
8.80	193.67	2.00	0.00	0.84	0.00	8.90	267.42	2.00	0.00	0.84	0.00
9.00	311.07	2.00	0.00	0.84	0.00	9.10	290.51	2.00	0.00	0.83	0.00
9.20	225.96	2.00	0.00	0.83	0.00	9.30	167.41	0.83	0.80	0.83	0.01
9.40	123.06	0.40	1.63	0.83	0.02	9.50	106.47	0.31	1.84	0.83	0.02
9.60	100.72	0.28	1.92	0.83	0.02	9.70	100.65	0.27	1.91	0.82	0.02
9.80	103.70	0.29	1.86	0.82	0.02	9.90	106.25	0.30	1.82	0.82	0.02
10.00	106.58	0.30	1.81	0.82	0.02	10.10	106.04	0.29	1.82	0.82	0.02
10.20	105.04	0.29	1.83	0.81	0.02	10.30	103.81	0.28	1.84	0.81	0.02
10.40	101.87	0.27	1.87	0.81	0.02	10.50	99.80	0.26	1.89	0.81	0.02
10.60	99.38	0.26	1.90	0.81	0.02	10.70	101.47	0.27	1.86	0.81	0.02
10.80	105.63	0.28	1.80	0.80	0.02	10.90	110.00	0.30	1.73	0.80	0.02
11.00	113.24	2.00	0.00	0.80	0.00	11.10	115.78	2.00	0.00	0.80	0.00
11.20	119.12	2.00	0.00	0.80	0.00	11.30	159.79	2.00	0.00	0.79	0.00
11.40	233.07	2.00	0.00	0.79	0.00	11.50	124.40	2.00	0.00	0.79	0.00
11.60	122.14	2.00	0.00	0.79	0.00	11.70	118.19	2.00	0.00	0.79	0.00
11.80	112.93	2.00	0.00	0.79	0.00	11.90	111.73	0.77	0.39	0.78	0.00
12.00	120.43	0.84	0.39	0.78	0.00	12.10	131.99	1.16	0.01	0.78	0.00
12.20	133.48	1.56	0.00	0.78	0.00	12.30	241.94	2.00	0.00	0.78	0.00
12.40	150.46	0.56	1.30	0.77	0.02	12.50	112.94	0.30	1.63	0.77	0.02
12.60	115.16	0.31	1.60	0.77	0.02	12.70	144.97	0.51	1.33	0.77	0.02
12.80	207.78	2.00	0.00	0.77	0.00	12.90	134.79	1.84	0.00	0.77	0.00
13.00	135.39	1.46	0.00	0.76	0.00	13.10	134.12	1.13	0.01	0.76	0.00
13.20	131.96	0.89	0.02	0.76	0.00	13.30	129.16	0.77	0.38	0.76	0.00
13.40	124.80	0.67	0.38	0.76	0.00	13.50	119.25	0.59	0.38	0.75	0.00
13.60	114.12	0.53	0.38	0.75	0.00	13.70	110.30	0.51	0.38	0.75	0.00
13.80	105.35	0.51	0.37	0.75	0.00	13.90	100.08	0.51	0.37	0.75	0.00
14.00	95.03	0.49	0.37	0.75	0.00	14.10	92.13	0.47	0.37	0.74	0.00
14.20	93.54	0.46	0.37	0.74	0.00	14.30	100.58	0.52	0.37	0.74	0.00
14.40	109.14	0.61	0.37	0.74	0.00	14.50	113.98	0.64	0.37	0.74	0.00
14.60	115.06	0.60	0.37	0.73	0.00	14.70	115.27	0.52	0.37	0.73	0.00
14.80	116.57	0.48	0.37	0.73	0.00	14.90	116.52	0.47	0.36	0.73	0.00
15.00	113.05	0.47	0.36	0.73	0.00	15.10	108.04	0.47	0.36	0.73	0.00
15.20	103.61	0.46	0.36	0.72	0.00	15.30	100.27	0.46	0.36	0.72	0.00
15.40	97.93	0.46	0.36	0.72	0.00	15.50	97.31	0.46	0.36	0.72	0.00
15.60	99.43	0.46	0.36	0.72	0.00	15.70	106.52	0.50	0.36	0.71	0.00
15.80	116.20	0.57	0.36	0.71	0.00	15.90	125.19	0.63	0.36	0.71	0.00
16.00	130.36	0.65	0.35	0.71	0.00	16.10	131.94	0.65	0.35	0.71	0.00
16.20	128.33	0.60	0.35	0.71	0.00	16.30	120.04	0.50	0.35	0.70	0.00
16.40	107.79	0.39	0.35	0.70	0.00	16.50	97.08	0.31	0.35	0.70	0.00
16.60	92.57	0.28	0.35	0.70	0.00	16.70	96.33	0.33	0.35	0.70	0.00
16.80	101.72	0.42	0.35	0.69	0.00	16.90	103.38	0.48	0.35	0.69	0.00
17.00	99.77	0.47	0.35	0.69	0.00	17.10	93.88	0.38	0.34	0.69	0.00
17.20	87.21	0.27	0.34	0.69	0.00	17.30	81.29	0.20	0.34	0.69	0.00
17.40	78.90	0.18	0.34	0.68	0.00	17.50	79.45	0.20	0.34	0.68	0.00
17.60	85.35	0.26	0.34	0.68	0.00	17.70	94.43	0.34	0.34	0.68	0.00
17.80	106.39	0.45	0.34	0.68	0.00	17.90	115.24	0.53	0.34	0.67	0.00
18.00	121.60	0.59	0.34	0.67	0.00	18.10	127.56	0.64	0.34	0.67	0.00
18.20	134.61	0.71	0.33	0.67	0.00	18.30	142.78	0.81	0.33	0.67	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
18.40	149.44	0.92	0.01	0.67	0.00	18.50	154.33	2.00	0.00	0.66	0.00
18.60	155.98	2.00	0.00	0.66	0.00	18.70	153.88	2.00	0.00	0.66	0.00
18.80	148.07	2.00	0.00	0.66	0.00	18.90	194.85	2.00	0.00	0.66	0.00
19.00	133.67	2.00	0.00	0.65	0.00	19.10	131.93	2.00	0.00	0.65	0.00
19.20	133.34	2.00	0.00	0.65	0.00	19.30	134.36	2.00	0.00	0.65	0.00
19.40	134.27	2.00	0.00	0.65	0.00	19.50	137.72	2.00	0.00	0.65	0.00
19.60	141.30	2.00	0.00	0.64	0.00	19.70	134.56	2.00	0.00	0.64	0.00
19.80	134.09	2.00	0.00	0.64	0.00	19.90	148.22	2.00	0.00	0.64	0.00
20.00	158.59	2.00	0.00	0.64	0.00	20.10	173.72	2.00	0.00	0.63	0.00
20.20	146.98	2.00	0.00	0.63	0.00	20.30	136.07	2.00	0.00	0.63	0.00
20.40	128.60	2.00	0.00	0.63	0.00	20.50	119.45	0.69	0.31	0.63	0.00
20.60	109.61	0.59	0.31	0.63	0.00	20.70	101.33	0.53	0.31	0.62	0.00
20.80	96.57	0.49	0.31	0.62	0.00	20.90	95.21	0.49	0.31	0.62	0.00
21.00	93.93	0.48	0.31	0.62	0.00	21.10	91.14	0.44	0.31	0.62	0.00
21.20	87.10	0.38	0.31	0.61	0.00	21.30	83.63	0.34	0.31	0.61	0.00
21.40	83.80	0.32	0.31	0.61	0.00	21.50	90.29	0.36	0.30	0.61	0.00
21.60	104.05	0.46	0.30	0.61	0.00	21.70	120.34	0.63	0.30	0.61	0.00
21.80	133.07	0.83	0.30	0.60	0.00	21.90	139.48	0.99	0.01	0.60	0.00
22.00	141.48	1.05	0.01	0.60	0.00	22.10	142.78	1.02	0.01	0.60	0.00
22.20	145.89	0.98	0.01	0.60	0.00	22.30	150.49	0.99	0.01	0.59	0.00
22.40	154.82	1.09	0.01	0.59	0.00	22.50	155.60	1.28	0.00	0.59	0.00
22.60	150.32	1.53	0.00	0.59	0.00	22.70	268.56	2.00	0.00	0.59	0.00
22.80	178.05	0.70	0.63	0.59	0.01	22.90	143.79	0.41	1.01	0.58	0.01
23.00	157.50	0.51	0.94	0.58	0.01	23.10	217.72	2.00	0.00	0.58	0.00
23.20	135.01	1.52	0.00	0.58	0.00	23.30	143.34	1.39	0.00	0.58	0.00
23.40	147.53	1.23	0.00	0.57	0.00	23.50	147.32	1.02	0.01	0.57	0.00
23.60	146.07	0.83	0.29	0.57	0.00	23.70	145.74	0.73	0.28	0.57	0.00
23.80	142.23	0.68	0.28	0.57	0.00	23.90	133.35	0.62	0.28	0.57	0.00
24.00	120.18	0.53	0.28	0.56	0.00	24.10	109.01	0.44	0.28	0.56	0.00
24.20	102.84	0.39	0.28	0.56	0.00	24.30	102.28	0.38	0.28	0.56	0.00
24.40	105.43	0.40	0.28	0.56	0.00	24.50	108.26	0.43	0.28	0.55	0.00
24.60	106.67	0.42	0.28	0.55	0.00	24.70	100.75	0.37	0.28	0.55	0.00
24.80	93.07	0.32	0.27	0.55	0.00	24.90	86.47	0.28	0.27	0.55	0.00
25.00	83.52	0.27	0.27	0.55	0.00	25.10	83.73	0.27	0.27	0.54	0.00
25.20	87.60	0.28	0.27	0.54	0.00	25.30	94.30	0.32	0.27	0.54	0.00
25.40	100.93	0.37	0.27	0.54	0.00	25.50	105.30	0.39	0.27	0.54	0.00
25.60	107.36	0.40	0.27	0.53	0.00	25.70	107.22	0.38	0.27	0.53	0.00
25.80	105.07	0.35	0.27	0.53	0.00	25.90	104.06	0.32	0.26	0.53	0.00
26.00	107.69	0.34	0.26	0.53	0.00	26.10	115.94	0.40	0.26	0.53	0.00
26.20	123.61	0.46	0.26	0.52	0.00	26.30	128.26	0.50	0.26	0.52	0.00
26.40	130.62	0.52	0.26	0.52	0.00	26.50	132.04	0.52	0.26	0.52	0.00
26.60	133.25	0.51	0.26	0.52	0.00	26.70	134.20	0.51	0.26	0.51	0.00
26.80	135.04	0.51	0.26	0.51	0.00	26.90	135.97	0.51	0.26	0.51	0.00
27.00	136.64	0.51	0.25	0.51	0.00	27.10	136.88	0.50	0.25	0.51	0.00
27.20	136.47	0.50	0.25	0.51	0.00	27.30	134.41	0.49	0.25	0.50	0.00
27.40	129.24	0.46	0.25	0.50	0.00	27.50	121.84	0.42	0.25	0.50	0.00
27.60	114.51	0.38	0.25	0.50	0.00	27.70	109.46	0.36	0.25	0.50	0.00
27.80	106.68	0.36	0.25	0.49	0.00	27.90	106.03	0.37	0.25	0.49	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
28.00	107.03	0.38	0.25	0.49	0.00	28.10	108.37	0.39	0.24	0.49	0.00
28.20	110.43	0.41	0.24	0.49	0.00	28.30	112.26	0.44	0.24	0.49	0.00
28.40	113.72	0.47	0.24	0.48	0.00	28.50	114.46	0.49	0.24	0.48	0.00
28.60	116.48	0.53	0.24	0.48	0.00	28.70	118.95	0.57	0.24	0.48	0.00
28.80	121.06	0.59	0.24	0.48	0.00	28.90	122.36	0.60	0.24	0.47	0.00
29.00	123.50	0.60	0.24	0.47	0.00	29.10	123.61	0.59	0.24	0.47	0.00
29.20	122.04	0.59	0.23	0.47	0.00	29.30	118.22	0.57	0.23	0.47	0.00
29.40	112.62	0.53	0.23	0.47	0.00	29.50	107.30	0.49	0.23	0.46	0.00
29.60	104.58	0.47	0.23	0.46	0.00	29.70	106.96	0.51	0.23	0.46	0.00
29.80	110.50	0.55	0.23	0.46	0.00	29.90	113.64	0.57	0.23	0.46	0.00
30.00	116.63	0.60	0.23	0.45	0.00	30.10	118.88	0.62	0.23	0.45	0.00
30.20	119.91	0.64	0.23	0.45	0.00	30.30	118.41	0.61	0.22	0.45	0.00
30.40	116.67	0.59	0.22	0.45	0.00	30.50	115.77	0.58	0.22	0.45	0.00
30.60	115.52	0.54	0.22	0.44	0.00	30.70	117.55	0.51	0.22	0.44	0.00
30.80	125.41	0.57	0.22	0.44	0.00	30.90	136.92	0.78	0.22	0.44	0.00
31.00	143.72	2.00	0.00	0.44	0.00	31.10	140.06	2.00	0.00	0.43	0.00
31.20	164.65	2.00	0.00	0.43	0.00	31.30	120.67	2.00	0.00	0.43	0.00
31.40	118.39	2.00	0.00	0.43	0.00	31.50	119.70	0.26	0.86	0.43	0.01
31.60	119.29	0.26	0.86	0.43	0.01	31.70	116.57	0.25	0.87	0.42	0.01
31.80	114.90	0.24	0.88	0.42	0.01	31.90	114.60	0.24	0.88	0.42	0.01
32.00	113.24	0.24	0.88	0.42	0.01	32.10	109.98	0.23	0.90	0.42	0.01
32.20	107.01	0.21	0.92	0.41	0.01	32.30	107.29	0.22	0.91	0.41	0.01
32.40	110.91	2.00	0.00	0.41	0.00	32.50	117.14	2.00	0.00	0.41	0.00
32.60	125.85	2.00	0.00	0.41	0.00	32.70	193.64	2.00	0.00	0.41	0.00
32.80	140.82	2.00	0.00	0.40	0.00	32.90	139.16	2.00	0.00	0.40	0.00
33.00	131.21	0.68	0.20	0.40	0.00	33.10	120.88	0.53	0.20	0.40	0.00
33.20	111.78	0.46	0.20	0.40	0.00	33.30	106.22	0.46	0.20	0.39	0.00
33.40	101.98	0.46	0.20	0.39	0.00	33.50	98.61	0.42	0.20	0.39	0.00
33.60	100.53	0.43	0.19	0.39	0.00	33.70	105.05	0.48	0.19	0.39	0.00
33.80	108.34	0.52	0.19	0.39	0.00	33.90	109.90	0.55	0.19	0.38	0.00
34.00	112.22	0.58	0.19	0.38	0.00	34.10	116.39	0.62	0.19	0.38	0.00
34.20	119.70	0.62	0.19	0.38	0.00	34.30	125.97	0.64	0.19	0.38	0.00
34.40	141.78	0.81	0.19	0.37	0.00	34.50	158.74	2.00	0.00	0.37	0.00
34.60	163.38	2.00	0.00	0.37	0.00	34.70	220.98	2.00	0.00	0.37	0.00
34.80	143.11	2.00	0.00	0.37	0.00	34.90	142.02	2.00	0.00	0.37	0.00
35.00	147.48	2.00	0.00	0.36	0.00	35.10	155.49	2.00	0.00	0.36	0.00
35.20	164.43	2.00	0.00	0.36	0.00	35.30	173.87	2.00	0.00	0.36	0.00
35.40	182.05	2.00	0.00	0.36	0.00	35.50	186.30	0.76	0.29	0.35	0.00
35.60	184.86	0.74	0.36	0.35	0.00	35.70	179.62	0.69	0.38	0.35	0.00
35.80	171.55	2.00	0.00	0.35	0.00	35.90	162.10	2.00	0.00	0.35	0.00
36.00	152.06	2.00	0.00	0.35	0.00	36.10	145.72	2.00	0.00	0.34	0.00
36.20	146.32	2.00	0.00	0.34	0.00	36.30	153.12	2.00	0.00	0.34	0.00
36.40	161.10	2.00	0.00	0.34	0.00	36.50	164.17	2.00	0.00	0.34	0.00
36.60	166.66	2.00	0.00	0.33	0.00	36.70	178.50	2.00	0.00	0.33	0.00
36.80	199.49	2.00	0.00	0.33	0.00	36.90	218.63	2.00	0.00	0.33	0.00
37.00	234.36	2.00	0.00	0.33	0.00	37.10	244.58	2.00	0.00	0.33	0.00
37.20	248.10	2.00	0.00	0.32	0.00	37.30	243.25	2.00	0.00	0.32	0.00
37.40	233.40	2.00	0.00	0.32	0.00	37.50	221.78	2.00	0.00	0.32	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
37.60	210.53	2.00	0.00	0.32	0.00	37.70	202.21	2.00	0.00	0.31	0.00
37.80	198.83	0.91	0.18	0.31	0.00	37.90	201.20	2.00	0.00	0.31	0.00
38.00	208.20	2.00	0.00	0.31	0.00	38.10	217.04	2.00	0.00	0.31	0.00
38.20	225.56	2.00	0.00	0.31	0.00	38.30	232.42	2.00	0.00	0.30	0.00
38.40	237.27	2.00	0.00	0.30	0.00	38.50	240.44	2.00	0.00	0.30	0.00
38.60	241.49	2.00	0.00	0.30	0.00	38.70	239.89	2.00	0.00	0.30	0.00
38.80	235.81	2.00	0.00	0.29	0.00	38.90	230.49	2.00	0.00	0.29	0.00
39.00	225.14	2.00	0.00	0.29	0.00	39.10	220.27	2.00	0.00	0.29	0.00
39.20	216.67	2.00	0.00	0.29	0.00	39.30	215.07	2.00	0.00	0.29	0.00
39.40	216.08	2.00	0.00	0.28	0.00	39.50	219.76	2.00	0.00	0.28	0.00
39.60	226.10	2.00	0.00	0.28	0.00	39.70	235.07	2.00	0.00	0.28	0.00
39.80	246.15	2.00	0.00	0.28	0.00	39.90	258.19	2.00	0.00	0.27	0.00
40.00	269.15	2.00	0.00	0.27	0.00	40.10	278.88	2.00	0.00	0.27	0.00
40.20	286.91	2.00	0.00	0.27	0.00	40.30	293.69	2.00	0.00	0.27	0.00
40.40	298.50	2.00	0.00	0.27	0.00	40.50	301.93	2.00	0.00	0.26	0.00
40.60	305.08	2.00	0.00	0.26	0.00	40.70	308.25	2.00	0.00	0.26	0.00
40.80	310.12	2.00	0.00	0.26	0.00	40.90	309.42	2.00	0.00	0.26	0.00
41.00	306.29	2.00	0.00	0.25	0.00	41.10	302.19	2.00	0.00	0.25	0.00
41.20	297.74	2.00	0.00	0.25	0.00	41.30	292.57	2.00	0.00	0.25	0.00
41.40	284.54	2.00	0.00	0.25	0.00	41.50	272.15	2.00	0.00	0.25	0.00
41.60	255.30	2.00	0.00	0.24	0.00	41.70	236.47	2.00	0.00	0.24	0.00
41.80	219.18	2.00	0.00	0.24	0.00	41.90	203.34	2.00	0.00	0.24	0.00
42.00	189.41	0.83	0.19	0.24	0.00	42.10	178.56	0.71	0.25	0.23	0.00
42.20	172.42	0.65	0.26	0.23	0.00	42.30	167.43	0.60	0.33	0.23	0.00
42.40	158.76	0.53	0.37	0.23	0.00	42.50	148.30	0.45	0.38	0.23	0.00
42.60	141.26	0.40	0.40	0.23	0.00	42.70	137.62	0.38	0.40	0.22	0.00
42.80	135.07	0.36	0.41	0.22	0.00	42.90	132.89	2.00	0.00	0.22	0.00
43.00	133.70	2.00	0.00	0.22	0.00	43.10	139.79	2.00	0.00	0.22	0.00
43.20	149.17	2.00	0.00	0.21	0.00	43.30	154.44	2.00	0.00	0.21	0.00
43.40	152.17	0.48	0.35	0.21	0.00	43.50	145.47	0.43	0.36	0.21	0.00
43.60	139.74	0.40	0.37	0.21	0.00	43.70	136.98	0.38	0.37	0.21	0.00
43.80	137.20	0.38	0.37	0.20	0.00	43.90	139.40	0.39	0.36	0.20	0.00
44.00	142.77	0.42	0.35	0.20	0.00	44.10	147.36	0.45	0.34	0.20	0.00
44.20	153.26	0.49	0.32	0.20	0.00	44.30	159.70	0.55	0.31	0.19	0.00
44.40	163.08	0.58	0.29	0.19	0.00	44.50	160.41	0.55	0.29	0.19	0.00
44.60	153.87	0.50	0.31	0.19	0.00	44.70	148.70	0.46	0.32	0.19	0.00
44.80	146.92	0.45	0.32	0.19	0.00	44.90	148.17	0.46	0.31	0.18	0.00
45.00	151.12	0.48	0.30	0.18	0.00	45.10	153.78	0.50	0.30	0.18	0.00
45.20	155.09	0.51	0.29	0.18	0.00	45.30	155.47	0.52	0.29	0.18	0.00
45.40	155.87	0.52	0.28	0.17	0.00	45.50	155.93	0.52	0.28	0.17	0.00
45.60	153.97	0.51	0.28	0.17	0.00	45.70	149.85	0.48	0.28	0.17	0.00
45.80	145.28	0.44	0.29	0.17	0.00	45.90	141.93	0.42	0.29	0.17	0.00
46.00	140.37	0.41	0.29	0.16	0.00	46.10	140.33	0.41	0.29	0.16	0.00
46.20	141.79	0.42	0.28	0.16	0.00	46.30	143.75	0.43	0.27	0.16	0.00
46.40	144.70	0.44	0.27	0.16	0.00	46.50	145.76	0.45	0.27	0.15	0.00
46.60	149.12	0.47	0.26	0.15	0.00	46.70	154.91	2.00	0.00	0.15	0.00
46.80	161.37	2.00	0.00	0.15	0.00	46.90	165.91	2.00	0.00	0.15	0.00
47.00	169.55	2.00	0.00	0.15	0.00	47.10	170.35	2.00	0.00	0.14	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
47.20	168.63	0.65	0.20	0.14	0.00	47.30	164.47	0.61	0.21	0.14	0.00
47.40	161.58	0.58	0.21	0.14	0.00	47.50	161.33	0.58	0.21	0.14	0.00
47.60	229.98	2.00	0.00	0.13	0.00	47.70	160.21	1.90	0.00	0.13	0.00
47.80	153.58	1.46	0.00	0.13	0.00	47.90	146.31	1.24	0.00	0.13	0.00
48.00	141.01	1.18	0.00	0.13	0.00	48.10	141.08	1.17	0.00	0.13	0.00
48.20	149.41	1.22	0.00	0.12	0.00	48.30	165.15	1.32	0.00	0.12	0.00
48.40	179.87	1.47	0.00	0.12	0.00	48.50	185.63	1.59	0.00	0.12	0.00
48.60	182.33	1.58	0.00	0.12	0.00	48.70	173.95	1.45	0.00	0.11	0.00
48.80	166.43	1.33	0.00	0.11	0.00	48.90	160.86	1.26	0.00	0.11	0.00
49.00	156.88	1.22	0.00	0.11	0.00	49.10	153.90	1.20	0.00	0.11	0.00
49.20	150.91	1.16	0.00	0.11	0.00	49.30	147.20	1.10	0.00	0.10	0.00
49.40	140.97	0.98	0.00	0.10	0.00	49.50	132.46	0.82	0.05	0.10	0.00
49.60	123.51	0.69	0.05	0.10	0.00	49.70	117.01	0.61	0.05	0.10	0.00
49.80	113.79	0.59	0.05	0.09	0.00						

Total estimated settlement: 1.28**Abbreviations**

$Q_{tn,cs}$:	Equivalent clean sand normalized cone resistance
FS:	Factor of safety against liquefaction
e_v (%):	Post-liquefaction volumetric strain
DF:	e_v depth weighting factor
Settlement:	Calculated settlement

:: Strength loss calculation (Robertson (2009)) ::

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.10	40.35	76.26	1.41	107.26	2.09	0.76	0.76
0.20	41.58	78.57	1.40	110.29	2.09	0.77	0.77
0.30	45.23	85.47	1.38	117.58	2.07	0.78	0.78
0.40	51.74	97.76	1.33	130.28	2.03	0.80	0.80
0.50	57.90	109.39	1.31	143.10	2.00	0.82	0.82
0.60	62.33	117.75	1.30	153.38	1.99	0.83	0.83
0.70	64.56	121.94	1.31	159.37	2.00	0.84	0.84
0.80	64.46	121.74	1.32	160.23	2.01	0.84	0.84
0.90	62.11	117.30	1.34	156.76	2.03	0.84	0.84
1.00	57.54	108.64	1.38	150.41	2.07	0.83	0.83
1.10	51.75	97.69	1.49	145.34	2.14	0.82	0.82
1.20	45.44	85.75	1.68	144.23	2.23	0.82	0.82
1.30	39.26	74.06	1.99	147.46	2.32	0.82	0.82
1.40	33.94	63.99	2.40	153.47	2.40	0.83	0.83
1.50	30.81	58.07	2.72	157.77	2.46	0.84	0.84
1.60	30.91	58.25	2.68	156.13	2.45	0.84	0.84
1.70	33.33	62.80	2.37	148.82	2.40	0.83	0.83
1.80	36.69	69.15	2.04	140.85	2.33	0.81	0.81
1.90	39.74	74.90	1.81	135.65	2.27	0.81	0.81
2.00	42.16	79.46	1.70	134.91	2.23	0.81	0.81
2.10	43.95	82.83	1.65	136.83	2.21	0.81	0.81
2.20	45.84	86.40	1.62	140.13	2.20	0.81	0.81
2.30	48.69	91.77	1.56	143.13	2.18	0.82	0.82
2.40	53.22	100.32	1.46	146.87	2.13	0.82	0.82
2.50	59.55	112.27	1.37	154.22	2.07	0.83	0.83
2.60	66.89	126.14	1.31	165.65	2.01	0.85	0.85
2.70	74.02	139.60	1.28	178.70	1.96	0.86	0.86
2.80	79.74	150.41	1.26	190.22	1.94	0.88	0.88
2.90	83.24	157.01	1.26	198.22	1.94	0.88	0.88
3.00	83.91	158.26	1.27	201.38	1.95	0.89	0.89
3.10	81.73	154.13	1.29	199.01	1.98	0.89	0.89
3.20	77.93	146.95	1.31	193.19	2.01	0.88	0.88
3.30	74.96	141.31	1.33	188.08	2.03	0.87	0.87
3.40	74.74	140.88	1.33	187.49	2.03	0.87	0.87
3.50	76.96	145.07	1.32	191.33	2.01	0.88	0.88
3.60	80.33	151.43	1.30	197.41	2.00	0.88	0.88
3.70	84.17	158.68	1.29	204.53	1.98	0.89	0.89
3.80	89.18	168.13	1.27	213.96	1.95	0.90	0.90
3.90	95.46	179.99	1.25	225.79	1.93	0.91	0.91
4.00	102.50	193.28	1.24	239.52	1.90	0.93	0.93
4.10	112.12	211.45	1.22	258.89	1.88	0.94	0.94
4.20	123.24	232.46	1.21	281.19	1.86	0.96	0.96
4.30	133.99	252.77	1.19	301.48	1.84	0.98	0.98
4.40	142.54	268.92	1.17	315.65	1.82	0.99	0.99
4.50	150.23	283.44	1.15	327.13	1.80	1.00	1.00
4.60	159.06	300.11	1.13	340.10	1.78	1.01	1.01
4.70	168.40	317.76	1.11	353.89	1.77	1.02	1.02
4.80	177.80	332.27	1.10	364.92	1.76	1.02	1.02

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
4.90	185.66	342.32	1.09	373.45	1.75	1.03	1.03
5.00	191.18	348.87	1.09	381.42	1.76	1.04	1.04
5.10	193.58	350.80	1.11	388.21	1.76	1.04	1.04
5.20	192.78	348.06	1.13	392.78	1.78	1.04	1.04
5.30	188.43	339.67	1.15	391.90	1.80	1.04	1.04
5.40	181.46	326.69	1.18	384.28	1.82	1.04	1.04
5.50	173.48	311.38	1.19	371.36	1.84	1.03	1.03
5.60	166.49	297.27	1.20	357.63	1.85	1.02	1.02
5.70	160.17	284.19	1.21	344.11	1.86	1.01	1.01
5.80	154.54	272.12	1.22	330.85	1.87	1.00	1.00
5.90	151.20	263.49	1.22	320.22	1.87	0.99	0.99
6.00	150.36	258.74	1.21	313.09	1.86	0.99	0.99
6.10	151.58	257.09	1.20	309.17	1.85	0.98	0.98
6.20	152.65	255.63	1.20	305.65	1.84	0.98	0.98
6.30	153.98	254.68	1.19	302.66	1.84	0.98	0.98
6.40	155.02	253.52	1.18	299.93	1.83	0.98	0.98
6.50	155.21	251.42	1.18	297.06	1.83	0.98	0.98
6.60	154.44	248.22	1.18	293.82	1.83	0.97	0.97
6.70	153.63	245.07	1.19	290.81	1.83	0.97	0.97
6.80	153.80	243.41	1.19	289.23	1.84	0.97	0.97
6.90	154.54	242.67	1.19	288.73	1.84	0.97	0.97
7.00	154.90	241.69	1.19	288.69	1.84	0.97	0.97
7.10	153.81	238.72	1.20	286.92	1.85	0.97	0.97
7.20	150.50	232.63	1.21	281.89	1.86	0.96	0.96
7.30	144.74	223.06	1.22	272.94	1.88	0.96	0.96
7.40	136.62	210.20	1.24	260.26	1.90	0.94	0.94
7.50	127.15	195.62	1.26	245.62	1.93	0.93	0.93
7.60	118.12	181.65	1.27	231.24	1.95	0.92	0.92
7.70	108.93	167.35	1.29	216.02	1.98	0.90	0.90
7.80	101.20	154.92	1.30	201.92	2.00	0.89	0.89
7.90	96.54	146.66	1.30	191.39	2.00	0.88	0.88
8.00	91.21	137.66	1.31	180.26	2.00	0.86	0.86
8.10	83.87	126.67	1.33	167.92	2.02	0.85	0.85
8.20	73.95	112.49	1.37	154.13	2.06	0.83	0.83
8.30	65.66	100.90	1.44	145.75	2.12	0.82	0.82
8.40	58.44	90.94	1.57	142.64	2.18	0.82	0.82
8.50	50.44	79.84	1.80	143.46	2.26	0.82	0.82
8.60	41.90	67.67	2.18	147.70	2.36	0.82	0.82
8.70	33.76	55.64	2.75	152.84	2.46	0.83	0.83
8.80	26.20	43.97	3.49	153.38	2.57	0.88	0.88
8.90	21.14	35.90	4.21	151.04	2.65	0.95	0.95
9.00	19.30	32.88	4.58	150.74	2.69	0.99	0.99
9.10	20.38	34.45	4.40	151.53	2.67	0.97	0.97
9.20	22.74	37.82	3.89	147.04	2.62	0.91	0.91
9.30	23.71	38.80	3.46	134.37	2.57	0.85	0.85
9.40	23.62	38.05	3.13	119.08	2.52	0.79	0.79
9.50	22.74	36.21	2.94	106.47	2.49	0.76	0.76
9.60	22.51	35.54	2.83	100.72	2.48	0.75	0.75

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.70	22.82	35.87	2.81	100.65	2.47	0.75	0.75
9.80	23.67	37.07	2.80	103.70	2.47	0.75	0.75
9.90	26.17	40.64	2.61	106.25	2.44	0.76	0.76
10.00	29.98	45.91	2.32	106.58	2.39	0.76	0.76
10.10	33.87	51.13	2.07	106.04	2.34	0.76	0.76
10.20	36.11	53.96	1.95	105.04	2.31	0.76	0.76
10.30	36.87	54.74	1.90	103.81	2.29	0.76	0.76
10.40	37.04	54.68	1.86	101.87	2.28	0.75	0.75
10.50	37.04	54.38	1.84	99.80	2.28	0.75	0.75
10.60	36.91	54.01	1.84	99.38	2.28	0.75	0.75
10.70	36.31	53.16	1.91	101.47	2.30	0.75	0.75
10.80	35.51	52.14	2.03	105.63	2.33	0.76	0.76
10.90	34.67	51.05	2.15	110.00	2.36	0.77	0.77
11.00	33.49	49.41	2.29	113.24	2.38	0.77	0.77
11.10	30.97	45.89	2.52	115.78	2.43	0.78	0.78
11.20	27.24	40.67	2.93	119.12	2.49	0.78	0.78
11.30	22.91	34.54	3.55	122.60	2.58	0.84	0.84
11.40	18.96	28.83	4.33	124.91	2.66	0.92	0.92
11.50	15.45	23.64	5.26	124.40	2.75	0.79	0.79
11.60	12.82	19.66	6.21	122.14	2.83	0.79	0.79
11.70	10.68	16.37	7.22	118.19	2.90	0.78	0.78
11.80	8.66	13.12	8.60	112.93	2.99	0.77	0.77
11.90	7.50	11.15	10.02	111.73	3.07	0.43	0.80
12.00	8.19	12.24	9.84	120.43	3.06	0.56	0.87
12.10	11.14	16.97	7.78	131.99	2.94	0.80	0.80
12.20	15.23	22.88	5.83	133.48	2.80	0.80	0.80
12.30	19.15	28.22	4.43	124.86	2.67	0.93	0.93
12.40	21.99	31.83	3.58	113.85	2.58	0.83	0.83
12.50	24.28	34.72	3.14	108.89	2.52	0.77	0.77
12.60	25.49	36.34	3.11	112.93	2.52	0.77	0.77
12.70	25.26	36.13	3.38	121.95	2.55	0.82	0.82
12.80	22.79	32.82	3.97	130.28	2.62	0.90	0.90
12.90	19.03	27.60	4.88	134.79	2.72	0.81	0.81
13.00	15.05	21.95	6.17	135.39	2.82	0.81	0.81
13.10	11.64	17.00	7.89	134.12	2.95	0.80	0.80
13.20	9.43	13.47	9.79	131.96	3.06	0.72	0.96
13.30	8.27	11.61	11.13	129.16	3.13	0.72	0.83
13.40	7.40	10.22	12.22	124.80	3.18	0.64	0.73
13.50	6.61	8.94	13.34	119.25	3.23	0.53	0.64
13.60	6.06	8.06	14.16	114.12	3.26	0.51	0.58
13.70	5.98	7.90	13.96	110.30	3.25	0.47	0.56
13.80	5.98	7.87	13.39	105.35	3.23	0.42	0.56
13.90	5.98	7.83	12.78	100.08	3.20	0.37	0.56
14.00	5.83	7.57	12.55	95.03	3.19	0.33	0.54
14.10	5.63	7.24	12.72	92.13	3.20	0.29	0.52
14.20	5.64	7.22	12.95	93.54	3.21	0.30	0.52
14.30	6.24	8.10	12.42	100.58	3.19	0.37	0.58
14.40	7.17	9.47	11.53	109.14	3.14	0.48	0.68

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
14.50	7.57	10.02	11.38	113.98	3.14	0.56	0.72
14.60	7.18	9.39	12.25	115.06	3.18	0.52	0.67
14.70	6.44	8.26	13.95	115.27	3.25	0.49	0.59
14.80	6.04	7.63	15.27	116.57	3.30	0.53	0.55
14.90	5.98	7.51	15.52	116.52	3.31	0.54	0.54
15.00	5.98	7.47	15.13	113.05	3.30	0.49	0.53
15.10	5.98	7.44	14.52	108.04	3.27	0.43	0.53
15.20	5.98	7.41	13.98	103.61	3.25	0.40	0.53
15.30	5.98	7.38	13.59	100.27	3.24	0.37	0.53
15.40	5.98	7.35	13.33	97.93	3.23	0.35	0.52
15.50	5.98	7.32	13.30	97.31	3.22	0.34	0.52
15.60	6.05	7.40	13.44	99.43	3.23	0.36	0.53
15.70	6.60	8.15	13.06	106.52	3.21	0.40	0.58
15.80	7.40	9.26	12.54	116.20	3.19	0.54	0.66
15.90	8.12	10.25	12.21	125.19	3.18	0.66	0.73
16.00	8.37	10.57	12.33	130.36	3.18	0.70	0.76
16.10	8.36	10.52	12.54	131.94	3.19	0.72	0.75
16.20	7.83	9.73	13.19	128.33	3.22	0.70	0.69
16.30	6.82	8.26	14.53	120.04	3.27	0.56	0.59
16.40	5.50	6.37	16.91	107.79	3.36	0.42	0.46
16.50	4.57	5.04	19.26	97.08	3.44	0.32	0.36
16.60	4.32	4.66	19.86	92.57	3.46	0.27	0.33
16.70	4.93	5.50	17.52	96.33	3.38	0.31	0.39
16.80	5.99	6.95	14.63	101.72	3.28	0.41	0.50
16.90	6.79	8.03	12.87	103.38	3.21	0.43	0.57
17.00	6.62	7.76	12.86	99.77	3.21	0.38	0.55
17.10	5.62	6.35	14.78	93.88	3.28	0.32	0.45
17.20	4.35	4.58	19.04	87.21	3.43	0.26	0.33
17.30	3.44	3.32	24.47	81.29	3.58	0.20	0.24
17.40	3.24	3.04	25.98	78.90	3.62	0.19	0.22
17.50	3.46	3.32	23.95	79.45	3.57	0.21	0.24
17.60	4.20	4.31	19.81	85.35	3.46	0.22	0.31
17.70	5.21	5.66	16.67	94.43	3.35	0.31	0.40
17.80	6.62	7.55	14.10	106.39	3.26	0.42	0.54
17.90	7.68	8.94	12.89	115.24	3.21	0.55	0.64
18.00	8.46	9.95	12.22	121.60	3.18	0.59	0.71
18.10	9.19	10.90	11.71	127.56	3.15	0.64	0.78
18.20	10.11	12.08	11.15	134.61	3.13	0.77	0.86
18.30	11.39	13.73	10.40	142.78	3.09	0.87	0.98
18.40	12.95	15.75	9.49	149.44	3.04	1.00	1.13
18.50	15.09	18.52	8.33	154.33	2.97	0.83	0.83
18.60	17.76	21.88	7.13	155.98	2.89	0.83	0.83
18.70	21.28	26.10	5.90	153.88	2.80	0.83	0.83
18.80	25.82	31.44	4.71	148.07	2.70	0.82	0.82
18.90	31.54	38.07	3.68	140.07	2.59	0.88	0.88
19.00	37.82	45.24	2.95	133.67	2.50	0.80	0.80
19.10	43.39	51.55	2.56	131.93	2.43	0.80	0.80
19.20	48.52	57.34	2.33	133.34	2.39	0.80	0.80

:: Strength loss calculation (Robertson (2009)) :: (continued)							
Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
19.30	55.06	64.65	2.08	134.36	2.34	0.80	0.80
19.40	66.32	77.08	1.74	134.27	2.25	0.80	0.80
19.50	80.83	92.82	1.48	137.72	2.14	0.81	0.81
19.60	88.75	101.14	1.40	141.30	2.08	0.81	0.81
19.70	81.34	92.71	1.45	134.56	2.12	0.81	0.81
19.80	68.26	78.36	1.71	134.09	2.24	0.80	0.80
19.90	59.34	68.63	2.16	148.22	2.36	0.82	0.82
20.00	53.32	61.83	2.56	158.59	2.43	0.84	0.84
20.10	41.41	48.08	3.25	156.41	2.54	0.86	0.86
20.20	26.61	30.82	4.77	146.98	2.71	0.82	0.82
20.30	17.09	19.57	6.95	136.07	2.88	0.81	0.81
20.40	13.44	15.07	8.53	128.60	2.99	0.80	0.80
20.50	11.12	12.17	9.81	119.45	3.06	0.60	0.87
20.60	9.65	10.33	10.61	109.61	3.10	0.48	0.74
20.70	8.78	9.23	10.97	101.33	3.12	0.37	0.66
20.80	8.37	8.70	11.10	96.57	3.12	0.35	0.62
20.90	8.37	8.67	10.98	95.21	3.12	0.35	0.62
21.00	8.21	8.46	11.11	93.93	3.12	0.34	0.60
21.10	7.65	7.74	11.77	91.14	3.16	0.31	0.55
21.20	6.85	6.76	12.89	87.10	3.21	0.26	0.48
21.30	6.21	5.96	14.03	83.63	3.25	0.23	0.43
21.40	6.04	5.75	14.58	83.80	3.28	0.23	0.41
21.50	6.56	6.34	14.24	90.29	3.26	0.26	0.45
21.60	8.06	8.11	12.83	104.05	3.20	0.38	0.58
21.70	10.65	11.16	10.78	120.34	3.11	0.59	0.80
21.80	13.72	14.76	9.01	133.07	3.01	0.82	1.05
21.90	16.18	17.62	7.92	139.48	2.95	0.81	0.81
22.00	17.19	18.75	7.55	141.48	2.92	0.82	0.82
22.10	16.91	18.34	7.78	142.78	2.94	0.82	0.82
22.20	16.26	17.53	8.32	145.89	2.97	0.82	0.82
22.30	16.46	17.70	8.50	150.49	2.98	0.83	0.83
22.40	18.11	19.55	7.92	154.82	2.95	0.83	0.83
22.50	21.27	23.06	6.75	155.60	2.87	0.83	0.83
22.60	25.33	27.46	5.47	150.32	2.77	0.83	0.83
22.70	29.04	31.36	4.42	138.72	2.67	0.95	0.95
22.80	31.21	33.53	3.73	125.00	2.60	0.86	0.86
22.90	31.37	33.54	3.46	115.88	2.56	0.82	0.82
23.00	29.97	31.93	3.63	115.94	2.59	0.84	0.84
23.10	27.89	29.64	4.19	124.09	2.65	0.91	0.91
23.20	25.85	27.43	4.92	135.01	2.72	0.81	0.81
23.30	23.86	25.23	5.68	143.34	2.79	0.82	0.82
23.40	21.26	22.35	6.60	147.53	2.86	0.82	0.82
23.50	17.88	18.55	7.94	147.32	2.95	0.82	0.82
23.60	14.85	15.09	9.68	146.07	3.05	0.90	1.08
23.70	13.28	13.28	10.97	145.74	3.12	0.89	0.95
23.80	12.51	12.39	11.48	142.23	3.14	0.92	0.88
23.90	11.58	11.31	11.79	133.35	3.16	0.74	0.81
24.00	10.09	9.63	12.48	120.18	3.19	0.54	0.69

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
24.10	8.71	8.07	13.51	109.01	3.23	0.45	0.58
24.20	7.82	7.07	14.55	102.84	3.28	0.37	0.50
24.30	7.70	6.90	14.82	102.28	3.29	0.36	0.49
24.40	8.15	7.38	14.29	105.43	3.27	0.43	0.53
24.50	8.70	7.96	13.60	108.26	3.24	0.46	0.57
24.60	8.57	7.78	13.70	106.67	3.24	0.45	0.56
24.70	7.74	6.86	14.69	100.75	3.28	0.38	0.49
24.80	6.79	5.80	16.04	93.07	3.33	0.29	0.41
24.90	6.15	5.09	17.00	86.47	3.37	0.25	0.36
25.00	5.98	4.89	17.09	83.52	3.37	0.23	0.35
25.10	6.01	4.90	17.07	83.73	3.37	0.23	0.35
25.20	6.34	5.24	16.71	87.60	3.36	0.25	0.37
25.30	7.03	5.97	15.79	94.30	3.32	0.31	0.43
25.40	7.80	6.77	14.90	100.93	3.29	0.39	0.48
25.50	8.27	7.25	14.52	105.30	3.27	0.42	0.52
25.60	8.37	7.33	14.64	107.36	3.28	0.43	0.52
25.70	8.13	7.05	15.20	107.22	3.30	0.44	0.50
25.80	7.53	6.40	16.43	105.07	3.35	0.41	0.46
25.90	7.11	5.93	17.55	104.06	3.38	0.36	0.42
26.00	7.40	6.22	17.32	107.69	3.38	0.41	0.44
26.10	8.52	7.37	15.73	115.94	3.32	0.51	0.53
26.20	9.73	8.62	14.35	123.61	3.27	0.62	0.62
26.30	10.47	9.37	13.69	128.26	3.24	0.67	0.67
26.40	10.75	9.63	13.57	130.62	3.24	0.68	0.69
26.50	10.76	9.61	13.74	132.04	3.24	0.70	0.69
26.60	10.76	9.58	13.91	133.25	3.25	0.71	0.68
26.70	10.76	9.55	14.06	134.20	3.26	0.72	0.68
26.80	10.76	9.52	14.19	135.04	3.26	0.73	0.68
26.90	10.76	9.48	14.34	135.97	3.27	0.74	0.68
27.00	10.76	9.45	14.45	136.64	3.27	0.75	0.68
27.10	10.76	9.42	14.53	136.88	3.27	0.75	0.67
27.20	10.76	9.39	14.53	136.47	3.27	0.75	0.67
27.30	10.62	9.22	14.57	134.41	3.28	0.73	0.66
27.40	10.09	8.65	14.95	129.24	3.29	0.68	0.62
27.50	9.29	7.81	15.59	121.84	3.32	0.56	0.56
27.60	8.63	7.12	16.08	114.51	3.33	0.48	0.51
27.70	8.37	6.83	16.02	109.46	3.33	0.45	0.49
27.80	8.37	6.81	15.67	106.68	3.32	0.42	0.49
27.90	8.49	6.91	15.34	106.03	3.31	0.41	0.49
28.00	8.69	7.09	15.10	107.03	3.30	0.43	0.51
28.10	8.89	7.27	14.91	108.37	3.29	0.45	0.52
28.20	9.37	7.73	14.29	110.43	3.27	0.45	0.55
28.30	9.97	8.30	13.53	112.26	3.23	0.50	0.59
28.40	10.57	8.87	12.83	113.72	3.20	0.51	0.63
28.50	10.98	9.25	12.38	114.46	3.18	0.50	0.66
28.60	11.67	9.90	11.76	116.48	3.16	0.53	0.71
28.70	12.47	10.66	11.16	118.95	3.13	0.59	0.76
28.80	13.04	11.19	10.82	121.06	3.11	0.60	0.80

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
28.90	13.15	11.26	10.87	122.36	3.11	0.62	0.80
29.00	13.15	11.23	11.00	123.50	3.12	0.64	0.80
29.10	13.15	11.19	11.04	123.61	3.12	0.64	0.80
29.20	13.15	11.16	10.93	122.04	3.12	0.62	0.80
29.30	12.81	10.80	10.94	118.22	3.12	0.59	0.77
29.40	12.02	10.01	11.25	112.62	3.13	0.51	0.71
29.50	11.23	9.21	11.65	107.30	3.15	0.43	0.66
29.60	10.91	8.88	11.78	104.58	3.16	0.41	0.63
29.70	11.76	9.66	11.07	106.96	3.12	0.43	0.69
29.80	12.59	10.43	10.59	110.50	3.10	0.52	0.75
29.90	13.04	10.83	10.49	113.64	3.09	0.54	0.77
30.00	13.53	11.27	10.35	116.63	3.09	0.53	0.81
30.10	14.07	11.76	10.11	118.88	3.07	0.62	0.84
30.20	14.43	12.07	9.94	119.91	3.06	0.62	0.86
30.30	13.96	11.58	10.22	118.41	3.08	0.57	0.83
30.40	13.58	11.19	10.42	116.67	3.09	0.55	0.80
30.50	13.33	10.92	10.60	115.77	3.10	0.56	0.78
30.60	12.70	10.30	11.21	115.52	3.13	0.54	0.74
30.70	12.12	9.72	12.09	117.55	3.17	0.52	0.69
30.80	13.30	10.80	11.61	125.41	3.15	0.59	0.77
30.90	17.68	14.86	9.21	136.92	3.02	0.81	1.06
31.00	25.04	21.68	6.63	143.72	2.86	0.82	0.82
31.10	33.65	29.66	4.72	140.06	2.70	0.81	0.81
31.20	41.52	36.92	3.50	129.37	2.57	0.85	0.85
31.30	47.08	42.02	2.87	120.67	2.48	0.78	0.78
31.40	50.34	44.94	2.63	118.39	2.45	0.78	0.78
31.50	51.88	46.26	2.59	119.70	2.44	0.78	0.78
31.60	53.14	47.32	2.52	119.29	2.43	0.78	0.78
31.70	54.44	48.41	2.41	116.57	2.41	0.78	0.78
31.80	55.69	49.46	2.32	114.90	2.39	0.77	0.77
31.90	56.99	50.55	2.27	114.60	2.38	0.77	0.77
32.00	58.46	51.79	2.19	113.24	2.36	0.77	0.77
32.10	59.74	52.86	2.08	109.98	2.34	0.77	0.77
32.20	60.86	53.78	1.99	107.01	2.32	0.76	0.76
32.30	62.07	54.77	1.96	107.29	2.31	0.76	0.76
32.40	62.52	55.04	2.01	110.91	2.32	0.77	0.77
32.50	59.72	52.33	2.24	117.14	2.37	0.78	0.78
32.60	52.72	45.80	2.75	125.85	2.46	0.79	0.79
32.70	42.27	36.19	3.74	135.27	2.60	0.88	0.88
32.80	31.38	26.26	5.36	140.82	2.76	0.81	0.81
32.90	22.36	18.12	7.68	139.16	2.93	0.81	0.81
33.00	16.47	12.87	10.19	131.21	3.08	0.73	0.92
33.10	13.22	9.97	12.13	120.88	3.17	0.58	0.71
33.20	11.88	8.77	12.75	111.78	3.20	0.45	0.63
33.30	11.95	8.80	12.07	106.22	3.17	0.43	0.63
33.40	11.78	8.63	11.82	101.98	3.16	0.43	0.62
33.50	11.11	8.02	12.30	98.61	3.18	0.34	0.57
33.60	11.31	8.17	12.30	100.53	3.18	0.33	0.58

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
33.70	12.29	9.01	11.66	105.05	3.15	0.48	0.64
33.80	13.31	9.86	10.98	108.34	3.12	0.48	0.70
33.90	13.96	10.41	10.56	109.90	3.10	0.45	0.74
34.00	14.67	11.00	10.21	112.22	3.08	0.54	0.79
34.10	15.54	11.71	9.94	116.39	3.06	0.56	0.84
34.20	15.54	11.68	10.25	119.70	3.08	0.59	0.83
34.30	16.11	12.14	10.38	125.97	3.09	0.64	0.87
34.40	19.78	15.26	9.29	141.78	3.03	0.77	1.09
34.50	27.81	22.07	7.19	158.74	2.90	0.84	0.84
34.60	38.35	31.15	5.24	163.38	2.75	0.84	0.84
34.70	49.92	41.21	3.74	154.16	2.60	0.91	0.91
34.80	62.64	52.31	2.74	143.11	2.46	0.82	0.82
34.90	79.13	66.70	2.13	142.02	2.35	0.82	0.82
35.00	99.48	84.48	1.75	147.48	2.25	0.82	0.82
35.10	120.93	103.28	1.51	155.49	2.15	0.83	0.83
35.20	140.29	120.35	1.37	164.43	2.06	0.85	0.85
35.30	155.97	134.18	1.30	173.87	1.99	0.86	0.86
35.40	167.22	144.01	1.26	182.05	1.94	0.87	0.87
35.50	172.04	148.00	1.26	186.30	1.93	0.87	0.87
35.60	169.35	145.24	1.27	184.86	1.95	0.87	0.87
35.70	162.62	138.93	1.29	179.62	1.98	0.86	0.86
35.80	153.39	130.51	1.31	171.55	2.01	0.85	0.85
35.90	142.33	120.54	1.34	162.10	2.04	0.84	0.84
36.00	127.98	107.67	1.41	152.06	2.10	0.83	0.83
36.10	111.52	92.97	1.57	145.72	2.18	0.82	0.82
36.20	94.75	78.10	1.87	146.32	2.29	0.82	0.82
36.30	81.09	66.05	2.32	153.12	2.39	0.83	0.83
36.40	77.71	62.92	2.56	161.10	2.43	0.84	0.84
36.50	89.74	73.00	2.25	164.17	2.38	0.85	0.85
36.60	116.69	95.99	1.74	166.66	2.24	0.85	0.85
36.70	151.21	125.75	1.42	178.50	2.10	0.86	0.86
36.80	183.51	153.75	1.30	199.49	1.99	0.89	0.89
36.90	207.83	174.76	1.25	218.63	1.92	0.91	0.91
37.00	225.84	190.03	1.23	234.36	1.89	0.92	0.92
37.10	236.91	199.16	1.23	244.58	1.89	0.93	0.93
37.20	240.81	202.11	1.23	248.10	1.89	0.93	0.93
37.30	235.84	197.44	1.23	243.25	1.89	0.93	0.93
37.40	225.38	188.09	1.24	233.40	1.91	0.92	0.92
37.50	213.17	177.28	1.25	221.78	1.92	0.91	0.91
37.60	201.83	167.31	1.26	210.53	1.93	0.90	0.90
37.70	194.32	160.72	1.26	202.21	1.93	0.89	0.89
37.80	192.34	158.91	1.25	198.83	1.92	0.89	0.89
37.90	195.72	161.54	1.25	201.20	1.91	0.89	0.89
38.00	202.49	166.84	1.25	208.20	1.92	0.90	0.90
38.10	209.96	172.55	1.26	217.04	1.93	0.90	0.90
38.20	216.55	177.42	1.27	225.56	1.95	0.91	0.91
38.30	221.69	181.09	1.28	232.42	1.97	0.92	0.92
38.40	225.49	183.72	1.29	237.27	1.98	0.92	0.92

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
38.50	228.03	185.33	1.30	240.44	1.99	0.93	0.93
38.60	228.61	185.34	1.30	241.49	1.99	0.93	0.93
38.70	226.29	182.93	1.31	239.89	2.00	0.93	0.93
38.80	221.32	178.34	1.32	235.81	2.02	0.92	0.92
38.90	215.06	172.72	1.33	230.49	2.03	0.92	0.92
39.00	208.89	167.21	1.35	225.14	2.04	0.91	0.91
39.10	203.92	162.78	1.35	220.27	2.05	0.91	0.91
39.20	201.00	160.10	1.35	216.67	2.05	0.90	0.90
39.30	200.94	159.85	1.35	215.07	2.04	0.90	0.90
39.40	203.86	162.06	1.33	216.08	2.03	0.90	0.90
39.50	209.63	166.61	1.32	219.76	2.01	0.91	0.91
39.60	217.99	173.26	1.30	226.10	2.00	0.91	0.91
39.70	228.76	181.83	1.29	235.07	1.98	0.92	0.92
39.80	241.19	191.65	1.28	246.15	1.97	0.93	0.93
39.90	254.27	201.91	1.28	258.19	1.96	0.94	0.94
40.00	265.96	210.97	1.28	269.15	1.96	0.95	0.95
40.10	276.78	219.35	1.27	278.88	1.95	0.96	0.96
40.20	286.88	227.30	1.26	286.91	1.94	0.97	0.97
40.30	297.01	235.49	1.25	293.69	1.92	0.97	0.97
40.40	305.93	242.83	1.23	298.50	1.89	0.98	0.98
40.50	313.36	248.89	1.21	301.93	1.87	0.98	0.98
40.60	319.25	253.48	1.20	305.08	1.85	0.98	0.98
40.70	323.81	256.78	1.20	308.25	1.85	0.98	0.98
40.80	326.58	258.58	1.20	310.12	1.85	0.99	0.99
40.90	326.95	258.50	1.20	309.42	1.85	0.99	0.99
41.00	324.52	256.18	1.20	306.29	1.84	0.98	0.98
41.10	319.51	251.59	1.20	302.19	1.85	0.98	0.98
41.20	312.79	245.39	1.21	297.74	1.87	0.98	0.98
41.30	304.61	237.91	1.23	292.57	1.89	0.97	0.97
41.40	293.60	228.19	1.25	284.54	1.92	0.97	0.97
41.50	278.40	215.25	1.26	272.15	1.94	0.96	0.96
41.60	258.94	199.13	1.28	255.30	1.97	0.94	0.94
41.70	237.94	182.03	1.30	236.47	1.99	0.92	0.92
41.80	218.97	166.71	1.31	219.18	2.01	0.91	0.91
41.90	200.61	151.83	1.34	203.34	2.04	0.89	0.89
42.00	180.78	135.61	1.40	189.41	2.08	0.88	0.88
42.10	157.20	116.35	1.53	178.56	2.17	0.86	0.86
42.20	132.67	96.63	1.78	172.42	2.26	0.86	0.86
42.30	112.50	80.76	2.07	167.43	2.34	0.85	0.85
42.40	103.27	73.67	2.16	158.76	2.36	0.84	0.84
42.50	106.36	76.23	1.95	148.30	2.31	0.82	0.82
42.60	116.27	84.17	1.68	141.26	2.22	0.81	0.81
42.70	123.96	90.41	1.52	137.62	2.16	0.81	0.81
42.80	125.54	91.71	1.47	135.07	2.13	0.81	0.81
42.90	120.85	87.83	1.51	132.89	2.15	0.80	0.80
43.00	111.91	80.40	1.66	133.70	2.22	0.80	0.80
43.10	101.40	71.75	1.95	139.79	2.31	0.81	0.81
43.20	92.75	64.68	2.31	149.17	2.39	0.83	0.83

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
43.30	88.83	61.44	2.51	154.44	2.43	0.83	0.83
43.40	90.15	62.36	2.44	152.17	2.41	0.83	0.83
43.50	94.42	65.64	2.22	145.47	2.37	0.82	0.82
43.60	98.83	69.05	2.02	139.74	2.33	0.81	0.81
43.70	101.21	70.83	1.93	136.98	2.30	0.81	0.81
43.80	101.76	71.10	1.93	137.20	2.30	0.81	0.81
43.90	101.61	70.76	1.97	139.40	2.31	0.81	0.81
44.00	101.41	70.34	2.03	142.77	2.33	0.82	0.82
44.10	101.33	69.98	2.11	147.36	2.34	0.82	0.82
44.20	101.20	69.56	2.20	153.26	2.37	0.83	0.83
44.30	102.65	70.30	2.27	159.70	2.38	0.84	0.84
44.40	107.15	73.43	2.22	163.08	2.37	0.84	0.84
44.50	115.17	79.40	2.02	160.41	2.32	0.84	0.84
44.60	124.33	86.49	1.78	153.87	2.26	0.83	0.83
44.70	131.80	92.40	1.61	148.70	2.20	0.83	0.83
44.80	135.88	95.58	1.54	146.92	2.17	0.82	0.82
44.90	137.36	96.48	1.54	148.17	2.17	0.82	0.82
45.00	138.06	96.63	1.56	151.12	2.18	0.83	0.83
45.10	138.23	96.38	1.60	153.78	2.19	0.83	0.83
45.20	137.03	95.17	1.63	155.09	2.21	0.83	0.83
45.30	133.73	92.39	1.68	155.47	2.23	0.83	0.83
45.40	129.36	88.83	1.75	155.87	2.25	0.83	0.83
45.50	126.45	86.43	1.80	155.93	2.27	0.83	0.83
45.60	127.21	86.93	1.77	153.97	2.26	0.83	0.83
45.70	131.34	90.15	1.66	149.85	2.22	0.83	0.83
45.80	136.70	94.47	1.54	145.28	2.17	0.82	0.82
45.90	140.90	97.96	1.45	141.93	2.12	0.82	0.82
46.00	142.26	99.07	1.42	140.37	2.10	0.81	0.81
46.10	140.88	97.75	1.44	140.33	2.11	0.81	0.81
46.20	137.87	94.97	1.49	141.79	2.14	0.82	0.82
46.30	135.03	92.38	1.56	143.75	2.18	0.82	0.82
46.40	133.22	90.73	1.59	144.70	2.19	0.82	0.82
46.50	132.83	90.17	1.62	145.76	2.20	0.82	0.82
46.60	133.78	90.50	1.65	149.12	2.21	0.83	0.83
46.70	134.60	90.57	1.71	154.91	2.24	0.83	0.83
46.80	132.80	88.68	1.82	161.37	2.27	0.84	0.84
46.90	125.89	83.19	1.99	165.91	2.32	0.85	0.85
47.00	115.97	75.67	2.24	169.55	2.37	0.85	0.85
47.10	104.67	67.40	2.53	170.35	2.43	0.85	0.85
47.20	98.78	63.13	2.67	168.63	2.45	0.85	0.85
47.30	98.47	62.90	2.62	164.47	2.44	0.85	0.85
47.40	96.95	61.77	2.62	161.58	2.44	0.84	0.84
47.50	88.26	55.55	2.90	161.33	2.49	0.84	0.84
47.60	70.99	43.46	3.72	161.81	2.60	0.92	0.92
47.70	54.66	32.30	4.96	160.21	2.72	0.84	0.84
47.80	43.11	24.66	6.23	153.58	2.83	0.83	0.83
47.90	37.26	21.04	6.95	146.31	2.88	0.82	0.82
48.00	35.46	19.90	7.09	141.01	2.89	0.81	0.81

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
48.10	35.37	19.80	7.12	141.08	2.89	0.81	0.81
48.20	36.65	20.54	7.28	149.41	2.90	0.83	0.83
48.30	39.52	22.24	7.43	165.15	2.91	0.85	0.85
48.40	43.87	24.83	7.24	179.87	2.90	0.86	0.86
48.50	47.02	26.68	6.96	185.63	2.88	0.87	0.87
48.60	46.83	26.51	6.88	182.33	2.88	0.87	0.87
48.70	43.44	24.41	7.13	173.95	2.89	0.86	0.86
48.80	39.99	22.29	7.47	166.43	2.92	0.85	0.85
48.90	37.97	21.03	7.65	160.86	2.93	0.84	0.84
49.00	37.11	20.47	7.66	156.88	2.93	0.84	0.84
49.10	36.51	20.07	7.67	153.90	2.93	0.83	0.83
49.20	35.49	19.43	7.77	150.91	2.94	0.83	0.83
49.30	33.74	18.34	8.03	147.20	2.95	0.82	0.82
49.40	30.37	16.30	8.65	140.97	2.99	0.81	0.81
49.50	26.08	13.72	9.65	132.46	3.05	0.75	0.98
49.60	22.32	11.46	10.77	123.51	3.11	0.61	0.82
49.70	20.21	10.20	11.47	117.01	3.14	0.54	0.73
49.80	19.41	9.70	11.73	113.79	3.15	0.50	0.69

Abbreviations

q_t :	Total cone resistance
K_c :	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c :	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

LIQUEFACTION ANALYSIS REPORT

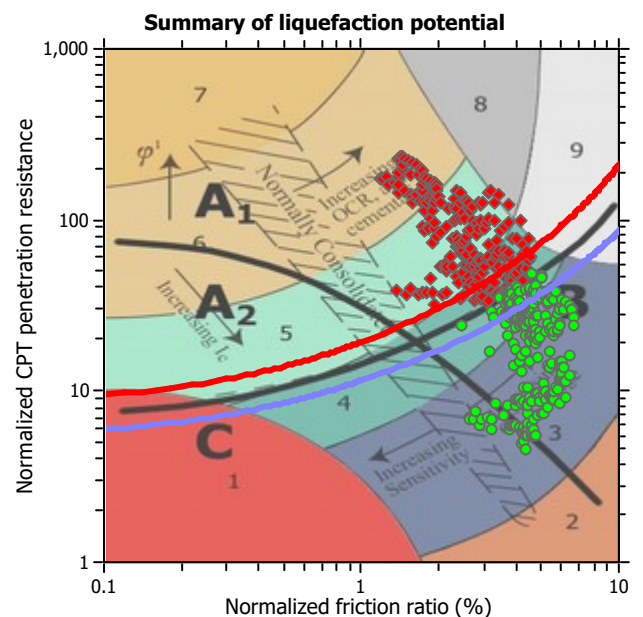
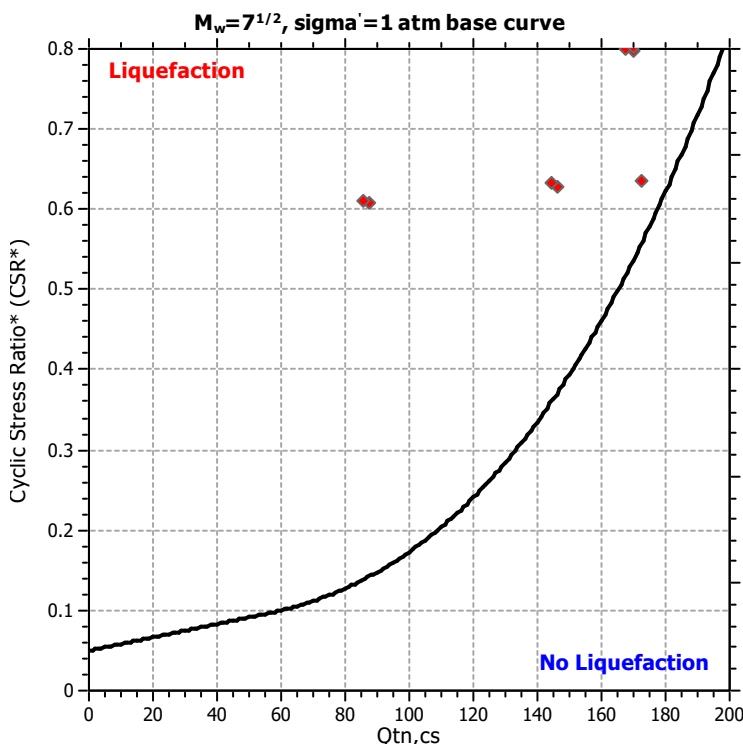
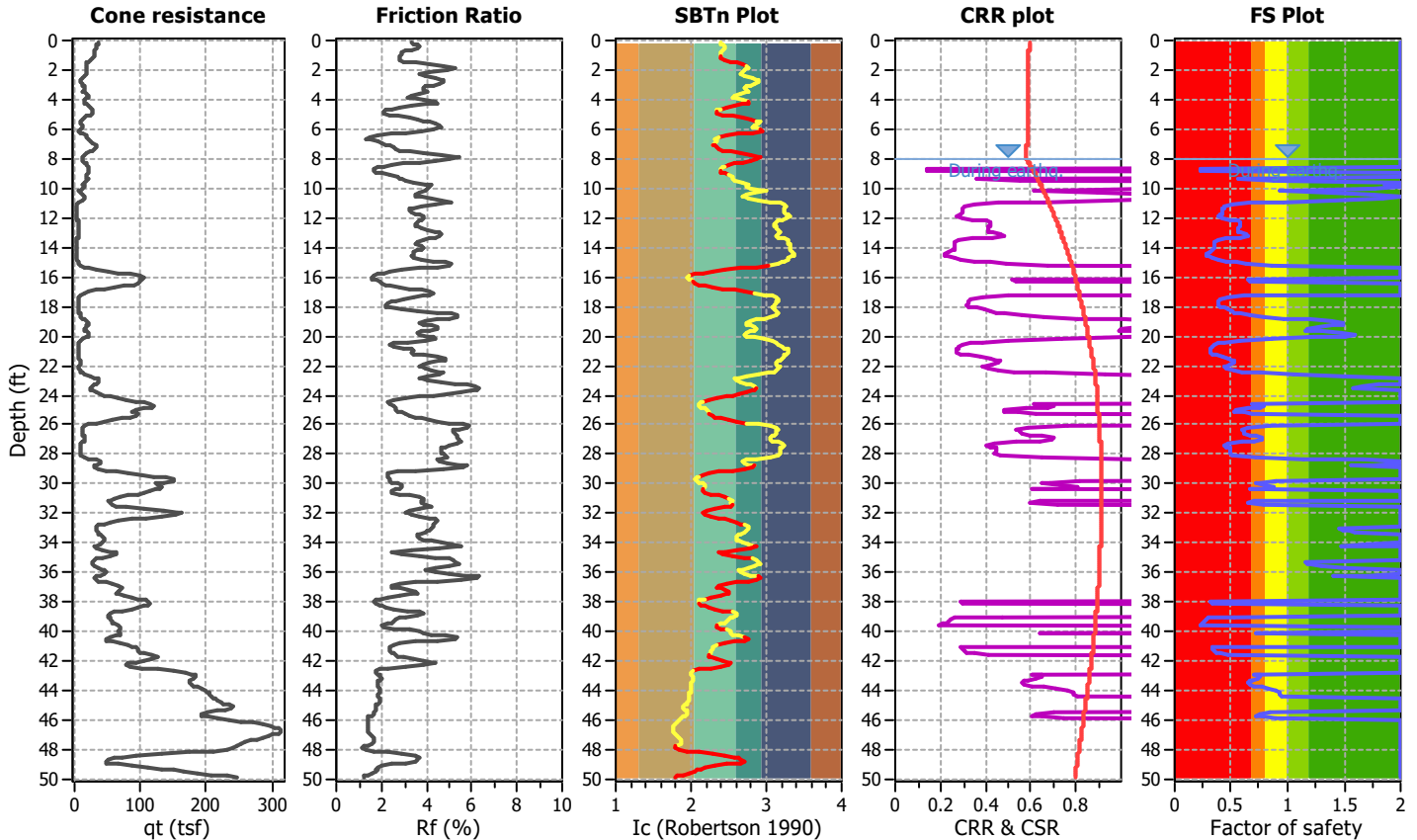
Project title : 21-483 Equestrian Estates

Location : Avenue 64 at Harrison Street, Thermal California

CPT file : CPT-5 Robt 2009

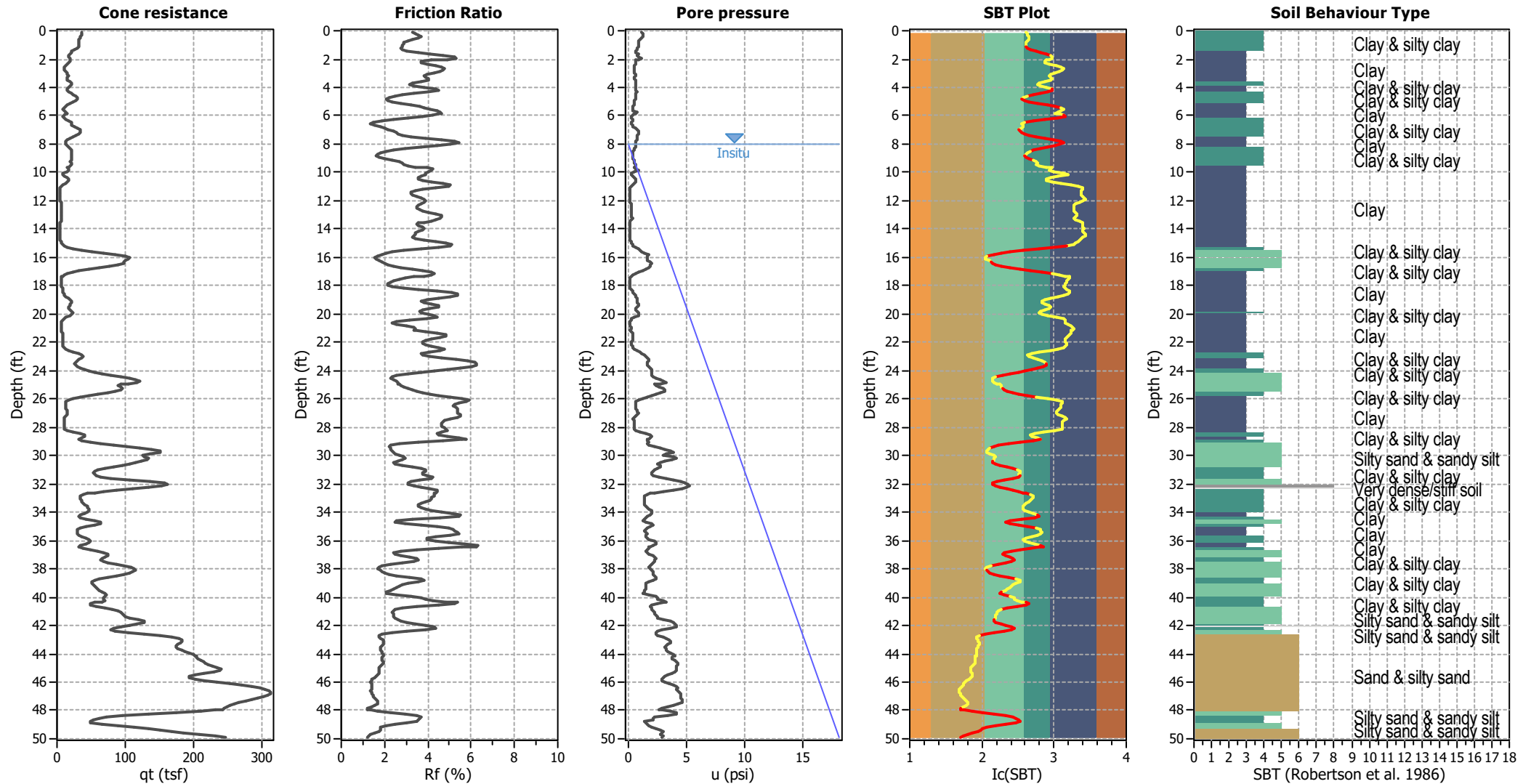
Input parameters and analysis data

Analysis method:	Robertson (2009)	G.W.T. (in-situ):	8.00 ft	Use fill:	No	Clay like behavior	
Fines correction method:	Robertson (2009)	G.W.T. (earthq.):	8.00 ft	Fill height:	N/A	applied:	All soils
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude M_w :	7.34	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.74	Unit weight calculation:	Based on SBT	K_o applied:	No	MSF method:	Method based



Zone A₁: Cyclic liquefaction likely depending on size and duration of cyclic loading
 Zone A₂: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
 Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
 Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



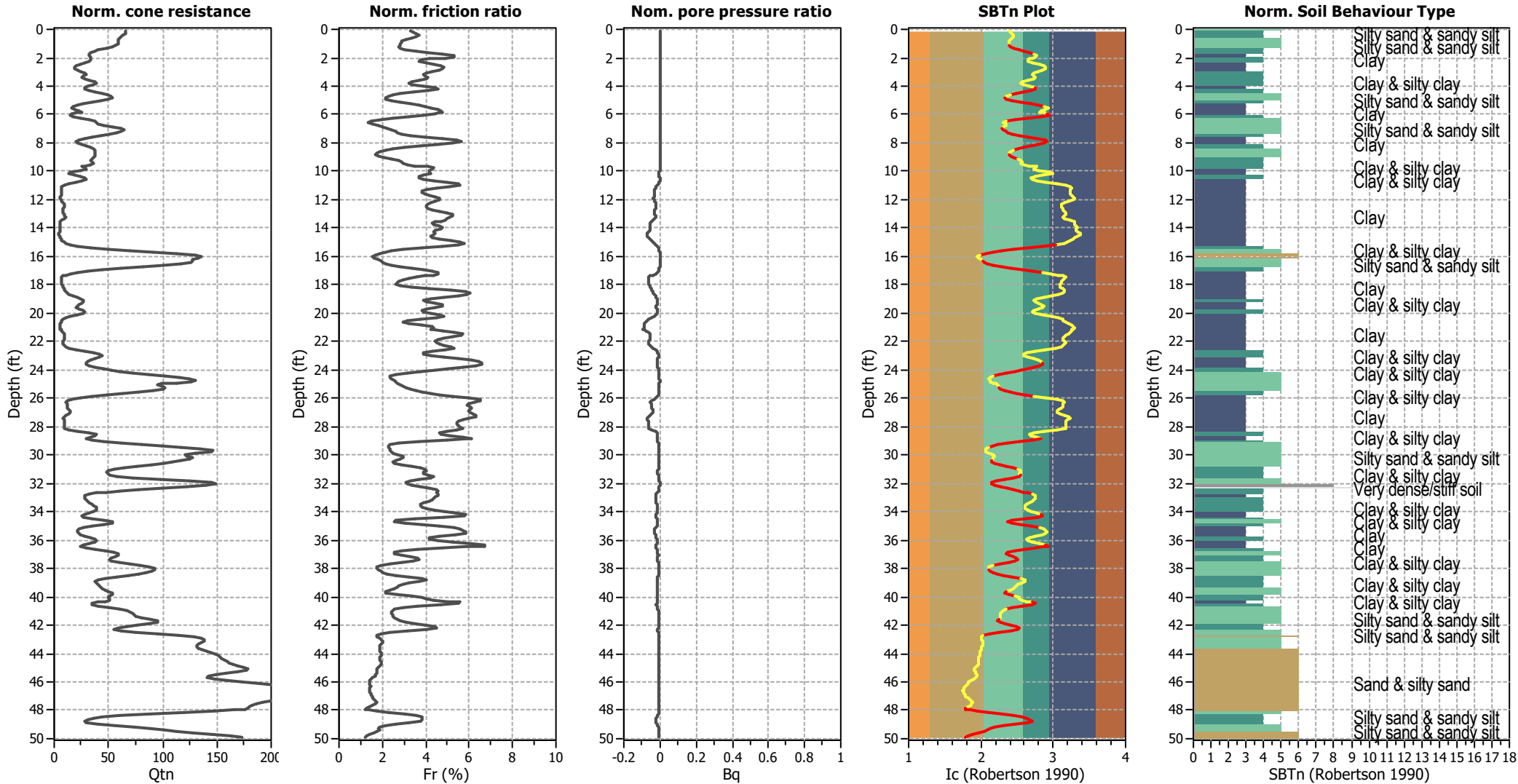
Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	No
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

SBT legend

1. Sensitive fine grained	4. Clayey silt to silty	7. Gravely sand to sand
2. Organic material	5. Silty sand to sandy silt	8. Very stiff sand to
3. Clay to silty clay	6. Clean sand to silty sand	9. Very stiff fine grained

CPT basic interpretation plots (normalized)



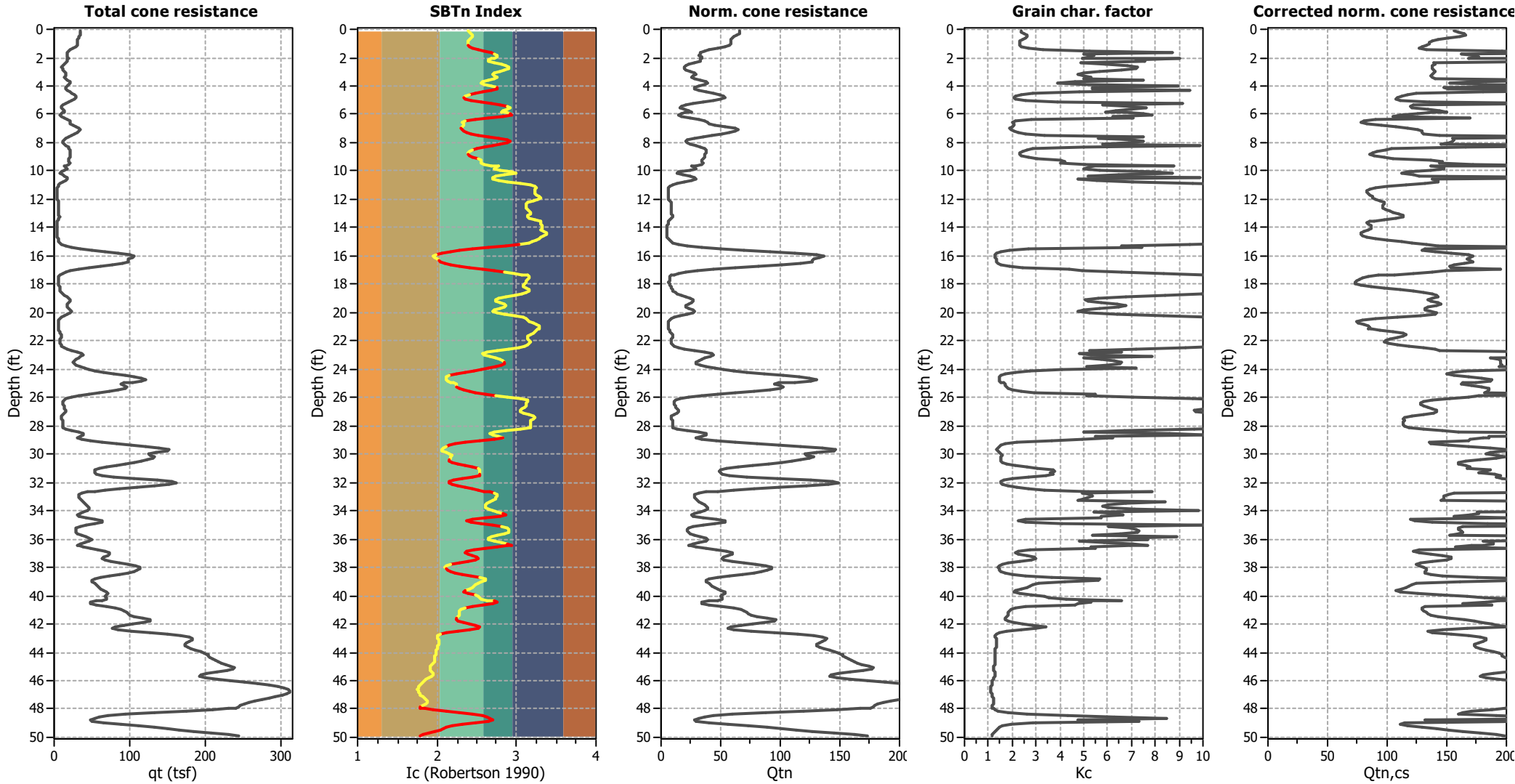
Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	No
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

SBTn legend

1. Sensitive fine grained	4. Clayey silt to silty	7. Gravely sand to sand
2. Organic material	5. Silty sand to sandy silt	8. Very stiff sand to
3. Clay to silty clay	6. Clean sand to silty sand	9. Very stiff fine grained

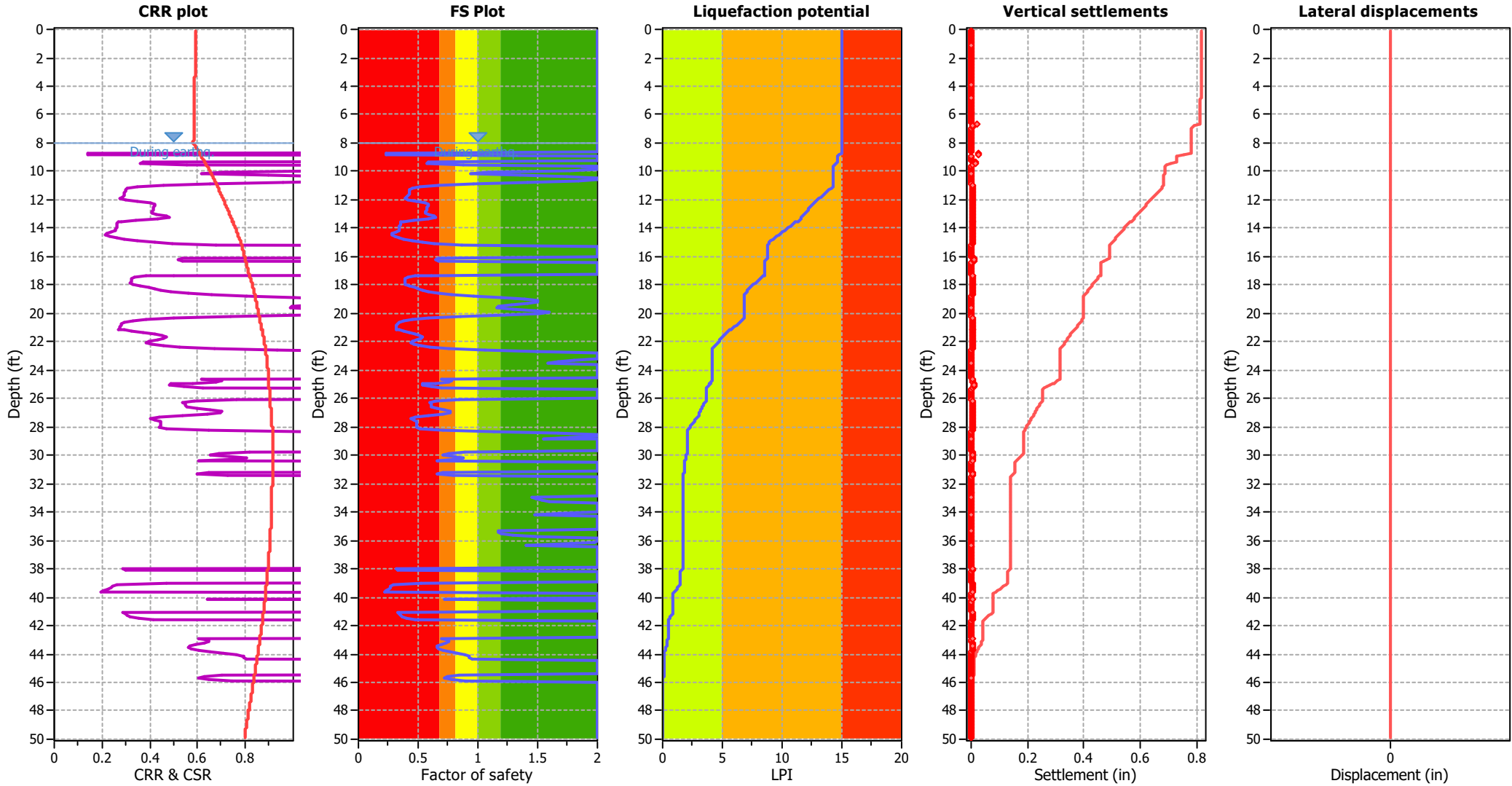
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	No
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	No
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

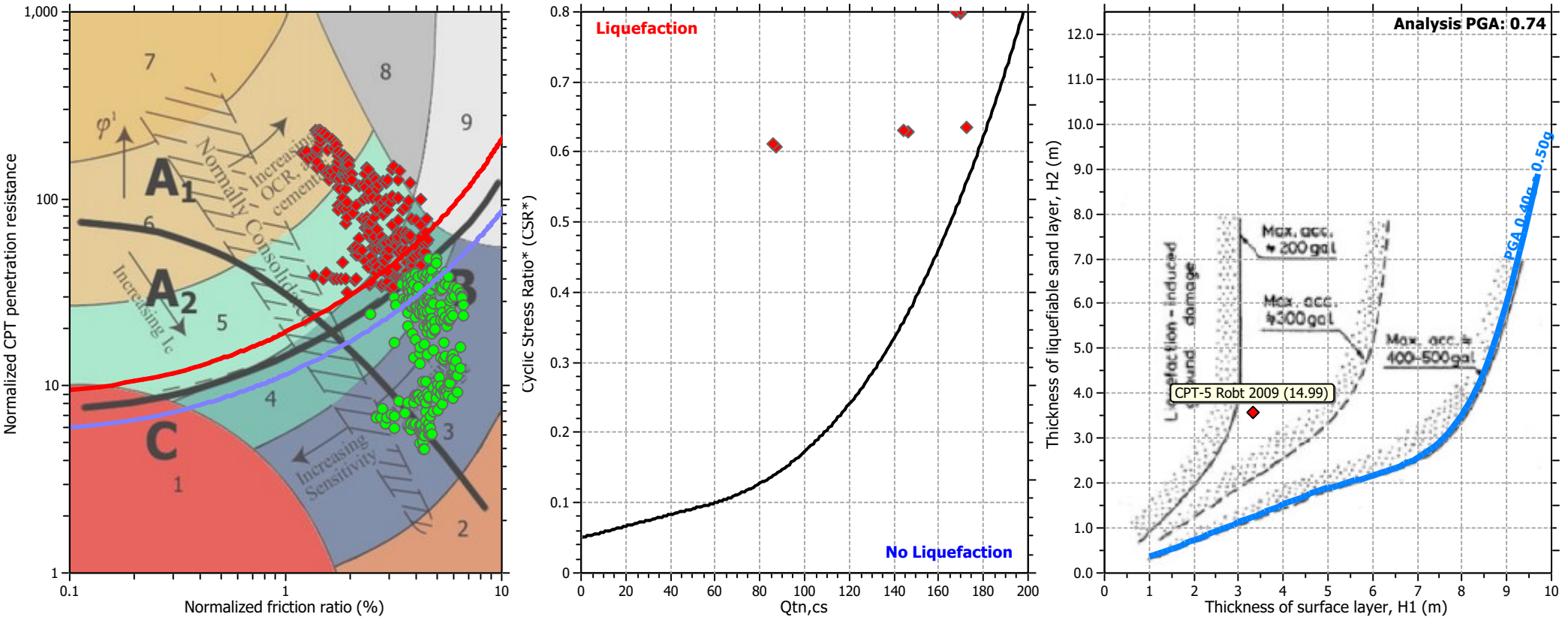
F.S. color scheme

- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

LPI color scheme

- Very high risk
- High risk
- Low risk

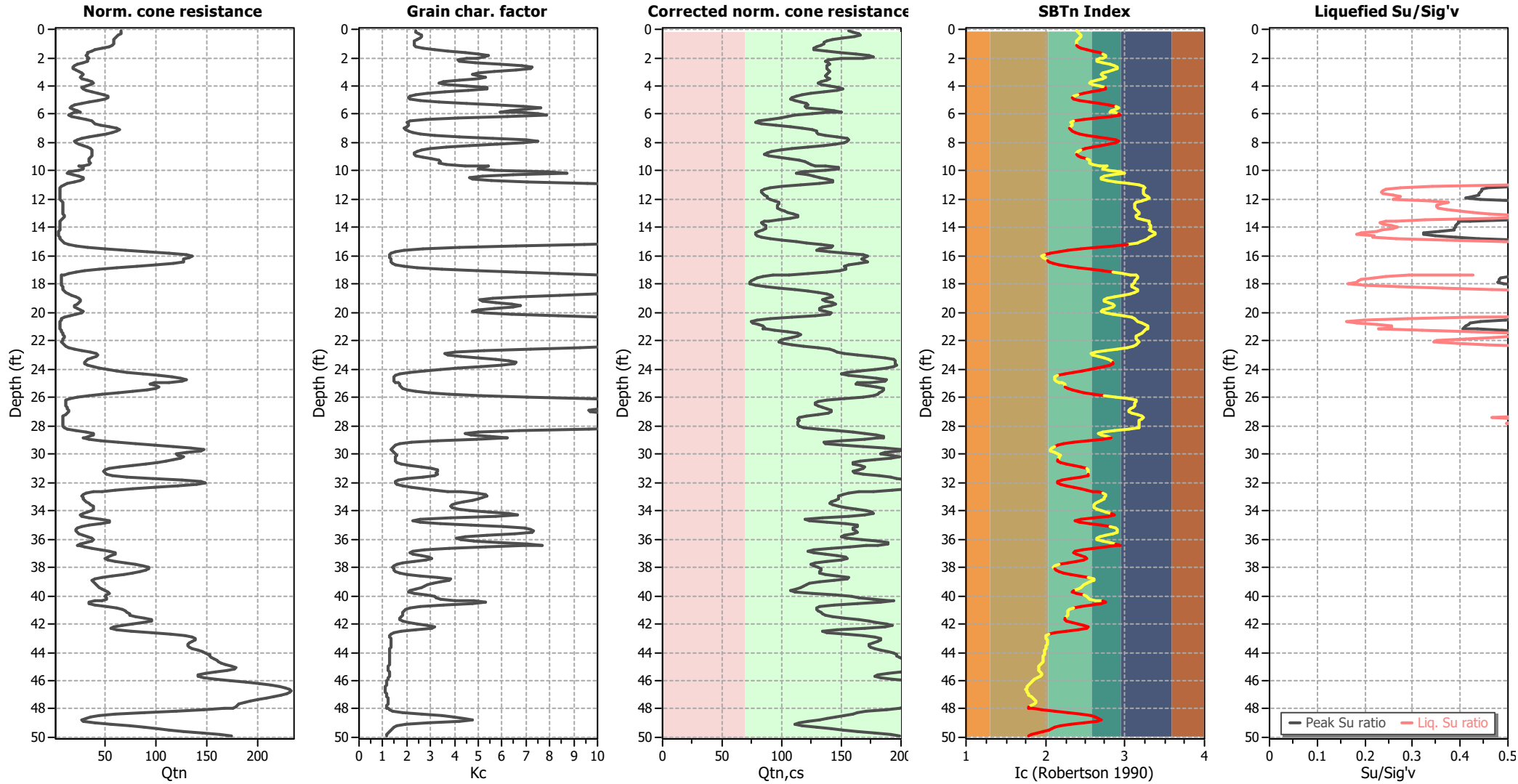
Liquefaction analysis summary plots



Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on I_c value	I_c cut-off value:	2.60	K_o applied:	No
Earthquake magnitude M_w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

Check for strength loss plots (Robertson (2010))



Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on I_c value	I_c cut-off value:	2.60	K_o applied:	No
Earthquake magnitude M_w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

Transition layer No	Number of points	Depth	SBT _n number	SBT _n description
Transition layer 1	7	Start depth: 1.20 (ft)	5	Silty sand & sandy silt
		End depth: 1.80 (ft)	3	Clay
Transition layer 2	6	Start depth: 4.20 (ft)	3	Clay
		End depth: 4.70 (ft)	5	Silty sand & sandy silt
Transition layer 3	7	Start depth: 4.90 (ft)	5	Silty sand & sandy silt
		End depth: 5.50 (ft)	3	Clay
Transition layer 4	6	Start depth: 6.10 (ft)	3	Clay
		End depth: 6.60 (ft)	5	Silty sand & sandy silt
Transition layer 5	9	Start depth: 7.10 (ft)	5	Silty sand & sandy silt
		End depth: 7.90 (ft)	3	Clay
Transition layer 6	8	Start depth: 7.90 (ft)	3	Clay
		End depth: 8.60 (ft)	5	Silty sand & sandy silt
Transition layer 7	4	Start depth: 8.90 (ft)	5	Silty sand & sandy silt
		End depth: 9.20 (ft)	4	Clay & silty clay
Transition layer 8	8	Start depth: 15.30 (ft)	3	Clay
		End depth: 16.00 (ft)	6	Sand & silty sand
Transition layer 9	9	Start depth: 16.40 (ft)	5	Silty sand & sandy silt
		End depth: 17.20 (ft)	3	Clay
Transition layer 10	10	Start depth: 23.60 (ft)	3	Clay
		End depth: 24.50 (ft)	5	Silty sand & sandy silt
Transition layer 11	7	Start depth: 25.40 (ft)	5	Silty sand & sandy silt
		End depth: 26.00 (ft)	3	Clay
Transition layer 12	8	Start depth: 28.90 (ft)	3	Clay
		End depth: 29.60 (ft)	5	Silty sand & sandy silt
Transition layer 13	7	Start depth: 30.50 (ft)	5	Silty sand & sandy silt
		End depth: 31.10 (ft)	4	Clay & silty clay
Transition layer 14	5	Start depth: 31.50 (ft)	4	Clay & silty clay
		End depth: 31.90 (ft)	5	Silty sand & sandy silt
Transition layer 15	10	Start depth: 32.00 (ft)	5	Silty sand & sandy silt
		End depth: 32.90 (ft)	3	Clay
Transition layer 16	5	Start depth: 34.30 (ft)	3	Clay
		End depth: 34.70 (ft)	5	Silty sand & sandy silt
Transition layer 17	6	Start depth: 34.70 (ft)	5	Silty sand & sandy silt
		End depth: 35.20 (ft)	3	Clay
Transition layer 18	6	Start depth: 36.40 (ft)	3	Clay
		End depth: 36.90 (ft)	5	Silty sand & sandy silt
Transition layer 19	4	Start depth: 37.00 (ft)	5	Silty sand & sandy silt
		End depth: 37.30 (ft)	4	Clay & silty clay
Transition layer 20	6	Start depth: 37.40 (ft)	4	Clay & silty clay
		End depth: 37.90 (ft)	5	Silty sand & sandy silt
Transition layer 21	7	Start depth: 38.20 (ft)	5	Silty sand & sandy silt
		End depth: 38.80 (ft)	4	Clay & silty clay
Transition layer 22	4	Start depth: 39.70 (ft)	5	Silty sand & sandy silt
		End depth: 40.00 (ft)	4	Clay & silty clay
Transition layer 23	6	Start depth: 40.50 (ft)	3	Clay
		End depth: 41.00 (ft)	5	Silty sand & sandy silt

Transition layer No	Number of points	Depth	SBT _n number	SBT _n description
Transition layer 24	6	Start depth: 41.70 (ft)	5	Silty sand & sandy silt
		End depth: 42.20 (ft)	4	Clay & silty clay
Transition layer 25	6	Start depth: 42.30 (ft)	4	Clay & silty clay
		End depth: 42.80 (ft)	6	Sand & silty sand
Transition layer 26	10	Start depth: 47.90 (ft)	6	Sand & silty sand
		End depth: 48.80 (ft)	4	Clay & silty clay
Transition layer 27	12	Start depth: 48.80 (ft)	4	Clay & silty clay
		End depth: 49.90 (ft)	6	Sand & silty sand

Start depth: Depth where the transition layer begins

End depth: Depth where the transition layer ends

:: Field input data ::						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1	0.10	34.66	1.14	1.14	26.30	120.03
2	0.20	35.71	1.20	1.20	26.65	120.28
3	0.30	35.06	1.26	1.26	27.40	120.50
4	0.40	33.38	1.26	1.26	28.15	120.38
5	0.50	32.46	1.18	1.18	28.27	119.85
6	0.60	31.52	1.04	1.04	27.60	119.07
7	0.70	31.06	0.94	0.94	26.77	118.34
8	0.80	31.06	0.90	0.90	26.21	117.93
9	0.90	31.06	0.88	0.88	25.98	117.79
10	1.00	31.06	0.88	0.88	25.91	117.70
11	1.10	30.81	0.87	0.87	26.07	117.36
12	1.20	28.77	0.79	0.79	26.64	116.75
13	1.30	26.25	0.72	0.72	28.49	115.66
14	1.40	20.82	0.62	0.62	31.75	114.57
15	1.50	17.28	0.60	0.60	35.16	114.90
16	1.60	21.14	0.87	0.87	39.12	114.96
17	1.70	14.85	0.72	0.72	41.83	115.72
18	1.80	15.81	0.86	0.86	43.98	116.38
19	1.90	20.33	1.12	1.12	43.10	116.91
20	2.00	17.63	0.87	0.87	41.55	116.48
21	2.10	16.62	0.68	0.68	39.41	115.05
22	2.20	18.95	0.66	0.66	37.61	114.25
23	2.30	17.81	0.63	0.63	37.95	113.89
24	2.40	15.10	0.61	0.61	41.41	113.16
25	2.50	12.51	0.56	0.56	46.22	112.10
26	2.60	10.40	0.49	0.49	50.39	111.00
27	2.70	9.56	0.45	0.45	52.14	110.60
28	2.80	10.60	0.51	0.51	51.84	110.68
29	2.90	10.75	0.50	0.50	49.20	111.45
30	3.00	12.88	0.56	0.56	45.26	112.34
31	3.10	15.85	0.63	0.63	41.80	113.10
32	3.20	16.19	0.61	0.61	40.66	113.16
33	3.30	14.40	0.55	0.55	41.88	112.69
34	3.40	13.26	0.55	0.55	43.33	112.54
35	3.50	14.27	0.60	0.60	41.88	113.14
36	3.60	17.48	0.66	0.66	37.94	114.01
37	3.70	20.66	0.67	0.67	34.19	114.54
38	3.80	21.88	0.65	0.65	33.00	114.60
39	3.90	19.87	0.65	0.65	34.86	114.30
40	4.00	16.35	0.64	0.64	39.37	113.89
41	4.10	13.95	0.64	0.64	43.56	113.73
42	4.20	14.34	0.68	0.68	43.71	114.06
43	4.30	17.02	0.72	0.72	39.83	114.50
44	4.40	19.96	0.68	0.68	34.46	114.78
45	4.50	23.48	0.65	0.65	29.83	114.91
46	4.60	26.63	0.65	0.65	26.47	115.08
47	4.70	28.93	0.64	0.64	24.42	115.05
48	4.80	29.27	0.60	0.60	23.66	114.69

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
49	4.90	27.28	0.56	0.56	24.62	114.18
50	5.00	23.74	0.56	0.56	27.69	113.61
51	5.10	18.98	0.54	0.54	32.95	112.58
52	5.20	13.36	0.45	0.45	39.56	111.14
53	5.30	10.79	0.40	0.40	45.85	109.65
54	5.40	9.84	0.38	0.38	50.63	108.45
55	5.50	7.95	0.33	0.33	53.73	107.98
56	5.60	8.27	0.36	0.36	51.02	110.36
57	5.70	15.13	0.70	0.70	48.13	112.28
58	5.80	13.75	0.64	0.64	46.24	113.32
59	5.90	12.24	0.56	0.56	49.71	111.32
60	6.00	8.05	0.34	0.34	53.36	108.78
61	6.10	7.17	0.27	0.27	54.87	106.31
62	6.20	8.22	0.27	0.27	47.65	106.57
63	6.30	12.54	0.32	0.32	37.47	108.07
64	6.40	18.28	0.36	0.36	29.62	108.98
65	6.50	20.85	0.30	0.30	24.68	108.56
66	6.60	20.76	0.22	0.22	23.13	108.42
67	6.70	21.43	0.33	0.33	23.99	109.56
68	6.80	22.43	0.43	0.43	24.11	112.15
69	6.90	29.74	0.58	0.58	23.10	114.54
70	7.00	34.64	0.74	0.74	22.31	116.37
71	7.10	34.64	0.83	0.83	22.86	117.45
72	7.20	33.84	0.89	0.89	24.02	117.64
73	7.30	31.44	0.83	0.83	25.39	117.20
74	7.40	27.57	0.74	0.74	27.80	116.44
75	7.50	22.99	0.74	0.74	31.91	115.78
76	7.60	18.86	0.75	0.75	37.94	115.16
77	7.70	14.65	0.71	0.71	44.85	114.23
78	7.80	11.48	0.63	0.63	51.04	113.21
79	7.90	10.75	0.60	0.60	53.33	112.66
80	8.00	11.85	0.62	0.62	50.61	112.76
81	8.10	13.77	0.61	0.61	45.85	112.92
82	8.20	15.32	0.57	0.57	40.20	113.03
83	8.30	18.30	0.56	0.56	34.77	112.76
84	8.40	20.55	0.48	0.48	30.81	112.22
85	8.50	20.79	0.41	0.41	28.47	111.58
86	8.60	21.40	0.41	0.41	27.07	110.84
87	8.70	21.50	0.35	0.35	26.17	110.35
88	8.80	21.50	0.33	0.33	25.90	110.13
89	8.90	21.50	0.38	0.38	26.60	110.62
90	9.00	21.50	0.42	0.42	28.55	111.42
91	9.10	19.68	0.47	0.47	31.18	112.00
92	9.20	17.89	0.51	0.51	33.14	112.61
93	9.30	19.75	0.56	0.56	33.51	113.19
94	9.40	20.94	0.59	0.59	33.16	113.73
95	9.50	20.41	0.61	0.61	34.85	113.60
96	9.60	16.30	0.56	0.56	39.22	112.59

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
97	9.70	11.30	0.46	0.46	44.11	112.27
98	9.80	13.85	0.62	0.62	42.88	113.94
99	9.90	21.75	0.90	0.90	41.92	114.24
100	10.00	13.42	0.51	0.51	45.12	112.03
101	10.10	4.85	0.20	0.20	54.94	107.32
102	10.20	6.95	0.28	0.28	58.22	106.09
103	10.30	10.42	0.39	0.39	48.80	109.13
104	10.40	14.21	0.50	0.50	42.97	111.40
105	10.50	16.71	0.57	0.57	40.18	113.03
106	10.60	17.87	0.66	0.66	40.65	113.79
107	10.70	15.71	0.67	0.67	44.47	113.35
108	10.80	10.81	0.53	0.53	51.54	111.56
109	10.90	7.42	0.39	0.39	61.61	108.57
110	11.00	5.41	0.27	0.27	70.86	105.21
111	11.10	4.18	0.18	0.18	76.18	102.13
112	11.20	3.98	0.15	0.15	77.30	99.92
113	11.30	3.98	0.13	0.13	76.00	98.99
114	11.40	3.98	0.13	0.13	75.19	98.63
115	11.50	3.98	0.13	0.13	75.26	98.59
116	11.60	3.98	0.13	0.13	76.01	98.81
117	11.70	3.98	0.14	0.14	77.28	99.22
118	11.80	3.98	0.15	0.15	79.26	99.49
119	11.90	3.79	0.15	0.15	81.33	99.47
120	12.00	3.64	0.14	0.14	79.02	100.20
121	12.10	4.78	0.18	0.18	73.77	101.41
122	12.20	5.57	0.21	0.21	68.89	102.45
123	12.30	5.57	0.20	0.20	66.87	102.69
124	12.40	5.57	0.19	0.19	66.63	102.55
125	12.50	5.57	0.20	0.20	66.78	102.55
126	12.60	5.57	0.20	0.20	67.37	102.72
127	12.70	5.57	0.21	0.21	68.41	103.07
128	12.80	5.57	0.22	0.22	69.85	103.56
129	12.90	5.57	0.24	0.24	71.47	104.10
130	13.00	5.57	0.26	0.26	71.49	104.89
131	13.10	6.23	0.30	0.30	69.09	105.82
132	13.20	7.13	0.32	0.32	67.81	105.95
133	13.30	6.16	0.27	0.27	70.05	104.76
134	13.40	4.53	0.19	0.19	75.86	102.47
135	13.50	3.98	0.15	0.15	80.73	100.37
136	13.60	3.98	0.14	0.14	81.27	99.41
137	13.70	3.98	0.13	0.13	80.75	99.16
138	13.80	3.98	0.14	0.14	81.37	99.32
139	13.90	3.98	0.15	0.15	82.66	99.71
140	14.00	3.98	0.16	0.16	83.48	99.94
141	14.10	3.98	0.15	0.15	83.14	99.76
142	14.20	3.98	0.14	0.14	82.16	99.35
143	14.30	3.98	0.13	0.13	84.08	98.52
144	14.40	3.32	0.11	0.11	87.48	97.76

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
145	14.50	3.19	0.11	0.11	87.48	97.69
146	14.60	3.98	0.13	0.13	84.44	98.16
147	14.70	3.98	0.13	0.13	81.09	99.33
148	14.80	4.30	0.16	0.16	79.32	101.05
149	14.90	5.25	0.22	0.22	76.37	103.48
150	15.00	6.18	0.30	0.30	72.85	105.82
151	15.10	7.10	0.37	0.37	69.49	107.62
152	15.20	8.08	0.42	0.42	60.98	110.35
153	15.30	13.31	0.64	0.64	49.41	113.51
154	15.40	21.50	0.86	0.86	37.83	116.66
155	15.50	33.88	1.02	1.02	28.60	118.94
156	15.60	48.69	1.12	1.12	21.88	121.07
157	15.70	68.22	1.41	1.41	17.76	123.18
158	15.80	86.56	1.76	1.76	14.65	124.50
159	15.90	100.71	1.60	1.60	12.46	125.29
160	16.00	113.74	1.67	1.67	11.54	125.27
161	16.10	102.63	1.66	1.66	12.02	125.29
162	16.20	92.86	1.65	1.65	13.10	125.54
163	16.30	100.77	1.92	1.92	13.78	126.03
164	16.40	101.14	2.04	2.04	14.36	126.38
165	16.50	90.78	1.94	1.94	15.70	126.05
166	16.60	76.93	1.82	1.82	18.14	125.31
167	16.70	62.22	1.76	1.76	21.88	124.22
168	16.80	45.33	1.54	1.54	27.12	122.57
169	16.90	30.43	1.20	1.20	33.84	120.13
170	17.00	20.78	0.89	0.89	41.59	117.05
171	17.10	14.24	0.62	0.62	49.20	113.72
172	17.20	10.42	0.43	0.43	56.74	110.19
173	17.30	7.62	0.29	0.29	63.58	106.70
174	17.40	6.02	0.20	0.20	68.69	103.61
175	17.50	5.57	0.16	0.16	70.47	101.58
176	17.60	5.57	0.15	0.15	69.51	100.49
177	17.70	5.57	0.13	0.13	68.04	99.83
178	17.80	5.57	0.13	0.13	67.10	99.38
179	17.90	5.57	0.12	0.12	66.45	99.04
180	18.00	5.57	0.11	0.11	65.65	99.29
181	18.10	6.00	0.14	0.14	64.37	100.60
182	18.20	6.94	0.19	0.19	65.01	102.82
183	18.30	7.17	0.25	0.25	67.38	105.03
184	18.40	7.17	0.32	0.32	69.86	107.16
185	18.50	8.16	0.43	0.43	70.11	108.93
186	18.60	9.05	0.49	0.49	67.41	110.54
187	18.70	10.41	0.57	0.57	62.96	111.98
188	18.80	12.71	0.66	0.66	56.94	113.39
189	18.90	15.69	0.73	0.73	50.04	114.69
190	19.00	19.82	0.78	0.78	44.92	115.31
191	19.10	20.89	0.73	0.73	42.32	115.64
192	19.20	20.69	0.77	0.77	42.75	115.85

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
193	19.30	19.95	0.85	0.85	45.31	115.98
194	19.40	17.55	0.82	0.82	48.36	115.57
195	19.50	15.51	0.71	0.71	50.08	114.76
196	19.60	15.84	0.66	0.66	48.85	114.17
197	19.70	17.54	0.65	0.65	45.16	114.65
198	19.80	21.46	0.76	0.76	41.90	115.66
199	19.90	23.89	0.86	0.86	40.85	116.64
200	20.00	22.86	0.91	0.91	43.07	116.69
201	20.10	17.95	0.83	0.83	48.54	115.18
202	20.20	11.57	0.53	0.53	56.74	112.13
203	20.30	8.08	0.31	0.31	64.26	107.94
204	20.40	7.11	0.21	0.21	67.57	104.13
205	20.50	6.20	0.15	0.15	68.48	101.43
206	20.60	5.57	0.12	0.12	70.26	99.95
207	20.70	5.57	0.14	0.14	73.45	100.23
208	20.80	5.57	0.17	0.17	76.83	101.36
209	20.90	5.49	0.19	0.19	79.45	102.13
210	21.00	5.48	0.19	0.19	80.11	102.23
211	21.10	5.52	0.18	0.18	79.81	101.97
212	21.20	5.42	0.17	0.17	77.76	102.77
213	21.30	6.55	0.24	0.24	76.80	104.57
214	21.40	7.17	0.32	0.32	75.26	106.75
215	21.50	7.83	0.39	0.39	73.55	108.27
216	21.60	8.73	0.43	0.43	71.40	108.90
217	21.70	8.76	0.40	0.40	69.08	108.81
218	21.80	8.76	0.36	0.36	67.86	108.08
219	21.90	8.44	0.32	0.32	68.20	107.05
220	22.00	7.50	0.27	0.27	69.86	106.13
221	22.10	7.17	0.27	0.27	71.03	105.96
222	22.20	7.89	0.31	0.31	69.97	106.79
223	22.30	8.78	0.36	0.36	67.91	108.22
224	22.40	9.68	0.43	0.43	65.80	109.99
225	22.50	11.24	0.55	0.55	60.43	112.52
226	22.60	16.11	0.78	0.78	51.87	115.20
227	22.70	23.09	0.97	0.97	43.02	117.69
228	22.80	31.69	1.14	1.14	36.88	119.75
229	22.90	38.68	1.38	1.38	34.50	121.26
230	23.00	38.61	1.55	1.55	35.23	122.23
231	23.10	35.57	1.66	1.66	38.27	122.56
232	23.20	31.61	1.69	1.69	42.04	122.56
233	23.30	28.79	1.71	1.71	45.49	122.33
234	23.40	26.69	1.66	1.66	47.96	121.98
235	23.50	25.18	1.58	1.58	49.31	121.68
236	23.60	25.14	1.59	1.59	49.11	121.77
237	23.70	27.57	1.71	1.71	46.66	122.39
238	23.80	32.85	1.85	1.85	42.37	123.30
239	23.90	39.81	1.97	1.97	37.58	124.12
240	24.00	46.73	2.01	2.01	33.28	124.67

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
241	24.10	52.98	1.98	1.98	29.02	125.09
242	24.20	63.75	2.01	2.01	24.54	125.49
243	24.30	78.48	1.98	1.98	20.44	126.12
244	24.40	94.72	2.11	2.11	17.66	127.04
245	24.50	108.37	2.44	2.44	16.44	128.21
246	24.60	116.41	2.80	2.80	16.21	129.29
247	24.70	120.60	3.06	3.06	16.35	130.09
248	24.80	124.03	3.26	3.26	16.96	129.98
249	24.90	104.48	2.76	2.76	18.10	129.03
250	25.00	85.21	2.25	2.25	19.45	127.87
251	25.10	86.59	2.35	2.35	20.23	127.67
252	25.20	92.99	2.67	2.67	20.33	128.52
253	25.30	98.39	3.01	3.01	20.70	129.28
254	25.40	96.08	3.13	3.13	21.72	129.55
255	25.50	86.73	3.07	3.07	23.59	129.15
256	25.60	73.25	2.80	2.80	26.39	128.14
257	25.70	58.28	2.39	2.39	30.20	126.63
258	25.80	44.63	2.03	2.03	35.43	124.75
259	25.90	32.31	1.68	1.68	42.53	122.45
260	26.00	21.40	1.25	1.25	51.56	119.66
261	26.10	14.70	0.89	0.89	61.54	116.51
262	26.20	11.45	0.66	0.66	67.83	114.12
263	26.30	11.60	0.63	0.63	68.85	112.99
264	26.40	12.14	0.62	0.62	67.65	112.82
265	26.50	11.95	0.61	0.61	67.30	112.86
266	26.60	11.95	0.63	0.63	67.37	113.15
267	26.70	12.65	0.69	0.69	65.88	113.89
268	26.80	14.34	0.77	0.77	63.63	114.68
269	26.90	15.19	0.81	0.81	61.79	115.29
270	27.00	15.52	0.83	0.83	61.98	115.37
271	27.10	14.40	0.80	0.80	64.34	114.80
272	27.20	12.16	0.68	0.68	69.38	113.25
273	27.30	9.27	0.50	0.50	74.61	111.36
274	27.40	8.76	0.44	0.44	75.56	110.29
275	27.50	10.35	0.49	0.49	73.35	110.32
276	27.60	10.35	0.49	0.49	71.13	110.67
277	27.70	10.35	0.48	0.48	70.96	110.58
278	27.80	10.35	0.47	0.47	71.05	110.57
279	27.90	10.35	0.49	0.49	71.29	110.63
280	28.00	10.35	0.49	0.49	71.80	110.78
281	28.10	10.36	0.50	0.50	70.55	111.48
282	28.20	12.07	0.60	0.60	61.79	114.31
283	28.30	21.29	1.03	1.03	49.87	118.13
284	28.40	34.11	1.48	1.48	41.81	121.45
285	28.50	42.17	1.82	1.82	39.05	123.32
286	28.60	40.15	1.97	1.97	40.38	123.84
287	28.70	33.68	1.87	1.87	44.23	123.50
288	28.80	29.73	1.77	1.77	47.76	122.82

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
289	28.90	28.47	1.68	1.68	47.37	122.48
290	29.00	32.92	1.65	1.65	41.54	122.76
291	29.10	45.19	1.70	1.70	32.50	123.45
292	29.20	63.64	1.67	1.67	24.82	124.41
293	29.30	83.01	1.81	1.81	20.11	125.75
294	29.40	100.69	2.24	2.24	17.69	127.57
295	29.50	120.75	2.79	2.79	16.17	129.28
296	29.60	139.64	3.13	3.13	15.09	130.77
297	29.70	155.79	3.62	3.62	14.57	131.75
298	29.80	158.58	3.85	3.85	14.91	131.79
299	29.90	133.95	3.23	3.23	16.19	131.06
300	30.00	111.62	2.95	2.95	17.70	130.88
301	30.10	128.93	3.85	3.85	18.39	131.56
302	30.20	139.28	4.15	4.15	18.16	132.17
303	30.30	130.61	3.70	3.70	17.86	131.68
304	30.40	122.14	3.17	3.17	17.60	130.49
305	30.50	115.80	2.69	2.69	17.54	129.38
306	30.60	107.57	2.54	2.54	18.55	128.79
307	30.70	96.38	2.71	2.71	21.09	128.57
308	30.80	81.49	2.76	2.76	24.68	128.21
309	30.90	67.35	2.55	2.55	28.37	127.37
310	31.00	57.59	2.27	2.27	31.24	126.31
311	31.10	52.71	2.07	2.07	32.65	125.44
312	31.20	51.96	1.97	1.97	32.70	125.03
313	31.30	53.72	1.96	1.96	32.36	125.22
314	31.40	56.20	2.19	2.19	32.60	126.00
315	31.50	58.44	2.57	2.57	32.01	127.51
316	31.60	72.72	3.21	3.21	28.55	129.50
317	31.70	103.82	3.93	3.93	23.35	131.55
318	31.80	141.49	4.47	4.47	19.46	133.12
319	31.90	162.19	4.85	4.85	17.56	134.08
320	32.00	165.45	5.09	5.09	17.47	134.52
321	32.10	157.32	5.20	5.20	18.80	134.45
322	32.20	134.40	5.01	5.01	21.30	133.91
323	32.30	108.77	4.64	4.64	24.78	132.71
324	32.40	84.10	3.83	3.83	28.51	130.94
325	32.50	66.38	2.96	2.96	31.91	128.67
326	32.60	53.27	2.30	2.30	35.02	126.32
327	32.70	42.89	1.85	1.85	38.32	124.22
328	32.80	35.93	1.57	1.57	41.54	122.52
329	32.90	32.06	1.38	1.38	43.44	121.40
330	33.00	31.80	1.32	1.32	43.59	121.02
331	33.10	33.67	1.38	1.38	42.92	121.18
332	33.20	34.60	1.43	1.43	42.05	121.41
333	33.30	35.33	1.40	1.40	40.79	121.50
334	33.40	37.59	1.38	1.38	38.84	121.61
335	33.50	40.87	1.42	1.42	37.12	121.97
336	33.60	43.05	1.52	1.52	36.18	122.56

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
337	33.70	44.89	1.65	1.65	35.88	123.23
338	33.80	46.96	1.78	1.78	36.23	123.92
339	33.90	47.18	1.96	1.96	37.49	124.42
340	34.00	44.30	2.04	2.04	40.12	124.60
341	34.10	39.29	2.04	2.04	43.92	124.28
342	34.20	33.66	1.92	1.92	47.95	123.50
343	34.30	29.54	1.68	1.68	49.51	122.58
344	34.40	31.08	1.51	1.51	45.29	121.94
345	34.50	39.58	1.40	1.40	35.82	121.76
346	34.60	55.19	1.24	1.24	28.02	122.39
347	34.70	69.17	1.50	1.50	25.56	123.77
348	34.80	67.52	2.00	2.00	27.73	124.97
349	34.90	54.56	2.09	2.09	33.26	125.09
350	35.00	41.11	1.91	1.91	40.32	124.03
351	35.10	31.86	1.64	1.64	46.91	122.61
352	35.20	28.07	1.47	1.47	50.83	121.52
353	35.30	27.63	1.42	1.42	52.05	121.29
354	35.40	28.67	1.55	1.55	52.49	121.51
355	35.50	28.39	1.61	1.61	52.08	121.77
356	35.60	29.63	1.55	1.55	49.09	121.96
357	35.70	35.50	1.56	1.56	43.73	122.27
358	35.80	42.33	1.59	1.59	39.30	123.00
359	35.90	46.92	1.79	1.79	37.26	124.18
360	36.00	51.24	2.20	2.20	38.09	125.31
361	36.10	48.45	2.42	2.42	41.11	125.88
362	36.20	40.71	2.40	2.40	46.12	125.51
363	36.30	33.17	2.17	2.17	51.52	124.51
364	36.40	28.97	1.89	1.89	53.98	123.41
365	36.50	29.96	1.72	1.72	50.80	122.93
366	36.60	37.11	1.73	1.73	43.47	123.00
367	36.70	46.63	1.65	1.65	35.44	123.32
368	36.80	58.10	1.56	1.56	29.06	123.62
369	36.90	68.89	1.60	1.60	25.33	124.23
370	37.00	75.65	1.80	1.80	24.48	125.15
371	37.10	75.29	2.08	2.08	25.72	126.02
372	37.20	70.69	2.28	2.28	28.08	126.51
373	37.30	65.34	2.33	2.33	30.34	126.58
374	37.40	62.12	2.29	2.29	31.16	126.47
375	37.50	64.91	2.24	2.24	29.63	126.36
376	37.60	73.25	2.13	2.13	25.91	126.26
377	37.70	86.14	1.96	1.96	21.65	126.09
378	37.80	98.77	1.82	1.82	18.22	125.98
379	37.90	108.63	1.80	1.80	16.28	126.19
380	38.00	115.25	1.94	1.94	15.74	126.61
381	38.10	114.97	2.05	2.05	16.14	127.01
382	38.20	110.63	2.11	2.11	16.96	127.12
383	38.30	105.76	2.09	2.09	18.08	127.05
384	38.40	98.70	2.09	2.09	19.92	126.98

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
385	38.50	87.30	2.21	2.21	23.15	127.02
386	38.60	73.69	2.38	2.38	27.72	126.92
387	38.70	60.85	2.37	2.37	32.56	126.35
388	38.80	51.36	2.08	2.08	35.69	125.29
389	38.90	48.51	1.75	1.75	35.65	124.06
390	39.00	50.58	1.53	1.53	33.51	123.19
391	39.10	53.22	1.46	1.46	31.38	122.84
392	39.20	55.15	1.46	1.46	30.12	122.81
393	39.30	56.55	1.45	1.45	29.20	122.87
394	39.40	58.57	1.45	1.45	28.06	122.86
395	39.50	61.39	1.41	1.41	26.45	122.78
396	39.60	65.19	1.34	1.34	24.44	122.66
397	39.70	70.41	1.30	1.30	23.80	123.40
398	39.80	74.10	1.74	1.74	26.14	125.03
399	39.90	67.59	2.41	2.41	29.56	126.37
400	40.00	63.77	2.46	2.46	31.87	127.09
401	40.10	68.83	2.49	2.49	32.32	127.72
402	40.20	72.50	3.01	3.01	33.56	128.46
403	40.30	65.62	3.28	3.28	36.88	128.75
404	40.40	54.60	3.07	3.07	41.02	128.04
405	40.50	46.46	2.55	2.55	43.32	126.60
406	40.60	44.46	2.03	2.03	40.81	125.32
407	40.70	53.05	1.87	1.87	34.16	124.98
408	40.80	70.44	1.96	1.96	27.94	125.50
409	40.90	84.10	2.03	2.03	24.27	126.20
410	41.00	88.98	2.12	2.12	22.60	126.72
411	41.10	92.93	2.21	2.21	22.08	127.06
412	41.20	94.75	2.26	2.26	21.72	127.40
413	41.30	98.24	2.35	2.35	21.53	127.71
414	41.40	100.38	2.45	2.45	21.50	128.00
415	41.50	100.35	2.50	2.50	21.06	128.81
416	41.60	118.10	3.03	3.03	20.37	130.07
417	41.70	134.16	3.64	3.64	20.22	131.26
418	41.80	128.80	3.84	3.84	21.34	131.93
419	41.90	118.04	4.05	4.05	23.84	132.01
420	42.00	103.50	4.08	4.08	26.99	131.91
421	42.10	92.50	4.12	4.12	30.13	131.37
422	42.20	80.16	3.67	3.67	32.08	130.30
423	42.30	72.29	2.89	2.89	31.18	128.98
424	42.40	80.37	2.51	2.51	26.59	128.01
425	42.50	100.78	2.32	2.32	20.83	127.93
426	42.60	126.94	2.32	2.32	16.36	128.50
427	42.70	153.49	2.57	2.57	13.94	129.52
428	42.80	170.89	2.94	2.94	13.01	130.65
429	42.90	180.62	3.30	3.30	12.95	131.57
430	43.00	183.96	3.54	3.54	13.20	132.13
431	43.10	183.33	3.65	3.65	13.50	132.32
432	43.20	179.38	3.58	3.58	13.69	132.19

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
433	43.30	175.11	3.41	3.41	13.68	131.87
434	43.40	173.36	3.25	3.25	13.52	131.53
435	43.50	173.21	3.15	3.15	13.31	131.37
436	43.60	175.66	3.20	3.20	13.10	131.44
437	43.70	181.13	3.30	3.30	12.91	131.72
438	43.80	187.55	3.44	3.44	12.77	132.14
439	43.90	194.31	3.67	3.67	12.73	132.63
440	44.00	199.87	3.90	3.90	12.73	133.05
441	44.10	203.26	3.98	3.98	12.68	133.26
442	44.20	203.67	3.93	3.93	12.49	133.20
443	44.30	203.85	3.78	3.78	12.25	133.08
444	44.40	206.73	3.78	3.78	12.11	133.13
445	44.50	210.23	3.96	3.96	12.14	133.41
446	44.60	214.11	4.18	4.18	12.19	133.72
447	44.70	217.87	4.22	4.22	12.11	133.91
448	44.80	220.77	4.22	4.22	11.83	133.96
449	44.90	225.92	4.18	4.18	11.37	133.95
450	45.00	234.12	4.11	4.11	10.86	134.00
451	45.10	241.83	4.18	4.18	10.53	134.05
452	45.20	241.32	4.17	4.17	10.53	133.95
453	45.30	230.23	3.98	3.98	10.82	133.58
454	45.40	215.31	3.72	3.72	11.24	132.95
455	45.50	200.43	3.40	3.40	11.61	132.20
456	45.60	190.45	3.12	3.12	11.63	131.52
457	45.70	190.71	2.94	2.94	11.19	131.06
458	45.80	197.95	2.84	2.84	10.39	130.98
459	45.90	213.53	2.91	2.91	9.54	131.34
460	46.00	233.97	3.17	3.17	8.89	132.05
461	46.10	252.54	3.49	3.49	8.48	132.96
462	46.20	271.60	3.88	3.88	8.21	133.78
463	46.30	287.27	4.16	4.16	7.93	134.37
464	46.40	298.42	4.24	4.24	7.59	134.63
465	46.50	305.26	4.17	4.17	7.29	134.72
466	46.60	310.07	4.20	4.20	7.18	134.85
467	46.70	313.73	4.40	4.40	7.27	135.09
468	46.80	313.58	4.54	4.54	7.46	135.25
469	46.90	308.86	4.49	4.49	7.70	135.28
470	47.00	302.35	4.52	4.52	8.00	135.25
471	47.10	294.37	4.56	4.56	8.46	135.26
472	47.20	285.17	4.63	4.63	9.01	135.27
473	47.30	274.90	4.68	4.68	9.52	135.19
474	47.40	265.74	4.57	4.57	9.83	134.92
475	47.50	257.78	4.28	4.28	9.81	134.42
476	47.60	251.30	3.91	3.91	9.43	133.66
477	47.70	246.83	3.43	3.43	8.75	132.71
478	47.80	244.57	2.93	2.93	7.96	131.76
479	47.90	244.45	2.69	2.69	7.77	131.31
480	48.00	236.24	2.93	2.93	8.92	131.77

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
481	48.10	214.58	3.60	3.60	11.71	132.58
482	48.20	176.62	4.13	4.13	16.08	132.93
483	48.30	132.04	4.15	4.15	21.80	132.17
484	48.40	91.43	3.43	3.43	28.47	130.09
485	48.50	61.13	2.30	2.30	33.74	127.75
486	48.60	61.75	2.15	2.15	36.51	126.01
487	48.70	58.17	2.12	2.12	38.91	124.62
488	48.80	38.33	1.41	1.41	40.60	123.43
489	48.90	46.32	1.47	1.47	37.70	122.71
490	49.00	63.04	1.60	1.60	29.79	124.01
491	49.10	86.60	1.80	1.80	23.02	125.52
492	49.20	114.00	2.02	2.02	18.73	127.07
493	49.30	135.60	2.36	2.36	16.51	128.59
494	49.40	151.25	2.79	2.79	15.38	129.88
495	49.50	166.37	3.06	3.06	14.06	130.52
496	49.60	181.99	2.82	2.82	12.19	130.80
497	49.70	207.38	2.81	2.81	10.16	131.02
498	49.80	236.80	2.98	2.98	8.69	131.33
499	49.90	249.95	2.90	2.90	7.92	131.55

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q _c :	Measured cone resistance (tsf)
f _s :	Sleeve friction resistance (tsf)
u:	Pore pressure (tsf)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (pcf)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1	0.10	0.01	0.00	0.01	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
2	0.20	0.01	0.00	0.01	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
3	0.30	0.02	0.00	0.02	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
4	0.40	0.02	0.00	0.02	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
5	0.50	0.03	0.00	0.03	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
6	0.60	0.04	0.00	0.04	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
7	0.70	0.04	0.00	0.04	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
8	0.80	0.05	0.00	0.05	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
9	0.90	0.05	0.00	0.05	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
10	1.00	0.06	0.00	0.06	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
11	1.10	0.07	0.00	0.07	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
12	1.20	0.07	0.00	0.07	1.00	0.481	1.06	0.455	1.00	1.30	2.000	Yes
13	1.30	0.08	0.00	0.08	1.00	0.480	1.06	0.455	1.00	1.30	2.000	Yes
14	1.40	0.08	0.00	0.08	1.00	0.480	1.06	0.455	1.00	1.30	2.000	Yes
15	1.50	0.09	0.00	0.09	1.00	0.480	1.06	0.455	1.00	1.30	2.000	Yes
16	1.60	0.09	0.00	0.09	1.00	0.480	1.06	0.455	1.00	1.30	2.000	Yes
17	1.70	0.10	0.00	0.10	1.00	0.480	1.06	0.454	1.00	1.30	2.000	Yes
18	1.80	0.11	0.00	0.11	1.00	0.480	1.06	0.454	1.00	1.30	2.000	Yes
19	1.90	0.11	0.00	0.11	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
20	2.00	0.12	0.00	0.12	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
21	2.10	0.12	0.00	0.12	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
22	2.20	0.13	0.00	0.13	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
23	2.30	0.13	0.00	0.13	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
24	2.40	0.14	0.00	0.14	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
25	2.50	0.15	0.00	0.15	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
26	2.60	0.15	0.00	0.15	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
27	2.70	0.16	0.00	0.16	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
28	2.80	0.16	0.00	0.16	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
29	2.90	0.17	0.00	0.17	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
30	3.00	0.17	0.00	0.17	0.99	0.479	1.06	0.453	1.00	1.30	2.000	No
31	3.10	0.18	0.00	0.18	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
32	3.20	0.19	0.00	0.19	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
33	3.30	0.19	0.00	0.19	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
34	3.40	0.20	0.00	0.20	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
35	3.50	0.20	0.00	0.20	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
36	3.60	0.21	0.00	0.21	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
37	3.70	0.21	0.00	0.21	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
38	3.80	0.22	0.00	0.22	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
39	3.90	0.22	0.00	0.22	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
40	4.00	0.23	0.00	0.23	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
41	4.10	0.24	0.00	0.24	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
42	4.20	0.24	0.00	0.24	0.99	0.477	1.06	0.452	1.00	1.30	2.000	Yes
43	4.30	0.25	0.00	0.25	0.99	0.477	1.06	0.452	1.00	1.30	2.000	Yes
44	4.40	0.25	0.00	0.25	0.99	0.477	1.06	0.452	1.00	1.30	2.000	Yes
45	4.50	0.26	0.00	0.26	0.99	0.477	1.06	0.451	1.00	1.30	2.000	Yes
46	4.60	0.26	0.00	0.26	0.99	0.477	1.06	0.451	1.00	1.30	2.000	Yes
47	4.70	0.27	0.00	0.27	0.99	0.477	1.06	0.451	1.00	1.30	2.000	Yes
48	4.80	0.28	0.00	0.28	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
49	4.90	0.28	0.00	0.28	0.99	0.476	1.06	0.451	1.00	1.30	2.000	Yes
50	5.00	0.29	0.00	0.29	0.99	0.476	1.06	0.451	1.00	1.30	2.000	Yes
51	5.10	0.29	0.00	0.29	0.99	0.476	1.06	0.451	1.00	1.30	2.000	Yes
52	5.20	0.30	0.00	0.30	0.99	0.476	1.06	0.451	1.00	1.30	2.000	Yes
53	5.30	0.30	0.00	0.30	0.99	0.476	1.06	0.451	1.00	1.30	2.000	Yes
54	5.40	0.31	0.00	0.31	0.99	0.476	1.06	0.450	1.00	1.30	2.000	Yes
55	5.50	0.32	0.00	0.32	0.99	0.476	1.06	0.450	1.00	1.30	2.000	Yes
56	5.60	0.32	0.00	0.32	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
57	5.70	0.33	0.00	0.33	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
58	5.80	0.33	0.00	0.33	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
59	5.90	0.34	0.00	0.34	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
60	6.00	0.34	0.00	0.34	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
61	6.10	0.35	0.00	0.35	0.99	0.475	1.06	0.450	1.00	1.30	2.000	Yes
62	6.20	0.35	0.00	0.35	0.99	0.475	1.06	0.450	1.00	1.30	2.000	Yes
63	6.30	0.36	0.00	0.36	0.99	0.475	1.06	0.450	1.00	1.30	2.000	Yes
64	6.40	0.36	0.00	0.36	0.99	0.475	1.06	0.449	1.00	1.30	2.000	Yes
65	6.50	0.37	0.00	0.37	0.99	0.475	1.06	0.449	1.00	1.30	2.000	Yes
66	6.60	0.38	0.00	0.38	0.99	0.475	1.06	0.449	1.00	1.30	2.000	Yes
67	6.70	0.38	0.00	0.38	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
68	6.80	0.39	0.00	0.39	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
69	6.90	0.39	0.00	0.39	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
70	7.00	0.40	0.00	0.40	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
71	7.10	0.40	0.00	0.40	0.99	0.474	1.06	0.449	1.00	1.30	2.000	Yes
72	7.20	0.41	0.00	0.41	0.99	0.474	1.06	0.449	1.00	1.30	2.000	Yes
73	7.30	0.42	0.00	0.42	0.99	0.474	1.06	0.449	1.00	1.30	2.000	Yes
74	7.40	0.42	0.00	0.42	0.98	0.474	1.06	0.448	1.00	1.30	2.000	Yes
75	7.50	0.43	0.00	0.43	0.98	0.474	1.06	0.448	1.00	1.30	2.000	Yes
76	7.60	0.43	0.00	0.43	0.98	0.473	1.06	0.448	1.00	1.30	2.000	Yes
77	7.70	0.44	0.00	0.44	0.98	0.473	1.06	0.448	1.00	1.30	2.000	Yes
78	7.80	0.44	0.00	0.44	0.98	0.473	1.06	0.448	1.00	1.30	2.000	Yes
79	7.90	0.45	0.00	0.45	0.98	0.473	1.06	0.448	1.00	1.30	2.000	Yes
80	8.00	0.46	0.00	0.46	0.98	0.473	1.06	0.448	1.00	1.30	2.000	Yes
81	8.10	0.46	0.00	0.46	0.98	0.476	1.06	0.451	1.00	1.30	2.000	Yes
82	8.20	0.47	0.01	0.46	0.98	0.479	1.06	0.454	1.00	1.30	2.000	Yes
83	8.30	0.47	0.01	0.46	0.98	0.482	1.06	0.457	1.00	1.30	2.000	Yes
84	8.40	0.48	0.01	0.47	0.98	0.485	1.06	0.459	1.00	1.30	2.000	Yes
85	8.50	0.48	0.02	0.47	0.98	0.488	1.06	0.462	1.00	1.30	2.000	Yes
86	8.60	0.49	0.02	0.47	0.98	0.491	1.06	0.465	1.00	1.30	2.000	Yes
87	8.70	0.49	0.02	0.47	0.98	0.494	1.06	0.468	1.00	1.30	0.608	No
88	8.80	0.50	0.02	0.48	0.98	0.497	1.06	0.470	1.00	1.30	0.612	No
89	8.90	0.51	0.03	0.48	0.98	0.500	1.06	0.473	1.00	1.30	2.000	Yes
90	9.00	0.51	0.03	0.48	0.98	0.503	1.06	0.476	1.00	1.30	2.000	Yes
91	9.10	0.52	0.03	0.48	0.98	0.505	1.06	0.478	1.00	1.30	2.000	Yes
92	9.20	0.52	0.04	0.49	0.98	0.508	1.06	0.481	1.00	1.30	2.000	Yes
93	9.30	0.53	0.04	0.49	0.98	0.511	1.06	0.484	1.00	1.30	0.629	No
94	9.40	0.53	0.04	0.49	0.98	0.514	1.06	0.486	1.00	1.30	0.632	No
95	9.50	0.54	0.05	0.49	0.98	0.516	1.06	0.489	1.00	1.30	0.635	No
96	9.60	0.55	0.05	0.50	0.98	0.519	1.06	0.491	1.00	1.30	0.639	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
97	9.70	0.55	0.05	0.50	0.98	0.521	1.06	0.494	1.00	1.30	0.642	No
98	9.80	0.56	0.06	0.50	0.98	0.524	1.06	0.496	1.00	1.30	0.645	No
99	9.90	0.56	0.06	0.50	0.98	0.527	1.06	0.498	1.00	1.30	0.648	No
100	10.00	0.57	0.06	0.51	0.98	0.529	1.06	0.501	1.00	1.30	0.651	No
101	10.10	0.57	0.07	0.51	0.98	0.532	1.06	0.503	1.00	1.30	0.654	No
102	10.20	0.58	0.07	0.51	0.98	0.534	1.06	0.506	1.00	1.30	0.657	No
103	10.30	0.58	0.07	0.51	0.98	0.537	1.06	0.508	1.00	1.30	0.660	No
104	10.40	0.59	0.07	0.51	0.98	0.539	1.06	0.510	1.00	1.30	0.663	No
105	10.50	0.60	0.08	0.52	0.98	0.541	1.06	0.512	1.00	1.30	0.666	No
106	10.60	0.60	0.08	0.52	0.98	0.544	1.06	0.515	1.00	1.30	0.669	No
107	10.70	0.61	0.08	0.52	0.98	0.546	1.06	0.517	1.00	1.30	0.672	No
108	10.80	0.61	0.09	0.52	0.98	0.548	1.06	0.519	1.00	1.30	0.675	No
109	10.90	0.62	0.09	0.53	0.98	0.551	1.06	0.521	1.00	1.30	0.678	No
110	11.00	0.62	0.09	0.53	0.98	0.553	1.06	0.524	1.00	1.30	0.681	No
111	11.10	0.63	0.10	0.53	0.98	0.555	1.06	0.526	1.00	1.30	0.683	No
112	11.20	0.63	0.10	0.53	0.98	0.558	1.06	0.528	1.00	1.30	0.686	No
113	11.30	0.64	0.10	0.54	0.98	0.560	1.06	0.530	1.00	1.30	0.689	No
114	11.40	0.64	0.11	0.54	0.98	0.562	1.06	0.532	1.00	1.30	0.692	No
115	11.50	0.65	0.11	0.54	0.98	0.565	1.06	0.534	1.00	1.30	0.695	No
116	11.60	0.65	0.11	0.54	0.98	0.567	1.06	0.537	1.00	1.30	0.698	No
117	11.70	0.66	0.12	0.54	0.98	0.569	1.06	0.539	1.00	1.30	0.700	No
118	11.80	0.66	0.12	0.54	0.98	0.571	1.06	0.541	1.00	1.30	0.703	No
119	11.90	0.67	0.12	0.55	0.98	0.574	1.06	0.543	1.00	1.30	0.706	No
120	12.00	0.67	0.12	0.55	0.97	0.576	1.06	0.545	1.00	1.30	0.709	No
121	12.10	0.68	0.13	0.55	0.97	0.578	1.06	0.547	1.00	1.30	0.711	No
122	12.20	0.68	0.13	0.55	0.97	0.580	1.06	0.549	1.00	1.30	0.714	No
123	12.30	0.69	0.13	0.55	0.97	0.582	1.06	0.551	1.00	1.30	0.716	No
124	12.40	0.69	0.14	0.56	0.97	0.584	1.06	0.553	1.00	1.30	0.719	No
125	12.50	0.70	0.14	0.56	0.97	0.586	1.06	0.555	1.00	1.30	0.722	No
126	12.60	0.70	0.14	0.56	0.97	0.588	1.06	0.557	1.00	1.30	0.724	No
127	12.70	0.71	0.15	0.56	0.97	0.590	1.06	0.559	1.00	1.30	0.727	No
128	12.80	0.71	0.15	0.56	0.97	0.592	1.06	0.561	1.00	1.30	0.729	No
129	12.90	0.72	0.15	0.57	0.97	0.594	1.06	0.563	1.00	1.30	0.731	No
130	13.00	0.72	0.16	0.57	0.97	0.596	1.06	0.565	1.00	1.30	0.734	No
131	13.10	0.73	0.16	0.57	0.97	0.598	1.06	0.566	1.00	1.30	0.736	No
132	13.20	0.73	0.16	0.57	0.97	0.600	1.06	0.568	1.00	1.30	0.739	No
133	13.30	0.74	0.17	0.57	0.97	0.602	1.06	0.570	1.00	1.30	0.741	No
134	13.40	0.75	0.17	0.58	0.97	0.604	1.06	0.572	1.00	1.30	0.743	No
135	13.50	0.75	0.17	0.58	0.97	0.606	1.06	0.574	1.00	1.30	0.746	No
136	13.60	0.76	0.17	0.58	0.97	0.608	1.06	0.576	1.00	1.30	0.748	No
137	13.70	0.76	0.18	0.58	0.97	0.610	1.06	0.577	1.00	1.30	0.751	No
138	13.80	0.77	0.18	0.58	0.97	0.612	1.06	0.579	1.00	1.30	0.753	No
139	13.90	0.77	0.18	0.59	0.97	0.614	1.06	0.581	1.00	1.30	0.755	No
140	14.00	0.78	0.19	0.59	0.97	0.616	1.06	0.583	1.00	1.30	0.758	No
141	14.10	0.78	0.19	0.59	0.97	0.617	1.06	0.584	1.00	1.30	0.760	No
142	14.20	0.79	0.19	0.59	0.97	0.619	1.06	0.586	1.00	1.30	0.762	No
143	14.30	0.79	0.20	0.59	0.97	0.621	1.06	0.588	1.00	1.30	0.764	No
144	14.40	0.79	0.20	0.60	0.97	0.623	1.06	0.590	1.00	1.30	0.767	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
145	14.50	0.80	0.20	0.60	0.97	0.625	1.06	0.591	1.00	1.30	0.769	No
146	14.60	0.80	0.21	0.60	0.97	0.627	1.06	0.593	1.00	1.30	0.771	No
147	14.70	0.81	0.21	0.60	0.97	0.628	1.06	0.595	1.00	1.30	0.773	No
148	14.80	0.81	0.21	0.60	0.97	0.630	1.06	0.597	1.00	1.30	0.776	No
149	14.90	0.82	0.22	0.60	0.97	0.632	1.06	0.598	1.00	1.30	0.778	No
150	15.00	0.83	0.22	0.61	0.97	0.634	1.06	0.600	1.00	1.30	0.780	No
151	15.10	0.83	0.22	0.61	0.97	0.635	1.06	0.601	1.00	1.30	0.782	No
152	15.20	0.84	0.22	0.61	0.97	0.637	1.06	0.603	1.00	1.30	0.784	No
153	15.30	0.84	0.23	0.61	0.97	0.638	1.06	0.604	1.00	1.30	2.000	Yes
154	15.40	0.85	0.23	0.62	0.97	0.640	1.06	0.606	1.00	1.30	2.000	Yes
155	15.50	0.85	0.23	0.62	0.97	0.641	1.06	0.607	1.00	1.30	2.000	Yes
156	15.60	0.86	0.24	0.62	0.97	0.642	1.06	0.608	1.00	1.30	2.000	Yes
157	15.70	0.87	0.24	0.63	0.97	0.644	1.06	0.609	1.00	1.30	2.000	Yes
158	15.80	0.87	0.24	0.63	0.97	0.645	1.06	0.611	1.00	1.30	2.000	Yes
159	15.90	0.88	0.25	0.63	0.97	0.646	1.06	0.612	1.00	1.30	2.000	Yes
160	16.00	0.88	0.25	0.63	0.97	0.648	1.06	0.613	1.00	1.30	2.000	Yes
161	16.10	0.89	0.25	0.64	0.97	0.649	1.06	0.614	1.00	1.30	0.798	No
162	16.20	0.90	0.26	0.64	0.97	0.650	1.06	0.615	1.00	1.30	0.800	No
163	16.30	0.90	0.26	0.64	0.97	0.651	1.06	0.616	1.00	1.30	0.801	No
164	16.40	0.91	0.26	0.65	0.97	0.652	1.06	0.618	1.00	1.30	2.000	Yes
165	16.50	0.92	0.27	0.65	0.97	0.654	1.06	0.619	1.00	1.30	2.000	Yes
166	16.60	0.92	0.27	0.65	0.97	0.655	1.06	0.620	1.00	1.30	2.000	Yes
167	16.70	0.93	0.27	0.66	0.96	0.656	1.06	0.621	1.00	1.30	2.000	Yes
168	16.80	0.93	0.27	0.66	0.96	0.657	1.06	0.622	1.00	1.30	2.000	Yes
169	16.90	0.94	0.28	0.66	0.96	0.658	1.06	0.623	1.00	1.30	2.000	Yes
170	17.00	0.95	0.28	0.67	0.96	0.659	1.06	0.624	1.00	1.30	2.000	Yes
171	17.10	0.95	0.28	0.67	0.96	0.661	1.06	0.625	1.00	1.30	2.000	Yes
172	17.20	0.96	0.29	0.67	0.96	0.662	1.06	0.627	1.00	1.30	2.000	Yes
173	17.30	0.96	0.29	0.67	0.96	0.663	1.06	0.628	1.00	1.30	0.816	No
174	17.40	0.97	0.29	0.67	0.96	0.665	1.06	0.629	1.00	1.30	0.818	No
175	17.50	0.97	0.30	0.68	0.96	0.666	1.06	0.631	1.00	1.30	0.820	No
176	17.60	0.98	0.30	0.68	0.96	0.667	1.06	0.632	1.00	1.30	0.821	No
177	17.70	0.98	0.30	0.68	0.96	0.669	1.06	0.633	1.00	1.30	0.823	No
178	17.80	0.99	0.31	0.68	0.96	0.670	1.06	0.634	1.00	1.30	0.825	No
179	17.90	0.99	0.31	0.68	0.96	0.672	1.06	0.636	1.00	1.30	0.827	No
180	18.00	1.00	0.31	0.69	0.96	0.673	1.06	0.637	1.00	1.30	0.828	No
181	18.10	1.00	0.32	0.69	0.96	0.674	1.06	0.638	1.00	1.30	0.830	No
182	18.20	1.01	0.32	0.69	0.96	0.676	1.06	0.640	1.00	1.30	0.831	No
183	18.30	1.01	0.32	0.69	0.96	0.677	1.06	0.641	1.00	1.30	0.833	No
184	18.40	1.02	0.32	0.69	0.96	0.678	1.06	0.642	1.00	1.30	0.835	No
185	18.50	1.02	0.33	0.70	0.96	0.679	1.06	0.643	1.00	1.30	0.836	No
186	18.60	1.03	0.33	0.70	0.96	0.680	1.06	0.644	1.00	1.30	0.837	No
187	18.70	1.04	0.33	0.70	0.96	0.682	1.06	0.645	1.00	1.30	0.839	No
188	18.80	1.04	0.34	0.70	0.96	0.683	1.06	0.646	1.00	1.30	0.840	No
189	18.90	1.05	0.34	0.71	0.96	0.684	1.06	0.647	1.00	1.30	0.841	No
190	19.00	1.05	0.34	0.71	0.96	0.685	1.06	0.648	1.00	1.30	0.843	No
191	19.10	1.06	0.35	0.71	0.96	0.686	1.06	0.649	1.00	1.30	0.844	No
192	19.20	1.06	0.35	0.71	0.96	0.687	1.06	0.650	1.00	1.30	0.845	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
193	19.30	1.07	0.35	0.72	0.96	0.688	1.06	0.651	1.00	1.30	0.846	No
194	19.40	1.08	0.36	0.72	0.96	0.689	1.06	0.652	1.00	1.30	0.848	No
195	19.50	1.08	0.36	0.72	0.96	0.690	1.06	0.653	1.00	1.30	0.849	No
196	19.60	1.09	0.36	0.73	0.96	0.691	1.06	0.654	1.00	1.30	0.850	No
197	19.70	1.09	0.37	0.73	0.96	0.692	1.06	0.655	1.00	1.30	0.851	No
198	19.80	1.10	0.37	0.73	0.96	0.693	1.06	0.656	1.00	1.30	0.852	No
199	19.90	1.10	0.37	0.73	0.96	0.693	1.06	0.656	1.00	1.30	0.853	No
200	20.00	1.11	0.37	0.74	0.96	0.694	1.06	0.657	1.00	1.30	0.855	No
201	20.10	1.12	0.38	0.74	0.96	0.695	1.06	0.658	1.00	1.30	0.856	No
202	20.20	1.12	0.38	0.74	0.96	0.696	1.06	0.659	1.00	1.30	0.857	No
203	20.30	1.13	0.38	0.74	0.96	0.697	1.06	0.660	1.00	1.30	0.858	No
204	20.40	1.13	0.39	0.75	0.96	0.698	1.06	0.661	1.00	1.30	0.859	No
205	20.50	1.14	0.39	0.75	0.96	0.699	1.06	0.662	1.00	1.30	0.861	No
206	20.60	1.14	0.39	0.75	0.96	0.701	1.06	0.663	1.00	1.30	0.862	No
207	20.70	1.15	0.40	0.75	0.96	0.702	1.06	0.664	1.00	1.30	0.864	No
208	20.80	1.15	0.40	0.75	0.95	0.703	1.06	0.665	1.00	1.30	0.865	No
209	20.90	1.16	0.40	0.76	0.95	0.704	1.06	0.666	1.00	1.30	0.866	No
210	21.00	1.16	0.41	0.76	0.95	0.705	1.06	0.667	1.00	1.30	0.867	No
211	21.10	1.17	0.41	0.76	0.95	0.706	1.06	0.668	1.00	1.30	0.869	No
212	21.20	1.17	0.41	0.76	0.95	0.707	1.06	0.669	1.00	1.30	0.870	No
213	21.30	1.18	0.41	0.76	0.95	0.708	1.06	0.670	1.00	1.30	0.871	No
214	21.40	1.18	0.42	0.77	0.95	0.709	1.06	0.671	1.00	1.30	0.872	No
215	21.50	1.19	0.42	0.77	0.95	0.710	1.06	0.672	1.00	1.30	0.873	No
216	21.60	1.19	0.42	0.77	0.95	0.711	1.06	0.673	1.00	1.30	0.875	No
217	21.70	1.20	0.43	0.77	0.95	0.712	1.06	0.674	1.00	1.30	0.876	No
218	21.80	1.21	0.43	0.77	0.95	0.712	1.06	0.674	1.00	1.30	0.877	No
219	21.90	1.21	0.43	0.78	0.95	0.713	1.06	0.675	1.00	1.30	0.878	No
220	22.00	1.22	0.44	0.78	0.95	0.714	1.06	0.676	1.00	1.30	0.879	No
221	22.10	1.22	0.44	0.78	0.95	0.715	1.06	0.677	1.00	1.30	0.880	No
222	22.20	1.23	0.44	0.78	0.95	0.716	1.06	0.678	1.00	1.30	0.881	No
223	22.30	1.23	0.45	0.79	0.95	0.717	1.06	0.679	1.00	1.30	0.882	No
224	22.40	1.24	0.45	0.79	0.95	0.718	1.06	0.679	1.00	1.30	0.883	No
225	22.50	1.24	0.45	0.79	0.95	0.718	1.06	0.680	1.00	1.30	0.884	No
226	22.60	1.25	0.46	0.79	0.95	0.719	1.06	0.681	1.00	1.30	0.885	No
227	22.70	1.25	0.46	0.80	0.95	0.720	1.06	0.681	1.00	1.30	0.886	No
228	22.80	1.26	0.46	0.80	0.95	0.720	1.06	0.682	1.00	1.30	0.886	No
229	22.90	1.27	0.46	0.80	0.95	0.721	1.06	0.682	1.00	1.30	0.887	No
230	23.00	1.27	0.47	0.80	0.95	0.721	1.06	0.683	1.00	1.30	0.888	No
231	23.10	1.28	0.47	0.81	0.95	0.722	1.06	0.683	1.00	1.30	0.889	No
232	23.20	1.29	0.47	0.81	0.95	0.723	1.06	0.684	1.00	1.30	0.889	No
233	23.30	1.29	0.48	0.81	0.95	0.723	1.06	0.684	1.00	1.30	0.890	No
234	23.40	1.30	0.48	0.82	0.95	0.724	1.06	0.685	1.00	1.30	0.890	No
235	23.50	1.30	0.48	0.82	0.95	0.724	1.06	0.685	1.00	1.30	0.891	No
236	23.60	1.31	0.49	0.82	0.95	0.725	1.06	0.686	1.00	1.30	2.000	Yes
237	23.70	1.32	0.49	0.83	0.95	0.725	1.06	0.686	1.00	1.30	2.000	Yes
238	23.80	1.32	0.49	0.83	0.95	0.726	1.06	0.687	1.00	1.30	2.000	Yes
239	23.90	1.33	0.50	0.83	0.95	0.726	1.06	0.687	1.00	1.30	2.000	Yes
240	24.00	1.33	0.50	0.84	0.95	0.726	1.06	0.688	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
241	24.10	1.34	0.50	0.84	0.94	0.727	1.06	0.688	1.00	1.30	2.000	Yes
242	24.20	1.35	0.51	0.84	0.94	0.727	1.06	0.688	1.00	1.30	2.000	Yes
243	24.30	1.35	0.51	0.84	0.94	0.728	1.06	0.689	1.00	1.30	2.000	Yes
244	24.40	1.36	0.51	0.85	0.94	0.728	1.06	0.689	1.00	1.30	2.000	Yes
245	24.50	1.37	0.51	0.85	0.94	0.728	1.06	0.690	1.00	1.30	2.000	Yes
246	24.60	1.37	0.52	0.85	0.94	0.729	1.06	0.690	1.00	1.30	0.897	No
247	24.70	1.38	0.52	0.86	0.94	0.729	1.06	0.690	1.00	1.30	0.897	No
248	24.80	1.39	0.52	0.86	0.94	0.729	1.06	0.690	1.00	1.30	0.897	No
249	24.90	1.39	0.53	0.86	0.94	0.730	1.06	0.691	1.00	1.30	0.898	No
250	25.00	1.40	0.53	0.87	0.94	0.730	1.06	0.691	1.00	1.30	0.898	No
251	25.10	1.40	0.53	0.87	0.94	0.730	1.06	0.691	1.00	1.30	0.899	No
252	25.20	1.41	0.54	0.87	0.94	0.731	1.06	0.692	1.00	1.30	0.899	No
253	25.30	1.42	0.54	0.88	0.94	0.731	1.06	0.692	1.00	1.30	0.899	No
254	25.40	1.42	0.54	0.88	0.94	0.731	1.06	0.692	1.00	1.30	2.000	Yes
255	25.50	1.43	0.55	0.88	0.94	0.731	1.06	0.692	1.00	1.30	2.000	Yes
256	25.60	1.44	0.55	0.89	0.94	0.732	1.06	0.693	1.00	1.30	2.000	Yes
257	25.70	1.44	0.55	0.89	0.94	0.732	1.06	0.693	1.00	1.30	2.000	Yes
258	25.80	1.45	0.56	0.89	0.94	0.732	1.06	0.693	1.00	1.30	2.000	Yes
259	25.90	1.46	0.56	0.90	0.94	0.733	1.06	0.693	1.00	1.30	2.000	Yes
260	26.00	1.46	0.56	0.90	0.94	0.733	1.06	0.694	1.00	1.30	2.000	Yes
261	26.10	1.47	0.56	0.90	0.94	0.733	1.06	0.694	1.00	1.30	0.902	No
262	26.20	1.47	0.57	0.91	0.94	0.734	1.06	0.695	1.00	1.30	0.903	No
263	26.30	1.48	0.57	0.91	0.94	0.734	1.06	0.695	1.00	1.30	0.904	No
264	26.40	1.48	0.57	0.91	0.94	0.735	1.06	0.695	1.00	1.30	0.904	No
265	26.50	1.49	0.58	0.91	0.94	0.735	1.06	0.696	1.00	1.30	0.905	No
266	26.60	1.50	0.58	0.92	0.94	0.736	1.06	0.696	1.00	1.30	0.905	No
267	26.70	1.50	0.58	0.92	0.94	0.736	1.06	0.697	1.00	1.30	0.906	No
268	26.80	1.51	0.59	0.92	0.94	0.736	1.06	0.697	1.00	1.30	0.906	No
269	26.90	1.51	0.59	0.92	0.93	0.737	1.06	0.697	1.00	1.30	0.907	No
270	27.00	1.52	0.59	0.93	0.93	0.737	1.06	0.698	1.00	1.30	0.907	No
271	27.10	1.52	0.60	0.93	0.93	0.737	1.06	0.698	1.00	1.30	0.908	No
272	27.20	1.53	0.60	0.93	0.93	0.738	1.06	0.699	1.00	1.30	0.908	No
273	27.30	1.54	0.60	0.93	0.93	0.738	1.06	0.699	1.00	1.30	0.909	No
274	27.40	1.54	0.61	0.94	0.93	0.739	1.06	0.699	1.00	1.30	0.909	No
275	27.50	1.55	0.61	0.94	0.93	0.739	1.06	0.700	1.00	1.30	0.910	No
276	27.60	1.55	0.61	0.94	0.93	0.740	1.06	0.700	1.00	1.30	0.910	No
277	27.70	1.56	0.61	0.94	0.93	0.740	1.06	0.700	1.00	1.30	0.911	No
278	27.80	1.56	0.62	0.95	0.93	0.740	1.06	0.701	1.00	1.30	0.911	No
279	27.90	1.57	0.62	0.95	0.93	0.741	1.06	0.701	1.00	1.30	0.912	No
280	28.00	1.57	0.62	0.95	0.93	0.741	1.06	0.702	1.00	1.30	0.912	No
281	28.10	1.58	0.63	0.95	0.93	0.741	1.06	0.702	1.00	1.30	0.912	No
282	28.20	1.59	0.63	0.96	0.93	0.742	1.06	0.702	1.00	1.30	0.913	No
283	28.30	1.59	0.63	0.96	0.93	0.742	1.06	0.702	1.00	1.30	0.913	No
284	28.40	1.60	0.64	0.96	0.93	0.742	1.06	0.703	1.00	1.30	0.913	No
285	28.50	1.60	0.64	0.96	0.93	0.742	1.06	0.703	1.00	1.30	0.914	No
286	28.60	1.61	0.64	0.97	0.93	0.742	1.06	0.703	1.00	1.30	0.914	No
287	28.70	1.62	0.65	0.97	0.93	0.743	1.06	0.703	1.00	1.30	0.914	No
288	28.80	1.62	0.65	0.97	0.93	0.743	1.06	0.703	1.00	1.30	0.914	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
289	28.90	1.63	0.65	0.98	0.93	0.743	1.06	0.703	1.00	1.30	2.000	Yes
290	29.00	1.63	0.66	0.98	0.93	0.743	1.06	0.703	1.00	1.30	2.000	Yes
291	29.10	1.64	0.66	0.98	0.92	0.743	1.06	0.703	1.00	1.30	2.000	Yes
292	29.20	1.65	0.66	0.99	0.92	0.743	1.06	0.704	1.00	1.30	2.000	Yes
293	29.30	1.65	0.66	0.99	0.92	0.743	1.06	0.704	1.00	1.30	2.000	Yes
294	29.40	1.66	0.67	0.99	0.92	0.743	1.06	0.704	1.00	1.30	2.000	Yes
295	29.50	1.67	0.67	1.00	0.92	0.743	1.06	0.704	1.00	1.30	2.000	Yes
296	29.60	1.67	0.67	1.00	0.92	0.743	1.06	0.704	1.00	1.30	2.000	Yes
297	29.70	1.68	0.68	1.00	0.92	0.743	1.06	0.704	1.00	1.30	0.915	No
298	29.80	1.69	0.68	1.01	0.92	0.743	1.06	0.703	1.00	1.30	0.915	No
299	29.90	1.69	0.68	1.01	0.92	0.743	1.06	0.703	1.00	1.30	0.914	No
300	30.00	1.70	0.69	1.01	0.92	0.743	1.06	0.703	1.00	1.30	0.914	No
301	30.10	1.71	0.69	1.02	0.92	0.743	1.06	0.703	1.00	1.30	0.914	No
302	30.20	1.71	0.69	1.02	0.92	0.743	1.06	0.703	1.00	1.30	0.914	No
303	30.30	1.72	0.70	1.02	0.92	0.743	1.06	0.703	1.00	1.30	0.914	No
304	30.40	1.73	0.70	1.03	0.92	0.743	1.06	0.703	1.00	1.30	0.914	No
305	30.50	1.73	0.70	1.03	0.92	0.743	1.06	0.703	1.00	1.30	2.000	Yes
306	30.60	1.74	0.71	1.03	0.92	0.743	1.06	0.703	1.00	1.30	2.000	Yes
307	30.70	1.74	0.71	1.04	0.92	0.743	1.06	0.703	1.00	1.30	2.000	Yes
308	30.80	1.75	0.71	1.04	0.92	0.742	1.06	0.703	1.00	1.30	2.000	Yes
309	30.90	1.76	0.71	1.04	0.92	0.742	1.06	0.703	1.00	1.30	2.000	Yes
310	31.00	1.76	0.72	1.05	0.92	0.742	1.06	0.703	1.00	1.30	2.000	Yes
311	31.10	1.77	0.72	1.05	0.91	0.742	1.06	0.703	1.00	1.30	2.000	Yes
312	31.20	1.78	0.72	1.05	0.91	0.742	1.06	0.703	1.00	1.30	0.913	No
313	31.30	1.78	0.73	1.06	0.91	0.742	1.06	0.703	1.00	1.30	0.913	No
314	31.40	1.79	0.73	1.06	0.91	0.742	1.06	0.703	1.00	1.30	0.913	No
315	31.50	1.79	0.73	1.06	0.91	0.742	1.06	0.702	1.00	1.30	2.000	Yes
316	31.60	1.80	0.74	1.07	0.91	0.742	1.06	0.702	1.00	1.30	2.000	Yes
317	31.70	1.81	0.74	1.07	0.91	0.742	1.06	0.702	1.00	1.30	2.000	Yes
318	31.80	1.81	0.74	1.07	0.91	0.742	1.06	0.702	1.00	1.30	2.000	Yes
319	31.90	1.82	0.75	1.08	0.91	0.741	1.06	0.702	1.00	1.30	2.000	Yes
320	32.00	1.83	0.75	1.08	0.91	0.741	1.06	0.702	1.00	1.30	2.000	Yes
321	32.10	1.83	0.75	1.08	0.91	0.741	1.06	0.701	1.00	1.30	2.000	Yes
322	32.20	1.84	0.76	1.09	0.91	0.741	1.06	0.701	1.00	1.30	2.000	Yes
323	32.30	1.85	0.76	1.09	0.91	0.741	1.06	0.701	1.00	1.30	2.000	Yes
324	32.40	1.85	0.76	1.09	0.91	0.740	1.06	0.701	1.00	1.30	2.000	Yes
325	32.50	1.86	0.76	1.10	0.91	0.740	1.06	0.701	1.00	1.30	2.000	Yes
326	32.60	1.87	0.77	1.10	0.91	0.740	1.06	0.701	1.00	1.30	2.000	Yes
327	32.70	1.87	0.77	1.10	0.91	0.740	1.06	0.700	1.00	1.30	2.000	Yes
328	32.80	1.88	0.77	1.11	0.90	0.740	1.06	0.700	1.00	1.30	2.000	Yes
329	32.90	1.89	0.78	1.11	0.90	0.740	1.06	0.700	1.00	1.30	2.000	Yes
330	33.00	1.89	0.78	1.11	0.90	0.740	1.06	0.700	1.00	1.30	0.910	No
331	33.10	1.90	0.78	1.11	0.90	0.740	1.06	0.700	1.00	1.30	0.910	No
332	33.20	1.90	0.79	1.12	0.90	0.739	1.06	0.700	1.00	1.30	0.910	No
333	33.30	1.91	0.79	1.12	0.90	0.739	1.06	0.700	1.00	1.30	0.910	No
334	33.40	1.92	0.79	1.12	0.90	0.739	1.06	0.700	1.00	1.30	0.910	No
335	33.50	1.92	0.80	1.13	0.90	0.739	1.06	0.700	1.00	1.30	0.910	No
336	33.60	1.93	0.80	1.13	0.90	0.739	1.06	0.700	1.00	1.30	0.909	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
337	33.70	1.93	0.80	1.13	0.90	0.739	1.06	0.699	1.00	1.30	0.909	No
338	33.80	1.94	0.80	1.14	0.90	0.739	1.06	0.699	1.00	1.30	0.909	No
339	33.90	1.95	0.81	1.14	0.90	0.738	1.06	0.699	1.00	1.30	0.909	No
340	34.00	1.95	0.81	1.14	0.90	0.738	1.06	0.699	1.00	1.30	0.909	No
341	34.10	1.96	0.81	1.15	0.90	0.738	1.06	0.699	1.00	1.30	0.908	No
342	34.20	1.97	0.82	1.15	0.90	0.738	1.06	0.698	1.00	1.30	0.908	No
343	34.30	1.97	0.82	1.15	0.90	0.738	1.06	0.698	1.00	1.30	2.000	Yes
344	34.40	1.98	0.82	1.15	0.89	0.738	1.06	0.698	1.00	1.30	2.000	Yes
345	34.50	1.98	0.83	1.16	0.89	0.737	1.06	0.698	1.00	1.30	2.000	Yes
346	34.60	1.99	0.83	1.16	0.89	0.737	1.06	0.698	1.00	1.30	2.000	Yes
347	34.70	2.00	0.83	1.16	0.89	0.737	1.06	0.698	1.00	1.30	2.000	Yes
348	34.80	2.00	0.84	1.17	0.89	0.737	1.06	0.697	1.00	1.30	2.000	Yes
349	34.90	2.01	0.84	1.17	0.89	0.736	1.06	0.697	1.00	1.30	2.000	Yes
350	35.00	2.01	0.84	1.17	0.89	0.736	1.06	0.697	1.00	1.30	2.000	Yes
351	35.10	2.02	0.85	1.18	0.89	0.736	1.06	0.697	1.00	1.30	2.000	Yes
352	35.20	2.03	0.85	1.18	0.89	0.736	1.06	0.696	1.00	1.30	2.000	Yes
353	35.30	2.03	0.85	1.18	0.89	0.735	1.06	0.696	1.00	1.30	0.905	No
354	35.40	2.04	0.85	1.18	0.89	0.735	1.06	0.696	1.00	1.30	0.905	No
355	35.50	2.05	0.86	1.19	0.89	0.735	1.06	0.696	1.00	1.30	0.905	No
356	35.60	2.05	0.86	1.19	0.89	0.735	1.06	0.696	1.00	1.30	0.904	No
357	35.70	2.06	0.86	1.19	0.89	0.735	1.06	0.695	1.00	1.30	0.904	No
358	35.80	2.06	0.87	1.20	0.88	0.734	1.06	0.695	1.00	1.30	0.904	No
359	35.90	2.07	0.87	1.20	0.88	0.734	1.06	0.695	1.00	1.30	0.903	No
360	36.00	2.08	0.87	1.20	0.88	0.734	1.06	0.694	1.00	1.30	0.903	No
361	36.10	2.08	0.88	1.21	0.88	0.733	1.06	0.694	1.00	1.30	0.902	No
362	36.20	2.09	0.88	1.21	0.88	0.733	1.06	0.694	1.00	1.30	0.902	No
363	36.30	2.09	0.88	1.21	0.88	0.733	1.06	0.694	1.00	1.30	0.902	No
364	36.40	2.10	0.89	1.22	0.88	0.732	1.06	0.693	1.00	1.30	2.000	Yes
365	36.50	2.11	0.89	1.22	0.88	0.732	1.06	0.693	1.00	1.30	2.000	Yes
366	36.60	2.11	0.89	1.22	0.88	0.732	1.06	0.693	1.00	1.30	2.000	Yes
367	36.70	2.12	0.90	1.22	0.88	0.731	1.06	0.692	1.00	1.30	2.000	Yes
368	36.80	2.13	0.90	1.23	0.88	0.731	1.06	0.692	1.00	1.30	2.000	Yes
369	36.90	2.13	0.90	1.23	0.88	0.731	1.06	0.692	1.00	1.30	2.000	Yes
370	37.00	2.14	0.90	1.23	0.88	0.730	1.06	0.691	1.00	1.30	2.000	Yes
371	37.10	2.14	0.91	1.24	0.88	0.730	1.06	0.691	1.00	1.30	2.000	Yes
372	37.20	2.15	0.91	1.24	0.87	0.730	1.06	0.691	1.00	1.30	2.000	Yes
373	37.30	2.16	0.91	1.24	0.87	0.729	1.06	0.690	1.00	1.30	2.000	Yes
374	37.40	2.16	0.92	1.25	0.87	0.729	1.06	0.690	1.00	1.30	2.000	Yes
375	37.50	2.17	0.92	1.25	0.87	0.728	1.06	0.690	1.00	1.30	2.000	Yes
376	37.60	2.18	0.92	1.25	0.87	0.728	1.06	0.689	1.00	1.30	2.000	Yes
377	37.70	2.18	0.93	1.26	0.87	0.728	1.06	0.689	1.00	1.30	2.000	Yes
378	37.80	2.19	0.93	1.26	0.87	0.727	1.06	0.688	1.00	1.30	2.000	Yes
379	37.90	2.20	0.93	1.26	0.87	0.727	1.06	0.688	1.00	1.30	2.000	Yes
380	38.00	2.20	0.94	1.27	0.87	0.726	1.06	0.688	1.00	1.30	0.894	No
381	38.10	2.21	0.94	1.27	0.87	0.726	1.06	0.687	1.00	1.30	0.893	No
382	38.20	2.21	0.94	1.27	0.87	0.725	1.06	0.687	1.00	1.30	2.000	Yes
383	38.30	2.22	0.95	1.28	0.87	0.725	1.06	0.686	1.00	1.30	2.000	Yes
384	38.40	2.23	0.95	1.28	0.86	0.725	1.06	0.686	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
385	38.50	2.23	0.95	1.28	0.86	0.724	1.06	0.685	1.00	1.30	2.000	Yes
386	38.60	2.24	0.95	1.28	0.86	0.724	1.06	0.685	1.00	1.30	2.000	Yes
387	38.70	2.25	0.96	1.29	0.86	0.723	1.06	0.685	1.00	1.30	2.000	Yes
388	38.80	2.25	0.96	1.29	0.86	0.723	1.06	0.684	1.00	1.30	2.000	Yes
389	38.90	2.26	0.96	1.29	0.86	0.722	1.06	0.684	1.00	1.30	0.889	No
390	39.00	2.26	0.97	1.30	0.86	0.722	1.06	0.683	1.00	1.30	0.888	No
391	39.10	2.27	0.97	1.30	0.86	0.721	1.06	0.683	1.00	1.30	0.888	No
392	39.20	2.28	0.97	1.30	0.86	0.721	1.06	0.682	1.00	1.30	0.887	No
393	39.30	2.28	0.98	1.31	0.86	0.720	1.06	0.682	1.00	1.30	0.887	No
394	39.40	2.29	0.98	1.31	0.86	0.720	1.06	0.682	1.00	1.30	0.886	No
395	39.50	2.30	0.98	1.31	0.86	0.720	1.06	0.681	1.00	1.30	0.886	No
396	39.60	2.30	0.99	1.32	0.85	0.719	1.06	0.681	1.00	1.30	0.885	No
397	39.70	2.31	0.99	1.32	0.85	0.719	1.06	0.680	1.00	1.30	2.000	Yes
398	39.80	2.31	0.99	1.32	0.85	0.718	1.06	0.680	1.00	1.30	2.000	Yes
399	39.90	2.32	1.00	1.32	0.85	0.718	1.06	0.679	1.00	1.30	2.000	Yes
400	40.00	2.33	1.00	1.33	0.85	0.717	1.06	0.679	1.00	1.30	2.000	Yes
401	40.10	2.33	1.00	1.33	0.85	0.717	1.06	0.678	1.00	1.30	0.882	No
402	40.20	2.34	1.00	1.33	0.85	0.716	1.06	0.678	1.00	1.30	0.881	No
403	40.30	2.35	1.01	1.34	0.85	0.715	1.06	0.677	1.00	1.30	0.880	No
404	40.40	2.35	1.01	1.34	0.85	0.715	1.06	0.677	1.00	1.30	0.880	No
405	40.50	2.36	1.01	1.34	0.85	0.714	1.06	0.676	1.00	1.30	2.000	Yes
406	40.60	2.36	1.02	1.35	0.85	0.714	1.06	0.676	1.00	1.30	2.000	Yes
407	40.70	2.37	1.02	1.35	0.84	0.713	1.06	0.675	1.00	1.30	2.000	Yes
408	40.80	2.38	1.02	1.35	0.84	0.713	1.06	0.675	1.00	1.30	2.000	Yes
409	40.90	2.38	1.03	1.36	0.84	0.712	1.06	0.674	1.00	1.30	2.000	Yes
410	41.00	2.39	1.03	1.36	0.84	0.712	1.06	0.674	1.00	1.30	2.000	Yes
411	41.10	2.40	1.03	1.36	0.84	0.711	1.06	0.673	1.00	1.30	0.875	No
412	41.20	2.40	1.04	1.37	0.84	0.710	1.06	0.673	1.00	1.30	0.874	No
413	41.30	2.41	1.04	1.37	0.84	0.710	1.06	0.672	1.00	1.30	0.874	No
414	41.40	2.42	1.04	1.37	0.84	0.709	1.06	0.671	1.00	1.30	0.873	No
415	41.50	2.42	1.05	1.38	0.84	0.709	1.06	0.671	1.00	1.30	0.872	No
416	41.60	2.43	1.05	1.38	0.84	0.708	1.06	0.670	1.00	1.30	0.871	No
417	41.70	2.43	1.05	1.38	0.84	0.707	1.06	0.670	1.00	1.30	2.000	Yes
418	41.80	2.44	1.05	1.39	0.83	0.707	1.06	0.669	1.00	1.30	2.000	Yes
419	41.90	2.45	1.06	1.39	0.83	0.706	1.06	0.668	1.00	1.30	2.000	Yes
420	42.00	2.45	1.06	1.39	0.83	0.705	1.06	0.668	1.00	1.30	2.000	Yes
421	42.10	2.46	1.06	1.40	0.83	0.705	1.06	0.667	1.00	1.30	2.000	Yes
422	42.20	2.47	1.07	1.40	0.83	0.704	1.06	0.667	1.00	1.30	2.000	Yes
423	42.30	2.47	1.07	1.40	0.83	0.704	1.06	0.666	1.00	1.30	2.000	Yes
424	42.40	2.48	1.07	1.41	0.83	0.703	1.06	0.665	1.00	1.30	2.000	Yes
425	42.50	2.49	1.08	1.41	0.83	0.702	1.06	0.665	1.00	1.30	2.000	Yes
426	42.60	2.49	1.08	1.41	0.83	0.702	1.06	0.664	1.00	1.30	2.000	Yes
427	42.70	2.50	1.08	1.42	0.83	0.701	1.06	0.664	1.00	1.30	2.000	Yes
428	42.80	2.51	1.09	1.42	0.83	0.700	1.06	0.663	1.00	1.30	2.000	Yes
429	42.90	2.51	1.09	1.42	0.82	0.700	1.06	0.662	1.00	1.30	0.861	No
430	43.00	2.52	1.09	1.43	0.82	0.699	1.06	0.662	1.00	1.30	0.860	No
431	43.10	2.53	1.10	1.43	0.82	0.698	1.06	0.661	1.00	1.30	0.859	No
432	43.20	2.53	1.10	1.43	0.82	0.698	1.06	0.660	1.00	1.30	0.858	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
433	43.30	2.54	1.10	1.44	0.82	0.697	1.06	0.660	1.00	1.30	0.858	No
434	43.40	2.55	1.10	1.44	0.82	0.696	1.06	0.659	1.00	1.30	0.857	No
435	43.50	2.55	1.11	1.44	0.82	0.695	1.06	0.658	1.00	1.30	0.856	No
436	43.60	2.56	1.11	1.45	0.82	0.695	1.06	0.658	1.00	1.30	0.855	No
437	43.70	2.57	1.11	1.45	0.82	0.694	1.06	0.657	1.00	1.30	0.854	No
438	43.80	2.57	1.12	1.46	0.82	0.693	1.06	0.656	1.00	1.30	0.853	No
439	43.90	2.58	1.12	1.46	0.81	0.693	1.06	0.656	1.00	1.30	0.852	No
440	44.00	2.59	1.12	1.46	0.81	0.692	1.06	0.655	1.00	1.30	0.851	No
441	44.10	2.59	1.13	1.47	0.81	0.691	1.06	0.654	1.00	1.30	0.851	No
442	44.20	2.60	1.13	1.47	0.81	0.690	1.06	0.654	1.00	1.30	0.850	No
443	44.30	2.61	1.13	1.47	0.81	0.690	1.06	0.653	1.00	1.30	0.849	No
444	44.40	2.61	1.14	1.48	0.81	0.689	1.06	0.652	1.00	1.30	0.848	No
445	44.50	2.62	1.14	1.48	0.81	0.688	1.06	0.651	1.00	1.30	0.847	No
446	44.60	2.63	1.14	1.48	0.81	0.687	1.06	0.651	1.00	1.30	0.846	No
447	44.70	2.63	1.15	1.49	0.81	0.687	1.06	0.650	1.00	1.30	0.845	No
448	44.80	2.64	1.15	1.49	0.81	0.686	1.06	0.649	1.00	1.30	0.844	No
449	44.90	2.65	1.15	1.49	0.80	0.685	1.06	0.649	1.00	1.30	0.843	No
450	45.00	2.65	1.15	1.50	0.80	0.684	1.06	0.648	1.00	1.30	0.842	No
451	45.10	2.66	1.16	1.50	0.80	0.684	1.06	0.647	1.00	1.30	0.841	No
452	45.20	2.67	1.16	1.51	0.80	0.683	1.06	0.646	1.00	1.30	0.840	No
453	45.30	2.67	1.16	1.51	0.80	0.682	1.06	0.646	1.00	1.30	0.839	No
454	45.40	2.68	1.17	1.51	0.80	0.681	1.06	0.645	1.00	1.30	0.839	No
455	45.50	2.69	1.17	1.52	0.80	0.681	1.06	0.644	1.00	1.30	0.838	No
456	45.60	2.69	1.17	1.52	0.80	0.680	1.06	0.644	1.00	1.30	0.837	No
457	45.70	2.70	1.18	1.52	0.80	0.679	1.06	0.643	1.00	1.30	0.836	No
458	45.80	2.71	1.18	1.53	0.80	0.678	1.06	0.642	1.00	1.30	0.835	No
459	45.90	2.71	1.18	1.53	0.79	0.678	1.06	0.642	1.00	1.30	0.834	No
460	46.00	2.72	1.19	1.53	0.79	0.677	1.06	0.641	1.00	1.30	0.833	No
461	46.10	2.73	1.19	1.54	0.79	0.676	1.06	0.640	1.00	1.30	0.832	No
462	46.20	2.73	1.19	1.54	0.79	0.675	1.06	0.639	1.00	1.30	0.831	No
463	46.30	2.74	1.19	1.54	0.79	0.675	1.06	0.639	1.00	1.30	0.830	No
464	46.40	2.75	1.20	1.55	0.79	0.674	1.06	0.638	1.00	1.30	0.829	No
465	46.50	2.75	1.20	1.55	0.79	0.673	1.06	0.637	1.00	1.30	0.828	No
466	46.60	2.76	1.20	1.55	0.79	0.672	1.06	0.636	1.00	1.30	0.827	No
467	46.70	2.77	1.21	1.56	0.79	0.671	1.06	0.636	1.00	1.30	0.826	No
468	46.80	2.77	1.21	1.56	0.79	0.671	1.06	0.635	1.00	1.30	0.825	No
469	46.90	2.78	1.21	1.57	0.78	0.670	1.06	0.634	1.00	1.30	0.824	No
470	47.00	2.79	1.22	1.57	0.78	0.669	1.06	0.633	1.00	1.30	0.823	No
471	47.10	2.79	1.22	1.57	0.78	0.668	1.06	0.633	1.00	1.30	0.822	No
472	47.20	2.80	1.22	1.58	0.78	0.667	1.06	0.632	1.00	1.30	0.821	No
473	47.30	2.81	1.23	1.58	0.78	0.667	1.06	0.631	1.00	1.30	0.820	No
474	47.40	2.81	1.23	1.58	0.78	0.666	1.06	0.630	1.00	1.30	0.819	No
475	47.50	2.82	1.23	1.59	0.78	0.665	1.06	0.630	1.00	1.30	0.818	No
476	47.60	2.83	1.24	1.59	0.78	0.664	1.06	0.629	1.00	1.30	0.817	No
477	47.70	2.83	1.24	1.59	0.78	0.663	1.06	0.628	1.00	1.30	0.816	No
478	47.80	2.84	1.24	1.60	0.78	0.663	1.06	0.627	1.00	1.30	0.816	No
479	47.90	2.85	1.24	1.60	0.77	0.662	1.06	0.627	1.00	1.30	2.000	Yes
480	48.00	2.85	1.25	1.60	0.77	0.661	1.06	0.626	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
481	48.10	2.86	1.25	1.61	0.77	0.660	1.06	0.625	1.00	1.30	2.000	Yes
482	48.20	2.87	1.25	1.61	0.77	0.660	1.06	0.624	1.00	1.30	2.000	Yes
483	48.30	2.87	1.26	1.62	0.77	0.659	1.06	0.624	1.00	1.30	2.000	Yes
484	48.40	2.88	1.26	1.62	0.77	0.658	1.06	0.623	1.00	1.30	2.000	Yes
485	48.50	2.89	1.26	1.62	0.77	0.657	1.06	0.622	1.00	1.30	2.000	Yes
486	48.60	2.89	1.27	1.63	0.77	0.657	1.06	0.621	1.00	1.30	2.000	Yes
487	48.70	2.90	1.27	1.63	0.77	0.656	1.06	0.621	1.00	1.30	2.000	Yes
488	48.80	2.90	1.27	1.63	0.76	0.655	1.06	0.620	1.00	1.30	2.000	Yes
489	48.90	2.91	1.28	1.63	0.76	0.654	1.06	0.619	1.00	1.30	2.000	Yes
490	49.00	2.92	1.28	1.64	0.76	0.654	1.06	0.619	1.00	1.30	2.000	Yes
491	49.10	2.92	1.28	1.64	0.76	0.653	1.06	0.618	1.00	1.30	2.000	Yes
492	49.20	2.93	1.29	1.64	0.76	0.652	1.06	0.617	1.00	1.30	2.000	Yes
493	49.30	2.94	1.29	1.65	0.76	0.651	1.06	0.617	1.00	1.30	2.000	Yes
494	49.40	2.94	1.29	1.65	0.76	0.651	1.06	0.616	1.00	1.30	2.000	Yes
495	49.50	2.95	1.29	1.65	0.76	0.650	1.06	0.615	1.00	1.30	2.000	Yes
496	49.60	2.96	1.30	1.66	0.76	0.649	1.06	0.614	1.00	1.30	2.000	Yes
497	49.70	2.96	1.30	1.66	0.76	0.648	1.06	0.614	1.00	1.30	2.000	Yes
498	49.80	2.97	1.30	1.66	0.75	0.648	1.06	0.613	1.00	1.30	2.000	Yes
499	49.90	2.97	1.31	1.67	0.75	0.647	1.06	0.612	1.00	1.30	2.000	Yes

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
 σ_v : Total overburden pressure at test point (tsf)
 u_0 : Water pressure at test point (tsf)
 σ_v' : Effective overburden pressure based on GWT during earthquake (tsf)
 r_d : Nonlinear shear mass factor
 CSR: Cyclic Stress Ratio
 MSF: Magnitude Scaling Factor
 CSR_{eq}: CSR adjusted for M=7.5
 K_σ : Effective overburden stress factor
 CSR*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::												
Point ID	Depth (ft)	q _k (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1	0.10	35.03	2.40	3.31	0.76	66.19	2.36	156.19	4.000	No	No	2.00
2	0.20	35.16	2.41	3.41	0.77	66.44	2.40	159.73	4.000	No	No	2.00
3	0.30	34.73	2.42	3.57	0.77	65.62	2.50	164.28	4.000	No	No	2.00
4	0.40	33.65	2.44	3.67	0.78	63.56	2.61	165.68	4.000	No	No	2.00
5	0.50	32.47	2.44	3.58	0.78	61.31	2.62	160.84	4.000	No	No	2.00
6	0.60	31.69	2.43	3.32	0.78	59.84	2.53	151.50	4.000	No	No	2.00
7	0.70	31.23	2.41	3.07	0.77	58.94	2.42	142.68	4.000	No	No	2.00
8	0.80	31.07	2.39	2.92	0.76	58.64	2.35	137.66	4.000	No	No	2.00
9	0.90	31.07	2.39	2.86	0.76	58.63	2.32	135.92	4.000	No	No	2.00
10	1.00	30.99	2.39	2.84	0.76	58.46	2.31	135.02	4.000	No	No	2.00
11	1.10	30.22	2.39	2.80	0.76	57.00	2.33	132.82	4.000	No	No	2.00
12	1.20	28.62	2.41	2.78	0.77	53.96	2.40	129.71	4.000	Yes	No	2.00
13	1.30	25.29	2.45	2.82	0.79	47.65	2.65	126.49	4.000	Yes	No	2.00
14	1.40	21.46	2.52	3.03	0.82	40.40	3.28	132.51	4.000	Yes	No	2.00
15	1.50	19.76	2.60	3.54	0.84	37.17	5.27	195.89	4.000	Yes	No	2.00
16	1.60	17.77	2.67	4.12	0.87	33.40	8.69	290.27	4.000	Yes	No	2.00
17	1.70	17.28	2.73	4.74	0.89	32.47	4.98	161.78	4.000	Yes	Yes	2.00
18	1.80	17.01	2.76	5.30	0.91	31.95	5.42	173.34	4.000	Yes	Yes	2.00
19	1.90	17.94	2.75	5.31	0.90	33.69	5.24	176.60	4.000	No	Yes	2.00
20	2.00	18.20	2.72	4.91	0.89	34.19	4.93	168.40	4.000	No	Yes	2.00
21	2.10	17.74	2.68	4.18	0.88	33.31	9.00	299.75	4.000	No	No	2.00
22	2.20	17.81	2.65	3.73	0.86	33.41	7.23	241.40	4.000	No	No	2.00
23	2.30	17.30	2.65	3.70	0.87	32.44	7.54	244.51	4.000	No	No	2.00
24	2.40	15.15	2.72	3.99	0.89	28.37	4.90	138.92	4.000	No	Yes	2.00
25	2.50	12.68	2.80	4.40	0.93	23.68	5.90	139.78	4.000	No	Yes	2.00
26	2.60	10.83	2.87	4.68	0.95	20.18	6.83	137.90	4.000	No	Yes	2.00
27	2.70	10.19	2.90	4.81	0.96	18.96	7.24	137.27	4.000	No	Yes	2.00
28	2.80	10.31	2.90	4.79	0.96	19.18	7.17	137.46	4.000	No	Yes	2.00
29	2.90	11.42	2.85	4.64	0.95	21.26	6.56	139.51	4.000	No	Yes	2.00
30	3.00	13.17	2.79	4.32	0.92	24.56	5.69	139.87	4.000	No	Yes	2.00
31	3.10	14.98	2.73	4.03	0.90	27.98	4.98	139.23	4.000	No	Yes	2.00
32	3.20	15.49	2.70	3.89	0.89	28.93	4.75	137.31	4.000	No	Yes	2.00
33	3.30	14.62	2.73	3.94	0.90	27.28	4.99	136.17	4.000	No	Yes	2.00
34	3.40	13.98	2.75	4.10	0.91	26.06	5.29	137.84	4.000	No	Yes	2.00
35	3.50	15.01	2.73	4.05	0.90	27.99	4.99	139.69	4.000	No	Yes	2.00
36	3.60	17.48	2.65	3.72	0.87	32.64	7.53	245.77	4.000	No	No	2.00
37	3.70	20.02	2.58	3.33	0.84	37.43	4.62	173.01	4.000	No	No	2.00
38	3.80	20.81	2.55	3.19	0.83	38.92	3.92	152.62	4.000	No	No	2.00
39	3.90	19.38	2.59	3.37	0.85	36.20	5.07	183.38	4.000	No	No	2.00
40	4.00	16.73	2.68	3.89	0.88	31.19	8.96	279.39	4.000	No	No	2.00
41	4.10	14.89	2.76	4.45	0.91	27.70	5.34	147.79	4.000	No	Yes	2.00
42	4.20	15.11	2.76	4.56	0.91	28.11	5.37	150.90	4.000	Yes	Yes	2.00
43	4.30	17.12	2.69	4.10	0.89	31.89	9.46	301.57	4.000	Yes	No	2.00
44	4.40	20.17	2.58	3.42	0.85	37.64	4.80	180.53	4.000	Yes	No	2.00
45	4.50	23.37	2.48	2.85	0.81	43.68	2.85	124.44	4.000	Yes	No	2.00
46	4.60	26.36	2.40	2.48	0.78	49.32	2.38	117.41	4.000	Yes	No	2.00
47	4.70	28.28	2.35	2.25	0.76	52.95	2.13	112.80	4.000	Yes	No	2.00
48	4.80	28.50	2.33	2.12	0.75	53.35	2.04	109.09	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _k (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
49	4.90	26.77	2.36	2.15	0.76	50.07	2.15	107.83	4.000	Yes	No	2.00
50	5.00	23.34	2.43	2.40	0.79	43.58	2.54	110.85	4.000	Yes	No	2.00
51	5.10	18.70	2.55	2.80	0.84	34.79	3.90	135.58	4.000	Yes	No	2.00
52	5.20	14.38	2.68	3.29	0.89	26.62	9.16	243.87	4.000	Yes	No	2.00
53	5.30	11.34	2.80	3.71	0.93	20.85	5.82	121.41	4.000	Yes	Yes	2.00
54	5.40	9.53	2.88	3.99	0.96	17.43	6.89	120.05	4.000	Yes	Yes	2.00
55	5.50	8.69	2.93	4.25	0.98	15.83	7.62	120.59	4.000	Yes	Yes	2.00
56	5.60	10.46	2.88	4.57	0.96	19.16	6.98	133.71	4.000	No	Yes	2.00
57	5.70	12.39	2.84	4.72	0.95	22.80	6.32	144.16	4.000	No	Yes	2.00
58	5.80	13.72	2.80	4.73	0.93	25.30	5.91	149.41	4.000	No	Yes	2.00
59	5.90	11.35	2.86	4.66	0.96	20.82	6.68	139.04	4.000	No	Yes	2.00
60	6.00	9.16	2.92	4.42	0.98	16.66	7.53	125.43	4.000	No	Yes	2.00
61	6.10	7.81	2.95	3.93	0.99	14.11	7.89	111.36	4.000	Yes	Yes	2.00
62	6.20	9.31	2.83	3.20	0.94	16.93	6.22	105.22	4.000	Yes	Yes	2.00
63	6.30	13.02	2.64	2.49	0.87	23.93	7.10	169.86	4.000	Yes	No	2.00
64	6.40	17.23	2.48	1.92	0.81	31.87	2.82	89.84	4.000	Yes	No	2.00
65	6.50	19.97	2.36	1.49	0.77	37.05	2.16	80.05	4.000	Yes	No	2.00
66	6.60	21.02	2.32	1.36	0.75	39.02	1.99	77.54	4.000	Yes	No	2.00
67	6.70	21.55	2.34	1.54	0.76	40.00	2.08	83.30	4.000	No	No	2.00
68	6.80	24.54	2.34	1.84	0.76	45.65	2.10	95.64	4.000	No	No	2.00
69	6.90	28.95	2.32	2.04	0.75	53.97	1.98	107.12	4.000	No	No	2.00
70	7.00	33.02	2.29	2.20	0.74	61.66	1.90	117.36	4.000	No	No	2.00
71	7.10	34.38	2.31	2.41	0.75	64.23	1.96	125.84	4.000	Yes	No	2.00
72	7.20	33.32	2.34	2.58	0.76	62.20	2.09	129.71	4.000	Yes	No	2.00
73	7.30	30.96	2.37	2.69	0.77	57.74	2.25	129.63	4.000	Yes	No	2.00
74	7.40	27.34	2.43	2.86	0.80	50.89	2.56	130.17	4.000	Yes	No	2.00
75	7.50	23.15	2.53	3.28	0.83	42.95	3.36	144.32	4.000	Yes	No	2.00
76	7.60	18.85	2.65	3.98	0.88	34.80	7.52	261.78	4.000	Yes	No	2.00
77	7.70	15.01	2.78	4.78	0.93	27.54	5.61	154.44	4.000	Yes	Yes	2.00
78	7.80	12.30	2.88	5.45	0.97	22.42	6.98	156.54	4.000	Yes	Yes	2.00
79	7.90	11.37	2.92	5.64	0.98	20.64	7.52	155.17	4.000	Yes	Yes	2.00
80	8.00	12.13	2.88	5.24	0.97	22.07	6.88	151.91	4.000	Yes	Yes	2.00
81	8.10	13.66	2.80	4.55	0.94	24.94	5.82	145.18	4.000	Yes	Yes	2.00
82	8.20	15.81	2.70	3.78	0.90	29.00	9.88	286.40	4.000	Yes	No	2.00
83	8.30	18.07	2.59	3.04	0.86	33.25	5.00	166.34	4.000	Yes	No	2.00
84	8.40	19.89	2.50	2.48	0.83	36.12	2.86	103.17	4.000	Yes	No	2.00
85	8.50	20.92	2.45	2.12	0.81	37.25	2.65	98.76	4.000	Yes	No	2.00
86	8.60	21.23	2.42	1.88	0.79	37.28	2.46	91.72	4.000	Yes	No	2.00
87	8.70	21.47	2.39	1.73	0.79	37.31	2.34	87.43	0.142	No	No	0.23
88	8.80	21.51	2.39	1.68	0.78	37.14	2.31	85.73	0.139	No	No	0.23
89	8.90	21.51	2.40	1.80	0.79	37.18	2.40	89.20	4.000	Yes	No	2.00
90	9.00	20.90	2.45	2.08	0.81	36.46	2.66	97.11	4.000	Yes	No	2.00
91	9.10	19.70	2.51	2.44	0.83	34.77	3.02	105.02	4.000	Yes	No	2.00
92	9.20	19.12	2.55	2.77	0.85	33.99	4.00	136.03	4.000	Yes	No	2.00
93	9.30	19.54	2.56	2.91	0.85	34.68	4.21	146.00	0.369	No	No	0.59
94	9.40	20.38	2.55	2.96	0.85	35.97	4.01	144.33	0.360	No	No	0.57
95	9.50	19.23	2.59	3.15	0.86	34.07	5.06	172.27	0.555	No	No	0.87
96	9.60	16.01	2.68	3.52	0.89	28.79	8.80	253.31	3.600	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _t (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
97	9.70	13.82	2.77	4.12	0.93	25.09	5.45	136.76	1.197	No	Yes	1.86
98	9.80	15.64	2.74	4.38	0.92	28.37	5.20	147.38	1.353	No	Yes	2.00
99	9.90	16.35	2.73	4.29	0.91	29.41	5.00	147.04	1.403	No	Yes	2.00
100	10.00	13.35	2.78	4.19	0.93	24.09	5.67	136.49	1.149	No	Yes	1.76
101	10.10	8.41	2.95	4.19	1.00	14.82	7.91	117.16	0.707	No	Yes	1.08
102	10.20	7.41	3.00	4.24	1.00	12.92	8.72	112.59	0.616	No	Yes	0.94
103	10.30	10.53	2.85	3.92	0.96	18.81	6.47	121.71	0.897	No	Yes	1.36
104	10.40	13.79	2.75	3.69	0.92	24.22	5.21	126.27	1.155	No	Yes	1.74
105	10.50	16.27	2.69	3.67	0.90	28.24	9.86	278.42	3.600	No	No	2.00
106	10.60	16.77	2.70	3.91	0.91	29.07	4.74	137.94	1.387	No	Yes	2.00
107	10.70	14.80	2.77	4.37	0.93	25.89	5.53	143.09	1.235	No	Yes	1.84
108	10.80	11.32	2.89	4.96	0.98	20.07	7.10	142.45	0.957	No	Yes	1.42
109	10.90	7.88	3.05	5.48	1.00	13.73	9.59	131.66	0.655	No	Yes	0.97
110	11.00	5.67	3.17	5.56	1.00	9.54	12.11	115.56	0.455	No	Yes	0.67
111	11.10	4.53	3.24	5.10	1.00	7.34	13.68	100.33	0.350	No	Yes	0.51
112	11.20	4.05	3.25	4.46	1.00	6.41	14.02	89.78	0.306	No	Yes	0.45
113	11.30	3.98	3.24	4.04	1.00	6.25	13.62	85.17	0.298	No	Yes	0.43
114	11.40	3.98	3.23	3.84	1.00	6.22	13.38	83.25	0.297	No	Yes	0.43
115	11.50	3.98	3.23	3.83	1.00	6.19	13.40	82.98	0.295	No	Yes	0.43
116	11.60	3.98	3.24	3.95	1.00	6.16	13.63	83.97	0.294	No	Yes	0.42
117	11.70	3.98	3.25	4.19	1.00	6.13	14.01	85.91	0.293	No	Yes	0.42
118	11.80	3.92	3.28	4.46	1.00	5.99	14.62	87.52	0.286	No	Yes	0.41
119	11.90	3.81	3.30	4.66	1.00	5.75	15.27	87.81	0.274	No	Yes	0.39
120	12.00	4.07	3.28	4.65	1.00	6.21	14.54	90.30	0.296	No	Yes	0.42
121	12.10	4.67	3.21	4.46	1.00	7.26	12.96	94.05	0.346	No	Yes	0.49
122	12.20	5.31	3.15	4.25	1.00	8.39	11.56	96.95	0.400	No	Yes	0.56
123	12.30	5.58	3.12	4.09	1.00	8.83	10.99	97.04	0.421	No	Yes	0.59
124	12.40	5.58	3.12	4.02	1.00	8.79	10.93	96.01	0.419	No	Yes	0.58
125	12.50	5.58	3.12	4.02	1.00	8.74	10.97	95.92	0.417	No	Yes	0.58
126	12.60	5.58	3.13	4.12	1.00	8.70	11.13	96.89	0.415	No	Yes	0.57
127	12.70	5.58	3.14	4.33	1.00	8.66	11.42	98.95	0.413	No	Yes	0.57
128	12.80	5.58	3.16	4.63	1.00	8.62	11.83	101.97	0.411	No	Yes	0.56
129	12.90	5.58	3.18	4.99	1.00	8.58	12.29	105.47	0.409	No	Yes	0.56
130	13.00	5.80	3.18	5.26	1.00	8.93	12.29	109.74	0.426	No	Yes	0.58
131	13.10	6.32	3.15	5.27	1.00	9.79	11.61	113.73	0.467	No	Yes	0.63
132	13.20	6.51	3.13	5.13	1.00	10.09	11.25	113.54	0.481	No	Yes	0.65
133	13.30	5.94	3.16	4.99	1.00	9.05	11.88	107.61	0.432	No	Yes	0.58
134	13.40	4.89	3.24	4.89	1.00	7.19	13.58	97.66	0.343	No	Yes	0.46
135	13.50	4.17	3.30	4.70	1.00	5.90	15.08	89.03	0.282	No	Yes	0.38
136	13.60	3.98	3.30	4.43	1.00	5.56	15.25	84.82	0.265	No	Yes	0.35
137	13.70	3.98	3.30	4.28	1.00	5.54	15.09	83.51	0.264	No	Yes	0.35
138	13.80	3.98	3.30	4.39	1.00	5.51	15.28	84.20	0.263	No	Yes	0.35
139	13.90	3.98	3.32	4.64	1.00	5.48	15.69	86.06	0.262	No	Yes	0.35
140	14.00	3.98	3.33	4.79	1.00	5.46	15.96	87.11	0.260	No	Yes	0.34
141	14.10	3.98	3.32	4.68	1.00	5.43	15.85	86.08	0.259	No	Yes	0.34
142	14.20	3.98	3.31	4.43	1.00	5.41	15.53	83.99	0.258	No	Yes	0.34
143	14.30	3.76	3.34	4.34	1.00	5.01	16.15	80.89	0.239	No	Yes	0.31
144	14.40	3.50	3.37	4.41	1.00	4.54	17.28	78.42	0.217	No	Yes	0.28

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
145	14.50	3.50	3.37	4.38	1.00	4.52	17.28	78.04	0.215	No	Yes	0.28
146	14.60	3.72	3.34	4.24	1.00	4.87	16.27	79.17	0.232	No	Yes	0.30
147	14.70	4.09	3.30	4.27	1.00	5.46	15.19	83.01	0.261	No	Yes	0.34
148	14.80	4.51	3.28	4.64	1.00	6.14	14.64	89.86	0.293	No	Yes	0.38
149	14.90	5.25	3.24	5.14	1.00	7.32	13.74	100.58	0.349	No	Yes	0.45
150	15.00	6.18	3.20	5.54	1.00	8.82	12.69	111.96	0.421	No	Yes	0.54
151	15.10	7.12	3.15	5.75	1.00	10.33	11.72	121.16	0.493	No	Yes	0.63
152	15.20	9.50	3.04	5.50	1.00	14.17	9.42	133.51	0.676	No	Yes	0.86
153	15.30	14.31	2.86	4.76	0.97	21.55	6.61	142.43	4.000	Yes	Yes	2.00
154	15.40	22.91	2.65	3.82	0.89	33.70	7.42	249.99	4.000	Yes	No	2.00
155	15.50	34.71	2.45	2.96	0.81	49.46	2.67	132.07	4.000	Yes	No	2.00
156	15.60	50.28	2.28	2.40	0.75	69.50	1.86	129.32	4.000	Yes	No	2.00
157	15.70	67.84	2.16	2.14	0.70	91.62	1.53	140.05	4.000	Yes	No	2.00
158	15.80	85.19	2.06	1.88	0.66	112.65	1.37	154.02	4.000	Yes	No	2.00
159	15.90	100.36	1.98	1.69	0.63	130.44	1.29	168.64	4.000	Yes	No	2.00
160	16.00	105.72	1.95	1.57	0.62	136.09	1.27	172.49	4.000	Yes	No	2.00
161	16.10	103.10	1.96	1.62	0.63	132.76	1.28	169.98	0.537	No	No	0.67
162	16.20	98.78	2.01	1.78	0.64	127.74	1.31	167.57	0.518	No	No	0.65
163	16.30	98.29	2.03	1.92	0.65	127.29	1.33	169.86	0.536	No	No	0.67
164	16.40	97.60	2.05	2.03	0.66	126.46	1.36	171.44	4.000	Yes	No	2.00
165	16.50	89.65	2.10	2.18	0.68	116.68	1.41	164.92	4.000	Yes	No	2.00
166	16.60	76.67	2.17	2.43	0.71	100.71	1.55	156.50	4.000	Yes	No	2.00
167	16.70	61.52	2.28	2.81	0.75	81.89	1.86	152.38	4.000	Yes	No	2.00
168	16.80	46.02	2.42	3.32	0.80	62.21	2.47	153.43	4.000	Yes	No	2.00
169	16.90	32.20	2.57	3.87	0.86	44.17	4.41	194.75	4.000	Yes	No	2.00
170	17.00	21.83	2.72	4.33	0.92	30.21	4.93	149.00	4.000	Yes	Yes	2.00
171	17.10	15.15	2.85	4.56	0.97	20.96	6.56	137.50	4.000	Yes	Yes	2.00
172	17.20	10.77	2.97	4.56	1.00	14.63	8.35	122.13	4.000	Yes	Yes	2.00
173	17.30	8.03	3.07	4.34	1.00	10.50	10.10	106.07	0.501	No	Yes	0.61
174	17.40	6.41	3.14	3.98	1.00	8.07	11.50	92.75	0.385	No	Yes	0.47
175	17.50	5.73	3.17	3.59	1.00	7.02	12.00	84.31	0.335	No	Yes	0.41
176	17.60	5.58	3.15	3.22	1.00	6.78	11.73	79.47	0.323	No	Yes	0.39
177	17.70	5.58	3.13	2.95	1.00	6.75	11.32	76.40	0.322	No	Yes	0.39
178	17.80	5.58	3.12	2.77	1.00	6.72	11.06	74.35	0.321	No	Yes	0.39
179	17.90	5.58	3.11	2.65	1.00	6.70	10.88	72.87	0.319	No	Yes	0.39
180	18.00	5.72	3.10	2.64	1.00	6.88	10.66	73.35	0.328	No	Yes	0.40
181	18.10	6.17	3.08	2.81	1.00	7.51	10.32	77.52	0.358	No	Yes	0.43
182	18.20	6.71	3.09	3.36	1.00	8.26	10.49	86.59	0.394	No	Yes	0.47
183	18.30	7.09	3.13	4.18	1.00	8.79	11.14	97.84	0.419	No	Yes	0.50
184	18.40	7.50	3.16	5.15	1.00	9.34	11.83	110.45	0.445	No	Yes	0.53
185	18.50	8.13	3.16	5.83	1.00	10.20	11.90	121.37	0.487	No	Yes	0.58
186	18.60	9.21	3.13	6.05	1.00	11.70	11.14	130.42	0.558	No	Yes	0.67
187	18.70	10.73	3.06	5.91	1.00	13.82	9.94	137.35	0.659	No	Yes	0.79
188	18.80	12.95	2.98	5.47	1.00	16.91	8.40	141.97	0.807	No	Yes	0.96
189	18.90	16.09	2.87	4.82	0.98	21.07	6.75	142.29	1.005	No	Yes	1.19
190	19.00	18.81	2.78	4.22	0.94	24.48	5.62	137.61	1.167	No	Yes	1.39
191	19.10	20.48	2.73	3.92	0.93	26.48	5.08	134.56	1.263	No	Yes	1.50
192	19.20	20.52	2.74	4.02	0.93	26.47	5.17	136.81	1.263	No	Yes	1.49

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _t (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
193	19.30	19.41	2.79	4.43	0.95	25.03	5.71	142.80	1.194	No	Yes	1.41
194	19.40	17.68	2.84	4.77	0.97	22.76	6.37	145.07	1.086	No	Yes	1.28
195	19.50	16.31	2.87	4.78	0.98	20.89	6.76	141.25	0.996	No	Yes	1.17
196	19.60	16.30	2.85	4.42	0.97	20.74	6.48	134.47	0.989	No	Yes	1.16
197	19.70	18.29	2.79	4.01	0.95	23.15	5.67	131.33	1.104	No	Yes	1.30
198	19.80	20.97	2.73	3.81	0.92	26.45	5.00	132.10	1.261	No	Yes	1.48
199	19.90	22.75	2.71	3.89	0.92	28.62	4.78	136.95	1.365	No	Yes	1.60
200	20.00	21.58	2.75	4.22	0.93	27.13	5.24	142.04	1.294	No	Yes	1.51
201	20.10	17.47	2.84	4.61	0.97	21.89	6.41	140.38	1.044	No	Yes	1.22
202	20.20	12.54	2.97	4.86	1.00	15.41	8.35	128.64	0.735	No	Yes	0.86
203	20.30	8.93	3.08	4.50	1.00	10.49	10.29	107.93	0.500	No	Yes	0.58
204	20.40	7.14	3.13	3.74	1.00	8.05	11.19	90.08	0.384	No	Yes	0.45
205	20.50	6.30	3.14	3.13	1.00	6.91	11.44	79.02	0.329	No	Yes	0.38
206	20.60	5.79	3.16	2.93	1.00	6.20	11.94	74.02	0.296	No	Yes	0.34
207	20.70	5.58	3.21	3.23	1.00	5.90	12.86	75.85	0.281	No	Yes	0.33
208	20.80	5.55	3.25	3.80	1.00	5.83	13.87	80.95	0.278	No	Yes	0.32
209	20.90	5.51	3.28	4.27	1.00	5.77	14.68	84.69	0.275	No	Yes	0.32
210	21.00	5.50	3.29	4.36	1.00	5.72	14.89	85.19	0.273	No	Yes	0.31
211	21.10	5.47	3.28	4.24	1.00	5.67	14.79	83.89	0.271	No	Yes	0.31
212	21.20	5.83	3.26	4.28	1.00	6.12	14.16	86.65	0.292	No	Yes	0.34
213	21.30	6.38	3.25	4.75	1.00	6.82	13.86	94.51	0.325	No	Yes	0.37
214	21.40	7.19	3.23	5.33	1.00	7.84	13.40	105.08	0.374	No	Yes	0.43
215	21.50	7.91	3.21	5.68	1.00	8.76	12.89	112.96	0.418	No	Yes	0.48
216	21.60	8.45	3.18	5.61	1.00	9.42	12.27	115.54	0.449	No	Yes	0.51
217	21.70	8.76	3.15	5.26	1.00	9.78	11.61	113.59	0.467	No	Yes	0.53
218	21.80	8.66	3.13	4.84	1.00	9.62	11.27	108.42	0.459	No	Yes	0.52
219	21.90	8.24	3.14	4.54	1.00	9.05	11.36	102.78	0.432	No	Yes	0.49
220	22.00	7.71	3.16	4.43	1.00	8.33	11.83	98.57	0.397	No	Yes	0.45
221	22.10	7.52	3.17	4.49	1.00	8.07	12.16	98.11	0.385	No	Yes	0.44
222	22.20	7.95	3.16	4.63	1.00	8.58	11.86	101.78	0.409	No	Yes	0.46
223	22.30	8.79	3.13	4.85	1.00	9.62	11.28	108.47	0.459	No	Yes	0.52
224	22.40	9.90	3.10	5.17	1.00	11.00	10.70	117.69	0.525	No	Yes	0.59
225	22.50	12.35	3.03	5.30	1.00	14.05	9.28	130.38	0.670	No	Yes	0.76
226	22.60	16.82	2.90	4.92	0.99	19.58	7.18	140.54	0.934	No	Yes	1.06
227	22.70	23.64	2.75	4.29	0.93	27.60	5.22	144.22	1.317	No	Yes	1.49
228	22.80	31.17	2.63	3.88	0.89	36.29	6.58	238.98	3.600	No	No	2.00
229	22.90	36.34	2.58	3.86	0.87	42.22	4.82	203.56	4.000	No	No	2.00
230	23.00	37.64	2.60	4.21	0.88	43.70	5.32	232.50	4.000	No	No	2.00
231	23.10	35.29	2.66	4.80	0.90	40.99	7.84	321.34	3.600	No	No	2.00
232	23.20	32.02	2.73	5.49	0.93	37.18	5.02	186.79	1.774	No	Yes	1.99
233	23.30	29.06	2.79	6.09	0.95	33.69	5.75	193.53	1.607	No	Yes	1.81
234	23.40	26.91	2.83	6.45	0.97	31.10	6.28	195.41	1.483	No	Yes	1.67
235	23.50	25.69	2.86	6.61	0.98	29.58	6.59	194.81	1.411	No	Yes	1.58
236	23.60	25.99	2.85	6.59	0.98	29.81	6.54	195.02	4.000	Yes	Yes	2.00
237	23.70	28.55	2.81	6.30	0.96	32.65	6.00	195.78	4.000	Yes	Yes	2.00
238	23.80	33.44	2.74	5.74	0.93	38.10	5.09	194.00	4.000	Yes	Yes	2.00
239	23.90	39.82	2.64	5.05	0.90	45.14	7.19	324.77	4.000	Yes	No	2.00
240	24.00	46.53	2.56	4.40	0.86	52.41	4.08	213.85	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
241	24.10	54.51	2.46	3.76	0.83	60.94	2.73	166.42	4.000	Yes	No	2.00
242	24.20	65.10	2.35	3.12	0.79	72.15	2.14	154.76	4.000	Yes	No	2.00
243	24.30	79.01	2.24	2.62	0.74	86.81	1.73	150.17	4.000	Yes	No	2.00
244	24.40	93.89	2.16	2.35	0.71	102.42	1.52	155.95	4.000	Yes	No	2.00
245	24.50	106.54	2.12	2.33	0.70	115.72	1.45	167.93	4.000	Yes	No	2.00
246	24.60	115.17	2.11	2.43	0.70	124.79	1.44	179.54	0.618	No	No	0.69
247	24.70	120.39	2.12	2.55	0.70	130.21	1.45	188.31	0.701	No	No	0.78
248	24.80	116.41	2.14	2.63	0.71	125.70	1.48	186.07	0.679	No	No	0.76
249	24.90	104.61	2.17	2.67	0.72	112.80	1.55	174.94	0.578	No	No	0.64
250	25.00	92.13	2.21	2.70	0.73	99.19	1.65	163.53	0.487	No	No	0.54
251	25.10	88.30	2.24	2.79	0.74	94.90	1.71	162.47	0.479	No	No	0.53
252	25.20	92.70	2.24	2.93	0.74	99.44	1.72	171.07	0.546	No	No	0.61
253	25.30	95.86	2.25	3.11	0.75	102.67	1.75	179.84	0.621	No	No	0.69
254	25.40	93.78	2.28	3.32	0.76	100.31	1.85	185.09	4.000	Yes	No	2.00
255	25.50	85.40	2.33	3.57	0.78	91.26	2.04	185.93	4.000	Yes	No	2.00
256	25.60	72.79	2.40	3.86	0.81	77.70	2.37	184.22	4.000	Yes	No	2.00
257	25.70	58.75	2.49	4.20	0.84	62.59	2.91	181.87	4.000	Yes	No	2.00
258	25.80	45.10	2.60	4.66	0.88	47.88	5.46	261.58	4.000	Yes	No	2.00
259	25.90	32.80	2.74	5.27	0.94	34.58	5.12	177.19	4.000	Yes	Yes	2.00
260	26.00	22.82	2.89	5.96	0.99	23.72	7.10	168.46	4.000	Yes	Yes	2.00
261	26.10	15.86	3.04	6.49	1.00	15.95	9.57	152.57	0.761	No	Yes	0.84
262	26.20	12.59	3.13	6.54	1.00	12.29	11.26	138.34	0.586	No	Yes	0.65
263	26.30	11.74	3.15	6.22	1.00	11.30	11.54	130.48	0.539	No	Yes	0.60
264	26.40	11.90	3.13	5.96	1.00	11.45	11.21	128.32	0.546	No	Yes	0.60
265	26.50	12.02	3.12	5.91	1.00	11.53	11.11	128.19	0.550	No	Yes	0.61
266	26.60	12.19	3.13	6.02	1.00	11.68	11.13	130.07	0.557	No	Yes	0.62
267	26.70	12.99	3.11	6.08	1.00	12.51	10.72	134.19	0.597	No	Yes	0.66
268	26.80	14.07	3.07	6.02	1.00	13.65	10.12	138.10	0.651	No	Yes	0.72
269	26.90	15.03	3.05	5.96	1.00	14.64	9.63	141.00	0.698	No	Yes	0.77
270	27.00	15.05	3.05	6.01	1.00	14.62	9.68	141.53	0.697	No	Yes	0.77
271	27.10	14.04	3.08	6.15	1.00	13.48	10.31	138.95	0.643	No	Yes	0.71
272	27.20	11.95	3.15	6.31	1.00	11.20	11.70	130.94	0.534	No	Yes	0.59
273	27.30	10.07	3.22	6.30	1.00	9.14	13.21	120.75	0.436	No	Yes	0.48
274	27.40	9.47	3.23	5.98	1.00	8.47	13.49	114.25	0.404	No	Yes	0.44
275	27.50	9.83	3.20	5.68	1.00	8.83	12.83	113.31	0.421	No	Yes	0.46
276	27.60	10.36	3.18	5.50	1.00	9.36	12.19	114.18	0.447	No	Yes	0.49
277	27.70	10.36	3.17	5.43	1.00	9.33	12.14	113.35	0.445	No	Yes	0.49
278	27.80	10.36	3.17	5.44	1.00	9.30	12.17	113.23	0.444	No	Yes	0.49
279	27.90	10.36	3.18	5.48	1.00	9.28	12.24	113.51	0.442	No	Yes	0.49
280	28.00	10.36	3.18	5.59	1.00	9.25	12.38	114.54	0.441	No	Yes	0.48
281	28.10	10.94	3.17	5.68	1.00	9.82	12.02	118.10	0.468	No	Yes	0.51
282	28.20	14.59	3.05	5.47	1.00	13.61	9.63	131.07	0.649	No	Yes	0.71
283	28.30	22.51	2.87	4.96	0.99	21.80	6.71	146.37	1.040	No	Yes	1.14
284	28.40	32.54	2.73	4.66	0.93	32.00	4.98	159.28	1.526	No	Yes	1.67
285	28.50	38.83	2.67	4.72	0.91	38.31	8.62	330.06	3.600	No	No	2.00
286	28.60	38.69	2.70	5.09	0.92	38.08	10.09	384.44	3.600	No	No	2.00
287	28.70	34.55	2.77	5.68	0.95	33.80	5.48	185.09	1.612	No	Yes	1.76
288	28.80	30.65	2.83	6.11	0.97	29.76	6.24	185.71	1.420	No	Yes	1.55

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
289	28.90	30.40	2.82	5.91	0.97	29.40	6.15	180.95	4.000	Yes	Yes	2.00
290	29.00	35.55	2.72	4.95	0.93	34.46	4.92	169.60	4.000	Yes	Yes	2.00
291	29.10	47.27	2.54	3.67	0.86	45.99	3.66	168.11	4.000	Yes	No	2.00
292	29.20	63.97	2.36	2.77	0.80	62.34	2.18	135.74	4.000	Yes	No	2.00
293	29.30	82.47	2.23	2.36	0.75	80.36	1.70	136.78	4.000	Yes	No	2.00
294	29.40	101.51	2.16	2.28	0.72	98.87	1.52	150.70	4.000	Yes	No	2.00
295	29.50	120.40	2.11	2.29	0.70	117.15	1.44	168.35	4.000	Yes	No	2.00
296	29.60	138.78	2.08	2.32	0.69	134.84	1.39	186.85	4.000	Yes	No	2.00
297	29.70	151.39	2.06	2.36	0.68	146.84	1.36	200.29	4.000	No	No	2.00
298	29.80	149.49	2.07	2.41	0.69	144.67	1.38	199.31	0.816	No	No	0.89
299	29.90	134.76	2.11	2.51	0.70	130.04	1.44	187.01	0.688	No	No	0.75
300	30.00	124.88	2.16	2.72	0.72	120.19	1.52	183.25	0.652	No	No	0.71
301	30.10	126.66	2.18	2.92	0.73	121.66	1.57	191.06	0.729	No	No	0.80
302	30.20	133.00	2.17	2.97	0.73	127.49	1.55	198.22	0.804	No	No	0.88
303	30.30	130.73	2.17	2.85	0.72	124.96	1.54	191.86	0.737	No	No	0.81
304	30.40	122.90	2.16	2.63	0.72	117.07	1.52	177.76	0.602	No	No	0.66
305	30.50	115.21	2.16	2.47	0.72	109.38	1.51	165.69	4.000	Yes	No	2.00
306	30.60	106.62	2.19	2.53	0.73	100.89	1.58	159.60	4.000	Yes	No	2.00
307	30.70	95.19	2.26	2.86	0.76	89.73	1.79	160.35	4.000	Yes	No	2.00
308	30.80	81.78	2.36	3.34	0.80	76.72	2.16	165.73	4.000	Yes	No	2.00
309	30.90	68.85	2.45	3.76	0.83	64.18	2.64	169.28	4.000	Yes	No	2.00
310	31.00	59.25	2.51	3.99	0.86	54.87	3.04	167.08	4.000	Yes	No	2.00
311	31.10	54.12	2.54	4.02	0.87	49.84	3.74	186.24	4.000	Yes	No	2.00
312	31.20	52.83	2.54	3.92	0.87	48.48	3.76	182.33	0.644	No	No	0.70
313	31.30	53.99	2.54	3.91	0.87	49.46	3.59	177.30	0.598	No	No	0.66
314	31.40	56.15	2.54	4.12	0.87	51.36	3.71	190.56	0.724	No	No	0.79
315	31.50	62.49	2.53	4.38	0.86	57.19	3.41	194.81	4.000	Yes	No	2.00
316	31.60	78.37	2.45	4.23	0.83	71.97	2.66	191.72	4.000	Yes	No	2.00
317	31.70	106.07	2.32	3.71	0.79	97.78	2.01	196.67	4.000	Yes	No	2.00
318	31.80	135.90	2.21	3.29	0.74	125.49	1.65	206.96	4.000	Yes	No	2.00
319	31.90	156.45	2.16	3.11	0.72	144.41	1.52	218.92	4.000	Yes	No	2.00
320	32.00	161.73	2.15	3.16	0.72	148.97	1.51	225.02	4.000	Yes	No	2.00
321	32.10	152.47	2.19	3.38	0.74	139.95	1.60	223.85	4.000	Yes	No	2.00
322	32.20	133.57	2.27	3.76	0.76	122.00	1.81	220.31	4.000	Yes	No	2.00
323	32.30	109.16	2.36	4.19	0.80	99.04	2.17	215.22	4.000	Yes	No	2.00
324	32.40	86.47	2.45	4.50	0.84	77.81	2.66	206.72	4.000	Yes	No	2.00
325	32.50	67.96	2.53	4.58	0.86	60.56	3.36	203.45	4.000	Yes	No	2.00
326	32.60	54.22	2.59	4.53	0.89	47.80	5.17	247.28	4.000	Yes	No	2.00
327	32.70	44.06	2.66	4.52	0.92	38.38	7.88	302.64	4.000	Yes	No	2.00
328	32.80	36.99	2.72	4.56	0.94	31.83	4.92	156.67	4.000	Yes	Yes	2.00
329	32.90	33.29	2.75	4.53	0.95	28.38	5.31	150.72	4.000	Yes	Yes	2.00
330	33.00	32.53	2.76	4.44	0.95	27.62	5.34	147.55	1.318	No	Yes	1.45
331	33.10	33.38	2.75	4.38	0.95	28.32	5.20	147.34	1.351	No	Yes	1.48
332	33.20	34.55	2.73	4.31	0.94	29.30	5.02	147.24	1.398	No	Yes	1.54
333	33.30	35.86	2.71	4.14	0.93	30.41	4.77	145.11	1.451	No	Yes	1.59
334	33.40	37.95	2.67	3.89	0.92	32.22	8.40	270.78	3.600	No	No	2.00
335	33.50	40.53	2.64	3.73	0.91	34.46	6.79	234.17	3.600	No	No	2.00
336	33.60	42.96	2.62	3.73	0.90	36.56	6.02	220.10	3.600	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
337	33.70	44.99	2.61	3.84	0.90	38.28	5.79	221.59	3.600	No	No	2.00
338	33.80	46.37	2.62	4.05	0.90	39.39	6.07	238.92	3.600	No	No	2.00
339	33.90	46.18	2.64	4.36	0.91	39.09	7.11	278.05	3.600	No	No	2.00
340	34.00	43.62	2.69	4.83	0.93	36.68	9.79	359.09	3.600	No	No	2.00
341	34.10	39.11	2.76	5.38	0.96	32.55	5.41	176.17	1.553	No	Yes	1.71
342	34.20	34.19	2.83	5.83	0.98	28.10	6.28	176.54	1.341	No	Yes	1.48
343	34.30	31.45	2.86	5.78	0.99	25.62	6.63	169.90	4.000	Yes	Yes	2.00
344	34.40	33.42	2.79	4.86	0.97	27.32	5.70	155.78	4.000	Yes	Yes	2.00
345	34.50	41.97	2.61	3.46	0.90	34.87	5.74	200.32	4.000	Yes	No	2.00
346	34.60	54.67	2.44	2.62	0.83	46.11	2.59	119.37	4.000	Yes	No	2.00
347	34.70	63.98	2.38	2.55	0.81	54.25	2.27	122.97	4.000	Yes	No	2.00
348	34.80	63.78	2.43	3.02	0.83	53.84	2.55	137.27	4.000	Yes	No	2.00
349	34.90	54.43	2.56	3.82	0.88	45.37	4.07	184.58	4.000	Yes	No	2.00
350	35.00	42.54	2.70	4.64	0.93	34.80	10.02	348.76	4.000	Yes	No	2.00
351	35.10	33.70	2.82	5.28	0.98	27.01	6.05	163.48	4.000	Yes	Yes	2.00
352	35.20	29.21	2.88	5.56	1.00	23.06	6.93	159.94	4.000	Yes	Yes	2.00
353	35.30	28.14	2.90	5.67	1.00	22.10	7.22	159.50	1.054	No	Yes	1.16
354	35.40	28.25	2.91	5.82	1.00	22.13	7.32	162.04	1.056	No	Yes	1.17
355	35.50	28.92	2.90	5.83	1.00	22.63	7.23	163.54	1.080	No	Yes	1.19
356	35.60	31.20	2.85	5.39	0.99	24.50	6.54	160.16	1.169	No	Yes	1.29
357	35.70	35.84	2.76	4.63	0.96	28.45	5.37	152.87	1.357	No	Yes	1.50
358	35.80	41.61	2.68	4.16	0.93	33.35	8.88	296.08	3.600	No	No	2.00
359	35.90	46.85	2.64	4.15	0.91	37.75	6.92	261.07	3.600	No	No	2.00
360	36.00	48.90	2.65	4.56	0.92	39.35	7.66	301.48	3.600	No	No	2.00
361	36.10	46.83	2.71	5.23	0.94	37.40	4.84	180.94	1.784	No	Yes	1.98
362	36.20	40.81	2.80	6.02	0.97	32.14	5.88	189.00	1.533	No	Yes	1.70
363	36.30	34.31	2.89	6.68	1.00	26.58	7.09	188.59	1.268	No	Yes	1.41
364	36.40	30.73	2.93	6.72	1.00	23.56	7.68	180.83	4.000	Yes	Yes	2.00
365	36.50	32.04	2.88	5.93	1.00	24.57	6.93	170.18	4.000	Yes	Yes	2.00
366	36.60	37.92	2.76	4.73	0.96	29.50	5.32	156.90	4.000	Yes	Yes	2.00
367	36.70	47.30	2.60	3.64	0.90	37.46	5.47	204.72	4.000	Yes	No	2.00
368	36.80	57.90	2.46	2.87	0.85	46.49	2.74	127.19	4.000	Yes	No	2.00
369	36.90	67.57	2.37	2.53	0.81	54.71	2.24	122.48	4.000	Yes	No	2.00
370	37.00	73.31	2.35	2.57	0.80	59.46	2.14	127.09	4.000	Yes	No	2.00
371	37.10	73.91	2.38	2.86	0.82	59.72	2.29	136.52	4.000	Yes	No	2.00
372	37.20	70.47	2.44	3.26	0.84	56.54	2.60	146.83	4.000	Yes	No	2.00
373	37.30	66.08	2.49	3.59	0.86	52.61	2.93	153.93	4.000	Yes	No	2.00
374	37.40	64.16	2.51	3.69	0.87	50.85	3.01	153.05	4.000	Yes	No	2.00
375	37.50	66.79	2.48	3.44	0.85	53.00	2.82	149.45	4.000	Yes	No	2.00
376	37.60	74.80	2.39	2.91	0.82	59.77	2.31	138.09	4.000	Yes	No	2.00
377	37.70	86.08	2.28	2.35	0.78	69.42	1.84	127.65	4.000	Yes	No	2.00
378	37.80	97.88	2.18	1.94	0.74	79.53	1.56	123.99	4.000	Yes	No	2.00
379	37.90	107.58	2.12	1.76	0.72	87.78	1.44	126.65	4.000	Yes	No	2.00
380	38.00	112.98	2.10	1.74	0.71	92.22	1.42	130.53	0.287	No	No	0.32
381	38.10	113.65	2.11	1.82	0.71	92.51	1.44	132.78	0.298	No	No	0.33
382	38.20	110.48	2.14	1.93	0.72	89.55	1.48	132.53	4.000	Yes	No	2.00
383	38.30	105.06	2.17	2.04	0.74	84.69	1.55	131.22	4.000	Yes	No	2.00
384	38.40	97.28	2.23	2.24	0.76	77.83	1.69	131.23	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _k (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
385	38.50	86.60	2.32	2.64	0.79	68.49	1.99	136.26	4.000	Yes	No	2.00
386	38.60	73.98	2.43	3.23	0.84	57.63	2.55	146.85	4.000	Yes	No	2.00
387	38.70	62.00	2.54	3.81	0.88	47.51	3.69	175.12	4.000	Yes	No	2.00
388	38.80	53.61	2.61	4.02	0.90	40.54	5.65	229.02	4.000	Yes	No	2.00
389	38.90	50.18	2.61	3.72	0.90	37.75	5.62	212.25	3.600	No	No	2.00
390	39.00	50.79	2.56	3.25	0.89	38.28	4.21	161.33	0.471	No	No	0.53
391	39.10	53.01	2.52	2.92	0.87	40.08	3.11	124.58	0.260	No	No	0.29
392	39.20	54.99	2.49	2.77	0.86	41.65	2.89	120.48	0.243	No	No	0.27
393	39.30	56.78	2.47	2.67	0.85	43.04	2.76	118.64	0.235	No	No	0.27
394	39.40	58.86	2.44	2.54	0.84	44.69	2.59	115.94	0.225	No	No	0.25
395	39.50	61.74	2.40	2.35	0.83	47.02	2.38	111.83	0.210	No	No	0.24
396	39.60	65.69	2.35	2.13	0.81	50.25	2.13	107.16	0.194	No	No	0.22
397	39.70	69.92	2.33	2.16	0.80	53.57	2.06	110.39	4.000	Yes	No	2.00
398	39.80	70.73	2.39	2.66	0.82	53.83	2.34	125.93	4.000	Yes	No	2.00
399	39.90	68.52	2.47	3.33	0.86	51.62	2.81	145.04	4.000	Yes	No	2.00
400	40.00	66.77	2.53	3.81	0.88	49.92	3.34	166.60	4.000	Yes	No	2.00
401	40.10	68.40	2.54	4.01	0.88	51.03	3.56	181.70	0.638	No	No	0.72
402	40.20	69.02	2.56	4.39	0.89	51.27	4.24	217.36	4.000	No	No	2.00
403	40.30	64.29	2.63	5.04	0.92	47.22	6.59	311.00	3.600	No	No	2.00
404	40.40	55.60	2.71	5.58	0.95	40.21	4.82	193.81	1.918	No	Yes	2.00
405	40.50	48.54	2.75	5.53	0.96	34.67	5.29	183.22	4.000	Yes	Yes	2.00
406	40.60	48.02	2.71	4.71	0.94	34.33	4.78	164.01	4.000	Yes	Yes	2.00
407	40.70	56.01	2.58	3.64	0.90	40.74	4.60	187.62	4.000	Yes	No	2.00
408	40.80	69.22	2.44	2.92	0.84	51.33	2.58	132.29	4.000	Yes	No	2.00
409	40.90	81.20	2.35	2.58	0.81	60.92	2.11	128.74	4.000	Yes	No	2.00
410	41.00	88.70	2.30	2.46	0.79	66.86	1.93	129.21	4.000	Yes	No	2.00
411	41.10	92.25	2.29	2.44	0.79	69.57	1.88	130.80	0.288	No	No	0.33
412	41.20	95.34	2.28	2.45	0.78	71.89	1.85	132.67	0.297	No	No	0.34
413	41.30	97.82	2.27	2.46	0.78	73.70	1.83	134.68	0.307	No	No	0.35
414	41.40	99.69	2.27	2.50	0.78	75.00	1.82	136.86	0.318	No	No	0.36
415	41.50	106.32	2.26	2.56	0.78	80.05	1.78	142.79	0.351	No	No	0.40
416	41.60	117.58	2.24	2.65	0.77	88.73	1.72	152.96	0.413	No	No	0.47
417	41.70	127.07	2.24	2.81	0.77	95.89	1.71	164.07	4.000	Yes	No	2.00
418	41.80	127.05	2.27	3.08	0.78	95.37	1.81	172.61	4.000	Yes	No	2.00
419	41.90	116.84	2.34	3.49	0.81	86.76	2.07	179.16	4.000	Yes	No	2.00
420	42.00	104.74	2.41	3.99	0.84	76.78	2.45	188.10	4.000	Yes	No	2.00
421	42.10	92.11	2.49	4.41	0.86	66.64	2.89	192.82	4.000	Yes	No	2.00
422	42.20	81.70	2.53	4.49	0.88	58.50	3.44	201.46	4.000	Yes	No	2.00
423	42.30	77.65	2.51	4.02	0.87	55.50	3.02	167.51	4.000	Yes	No	2.00
424	42.40	84.52	2.40	3.14	0.83	61.14	2.40	146.57	4.000	Yes	No	2.00
425	42.50	102.73	2.25	2.38	0.78	75.81	1.76	133.70	4.000	Yes	No	2.00
426	42.60	127.10	2.12	1.93	0.72	95.47	1.45	138.14	4.000	Yes	No	2.00
427	42.70	150.48	2.04	1.76	0.69	114.23	1.34	153.07	4.000	Yes	No	2.00
428	42.80	168.38	2.00	1.77	0.68	128.30	1.31	167.96	4.000	Yes	No	2.00
429	42.90	178.54	2.00	1.85	0.68	135.96	1.31	177.73	0.602	No	No	0.70
430	43.00	182.69	2.01	1.94	0.68	138.77	1.32	182.50	0.645	No	No	0.75
431	43.10	182.27	2.02	2.00	0.69	138.04	1.32	182.89	0.649	No	No	0.76
432	43.20	179.32	2.03	2.01	0.69	135.43	1.33	180.31	0.625	No	No	0.73

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
433	43.30	176.00	2.03	1.97	0.69	132.65	1.33	176.56	0.592	No	No	0.69
434	43.40	173.94	2.02	1.91	0.69	130.94	1.33	173.54	0.566	No	No	0.66
435	43.50	174.12	2.01	1.87	0.69	130.97	1.32	172.68	0.559	No	No	0.65
436	43.60	176.71	2.01	1.85	0.68	132.84	1.31	174.28	0.572	No	No	0.67
437	43.70	181.49	2.00	1.85	0.68	136.36	1.31	178.11	0.605	No	No	0.71
438	43.80	187.71	1.99	1.87	0.68	140.96	1.30	183.48	0.654	No	No	0.77
439	43.90	193.96	1.99	1.92	0.68	145.49	1.30	189.21	0.710	No	No	0.83
440	44.00	199.20	1.99	1.96	0.68	149.21	1.30	194.05	0.760	No	No	0.89
441	44.10	202.32	1.99	1.97	0.68	151.36	1.30	196.61	0.787	No	No	0.93
442	44.20	203.65	1.98	1.94	0.67	152.24	1.29	196.91	0.790	No	No	0.93
443	44.30	204.80	1.97	1.90	0.67	153.02	1.29	196.89	0.790	No	No	0.93
444	44.40	206.99	1.97	1.88	0.67	154.52	1.28	198.22	0.804	No	No	0.95
445	44.50	210.41	1.97	1.91	0.67	156.81	1.28	201.32	4.000	No	No	2.00
446	44.60	214.13	1.97	1.95	0.67	159.31	1.29	204.72	4.000	No	No	2.00
447	44.70	217.64	1.97	1.96	0.67	161.74	1.28	207.51	4.000	No	No	2.00
448	44.80	221.58	1.96	1.92	0.67	164.66	1.28	209.99	4.000	No	No	2.00
449	44.90	227.00	1.94	1.86	0.66	168.85	1.26	213.26	4.000	No	No	2.00
450	45.00	234.02	1.92	1.80	0.65	174.31	1.25	217.83	4.000	No	No	2.00
451	45.10	239.15	1.91	1.76	0.65	178.21	1.24	221.09	4.000	No	No	2.00
452	45.20	237.85	1.91	1.75	0.65	176.94	1.24	219.53	4.000	No	No	2.00
453	45.30	229.01	1.92	1.75	0.65	169.74	1.25	211.91	4.000	No	No	2.00
454	45.40	215.37	1.93	1.74	0.66	158.89	1.26	200.16	4.000	No	No	2.00
455	45.50	202.11	1.95	1.71	0.66	148.45	1.27	188.42	0.702	No	No	0.84
456	45.60	193.91	1.95	1.65	0.66	142.10	1.27	180.45	0.626	No	No	0.75
457	45.70	193.08	1.93	1.56	0.66	141.60	1.26	178.17	0.606	No	No	0.73
458	45.80	200.77	1.90	1.46	0.65	147.76	1.24	182.74	0.648	No	No	0.78
459	45.90	215.19	1.86	1.40	0.63	159.08	1.21	192.70	0.745	No	No	0.89
460	46.00	233.39	1.84	1.38	0.62	173.14	1.19	205.69	4.000	No	No	2.00
461	46.10	252.76	1.82	1.40	0.61	187.87	1.17	219.97	4.000	No	No	2.00
462	46.20	270.53	1.80	1.43	0.61	201.28	1.16	233.02	4.000	No	No	2.00
463	46.30	285.82	1.79	1.45	0.61	212.86	1.14	243.21	4.000	No	No	2.00
464	46.40	297.04	1.77	1.42	0.60	221.49	1.12	248.44	4.000	No	No	2.00
465	46.50	304.64	1.76	1.39	0.59	227.35	1.10	250.22	4.000	No	No	2.00
466	46.60	309.75	1.75	1.39	0.59	231.05	1.09	252.23	4.000	No	No	2.00
467	46.70	312.52	1.76	1.41	0.59	232.63	1.10	255.70	4.000	No	No	2.00
468	46.80	312.12	1.77	1.45	0.60	231.67	1.11	257.78	4.000	No	No	2.00
469	46.90	308.33	1.78	1.48	0.60	228.10	1.13	257.39	4.000	No	No	2.00
470	47.00	301.93	1.79	1.51	0.61	222.50	1.15	255.10	4.000	No	No	2.00
471	47.10	294.03	1.82	1.57	0.62	215.62	1.17	252.16	4.000	No	No	2.00
472	47.20	284.88	1.84	1.64	0.63	207.74	1.19	247.76	4.000	No	No	2.00
473	47.30	275.33	1.86	1.70	0.63	199.71	1.21	241.83	4.000	No	No	2.00
474	47.40	266.20	1.88	1.71	0.64	192.33	1.22	234.75	4.000	No	No	2.00
475	47.50	258.33	1.88	1.67	0.64	186.32	1.22	227.31	4.000	No	No	2.00
476	47.60	252.03	1.86	1.55	0.63	181.90	1.21	219.72	4.000	No	No	2.00
477	47.70	247.62	1.83	1.40	0.62	179.26	1.18	211.94	4.000	No	No	2.00
478	47.80	245.33	1.79	1.24	0.61	178.34	1.14	204.06	4.000	No	No	2.00
479	47.90	241.79	1.78	1.19	0.61	175.75	1.13	199.14	4.000	Yes	No	2.00
480	48.00	231.80	1.84	1.34	0.63	166.75	1.19	198.34	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
481	48.10	209.20	1.95	1.72	0.67	147.31	1.27	187.38	4.000	Yes	No	2.00
482	48.20	174.47	2.11	2.31	0.73	119.30	1.43	170.86	4.000	Yes	No	2.00
483	48.30	133.42	2.28	2.99	0.80	88.12	1.85	163.29	4.000	Yes	No	2.00
484	48.40	94.91	2.45	3.58	0.86	60.35	2.65	160.03	4.000	Yes	No	2.00
485	48.50	71.47	2.57	3.83	0.90	44.05	4.35	191.52	4.000	Yes	No	2.00
486	48.60	60.38	2.62	3.81	0.93	36.51	6.29	229.52	4.000	Yes	No	2.00
487	48.70	52.78	2.67	3.80	0.94	31.38	8.47	265.84	4.000	Yes	No	2.00
488	48.80	47.63	2.70	3.73	0.96	27.94	4.74	132.29	4.000	Yes	Yes	2.00
489	48.90	49.25	2.65	3.22	0.94	29.16	7.31	213.06	4.000	Yes	No	2.00
490	49.00	65.35	2.48	2.60	0.87	40.31	2.84	114.60	4.000	Yes	No	2.00
491	49.10	87.91	2.31	2.13	0.81	56.32	1.98	111.28	4.000	Yes	No	2.00
492	49.20	112.10	2.19	1.89	0.76	73.73	1.59	117.57	4.000	Yes	No	2.00
493	49.30	133.65	2.12	1.83	0.74	89.17	1.45	129.73	4.000	Yes	No	2.00
494	49.40	151.11	2.09	1.85	0.72	101.56	1.40	142.05	4.000	Yes	No	2.00
495	49.50	166.58	2.04	1.77	0.71	112.85	1.34	151.72	4.000	Yes	No	2.00
496	49.60	185.29	1.97	1.59	0.68	127.04	1.29	163.26	4.000	Yes	No	2.00
497	49.70	208.76	1.89	1.40	0.65	145.19	1.23	178.64	4.000	Yes	No	2.00
498	49.80	231.42	1.83	1.27	0.62	162.73	1.18	191.98	4.000	Yes	No	2.00
499	49.90	245.61	1.79	1.21	0.61	173.66	1.14	198.32	4.000	Yes	No	2.00

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q_t :	Total cone resistance
I_c :	Soil behavior type index
Fr:	Normalized friction ratio (%)
n:	Stress exponent
Q_{tn} :	Normalized cone resistance
K_c :	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Normalized and adjusted cone resistance
CRR _{7.5} :	Cyclic resistance ratio for $M_w=7.5$
FS:	Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
0.10	2.00	0.00	0.00	0.10	0.00	0.20	2.00	0.00	0.00	0.10	0.00
0.30	2.00	0.00	0.00	0.10	0.00	0.40	2.00	0.00	0.00	0.10	0.00
0.50	2.00	0.00	0.00	0.10	0.00	0.60	2.00	0.00	0.00	0.10	0.00
0.70	2.00	0.00	0.00	0.10	0.00	0.80	2.00	0.00	0.00	0.10	0.00
0.90	2.00	0.00	0.00	0.10	0.00	1.00	2.00	0.00	0.00	0.10	0.00
1.10	2.00	0.00	0.00	0.10	0.00	1.20	2.00	0.00	0.00	0.10	0.00
1.30	2.00	0.00	0.00	0.10	0.00	1.40	2.00	0.00	0.00	0.10	0.00
1.50	2.00	0.00	0.00	0.10	0.00	1.60	2.00	0.00	0.00	0.10	0.00
1.70	2.00	0.00	0.00	0.10	0.00	1.80	2.00	0.00	0.00	0.10	0.00
1.90	2.00	0.00	0.00	0.10	0.00	2.00	2.00	0.00	0.00	0.10	0.00
2.10	2.00	0.00	0.00	0.10	0.00	2.20	2.00	0.00	0.00	0.10	0.00
2.30	2.00	0.00	0.00	0.10	0.00	2.40	2.00	0.00	0.00	0.10	0.00
2.50	2.00	0.00	0.00	0.10	0.00	2.60	2.00	0.00	0.00	0.10	0.00
2.70	2.00	0.00	0.00	0.10	0.00	2.80	2.00	0.00	0.00	0.10	0.00
2.90	2.00	0.00	0.00	0.10	0.00	3.00	2.00	0.00	0.00	0.10	0.00
3.10	2.00	0.00	0.00	0.10	0.00	3.20	2.00	0.00	0.00	0.10	0.00
3.30	2.00	0.00	0.00	0.10	0.00	3.40	2.00	0.00	0.00	0.10	0.00
3.50	2.00	0.00	0.00	0.10	0.00	3.60	2.00	0.00	0.00	0.10	0.00
3.70	2.00	0.00	0.00	0.10	0.00	3.80	2.00	0.00	0.00	0.10	0.00
3.90	2.00	0.00	0.00	0.10	0.00	4.00	2.00	0.00	0.00	0.10	0.00
4.10	2.00	0.00	0.00	0.10	0.00	4.20	2.00	0.00	0.00	0.10	0.00
4.30	2.00	0.00	0.00	0.10	0.00	4.40	2.00	0.00	0.00	0.10	0.00
4.50	2.00	0.00	0.00	0.10	0.00	4.60	2.00	0.00	0.00	0.10	0.00
4.70	2.00	0.00	0.00	0.10	0.00	4.80	2.00	0.00	0.00	0.10	0.00
4.90	2.00	0.00	0.00	0.10	0.00	5.00	2.00	0.00	0.00	0.10	0.00
5.10	2.00	0.00	0.00	0.10	0.00	5.20	2.00	0.00	0.00	0.10	0.00
5.30	2.00	0.00	0.00	0.10	0.00	5.40	2.00	0.00	0.00	0.10	0.00
5.50	2.00	0.00	0.00	0.10	0.00	5.60	2.00	0.00	0.00	0.10	0.00
5.70	2.00	0.00	0.00	0.10	0.00	5.80	2.00	0.00	0.00	0.10	0.00
5.90	2.00	0.00	0.00	0.10	0.00	6.00	2.00	0.00	0.00	0.10	0.00
6.10	2.00	0.00	0.00	0.10	0.00	6.20	2.00	0.00	0.00	0.10	0.00
6.30	2.00	0.00	0.00	0.10	0.00	6.40	2.00	0.00	0.00	0.10	0.00
6.50	2.00	0.00	0.00	0.10	0.00	6.60	2.00	0.00	0.00	0.10	0.00
6.70	2.00	0.00	0.00	0.10	0.00	6.80	2.00	0.00	0.00	0.10	0.00
6.90	2.00	0.00	0.00	0.10	0.00	7.00	2.00	0.00	0.00	0.10	0.00
7.10	2.00	0.00	0.00	0.10	0.00	7.20	2.00	0.00	0.00	0.10	0.00
7.30	2.00	0.00	0.00	0.10	0.00	7.40	2.00	0.00	0.00	0.10	0.00
7.50	2.00	0.00	0.00	0.10	0.00	7.60	2.00	0.00	0.00	0.10	0.00
7.70	2.00	0.00	0.00	0.10	0.00	7.80	2.00	0.00	0.00	0.10	0.00
7.90	2.00	0.00	0.00	0.10	0.00	8.00	2.00	0.00	0.00	0.10	0.00
8.10	2.00	0.00	0.00	0.10	0.00	8.20	2.00	0.00	0.00	0.10	0.00
8.30	2.00	0.00	0.00	0.10	0.00	8.40	2.00	0.00	0.00	0.10	0.00
8.50	2.00	0.00	0.00	0.10	0.00	8.60	2.00	0.00	0.00	0.10	0.00
8.70	0.23	0.00	0.00	0.10	0.20	8.80	0.23	0.00	0.00	0.10	0.20
8.90	2.00	0.00	0.00	0.10	0.00	9.00	2.00	0.00	0.00	0.10	0.00
9.10	2.00	0.00	0.00	0.10	0.00	9.20	2.00	0.00	0.00	0.10	0.00
9.30	0.59	0.00	0.00	0.10	0.11	9.40	0.57	0.00	0.00	0.10	0.11
9.50	0.87	0.00	0.00	0.10	0.03	9.60	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
9.70	1.86	0.00	0.00	0.10	0.00	9.80	2.00	0.00	0.00	0.10	0.00
9.90	2.00	0.00	0.00	0.10	0.00	10.00	1.76	0.00	0.00	0.10	0.00
10.10	1.08	0.00	0.00	0.10	0.00	10.20	0.94	0.00	0.00	0.10	0.02
10.30	1.36	0.00	0.00	0.10	0.00	10.40	1.74	0.00	0.00	0.10	0.00
10.50	2.00	0.00	0.00	0.10	0.00	10.60	2.00	0.00	0.00	0.10	0.00
10.70	1.84	0.00	0.00	0.10	0.00	10.80	1.42	0.00	0.00	0.10	0.00
10.90	0.97	0.00	0.00	0.10	0.01	11.00	0.67	0.00	0.00	0.10	0.08
11.10	0.51	0.00	0.00	0.10	0.12	11.20	0.45	0.00	0.00	0.10	0.14
11.30	0.43	0.00	0.00	0.10	0.14	11.40	0.43	0.00	0.00	0.10	0.14
11.50	0.43	0.00	0.00	0.10	0.14	11.60	0.42	0.00	0.00	0.10	0.15
11.70	0.42	0.00	0.00	0.10	0.15	11.80	0.41	0.00	0.00	0.10	0.15
11.90	0.39	0.00	0.00	0.10	0.15	12.00	0.42	0.00	0.00	0.10	0.14
12.10	0.49	0.00	0.00	0.10	0.13	12.20	0.56	0.00	0.00	0.10	0.11
12.30	0.59	0.00	0.00	0.10	0.10	12.40	0.58	0.00	0.00	0.10	0.10
12.50	0.58	0.00	0.00	0.10	0.10	12.60	0.57	0.00	0.00	0.10	0.11
12.70	0.57	0.00	0.00	0.10	0.11	12.80	0.56	0.00	0.00	0.10	0.11
12.90	0.56	0.00	0.00	0.10	0.11	13.00	0.58	0.00	0.00	0.10	0.10
13.10	0.63	0.00	0.00	0.10	0.09	13.20	0.65	0.00	0.00	0.10	0.08
13.30	0.58	0.00	0.00	0.10	0.10	13.40	0.46	0.00	0.00	0.10	0.13
13.50	0.38	0.00	0.00	0.10	0.15	13.60	0.35	0.00	0.00	0.10	0.16
13.70	0.35	0.00	0.00	0.10	0.16	13.80	0.35	0.00	0.00	0.10	0.16
13.90	0.35	0.00	0.00	0.10	0.16	14.00	0.34	0.00	0.00	0.10	0.16
14.10	0.34	0.00	0.00	0.10	0.16	14.20	0.34	0.00	0.00	0.10	0.16
14.30	0.31	0.00	0.00	0.10	0.16	14.40	0.28	0.00	0.00	0.10	0.17
14.50	0.28	0.00	0.00	0.10	0.17	14.60	0.30	0.00	0.00	0.10	0.17
14.70	0.34	0.00	0.00	0.10	0.16	14.80	0.38	0.00	0.00	0.10	0.15
14.90	0.45	0.00	0.00	0.10	0.13	15.00	0.54	0.00	0.00	0.10	0.11
15.10	0.63	0.00	0.00	0.10	0.09	15.20	0.86	0.00	0.00	0.10	0.03
15.30	2.00	0.00	0.00	0.10	0.00	15.40	2.00	0.00	0.00	0.10	0.00
15.50	2.00	0.00	0.00	0.10	0.00	15.60	2.00	0.00	0.00	0.10	0.00
15.70	2.00	0.00	0.00	0.10	0.00	15.80	2.00	0.00	0.00	0.10	0.00
15.90	2.00	0.00	0.00	0.10	0.00	16.00	2.00	0.00	0.00	0.10	0.00
16.10	0.67	0.00	0.00	0.10	0.08	16.20	0.65	0.00	0.00	0.10	0.08
16.30	0.67	0.00	0.00	0.10	0.08	16.40	2.00	0.00	0.00	0.10	0.00
16.50	2.00	0.00	0.00	0.10	0.00	16.60	2.00	0.00	0.00	0.10	0.00
16.70	2.00	0.00	0.00	0.10	0.00	16.80	2.00	0.00	0.00	0.10	0.00
16.90	2.00	0.00	0.00	0.10	0.00	17.00	2.00	0.00	0.00	0.10	0.00
17.10	2.00	0.00	0.00	0.10	0.00	17.20	2.00	0.00	0.00	0.10	0.00
17.30	0.61	0.00	0.00	0.10	0.09	17.40	0.47	0.00	0.00	0.10	0.12
17.50	0.41	0.00	0.00	0.10	0.13	17.60	0.39	0.00	0.00	0.10	0.14
17.70	0.39	0.00	0.00	0.10	0.14	17.80	0.39	0.00	0.00	0.10	0.14
17.90	0.39	0.00	0.00	0.10	0.14	18.00	0.40	0.00	0.00	0.10	0.13
18.10	0.43	0.00	0.00	0.10	0.13	18.20	0.47	0.00	0.00	0.10	0.12
18.30	0.50	0.00	0.00	0.10	0.11	18.40	0.53	0.00	0.00	0.10	0.10
18.50	0.58	0.00	0.00	0.10	0.09	18.60	0.67	0.00	0.00	0.10	0.07
18.70	0.79	0.00	0.00	0.10	0.05	18.80	0.96	0.00	0.00	0.10	0.01
18.90	1.19	0.00	0.00	0.10	0.00	19.00	1.39	0.00	0.00	0.10	0.00
19.10	1.50	0.00	0.00	0.10	0.00	19.20	1.49	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
19.30	1.41	0.00	0.00	0.10	0.00	19.40	1.28	0.00	0.00	0.10	0.00
19.50	1.17	0.00	0.00	0.10	0.00	19.60	1.16	0.00	0.00	0.10	0.00
19.70	1.30	0.00	0.00	0.10	0.00	19.80	1.48	0.00	0.00	0.10	0.00
19.90	1.60	0.00	0.00	0.10	0.00	20.00	1.51	0.00	0.00	0.10	0.00
20.10	1.22	0.00	0.00	0.10	0.00	20.20	0.86	0.00	0.00	0.10	0.03
20.30	0.58	0.00	0.00	0.10	0.09	20.40	0.45	0.00	0.00	0.10	0.12
20.50	0.38	0.00	0.00	0.10	0.13	20.60	0.34	0.00	0.00	0.10	0.14
20.70	0.33	0.00	0.00	0.10	0.14	20.80	0.32	0.00	0.00	0.10	0.14
20.90	0.32	0.00	0.00	0.10	0.14	21.00	0.31	0.00	0.00	0.10	0.14
21.10	0.31	0.00	0.00	0.10	0.14	21.20	0.34	0.00	0.00	0.10	0.14
21.30	0.37	0.00	0.00	0.10	0.13	21.40	0.43	0.00	0.00	0.10	0.12
21.50	0.48	0.00	0.00	0.10	0.11	21.60	0.51	0.00	0.00	0.10	0.10
21.70	0.53	0.00	0.00	0.10	0.10	21.80	0.52	0.00	0.00	0.10	0.10
21.90	0.49	0.00	0.00	0.10	0.10	22.00	0.45	0.00	0.00	0.10	0.11
22.10	0.44	0.00	0.00	0.10	0.11	22.20	0.46	0.00	0.00	0.10	0.11
22.30	0.52	0.00	0.00	0.10	0.10	22.40	0.59	0.00	0.00	0.10	0.08
22.50	0.76	0.00	0.00	0.10	0.05	22.60	1.06	0.00	0.00	0.10	0.00
22.70	1.49	0.00	0.00	0.10	0.00	22.80	2.00	0.00	0.00	0.10	0.00
22.90	2.00	0.00	0.00	0.10	0.00	23.00	2.00	0.00	0.00	0.10	0.00
23.10	2.00	0.00	0.00	0.10	0.00	23.20	1.99	0.00	0.00	0.10	0.00
23.30	1.81	0.00	0.00	0.10	0.00	23.40	1.67	0.00	0.00	0.10	0.00
23.50	1.58	0.00	0.00	0.10	0.00	23.60	2.00	0.00	0.00	0.10	0.00
23.70	2.00	0.00	0.00	0.10	0.00	23.80	2.00	0.00	0.00	0.10	0.00
23.90	2.00	0.00	0.00	0.10	0.00	24.00	2.00	0.00	0.00	0.10	0.00
24.10	2.00	0.00	0.00	0.10	0.00	24.20	2.00	0.00	0.00	0.10	0.00
24.30	2.00	0.00	0.00	0.10	0.00	24.40	2.00	0.00	0.00	0.10	0.00
24.50	2.00	0.00	0.00	0.10	0.00	24.60	0.69	0.00	0.00	0.10	0.06
24.70	0.78	0.00	0.00	0.10	0.04	24.80	0.76	0.00	0.00	0.10	0.05
24.90	0.64	0.00	0.00	0.10	0.07	25.00	0.54	0.00	0.00	0.10	0.09
25.10	0.53	0.00	0.00	0.10	0.09	25.20	0.61	0.00	0.00	0.10	0.07
25.30	0.69	0.00	0.00	0.10	0.06	25.40	2.00	0.00	0.00	0.10	0.00
25.50	2.00	0.00	0.00	0.10	0.00	25.60	2.00	0.00	0.00	0.10	0.00
25.70	2.00	0.00	0.00	0.10	0.00	25.80	2.00	0.00	0.00	0.10	0.00
25.90	2.00	0.00	0.00	0.10	0.00	26.00	2.00	0.00	0.00	0.10	0.00
26.10	0.84	0.00	0.00	0.10	0.03	26.20	0.65	0.00	0.00	0.10	0.06
26.30	0.60	0.00	0.00	0.10	0.07	26.40	0.60	0.00	0.00	0.10	0.07
26.50	0.61	0.00	0.00	0.10	0.07	26.60	0.62	0.00	0.00	0.10	0.07
26.70	0.66	0.00	0.00	0.10	0.06	26.80	0.72	0.00	0.00	0.10	0.05
26.90	0.77	0.00	0.00	0.10	0.04	27.00	0.77	0.00	0.00	0.10	0.04
27.10	0.71	0.00	0.00	0.10	0.05	27.20	0.59	0.00	0.00	0.10	0.07
27.30	0.48	0.00	0.00	0.10	0.09	27.40	0.44	0.00	0.00	0.10	0.10
27.50	0.46	0.00	0.00	0.10	0.10	27.60	0.49	0.00	0.00	0.10	0.09
27.70	0.49	0.00	0.00	0.10	0.09	27.80	0.49	0.00	0.00	0.10	0.09
27.90	0.49	0.00	0.00	0.10	0.09	28.00	0.48	0.00	0.00	0.10	0.09
28.10	0.51	0.00	0.00	0.10	0.08	28.20	0.71	0.00	0.00	0.10	0.05
28.30	1.14	0.00	0.00	0.10	0.00	28.40	1.67	0.00	0.00	0.10	0.00
28.50	2.00	0.00	0.00	0.10	0.00	28.60	2.00	0.00	0.00	0.10	0.00
28.70	1.76	0.00	0.00	0.10	0.00	28.80	1.55	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
28.90	2.00	0.00	0.00	0.10	0.00	29.00	2.00	0.00	0.00	0.10	0.00
29.10	2.00	0.00	0.00	0.10	0.00	29.20	2.00	0.00	0.00	0.10	0.00
29.30	2.00	0.00	0.00	0.10	0.00	29.40	2.00	0.00	0.00	0.10	0.00
29.50	2.00	0.00	0.00	0.10	0.00	29.60	2.00	0.00	0.00	0.10	0.00
29.70	2.00	0.00	0.00	0.10	0.00	29.80	0.89	0.00	0.00	0.10	0.02
29.90	0.75	0.00	0.00	0.10	0.04	30.00	0.71	0.00	0.00	0.10	0.05
30.10	0.80	0.00	0.00	0.10	0.03	30.20	0.88	0.00	0.00	0.10	0.02
30.30	0.81	0.00	0.00	0.10	0.03	30.40	0.66	0.00	0.00	0.10	0.06
30.50	2.00	0.00	0.00	0.10	0.00	30.60	2.00	0.00	0.00	0.10	0.00
30.70	2.00	0.00	0.00	0.10	0.00	30.80	2.00	0.00	0.00	0.10	0.00
30.90	2.00	0.00	0.00	0.10	0.00	31.00	2.00	0.00	0.00	0.10	0.00
31.10	2.00	0.00	0.00	0.10	0.00	31.20	0.70	0.00	0.00	0.10	0.05
31.30	0.66	0.00	0.00	0.10	0.05	31.40	0.79	0.00	0.00	0.10	0.03
31.50	2.00	0.00	0.00	0.10	0.00	31.60	2.00	0.00	0.00	0.10	0.00
31.70	2.00	0.00	0.00	0.10	0.00	31.80	2.00	0.00	0.00	0.10	0.00
31.90	2.00	0.00	0.00	0.10	0.00	32.00	2.00	0.00	0.00	0.10	0.00
32.10	2.00	0.00	0.00	0.10	0.00	32.20	2.00	0.00	0.00	0.10	0.00
32.30	2.00	0.00	0.00	0.10	0.00	32.40	2.00	0.00	0.00	0.10	0.00
32.50	2.00	0.00	0.00	0.10	0.00	32.60	2.00	0.00	0.00	0.10	0.00
32.70	2.00	0.00	0.00	0.10	0.00	32.80	2.00	0.00	0.00	0.10	0.00
32.90	2.00	0.00	0.00	0.10	0.00	33.00	1.45	0.00	0.00	0.10	0.00
33.10	1.48	0.00	0.00	0.10	0.00	33.20	1.54	0.00	0.00	0.10	0.00
33.30	1.59	0.00	0.00	0.10	0.00	33.40	2.00	0.00	0.00	0.10	0.00
33.50	2.00	0.00	0.00	0.10	0.00	33.60	2.00	0.00	0.00	0.10	0.00
33.70	2.00	0.00	0.00	0.10	0.00	33.80	2.00	0.00	0.00	0.10	0.00
33.90	2.00	0.00	0.00	0.10	0.00	34.00	2.00	0.00	0.00	0.10	0.00
34.10	1.71	0.00	0.00	0.10	0.00	34.20	1.48	0.00	0.00	0.10	0.00
34.30	2.00	0.00	0.00	0.10	0.00	34.40	2.00	0.00	0.00	0.10	0.00
34.50	2.00	0.00	0.00	0.10	0.00	34.60	2.00	0.00	0.00	0.10	0.00
34.70	2.00	0.00	0.00	0.10	0.00	34.80	2.00	0.00	0.00	0.10	0.00
34.90	2.00	0.00	0.00	0.10	0.00	35.00	2.00	0.00	0.00	0.10	0.00
35.10	2.00	0.00	0.00	0.10	0.00	35.20	2.00	0.00	0.00	0.10	0.00
35.30	1.16	0.00	0.00	0.10	0.00	35.40	1.17	0.00	0.00	0.10	0.00
35.50	1.19	0.00	0.00	0.10	0.00	35.60	1.29	0.00	0.00	0.10	0.00
35.70	1.50	0.00	0.00	0.10	0.00	35.80	2.00	0.00	0.00	0.10	0.00
35.90	2.00	0.00	0.00	0.10	0.00	36.00	2.00	0.00	0.00	0.10	0.00
36.10	1.98	0.00	0.00	0.10	0.00	36.20	1.70	0.00	0.00	0.10	0.00
36.30	1.41	0.00	0.00	0.10	0.00	36.40	2.00	0.00	0.00	0.10	0.00
36.50	2.00	0.00	0.00	0.10	0.00	36.60	2.00	0.00	0.00	0.10	0.00
36.70	2.00	0.00	0.00	0.10	0.00	36.80	2.00	0.00	0.00	0.10	0.00
36.90	2.00	0.00	0.00	0.10	0.00	37.00	2.00	0.00	0.00	0.10	0.00
37.10	2.00	0.00	0.00	0.10	0.00	37.20	2.00	0.00	0.00	0.10	0.00
37.30	2.00	0.00	0.00	0.10	0.00	37.40	2.00	0.00	0.00	0.10	0.00
37.50	2.00	0.00	0.00	0.10	0.00	37.60	2.00	0.00	0.00	0.10	0.00
37.70	2.00	0.00	0.00	0.10	0.00	37.80	2.00	0.00	0.00	0.10	0.00
37.90	2.00	0.00	0.00	0.10	0.00	38.00	0.32	0.00	0.00	0.10	0.09
38.10	0.33	0.00	0.00	0.10	0.09	38.20	2.00	0.00	0.00	0.10	0.00
38.30	2.00	0.00	0.00	0.10	0.00	38.40	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
38.50	2.00	0.00	0.00	0.10	0.00	38.60	2.00	0.00	0.00	0.10	0.00
38.70	2.00	0.00	0.00	0.10	0.00	38.80	2.00	0.00	0.00	0.10	0.00
38.90	2.00	0.00	0.00	0.10	0.00	39.00	0.53	0.00	0.00	0.10	0.06
39.10	0.29	0.00	0.00	0.10	0.09	39.20	0.27	0.00	0.00	0.10	0.09
39.30	0.27	0.00	0.00	0.10	0.09	39.40	0.25	0.00	0.00	0.10	0.09
39.50	0.24	0.00	0.00	0.10	0.09	39.60	0.22	0.00	0.00	0.10	0.09
39.70	2.00	0.00	0.00	0.10	0.00	39.80	2.00	0.00	0.00	0.10	0.00
39.90	2.00	0.00	0.00	0.10	0.00	40.00	2.00	0.00	0.00	0.10	0.00
40.10	0.72	0.00	0.00	0.10	0.03	40.20	2.00	0.00	0.00	0.10	0.00
40.30	2.00	0.00	0.00	0.10	0.00	40.40	2.00	0.00	0.00	0.10	0.00
40.50	2.00	0.00	0.00	0.10	0.00	40.60	2.00	0.00	0.00	0.10	0.00
40.70	2.00	0.00	0.00	0.10	0.00	40.80	2.00	0.00	0.00	0.10	0.00
40.90	2.00	0.00	0.00	0.10	0.00	41.00	2.00	0.00	0.00	0.10	0.00
41.10	0.33	0.00	0.00	0.10	0.08	41.20	0.34	0.00	0.00	0.10	0.07
41.30	0.35	0.00	0.00	0.10	0.07	41.40	0.36	0.00	0.00	0.10	0.07
41.50	0.40	0.00	0.00	0.10	0.07	41.60	0.47	0.00	0.00	0.10	0.06
41.70	2.00	0.00	0.00	0.10	0.00	41.80	2.00	0.00	0.00	0.10	0.00
41.90	2.00	0.00	0.00	0.10	0.00	42.00	2.00	0.00	0.00	0.10	0.00
42.10	2.00	0.00	0.00	0.10	0.00	42.20	2.00	0.00	0.00	0.10	0.00
42.30	2.00	0.00	0.00	0.10	0.00	42.40	2.00	0.00	0.00	0.10	0.00
42.50	2.00	0.00	0.00	0.10	0.00	42.60	2.00	0.00	0.00	0.10	0.00
42.70	2.00	0.00	0.00	0.10	0.00	42.80	2.00	0.00	0.00	0.10	0.00
42.90	0.70	0.00	0.00	0.10	0.03	43.00	0.75	0.00	0.00	0.10	0.03
43.10	0.76	0.00	0.00	0.10	0.03	43.20	0.73	0.00	0.00	0.10	0.03
43.30	0.69	0.00	0.00	0.10	0.03	43.40	0.66	0.00	0.00	0.10	0.04
43.50	0.65	0.00	0.00	0.10	0.04	43.60	0.67	0.00	0.00	0.10	0.03
43.70	0.71	0.00	0.00	0.10	0.03	43.80	0.77	0.00	0.00	0.10	0.02
43.90	0.83	0.00	0.00	0.10	0.02	44.00	0.89	0.00	0.00	0.10	0.01
44.10	0.93	0.00	0.00	0.10	0.01	44.20	0.93	0.00	0.00	0.10	0.01
44.30	0.93	0.00	0.00	0.10	0.01	44.40	0.95	0.00	0.00	0.10	0.01
44.50	2.00	0.00	0.00	0.10	0.00	44.60	2.00	0.00	0.00	0.10	0.00
44.70	2.00	0.00	0.00	0.10	0.00	44.80	2.00	0.00	0.00	0.10	0.00
44.90	2.00	0.00	0.00	0.10	0.00	45.00	2.00	0.00	0.00	0.10	0.00
45.10	2.00	0.00	0.00	0.10	0.00	45.20	2.00	0.00	0.00	0.10	0.00
45.30	2.00	0.00	0.00	0.10	0.00	45.40	2.00	0.00	0.00	0.10	0.00
45.50	0.84	0.00	0.00	0.10	0.02	45.60	0.75	0.00	0.00	0.10	0.02
45.70	0.73	0.00	0.00	0.10	0.03	45.80	0.78	0.00	0.00	0.10	0.02
45.90	0.89	0.00	0.00	0.10	0.01	46.00	2.00	0.00	0.00	0.10	0.00
46.10	2.00	0.00	0.00	0.10	0.00	46.20	2.00	0.00	0.00	0.10	0.00
46.30	2.00	0.00	0.00	0.10	0.00	46.40	2.00	0.00	0.00	0.10	0.00
46.50	2.00	0.00	0.00	0.10	0.00	46.60	2.00	0.00	0.00	0.10	0.00
46.70	2.00	0.00	0.00	0.10	0.00	46.80	2.00	0.00	0.00	0.10	0.00
46.90	2.00	0.00	0.00	0.10	0.00	47.00	2.00	0.00	0.00	0.10	0.00
47.10	2.00	0.00	0.00	0.10	0.00	47.20	2.00	0.00	0.00	0.10	0.00
47.30	2.00	0.00	0.00	0.10	0.00	47.40	2.00	0.00	0.00	0.10	0.00
47.50	2.00	0.00	0.00	0.10	0.00	47.60	2.00	0.00	0.00	0.10	0.00
47.70	2.00	0.00	0.00	0.10	0.00	47.80	2.00	0.00	0.00	0.10	0.00
47.90	2.00	0.00	0.00	0.10	0.00	48.00	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
48.10	2.00	0.00	0.00	0.10	0.00	48.20	2.00	0.00	0.00	0.10	0.00
48.30	2.00	0.00	0.00	0.10	0.00	48.40	2.00	0.00	0.00	0.10	0.00
48.50	2.00	0.00	0.00	0.10	0.00	48.60	2.00	0.00	0.00	0.10	0.00
48.70	2.00	0.00	0.00	0.10	0.00	48.80	2.00	0.00	0.00	0.10	0.00
48.90	2.00	0.00	0.00	0.10	0.00	49.00	2.00	0.00	0.00	0.10	0.00
49.10	2.00	0.00	0.00	0.10	0.00	49.20	2.00	0.00	0.00	0.10	0.00
49.30	2.00	0.00	0.00	0.10	0.00	49.40	2.00	0.00	0.00	0.10	0.00
49.50	2.00	0.00	0.00	0.10	0.00	49.60	2.00	0.00	0.00	0.10	0.00
49.70	2.00	0.00	0.00	0.10	0.00	49.80	2.00	0.00	0.00	0.10	0.00
49.90	2.00	0.00	0.00	0.10	0.00						

Overall liquefaction potential: 14.99

LPI = 0.00 - Liquefaction risk very low

LPI between 0.00 and 5.00 - Liquefaction risk low

LPI between 5.00 and 15.00 - Liquefaction risk high

LPI > 15.00 - Liquefaction risk very high

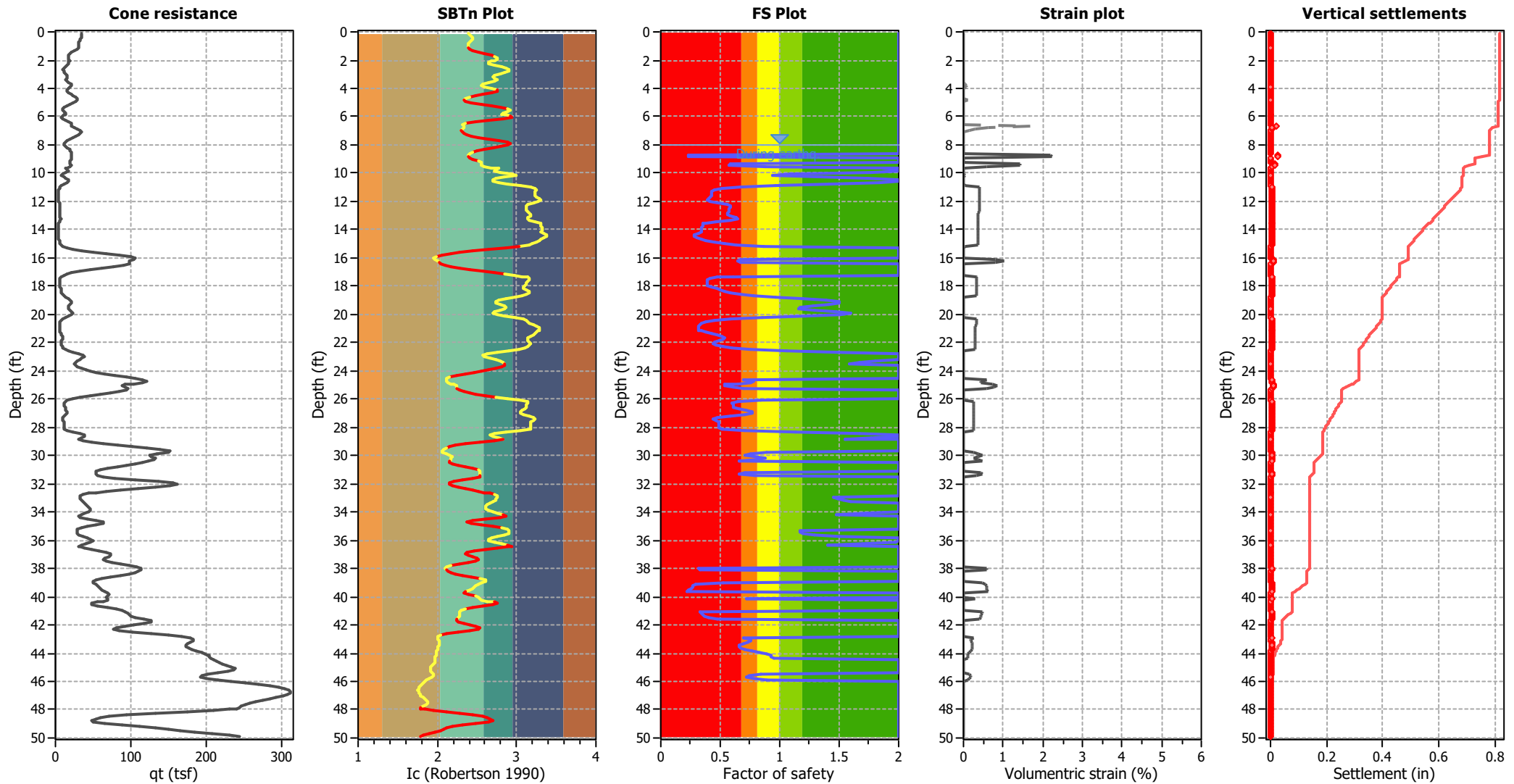
Abbreviations

FS: Calculated factor of safety for test point

F_L: 1 - FSw_z: Function value of the extend of soil liquefaction according to depthd_z: Layer thickness (ft)

LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

- q_c: Total cone resistance (cone resistance q_c corrected for pore water effects)
- I_c: Soil Behaviour Type Index
- FS: Calculated Factor of Safety against liquefaction
- Volumetric strain: Post-liquefaction volumetric strain

:: Post-earthquake settlement of dry sands ::												
Depth (ft)	Ic	Q _{tn}	Kc	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _r (%)	Settle. (in)
0.10	2.40	66.19	2.36	156.19	38	656	0.59	0.000	0.00	13.69	0.00	0.000
0.20	2.41	66.44	2.40	159.73	39	666	0.59	0.001	0.00	13.69	0.00	0.000
0.30	2.42	65.62	2.50	164.28	41	673	0.59	0.002	0.00	13.69	0.00	0.000
0.40	2.44	63.56	2.61	165.68	42	667	0.59	0.002	0.00	13.69	0.00	0.000
0.50	2.44	61.31	2.62	160.84	40	645	0.59	0.003	0.00	13.69	0.00	0.000
0.60	2.43	59.84	2.53	151.50	38	617	0.59	0.004	0.00	13.69	0.00	0.000
0.70	2.41	58.94	2.42	142.68	35	593	0.59	0.005	0.00	13.69	0.00	0.000
0.80	2.39	58.64	2.35	137.66	34	580	0.59	0.006	0.00	13.69	0.00	0.000
0.90	2.39	58.63	2.32	135.92	33	575	0.59	0.007	0.00	13.69	0.00	0.000
1.00	2.39	58.46	2.31	135.02	33	572	0.59	0.008	0.00	13.69	0.00	0.000
1.10	2.39	57.00	2.33	132.82	33	561	0.59	0.009	0.01	13.69	0.00	0.000
1.20	2.41	53.96	2.40	129.71	0	0	0.59	0.000	0.00	13.69	0.00	0.000
1.30	2.45	47.65	2.65	126.49	0	0	0.59	0.000	0.00	13.69	0.00	0.000
1.40	2.52	40.40	3.15	127.07	0	0	0.59	0.000	0.00	13.69	0.00	0.000
1.50	2.60	37.17	3.72	138.20	0	0	0.59	0.000	0.00	0.00	0.00	0.000
1.60	2.67	33.40	4.45	148.53	0	0	0.59	0.000	0.00	0.00	0.00	0.000
1.70	2.73	32.47	4.98	161.78	0	0	0.59	0.000	0.00	0.00	0.00	0.000
1.80	2.76	31.95	5.42	173.34	0	0	0.59	0.000	0.00	0.00	0.00	0.000
1.90	2.75	33.69	5.24	176.60	0	0	0.59	0.000	0.00	0.00	0.00	0.000
2.00	2.72	34.19	4.93	168.40	0	0	0.59	0.000	0.00	0.00	0.00	0.000
2.10	2.68	33.31	4.50	149.97	0	0	0.59	0.000	0.00	0.00	0.00	0.000
2.20	2.65	33.41	4.16	139.04	0	0	0.59	0.000	0.00	0.00	0.00	0.000
2.30	2.65	32.44	4.23	137.06	0	0	0.59	0.000	0.00	0.00	0.00	0.000
2.40	2.72	28.37	4.90	138.92	0	0	0.59	0.000	0.00	0.00	0.00	0.000
2.50	2.80	23.68	5.90	139.78	0	0	0.59	0.000	0.00	0.00	0.00	0.000
2.60	2.87	20.18	6.83	137.90	0	0	0.59	0.000	0.00	0.00	0.00	0.000
2.70	2.90	18.96	7.24	137.27	0	0	0.59	0.000	0.00	0.00	0.00	0.000
2.80	2.90	19.18	7.17	137.46	0	0	0.59	0.000	0.00	0.00	0.00	0.000
2.90	2.85	21.26	6.56	139.51	0	0	0.59	0.000	0.00	0.00	0.00	0.000
3.00	2.79	24.56	5.69	139.87	0	0	0.59	0.000	0.00	0.00	0.00	0.000
3.10	2.73	27.98	4.98	139.23	0	0	0.59	0.000	0.00	0.00	0.00	0.000
3.20	2.70	28.93	4.75	137.31	0	0	0.59	0.000	0.00	0.00	0.00	0.000
3.30	2.73	27.28	4.99	136.17	0	0	0.59	0.000	0.00	0.00	0.00	0.000
3.40	2.75	26.06	5.29	137.84	0	0	0.59	0.000	0.00	0.00	0.00	0.000
3.50	2.73	27.99	4.99	139.69	0	0	0.59	0.000	0.00	0.00	0.00	0.000
3.60	2.65	32.64	4.22	137.86	0	0	0.59	0.000	0.00	0.00	0.00	0.000
3.70	2.58	37.43	3.55	132.82	36	465	0.59	0.119	0.06	13.69	0.05	0.001
3.80	2.55	38.92	3.35	130.32	34	468	0.59	0.123	0.06	13.69	0.06	0.001
3.90	2.59	36.20	3.67	132.70	36	458	0.59	0.143	0.07	13.69	0.06	0.001
4.00	2.68	31.19	4.50	140.21	0	0	0.59	0.000	0.00	0.00	0.00	0.000
4.10	2.76	27.70	5.34	147.79	0	0	0.59	0.000	0.00	0.00	0.00	0.000
4.20	2.76	28.11	5.37	150.90	0	0	0.59	0.000	0.00	0.00	0.00	0.000
4.30	2.69	31.89	4.58	146.16	0	0	0.59	0.000	0.00	0.00	0.00	0.000
4.40	2.58	37.64	3.60	135.32	0	0	0.59	0.000	0.00	0.00	0.00	0.000
4.50	2.48	43.68	2.85	124.44	0	0	0.59	0.000	0.00	13.69	0.00	0.000
4.60	2.40	49.32	2.38	117.41	0	0	0.59	0.000	0.00	13.69	0.00	0.000
4.70	2.35	52.95	2.13	112.80	0	0	0.59	0.000	0.00	13.69	0.00	0.000
4.80	2.33	53.35	2.04	109.09	26	486	0.59	0.180	0.13	13.69	0.11	0.001

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
4.90	2.36	50.07	2.15	107.83	0	0	0.59	0.000	0.00	13.69	0.00	0.000
5.00	2.43	43.58	2.54	110.85	0	0	0.59	0.000	0.00	13.69	0.00	0.000
5.10	2.55	34.79	3.34	116.24	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.20	2.68	26.62	4.53	120.63	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.30	2.80	20.85	5.82	121.41	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.40	2.88	17.43	6.89	120.05	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.50	2.93	15.83	7.62	120.59	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.60	2.88	19.16	6.98	133.71	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.70	2.84	22.80	6.32	144.16	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.80	2.80	25.30	5.91	149.41	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.90	2.86	20.82	6.68	139.04	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.00	2.92	16.66	7.53	125.43	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.10	2.95	14.11	7.89	111.36	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.20	2.83	16.93	6.22	105.22	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.30	2.64	23.93	4.14	98.95	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.40	2.48	31.87	2.82	89.84	0	0	0.58	0.000	0.00	13.69	0.00	0.000
6.50	2.36	37.05	2.16	80.05	0	0	0.58	0.000	0.00	13.69	0.00	0.000
6.60	2.32	39.02	1.99	77.54	0	0	0.58	0.000	0.00	13.69	0.00	0.000
6.70	2.34	40.00	2.08	83.30	20	368	0.58	2.003	2.01	13.69	1.69	0.020
6.80	2.34	45.65	2.10	95.64	23	422	0.58	0.895	0.76	13.69	0.64	0.008
6.90	2.32	53.97	1.98	107.12	25	482	0.58	0.446	0.34	13.69	0.28	0.003
7.00	2.29	61.66	1.90	117.36	28	536	0.58	0.276	0.19	13.69	0.16	0.002
7.10	2.31	64.23	1.96	125.84	0	0	0.58	0.000	0.00	13.69	0.00	0.000
7.20	2.34	62.20	2.09	129.71	0	0	0.58	0.000	0.00	13.69	0.00	0.000
7.30	2.37	57.74	2.25	129.63	0	0	0.58	0.000	0.00	13.69	0.00	0.000
7.40	2.43	50.89	2.56	130.17	0	0	0.58	0.000	0.00	13.69	0.00	0.000
7.50	2.53	42.95	3.17	136.23	0	0	0.58	0.000	0.00	13.69	0.00	0.000
7.60	2.65	34.80	4.22	146.94	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.70	2.78	27.54	5.61	154.44	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.80	2.88	22.42	6.98	156.54	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.90	2.92	20.64	7.52	155.17	0	0	0.58	0.000	0.00	0.00	0.00	0.000

Total estimated settlement: 0.04**Abbreviations**

Q_{tn}: Equivalent clean sand normalized cone resistance
 K_c: Fines correction factor
 Q_{tn,cs}: Post-liquefaction volumetric strain
 G_{max}: Small strain shear modulus
 CSR: Soil cyclic stress ratio
 γ: Cyclic shear strain
 e_{vol(15)}: Volumetric strain after 15 cycles
 N_c: Equivalent number of cycles
 e_v: Volumetric strain
 Settle.: Calculated settlement

:: Post-earthquake settlement due to soil liquefaction ::

Depth (ft)	Q _{tn,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	Q _{tn,cs}	FS	e _v (%)	DF	Settlement (in)
8.00	151.91	2.00	0.00	0.85	0.00	8.10	145.18	2.00	0.00	0.85	0.00
8.20	286.40	2.00	0.00	0.85	0.00	8.30	166.34	2.00	0.00	0.85	0.00
8.40	103.17	2.00	0.00	0.85	0.00	8.50	98.76	2.00	0.00	0.85	0.00
8.60	91.72	2.00	0.00	0.84	0.00	8.70	87.43	0.23	2.20	0.84	0.03

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
8.80	85.73	0.23	2.23	0.84	0.03	8.90	89.20	2.00	0.00	0.84	0.00
9.00	97.11	2.00	0.00	0.84	0.00	9.10	105.02	2.00	0.00	0.83	0.00
9.20	136.03	2.00	0.00	0.83	0.00	9.30	146.00	0.59	1.42	0.83	0.02
9.40	144.33	0.57	1.43	0.83	0.02	9.50	172.27	0.87	0.58	0.83	0.01
9.60	253.31	2.00	0.00	0.83	0.00	9.70	136.76	1.86	0.00	0.82	0.00
9.80	147.38	2.00	0.00	0.82	0.00	9.90	147.04	2.00	0.00	0.82	0.00
10.00	136.49	1.76	0.00	0.82	0.00	10.10	117.16	1.08	0.01	0.82	0.00
10.20	112.59	0.94	0.02	0.81	0.00	10.30	121.71	1.36	0.01	0.81	0.00
10.40	126.27	1.74	0.00	0.81	0.00	10.50	278.42	2.00	0.00	0.81	0.00
10.60	137.94	2.00	0.00	0.81	0.00	10.70	143.09	1.84	0.00	0.81	0.00
10.80	142.45	1.42	0.00	0.80	0.00	10.90	131.66	0.97	0.02	0.80	0.00
11.00	115.56	0.67	0.40	0.80	0.00	11.10	100.33	0.51	0.40	0.80	0.00
11.20	89.78	0.45	0.40	0.80	0.00	11.30	85.17	0.43	0.40	0.79	0.00
11.40	83.25	0.43	0.40	0.79	0.00	11.50	82.98	0.43	0.40	0.79	0.00
11.60	83.97	0.42	0.39	0.79	0.00	11.70	85.91	0.42	0.39	0.79	0.00
11.80	87.52	0.41	0.39	0.79	0.00	11.90	87.81	0.39	0.39	0.78	0.00
12.00	90.30	0.42	0.39	0.78	0.00	12.10	94.05	0.49	0.39	0.78	0.00
12.20	96.95	0.56	0.39	0.78	0.00	12.30	97.04	0.59	0.39	0.78	0.00
12.40	96.01	0.58	0.39	0.77	0.00	12.50	95.92	0.58	0.39	0.77	0.00
12.60	96.89	0.57	0.39	0.77	0.00	12.70	98.95	0.57	0.38	0.77	0.00
12.80	101.97	0.56	0.38	0.77	0.00	12.90	105.47	0.56	0.38	0.77	0.00
13.00	109.74	0.58	0.38	0.76	0.00	13.10	113.73	0.63	0.38	0.76	0.00
13.20	113.54	0.65	0.38	0.76	0.00	13.30	107.61	0.58	0.38	0.76	0.00
13.40	97.66	0.46	0.38	0.76	0.00	13.50	89.03	0.38	0.38	0.75	0.00
13.60	84.82	0.35	0.38	0.75	0.00	13.70	83.51	0.35	0.38	0.75	0.00
13.80	84.20	0.35	0.37	0.75	0.00	13.90	86.06	0.35	0.37	0.75	0.00
14.00	87.11	0.34	0.37	0.75	0.00	14.10	86.08	0.34	0.37	0.74	0.00
14.20	83.99	0.34	0.37	0.74	0.00	14.30	80.89	0.31	0.37	0.74	0.00
14.40	78.42	0.28	0.37	0.74	0.00	14.50	78.04	0.28	0.37	0.74	0.00
14.60	79.17	0.30	0.37	0.73	0.00	14.70	83.01	0.34	0.37	0.73	0.00
14.80	89.86	0.38	0.37	0.73	0.00	14.90	100.58	0.45	0.36	0.73	0.00
15.00	111.96	0.54	0.36	0.73	0.00	15.10	121.16	0.63	0.36	0.73	0.00
15.20	133.51	0.86	0.02	0.72	0.00	15.30	142.43	2.00	0.00	0.72	0.00
15.40	249.99	2.00	0.00	0.72	0.00	15.50	132.07	2.00	0.00	0.72	0.00
15.60	129.32	2.00	0.00	0.72	0.00	15.70	140.05	2.00	0.00	0.71	0.00
15.80	154.02	2.00	0.00	0.71	0.00	15.90	168.64	2.00	0.00	0.71	0.00
16.00	172.49	2.00	0.00	0.71	0.00	16.10	169.98	0.67	0.82	0.71	0.01
16.20	167.57	0.65	1.01	0.71	0.01	16.30	169.86	0.67	0.82	0.70	0.01
16.40	171.44	2.00	0.00	0.70	0.00	16.50	164.92	2.00	0.00	0.70	0.00
16.60	156.50	2.00	0.00	0.70	0.00	16.70	152.38	2.00	0.00	0.70	0.00
16.80	153.43	2.00	0.00	0.69	0.00	16.90	194.75	2.00	0.00	0.69	0.00
17.00	149.00	2.00	0.00	0.69	0.00	17.10	137.50	2.00	0.00	0.69	0.00
17.20	122.13	2.00	0.00	0.69	0.00	17.30	106.07	0.61	0.34	0.69	0.00
17.40	92.75	0.47	0.34	0.68	0.00	17.50	84.31	0.41	0.34	0.68	0.00
17.60	79.47	0.39	0.34	0.68	0.00	17.70	76.40	0.39	0.34	0.68	0.00
17.80	74.35	0.39	0.34	0.68	0.00	17.90	72.87	0.39	0.34	0.67	0.00
18.00	73.35	0.40	0.34	0.67	0.00	18.10	77.52	0.43	0.34	0.67	0.00
18.20	86.59	0.47	0.33	0.67	0.00	18.30	97.84	0.50	0.33	0.67	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
18.40	110.45	0.53	0.33	0.67	0.00	18.50	121.37	0.58	0.33	0.66	0.00
18.60	130.42	0.67	0.33	0.66	0.00	18.70	137.35	0.79	0.33	0.66	0.00
18.80	141.97	0.96	0.01	0.66	0.00	18.90	142.29	1.19	0.01	0.66	0.00
19.00	137.61	1.39	0.00	0.65	0.00	19.10	134.56	1.50	0.00	0.65	0.00
19.20	136.81	1.49	0.00	0.65	0.00	19.30	142.80	1.41	0.00	0.65	0.00
19.40	145.07	1.28	0.00	0.65	0.00	19.50	141.25	1.17	0.01	0.65	0.00
19.60	134.47	1.16	0.01	0.64	0.00	19.70	131.33	1.30	0.00	0.64	0.00
19.80	132.10	1.48	0.00	0.64	0.00	19.90	136.95	1.60	0.00	0.64	0.00
20.00	142.04	1.51	0.00	0.64	0.00	20.10	140.38	1.22	0.00	0.63	0.00
20.20	128.64	0.86	0.01	0.63	0.00	20.30	107.93	0.58	0.32	0.63	0.00
20.40	90.08	0.45	0.31	0.63	0.00	20.50	79.02	0.38	0.31	0.63	0.00
20.60	74.02	0.34	0.31	0.63	0.00	20.70	75.85	0.33	0.31	0.62	0.00
20.80	80.95	0.32	0.31	0.62	0.00	20.90	84.69	0.32	0.31	0.62	0.00
21.00	85.19	0.31	0.31	0.62	0.00	21.10	83.89	0.31	0.31	0.62	0.00
21.20	86.65	0.34	0.31	0.61	0.00	21.30	94.51	0.37	0.31	0.61	0.00
21.40	105.08	0.43	0.31	0.61	0.00	21.50	112.96	0.48	0.30	0.61	0.00
21.60	115.54	0.51	0.30	0.61	0.00	21.70	113.59	0.53	0.30	0.61	0.00
21.80	108.42	0.52	0.30	0.60	0.00	21.90	102.78	0.49	0.30	0.60	0.00
22.00	98.57	0.45	0.30	0.60	0.00	22.10	98.11	0.44	0.30	0.60	0.00
22.20	101.78	0.46	0.30	0.60	0.00	22.30	108.47	0.52	0.30	0.59	0.00
22.40	117.69	0.59	0.30	0.59	0.00	22.50	130.38	0.76	0.30	0.59	0.00
22.60	140.54	1.06	0.01	0.59	0.00	22.70	144.22	1.49	0.00	0.59	0.00
22.80	238.98	2.00	0.00	0.59	0.00	22.90	203.56	2.00	0.00	0.58	0.00
23.00	232.50	2.00	0.00	0.58	0.00	23.10	321.34	2.00	0.00	0.58	0.00
23.20	186.79	1.99	0.00	0.58	0.00	23.30	193.53	1.81	0.00	0.58	0.00
23.40	195.41	1.67	0.00	0.57	0.00	23.50	194.81	1.58	0.00	0.57	0.00
23.60	195.02	2.00	0.00	0.57	0.00	23.70	195.78	2.00	0.00	0.57	0.00
23.80	194.00	2.00	0.00	0.57	0.00	23.90	324.77	2.00	0.00	0.57	0.00
24.00	213.85	2.00	0.00	0.56	0.00	24.10	166.42	2.00	0.00	0.56	0.00
24.20	154.76	2.00	0.00	0.56	0.00	24.30	150.17	2.00	0.00	0.56	0.00
24.40	155.95	2.00	0.00	0.56	0.00	24.50	167.93	2.00	0.00	0.55	0.00
24.60	179.54	0.69	0.59	0.55	0.01	24.70	188.31	0.78	0.44	0.55	0.01
24.80	186.07	0.76	0.45	0.55	0.01	24.90	174.94	0.64	0.74	0.55	0.01
25.00	163.53	0.54	0.85	0.55	0.01	25.10	162.47	0.53	0.85	0.54	0.01
25.20	171.07	0.61	0.75	0.54	0.01	25.30	179.84	0.69	0.58	0.54	0.01
25.40	185.09	2.00	0.00	0.54	0.00	25.50	185.93	2.00	0.00	0.54	0.00
25.60	184.22	2.00	0.00	0.53	0.00	25.70	181.87	2.00	0.00	0.53	0.00
25.80	261.58	2.00	0.00	0.53	0.00	25.90	177.19	2.00	0.00	0.53	0.00
26.00	168.46	2.00	0.00	0.53	0.00	26.10	152.57	0.84	0.01	0.53	0.00
26.20	138.34	0.65	0.26	0.52	0.00	26.30	130.48	0.60	0.26	0.52	0.00
26.40	128.32	0.60	0.26	0.52	0.00	26.50	128.19	0.61	0.26	0.52	0.00
26.60	130.07	0.62	0.26	0.52	0.00	26.70	134.19	0.66	0.26	0.51	0.00
26.80	138.10	0.72	0.26	0.51	0.00	26.90	141.00	0.77	0.26	0.51	0.00
27.00	141.53	0.77	0.25	0.51	0.00	27.10	138.95	0.71	0.25	0.51	0.00
27.20	130.94	0.59	0.25	0.51	0.00	27.30	120.75	0.48	0.25	0.50	0.00
27.40	114.25	0.44	0.25	0.50	0.00	27.50	113.31	0.46	0.25	0.50	0.00
27.60	114.18	0.49	0.25	0.50	0.00	27.70	113.35	0.49	0.25	0.50	0.00
27.80	113.23	0.49	0.25	0.49	0.00	27.90	113.51	0.49	0.25	0.49	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
28.00	114.54	0.48	0.25	0.49	0.00	28.10	118.10	0.51	0.24	0.49	0.00
28.20	131.07	0.71	0.24	0.49	0.00	28.30	146.37	1.14	0.00	0.49	0.00
28.40	159.28	1.67	0.00	0.48	0.00	28.50	330.06	2.00	0.00	0.48	0.00
28.60	384.44	2.00	0.00	0.48	0.00	28.70	185.09	1.76	0.00	0.48	0.00
28.80	185.71	1.55	0.00	0.48	0.00	28.90	180.95	2.00	0.00	0.47	0.00
29.00	169.60	2.00	0.00	0.47	0.00	29.10	168.11	2.00	0.00	0.47	0.00
29.20	135.74	2.00	0.00	0.47	0.00	29.30	136.78	2.00	0.00	0.47	0.00
29.40	150.70	2.00	0.00	0.47	0.00	29.50	168.35	2.00	0.00	0.46	0.00
29.60	186.85	2.00	0.00	0.46	0.00	29.70	200.29	2.00	0.00	0.46	0.00
29.80	199.31	0.89	0.26	0.46	0.00	29.90	187.01	0.75	0.37	0.46	0.00
30.00	183.25	0.71	0.47	0.45	0.01	30.10	191.06	0.80	0.36	0.45	0.00
30.20	198.22	0.88	0.26	0.45	0.00	30.30	191.86	0.81	0.35	0.45	0.00
30.40	177.76	0.66	0.49	0.45	0.01	30.50	165.69	2.00	0.00	0.45	0.00
30.60	159.60	2.00	0.00	0.44	0.00	30.70	160.35	2.00	0.00	0.44	0.00
30.80	165.73	2.00	0.00	0.44	0.00	30.90	169.28	2.00	0.00	0.44	0.00
31.00	167.08	2.00	0.00	0.44	0.00	31.10	186.24	2.00	0.00	0.43	0.00
31.20	182.33	0.70	0.45	0.43	0.01	31.30	177.30	0.66	0.47	0.43	0.01
31.40	190.56	0.79	0.34	0.43	0.00	31.50	194.81	2.00	0.00	0.43	0.00
31.60	191.72	2.00	0.00	0.43	0.00	31.70	196.67	2.00	0.00	0.42	0.00
31.80	206.96	2.00	0.00	0.42	0.00	31.90	218.92	2.00	0.00	0.42	0.00
32.00	225.02	2.00	0.00	0.42	0.00	32.10	223.85	2.00	0.00	0.42	0.00
32.20	220.31	2.00	0.00	0.41	0.00	32.30	215.22	2.00	0.00	0.41	0.00
32.40	206.72	2.00	0.00	0.41	0.00	32.50	203.45	2.00	0.00	0.41	0.00
32.60	247.28	2.00	0.00	0.41	0.00	32.70	302.64	2.00	0.00	0.41	0.00
32.80	156.67	2.00	0.00	0.40	0.00	32.90	150.72	2.00	0.00	0.40	0.00
33.00	147.55	1.45	0.00	0.40	0.00	33.10	147.34	1.48	0.00	0.40	0.00
33.20	147.24	1.54	0.00	0.40	0.00	33.30	145.11	1.59	0.00	0.39	0.00
33.40	270.78	2.00	0.00	0.39	0.00	33.50	234.17	2.00	0.00	0.39	0.00
33.60	220.10	2.00	0.00	0.39	0.00	33.70	221.59	2.00	0.00	0.39	0.00
33.80	238.92	2.00	0.00	0.39	0.00	33.90	278.05	2.00	0.00	0.38	0.00
34.00	359.09	2.00	0.00	0.38	0.00	34.10	176.17	1.71	0.00	0.38	0.00
34.20	176.54	1.48	0.00	0.38	0.00	34.30	169.90	2.00	0.00	0.38	0.00
34.40	155.78	2.00	0.00	0.37	0.00	34.50	200.32	2.00	0.00	0.37	0.00
34.60	119.37	2.00	0.00	0.37	0.00	34.70	122.97	2.00	0.00	0.37	0.00
34.80	137.27	2.00	0.00	0.37	0.00	34.90	184.58	2.00	0.00	0.37	0.00
35.00	348.76	2.00	0.00	0.36	0.00	35.10	163.48	2.00	0.00	0.36	0.00
35.20	159.94	2.00	0.00	0.36	0.00	35.30	159.50	1.16	0.00	0.36	0.00
35.40	162.04	1.17	0.00	0.36	0.00	35.50	163.54	1.19	0.00	0.35	0.00
35.60	160.16	1.29	0.00	0.35	0.00	35.70	152.87	1.50	0.00	0.35	0.00
35.80	296.08	2.00	0.00	0.35	0.00	35.90	261.07	2.00	0.00	0.35	0.00
36.00	301.48	2.00	0.00	0.35	0.00	36.10	180.94	1.98	0.00	0.34	0.00
36.20	189.00	1.70	0.00	0.34	0.00	36.30	188.59	1.41	0.00	0.34	0.00
36.40	180.83	2.00	0.00	0.34	0.00	36.50	170.18	2.00	0.00	0.34	0.00
36.60	156.90	2.00	0.00	0.33	0.00	36.70	204.72	2.00	0.00	0.33	0.00
36.80	127.19	2.00	0.00	0.33	0.00	36.90	122.48	2.00	0.00	0.33	0.00
37.00	127.09	2.00	0.00	0.33	0.00	37.10	136.52	2.00	0.00	0.33	0.00
37.20	146.83	2.00	0.00	0.32	0.00	37.30	153.93	2.00	0.00	0.32	0.00
37.40	153.05	2.00	0.00	0.32	0.00	37.50	149.45	2.00	0.00	0.32	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
37.60	138.09	2.00	0.00	0.32	0.00	37.70	127.65	2.00	0.00	0.31	0.00
37.80	123.99	2.00	0.00	0.31	0.00	37.90	126.65	2.00	0.00	0.31	0.00
38.00	130.53	0.32	0.58	0.31	0.01	38.10	132.78	0.33	0.57	0.31	0.01
38.20	132.53	2.00	0.00	0.31	0.00	38.30	131.22	2.00	0.00	0.30	0.00
38.40	131.23	2.00	0.00	0.30	0.00	38.50	136.26	2.00	0.00	0.30	0.00
38.60	146.85	2.00	0.00	0.30	0.00	38.70	175.12	2.00	0.00	0.30	0.00
38.80	229.02	2.00	0.00	0.29	0.00	38.90	212.25	2.00	0.00	0.29	0.00
39.00	161.33	0.53	0.46	0.29	0.01	39.10	124.58	0.29	0.56	0.29	0.01
39.20	120.48	0.27	0.58	0.29	0.01	39.30	118.64	0.27	0.58	0.29	0.01
39.40	115.94	0.25	0.59	0.28	0.01	39.50	111.83	0.24	0.60	0.28	0.01
39.60	107.16	0.22	0.62	0.28	0.01	39.70	110.39	2.00	0.00	0.28	0.00
39.80	125.93	2.00	0.00	0.28	0.00	39.90	145.04	2.00	0.00	0.27	0.00
40.00	166.60	2.00	0.00	0.27	0.00	40.10	181.70	0.72	0.29	0.27	0.00
40.20	217.36	2.00	0.00	0.27	0.00	40.30	311.00	2.00	0.00	0.27	0.00
40.40	193.81	2.00	0.00	0.27	0.00	40.50	183.22	2.00	0.00	0.26	0.00
40.60	164.01	2.00	0.00	0.26	0.00	40.70	187.62	2.00	0.00	0.26	0.00
40.80	132.29	2.00	0.00	0.26	0.00	40.90	128.74	2.00	0.00	0.26	0.00
41.00	129.21	2.00	0.00	0.25	0.00	41.10	130.80	0.33	0.47	0.25	0.01
41.20	132.67	0.34	0.46	0.25	0.01	41.30	134.68	0.35	0.46	0.25	0.01
41.40	136.86	0.36	0.45	0.25	0.01	41.50	142.79	0.40	0.43	0.25	0.01
41.60	152.96	0.47	0.40	0.24	0.00	41.70	164.07	2.00	0.00	0.24	0.00
41.80	172.61	2.00	0.00	0.24	0.00	41.90	179.16	2.00	0.00	0.24	0.00
42.00	188.10	2.00	0.00	0.24	0.00	42.10	192.82	2.00	0.00	0.23	0.00
42.20	201.46	2.00	0.00	0.23	0.00	42.30	167.51	2.00	0.00	0.23	0.00
42.40	146.57	2.00	0.00	0.23	0.00	42.50	133.70	2.00	0.00	0.23	0.00
42.60	138.14	2.00	0.00	0.23	0.00	42.70	153.07	2.00	0.00	0.22	0.00
42.80	167.96	2.00	0.00	0.22	0.00	42.90	177.73	0.70	0.24	0.22	0.00
43.00	182.50	0.75	0.18	0.22	0.00	43.10	182.89	0.76	0.18	0.22	0.00
43.20	180.31	0.73	0.23	0.21	0.00	43.30	176.56	0.69	0.23	0.21	0.00
43.40	173.54	0.66	0.24	0.21	0.00	43.50	172.68	0.65	0.24	0.21	0.00
43.60	174.28	0.67	0.23	0.21	0.00	43.70	178.11	0.71	0.22	0.21	0.00
43.80	183.48	0.77	0.17	0.20	0.00	43.90	189.21	0.83	0.16	0.20	0.00
44.00	194.05	0.89	0.12	0.20	0.00	44.10	196.61	0.93	0.11	0.20	0.00
44.20	196.91	0.93	0.11	0.20	0.00	44.30	196.89	0.93	0.11	0.19	0.00
44.40	198.22	0.95	0.11	0.19	0.00	44.50	201.32	2.00	0.00	0.19	0.00
44.60	204.72	2.00	0.00	0.19	0.00	44.70	207.51	2.00	0.00	0.19	0.00
44.80	209.99	2.00	0.00	0.19	0.00	44.90	213.26	2.00	0.00	0.18	0.00
45.00	217.83	2.00	0.00	0.18	0.00	45.10	221.09	2.00	0.00	0.18	0.00
45.20	219.53	2.00	0.00	0.18	0.00	45.30	211.91	2.00	0.00	0.18	0.00
45.40	200.16	2.00	0.00	0.17	0.00	45.50	188.42	0.84	0.14	0.17	0.00
45.60	180.45	0.75	0.18	0.17	0.00	45.70	178.17	0.73	0.18	0.17	0.00
45.80	182.74	0.78	0.14	0.17	0.00	45.90	192.70	0.89	0.10	0.17	0.00
46.00	205.69	2.00	0.00	0.16	0.00	46.10	219.97	2.00	0.00	0.16	0.00
46.20	233.02	2.00	0.00	0.16	0.00	46.30	243.21	2.00	0.00	0.16	0.00
46.40	248.44	2.00	0.00	0.16	0.00	46.50	250.22	2.00	0.00	0.15	0.00
46.60	252.23	2.00	0.00	0.15	0.00	46.70	255.70	2.00	0.00	0.15	0.00
46.80	257.78	2.00	0.00	0.15	0.00	46.90	257.39	2.00	0.00	0.15	0.00
47.00	255.10	2.00	0.00	0.15	0.00	47.10	252.16	2.00	0.00	0.14	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
47.20	247.76	2.00	0.00	0.14	0.00	47.30	241.83	2.00	0.00	0.14	0.00
47.40	234.75	2.00	0.00	0.14	0.00	47.50	227.31	2.00	0.00	0.14	0.00
47.60	219.72	2.00	0.00	0.13	0.00	47.70	211.94	2.00	0.00	0.13	0.00
47.80	204.06	2.00	0.00	0.13	0.00	47.90	199.14	2.00	0.00	0.13	0.00
48.00	198.34	2.00	0.00	0.13	0.00	48.10	187.38	2.00	0.00	0.13	0.00
48.20	170.86	2.00	0.00	0.12	0.00	48.30	163.29	2.00	0.00	0.12	0.00
48.40	160.03	2.00	0.00	0.12	0.00	48.50	191.52	2.00	0.00	0.12	0.00
48.60	229.52	2.00	0.00	0.12	0.00	48.70	265.84	2.00	0.00	0.11	0.00
48.80	132.29	2.00	0.00	0.11	0.00	48.90	213.06	2.00	0.00	0.11	0.00
49.00	114.60	2.00	0.00	0.11	0.00	49.10	111.28	2.00	0.00	0.11	0.00
49.20	117.57	2.00	0.00	0.11	0.00	49.30	129.73	2.00	0.00	0.10	0.00
49.40	142.05	2.00	0.00	0.10	0.00	49.50	151.72	2.00	0.00	0.10	0.00
49.60	163.26	2.00	0.00	0.10	0.00	49.70	178.64	2.00	0.00	0.10	0.00
49.80	191.98	2.00	0.00	0.09	0.00	49.90	198.32	2.00	0.00	0.09	0.00

Total estimated settlement: 0.78**Abbreviations**

$Q_{tn,cs}$:	Equivalent clean sand normalized cone resistance
FS:	Factor of safety against liquefaction
e_v (%):	Post-liquefaction volumetric strain
DF:	e_v depth weighting factor
Settlement:	Calculated settlement

:: Strength loss calculation (Robertson (2009)) ::

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.10	35.03	66.19	2.36	156.19	2.40	0.84	0.84
0.20	35.16	66.44	2.40	159.73	2.41	0.84	0.84
0.30	34.73	65.62	2.50	164.28	2.42	0.85	0.85
0.40	33.65	63.56	2.61	165.68	2.44	0.85	0.85
0.50	32.47	61.31	2.62	160.84	2.44	0.84	0.84
0.60	31.69	59.84	2.53	151.50	2.43	0.83	0.83
0.70	31.23	58.94	2.42	142.68	2.41	0.82	0.82
0.80	31.07	58.64	2.35	137.66	2.39	0.81	0.81
0.90	31.07	58.63	2.32	135.92	2.39	0.81	0.81
1.00	30.99	58.46	2.31	135.02	2.39	0.81	0.81
1.10	30.22	57.00	2.33	132.82	2.39	0.80	0.80
1.20	28.62	53.96	2.40	129.71	2.41	0.80	0.80
1.30	25.29	47.65	2.65	126.49	2.45	0.79	0.79
1.40	21.46	40.40	3.15	127.07	2.52	0.80	0.80
1.50	19.76	37.17	3.72	138.20	2.60	0.88	0.88
1.60	17.77	33.40	4.45	148.53	2.67	0.97	0.97
1.70	17.28	32.47	4.98	161.78	2.73	0.84	0.84
1.80	17.01	31.95	5.42	173.34	2.76	0.86	0.86
1.90	17.94	33.69	5.24	176.60	2.75	0.86	0.86
2.00	18.20	34.19	4.93	168.40	2.72	0.85	0.85
2.10	17.74	33.31	4.50	149.97	2.68	0.98	0.98
2.20	17.81	33.41	4.16	139.04	2.65	0.93	0.93
2.30	17.30	32.44	4.23	137.06	2.65	0.93	0.93
2.40	15.15	28.37	4.90	138.92	2.72	0.81	0.81
2.50	12.68	23.68	5.90	139.78	2.80	0.81	0.81
2.60	10.83	20.18	6.83	137.90	2.87	0.81	0.81
2.70	10.19	18.96	7.24	137.27	2.90	0.81	0.81
2.80	10.31	19.18	7.17	137.46	2.90	0.81	0.81
2.90	11.42	21.26	6.56	139.51	2.85	0.81	0.81
3.00	13.17	24.56	5.69	139.87	2.79	0.81	0.81
3.10	14.98	27.98	4.98	139.23	2.73	0.81	0.81
3.20	15.49	28.93	4.75	137.31	2.70	0.81	0.81
3.30	14.62	27.28	4.99	136.17	2.73	0.81	0.81
3.40	13.98	26.06	5.29	137.84	2.75	0.81	0.81
3.50	15.01	27.99	4.99	139.69	2.73	0.81	0.81
3.60	17.48	32.64	4.22	137.86	2.65	0.93	0.93
3.70	20.02	37.43	3.55	132.82	2.58	0.86	0.86
3.80	20.81	38.92	3.35	130.32	2.55	0.83	0.83
3.90	19.38	36.20	3.67	132.70	2.59	0.87	0.87
4.00	16.73	31.19	4.50	140.21	2.68	0.96	0.96
4.10	14.89	27.70	5.34	147.79	2.76	0.82	0.82
4.20	15.11	28.11	5.37	150.90	2.76	0.83	0.83
4.30	17.12	31.89	4.58	146.16	2.69	0.98	0.98
4.40	20.17	37.64	3.60	135.32	2.58	0.87	0.87
4.50	23.37	43.68	2.85	124.44	2.48	0.79	0.79
4.60	26.36	49.32	2.38	117.41	2.40	0.78	0.78
4.70	28.28	52.95	2.13	112.80	2.35	0.77	0.77
4.80	28.50	53.35	2.04	109.09	2.33	0.76	0.76

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
4.90	26.77	50.07	2.15	107.83	2.36	0.76	0.76
5.00	23.34	43.58	2.54	110.85	2.43	0.77	0.77
5.10	18.70	34.79	3.34	116.24	2.55	0.81	0.81
5.20	14.38	26.62	4.53	120.63	2.68	0.93	0.93
5.30	11.34	20.85	5.82	121.41	2.80	0.79	0.79
5.40	9.53	17.43	6.89	120.05	2.88	0.78	0.78
5.50	8.69	15.83	7.62	120.59	2.93	0.78	0.78
5.60	10.46	19.16	6.98	133.71	2.88	0.80	0.80
5.70	12.39	22.80	6.32	144.16	2.84	0.82	0.82
5.80	13.72	25.30	5.91	149.41	2.80	0.83	0.83
5.90	11.35	20.82	6.68	139.04	2.86	0.81	0.81
6.00	9.16	16.66	7.53	125.43	2.92	0.79	0.79
6.10	7.81	14.11	7.89	111.36	2.95	0.77	0.77
6.20	9.31	16.93	6.22	105.22	2.83	0.76	0.76
6.30	13.02	23.93	4.14	98.95	2.64	0.85	0.85
6.40	17.23	31.87	2.82	89.84	2.48	0.73	0.73
6.50	19.97	37.05	2.16	80.05	2.36	0.59	0.71
6.60	21.02	39.02	1.99	77.54	2.32	0.48	0.70
6.70	21.55	40.00	2.08	83.30	2.34	0.71	0.71
6.80	24.54	45.65	2.10	95.64	2.34	0.74	0.74
6.90	28.95	53.97	1.98	107.12	2.32	0.76	0.76
7.00	33.02	61.66	1.90	117.36	2.29	0.78	0.78
7.10	34.38	64.23	1.96	125.84	2.31	0.79	0.79
7.20	33.32	62.20	2.09	129.71	2.34	0.80	0.80
7.30	30.96	57.74	2.25	129.63	2.37	0.80	0.80
7.40	27.34	50.89	2.56	130.17	2.43	0.80	0.80
7.50	23.15	42.95	3.17	136.23	2.53	0.82	0.82
7.60	18.85	34.80	4.22	146.94	2.65	0.95	0.95
7.70	15.01	27.54	5.61	154.44	2.78	0.83	0.83
7.80	12.30	22.42	6.98	156.54	2.88	0.84	0.84
7.90	11.37	20.64	7.52	155.17	2.92	0.83	0.83
8.00	12.13	22.07	6.88	151.91	2.88	0.83	0.83
8.10	13.66	24.94	5.82	145.18	2.80	0.82	0.82
8.20	15.81	29.00	4.66	134.99	2.70	0.97	0.97
8.30	18.07	33.25	3.65	121.36	2.59	0.85	0.85
8.40	19.89	36.12	3.00	108.28	2.50	0.75	0.75
8.50	20.92	37.25	2.65	98.76	2.45	0.75	0.75
8.60	21.23	37.28	2.46	91.72	2.42	0.73	0.73
8.70	21.47	37.31	2.34	87.43	2.39	0.72	0.72
8.80	21.51	37.14	2.31	85.73	2.39	0.72	0.72
8.90	21.51	37.18	2.40	89.20	2.40	0.73	0.73
9.00	20.90	36.46	2.66	97.11	2.45	0.74	0.74
9.10	19.70	34.77	3.06	106.28	2.51	0.76	0.76
9.20	19.12	33.99	3.37	114.62	2.55	0.81	0.81
9.30	19.54	34.68	3.43	119.05	2.56	0.82	0.82
9.40	20.38	35.97	3.38	121.40	2.55	0.82	0.82
9.50	19.23	34.07	3.66	124.82	2.59	0.86	0.86
9.60	16.01	28.79	4.47	128.58	2.68	0.94	0.94

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.70	13.82	25.09	5.45	136.76	2.77	0.81	0.81
9.80	15.64	28.37	5.20	147.38	2.74	0.82	0.82
9.90	16.35	29.41	5.00	147.04	2.73	0.82	0.82
10.00	13.35	24.09	5.67	136.49	2.78	0.81	0.81
10.10	8.41	14.82	7.91	117.16	2.95	0.78	0.78
10.20	7.41	12.92	8.72	112.59	3.00	0.77	0.77
10.30	10.53	18.81	6.47	121.71	2.85	0.79	0.79
10.40	13.79	24.22	5.21	126.27	2.75	0.79	0.79
10.50	16.27	28.24	4.65	131.40	2.69	0.96	0.96
10.60	16.77	29.07	4.74	137.94	2.70	0.81	0.81
10.70	14.80	25.89	5.53	143.09	2.77	0.82	0.82
10.80	11.32	20.07	7.10	142.45	2.89	0.82	0.82
10.90	7.88	13.73	9.59	131.66	3.05	0.74	0.98
11.00	5.67	9.54	12.11	115.56	3.17	0.51	0.68
11.10	4.53	7.34	13.68	100.33	3.24	0.34	0.52
11.20	4.05	6.41	14.02	89.78	3.25	0.27	0.46
11.30	3.98	6.25	13.62	85.17	3.24	0.24	0.45
11.40	3.98	6.22	13.38	83.25	3.23	0.24	0.44
11.50	3.98	6.19	13.40	82.98	3.23	0.23	0.44
11.60	3.98	6.16	13.63	83.97	3.24	0.24	0.44
11.70	3.98	6.13	14.01	85.91	3.25	0.26	0.44
11.80	3.92	5.99	14.62	87.52	3.28	0.27	0.43
11.90	3.81	5.75	15.27	87.81	3.30	0.27	0.41
12.00	4.07	6.21	14.54	90.30	3.28	0.26	0.44
12.10	4.67	7.26	12.96	94.05	3.21	0.34	0.52
12.20	5.31	8.39	11.56	96.95	3.15	0.38	0.60
12.30	5.58	8.83	10.99	97.04	3.12	0.36	0.63
12.40	5.58	8.79	10.93	96.01	3.12	0.35	0.63
12.50	5.58	8.74	10.97	95.92	3.12	0.35	0.62
12.60	5.58	8.70	11.13	96.89	3.13	0.35	0.62
12.70	5.58	8.66	11.42	98.95	3.14	0.37	0.62
12.80	5.58	8.62	11.83	101.97	3.16	0.40	0.62
12.90	5.58	8.58	12.29	105.47	3.18	0.43	0.61
13.00	5.80	8.93	12.29	109.74	3.18	0.46	0.64
13.10	6.32	9.79	11.61	113.73	3.15	0.52	0.70
13.20	6.51	10.09	11.25	113.54	3.13	0.57	0.72
13.30	5.94	9.05	11.88	107.61	3.16	0.47	0.65
13.40	4.89	7.19	13.58	97.66	3.24	0.33	0.51
13.50	4.17	5.90	15.08	89.03	3.30	0.26	0.42
13.60	3.98	5.56	15.25	84.82	3.30	0.24	0.40
13.70	3.98	5.54	15.09	83.51	3.30	0.23	0.40
13.80	3.98	5.51	15.28	84.20	3.30	0.24	0.39
13.90	3.98	5.48	15.69	86.06	3.32	0.26	0.39
14.00	3.98	5.46	15.96	87.11	3.33	0.27	0.39
14.10	3.98	5.43	15.85	86.08	3.32	0.26	0.39
14.20	3.98	5.41	15.53	83.99	3.31	0.23	0.39
14.30	3.76	5.01	16.15	80.89	3.34	0.23	0.36
14.40	3.50	4.54	17.28	78.42	3.37	0.19	0.32

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
14.50	3.50	4.52	17.28	78.04	3.37	0.18	0.32
14.60	3.72	4.87	16.27	79.17	3.34	0.22	0.35
14.70	4.09	5.46	15.19	83.01	3.30	0.22	0.39
14.80	4.51	6.14	14.64	89.86	3.28	0.26	0.44
14.90	5.25	7.32	13.74	100.58	3.24	0.37	0.52
15.00	6.18	8.82	12.69	111.96	3.20	0.49	0.63
15.10	7.12	10.33	11.72	121.16	3.15	0.60	0.74
15.20	9.50	14.17	9.42	133.51	3.04	0.69	1.01
15.30	14.31	21.55	6.61	142.43	2.86	0.82	0.82
15.40	22.91	33.70	4.20	141.57	2.65	0.94	0.94
15.50	34.71	49.46	2.67	132.07	2.45	0.80	0.80
15.60	50.28	69.50	1.86	129.32	2.28	0.80	0.80
15.70	67.84	91.62	1.53	140.05	2.16	0.81	0.81
15.80	85.19	112.65	1.37	154.02	2.06	0.83	0.83
15.90	100.36	130.44	1.29	168.64	1.98	0.85	0.85
16.00	105.72	136.09	1.27	172.49	1.95	0.86	0.86
16.10	103.10	132.76	1.28	169.98	1.96	0.85	0.85
16.20	98.78	127.74	1.31	167.57	2.01	0.85	0.85
16.30	98.29	127.29	1.33	169.86	2.03	0.85	0.85
16.40	97.60	126.46	1.36	171.44	2.05	0.85	0.85
16.50	89.65	116.68	1.41	164.92	2.10	0.85	0.85
16.60	76.67	100.71	1.55	156.50	2.17	0.84	0.84
16.70	61.52	81.89	1.86	152.38	2.28	0.83	0.83
16.80	46.02	62.21	2.47	153.43	2.42	0.83	0.83
16.90	32.20	44.17	3.49	154.14	2.57	0.88	0.88
17.00	21.83	30.21	4.93	149.00	2.72	0.83	0.83
17.10	15.15	20.96	6.56	137.50	2.85	0.81	0.81
17.20	10.77	14.63	8.35	122.13	2.97	0.79	0.79
17.30	8.03	10.50	10.10	106.07	3.07	0.43	0.75
17.40	6.41	8.07	11.50	92.75	3.14	0.29	0.58
17.50	5.73	7.02	12.00	84.31	3.17	0.24	0.50
17.60	5.58	6.78	11.73	79.47	3.15	0.22	0.48
17.70	5.58	6.75	11.32	76.40	3.13	0.19	0.48
17.80	5.58	6.72	11.06	74.35	3.12	0.19	0.48
17.90	5.58	6.70	10.88	72.87	3.11	0.18	0.48
18.00	5.72	6.88	10.66	73.35	3.10	0.16	0.49
18.10	6.17	7.51	10.32	77.52	3.08	0.20	0.54
18.20	6.71	8.26	10.49	86.59	3.09	0.27	0.59
18.30	7.09	8.79	11.14	97.84	3.13	0.36	0.63
18.40	7.50	9.34	11.83	110.45	3.16	0.47	0.67
18.50	8.13	10.20	11.90	121.37	3.16	0.61	0.73
18.60	9.21	11.70	11.14	130.42	3.13	0.70	0.84
18.70	10.73	13.82	9.94	137.35	3.06	0.81	0.99
18.80	12.95	16.91	8.40	141.97	2.98	0.82	0.82
18.90	16.09	21.07	6.75	142.29	2.87	0.82	0.82
19.00	18.81	24.48	5.62	137.61	2.78	0.81	0.81
19.10	20.48	26.48	5.08	134.56	2.73	0.81	0.81
19.20	20.52	26.47	5.17	136.81	2.74	0.81	0.81

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
19.30	19.41	25.03	5.71	142.80	2.79	0.82	0.82
19.40	17.68	22.76	6.37	145.07	2.84	0.82	0.82
19.50	16.31	20.89	6.76	141.25	2.87	0.81	0.81
19.60	16.30	20.74	6.48	134.47	2.85	0.81	0.81
19.70	18.29	23.15	5.67	131.33	2.79	0.80	0.80
19.80	20.97	26.45	5.00	132.10	2.73	0.80	0.80
19.90	22.75	28.62	4.78	136.95	2.71	0.81	0.81
20.00	21.58	27.13	5.24	142.04	2.75	0.82	0.82
20.10	17.47	21.89	6.41	140.38	2.84	0.81	0.81
20.20	12.54	15.41	8.35	128.64	2.97	0.80	0.80
20.30	8.93	10.49	10.29	107.93	3.08	0.42	0.75
20.40	7.14	8.05	11.19	90.08	3.13	0.29	0.58
20.50	6.30	6.91	11.44	79.02	3.14	0.20	0.49
20.60	5.79	6.20	11.94	74.02	3.16	0.16	0.44
20.70	5.58	5.90	12.86	75.85	3.21	0.18	0.42
20.80	5.55	5.83	13.87	80.95	3.25	0.23	0.42
20.90	5.51	5.77	14.68	84.69	3.28	0.26	0.41
21.00	5.50	5.72	14.89	85.19	3.29	0.26	0.41
21.10	5.47	5.67	14.79	83.89	3.28	0.24	0.41
21.20	5.83	6.12	14.16	86.65	3.26	0.23	0.44
21.30	6.38	6.82	13.86	94.51	3.25	0.32	0.49
21.40	7.19	7.84	13.40	105.08	3.23	0.42	0.56
21.50	7.91	8.76	12.89	112.96	3.21	0.51	0.63
21.60	8.45	9.42	12.27	115.54	3.18	0.56	0.67
21.70	8.76	9.78	11.61	113.59	3.15	0.52	0.70
21.80	8.66	9.62	11.27	108.42	3.13	0.47	0.69
21.90	8.24	9.05	11.36	102.78	3.14	0.41	0.65
22.00	7.71	8.33	11.83	98.57	3.16	0.35	0.60
22.10	7.52	8.07	12.16	98.11	3.17	0.34	0.58
22.20	7.95	8.58	11.86	101.78	3.16	0.39	0.61
22.30	8.79	9.62	11.28	108.47	3.13	0.46	0.69
22.40	9.90	11.00	10.70	117.69	3.10	0.55	0.79
22.50	12.35	14.05	9.28	130.38	3.03	0.70	1.00
22.60	16.82	19.58	7.18	140.54	2.90	0.81	0.81
22.70	23.64	27.60	5.22	144.22	2.75	0.82	0.82
22.80	31.17	36.29	4.03	146.10	2.63	0.93	0.93
22.90	36.34	42.22	3.60	152.07	2.58	0.89	0.89
23.00	37.64	43.70	3.73	163.02	2.60	0.92	0.92
23.10	35.29	40.99	4.29	175.65	2.66	0.99	0.99
23.20	32.02	37.18	5.02	186.79	2.73	0.87	0.87
23.30	29.06	33.69	5.75	193.53	2.79	0.88	0.88
23.40	26.91	31.10	6.28	195.41	2.83	0.88	0.88
23.50	25.69	29.58	6.59	194.81	2.86	0.88	0.88
23.60	25.99	29.81	6.54	195.02	2.85	0.88	0.88
23.70	28.55	32.65	6.00	195.78	2.81	0.88	0.88
23.80	33.44	38.10	5.09	194.00	2.74	0.88	0.88
23.90	39.82	45.14	4.16	187.57	2.64	1.00	1.00
24.00	46.53	52.41	3.40	177.95	2.56	0.90	0.90

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
24.10	54.51	60.94	2.73	166.42	2.46	0.85	0.85
24.20	65.10	72.15	2.14	154.76	2.35	0.83	0.83
24.30	79.01	86.81	1.73	150.17	2.24	0.83	0.83
24.40	93.89	102.42	1.52	155.95	2.16	0.83	0.83
24.50	106.54	115.72	1.45	167.93	2.12	0.85	0.85
24.60	115.17	124.79	1.44	179.54	2.11	0.86	0.86
24.70	120.39	130.21	1.45	188.31	2.12	0.87	0.87
24.80	116.41	125.70	1.48	186.07	2.14	0.87	0.87
24.90	104.61	112.80	1.55	174.94	2.17	0.86	0.86
25.00	92.13	99.19	1.65	163.53	2.21	0.84	0.84
25.10	88.30	94.90	1.71	162.47	2.24	0.84	0.84
25.20	92.70	99.44	1.72	171.07	2.24	0.85	0.85
25.30	95.86	102.67	1.75	179.84	2.25	0.86	0.86
25.40	93.78	100.31	1.85	185.09	2.28	0.87	0.87
25.50	85.40	91.26	2.04	185.93	2.33	0.87	0.87
25.60	72.79	77.70	2.37	184.22	2.40	0.87	0.87
25.70	58.75	62.59	2.91	181.87	2.49	0.87	0.87
25.80	45.10	47.88	3.77	180.31	2.60	0.95	0.95
25.90	32.80	34.58	5.12	177.19	2.74	0.86	0.86
26.00	22.82	23.72	7.10	168.46	2.89	0.85	0.85
26.10	15.86	15.95	9.57	152.57	3.04	0.99	1.14
26.20	12.59	12.29	11.26	138.34	3.13	0.73	0.88
26.30	11.74	11.30	11.54	130.48	3.15	0.69	0.81
26.40	11.90	11.45	11.21	128.32	3.13	0.68	0.82
26.50	12.02	11.53	11.11	128.19	3.12	0.67	0.82
26.60	12.19	11.68	11.13	130.07	3.13	0.69	0.83
26.70	12.99	12.51	10.72	134.19	3.11	0.75	0.89
26.80	14.07	13.65	10.12	138.10	3.07	0.84	0.97
26.90	15.03	14.64	9.63	141.00	3.05	0.88	1.05
27.00	15.05	14.62	9.68	141.53	3.05	0.90	1.04
27.10	14.04	13.48	10.31	138.95	3.08	0.86	0.96
27.20	11.95	11.20	11.70	130.94	3.15	0.73	0.80
27.30	10.07	9.14	13.21	120.75	3.22	0.53	0.65
27.40	9.47	8.47	13.49	114.25	3.23	0.47	0.60
27.50	9.83	8.83	12.83	113.31	3.20	0.52	0.63
27.60	10.36	9.36	12.19	114.18	3.18	0.52	0.67
27.70	10.36	9.33	12.14	113.35	3.17	0.51	0.67
27.80	10.36	9.30	12.17	113.23	3.17	0.50	0.66
27.90	10.36	9.28	12.24	113.51	3.18	0.51	0.66
28.00	10.36	9.25	12.38	114.54	3.18	0.52	0.66
28.10	10.94	9.82	12.02	118.10	3.17	0.52	0.70
28.20	14.59	13.61	9.63	131.07	3.05	0.63	0.97
28.30	22.51	21.80	6.71	146.37	2.87	0.82	0.82
28.40	32.54	32.00	4.98	159.28	2.73	0.84	0.84
28.50	38.83	38.31	4.43	169.83	2.67	1.00	1.00
28.60	38.69	38.08	4.69	178.69	2.70	1.04	1.04
28.70	34.55	33.80	5.48	185.09	2.77	0.87	0.87
28.80	30.65	29.76	6.24	185.71	2.83	0.87	0.87

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
28.90	30.40	29.40	6.15	180.95	2.82	0.87	0.87
29.00	35.55	34.46	4.92	169.60	2.72	0.85	0.85
29.10	47.27	45.99	3.27	150.23	2.54	0.85	0.85
29.20	63.97	62.34	2.18	135.74	2.36	0.81	0.81
29.30	82.47	80.36	1.70	136.78	2.23	0.81	0.81
29.40	101.51	98.87	1.52	150.70	2.16	0.83	0.83
29.50	120.40	117.15	1.44	168.35	2.11	0.85	0.85
29.60	138.78	134.84	1.39	186.85	2.08	0.87	0.87
29.70	151.39	146.84	1.36	200.29	2.06	0.89	0.89
29.80	149.49	144.67	1.38	199.31	2.07	0.89	0.89
29.90	134.76	130.04	1.44	187.01	2.11	0.87	0.87
30.00	124.88	120.19	1.52	183.25	2.16	0.87	0.87
30.10	126.66	121.66	1.57	191.06	2.18	0.88	0.88
30.20	133.00	127.49	1.55	198.22	2.17	0.88	0.88
30.30	130.73	124.96	1.54	191.86	2.17	0.88	0.88
30.40	122.90	117.07	1.52	177.76	2.16	0.86	0.86
30.50	115.21	109.38	1.51	165.69	2.16	0.85	0.85
30.60	106.62	100.89	1.58	159.60	2.19	0.84	0.84
30.70	95.19	89.73	1.79	160.35	2.26	0.84	0.84
30.80	81.78	76.72	2.16	165.73	2.36	0.85	0.85
30.90	68.85	64.18	2.64	169.28	2.45	0.85	0.85
31.00	59.25	54.87	3.06	168.18	2.51	0.85	0.85
31.10	54.12	49.84	3.29	164.08	2.54	0.87	0.87
31.20	52.83	48.48	3.30	159.96	2.54	0.87	0.87
31.30	53.99	49.46	3.24	160.45	2.54	0.86	0.86
31.40	56.15	51.36	3.28	168.66	2.54	0.88	0.88
31.50	62.49	57.19	3.19	182.27	2.53	0.88	0.88
31.60	78.37	71.97	2.66	191.72	2.45	0.88	0.88
31.70	106.07	97.78	2.01	196.67	2.32	0.88	0.88
31.80	135.90	125.49	1.65	206.96	2.21	0.89	0.89
31.90	156.45	144.41	1.52	218.92	2.16	0.91	0.91
32.00	161.73	148.97	1.51	225.02	2.15	0.91	0.91
32.10	152.47	139.95	1.60	223.85	2.19	0.91	0.91
32.20	133.57	122.00	1.81	220.31	2.27	0.91	0.91
32.30	109.16	99.04	2.17	215.22	2.36	0.90	0.90
32.40	86.47	77.81	2.66	206.72	2.45	0.89	0.89
32.50	67.96	60.56	3.17	192.08	2.53	0.89	0.89
32.60	54.22	47.80	3.69	176.53	2.59	0.93	0.93
32.70	44.06	38.38	4.29	164.82	2.66	0.98	0.98
32.80	36.99	31.83	4.92	156.67	2.72	0.84	0.84
32.90	33.29	28.38	5.31	150.72	2.75	0.83	0.83
33.00	32.53	27.62	5.34	147.55	2.76	0.82	0.82
33.10	33.38	28.32	5.20	147.34	2.75	0.82	0.82
33.20	34.55	29.30	5.02	147.24	2.73	0.82	0.82
33.30	35.86	30.41	4.77	145.11	2.71	0.82	0.82
33.40	37.95	32.22	4.39	141.56	2.67	0.95	0.95
33.50	40.53	34.46	4.07	140.30	2.64	0.92	0.92
33.60	42.96	36.56	3.90	142.53	2.62	0.91	0.91

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
33.70	44.99	38.28	3.84	147.15	2.61	0.91	0.91
33.80	46.37	39.39	3.91	153.98	2.62	0.93	0.93
33.90	46.18	39.09	4.14	161.77	2.64	0.96	0.96
34.00	43.62	36.68	4.64	170.22	2.69	1.02	1.02
34.10	39.11	32.55	5.41	176.17	2.76	0.86	0.86
34.20	34.19	28.10	6.28	176.54	2.83	0.86	0.86
34.30	31.45	25.62	6.63	169.90	2.86	0.85	0.85
34.40	33.42	27.32	5.70	155.78	2.79	0.83	0.83
34.50	41.97	34.87	3.83	133.69	2.61	0.89	0.89
34.60	54.67	46.11	2.59	119.37	2.44	0.78	0.78
34.70	63.98	54.25	2.27	122.97	2.38	0.79	0.79
34.80	63.78	53.84	2.55	137.27	2.43	0.81	0.81
34.90	54.43	45.37	3.39	153.88	2.56	0.87	0.87
35.00	42.54	34.80	4.68	162.86	2.70	1.01	1.01
35.10	33.70	27.01	6.05	163.48	2.82	0.84	0.84
35.20	29.21	23.06	6.93	159.94	2.88	0.84	0.84
35.30	28.14	22.10	7.22	159.50	2.90	0.84	0.84
35.40	28.25	22.13	7.32	162.04	2.91	0.84	0.84
35.50	28.92	22.63	7.23	163.54	2.90	0.84	0.84
35.60	31.20	24.50	6.54	160.16	2.85	0.84	0.84
35.70	35.84	28.45	5.37	152.87	2.76	0.83	0.83
35.80	41.61	33.35	4.48	149.43	2.68	0.97	0.97
35.90	46.85	37.75	4.10	154.66	2.64	0.95	0.95
36.00	48.90	39.35	4.25	167.23	2.65	0.98	0.98
36.10	46.83	37.40	4.84	180.94	2.71	0.87	0.87
36.20	40.81	32.14	5.88	189.00	2.80	0.87	0.87
36.30	34.31	26.58	7.09	188.59	2.89	0.87	0.87
36.40	30.73	23.56	7.68	180.83	2.93	0.87	0.87
36.50	32.04	24.57	6.93	170.18	2.88	0.85	0.85
36.60	37.92	29.50	5.32	156.90	2.76	0.84	0.84
36.70	47.30	37.46	3.77	141.07	2.60	0.89	0.89
36.80	57.90	46.49	2.74	127.19	2.46	0.79	0.79
36.90	67.57	54.71	2.24	122.48	2.37	0.79	0.79
37.00	73.31	59.46	2.14	127.09	2.35	0.79	0.79
37.10	73.91	59.72	2.29	136.52	2.38	0.81	0.81
37.20	70.47	56.54	2.60	146.83	2.44	0.82	0.82
37.30	66.08	52.61	2.93	153.93	2.49	0.83	0.83
37.40	64.16	50.85	3.05	155.23	2.51	0.83	0.83
37.50	66.79	53.00	2.82	149.45	2.48	0.83	0.83
37.60	74.80	59.77	2.31	138.09	2.39	0.81	0.81
37.70	86.08	69.42	1.84	127.65	2.28	0.79	0.79
37.80	97.88	79.53	1.56	123.99	2.18	0.79	0.79
37.90	107.58	87.78	1.44	126.65	2.12	0.79	0.79
38.00	112.98	92.22	1.42	130.53	2.10	0.80	0.80
38.10	113.65	92.51	1.44	132.78	2.11	0.80	0.80
38.20	110.48	89.55	1.48	132.53	2.14	0.80	0.80
38.30	105.06	84.69	1.55	131.22	2.17	0.80	0.80
38.40	97.28	77.83	1.69	131.23	2.23	0.80	0.80

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
38.50	86.60	68.49	1.99	136.26	2.32	0.81	0.81
38.60	73.98	57.63	2.55	146.85	2.43	0.82	0.82
38.70	62.00	47.51	3.28	155.65	2.54	0.86	0.86
38.80	53.61	40.54	3.81	154.50	2.61	0.92	0.92
38.90	50.18	37.75	3.80	143.62	2.61	0.90	0.90
39.00	50.79	38.28	3.43	131.47	2.56	0.84	0.84
39.10	53.01	40.08	3.09	123.72	2.52	0.79	0.79
39.20	54.99	41.65	2.89	120.48	2.49	0.78	0.78
39.30	56.78	43.04	2.76	118.64	2.47	0.78	0.78
39.40	58.86	44.69	2.59	115.94	2.44	0.78	0.78
39.50	61.74	47.02	2.38	111.83	2.40	0.77	0.77
39.60	65.69	50.25	2.13	107.16	2.35	0.76	0.76
39.70	69.92	53.57	2.06	110.39	2.33	0.77	0.77
39.80	70.73	53.83	2.34	125.93	2.39	0.79	0.79
39.90	68.52	51.62	2.81	145.04	2.47	0.82	0.82
40.00	66.77	49.92	3.16	157.96	2.53	0.85	0.85
40.10	68.40	51.03	3.24	165.16	2.54	0.87	0.87
40.20	69.02	51.27	3.44	176.44	2.56	0.90	0.90
40.30	64.29	47.22	4.03	190.11	2.63	0.99	0.99
40.40	55.60	40.21	4.82	193.81	2.71	0.88	0.88
40.50	48.54	34.67	5.29	183.22	2.75	0.87	0.87
40.60	48.02	34.33	4.78	164.01	2.71	0.85	0.85
40.70	56.01	40.74	3.54	144.39	2.58	0.87	0.87
40.80	69.22	51.33	2.58	132.29	2.44	0.80	0.80
40.90	81.20	60.92	2.11	128.74	2.35	0.80	0.80
41.00	88.70	66.86	1.93	129.21	2.30	0.80	0.80
41.10	92.25	69.57	1.88	130.80	2.29	0.80	0.80
41.20	95.34	71.89	1.85	132.67	2.28	0.80	0.80
41.30	97.82	73.70	1.83	134.68	2.27	0.81	0.81
41.40	99.69	75.00	1.82	136.86	2.27	0.81	0.81
41.50	106.32	80.05	1.78	142.79	2.26	0.82	0.82
41.60	117.58	88.73	1.72	152.96	2.24	0.83	0.83
41.70	127.07	95.89	1.71	164.07	2.24	0.85	0.85
41.80	127.05	95.37	1.81	172.61	2.27	0.86	0.86
41.90	116.84	86.76	2.07	179.16	2.34	0.86	0.86
42.00	104.74	76.78	2.45	188.10	2.41	0.87	0.87
42.10	92.11	66.64	2.89	192.82	2.49	0.88	0.88
42.20	81.70	58.50	3.20	187.14	2.53	0.89	0.89
42.30	77.65	55.50	3.06	169.59	2.51	0.85	0.85
42.40	84.52	61.14	2.40	146.57	2.40	0.82	0.82
42.50	102.73	75.81	1.76	133.70	2.25	0.80	0.80
42.60	127.10	95.47	1.45	138.14	2.12	0.81	0.81
42.70	150.48	114.23	1.34	153.07	2.04	0.83	0.83
42.80	168.38	128.30	1.31	167.96	2.00	0.85	0.85
42.90	178.54	135.96	1.31	177.73	2.00	0.86	0.86
43.00	182.69	138.77	1.32	182.50	2.01	0.87	0.87
43.10	182.27	138.04	1.32	182.89	2.02	0.87	0.87
43.20	179.32	135.43	1.33	180.31	2.03	0.86	0.86

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
43.30	176.00	132.65	1.33	176.56	2.03	0.86	0.86
43.40	173.94	130.94	1.33	173.54	2.02	0.86	0.86
43.50	174.12	130.97	1.32	172.68	2.01	0.86	0.86
43.60	176.71	132.84	1.31	174.28	2.01	0.86	0.86
43.70	181.49	136.36	1.31	178.11	2.00	0.86	0.86
43.80	187.71	140.96	1.30	183.48	1.99	0.87	0.87
43.90	193.96	145.49	1.30	189.21	1.99	0.88	0.88
44.00	199.20	149.21	1.30	194.05	1.99	0.88	0.88
44.10	202.32	151.36	1.30	196.61	1.99	0.88	0.88
44.20	203.65	152.24	1.29	196.91	1.98	0.88	0.88
44.30	204.80	153.02	1.29	196.89	1.97	0.88	0.88
44.40	206.99	154.52	1.28	198.22	1.97	0.88	0.88
44.50	210.41	156.81	1.28	201.32	1.97	0.89	0.89
44.60	214.13	159.31	1.29	204.72	1.97	0.89	0.89
44.70	217.64	161.74	1.28	207.51	1.97	0.89	0.89
44.80	221.58	164.66	1.28	209.99	1.96	0.90	0.90
44.90	227.00	168.85	1.26	213.26	1.94	0.90	0.90
45.00	234.02	174.31	1.25	217.83	1.92	0.91	0.91
45.10	239.15	178.21	1.24	221.09	1.91	0.91	0.91
45.20	237.85	176.94	1.24	219.53	1.91	0.91	0.91
45.30	229.01	169.74	1.25	211.91	1.92	0.90	0.90
45.40	215.37	158.89	1.26	200.16	1.93	0.89	0.89
45.50	202.11	148.45	1.27	188.42	1.95	0.87	0.87
45.60	193.91	142.10	1.27	180.45	1.95	0.87	0.87
45.70	193.08	141.60	1.26	178.17	1.93	0.86	0.86
45.80	200.77	147.76	1.24	182.74	1.90	0.87	0.87
45.90	215.19	159.08	1.21	192.70	1.86	0.88	0.88
46.00	233.39	173.14	1.19	205.69	1.84	0.89	0.89
46.10	252.76	187.87	1.17	219.97	1.82	0.91	0.91
46.20	270.53	201.28	1.16	233.02	1.80	0.92	0.92
46.30	285.82	212.86	1.14	243.21	1.79	0.93	0.93
46.40	297.04	221.49	1.12	248.44	1.77	0.93	0.93
46.50	304.64	227.35	1.10	250.22	1.76	0.94	0.94
46.60	309.75	231.05	1.09	252.23	1.75	0.94	0.94
46.70	312.52	232.63	1.10	255.70	1.76	0.94	0.94
46.80	312.12	231.67	1.11	257.78	1.77	0.94	0.94
46.90	308.33	228.10	1.13	257.39	1.78	0.94	0.94
47.00	301.93	222.50	1.15	255.10	1.79	0.94	0.94
47.10	294.03	215.62	1.17	252.16	1.82	0.94	0.94
47.20	284.88	207.74	1.19	247.76	1.84	0.93	0.93
47.30	275.33	199.71	1.21	241.83	1.86	0.93	0.93
47.40	266.20	192.33	1.22	234.75	1.88	0.92	0.92
47.50	258.33	186.32	1.22	227.31	1.88	0.91	0.91
47.60	252.03	181.90	1.21	219.72	1.86	0.91	0.91
47.70	247.62	179.26	1.18	211.94	1.83	0.90	0.90
47.80	245.33	178.34	1.14	204.06	1.79	0.89	0.89
47.90	241.79	175.75	1.13	199.14	1.78	0.89	0.89
48.00	231.80	166.75	1.19	198.34	1.84	0.89	0.89

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
48.10	209.20	147.31	1.27	187.38	1.95	0.87	0.87
48.20	174.47	119.30	1.43	170.86	2.11	0.85	0.85
48.30	133.42	88.12	1.85	163.29	2.28	0.84	0.84
48.40	94.91	60.35	2.65	160.03	2.45	0.84	0.84
48.50	71.47	44.05	3.47	152.95	2.57	0.88	0.88
48.60	60.38	36.51	3.96	144.56	2.62	0.92	0.92
48.70	52.78	31.38	4.41	138.25	2.67	0.95	0.95
48.80	47.63	27.94	4.74	132.29	2.70	0.80	0.80
48.90	49.25	29.16	4.18	121.84	2.65	0.90	0.90
49.00	65.35	40.31	2.84	114.60	2.48	0.77	0.77
49.10	87.91	56.32	1.98	111.28	2.31	0.77	0.77
49.20	112.10	73.73	1.59	117.57	2.19	0.78	0.78
49.30	133.65	89.17	1.45	129.73	2.12	0.80	0.80
49.40	151.11	101.56	1.40	142.05	2.09	0.82	0.82
49.50	166.58	112.85	1.34	151.72	2.04	0.83	0.83
49.60	185.29	127.04	1.29	163.26	1.97	0.84	0.84
49.70	208.76	145.19	1.23	178.64	1.89	0.86	0.86
49.80	231.42	162.73	1.18	191.98	1.83	0.88	0.88
49.90	245.61	173.66	1.14	198.32	1.79	0.89	0.89

Abbreviations

q_t :	Total cone resistance
K_c :	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c :	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

LIQUEFACTION ANALYSIS REPORT

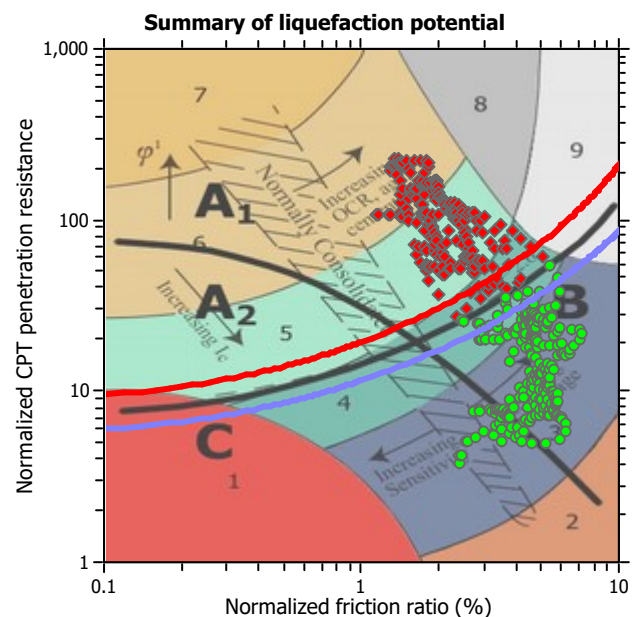
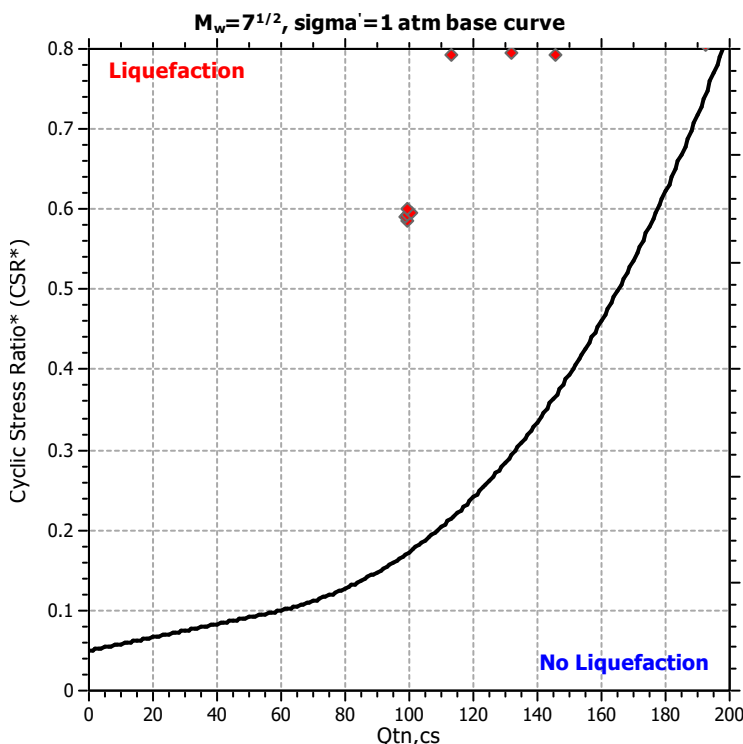
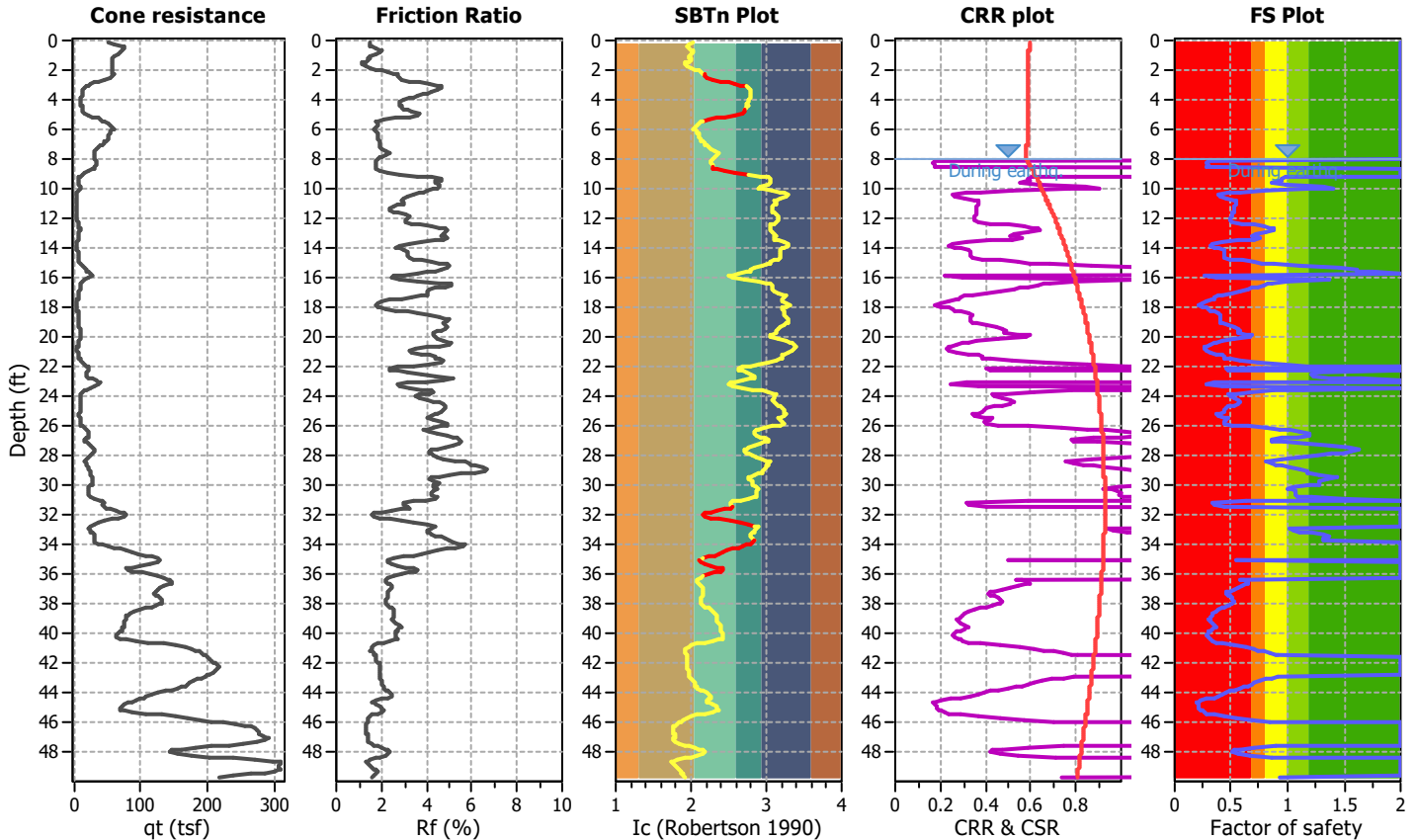
Project title : 21-483 Equestrian Estates

Location : Avenue 64 at Harrison Street, Thermal California

CPT file : CPT-6 Robt 2009

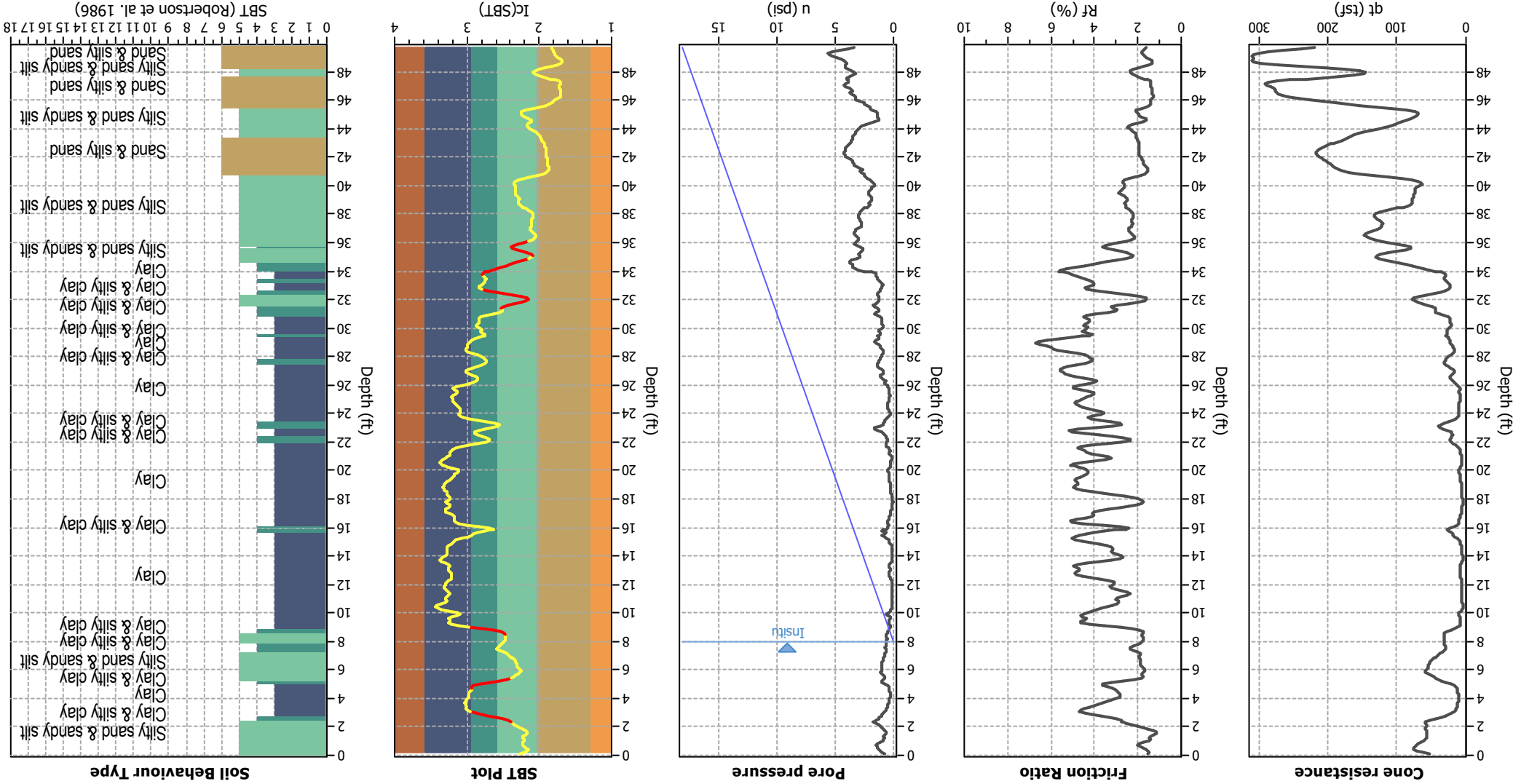
Input parameters and analysis data

Analysis method:	Robertson (2009)	G.W.T. (in-situ):	8.00 ft	Use fill:	No	Clay like behavior	
Fines correction method:	Robertson (2009)	G.W.T. (earthq.):	8.00 ft	Fill height:	N/A	applied:	All soils
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude M_w :	7.34	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.74	Unit weight calculation:	Based on SBT	K_o applied:	No	MSF method:	Method based



Zone A₁: Cyclic liquefaction likely depending on size and duration of cyclic loading
 Zone A₂: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
 Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
 Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots

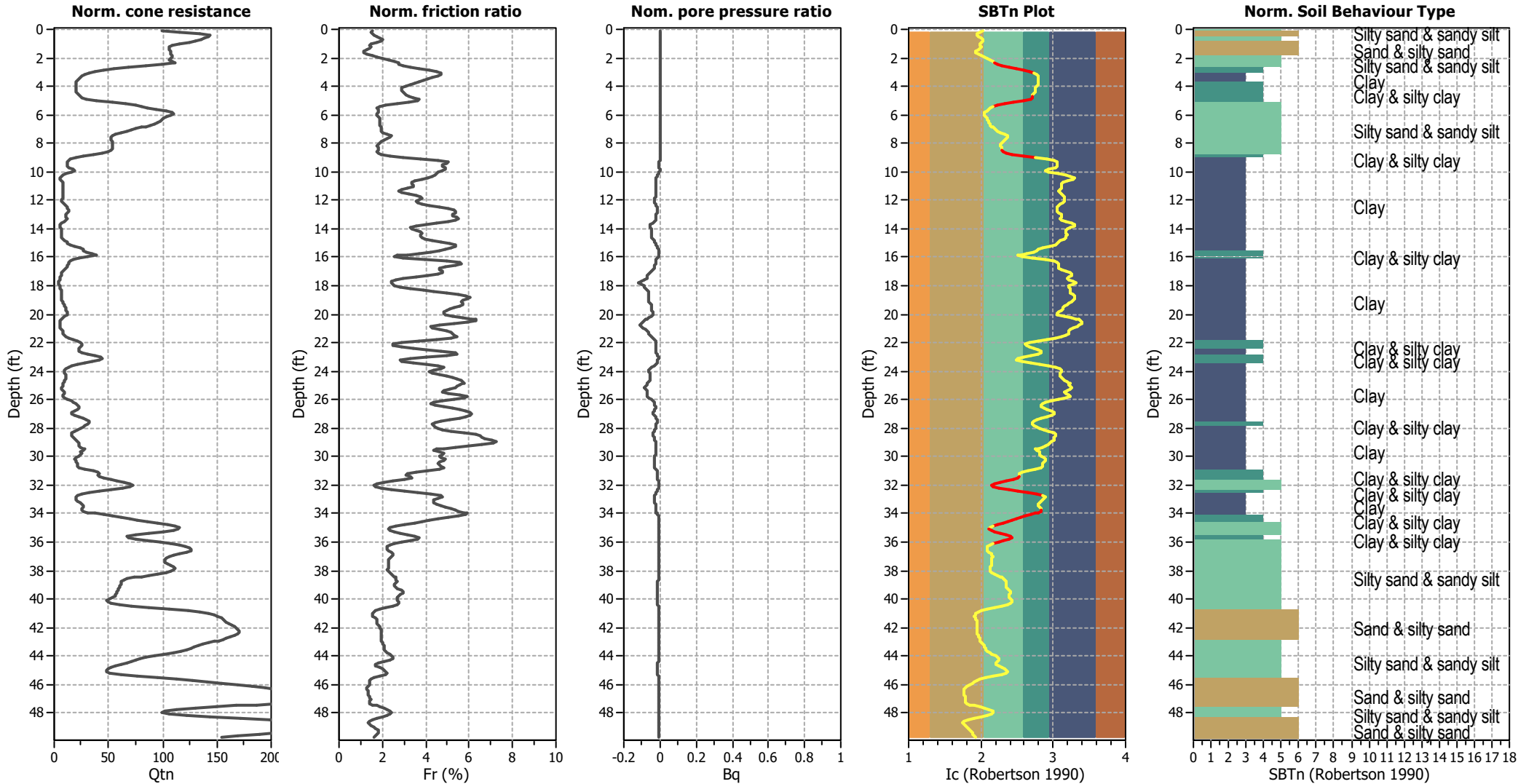


Input parameters and analysis data

Analysis method:	Robertson (2009)	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Transition detect. applied:	Yes
Points to test:	Based on Ic value	K _g applied:	No
Earthquake magnitude M _w :	7.34	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Limit depth:	N/A
Depth to water table (earthq.):	8.00 ft	Unit weight calculation:	Based on SBT
		Use fill:	No
		Fill height:	N/A

SBT legend	
1. Sensitive fine grained	2. Organic material
3. Clay to silty clay	4. Clayey silt to silty
5. Silty sand to sandy silt	6. Clean sand to silty sand
7. Gravely sand to sand	8. Very stiff sand to
9. Very stiff fine grained	

CPT basic interpretation plots (normalized)



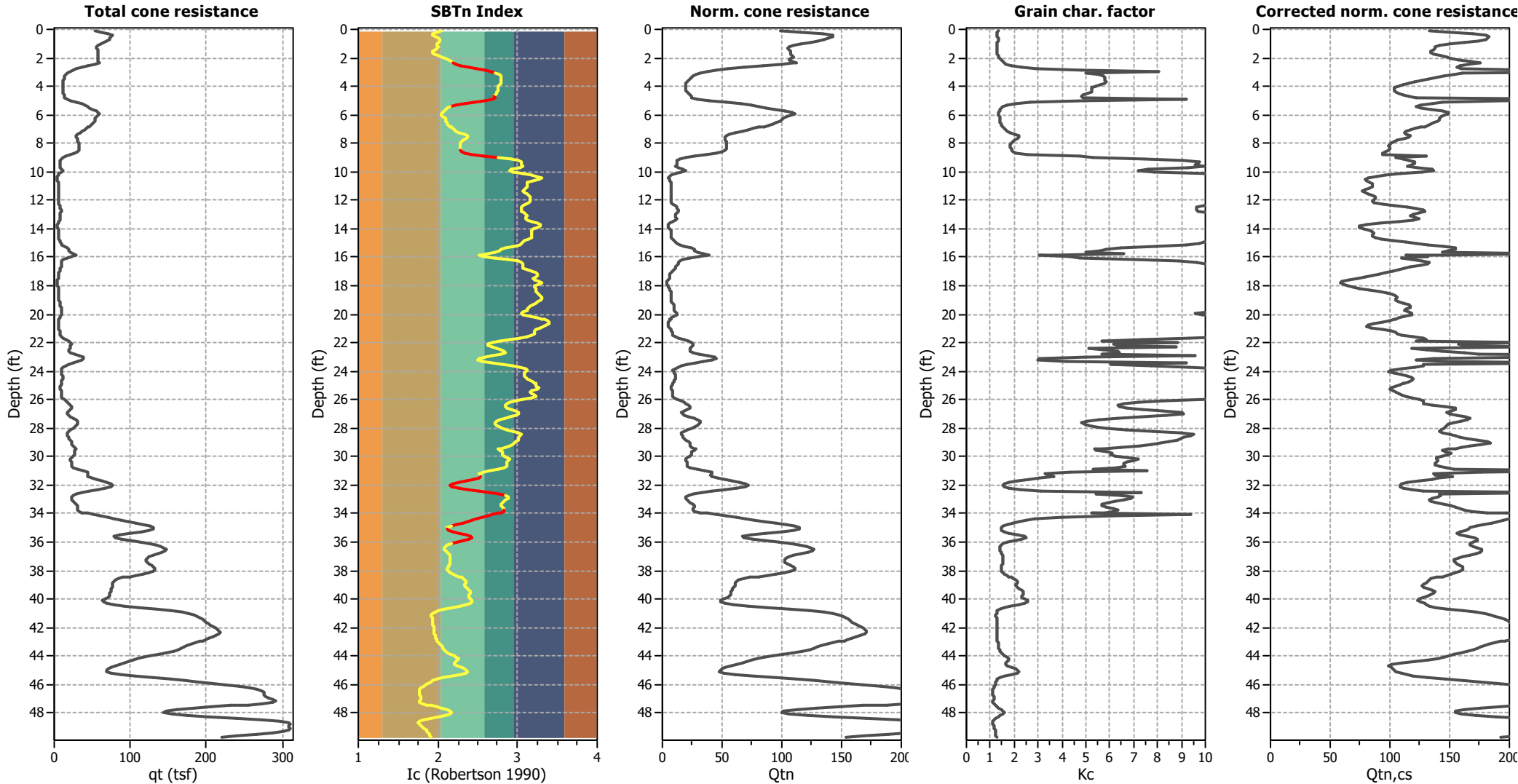
Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	No
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

SBTn legend

1. Sensitive fine grained	4. Clayey silt to silty	7. Gravely sand to sand
2. Organic material	5. Silty sand to sandy silt	8. Very stiff sand to
3. Clay to silty clay	6. Clean sand to silty sand	9. Very stiff fine grained

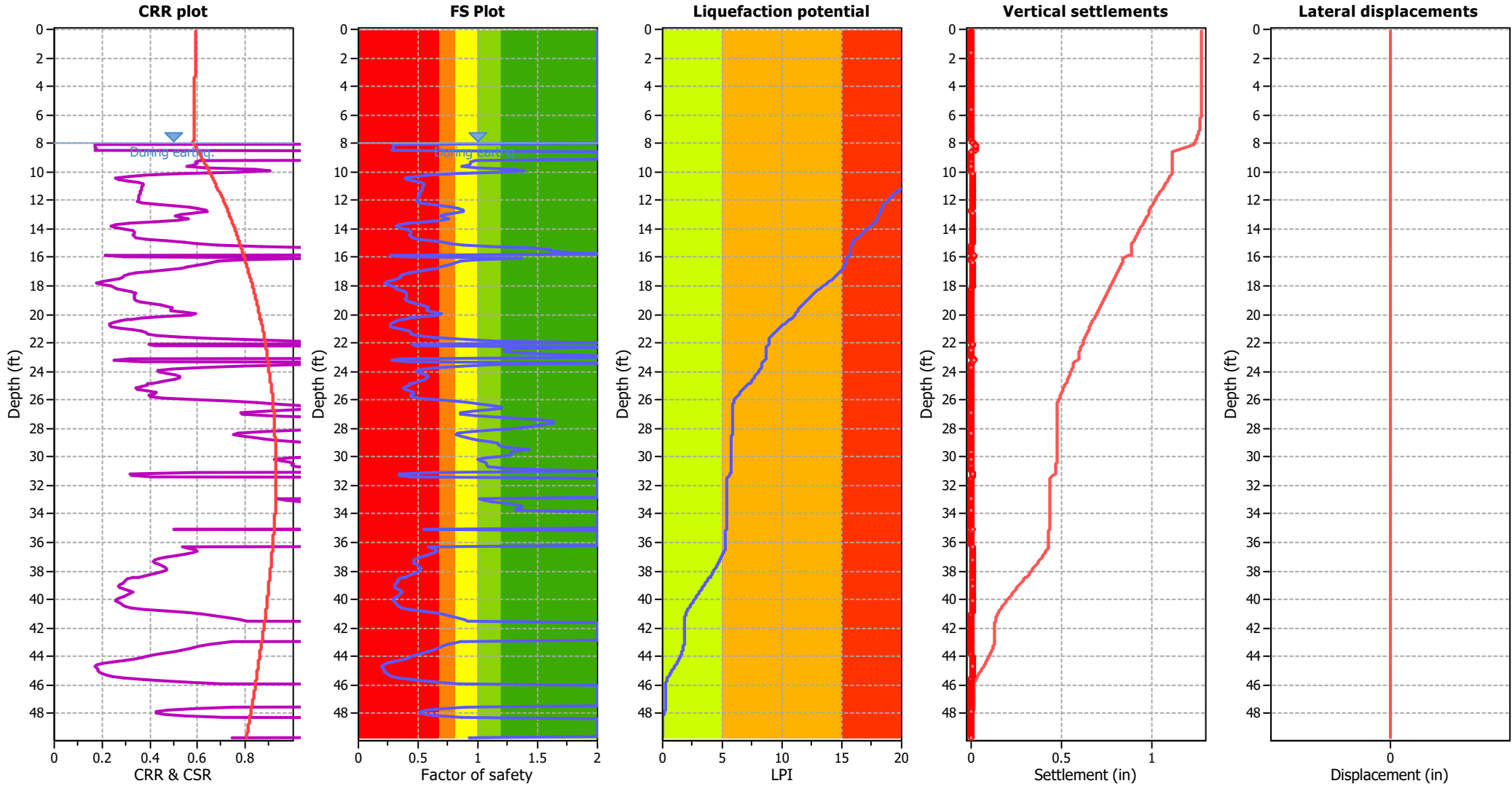
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	No
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (earthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	No
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

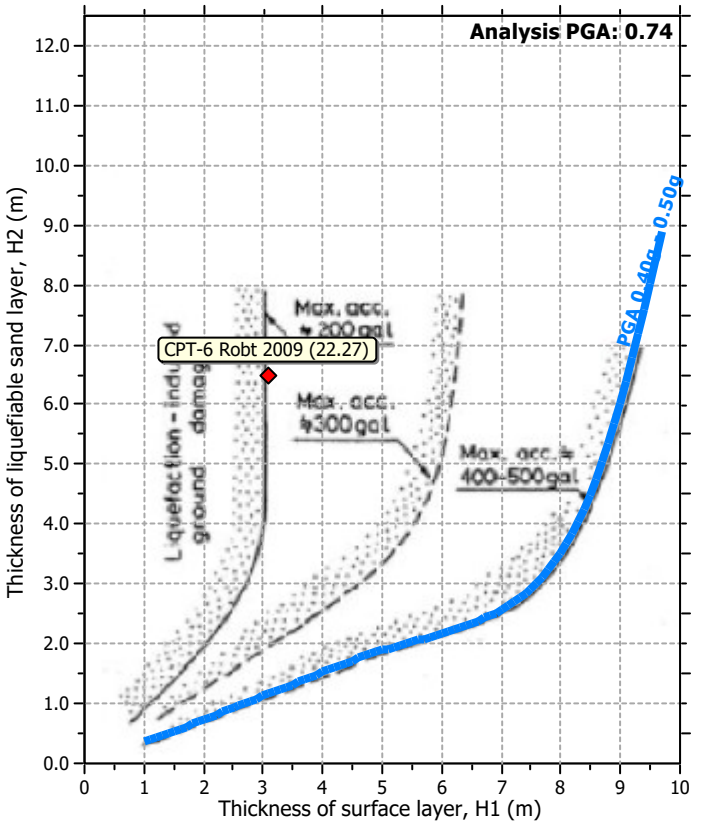
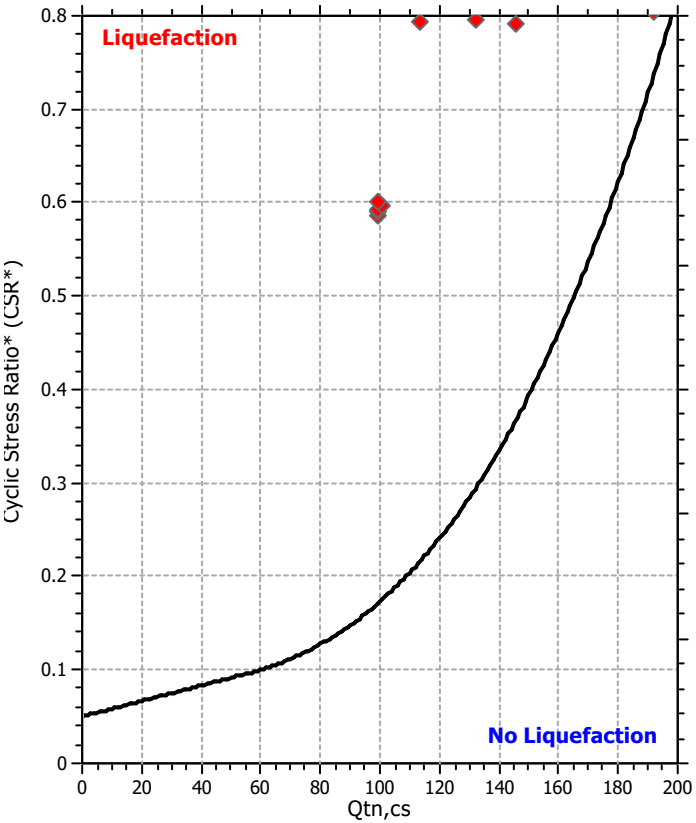
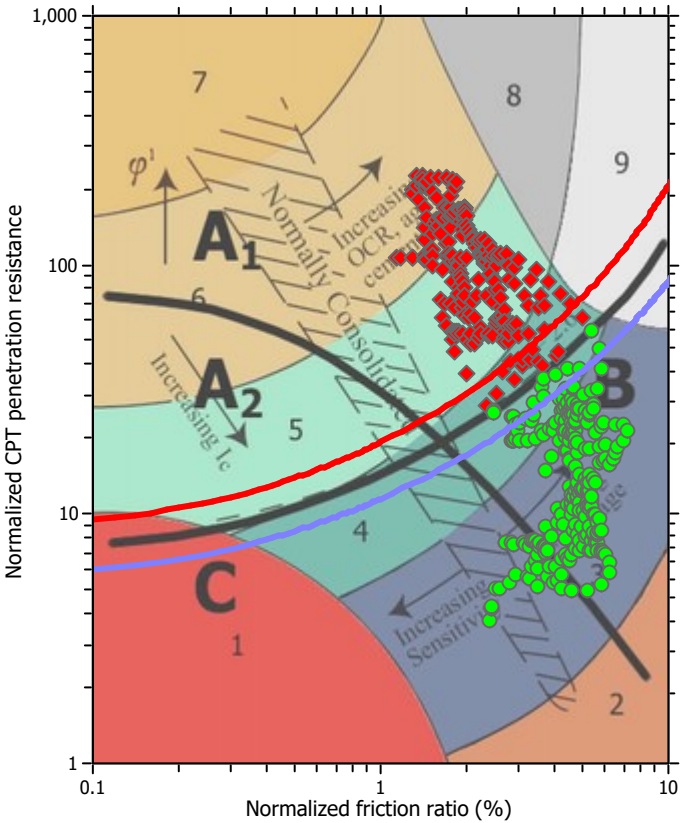
F.S. color scheme

- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

LPI color scheme

- Very high risk
- High risk
- Low risk

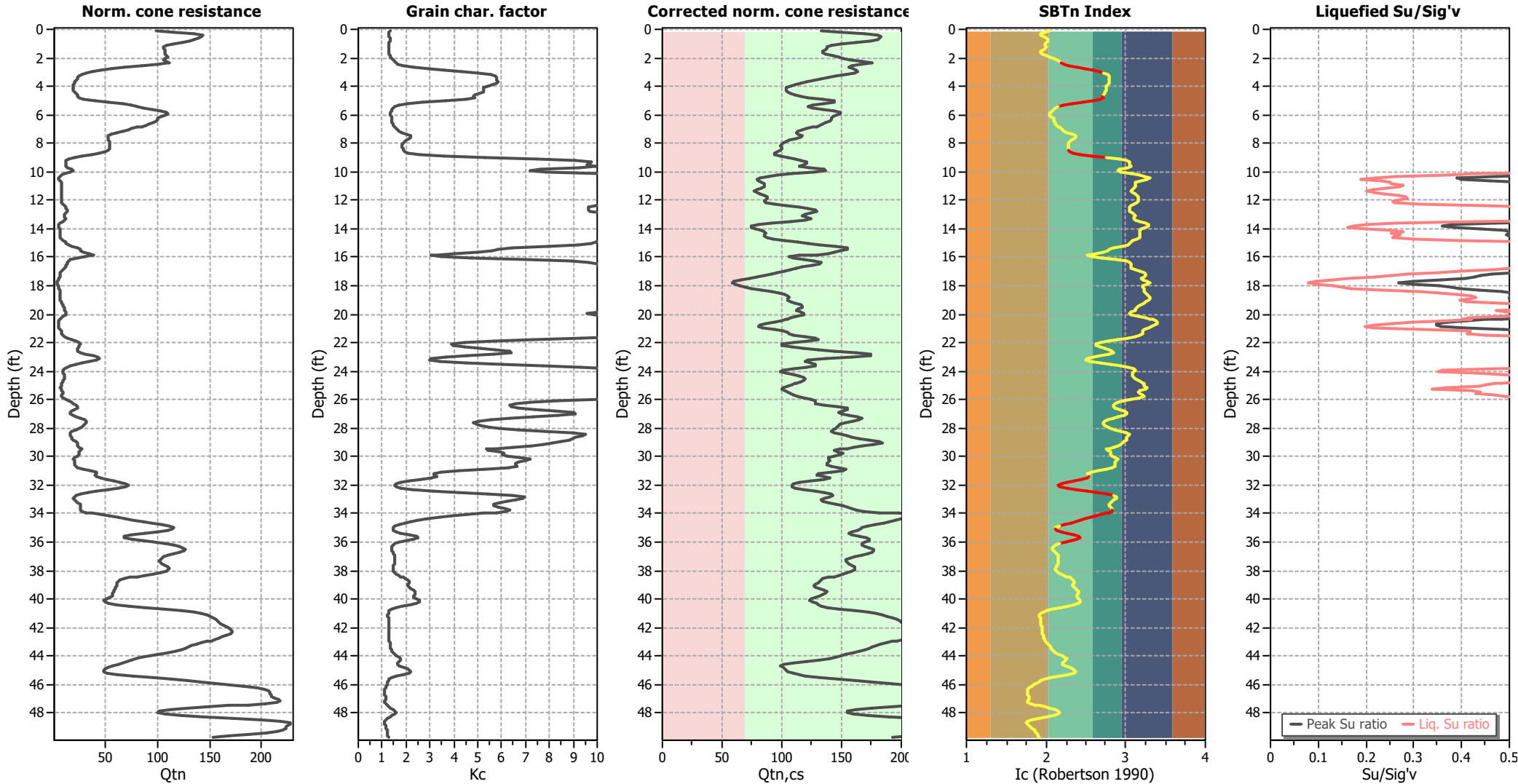
Liquefaction analysis summary plots



Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on I_c value	I_c cut-off value:	2.60	K_o applied:	No
Earthquake magnitude M_w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

Check for strength loss plots (Robertson (2010))



Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on I_c value	I_c cut-off value:	2.60	K_o applied:	No
Earthquake magnitude M_w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

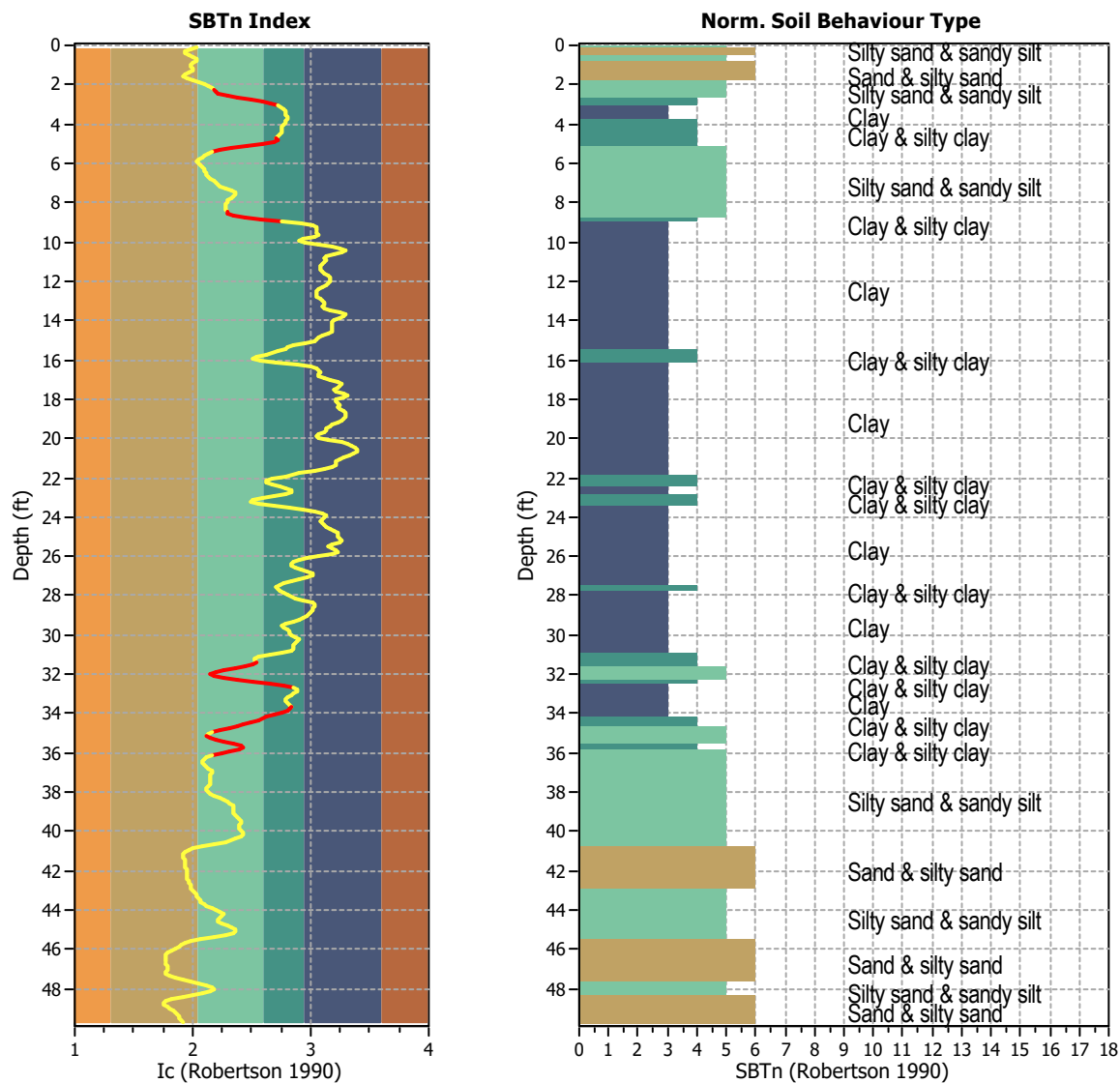
TRANSITION LAYER DETECTION ALGORITHM REPORT

Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vise-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between $1.80 < I_c < 3.0$) and a rate of change of I_c . Transitions typically occur when the rate of change of I_c is fast (i.e. ΔI_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties

I_c minimum check value: 1.70
 I_c maximum check value: 3.00
 I_c change ratio value: 0.0250
Minimum number of points in layer: 4

General statistics

Total points in CPT file: 497
Total points excluded: 61
Exclusion percentage: 12.27%
Number of layers detected: 8

Transition layer No	Number of points	Depth	SBT _n number	SBT _n description
Transition layer 1	9	Start depth: 2.40 (ft)	5	Silty sand & sandy silt
		End depth: 3.20 (ft)	3	Clay
Transition layer 2	8	Start depth: 4.80 (ft)	4	Clay & silty clay
		End depth: 5.50 (ft)	5	Silty sand & sandy silt
Transition layer 3	6	Start depth: 8.60 (ft)	5	Silty sand & sandy silt
		End depth: 9.10 (ft)	3	Clay
Transition layer 4	6	Start depth: 31.50 (ft)	4	Clay & silty clay
		End depth: 32.00 (ft)	5	Silty sand & sandy silt
Transition layer 5	8	Start depth: 32.10 (ft)	5	Silty sand & sandy silt
		End depth: 32.80 (ft)	3	Clay
Transition layer 6	13	Start depth: 33.80 (ft)	3	Clay
		End depth: 35.00 (ft)	5	Silty sand & sandy silt
Transition layer 7	5	Start depth: 35.20 (ft)	5	Silty sand & sandy silt
		End depth: 35.60 (ft)	4	Clay & silty clay
Transition layer 8	6	Start depth: 35.70 (ft)	4	Clay & silty clay
		End depth: 36.20 (ft)	5	Silty sand & sandy silt

Start depth: Depth where the transition layer begins

End depth: Depth where the transition layer ends

:: Field input data ::						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1	0.10	48.00	0.73	0.73	13.89	118.30
2	0.20	61.60	0.94	0.94	12.43	119.69
3	0.30	74.47	1.09	1.09	11.39	121.26
4	0.40	77.45	1.23	1.23	11.34	122.24
5	0.50	75.25	1.33	1.33	12.14	122.84
6	0.60	72.97	1.41	1.41	13.07	123.23
7	0.70	71.93	1.47	1.47	13.72	123.35
8	0.80	69.82	1.43	1.43	13.67	122.77
9	0.90	65.99	1.13	1.13	13.02	121.37
10	1.00	61.41	0.83	0.83	12.48	119.76
11	1.10	57.01	0.82	0.82	12.46	118.69
12	1.20	55.11	0.80	0.80	12.96	118.57
13	1.30	55.77	0.82	0.82	12.76	118.36
14	1.40	56.73	0.75	0.75	12.00	117.83
15	1.50	56.89	0.62	0.62	11.19	117.09
16	1.60	56.30	0.60	0.60	11.00	116.86
17	1.70	56.47	0.69	0.69	11.86	117.80
18	1.80	57.67	0.88	0.88	13.11	119.16
19	1.90	58.37	1.04	1.04	14.31	120.32
20	2.00	57.87	1.14	1.14	15.60	121.09
21	2.10	54.99	1.24	1.24	16.94	121.89
22	2.20	56.26	1.45	1.45	18.03	122.97
23	2.30	61.09	1.72	1.72	18.39	123.72
24	2.40	60.46	1.67	1.67	18.66	123.66
25	2.50	53.61	1.43	1.43	19.71	122.74
26	2.60	44.47	1.29	1.29	22.08	121.49
27	2.70	35.89	1.19	1.19	25.80	120.24
28	2.80	28.28	1.06	1.06	30.15	119.04
29	2.90	23.56	0.98	0.98	34.51	117.92
30	3.00	20.18	0.92	0.92	38.47	116.86
31	3.10	16.92	0.81	0.81	41.94	115.60
32	3.20	14.43	0.68	0.68	44.53	114.17
33	3.30	13.20	0.59	0.59	45.55	112.97
34	3.40	13.04	0.55	0.55	45.67	112.11
35	3.50	12.44	0.50	0.50	45.61	111.38
36	3.60	11.77	0.45	0.45	45.83	110.47
37	3.70	11.08	0.40	0.40	45.96	109.56
38	3.80	10.67	0.36	0.36	45.70	108.79
39	3.90	10.67	0.34	0.34	44.99	108.20
40	4.00	10.67	0.32	0.32	43.93	107.68
41	4.10	10.67	0.29	0.29	43.24	107.34
42	4.20	10.67	0.30	0.30	43.09	107.25
43	4.30	10.67	0.31	0.31	43.21	107.30
44	4.40	10.67	0.30	0.30	42.99	107.62
45	4.50	11.38	0.33	0.33	42.07	108.37
46	4.60	12.78	0.39	0.39	41.20	109.19
47	4.70	13.04	0.40	0.40	40.99	109.93
48	4.80	13.06	0.43	0.43	41.26	110.82

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
49	4.90	14.39	0.53	0.53	39.59	113.05
50	5.00	20.29	0.78	0.78	34.72	115.72
51	5.10	28.72	0.98	0.98	28.84	117.78
52	5.20	36.26	0.98	0.98	23.76	118.47
53	5.30	40.53	0.85	0.85	19.95	118.10
54	5.40	42.67	0.73	0.73	17.64	117.71
55	5.50	45.50	0.79	0.79	16.52	118.08
56	5.60	49.97	0.91	0.91	15.96	119.16
57	5.70	55.30	1.03	1.03	15.24	120.06
58	5.80	59.04	1.07	1.07	14.44	120.40
59	5.90	59.85	0.99	0.99	14.00	120.25
60	6.00	57.56	0.96	0.96	14.22	119.98
61	6.10	54.43	0.98	0.98	14.88	119.87
62	6.20	53.33	0.98	0.98	15.48	119.90
63	6.30	53.33	1.00	1.00	15.64	119.88
64	6.40	52.98	0.98	0.98	15.75	119.75
65	6.50	51.37	0.94	0.94	16.04	119.49
66	6.60	49.32	0.92	0.92	16.45	119.26
67	6.70	48.55	0.92	0.92	16.91	119.05
68	6.80	46.89	0.89	0.89	17.47	118.76
69	6.90	43.63	0.85	0.85	18.15	118.30
70	7.00	41.13	0.81	0.81	18.81	117.74
71	7.10	39.45	0.75	0.75	19.27	117.16
72	7.20	37.56	0.70	0.70	20.00	116.52
73	7.30	33.78	0.66	0.66	21.46	115.97
74	7.40	29.93	0.66	0.66	23.54	115.67
75	7.50	28.02	0.68	0.68	25.00	115.67
76	7.60	29.00	0.70	0.70	25.10	115.59
77	7.70	29.63	0.64	0.64	24.33	115.30
78	7.80	29.63	0.59	0.59	23.42	114.92
79	7.90	30.77	0.59	0.59	22.62	114.72
80	8.00	32.00	0.58	0.58	22.06	114.66
81	8.10	32.00	0.56	0.56	21.60	114.50
82	8.20	32.00	0.54	0.54	21.60	114.46
83	8.30	32.00	0.57	0.57	21.76	114.55
84	8.40	32.00	0.58	0.58	21.95	114.67
85	8.50	32.00	0.57	0.57	22.08	114.49
86	8.60	30.74	0.54	0.54	22.50	113.89
87	8.70	27.62	0.48	0.48	24.14	112.80
88	8.80	21.58	0.41	0.41	27.87	111.27
89	8.90	14.98	0.36	0.36	34.42	109.31
90	9.00	9.98	0.29	0.29	43.44	107.64
91	9.10	8.13	0.29	0.29	53.09	106.63
92	9.20	7.12	0.31	0.31	59.77	106.49
93	9.30	6.62	0.32	0.32	62.24	106.92
94	9.40	7.57	0.36	0.36	62.05	106.94
95	9.50	7.24	0.31	0.31	61.68	106.50
96	9.60	6.32	0.26	0.26	62.88	105.87

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
97	9.70	6.48	0.29	0.29	60.30	107.40
98	9.80	9.91	0.47	0.47	53.86	110.12
99	9.90	13.34	0.60	0.60	51.99	110.60
100	10.00	8.48	0.35	0.35	54.71	108.82
101	10.10	5.53	0.22	0.22	63.33	104.83
102	10.20	4.96	0.19	0.19	71.30	101.73
103	10.30	3.80	0.14	0.14	76.09	99.76
104	10.40	3.38	0.12	0.12	80.76	97.65
105	10.50	3.18	0.10	0.10	78.27	97.35
106	10.60	4.08	0.12	0.12	72.44	98.02
107	10.70	4.74	0.13	0.13	67.72	99.01
108	10.80	4.74	0.14	0.14	66.54	99.60
109	10.90	4.74	0.15	0.15	67.18	99.80
110	11.00	4.74	0.14	0.14	67.13	99.72
111	11.10	4.74	0.13	0.13	65.94	99.17
112	11.20	4.74	0.12	0.12	64.45	98.48
113	11.30	4.74	0.11	0.11	63.60	98.05
114	11.40	4.74	0.11	0.11	63.73	98.04
115	11.50	4.74	0.12	0.12	64.87	98.48
116	11.60	4.74	0.13	0.13	66.70	99.19
117	11.70	4.74	0.15	0.15	68.55	99.89
118	11.80	4.74	0.16	0.16	69.86	100.35
119	11.90	4.74	0.16	0.16	70.17	100.41
120	12.00	4.74	0.15	0.15	69.77	100.20
121	12.10	4.74	0.14	0.14	69.36	99.98
122	12.20	4.74	0.14	0.14	68.14	100.46
123	12.30	5.38	0.17	0.17	65.22	102.32
124	12.40	6.88	0.25	0.25	62.94	104.55
125	12.50	7.40	0.31	0.31	61.69	106.55
126	12.60	7.89	0.37	0.37	61.85	107.83
127	12.70	8.30	0.40	0.40	61.70	108.69
128	12.80	8.54	0.43	0.43	61.92	108.93
129	12.90	8.15	0.40	0.40	63.82	108.12
130	13.00	6.54	0.30	0.30	65.90	107.05
131	13.10	6.60	0.30	0.30	67.08	106.64
132	13.20	7.35	0.36	0.36	66.36	107.40
133	13.30	7.63	0.39	0.39	65.36	108.01
134	13.40	7.70	0.37	0.37	66.80	107.11
135	13.50	5.87	0.25	0.25	70.68	104.73
136	13.60	4.22	0.15	0.15	76.84	101.22
137	13.70	3.75	0.12	0.12	80.58	98.39
138	13.80	3.71	0.10	0.10	79.89	97.07
139	13.90	3.78	0.10	0.10	76.32	97.26
140	14.00	4.48	0.12	0.12	72.99	98.54
141	14.10	5.03	0.15	0.15	70.91	100.05
142	14.20	5.14	0.17	0.17	71.39	100.61
143	14.30	4.75	0.15	0.15	71.60	100.80
144	14.40	5.14	0.16	0.16	71.83	100.64

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
145	14.50	5.01	0.16	0.16	71.41	100.72
146	14.60	4.94	0.16	0.16	70.94	101.11
147	14.70	5.54	0.18	0.18	68.80	102.50
148	14.80	6.60	0.24	0.24	65.06	104.99
149	14.90	8.26	0.34	0.34	62.92	107.13
150	15.00	8.62	0.40	0.40	62.18	108.66
151	15.10	8.79	0.43	0.43	60.24	110.31
152	15.20	11.54	0.58	0.58	55.06	112.72
153	15.30	16.02	0.81	0.81	48.79	115.30
154	15.40	20.58	0.97	0.97	46.04	115.97
155	15.50	16.90	0.72	0.72	44.89	115.63
156	15.60	16.68	0.68	0.68	41.88	115.90
157	15.70	25.96	0.99	0.99	36.89	116.92
158	15.80	29.72	0.91	0.91	32.60	117.11
159	15.90	27.63	0.63	0.63	31.23	115.53
160	16.00	22.70	0.52	0.52	33.70	113.21
161	16.10	15.31	0.45	0.45	40.86	111.35
162	16.20	10.66	0.40	0.40	51.17	110.14
163	16.30	9.56	0.44	0.44	58.87	110.26
164	16.40	10.25	0.54	0.54	61.83	110.78
165	16.50	9.81	0.52	0.52	63.23	110.52
166	16.60	8.49	0.41	0.41	63.61	109.54
167	16.70	8.79	0.38	0.38	63.50	108.28
168	16.80	8.31	0.33	0.33	63.56	107.51
169	16.90	7.60	0.31	0.31	66.50	106.40
170	17.00	6.40	0.26	0.26	70.66	105.27
171	17.10	5.80	0.23	0.23	75.45	103.78
172	17.20	5.02	0.19	0.19	77.40	102.49
173	17.30	5.05	0.17	0.17	76.90	101.22
174	17.40	5.14	0.15	0.15	74.78	99.90
175	17.50	4.74	0.11	0.11	72.88	98.29
176	17.60	4.60	0.09	0.09	74.47	96.01
177	17.70	3.67	0.06	0.06	78.67	93.98
178	17.80	3.16	0.05	0.05	82.07	92.94
179	17.90	3.73	0.07	0.07	78.63	94.13
180	18.00	4.65	0.09	0.09	74.21	95.91
181	18.10	4.74	0.10	0.10	74.22	97.27
182	18.20	4.42	0.11	0.11	75.58	98.86
183	18.30	5.23	0.16	0.16	75.97	100.99
184	18.40	5.93	0.21	0.21	75.30	102.94
185	18.50	5.93	0.24	0.24	76.46	104.26
186	18.60	5.93	0.27	0.27	78.72	105.00
187	18.70	5.93	0.29	0.29	80.29	105.49
188	18.80	5.93	0.30	0.30	80.98	105.67
189	18.90	5.93	0.29	0.29	80.77	105.55
190	19.00	5.93	0.28	0.28	79.48	105.52
191	19.10	6.28	0.29	0.29	77.42	106.06
192	19.20	6.98	0.34	0.34	74.94	107.10

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
193	19.30	7.66	0.39	0.39	72.01	108.05
194	19.40	8.30	0.40	0.40	69.82	108.49
195	19.50	8.36	0.39	0.39	67.85	108.65
196	19.60	8.72	0.40	0.40	67.54	108.27
197	19.70	8.03	0.34	0.34	66.95	108.07
198	19.80	8.44	0.36	0.36	63.58	108.99
199	19.90	11.48	0.50	0.50	61.49	109.77
200	20.00	10.27	0.44	0.44	62.66	109.68
201	20.10	7.73	0.35	0.35	69.22	108.01
202	20.20	6.35	0.30	0.30	77.36	106.47
203	20.30	5.93	0.29	0.29	82.23	105.90
204	20.40	5.93	0.31	0.31	85.01	105.56
205	20.50	5.44	0.28	0.28	87.78	104.75
206	20.60	4.76	0.22	0.22	89.54	103.39
207	20.70	4.74	0.19	0.19	89.02	101.95
208	20.80	4.74	0.16	0.16	86.39	100.97
209	20.90	4.74	0.15	0.15	83.75	100.62
210	21.00	5.09	0.16	0.16	79.70	101.94
211	21.10	6.42	0.24	0.24	76.22	104.23
212	21.20	7.30	0.31	0.31	74.32	105.90
213	21.30	7.11	0.32	0.32	74.08	106.59
214	21.40	7.18	0.31	0.31	73.89	106.84
215	21.50	7.64	0.34	0.34	71.78	107.83
216	21.60	8.93	0.43	0.43	67.12	109.81
217	21.70	11.60	0.57	0.57	60.52	111.77
218	21.80	14.38	0.63	0.63	52.39	113.32
219	21.90	18.47	0.65	0.65	45.03	113.81
220	22.00	21.26	0.57	0.57	39.27	113.47
221	22.10	22.05	0.47	0.47	36.35	112.86
222	22.20	21.76	0.49	0.49	36.60	112.80
223	22.30	20.70	0.56	0.56	39.18	113.38
224	22.40	19.46	0.62	0.62	42.37	114.18
225	22.50	19.26	0.71	0.71	45.51	115.09
226	22.60	18.96	0.83	0.83	48.09	116.37
227	22.70	19.87	1.02	1.02	48.36	118.34
228	22.80	25.44	1.40	1.40	45.11	120.38
229	22.90	32.47	1.61	1.61	39.92	121.84
230	23.00	38.55	1.57	1.57	34.79	121.83
231	23.10	40.24	1.18	1.18	31.29	120.58
232	23.20	36.60	0.88	0.88	30.57	118.82
233	23.30	30.45	0.86	0.86	33.50	117.35
234	23.40	23.72	0.78	0.78	39.59	116.23
235	23.50	18.02	0.70	0.70	46.84	114.82
236	23.60	14.35	0.62	0.62	54.31	113.24
237	23.70	11.59	0.52	0.52	60.70	111.36
238	23.80	9.50	0.38	0.38	65.44	109.12
239	23.90	8.27	0.30	0.30	67.21	107.29
240	24.00	8.50	0.29	0.29	66.14	107.12

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
241	24.10	9.83	0.36	0.36	64.93	108.05
242	24.20	10.03	0.40	0.40	64.35	109.33
243	24.30	10.55	0.46	0.46	65.05	110.15
244	24.40	10.67	0.49	0.49	66.18	110.56
245	24.50	10.07	0.48	0.48	67.70	110.58
246	24.60	9.83	0.48	0.48	70.13	110.18
247	24.70	8.95	0.44	0.44	72.58	109.63
248	24.80	8.30	0.41	0.41	74.70	109.03
249	24.90	8.30	0.40	0.40	75.36	108.64
250	25.00	8.30	0.38	0.38	74.89	108.42
251	25.10	8.28	0.37	0.37	76.18	107.75
252	25.20	7.16	0.31	0.31	78.16	106.92
253	25.30	6.83	0.29	0.29	76.25	106.90
254	25.40	8.94	0.36	0.36	71.90	107.60
255	25.50	9.55	0.38	0.38	69.47	108.33
256	25.60	8.76	0.37	0.37	70.97	108.61
257	25.70	8.65	0.40	0.40	74.43	108.79
258	25.80	8.36	0.42	0.42	75.22	109.41
259	25.90	9.20	0.47	0.47	71.56	110.48
260	26.00	11.64	0.56	0.56	63.37	112.26
261	26.10	15.73	0.69	0.69	56.40	113.64
262	26.20	17.30	0.69	0.69	51.91	114.38
263	26.30	17.85	0.67	0.67	49.38	115.05
264	26.40	20.56	0.82	0.82	48.27	116.28
265	26.50	22.52	1.01	1.01	48.38	117.65
266	26.60	22.30	1.11	1.11	49.93	118.29
267	26.70	20.60	1.08	1.08	52.80	117.89
268	26.80	17.36	0.92	0.92	56.32	116.95
269	26.90	15.53	0.85	0.85	59.44	116.13
270	27.00	15.44	0.87	0.87	59.65	116.31
271	27.10	17.71	0.99	0.99	56.70	117.47
272	27.20	21.67	1.19	1.19	52.52	118.93
273	27.30	25.17	1.34	1.34	48.29	120.18
274	27.40	29.08	1.42	1.42	44.62	120.86
275	27.50	31.73	1.40	1.40	42.14	120.88
276	27.60	30.84	1.27	1.27	41.14	120.48
277	27.70	29.52	1.20	1.20	41.55	119.92
278	27.80	28.15	1.16	1.16	42.61	119.51
279	27.90	26.75	1.13	1.13	44.09	119.05
280	28.00	24.61	1.05	1.05	46.30	118.33
281	28.10	21.36	0.94	0.94	49.72	117.33
282	28.20	17.96	0.85	0.85	54.41	116.41
283	28.30	15.97	0.84	0.84	59.14	116.07
284	28.40	15.64	0.91	0.91	61.26	116.54
285	28.50	17.25	1.03	1.03	60.76	117.26
286	28.60	18.37	1.09	1.09	59.76	117.87
287	28.70	18.37	1.12	1.12	59.16	118.56
288	28.80	19.95	1.29	1.29	58.77	119.55

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
289	28.90	21.95	1.51	1.51	57.34	120.60
290	29.00	23.79	1.59	1.59	55.79	121.04
291	29.10	23.76	1.48	1.48	54.29	120.60
292	29.20	22.52	1.23	1.23	52.14	120.04
293	29.30	24.90	1.25	1.25	48.72	119.96
294	29.40	29.06	1.34	1.34	45.31	120.13
295	29.50	29.63	1.21	1.21	43.63	119.84
296	29.60	27.10	1.08	1.08	44.10	119.16
297	29.70	25.19	1.08	1.08	46.24	119.01
298	29.80	25.05	1.20	1.20	46.99	119.41
299	29.90	27.52	1.26	1.26	46.71	119.26
300	30.00	25.20	1.00	1.00	47.64	118.48
301	30.10	20.43	0.91	0.91	49.98	117.42
302	30.20	20.20	0.93	0.93	52.05	117.16
303	30.30	21.55	0.96	0.96	51.10	117.38
304	30.40	22.52	0.97	0.97	49.84	117.51
305	30.50	22.52	0.95	0.95	49.35	117.55
306	30.60	22.52	0.96	0.96	49.43	117.56
307	30.70	22.52	0.97	0.97	49.55	117.92
308	30.80	23.73	1.08	1.08	47.97	119.09
309	30.90	29.55	1.36	1.36	43.52	120.81
310	31.00	39.02	1.60	1.60	37.95	122.09
311	31.10	45.58	1.53	1.53	33.67	122.26
312	31.20	45.25	1.28	1.28	31.72	121.61
313	31.30	41.98	1.19	1.19	31.97	121.31
314	31.40	42.63	1.40	1.40	32.50	122.03
315	31.50	48.49	1.64	1.64	31.29	123.08
316	31.60	55.32	1.69	1.69	28.22	123.58
317	31.70	62.06	1.52	1.52	24.52	123.36
318	31.80	68.38	1.32	1.32	21.17	122.90
319	31.90	74.66	1.28	1.28	18.64	122.50
320	32.00	79.14	1.20	1.20	17.52	122.32
321	32.10	77.33	1.19	1.19	18.16	122.29
322	32.20	68.13	1.29	1.29	20.94	122.37
323	32.30	56.33	1.37	1.37	25.61	122.23
324	32.40	44.71	1.35	1.35	31.36	121.56
325	32.50	34.78	1.22	1.22	37.74	120.61
326	32.60	28.44	1.17	1.17	44.05	119.62
327	32.70	24.30	1.11	1.11	48.85	118.81
328	32.80	22.52	1.01	1.01	50.97	118.09
329	32.90	22.52	0.94	0.94	50.64	117.57
330	33.00	23.07	0.92	0.92	49.20	117.60
331	33.10	24.87	0.99	0.99	47.74	118.14
332	33.20	26.95	1.10	1.10	46.30	119.08
333	33.30	29.54	1.24	1.24	45.27	120.07
334	33.40	31.36	1.37	1.37	45.20	120.77
335	33.50	30.55	1.41	1.41	46.14	121.11
336	33.60	29.39	1.44	1.44	47.52	121.20

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
337	33.70	29.04	1.46	1.46	48.20	121.42
338	33.80	30.40	1.55	1.55	47.52	122.28
339	33.90	35.17	1.89	1.89	45.73	124.00
340	34.00	42.93	2.48	2.48	43.06	126.02
341	34.10	51.69	2.99	2.99	39.78	127.71
342	34.20	60.90	3.26	3.26	36.31	128.90
343	34.30	70.42	3.47	3.47	33.02	129.61
344	34.40	78.27	3.50	3.50	30.07	130.06
345	34.50	86.70	3.49	3.49	27.59	130.46
346	34.60	95.97	3.69	3.69	25.22	130.85
347	34.70	106.75	3.71	3.71	22.83	131.15
348	34.80	118.46	3.57	3.57	20.17	131.01
349	34.90	126.90	3.15	3.15	17.90	130.58
350	35.00	130.93	2.89	2.89	16.53	130.12
351	35.10	130.59	2.90	2.90	16.33	129.94
352	35.20	126.40	2.93	2.93	17.07	129.79
353	35.30	115.74	2.84	2.84	18.67	129.45
354	35.40	99.53	2.74	2.74	21.13	128.86
355	35.50	84.44	2.62	2.62	24.33	128.34
356	35.60	74.88	2.65	2.65	26.85	128.18
357	35.70	76.49	2.82	2.82	27.39	128.63
358	35.80	86.83	3.10	3.10	25.82	129.46
359	35.90	100.50	3.36	3.36	23.19	130.15
360	36.00	114.24	3.29	3.29	20.41	130.42
361	36.10	125.42	3.08	3.08	18.04	130.38
362	36.20	134.03	3.02	3.02	16.43	130.33
363	36.30	139.79	3.01	3.01	15.56	130.45
364	36.40	144.62	3.09	3.09	15.22	130.70
365	36.50	147.54	3.24	3.24	15.25	131.01
366	36.60	147.82	3.36	3.36	15.60	131.21
367	36.70	143.26	3.37	3.37	16.22	131.17
368	36.80	134.87	3.28	3.28	16.99	130.92
369	36.90	127.95	3.18	3.18	17.57	130.52
370	37.00	124.31	2.99	2.99	17.67	130.05
371	37.10	122.73	2.78	2.78	17.51	129.61
372	37.20	120.81	2.71	2.71	17.39	129.31
373	37.30	119.96	2.69	2.69	17.40	129.25
374	37.40	121.58	2.73	2.73	17.40	129.39
375	37.50	124.03	2.83	2.83	17.27	129.63
376	37.60	127.71	2.90	2.90	17.02	129.87
377	37.70	131.28	2.93	2.93	16.69	130.01
378	37.80	133.34	2.94	2.94	16.48	130.08
379	37.90	133.15	2.95	2.95	16.48	130.05
380	38.00	130.81	2.90	2.90	16.81	129.90
381	38.10	124.70	2.83	2.83	17.48	129.62
382	38.20	116.16	2.74	2.74	18.51	129.19
383	38.30	106.68	2.60	2.60	19.82	128.73
384	38.40	98.47	2.53	2.53	21.09	128.10

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
385	38.50	89.98	2.30	2.30	22.20	127.35
386	38.60	83.06	2.07	2.07	23.07	126.58
387	38.70	78.95	2.00	2.00	23.91	126.18
388	38.80	77.26	2.06	2.06	24.39	126.01
389	38.90	77.04	1.97	1.97	24.35	125.82
390	39.00	77.04	1.86	1.86	24.10	125.63
391	39.10	76.97	1.91	1.91	24.08	125.49
392	39.20	75.61	1.88	1.88	24.52	125.56
393	39.30	74.67	1.93	1.93	25.21	125.77
394	39.40	74.67	2.10	2.10	25.95	126.08
395	39.50	74.23	2.15	2.15	26.53	126.27
396	39.60	73.01	2.11	2.11	26.61	126.11
397	39.70	72.31	1.99	1.99	26.30	125.81
398	39.80	72.98	1.91	1.91	26.06	125.57
399	39.90	71.88	1.92	1.92	26.19	125.05
400	40.00	65.45	1.65	1.65	26.86	124.49
401	40.10	62.30	1.59	1.59	27.62	124.11
402	40.20	63.23	1.73	1.73	27.82	124.40
403	40.30	67.48	1.83	1.83	26.92	125.08
404	40.40	75.72	1.97	1.97	24.89	126.01
405	40.50	89.55	2.24	2.24	21.86	127.10
406	40.60	110.40	2.42	2.42	18.37	128.10
407	40.70	134.32	2.47	2.47	15.16	128.83
408	40.80	155.86	2.52	2.52	13.02	129.45
409	40.90	169.99	2.71	2.71	11.92	130.01
410	41.00	177.44	2.84	2.84	11.22	130.26
411	41.10	182.86	2.66	2.66	10.86	130.49
412	41.20	187.98	2.88	2.88	10.76	130.82
413	41.30	192.20	3.15	3.15	11.03	131.41
414	41.40	195.09	3.32	3.32	11.28	131.86
415	41.50	196.62	3.43	3.43	11.37	132.13
416	41.60	199.14	3.48	3.48	11.38	132.31
417	41.70	201.91	3.53	3.53	11.34	132.50
418	41.80	205.54	3.65	3.65	11.36	132.77
419	41.90	209.45	3.82	3.82	11.49	133.16
420	42.00	212.56	4.05	4.05	11.63	133.51
421	42.10	215.33	4.16	4.16	11.71	133.75
422	42.20	216.86	4.19	4.19	11.70	133.86
423	42.30	218.08	4.20	4.20	11.65	133.86
424	42.40	217.20	4.14	4.14	11.71	133.79
425	42.50	212.51	4.09	4.09	11.91	133.67
426	42.60	207.25	4.08	4.08	12.17	133.52
427	42.70	203.31	3.98	3.98	12.35	133.33
428	42.80	199.90	3.86	3.86	12.44	133.11
429	42.90	196.55	3.79	3.79	12.58	132.89
430	43.00	191.59	3.71	3.71	12.84	132.68
431	43.10	185.34	3.63	3.63	13.20	132.45
432	43.20	179.02	3.56	3.56	13.64	132.25

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
433	43.30	173.58	3.53	3.53	14.07	132.09
434	43.40	169.82	3.51	3.51	14.41	131.96
435	43.50	167.09	3.46	3.46	14.66	131.81
436	43.60	163.43	3.38	3.38	14.95	131.57
437	43.70	156.70	3.27	3.27	15.53	131.32
438	43.80	147.72	3.24	3.24	16.42	130.99
439	43.90	137.11	3.13	3.13	17.61	130.58
440	44.00	125.53	2.98	2.98	18.94	130.11
441	44.10	115.81	2.90	2.90	20.16	129.57
442	44.20	108.59	2.71	2.71	20.91	128.89
443	44.30	102.86	2.40	2.40	20.82	127.87
444	44.40	98.43	1.98	1.98	20.10	126.45
445	44.50	92.79	1.56	1.56	19.31	124.82
446	44.60	86.06	1.30	1.30	19.32	123.48
447	44.70	79.25	1.27	1.27	20.52	122.91
448	44.80	73.95	1.35	1.35	22.35	122.93
449	44.90	70.90	1.40	1.40	23.75	122.98
450	45.00	69.30	1.36	1.36	24.55	122.90
451	45.10	67.51	1.34	1.34	24.98	123.10
452	45.20	70.37	1.52	1.52	24.45	124.01
453	45.30	83.69	1.81	1.81	21.99	125.42
454	45.40	106.72	2.03	2.03	18.24	126.62
455	45.50	131.24	2.05	2.05	14.85	127.57
456	45.60	154.31	2.20	2.20	12.64	128.44
457	45.70	172.39	2.47	2.47	11.30	129.25
458	45.80	187.52	2.55	2.55	10.57	130.18
459	45.90	204.73	2.92	2.92	9.94	131.08
460	46.00	225.13	3.26	3.26	9.23	131.85
461	46.10	243.98	3.24	3.24	8.43	132.32
462	46.20	258.17	3.29	3.29	7.70	132.52
463	46.30	268.40	3.33	3.33	7.46	132.87
464	46.40	273.76	3.61	3.61	7.51	133.27
465	46.50	275.88	3.78	3.78	7.51	133.42
466	46.60	276.15	3.51	3.51	7.49	133.43
467	46.70	276.20	3.62	3.62	7.45	133.42
468	46.80	277.65	3.76	3.76	7.77	133.82
469	46.90	280.95	4.11	4.11	7.94	134.22
470	47.00	288.52	4.20	4.20	7.89	134.48
471	47.10	294.68	4.10	4.10	7.61	134.38
472	47.20	291.06	3.90	3.90	7.61	134.13
473	47.30	275.60	3.86	3.86	8.14	133.90
474	47.40	254.91	3.91	3.91	9.25	133.76
475	47.50	232.39	3.97	3.97	10.75	133.58
476	47.60	207.07	3.94	3.94	12.46	133.20
477	47.70	182.30	3.74	3.74	14.33	132.62
478	47.80	159.89	3.52	3.52	16.18	131.87
479	47.90	141.67	3.28	3.28	17.68	131.35
480	48.00	139.40	3.33	3.33	18.16	131.36

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
481	48.10	151.90	3.59	3.59	17.32	131.88
482	48.20	171.46	3.81	3.81	15.50	132.67
483	48.30	201.25	4.06	4.06	13.14	133.38
484	48.40	238.19	4.14	4.14	10.72	133.95
485	48.50	276.32	4.11	4.11	8.72	134.26
486	48.60	302.56	4.03	4.03	7.47	134.42
487	48.70	313.39	4.06	4.06	7.05	134.59
488	48.80	310.91	4.24	4.24	7.28	134.88
489	48.90	306.35	4.51	4.51	7.81	135.32
490	49.00	308.28	4.87	4.87	8.36	135.85
491	49.10	311.39	5.26	5.26	8.82	136.32
492	49.20	308.77	5.46	5.46	9.27	136.62
493	49.30	302.93	5.57	5.57	9.63	136.58
494	49.40	290.32	5.28	5.28	9.89	136.09
495	49.50	269.17	4.65	4.65	10.10	135.05
496	49.60	238.64	3.86	3.86	10.50	133.67
497	49.70	209.41	3.32	3.32	10.90	132.59

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q _c :	Measured cone resistance (tsf)
f _s :	Sleeve friction resistance (tsf)
u:	Pore pressure (tsf)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (pcf)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1	0.10	0.01	0.00	0.01	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
2	0.20	0.01	0.00	0.01	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
3	0.30	0.02	0.00	0.02	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
4	0.40	0.02	0.00	0.02	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
5	0.50	0.03	0.00	0.03	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
6	0.60	0.04	0.00	0.04	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
7	0.70	0.04	0.00	0.04	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
8	0.80	0.05	0.00	0.05	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
9	0.90	0.05	0.00	0.05	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
10	1.00	0.06	0.00	0.06	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
11	1.10	0.07	0.00	0.07	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
12	1.20	0.07	0.00	0.07	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
13	1.30	0.08	0.00	0.08	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
14	1.40	0.08	0.00	0.08	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
15	1.50	0.09	0.00	0.09	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
16	1.60	0.10	0.00	0.10	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
17	1.70	0.10	0.00	0.10	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
18	1.80	0.11	0.00	0.11	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
19	1.90	0.11	0.00	0.11	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
20	2.00	0.12	0.00	0.12	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
21	2.10	0.13	0.00	0.13	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
22	2.20	0.13	0.00	0.13	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
23	2.30	0.14	0.00	0.14	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
24	2.40	0.14	0.00	0.14	1.00	0.479	1.06	0.454	1.00	1.30	2.000	Yes
25	2.50	0.15	0.00	0.15	1.00	0.479	1.06	0.454	1.00	1.30	2.000	Yes
26	2.60	0.16	0.00	0.16	1.00	0.479	1.06	0.453	1.00	1.30	2.000	Yes
27	2.70	0.16	0.00	0.16	1.00	0.479	1.06	0.453	1.00	1.30	2.000	Yes
28	2.80	0.17	0.00	0.17	1.00	0.479	1.06	0.453	1.00	1.30	2.000	Yes
29	2.90	0.17	0.00	0.17	1.00	0.479	1.06	0.453	1.00	1.30	2.000	Yes
30	3.00	0.18	0.00	0.18	0.99	0.479	1.06	0.453	1.00	1.30	2.000	Yes
31	3.10	0.19	0.00	0.19	0.99	0.478	1.06	0.453	1.00	1.30	2.000	Yes
32	3.20	0.19	0.00	0.19	0.99	0.478	1.06	0.453	1.00	1.30	2.000	Yes
33	3.30	0.20	0.00	0.20	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
34	3.40	0.20	0.00	0.20	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
35	3.50	0.21	0.00	0.21	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
36	3.60	0.21	0.00	0.21	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
37	3.70	0.22	0.00	0.22	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
38	3.80	0.23	0.00	0.23	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
39	3.90	0.23	0.00	0.23	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
40	4.00	0.24	0.00	0.24	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
41	4.10	0.24	0.00	0.24	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
42	4.20	0.25	0.00	0.25	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
43	4.30	0.25	0.00	0.25	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
44	4.40	0.26	0.00	0.26	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
45	4.50	0.26	0.00	0.26	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
46	4.60	0.27	0.00	0.27	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
47	4.70	0.27	0.00	0.27	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
48	4.80	0.28	0.00	0.28	0.99	0.477	1.06	0.451	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
49	4.90	0.29	0.00	0.29	0.99	0.476	1.06	0.451	1.00	1.30	2.000	Yes
50	5.00	0.29	0.00	0.29	0.99	0.476	1.06	0.451	1.00	1.30	2.000	Yes
51	5.10	0.30	0.00	0.30	0.99	0.476	1.06	0.451	1.00	1.30	2.000	Yes
52	5.20	0.30	0.00	0.30	0.99	0.476	1.06	0.451	1.00	1.30	2.000	Yes
53	5.30	0.31	0.00	0.31	0.99	0.476	1.06	0.451	1.00	1.30	2.000	Yes
54	5.40	0.31	0.00	0.31	0.99	0.476	1.06	0.450	1.00	1.30	2.000	Yes
55	5.50	0.32	0.00	0.32	0.99	0.476	1.06	0.450	1.00	1.30	2.000	Yes
56	5.60	0.33	0.00	0.33	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
57	5.70	0.33	0.00	0.33	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
58	5.80	0.34	0.00	0.34	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
59	5.90	0.34	0.00	0.34	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
60	6.00	0.35	0.00	0.35	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
61	6.10	0.36	0.00	0.36	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
62	6.20	0.36	0.00	0.36	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
63	6.30	0.37	0.00	0.37	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
64	6.40	0.37	0.00	0.37	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
65	6.50	0.38	0.00	0.38	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
66	6.60	0.39	0.00	0.39	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
67	6.70	0.39	0.00	0.39	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
68	6.80	0.40	0.00	0.40	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
69	6.90	0.40	0.00	0.40	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
70	7.00	0.41	0.00	0.41	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
71	7.10	0.42	0.00	0.42	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
72	7.20	0.42	0.00	0.42	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
73	7.30	0.43	0.00	0.43	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
74	7.40	0.43	0.00	0.43	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
75	7.50	0.44	0.00	0.44	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
76	7.60	0.44	0.00	0.44	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
77	7.70	0.45	0.00	0.45	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
78	7.80	0.46	0.00	0.46	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
79	7.90	0.46	0.00	0.46	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
80	8.00	0.47	0.00	0.47	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
81	8.10	0.47	0.00	0.47	0.98	0.476	1.06	0.451	1.00	1.30	0.586	No
82	8.20	0.48	0.01	0.47	0.98	0.479	1.06	0.454	1.00	1.30	0.590	No
83	8.30	0.49	0.01	0.48	0.98	0.482	1.06	0.456	1.00	1.30	0.593	No
84	8.40	0.49	0.01	0.48	0.98	0.485	1.06	0.459	1.00	1.30	0.597	No
85	8.50	0.50	0.02	0.48	0.98	0.488	1.06	0.462	1.00	1.30	0.600	No
86	8.60	0.50	0.02	0.48	0.98	0.491	1.06	0.465	1.00	1.30	2.000	Yes
87	8.70	0.51	0.02	0.49	0.98	0.494	1.06	0.467	1.00	1.30	2.000	Yes
88	8.80	0.51	0.02	0.49	0.98	0.496	1.06	0.470	1.00	1.30	2.000	Yes
89	8.90	0.52	0.03	0.49	0.98	0.499	1.06	0.472	1.00	1.30	2.000	Yes
90	9.00	0.52	0.03	0.49	0.98	0.502	1.06	0.475	1.00	1.30	2.000	Yes
91	9.10	0.53	0.03	0.50	0.98	0.505	1.06	0.478	1.00	1.30	2.000	Yes
92	9.20	0.53	0.04	0.50	0.98	0.507	1.06	0.480	1.00	1.30	0.624	No
93	9.30	0.54	0.04	0.50	0.98	0.510	1.06	0.483	1.00	1.30	0.628	No
94	9.40	0.55	0.04	0.50	0.98	0.513	1.06	0.485	1.00	1.30	0.631	No
95	9.50	0.55	0.05	0.50	0.98	0.515	1.06	0.488	1.00	1.30	0.634	No
96	9.60	0.56	0.05	0.51	0.98	0.518	1.06	0.490	1.00	1.30	0.637	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
97	9.70	0.56	0.05	0.51	0.98	0.520	1.06	0.493	1.00	1.30	0.640	No
98	9.80	0.57	0.06	0.51	0.98	0.523	1.06	0.495	1.00	1.30	0.644	No
99	9.90	0.57	0.06	0.51	0.98	0.525	1.06	0.497	1.00	1.30	0.647	No
100	10.00	0.58	0.06	0.52	0.98	0.528	1.06	0.500	1.00	1.30	0.650	No
101	10.10	0.58	0.07	0.52	0.98	0.530	1.06	0.502	1.00	1.30	0.653	No
102	10.20	0.59	0.07	0.52	0.98	0.533	1.06	0.504	1.00	1.30	0.656	No
103	10.30	0.59	0.07	0.52	0.98	0.535	1.06	0.507	1.00	1.30	0.659	No
104	10.40	0.60	0.07	0.52	0.98	0.538	1.06	0.509	1.00	1.30	0.662	No
105	10.50	0.60	0.08	0.53	0.98	0.540	1.06	0.512	1.00	1.30	0.665	No
106	10.60	0.61	0.08	0.53	0.98	0.543	1.06	0.514	1.00	1.30	0.668	No
107	10.70	0.61	0.08	0.53	0.98	0.545	1.06	0.516	1.00	1.30	0.671	No
108	10.80	0.62	0.09	0.53	0.98	0.548	1.06	0.518	1.00	1.30	0.674	No
109	10.90	0.62	0.09	0.53	0.98	0.550	1.06	0.521	1.00	1.30	0.677	No
110	11.00	0.63	0.09	0.53	0.98	0.552	1.06	0.523	1.00	1.30	0.680	No
111	11.10	0.63	0.10	0.54	0.98	0.555	1.06	0.525	1.00	1.30	0.683	No
112	11.20	0.64	0.10	0.54	0.98	0.557	1.06	0.527	1.00	1.30	0.685	No
113	11.30	0.64	0.10	0.54	0.98	0.559	1.06	0.529	1.00	1.30	0.688	No
114	11.40	0.65	0.11	0.54	0.98	0.562	1.06	0.532	1.00	1.30	0.691	No
115	11.50	0.65	0.11	0.54	0.98	0.564	1.06	0.534	1.00	1.30	0.694	No
116	11.60	0.66	0.11	0.55	0.98	0.566	1.06	0.536	1.00	1.30	0.697	No
117	11.70	0.66	0.12	0.55	0.98	0.568	1.06	0.538	1.00	1.30	0.699	No
118	11.80	0.67	0.12	0.55	0.98	0.570	1.06	0.540	1.00	1.30	0.702	No
119	11.90	0.67	0.12	0.55	0.98	0.573	1.06	0.542	1.00	1.30	0.705	No
120	12.00	0.68	0.12	0.55	0.97	0.575	1.06	0.544	1.00	1.30	0.707	No
121	12.10	0.68	0.13	0.55	0.97	0.577	1.06	0.546	1.00	1.30	0.710	No
122	12.20	0.69	0.13	0.56	0.97	0.579	1.06	0.548	1.00	1.30	0.713	No
123	12.30	0.69	0.13	0.56	0.97	0.581	1.06	0.550	1.00	1.30	0.715	No
124	12.40	0.70	0.14	0.56	0.97	0.583	1.06	0.552	1.00	1.30	0.718	No
125	12.50	0.70	0.14	0.56	0.97	0.585	1.06	0.554	1.00	1.30	0.720	No
126	12.60	0.71	0.14	0.57	0.97	0.587	1.06	0.556	1.00	1.30	0.723	No
127	12.70	0.71	0.15	0.57	0.97	0.589	1.06	0.558	1.00	1.30	0.725	No
128	12.80	0.72	0.15	0.57	0.97	0.591	1.06	0.560	1.00	1.30	0.728	No
129	12.90	0.72	0.15	0.57	0.97	0.593	1.06	0.561	1.00	1.30	0.730	No
130	13.00	0.73	0.16	0.57	0.97	0.595	1.06	0.563	1.00	1.30	0.732	No
131	13.10	0.74	0.16	0.58	0.97	0.597	1.06	0.565	1.00	1.30	0.735	No
132	13.20	0.74	0.16	0.58	0.97	0.599	1.06	0.567	1.00	1.30	0.737	No
133	13.30	0.75	0.17	0.58	0.97	0.601	1.06	0.569	1.00	1.30	0.739	No
134	13.40	0.75	0.17	0.58	0.97	0.603	1.06	0.570	1.00	1.30	0.742	No
135	13.50	0.76	0.17	0.59	0.97	0.604	1.06	0.572	1.00	1.30	0.744	No
136	13.60	0.76	0.17	0.59	0.97	0.606	1.06	0.574	1.00	1.30	0.746	No
137	13.70	0.77	0.18	0.59	0.97	0.608	1.06	0.576	1.00	1.30	0.749	No
138	13.80	0.77	0.18	0.59	0.97	0.610	1.06	0.578	1.00	1.30	0.751	No
139	13.90	0.78	0.18	0.59	0.97	0.612	1.06	0.579	1.00	1.30	0.753	No
140	14.00	0.78	0.19	0.59	0.97	0.614	1.06	0.581	1.00	1.30	0.756	No
141	14.10	0.79	0.19	0.60	0.97	0.616	1.06	0.583	1.00	1.30	0.758	No
142	14.20	0.79	0.19	0.60	0.97	0.618	1.06	0.585	1.00	1.30	0.760	No
143	14.30	0.80	0.20	0.60	0.97	0.619	1.06	0.586	1.00	1.30	0.762	No
144	14.40	0.80	0.20	0.60	0.97	0.621	1.06	0.588	1.00	1.30	0.765	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
145	14.50	0.81	0.20	0.60	0.97	0.623	1.06	0.590	1.00	1.30	0.767	No
146	14.60	0.81	0.21	0.61	0.97	0.625	1.06	0.591	1.00	1.30	0.769	No
147	14.70	0.82	0.21	0.61	0.97	0.627	1.06	0.593	1.00	1.30	0.771	No
148	14.80	0.82	0.21	0.61	0.97	0.628	1.06	0.595	1.00	1.30	0.773	No
149	14.90	0.83	0.22	0.61	0.97	0.630	1.06	0.596	1.00	1.30	0.775	No
150	15.00	0.83	0.22	0.61	0.97	0.631	1.06	0.598	1.00	1.30	0.777	No
151	15.10	0.84	0.22	0.62	0.97	0.633	1.06	0.599	1.00	1.30	0.779	No
152	15.20	0.84	0.22	0.62	0.97	0.635	1.06	0.601	1.00	1.30	0.781	No
153	15.30	0.85	0.23	0.62	0.97	0.636	1.06	0.602	1.00	1.30	0.783	No
154	15.40	0.86	0.23	0.62	0.97	0.637	1.06	0.603	1.00	1.30	0.784	No
155	15.50	0.86	0.23	0.63	0.97	0.639	1.06	0.605	1.00	1.30	0.786	No
156	15.60	0.87	0.24	0.63	0.97	0.640	1.06	0.606	1.00	1.30	0.788	No
157	15.70	0.87	0.24	0.63	0.97	0.642	1.06	0.607	1.00	1.30	0.790	No
158	15.80	0.88	0.24	0.64	0.97	0.643	1.06	0.609	1.00	1.30	0.791	No
159	15.90	0.88	0.25	0.64	0.97	0.644	1.06	0.610	1.00	1.30	0.793	No
160	16.00	0.89	0.25	0.64	0.97	0.646	1.06	0.611	1.00	1.30	0.795	No
161	16.10	0.90	0.25	0.64	0.97	0.647	1.06	0.613	1.00	1.30	0.797	No
162	16.20	0.90	0.26	0.65	0.97	0.649	1.06	0.614	1.00	1.30	0.798	No
163	16.30	0.91	0.26	0.65	0.97	0.650	1.06	0.615	1.00	1.30	0.800	No
164	16.40	0.91	0.26	0.65	0.97	0.652	1.06	0.617	1.00	1.30	0.802	No
165	16.50	0.92	0.27	0.65	0.97	0.653	1.06	0.618	1.00	1.30	0.803	No
166	16.60	0.92	0.27	0.66	0.97	0.654	1.06	0.619	1.00	1.30	0.805	No
167	16.70	0.93	0.27	0.66	0.96	0.656	1.06	0.621	1.00	1.30	0.807	No
168	16.80	0.93	0.27	0.66	0.96	0.657	1.06	0.622	1.00	1.30	0.809	No
169	16.90	0.94	0.28	0.66	0.96	0.658	1.06	0.623	1.00	1.30	0.810	No
170	17.00	0.94	0.28	0.66	0.96	0.660	1.06	0.625	1.00	1.30	0.812	No
171	17.10	0.95	0.28	0.67	0.96	0.661	1.06	0.626	1.00	1.30	0.814	No
172	17.20	0.96	0.29	0.67	0.96	0.663	1.06	0.627	1.00	1.30	0.816	No
173	17.30	0.96	0.29	0.67	0.96	0.664	1.06	0.629	1.00	1.30	0.817	No
174	17.40	0.97	0.29	0.67	0.96	0.666	1.06	0.630	1.00	1.30	0.819	No
175	17.50	0.97	0.30	0.67	0.96	0.667	1.06	0.631	1.00	1.30	0.821	No
176	17.60	0.97	0.30	0.68	0.96	0.668	1.06	0.633	1.00	1.30	0.823	No
177	17.70	0.98	0.30	0.68	0.96	0.670	1.06	0.634	1.00	1.30	0.824	No
178	17.80	0.98	0.31	0.68	0.96	0.671	1.06	0.636	1.00	1.30	0.826	No
179	17.90	0.99	0.31	0.68	0.96	0.673	1.06	0.637	1.00	1.30	0.828	No
180	18.00	0.99	0.31	0.68	0.96	0.674	1.06	0.638	1.00	1.30	0.830	No
181	18.10	1.00	0.32	0.68	0.96	0.676	1.06	0.640	1.00	1.30	0.832	No
182	18.20	1.00	0.32	0.69	0.96	0.677	1.06	0.641	1.00	1.30	0.833	No
183	18.30	1.01	0.32	0.69	0.96	0.678	1.06	0.642	1.00	1.30	0.835	No
184	18.40	1.01	0.32	0.69	0.96	0.680	1.06	0.643	1.00	1.30	0.837	No
185	18.50	1.02	0.33	0.69	0.96	0.681	1.06	0.645	1.00	1.30	0.838	No
186	18.60	1.02	0.33	0.69	0.96	0.682	1.06	0.646	1.00	1.30	0.840	No
187	18.70	1.03	0.33	0.70	0.96	0.683	1.06	0.647	1.00	1.30	0.841	No
188	18.80	1.03	0.34	0.70	0.96	0.685	1.06	0.648	1.00	1.30	0.843	No
189	18.90	1.04	0.34	0.70	0.96	0.686	1.06	0.649	1.00	1.30	0.844	No
190	19.00	1.05	0.34	0.70	0.96	0.687	1.06	0.650	1.00	1.30	0.845	No
191	19.10	1.05	0.35	0.70	0.96	0.688	1.06	0.651	1.00	1.30	0.847	No
192	19.20	1.06	0.35	0.71	0.96	0.689	1.06	0.653	1.00	1.30	0.848	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
193	19.30	1.06	0.35	0.71	0.96	0.690	1.06	0.654	1.00	1.30	0.850	No
194	19.40	1.07	0.36	0.71	0.96	0.692	1.06	0.655	1.00	1.30	0.851	No
195	19.50	1.07	0.36	0.71	0.96	0.693	1.06	0.656	1.00	1.30	0.852	No
196	19.60	1.08	0.36	0.72	0.96	0.694	1.06	0.657	1.00	1.30	0.854	No
197	19.70	1.08	0.37	0.72	0.96	0.695	1.06	0.658	1.00	1.30	0.855	No
198	19.80	1.09	0.37	0.72	0.96	0.696	1.06	0.659	1.00	1.30	0.856	No
199	19.90	1.09	0.37	0.72	0.96	0.697	1.06	0.660	1.00	1.30	0.858	No
200	20.00	1.10	0.37	0.73	0.96	0.698	1.06	0.661	1.00	1.30	0.859	No
201	20.10	1.10	0.38	0.73	0.96	0.699	1.06	0.662	1.00	1.30	0.860	No
202	20.20	1.11	0.38	0.73	0.96	0.700	1.06	0.663	1.00	1.30	0.861	No
203	20.30	1.12	0.38	0.73	0.96	0.701	1.06	0.664	1.00	1.30	0.863	No
204	20.40	1.12	0.39	0.73	0.96	0.702	1.06	0.665	1.00	1.30	0.864	No
205	20.50	1.13	0.39	0.74	0.96	0.703	1.06	0.666	1.00	1.30	0.865	No
206	20.60	1.13	0.39	0.74	0.96	0.704	1.06	0.667	1.00	1.30	0.867	No
207	20.70	1.14	0.40	0.74	0.96	0.705	1.06	0.668	1.00	1.30	0.868	No
208	20.80	1.14	0.40	0.74	0.95	0.706	1.06	0.669	1.00	1.30	0.869	No
209	20.90	1.15	0.40	0.74	0.95	0.708	1.06	0.670	1.00	1.30	0.871	No
210	21.00	1.15	0.41	0.75	0.95	0.709	1.06	0.671	1.00	1.30	0.872	No
211	21.10	1.16	0.41	0.75	0.95	0.710	1.06	0.672	1.00	1.30	0.873	No
212	21.20	1.16	0.41	0.75	0.95	0.711	1.06	0.673	1.00	1.30	0.874	No
213	21.30	1.17	0.41	0.75	0.95	0.712	1.06	0.674	1.00	1.30	0.876	No
214	21.40	1.17	0.42	0.75	0.95	0.712	1.06	0.674	1.00	1.30	0.877	No
215	21.50	1.18	0.42	0.76	0.95	0.713	1.06	0.675	1.00	1.30	0.878	No
216	21.60	1.18	0.42	0.76	0.95	0.714	1.06	0.676	1.00	1.30	0.879	No
217	21.70	1.19	0.43	0.76	0.95	0.715	1.06	0.677	1.00	1.30	0.880	No
218	21.80	1.19	0.43	0.76	0.95	0.716	1.06	0.678	1.00	1.30	0.881	No
219	21.90	1.20	0.43	0.77	0.95	0.717	1.06	0.678	1.00	1.30	0.882	No
220	22.00	1.21	0.44	0.77	0.95	0.717	1.06	0.679	1.00	1.30	0.883	No
221	22.10	1.21	0.44	0.77	0.95	0.718	1.06	0.680	1.00	1.30	0.884	No
222	22.20	1.22	0.44	0.77	0.95	0.719	1.06	0.681	1.00	1.30	0.885	No
223	22.30	1.22	0.45	0.78	0.95	0.720	1.06	0.681	1.00	1.30	0.886	No
224	22.40	1.23	0.45	0.78	0.95	0.720	1.06	0.682	1.00	1.30	0.887	No
225	22.50	1.23	0.45	0.78	0.95	0.721	1.06	0.683	1.00	1.30	0.888	No
226	22.60	1.24	0.46	0.78	0.95	0.722	1.06	0.683	1.00	1.30	0.888	No
227	22.70	1.25	0.46	0.79	0.95	0.723	1.06	0.684	1.00	1.30	0.889	No
228	22.80	1.25	0.46	0.79	0.95	0.723	1.06	0.685	1.00	1.30	0.890	No
229	22.90	1.26	0.46	0.79	0.95	0.724	1.06	0.685	1.00	1.30	0.891	No
230	23.00	1.26	0.47	0.80	0.95	0.724	1.06	0.686	1.00	1.30	0.891	No
231	23.10	1.27	0.47	0.80	0.95	0.725	1.06	0.686	1.00	1.30	0.892	No
232	23.20	1.28	0.47	0.80	0.95	0.725	1.06	0.687	1.00	1.30	0.893	No
233	23.30	1.28	0.48	0.81	0.95	0.726	1.06	0.687	1.00	1.30	0.893	No
234	23.40	1.29	0.48	0.81	0.95	0.727	1.06	0.688	1.00	1.30	0.894	No
235	23.50	1.29	0.48	0.81	0.95	0.727	1.06	0.688	1.00	1.30	0.895	No
236	23.60	1.30	0.49	0.81	0.95	0.728	1.06	0.689	1.00	1.30	0.896	No
237	23.70	1.31	0.49	0.82	0.95	0.729	1.06	0.690	1.00	1.30	0.897	No
238	23.80	1.31	0.49	0.82	0.95	0.729	1.06	0.690	1.00	1.30	0.897	No
239	23.90	1.32	0.50	0.82	0.95	0.730	1.06	0.691	1.00	1.30	0.898	No
240	24.00	1.32	0.50	0.82	0.95	0.731	1.06	0.692	1.00	1.30	0.899	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
241	24.10	1.33	0.50	0.82	0.94	0.731	1.06	0.692	1.00	1.30	0.900	No
242	24.20	1.33	0.51	0.83	0.94	0.732	1.06	0.693	1.00	1.30	0.901	No
243	24.30	1.34	0.51	0.83	0.94	0.733	1.06	0.694	1.00	1.30	0.902	No
244	24.40	1.34	0.51	0.83	0.94	0.733	1.06	0.694	1.00	1.30	0.903	No
245	24.50	1.35	0.51	0.83	0.94	0.734	1.06	0.695	1.00	1.30	0.903	No
246	24.60	1.35	0.52	0.84	0.94	0.735	1.06	0.695	1.00	1.30	0.904	No
247	24.70	1.36	0.52	0.84	0.94	0.735	1.06	0.696	1.00	1.30	0.905	No
248	24.80	1.37	0.52	0.84	0.94	0.736	1.06	0.697	1.00	1.30	0.906	No
249	24.90	1.37	0.53	0.84	0.94	0.737	1.06	0.697	1.00	1.30	0.906	No
250	25.00	1.38	0.53	0.85	0.94	0.737	1.06	0.698	1.00	1.30	0.907	No
251	25.10	1.38	0.53	0.85	0.94	0.738	1.06	0.698	1.00	1.30	0.908	No
252	25.20	1.39	0.54	0.85	0.94	0.738	1.06	0.699	1.00	1.30	0.909	No
253	25.30	1.39	0.54	0.85	0.94	0.739	1.06	0.700	1.00	1.30	0.909	No
254	25.40	1.40	0.54	0.85	0.94	0.740	1.06	0.700	1.00	1.30	0.910	No
255	25.50	1.40	0.55	0.86	0.94	0.740	1.06	0.701	1.00	1.30	0.911	No
256	25.60	1.41	0.55	0.86	0.94	0.741	1.06	0.701	1.00	1.30	0.912	No
257	25.70	1.41	0.55	0.86	0.94	0.741	1.06	0.702	1.00	1.30	0.912	No
258	25.80	1.42	0.56	0.86	0.94	0.742	1.06	0.702	1.00	1.30	0.913	No
259	25.90	1.42	0.56	0.87	0.94	0.742	1.06	0.703	1.00	1.30	0.914	No
260	26.00	1.43	0.56	0.87	0.94	0.743	1.06	0.703	1.00	1.30	0.914	No
261	26.10	1.44	0.56	0.87	0.94	0.743	1.06	0.704	1.00	1.30	0.915	No
262	26.20	1.44	0.57	0.87	0.94	0.744	1.06	0.704	1.00	1.30	0.915	No
263	26.30	1.45	0.57	0.88	0.94	0.744	1.06	0.705	1.00	1.30	0.916	No
264	26.40	1.45	0.57	0.88	0.94	0.745	1.06	0.705	1.00	1.30	0.916	No
265	26.50	1.46	0.58	0.88	0.94	0.745	1.06	0.705	1.00	1.30	0.917	No
266	26.60	1.47	0.58	0.88	0.94	0.745	1.06	0.706	1.00	1.30	0.917	No
267	26.70	1.47	0.58	0.89	0.94	0.746	1.06	0.706	1.00	1.30	0.918	No
268	26.80	1.48	0.59	0.89	0.94	0.746	1.06	0.706	1.00	1.30	0.918	No
269	26.90	1.48	0.59	0.89	0.93	0.746	1.06	0.707	1.00	1.30	0.919	No
270	27.00	1.49	0.59	0.90	0.93	0.747	1.06	0.707	1.00	1.30	0.919	No
271	27.10	1.49	0.60	0.90	0.93	0.747	1.06	0.707	1.00	1.30	0.919	No
272	27.20	1.50	0.60	0.90	0.93	0.747	1.06	0.707	1.00	1.30	0.920	No
273	27.30	1.51	0.60	0.90	0.93	0.748	1.06	0.708	1.00	1.30	0.920	No
274	27.40	1.51	0.61	0.91	0.93	0.748	1.06	0.708	1.00	1.30	0.920	No
275	27.50	1.52	0.61	0.91	0.93	0.748	1.06	0.708	1.00	1.30	0.921	No
276	27.60	1.52	0.61	0.91	0.93	0.748	1.06	0.708	1.00	1.30	0.921	No
277	27.70	1.53	0.61	0.92	0.93	0.749	1.06	0.709	1.00	1.30	0.921	No
278	27.80	1.54	0.62	0.92	0.93	0.749	1.06	0.709	1.00	1.30	0.922	No
279	27.90	1.54	0.62	0.92	0.93	0.749	1.06	0.709	1.00	1.30	0.922	No
280	28.00	1.55	0.62	0.92	0.93	0.749	1.06	0.709	1.00	1.30	0.922	No
281	28.10	1.55	0.63	0.93	0.93	0.750	1.06	0.710	1.00	1.30	0.922	No
282	28.20	1.56	0.63	0.93	0.93	0.750	1.06	0.710	1.00	1.30	0.923	No
283	28.30	1.57	0.63	0.93	0.93	0.750	1.06	0.710	1.00	1.30	0.923	No
284	28.40	1.57	0.64	0.94	0.93	0.750	1.06	0.710	1.00	1.30	0.923	No
285	28.50	1.58	0.64	0.94	0.93	0.751	1.06	0.711	1.00	1.30	0.924	No
286	28.60	1.58	0.64	0.94	0.93	0.751	1.06	0.711	1.00	1.30	0.924	No
287	28.70	1.59	0.65	0.94	0.93	0.751	1.06	0.711	1.00	1.30	0.924	No
288	28.80	1.60	0.65	0.95	0.93	0.751	1.06	0.711	1.00	1.30	0.924	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
289	28.90	1.60	0.65	0.95	0.93	0.751	1.06	0.711	1.00	1.30	0.925	No
290	29.00	1.61	0.66	0.95	0.93	0.751	1.06	0.711	1.00	1.30	0.925	No
291	29.10	1.61	0.66	0.96	0.92	0.752	1.06	0.711	1.00	1.30	0.925	No
292	29.20	1.62	0.66	0.96	0.92	0.752	1.06	0.712	1.00	1.30	0.925	No
293	29.30	1.63	0.66	0.96	0.92	0.752	1.06	0.712	1.00	1.30	0.925	No
294	29.40	1.63	0.67	0.96	0.92	0.752	1.06	0.712	1.00	1.30	0.925	No
295	29.50	1.64	0.67	0.97	0.92	0.752	1.06	0.712	1.00	1.30	0.926	No
296	29.60	1.64	0.67	0.97	0.92	0.752	1.06	0.712	1.00	1.30	0.926	No
297	29.70	1.65	0.68	0.97	0.92	0.752	1.06	0.712	1.00	1.30	0.926	No
298	29.80	1.66	0.68	0.98	0.92	0.752	1.06	0.712	1.00	1.30	0.926	No
299	29.90	1.66	0.68	0.98	0.92	0.753	1.06	0.712	1.00	1.30	0.926	No
300	30.00	1.67	0.69	0.98	0.92	0.753	1.06	0.713	1.00	1.30	0.926	No
301	30.10	1.67	0.69	0.98	0.92	0.753	1.06	0.713	1.00	1.30	0.926	No
302	30.20	1.68	0.69	0.99	0.92	0.753	1.06	0.713	1.00	1.30	0.927	No
303	30.30	1.68	0.70	0.99	0.92	0.753	1.06	0.713	1.00	1.30	0.927	No
304	30.40	1.69	0.70	0.99	0.92	0.753	1.06	0.713	1.00	1.30	0.927	No
305	30.50	1.70	0.70	0.99	0.92	0.753	1.06	0.713	1.00	1.30	0.927	No
306	30.60	1.70	0.71	1.00	0.92	0.753	1.06	0.713	1.00	1.30	0.927	No
307	30.70	1.71	0.71	1.00	0.92	0.753	1.06	0.713	1.00	1.30	0.927	No
308	30.80	1.71	0.71	1.00	0.92	0.753	1.06	0.713	1.00	1.30	0.927	No
309	30.90	1.72	0.71	1.01	0.92	0.753	1.06	0.713	1.00	1.30	0.927	No
310	31.00	1.73	0.72	1.01	0.92	0.753	1.06	0.713	1.00	1.30	0.927	No
311	31.10	1.73	0.72	1.01	0.91	0.753	1.06	0.713	1.00	1.30	0.927	No
312	31.20	1.74	0.72	1.01	0.91	0.753	1.06	0.713	1.00	1.30	0.927	No
313	31.30	1.74	0.73	1.02	0.91	0.753	1.06	0.713	1.00	1.30	0.927	No
314	31.40	1.75	0.73	1.02	0.91	0.753	1.06	0.713	1.00	1.30	0.927	No
315	31.50	1.76	0.73	1.02	0.91	0.753	1.06	0.713	1.00	1.30	2.000	Yes
316	31.60	1.76	0.74	1.03	0.91	0.753	1.06	0.713	1.00	1.30	2.000	Yes
317	31.70	1.77	0.74	1.03	0.91	0.753	1.06	0.713	1.00	1.30	2.000	Yes
318	31.80	1.78	0.74	1.03	0.91	0.753	1.06	0.713	1.00	1.30	2.000	Yes
319	31.90	1.78	0.75	1.04	0.91	0.753	1.06	0.713	1.00	1.30	2.000	Yes
320	32.00	1.79	0.75	1.04	0.91	0.753	1.06	0.713	1.00	1.30	2.000	Yes
321	32.10	1.79	0.75	1.04	0.91	0.753	1.06	0.713	1.00	1.30	2.000	Yes
322	32.20	1.80	0.76	1.04	0.91	0.753	1.06	0.713	1.00	1.30	2.000	Yes
323	32.30	1.81	0.76	1.05	0.91	0.753	1.06	0.713	1.00	1.30	2.000	Yes
324	32.40	1.81	0.76	1.05	0.91	0.753	1.06	0.712	1.00	1.30	2.000	Yes
325	32.50	1.82	0.76	1.05	0.91	0.753	1.06	0.712	1.00	1.30	2.000	Yes
326	32.60	1.82	0.77	1.06	0.91	0.753	1.06	0.712	1.00	1.30	2.000	Yes
327	32.70	1.83	0.77	1.06	0.91	0.752	1.06	0.712	1.00	1.30	2.000	Yes
328	32.80	1.84	0.77	1.06	0.90	0.752	1.06	0.712	1.00	1.30	2.000	Yes
329	32.90	1.84	0.78	1.06	0.90	0.752	1.06	0.712	1.00	1.30	0.926	No
330	33.00	1.85	0.78	1.07	0.90	0.752	1.06	0.712	1.00	1.30	0.926	No
331	33.10	1.85	0.78	1.07	0.90	0.752	1.06	0.712	1.00	1.30	0.926	No
332	33.20	1.86	0.79	1.07	0.90	0.752	1.06	0.712	1.00	1.30	0.926	No
333	33.30	1.87	0.79	1.08	0.90	0.752	1.06	0.712	1.00	1.30	0.925	No
334	33.40	1.87	0.79	1.08	0.90	0.752	1.06	0.712	1.00	1.30	0.925	No
335	33.50	1.88	0.80	1.08	0.90	0.752	1.06	0.712	1.00	1.30	0.925	No
336	33.60	1.88	0.80	1.08	0.90	0.752	1.06	0.711	1.00	1.30	0.925	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
337	33.70	1.89	0.80	1.09	0.90	0.751	1.06	0.711	1.00	1.30	0.925	No
338	33.80	1.90	0.80	1.09	0.90	0.751	1.06	0.711	1.00	1.30	2.000	Yes
339	33.90	1.90	0.81	1.09	0.90	0.751	1.06	0.711	1.00	1.30	2.000	Yes
340	34.00	1.91	0.81	1.10	0.90	0.751	1.06	0.711	1.00	1.30	2.000	Yes
341	34.10	1.91	0.81	1.10	0.90	0.751	1.06	0.710	1.00	1.30	2.000	Yes
342	34.20	1.92	0.82	1.10	0.90	0.750	1.06	0.710	1.00	1.30	2.000	Yes
343	34.30	1.93	0.82	1.11	0.90	0.750	1.06	0.710	1.00	1.30	2.000	Yes
344	34.40	1.93	0.82	1.11	0.89	0.750	1.06	0.710	1.00	1.30	2.000	Yes
345	34.50	1.94	0.83	1.11	0.89	0.749	1.06	0.709	1.00	1.30	2.000	Yes
346	34.60	1.95	0.83	1.12	0.89	0.749	1.06	0.709	1.00	1.30	2.000	Yes
347	34.70	1.95	0.83	1.12	0.89	0.749	1.06	0.709	1.00	1.30	2.000	Yes
348	34.80	1.96	0.84	1.12	0.89	0.748	1.06	0.708	1.00	1.30	2.000	Yes
349	34.90	1.97	0.84	1.13	0.89	0.748	1.06	0.708	1.00	1.30	2.000	Yes
350	35.00	1.97	0.84	1.13	0.89	0.747	1.06	0.708	1.00	1.30	2.000	Yes
351	35.10	1.98	0.85	1.13	0.89	0.747	1.06	0.707	1.00	1.30	0.919	No
352	35.20	1.99	0.85	1.14	0.89	0.747	1.06	0.707	1.00	1.30	2.000	Yes
353	35.30	1.99	0.85	1.14	0.89	0.746	1.06	0.707	1.00	1.30	2.000	Yes
354	35.40	2.00	0.85	1.14	0.89	0.746	1.06	0.706	1.00	1.30	2.000	Yes
355	35.50	2.01	0.86	1.15	0.89	0.746	1.06	0.706	1.00	1.30	2.000	Yes
356	35.60	2.01	0.86	1.15	0.89	0.745	1.06	0.706	1.00	1.30	2.000	Yes
357	35.70	2.02	0.86	1.15	0.89	0.745	1.06	0.705	1.00	1.30	2.000	Yes
358	35.80	2.03	0.87	1.16	0.88	0.745	1.06	0.705	1.00	1.30	2.000	Yes
359	35.90	2.03	0.87	1.16	0.88	0.744	1.06	0.704	1.00	1.30	2.000	Yes
360	36.00	2.04	0.87	1.16	0.88	0.744	1.06	0.704	1.00	1.30	2.000	Yes
361	36.10	2.04	0.88	1.17	0.88	0.743	1.06	0.704	1.00	1.30	2.000	Yes
362	36.20	2.05	0.88	1.17	0.88	0.743	1.06	0.703	1.00	1.30	2.000	Yes
363	36.30	2.06	0.88	1.17	0.88	0.742	1.06	0.703	1.00	1.30	0.914	No
364	36.40	2.06	0.89	1.18	0.88	0.742	1.06	0.702	1.00	1.30	0.913	No
365	36.50	2.07	0.89	1.18	0.88	0.742	1.06	0.702	1.00	1.30	0.913	No
366	36.60	2.08	0.89	1.18	0.88	0.741	1.06	0.702	1.00	1.30	0.912	No
367	36.70	2.08	0.90	1.19	0.88	0.741	1.06	0.701	1.00	1.30	0.912	No
368	36.80	2.09	0.90	1.19	0.88	0.740	1.06	0.701	1.00	1.30	0.911	No
369	36.90	2.10	0.90	1.20	0.88	0.740	1.06	0.700	1.00	1.30	0.910	No
370	37.00	2.10	0.90	1.20	0.88	0.739	1.06	0.700	1.00	1.30	0.910	No
371	37.10	2.11	0.91	1.20	0.88	0.739	1.06	0.699	1.00	1.30	0.909	No
372	37.20	2.12	0.91	1.21	0.87	0.738	1.06	0.699	1.00	1.30	0.909	No
373	37.30	2.12	0.91	1.21	0.87	0.738	1.06	0.699	1.00	1.30	0.908	No
374	37.40	2.13	0.92	1.21	0.87	0.738	1.06	0.698	1.00	1.30	0.908	No
375	37.50	2.14	0.92	1.22	0.87	0.737	1.06	0.698	1.00	1.30	0.907	No
376	37.60	2.14	0.92	1.22	0.87	0.737	1.06	0.697	1.00	1.30	0.906	No
377	37.70	2.15	0.93	1.22	0.87	0.736	1.06	0.697	1.00	1.30	0.906	No
378	37.80	2.16	0.93	1.23	0.87	0.736	1.06	0.696	1.00	1.30	0.905	No
379	37.90	2.16	0.93	1.23	0.87	0.735	1.06	0.696	1.00	1.30	0.905	No
380	38.00	2.17	0.94	1.23	0.87	0.735	1.06	0.695	1.00	1.30	0.904	No
381	38.10	2.17	0.94	1.24	0.87	0.734	1.06	0.695	1.00	1.30	0.903	No
382	38.20	2.18	0.94	1.24	0.87	0.734	1.06	0.694	1.00	1.30	0.903	No
383	38.30	2.19	0.95	1.24	0.87	0.733	1.06	0.694	1.00	1.30	0.902	No
384	38.40	2.19	0.95	1.25	0.86	0.733	1.06	0.694	1.00	1.30	0.902	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
385	38.50	2.20	0.95	1.25	0.86	0.732	1.06	0.693	1.00	1.30	0.901	No
386	38.60	2.21	0.95	1.25	0.86	0.732	1.06	0.693	1.00	1.30	0.900	No
387	38.70	2.21	0.96	1.26	0.86	0.731	1.06	0.692	1.00	1.30	0.900	No
388	38.80	2.22	0.96	1.26	0.86	0.731	1.06	0.692	1.00	1.30	0.899	No
389	38.90	2.23	0.96	1.26	0.86	0.730	1.06	0.691	1.00	1.30	0.899	No
390	39.00	2.23	0.97	1.26	0.86	0.730	1.06	0.691	1.00	1.30	0.898	No
391	39.10	2.24	0.97	1.27	0.86	0.729	1.06	0.690	1.00	1.30	0.897	No
392	39.20	2.24	0.97	1.27	0.86	0.729	1.06	0.690	1.00	1.30	0.897	No
393	39.30	2.25	0.98	1.27	0.86	0.728	1.06	0.689	1.00	1.30	0.896	No
394	39.40	2.26	0.98	1.28	0.86	0.728	1.06	0.689	1.00	1.30	0.896	No
395	39.50	2.26	0.98	1.28	0.86	0.727	1.06	0.688	1.00	1.30	0.895	No
396	39.60	2.27	0.99	1.28	0.85	0.727	1.06	0.688	1.00	1.30	0.894	No
397	39.70	2.28	0.99	1.29	0.85	0.726	1.06	0.687	1.00	1.30	0.894	No
398	39.80	2.28	0.99	1.29	0.85	0.726	1.06	0.687	1.00	1.30	0.893	No
399	39.90	2.29	1.00	1.29	0.85	0.725	1.06	0.686	1.00	1.30	0.892	No
400	40.00	2.29	1.00	1.30	0.85	0.725	1.06	0.686	1.00	1.30	0.892	No
401	40.10	2.30	1.00	1.30	0.85	0.724	1.06	0.685	1.00	1.30	0.891	No
402	40.20	2.31	1.00	1.30	0.85	0.724	1.06	0.685	1.00	1.30	0.890	No
403	40.30	2.31	1.01	1.31	0.85	0.723	1.06	0.684	1.00	1.30	0.890	No
404	40.40	2.32	1.01	1.31	0.85	0.722	1.06	0.684	1.00	1.30	0.889	No
405	40.50	2.33	1.01	1.31	0.85	0.722	1.06	0.683	1.00	1.30	0.888	No
406	40.60	2.33	1.02	1.32	0.85	0.721	1.06	0.683	1.00	1.30	0.888	No
407	40.70	2.34	1.02	1.32	0.84	0.721	1.06	0.682	1.00	1.30	0.887	No
408	40.80	2.35	1.02	1.32	0.84	0.720	1.06	0.682	1.00	1.30	0.886	No
409	40.90	2.35	1.03	1.33	0.84	0.719	1.06	0.681	1.00	1.30	0.885	No
410	41.00	2.36	1.03	1.33	0.84	0.719	1.06	0.681	1.00	1.30	0.885	No
411	41.10	2.36	1.03	1.33	0.84	0.718	1.06	0.680	1.00	1.30	0.884	No
412	41.20	2.37	1.04	1.34	0.84	0.718	1.06	0.679	1.00	1.30	0.883	No
413	41.30	2.38	1.04	1.34	0.84	0.717	1.06	0.679	1.00	1.30	0.882	No
414	41.40	2.38	1.04	1.34	0.84	0.716	1.06	0.678	1.00	1.30	0.881	No
415	41.50	2.39	1.05	1.35	0.84	0.716	1.06	0.677	1.00	1.30	0.881	No
416	41.60	2.40	1.05	1.35	0.84	0.715	1.06	0.677	1.00	1.30	0.880	No
417	41.70	2.40	1.05	1.35	0.84	0.714	1.06	0.676	1.00	1.30	0.879	No
418	41.80	2.41	1.05	1.36	0.83	0.714	1.06	0.676	1.00	1.30	0.878	No
419	41.90	2.42	1.06	1.36	0.83	0.713	1.06	0.675	1.00	1.30	0.877	No
420	42.00	2.42	1.06	1.36	0.83	0.712	1.06	0.674	1.00	1.30	0.876	No
421	42.10	2.43	1.06	1.37	0.83	0.711	1.06	0.674	1.00	1.30	0.876	No
422	42.20	2.44	1.07	1.37	0.83	0.711	1.06	0.673	1.00	1.30	0.875	No
423	42.30	2.44	1.07	1.37	0.83	0.710	1.06	0.672	1.00	1.30	0.874	No
424	42.40	2.45	1.07	1.38	0.83	0.709	1.06	0.672	1.00	1.30	0.873	No
425	42.50	2.46	1.08	1.38	0.83	0.709	1.06	0.671	1.00	1.30	0.872	No
426	42.60	2.46	1.08	1.39	0.83	0.708	1.06	0.670	1.00	1.30	0.871	No
427	42.70	2.47	1.08	1.39	0.83	0.707	1.06	0.669	1.00	1.30	0.870	No
428	42.80	2.48	1.09	1.39	0.83	0.707	1.06	0.669	1.00	1.30	0.869	No
429	42.90	2.48	1.09	1.40	0.82	0.706	1.06	0.668	1.00	1.30	0.869	No
430	43.00	2.49	1.09	1.40	0.82	0.705	1.06	0.667	1.00	1.30	0.868	No
431	43.10	2.50	1.10	1.40	0.82	0.704	1.06	0.667	1.00	1.30	0.867	No
432	43.20	2.50	1.10	1.41	0.82	0.704	1.06	0.666	1.00	1.30	0.866	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
433	43.30	2.51	1.10	1.41	0.82	0.703	1.06	0.665	1.00	1.30	0.865	No
434	43.40	2.52	1.10	1.41	0.82	0.702	1.06	0.665	1.00	1.30	0.864	No
435	43.50	2.52	1.11	1.42	0.82	0.701	1.06	0.664	1.00	1.30	0.863	No
436	43.60	2.53	1.11	1.42	0.82	0.701	1.06	0.663	1.00	1.30	0.862	No
437	43.70	2.54	1.11	1.42	0.82	0.700	1.06	0.663	1.00	1.30	0.861	No
438	43.80	2.54	1.12	1.43	0.82	0.699	1.06	0.662	1.00	1.30	0.861	No
439	43.90	2.55	1.12	1.43	0.81	0.699	1.06	0.661	1.00	1.30	0.860	No
440	44.00	2.56	1.12	1.43	0.81	0.698	1.06	0.661	1.00	1.30	0.859	No
441	44.10	2.56	1.13	1.44	0.81	0.697	1.06	0.660	1.00	1.30	0.858	No
442	44.20	2.57	1.13	1.44	0.81	0.696	1.06	0.659	1.00	1.30	0.857	No
443	44.30	2.58	1.13	1.44	0.81	0.696	1.06	0.659	1.00	1.30	0.856	No
444	44.40	2.58	1.14	1.45	0.81	0.695	1.06	0.658	1.00	1.30	0.855	No
445	44.50	2.59	1.14	1.45	0.81	0.694	1.06	0.657	1.00	1.30	0.855	No
446	44.60	2.59	1.14	1.45	0.81	0.694	1.06	0.657	1.00	1.30	0.854	No
447	44.70	2.60	1.15	1.46	0.81	0.693	1.06	0.656	1.00	1.30	0.853	No
448	44.80	2.61	1.15	1.46	0.81	0.692	1.06	0.655	1.00	1.30	0.852	No
449	44.90	2.61	1.15	1.46	0.80	0.692	1.06	0.655	1.00	1.30	0.851	No
450	45.00	2.62	1.15	1.47	0.80	0.691	1.06	0.654	1.00	1.30	0.850	No
451	45.10	2.63	1.16	1.47	0.80	0.690	1.06	0.654	1.00	1.30	0.850	No
452	45.20	2.63	1.16	1.47	0.80	0.690	1.06	0.653	1.00	1.30	0.849	No
453	45.30	2.64	1.16	1.47	0.80	0.689	1.06	0.652	1.00	1.30	0.848	No
454	45.40	2.64	1.17	1.48	0.80	0.688	1.06	0.652	1.00	1.30	0.847	No
455	45.50	2.65	1.17	1.48	0.80	0.688	1.06	0.651	1.00	1.30	0.846	No
456	45.60	2.66	1.17	1.48	0.80	0.687	1.06	0.650	1.00	1.30	0.845	No
457	45.70	2.66	1.18	1.49	0.80	0.686	1.06	0.650	1.00	1.30	0.844	No
458	45.80	2.67	1.18	1.49	0.80	0.685	1.06	0.649	1.00	1.30	0.843	No
459	45.90	2.68	1.18	1.49	0.79	0.685	1.06	0.648	1.00	1.30	0.843	No
460	46.00	2.68	1.19	1.50	0.79	0.684	1.06	0.647	1.00	1.30	0.842	No
461	46.10	2.69	1.19	1.50	0.79	0.683	1.06	0.647	1.00	1.30	0.841	No
462	46.20	2.70	1.19	1.50	0.79	0.682	1.06	0.646	1.00	1.30	0.840	No
463	46.30	2.70	1.19	1.51	0.79	0.681	1.06	0.645	1.00	1.30	0.839	No
464	46.40	2.71	1.20	1.51	0.79	0.681	1.06	0.644	1.00	1.30	0.838	No
465	46.50	2.72	1.20	1.52	0.79	0.680	1.06	0.644	1.00	1.30	0.837	No
466	46.60	2.72	1.20	1.52	0.79	0.679	1.06	0.643	1.00	1.30	0.836	No
467	46.70	2.73	1.21	1.52	0.79	0.678	1.06	0.642	1.00	1.30	0.835	No
468	46.80	2.74	1.21	1.53	0.79	0.677	1.06	0.641	1.00	1.30	0.834	No
469	46.90	2.74	1.21	1.53	0.78	0.677	1.06	0.641	1.00	1.30	0.833	No
470	47.00	2.75	1.22	1.53	0.78	0.676	1.06	0.640	1.00	1.30	0.832	No
471	47.10	2.76	1.22	1.54	0.78	0.675	1.06	0.639	1.00	1.30	0.831	No
472	47.20	2.76	1.22	1.54	0.78	0.674	1.06	0.638	1.00	1.30	0.830	No
473	47.30	2.77	1.23	1.54	0.78	0.673	1.06	0.637	1.00	1.30	0.829	No
474	47.40	2.78	1.23	1.55	0.78	0.673	1.06	0.637	1.00	1.30	0.828	No
475	47.50	2.78	1.23	1.55	0.78	0.672	1.06	0.636	1.00	1.30	0.827	No
476	47.60	2.79	1.24	1.55	0.78	0.671	1.06	0.635	1.00	1.30	0.826	No
477	47.70	2.80	1.24	1.56	0.78	0.670	1.06	0.634	1.00	1.30	0.825	No
478	47.80	2.80	1.24	1.56	0.78	0.669	1.06	0.634	1.00	1.30	0.824	No
479	47.90	2.81	1.24	1.57	0.77	0.669	1.06	0.633	1.00	1.30	0.823	No
480	48.00	2.82	1.25	1.57	0.77	0.668	1.06	0.632	1.00	1.30	0.822	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
481	48.10	2.82	1.25	1.57	0.77	0.667	1.06	0.631	1.00	1.30	0.821	No
482	48.20	2.83	1.25	1.58	0.77	0.666	1.06	0.631	1.00	1.30	0.820	No
483	48.30	2.84	1.26	1.58	0.77	0.665	1.06	0.630	1.00	1.30	0.819	No
484	48.40	2.84	1.26	1.58	0.77	0.665	1.06	0.629	1.00	1.30	0.818	No
485	48.50	2.85	1.26	1.59	0.77	0.664	1.06	0.628	1.00	1.30	0.817	No
486	48.60	2.86	1.27	1.59	0.77	0.663	1.06	0.627	1.00	1.30	0.816	No
487	48.70	2.86	1.27	1.59	0.77	0.662	1.06	0.627	1.00	1.30	0.815	No
488	48.80	2.87	1.27	1.60	0.76	0.661	1.06	0.626	1.00	1.30	0.814	No
489	48.90	2.88	1.28	1.60	0.76	0.660	1.06	0.625	1.00	1.30	0.813	No
490	49.00	2.88	1.28	1.60	0.76	0.660	1.06	0.624	1.00	1.30	0.812	No
491	49.10	2.89	1.28	1.61	0.76	0.659	1.06	0.624	1.00	1.30	0.811	No
492	49.20	2.90	1.29	1.61	0.76	0.658	1.06	0.623	1.00	1.30	0.810	No
493	49.30	2.90	1.29	1.62	0.76	0.657	1.06	0.622	1.00	1.30	0.809	No
494	49.40	2.91	1.29	1.62	0.76	0.656	1.06	0.621	1.00	1.30	0.807	No
495	49.50	2.92	1.29	1.62	0.76	0.655	1.06	0.620	1.00	1.30	0.806	No
496	49.60	2.92	1.30	1.63	0.76	0.654	1.06	0.620	1.00	1.30	0.805	No
497	49.70	2.93	1.30	1.63	0.76	0.654	1.06	0.619	1.00	1.30	0.804	No

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
 σ_v : Total overburden pressure at test point (tsf)
 u_0 : Water pressure at test point (tsf)
 σ_v' : Effective overburden pressure based on GWT during earthquake (tsf)
 r_d : Nonlinear shear mass factor
 CSR: Cyclic Stress Ratio
 MSF: Magnitude Scaling Factor
 CSR_{eq}: CSR adjusted for M=7.5
 K_σ : Effective overburden stress factor
 CSR*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::												
Point ID	Depth (ft)	q _t (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1	0.10	52.54	2.03	1.52	0.63	99.31	1.34	132.89	4.000	No	No	2.00
2	0.20	61.37	1.98	1.50	0.61	115.98	1.29	149.82	4.000	No	No	2.00
3	0.30	71.19	1.94	1.52	0.59	134.53	1.26	169.99	4.000	No	No	2.00
4	0.40	75.74	1.94	1.60	0.59	143.12	1.26	180.64	4.000	No	No	2.00
5	0.50	75.24	1.97	1.76	0.60	142.16	1.28	182.50	4.000	No	No	2.00
6	0.60	73.40	2.00	1.91	0.62	138.67	1.31	181.81	4.000	No	No	2.00
7	0.70	71.59	2.03	2.01	0.62	135.24	1.33	180.18	4.000	No	No	2.00
8	0.80	69.27	2.03	1.94	0.62	130.83	1.33	174.09	4.000	No	No	2.00
9	0.90	65.76	2.00	1.72	0.62	124.19	1.31	162.62	4.000	No	No	2.00
10	1.00	61.48	1.98	1.51	0.61	116.10	1.29	150.16	4.000	No	No	2.00
11	1.10	57.86	1.98	1.41	0.61	109.23	1.29	141.21	4.000	No	No	2.00
12	1.20	55.98	2.00	1.45	0.62	105.67	1.31	138.17	4.000	No	No	2.00
13	1.30	55.88	1.99	1.41	0.61	105.48	1.30	137.29	4.000	No	No	2.00
14	1.40	56.48	1.96	1.30	0.60	106.59	1.28	136.42	4.000	No	No	2.00
15	1.50	56.65	1.93	1.17	0.59	106.91	1.26	134.53	4.000	No	No	2.00
16	1.60	56.56	1.92	1.14	0.59	106.73	1.25	133.75	4.000	No	No	2.00
17	1.70	56.82	1.96	1.28	0.60	107.21	1.28	136.80	4.000	No	No	2.00
18	1.80	57.51	2.01	1.52	0.62	108.50	1.31	142.37	4.000	No	No	2.00
19	1.90	57.98	2.05	1.76	0.64	109.38	1.35	148.06	4.000	No	No	2.00
20	2.00	57.09	2.09	2.00	0.65	107.68	1.41	151.68	4.000	No	No	2.00
21	2.10	56.39	2.14	2.27	0.67	106.34	1.48	157.28	4.000	No	No	2.00
22	2.20	57.47	2.17	2.56	0.68	108.37	1.55	167.55	4.000	No	No	2.00
23	2.30	59.29	2.18	2.72	0.69	111.81	1.57	175.63	4.000	No	No	2.00
24	2.40	58.41	2.19	2.76	0.69	110.13	1.59	175.07	4.000	Yes	No	2.00
25	2.50	52.87	2.22	2.78	0.70	99.64	1.67	166.32	4.000	Yes	No	2.00
26	2.60	44.67	2.29	2.93	0.73	84.15	1.88	158.20	4.000	Yes	No	2.00
27	2.70	36.23	2.39	3.27	0.77	68.17	2.30	156.59	4.000	Yes	No	2.00
28	2.80	29.26	2.49	3.70	0.81	54.98	2.90	159.28	4.000	Yes	No	2.00
29	2.90	24.02	2.58	4.13	0.84	45.07	4.83	217.87	4.000	Yes	No	2.00
30	3.00	20.23	2.66	4.50	0.87	37.90	8.03	304.37	4.000	Yes	No	2.00
31	3.10	17.19	2.73	4.72	0.90	32.14	5.00	160.83	4.000	Yes	Yes	2.00
32	3.20	14.86	2.77	4.72	0.92	27.73	5.54	153.60	4.000	Yes	Yes	2.00
33	3.30	13.57	2.79	4.54	0.92	25.27	5.76	145.45	4.000	No	Yes	2.00
34	3.40	12.90	2.79	4.32	0.92	24.00	5.78	138.77	4.000	No	Yes	2.00
35	3.50	12.42	2.79	4.11	0.92	23.09	5.77	133.19	4.000	No	Yes	2.00
36	3.60	11.77	2.80	3.91	0.93	21.84	5.82	127.05	4.000	No	Yes	2.00
37	3.70	11.18	2.80	3.70	0.93	20.72	5.85	121.10	4.000	No	Yes	2.00
38	3.80	10.81	2.79	3.49	0.93	20.01	5.79	115.82	4.000	No	Yes	2.00
39	3.90	10.67	2.78	3.28	0.92	19.74	5.64	111.25	4.000	No	Yes	2.00
40	4.00	10.67	2.76	3.06	0.91	19.72	5.41	106.79	4.000	No	Yes	2.00
41	4.10	10.67	2.75	2.92	0.91	19.71	5.27	103.89	4.000	No	Yes	2.00
42	4.20	10.67	2.75	2.88	0.91	19.70	5.24	103.20	4.000	No	Yes	2.00
43	4.30	10.67	2.75	2.91	0.91	19.69	5.26	103.67	4.000	No	Yes	2.00
44	4.40	10.91	2.75	2.95	0.91	20.13	5.22	105.06	4.000	No	Yes	2.00
45	4.50	11.61	2.73	3.00	0.90	21.45	5.03	107.92	4.000	No	Yes	2.00
46	4.60	12.40	2.71	3.07	0.90	22.94	4.85	111.34	4.000	No	Yes	2.00
47	4.70	12.96	2.71	3.20	0.90	23.99	4.81	115.45	4.000	No	Yes	2.00
48	4.80	13.50	2.72	3.42	0.90	24.99	4.87	121.62	4.000	Yes	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _t (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
49	4.90	15.92	2.68	3.72	0.89	29.55	9.19	271.63	4.000	Yes	No	2.00
50	5.00	21.14	2.59	3.65	0.85	39.41	4.97	195.79	4.000	Yes	No	2.00
51	5.10	28.44	2.46	3.25	0.80	53.19	2.70	143.86	4.000	Yes	No	2.00
52	5.20	35.19	2.33	2.68	0.75	65.93	2.06	135.60	4.000	Yes	No	2.00
53	5.30	39.84	2.23	2.16	0.71	74.72	1.69	126.16	4.000	Yes	No	2.00
54	5.40	42.91	2.16	1.85	0.69	80.52	1.52	122.49	4.000	Yes	No	2.00
55	5.50	46.06	2.12	1.77	0.67	86.45	1.46	125.82	4.000	Yes	No	2.00
56	5.60	50.27	2.10	1.83	0.67	94.40	1.43	134.63	4.000	No	No	2.00
57	5.70	54.79	2.08	1.84	0.66	102.93	1.39	143.31	4.000	No	No	2.00
58	5.80	58.08	2.05	1.79	0.65	109.14	1.36	148.30	4.000	No	No	2.00
59	5.90	58.83	2.04	1.72	0.64	110.56	1.34	148.38	4.000	No	No	2.00
60	6.00	57.29	2.05	1.72	0.65	107.63	1.35	145.34	4.000	No	No	2.00
61	6.10	55.12	2.07	1.78	0.66	103.52	1.38	142.51	4.000	No	No	2.00
62	6.20	53.71	2.09	1.85	0.66	100.84	1.40	141.50	4.000	No	No	2.00
63	6.30	53.23	2.09	1.87	0.67	99.92	1.41	140.97	4.000	No	No	2.00
64	6.40	52.58	2.10	1.87	0.67	98.66	1.42	139.69	4.000	No	No	2.00
65	6.50	51.24	2.11	1.87	0.67	95.51	1.43	136.61	4.000	No	No	2.00
66	6.60	49.76	2.12	1.88	0.68	92.26	1.45	133.92	4.000	No	No	2.00
67	6.70	48.27	2.14	1.90	0.68	89.06	1.48	131.53	4.000	No	No	2.00
68	6.80	46.37	2.15	1.93	0.69	85.23	1.51	128.73	4.000	No	No	2.00
69	6.90	43.90	2.17	1.95	0.70	80.47	1.55	125.10	4.000	No	No	2.00
70	7.00	41.42	2.19	1.96	0.71	75.68	1.60	121.15	4.000	No	No	2.00
71	7.10	39.39	2.21	1.93	0.71	71.59	1.64	117.05	4.000	No	No	2.00
72	7.20	36.94	2.23	1.93	0.72	66.93	1.69	113.30	4.000	No	No	2.00
73	7.30	33.77	2.27	2.02	0.74	61.39	1.82	111.80	4.000	No	No	2.00
74	7.40	30.59	2.33	2.22	0.76	56.04	2.03	113.86	4.000	No	No	2.00
75	7.50	28.99	2.36	2.38	0.77	53.21	2.20	116.98	4.000	No	No	2.00
76	7.60	28.89	2.37	2.37	0.77	52.54	2.21	116.13	4.000	No	No	2.00
77	7.70	29.43	2.35	2.22	0.77	52.67	2.12	111.66	4.000	No	No	2.00
78	7.80	30.02	2.32	2.05	0.76	52.84	2.02	106.66	4.000	No	No	2.00
79	7.90	30.81	2.30	1.93	0.75	53.39	1.94	103.32	4.000	No	No	2.00
80	8.00	31.60	2.29	1.85	0.74	53.97	1.88	101.38	4.000	No	No	2.00
81	8.10	32.01	2.27	1.78	0.74	54.24	1.83	99.49	0.172	No	No	0.29
82	8.20	32.01	2.27	1.77	0.74	54.02	1.83	99.05	0.170	No	No	0.29
83	8.30	32.01	2.28	1.79	0.74	53.87	1.85	99.63	0.172	No	No	0.29
84	8.40	32.01	2.28	1.82	0.74	53.73	1.87	100.35	0.174	No	No	0.29
85	8.50	31.59	2.29	1.81	0.74	52.85	1.88	99.39	0.171	No	No	0.29
86	8.60	30.13	2.30	1.78	0.75	50.34	1.92	96.76	4.000	Yes	No	2.00
87	8.70	26.66	2.34	1.81	0.77	44.83	2.10	94.10	4.000	Yes	No	2.00
88	8.80	21.40	2.44	1.98	0.80	36.66	2.57	94.17	4.000	Yes	No	2.00
89	8.90	15.52	2.58	2.35	0.86	27.38	4.77	130.69	4.000	Yes	No	2.00
90	9.00	11.03	2.75	2.98	0.92	19.86	5.31	105.48	4.000	Yes	Yes	2.00
91	9.10	8.41	2.92	3.79	0.98	14.90	7.46	111.19	4.000	Yes	Yes	2.00
92	9.20	7.29	3.02	4.55	1.00	12.77	9.11	116.38	0.609	No	Yes	0.98
93	9.30	7.11	3.05	5.01	1.00	12.41	9.75	121.03	0.592	No	Yes	0.94
94	9.40	7.15	3.05	4.99	1.00	12.48	9.70	121.03	0.595	No	Yes	0.94
95	9.50	7.05	3.05	4.80	1.00	12.28	9.60	117.92	0.586	No	Yes	0.92
96	9.60	6.68	3.06	4.75	1.00	11.58	9.92	114.87	0.552	No	Yes	0.87

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
97	9.70	7.58	3.03	4.90	1.00	13.26	9.25	122.59	0.632	No	Yes	0.99
98	9.80	9.92	2.93	4.88	0.99	17.67	7.65	135.12	0.843	No	Yes	1.31
99	9.90	10.58	2.90	4.76	0.98	18.92	7.20	136.29	0.902	No	Yes	1.40
100	10.00	9.12	2.94	4.60	1.00	16.15	7.85	126.77	0.770	No	Yes	1.19
101	10.10	6.33	3.07	4.47	1.00	10.86	10.04	108.97	0.518	No	Yes	0.79
102	10.20	4.77	3.18	4.43	1.00	7.90	12.24	96.67	0.377	No	Yes	0.57
103	10.30	4.05	3.24	4.32	1.00	6.53	13.65	89.12	0.311	No	Yes	0.47
104	10.40	3.45	3.30	4.13	1.00	5.40	15.09	81.42	0.257	No	Yes	0.39
105	10.50	3.55	3.27	3.81	1.00	5.56	14.31	79.63	0.265	No	Yes	0.40
106	10.60	4.00	3.19	3.48	1.00	6.41	12.57	80.62	0.306	No	Yes	0.46
107	10.70	4.52	3.13	3.32	1.00	7.39	11.23	82.95	0.352	No	Yes	0.53
108	10.80	4.74	3.11	3.36	1.00	7.77	10.90	84.78	0.371	No	Yes	0.55
109	10.90	4.74	3.12	3.45	1.00	7.74	11.08	85.75	0.369	No	Yes	0.55
110	11.00	4.74	3.12	3.42	1.00	7.70	11.07	85.22	0.367	No	Yes	0.54
111	11.10	4.74	3.11	3.18	1.00	7.67	10.74	82.33	0.366	No	Yes	0.54
112	11.20	4.74	3.09	2.89	1.00	7.63	10.34	78.87	0.364	No	Yes	0.53
113	11.30	4.74	3.07	2.73	1.00	7.60	10.11	76.79	0.362	No	Yes	0.53
114	11.40	4.74	3.08	2.73	1.00	7.56	10.14	76.71	0.361	No	Yes	0.52
115	11.50	4.74	3.09	2.90	1.00	7.53	10.45	78.67	0.359	No	Yes	0.52
116	11.60	4.74	3.12	3.21	1.00	7.49	10.95	82.04	0.357	No	Yes	0.51
117	11.70	4.74	3.14	3.53	1.00	7.46	11.46	85.49	0.356	No	Yes	0.51
118	11.80	4.74	3.16	3.76	1.00	7.42	11.83	87.84	0.354	No	Yes	0.50
119	11.90	4.74	3.16	3.80	1.00	7.39	11.92	88.08	0.352	No	Yes	0.50
120	12.00	4.74	3.16	3.69	1.00	7.36	11.80	86.83	0.351	No	Yes	0.50
121	12.10	4.74	3.15	3.59	1.00	7.32	11.69	85.58	0.349	No	Yes	0.49
122	12.20	4.96	3.14	3.60	1.00	7.67	11.35	87.05	0.366	No	Yes	0.51
123	12.30	5.67	3.10	3.80	1.00	8.92	10.54	94.00	0.425	No	Yes	0.59
124	12.40	6.56	3.06	4.17	1.00	10.46	9.94	103.89	0.499	No	Yes	0.69
125	12.50	7.40	3.05	4.61	1.00	11.89	9.61	114.26	0.567	No	Yes	0.79
126	12.60	7.87	3.05	5.03	1.00	12.67	9.65	122.25	0.604	No	Yes	0.84
127	12.70	8.25	3.05	5.29	1.00	13.28	9.61	127.62	0.633	No	Yes	0.87
128	12.80	8.33	3.05	5.39	1.00	13.37	9.67	129.20	0.638	No	Yes	0.88
129	12.90	7.75	3.08	5.36	1.00	12.28	10.17	124.86	0.586	No	Yes	0.80
130	13.00	7.10	3.11	5.26	1.00	11.10	10.73	119.06	0.529	No	Yes	0.72
131	13.10	6.84	3.12	5.26	1.00	10.58	11.05	116.97	0.505	No	Yes	0.69
132	13.20	7.20	3.11	5.42	1.00	11.16	10.85	121.15	0.532	No	Yes	0.72
133	13.30	7.57	3.10	5.48	1.00	11.74	10.58	124.24	0.560	No	Yes	0.76
134	13.40	7.08	3.12	5.34	1.00	10.84	10.98	119.02	0.517	No	Yes	0.70
135	13.50	5.94	3.17	5.00	1.00	8.85	12.06	106.77	0.422	No	Yes	0.57
136	13.60	4.62	3.25	4.52	1.00	6.57	13.88	91.14	0.313	No	Yes	0.42
137	13.70	3.90	3.29	4.00	1.00	5.32	15.03	79.92	0.254	No	Yes	0.34
138	13.80	3.75	3.29	3.56	1.00	5.04	14.82	74.67	0.240	No	Yes	0.32
139	13.90	3.99	3.24	3.31	1.00	5.43	13.72	74.43	0.259	No	Yes	0.34
140	14.00	4.43	3.20	3.36	1.00	6.14	12.73	78.17	0.293	No	Yes	0.39
141	14.10	4.88	3.17	3.56	1.00	6.87	12.13	83.37	0.328	No	Yes	0.43
142	14.20	4.97	3.18	3.74	1.00	6.99	12.27	85.77	0.334	No	Yes	0.44
143	14.30	5.01	3.18	3.80	1.00	7.02	12.33	86.52	0.335	No	Yes	0.44
144	14.40	4.97	3.18	3.77	1.00	6.92	12.39	85.77	0.330	No	Yes	0.43

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
145	14.50	5.03	3.18	3.75	1.00	6.99	12.27	85.83	0.334	No	Yes	0.44
146	14.60	5.16	3.17	3.80	1.00	7.18	12.14	87.21	0.343	No	Yes	0.45
147	14.70	5.69	3.15	3.97	1.00	8.02	11.53	92.49	0.383	No	Yes	0.50
148	14.80	6.80	3.09	4.29	1.00	9.80	10.50	102.97	0.468	No	Yes	0.60
149	14.90	7.83	3.06	4.68	1.00	11.44	9.93	113.58	0.546	No	Yes	0.70
150	15.00	8.56	3.05	5.07	1.00	12.58	9.73	122.43	0.600	No	Yes	0.77
151	15.10	9.66	3.03	5.35	1.00	14.29	9.23	131.93	0.682	No	Yes	0.88
152	15.20	12.13	2.95	5.39	1.00	18.22	7.94	144.57	0.869	No	Yes	1.11
153	15.30	16.06	2.85	5.18	0.96	24.00	6.47	155.26	1.145	No	Yes	1.46
154	15.40	17.85	2.80	4.91	0.95	26.45	5.86	155.04	1.261	No	Yes	1.61
155	15.50	18.07	2.78	4.61	0.94	26.56	5.62	149.18	1.267	No	Yes	1.61
156	15.60	19.86	2.73	4.20	0.92	28.90	4.99	144.22	1.378	No	Yes	1.75
157	15.70	24.13	2.63	3.69	0.88	34.60	6.59	228.19	3.600	No	No	2.00
158	15.80	27.78	2.54	3.12	0.85	39.20	3.71	145.43	0.366	No	No	0.46
159	15.90	26.70	2.51	2.66	0.84	37.25	3.04	113.31	0.215	No	No	0.27
160	16.00	21.89	2.57	2.54	0.86	30.53	4.33	132.13	0.295	No	No	0.37
161	16.10	16.23	2.71	2.98	0.91	22.82	4.79	109.24	1.089	No	Yes	1.37
162	16.20	11.85	2.89	3.94	0.98	16.80	7.01	117.79	0.801	No	Yes	1.00
163	16.30	10.16	3.01	4.98	1.00	14.29	8.88	126.88	0.681	No	Yes	0.85
164	16.40	9.88	3.05	5.57	1.00	13.79	9.64	132.99	0.658	No	Yes	0.82
165	16.50	9.52	3.07	5.67	1.00	13.18	10.01	131.99	0.629	No	Yes	0.78
166	16.60	9.04	3.07	5.36	1.00	12.38	10.11	125.22	0.591	No	Yes	0.73
167	16.70	8.54	3.07	4.90	1.00	11.57	10.08	116.69	0.552	No	Yes	0.68
168	16.80	8.24	3.07	4.65	1.00	11.07	10.10	111.84	0.528	No	Yes	0.65
169	16.90	7.44	3.11	4.64	1.00	9.83	10.89	107.02	0.469	No	Yes	0.58
170	17.00	6.60	3.17	4.75	1.00	8.52	12.06	102.76	0.406	No	Yes	0.50
171	17.10	5.74	3.23	4.79	1.00	7.20	13.46	96.84	0.343	No	Yes	0.42
172	17.20	5.29	3.26	4.57	1.00	6.49	14.05	91.17	0.310	No	Yes	0.38
173	17.30	5.07	3.25	4.11	1.00	6.14	13.89	85.25	0.293	No	Yes	0.36
174	17.40	4.98	3.22	3.54	1.00	5.97	13.26	79.16	0.285	No	Yes	0.35
175	17.50	4.83	3.20	2.99	1.00	5.72	12.70	72.67	0.273	No	Yes	0.33
176	17.60	4.34	3.22	2.60	1.00	4.98	13.17	65.53	0.237	No	Yes	0.29
177	17.70	3.81	3.27	2.44	1.00	4.18	14.44	60.34	0.199	No	Yes	0.24
178	17.80	3.52	3.31	2.43	1.00	3.74	15.50	57.97	0.178	No	Yes	0.22
179	17.90	3.85	3.27	2.46	1.00	4.20	14.42	60.62	0.200	No	Yes	0.24
180	18.00	4.37	3.22	2.54	1.00	4.96	13.09	64.89	0.236	No	Yes	0.28
181	18.10	4.60	3.22	2.82	1.00	5.28	13.09	69.07	0.252	No	Yes	0.30
182	18.20	4.80	3.23	3.29	1.00	5.54	13.50	74.74	0.264	No	Yes	0.32
183	18.30	5.19	3.24	3.88	1.00	6.09	13.62	82.93	0.291	No	Yes	0.35
184	18.40	5.70	3.23	4.39	1.00	6.79	13.41	91.12	0.324	No	Yes	0.39
185	18.50	5.93	3.24	4.95	1.00	7.10	13.76	97.74	0.339	No	Yes	0.40
186	18.60	5.93	3.27	5.48	1.00	7.07	14.45	102.22	0.337	No	Yes	0.40
187	18.70	5.93	3.29	5.86	1.00	7.04	14.94	105.25	0.336	No	Yes	0.40
188	18.80	5.93	3.30	6.02	1.00	7.02	15.16	106.33	0.335	No	Yes	0.40
189	18.90	5.93	3.30	5.93	1.00	6.99	15.09	105.44	0.333	No	Yes	0.39
190	19.00	6.05	3.28	5.73	1.00	7.12	14.69	104.64	0.340	No	Yes	0.40
191	19.10	6.40	3.26	5.67	1.00	7.59	14.05	106.71	0.362	No	Yes	0.43
192	19.20	6.98	3.22	5.73	1.00	8.38	13.31	111.49	0.400	No	Yes	0.47

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
193	19.30	7.65	3.19	5.69	1.00	9.29	12.45	115.67	0.443	No	Yes	0.52
194	19.40	8.11	3.16	5.54	1.00	9.90	11.82	117.04	0.472	No	Yes	0.56
195	19.50	8.46	3.13	5.32	1.00	10.36	11.27	116.72	0.494	No	Yes	0.58
196	19.60	8.38	3.13	5.13	1.00	10.20	11.18	113.99	0.486	No	Yes	0.57
197	19.70	8.40	3.12	4.98	1.00	10.19	11.02	112.26	0.486	No	Yes	0.57
198	19.80	9.32	3.07	4.84	1.00	11.43	10.10	115.49	0.545	No	Yes	0.64
199	19.90	10.07	3.04	4.82	1.00	12.42	9.55	118.65	0.592	No	Yes	0.69
200	20.00	9.83	3.06	4.93	1.00	12.05	9.86	118.78	0.575	No	Yes	0.67
201	20.10	8.12	3.15	5.20	1.00	9.65	11.65	112.39	0.460	No	Yes	0.54
202	20.20	6.67	3.25	5.68	1.00	7.62	14.04	107.02	0.364	No	Yes	0.42
203	20.30	6.07	3.31	6.08	1.00	6.77	15.55	105.35	0.323	No	Yes	0.37
204	20.40	5.77	3.35	6.30	1.00	6.33	16.46	104.19	0.302	No	Yes	0.35
205	20.50	5.38	3.38	6.31	1.00	5.78	17.38	100.44	0.276	No	Yes	0.32
206	20.60	4.98	3.40	5.93	1.00	5.22	17.98	93.85	0.249	No	Yes	0.29
207	20.70	4.75	3.39	5.28	1.00	4.88	17.80	86.94	0.233	No	Yes	0.27
208	20.80	4.74	3.36	4.63	1.00	4.85	16.91	82.10	0.232	No	Yes	0.27
209	20.90	4.86	3.33	4.25	1.00	4.99	16.05	80.08	0.238	No	Yes	0.27
210	21.00	5.42	3.28	4.27	1.00	5.72	14.76	84.44	0.273	No	Yes	0.31
211	21.10	6.27	3.24	4.64	1.00	6.84	13.69	93.64	0.326	No	Yes	0.37
212	21.20	6.95	3.22	4.99	1.00	7.71	13.12	101.21	0.368	No	Yes	0.42
213	21.30	7.20	3.21	5.19	1.00	8.02	13.05	104.65	0.383	No	Yes	0.44
214	21.40	7.31	3.21	5.24	1.00	8.14	12.99	105.76	0.388	No	Yes	0.44
215	21.50	7.92	3.18	5.33	1.00	8.91	12.38	110.30	0.425	No	Yes	0.48
216	21.60	9.40	3.12	5.42	1.00	10.82	11.06	119.72	0.516	No	Yes	0.59
217	21.70	11.65	3.03	5.18	1.00	13.73	9.30	127.74	0.655	No	Yes	0.74
218	21.80	14.83	2.91	4.53	0.99	17.80	7.30	129.88	0.849	No	Yes	0.96
219	21.90	18.05	2.78	3.67	0.95	21.59	5.65	121.93	1.030	No	Yes	1.17
220	22.00	20.60	2.68	2.91	0.91	24.47	8.85	216.54	3.600	No	No	2.00
221	22.10	21.70	2.62	2.49	0.88	25.59	6.15	157.53	0.399	No	No	0.45
222	22.20	21.51	2.63	2.50	0.89	25.30	6.36	160.86	0.420	No	No	0.48
223	22.30	20.65	2.68	2.87	0.91	24.29	8.76	212.67	3.600	No	No	2.00
224	22.40	19.82	2.74	3.39	0.93	23.33	5.09	118.80	1.113	No	Yes	1.26
225	22.50	19.24	2.79	4.00	0.95	22.68	5.75	130.33	1.082	No	Yes	1.22
226	22.60	19.38	2.84	4.72	0.97	22.88	6.31	144.45	1.091	No	Yes	1.23
227	22.70	21.44	2.84	5.37	0.97	25.41	6.37	161.91	1.212	No	Yes	1.36
228	22.80	25.94	2.78	5.45	0.95	30.77	5.66	174.25	1.468	No	Yes	1.65
229	22.90	32.18	2.69	4.94	0.91	37.99	9.56	363.33	3.600	No	No	2.00
230	23.00	37.11	2.59	4.06	0.87	43.42	5.02	217.91	4.000	No	No	2.00
231	23.10	38.48	2.51	3.26	0.85	44.58	3.07	136.81	0.318	No	No	0.36
232	23.20	35.78	2.50	2.83	0.84	41.14	2.96	121.84	0.248	No	No	0.28
233	23.30	30.27	2.56	2.91	0.86	34.70	4.21	145.91	0.369	No	No	0.41
234	23.40	24.07	2.68	3.43	0.91	27.54	9.20	253.25	3.600	No	No	2.00
235	23.50	18.71	2.81	4.03	0.96	21.26	6.04	128.36	1.014	No	Yes	1.13
236	23.60	14.66	2.94	4.59	1.00	16.44	7.75	127.45	0.784	No	Yes	0.88
237	23.70	11.82	3.03	4.84	1.00	12.90	9.35	120.59	0.615	No	Yes	0.69
238	23.80	9.79	3.10	4.71	1.00	10.37	10.60	109.99	0.495	No	Yes	0.55
239	23.90	8.76	3.12	4.34	1.00	9.08	11.09	100.73	0.433	No	Yes	0.48
240	24.00	8.87	3.11	4.16	1.00	9.18	10.79	99.13	0.438	No	Yes	0.49

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
241	24.10	9.46	3.09	4.29	1.00	9.86	10.47	103.24	0.471	No	Yes	0.52
242	24.20	10.14	3.08	4.61	1.00	10.66	10.31	109.87	0.508	No	Yes	0.56
243	24.30	10.42	3.09	4.95	1.00	10.96	10.50	115.03	0.523	No	Yes	0.58
244	24.40	10.44	3.11	5.23	1.00	10.93	10.81	118.15	0.522	No	Yes	0.58
245	24.50	10.20	3.13	5.44	1.00	10.61	11.23	119.08	0.506	No	Yes	0.56
246	24.60	9.62	3.16	5.61	1.00	9.89	11.91	117.72	0.472	No	Yes	0.52
247	24.70	9.03	3.19	5.73	1.00	9.15	12.61	115.38	0.436	No	Yes	0.48
248	24.80	8.52	3.22	5.78	1.00	8.51	13.24	112.62	0.406	No	Yes	0.45
249	24.90	8.30	3.23	5.70	1.00	8.22	13.43	110.39	0.392	No	Yes	0.43
250	25.00	8.30	3.22	5.54	1.00	8.18	13.29	108.74	0.390	No	Yes	0.43
251	25.10	7.91	3.24	5.45	1.00	7.70	13.68	105.37	0.368	No	Yes	0.40
252	25.20	7.42	3.26	5.37	1.00	7.10	14.28	101.43	0.339	No	Yes	0.37
253	25.30	7.65	3.24	5.12	1.00	7.34	13.70	100.49	0.350	No	Yes	0.38
254	25.40	8.44	3.19	4.84	1.00	8.24	12.41	102.35	0.393	No	Yes	0.43
255	25.50	9.09	3.15	4.79	1.00	8.97	11.72	105.07	0.428	No	Yes	0.47
256	25.60	8.99	3.17	5.06	1.00	8.82	12.15	107.19	0.421	No	Yes	0.46
257	25.70	8.59	3.22	5.55	1.00	8.33	13.16	109.64	0.398	No	Yes	0.44
258	25.80	8.74	3.23	5.89	1.00	8.48	13.39	113.49	0.404	No	Yes	0.44
259	25.90	9.74	3.18	5.79	1.00	9.60	12.32	118.19	0.458	No	Yes	0.50
260	26.00	12.20	3.07	5.30	1.00	12.39	10.05	124.53	0.591	No	Yes	0.65
261	26.10	14.90	2.97	4.79	1.00	15.45	8.26	127.68	0.737	No	Yes	0.81
262	26.20	16.97	2.90	4.39	1.00	17.75	7.19	127.57	0.847	No	Yes	0.93
263	26.30	18.58	2.86	4.23	0.98	19.47	6.60	128.59	0.929	No	Yes	1.01
264	26.40	20.32	2.84	4.41	0.97	21.35	6.35	135.65	1.019	No	Yes	1.11
265	26.50	21.81	2.84	4.82	0.97	22.96	6.38	146.44	1.095	No	Yes	1.19
266	26.60	21.82	2.87	5.26	0.98	22.94	6.73	154.29	1.094	No	Yes	1.19
267	26.70	20.10	2.91	5.59	1.00	20.99	7.40	155.21	1.001	No	Yes	1.09
268	26.80	17.84	2.97	5.82	1.00	18.38	8.24	151.54	0.877	No	Yes	0.95
269	26.90	16.12	3.01	6.02	1.00	16.39	9.03	147.95	0.782	No	Yes	0.85
270	27.00	16.24	3.02	6.12	1.00	16.47	9.08	149.51	0.785	No	Yes	0.85
271	27.10	18.29	2.97	6.05	1.00	18.69	8.34	155.81	0.891	No	Yes	0.97
272	27.20	21.53	2.91	5.86	1.00	22.23	7.33	162.90	1.060	No	Yes	1.15
273	27.30	25.33	2.84	5.54	0.97	26.24	6.36	166.84	1.252	No	Yes	1.36
274	27.40	28.68	2.78	5.11	0.95	29.72	5.56	165.22	1.418	No	Yes	1.54
275	27.50	30.57	2.73	4.69	0.93	31.61	5.04	159.41	1.508	No	Yes	1.64
276	27.60	30.71	2.71	4.42	0.93	31.63	4.84	153.17	1.509	No	Yes	1.64
277	27.70	29.52	2.72	4.32	0.93	30.25	4.92	148.96	1.443	No	Yes	1.57
278	27.80	28.15	2.74	4.36	0.94	28.72	5.14	147.60	1.370	No	Yes	1.49
279	27.90	26.52	2.77	4.45	0.95	26.91	5.45	146.60	1.284	No	Yes	1.39
280	28.00	24.26	2.81	4.58	0.96	24.44	5.92	144.70	1.166	No	Yes	1.26
281	28.10	21.33	2.86	4.78	0.98	21.28	6.68	142.17	1.015	No	Yes	1.10
282	28.20	18.44	2.94	5.19	1.00	18.16	7.78	141.26	0.866	No	Yes	0.94
283	28.30	16.54	3.01	5.79	1.00	16.05	8.95	143.70	0.766	No	Yes	0.83
284	28.40	16.30	3.04	6.31	1.00	15.75	9.49	149.51	0.751	No	Yes	0.81
285	28.50	17.10	3.03	6.50	1.00	16.55	9.37	155.00	0.789	No	Yes	0.85
286	28.60	18.01	3.02	6.56	1.00	17.46	9.11	159.06	0.833	No	Yes	0.90
287	28.70	18.92	3.01	6.73	1.00	18.36	8.95	164.43	0.876	No	Yes	0.95
288	28.80	20.11	3.00	7.06	1.00	19.56	8.86	173.27	0.933	No	Yes	1.01

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _k (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
289	28.90	21.92	2.98	7.22	1.00	21.40	8.50	181.84	1.021	No	Yes	1.10
290	29.00	23.18	2.96	7.08	1.00	22.66	8.11	183.89	1.081	No	Yes	1.17
291	29.10	23.37	2.94	6.60	1.00	22.78	7.75	176.56	1.087	No	Yes	1.18
292	29.20	23.75	2.90	5.98	1.00	23.10	7.24	167.18	1.102	No	Yes	1.19
293	29.30	25.51	2.85	5.35	0.98	24.81	6.45	160.15	1.184	No	Yes	1.28
294	29.40	27.88	2.79	4.83	0.96	27.13	5.70	154.78	1.294	No	Yes	1.40
295	29.50	28.61	2.76	4.48	0.95	27.77	5.35	148.60	1.325	No	Yes	1.43
296	29.60	27.32	2.77	4.36	0.95	26.37	5.45	143.70	1.258	No	Yes	1.36
297	29.70	25.80	2.80	4.62	0.96	24.76	5.91	146.26	1.181	No	Yes	1.28
298	29.80	25.94	2.82	4.85	0.97	24.84	6.07	150.77	1.185	No	Yes	1.28
299	29.90	25.94	2.81	4.75	0.97	24.76	6.01	148.73	1.181	No	Yes	1.28
300	30.00	24.40	2.83	4.65	0.97	23.13	6.21	143.69	1.103	No	Yes	1.19
301	30.10	21.96	2.87	4.68	0.99	20.61	6.74	138.86	0.983	No	Yes	1.06
302	30.20	20.74	2.90	4.89	1.00	19.33	7.22	139.54	0.922	No	Yes	1.00
303	30.30	21.44	2.89	4.81	1.00	19.97	7.00	139.71	0.952	No	Yes	1.03
304	30.40	22.21	2.87	4.66	0.99	20.68	6.71	138.69	0.986	No	Yes	1.06
305	30.50	22.53	2.86	4.60	0.99	20.93	6.60	138.08	0.998	No	Yes	1.08
306	30.60	22.53	2.86	4.60	0.99	20.87	6.61	138.02	0.995	No	Yes	1.07
307	30.70	22.94	2.86	4.72	0.99	21.21	6.64	140.86	1.012	No	Yes	1.09
308	30.80	25.28	2.83	4.82	0.98	23.47	6.29	147.55	1.120	No	Yes	1.21
309	30.90	30.78	2.76	4.63	0.95	28.82	5.33	153.56	1.375	No	Yes	1.48
310	31.00	38.07	2.65	4.11	0.91	35.87	7.54	270.36	3.600	No	No	2.00
311	31.10	43.30	2.56	3.53	0.88	40.86	4.31	175.96	0.587	No	No	0.63
312	31.20	44.29	2.52	3.13	0.86	41.68	3.27	136.24	0.315	No	No	0.34
313	31.30	43.30	2.53	3.10	0.86	40.62	3.39	137.54	0.322	No	No	0.35
314	31.40	44.39	2.54	3.30	0.87	41.57	3.66	151.98	0.406	No	No	0.44
315	31.50	48.84	2.51	3.35	0.86	45.77	3.07	140.34	4.000	Yes	No	2.00
316	31.60	55.32	2.44	3.02	0.83	51.89	2.62	135.76	4.000	Yes	No	2.00
317	31.70	61.94	2.35	2.51	0.80	58.11	2.14	124.50	4.000	Yes	No	2.00
318	31.80	68.38	2.26	2.06	0.76	64.12	1.79	115.05	4.000	Yes	No	2.00
319	31.90	74.08	2.19	1.75	0.73	69.40	1.59	110.24	4.000	Yes	No	2.00
320	32.00	77.06	2.15	1.62	0.72	72.09	1.51	109.09	4.000	Yes	No	2.00
321	32.10	74.88	2.17	1.68	0.73	69.86	1.56	108.63	4.000	Yes	No	2.00
322	32.20	67.28	2.26	1.96	0.76	62.48	1.77	110.79	4.000	Yes	No	2.00
323	32.30	56.41	2.38	2.45	0.81	52.01	2.27	118.21	4.000	Yes	No	2.00
324	32.40	45.30	2.51	3.02	0.86	41.34	3.10	128.06	4.000	Yes	No	2.00
325	32.50	36.00	2.65	3.64	0.91	32.42	7.34	237.90	4.000	Yes	No	2.00
326	32.60	29.19	2.77	4.26	0.95	25.90	5.44	140.87	4.000	Yes	Yes	2.00
327	32.70	25.10	2.85	4.71	0.99	21.97	6.48	142.38	4.000	Yes	Yes	2.00
328	32.80	23.13	2.88	4.80	1.00	20.04	6.97	139.64	4.000	Yes	Yes	2.00
329	32.90	22.72	2.88	4.59	1.00	19.60	6.89	135.06	0.935	No	Yes	1.01
330	33.00	23.50	2.85	4.39	0.99	20.28	6.56	133.08	0.967	No	Yes	1.05
331	33.10	24.98	2.83	4.34	0.98	21.61	6.24	134.74	1.031	No	Yes	1.11
332	33.20	27.13	2.81	4.39	0.97	23.56	5.92	139.45	1.124	No	Yes	1.21
333	33.30	29.30	2.79	4.51	0.96	25.51	5.70	145.36	1.217	No	Yes	1.31
334	33.40	30.50	2.79	4.69	0.96	26.55	5.68	150.86	1.267	No	Yes	1.37
335	33.50	30.45	2.80	4.93	0.97	26.43	5.88	155.49	1.261	No	Yes	1.36
336	33.60	29.68	2.83	5.17	0.98	25.63	6.19	158.58	1.223	No	Yes	1.32

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
337	33.70	29.63	2.84	5.35	0.98	25.51	6.34	161.64	1.217	No	Yes	1.32
338	33.80	31.56	2.83	5.51	0.98	27.21	6.19	168.34	4.000	Yes	Yes	2.00
339	33.90	36.20	2.80	5.75	0.97	31.38	5.80	181.86	4.000	Yes	Yes	2.00
340	34.00	43.30	2.75	5.92	0.95	37.79	5.23	197.76	4.000	Yes	Yes	2.00
341	34.10	51.88	2.69	5.82	0.93	45.54	9.40	428.21	4.000	Yes	No	2.00
342	34.20	61.05	2.62	5.48	0.90	53.80	6.13	329.55	4.000	Yes	No	2.00
343	34.30	69.91	2.55	5.02	0.87	61.76	3.94	243.15	4.000	Yes	No	2.00
344	34.40	78.51	2.49	4.56	0.85	69.46	2.88	200.38	4.000	Yes	No	2.00
345	34.50	87.03	2.43	4.18	0.83	77.07	2.53	194.99	4.000	Yes	No	2.00
346	34.60	96.53	2.37	3.84	0.81	85.55	2.23	190.38	4.000	Yes	No	2.00
347	34.70	107.11	2.31	3.47	0.78	95.01	1.96	185.82	4.000	Yes	No	2.00
348	34.80	117.42	2.23	3.01	0.75	104.24	1.71	177.94	4.000	Yes	No	2.00
349	34.90	125.48	2.17	2.59	0.73	111.44	1.54	171.37	4.000	Yes	No	2.00
350	35.00	129.52	2.12	2.34	0.71	114.95	1.46	167.39	4.000	Yes	No	2.00
351	35.10	129.35	2.12	2.28	0.71	114.57	1.45	165.58	0.502	No	No	0.55
352	35.20	124.29	2.14	2.36	0.72	109.70	1.49	163.04	4.000	Yes	No	2.00
353	35.30	113.93	2.19	2.53	0.74	100.05	1.59	159.12	4.000	Yes	No	2.00
354	35.40	99.94	2.26	2.79	0.77	87.17	1.79	156.05	4.000	Yes	No	2.00
355	35.50	86.32	2.35	3.17	0.80	74.67	2.12	158.35	4.000	Yes	No	2.00
356	35.60	78.64	2.41	3.52	0.82	67.57	2.43	164.27	4.000	Yes	No	2.00
357	35.70	79.44	2.42	3.69	0.83	68.08	2.50	170.36	4.000	Yes	No	2.00
358	35.80	87.98	2.39	3.60	0.81	75.51	2.30	173.61	4.000	Yes	No	2.00
359	35.90	100.57	2.32	3.30	0.79	86.56	1.99	172.57	4.000	Yes	No	2.00
360	36.00	113.44	2.24	2.91	0.76	97.90	1.73	169.10	4.000	Yes	No	2.00
361	36.10	124.61	2.17	2.55	0.73	107.76	1.55	166.69	4.000	Yes	No	2.00
362	36.20	133.12	2.12	2.32	0.71	115.22	1.45	167.10	4.000	Yes	No	2.00
363	36.30	139.52	2.09	2.21	0.70	120.72	1.41	169.85	0.536	No	No	0.59
364	36.40	144.03	2.08	2.19	0.70	124.47	1.39	173.16	0.563	No	No	0.62
365	36.50	146.71	2.08	2.23	0.70	126.55	1.39	176.23	0.589	No	No	0.65
366	36.60	146.25	2.09	2.30	0.70	125.83	1.41	177.27	0.598	No	No	0.66
367	36.70	142.03	2.11	2.38	0.71	121.77	1.44	175.32	0.581	No	No	0.64
368	36.80	135.41	2.14	2.46	0.72	115.63	1.48	171.37	0.548	No	No	0.60
369	36.90	129.09	2.16	2.48	0.73	109.83	1.52	166.54	0.510	No	No	0.56
370	37.00	125.04	2.16	2.43	0.73	106.08	1.52	161.53	0.472	No	No	0.52
371	37.10	122.66	2.15	2.35	0.73	103.83	1.51	157.09	0.441	No	No	0.48
372	37.20	121.21	2.15	2.29	0.73	102.39	1.51	154.12	0.420	No	No	0.46
373	37.30	120.82	2.15	2.28	0.73	101.84	1.51	153.40	0.416	No	No	0.46
374	37.40	121.89	2.15	2.30	0.73	102.55	1.51	154.48	0.423	No	No	0.47
375	37.50	124.48	2.15	2.31	0.73	104.56	1.50	156.68	0.438	No	No	0.48
376	37.60	127.71	2.14	2.30	0.72	107.15	1.48	158.98	0.454	No	No	0.50
377	37.70	130.82	2.13	2.27	0.72	109.64	1.46	160.57	0.465	No	No	0.51
378	37.80	132.63	2.12	2.25	0.72	110.99	1.45	161.33	0.470	No	No	0.52
379	37.90	132.47	2.12	2.25	0.72	110.63	1.45	160.78	0.467	No	No	0.52
380	38.00	129.59	2.13	2.27	0.72	107.90	1.47	158.76	0.452	No	No	0.50
381	38.10	123.93	2.15	2.32	0.73	102.77	1.51	155.28	0.428	No	No	0.47
382	38.20	115.89	2.19	2.39	0.74	95.60	1.58	150.97	0.400	No	No	0.44
383	38.30	107.14	2.22	2.50	0.76	87.86	1.68	147.41	0.378	No	No	0.42
384	38.40	98.41	2.26	2.57	0.77	80.20	1.79	143.33	0.354	No	No	0.39

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
385	38.50	90.54	2.29	2.60	0.78	73.34	1.89	138.77	0.329	No	No	0.36
386	38.60	84.03	2.31	2.59	0.79	67.69	1.98	134.10	0.304	No	No	0.34
387	38.70	79.79	2.34	2.63	0.80	63.95	2.07	132.56	0.297	No	No	0.33
388	38.80	77.78	2.35	2.66	0.80	62.11	2.13	132.12	0.294	No	No	0.33
389	38.90	77.14	2.35	2.63	0.80	61.46	2.12	130.45	0.286	No	No	0.32
390	39.00	77.04	2.34	2.56	0.80	61.28	2.09	128.29	0.276	No	No	0.31
391	39.10	76.57	2.34	2.54	0.80	60.76	2.09	127.11	0.271	No	No	0.30
392	39.20	75.78	2.35	2.60	0.81	59.94	2.14	128.39	0.277	No	No	0.31
393	39.30	75.01	2.37	2.71	0.81	59.12	2.22	131.47	0.291	No	No	0.33
394	39.40	74.55	2.39	2.85	0.82	58.54	2.31	135.50	0.311	No	No	0.35
395	39.50	74.00	2.40	2.96	0.83	57.91	2.39	138.37	0.326	No	No	0.36
396	39.60	73.21	2.40	2.94	0.83	57.14	2.40	137.08	0.320	No	No	0.36
397	39.70	72.79	2.40	2.84	0.82	56.71	2.36	133.79	0.303	No	No	0.34
398	39.80	72.42	2.39	2.77	0.82	56.32	2.33	131.12	0.290	No	No	0.32
399	39.90	70.13	2.39	2.70	0.82	54.35	2.35	127.47	0.273	No	No	0.31
400	40.00	66.57	2.41	2.68	0.83	51.32	2.43	124.84	0.261	No	No	0.29
401	40.10	63.68	2.43	2.70	0.84	48.85	2.53	123.76	0.256	No	No	0.29
402	40.20	64.36	2.43	2.77	0.84	49.26	2.56	126.17	0.267	No	No	0.30
403	40.30	68.83	2.41	2.77	0.83	52.79	2.44	128.80	0.279	No	No	0.31
404	40.40	77.61	2.36	2.67	0.81	59.87	2.19	130.84	0.288	No	No	0.32
405	40.50	91.92	2.28	2.47	0.78	71.57	1.86	133.06	0.299	No	No	0.34
406	40.60	111.46	2.18	2.18	0.74	87.73	1.57	137.70	0.323	No	No	0.36
407	40.70	133.56	2.08	1.88	0.70	106.20	1.39	147.50	0.378	No	No	0.43
408	40.80	153.43	2.00	1.70	0.68	122.84	1.31	160.84	0.467	No	No	0.53
409	40.90	167.80	1.96	1.63	0.66	134.76	1.28	172.18	0.555	No	No	0.63
410	41.00	176.80	1.93	1.57	0.65	142.18	1.26	179.01	0.614	No	No	0.69
411	41.10	182.80	1.92	1.55	0.64	147.00	1.25	183.71	0.657	No	No	0.74
412	41.20	187.72	1.92	1.56	0.64	150.81	1.25	188.04	0.698	No	No	0.79
413	41.30	191.80	1.93	1.65	0.65	153.71	1.25	192.76	0.746	No	No	0.85
414	41.40	194.68	1.94	1.72	0.65	155.63	1.26	196.20	0.782	No	No	0.89
415	41.50	197.00	1.94	1.75	0.65	157.18	1.26	198.54	0.808	No	No	0.92
416	41.60	199.27	1.94	1.77	0.65	158.73	1.26	200.53	4.000	No	No	2.00
417	41.70	202.25	1.94	1.78	0.65	160.87	1.26	203.05	4.000	No	No	2.00
418	41.80	205.69	1.94	1.81	0.65	163.33	1.26	206.23	4.000	No	No	2.00
419	41.90	209.24	1.94	1.86	0.66	165.81	1.27	209.96	4.000	No	No	2.00
420	42.00	212.51	1.95	1.91	0.66	168.04	1.27	213.39	4.000	No	No	2.00
421	42.10	214.98	1.95	1.94	0.66	169.66	1.27	215.83	4.000	No	No	2.00
422	42.20	216.82	1.95	1.95	0.66	170.83	1.27	217.24	4.000	No	No	2.00
423	42.30	217.44	1.95	1.94	0.66	171.05	1.27	217.32	4.000	No	No	2.00
424	42.40	215.99	1.95	1.94	0.66	169.56	1.27	215.68	4.000	No	No	2.00
425	42.50	212.38	1.96	1.96	0.66	166.26	1.28	212.38	4.000	No	No	2.00
426	42.60	207.75	1.97	1.97	0.67	162.14	1.28	208.26	4.000	No	No	2.00
427	42.70	203.54	1.98	1.98	0.67	158.42	1.29	204.30	4.000	No	No	2.00
428	42.80	199.98	1.98	1.96	0.67	155.27	1.29	200.66	4.000	No	No	2.00
429	42.90	196.07	1.99	1.96	0.67	151.85	1.30	196.82	0.789	No	No	0.91
430	43.00	191.21	2.00	1.97	0.68	147.63	1.30	192.48	0.743	No	No	0.86
431	43.10	185.37	2.01	1.99	0.68	142.60	1.31	187.51	0.693	No	No	0.80
432	43.20	179.37	2.03	2.02	0.69	137.43	1.33	182.72	0.647	No	No	0.75

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _t (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
433	43.30	174.19	2.04	2.06	0.69	132.95	1.34	178.78	0.611	No	No	0.71
434	43.40	170.22	2.05	2.09	0.70	129.47	1.36	175.77	0.585	No	No	0.68
435	43.50	166.83	2.06	2.10	0.70	126.51	1.37	173.01	0.562	No	No	0.65
436	43.60	162.46	2.07	2.11	0.71	122.78	1.38	169.39	0.532	No	No	0.62
437	43.70	156.00	2.09	2.15	0.71	117.35	1.41	164.91	0.497	No	No	0.58
438	43.80	147.22	2.12	2.22	0.73	110.07	1.45	159.59	0.458	No	No	0.53
439	43.90	136.83	2.16	2.32	0.74	101.53	1.52	154.22	0.421	No	No	0.49
440	44.00	126.19	2.20	2.43	0.76	92.88	1.61	149.55	0.391	No	No	0.46
441	44.10	116.68	2.23	2.51	0.77	85.22	1.71	145.40	0.366	No	No	0.43
442	44.20	109.12	2.26	2.50	0.78	79.22	1.77	140.29	0.337	No	No	0.39
443	44.30	103.32	2.25	2.34	0.78	74.80	1.76	131.81	0.293	No	No	0.34
444	44.40	98.06	2.23	2.07	0.77	70.93	1.70	120.62	0.243	No	No	0.28
445	44.50	92.45	2.21	1.80	0.76	66.83	1.64	109.45	0.202	No	No	0.24
446	44.60	86.05	2.21	1.65	0.76	61.96	1.64	101.53	0.177	No	No	0.21
447	44.70	79.77	2.24	1.69	0.77	56.96	1.74	98.89	0.170	No	No	0.20
448	44.80	74.72	2.30	1.86	0.79	52.81	1.91	100.74	0.175	No	No	0.21
449	44.90	71.40	2.33	1.99	0.81	50.06	2.06	102.88	0.181	No	No	0.21
450	45.00	69.26	2.35	2.05	0.82	48.29	2.15	103.62	0.183	No	No	0.22
451	45.10	69.08	2.36	2.12	0.82	48.01	2.20	105.41	0.189	No	No	0.22
452	45.20	73.88	2.35	2.19	0.82	51.46	2.13	109.83	0.203	No	No	0.24
453	45.30	86.95	2.29	2.12	0.79	61.29	1.87	114.69	0.220	No	No	0.26
454	45.40	107.24	2.18	1.88	0.75	76.96	1.56	120.09	0.241	No	No	0.28
455	45.50	130.79	2.07	1.63	0.71	95.46	1.38	131.29	0.290	No	No	0.34
456	45.60	152.68	1.99	1.49	0.68	112.72	1.30	146.32	0.371	No	No	0.44
457	45.70	171.44	1.94	1.43	0.66	127.47	1.26	160.76	0.466	No	No	0.55
458	45.80	188.25	1.91	1.43	0.65	140.48	1.24	174.46	0.574	No	No	0.68
459	45.90	205.84	1.88	1.43	0.64	154.08	1.22	188.59	0.704	No	No	0.84
460	46.00	224.66	1.85	1.42	0.63	168.78	1.20	202.68	4.000	No	No	2.00
461	46.10	242.48	1.81	1.36	0.61	182.92	1.17	213.72	4.000	No	No	2.00
462	46.20	256.90	1.78	1.29	0.60	194.52	1.13	219.56	4.000	No	No	2.00
463	46.30	266.83	1.77	1.29	0.60	202.14	1.11	224.94	4.000	No	No	2.00
464	46.40	272.73	1.77	1.32	0.60	206.29	1.12	230.21	4.000	No	No	2.00
465	46.50	275.32	1.77	1.33	0.60	207.95	1.12	232.12	4.000	No	No	2.00
466	46.60	276.13	1.77	1.33	0.60	208.29	1.11	232.18	4.000	No	No	2.00
467	46.70	276.72	1.77	1.32	0.60	208.48	1.11	231.87	4.000	No	No	2.00
468	46.80	278.32	1.78	1.39	0.60	208.95	1.13	236.67	4.000	No	No	2.00
469	46.90	282.43	1.79	1.44	0.60	211.50	1.14	241.72	4.000	No	No	2.00
470	47.00	288.11	1.79	1.45	0.60	215.55	1.14	245.68	4.000	No	No	2.00
471	47.10	291.48	1.78	1.41	0.60	218.17	1.12	244.99	4.000	No	No	2.00
472	47.20	287.17	1.78	1.39	0.60	214.60	1.12	241.01	4.000	No	No	2.00
473	47.30	273.91	1.80	1.43	0.61	203.55	1.15	234.91	4.000	No	No	2.00
474	47.40	254.36	1.85	1.55	0.63	187.22	1.20	224.98	4.000	No	No	2.00
475	47.50	231.51	1.91	1.72	0.65	168.39	1.25	209.93	4.000	No	No	2.00
476	47.60	207.31	1.98	1.90	0.68	148.87	1.29	192.44	0.743	No	No	0.90
477	47.70	183.14	2.05	2.07	0.70	129.76	1.35	175.74	0.585	No	No	0.71
478	47.80	161.34	2.11	2.22	0.73	112.83	1.44	162.17	0.477	No	No	0.58
479	47.90	147.04	2.16	2.34	0.75	101.74	1.52	155.05	0.427	No	No	0.52
480	48.00	144.37	2.17	2.40	0.75	99.47	1.56	154.69	0.424	No	No	0.52

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
481	48.10	154.30	2.15	2.36	0.74	106.68	1.50	160.14	0.462	No	No	0.56
482	48.20	174.92	2.09	2.22	0.72	122.07	1.40	171.37	0.548	No	No	0.67
483	48.30	203.69	2.01	1.99	0.69	144.04	1.31	189.13	0.709	No	No	0.87
484	48.40	238.64	1.91	1.74	0.65	171.26	1.25	213.37	4.000	No	No	2.00
485	48.50	272.42	1.83	1.52	0.62	198.09	1.18	233.98	4.000	No	No	2.00
486	48.60	297.48	1.77	1.38	0.60	218.17	1.11	242.89	4.000	No	No	2.00
487	48.70	309.01	1.75	1.34	0.59	227.10	1.08	245.68	4.000	No	No	2.00
488	48.80	310.28	1.76	1.39	0.60	227.31	1.10	249.99	4.000	No	No	2.00
489	48.90	308.58	1.79	1.49	0.61	224.81	1.14	255.28	4.000	No	No	2.00
490	49.00	308.74	1.81	1.60	0.62	223.69	1.16	260.57	4.000	No	No	2.00
491	49.10	309.55	1.83	1.69	0.62	223.18	1.19	264.58	4.000	No	No	2.00
492	49.20	307.77	1.85	1.78	0.63	220.85	1.20	265.53	4.000	No	No	2.00
493	49.30	300.75	1.87	1.83	0.64	214.88	1.21	260.96	4.000	No	No	2.00
494	49.40	287.55	1.88	1.81	0.64	204.67	1.22	250.19	4.000	No	No	2.00
495	49.50	266.11	1.89	1.75	0.65	188.68	1.23	231.85	4.000	No	No	2.00
496	49.60	239.13	1.90	1.67	0.65	168.63	1.24	209.07	4.000	No	No	2.00
497	49.70	219.20	1.92	1.62	0.66	153.76	1.25	192.28	0.741	No	No	0.92

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q_t :	Total cone resistance
I_c :	Soil behavior type index
Fr:	Normalized friction ratio (%)
n:	Stress exponent
Q_{tn} :	Normalized cone resistance
K_c :	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Normalized and adjusted cone resistance
CRR _{7.5} :	Cyclic resistance ratio for $M_w=7.5$
FS:	Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
0.10	2.00	0.00	0.00	0.10	0.00	0.20	2.00	0.00	0.00	0.10	0.00
0.30	2.00	0.00	0.00	0.10	0.00	0.40	2.00	0.00	0.00	0.10	0.00
0.50	2.00	0.00	0.00	0.10	0.00	0.60	2.00	0.00	0.00	0.10	0.00
0.70	2.00	0.00	0.00	0.10	0.00	0.80	2.00	0.00	0.00	0.10	0.00
0.90	2.00	0.00	0.00	0.10	0.00	1.00	2.00	0.00	0.00	0.10	0.00
1.10	2.00	0.00	0.00	0.10	0.00	1.20	2.00	0.00	0.00	0.10	0.00
1.30	2.00	0.00	0.00	0.10	0.00	1.40	2.00	0.00	0.00	0.10	0.00
1.50	2.00	0.00	0.00	0.10	0.00	1.60	2.00	0.00	0.00	0.10	0.00
1.70	2.00	0.00	0.00	0.10	0.00	1.80	2.00	0.00	0.00	0.10	0.00
1.90	2.00	0.00	0.00	0.10	0.00	2.00	2.00	0.00	0.00	0.10	0.00
2.10	2.00	0.00	0.00	0.10	0.00	2.20	2.00	0.00	0.00	0.10	0.00
2.30	2.00	0.00	0.00	0.10	0.00	2.40	2.00	0.00	0.00	0.10	0.00
2.50	2.00	0.00	0.00	0.10	0.00	2.60	2.00	0.00	0.00	0.10	0.00
2.70	2.00	0.00	0.00	0.10	0.00	2.80	2.00	0.00	0.00	0.10	0.00
2.90	2.00	0.00	0.00	0.10	0.00	3.00	2.00	0.00	0.00	0.10	0.00
3.10	2.00	0.00	0.00	0.10	0.00	3.20	2.00	0.00	0.00	0.10	0.00
3.30	2.00	0.00	0.00	0.10	0.00	3.40	2.00	0.00	0.00	0.10	0.00
3.50	2.00	0.00	0.00	0.10	0.00	3.60	2.00	0.00	0.00	0.10	0.00
3.70	2.00	0.00	0.00	0.10	0.00	3.80	2.00	0.00	0.00	0.10	0.00
3.90	2.00	0.00	0.00	0.10	0.00	4.00	2.00	0.00	0.00	0.10	0.00
4.10	2.00	0.00	0.00	0.10	0.00	4.20	2.00	0.00	0.00	0.10	0.00
4.30	2.00	0.00	0.00	0.10	0.00	4.40	2.00	0.00	0.00	0.10	0.00
4.50	2.00	0.00	0.00	0.10	0.00	4.60	2.00	0.00	0.00	0.10	0.00
4.70	2.00	0.00	0.00	0.10	0.00	4.80	2.00	0.00	0.00	0.10	0.00
4.90	2.00	0.00	0.00	0.10	0.00	5.00	2.00	0.00	0.00	0.10	0.00
5.10	2.00	0.00	0.00	0.10	0.00	5.20	2.00	0.00	0.00	0.10	0.00
5.30	2.00	0.00	0.00	0.10	0.00	5.40	2.00	0.00	0.00	0.10	0.00
5.50	2.00	0.00	0.00	0.10	0.00	5.60	2.00	0.00	0.00	0.10	0.00
5.70	2.00	0.00	0.00	0.10	0.00	5.80	2.00	0.00	0.00	0.10	0.00
5.90	2.00	0.00	0.00	0.10	0.00	6.00	2.00	0.00	0.00	0.10	0.00
6.10	2.00	0.00	0.00	0.10	0.00	6.20	2.00	0.00	0.00	0.10	0.00
6.30	2.00	0.00	0.00	0.10	0.00	6.40	2.00	0.00	0.00	0.10	0.00
6.50	2.00	0.00	0.00	0.10	0.00	6.60	2.00	0.00	0.00	0.10	0.00
6.70	2.00	0.00	0.00	0.10	0.00	6.80	2.00	0.00	0.00	0.10	0.00
6.90	2.00	0.00	0.00	0.10	0.00	7.00	2.00	0.00	0.00	0.10	0.00
7.10	2.00	0.00	0.00	0.10	0.00	7.20	2.00	0.00	0.00	0.10	0.00
7.30	2.00	0.00	0.00	0.10	0.00	7.40	2.00	0.00	0.00	0.10	0.00
7.50	2.00	0.00	0.00	0.10	0.00	7.60	2.00	0.00	0.00	0.10	0.00
7.70	2.00	0.00	0.00	0.10	0.00	7.80	2.00	0.00	0.00	0.10	0.00
7.90	2.00	0.00	0.00	0.10	0.00	8.00	2.00	0.00	0.00	0.10	0.00
8.10	0.29	0.00	0.00	0.10	0.19	8.20	0.29	0.00	0.00	0.10	0.19
8.30	0.29	0.00	0.00	0.10	0.19	8.40	0.29	0.00	0.00	0.10	0.19
8.50	0.29	0.00	0.00	0.10	0.19	8.60	2.00	0.00	0.00	0.10	0.00
8.70	2.00	0.00	0.00	0.10	0.00	8.80	2.00	0.00	0.00	0.10	0.00
8.90	2.00	0.00	0.00	0.10	0.00	9.00	2.00	0.00	0.00	0.10	0.00
9.10	2.00	0.00	0.00	0.10	0.00	9.20	0.98	0.00	0.00	0.10	0.01
9.30	0.94	0.00	0.00	0.10	0.01	9.40	0.94	0.00	0.00	0.10	0.01
9.50	0.92	0.00	0.00	0.10	0.02	9.60	0.87	0.00	0.00	0.10	0.03

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
9.70	0.99	0.00	0.00	0.10	0.00	9.80	1.31	0.00	0.00	0.10	0.00
9.90	1.40	0.00	0.00	0.10	0.00	10.00	1.19	0.00	0.00	0.10	0.00
10.10	0.79	0.00	0.00	0.10	0.05	10.20	0.57	0.00	0.00	0.10	0.11
10.30	0.47	0.00	0.00	0.10	0.14	10.40	0.39	0.00	0.00	0.10	0.16
10.50	0.40	0.00	0.00	0.10	0.15	10.60	0.46	0.00	0.00	0.10	0.14
10.70	0.53	0.00	0.00	0.10	0.12	10.80	0.55	0.00	0.00	0.10	0.11
10.90	0.55	0.00	0.00	0.10	0.12	11.00	0.54	0.00	0.00	0.10	0.12
11.10	0.54	0.00	0.00	0.10	0.12	11.20	0.53	0.00	0.00	0.10	0.12
11.30	0.53	0.00	0.00	0.10	0.12	11.40	0.52	0.00	0.00	0.10	0.12
11.50	0.52	0.00	0.00	0.10	0.12	11.60	0.51	0.00	0.00	0.10	0.12
11.70	0.51	0.00	0.00	0.10	0.12	11.80	0.50	0.00	0.00	0.10	0.12
11.90	0.50	0.00	0.00	0.10	0.12	12.00	0.50	0.00	0.00	0.10	0.13
12.10	0.49	0.00	0.00	0.10	0.13	12.20	0.51	0.00	0.00	0.10	0.12
12.30	0.59	0.00	0.00	0.10	0.10	12.40	0.69	0.00	0.00	0.10	0.08
12.50	0.79	0.00	0.00	0.10	0.05	12.60	0.84	0.00	0.00	0.10	0.04
12.70	0.87	0.00	0.00	0.10	0.03	12.80	0.88	0.00	0.00	0.10	0.03
12.90	0.80	0.00	0.00	0.10	0.05	13.00	0.72	0.00	0.00	0.10	0.07
13.10	0.69	0.00	0.00	0.10	0.08	13.20	0.72	0.00	0.00	0.10	0.07
13.30	0.76	0.00	0.00	0.10	0.06	13.40	0.70	0.00	0.00	0.10	0.07
13.50	0.57	0.00	0.00	0.10	0.10	13.60	0.42	0.00	0.00	0.10	0.14
13.70	0.34	0.00	0.00	0.10	0.16	13.80	0.32	0.00	0.00	0.10	0.16
13.90	0.34	0.00	0.00	0.10	0.16	14.00	0.39	0.00	0.00	0.10	0.15
14.10	0.43	0.00	0.00	0.10	0.14	14.20	0.44	0.00	0.00	0.10	0.13
14.30	0.44	0.00	0.00	0.10	0.13	14.40	0.43	0.00	0.00	0.10	0.14
14.50	0.44	0.00	0.00	0.10	0.13	14.60	0.45	0.00	0.00	0.10	0.13
14.70	0.50	0.00	0.00	0.10	0.12	14.80	0.60	0.00	0.00	0.10	0.09
14.90	0.70	0.00	0.00	0.10	0.07	15.00	0.77	0.00	0.00	0.10	0.05
15.10	0.88	0.00	0.00	0.10	0.03	15.20	1.11	0.00	0.00	0.10	0.00
15.30	1.46	0.00	0.00	0.10	0.00	15.40	1.61	0.00	0.00	0.10	0.00
15.50	1.61	0.00	0.00	0.10	0.00	15.60	1.75	0.00	0.00	0.10	0.00
15.70	2.00	0.00	0.00	0.10	0.00	15.80	0.46	0.00	0.00	0.10	0.12
15.90	0.27	0.00	0.00	0.10	0.17	16.00	0.37	0.00	0.00	0.10	0.15
16.10	1.37	0.00	0.00	0.10	0.00	16.20	1.00	0.00	0.00	0.10	0.00
16.30	0.85	0.00	0.00	0.10	0.03	16.40	0.82	0.00	0.00	0.10	0.04
16.50	0.78	0.00	0.00	0.10	0.05	16.60	0.73	0.00	0.00	0.10	0.06
16.70	0.68	0.00	0.00	0.10	0.07	16.80	0.65	0.00	0.00	0.10	0.08
16.90	0.58	0.00	0.00	0.10	0.10	17.00	0.50	0.00	0.00	0.10	0.11
17.10	0.42	0.00	0.00	0.10	0.13	17.20	0.38	0.00	0.00	0.10	0.14
17.30	0.36	0.00	0.00	0.10	0.14	17.40	0.35	0.00	0.00	0.10	0.15
17.50	0.33	0.00	0.00	0.10	0.15	17.60	0.29	0.00	0.00	0.10	0.16
17.70	0.24	0.00	0.00	0.10	0.17	17.80	0.22	0.00	0.00	0.10	0.17
17.90	0.24	0.00	0.00	0.10	0.17	18.00	0.28	0.00	0.00	0.10	0.16
18.10	0.30	0.00	0.00	0.10	0.15	18.20	0.32	0.00	0.00	0.10	0.15
18.30	0.35	0.00	0.00	0.10	0.14	18.40	0.39	0.00	0.00	0.10	0.13
18.50	0.40	0.00	0.00	0.10	0.13	18.60	0.40	0.00	0.00	0.10	0.13
18.70	0.40	0.00	0.00	0.10	0.13	18.80	0.40	0.00	0.00	0.10	0.13
18.90	0.39	0.00	0.00	0.10	0.13	19.00	0.40	0.00	0.00	0.10	0.13
19.10	0.43	0.00	0.00	0.10	0.12	19.20	0.47	0.00	0.00	0.10	0.11

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
19.30	0.52	0.00	0.00	0.10	0.10	19.40	0.56	0.00	0.00	0.10	0.10
19.50	0.58	0.00	0.00	0.10	0.09	19.60	0.57	0.00	0.00	0.10	0.09
19.70	0.57	0.00	0.00	0.10	0.09	19.80	0.64	0.00	0.00	0.10	0.08
19.90	0.69	0.00	0.00	0.10	0.07	20.00	0.67	0.00	0.00	0.10	0.07
20.10	0.54	0.00	0.00	0.10	0.10	20.20	0.42	0.00	0.00	0.10	0.12
20.30	0.37	0.00	0.00	0.10	0.13	20.40	0.35	0.00	0.00	0.10	0.14
20.50	0.32	0.00	0.00	0.10	0.14	20.60	0.29	0.00	0.00	0.10	0.15
20.70	0.27	0.00	0.00	0.10	0.15	20.80	0.27	0.00	0.00	0.10	0.15
20.90	0.27	0.00	0.00	0.10	0.15	21.00	0.31	0.00	0.00	0.10	0.14
21.10	0.37	0.00	0.00	0.10	0.13	21.20	0.42	0.00	0.00	0.10	0.12
21.30	0.44	0.00	0.00	0.10	0.12	21.40	0.44	0.00	0.00	0.10	0.11
21.50	0.48	0.00	0.00	0.10	0.11	21.60	0.59	0.00	0.00	0.10	0.08
21.70	0.74	0.00	0.00	0.10	0.05	21.80	0.96	0.00	0.00	0.10	0.01
21.90	1.17	0.00	0.00	0.10	0.00	22.00	2.00	0.00	0.00	0.10	0.00
22.10	0.45	0.00	0.00	0.10	0.11	22.20	0.48	0.00	0.00	0.10	0.11
22.30	2.00	0.00	0.00	0.10	0.00	22.40	1.26	0.00	0.00	0.10	0.00
22.50	1.22	0.00	0.00	0.10	0.00	22.60	1.23	0.00	0.00	0.10	0.00
22.70	1.36	0.00	0.00	0.10	0.00	22.80	1.65	0.00	0.00	0.10	0.00
22.90	2.00	0.00	0.00	0.10	0.00	23.00	2.00	0.00	0.00	0.10	0.00
23.10	0.36	0.00	0.00	0.10	0.13	23.20	0.28	0.00	0.00	0.10	0.14
23.30	0.41	0.00	0.00	0.10	0.12	23.40	2.00	0.00	0.00	0.10	0.00
23.50	1.13	0.00	0.00	0.10	0.00	23.60	0.88	0.00	0.00	0.10	0.02
23.70	0.69	0.00	0.00	0.10	0.06	23.80	0.55	0.00	0.00	0.10	0.09
23.90	0.48	0.00	0.00	0.10	0.10	24.00	0.49	0.00	0.00	0.10	0.10
24.10	0.52	0.00	0.00	0.10	0.09	24.20	0.56	0.00	0.00	0.10	0.08
24.30	0.58	0.00	0.00	0.10	0.08	24.40	0.58	0.00	0.00	0.10	0.08
24.50	0.56	0.00	0.00	0.10	0.08	24.60	0.52	0.00	0.00	0.10	0.09
24.70	0.48	0.00	0.00	0.10	0.10	24.80	0.45	0.00	0.00	0.10	0.10
24.90	0.43	0.00	0.00	0.10	0.11	25.00	0.43	0.00	0.00	0.10	0.11
25.10	0.40	0.00	0.00	0.10	0.11	25.20	0.37	0.00	0.00	0.10	0.12
25.30	0.38	0.00	0.00	0.10	0.12	25.40	0.43	0.00	0.00	0.10	0.11
25.50	0.47	0.00	0.00	0.10	0.10	25.60	0.46	0.00	0.00	0.10	0.10
25.70	0.44	0.00	0.00	0.10	0.10	25.80	0.44	0.00	0.00	0.10	0.10
25.90	0.50	0.00	0.00	0.10	0.09	26.00	0.65	0.00	0.00	0.10	0.07
26.10	0.81	0.00	0.00	0.10	0.04	26.20	0.93	0.00	0.00	0.10	0.01
26.30	1.01	0.00	0.00	0.10	0.00	26.40	1.11	0.00	0.00	0.10	0.00
26.50	1.19	0.00	0.00	0.10	0.00	26.60	1.19	0.00	0.00	0.10	0.00
26.70	1.09	0.00	0.00	0.10	0.00	26.80	0.95	0.00	0.00	0.10	0.01
26.90	0.85	0.00	0.00	0.10	0.03	27.00	0.85	0.00	0.00	0.10	0.03
27.10	0.97	0.00	0.00	0.10	0.01	27.20	1.15	0.00	0.00	0.10	0.00
27.30	1.36	0.00	0.00	0.10	0.00	27.40	1.54	0.00	0.00	0.10	0.00
27.50	1.64	0.00	0.00	0.10	0.00	27.60	1.64	0.00	0.00	0.10	0.00
27.70	1.57	0.00	0.00	0.10	0.00	27.80	1.49	0.00	0.00	0.10	0.00
27.90	1.39	0.00	0.00	0.10	0.00	28.00	1.26	0.00	0.00	0.10	0.00
28.10	1.10	0.00	0.00	0.10	0.00	28.20	0.94	0.00	0.00	0.10	0.01
28.30	0.83	0.00	0.00	0.10	0.03	28.40	0.81	0.00	0.00	0.10	0.03
28.50	0.85	0.00	0.00	0.10	0.03	28.60	0.90	0.00	0.00	0.10	0.02
28.70	0.95	0.00	0.00	0.10	0.01	28.80	1.01	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
28.90	1.10	0.00	0.00	0.10	0.00	29.00	1.17	0.00	0.00	0.10	0.00
29.10	1.18	0.00	0.00	0.10	0.00	29.20	1.19	0.00	0.00	0.10	0.00
29.30	1.28	0.00	0.00	0.10	0.00	29.40	1.40	0.00	0.00	0.10	0.00
29.50	1.43	0.00	0.00	0.10	0.00	29.60	1.36	0.00	0.00	0.10	0.00
29.70	1.28	0.00	0.00	0.10	0.00	29.80	1.28	0.00	0.00	0.10	0.00
29.90	1.28	0.00	0.00	0.10	0.00	30.00	1.19	0.00	0.00	0.10	0.00
30.10	1.06	0.00	0.00	0.10	0.00	30.20	1.00	0.00	0.00	0.10	0.00
30.30	1.03	0.00	0.00	0.10	0.00	30.40	1.06	0.00	0.00	0.10	0.00
30.50	1.08	0.00	0.00	0.10	0.00	30.60	1.07	0.00	0.00	0.10	0.00
30.70	1.09	0.00	0.00	0.10	0.00	30.80	1.21	0.00	0.00	0.10	0.00
30.90	1.48	0.00	0.00	0.10	0.00	31.00	2.00	0.00	0.00	0.10	0.00
31.10	0.63	0.00	0.00	0.10	0.06	31.20	0.34	0.00	0.00	0.10	0.11
31.30	0.35	0.00	0.00	0.10	0.10	31.40	0.44	0.00	0.00	0.10	0.09
31.50	2.00	0.00	0.00	0.10	0.00	31.60	2.00	0.00	0.00	0.10	0.00
31.70	2.00	0.00	0.00	0.10	0.00	31.80	2.00	0.00	0.00	0.10	0.00
31.90	2.00	0.00	0.00	0.10	0.00	32.00	2.00	0.00	0.00	0.10	0.00
32.10	2.00	0.00	0.00	0.10	0.00	32.20	2.00	0.00	0.00	0.10	0.00
32.30	2.00	0.00	0.00	0.10	0.00	32.40	2.00	0.00	0.00	0.10	0.00
32.50	2.00	0.00	0.00	0.10	0.00	32.60	2.00	0.00	0.00	0.10	0.00
32.70	2.00	0.00	0.00	0.10	0.00	32.80	2.00	0.00	0.00	0.10	0.00
32.90	1.01	0.00	0.00	0.10	0.00	33.00	1.05	0.00	0.00	0.10	0.00
33.10	1.11	0.00	0.00	0.10	0.00	33.20	1.21	0.00	0.00	0.10	0.00
33.30	1.31	0.00	0.00	0.10	0.00	33.40	1.37	0.00	0.00	0.10	0.00
33.50	1.36	0.00	0.00	0.10	0.00	33.60	1.32	0.00	0.00	0.10	0.00
33.70	1.32	0.00	0.00	0.10	0.00	33.80	2.00	0.00	0.00	0.10	0.00
33.90	2.00	0.00	0.00	0.10	0.00	34.00	2.00	0.00	0.00	0.10	0.00
34.10	2.00	0.00	0.00	0.10	0.00	34.20	2.00	0.00	0.00	0.10	0.00
34.30	2.00	0.00	0.00	0.10	0.00	34.40	2.00	0.00	0.00	0.10	0.00
34.50	2.00	0.00	0.00	0.10	0.00	34.60	2.00	0.00	0.00	0.10	0.00
34.70	2.00	0.00	0.00	0.10	0.00	34.80	2.00	0.00	0.00	0.10	0.00
34.90	2.00	0.00	0.00	0.10	0.00	35.00	2.00	0.00	0.00	0.10	0.00
35.10	0.55	0.00	0.00	0.10	0.06	35.20	2.00	0.00	0.00	0.10	0.00
35.30	2.00	0.00	0.00	0.10	0.00	35.40	2.00	0.00	0.00	0.10	0.00
35.50	2.00	0.00	0.00	0.10	0.00	35.60	2.00	0.00	0.00	0.10	0.00
35.70	2.00	0.00	0.00	0.10	0.00	35.80	2.00	0.00	0.00	0.10	0.00
35.90	2.00	0.00	0.00	0.10	0.00	36.00	2.00	0.00	0.00	0.10	0.00
36.10	2.00	0.00	0.00	0.10	0.00	36.20	2.00	0.00	0.00	0.10	0.00
36.30	0.59	0.00	0.00	0.10	0.06	36.40	0.62	0.00	0.00	0.10	0.05
36.50	0.65	0.00	0.00	0.10	0.05	36.60	0.66	0.00	0.00	0.10	0.05
36.70	0.64	0.00	0.00	0.10	0.05	36.80	0.60	0.00	0.00	0.10	0.05
36.90	0.56	0.00	0.00	0.10	0.06	37.00	0.52	0.00	0.00	0.10	0.06
37.10	0.48	0.00	0.00	0.10	0.07	37.20	0.46	0.00	0.00	0.10	0.07
37.30	0.46	0.00	0.00	0.10	0.07	37.40	0.47	0.00	0.00	0.10	0.07
37.50	0.48	0.00	0.00	0.10	0.07	37.60	0.50	0.00	0.00	0.10	0.07
37.70	0.51	0.00	0.00	0.10	0.06	37.80	0.52	0.00	0.00	0.10	0.06
37.90	0.52	0.00	0.00	0.10	0.06	38.00	0.50	0.00	0.00	0.10	0.06
38.10	0.47	0.00	0.00	0.10	0.07	38.20	0.44	0.00	0.00	0.10	0.07
38.30	0.42	0.00	0.00	0.10	0.07	38.40	0.39	0.00	0.00	0.10	0.08

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
38.50	0.36	0.00	0.00	0.10	0.08	38.60	0.34	0.00	0.00	0.10	0.08
38.70	0.33	0.00	0.00	0.10	0.08	38.80	0.33	0.00	0.00	0.10	0.08
38.90	0.32	0.00	0.00	0.10	0.08	39.00	0.31	0.00	0.00	0.10	0.09
39.10	0.30	0.00	0.00	0.10	0.09	39.20	0.31	0.00	0.00	0.10	0.08
39.30	0.33	0.00	0.00	0.10	0.08	39.40	0.35	0.00	0.00	0.10	0.08
39.50	0.36	0.00	0.00	0.10	0.08	39.60	0.36	0.00	0.00	0.10	0.08
39.70	0.34	0.00	0.00	0.10	0.08	39.80	0.32	0.00	0.00	0.10	0.08
39.90	0.31	0.00	0.00	0.10	0.08	40.00	0.29	0.00	0.00	0.10	0.08
40.10	0.29	0.00	0.00	0.10	0.08	40.20	0.30	0.00	0.00	0.10	0.08
40.30	0.31	0.00	0.00	0.10	0.08	40.40	0.32	0.00	0.00	0.10	0.08
40.50	0.34	0.00	0.00	0.10	0.08	40.60	0.36	0.00	0.00	0.10	0.07
40.70	0.43	0.00	0.00	0.10	0.07	40.80	0.53	0.00	0.00	0.10	0.05
40.90	0.63	0.00	0.00	0.10	0.04	41.00	0.69	0.00	0.00	0.10	0.04
41.10	0.74	0.00	0.00	0.10	0.03	41.20	0.79	0.00	0.00	0.10	0.02
41.30	0.85	0.00	0.00	0.10	0.02	41.40	0.89	0.00	0.00	0.10	0.01
41.50	0.92	0.00	0.00	0.10	0.01	41.60	2.00	0.00	0.00	0.10	0.00
41.70	2.00	0.00	0.00	0.10	0.00	41.80	2.00	0.00	0.00	0.10	0.00
41.90	2.00	0.00	0.00	0.10	0.00	42.00	2.00	0.00	0.00	0.10	0.00
42.10	2.00	0.00	0.00	0.10	0.00	42.20	2.00	0.00	0.00	0.10	0.00
42.30	2.00	0.00	0.00	0.10	0.00	42.40	2.00	0.00	0.00	0.10	0.00
42.50	2.00	0.00	0.00	0.10	0.00	42.60	2.00	0.00	0.00	0.10	0.00
42.70	2.00	0.00	0.00	0.10	0.00	42.80	2.00	0.00	0.00	0.10	0.00
42.90	0.91	0.00	0.00	0.10	0.01	43.00	0.86	0.00	0.00	0.10	0.02
43.10	0.80	0.00	0.00	0.10	0.02	43.20	0.75	0.00	0.00	0.10	0.03
43.30	0.71	0.00	0.00	0.10	0.03	43.40	0.68	0.00	0.00	0.10	0.03
43.50	0.65	0.00	0.00	0.10	0.04	43.60	0.62	0.00	0.00	0.10	0.04
43.70	0.58	0.00	0.00	0.10	0.04	43.80	0.53	0.00	0.00	0.10	0.05
43.90	0.49	0.00	0.00	0.10	0.05	44.00	0.46	0.00	0.00	0.10	0.05
44.10	0.43	0.00	0.00	0.10	0.06	44.20	0.39	0.00	0.00	0.10	0.06
44.30	0.34	0.00	0.00	0.10	0.07	44.40	0.28	0.00	0.00	0.10	0.07
44.50	0.24	0.00	0.00	0.10	0.07	44.60	0.21	0.00	0.00	0.10	0.08
44.70	0.20	0.00	0.00	0.10	0.08	44.80	0.21	0.00	0.00	0.10	0.08
44.90	0.21	0.00	0.00	0.10	0.08	45.00	0.22	0.00	0.00	0.10	0.08
45.10	0.22	0.00	0.00	0.10	0.07	45.20	0.24	0.00	0.00	0.10	0.07
45.30	0.26	0.00	0.00	0.10	0.07	45.40	0.28	0.00	0.00	0.10	0.07
45.50	0.34	0.00	0.00	0.10	0.06	45.60	0.44	0.00	0.00	0.10	0.05
45.70	0.55	0.00	0.00	0.10	0.04	45.80	0.68	0.00	0.00	0.10	0.03
45.90	0.84	0.00	0.00	0.10	0.02	46.00	2.00	0.00	0.00	0.10	0.00
46.10	2.00	0.00	0.00	0.10	0.00	46.20	2.00	0.00	0.00	0.10	0.00
46.30	2.00	0.00	0.00	0.10	0.00	46.40	2.00	0.00	0.00	0.10	0.00
46.50	2.00	0.00	0.00	0.10	0.00	46.60	2.00	0.00	0.00	0.10	0.00
46.70	2.00	0.00	0.00	0.10	0.00	46.80	2.00	0.00	0.00	0.10	0.00
46.90	2.00	0.00	0.00	0.10	0.00	47.00	2.00	0.00	0.00	0.10	0.00
47.10	2.00	0.00	0.00	0.10	0.00	47.20	2.00	0.00	0.00	0.10	0.00
47.30	2.00	0.00	0.00	0.10	0.00	47.40	2.00	0.00	0.00	0.10	0.00
47.50	2.00	0.00	0.00	0.10	0.00	47.60	0.90	0.00	0.00	0.10	0.01
47.70	0.71	0.00	0.00	0.10	0.02	47.80	0.58	0.00	0.00	0.10	0.03
47.90	0.52	0.00	0.00	0.10	0.04	48.00	0.52	0.00	0.00	0.10	0.04

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
48.10	0.56	0.00	0.00	0.10	0.04	48.20	0.67	0.00	0.00	0.10	0.03
48.30	0.87	0.00	0.00	0.10	0.01	48.40	2.00	0.00	0.00	0.10	0.00
48.50	2.00	0.00	0.00	0.10	0.00	48.60	2.00	0.00	0.00	0.10	0.00
48.70	2.00	0.00	0.00	0.10	0.00	48.80	2.00	0.00	0.00	0.10	0.00
48.90	2.00	0.00	0.00	0.10	0.00	49.00	2.00	0.00	0.00	0.10	0.00
49.10	2.00	0.00	0.00	0.10	0.00	49.20	2.00	0.00	0.00	0.10	0.00
49.30	2.00	0.00	0.00	0.10	0.00	49.40	2.00	0.00	0.00	0.10	0.00
49.50	2.00	0.00	0.00	0.10	0.00	49.60	2.00	0.00	0.00	0.10	0.00
49.70	0.92	0.00	0.00	0.10	0.01						

Overall liquefaction potential: 22.27

LPI = 0.00 - Liquefaction risk very low

LPI between 0.00 and 5.00 - Liquefaction risk low

LPI between 5.00 and 15.00 - Liquefaction risk high

LPI > 15.00 - Liquefaction risk very high

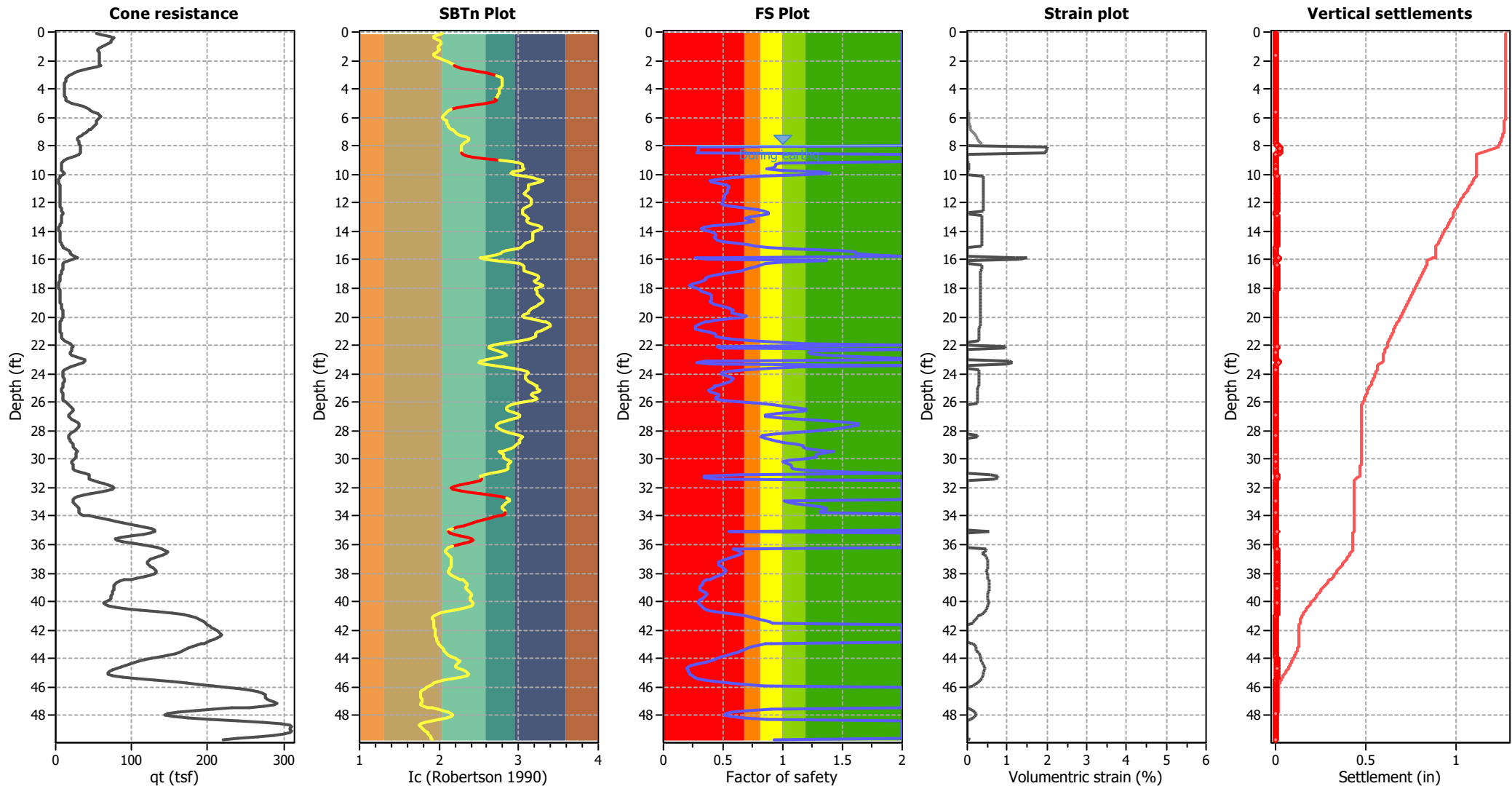
Abbreviations

FS: Calculated factor of safety for test point

F_L: 1 - FSw_z: Function value of the extend of soil liquefaction according to depthd_z: Layer thickness (ft)

LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

- q_c : Total cone resistance (cone resistance q_c corrected for pore water effects)
- I_c : Soil Behaviour Type Index
- FS: Calculated Factor of Safety against liquefaction
- Volumetric strain: Post-liquefaction volumetric strain

:: Post-earthquake settlement of dry sands ::												
Depth (ft)	Ic	Q _{tn}	Kc	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _r (%)	Settle. (in)
0.10	2.03	99.31	1.34	132.89	28	621	0.59	0.001	0.00	13.69	0.00	0.000
0.20	1.98	115.98	1.29	149.82	31	678	0.59	0.001	0.00	13.69	0.00	0.000
0.30	1.94	134.53	1.26	169.99	35	748	0.59	0.001	0.00	13.69	0.00	0.000
0.40	1.94	143.12	1.26	180.64	37	793	0.59	0.002	0.00	13.69	0.00	0.000
0.50	1.97	142.16	1.28	182.50	38	820	0.59	0.002	0.00	13.69	0.00	0.000
0.60	2.00	138.67	1.31	181.81	38	836	0.59	0.003	0.00	13.69	0.00	0.000
0.70	2.03	135.24	1.33	180.18	38	840	0.59	0.003	0.00	13.69	0.00	0.000
0.80	2.03	130.83	1.33	174.09	37	811	0.59	0.004	0.00	13.69	0.00	0.000
0.90	2.00	124.19	1.31	162.62	34	747	0.59	0.005	0.00	13.69	0.00	0.000
1.00	1.98	116.10	1.29	150.16	31	681	0.59	0.006	0.00	13.69	0.00	0.000
1.10	1.98	109.23	1.29	141.21	29	640	0.59	0.007	0.00	13.69	0.00	0.000
1.20	2.00	105.67	1.31	138.17	29	634	0.59	0.008	0.01	13.69	0.01	0.000
1.30	1.99	105.48	1.30	137.29	28	627	0.59	0.010	0.01	13.69	0.01	0.000
1.40	1.96	106.59	1.28	136.42	28	610	0.59	0.011	0.01	13.69	0.01	0.000
1.50	1.93	106.91	1.26	134.53	27	588	0.59	0.013	0.01	13.69	0.01	0.000
1.60	1.92	106.73	1.25	133.75	27	581	0.59	0.015	0.01	13.69	0.01	0.000
1.70	1.96	107.21	1.28	136.80	28	610	0.59	0.014	0.01	13.69	0.01	0.000
1.80	2.01	108.50	1.31	142.37	30	655	0.59	0.014	0.01	13.69	0.01	0.000
1.90	2.05	109.38	1.35	148.06	31	697	0.59	0.013	0.01	13.69	0.01	0.000
2.00	2.09	107.68	1.41	151.68	33	726	0.59	0.013	0.01	13.69	0.01	0.000
2.10	2.14	106.34	1.48	157.28	35	758	0.59	0.013	0.01	13.69	0.01	0.000
2.20	2.17	108.37	1.55	167.55	37	806	0.59	0.012	0.01	13.69	0.01	0.000
2.30	2.18	111.81	1.57	175.63	39	844	0.59	0.012	0.01	13.69	0.00	0.000
2.40	2.19	110.13	1.59	175.07	0	0	0.59	0.000	0.00	13.69	0.00	0.000
2.50	2.22	99.64	1.67	166.32	0	0	0.59	0.000	0.00	13.69	0.00	0.000
2.60	2.29	84.15	1.88	158.20	0	0	0.59	0.000	0.00	13.69	0.00	0.000
2.70	2.39	68.17	2.30	156.59	0	0	0.59	0.000	0.00	13.69	0.00	0.000
2.80	2.49	54.98	2.90	159.28	0	0	0.59	0.000	0.00	13.69	0.00	0.000
2.90	2.58	45.07	3.61	162.50	0	0	0.59	0.000	0.00	0.00	0.00	0.000
3.00	2.66	37.90	4.32	163.83	0	0	0.59	0.000	0.00	0.00	0.00	0.000
3.10	2.73	32.14	5.00	160.83	0	0	0.59	0.000	0.00	0.00	0.00	0.000
3.20	2.77	27.73	5.54	153.60	0	0	0.59	0.000	0.00	0.00	0.00	0.000
3.30	2.79	25.27	5.76	145.45	0	0	0.59	0.000	0.00	0.00	0.00	0.000
3.40	2.79	24.00	5.78	138.77	0	0	0.59	0.000	0.00	0.00	0.00	0.000
3.50	2.79	23.09	5.77	133.19	0	0	0.59	0.000	0.00	0.00	0.00	0.000
3.60	2.80	21.84	5.82	127.05	0	0	0.59	0.000	0.00	0.00	0.00	0.000
3.70	2.80	20.72	5.85	121.10	0	0	0.59	0.000	0.00	0.00	0.00	0.000
3.80	2.79	20.01	5.79	115.82	0	0	0.59	0.000	0.00	0.00	0.00	0.000
3.90	2.78	19.74	5.64	111.25	0	0	0.59	0.000	0.00	0.00	0.00	0.000
4.00	2.76	19.72	5.41	106.79	0	0	0.59	0.000	0.00	0.00	0.00	0.000
4.10	2.75	19.71	5.27	103.89	0	0	0.59	0.000	0.00	0.00	0.00	0.000
4.20	2.75	19.70	5.24	103.20	0	0	0.59	0.000	0.00	0.00	0.00	0.000
4.30	2.75	19.69	5.26	103.67	0	0	0.59	0.000	0.00	0.00	0.00	0.000
4.40	2.75	20.13	5.22	105.06	0	0	0.59	0.000	0.00	0.00	0.00	0.000
4.50	2.73	21.45	5.03	107.92	0	0	0.59	0.000	0.00	0.00	0.00	0.000
4.60	2.71	22.94	4.85	111.34	0	0	0.59	0.000	0.00	0.00	0.00	0.000
4.70	2.71	23.99	4.81	115.45	0	0	0.59	0.000	0.00	0.00	0.00	0.000
4.80	2.72	24.99	4.87	121.62	0	0	0.59	0.000	0.00	0.00	0.00	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
4.90	2.68	29.55	4.54	134.08	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.00	2.59	39.41	3.64	143.48	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.10	2.46	53.19	2.70	143.86	0	0	0.59	0.000	0.00	13.69	0.00	0.000
5.20	2.33	65.93	2.06	135.60	0	0	0.59	0.000	0.00	13.69	0.00	0.000
5.30	2.23	74.72	1.69	126.16	0	0	0.59	0.000	0.00	13.69	0.00	0.000
5.40	2.16	80.52	1.52	122.49	0	0	0.59	0.000	0.00	13.69	0.00	0.000
5.50	2.12	86.45	1.46	125.82	0	0	0.59	0.000	0.00	13.69	0.00	0.000
5.60	2.10	94.40	1.43	134.63	29	646	0.59	0.086	0.05	13.69	0.05	0.001
5.70	2.08	102.93	1.39	143.31	31	684	0.59	0.074	0.04	13.69	0.04	0.000
5.80	2.05	109.14	1.36	148.30	32	700	0.59	0.071	0.04	13.69	0.04	0.000
5.90	2.04	110.56	1.34	148.38	31	695	0.58	0.075	0.04	13.69	0.04	0.000
6.00	2.05	107.63	1.35	145.34	31	684	0.58	0.082	0.05	13.69	0.04	0.001
6.10	2.07	103.52	1.38	142.51	30	677	0.58	0.087	0.05	13.69	0.04	0.001
6.20	2.09	100.84	1.40	141.50	30	677	0.58	0.090	0.05	13.69	0.05	0.001
6.30	2.09	99.92	1.41	140.97	30	675	0.58	0.094	0.06	13.69	0.05	0.001
6.40	2.10	98.66	1.42	139.69	30	670	0.58	0.100	0.06	13.69	0.05	0.001
6.50	2.11	95.51	1.43	136.61	30	660	0.58	0.108	0.07	13.69	0.06	0.001
6.60	2.12	92.26	1.45	133.92	29	652	0.58	0.117	0.07	13.69	0.06	0.001
6.70	2.14	89.06	1.48	131.53	29	644	0.58	0.126	0.08	13.69	0.07	0.001
6.80	2.15	85.23	1.51	128.73	28	632	0.58	0.139	0.09	13.69	0.08	0.001
6.90	2.17	80.47	1.55	125.10	28	615	0.58	0.160	0.11	13.69	0.09	0.001
7.00	2.19	75.68	1.60	121.15	27	594	0.58	0.190	0.13	13.69	0.11	0.001
7.10	2.21	71.59	1.64	117.05	26	575	0.58	0.226	0.16	13.69	0.13	0.002
7.20	2.23	66.93	1.69	113.30	26	553	0.58	0.277	0.20	13.69	0.17	0.002
7.30	2.27	61.39	1.82	111.80	26	532	0.58	0.343	0.25	13.69	0.21	0.003
7.40	2.33	56.04	2.03	113.86	27	517	0.58	0.409	0.28	13.69	0.24	0.003
7.50	2.36	53.21	2.20	116.98	28	513	0.58	0.439	0.29	13.69	0.24	0.003
7.60	2.37	52.54	2.21	116.13	28	513	0.58	0.455	0.30	13.69	0.25	0.003
7.70	2.35	52.67	2.12	111.66	27	510	0.58	0.487	0.34	13.69	0.28	0.003
7.80	2.32	52.84	2.02	106.66	25	505	0.58	0.530	0.40	13.69	0.33	0.004
7.90	2.30	53.39	1.94	103.32	24	504	0.58	0.550	0.43	13.69	0.36	0.004

Total estimated settlement: 0.04**Abbreviations**

Q_{tn}: Equivalent clean sand normalized cone resistance
 K_c: Fines correction factor
 Q_{tn,cs}: Post-liquefaction volumetric strain
 G_{max}: Small strain shear modulus
 CSR: Soil cyclic stress ratio
 γ: Cyclic shear strain
 e_{vol(15)}: Volumetric strain after 15 cycles
 N_c: Equivalent number of cycles
 e_v: Volumetric strain
 Settle.: Calculated settlement

:: Post-earthquake settlement due to soil liquefaction ::

Depth (ft)	Q _{tn,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	Q _{tn,cs}	FS	e _v (%)	DF	Settlement (in)
8.00	101.38	2.00	0.00	0.85	0.00	8.10	99.49	0.29	2.00	0.85	0.02
8.20	99.05	0.29	2.00	0.85	0.02	8.30	99.63	0.29	1.99	0.85	0.02
8.40	100.35	0.29	1.97	0.85	0.02	8.50	99.39	0.29	1.99	0.85	0.02
8.60	96.76	2.00	0.00	0.84	0.00	8.70	94.10	2.00	0.00	0.84	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
8.80	94.17	2.00	0.00	0.84	0.00	8.90	130.69	2.00	0.00	0.84	0.00
9.00	105.48	2.00	0.00	0.84	0.00	9.10	111.19	2.00	0.00	0.83	0.00
9.20	116.38	0.98	0.02	0.83	0.00	9.30	121.03	0.94	0.03	0.83	0.00
9.40	121.03	0.94	0.03	0.83	0.00	9.50	117.92	0.92	0.03	0.83	0.00
9.60	114.87	0.87	0.03	0.83	0.00	9.70	122.59	0.99	0.02	0.82	0.00
9.80	135.12	1.31	0.01	0.82	0.00	9.90	136.29	1.40	0.01	0.82	0.00
10.00	126.77	1.19	0.01	0.82	0.00	10.10	108.97	0.79	0.41	0.82	0.00
10.20	96.67	0.57	0.41	0.81	0.00	10.30	89.12	0.47	0.41	0.81	0.00
10.40	81.42	0.39	0.41	0.81	0.00	10.50	79.63	0.40	0.40	0.81	0.00
10.60	80.62	0.46	0.40	0.81	0.00	10.70	82.95	0.53	0.40	0.81	0.00
10.80	84.78	0.55	0.40	0.80	0.00	10.90	85.75	0.55	0.40	0.80	0.00
11.00	85.22	0.54	0.40	0.80	0.00	11.10	82.33	0.54	0.40	0.80	0.00
11.20	78.87	0.53	0.40	0.80	0.00	11.30	76.79	0.53	0.40	0.79	0.00
11.40	76.71	0.52	0.40	0.79	0.00	11.50	78.67	0.52	0.40	0.79	0.00
11.60	82.04	0.51	0.39	0.79	0.00	11.70	85.49	0.51	0.39	0.79	0.00
11.80	87.84	0.50	0.39	0.79	0.00	11.90	88.08	0.50	0.39	0.78	0.00
12.00	86.83	0.50	0.39	0.78	0.00	12.10	85.58	0.49	0.39	0.78	0.00
12.20	87.05	0.51	0.39	0.78	0.00	12.30	94.00	0.59	0.39	0.78	0.00
12.40	103.89	0.69	0.39	0.77	0.00	12.50	114.26	0.79	0.39	0.77	0.00
12.60	122.25	0.84	0.39	0.77	0.00	12.70	127.62	0.87	0.02	0.77	0.00
12.80	129.20	0.88	0.02	0.77	0.00	12.90	124.86	0.80	0.38	0.77	0.00
13.00	119.06	0.72	0.38	0.76	0.00	13.10	116.97	0.69	0.38	0.76	0.00
13.20	121.15	0.72	0.38	0.76	0.00	13.30	124.24	0.76	0.38	0.76	0.00
13.40	119.02	0.70	0.38	0.76	0.00	13.50	106.77	0.57	0.38	0.75	0.00
13.60	91.14	0.42	0.38	0.75	0.00	13.70	79.92	0.34	0.38	0.75	0.00
13.80	74.67	0.32	0.37	0.75	0.00	13.90	74.43	0.34	0.37	0.75	0.00
14.00	78.17	0.39	0.37	0.75	0.00	14.10	83.37	0.43	0.37	0.74	0.00
14.20	85.77	0.44	0.37	0.74	0.00	14.30	86.52	0.44	0.37	0.74	0.00
14.40	85.77	0.43	0.37	0.74	0.00	14.50	85.83	0.44	0.37	0.74	0.00
14.60	87.21	0.45	0.37	0.73	0.00	14.70	92.49	0.50	0.37	0.73	0.00
14.80	102.97	0.60	0.37	0.73	0.00	14.90	113.58	0.70	0.36	0.73	0.00
15.00	122.43	0.77	0.36	0.73	0.00	15.10	131.93	0.88	0.02	0.73	0.00
15.20	144.57	1.11	0.01	0.72	0.00	15.30	155.26	1.46	0.00	0.72	0.00
15.40	155.04	1.61	0.00	0.72	0.00	15.50	149.18	1.61	0.00	0.72	0.00
15.60	144.22	1.75	0.00	0.72	0.00	15.70	228.19	2.00	0.00	0.71	0.00
15.80	145.43	0.46	1.23	0.71	0.01	15.90	113.31	0.27	1.50	0.71	0.02
16.00	132.13	0.37	1.32	0.71	0.02	16.10	109.24	1.37	0.00	0.71	0.00
16.20	117.79	1.00	0.01	0.71	0.00	16.30	126.88	0.85	0.02	0.70	0.00
16.40	132.99	0.82	0.35	0.70	0.00	16.50	131.99	0.78	0.35	0.70	0.00
16.60	125.22	0.73	0.35	0.70	0.00	16.70	116.69	0.68	0.35	0.70	0.00
16.80	111.84	0.65	0.35	0.69	0.00	16.90	107.02	0.58	0.35	0.69	0.00
17.00	102.76	0.50	0.35	0.69	0.00	17.10	96.84	0.42	0.34	0.69	0.00
17.20	91.17	0.38	0.34	0.69	0.00	17.30	85.25	0.36	0.34	0.69	0.00
17.40	79.16	0.35	0.34	0.68	0.00	17.50	72.67	0.33	0.34	0.68	0.00
17.60	65.53	0.29	0.34	0.68	0.00	17.70	60.34	0.24	0.34	0.68	0.00
17.80	57.97	0.22	0.34	0.68	0.00	17.90	60.62	0.24	0.34	0.67	0.00
18.00	64.89	0.28	0.34	0.67	0.00	18.10	69.07	0.30	0.34	0.67	0.00
18.20	74.74	0.32	0.33	0.67	0.00	18.30	82.93	0.35	0.33	0.67	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
18.40	91.12	0.39	0.33	0.67	0.00	18.50	97.74	0.40	0.33	0.66	0.00
18.60	102.22	0.40	0.33	0.66	0.00	18.70	105.25	0.40	0.33	0.66	0.00
18.80	106.33	0.40	0.33	0.66	0.00	18.90	105.44	0.39	0.33	0.66	0.00
19.00	104.64	0.40	0.33	0.65	0.00	19.10	106.71	0.43	0.33	0.65	0.00
19.20	111.49	0.47	0.33	0.65	0.00	19.30	115.67	0.52	0.32	0.65	0.00
19.40	117.04	0.56	0.32	0.65	0.00	19.50	116.72	0.58	0.32	0.65	0.00
19.60	113.99	0.57	0.32	0.64	0.00	19.70	112.26	0.57	0.32	0.64	0.00
19.80	115.49	0.64	0.32	0.64	0.00	19.90	118.65	0.69	0.32	0.64	0.00
20.00	118.78	0.67	0.32	0.64	0.00	20.10	112.39	0.54	0.32	0.63	0.00
20.20	107.02	0.42	0.32	0.63	0.00	20.30	105.35	0.37	0.32	0.63	0.00
20.40	104.19	0.35	0.31	0.63	0.00	20.50	100.44	0.32	0.31	0.63	0.00
20.60	93.85	0.29	0.31	0.63	0.00	20.70	86.94	0.27	0.31	0.62	0.00
20.80	82.10	0.27	0.31	0.62	0.00	20.90	80.08	0.27	0.31	0.62	0.00
21.00	84.44	0.31	0.31	0.62	0.00	21.10	93.64	0.37	0.31	0.62	0.00
21.20	101.21	0.42	0.31	0.61	0.00	21.30	104.65	0.44	0.31	0.61	0.00
21.40	105.76	0.44	0.31	0.61	0.00	21.50	110.30	0.48	0.30	0.61	0.00
21.60	119.72	0.59	0.30	0.61	0.00	21.70	127.74	0.74	0.30	0.61	0.00
21.80	129.88	0.96	0.01	0.60	0.00	21.90	121.93	1.17	0.00	0.60	0.00
22.00	216.54	2.00	0.00	0.60	0.00	22.10	157.53	0.45	0.96	0.60	0.01
22.20	160.86	0.48	0.94	0.60	0.01	22.30	212.67	2.00	0.00	0.59	0.00
22.40	118.80	1.26	0.00	0.59	0.00	22.50	130.33	1.22	0.00	0.59	0.00
22.60	144.45	1.23	0.00	0.59	0.00	22.70	161.91	1.36	0.00	0.59	0.00
22.80	174.25	1.65	0.00	0.59	0.00	22.90	363.33	2.00	0.00	0.58	0.00
23.00	217.91	2.00	0.00	0.58	0.00	23.10	136.81	0.36	1.05	0.58	0.01
23.20	121.84	0.28	1.15	0.58	0.01	23.30	145.91	0.41	0.99	0.58	0.01
23.40	253.25	2.00	0.00	0.57	0.00	23.50	128.36	1.13	0.00	0.57	0.00
23.60	127.45	0.88	0.01	0.57	0.00	23.70	120.59	0.69	0.28	0.57	0.00
23.80	109.99	0.55	0.28	0.57	0.00	23.90	100.73	0.48	0.28	0.57	0.00
24.00	99.13	0.49	0.28	0.56	0.00	24.10	103.24	0.52	0.28	0.56	0.00
24.20	109.87	0.56	0.28	0.56	0.00	24.30	115.03	0.58	0.28	0.56	0.00
24.40	118.15	0.58	0.28	0.56	0.00	24.50	119.08	0.56	0.28	0.55	0.00
24.60	117.72	0.52	0.28	0.55	0.00	24.70	115.38	0.48	0.28	0.55	0.00
24.80	112.62	0.45	0.27	0.55	0.00	24.90	110.39	0.43	0.27	0.55	0.00
25.00	108.74	0.43	0.27	0.55	0.00	25.10	105.37	0.40	0.27	0.54	0.00
25.20	101.43	0.37	0.27	0.54	0.00	25.30	100.49	0.38	0.27	0.54	0.00
25.40	102.35	0.43	0.27	0.54	0.00	25.50	105.07	0.47	0.27	0.54	0.00
25.60	107.19	0.46	0.27	0.53	0.00	25.70	109.64	0.44	0.27	0.53	0.00
25.80	113.49	0.44	0.27	0.53	0.00	25.90	118.19	0.50	0.26	0.53	0.00
26.00	124.53	0.65	0.26	0.53	0.00	26.10	127.68	0.81	0.26	0.53	0.00
26.20	127.57	0.93	0.01	0.52	0.00	26.30	128.59	1.01	0.01	0.52	0.00
26.40	135.65	1.11	0.00	0.52	0.00	26.50	146.44	1.19	0.00	0.52	0.00
26.60	154.29	1.19	0.00	0.52	0.00	26.70	155.21	1.09	0.00	0.51	0.00
26.80	151.54	0.95	0.01	0.51	0.00	26.90	147.95	0.85	0.01	0.51	0.00
27.00	149.51	0.85	0.01	0.51	0.00	27.10	155.81	0.97	0.01	0.51	0.00
27.20	162.90	1.15	0.00	0.51	0.00	27.30	166.84	1.36	0.00	0.50	0.00
27.40	165.22	1.54	0.00	0.50	0.00	27.50	159.41	1.64	0.00	0.50	0.00
27.60	153.17	1.64	0.00	0.50	0.00	27.70	148.96	1.57	0.00	0.50	0.00
27.80	147.60	1.49	0.00	0.49	0.00	27.90	146.60	1.39	0.00	0.49	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
28.00	144.70	1.26	0.00	0.49	0.00	28.10	142.17	1.10	0.00	0.49	0.00
28.20	141.26	0.94	0.01	0.49	0.00	28.30	143.70	0.83	0.24	0.49	0.00
28.40	149.51	0.81	0.24	0.48	0.00	28.50	155.00	0.85	0.01	0.48	0.00
28.60	159.06	0.90	0.01	0.48	0.00	28.70	164.43	0.95	0.01	0.48	0.00
28.80	173.27	1.01	0.01	0.48	0.00	28.90	181.84	1.10	0.00	0.47	0.00
29.00	183.89	1.17	0.00	0.47	0.00	29.10	176.56	1.18	0.00	0.47	0.00
29.20	167.18	1.19	0.00	0.47	0.00	29.30	160.15	1.28	0.00	0.47	0.00
29.40	154.78	1.40	0.00	0.47	0.00	29.50	148.60	1.43	0.00	0.46	0.00
29.60	143.70	1.36	0.00	0.46	0.00	29.70	146.26	1.28	0.00	0.46	0.00
29.80	150.77	1.28	0.00	0.46	0.00	29.90	148.73	1.28	0.00	0.46	0.00
30.00	143.69	1.19	0.00	0.45	0.00	30.10	138.86	1.06	0.00	0.45	0.00
30.20	139.54	1.00	0.01	0.45	0.00	30.30	139.71	1.03	0.00	0.45	0.00
30.40	138.69	1.06	0.00	0.45	0.00	30.50	138.08	1.08	0.00	0.45	0.00
30.60	138.02	1.07	0.00	0.44	0.00	30.70	140.86	1.09	0.00	0.44	0.00
30.80	147.55	1.21	0.00	0.44	0.00	30.90	153.56	1.48	0.00	0.44	0.00
31.00	270.36	2.00	0.00	0.44	0.00	31.10	175.96	0.63	0.58	0.43	0.01
31.20	136.24	0.34	0.78	0.43	0.01	31.30	137.54	0.35	0.78	0.43	0.01
31.40	151.98	0.44	0.71	0.43	0.01	31.50	140.34	2.00	0.00	0.43	0.00
31.60	135.76	2.00	0.00	0.43	0.00	31.70	124.50	2.00	0.00	0.42	0.00
31.80	115.05	2.00	0.00	0.42	0.00	31.90	110.24	2.00	0.00	0.42	0.00
32.00	109.09	2.00	0.00	0.42	0.00	32.10	108.63	2.00	0.00	0.42	0.00
32.20	110.79	2.00	0.00	0.41	0.00	32.30	118.21	2.00	0.00	0.41	0.00
32.40	128.06	2.00	0.00	0.41	0.00	32.50	237.90	2.00	0.00	0.41	0.00
32.60	140.87	2.00	0.00	0.41	0.00	32.70	142.38	2.00	0.00	0.41	0.00
32.80	139.64	2.00	0.00	0.40	0.00	32.90	135.06	1.01	0.00	0.40	0.00
33.00	133.08	1.05	0.00	0.40	0.00	33.10	134.74	1.11	0.00	0.40	0.00
33.20	139.45	1.21	0.00	0.40	0.00	33.30	145.36	1.31	0.00	0.39	0.00
33.40	150.86	1.37	0.00	0.39	0.00	33.50	155.49	1.36	0.00	0.39	0.00
33.60	158.58	1.32	0.00	0.39	0.00	33.70	161.64	1.32	0.00	0.39	0.00
33.80	168.34	2.00	0.00	0.39	0.00	33.90	181.86	2.00	0.00	0.38	0.00
34.00	197.76	2.00	0.00	0.38	0.00	34.10	428.21	2.00	0.00	0.38	0.00
34.20	329.55	2.00	0.00	0.38	0.00	34.30	243.15	2.00	0.00	0.38	0.00
34.40	200.38	2.00	0.00	0.37	0.00	34.50	194.99	2.00	0.00	0.37	0.00
34.60	190.38	2.00	0.00	0.37	0.00	34.70	185.82	2.00	0.00	0.37	0.00
34.80	177.94	2.00	0.00	0.37	0.00	34.90	171.37	2.00	0.00	0.37	0.00
35.00	167.39	2.00	0.00	0.36	0.00	35.10	165.58	0.55	0.56	0.36	0.01
35.20	163.04	2.00	0.00	0.36	0.00	35.30	159.12	2.00	0.00	0.36	0.00
35.40	156.05	2.00	0.00	0.36	0.00	35.50	158.35	2.00	0.00	0.35	0.00
35.60	164.27	2.00	0.00	0.35	0.00	35.70	170.36	2.00	0.00	0.35	0.00
35.80	173.61	2.00	0.00	0.35	0.00	35.90	172.57	2.00	0.00	0.35	0.00
36.00	169.10	2.00	0.00	0.35	0.00	36.10	166.69	2.00	0.00	0.34	0.00
36.20	167.10	2.00	0.00	0.34	0.00	36.30	169.85	0.59	0.48	0.34	0.01
36.40	173.16	0.62	0.46	0.34	0.01	36.50	176.23	0.65	0.45	0.34	0.01
36.60	177.27	0.66	0.36	0.33	0.00	36.70	175.32	0.64	0.45	0.33	0.01
36.80	171.37	0.60	0.46	0.33	0.01	36.90	166.54	0.56	0.48	0.33	0.01
37.00	161.53	0.52	0.52	0.33	0.01	37.10	157.09	0.48	0.53	0.33	0.01
37.20	154.12	0.46	0.53	0.32	0.01	37.30	153.40	0.46	0.53	0.32	0.01
37.40	154.48	0.47	0.52	0.32	0.01	37.50	156.68	0.48	0.51	0.32	0.01

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
37.60	158.98	0.50	0.51	0.32	0.01	37.70	160.57	0.51	0.50	0.31	0.01
37.80	161.33	0.52	0.49	0.31	0.01	37.90	160.78	0.52	0.49	0.31	0.01
38.00	158.76	0.50	0.49	0.31	0.01	38.10	155.28	0.47	0.50	0.31	0.01
38.20	150.97	0.44	0.51	0.31	0.01	38.30	147.41	0.42	0.52	0.30	0.01
38.40	143.33	0.39	0.52	0.30	0.01	38.50	138.77	0.36	0.54	0.30	0.01
38.60	134.10	0.34	0.55	0.30	0.01	38.70	132.56	0.33	0.55	0.30	0.01
38.80	132.12	0.33	0.55	0.29	0.01	38.90	130.45	0.32	0.55	0.29	0.01
39.00	128.29	0.31	0.55	0.29	0.01	39.10	127.11	0.30	0.55	0.29	0.01
39.20	128.39	0.31	0.55	0.29	0.01	39.30	131.47	0.33	0.53	0.29	0.01
39.40	135.50	0.35	0.52	0.28	0.01	39.50	138.37	0.36	0.50	0.28	0.01
39.60	137.08	0.36	0.51	0.28	0.01	39.70	133.79	0.34	0.51	0.28	0.01
39.80	131.12	0.32	0.52	0.28	0.01	39.90	127.47	0.31	0.53	0.27	0.01
40.00	124.84	0.29	0.53	0.27	0.01	40.10	123.76	0.29	0.53	0.27	0.01
40.20	126.17	0.30	0.52	0.27	0.01	40.30	128.80	0.31	0.51	0.27	0.01
40.40	130.84	0.32	0.50	0.27	0.01	40.50	133.06	0.34	0.49	0.26	0.01
40.60	137.70	0.36	0.47	0.26	0.01	40.70	147.50	0.43	0.44	0.26	0.01
40.80	160.84	0.53	0.41	0.26	0.00	40.90	172.18	0.63	0.35	0.26	0.00
41.00	179.01	0.69	0.27	0.25	0.00	41.10	183.71	0.74	0.26	0.25	0.00
41.20	188.04	0.79	0.20	0.25	0.00	41.30	192.76	0.85	0.19	0.25	0.00
41.40	196.20	0.89	0.14	0.25	0.00	41.50	198.54	0.92	0.14	0.25	0.00
41.60	200.53	2.00	0.00	0.24	0.00	41.70	203.05	2.00	0.00	0.24	0.00
41.80	206.23	2.00	0.00	0.24	0.00	41.90	209.96	2.00	0.00	0.24	0.00
42.00	213.39	2.00	0.00	0.24	0.00	42.10	215.83	2.00	0.00	0.23	0.00
42.20	217.24	2.00	0.00	0.23	0.00	42.30	217.32	2.00	0.00	0.23	0.00
42.40	215.68	2.00	0.00	0.23	0.00	42.50	212.38	2.00	0.00	0.23	0.00
42.60	208.26	2.00	0.00	0.23	0.00	42.70	204.30	2.00	0.00	0.22	0.00
42.80	200.66	2.00	0.00	0.22	0.00	42.90	196.82	0.91	0.13	0.22	0.00
43.00	192.48	0.86	0.13	0.22	0.00	43.10	187.51	0.80	0.18	0.22	0.00
43.20	182.72	0.75	0.22	0.21	0.00	43.30	178.78	0.71	0.23	0.21	0.00
43.40	175.77	0.68	0.23	0.21	0.00	43.50	173.01	0.65	0.24	0.21	0.00
43.60	169.39	0.62	0.29	0.21	0.00	43.70	164.91	0.58	0.30	0.21	0.00
43.80	159.59	0.53	0.32	0.20	0.00	43.90	154.22	0.49	0.33	0.20	0.00
44.00	149.55	0.46	0.34	0.20	0.00	44.10	145.40	0.43	0.34	0.20	0.00
44.20	140.29	0.39	0.35	0.20	0.00	44.30	131.81	0.34	0.36	0.19	0.00
44.40	120.62	0.28	0.39	0.19	0.00	44.50	109.45	0.24	0.41	0.19	0.00
44.60	101.53	0.21	0.44	0.19	0.01	44.70	98.89	0.20	0.44	0.19	0.01
44.80	100.74	0.21	0.43	0.19	0.01	44.90	102.88	0.21	0.42	0.18	0.01
45.00	103.62	0.22	0.41	0.18	0.00	45.10	105.41	0.22	0.40	0.18	0.00
45.20	109.83	0.24	0.39	0.18	0.00	45.30	114.69	0.26	0.37	0.18	0.00
45.40	120.09	0.28	0.35	0.17	0.00	45.50	131.29	0.34	0.32	0.17	0.00
45.60	146.32	0.44	0.29	0.17	0.00	45.70	160.76	0.55	0.26	0.17	0.00
45.80	174.46	0.68	0.19	0.17	0.00	45.90	188.59	0.84	0.13	0.17	0.00
46.00	202.68	2.00	0.00	0.16	0.00	46.10	213.72	2.00	0.00	0.16	0.00
46.20	219.56	2.00	0.00	0.16	0.00	46.30	224.94	2.00	0.00	0.16	0.00
46.40	230.21	2.00	0.00	0.16	0.00	46.50	232.12	2.00	0.00	0.15	0.00
46.60	232.18	2.00	0.00	0.15	0.00	46.70	231.87	2.00	0.00	0.15	0.00
46.80	236.67	2.00	0.00	0.15	0.00	46.90	241.72	2.00	0.00	0.15	0.00
47.00	245.68	2.00	0.00	0.15	0.00	47.10	244.99	2.00	0.00	0.14	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
47.20	241.01	2.00	0.00	0.14	0.00	47.30	234.91	2.00	0.00	0.14	0.00
47.40	224.98	2.00	0.00	0.14	0.00	47.50	209.93	2.00	0.00	0.14	0.00
47.60	192.44	0.90	0.08	0.13	0.00	47.70	175.74	0.71	0.15	0.13	0.00
47.80	162.17	0.58	0.20	0.13	0.00	47.90	155.05	0.52	0.21	0.13	0.00
48.00	154.69	0.52	0.21	0.13	0.00	48.10	160.14	0.56	0.19	0.13	0.00
48.20	171.37	0.67	0.14	0.12	0.00	48.30	189.13	0.87	0.07	0.12	0.00
48.40	213.37	2.00	0.00	0.12	0.00	48.50	233.98	2.00	0.00	0.12	0.00
48.60	242.89	2.00	0.00	0.12	0.00	48.70	245.68	2.00	0.00	0.11	0.00
48.80	249.99	2.00	0.00	0.11	0.00	48.90	255.28	2.00	0.00	0.11	0.00
49.00	260.57	2.00	0.00	0.11	0.00	49.10	264.58	2.00	0.00	0.11	0.00
49.20	265.53	2.00	0.00	0.11	0.00	49.30	260.96	2.00	0.00	0.10	0.00
49.40	250.19	2.00	0.00	0.10	0.00	49.50	231.85	2.00	0.00	0.10	0.00
49.60	209.07	2.00	0.00	0.10	0.00	49.70	192.28	0.92	0.06	0.10	0.00

Total estimated settlement: 1.23**Abbreviations**

$Q_{tn,cs}$:	Equivalent clean sand normalized cone resistance
FS:	Factor of safety against liquefaction
e_v (%):	Post-liquefaction volumetric strain
DF:	e_v depth weighting factor
Settlement:	Calculated settlement

:: Strength loss calculation (Robertson (2009)) ::

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.10	52.54	99.31	1.34	132.89	2.03	0.80	0.80
0.20	61.37	115.98	1.29	149.82	1.98	0.83	0.83
0.30	71.19	134.53	1.26	169.99	1.94	0.85	0.85
0.40	75.74	143.12	1.26	180.64	1.94	0.87	0.87
0.50	75.24	142.16	1.28	182.50	1.97	0.87	0.87
0.60	73.40	138.67	1.31	181.81	2.00	0.87	0.87
0.70	71.59	135.24	1.33	180.18	2.03	0.86	0.86
0.80	69.27	130.83	1.33	174.09	2.03	0.86	0.86
0.90	65.76	124.19	1.31	162.62	2.00	0.84	0.84
1.00	61.48	116.10	1.29	150.16	1.98	0.83	0.83
1.10	57.86	109.23	1.29	141.21	1.98	0.81	0.81
1.20	55.98	105.67	1.31	138.17	2.00	0.81	0.81
1.30	55.88	105.48	1.30	137.29	1.99	0.81	0.81
1.40	56.48	106.59	1.28	136.42	1.96	0.81	0.81
1.50	56.65	106.91	1.26	134.53	1.93	0.81	0.81
1.60	56.56	106.73	1.25	133.75	1.92	0.80	0.80
1.70	56.82	107.21	1.28	136.80	1.96	0.81	0.81
1.80	57.51	108.50	1.31	142.37	2.01	0.82	0.82
1.90	57.98	109.38	1.35	148.06	2.05	0.82	0.82
2.00	57.09	107.68	1.41	151.68	2.09	0.83	0.83
2.10	56.39	106.34	1.48	157.28	2.14	0.84	0.84
2.20	57.47	108.37	1.55	167.55	2.17	0.85	0.85
2.30	59.29	111.81	1.57	175.63	2.18	0.86	0.86
2.40	58.41	110.13	1.59	175.07	2.19	0.86	0.86
2.50	52.87	99.64	1.67	166.32	2.22	0.85	0.85
2.60	44.67	84.15	1.88	158.20	2.29	0.84	0.84
2.70	36.23	68.17	2.30	156.59	2.39	0.84	0.84
2.80	29.26	54.98	2.90	159.28	2.49	0.84	0.84
2.90	24.02	45.07	3.61	162.50	2.58	0.91	0.91
3.00	20.23	37.90	4.32	163.83	2.66	0.98	0.98
3.10	17.19	32.14	5.00	160.83	2.73	0.84	0.84
3.20	14.86	27.73	5.54	153.60	2.77	0.83	0.83
3.30	13.57	25.27	5.76	145.45	2.79	0.82	0.82
3.40	12.90	24.00	5.78	138.77	2.79	0.81	0.81
3.50	12.42	23.09	5.77	133.19	2.79	0.80	0.80
3.60	11.77	21.84	5.82	127.05	2.80	0.79	0.79
3.70	11.18	20.72	5.85	121.10	2.80	0.78	0.78
3.80	10.81	20.01	5.79	115.82	2.79	0.78	0.78
3.90	10.67	19.74	5.64	111.25	2.78	0.77	0.77
4.00	10.67	19.72	5.41	106.79	2.76	0.76	0.76
4.10	10.67	19.71	5.27	103.89	2.75	0.76	0.76
4.20	10.67	19.70	5.24	103.20	2.75	0.75	0.75
4.30	10.67	19.69	5.26	103.67	2.75	0.75	0.75
4.40	10.91	20.13	5.22	105.06	2.75	0.76	0.76
4.50	11.61	21.45	5.03	107.92	2.73	0.76	0.76
4.60	12.40	22.94	4.85	111.34	2.71	0.77	0.77
4.70	12.96	23.99	4.81	115.45	2.71	0.78	0.78
4.80	13.50	24.99	4.87	121.62	2.72	0.79	0.79

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
4.90	15.92	29.55	4.54	134.08	2.68	0.95	0.95
5.00	21.14	39.41	3.64	143.48	2.59	0.88	0.88
5.10	28.44	53.19	2.70	143.86	2.46	0.82	0.82
5.20	35.19	65.93	2.06	135.60	2.33	0.81	0.81
5.30	39.84	74.72	1.69	126.16	2.23	0.79	0.79
5.40	42.91	80.52	1.52	122.49	2.16	0.79	0.79
5.50	46.06	86.45	1.46	125.82	2.12	0.79	0.79
5.60	50.27	94.40	1.43	134.63	2.10	0.81	0.81
5.70	54.79	102.93	1.39	143.31	2.08	0.82	0.82
5.80	58.08	109.14	1.36	148.30	2.05	0.82	0.82
5.90	58.83	110.56	1.34	148.38	2.04	0.82	0.82
6.00	57.29	107.63	1.35	145.34	2.05	0.82	0.82
6.10	55.12	103.52	1.38	142.51	2.07	0.82	0.82
6.20	53.71	100.84	1.40	141.50	2.09	0.82	0.82
6.30	53.23	99.92	1.41	140.97	2.09	0.81	0.81
6.40	52.58	98.66	1.42	139.69	2.10	0.81	0.81
6.50	51.24	95.51	1.43	136.61	2.11	0.81	0.81
6.60	49.76	92.26	1.45	133.92	2.12	0.80	0.80
6.70	48.27	89.06	1.48	131.53	2.14	0.80	0.80
6.80	46.37	85.23	1.51	128.73	2.15	0.80	0.80
6.90	43.90	80.47	1.55	125.10	2.17	0.79	0.79
7.00	41.42	75.68	1.60	121.15	2.19	0.78	0.78
7.10	39.39	71.59	1.64	117.05	2.21	0.78	0.78
7.20	36.94	66.93	1.69	113.30	2.23	0.77	0.77
7.30	33.77	61.39	1.82	111.80	2.27	0.77	0.77
7.40	30.59	56.04	2.03	113.86	2.33	0.77	0.77
7.50	28.99	53.21	2.20	116.98	2.36	0.78	0.78
7.60	28.89	52.54	2.21	116.13	2.37	0.78	0.78
7.70	29.43	52.67	2.12	111.66	2.35	0.77	0.77
7.80	30.02	52.84	2.02	106.66	2.32	0.76	0.76
7.90	30.81	53.39	1.94	103.32	2.30	0.75	0.75
8.00	31.60	53.97	1.88	101.38	2.29	0.75	0.75
8.10	32.01	54.24	1.83	99.49	2.27	0.75	0.75
8.20	32.01	54.02	1.83	99.05	2.27	0.75	0.75
8.30	32.01	53.87	1.85	99.63	2.28	0.75	0.75
8.40	32.01	53.73	1.87	100.35	2.28	0.75	0.75
8.50	31.59	52.85	1.88	99.39	2.29	0.75	0.75
8.60	30.13	50.34	1.92	96.76	2.30	0.74	0.74
8.70	26.66	44.83	2.10	94.10	2.34	0.74	0.74
8.80	21.40	36.66	2.57	94.17	2.44	0.74	0.74
8.90	15.52	27.38	3.59	98.28	2.58	0.80	0.80
9.00	11.03	19.86	5.31	105.48	2.75	0.76	0.76
9.10	8.41	14.90	7.46	111.19	2.92	0.77	0.77
9.20	7.29	12.77	9.11	116.38	3.02	0.63	0.97
9.30	7.11	12.41	9.75	121.03	3.05	0.64	0.94
9.40	7.15	12.48	9.70	121.03	3.05	0.71	0.94
9.50	7.05	12.28	9.60	117.92	3.05	0.62	0.92
9.60	6.68	11.58	9.92	114.87	3.06	0.52	0.86

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.70	7.58	13.26	9.25	122.59	3.03	0.58	0.99
9.80	9.92	17.67	7.65	135.12	2.93	0.81	0.81
9.90	10.58	18.92	7.20	136.29	2.90	0.81	0.81
10.00	9.12	16.15	7.85	126.77	2.94	0.79	0.79
10.10	6.33	10.86	10.04	108.97	3.07	0.43	0.79
10.20	4.77	7.90	12.24	96.67	3.18	0.37	0.57
10.30	4.05	6.53	13.65	89.12	3.24	0.27	0.47
10.40	3.45	5.40	15.09	81.42	3.30	0.22	0.39
10.50	3.55	5.56	14.31	79.63	3.27	0.19	0.40
10.60	4.00	6.41	12.57	80.62	3.19	0.23	0.46
10.70	4.52	7.39	11.23	82.95	3.13	0.25	0.53
10.80	4.74	7.77	10.90	84.78	3.11	0.25	0.56
10.90	4.74	7.74	11.08	85.75	3.12	0.28	0.55
11.00	4.74	7.70	11.07	85.22	3.12	0.27	0.55
11.10	4.74	7.67	10.74	82.33	3.11	0.24	0.55
11.20	4.74	7.63	10.34	78.87	3.09	0.22	0.55
11.30	4.74	7.60	10.11	76.79	3.07	0.20	0.54
11.40	4.74	7.56	10.14	76.71	3.08	0.20	0.54
11.50	4.74	7.53	10.45	78.67	3.09	0.22	0.54
11.60	4.74	7.49	10.95	82.04	3.12	0.24	0.54
11.70	4.74	7.46	11.46	85.49	3.14	0.27	0.53
11.80	4.74	7.42	11.83	87.84	3.16	0.28	0.53
11.90	4.74	7.39	11.92	88.08	3.16	0.29	0.53
12.00	4.74	7.36	11.80	86.83	3.16	0.27	0.53
12.10	4.74	7.32	11.69	85.58	3.15	0.26	0.52
12.20	4.96	7.67	11.35	87.05	3.14	0.26	0.55
12.30	5.67	8.92	10.54	94.00	3.10	0.31	0.64
12.40	6.56	10.46	9.94	103.89	3.06	0.44	0.75
12.50	7.40	11.89	9.61	114.26	3.05	0.55	0.85
12.60	7.87	12.67	9.65	122.25	3.05	0.65	0.91
12.70	8.25	13.28	9.61	127.62	3.05	0.71	0.95
12.80	8.33	13.37	9.67	129.20	3.05	0.75	0.95
12.90	7.75	12.28	10.17	124.86	3.08	0.70	0.88
13.00	7.10	11.10	10.73	119.06	3.11	0.53	0.79
13.10	6.84	10.58	11.05	116.97	3.12	0.52	0.76
13.20	7.20	11.16	10.85	121.15	3.11	0.62	0.80
13.30	7.57	11.74	10.58	124.24	3.10	0.67	0.84
13.40	7.08	10.84	10.98	119.02	3.12	0.64	0.77
13.50	5.94	8.85	12.06	106.77	3.17	0.43	0.63
13.60	4.62	6.57	13.88	91.14	3.25	0.26	0.47
13.70	3.90	5.32	15.03	79.92	3.29	0.20	0.38
13.80	3.75	5.04	14.82	74.67	3.29	0.17	0.36
13.90	3.99	5.43	13.72	74.43	3.24	0.16	0.39
14.00	4.43	6.14	12.73	78.17	3.20	0.20	0.44
14.10	4.88	6.87	12.13	83.37	3.17	0.25	0.49
14.20	4.97	6.99	12.27	85.77	3.18	0.28	0.50
14.30	5.01	7.02	12.33	86.52	3.18	0.25	0.50
14.40	4.97	6.92	12.39	85.77	3.18	0.27	0.49

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
14.50	5.03	6.99	12.27	85.83	3.18	0.26	0.50
14.60	5.16	7.18	12.14	87.21	3.17	0.26	0.51
14.70	5.69	8.02	11.53	92.49	3.15	0.30	0.57
14.80	6.80	9.80	10.50	102.97	3.09	0.39	0.70
14.90	7.83	11.44	9.93	113.58	3.06	0.56	0.82
15.00	8.56	12.58	9.73	122.43	3.05	0.65	0.90
15.10	9.66	14.29	9.23	131.93	3.03	0.70	1.02
15.20	12.13	18.22	7.94	144.57	2.95	0.82	0.82
15.30	16.06	24.00	6.47	155.26	2.85	0.83	0.83
15.40	17.85	26.45	5.86	155.04	2.80	0.83	0.83
15.50	18.07	26.56	5.62	149.18	2.78	0.83	0.83
15.60	19.86	28.90	4.99	144.22	2.73	0.82	0.82
15.70	24.13	34.60	4.03	139.38	2.63	0.92	0.92
15.80	27.78	39.20	3.28	128.71	2.54	0.82	0.82
15.90	26.70	37.25	3.06	114.13	2.51	0.77	0.77
16.00	21.89	30.53	3.47	105.84	2.57	0.80	0.80
16.10	16.23	22.82	4.79	109.24	2.71	0.76	0.76
16.20	11.85	16.80	7.01	117.79	2.89	0.78	0.78
16.30	10.16	14.29	8.88	126.88	3.01	0.68	1.02
16.40	9.88	13.79	9.64	132.99	3.05	0.83	0.98
16.50	9.52	13.18	10.01	131.99	3.07	0.79	0.94
16.60	9.04	12.38	10.11	125.22	3.07	0.62	0.88
16.70	8.54	11.57	10.08	116.69	3.07	0.57	0.83
16.80	8.24	11.07	10.10	111.84	3.07	0.50	0.79
16.90	7.44	9.83	10.89	107.02	3.11	0.47	0.70
17.00	6.60	8.52	12.06	102.76	3.17	0.40	0.61
17.10	5.74	7.20	13.46	96.84	3.23	0.35	0.51
17.20	5.29	6.49	14.05	91.17	3.26	0.29	0.46
17.30	5.07	6.14	13.89	85.25	3.25	0.25	0.44
17.40	4.98	5.97	13.26	79.16	3.22	0.22	0.43
17.50	4.83	5.72	12.70	72.67	3.20	0.16	0.41
17.60	4.34	4.98	13.17	65.53	3.22	0.13	0.36
17.70	3.81	4.18	14.44	60.34	3.27	0.09	0.30
17.80	3.52	3.74	15.50	57.97	3.31	0.08	0.27
17.90	3.85	4.20	14.42	60.62	3.27	0.10	0.30
18.00	4.37	4.96	13.09	64.89	3.22	0.13	0.35
18.10	4.60	5.28	13.09	69.07	3.22	0.15	0.38
18.20	4.80	5.54	13.50	74.74	3.23	0.17	0.40
18.30	5.19	6.09	13.62	82.93	3.24	0.23	0.44
18.40	5.70	6.79	13.41	91.12	3.23	0.31	0.49
18.50	5.93	7.10	13.76	97.74	3.24	0.35	0.51
18.60	5.93	7.07	14.45	102.22	3.27	0.39	0.51
18.70	5.93	7.04	14.94	105.25	3.29	0.42	0.50
18.80	5.93	7.02	15.16	106.33	3.30	0.43	0.50
18.90	5.93	6.99	15.09	105.44	3.30	0.42	0.50
19.00	6.05	7.12	14.69	104.64	3.28	0.40	0.51
19.10	6.40	7.59	14.05	106.71	3.26	0.41	0.54
19.20	6.98	8.38	13.31	111.49	3.22	0.48	0.60

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
19.30	7.65	9.29	12.45	115.67	3.19	0.55	0.66
19.40	8.11	9.90	11.82	117.04	3.16	0.56	0.71
19.50	8.46	10.36	11.27	116.72	3.13	0.54	0.74
19.60	8.38	10.20	11.18	113.99	3.13	0.55	0.73
19.70	8.40	10.19	11.02	112.26	3.12	0.47	0.73
19.80	9.32	11.43	10.10	115.49	3.07	0.50	0.82
19.90	10.07	12.42	9.55	118.65	3.04	0.69	0.89
20.00	9.83	12.05	9.86	118.78	3.06	0.61	0.86
20.10	8.12	9.65	11.65	112.39	3.15	0.48	0.69
20.20	6.67	7.62	14.04	107.02	3.25	0.41	0.54
20.30	6.07	6.77	15.55	105.35	3.31	0.40	0.48
20.40	5.77	6.33	16.46	104.19	3.35	0.42	0.45
20.50	5.38	5.78	17.38	100.44	3.38	0.38	0.41
20.60	4.98	5.22	17.98	93.85	3.40	0.30	0.37
20.70	4.75	4.88	17.80	86.94	3.39	0.26	0.35
20.80	4.74	4.85	16.91	82.10	3.36	0.22	0.35
20.90	4.86	4.99	16.05	80.08	3.33	0.20	0.36
21.00	5.42	5.72	14.76	84.44	3.28	0.22	0.41
21.10	6.27	6.84	13.69	93.64	3.24	0.32	0.49
21.20	6.95	7.71	13.12	101.21	3.22	0.42	0.55
21.30	7.20	8.02	13.05	104.65	3.21	0.42	0.57
21.40	7.31	8.14	12.99	105.76	3.21	0.41	0.58
21.50	7.92	8.91	12.38	110.30	3.18	0.45	0.64
21.60	9.40	10.82	11.06	119.72	3.12	0.56	0.77
21.70	11.65	13.73	9.30	127.74	3.03	0.75	0.98
21.80	14.83	17.80	7.30	129.88	2.91	0.80	0.80
21.90	18.05	21.59	5.65	121.93	2.78	0.79	0.79
22.00	20.60	24.47	4.48	109.52	2.68	0.90	0.90
22.10	21.70	25.59	3.93	100.57	2.62	0.84	0.84
22.20	21.51	25.30	3.98	100.57	2.63	0.84	0.84
22.30	20.65	24.29	4.46	108.29	2.68	0.90	0.90
22.40	19.82	23.33	5.09	118.80	2.74	0.78	0.78
22.50	19.24	22.68	5.75	130.33	2.79	0.80	0.80
22.60	19.38	22.88	6.31	144.45	2.84	0.82	0.82
22.70	21.44	25.41	6.37	161.91	2.84	0.84	0.84
22.80	25.94	30.77	5.66	174.25	2.78	0.86	0.86
22.90	32.18	37.99	4.60	174.83	2.69	1.02	1.02
23.00	37.11	43.42	3.65	158.64	2.59	0.91	0.91
23.10	38.48	44.58	3.07	137.00	2.51	0.81	0.81
23.20	35.78	41.14	2.96	121.84	2.50	0.79	0.79
23.30	30.27	34.70	3.43	119.07	2.56	0.82	0.82
23.40	24.07	27.54	4.54	124.97	2.68	0.94	0.94
23.50	18.71	21.26	6.04	128.36	2.81	0.80	0.80
23.60	14.66	16.44	7.75	127.45	2.94	0.79	0.79
23.70	11.82	12.90	9.35	120.59	3.03	0.64	0.92
23.80	9.79	10.37	10.60	109.99	3.10	0.47	0.74
23.90	8.76	9.08	11.09	100.73	3.12	0.36	0.65
24.00	8.87	9.18	10.79	99.13	3.11	0.35	0.66

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
24.10	9.46	9.86	10.47	103.24	3.09	0.43	0.70
24.20	10.14	10.66	10.31	109.87	3.08	0.49	0.76
24.30	10.42	10.96	10.50	115.03	3.09	0.55	0.78
24.40	10.44	10.93	10.81	118.15	3.11	0.59	0.78
24.50	10.20	10.61	11.23	119.08	3.13	0.57	0.76
24.60	9.62	9.89	11.91	117.72	3.16	0.57	0.71
24.70	9.03	9.15	12.61	115.38	3.19	0.52	0.65
24.80	8.52	8.51	13.24	112.62	3.22	0.48	0.61
24.90	8.30	8.22	13.43	110.39	3.23	0.47	0.59
25.00	8.30	8.18	13.29	108.74	3.22	0.45	0.58
25.10	7.91	7.70	13.68	105.37	3.24	0.44	0.55
25.20	7.42	7.10	14.28	101.43	3.26	0.37	0.51
25.30	7.65	7.34	13.70	100.49	3.24	0.34	0.52
25.40	8.44	8.24	12.41	102.35	3.19	0.42	0.59
25.50	9.09	8.97	11.72	105.07	3.15	0.44	0.64
25.60	8.99	8.82	12.15	107.19	3.17	0.43	0.63
25.70	8.59	8.33	13.16	109.64	3.22	0.47	0.60
25.80	8.74	8.48	13.39	113.49	3.23	0.49	0.61
25.90	9.74	9.60	12.32	118.19	3.18	0.54	0.69
26.00	12.20	12.39	10.05	124.53	3.07	0.64	0.89
26.10	14.90	15.45	8.26	127.68	2.97	0.79	0.79
26.20	16.97	17.75	7.19	127.57	2.90	0.79	0.79
26.30	18.58	19.47	6.60	128.59	2.86	0.80	0.80
26.40	20.32	21.35	6.35	135.65	2.84	0.81	0.81
26.50	21.81	22.96	6.38	146.44	2.84	0.82	0.82
26.60	21.82	22.94	6.73	154.29	2.87	0.83	0.83
26.70	20.10	20.99	7.40	155.21	2.91	0.83	0.83
26.80	17.84	18.38	8.24	151.54	2.97	0.83	0.83
26.90	16.12	16.39	9.03	147.95	3.01	0.95	1.17
27.00	16.24	16.47	9.08	149.51	3.02	0.97	1.18
27.10	18.29	18.69	8.34	155.81	2.97	0.83	0.83
27.20	21.53	22.23	7.33	162.90	2.91	0.84	0.84
27.30	25.33	26.24	6.36	166.84	2.84	0.85	0.85
27.40	28.68	29.72	5.56	165.22	2.78	0.85	0.85
27.50	30.57	31.61	5.04	159.41	2.73	0.84	0.84
27.60	30.71	31.63	4.84	153.17	2.71	0.83	0.83
27.70	29.52	30.25	4.92	148.96	2.72	0.83	0.83
27.80	28.15	28.72	5.14	147.60	2.74	0.82	0.82
27.90	26.52	26.91	5.45	146.60	2.77	0.82	0.82
28.00	24.26	24.44	5.92	144.70	2.81	0.82	0.82
28.10	21.33	21.28	6.68	142.17	2.86	0.82	0.82
28.20	18.44	18.16	7.78	141.26	2.94	0.81	0.81
28.30	16.54	16.05	8.95	143.70	3.01	0.91	1.15
28.40	16.30	15.75	9.49	149.51	3.04	0.97	1.12
28.50	17.10	16.55	9.37	155.00	3.03	1.10	1.18
28.60	18.01	17.46	9.11	159.06	3.02	1.16	1.25
28.70	18.92	18.36	8.95	164.43	3.01	1.18	1.31
28.80	20.11	19.56	8.86	173.27	3.00	1.37	1.40

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
28.90	21.92	21.40	8.50	181.84	2.98	0.87	0.87
29.00	23.18	22.66	8.11	183.89	2.96	0.87	0.87
29.10	23.37	22.78	7.75	176.56	2.94	0.86	0.86
29.20	23.75	23.10	7.24	167.18	2.90	0.85	0.85
29.30	25.51	24.81	6.45	160.15	2.85	0.84	0.84
29.40	27.88	27.13	5.70	154.78	2.79	0.83	0.83
29.50	28.61	27.77	5.35	148.60	2.76	0.83	0.83
29.60	27.32	26.37	5.45	143.70	2.77	0.82	0.82
29.70	25.80	24.76	5.91	146.26	2.80	0.82	0.82
29.80	25.94	24.84	6.07	150.77	2.82	0.83	0.83
29.90	25.94	24.76	6.01	148.73	2.81	0.83	0.83
30.00	24.40	23.13	6.21	143.69	2.83	0.82	0.82
30.10	21.96	20.61	6.74	138.86	2.87	0.81	0.81
30.20	20.74	19.33	7.22	139.54	2.90	0.81	0.81
30.30	21.44	19.97	7.00	139.71	2.89	0.81	0.81
30.40	22.21	20.68	6.71	138.69	2.87	0.81	0.81
30.50	22.53	20.93	6.60	138.08	2.86	0.81	0.81
30.60	22.53	20.87	6.61	138.02	2.86	0.81	0.81
30.70	22.94	21.21	6.64	140.86	2.86	0.81	0.81
30.80	25.28	23.47	6.29	147.55	2.83	0.82	0.82
30.90	30.78	28.82	5.33	153.56	2.76	0.83	0.83
31.00	38.07	35.87	4.23	151.55	2.65	0.95	0.95
31.10	43.30	40.86	3.46	141.39	2.56	0.86	0.86
31.20	44.29	41.68	3.14	130.94	2.52	0.81	0.81
31.30	43.30	40.62	3.18	129.18	2.53	0.81	0.81
31.40	44.39	41.57	3.27	135.81	2.54	0.83	0.83
31.50	48.84	45.77	3.07	140.63	2.51	0.81	0.81
31.60	55.32	51.89	2.62	135.76	2.44	0.81	0.81
31.70	61.94	58.11	2.14	124.50	2.35	0.79	0.79
31.80	68.38	64.12	1.79	115.05	2.26	0.77	0.77
31.90	74.08	69.40	1.59	110.24	2.19	0.77	0.77
32.00	77.06	72.09	1.51	109.09	2.15	0.76	0.76
32.10	74.88	69.86	1.56	108.63	2.17	0.76	0.76
32.20	67.28	62.48	1.77	110.79	2.26	0.77	0.77
32.30	56.41	52.01	2.27	118.21	2.38	0.78	0.78
32.40	45.30	41.34	3.08	127.47	2.51	0.80	0.80
32.50	36.00	32.42	4.18	135.68	2.65	0.92	0.92
32.60	29.19	25.90	5.44	140.87	2.77	0.81	0.81
32.70	25.10	21.97	6.48	142.38	2.85	0.82	0.82
32.80	23.13	20.04	6.97	139.64	2.88	0.81	0.81
32.90	22.72	19.60	6.89	135.06	2.88	0.81	0.81
33.00	23.50	20.28	6.56	133.08	2.85	0.80	0.80
33.10	24.98	21.61	6.24	134.74	2.83	0.81	0.81
33.20	27.13	23.56	5.92	139.45	2.81	0.81	0.81
33.30	29.30	25.51	5.70	145.36	2.79	0.82	0.82
33.40	30.50	26.55	5.68	150.86	2.79	0.83	0.83
33.50	30.45	26.43	5.88	155.49	2.80	0.83	0.83
33.60	29.68	25.63	6.19	158.58	2.83	0.84	0.84

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
33.70	29.63	25.51	6.34	161.64	2.84	0.84	0.84
33.80	31.56	27.21	6.19	168.34	2.83	0.85	0.85
33.90	36.20	31.38	5.80	181.86	2.80	0.87	0.87
34.00	43.30	37.79	5.23	197.76	2.75	0.88	0.88
34.10	51.88	45.54	4.57	208.30	2.69	1.07	1.07
34.20	61.05	53.80	3.92	211.04	2.62	1.00	1.00
34.30	69.91	61.76	3.35	207.07	2.55	0.93	0.93
34.40	78.51	69.46	2.88	200.38	2.49	0.89	0.89
34.50	87.03	77.07	2.53	194.99	2.43	0.88	0.88
34.60	96.53	85.55	2.23	190.38	2.37	0.88	0.88
34.70	107.11	95.01	1.96	185.82	2.31	0.87	0.87
34.80	117.42	104.24	1.71	177.94	2.23	0.86	0.86
34.90	125.48	111.44	1.54	171.37	2.17	0.85	0.85
35.00	129.52	114.95	1.46	167.39	2.12	0.85	0.85
35.10	129.35	114.57	1.45	165.58	2.12	0.85	0.85
35.20	124.29	109.70	1.49	163.04	2.14	0.84	0.84
35.30	113.93	100.05	1.59	159.12	2.19	0.84	0.84
35.40	99.94	87.17	1.79	156.05	2.26	0.83	0.83
35.50	86.32	74.67	2.12	158.35	2.35	0.84	0.84
35.60	78.64	67.57	2.43	164.27	2.41	0.85	0.85
35.70	79.44	68.08	2.50	170.36	2.42	0.85	0.85
35.80	87.98	75.51	2.30	173.61	2.39	0.86	0.86
35.90	100.57	86.56	1.99	172.57	2.32	0.86	0.86
36.00	113.44	97.90	1.73	169.10	2.24	0.85	0.85
36.10	124.61	107.76	1.55	166.69	2.17	0.85	0.85
36.20	133.12	115.22	1.45	167.10	2.12	0.85	0.85
36.30	139.52	120.72	1.41	169.85	2.09	0.85	0.85
36.40	144.03	124.47	1.39	173.16	2.08	0.86	0.86
36.50	146.71	126.55	1.39	176.23	2.08	0.86	0.86
36.60	146.25	125.83	1.41	177.27	2.09	0.86	0.86
36.70	142.03	121.77	1.44	175.32	2.11	0.86	0.86
36.80	135.41	115.63	1.48	171.37	2.14	0.85	0.85
36.90	129.09	109.83	1.52	166.54	2.16	0.85	0.85
37.00	125.04	106.08	1.52	161.53	2.16	0.84	0.84
37.10	122.66	103.83	1.51	157.09	2.15	0.84	0.84
37.20	121.21	102.39	1.51	154.12	2.15	0.83	0.83
37.30	120.82	101.84	1.51	153.40	2.15	0.83	0.83
37.40	121.89	102.55	1.51	154.48	2.15	0.83	0.83
37.50	124.48	104.56	1.50	156.68	2.15	0.84	0.84
37.60	127.71	107.15	1.48	158.98	2.14	0.84	0.84
37.70	130.82	109.64	1.46	160.57	2.13	0.84	0.84
37.80	132.63	110.99	1.45	161.33	2.12	0.84	0.84
37.90	132.47	110.63	1.45	160.78	2.12	0.84	0.84
38.00	129.59	107.90	1.47	158.76	2.13	0.84	0.84
38.10	123.93	102.77	1.51	155.28	2.15	0.83	0.83
38.20	115.89	95.60	1.58	150.97	2.19	0.83	0.83
38.30	107.14	87.86	1.68	147.41	2.22	0.82	0.82
38.40	98.41	80.20	1.79	143.33	2.26	0.82	0.82

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
38.50	90.54	73.34	1.89	138.77	2.29	0.81	0.81
38.60	84.03	67.69	1.98	134.10	2.31	0.80	0.80
38.70	79.79	63.95	2.07	132.56	2.34	0.80	0.80
38.80	77.78	62.11	2.13	132.12	2.35	0.80	0.80
38.90	77.14	61.46	2.12	130.45	2.35	0.80	0.80
39.00	77.04	61.28	2.09	128.29	2.34	0.80	0.80
39.10	76.57	60.76	2.09	127.11	2.34	0.79	0.79
39.20	75.78	59.94	2.14	128.39	2.35	0.80	0.80
39.30	75.01	59.12	2.22	131.47	2.37	0.80	0.80
39.40	74.55	58.54	2.31	135.50	2.39	0.81	0.81
39.50	74.00	57.91	2.39	138.37	2.40	0.81	0.81
39.60	73.21	57.14	2.40	137.08	2.40	0.81	0.81
39.70	72.79	56.71	2.36	133.79	2.40	0.80	0.80
39.80	72.42	56.32	2.33	131.12	2.39	0.80	0.80
39.90	70.13	54.35	2.35	127.47	2.39	0.79	0.79
40.00	66.57	51.32	2.43	124.84	2.41	0.79	0.79
40.10	63.68	48.85	2.53	123.76	2.43	0.79	0.79
40.20	64.36	49.26	2.56	126.17	2.43	0.79	0.79
40.30	68.83	52.79	2.44	128.80	2.41	0.80	0.80
40.40	77.61	59.87	2.19	130.84	2.36	0.80	0.80
40.50	91.92	71.57	1.86	133.06	2.28	0.80	0.80
40.60	111.46	87.73	1.57	137.70	2.18	0.81	0.81
40.70	133.56	106.20	1.39	147.50	2.08	0.82	0.82
40.80	153.43	122.84	1.31	160.84	2.00	0.84	0.84
40.90	167.80	134.76	1.28	172.18	1.96	0.86	0.86
41.00	176.80	142.18	1.26	179.01	1.93	0.86	0.86
41.10	182.80	147.00	1.25	183.71	1.92	0.87	0.87
41.20	187.72	150.81	1.25	188.04	1.92	0.87	0.87
41.30	191.80	153.71	1.25	192.76	1.93	0.88	0.88
41.40	194.68	155.63	1.26	196.20	1.94	0.88	0.88
41.50	197.00	157.18	1.26	198.54	1.94	0.89	0.89
41.60	199.27	158.73	1.26	200.53	1.94	0.89	0.89
41.70	202.25	160.87	1.26	203.05	1.94	0.89	0.89
41.80	205.69	163.33	1.26	206.23	1.94	0.89	0.89
41.90	209.24	165.81	1.27	209.96	1.94	0.90	0.90
42.00	212.51	168.04	1.27	213.39	1.95	0.90	0.90
42.10	214.98	169.66	1.27	215.83	1.95	0.90	0.90
42.20	216.82	170.83	1.27	217.24	1.95	0.90	0.90
42.30	217.44	171.05	1.27	217.32	1.95	0.90	0.90
42.40	215.99	169.56	1.27	215.68	1.95	0.90	0.90
42.50	212.38	166.26	1.28	212.38	1.96	0.90	0.90
42.60	207.75	162.14	1.28	208.26	1.97	0.90	0.90
42.70	203.54	158.42	1.29	204.30	1.98	0.89	0.89
42.80	199.98	155.27	1.29	200.66	1.98	0.89	0.89
42.90	196.07	151.85	1.30	196.82	1.99	0.88	0.88
43.00	191.21	147.63	1.30	192.48	2.00	0.88	0.88
43.10	185.37	142.60	1.31	187.51	2.01	0.87	0.87
43.20	179.37	137.43	1.33	182.72	2.03	0.87	0.87

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
43.30	174.19	132.95	1.34	178.78	2.04	0.86	0.86
43.40	170.22	129.47	1.36	175.77	2.05	0.86	0.86
43.50	166.83	126.51	1.37	173.01	2.06	0.86	0.86
43.60	162.46	122.78	1.38	169.39	2.07	0.85	0.85
43.70	156.00	117.35	1.41	164.91	2.09	0.85	0.85
43.80	147.22	110.07	1.45	159.59	2.12	0.84	0.84
43.90	136.83	101.53	1.52	154.22	2.16	0.83	0.83
44.00	126.19	92.88	1.61	149.55	2.20	0.83	0.83
44.10	116.68	85.22	1.71	145.40	2.23	0.82	0.82
44.20	109.12	79.22	1.77	140.29	2.26	0.81	0.81
44.30	103.32	74.80	1.76	131.81	2.25	0.80	0.80
44.40	98.06	70.93	1.70	120.62	2.23	0.78	0.78
44.50	92.45	66.83	1.64	109.45	2.21	0.77	0.77
44.60	86.05	61.96	1.64	101.53	2.21	0.75	0.75
44.70	79.77	56.96	1.74	98.89	2.24	0.75	0.75
44.80	74.72	52.81	1.91	100.74	2.30	0.75	0.75
44.90	71.40	50.06	2.06	102.88	2.33	0.75	0.75
45.00	69.26	48.29	2.15	103.62	2.35	0.75	0.75
45.10	69.08	48.01	2.20	105.41	2.36	0.76	0.76
45.20	73.88	51.46	2.13	109.83	2.35	0.77	0.77
45.30	86.95	61.29	1.87	114.69	2.29	0.77	0.77
45.40	107.24	76.96	1.56	120.09	2.18	0.78	0.78
45.50	130.79	95.46	1.38	131.29	2.07	0.80	0.80
45.60	152.68	112.72	1.30	146.32	1.99	0.82	0.82
45.70	171.44	127.47	1.26	160.76	1.94	0.84	0.84
45.80	188.25	140.48	1.24	174.46	1.91	0.86	0.86
45.90	205.84	154.08	1.22	188.59	1.88	0.87	0.87
46.00	224.66	168.78	1.20	202.68	1.85	0.89	0.89
46.10	242.48	182.92	1.17	213.72	1.81	0.90	0.90
46.20	256.90	194.52	1.13	219.56	1.78	0.91	0.91
46.30	266.83	202.14	1.11	224.94	1.77	0.91	0.91
46.40	272.73	206.29	1.12	230.21	1.77	0.92	0.92
46.50	275.32	207.95	1.12	232.12	1.77	0.92	0.92
46.60	276.13	208.29	1.11	232.18	1.77	0.92	0.92
46.70	276.72	208.48	1.11	231.87	1.77	0.92	0.92
46.80	278.32	208.95	1.13	236.67	1.78	0.92	0.92
46.90	282.43	211.50	1.14	241.72	1.79	0.93	0.93
47.00	288.11	215.55	1.14	245.68	1.79	0.93	0.93
47.10	291.48	218.17	1.12	244.99	1.78	0.93	0.93
47.20	287.17	214.60	1.12	241.01	1.78	0.93	0.93
47.30	273.91	203.55	1.15	234.91	1.80	0.92	0.92
47.40	254.36	187.22	1.20	224.98	1.85	0.91	0.91
47.50	231.51	168.39	1.25	209.93	1.91	0.90	0.90
47.60	207.31	148.87	1.29	192.44	1.98	0.88	0.88
47.70	183.14	129.76	1.35	175.74	2.05	0.86	0.86
47.80	161.34	112.83	1.44	162.17	2.11	0.84	0.84
47.90	147.04	101.74	1.52	155.05	2.16	0.83	0.83
48.00	144.37	99.47	1.56	154.69	2.17	0.83	0.83

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
48.10	154.30	106.68	1.50	160.14	2.15	0.84	0.84
48.20	174.92	122.07	1.40	171.37	2.09	0.85	0.85
48.30	203.69	144.04	1.31	189.13	2.01	0.87	0.87
48.40	238.64	171.26	1.25	213.37	1.91	0.90	0.90
48.50	272.42	198.09	1.18	233.98	1.83	0.92	0.92
48.60	297.48	218.17	1.11	242.89	1.77	0.93	0.93
48.70	309.01	227.10	1.08	245.68	1.75	0.93	0.93
48.80	310.28	227.31	1.10	249.99	1.76	0.94	0.94
48.90	308.58	224.81	1.14	255.28	1.79	0.94	0.94
49.00	308.74	223.69	1.16	260.57	1.81	0.95	0.95
49.10	309.55	223.18	1.19	264.58	1.83	0.95	0.95
49.20	307.77	220.85	1.20	265.53	1.85	0.95	0.95
49.30	300.75	214.88	1.21	260.96	1.87	0.95	0.95
49.40	287.55	204.67	1.22	250.19	1.88	0.94	0.94
49.50	266.11	188.68	1.23	231.85	1.89	0.92	0.92
49.60	239.13	168.63	1.24	209.07	1.90	0.90	0.90
49.70	219.20	153.76	1.25	192.28	1.92	0.88	0.88

Abbreviations

q_t :	Total cone resistance
K_c :	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c :	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

LIQUEFACTION ANALYSIS REPORT

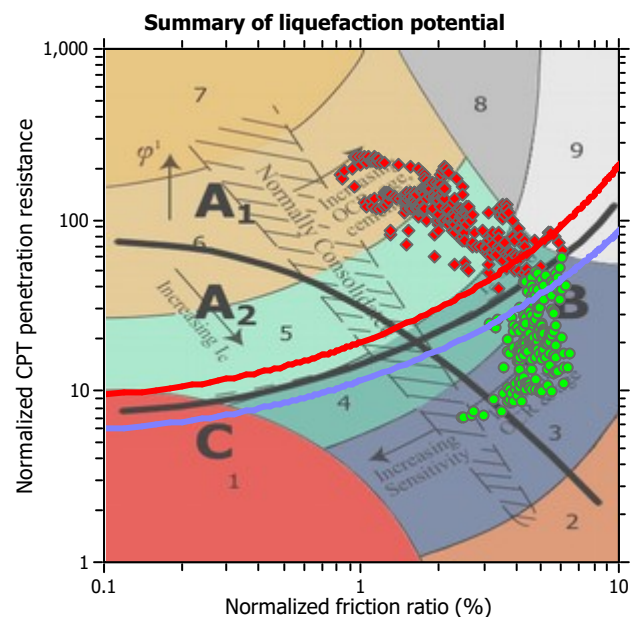
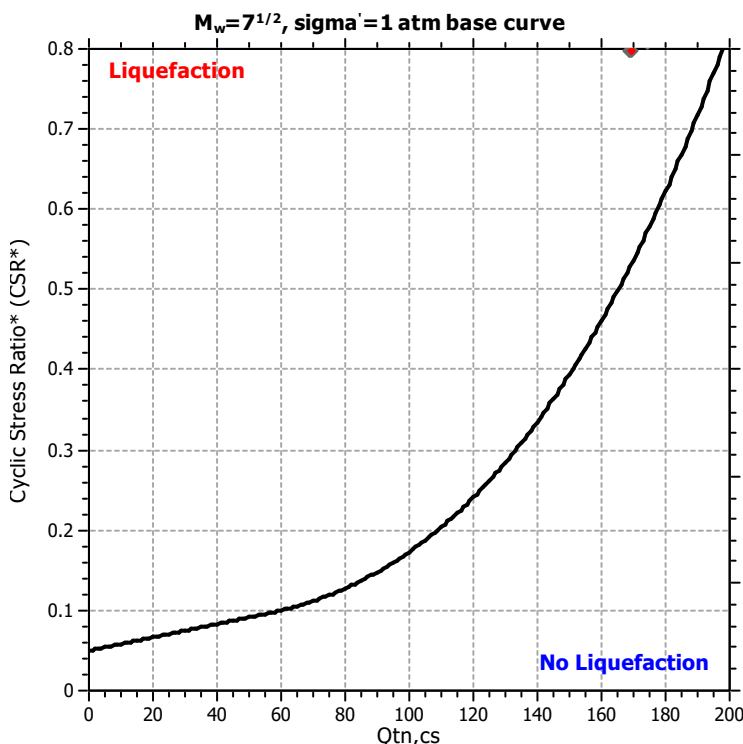
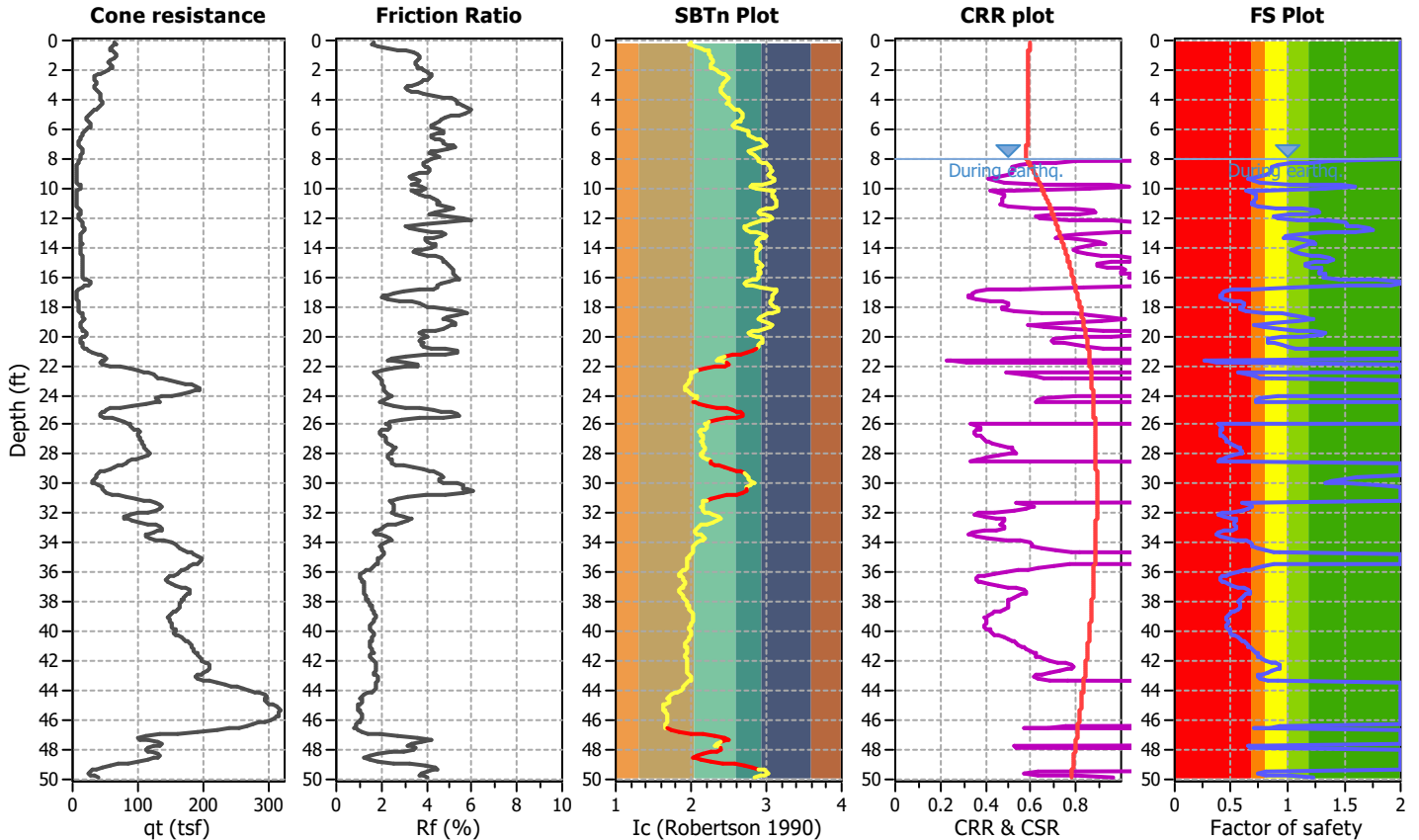
Project title : 21-483 Equestrian Estates

Location : Avenue 64 at Harrison Street, Thermal California

CPT file : CPT-7 Robt 2009

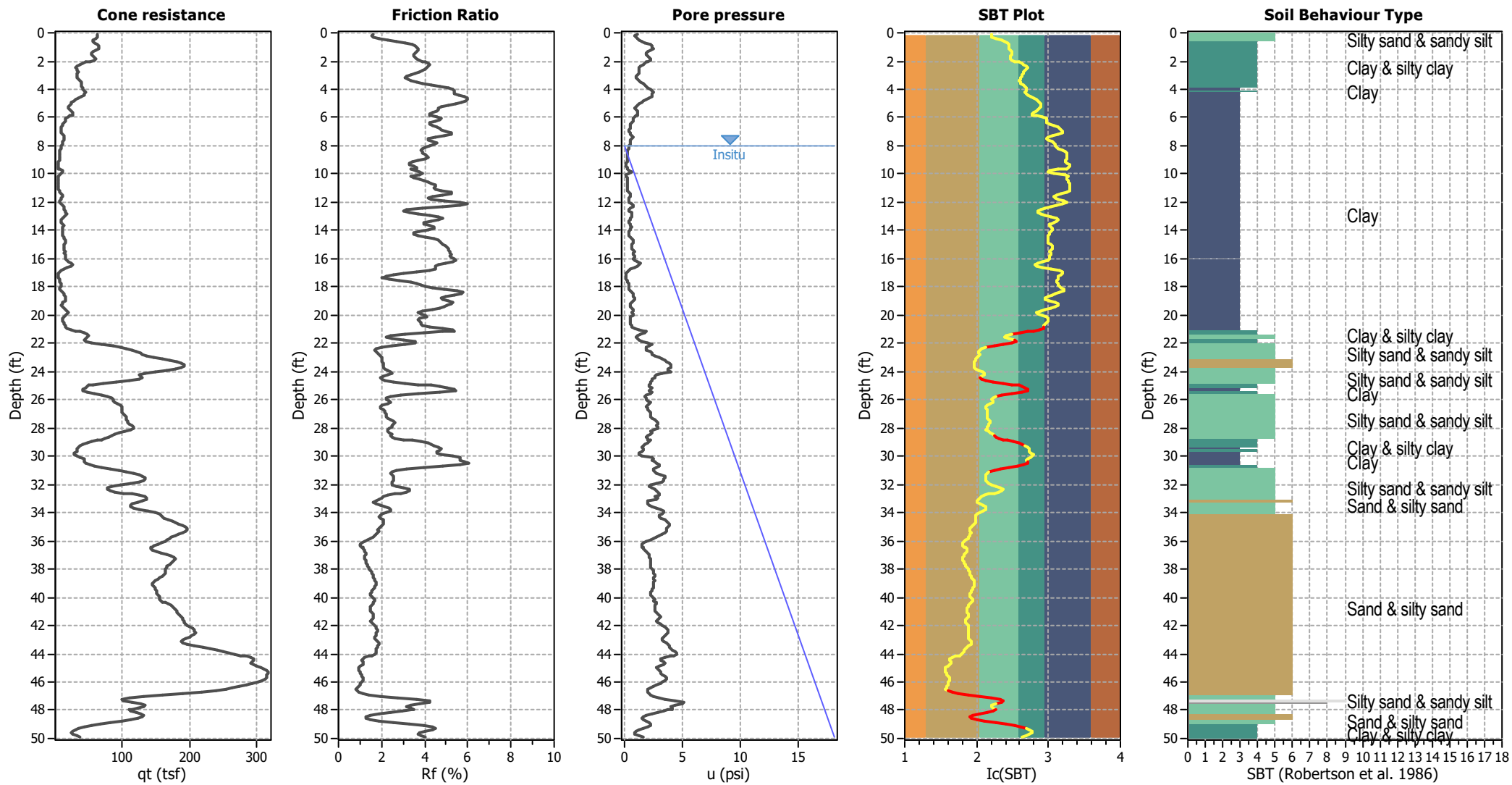
Input parameters and analysis data

Analysis method:	Robertson (2009)	G.W.T. (in-situ):	8.00 ft	Use fill:	No	Clay like behavior	
Fines correction method:	Robertson (2009)	G.W.T. (earthq.):	8.00 ft	Fill height:	N/A	applied:	All soils
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude M_w :	7.34	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.74	Unit weight calculation:	Based on SBT	K_o applied:	No	MSF method:	Method based



Zone A1: Cyclic liquefaction likely depending on size and duration of cyclic loading
 Zone A2: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
 Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
 Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



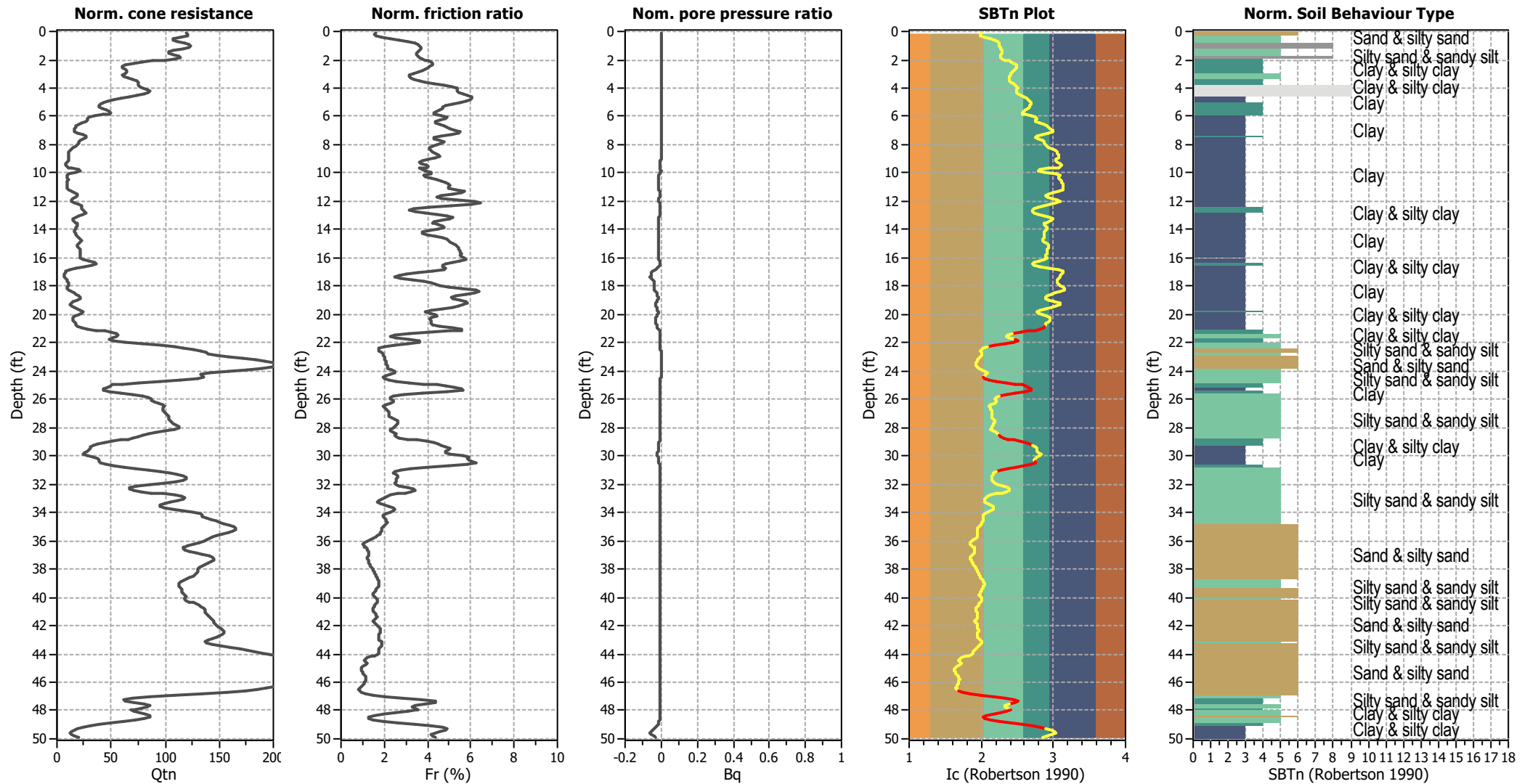
Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	No
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

SBT legend

1. Sensitive fine grained	4. Clayey silt to silty	7. Gravely sand to sand
2. Organic material	5. Silty sand to sandy silt	8. Very stiff sand to
3. Clay to silty clay	6. Clean sand to silty sand	9. Very stiff fine grained

CPT basic interpretation plots (normalized)



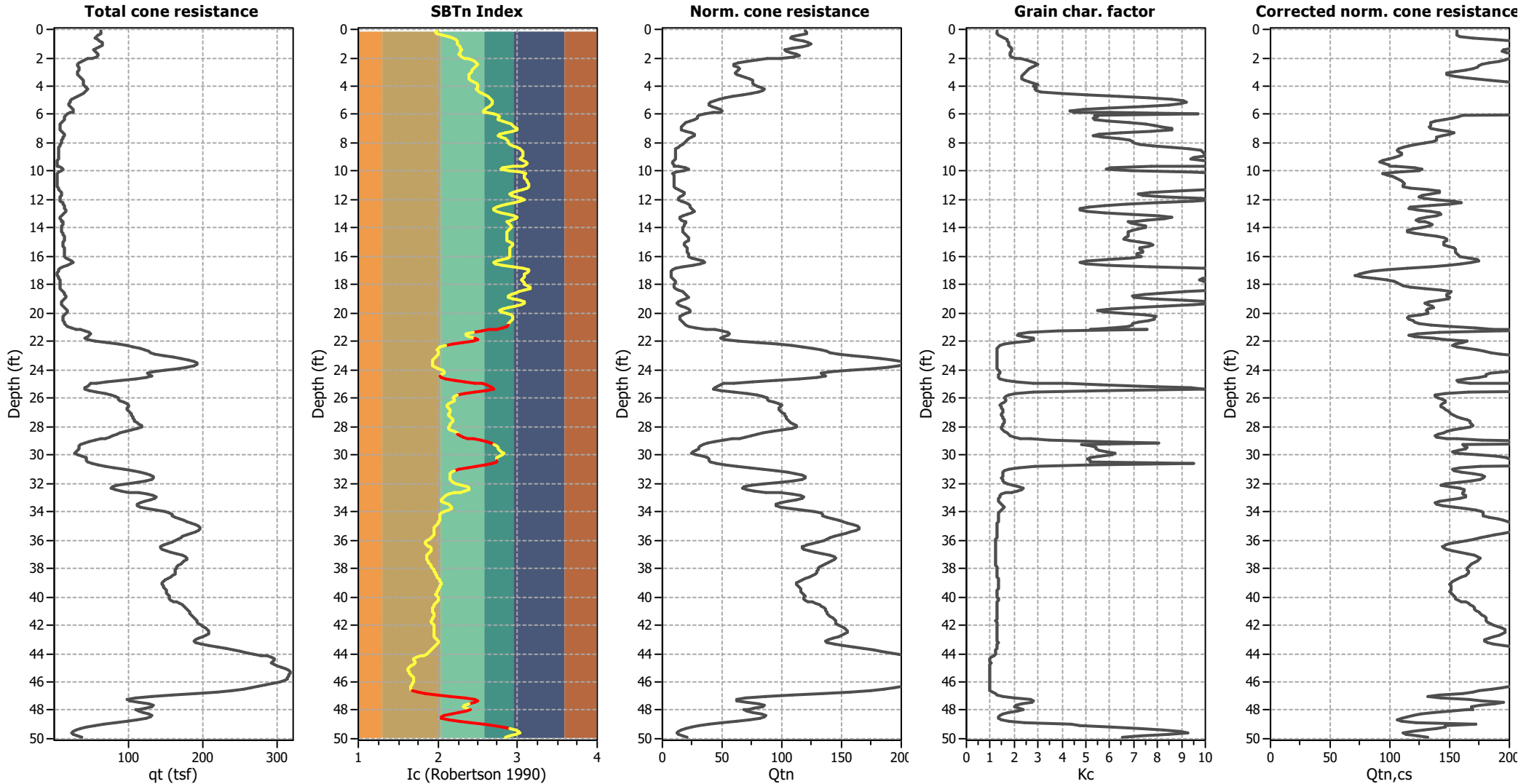
Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	No
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

SBTn legend

1. Sensitive fine grained	4. Clayey silt to silty	7. Gravely sand to sand
2. Organic material	5. Silty sand to sandy silt	8. Very stiff sand to
3. Clay to silty clay	6. Clean sand to silty sand	9. Very stiff fine grained

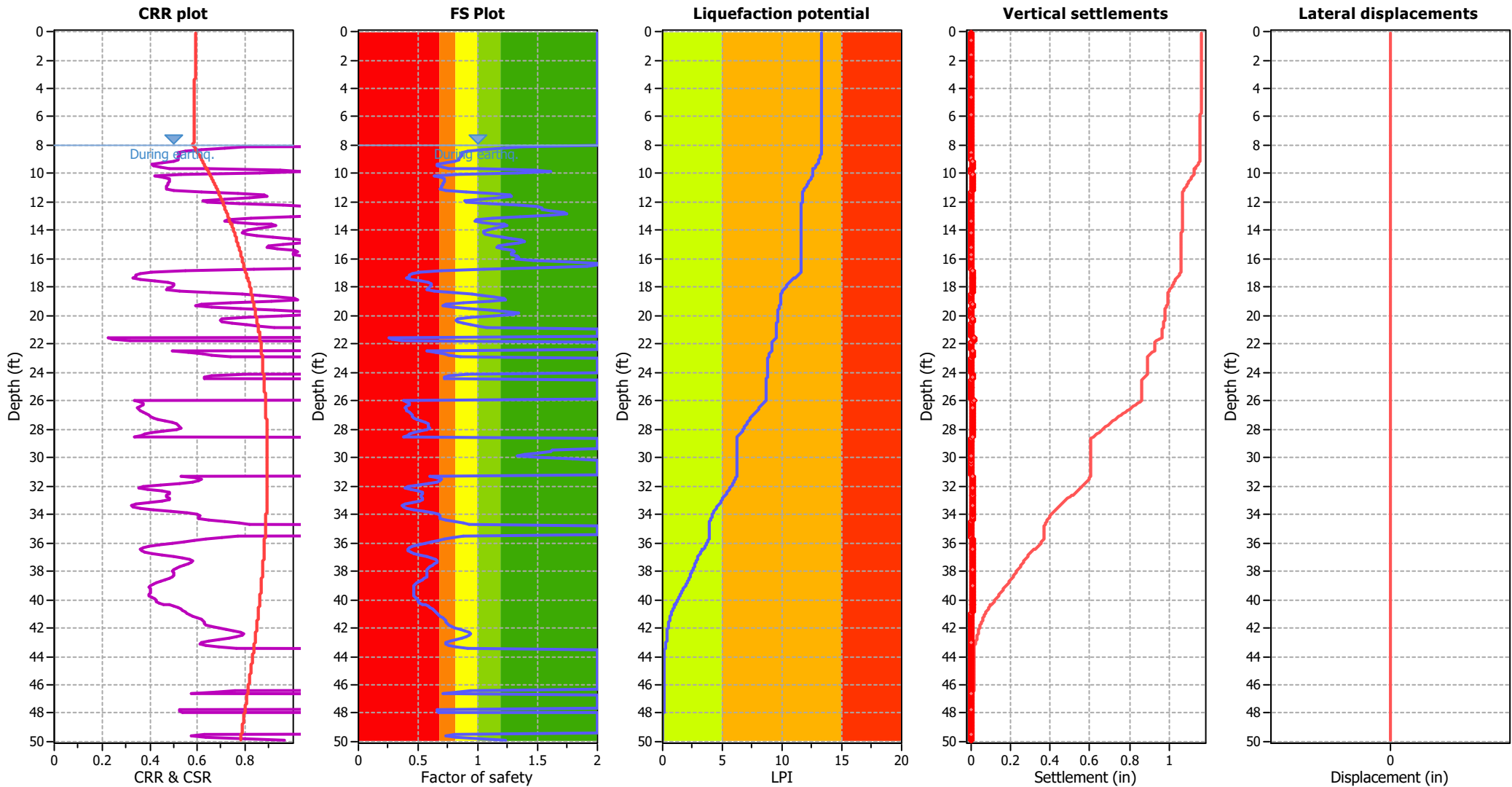
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	No
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (earthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	No
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

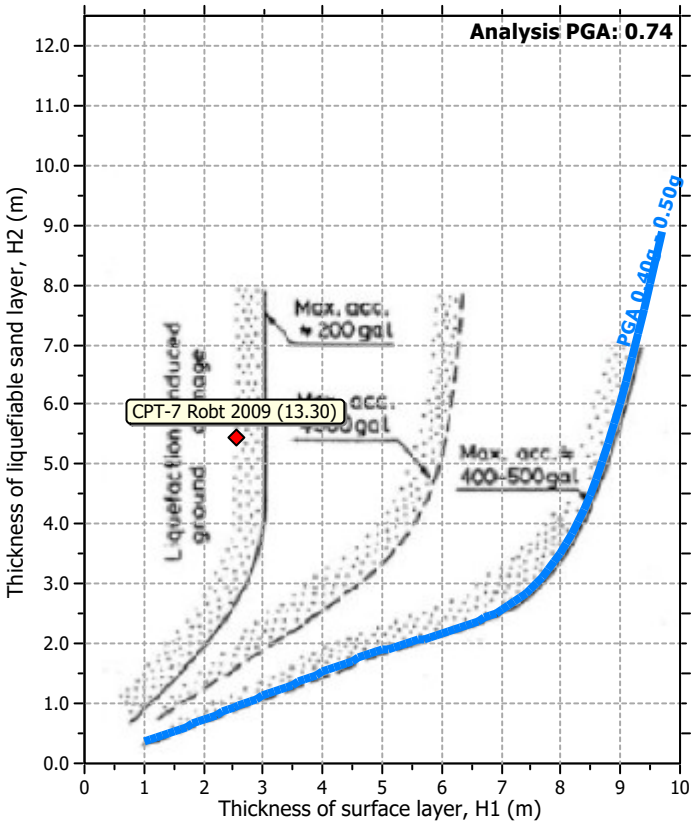
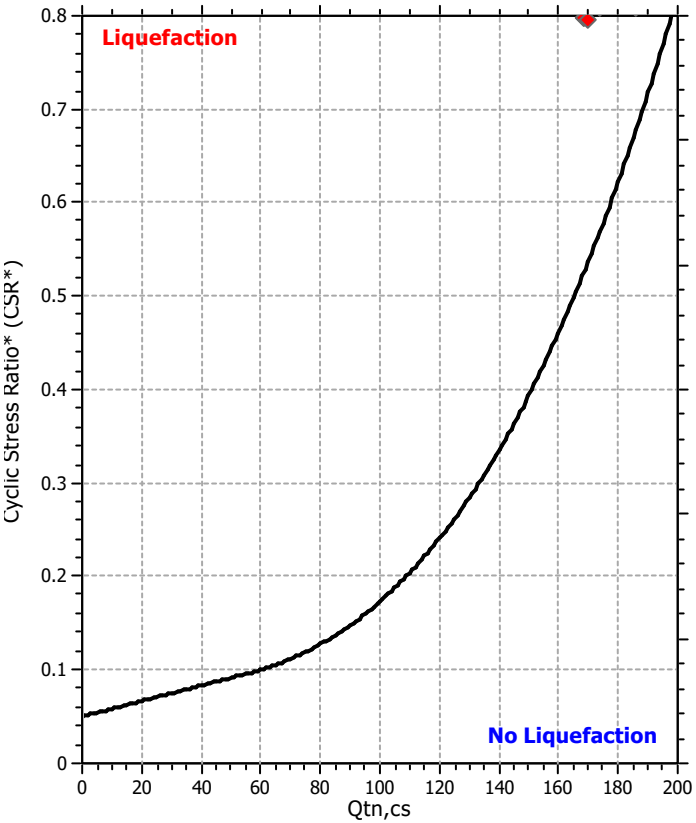
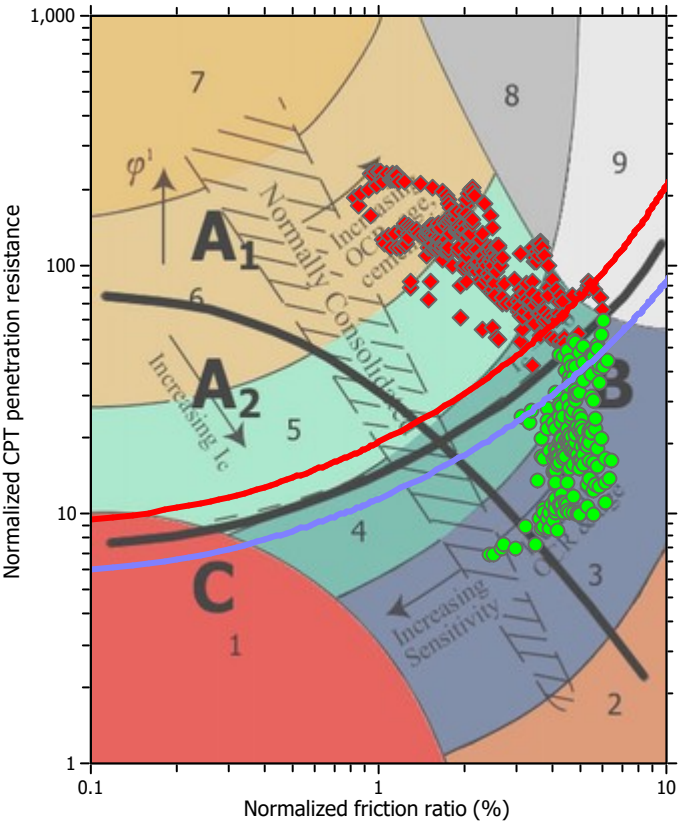
F.S. color scheme

- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

LPI color scheme

- Very high risk
- High risk
- Low risk

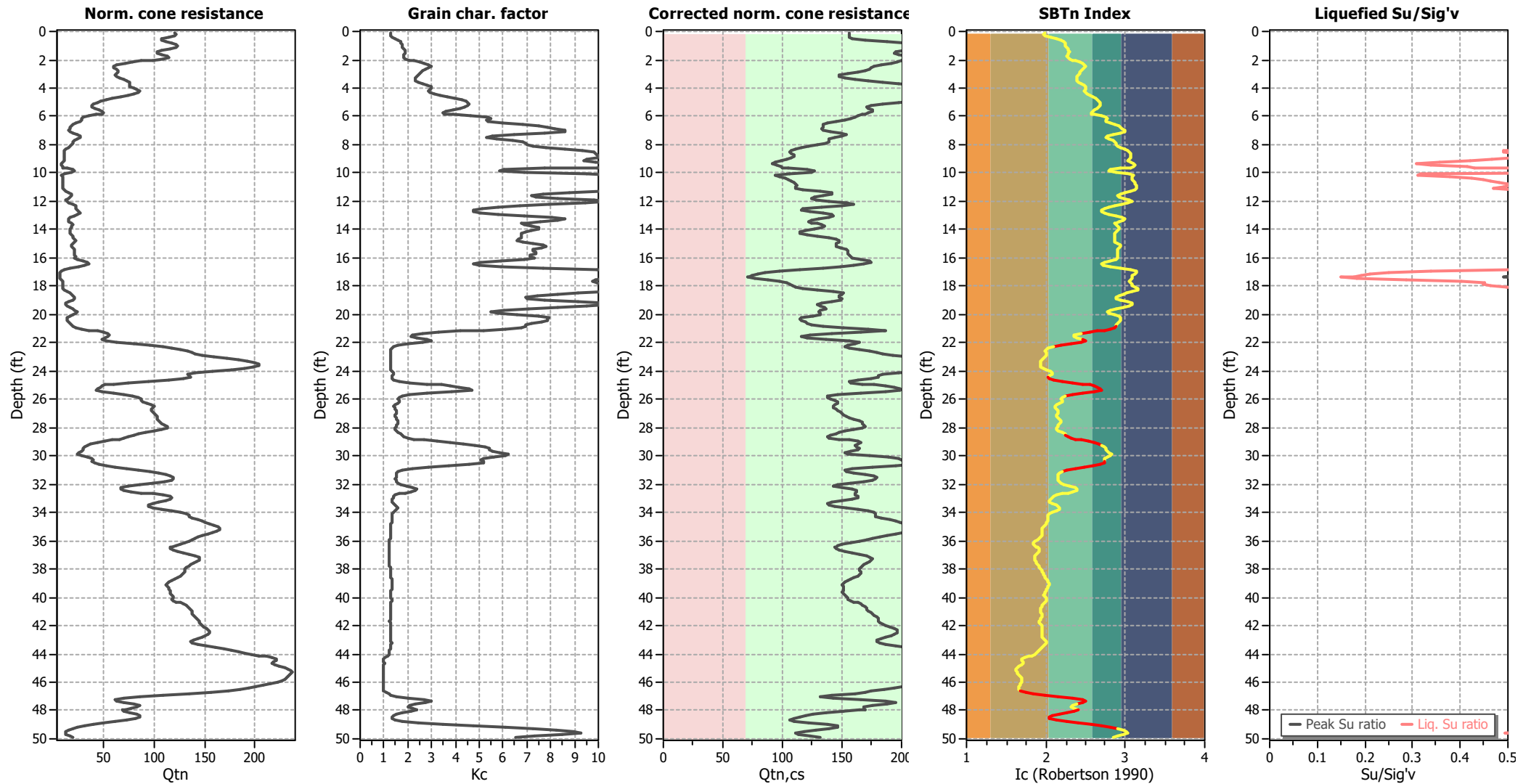
Liquefaction analysis summary plots



Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on I_c value	I_c cut-off value:	2.60	K_o applied:	No
Earthquake magnitude M_w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

Check for strength loss plots (Robertson (2010))



Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on I_c value	I_c cut-off value:	2.60	K_o applied:	No
Earthquake magnitude M_w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

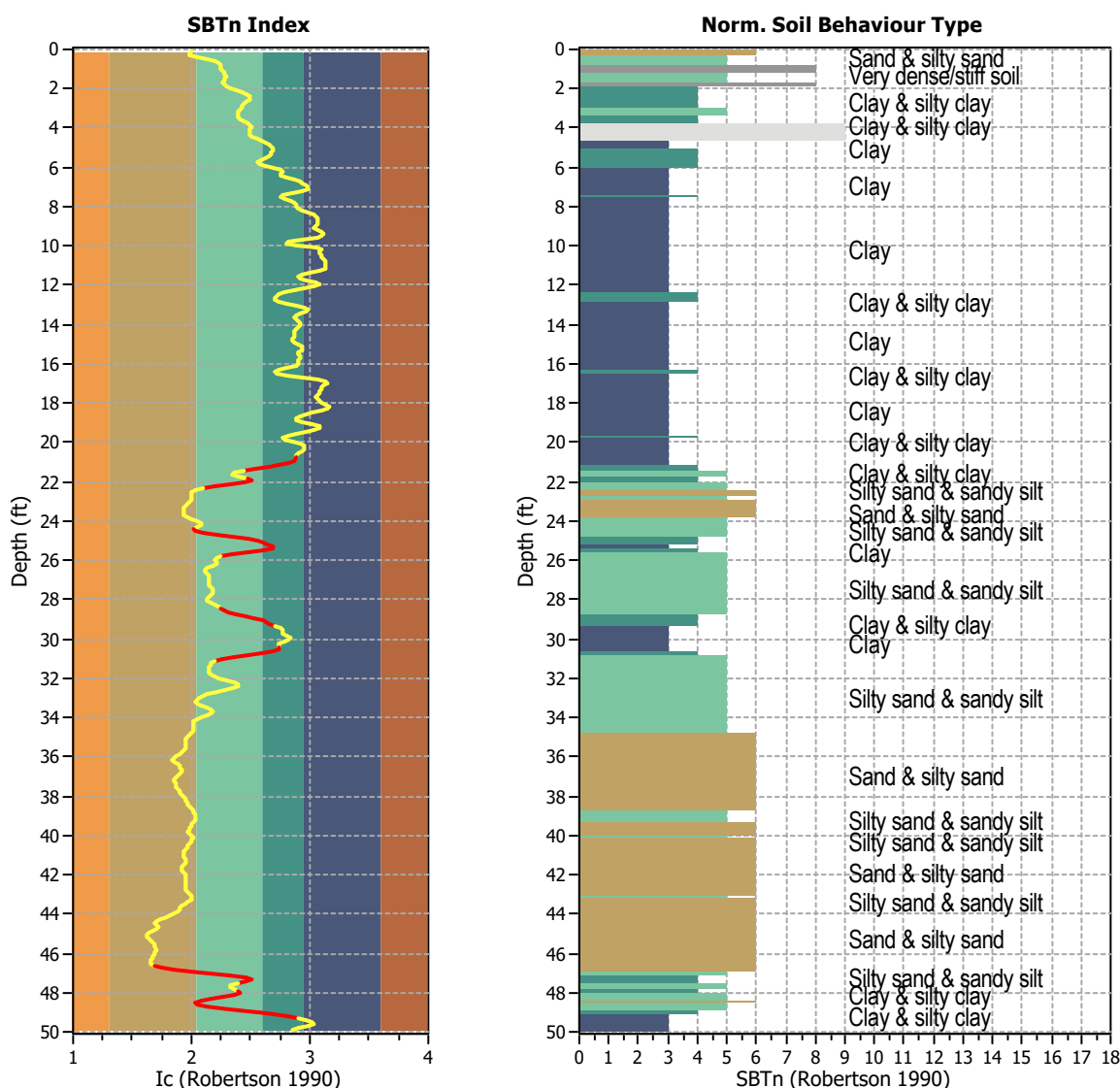
TRANSITION LAYER DETECTION ALGORITHM REPORT

Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vice-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between $1.80 < I_c < 3.0$) and a rate of change of I_c . Transitions typically occur when the rate of change of I_c is fast (i.e. ΔI_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties

I_c minimum check value: 1.70
 I_c maximum check value: 3.00
 I_c change ratio value: 0.0250
 Minimum number of points in layer: 4

General statistics

Total points in CPT file: 499
 Total points excluded: 71
 Exclusion percentage: 14.23%
 Number of layers detected: 10

Transition layer No	Number of points	Depth	SBT _n number	SBT _n description
Transition layer 1	7	Start depth: 20.90 (ft)	3	Clay
		End depth: 21.50 (ft)	5	Silty sand & sandy silt
Transition layer 2	6	Start depth: 21.90 (ft)	4	Clay & silty clay
		End depth: 22.40 (ft)	5	Silty sand & sandy silt
Transition layer 3	9	Start depth: 24.50 (ft)	5	Silty sand & sandy silt
		End depth: 25.30 (ft)	3	Clay
Transition layer 4	6	Start depth: 25.40 (ft)	3	Clay
		End depth: 25.90 (ft)	5	Silty sand & sandy silt
Transition layer 5	9	Start depth: 28.60 (ft)	5	Silty sand & sandy silt
		End depth: 29.40 (ft)	3	Clay
Transition layer 6	8	Start depth: 30.50 (ft)	3	Clay
		End depth: 31.20 (ft)	5	Silty sand & sandy silt
Transition layer 7	7	Start depth: 46.70 (ft)	6	Sand & silty sand
		End depth: 47.30 (ft)	4	Clay & silty clay
Transition layer 8	4	Start depth: 47.30 (ft)	4	Clay & silty clay
		End depth: 47.60 (ft)	5	Silty sand & sandy silt
Transition layer 9	6	Start depth: 48.00 (ft)	4	Clay & silty clay
		End depth: 48.50 (ft)	6	Sand & silty sand
Transition layer 10	9	Start depth: 48.60 (ft)	5	Silty sand & sandy silt
		End depth: 49.40 (ft)	3	Clay

Start depth: Depth where the transition layer begins

End depth: Depth where the transition layer ends

:: Field input data ::						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1	0.10	62.12	1.11	1.11	12.86	120.61
2	0.20	65.67	0.88	0.88	12.36	120.37
3	0.30	64.54	1.00	1.00	12.58	120.43
4	0.40	60.51	1.14	1.14	14.54	121.22
5	0.50	56.13	1.28	1.28	16.79	122.03
6	0.60	54.87	1.47	1.47	18.69	123.18
7	0.70	58.51	1.82	1.82	19.86	124.64
8	0.80	63.65	2.21	2.21	20.42	125.87
9	0.90	65.07	2.35	2.35	20.65	126.55
10	1.00	65.20	2.36	2.36	20.78	126.84
11	1.10	66.36	2.45	2.45	21.04	126.76
12	1.20	62.10	2.31	2.31	21.48	126.33
13	1.30	56.71	2.05	2.05	22.02	125.47
14	1.40	52.83	1.85	1.85	22.20	124.82
15	1.50	54.10	1.87	1.87	21.95	124.79
16	1.60	57.95	2.02	2.02	21.63	125.21
17	1.70	59.39	2.11	2.11	21.40	125.75
18	1.80	61.72	2.24	2.24	21.53	126.06
19	1.90	60.58	2.25	2.25	22.33	125.82
20	2.00	51.35	2.00	2.00	23.76	125.16
21	2.10	46.06	1.87	1.87	25.62	124.29
22	2.20	42.60	1.79	1.79	27.21	123.50
23	2.30	37.67	1.60	1.60	28.72	122.52
24	2.40	32.86	1.38	1.38	30.08	121.38
25	2.50	30.55	1.26	1.26	30.56	120.66
26	2.60	31.93	1.28	1.28	30.07	120.55
27	2.70	33.72	1.31	1.31	29.15	120.75
28	2.80	34.59	1.31	1.31	28.26	120.79
29	2.90	35.10	1.26	1.26	27.78	120.28
30	3.00	32.25	1.07	1.07	27.21	119.57
31	3.10	32.25	1.00	1.00	26.74	118.93
32	3.20	32.91	1.00	1.00	26.29	119.03
33	3.30	34.32	1.09	1.09	26.07	119.68
34	3.40	36.94	1.24	1.24	25.97	120.69
35	3.50	39.82	1.41	1.41	26.17	121.72
36	3.60	40.61	1.57	1.57	26.90	122.59
37	3.70	40.38	1.73	1.73	28.23	123.28
38	3.80	39.72	1.88	1.88	29.63	123.93
39	3.90	40.08	2.06	2.06	30.58	124.61
40	4.00	42.01	2.25	2.25	30.73	125.32
41	4.10	44.76	2.42	2.42	30.30	125.84
42	4.20	46.13	2.44	2.44	30.00	126.06
43	4.30	45.11	2.41	2.41	30.31	126.02
44	4.40	43.15	2.41	2.41	31.41	125.81
45	4.50	39.94	2.35	2.35	33.04	125.35
46	4.60	35.50	2.15	2.15	34.85	124.51
47	4.70	31.31	1.89	1.89	36.67	123.32
48	4.80	27.40	1.62	1.62	38.05	122.08

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
49	4.90	25.36	1.45	1.45	39.04	120.85
50	5.00	23.26	1.26	1.26	39.50	119.69
51	5.10	21.46	1.09	1.09	39.62	118.52
52	5.20	20.47	0.97	0.97	39.40	117.63
53	5.30	20.31	0.93	0.93	38.89	117.40
54	5.40	21.51	1.00	1.00	37.81	117.90
55	5.50	24.20	1.11	1.11	36.16	118.69
56	5.60	26.63	1.17	1.17	34.54	119.19
57	5.70	27.19	1.15	1.15	33.69	119.18
58	5.80	26.09	1.08	1.08	34.02	118.82
59	5.90	24.20	1.04	1.04	36.19	117.88
60	6.00	18.70	0.87	0.87	40.05	116.46
61	6.10	14.43	0.71	0.71	43.63	115.26
62	6.20	15.81	0.76	0.76	44.36	114.70
63	6.30	16.36	0.73	0.73	43.33	114.37
64	6.40	14.76	0.61	0.61	43.82	113.29
65	6.50	12.58	0.52	0.52	46.47	111.81
66	6.60	10.49	0.46	0.46	50.25	110.66
67	6.70	9.56	0.45	0.45	53.27	110.07
68	6.80	9.56	0.45	0.45	54.66	109.83
69	6.90	9.28	0.44	0.44	56.00	109.52
70	7.00	8.34	0.41	0.41	57.63	109.42
71	7.10	8.53	0.45	0.45	57.76	110.14
72	7.20	10.24	0.56	0.56	54.15	111.75
73	7.30	13.08	0.67	0.67	48.64	113.29
74	7.40	15.78	0.70	0.70	44.63	113.79
75	7.50	15.32	0.61	0.61	43.44	113.29
76	7.60	13.16	0.53	0.53	45.32	112.25
77	7.70	11.50	0.52	0.52	48.51	111.58
78	7.80	11.15	0.52	0.52	50.36	111.28
79	7.90	11.15	0.50	0.50	50.81	110.77
80	8.00	10.29	0.43	0.43	51.12	109.83
81	8.10	9.38	0.37	0.37	52.33	108.55
82	8.20	8.44	0.32	0.32	54.41	107.26
83	8.30	7.38	0.28	0.28	57.67	105.89
84	8.40	6.21	0.24	0.24	60.69	104.85
85	8.50	6.16	0.24	0.24	62.40	104.43
86	8.60	6.37	0.25	0.25	62.61	104.68
87	8.70	6.37	0.26	0.26	62.98	104.97
88	8.80	6.30	0.27	0.27	63.52	104.95
89	8.90	6.17	0.25	0.25	62.96	104.65
90	9.00	6.31	0.23	0.23	61.40	104.09
91	9.10	6.37	0.21	0.21	60.92	103.19
92	9.20	5.58	0.18	0.18	62.72	102.02
93	9.30	4.78	0.16	0.16	65.72	101.25
94	9.40	4.94	0.17	0.17	66.65	101.70
95	9.50	5.65	0.21	0.21	65.12	102.72
96	9.60	5.97	0.22	0.22	62.99	103.28

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
97	9.70	6.07	0.21	0.21	54.27	105.40
98	9.80	11.23	0.35	0.35	46.96	109.41
99	9.90	16.32	0.63	0.63	45.98	110.74
100	10.00	9.46	0.40	0.40	50.63	109.22
101	10.10	4.78	0.17	0.17	61.38	104.46
102	10.20	5.12	0.16	0.16	65.59	101.63
103	10.30	5.83	0.20	0.20	63.94	102.57
104	10.40	5.97	0.22	0.22	63.85	103.56
105	10.50	5.97	0.24	0.24	64.87	104.08
106	10.60	5.97	0.25	0.25	65.90	104.43
107	10.70	5.97	0.26	0.26	66.82	104.72
108	10.80	5.97	0.27	0.27	67.67	104.98
109	10.90	5.97	0.28	0.28	68.01	105.06
110	11.00	5.97	0.27	0.27	67.85	104.94
111	11.10	5.97	0.26	0.26	67.94	105.00
112	11.20	6.04	0.28	0.28	67.45	106.17
113	11.30	7.21	0.38	0.38	63.75	108.66
114	11.40	10.03	0.55	0.55	58.43	110.65
115	11.50	11.35	0.56	0.56	53.98	111.43
116	11.60	11.35	0.48	0.48	51.85	110.88
117	11.70	10.78	0.43	0.43	52.74	109.75
118	11.80	8.88	0.38	0.38	56.55	108.82
119	11.90	7.64	0.37	0.37	62.43	108.53
120	12.00	7.53	0.43	0.43	64.58	109.85
121	12.10	9.60	0.60	0.60	61.12	112.05
122	12.20	12.53	0.75	0.75	55.12	113.62
123	12.30	14.26	0.71	0.71	49.91	113.74
124	12.40	14.57	0.55	0.55	45.65	112.53
125	12.50	14.33	0.43	0.43	42.45	111.26
126	12.60	15.10	0.43	0.43	40.64	111.53
127	12.70	17.53	0.57	0.57	40.67	112.76
128	12.80	17.50	0.65	0.65	42.20	113.85
129	12.90	16.02	0.68	0.68	45.76	113.83
130	13.00	13.08	0.62	0.62	50.73	112.89
131	13.10	10.27	0.51	0.51	55.51	111.47
132	13.20	9.56	0.45	0.45	57.78	110.10
133	13.30	9.56	0.40	0.40	56.50	109.40
134	13.40	10.05	0.39	0.39	53.61	109.60
135	13.50	11.78	0.46	0.46	51.23	110.49
136	13.60	12.90	0.52	0.52	50.18	111.43
137	13.70	12.74	0.54	0.54	50.60	111.99
138	13.80	12.58	0.57	0.57	52.07	111.96
139	13.90	11.65	0.53	0.53	53.13	111.53
140	14.00	11.15	0.47	0.47	53.18	110.70
141	14.10	11.15	0.42	0.42	52.04	109.85
142	14.20	11.15	0.38	0.38	50.88	109.28
143	14.30	11.16	0.37	0.37	50.20	109.46
144	14.40	12.06	0.44	0.44	50.15	110.44

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
145	14.50	12.99	0.53	0.53	50.14	111.85
146	14.60	13.93	0.62	0.62	50.06	113.12
147	14.70	14.88	0.69	0.69	49.55	114.09
148	14.80	15.80	0.75	0.75	49.44	114.51
149	14.90	15.15	0.72	0.72	50.36	114.29
150	15.00	13.46	0.65	0.65	52.23	113.71
151	15.10	12.74	0.63	0.63	53.98	113.27
152	15.20	12.74	0.64	0.64	54.50	113.33
153	15.30	13.23	0.67	0.67	53.67	113.93
154	15.40	14.80	0.76	0.76	52.31	114.72
155	15.50	15.88	0.82	0.82	52.17	114.92
156	15.60	13.94	0.72	0.72	52.62	114.87
157	15.70	14.32	0.75	0.75	52.66	114.94
158	15.80	16.07	0.84	0.84	51.78	115.33
159	15.90	15.89	0.82	0.82	51.70	115.48
160	16.00	14.87	0.79	0.79	52.38	115.58
161	16.10	15.70	0.88	0.88	50.63	116.73
162	16.20	20.96	1.14	1.14	46.27	118.49
163	16.30	26.45	1.33	1.33	42.36	119.66
164	16.40	27.11	1.24	1.24	40.60	119.63
165	16.50	24.54	1.07	1.07	41.87	118.34
166	16.60	18.69	0.84	0.84	46.34	115.95
167	16.70	12.01	0.56	0.56	53.94	112.58
168	16.80	8.20	0.35	0.35	63.04	108.53
169	16.90	6.52	0.23	0.23	68.24	104.90
170	17.00	5.97	0.17	0.17	68.56	102.33
171	17.10	5.97	0.15	0.15	66.69	100.78
172	17.20	5.97	0.13	0.13	64.81	99.93
173	17.30	5.97	0.12	0.12	64.79	99.07
174	17.40	5.42	0.11	0.11	64.52	98.97
175	17.50	6.03	0.13	0.13	64.03	100.62
176	17.60	7.35	0.20	0.20	62.75	103.49
177	17.70	8.34	0.28	0.28	62.31	105.74
178	17.80	8.53	0.32	0.32	62.86	106.83
179	17.90	8.36	0.32	0.32	63.84	107.19
180	18.00	8.36	0.33	0.33	64.95	107.44
181	18.10	8.36	0.36	0.36	67.40	107.80
182	18.20	7.76	0.38	0.38	69.99	108.61
183	18.30	8.26	0.46	0.46	69.58	110.41
184	18.40	10.77	0.64	0.64	64.87	112.73
185	18.50	13.65	0.80	0.80	59.87	114.32
186	18.60	14.54	0.78	0.78	56.56	114.73
187	18.70	14.34	0.70	0.70	53.10	115.00
188	18.80	17.54	0.82	0.82	51.01	115.44
189	18.90	17.97	0.87	0.87	51.09	115.72
190	19.00	15.09	0.78	0.78	54.33	115.00
191	19.10	12.43	0.67	0.67	59.98	113.38
192	19.20	9.96	0.53	0.53	64.43	111.80

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
193	19.30	9.56	0.48	0.48	64.73	111.22
194	19.40	11.42	0.56	0.56	61.22	111.99
195	19.50	13.35	0.65	0.65	56.44	113.23
196	19.60	15.38	0.69	0.69	51.44	114.22
197	19.70	18.28	0.72	0.72	46.98	114.59
198	19.80	19.54	0.67	0.67	44.39	115.03
199	19.90	20.23	0.76	0.76	45.58	115.04
200	20.00	16.72	0.74	0.74	49.34	114.17
201	20.10	12.54	0.51	0.51	53.36	112.57
202	20.20	12.54	0.46	0.46	54.92	110.89
203	20.30	12.26	0.44	0.44	54.74	110.67
204	20.40	12.34	0.47	0.47	54.89	110.97
205	20.50	13.04	0.51	0.51	53.87	111.57
206	20.60	14.29	0.54	0.54	51.97	112.28
207	20.70	15.53	0.58	0.58	50.93	113.04
208	20.80	15.80	0.65	0.65	50.79	114.36
209	20.90	17.69	0.84	0.84	50.10	116.70
210	21.00	22.85	1.23	1.23	47.01	119.74
211	21.10	30.95	1.73	1.73	42.76	122.10
212	21.20	36.95	1.89	1.89	37.99	123.36
213	21.30	42.88	1.77	1.77	32.84	123.29
214	21.40	48.29	1.43	1.43	28.05	122.38
215	21.50	50.56	1.15	1.15	24.82	121.09
216	21.60	48.73	1.01	1.01	24.24	120.28
217	21.70	44.97	1.08	1.08	26.24	120.39
218	21.80	41.67	1.27	1.27	29.46	121.37
219	21.90	41.81	1.56	1.56	30.68	123.13
220	22.00	53.30	2.04	2.04	28.09	125.04
221	22.10	71.40	2.32	2.32	23.43	126.27
222	22.20	86.36	2.11	2.11	18.88	126.63
223	22.30	100.73	1.92	1.92	15.56	126.34
224	22.40	107.91	1.82	1.82	13.72	126.24
225	22.50	112.51	1.86	1.86	12.92	126.78
226	22.60	125.62	2.21	2.21	12.78	127.58
227	22.70	127.85	2.37	2.37	12.87	128.28
228	22.80	126.96	2.42	2.42	13.07	128.73
229	22.90	132.58	2.60	2.60	12.92	129.43
230	23.00	148.53	2.97	2.97	12.48	130.33
231	23.10	161.03	3.23	3.23	11.94	131.21
232	23.20	171.66	3.45	3.45	11.56	131.89
233	23.30	180.86	3.69	3.69	11.34	132.48
234	23.40	188.14	3.92	3.92	11.23	132.97
235	23.50	192.96	4.05	4.05	11.19	133.25
236	23.60	193.28	4.06	4.06	11.22	133.28
237	23.70	188.79	3.97	3.97	11.41	133.08
238	23.80	179.85	3.82	3.82	11.92	132.77
239	23.90	167.36	3.74	3.74	13.07	132.61
240	24.00	152.93	3.99	3.99	14.44	131.96

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
241	24.10	128.06	3.23	3.23	15.43	130.96
242	24.20	120.75	2.69	2.69	15.11	129.79
243	24.30	130.48	2.68	2.68	14.12	129.25
244	24.40	134.08	2.57	2.57	13.50	129.02
245	24.50	127.67	2.40	2.40	14.05	128.67
246	24.60	112.13	2.44	2.44	15.90	128.09
247	24.70	91.10	2.29	2.29	19.38	127.41
248	24.80	70.09	2.20	2.20	24.09	126.50
249	24.90	55.08	2.13	2.13	29.38	125.73
250	25.00	47.92	2.10	2.10	33.53	125.31
251	25.10	46.01	2.15	2.15	35.64	125.53
252	25.20	48.30	2.42	2.42	37.64	125.59
253	25.30	40.96	2.27	2.27	39.78	125.44
254	25.40	37.60	2.15	2.15	40.27	125.28
255	25.50	45.69	2.32	2.32	35.93	125.60
256	25.60	59.12	2.25	2.25	29.40	125.83
257	25.70	70.65	1.91	1.91	24.01	125.60
258	25.80	78.06	1.77	1.77	20.71	125.47
259	25.90	85.13	1.92	1.92	19.26	125.67
260	26.00	87.95	1.93	1.93	18.85	126.02
261	26.10	87.87	1.97	1.97	19.31	126.45
262	26.20	87.00	2.27	2.27	19.35	126.78
263	26.30	93.02	2.17	2.17	18.31	126.87
264	26.40	101.50	1.94	1.94	16.83	126.57
265	26.50	100.65	1.91	1.91	16.09	126.34
266	26.60	99.24	1.95	1.95	16.44	126.43
267	26.70	98.75	2.03	2.03	16.91	126.70
268	26.80	99.34	2.14	2.14	17.25	127.00
269	26.90	100.26	2.20	2.20	17.37	127.26
270	27.00	102.18	2.24	2.24	17.28	127.47
271	27.10	104.61	2.29	2.29	17.13	127.62
272	27.20	105.31	2.29	2.29	17.12	127.80
273	27.30	106.02	2.39	2.39	17.44	128.11
274	27.40	106.45	2.58	2.58	18.00	128.60
275	27.50	107.27	2.78	2.78	18.48	129.07
276	27.60	108.97	2.87	2.87	18.55	129.33
277	27.70	111.05	2.84	2.84	18.18	129.40
278	27.80	114.11	2.80	2.80	17.73	129.50
279	27.90	117.82	2.92	2.92	17.36	129.62
280	28.00	119.46	2.91	2.91	17.01	129.37
281	28.10	114.35	2.51	2.51	16.90	128.66
282	28.20	105.16	2.25	2.25	17.71	127.93
283	28.30	94.00	2.36	2.36	19.01	127.45
284	28.40	89.72	2.24	2.24	20.28	127.04
285	28.50	84.46	2.03	2.03	20.76	126.38
286	28.60	79.30	1.90	1.90	21.64	125.93
287	28.70	75.30	1.99	1.99	23.18	125.79
288	28.80	69.49	2.04	2.04	25.54	126.01

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
289	28.90	64.38	2.23	2.23	28.62	125.96
290	29.00	54.68	2.17	2.17	32.16	125.55
291	29.10	46.36	1.96	1.96	35.58	124.66
292	29.20	41.69	1.79	1.79	38.50	123.57
293	29.30	36.17	1.59	1.59	40.97	122.75
294	29.40	33.64	1.57	1.57	43.00	122.38
295	29.50	34.22	1.66	1.66	43.89	122.40
296	29.60	34.24	1.64	1.64	43.88	122.30
297	29.70	33.20	1.50	1.50	44.57	121.53
298	29.80	28.58	1.26	1.26	46.00	120.71
299	29.90	27.15	1.27	1.27	47.71	120.62
300	30.00	29.51	1.51	1.51	47.14	122.69
301	30.10	40.11	2.36	2.36	44.95	124.72
302	30.20	44.56	2.55	2.55	42.71	125.95
303	30.30	44.79	2.38	2.38	42.23	126.30
304	30.40	44.42	2.63	2.63	42.91	126.46
305	30.50	43.75	2.73	2.73	42.81	127.09
306	30.60	50.30	2.97	2.97	39.90	127.67
307	30.70	60.15	3.00	3.00	35.08	128.01
308	30.80	68.63	2.70	2.70	29.81	127.98
309	30.90	79.95	2.51	2.51	24.94	127.95
310	31.00	95.74	2.54	2.54	21.22	128.19
311	31.10	108.20	2.58	2.58	18.95	128.70
312	31.20	116.40	2.74	2.74	17.90	129.43
313	31.30	125.14	3.11	3.11	17.61	130.33
314	31.40	132.59	3.46	3.46	17.53	131.01
315	31.50	134.16	3.49	3.49	17.33	131.26
316	31.60	134.92	3.37	3.37	17.19	131.19
317	31.70	133.66	3.35	3.35	17.30	130.97
318	31.80	127.28	3.25	3.25	17.79	130.39
319	31.90	113.49	2.79	2.79	18.65	129.27
320	32.00	97.18	2.30	2.30	20.17	127.91
321	32.10	82.95	2.17	2.17	22.56	127.10
322	32.20	75.89	2.32	2.32	25.11	127.21
323	32.30	76.91	2.59	2.59	26.31	127.76
324	32.40	81.31	2.75	2.75	25.83	128.38
325	32.50	88.72	2.85	2.85	24.20	128.91
326	32.60	99.73	2.95	2.95	21.87	129.41
327	32.70	114.05	3.00	3.00	19.29	129.79
328	32.80	128.47	2.96	2.96	16.92	129.78
329	32.90	135.28	2.65	2.65	15.59	129.77
330	33.00	136.97	2.82	2.82	14.94	129.63
331	33.10	137.32	2.73	2.73	14.43	129.04
332	33.20	131.16	2.05	2.05	14.05	128.05
333	33.30	121.17	1.95	1.95	14.15	127.08
334	33.40	114.56	2.02	2.02	15.40	127.07
335	33.50	110.40	2.15	2.15	16.68	127.46
336	33.60	109.94	2.36	2.36	17.68	128.18

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
337	33.70	114.61	2.69	2.69	18.16	129.23
338	33.80	125.09	3.15	3.15	17.82	130.33
339	33.90	139.40	3.43	3.43	16.76	131.05
340	34.00	150.31	3.36	3.36	15.36	131.28
341	34.10	158.13	3.20	3.20	14.15	131.06
342	34.20	159.43	2.99	2.99	13.52	130.77
343	34.30	156.51	2.94	2.94	13.43	130.76
344	34.40	160.32	3.17	3.17	13.54	131.26
345	34.50	171.85	3.55	3.55	13.58	131.90
346	34.60	175.59	3.69	3.69	13.48	132.37
347	34.70	178.50	3.75	3.75	13.36	132.62
348	34.80	183.69	3.85	3.85	13.06	132.79
349	34.90	189.77	3.86	3.86	12.56	132.85
350	35.00	195.04	3.72	3.72	11.98	132.76
351	35.10	197.97	3.62	3.62	11.62	132.64
352	35.20	197.15	3.63	3.63	11.58	132.57
353	35.30	193.85	3.62	3.62	11.71	132.44
354	35.40	189.59	3.48	3.48	11.78	132.12
355	35.50	184.43	3.26	3.26	11.72	131.62
356	35.60	178.42	3.01	3.01	11.57	130.96
357	35.70	172.55	2.74	2.74	11.31	130.25
358	35.80	169.23	2.50	2.50	10.90	129.49
359	35.90	167.16	2.25	2.25	10.28	128.61
360	36.00	164.14	1.92	1.92	9.62	127.58
361	36.10	158.65	1.67	1.67	9.13	126.50
362	36.20	151.89	1.51	1.51	9.08	125.74
363	36.30	146.37	1.48	1.48	9.44	125.48
364	36.40	143.07	1.56	1.56	9.96	125.62
365	36.50	142.15	1.62	1.62	10.39	125.87
366	36.60	142.29	1.66	1.66	10.62	126.15
367	36.70	144.50	1.74	1.74	10.71	126.55
368	36.80	149.98	1.87	1.87	10.63	127.05
369	36.90	157.12	1.98	1.98	10.39	127.61
370	37.00	165.79	2.09	2.09	10.01	128.05
371	37.10	172.94	2.14	2.14	9.57	128.32
372	37.20	178.15	2.12	2.12	9.31	128.52
373	37.30	180.12	2.20	2.20	9.29	128.66
374	37.40	178.24	2.25	2.25	9.48	128.74
375	37.50	175.41	2.21	2.21	9.70	128.71
376	37.60	172.60	2.21	2.21	9.96	128.68
377	37.70	169.84	2.25	2.25	10.28	128.70
378	37.80	167.17	2.26	2.26	10.62	128.74
379	37.90	164.65	2.28	2.28	10.94	128.82
380	38.00	163.65	2.35	2.35	11.28	128.99
381	38.10	163.65	2.44	2.44	11.58	129.22
382	38.20	163.65	2.51	2.51	11.78	129.38
383	38.30	163.65	2.52	2.52	11.97	129.52
384	38.40	163.06	2.59	2.59	12.22	129.61

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
385	38.50	160.28	2.62	2.62	12.53	129.60
386	38.60	156.28	2.55	2.55	12.84	129.50
387	38.70	153.03	2.53	2.53	13.18	129.40
388	38.80	150.19	2.57	2.57	13.54	129.33
389	38.90	146.91	2.54	2.54	13.85	129.25
390	39.00	144.63	2.50	2.50	14.01	129.15
391	39.10	144.61	2.50	2.50	13.99	129.09
392	39.20	146.23	2.48	2.48	13.78	129.06
393	39.30	148.58	2.45	2.45	13.49	128.99
394	39.40	149.32	2.40	2.40	13.17	128.87
395	39.50	150.21	2.33	2.33	12.90	128.72
396	39.60	151.05	2.29	2.29	12.65	128.52
397	39.70	149.98	2.20	2.20	12.40	128.42
398	39.80	153.45	2.22	2.22	12.24	128.47
399	39.90	156.55	2.32	2.32	12.46	128.85
400	40.00	155.18	2.53	2.53	12.93	129.21
401	40.10	152.74	2.58	2.58	13.25	129.44
402	40.20	155.87	2.56	2.56	13.15	129.56
403	40.30	161.19	2.63	2.63	12.84	129.73
404	40.40	165.15	2.69	2.69	12.55	129.92
405	40.50	168.76	2.70	2.70	12.23	130.02
406	40.60	172.47	2.68	2.68	11.87	130.02
407	40.70	174.92	2.64	2.64	11.49	129.96
408	40.80	177.50	2.59	2.59	11.19	129.92
409	40.90	179.68	2.60	2.60	11.05	129.96
410	41.00	180.41	2.66	2.66	11.15	130.15
411	41.10	181.21	2.77	2.77	11.39	130.44
412	41.20	182.62	2.91	2.91	11.59	130.73
413	41.30	184.37	2.97	2.97	11.72	131.00
414	41.40	186.92	3.07	3.07	11.67	131.15
415	41.50	189.15	3.06	3.06	11.38	131.08
416	41.60	191.15	2.85	2.85	10.98	130.87
417	41.70	192.32	2.80	2.80	10.77	130.77
418	41.80	192.51	2.92	2.92	10.94	130.99
419	41.90	193.81	3.10	3.10	11.29	131.42
420	42.00	196.74	3.31	3.31	11.56	131.87
421	42.10	200.73	3.46	3.46	11.69	132.25
422	42.20	204.20	3.57	3.57	11.76	132.58
423	42.30	206.83	3.72	3.72	11.83	132.83
424	42.40	208.60	3.78	3.78	11.83	132.94
425	42.50	208.79	3.71	3.71	11.73	132.86
426	42.60	207.34	3.60	3.60	11.66	132.67
427	42.70	203.82	3.52	3.52	11.63	132.39
428	42.80	199.71	3.36	3.36	11.68	132.09
429	42.90	195.04	3.24	3.24	11.91	131.87
430	43.00	189.24	3.30	3.30	12.39	131.86
431	43.10	186.13	3.44	3.44	12.92	132.08
432	43.20	188.06	3.58	3.58	13.08	132.40

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
433	43.30	196.05	3.72	3.72	12.78	132.76
434	43.40	207.87	3.84	3.84	12.20	133.12
435	43.50	219.31	3.94	3.94	11.55	133.45
436	43.60	230.68	4.03	4.03	10.99	133.77
437	43.70	241.27	4.17	4.17	10.58	134.10
438	43.80	250.16	4.32	4.32	10.29	134.43
439	43.90	257.85	4.45	4.45	10.00	134.71
440	44.00	267.83	4.52	4.52	9.46	134.79
441	44.10	278.09	4.29	4.29	8.69	134.58
442	44.20	284.44	3.95	3.95	7.73	134.08
443	44.30	291.84	3.56	3.56	6.75	133.40
444	44.40	296.88	3.17	3.17	6.08	132.84
445	44.50	295.68	3.12	3.12	5.94	132.67
446	44.60	291.63	3.34	3.34	6.27	132.91
447	44.70	290.21	3.51	3.51	6.45	133.07
448	44.80	293.38	3.34	3.34	6.14	132.85
449	44.90	299.36	3.02	3.02	5.49	132.35
450	45.00	305.12	2.80	2.80	4.94	131.97
451	45.10	310.53	2.83	2.83	4.77	132.04
452	45.20	315.26	3.05	3.05	4.84	132.34
453	45.30	318.00	3.12	3.12	4.99	132.63
454	45.40	316.61	3.18	3.18	5.18	132.83
455	45.50	313.71	3.31	3.31	5.46	133.09
456	45.60	313.78	3.48	3.48	5.77	133.41
457	45.70	314.24	3.63	3.63	6.00	133.64
458	45.80	312.48	3.65	3.65	6.06	133.63
459	45.90	309.29	3.49	3.49	5.99	133.34
460	46.00	303.00	3.26	3.26	5.88	132.88
461	46.10	294.16	3.07	3.07	5.75	132.23
462	46.20	283.73	2.75	2.75	5.63	131.51
463	46.30	273.33	2.50	2.50	5.43	130.65
464	46.40	264.12	2.23	2.23	5.28	129.82
465	46.50	254.52	2.03	2.03	5.30	129.12
466	46.60	241.59	1.97	1.97	5.80	128.74
467	46.70	221.77	2.03	2.03	7.02	128.59
468	46.80	191.87	2.09	2.09	9.22	128.57
469	46.90	158.27	2.24	2.24	12.74	128.69
470	47.00	128.04	2.53	2.53	17.72	129.08
471	47.10	106.41	2.96	2.96	23.55	129.72
472	47.20	94.27	3.45	3.45	28.72	130.82
473	47.30	96.77	4.33	4.33	30.73	132.24
474	47.40	114.24	5.15	5.15	29.15	133.35
475	47.50	130.91	5.00	5.00	26.04	133.65
476	47.60	138.57	4.38	4.38	23.74	133.20
477	47.70	133.49	4.06	4.06	23.40	132.66
478	47.80	122.92	4.14	4.14	24.83	132.34
479	47.90	113.19	4.11	4.11	26.41	132.02
480	48.00	108.80	3.81	3.81	26.50	131.48

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
481	48.10	111.26	3.40	3.40	24.53	130.70
482	48.20	119.50	2.91	2.91	21.21	129.74
483	48.30	129.41	2.38	2.38	17.74	128.48
484	48.40	133.97	1.89	1.89	15.12	127.06
485	48.50	131.64	1.58	1.58	13.90	125.83
486	48.60	125.12	1.49	1.49	14.36	125.25
487	48.70	114.32	1.59	1.59	16.69	125.43
488	48.80	99.24	1.85	1.85	20.92	125.98
489	48.90	82.59	2.12	2.12	26.89	126.43
490	49.00	66.86	2.30	2.30	33.78	126.42
491	49.10	54.46	2.26	2.26	40.76	125.73
492	49.20	43.64	1.96	1.96	46.99	124.42
493	49.30	35.72	1.63	1.63	52.15	122.56
494	49.40	29.29	1.27	1.27	56.31	120.52
495	49.50	25.18	1.01	1.01	59.25	118.55
496	49.60	23.12	0.86	0.86	60.41	117.25
497	49.70	23.18	0.83	0.83	57.24	118.02
498	49.80	32.45	1.22	1.22	52.58	120.36
499	49.90	41.22	1.69	1.69	49.14	122.29

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q _c :	Measured cone resistance (tsf)
f _s :	Sleeve friction resistance (tsf)
u:	Pore pressure (tsf)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (pcf)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1	0.10	0.01	0.00	0.01	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
2	0.20	0.01	0.00	0.01	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
3	0.30	0.02	0.00	0.02	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
4	0.40	0.02	0.00	0.02	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
5	0.50	0.03	0.00	0.03	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
6	0.60	0.04	0.00	0.04	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
7	0.70	0.04	0.00	0.04	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
8	0.80	0.05	0.00	0.05	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
9	0.90	0.06	0.00	0.06	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
10	1.00	0.06	0.00	0.06	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
11	1.10	0.07	0.00	0.07	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
12	1.20	0.07	0.00	0.07	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
13	1.30	0.08	0.00	0.08	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
14	1.40	0.09	0.00	0.09	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
15	1.50	0.09	0.00	0.09	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
16	1.60	0.10	0.00	0.10	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
17	1.70	0.11	0.00	0.11	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
18	1.80	0.11	0.00	0.11	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
19	1.90	0.12	0.00	0.12	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
20	2.00	0.12	0.00	0.12	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
21	2.10	0.13	0.00	0.13	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
22	2.20	0.14	0.00	0.14	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
23	2.30	0.14	0.00	0.14	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
24	2.40	0.15	0.00	0.15	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
25	2.50	0.16	0.00	0.16	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
26	2.60	0.16	0.00	0.16	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
27	2.70	0.17	0.00	0.17	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
28	2.80	0.17	0.00	0.17	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
29	2.90	0.18	0.00	0.18	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
30	3.00	0.19	0.00	0.19	0.99	0.479	1.06	0.453	1.00	1.30	2.000	No
31	3.10	0.19	0.00	0.19	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
32	3.20	0.20	0.00	0.20	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
33	3.30	0.20	0.00	0.20	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
34	3.40	0.21	0.00	0.21	0.99	0.478	1.06	0.453	1.00	1.30	2.000	No
35	3.50	0.22	0.00	0.22	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
36	3.60	0.22	0.00	0.22	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
37	3.70	0.23	0.00	0.23	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
38	3.80	0.23	0.00	0.23	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
39	3.90	0.24	0.00	0.24	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
40	4.00	0.25	0.00	0.25	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
41	4.10	0.25	0.00	0.25	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
42	4.20	0.26	0.00	0.26	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
43	4.30	0.26	0.00	0.26	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
44	4.40	0.27	0.00	0.27	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
45	4.50	0.28	0.00	0.28	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
46	4.60	0.28	0.00	0.28	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
47	4.70	0.29	0.00	0.29	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
48	4.80	0.30	0.00	0.30	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
49	4.90	0.30	0.00	0.30	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
50	5.00	0.31	0.00	0.31	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
51	5.10	0.31	0.00	0.31	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
52	5.20	0.32	0.00	0.32	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
53	5.30	0.33	0.00	0.33	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
54	5.40	0.33	0.00	0.33	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
55	5.50	0.34	0.00	0.34	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
56	5.60	0.34	0.00	0.34	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
57	5.70	0.35	0.00	0.35	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
58	5.80	0.36	0.00	0.36	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
59	5.90	0.36	0.00	0.36	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
60	6.00	0.37	0.00	0.37	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
61	6.10	0.37	0.00	0.37	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
62	6.20	0.38	0.00	0.38	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
63	6.30	0.38	0.00	0.38	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
64	6.40	0.39	0.00	0.39	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
65	6.50	0.40	0.00	0.40	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
66	6.60	0.40	0.00	0.40	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
67	6.70	0.41	0.00	0.41	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
68	6.80	0.41	0.00	0.41	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
69	6.90	0.42	0.00	0.42	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
70	7.00	0.42	0.00	0.42	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
71	7.10	0.43	0.00	0.43	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
72	7.20	0.43	0.00	0.43	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
73	7.30	0.44	0.00	0.44	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
74	7.40	0.45	0.00	0.45	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
75	7.50	0.45	0.00	0.45	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
76	7.60	0.46	0.00	0.46	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
77	7.70	0.46	0.00	0.46	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
78	7.80	0.47	0.00	0.47	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
79	7.90	0.47	0.00	0.47	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
80	8.00	0.48	0.00	0.48	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
81	8.10	0.48	0.00	0.48	0.98	0.476	1.06	0.451	1.00	1.30	0.586	No
82	8.20	0.49	0.01	0.48	0.98	0.479	1.06	0.453	1.00	1.30	0.589	No
83	8.30	0.50	0.01	0.49	0.98	0.482	1.06	0.456	1.00	1.30	0.593	No
84	8.40	0.50	0.01	0.49	0.98	0.485	1.06	0.459	1.00	1.30	0.596	No
85	8.50	0.51	0.02	0.49	0.98	0.488	1.06	0.462	1.00	1.30	0.600	No
86	8.60	0.51	0.02	0.49	0.98	0.490	1.06	0.464	1.00	1.30	0.603	No
87	8.70	0.52	0.02	0.49	0.98	0.493	1.06	0.467	1.00	1.30	0.607	No
88	8.80	0.52	0.02	0.50	0.98	0.496	1.06	0.469	1.00	1.30	0.610	No
89	8.90	0.53	0.03	0.50	0.98	0.499	1.06	0.472	1.00	1.30	0.614	No
90	9.00	0.53	0.03	0.50	0.98	0.501	1.06	0.475	1.00	1.30	0.617	No
91	9.10	0.54	0.03	0.50	0.98	0.504	1.06	0.477	1.00	1.30	0.620	No
92	9.20	0.54	0.04	0.50	0.98	0.507	1.06	0.480	1.00	1.30	0.624	No
93	9.30	0.55	0.04	0.51	0.98	0.509	1.06	0.482	1.00	1.30	0.627	No
94	9.40	0.55	0.04	0.51	0.98	0.512	1.06	0.485	1.00	1.30	0.630	No
95	9.50	0.56	0.05	0.51	0.98	0.515	1.06	0.487	1.00	1.30	0.633	No
96	9.60	0.56	0.05	0.51	0.98	0.517	1.06	0.490	1.00	1.30	0.637	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
97	9.70	0.57	0.05	0.51	0.98	0.520	1.06	0.492	1.00	1.30	0.640	No
98	9.80	0.57	0.06	0.52	0.98	0.522	1.06	0.494	1.00	1.30	0.643	No
99	9.90	0.58	0.06	0.52	0.98	0.525	1.06	0.497	1.00	1.30	0.646	No
100	10.00	0.58	0.06	0.52	0.98	0.527	1.06	0.499	1.00	1.30	0.649	No
101	10.10	0.59	0.07	0.52	0.98	0.530	1.06	0.501	1.00	1.30	0.652	No
102	10.20	0.59	0.07	0.53	0.98	0.532	1.06	0.504	1.00	1.30	0.655	No
103	10.30	0.60	0.07	0.53	0.98	0.535	1.06	0.506	1.00	1.30	0.658	No
104	10.40	0.60	0.07	0.53	0.98	0.537	1.06	0.508	1.00	1.30	0.661	No
105	10.50	0.61	0.08	0.53	0.98	0.539	1.06	0.511	1.00	1.30	0.664	No
106	10.60	0.62	0.08	0.53	0.98	0.542	1.06	0.513	1.00	1.30	0.667	No
107	10.70	0.62	0.08	0.54	0.98	0.544	1.06	0.515	1.00	1.30	0.670	No
108	10.80	0.63	0.09	0.54	0.98	0.546	1.06	0.517	1.00	1.30	0.672	No
109	10.90	0.63	0.09	0.54	0.98	0.549	1.06	0.519	1.00	1.30	0.675	No
110	11.00	0.64	0.09	0.54	0.98	0.551	1.06	0.522	1.00	1.30	0.678	No
111	11.10	0.64	0.10	0.54	0.98	0.553	1.06	0.524	1.00	1.30	0.681	No
112	11.20	0.65	0.10	0.55	0.98	0.555	1.06	0.526	1.00	1.30	0.684	No
113	11.30	0.65	0.10	0.55	0.98	0.558	1.06	0.528	1.00	1.30	0.686	No
114	11.40	0.66	0.11	0.55	0.98	0.560	1.06	0.530	1.00	1.30	0.689	No
115	11.50	0.66	0.11	0.55	0.98	0.562	1.06	0.532	1.00	1.30	0.692	No
116	11.60	0.67	0.11	0.56	0.98	0.564	1.06	0.534	1.00	1.30	0.694	No
117	11.70	0.67	0.12	0.56	0.98	0.566	1.06	0.536	1.00	1.30	0.697	No
118	11.80	0.68	0.12	0.56	0.98	0.568	1.06	0.538	1.00	1.30	0.699	No
119	11.90	0.69	0.12	0.56	0.98	0.570	1.06	0.540	1.00	1.30	0.702	No
120	12.00	0.69	0.12	0.57	0.97	0.572	1.06	0.542	1.00	1.30	0.704	No
121	12.10	0.70	0.13	0.57	0.97	0.574	1.06	0.544	1.00	1.30	0.707	No
122	12.20	0.70	0.13	0.57	0.97	0.576	1.06	0.546	1.00	1.30	0.709	No
123	12.30	0.71	0.13	0.57	0.97	0.578	1.06	0.547	1.00	1.30	0.712	No
124	12.40	0.71	0.14	0.58	0.97	0.580	1.06	0.549	1.00	1.30	0.714	No
125	12.50	0.72	0.14	0.58	0.97	0.582	1.06	0.551	1.00	1.30	0.716	No
126	12.60	0.72	0.14	0.58	0.97	0.584	1.06	0.553	1.00	1.30	0.719	No
127	12.70	0.73	0.15	0.58	0.97	0.586	1.06	0.555	1.00	1.30	0.721	No
128	12.80	0.74	0.15	0.59	0.97	0.588	1.06	0.556	1.00	1.30	0.723	No
129	12.90	0.74	0.15	0.59	0.97	0.590	1.06	0.558	1.00	1.30	0.726	No
130	13.00	0.75	0.16	0.59	0.97	0.591	1.06	0.560	1.00	1.30	0.728	No
131	13.10	0.75	0.16	0.59	0.97	0.593	1.06	0.562	1.00	1.30	0.730	No
132	13.20	0.76	0.16	0.60	0.97	0.595	1.06	0.563	1.00	1.30	0.732	No
133	13.30	0.76	0.17	0.60	0.97	0.597	1.06	0.565	1.00	1.30	0.735	No
134	13.40	0.77	0.17	0.60	0.97	0.599	1.06	0.567	1.00	1.30	0.737	No
135	13.50	0.77	0.17	0.60	0.97	0.600	1.06	0.568	1.00	1.30	0.739	No
136	13.60	0.78	0.17	0.61	0.97	0.602	1.06	0.570	1.00	1.30	0.741	No
137	13.70	0.79	0.18	0.61	0.97	0.604	1.06	0.572	1.00	1.30	0.743	No
138	13.80	0.79	0.18	0.61	0.97	0.606	1.06	0.573	1.00	1.30	0.745	No
139	13.90	0.80	0.18	0.61	0.97	0.607	1.06	0.575	1.00	1.30	0.747	No
140	14.00	0.80	0.19	0.62	0.97	0.609	1.06	0.576	1.00	1.30	0.749	No
141	14.10	0.81	0.19	0.62	0.97	0.611	1.06	0.578	1.00	1.30	0.751	No
142	14.20	0.81	0.19	0.62	0.97	0.612	1.06	0.580	1.00	1.30	0.754	No
143	14.30	0.82	0.20	0.62	0.97	0.614	1.06	0.581	1.00	1.30	0.756	No
144	14.40	0.82	0.20	0.62	0.97	0.616	1.06	0.583	1.00	1.30	0.758	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
145	14.50	0.83	0.20	0.63	0.97	0.617	1.06	0.584	1.00	1.30	0.760	No
146	14.60	0.84	0.21	0.63	0.97	0.619	1.06	0.586	1.00	1.30	0.761	No
147	14.70	0.84	0.21	0.63	0.97	0.620	1.06	0.587	1.00	1.30	0.763	No
148	14.80	0.85	0.21	0.63	0.97	0.622	1.06	0.589	1.00	1.30	0.765	No
149	14.90	0.85	0.22	0.64	0.97	0.623	1.06	0.590	1.00	1.30	0.767	No
150	15.00	0.86	0.22	0.64	0.97	0.625	1.06	0.591	1.00	1.30	0.769	No
151	15.10	0.86	0.22	0.64	0.97	0.626	1.06	0.593	1.00	1.30	0.771	No
152	15.20	0.87	0.22	0.65	0.97	0.628	1.06	0.594	1.00	1.30	0.773	No
153	15.30	0.88	0.23	0.65	0.97	0.629	1.06	0.596	1.00	1.30	0.774	No
154	15.40	0.88	0.23	0.65	0.97	0.631	1.06	0.597	1.00	1.30	0.776	No
155	15.50	0.89	0.23	0.65	0.97	0.632	1.06	0.598	1.00	1.30	0.778	No
156	15.60	0.89	0.24	0.66	0.97	0.634	1.06	0.600	1.00	1.30	0.780	No
157	15.70	0.90	0.24	0.66	0.97	0.635	1.06	0.601	1.00	1.30	0.781	No
158	15.80	0.90	0.24	0.66	0.97	0.636	1.06	0.602	1.00	1.30	0.783	No
159	15.90	0.91	0.25	0.66	0.97	0.638	1.06	0.604	1.00	1.30	0.785	No
160	16.00	0.92	0.25	0.67	0.97	0.639	1.06	0.605	1.00	1.30	0.786	No
161	16.10	0.92	0.25	0.67	0.97	0.640	1.06	0.606	1.00	1.30	0.788	No
162	16.20	0.93	0.26	0.67	0.97	0.642	1.06	0.607	1.00	1.30	0.790	No
163	16.30	0.93	0.26	0.67	0.97	0.643	1.06	0.609	1.00	1.30	0.791	No
164	16.40	0.94	0.26	0.68	0.97	0.644	1.06	0.610	1.00	1.30	0.793	No
165	16.50	0.95	0.27	0.68	0.97	0.645	1.06	0.611	1.00	1.30	0.794	No
166	16.60	0.95	0.27	0.68	0.97	0.647	1.06	0.612	1.00	1.30	0.796	No
167	16.70	0.96	0.27	0.69	0.96	0.648	1.06	0.613	1.00	1.30	0.797	No
168	16.80	0.96	0.27	0.69	0.96	0.649	1.06	0.615	1.00	1.30	0.799	No
169	16.90	0.97	0.28	0.69	0.96	0.651	1.06	0.616	1.00	1.30	0.801	No
170	17.00	0.97	0.28	0.69	0.96	0.652	1.06	0.617	1.00	1.30	0.802	No
171	17.10	0.98	0.28	0.69	0.96	0.653	1.06	0.618	1.00	1.30	0.804	No
172	17.20	0.98	0.29	0.70	0.96	0.655	1.06	0.620	1.00	1.30	0.806	No
173	17.30	0.99	0.29	0.70	0.96	0.656	1.06	0.621	1.00	1.30	0.808	No
174	17.40	0.99	0.29	0.70	0.96	0.658	1.06	0.623	1.00	1.30	0.809	No
175	17.50	1.00	0.30	0.70	0.96	0.659	1.06	0.624	1.00	1.30	0.811	No
176	17.60	1.00	0.30	0.70	0.96	0.660	1.06	0.625	1.00	1.30	0.813	No
177	17.70	1.01	0.30	0.71	0.96	0.662	1.06	0.626	1.00	1.30	0.814	No
178	17.80	1.01	0.31	0.71	0.96	0.663	1.06	0.627	1.00	1.30	0.816	No
179	17.90	1.02	0.31	0.71	0.96	0.664	1.06	0.629	1.00	1.30	0.817	No
180	18.00	1.02	0.31	0.71	0.96	0.665	1.06	0.630	1.00	1.30	0.819	No
181	18.10	1.03	0.32	0.71	0.96	0.667	1.06	0.631	1.00	1.30	0.820	No
182	18.20	1.04	0.32	0.72	0.96	0.668	1.06	0.632	1.00	1.30	0.822	No
183	18.30	1.04	0.32	0.72	0.96	0.669	1.06	0.633	1.00	1.30	0.823	No
184	18.40	1.05	0.32	0.72	0.96	0.670	1.06	0.634	1.00	1.30	0.824	No
185	18.50	1.05	0.33	0.72	0.96	0.671	1.06	0.635	1.00	1.30	0.826	No
186	18.60	1.06	0.33	0.73	0.96	0.672	1.06	0.636	1.00	1.30	0.827	No
187	18.70	1.06	0.33	0.73	0.96	0.673	1.06	0.637	1.00	1.30	0.828	No
188	18.80	1.07	0.34	0.73	0.96	0.674	1.06	0.638	1.00	1.30	0.830	No
189	18.90	1.07	0.34	0.73	0.96	0.675	1.06	0.639	1.00	1.30	0.831	No
190	19.00	1.08	0.34	0.74	0.96	0.676	1.06	0.640	1.00	1.30	0.832	No
191	19.10	1.09	0.35	0.74	0.96	0.677	1.06	0.641	1.00	1.30	0.833	No
192	19.20	1.09	0.35	0.74	0.96	0.678	1.06	0.642	1.00	1.30	0.835	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
193	19.30	1.10	0.35	0.74	0.96	0.679	1.06	0.643	1.00	1.30	0.836	No
194	19.40	1.10	0.36	0.75	0.96	0.680	1.06	0.644	1.00	1.30	0.837	No
195	19.50	1.11	0.36	0.75	0.96	0.681	1.06	0.645	1.00	1.30	0.839	No
196	19.60	1.11	0.36	0.75	0.96	0.682	1.06	0.646	1.00	1.30	0.840	No
197	19.70	1.12	0.37	0.76	0.96	0.683	1.06	0.647	1.00	1.30	0.841	No
198	19.80	1.13	0.37	0.76	0.96	0.684	1.06	0.648	1.00	1.30	0.842	No
199	19.90	1.13	0.37	0.76	0.96	0.685	1.06	0.649	1.00	1.30	0.843	No
200	20.00	1.14	0.37	0.76	0.96	0.686	1.06	0.649	1.00	1.30	0.844	No
201	20.10	1.14	0.38	0.77	0.96	0.687	1.06	0.650	1.00	1.30	0.846	No
202	20.20	1.15	0.38	0.77	0.96	0.688	1.06	0.651	1.00	1.30	0.847	No
203	20.30	1.15	0.38	0.77	0.96	0.689	1.06	0.652	1.00	1.30	0.848	No
204	20.40	1.16	0.39	0.77	0.96	0.690	1.06	0.653	1.00	1.30	0.849	No
205	20.50	1.17	0.39	0.78	0.96	0.691	1.06	0.654	1.00	1.30	0.850	No
206	20.60	1.17	0.39	0.78	0.96	0.692	1.06	0.655	1.00	1.30	0.851	No
207	20.70	1.18	0.40	0.78	0.96	0.693	1.06	0.656	1.00	1.30	0.852	No
208	20.80	1.18	0.40	0.78	0.95	0.694	1.06	0.657	1.00	1.30	0.853	No
209	20.90	1.19	0.40	0.79	0.95	0.694	1.06	0.657	1.00	1.30	2.000	Yes
210	21.00	1.19	0.41	0.79	0.95	0.695	1.06	0.658	1.00	1.30	2.000	Yes
211	21.10	1.20	0.41	0.79	0.95	0.696	1.06	0.659	1.00	1.30	2.000	Yes
212	21.20	1.21	0.41	0.79	0.95	0.697	1.06	0.659	1.00	1.30	2.000	Yes
213	21.30	1.21	0.41	0.80	0.95	0.697	1.06	0.660	1.00	1.30	2.000	Yes
214	21.40	1.22	0.42	0.80	0.95	0.698	1.06	0.661	1.00	1.30	2.000	Yes
215	21.50	1.22	0.42	0.80	0.95	0.699	1.06	0.661	1.00	1.30	2.000	Yes
216	21.60	1.23	0.42	0.81	0.95	0.699	1.06	0.662	1.00	1.30	0.861	No
217	21.70	1.24	0.43	0.81	0.95	0.700	1.06	0.663	1.00	1.30	0.861	No
218	21.80	1.24	0.43	0.81	0.95	0.701	1.06	0.663	1.00	1.30	0.862	No
219	21.90	1.25	0.43	0.82	0.95	0.701	1.06	0.664	1.00	1.30	2.000	Yes
220	22.00	1.26	0.44	0.82	0.95	0.702	1.06	0.664	1.00	1.30	2.000	Yes
221	22.10	1.26	0.44	0.82	0.95	0.702	1.06	0.665	1.00	1.30	2.000	Yes
222	22.20	1.27	0.44	0.82	0.95	0.703	1.06	0.666	1.00	1.30	2.000	Yes
223	22.30	1.27	0.45	0.83	0.95	0.704	1.06	0.666	1.00	1.30	2.000	Yes
224	22.40	1.28	0.45	0.83	0.95	0.704	1.06	0.667	1.00	1.30	2.000	Yes
225	22.50	1.29	0.45	0.83	0.95	0.705	1.06	0.667	1.00	1.30	0.867	No
226	22.60	1.29	0.46	0.84	0.95	0.705	1.06	0.668	1.00	1.30	0.868	No
227	22.70	1.30	0.46	0.84	0.95	0.706	1.06	0.668	1.00	1.30	0.868	No
228	22.80	1.31	0.46	0.84	0.95	0.706	1.06	0.668	1.00	1.30	0.869	No
229	22.90	1.31	0.46	0.85	0.95	0.707	1.06	0.669	1.00	1.30	0.870	No
230	23.00	1.32	0.47	0.85	0.95	0.707	1.06	0.669	1.00	1.30	0.870	No
231	23.10	1.33	0.47	0.85	0.95	0.707	1.06	0.670	1.00	1.30	0.871	No
232	23.20	1.33	0.47	0.86	0.95	0.708	1.06	0.670	1.00	1.30	0.871	No
233	23.30	1.34	0.48	0.86	0.95	0.708	1.06	0.670	1.00	1.30	0.872	No
234	23.40	1.35	0.48	0.86	0.95	0.709	1.06	0.671	1.00	1.30	0.872	No
235	23.50	1.35	0.48	0.87	0.95	0.709	1.06	0.671	1.00	1.30	0.873	No
236	23.60	1.36	0.49	0.87	0.95	0.709	1.06	0.672	1.00	1.30	0.873	No
237	23.70	1.37	0.49	0.88	0.95	0.710	1.06	0.672	1.00	1.30	0.873	No
238	23.80	1.37	0.49	0.88	0.95	0.710	1.06	0.672	1.00	1.30	0.874	No
239	23.90	1.38	0.50	0.88	0.95	0.710	1.06	0.673	1.00	1.30	0.874	No
240	24.00	1.39	0.50	0.89	0.95	0.711	1.06	0.673	1.00	1.30	0.875	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
241	24.10	1.39	0.50	0.89	0.94	0.711	1.06	0.673	1.00	1.30	0.875	No
242	24.20	1.40	0.51	0.89	0.94	0.712	1.06	0.674	1.00	1.30	0.876	No
243	24.30	1.40	0.51	0.90	0.94	0.712	1.06	0.674	1.00	1.30	0.876	No
244	24.40	1.41	0.51	0.90	0.94	0.712	1.06	0.674	1.00	1.30	0.877	No
245	24.50	1.42	0.51	0.90	0.94	0.713	1.06	0.675	1.00	1.30	2.000	Yes
246	24.60	1.42	0.52	0.91	0.94	0.713	1.06	0.675	1.00	1.30	2.000	Yes
247	24.70	1.43	0.52	0.91	0.94	0.713	1.06	0.675	1.00	1.30	2.000	Yes
248	24.80	1.44	0.52	0.91	0.94	0.714	1.06	0.676	1.00	1.30	2.000	Yes
249	24.90	1.44	0.53	0.92	0.94	0.714	1.06	0.676	1.00	1.30	2.000	Yes
250	25.00	1.45	0.53	0.92	0.94	0.714	1.06	0.676	1.00	1.30	2.000	Yes
251	25.10	1.46	0.53	0.92	0.94	0.715	1.06	0.677	1.00	1.30	2.000	Yes
252	25.20	1.46	0.54	0.93	0.94	0.715	1.06	0.677	1.00	1.30	2.000	Yes
253	25.30	1.47	0.54	0.93	0.94	0.716	1.06	0.677	1.00	1.30	2.000	Yes
254	25.40	1.47	0.54	0.93	0.94	0.716	1.06	0.678	1.00	1.30	2.000	Yes
255	25.50	1.48	0.55	0.93	0.94	0.716	1.06	0.678	1.00	1.30	2.000	Yes
256	25.60	1.49	0.55	0.94	0.94	0.717	1.06	0.678	1.00	1.30	2.000	Yes
257	25.70	1.49	0.55	0.94	0.94	0.717	1.06	0.679	1.00	1.30	2.000	Yes
258	25.80	1.50	0.56	0.94	0.94	0.717	1.06	0.679	1.00	1.30	2.000	Yes
259	25.90	1.51	0.56	0.95	0.94	0.718	1.06	0.679	1.00	1.30	2.000	Yes
260	26.00	1.51	0.56	0.95	0.94	0.718	1.06	0.680	1.00	1.30	0.883	No
261	26.10	1.52	0.56	0.95	0.94	0.718	1.06	0.680	1.00	1.30	0.884	No
262	26.20	1.52	0.57	0.96	0.94	0.718	1.06	0.680	1.00	1.30	0.884	No
263	26.30	1.53	0.57	0.96	0.94	0.719	1.06	0.680	1.00	1.30	0.884	No
264	26.40	1.54	0.57	0.96	0.94	0.719	1.06	0.681	1.00	1.30	0.885	No
265	26.50	1.54	0.58	0.97	0.94	0.719	1.06	0.681	1.00	1.30	0.885	No
266	26.60	1.55	0.58	0.97	0.94	0.719	1.06	0.681	1.00	1.30	0.885	No
267	26.70	1.56	0.58	0.97	0.94	0.720	1.06	0.681	1.00	1.30	0.886	No
268	26.80	1.56	0.59	0.98	0.94	0.720	1.06	0.682	1.00	1.30	0.886	No
269	26.90	1.57	0.59	0.98	0.93	0.720	1.06	0.682	1.00	1.30	0.886	No
270	27.00	1.58	0.59	0.98	0.93	0.720	1.06	0.682	1.00	1.30	0.887	No
271	27.10	1.58	0.60	0.99	0.93	0.721	1.06	0.682	1.00	1.30	0.887	No
272	27.20	1.59	0.60	0.99	0.93	0.721	1.06	0.682	1.00	1.30	0.887	No
273	27.30	1.59	0.60	0.99	0.93	0.721	1.06	0.683	1.00	1.30	0.887	No
274	27.40	1.60	0.61	1.00	0.93	0.721	1.06	0.683	1.00	1.30	0.888	No
275	27.50	1.61	0.61	1.00	0.93	0.721	1.06	0.683	1.00	1.30	0.888	No
276	27.60	1.61	0.61	1.00	0.93	0.722	1.06	0.683	1.00	1.30	0.888	No
277	27.70	1.62	0.61	1.01	0.93	0.722	1.06	0.683	1.00	1.30	0.888	No
278	27.80	1.63	0.62	1.01	0.93	0.722	1.06	0.683	1.00	1.30	0.888	No
279	27.90	1.63	0.62	1.01	0.93	0.722	1.06	0.683	1.00	1.30	0.888	No
280	28.00	1.64	0.62	1.02	0.93	0.722	1.06	0.684	1.00	1.30	0.889	No
281	28.10	1.65	0.63	1.02	0.93	0.722	1.06	0.684	1.00	1.30	0.889	No
282	28.20	1.65	0.63	1.02	0.93	0.722	1.06	0.684	1.00	1.30	0.889	No
283	28.30	1.66	0.63	1.03	0.93	0.722	1.06	0.684	1.00	1.30	0.889	No
284	28.40	1.67	0.64	1.03	0.93	0.723	1.06	0.684	1.00	1.30	0.889	No
285	28.50	1.67	0.64	1.03	0.93	0.723	1.06	0.684	1.00	1.30	0.889	No
286	28.60	1.68	0.64	1.04	0.93	0.723	1.06	0.684	1.00	1.30	2.000	Yes
287	28.70	1.68	0.65	1.04	0.93	0.723	1.06	0.684	1.00	1.30	2.000	Yes
288	28.80	1.69	0.65	1.04	0.93	0.723	1.06	0.685	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
289	28.90	1.70	0.65	1.04	0.93	0.723	1.06	0.685	1.00	1.30	2.000	Yes
290	29.00	1.70	0.66	1.05	0.93	0.723	1.06	0.685	1.00	1.30	2.000	Yes
291	29.10	1.71	0.66	1.05	0.92	0.724	1.06	0.685	1.00	1.30	2.000	Yes
292	29.20	1.72	0.66	1.05	0.92	0.724	1.06	0.685	1.00	1.30	2.000	Yes
293	29.30	1.72	0.66	1.06	0.92	0.724	1.06	0.685	1.00	1.30	2.000	Yes
294	29.40	1.73	0.67	1.06	0.92	0.724	1.06	0.685	1.00	1.30	2.000	Yes
295	29.50	1.73	0.67	1.06	0.92	0.724	1.06	0.685	1.00	1.30	0.891	No
296	29.60	1.74	0.67	1.07	0.92	0.724	1.06	0.686	1.00	1.30	0.891	No
297	29.70	1.75	0.68	1.07	0.92	0.724	1.06	0.686	1.00	1.30	0.891	No
298	29.80	1.75	0.68	1.07	0.92	0.724	1.06	0.686	1.00	1.30	0.892	No
299	29.90	1.76	0.68	1.08	0.92	0.725	1.06	0.686	1.00	1.30	0.892	No
300	30.00	1.76	0.69	1.08	0.92	0.725	1.06	0.686	1.00	1.30	0.892	No
301	30.10	1.77	0.69	1.08	0.92	0.725	1.06	0.686	1.00	1.30	0.892	No
302	30.20	1.78	0.69	1.08	0.92	0.725	1.06	0.686	1.00	1.30	0.892	No
303	30.30	1.78	0.70	1.09	0.92	0.725	1.06	0.686	1.00	1.30	0.892	No
304	30.40	1.79	0.70	1.09	0.92	0.725	1.06	0.686	1.00	1.30	0.892	No
305	30.50	1.80	0.70	1.09	0.92	0.725	1.06	0.686	1.00	1.30	2.000	Yes
306	30.60	1.80	0.71	1.10	0.92	0.725	1.06	0.686	1.00	1.30	2.000	Yes
307	30.70	1.81	0.71	1.10	0.92	0.725	1.06	0.686	1.00	1.30	2.000	Yes
308	30.80	1.82	0.71	1.10	0.92	0.725	1.06	0.686	1.00	1.30	2.000	Yes
309	30.90	1.82	0.71	1.11	0.92	0.725	1.06	0.686	1.00	1.30	2.000	Yes
310	31.00	1.83	0.72	1.11	0.92	0.725	1.06	0.686	1.00	1.30	2.000	Yes
311	31.10	1.83	0.72	1.11	0.91	0.725	1.06	0.686	1.00	1.30	2.000	Yes
312	31.20	1.84	0.72	1.12	0.91	0.725	1.06	0.686	1.00	1.30	2.000	Yes
313	31.30	1.85	0.73	1.12	0.91	0.725	1.06	0.686	1.00	1.30	0.892	No
314	31.40	1.85	0.73	1.12	0.91	0.725	1.06	0.686	1.00	1.30	0.892	No
315	31.50	1.86	0.73	1.13	0.91	0.724	1.06	0.686	1.00	1.30	0.892	No
316	31.60	1.87	0.74	1.13	0.91	0.724	1.06	0.686	1.00	1.30	0.891	No
317	31.70	1.87	0.74	1.13	0.91	0.724	1.06	0.686	1.00	1.30	0.891	No
318	31.80	1.88	0.74	1.14	0.91	0.724	1.06	0.685	1.00	1.30	0.891	No
319	31.90	1.89	0.75	1.14	0.91	0.724	1.06	0.685	1.00	1.30	0.891	No
320	32.00	1.89	0.75	1.14	0.91	0.724	1.06	0.685	1.00	1.30	0.891	No
321	32.10	1.90	0.75	1.15	0.91	0.724	1.06	0.685	1.00	1.30	0.891	No
322	32.20	1.91	0.76	1.15	0.91	0.724	1.06	0.685	1.00	1.30	0.891	No
323	32.30	1.91	0.76	1.15	0.91	0.724	1.06	0.685	1.00	1.30	0.891	No
324	32.40	1.92	0.76	1.16	0.91	0.724	1.06	0.685	1.00	1.30	0.890	No
325	32.50	1.92	0.76	1.16	0.91	0.723	1.06	0.685	1.00	1.30	0.890	No
326	32.60	1.93	0.77	1.16	0.91	0.723	1.06	0.685	1.00	1.30	0.890	No
327	32.70	1.94	0.77	1.17	0.91	0.723	1.06	0.685	1.00	1.30	0.890	No
328	32.80	1.94	0.77	1.17	0.90	0.723	1.06	0.684	1.00	1.30	0.890	No
329	32.90	1.95	0.78	1.17	0.90	0.723	1.06	0.684	1.00	1.30	0.890	No
330	33.00	1.96	0.78	1.18	0.90	0.723	1.06	0.684	1.00	1.30	0.889	No
331	33.10	1.96	0.78	1.18	0.90	0.723	1.06	0.684	1.00	1.30	0.889	No
332	33.20	1.97	0.79	1.18	0.90	0.722	1.06	0.684	1.00	1.30	0.889	No
333	33.30	1.98	0.79	1.19	0.90	0.722	1.06	0.684	1.00	1.30	0.889	No
334	33.40	1.98	0.79	1.19	0.90	0.722	1.06	0.684	1.00	1.30	0.889	No
335	33.50	1.99	0.80	1.19	0.90	0.722	1.06	0.683	1.00	1.30	0.888	No
336	33.60	2.00	0.80	1.20	0.90	0.722	1.06	0.683	1.00	1.30	0.888	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
337	33.70	2.00	0.80	1.20	0.90	0.722	1.06	0.683	1.00	1.30	0.888	No
338	33.80	2.01	0.80	1.20	0.90	0.721	1.06	0.683	1.00	1.30	0.888	No
339	33.90	2.02	0.81	1.21	0.90	0.721	1.06	0.683	1.00	1.30	0.887	No
340	34.00	2.02	0.81	1.21	0.90	0.721	1.06	0.682	1.00	1.30	0.887	No
341	34.10	2.03	0.81	1.21	0.90	0.721	1.06	0.682	1.00	1.30	0.887	No
342	34.20	2.03	0.82	1.22	0.90	0.720	1.06	0.682	1.00	1.30	0.887	No
343	34.30	2.04	0.82	1.22	0.90	0.720	1.06	0.682	1.00	1.30	0.886	No
344	34.40	2.05	0.82	1.22	0.89	0.720	1.06	0.681	1.00	1.30	0.886	No
345	34.50	2.05	0.83	1.23	0.89	0.720	1.06	0.681	1.00	1.30	0.886	No
346	34.60	2.06	0.83	1.23	0.89	0.719	1.06	0.681	1.00	1.30	0.885	No
347	34.70	2.07	0.83	1.23	0.89	0.719	1.06	0.681	1.00	1.30	0.885	No
348	34.80	2.07	0.84	1.24	0.89	0.719	1.06	0.680	1.00	1.30	0.885	No
349	34.90	2.08	0.84	1.24	0.89	0.718	1.06	0.680	1.00	1.30	0.884	No
350	35.00	2.09	0.84	1.25	0.89	0.718	1.06	0.680	1.00	1.30	0.884	No
351	35.10	2.09	0.85	1.25	0.89	0.718	1.06	0.680	1.00	1.30	0.883	No
352	35.20	2.10	0.85	1.25	0.89	0.718	1.06	0.679	1.00	1.30	0.883	No
353	35.30	2.11	0.85	1.26	0.89	0.717	1.06	0.679	1.00	1.30	0.883	No
354	35.40	2.11	0.85	1.26	0.89	0.717	1.06	0.679	1.00	1.30	0.882	No
355	35.50	2.12	0.86	1.26	0.89	0.717	1.06	0.678	1.00	1.30	0.882	No
356	35.60	2.13	0.86	1.27	0.89	0.716	1.06	0.678	1.00	1.30	0.881	No
357	35.70	2.13	0.86	1.27	0.89	0.716	1.06	0.678	1.00	1.30	0.881	No
358	35.80	2.14	0.87	1.27	0.88	0.716	1.06	0.677	1.00	1.30	0.881	No
359	35.90	2.15	0.87	1.28	0.88	0.715	1.06	0.677	1.00	1.30	0.880	No
360	36.00	2.15	0.87	1.28	0.88	0.715	1.06	0.677	1.00	1.30	0.880	No
361	36.10	2.16	0.88	1.28	0.88	0.715	1.06	0.677	1.00	1.30	0.880	No
362	36.20	2.17	0.88	1.29	0.88	0.714	1.06	0.676	1.00	1.30	0.879	No
363	36.30	2.17	0.88	1.29	0.88	0.714	1.06	0.676	1.00	1.30	0.879	No
364	36.40	2.18	0.89	1.29	0.88	0.714	1.06	0.676	1.00	1.30	0.879	No
365	36.50	2.18	0.89	1.30	0.88	0.714	1.06	0.676	1.00	1.30	0.878	No
366	36.60	2.19	0.89	1.30	0.88	0.713	1.06	0.675	1.00	1.30	0.878	No
367	36.70	2.20	0.90	1.30	0.88	0.713	1.06	0.675	1.00	1.30	0.877	No
368	36.80	2.20	0.90	1.31	0.88	0.713	1.06	0.675	1.00	1.30	0.877	No
369	36.90	2.21	0.90	1.31	0.88	0.712	1.06	0.674	1.00	1.30	0.877	No
370	37.00	2.22	0.90	1.31	0.88	0.712	1.06	0.674	1.00	1.30	0.876	No
371	37.10	2.22	0.91	1.31	0.88	0.712	1.06	0.674	1.00	1.30	0.876	No
372	37.20	2.23	0.91	1.32	0.87	0.711	1.06	0.673	1.00	1.30	0.875	No
373	37.30	2.24	0.91	1.32	0.87	0.711	1.06	0.673	1.00	1.30	0.875	No
374	37.40	2.24	0.92	1.32	0.87	0.710	1.06	0.673	1.00	1.30	0.874	No
375	37.50	2.25	0.92	1.33	0.87	0.710	1.06	0.672	1.00	1.30	0.874	No
376	37.60	2.26	0.92	1.33	0.87	0.710	1.06	0.672	1.00	1.30	0.873	No
377	37.70	2.26	0.93	1.33	0.87	0.709	1.06	0.671	1.00	1.30	0.873	No
378	37.80	2.27	0.93	1.34	0.87	0.709	1.06	0.671	1.00	1.30	0.872	No
379	37.90	2.27	0.93	1.34	0.87	0.708	1.06	0.671	1.00	1.30	0.872	No
380	38.00	2.28	0.94	1.34	0.87	0.708	1.06	0.670	1.00	1.30	0.871	No
381	38.10	2.29	0.94	1.35	0.87	0.708	1.06	0.670	1.00	1.30	0.871	No
382	38.20	2.29	0.94	1.35	0.87	0.707	1.06	0.669	1.00	1.30	0.870	No
383	38.30	2.30	0.95	1.35	0.87	0.707	1.06	0.669	1.00	1.30	0.870	No
384	38.40	2.31	0.95	1.36	0.86	0.706	1.06	0.669	1.00	1.30	0.869	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
385	38.50	2.31	0.95	1.36	0.86	0.706	1.06	0.668	1.00	1.30	0.869	No
386	38.60	2.32	0.95	1.36	0.86	0.705	1.06	0.668	1.00	1.30	0.868	No
387	38.70	2.33	0.96	1.37	0.86	0.705	1.06	0.667	1.00	1.30	0.868	No
388	38.80	2.33	0.96	1.37	0.86	0.705	1.06	0.667	1.00	1.30	0.867	No
389	38.90	2.34	0.96	1.37	0.86	0.704	1.06	0.667	1.00	1.30	0.867	No
390	39.00	2.35	0.97	1.38	0.86	0.704	1.06	0.666	1.00	1.30	0.866	No
391	39.10	2.35	0.97	1.38	0.86	0.703	1.06	0.666	1.00	1.30	0.865	No
392	39.20	2.36	0.97	1.38	0.86	0.703	1.06	0.665	1.00	1.30	0.865	No
393	39.30	2.36	0.98	1.39	0.86	0.702	1.06	0.665	1.00	1.30	0.864	No
394	39.40	2.37	0.98	1.39	0.86	0.702	1.06	0.664	1.00	1.30	0.864	No
395	39.50	2.38	0.98	1.39	0.86	0.701	1.06	0.664	1.00	1.30	0.863	No
396	39.60	2.38	0.99	1.40	0.85	0.701	1.06	0.663	1.00	1.30	0.862	No
397	39.70	2.39	0.99	1.40	0.85	0.700	1.06	0.663	1.00	1.30	0.862	No
398	39.80	2.40	0.99	1.40	0.85	0.700	1.06	0.663	1.00	1.30	0.861	No
399	39.90	2.40	1.00	1.41	0.85	0.699	1.06	0.662	1.00	1.30	0.861	No
400	40.00	2.41	1.00	1.41	0.85	0.699	1.06	0.662	1.00	1.30	0.860	No
401	40.10	2.42	1.00	1.41	0.85	0.698	1.06	0.661	1.00	1.30	0.859	No
402	40.20	2.42	1.00	1.42	0.85	0.698	1.06	0.661	1.00	1.30	0.859	No
403	40.30	2.43	1.01	1.42	0.85	0.697	1.06	0.660	1.00	1.30	0.858	No
404	40.40	2.44	1.01	1.42	0.85	0.697	1.06	0.660	1.00	1.30	0.858	No
405	40.50	2.44	1.01	1.43	0.85	0.696	1.06	0.659	1.00	1.30	0.857	No
406	40.60	2.45	1.02	1.43	0.85	0.696	1.06	0.659	1.00	1.30	0.856	No
407	40.70	2.46	1.02	1.44	0.84	0.695	1.06	0.658	1.00	1.30	0.856	No
408	40.80	2.46	1.02	1.44	0.84	0.695	1.06	0.658	1.00	1.30	0.855	No
409	40.90	2.47	1.03	1.44	0.84	0.694	1.06	0.657	1.00	1.30	0.854	No
410	41.00	2.47	1.03	1.45	0.84	0.694	1.06	0.657	1.00	1.30	0.854	No
411	41.10	2.48	1.03	1.45	0.84	0.693	1.06	0.656	1.00	1.30	0.853	No
412	41.20	2.49	1.04	1.45	0.84	0.692	1.06	0.656	1.00	1.30	0.852	No
413	41.30	2.49	1.04	1.46	0.84	0.692	1.06	0.655	1.00	1.30	0.851	No
414	41.40	2.50	1.04	1.46	0.84	0.691	1.06	0.654	1.00	1.30	0.851	No
415	41.50	2.51	1.05	1.46	0.84	0.691	1.06	0.654	1.00	1.30	0.850	No
416	41.60	2.51	1.05	1.47	0.84	0.690	1.06	0.653	1.00	1.30	0.849	No
417	41.70	2.52	1.05	1.47	0.84	0.690	1.06	0.653	1.00	1.30	0.849	No
418	41.80	2.53	1.05	1.47	0.83	0.689	1.06	0.652	1.00	1.30	0.848	No
419	41.90	2.53	1.06	1.48	0.83	0.688	1.06	0.652	1.00	1.30	0.847	No
420	42.00	2.54	1.06	1.48	0.83	0.688	1.06	0.651	1.00	1.30	0.846	No
421	42.10	2.55	1.06	1.48	0.83	0.687	1.06	0.651	1.00	1.30	0.846	No
422	42.20	2.55	1.07	1.49	0.83	0.687	1.06	0.650	1.00	1.30	0.845	No
423	42.30	2.56	1.07	1.49	0.83	0.686	1.06	0.649	1.00	1.30	0.844	No
424	42.40	2.57	1.07	1.49	0.83	0.685	1.06	0.649	1.00	1.30	0.843	No
425	42.50	2.57	1.08	1.50	0.83	0.685	1.06	0.648	1.00	1.30	0.843	No
426	42.60	2.58	1.08	1.50	0.83	0.684	1.06	0.648	1.00	1.30	0.842	No
427	42.70	2.59	1.08	1.50	0.83	0.683	1.06	0.647	1.00	1.30	0.841	No
428	42.80	2.59	1.09	1.51	0.83	0.683	1.06	0.646	1.00	1.30	0.840	No
429	42.90	2.60	1.09	1.51	0.82	0.682	1.06	0.646	1.00	1.30	0.839	No
430	43.00	2.61	1.09	1.51	0.82	0.682	1.06	0.645	1.00	1.30	0.839	No
431	43.10	2.61	1.10	1.52	0.82	0.681	1.06	0.645	1.00	1.30	0.838	No
432	43.20	2.62	1.10	1.52	0.82	0.680	1.06	0.644	1.00	1.30	0.837	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
433	43.30	2.63	1.10	1.53	0.82	0.680	1.06	0.643	1.00	1.30	0.836	No
434	43.40	2.63	1.10	1.53	0.82	0.679	1.06	0.643	1.00	1.30	0.836	No
435	43.50	2.64	1.11	1.53	0.82	0.678	1.06	0.642	1.00	1.30	0.835	No
436	43.60	2.65	1.11	1.54	0.82	0.678	1.06	0.641	1.00	1.30	0.834	No
437	43.70	2.65	1.11	1.54	0.82	0.677	1.06	0.641	1.00	1.30	0.833	No
438	43.80	2.66	1.12	1.54	0.82	0.676	1.06	0.640	1.00	1.30	0.832	No
439	43.90	2.67	1.12	1.55	0.81	0.676	1.06	0.639	1.00	1.30	0.831	No
440	44.00	2.67	1.12	1.55	0.81	0.675	1.06	0.639	1.00	1.30	0.831	No
441	44.10	2.68	1.13	1.55	0.81	0.674	1.06	0.638	1.00	1.30	0.830	No
442	44.20	2.69	1.13	1.56	0.81	0.673	1.06	0.638	1.00	1.30	0.829	No
443	44.30	2.69	1.13	1.56	0.81	0.673	1.06	0.637	1.00	1.30	0.828	No
444	44.40	2.70	1.14	1.56	0.81	0.672	1.06	0.636	1.00	1.30	0.827	No
445	44.50	2.71	1.14	1.57	0.81	0.671	1.06	0.636	1.00	1.30	0.826	No
446	44.60	2.71	1.14	1.57	0.81	0.671	1.06	0.635	1.00	1.30	0.825	No
447	44.70	2.72	1.15	1.57	0.81	0.670	1.06	0.634	1.00	1.30	0.825	No
448	44.80	2.73	1.15	1.58	0.81	0.669	1.06	0.634	1.00	1.30	0.824	No
449	44.90	2.73	1.15	1.58	0.80	0.669	1.06	0.633	1.00	1.30	0.823	No
450	45.00	2.74	1.15	1.59	0.80	0.668	1.06	0.632	1.00	1.30	0.822	No
451	45.10	2.75	1.16	1.59	0.80	0.667	1.06	0.632	1.00	1.30	0.821	No
452	45.20	2.75	1.16	1.59	0.80	0.667	1.06	0.631	1.00	1.30	0.820	No
453	45.30	2.76	1.16	1.60	0.80	0.666	1.06	0.630	1.00	1.30	0.819	No
454	45.40	2.77	1.17	1.60	0.80	0.665	1.06	0.630	1.00	1.30	0.819	No
455	45.50	2.77	1.17	1.60	0.80	0.664	1.06	0.629	1.00	1.30	0.818	No
456	45.60	2.78	1.17	1.61	0.80	0.664	1.06	0.628	1.00	1.30	0.817	No
457	45.70	2.79	1.18	1.61	0.80	0.663	1.06	0.628	1.00	1.30	0.816	No
458	45.80	2.79	1.18	1.61	0.80	0.662	1.06	0.627	1.00	1.30	0.815	No
459	45.90	2.80	1.18	1.62	0.79	0.662	1.06	0.626	1.00	1.30	0.814	No
460	46.00	2.81	1.19	1.62	0.79	0.661	1.06	0.626	1.00	1.30	0.813	No
461	46.10	2.81	1.19	1.62	0.79	0.660	1.06	0.625	1.00	1.30	0.812	No
462	46.20	2.82	1.19	1.63	0.79	0.660	1.06	0.624	1.00	1.30	0.812	No
463	46.30	2.83	1.19	1.63	0.79	0.659	1.06	0.624	1.00	1.30	0.811	No
464	46.40	2.83	1.20	1.63	0.79	0.658	1.06	0.623	1.00	1.30	0.810	No
465	46.50	2.84	1.20	1.64	0.79	0.657	1.06	0.622	1.00	1.30	0.809	No
466	46.60	2.85	1.20	1.64	0.79	0.657	1.06	0.622	1.00	1.30	0.808	No
467	46.70	2.85	1.21	1.64	0.79	0.656	1.06	0.621	1.00	1.30	2.000	Yes
468	46.80	2.86	1.21	1.65	0.79	0.655	1.06	0.620	1.00	1.30	2.000	Yes
469	46.90	2.86	1.21	1.65	0.78	0.655	1.06	0.620	1.00	1.30	2.000	Yes
470	47.00	2.87	1.22	1.65	0.78	0.654	1.06	0.619	1.00	1.30	2.000	Yes
471	47.10	2.88	1.22	1.66	0.78	0.653	1.06	0.618	1.00	1.30	2.000	Yes
472	47.20	2.88	1.22	1.66	0.78	0.653	1.06	0.618	1.00	1.30	2.000	Yes
473	47.30	2.89	1.23	1.66	0.78	0.652	1.06	0.617	1.00	1.30	2.000	Yes
474	47.40	2.90	1.23	1.67	0.78	0.651	1.06	0.616	1.00	1.30	2.000	Yes
475	47.50	2.90	1.23	1.67	0.78	0.650	1.06	0.616	1.00	1.30	2.000	Yes
476	47.60	2.91	1.24	1.68	0.78	0.650	1.06	0.615	1.00	1.30	2.000	Yes
477	47.70	2.92	1.24	1.68	0.78	0.649	1.06	0.614	1.00	1.30	0.798	No
478	47.80	2.92	1.24	1.68	0.78	0.648	1.06	0.614	1.00	1.30	0.798	No
479	47.90	2.93	1.24	1.69	0.77	0.647	1.06	0.613	1.00	1.30	0.797	No
480	48.00	2.94	1.25	1.69	0.77	0.647	1.06	0.612	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
481	48.10	2.94	1.25	1.69	0.77	0.646	1.06	0.611	1.00	1.30	2.000	Yes
482	48.20	2.95	1.25	1.70	0.77	0.645	1.06	0.611	1.00	1.30	2.000	Yes
483	48.30	2.96	1.26	1.70	0.77	0.644	1.06	0.610	1.00	1.30	2.000	Yes
484	48.40	2.96	1.26	1.70	0.77	0.644	1.06	0.609	1.00	1.30	2.000	Yes
485	48.50	2.97	1.26	1.71	0.77	0.643	1.06	0.609	1.00	1.30	2.000	Yes
486	48.60	2.98	1.27	1.71	0.77	0.642	1.06	0.608	1.00	1.30	2.000	Yes
487	48.70	2.98	1.27	1.71	0.77	0.642	1.06	0.607	1.00	1.30	2.000	Yes
488	48.80	2.99	1.27	1.72	0.76	0.641	1.06	0.607	1.00	1.30	2.000	Yes
489	48.90	2.99	1.28	1.72	0.76	0.640	1.06	0.606	1.00	1.30	2.000	Yes
490	49.00	3.00	1.28	1.72	0.76	0.640	1.06	0.605	1.00	1.30	2.000	Yes
491	49.10	3.01	1.28	1.72	0.76	0.639	1.06	0.605	1.00	1.30	2.000	Yes
492	49.20	3.01	1.29	1.73	0.76	0.638	1.06	0.604	1.00	1.30	2.000	Yes
493	49.30	3.02	1.29	1.73	0.76	0.638	1.06	0.604	1.00	1.30	2.000	Yes
494	49.40	3.03	1.29	1.73	0.76	0.637	1.06	0.603	1.00	1.30	2.000	Yes
495	49.50	3.03	1.29	1.74	0.76	0.636	1.06	0.602	1.00	1.30	0.783	No
496	49.60	3.04	1.30	1.74	0.76	0.636	1.06	0.602	1.00	1.30	0.782	No
497	49.70	3.04	1.30	1.74	0.76	0.635	1.06	0.601	1.00	1.30	0.781	No
498	49.80	3.05	1.30	1.75	0.75	0.634	1.06	0.600	1.00	1.30	0.781	No
499	49.90	3.06	1.31	1.75	0.75	0.634	1.06	0.600	1.00	1.30	0.780	No

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
 σ_v : Total overburden pressure at test point (tsf)
 u_0 : Water pressure at test point (tsf)
 σ_v' : Effective overburden pressure based on GWT during earthquake (tsf)
 r_d : Nonlinear shear mass factor
 CSR: Cyclic Stress Ratio
 MSF: Magnitude Scaling Factor
 CSR_{eq}: CSR adjusted for M=7.5
 K_σ : Effective overburden stress factor
 CSR*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::												
Point ID	Depth (ft)	q _t (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1	0.10	63.32	2.00	1.63	0.61	119.66	1.30	156.12	4.000	No	No	2.00
2	0.20	64.12	1.98	1.55	0.60	121.18	1.29	156.29	4.000	No	No	2.00
3	0.30	63.59	1.99	1.58	0.61	120.15	1.30	155.76	4.000	No	No	2.00
4	0.40	60.41	2.06	1.88	0.63	114.13	1.36	155.54	4.000	No	No	2.00
5	0.50	57.19	2.13	2.27	0.66	108.04	1.47	158.82	4.000	No	No	2.00
6	0.60	56.53	2.19	2.69	0.69	106.77	1.59	169.97	4.000	No	No	2.00
7	0.70	59.04	2.23	3.10	0.70	111.51	1.68	187.49	4.000	No	No	2.00
8	0.80	62.44	2.24	3.40	0.71	117.93	1.73	203.76	4.000	No	No	2.00
9	0.90	64.67	2.25	3.57	0.71	122.13	1.75	213.48	4.000	No	No	2.00
10	1.00	65.58	2.25	3.64	0.71	123.84	1.76	217.84	4.000	No	No	2.00
11	1.10	64.59	2.26	3.68	0.71	121.95	1.78	217.35	4.000	No	No	2.00
12	1.20	61.76	2.27	3.68	0.72	116.59	1.82	212.53	4.000	No	No	2.00
13	1.30	57.24	2.29	3.62	0.72	108.04	1.88	202.58	4.000	No	No	2.00
14	1.40	54.57	2.29	3.53	0.73	102.99	1.89	194.84	4.000	No	No	2.00
15	1.50	54.99	2.28	3.48	0.72	103.76	1.87	193.76	4.000	No	No	2.00
16	1.60	57.17	2.28	3.50	0.72	107.88	1.84	198.15	4.000	No	No	2.00
17	1.70	59.72	2.27	3.56	0.72	112.67	1.82	204.57	4.000	No	No	2.00
18	1.80	60.59	2.27	3.64	0.72	114.32	1.83	208.96	4.000	No	No	2.00
19	1.90	57.91	2.29	3.75	0.73	109.24	1.91	208.12	4.000	No	No	2.00
20	2.00	52.69	2.33	3.88	0.74	99.36	2.06	204.26	4.000	No	No	2.00
21	2.10	46.70	2.38	4.05	0.76	88.02	2.27	200.15	4.000	No	No	2.00
22	2.20	42.14	2.42	4.17	0.78	79.39	2.48	196.72	4.000	No	No	2.00
23	2.30	37.73	2.46	4.23	0.79	71.05	2.69	190.95	4.000	No	No	2.00
24	2.40	33.71	2.49	4.21	0.80	63.44	2.89	183.12	4.000	No	No	2.00
25	2.50	31.80	2.50	4.13	0.81	59.81	2.96	177.04	4.000	No	No	2.00
26	2.60	32.09	2.49	4.02	0.80	60.34	2.89	174.10	4.000	No	No	2.00
27	2.70	33.43	2.47	3.91	0.80	62.88	2.75	172.91	4.000	No	No	2.00
28	2.80	34.49	2.44	3.77	0.79	64.86	2.62	170.11	4.000	No	No	2.00
29	2.90	34.00	2.43	3.59	0.79	63.92	2.56	163.33	4.000	No	No	2.00
30	3.00	33.22	2.42	3.36	0.78	62.43	2.48	154.72	4.000	No	No	2.00
31	3.10	32.49	2.41	3.17	0.78	61.04	2.42	147.49	4.000	No	No	2.00
32	3.20	33.17	2.40	3.12	0.77	62.33	2.36	147.00	4.000	No	No	2.00
33	3.30	34.74	2.39	3.21	0.77	65.27	2.33	152.13	4.000	No	No	2.00
34	3.40	37.04	2.39	3.38	0.77	69.63	2.32	161.38	4.000	No	No	2.00
35	3.50	39.15	2.39	3.61	0.77	73.59	2.34	172.41	4.000	No	No	2.00
36	3.60	40.29	2.41	3.92	0.78	75.74	2.44	184.64	4.000	No	No	2.00
37	3.70	40.26	2.44	4.31	0.79	75.67	2.62	198.15	4.000	No	No	2.00
38	3.80	40.09	2.48	4.74	0.80	75.33	2.82	212.41	4.000	No	No	2.00
39	3.90	40.64	2.50	5.11	0.81	76.35	2.96	226.23	4.000	No	No	2.00
40	4.00	42.32	2.50	5.34	0.81	79.52	2.82	224.37	4.000	No	No	2.00
41	4.10	44.34	2.49	5.38	0.81	83.32	2.92	243.30	4.000	No	No	2.00
42	4.20	45.37	2.48	5.38	0.81	85.27	2.88	245.18	4.000	No	No	2.00
43	4.30	44.83	2.49	5.43	0.81	84.24	2.92	246.11	4.000	No	No	2.00
44	4.40	42.77	2.52	5.63	0.82	80.33	3.12	250.85	4.000	No	No	2.00
45	4.50	39.56	2.55	5.86	0.84	74.26	3.94	292.83	4.000	No	No	2.00
46	4.60	35.62	2.59	6.02	0.85	66.78	5.06	337.68	4.000	No	No	2.00
47	4.70	31.43	2.63	6.05	0.86	58.86	6.41	377.38	4.000	No	No	2.00
48	4.80	28.05	2.65	5.96	0.88	52.45	7.63	400.29	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _t (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
49	4.90	25.36	2.67	5.77	0.88	47.36	8.61	407.59	4.000	No	No	2.00
50	5.00	23.37	2.68	5.50	0.89	43.60	9.10	396.53	4.000	No	No	2.00
51	5.10	21.74	2.68	5.16	0.89	40.51	9.22	373.68	4.000	No	No	2.00
52	5.20	20.76	2.68	4.86	0.89	38.63	8.99	347.15	4.000	No	No	2.00
53	5.30	20.78	2.67	4.71	0.88	38.66	8.45	326.66	4.000	No	No	2.00
54	5.40	22.02	2.65	4.67	0.88	41.00	7.41	303.67	4.000	No	No	2.00
55	5.50	24.13	2.62	4.59	0.86	44.97	6.00	269.97	4.000	No	No	2.00
56	5.60	26.02	2.58	4.45	0.85	48.54	4.85	235.34	4.000	No	No	2.00
57	5.70	26.65	2.57	4.30	0.84	49.72	4.32	214.76	4.000	No	No	2.00
58	5.80	25.84	2.57	4.27	0.85	48.17	4.52	217.86	4.000	No	No	2.00
59	5.90	23.01	2.62	4.39	0.86	42.81	6.03	258.30	4.000	No	No	2.00
60	6.00	19.12	2.69	4.65	0.89	35.45	9.71	344.13	4.000	No	No	2.00
61	6.10	16.32	2.76	4.89	0.92	30.15	5.35	161.34	4.000	No	Yes	2.00
62	6.20	15.54	2.77	4.84	0.92	28.66	5.50	157.72	4.000	No	Yes	2.00
63	6.30	15.65	2.75	4.59	0.92	28.86	5.29	152.63	4.000	No	Yes	2.00
64	6.40	14.57	2.76	4.36	0.92	26.81	5.39	144.51	4.000	No	Yes	2.00
65	6.50	12.62	2.81	4.34	0.94	23.10	5.96	137.59	4.000	No	Yes	2.00
66	6.60	10.88	2.87	4.54	0.96	19.81	6.80	134.72	4.000	No	Yes	2.00
67	6.70	9.87	2.92	4.79	0.98	17.90	7.51	134.34	4.000	No	Yes	2.00
68	6.80	9.47	2.94	4.92	0.99	17.12	7.84	134.24	4.000	No	Yes	2.00
69	6.90	9.06	2.96	5.01	1.00	16.34	8.17	133.47	4.000	No	Yes	2.00
70	7.00	8.72	2.99	5.21	1.00	15.69	8.57	134.43	4.000	No	Yes	2.00
71	7.10	9.04	2.99	5.48	1.00	16.28	8.60	140.05	4.000	No	Yes	2.00
72	7.20	10.62	2.93	5.47	0.99	19.26	7.72	148.60	4.000	No	Yes	2.00
73	7.30	13.04	2.85	5.09	0.95	23.82	6.44	153.29	4.000	No	Yes	2.00
74	7.40	14.73	2.78	4.62	0.93	27.01	5.56	150.18	4.000	No	Yes	2.00
75	7.50	14.76	2.75	4.30	0.92	27.04	5.31	143.64	4.000	No	Yes	2.00
76	7.60	13.33	2.79	4.29	0.93	24.34	5.71	138.90	4.000	No	Yes	2.00
77	7.70	11.94	2.84	4.56	0.95	21.70	6.41	139.00	4.000	No	Yes	2.00
78	7.80	11.27	2.87	4.74	0.97	20.42	6.83	139.42	4.000	No	Yes	2.00
79	7.90	10.87	2.88	4.65	0.97	19.65	6.93	136.20	4.000	No	Yes	2.00
80	8.00	10.28	2.89	4.42	0.97	18.52	7.00	129.68	4.000	No	Yes	2.00
81	8.10	9.38	2.91	4.22	0.98	16.81	7.28	122.43	0.802	No	Yes	1.37
82	8.20	8.40	2.94	4.12	0.99	14.96	7.78	116.38	0.714	No	Yes	1.21
83	8.30	7.35	2.99	4.12	1.00	12.95	8.58	111.11	0.618	No	Yes	1.04
84	8.40	6.58	3.03	4.18	1.00	11.50	9.35	107.50	0.549	No	Yes	0.92
85	8.50	6.25	3.06	4.25	1.00	10.85	9.79	106.28	0.518	No	Yes	0.86
86	8.60	6.30	3.06	4.35	1.00	10.95	9.85	107.81	0.522	No	Yes	0.87
87	8.70	6.35	3.07	4.48	1.00	11.03	9.95	109.72	0.526	No	Yes	0.87
88	8.80	6.29	3.07	4.54	1.00	10.90	10.09	109.93	0.520	No	Yes	0.85
89	8.90	6.27	3.06	4.38	1.00	10.85	9.94	107.84	0.517	No	Yes	0.84
90	9.00	6.29	3.04	4.04	1.00	10.88	9.53	103.70	0.519	No	Yes	0.84
91	9.10	6.09	3.04	3.75	1.00	10.50	9.41	98.73	0.501	No	Yes	0.81
92	9.20	5.58	3.06	3.62	1.00	9.52	9.88	94.03	0.454	No	Yes	0.73
93	9.30	5.10	3.10	3.72	1.00	8.61	10.68	91.95	0.411	No	Yes	0.66
94	9.40	5.13	3.12	3.93	1.00	8.64	10.93	94.52	0.412	No	Yes	0.65
95	9.50	5.52	3.10	4.06	1.00	9.39	10.52	98.73	0.448	No	Yes	0.71
96	9.60	5.90	3.07	3.99	1.00	10.09	9.95	100.37	0.481	No	Yes	0.76

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _k (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
97	9.70	7.76	2.94	3.61	0.99	13.59	7.75	105.29	0.648	No	Yes	1.01
98	9.80	11.21	2.82	3.73	0.95	19.82	6.06	120.15	0.945	No	Yes	1.47
99	9.90	12.34	2.80	3.92	0.94	21.72	5.85	127.08	1.036	No	Yes	1.60
100	10.00	10.19	2.88	4.16	0.97	18.04	6.89	124.23	0.860	No	Yes	1.33
101	10.10	6.46	3.04	4.14	1.00	11.09	9.52	105.62	0.529	No	Yes	0.81
102	10.20	5.25	3.10	3.80	1.00	8.79	10.64	93.57	0.419	No	Yes	0.64
103	10.30	5.64	3.08	3.89	1.00	9.53	10.20	97.26	0.455	No	Yes	0.69
104	10.40	5.93	3.08	4.15	1.00	10.04	10.18	102.21	0.479	No	Yes	0.72
105	10.50	5.98	3.09	4.41	1.00	10.09	10.45	105.41	0.481	No	Yes	0.72
106	10.60	5.98	3.11	4.62	1.00	10.04	10.73	107.70	0.479	No	Yes	0.72
107	10.70	5.98	3.12	4.82	1.00	9.99	10.98	109.69	0.476	No	Yes	0.71
108	10.80	5.98	3.13	5.00	1.00	9.94	11.21	111.47	0.474	No	Yes	0.71
109	10.90	5.98	3.13	5.05	1.00	9.89	11.31	111.87	0.472	No	Yes	0.70
110	11.00	5.98	3.13	4.98	1.00	9.84	11.27	110.87	0.469	No	Yes	0.69
111	11.10	6.00	3.13	5.00	1.00	9.83	11.29	111.03	0.469	No	Yes	0.69
112	11.20	6.41	3.13	5.33	1.00	10.54	11.16	117.58	0.503	No	Yes	0.74
113	11.30	7.76	3.08	5.70	1.00	12.95	10.15	131.45	0.618	No	Yes	0.90
114	11.40	9.54	3.00	5.59	1.00	16.09	8.77	141.14	0.768	No	Yes	1.11
115	11.50	10.92	2.93	5.15	0.99	18.41	7.68	141.33	0.878	No	Yes	1.27
116	11.60	11.17	2.90	4.63	0.98	18.63	7.17	133.57	0.889	No	Yes	1.28
117	11.70	10.34	2.91	4.42	0.99	17.15	7.38	126.54	0.818	No	Yes	1.17
118	11.80	9.11	2.97	4.66	1.00	15.02	8.30	124.65	0.716	No	Yes	1.02
119	11.90	8.03	3.06	5.36	1.00	13.03	9.80	127.66	0.621	No	Yes	0.89
120	12.00	8.26	3.09	6.17	1.00	13.38	10.37	138.78	0.638	No	Yes	0.91
121	12.10	9.89	3.04	6.46	1.00	16.18	9.46	153.07	0.772	No	Yes	1.09
122	12.20	12.14	2.95	6.01	1.00	20.03	7.95	159.25	0.955	No	Yes	1.35
123	12.30	13.79	2.87	5.12	0.97	22.39	6.72	150.55	1.068	No	Yes	1.50
124	12.40	14.39	2.79	4.09	0.94	22.93	5.78	132.52	1.094	No	Yes	1.53
125	12.50	14.67	2.74	3.35	0.92	23.00	5.11	117.45	1.097	No	Yes	1.53
126	12.60	15.66	2.70	3.18	0.91	24.33	4.74	115.42	1.161	No	Yes	1.61
127	12.70	16.72	2.70	3.44	0.91	25.94	4.75	123.21	1.238	No	Yes	1.72
128	12.80	17.02	2.73	3.89	0.92	26.50	5.06	133.95	1.264	No	Yes	1.75
129	12.90	15.54	2.80	4.41	0.94	24.33	5.80	141.15	1.160	No	Yes	1.60
130	13.00	13.13	2.88	4.90	0.98	20.65	6.91	142.74	0.985	No	Yes	1.35
131	13.10	10.98	2.96	5.18	1.00	17.23	8.04	138.59	0.822	No	Yes	1.13
132	13.20	9.80	2.99	5.05	1.00	15.17	8.61	130.62	0.724	No	Yes	0.99
133	13.30	9.73	2.97	4.64	1.00	14.98	8.29	124.20	0.715	No	Yes	0.97
134	13.40	10.47	2.93	4.30	0.99	16.08	7.59	122.03	0.767	No	Yes	1.04
135	13.50	11.58	2.89	4.21	0.98	17.71	7.03	124.47	0.845	No	Yes	1.14
136	13.60	12.48	2.87	4.32	0.97	19.03	6.78	129.09	0.908	No	Yes	1.22
137	13.70	12.75	2.88	4.53	0.98	19.41	6.88	133.53	0.926	No	Yes	1.25
138	13.80	12.33	2.90	4.73	0.98	18.74	7.22	135.37	0.894	No	Yes	1.20
139	13.90	11.80	2.92	4.74	0.99	17.85	7.47	133.41	0.852	No	Yes	1.14
140	14.00	11.32	2.92	4.49	0.99	17.01	7.49	127.31	0.811	No	Yes	1.08
141	14.10	11.16	2.90	4.09	0.98	16.61	7.22	119.87	0.792	No	Yes	1.05
142	14.20	11.16	2.88	3.78	0.98	16.49	6.95	114.51	0.786	No	Yes	1.04
143	14.30	11.46	2.87	3.73	0.97	16.86	6.79	114.46	0.804	No	Yes	1.06
144	14.40	12.08	2.87	3.97	0.97	17.76	6.78	120.36	0.847	No	Yes	1.12

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
145	14.50	13.00	2.87	4.33	0.97	19.14	6.77	129.64	0.913	No	Yes	1.20
146	14.60	13.94	2.87	4.68	0.97	20.52	6.76	138.64	0.979	No	Yes	1.29
147	14.70	14.88	2.86	4.88	0.97	21.86	6.64	145.18	1.043	No	Yes	1.37
148	14.80	15.29	2.86	4.98	0.97	22.38	6.62	148.08	1.068	No	Yes	1.40
149	14.90	14.81	2.87	5.05	0.98	21.62	6.83	147.59	1.031	No	Yes	1.34
150	15.00	13.79	2.90	5.16	0.99	20.07	7.26	145.73	0.957	No	Yes	1.25
151	15.10	12.99	2.93	5.28	1.00	18.84	7.67	144.60	0.899	No	Yes	1.17
152	15.20	12.91	2.94	5.38	1.00	18.67	7.80	145.60	0.890	No	Yes	1.15
153	15.30	13.60	2.93	5.43	1.00	19.60	7.60	148.96	0.935	No	Yes	1.21
154	15.40	14.65	2.91	5.46	0.99	21.04	7.28	153.13	1.003	No	Yes	1.29
155	15.50	14.88	2.90	5.49	0.99	21.29	7.25	154.28	1.016	No	Yes	1.31
156	15.60	14.72	2.91	5.53	0.99	20.99	7.35	154.30	1.001	No	Yes	1.28
157	15.70	14.79	2.91	5.55	0.99	21.00	7.36	154.60	1.002	No	Yes	1.28
158	15.80	15.44	2.90	5.52	0.98	21.83	7.15	156.19	1.041	No	Yes	1.33
159	15.90	15.62	2.90	5.54	0.98	22.01	7.14	157.05	1.050	No	Yes	1.34
160	16.00	15.50	2.91	5.68	0.99	21.77	7.29	158.82	1.039	No	Yes	1.32
161	16.10	17.19	2.88	5.76	0.98	24.08	6.89	165.86	1.148	No	Yes	1.46
162	16.20	21.05	2.80	5.53	0.95	29.29	5.91	173.16	1.397	No	Yes	1.77
163	16.30	24.86	2.74	5.17	0.92	34.27	5.09	174.43	1.635	No	Yes	2.00
164	16.40	26.05	2.70	4.83	0.91	35.63	4.73	168.71	1.700	No	Yes	2.00
165	16.50	23.46	2.73	4.67	0.92	31.96	4.99	159.48	1.525	No	Yes	1.92
166	16.60	18.42	2.81	4.71	0.95	25.05	5.93	148.44	1.195	No	Yes	1.50
167	16.70	12.98	2.93	4.85	1.00	17.53	7.67	134.33	0.836	No	Yes	1.05
168	16.80	8.92	3.07	4.78	1.00	11.56	9.96	115.18	0.552	No	Yes	0.69
169	16.90	6.90	3.14	4.25	1.00	8.60	11.37	97.81	0.410	No	Yes	0.51
170	17.00	6.16	3.14	3.55	1.00	7.49	11.46	85.89	0.357	No	Yes	0.45
171	17.10	5.97	3.12	3.02	1.00	7.20	10.94	78.82	0.344	No	Yes	0.43
172	17.20	5.97	3.09	2.68	1.00	7.18	10.43	74.86	0.342	No	Yes	0.42
173	17.30	5.79	3.09	2.51	1.00	6.88	10.43	71.77	0.328	No	Yes	0.41
174	17.40	5.81	3.09	2.47	1.00	6.88	10.36	71.28	0.328	No	Yes	0.41
175	17.50	6.26	3.08	2.75	1.00	7.51	10.23	76.80	0.358	No	Yes	0.44
176	17.60	7.24	3.06	3.28	1.00	8.87	9.88	87.63	0.423	No	Yes	0.52
177	17.70	8.07	3.06	3.80	1.00	10.01	9.77	97.83	0.478	No	Yes	0.59
178	17.80	8.41	3.06	4.15	1.00	10.45	9.91	103.65	0.499	No	Yes	0.61
179	17.90	8.42	3.08	4.36	1.00	10.43	10.17	106.06	0.497	No	Yes	0.61
180	18.00	8.37	3.09	4.56	1.00	10.31	10.47	107.95	0.492	No	Yes	0.60
181	18.10	8.17	3.13	4.96	1.00	9.99	11.14	111.30	0.476	No	Yes	0.58
182	18.20	8.13	3.16	5.59	1.00	9.90	11.87	117.52	0.472	No	Yes	0.57
183	18.30	8.94	3.16	6.22	1.00	10.98	11.75	129.03	0.524	No	Yes	0.64
184	18.40	10.90	3.09	6.41	1.00	13.66	10.45	142.71	0.651	No	Yes	0.79
185	18.50	13.00	3.02	6.19	1.00	16.49	9.14	150.66	0.787	No	Yes	0.95
186	18.60	14.19	2.97	5.78	1.00	18.06	8.30	149.99	0.862	No	Yes	1.04
187	18.70	15.48	2.92	5.31	1.00	19.74	7.47	147.34	0.941	No	Yes	1.14
188	18.80	16.63	2.88	5.10	0.98	21.12	6.98	147.37	1.008	No	Yes	1.21
189	18.90	16.88	2.89	5.19	0.98	21.38	6.99	149.51	1.020	No	Yes	1.23
190	19.00	15.17	2.94	5.47	1.00	19.11	7.76	148.27	0.911	No	Yes	1.10
191	19.10	12.50	3.02	5.77	1.00	15.42	9.16	141.32	0.736	No	Yes	0.88
192	19.20	10.65	3.09	5.85	1.00	12.88	10.33	133.05	0.614	No	Yes	0.74

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
193	19.30	10.32	3.09	5.67	1.00	12.38	10.41	128.88	0.590	No	Yes	0.71
194	19.40	11.45	3.04	5.42	1.00	13.84	9.48	131.31	0.660	No	Yes	0.79
195	19.50	13.39	2.97	5.14	1.00	16.38	8.27	135.51	0.781	No	Yes	0.93
196	19.60	15.68	2.89	4.71	0.99	19.27	7.07	136.32	0.919	No	Yes	1.09
197	19.70	17.74	2.82	4.16	0.96	21.71	6.07	131.71	1.036	No	Yes	1.23
198	19.80	19.36	2.77	3.92	0.94	23.60	5.51	130.07	1.126	No	Yes	1.34
199	19.90	18.84	2.79	4.07	0.95	22.91	5.76	132.05	1.093	No	Yes	1.30
200	20.00	16.51	2.86	4.35	0.97	19.98	6.59	131.72	0.953	No	Yes	1.13
201	20.10	13.94	2.92	4.44	1.00	16.72	7.53	125.84	0.797	No	Yes	0.94
202	20.20	12.46	2.95	4.15	1.00	14.72	7.90	116.35	0.702	No	Yes	0.83
203	20.30	12.39	2.94	4.06	1.00	14.58	7.86	114.59	0.695	No	Yes	0.82
204	20.40	12.55	2.95	4.15	1.00	14.74	7.90	116.39	0.703	No	Yes	0.83
205	20.50	13.23	2.93	4.19	1.00	15.56	7.65	119.00	0.742	No	Yes	0.87
206	20.60	14.29	2.90	4.13	0.99	16.83	7.20	121.13	0.803	No	Yes	0.94
207	20.70	15.22	2.88	4.20	0.99	17.91	6.96	124.61	0.854	No	Yes	1.00
208	20.80	16.35	2.88	4.54	0.98	19.28	6.93	133.55	0.920	No	Yes	1.08
209	20.90	18.79	2.87	5.14	0.98	22.28	6.77	150.76	4.000	Yes	Yes	2.00
210	21.00	23.85	2.82	5.59	0.96	28.40	6.07	172.52	4.000	Yes	Yes	2.00
211	21.10	30.27	2.74	5.56	0.93	36.02	5.17	186.26	4.000	Yes	Yes	2.00
212	21.20	36.95	2.65	5.02	0.90	43.70	7.57	330.91	4.000	Yes	No	2.00
213	21.30	42.73	2.55	4.08	0.86	50.01	3.83	191.76	4.000	Yes	No	2.00
214	21.40	47.27	2.44	3.14	0.82	54.66	2.59	141.74	4.000	Yes	No	2.00
215	21.50	49.21	2.36	2.49	0.79	56.33	2.18	122.62	4.000	Yes	No	2.00
216	21.60	48.10	2.35	2.30	0.78	54.78	2.11	115.61	0.224	No	No	0.26
217	21.70	45.14	2.40	2.55	0.80	51.43	2.35	120.95	0.245	No	No	0.28
218	21.80	42.84	2.47	3.13	0.83	48.96	2.80	136.86	0.318	No	No	0.37
219	21.90	45.62	2.50	3.66	0.84	52.21	2.80	146.36	4.000	Yes	No	2.00
220	22.00	55.53	2.44	3.64	0.82	63.30	2.60	164.44	4.000	Yes	No	2.00
221	22.10	70.39	2.32	3.12	0.77	79.47	2.02	160.56	4.000	Yes	No	2.00
222	22.20	86.19	2.20	2.49	0.73	96.17	1.61	154.39	4.000	Yes	No	2.00
223	22.30	98.36	2.09	2.01	0.69	108.57	1.41	152.73	4.000	Yes	No	2.00
224	22.40	107.08	2.03	1.76	0.66	117.31	1.33	156.28	4.000	Yes	No	2.00
225	22.50	115.37	2.00	1.72	0.65	125.86	1.31	164.41	0.493	No	No	0.57
226	22.60	122.02	1.99	1.78	0.65	132.79	1.30	172.90	0.561	No	No	0.65
227	22.70	126.84	2.00	1.86	0.65	137.78	1.30	179.79	0.620	No	No	0.71
228	22.80	129.17	2.00	1.93	0.65	140.06	1.31	183.60	0.656	No	No	0.75
229	22.90	136.06	2.00	1.98	0.65	147.16	1.31	192.22	0.741	No	No	0.85
230	23.00	147.42	1.98	2.01	0.65	158.93	1.29	205.52	4.000	No	No	2.00
231	23.10	160.45	1.96	2.02	0.64	172.36	1.28	220.33	4.000	No	No	2.00
232	23.20	171.23	1.95	2.03	0.63	183.35	1.27	232.50	4.000	No	No	2.00
233	23.30	180.27	1.94	2.06	0.63	192.47	1.26	242.96	4.000	No	No	2.00
234	23.40	187.37	1.93	2.09	0.63	199.53	1.26	251.28	4.000	No	No	2.00
235	23.50	191.52	1.93	2.11	0.63	203.42	1.26	255.94	4.000	No	No	2.00
236	23.60	191.73	1.93	2.11	0.63	203.15	1.26	255.76	4.000	No	No	2.00
237	23.70	187.36	1.94	2.12	0.63	198.09	1.26	250.43	4.000	No	No	2.00
238	23.80	178.72	1.96	2.17	0.64	188.68	1.28	241.10	4.000	No	No	2.00
239	23.90	166.77	2.00	2.33	0.66	176.03	1.31	230.76	4.000	No	No	2.00
240	24.00	149.50	2.05	2.47	0.67	157.77	1.36	214.38	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
241	24.10	133.96	2.09	2.49	0.69	141.16	1.40	197.71	0.799	No	No	0.91
242	24.20	126.47	2.08	2.29	0.68	132.75	1.39	184.07	0.660	No	No	0.75
243	24.30	128.47	2.04	2.09	0.67	134.23	1.35	180.75	0.629	No	No	0.72
244	24.40	130.78	2.02	1.97	0.66	136.14	1.32	180.37	0.626	No	No	0.71
245	24.50	124.66	2.04	2.01	0.67	129.53	1.34	174.11	4.000	Yes	No	2.00
246	24.60	110.33	2.10	2.19	0.69	114.62	1.42	163.11	4.000	Yes	No	2.00
247	24.70	91.14	2.21	2.58	0.74	94.77	1.64	155.70	4.000	Yes	No	2.00
248	24.80	72.12	2.34	3.12	0.79	75.03	2.09	157.06	4.000	Yes	No	2.00
249	24.90	57.73	2.47	3.80	0.83	60.01	2.78	167.00	4.000	Yes	No	2.00
250	25.00	49.70	2.56	4.40	0.87	51.55	4.22	217.76	4.000	Yes	No	2.00
251	25.10	47.44	2.61	4.83	0.89	49.10	5.61	275.57	4.000	Yes	No	2.00
252	25.20	45.12	2.65	5.22	0.90	46.57	7.25	337.76	4.000	Yes	No	2.00
253	25.30	42.32	2.69	5.58	0.92	43.53	9.41	409.65	4.000	Yes	No	2.00
254	25.40	41.45	2.70	5.62	0.92	42.49	9.97	423.48	4.000	Yes	No	2.00
255	25.50	47.50	2.61	4.87	0.89	48.57	5.83	283.09	4.000	Yes	No	2.00
256	25.60	58.52	2.47	3.79	0.84	59.61	2.79	166.06	4.000	Yes	No	2.00
257	25.70	69.31	2.34	2.92	0.79	70.27	2.08	146.49	4.000	Yes	No	2.00
258	25.80	77.97	2.25	2.44	0.75	78.74	1.75	138.03	4.000	Yes	No	2.00
259	25.90	83.74	2.21	2.28	0.74	84.31	1.63	137.77	4.000	Yes	No	2.00
260	26.00	87.01	2.20	2.27	0.73	87.39	1.60	140.10	0.336	No	No	0.38
261	26.10	87.64	2.21	2.39	0.74	87.86	1.64	143.93	0.357	No	No	0.40
262	26.20	89.33	2.21	2.43	0.74	89.36	1.64	146.64	0.373	No	No	0.42
263	26.30	93.87	2.18	2.30	0.73	93.64	1.57	146.57	0.373	No	No	0.42
264	26.40	98.42	2.13	2.07	0.71	97.85	1.47	144.09	0.358	No	No	0.40
265	26.50	100.49	2.11	1.95	0.70	99.62	1.43	142.74	0.350	No	No	0.40
266	26.60	99.58	2.12	2.00	0.70	98.50	1.45	142.91	0.351	No	No	0.40
267	26.70	99.14	2.14	2.09	0.71	97.88	1.48	144.55	0.361	No	No	0.41
268	26.80	99.48	2.15	2.17	0.71	98.02	1.50	146.75	0.374	No	No	0.42
269	26.90	100.62	2.15	2.21	0.72	98.93	1.50	148.83	0.387	No	No	0.44
270	27.00	102.38	2.15	2.23	0.71	100.44	1.50	150.56	0.397	No	No	0.45
271	27.10	104.07	2.14	2.22	0.71	101.85	1.49	151.74	0.405	No	No	0.46
272	27.20	105.35	2.14	2.24	0.71	102.88	1.49	153.24	0.415	No	No	0.47
273	27.30	105.96	2.15	2.32	0.72	103.26	1.51	155.76	0.431	No	No	0.49
274	27.40	106.62	2.17	2.46	0.72	103.70	1.54	160.19	0.462	No	No	0.52
275	27.50	107.61	2.18	2.59	0.73	104.45	1.58	164.74	0.496	No	No	0.56
276	27.60	109.14	2.19	2.63	0.73	105.71	1.58	167.22	0.515	No	No	0.58
277	27.70	111.42	2.18	2.58	0.73	107.65	1.56	167.55	0.517	No	No	0.58
278	27.80	114.37	2.16	2.53	0.72	110.25	1.53	168.34	0.524	No	No	0.59
279	27.90	117.17	2.15	2.49	0.72	112.69	1.50	169.46	0.533	No	No	0.60
280	28.00	117.25	2.14	2.40	0.71	112.47	1.48	166.81	0.512	No	No	0.58
281	28.10	113.03	2.14	2.29	0.71	108.10	1.48	159.62	0.458	No	No	0.52
282	28.20	104.54	2.16	2.30	0.72	99.66	1.53	152.02	0.407	No	No	0.46
283	28.30	96.33	2.20	2.41	0.74	91.54	1.62	147.84	0.381	No	No	0.43
284	28.40	89.43	2.24	2.52	0.75	84.70	1.72	145.31	0.365	No	No	0.41
285	28.50	84.52	2.25	2.49	0.76	79.78	1.76	140.20	0.336	No	No	0.38
286	28.60	79.72	2.28	2.53	0.77	74.99	1.84	137.82	4.000	Yes	No	2.00
287	28.70	74.73	2.32	2.71	0.78	70.04	1.99	139.59	4.000	Yes	No	2.00
288	28.80	69.75	2.38	3.07	0.81	65.14	2.26	147.46	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
289	28.90	62.88	2.45	3.51	0.83	58.43	2.67	156.21	4.000	Yes	No	2.00
290	29.00	55.17	2.53	3.96	0.86	50.94	3.48	177.37	4.000	Yes	No	2.00
291	29.10	47.60	2.60	4.30	0.89	43.63	5.57	243.07	4.000	Yes	No	2.00
292	29.20	41.43	2.66	4.48	0.91	37.66	8.06	303.64	4.000	Yes	No	2.00
293	29.30	37.19	2.71	4.65	0.93	33.54	4.81	161.27	4.000	Yes	Yes	2.00
294	29.40	34.70	2.75	4.86	0.95	31.10	5.22	162.34	4.000	Yes	Yes	2.00
295	29.50	34.06	2.76	5.01	0.95	30.41	5.41	164.37	1.450	No	Yes	1.63
296	29.60	33.91	2.76	4.97	0.95	30.18	5.40	163.10	1.440	No	Yes	1.62
297	29.70	32.03	2.78	4.85	0.96	28.33	5.55	157.22	1.352	No	Yes	1.52
298	29.80	29.66	2.80	4.82	0.97	26.04	5.86	152.48	1.242	No	Yes	1.39
299	29.90	28.43	2.83	5.05	0.98	24.82	6.23	154.62	1.184	No	Yes	1.33
300	30.00	32.28	2.82	5.62	0.98	28.32	6.10	172.81	1.351	No	Yes	1.51
301	30.10	38.09	2.78	5.89	0.96	33.62	5.63	189.28	1.604	No	Yes	1.80
302	30.20	43.19	2.74	5.87	0.95	38.24	5.16	197.31	1.824	No	Yes	2.00
303	30.30	44.63	2.73	5.88	0.94	39.45	5.06	199.76	1.882	No	Yes	2.00
304	30.40	44.36	2.75	6.06	0.95	39.09	5.20	203.30	1.865	No	Yes	2.00
305	30.50	46.20	2.74	6.25	0.95	40.66	5.18	210.68	4.000	Yes	Yes	2.00
306	30.60	51.44	2.69	5.84	0.93	45.36	9.54	432.78	4.000	Yes	No	2.00
307	30.70	59.73	2.59	4.99	0.89	52.86	5.21	275.43	4.000	Yes	No	2.00
308	30.80	69.61	2.48	4.03	0.85	61.82	2.85	175.99	4.000	Yes	No	2.00
309	30.90	81.48	2.36	3.24	0.80	72.59	2.19	159.10	4.000	Yes	No	2.00
310	31.00	94.67	2.26	2.74	0.77	84.56	1.80	152.10	4.000	Yes	No	2.00
311	31.10	106.82	2.20	2.49	0.74	95.53	1.61	153.84	4.000	Yes	No	2.00
312	31.20	116.62	2.17	2.45	0.73	104.28	1.54	160.36	4.000	Yes	No	2.00
313	31.30	124.76	2.16	2.52	0.73	111.44	1.52	169.30	0.531	No	No	0.60
314	31.40	130.68	2.16	2.60	0.72	116.55	1.51	176.48	0.591	No	No	0.66
315	31.50	133.94	2.15	2.61	0.72	119.25	1.50	179.13	0.615	No	No	0.69
316	31.60	134.30	2.14	2.57	0.72	119.31	1.49	178.20	0.606	No	No	0.68
317	31.70	132.00	2.15	2.56	0.72	116.97	1.50	175.44	0.582	No	No	0.65
318	31.80	124.86	2.16	2.54	0.73	110.25	1.53	168.77	0.527	No	No	0.59
319	31.90	112.69	2.19	2.51	0.74	99.05	1.59	157.38	0.443	No	No	0.50
320	32.00	97.91	2.23	2.52	0.76	85.54	1.71	146.00	0.369	No	No	0.41
321	32.10	85.37	2.30	2.71	0.78	74.05	1.93	142.83	0.351	No	No	0.39
322	32.20	78.62	2.37	3.08	0.81	67.76	2.21	149.84	0.393	No	No	0.44
323	32.30	78.07	2.40	3.35	0.82	67.05	2.36	158.28	0.449	No	No	0.50
324	32.40	82.35	2.39	3.39	0.81	70.67	2.30	162.57	0.480	No	No	0.54
325	32.50	89.96	2.34	3.24	0.80	77.28	2.11	162.74	0.481	No	No	0.54
326	32.60	100.87	2.28	2.97	0.77	86.85	1.86	161.56	0.472	No	No	0.53
327	32.70	114.12	2.21	2.65	0.75	98.53	1.64	161.25	0.470	No	No	0.53
328	32.80	125.97	2.14	2.31	0.72	109.00	1.48	161.04	0.468	No	No	0.53
329	32.90	133.61	2.09	2.13	0.70	115.67	1.41	162.86	0.482	No	No	0.54
330	33.00	136.56	2.07	2.03	0.69	118.12	1.38	162.91	0.482	No	No	0.54
331	33.10	135.19	2.05	1.90	0.69	116.76	1.36	158.61	0.451	No	No	0.51
332	33.20	129.92	2.04	1.75	0.68	111.98	1.34	150.52	0.397	No	No	0.45
333	33.30	122.33	2.04	1.67	0.68	105.12	1.35	141.68	0.344	No	No	0.39
334	33.40	115.41	2.09	1.80	0.70	98.69	1.40	138.12	0.325	No	No	0.37
335	33.50	111.66	2.13	1.98	0.72	95.06	1.46	139.16	0.331	No	No	0.37
336	33.60	111.68	2.16	2.19	0.73	94.74	1.52	144.33	0.360	No	No	0.40

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
337	33.70	116.59	2.17	2.39	0.74	98.70	1.55	153.47	0.416	No	No	0.47
338	33.80	126.41	2.16	2.48	0.73	106.98	1.53	163.95	0.490	No	No	0.55
339	33.90	138.32	2.13	2.43	0.72	117.17	1.47	172.07	0.554	No	No	0.62
340	34.00	149.33	2.09	2.26	0.70	126.67	1.40	177.04	0.596	No	No	0.67
341	34.10	156.01	2.04	2.07	0.69	132.42	1.35	178.45	0.609	No	No	0.69
342	34.20	158.07	2.02	1.95	0.68	134.09	1.33	177.73	0.602	No	No	0.68
343	34.30	158.80	2.02	1.94	0.68	134.48	1.32	177.83	0.603	No	No	0.68
344	34.40	162.94	2.02	2.00	0.68	137.73	1.33	182.67	0.647	No	No	0.73
345	34.50	169.31	2.02	2.08	0.68	142.88	1.33	189.67	0.715	No	No	0.81
346	34.60	175.37	2.02	2.11	0.68	147.80	1.32	195.71	0.777	No	No	0.88
347	34.70	179.32	2.01	2.12	0.68	150.90	1.32	199.20	0.815	No	No	0.92
348	34.80	184.04	2.00	2.10	0.67	154.72	1.31	202.79	4.000	No	No	2.00
349	34.90	189.55	1.99	2.03	0.67	159.27	1.30	206.34	4.000	No	No	2.00
350	35.00	194.31	1.96	1.94	0.66	163.22	1.28	208.83	4.000	No	No	2.00
351	35.10	196.77	1.95	1.88	0.65	165.14	1.27	209.65	4.000	No	No	2.00
352	35.20	196.37	1.95	1.86	0.65	164.51	1.27	208.69	4.000	No	No	2.00
353	35.30	193.58	1.95	1.87	0.65	161.78	1.27	205.79	4.000	No	No	2.00
354	35.40	189.34	1.96	1.84	0.65	157.88	1.27	201.11	4.000	No	No	2.00
355	35.50	184.20	1.95	1.78	0.65	153.28	1.27	195.01	0.770	No	No	0.87
356	35.60	178.51	1.95	1.70	0.65	148.27	1.27	188.06	0.699	No	No	0.79
357	35.70	173.44	1.94	1.60	0.65	143.85	1.26	181.47	0.636	No	No	0.72
358	35.80	169.68	1.92	1.49	0.64	140.61	1.25	175.85	0.586	No	No	0.67
359	35.90	166.88	1.90	1.35	0.63	138.27	1.23	170.58	0.542	No	No	0.62
360	36.00	163.35	1.87	1.21	0.62	135.35	1.21	164.34	0.493	No	No	0.56
361	36.10	158.25	1.85	1.09	0.61	131.07	1.20	156.95	0.440	No	No	0.50
362	36.20	152.33	1.84	1.03	0.61	125.91	1.20	150.54	0.397	No	No	0.45
363	36.30	147.13	1.86	1.04	0.62	121.22	1.21	146.45	0.372	No	No	0.42
364	36.40	143.89	1.88	1.10	0.63	118.12	1.22	144.64	0.361	No	No	0.41
365	36.50	142.53	1.90	1.15	0.64	116.63	1.24	144.26	0.359	No	No	0.41
366	36.60	143.00	1.91	1.19	0.64	116.75	1.24	145.14	0.364	No	No	0.42
367	36.70	145.61	1.91	1.23	0.64	118.68	1.25	147.82	0.380	No	No	0.43
368	36.80	150.56	1.91	1.26	0.64	122.60	1.24	152.46	0.410	No	No	0.47
369	36.90	157.66	1.90	1.27	0.64	128.36	1.24	158.76	0.452	No	No	0.52
370	37.00	165.31	1.88	1.27	0.63	134.63	1.23	165.06	0.498	No	No	0.57
371	37.10	172.32	1.87	1.24	0.62	140.40	1.21	170.24	0.539	No	No	0.62
372	37.20	177.10	1.85	1.23	0.62	144.25	1.20	173.64	0.567	No	No	0.65
373	37.30	178.87	1.85	1.24	0.62	145.48	1.20	175.04	0.579	No	No	0.66
374	37.40	177.96	1.86	1.26	0.62	144.39	1.21	174.63	0.575	No	No	0.66
375	37.50	175.45	1.87	1.28	0.63	141.98	1.22	172.74	0.559	No	No	0.64
376	37.60	172.65	1.88	1.30	0.63	139.32	1.22	170.61	0.542	No	No	0.62
377	37.70	169.90	1.90	1.34	0.64	136.69	1.23	168.64	0.526	No	No	0.60
378	37.80	167.26	1.91	1.37	0.64	134.14	1.24	166.75	0.511	No	No	0.59
379	37.90	165.19	1.92	1.41	0.65	132.09	1.25	165.34	0.500	No	No	0.57
380	38.00	164.02	1.94	1.46	0.65	130.76	1.26	164.82	0.496	No	No	0.57
381	38.10	163.69	1.95	1.51	0.66	130.12	1.27	165.07	0.498	No	No	0.57
382	38.20	163.69	1.96	1.54	0.66	129.81	1.27	165.36	0.501	No	No	0.58
383	38.30	163.49	1.96	1.57	0.66	129.34	1.28	165.43	0.501	No	No	0.58
384	38.40	162.37	1.97	1.61	0.67	128.10	1.29	164.72	0.496	No	No	0.57

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
385	38.50	159.91	1.98	1.64	0.67	125.77	1.29	162.83	0.482	No	No	0.55
386	38.60	156.57	2.00	1.66	0.68	122.75	1.30	160.06	0.461	No	No	0.53
387	38.70	153.20	2.01	1.69	0.68	119.72	1.31	157.36	0.442	No	No	0.51
388	38.80	150.08	2.02	1.72	0.69	116.88	1.33	155.01	0.426	No	No	0.49
389	38.90	147.28	2.03	1.75	0.69	114.34	1.34	152.87	0.412	No	No	0.48
390	39.00	145.42	2.04	1.75	0.69	112.61	1.34	151.20	0.401	No	No	0.46
391	39.10	145.19	2.04	1.74	0.69	112.25	1.34	150.60	0.398	No	No	0.46
392	39.20	146.51	2.03	1.72	0.69	113.17	1.33	151.00	0.400	No	No	0.46
393	39.30	148.08	2.02	1.68	0.69	114.32	1.32	151.41	0.403	No	No	0.47
394	39.40	149.40	2.01	1.63	0.68	115.30	1.31	151.51	0.403	No	No	0.47
395	39.50	150.23	2.00	1.58	0.68	115.88	1.31	151.30	0.402	No	No	0.47
396	39.60	150.45	1.99	1.54	0.67	115.97	1.30	150.55	0.397	No	No	0.46
397	39.70	151.53	1.98	1.50	0.67	116.74	1.29	150.71	0.398	No	No	0.46
398	39.80	153.36	1.97	1.49	0.67	118.05	1.29	151.87	0.406	No	No	0.47
399	39.90	155.09	1.98	1.54	0.67	119.10	1.29	153.97	0.419	No	No	0.49
400	40.00	154.86	2.00	1.63	0.68	118.49	1.31	154.83	0.425	No	No	0.49
401	40.10	154.63	2.01	1.68	0.68	117.96	1.32	155.31	0.428	No	No	0.50
402	40.20	156.64	2.01	1.68	0.68	119.36	1.31	156.78	0.438	No	No	0.51
403	40.30	160.77	2.00	1.66	0.68	122.51	1.30	159.73	0.459	No	No	0.53
404	40.40	165.07	1.99	1.64	0.67	125.78	1.30	162.91	0.482	No	No	0.56
405	40.50	168.83	1.97	1.62	0.67	128.65	1.29	165.46	0.501	No	No	0.58
406	40.60	172.09	1.96	1.58	0.66	131.16	1.28	167.39	0.516	No	No	0.60
407	40.70	175.00	1.94	1.53	0.66	133.42	1.27	168.92	0.528	No	No	0.62
408	40.80	177.41	1.93	1.49	0.65	135.24	1.26	170.18	0.538	No	No	0.63
409	40.90	179.23	1.93	1.48	0.65	136.52	1.25	171.30	0.547	No	No	0.64
410	41.00	180.47	1.93	1.50	0.65	137.19	1.26	172.48	0.557	No	No	0.65
411	41.10	181.45	1.94	1.55	0.66	137.57	1.26	173.82	0.568	No	No	0.67
412	41.20	182.77	1.95	1.60	0.66	138.22	1.27	175.39	0.582	No	No	0.68
413	41.30	184.68	1.95	1.64	0.66	139.37	1.27	177.32	0.599	No	No	0.70
414	41.40	186.86	1.95	1.65	0.66	140.83	1.27	179.01	0.613	No	No	0.72
415	41.50	189.12	1.94	1.60	0.66	142.53	1.26	180.06	0.623	No	No	0.73
416	41.60	190.91	1.92	1.54	0.65	143.95	1.25	180.34	0.625	No	No	0.74
417	41.70	192.03	1.92	1.51	0.65	144.73	1.25	180.50	0.627	No	No	0.74
418	41.80	192.92	1.92	1.54	0.65	145.05	1.25	181.54	0.636	No	No	0.75
419	41.90	194.40	1.94	1.62	0.66	145.67	1.26	183.70	0.656	No	No	0.77
420	42.00	197.14	1.95	1.69	0.66	147.32	1.27	186.79	0.686	No	No	0.81
421	42.10	200.61	1.95	1.74	0.66	149.60	1.27	190.20	0.720	No	No	0.85
422	42.20	203.97	1.96	1.78	0.67	151.83	1.27	193.36	0.752	No	No	0.89
423	42.30	206.60	1.96	1.81	0.67	153.50	1.28	195.75	0.778	No	No	0.92
424	42.40	208.12	1.96	1.82	0.67	154.40	1.28	196.88	0.790	No	No	0.94
425	42.50	208.30	1.95	1.80	0.67	154.35	1.27	196.42	0.785	No	No	0.93
426	42.60	206.70	1.95	1.77	0.66	152.96	1.27	194.35	0.763	No	No	0.91
427	42.70	203.68	1.95	1.74	0.66	150.46	1.27	191.08	0.729	No	No	0.87
428	42.80	199.57	1.95	1.71	0.66	147.12	1.27	187.01	0.688	No	No	0.82
429	42.90	194.71	1.96	1.72	0.67	143.07	1.28	182.77	0.648	No	No	0.77
430	43.00	190.18	1.98	1.77	0.68	139.13	1.29	179.57	0.619	No	No	0.74
431	43.10	187.86	2.00	1.86	0.68	136.81	1.31	178.70	0.611	No	No	0.73
432	43.20	190.13	2.00	1.91	0.69	138.14	1.31	181.14	0.633	No	No	0.76

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
433	43.30	197.38	1.99	1.91	0.68	143.46	1.30	186.81	0.686	No	No	0.82
434	43.40	207.80	1.97	1.87	0.67	151.34	1.29	194.55	0.765	No	No	0.92
435	43.50	219.34	1.95	1.82	0.66	160.16	1.27	203.06	4.000	No	No	2.00
436	43.60	230.48	1.92	1.78	0.66	168.65	1.25	211.34	4.000	No	No	2.00
437	43.70	240.76	1.91	1.75	0.65	176.40	1.24	219.09	4.000	No	No	2.00
438	43.80	249.82	1.90	1.75	0.65	183.13	1.23	226.01	4.000	No	No	2.00
439	43.90	258.68	1.88	1.73	0.64	189.73	1.23	232.53	4.000	No	No	2.00
440	44.00	267.99	1.86	1.67	0.63	196.97	1.21	238.11	4.000	No	No	2.00
441	44.10	276.85	1.83	1.55	0.62	204.25	1.18	241.03	4.000	No	No	2.00
442	44.20	284.85	1.78	1.39	0.60	211.29	1.13	238.83	4.000	No	No	2.00
443	44.30	291.10	1.73	1.23	0.58	217.20	1.06	229.18	4.000	No	No	2.00
444	44.40	294.85	1.70	1.12	0.57	220.87	1.00	220.87	4.000	No	No	2.00
445	44.50	294.77	1.69	1.10	0.57	220.75	1.00	220.75	4.000	No	No	2.00
446	44.60	292.55	1.71	1.15	0.57	218.20	1.00	218.92	4.000	No	No	2.00
447	44.70	291.79	1.72	1.18	0.58	217.01	1.02	222.23	4.000	No	No	2.00
448	44.80	294.37	1.70	1.13	0.57	219.18	1.00	219.18	4.000	No	No	2.00
449	44.90	299.33	1.67	1.03	0.56	223.84	1.00	223.84	4.000	No	No	2.00
450	45.00	305.05	1.63	0.95	0.55	228.94	1.00	228.94	4.000	No	No	2.00
451	45.10	310.35	1.62	0.94	0.54	233.00	1.00	233.00	4.000	No	No	2.00
452	45.20	314.64	1.63	0.96	0.55	235.82	1.00	235.82	4.000	No	No	2.00
453	45.30	316.67	1.64	0.99	0.55	236.72	1.00	236.72	4.000	No	No	2.00
454	45.40	316.15	1.65	1.02	0.55	235.62	1.00	235.62	4.000	No	No	2.00
455	45.50	314.75	1.66	1.07	0.56	233.66	1.00	233.66	4.000	No	No	2.00
456	45.60	313.96	1.68	1.12	0.57	232.13	1.00	232.13	4.000	No	No	2.00
457	45.70	313.55	1.69	1.15	0.57	231.06	1.00	231.06	4.000	No	No	2.00
458	45.80	312.06	1.70	1.16	0.57	229.50	1.00	229.50	4.000	No	No	2.00
459	45.90	308.31	1.69	1.13	0.57	226.55	1.00	226.55	4.000	No	No	2.00
460	46.00	302.20	1.69	1.09	0.57	221.94	1.00	221.94	4.000	No	No	2.00
461	46.10	293.67	1.68	1.04	0.57	215.60	1.00	215.60	4.000	No	No	2.00
462	46.20	283.78	1.67	0.99	0.56	208.21	1.00	208.21	4.000	No	No	2.00
463	46.30	273.76	1.66	0.92	0.56	200.90	1.00	200.90	4.000	No	No	2.00
464	46.40	264.02	1.65	0.86	0.56	193.71	1.00	193.71	0.756	No	No	0.93
465	46.50	253.44	1.66	0.83	0.56	185.59	1.00	185.59	0.674	No	No	0.83
466	46.60	239.32	1.68	0.85	0.57	174.12	1.00	174.12	0.571	No	No	0.71
467	46.70	218.44	1.75	0.94	0.59	156.86	1.08	169.18	4.000	Yes	No	2.00
468	46.80	190.67	1.85	1.13	0.63	134.12	1.20	161.00	4.000	Yes	No	2.00
469	46.90	159.42	1.99	1.46	0.69	108.98	1.30	141.79	4.000	Yes	No	2.00
470	47.00	130.94	2.16	2.01	0.75	86.50	1.53	132.00	4.000	Yes	No	2.00
471	47.10	109.62	2.33	2.79	0.82	69.95	2.03	142.18	4.000	Yes	No	2.00
472	47.20	99.20	2.46	3.72	0.86	61.64	2.69	165.64	4.000	Yes	No	2.00
473	47.30	101.82	2.50	4.36	0.88	62.70	2.82	176.86	4.000	Yes	No	2.00
474	47.40	114.04	2.47	4.34	0.87	70.74	2.75	194.52	4.000	Yes	No	2.00
475	47.50	127.97	2.39	3.87	0.84	80.48	2.33	187.25	4.000	Yes	No	2.00
476	47.60	134.39	2.33	3.41	0.82	85.31	2.05	175.23	4.000	Yes	No	2.00
477	47.70	131.72	2.32	3.26	0.82	83.56	2.02	168.52	0.525	No	No	0.66
478	47.80	123.26	2.36	3.41	0.83	77.42	2.18	168.66	0.526	No	No	0.66
479	47.90	115.03	2.40	3.59	0.84	71.49	2.37	169.66	0.534	No	No	0.67
480	48.00	111.14	2.40	3.49	0.85	68.85	2.38	164.20	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
481	48.10	113.23	2.35	3.06	0.83	70.68	2.14	151.48	4.000	Yes	No	2.00
482	48.20	120.10	2.26	2.47	0.79	76.16	1.80	136.95	4.000	Yes	No	2.00
483	48.30	127.66	2.16	1.92	0.75	82.45	1.53	125.94	4.000	Yes	No	2.00
484	48.40	131.70	2.08	1.51	0.72	86.31	1.39	119.72	4.000	Yes	No	2.00
485	48.50	130.27	2.03	1.30	0.71	85.89	1.34	114.96	4.000	Yes	No	2.00
486	48.60	123.72	2.05	1.29	0.71	81.11	1.36	109.95	4.000	Yes	No	2.00
487	48.70	112.92	2.13	1.49	0.74	72.70	1.46	106.49	4.000	Yes	No	2.00
488	48.80	98.74	2.26	1.93	0.79	61.77	1.77	109.45	4.000	Yes	No	2.00
489	48.90	82.92	2.41	2.61	0.85	50.01	2.44	121.83	4.000	Yes	No	2.00
490	49.00	68.00	2.57	3.42	0.91	39.45	4.37	172.46	4.000	Yes	No	2.00
491	49.10	55.01	2.71	4.18	0.96	30.71	4.77	146.38	4.000	Yes	Yes	2.00
492	49.20	44.63	2.82	4.69	1.00	24.09	6.07	146.17	4.000	Yes	Yes	2.00
493	49.30	36.24	2.90	4.88	1.00	19.19	7.24	138.98	4.000	Yes	Yes	2.00
494	49.40	30.08	2.97	4.82	1.00	15.61	8.24	128.62	4.000	Yes	Yes	2.00
495	49.50	25.88	3.01	4.59	1.00	13.16	8.98	118.11	0.628	No	Yes	0.80
496	49.60	23.84	3.03	4.33	1.00	11.96	9.27	110.93	0.570	No	Yes	0.73
497	49.70	26.26	2.98	4.18	1.00	13.33	8.47	112.92	0.636	No	Yes	0.81
498	49.80	32.30	2.91	4.26	1.00	16.76	7.34	123.05	0.800	No	Yes	1.02
499	49.90	38.31	2.85	4.35	1.00	20.17	6.55	132.08	0.962	No	Yes	1.23

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q_t :	Total cone resistance
I_c :	Soil behavior type index
Fr:	Normalized friction ratio (%)
n:	Stress exponent
Q_{tn} :	Normalized cone resistance
K_c :	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Normalized and adjusted cone resistance
CRR _{7.5} :	Cyclic resistance ratio for $M_w=7.5$
FS:	Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
0.10	2.00	0.00	0.00	0.10	0.00	0.20	2.00	0.00	0.00	0.10	0.00
0.30	2.00	0.00	0.00	0.10	0.00	0.40	2.00	0.00	0.00	0.10	0.00
0.50	2.00	0.00	0.00	0.10	0.00	0.60	2.00	0.00	0.00	0.10	0.00
0.70	2.00	0.00	0.00	0.10	0.00	0.80	2.00	0.00	0.00	0.10	0.00
0.90	2.00	0.00	0.00	0.10	0.00	1.00	2.00	0.00	0.00	0.10	0.00
1.10	2.00	0.00	0.00	0.10	0.00	1.20	2.00	0.00	0.00	0.10	0.00
1.30	2.00	0.00	0.00	0.10	0.00	1.40	2.00	0.00	0.00	0.10	0.00
1.50	2.00	0.00	0.00	0.10	0.00	1.60	2.00	0.00	0.00	0.10	0.00
1.70	2.00	0.00	0.00	0.10	0.00	1.80	2.00	0.00	0.00	0.10	0.00
1.90	2.00	0.00	0.00	0.10	0.00	2.00	2.00	0.00	0.00	0.10	0.00
2.10	2.00	0.00	0.00	0.10	0.00	2.20	2.00	0.00	0.00	0.10	0.00
2.30	2.00	0.00	0.00	0.10	0.00	2.40	2.00	0.00	0.00	0.10	0.00
2.50	2.00	0.00	0.00	0.10	0.00	2.60	2.00	0.00	0.00	0.10	0.00
2.70	2.00	0.00	0.00	0.10	0.00	2.80	2.00	0.00	0.00	0.10	0.00
2.90	2.00	0.00	0.00	0.10	0.00	3.00	2.00	0.00	0.00	0.10	0.00
3.10	2.00	0.00	0.00	0.10	0.00	3.20	2.00	0.00	0.00	0.10	0.00
3.30	2.00	0.00	0.00	0.10	0.00	3.40	2.00	0.00	0.00	0.10	0.00
3.50	2.00	0.00	0.00	0.10	0.00	3.60	2.00	0.00	0.00	0.10	0.00
3.70	2.00	0.00	0.00	0.10	0.00	3.80	2.00	0.00	0.00	0.10	0.00
3.90	2.00	0.00	0.00	0.10	0.00	4.00	2.00	0.00	0.00	0.10	0.00
4.10	2.00	0.00	0.00	0.10	0.00	4.20	2.00	0.00	0.00	0.10	0.00
4.30	2.00	0.00	0.00	0.10	0.00	4.40	2.00	0.00	0.00	0.10	0.00
4.50	2.00	0.00	0.00	0.10	0.00	4.60	2.00	0.00	0.00	0.10	0.00
4.70	2.00	0.00	0.00	0.10	0.00	4.80	2.00	0.00	0.00	0.10	0.00
4.90	2.00	0.00	0.00	0.10	0.00	5.00	2.00	0.00	0.00	0.10	0.00
5.10	2.00	0.00	0.00	0.10	0.00	5.20	2.00	0.00	0.00	0.10	0.00
5.30	2.00	0.00	0.00	0.10	0.00	5.40	2.00	0.00	0.00	0.10	0.00
5.50	2.00	0.00	0.00	0.10	0.00	5.60	2.00	0.00	0.00	0.10	0.00
5.70	2.00	0.00	0.00	0.10	0.00	5.80	2.00	0.00	0.00	0.10	0.00
5.90	2.00	0.00	0.00	0.10	0.00	6.00	2.00	0.00	0.00	0.10	0.00
6.10	2.00	0.00	0.00	0.10	0.00	6.20	2.00	0.00	0.00	0.10	0.00
6.30	2.00	0.00	0.00	0.10	0.00	6.40	2.00	0.00	0.00	0.10	0.00
6.50	2.00	0.00	0.00	0.10	0.00	6.60	2.00	0.00	0.00	0.10	0.00
6.70	2.00	0.00	0.00	0.10	0.00	6.80	2.00	0.00	0.00	0.10	0.00
6.90	2.00	0.00	0.00	0.10	0.00	7.00	2.00	0.00	0.00	0.10	0.00
7.10	2.00	0.00	0.00	0.10	0.00	7.20	2.00	0.00	0.00	0.10	0.00
7.30	2.00	0.00	0.00	0.10	0.00	7.40	2.00	0.00	0.00	0.10	0.00
7.50	2.00	0.00	0.00	0.10	0.00	7.60	2.00	0.00	0.00	0.10	0.00
7.70	2.00	0.00	0.00	0.10	0.00	7.80	2.00	0.00	0.00	0.10	0.00
7.90	2.00	0.00	0.00	0.10	0.00	8.00	2.00	0.00	0.00	0.10	0.00
8.10	1.37	0.00	0.00	0.10	0.00	8.20	1.21	0.00	0.00	0.10	0.00
8.30	1.04	0.00	0.00	0.10	0.00	8.40	0.92	0.00	0.00	0.10	0.02
8.50	0.86	0.00	0.00	0.10	0.04	8.60	0.87	0.00	0.00	0.10	0.04
8.70	0.87	0.00	0.00	0.10	0.04	8.80	0.85	0.00	0.00	0.10	0.04
8.90	0.84	0.00	0.00	0.10	0.04	9.00	0.84	0.00	0.00	0.10	0.04
9.10	0.81	0.00	0.00	0.10	0.05	9.20	0.73	0.00	0.00	0.10	0.07
9.30	0.66	0.00	0.00	0.10	0.09	9.40	0.65	0.00	0.00	0.10	0.09
9.50	0.71	0.00	0.00	0.10	0.08	9.60	0.76	0.00	0.00	0.10	0.06

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
9.70	1.01	0.00	0.00	0.10	0.00	9.80	1.47	0.00	0.00	0.10	0.00
9.90	1.60	0.00	0.00	0.10	0.00	10.00	1.33	0.00	0.00	0.10	0.00
10.10	0.81	0.00	0.00	0.10	0.05	10.20	0.64	0.00	0.00	0.10	0.09
10.30	0.69	0.00	0.00	0.10	0.08	10.40	0.72	0.00	0.00	0.10	0.07
10.50	0.72	0.00	0.00	0.10	0.07	10.60	0.72	0.00	0.00	0.10	0.07
10.70	0.71	0.00	0.00	0.10	0.07	10.80	0.71	0.00	0.00	0.10	0.08
10.90	0.70	0.00	0.00	0.10	0.08	11.00	0.69	0.00	0.00	0.10	0.08
11.10	0.69	0.00	0.00	0.10	0.08	11.20	0.74	0.00	0.00	0.10	0.07
11.30	0.90	0.00	0.00	0.10	0.03	11.40	1.11	0.00	0.00	0.10	0.00
11.50	1.27	0.00	0.00	0.10	0.00	11.60	1.28	0.00	0.00	0.10	0.00
11.70	1.17	0.00	0.00	0.10	0.00	11.80	1.02	0.00	0.00	0.10	0.00
11.90	0.89	0.00	0.00	0.10	0.03	12.00	0.91	0.00	0.00	0.10	0.02
12.10	1.09	0.00	0.00	0.10	0.00	12.20	1.35	0.00	0.00	0.10	0.00
12.30	1.50	0.00	0.00	0.10	0.00	12.40	1.53	0.00	0.00	0.10	0.00
12.50	1.53	0.00	0.00	0.10	0.00	12.60	1.61	0.00	0.00	0.10	0.00
12.70	1.72	0.00	0.00	0.10	0.00	12.80	1.75	0.00	0.00	0.10	0.00
12.90	1.60	0.00	0.00	0.10	0.00	13.00	1.35	0.00	0.00	0.10	0.00
13.10	1.13	0.00	0.00	0.10	0.00	13.20	0.99	0.00	0.00	0.10	0.00
13.30	0.97	0.00	0.00	0.10	0.01	13.40	1.04	0.00	0.00	0.10	0.00
13.50	1.14	0.00	0.00	0.10	0.00	13.60	1.22	0.00	0.00	0.10	0.00
13.70	1.25	0.00	0.00	0.10	0.00	13.80	1.20	0.00	0.00	0.10	0.00
13.90	1.14	0.00	0.00	0.10	0.00	14.00	1.08	0.00	0.00	0.10	0.00
14.10	1.05	0.00	0.00	0.10	0.00	14.20	1.04	0.00	0.00	0.10	0.00
14.30	1.06	0.00	0.00	0.10	0.00	14.40	1.12	0.00	0.00	0.10	0.00
14.50	1.20	0.00	0.00	0.10	0.00	14.60	1.29	0.00	0.00	0.10	0.00
14.70	1.37	0.00	0.00	0.10	0.00	14.80	1.40	0.00	0.00	0.10	0.00
14.90	1.34	0.00	0.00	0.10	0.00	15.00	1.25	0.00	0.00	0.10	0.00
15.10	1.17	0.00	0.00	0.10	0.00	15.20	1.15	0.00	0.00	0.10	0.00
15.30	1.21	0.00	0.00	0.10	0.00	15.40	1.29	0.00	0.00	0.10	0.00
15.50	1.31	0.00	0.00	0.10	0.00	15.60	1.28	0.00	0.00	0.10	0.00
15.70	1.28	0.00	0.00	0.10	0.00	15.80	1.33	0.00	0.00	0.10	0.00
15.90	1.34	0.00	0.00	0.10	0.00	16.00	1.32	0.00	0.00	0.10	0.00
16.10	1.46	0.00	0.00	0.10	0.00	16.20	1.77	0.00	0.00	0.10	0.00
16.30	2.00	0.00	0.00	0.10	0.00	16.40	2.00	0.00	0.00	0.10	0.00
16.50	1.92	0.00	0.00	0.10	0.00	16.60	1.50	0.00	0.00	0.10	0.00
16.70	1.05	0.00	0.00	0.10	0.00	16.80	0.69	0.00	0.00	0.10	0.07
16.90	0.51	0.00	0.00	0.10	0.11	17.00	0.45	0.00	0.00	0.10	0.13
17.10	0.43	0.00	0.00	0.10	0.13	17.20	0.42	0.00	0.00	0.10	0.13
17.30	0.41	0.00	0.00	0.10	0.13	17.40	0.41	0.00	0.00	0.10	0.13
17.50	0.44	0.00	0.00	0.10	0.12	17.60	0.52	0.00	0.00	0.10	0.11
17.70	0.59	0.00	0.00	0.10	0.09	17.80	0.61	0.00	0.00	0.10	0.09
17.90	0.61	0.00	0.00	0.10	0.09	18.00	0.60	0.00	0.00	0.10	0.09
18.10	0.58	0.00	0.00	0.10	0.09	18.20	0.57	0.00	0.00	0.10	0.09
18.30	0.64	0.00	0.00	0.10	0.08	18.40	0.79	0.00	0.00	0.10	0.05
18.50	0.95	0.00	0.00	0.10	0.01	18.60	1.04	0.00	0.00	0.10	0.00
18.70	1.14	0.00	0.00	0.10	0.00	18.80	1.21	0.00	0.00	0.10	0.00
18.90	1.23	0.00	0.00	0.10	0.00	19.00	1.10	0.00	0.00	0.10	0.00
19.10	0.88	0.00	0.00	0.10	0.03	19.20	0.74	0.00	0.00	0.10	0.06

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
19.30	0.71	0.00	0.00	0.10	0.06	19.40	0.79	0.00	0.00	0.10	0.05
19.50	0.93	0.00	0.00	0.10	0.01	19.60	1.09	0.00	0.00	0.10	0.00
19.70	1.23	0.00	0.00	0.10	0.00	19.80	1.34	0.00	0.00	0.10	0.00
19.90	1.30	0.00	0.00	0.10	0.00	20.00	1.13	0.00	0.00	0.10	0.00
20.10	0.94	0.00	0.00	0.10	0.01	20.20	0.83	0.00	0.00	0.10	0.04
20.30	0.82	0.00	0.00	0.10	0.04	20.40	0.83	0.00	0.00	0.10	0.04
20.50	0.87	0.00	0.00	0.10	0.03	20.60	0.94	0.00	0.00	0.10	0.01
20.70	1.00	0.00	0.00	0.10	0.00	20.80	1.08	0.00	0.00	0.10	0.00
20.90	2.00	0.00	0.00	0.10	0.00	21.00	2.00	0.00	0.00	0.10	0.00
21.10	2.00	0.00	0.00	0.10	0.00	21.20	2.00	0.00	0.00	0.10	0.00
21.30	2.00	0.00	0.00	0.10	0.00	21.40	2.00	0.00	0.00	0.10	0.00
21.50	2.00	0.00	0.00	0.10	0.00	21.60	0.26	0.00	0.00	0.10	0.15
21.70	0.28	0.00	0.00	0.10	0.15	21.80	0.37	0.00	0.00	0.10	0.13
21.90	2.00	0.00	0.00	0.10	0.00	22.00	2.00	0.00	0.00	0.10	0.00
22.10	2.00	0.00	0.00	0.10	0.00	22.20	2.00	0.00	0.00	0.10	0.00
22.30	2.00	0.00	0.00	0.10	0.00	22.40	2.00	0.00	0.00	0.10	0.00
22.50	0.57	0.00	0.00	0.10	0.09	22.60	0.65	0.00	0.00	0.10	0.07
22.70	0.71	0.00	0.00	0.10	0.06	22.80	0.75	0.00	0.00	0.10	0.05
22.90	0.85	0.00	0.00	0.10	0.03	23.00	2.00	0.00	0.00	0.10	0.00
23.10	2.00	0.00	0.00	0.10	0.00	23.20	2.00	0.00	0.00	0.10	0.00
23.30	2.00	0.00	0.00	0.10	0.00	23.40	2.00	0.00	0.00	0.10	0.00
23.50	2.00	0.00	0.00	0.10	0.00	23.60	2.00	0.00	0.00	0.10	0.00
23.70	2.00	0.00	0.00	0.10	0.00	23.80	2.00	0.00	0.00	0.10	0.00
23.90	2.00	0.00	0.00	0.10	0.00	24.00	2.00	0.00	0.00	0.10	0.00
24.10	0.91	0.00	0.00	0.10	0.02	24.20	0.75	0.00	0.00	0.10	0.05
24.30	0.72	0.00	0.00	0.10	0.05	24.40	0.71	0.00	0.00	0.10	0.05
24.50	2.00	0.00	0.00	0.10	0.00	24.60	2.00	0.00	0.00	0.10	0.00
24.70	2.00	0.00	0.00	0.10	0.00	24.80	2.00	0.00	0.00	0.10	0.00
24.90	2.00	0.00	0.00	0.10	0.00	25.00	2.00	0.00	0.00	0.10	0.00
25.10	2.00	0.00	0.00	0.10	0.00	25.20	2.00	0.00	0.00	0.10	0.00
25.30	2.00	0.00	0.00	0.10	0.00	25.40	2.00	0.00	0.00	0.10	0.00
25.50	2.00	0.00	0.00	0.10	0.00	25.60	2.00	0.00	0.00	0.10	0.00
25.70	2.00	0.00	0.00	0.10	0.00	25.80	2.00	0.00	0.00	0.10	0.00
25.90	2.00	0.00	0.00	0.10	0.00	26.00	0.38	0.62	0.37	0.10	0.11
26.10	0.40	0.00	0.00	0.10	0.11	26.20	0.42	0.00	0.00	0.10	0.11
26.30	0.42	0.00	0.00	0.10	0.11	26.40	0.40	0.00	0.00	0.10	0.11
26.50	0.40	0.00	0.00	0.10	0.11	26.60	0.40	0.00	0.00	0.10	0.11
26.70	0.41	0.00	0.00	0.10	0.11	26.80	0.42	0.00	0.00	0.10	0.10
26.90	0.44	0.00	0.00	0.10	0.10	27.00	0.45	0.00	0.00	0.10	0.10
27.10	0.46	0.00	0.00	0.10	0.10	27.20	0.47	0.00	0.00	0.10	0.10
27.30	0.49	0.00	0.00	0.10	0.09	27.40	0.52	0.00	0.00	0.10	0.09
27.50	0.56	0.00	0.00	0.10	0.08	27.60	0.58	0.00	0.00	0.10	0.07
27.70	0.58	0.00	0.00	0.10	0.07	27.80	0.59	0.00	0.00	0.10	0.07
27.90	0.60	0.00	0.00	0.10	0.07	28.00	0.58	0.00	0.00	0.10	0.07
28.10	0.52	0.00	0.00	0.10	0.08	28.20	0.46	0.00	0.00	0.10	0.09
28.30	0.43	0.00	0.00	0.10	0.10	28.40	0.41	0.00	0.00	0.10	0.10
28.50	0.38	0.62	0.37	0.10	0.11	28.60	2.00	0.00	0.00	0.10	0.00
28.70	2.00	0.00	0.00	0.10	0.00	28.80	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
28.90	2.00	0.00	0.00	0.10	0.00	29.00	2.00	0.00	0.00	0.10	0.00
29.10	2.00	0.00	0.00	0.10	0.00	29.20	2.00	0.00	0.00	0.10	0.00
29.30	2.00	0.00	0.00	0.10	0.00	29.40	2.00	0.00	0.00	0.10	0.00
29.50	1.63	0.00	0.00	0.10	0.00	29.60	1.62	0.00	0.00	0.10	0.00
29.70	1.52	0.00	0.00	0.10	0.00	29.80	1.39	0.00	0.00	0.10	0.00
29.90	1.33	0.00	0.00	0.10	0.00	30.00	1.51	0.00	0.00	0.10	0.00
30.10	1.80	0.00	0.00	0.10	0.00	30.20	2.00	0.00	0.00	0.10	0.00
30.30	2.00	0.00	0.00	0.10	0.00	30.40	2.00	0.00	0.00	0.10	0.00
30.50	2.00	0.00	0.00	0.10	0.00	30.60	2.00	0.00	0.00	0.10	0.00
30.70	2.00	0.00	0.00	0.10	0.00	30.80	2.00	0.00	0.00	0.10	0.00
30.90	2.00	0.00	0.00	0.10	0.00	31.00	2.00	0.00	0.00	0.10	0.00
31.10	2.00	0.00	0.00	0.10	0.00	31.20	2.00	0.00	0.00	0.10	0.00
31.30	0.60	0.00	0.00	0.10	0.06	31.40	0.66	0.00	0.00	0.10	0.05
31.50	0.69	0.00	0.00	0.10	0.05	31.60	0.68	0.00	0.00	0.10	0.05
31.70	0.65	0.00	0.00	0.10	0.05	31.80	0.59	0.00	0.00	0.10	0.06
31.90	0.50	0.00	0.00	0.10	0.08	32.00	0.41	0.00	0.00	0.10	0.09
32.10	0.39	0.00	0.00	0.10	0.09	32.20	0.44	0.00	0.00	0.10	0.09
32.30	0.50	0.00	0.00	0.10	0.08	32.40	0.54	0.00	0.00	0.10	0.07
32.50	0.54	0.00	0.00	0.10	0.07	32.60	0.53	0.00	0.00	0.10	0.07
32.70	0.53	0.00	0.00	0.10	0.07	32.80	0.53	0.00	0.00	0.10	0.07
32.90	0.54	0.00	0.00	0.10	0.07	33.00	0.54	0.00	0.00	0.10	0.07
33.10	0.51	0.00	0.00	0.10	0.07	33.20	0.45	0.00	0.00	0.10	0.08
33.30	0.39	0.61	0.38	0.10	0.09	33.40	0.37	0.63	0.36	0.10	0.09
33.50	0.37	0.63	0.37	0.10	0.09	33.60	0.40	0.00	0.00	0.10	0.09
33.70	0.47	0.00	0.00	0.10	0.08	33.80	0.55	0.00	0.00	0.10	0.07
33.90	0.62	0.00	0.00	0.10	0.06	34.00	0.67	0.00	0.00	0.10	0.05
34.10	0.69	0.00	0.00	0.10	0.05	34.20	0.68	0.00	0.00	0.10	0.05
34.30	0.68	0.00	0.00	0.10	0.05	34.40	0.73	0.00	0.00	0.10	0.04
34.50	0.81	0.00	0.00	0.10	0.03	34.60	0.88	0.00	0.00	0.10	0.02
34.70	0.92	0.00	0.00	0.10	0.01	34.80	2.00	0.00	0.00	0.10	0.00
34.90	2.00	0.00	0.00	0.10	0.00	35.00	2.00	0.00	0.00	0.10	0.00
35.10	2.00	0.00	0.00	0.10	0.00	35.20	2.00	0.00	0.00	0.10	0.00
35.30	2.00	0.00	0.00	0.10	0.00	35.40	2.00	0.00	0.00	0.10	0.00
35.50	0.87	0.00	0.00	0.10	0.02	35.60	0.79	0.00	0.00	0.10	0.03
35.70	0.72	0.00	0.00	0.10	0.04	35.80	0.67	0.00	0.00	0.10	0.05
35.90	0.62	0.00	0.00	0.10	0.05	36.00	0.56	0.00	0.00	0.10	0.06
36.10	0.50	0.00	0.00	0.10	0.07	36.20	0.45	0.00	0.00	0.10	0.07
36.30	0.42	0.00	0.00	0.10	0.08	36.40	0.41	0.00	0.00	0.10	0.08
36.50	0.41	0.00	0.00	0.10	0.08	36.60	0.42	0.00	0.00	0.10	0.08
36.70	0.43	0.00	0.00	0.10	0.08	36.80	0.47	0.00	0.00	0.10	0.07
36.90	0.52	0.00	0.00	0.10	0.06	37.00	0.57	0.00	0.00	0.10	0.06
37.10	0.62	0.00	0.00	0.10	0.05	37.20	0.65	0.00	0.00	0.10	0.05
37.30	0.66	0.00	0.00	0.10	0.04	37.40	0.66	0.00	0.00	0.10	0.04
37.50	0.64	0.00	0.00	0.10	0.05	37.60	0.62	0.00	0.00	0.10	0.05
37.70	0.60	0.00	0.00	0.10	0.05	37.80	0.59	0.00	0.00	0.10	0.05
37.90	0.57	0.00	0.00	0.10	0.05	38.00	0.57	0.00	0.00	0.10	0.06
38.10	0.57	0.00	0.00	0.10	0.05	38.20	0.58	0.00	0.00	0.10	0.05
38.30	0.58	0.00	0.00	0.10	0.05	38.40	0.57	0.00	0.00	0.10	0.05

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
38.50	0.55	0.00	0.00	0.10	0.06	38.60	0.53	0.00	0.00	0.10	0.06
38.70	0.51	0.00	0.00	0.10	0.06	38.80	0.49	0.00	0.00	0.10	0.06
38.90	0.48	0.00	0.00	0.10	0.07	39.00	0.46	0.00	0.00	0.10	0.07
39.10	0.46	0.00	0.00	0.10	0.07	39.20	0.46	0.00	0.00	0.10	0.07
39.30	0.47	0.00	0.00	0.10	0.07	39.40	0.47	0.00	0.00	0.10	0.06
39.50	0.47	0.00	0.00	0.10	0.06	39.60	0.46	0.00	0.00	0.10	0.07
39.70	0.46	0.00	0.00	0.10	0.06	39.80	0.47	0.00	0.00	0.10	0.06
39.90	0.49	0.00	0.00	0.10	0.06	40.00	0.49	0.00	0.00	0.10	0.06
40.10	0.50	0.00	0.00	0.10	0.06	40.20	0.51	0.00	0.00	0.10	0.06
40.30	0.53	0.00	0.00	0.10	0.05	40.40	0.56	0.00	0.00	0.10	0.05
40.50	0.58	0.00	0.00	0.10	0.05	40.60	0.60	0.00	0.00	0.10	0.05
40.70	0.62	0.00	0.00	0.10	0.04	40.80	0.63	0.00	0.00	0.10	0.04
40.90	0.64	0.00	0.00	0.10	0.04	41.00	0.65	0.00	0.00	0.10	0.04
41.10	0.67	0.00	0.00	0.10	0.04	41.20	0.68	0.00	0.00	0.10	0.04
41.30	0.70	0.00	0.00	0.10	0.03	41.40	0.72	0.00	0.00	0.10	0.03
41.50	0.73	0.00	0.00	0.10	0.03	41.60	0.74	0.00	0.00	0.10	0.03
41.70	0.74	0.00	0.00	0.10	0.03	41.80	0.75	0.00	0.00	0.10	0.03
41.90	0.77	0.00	0.00	0.10	0.02	42.00	0.81	0.00	0.00	0.10	0.02
42.10	0.85	0.00	0.00	0.10	0.02	42.20	0.89	0.00	0.00	0.10	0.01
42.30	0.92	0.00	0.00	0.10	0.01	42.40	0.94	0.00	0.00	0.10	0.01
42.50	0.93	0.00	0.00	0.10	0.01	42.60	0.91	0.00	0.00	0.10	0.01
42.70	0.87	0.00	0.00	0.10	0.01	42.80	0.82	0.00	0.00	0.10	0.02
42.90	0.77	0.00	0.00	0.10	0.02	43.00	0.74	0.00	0.00	0.10	0.03
43.10	0.73	0.00	0.00	0.10	0.03	43.20	0.76	0.00	0.00	0.10	0.03
43.30	0.82	0.00	0.00	0.10	0.02	43.40	0.92	0.00	0.00	0.10	0.01
43.50	2.00	0.00	0.00	0.10	0.00	43.60	2.00	0.00	0.00	0.10	0.00
43.70	2.00	0.00	0.00	0.10	0.00	43.80	2.00	0.00	0.00	0.10	0.00
43.90	2.00	0.00	0.00	0.10	0.00	44.00	2.00	0.00	0.00	0.10	0.00
44.10	2.00	0.00	0.00	0.10	0.00	44.20	2.00	0.00	0.00	0.10	0.00
44.30	2.00	0.00	0.00	0.10	0.00	44.40	2.00	0.00	0.00	0.10	0.00
44.50	2.00	0.00	0.00	0.10	0.00	44.60	2.00	0.00	0.00	0.10	0.00
44.70	2.00	0.00	0.00	0.10	0.00	44.80	2.00	0.00	0.00	0.10	0.00
44.90	2.00	0.00	0.00	0.10	0.00	45.00	2.00	0.00	0.00	0.10	0.00
45.10	2.00	0.00	0.00	0.10	0.00	45.20	2.00	0.00	0.00	0.10	0.00
45.30	2.00	0.00	0.00	0.10	0.00	45.40	2.00	0.00	0.00	0.10	0.00
45.50	2.00	0.00	0.00	0.10	0.00	45.60	2.00	0.00	0.00	0.10	0.00
45.70	2.00	0.00	0.00	0.10	0.00	45.80	2.00	0.00	0.00	0.10	0.00
45.90	2.00	0.00	0.00	0.10	0.00	46.00	2.00	0.00	0.00	0.10	0.00
46.10	2.00	0.00	0.00	0.10	0.00	46.20	2.00	0.00	0.00	0.10	0.00
46.30	2.00	0.00	0.00	0.10	0.00	46.40	0.93	0.00	0.00	0.10	0.01
46.50	0.83	0.00	0.00	0.10	0.01	46.60	0.71	0.00	0.00	0.10	0.03
46.70	2.00	0.00	0.00	0.10	0.00	46.80	2.00	0.00	0.00	0.10	0.00
46.90	2.00	0.00	0.00	0.10	0.00	47.00	2.00	0.00	0.00	0.10	0.00
47.10	2.00	0.00	0.00	0.10	0.00	47.20	2.00	0.00	0.00	0.10	0.00
47.30	2.00	0.00	0.00	0.10	0.00	47.40	2.00	0.00	0.00	0.10	0.00
47.50	2.00	0.00	0.00	0.10	0.00	47.60	2.00	0.00	0.00	0.10	0.00
47.70	0.66	0.00	0.00	0.10	0.03	47.80	0.66	0.00	0.00	0.10	0.03
47.90	0.67	0.00	0.00	0.10	0.03	48.00	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
48.10	2.00	0.00	0.00	0.10	0.00	48.20	2.00	0.00	0.00	0.10	0.00
48.30	2.00	0.00	0.00	0.10	0.00	48.40	2.00	0.00	0.00	0.10	0.00
48.50	2.00	0.00	0.00	0.10	0.00	48.60	2.00	0.00	0.00	0.10	0.00
48.70	2.00	0.00	0.00	0.10	0.00	48.80	2.00	0.00	0.00	0.10	0.00
48.90	2.00	0.00	0.00	0.10	0.00	49.00	2.00	0.00	0.00	0.10	0.00
49.10	2.00	0.00	0.00	0.10	0.00	49.20	2.00	0.00	0.00	0.10	0.00
49.30	2.00	0.00	0.00	0.10	0.00	49.40	2.00	0.00	0.00	0.10	0.00
49.50	0.80	0.00	0.00	0.10	0.01	49.60	0.73	0.00	0.00	0.10	0.02
49.70	0.81	0.00	0.00	0.10	0.01	49.80	1.02	0.00	0.00	0.10	0.00
49.90	1.23	0.00	0.00	0.10	0.00						

Overall liquefaction potential: 13.30

LPI = 0.00 - Liquefaction risk very low

LPI between 0.00 and 5.00 - Liquefaction risk low

LPI between 5.00 and 15.00 - Liquefaction risk high

LPI > 15.00 - Liquefaction risk very high

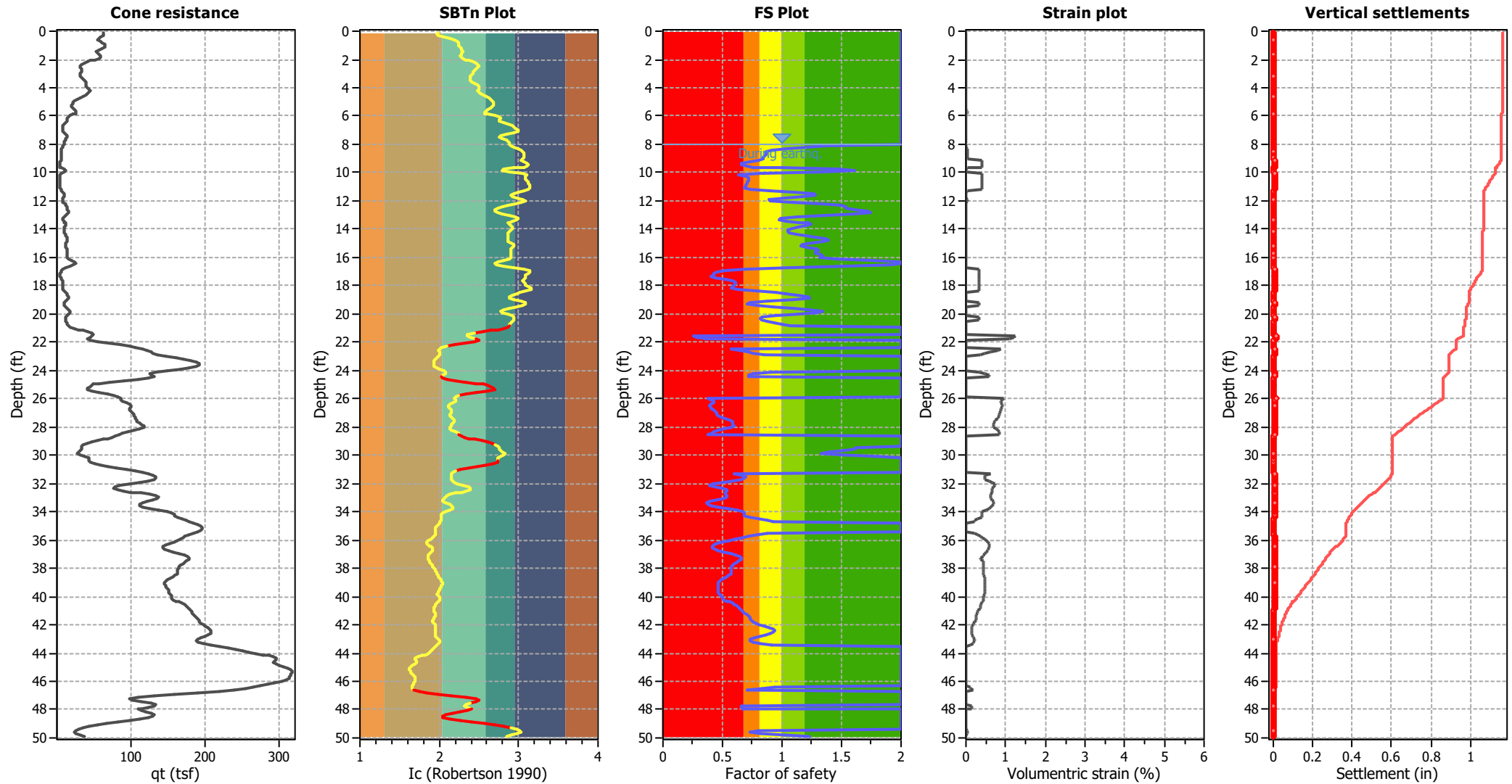
Abbreviations

FS: Calculated factor of safety for test point

F_L: 1 - FSw_z: Function value of the extend of soil liquefaction according to depthd_z: Layer thickness (ft)

LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

q_c : Total cone resistance (cone resistance q_c corrected for pore water effects)
 I_c : Soil Behaviour Type Index
 FS: Calculated Factor of Safety against liquefaction
 Volumetric strain: Post-liquefaction volumetric strain

:: Post-earthquake settlement of dry sands ::												
Depth (ft)	Ic	Q _{tn}	Kc	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _r (%)	Settle. (in)
0.10	2.00	119.66	1.30	156.12	32	714	0.59	0.000	0.00	13.69	0.00	0.000
0.20	1.98	121.18	1.29	156.29	32	706	0.59	0.001	0.00	13.69	0.00	0.000
0.30	1.99	120.15	1.30	155.76	32	708	0.59	0.001	0.00	13.69	0.00	0.000
0.40	2.06	114.13	1.36	155.54	33	735	0.59	0.002	0.00	13.69	0.00	0.000
0.50	2.13	108.04	1.47	158.82	35	765	0.59	0.002	0.00	13.69	0.00	0.000
0.60	2.19	106.77	1.59	169.97	38	815	0.59	0.003	0.00	13.69	0.00	0.000
0.70	2.23	111.51	1.68	187.49	43	889	0.59	0.003	0.00	13.69	0.00	0.000
0.80	2.24	117.93	1.73	203.76	47	960	0.59	0.003	0.00	13.69	0.00	0.000
0.90	2.25	122.13	1.75	213.48	49	1002	0.59	0.003	0.00	13.69	0.00	0.000
1.00	2.25	123.84	1.76	217.84	50	1021	0.59	0.003	0.00	13.69	0.00	0.000
1.10	2.26	121.95	1.78	217.35	50	1015	0.59	0.004	0.00	13.69	0.00	0.000
1.20	2.27	116.59	1.82	212.53	49	986	0.59	0.004	0.00	13.69	0.00	0.000
1.30	2.29	108.04	1.88	202.58	47	931	0.59	0.005	0.00	13.69	0.00	0.000
1.40	2.29	102.99	1.89	194.84	46	892	0.59	0.006	0.00	13.69	0.00	0.000
1.50	2.28	103.76	1.87	193.76	45	891	0.59	0.007	0.00	13.69	0.00	0.000
1.60	2.28	107.88	1.84	198.15	46	917	0.59	0.007	0.00	13.69	0.00	0.000
1.70	2.27	112.67	1.82	204.57	48	950	0.59	0.007	0.00	13.69	0.00	0.000
1.80	2.27	114.32	1.83	208.96	49	968	0.59	0.007	0.00	13.69	0.00	0.000
1.90	2.29	109.24	1.91	208.12	49	951	0.59	0.008	0.00	13.69	0.00	0.000
2.00	2.33	99.36	2.06	204.26	49	908	0.59	0.009	0.00	13.69	0.00	0.000
2.10	2.38	88.02	2.27	200.15	49	854	0.59	0.011	0.00	13.69	0.00	0.000
2.20	2.42	79.39	2.48	196.72	49	809	0.59	0.013	0.00	13.69	0.00	0.000
2.30	2.46	71.05	2.69	190.95	48	758	0.59	0.015	0.01	13.69	0.00	0.000
2.40	2.49	63.44	2.89	183.12	47	704	0.59	0.019	0.01	13.69	0.01	0.000
2.50	2.50	59.81	2.96	177.04	46	673	0.59	0.022	0.01	13.69	0.01	0.000
2.60	2.49	60.34	2.89	174.10	45	669	0.59	0.023	0.01	13.69	0.01	0.000
2.70	2.47	62.88	2.75	172.91	44	679	0.59	0.024	0.01	13.69	0.01	0.000
2.80	2.44	64.86	2.62	170.11	43	683	0.59	0.025	0.01	13.69	0.01	0.000
2.90	2.43	63.92	2.56	163.33	41	663	0.59	0.028	0.01	13.69	0.01	0.000
3.00	2.42	62.43	2.48	154.72	38	636	0.59	0.033	0.01	13.69	0.01	0.000
3.10	2.41	61.04	2.42	147.49	36	613	0.59	0.038	0.02	13.69	0.02	0.000
3.20	2.40	62.33	2.36	147.00	36	618	0.59	0.039	0.02	13.69	0.02	0.000
3.30	2.39	65.27	2.33	152.13	37	642	0.59	0.037	0.02	13.69	0.02	0.000
3.40	2.39	69.63	2.32	161.38	40	683	0.59	0.033	0.01	13.69	0.01	0.000
3.50	2.39	73.59	2.34	172.41	42	726	0.59	0.030	0.01	13.69	0.01	0.000
3.60	2.41	75.74	2.44	184.64	46	765	0.59	0.028	0.01	13.69	0.01	0.000
3.70	2.44	75.67	2.62	198.15	50	796	0.59	0.026	0.01	13.69	0.01	0.000
3.80	2.48	75.33	2.82	212.41	54	825	0.59	0.025	0.01	13.69	0.01	0.000
3.90	2.50	76.35	2.96	226.23	58	859	0.59	0.024	0.01	13.69	0.01	0.000
4.00	2.50	79.52	2.99	237.41	61	899	0.59	0.023	0.01	13.69	0.01	0.000
4.10	2.49	83.32	2.92	243.30	62	930	0.59	0.022	0.01	13.69	0.01	0.000
4.20	2.48	85.27	2.88	245.18	63	944	0.59	0.022	0.01	13.69	0.01	0.000
4.30	2.49	84.24	2.92	246.11	63	941	0.59	0.023	0.01	13.69	0.01	0.000
4.40	2.52	80.33	3.09	248.37	65	926	0.59	0.025	0.01	13.69	0.01	0.000
4.50	2.55	74.26	3.35	249.12	66	895	0.59	0.028	0.01	13.69	0.01	0.000
4.60	2.59	66.78	3.66	244.66	66	844	0.59	0.032	0.01	13.69	0.01	0.000
4.70	2.63	58.86	3.99	234.70	0	0	0.59	0.000	0.00	0.00	0.00	0.000
4.80	2.65	52.45	4.24	222.61	0	0	0.59	0.000	0.00	0.00	0.00	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
4.90	2.67	47.36	4.43	209.85	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.00	2.68	43.60	4.52	197.05	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.10	2.68	40.51	4.54	184.02	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.20	2.68	38.63	4.50	173.86	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.30	2.67	38.66	4.40	170.17	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.40	2.65	41.00	4.20	172.14	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.50	2.62	44.97	3.89	175.14	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.60	2.58	48.54	3.61	175.19	47	609	0.59	0.118	0.04	13.69	0.04	0.000
5.70	2.57	49.72	3.46	172.24	46	610	0.59	0.121	0.04	13.69	0.04	0.000
5.80	2.57	48.17	3.52	169.63	45	596	0.59	0.137	0.05	13.69	0.04	0.001
5.90	2.62	42.81	3.90	167.03	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.00	2.69	35.45	4.63	164.01	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.10	2.76	30.15	5.35	161.34	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.20	2.77	28.66	5.50	157.72	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.30	2.75	28.86	5.29	152.63	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.40	2.76	26.81	5.39	144.51	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.50	2.81	23.10	5.96	137.59	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.60	2.87	19.81	6.80	134.72	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.70	2.92	17.90	7.51	134.34	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.80	2.94	17.12	7.84	134.24	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.90	2.96	16.34	8.17	133.47	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.00	2.99	15.69	8.57	134.43	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.10	2.99	16.28	8.60	140.05	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.20	2.93	19.26	7.72	148.60	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.30	2.85	23.82	6.44	153.29	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.40	2.78	27.01	5.56	150.18	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.50	2.75	27.04	5.31	143.64	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.60	2.79	24.34	5.71	138.90	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.70	2.84	21.70	6.41	139.00	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.80	2.87	20.42	6.83	139.42	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.90	2.88	19.65	6.93	136.20	0	0	0.58	0.000	0.00	0.00	0.00	0.000

Total estimated settlement: 0.00**Abbreviations**

Q_{tn}: Equivalent clean sand normalized cone resistance
 K_c: Fines correction factor
 Q_{tn,cs}: Post-liquefaction volumetric strain
 G_{max}: Small strain shear modulus
 CSR: Soil cyclic stress ratio
 γ: Cyclic shear strain
 e_{vol(15)}: Volumetric strain after 15 cycles
 N_c: Equivalent number of cycles
 e_v: Volumetric strain
 Settle.: Calculated settlement

:: Post-earthquake settlement due to soil liquefaction ::

Depth (ft)	Q _{tn,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	Q _{tn,cs}	FS	e _v (%)	DF	Settlement (in)
8.00	129.68	2.00	0.00	0.85	0.00	8.10	122.43	1.37	0.01	0.85	0.00
8.20	116.38	1.21	0.01	0.85	0.00	8.30	111.11	1.04	0.02	0.85	0.00
8.40	107.50	0.92	0.03	0.85	0.00	8.50	106.28	0.86	0.04	0.85	0.00
8.60	107.81	0.87	0.04	0.84	0.00	8.70	109.72	0.87	0.04	0.84	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
8.80	109.93	0.85	0.04	0.84	0.00	8.90	107.84	0.84	0.04	0.84	0.00
9.00	103.70	0.84	0.04	0.84	0.00	9.10	98.73	0.81	0.42	0.83	0.01
9.20	94.03	0.73	0.42	0.83	0.00	9.30	91.95	0.66	0.42	0.83	0.00
9.40	94.52	0.65	0.41	0.83	0.00	9.50	98.73	0.71	0.41	0.83	0.00
9.60	100.37	0.76	0.41	0.83	0.00	9.70	105.29	1.01	0.02	0.82	0.00
9.80	120.15	1.47	0.00	0.82	0.00	9.90	127.08	1.60	0.00	0.82	0.00
10.00	124.23	1.33	0.01	0.82	0.00	10.10	105.62	0.81	0.41	0.82	0.00
10.20	93.57	0.64	0.41	0.81	0.00	10.30	97.26	0.69	0.41	0.81	0.00
10.40	102.21	0.72	0.41	0.81	0.00	10.50	105.41	0.72	0.40	0.81	0.00
10.60	107.70	0.72	0.40	0.81	0.00	10.70	109.69	0.71	0.40	0.81	0.00
10.80	111.47	0.71	0.40	0.80	0.00	10.90	111.87	0.70	0.40	0.80	0.00
11.00	110.87	0.69	0.40	0.80	0.00	11.10	111.03	0.69	0.40	0.80	0.00
11.20	117.58	0.74	0.40	0.80	0.00	11.30	131.45	0.90	0.02	0.79	0.00
11.40	141.14	1.11	0.01	0.79	0.00	11.50	141.33	1.27	0.01	0.79	0.00
11.60	133.57	1.28	0.01	0.79	0.00	11.70	126.54	1.17	0.01	0.79	0.00
11.80	124.65	1.02	0.01	0.79	0.00	11.90	127.66	0.89	0.02	0.78	0.00
12.00	138.78	0.91	0.02	0.78	0.00	12.10	153.07	1.09	0.01	0.78	0.00
12.20	159.25	1.35	0.01	0.78	0.00	12.30	150.55	1.50	0.00	0.78	0.00
12.40	132.52	1.53	0.00	0.77	0.00	12.50	117.45	1.53	0.00	0.77	0.00
12.60	115.42	1.61	0.00	0.77	0.00	12.70	123.21	1.72	0.00	0.77	0.00
12.80	133.95	1.75	0.00	0.77	0.00	12.90	141.15	1.60	0.00	0.77	0.00
13.00	142.74	1.35	0.00	0.76	0.00	13.10	138.59	1.13	0.01	0.76	0.00
13.20	130.62	0.99	0.01	0.76	0.00	13.30	124.20	0.97	0.02	0.76	0.00
13.40	122.03	1.04	0.01	0.76	0.00	13.50	124.47	1.14	0.01	0.75	0.00
13.60	129.09	1.22	0.01	0.75	0.00	13.70	133.53	1.25	0.01	0.75	0.00
13.80	135.37	1.20	0.01	0.75	0.00	13.90	133.41	1.14	0.01	0.75	0.00
14.00	127.31	1.08	0.01	0.75	0.00	14.10	119.87	1.05	0.01	0.74	0.00
14.20	114.51	1.04	0.01	0.74	0.00	14.30	114.46	1.06	0.01	0.74	0.00
14.40	120.36	1.12	0.01	0.74	0.00	14.50	129.64	1.20	0.01	0.74	0.00
14.60	138.64	1.29	0.01	0.73	0.00	14.70	145.18	1.37	0.00	0.73	0.00
14.80	148.08	1.40	0.00	0.73	0.00	14.90	147.59	1.34	0.00	0.73	0.00
15.00	145.73	1.25	0.01	0.73	0.00	15.10	144.60	1.17	0.01	0.73	0.00
15.20	145.60	1.15	0.01	0.72	0.00	15.30	148.96	1.21	0.01	0.72	0.00
15.40	153.13	1.29	0.00	0.72	0.00	15.50	154.28	1.31	0.00	0.72	0.00
15.60	154.30	1.28	0.00	0.72	0.00	15.70	154.60	1.28	0.00	0.71	0.00
15.80	156.19	1.33	0.00	0.71	0.00	15.90	157.05	1.34	0.00	0.71	0.00
16.00	158.82	1.32	0.00	0.71	0.00	16.10	165.86	1.46	0.00	0.71	0.00
16.20	173.16	1.77	0.00	0.71	0.00	16.30	174.43	2.00	0.00	0.70	0.00
16.40	168.71	2.00	0.00	0.70	0.00	16.50	159.48	1.92	0.00	0.70	0.00
16.60	148.44	1.50	0.00	0.70	0.00	16.70	134.33	1.05	0.01	0.70	0.00
16.80	115.18	0.69	0.35	0.69	0.00	16.90	97.81	0.51	0.35	0.69	0.00
17.00	85.89	0.45	0.35	0.69	0.00	17.10	78.82	0.43	0.34	0.69	0.00
17.20	74.86	0.42	0.34	0.69	0.00	17.30	71.77	0.41	0.34	0.69	0.00
17.40	71.28	0.41	0.34	0.68	0.00	17.50	76.80	0.44	0.34	0.68	0.00
17.60	87.63	0.52	0.34	0.68	0.00	17.70	97.83	0.59	0.34	0.68	0.00
17.80	103.65	0.61	0.34	0.68	0.00	17.90	106.06	0.61	0.34	0.67	0.00
18.00	107.95	0.60	0.34	0.67	0.00	18.10	111.30	0.58	0.34	0.67	0.00
18.20	117.52	0.57	0.33	0.67	0.00	18.30	129.03	0.64	0.33	0.67	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
18.40	142.71	0.79	0.33	0.67	0.00	18.50	150.66	0.95	0.01	0.66	0.00
18.60	149.99	1.04	0.01	0.66	0.00	18.70	147.34	1.14	0.01	0.66	0.00
18.80	147.37	1.21	0.01	0.66	0.00	18.90	149.51	1.23	0.00	0.66	0.00
19.00	148.27	1.10	0.01	0.65	0.00	19.10	141.32	0.88	0.01	0.65	0.00
19.20	133.05	0.74	0.33	0.65	0.00	19.30	128.88	0.71	0.32	0.65	0.00
19.40	131.31	0.79	0.32	0.65	0.00	19.50	135.51	0.93	0.01	0.65	0.00
19.60	136.32	1.09	0.01	0.64	0.00	19.70	131.71	1.23	0.00	0.64	0.00
19.80	130.07	1.34	0.00	0.64	0.00	19.90	132.05	1.30	0.00	0.64	0.00
20.00	131.72	1.13	0.01	0.64	0.00	20.10	125.84	0.94	0.01	0.63	0.00
20.20	116.35	0.83	0.32	0.63	0.00	20.30	114.59	0.82	0.32	0.63	0.00
20.40	116.39	0.83	0.31	0.63	0.00	20.50	119.00	0.87	0.01	0.63	0.00
20.60	121.13	0.94	0.01	0.63	0.00	20.70	124.61	1.00	0.01	0.62	0.00
20.80	133.55	1.08	0.01	0.62	0.00	20.90	150.76	2.00	0.00	0.62	0.00
21.00	172.52	2.00	0.00	0.62	0.00	21.10	186.26	2.00	0.00	0.62	0.00
21.20	330.91	2.00	0.00	0.61	0.00	21.30	191.76	2.00	0.00	0.61	0.00
21.40	141.74	2.00	0.00	0.61	0.00	21.50	122.62	2.00	0.00	0.61	0.00
21.60	115.61	0.26	1.26	0.61	0.02	21.70	120.95	0.28	1.21	0.61	0.01
21.80	136.86	0.37	1.09	0.60	0.01	21.90	146.36	2.00	0.00	0.60	0.00
22.00	164.44	2.00	0.00	0.60	0.00	22.10	160.56	2.00	0.00	0.60	0.00
22.20	154.39	2.00	0.00	0.60	0.00	22.30	152.73	2.00	0.00	0.59	0.00
22.40	156.28	2.00	0.00	0.59	0.00	22.50	164.41	0.57	0.87	0.59	0.01
22.60	172.90	0.65	0.81	0.59	0.01	22.70	179.79	0.71	0.63	0.59	0.01
22.80	183.60	0.75	0.49	0.59	0.01	22.90	192.22	0.85	0.35	0.58	0.00
23.00	205.52	2.00	0.00	0.58	0.00	23.10	220.33	2.00	0.00	0.58	0.00
23.20	232.50	2.00	0.00	0.58	0.00	23.30	242.96	2.00	0.00	0.58	0.00
23.40	251.28	2.00	0.00	0.57	0.00	23.50	255.94	2.00	0.00	0.57	0.00
23.60	255.76	2.00	0.00	0.57	0.00	23.70	250.43	2.00	0.00	0.57	0.00
23.80	241.10	2.00	0.00	0.57	0.00	23.90	230.76	2.00	0.00	0.57	0.00
24.00	214.38	2.00	0.00	0.56	0.00	24.10	197.71	0.91	0.32	0.56	0.00
24.20	184.07	0.75	0.47	0.56	0.01	24.30	180.75	0.72	0.59	0.56	0.01
24.40	180.37	0.71	0.59	0.56	0.01	24.50	174.11	2.00	0.00	0.55	0.00
24.60	163.11	2.00	0.00	0.55	0.00	24.70	155.70	2.00	0.00	0.55	0.00
24.80	157.06	2.00	0.00	0.55	0.00	24.90	167.00	2.00	0.00	0.55	0.00
25.00	217.76	2.00	0.00	0.55	0.00	25.10	275.57	2.00	0.00	0.54	0.00
25.20	337.76	2.00	0.00	0.54	0.00	25.30	409.65	2.00	0.00	0.54	0.00
25.40	423.48	2.00	0.00	0.54	0.00	25.50	283.09	2.00	0.00	0.54	0.00
25.60	166.06	2.00	0.00	0.53	0.00	25.70	146.49	2.00	0.00	0.53	0.00
25.80	138.03	2.00	0.00	0.53	0.00	25.90	137.77	2.00	0.00	0.53	0.00
26.00	140.10	0.38	0.93	0.53	0.01	26.10	143.93	0.40	0.91	0.53	0.01
26.20	146.64	0.42	0.89	0.52	0.01	26.30	146.57	0.42	0.89	0.52	0.01
26.40	144.09	0.40	0.90	0.52	0.01	26.50	142.74	0.40	0.90	0.52	0.01
26.60	142.91	0.40	0.90	0.52	0.01	26.70	144.55	0.41	0.89	0.51	0.01
26.80	146.75	0.42	0.87	0.51	0.01	26.90	148.83	0.44	0.86	0.51	0.01
27.00	150.56	0.45	0.85	0.51	0.01	27.10	151.74	0.46	0.84	0.51	0.01
27.20	153.24	0.47	0.83	0.51	0.01	27.30	155.76	0.49	0.82	0.50	0.01
27.40	160.19	0.52	0.80	0.50	0.01	27.50	164.74	0.56	0.74	0.50	0.01
27.60	167.22	0.58	0.72	0.50	0.01	27.70	167.55	0.58	0.71	0.50	0.01
27.80	168.34	0.59	0.71	0.49	0.01	27.90	169.46	0.60	0.70	0.49	0.01

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
28.00	166.81	0.58	0.71	0.49	0.01	28.10	159.62	0.52	0.78	0.49	0.01
28.20	152.02	0.46	0.81	0.49	0.01	28.30	147.84	0.43	0.82	0.49	0.01
28.40	145.31	0.41	0.83	0.48	0.01	28.50	140.20	0.38	0.85	0.48	0.01
28.60	137.82	2.00	0.00	0.48	0.00	28.70	139.59	2.00	0.00	0.48	0.00
28.80	147.46	2.00	0.00	0.48	0.00	28.90	156.21	2.00	0.00	0.47	0.00
29.00	177.37	2.00	0.00	0.47	0.00	29.10	243.07	2.00	0.00	0.47	0.00
29.20	303.64	2.00	0.00	0.47	0.00	29.30	161.27	2.00	0.00	0.47	0.00
29.40	162.34	2.00	0.00	0.47	0.00	29.50	164.37	1.63	0.00	0.46	0.00
29.60	163.10	1.62	0.00	0.46	0.00	29.70	157.22	1.52	0.00	0.46	0.00
29.80	152.48	1.39	0.00	0.46	0.00	29.90	154.62	1.33	0.00	0.46	0.00
30.00	172.81	1.51	0.00	0.45	0.00	30.10	189.28	1.80	0.00	0.45	0.00
30.20	197.31	2.00	0.00	0.45	0.00	30.30	199.76	2.00	0.00	0.45	0.00
30.40	203.30	2.00	0.00	0.45	0.00	30.50	210.68	2.00	0.00	0.45	0.00
30.60	432.78	2.00	0.00	0.44	0.00	30.70	275.43	2.00	0.00	0.44	0.00
30.80	175.99	2.00	0.00	0.44	0.00	30.90	159.10	2.00	0.00	0.44	0.00
31.00	152.10	2.00	0.00	0.44	0.00	31.10	153.84	2.00	0.00	0.43	0.00
31.20	160.36	2.00	0.00	0.43	0.00	31.30	169.30	0.60	0.61	0.43	0.01
31.40	176.48	0.66	0.47	0.43	0.01	31.50	179.13	0.69	0.46	0.43	0.01
31.60	178.20	0.68	0.46	0.43	0.01	31.70	175.44	0.65	0.47	0.42	0.01
31.80	168.77	0.59	0.60	0.42	0.01	31.90	157.38	0.50	0.68	0.42	0.01
32.00	146.00	0.41	0.72	0.42	0.01	32.10	142.83	0.39	0.73	0.42	0.01
32.20	149.84	0.44	0.70	0.41	0.01	32.30	158.28	0.50	0.66	0.41	0.01
32.40	162.57	0.54	0.64	0.41	0.01	32.50	162.74	0.54	0.64	0.41	0.01
32.60	161.56	0.53	0.64	0.41	0.01	32.70	161.25	0.53	0.64	0.41	0.01
32.80	161.04	0.53	0.64	0.40	0.01	32.90	162.86	0.54	0.63	0.40	0.01
33.00	162.91	0.54	0.63	0.40	0.01	33.10	158.61	0.51	0.64	0.40	0.01
33.20	150.52	0.45	0.66	0.40	0.01	33.30	141.68	0.39	0.69	0.39	0.01
33.40	138.12	0.37	0.70	0.39	0.01	33.50	139.16	0.37	0.70	0.39	0.01
33.60	144.33	0.40	0.67	0.39	0.01	33.70	153.47	0.47	0.64	0.39	0.01
33.80	163.95	0.55	0.57	0.39	0.01	33.90	172.07	0.62	0.53	0.38	0.01
34.00	177.04	0.67	0.42	0.38	0.01	34.10	178.45	0.69	0.41	0.38	0.00
34.20	177.73	0.68	0.41	0.38	0.00	34.30	177.83	0.68	0.41	0.38	0.00
34.40	182.67	0.73	0.39	0.37	0.00	34.50	189.67	0.81	0.30	0.37	0.00
34.60	195.71	0.88	0.22	0.37	0.00	34.70	199.20	0.92	0.21	0.37	0.00
34.80	202.79	2.00	0.00	0.37	0.00	34.90	206.34	2.00	0.00	0.37	0.00
35.00	208.83	2.00	0.00	0.36	0.00	35.10	209.65	2.00	0.00	0.36	0.00
35.20	208.69	2.00	0.00	0.36	0.00	35.30	205.79	2.00	0.00	0.36	0.00
35.40	201.11	2.00	0.00	0.36	0.00	35.50	195.01	0.87	0.21	0.35	0.00
35.60	188.06	0.79	0.29	0.35	0.00	35.70	181.47	0.72	0.37	0.35	0.00
35.80	175.85	0.67	0.39	0.35	0.00	35.90	170.58	0.62	0.49	0.35	0.01
36.00	164.34	0.56	0.51	0.35	0.01	36.10	156.95	0.50	0.55	0.34	0.01
36.20	150.54	0.45	0.57	0.34	0.01	36.30	146.45	0.42	0.58	0.34	0.01
36.40	144.64	0.41	0.58	0.34	0.01	36.50	144.26	0.41	0.58	0.34	0.01
36.60	145.14	0.42	0.58	0.33	0.01	36.70	147.82	0.43	0.56	0.33	0.01
36.80	152.46	0.47	0.55	0.33	0.01	36.90	158.76	0.52	0.53	0.33	0.01
37.00	165.06	0.57	0.48	0.33	0.01	37.10	170.24	0.62	0.46	0.33	0.01
37.20	173.64	0.65	0.44	0.32	0.01	37.30	175.04	0.66	0.36	0.32	0.00
37.40	174.63	0.66	0.36	0.32	0.00	37.50	172.74	0.64	0.44	0.32	0.01

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
37.60	170.61	0.62	0.44	0.32	0.01	37.70	168.64	0.60	0.45	0.31	0.01
37.80	166.75	0.59	0.45	0.31	0.01	37.90	165.34	0.57	0.46	0.31	0.01
38.00	164.82	0.57	0.45	0.31	0.01	38.10	165.07	0.57	0.45	0.31	0.01
38.20	165.36	0.58	0.45	0.31	0.01	38.30	165.43	0.58	0.44	0.30	0.01
38.40	164.72	0.57	0.44	0.30	0.01	38.50	162.83	0.55	0.45	0.30	0.01
38.60	160.06	0.53	0.47	0.30	0.01	38.70	157.36	0.51	0.48	0.30	0.01
38.80	155.01	0.49	0.48	0.29	0.01	38.90	152.87	0.48	0.48	0.29	0.01
39.00	151.20	0.46	0.48	0.29	0.01	39.10	150.60	0.46	0.48	0.29	0.01
39.20	151.00	0.46	0.48	0.29	0.01	39.30	151.41	0.47	0.47	0.29	0.01
39.40	151.51	0.47	0.47	0.28	0.01	39.50	151.30	0.47	0.47	0.28	0.01
39.60	150.55	0.46	0.47	0.28	0.01	39.70	150.71	0.46	0.46	0.28	0.01
39.80	151.87	0.47	0.46	0.28	0.01	39.90	153.97	0.49	0.45	0.27	0.01
40.00	154.83	0.49	0.45	0.27	0.01	40.10	155.31	0.50	0.44	0.27	0.01
40.20	156.78	0.51	0.43	0.27	0.01	40.30	159.73	0.53	0.43	0.27	0.01
40.40	162.91	0.56	0.40	0.27	0.00	40.50	165.46	0.58	0.39	0.26	0.00
40.60	167.39	0.60	0.38	0.26	0.00	40.70	168.92	0.62	0.37	0.26	0.00
40.80	170.18	0.63	0.36	0.26	0.00	40.90	171.30	0.64	0.36	0.26	0.00
41.00	172.48	0.65	0.29	0.25	0.00	41.10	173.82	0.67	0.28	0.25	0.00
41.20	175.39	0.68	0.28	0.25	0.00	41.30	177.32	0.70	0.27	0.25	0.00
41.40	179.01	0.72	0.27	0.25	0.00	41.50	180.06	0.73	0.26	0.25	0.00
41.60	180.34	0.74	0.26	0.24	0.00	41.70	180.50	0.74	0.26	0.24	0.00
41.80	181.54	0.75	0.20	0.24	0.00	41.90	183.70	0.77	0.20	0.24	0.00
42.00	186.79	0.81	0.19	0.24	0.00	42.10	190.20	0.85	0.14	0.23	0.00
42.20	193.36	0.89	0.14	0.23	0.00	42.30	195.75	0.92	0.13	0.23	0.00
42.40	196.88	0.94	0.13	0.23	0.00	42.50	196.42	0.93	0.13	0.23	0.00
42.60	194.35	0.91	0.13	0.23	0.00	42.70	191.08	0.87	0.13	0.22	0.00
42.80	187.01	0.82	0.18	0.22	0.00	42.90	182.77	0.77	0.19	0.22	0.00
43.00	179.57	0.74	0.23	0.22	0.00	43.10	178.70	0.73	0.23	0.22	0.00
43.20	181.14	0.76	0.18	0.21	0.00	43.30	186.81	0.82	0.17	0.21	0.00
43.40	194.55	0.92	0.12	0.21	0.00	43.50	203.06	2.00	0.00	0.21	0.00
43.60	211.34	2.00	0.00	0.21	0.00	43.70	219.09	2.00	0.00	0.21	0.00
43.80	226.01	2.00	0.00	0.20	0.00	43.90	232.53	2.00	0.00	0.20	0.00
44.00	238.11	2.00	0.00	0.20	0.00	44.10	241.03	2.00	0.00	0.20	0.00
44.20	238.83	2.00	0.00	0.20	0.00	44.30	229.18	2.00	0.00	0.19	0.00
44.40	220.87	2.00	0.00	0.19	0.00	44.50	220.75	2.00	0.00	0.19	0.00
44.60	218.92	2.00	0.00	0.19	0.00	44.70	222.23	2.00	0.00	0.19	0.00
44.80	219.18	2.00	0.00	0.19	0.00	44.90	223.84	2.00	0.00	0.18	0.00
45.00	228.94	2.00	0.00	0.18	0.00	45.10	233.00	2.00	0.00	0.18	0.00
45.20	235.82	2.00	0.00	0.18	0.00	45.30	236.72	2.00	0.00	0.18	0.00
45.40	235.62	2.00	0.00	0.17	0.00	45.50	233.66	2.00	0.00	0.17	0.00
45.60	232.13	2.00	0.00	0.17	0.00	45.70	231.06	2.00	0.00	0.17	0.00
45.80	229.50	2.00	0.00	0.17	0.00	45.90	226.55	2.00	0.00	0.17	0.00
46.00	221.94	2.00	0.00	0.16	0.00	46.10	215.60	2.00	0.00	0.16	0.00
46.20	208.21	2.00	0.00	0.16	0.00	46.30	200.90	2.00	0.00	0.16	0.00
46.40	193.71	0.93	0.09	0.16	0.00	46.50	185.59	0.83	0.13	0.15	0.00
46.60	174.12	0.71	0.17	0.15	0.00	46.70	169.18	2.00	0.00	0.15	0.00
46.80	161.00	2.00	0.00	0.15	0.00	46.90	141.79	2.00	0.00	0.15	0.00
47.00	132.00	2.00	0.00	0.15	0.00	47.10	142.18	2.00	0.00	0.14	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
47.20	165.64	2.00	0.00	0.14	0.00	47.30	176.86	2.00	0.00	0.14	0.00
47.40	194.52	2.00	0.00	0.14	0.00	47.50	187.25	2.00	0.00	0.14	0.00
47.60	175.23	2.00	0.00	0.13	0.00	47.70	168.52	0.66	0.16	0.13	0.00
47.80	168.66	0.66	0.15	0.13	0.00	47.90	169.66	0.67	0.15	0.13	0.00
48.00	164.20	2.00	0.00	0.13	0.00	48.10	151.48	2.00	0.00	0.13	0.00
48.20	136.95	2.00	0.00	0.12	0.00	48.30	125.94	2.00	0.00	0.12	0.00
48.40	119.72	2.00	0.00	0.12	0.00	48.50	114.96	2.00	0.00	0.12	0.00
48.60	109.95	2.00	0.00	0.12	0.00	48.70	106.49	2.00	0.00	0.11	0.00
48.80	109.45	2.00	0.00	0.11	0.00	48.90	121.83	2.00	0.00	0.11	0.00
49.00	172.46	2.00	0.00	0.11	0.00	49.10	146.38	2.00	0.00	0.11	0.00
49.20	146.17	2.00	0.00	0.11	0.00	49.30	138.98	2.00	0.00	0.10	0.00
49.40	128.62	2.00	0.00	0.10	0.00	49.50	118.11	0.80	0.05	0.10	0.00
49.60	110.93	0.73	0.05	0.10	0.00	49.70	112.92	0.81	0.05	0.10	0.00
49.80	123.05	1.02	0.00	0.09	0.00	49.90	132.08	1.23	0.00	0.09	0.00

Total estimated settlement: 1.16**Abbreviations**

$Q_{tn,cs}$:	Equivalent clean sand normalized cone resistance
FS:	Factor of safety against liquefaction
e_v (%):	Post-liquefaction volumetric strain
DF:	e_v depth weighting factor
Settlement:	Calculated settlement

:: Strength loss calculation (Robertson (2009)) ::

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.10	63.32	119.66	1.30	156.12	2.00	0.84	0.84
0.20	64.12	121.18	1.29	156.29	1.98	0.84	0.84
0.30	63.59	120.15	1.30	155.76	1.99	0.83	0.83
0.40	60.41	114.13	1.36	155.54	2.06	0.83	0.83
0.50	57.19	108.04	1.47	158.82	2.13	0.84	0.84
0.60	56.53	106.77	1.59	169.97	2.19	0.85	0.85
0.70	59.04	111.51	1.68	187.49	2.23	0.87	0.87
0.80	62.44	117.93	1.73	203.76	2.24	0.89	0.89
0.90	64.67	122.13	1.75	213.48	2.25	0.90	0.90
1.00	65.58	123.84	1.76	217.84	2.25	0.91	0.91
1.10	64.59	121.95	1.78	217.35	2.26	0.90	0.90
1.20	61.76	116.59	1.82	212.53	2.27	0.90	0.90
1.30	57.24	108.04	1.88	202.58	2.29	0.89	0.89
1.40	54.57	102.99	1.89	194.84	2.29	0.88	0.88
1.50	54.99	103.76	1.87	193.76	2.28	0.88	0.88
1.60	57.17	107.88	1.84	198.15	2.28	0.88	0.88
1.70	59.72	112.67	1.82	204.57	2.27	0.89	0.89
1.80	60.59	114.32	1.83	208.96	2.27	0.90	0.90
1.90	57.91	109.24	1.91	208.12	2.29	0.90	0.90
2.00	52.69	99.36	2.06	204.26	2.33	0.89	0.89
2.10	46.70	88.02	2.27	200.15	2.38	0.89	0.89
2.20	42.14	79.39	2.48	196.72	2.42	0.88	0.88
2.30	37.73	71.05	2.69	190.95	2.46	0.88	0.88
2.40	33.71	63.44	2.89	183.12	2.49	0.87	0.87
2.50	31.80	59.81	2.96	177.04	2.50	0.86	0.86
2.60	32.09	60.34	2.89	174.10	2.49	0.86	0.86
2.70	33.43	62.88	2.75	172.91	2.47	0.86	0.86
2.80	34.49	64.86	2.62	170.11	2.44	0.85	0.85
2.90	34.00	63.92	2.56	163.33	2.43	0.84	0.84
3.00	33.22	62.43	2.48	154.72	2.42	0.83	0.83
3.10	32.49	61.04	2.42	147.49	2.41	0.82	0.82
3.20	33.17	62.33	2.36	147.00	2.40	0.82	0.82
3.30	34.74	65.27	2.33	152.13	2.39	0.83	0.83
3.40	37.04	69.63	2.32	161.38	2.39	0.84	0.84
3.50	39.15	73.59	2.34	172.41	2.39	0.86	0.86
3.60	40.29	75.74	2.44	184.64	2.41	0.87	0.87
3.70	40.26	75.67	2.62	198.15	2.44	0.88	0.88
3.80	40.09	75.33	2.82	212.41	2.48	0.90	0.90
3.90	40.64	76.35	2.96	226.23	2.50	0.91	0.91
4.00	42.32	79.52	2.99	237.41	2.50	0.91	0.91
4.10	44.34	83.32	2.92	243.30	2.49	0.93	0.93
4.20	45.37	85.27	2.88	245.18	2.48	0.93	0.93
4.30	44.83	84.24	2.92	246.11	2.49	0.93	0.93
4.40	42.77	80.33	3.09	248.37	2.52	0.94	0.94
4.50	39.56	74.26	3.35	249.12	2.55	0.97	0.97
4.60	35.62	66.78	3.66	244.66	2.59	1.01	1.01
4.70	31.43	58.86	3.99	234.70	2.63	1.03	1.03
4.80	28.05	52.45	4.24	222.61	2.65	1.05	1.05

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
4.90	25.36	47.36	4.43	209.85	2.67	1.05	1.05
5.00	23.37	43.60	4.52	197.05	2.68	1.05	1.05
5.10	21.74	40.51	4.54	184.02	2.68	1.03	1.03
5.20	20.76	38.63	4.50	173.86	2.68	1.01	1.01
5.30	20.78	38.66	4.40	170.17	2.67	1.00	1.00
5.40	22.02	41.00	4.20	172.14	2.65	0.98	0.98
5.50	24.13	44.97	3.89	175.14	2.62	0.95	0.95
5.60	26.02	48.54	3.61	175.19	2.58	0.92	0.92
5.70	26.65	49.72	3.46	172.24	2.57	0.90	0.90
5.80	25.84	48.17	3.52	169.63	2.57	0.91	0.91
5.90	23.01	42.81	3.90	167.03	2.62	0.94	0.94
6.00	19.12	35.45	4.63	164.01	2.69	1.01	1.01
6.10	16.32	30.15	5.35	161.34	2.76	0.84	0.84
6.20	15.54	28.66	5.50	157.72	2.77	0.84	0.84
6.30	15.65	28.86	5.29	152.63	2.75	0.83	0.83
6.40	14.57	26.81	5.39	144.51	2.76	0.82	0.82
6.50	12.62	23.10	5.96	137.59	2.81	0.81	0.81
6.60	10.88	19.81	6.80	134.72	2.87	0.81	0.81
6.70	9.87	17.90	7.51	134.34	2.92	0.80	0.80
6.80	9.47	17.12	7.84	134.24	2.94	0.80	0.80
6.90	9.06	16.34	8.17	133.47	2.96	0.80	0.80
7.00	8.72	15.69	8.57	134.43	2.99	0.81	0.81
7.10	9.04	16.28	8.60	140.05	2.99	0.81	0.81
7.20	10.62	19.26	7.72	148.60	2.93	0.83	0.83
7.30	13.04	23.82	6.44	153.29	2.85	0.83	0.83
7.40	14.73	27.01	5.56	150.18	2.78	0.83	0.83
7.50	14.76	27.04	5.31	143.64	2.75	0.82	0.82
7.60	13.33	24.34	5.71	138.90	2.79	0.81	0.81
7.70	11.94	21.70	6.41	139.00	2.84	0.81	0.81
7.80	11.27	20.42	6.83	139.42	2.87	0.81	0.81
7.90	10.87	19.65	6.93	136.20	2.88	0.81	0.81
8.00	10.28	18.52	7.00	129.68	2.89	0.80	0.80
8.10	9.38	16.81	7.28	122.43	2.91	0.79	0.79
8.20	8.40	14.96	7.78	116.38	2.94	0.78	0.78
8.30	7.35	12.95	8.58	111.11	2.99	0.77	0.77
8.40	6.58	11.50	9.35	107.50	3.03	0.49	0.89
8.50	6.25	10.85	9.79	106.28	3.06	0.49	0.84
8.60	6.30	10.95	9.85	107.81	3.06	0.51	0.84
8.70	6.35	11.03	9.95	109.72	3.07	0.53	0.84
8.80	6.29	10.90	10.09	109.93	3.07	0.54	0.83
8.90	6.27	10.85	9.94	107.84	3.06	0.51	0.82
9.00	6.29	10.88	9.53	103.70	3.04	0.47	0.82
9.10	6.09	10.50	9.41	98.73	3.04	0.42	0.79
9.20	5.58	9.52	9.88	94.03	3.06	0.36	0.71
9.30	5.10	8.61	10.68	91.95	3.10	0.31	0.64
9.40	5.13	8.64	10.93	94.52	3.12	0.34	0.64
9.50	5.52	9.39	10.52	98.73	3.10	0.41	0.70
9.60	5.90	10.09	9.95	100.37	3.07	0.43	0.74

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.70	7.76	13.59	7.75	105.29	2.94	0.76	0.76
9.80	11.21	19.82	6.06	120.15	2.82	0.78	0.78
9.90	12.34	21.72	5.85	127.08	2.80	0.79	0.79
10.00	10.19	18.04	6.89	124.23	2.88	0.79	0.79
10.10	6.46	11.09	9.52	105.62	3.04	0.32	0.80
10.20	5.25	8.79	10.64	93.57	3.10	0.31	0.63
10.30	5.64	9.53	10.20	97.26	3.08	0.38	0.68
10.40	5.93	10.04	10.18	102.21	3.08	0.42	0.72
10.50	5.98	10.09	10.45	105.41	3.09	0.45	0.72
10.60	5.98	10.04	10.73	107.70	3.11	0.46	0.72
10.70	5.98	9.99	10.98	109.69	3.12	0.48	0.71
10.80	5.98	9.94	11.21	111.47	3.13	0.50	0.71
10.90	5.98	9.89	11.31	111.87	3.13	0.51	0.71
11.00	5.98	9.84	11.27	110.87	3.13	0.49	0.70
11.10	6.00	9.83	11.29	111.03	3.13	0.47	0.70
11.20	6.41	10.54	11.16	117.58	3.13	0.51	0.75
11.30	7.76	12.95	10.15	131.45	3.08	0.70	0.93
11.40	9.54	16.09	8.77	141.14	3.00	0.81	0.81
11.50	10.92	18.41	7.68	141.33	2.93	0.81	0.81
11.60	11.17	18.63	7.17	133.57	2.90	0.80	0.80
11.70	10.34	17.15	7.38	126.54	2.91	0.79	0.79
11.80	9.11	15.02	8.30	124.65	2.97	0.79	0.79
11.90	8.03	13.03	9.80	127.66	3.06	0.66	0.93
12.00	8.26	13.38	10.37	138.78	3.09	0.76	0.96
12.10	9.89	16.18	9.46	153.07	3.04	1.05	1.16
12.20	12.14	20.03	7.95	159.25	2.95	0.84	0.84
12.30	13.79	22.39	6.72	150.55	2.87	0.83	0.83
12.40	14.39	22.93	5.78	132.52	2.79	0.80	0.80
12.50	14.67	23.00	5.11	117.45	2.74	0.78	0.78
12.60	15.66	24.33	4.74	115.42	2.70	0.78	0.78
12.70	16.72	25.94	4.75	123.21	2.70	0.79	0.79
12.80	17.02	26.50	5.06	133.95	2.73	0.80	0.80
12.90	15.54	24.33	5.80	141.15	2.80	0.81	0.81
13.00	13.13	20.65	6.91	142.74	2.88	0.82	0.82
13.10	10.98	17.23	8.04	138.59	2.96	0.81	0.81
13.20	9.80	15.17	8.61	130.62	2.99	0.80	0.80
13.30	9.73	14.98	8.29	124.20	2.97	0.79	0.79
13.40	10.47	16.08	7.59	122.03	2.93	0.79	0.79
13.50	11.58	17.71	7.03	124.47	2.89	0.79	0.79
13.60	12.48	19.03	6.78	129.09	2.87	0.80	0.80
13.70	12.75	19.41	6.88	133.53	2.88	0.80	0.80
13.80	12.33	18.74	7.22	135.37	2.90	0.81	0.81
13.90	11.80	17.85	7.47	133.41	2.92	0.80	0.80
14.00	11.32	17.01	7.49	127.31	2.92	0.79	0.79
14.10	11.16	16.61	7.22	119.87	2.90	0.78	0.78
14.20	11.16	16.49	6.95	114.51	2.88	0.77	0.77
14.30	11.46	16.86	6.79	114.46	2.87	0.77	0.77
14.40	12.08	17.76	6.78	120.36	2.87	0.78	0.78

:: Strength loss calculation (Robertson (2009)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
14.50	13.00	19.14	6.77	129.64	2.87	0.80	0.80
14.60	13.94	20.52	6.76	138.64	2.87	0.81	0.81
14.70	14.88	21.86	6.64	145.18	2.86	0.82	0.82
14.80	15.29	22.38	6.62	148.08	2.86	0.82	0.82
14.90	14.81	21.62	6.83	147.59	2.87	0.82	0.82
15.00	13.79	20.07	7.26	145.73	2.90	0.82	0.82
15.10	12.99	18.84	7.67	144.60	2.93	0.82	0.82
15.20	12.91	18.67	7.80	145.60	2.94	0.82	0.82
15.30	13.60	19.60	7.60	148.96	2.93	0.83	0.83
15.40	14.65	21.04	7.28	153.13	2.91	0.83	0.83
15.50	14.88	21.29	7.25	154.28	2.90	0.83	0.83
15.60	14.72	20.99	7.35	154.30	2.91	0.83	0.83
15.70	14.79	21.00	7.36	154.60	2.91	0.83	0.83
15.80	15.44	21.83	7.15	156.19	2.90	0.84	0.84
15.90	15.62	22.01	7.14	157.05	2.90	0.84	0.84
16.00	15.50	21.77	7.29	158.82	2.91	0.84	0.84
16.10	17.19	24.08	6.89	165.86	2.88	0.85	0.85
16.20	21.05	29.29	5.91	173.16	2.80	0.86	0.86
16.30	24.86	34.27	5.09	174.43	2.74	0.86	0.86
16.40	26.05	35.63	4.73	168.71	2.70	0.85	0.85
16.50	23.46	31.96	4.99	159.48	2.73	0.84	0.84
16.60	18.42	25.05	5.93	148.44	2.81	0.82	0.82
16.70	12.98	17.53	7.67	134.33	2.93	0.80	0.80
16.80	8.92	11.56	9.96	115.18	3.07	0.51	0.83
16.90	6.90	8.60	11.37	97.81	3.14	0.34	0.61
17.00	6.16	7.49	11.46	85.89	3.14	0.25	0.54
17.10	5.97	7.20	10.94	78.82	3.12	0.21	0.51
17.20	5.97	7.18	10.43	74.86	3.09	0.19	0.51
17.30	5.79	6.88	10.43	71.77	3.09	0.18	0.49
17.40	5.81	6.88	10.36	71.28	3.09	0.15	0.49
17.50	6.26	7.51	10.23	76.80	3.08	0.18	0.54
17.60	7.24	8.87	9.88	87.63	3.06	0.29	0.63
17.70	8.07	10.01	9.77	97.83	3.06	0.40	0.72
17.80	8.41	10.45	9.91	103.65	3.06	0.45	0.75
17.90	8.42	10.43	10.17	106.06	3.08	0.45	0.74
18.00	8.37	10.31	10.47	107.95	3.09	0.46	0.74
18.10	8.17	9.99	11.14	111.30	3.13	0.50	0.71
18.20	8.13	9.90	11.87	117.52	3.16	0.53	0.71
18.30	8.94	10.98	11.75	129.03	3.16	0.63	0.78
18.40	10.90	13.66	10.45	142.71	3.09	0.89	0.98
18.50	13.00	16.49	9.14	150.66	3.02	1.10	1.18
18.60	14.19	18.06	8.30	149.99	2.97	0.83	0.83
18.70	15.48	19.74	7.47	147.34	2.92	0.82	0.82
18.80	16.63	21.12	6.98	147.37	2.88	0.82	0.82
18.90	16.88	21.38	6.99	149.51	2.89	0.83	0.83
19.00	15.17	19.11	7.76	148.27	2.94	0.82	0.82
19.10	12.50	15.42	9.16	141.32	3.02	0.90	1.10
19.20	10.65	12.88	10.33	133.05	3.09	0.71	0.92

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
19.30	10.32	12.38	10.41	128.88	3.09	0.65	0.88
19.40	11.45	13.84	9.48	131.31	3.04	0.74	0.99
19.50	13.39	16.38	8.27	135.51	2.97	0.81	0.81
19.60	15.68	19.27	7.07	136.32	2.89	0.81	0.81
19.70	17.74	21.71	6.07	131.71	2.82	0.80	0.80
19.80	19.36	23.60	5.51	130.07	2.77	0.80	0.80
19.90	18.84	22.91	5.76	132.05	2.79	0.80	0.80
20.00	16.51	19.98	6.59	131.72	2.86	0.80	0.80
20.10	13.94	16.72	7.53	125.84	2.92	0.79	0.79
20.20	12.46	14.72	7.90	116.35	2.95	0.78	0.78
20.30	12.39	14.58	7.86	114.59	2.94	0.77	0.77
20.40	12.55	14.74	7.90	116.39	2.95	0.78	0.78
20.50	13.23	15.56	7.65	119.00	2.93	0.78	0.78
20.60	14.29	16.83	7.20	121.13	2.90	0.78	0.78
20.70	15.22	17.91	6.96	124.61	2.88	0.79	0.79
20.80	16.35	19.28	6.93	133.55	2.88	0.80	0.80
20.90	18.79	22.28	6.77	150.76	2.87	0.83	0.83
21.00	23.85	28.40	6.07	172.52	2.82	0.86	0.86
21.10	30.27	36.02	5.17	186.26	2.74	0.87	0.87
21.20	36.95	43.70	4.23	184.94	2.65	1.00	1.00
21.30	42.73	50.01	3.32	166.14	2.55	0.88	0.88
21.40	47.27	54.66	2.59	141.74	2.44	0.82	0.82
21.50	49.21	56.33	2.18	122.62	2.36	0.79	0.79
21.60	48.10	54.78	2.11	115.61	2.35	0.78	0.78
21.70	45.14	51.43	2.35	120.95	2.40	0.78	0.78
21.80	42.84	48.96	2.80	136.86	2.47	0.81	0.81
21.90	45.62	52.21	2.98	155.52	2.50	0.82	0.82
22.00	55.53	63.30	2.60	164.44	2.44	0.85	0.85
22.10	70.39	79.47	2.02	160.56	2.32	0.84	0.84
22.20	86.19	96.17	1.61	154.39	2.20	0.83	0.83
22.30	98.36	108.57	1.41	152.73	2.09	0.83	0.83
22.40	107.08	117.31	1.33	156.28	2.03	0.84	0.84
22.50	115.37	125.86	1.31	164.41	2.00	0.85	0.85
22.60	122.02	132.79	1.30	172.90	1.99	0.86	0.86
22.70	126.84	137.78	1.30	179.79	2.00	0.86	0.86
22.80	129.17	140.06	1.31	183.60	2.00	0.87	0.87
22.90	136.06	147.16	1.31	192.22	2.00	0.88	0.88
23.00	147.42	158.93	1.29	205.52	1.98	0.89	0.89
23.10	160.45	172.36	1.28	220.33	1.96	0.91	0.91
23.20	171.23	183.35	1.27	232.50	1.95	0.92	0.92
23.30	180.27	192.47	1.26	242.96	1.94	0.93	0.93
23.40	187.37	199.53	1.26	251.28	1.93	0.94	0.94
23.50	191.52	203.42	1.26	255.94	1.93	0.94	0.94
23.60	191.73	203.15	1.26	255.76	1.93	0.94	0.94
23.70	187.36	198.09	1.26	250.43	1.94	0.94	0.94
23.80	178.72	188.68	1.28	241.10	1.96	0.93	0.93
23.90	166.77	176.03	1.31	230.76	2.00	0.92	0.92
24.00	149.50	157.77	1.36	214.38	2.05	0.90	0.90

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
24.10	133.96	141.16	1.40	197.71	2.09	0.88	0.88
24.20	126.47	132.75	1.39	184.07	2.08	0.87	0.87
24.30	128.47	134.23	1.35	180.75	2.04	0.87	0.87
24.40	130.78	136.14	1.32	180.37	2.02	0.86	0.86
24.50	124.66	129.53	1.34	174.11	2.04	0.86	0.86
24.60	110.33	114.62	1.42	163.11	2.10	0.84	0.84
24.70	91.14	94.77	1.64	155.70	2.21	0.83	0.83
24.80	72.12	75.03	2.09	157.06	2.34	0.84	0.84
24.90	57.73	60.01	2.78	167.00	2.47	0.85	0.85
25.00	49.70	51.55	3.44	177.19	2.56	0.91	0.91
25.10	47.44	49.10	3.80	186.68	2.61	0.96	0.96
25.20	45.12	46.57	4.17	194.07	2.65	1.01	1.01
25.30	42.32	43.53	4.58	199.18	2.69	1.05	1.05
25.40	41.45	42.49	4.67	198.44	2.70	1.06	1.06
25.50	47.50	48.57	3.85	187.17	2.61	0.96	0.96
25.60	58.52	59.61	2.79	166.06	2.47	0.85	0.85
25.70	69.31	70.27	2.08	146.49	2.34	0.82	0.82
25.80	77.97	78.74	1.75	138.03	2.25	0.81	0.81
25.90	83.74	84.31	1.63	137.77	2.21	0.81	0.81
26.00	87.01	87.39	1.60	140.10	2.20	0.81	0.81
26.10	87.64	87.86	1.64	143.93	2.21	0.82	0.82
26.20	89.33	89.36	1.64	146.64	2.21	0.82	0.82
26.30	93.87	93.64	1.57	146.57	2.18	0.82	0.82
26.40	98.42	97.85	1.47	144.09	2.13	0.82	0.82
26.50	100.49	99.62	1.43	142.74	2.11	0.82	0.82
26.60	99.58	98.50	1.45	142.91	2.12	0.82	0.82
26.70	99.14	97.88	1.48	144.55	2.14	0.82	0.82
26.80	99.48	98.02	1.50	146.75	2.15	0.82	0.82
26.90	100.62	98.93	1.50	148.83	2.15	0.83	0.83
27.00	102.38	100.44	1.50	150.56	2.15	0.83	0.83
27.10	104.07	101.85	1.49	151.74	2.14	0.83	0.83
27.20	105.35	102.88	1.49	153.24	2.14	0.83	0.83
27.30	105.96	103.26	1.51	155.76	2.15	0.83	0.83
27.40	106.62	103.70	1.54	160.19	2.17	0.84	0.84
27.50	107.61	104.45	1.58	164.74	2.18	0.85	0.85
27.60	109.14	105.71	1.58	167.22	2.19	0.85	0.85
27.70	111.42	107.65	1.56	167.55	2.18	0.85	0.85
27.80	114.37	110.25	1.53	168.34	2.16	0.85	0.85
27.90	117.17	112.69	1.50	169.46	2.15	0.85	0.85
28.00	117.25	112.47	1.48	166.81	2.14	0.85	0.85
28.10	113.03	108.10	1.48	159.62	2.14	0.84	0.84
28.20	104.54	99.66	1.53	152.02	2.16	0.83	0.83
28.30	96.33	91.54	1.62	147.84	2.20	0.82	0.82
28.40	89.43	84.70	1.72	145.31	2.24	0.82	0.82
28.50	84.52	79.78	1.76	140.20	2.25	0.81	0.81
28.60	79.72	74.99	1.84	137.82	2.28	0.81	0.81
28.70	74.73	70.04	1.99	139.59	2.32	0.81	0.81
28.80	69.75	65.14	2.26	147.46	2.38	0.82	0.82

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
28.90	62.88	58.43	2.67	156.21	2.45	0.84	0.84
29.00	55.17	50.94	3.21	163.60	2.53	0.86	0.86
29.10	47.60	43.63	3.79	165.44	2.60	0.93	0.93
29.20	41.43	37.66	4.33	163.01	2.66	0.98	0.98
29.30	37.19	33.54	4.81	161.27	2.71	0.84	0.84
29.40	34.70	31.10	5.22	162.34	2.75	0.84	0.84
29.50	34.06	30.41	5.41	164.37	2.76	0.85	0.85
29.60	33.91	30.18	5.40	163.10	2.76	0.84	0.84
29.70	32.03	28.33	5.55	157.22	2.78	0.84	0.84
29.80	29.66	26.04	5.86	152.48	2.80	0.83	0.83
29.90	28.43	24.82	6.23	154.62	2.83	0.83	0.83
30.00	32.28	28.32	6.10	172.81	2.82	0.86	0.86
30.10	38.09	33.62	5.63	189.28	2.78	0.88	0.88
30.20	43.19	38.24	5.16	197.31	2.74	0.88	0.88
30.30	44.63	39.45	5.06	199.76	2.73	0.89	0.89
30.40	44.36	39.09	5.20	203.30	2.75	0.89	0.89
30.50	46.20	40.66	5.18	210.68	2.74	0.90	0.90
30.60	51.44	45.36	4.60	208.57	2.69	1.07	1.07
30.70	59.73	52.86	3.70	195.73	2.59	0.96	0.96
30.80	69.61	61.82	2.85	175.99	2.48	0.86	0.86
30.90	81.48	72.59	2.19	159.10	2.36	0.84	0.84
31.00	94.67	84.56	1.80	152.10	2.26	0.83	0.83
31.10	106.82	95.53	1.61	153.84	2.20	0.83	0.83
31.20	116.62	104.28	1.54	160.36	2.17	0.84	0.84
31.30	124.76	111.44	1.52	169.30	2.16	0.85	0.85
31.40	130.68	116.55	1.51	176.48	2.16	0.86	0.86
31.50	133.94	119.25	1.50	179.13	2.15	0.86	0.86
31.60	134.30	119.31	1.49	178.20	2.14	0.86	0.86
31.70	132.00	116.97	1.50	175.44	2.15	0.86	0.86
31.80	124.86	110.25	1.53	168.77	2.16	0.85	0.85
31.90	112.69	99.05	1.59	157.38	2.19	0.84	0.84
32.00	97.91	85.54	1.71	146.00	2.23	0.82	0.82
32.10	85.37	74.05	1.93	142.83	2.30	0.82	0.82
32.20	78.62	67.76	2.21	149.84	2.37	0.83	0.83
32.30	78.07	67.05	2.36	158.28	2.40	0.84	0.84
32.40	82.35	70.67	2.30	162.57	2.39	0.84	0.84
32.50	89.96	77.28	2.11	162.74	2.34	0.84	0.84
32.60	100.87	86.85	1.86	161.56	2.28	0.84	0.84
32.70	114.12	98.53	1.64	161.25	2.21	0.84	0.84
32.80	125.97	109.00	1.48	161.04	2.14	0.84	0.84
32.90	133.61	115.67	1.41	162.86	2.09	0.84	0.84
33.00	136.56	118.12	1.38	162.91	2.07	0.84	0.84
33.10	135.19	116.76	1.36	158.61	2.05	0.84	0.84
33.20	129.92	111.98	1.34	150.52	2.04	0.83	0.83
33.30	122.33	105.12	1.35	141.68	2.04	0.82	0.82
33.40	115.41	98.69	1.40	138.12	2.09	0.81	0.81
33.50	111.66	95.06	1.46	139.16	2.13	0.81	0.81
33.60	111.68	94.74	1.52	144.33	2.16	0.82	0.82

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
33.70	116.59	98.70	1.55	153.47	2.17	0.83	0.83
33.80	126.41	106.98	1.53	163.95	2.16	0.85	0.85
33.90	138.32	117.17	1.47	172.07	2.13	0.86	0.86
34.00	149.33	126.67	1.40	177.04	2.09	0.86	0.86
34.10	156.01	132.42	1.35	178.45	2.04	0.86	0.86
34.20	158.07	134.09	1.33	177.73	2.02	0.86	0.86
34.30	158.80	134.48	1.32	177.83	2.02	0.86	0.86
34.40	162.94	137.73	1.33	182.67	2.02	0.87	0.87
34.50	169.31	142.88	1.33	189.67	2.02	0.88	0.88
34.60	175.37	147.80	1.32	195.71	2.02	0.88	0.88
34.70	179.32	150.90	1.32	199.20	2.01	0.89	0.89
34.80	184.04	154.72	1.31	202.79	2.00	0.89	0.89
34.90	189.55	159.27	1.30	206.34	1.99	0.89	0.89
35.00	194.31	163.22	1.28	208.83	1.96	0.90	0.90
35.10	196.77	165.14	1.27	209.65	1.95	0.90	0.90
35.20	196.37	164.51	1.27	208.69	1.95	0.90	0.90
35.30	193.58	161.78	1.27	205.79	1.95	0.89	0.89
35.40	189.34	157.88	1.27	201.11	1.96	0.89	0.89
35.50	184.20	153.28	1.27	195.01	1.95	0.88	0.88
35.60	178.51	148.27	1.27	188.06	1.95	0.87	0.87
35.70	173.44	143.85	1.26	181.47	1.94	0.87	0.87
35.80	169.68	140.61	1.25	175.85	1.92	0.86	0.86
35.90	166.88	138.27	1.23	170.58	1.90	0.85	0.85
36.00	163.35	135.35	1.21	164.34	1.87	0.85	0.85
36.10	158.25	131.07	1.20	156.95	1.85	0.84	0.84
36.20	152.33	125.91	1.20	150.54	1.84	0.83	0.83
36.30	147.13	121.22	1.21	146.45	1.86	0.82	0.82
36.40	143.89	118.12	1.22	144.64	1.88	0.82	0.82
36.50	142.53	116.63	1.24	144.26	1.90	0.82	0.82
36.60	143.00	116.75	1.24	145.14	1.91	0.82	0.82
36.70	145.61	118.68	1.25	147.82	1.91	0.82	0.82
36.80	150.56	122.60	1.24	152.46	1.91	0.83	0.83
36.90	157.66	128.36	1.24	158.76	1.90	0.84	0.84
37.00	165.31	134.63	1.23	165.06	1.88	0.85	0.85
37.10	172.32	140.40	1.21	170.24	1.87	0.85	0.85
37.20	177.10	144.25	1.20	173.64	1.85	0.86	0.86
37.30	178.87	145.48	1.20	175.04	1.85	0.86	0.86
37.40	177.96	144.39	1.21	174.63	1.86	0.86	0.86
37.50	175.45	141.98	1.22	172.74	1.87	0.86	0.86
37.60	172.65	139.32	1.22	170.61	1.88	0.85	0.85
37.70	169.90	136.69	1.23	168.64	1.90	0.85	0.85
37.80	167.26	134.14	1.24	166.75	1.91	0.85	0.85
37.90	165.19	132.09	1.25	165.34	1.92	0.85	0.85
38.00	164.02	130.76	1.26	164.82	1.94	0.85	0.85
38.10	163.69	130.12	1.27	165.07	1.95	0.85	0.85
38.20	163.69	129.81	1.27	165.36	1.96	0.85	0.85
38.30	163.49	129.34	1.28	165.43	1.96	0.85	0.85
38.40	162.37	128.10	1.29	164.72	1.97	0.85	0.85

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
38.50	159.91	125.77	1.29	162.83	1.98	0.84	0.84
38.60	156.57	122.75	1.30	160.06	2.00	0.84	0.84
38.70	153.20	119.72	1.31	157.36	2.01	0.84	0.84
38.80	150.08	116.88	1.33	155.01	2.02	0.83	0.83
38.90	147.28	114.34	1.34	152.87	2.03	0.83	0.83
39.00	145.42	112.61	1.34	151.20	2.04	0.83	0.83
39.10	145.19	112.25	1.34	150.60	2.04	0.83	0.83
39.20	146.51	113.17	1.33	151.00	2.03	0.83	0.83
39.30	148.08	114.32	1.32	151.41	2.02	0.83	0.83
39.40	149.40	115.30	1.31	151.51	2.01	0.83	0.83
39.50	150.23	115.88	1.31	151.30	2.00	0.83	0.83
39.60	150.45	115.97	1.30	150.55	1.99	0.83	0.83
39.70	151.53	116.74	1.29	150.71	1.98	0.83	0.83
39.80	153.36	118.05	1.29	151.87	1.97	0.83	0.83
39.90	155.09	119.10	1.29	153.97	1.98	0.83	0.83
40.00	154.86	118.49	1.31	154.83	2.00	0.83	0.83
40.10	154.63	117.96	1.32	155.31	2.01	0.83	0.83
40.20	156.64	119.36	1.31	156.78	2.01	0.84	0.84
40.30	160.77	122.51	1.30	159.73	2.00	0.84	0.84
40.40	165.07	125.78	1.30	162.91	1.99	0.84	0.84
40.50	168.83	128.65	1.29	165.46	1.97	0.85	0.85
40.60	172.09	131.16	1.28	167.39	1.96	0.85	0.85
40.70	175.00	133.42	1.27	168.92	1.94	0.85	0.85
40.80	177.41	135.24	1.26	170.18	1.93	0.85	0.85
40.90	179.23	136.52	1.25	171.30	1.93	0.85	0.85
41.00	180.47	137.19	1.26	172.48	1.93	0.86	0.86
41.10	181.45	137.57	1.26	173.82	1.94	0.86	0.86
41.20	182.77	138.22	1.27	175.39	1.95	0.86	0.86
41.30	184.68	139.37	1.27	177.32	1.95	0.86	0.86
41.40	186.86	140.83	1.27	179.01	1.95	0.86	0.86
41.50	189.12	142.53	1.26	180.06	1.94	0.86	0.86
41.60	190.91	143.95	1.25	180.34	1.92	0.86	0.86
41.70	192.03	144.73	1.25	180.50	1.92	0.87	0.87
41.80	192.92	145.05	1.25	181.54	1.92	0.87	0.87
41.90	194.40	145.67	1.26	183.70	1.94	0.87	0.87
42.00	197.14	147.32	1.27	186.79	1.95	0.87	0.87
42.10	200.61	149.60	1.27	190.20	1.95	0.88	0.88
42.20	203.97	151.83	1.27	193.36	1.96	0.88	0.88
42.30	206.60	153.50	1.28	195.75	1.96	0.88	0.88
42.40	208.12	154.40	1.28	196.88	1.96	0.88	0.88
42.50	208.30	154.35	1.27	196.42	1.95	0.88	0.88
42.60	206.70	152.96	1.27	194.35	1.95	0.88	0.88
42.70	203.68	150.46	1.27	191.08	1.95	0.88	0.88
42.80	199.57	147.12	1.27	187.01	1.95	0.87	0.87
42.90	194.71	143.07	1.28	182.77	1.96	0.87	0.87
43.00	190.18	139.13	1.29	179.57	1.98	0.86	0.86
43.10	187.86	136.81	1.31	178.70	2.00	0.86	0.86
43.20	190.13	138.14	1.31	181.14	2.00	0.87	0.87

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)'/σ'_v}	S _{u(peak)'/σ'_v}
43.30	197.38	143.46	1.30	186.81	1.99	0.87	0.87
43.40	207.80	151.34	1.29	194.55	1.97	0.88	0.88
43.50	219.34	160.16	1.27	203.06	1.95	0.89	0.89
43.60	230.48	168.65	1.25	211.34	1.92	0.90	0.90
43.70	240.76	176.40	1.24	219.09	1.91	0.91	0.91
43.80	249.82	183.13	1.23	226.01	1.90	0.91	0.91
43.90	258.68	189.73	1.23	232.53	1.88	0.92	0.92
44.00	267.99	196.97	1.21	238.11	1.86	0.92	0.92
44.10	276.85	204.25	1.18	241.03	1.83	0.93	0.93
44.20	284.85	211.29	1.13	238.83	1.78	0.93	0.93
44.30	291.10	217.20	1.06	229.18	1.73	0.92	0.92
44.40	294.85	220.87	1.00	220.87	1.70	0.91	0.91
44.50	294.77	220.75	1.00	220.75	1.69	0.91	0.91
44.60	292.55	218.20	1.00	218.92	1.71	0.91	0.91
44.70	291.79	217.01	1.02	222.23	1.72	0.91	0.91
44.80	294.37	219.18	1.00	219.18	1.70	0.91	0.91
44.90	299.33	223.84	1.00	223.84	1.67	0.91	0.91
45.00	305.05	228.94	1.00	228.94	1.63	0.92	0.92
45.10	310.35	233.00	1.00	233.00	1.62	0.92	0.92
45.20	314.64	235.82	1.00	235.82	1.63	0.92	0.92
45.30	316.67	236.72	1.00	236.72	1.64	0.92	0.92
45.40	316.15	235.62	1.00	235.62	1.65	0.92	0.92
45.50	314.75	233.66	1.00	233.66	1.66	0.92	0.92
45.60	313.96	232.13	1.00	232.13	1.68	0.92	0.92
45.70	313.55	231.06	1.00	231.06	1.69	0.92	0.92
45.80	312.06	229.50	1.00	229.50	1.70	0.92	0.92
45.90	308.31	226.55	1.00	226.55	1.69	0.91	0.91
46.00	302.20	221.94	1.00	221.94	1.69	0.91	0.91
46.10	293.67	215.60	1.00	215.60	1.68	0.90	0.90
46.20	283.78	208.21	1.00	208.21	1.67	0.90	0.90
46.30	273.76	200.90	1.00	200.90	1.66	0.89	0.89
46.40	264.02	193.71	1.00	193.71	1.65	0.88	0.88
46.50	253.44	185.59	1.00	185.59	1.66	0.87	0.87
46.60	239.32	174.12	1.00	174.12	1.68	0.86	0.86
46.70	218.44	156.86	1.08	169.18	1.75	0.85	0.85
46.80	190.67	134.12	1.20	161.00	1.85	0.84	0.84
46.90	159.42	108.98	1.30	141.79	1.99	0.82	0.82
47.00	130.94	86.50	1.53	132.00	2.16	0.80	0.80
47.10	109.62	69.95	2.03	142.18	2.33	0.82	0.82
47.20	99.20	61.64	2.69	165.64	2.46	0.85	0.85
47.30	101.82	62.70	2.99	187.16	2.50	0.86	0.86
47.40	114.04	70.74	2.75	194.52	2.47	0.88	0.88
47.50	127.97	80.48	2.33	187.25	2.39	0.87	0.87
47.60	134.39	85.31	2.05	175.23	2.33	0.86	0.86
47.70	131.72	83.56	2.02	168.52	2.32	0.85	0.85
47.80	123.26	77.42	2.18	168.66	2.36	0.85	0.85
47.90	115.03	71.49	2.37	169.66	2.40	0.85	0.85
48.00	111.14	68.85	2.38	164.20	2.40	0.85	0.85

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
48.10	113.23	70.68	2.14	151.48	2.35	0.83	0.83
48.20	120.10	76.16	1.80	136.95	2.26	0.81	0.81
48.30	127.66	82.45	1.53	125.94	2.16	0.79	0.79
48.40	131.70	86.31	1.39	119.72	2.08	0.78	0.78
48.50	130.27	85.89	1.34	114.96	2.03	0.77	0.77
48.60	123.72	81.11	1.36	109.95	2.05	0.77	0.77
48.70	112.92	72.70	1.46	106.49	2.13	0.76	0.76
48.80	98.74	61.77	1.77	109.45	2.26	0.77	0.77
48.90	82.92	50.01	2.44	121.83	2.41	0.79	0.79
49.00	68.00	39.45	3.48	137.25	2.57	0.86	0.86
49.10	55.01	30.71	4.77	146.38	2.71	0.82	0.82
49.20	44.63	24.09	6.07	146.17	2.82	0.82	0.82
49.30	36.24	19.19	7.24	138.98	2.90	0.81	0.81
49.40	30.08	15.61	8.24	128.62	2.97	0.80	0.80
49.50	25.88	13.16	8.98	118.11	3.01	0.58	0.94
49.60	23.84	11.96	9.27	110.93	3.03	0.50	0.85
49.70	26.26	13.33	8.47	112.92	2.98	0.77	0.77
49.80	32.30	16.76	7.34	123.05	2.91	0.79	0.79
49.90	38.31	20.17	6.55	132.08	2.85	0.80	0.80

Abbreviations

q_t :	Total cone resistance
K_c :	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c :	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

LIQUEFACTION ANALYSIS REPORT

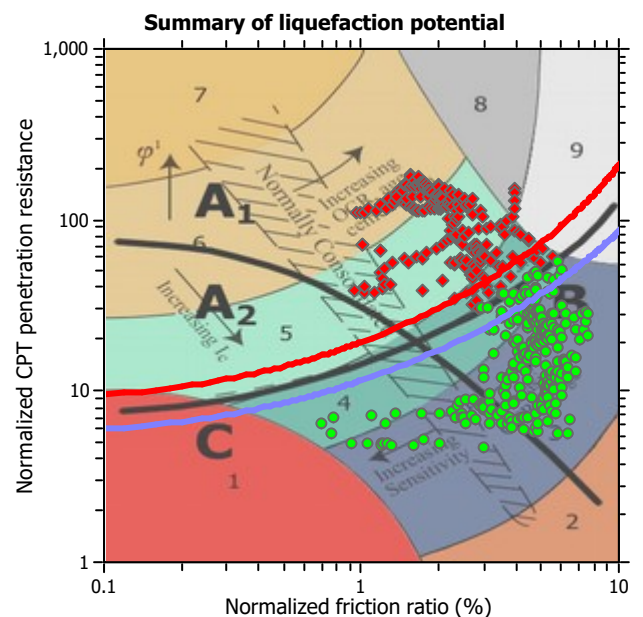
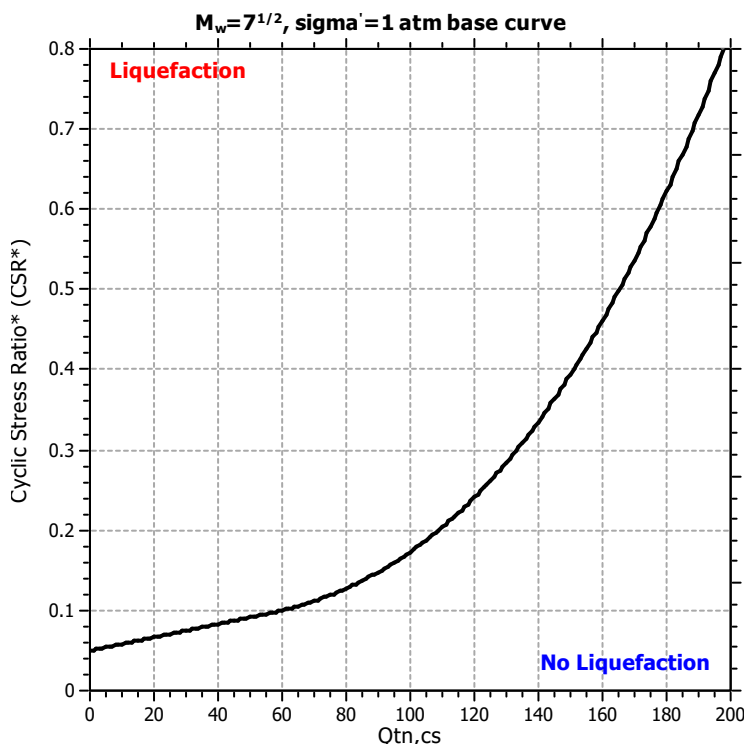
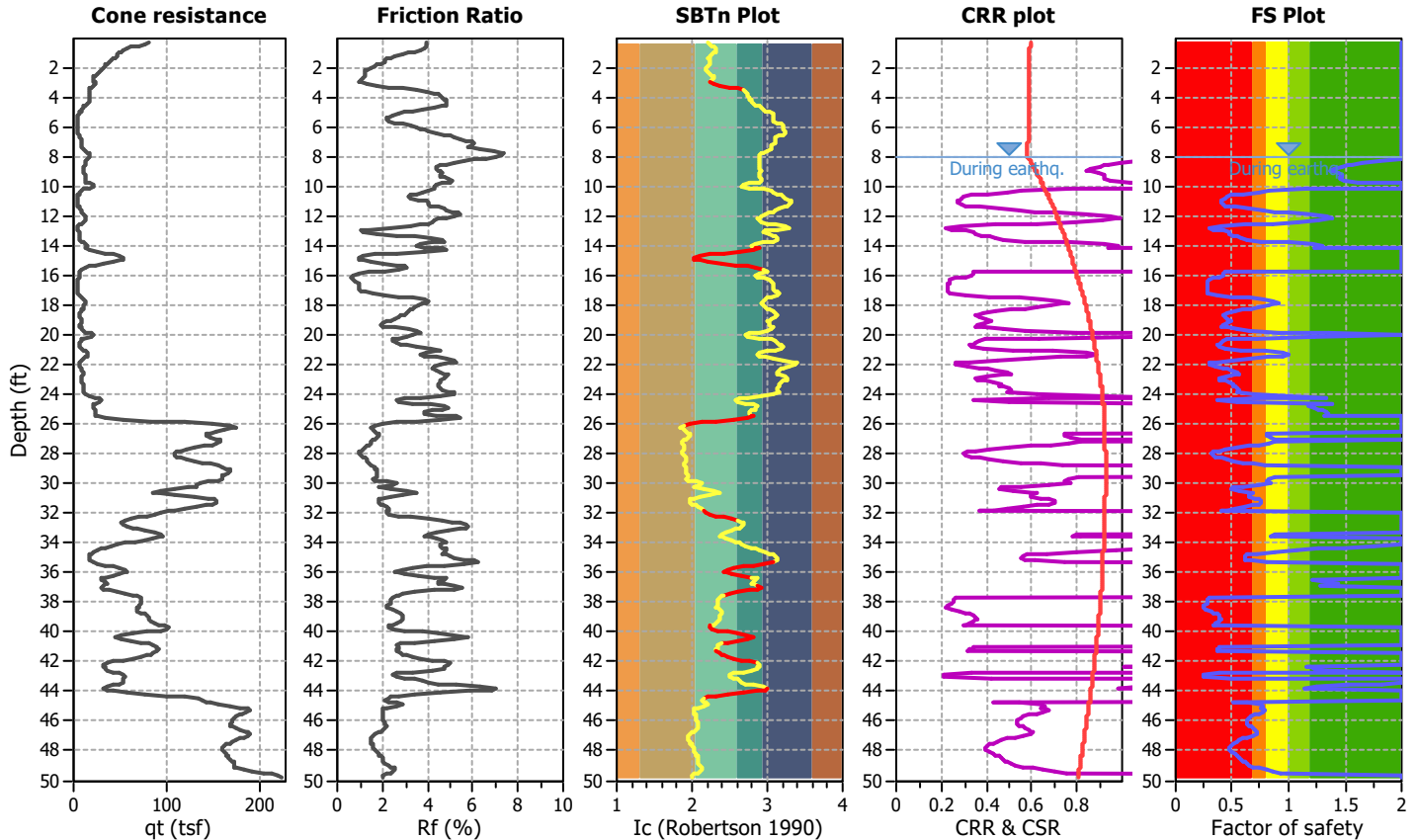
Project title : 21-483 Equestrian Estates

Location : Avenue 64 at Harrison Street, Thermal California

CPT file : CPT-8 Robt 2009

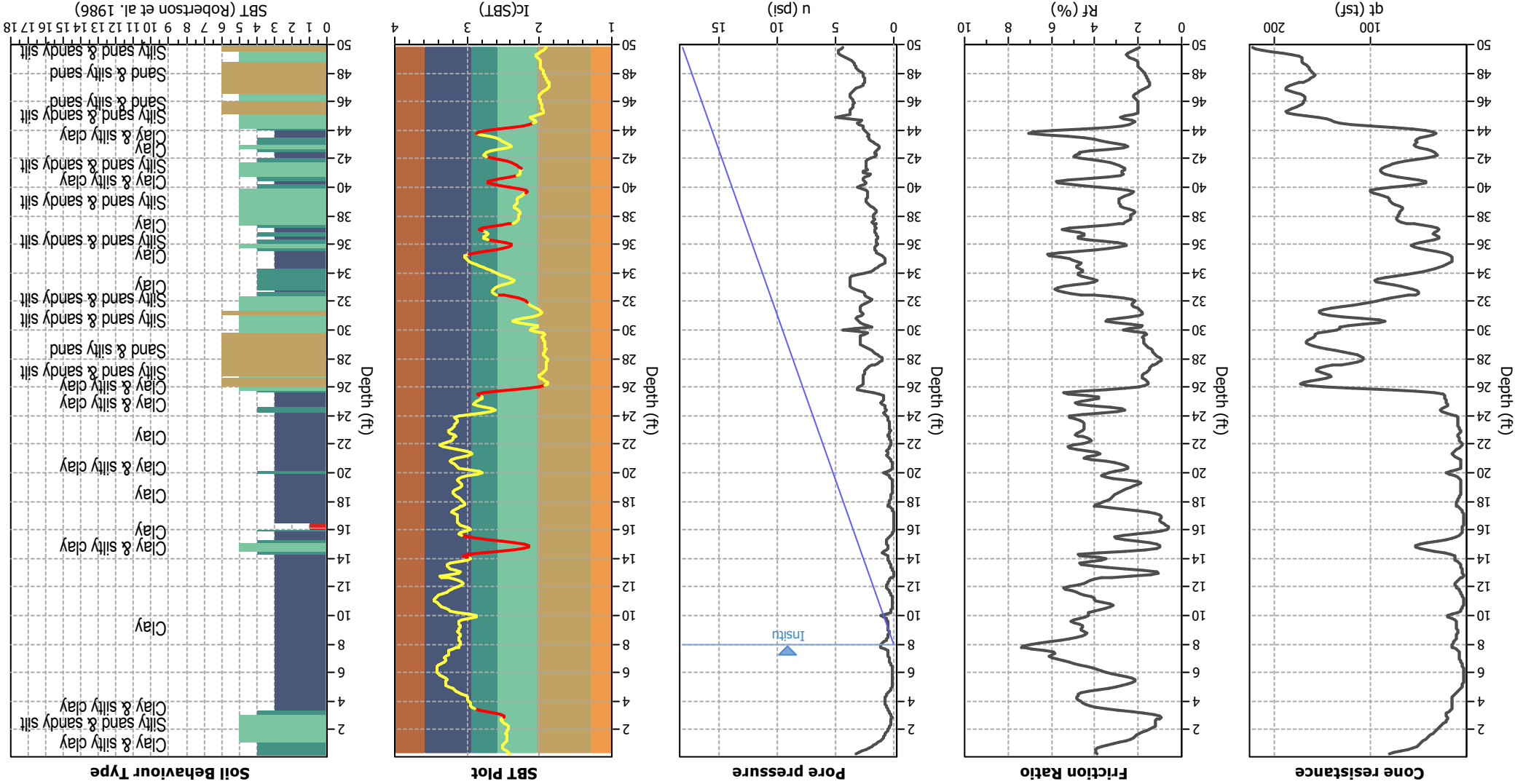
Input parameters and analysis data

Analysis method:	Robertson (2009)	G.W.T. (in-situ):	8.00 ft	Use fill:	No	Clay like behavior	
Fines correction method:	Robertson (2009)	G.W.T. (earthq.):	8.00 ft	Fill height:	N/A	applied:	All soils
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude M_w :	7.34	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.74	Unit weight calculation:	Based on SBT	K_o applied:	No	MSF method:	Method based



Zone A₁: Cyclic liquefaction likely depending on size and duration of cyclic loading
Zone A₂: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

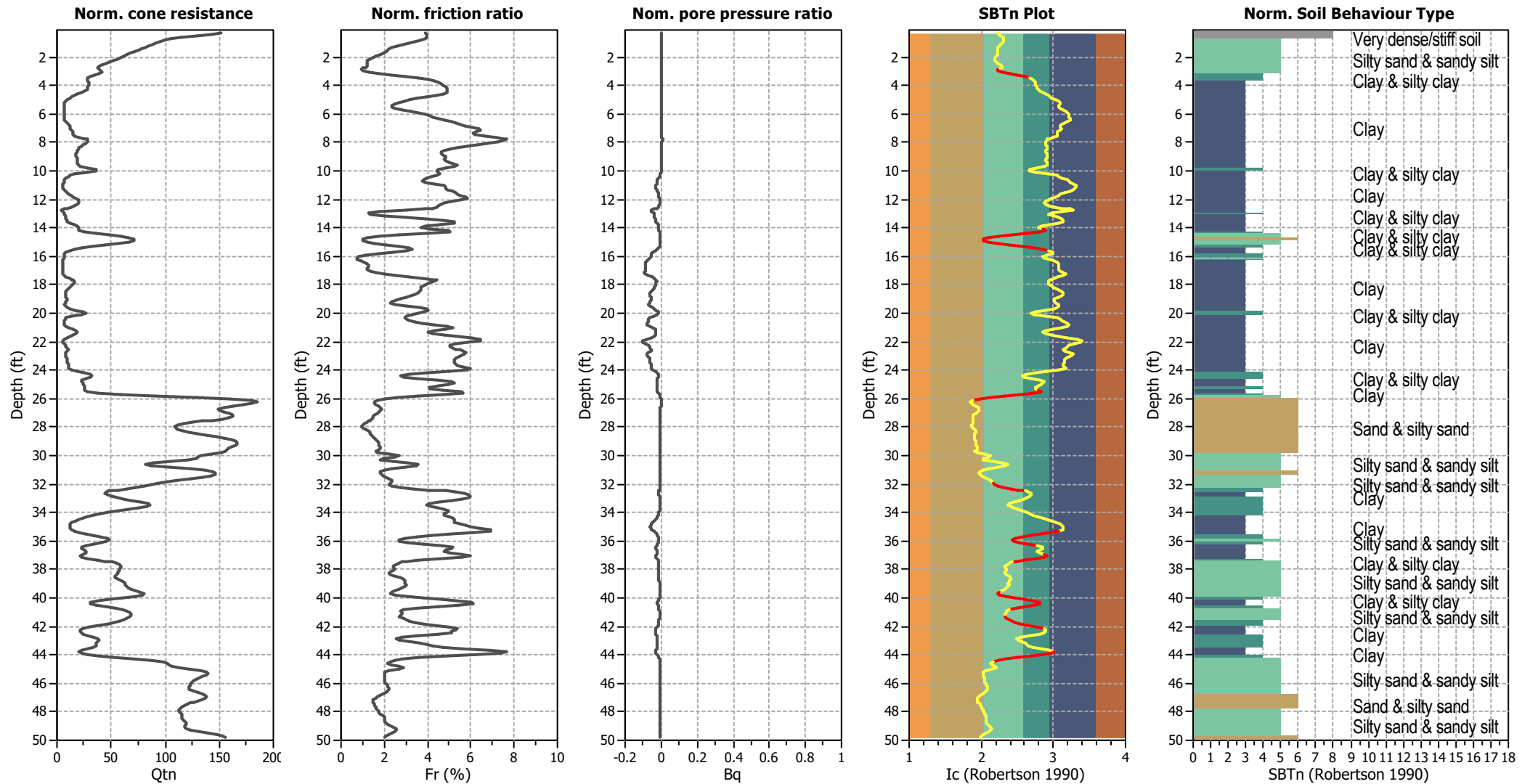
CPT basic interpretation plots



Input parameters and analysis data

Analysis method:	Robertson (2009)	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Limit depth applied:	No
Points to test:	Based on Ic value	Clay like behavior applied:	All soils
Earthquake magnitude M_w :	7.34	K_0 applied:	No
Peak ground acceleration:	0.74	Transition detect. applied:	Yes
Depth to water table (instu):	8.00 ft	Limit depth:	N/A
Fill height:	N/A	Unit weight:	N/A
Use fill:	No	Based on SBT	
Unit weight calculation:	Based on SBT		
Ic cut-off value:	2.60		
Average results interval:	3		
Depth to water table (earthq.):	8.00 ft		

CPT basic interpretation plots (normalized)



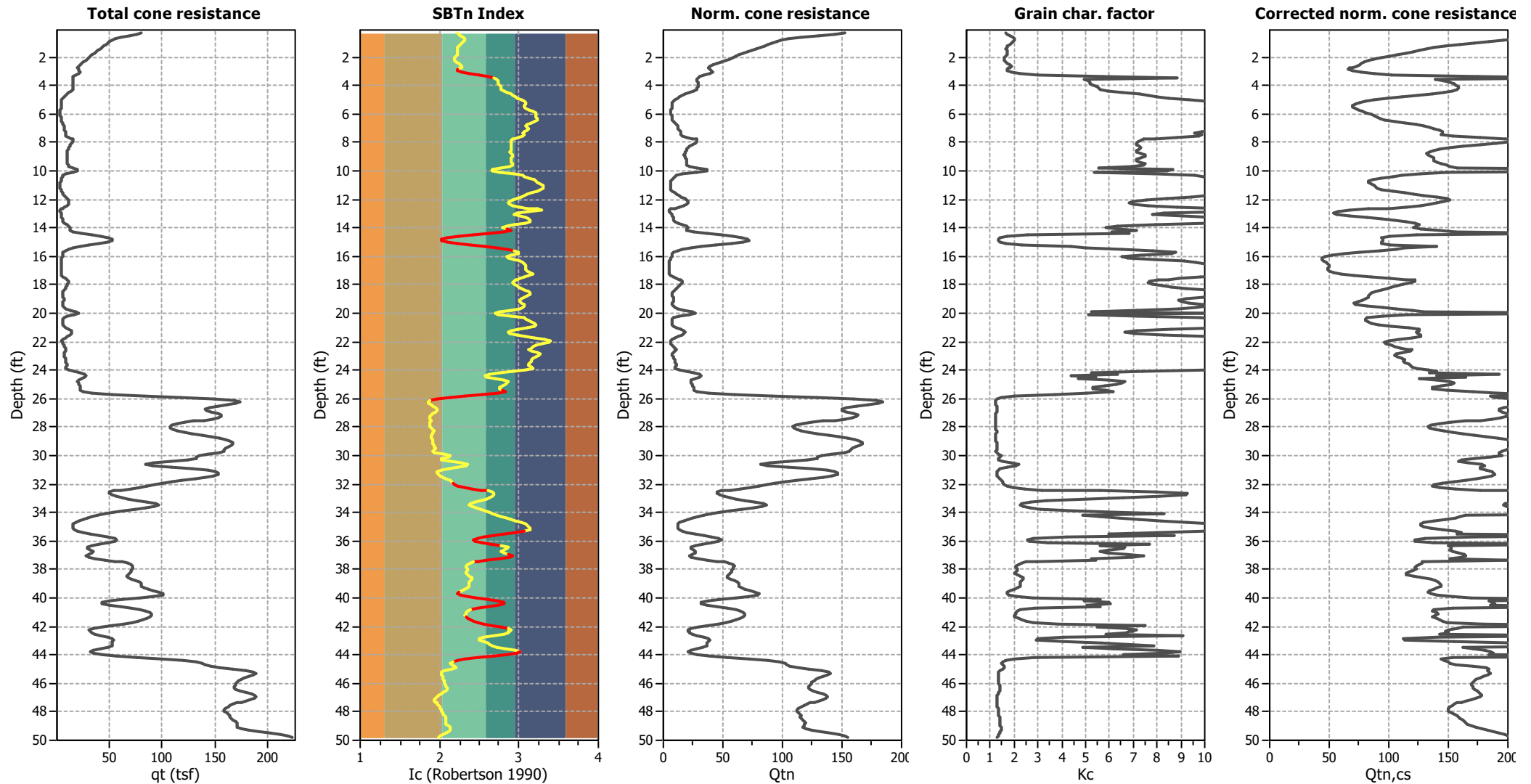
Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	No
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

SBTn legend

1. Sensitive fine grained	4. Clayey silt to silty	7. Gravely sand to sand
2. Organic material	5. Silty sand to sandy silt	8. Very stiff sand to
3. Clay to silty clay	6. Clean sand to silty sand	9. Very stiff fine grained

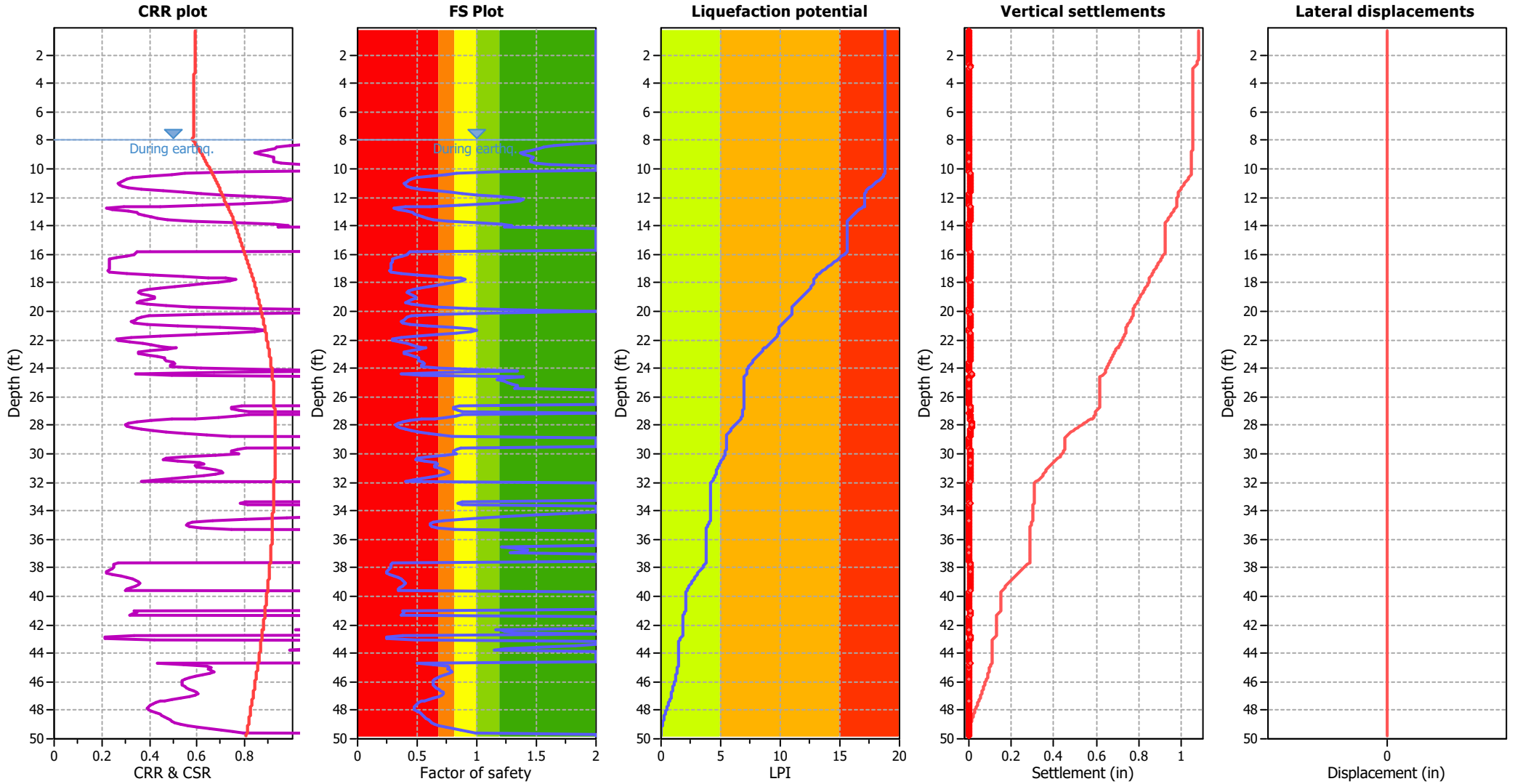
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on I_c value	I_c cut-off value:	2.60	K_o applied:	No
Earthquake magnitude M_w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (earthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	No
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

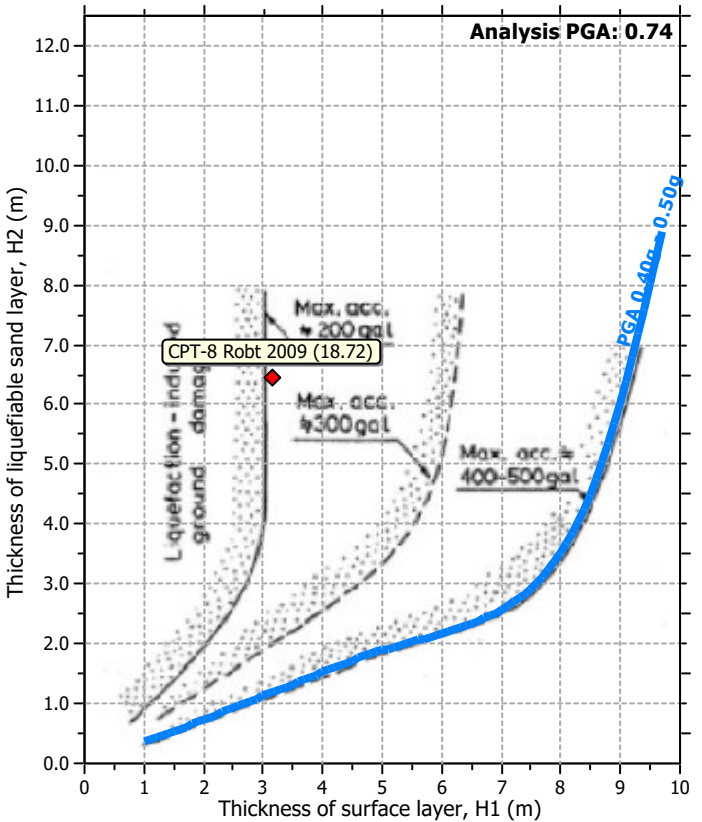
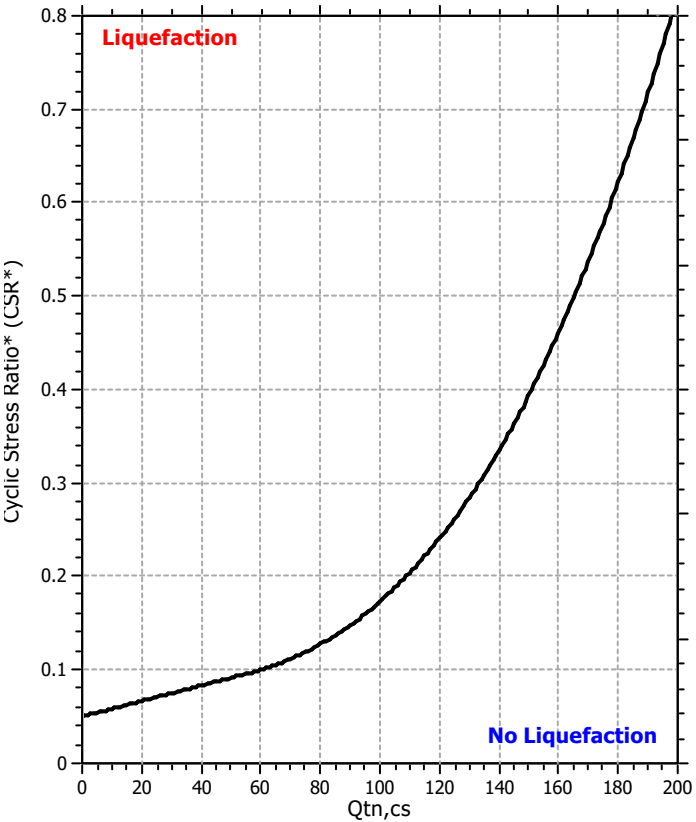
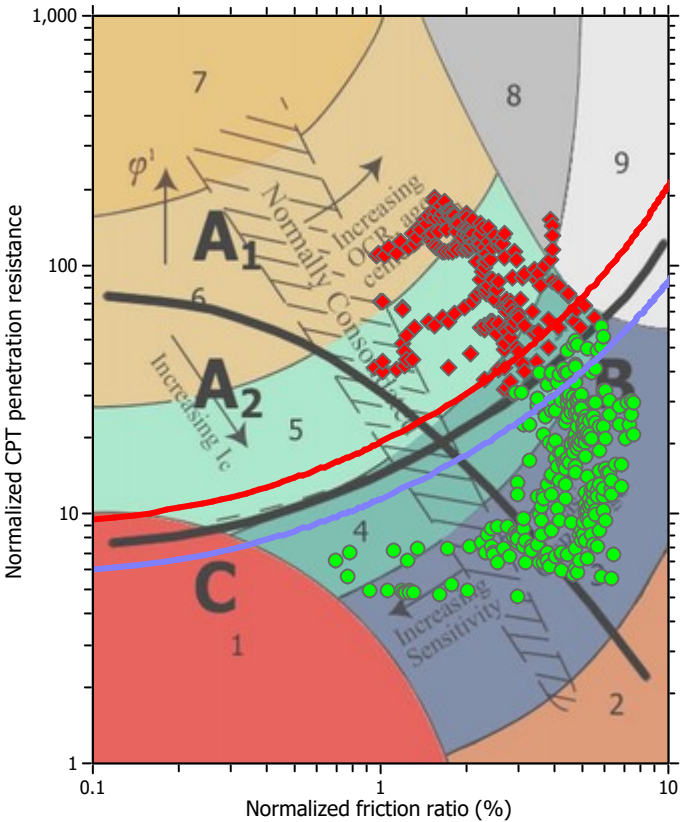
F.S. color scheme

- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

LPI color scheme

- Very high risk
- High risk
- Low risk

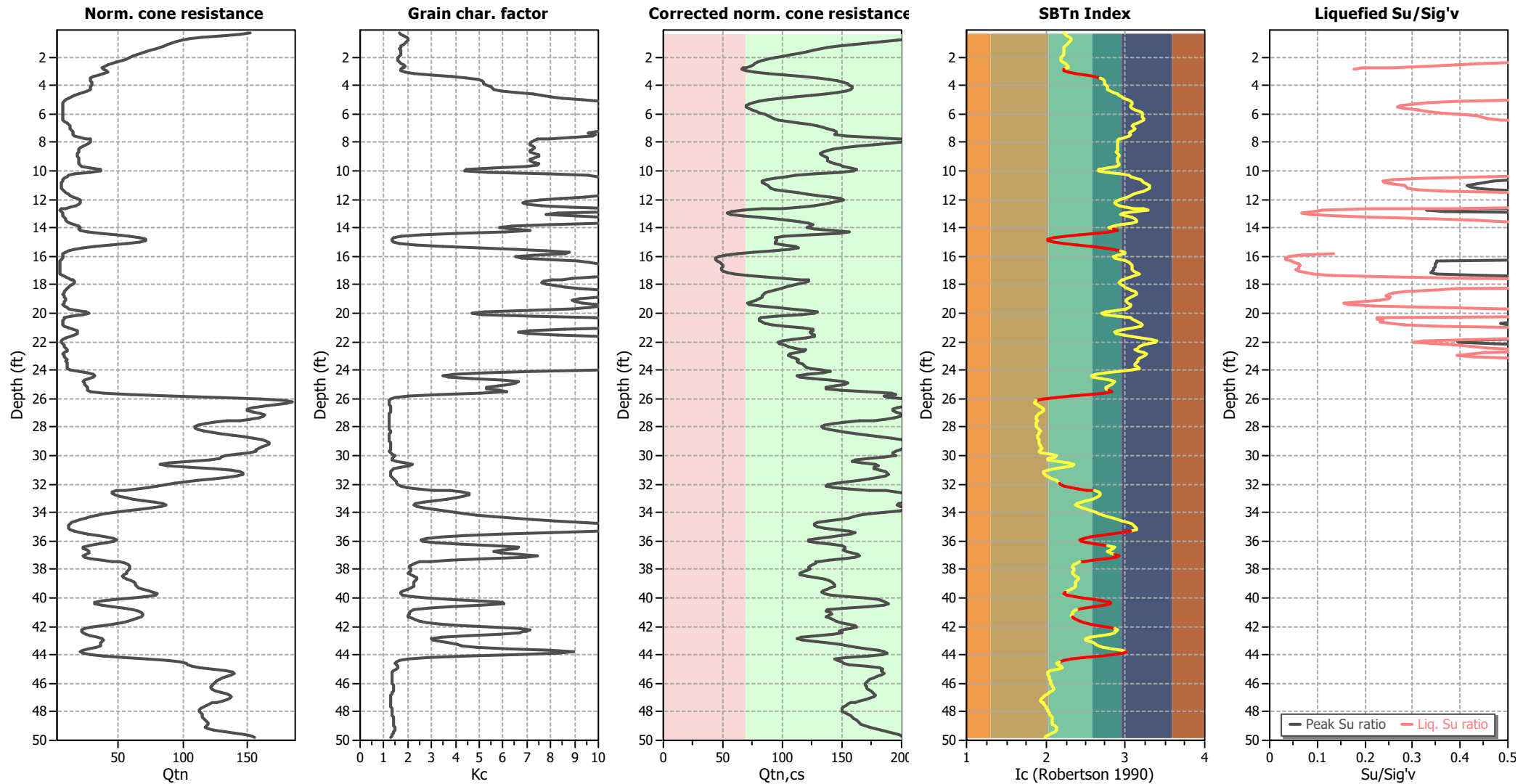
Liquefaction analysis summary plots



Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on I_c value	I_c cut-off value:	2.60	K_o applied:	No
Earthquake magnitude M_w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

Check for strength loss plots (Robertson (2010))



Input parameters and analysis data

Analysis method:	Robertson (2009)	Depth to water table (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	Robertson (2009)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	No
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	All soils
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

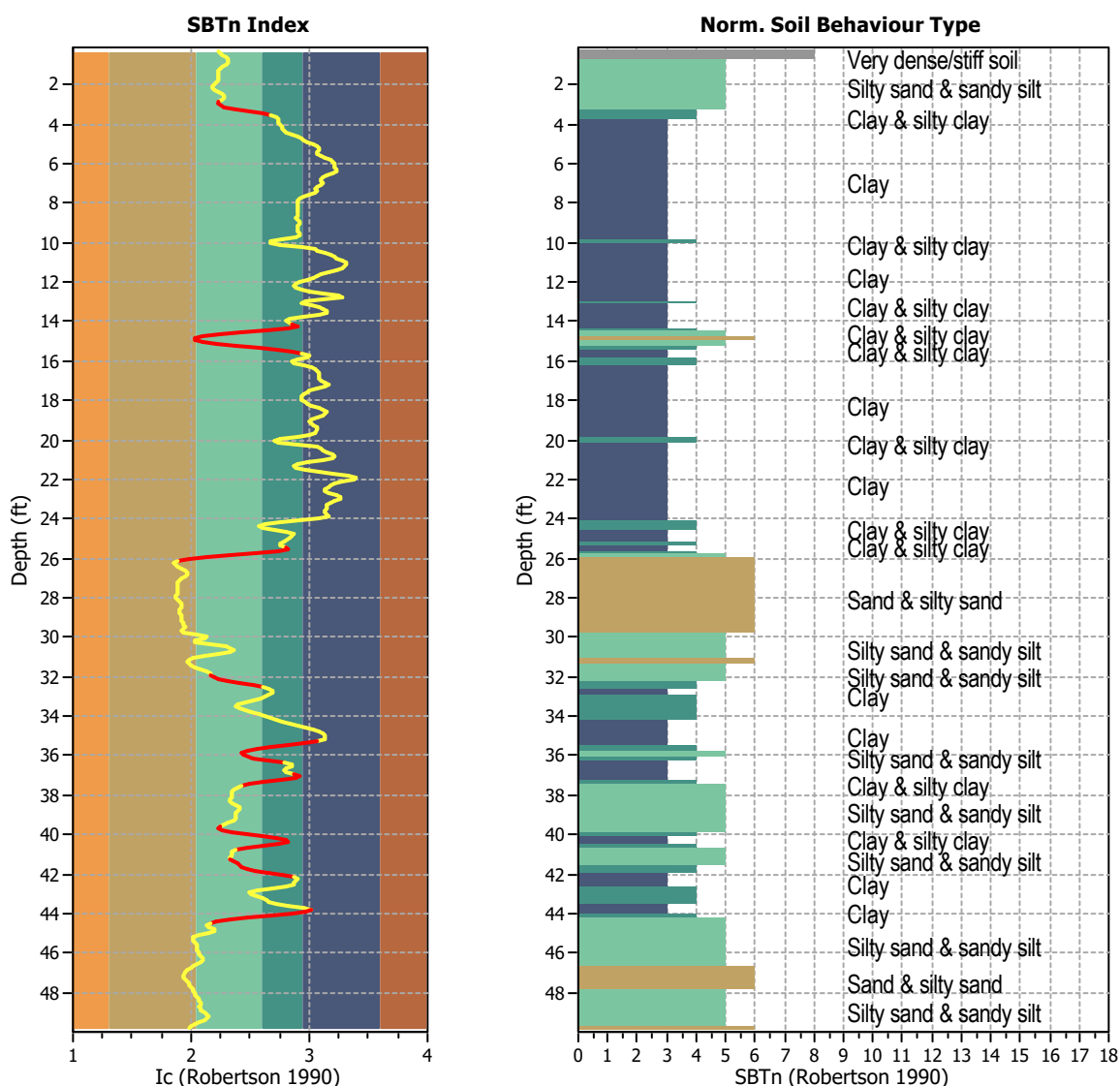
TRANSITION LAYER DETECTION ALGORITHM REPORT

Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vice-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between $1.80 < I_c < 3.0$) and a rate of change of I_c . Transitions typically occur when the rate of change of I_c is fast (i.e. ΔI_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties

I_c minimum check value: 1.70
 I_c maximum check value: 3.00
 I_c change ratio value: 0.0250
 Minimum number of points in layer: 4

General statistics

Total points in CPT file: 496
 Total points excluded: 86
 Exclusion percentage: 17.34%
 Number of layers detected: 12

Transition layer No	Number of points	Depth	SBT _n number	SBT _n description
Transition layer 1	7	Start depth: 3.00 (ft)	5	Silty sand & sandy silt
		End depth: 3.60 (ft)	4	Clay & silty clay
Transition layer 2	7	Start depth: 14.20 (ft)	3	Clay
		End depth: 14.80 (ft)	6	Sand & silty sand
Transition layer 3	9	Start depth: 14.90 (ft)	6	Sand & silty sand
		End depth: 15.70 (ft)	3	Clay
Transition layer 4	8	Start depth: 25.50 (ft)	3	Clay
		End depth: 26.20 (ft)	6	Sand & silty sand
Transition layer 5	7	Start depth: 32.00 (ft)	5	Silty sand & sandy silt
		End depth: 32.60 (ft)	4	Clay & silty clay
Transition layer 6	6	Start depth: 35.40 (ft)	3	Clay
		End depth: 35.90 (ft)	5	Silty sand & sandy silt
Transition layer 7	5	Start depth: 36.00 (ft)	5	Silty sand & sandy silt
		End depth: 36.40 (ft)	3	Clay
Transition layer 8	7	Start depth: 37.00 (ft)	3	Clay
		End depth: 37.60 (ft)	5	Silty sand & sandy silt
Transition layer 9	7	Start depth: 39.70 (ft)	5	Silty sand & sandy silt
		End depth: 40.30 (ft)	3	Clay
Transition layer 10	6	Start depth: 40.40 (ft)	3	Clay
		End depth: 40.90 (ft)	5	Silty sand & sandy silt
Transition layer 11	9	Start depth: 41.40 (ft)	5	Silty sand & sandy silt
		End depth: 42.20 (ft)	3	Clay
Transition layer 12	8	Start depth: 43.90 (ft)	3	Clay
		End depth: 44.60 (ft)	5	Silty sand & sandy silt

Start depth: Depth where the transition layer begins

End depth: Depth where the transition layer ends

:: Field input data ::						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1	0.30	81.74	3.21	3.21	19.79	129.38
2	0.40	78.01	3.05	3.05	20.35	128.86
3	0.50	68.49	2.73	2.73	21.35	127.94
4	0.60	60.12	2.42	2.42	22.53	126.78
5	0.70	54.52	2.13	2.13	23.18	125.70
6	0.80	52.21	1.93	1.93	23.16	124.74
7	0.90	50.28	1.73	1.73	22.73	123.84
8	1.00	48.32	1.53	1.53	22.09	122.87
9	1.10	46.83	1.34	1.34	21.34	121.79
10	1.20	44.95	1.15	1.15	20.52	120.68
11	1.30	43.53	1.00	1.00	19.91	119.62
12	1.40	41.68	0.91	0.91	19.74	118.78
13	1.50	39.61	0.86	0.86	19.90	118.06
14	1.60	37.60	0.78	0.78	20.09	117.27
15	1.70	35.58	0.69	0.69	20.07	116.30
16	1.80	33.68	0.61	0.61	19.82	115.25
17	1.90	32.56	0.53	0.53	19.36	114.15
18	2.00	31.45	0.46	0.46	18.82	112.92
19	2.10	29.55	0.38	0.38	18.42	111.66
20	2.20	28.10	0.33	0.33	18.47	110.49
21	2.30	26.06	0.30	0.30	19.13	109.59
22	2.40	23.60	0.28	0.28	20.19	108.90
23	2.50	22.19	0.27	0.27	21.27	108.24
24	2.60	20.77	0.25	0.25	21.88	107.55
25	2.70	19.84	0.23	0.23	21.84	106.68
26	2.80	19.71	0.20	0.20	21.05	105.86
27	2.90	20.36	0.18	0.18	20.05	105.63
28	3.00	21.73	0.20	0.20	20.05	106.69
29	3.10	22.91	0.28	0.28	21.90	108.64
30	3.20	21.66	0.38	0.38	25.58	110.11
31	3.30	17.70	0.41	0.41	30.60	111.08
32	3.40	16.02	0.48	0.48	35.81	111.65
33	3.50	15.13	0.54	0.54	39.29	112.42
34	3.60	15.13	0.60	0.60	41.50	113.12
35	3.70	15.13	0.65	0.65	42.59	113.76
36	3.80	15.51	0.70	0.70	42.79	114.36
37	3.90	16.46	0.75	0.75	42.80	114.71
38	4.00	16.06	0.74	0.74	43.33	114.80
39	4.10	15.15	0.73	0.73	44.27	114.73
40	4.20	15.17	0.74	0.74	44.70	114.70
41	4.30	15.53	0.74	0.74	44.99	114.51
42	4.40	14.36	0.69	0.69	46.35	113.76
43	4.50	11.94	0.58	0.58	49.16	112.33
44	4.60	9.91	0.47	0.47	52.10	110.48
45	4.70	8.82	0.38	0.38	53.77	108.49
46	4.80	7.90	0.29	0.29	55.22	106.19
47	4.90	6.23	0.20	0.20	57.22	103.67
48	5.00	5.29	0.16	0.16	60.62	100.89

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
49	5.10	4.35	0.12	0.12	63.31	98.72
50	5.20	3.98	0.10	0.10	64.77	97.05
51	5.30	3.98	0.09	0.09	64.34	96.14
52	5.40	3.98	0.08	0.08	63.46	95.71
53	5.50	3.98	0.08	0.08	63.46	95.69
54	5.60	3.98	0.09	0.09	64.82	96.09
55	5.70	3.89	0.10	0.10	67.65	96.65
56	5.80	3.65	0.11	0.11	70.98	97.20
57	5.90	3.58	0.12	0.12	73.34	97.88
58	6.00	3.78	0.13	0.13	73.96	98.76
59	6.10	3.98	0.15	0.15	73.95	99.49
60	6.20	3.98	0.15	0.15	74.33	99.99
61	6.30	3.98	0.16	0.16	75.36	100.35
62	6.40	3.98	0.17	0.17	75.15	101.33
63	6.50	4.60	0.22	0.22	73.05	102.99
64	6.60	5.51	0.27	0.27	69.49	104.94
65	6.70	6.40	0.33	0.33	66.30	106.67
66	6.80	7.17	0.38	0.38	64.97	107.80
67	6.90	7.17	0.41	0.41	65.50	108.40
68	7.00	6.85	0.42	0.42	66.60	108.75
69	7.10	7.14	0.44	0.44	65.22	109.49
70	7.20	8.58	0.51	0.51	62.69	110.11
71	7.30	8.76	0.50	0.50	61.53	110.23
72	7.40	7.87	0.45	0.45	62.76	109.93
73	7.50	7.62	0.47	0.47	62.31	111.21
74	7.60	10.70	0.73	0.73	58.65	114.09
75	7.70	14.62	1.07	1.07	54.99	116.57
76	7.80	15.53	1.17	1.17	53.08	117.80
77	7.90	15.53	1.14	1.14	52.47	117.89
78	8.00	15.49	1.09	1.09	52.04	117.40
79	8.10	14.67	0.97	0.97	51.77	116.50
80	8.20	13.50	0.82	0.82	51.75	115.20
81	8.30	12.44	0.69	0.69	52.17	113.68
82	8.40	11.03	0.57	0.57	52.43	112.36
83	8.50	10.75	0.52	0.52	52.34	111.37
84	8.60	10.75	0.49	0.49	51.63	110.85
85	8.70	10.65	0.46	0.46	51.58	110.34
86	8.80	9.95	0.43	0.43	52.36	109.91
87	8.90	9.56	0.43	0.43	53.32	109.87
88	9.00	9.98	0.47	0.47	53.24	110.29
89	9.10	10.67	0.50	0.50	52.41	110.67
90	9.20	10.75	0.48	0.48	51.67	110.82
91	9.30	10.75	0.48	0.48	51.68	110.87
92	9.40	10.75	0.51	0.51	52.29	111.11
93	9.50	10.75	0.53	0.53	53.12	111.44
94	9.60	10.75	0.55	0.55	53.04	111.95
95	9.70	11.72	0.61	0.61	50.87	112.63
96	9.80	13.65	0.65	0.65	44.49	114.64

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
97	9.90	21.35	0.93	0.93	39.07	116.71
98	10.00	25.42	1.08	1.08	38.83	116.55
99	10.10	13.64	0.59	0.59	43.60	113.82
100	10.20	6.62	0.30	0.30	54.70	108.76
101	10.30	6.97	0.28	0.28	61.68	105.35
102	10.40	6.44	0.23	0.23	63.05	103.82
103	10.50	4.76	0.17	0.17	67.23	101.54
104	10.60	3.98	0.13	0.13	72.09	99.38
105	10.70	3.98	0.12	0.12	74.03	98.41
106	10.80	3.88	0.12	0.12	75.77	98.35
107	10.90	3.64	0.13	0.13	79.19	98.75
108	11.00	3.58	0.15	0.15	82.17	99.13
109	11.10	3.58	0.15	0.15	82.20	99.46
110	11.20	3.80	0.15	0.15	80.81	99.79
111	11.30	3.98	0.16	0.16	79.04	100.64
112	11.40	4.34	0.19	0.19	75.21	102.69
113	11.50	5.78	0.28	0.28	69.77	104.94
114	11.60	7.01	0.34	0.34	65.62	106.60
115	11.70	7.17	0.35	0.35	63.33	108.03
116	11.80	8.17	0.45	0.45	60.98	109.77
117	11.90	10.23	0.58	0.58	57.09	111.52
118	12.00	11.87	0.62	0.62	53.57	112.34
119	12.10	12.07	0.57	0.57	51.25	112.32
120	12.20	12.17	0.54	0.54	50.39	111.81
121	12.30	11.71	0.51	0.51	51.25	110.91
122	12.40	9.82	0.41	0.41	53.86	109.33
123	12.50	7.81	0.31	0.31	58.77	106.80
124	12.60	5.80	0.21	0.21	66.12	103.30
125	12.70	3.78	0.12	0.12	76.14	98.80
126	12.80	2.58	0.06	0.06	79.41	94.35
127	12.90	3.41	0.05	0.05	67.11	91.57
128	13.00	4.76	0.04	0.04	56.41	91.21
129	13.10	4.78	0.04	0.04	54.53	92.87
130	13.20	4.78	0.08	0.08	59.66	96.06
131	13.30	5.04	0.13	0.13	64.19	99.65
132	13.40	5.75	0.20	0.20	66.72	102.34
133	13.50	5.97	0.25	0.25	68.52	104.19
134	13.60	5.97	0.28	0.28	68.47	105.90
135	13.70	7.27	0.36	0.36	63.80	107.69
136	13.80	9.56	0.43	0.43	54.92	109.49
137	13.90	12.84	0.46	0.46	48.27	110.45
138	14.00	14.00	0.44	0.44	46.00	110.79
139	14.10	12.41	0.46	0.46	48.61	111.00
140	14.20	10.88	0.53	0.53	51.64	112.57
141	14.30	14.45	0.78	0.78	47.02	115.21
142	14.40	23.31	1.02	1.02	37.19	117.24
143	14.50	33.06	0.91	0.91	27.67	117.74
144	14.60	42.36	0.66	0.66	20.37	116.81

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
145	14.70	49.23	0.54	0.54	15.71	115.61
146	14.80	53.79	0.50	0.50	13.75	115.19
147	14.90	54.94	0.53	0.53	13.74	115.34
148	15.00	50.74	0.57	0.57	15.63	115.76
149	15.10	42.11	0.64	0.64	19.63	115.78
150	15.20	29.95	0.64	0.64	25.79	115.14
151	15.30	20.82	0.58	0.58	33.84	113.62
152	15.40	14.75	0.48	0.48	41.79	111.37
153	15.50	10.94	0.34	0.34	48.93	108.28
154	15.60	7.68	0.20	0.20	54.55	104.36
155	15.70	5.86	0.12	0.12	58.41	99.84
156	15.80	5.16	0.07	0.07	57.64	95.64
157	15.90	5.11	0.04	0.04	52.37	92.42
158	16.00	5.81	0.03	0.03	49.10	89.90
159	16.10	5.09	0.03	0.03	50.06	88.22
160	16.20	3.98	0.02	0.02	54.76	87.36
161	16.30	3.98	0.03	0.03	59.85	87.62
162	16.40	3.98	0.03	0.03	61.77	88.71
163	16.50	3.98	0.04	0.04	63.29	89.52
164	16.60	3.98	0.04	0.04	64.12	89.92
165	16.70	3.98	0.04	0.04	64.25	89.92
166	16.80	3.98	0.04	0.04	63.85	89.63
167	16.90	3.98	0.04	0.04	63.83	89.56
168	17.00	3.98	0.04	0.04	65.08	90.17
169	17.10	3.98	0.05	0.05	68.33	91.47
170	17.20	3.86	0.06	0.06	70.67	93.57
171	17.30	4.40	0.08	0.08	67.25	97.69
172	17.40	6.80	0.17	0.17	62.58	102.17
173	17.50	8.41	0.28	0.28	58.86	106.03
174	17.60	9.78	0.38	0.38	57.25	108.60
175	17.70	10.96	0.46	0.46	55.50	110.02
176	17.80	11.67	0.47	0.47	53.95	110.39
177	17.90	11.51	0.43	0.43	53.68	109.82
178	18.00	10.29	0.37	0.37	54.59	108.84
179	18.10	9.55	0.33	0.33	56.29	107.67
180	18.20	8.88	0.29	0.29	57.83	106.64
181	18.30	8.19	0.26	0.26	60.14	105.53
182	18.40	7.20	0.23	0.23	63.63	104.27
183	18.50	6.18	0.19	0.19	66.82	103.00
184	18.60	5.97	0.17	0.17	68.39	102.02
185	18.70	5.97	0.17	0.17	68.06	101.63
186	18.80	6.02	0.17	0.17	66.02	101.72
187	18.90	6.71	0.17	0.17	62.97	101.87
188	19.00	7.17	0.17	0.17	60.06	101.90
189	19.10	7.17	0.16	0.16	58.89	101.31
190	19.20	6.71	0.13	0.13	59.38	100.10
191	19.30	6.02	0.11	0.11	60.64	99.08
192	19.40	5.97	0.11	0.11	62.91	99.35

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
193	19.50	6.18	0.15	0.15	63.55	101.90
194	19.60	7.79	0.24	0.24	61.83	105.03
195	19.70	9.59	0.34	0.34	58.88	107.55
196	19.80	10.58	0.40	0.40	51.80	111.02
197	19.90	18.07	0.68	0.68	43.18	114.48
198	20.00	27.47	0.93	0.93	40.41	115.05
199	20.10	16.74	0.49	0.49	42.62	112.73
200	20.20	8.02	0.21	0.21	51.99	106.77
201	20.30	6.61	0.16	0.16	62.53	102.26
202	20.40	6.36	0.16	0.16	65.06	101.55
203	20.50	6.57	0.17	0.17	67.05	101.55
204	20.60	6.00	0.16	0.16	69.15	101.85
205	20.70	5.97	0.18	0.18	72.33	102.25
206	20.80	5.97	0.20	0.20	74.07	103.47
207	20.90	6.45	0.26	0.26	72.52	105.95
208	21.00	8.57	0.41	0.41	66.18	109.02
209	21.10	11.84	0.55	0.55	57.80	111.36
210	21.20	14.73	0.58	0.58	51.72	112.42
211	21.30	15.49	0.54	0.54	49.60	112.48
212	21.40	14.13	0.54	0.54	51.35	112.32
213	21.50	12.74	0.56	0.56	56.59	111.91
214	21.60	10.38	0.52	0.52	63.97	110.83
215	21.70	7.70	0.41	0.41	73.18	108.98
216	21.80	6.13	0.33	0.33	83.52	106.51
217	21.90	4.78	0.24	0.24	89.71	104.59
218	22.00	4.92	0.22	0.22	87.27	104.03
219	22.10	6.30	0.27	0.27	79.96	104.90
220	22.20	7.17	0.30	0.30	74.17	106.10
221	22.30	7.68	0.32	0.32	71.80	106.93
222	22.40	7.96	0.35	0.35	70.30	107.82
223	22.50	8.72	0.40	0.40	67.96	109.16
224	22.60	10.30	0.49	0.49	67.54	109.84
225	22.70	9.08	0.45	0.45	70.08	109.40
226	22.80	7.05	0.35	0.35	74.88	108.04
227	22.90	6.92	0.33	0.33	78.39	106.75
228	23.00	6.72	0.30	0.30	77.43	106.64
229	23.10	7.30	0.33	0.33	74.19	107.40
230	23.20	8.76	0.40	0.40	71.27	108.25
231	23.30	8.76	0.40	0.40	69.36	108.78
232	23.40	8.76	0.39	0.39	69.35	108.74
233	23.50	8.76	0.39	0.39	68.89	108.99
234	23.60	9.31	0.43	0.43	67.52	109.61
235	23.70	10.24	0.48	0.48	67.37	109.98
236	23.80	9.37	0.45	0.45	69.28	109.99
237	23.90	8.47	0.44	0.44	70.51	110.49
238	24.00	10.37	0.57	0.57	64.21	112.50
239	24.10	15.82	0.79	0.79	52.77	114.99
240	24.20	22.90	0.90	0.90	43.04	116.41

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
241	24.30	27.66	0.79	0.79	36.58	116.48
242	24.40	28.65	0.67	0.67	33.78	116.09
243	24.50	27.94	0.73	0.73	35.34	115.98
244	24.60	23.58	0.79	0.79	40.49	116.08
245	24.70	18.54	0.80	0.80	46.65	116.41
246	24.80	19.18	0.95	0.95	49.70	117.11
247	24.90	21.65	1.08	1.08	49.13	117.77
248	25.00	21.56	1.01	1.01	47.87	117.73
249	25.10	20.95	0.90	0.90	45.70	117.29
250	25.20	23.57	0.88	0.88	43.41	116.98
251	25.30	24.32	0.86	0.86	43.33	117.06
252	25.40	21.49	0.92	0.92	45.90	117.88
253	25.50	22.36	1.21	1.21	47.32	120.05
254	25.60	30.43	1.78	1.78	42.16	123.24
255	25.70	48.12	2.48	2.48	32.58	126.49
256	25.80	80.56	3.06	3.06	23.48	128.81
257	25.90	119.40	3.14	3.14	16.76	130.10
258	26.00	153.29	2.99	2.99	12.37	130.36
259	26.10	172.88	2.69	2.69	10.08	130.23
260	26.20	176.79	2.63	2.63	9.27	129.99
261	26.30	171.15	2.63	2.63	9.47	129.83
262	26.40	161.95	2.58	2.58	10.14	129.67
263	26.50	152.17	2.59	2.59	10.97	129.51
264	26.60	144.69	2.62	2.62	11.81	129.42
265	26.70	138.95	2.61	2.61	12.26	129.34
266	26.80	140.03	2.57	2.57	12.12	129.29
267	26.90	146.85	2.55	2.55	11.51	129.26
268	27.00	152.97	2.50	2.50	10.81	129.23
269	27.10	157.26	2.44	2.44	10.25	129.07
270	27.20	157.72	2.33	2.33	9.95	128.80
271	27.30	154.12	2.23	2.23	9.90	128.40
272	27.40	147.65	2.11	2.11	9.99	127.83
273	27.50	140.17	1.91	1.91	10.10	126.96
274	27.60	129.80	1.64	1.64	10.11	125.81
275	27.70	120.61	1.40	1.40	10.05	124.48
276	27.80	113.32	1.19	1.19	9.89	123.19
277	27.90	108.27	1.03	1.03	9.68	122.17
278	28.00	106.54	0.97	0.97	9.69	121.79
279	28.10	106.79	1.05	1.05	10.09	122.31
280	28.20	109.71	1.25	1.25	10.63	123.30
281	28.30	114.29	1.42	1.42	11.00	124.35
282	28.40	119.65	1.57	1.57	10.96	125.22
283	28.50	128.28	1.70	1.70	10.67	125.98
284	28.60	137.15	1.83	1.83	10.39	126.85
285	28.70	146.48	2.08	2.08	10.34	127.83
286	28.80	154.57	2.37	2.37	10.50	128.82
287	28.90	160.11	2.62	2.62	10.70	129.63
288	29.00	164.67	2.81	2.81	10.84	130.18

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
289	29.10	167.60	2.89	2.89	10.88	130.47
290	29.20	168.14	2.90	2.90	10.91	130.52
291	29.30	165.83	2.86	2.86	11.07	130.46
292	29.40	161.84	2.86	2.86	11.39	130.43
293	29.50	158.94	2.93	2.93	11.62	130.35
294	29.60	157.73	2.81	2.81	11.42	130.04
295	29.70	158.42	2.53	2.53	10.77	129.41
296	29.80	158.37	2.25	2.25	11.37	129.56
297	29.90	146.79	3.03	3.03	14.43	130.94
298	30.00	126.66	4.37	4.37	16.73	131.62
299	30.10	131.94	3.40	3.40	16.05	130.77
300	30.20	138.08	1.92	1.92	13.72	128.89
301	30.30	125.14	2.19	2.19	13.80	127.88
302	30.40	107.71	2.57	2.57	17.67	128.48
303	30.50	89.25	2.84	2.84	22.06	128.79
304	30.60	78.49	2.94	2.94	24.80	129.08
305	30.70	86.50	3.15	3.15	23.74	129.59
306	30.80	107.64	3.26	3.26	19.92	130.13
307	30.90	131.67	3.08	3.08	16.05	130.19
308	31.00	146.55	2.71	2.71	13.50	129.96
309	31.10	151.34	2.67	2.67	12.36	129.81
310	31.20	153.69	2.77	2.77	12.24	129.97
311	31.30	154.10	2.84	2.84	12.50	130.15
312	31.40	150.62	2.88	2.88	13.07	130.20
313	31.50	142.50	2.91	2.91	14.06	130.11
314	31.60	130.52	2.88	2.88	15.43	129.84
315	31.70	117.89	2.79	2.79	16.75	129.26
316	31.80	107.64	2.51	2.51	17.61	128.40
317	31.90	100.35	2.19	2.19	18.03	127.34
318	32.00	93.07	1.96	1.96	18.63	126.47
319	32.10	85.80	1.91	1.91	20.12	126.15
320	32.20	79.35	2.08	2.08	22.89	126.36
321	32.30	70.33	2.32	2.32	26.83	126.70
322	32.40	60.04	2.47	2.47	31.50	126.82
323	32.50	52.30	2.52	2.52	35.65	126.73
324	32.60	49.20	2.54	2.54	38.33	126.73
325	32.70	48.98	2.65	2.65	39.64	127.11
326	32.80	50.77	2.96	2.96	39.62	127.93
327	32.90	56.84	3.36	3.36	38.55	128.88
328	33.00	62.92	3.60	3.60	36.88	129.62
329	33.10	66.85	3.69	3.69	34.75	130.13
330	33.20	74.49	3.78	3.78	31.87	130.52
331	33.30	86.21	3.80	3.80	28.55	130.84
332	33.40	96.39	3.72	3.72	26.19	131.01
333	33.50	98.33	3.71	3.71	25.56	131.05
334	33.60	93.15	3.77	3.77	26.62	130.99
335	33.70	85.71	3.79	3.79	28.77	130.69
336	33.80	75.23	3.57	3.57	31.34	129.93

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
337	33.90	63.53	3.10	3.10	34.02	128.63
338	34.00	53.49	2.54	2.54	36.51	126.89
339	34.10	45.17	2.05	2.05	38.72	125.11
340	34.20	39.58	1.76	1.76	41.35	123.55
341	34.30	33.92	1.59	1.59	44.73	122.28
342	34.40	28.70	1.42	1.42	48.51	121.08
343	34.50	25.40	1.25	1.25	52.18	119.52
344	34.60	20.92	0.96	0.96	56.09	117.63
345	34.70	16.63	0.76	0.76	60.45	115.91
346	34.80	15.71	0.76	0.76	64.53	115.03
347	34.90	15.13	0.77	0.77	66.36	115.00
348	35.00	15.13	0.78	0.78	67.30	115.24
349	35.10	15.54	0.84	0.84	68.13	115.97
350	35.20	16.16	1.00	1.00	67.91	117.28
351	35.30	18.48	1.22	1.22	63.29	119.11
352	35.40	25.08	1.48	1.48	55.41	120.64
353	35.50	31.71	1.53	1.53	46.68	121.88
354	35.60	40.14	1.59	1.59	39.13	122.74
355	35.70	50.05	1.68	1.68	33.50	123.32
356	35.80	56.32	1.61	1.61	29.53	123.45
357	35.90	59.66	1.47	1.47	27.66	123.03
358	36.00	56.36	1.36	1.36	28.38	122.66
359	36.10	49.18	1.45	1.45	32.03	122.45
360	36.20	40.79	1.52	1.52	38.12	122.15
361	36.30	32.02	1.45	1.45	44.90	121.54
362	36.40	27.29	1.37	1.37	49.46	121.00
363	36.50	28.65	1.39	1.39	49.23	121.00
364	36.60	32.59	1.45	1.45	46.44	121.50
365	36.70	35.56	1.53	1.53	44.90	122.07
366	36.80	35.36	1.64	1.64	46.16	122.37
367	36.90	31.38	1.65	1.65	49.80	122.21
368	37.00	26.96	1.57	1.57	53.00	121.80
369	37.10	27.42	1.52	1.52	50.78	121.85
370	37.20	35.85	1.61	1.61	43.20	122.33
371	37.30	46.57	1.57	1.57	35.37	122.94
372	37.40	56.16	1.54	1.54	30.19	123.55
373	37.50	63.66	1.72	1.72	27.51	124.26
374	37.60	68.39	1.84	1.84	25.97	124.79
375	37.70	71.99	1.78	1.78	24.79	124.85
376	37.80	72.87	1.68	1.68	23.96	124.68
377	37.90	72.77	1.69	1.69	23.91	124.62
378	38.00	71.88	1.74	1.74	24.22	124.62
379	38.10	70.77	1.70	1.70	24.23	124.42
380	38.20	70.48	1.57	1.57	23.79	123.96
381	38.30	69.97	1.45	1.45	23.57	123.58
382	38.40	68.11	1.48	1.48	24.25	123.56
383	38.50	65.64	1.60	1.60	25.63	124.03
384	38.60	65.89	1.78	1.78	26.62	124.79

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
385	38.70	70.20	1.99	1.99	26.62	125.63
386	38.80	75.49	2.15	2.15	26.04	126.33
387	38.90	78.96	2.25	2.25	25.58	126.79
388	39.00	80.00	2.31	2.31	25.49	127.06
389	39.10	80.00	2.35	2.35	25.59	127.15
390	39.20	79.68	2.33	2.33	25.39	127.16
391	39.30	81.99	2.30	2.30	24.58	127.11
392	39.40	86.23	2.24	2.24	23.24	127.09
393	39.50	91.35	2.21	2.21	21.77	127.12
394	39.60	96.87	2.20	2.20	20.48	127.21
395	39.70	101.59	2.21	2.21	19.82	127.49
396	39.80	103.90	2.37	2.37	20.94	128.10
397	39.90	94.88	2.81	2.81	24.39	128.71
398	40.00	76.56	3.09	3.09	29.46	128.78
399	40.10	63.55	2.90	2.90	35.63	127.98
400	40.20	48.19	2.51	2.51	41.52	126.77
401	40.30	39.55	2.33	2.33	46.63	125.95
402	40.40	40.66	2.47	2.47	46.85	126.13
403	40.50	49.02	2.67	2.67	42.10	126.83
404	40.60	60.54	2.68	2.68	35.66	127.30
405	40.70	72.21	2.47	2.47	29.86	127.21
406	40.80	80.59	2.17	2.17	25.68	126.80
407	40.90	85.19	2.04	2.04	24.22	127.08
408	41.00	88.46	2.58	2.58	24.05	127.58
409	41.10	89.71	2.56	2.56	23.93	127.81
410	41.20	90.19	2.23	2.23	23.47	127.57
411	41.30	89.19	2.34	2.34	23.56	127.36
412	41.40	85.76	2.39	2.39	24.72	127.42
413	41.50	81.08	2.37	2.37	26.04	127.32
414	41.60	77.00	2.36	2.36	27.49	127.15
415	41.70	72.62	2.35	2.35	29.56	126.95
416	41.80	64.56	2.36	2.36	32.90	126.58
417	41.90	53.26	2.27	2.27	37.93	125.84
418	42.00	41.94	2.06	2.06	44.24	124.50
419	42.10	32.29	1.67	1.67	49.80	122.90
420	42.20	29.31	1.44	1.44	51.80	121.74
421	42.30	31.82	1.46	1.46	51.01	121.60
422	42.40	33.30	1.57	1.57	50.35	121.97
423	42.50	32.60	1.61	1.61	49.71	122.12
424	42.60	34.07	1.52	1.52	46.11	121.99
425	42.70	40.87	1.38	1.38	39.46	121.73
426	42.80	49.10	1.25	1.25	33.33	121.54
427	42.90	54.41	1.21	1.21	30.63	121.86
428	43.00	55.21	1.43	1.43	30.98	122.51
429	43.10	53.11	1.57	1.57	33.32	123.41
430	43.20	51.64	1.80	1.80	35.68	124.23
431	43.30	52.23	2.03	2.03	37.09	124.94
432	43.40	53.62	2.12	2.12	38.29	125.37

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
433	43.50	50.71	2.17	2.17	41.40	125.42
434	43.60	41.20	2.23	2.23	47.52	125.04
435	43.70	32.20	2.13	2.13	55.16	124.62
436	43.80	29.84	2.19	2.19	59.21	124.59
437	43.90	33.24	2.38	2.38	56.61	125.20
438	44.00	40.62	2.51	2.51	49.28	126.12
439	44.10	53.40	2.61	2.61	39.30	127.05
440	44.20	74.80	2.63	2.63	29.83	127.86
441	44.30	100.54	2.58	2.58	23.34	128.82
442	44.40	122.67	2.96	2.96	19.66	129.67
443	44.50	135.35	3.09	3.09	17.89	130.21
444	44.60	139.36	2.93	2.93	16.82	130.18
445	44.70	140.32	2.79	2.79	17.30	130.82
446	44.80	143.09	3.83	3.83	18.81	132.35
447	44.90	153.27	5.03	5.03	18.99	133.41
448	45.00	166.84	4.35	4.35	17.32	133.54
449	45.10	179.58	3.72	3.72	14.90	132.95
450	45.20	188.85	3.74	3.74	13.62	132.64
451	45.30	189.48	3.71	3.71	13.44	132.67
452	45.40	185.74	3.73	3.73	13.61	132.57
453	45.50	181.11	3.64	3.64	13.89	132.41
454	45.60	177.29	3.56	3.56	14.10	132.20
455	45.70	174.19	3.50	3.50	14.27	132.02
456	45.80	171.44	3.44	3.44	14.40	131.90
457	45.90	170.82	3.43	3.43	14.53	131.84
458	46.00	169.67	3.44	3.44	14.71	131.87
459	46.10	168.43	3.50	3.50	14.98	131.98
460	46.20	168.29	3.59	3.59	15.30	132.13
461	46.30	167.59	3.69	3.69	15.56	132.32
462	46.40	168.65	3.78	3.78	15.53	132.45
463	46.50	173.30	3.76	3.76	15.09	132.48
464	46.60	178.80	3.65	3.65	14.32	132.39
465	46.70	184.70	3.53	3.53	13.50	132.22
466	46.80	188.94	3.41	3.41	12.78	131.95
467	46.90	189.52	3.20	3.20	12.14	131.49
468	47.00	187.48	2.90	2.90	11.63	130.89
469	47.10	183.81	2.68	2.68	11.36	130.31
470	47.20	178.60	2.58	2.58	11.39	129.90
471	47.30	173.82	2.52	2.52	11.64	129.68
472	47.40	170.46	2.52	2.52	11.98	129.58
473	47.50	166.99	2.54	2.54	12.34	129.55
474	47.60	164.02	2.53	2.53	12.68	129.53
475	47.70	161.89	2.54	2.54	13.02	129.54
476	47.80	159.80	2.60	2.60	13.32	129.56
477	47.90	157.75	2.58	2.58	13.62	129.65
478	48.00	157.85	2.66	2.66	13.82	129.83
479	48.10	160.73	2.79	2.79	14.02	130.20
480	48.20	163.77	2.95	2.95	14.26	130.61

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
481	48.30	164.50	3.10	3.10	14.61	130.97
482	48.40	163.79	3.22	3.22	14.95	131.25
483	48.50	164.74	3.30	3.30	15.12	131.45
484	48.60	167.31	3.36	3.36	15.08	131.62
485	48.70	169.92	3.41	3.41	14.99	131.77
486	48.80	171.62	3.46	3.46	15.04	131.94
487	48.90	171.70	3.57	3.57	15.40	132.23
488	49.00	171.00	3.83	3.83	16.05	132.65
489	49.10	170.82	4.11	4.11	16.75	133.16
490	49.20	172.60	4.39	4.39	17.11	133.68
491	49.30	180.27	4.66	4.66	16.86	134.13
492	49.40	191.35	4.76	4.76	16.06	134.45
493	49.50	203.17	4.76	4.76	14.99	134.61
494	49.60	214.00	4.69	4.69	13.97	134.59
495	49.70	220.20	4.52	4.52	13.11	134.46
496	49.80	224.41	4.36	4.36	12.62	134.32

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q _c :	Measured cone resistance (tsf)
f _s :	Sleeve friction resistance (tsf)
u:	Pore pressure (tsf)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (pcf)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1	0.30	0.02	0.00	0.02	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
2	0.40	0.03	0.00	0.03	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
3	0.50	0.03	0.00	0.03	1.00	0.481	1.06	0.456	1.00	1.30	2.000	No
4	0.60	0.04	0.00	0.04	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
5	0.70	0.04	0.00	0.04	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
6	0.80	0.05	0.00	0.05	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
7	0.90	0.06	0.00	0.06	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
8	1.00	0.06	0.00	0.06	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
9	1.10	0.07	0.00	0.07	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
10	1.20	0.08	0.00	0.08	1.00	0.481	1.06	0.455	1.00	1.30	2.000	No
11	1.30	0.08	0.00	0.08	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
12	1.40	0.09	0.00	0.09	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
13	1.50	0.09	0.00	0.09	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
14	1.60	0.10	0.00	0.10	1.00	0.480	1.06	0.455	1.00	1.30	2.000	No
15	1.70	0.11	0.00	0.11	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
16	1.80	0.11	0.00	0.11	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
17	1.90	0.12	0.00	0.12	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
18	2.00	0.12	0.00	0.12	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
19	2.10	0.13	0.00	0.13	1.00	0.480	1.06	0.454	1.00	1.30	2.000	No
20	2.20	0.13	0.00	0.13	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
21	2.30	0.14	0.00	0.14	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
22	2.40	0.14	0.00	0.14	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
23	2.50	0.15	0.00	0.15	1.00	0.479	1.06	0.454	1.00	1.30	2.000	No
24	2.60	0.16	0.00	0.16	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
25	2.70	0.16	0.00	0.16	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
26	2.80	0.17	0.00	0.17	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
27	2.90	0.17	0.00	0.17	1.00	0.479	1.06	0.453	1.00	1.30	2.000	No
28	3.00	0.18	0.00	0.18	0.99	0.479	1.06	0.453	1.00	1.30	2.000	Yes
29	3.10	0.18	0.00	0.18	0.99	0.478	1.06	0.453	1.00	1.30	2.000	Yes
30	3.20	0.19	0.00	0.19	0.99	0.478	1.06	0.453	1.00	1.30	2.000	Yes
31	3.30	0.19	0.00	0.19	0.99	0.478	1.06	0.453	1.00	1.30	2.000	Yes
32	3.40	0.20	0.00	0.20	0.99	0.478	1.06	0.453	1.00	1.30	2.000	Yes
33	3.50	0.20	0.00	0.20	0.99	0.478	1.06	0.452	1.00	1.30	2.000	Yes
34	3.60	0.21	0.00	0.21	0.99	0.478	1.06	0.452	1.00	1.30	2.000	Yes
35	3.70	0.22	0.00	0.22	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
36	3.80	0.22	0.00	0.22	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
37	3.90	0.23	0.00	0.23	0.99	0.478	1.06	0.452	1.00	1.30	2.000	No
38	4.00	0.23	0.00	0.23	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
39	4.10	0.24	0.00	0.24	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
40	4.20	0.24	0.00	0.24	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
41	4.30	0.25	0.00	0.25	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
42	4.40	0.26	0.00	0.26	0.99	0.477	1.06	0.452	1.00	1.30	2.000	No
43	4.50	0.26	0.00	0.26	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
44	4.60	0.27	0.00	0.27	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
45	4.70	0.27	0.00	0.27	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
46	4.80	0.28	0.00	0.28	0.99	0.477	1.06	0.451	1.00	1.30	2.000	No
47	4.90	0.28	0.00	0.28	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
48	5.00	0.29	0.00	0.29	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
49	5.10	0.29	0.00	0.29	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
50	5.20	0.30	0.00	0.30	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
51	5.30	0.30	0.00	0.30	0.99	0.476	1.06	0.451	1.00	1.30	2.000	No
52	5.40	0.31	0.00	0.31	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
53	5.50	0.31	0.00	0.31	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
54	5.60	0.32	0.00	0.32	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
55	5.70	0.32	0.00	0.32	0.99	0.476	1.06	0.450	1.00	1.30	2.000	No
56	5.80	0.33	0.00	0.33	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
57	5.90	0.33	0.00	0.33	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
58	6.00	0.34	0.00	0.34	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
59	6.10	0.34	0.00	0.34	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
60	6.20	0.35	0.00	0.35	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
61	6.30	0.35	0.00	0.35	0.99	0.475	1.06	0.450	1.00	1.30	2.000	No
62	6.40	0.36	0.00	0.36	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
63	6.50	0.36	0.00	0.36	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
64	6.60	0.37	0.00	0.37	0.99	0.475	1.06	0.449	1.00	1.30	2.000	No
65	6.70	0.37	0.00	0.37	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
66	6.80	0.38	0.00	0.38	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
67	6.90	0.38	0.00	0.38	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
68	7.00	0.39	0.00	0.39	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
69	7.10	0.39	0.00	0.39	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
70	7.20	0.40	0.00	0.40	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
71	7.30	0.40	0.00	0.40	0.99	0.474	1.06	0.449	1.00	1.30	2.000	No
72	7.40	0.41	0.00	0.41	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
73	7.50	0.42	0.00	0.42	0.98	0.474	1.06	0.448	1.00	1.30	2.000	No
74	7.60	0.42	0.00	0.42	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
75	7.70	0.43	0.00	0.43	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
76	7.80	0.43	0.00	0.43	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
77	7.90	0.44	0.00	0.44	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
78	8.00	0.44	0.00	0.44	0.98	0.473	1.06	0.448	1.00	1.30	2.000	No
79	8.10	0.45	0.00	0.45	0.98	0.476	1.06	0.451	1.00	1.30	0.586	No
80	8.20	0.46	0.01	0.45	0.98	0.479	1.06	0.454	1.00	1.30	0.590	No
81	8.30	0.46	0.01	0.45	0.98	0.483	1.06	0.457	1.00	1.30	0.594	No
82	8.40	0.47	0.01	0.46	0.98	0.486	1.06	0.460	1.00	1.30	0.598	No
83	8.50	0.47	0.02	0.46	0.98	0.489	1.06	0.463	1.00	1.30	0.601	No
84	8.60	0.48	0.02	0.46	0.98	0.492	1.06	0.465	1.00	1.30	0.605	No
85	8.70	0.48	0.02	0.46	0.98	0.495	1.06	0.468	1.00	1.30	0.609	No
86	8.80	0.49	0.02	0.46	0.98	0.498	1.06	0.471	1.00	1.30	0.612	No
87	8.90	0.50	0.03	0.47	0.98	0.500	1.06	0.474	1.00	1.30	0.616	No
88	9.00	0.50	0.03	0.47	0.98	0.503	1.06	0.476	1.00	1.30	0.619	No
89	9.10	0.51	0.03	0.47	0.98	0.506	1.06	0.479	1.00	1.30	0.623	No
90	9.20	0.51	0.04	0.47	0.98	0.509	1.06	0.482	1.00	1.30	0.626	No
91	9.30	0.52	0.04	0.48	0.98	0.512	1.06	0.484	1.00	1.30	0.630	No
92	9.40	0.52	0.04	0.48	0.98	0.515	1.06	0.487	1.00	1.30	0.633	No
93	9.50	0.53	0.05	0.48	0.98	0.517	1.06	0.490	1.00	1.30	0.637	No
94	9.60	0.53	0.05	0.48	0.98	0.520	1.06	0.492	1.00	1.30	0.640	No
95	9.70	0.54	0.05	0.49	0.98	0.523	1.06	0.495	1.00	1.30	0.643	No
96	9.80	0.55	0.06	0.49	0.98	0.525	1.06	0.497	1.00	1.30	0.646	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
97	9.90	0.55	0.06	0.49	0.98	0.528	1.06	0.500	1.00	1.30	0.650	No
98	10.00	0.56	0.06	0.49	0.98	0.530	1.06	0.502	1.00	1.30	0.653	No
99	10.10	0.56	0.07	0.50	0.98	0.533	1.06	0.504	1.00	1.30	0.656	No
100	10.20	0.57	0.07	0.50	0.98	0.535	1.06	0.507	1.00	1.30	0.659	No
101	10.30	0.57	0.07	0.50	0.98	0.538	1.06	0.509	1.00	1.30	0.662	No
102	10.40	0.58	0.07	0.50	0.98	0.540	1.06	0.512	1.00	1.30	0.665	No
103	10.50	0.58	0.08	0.51	0.98	0.543	1.06	0.514	1.00	1.30	0.668	No
104	10.60	0.59	0.08	0.51	0.98	0.546	1.06	0.516	1.00	1.30	0.671	No
105	10.70	0.59	0.08	0.51	0.98	0.548	1.06	0.519	1.00	1.30	0.674	No
106	10.80	0.60	0.09	0.51	0.98	0.550	1.06	0.521	1.00	1.30	0.677	No
107	10.90	0.60	0.09	0.51	0.98	0.553	1.06	0.523	1.00	1.30	0.680	No
108	11.00	0.61	0.09	0.51	0.98	0.555	1.06	0.526	1.00	1.30	0.683	No
109	11.10	0.61	0.10	0.52	0.98	0.558	1.06	0.528	1.00	1.30	0.686	No
110	11.20	0.62	0.10	0.52	0.98	0.560	1.06	0.530	1.00	1.30	0.689	No
111	11.30	0.62	0.10	0.52	0.98	0.563	1.06	0.533	1.00	1.30	0.692	No
112	11.40	0.63	0.11	0.52	0.98	0.565	1.06	0.535	1.00	1.30	0.695	No
113	11.50	0.63	0.11	0.52	0.98	0.567	1.06	0.537	1.00	1.30	0.698	No
114	11.60	0.64	0.11	0.53	0.98	0.569	1.06	0.539	1.00	1.30	0.701	No
115	11.70	0.64	0.12	0.53	0.98	0.572	1.06	0.541	1.00	1.30	0.703	No
116	11.80	0.65	0.12	0.53	0.98	0.574	1.06	0.543	1.00	1.30	0.706	No
117	11.90	0.66	0.12	0.53	0.98	0.576	1.06	0.545	1.00	1.30	0.709	No
118	12.00	0.66	0.12	0.54	0.97	0.578	1.06	0.547	1.00	1.30	0.711	No
119	12.10	0.67	0.13	0.54	0.97	0.580	1.06	0.549	1.00	1.30	0.714	No
120	12.20	0.67	0.13	0.54	0.97	0.582	1.06	0.551	1.00	1.30	0.716	No
121	12.30	0.68	0.13	0.54	0.97	0.584	1.06	0.553	1.00	1.30	0.719	No
122	12.40	0.68	0.14	0.55	0.97	0.586	1.06	0.555	1.00	1.30	0.721	No
123	12.50	0.69	0.14	0.55	0.97	0.588	1.06	0.557	1.00	1.30	0.724	No
124	12.60	0.69	0.14	0.55	0.97	0.590	1.06	0.559	1.00	1.30	0.727	No
125	12.70	0.70	0.15	0.55	0.97	0.593	1.06	0.561	1.00	1.30	0.729	No
126	12.80	0.70	0.15	0.55	0.97	0.595	1.06	0.563	1.00	1.30	0.732	No
127	12.90	0.71	0.15	0.56	0.97	0.597	1.06	0.565	1.00	1.30	0.735	No
128	13.00	0.71	0.16	0.56	0.97	0.599	1.06	0.567	1.00	1.30	0.737	No
129	13.10	0.72	0.16	0.56	0.97	0.601	1.06	0.569	1.00	1.30	0.740	No
130	13.20	0.72	0.16	0.56	0.97	0.603	1.06	0.571	1.00	1.30	0.742	No
131	13.30	0.73	0.17	0.56	0.97	0.605	1.06	0.573	1.00	1.30	0.745	No
132	13.40	0.73	0.17	0.56	0.97	0.607	1.06	0.575	1.00	1.30	0.747	No
133	13.50	0.74	0.17	0.57	0.97	0.609	1.06	0.577	1.00	1.30	0.750	No
134	13.60	0.74	0.17	0.57	0.97	0.611	1.06	0.578	1.00	1.30	0.752	No
135	13.70	0.75	0.18	0.57	0.97	0.613	1.06	0.580	1.00	1.30	0.754	No
136	13.80	0.75	0.18	0.57	0.97	0.615	1.06	0.582	1.00	1.30	0.756	No
137	13.90	0.76	0.18	0.58	0.97	0.616	1.06	0.584	1.00	1.30	0.759	No
138	14.00	0.76	0.19	0.58	0.97	0.618	1.06	0.585	1.00	1.30	0.761	No
139	14.10	0.77	0.19	0.58	0.97	0.620	1.06	0.587	1.00	1.30	0.763	No
140	14.20	0.78	0.19	0.58	0.97	0.622	1.06	0.589	1.00	1.30	2.000	Yes
141	14.30	0.78	0.20	0.59	0.97	0.623	1.06	0.590	1.00	1.30	2.000	Yes
142	14.40	0.79	0.20	0.59	0.97	0.625	1.06	0.592	1.00	1.30	2.000	Yes
143	14.50	0.79	0.20	0.59	0.97	0.627	1.06	0.593	1.00	1.30	2.000	Yes
144	14.60	0.80	0.21	0.59	0.97	0.628	1.06	0.595	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
145	14.70	0.81	0.21	0.60	0.97	0.630	1.06	0.596	1.00	1.30	2.000	Yes
146	14.80	0.81	0.21	0.60	0.97	0.631	1.06	0.598	1.00	1.30	2.000	Yes
147	14.90	0.82	0.22	0.60	0.97	0.633	1.06	0.599	1.00	1.30	2.000	Yes
148	15.00	0.82	0.22	0.60	0.97	0.634	1.06	0.600	1.00	1.30	2.000	Yes
149	15.10	0.83	0.22	0.61	0.97	0.636	1.06	0.602	1.00	1.30	2.000	Yes
150	15.20	0.83	0.22	0.61	0.97	0.637	1.06	0.603	1.00	1.30	2.000	Yes
151	15.30	0.84	0.23	0.61	0.97	0.639	1.06	0.605	1.00	1.30	2.000	Yes
152	15.40	0.85	0.23	0.61	0.97	0.640	1.06	0.606	1.00	1.30	2.000	Yes
153	15.50	0.85	0.23	0.62	0.97	0.642	1.06	0.608	1.00	1.30	2.000	Yes
154	15.60	0.86	0.24	0.62	0.97	0.644	1.06	0.609	1.00	1.30	2.000	Yes
155	15.70	0.86	0.24	0.62	0.97	0.645	1.06	0.611	1.00	1.30	2.000	Yes
156	15.80	0.87	0.24	0.62	0.97	0.647	1.06	0.612	1.00	1.30	0.796	No
157	15.90	0.87	0.25	0.62	0.97	0.649	1.06	0.614	1.00	1.30	0.798	No
158	16.00	0.87	0.25	0.63	0.97	0.650	1.06	0.616	1.00	1.30	0.800	No
159	16.10	0.88	0.25	0.63	0.97	0.652	1.06	0.617	1.00	1.30	0.803	No
160	16.20	0.88	0.26	0.63	0.97	0.654	1.06	0.619	1.00	1.30	0.805	No
161	16.30	0.89	0.26	0.63	0.97	0.656	1.06	0.621	1.00	1.30	0.807	No
162	16.40	0.89	0.26	0.63	0.97	0.658	1.06	0.622	1.00	1.30	0.809	No
163	16.50	0.90	0.27	0.63	0.97	0.659	1.06	0.624	1.00	1.30	0.811	No
164	16.60	0.90	0.27	0.63	0.97	0.661	1.06	0.626	1.00	1.30	0.813	No
165	16.70	0.91	0.27	0.63	0.96	0.663	1.06	0.627	1.00	1.30	0.815	No
166	16.80	0.91	0.27	0.64	0.96	0.664	1.06	0.629	1.00	1.30	0.818	No
167	16.90	0.91	0.28	0.64	0.96	0.666	1.06	0.631	1.00	1.30	0.820	No
168	17.00	0.92	0.28	0.64	0.96	0.668	1.06	0.632	1.00	1.30	0.822	No
169	17.10	0.92	0.28	0.64	0.96	0.669	1.06	0.634	1.00	1.30	0.824	No
170	17.20	0.93	0.29	0.64	0.96	0.671	1.06	0.635	1.00	1.30	0.826	No
171	17.30	0.93	0.29	0.64	0.96	0.672	1.06	0.637	1.00	1.30	0.828	No
172	17.40	0.94	0.29	0.65	0.96	0.674	1.06	0.638	1.00	1.30	0.829	No
173	17.50	0.94	0.30	0.65	0.96	0.675	1.06	0.639	1.00	1.30	0.831	No
174	17.60	0.95	0.30	0.65	0.96	0.677	1.06	0.640	1.00	1.30	0.833	No
175	17.70	0.95	0.30	0.65	0.96	0.678	1.06	0.642	1.00	1.30	0.834	No
176	17.80	0.96	0.31	0.65	0.96	0.679	1.06	0.643	1.00	1.30	0.836	No
177	17.90	0.97	0.31	0.66	0.96	0.680	1.06	0.644	1.00	1.30	0.837	No
178	18.00	0.97	0.31	0.66	0.96	0.682	1.06	0.645	1.00	1.30	0.839	No
179	18.10	0.98	0.32	0.66	0.96	0.683	1.06	0.646	1.00	1.30	0.840	No
180	18.20	0.98	0.32	0.66	0.96	0.684	1.06	0.648	1.00	1.30	0.842	No
181	18.30	0.99	0.32	0.67	0.96	0.685	1.06	0.649	1.00	1.30	0.844	No
182	18.40	0.99	0.32	0.67	0.96	0.687	1.06	0.650	1.00	1.30	0.845	No
183	18.50	1.00	0.33	0.67	0.96	0.688	1.06	0.651	1.00	1.30	0.847	No
184	18.60	1.00	0.33	0.67	0.96	0.689	1.06	0.653	1.00	1.30	0.848	No
185	18.70	1.01	0.33	0.67	0.96	0.691	1.06	0.654	1.00	1.30	0.850	No
186	18.80	1.01	0.34	0.68	0.96	0.692	1.06	0.655	1.00	1.30	0.851	No
187	18.90	1.02	0.34	0.68	0.96	0.693	1.06	0.656	1.00	1.30	0.853	No
188	19.00	1.02	0.34	0.68	0.96	0.694	1.06	0.657	1.00	1.30	0.855	No
189	19.10	1.03	0.35	0.68	0.96	0.696	1.06	0.659	1.00	1.30	0.856	No
190	19.20	1.03	0.35	0.68	0.96	0.697	1.06	0.660	1.00	1.30	0.858	No
191	19.30	1.04	0.35	0.69	0.96	0.698	1.06	0.661	1.00	1.30	0.859	No
192	19.40	1.04	0.36	0.69	0.96	0.700	1.06	0.662	1.00	1.30	0.861	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
193	19.50	1.05	0.36	0.69	0.96	0.701	1.06	0.663	1.00	1.30	0.862	No
194	19.60	1.05	0.36	0.69	0.96	0.702	1.06	0.664	1.00	1.30	0.864	No
195	19.70	1.06	0.37	0.69	0.96	0.703	1.06	0.666	1.00	1.30	0.865	No
196	19.80	1.06	0.37	0.70	0.96	0.704	1.06	0.667	1.00	1.30	0.866	No
197	19.90	1.07	0.37	0.70	0.96	0.705	1.06	0.667	1.00	1.30	0.868	No
198	20.00	1.08	0.37	0.70	0.96	0.706	1.06	0.668	1.00	1.30	0.869	No
199	20.10	1.08	0.38	0.70	0.96	0.707	1.06	0.669	1.00	1.30	0.870	No
200	20.20	1.09	0.38	0.71	0.96	0.708	1.06	0.670	1.00	1.30	0.871	No
201	20.30	1.09	0.38	0.71	0.96	0.709	1.06	0.671	1.00	1.30	0.873	No
202	20.40	1.10	0.39	0.71	0.96	0.710	1.06	0.672	1.00	1.30	0.874	No
203	20.50	1.10	0.39	0.71	0.96	0.711	1.06	0.673	1.00	1.30	0.875	No
204	20.60	1.11	0.39	0.71	0.96	0.713	1.06	0.675	1.00	1.30	0.877	No
205	20.70	1.11	0.40	0.72	0.96	0.714	1.06	0.676	1.00	1.30	0.878	No
206	20.80	1.12	0.40	0.72	0.95	0.715	1.06	0.677	1.00	1.30	0.880	No
207	20.90	1.12	0.40	0.72	0.95	0.716	1.06	0.678	1.00	1.30	0.881	No
208	21.00	1.13	0.41	0.72	0.95	0.717	1.06	0.678	1.00	1.30	0.882	No
209	21.10	1.13	0.41	0.72	0.95	0.718	1.06	0.679	1.00	1.30	0.883	No
210	21.20	1.14	0.41	0.73	0.95	0.718	1.06	0.680	1.00	1.30	0.884	No
211	21.30	1.14	0.41	0.73	0.95	0.719	1.06	0.681	1.00	1.30	0.885	No
212	21.40	1.15	0.42	0.73	0.95	0.720	1.06	0.682	1.00	1.30	0.886	No
213	21.50	1.16	0.42	0.73	0.95	0.721	1.06	0.683	1.00	1.30	0.887	No
214	21.60	1.16	0.42	0.74	0.95	0.722	1.06	0.683	1.00	1.30	0.888	No
215	21.70	1.17	0.43	0.74	0.95	0.723	1.06	0.684	1.00	1.30	0.889	No
216	21.80	1.17	0.43	0.74	0.95	0.724	1.06	0.685	1.00	1.30	0.891	No
217	21.90	1.18	0.43	0.74	0.95	0.725	1.06	0.686	1.00	1.30	0.892	No
218	22.00	1.18	0.44	0.75	0.95	0.726	1.06	0.687	1.00	1.30	0.893	No
219	22.10	1.19	0.44	0.75	0.95	0.726	1.06	0.688	1.00	1.30	0.894	No
220	22.20	1.19	0.44	0.75	0.95	0.727	1.06	0.689	1.00	1.30	0.895	No
221	22.30	1.20	0.45	0.75	0.95	0.728	1.06	0.689	1.00	1.30	0.896	No
222	22.40	1.20	0.45	0.75	0.95	0.729	1.06	0.690	1.00	1.30	0.897	No
223	22.50	1.21	0.45	0.76	0.95	0.730	1.06	0.691	1.00	1.30	0.898	No
224	22.60	1.22	0.46	0.76	0.95	0.731	1.06	0.692	1.00	1.30	0.899	No
225	22.70	1.22	0.46	0.76	0.95	0.732	1.06	0.692	1.00	1.30	0.900	No
226	22.80	1.23	0.46	0.76	0.95	0.732	1.06	0.693	1.00	1.30	0.901	No
227	22.90	1.23	0.46	0.77	0.95	0.733	1.06	0.694	1.00	1.30	0.902	No
228	23.00	1.24	0.47	0.77	0.95	0.734	1.06	0.695	1.00	1.30	0.903	No
229	23.10	1.24	0.47	0.77	0.95	0.735	1.06	0.696	1.00	1.30	0.904	No
230	23.20	1.25	0.47	0.77	0.95	0.736	1.06	0.696	1.00	1.30	0.905	No
231	23.30	1.25	0.48	0.78	0.95	0.736	1.06	0.697	1.00	1.30	0.906	No
232	23.40	1.26	0.48	0.78	0.95	0.737	1.06	0.698	1.00	1.30	0.907	No
233	23.50	1.26	0.48	0.78	0.95	0.738	1.06	0.698	1.00	1.30	0.908	No
234	23.60	1.27	0.49	0.78	0.95	0.738	1.06	0.699	1.00	1.30	0.909	No
235	23.70	1.27	0.49	0.78	0.95	0.739	1.06	0.700	1.00	1.30	0.910	No
236	23.80	1.28	0.49	0.79	0.95	0.740	1.06	0.700	1.00	1.30	0.911	No
237	23.90	1.29	0.50	0.79	0.95	0.741	1.06	0.701	1.00	1.30	0.911	No
238	24.00	1.29	0.50	0.79	0.95	0.741	1.06	0.702	1.00	1.30	0.912	No
239	24.10	1.30	0.50	0.79	0.94	0.742	1.06	0.702	1.00	1.30	0.913	No
240	24.20	1.30	0.51	0.80	0.94	0.742	1.06	0.703	1.00	1.30	0.913	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
241	24.30	1.31	0.51	0.80	0.94	0.743	1.06	0.703	1.00	1.30	0.914	No
242	24.40	1.31	0.51	0.80	0.94	0.743	1.06	0.704	1.00	1.30	0.915	No
243	24.50	1.32	0.51	0.81	0.94	0.744	1.06	0.704	1.00	1.30	0.915	No
244	24.60	1.33	0.52	0.81	0.94	0.744	1.06	0.705	1.00	1.30	0.916	No
245	24.70	1.33	0.52	0.81	0.94	0.745	1.06	0.705	1.00	1.30	0.917	No
246	24.80	1.34	0.52	0.81	0.94	0.745	1.06	0.706	1.00	1.30	0.917	No
247	24.90	1.34	0.53	0.82	0.94	0.746	1.06	0.706	1.00	1.30	0.918	No
248	25.00	1.35	0.53	0.82	0.94	0.746	1.06	0.706	1.00	1.30	0.918	No
249	25.10	1.36	0.53	0.82	0.94	0.747	1.06	0.707	1.00	1.30	0.919	No
250	25.20	1.36	0.54	0.82	0.94	0.747	1.06	0.707	1.00	1.30	0.920	No
251	25.30	1.37	0.54	0.83	0.94	0.748	1.06	0.708	1.00	1.30	0.920	No
252	25.40	1.37	0.54	0.83	0.94	0.748	1.06	0.708	1.00	1.30	0.921	No
253	25.50	1.38	0.55	0.83	0.94	0.748	1.06	0.709	1.00	1.30	2.000	Yes
254	25.60	1.39	0.55	0.84	0.94	0.749	1.06	0.709	1.00	1.30	2.000	Yes
255	25.70	1.39	0.55	0.84	0.94	0.749	1.06	0.709	1.00	1.30	2.000	Yes
256	25.80	1.40	0.56	0.84	0.94	0.749	1.06	0.709	1.00	1.30	2.000	Yes
257	25.90	1.40	0.56	0.85	0.94	0.749	1.06	0.709	1.00	1.30	2.000	Yes
258	26.00	1.41	0.56	0.85	0.94	0.750	1.06	0.710	1.00	1.30	2.000	Yes
259	26.10	1.42	0.56	0.85	0.94	0.750	1.06	0.710	1.00	1.30	2.000	Yes
260	26.20	1.42	0.57	0.86	0.94	0.750	1.06	0.710	1.00	1.30	2.000	Yes
261	26.30	1.43	0.57	0.86	0.94	0.750	1.06	0.710	1.00	1.30	0.923	No
262	26.40	1.44	0.57	0.86	0.94	0.750	1.06	0.710	1.00	1.30	0.923	No
263	26.50	1.44	0.58	0.87	0.94	0.750	1.06	0.710	1.00	1.30	0.923	No
264	26.60	1.45	0.58	0.87	0.94	0.751	1.06	0.710	1.00	1.30	0.924	No
265	26.70	1.46	0.58	0.87	0.94	0.751	1.06	0.711	1.00	1.30	0.924	No
266	26.80	1.46	0.59	0.88	0.94	0.751	1.06	0.711	1.00	1.30	0.924	No
267	26.90	1.47	0.59	0.88	0.93	0.751	1.06	0.711	1.00	1.30	0.924	No
268	27.00	1.48	0.59	0.88	0.93	0.751	1.06	0.711	1.00	1.30	0.924	No
269	27.10	1.48	0.60	0.89	0.93	0.751	1.06	0.711	1.00	1.30	0.924	No
270	27.20	1.49	0.60	0.89	0.93	0.751	1.06	0.711	1.00	1.30	0.925	No
271	27.30	1.50	0.60	0.89	0.93	0.751	1.06	0.711	1.00	1.30	0.925	No
272	27.40	1.50	0.61	0.90	0.93	0.752	1.06	0.711	1.00	1.30	0.925	No
273	27.50	1.51	0.61	0.90	0.93	0.752	1.06	0.712	1.00	1.30	0.925	No
274	27.60	1.51	0.61	0.90	0.93	0.752	1.06	0.712	1.00	1.30	0.925	No
275	27.70	1.52	0.61	0.91	0.93	0.752	1.06	0.712	1.00	1.30	0.925	No
276	27.80	1.53	0.62	0.91	0.93	0.752	1.06	0.712	1.00	1.30	0.926	No
277	27.90	1.53	0.62	0.91	0.93	0.752	1.06	0.712	1.00	1.30	0.926	No
278	28.00	1.54	0.62	0.91	0.93	0.752	1.06	0.712	1.00	1.30	0.926	No
279	28.10	1.54	0.63	0.92	0.93	0.753	1.06	0.712	1.00	1.30	0.926	No
280	28.20	1.55	0.63	0.92	0.93	0.753	1.06	0.713	1.00	1.30	0.926	No
281	28.30	1.56	0.63	0.92	0.93	0.753	1.06	0.713	1.00	1.30	0.927	No
282	28.40	1.56	0.64	0.93	0.93	0.753	1.06	0.713	1.00	1.30	0.927	No
283	28.50	1.57	0.64	0.93	0.93	0.753	1.06	0.713	1.00	1.30	0.927	No
284	28.60	1.58	0.64	0.93	0.93	0.753	1.06	0.713	1.00	1.30	0.927	No
285	28.70	1.58	0.65	0.94	0.93	0.753	1.06	0.713	1.00	1.30	0.927	No
286	28.80	1.59	0.65	0.94	0.93	0.753	1.06	0.713	1.00	1.30	0.927	No
287	28.90	1.60	0.65	0.94	0.93	0.753	1.06	0.713	1.00	1.30	0.927	No
288	29.00	1.60	0.66	0.95	0.93	0.753	1.06	0.713	1.00	1.30	0.927	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
289	29.10	1.61	0.66	0.95	0.92	0.753	1.06	0.713	1.00	1.30	0.927	No
290	29.20	1.62	0.66	0.95	0.92	0.753	1.06	0.713	1.00	1.30	0.927	No
291	29.30	1.62	0.66	0.96	0.92	0.753	1.06	0.713	1.00	1.30	0.927	No
292	29.40	1.63	0.67	0.96	0.92	0.753	1.06	0.713	1.00	1.30	0.927	No
293	29.50	1.63	0.67	0.96	0.92	0.753	1.06	0.713	1.00	1.30	0.927	No
294	29.60	1.64	0.67	0.97	0.92	0.753	1.06	0.713	1.00	1.30	0.927	No
295	29.70	1.65	0.68	0.97	0.92	0.753	1.06	0.713	1.00	1.30	0.927	No
296	29.80	1.65	0.68	0.97	0.92	0.753	1.06	0.713	1.00	1.30	0.926	No
297	29.90	1.66	0.68	0.98	0.92	0.753	1.06	0.713	1.00	1.30	0.926	No
298	30.00	1.67	0.69	0.98	0.92	0.753	1.06	0.713	1.00	1.30	0.926	No
299	30.10	1.67	0.69	0.98	0.92	0.753	1.06	0.712	1.00	1.30	0.926	No
300	30.20	1.68	0.69	0.99	0.92	0.753	1.06	0.712	1.00	1.30	0.926	No
301	30.30	1.69	0.70	0.99	0.92	0.752	1.06	0.712	1.00	1.30	0.926	No
302	30.40	1.69	0.70	0.99	0.92	0.752	1.06	0.712	1.00	1.30	0.926	No
303	30.50	1.70	0.70	1.00	0.92	0.752	1.06	0.712	1.00	1.30	0.926	No
304	30.60	1.71	0.71	1.00	0.92	0.752	1.06	0.712	1.00	1.30	0.926	No
305	30.70	1.71	0.71	1.00	0.92	0.752	1.06	0.712	1.00	1.30	0.926	No
306	30.80	1.72	0.71	1.01	0.92	0.752	1.06	0.712	1.00	1.30	0.925	No
307	30.90	1.73	0.71	1.01	0.92	0.752	1.06	0.712	1.00	1.30	0.925	No
308	31.00	1.73	0.72	1.01	0.92	0.752	1.06	0.712	1.00	1.30	0.925	No
309	31.10	1.74	0.72	1.02	0.91	0.752	1.06	0.712	1.00	1.30	0.925	No
310	31.20	1.74	0.72	1.02	0.91	0.752	1.06	0.711	1.00	1.30	0.925	No
311	31.30	1.75	0.73	1.02	0.91	0.751	1.06	0.711	1.00	1.30	0.925	No
312	31.40	1.76	0.73	1.03	0.91	0.751	1.06	0.711	1.00	1.30	0.924	No
313	31.50	1.76	0.73	1.03	0.91	0.751	1.06	0.711	1.00	1.30	0.924	No
314	31.60	1.77	0.74	1.03	0.91	0.751	1.06	0.711	1.00	1.30	0.924	No
315	31.70	1.78	0.74	1.04	0.91	0.751	1.06	0.711	1.00	1.30	0.924	No
316	31.80	1.78	0.74	1.04	0.91	0.751	1.06	0.711	1.00	1.30	0.924	No
317	31.90	1.79	0.75	1.04	0.91	0.750	1.06	0.710	1.00	1.30	0.924	No
318	32.00	1.80	0.75	1.05	0.91	0.750	1.06	0.710	1.00	1.30	2.000	Yes
319	32.10	1.80	0.75	1.05	0.91	0.750	1.06	0.710	1.00	1.30	2.000	Yes
320	32.20	1.81	0.76	1.05	0.91	0.750	1.06	0.710	1.00	1.30	2.000	Yes
321	32.30	1.82	0.76	1.06	0.91	0.750	1.06	0.710	1.00	1.30	2.000	Yes
322	32.40	1.82	0.76	1.06	0.91	0.750	1.06	0.710	1.00	1.30	2.000	Yes
323	32.50	1.83	0.76	1.06	0.91	0.750	1.06	0.710	1.00	1.30	2.000	Yes
324	32.60	1.83	0.77	1.07	0.91	0.749	1.06	0.709	1.00	1.30	2.000	Yes
325	32.70	1.84	0.77	1.07	0.91	0.749	1.06	0.709	1.00	1.30	0.922	No
326	32.80	1.85	0.77	1.07	0.90	0.749	1.06	0.709	1.00	1.30	0.922	No
327	32.90	1.85	0.78	1.08	0.90	0.749	1.06	0.709	1.00	1.30	0.922	No
328	33.00	1.86	0.78	1.08	0.90	0.749	1.06	0.709	1.00	1.30	0.921	No
329	33.10	1.87	0.78	1.08	0.90	0.748	1.06	0.708	1.00	1.30	0.921	No
330	33.20	1.87	0.79	1.09	0.90	0.748	1.06	0.708	1.00	1.30	0.921	No
331	33.30	1.88	0.79	1.09	0.90	0.748	1.06	0.708	1.00	1.30	0.920	No
332	33.40	1.89	0.79	1.09	0.90	0.748	1.06	0.708	1.00	1.30	0.920	No
333	33.50	1.89	0.80	1.10	0.90	0.747	1.06	0.707	1.00	1.30	0.920	No
334	33.60	1.90	0.80	1.10	0.90	0.747	1.06	0.707	1.00	1.30	0.919	No
335	33.70	1.91	0.80	1.10	0.90	0.747	1.06	0.707	1.00	1.30	0.919	No
336	33.80	1.91	0.80	1.11	0.90	0.746	1.06	0.707	1.00	1.30	0.919	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
337	33.90	1.92	0.81	1.11	0.90	0.746	1.06	0.706	1.00	1.30	0.918	No
338	34.00	1.93	0.81	1.11	0.90	0.746	1.06	0.706	1.00	1.30	0.918	No
339	34.10	1.93	0.81	1.12	0.90	0.746	1.06	0.706	1.00	1.30	0.918	No
340	34.20	1.94	0.82	1.12	0.90	0.746	1.06	0.706	1.00	1.30	0.917	No
341	34.30	1.94	0.82	1.12	0.90	0.745	1.06	0.706	1.00	1.30	0.917	No
342	34.40	1.95	0.82	1.13	0.89	0.745	1.06	0.705	1.00	1.30	0.917	No
343	34.50	1.96	0.83	1.13	0.89	0.745	1.06	0.705	1.00	1.30	0.917	No
344	34.60	1.96	0.83	1.13	0.89	0.745	1.06	0.705	1.00	1.30	0.917	No
345	34.70	1.97	0.83	1.13	0.89	0.745	1.06	0.705	1.00	1.30	0.916	No
346	34.80	1.97	0.84	1.14	0.89	0.745	1.06	0.705	1.00	1.30	0.916	No
347	34.90	1.98	0.84	1.14	0.89	0.744	1.06	0.705	1.00	1.30	0.916	No
348	35.00	1.98	0.84	1.14	0.89	0.744	1.06	0.705	1.00	1.30	0.916	No
349	35.10	1.99	0.85	1.14	0.89	0.744	1.06	0.704	1.00	1.30	0.916	No
350	35.20	2.00	0.85	1.15	0.89	0.744	1.06	0.704	1.00	1.30	0.916	No
351	35.30	2.00	0.85	1.15	0.89	0.744	1.06	0.704	1.00	1.30	0.915	No
352	35.40	2.01	0.85	1.15	0.89	0.744	1.06	0.704	1.00	1.30	2.000	Yes
353	35.50	2.01	0.86	1.16	0.89	0.743	1.06	0.704	1.00	1.30	2.000	Yes
354	35.60	2.02	0.86	1.16	0.89	0.743	1.06	0.703	1.00	1.30	2.000	Yes
355	35.70	2.03	0.86	1.16	0.89	0.743	1.06	0.703	1.00	1.30	2.000	Yes
356	35.80	2.03	0.87	1.17	0.88	0.742	1.06	0.703	1.00	1.30	2.000	Yes
357	35.90	2.04	0.87	1.17	0.88	0.742	1.06	0.703	1.00	1.30	2.000	Yes
358	36.00	2.05	0.87	1.17	0.88	0.742	1.06	0.702	1.00	1.30	2.000	Yes
359	36.10	2.05	0.88	1.17	0.88	0.742	1.06	0.702	1.00	1.30	2.000	Yes
360	36.20	2.06	0.88	1.18	0.88	0.741	1.06	0.702	1.00	1.30	2.000	Yes
361	36.30	2.06	0.88	1.18	0.88	0.741	1.06	0.701	1.00	1.30	2.000	Yes
362	36.40	2.07	0.89	1.18	0.88	0.741	1.06	0.701	1.00	1.30	2.000	Yes
363	36.50	2.08	0.89	1.19	0.88	0.740	1.06	0.701	1.00	1.30	0.911	No
364	36.60	2.08	0.89	1.19	0.88	0.740	1.06	0.701	1.00	1.30	0.911	No
365	36.70	2.09	0.90	1.19	0.88	0.740	1.06	0.700	1.00	1.30	0.910	No
366	36.80	2.09	0.90	1.20	0.88	0.739	1.06	0.700	1.00	1.30	0.910	No
367	36.90	2.10	0.90	1.20	0.88	0.739	1.06	0.700	1.00	1.30	0.909	No
368	37.00	2.11	0.90	1.20	0.88	0.739	1.06	0.699	1.00	1.30	2.000	Yes
369	37.10	2.11	0.91	1.20	0.88	0.738	1.06	0.699	1.00	1.30	2.000	Yes
370	37.20	2.12	0.91	1.21	0.87	0.738	1.06	0.699	1.00	1.30	2.000	Yes
371	37.30	2.12	0.91	1.21	0.87	0.738	1.06	0.698	1.00	1.30	2.000	Yes
372	37.40	2.13	0.92	1.21	0.87	0.737	1.06	0.698	1.00	1.30	2.000	Yes
373	37.50	2.14	0.92	1.22	0.87	0.737	1.06	0.697	1.00	1.30	2.000	Yes
374	37.60	2.14	0.92	1.22	0.87	0.736	1.06	0.697	1.00	1.30	2.000	Yes
375	37.70	2.15	0.93	1.22	0.87	0.736	1.06	0.697	1.00	1.30	0.906	No
376	37.80	2.16	0.93	1.23	0.87	0.736	1.06	0.696	1.00	1.30	0.905	No
377	37.90	2.16	0.93	1.23	0.87	0.735	1.06	0.696	1.00	1.30	0.905	No
378	38.00	2.17	0.94	1.23	0.87	0.735	1.06	0.695	1.00	1.30	0.904	No
379	38.10	2.17	0.94	1.24	0.87	0.734	1.06	0.695	1.00	1.30	0.904	No
380	38.20	2.18	0.94	1.24	0.87	0.734	1.06	0.695	1.00	1.30	0.903	No
381	38.30	2.19	0.95	1.24	0.87	0.733	1.06	0.694	1.00	1.30	0.903	No
382	38.40	2.19	0.95	1.24	0.86	0.733	1.06	0.694	1.00	1.30	0.902	No
383	38.50	2.20	0.95	1.25	0.86	0.733	1.06	0.693	1.00	1.30	0.901	No
384	38.60	2.21	0.95	1.25	0.86	0.732	1.06	0.693	1.00	1.30	0.901	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
385	38.70	2.21	0.96	1.25	0.86	0.732	1.06	0.693	1.00	1.30	0.900	No
386	38.80	2.22	0.96	1.26	0.86	0.731	1.06	0.692	1.00	1.30	0.900	No
387	38.90	2.22	0.96	1.26	0.86	0.731	1.06	0.692	1.00	1.30	0.899	No
388	39.00	2.23	0.97	1.26	0.86	0.730	1.06	0.691	1.00	1.30	0.898	No
389	39.10	2.24	0.97	1.27	0.86	0.730	1.06	0.691	1.00	1.30	0.898	No
390	39.20	2.24	0.97	1.27	0.86	0.729	1.06	0.690	1.00	1.30	0.897	No
391	39.30	2.25	0.98	1.27	0.86	0.729	1.06	0.690	1.00	1.30	0.897	No
392	39.40	2.26	0.98	1.28	0.86	0.728	1.06	0.689	1.00	1.30	0.896	No
393	39.50	2.26	0.98	1.28	0.86	0.727	1.06	0.689	1.00	1.30	0.895	No
394	39.60	2.27	0.99	1.28	0.85	0.727	1.06	0.688	1.00	1.30	0.895	No
395	39.70	2.28	0.99	1.29	0.85	0.726	1.06	0.688	1.00	1.30	2.000	Yes
396	39.80	2.28	0.99	1.29	0.85	0.726	1.06	0.687	1.00	1.30	2.000	Yes
397	39.90	2.29	1.00	1.29	0.85	0.725	1.06	0.687	1.00	1.30	2.000	Yes
398	40.00	2.29	1.00	1.30	0.85	0.725	1.06	0.686	1.00	1.30	2.000	Yes
399	40.10	2.30	1.00	1.30	0.85	0.724	1.06	0.686	1.00	1.30	2.000	Yes
400	40.20	2.31	1.00	1.30	0.85	0.724	1.06	0.685	1.00	1.30	2.000	Yes
401	40.30	2.31	1.01	1.31	0.85	0.723	1.06	0.684	1.00	1.30	2.000	Yes
402	40.40	2.32	1.01	1.31	0.85	0.723	1.06	0.684	1.00	1.30	2.000	Yes
403	40.50	2.33	1.01	1.31	0.85	0.722	1.06	0.683	1.00	1.30	2.000	Yes
404	40.60	2.33	1.02	1.32	0.85	0.721	1.06	0.683	1.00	1.30	2.000	Yes
405	40.70	2.34	1.02	1.32	0.84	0.721	1.06	0.682	1.00	1.30	2.000	Yes
406	40.80	2.35	1.02	1.32	0.84	0.720	1.06	0.682	1.00	1.30	2.000	Yes
407	40.90	2.35	1.03	1.32	0.84	0.720	1.06	0.681	1.00	1.30	2.000	Yes
408	41.00	2.36	1.03	1.33	0.84	0.719	1.06	0.681	1.00	1.30	0.885	No
409	41.10	2.36	1.03	1.33	0.84	0.718	1.06	0.680	1.00	1.30	0.884	No
410	41.20	2.37	1.04	1.33	0.84	0.718	1.06	0.680	1.00	1.30	0.883	No
411	41.30	2.38	1.04	1.34	0.84	0.717	1.06	0.679	1.00	1.30	0.883	No
412	41.40	2.38	1.04	1.34	0.84	0.717	1.06	0.678	1.00	1.30	2.000	Yes
413	41.50	2.39	1.05	1.34	0.84	0.716	1.06	0.678	1.00	1.30	2.000	Yes
414	41.60	2.40	1.05	1.35	0.84	0.715	1.06	0.677	1.00	1.30	2.000	Yes
415	41.70	2.40	1.05	1.35	0.84	0.715	1.06	0.677	1.00	1.30	2.000	Yes
416	41.80	2.41	1.05	1.35	0.83	0.714	1.06	0.676	1.00	1.30	2.000	Yes
417	41.90	2.41	1.06	1.36	0.83	0.714	1.06	0.675	1.00	1.30	2.000	Yes
418	42.00	2.42	1.06	1.36	0.83	0.713	1.06	0.675	1.00	1.30	2.000	Yes
419	42.10	2.43	1.06	1.36	0.83	0.712	1.06	0.674	1.00	1.30	2.000	Yes
420	42.20	2.43	1.07	1.37	0.83	0.712	1.06	0.674	1.00	1.30	2.000	Yes
421	42.30	2.44	1.07	1.37	0.83	0.711	1.06	0.673	1.00	1.30	0.875	No
422	42.40	2.45	1.07	1.37	0.83	0.711	1.06	0.673	1.00	1.30	0.875	No
423	42.50	2.45	1.08	1.38	0.83	0.710	1.06	0.672	1.00	1.30	0.874	No
424	42.60	2.46	1.08	1.38	0.83	0.709	1.06	0.672	1.00	1.30	0.873	No
425	42.70	2.46	1.08	1.38	0.83	0.709	1.06	0.671	1.00	1.30	0.872	No
426	42.80	2.47	1.09	1.38	0.83	0.708	1.06	0.670	1.00	1.30	0.872	No
427	42.90	2.48	1.09	1.39	0.82	0.708	1.06	0.670	1.00	1.30	0.871	No
428	43.00	2.48	1.09	1.39	0.82	0.707	1.06	0.669	1.00	1.30	0.870	No
429	43.10	2.49	1.10	1.39	0.82	0.706	1.06	0.669	1.00	1.30	0.869	No
430	43.20	2.49	1.10	1.40	0.82	0.706	1.06	0.668	1.00	1.30	0.869	No
431	43.30	2.50	1.10	1.40	0.82	0.705	1.06	0.668	1.00	1.30	0.868	No
432	43.40	2.51	1.10	1.40	0.82	0.705	1.06	0.667	1.00	1.30	0.867	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
433	43.50	2.51	1.11	1.41	0.82	0.704	1.06	0.666	1.00	1.30	0.866	No
434	43.60	2.52	1.11	1.41	0.82	0.703	1.06	0.666	1.00	1.30	0.865	No
435	43.70	2.53	1.11	1.41	0.82	0.703	1.06	0.665	1.00	1.30	0.865	No
436	43.80	2.53	1.12	1.42	0.82	0.702	1.06	0.664	1.00	1.30	0.864	No
437	43.90	2.54	1.12	1.42	0.81	0.701	1.06	0.664	1.00	1.30	2.000	Yes
438	44.00	2.54	1.12	1.42	0.81	0.701	1.06	0.663	1.00	1.30	2.000	Yes
439	44.10	2.55	1.13	1.42	0.81	0.700	1.06	0.662	1.00	1.30	2.000	Yes
440	44.20	2.56	1.13	1.43	0.81	0.699	1.06	0.662	1.00	1.30	2.000	Yes
441	44.30	2.56	1.13	1.43	0.81	0.698	1.06	0.661	1.00	1.30	2.000	Yes
442	44.40	2.57	1.14	1.43	0.81	0.698	1.06	0.660	1.00	1.30	2.000	Yes
443	44.50	2.58	1.14	1.44	0.81	0.697	1.06	0.660	1.00	1.30	2.000	Yes
444	44.60	2.58	1.14	1.44	0.81	0.696	1.06	0.659	1.00	1.30	2.000	Yes
445	44.70	2.59	1.15	1.44	0.81	0.695	1.06	0.658	1.00	1.30	0.856	No
446	44.80	2.60	1.15	1.45	0.81	0.695	1.06	0.658	1.00	1.30	0.855	No
447	44.90	2.60	1.15	1.45	0.80	0.694	1.06	0.657	1.00	1.30	0.854	No
448	45.00	2.61	1.15	1.46	0.80	0.693	1.06	0.656	1.00	1.30	0.853	No
449	45.10	2.62	1.16	1.46	0.80	0.692	1.06	0.655	1.00	1.30	0.852	No
450	45.20	2.62	1.16	1.46	0.80	0.692	1.06	0.655	1.00	1.30	0.851	No
451	45.30	2.63	1.16	1.47	0.80	0.691	1.06	0.654	1.00	1.30	0.850	No
452	45.40	2.64	1.17	1.47	0.80	0.690	1.06	0.653	1.00	1.30	0.849	No
453	45.50	2.64	1.17	1.47	0.80	0.689	1.06	0.652	1.00	1.30	0.848	No
454	45.60	2.65	1.17	1.48	0.80	0.688	1.06	0.652	1.00	1.30	0.847	No
455	45.70	2.66	1.18	1.48	0.80	0.688	1.06	0.651	1.00	1.30	0.846	No
456	45.80	2.66	1.18	1.48	0.80	0.687	1.06	0.650	1.00	1.30	0.845	No
457	45.90	2.67	1.18	1.49	0.79	0.686	1.06	0.650	1.00	1.30	0.844	No
458	46.00	2.68	1.19	1.49	0.79	0.685	1.06	0.649	1.00	1.30	0.843	No
459	46.10	2.68	1.19	1.49	0.79	0.685	1.06	0.648	1.00	1.30	0.842	No
460	46.20	2.69	1.19	1.50	0.79	0.684	1.06	0.647	1.00	1.30	0.841	No
461	46.30	2.70	1.19	1.50	0.79	0.683	1.06	0.647	1.00	1.30	0.840	No
462	46.40	2.70	1.20	1.50	0.79	0.682	1.06	0.646	1.00	1.30	0.840	No
463	46.50	2.71	1.20	1.51	0.79	0.681	1.06	0.645	1.00	1.30	0.839	No
464	46.60	2.72	1.20	1.51	0.79	0.681	1.06	0.644	1.00	1.30	0.838	No
465	46.70	2.72	1.21	1.51	0.79	0.680	1.06	0.644	1.00	1.30	0.837	No
466	46.80	2.73	1.21	1.52	0.79	0.679	1.06	0.643	1.00	1.30	0.836	No
467	46.90	2.74	1.21	1.52	0.78	0.678	1.06	0.642	1.00	1.30	0.835	No
468	47.00	2.74	1.22	1.53	0.78	0.677	1.06	0.641	1.00	1.30	0.834	No
469	47.10	2.75	1.22	1.53	0.78	0.677	1.06	0.641	1.00	1.30	0.833	No
470	47.20	2.76	1.22	1.53	0.78	0.676	1.06	0.640	1.00	1.30	0.832	No
471	47.30	2.76	1.23	1.54	0.78	0.675	1.06	0.639	1.00	1.30	0.831	No
472	47.40	2.77	1.23	1.54	0.78	0.674	1.06	0.638	1.00	1.30	0.830	No
473	47.50	2.77	1.23	1.54	0.78	0.674	1.06	0.638	1.00	1.30	0.829	No
474	47.60	2.78	1.24	1.55	0.78	0.673	1.06	0.637	1.00	1.30	0.828	No
475	47.70	2.79	1.24	1.55	0.78	0.672	1.06	0.636	1.00	1.30	0.827	No
476	47.80	2.79	1.24	1.55	0.78	0.671	1.06	0.635	1.00	1.30	0.826	No
477	47.90	2.80	1.24	1.56	0.77	0.670	1.06	0.635	1.00	1.30	0.825	No
478	48.00	2.81	1.25	1.56	0.77	0.670	1.06	0.634	1.00	1.30	0.824	No
479	48.10	2.81	1.25	1.56	0.77	0.669	1.06	0.633	1.00	1.30	0.823	No
480	48.20	2.82	1.25	1.57	0.77	0.668	1.06	0.632	1.00	1.30	0.822	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
481	48.30	2.83	1.26	1.57	0.77	0.667	1.06	0.632	1.00	1.30	0.821	No
482	48.40	2.83	1.26	1.57	0.77	0.666	1.06	0.631	1.00	1.30	0.820	No
483	48.50	2.84	1.26	1.58	0.77	0.666	1.06	0.630	1.00	1.30	0.819	No
484	48.60	2.85	1.27	1.58	0.77	0.665	1.06	0.629	1.00	1.30	0.818	No
485	48.70	2.85	1.27	1.58	0.77	0.664	1.06	0.629	1.00	1.30	0.817	No
486	48.80	2.86	1.27	1.59	0.76	0.663	1.06	0.628	1.00	1.30	0.816	No
487	48.90	2.87	1.28	1.59	0.76	0.662	1.06	0.627	1.00	1.30	0.815	No
488	49.00	2.87	1.28	1.59	0.76	0.662	1.06	0.626	1.00	1.30	0.814	No
489	49.10	2.88	1.28	1.60	0.76	0.661	1.06	0.625	1.00	1.30	0.813	No
490	49.20	2.89	1.29	1.60	0.76	0.660	1.06	0.625	1.00	1.30	0.812	No
491	49.30	2.89	1.29	1.60	0.76	0.659	1.06	0.624	1.00	1.30	0.811	No
492	49.40	2.90	1.29	1.61	0.76	0.658	1.06	0.623	1.00	1.30	0.810	No
493	49.50	2.91	1.29	1.61	0.76	0.657	1.06	0.622	1.00	1.30	0.809	No
494	49.60	2.91	1.30	1.61	0.76	0.657	1.06	0.622	1.00	1.30	0.808	No
495	49.70	2.92	1.30	1.62	0.76	0.656	1.06	0.621	1.00	1.30	0.807	No
496	49.80	2.93	1.30	1.62	0.75	0.655	1.06	0.620	1.00	1.30	0.806	No

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
 σ_v : Total overburden pressure at test point (tsf)
 u_0 : Water pressure at test point (tsf)
 σ_v' : Effective overburden pressure based on GWT during earthquake (tsf)
 r_d : Nonlinear shear mass factor
 CSR: Cyclic Stress Ratio
 MSF: Magnitude Scaling Factor
 CSR_{eq} : CSR adjusted for M=7.5
 K_σ : Effective overburden stress factor
 CSR*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::												
Point ID	Depth (ft)	q _t (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1	0.30	80.54	2.22	3.92	0.70	152.20	1.68	255.05	4.000	No	No	2.00
2	0.40	76.12	2.24	3.93	0.70	143.84	1.72	247.62	4.000	No	No	2.00
3	0.50	68.91	2.27	3.96	0.72	130.19	1.81	235.68	4.000	No	No	2.00
4	0.60	61.08	2.30	3.97	0.73	115.37	1.93	222.13	4.000	No	No	2.00
5	0.70	55.64	2.32	3.88	0.74	105.09	1.99	209.42	4.000	No	No	2.00
6	0.80	52.36	2.32	3.69	0.74	98.88	1.99	196.91	4.000	No	No	2.00
7	0.90	50.29	2.31	3.45	0.73	94.95	1.95	184.73	4.000	No	No	2.00
8	1.00	48.50	2.29	3.17	0.72	91.55	1.88	172.20	4.000	No	No	2.00
9	1.10	46.72	2.27	2.87	0.72	88.17	1.81	159.58	4.000	No	No	2.00
10	1.20	45.12	2.24	2.59	0.71	85.14	1.74	147.83	4.000	No	No	2.00
11	1.30	43.40	2.23	2.36	0.70	81.89	1.69	138.02	4.000	No	No	2.00
12	1.40	41.62	2.22	2.22	0.70	78.51	1.67	131.20	4.000	No	No	2.00
13	1.50	39.65	2.23	2.15	0.70	74.76	1.68	125.92	4.000	No	No	2.00
14	1.60	37.61	2.23	2.07	0.71	70.90	1.70	120.55	4.000	No	No	2.00
15	1.70	35.63	2.23	1.95	0.71	67.15	1.70	114.04	4.000	No	No	2.00
16	1.80	33.95	2.22	1.80	0.70	63.96	1.68	107.33	4.000	No	No	2.00
17	1.90	32.57	2.21	1.64	0.70	61.34	1.64	100.71	4.000	No	No	2.00
18	2.00	31.19	2.19	1.47	0.69	58.72	1.60	94.03	4.000	No	No	2.00
19	2.10	29.70	2.18	1.32	0.69	55.90	1.57	87.92	4.000	No	No	2.00
20	2.20	27.91	2.18	1.22	0.69	52.50	1.58	82.75	4.000	No	No	2.00
21	2.30	25.92	2.20	1.19	0.70	48.74	1.62	79.15	4.000	No	No	2.00
22	2.40	23.95	2.24	1.21	0.71	45.00	1.71	76.89	4.000	No	No	2.00
23	2.50	22.19	2.27	1.22	0.72	41.66	1.80	75.13	4.000	No	No	2.00
24	2.60	20.94	2.28	1.20	0.73	39.28	1.86	73.11	4.000	No	No	2.00
25	2.70	20.11	2.28	1.13	0.73	37.71	1.86	70.03	4.000	No	No	2.00
26	2.80	19.97	2.26	1.02	0.72	37.44	1.78	66.76	4.000	No	No	2.00
27	2.90	20.60	2.23	0.95	0.71	38.62	1.70	65.53	4.000	No	No	2.00
28	3.00	21.67	2.23	1.02	0.71	40.63	1.70	68.92	4.000	Yes	No	2.00
29	3.10	22.10	2.28	1.30	0.73	41.44	1.86	77.20	4.000	Yes	No	2.00
30	3.20	20.76	2.38	1.73	0.77	38.89	2.27	88.23	4.000	Yes	No	2.00
31	3.30	18.46	2.50	2.31	0.81	34.54	2.97	102.45	4.000	Yes	No	2.00
32	3.40	16.29	2.61	2.96	0.85	30.41	5.74	174.56	4.000	Yes	No	2.00
33	3.50	15.43	2.68	3.54	0.88	28.79	8.87	255.39	4.000	Yes	No	2.00
34	3.60	15.14	2.72	4.00	0.90	28.22	4.92	138.72	4.000	Yes	Yes	2.00
35	3.70	15.27	2.74	4.32	0.90	28.45	5.14	146.14	4.000	No	Yes	2.00
36	3.80	15.71	2.74	4.51	0.91	29.28	5.18	151.59	4.000	No	Yes	2.00
37	3.90	16.02	2.74	4.60	0.91	29.85	5.18	154.64	4.000	No	Yes	2.00
38	4.00	15.90	2.75	4.71	0.91	29.62	5.29	156.64	4.000	No	Yes	2.00
39	4.10	15.47	2.77	4.84	0.92	28.80	5.49	157.97	4.000	No	Yes	2.00
40	4.20	15.30	2.78	4.90	0.92	28.45	5.58	158.67	4.000	No	Yes	2.00
41	4.30	15.03	2.78	4.89	0.92	27.94	5.64	157.49	4.000	No	Yes	2.00
42	4.40	13.95	2.81	4.89	0.93	25.89	5.93	153.53	4.000	No	Yes	2.00
43	4.50	12.08	2.85	4.89	0.95	22.33	6.55	146.36	4.000	No	Yes	2.00
44	4.60	10.23	2.90	4.76	0.97	18.83	7.23	136.13	4.000	No	Yes	2.00
45	4.70	8.88	2.93	4.40	0.98	16.27	7.62	124.04	4.000	No	Yes	2.00
46	4.80	7.65	2.95	3.94	0.99	13.94	7.97	111.15	4.000	No	Yes	2.00
47	4.90	6.48	2.98	3.52	1.00	11.71	8.47	99.11	4.000	No	Yes	2.00
48	5.00	5.29	3.03	3.18	1.00	9.46	9.33	88.23	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _t (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
49	5.10	4.54	3.07	2.93	1.00	8.03	10.03	80.61	4.000	No	Yes	2.00
50	5.20	4.11	3.09	2.69	1.00	7.20	10.42	75.03	4.000	No	Yes	2.00
51	5.30	3.98	3.08	2.48	1.00	6.96	10.31	71.71	4.000	No	Yes	2.00
52	5.40	3.98	3.07	2.35	1.00	6.95	10.07	69.99	4.000	No	Yes	2.00
53	5.50	3.98	3.07	2.34	1.00	6.94	10.07	69.90	4.000	No	Yes	2.00
54	5.60	3.95	3.09	2.51	1.00	6.87	10.44	71.71	4.000	No	Yes	2.00
55	5.70	3.84	3.13	2.82	1.00	6.65	11.21	74.59	4.000	No	Yes	2.00
56	5.80	3.71	3.17	3.20	1.00	6.39	12.15	77.69	4.000	No	Yes	2.00
57	5.90	3.67	3.20	3.57	1.00	6.32	12.83	81.04	4.000	No	Yes	2.00
58	6.00	3.78	3.21	3.86	1.00	6.51	13.01	84.78	4.000	No	Yes	2.00
59	6.10	3.92	3.21	4.07	1.00	6.76	13.01	87.91	4.000	No	Yes	2.00
60	6.20	3.98	3.22	4.26	1.00	6.88	13.13	90.26	4.000	No	Yes	2.00
61	6.30	3.98	3.23	4.47	1.00	6.87	13.43	92.23	4.000	No	Yes	2.00
62	6.40	4.19	3.23	4.77	1.00	7.25	13.37	96.86	4.000	No	Yes	2.00
63	6.50	4.70	3.20	5.08	1.00	8.20	12.75	104.54	4.000	No	Yes	2.00
64	6.60	5.51	3.15	5.32	1.00	9.72	11.72	113.91	4.000	No	Yes	2.00
65	6.70	6.36	3.11	5.50	1.00	11.33	10.84	122.78	4.000	No	Yes	2.00
66	6.80	6.92	3.09	5.73	1.00	12.36	10.48	129.51	4.000	No	Yes	2.00
67	6.90	7.07	3.10	6.03	1.00	12.64	10.62	134.19	4.000	No	Yes	2.00
68	7.00	7.06	3.12	6.35	1.00	12.61	10.92	137.66	4.000	No	Yes	2.00
69	7.10	7.53	3.10	6.43	1.00	13.49	10.54	142.25	4.000	No	Yes	2.00
70	7.20	8.17	3.06	6.25	1.00	14.68	9.87	144.89	4.000	No	Yes	2.00
71	7.30	8.41	3.04	6.11	1.00	15.13	9.56	144.74	4.000	No	Yes	2.00
72	7.40	8.09	3.06	6.19	1.00	14.51	9.89	143.48	4.000	No	Yes	2.00
73	7.50	8.74	3.06	6.63	1.00	15.73	9.77	153.65	4.000	No	Yes	2.00
74	7.60	10.99	3.00	7.17	1.00	19.98	8.83	176.32	4.000	No	Yes	2.00
75	7.70	13.63	2.95	7.50	0.99	24.96	7.92	197.63	4.000	No	Yes	2.00
76	7.80	15.24	2.92	7.62	0.98	27.99	7.46	208.82	4.000	No	Yes	2.00
77	7.90	15.53	2.91	7.52	0.98	28.53	7.32	208.71	4.000	No	Yes	2.00
78	8.00	15.24	2.90	7.22	0.98	27.97	7.21	201.78	4.000	No	Yes	2.00
79	8.10	14.56	2.90	6.80	0.97	26.68	7.15	190.81	1.272	No	Yes	2.00
80	8.20	13.55	2.90	6.29	0.97	24.74	7.15	176.83	1.180	No	Yes	2.00
81	8.30	12.33	2.90	5.81	0.98	22.44	7.25	162.63	1.070	No	Yes	1.80
82	8.40	11.42	2.91	5.39	0.98	20.70	7.31	151.23	0.987	No	Yes	1.65
83	8.50	10.85	2.91	5.06	0.98	19.62	7.28	142.92	0.936	No	Yes	1.56
84	8.60	10.72	2.89	4.79	0.97	19.37	7.12	137.89	0.924	No	Yes	1.53
85	8.70	10.46	2.89	4.63	0.97	18.85	7.11	134.00	0.899	No	Yes	1.48
86	8.80	10.06	2.91	4.61	0.98	18.09	7.29	131.89	0.863	No	Yes	1.41
87	8.90	9.83	2.92	4.73	0.99	17.65	7.52	132.73	0.842	No	Yes	1.37
88	9.00	10.07	2.92	4.85	0.98	18.10	7.50	135.70	0.863	No	Yes	1.39
89	9.10	10.47	2.91	4.85	0.98	18.84	7.30	137.55	0.899	No	Yes	1.44
90	9.20	10.73	2.89	4.78	0.98	19.32	7.13	137.71	0.921	No	Yes	1.47
91	9.30	10.76	2.89	4.80	0.98	19.36	7.13	138.04	0.923	No	Yes	1.47
92	9.40	10.76	2.90	4.96	0.98	19.35	7.27	140.71	0.923	No	Yes	1.46
93	9.50	10.76	2.92	5.19	0.98	19.34	7.47	144.46	0.922	No	Yes	1.45
94	9.60	11.08	2.92	5.35	0.98	19.94	7.45	148.57	0.951	No	Yes	1.49
95	9.70	12.05	2.88	5.23	0.97	21.76	6.94	151.08	1.038	No	Yes	1.61
96	9.80	15.58	2.77	4.84	0.93	28.43	5.53	157.22	1.356	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
97	9.90	20.15	2.67	4.52	0.89	36.68	8.63	316.66	3.600	No	No	2.00
98	10.00	20.15	2.67	4.42	0.89	36.43	8.39	305.72	3.600	No	No	2.00
99	10.10	15.24	2.76	4.47	0.92	27.73	5.35	148.25	1.323	No	Yes	2.00
100	10.20	9.08	2.94	4.58	0.99	16.10	7.85	126.32	0.768	No	Yes	1.17
101	10.30	6.68	3.05	4.44	1.00	11.55	9.60	110.91	0.551	No	Yes	0.83
102	10.40	6.06	3.07	4.15	1.00	10.36	9.96	103.26	0.494	No	Yes	0.74
103	10.50	5.06	3.12	3.94	1.00	8.47	11.09	93.94	0.404	No	Yes	0.60
104	10.60	4.24	3.19	3.81	1.00	6.91	12.47	86.12	0.329	No	Yes	0.49
105	10.70	3.95	3.21	3.73	1.00	6.34	13.04	82.70	0.303	No	Yes	0.45
106	10.80	3.84	3.24	3.87	1.00	6.12	13.55	82.97	0.292	No	Yes	0.43
107	10.90	3.70	3.28	4.31	1.00	5.86	14.60	85.56	0.280	No	Yes	0.41
108	11.00	3.61	3.31	4.75	1.00	5.67	15.54	88.03	0.270	No	Yes	0.40
109	11.10	3.66	3.31	4.86	1.00	5.76	15.55	89.50	0.275	No	Yes	0.40
110	11.20	3.79	3.30	4.83	1.00	6.00	15.10	90.61	0.286	No	Yes	0.42
111	11.30	4.04	3.28	4.92	1.00	6.46	14.55	94.08	0.308	No	Yes	0.45
112	11.40	4.70	3.23	5.20	1.00	7.70	13.39	103.11	0.367	No	Yes	0.53
113	11.50	5.71	3.16	5.32	1.00	9.60	11.81	113.38	0.458	No	Yes	0.66
114	11.60	6.66	3.10	5.35	1.00	11.38	10.65	121.21	0.543	No	Yes	0.77
115	11.70	7.46	3.07	5.53	1.00	12.87	10.04	129.20	0.614	No	Yes	0.87
116	11.80	8.53	3.04	5.80	1.00	14.82	9.42	139.67	0.707	No	Yes	1.00
117	11.90	10.10	2.98	5.81	1.00	17.69	8.43	149.16	0.844	No	Yes	1.19
118	12.00	11.40	2.92	5.49	0.99	19.88	7.58	150.64	0.948	No	Yes	1.33
119	12.10	12.05	2.89	5.07	0.98	20.78	7.03	146.07	0.991	No	Yes	1.39
120	12.20	11.99	2.87	4.76	0.97	20.50	6.83	140.04	0.978	No	Yes	1.36
121	12.30	11.24	2.89	4.61	0.98	19.11	7.03	134.38	0.912	No	Yes	1.27
122	12.40	9.78	2.93	4.52	0.99	16.56	7.65	126.64	0.790	No	Yes	1.09
123	12.50	7.81	3.00	4.40	1.00	12.99	8.86	115.04	0.620	No	Yes	0.86
124	12.60	5.80	3.11	4.21	1.00	9.27	10.79	100.03	0.442	No	Yes	0.61
125	12.70	4.05	3.24	3.90	1.00	6.07	13.67	83.00	0.290	No	Yes	0.40
126	12.80	3.26	3.28	3.00	1.00	4.61	14.67	67.56	0.220	No	Yes	0.30
127	12.90	3.58	3.12	1.77	1.00	5.17	11.06	57.22	0.247	No	Yes	0.34
128	13.00	4.31	2.97	1.26	1.00	6.47	8.27	53.47	0.309	No	Yes	0.42
129	13.10	4.77	2.94	1.36	1.00	7.24	7.81	56.56	0.346	No	Yes	0.47
130	13.20	4.87	3.02	2.04	1.00	7.40	9.08	67.21	0.353	No	Yes	0.48
131	13.30	5.19	3.08	3.03	1.00	7.94	10.27	81.56	0.379	No	Yes	0.51
132	13.40	5.59	3.12	3.93	1.00	8.61	10.95	94.34	0.411	No	Yes	0.55
133	13.50	5.90	3.14	4.67	1.00	9.12	11.45	104.49	0.435	No	Yes	0.58
134	13.60	6.41	3.14	5.23	1.00	9.97	11.44	114.07	0.476	No	Yes	0.63
135	13.70	7.60	3.08	5.22	1.00	12.02	10.16	122.14	0.573	No	Yes	0.76
136	13.80	9.89	2.95	4.58	1.00	15.95	7.90	126.04	0.761	No	Yes	1.01
137	13.90	12.14	2.84	3.92	0.96	19.30	6.35	122.59	0.920	No	Yes	1.21
138	14.00	13.09	2.80	3.69	0.94	20.64	5.85	120.81	0.984	No	Yes	1.29
139	14.10	12.44	2.84	4.09	0.96	19.65	6.43	126.36	0.937	No	Yes	1.23
140	14.20	12.59	2.89	4.98	0.98	20.04	7.12	142.74	4.000	Yes	Yes	2.00
141	14.30	16.22	2.82	5.03	0.95	25.64	6.08	155.81	4.000	Yes	Yes	2.00
142	14.40	23.62	2.64	3.96	0.88	36.25	6.85	248.34	4.000	Yes	No	2.00
143	14.50	32.92	2.43	2.69	0.80	48.52	2.54	123.26	4.000	Yes	No	2.00
144	14.60	41.56	2.24	1.73	0.73	58.81	1.72	101.36	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
145	14.70	48.47	2.10	1.19	0.68	66.43	1.41	93.93	4.000	Yes	No	2.00
146	14.80	52.66	2.03	1.01	0.65	71.00	1.33	94.66	4.000	Yes	No	2.00
147	14.90	53.17	2.03	1.02	0.65	71.48	1.33	95.28	4.000	Yes	No	2.00
148	15.00	49.27	2.09	1.19	0.68	66.90	1.41	94.32	4.000	Yes	No	2.00
149	15.10	40.94	2.22	1.54	0.72	56.71	1.66	94.32	4.000	Yes	No	2.00
150	15.20	30.97	2.38	2.05	0.79	43.98	2.29	100.91	4.000	Yes	No	2.00
151	15.30	21.85	2.57	2.69	0.86	31.75	4.41	139.95	4.000	Yes	No	2.00
152	15.40	15.51	2.72	3.18	0.92	22.82	4.97	113.49	4.000	Yes	Yes	2.00
153	15.50	11.13	2.85	3.32	0.97	16.35	6.50	106.32	4.000	Yes	Yes	2.00
154	15.60	8.16	2.94	3.03	1.00	11.81	7.81	92.23	4.000	Yes	Yes	2.00
155	15.70	6.23	3.00	2.43	1.00	8.66	8.76	75.87	4.000	Yes	Yes	2.00
156	15.80	5.38	2.99	1.71	1.00	7.25	8.57	62.13	0.346	No	Yes	0.43
157	15.90	5.36	2.91	1.11	0.99	7.15	7.29	52.12	0.341	No	Yes	0.43
158	16.00	5.34	2.85	0.79	0.97	7.01	6.54	45.85	0.334	No	Yes	0.42
159	16.10	4.96	2.87	0.71	0.97	6.42	6.76	43.41	0.306	No	Yes	0.38
160	16.20	4.35	2.94	0.77	1.00	5.52	7.86	43.43	0.264	No	Yes	0.33
161	16.30	3.98	3.02	0.92	1.00	4.92	9.13	44.92	0.235	No	Yes	0.29
162	16.40	3.98	3.05	1.07	1.00	4.90	9.63	47.20	0.234	No	Yes	0.29
163	16.50	3.98	3.07	1.20	1.00	4.89	10.03	48.98	0.233	No	Yes	0.29
164	16.60	3.98	3.08	1.27	1.00	4.87	10.25	49.89	0.232	No	Yes	0.29
165	16.70	3.98	3.08	1.27	1.00	4.85	10.28	49.88	0.231	No	Yes	0.28
166	16.80	3.98	3.08	1.22	1.00	4.83	10.18	49.18	0.231	No	Yes	0.28
167	16.90	3.98	3.08	1.21	1.00	4.82	10.17	48.98	0.230	No	Yes	0.28
168	17.00	3.98	3.09	1.32	1.00	4.80	10.51	50.42	0.229	No	Yes	0.28
169	17.10	3.94	3.14	1.61	1.00	4.72	11.40	53.77	0.225	No	Yes	0.27
170	17.20	4.08	3.17	2.02	1.00	4.92	12.06	59.31	0.235	No	Yes	0.28
171	17.30	5.02	3.12	2.56	1.00	6.36	11.10	70.59	0.303	No	Yes	0.37
172	17.40	6.54	3.06	3.15	1.00	8.69	9.84	85.46	0.414	No	Yes	0.50
173	17.50	8.33	3.01	3.74	1.00	11.42	8.88	101.36	0.545	No	Yes	0.66
174	17.60	9.72	2.98	4.25	1.00	13.50	8.48	114.46	0.644	No	Yes	0.77
175	17.70	10.81	2.95	4.43	1.00	15.11	8.04	121.56	0.721	No	Yes	0.86
176	17.80	11.39	2.93	4.33	1.00	15.92	7.67	122.06	0.759	No	Yes	0.91
177	17.90	11.17	2.93	4.13	1.00	15.50	7.60	117.86	0.739	No	Yes	0.88
178	18.00	10.46	2.94	3.96	1.00	14.39	7.82	112.59	0.687	No	Yes	0.82
179	18.10	9.58	2.97	3.83	1.00	13.01	8.24	107.14	0.621	No	Yes	0.74
180	18.20	8.88	2.99	3.72	1.00	11.90	8.62	102.55	0.568	No	Yes	0.67
181	18.30	8.09	3.02	3.67	1.00	10.67	9.21	98.23	0.509	No	Yes	0.60
182	18.40	7.19	3.07	3.68	1.00	9.28	10.12	93.89	0.443	No	Yes	0.52
183	18.50	6.45	3.12	3.64	1.00	8.14	10.98	89.39	0.388	No	Yes	0.46
184	18.60	6.04	3.14	3.53	1.00	7.50	11.41	85.63	0.358	No	Yes	0.42
185	18.70	5.99	3.14	3.39	1.00	7.40	11.32	83.75	0.353	No	Yes	0.42
186	18.80	6.24	3.11	3.23	1.00	7.73	10.76	83.19	0.369	No	Yes	0.43
187	18.90	6.64	3.07	3.01	1.00	8.29	9.94	82.40	0.395	No	Yes	0.46
188	19.00	7.02	3.02	2.77	1.00	8.82	9.19	80.99	0.421	No	Yes	0.49
189	19.10	7.02	3.01	2.56	1.00	8.78	8.89	78.06	0.419	No	Yes	0.49
190	19.20	6.63	3.01	2.37	1.00	8.19	9.01	73.79	0.391	No	Yes	0.46
191	19.30	6.23	3.03	2.27	1.00	7.58	9.33	70.76	0.362	No	Yes	0.42
192	19.40	6.06	3.06	2.46	1.00	7.30	9.93	72.47	0.348	No	Yes	0.40

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
193	19.50	6.65	3.07	3.02	1.00	8.13	10.10	82.07	0.388	No	Yes	0.45
194	19.60	7.86	3.05	3.61	1.00	9.84	9.64	94.93	0.470	No	Yes	0.54
195	19.70	9.33	3.01	3.96	1.00	11.92	8.88	105.88	0.568	No	Yes	0.66
196	19.80	12.75	2.90	4.05	0.99	16.70	7.16	119.55	0.797	No	Yes	0.92
197	19.90	18.72	2.75	3.80	0.93	24.54	5.26	129.05	1.171	No	Yes	1.35
198	20.00	20.77	2.70	3.55	0.91	27.08	10.12	274.17	3.600	No	No	2.00
199	20.10	17.42	2.74	3.31	0.93	22.53	5.14	115.85	1.075	No	Yes	1.24
200	20.20	10.46	2.90	3.02	0.99	13.21	7.20	95.19	0.630	No	Yes	0.72
201	20.30	7.00	3.06	2.96	1.00	8.34	9.83	82.00	0.398	No	Yes	0.46
202	20.40	6.52	3.09	3.00	1.00	7.63	10.50	80.15	0.364	No	Yes	0.42
203	20.50	6.31	3.12	3.15	1.00	7.32	11.04	80.81	0.349	No	Yes	0.40
204	20.60	6.18	3.15	3.39	1.00	7.11	11.63	82.66	0.339	No	Yes	0.39
205	20.70	5.98	3.19	3.78	1.00	6.80	12.54	85.31	0.325	No	Yes	0.37
206	20.80	6.14	3.21	4.30	1.00	6.99	13.05	91.20	0.333	No	Yes	0.38
207	20.90	7.00	3.19	4.93	1.00	8.17	12.59	102.84	0.389	No	Yes	0.44
208	21.00	8.96	3.11	5.18	1.00	10.84	10.81	117.14	0.517	No	Yes	0.59
209	21.10	11.72	2.99	4.83	1.00	14.61	8.61	125.79	0.697	No	Yes	0.79
210	21.20	14.03	2.90	4.31	0.99	17.64	7.14	125.93	0.841	No	Yes	0.95
211	21.30	14.79	2.86	4.04	0.97	18.52	6.65	123.20	0.884	No	Yes	1.00
212	21.40	14.13	2.89	4.22	0.99	17.62	7.05	124.31	0.841	No	Yes	0.95
213	21.50	12.43	2.97	4.79	1.00	15.33	8.31	127.42	0.731	No	Yes	0.82
214	21.60	10.28	3.08	5.45	1.00	12.37	10.21	126.24	0.590	No	Yes	0.66
215	21.70	8.08	3.20	6.05	1.00	9.34	12.78	119.42	0.446	No	Yes	0.50
216	21.80	6.21	3.33	6.46	1.00	6.79	15.97	108.41	0.324	No	Yes	0.36
217	21.90	5.28	3.40	6.44	1.00	5.52	18.04	99.49	0.263	No	Yes	0.30
218	22.00	5.34	3.37	5.86	1.00	5.57	17.21	95.84	0.266	No	Yes	0.30
219	22.10	6.13	3.29	5.30	1.00	6.61	14.84	98.07	0.315	No	Yes	0.35
220	22.20	7.05	3.22	5.03	1.00	7.81	13.08	102.14	0.373	No	Yes	0.42
221	22.30	7.61	3.18	5.03	1.00	8.52	12.38	105.47	0.406	No	Yes	0.45
222	22.40	8.13	3.16	5.14	1.00	9.17	11.95	109.64	0.437	No	Yes	0.49
223	22.50	9.00	3.13	5.30	1.00	10.29	11.30	116.23	0.491	No	Yes	0.55
224	22.60	9.37	3.13	5.48	1.00	10.74	11.18	120.09	0.512	No	Yes	0.57
225	22.70	8.82	3.16	5.66	1.00	9.97	11.89	118.55	0.476	No	Yes	0.53
226	22.80	7.69	3.22	5.78	1.00	8.46	13.29	112.37	0.403	No	Yes	0.45
227	22.90	6.90	3.27	5.72	1.00	7.40	14.35	106.12	0.353	No	Yes	0.39
228	23.00	6.98	3.26	5.55	1.00	7.47	14.06	105.03	0.356	No	Yes	0.39
229	23.10	7.60	3.22	5.41	1.00	8.24	13.08	107.82	0.393	No	Yes	0.43
230	23.20	8.28	3.18	5.33	1.00	9.09	12.23	111.21	0.434	No	Yes	0.48
231	23.30	8.77	3.15	5.27	1.00	9.69	11.69	113.23	0.462	No	Yes	0.51
232	23.40	8.77	3.15	5.24	1.00	9.65	11.69	112.79	0.460	No	Yes	0.51
233	23.50	8.95	3.15	5.26	1.00	9.85	11.56	113.85	0.470	No	Yes	0.52
234	23.60	9.45	3.13	5.29	1.00	10.45	11.17	116.74	0.498	No	Yes	0.55
235	23.70	9.65	3.13	5.39	1.00	10.67	11.13	118.76	0.509	No	Yes	0.56
236	23.80	9.37	3.15	5.65	1.00	10.27	11.66	119.81	0.490	No	Yes	0.54
237	23.90	9.41	3.17	6.01	1.00	10.29	12.01	123.61	0.491	No	Yes	0.54
238	24.00	11.56	3.08	5.84	1.00	12.97	10.27	133.21	0.619	No	Yes	0.68
239	24.10	16.37	2.91	4.98	1.00	18.95	7.39	140.03	0.904	No	Yes	0.99
240	24.20	22.14	2.75	3.96	0.93	25.65	5.23	134.10	1.223	No	Yes	1.34

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q_t (tsf)	I_c	F_r (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
241	24.30	26.41	2.62	3.13	0.89	30.40	6.34	192.89	0.673	No	No	0.74
242	24.40	28.09	2.57	2.72	0.87	32.14	4.37	140.59	0.338	No	No	0.37
243	24.50	26.73	2.60	2.87	0.88	30.52	5.40	164.76	0.496	No	No	0.54
244	24.60	23.36	2.70	3.51	0.92	26.67	4.71	125.71	1.272	No	Yes	1.39
245	24.70	20.44	2.81	4.43	0.96	23.31	6.00	139.79	1.112	No	Yes	1.21
246	24.80	19.80	2.86	5.10	0.98	22.57	6.68	150.66	1.076	No	Yes	1.17
247	24.90	20.81	2.85	5.21	0.98	23.69	6.54	155.06	1.130	No	Yes	1.23
248	25.00	21.40	2.83	4.98	0.97	24.28	6.26	152.06	1.158	No	Yes	1.26
249	25.10	22.04	2.79	4.50	0.95	24.87	5.79	143.99	1.186	No	Yes	1.29
250	25.20	22.96	2.75	4.07	0.94	25.79	5.30	136.81	1.230	No	Yes	1.34
251	25.30	23.14	2.75	4.07	0.94	25.91	5.29	137.02	1.236	No	Yes	1.34
252	25.40	22.74	2.80	4.67	0.96	25.46	5.83	148.46	1.214	No	Yes	1.32
253	25.50	24.78	2.82	5.58	0.96	27.85	6.14	171.07	4.000	Yes	Yes	2.00
254	25.60	33.66	2.73	5.65	0.93	37.98	5.05	191.70	4.000	Yes	Yes	2.00
255	25.70	53.07	2.54	4.72	0.86	59.58	3.70	220.35	4.000	Yes	No	2.00
256	25.80	82.74	2.33	3.56	0.78	91.73	2.03	185.82	4.000	Yes	No	2.00
257	25.90	117.80	2.13	2.63	0.70	128.70	1.47	189.05	4.000	Yes	No	2.00
258	26.00	148.57	1.98	2.00	0.64	160.21	1.29	206.69	4.000	Yes	No	2.00
259	26.10	167.69	1.89	1.67	0.61	179.21	1.23	220.06	4.000	Yes	No	2.00
260	26.20	173.65	1.85	1.54	0.60	184.66	1.20	222.02	4.000	Yes	No	2.00
261	26.30	170.00	1.86	1.55	0.60	180.46	1.21	218.21	4.000	No	No	2.00
262	26.40	161.80	1.89	1.62	0.61	171.65	1.23	211.10	4.000	No	No	2.00
263	26.50	152.97	1.92	1.71	0.62	162.24	1.25	203.19	4.000	No	No	2.00
264	26.60	145.31	1.96	1.81	0.64	154.04	1.27	196.34	0.784	No	No	0.85
265	26.70	141.26	1.97	1.86	0.64	149.53	1.29	192.44	0.743	No	No	0.80
266	26.80	141.98	1.97	1.84	0.64	149.87	1.28	192.32	0.742	No	No	0.80
267	26.90	146.65	1.95	1.75	0.63	154.22	1.27	195.36	0.773	No	No	0.84
268	27.00	152.40	1.92	1.65	0.62	159.62	1.25	199.23	0.815	No	No	0.88
269	27.10	156.02	1.89	1.57	0.61	162.81	1.23	200.73	4.000	No	No	2.00
270	27.20	156.40	1.88	1.51	0.61	162.70	1.22	199.17	0.815	No	No	0.88
271	27.30	153.19	1.88	1.47	0.61	158.95	1.22	194.36	0.763	No	No	0.82
272	27.40	147.34	1.88	1.43	0.61	152.52	1.23	186.92	0.687	No	No	0.74
273	27.50	139.24	1.89	1.37	0.61	143.76	1.23	176.64	0.593	No	No	0.64
274	27.60	130.22	1.89	1.28	0.61	134.07	1.23	164.76	0.496	No	No	0.54
275	27.70	121.27	1.89	1.18	0.61	124.45	1.23	152.73	0.411	No	No	0.44
276	27.80	114.09	1.88	1.07	0.61	116.70	1.22	142.65	0.350	No	No	0.38
277	27.90	109.39	1.87	0.99	0.61	111.55	1.22	135.64	0.312	No	No	0.34
278	28.00	107.21	1.87	0.96	0.61	109.08	1.22	132.69	0.297	No	No	0.32
279	28.10	107.70	1.89	1.03	0.61	109.46	1.23	134.46	0.306	No	No	0.33
280	28.20	110.28	1.91	1.14	0.62	112.03	1.24	139.30	0.331	No	No	0.36
281	28.30	114.57	1.92	1.25	0.63	116.29	1.25	145.75	0.368	No	No	0.40
282	28.40	120.76	1.92	1.31	0.63	122.38	1.25	153.25	0.415	No	No	0.45
283	28.50	128.38	1.91	1.34	0.62	129.85	1.24	161.60	0.472	No	No	0.51
284	28.60	137.33	1.90	1.38	0.62	138.63	1.24	171.49	0.549	No	No	0.59
285	28.70	146.10	1.90	1.45	0.62	147.25	1.24	181.91	0.640	No	No	0.69
286	28.80	153.76	1.90	1.55	0.62	154.76	1.24	191.87	0.737	No	No	0.80
287	28.90	159.82	1.91	1.64	0.62	160.63	1.25	200.03	4.000	No	No	2.00
288	29.00	164.17	1.92	1.71	0.63	164.70	1.25	205.70	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
289	29.10	166.84	1.92	1.74	0.63	167.05	1.25	208.83	4.000	No	No	2.00
290	29.20	167.23	1.92	1.74	0.63	167.07	1.25	208.99	4.000	No	No	2.00
291	29.30	165.31	1.93	1.76	0.63	164.80	1.26	206.83	4.000	No	No	2.00
292	29.40	162.24	1.94	1.80	0.63	161.42	1.26	203.98	4.000	No	No	2.00
293	29.50	159.54	1.95	1.81	0.64	158.40	1.27	201.12	4.000	No	No	2.00
294	29.60	158.40	1.94	1.76	0.64	156.86	1.26	198.33	0.806	No	No	0.87
295	29.70	158.21	1.92	1.62	0.63	156.18	1.25	194.79	0.767	No	No	0.83
296	29.80	154.57	1.94	1.70	0.63	152.33	1.26	192.38	0.742	No	No	0.80
297	29.90	143.99	2.05	2.26	0.68	141.96	1.36	192.82	0.747	No	No	0.81
298	30.00	135.18	2.13	2.70	0.71	133.15	1.47	195.31	0.773	No	No	0.83
299	30.10	132.28	2.11	2.47	0.70	129.84	1.43	185.80	0.677	No	No	0.73
300	30.20	131.76	2.03	1.92	0.67	128.75	1.33	171.55	0.550	No	No	0.59
301	30.30	123.68	2.03	1.83	0.67	120.49	1.33	160.84	0.467	No	No	0.50
302	30.40	107.40	2.16	2.40	0.72	104.49	1.52	159.11	0.455	No	No	0.49
303	30.50	91.85	2.29	3.09	0.77	89.16	1.88	167.52	0.517	No	No	0.56
304	30.60	84.79	2.36	3.58	0.80	82.08	2.18	178.54	0.609	No	No	0.66
305	30.70	90.92	2.33	3.50	0.79	87.85	2.05	180.41	0.626	No	No	0.68
306	30.80	108.65	2.23	2.96	0.75	104.82	1.69	176.75	0.594	No	No	0.64
307	30.90	128.66	2.11	2.38	0.70	123.87	1.43	177.20	0.597	No	No	0.65
308	31.00	143.23	2.02	1.99	0.67	137.56	1.32	182.22	0.643	No	No	0.69
309	31.10	150.57	1.98	1.83	0.65	144.28	1.29	186.10	0.679	No	No	0.73
310	31.20	153.08	1.97	1.82	0.65	146.38	1.29	188.32	0.701	No	No	0.76
311	31.30	152.85	1.98	1.87	0.65	145.85	1.29	188.71	0.705	No	No	0.76
312	31.40	149.11	2.00	1.95	0.66	141.97	1.31	186.10	0.679	No	No	0.73
313	31.50	141.26	2.04	2.07	0.68	134.15	1.34	180.37	0.626	No	No	0.68
314	31.60	130.34	2.09	2.22	0.69	123.43	1.40	172.88	0.561	No	No	0.61
315	31.70	118.72	2.13	2.33	0.71	112.05	1.47	164.46	0.494	No	No	0.53
316	31.80	108.66	2.16	2.33	0.72	102.19	1.52	155.22	0.428	No	No	0.46
317	31.90	100.38	2.17	2.25	0.73	94.06	1.55	145.43	0.366	No	No	0.40
318	32.00	93.10	2.19	2.21	0.73	86.92	1.59	137.98	4.000	Yes	No	2.00
319	32.10	86.10	2.23	2.35	0.75	80.08	1.70	136.33	4.000	Yes	No	2.00
320	32.20	78.52	2.31	2.74	0.78	72.72	1.96	142.75	4.000	Yes	No	2.00
321	32.30	69.94	2.41	3.36	0.82	64.43	2.43	156.46	4.000	Yes	No	2.00
322	32.40	60.92	2.52	4.13	0.86	55.75	3.16	176.27	4.000	Yes	No	2.00
323	32.50	53.88	2.61	4.82	0.89	48.96	5.62	275.21	4.000	Yes	No	2.00
324	32.60	50.19	2.66	5.31	0.91	45.36	7.90	358.36	4.000	Yes	No	2.00
325	32.70	49.69	2.68	5.68	0.92	44.75	9.24	413.70	3.600	No	No	2.00
326	32.80	52.24	2.68	5.93	0.92	47.00	9.23	433.93	3.600	No	No	2.00
327	32.90	56.89	2.66	6.01	0.92	51.19	8.11	415.14	3.600	No	No	2.00
328	33.00	62.25	2.63	5.88	0.90	56.03	6.59	369.18	3.600	No	No	2.00
329	33.10	68.14	2.59	5.57	0.89	61.33	4.99	305.98	4.000	No	No	2.00
330	33.20	75.90	2.53	5.08	0.86	68.36	3.34	228.35	4.000	No	No	2.00
331	33.30	85.75	2.45	4.49	0.84	77.30	2.66	205.91	4.000	No	No	2.00
332	33.40	93.70	2.39	4.08	0.81	84.46	2.35	198.06	0.803	No	No	0.87
333	33.50	96.01	2.38	3.97	0.81	86.38	2.27	195.78	0.778	No	No	0.85
334	33.60	92.45	2.41	4.15	0.82	82.87	2.40	198.97	0.813	No	No	0.88
335	33.70	84.75	2.46	4.48	0.84	75.56	2.69	203.61	4.000	No	No	2.00
336	33.80	74.88	2.51	4.78	0.86	66.31	3.09	205.05	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
337	33.90	64.13	2.57	4.94	0.88	56.33	4.52	254.57	4.000	No	No	2.00
338	34.00	54.10	2.62	4.91	0.90	47.08	6.28	295.69	3.600	No	No	2.00
339	34.10	46.11	2.67	4.79	0.92	39.73	8.28	329.07	3.600	No	No	2.00
340	34.20	39.59	2.72	4.78	0.94	33.73	4.88	164.76	1.609	No	Yes	1.75
341	34.30	34.09	2.78	4.95	0.96	28.69	5.58	160.14	1.368	No	Yes	1.49
342	34.40	29.36	2.84	5.18	0.99	24.36	6.41	156.10	1.162	No	Yes	1.27
343	34.50	25.02	2.90	5.25	1.00	20.43	7.25	148.09	0.975	No	Yes	1.06
344	34.60	21.00	2.96	5.20	1.00	16.82	8.19	137.74	0.802	No	Yes	0.88
345	34.70	17.76	3.03	5.24	1.00	13.93	9.28	129.28	0.664	No	Yes	0.72
346	34.80	15.83	3.09	5.51	1.00	12.19	10.36	126.28	0.581	No	Yes	0.63
347	34.90	15.33	3.11	5.75	1.00	11.72	10.85	127.20	0.559	No	Yes	0.61
348	35.00	15.28	3.12	5.98	1.00	11.64	11.11	129.34	0.555	No	Yes	0.61
349	35.10	15.62	3.14	6.39	1.00	11.91	11.34	135.08	0.568	No	Yes	0.62
350	35.20	16.74	3.13	6.91	1.00	12.85	11.28	144.97	0.613	No	Yes	0.67
351	35.30	19.92	3.07	6.88	1.00	15.58	10.03	156.19	0.743	No	Yes	0.81
352	35.40	25.11	2.95	6.10	1.00	20.03	8.02	160.65	4.000	Yes	Yes	2.00
353	35.50	32.33	2.81	5.06	0.98	26.27	6.00	157.69	4.000	Yes	Yes	2.00
354	35.60	40.65	2.67	4.14	0.92	33.55	8.70	291.85	4.000	Yes	No	2.00
355	35.70	48.86	2.56	3.48	0.88	40.74	4.21	171.45	4.000	Yes	No	2.00
356	35.80	55.37	2.47	2.98	0.85	46.44	2.81	130.29	4.000	Yes	No	2.00
357	35.90	57.47	2.43	2.68	0.83	48.24	2.54	122.48	4.000	Yes	No	2.00
358	36.00	55.09	2.45	2.69	0.84	46.03	2.64	121.48	4.000	Yes	No	2.00
359	36.10	48.80	2.53	3.09	0.87	40.35	3.42	137.96	4.000	Yes	No	2.00
360	36.20	40.68	2.66	3.82	0.92	33.09	7.69	254.56	4.000	Yes	No	2.00
361	36.30	33.39	2.78	4.62	0.97	26.63	5.62	149.63	4.000	Yes	Yes	2.00
362	36.40	29.34	2.86	5.15	1.00	23.06	6.62	152.64	4.000	Yes	Yes	2.00
363	36.50	29.53	2.85	5.11	0.99	23.16	6.57	152.12	1.105	No	Yes	1.21
364	36.60	32.29	2.81	4.82	0.98	25.47	5.95	151.52	1.215	No	Yes	1.33
365	36.70	34.52	2.78	4.75	0.97	27.32	5.62	153.45	1.303	No	Yes	1.43
366	36.80	34.12	2.80	5.03	0.97	26.88	5.89	158.27	1.282	No	Yes	1.41
367	36.90	31.26	2.86	5.56	1.00	24.34	6.70	163.05	1.161	No	Yes	1.28
368	37.00	28.61	2.92	5.96	1.00	22.06	7.44	164.19	4.000	Yes	Yes	2.00
369	37.10	30.10	2.88	5.59	1.00	23.24	6.92	160.90	4.000	Yes	Yes	2.00
370	37.20	36.63	2.75	4.53	0.96	28.76	5.26	151.31	4.000	Yes	Yes	2.00
371	37.30	46.22	2.60	3.57	0.90	36.94	5.42	200.14	4.000	Yes	No	2.00
372	37.40	55.48	2.49	3.02	0.86	44.85	2.90	130.26	4.000	Yes	No	2.00
373	37.50	62.76	2.43	2.81	0.83	51.02	2.52	128.52	4.000	Yes	No	2.00
374	37.60	68.04	2.39	2.70	0.82	55.45	2.32	128.50	4.000	Yes	No	2.00
375	37.70	71.11	2.36	2.57	0.81	58.00	2.17	126.04	0.266	No	No	0.29
376	37.80	72.57	2.34	2.44	0.80	59.17	2.08	122.99	0.253	No	No	0.28
377	37.90	72.53	2.34	2.42	0.80	59.02	2.07	122.32	0.250	No	No	0.28
378	38.00	71.83	2.34	2.46	0.80	58.28	2.11	122.81	0.252	No	No	0.28
379	38.10	71.07	2.35	2.42	0.80	57.52	2.11	121.29	0.246	No	No	0.27
380	38.20	70.43	2.33	2.31	0.80	56.90	2.06	117.17	0.230	No	No	0.25
381	38.30	69.54	2.33	2.23	0.80	56.06	2.04	114.12	0.218	No	No	0.24
382	38.40	67.93	2.35	2.29	0.80	54.55	2.11	115.14	0.222	No	No	0.25
383	38.50	66.57	2.38	2.51	0.82	53.19	2.28	121.02	0.245	No	No	0.27
384	38.60	67.27	2.41	2.75	0.83	53.57	2.40	128.60	0.278	No	No	0.31

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
385	38.70	70.56	2.41	2.89	0.83	56.15	2.40	134.82	0.308	No	No	0.34
386	38.80	74.92	2.39	2.93	0.82	59.66	2.33	138.76	0.328	No	No	0.37
387	38.90	78.18	2.38	2.95	0.82	62.25	2.27	141.24	0.342	No	No	0.38
388	39.00	79.69	2.38	2.98	0.82	63.35	2.26	143.06	0.352	No	No	0.39
389	39.10	79.93	2.38	3.00	0.82	63.40	2.27	143.96	0.357	No	No	0.40
390	39.20	80.59	2.37	2.97	0.81	63.82	2.25	143.34	0.354	No	No	0.39
391	39.30	82.67	2.35	2.85	0.81	65.46	2.15	140.67	0.339	No	No	0.38
392	39.40	86.56	2.32	2.67	0.79	68.65	2.00	137.30	0.321	No	No	0.36
393	39.50	91.52	2.28	2.49	0.78	72.75	1.85	134.59	0.307	No	No	0.34
394	39.60	96.64	2.24	2.34	0.77	76.97	1.73	133.36	0.301	No	No	0.34
395	39.70	100.82	2.22	2.29	0.76	80.33	1.68	134.76	4.000	Yes	No	2.00
396	39.80	100.16	2.26	2.51	0.77	79.44	1.77	140.84	4.000	Yes	No	2.00
397	39.90	91.82	2.35	3.08	0.81	72.01	2.13	153.15	4.000	Yes	No	2.00
398	40.00	78.37	2.47	3.85	0.85	60.48	2.79	169.03	4.000	Yes	No	2.00
399	40.10	62.81	2.61	4.68	0.90	47.50	5.60	266.17	4.000	Yes	No	2.00
400	40.20	50.47	2.72	5.35	0.95	37.38	4.92	183.83	4.000	Yes	Yes	2.00
401	40.30	42.83	2.81	6.01	0.98	31.15	5.99	186.64	4.000	Yes	Yes	2.00
402	40.40	43.11	2.81	6.11	0.98	31.27	6.04	188.86	4.000	Yes	Yes	2.00
403	40.50	50.11	2.73	5.46	0.95	36.80	5.04	185.32	4.000	Yes	Yes	2.00
404	40.60	60.63	2.61	4.48	0.91	45.25	5.63	254.80	4.000	Yes	No	2.00
405	40.70	71.15	2.48	3.55	0.86	53.85	2.85	153.69	4.000	Yes	No	2.00
406	40.80	79.36	2.38	2.89	0.82	60.65	2.28	138.37	4.000	Yes	No	2.00
407	40.90	84.78	2.34	2.75	0.81	64.99	2.11	136.99	4.000	Yes	No	2.00
408	41.00	87.82	2.34	2.80	0.80	67.27	2.09	140.49	0.338	No	No	0.38
409	41.10	89.49	2.34	2.82	0.80	68.46	2.07	142.01	0.346	No	No	0.39
410	41.20	89.73	2.33	2.72	0.80	68.58	2.02	138.85	0.329	No	No	0.37
411	41.30	88.42	2.33	2.70	0.80	67.39	2.03	137.12	0.320	No	No	0.36
412	41.40	85.38	2.36	2.85	0.81	64.71	2.17	140.14	4.000	Yes	No	2.00
413	41.50	81.32	2.39	3.01	0.82	61.22	2.33	142.45	4.000	Yes	No	2.00
414	41.60	76.93	2.43	3.17	0.84	57.52	2.52	144.69	4.000	Yes	No	2.00
415	41.70	71.43	2.47	3.41	0.86	52.92	2.81	148.63	4.000	Yes	No	2.00
416	41.80	63.51	2.55	3.81	0.89	46.42	3.87	179.51	4.000	Yes	No	2.00
417	41.90	53.29	2.65	4.38	0.92	38.19	7.52	287.13	4.000	Yes	No	2.00
418	42.00	42.53	2.77	4.99	0.97	29.71	5.48	162.75	4.000	Yes	Yes	2.00
419	42.10	34.54	2.86	5.37	1.00	23.55	6.70	157.74	4.000	Yes	Yes	2.00
420	42.20	31.16	2.90	5.30	1.00	21.03	7.16	150.55	4.000	Yes	Yes	2.00
421	42.30	31.50	2.88	5.13	1.00	21.22	6.98	148.03	1.012	No	Yes	1.16
422	42.40	32.59	2.87	5.13	1.00	21.97	6.82	149.89	1.048	No	Yes	1.20
423	42.50	33.35	2.86	5.08	1.00	22.46	6.68	150.00	1.072	No	Yes	1.23
424	42.60	35.87	2.80	4.51	0.98	24.35	5.88	143.15	1.162	No	Yes	1.33
425	42.70	41.37	2.68	3.56	0.94	28.64	9.06	259.40	3.600	No	No	2.00
426	42.80	48.14	2.56	2.81	0.89	33.98	4.11	139.65	0.333	No	No	0.38
427	42.90	52.92	2.50	2.57	0.87	37.69	2.97	111.97	0.211	No	No	0.24
428	43.00	54.26	2.51	2.72	0.87	38.58	2.93	113.09	0.215	No	No	0.25
429	43.10	53.34	2.56	3.15	0.89	37.62	4.10	154.38	0.422	No	No	0.49
430	43.20	52.35	2.61	3.61	0.91	36.62	5.64	206.66	3.600	No	No	2.00
431	43.30	52.52	2.63	3.96	0.92	36.55	6.76	247.19	3.600	No	No	2.00
432	43.40	52.22	2.66	4.24	0.93	36.15	7.85	283.95	3.600	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)												
Point ID	Depth (ft)	q _c (tsf)	I _c	Fr (%)	n	Q _{tn}	K _c	Q _{tn,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
433	43.50	48.54	2.72	4.72	0.95	33.19	4.89	162.45	1.583	No	Yes	1.83
434	43.60	41.40	2.83	5.60	0.99	27.65	6.19	171.06	1.319	No	Yes	1.52
435	43.70	34.45	2.95	6.84	1.00	22.61	7.96	179.95	1.078	No	Yes	1.25
436	43.80	31.79	3.01	7.64	1.00	20.68	8.97	185.44	0.986	No	Yes	1.14
437	43.90	34.60	2.97	7.36	1.00	22.61	8.32	188.01	4.000	Yes	Yes	2.00
438	44.00	42.45	2.86	6.26	1.00	28.08	6.58	184.73	4.000	Yes	Yes	2.00
439	44.10	56.31	2.68	4.81	0.94	38.44	8.88	341.33	4.000	Yes	No	2.00
440	44.20	76.28	2.48	3.54	0.86	53.80	2.85	153.28	4.000	Yes	No	2.00
441	44.30	99.38	2.32	2.81	0.80	71.80	2.01	144.35	4.000	Yes	No	2.00
442	44.40	119.56	2.22	2.46	0.76	87.63	1.67	145.92	4.000	Yes	No	2.00
443	44.50	132.51	2.17	2.30	0.74	97.74	1.54	150.24	4.000	Yes	No	2.00
444	44.60	138.38	2.13	2.16	0.73	102.38	1.47	150.70	4.000	Yes	No	2.00
445	44.70	140.97	2.15	2.30	0.74	103.95	1.50	155.94	0.433	No	No	0.51
446	44.80	145.61	2.19	2.72	0.75	106.65	1.60	170.66	0.542	No	No	0.63
447	44.90	154.46	2.20	2.90	0.76	112.95	1.61	182.24	0.643	No	No	0.75
448	45.00	166.62	2.15	2.66	0.74	122.52	1.50	183.93	0.659	No	No	0.77
449	45.10	178.48	2.07	2.24	0.71	132.40	1.38	182.40	0.644	No	No	0.76
450	45.20	186.02	2.02	2.03	0.69	138.62	1.33	184.20	0.661	No	No	0.78
451	45.30	188.08	2.02	2.01	0.69	140.04	1.32	185.25	0.671	No	No	0.79
452	45.40	185.50	2.02	2.02	0.69	137.74	1.33	183.02	0.650	No	No	0.77
453	45.50	181.44	2.03	2.04	0.69	134.28	1.34	179.72	0.620	No	No	0.73
454	45.60	177.58	2.04	2.04	0.70	131.04	1.35	176.34	0.590	No	No	0.70
455	45.70	174.36	2.05	2.04	0.70	128.30	1.35	173.50	0.566	No	No	0.67
456	45.80	172.20	2.05	2.04	0.70	126.39	1.36	171.53	0.549	No	No	0.65
457	45.90	170.69	2.06	2.05	0.70	124.98	1.36	170.25	0.539	No	No	0.64
458	46.00	169.69	2.06	2.07	0.71	123.92	1.37	169.73	0.535	No	No	0.63
459	46.10	168.85	2.07	2.11	0.71	122.93	1.38	169.73	0.535	No	No	0.63
460	46.20	168.16	2.08	2.17	0.71	122.03	1.39	170.19	0.538	No	No	0.64
461	46.30	168.23	2.09	2.23	0.72	121.73	1.41	171.23	0.547	No	No	0.65
462	46.40	169.90	2.09	2.24	0.72	122.75	1.41	172.53	0.558	No	No	0.66
463	46.50	173.64	2.08	2.18	0.71	125.52	1.39	173.95	0.570	No	No	0.68
464	46.60	178.99	2.05	2.07	0.70	129.70	1.35	175.62	0.584	No	No	0.70
465	46.70	184.20	2.02	1.94	0.69	133.83	1.32	177.31	0.598	No	No	0.72
466	46.80	187.77	1.99	1.83	0.68	136.74	1.30	178.03	0.605	No	No	0.72
467	46.90	188.69	1.97	1.70	0.67	137.65	1.28	176.71	0.593	No	No	0.71
468	47.00	186.98	1.95	1.59	0.66	136.54	1.27	173.38	0.565	No	No	0.68
469	47.10	183.33	1.94	1.51	0.66	133.82	1.26	168.99	0.529	No	No	0.64
470	47.20	178.78	1.94	1.47	0.66	130.22	1.26	164.54	0.494	No	No	0.59
471	47.30	174.33	1.95	1.48	0.67	126.56	1.27	160.75	0.466	No	No	0.56
472	47.40	170.46	1.96	1.51	0.67	123.28	1.28	157.73	0.445	No	No	0.54
473	47.50	167.19	1.98	1.54	0.68	120.45	1.29	155.30	0.428	No	No	0.52
474	47.60	164.34	1.99	1.57	0.68	117.95	1.30	153.25	0.415	No	No	0.50
475	47.70	161.94	2.00	1.61	0.69	115.81	1.31	151.63	0.404	No	No	0.49
476	47.80	159.85	2.01	1.64	0.69	113.93	1.32	150.26	0.396	No	No	0.48
477	47.90	158.50	2.02	1.68	0.69	112.59	1.33	149.62	0.391	No	No	0.47
478	48.00	158.82	2.03	1.72	0.70	112.51	1.34	150.31	0.396	No	No	0.48
479	48.10	160.82	2.04	1.77	0.70	113.66	1.34	152.65	0.411	No	No	0.50
480	48.20	163.04	2.05	1.84	0.70	114.92	1.35	155.37	0.429	No	No	0.52

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
481	48.30	164.06	2.06	1.92	0.71	115.25	1.37	157.39	0.443	No	No	0.54
482	48.40	164.39	2.07	1.99	0.71	115.09	1.38	158.78	0.452	No	No	0.55
483	48.50	165.33	2.08	2.03	0.72	115.47	1.39	160.12	0.462	No	No	0.56
484	48.60	167.37	2.08	2.04	0.72	116.74	1.39	161.72	0.473	No	No	0.58
485	48.70	169.66	2.07	2.04	0.71	118.23	1.38	163.29	0.485	No	No	0.59
486	48.80	171.13	2.07	2.07	0.72	119.04	1.38	164.67	0.495	No	No	0.61
487	48.90	171.49	2.09	2.15	0.72	118.87	1.40	166.37	0.508	No	No	0.62
488	49.00	171.23	2.11	2.28	0.73	118.08	1.43	168.94	0.528	No	No	0.65
489	49.10	171.53	2.13	2.44	0.74	117.67	1.47	172.78	0.560	No	No	0.69
490	49.20	174.62	2.14	2.55	0.74	119.41	1.49	177.75	0.602	No	No	0.74
491	49.30	181.47	2.13	2.58	0.74	124.10	1.47	182.96	0.650	No	No	0.80
492	49.40	191.66	2.11	2.50	0.73	131.49	1.43	188.20	0.700	No	No	0.86
493	49.50	202.91	2.07	2.37	0.72	139.89	1.38	193.23	0.751	No	No	0.93
494	49.60	212.53	2.04	2.22	0.70	147.20	1.34	197.41	0.795	No	No	0.98
495	49.70	219.60	2.01	2.09	0.69	152.68	1.31	200.36	4.000	No	No	2.00
496	49.80	223.07	1.99	2.00	0.68	155.33	1.30	201.52	4.000	No	No	2.00

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q_t :	Total cone resistance
I_c :	Soil behavior type index
Fr:	Normalized friction ratio (%)
n:	Stress exponent
Q_{tn} :	Normalized cone resistance
K_c :	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Normalized and adjusted cone resistance
CRR _{7.5} :	Cyclic resistance ratio for $M_w=7.5$
FS:	Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
0.30	2.00	0.00	0.00	0.10	0.00	0.40	2.00	0.00	0.00	0.10	0.00
0.50	2.00	0.00	0.00	0.10	0.00	0.60	2.00	0.00	0.00	0.10	0.00
0.70	2.00	0.00	0.00	0.10	0.00	0.80	2.00	0.00	0.00	0.10	0.00
0.90	2.00	0.00	0.00	0.10	0.00	1.00	2.00	0.00	0.00	0.10	0.00
1.10	2.00	0.00	0.00	0.10	0.00	1.20	2.00	0.00	0.00	0.10	0.00
1.30	2.00	0.00	0.00	0.10	0.00	1.40	2.00	0.00	0.00	0.10	0.00
1.50	2.00	0.00	0.00	0.10	0.00	1.60	2.00	0.00	0.00	0.10	0.00
1.70	2.00	0.00	0.00	0.10	0.00	1.80	2.00	0.00	0.00	0.10	0.00
1.90	2.00	0.00	0.00	0.10	0.00	2.00	2.00	0.00	0.00	0.10	0.00
2.10	2.00	0.00	0.00	0.10	0.00	2.20	2.00	0.00	0.00	0.10	0.00
2.30	2.00	0.00	0.00	0.10	0.00	2.40	2.00	0.00	0.00	0.10	0.00
2.50	2.00	0.00	0.00	0.10	0.00	2.60	2.00	0.00	0.00	0.10	0.00
2.70	2.00	0.00	0.00	0.10	0.00	2.80	2.00	0.00	0.00	0.10	0.00
2.90	2.00	0.00	0.00	0.10	0.00	3.00	2.00	0.00	0.00	0.10	0.00
3.10	2.00	0.00	0.00	0.10	0.00	3.20	2.00	0.00	0.00	0.10	0.00
3.30	2.00	0.00	0.00	0.10	0.00	3.40	2.00	0.00	0.00	0.10	0.00
3.50	2.00	0.00	0.00	0.10	0.00	3.60	2.00	0.00	0.00	0.10	0.00
3.70	2.00	0.00	0.00	0.10	0.00	3.80	2.00	0.00	0.00	0.10	0.00
3.90	2.00	0.00	0.00	0.10	0.00	4.00	2.00	0.00	0.00	0.10	0.00
4.10	2.00	0.00	0.00	0.10	0.00	4.20	2.00	0.00	0.00	0.10	0.00
4.30	2.00	0.00	0.00	0.10	0.00	4.40	2.00	0.00	0.00	0.10	0.00
4.50	2.00	0.00	0.00	0.10	0.00	4.60	2.00	0.00	0.00	0.10	0.00
4.70	2.00	0.00	0.00	0.10	0.00	4.80	2.00	0.00	0.00	0.10	0.00
4.90	2.00	0.00	0.00	0.10	0.00	5.00	2.00	0.00	0.00	0.10	0.00
5.10	2.00	0.00	0.00	0.10	0.00	5.20	2.00	0.00	0.00	0.10	0.00
5.30	2.00	0.00	0.00	0.10	0.00	5.40	2.00	0.00	0.00	0.10	0.00
5.50	2.00	0.00	0.00	0.10	0.00	5.60	2.00	0.00	0.00	0.10	0.00
5.70	2.00	0.00	0.00	0.10	0.00	5.80	2.00	0.00	0.00	0.10	0.00
5.90	2.00	0.00	0.00	0.10	0.00	6.00	2.00	0.00	0.00	0.10	0.00
6.10	2.00	0.00	0.00	0.10	0.00	6.20	2.00	0.00	0.00	0.10	0.00
6.30	2.00	0.00	0.00	0.10	0.00	6.40	2.00	0.00	0.00	0.10	0.00
6.50	2.00	0.00	0.00	0.10	0.00	6.60	2.00	0.00	0.00	0.10	0.00
6.70	2.00	0.00	0.00	0.10	0.00	6.80	2.00	0.00	0.00	0.10	0.00
6.90	2.00	0.00	0.00	0.10	0.00	7.00	2.00	0.00	0.00	0.10	0.00
7.10	2.00	0.00	0.00	0.10	0.00	7.20	2.00	0.00	0.00	0.10	0.00
7.30	2.00	0.00	0.00	0.10	0.00	7.40	2.00	0.00	0.00	0.10	0.00
7.50	2.00	0.00	0.00	0.10	0.00	7.60	2.00	0.00	0.00	0.10	0.00
7.70	2.00	0.00	0.00	0.10	0.00	7.80	2.00	0.00	0.00	0.10	0.00
7.90	2.00	0.00	0.00	0.10	0.00	8.00	2.00	0.00	0.00	0.10	0.00
8.10	2.00	0.00	0.00	0.10	0.00	8.20	2.00	0.00	0.00	0.10	0.00
8.30	1.80	0.00	0.00	0.10	0.00	8.40	1.65	0.00	0.00	0.10	0.00
8.50	1.56	0.00	0.00	0.10	0.00	8.60	1.53	0.00	0.00	0.10	0.00
8.70	1.48	0.00	0.00	0.10	0.00	8.80	1.41	0.00	0.00	0.10	0.00
8.90	1.37	0.00	0.00	0.10	0.00	9.00	1.39	0.00	0.00	0.10	0.00
9.10	1.44	0.00	0.00	0.10	0.00	9.20	1.47	0.00	0.00	0.10	0.00
9.30	1.47	0.00	0.00	0.10	0.00	9.40	1.46	0.00	0.00	0.10	0.00
9.50	1.45	0.00	0.00	0.10	0.00	9.60	1.49	0.00	0.00	0.10	0.00
9.70	1.61	0.00	0.00	0.10	0.00	9.80	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
9.90	2.00	0.00	0.00	0.10	0.00	10.00	2.00	0.00	0.00	0.10	0.00
10.10	2.00	0.00	0.00	0.10	0.00	10.20	1.17	0.00	0.00	0.10	0.00
10.30	0.83	0.00	0.00	0.10	0.04	10.40	0.74	0.00	0.00	0.10	0.07
10.50	0.60	0.00	0.00	0.10	0.10	10.60	0.49	0.00	0.00	0.10	0.13
10.70	0.45	0.00	0.00	0.10	0.14	10.80	0.43	0.00	0.00	0.10	0.14
10.90	0.41	0.00	0.00	0.10	0.15	11.00	0.40	0.00	0.00	0.10	0.15
11.10	0.40	0.00	0.00	0.10	0.15	11.20	0.42	0.00	0.00	0.10	0.15
11.30	0.45	0.00	0.00	0.10	0.14	11.40	0.53	0.00	0.00	0.10	0.12
11.50	0.66	0.00	0.00	0.10	0.09	11.60	0.77	0.00	0.00	0.10	0.06
11.70	0.87	0.00	0.00	0.10	0.03	11.80	1.00	0.00	0.00	0.10	0.00
11.90	1.19	0.00	0.00	0.10	0.00	12.00	1.33	0.00	0.00	0.10	0.00
12.10	1.39	0.00	0.00	0.10	0.00	12.20	1.36	0.00	0.00	0.10	0.00
12.30	1.27	0.00	0.00	0.10	0.00	12.40	1.09	0.00	0.00	0.10	0.00
12.50	0.86	0.00	0.00	0.10	0.04	12.60	0.61	0.00	0.00	0.10	0.10
12.70	0.40	0.00	0.00	0.10	0.15	12.80	0.30	0.00	0.00	0.10	0.17
12.90	0.34	0.00	0.00	0.10	0.16	13.00	0.42	0.00	0.00	0.10	0.14
13.10	0.47	0.00	0.00	0.10	0.13	13.20	0.48	0.00	0.00	0.10	0.13
13.30	0.51	0.00	0.00	0.10	0.12	13.40	0.55	0.00	0.00	0.10	0.11
13.50	0.58	0.00	0.00	0.10	0.10	13.60	0.63	0.00	0.00	0.10	0.09
13.70	0.76	0.00	0.00	0.10	0.06	13.80	1.01	0.00	0.00	0.10	0.00
13.90	1.21	0.00	0.00	0.10	0.00	14.00	1.29	0.00	0.00	0.10	0.00
14.10	1.23	0.00	0.00	0.10	0.00	14.20	2.00	0.00	0.00	0.10	0.00
14.30	2.00	0.00	0.00	0.10	0.00	14.40	2.00	0.00	0.00	0.10	0.00
14.50	2.00	0.00	0.00	0.10	0.00	14.60	2.00	0.00	0.00	0.10	0.00
14.70	2.00	0.00	0.00	0.10	0.00	14.80	2.00	0.00	0.00	0.10	0.00
14.90	2.00	0.00	0.00	0.10	0.00	15.00	2.00	0.00	0.00	0.10	0.00
15.10	2.00	0.00	0.00	0.10	0.00	15.20	2.00	0.00	0.00	0.10	0.00
15.30	2.00	0.00	0.00	0.10	0.00	15.40	2.00	0.00	0.00	0.10	0.00
15.50	2.00	0.00	0.00	0.10	0.00	15.60	2.00	0.00	0.00	0.10	0.00
15.70	2.00	0.00	0.00	0.10	0.00	15.80	0.43	0.00	0.00	0.10	0.13
15.90	0.43	0.00	0.00	0.10	0.13	16.00	0.42	0.00	0.00	0.10	0.13
16.10	0.38	0.00	0.00	0.10	0.14	16.20	0.33	0.00	0.00	0.10	0.15
16.30	0.29	0.00	0.00	0.10	0.16	16.40	0.29	0.00	0.00	0.10	0.16
16.50	0.29	0.00	0.00	0.10	0.16	16.60	0.29	0.00	0.00	0.10	0.16
16.70	0.28	0.00	0.00	0.10	0.16	16.80	0.28	0.00	0.00	0.10	0.16
16.90	0.28	0.00	0.00	0.10	0.16	17.00	0.28	0.00	0.00	0.10	0.16
17.10	0.27	0.00	0.00	0.10	0.16	17.20	0.28	0.00	0.00	0.10	0.16
17.30	0.37	0.00	0.00	0.10	0.14	17.40	0.50	0.00	0.00	0.10	0.11
17.50	0.66	0.00	0.00	0.10	0.08	17.60	0.77	0.00	0.00	0.10	0.05
17.70	0.86	0.00	0.00	0.10	0.03	17.80	0.91	0.00	0.00	0.10	0.02
17.90	0.88	0.00	0.00	0.10	0.03	18.00	0.82	0.00	0.00	0.10	0.04
18.10	0.74	0.00	0.00	0.10	0.06	18.20	0.67	0.00	0.00	0.10	0.07
18.30	0.60	0.00	0.00	0.10	0.09	18.40	0.52	0.00	0.00	0.10	0.10
18.50	0.46	0.00	0.00	0.10	0.12	18.60	0.42	0.00	0.00	0.10	0.13
18.70	0.42	0.00	0.00	0.10	0.13	18.80	0.43	0.00	0.00	0.10	0.12
18.90	0.46	0.00	0.00	0.10	0.12	19.00	0.49	0.00	0.00	0.10	0.11
19.10	0.49	0.00	0.00	0.10	0.11	19.20	0.46	0.00	0.00	0.10	0.12
19.30	0.42	0.00	0.00	0.10	0.12	19.40	0.40	0.00	0.00	0.10	0.13

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
19.50	0.45	0.00	0.00	0.10	0.12	19.60	0.54	0.00	0.00	0.10	0.10
19.70	0.66	0.00	0.00	0.10	0.07	19.80	0.92	0.00	0.00	0.10	0.02
19.90	1.35	0.00	0.00	0.10	0.00	20.00	2.00	0.00	0.00	0.10	0.00
20.10	1.24	0.00	0.00	0.10	0.00	20.20	0.72	0.00	0.00	0.10	0.06
20.30	0.46	0.00	0.00	0.10	0.11	20.40	0.42	0.00	0.00	0.10	0.12
20.50	0.40	0.00	0.00	0.10	0.13	20.60	0.39	0.00	0.00	0.10	0.13
20.70	0.37	0.00	0.00	0.10	0.13	20.80	0.38	0.00	0.00	0.10	0.13
20.90	0.44	0.00	0.00	0.10	0.12	21.00	0.59	0.00	0.00	0.10	0.09
21.10	0.79	0.00	0.00	0.10	0.04	21.20	0.95	0.00	0.00	0.10	0.01
21.30	1.00	0.00	0.00	0.10	0.00	21.40	0.95	0.00	0.00	0.10	0.01
21.50	0.82	0.00	0.00	0.10	0.04	21.60	0.66	0.00	0.00	0.10	0.07
21.70	0.50	0.00	0.00	0.10	0.10	21.80	0.36	0.00	0.00	0.10	0.13
21.90	0.30	0.00	0.00	0.10	0.14	22.00	0.30	0.00	0.00	0.10	0.14
22.10	0.35	0.00	0.00	0.10	0.13	22.20	0.42	0.00	0.00	0.10	0.12
22.30	0.45	0.00	0.00	0.10	0.11	22.40	0.49	0.00	0.00	0.10	0.10
22.50	0.55	0.00	0.00	0.10	0.09	22.60	0.57	0.00	0.00	0.10	0.09
22.70	0.53	0.00	0.00	0.10	0.09	22.80	0.45	0.00	0.00	0.10	0.11
22.90	0.39	0.00	0.00	0.10	0.12	23.00	0.39	0.00	0.00	0.10	0.12
23.10	0.43	0.00	0.00	0.10	0.11	23.20	0.48	0.00	0.00	0.10	0.10
23.30	0.51	0.00	0.00	0.10	0.10	23.40	0.51	0.00	0.00	0.10	0.10
23.50	0.52	0.00	0.00	0.10	0.09	23.60	0.55	0.00	0.00	0.10	0.09
23.70	0.56	0.00	0.00	0.10	0.09	23.80	0.54	0.00	0.00	0.10	0.09
23.90	0.54	0.00	0.00	0.10	0.09	24.00	0.68	0.00	0.00	0.10	0.06
24.10	0.99	0.00	0.00	0.10	0.00	24.20	1.34	0.00	0.00	0.10	0.00
24.30	0.74	0.00	0.00	0.10	0.05	24.40	0.37	0.00	0.00	0.10	0.12
24.50	0.54	0.00	0.00	0.10	0.09	24.60	1.39	0.00	0.00	0.10	0.00
24.70	1.21	0.00	0.00	0.10	0.00	24.80	1.17	0.00	0.00	0.10	0.00
24.90	1.23	0.00	0.00	0.10	0.00	25.00	1.26	0.00	0.00	0.10	0.00
25.10	1.29	0.00	0.00	0.10	0.00	25.20	1.34	0.00	0.00	0.10	0.00
25.30	1.34	0.00	0.00	0.10	0.00	25.40	1.32	0.00	0.00	0.10	0.00
25.50	2.00	0.00	0.00	0.10	0.00	25.60	2.00	0.00	0.00	0.10	0.00
25.70	2.00	0.00	0.00	0.10	0.00	25.80	2.00	0.00	0.00	0.10	0.00
25.90	2.00	0.00	0.00	0.10	0.00	26.00	2.00	0.00	0.00	0.10	0.00
26.10	2.00	0.00	0.00	0.10	0.00	26.20	2.00	0.00	0.00	0.10	0.00
26.30	2.00	0.00	0.00	0.10	0.00	26.40	2.00	0.00	0.00	0.10	0.00
26.50	2.00	0.00	0.00	0.10	0.00	26.60	0.85	0.00	0.00	0.10	0.03
26.70	0.80	0.00	0.00	0.10	0.04	26.80	0.80	0.00	0.00	0.10	0.04
26.90	0.84	0.00	0.00	0.10	0.03	27.00	0.88	0.00	0.00	0.10	0.02
27.10	2.00	0.00	0.00	0.10	0.00	27.20	0.88	0.00	0.00	0.10	0.02
27.30	0.82	0.00	0.00	0.10	0.03	27.40	0.74	0.00	0.00	0.10	0.05
27.50	0.64	0.00	0.00	0.10	0.06	27.60	0.54	0.00	0.00	0.10	0.08
27.70	0.44	0.00	0.00	0.10	0.10	27.80	0.38	0.62	0.37	0.10	0.11
27.90	0.34	0.66	0.34	0.10	0.12	28.00	0.32	0.68	0.33	0.10	0.12
28.10	0.33	0.67	0.34	0.10	0.12	28.20	0.36	0.64	0.36	0.10	0.11
28.30	0.40	0.00	0.00	0.10	0.10	28.40	0.45	0.00	0.00	0.10	0.10
28.50	0.51	0.00	0.00	0.10	0.08	28.60	0.59	0.00	0.00	0.10	0.07
28.70	0.69	0.00	0.00	0.10	0.05	28.80	0.80	0.00	0.00	0.10	0.04
28.90	2.00	0.00	0.00	0.10	0.00	29.00	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
29.10	2.00	0.00	0.00	0.10	0.00	29.20	2.00	0.00	0.00	0.10	0.00
29.30	2.00	0.00	0.00	0.10	0.00	29.40	2.00	0.00	0.00	0.10	0.00
29.50	2.00	0.00	0.00	0.10	0.00	29.60	0.87	0.00	0.00	0.10	0.02
29.70	0.83	0.00	0.00	0.10	0.03	29.80	0.80	0.00	0.00	0.10	0.03
29.90	0.81	0.00	0.00	0.10	0.03	30.00	0.83	0.00	0.00	0.10	0.03
30.10	0.73	0.00	0.00	0.10	0.04	30.20	0.59	0.00	0.00	0.10	0.07
30.30	0.50	0.00	0.00	0.10	0.08	30.40	0.49	0.00	0.00	0.10	0.08
30.50	0.56	0.00	0.00	0.10	0.07	30.60	0.66	0.00	0.00	0.10	0.06
30.70	0.68	0.00	0.00	0.10	0.05	30.80	0.64	0.00	0.00	0.10	0.06
30.90	0.65	0.00	0.00	0.10	0.06	31.00	0.69	0.00	0.00	0.10	0.05
31.10	0.73	0.00	0.00	0.10	0.04	31.20	0.76	0.00	0.00	0.10	0.04
31.30	0.76	0.00	0.00	0.10	0.04	31.40	0.73	0.00	0.00	0.10	0.04
31.50	0.68	0.00	0.00	0.10	0.05	31.60	0.61	0.00	0.00	0.10	0.06
31.70	0.53	0.00	0.00	0.10	0.07	31.80	0.46	0.00	0.00	0.10	0.08
31.90	0.40	0.00	0.00	0.10	0.09	32.00	2.00	0.00	0.00	0.10	0.00
32.10	2.00	0.00	0.00	0.10	0.00	32.20	2.00	0.00	0.00	0.10	0.00
32.30	2.00	0.00	0.00	0.10	0.00	32.40	2.00	0.00	0.00	0.10	0.00
32.50	2.00	0.00	0.00	0.10	0.00	32.60	2.00	0.00	0.00	0.10	0.00
32.70	2.00	0.00	0.00	0.10	0.00	32.80	2.00	0.00	0.00	0.10	0.00
32.90	2.00	0.00	0.00	0.10	0.00	33.00	2.00	0.00	0.00	0.10	0.00
33.10	2.00	0.00	0.00	0.10	0.00	33.20	2.00	0.00	0.00	0.10	0.00
33.30	2.00	0.00	0.00	0.10	0.00	33.40	0.87	0.00	0.00	0.10	0.02
33.50	0.85	0.00	0.00	0.10	0.02	33.60	0.88	0.00	0.00	0.10	0.02
33.70	2.00	0.00	0.00	0.10	0.00	33.80	2.00	0.00	0.00	0.10	0.00
33.90	2.00	0.00	0.00	0.10	0.00	34.00	2.00	0.00	0.00	0.10	0.00
34.10	2.00	0.00	0.00	0.10	0.00	34.20	1.75	0.00	0.00	0.10	0.00
34.30	1.49	0.00	0.00	0.10	0.00	34.40	1.27	0.00	0.00	0.10	0.00
34.50	1.06	0.00	0.00	0.10	0.00	34.60	0.88	0.00	0.00	0.10	0.02
34.70	0.72	0.00	0.00	0.10	0.04	34.80	0.63	0.00	0.00	0.10	0.05
34.90	0.61	0.00	0.00	0.10	0.06	35.00	0.61	0.00	0.00	0.10	0.06
35.10	0.62	0.00	0.00	0.10	0.05	35.20	0.67	0.00	0.00	0.10	0.05
35.30	0.81	0.00	0.00	0.10	0.03	35.40	2.00	0.00	0.00	0.10	0.00
35.50	2.00	0.00	0.00	0.10	0.00	35.60	2.00	0.00	0.00	0.10	0.00
35.70	2.00	0.00	0.00	0.10	0.00	35.80	2.00	0.00	0.00	0.10	0.00
35.90	2.00	0.00	0.00	0.10	0.00	36.00	2.00	0.00	0.00	0.10	0.00
36.10	2.00	0.00	0.00	0.10	0.00	36.20	2.00	0.00	0.00	0.10	0.00
36.30	2.00	0.00	0.00	0.10	0.00	36.40	2.00	0.00	0.00	0.10	0.00
36.50	1.21	0.00	0.00	0.10	0.00	36.60	1.33	0.00	0.00	0.10	0.00
36.70	1.43	0.00	0.00	0.10	0.00	36.80	1.41	0.00	0.00	0.10	0.00
36.90	1.28	0.00	0.00	0.10	0.00	37.00	2.00	0.00	0.00	0.10	0.00
37.10	2.00	0.00	0.00	0.10	0.00	37.20	2.00	0.00	0.00	0.10	0.00
37.30	2.00	0.00	0.00	0.10	0.00	37.40	2.00	0.00	0.00	0.10	0.00
37.50	2.00	0.00	0.00	0.10	0.00	37.60	2.00	0.00	0.00	0.10	0.00
37.70	0.29	0.71	0.32	0.10	0.09	37.80	0.28	0.72	0.31	0.10	0.09
37.90	0.28	0.72	0.31	0.10	0.09	38.00	0.28	0.72	0.31	0.10	0.09
38.10	0.27	0.73	0.31	0.10	0.09	38.20	0.25	0.75	0.30	0.10	0.09
38.30	0.24	0.76	0.29	0.10	0.10	38.40	0.25	0.75	0.30	0.10	0.10
38.50	0.27	0.73	0.31	0.10	0.09	38.60	0.31	0.69	0.33	0.10	0.09

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
38.70	0.34	0.66	0.35	0.10	0.08	38.80	0.37	0.63	0.36	0.10	0.08
38.90	0.38	0.00	0.00	0.10	0.08	39.00	0.39	0.00	0.00	0.10	0.08
39.10	0.40	0.00	0.00	0.10	0.07	39.20	0.39	0.00	0.00	0.10	0.07
39.30	0.38	0.62	0.37	0.10	0.08	39.40	0.36	0.64	0.36	0.10	0.08
39.50	0.34	0.66	0.35	0.10	0.08	39.60	0.34	0.66	0.34	0.10	0.08
39.70	2.00	0.00	0.00	0.10	0.00	39.80	2.00	0.00	0.00	0.10	0.00
39.90	2.00	0.00	0.00	0.10	0.00	40.00	2.00	0.00	0.00	0.10	0.00
40.10	2.00	0.00	0.00	0.10	0.00	40.20	2.00	0.00	0.00	0.10	0.00
40.30	2.00	0.00	0.00	0.10	0.00	40.40	2.00	0.00	0.00	0.10	0.00
40.50	2.00	0.00	0.00	0.10	0.00	40.60	2.00	0.00	0.00	0.10	0.00
40.70	2.00	0.00	0.00	0.10	0.00	40.80	2.00	0.00	0.00	0.10	0.00
40.90	2.00	0.00	0.00	0.10	0.00	41.00	0.38	0.00	0.00	0.10	0.07
41.10	0.39	0.00	0.00	0.10	0.07	41.20	0.37	0.63	0.37	0.10	0.07
41.30	0.36	0.64	0.36	0.10	0.07	41.40	2.00	0.00	0.00	0.10	0.00
41.50	2.00	0.00	0.00	0.10	0.00	41.60	2.00	0.00	0.00	0.10	0.00
41.70	2.00	0.00	0.00	0.10	0.00	41.80	2.00	0.00	0.00	0.10	0.00
41.90	2.00	0.00	0.00	0.10	0.00	42.00	2.00	0.00	0.00	0.10	0.00
42.10	2.00	0.00	0.00	0.10	0.00	42.20	2.00	0.00	0.00	0.10	0.00
42.30	1.16	0.00	0.00	0.10	0.00	42.40	1.20	0.00	0.00	0.10	0.00
42.50	1.23	0.00	0.00	0.10	0.00	42.60	1.33	0.00	0.00	0.10	0.00
42.70	2.00	0.00	0.00	0.10	0.00	42.80	0.38	0.00	0.00	0.10	0.07
42.90	0.24	0.76	0.29	0.10	0.08	43.00	0.25	0.75	0.30	0.10	0.08
43.10	0.49	0.00	0.00	0.10	0.05	43.20	2.00	0.00	0.00	0.10	0.00
43.30	2.00	0.00	0.00	0.10	0.00	43.40	2.00	0.00	0.00	0.10	0.00
43.50	1.83	0.00	0.00	0.10	0.00	43.60	1.52	0.00	0.00	0.10	0.00
43.70	1.25	0.00	0.00	0.10	0.00	43.80	1.14	0.00	0.00	0.10	0.00
43.90	2.00	0.00	0.00	0.10	0.00	44.00	2.00	0.00	0.00	0.10	0.00
44.10	2.00	0.00	0.00	0.10	0.00	44.20	2.00	0.00	0.00	0.10	0.00
44.30	2.00	0.00	0.00	0.10	0.00	44.40	2.00	0.00	0.00	0.10	0.00
44.50	2.00	0.00	0.00	0.10	0.00	44.60	2.00	0.00	0.00	0.10	0.00
44.70	0.51	0.00	0.00	0.10	0.05	44.80	0.63	0.00	0.00	0.10	0.04
44.90	0.75	0.00	0.00	0.10	0.02	45.00	0.77	0.00	0.00	0.10	0.02
45.10	0.76	0.00	0.00	0.10	0.02	45.20	0.78	0.00	0.00	0.10	0.02
45.30	0.79	0.00	0.00	0.10	0.02	45.40	0.77	0.00	0.00	0.10	0.02
45.50	0.73	0.00	0.00	0.10	0.03	45.60	0.70	0.00	0.00	0.10	0.03
45.70	0.67	0.00	0.00	0.10	0.03	45.80	0.65	0.00	0.00	0.10	0.03
45.90	0.64	0.00	0.00	0.10	0.03	46.00	0.63	0.00	0.00	0.10	0.03
46.10	0.63	0.00	0.00	0.10	0.03	46.20	0.64	0.00	0.00	0.10	0.03
46.30	0.65	0.00	0.00	0.10	0.03	46.40	0.66	0.00	0.00	0.10	0.03
46.50	0.68	0.00	0.00	0.10	0.03	46.60	0.70	0.00	0.00	0.10	0.03
46.70	0.72	0.00	0.00	0.10	0.03	46.80	0.72	0.00	0.00	0.10	0.02
46.90	0.71	0.00	0.00	0.10	0.03	47.00	0.68	0.00	0.00	0.10	0.03
47.10	0.64	0.00	0.00	0.10	0.03	47.20	0.59	0.00	0.00	0.10	0.03
47.30	0.56	0.00	0.00	0.10	0.04	47.40	0.54	0.00	0.00	0.10	0.04
47.50	0.52	0.00	0.00	0.10	0.04	47.60	0.50	0.00	0.00	0.10	0.04
47.70	0.49	0.00	0.00	0.10	0.04	47.80	0.48	0.00	0.00	0.10	0.04
47.90	0.47	0.00	0.00	0.10	0.04	48.00	0.48	0.00	0.00	0.10	0.04
48.10	0.50	0.00	0.00	0.10	0.04	48.20	0.52	0.00	0.00	0.10	0.04

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F _L	w _z	d _z	LPI	Depth (ft)	FS	F _L	w _z	d _z	LPI
48.30	0.54	0.00	0.00	0.10	0.04	48.40	0.55	0.00	0.00	0.10	0.04
48.50	0.56	0.00	0.00	0.10	0.03	48.60	0.58	0.00	0.00	0.10	0.03
48.70	0.59	0.00	0.00	0.10	0.03	48.80	0.61	0.00	0.00	0.10	0.03
48.90	0.62	0.00	0.00	0.10	0.03	49.00	0.65	0.00	0.00	0.10	0.03
49.10	0.69	0.00	0.00	0.10	0.02	49.20	0.74	0.00	0.00	0.10	0.02
49.30	0.80	0.00	0.00	0.10	0.02	49.40	0.86	0.00	0.00	0.10	0.01
49.50	0.93	0.00	0.00	0.10	0.01	49.60	0.98	0.00	0.00	0.10	0.00
49.70	2.00	0.00	0.00	0.10	0.00	49.80	2.00	0.00	0.00	0.10	0.00

Overall liquefaction potential: 18.72

LPI = 0.00 - Liquefaction risk very low

LPI between 0.00 and 5.00 - Liquefaction risk low

LPI between 5.00 and 15.00 - Liquefaction risk high

LPI > 15.00 - Liquefaction risk very high

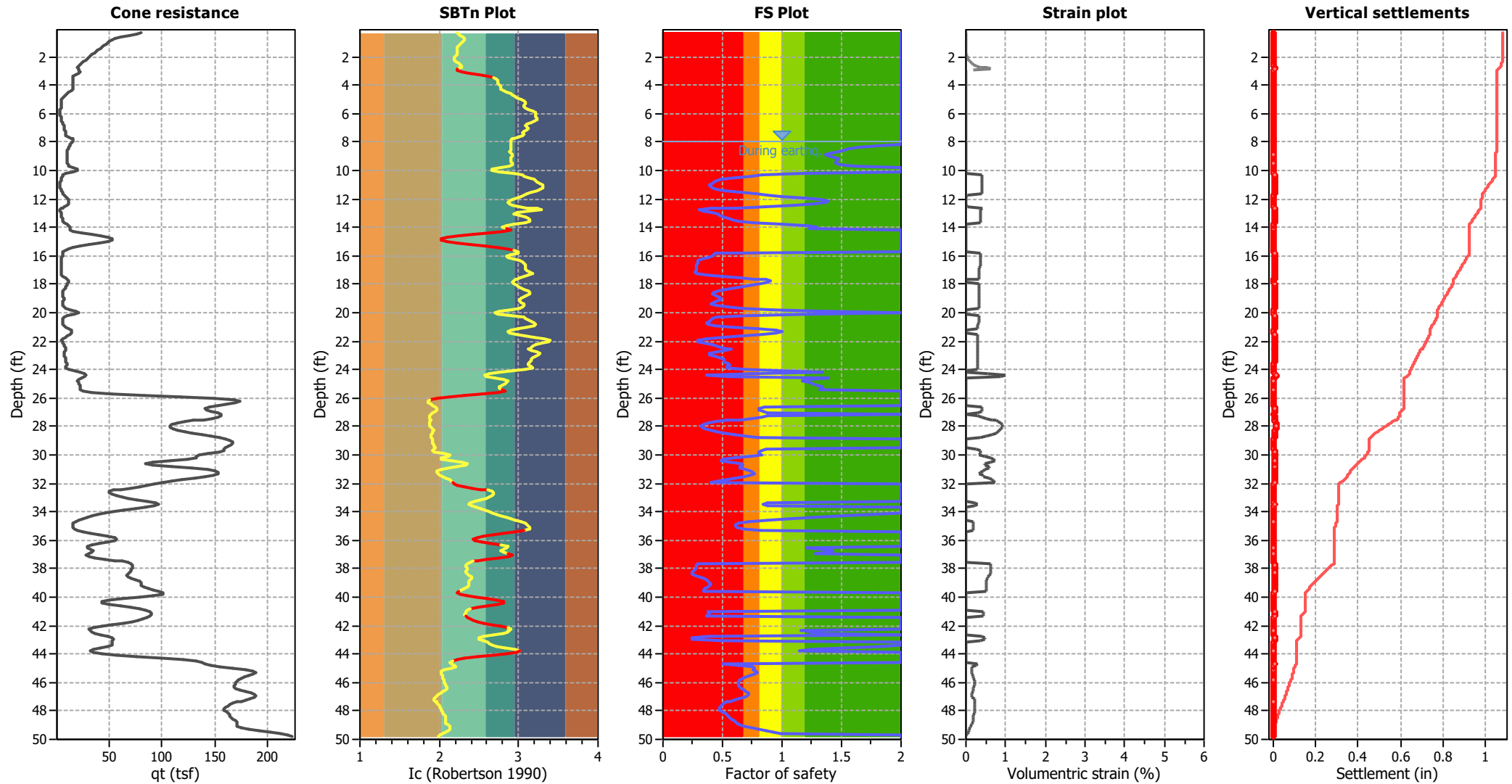
Abbreviations

FS: Calculated factor of safety for test point

F_L: 1 - FSw_z: Function value of the extend of soil liquefaction according to depthd_z: Layer thickness (ft)

LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

q_c : Total cone resistance (cone resistance q_c corrected for pore water effects)
 I_c : Soil Behaviour Type Index
 FS: Calculated Factor of Safety against liquefaction
 Volumetric strain: Post-liquefaction volumetric strain

:: Post-earthquake settlement of dry sands ::												
Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _r (%)	Settle. (in)
0.30	2.22	152.20	1.68	255.05	58	1211	0.59	0.001	0.00	13.69	0.00	0.000
0.40	2.24	143.84	1.72	247.62	57	1168	0.59	0.001	0.00	13.69	0.00	0.000
0.50	2.27	130.19	1.81	235.68	55	1095	0.59	0.002	0.00	13.69	0.00	0.000
0.60	2.30	115.37	1.93	222.13	52	1011	0.59	0.002	0.00	13.69	0.00	0.000
0.70	2.32	105.09	1.99	209.42	50	942	0.59	0.003	0.00	13.69	0.00	0.000
0.80	2.32	98.88	1.99	196.91	47	886	0.59	0.003	0.00	13.69	0.00	0.000
0.90	2.31	94.95	1.95	184.73	44	838	0.59	0.004	0.00	13.69	0.00	0.000
1.00	2.29	91.55	1.88	172.20	40	790	0.59	0.005	0.00	13.69	0.00	0.000
1.10	2.27	88.17	1.81	159.58	37	742	0.59	0.006	0.00	13.69	0.00	0.000
1.20	2.24	85.14	1.74	147.83	34	695	0.59	0.008	0.00	13.69	0.00	0.000
1.30	2.23	81.89	1.69	138.02	31	654	0.59	0.009	0.01	13.69	0.01	0.000
1.40	2.22	78.51	1.67	131.20	30	623	0.59	0.011	0.01	13.69	0.01	0.000
1.50	2.23	74.76	1.68	125.92	29	597	0.59	0.013	0.01	13.69	0.01	0.000
1.60	2.23	70.90	1.70	120.55	28	570	0.59	0.016	0.01	13.69	0.01	0.000
1.70	2.23	67.15	1.70	114.04	26	540	0.59	0.020	0.01	13.69	0.01	0.000
1.80	2.22	63.96	1.68	107.33	24	509	0.59	0.025	0.02	13.69	0.02	0.000
1.90	2.21	61.34	1.64	100.71	23	480	0.59	0.032	0.03	13.69	0.03	0.000
2.00	2.19	58.72	1.60	94.03	21	450	0.59	0.043	0.04	13.69	0.04	0.000
2.10	2.18	55.90	1.57	87.92	20	422	0.59	0.058	0.06	13.69	0.05	0.001
2.20	2.18	52.50	1.58	82.75	19	397	0.59	0.079	0.09	13.69	0.08	0.001
2.30	2.20	48.74	1.62	79.15	18	378	0.59	0.106	0.12	13.69	0.11	0.001
2.40	2.24	45.00	1.71	76.89	18	363	0.59	0.139	0.16	13.69	0.15	0.002
2.50	2.27	41.66	1.80	75.13	17	350	0.59	0.182	0.22	13.69	0.20	0.002
2.60	2.28	39.28	1.86	73.11	17	337	0.59	0.240	0.29	13.69	0.27	0.003
2.70	2.28	37.71	1.86	70.03	16	323	0.59	0.329	0.42	13.69	0.38	0.005
2.80	2.26	37.44	1.78	66.76	15	312	0.59	0.438	0.60	13.69	0.54	0.007
2.90	2.23	38.62	1.70	65.53	15	310	0.59	0.494	0.70	13.69	0.64	0.008
3.00	2.23	40.63	1.70	68.92	0	0	0.59	0.000	0.00	13.69	0.00	0.000
3.10	2.28	41.44	1.86	77.20	0	0	0.59	0.000	0.00	13.69	0.00	0.000
3.20	2.38	38.89	2.27	88.23	0	0	0.59	0.000	0.00	13.69	0.00	0.000
3.30	2.50	34.54	2.97	102.45	0	0	0.59	0.000	0.00	13.69	0.00	0.000
3.40	2.61	30.41	3.83	116.57	0	0	0.59	0.000	0.00	0.00	0.00	0.000
3.50	2.68	28.79	4.48	128.96	0	0	0.59	0.000	0.00	0.00	0.00	0.000
3.60	2.72	28.22	4.92	138.72	0	0	0.59	0.000	0.00	0.00	0.00	0.000
3.70	2.74	28.45	5.14	146.14	0	0	0.59	0.000	0.00	0.00	0.00	0.000
3.80	2.74	29.28	5.18	151.59	0	0	0.59	0.000	0.00	0.00	0.00	0.000
3.90	2.74	29.85	5.18	154.64	0	0	0.59	0.000	0.00	0.00	0.00	0.000
4.00	2.75	29.62	5.29	156.64	0	0	0.59	0.000	0.00	0.00	0.00	0.000
4.10	2.77	28.80	5.49	157.97	0	0	0.59	0.000	0.00	0.00	0.00	0.000
4.20	2.78	28.45	5.58	158.67	0	0	0.59	0.000	0.00	0.00	0.00	0.000
4.30	2.78	27.94	5.64	157.49	0	0	0.59	0.000	0.00	0.00	0.00	0.000
4.40	2.81	25.89	5.93	153.53	0	0	0.59	0.000	0.00	0.00	0.00	0.000
4.50	2.85	22.33	6.55	146.36	0	0	0.59	0.000	0.00	0.00	0.00	0.000
4.60	2.90	18.83	7.23	136.13	0	0	0.59	0.000	0.00	0.00	0.00	0.000
4.70	2.93	16.27	7.62	124.04	0	0	0.59	0.000	0.00	0.00	0.00	0.000
4.80	2.95	13.94	7.97	111.15	0	0	0.59	0.000	0.00	0.00	0.00	0.000
4.90	2.98	11.71	8.47	99.11	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.00	3.03	9.46	9.33	88.23	0	0	0.59	0.000	0.00	0.00	0.00	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
5.10	3.07	8.03	10.03	80.61	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.20	3.09	7.20	10.42	75.03	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.30	3.08	6.96	10.31	71.71	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.40	3.07	6.95	10.07	69.99	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.50	3.07	6.94	10.07	69.90	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.60	3.09	6.87	10.44	71.71	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.70	3.13	6.65	11.21	74.59	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.80	3.17	6.39	12.15	77.69	0	0	0.59	0.000	0.00	0.00	0.00	0.000
5.90	3.20	6.32	12.83	81.04	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.00	3.21	6.51	13.01	84.78	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.10	3.21	6.76	13.01	87.91	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.20	3.22	6.88	13.13	90.26	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.30	3.23	6.87	13.43	92.23	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.40	3.23	7.25	13.37	96.86	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.50	3.20	8.20	12.75	104.54	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.60	3.15	9.72	11.72	113.91	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.70	3.11	11.33	10.84	122.78	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.80	3.09	12.36	10.48	129.51	0	0	0.58	0.000	0.00	0.00	0.00	0.000
6.90	3.10	12.64	10.62	134.19	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.00	3.12	12.61	10.92	137.66	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.10	3.10	13.49	10.54	142.25	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.20	3.06	14.68	9.87	144.89	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.30	3.04	15.13	9.56	144.74	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.40	3.06	14.51	9.89	143.48	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.50	3.06	15.73	9.77	153.65	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.60	3.00	19.98	8.83	176.32	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.70	2.95	24.96	7.92	197.63	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.80	2.92	27.99	7.46	208.82	0	0	0.58	0.000	0.00	0.00	0.00	0.000
7.90	2.91	28.53	7.32	208.71	0	0	0.58	0.000	0.00	0.00	0.00	0.000

Total estimated settlement: 0.03**Abbreviations**

Q_{tn}: Equivalent clean sand normalized cone resistance
 K_c: Fines correction factor
 Q_{tn,cs}: Post-liquefaction volumetric strain
 G_{max}: Small strain shear modulus
 CSR: Soil cyclic stress ratio
 γ: Cyclic shear strain
 e_{vol(15)}: Volumetric strain after 15 cycles
 N_c: Equivalent number of cycles
 e_v: Volumetric strain
 Settle.: Calculated settlement

:: Post-earthquake settlement due to soil liquefaction ::

Depth (ft)	Q _{tn,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	Q _{tn,cs}	FS	e _v (%)	DF	Settlement (in)
8.00	201.78	2.00	0.00	0.85	0.00	8.10	190.81	2.00	0.00	0.85	0.00
8.20	176.83	2.00	0.00	0.85	0.00	8.30	162.63	1.80	0.00	0.85	0.00
8.40	151.23	1.65	0.00	0.85	0.00	8.50	142.92	1.56	0.00	0.85	0.00
8.60	137.89	1.53	0.00	0.84	0.00	8.70	134.00	1.48	0.00	0.84	0.00
8.80	131.89	1.41	0.01	0.84	0.00	8.90	132.73	1.37	0.01	0.84	0.00
9.00	135.70	1.39	0.01	0.84	0.00	9.10	137.55	1.44	0.00	0.83	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
9.20	137.71	1.47	0.00	0.83	0.00	9.30	138.04	1.47	0.00	0.83	0.00
9.40	140.71	1.46	0.00	0.83	0.00	9.50	144.46	1.45	0.00	0.83	0.00
9.60	148.57	1.49	0.00	0.83	0.00	9.70	151.08	1.61	0.00	0.82	0.00
9.80	157.22	2.00	0.00	0.82	0.00	9.90	316.66	2.00	0.00	0.82	0.00
10.00	305.72	2.00	0.00	0.82	0.00	10.10	148.25	2.00	0.00	0.82	0.00
10.20	126.32	1.17	0.01	0.81	0.00	10.30	110.91	0.83	0.41	0.81	0.00
10.40	103.26	0.74	0.41	0.81	0.00	10.50	93.94	0.60	0.40	0.81	0.00
10.60	86.12	0.49	0.40	0.81	0.00	10.70	82.70	0.45	0.40	0.81	0.00
10.80	82.97	0.43	0.40	0.80	0.00	10.90	85.56	0.41	0.40	0.80	0.00
11.00	88.03	0.40	0.40	0.80	0.00	11.10	89.50	0.40	0.40	0.80	0.00
11.20	90.61	0.42	0.40	0.80	0.00	11.30	94.08	0.45	0.40	0.79	0.00
11.40	103.11	0.53	0.40	0.79	0.00	11.50	113.38	0.66	0.40	0.79	0.00
11.60	121.21	0.77	0.39	0.79	0.00	11.70	129.20	0.87	0.02	0.79	0.00
11.80	139.67	1.00	0.02	0.79	0.00	11.90	149.16	1.19	0.01	0.78	0.00
12.00	150.64	1.33	0.01	0.78	0.00	12.10	146.07	1.39	0.00	0.78	0.00
12.20	140.04	1.36	0.00	0.78	0.00	12.30	134.38	1.27	0.01	0.78	0.00
12.40	126.64	1.09	0.01	0.77	0.00	12.50	115.04	0.86	0.02	0.77	0.00
12.60	100.03	0.61	0.39	0.77	0.00	12.70	83.00	0.40	0.38	0.77	0.00
12.80	67.56	0.30	0.38	0.77	0.00	12.90	57.22	0.34	0.38	0.77	0.00
13.00	53.47	0.42	0.38	0.76	0.00	13.10	56.56	0.47	0.38	0.76	0.00
13.20	67.21	0.48	0.38	0.76	0.00	13.30	81.56	0.51	0.38	0.76	0.00
13.40	94.34	0.55	0.38	0.76	0.00	13.50	104.49	0.58	0.38	0.75	0.00
13.60	114.07	0.63	0.38	0.75	0.00	13.70	122.14	0.76	0.38	0.75	0.00
13.80	126.04	1.01	0.01	0.75	0.00	13.90	122.59	1.21	0.01	0.75	0.00
14.00	120.81	1.29	0.01	0.75	0.00	14.10	126.36	1.23	0.01	0.74	0.00
14.20	142.74	2.00	0.00	0.74	0.00	14.30	155.81	2.00	0.00	0.74	0.00
14.40	248.34	2.00	0.00	0.74	0.00	14.50	123.26	2.00	0.00	0.74	0.00
14.60	101.36	2.00	0.00	0.73	0.00	14.70	93.93	2.00	0.00	0.73	0.00
14.80	94.66	2.00	0.00	0.73	0.00	14.90	95.28	2.00	0.00	0.73	0.00
15.00	94.32	2.00	0.00	0.73	0.00	15.10	94.32	2.00	0.00	0.73	0.00
15.20	100.91	2.00	0.00	0.72	0.00	15.30	139.95	2.00	0.00	0.72	0.00
15.40	113.49	2.00	0.00	0.72	0.00	15.50	106.32	2.00	0.00	0.72	0.00
15.60	92.23	2.00	0.00	0.72	0.00	15.70	75.87	2.00	0.00	0.71	0.00
15.80	62.13	0.43	0.36	0.71	0.00	15.90	52.12	0.43	0.36	0.71	0.00
16.00	45.85	0.42	0.35	0.71	0.00	16.10	43.41	0.38	0.35	0.71	0.00
16.20	43.43	0.33	0.35	0.71	0.00	16.30	44.92	0.29	0.35	0.70	0.00
16.40	47.20	0.29	0.35	0.70	0.00	16.50	48.98	0.29	0.35	0.70	0.00
16.60	49.89	0.29	0.35	0.70	0.00	16.70	49.88	0.28	0.35	0.70	0.00
16.80	49.18	0.28	0.35	0.69	0.00	16.90	48.98	0.28	0.35	0.69	0.00
17.00	50.42	0.28	0.35	0.69	0.00	17.10	53.77	0.27	0.34	0.69	0.00
17.20	59.31	0.28	0.34	0.69	0.00	17.30	70.59	0.37	0.34	0.69	0.00
17.40	85.46	0.50	0.34	0.68	0.00	17.50	101.36	0.66	0.34	0.68	0.00
17.60	114.46	0.77	0.34	0.68	0.00	17.70	121.56	0.86	0.02	0.68	0.00
17.80	122.06	0.91	0.01	0.68	0.00	17.90	117.86	0.88	0.01	0.67	0.00
18.00	112.59	0.82	0.34	0.67	0.00	18.10	107.14	0.74	0.34	0.67	0.00
18.20	102.55	0.67	0.33	0.67	0.00	18.30	98.23	0.60	0.33	0.67	0.00
18.40	93.89	0.52	0.33	0.67	0.00	18.50	89.39	0.46	0.33	0.66	0.00
18.60	85.63	0.42	0.33	0.66	0.00	18.70	83.75	0.42	0.33	0.66	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
18.80	83.19	0.43	0.33	0.66	0.00	18.90	82.40	0.46	0.33	0.66	0.00
19.00	80.99	0.49	0.33	0.65	0.00	19.10	78.06	0.49	0.33	0.65	0.00
19.20	73.79	0.46	0.33	0.65	0.00	19.30	70.76	0.42	0.32	0.65	0.00
19.40	72.47	0.40	0.32	0.65	0.00	19.50	82.07	0.45	0.32	0.65	0.00
19.60	94.93	0.54	0.32	0.64	0.00	19.70	105.88	0.66	0.32	0.64	0.00
19.80	119.55	0.92	0.01	0.64	0.00	19.90	129.05	1.35	0.00	0.64	0.00
20.00	274.17	2.00	0.00	0.64	0.00	20.10	115.85	1.24	0.00	0.63	0.00
20.20	95.19	0.72	0.32	0.63	0.00	20.30	82.00	0.46	0.32	0.63	0.00
20.40	80.15	0.42	0.31	0.63	0.00	20.50	80.81	0.40	0.31	0.63	0.00
20.60	82.66	0.39	0.31	0.63	0.00	20.70	85.31	0.37	0.31	0.62	0.00
20.80	91.20	0.38	0.31	0.62	0.00	20.90	102.84	0.44	0.31	0.62	0.00
21.00	117.14	0.59	0.31	0.62	0.00	21.10	125.79	0.79	0.31	0.62	0.00
21.20	125.93	0.95	0.01	0.61	0.00	21.30	123.20	1.00	0.01	0.61	0.00
21.40	124.31	0.95	0.01	0.61	0.00	21.50	127.42	0.82	0.30	0.61	0.00
21.60	126.24	0.66	0.30	0.61	0.00	21.70	119.42	0.50	0.30	0.61	0.00
21.80	108.41	0.36	0.30	0.60	0.00	21.90	99.49	0.30	0.30	0.60	0.00
22.00	95.84	0.30	0.30	0.60	0.00	22.10	98.07	0.35	0.30	0.60	0.00
22.20	102.14	0.42	0.30	0.60	0.00	22.30	105.47	0.45	0.30	0.59	0.00
22.40	109.64	0.49	0.30	0.59	0.00	22.50	116.23	0.55	0.30	0.59	0.00
22.60	120.09	0.57	0.29	0.59	0.00	22.70	118.55	0.53	0.29	0.59	0.00
22.80	112.37	0.45	0.29	0.59	0.00	22.90	106.12	0.39	0.29	0.58	0.00
23.00	105.03	0.39	0.29	0.58	0.00	23.10	107.82	0.43	0.29	0.58	0.00
23.20	111.21	0.48	0.29	0.58	0.00	23.30	113.23	0.51	0.29	0.58	0.00
23.40	112.79	0.51	0.29	0.57	0.00	23.50	113.85	0.52	0.29	0.57	0.00
23.60	116.74	0.55	0.29	0.57	0.00	23.70	118.76	0.56	0.28	0.57	0.00
23.80	119.81	0.54	0.28	0.57	0.00	23.90	123.61	0.54	0.28	0.57	0.00
24.00	133.21	0.68	0.28	0.56	0.00	24.10	140.03	0.99	0.01	0.56	0.00
24.20	134.10	1.34	0.00	0.56	0.00	24.30	192.89	0.74	0.54	0.56	0.01
24.40	140.59	0.37	0.98	0.56	0.01	24.50	164.76	0.54	0.86	0.55	0.01
24.60	125.71	1.39	0.00	0.55	0.00	24.70	139.79	1.21	0.00	0.55	0.00
24.80	150.66	1.17	0.00	0.55	0.00	24.90	155.06	1.23	0.00	0.55	0.00
25.00	152.06	1.26	0.00	0.55	0.00	25.10	143.99	1.29	0.00	0.54	0.00
25.20	136.81	1.34	0.00	0.54	0.00	25.30	137.02	1.34	0.00	0.54	0.00
25.40	148.46	1.32	0.00	0.54	0.00	25.50	171.07	2.00	0.00	0.54	0.00
25.60	191.70	2.00	0.00	0.53	0.00	25.70	220.35	2.00	0.00	0.53	0.00
25.80	185.82	2.00	0.00	0.53	0.00	25.90	189.05	2.00	0.00	0.53	0.00
26.00	206.69	2.00	0.00	0.53	0.00	26.10	220.06	2.00	0.00	0.53	0.00
26.20	222.02	2.00	0.00	0.52	0.00	26.30	218.21	2.00	0.00	0.52	0.00
26.40	211.10	2.00	0.00	0.52	0.00	26.50	203.19	2.00	0.00	0.52	0.00
26.60	196.34	0.85	0.39	0.52	0.00	26.70	192.44	0.80	0.40	0.51	0.00
26.80	192.32	0.80	0.40	0.51	0.00	26.90	195.36	0.84	0.39	0.51	0.00
27.00	199.23	0.88	0.29	0.51	0.00	27.10	200.73	2.00	0.00	0.51	0.00
27.20	199.17	0.88	0.29	0.51	0.00	27.30	194.36	0.82	0.39	0.50	0.00
27.40	186.92	0.74	0.51	0.50	0.01	27.50	176.64	0.64	0.67	0.50	0.01
27.60	164.76	0.54	0.77	0.50	0.01	27.70	152.73	0.44	0.82	0.50	0.01
27.80	142.65	0.38	0.86	0.49	0.01	27.90	135.64	0.34	0.90	0.49	0.01
28.00	132.69	0.32	0.91	0.49	0.01	28.10	134.46	0.33	0.90	0.49	0.01
28.20	139.30	0.36	0.87	0.49	0.01	28.30	145.75	0.40	0.83	0.49	0.01

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
28.40	153.25	0.45	0.80	0.48	0.01	28.50	161.60	0.51	0.76	0.48	0.01
28.60	171.49	0.59	0.67	0.48	0.01	28.70	181.91	0.69	0.50	0.48	0.01
28.80	191.87	0.80	0.37	0.48	0.00	28.90	200.03	2.00	0.00	0.47	0.00
29.00	205.70	2.00	0.00	0.47	0.00	29.10	208.83	2.00	0.00	0.47	0.00
29.20	208.99	2.00	0.00	0.47	0.00	29.30	206.83	2.00	0.00	0.47	0.00
29.40	203.98	2.00	0.00	0.47	0.00	29.50	201.12	2.00	0.00	0.46	0.00
29.60	198.33	0.87	0.26	0.46	0.00	29.70	194.79	0.83	0.35	0.46	0.00
29.80	192.38	0.80	0.36	0.46	0.00	29.90	192.82	0.81	0.36	0.46	0.00
30.00	195.31	0.83	0.35	0.45	0.00	30.10	185.80	0.73	0.46	0.45	0.01
30.20	171.55	0.59	0.63	0.45	0.01	30.30	160.84	0.50	0.71	0.45	0.01
30.40	159.11	0.49	0.71	0.45	0.01	30.50	167.52	0.56	0.64	0.45	0.01
30.60	178.54	0.66	0.48	0.44	0.01	30.70	180.41	0.68	0.47	0.44	0.01
30.80	176.75	0.64	0.58	0.44	0.01	30.90	177.20	0.65	0.58	0.44	0.01
31.00	182.22	0.69	0.46	0.44	0.01	31.10	186.10	0.73	0.44	0.43	0.01
31.20	188.32	0.76	0.35	0.43	0.00	31.30	188.71	0.76	0.35	0.43	0.00
31.40	186.10	0.73	0.44	0.43	0.01	31.50	180.37	0.68	0.45	0.43	0.01
31.60	172.88	0.61	0.58	0.43	0.01	31.70	164.46	0.53	0.66	0.42	0.01
31.80	155.22	0.46	0.69	0.42	0.01	31.90	145.43	0.40	0.72	0.42	0.01
32.00	137.98	2.00	0.00	0.42	0.00	32.10	136.33	2.00	0.00	0.42	0.00
32.20	142.75	2.00	0.00	0.41	0.00	32.30	156.46	2.00	0.00	0.41	0.00
32.40	176.27	2.00	0.00	0.41	0.00	32.50	275.21	2.00	0.00	0.41	0.00
32.60	358.36	2.00	0.00	0.41	0.00	32.70	413.70	2.00	0.00	0.41	0.00
32.80	433.93	2.00	0.00	0.40	0.00	32.90	415.14	2.00	0.00	0.40	0.00
33.00	369.18	2.00	0.00	0.40	0.00	33.10	305.98	2.00	0.00	0.40	0.00
33.20	228.35	2.00	0.00	0.40	0.00	33.30	205.91	2.00	0.00	0.39	0.00
33.40	198.06	0.87	0.22	0.39	0.00	33.50	195.78	0.85	0.30	0.39	0.00
33.60	198.97	0.88	0.22	0.39	0.00	33.70	203.61	2.00	0.00	0.39	0.00
33.80	205.05	2.00	0.00	0.39	0.00	33.90	254.57	2.00	0.00	0.38	0.00
34.00	295.69	2.00	0.00	0.38	0.00	34.10	329.07	2.00	0.00	0.38	0.00
34.20	164.76	1.75	0.00	0.38	0.00	34.30	160.14	1.49	0.00	0.38	0.00
34.40	156.10	1.27	0.00	0.37	0.00	34.50	148.09	1.06	0.00	0.37	0.00
34.60	137.74	0.88	0.01	0.37	0.00	34.70	129.28	0.72	0.18	0.37	0.00
34.80	126.28	0.63	0.18	0.37	0.00	34.90	127.20	0.61	0.18	0.37	0.00
35.00	129.34	0.61	0.18	0.36	0.00	35.10	135.08	0.62	0.18	0.36	0.00
35.20	144.97	0.67	0.18	0.36	0.00	35.30	156.19	0.81	0.18	0.36	0.00
35.40	160.65	2.00	0.00	0.36	0.00	35.50	157.69	2.00	0.00	0.35	0.00
35.60	291.85	2.00	0.00	0.35	0.00	35.70	171.45	2.00	0.00	0.35	0.00
35.80	130.29	2.00	0.00	0.35	0.00	35.90	122.48	2.00	0.00	0.35	0.00
36.00	121.48	2.00	0.00	0.35	0.00	36.10	137.96	2.00	0.00	0.34	0.00
36.20	254.56	2.00	0.00	0.34	0.00	36.30	149.63	2.00	0.00	0.34	0.00
36.40	152.64	2.00	0.00	0.34	0.00	36.50	152.12	1.21	0.00	0.34	0.00
36.60	151.52	1.33	0.00	0.33	0.00	36.70	153.45	1.43	0.00	0.33	0.00
36.80	158.27	1.41	0.00	0.33	0.00	36.90	163.05	1.28	0.00	0.33	0.00
37.00	164.19	2.00	0.00	0.33	0.00	37.10	160.90	2.00	0.00	0.33	0.00
37.20	151.31	2.00	0.00	0.32	0.00	37.30	200.14	2.00	0.00	0.32	0.00
37.40	130.26	2.00	0.00	0.32	0.00	37.50	128.52	2.00	0.00	0.32	0.00
37.60	128.50	2.00	0.00	0.32	0.00	37.70	126.04	0.29	0.61	0.31	0.01
37.80	122.99	0.28	0.62	0.31	0.01	37.90	122.32	0.28	0.62	0.31	0.01

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
38.00	122.81	0.28	0.61	0.31	0.01	38.10	121.29	0.27	0.61	0.31	0.01
38.20	117.17	0.25	0.63	0.31	0.01	38.30	114.12	0.24	0.64	0.30	0.01
38.40	115.14	0.25	0.63	0.30	0.01	38.50	121.02	0.27	0.60	0.30	0.01
38.60	128.60	0.31	0.57	0.30	0.01	38.70	134.82	0.34	0.54	0.30	0.01
38.80	138.76	0.37	0.53	0.29	0.01	38.90	141.24	0.38	0.52	0.29	0.01
39.00	143.06	0.39	0.51	0.29	0.01	39.10	143.96	0.40	0.50	0.29	0.01
39.20	143.34	0.39	0.50	0.29	0.01	39.30	140.67	0.38	0.50	0.29	0.01
39.40	137.30	0.36	0.51	0.28	0.01	39.50	134.59	0.34	0.52	0.28	0.01
39.60	133.36	0.34	0.52	0.28	0.01	39.70	134.76	2.00	0.00	0.28	0.00
39.80	140.84	2.00	0.00	0.28	0.00	39.90	153.15	2.00	0.00	0.27	0.00
40.00	169.03	2.00	0.00	0.27	0.00	40.10	266.17	2.00	0.00	0.27	0.00
40.20	183.83	2.00	0.00	0.27	0.00	40.30	186.64	2.00	0.00	0.27	0.00
40.40	188.86	2.00	0.00	0.27	0.00	40.50	185.32	2.00	0.00	0.26	0.00
40.60	254.80	2.00	0.00	0.26	0.00	40.70	153.69	2.00	0.00	0.26	0.00
40.80	138.37	2.00	0.00	0.26	0.00	40.90	136.99	2.00	0.00	0.26	0.00
41.00	140.49	0.38	0.45	0.25	0.01	41.10	142.01	0.39	0.44	0.25	0.01
41.20	138.85	0.37	0.45	0.25	0.01	41.30	137.12	0.36	0.45	0.25	0.01
41.40	140.14	2.00	0.00	0.25	0.00	41.50	142.45	2.00	0.00	0.25	0.00
41.60	144.69	2.00	0.00	0.24	0.00	41.70	148.63	2.00	0.00	0.24	0.00
41.80	179.51	2.00	0.00	0.24	0.00	41.90	287.13	2.00	0.00	0.24	0.00
42.00	162.75	2.00	0.00	0.24	0.00	42.10	157.74	2.00	0.00	0.23	0.00
42.20	150.55	2.00	0.00	0.23	0.00	42.30	148.03	1.16	0.00	0.23	0.00
42.40	149.89	1.20	0.00	0.23	0.00	42.50	150.00	1.23	0.00	0.23	0.00
42.60	143.15	1.33	0.00	0.23	0.00	42.70	259.40	2.00	0.00	0.22	0.00
42.80	139.65	0.38	0.39	0.22	0.00	42.90	111.97	0.24	0.47	0.22	0.01
43.00	113.09	0.25	0.46	0.22	0.01	43.10	154.38	0.49	0.35	0.22	0.00
43.20	206.66	2.00	0.00	0.21	0.00	43.30	247.19	2.00	0.00	0.21	0.00
43.40	283.95	2.00	0.00	0.21	0.00	43.50	162.45	1.83	0.00	0.21	0.00
43.60	171.06	1.52	0.00	0.21	0.00	43.70	179.95	1.25	0.00	0.21	0.00
43.80	185.44	1.14	0.00	0.20	0.00	43.90	188.01	2.00	0.00	0.20	0.00
44.00	184.73	2.00	0.00	0.20	0.00	44.10	341.33	2.00	0.00	0.20	0.00
44.20	153.28	2.00	0.00	0.20	0.00	44.30	144.35	2.00	0.00	0.19	0.00
44.40	145.92	2.00	0.00	0.19	0.00	44.50	150.24	2.00	0.00	0.19	0.00
44.60	150.70	2.00	0.00	0.19	0.00	44.70	155.94	0.51	0.30	0.19	0.00
44.80	170.66	0.63	0.26	0.19	0.00	44.90	182.24	0.75	0.16	0.18	0.00
45.00	183.93	0.77	0.15	0.18	0.00	45.10	182.40	0.76	0.15	0.18	0.00
45.20	184.20	0.78	0.15	0.18	0.00	45.30	185.25	0.79	0.15	0.18	0.00
45.40	183.02	0.77	0.15	0.17	0.00	45.50	179.72	0.73	0.18	0.17	0.00
45.60	176.34	0.70	0.19	0.17	0.00	45.70	173.50	0.67	0.19	0.17	0.00
45.80	171.53	0.65	0.23	0.17	0.00	45.90	170.25	0.64	0.23	0.17	0.00
46.00	169.73	0.63	0.23	0.16	0.00	46.10	169.73	0.63	0.23	0.16	0.00
46.20	170.19	0.64	0.22	0.16	0.00	46.30	171.23	0.65	0.18	0.16	0.00
46.40	172.53	0.66	0.18	0.16	0.00	46.50	173.95	0.68	0.17	0.15	0.00
46.60	175.62	0.70	0.17	0.15	0.00	46.70	177.31	0.72	0.16	0.15	0.00
46.80	178.03	0.72	0.16	0.15	0.00	46.90	176.71	0.71	0.16	0.15	0.00
47.00	173.38	0.68	0.16	0.15	0.00	47.10	168.99	0.64	0.20	0.14	0.00
47.20	164.54	0.59	0.21	0.14	0.00	47.30	160.75	0.56	0.21	0.14	0.00
47.40	157.73	0.54	0.22	0.14	0.00	47.50	155.30	0.52	0.22	0.14	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
47.60	153.25	0.50	0.22	0.13	0.00	47.70	151.63	0.49	0.22	0.13	0.00
47.80	150.26	0.48	0.22	0.13	0.00	47.90	149.62	0.47	0.22	0.13	0.00
48.00	150.31	0.48	0.21	0.13	0.00	48.10	152.65	0.50	0.21	0.13	0.00
48.20	155.37	0.52	0.20	0.12	0.00	48.30	157.39	0.54	0.20	0.12	0.00
48.40	158.78	0.55	0.19	0.12	0.00	48.50	160.12	0.56	0.18	0.12	0.00
48.60	161.72	0.58	0.18	0.12	0.00	48.70	163.29	0.59	0.17	0.11	0.00
48.80	164.67	0.61	0.17	0.11	0.00	48.90	166.37	0.62	0.16	0.11	0.00
49.00	168.94	0.65	0.15	0.11	0.00	49.10	172.78	0.69	0.12	0.11	0.00
49.20	177.75	0.74	0.11	0.11	0.00	49.30	182.96	0.80	0.09	0.10	0.00
49.40	188.20	0.86	0.06	0.10	0.00	49.50	193.23	0.93	0.06	0.10	0.00
49.60	197.41	0.98	0.05	0.10	0.00	49.70	200.36	2.00	0.00	0.10	0.00
49.80	201.52	2.00	0.00	0.09	0.00						

Total estimated settlement: 1.05**Abbreviations**

$Q_{tn,cs}$: Equivalent clean sand normalized cone resistance
 FS: Factor of safety against liquefaction
 e_v (%): Post-liquefaction volumetric strain
 DF: e_v depth weighting factor
 Settlement: Calculated settlement

:: Strength loss calculation (Robertson (2009)) ::

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.30	80.54	152.20	1.68	255.05	2.22	0.94	0.94
0.40	76.12	143.84	1.72	247.62	2.24	0.93	0.93
0.50	68.91	130.19	1.81	235.68	2.27	0.92	0.92
0.60	61.08	115.37	1.93	222.13	2.30	0.91	0.91
0.70	55.64	105.09	1.99	209.42	2.32	0.90	0.90
0.80	52.36	98.88	1.99	196.91	2.32	0.88	0.88
0.90	50.29	94.95	1.95	184.73	2.31	0.87	0.87
1.00	48.50	91.55	1.88	172.20	2.29	0.86	0.86
1.10	46.72	88.17	1.81	159.58	2.27	0.84	0.84
1.20	45.12	85.14	1.74	147.83	2.24	0.82	0.82
1.30	43.40	81.89	1.69	138.02	2.23	0.81	0.81
1.40	41.62	78.51	1.67	131.20	2.22	0.80	0.80
1.50	39.65	74.76	1.68	125.92	2.23	0.79	0.79
1.60	37.61	70.90	1.70	120.55	2.23	0.78	0.78
1.70	35.63	67.15	1.70	114.04	2.23	0.77	0.77
1.80	33.95	63.96	1.68	107.33	2.22	0.76	0.76
1.90	32.57	61.34	1.64	100.71	2.21	0.75	0.75
2.00	31.19	58.72	1.60	94.03	2.19	0.74	0.74
2.10	29.70	55.90	1.57	87.92	2.18	0.72	0.72
2.20	27.91	52.50	1.58	82.75	2.18	0.71	0.71
2.30	25.92	48.74	1.62	79.15	2.20	0.54	0.71
2.40	23.95	45.00	1.71	76.89	2.24	0.45	0.70
2.50	22.19	41.66	1.80	75.13	2.27	0.39	0.70
2.60	20.94	39.28	1.86	73.11	2.28	0.33	0.69
2.70	20.11	37.71	1.86	70.03	2.28	0.26	0.68
2.80	19.97	37.44	1.78	66.76	2.26	0.20	0.68
2.90	20.60	38.62	1.70	65.53	2.23	0.18	0.67
3.00	21.67	40.63	1.70	68.92	2.23	0.23	0.68
3.10	22.10	41.44	1.86	77.20	2.28	0.46	0.70
3.20	20.76	38.89	2.27	88.23	2.38	0.72	0.72
3.30	18.46	34.54	2.97	102.45	2.50	0.75	0.75
3.40	16.29	30.41	3.83	116.57	2.61	0.86	0.86
3.50	15.43	28.79	4.48	128.96	2.68	0.94	0.94
3.60	15.14	28.22	4.92	138.72	2.72	0.81	0.81
3.70	15.27	28.45	5.14	146.14	2.74	0.82	0.82
3.80	15.71	29.28	5.18	151.59	2.74	0.83	0.83
3.90	16.02	29.85	5.18	154.64	2.74	0.83	0.83
4.00	15.90	29.62	5.29	156.64	2.75	0.84	0.84
4.10	15.47	28.80	5.49	157.97	2.77	0.84	0.84
4.20	15.30	28.45	5.58	158.67	2.78	0.84	0.84
4.30	15.03	27.94	5.64	157.49	2.78	0.84	0.84
4.40	13.95	25.89	5.93	153.53	2.81	0.83	0.83
4.50	12.08	22.33	6.55	146.36	2.85	0.82	0.82
4.60	10.23	18.83	7.23	136.13	2.90	0.81	0.81
4.70	8.88	16.27	7.62	124.04	2.93	0.79	0.79
4.80	7.65	13.94	7.97	111.15	2.95	0.77	0.77
4.90	6.48	11.71	8.47	99.11	2.98	0.75	0.75
5.00	5.29	9.46	9.33	88.23	3.03	0.54	1.24

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
5.10	4.54	8.03	10.03	80.61	3.07	0.40	1.04
5.20	4.11	7.20	10.42	75.03	3.09	0.33	0.92
5.30	3.98	6.96	10.31	71.71	3.08	0.30	0.87
5.40	3.98	6.95	10.07	69.99	3.07	0.28	0.86
5.50	3.98	6.94	10.07	69.90	3.07	0.27	0.84
5.60	3.95	6.87	10.44	71.71	3.09	0.28	0.82
5.70	3.84	6.65	11.21	74.59	3.13	0.31	0.78
5.80	3.71	6.39	12.15	77.69	3.17	0.33	0.74
5.90	3.67	6.32	12.83	81.04	3.20	0.35	0.72
6.00	3.78	6.51	13.01	84.78	3.21	0.40	0.73
6.10	3.92	6.76	13.01	87.91	3.21	0.44	0.75
6.20	3.98	6.88	13.13	90.26	3.22	0.45	0.75
6.30	3.98	6.87	13.43	92.23	3.23	0.46	0.74
6.40	4.19	7.25	13.37	96.86	3.23	0.48	0.77
6.50	4.70	8.20	12.75	104.54	3.20	0.60	0.86
6.60	5.51	9.72	11.72	113.91	3.15	0.75	1.00
6.70	6.36	11.33	10.84	122.78	3.11	0.89	1.15
6.80	6.92	12.36	10.48	129.51	3.09	1.02	1.24
6.90	7.07	12.64	10.62	134.19	3.10	1.07	1.25
7.00	7.06	12.61	10.92	137.66	3.12	1.08	1.23
7.10	7.53	13.49	10.54	142.25	3.10	1.13	1.30
7.20	8.17	14.68	9.87	144.89	3.06	1.29	1.39
7.30	8.41	15.13	9.56	144.74	3.04	1.23	1.41
7.40	8.09	14.51	9.89	143.48	3.06	1.11	1.34
7.50	8.74	15.73	9.77	153.65	3.06	1.14	1.43
7.60	10.99	19.98	8.83	176.32	3.00	1.73	1.79
7.70	13.63	24.96	7.92	197.63	2.95	0.88	0.88
7.80	15.24	27.99	7.46	208.82	2.92	0.90	0.90
7.90	15.53	28.53	7.32	208.71	2.91	0.90	0.90
8.00	15.24	27.97	7.21	201.78	2.90	0.89	0.89
8.10	14.56	26.68	7.15	190.81	2.90	0.88	0.88
8.20	13.55	24.74	7.15	176.83	2.90	0.86	0.86
8.30	12.33	22.44	7.25	162.63	2.90	0.84	0.84
8.40	11.42	20.70	7.31	151.23	2.91	0.83	0.83
8.50	10.85	19.62	7.28	142.92	2.91	0.82	0.82
8.60	10.72	19.37	7.12	137.89	2.89	0.81	0.81
8.70	10.46	18.85	7.11	134.00	2.89	0.80	0.80
8.80	10.06	18.09	7.29	131.89	2.91	0.80	0.80
8.90	9.83	17.65	7.52	132.73	2.92	0.80	0.80
9.00	10.07	18.10	7.50	135.70	2.92	0.81	0.81
9.10	10.47	18.84	7.30	137.55	2.91	0.81	0.81
9.20	10.73	19.32	7.13	137.71	2.89	0.81	0.81
9.30	10.76	19.36	7.13	138.04	2.89	0.81	0.81
9.40	10.76	19.35	7.27	140.71	2.90	0.81	0.81
9.50	10.76	19.34	7.47	144.46	2.92	0.82	0.82
9.60	11.08	19.94	7.45	148.57	2.92	0.83	0.83
9.70	12.05	21.76	6.94	151.08	2.88	0.83	0.83
9.80	15.58	28.43	5.53	157.22	2.77	0.84	0.84

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.90	20.15	36.68	4.44	162.70	2.67	0.99	0.99
10.00	20.15	36.43	4.39	159.98	2.67	0.98	0.98
10.10	15.24	27.73	5.35	148.25	2.76	0.82	0.82
10.20	9.08	16.10	7.85	126.32	2.94	0.79	0.79
10.30	6.68	11.55	9.60	110.91	3.05	0.57	0.87
10.40	6.06	10.36	9.96	103.26	3.07	0.46	0.78
10.50	5.06	8.47	11.09	93.94	3.12	0.33	0.63
10.60	4.24	6.91	12.47	86.12	3.19	0.26	0.51
10.70	3.95	6.34	13.04	82.70	3.21	0.24	0.47
10.80	3.84	6.12	13.55	82.97	3.24	0.24	0.45
10.90	3.70	5.86	14.60	85.56	3.28	0.26	0.43
11.00	3.61	5.67	15.54	88.03	3.31	0.28	0.42
11.10	3.66	5.76	15.55	89.50	3.31	0.29	0.42
11.20	3.79	6.00	15.10	90.61	3.30	0.29	0.44
11.30	4.04	6.46	14.55	94.08	3.28	0.31	0.47
11.40	4.70	7.70	13.39	103.11	3.23	0.37	0.56
11.50	5.71	9.60	11.81	113.38	3.16	0.53	0.69
11.60	6.66	11.38	10.65	121.21	3.10	0.64	0.82
11.70	7.46	12.87	10.04	129.20	3.07	0.66	0.92
11.80	8.53	14.82	9.42	139.67	3.04	0.84	1.06
11.90	10.10	17.69	8.43	149.16	2.98	0.83	0.83
12.00	11.40	19.88	7.58	150.64	2.92	0.83	0.83
12.10	12.05	20.78	7.03	146.07	2.89	0.82	0.82
12.20	11.99	20.50	6.83	140.04	2.87	0.81	0.81
12.30	11.24	19.11	7.03	134.38	2.89	0.80	0.80
12.40	9.78	16.56	7.65	126.64	2.93	0.79	0.79
12.50	7.81	12.99	8.86	115.04	3.00	0.57	0.93
12.60	5.80	9.27	10.79	100.03	3.11	0.39	0.66
12.70	4.05	6.07	13.67	83.00	3.24	0.21	0.43
12.80	3.26	4.61	14.67	67.56	3.28	0.11	0.33
12.90	3.58	5.17	11.06	57.22	3.12	0.09	0.37
13.00	4.31	6.47	8.27	53.47	2.97	0.07	0.64
13.10	4.77	7.24	7.81	56.56	2.94	0.09	0.65
13.20	4.87	7.40	9.08	67.21	3.02	0.14	0.53
13.30	5.19	7.94	10.27	81.56	3.08	0.23	0.57
13.40	5.59	8.61	10.95	94.34	3.12	0.35	0.62
13.50	5.90	9.12	11.45	104.49	3.14	0.44	0.65
13.60	6.41	9.97	11.44	114.07	3.14	0.49	0.71
13.70	7.60	12.02	10.16	122.14	3.08	0.63	0.86
13.80	9.89	15.95	7.90	126.04	2.95	0.79	0.79
13.90	12.14	19.30	6.35	122.59	2.84	0.79	0.79
14.00	13.09	20.64	5.85	120.81	2.80	0.78	0.78
14.10	12.44	19.65	6.43	126.36	2.84	0.79	0.79
14.20	12.59	20.04	7.12	142.74	2.89	0.82	0.82
14.30	16.22	25.64	6.08	155.81	2.82	0.83	0.83
14.40	23.62	36.25	4.08	148.02	2.64	0.93	0.93
14.50	32.92	48.52	2.54	123.26	2.43	0.79	0.79
14.60	41.56	58.81	1.72	101.36	2.24	0.75	0.75

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
14.70	48.47	66.43	1.41	93.93	2.10	0.74	0.74
14.80	52.66	71.00	1.33	94.66	2.03	0.74	0.74
14.90	53.17	71.48	1.33	95.28	2.03	0.74	0.74
15.00	49.27	66.90	1.41	94.32	2.09	0.74	0.74
15.10	40.94	56.71	1.66	94.32	2.22	0.74	0.74
15.20	30.97	43.98	2.29	100.91	2.38	0.75	0.75
15.30	21.85	31.75	3.49	110.79	2.57	0.81	0.81
15.40	15.51	22.82	4.97	113.49	2.72	0.77	0.77
15.50	11.13	16.35	6.50	106.32	2.85	0.76	0.76
15.60	8.16	11.81	7.81	92.23	2.94	0.73	0.73
15.70	6.23	8.66	8.76	75.87	3.00	0.41	0.70
15.80	5.38	7.25	8.57	62.13	2.99	0.13	0.66
15.90	5.36	7.15	7.29	52.12	2.91	0.06	0.63
16.00	5.34	7.01	6.54	45.85	2.85	0.04	0.62
16.10	4.96	6.42	6.76	43.41	2.87	0.03	0.62
16.20	4.35	5.52	7.86	43.43	2.94	0.03	0.62
16.30	3.98	4.92	9.13	44.92	3.02	0.05	0.35
16.40	3.98	4.90	9.63	47.20	3.05	0.05	0.35
16.50	3.98	4.89	10.03	48.98	3.07	0.06	0.35
16.60	3.98	4.87	10.25	49.89	3.08	0.06	0.35
16.70	3.98	4.85	10.28	49.88	3.08	0.06	0.35
16.80	3.98	4.83	10.18	49.18	3.08	0.06	0.35
16.90	3.98	4.82	10.17	48.98	3.08	0.06	0.34
17.00	3.98	4.80	10.51	50.42	3.09	0.06	0.34
17.10	3.94	4.72	11.40	53.77	3.14	0.07	0.34
17.20	4.08	4.92	12.06	59.31	3.17	0.09	0.35
17.30	5.02	6.36	11.10	70.59	3.12	0.13	0.45
17.40	6.54	8.69	9.84	85.46	3.06	0.26	0.62
17.50	8.33	11.42	8.88	101.36	3.01	0.43	0.82
17.60	9.72	13.50	8.48	114.46	2.98	0.77	0.77
17.70	10.81	15.11	8.04	121.56	2.95	0.79	0.79
17.80	11.39	15.92	7.67	122.06	2.93	0.79	0.79
17.90	11.17	15.50	7.60	117.86	2.93	0.78	0.78
18.00	10.46	14.39	7.82	112.59	2.94	0.77	0.77
18.10	9.58	13.01	8.24	107.14	2.97	0.76	0.76
18.20	8.88	11.90	8.62	102.55	2.99	0.75	0.75
18.30	8.09	10.67	9.21	98.23	3.02	0.39	0.76
18.40	7.19	9.28	10.12	93.89	3.07	0.35	0.66
18.50	6.45	8.14	10.98	89.39	3.12	0.29	0.58
18.60	6.04	7.50	11.41	85.63	3.14	0.26	0.54
18.70	5.99	7.40	11.32	83.75	3.14	0.25	0.53
18.80	6.24	7.73	10.76	83.19	3.11	0.24	0.55
18.90	6.64	8.29	9.94	82.40	3.07	0.25	0.59
19.00	7.02	8.82	9.19	80.99	3.02	0.25	0.63
19.10	7.02	8.78	8.89	78.06	3.01	0.23	0.63
19.20	6.63	8.19	9.01	73.79	3.01	0.20	0.59
19.30	6.23	7.58	9.33	70.76	3.03	0.16	0.54
19.40	6.06	7.30	9.93	72.47	3.06	0.16	0.52

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
19.50	6.65	8.13	10.10	82.07	3.07	0.22	0.58
19.60	7.86	9.84	9.64	94.93	3.05	0.35	0.70
19.70	9.33	11.92	8.88	105.88	3.01	0.49	0.85
19.80	12.75	16.70	7.16	119.55	2.90	0.78	0.78
19.90	18.72	24.54	5.26	129.05	2.75	0.80	0.80
20.00	20.77	27.08	4.70	127.19	2.70	0.96	0.96
20.10	17.42	22.53	5.14	115.85	2.74	0.78	0.78
20.20	10.46	13.21	7.20	95.19	2.90	0.74	0.74
20.30	7.00	8.34	9.83	82.00	3.06	0.23	0.60
20.40	6.52	7.63	10.50	80.15	3.09	0.23	0.55
20.50	6.31	7.32	11.04	80.81	3.12	0.24	0.52
20.60	6.18	7.11	11.63	82.66	3.15	0.23	0.51
20.70	5.98	6.80	12.54	85.31	3.19	0.26	0.49
20.80	6.14	6.99	13.05	91.20	3.21	0.28	0.50
20.90	7.00	8.17	12.59	102.84	3.19	0.36	0.58
21.00	8.96	10.84	10.81	117.14	3.11	0.56	0.77
21.10	11.72	14.61	8.61	125.79	2.99	0.79	0.79
21.20	14.03	17.64	7.14	125.93	2.90	0.79	0.79
21.30	14.79	18.52	6.65	123.20	2.86	0.79	0.79
21.40	14.13	17.62	7.05	124.31	2.89	0.79	0.79
21.50	12.43	15.33	8.31	127.42	2.97	0.79	0.79
21.60	10.28	12.37	10.21	126.24	3.08	0.70	0.88
21.70	8.08	9.34	12.78	119.42	3.20	0.55	0.67
21.80	6.21	6.79	15.97	108.41	3.33	0.44	0.48
21.90	5.28	5.52	18.04	99.49	3.40	0.32	0.39
22.00	5.34	5.57	17.21	95.84	3.37	0.30	0.40
22.10	6.13	6.61	14.84	98.07	3.29	0.36	0.47
22.20	7.05	7.81	13.08	102.14	3.22	0.40	0.56
22.30	7.61	8.52	12.38	105.47	3.18	0.43	0.61
22.40	8.13	9.17	11.95	109.64	3.16	0.46	0.66
22.50	9.00	10.29	11.30	116.23	3.13	0.53	0.73
22.60	9.37	10.74	11.18	120.09	3.13	0.65	0.77
22.70	8.82	9.97	11.89	118.55	3.16	0.59	0.71
22.80	7.69	8.46	13.29	112.37	3.22	0.45	0.60
22.90	6.90	7.40	14.35	106.12	3.27	0.42	0.53
23.00	6.98	7.47	14.06	105.03	3.26	0.39	0.53
23.10	7.60	8.24	13.08	107.82	3.22	0.43	0.59
23.20	8.28	9.09	12.23	111.21	3.18	0.52	0.65
23.30	8.77	9.69	11.69	113.23	3.15	0.51	0.69
23.40	8.77	9.65	11.69	112.79	3.15	0.50	0.69
23.50	8.95	9.85	11.56	113.85	3.15	0.50	0.70
23.60	9.45	10.45	11.17	116.74	3.13	0.55	0.75
23.70	9.65	10.67	11.13	118.76	3.13	0.61	0.76
23.80	9.37	10.27	11.66	119.81	3.15	0.57	0.73
23.90	9.41	10.29	12.01	123.61	3.17	0.56	0.73
24.00	11.56	12.97	10.27	133.21	3.08	0.72	0.93
24.10	16.37	18.95	7.39	140.03	2.91	0.81	0.81
24.20	22.14	25.65	5.23	134.10	2.75	0.80	0.80

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
24.30	26.41	30.40	3.97	120.78	2.62	0.88	0.88
24.40	28.09	32.14	3.48	111.85	2.57	0.81	0.81
24.50	26.73	30.52	3.75	114.45	2.60	0.85	0.85
24.60	23.36	26.67	4.71	125.71	2.70	0.79	0.79
24.70	20.44	23.31	6.00	139.79	2.81	0.81	0.81
24.80	19.80	22.57	6.68	150.66	2.86	0.83	0.83
24.90	20.81	23.69	6.54	155.06	2.85	0.83	0.83
25.00	21.40	24.28	6.26	152.06	2.83	0.83	0.83
25.10	22.04	24.87	5.79	143.99	2.79	0.82	0.82
25.20	22.96	25.79	5.30	136.81	2.75	0.81	0.81
25.30	23.14	25.91	5.29	137.02	2.75	0.81	0.81
25.40	22.74	25.46	5.83	148.46	2.80	0.82	0.82
25.50	24.78	27.85	6.14	171.07	2.82	0.85	0.85
25.60	33.66	37.98	5.05	191.70	2.73	0.88	0.88
25.70	53.07	59.58	3.28	195.43	2.54	0.91	0.91
25.80	82.74	91.73	2.03	185.82	2.33	0.87	0.87
25.90	117.80	128.70	1.47	189.05	2.13	0.87	0.87
26.00	148.57	160.21	1.29	206.69	1.98	0.89	0.89
26.10	167.69	179.21	1.23	220.06	1.89	0.91	0.91
26.20	173.65	184.66	1.20	222.02	1.85	0.91	0.91
26.30	170.00	180.46	1.21	218.21	1.86	0.91	0.91
26.40	161.80	171.65	1.23	211.10	1.89	0.90	0.90
26.50	152.97	162.24	1.25	203.19	1.92	0.89	0.89
26.60	145.31	154.04	1.27	196.34	1.96	0.88	0.88
26.70	141.26	149.53	1.29	192.44	1.97	0.88	0.88
26.80	141.98	149.87	1.28	192.32	1.97	0.88	0.88
26.90	146.65	154.22	1.27	195.36	1.95	0.88	0.88
27.00	152.40	159.62	1.25	199.23	1.92	0.89	0.89
27.10	156.02	162.81	1.23	200.73	1.89	0.89	0.89
27.20	156.40	162.70	1.22	199.17	1.88	0.89	0.89
27.30	153.19	158.95	1.22	194.36	1.88	0.88	0.88
27.40	147.34	152.52	1.23	186.92	1.88	0.87	0.87
27.50	139.24	143.76	1.23	176.64	1.89	0.86	0.86
27.60	130.22	134.07	1.23	164.76	1.89	0.85	0.85
27.70	121.27	124.45	1.23	152.73	1.89	0.83	0.83
27.80	114.09	116.70	1.22	142.65	1.88	0.82	0.82
27.90	109.39	111.55	1.22	135.64	1.87	0.81	0.81
28.00	107.21	109.08	1.22	132.69	1.87	0.80	0.80
28.10	107.70	109.46	1.23	134.46	1.89	0.81	0.81
28.20	110.28	112.03	1.24	139.30	1.91	0.81	0.81
28.30	114.57	116.29	1.25	145.75	1.92	0.82	0.82
28.40	120.76	122.38	1.25	153.25	1.92	0.83	0.83
28.50	128.38	129.85	1.24	161.60	1.91	0.84	0.84
28.60	137.33	138.63	1.24	171.49	1.90	0.85	0.85
28.70	146.10	147.25	1.24	181.91	1.90	0.87	0.87
28.80	153.76	154.76	1.24	191.87	1.90	0.88	0.88
28.90	159.82	160.63	1.25	200.03	1.91	0.89	0.89
29.00	164.17	164.70	1.25	205.70	1.92	0.89	0.89

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
29.10	166.84	167.05	1.25	208.83	1.92	0.90	0.90
29.20	167.23	167.07	1.25	208.99	1.92	0.90	0.90
29.30	165.31	164.80	1.26	206.83	1.93	0.89	0.89
29.40	162.24	161.42	1.26	203.98	1.94	0.89	0.89
29.50	159.54	158.40	1.27	201.12	1.95	0.89	0.89
29.60	158.40	156.86	1.26	198.33	1.94	0.89	0.89
29.70	158.21	156.18	1.25	194.79	1.92	0.88	0.88
29.80	154.57	152.33	1.26	192.38	1.94	0.88	0.88
29.90	143.99	141.96	1.36	192.82	2.05	0.88	0.88
30.00	135.18	133.15	1.47	195.31	2.13	0.88	0.88
30.10	132.28	129.84	1.43	185.80	2.11	0.87	0.87
30.20	131.76	128.75	1.33	171.55	2.03	0.85	0.85
30.30	123.68	120.49	1.33	160.84	2.03	0.84	0.84
30.40	107.40	104.49	1.52	159.11	2.16	0.84	0.84
30.50	91.85	89.16	1.88	167.52	2.29	0.85	0.85
30.60	84.79	82.08	2.18	178.54	2.36	0.86	0.86
30.70	90.92	87.85	2.05	180.41	2.33	0.86	0.86
30.80	108.65	104.82	1.69	176.75	2.23	0.86	0.86
30.90	128.66	123.87	1.43	177.20	2.11	0.86	0.86
31.00	143.23	137.56	1.32	182.22	2.02	0.87	0.87
31.10	150.57	144.28	1.29	186.10	1.98	0.87	0.87
31.20	153.08	146.38	1.29	188.32	1.97	0.87	0.87
31.30	152.85	145.85	1.29	188.71	1.98	0.87	0.87
31.40	149.11	141.97	1.31	186.10	2.00	0.87	0.87
31.50	141.26	134.15	1.34	180.37	2.04	0.86	0.86
31.60	130.34	123.43	1.40	172.88	2.09	0.86	0.86
31.70	118.72	112.05	1.47	164.46	2.13	0.85	0.85
31.80	108.66	102.19	1.52	155.22	2.16	0.83	0.83
31.90	100.38	94.06	1.55	145.43	2.17	0.82	0.82
32.00	93.10	86.92	1.59	137.98	2.19	0.81	0.81
32.10	86.10	80.08	1.70	136.33	2.23	0.81	0.81
32.20	78.52	72.72	1.96	142.75	2.31	0.82	0.82
32.30	69.94	64.43	2.43	156.46	2.41	0.84	0.84
32.40	60.92	55.75	3.11	173.12	2.52	0.86	0.86
32.50	53.88	48.96	3.80	186.26	2.61	0.96	0.96
32.60	50.19	45.36	4.30	194.91	2.66	1.02	1.02
32.70	49.69	44.75	4.55	203.44	2.68	1.06	1.06
32.80	52.24	47.00	4.54	213.56	2.68	1.07	1.07
32.90	56.89	51.19	4.34	222.04	2.66	1.06	1.06
33.00	62.25	56.03	4.03	225.59	2.63	1.03	1.03
33.10	68.14	61.33	3.65	223.61	2.59	0.98	0.98
33.20	75.90	68.36	3.17	216.38	2.53	0.92	0.92
33.30	85.75	77.30	2.66	205.91	2.45	0.89	0.89
33.40	93.70	84.46	2.35	198.06	2.39	0.88	0.88
33.50	96.01	86.38	2.27	195.78	2.38	0.88	0.88
33.60	92.45	82.87	2.40	198.97	2.41	0.89	0.89
33.70	84.75	75.56	2.69	203.61	2.46	0.89	0.89
33.80	74.88	66.31	3.08	204.33	2.51	0.89	0.89

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
33.90	64.13	56.33	3.52	198.30	2.57	0.94	0.94
34.00	54.10	47.08	3.96	186.34	2.62	0.97	0.97
34.10	46.11	39.73	4.37	173.63	2.67	1.00	1.00
34.20	39.59	33.73	4.88	164.76	2.72	0.85	0.85
34.30	34.09	28.69	5.58	160.14	2.78	0.84	0.84
34.40	29.36	24.36	6.41	156.10	2.84	0.84	0.84
34.50	25.02	20.43	7.25	148.09	2.90	0.82	0.82
34.60	21.00	16.82	8.19	137.74	2.96	0.81	0.81
34.70	17.76	13.93	9.28	129.28	3.03	0.67	0.99
34.80	15.83	12.19	10.36	126.28	3.09	0.67	0.87
34.90	15.33	11.72	10.85	127.20	3.11	0.67	0.84
35.00	15.28	11.64	11.11	129.34	3.12	0.68	0.83
35.10	15.62	11.91	11.34	135.08	3.14	0.73	0.85
35.20	16.74	12.85	11.28	144.97	3.13	0.87	0.92
35.30	19.92	15.58	10.03	156.19	3.07	1.06	1.11
35.40	25.11	20.03	8.02	160.65	2.95	0.84	0.84
35.50	32.33	26.27	6.00	157.69	2.81	0.84	0.84
35.60	40.65	33.55	4.45	149.25	2.67	0.97	0.97
35.70	48.86	40.74	3.43	139.85	2.56	0.85	0.85
35.80	55.37	46.44	2.81	130.29	2.47	0.80	0.80
35.90	57.47	48.24	2.54	122.48	2.43	0.79	0.79
36.00	55.09	46.03	2.64	121.48	2.45	0.79	0.79
36.10	48.80	40.35	3.19	128.75	2.53	0.81	0.81
36.20	40.68	33.09	4.26	140.85	2.66	0.94	0.94
36.30	33.39	26.63	5.62	149.63	2.78	0.83	0.83
36.40	29.34	23.06	6.62	152.64	2.86	0.83	0.83
36.50	29.53	23.16	6.57	152.12	2.85	0.83	0.83
36.60	32.29	25.47	5.95	151.52	2.81	0.83	0.83
36.70	34.52	27.32	5.62	153.45	2.78	0.83	0.83
36.80	34.12	26.88	5.89	158.27	2.80	0.84	0.84
36.90	31.26	24.34	6.70	163.05	2.86	0.84	0.84
37.00	28.61	22.06	7.44	164.19	2.92	0.85	0.85
37.10	30.10	23.24	6.92	160.90	2.88	0.84	0.84
37.20	36.63	28.76	5.26	151.31	2.75	0.83	0.83
37.30	46.22	36.94	3.75	138.69	2.60	0.89	0.89
37.40	55.48	44.85	2.90	130.26	2.49	0.80	0.80
37.50	62.76	51.02	2.52	128.52	2.43	0.80	0.80
37.60	68.04	55.45	2.32	128.50	2.39	0.80	0.80
37.70	71.11	58.00	2.17	126.04	2.36	0.79	0.79
37.80	72.57	59.17	2.08	122.99	2.34	0.79	0.79
37.90	72.53	59.02	2.07	122.32	2.34	0.79	0.79
38.00	71.83	58.28	2.11	122.81	2.34	0.79	0.79
38.10	71.07	57.52	2.11	121.29	2.35	0.78	0.78
38.20	70.43	56.90	2.06	117.17	2.33	0.78	0.78
38.30	69.54	56.06	2.04	114.12	2.33	0.77	0.77
38.40	67.93	54.55	2.11	115.14	2.35	0.77	0.77
38.50	66.57	53.19	2.28	121.02	2.38	0.78	0.78
38.60	67.27	53.57	2.40	128.60	2.41	0.80	0.80

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
38.70	70.56	56.15	2.40	134.82	2.41	0.81	0.81
38.80	74.92	59.66	2.33	138.76	2.39	0.81	0.81
38.90	78.18	62.25	2.27	141.24	2.38	0.81	0.81
39.00	79.69	63.35	2.26	143.06	2.38	0.82	0.82
39.10	79.93	63.40	2.27	143.96	2.38	0.82	0.82
39.20	80.59	63.82	2.25	143.34	2.37	0.82	0.82
39.30	82.67	65.46	2.15	140.67	2.35	0.81	0.81
39.40	86.56	68.65	2.00	137.30	2.32	0.81	0.81
39.50	91.52	72.75	1.85	134.59	2.28	0.81	0.81
39.60	96.64	76.97	1.73	133.36	2.24	0.80	0.80
39.70	100.82	80.33	1.68	134.76	2.22	0.81	0.81
39.80	100.16	79.44	1.77	140.84	2.26	0.81	0.81
39.90	91.82	72.01	2.13	153.15	2.35	0.83	0.83
40.00	78.37	60.48	2.79	169.03	2.47	0.85	0.85
40.10	62.81	47.50	3.80	180.50	2.61	0.95	0.95
40.20	50.47	37.38	4.92	183.83	2.72	0.87	0.87
40.30	42.83	31.15	5.99	186.64	2.81	0.87	0.87
40.40	43.11	31.27	6.04	188.86	2.81	0.87	0.87
40.50	50.11	36.80	5.04	185.32	2.73	0.87	0.87
40.60	60.63	45.25	3.81	172.25	2.61	0.94	0.94
40.70	71.15	53.85	2.85	153.69	2.48	0.83	0.83
40.80	79.36	60.65	2.28	138.37	2.38	0.81	0.81
40.90	84.78	64.99	2.11	136.99	2.34	0.81	0.81
41.00	87.82	67.27	2.09	140.49	2.34	0.81	0.81
41.10	89.49	68.46	2.07	142.01	2.34	0.82	0.82
41.20	89.73	68.58	2.02	138.85	2.33	0.81	0.81
41.30	88.42	67.39	2.03	137.12	2.33	0.81	0.81
41.40	85.38	64.71	2.17	140.14	2.36	0.81	0.81
41.50	81.32	61.22	2.33	142.45	2.39	0.82	0.82
41.60	76.93	57.52	2.52	144.69	2.43	0.82	0.82
41.70	71.43	52.92	2.81	148.63	2.47	0.83	0.83
41.80	63.51	46.42	3.33	154.67	2.55	0.86	0.86
41.90	53.29	38.19	4.22	161.22	2.65	0.97	0.97
42.00	42.53	29.71	5.48	162.75	2.77	0.84	0.84
42.10	34.54	23.55	6.70	157.74	2.86	0.84	0.84
42.20	31.16	21.03	7.16	150.55	2.90	0.83	0.83
42.30	31.50	21.22	6.98	148.03	2.88	0.82	0.82
42.40	32.59	21.97	6.82	149.89	2.87	0.83	0.83
42.50	33.35	22.46	6.68	150.00	2.86	0.83	0.83
42.60	35.87	24.35	5.88	143.15	2.80	0.82	0.82
42.70	41.37	28.64	4.51	129.26	2.68	0.94	0.94
42.80	48.14	33.98	3.40	115.68	2.56	0.81	0.81
42.90	52.92	37.69	2.97	111.97	2.50	0.77	0.77
43.00	54.26	38.58	3.02	116.71	2.51	0.77	0.77
43.10	53.34	37.62	3.40	127.99	2.56	0.83	0.83
43.20	52.35	36.62	3.81	139.50	2.61	0.89	0.89
43.30	52.52	36.55	4.06	148.56	2.63	0.93	0.93
43.40	52.22	36.15	4.29	155.03	2.66	0.96	0.96

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
43.50	48.54	33.19	4.89	162.45	2.72	0.84	0.84
43.60	41.40	27.65	6.19	171.06	2.83	0.85	0.85
43.70	34.45	22.61	7.96	179.95	2.95	0.86	0.86
43.80	31.79	20.68	8.97	185.44	3.01	1.55	1.48
43.90	34.60	22.61	8.32	188.01	2.97	0.87	0.87
44.00	42.45	28.08	6.58	184.73	2.86	0.87	0.87
44.10	56.31	38.44	4.48	172.25	2.68	1.01	1.01
44.20	76.28	53.80	2.85	153.28	2.48	0.83	0.83
44.30	99.38	71.80	2.01	144.35	2.32	0.82	0.82
44.40	119.56	87.63	1.67	145.92	2.22	0.82	0.82
44.50	132.51	97.74	1.54	150.24	2.17	0.83	0.83
44.60	138.38	102.38	1.47	150.70	2.13	0.83	0.83
44.70	140.97	103.95	1.50	155.94	2.15	0.83	0.83
44.80	145.61	106.65	1.60	170.66	2.19	0.85	0.85
44.90	154.46	112.95	1.61	182.24	2.20	0.87	0.87
45.00	166.62	122.52	1.50	183.93	2.15	0.87	0.87
45.10	178.48	132.40	1.38	182.40	2.07	0.87	0.87
45.20	186.02	138.62	1.33	184.20	2.02	0.87	0.87
45.30	188.08	140.04	1.32	185.25	2.02	0.87	0.87
45.40	185.50	137.74	1.33	183.02	2.02	0.87	0.87
45.50	181.44	134.28	1.34	179.72	2.03	0.86	0.86
45.60	177.58	131.04	1.35	176.34	2.04	0.86	0.86
45.70	174.36	128.30	1.35	173.50	2.05	0.86	0.86
45.80	172.20	126.39	1.36	171.53	2.05	0.85	0.85
45.90	170.69	124.98	1.36	170.25	2.06	0.85	0.85
46.00	169.69	123.92	1.37	169.73	2.06	0.85	0.85
46.10	168.85	122.93	1.38	169.73	2.07	0.85	0.85
46.20	168.16	122.03	1.39	170.19	2.08	0.85	0.85
46.30	168.23	121.73	1.41	171.23	2.09	0.85	0.85
46.40	169.90	122.75	1.41	172.53	2.09	0.86	0.86
46.50	173.64	125.52	1.39	173.95	2.08	0.86	0.86
46.60	178.99	129.70	1.35	175.62	2.05	0.86	0.86
46.70	184.20	133.83	1.32	177.31	2.02	0.86	0.86
46.80	187.77	136.74	1.30	178.03	1.99	0.86	0.86
46.90	188.69	137.65	1.28	176.71	1.97	0.86	0.86
47.00	186.98	136.54	1.27	173.38	1.95	0.86	0.86
47.10	183.33	133.82	1.26	168.99	1.94	0.85	0.85
47.20	178.78	130.22	1.26	164.54	1.94	0.85	0.85
47.30	174.33	126.56	1.27	160.75	1.95	0.84	0.84
47.40	170.46	123.28	1.28	157.73	1.96	0.84	0.84
47.50	167.19	120.45	1.29	155.30	1.98	0.83	0.83
47.60	164.34	117.95	1.30	153.25	1.99	0.83	0.83
47.70	161.94	115.81	1.31	151.63	2.00	0.83	0.83
47.80	159.85	113.93	1.32	150.26	2.01	0.83	0.83
47.90	158.50	112.59	1.33	149.62	2.02	0.83	0.83
48.00	158.82	112.51	1.34	150.31	2.03	0.83	0.83
48.10	160.82	113.66	1.34	152.65	2.04	0.83	0.83
48.20	163.04	114.92	1.35	155.37	2.05	0.83	0.83

:: Strength loss calculation (Robertson (2009)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
48.30	164.06	115.25	1.37	157.39	2.06	0.84	0.84
48.40	164.39	115.09	1.38	158.78	2.07	0.84	0.84
48.50	165.33	115.47	1.39	160.12	2.08	0.84	0.84
48.60	167.37	116.74	1.39	161.72	2.08	0.84	0.84
48.70	169.66	118.23	1.38	163.29	2.07	0.84	0.84
48.80	171.13	119.04	1.38	164.67	2.07	0.85	0.85
48.90	171.49	118.87	1.40	166.37	2.09	0.85	0.85
49.00	171.23	118.08	1.43	168.94	2.11	0.85	0.85
49.10	171.53	117.67	1.47	172.78	2.13	0.86	0.86
49.20	174.62	119.41	1.49	177.75	2.14	0.86	0.86
49.30	181.47	124.10	1.47	182.96	2.13	0.87	0.87
49.40	191.66	131.49	1.43	188.20	2.11	0.87	0.87
49.50	202.91	139.89	1.38	193.23	2.07	0.88	0.88
49.60	212.53	147.20	1.34	197.41	2.04	0.88	0.88
49.70	219.60	152.68	1.31	200.36	2.01	0.89	0.89
49.80	223.07	155.33	1.30	201.52	1.99	0.89	0.89

Abbreviations

q_t :	Total cone resistance
K_c :	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c :	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

LIQUEFACTION ANALYSIS REPORT

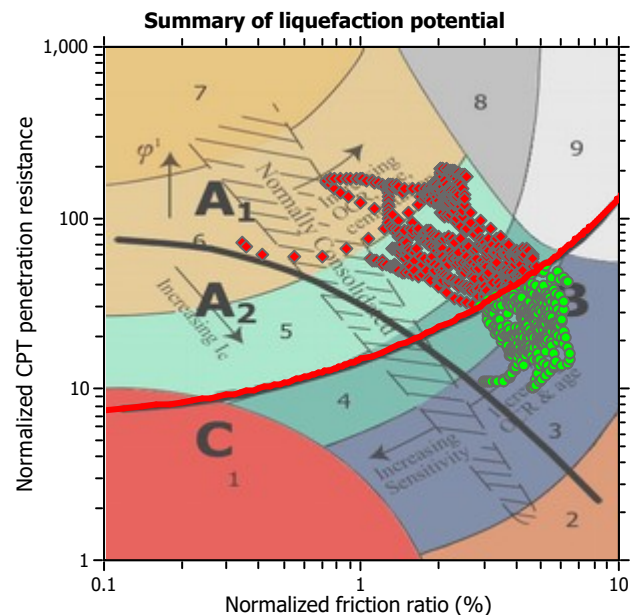
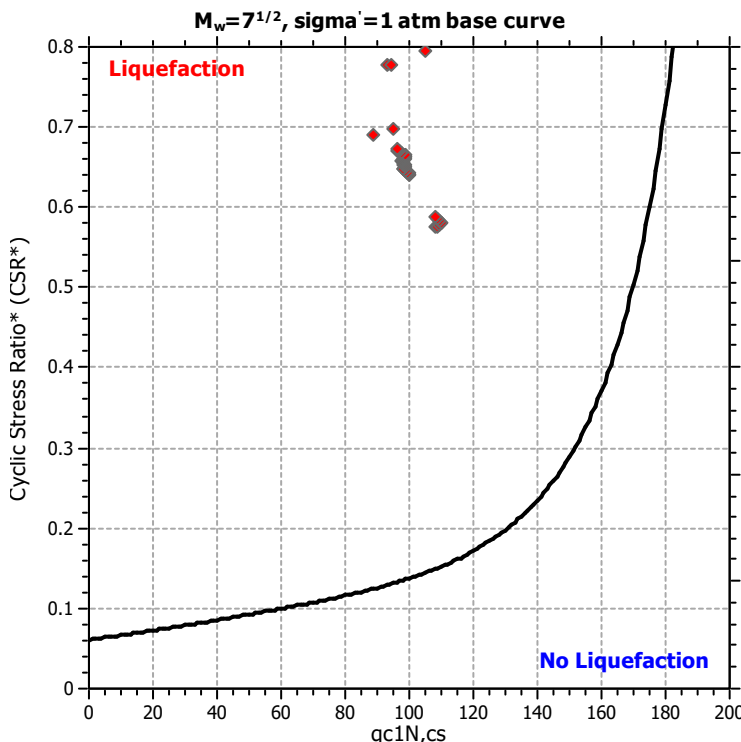
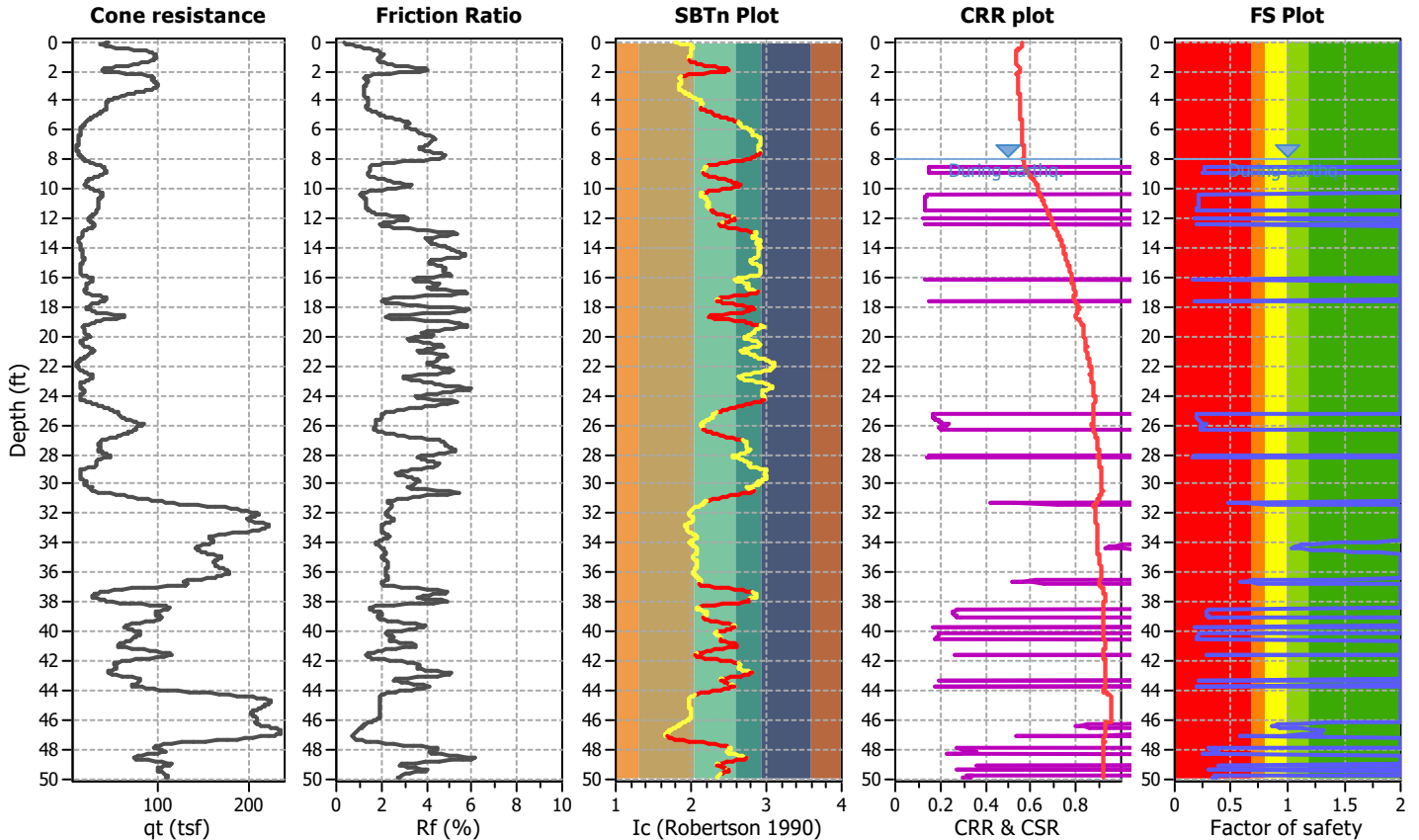
Project title : 21-483 Equestrian Estates

Location : Avenue 64 at Harrison Street, Thermal California

CPT file : CPT-1 B&I 2014

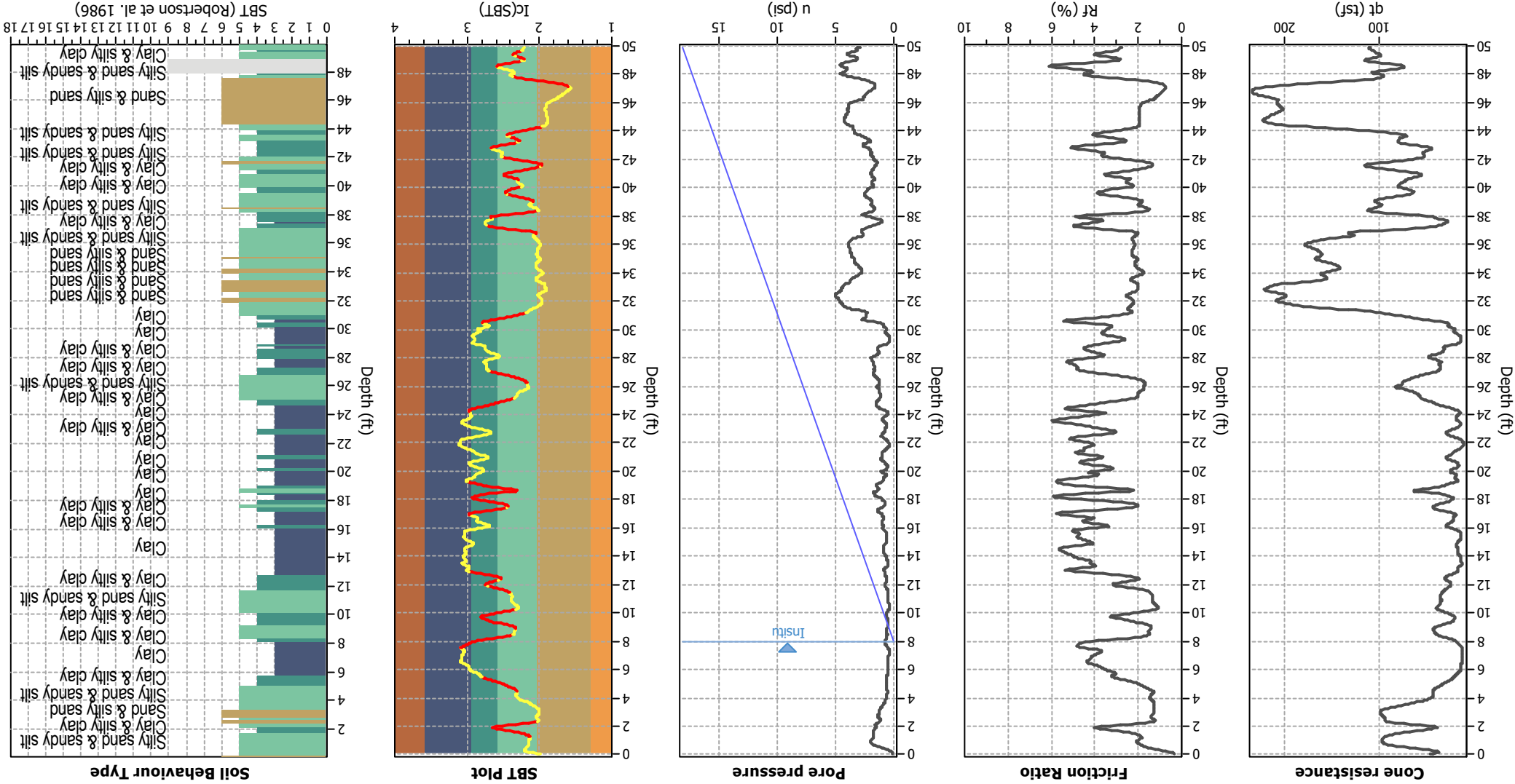
Input parameters and analysis data

Analysis method:	B&I (2014)	G.W.T. (in-situ):	8.00 ft	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	8.00 ft	Fill height:	N/A	Limit depth applied:	No
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth:	N/A
Earthquake magnitude M_w :	7.34	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.74	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		

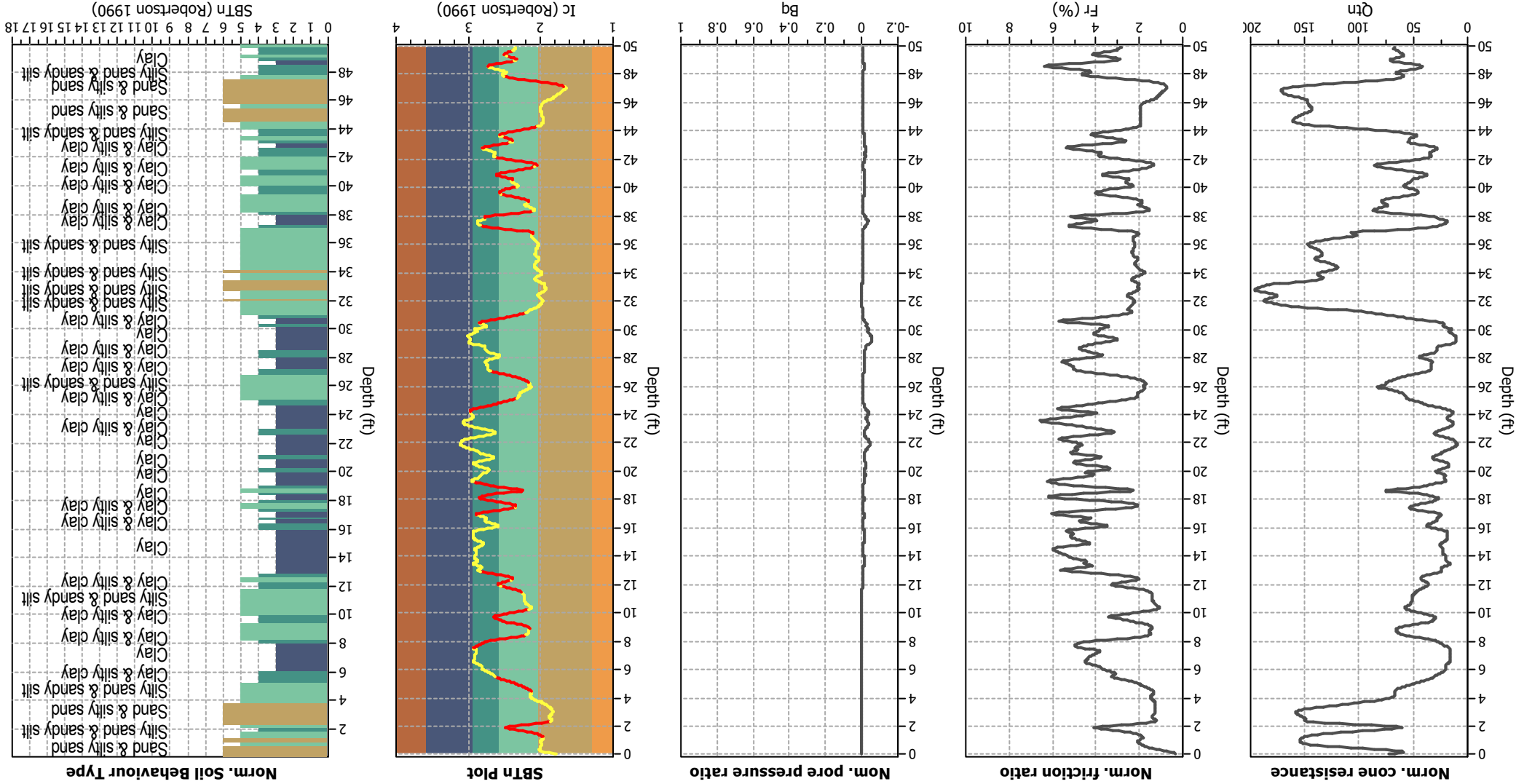


Zone A₁: Cyclic liquefaction likely depending on size and duration of cyclic loading
 Zone A₂: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
 Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
 Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



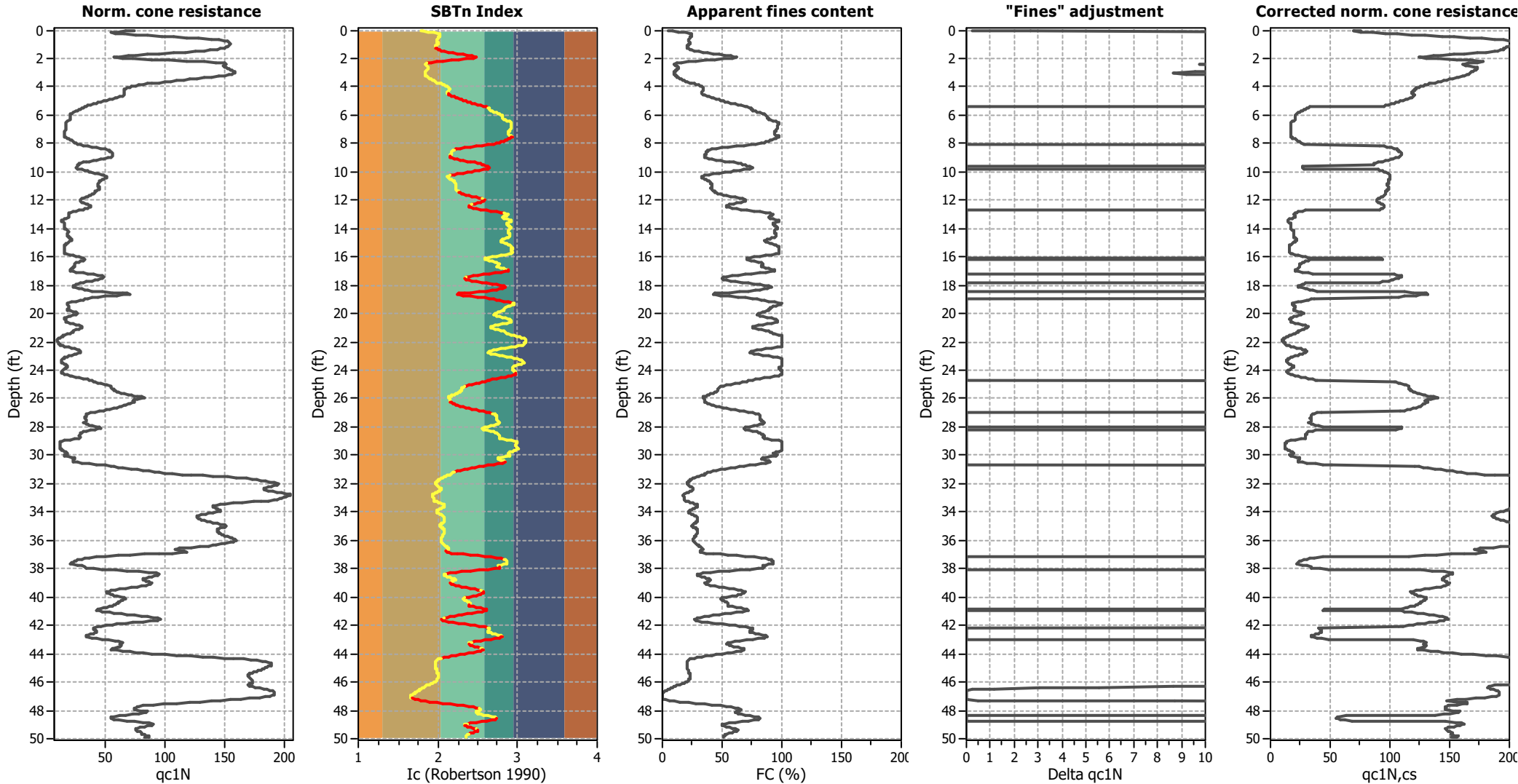
CPT basic interpretation plots (normalized)



Input parameters and analysis data

Analysis method:	B&I (2014)
Fines correction method:	B&I (2014)
Points to test:	Based on Ic value
Earthquake magnitude M_w :	7.34
Peak ground acceleration:	0.74
Depth to water table (instu):	8.00 ft
Depth to GWT (earthq.):	8.00 ft
Average results interval:	3
Ic cut-off value:	2.60
Unit weight calculation:	Based on SBT
Use fill:	No
Fill height:	N/A
Fill weight:	N/A
Transition detect. applied:	Yes
Clay like behavior applied:	Sands only
Limit depth:	No
Limit depth applied:	No
Limit depth:	N/A

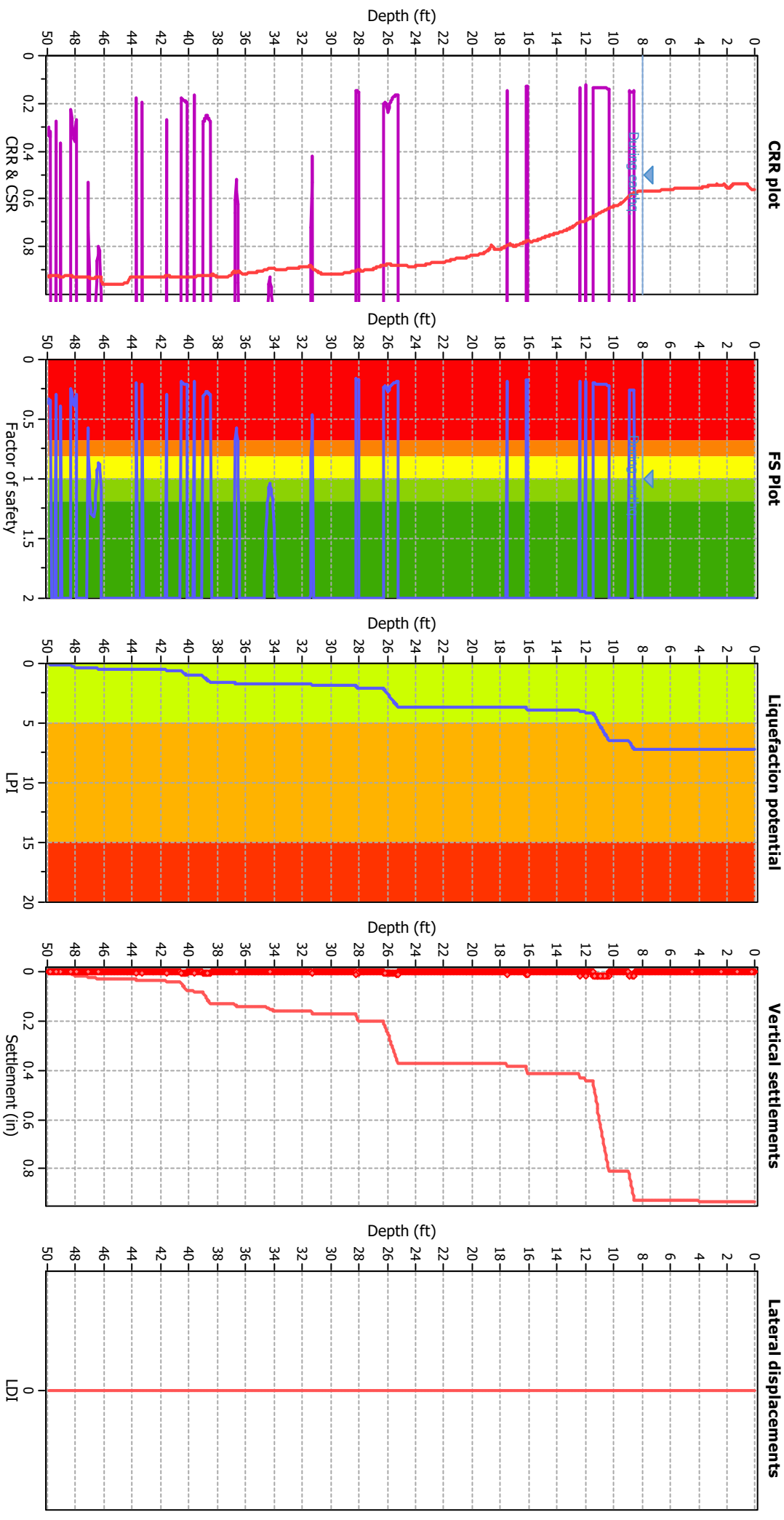
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _g applied:	Yes
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)
Fines correction method:	B&I (2014)
Points to test:	Based on Ic value
Earthquake magnitude M_w :	7.34
Peak ground acceleration:	0.74
Depth to water table (instn):	8.00 ft
Depth to GWT (ethq.):	8.00 ft
Average results interval:	3
Ic cut-off value:	2.60
Unit weight calculation:	Based on SBT
Use fill:	No
Fill height:	N/A
Fill weight:	N/A
Transition detect. applied:	Yes
K_u applied:	Yes
Clay like behavior applied:	Yes
Limit depth applied:	No
Limit depth:	N/A

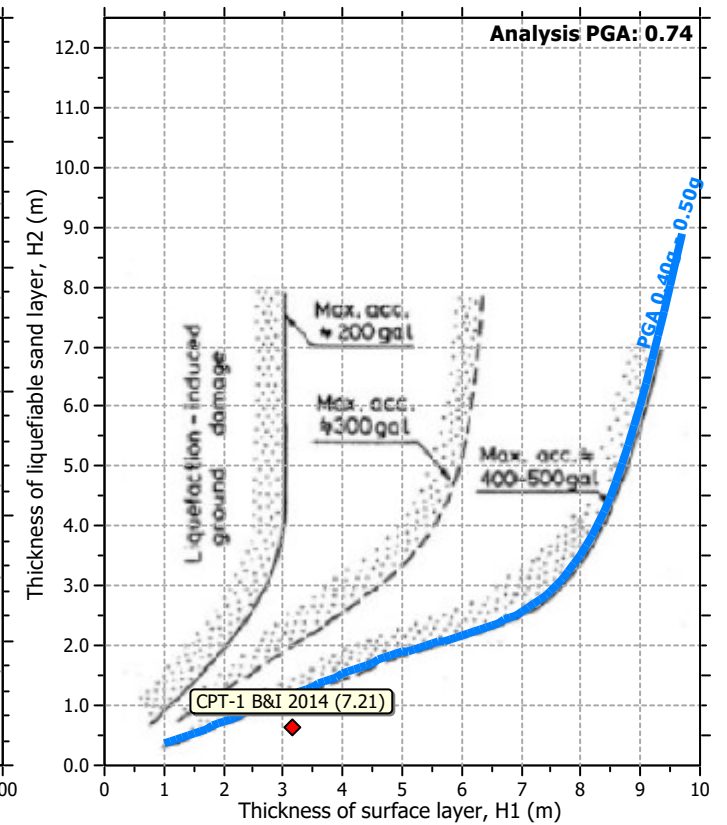
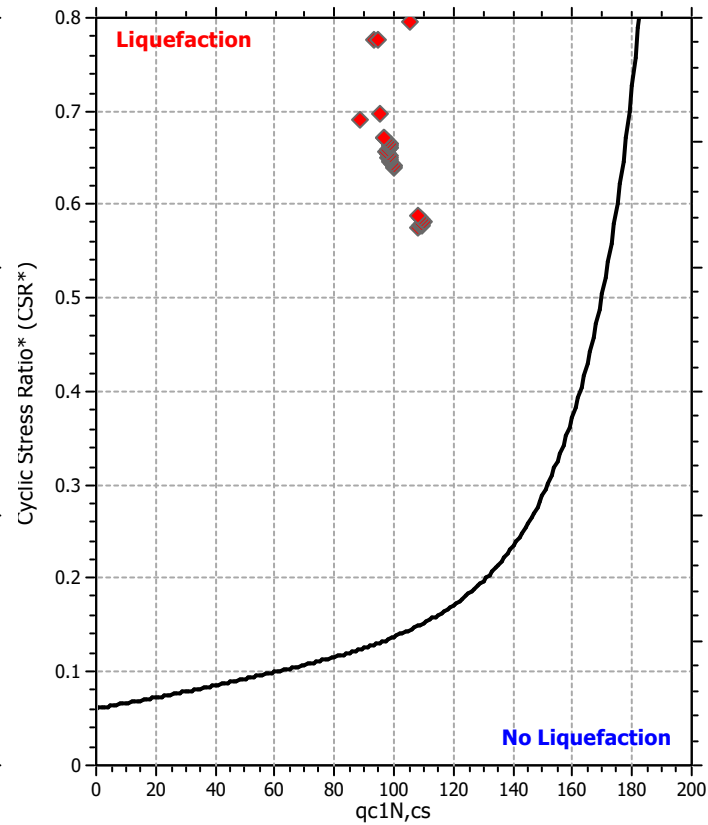
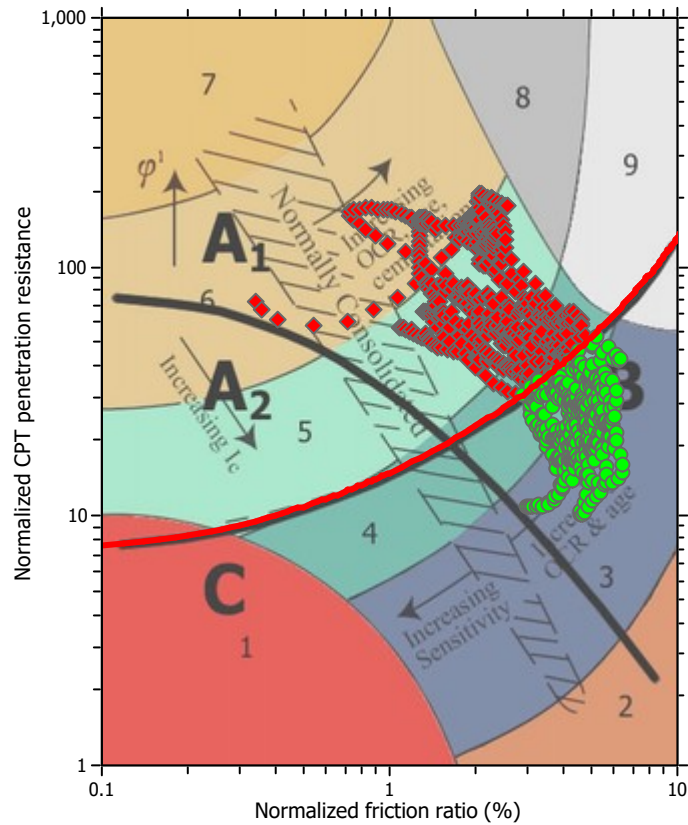
F.S. color scheme

Almost certain it will liquify
Very likely to liquify
Liquefaction and no liq. are equally likely
Unlike to liquify
Almost certain it will not liquify

LPI color scheme

Very high risk
High risk
Low risk

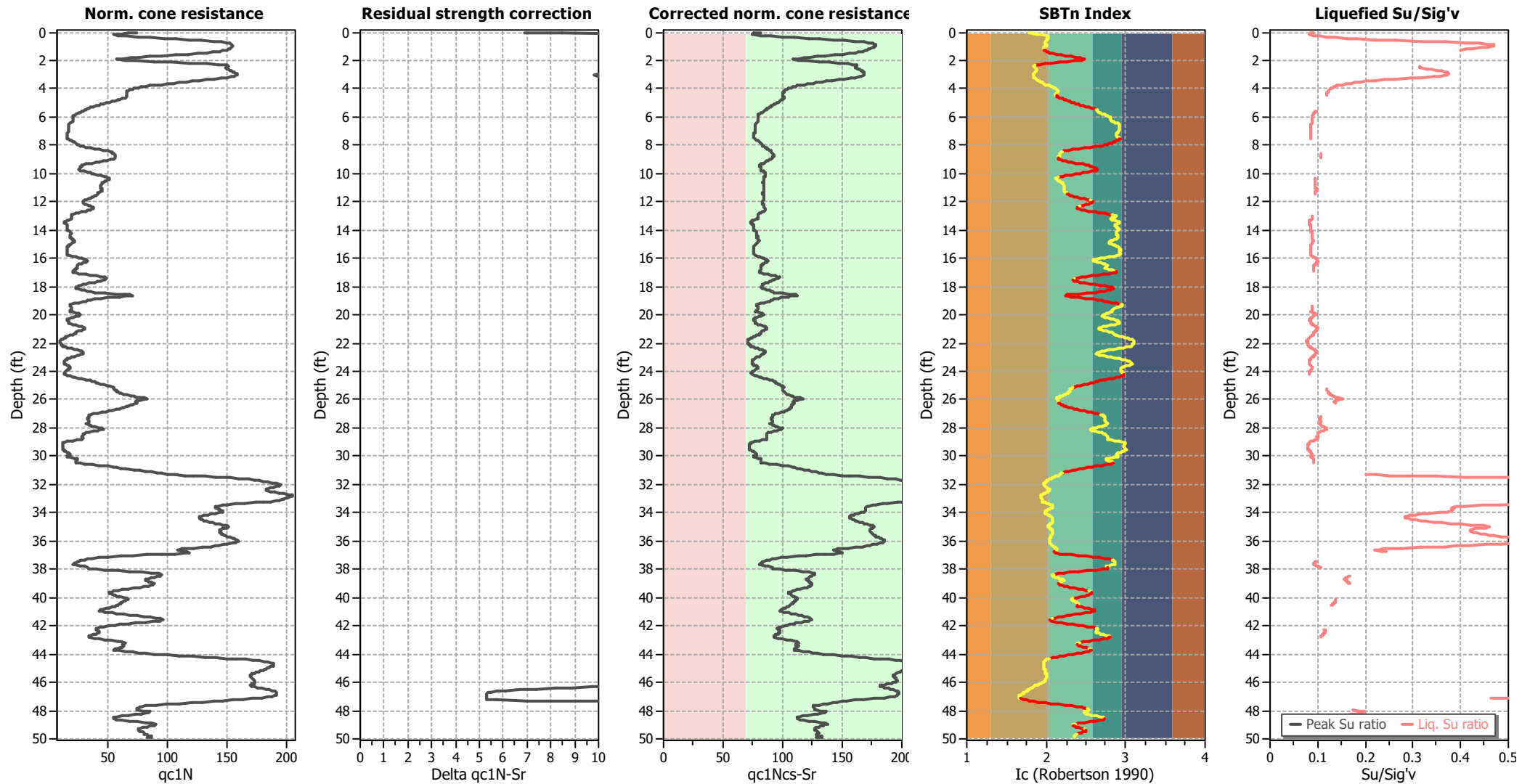
Liquefaction analysis summary plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	Yes
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

Check for strength loss plots (Idriss & Boulanger (2008))



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	Yes
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

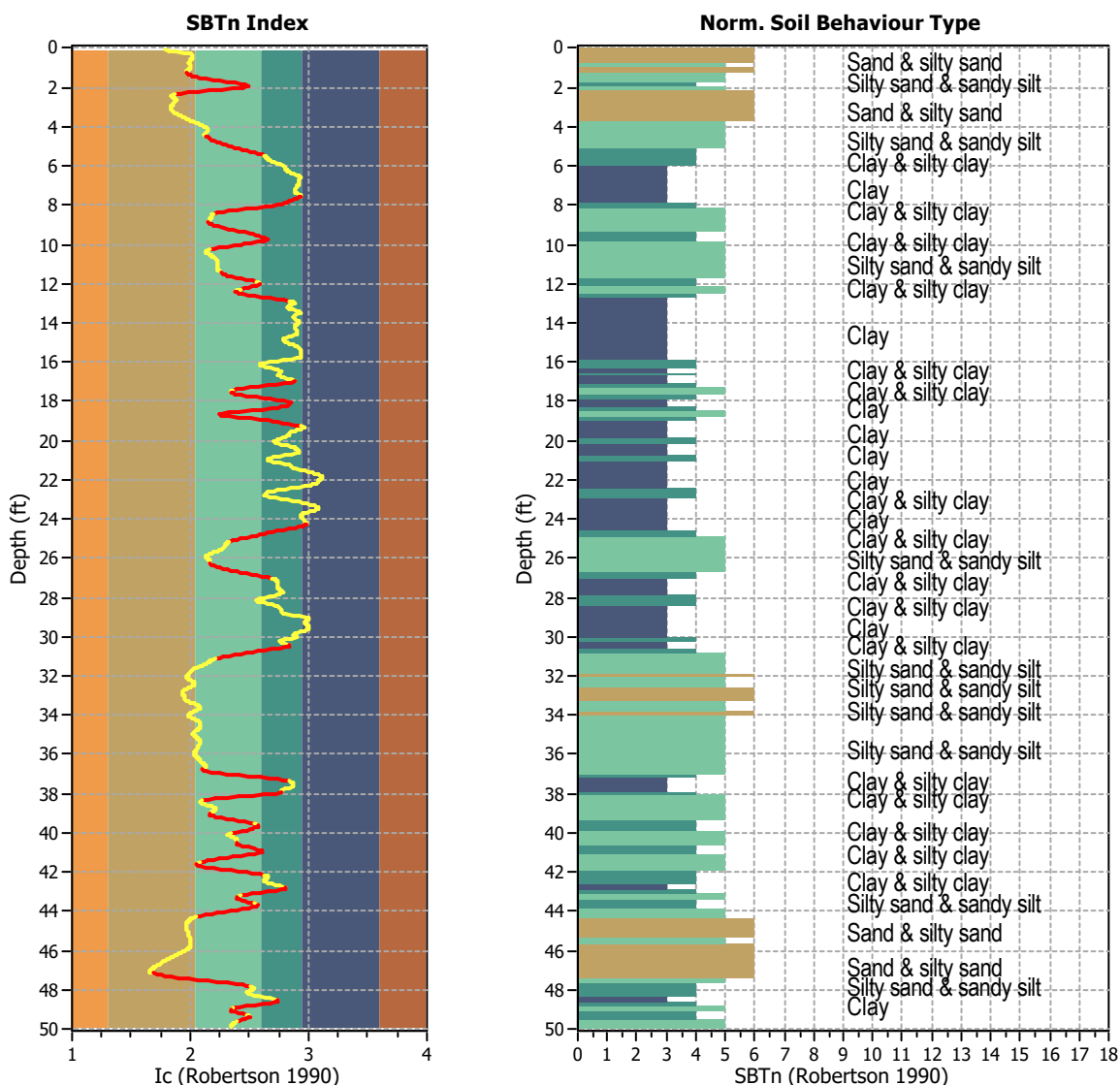
TRANSITION LAYER DETECTION ALGORITHM REPORT

Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vice-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between $1.80 < I_c < 3.0$) and a rate of change of I_c . Transitions typically occur when the rate of change of I_c is fast (i.e. ΔI_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties

I_c minimum check value: 1.70
 I_c maximum check value: 3.00
 I_c change ratio value: 0.0250
 Minimum number of points in layer: 4

General statistics

Total points in CPT file: 998
 Total points excluded: 355
 Exclusion percentage: 35.57%
 Number of layers detected: 30

Transition layer No	Number of points	Depth	SBT _n number	SBT _n description
Transition layer 1	13	Start depth: 1.30 (ft)	6	Sand & silty sand
		End depth: 1.90 (ft)	4	Clay & silty clay
Transition layer 2	10	Start depth: 1.95 (ft)	4	Clay & silty clay
		End depth: 2.40 (ft)	6	Sand & silty sand
Transition layer 3	20	Start depth: 4.55 (ft)	5	Silty sand & sandy silt
		End depth: 5.50 (ft)	4	Clay & silty clay
Transition layer 4	19	Start depth: 7.60 (ft)	3	Clay
		End depth: 8.50 (ft)	5	Silty sand & sandy silt
Transition layer 5	16	Start depth: 8.95 (ft)	5	Silty sand & sandy silt
		End depth: 9.70 (ft)	4	Clay & silty clay
Transition layer 6	12	Start depth: 9.75 (ft)	4	Clay & silty clay
		End depth: 10.30 (ft)	5	Silty sand & sandy silt
Transition layer 7	10	Start depth: 11.50 (ft)	5	Silty sand & sandy silt
		End depth: 11.95 (ft)	4	Clay & silty clay
Transition layer 8	7	Start depth: 12.05 (ft)	4	Clay & silty clay
		End depth: 12.35 (ft)	5	Silty sand & sandy silt
Transition layer 9	11	Start depth: 12.45 (ft)	5	Silty sand & sandy silt
		End depth: 12.95 (ft)	3	Clay
Transition layer 10	11	Start depth: 17.00 (ft)	3	Clay
		End depth: 17.50 (ft)	5	Silty sand & sandy silt
Transition layer 11	11	Start depth: 17.60 (ft)	5	Silty sand & sandy silt
		End depth: 18.10 (ft)	3	Clay
Transition layer 12	11	Start depth: 18.15 (ft)	3	Clay
		End depth: 18.65 (ft)	5	Silty sand & sandy silt
Transition layer 13	13	Start depth: 18.70 (ft)	5	Silty sand & sandy silt
		End depth: 19.30 (ft)	3	Clay
Transition layer 14	19	Start depth: 24.30 (ft)	3	Clay
		End depth: 25.20 (ft)	5	Silty sand & sandy silt
Transition layer 15	17	Start depth: 26.30 (ft)	5	Silty sand & sandy silt
		End depth: 27.10 (ft)	4	Clay & silty clay
Transition layer 16	15	Start depth: 30.50 (ft)	3	Clay
		End depth: 31.20 (ft)	5	Silty sand & sandy silt
Transition layer 17	13	Start depth: 36.80 (ft)	5	Silty sand & sandy silt
		End depth: 37.40 (ft)	3	Clay
Transition layer 18	10	Start depth: 37.95 (ft)	3	Clay
		End depth: 38.40 (ft)	5	Silty sand & sandy silt
Transition layer 19	11	Start depth: 39.10 (ft)	5	Silty sand & sandy silt
		End depth: 39.60 (ft)	4	Clay & silty clay
Transition layer 20	9	Start depth: 39.70 (ft)	4	Clay & silty clay
		End depth: 40.10 (ft)	5	Silty sand & sandy silt
Transition layer 21	7	Start depth: 40.60 (ft)	5	Silty sand & sandy silt
		End depth: 40.90 (ft)	4	Clay & silty clay
Transition layer 22	13	Start depth: 40.95 (ft)	4	Clay & silty clay
		End depth: 41.55 (ft)	5	Silty sand & sandy silt
Transition layer 23	12	Start depth: 41.65 (ft)	5	Silty sand & sandy silt
		End depth: 42.20 (ft)	4	Clay & silty clay

Transition layer No	Number of points	Depth	SBT _n number	SBT _n description
Transition layer 24	9	Start depth: 42.85 (ft)	3	Clay
		End depth: 43.25 (ft)	5	Silty sand & sandy silt
Transition layer 25	7	Start depth: 43.35 (ft)	5	Silty sand & sandy silt
		End depth: 43.65 (ft)	4	Clay & silty clay
Transition layer 26	13	Start depth: 43.75 (ft)	4	Clay & silty clay
		End depth: 44.35 (ft)	5	Silty sand & sandy silt
Transition layer 27	15	Start depth: 47.20 (ft)	6	Sand & silty sand
		End depth: 47.90 (ft)	4	Clay & silty clay
Transition layer 28	9	Start depth: 48.60 (ft)	3	Clay
		End depth: 49.00 (ft)	5	Silty sand & sandy silt
Transition layer 29	6	Start depth: 49.10 (ft)	5	Silty sand & sandy silt
		End depth: 49.35 (ft)	4	Clay & silty clay
Transition layer 30	6	Start depth: 49.45 (ft)	4	Clay & silty clay
		End depth: 49.70 (ft)	5	Silty sand & sandy silt

Start depth: Depth where the transition layer begins

End depth: Depth where the transition layer ends

:: Field input data ::						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1	0.05	46.61	0.17	0.17	5.00	105.92
2	0.10	41.73	0.12	0.12	5.00	105.56
3	0.15	38.20	0.16	0.16	5.00	105.58
4	0.20	34.72	0.19	0.19	11.72	107.29
5	0.25	36.71	0.26	0.26	12.99	109.44
6	0.30	41.02	0.36	0.36	13.37	112.03
7	0.35	47.26	0.49	0.49	13.50	114.59
8	0.40	53.15	0.65	0.65	13.39	116.94
9	0.45	60.84	0.84	0.84	13.36	118.98
10	0.50	66.84	1.03	1.03	13.18	120.73
11	0.55	74.08	1.22	1.22	13.07	122.20
12	0.60	80.26	1.41	1.41	12.87	123.46
13	0.65	86.58	1.59	1.59	12.75	124.46
14	0.70	90.81	1.73	1.73	12.68	125.22
15	0.75	93.59	1.84	1.84	12.70	125.73
16	0.80	95.01	1.91	1.91	12.79	126.08
17	0.85	95.71	1.96	1.96	12.87	126.29
18	0.90	96.26	1.99	1.99	12.93	126.42
19	0.95	96.40	2.00	2.00	12.88	126.42
20	1.00	96.47	1.96	1.96	12.76	126.32
21	1.05	96.35	1.91	1.91	12.52	126.11
22	1.10	96.08	1.83	1.83	12.30	125.87
23	1.15	95.50	1.78	1.78	12.10	125.61
24	1.20	94.73	1.73	1.73	12.06	125.45
25	1.25	93.78	1.73	1.73	12.18	125.33
26	1.30	91.81	1.72	1.72	12.49	125.31
27	1.35	89.77	1.74	1.74	12.93	125.23
28	1.40	86.25	1.73	1.73	13.54	125.19
29	1.45	82.97	1.75	1.75	14.36	125.13
30	1.50	78.61	1.77	1.77	15.44	125.06
31	1.55	72.91	1.77	1.77	16.86	124.95
32	1.60	66.87	1.80	1.80	18.61	124.66
33	1.65	59.23	1.73	1.73	20.68	124.35
34	1.70	53.45	1.73	1.73	22.93	123.87
35	1.75	47.26	1.65	1.65	25.23	123.51
36	1.80	43.36	1.66	1.66	27.39	123.03
37	1.85	39.40	1.58	1.58	29.18	122.67
38	1.90	37.27	1.54	1.54	30.23	122.23
39	1.95	36.39	1.47	1.47	29.92	122.19
40	2.00	40.23	1.54	1.54	27.97	122.36
41	2.05	45.90	1.54	1.54	24.76	122.99
42	2.10	55.81	1.63	1.63	21.15	123.39
43	2.15	64.60	1.55	1.55	17.79	123.69
44	2.20	73.88	1.49	1.49	14.82	123.64
45	2.25	82.86	1.40	1.40	12.44	123.41
46	2.30	89.17	1.27	1.27	10.64	123.05
47	2.35	93.51	1.20	1.20	9.50	122.64
48	2.40	94.40	1.14	1.14	9.02	122.43

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
49	2.45	93.84	1.15	1.15	9.00	122.39
50	2.50	93.33	1.18	1.18	9.27	122.59
51	2.55	92.98	1.24	1.24	9.58	122.89
52	2.60	93.48	1.29	1.29	9.84	123.19
53	2.65	94.13	1.33	1.33	9.92	123.41
54	2.70	95.28	1.34	1.34	9.85	123.49
55	2.75	96.16	1.33	1.33	9.67	123.49
56	2.80	97.09	1.31	1.31	9.46	123.43
57	2.85	97.81	1.30	1.30	9.27	123.35
58	2.90	98.36	1.28	1.28	9.09	123.27
59	2.95	98.74	1.26	1.26	8.96	123.18
60	3.00	98.69	1.25	1.25	8.89	123.10
61	3.05	98.31	1.24	1.24	8.89	123.02
62	3.10	97.40	1.23	1.23	8.94	122.93
63	3.15	96.27	1.21	1.21	9.04	122.78
64	3.20	93.65	1.18	1.18	9.20	122.56
65	3.25	91.01	1.15	1.15	9.44	122.22
66	3.30	86.75	1.09	1.09	9.72	121.84
67	3.35	83.29	1.05	1.05	10.05	121.39
68	3.40	79.32	1.00	1.00	10.40	120.94
69	3.45	75.50	0.95	0.95	10.77	120.47
70	3.50	72.09	0.91	0.91	11.15	120.00
71	3.55	68.64	0.87	0.87	11.52	119.56
72	3.60	65.87	0.83	0.83	11.91	119.09
73	3.65	62.43	0.79	0.79	12.33	118.61
74	3.70	59.25	0.75	0.75	12.85	118.12
75	3.75	55.87	0.72	0.72	13.42	117.70
76	3.80	53.31	0.70	0.70	14.09	117.43
77	3.85	51.22	0.70	0.70	14.77	117.22
78	3.90	48.90	0.69	0.69	15.42	117.06
79	3.95	47.23	0.68	0.68	15.99	116.80
80	4.00	45.38	0.66	0.66	16.42	116.52
81	4.05	44.01	0.64	0.64	16.78	116.21
82	4.10	42.79	0.62	0.62	17.05	115.96
83	4.15	42.03	0.61	0.61	17.21	115.75
84	4.20	41.69	0.60	0.60	17.22	115.60
85	4.25	41.69	0.59	0.59	17.08	115.43
86	4.30	41.69	0.57	0.57	16.86	115.24
87	4.35	41.69	0.55	0.55	16.60	115.02
88	4.40	41.69	0.54	0.54	16.46	114.90
89	4.45	41.69	0.54	0.54	16.46	114.90
90	4.50	41.69	0.55	0.55	16.72	115.09
91	4.55	41.51	0.58	0.58	17.11	115.33
92	4.60	41.14	0.60	0.60	17.67	115.57
93	4.65	40.22	0.62	0.62	18.28	115.71
94	4.70	39.19	0.63	0.63	19.01	115.75
95	4.75	37.70	0.63	0.63	19.83	115.77
96	4.80	36.46	0.64	0.64	20.75	115.75

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
97	4.85	34.91	0.64	0.64	21.68	115.72
98	4.90	33.65	0.65	0.65	22.56	115.58
99	4.95	32.20	0.63	0.63	23.38	115.38
100	5.00	30.82	0.62	0.62	24.26	115.17
101	5.05	29.53	0.62	0.62	25.28	114.98
102	5.10	28.00	0.61	0.61	26.50	114.90
103	5.15	26.77	0.63	0.63	27.87	114.79
104	5.20	25.24	0.62	0.62	29.40	114.75
105	5.25	23.95	0.63	0.63	31.00	114.64
106	5.30	22.59	0.63	0.63	32.62	114.56
107	5.35	21.49	0.64	0.64	34.10	114.45
108	5.40	20.65	0.64	0.64	35.39	114.35
109	5.45	19.88	0.63	0.63	36.41	114.20
110	5.50	19.26	0.62	0.62	37.21	113.94
111	5.55	18.51	0.59	0.59	37.67	113.61
112	5.60	18.15	0.57	0.57	37.90	113.23
113	5.65	17.78	0.55	0.55	38.09	112.80
114	5.70	17.02	0.51	0.51	38.59	112.37
115	5.75	16.27	0.49	0.49	39.57	111.86
116	5.80	15.11	0.47	0.47	40.88	111.45
117	5.85	14.40	0.46	0.46	42.38	111.08
118	5.90	13.70	0.45	0.45	43.73	110.93
119	5.95	13.34	0.46	0.46	44.87	110.86
120	6.00	13.10	0.46	0.46	45.65	110.93
121	6.05	13.10	0.47	0.47	46.11	111.02
122	6.10	13.10	0.48	0.48	46.36	111.13
123	6.15	13.10	0.48	0.48	46.55	111.22
124	6.20	13.10	0.49	0.49	46.79	111.32
125	6.25	13.10	0.50	0.50	47.11	111.46
126	6.30	13.10	0.51	0.51	47.68	111.60
127	6.35	12.87	0.52	0.52	48.71	111.56
128	6.40	12.10	0.50	0.50	50.19	111.36
129	6.45	11.47	0.49	0.49	51.95	110.96
130	6.50	10.74	0.47	0.47	53.19	110.70
131	6.55	10.72	0.47	0.47	53.79	110.50
132	6.60	10.72	0.47	0.47	53.73	110.46
133	6.65	10.72	0.46	0.46	53.54	110.37
134	6.70	10.72	0.45	0.45	53.35	110.29
135	6.75	10.72	0.45	0.45	53.21	110.23
136	6.80	10.72	0.45	0.45	53.13	110.19
137	6.85	10.72	0.45	0.45	53.08	110.17
138	6.90	10.72	0.45	0.45	52.96	110.11
139	6.95	10.72	0.44	0.44	52.78	110.03
140	7.00	10.72	0.43	0.43	52.50	109.91
141	7.05	10.72	0.42	0.42	52.22	109.79
142	7.10	10.72	0.42	0.42	51.90	109.64
143	7.15	10.72	0.41	0.41	51.57	109.50
144	7.20	10.72	0.40	0.40	51.21	109.34

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
145	7.25	10.72	0.39	0.39	51.02	109.25
146	7.30	10.72	0.39	0.39	51.03	109.25
147	7.35	10.72	0.40	0.40	51.46	109.43
148	7.40	10.72	0.42	0.42	52.10	109.70
149	7.45	10.72	0.44	0.44	52.98	110.07
150	7.50	10.72	0.46	0.46	53.72	110.47
151	7.55	10.87	0.49	0.49	53.90	111.08
152	7.60	11.65	0.55	0.55	53.38	111.82
153	7.65	12.44	0.60	0.60	52.15	112.71
154	7.70	13.57	0.66	0.66	50.82	113.41
155	7.75	14.27	0.68	0.68	49.51	113.98
156	7.80	14.94	0.71	0.71	48.37	114.39
157	7.85	15.69	0.74	0.74	47.26	114.73
158	7.90	16.31	0.75	0.75	46.06	115.02
159	7.95	17.08	0.77	0.77	44.58	115.18
160	8.00	17.93	0.76	0.76	42.72	115.28
161	8.05	19.02	0.75	0.75	40.15	115.27
162	8.10	20.72	0.72	0.72	37.16	115.18
163	8.15	22.44	0.67	0.67	33.46	114.98
164	8.20	25.12	0.62	0.62	29.90	114.74
165	8.25	27.59	0.59	0.59	26.45	114.65
166	8.30	31.03	0.58	0.58	23.75	114.68
167	8.35	33.67	0.57	0.57	21.57	114.84
168	8.40	36.38	0.58	0.58	20.01	114.90
169	8.45	37.83	0.56	0.56	19.01	115.02
170	8.50	38.90	0.57	0.57	18.46	115.11
171	8.55	39.68	0.58	0.58	18.26	115.35
172	8.60	40.30	0.60	0.60	18.16	115.60
173	8.65	41.04	0.62	0.62	18.09	115.81
174	8.70	41.40	0.63	0.63	17.97	115.92
175	8.75	41.69	0.63	0.63	17.82	115.90
176	8.80	41.69	0.61	0.61	17.64	115.77
177	8.85	41.56	0.60	0.60	17.48	115.56
178	8.90	41.17	0.58	0.58	17.44	115.29
179	8.95	40.14	0.56	0.56	17.61	114.99
180	9.00	38.72	0.54	0.54	18.15	114.64
181	9.05	36.25	0.52	0.52	19.02	114.30
182	9.10	34.02	0.51	0.51	20.25	113.93
183	9.15	31.32	0.50	0.50	21.68	113.67
184	9.20	29.34	0.50	0.50	23.32	113.39
185	9.25	27.07	0.49	0.49	25.09	113.21
186	9.30	25.10	0.50	0.50	26.97	112.94
187	9.35	23.13	0.49	0.49	28.92	112.74
188	9.40	21.64	0.49	0.49	30.68	112.57
189	9.45	20.74	0.49	0.49	32.12	112.58
190	9.50	20.35	0.51	0.51	33.22	112.72
191	9.55	20.03	0.53	0.53	34.22	112.93
192	9.60	19.67	0.55	0.55	35.42	113.25

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
193	9.65	19.33	0.59	0.59	36.65	113.59
194	9.70	19.06	0.62	0.62	37.86	114.01
195	9.75	19.06	0.66	0.66	37.96	114.26
196	9.80	19.97	0.65	0.65	36.62	114.57
197	9.85	22.27	0.67	0.67	34.01	114.70
198	9.90	24.20	0.64	0.64	31.29	114.87
199	9.95	26.24	0.64	0.64	29.13	114.86
200	10.00	27.33	0.62	0.62	27.31	114.78
201	10.05	28.63	0.59	0.59	25.24	114.58
202	10.10	31.35	0.55	0.55	22.90	114.23
203	10.15	33.32	0.50	0.50	20.71	113.84
204	10.20	35.56	0.46	0.46	18.94	113.35
205	10.25	36.96	0.43	0.43	17.61	112.98
206	10.30	38.16	0.41	0.41	16.81	112.71
207	10.35	38.54	0.41	0.41	16.53	112.68
208	10.40	38.45	0.42	0.42	16.68	112.72
209	10.45	37.68	0.42	0.42	17.10	112.82
210	10.50	36.81	0.43	0.43	17.62	112.83
211	10.55	35.74	0.43	0.43	18.13	112.81
212	10.60	35.04	0.43	0.43	18.59	112.80
213	10.65	34.55	0.44	0.44	18.96	112.89
214	10.70	34.55	0.45	0.45	19.27	113.03
215	10.75	34.37	0.46	0.46	19.54	113.15
216	10.80	34.00	0.46	0.46	19.76	113.16
217	10.85	33.67	0.46	0.46	19.94	113.10
218	10.90	33.38	0.45	0.45	19.99	113.08
219	10.95	33.75	0.46	0.46	19.96	113.12
220	11.00	34.06	0.46	0.46	19.86	113.22
221	11.05	34.45	0.47	0.47	19.79	113.29
222	11.10	34.55	0.47	0.47	19.76	113.34
223	11.15	34.55	0.47	0.47	19.77	113.35
224	11.20	34.55	0.47	0.47	19.80	113.34
225	11.25	34.44	0.47	0.47	19.92	113.26
226	11.30	33.67	0.46	0.46	20.14	113.15
227	11.35	33.06	0.45	0.45	20.51	113.03
228	11.40	32.29	0.45	0.45	20.89	113.04
229	11.45	32.16	0.46	0.46	21.25	113.14
230	11.50	32.14	0.48	0.48	21.66	113.28
231	11.55	31.42	0.49	0.49	22.24	113.43
232	11.60	30.70	0.50	0.50	23.13	113.58
233	11.65	29.54	0.52	0.52	24.33	113.88
234	11.70	28.61	0.57	0.57	25.84	114.25
235	11.75	27.49	0.61	0.61	27.67	114.74
236	11.80	26.19	0.66	0.66	29.60	115.11
237	11.85	24.90	0.69	0.69	31.58	115.42
238	11.90	23.77	0.72	0.72	33.17	115.56
239	11.95	23.10	0.73	0.73	34.38	115.66
240	12.00	22.71	0.74	0.74	34.74	115.61

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
241	12.05	22.87	0.72	0.72	34.49	115.49
242	12.10	23.23	0.70	0.70	33.43	115.28
243	12.15	24.27	0.66	0.66	32.07	115.09
244	12.20	25.30	0.64	0.64	30.35	114.92
245	12.25	26.84	0.62	0.62	28.76	114.76
246	12.30	27.90	0.59	0.59	27.21	114.58
247	12.35	29.04	0.57	0.57	26.20	114.45
248	12.40	29.46	0.57	0.57	25.65	114.44
249	12.45	29.74	0.58	0.58	25.96	114.63
250	12.50	29.00	0.61	0.61	26.82	114.93
251	12.55	28.16	0.65	0.65	28.37	115.26
252	12.60	26.61	0.69	0.69	30.26	115.52
253	12.65	24.94	0.72	0.72	32.61	115.61
254	12.70	22.74	0.73	0.73	35.45	115.59
255	12.75	20.36	0.75	0.75	38.69	115.40
256	12.80	18.25	0.74	0.74	42.23	115.26
257	12.85	16.73	0.76	0.76	45.46	115.16
258	12.90	15.93	0.78	0.78	48.13	115.29
259	12.95	15.55	0.82	0.82	49.73	115.47
260	13.00	15.49	0.84	0.84	50.61	115.65
261	13.05	15.49	0.85	0.85	50.37	115.67
262	13.10	15.85	0.82	0.82	49.54	115.56
263	13.15	16.08	0.79	0.79	48.19	115.23
264	13.20	16.08	0.73	0.73	47.29	114.64
265	13.25	15.33	0.65	0.65	47.11	113.65
266	13.30	13.83	0.55	0.55	48.03	112.48
267	13.35	12.50	0.49	0.49	49.82	111.27
268	13.40	11.28	0.44	0.44	51.98	110.60
269	13.45	10.90	0.46	0.46	53.59	110.39
270	13.50	10.97	0.47	0.47	53.74	110.72
271	13.55	11.75	0.50	0.50	52.68	111.12
272	13.60	12.38	0.52	0.52	51.06	111.58
273	13.65	13.09	0.53	0.53	50.28	111.93
274	13.70	13.10	0.56	0.56	50.24	112.25
275	13.75	13.10	0.58	0.58	50.93	112.55
276	13.80	13.10	0.60	0.60	51.58	112.81
277	13.85	13.10	0.62	0.62	52.22	113.07
278	13.90	13.10	0.64	0.64	52.66	113.24
279	13.95	13.10	0.65	0.65	52.96	113.37
280	14.00	13.15	0.65	0.65	52.71	113.62
281	14.05	13.88	0.69	0.69	52.19	114.02
282	14.10	14.51	0.74	0.74	51.48	114.64
283	14.15	15.28	0.80	0.80	51.13	115.14
284	14.20	15.49	0.82	0.82	51.08	115.49
285	14.25	15.49	0.84	0.84	51.25	115.63
286	14.30	15.49	0.84	0.84	51.47	115.71
287	14.35	15.49	0.85	0.85	51.73	115.80
288	14.40	15.49	0.87	0.87	52.02	115.90

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
289	14.45	15.49	0.88	0.88	52.30	116.00
290	14.50	15.49	0.88	0.88	52.25	116.06
291	14.55	15.74	0.89	0.89	51.86	116.11
292	14.60	16.10	0.89	0.89	50.82	116.17
293	14.65	16.81	0.88	0.88	49.51	116.19
294	14.70	17.36	0.86	0.86	47.93	116.07
295	14.75	17.75	0.82	0.82	46.63	115.84
296	14.80	17.87	0.78	0.78	45.50	115.49
297	14.85	17.87	0.74	0.74	45.07	115.10
298	14.90	17.27	0.70	0.70	45.15	114.67
299	14.95	16.61	0.67	0.67	45.95	114.28
300	15.00	15.86	0.66	0.66	46.99	113.95
301	15.05	15.24	0.64	0.64	48.33	113.68
302	15.10	14.46	0.63	0.63	49.69	113.40
303	15.15	13.83	0.61	0.61	51.20	113.10
304	15.20	13.12	0.60	0.60	52.38	112.95
305	15.25	13.10	0.61	0.61	53.22	112.94
306	15.30	13.10	0.62	0.62	53.58	113.07
307	15.35	13.10	0.63	0.63	53.82	113.15
308	15.40	13.10	0.63	0.63	53.93	113.18
309	15.45	13.10	0.63	0.63	53.92	113.15
310	15.50	13.10	0.62	0.62	53.83	113.10
311	15.55	13.10	0.62	0.62	53.74	113.04
312	15.60	13.10	0.62	0.62	53.76	113.03
313	15.65	13.10	0.62	0.62	54.02	113.12
314	15.70	13.10	0.64	0.64	54.11	113.44
315	15.75	13.72	0.69	0.69	53.72	114.07
316	15.80	14.83	0.77	0.77	51.83	115.00
317	15.85	17.13	0.85	0.85	49.12	116.00
318	15.90	19.41	0.93	0.93	45.59	116.84
319	15.95	22.07	0.95	0.95	42.37	117.38
320	16.00	24.09	0.96	0.96	39.16	117.64
321	16.05	26.39	0.93	0.93	36.82	117.76
322	16.10	27.56	0.93	0.93	35.08	117.84
323	16.15	28.58	0.93	0.93	34.85	118.02
324	16.20	27.86	0.98	0.98	35.50	118.23
325	16.25	26.98	1.02	1.02	37.32	118.38
326	16.30	25.04	1.04	1.04	39.25	118.37
327	16.35	23.68	1.03	1.03	41.34	118.18
328	16.40	22.18	1.01	1.01	42.79	117.91
329	16.45	21.45	0.98	0.98	43.82	117.59
330	16.50	20.85	0.95	0.95	44.04	117.29
331	16.55	20.85	0.91	0.91	43.83	117.00
332	16.60	20.85	0.88	0.88	43.18	116.68
333	16.65	20.85	0.83	0.83	42.84	116.43
334	16.70	20.62	0.83	0.83	42.97	116.31
335	16.75	20.26	0.84	0.84	43.94	116.46
336	16.80	19.91	0.90	0.90	45.35	116.74

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
337	16.85	19.46	0.94	0.94	47.30	116.99
338	16.90	18.31	0.96	0.96	49.22	117.14
339	16.95	17.87	0.99	0.99	50.95	117.33
340	17.00	17.87	1.05	1.05	50.92	117.87
341	17.05	20.05	1.16	1.16	49.31	118.73
342	17.10	22.85	1.29	1.29	45.77	119.77
343	17.15	27.25	1.39	1.39	41.96	120.62
344	17.20	31.00	1.43	1.43	37.79	121.21
345	17.25	35.65	1.42	1.42	34.25	121.43
346	17.30	38.77	1.36	1.36	30.83	121.32
347	17.35	42.09	1.23	1.23	28.22	120.87
348	17.40	42.92	1.10	1.10	26.01	120.14
349	17.45	43.34	0.97	0.97	24.74	119.31
350	17.50	42.20	0.88	0.88	24.04	118.54
351	17.55	40.99	0.82	0.82	24.11	117.94
352	17.60	39.06	0.78	0.78	24.65	117.49
353	17.65	36.97	0.77	0.77	25.72	117.14
354	17.70	34.50	0.75	0.75	27.50	116.83
355	17.75	30.68	0.75	0.75	29.89	116.54
356	17.80	27.72	0.75	0.75	33.02	116.47
357	17.85	25.47	0.81	0.81	36.10	116.64
358	17.90	24.13	0.87	0.87	39.28	117.08
359	17.95	22.88	0.95	0.95	42.21	117.46
360	18.00	21.52	1.00	1.00	45.25	117.79
361	18.05	20.28	1.06	1.06	47.67	118.20
362	18.10	20.66	1.16	1.16	48.99	118.87
363	18.15	21.92	1.30	1.30	48.29	119.97
364	18.20	25.41	1.52	1.52	46.71	120.94
365	18.25	27.34	1.59	1.59	44.58	121.63
366	18.30	29.14	1.59	1.59	42.36	121.90
367	18.35	31.56	1.58	1.58	39.64	122.06
368	18.40	34.82	1.57	1.57	35.64	122.57
369	18.45	43.65	1.70	1.70	31.45	123.16
370	18.50	50.71	1.71	1.71	27.08	123.68
371	18.55	59.41	1.64	1.64	23.83	123.68
372	18.60	62.81	1.51	1.51	21.21	123.31
373	18.65	65.16	1.35	1.35	20.42	122.78
374	18.70	59.74	1.32	1.32	20.90	122.31
375	18.75	54.39	1.31	1.31	23.49	122.07
376	18.80	45.86	1.37	1.37	26.79	121.90
377	18.85	40.54	1.40	1.40	30.93	121.72
378	18.90	35.18	1.41	1.41	34.51	121.57
379	18.95	32.48	1.45	1.45	37.92	121.50
380	19.00	30.21	1.50	1.50	40.48	121.53
381	19.05	28.89	1.52	1.52	42.71	121.44
382	19.10	26.97	1.49	1.49	44.90	120.92
383	19.15	23.31	1.31	1.31	47.56	119.97
384	19.20	20.17	1.15	1.15	51.07	118.56

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
385	19.25	16.67	0.97	0.97	54.00	117.45
386	19.30	16.32	0.95	0.95	55.93	116.74
387	19.35	16.24	0.94	0.94	55.43	116.66
388	19.40	17.01	0.93	0.93	54.16	116.65
389	19.45	17.63	0.92	0.92	52.22	116.62
390	19.50	18.39	0.89	0.89	50.63	116.45
391	19.55	18.46	0.84	0.84	49.24	116.10
392	19.60	18.40	0.78	0.78	48.55	115.52
393	19.65	17.66	0.71	0.71	48.08	114.87
394	19.70	17.25	0.66	0.66	47.90	114.31
395	19.75	17.17	0.64	0.64	47.24	114.39
396	19.80	18.72	0.72	0.72	46.29	115.34
397	19.85	21.25	0.88	0.88	44.96	116.68
398	19.90	23.41	1.00	1.00	43.79	117.89
399	19.95	25.02	1.09	1.09	42.57	118.18
400	20.00	24.62	0.96	0.96	41.67	117.70
401	20.05	23.26	0.81	0.81	41.00	116.46
402	20.10	21.60	0.68	0.68	41.21	115.17
403	20.15	19.79	0.61	0.61	42.32	114.06
404	20.20	17.97	0.56	0.56	44.37	113.20
405	20.25	16.28	0.53	0.53	46.94	112.52
406	20.30	14.87	0.51	0.51	49.31	112.20
407	20.35	14.63	0.53	0.53	50.83	112.34
408	20.40	15.09	0.58	0.58	51.57	112.92
409	20.45	15.46	0.63	0.63	52.12	113.52
410	20.50	15.49	0.67	0.67	52.91	114.03
411	20.55	15.53	0.71	0.71	53.50	114.44
412	20.60	15.91	0.75	0.75	53.44	114.98
413	20.65	16.90	0.81	0.81	51.94	115.76
414	20.70	19.21	0.90	0.90	49.52	116.69
415	20.75	21.61	0.98	0.98	46.39	117.61
416	20.80	24.43	1.05	1.05	43.58	118.30
417	20.85	26.56	1.08	1.08	41.14	118.73
418	20.90	28.15	1.08	1.08	39.40	118.89
419	20.95	28.92	1.06	1.06	38.33	118.80
420	21.00	28.65	1.02	1.02	38.25	118.61
421	21.05	27.52	1.00	1.00	39.16	118.40
422	21.10	25.95	1.00	1.00	41.06	118.30
423	21.15	24.28	1.03	1.03	43.51	118.18
424	21.20	22.41	1.02	1.02	46.06	118.13
425	21.25	21.44	1.05	1.05	47.80	118.08
426	21.30	21.44	1.06	1.06	48.74	118.00
427	21.35	20.78	1.01	1.01	49.07	117.61
428	21.40	19.69	0.91	0.91	50.03	116.76
429	21.45	17.48	0.79	0.79	51.57	115.61
430	21.50	15.60	0.69	0.69	53.86	114.51
431	21.55	14.45	0.65	0.65	56.09	113.67
432	21.60	13.53	0.61	0.61	58.17	112.94

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
433	21.65	12.38	0.55	0.55	60.16	112.10
434	21.70	11.41	0.50	0.50	62.17	111.04
435	21.75	10.40	0.43	0.43	63.93	110.08
436	21.80	9.86	0.40	0.40	65.29	109.26
437	21.85	9.53	0.38	0.38	66.12	108.91
438	21.90	9.53	0.39	0.39	66.34	108.95
439	21.95	9.83	0.41	0.41	66.00	109.44
440	22.00	10.38	0.45	0.45	65.33	110.09
441	22.05	10.84	0.49	0.49	64.75	110.83
442	22.10	11.27	0.53	0.53	64.38	111.51
443	22.15	11.71	0.57	0.57	63.95	112.23
444	22.20	12.34	0.63	0.63	62.83	113.09
445	22.25	13.56	0.70	0.70	61.23	113.97
446	22.30	14.61	0.76	0.76	59.20	114.81
447	22.35	15.79	0.82	0.82	56.36	115.77
448	22.40	18.45	0.93	0.93	52.98	116.74
449	22.45	20.86	1.01	1.01	49.12	117.73
450	22.50	23.95	1.07	1.07	45.81	118.31
451	22.55	25.72	1.06	1.06	42.76	118.52
452	22.60	27.23	1.00	1.00	40.41	118.33
453	22.65	27.97	0.94	0.94	38.38	117.95
454	22.70	28.53	0.88	0.88	37.28	117.50
455	22.75	27.79	0.83	0.83	36.87	117.04
456	22.80	26.94	0.79	0.79	37.63	116.69
457	22.85	25.39	0.79	0.79	39.06	116.41
458	22.90	23.70	0.78	0.78	41.37	116.14
459	22.95	21.52	0.76	0.76	44.03	115.71
460	23.00	19.45	0.72	0.72	47.04	115.18
461	23.05	17.63	0.69	0.69	49.97	114.57
462	23.10	16.10	0.66	0.66	52.76	114.04
463	23.15	15.02	0.64	0.64	55.53	113.55
464	23.20	13.88	0.61	0.61	57.90	113.25
465	23.25	13.44	0.62	0.62	60.02	113.12
466	23.30	13.10	0.63	0.63	61.48	113.26
467	23.35	13.10	0.66	0.66	62.79	113.62
468	23.40	13.20	0.71	0.71	63.64	114.16
469	23.45	13.58	0.78	0.78	63.98	114.85
470	23.50	14.29	0.85	0.85	63.25	115.61
471	23.55	15.40	0.93	0.93	61.63	116.37
472	23.60	16.72	0.99	0.99	59.33	116.97
473	23.65	17.91	1.01	1.01	57.26	117.26
474	23.70	18.29	0.99	0.99	55.65	117.15
475	23.75	18.20	0.92	0.92	54.85	116.65
476	23.80	17.43	0.83	0.83	54.44	115.93
477	23.85	16.79	0.75	0.75	54.35	115.07
478	23.90	16.08	0.68	0.68	54.59	114.18
479	23.95	15.02	0.60	0.60	55.05	113.20
480	24.00	14.14	0.53	0.53	55.76	112.21

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
481	24.05	13.37	0.48	0.48	56.07	111.36
482	24.10	13.10	0.45	0.45	56.48	110.96
483	24.15	13.10	0.47	0.47	56.65	111.18
484	24.20	13.67	0.52	0.52	57.22	112.08
485	24.25	14.42	0.62	0.62	57.01	113.51
486	24.30	16.28	0.77	0.77	56.63	115.18
487	24.35	17.94	0.93	0.93	55.20	116.82
488	24.40	20.27	1.09	1.09	53.62	118.21
489	24.45	22.36	1.23	1.23	51.19	119.26
490	24.50	24.92	1.31	1.31	48.38	120.15
491	24.55	28.24	1.41	1.41	45.23	120.85
492	24.60	31.36	1.47	1.47	42.27	121.53
493	24.65	34.81	1.55	1.55	39.82	121.97
494	24.70	36.94	1.55	1.55	37.86	122.27
495	24.75	38.78	1.55	1.55	36.30	122.35
496	24.80	40.19	1.52	1.52	34.83	122.32
497	24.85	41.70	1.47	1.47	33.30	122.27
498	24.90	44.02	1.46	1.46	31.56	122.17
499	24.95	46.24	1.39	1.39	29.65	122.14
500	25.00	49.61	1.37	1.37	27.74	122.01
501	25.05	51.98	1.31	1.31	25.96	121.91
502	25.10	54.59	1.26	1.26	24.60	121.66
503	25.15	55.10	1.20	1.20	23.61	121.39
504	25.20	55.43	1.14	1.14	23.04	121.13
505	25.25	55.81	1.13	1.13	22.69	121.01
506	25.30	56.31	1.13	1.13	22.48	121.05
507	25.35	57.28	1.15	1.15	22.31	121.15
508	25.40	57.95	1.16	1.16	22.19	121.30
509	25.45	58.66	1.19	1.19	22.02	121.48
510	25.50	60.18	1.22	1.22	21.75	121.66
511	25.55	61.67	1.23	1.23	21.26	121.83
512	25.60	63.98	1.24	1.24	20.58	121.93
513	25.65	66.38	1.23	1.23	19.76	122.08
514	25.70	69.87	1.25	1.25	18.98	122.24
515	25.75	72.46	1.26	1.26	18.31	122.46
516	25.80	75.09	1.29	1.29	17.77	122.72
517	25.85	78.43	1.34	1.34	17.35	123.07
518	25.90	81.26	1.40	1.40	17.00	123.51
519	25.95	84.86	1.48	1.48	16.93	123.79
520	26.00	83.19	1.47	1.47	17.07	123.72
521	26.05	78.81	1.37	1.37	17.41	123.32
522	26.10	76.00	1.30	1.30	17.64	122.80
523	26.15	74.13	1.24	1.24	17.63	122.56
524	26.20	76.04	1.27	1.27	17.57	122.51
525	26.25	76.16	1.28	1.28	17.65	122.59
526	26.30	74.43	1.28	1.28	17.97	122.58
527	26.35	72.86	1.28	1.28	18.48	122.55
528	26.40	71.12	1.29	1.29	19.06	122.54

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
529	26.45	69.18	1.30	1.30	19.83	122.64
530	26.50	67.53	1.37	1.37	20.74	122.81
531	26.55	65.60	1.42	1.42	21.82	123.05
532	26.60	63.73	1.48	1.48	23.02	123.27
533	26.65	61.25	1.54	1.54	24.37	123.44
534	26.70	58.32	1.58	1.58	25.97	123.59
535	26.75	55.40	1.66	1.66	27.69	123.70
536	26.80	52.58	1.70	1.70	29.59	123.86
537	26.85	49.97	1.77	1.77	31.56	123.86
538	26.90	46.20	1.76	1.76	33.68	123.78
539	26.95	42.98	1.76	1.76	35.96	123.50
540	27.00	39.29	1.71	1.71	38.11	123.21
541	27.05	37.08	1.68	1.68	40.00	122.93
542	27.10	35.49	1.67	1.67	41.21	122.81
543	27.15	35.23	1.69	1.69	41.91	122.77
544	27.20	35.08	1.69	1.69	42.14	122.78
545	27.25	34.96	1.68	1.68	42.29	122.72
546	27.30	34.57	1.65	1.65	42.44	122.62
547	27.35	34.18	1.64	1.64	42.55	122.60
548	27.40	34.67	1.67	1.67	42.62	122.71
549	27.45	35.09	1.72	1.72	42.60	122.93
550	27.50	35.60	1.77	1.77	42.74	123.13
551	27.55	35.52	1.80	1.80	43.03	123.25
552	27.60	35.16	1.81	1.81	43.65	123.21
553	27.65	33.84	1.77	1.77	44.43	123.08
554	27.70	32.92	1.75	1.75	44.85	123.06
555	27.75	34.06	1.81	1.81	44.64	123.20
556	27.80	35.25	1.85	1.85	43.68	123.49
557	27.85	37.07	1.89	1.89	42.41	123.72
558	27.90	38.91	1.90	1.90	40.76	123.88
559	27.95	41.04	1.88	1.88	38.72	124.11
560	28.00	45.10	1.94	1.94	36.51	124.26
561	28.05	47.74	1.89	1.89	34.72	124.28
562	28.10	48.12	1.80	1.80	33.61	123.90
563	28.15	46.63	1.64	1.64	33.57	123.33
564	28.20	43.45	1.54	1.54	34.38	122.62
565	28.25	39.78	1.44	1.44	36.14	121.98
566	28.30	36.17	1.37	1.37	38.22	121.35
567	28.35	33.20	1.31	1.31	40.25	120.89
568	28.40	31.71	1.29	1.29	41.63	120.66
569	28.45	31.56	1.31	1.31	42.48	120.67
570	28.50	31.27	1.33	1.33	43.10	120.77
571	28.55	30.88	1.35	1.35	43.79	120.84
572	28.60	30.41	1.37	1.37	44.41	120.88
573	28.65	30.18	1.37	1.37	44.65	120.95
574	28.70	30.76	1.40	1.40	44.56	120.97
575	28.75	30.75	1.37	1.37	44.29	120.85
576	28.80	30.24	1.31	1.31	44.82	120.20

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
577	28.85	26.57	1.11	1.11	46.41	118.94
578	28.90	22.16	0.88	0.88	49.63	116.93
579	28.95	17.49	0.66	0.66	53.54	114.60
580	29.00	14.68	0.52	0.52	56.89	112.55
581	29.05	13.90	0.46	0.46	58.28	111.15
582	29.10	13.49	0.42	0.42	58.27	110.30
583	29.15	13.12	0.38	0.38	57.72	109.60
584	29.20	13.10	0.36	0.36	57.08	109.09
585	29.25	13.10	0.34	0.34	56.48	108.80
586	29.30	13.10	0.34	0.34	56.44	108.76
587	29.35	13.10	0.35	0.35	56.86	108.93
588	29.40	13.10	0.37	0.37	57.67	109.28
589	29.45	13.10	0.39	0.39	58.59	109.66
590	29.50	13.12	0.41	0.41	58.99	110.23
591	29.55	13.84	0.46	0.46	58.91	110.92
592	29.60	14.47	0.50	0.50	58.21	111.71
593	29.65	15.24	0.54	0.54	57.32	112.48
594	29.70	16.23	0.59	0.59	55.86	113.32
595	29.75	17.73	0.66	0.66	54.20	114.17
596	29.80	19.06	0.71	0.71	52.32	114.86
597	29.85	20.25	0.73	0.73	51.04	115.18
598	29.90	20.25	0.72	0.72	50.49	115.07
599	29.95	19.51	0.68	0.68	51.56	114.45
600	30.00	17.18	0.60	0.60	52.61	113.99
601	30.05	17.83	0.62	0.62	52.45	113.96
602	30.10	19.63	0.67	0.67	49.47	114.87
603	30.15	23.44	0.77	0.77	46.00	115.89
604	30.20	26.21	0.83	0.83	43.70	116.61
605	30.25	26.21	0.83	0.83	43.04	116.91
606	30.30	25.88	0.84	0.84	43.88	117.02
607	30.35	25.12	0.88	0.88	45.43	117.37
608	30.40	24.81	0.97	0.97	47.50	118.00
609	30.45	24.79	1.10	1.10	48.48	119.36
610	30.50	28.91	1.43	1.43	48.25	121.15
611	30.55	33.14	1.79	1.79	46.13	123.25
612	30.60	40.25	2.23	2.23	43.50	124.97
613	30.65	46.61	2.52	2.52	40.09	126.34
614	30.70	54.51	2.72	2.72	36.89	127.02
615	30.75	58.83	2.62	2.62	33.94	127.25
616	30.80	62.66	2.51	2.51	31.46	127.13
617	30.85	66.39	2.43	2.43	29.31	127.03
618	30.90	70.51	2.37	2.37	27.29	127.13
619	30.95	77.25	2.44	2.44	25.41	127.29
620	31.00	82.60	2.41	2.41	23.62	127.49
621	31.05	88.38	2.39	2.39	21.93	127.55
622	31.10	94.04	2.34	2.34	20.46	127.59
623	31.15	98.69	2.31	2.31	19.28	127.67
624	31.20	103.34	2.35	2.35	18.54	127.95

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
625	31.25	108.29	2.49	2.49	18.06	128.48
626	31.30	115.33	2.72	2.72	17.74	129.25
627	31.35	123.56	3.02	3.02	17.38	130.09
628	31.40	132.15	3.29	3.29	16.94	130.94
629	31.45	142.74	3.59	3.59	16.38	131.64
630	31.50	152.00	3.78	3.78	15.70	132.32
631	31.55	164.56	4.04	4.04	15.03	132.84
632	31.60	172.85	4.17	4.17	14.42	133.30
633	31.65	181.49	4.31	4.31	13.93	133.58
634	31.70	186.78	4.36	4.36	13.52	133.78
635	31.75	191.24	4.38	4.38	13.19	133.90
636	31.80	195.01	4.41	4.41	12.93	134.00
637	31.85	198.22	4.45	4.45	12.72	134.12
638	31.90	202.41	4.52	4.52	12.53	134.26
639	31.95	206.31	4.58	4.58	12.36	134.42
640	32.00	210.25	4.66	4.66	12.26	134.52
641	32.05	210.25	4.67	4.67	12.27	134.60
642	32.10	209.54	4.71	4.71	12.40	134.62
643	32.15	206.82	4.72	4.72	12.64	134.66
644	32.20	204.44	4.79	4.79	12.96	134.70
645	32.25	201.49	4.85	4.85	13.34	134.80
646	32.30	199.41	4.97	4.97	13.68	134.88
647	32.35	197.74	5.01	5.01	13.94	134.97
648	32.40	197.74	5.07	5.07	13.99	134.99
649	32.45	199.01	5.01	5.01	13.84	134.99
650	32.50	202.48	4.98	4.98	13.47	134.92
651	32.55	206.10	4.85	4.85	13.01	134.85
652	32.60	210.31	4.77	4.77	12.48	134.74
653	32.65	214.96	4.67	4.67	12.00	134.65
654	32.70	218.74	4.60	4.60	11.58	134.58
655	32.75	222.22	4.55	4.55	11.29	134.52
656	32.80	222.80	4.50	4.50	11.14	134.46
657	32.85	221.68	4.46	4.46	11.15	134.40
658	32.90	219.51	4.45	4.45	11.25	134.35
659	32.95	217.27	4.44	4.44	11.37	134.31
660	33.00	215.77	4.43	4.43	11.45	134.24
661	33.05	214.29	4.37	4.37	11.49	134.14
662	33.10	211.97	4.30	4.30	11.52	133.98
663	33.15	208.73	4.20	4.20	11.60	133.80
664	33.20	204.40	4.12	4.12	11.78	133.58
665	33.25	197.51	4.01	4.01	12.08	133.35
666	33.30	190.65	3.94	3.94	12.54	133.06
667	33.35	180.28	3.81	3.81	13.13	132.82
668	33.40	173.09	3.81	3.81	13.80	132.59
669	33.45	165.46	3.75	3.75	14.45	132.47
670	33.50	160.87	3.77	3.77	14.96	132.30
671	33.55	156.56	3.68	3.68	15.25	132.15
672	33.60	154.73	3.61	3.61	15.28	131.93

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
673	33.65	154.17	3.49	3.49	15.08	131.76
674	33.70	156.11	3.43	3.43	14.68	131.55
675	33.75	157.34	3.29	3.29	14.23	131.35
676	33.80	158.61	3.18	3.18	13.71	131.09
677	33.85	160.27	3.05	3.05	13.25	130.86
678	33.90	161.65	2.97	2.97	12.84	130.61
679	33.95	161.48	2.86	2.86	12.60	130.39
680	34.00	159.88	2.79	2.79	12.54	130.13
681	34.05	155.64	2.71	2.71	12.73	129.96
682	34.10	152.39	2.72	2.72	13.08	129.85
683	34.15	148.87	2.73	2.73	13.56	129.86
684	34.20	145.66	2.78	2.78	14.03	129.89
685	34.25	143.14	2.81	2.81	14.48	129.94
686	34.30	141.21	2.84	2.84	14.82	130.02
687	34.35	140.93	2.90	2.90	15.05	130.13
688	34.40	141.68	2.95	2.95	15.15	130.27
689	34.45	142.92	3.00	3.00	15.19	130.42
690	34.50	144.29	3.06	3.06	15.20	130.60
691	34.55	146.16	3.14	3.14	15.23	130.80
692	34.60	147.94	3.22	3.22	15.22	131.02
693	34.65	150.65	3.30	3.30	15.13	131.21
694	34.70	153.30	3.34	3.34	14.93	131.36
695	34.75	156.56	3.37	3.37	14.64	131.47
696	34.80	160.35	3.38	3.38	14.29	131.56
697	34.85	163.76	3.39	3.39	13.94	131.63
698	34.90	167.21	3.40	3.40	13.69	131.71
699	34.95	168.56	3.42	3.42	13.58	131.77
700	35.00	168.56	3.44	3.44	13.68	131.83
701	35.05	166.95	3.49	3.49	13.90	131.88
702	35.10	164.91	3.52	3.52	14.22	131.94
703	35.15	163.08	3.57	3.57	14.53	132.00
704	35.20	161.81	3.61	3.61	14.81	132.07
705	35.25	161.03	3.65	3.65	14.99	132.13
706	35.30	160.81	3.67	3.67	15.10	132.17
707	35.35	160.81	3.68	3.68	15.13	132.20
708	35.40	161.44	3.69	3.69	15.12	132.23
709	35.45	162.14	3.71	3.71	15.09	132.28
710	35.50	163.28	3.73	3.73	15.05	132.34
711	35.55	164.20	3.76	3.76	15.00	132.40
712	35.60	165.36	3.78	3.78	14.92	132.45
713	35.65	166.80	3.79	3.79	14.80	132.49
714	35.70	168.57	3.79	3.79	14.62	132.54
715	35.75	171.06	3.80	3.80	14.43	132.59
716	35.80	173.20	3.82	3.82	14.24	132.66
717	35.85	175.52	3.85	3.85	14.10	132.72
718	35.90	177.01	3.86	3.86	13.97	132.78
719	35.95	178.52	3.87	3.87	13.89	132.81
720	36.00	178.68	3.88	3.88	13.88	132.84

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
721	36.05	178.51	3.89	3.89	13.95	132.82
722	36.10	176.27	3.87	3.87	14.09	132.77
723	36.15	173.83	3.83	3.83	14.30	132.65
724	36.20	169.57	3.77	3.77	14.56	132.52
725	36.25	165.90	3.73	3.73	14.87	132.35
726	36.30	161.54	3.67	3.67	15.18	132.19
727	36.35	158.06	3.61	3.61	15.44	131.98
728	36.40	154.18	3.51	3.51	15.74	131.66
729	36.45	146.13	3.31	3.31	16.05	131.18
730	36.50	138.82	3.09	3.09	16.48	130.49
731	36.55	128.72	2.81	2.81	16.75	129.85
732	36.60	126.07	2.68	2.68	16.88	129.33
733	36.65	124.83	2.59	2.59	16.59	129.15
734	36.70	129.68	2.61	2.61	16.24	129.19
735	36.75	133.03	2.67	2.67	15.90	129.36
736	36.80	134.88	2.71	2.71	16.04	129.50
737	36.85	130.66	2.76	2.76	16.69	129.49
738	36.90	121.79	2.73	2.73	18.19	129.38
739	36.95	109.14	2.78	2.78	20.33	129.14
740	37.00	96.56	2.75	2.75	23.25	128.80
741	37.05	82.92	2.70	2.70	26.54	128.34
742	37.10	71.96	2.64	2.64	30.46	127.61
743	37.15	58.55	2.39	2.39	34.64	126.84
744	37.20	50.87	2.32	2.32	39.07	125.87
745	37.25	43.47	2.11	2.11	42.75	125.10
746	37.30	39.57	1.99	1.99	45.63	124.20
747	37.35	36.23	1.80	1.80	47.64	123.28
748	37.40	32.76	1.58	1.58	48.93	122.23
749	37.45	30.86	1.41	1.41	49.73	121.20
750	37.50	29.35	1.27	1.27	49.89	120.31
751	37.55	28.32	1.15	1.15	49.93	119.51
752	37.60	27.29	1.06	1.06	50.03	118.70
753	37.65	25.80	0.95	0.95	49.84	118.20
754	37.70	26.71	0.96	0.96	47.90	118.61
755	37.75	32.44	1.16	1.16	45.74	119.96
756	37.80	36.33	1.43	1.43	43.87	121.72
757	37.85	40.48	1.73	1.73	44.11	123.05
758	37.90	39.91	1.91	1.91	44.62	123.92
759	37.95	40.56	2.00	2.00	44.13	124.86
760	38.00	48.45	2.38	2.38	41.19	125.83
761	38.05	56.92	2.51	2.51	36.54	127.00
762	38.10	70.06	2.71	2.71	31.58	127.55
763	38.15	80.78	2.52	2.52	26.94	127.80
764	38.20	92.06	2.38	2.38	22.78	127.47
765	38.25	101.52	2.09	2.09	19.62	127.07
766	38.30	108.15	1.94	1.94	17.22	126.48
767	38.35	112.03	1.76	1.76	15.91	126.05
768	38.40	112.18	1.69	1.69	15.26	125.63

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
769	38.45	110.32	1.63	1.63	15.34	125.46
770	38.50	107.72	1.66	1.66	15.75	125.39
771	38.55	105.09	1.69	1.69	16.48	125.50
772	38.60	102.06	1.75	1.75	17.30	125.65
773	38.65	99.59	1.81	1.81	18.25	125.83
774	38.70	96.51	1.87	1.87	19.04	126.02
775	38.75	95.89	1.93	1.93	19.60	126.18
776	38.80	95.89	1.96	1.96	19.67	126.29
777	38.85	97.66	1.95	1.95	19.41	126.31
778	38.90	99.32	1.93	1.93	18.86	126.26
779	38.95	101.64	1.88	1.88	18.32	126.20
780	39.00	103.32	1.87	1.87	17.83	126.18
781	39.05	105.21	1.87	1.87	17.72	126.25
782	39.10	104.28	1.92	1.92	17.94	126.37
783	39.15	102.78	1.97	1.97	18.68	126.54
784	39.20	99.07	2.05	2.05	19.69	126.74
785	39.25	95.81	2.14	2.14	21.05	126.96
786	39.30	91.42	2.24	2.24	22.65	127.18
787	39.35	86.40	2.34	2.34	24.56	127.28
788	39.40	79.80	2.37	2.37	26.74	127.35
789	39.45	74.71	2.46	2.46	28.93	127.33
790	39.50	70.30	2.49	2.49	31.01	127.38
791	39.55	66.90	2.56	2.56	32.63	127.33
792	39.60	64.56	2.53	2.53	33.89	127.21
793	39.65	62.15	2.48	2.48	34.21	126.98
794	39.70	62.82	2.38	2.38	33.87	126.77
795	39.75	64.20	2.33	2.33	32.93	126.64
796	39.80	65.76	2.30	2.30	32.07	126.60
797	39.85	67.26	2.29	2.29	31.24	126.65
798	39.90	69.59	2.31	2.31	29.94	126.57
799	39.95	72.81	2.15	2.15	27.97	126.35
800	40.00	77.65	1.99	1.99	25.71	125.85
801	40.05	79.56	1.80	1.80	23.92	125.38
802	40.10	80.88	1.72	1.72	23.20	125.08
803	40.15	79.75	1.75	1.75	23.30	125.07
804	40.20	78.69	1.79	1.79	23.96	125.19
805	40.25	77.15	1.83	1.83	24.66	125.31
806	40.30	75.88	1.88	1.88	25.38	125.41
807	40.35	74.46	1.90	1.90	25.96	125.44
808	40.40	73.40	1.89	1.89	26.33	125.37
809	40.45	72.44	1.85	1.85	26.42	125.15
810	40.50	71.29	1.76	1.76	26.32	124.83
811	40.55	70.36	1.68	1.68	26.14	124.44
812	40.60	69.22	1.60	1.60	26.33	124.20
813	40.65	67.32	1.62	1.62	26.97	124.10
814	40.70	65.17	1.66	1.66	28.40	124.26
815	40.75	62.21	1.77	1.77	30.13	124.48
816	40.80	59.64	1.84	1.84	32.27	124.70

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
817	40.85	56.25	1.91	1.91	34.07	124.80
818	40.90	54.53	1.93	1.93	35.56	124.81
819	40.95	53.07	1.93	1.93	35.79	124.84
820	41.00	55.63	1.95	1.95	35.05	124.94
821	41.05	58.75	1.95	1.95	32.86	125.14
822	41.10	65.48	1.95	1.95	30.34	125.31
823	41.15	71.00	1.92	1.92	27.48	125.43
824	41.20	77.99	1.87	1.87	25.03	125.48
825	41.25	83.90	1.83	1.83	22.80	125.53
826	41.30	90.29	1.81	1.81	20.82	125.57
827	41.35	97.44	1.76	1.76	19.06	125.58
828	41.40	103.25	1.72	1.72	17.44	125.53
829	41.45	109.26	1.66	1.66	16.18	125.44
830	41.50	113.00	1.62	1.62	15.13	125.33
831	41.55	116.73	1.58	1.58	14.55	125.18
832	41.60	115.67	1.53	1.53	14.30	124.99
833	41.65	113.62	1.50	1.50	14.63	124.71
834	41.70	106.46	1.45	1.45	15.38	124.44
835	41.75	99.85	1.44	1.44	16.74	124.13
836	41.80	90.26	1.42	1.42	18.66	124.04
837	41.85	82.70	1.52	1.52	21.22	124.03
838	41.90	74.27	1.58	1.58	24.02	124.20
839	41.95	69.10	1.67	1.67	26.71	124.27
840	42.00	64.39	1.71	1.71	29.27	124.27
841	42.05	58.46	1.71	1.71	31.81	124.17
842	42.10	54.53	1.74	1.74	34.57	124.07
843	42.15	50.52	1.77	1.77	36.62	124.16
844	42.20	50.59	1.85	1.85	37.92	124.37
845	42.25	51.29	1.94	1.94	38.02	124.64
846	42.30	52.40	1.95	1.95	37.74	124.79
847	42.35	53.12	1.95	1.95	37.17	124.78
848	42.40	53.51	1.90	1.90	36.83	124.72
849	42.45	53.39	1.90	1.90	36.76	124.67
850	42.50	53.03	1.91	1.91	37.30	124.71
851	42.55	51.71	1.95	1.95	38.22	124.76
852	42.60	50.25	1.98	1.98	39.74	124.78
853	42.65	47.58	2.00	2.00	41.51	124.79
854	42.70	45.57	2.03	2.03	43.69	124.80
855	42.75	43.27	2.08	2.08	45.41	124.93
856	42.80	43.40	2.18	2.18	46.59	125.21
857	42.85	44.19	2.30	2.30	46.03	125.74
858	42.90	48.88	2.48	2.48	44.40	126.35
859	42.95	53.41	2.61	2.61	41.44	126.99
860	43.00	60.38	2.69	2.69	38.33	127.40
861	43.05	65.96	2.67	2.67	34.89	127.62
862	43.10	72.69	2.58	2.58	31.93	127.56
863	43.15	76.58	2.42	2.42	29.30	127.29
864	43.20	79.81	2.25	2.25	27.44	126.82

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
865	43.25	79.81	2.06	2.06	26.26	126.36
866	43.30	79.43	1.98	1.98	25.91	126.03
867	43.35	78.27	1.98	1.98	26.18	126.08
868	43.40	78.49	2.11	2.11	26.87	126.45
869	43.45	79.21	2.29	2.29	27.88	126.95
870	43.50	77.48	2.44	2.44	29.09	127.37
871	43.55	75.54	2.55	2.55	30.68	127.61
872	43.60	71.69	2.62	2.62	32.21	127.79
873	43.65	70.11	2.71	2.71	33.62	127.99
874	43.70	69.73	2.85	2.85	34.03	128.41
875	43.75	74.52	3.07	3.07	33.60	129.02
876	43.80	80.44	3.31	3.31	32.12	129.61
877	43.85	87.45	3.37	3.37	30.38	130.03
878	43.90	93.33	3.39	3.39	28.31	130.23
879	43.95	100.55	3.33	3.33	26.24	130.40
880	44.00	109.39	3.36	3.36	23.95	130.61
881	44.05	121.50	3.39	3.39	21.80	130.95
882	44.10	133.73	3.48	3.48	19.84	131.30
883	44.15	145.26	3.53	3.53	18.11	131.61
884	44.20	157.84	3.53	3.53	16.61	131.82
885	44.25	167.43	3.51	3.51	15.22	131.94
886	44.30	178.57	3.47	3.47	14.20	132.12
887	44.35	187.35	3.59	3.59	13.46	132.42
888	44.40	196.70	3.76	3.76	13.05	132.82
889	44.45	203.90	3.90	3.90	12.75	133.18
890	44.50	209.59	4.01	4.01	12.53	133.46
891	44.55	214.62	4.11	4.11	12.36	133.68
892	44.60	217.90	4.17	4.17	12.22	133.85
893	44.65	221.27	4.23	4.23	12.13	133.97
894	44.70	222.76	4.26	4.26	12.06	134.06
895	44.75	223.91	4.29	4.29	12.04	134.10
896	44.80	223.54	4.28	4.28	12.05	134.10
897	44.85	222.85	4.27	4.27	12.09	134.06
898	44.90	221.31	4.24	4.24	12.14	134.00
899	44.95	219.81	4.21	4.21	12.20	133.93
900	45.00	218.02	4.17	4.17	12.26	133.86
901	45.05	216.62	4.15	4.15	12.32	133.80
902	45.10	215.34	4.12	4.12	12.38	133.73
903	45.15	213.80	4.09	4.09	12.44	133.67
904	45.20	212.24	4.06	4.06	12.52	133.58
905	45.25	209.95	4.02	4.02	12.60	133.49
906	45.30	208.00	3.98	3.98	12.69	133.40
907	45.35	206.00	3.94	3.94	12.79	133.33
908	45.40	204.53	3.94	3.94	12.90	133.29
909	45.45	203.39	3.95	3.95	13.02	133.28
910	45.50	202.22	3.95	3.95	13.10	133.28
911	45.55	202.33	3.95	3.95	13.11	133.27
912	45.60	203.06	3.94	3.94	13.04	133.27

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
913	45.65	204.07	3.93	3.93	12.95	133.26
914	45.70	204.99	3.92	3.92	12.88	133.27
915	45.75	205.75	3.94	3.94	12.83	133.29
916	45.80	206.51	3.94	3.94	12.77	133.30
917	45.85	207.67	3.93	3.93	12.65	133.27
918	45.90	208.12	3.87	3.87	12.46	133.16
919	45.95	208.46	3.75	3.75	12.17	132.94
920	46.00	208.46	3.59	3.59	11.82	132.65
921	46.05	208.29	3.42	3.42	11.39	132.25
922	46.10	207.52	3.20	3.20	10.94	131.82
923	46.15	207.09	3.02	3.02	10.43	131.32
924	46.20	206.71	2.79	2.79	9.97	130.90
925	46.25	208.16	2.69	2.69	9.51	130.54
926	46.30	209.99	2.60	2.60	9.16	130.38
927	46.35	213.74	2.58	2.58	8.85	130.30
928	46.40	216.96	2.57	2.57	8.56	130.30
929	46.45	221.22	2.55	2.55	8.28	130.28
930	46.50	224.45	2.52	2.52	7.95	130.22
931	46.55	228.05	2.46	2.46	7.63	130.10
932	46.60	230.85	2.40	2.40	7.29	129.95
933	46.65	233.34	2.34	2.34	7.01	129.79
934	46.70	234.67	2.28	2.28	6.77	129.61
935	46.75	234.67	2.22	2.22	6.54	129.37
936	46.80	234.67	2.11	2.11	6.30	129.07
937	46.85	234.67	2.02	2.02	6.03	128.73
938	46.90	234.67	1.92	1.92	5.76	128.38
939	46.95	234.28	1.83	1.83	5.51	127.97
940	47.00	231.86	1.72	1.72	5.32	127.54
941	47.05	227.98	1.63	1.63	5.27	127.14
942	47.10	222.05	1.58	1.58	5.44	126.86
943	47.15	213.33	1.58	1.58	5.82	126.70
944	47.20	204.34	1.58	1.58	6.37	126.63
945	47.25	195.72	1.60	1.60	7.01	126.58
946	47.30	186.09	1.62	1.62	7.77	126.60
947	47.35	176.89	1.67	1.67	8.93	126.80
948	47.40	163.37	1.84	1.84	10.44	127.10
949	47.45	151.42	1.96	1.96	12.43	127.48
950	47.50	138.07	2.12	2.12	14.68	127.79
951	47.55	125.10	2.28	2.28	17.29	128.11
952	47.60	114.45	2.46	2.46	20.25	128.48
953	47.65	104.04	2.70	2.70	23.13	128.93
954	47.70	99.74	2.96	2.96	25.85	129.56
955	47.75	97.86	3.35	3.35	27.91	130.24
956	47.80	96.67	3.65	3.65	29.76	130.94
957	47.85	95.57	4.01	4.01	31.19	131.45
958	47.90	94.82	4.19	4.19	32.23	131.89
959	47.95	95.95	4.40	4.40	32.35	132.25
960	48.00	100.76	4.55	4.55	31.86	132.55

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
961	48.05	104.27	4.60	4.60	30.84	132.71
962	48.10	108.12	4.54	4.54	30.09	132.68
963	48.15	107.18	4.40	4.40	29.62	132.51
964	48.20	105.47	4.26	4.26	29.98	132.24
965	48.25	99.84	4.18	4.18	30.87	131.97
966	48.30	94.56	4.11	4.11	32.52	131.69
967	48.35	87.16	4.04	4.04	34.46	131.42
968	48.40	81.18	4.00	4.00	36.90	131.19
969	48.45	75.16	4.04	4.04	39.22	131.14
970	48.50	72.92	4.20	4.20	41.31	131.28
971	48.55	71.86	4.41	4.41	42.36	131.51
972	48.60	72.80	4.49	4.49	42.48	131.76
973	48.65	75.61	4.59	4.59	41.30	131.91
974	48.70	80.23	4.53	4.53	39.12	132.11
975	48.75	88.04	4.56	4.56	36.10	132.17
976	48.80	95.88	4.34	4.34	32.78	132.20
977	48.85	105.37	4.19	4.19	29.63	131.98
978	48.90	111.15	3.85	3.85	27.00	131.65
979	48.95	115.44	3.57	3.57	25.16	131.15
980	49.00	115.24	3.32	3.32	24.10	130.69
981	49.05	113.81	3.16	3.16	23.94	130.32
982	49.10	110.19	3.13	3.13	24.39	130.14
983	49.15	106.83	3.16	3.16	25.49	130.14
984	49.20	102.19	3.28	3.28	26.83	130.29
985	49.25	99.75	3.44	3.44	28.45	130.63
986	49.30	97.87	3.73	3.73	29.73	131.03
987	49.35	97.97	3.91	3.91	30.67	131.41
988	49.40	98.43	4.05	4.05	30.76	131.59
989	49.45	100.30	3.98	3.98	30.29	131.58
990	49.50	101.97	3.84	3.84	29.22	131.37
991	49.55	104.29	3.64	3.64	28.08	131.03
992	49.60	104.83	3.41	3.41	26.89	130.55
993	49.65	104.83	3.13	3.13	25.95	130.18
994	49.70	106.85	3.11	3.11	25.30	130.03
995	49.75	108.90	3.18	3.18	24.88	130.17
996	49.80	111.97	3.24	3.24	24.63	130.26
997	49.85	111.42	3.18	3.18	24.38	130.02
998	49.90	107.22	2.89	2.89	24.27	129.71

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q _c :	Measured cone resistance (tsf)
f _s :	Sleeve friction resistance (tsf)
u:	Pore pressure (tsf)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (pcf)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
1	0.05	0.00	0.00	0.00	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
2	0.10	0.01	0.00	0.01	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
3	0.15	0.01	0.00	0.01	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
4	0.20	0.01	0.00	0.01	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
5	0.25	0.01	0.00	0.01	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
6	0.30	0.02	0.00	0.02	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
7	0.35	0.02	0.00	0.02	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
8	0.40	0.02	0.00	0.02	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
9	0.45	0.02	0.00	0.02	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
10	0.50	0.03	0.00	0.03	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
11	0.55	0.03	0.00	0.03	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
12	0.60	0.03	0.00	0.03	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
13	0.65	0.04	0.00	0.04	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
14	0.70	0.04	0.00	0.04	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
15	0.75	0.04	0.00	0.04	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
16	0.80	0.05	0.00	0.05	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
17	0.85	0.05	0.00	0.05	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
18	0.90	0.05	0.00	0.05	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
19	0.95	0.06	0.00	0.06	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
20	1.00	0.06	0.00	0.06	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
21	1.05	0.06	0.00	0.06	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
22	1.10	0.07	0.00	0.07	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
23	1.15	0.07	0.00	0.07	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
24	1.20	0.07	0.00	0.07	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
25	1.25	0.07	0.00	0.07	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
26	1.30	0.08	0.00	0.08	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
27	1.35	0.08	0.00	0.08	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
28	1.40	0.08	0.00	0.08	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
29	1.45	0.09	0.00	0.09	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
30	1.50	0.09	0.00	0.09	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
31	1.55	0.09	0.00	0.09	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
32	1.60	0.10	0.00	0.10	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
33	1.65	0.10	0.00	0.10	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
34	1.70	0.10	0.00	0.10	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
35	1.75	0.11	0.00	0.11	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
36	1.80	0.11	0.00	0.11	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
37	1.85	0.11	0.00	0.11	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
38	1.90	0.12	0.00	0.12	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
39	1.95	0.12	0.00	0.12	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
40	2.00	0.12	0.00	0.12	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
41	2.05	0.12	0.00	0.12	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
42	2.10	0.13	0.00	0.13	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
43	2.15	0.13	0.00	0.13	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
44	2.20	0.13	0.00	0.13	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
45	2.25	0.14	0.00	0.14	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
46	2.30	0.14	0.00	0.14	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
47	2.35	0.14	0.00	0.14	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
48	2.40	0.15	0.00	0.15	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
49	2.45	0.15	0.00	0.15	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
50	2.50	0.15	0.00	0.15	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
51	2.55	0.16	0.00	0.16	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
52	2.60	0.16	0.00	0.16	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
53	2.65	0.16	0.00	0.16	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
54	2.70	0.16	0.00	0.16	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
55	2.75	0.17	0.00	0.17	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
56	2.80	0.17	0.00	0.17	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
57	2.85	0.17	0.00	0.17	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
58	2.90	0.18	0.00	0.18	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
59	2.95	0.18	0.00	0.18	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
60	3.00	0.18	0.00	0.18	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
61	3.05	0.19	0.00	0.19	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
62	3.10	0.19	0.00	0.19	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
63	3.15	0.19	0.00	0.19	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
64	3.20	0.20	0.00	0.20	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
65	3.25	0.20	0.00	0.20	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
66	3.30	0.20	0.00	0.20	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
67	3.35	0.20	0.00	0.20	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
68	3.40	0.21	0.00	0.21	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
69	3.45	0.21	0.00	0.21	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
70	3.50	0.21	0.00	0.21	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
71	3.55	0.22	0.00	0.22	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
72	3.60	0.22	0.00	0.22	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
73	3.65	0.22	0.00	0.22	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
74	3.70	0.23	0.00	0.23	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
75	3.75	0.23	0.00	0.23	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
76	3.80	0.23	0.00	0.23	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
77	3.85	0.23	0.00	0.23	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
78	3.90	0.24	0.00	0.24	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
79	3.95	0.24	0.00	0.24	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
80	4.00	0.24	0.00	0.24	1.00	0.479	1.04	0.460	1.10	1.30	2.000	No
81	4.05	0.25	0.00	0.25	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
82	4.10	0.25	0.00	0.25	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
83	4.15	0.25	0.00	0.25	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
84	4.20	0.25	0.00	0.25	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
85	4.25	0.26	0.00	0.26	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
86	4.30	0.26	0.00	0.26	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
87	4.35	0.26	0.00	0.26	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
88	4.40	0.27	0.00	0.27	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
89	4.45	0.27	0.00	0.27	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
90	4.50	0.27	0.00	0.27	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
91	4.55	0.27	0.00	0.27	1.00	0.479	1.04	0.459	1.10	1.30	2.000	Yes
92	4.60	0.28	0.00	0.28	1.00	0.479	1.04	0.459	1.10	1.30	2.000	Yes
93	4.65	0.28	0.00	0.28	1.00	0.479	1.04	0.459	1.10	1.30	2.000	Yes
94	4.70	0.28	0.00	0.28	0.99	0.479	1.04	0.459	1.10	1.30	2.000	Yes
95	4.75	0.29	0.00	0.29	0.99	0.478	1.04	0.459	1.10	1.30	2.000	Yes
96	4.80	0.29	0.00	0.29	0.99	0.478	1.04	0.459	1.10	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
97	4.85	0.29	0.00	0.29	0.99	0.478	1.04	0.458	1.10	1.30	2.000	Yes
98	4.90	0.29	0.00	0.29	0.99	0.478	1.04	0.458	1.10	1.30	2.000	Yes
99	4.95	0.30	0.00	0.30	0.99	0.478	1.04	0.458	1.10	1.30	2.000	Yes
100	5.00	0.30	0.00	0.30	0.99	0.478	1.04	0.458	1.10	1.30	2.000	Yes
101	5.05	0.30	0.00	0.30	0.99	0.478	1.04	0.458	1.10	1.30	2.000	Yes
102	5.10	0.31	0.00	0.31	0.99	0.478	1.04	0.458	1.10	1.30	2.000	Yes
103	5.15	0.31	0.00	0.31	0.99	0.478	1.04	0.458	1.10	1.30	2.000	Yes
104	5.20	0.31	0.00	0.31	0.99	0.478	1.04	0.458	1.10	1.30	2.000	Yes
105	5.25	0.32	0.00	0.32	0.99	0.478	1.04	0.458	1.10	1.30	2.000	Yes
106	5.30	0.32	0.00	0.32	0.99	0.478	1.04	0.458	1.10	1.30	2.000	Yes
107	5.35	0.32	0.00	0.32	0.99	0.478	1.04	0.458	1.10	1.30	2.000	Yes
108	5.40	0.32	0.00	0.32	0.99	0.478	1.04	0.458	1.10	1.30	2.000	Yes
109	5.45	0.33	0.00	0.33	0.99	0.478	1.04	0.458	1.10	1.30	2.000	Yes
110	5.50	0.33	0.00	0.33	0.99	0.477	1.04	0.458	1.10	1.30	2.000	Yes
111	5.55	0.33	0.00	0.33	0.99	0.477	1.04	0.458	1.10	1.30	2.000	No
112	5.60	0.33	0.00	0.33	0.99	0.477	1.04	0.458	1.10	1.30	2.000	No
113	5.65	0.34	0.00	0.34	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
114	5.70	0.34	0.00	0.34	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
115	5.75	0.34	0.00	0.34	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
116	5.80	0.35	0.00	0.35	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
117	5.85	0.35	0.00	0.35	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
118	5.90	0.35	0.00	0.35	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
119	5.95	0.35	0.00	0.35	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
120	6.00	0.36	0.00	0.36	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
121	6.05	0.36	0.00	0.36	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
122	6.10	0.36	0.00	0.36	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
123	6.15	0.37	0.00	0.37	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
124	6.20	0.37	0.00	0.37	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
125	6.25	0.37	0.00	0.37	0.99	0.476	1.04	0.457	1.10	1.30	2.000	No
126	6.30	0.37	0.00	0.37	0.99	0.476	1.04	0.457	1.09	1.30	2.000	No
127	6.35	0.38	0.00	0.38	0.99	0.476	1.04	0.457	1.09	1.30	2.000	No
128	6.40	0.38	0.00	0.38	0.99	0.476	1.04	0.456	1.09	1.30	2.000	No
129	6.45	0.38	0.00	0.38	0.99	0.476	1.04	0.456	1.09	1.30	2.000	No
130	6.50	0.39	0.00	0.39	0.99	0.476	1.04	0.456	1.09	1.30	2.000	No
131	6.55	0.39	0.00	0.39	0.99	0.476	1.04	0.456	1.09	1.30	2.000	No
132	6.60	0.39	0.00	0.39	0.99	0.476	1.04	0.456	1.09	1.30	2.000	No
133	6.65	0.39	0.00	0.39	0.99	0.476	1.04	0.456	1.09	1.30	2.000	No
134	6.70	0.40	0.00	0.40	0.99	0.476	1.04	0.456	1.09	1.30	2.000	No
135	6.75	0.40	0.00	0.40	0.99	0.476	1.04	0.456	1.09	1.30	2.000	No
136	6.80	0.40	0.00	0.40	0.99	0.476	1.04	0.456	1.09	1.30	2.000	No
137	6.85	0.40	0.00	0.40	0.99	0.476	1.04	0.456	1.08	1.30	2.000	No
138	6.90	0.41	0.00	0.41	0.99	0.476	1.04	0.456	1.08	1.30	2.000	No
139	6.95	0.41	0.00	0.41	0.99	0.475	1.04	0.456	1.08	1.30	2.000	No
140	7.00	0.41	0.00	0.41	0.99	0.475	1.04	0.456	1.08	1.30	2.000	No
141	7.05	0.42	0.00	0.42	0.99	0.475	1.04	0.456	1.08	1.30	2.000	No
142	7.10	0.42	0.00	0.42	0.99	0.475	1.04	0.455	1.08	1.30	2.000	No
143	7.15	0.42	0.00	0.42	0.99	0.475	1.04	0.455	1.08	1.30	2.000	No
144	7.20	0.42	0.00	0.42	0.99	0.475	1.04	0.455	1.08	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
145	7.25	0.43	0.00	0.43	0.99	0.475	1.04	0.455	1.08	1.30	2.000	No
146	7.30	0.43	0.00	0.43	0.99	0.475	1.04	0.455	1.08	1.30	2.000	No
147	7.35	0.43	0.00	0.43	0.99	0.475	1.04	0.455	1.08	1.30	2.000	No
148	7.40	0.43	0.00	0.43	0.99	0.475	1.04	0.455	1.08	1.30	2.000	No
149	7.45	0.44	0.00	0.44	0.99	0.475	1.04	0.455	1.08	1.30	2.000	No
150	7.50	0.44	0.00	0.44	0.99	0.475	1.04	0.455	1.08	1.30	2.000	No
151	7.55	0.44	0.00	0.44	0.99	0.475	1.04	0.455	1.08	1.30	2.000	No
152	7.60	0.45	0.00	0.45	0.99	0.475	1.04	0.455	1.08	1.30	2.000	Yes
153	7.65	0.45	0.00	0.45	0.99	0.474	1.04	0.455	1.08	1.30	2.000	Yes
154	7.70	0.45	0.00	0.45	0.99	0.474	1.04	0.455	1.08	1.30	2.000	Yes
155	7.75	0.45	0.00	0.45	0.99	0.474	1.04	0.455	1.08	1.30	2.000	Yes
156	7.80	0.46	0.00	0.46	0.99	0.474	1.04	0.455	1.08	1.30	2.000	Yes
157	7.85	0.46	0.00	0.46	0.99	0.474	1.04	0.454	1.08	1.30	2.000	Yes
158	7.90	0.46	0.00	0.46	0.99	0.474	1.04	0.454	1.08	1.30	2.000	Yes
159	7.95	0.47	0.00	0.47	0.99	0.474	1.04	0.454	1.08	1.30	2.000	Yes
160	8.00	0.47	0.00	0.47	0.99	0.474	1.04	0.454	1.08	1.30	2.000	Yes
161	8.05	0.47	0.00	0.47	0.99	0.475	1.04	0.456	1.08	1.30	2.000	Yes
162	8.10	0.47	0.00	0.47	0.98	0.477	1.04	0.457	1.08	1.30	2.000	Yes
163	8.15	0.48	0.00	0.47	0.98	0.478	1.04	0.459	1.08	1.30	2.000	Yes
164	8.20	0.48	0.01	0.47	0.98	0.480	1.04	0.460	1.08	1.30	2.000	Yes
165	8.25	0.48	0.01	0.48	0.98	0.481	1.04	0.461	1.08	1.30	2.000	Yes
166	8.30	0.49	0.01	0.48	0.98	0.483	1.04	0.463	1.09	1.30	2.000	Yes
167	8.35	0.49	0.01	0.48	0.98	0.484	1.04	0.464	1.09	1.30	2.000	Yes
168	8.40	0.49	0.01	0.48	0.98	0.486	1.04	0.465	1.09	1.30	2.000	Yes
169	8.45	0.49	0.01	0.48	0.98	0.487	1.04	0.467	1.09	1.30	2.000	Yes
170	8.50	0.50	0.02	0.48	0.98	0.489	1.04	0.468	1.09	1.30	2.000	Yes
171	8.55	0.50	0.02	0.48	0.98	0.490	1.04	0.470	1.09	1.30	0.576	No
172	8.60	0.50	0.02	0.48	0.98	0.491	1.04	0.471	1.09	1.30	0.577	No
173	8.65	0.51	0.02	0.49	0.98	0.493	1.04	0.472	1.09	1.30	0.578	No
174	8.70	0.51	0.02	0.49	0.98	0.494	1.04	0.474	1.09	1.30	0.580	No
175	8.75	0.51	0.02	0.49	0.98	0.495	1.04	0.475	1.09	1.30	0.582	No
176	8.80	0.51	0.02	0.49	0.98	0.497	1.04	0.476	1.09	1.30	0.584	No
177	8.85	0.52	0.03	0.49	0.98	0.498	1.04	0.477	1.09	1.30	0.586	No
178	8.90	0.52	0.03	0.49	0.98	0.500	1.04	0.479	1.09	1.30	0.588	No
179	8.95	0.52	0.03	0.49	0.98	0.501	1.04	0.480	1.09	1.30	2.000	Yes
180	9.00	0.53	0.03	0.49	0.98	0.502	1.04	0.481	1.08	1.30	2.000	Yes
181	9.05	0.53	0.03	0.50	0.98	0.504	1.04	0.483	1.08	1.30	2.000	Yes
182	9.10	0.53	0.03	0.50	0.98	0.505	1.04	0.484	1.08	1.30	2.000	Yes
183	9.15	0.53	0.04	0.50	0.98	0.506	1.04	0.485	1.08	1.30	2.000	Yes
184	9.20	0.54	0.04	0.50	0.98	0.507	1.04	0.486	1.08	1.30	2.000	Yes
185	9.25	0.54	0.04	0.50	0.98	0.509	1.04	0.488	1.08	1.30	2.000	Yes
186	9.30	0.54	0.04	0.50	0.98	0.510	1.04	0.489	1.07	1.30	2.000	Yes
187	9.35	0.55	0.04	0.50	0.98	0.511	1.04	0.490	1.07	1.30	2.000	Yes
188	9.40	0.55	0.04	0.51	0.98	0.513	1.04	0.491	1.07	1.30	2.000	Yes
189	9.45	0.55	0.05	0.51	0.98	0.514	1.04	0.493	1.07	1.30	2.000	Yes
190	9.50	0.55	0.05	0.51	0.98	0.515	1.04	0.494	1.07	1.30	2.000	Yes
191	9.55	0.56	0.05	0.51	0.98	0.516	1.04	0.495	1.07	1.30	2.000	Yes
192	9.60	0.56	0.05	0.51	0.98	0.518	1.04	0.496	1.07	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
193	9.65	0.56	0.05	0.51	0.98	0.519	1.04	0.497	1.07	1.30	2.000	Yes
194	9.70	0.57	0.05	0.51	0.98	0.520	1.04	0.498	1.07	1.30	2.000	Yes
195	9.75	0.57	0.05	0.51	0.98	0.521	1.04	0.500	1.07	1.30	2.000	Yes
196	9.80	0.57	0.06	0.52	0.98	0.523	1.04	0.501	1.07	1.30	2.000	Yes
197	9.85	0.57	0.06	0.52	0.98	0.524	1.04	0.502	1.07	1.30	2.000	Yes
198	9.90	0.58	0.06	0.52	0.98	0.525	1.04	0.503	1.07	1.30	2.000	Yes
199	9.95	0.58	0.06	0.52	0.98	0.526	1.04	0.504	1.07	1.30	2.000	Yes
200	10.00	0.58	0.06	0.52	0.98	0.527	1.04	0.505	1.07	1.30	2.000	Yes
201	10.05	0.59	0.06	0.52	0.98	0.528	1.04	0.507	1.07	1.30	2.000	Yes
202	10.10	0.59	0.07	0.52	0.98	0.530	1.04	0.508	1.07	1.30	2.000	Yes
203	10.15	0.59	0.07	0.52	0.98	0.531	1.04	0.509	1.07	1.30	2.000	Yes
204	10.20	0.59	0.07	0.53	0.98	0.532	1.04	0.510	1.07	1.30	2.000	Yes
205	10.25	0.60	0.07	0.53	0.98	0.533	1.04	0.511	1.07	1.30	2.000	Yes
206	10.30	0.60	0.07	0.53	0.98	0.534	1.04	0.512	1.07	1.30	2.000	Yes
207	10.35	0.60	0.07	0.53	0.98	0.535	1.04	0.513	1.07	1.30	0.639	No
208	10.40	0.61	0.07	0.53	0.98	0.537	1.04	0.514	1.07	1.30	0.641	No
209	10.45	0.61	0.08	0.53	0.98	0.538	1.04	0.515	1.07	1.30	0.642	No
210	10.50	0.61	0.08	0.53	0.98	0.539	1.04	0.516	1.07	1.30	0.644	No
211	10.55	0.61	0.08	0.53	0.98	0.540	1.04	0.518	1.07	1.30	0.646	No
212	10.60	0.62	0.08	0.54	0.98	0.541	1.04	0.519	1.07	1.30	0.648	No
213	10.65	0.62	0.08	0.54	0.98	0.542	1.04	0.520	1.07	1.30	0.649	No
214	10.70	0.62	0.08	0.54	0.98	0.543	1.04	0.521	1.07	1.30	0.650	No
215	10.75	0.63	0.09	0.54	0.98	0.544	1.04	0.522	1.07	1.30	0.652	No
216	10.80	0.63	0.09	0.54	0.98	0.545	1.04	0.523	1.07	1.30	0.654	No
217	10.85	0.63	0.09	0.54	0.98	0.547	1.04	0.524	1.07	1.30	0.655	No
218	10.90	0.63	0.09	0.54	0.98	0.548	1.04	0.525	1.07	1.30	0.657	No
219	10.95	0.64	0.09	0.54	0.98	0.549	1.04	0.526	1.07	1.30	0.658	No
220	11.00	0.64	0.09	0.55	0.98	0.550	1.04	0.527	1.07	1.30	0.659	No
221	11.05	0.64	0.10	0.55	0.98	0.551	1.04	0.528	1.07	1.30	0.660	No
222	11.10	0.65	0.10	0.55	0.98	0.552	1.04	0.529	1.07	1.30	0.662	No
223	11.15	0.65	0.10	0.55	0.98	0.553	1.04	0.530	1.07	1.30	0.663	No
224	11.20	0.65	0.10	0.55	0.97	0.554	1.04	0.531	1.07	1.30	0.665	No
225	11.25	0.65	0.10	0.55	0.97	0.555	1.04	0.532	1.07	1.30	0.666	No
226	11.30	0.66	0.10	0.55	0.97	0.556	1.04	0.533	1.07	1.30	0.668	No
227	11.35	0.66	0.10	0.55	0.97	0.557	1.04	0.534	1.07	1.30	0.670	No
228	11.40	0.66	0.11	0.56	0.97	0.558	1.04	0.535	1.07	1.30	0.671	No
229	11.45	0.67	0.11	0.56	0.97	0.559	1.04	0.536	1.07	1.30	0.673	No
230	11.50	0.67	0.11	0.56	0.97	0.560	1.04	0.537	1.07	1.30	2.000	Yes
231	11.55	0.67	0.11	0.56	0.97	0.561	1.04	0.538	1.07	1.30	2.000	Yes
232	11.60	0.67	0.11	0.56	0.97	0.562	1.04	0.539	1.07	1.30	2.000	Yes
233	11.65	0.68	0.11	0.56	0.97	0.563	1.04	0.540	1.06	1.30	2.000	Yes
234	11.70	0.68	0.12	0.56	0.97	0.564	1.04	0.541	1.06	1.30	2.000	Yes
235	11.75	0.68	0.12	0.57	0.97	0.565	1.04	0.542	1.06	1.30	2.000	Yes
236	11.80	0.68	0.12	0.57	0.97	0.566	1.04	0.542	1.06	1.30	2.000	Yes
237	11.85	0.69	0.12	0.57	0.97	0.567	1.04	0.543	1.06	1.30	2.000	Yes
238	11.90	0.69	0.12	0.57	0.97	0.568	1.04	0.544	1.06	1.30	2.000	Yes
239	11.95	0.69	0.12	0.57	0.97	0.569	1.04	0.545	1.06	1.30	2.000	Yes
240	12.00	0.70	0.12	0.57	0.97	0.570	1.04	0.546	1.06	1.30	0.691	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
241	12.05	0.70	0.13	0.57	0.97	0.571	1.04	0.547	1.06	1.30	2.000	Yes
242	12.10	0.70	0.13	0.57	0.97	0.572	1.04	0.548	1.06	1.30	2.000	Yes
243	12.15	0.71	0.13	0.58	0.97	0.573	1.04	0.549	1.06	1.30	2.000	Yes
244	12.20	0.71	0.13	0.58	0.97	0.573	1.04	0.550	1.06	1.30	2.000	Yes
245	12.25	0.71	0.13	0.58	0.97	0.574	1.04	0.551	1.06	1.30	2.000	Yes
246	12.30	0.71	0.13	0.58	0.97	0.575	1.04	0.551	1.06	1.30	2.000	Yes
247	12.35	0.72	0.14	0.58	0.97	0.576	1.04	0.552	1.06	1.30	2.000	Yes
248	12.40	0.72	0.14	0.58	0.97	0.577	1.04	0.553	1.06	1.30	0.698	No
249	12.45	0.72	0.14	0.58	0.97	0.578	1.04	0.554	1.06	1.30	2.000	Yes
250	12.50	0.73	0.14	0.58	0.97	0.579	1.04	0.555	1.06	1.30	2.000	Yes
251	12.55	0.73	0.14	0.59	0.97	0.580	1.04	0.556	1.06	1.30	2.000	Yes
252	12.60	0.73	0.14	0.59	0.97	0.581	1.04	0.557	1.06	1.30	2.000	Yes
253	12.65	0.73	0.15	0.59	0.97	0.582	1.04	0.557	1.06	1.30	2.000	Yes
254	12.70	0.74	0.15	0.59	0.97	0.582	1.04	0.558	1.06	1.30	2.000	Yes
255	12.75	0.74	0.15	0.59	0.97	0.583	1.04	0.559	1.06	1.30	2.000	Yes
256	12.80	0.74	0.15	0.59	0.97	0.584	1.04	0.560	1.05	1.30	2.000	Yes
257	12.85	0.75	0.15	0.59	0.97	0.585	1.04	0.561	1.05	1.30	2.000	Yes
258	12.90	0.75	0.15	0.60	0.97	0.586	1.04	0.561	1.05	1.30	2.000	Yes
259	12.95	0.75	0.15	0.60	0.97	0.587	1.04	0.562	1.05	1.30	2.000	Yes
260	13.00	0.75	0.16	0.60	0.97	0.588	1.04	0.563	1.05	1.30	0.719	No
261	13.05	0.76	0.16	0.60	0.97	0.588	1.04	0.564	1.05	1.30	0.721	No
262	13.10	0.76	0.16	0.60	0.97	0.589	1.04	0.565	1.05	1.30	0.722	No
263	13.15	0.76	0.16	0.60	0.97	0.590	1.04	0.565	1.05	1.30	0.723	No
264	13.20	0.77	0.16	0.60	0.97	0.591	1.04	0.566	1.05	1.30	0.724	No
265	13.25	0.77	0.16	0.60	0.97	0.592	1.04	0.567	1.05	1.30	0.725	No
266	13.30	0.77	0.17	0.61	0.97	0.592	1.04	0.568	1.05	1.30	0.728	No
267	13.35	0.77	0.17	0.61	0.97	0.593	1.04	0.569	1.05	1.30	0.729	No
268	13.40	0.78	0.17	0.61	0.97	0.594	1.04	0.569	1.05	1.30	0.731	No
269	13.45	0.78	0.17	0.61	0.97	0.595	1.04	0.570	1.05	1.30	0.733	No
270	13.50	0.78	0.17	0.61	0.97	0.596	1.04	0.571	1.05	1.30	0.734	No
271	13.55	0.79	0.17	0.61	0.97	0.597	1.04	0.572	1.05	1.30	0.734	No
272	13.60	0.79	0.17	0.61	0.97	0.597	1.04	0.573	1.05	1.30	0.735	No
273	13.65	0.79	0.18	0.61	0.97	0.598	1.04	0.573	1.05	1.30	0.736	No
274	13.70	0.79	0.18	0.62	0.97	0.599	1.04	0.574	1.05	1.30	0.737	No
275	13.75	0.80	0.18	0.62	0.97	0.600	1.04	0.575	1.05	1.30	0.738	No
276	13.80	0.80	0.18	0.62	0.97	0.601	1.04	0.576	1.05	1.30	0.739	No
277	13.85	0.80	0.18	0.62	0.97	0.601	1.04	0.576	1.05	1.30	0.740	No
278	13.90	0.80	0.18	0.62	0.97	0.602	1.04	0.577	1.05	1.30	0.741	No
279	13.95	0.81	0.19	0.62	0.97	0.603	1.04	0.578	1.05	1.30	0.742	No
280	14.00	0.81	0.19	0.62	0.97	0.604	1.04	0.579	1.05	1.30	0.743	No
281	14.05	0.81	0.19	0.62	0.96	0.604	1.04	0.579	1.05	1.30	0.744	No
282	14.10	0.82	0.19	0.63	0.96	0.605	1.04	0.580	1.05	1.30	0.745	No
283	14.15	0.82	0.19	0.63	0.96	0.606	1.04	0.581	1.05	1.30	0.745	No
284	14.20	0.82	0.19	0.63	0.96	0.607	1.04	0.581	1.05	1.30	0.746	No
285	14.25	0.82	0.20	0.63	0.96	0.607	1.04	0.582	1.05	1.30	0.747	No
286	14.30	0.83	0.20	0.63	0.96	0.608	1.04	0.583	1.05	1.30	0.748	No
287	14.35	0.83	0.20	0.63	0.96	0.609	1.04	0.584	1.05	1.30	0.749	No
288	14.40	0.83	0.20	0.63	0.96	0.610	1.04	0.584	1.05	1.30	0.750	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
289	14.45	0.84	0.20	0.64	0.96	0.610	1.04	0.585	1.05	1.30	0.751	No
290	14.50	0.84	0.20	0.64	0.96	0.611	1.04	0.586	1.05	1.30	0.752	No
291	14.55	0.84	0.20	0.64	0.96	0.612	1.04	0.586	1.05	1.30	0.753	No
292	14.60	0.85	0.21	0.64	0.96	0.612	1.04	0.587	1.05	1.30	0.754	No
293	14.65	0.85	0.21	0.64	0.96	0.613	1.04	0.588	1.05	1.30	0.755	No
294	14.70	0.85	0.21	0.64	0.96	0.614	1.04	0.588	1.05	1.30	0.756	No
295	14.75	0.85	0.21	0.64	0.96	0.614	1.04	0.589	1.05	1.30	0.756	No
296	14.80	0.86	0.21	0.64	0.96	0.615	1.04	0.590	1.05	1.30	0.757	No
297	14.85	0.86	0.21	0.65	0.96	0.616	1.04	0.590	1.05	1.30	0.758	No
298	14.90	0.86	0.22	0.65	0.96	0.617	1.04	0.591	1.04	1.30	0.760	No
299	14.95	0.87	0.22	0.65	0.96	0.617	1.04	0.592	1.04	1.30	0.761	No
300	15.00	0.87	0.22	0.65	0.96	0.618	1.04	0.592	1.04	1.30	0.762	No
301	15.05	0.87	0.22	0.65	0.96	0.619	1.04	0.593	1.04	1.30	0.764	No
302	15.10	0.87	0.22	0.65	0.96	0.619	1.04	0.594	1.04	1.30	0.765	No
303	15.15	0.88	0.22	0.65	0.96	0.620	1.04	0.594	1.04	1.30	0.766	No
304	15.20	0.88	0.22	0.65	0.96	0.621	1.04	0.595	1.04	1.30	0.768	No
305	15.25	0.88	0.23	0.66	0.96	0.621	1.04	0.596	1.04	1.30	0.769	No
306	15.30	0.89	0.23	0.66	0.96	0.622	1.04	0.596	1.04	1.30	0.770	No
307	15.35	0.89	0.23	0.66	0.96	0.623	1.04	0.597	1.04	1.30	0.771	No
308	15.40	0.89	0.23	0.66	0.96	0.623	1.04	0.597	1.04	1.30	0.771	No
309	15.45	0.89	0.23	0.66	0.96	0.624	1.04	0.598	1.04	1.30	0.772	No
310	15.50	0.90	0.23	0.66	0.96	0.625	1.04	0.599	1.04	1.30	0.773	No
311	15.55	0.90	0.24	0.66	0.96	0.625	1.04	0.599	1.04	1.30	0.774	No
312	15.60	0.90	0.24	0.67	0.96	0.626	1.04	0.600	1.04	1.30	0.775	No
313	15.65	0.90	0.24	0.67	0.96	0.627	1.04	0.601	1.04	1.30	0.776	No
314	15.70	0.91	0.24	0.67	0.96	0.627	1.04	0.601	1.04	1.30	0.777	No
315	15.75	0.91	0.24	0.67	0.96	0.628	1.04	0.602	1.04	1.30	0.778	No
316	15.80	0.91	0.24	0.67	0.96	0.628	1.04	0.602	1.04	1.30	0.778	No
317	15.85	0.92	0.24	0.67	0.96	0.629	1.04	0.603	1.04	1.30	0.778	No
318	15.90	0.92	0.25	0.67	0.96	0.630	1.04	0.604	1.04	1.30	0.777	No
319	15.95	0.92	0.25	0.67	0.96	0.630	1.04	0.604	1.04	1.30	0.777	No
320	16.00	0.93	0.25	0.68	0.96	0.631	1.04	0.605	1.04	1.30	0.777	No
321	16.05	0.93	0.25	0.68	0.96	0.631	1.04	0.605	1.04	1.30	0.777	No
322	16.10	0.93	0.25	0.68	0.96	0.632	1.04	0.606	1.04	1.30	0.777	No
323	16.15	0.93	0.25	0.68	0.96	0.633	1.04	0.606	1.05	1.30	0.777	No
324	16.20	0.94	0.26	0.68	0.96	0.633	1.04	0.607	1.04	1.30	0.778	No
325	16.25	0.94	0.26	0.68	0.96	0.634	1.04	0.607	1.04	1.30	0.780	No
326	16.30	0.94	0.26	0.68	0.96	0.634	1.04	0.608	1.04	1.30	0.782	No
327	16.35	0.95	0.26	0.69	0.96	0.635	1.04	0.609	1.04	1.30	0.783	No
328	16.40	0.95	0.26	0.69	0.96	0.635	1.04	0.609	1.04	1.30	0.785	No
329	16.45	0.95	0.26	0.69	0.96	0.636	1.04	0.610	1.04	1.30	0.786	No
330	16.50	0.95	0.27	0.69	0.96	0.637	1.04	0.610	1.04	1.30	0.787	No
331	16.55	0.96	0.27	0.69	0.96	0.637	1.04	0.611	1.04	1.30	0.788	No
332	16.60	0.96	0.27	0.69	0.96	0.638	1.04	0.611	1.04	1.30	0.789	No
333	16.65	0.96	0.27	0.69	0.96	0.638	1.04	0.612	1.04	1.30	0.790	No
334	16.70	0.97	0.27	0.69	0.96	0.639	1.04	0.612	1.04	1.30	0.791	No
335	16.75	0.97	0.27	0.70	0.95	0.639	1.04	0.613	1.04	1.30	0.792	No
336	16.80	0.97	0.27	0.70	0.95	0.640	1.04	0.613	1.04	1.30	0.793	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
337	16.85	0.98	0.28	0.70	0.95	0.640	1.04	0.614	1.04	1.30	0.794	No
338	16.90	0.98	0.28	0.70	0.95	0.641	1.04	0.614	1.04	1.30	0.795	No
339	16.95	0.98	0.28	0.70	0.95	0.642	1.04	0.615	1.04	1.30	0.796	No
340	17.00	0.98	0.28	0.70	0.95	0.642	1.04	0.615	1.04	1.30	2.000	Yes
341	17.05	0.99	0.28	0.70	0.95	0.643	1.04	0.616	1.04	1.30	2.000	Yes
342	17.10	0.99	0.28	0.71	0.95	0.643	1.04	0.616	1.04	1.30	2.000	Yes
343	17.15	0.99	0.29	0.71	0.95	0.644	1.04	0.617	1.04	1.30	2.000	Yes
344	17.20	1.00	0.29	0.71	0.95	0.644	1.04	0.617	1.04	1.30	2.000	Yes
345	17.25	1.00	0.29	0.71	0.95	0.645	1.04	0.618	1.04	1.30	2.000	Yes
346	17.30	1.00	0.29	0.71	0.95	0.645	1.04	0.618	1.04	1.30	2.000	Yes
347	17.35	1.01	0.29	0.71	0.95	0.646	1.04	0.619	1.05	1.30	2.000	Yes
348	17.40	1.01	0.29	0.71	0.95	0.646	1.04	0.619	1.04	1.30	2.000	Yes
349	17.45	1.01	0.29	0.72	0.95	0.647	1.04	0.620	1.04	1.30	2.000	Yes
350	17.50	1.01	0.30	0.72	0.95	0.647	1.04	0.620	1.04	1.30	2.000	Yes
351	17.55	1.02	0.30	0.72	0.95	0.648	1.04	0.621	1.04	1.30	0.795	No
352	17.60	1.02	0.30	0.72	0.95	0.648	1.04	0.621	1.04	1.30	2.000	Yes
353	17.65	1.02	0.30	0.72	0.95	0.649	1.04	0.622	1.04	1.30	2.000	Yes
354	17.70	1.03	0.30	0.72	0.95	0.649	1.04	0.622	1.04	1.30	2.000	Yes
355	17.75	1.03	0.30	0.72	0.95	0.650	1.04	0.623	1.04	1.30	2.000	Yes
356	17.80	1.03	0.31	0.73	0.95	0.650	1.04	0.623	1.04	1.30	2.000	Yes
357	17.85	1.03	0.31	0.73	0.95	0.651	1.04	0.623	1.04	1.30	2.000	Yes
358	17.90	1.04	0.31	0.73	0.95	0.651	1.04	0.624	1.04	1.30	2.000	Yes
359	17.95	1.04	0.31	0.73	0.95	0.651	1.04	0.624	1.04	1.30	2.000	Yes
360	18.00	1.04	0.31	0.73	0.95	0.652	1.04	0.625	1.03	1.30	2.000	Yes
361	18.05	1.05	0.31	0.73	0.95	0.652	1.04	0.625	1.03	1.30	2.000	Yes
362	18.10	1.05	0.32	0.73	0.95	0.653	1.04	0.626	1.03	1.30	2.000	Yes
363	18.15	1.05	0.32	0.74	0.95	0.653	1.04	0.626	1.03	1.30	2.000	Yes
364	18.20	1.06	0.32	0.74	0.95	0.654	1.04	0.627	1.04	1.30	2.000	Yes
365	18.25	1.06	0.32	0.74	0.95	0.654	1.04	0.627	1.04	1.30	2.000	Yes
366	18.30	1.06	0.32	0.74	0.95	0.655	1.04	0.627	1.04	1.30	2.000	Yes
367	18.35	1.06	0.32	0.74	0.95	0.655	1.04	0.628	1.04	1.30	2.000	Yes
368	18.40	1.07	0.32	0.74	0.95	0.655	1.04	0.628	1.04	1.30	2.000	Yes
369	18.45	1.07	0.33	0.74	0.95	0.656	1.04	0.629	1.04	1.30	2.000	Yes
370	18.50	1.07	0.33	0.75	0.95	0.656	1.04	0.629	1.04	1.30	2.000	Yes
371	18.55	1.08	0.33	0.75	0.95	0.657	1.04	0.629	1.05	1.30	2.000	Yes
372	18.60	1.08	0.33	0.75	0.95	0.657	1.04	0.630	1.05	1.30	2.000	Yes
373	18.65	1.08	0.33	0.75	0.95	0.657	1.04	0.630	1.05	1.30	2.000	Yes
374	18.70	1.09	0.33	0.75	0.95	0.658	1.04	0.631	1.04	1.30	2.000	Yes
375	18.75	1.09	0.34	0.75	0.95	0.658	1.04	0.631	1.04	1.30	2.000	Yes
376	18.80	1.09	0.34	0.76	0.95	0.659	1.04	0.631	1.04	1.30	2.000	Yes
377	18.85	1.10	0.34	0.76	0.95	0.659	1.04	0.632	1.04	1.30	2.000	Yes
378	18.90	1.10	0.34	0.76	0.95	0.660	1.04	0.632	1.04	1.30	2.000	Yes
379	18.95	1.10	0.34	0.76	0.95	0.660	1.04	0.632	1.03	1.30	2.000	Yes
380	19.00	1.10	0.34	0.76	0.95	0.660	1.04	0.633	1.03	1.30	2.000	Yes
381	19.05	1.11	0.34	0.76	0.95	0.661	1.04	0.633	1.03	1.30	2.000	Yes
382	19.10	1.11	0.35	0.76	0.95	0.661	1.04	0.634	1.03	1.30	2.000	Yes
383	19.15	1.11	0.35	0.77	0.95	0.661	1.04	0.634	1.03	1.30	2.000	Yes
384	19.20	1.12	0.35	0.77	0.95	0.662	1.04	0.634	1.03	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
385	19.25	1.12	0.35	0.77	0.95	0.662	1.04	0.635	1.03	1.30	2.000	Yes
386	19.30	1.12	0.35	0.77	0.94	0.663	1.04	0.635	1.03	1.30	2.000	Yes
387	19.35	1.12	0.35	0.77	0.94	0.663	1.04	0.636	1.03	1.30	0.831	No
388	19.40	1.13	0.36	0.77	0.94	0.664	1.04	0.636	1.03	1.30	0.831	No
389	19.45	1.13	0.36	0.77	0.94	0.664	1.04	0.636	1.03	1.30	0.831	No
390	19.50	1.13	0.36	0.77	0.94	0.664	1.04	0.637	1.03	1.30	0.832	No
391	19.55	1.14	0.36	0.78	0.94	0.665	1.04	0.637	1.03	1.30	0.832	No
392	19.60	1.14	0.36	0.78	0.94	0.665	1.04	0.638	1.03	1.30	0.833	No
393	19.65	1.14	0.36	0.78	0.94	0.666	1.04	0.638	1.03	1.30	0.834	No
394	19.70	1.15	0.37	0.78	0.94	0.666	1.04	0.638	1.03	1.30	0.835	No
395	19.75	1.15	0.37	0.78	0.94	0.666	1.04	0.639	1.03	1.30	0.836	No
396	19.80	1.15	0.37	0.78	0.94	0.667	1.04	0.639	1.03	1.30	0.836	No
397	19.85	1.15	0.37	0.78	0.94	0.667	1.04	0.639	1.03	1.30	0.835	No
398	19.90	1.16	0.37	0.79	0.94	0.668	1.04	0.640	1.03	1.30	0.835	No
399	19.95	1.16	0.37	0.79	0.94	0.668	1.04	0.640	1.03	1.30	0.835	No
400	20.00	1.16	0.37	0.79	0.94	0.668	1.04	0.641	1.03	1.30	0.836	No
401	20.05	1.17	0.38	0.79	0.94	0.669	1.04	0.641	1.03	1.30	0.837	No
402	20.10	1.17	0.38	0.79	0.94	0.669	1.04	0.641	1.03	1.30	0.838	No
403	20.15	1.17	0.38	0.79	0.94	0.669	1.04	0.642	1.03	1.30	0.840	No
404	20.20	1.17	0.38	0.79	0.94	0.670	1.04	0.642	1.03	1.30	0.841	No
405	20.25	1.18	0.38	0.79	0.94	0.670	1.04	0.642	1.03	1.30	0.842	No
406	20.30	1.18	0.38	0.80	0.94	0.671	1.04	0.643	1.02	1.30	0.843	No
407	20.35	1.18	0.39	0.80	0.94	0.671	1.04	0.643	1.02	1.30	0.844	No
408	20.40	1.19	0.39	0.80	0.94	0.671	1.04	0.644	1.02	1.30	0.844	No
409	20.45	1.19	0.39	0.80	0.94	0.672	1.04	0.644	1.02	1.30	0.845	No
410	20.50	1.19	0.39	0.80	0.94	0.672	1.04	0.644	1.02	1.30	0.845	No
411	20.55	1.19	0.39	0.80	0.94	0.673	1.04	0.645	1.02	1.30	0.846	No
412	20.60	1.20	0.39	0.80	0.94	0.673	1.04	0.645	1.02	1.30	0.846	No
413	20.65	1.20	0.39	0.81	0.94	0.673	1.04	0.645	1.02	1.30	0.847	No
414	20.70	1.20	0.40	0.81	0.94	0.674	1.04	0.646	1.02	1.30	0.846	No
415	20.75	1.21	0.40	0.81	0.94	0.674	1.04	0.646	1.03	1.30	0.846	No
416	20.80	1.21	0.40	0.81	0.94	0.674	1.04	0.646	1.03	1.30	0.845	No
417	20.85	1.21	0.40	0.81	0.94	0.675	1.04	0.647	1.03	1.30	0.845	No
418	20.90	1.21	0.40	0.81	0.94	0.675	1.04	0.647	1.03	1.30	0.845	No
419	20.95	1.22	0.40	0.81	0.94	0.675	1.04	0.647	1.03	1.30	0.845	No
420	21.00	1.22	0.41	0.81	0.94	0.676	1.04	0.648	1.03	1.30	0.846	No
421	21.05	1.22	0.41	0.82	0.94	0.676	1.04	0.648	1.03	1.30	0.847	No
422	21.10	1.23	0.41	0.82	0.94	0.676	1.04	0.648	1.03	1.30	0.848	No
423	21.15	1.23	0.41	0.82	0.94	0.677	1.04	0.649	1.02	1.30	0.849	No
424	21.20	1.23	0.41	0.82	0.94	0.677	1.04	0.649	1.02	1.30	0.851	No
425	21.25	1.24	0.41	0.82	0.94	0.677	1.04	0.649	1.02	1.30	0.852	No
426	21.30	1.24	0.41	0.82	0.94	0.678	1.04	0.649	1.02	1.30	0.852	No
427	21.35	1.24	0.42	0.82	0.94	0.678	1.04	0.650	1.02	1.30	0.853	No
428	21.40	1.24	0.42	0.83	0.94	0.678	1.04	0.650	1.02	1.30	0.854	No
429	21.45	1.25	0.42	0.83	0.94	0.679	1.04	0.650	1.02	1.30	0.855	No
430	21.50	1.25	0.42	0.83	0.94	0.679	1.04	0.651	1.02	1.30	0.856	No
431	21.55	1.25	0.42	0.83	0.94	0.679	1.04	0.651	1.02	1.30	0.857	No
432	21.60	1.26	0.42	0.83	0.94	0.680	1.04	0.651	1.02	1.30	0.858	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
433	21.65	1.26	0.43	0.83	0.94	0.680	1.04	0.652	1.02	1.30	0.859	No
434	21.70	1.26	0.43	0.83	0.93	0.680	1.04	0.652	1.02	1.30	0.860	No
435	21.75	1.26	0.43	0.83	0.93	0.681	1.04	0.652	1.02	1.30	0.861	No
436	21.80	1.27	0.43	0.84	0.93	0.681	1.04	0.653	1.02	1.30	0.862	No
437	21.85	1.27	0.43	0.84	0.93	0.681	1.04	0.653	1.02	1.30	0.862	No
438	21.90	1.27	0.43	0.84	0.93	0.682	1.04	0.653	1.02	1.30	0.863	No
439	21.95	1.27	0.44	0.84	0.93	0.682	1.04	0.654	1.02	1.30	0.863	No
440	22.00	1.28	0.44	0.84	0.93	0.682	1.04	0.654	1.02	1.30	0.864	No
441	22.05	1.28	0.44	0.84	0.93	0.683	1.04	0.654	1.02	1.30	0.864	No
442	22.10	1.28	0.44	0.84	0.93	0.683	1.04	0.655	1.02	1.30	0.865	No
443	22.15	1.29	0.44	0.84	0.93	0.684	1.04	0.655	1.02	1.30	0.865	No
444	22.20	1.29	0.44	0.85	0.93	0.684	1.04	0.655	1.02	1.30	0.865	No
445	22.25	1.29	0.44	0.85	0.93	0.684	1.04	0.656	1.02	1.30	0.865	No
446	22.30	1.29	0.45	0.85	0.93	0.684	1.04	0.656	1.02	1.30	0.865	No
447	22.35	1.30	0.45	0.85	0.93	0.685	1.04	0.656	1.02	1.30	0.866	No
448	22.40	1.30	0.45	0.85	0.93	0.685	1.04	0.657	1.02	1.30	0.865	No
449	22.45	1.30	0.45	0.85	0.93	0.685	1.04	0.657	1.02	1.30	0.865	No
450	22.50	1.31	0.45	0.85	0.93	0.686	1.04	0.657	1.02	1.30	0.864	No
451	22.55	1.31	0.45	0.86	0.93	0.686	1.04	0.657	1.02	1.30	0.864	No
452	22.60	1.31	0.46	0.86	0.93	0.686	1.04	0.658	1.02	1.30	0.864	No
453	22.65	1.31	0.46	0.86	0.93	0.686	1.04	0.658	1.02	1.30	0.864	No
454	22.70	1.32	0.46	0.86	0.93	0.687	1.04	0.658	1.02	1.30	0.865	No
455	22.75	1.32	0.46	0.86	0.93	0.687	1.04	0.658	1.02	1.30	0.866	No
456	22.80	1.32	0.46	0.86	0.93	0.687	1.04	0.659	1.02	1.30	0.866	No
457	22.85	1.33	0.46	0.86	0.93	0.688	1.04	0.659	1.02	1.30	0.867	No
458	22.90	1.33	0.46	0.86	0.93	0.688	1.04	0.659	1.02	1.30	0.868	No
459	22.95	1.33	0.47	0.87	0.93	0.688	1.04	0.659	1.02	1.30	0.870	No
460	23.00	1.34	0.47	0.87	0.93	0.688	1.04	0.660	1.02	1.30	0.871	No
461	23.05	1.34	0.47	0.87	0.93	0.689	1.04	0.660	1.02	1.30	0.872	No
462	23.10	1.34	0.47	0.87	0.93	0.689	1.04	0.660	1.02	1.30	0.873	No
463	23.15	1.34	0.47	0.87	0.93	0.689	1.04	0.661	1.02	1.30	0.873	No
464	23.20	1.35	0.47	0.87	0.93	0.689	1.04	0.661	1.02	1.30	0.874	No
465	23.25	1.35	0.48	0.87	0.93	0.690	1.04	0.661	1.02	1.30	0.875	No
466	23.30	1.35	0.48	0.87	0.93	0.690	1.04	0.661	1.02	1.30	0.875	No
467	23.35	1.36	0.48	0.88	0.93	0.690	1.04	0.662	1.02	1.30	0.876	No
468	23.40	1.36	0.48	0.88	0.93	0.691	1.04	0.662	1.02	1.30	0.876	No
469	23.45	1.36	0.48	0.88	0.93	0.691	1.04	0.662	1.02	1.30	0.877	No
470	23.50	1.36	0.48	0.88	0.93	0.691	1.04	0.662	1.02	1.30	0.877	No
471	23.55	1.37	0.49	0.88	0.93	0.691	1.04	0.663	1.02	1.30	0.877	No
472	23.60	1.37	0.49	0.88	0.93	0.692	1.04	0.663	1.02	1.30	0.877	No
473	23.65	1.37	0.49	0.88	0.93	0.692	1.04	0.663	1.02	1.30	0.877	No
474	23.70	1.38	0.49	0.89	0.93	0.692	1.04	0.663	1.02	1.30	0.877	No
475	23.75	1.38	0.49	0.89	0.93	0.692	1.04	0.664	1.02	1.30	0.878	No
476	23.80	1.38	0.49	0.89	0.93	0.693	1.04	0.664	1.02	1.30	0.879	No
477	23.85	1.38	0.49	0.89	0.93	0.693	1.04	0.664	1.02	1.30	0.879	No
478	23.90	1.39	0.50	0.89	0.93	0.693	1.04	0.664	1.02	1.30	0.880	No
479	23.95	1.39	0.50	0.89	0.93	0.693	1.04	0.665	1.01	1.30	0.881	No
480	24.00	1.39	0.50	0.89	0.93	0.694	1.04	0.665	1.01	1.30	0.881	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
481	24.05	1.40	0.50	0.89	0.92	0.694	1.04	0.665	1.01	1.30	0.882	No
482	24.10	1.40	0.50	0.90	0.92	0.694	1.04	0.665	1.01	1.30	0.883	No
483	24.15	1.40	0.50	0.90	0.92	0.694	1.04	0.666	1.01	1.30	0.883	No
484	24.20	1.40	0.51	0.90	0.92	0.695	1.04	0.666	1.01	1.30	0.883	No
485	24.25	1.41	0.51	0.90	0.92	0.695	1.04	0.666	1.01	1.30	0.883	No
486	24.30	1.41	0.51	0.90	0.92	0.695	1.04	0.666	1.01	1.30	2.000	Yes
487	24.35	1.41	0.51	0.90	0.92	0.695	1.04	0.667	1.01	1.30	2.000	Yes
488	24.40	1.42	0.51	0.90	0.92	0.696	1.04	0.667	1.01	1.30	2.000	Yes
489	24.45	1.42	0.51	0.91	0.92	0.696	1.04	0.667	1.01	1.30	2.000	Yes
490	24.50	1.42	0.51	0.91	0.92	0.696	1.04	0.667	1.01	1.30	2.000	Yes
491	24.55	1.42	0.52	0.91	0.92	0.696	1.04	0.667	1.02	1.30	2.000	Yes
492	24.60	1.43	0.52	0.91	0.92	0.696	1.04	0.668	1.02	1.30	2.000	Yes
493	24.65	1.43	0.52	0.91	0.92	0.697	1.04	0.668	1.02	1.30	2.000	Yes
494	24.70	1.43	0.52	0.91	0.92	0.697	1.04	0.668	1.02	1.30	2.000	Yes
495	24.75	1.44	0.52	0.91	0.92	0.697	1.04	0.668	1.02	1.30	2.000	Yes
496	24.80	1.44	0.52	0.92	0.92	0.697	1.04	0.668	1.02	1.30	2.000	Yes
497	24.85	1.44	0.53	0.92	0.92	0.697	1.04	0.668	1.02	1.30	2.000	Yes
498	24.90	1.45	0.53	0.92	0.92	0.698	1.04	0.669	1.02	1.30	2.000	Yes
499	24.95	1.45	0.53	0.92	0.92	0.698	1.04	0.669	1.02	1.30	2.000	Yes
500	25.00	1.45	0.53	0.92	0.92	0.698	1.04	0.669	1.02	1.30	2.000	Yes
501	25.05	1.45	0.53	0.92	0.92	0.698	1.04	0.669	1.02	1.30	2.000	Yes
502	25.10	1.46	0.53	0.92	0.92	0.698	1.04	0.669	1.02	1.30	2.000	Yes
503	25.15	1.46	0.54	0.93	0.92	0.698	1.04	0.669	1.02	1.30	2.000	Yes
504	25.20	1.46	0.54	0.93	0.92	0.699	1.04	0.670	1.02	1.30	2.000	Yes
505	25.25	1.47	0.54	0.93	0.92	0.699	1.04	0.670	1.02	1.30	0.877	No
506	25.30	1.47	0.54	0.93	0.92	0.699	1.04	0.670	1.02	1.30	0.878	No
507	25.35	1.47	0.54	0.93	0.92	0.699	1.04	0.670	1.02	1.30	0.878	No
508	25.40	1.48	0.54	0.93	0.92	0.699	1.04	0.670	1.02	1.30	0.878	No
509	25.45	1.48	0.54	0.93	0.92	0.699	1.04	0.670	1.02	1.30	0.878	No
510	25.50	1.48	0.55	0.94	0.92	0.700	1.04	0.671	1.02	1.30	0.878	No
511	25.55	1.49	0.55	0.94	0.92	0.700	1.04	0.671	1.02	1.30	0.877	No
512	25.60	1.49	0.55	0.94	0.92	0.700	1.04	0.671	1.02	1.30	0.877	No
513	25.65	1.49	0.55	0.94	0.92	0.700	1.04	0.671	1.02	1.30	0.876	No
514	25.70	1.49	0.55	0.94	0.92	0.700	1.04	0.671	1.02	1.30	0.875	No
515	25.75	1.50	0.55	0.94	0.92	0.700	1.04	0.671	1.02	1.30	0.875	No
516	25.80	1.50	0.56	0.95	0.92	0.700	1.04	0.671	1.02	1.30	0.874	No
517	25.85	1.50	0.56	0.95	0.92	0.701	1.04	0.672	1.02	1.30	0.873	No
518	25.90	1.51	0.56	0.95	0.92	0.701	1.04	0.672	1.02	1.30	0.872	No
519	25.95	1.51	0.56	0.95	0.92	0.701	1.04	0.672	1.02	1.30	0.870	No
520	26.00	1.51	0.56	0.95	0.92	0.701	1.04	0.672	1.02	1.30	0.872	No
521	26.05	1.52	0.56	0.95	0.92	0.701	1.04	0.672	1.01	1.30	0.874	No
522	26.10	1.52	0.56	0.95	0.92	0.701	1.04	0.672	1.01	1.30	0.876	No
523	26.15	1.52	0.57	0.96	0.92	0.701	1.04	0.672	1.01	1.30	0.878	No
524	26.20	1.53	0.57	0.96	0.92	0.702	1.04	0.672	1.01	1.30	0.877	No
525	26.25	1.53	0.57	0.96	0.92	0.702	1.04	0.673	1.01	1.30	0.877	No
526	26.30	1.53	0.57	0.96	0.92	0.702	1.04	0.673	1.01	1.30	2.000	Yes
527	26.35	1.53	0.57	0.96	0.91	0.702	1.04	0.673	1.01	1.30	2.000	Yes
528	26.40	1.54	0.57	0.96	0.91	0.702	1.04	0.673	1.01	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
529	26.45	1.54	0.58	0.96	0.91	0.702	1.04	0.673	1.01	1.30	2.000	Yes
530	26.50	1.54	0.58	0.97	0.91	0.702	1.04	0.673	1.01	1.30	2.000	Yes
531	26.55	1.55	0.58	0.97	0.91	0.703	1.04	0.673	1.01	1.30	2.000	Yes
532	26.60	1.55	0.58	0.97	0.91	0.703	1.04	0.673	1.01	1.30	2.000	Yes
533	26.65	1.55	0.58	0.97	0.91	0.703	1.04	0.674	1.01	1.30	2.000	Yes
534	26.70	1.56	0.58	0.97	0.91	0.703	1.04	0.674	1.01	1.30	2.000	Yes
535	26.75	1.56	0.59	0.97	0.91	0.703	1.04	0.674	1.01	1.30	2.000	Yes
536	26.80	1.56	0.59	0.98	0.91	0.703	1.04	0.674	1.01	1.30	2.000	Yes
537	26.85	1.57	0.59	0.98	0.91	0.703	1.04	0.674	1.01	1.30	2.000	Yes
538	26.90	1.57	0.59	0.98	0.91	0.703	1.04	0.674	1.01	1.30	2.000	Yes
539	26.95	1.57	0.59	0.98	0.91	0.703	1.04	0.674	1.01	1.30	2.000	Yes
540	27.00	1.57	0.59	0.98	0.91	0.704	1.04	0.674	1.01	1.30	2.000	Yes
541	27.05	1.58	0.59	0.98	0.91	0.704	1.04	0.674	1.01	1.30	2.000	Yes
542	27.10	1.58	0.60	0.98	0.91	0.704	1.04	0.675	1.01	1.30	2.000	Yes
543	27.15	1.58	0.60	0.99	0.91	0.704	1.04	0.675	1.01	1.30	0.896	No
544	27.20	1.59	0.60	0.99	0.91	0.704	1.04	0.675	1.01	1.30	0.897	No
545	27.25	1.59	0.60	0.99	0.91	0.704	1.04	0.675	1.01	1.30	0.897	No
546	27.30	1.59	0.60	0.99	0.91	0.704	1.04	0.675	1.01	1.30	0.898	No
547	27.35	1.60	0.60	0.99	0.91	0.704	1.04	0.675	1.01	1.30	0.898	No
548	27.40	1.60	0.61	0.99	0.91	0.704	1.04	0.675	1.01	1.30	0.898	No
549	27.45	1.60	0.61	1.00	0.91	0.705	1.04	0.675	1.01	1.30	0.898	No
550	27.50	1.61	0.61	1.00	0.91	0.705	1.04	0.675	1.01	1.30	0.898	No
551	27.55	1.61	0.61	1.00	0.91	0.705	1.04	0.676	1.01	1.30	0.899	No
552	27.60	1.61	0.61	1.00	0.91	0.705	1.04	0.676	1.01	1.30	0.899	No
553	27.65	1.61	0.61	1.00	0.91	0.705	1.04	0.676	1.01	1.30	0.900	No
554	27.70	1.62	0.61	1.00	0.91	0.705	1.04	0.676	1.01	1.30	0.900	No
555	27.75	1.62	0.62	1.00	0.91	0.705	1.04	0.676	1.01	1.30	0.900	No
556	27.80	1.62	0.62	1.01	0.91	0.705	1.04	0.676	1.01	1.30	0.900	No
557	27.85	1.63	0.62	1.01	0.91	0.705	1.04	0.676	1.01	1.30	0.900	No
558	27.90	1.63	0.62	1.01	0.91	0.705	1.04	0.676	1.01	1.30	0.900	No
559	27.95	1.63	0.62	1.01	0.91	0.706	1.04	0.676	1.01	1.30	0.899	No
560	28.00	1.64	0.62	1.01	0.91	0.706	1.04	0.676	1.01	1.30	0.898	No
561	28.05	1.64	0.63	1.01	0.91	0.706	1.04	0.676	1.00	1.30	0.897	No
562	28.10	1.64	0.63	1.02	0.91	0.706	1.04	0.676	1.00	1.30	0.898	No
563	28.15	1.65	0.63	1.02	0.91	0.706	1.04	0.677	1.00	1.30	0.899	No
564	28.20	1.65	0.63	1.02	0.91	0.706	1.04	0.677	1.00	1.30	0.900	No
565	28.25	1.65	0.63	1.02	0.91	0.706	1.04	0.677	1.00	1.30	0.901	No
566	28.30	1.65	0.63	1.02	0.91	0.706	1.04	0.677	1.00	1.30	0.903	No
567	28.35	1.66	0.63	1.02	0.91	0.706	1.04	0.677	1.00	1.30	0.904	No
568	28.40	1.66	0.64	1.02	0.91	0.706	1.04	0.677	1.00	1.30	0.904	No
569	28.45	1.66	0.64	1.03	0.91	0.706	1.04	0.677	1.00	1.30	0.905	No
570	28.50	1.67	0.64	1.03	0.91	0.707	1.04	0.677	1.00	1.30	0.905	No
571	28.55	1.67	0.64	1.03	0.90	0.707	1.04	0.677	1.00	1.30	0.905	No
572	28.60	1.67	0.64	1.03	0.90	0.707	1.04	0.677	1.00	1.30	0.906	No
573	28.65	1.68	0.64	1.03	0.90	0.707	1.04	0.678	1.00	1.30	0.906	No
574	28.70	1.68	0.65	1.03	0.90	0.707	1.04	0.678	1.00	1.30	0.906	No
575	28.75	1.68	0.65	1.03	0.90	0.707	1.04	0.678	1.00	1.30	0.906	No
576	28.80	1.68	0.65	1.04	0.90	0.707	1.04	0.678	1.00	1.30	0.907	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
577	28.85	1.69	0.65	1.04	0.90	0.707	1.04	0.678	1.00	1.30	0.908	No
578	28.90	1.69	0.65	1.04	0.90	0.707	1.04	0.678	1.00	1.30	0.909	No
579	28.95	1.69	0.65	1.04	0.90	0.708	1.04	0.678	1.00	1.30	0.910	No
580	29.00	1.70	0.66	1.04	0.90	0.708	1.04	0.678	1.00	1.30	0.911	No
581	29.05	1.70	0.66	1.04	0.90	0.708	1.04	0.678	1.00	1.30	0.911	No
582	29.10	1.70	0.66	1.04	0.90	0.708	1.04	0.679	1.00	1.30	0.912	No
583	29.15	1.70	0.66	1.04	0.90	0.708	1.04	0.679	1.00	1.30	0.912	No
584	29.20	1.71	0.66	1.05	0.90	0.708	1.04	0.679	1.00	1.30	0.912	No
585	29.25	1.71	0.66	1.05	0.90	0.708	1.04	0.679	1.00	1.30	0.913	No
586	29.30	1.71	0.66	1.05	0.90	0.709	1.04	0.679	1.00	1.30	0.913	No
587	29.35	1.72	0.67	1.05	0.90	0.709	1.04	0.679	1.00	1.30	0.913	No
588	29.40	1.72	0.67	1.05	0.90	0.709	1.04	0.679	1.00	1.30	0.914	No
589	29.45	1.72	0.67	1.05	0.90	0.709	1.04	0.680	1.00	1.30	0.914	No
590	29.50	1.72	0.67	1.05	0.90	0.709	1.04	0.680	1.00	1.30	0.914	No
591	29.55	1.73	0.67	1.05	0.90	0.709	1.04	0.680	1.00	1.30	0.914	No
592	29.60	1.73	0.67	1.06	0.90	0.709	1.04	0.680	1.00	1.30	0.915	No
593	29.65	1.73	0.68	1.06	0.90	0.710	1.04	0.680	1.00	1.30	0.915	No
594	29.70	1.73	0.68	1.06	0.90	0.710	1.04	0.680	1.00	1.30	0.915	No
595	29.75	1.74	0.68	1.06	0.90	0.710	1.04	0.680	1.00	1.30	0.915	No
596	29.80	1.74	0.68	1.06	0.90	0.710	1.04	0.680	1.00	1.30	0.915	No
597	29.85	1.74	0.68	1.06	0.90	0.710	1.04	0.681	1.00	1.30	0.915	No
598	29.90	1.75	0.68	1.06	0.90	0.710	1.04	0.681	1.00	1.30	0.915	No
599	29.95	1.75	0.68	1.06	0.90	0.710	1.04	0.681	1.00	1.30	0.915	No
600	30.00	1.75	0.69	1.07	0.90	0.710	1.04	0.681	1.00	1.30	0.916	No
601	30.05	1.75	0.69	1.07	0.90	0.711	1.04	0.681	1.00	1.30	0.916	No
602	30.10	1.76	0.69	1.07	0.90	0.711	1.04	0.681	1.00	1.30	0.916	No
603	30.15	1.76	0.69	1.07	0.90	0.711	1.04	0.681	1.00	1.30	0.916	No
604	30.20	1.76	0.69	1.07	0.90	0.711	1.04	0.681	1.00	1.30	0.916	No
605	30.25	1.77	0.69	1.07	0.90	0.711	1.04	0.681	1.00	1.30	0.916	No
606	30.30	1.77	0.70	1.07	0.90	0.711	1.04	0.681	1.00	1.30	0.916	No
607	30.35	1.77	0.70	1.08	0.90	0.711	1.04	0.682	1.00	1.30	0.916	No
608	30.40	1.78	0.70	1.08	0.90	0.711	1.04	0.682	1.00	1.30	0.917	No
609	30.45	1.78	0.70	1.08	0.90	0.711	1.04	0.682	1.00	1.30	0.917	No
610	30.50	1.78	0.70	1.08	0.90	0.711	1.04	0.682	1.00	1.30	2.000	Yes
611	30.55	1.78	0.70	1.08	0.90	0.711	1.04	0.682	1.00	1.30	2.000	Yes
612	30.60	1.79	0.71	1.08	0.90	0.711	1.04	0.682	1.00	1.30	2.000	Yes
613	30.65	1.79	0.71	1.08	0.90	0.711	1.04	0.682	1.00	1.30	2.000	Yes
614	30.70	1.79	0.71	1.09	0.90	0.711	1.04	0.682	1.00	1.30	2.000	Yes
615	30.75	1.80	0.71	1.09	0.89	0.711	1.04	0.682	1.00	1.30	2.000	Yes
616	30.80	1.80	0.71	1.09	0.89	0.711	1.04	0.682	1.00	1.30	2.000	Yes
617	30.85	1.80	0.71	1.09	0.89	0.711	1.04	0.682	1.00	1.30	2.000	Yes
618	30.90	1.81	0.71	1.09	0.89	0.711	1.04	0.682	1.00	1.30	2.000	Yes
619	30.95	1.81	0.72	1.09	0.89	0.711	1.04	0.682	1.00	1.30	2.000	Yes
620	31.00	1.81	0.72	1.10	0.89	0.711	1.04	0.682	0.99	1.30	2.000	Yes
621	31.05	1.82	0.72	1.10	0.89	0.711	1.04	0.682	0.99	1.30	2.000	Yes
622	31.10	1.82	0.72	1.10	0.89	0.712	1.04	0.682	0.99	1.30	2.000	Yes
623	31.15	1.82	0.72	1.10	0.89	0.712	1.04	0.682	0.99	1.30	2.000	Yes
624	31.20	1.83	0.72	1.10	0.89	0.712	1.04	0.682	0.99	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
625	31.25	1.83	0.73	1.10	0.89	0.712	1.04	0.682	0.99	1.30	0.891	No
626	31.30	1.83	0.73	1.11	0.89	0.712	1.04	0.682	0.99	1.30	0.887	No
627	31.35	1.84	0.73	1.11	0.89	0.711	1.04	0.682	0.99	1.30	0.882	No
628	31.40	1.84	0.73	1.11	0.89	0.711	1.04	0.682	0.99	1.30	0.878	No
629	31.45	1.84	0.73	1.11	0.89	0.711	1.04	0.682	0.99	1.30	0.879	No
630	31.50	1.85	0.73	1.11	0.89	0.711	1.04	0.682	0.99	1.30	0.881	No
631	31.55	1.85	0.73	1.11	0.89	0.711	1.04	0.682	0.98	1.30	0.882	No
632	31.60	1.85	0.74	1.12	0.89	0.711	1.04	0.682	0.98	1.30	0.882	No
633	31.65	1.86	0.74	1.12	0.89	0.711	1.04	0.682	0.98	1.30	0.883	No
634	31.70	1.86	0.74	1.12	0.89	0.711	1.04	0.682	0.98	1.30	0.883	No
635	31.75	1.86	0.74	1.12	0.89	0.711	1.04	0.682	0.98	1.30	0.884	No
636	31.80	1.87	0.74	1.12	0.89	0.711	1.04	0.682	0.98	1.30	0.884	No
637	31.85	1.87	0.74	1.12	0.89	0.711	1.04	0.682	0.98	1.30	0.884	No
638	31.90	1.87	0.75	1.13	0.89	0.711	1.04	0.682	0.98	1.30	0.885	No
639	31.95	1.88	0.75	1.13	0.89	0.711	1.04	0.682	0.98	1.30	0.885	No
640	32.00	1.88	0.75	1.13	0.89	0.711	1.04	0.681	0.98	1.30	0.885	No
641	32.05	1.88	0.75	1.13	0.89	0.711	1.04	0.681	0.98	1.30	0.886	No
642	32.10	1.89	0.75	1.13	0.89	0.711	1.04	0.681	0.98	1.30	0.886	No
643	32.15	1.89	0.75	1.14	0.89	0.711	1.04	0.681	0.98	1.30	0.887	No
644	32.20	1.89	0.76	1.14	0.89	0.711	1.04	0.681	0.98	1.30	0.887	No
645	32.25	1.90	0.76	1.14	0.89	0.711	1.04	0.681	0.98	1.30	0.887	No
646	32.30	1.90	0.76	1.14	0.89	0.711	1.04	0.681	0.98	1.30	0.888	No
647	32.35	1.90	0.76	1.14	0.89	0.711	1.04	0.681	0.98	1.30	0.888	No
648	32.40	1.91	0.76	1.14	0.89	0.711	1.04	0.681	0.98	1.30	0.888	No
649	32.45	1.91	0.76	1.15	0.89	0.711	1.04	0.681	0.98	1.30	0.889	No
650	32.50	1.91	0.76	1.15	0.89	0.710	1.04	0.681	0.98	1.30	0.889	No
651	32.55	1.92	0.77	1.15	0.89	0.710	1.04	0.681	0.98	1.30	0.889	No
652	32.60	1.92	0.77	1.15	0.89	0.710	1.04	0.681	0.97	1.30	0.890	No
653	32.65	1.92	0.77	1.15	0.89	0.710	1.04	0.681	0.97	1.30	0.890	No
654	32.70	1.93	0.77	1.16	0.89	0.710	1.04	0.681	0.97	1.30	0.891	No
655	32.75	1.93	0.77	1.16	0.89	0.710	1.04	0.681	0.97	1.30	0.891	No
656	32.80	1.93	0.77	1.16	0.89	0.710	1.04	0.681	0.97	1.30	0.891	No
657	32.85	1.94	0.78	1.16	0.89	0.710	1.04	0.681	0.97	1.30	0.892	No
658	32.90	1.94	0.78	1.16	0.88	0.710	1.04	0.681	0.97	1.30	0.892	No
659	32.95	1.94	0.78	1.16	0.88	0.710	1.04	0.680	0.97	1.30	0.892	No
660	33.00	1.95	0.78	1.17	0.88	0.710	1.04	0.680	0.97	1.30	0.893	No
661	33.05	1.95	0.78	1.17	0.88	0.710	1.04	0.680	0.97	1.30	0.893	No
662	33.10	1.95	0.78	1.17	0.88	0.710	1.04	0.680	0.97	1.30	0.893	No
663	33.15	1.96	0.78	1.17	0.88	0.710	1.04	0.680	0.97	1.30	0.894	No
664	33.20	1.96	0.79	1.17	0.88	0.710	1.04	0.680	0.97	1.30	0.894	No
665	33.25	1.96	0.79	1.18	0.88	0.710	1.04	0.680	0.97	1.30	0.894	No
666	33.30	1.97	0.79	1.18	0.88	0.710	1.04	0.680	0.97	1.30	0.895	No
667	33.35	1.97	0.79	1.18	0.88	0.709	1.04	0.680	0.97	1.30	0.895	No
668	33.40	1.97	0.79	1.18	0.88	0.709	1.04	0.680	0.97	1.30	0.895	No
669	33.45	1.98	0.79	1.18	0.88	0.709	1.04	0.680	0.97	1.30	0.896	No
670	33.50	1.98	0.80	1.18	0.88	0.709	1.04	0.680	0.97	1.30	0.896	No
671	33.55	1.98	0.80	1.19	0.88	0.709	1.04	0.680	0.97	1.30	0.895	No
672	33.60	1.99	0.80	1.19	0.88	0.709	1.04	0.680	0.97	1.30	0.894	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
673	33.65	1.99	0.80	1.19	0.88	0.709	1.04	0.680	0.97	1.30	0.894	No
674	33.70	1.99	0.80	1.19	0.88	0.709	1.04	0.680	0.97	1.30	0.894	No
675	33.75	2.00	0.80	1.19	0.88	0.709	1.04	0.680	0.97	1.30	0.894	No
676	33.80	2.00	0.80	1.19	0.88	0.709	1.04	0.680	0.97	1.30	0.894	No
677	33.85	2.00	0.81	1.20	0.88	0.709	1.04	0.680	0.97	1.30	0.894	No
678	33.90	2.01	0.81	1.20	0.88	0.709	1.04	0.680	0.97	1.30	0.894	No
679	33.95	2.01	0.81	1.20	0.88	0.709	1.04	0.679	0.97	1.30	0.893	No
680	34.00	2.01	0.81	1.20	0.88	0.709	1.04	0.679	0.97	1.30	0.893	No
681	34.05	2.02	0.81	1.20	0.88	0.709	1.04	0.679	0.97	1.30	0.892	No
682	34.10	2.02	0.81	1.20	0.88	0.709	1.04	0.679	0.97	1.30	0.892	No
683	34.15	2.02	0.82	1.21	0.88	0.709	1.04	0.679	0.97	1.30	0.892	No
684	34.20	2.03	0.82	1.21	0.88	0.709	1.04	0.679	0.97	1.30	0.892	No
685	34.25	2.03	0.82	1.21	0.88	0.709	1.04	0.679	0.97	1.30	0.892	No
686	34.30	2.03	0.82	1.21	0.88	0.709	1.04	0.679	0.97	1.30	0.893	No
687	34.35	2.03	0.82	1.21	0.88	0.709	1.04	0.679	0.97	1.30	0.893	No
688	34.40	2.04	0.82	1.21	0.88	0.708	1.04	0.679	0.97	1.30	0.893	No
689	34.45	2.04	0.83	1.22	0.88	0.708	1.04	0.679	0.97	1.30	0.894	No
690	34.50	2.04	0.83	1.22	0.88	0.708	1.04	0.679	0.97	1.30	0.895	No
691	34.55	2.05	0.83	1.22	0.88	0.708	1.04	0.679	0.97	1.30	0.896	No
692	34.60	2.05	0.83	1.22	0.88	0.708	1.04	0.679	0.96	1.30	0.896	No
693	34.65	2.05	0.83	1.22	0.88	0.708	1.04	0.679	0.96	1.30	0.898	No
694	34.70	2.06	0.83	1.22	0.88	0.708	1.04	0.679	0.96	1.30	0.899	No
695	34.75	2.06	0.83	1.23	0.88	0.708	1.04	0.679	0.96	1.30	0.900	No
696	34.80	2.06	0.84	1.23	0.88	0.708	1.04	0.679	0.96	1.30	0.901	No
697	34.85	2.07	0.84	1.23	0.88	0.708	1.04	0.679	0.96	1.30	0.902	No
698	34.90	2.07	0.84	1.23	0.88	0.708	1.04	0.679	0.96	1.30	0.904	No
699	34.95	2.07	0.84	1.23	0.88	0.708	1.04	0.678	0.96	1.30	0.904	No
700	35.00	2.08	0.84	1.24	0.87	0.708	1.04	0.678	0.95	1.30	0.905	No
701	35.05	2.08	0.84	1.24	0.87	0.708	1.04	0.678	0.95	1.30	0.905	No
702	35.10	2.08	0.85	1.24	0.87	0.708	1.04	0.678	0.95	1.30	0.905	No
703	35.15	2.09	0.85	1.24	0.87	0.708	1.04	0.678	0.95	1.30	0.905	No
704	35.20	2.09	0.85	1.24	0.87	0.708	1.04	0.678	0.95	1.30	0.905	No
705	35.25	2.09	0.85	1.24	0.87	0.707	1.04	0.678	0.95	1.30	0.906	No
706	35.30	2.10	0.85	1.25	0.87	0.707	1.04	0.678	0.95	1.30	0.906	No
707	35.35	2.10	0.85	1.25	0.87	0.707	1.04	0.678	0.95	1.30	0.906	No
708	35.40	2.10	0.85	1.25	0.87	0.707	1.04	0.678	0.95	1.30	0.907	No
709	35.45	2.11	0.86	1.25	0.87	0.707	1.04	0.678	0.95	1.30	0.908	No
710	35.50	2.11	0.86	1.25	0.87	0.707	1.04	0.678	0.95	1.30	0.908	No
711	35.55	2.11	0.86	1.25	0.87	0.707	1.04	0.678	0.95	1.30	0.909	No
712	35.60	2.12	0.86	1.26	0.87	0.707	1.04	0.678	0.95	1.30	0.910	No
713	35.65	2.12	0.86	1.26	0.87	0.707	1.04	0.678	0.95	1.30	0.910	No
714	35.70	2.12	0.86	1.26	0.87	0.707	1.04	0.677	0.95	1.30	0.910	No
715	35.75	2.13	0.87	1.26	0.87	0.707	1.04	0.677	0.95	1.30	0.911	No
716	35.80	2.13	0.87	1.26	0.87	0.707	1.04	0.677	0.95	1.30	0.911	No
717	35.85	2.13	0.87	1.26	0.87	0.707	1.04	0.677	0.95	1.30	0.911	No
718	35.90	2.14	0.87	1.27	0.87	0.706	1.04	0.677	0.95	1.30	0.912	No
719	35.95	2.14	0.87	1.27	0.87	0.706	1.04	0.677	0.95	1.30	0.912	No
720	36.00	2.14	0.87	1.27	0.87	0.706	1.04	0.677	0.95	1.30	0.912	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
721	36.05	2.15	0.88	1.27	0.87	0.706	1.04	0.677	0.94	1.30	0.913	No
722	36.10	2.15	0.88	1.27	0.87	0.706	1.04	0.677	0.94	1.30	0.913	No
723	36.15	2.15	0.88	1.28	0.87	0.706	1.04	0.677	0.94	1.30	0.913	No
724	36.20	2.16	0.88	1.28	0.87	0.706	1.04	0.677	0.94	1.30	0.913	No
725	36.25	2.16	0.88	1.28	0.87	0.706	1.04	0.677	0.94	1.30	0.913	No
726	36.30	2.16	0.88	1.28	0.87	0.706	1.04	0.677	0.95	1.30	0.911	No
727	36.35	2.17	0.88	1.28	0.87	0.706	1.04	0.676	0.95	1.30	0.910	No
728	36.40	2.17	0.89	1.28	0.87	0.706	1.04	0.676	0.95	1.30	0.908	No
729	36.45	2.17	0.89	1.29	0.87	0.706	1.04	0.676	0.95	1.30	0.904	No
730	36.50	2.18	0.89	1.29	0.87	0.706	1.04	0.676	0.96	1.30	0.901	No
731	36.55	2.18	0.89	1.29	0.87	0.705	1.04	0.676	0.96	1.30	0.905	No
732	36.60	2.18	0.89	1.29	0.87	0.705	1.04	0.676	0.96	1.30	0.907	No
733	36.65	2.19	0.89	1.29	0.87	0.705	1.04	0.676	0.96	1.30	0.907	No
734	36.70	2.19	0.90	1.29	0.87	0.705	1.04	0.676	0.96	1.30	0.906	No
735	36.75	2.19	0.90	1.30	0.87	0.705	1.04	0.676	0.96	1.30	0.905	No
736	36.80	2.20	0.90	1.30	0.87	0.705	1.04	0.676	0.96	1.30	2.000	Yes
737	36.85	2.20	0.90	1.30	0.87	0.705	1.04	0.676	0.96	1.30	2.000	Yes
738	36.90	2.20	0.90	1.30	0.87	0.705	1.04	0.676	0.96	1.30	2.000	Yes
739	36.95	2.21	0.90	1.30	0.87	0.705	1.04	0.676	0.96	1.30	2.000	Yes
740	37.00	2.21	0.90	1.30	0.87	0.705	1.04	0.676	0.97	1.30	2.000	Yes
741	37.05	2.21	0.91	1.31	0.87	0.705	1.04	0.676	0.97	1.30	2.000	Yes
742	37.10	2.22	0.91	1.31	0.86	0.705	1.04	0.675	0.97	1.30	2.000	Yes
743	37.15	2.22	0.91	1.31	0.86	0.705	1.04	0.675	0.97	1.30	2.000	Yes
744	37.20	2.22	0.91	1.31	0.86	0.705	1.04	0.675	0.98	1.30	2.000	Yes
745	37.25	2.22	0.91	1.31	0.86	0.705	1.04	0.675	0.98	1.30	2.000	Yes
746	37.30	2.23	0.91	1.31	0.86	0.705	1.04	0.675	0.98	1.30	2.000	Yes
747	37.35	2.23	0.92	1.32	0.86	0.705	1.04	0.675	0.98	1.30	2.000	Yes
748	37.40	2.23	0.92	1.32	0.86	0.704	1.04	0.675	0.98	1.30	2.000	Yes
749	37.45	2.24	0.92	1.32	0.86	0.704	1.04	0.675	0.98	1.30	0.925	No
750	37.50	2.24	0.92	1.32	0.86	0.704	1.04	0.675	0.98	1.30	0.926	No
751	37.55	2.24	0.92	1.32	0.86	0.704	1.04	0.675	0.98	1.30	0.926	No
752	37.60	2.25	0.92	1.32	0.86	0.704	1.04	0.675	0.98	1.30	0.926	No
753	37.65	2.25	0.93	1.32	0.86	0.704	1.04	0.675	0.98	1.30	0.926	No
754	37.70	2.25	0.93	1.33	0.86	0.704	1.04	0.675	0.98	1.30	0.926	No
755	37.75	2.26	0.93	1.33	0.86	0.704	1.04	0.675	0.98	1.30	0.926	No
756	37.80	2.26	0.93	1.33	0.86	0.704	1.04	0.675	0.98	1.30	0.926	No
757	37.85	2.26	0.93	1.33	0.86	0.704	1.04	0.675	0.98	1.30	0.925	No
758	37.90	2.26	0.93	1.33	0.86	0.704	1.04	0.675	0.98	1.30	0.926	No
759	37.95	2.27	0.93	1.33	0.86	0.704	1.04	0.675	0.98	1.30	2.000	Yes
760	38.00	2.27	0.94	1.33	0.86	0.704	1.04	0.675	0.97	1.30	2.000	Yes
761	38.05	2.27	0.94	1.34	0.86	0.704	1.04	0.675	0.97	1.30	2.000	Yes
762	38.10	2.28	0.94	1.34	0.86	0.704	1.04	0.675	0.97	1.30	2.000	Yes
763	38.15	2.28	0.94	1.34	0.86	0.704	1.04	0.675	0.97	1.30	2.000	Yes
764	38.20	2.28	0.94	1.34	0.86	0.704	1.04	0.675	0.96	1.30	2.000	Yes
765	38.25	2.29	0.94	1.34	0.86	0.704	1.04	0.675	0.96	1.30	2.000	Yes
766	38.30	2.29	0.95	1.34	0.86	0.704	1.04	0.674	0.96	1.30	2.000	Yes
767	38.35	2.29	0.95	1.35	0.86	0.704	1.04	0.674	0.96	1.30	2.000	Yes
768	38.40	2.30	0.95	1.35	0.86	0.704	1.04	0.674	0.96	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
769	38.45	2.30	0.95	1.35	0.86	0.704	1.04	0.674	0.96	1.30	0.919	No
770	38.50	2.30	0.95	1.35	0.86	0.703	1.04	0.674	0.96	1.30	0.919	No
771	38.55	2.31	0.95	1.35	0.86	0.703	1.04	0.674	0.96	1.30	0.919	No
772	38.60	2.31	0.95	1.35	0.86	0.703	1.04	0.674	0.96	1.30	0.920	No
773	38.65	2.31	0.96	1.36	0.86	0.703	1.04	0.674	0.96	1.30	0.920	No
774	38.70	2.31	0.96	1.36	0.86	0.703	1.04	0.674	0.96	1.30	0.920	No
775	38.75	2.32	0.96	1.36	0.86	0.703	1.04	0.674	0.96	1.30	0.920	No
776	38.80	2.32	0.96	1.36	0.86	0.703	1.04	0.674	0.96	1.30	0.920	No
777	38.85	2.32	0.96	1.36	0.86	0.703	1.04	0.674	0.96	1.30	0.920	No
778	38.90	2.33	0.96	1.36	0.86	0.703	1.04	0.674	0.96	1.30	0.920	No
779	38.95	2.33	0.97	1.36	0.86	0.703	1.04	0.674	0.96	1.30	0.920	No
780	39.00	2.33	0.97	1.37	0.86	0.703	1.04	0.674	0.96	1.30	0.920	No
781	39.05	2.34	0.97	1.37	0.86	0.703	1.04	0.674	0.96	1.30	0.920	No
782	39.10	2.34	0.97	1.37	0.86	0.703	1.04	0.673	0.96	1.30	2.000	Yes
783	39.15	2.34	0.97	1.37	0.85	0.703	1.04	0.673	0.96	1.30	2.000	Yes
784	39.20	2.35	0.97	1.37	0.85	0.703	1.04	0.673	0.96	1.30	2.000	Yes
785	39.25	2.35	0.98	1.37	0.85	0.702	1.04	0.673	0.96	1.30	2.000	Yes
786	39.30	2.35	0.98	1.38	0.85	0.702	1.04	0.673	0.96	1.30	2.000	Yes
787	39.35	2.36	0.98	1.38	0.85	0.702	1.04	0.673	0.96	1.30	2.000	Yes
788	39.40	2.36	0.98	1.38	0.85	0.702	1.04	0.673	0.96	1.30	2.000	Yes
789	39.45	2.36	0.98	1.38	0.85	0.702	1.04	0.673	0.96	1.30	2.000	Yes
790	39.50	2.37	0.98	1.38	0.85	0.702	1.04	0.673	0.97	1.30	2.000	Yes
791	39.55	2.37	0.98	1.38	0.85	0.702	1.04	0.673	0.97	1.30	2.000	Yes
792	39.60	2.37	0.99	1.39	0.85	0.702	1.04	0.673	0.97	1.30	2.000	Yes
793	39.65	2.38	0.99	1.39	0.85	0.702	1.04	0.673	0.97	1.30	0.925	No
794	39.70	2.38	0.99	1.39	0.85	0.702	1.04	0.673	0.97	1.30	2.000	Yes
795	39.75	2.38	0.99	1.39	0.85	0.702	1.04	0.673	0.97	1.30	2.000	Yes
796	39.80	2.38	0.99	1.39	0.85	0.702	1.04	0.672	0.97	1.30	2.000	Yes
797	39.85	2.39	0.99	1.39	0.85	0.701	1.04	0.672	0.97	1.30	2.000	Yes
798	39.90	2.39	1.00	1.40	0.85	0.701	1.04	0.672	0.96	1.30	2.000	Yes
799	39.95	2.39	1.00	1.40	0.85	0.701	1.04	0.672	0.96	1.30	2.000	Yes
800	40.00	2.40	1.00	1.40	0.85	0.701	1.04	0.672	0.96	1.30	2.000	Yes
801	40.05	2.40	1.00	1.40	0.85	0.701	1.04	0.672	0.96	1.30	2.000	Yes
802	40.10	2.40	1.00	1.40	0.85	0.701	1.04	0.672	0.96	1.30	2.000	Yes
803	40.15	2.41	1.00	1.40	0.85	0.701	1.04	0.672	0.96	1.30	0.924	No
804	40.20	2.41	1.00	1.41	0.85	0.701	1.04	0.672	0.96	1.30	0.924	No
805	40.25	2.41	1.01	1.41	0.85	0.701	1.04	0.672	0.96	1.30	0.925	No
806	40.30	2.42	1.01	1.41	0.85	0.701	1.04	0.672	0.96	1.30	0.925	No
807	40.35	2.42	1.01	1.41	0.85	0.701	1.04	0.672	0.96	1.30	0.925	No
808	40.40	2.42	1.01	1.41	0.85	0.701	1.04	0.672	0.96	1.30	0.925	No
809	40.45	2.43	1.01	1.41	0.85	0.701	1.04	0.671	0.96	1.30	0.925	No
810	40.50	2.43	1.01	1.41	0.85	0.701	1.04	0.671	0.96	1.30	0.925	No
811	40.55	2.43	1.02	1.42	0.85	0.700	1.04	0.671	0.96	1.30	0.925	No
812	40.60	2.43	1.02	1.42	0.85	0.700	1.04	0.671	0.96	1.30	2.000	Yes
813	40.65	2.44	1.02	1.42	0.85	0.700	1.04	0.671	0.96	1.30	2.000	Yes
814	40.70	2.44	1.02	1.42	0.85	0.700	1.04	0.671	0.96	1.30	2.000	Yes
815	40.75	2.44	1.02	1.42	0.85	0.700	1.04	0.671	0.96	1.30	2.000	Yes
816	40.80	2.45	1.02	1.42	0.85	0.700	1.04	0.671	0.97	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
817	40.85	2.45	1.02	1.43	0.85	0.700	1.04	0.671	0.97	1.30	2.000	Yes
818	40.90	2.45	1.03	1.43	0.85	0.700	1.04	0.671	0.97	1.30	2.000	Yes
819	40.95	2.46	1.03	1.43	0.85	0.700	1.04	0.671	0.97	1.30	2.000	Yes
820	41.00	2.46	1.03	1.43	0.85	0.700	1.04	0.671	0.97	1.30	2.000	Yes
821	41.05	2.46	1.03	1.43	0.85	0.700	1.04	0.671	0.96	1.30	2.000	Yes
822	41.10	2.47	1.03	1.43	0.85	0.700	1.04	0.671	0.96	1.30	2.000	Yes
823	41.15	2.47	1.03	1.43	0.85	0.700	1.04	0.670	0.96	1.30	2.000	Yes
824	41.20	2.47	1.04	1.44	0.84	0.699	1.04	0.670	0.96	1.30	2.000	Yes
825	41.25	2.48	1.04	1.44	0.84	0.699	1.04	0.670	0.96	1.30	2.000	Yes
826	41.30	2.48	1.04	1.44	0.84	0.699	1.04	0.670	0.96	1.30	2.000	Yes
827	41.35	2.48	1.04	1.44	0.84	0.699	1.04	0.670	0.95	1.30	2.000	Yes
828	41.40	2.48	1.04	1.44	0.84	0.699	1.04	0.670	0.95	1.30	2.000	Yes
829	41.45	2.49	1.04	1.44	0.84	0.699	1.04	0.670	0.95	1.30	2.000	Yes
830	41.50	2.49	1.05	1.45	0.84	0.699	1.04	0.670	0.95	1.30	2.000	Yes
831	41.55	2.49	1.05	1.45	0.84	0.699	1.04	0.670	0.95	1.30	2.000	Yes
832	41.60	2.50	1.05	1.45	0.84	0.699	1.04	0.670	0.95	1.30	0.924	No
833	41.65	2.50	1.05	1.45	0.84	0.699	1.04	0.670	0.95	1.30	2.000	Yes
834	41.70	2.50	1.05	1.45	0.84	0.699	1.04	0.670	0.95	1.30	2.000	Yes
835	41.75	2.51	1.05	1.45	0.84	0.699	1.04	0.670	0.95	1.30	2.000	Yes
836	41.80	2.51	1.05	1.46	0.84	0.698	1.04	0.669	0.96	1.30	2.000	Yes
837	41.85	2.51	1.06	1.46	0.84	0.698	1.04	0.669	0.96	1.30	2.000	Yes
838	41.90	2.52	1.06	1.46	0.84	0.698	1.04	0.669	0.96	1.30	2.000	Yes
839	41.95	2.52	1.06	1.46	0.84	0.698	1.04	0.669	0.96	1.30	2.000	Yes
840	42.00	2.52	1.06	1.46	0.84	0.698	1.04	0.669	0.96	1.30	2.000	Yes
841	42.05	2.53	1.06	1.46	0.84	0.698	1.04	0.669	0.96	1.30	2.000	Yes
842	42.10	2.53	1.06	1.46	0.84	0.698	1.04	0.669	0.96	1.30	2.000	Yes
843	42.15	2.53	1.07	1.47	0.84	0.698	1.04	0.669	0.96	1.30	2.000	Yes
844	42.20	2.53	1.07	1.47	0.84	0.698	1.04	0.669	0.96	1.30	2.000	Yes
845	42.25	2.54	1.07	1.47	0.84	0.698	1.04	0.669	0.96	1.30	0.927	No
846	42.30	2.54	1.07	1.47	0.84	0.698	1.04	0.669	0.96	1.30	0.927	No
847	42.35	2.54	1.07	1.47	0.84	0.698	1.04	0.669	0.96	1.30	0.927	No
848	42.40	2.55	1.07	1.47	0.84	0.697	1.04	0.669	0.96	1.30	0.927	No
849	42.45	2.55	1.07	1.48	0.84	0.697	1.04	0.668	0.96	1.30	0.927	No
850	42.50	2.55	1.08	1.48	0.84	0.697	1.04	0.668	0.96	1.30	0.927	No
851	42.55	2.56	1.08	1.48	0.84	0.697	1.04	0.668	0.96	1.30	0.927	No
852	42.60	2.56	1.08	1.48	0.84	0.697	1.04	0.668	0.96	1.30	0.927	No
853	42.65	2.56	1.08	1.48	0.84	0.697	1.04	0.668	0.96	1.30	0.927	No
854	42.70	2.57	1.08	1.48	0.84	0.697	1.04	0.668	0.96	1.30	0.927	No
855	42.75	2.57	1.08	1.48	0.84	0.697	1.04	0.668	0.96	1.30	0.927	No
856	42.80	2.57	1.09	1.49	0.84	0.697	1.04	0.668	0.96	1.30	0.927	No
857	42.85	2.58	1.09	1.49	0.84	0.697	1.04	0.668	0.96	1.30	2.000	Yes
858	42.90	2.58	1.09	1.49	0.84	0.697	1.04	0.668	0.96	1.30	2.000	Yes
859	42.95	2.58	1.09	1.49	0.84	0.696	1.04	0.668	0.96	1.30	2.000	Yes
860	43.00	2.58	1.09	1.49	0.84	0.696	1.04	0.667	0.96	1.30	2.000	Yes
861	43.05	2.59	1.09	1.49	0.84	0.696	1.04	0.667	0.96	1.30	2.000	Yes
862	43.10	2.59	1.10	1.50	0.84	0.696	1.04	0.667	0.95	1.30	2.000	Yes
863	43.15	2.59	1.10	1.50	0.84	0.696	1.04	0.667	0.95	1.30	2.000	Yes
864	43.20	2.60	1.10	1.50	0.84	0.696	1.04	0.667	0.95	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
865	43.25	2.60	1.10	1.50	0.83	0.696	1.04	0.667	0.95	1.30	2.000	Yes
866	43.30	2.60	1.10	1.50	0.83	0.696	1.04	0.667	0.95	1.30	0.926	No
867	43.35	2.61	1.10	1.50	0.83	0.696	1.04	0.667	0.95	1.30	2.000	Yes
868	43.40	2.61	1.10	1.51	0.83	0.696	1.04	0.667	0.95	1.30	2.000	Yes
869	43.45	2.61	1.11	1.51	0.83	0.695	1.04	0.667	0.95	1.30	2.000	Yes
870	43.50	2.62	1.11	1.51	0.83	0.695	1.04	0.666	0.95	1.30	2.000	Yes
871	43.55	2.62	1.11	1.51	0.83	0.695	1.04	0.666	0.95	1.30	2.000	Yes
872	43.60	2.62	1.11	1.51	0.83	0.695	1.04	0.666	0.95	1.30	2.000	Yes
873	43.65	2.63	1.11	1.51	0.83	0.695	1.04	0.666	0.95	1.30	2.000	Yes
874	43.70	2.63	1.11	1.52	0.83	0.695	1.04	0.666	0.95	1.30	0.926	No
875	43.75	2.63	1.12	1.52	0.83	0.695	1.04	0.666	0.95	1.30	2.000	Yes
876	43.80	2.64	1.12	1.52	0.83	0.695	1.04	0.666	0.95	1.30	2.000	Yes
877	43.85	2.64	1.12	1.52	0.83	0.695	1.04	0.666	0.95	1.30	2.000	Yes
878	43.90	2.64	1.12	1.52	0.83	0.694	1.04	0.666	0.94	1.30	2.000	Yes
879	43.95	2.65	1.12	1.52	0.83	0.694	1.04	0.665	0.94	1.30	2.000	Yes
880	44.00	2.65	1.12	1.53	0.83	0.694	1.04	0.665	0.94	1.30	2.000	Yes
881	44.05	2.65	1.12	1.53	0.83	0.694	1.04	0.665	0.93	1.30	2.000	Yes
882	44.10	2.66	1.13	1.53	0.83	0.694	1.04	0.665	0.92	1.30	2.000	Yes
883	44.15	2.66	1.13	1.53	0.83	0.694	1.04	0.665	0.91	1.30	2.000	Yes
884	44.20	2.66	1.13	1.53	0.83	0.694	1.04	0.665	0.90	1.30	2.000	Yes
885	44.25	2.67	1.13	1.53	0.83	0.694	1.04	0.665	0.90	1.30	2.000	Yes
886	44.30	2.67	1.13	1.54	0.83	0.693	1.04	0.665	0.89	1.30	2.000	Yes
887	44.35	2.67	1.13	1.54	0.83	0.693	1.04	0.664	0.89	1.30	2.000	Yes
888	44.40	2.67	1.14	1.54	0.83	0.693	1.04	0.664	0.89	1.30	0.953	No
889	44.45	2.68	1.14	1.54	0.83	0.693	1.04	0.664	0.89	1.30	0.954	No
890	44.50	2.68	1.14	1.54	0.83	0.693	1.04	0.664	0.89	1.30	0.954	No
891	44.55	2.68	1.14	1.54	0.83	0.693	1.04	0.664	0.89	1.30	0.954	No
892	44.60	2.69	1.14	1.55	0.83	0.693	1.04	0.664	0.89	1.30	0.954	No
893	44.65	2.69	1.14	1.55	0.83	0.692	1.04	0.664	0.89	1.30	0.954	No
894	44.70	2.70	1.15	1.55	0.83	0.692	1.04	0.664	0.89	1.30	0.954	No
895	44.75	2.70	1.15	1.55	0.83	0.692	1.04	0.663	0.89	1.30	0.955	No
896	44.80	2.70	1.15	1.55	0.83	0.692	1.04	0.663	0.88	1.30	0.955	No
897	44.85	2.71	1.15	1.56	0.83	0.692	1.04	0.663	0.88	1.30	0.955	No
898	44.90	2.71	1.15	1.56	0.83	0.692	1.04	0.663	0.88	1.30	0.955	No
899	44.95	2.71	1.15	1.56	0.83	0.692	1.04	0.663	0.88	1.30	0.955	No
900	45.00	2.72	1.15	1.56	0.83	0.691	1.04	0.663	0.88	1.30	0.956	No
901	45.05	2.72	1.16	1.56	0.83	0.691	1.04	0.663	0.88	1.30	0.956	No
902	45.10	2.72	1.16	1.56	0.83	0.691	1.04	0.662	0.88	1.30	0.956	No
903	45.15	2.73	1.16	1.57	0.83	0.691	1.04	0.662	0.88	1.30	0.956	No
904	45.20	2.73	1.16	1.57	0.83	0.691	1.04	0.662	0.88	1.30	0.956	No
905	45.25	2.73	1.16	1.57	0.83	0.691	1.04	0.662	0.88	1.30	0.956	No
906	45.30	2.74	1.16	1.57	0.82	0.691	1.04	0.662	0.88	1.30	0.957	No
907	45.35	2.74	1.17	1.57	0.82	0.690	1.04	0.662	0.88	1.30	0.957	No
908	45.40	2.74	1.17	1.57	0.82	0.690	1.04	0.662	0.88	1.30	0.957	No
909	45.45	2.75	1.17	1.58	0.82	0.690	1.04	0.661	0.88	1.30	0.957	No
910	45.50	2.75	1.17	1.58	0.82	0.690	1.04	0.661	0.88	1.30	0.957	No
911	45.55	2.75	1.17	1.58	0.82	0.690	1.04	0.661	0.88	1.30	0.957	No
912	45.60	2.76	1.17	1.58	0.82	0.690	1.04	0.661	0.88	1.30	0.958	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
913	45.65	2.76	1.17	1.58	0.82	0.690	1.04	0.661	0.88	1.30	0.958	No
914	45.70	2.76	1.18	1.59	0.82	0.689	1.04	0.661	0.88	1.30	0.958	No
915	45.75	2.77	1.18	1.59	0.82	0.689	1.04	0.661	0.88	1.30	0.958	No
916	45.80	2.77	1.18	1.59	0.82	0.689	1.04	0.661	0.88	1.30	0.958	No
917	45.85	2.77	1.18	1.59	0.82	0.689	1.04	0.660	0.88	1.30	0.958	No
918	45.90	2.78	1.18	1.59	0.82	0.689	1.04	0.660	0.88	1.30	0.959	No
919	45.95	2.78	1.18	1.59	0.82	0.689	1.04	0.660	0.88	1.30	0.959	No
920	46.00	2.78	1.19	1.60	0.82	0.689	1.04	0.660	0.88	1.30	0.959	No
921	46.05	2.79	1.19	1.60	0.82	0.688	1.04	0.660	0.88	1.30	0.959	No
922	46.10	2.79	1.19	1.60	0.82	0.688	1.04	0.660	0.88	1.30	0.954	No
923	46.15	2.79	1.19	1.60	0.82	0.688	1.04	0.660	0.89	1.30	0.943	No
924	46.20	2.79	1.19	1.60	0.82	0.688	1.04	0.659	0.90	1.30	0.934	No
925	46.25	2.80	1.19	1.60	0.82	0.688	1.04	0.659	0.90	1.30	0.928	No
926	46.30	2.80	1.19	1.61	0.82	0.688	1.04	0.659	0.91	1.30	0.927	No
927	46.35	2.80	1.20	1.61	0.82	0.688	1.04	0.659	0.91	1.30	0.927	No
928	46.40	2.81	1.20	1.61	0.82	0.687	1.04	0.659	0.91	1.30	0.927	No
929	46.45	2.81	1.20	1.61	0.82	0.687	1.04	0.659	0.91	1.30	0.927	No
930	46.50	2.81	1.20	1.61	0.82	0.687	1.04	0.659	0.91	1.30	0.927	No
931	46.55	2.82	1.20	1.61	0.82	0.687	1.04	0.659	0.90	1.30	0.927	No
932	46.60	2.82	1.20	1.62	0.82	0.687	1.04	0.658	0.90	1.30	0.930	No
933	46.65	2.82	1.21	1.62	0.82	0.687	1.04	0.658	0.90	1.30	0.932	No
934	46.70	2.83	1.21	1.62	0.82	0.687	1.04	0.658	0.90	1.30	0.934	No
935	46.75	2.83	1.21	1.62	0.82	0.687	1.04	0.658	0.90	1.30	0.934	No
936	46.80	2.83	1.21	1.62	0.82	0.686	1.04	0.658	0.90	1.30	0.934	No
937	46.85	2.84	1.21	1.63	0.82	0.686	1.04	0.658	0.90	1.30	0.934	No
938	46.90	2.84	1.21	1.63	0.82	0.686	1.04	0.658	0.90	1.30	0.934	No
939	46.95	2.84	1.22	1.63	0.82	0.686	1.04	0.658	0.90	1.30	0.933	No
940	47.00	2.85	1.22	1.63	0.82	0.686	1.04	0.657	0.90	1.30	0.931	No
941	47.05	2.85	1.22	1.63	0.82	0.686	1.04	0.657	0.90	1.30	0.928	No
942	47.10	2.85	1.22	1.63	0.82	0.686	1.04	0.657	0.91	1.30	0.927	No
943	47.15	2.86	1.22	1.63	0.82	0.686	1.04	0.657	0.92	1.30	0.926	No
944	47.20	2.86	1.22	1.64	0.82	0.685	1.04	0.657	0.92	1.30	2.000	Yes
945	47.25	2.86	1.22	1.64	0.82	0.685	1.04	0.657	0.93	1.30	2.000	Yes
946	47.30	2.87	1.23	1.64	0.82	0.685	1.04	0.657	0.93	1.30	2.000	Yes
947	47.35	2.87	1.23	1.64	0.81	0.685	1.04	0.657	0.93	1.30	2.000	Yes
948	47.40	2.87	1.23	1.64	0.81	0.685	1.04	0.657	0.93	1.30	2.000	Yes
949	47.45	2.88	1.23	1.64	0.81	0.685	1.04	0.656	0.92	1.30	2.000	Yes
950	47.50	2.88	1.23	1.65	0.81	0.685	1.04	0.656	0.92	1.30	2.000	Yes
951	47.55	2.88	1.23	1.65	0.81	0.685	1.04	0.656	0.92	1.30	2.000	Yes
952	47.60	2.88	1.24	1.65	0.81	0.684	1.04	0.656	0.93	1.30	2.000	Yes
953	47.65	2.89	1.24	1.65	0.81	0.684	1.04	0.656	0.93	1.30	2.000	Yes
954	47.70	2.89	1.24	1.65	0.81	0.684	1.04	0.656	0.93	1.30	2.000	Yes
955	47.75	2.89	1.24	1.65	0.81	0.684	1.04	0.656	0.93	1.30	2.000	Yes
956	47.80	2.90	1.24	1.66	0.81	0.684	1.04	0.656	0.93	1.30	2.000	Yes
957	47.85	2.90	1.24	1.66	0.81	0.684	1.04	0.655	0.93	1.30	2.000	Yes
958	47.90	2.90	1.24	1.66	0.81	0.684	1.04	0.655	0.93	1.30	2.000	Yes
959	47.95	2.91	1.25	1.66	0.81	0.684	1.04	0.655	0.93	1.30	0.924	No
960	48.00	2.91	1.25	1.66	0.81	0.683	1.04	0.655	0.93	1.30	0.924	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
961	48.05	2.91	1.25	1.66	0.81	0.683	1.04	0.655	0.92	1.30	0.925	No
962	48.10	2.92	1.25	1.67	0.81	0.683	1.04	0.655	0.92	1.30	0.925	No
963	48.15	2.92	1.25	1.67	0.81	0.683	1.04	0.655	0.92	1.30	0.925	No
964	48.20	2.92	1.25	1.67	0.81	0.683	1.04	0.654	0.92	1.30	0.925	No
965	48.25	2.93	1.26	1.67	0.81	0.683	1.04	0.654	0.93	1.30	0.924	No
966	48.30	2.93	1.26	1.67	0.81	0.682	1.04	0.654	0.93	1.30	0.924	No
967	48.35	2.93	1.26	1.68	0.81	0.682	1.04	0.654	0.93	1.30	0.923	No
968	48.40	2.94	1.26	1.68	0.81	0.682	1.04	0.654	0.94	1.30	0.923	No
969	48.45	2.94	1.26	1.68	0.81	0.682	1.04	0.654	0.94	1.30	0.922	No
970	48.50	2.94	1.26	1.68	0.81	0.682	1.04	0.654	0.94	1.30	0.922	No
971	48.55	2.95	1.27	1.68	0.81	0.682	1.04	0.653	0.94	1.30	0.922	No
972	48.60	2.95	1.27	1.68	0.81	0.682	1.04	0.653	0.94	1.30	2.000	Yes
973	48.65	2.95	1.27	1.69	0.81	0.681	1.04	0.653	0.94	1.30	2.000	Yes
974	48.70	2.96	1.27	1.69	0.81	0.681	1.04	0.653	0.94	1.30	2.000	Yes
975	48.75	2.96	1.27	1.69	0.81	0.681	1.04	0.653	0.93	1.30	2.000	Yes
976	48.80	2.96	1.27	1.69	0.81	0.681	1.04	0.653	0.93	1.30	2.000	Yes
977	48.85	2.97	1.27	1.69	0.81	0.681	1.04	0.653	0.92	1.30	2.000	Yes
978	48.90	2.97	1.28	1.69	0.81	0.681	1.04	0.652	0.92	1.30	2.000	Yes
979	48.95	2.97	1.28	1.70	0.81	0.681	1.04	0.652	0.92	1.30	2.000	Yes
980	49.00	2.98	1.28	1.70	0.81	0.680	1.04	0.652	0.92	1.30	2.000	Yes
981	49.05	2.98	1.28	1.70	0.81	0.680	1.04	0.652	0.92	1.30	0.925	No
982	49.10	2.98	1.28	1.70	0.81	0.680	1.04	0.652	0.92	1.30	2.000	Yes
983	49.15	2.99	1.28	1.70	0.81	0.680	1.04	0.652	0.92	1.30	2.000	Yes
984	49.20	2.99	1.29	1.70	0.81	0.680	1.04	0.652	0.92	1.30	2.000	Yes
985	49.25	2.99	1.29	1.71	0.81	0.680	1.04	0.652	0.93	1.30	2.000	Yes
986	49.30	3.00	1.29	1.71	0.81	0.680	1.04	0.651	0.93	1.30	2.000	Yes
987	49.35	3.00	1.29	1.71	0.81	0.679	1.04	0.651	0.93	1.30	2.000	Yes
988	49.40	3.00	1.29	1.71	0.80	0.679	1.04	0.651	0.92	1.30	0.923	No
989	49.45	3.01	1.29	1.71	0.80	0.679	1.04	0.651	0.92	1.30	2.000	Yes
990	49.50	3.01	1.29	1.71	0.80	0.679	1.04	0.651	0.92	1.30	2.000	Yes
991	49.55	3.01	1.30	1.72	0.80	0.679	1.04	0.651	0.92	1.30	2.000	Yes
992	49.60	3.02	1.30	1.72	0.80	0.679	1.04	0.651	0.92	1.30	2.000	Yes
993	49.65	3.02	1.30	1.72	0.80	0.679	1.04	0.650	0.92	1.30	2.000	Yes
994	49.70	3.02	1.30	1.72	0.80	0.678	1.04	0.650	0.92	1.30	2.000	Yes
995	49.75	3.03	1.30	1.72	0.80	0.678	1.04	0.650	0.92	1.30	0.924	No
996	49.80	3.03	1.30	1.73	0.80	0.678	1.04	0.650	0.92	1.30	0.924	No
997	49.85	3.03	1.31	1.73	0.80	0.678	1.04	0.650	0.92	1.30	0.924	No
998	49.90	3.04	1.31	1.73	0.80	0.678	1.04	0.650	0.92	1.30	0.923	No

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
 σ_v : Total overburden pressure at test point (tsf)
 u_0 : Water pressure at test point (tsf)
 σ_v' : Effective overburden pressure based on GWT during earthquake (tsf)
 r_d : Nonlinear shear mass factor
 CSR: Cyclic Stress Ratio
 MSF: Magnitude Scaling Factor
 CSR_{eq} : CSR adjusted for M=7.5
 K_σ : Effective overburden stress factor
 CSR*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1	0.05	44.98	5.43	1.78	0.56	1.70	74.88	0.27	75.15	4.000	No	No	2.00
2	0.10	42.18	8.00	1.81	0.57	1.70	67.04	2.71	69.75	4.000	No	No	2.00
3	0.15	38.22	13.11	1.88	0.56	1.70	61.37	14.69	76.06	4.000	No	No	2.00
4	0.20	36.54	19.26	1.95	0.53	1.70	55.78	29.46	85.24	4.000	No	No	2.00
5	0.25	37.48	23.13	2.00	0.51	1.70	58.97	37.44	96.41	4.000	No	No	2.00
6	0.30	41.67	24.22	2.02	0.48	1.70	65.90	40.44	106.34	4.000	No	No	2.00
7	0.35	47.15	24.61	2.02	0.46	1.70	75.94	42.80	118.74	4.000	No	No	2.00
8	0.40	53.76	24.29	2.02	0.44	1.70	85.40	43.84	129.24	4.000	No	No	2.00
9	0.45	60.29	24.22	2.02	0.41	1.70	97.75	45.81	143.56	4.000	No	No	2.00
10	0.50	67.27	23.69	2.01	0.40	1.70	107.39	46.37	153.77	4.000	No	No	2.00
11	0.55	73.74	23.36	2.00	0.38	1.70	119.02	47.59	166.61	4.000	No	No	2.00
12	0.60	80.33	22.77	2.00	0.36	1.70	128.94	47.87	176.81	4.000	No	No	2.00
13	0.65	85.91	22.41	1.99	0.35	1.70	139.11	48.60	187.71	4.000	No	No	2.00
14	0.70	90.35	22.21	1.99	0.34	1.70	145.90	49.16	195.06	4.000	No	No	2.00
15	0.75	93.16	22.27	1.99	0.33	1.70	150.37	49.99	200.36	4.000	No	No	2.00
16	0.80	94.80	22.52	1.99	0.32	1.70	152.65	50.99	203.64	4.000	No	No	2.00
17	0.85	95.69	22.75	2.00	0.32	1.70	153.77	51.74	205.51	4.000	No	No	2.00
18	0.90	96.15	22.94	2.00	0.32	1.70	154.65	52.35	207.00	4.000	No	No	2.00
19	0.95	96.40	22.79	2.00	0.32	1.70	154.87	52.02	206.89	4.000	No	No	2.00
20	1.00	96.43	22.43	1.99	0.32	1.70	155.00	51.13	206.13	4.000	No	No	2.00
21	1.05	96.33	21.73	1.98	0.32	1.70	154.79	49.27	204.06	4.000	No	No	2.00
22	1.10	96.00	21.06	1.98	0.33	1.70	154.36	47.38	201.74	4.000	No	No	2.00
23	1.15	95.46	20.44	1.97	0.33	1.70	153.43	45.50	198.93	4.000	No	No	2.00
24	1.20	94.69	20.33	1.97	0.33	1.70	152.19	45.01	197.20	4.000	No	No	2.00
25	1.25	93.46	20.68	1.97	0.33	1.70	150.67	45.79	196.46	4.000	No	No	2.00
26	1.30	91.81	21.62	1.98	0.34	1.70	147.50	47.87	195.37	4.000	Yes	No	2.00
27	1.35	89.30	22.95	2.00	0.34	1.70	144.23	50.72	194.95	4.000	Yes	No	2.00
28	1.40	86.36	24.73	2.02	0.34	1.70	138.57	53.78	192.35	4.000	Yes	No	2.00
29	1.45	82.64	27.06	2.05	0.34	1.70	133.31	57.42	190.72	4.000	Yes	No	2.00
30	1.50	78.19	30.01	2.09	0.35	1.70	126.30	60.91	187.21	4.000	Yes	No	2.00
31	1.55	72.82	33.74	2.13	0.36	1.70	117.14	63.92	181.06	4.000	Yes	No	2.00
32	1.60	66.36	38.09	2.19	0.37	1.70	107.44	66.20	173.63	4.000	Yes	No	2.00
33	1.65	59.88	42.92	2.25	0.38	1.70	95.17	67.04	162.20	4.000	Yes	No	2.00
34	1.70	53.34	47.88	2.31	0.40	1.70	85.88	67.67	153.55	4.000	Yes	No	2.00
35	1.75	48.05	52.65	2.37	0.41	1.70	75.93	67.30	143.22	4.000	Yes	No	2.00
36	1.80	43.36	56.91	2.42	0.43	1.70	69.67	67.22	136.89	4.000	Yes	No	2.00
37	1.85	40.03	60.27	2.47	0.44	1.70	63.30	66.54	129.84	4.000	Yes	No	2.00
38	1.90	37.71	62.18	2.49	0.45	1.70	59.88	66.13	126.01	4.000	Yes	No	2.00
39	1.95	37.98	61.62	2.48	0.45	1.70	58.46	65.58	124.04	4.000	Yes	No	2.00
40	2.00	40.86	58.01	2.44	0.44	1.70	64.63	66.20	130.84	4.000	Yes	No	2.00
41	2.05	47.34	51.70	2.36	0.42	1.70	73.74	66.30	140.05	4.000	Yes	No	2.00
42	2.10	55.46	43.97	2.26	0.39	1.70	89.67	66.36	156.03	4.000	Yes	No	2.00
43	2.15	64.79	36.07	2.16	0.38	1.70	103.79	63.43	167.23	4.000	Yes	No	2.00
44	2.20	73.80	28.34	2.07	0.36	1.70	118.69	56.80	175.50	4.000	Yes	No	2.00
45	2.25	81.99	21.47	1.98	0.36	1.70	133.13	45.36	178.49	4.000	Yes	No	2.00
46	2.30	88.53	15.82	1.91	0.37	1.70	143.26	29.59	172.85	4.000	Yes	No	2.00
47	2.35	92.37	11.96	1.86	0.38	1.70	150.23	15.97	166.20	4.000	Yes	No	2.00
48	2.40	93.93	10.29	1.84	0.38	1.70	151.66	10.12	161.78	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
49	2.45	93.87	10.20	1.84	0.39	1.70	150.77	9.78	160.55	4.000	No	No	2.00
50	2.50	93.40	11.17	1.85	0.38	1.70	149.95	13.10	163.05	4.000	No	No	2.00
51	2.55	93.28	12.26	1.87	0.38	1.70	149.38	17.01	166.39	4.000	No	No	2.00
52	2.60	93.55	13.13	1.88	0.37	1.70	150.20	20.33	170.53	4.000	No	No	2.00
53	2.65	94.32	13.41	1.88	0.37	1.70	151.23	21.43	172.66	4.000	No	No	2.00
54	2.70	95.21	13.16	1.88	0.37	1.70	153.09	20.62	173.71	4.000	No	No	2.00
55	2.75	96.20	12.55	1.87	0.37	1.70	154.49	18.40	172.90	4.000	No	No	2.00
56	2.80	97.04	11.85	1.86	0.37	1.70	155.99	15.82	171.81	4.000	No	No	2.00
57	2.85	97.77	11.16	1.85	0.37	1.70	157.14	13.34	170.48	4.000	No	No	2.00
58	2.90	98.32	10.55	1.84	0.37	1.70	158.02	11.19	169.21	4.000	No	No	2.00
59	2.95	98.61	10.06	1.84	0.37	1.70	158.65	9.56	168.21	4.000	No	No	2.00
60	3.00	98.60	9.82	1.84	0.38	1.70	158.56	8.75	167.30	4.000	No	No	2.00
61	3.05	98.15	9.80	1.84	0.38	1.70	157.95	8.69	166.64	4.000	No	No	2.00
62	3.10	97.34	9.98	1.84	0.38	1.70	156.48	9.22	165.70	4.000	No	No	2.00
63	3.15	95.79	10.37	1.84	0.38	1.70	154.67	10.47	165.14	4.000	No	No	2.00
64	3.20	93.66	10.92	1.85	0.38	1.70	150.47	12.22	162.69	4.000	No	No	2.00
65	3.25	90.49	11.77	1.86	0.39	1.70	146.22	15.06	161.27	4.000	No	No	2.00
66	3.30	87.03	12.73	1.87	0.39	1.70	139.37	18.18	157.55	4.000	No	No	2.00
67	3.35	83.13	13.87	1.89	0.39	1.70	133.82	21.91	155.73	4.000	No	No	2.00
68	3.40	79.38	15.02	1.90	0.40	1.70	127.43	25.43	152.87	4.000	No	No	2.00
69	3.45	75.65	16.24	1.92	0.40	1.70	121.30	28.88	150.18	4.000	No	No	2.00
70	3.50	72.09	17.46	1.93	0.41	1.70	115.83	32.08	147.91	4.000	No	No	2.00
71	3.55	68.88	18.63	1.95	0.41	1.70	110.28	34.76	145.04	4.000	No	No	2.00
72	3.60	65.66	19.86	1.96	0.41	1.70	105.83	37.45	143.27	4.000	No	No	2.00
73	3.65	62.53	21.13	1.98	0.42	1.70	100.31	39.74	140.04	4.000	No	No	2.00
74	3.70	59.19	22.69	2.00	0.42	1.70	95.19	42.37	137.56	4.000	No	No	2.00
75	3.75	56.15	24.38	2.02	0.43	1.70	89.77	44.75	134.52	4.000	No	No	2.00
76	3.80	53.48	26.30	2.04	0.43	1.70	85.65	47.31	132.96	4.000	No	No	2.00
77	3.85	51.15	28.19	2.06	0.43	1.70	82.30	49.53	131.82	4.000	No	No	2.00
78	3.90	49.13	29.97	2.09	0.44	1.70	78.56	51.16	129.72	4.000	No	No	2.00
79	3.95	47.18	31.47	2.11	0.44	1.70	75.89	52.41	128.30	4.000	No	No	2.00
80	4.00	45.55	32.61	2.12	0.45	1.70	72.92	53.04	125.95	4.000	No	No	2.00
81	4.05	44.07	33.54	2.13	0.45	1.70	70.71	53.51	124.21	4.000	No	No	2.00
82	4.10	42.95	34.22	2.14	0.45	1.70	68.75	53.74	122.49	4.000	No	No	2.00
83	4.15	42.18	34.62	2.15	0.45	1.70	67.53	53.85	121.38	4.000	No	No	2.00
84	4.20	41.81	34.65	2.15	0.46	1.70	66.99	53.76	120.74	4.000	No	No	2.00
85	4.25	41.70	34.29	2.14	0.46	1.70	66.99	53.42	120.41	4.000	No	No	2.00
86	4.30	41.70	33.73	2.13	0.46	1.70	66.99	52.88	119.87	4.000	No	No	2.00
87	4.35	41.70	33.06	2.13	0.46	1.70	66.99	52.22	119.20	4.000	No	No	2.00
88	4.40	41.70	32.71	2.12	0.46	1.70	66.99	51.86	118.84	4.000	No	No	2.00
89	4.45	41.70	32.70	2.12	0.46	1.70	66.99	51.85	118.84	4.000	No	No	2.00
90	4.50	41.64	33.37	2.13	0.46	1.70	66.99	52.53	119.52	4.000	No	No	2.00
91	4.55	41.46	34.36	2.14	0.46	1.70	66.70	53.42	120.12	4.000	Yes	No	2.00
92	4.60	40.97	35.77	2.16	0.46	1.70	66.09	54.56	120.65	4.000	Yes	No	2.00
93	4.65	40.19	37.27	2.18	0.46	1.70	64.63	55.47	120.10	4.000	Yes	No	2.00
94	4.70	39.05	39.03	2.20	0.46	1.70	62.97	56.43	119.39	4.000	Yes	No	2.00
95	4.75	37.79	40.97	2.22	0.46	1.70	60.57	57.19	117.76	4.000	Yes	No	2.00
96	4.80	36.36	43.08	2.25	0.46	1.70	58.58	58.01	116.59	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
97	4.85	35.02	45.17	2.28	0.47	1.70	56.09	58.55	114.63	4.000	Yes	No	2.00
98	4.90	33.60	47.07	2.30	0.47	1.70	54.07	59.00	113.07	4.000	Yes	No	2.00
99	4.95	32.24	48.83	2.32	0.47	1.70	51.74	59.20	110.94	4.000	Yes	No	2.00
100	5.00	30.86	50.67	2.35	0.48	1.70	49.52	59.40	108.91	4.000	Yes	No	2.00
101	5.05	29.46	52.75	2.37	0.48	1.70	47.45	59.66	107.11	4.000	Yes	No	2.00
102	5.10	28.11	55.17	2.40	0.49	1.70	44.99	59.84	104.83	4.000	Yes	No	2.00
103	5.15	26.68	57.82	2.44	0.49	1.70	43.01	60.14	103.15	4.000	Yes	No	2.00
104	5.20	25.33	60.67	2.47	0.50	1.70	40.55	60.27	100.82	4.000	Yes	No	2.00
105	5.25	23.93	63.56	2.51	0.50	1.70	38.47	60.42	98.89	4.000	Yes	No	2.00
106	5.30	22.69	66.40	2.54	0.51	1.70	36.29	60.44	96.74	4.000	Yes	No	2.00
107	5.35	21.59	68.91	2.57	0.51	1.70	34.53	60.46	94.99	4.000	Yes	No	2.00
108	5.40	20.68	71.05	2.60	0.51	1.70	33.18	0.00	33.18	4.000	Yes	Yes	2.00
109	5.45	19.94	72.70	2.62	0.52	1.70	31.93	0.00	31.93	4.000	Yes	Yes	2.00
110	5.50	19.22	73.99	2.64	0.52	1.70	30.94	0.00	30.94	4.000	Yes	Yes	2.00
111	5.55	18.65	74.72	2.65	0.52	1.70	29.75	0.00	29.75	4.000	No	Yes	2.00
112	5.60	18.16	75.08	2.65	0.52	1.70	29.16	0.00	29.16	4.000	No	Yes	2.00
113	5.65	17.66	75.38	2.65	0.52	1.70	28.57	0.00	28.57	4.000	No	Yes	2.00
114	5.70	17.03	76.14	2.66	0.53	1.70	27.35	0.00	27.35	4.000	No	Yes	2.00
115	5.75	16.14	77.66	2.68	0.53	1.70	26.14	0.00	26.14	4.000	No	Yes	2.00
116	5.80	15.27	79.64	2.71	0.54	1.70	24.28	0.00	24.28	4.000	No	Yes	2.00
117	5.85	14.41	81.86	2.74	0.54	1.70	23.14	0.00	23.14	4.000	No	Yes	2.00
118	5.90	13.82	83.81	2.76	0.54	1.70	22.01	0.00	22.01	4.000	No	Yes	2.00
119	5.95	13.39	85.44	2.78	0.54	1.70	21.44	0.00	21.44	4.000	No	Yes	2.00
120	6.00	13.19	86.52	2.79	0.55	1.70	21.05	0.00	21.05	4.000	No	Yes	2.00
121	6.05	13.11	87.16	2.80	0.55	1.70	21.05	0.00	21.05	4.000	No	Yes	2.00
122	6.10	13.11	87.51	2.81	0.55	1.70	21.05	0.00	21.05	4.000	No	Yes	2.00
123	6.15	13.11	87.77	2.81	0.55	1.70	21.05	0.00	21.05	4.000	No	Yes	2.00
124	6.20	13.11	88.10	2.81	0.55	1.70	21.05	0.00	21.05	4.000	No	Yes	2.00
125	6.25	13.11	88.53	2.82	0.55	1.70	21.05	0.00	21.05	4.000	No	Yes	2.00
126	6.30	13.03	89.31	2.83	0.54	1.70	21.05	0.00	21.05	4.000	No	Yes	2.00
127	6.35	12.70	90.70	2.85	0.55	1.70	20.68	0.00	20.68	4.000	No	Yes	2.00
128	6.40	12.15	92.66	2.87	0.55	1.70	19.44	0.00	19.44	4.000	No	Yes	2.00
129	6.45	11.44	94.93	2.90	0.55	1.70	18.43	0.00	18.43	4.000	No	Yes	2.00
130	6.50	10.99	96.51	2.92	0.56	1.70	17.26	0.00	17.26	4.000	No	Yes	2.00
131	6.55	10.74	97.28	2.93	0.56	1.70	17.22	0.00	17.22	4.000	No	Yes	2.00
132	6.60	10.73	97.20	2.93	0.56	1.70	17.22	0.00	17.22	4.000	No	Yes	2.00
133	6.65	10.73	96.96	2.92	0.56	1.70	17.22	0.00	17.22	4.000	No	Yes	2.00
134	6.70	10.73	96.71	2.92	0.56	1.70	17.22	0.00	17.22	4.000	No	Yes	2.00
135	6.75	10.73	96.54	2.92	0.56	1.70	17.22	0.00	17.22	4.000	No	Yes	2.00
136	6.80	10.73	96.44	2.92	0.56	1.70	17.22	0.00	17.22	4.000	No	Yes	2.00
137	6.85	10.73	96.38	2.92	0.56	1.70	17.22	0.00	17.22	4.000	No	Yes	2.00
138	6.90	10.73	96.23	2.92	0.56	1.70	17.22	0.00	17.22	4.000	No	Yes	2.00
139	6.95	10.73	95.99	2.91	0.56	1.69	17.17	0.00	17.17	4.000	No	Yes	2.00
140	7.00	10.73	95.64	2.91	0.56	1.69	17.11	0.00	17.11	4.000	No	Yes	2.00
141	7.05	10.73	95.28	2.90	0.56	1.68	17.06	0.00	17.06	4.000	No	Yes	2.00
142	7.10	10.73	94.87	2.90	0.56	1.68	17.00	0.00	17.00	4.000	No	Yes	2.00
143	7.15	10.73	94.45	2.89	0.56	1.67	16.94	0.00	16.94	4.000	No	Yes	2.00
144	7.20	10.73	93.98	2.89	0.56	1.67	16.89	0.00	16.89	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
145	7.25	10.73	93.74	2.88	0.56	1.66	16.83	0.00	16.83	4.000	No	Yes	2.00
146	7.30	10.73	93.75	2.88	0.56	1.66	16.77	0.00	16.77	4.000	No	Yes	2.00
147	7.35	10.73	94.31	2.89	0.56	1.65	16.71	0.00	16.71	4.000	No	Yes	2.00
148	7.40	10.73	95.13	2.90	0.56	1.64	16.66	0.00	16.66	4.000	No	Yes	2.00
149	7.45	10.73	96.26	2.92	0.56	1.64	16.60	0.00	16.60	4.000	No	Yes	2.00
150	7.50	10.78	97.18	2.93	0.56	1.63	16.54	0.00	16.54	4.000	No	Yes	2.00
151	7.55	11.09	97.42	2.93	0.56	1.63	16.70	0.00	16.70	4.000	No	Yes	2.00
152	7.60	11.66	96.76	2.92	0.55	1.61	17.77	0.00	17.77	4.000	Yes	Yes	2.00
153	7.65	12.56	95.19	2.90	0.55	1.60	18.86	0.00	18.86	4.000	Yes	Yes	2.00
154	7.70	13.44	93.47	2.88	0.55	1.59	20.42	0.00	20.42	4.000	Yes	Yes	2.00
155	7.75	14.27	91.76	2.86	0.54	1.58	21.35	0.00	21.35	4.000	Yes	Yes	2.00
156	7.80	14.98	90.25	2.84	0.54	1.57	22.23	0.00	22.23	4.000	Yes	Yes	2.00
157	7.85	15.66	88.75	2.82	0.54	1.57	23.21	0.00	23.21	4.000	Yes	Yes	2.00
158	7.90	16.37	87.10	2.80	0.54	1.56	24.00	0.00	24.00	4.000	Yes	Yes	2.00
159	7.95	17.12	85.02	2.78	0.53	1.55	25.00	0.00	25.00	4.000	Yes	Yes	2.00
160	8.00	18.02	82.36	2.74	0.53	1.54	26.10	0.00	26.10	4.000	Yes	Yes	2.00
161	8.05	19.23	78.55	2.69	0.53	1.53	27.57	0.00	27.57	4.000	Yes	Yes	2.00
162	8.10	20.74	73.90	2.64	0.52	1.52	29.85	0.00	29.85	4.000	Yes	Yes	2.00
163	8.15	22.77	67.83	2.56	0.52	1.52	32.18	59.56	91.74	4.000	Yes	No	2.00
164	8.20	25.06	61.59	2.48	0.51	1.51	35.76	59.16	94.91	4.000	Yes	No	2.00
165	8.25	27.92	55.08	2.40	0.50	1.50	39.06	58.19	97.25	4.000	Yes	No	2.00
166	8.30	30.77	49.61	2.33	0.50	1.49	43.56	57.38	100.94	4.000	Yes	No	2.00
167	8.35	33.70	44.91	2.27	0.49	1.48	47.00	56.10	103.10	4.000	Yes	No	2.00
168	8.40	35.97	41.40	2.23	0.49	1.47	50.55	55.01	105.56	4.000	Yes	No	2.00
169	8.45	37.71	39.05	2.20	0.48	1.47	52.43	53.93	106.36	4.000	Yes	No	2.00
170	8.50	38.81	37.71	2.18	0.48	1.46	53.77	53.28	107.05	4.000	Yes	No	2.00
171	8.55	39.63	37.22	2.18	0.48	1.46	54.70	53.13	107.83	0.149	No	No	0.26
172	8.60	40.35	36.98	2.17	0.48	1.46	55.42	53.11	108.53	0.150	No	No	0.26
173	8.65	40.92	36.82	2.17	0.48	1.45	56.29	53.18	109.47	0.151	No	No	0.26
174	8.70	41.39	36.52	2.17	0.48	1.45	56.69	53.03	109.72	0.152	No	No	0.26
175	8.75	41.61	36.16	2.16	0.48	1.45	57.00	52.81	109.81	0.152	No	No	0.26
176	8.80	41.66	35.71	2.16	0.48	1.45	56.96	52.43	109.40	0.151	No	No	0.26
177	8.85	41.48	35.30	2.15	0.48	1.45	56.76	52.04	108.80	0.150	No	No	0.26
178	8.90	40.97	35.19	2.15	0.48	1.44	56.23	51.83	108.05	0.149	No	No	0.25
179	8.95	40.02	35.62	2.16	0.48	1.45	54.86	51.88	106.74	4.000	Yes	No	2.00
180	9.00	38.38	36.96	2.17	0.49	1.45	52.96	52.52	105.47	4.000	Yes	No	2.00
181	9.05	36.34	39.06	2.20	0.49	1.45	49.68	53.28	102.95	4.000	Yes	No	2.00
182	9.10	33.87	41.95	2.24	0.50	1.45	46.73	54.40	101.13	4.000	Yes	No	2.00
183	9.15	31.57	45.17	2.28	0.50	1.46	43.18	55.26	98.44	4.000	Yes	No	2.00
184	9.20	29.25	48.71	2.32	0.51	1.46	40.52	56.21	96.72	4.000	Yes	No	2.00
185	9.25	27.17	52.37	2.37	0.51	1.46	37.47	56.83	94.30	4.000	Yes	No	2.00
186	9.30	25.10	56.10	2.41	0.52	1.47	34.83	57.35	92.18	4.000	Yes	No	2.00
187	9.35	23.30	59.79	2.46	0.52	1.47	32.18	57.68	89.86	4.000	Yes	No	2.00
188	9.40	21.84	63.00	2.50	0.53	1.48	30.17	57.92	88.10	4.000	Yes	No	2.00
189	9.45	20.92	65.53	2.53	0.53	1.48	28.92	58.14	87.06	4.000	Yes	No	2.00
190	9.50	20.38	67.43	2.56	0.53	1.47	28.36	58.38	86.74	4.000	Yes	No	2.00
191	9.55	20.02	69.12	2.58	0.53	1.47	27.90	58.58	86.48	4.000	Yes	No	2.00
192	9.60	19.68	71.10	2.60	0.53	1.47	27.37	0.00	27.37	4.000	Yes	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
193	9.65	19.36	73.10	2.63	0.53	1.47	26.87	0.00	26.87	4.000	Yes	Yes	2.00
194	9.70	19.16	75.02	2.65	0.53	1.47	26.48	0.00	26.48	4.000	Yes	Yes	2.00
195	9.75	19.37	75.18	2.65	0.53	1.47	26.44	0.00	26.44	4.000	Yes	Yes	2.00
196	9.80	20.44	73.05	2.63	0.53	1.46	27.61	0.00	27.61	4.000	Yes	Yes	2.00
197	9.85	22.15	68.76	2.57	0.52	1.45	30.58	59.29	89.87	4.000	Yes	No	2.00
198	9.90	24.24	64.09	2.51	0.52	1.45	33.06	59.00	92.06	4.000	Yes	No	2.00
199	9.95	25.93	60.17	2.46	0.51	1.44	35.67	58.76	94.43	4.000	Yes	No	2.00
200	10.00	27.41	56.75	2.42	0.51	1.44	37.07	58.17	95.25	4.000	Yes	No	2.00
201	10.05	29.11	52.67	2.37	0.51	1.43	38.74	57.28	96.02	4.000	Yes	No	2.00
202	10.10	31.11	47.80	2.31	0.50	1.42	42.18	56.25	98.43	4.000	Yes	No	2.00
203	10.15	33.42	42.98	2.25	0.50	1.42	44.73	54.50	99.23	4.000	Yes	No	2.00
204	10.20	35.29	38.87	2.20	0.50	1.42	47.59	52.66	100.25	4.000	Yes	No	2.00
205	10.25	36.90	35.62	2.16	0.50	1.41	49.42	50.64	100.06	4.000	Yes	No	2.00
206	10.30	37.89	33.60	2.13	0.50	1.41	50.95	49.24	100.20	4.000	Yes	No	2.00
207	10.35	38.39	32.89	2.12	0.50	1.41	51.40	48.68	100.08	0.138	No	No	0.22
208	10.40	38.23	33.26	2.13	0.50	1.41	51.22	48.99	100.21	0.138	No	No	0.21
209	10.45	37.66	34.33	2.14	0.50	1.41	50.16	49.72	99.89	0.137	No	No	0.21
210	10.50	36.75	35.66	2.16	0.50	1.41	48.98	50.58	99.55	0.137	No	No	0.21
211	10.55	35.87	36.92	2.17	0.50	1.41	47.56	51.24	98.79	0.136	No	No	0.21
212	10.60	35.11	38.02	2.19	0.50	1.41	46.59	51.83	98.42	0.135	No	No	0.21
213	10.65	34.72	38.92	2.20	0.50	1.41	45.90	52.28	98.18	0.135	No	No	0.21
214	10.70	34.49	39.65	2.21	0.50	1.40	45.82	52.75	98.57	0.136	No	No	0.21
215	10.75	34.31	40.29	2.22	0.50	1.40	45.53	53.10	98.63	0.136	No	No	0.21
216	10.80	34.02	40.81	2.22	0.50	1.40	45.00	53.29	98.29	0.135	No	No	0.21
217	10.85	33.69	41.22	2.23	0.50	1.40	44.54	53.43	97.97	0.135	No	No	0.21
218	10.90	33.60	41.33	2.23	0.50	1.40	44.14	53.40	97.53	0.134	No	No	0.20
219	10.95	33.73	41.27	2.23	0.50	1.40	44.54	53.46	98.00	0.135	No	No	0.21
220	11.00	34.09	41.04	2.23	0.50	1.39	44.88	53.41	98.28	0.135	No	No	0.21
221	11.05	34.36	40.89	2.22	0.50	1.39	45.30	53.41	98.72	0.136	No	No	0.21
222	11.10	34.52	40.81	2.22	0.50	1.39	45.38	53.38	98.76	0.136	No	No	0.21
223	11.15	34.55	40.83	2.22	0.50	1.39	45.33	53.38	98.71	0.136	No	No	0.20
224	11.20	34.52	40.90	2.22	0.50	1.39	45.28	53.41	98.69	0.136	No	No	0.20
225	11.25	34.22	41.17	2.23	0.50	1.39	45.09	53.53	98.62	0.136	No	No	0.20
226	11.30	33.73	41.69	2.23	0.50	1.39	44.10	53.60	97.70	0.135	No	No	0.20
227	11.35	33.01	42.53	2.24	0.50	1.39	43.28	53.88	97.16	0.134	No	No	0.20
228	11.40	32.51	43.41	2.26	0.51	1.39	42.28	54.12	96.39	0.133	No	No	0.20
229	11.45	32.21	44.21	2.27	0.51	1.38	42.05	54.49	96.54	0.133	No	No	0.20
230	11.50	31.92	45.13	2.28	0.51	1.38	41.96	54.93	96.89	4.000	Yes	No	2.00
231	11.55	31.43	46.38	2.29	0.51	1.38	41.00	55.29	96.30	4.000	Yes	No	2.00
232	11.60	30.56	48.30	2.32	0.51	1.38	40.04	55.91	95.95	4.000	Yes	No	2.00
233	11.65	29.63	50.82	2.35	0.51	1.38	38.53	56.54	95.07	4.000	Yes	No	2.00
234	11.70	28.56	53.88	2.39	0.51	1.38	37.29	57.31	94.59	4.000	Yes	No	2.00
235	11.75	27.44	57.44	2.43	0.51	1.38	35.82	58.03	93.86	4.000	Yes	No	2.00
236	11.80	26.20	61.03	2.48	0.51	1.38	34.14	58.56	92.70	4.000	Yes	No	2.00
237	11.85	24.96	64.60	2.52	0.52	1.38	32.48	58.95	91.44	4.000	Yes	No	2.00
238	11.90	23.94	67.34	2.55	0.52	1.38	31.03	59.13	90.16	4.000	Yes	No	2.00
239	11.95	23.21	69.38	2.58	0.52	1.38	30.15	59.28	89.43	4.000	Yes	No	2.00
240	12.00	22.90	69.98	2.59	0.52	1.38	29.64	59.25	88.88	0.125	No	No	0.18

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
241	12.05	22.95	69.57	2.58	0.52	1.38	29.79	59.21	89.01	4.000	Yes	No	2.00
242	12.10	23.46	67.78	2.56	0.52	1.38	30.21	58.98	89.20	4.000	Yes	No	2.00
243	12.15	24.27	65.46	2.53	0.52	1.37	31.49	58.86	90.34	4.000	Yes	No	2.00
244	12.20	25.48	62.39	2.49	0.52	1.37	32.74	58.50	91.24	4.000	Yes	No	2.00
245	12.25	26.69	59.49	2.46	0.51	1.36	34.61	58.28	92.89	4.000	Yes	No	2.00
246	12.30	27.94	56.55	2.42	0.51	1.36	35.90	57.79	93.69	4.000	Yes	No	2.00
247	12.35	28.81	54.59	2.39	0.51	1.36	37.26	57.54	94.80	4.000	Yes	No	2.00
248	12.40	29.42	53.50	2.38	0.51	1.36	37.76	57.31	95.07	0.131	No	No	0.19
249	12.45	29.41	54.11	2.39	0.51	1.35	38.04	57.59	95.63	4.000	Yes	No	2.00
250	12.50	28.97	55.80	2.41	0.51	1.35	37.07	57.88	94.95	4.000	Yes	No	2.00
251	12.55	27.93	58.76	2.45	0.51	1.35	35.98	58.46	94.44	4.000	Yes	No	2.00
252	12.60	26.58	62.25	2.49	0.51	1.35	34.04	58.84	92.87	4.000	Yes	No	2.00
253	12.65	24.77	66.38	2.54	0.52	1.36	31.94	59.19	91.12	4.000	Yes	No	2.00
254	12.70	22.69	71.15	2.60	0.52	1.36	29.19	0.00	29.19	4.000	Yes	Yes	2.00
255	12.75	20.46	76.30	2.67	0.53	1.36	26.22	0.00	26.22	4.000	Yes	Yes	2.00
256	12.80	18.46	81.63	2.73	0.54	1.37	23.57	0.00	23.57	4.000	Yes	Yes	2.00
257	12.85	16.98	86.26	2.79	0.54	1.37	21.64	0.00	21.64	4.000	Yes	Yes	2.00
258	12.90	16.08	89.91	2.84	0.55	1.37	20.61	0.00	20.61	4.000	Yes	Yes	2.00
259	12.95	15.67	92.06	2.86	0.55	1.37	20.11	0.00	20.11	4.000	Yes	Yes	2.00
260	13.00	15.52	93.20	2.88	0.55	1.37	20.00	0.00	20.00	4.000	No	Yes	2.00
261	13.05	15.62	92.89	2.87	0.55	1.36	19.99	0.00	19.99	4.000	No	Yes	2.00
262	13.10	15.82	91.81	2.86	0.55	1.36	20.41	0.00	20.41	4.000	No	Yes	2.00
263	13.15	16.02	90.01	2.84	0.55	1.36	20.68	0.00	20.68	4.000	No	Yes	2.00
264	13.20	15.84	88.78	2.82	0.55	1.36	20.66	0.00	20.66	4.000	No	Yes	2.00
265	13.25	15.09	88.53	2.82	0.55	1.36	19.70	0.00	19.70	4.000	No	Yes	2.00
266	13.30	13.89	89.79	2.83	0.56	1.36	17.82	0.00	17.82	4.000	No	Yes	2.00
267	13.35	12.54	92.17	2.86	0.56	1.37	16.13	0.00	16.13	4.000	No	Yes	2.00
268	13.40	11.57	94.98	2.90	0.57	1.37	14.58	0.00	14.58	4.000	No	Yes	2.00
269	13.45	11.06	97.02	2.93	0.57	1.37	14.09	0.00	14.09	4.000	No	Yes	2.00
270	13.50	11.21	97.21	2.93	0.57	1.37	14.16	0.00	14.16	4.000	No	Yes	2.00
271	13.55	11.71	95.88	2.91	0.56	1.36	15.12	0.00	15.12	4.000	No	Yes	2.00
272	13.60	12.41	93.79	2.88	0.56	1.36	15.89	0.00	15.89	4.000	No	Yes	2.00
273	13.65	12.87	92.78	2.87	0.56	1.35	16.77	0.00	16.77	4.000	No	Yes	2.00
274	13.70	13.11	92.72	2.87	0.56	1.35	16.76	0.00	16.76	4.000	No	Yes	2.00
275	13.75	13.11	93.63	2.88	0.56	1.35	16.74	0.00	16.74	4.000	No	Yes	2.00
276	13.80	13.11	94.46	2.89	0.56	1.35	16.72	0.00	16.72	4.000	No	Yes	2.00
277	13.85	13.11	95.28	2.90	0.56	1.35	16.70	0.00	16.70	4.000	No	Yes	2.00
278	13.90	13.11	95.85	2.91	0.56	1.35	16.68	0.00	16.68	4.000	No	Yes	2.00
279	13.95	13.13	96.23	2.92	0.56	1.35	16.66	0.00	16.66	4.000	No	Yes	2.00
280	14.00	13.39	95.92	2.91	0.56	1.34	16.69	0.00	16.69	4.000	No	Yes	2.00
281	14.05	13.85	95.25	2.90	0.56	1.34	17.58	0.00	17.58	4.000	No	Yes	2.00
282	14.10	14.57	94.34	2.89	0.55	1.34	18.33	0.00	18.33	4.000	No	Yes	2.00
283	14.15	15.10	93.88	2.89	0.55	1.33	19.25	0.00	19.25	4.000	No	Yes	2.00
284	14.20	15.43	93.81	2.89	0.55	1.33	19.48	0.00	19.48	4.000	No	Yes	2.00
285	14.25	15.50	94.03	2.89	0.55	1.33	19.46	0.00	19.46	4.000	No	Yes	2.00
286	14.30	15.50	94.32	2.89	0.55	1.33	19.44	0.00	19.44	4.000	No	Yes	2.00
287	14.35	15.50	94.66	2.90	0.55	1.33	19.41	0.00	19.41	4.000	No	Yes	2.00
288	14.40	15.50	95.03	2.90	0.55	1.32	19.39	0.00	19.39	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
289	14.45	15.50	95.39	2.90	0.55	1.32	19.37	0.00	19.37	4.000	No	Yes	2.00
290	14.50	15.58	95.32	2.90	0.55	1.32	19.35	0.00	19.35	4.000	No	Yes	2.00
291	14.55	15.79	94.82	2.90	0.55	1.32	19.63	0.00	19.63	4.000	No	Yes	2.00
292	14.60	16.23	93.48	2.88	0.55	1.32	20.04	0.00	20.04	4.000	No	Yes	2.00
293	14.65	16.77	91.76	2.86	0.54	1.31	20.89	0.00	20.89	4.000	No	Yes	2.00
294	14.70	17.32	89.66	2.83	0.54	1.31	21.52	0.00	21.52	4.000	No	Yes	2.00
295	14.75	17.67	87.88	2.81	0.54	1.31	21.97	0.00	21.97	4.000	No	Yes	2.00
296	14.80	17.84	86.32	2.79	0.54	1.31	22.09	0.00	22.09	4.000	No	Yes	2.00
297	14.85	17.68	85.70	2.78	0.54	1.31	22.07	0.00	22.07	4.000	No	Yes	2.00
298	14.90	17.26	85.82	2.79	0.54	1.31	21.34	0.00	21.34	4.000	No	Yes	2.00
299	14.95	16.59	86.93	2.80	0.55	1.31	20.52	0.00	20.52	4.000	No	Yes	2.00
300	15.00	15.91	88.37	2.82	0.55	1.31	19.60	0.00	19.60	4.000	No	Yes	2.00
301	15.05	15.20	90.18	2.84	0.55	1.31	18.83	0.00	18.83	4.000	No	Yes	2.00
302	15.10	14.52	92.00	2.86	0.56	1.31	17.88	0.00	17.88	4.000	No	Yes	2.00
303	15.15	13.81	93.98	2.89	0.56	1.31	17.10	0.00	17.10	4.000	No	Yes	2.00
304	15.20	13.36	95.49	2.91	0.56	1.31	16.22	0.00	16.22	4.000	No	Yes	2.00
305	15.25	13.12	96.55	2.92	0.56	1.31	16.18	0.00	16.18	4.000	No	Yes	2.00
306	15.30	13.11	97.01	2.93	0.56	1.31	16.17	0.00	16.17	4.000	No	Yes	2.00
307	15.35	13.11	97.31	2.93	0.56	1.30	16.15	0.00	16.15	4.000	No	Yes	2.00
308	15.40	13.11	97.45	2.93	0.56	1.30	16.13	0.00	16.13	4.000	No	Yes	2.00
309	15.45	13.11	97.43	2.93	0.56	1.30	16.11	0.00	16.11	4.000	No	Yes	2.00
310	15.50	13.11	97.32	2.93	0.56	1.30	16.10	0.00	16.10	4.000	No	Yes	2.00
311	15.55	13.11	97.21	2.93	0.56	1.30	16.08	0.00	16.08	4.000	No	Yes	2.00
312	15.60	13.11	97.23	2.93	0.56	1.30	16.06	0.00	16.06	4.000	No	Yes	2.00
313	15.65	13.11	97.57	2.93	0.56	1.30	16.05	0.00	16.05	4.000	No	Yes	2.00
314	15.70	13.32	97.67	2.93	0.56	1.29	16.03	0.00	16.03	4.000	No	Yes	2.00
315	15.75	13.90	97.18	2.93	0.56	1.29	16.75	0.00	16.75	4.000	No	Yes	2.00
316	15.80	15.24	94.79	2.90	0.55	1.29	18.05	0.00	18.05	4.000	No	Yes	2.00
317	15.85	17.13	91.24	2.85	0.55	1.28	20.74	0.00	20.74	4.000	No	Yes	2.00
318	15.90	19.55	86.44	2.79	0.54	1.28	23.40	0.00	23.40	4.000	No	Yes	2.00
319	15.95	21.87	81.85	2.74	0.53	1.27	26.48	0.00	26.48	4.000	No	Yes	2.00
320	16.00	24.20	77.03	2.68	0.52	1.26	28.79	0.00	28.79	4.000	No	Yes	2.00
321	16.05	26.03	73.37	2.63	0.52	1.26	31.42	0.00	31.42	4.000	No	Yes	2.00
322	16.10	27.52	70.55	2.59	0.51	1.26	32.73	60.26	92.98	0.129	No	No	0.17
323	16.15	28.01	70.16	2.59	0.51	1.25	33.86	60.51	94.37	0.131	No	No	0.17
324	16.20	27.82	71.23	2.60	0.51	1.25	33.00	0.00	33.00	4.000	No	Yes	2.00
325	16.25	26.64	74.16	2.64	0.51	1.25	31.95	0.00	31.95	4.000	No	Yes	2.00
326	16.30	25.25	77.18	2.68	0.52	1.26	29.71	0.00	29.71	4.000	No	Yes	2.00
327	16.35	23.65	80.32	2.72	0.52	1.26	28.11	0.00	28.11	4.000	No	Yes	2.00
328	16.40	22.45	82.45	2.74	0.53	1.26	26.35	0.00	26.35	4.000	No	Yes	2.00
329	16.45	21.50	83.94	2.76	0.53	1.26	25.48	0.00	25.48	4.000	No	Yes	2.00
330	16.50	21.06	84.25	2.77	0.53	1.26	24.76	0.00	24.76	4.000	No	Yes	2.00
331	16.55	20.86	83.95	2.76	0.53	1.26	24.74	0.00	24.74	4.000	No	Yes	2.00
332	16.60	20.86	83.02	2.75	0.53	1.25	24.72	0.00	24.72	4.000	No	Yes	2.00
333	16.65	20.78	82.52	2.74	0.53	1.25	24.69	0.00	24.69	4.000	No	Yes	2.00
334	16.70	20.59	82.72	2.75	0.54	1.25	24.41	0.00	24.41	4.000	No	Yes	2.00
335	16.75	20.27	84.11	2.76	0.54	1.25	23.97	0.00	23.97	4.000	No	Yes	2.00
336	16.80	19.89	86.10	2.79	0.54	1.25	23.54	0.00	23.54	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
337	16.85	19.24	88.79	2.82	0.54	1.25	22.99	0.00	22.99	4.000	No	Yes	2.00
338	16.90	18.56	91.38	2.85	0.54	1.25	21.64	0.00	21.64	4.000	No	Yes	2.00
339	16.95	18.03	93.65	2.88	0.54	1.25	21.11	0.00	21.11	4.000	No	Yes	2.00
340	17.00	18.61	93.61	2.88	0.54	1.25	21.09	0.00	21.09	4.000	Yes	Yes	2.00
341	17.05	20.27	91.49	2.86	0.54	1.24	23.56	0.00	23.56	4.000	Yes	Yes	2.00
342	17.10	23.40	86.69	2.80	0.53	1.24	26.73	0.00	26.73	4.000	Yes	Yes	2.00
343	17.15	27.05	81.24	2.73	0.51	1.23	31.67	0.00	31.67	4.000	Yes	Yes	2.00
344	17.20	31.32	74.91	2.65	0.50	1.22	35.84	0.00	35.84	4.000	Yes	Yes	2.00
345	17.25	35.16	69.17	2.58	0.49	1.22	40.96	62.38	103.35	4.000	Yes	No	2.00
346	17.30	38.86	63.27	2.50	0.48	1.21	44.40	62.03	106.43	4.000	Yes	No	2.00
347	17.35	41.28	58.48	2.44	0.48	1.21	48.02	61.73	109.75	4.000	Yes	No	2.00
348	17.40	42.80	54.22	2.39	0.48	1.21	48.93	60.59	109.52	4.000	Yes	No	2.00
349	17.45	42.83	51.66	2.36	0.48	1.21	49.37	59.75	109.12	4.000	Yes	No	2.00
350	17.50	42.19	50.22	2.34	0.48	1.21	48.11	58.84	106.95	4.000	Yes	No	2.00
351	17.55	40.76	50.35	2.34	0.49	1.21	46.75	58.53	105.29	0.145	No	No	0.18
352	17.60	39.02	51.47	2.36	0.49	1.21	44.59	58.41	103.00	4.000	Yes	No	2.00
353	17.65	36.86	53.63	2.38	0.50	1.21	42.25	58.57	100.81	4.000	Yes	No	2.00
354	17.70	34.06	57.11	2.43	0.50	1.21	39.47	58.94	98.41	4.000	Yes	No	2.00
355	17.75	30.98	61.56	2.48	0.51	1.21	35.20	58.99	94.19	4.000	Yes	No	2.00
356	17.80	27.97	67.08	2.55	0.52	1.22	31.85	59.31	91.16	4.000	Yes	No	2.00
357	17.85	25.78	72.21	2.62	0.52	1.22	29.30	0.00	29.30	4.000	Yes	Yes	2.00
358	17.90	24.17	77.22	2.68	0.53	1.22	27.76	0.00	27.76	4.000	Yes	Yes	2.00
359	17.95	22.86	81.61	2.73	0.53	1.22	26.32	0.00	26.32	4.000	Yes	Yes	2.00
360	18.00	21.57	85.97	2.79	0.53	1.22	24.77	0.00	24.77	4.000	Yes	Yes	2.00
361	18.05	20.83	89.29	2.83	0.54	1.22	23.35	0.00	23.35	4.000	Yes	Yes	2.00
362	18.10	20.97	91.07	2.85	0.54	1.22	23.74	0.00	23.74	4.000	Yes	Yes	2.00
363	18.15	22.68	90.14	2.84	0.53	1.21	25.13	0.00	25.13	4.000	Yes	Yes	2.00
364	18.20	24.91	87.98	2.81	0.52	1.21	28.98	0.00	28.98	4.000	Yes	Yes	2.00
365	18.25	27.32	85.01	2.78	0.51	1.20	31.08	0.00	31.08	4.000	Yes	Yes	2.00
366	18.30	29.37	81.82	2.74	0.51	1.20	33.04	0.00	33.04	4.000	Yes	Yes	2.00
367	18.35	31.86	77.77	2.68	0.50	1.20	35.66	0.00	35.66	4.000	Yes	Yes	2.00
368	18.40	36.70	71.47	2.61	0.49	1.19	39.20	0.00	39.20	4.000	Yes	Yes	2.00
369	18.45	43.08	64.37	2.52	0.47	1.18	48.70	63.53	112.23	4.000	Yes	No	2.00
370	18.50	51.28	56.30	2.42	0.46	1.17	56.24	63.31	119.55	4.000	Yes	No	2.00
371	18.55	57.67	49.77	2.33	0.44	1.17	65.44	63.23	128.67	4.000	Yes	No	2.00
372	18.60	62.48	44.11	2.26	0.44	1.16	69.04	61.24	130.28	4.000	Yes	No	2.00
373	18.65	62.59	42.32	2.24	0.43	1.16	71.48	60.75	132.24	4.000	Yes	No	2.00
374	18.70	59.78	43.43	2.26	0.45	1.16	65.74	60.01	125.75	4.000	Yes	No	2.00
375	18.75	53.35	49.06	2.33	0.45	1.17	59.97	61.47	121.44	4.000	Yes	No	2.00
376	18.80	46.95	55.74	2.41	0.47	1.17	50.83	61.63	112.46	4.000	Yes	No	2.00
377	18.85	40.55	63.45	2.51	0.48	1.18	45.05	62.26	107.31	4.000	Yes	No	2.00
378	18.90	36.09	69.60	2.58	0.50	1.18	39.22	61.96	101.18	4.000	Yes	No	2.00
379	18.95	32.65	75.10	2.65	0.50	1.18	36.25	0.00	36.25	4.000	Yes	Yes	2.00
380	19.00	30.55	79.03	2.70	0.51	1.18	33.76	0.00	33.76	4.000	Yes	Yes	2.00
381	19.05	28.71	82.33	2.74	0.51	1.18	32.28	0.00	32.28	4.000	Yes	Yes	2.00
382	19.10	26.41	85.47	2.78	0.52	1.18	30.17	0.00	30.17	4.000	Yes	Yes	2.00
383	19.15	23.50	89.15	2.83	0.53	1.19	26.15	0.00	26.15	4.000	Yes	Yes	2.00
384	19.20	20.07	93.80	2.89	0.54	1.19	22.67	0.00	22.67	4.000	Yes	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
385	19.25	17.73	97.54	2.93	0.55	1.19	18.80	0.00	18.80	4.000	Yes	Yes	2.00
386	19.30	16.42	99.93	2.96	0.55	1.19	18.38	0.00	18.38	4.000	Yes	Yes	2.00
387	19.35	16.54	99.30	2.95	0.55	1.19	18.28	0.00	18.28	4.000	No	Yes	2.00
388	19.40	16.98	97.74	2.93	0.55	1.19	19.12	0.00	19.12	4.000	No	Yes	2.00
389	19.45	17.69	95.29	2.90	0.55	1.19	19.78	0.00	19.78	4.000	No	Yes	2.00
390	19.50	18.17	93.23	2.88	0.55	1.19	20.59	0.00	20.59	4.000	No	Yes	2.00
391	19.55	18.43	91.40	2.86	0.55	1.18	20.66	0.00	20.66	4.000	No	Yes	2.00
392	19.60	18.19	90.48	2.84	0.55	1.18	20.58	0.00	20.58	4.000	No	Yes	2.00
393	19.65	17.78	89.86	2.84	0.55	1.18	19.75	0.00	19.75	4.000	No	Yes	2.00
394	19.70	17.37	89.60	2.83	0.55	1.18	19.28	0.00	19.28	4.000	No	Yes	2.00
395	19.75	17.72	88.71	2.82	0.55	1.18	19.18	0.00	19.18	4.000	No	Yes	2.00
396	19.80	19.06	87.42	2.81	0.55	1.18	20.85	0.00	20.85	4.000	No	Yes	2.00
397	19.85	21.14	85.56	2.78	0.54	1.17	23.59	0.00	23.59	4.000	No	Yes	2.00
398	19.90	23.24	83.90	2.76	0.53	1.17	25.91	0.00	25.91	4.000	No	Yes	2.00
399	19.95	24.36	82.13	2.74	0.53	1.17	27.62	0.00	27.62	4.000	No	Yes	2.00
400	20.00	24.31	80.81	2.72	0.53	1.17	27.17	0.00	27.17	4.000	No	Yes	2.00
401	20.05	23.17	79.81	2.71	0.53	1.17	25.69	0.00	25.69	4.000	No	Yes	2.00
402	20.10	21.56	80.12	2.71	0.54	1.17	23.88	0.00	23.88	4.000	No	Yes	2.00
403	20.15	19.80	81.77	2.73	0.54	1.17	21.89	0.00	21.89	4.000	No	Yes	2.00
404	20.20	18.02	84.72	2.77	0.55	1.17	19.89	0.00	19.89	4.000	No	Yes	2.00
405	20.25	16.38	88.30	2.82	0.56	1.17	18.04	0.00	18.04	4.000	No	Yes	2.00
406	20.30	15.27	91.49	2.86	0.56	1.17	16.48	0.00	16.48	4.000	No	Yes	2.00
407	20.35	14.87	93.49	2.88	0.56	1.17	16.21	0.00	16.21	4.000	No	Yes	2.00
408	20.40	15.07	94.45	2.89	0.56	1.17	16.69	0.00	16.69	4.000	No	Yes	2.00
409	20.45	15.35	95.15	2.90	0.56	1.17	17.08	0.00	17.08	4.000	No	Yes	2.00
410	20.50	15.50	96.16	2.91	0.56	1.17	17.09	0.00	17.09	4.000	No	Yes	2.00
411	20.55	15.65	96.91	2.92	0.56	1.17	17.12	0.00	17.12	4.000	No	Yes	2.00
412	20.60	16.12	96.83	2.92	0.56	1.16	17.52	0.00	17.52	4.000	No	Yes	2.00
413	20.65	17.35	94.93	2.90	0.55	1.16	18.57	0.00	18.57	4.000	No	Yes	2.00
414	20.70	19.25	91.77	2.86	0.54	1.16	21.05	0.00	21.05	4.000	No	Yes	2.00
415	20.75	21.77	87.55	2.81	0.54	1.16	23.61	0.00	23.61	4.000	No	Yes	2.00
416	20.80	24.22	83.60	2.76	0.53	1.15	26.60	0.00	26.60	4.000	No	Yes	2.00
417	20.85	26.40	80.02	2.71	0.52	1.15	28.85	0.00	28.85	4.000	No	Yes	2.00
418	20.90	27.89	77.39	2.68	0.52	1.15	30.52	0.00	30.52	4.000	No	Yes	2.00
419	20.95	28.59	75.75	2.66	0.52	1.15	31.31	0.00	31.31	4.000	No	Yes	2.00
420	21.00	28.38	75.62	2.66	0.52	1.14	31.00	0.00	31.00	4.000	No	Yes	2.00
421	21.05	27.39	77.03	2.68	0.52	1.14	29.77	0.00	29.77	4.000	No	Yes	2.00
422	21.10	25.93	79.91	2.71	0.52	1.14	28.08	0.00	28.08	4.000	No	Yes	2.00
423	21.15	24.23	83.50	2.76	0.53	1.15	26.27	0.00	26.27	4.000	No	Yes	2.00
424	21.20	22.73	87.10	2.80	0.53	1.15	24.27	0.00	24.27	4.000	No	Yes	2.00
425	21.25	21.78	89.47	2.83	0.54	1.15	23.21	0.00	23.21	4.000	No	Yes	2.00
426	21.30	21.24	90.73	2.85	0.54	1.14	23.19	0.00	23.19	4.000	No	Yes	2.00
427	21.35	20.65	91.17	2.85	0.54	1.14	22.47	0.00	22.47	4.000	No	Yes	2.00
428	21.40	19.33	92.45	2.87	0.54	1.14	21.29	0.00	21.29	4.000	No	Yes	2.00
429	21.45	17.60	94.45	2.89	0.55	1.15	18.92	0.00	18.92	4.000	No	Yes	2.00
430	21.50	15.86	97.35	2.93	0.56	1.15	16.90	0.00	16.90	4.000	No	Yes	2.00
431	21.55	14.54	100.00	2.96	0.56	1.15	15.65	0.00	15.65	4.000	No	Yes	2.00
432	21.60	13.46	100.00	3.00	0.56	1.15	14.65	0.00	14.65	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
433	21.65	12.45	100.00	3.02	0.57	1.15	13.41	0.00	13.41	4.000	No	Yes	2.00
434	21.70	11.41	100.00	3.05	0.57	1.15	12.37	0.00	12.37	4.000	No	Yes	2.00
435	21.75	10.56	100.00	3.08	0.58	1.15	11.27	0.00	11.27	4.000	No	Yes	2.00
436	21.80	9.94	100.00	3.10	0.58	1.15	10.68	0.00	10.68	4.000	No	Yes	2.00
437	21.85	9.64	100.00	3.11	0.58	1.15	10.32	0.00	10.32	4.000	No	Yes	2.00
438	21.90	9.63	100.00	3.11	0.58	1.14	10.31	0.00	10.31	4.000	No	Yes	2.00
439	21.95	9.92	100.00	3.11	0.58	1.14	10.62	0.00	10.62	4.000	No	Yes	2.00
440	22.00	10.36	100.00	3.10	0.58	1.14	11.21	0.00	11.21	4.000	No	Yes	2.00
441	22.05	10.84	100.00	3.09	0.58	1.14	11.68	0.00	11.68	4.000	No	Yes	2.00
442	22.10	11.28	100.00	3.08	0.57	1.14	12.13	0.00	12.13	4.000	No	Yes	2.00
443	22.15	11.78	100.00	3.08	0.57	1.14	12.59	0.00	12.59	4.000	No	Yes	2.00
444	22.20	12.54	100.00	3.06	0.57	1.14	13.25	0.00	13.25	4.000	No	Yes	2.00
445	22.25	13.51	100.00	3.04	0.57	1.13	14.53	0.00	14.53	4.000	No	Yes	2.00
446	22.30	14.66	100.00	3.01	0.56	1.13	15.63	0.00	15.63	4.000	No	Yes	2.00
447	22.35	16.29	100.00	2.97	0.56	1.13	16.86	0.00	16.86	4.000	No	Yes	2.00
448	22.40	18.38	96.25	2.92	0.55	1.13	19.65	0.00	19.65	4.000	No	Yes	2.00
449	22.45	21.10	91.25	2.85	0.54	1.12	22.16	0.00	22.16	4.000	No	Yes	2.00
450	22.50	23.53	86.75	2.80	0.53	1.12	25.37	0.00	25.37	4.000	No	Yes	2.00
451	22.55	25.65	82.41	2.74	0.53	1.12	27.19	0.00	27.19	4.000	No	Yes	2.00
452	22.60	26.99	78.94	2.70	0.52	1.12	28.74	0.00	28.74	4.000	No	Yes	2.00
453	22.65	27.93	75.83	2.66	0.52	1.12	29.49	0.00	29.49	4.000	No	Yes	2.00
454	22.70	28.11	74.11	2.64	0.52	1.11	30.06	0.00	30.06	4.000	No	Yes	2.00
455	22.75	27.77	73.45	2.63	0.52	1.11	29.27	0.00	29.27	4.000	No	Yes	2.00
456	22.80	26.72	74.65	2.65	0.53	1.11	28.36	0.00	28.36	4.000	No	Yes	2.00
457	22.85	25.36	76.87	2.67	0.53	1.11	26.73	0.00	26.73	4.000	No	Yes	2.00
458	22.90	23.55	80.37	2.72	0.53	1.11	24.95	0.00	24.95	4.000	No	Yes	2.00
459	22.95	21.57	84.24	2.77	0.54	1.11	22.67	0.00	22.67	4.000	No	Yes	2.00
460	23.00	19.55	88.44	2.82	0.55	1.11	20.50	0.00	20.50	4.000	No	Yes	2.00
461	23.05	17.74	92.37	2.87	0.55	1.12	18.59	0.00	18.59	4.000	No	Yes	2.00
462	23.10	16.26	95.97	2.91	0.56	1.12	16.97	0.00	16.97	4.000	No	Yes	2.00
463	23.15	15.01	99.43	2.96	0.56	1.12	15.83	0.00	15.83	4.000	No	Yes	2.00
464	23.20	14.12	100.00	2.99	0.56	1.12	14.62	0.00	14.62	4.000	No	Yes	2.00
465	23.25	13.48	100.00	3.02	0.57	1.11	14.15	0.00	14.15	4.000	No	Yes	2.00
466	23.30	13.22	100.00	3.04	0.57	1.11	13.79	0.00	13.79	4.000	No	Yes	2.00
467	23.35	13.14	100.00	3.06	0.57	1.11	13.78	0.00	13.78	4.000	No	Yes	2.00
468	23.40	13.31	100.00	3.07	0.57	1.11	13.87	0.00	13.87	4.000	No	Yes	2.00
469	23.45	13.70	100.00	3.08	0.57	1.11	14.26	0.00	14.26	4.000	No	Yes	2.00
470	23.50	14.44	100.00	3.07	0.56	1.11	14.98	0.00	14.98	4.000	No	Yes	2.00
471	23.55	15.48	100.00	3.05	0.56	1.11	16.12	0.00	16.12	4.000	No	Yes	2.00
472	23.60	16.69	100.00	3.01	0.55	1.11	17.47	0.00	17.47	4.000	No	Yes	2.00
473	23.65	17.65	100.00	2.98	0.55	1.10	18.68	0.00	18.68	4.000	No	Yes	2.00
474	23.70	18.15	99.58	2.96	0.55	1.10	19.06	0.00	19.06	4.000	No	Yes	2.00
475	23.75	17.98	98.59	2.94	0.55	1.10	18.95	0.00	18.95	4.000	No	Yes	2.00
476	23.80	17.49	98.08	2.94	0.55	1.10	18.14	0.00	18.14	4.000	No	Yes	2.00
477	23.85	16.78	97.98	2.94	0.56	1.10	17.47	0.00	17.47	4.000	No	Yes	2.00
478	23.90	15.98	98.27	2.94	0.56	1.10	16.73	0.00	16.73	4.000	No	Yes	2.00
479	23.95	15.09	98.84	2.95	0.56	1.10	15.62	0.00	15.62	4.000	No	Yes	2.00
480	24.00	14.19	99.71	2.96	0.56	1.10	14.71	0.00	14.71	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
481	24.05	13.55	100.00	2.96	0.57	1.10	13.90	0.00	13.90	4.000	No	Yes	2.00
482	24.10	13.20	100.00	2.97	0.57	1.10	13.61	0.00	13.61	4.000	No	Yes	2.00
483	24.15	13.30	100.00	2.97	0.57	1.10	13.60	0.00	13.60	4.000	No	Yes	2.00
484	24.20	13.74	100.00	2.98	0.57	1.10	14.18	0.00	14.18	4.000	No	Yes	2.00
485	24.25	14.80	100.00	2.98	0.56	1.10	14.94	0.00	14.94	4.000	No	Yes	2.00
486	24.30	16.23	100.00	2.97	0.56	1.09	16.83	0.00	16.83	4.000	Yes	Yes	2.00
487	24.35	18.18	99.02	2.95	0.55	1.09	18.51	0.00	18.51	4.000	Yes	Yes	2.00
488	24.40	20.21	97.06	2.93	0.54	1.09	20.87	0.00	20.87	4.000	Yes	Yes	2.00
489	24.45	22.53	93.96	2.89	0.54	1.09	22.98	0.00	22.98	4.000	Yes	Yes	2.00
490	24.50	25.19	90.26	2.84	0.53	1.09	25.56	0.00	25.56	4.000	Yes	Yes	2.00
491	24.55	28.19	85.93	2.79	0.52	1.08	28.90	0.00	28.90	4.000	Yes	Yes	2.00
492	24.60	31.49	81.70	2.73	0.51	1.08	32.03	0.00	32.03	4.000	Yes	Yes	2.00
493	24.65	34.39	78.04	2.69	0.50	1.08	35.47	0.00	35.47	4.000	Yes	Yes	2.00
494	24.70	36.86	75.02	2.65	0.50	1.08	37.58	0.00	37.58	4.000	Yes	Yes	2.00
495	24.75	38.66	72.53	2.62	0.49	1.07	39.40	0.00	39.40	4.000	Yes	Yes	2.00
496	24.80	40.24	70.13	2.59	0.49	1.07	40.78	62.52	103.30	4.000	Yes	No	2.00
497	24.85	41.99	67.56	2.56	0.49	1.07	42.26	62.42	104.67	4.000	Yes	No	2.00
498	24.90	44.00	64.55	2.52	0.48	1.07	44.54	62.39	106.93	4.000	Yes	No	2.00
499	24.95	46.64	61.13	2.48	0.48	1.07	46.73	62.13	108.86	4.000	Yes	No	2.00
500	25.00	49.30	57.56	2.43	0.47	1.07	50.05	62.01	112.07	4.000	Yes	No	2.00
501	25.05	52.08	54.12	2.39	0.47	1.07	52.38	61.49	113.87	4.000	Yes	No	2.00
502	25.10	53.91	51.36	2.35	0.46	1.06	54.93	61.13	116.06	4.000	Yes	No	2.00
503	25.15	55.06	49.33	2.33	0.47	1.06	55.41	60.39	115.80	4.000	Yes	No	2.00
504	25.20	55.46	48.12	2.31	0.47	1.06	55.70	59.92	115.62	4.000	Yes	No	2.00
505	25.25	55.87	47.37	2.30	0.47	1.06	56.04	59.65	115.69	0.162	No	No	0.19
506	25.30	56.48	46.90	2.30	0.46	1.06	56.50	59.54	116.04	0.163	No	No	0.19
507	25.35	57.20	46.54	2.29	0.46	1.06	57.41	59.60	117.01	0.165	No	No	0.19
508	25.40	57.98	46.27	2.29	0.46	1.06	58.03	59.62	117.66	0.166	No	No	0.19
509	25.45	58.95	45.92	2.29	0.46	1.06	58.70	59.61	118.30	0.168	No	No	0.19
510	25.50	60.19	45.32	2.28	0.46	1.06	60.14	59.67	119.81	0.171	No	No	0.19
511	25.55	61.96	44.22	2.27	0.45	1.06	61.57	59.42	120.99	0.174	No	No	0.20
512	25.60	64.03	42.69	2.25	0.45	1.06	63.81	59.08	122.88	0.178	No	No	0.20
513	25.65	66.76	40.80	2.22	0.45	1.05	66.13	58.43	124.56	0.182	No	No	0.21
514	25.70	69.59	38.96	2.20	0.44	1.05	69.51	57.94	127.45	0.190	No	No	0.22
515	25.75	72.49	37.36	2.18	0.44	1.05	72.01	57.27	129.28	0.195	No	No	0.22
516	25.80	75.35	36.02	2.16	0.44	1.05	74.55	56.71	131.25	0.202	No	No	0.23
517	25.85	78.28	34.97	2.15	0.43	1.05	77.75	56.46	134.22	0.212	No	No	0.24
518	25.90	81.53	34.09	2.14	0.43	1.05	80.46	56.21	136.67	0.221	No	No	0.25
519	25.95	83.12	33.90	2.14	0.42	1.05	83.91	56.78	140.68	0.238	No	No	0.27
520	26.00	82.31	34.27	2.14	0.42	1.05	82.23	56.79	139.02	0.230	No	No	0.26
521	26.05	79.36	35.12	2.15	0.43	1.05	77.91	56.65	134.56	0.213	No	No	0.24
522	26.10	76.33	35.70	2.16	0.43	1.05	75.13	56.56	131.68	0.203	No	No	0.23
523	26.15	75.41	35.68	2.16	0.44	1.05	73.26	56.11	129.37	0.196	No	No	0.22
524	26.20	75.46	35.52	2.16	0.44	1.04	75.06	56.37	131.44	0.202	No	No	0.23
525	26.25	75.56	35.72	2.16	0.43	1.04	75.13	56.57	131.69	0.203	No	No	0.23
526	26.30	74.50	36.53	2.17	0.44	1.04	73.39	56.89	130.28	4.000	Yes	No	2.00
527	26.35	72.82	37.76	2.18	0.44	1.04	71.80	57.54	129.35	4.000	Yes	No	2.00
528	26.40	71.07	39.16	2.20	0.44	1.04	70.06	58.22	128.27	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
529	26.45	69.30	40.96	2.22	0.44	1.04	68.11	59.03	127.14	4.000	Yes	No	2.00
530	26.50	67.46	43.06	2.25	0.44	1.04	66.45	59.97	126.42	4.000	Yes	No	2.00
531	26.55	65.64	45.46	2.28	0.45	1.04	64.51	60.86	125.37	4.000	Yes	No	2.00
532	26.60	63.55	48.07	2.31	0.45	1.04	62.64	61.71	124.35	4.000	Yes	No	2.00
533	26.65	61.12	50.89	2.35	0.45	1.04	60.18	62.33	122.51	4.000	Yes	No	2.00
534	26.70	58.35	54.12	2.39	0.46	1.04	57.28	62.83	120.11	4.000	Yes	No	2.00
535	26.75	55.46	57.47	2.43	0.46	1.04	54.40	63.19	117.59	4.000	Yes	No	2.00
536	26.80	52.67	61.02	2.48	0.47	1.04	51.61	63.47	115.08	4.000	Yes	No	2.00
537	26.85	49.61	64.55	2.52	0.47	1.04	49.03	63.67	112.70	4.000	Yes	No	2.00
538	26.90	46.41	68.22	2.57	0.48	1.04	45.33	63.45	108.78	4.000	Yes	No	2.00
539	26.95	42.85	71.99	2.61	0.49	1.04	42.16	0.00	42.16	4.000	Yes	Yes	2.00
540	27.00	39.81	75.40	2.65	0.50	1.04	38.54	0.00	38.54	4.000	Yes	Yes	2.00
541	27.05	37.31	78.31	2.69	0.50	1.04	36.36	0.00	36.36	4.000	Yes	Yes	2.00
542	27.10	35.96	80.13	2.71	0.50	1.04	34.78	0.00	34.78	4.000	Yes	Yes	2.00
543	27.15	35.29	81.16	2.73	0.50	1.04	34.50	0.00	34.50	4.000	No	Yes	2.00
544	27.20	35.12	81.51	2.73	0.51	1.04	34.33	0.00	34.33	4.000	No	Yes	2.00
545	27.25	34.89	81.72	2.73	0.51	1.03	34.18	0.00	34.18	4.000	No	Yes	2.00
546	27.30	34.59	81.95	2.74	0.51	1.03	33.78	0.00	33.78	4.000	No	Yes	2.00
547	27.35	34.50	82.10	2.74	0.51	1.03	33.37	0.00	33.37	4.000	No	Yes	2.00
548	27.40	34.67	82.21	2.74	0.51	1.03	33.83	0.00	33.83	4.000	No	Yes	2.00
549	27.45	35.15	82.18	2.74	0.51	1.03	34.20	0.00	34.20	4.000	No	Yes	2.00
550	27.50	35.43	82.38	2.74	0.50	1.03	34.68	0.00	34.68	4.000	No	Yes	2.00
551	27.55	35.45	82.80	2.75	0.50	1.03	34.57	0.00	34.57	4.000	No	Yes	2.00
552	27.60	34.87	83.70	2.76	0.51	1.03	34.19	0.00	34.19	4.000	No	Yes	2.00
553	27.65	34.00	84.81	2.77	0.51	1.03	32.89	0.00	32.89	4.000	No	Yes	2.00
554	27.70	33.63	85.40	2.78	0.51	1.03	31.98	0.00	31.98	4.000	No	Yes	2.00
555	27.75	34.10	85.10	2.78	0.51	1.03	33.06	0.00	33.06	4.000	No	Yes	2.00
556	27.80	35.49	83.73	2.76	0.51	1.03	34.17	0.00	34.17	4.000	No	Yes	2.00
557	27.85	37.10	81.90	2.74	0.50	1.02	35.91	0.00	35.91	4.000	No	Yes	2.00
558	27.90	39.04	79.46	2.71	0.50	1.02	37.65	0.00	37.65	4.000	No	Yes	2.00
559	27.95	41.71	76.35	2.67	0.49	1.02	39.68	0.00	39.68	4.000	No	Yes	2.00
560	28.00	44.66	72.87	2.62	0.48	1.02	43.55	0.00	43.55	4.000	No	Yes	2.00
561	28.05	47.02	69.95	2.59	0.48	1.02	46.05	64.02	110.07	0.152	No	No	0.17
562	28.10	47.52	68.10	2.56	0.48	1.02	46.39	63.73	110.12	0.152	No	No	0.17
563	28.15	46.09	68.03	2.56	0.48	1.02	44.93	63.29	108.22	0.149	No	No	0.17
564	28.20	43.31	69.39	2.58	0.49	1.02	41.85	62.68	104.53	0.144	No	No	0.16
565	28.25	39.82	72.27	2.62	0.50	1.02	38.30	0.00	38.30	4.000	No	Yes	2.00
566	28.30	36.40	75.58	2.66	0.51	1.02	34.80	0.00	34.80	4.000	No	Yes	2.00
567	28.35	33.71	78.69	2.70	0.51	1.02	31.93	0.00	31.93	4.000	No	Yes	2.00
568	28.40	32.17	80.75	2.72	0.52	1.02	30.48	0.00	30.48	4.000	No	Yes	2.00
569	28.45	31.53	82.00	2.74	0.52	1.02	30.31	0.00	30.31	4.000	No	Yes	2.00
570	28.50	31.26	82.90	2.75	0.52	1.02	30.01	0.00	30.01	4.000	No	Yes	2.00
571	28.55	30.87	83.90	2.76	0.52	1.01	29.62	0.00	29.62	4.000	No	Yes	2.00
572	28.60	30.51	84.77	2.77	0.52	1.01	29.15	0.00	29.15	4.000	No	Yes	2.00
573	28.65	30.47	85.12	2.78	0.52	1.01	28.91	0.00	28.91	4.000	No	Yes	2.00
574	28.70	30.58	84.99	2.77	0.52	1.01	29.44	0.00	29.44	4.000	No	Yes	2.00
575	28.75	30.60	84.62	2.77	0.52	1.01	29.41	0.00	29.41	4.000	No	Yes	2.00
576	28.80	29.20	85.36	2.78	0.52	1.01	28.90	0.00	28.90	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
577	28.85	26.34	87.57	2.81	0.53	1.01	25.38	0.00	25.38	4.000	No	Yes	2.00
578	28.90	22.09	91.93	2.86	0.54	1.01	21.16	0.00	21.16	4.000	No	Yes	2.00
579	28.95	18.12	96.96	2.92	0.56	1.01	16.69	0.00	16.69	4.000	No	Yes	2.00
580	29.00	15.37	100.00	2.98	0.57	1.01	14.00	0.00	14.00	4.000	No	Yes	2.00
581	29.05	14.03	100.00	3.00	0.57	1.01	13.25	0.00	13.25	4.000	No	Yes	2.00
582	29.10	13.51	100.00	3.00	0.57	1.01	12.85	0.00	12.85	4.000	No	Yes	2.00
583	29.15	13.24	100.00	2.99	0.57	1.01	12.49	0.00	12.49	4.000	No	Yes	2.00
584	29.20	13.11	100.00	2.98	0.57	1.01	12.47	0.00	12.47	4.000	No	Yes	2.00
585	29.25	13.11	100.00	2.97	0.57	1.01	12.46	0.00	12.46	4.000	No	Yes	2.00
586	29.30	13.11	100.00	2.97	0.57	1.01	12.45	0.00	12.45	4.000	No	Yes	2.00
587	29.35	13.11	100.00	2.98	0.57	1.00	12.44	0.00	12.44	4.000	No	Yes	2.00
588	29.40	13.11	100.00	2.99	0.57	1.00	12.44	0.00	12.44	4.000	No	Yes	2.00
589	29.45	13.11	100.00	3.00	0.57	1.00	12.43	0.00	12.43	4.000	No	Yes	2.00
590	29.50	13.36	100.00	3.01	0.57	1.00	12.43	0.00	12.43	4.000	No	Yes	2.00
591	29.55	13.81	100.00	3.01	0.57	1.00	13.11	0.00	13.11	4.000	No	Yes	2.00
592	29.60	14.52	100.00	3.00	0.57	1.00	13.69	0.00	13.69	4.000	No	Yes	2.00
593	29.65	15.32	100.00	2.98	0.57	1.00	14.42	0.00	14.42	4.000	No	Yes	2.00
594	29.70	16.41	99.84	2.96	0.56	1.00	15.35	0.00	15.35	4.000	No	Yes	2.00
595	29.75	17.69	97.78	2.93	0.56	1.00	16.75	0.00	16.75	4.000	No	Yes	2.00
596	29.80	19.03	95.41	2.91	0.55	1.00	18.00	0.00	18.00	4.000	No	Yes	2.00
597	29.85	19.87	93.77	2.88	0.55	1.00	19.10	0.00	19.10	4.000	No	Yes	2.00
598	29.90	20.01	93.05	2.88	0.55	1.00	19.09	0.00	19.09	4.000	No	Yes	2.00
599	29.95	18.99	94.44	2.89	0.55	1.00	18.37	0.00	18.37	4.000	No	Yes	2.00
600	30.00	18.18	95.79	2.91	0.56	1.00	16.18	0.00	16.18	4.000	No	Yes	2.00
601	30.05	18.22	95.58	2.91	0.56	1.00	16.77	0.00	16.77	4.000	No	Yes	2.00
602	30.10	20.31	91.71	2.86	0.55	0.99	18.45	0.00	18.45	4.000	No	Yes	2.00
603	30.15	23.10	87.01	2.80	0.54	0.99	22.02	0.00	22.02	4.000	No	Yes	2.00
604	30.20	25.29	83.76	2.76	0.53	0.99	24.61	0.00	24.61	4.000	No	Yes	2.00
605	30.25	26.11	82.81	2.75	0.54	0.99	24.59	0.00	24.59	4.000	No	Yes	2.00
606	30.30	25.75	84.02	2.76	0.54	0.99	24.27	0.00	24.27	4.000	No	Yes	2.00
607	30.35	25.28	86.22	2.79	0.54	0.99	23.53	0.00	23.53	4.000	No	Yes	2.00
608	30.40	24.92	89.07	2.83	0.54	0.99	23.23	0.00	23.23	4.000	No	Yes	2.00
609	30.45	26.19	90.39	2.84	0.54	0.99	23.20	0.00	23.20	4.000	No	Yes	2.00
610	30.50	28.97	90.09	2.84	0.53	0.99	27.04	0.00	27.04	4.000	Yes	Yes	2.00
611	30.55	34.13	87.19	2.80	0.51	0.99	30.98	0.00	30.98	4.000	Yes	Yes	2.00
612	30.60	40.03	83.47	2.76	0.50	0.99	37.61	0.00	37.61	4.000	Yes	Yes	2.00
613	30.65	47.16	78.44	2.69	0.48	0.99	43.54	0.00	43.54	4.000	Yes	Yes	2.00
614	30.70	53.35	73.48	2.63	0.46	0.99	50.91	0.00	50.91	4.000	Yes	Yes	2.00
615	30.75	58.70	68.64	2.57	0.45	0.99	54.91	66.32	121.23	4.000	Yes	No	2.00
616	30.80	62.66	64.39	2.52	0.45	0.99	58.46	66.32	124.79	4.000	Yes	No	2.00
617	30.85	66.56	60.51	2.47	0.44	0.99	61.91	66.23	128.14	4.000	Yes	No	2.00
618	30.90	71.42	56.71	2.42	0.43	0.99	65.73	66.07	131.80	4.000	Yes	No	2.00
619	30.95	76.82	53.01	2.38	0.42	0.99	71.99	66.38	138.38	4.000	Yes	No	2.00
620	31.00	82.78	49.33	2.33	0.41	0.99	76.95	66.07	143.02	4.000	Yes	No	2.00
621	31.05	88.37	45.71	2.28	0.41	0.99	82.31	65.55	147.86	4.000	Yes	No	2.00
622	31.10	93.74	42.42	2.24	0.40	0.99	87.55	64.80	152.35	4.000	Yes	No	2.00
623	31.15	98.72	39.69	2.21	0.39	0.98	91.85	63.84	155.69	4.000	Yes	No	2.00
624	31.20	103.47	37.91	2.19	0.39	0.98	96.14	63.38	159.52	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
625	31.25	109.02	36.74	2.17	0.38	0.98	100.72	63.38	164.10	0.418	No	No	0.47
626	31.30	115.77	35.95	2.16	0.37	0.98	107.25	64.11	171.36	0.528	No	No	0.59
627	31.35	123.72	35.05	2.15	0.36	0.98	114.91	64.90	179.80	0.721	No	No	0.82
628	31.40	132.87	33.93	2.14	0.35	0.98	122.90	65.41	188.31	1.040	No	No	1.18
629	31.45	142.35	32.48	2.12	0.33	0.98	132.77	65.74	198.50	1.740	No	No	1.98
630	31.50	153.16	30.71	2.10	0.32	0.98	141.38	65.03	206.41	2.769	No	No	2.00
631	31.55	163.20	28.91	2.07	0.31	0.98	153.10	64.50	217.60	4.000	No	No	2.00
632	31.60	173.03	27.21	2.05	0.30	0.98	160.79	62.85	223.64	4.000	No	No	2.00
633	31.65	180.44	25.84	2.04	0.29	0.98	168.82	61.49	230.31	4.000	No	No	2.00
634	31.70	186.57	24.66	2.02	0.29	0.98	173.70	59.67	233.37	4.000	No	No	2.00
635	31.75	191.07	23.71	2.01	0.28	0.98	177.79	58.03	235.83	4.000	No	No	2.00
636	31.80	194.89	22.95	2.00	0.28	0.98	181.24	56.61	237.85	4.000	No	No	2.00
637	31.85	198.61	22.32	1.99	0.28	0.98	184.16	55.35	239.51	4.000	No	No	2.00
638	31.90	202.38	21.76	1.98	0.28	0.98	188.01	54.33	242.34	4.000	No	No	2.00
639	31.95	206.39	21.24	1.98	0.27	0.98	191.59	53.30	244.89	4.000	No	No	2.00
640	32.00	209.00	20.93	1.97	0.27	0.98	195.20	52.87	248.07	4.000	No	No	2.00
641	32.05	210.08	20.96	1.97	0.27	0.98	195.12	52.96	248.08	4.000	No	No	2.00
642	32.10	208.94	21.36	1.98	0.27	0.98	194.38	54.09	248.47	4.000	No	No	2.00
643	32.15	207.00	22.09	1.99	0.27	0.98	191.76	55.85	247.61	4.000	No	No	2.00
644	32.20	204.32	23.02	2.00	0.27	0.98	189.47	58.13	247.60	4.000	No	No	2.00
645	32.25	201.85	24.14	2.01	0.27	0.98	186.65	60.60	247.25	4.000	No	No	2.00
646	32.30	199.62	25.14	2.03	0.27	0.98	184.65	62.71	247.36	4.000	No	No	2.00
647	32.35	198.37	25.88	2.04	0.27	0.98	183.02	64.14	247.16	4.000	No	No	2.00
648	32.40	198.24	26.01	2.04	0.27	0.98	182.95	64.42	247.36	4.000	No	No	2.00
649	32.45	199.82	25.58	2.03	0.27	0.98	184.05	63.64	247.69	4.000	No	No	2.00
650	32.50	202.60	24.52	2.02	0.27	0.98	187.19	61.65	248.84	4.000	No	No	2.00
651	32.55	206.36	23.17	2.00	0.27	0.98	190.46	58.69	249.16	4.000	No	No	2.00
652	32.60	210.53	21.60	1.98	0.27	0.98	194.27	54.79	249.06	4.000	No	No	2.00
653	32.65	214.74	20.14	1.96	0.27	0.98	198.49	50.77	249.26	4.000	No	No	2.00
654	32.70	218.70	18.82	1.95	0.27	0.98	201.87	46.66	248.53	4.000	No	No	2.00
655	32.75	221.32	17.91	1.94	0.27	0.98	205.00	43.66	248.67	4.000	No	No	2.00
656	32.80	222.30	17.44	1.93	0.27	0.98	205.43	41.92	247.35	4.000	No	No	2.00
657	32.85	221.39	17.46	1.93	0.27	0.98	204.28	41.88	246.16	4.000	No	No	2.00
658	32.90	219.55	17.77	1.93	0.27	0.97	202.17	42.84	245.01	4.000	No	No	2.00
659	32.95	217.58	18.17	1.94	0.28	0.97	200.00	44.08	244.08	4.000	No	No	2.00
660	33.00	215.84	18.42	1.94	0.28	0.97	198.52	44.80	243.32	4.000	No	No	2.00
661	33.05	214.08	18.55	1.94	0.28	0.97	197.05	45.11	242.17	4.000	No	No	2.00
662	33.10	211.73	18.63	1.95	0.28	0.97	194.78	45.11	239.90	4.000	No	No	2.00
663	33.15	208.42	18.89	1.95	0.28	0.97	191.66	45.66	237.32	4.000	No	No	2.00
664	33.20	203.60	19.45	1.96	0.29	0.97	187.54	47.03	234.57	4.000	No	No	2.00
665	33.25	197.58	20.39	1.97	0.29	0.97	181.05	49.20	230.25	4.000	No	No	2.00
666	33.30	189.54	21.77	1.98	0.30	0.97	174.61	52.36	226.97	4.000	No	No	2.00
667	33.35	181.40	23.52	2.01	0.30	0.97	164.90	55.45	220.35	4.000	No	No	2.00
668	33.40	173.00	25.47	2.03	0.31	0.97	158.17	58.79	216.96	4.000	No	No	2.00
669	33.45	166.53	27.31	2.05	0.31	0.97	151.03	61.20	212.23	4.000	No	No	2.00
670	33.50	161.02	28.70	2.07	0.32	0.97	146.72	62.88	209.60	3.398	No	No	2.00
671	33.55	157.44	29.51	2.08	0.32	0.96	142.65	63.43	206.08	2.712	No	No	2.00
672	33.60	155.20	29.57	2.08	0.32	0.96	140.87	63.17	204.04	2.394	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
673	33.65	155.05	29.03	2.08	0.33	0.96	140.26	62.16	202.42	2.174	No	No	2.00
674	33.70	155.92	27.95	2.06	0.33	0.96	141.96	60.65	202.60	2.198	No	No	2.00
675	33.75	157.40	26.68	2.05	0.33	0.96	142.99	58.51	201.50	2.061	No	No	2.00
676	33.80	158.78	25.23	2.03	0.33	0.96	144.03	55.79	199.83	1.873	No	No	2.00
677	33.85	160.22	23.89	2.01	0.33	0.96	145.44	53.10	198.54	1.744	No	No	1.95
678	33.90	161.17	22.67	2.00	0.33	0.96	146.58	50.41	197.00	1.604	No	No	1.79
679	33.95	161.04	21.95	1.99	0.34	0.96	146.31	48.55	194.86	1.433	No	No	1.60
680	34.00	159.04	21.79	1.98	0.34	0.96	144.74	47.92	192.66	1.281	No	No	1.44
681	34.05	156.01	22.34	1.99	0.34	0.96	140.76	48.69	189.44	1.096	No	No	1.23
682	34.10	152.34	23.40	2.00	0.35	0.96	137.72	50.72	188.43	1.046	No	No	1.17
683	34.15	149.01	24.77	2.02	0.35	0.96	134.46	53.17	187.63	1.008	No	No	1.13
684	34.20	145.93	26.14	2.04	0.35	0.96	131.47	55.36	186.83	0.972	No	No	1.09
685	34.25	143.37	27.38	2.05	0.35	0.95	129.12	57.21	186.33	0.950	No	No	1.07
686	34.30	141.80	28.33	2.07	0.35	0.95	127.30	58.47	185.77	0.927	No	No	1.04
687	34.35	141.31	28.95	2.07	0.35	0.95	127.01	59.42	186.43	0.954	No	No	1.07
688	34.40	141.88	29.24	2.08	0.35	0.95	127.65	60.00	187.65	1.009	No	No	1.13
689	34.45	143.01	29.34	2.08	0.34	0.95	128.75	60.37	189.11	1.080	No	No	1.21
690	34.50	144.50	29.38	2.08	0.34	0.95	129.96	60.67	190.63	1.160	No	No	1.30
691	34.55	146.18	29.44	2.08	0.34	0.95	131.63	61.11	192.74	1.286	No	No	1.44
692	34.60	148.30	29.41	2.08	0.34	0.95	133.22	61.38	194.60	1.414	No	No	1.58
693	34.65	150.68	29.17	2.08	0.33	0.95	135.66	61.48	197.15	1.617	No	No	1.80
694	34.70	153.55	28.65	2.07	0.33	0.95	138.04	61.09	199.12	1.801	No	No	2.00
695	34.75	156.78	27.82	2.06	0.33	0.95	140.96	60.23	201.19	2.024	No	No	2.00
696	34.80	160.27	26.87	2.05	0.33	0.95	144.37	59.13	203.50	2.318	No	No	2.00
697	34.85	163.82	25.86	2.04	0.32	0.95	147.42	57.70	205.12	2.556	No	No	2.00
698	34.90	166.56	25.17	2.03	0.32	0.95	150.53	56.80	207.33	2.933	No	No	2.00
699	34.95	168.16	24.85	2.02	0.32	0.95	151.69	56.32	208.01	3.064	No	No	2.00
700	35.00	168.07	25.14	2.03	0.32	0.95	151.64	56.93	208.57	3.176	No	No	2.00
701	35.05	166.85	25.77	2.03	0.32	0.95	150.11	57.99	208.10	3.081	No	No	2.00
702	35.10	165.03	26.67	2.05	0.32	0.95	148.19	59.46	207.65	2.994	No	No	2.00
703	35.15	163.32	27.54	2.06	0.32	0.95	146.47	60.77	207.24	2.917	No	No	2.00
704	35.20	162.03	28.29	2.07	0.32	0.95	145.27	61.89	207.16	2.902	No	No	2.00
705	35.25	161.27	28.79	2.07	0.32	0.95	144.50	62.60	207.10	2.891	No	No	2.00
706	35.30	160.94	29.09	2.08	0.32	0.95	144.25	63.05	207.30	2.927	No	No	2.00
707	35.35	161.08	29.18	2.08	0.32	0.95	144.19	63.18	207.37	2.941	No	No	2.00
708	35.40	161.52	29.16	2.08	0.32	0.95	144.70	63.26	207.97	3.055	No	No	2.00
709	35.45	162.34	29.07	2.08	0.32	0.95	145.28	63.22	208.50	3.162	No	No	2.00
710	35.50	163.26	28.96	2.07	0.32	0.95	146.27	63.23	209.50	3.374	No	No	2.00
711	35.55	164.33	28.82	2.07	0.32	0.95	147.05	63.15	210.20	3.534	No	No	2.00
712	35.60	165.51	28.60	2.07	0.32	0.95	148.05	62.97	211.02	3.734	No	No	2.00
713	35.65	166.97	28.28	2.07	0.31	0.95	149.31	62.65	211.95	3.978	No	No	2.00
714	35.70	168.87	27.78	2.06	0.31	0.95	150.85	62.05	212.90	4.000	No	No	2.00
715	35.75	171.00	27.26	2.05	0.31	0.95	153.07	61.49	214.56	4.000	No	No	2.00
716	35.80	173.32	26.73	2.05	0.31	0.95	154.96	60.82	215.78	4.000	No	No	2.00
717	35.85	175.30	26.31	2.04	0.31	0.95	157.02	60.36	217.38	4.000	No	No	2.00
718	35.90	177.07	25.95	2.04	0.31	0.95	158.32	59.85	218.17	4.000	No	No	2.00
719	35.95	178.13	25.74	2.03	0.31	0.95	159.64	59.65	219.29	4.000	No	No	2.00
720	36.00	178.63	25.70	2.03	0.31	0.95	159.72	59.56	219.28	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
721	36.05	177.88	25.91	2.04	0.30	0.95	159.50	59.98	219.48	4.000	No	No	2.00
722	36.10	176.26	26.29	2.04	0.31	0.94	157.37	60.38	217.76	4.000	No	No	2.00
723	36.15	173.28	26.89	2.05	0.31	0.94	155.07	61.15	216.22	4.000	No	No	2.00
724	36.20	169.82	27.62	2.06	0.31	0.94	151.09	61.79	212.87	4.000	No	No	2.00
725	36.25	165.72	28.47	2.07	0.32	0.94	147.66	62.66	210.32	3.564	No	No	2.00
726	36.30	161.89	29.30	2.08	0.32	0.94	143.60	63.27	206.88	2.851	No	No	2.00
727	36.35	157.98	30.02	2.09	0.32	0.94	140.35	63.77	204.12	2.405	No	No	2.00
728	36.40	152.84	30.82	2.10	0.33	0.94	136.73	64.24	200.97	1.999	No	No	2.00
729	36.45	146.42	31.65	2.11	0.34	0.94	129.27	63.86	193.14	1.312	No	No	1.45
730	36.50	137.93	32.77	2.12	0.35	0.93	122.52	63.90	186.42	0.954	No	No	1.06
731	36.55	131.24	33.46	2.13	0.36	0.93	113.23	62.73	175.96	0.622	No	No	0.69
732	36.60	126.58	33.79	2.13	0.37	0.93	110.76	62.56	173.32	0.565	No	No	0.62
733	36.65	126.90	33.05	2.13	0.37	0.93	109.54	61.43	170.97	0.521	No	No	0.57
734	36.70	129.22	32.12	2.11	0.36	0.93	113.88	61.23	175.11	0.603	No	No	0.67
735	36.75	132.57	31.24	2.10	0.36	0.93	116.85	60.70	177.55	0.660	No	No	0.73
736	36.80	132.90	31.60	2.11	0.36	0.93	118.51	61.53	180.04	4.000	Yes	No	2.00
737	36.85	129.15	33.29	2.13	0.36	0.93	114.66	62.84	177.50	4.000	Yes	No	2.00
738	36.90	120.57	37.05	2.18	0.37	0.93	106.64	65.04	171.68	4.000	Yes	No	2.00
739	36.95	109.20	42.13	2.24	0.38	0.92	95.22	66.50	161.72	4.000	Yes	No	2.00
740	37.00	96.25	48.55	2.32	0.40	0.92	83.92	67.51	151.43	4.000	Yes	No	2.00
741	37.05	83.85	55.26	2.40	0.42	0.91	71.70	67.18	138.88	4.000	Yes	No	2.00
742	37.10	71.18	62.60	2.50	0.44	0.91	61.96	66.84	128.80	4.000	Yes	No	2.00
743	37.15	60.50	69.81	2.59	0.47	0.91	50.11	65.18	115.29	4.000	Yes	No	2.00
744	37.20	51.00	76.89	2.67	0.48	0.90	43.37	0.00	43.37	4.000	Yes	Yes	2.00
745	37.25	44.67	82.40	2.74	0.50	0.90	36.91	0.00	36.91	4.000	Yes	Yes	2.00
746	37.30	39.79	86.49	2.79	0.51	0.90	33.51	0.00	33.51	4.000	Yes	Yes	2.00
747	37.35	36.21	89.25	2.83	0.51	0.89	30.62	0.00	30.62	4.000	Yes	Yes	2.00
748	37.40	33.31	90.99	2.85	0.52	0.89	27.61	0.00	27.61	4.000	Yes	Yes	2.00
749	37.45	31.01	92.06	2.86	0.53	0.89	25.97	0.00	25.97	4.000	No	Yes	2.00
750	37.50	29.53	92.26	2.87	0.53	0.89	24.66	0.00	24.66	4.000	No	Yes	2.00
751	37.55	28.34	92.32	2.87	0.54	0.89	23.77	0.00	23.77	4.000	No	Yes	2.00
752	37.60	27.15	92.45	2.87	0.54	0.89	22.87	0.00	22.87	4.000	No	Yes	2.00
753	37.65	26.61	92.19	2.86	0.54	0.89	21.59	0.00	21.59	4.000	No	Yes	2.00
754	37.70	28.33	89.61	2.83	0.54	0.89	22.35	0.00	22.35	4.000	No	Yes	2.00
755	37.75	31.84	86.65	2.80	0.53	0.89	27.22	0.00	27.22	4.000	No	Yes	2.00
756	37.80	36.44	84.01	2.76	0.52	0.89	30.54	0.00	30.54	4.000	No	Yes	2.00
757	37.85	38.93	84.35	2.77	0.50	0.89	34.08	0.00	34.08	4.000	No	Yes	2.00
758	37.90	40.34	85.08	2.78	0.51	0.89	33.58	0.00	33.58	4.000	No	Yes	2.00
759	37.95	43.01	84.37	2.77	0.50	0.89	34.12	0.00	34.12	4.000	Yes	Yes	2.00
760	38.00	48.68	80.11	2.71	0.49	0.89	40.90	0.00	40.90	4.000	Yes	Yes	2.00
761	38.05	58.51	72.92	2.62	0.47	0.90	48.21	0.00	48.21	4.000	Yes	Yes	2.00
762	38.10	69.29	64.59	2.52	0.44	0.90	59.65	66.72	126.37	4.000	Yes	No	2.00
763	38.15	81.00	56.03	2.41	0.43	0.90	69.02	66.73	135.75	4.000	Yes	No	2.00
764	38.20	91.48	47.56	2.31	0.41	0.91	78.90	65.68	144.59	4.000	Yes	No	2.00
765	38.25	100.61	40.47	2.22	0.40	0.91	87.17	63.31	150.48	4.000	Yes	No	2.00
766	38.30	107.26	34.64	2.15	0.40	0.91	92.89	59.54	152.43	4.000	Yes	No	2.00
767	38.35	110.81	31.26	2.10	0.40	0.91	96.18	56.41	152.59	4.000	Yes	No	2.00
768	38.40	111.54	29.52	2.08	0.40	0.91	96.18	54.12	150.30	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
769	38.45	110.10	29.74	2.08	0.41	0.91	94.48	54.08	148.55	0.280	No	No	0.30
770	38.50	107.73	30.85	2.10	0.41	0.91	92.15	55.06	147.21	0.271	No	No	0.30
771	38.55	104.98	32.76	2.12	0.41	0.90	89.84	56.84	146.68	0.268	No	No	0.29
772	38.60	102.27	34.86	2.15	0.41	0.90	87.17	58.47	145.65	0.263	No	No	0.29
773	38.65	99.41	37.19	2.18	0.41	0.90	85.01	60.15	145.16	0.260	No	No	0.28
774	38.70	97.36	39.11	2.20	0.41	0.90	82.27	61.09	143.36	0.250	No	No	0.27
775	38.75	96.13	40.43	2.22	0.41	0.90	81.72	61.96	143.68	0.252	No	No	0.27
776	38.80	96.51	40.59	2.22	0.41	0.90	81.68	62.07	143.75	0.252	No	No	0.27
777	38.85	97.65	39.99	2.21	0.41	0.90	83.20	62.00	145.19	0.260	No	No	0.28
778	38.90	99.57	38.68	2.20	0.41	0.90	84.60	61.31	145.90	0.264	No	No	0.29
779	38.95	101.45	37.38	2.18	0.41	0.90	86.58	60.68	147.26	0.272	No	No	0.30
780	39.00	103.41	36.17	2.16	0.41	0.90	87.99	59.92	147.91	0.276	No	No	0.30
781	39.05	104.30	35.91	2.16	0.40	0.90	89.62	60.05	149.67	0.287	No	No	0.31
782	39.10	104.12	36.45	2.17	0.40	0.90	88.77	60.36	149.13	4.000	Yes	No	2.00
783	39.15	102.07	38.25	2.19	0.40	0.90	87.45	61.63	149.08	4.000	Yes	No	2.00
784	39.20	99.25	40.65	2.22	0.41	0.90	84.17	62.72	146.89	4.000	Yes	No	2.00
785	39.25	95.46	43.76	2.26	0.41	0.90	81.32	64.12	145.44	4.000	Yes	No	2.00
786	39.30	91.24	47.27	2.30	0.42	0.90	77.45	65.16	142.61	4.000	Yes	No	2.00
787	39.35	85.91	51.29	2.35	0.42	0.89	73.05	65.94	138.98	4.000	Yes	No	2.00
788	39.40	80.34	55.64	2.41	0.43	0.89	67.25	66.11	133.36	4.000	Yes	No	2.00
789	39.45	74.97	59.80	2.46	0.44	0.89	62.80	66.26	129.06	4.000	Yes	No	2.00
790	39.50	70.67	63.59	2.51	0.45	0.89	58.95	66.25	125.21	4.000	Yes	No	2.00
791	39.55	67.29	66.43	2.54	0.45	0.89	55.99	66.12	122.11	4.000	Yes	No	2.00
792	39.60	64.57	68.57	2.57	0.46	0.88	53.94	66.02	119.96	4.000	Yes	No	2.00
793	39.65	63.21	69.10	2.58	0.46	0.88	51.83	65.52	117.35	0.166	No	No	0.18
794	39.70	63.09	68.53	2.57	0.46	0.88	52.37	65.56	117.93	4.000	Yes	No	2.00
795	39.75	64.30	66.93	2.55	0.46	0.88	53.53	65.53	119.06	4.000	Yes	No	2.00
796	39.80	65.78	65.45	2.53	0.46	0.88	54.84	65.55	120.39	4.000	Yes	No	2.00
797	39.85	67.57	63.98	2.51	0.45	0.88	56.10	65.54	121.64	4.000	Yes	No	2.00
798	39.90	69.92	61.66	2.48	0.45	0.88	58.06	65.48	123.54	4.000	Yes	No	2.00
799	39.95	73.38	58.00	2.44	0.45	0.88	60.79	65.13	125.93	4.000	Yes	No	2.00
800	40.00	76.70	53.62	2.38	0.44	0.88	64.93	64.71	129.64	4.000	Yes	No	2.00
801	40.05	79.39	49.97	2.34	0.44	0.88	66.51	63.61	130.11	4.000	Yes	No	2.00
802	40.10	80.09	48.46	2.32	0.44	0.88	67.60	63.19	130.80	4.000	Yes	No	2.00
803	40.15	79.80	48.67	2.32	0.44	0.88	66.59	63.02	129.61	0.196	No	No	0.21
804	40.20	78.56	50.05	2.34	0.44	0.88	65.65	63.42	129.07	0.195	No	No	0.21
805	40.25	77.27	51.49	2.36	0.44	0.88	64.29	63.68	127.98	0.192	No	No	0.21
806	40.30	75.86	52.95	2.37	0.44	0.88	63.18	63.98	127.16	0.189	No	No	0.20
807	40.35	74.61	54.11	2.39	0.45	0.88	61.93	64.09	126.01	0.186	No	No	0.20
808	40.40	73.46	54.84	2.40	0.45	0.88	60.98	64.10	125.08	0.184	No	No	0.20
809	40.45	72.40	55.01	2.40	0.45	0.88	60.13	63.93	124.06	0.181	No	No	0.20
810	40.50	71.39	54.82	2.40	0.45	0.88	59.09	63.58	122.67	0.178	No	No	0.19
811	40.55	70.32	54.47	2.39	0.45	0.88	58.26	63.22	121.48	0.175	No	No	0.19
812	40.60	68.99	54.85	2.40	0.46	0.88	57.25	63.08	120.34	4.000	Yes	No	2.00
813	40.65	67.26	56.09	2.41	0.46	0.87	55.60	63.06	118.66	4.000	Yes	No	2.00
814	40.70	64.92	58.81	2.45	0.46	0.87	53.75	63.43	117.18	4.000	Yes	No	2.00
815	40.75	62.36	62.01	2.49	0.47	0.87	51.21	63.63	114.84	4.000	Yes	No	2.00
816	40.80	59.39	65.80	2.53	0.47	0.87	49.01	63.97	112.98	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
817	40.85	56.83	68.86	2.57	0.48	0.87	46.12	63.81	109.93	4.000	Yes	No	2.00
818	40.90	54.64	71.34	2.60	0.48	0.87	44.65	0.00	44.65	4.000	Yes	Yes	2.00
819	40.95	54.44	71.71	2.61	0.48	0.87	43.39	0.00	43.39	4.000	Yes	Yes	2.00
820	41.00	55.85	70.49	2.59	0.48	0.87	45.53	63.98	109.51	4.000	Yes	No	2.00
821	41.05	59.98	66.82	2.55	0.47	0.87	48.13	63.95	112.08	4.000	Yes	No	2.00
822	41.10	65.10	62.39	2.49	0.46	0.87	53.82	64.47	118.29	4.000	Yes	No	2.00
823	41.15	71.52	57.07	2.43	0.45	0.87	58.47	64.18	122.66	4.000	Yes	No	2.00
824	41.20	77.66	52.25	2.37	0.44	0.87	64.42	64.03	128.45	4.000	Yes	No	2.00
825	41.25	84.09	47.59	2.31	0.43	0.88	69.42	63.24	132.66	4.000	Yes	No	2.00
826	41.30	90.57	43.25	2.25	0.43	0.88	74.85	62.18	137.04	4.000	Yes	No	2.00
827	41.35	97.02	39.16	2.20	0.42	0.88	80.95	60.82	141.77	4.000	Yes	No	2.00
828	41.40	103.34	35.19	2.15	0.41	0.88	85.86	58.50	144.36	4.000	Yes	No	2.00
829	41.45	108.53	31.98	2.11	0.41	0.88	90.94	56.18	147.11	4.000	Yes	No	2.00
830	41.50	113.02	29.18	2.08	0.41	0.88	94.02	53.22	147.24	4.000	Yes	No	2.00
831	41.55	115.16	27.59	2.06	0.41	0.88	97.15	51.49	148.64	4.000	Yes	No	2.00
832	41.60	115.36	26.88	2.05	0.41	0.88	96.11	50.18	146.28	0.266	No	No	0.29
833	41.65	111.94	27.80	2.06	0.41	0.88	94.33	51.27	145.60	4.000	Yes	No	2.00
834	41.70	106.66	29.84	2.09	0.42	0.88	88.13	52.94	141.07	4.000	Yes	No	2.00
835	41.75	98.88	33.42	2.13	0.42	0.87	82.50	55.97	138.47	4.000	Yes	No	2.00
836	41.80	90.96	38.21	2.19	0.43	0.87	74.31	58.49	132.80	4.000	Yes	No	2.00
837	41.85	82.43	44.14	2.26	0.44	0.87	67.90	60.97	128.87	4.000	Yes	No	2.00
838	41.90	75.38	50.17	2.34	0.45	0.87	60.74	62.17	122.91	4.000	Yes	No	2.00
839	41.95	69.28	55.58	2.41	0.46	0.86	56.36	63.10	119.46	4.000	Yes	No	2.00
840	42.00	64.01	60.44	2.47	0.46	0.86	52.37	63.53	115.90	4.000	Yes	No	2.00
841	42.05	59.15	64.99	2.52	0.48	0.86	47.37	63.30	110.67	4.000	Yes	No	2.00
842	42.10	54.53	69.70	2.58	0.48	0.86	44.07	63.39	107.46	4.000	Yes	No	2.00
843	42.15	51.91	73.05	2.63	0.49	0.85	40.69	0.00	40.69	4.000	Yes	Yes	2.00
844	42.20	50.83	75.11	2.65	0.49	0.85	40.75	0.00	40.75	4.000	Yes	Yes	2.00
845	42.25	51.46	75.27	2.65	0.49	0.85	41.31	0.00	41.31	4.000	No	Yes	2.00
846	42.30	52.30	74.82	2.65	0.49	0.85	42.21	0.00	42.21	4.000	No	Yes	2.00
847	42.35	53.04	73.93	2.64	0.48	0.85	42.79	0.00	42.79	4.000	No	Yes	2.00
848	42.40	53.37	73.38	2.63	0.48	0.85	43.09	0.00	43.09	4.000	No	Yes	2.00
849	42.45	53.34	73.27	2.63	0.48	0.85	42.97	0.00	42.97	4.000	No	Yes	2.00
850	42.50	52.74	74.13	2.64	0.48	0.85	42.64	0.00	42.64	4.000	No	Yes	2.00
851	42.55	51.69	75.57	2.66	0.49	0.85	41.53	0.00	41.53	4.000	No	Yes	2.00
852	42.60	49.87	77.92	2.69	0.49	0.85	40.30	0.00	40.30	4.000	No	Yes	2.00
853	42.65	47.83	80.57	2.72	0.49	0.85	38.07	0.00	38.07	4.000	No	Yes	2.00
854	42.70	45.50	83.75	2.76	0.50	0.85	36.40	0.00	36.40	4.000	No	Yes	2.00
855	42.75	44.11	86.19	2.79	0.50	0.84	34.48	0.00	34.48	4.000	No	Yes	2.00
856	42.80	43.65	87.82	2.81	0.50	0.84	34.58	0.00	34.58	4.000	No	Yes	2.00
857	42.85	45.52	87.05	2.80	0.50	0.84	35.21	0.00	35.21	4.000	Yes	Yes	2.00
858	42.90	48.86	84.77	2.77	0.49	0.85	39.06	0.00	39.06	4.000	Yes	Yes	2.00
859	42.95	54.26	80.47	2.72	0.48	0.85	42.80	0.00	42.80	4.000	Yes	Yes	2.00
860	43.00	59.96	75.75	2.66	0.47	0.85	48.58	0.00	48.58	4.000	Yes	Yes	2.00
861	43.05	66.38	70.24	2.59	0.46	0.85	53.22	66.17	119.39	4.000	Yes	No	2.00
862	43.10	71.78	65.21	2.53	0.45	0.86	58.86	66.65	125.51	4.000	Yes	No	2.00
863	43.15	76.39	60.48	2.47	0.44	0.86	62.10	66.27	128.37	4.000	Yes	No	2.00
864	43.20	78.77	56.99	2.42	0.44	0.86	64.78	65.90	130.68	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
865	43.25	79.71	54.69	2.40	0.44	0.86	64.71	65.06	129.78	4.000	Yes	No	2.00
866	43.30	79.20	54.00	2.39	0.44	0.86	64.34	64.70	129.05	0.195	No	No	0.21
867	43.35	78.76	54.56	2.39	0.44	0.86	63.33	64.64	127.97	4.000	Yes	No	2.00
868	43.40	78.69	55.90	2.41	0.44	0.86	63.51	65.17	128.68	4.000	Yes	No	2.00
869	43.45	78.43	57.83	2.44	0.44	0.86	64.12	66.00	130.12	4.000	Yes	No	2.00
870	43.50	77.44	60.10	2.46	0.44	0.86	62.64	66.31	128.95	4.000	Yes	No	2.00
871	43.55	74.94	63.00	2.50	0.44	0.85	60.99	66.68	127.67	4.000	Yes	No	2.00
872	43.60	72.49	65.68	2.53	0.45	0.85	57.72	66.44	124.16	4.000	Yes	No	2.00
873	43.65	70.55	68.11	2.56	0.45	0.85	56.38	66.63	123.01	4.000	Yes	No	2.00
874	43.70	71.50	68.80	2.57	0.45	0.85	56.04	66.68	122.72	0.178	No	No	0.19
875	43.75	74.94	68.08	2.56	0.44	0.85	60.06	67.68	127.74	4.000	Yes	No	2.00
876	43.80	80.85	65.54	2.53	0.43	0.86	65.05	68.50	133.55	4.000	Yes	No	2.00
877	43.85	87.12	62.46	2.49	0.42	0.86	70.99	69.36	140.35	4.000	Yes	No	2.00
878	43.90	93.83	58.64	2.45	0.41	0.86	75.96	69.56	145.53	4.000	Yes	No	2.00
879	43.95	101.14	54.67	2.40	0.40	0.86	82.12	69.80	151.92	4.000	Yes	No	2.00
880	44.00	110.53	50.02	2.34	0.39	0.87	89.69	69.77	159.46	4.000	Yes	No	2.00
881	44.05	121.59	45.43	2.28	0.37	0.87	100.17	69.94	170.11	4.000	Yes	No	2.00
882	44.10	133.55	40.99	2.22	0.36	0.88	110.81	69.47	180.28	4.000	Yes	No	2.00
883	44.15	145.66	36.86	2.17	0.34	0.88	120.89	68.16	189.06	4.000	Yes	No	2.00
884	44.20	156.89	33.10	2.13	0.33	0.88	131.92	66.36	198.28	4.000	Yes	No	2.00
885	44.25	168.00	29.41	2.08	0.33	0.89	140.21	62.78	202.99	4.000	Yes	No	2.00
886	44.30	177.83	26.61	2.05	0.32	0.89	149.96	59.67	209.63	4.000	Yes	No	2.00
887	44.35	187.59	24.50	2.02	0.31	0.89	157.62	56.55	214.17	4.000	Yes	No	2.00
888	44.40	196.04	23.31	2.00	0.30	0.89	165.96	55.09	221.05	4.000	No	No	2.00
889	44.45	203.45	22.42	1.99	0.30	0.89	172.39	53.79	226.18	4.000	No	No	2.00
890	44.50	209.43	21.74	1.98	0.29	0.90	177.45	52.67	230.13	4.000	No	No	2.00
891	44.55	214.10	21.22	1.98	0.29	0.90	181.95	51.85	233.80	4.000	No	No	2.00
892	44.60	217.99	20.81	1.97	0.28	0.90	184.84	51.02	235.85	4.000	No	No	2.00
893	44.65	220.70	20.53	1.97	0.28	0.90	187.85	50.58	238.43	4.000	No	No	2.00
894	44.70	222.71	20.34	1.97	0.28	0.90	189.13	50.13	239.26	4.000	No	No	2.00
895	44.75	223.47	20.28	1.97	0.28	0.90	190.12	50.07	240.20	4.000	No	No	2.00
896	44.80	223.50	20.29	1.97	0.28	0.90	189.71	50.07	239.78	4.000	No	No	2.00
897	44.85	222.63	20.40	1.97	0.28	0.90	189.03	50.34	239.37	4.000	No	No	2.00
898	44.90	221.39	20.56	1.97	0.28	0.90	187.56	50.62	238.17	4.000	No	No	2.00
899	44.95	219.77	20.75	1.97	0.28	0.90	186.15	51.02	237.17	4.000	No	No	2.00
900	45.00	218.21	20.94	1.97	0.28	0.90	184.45	51.37	235.82	4.000	No	No	2.00
901	45.05	216.72	21.13	1.98	0.29	0.89	183.12	51.74	234.86	4.000	No	No	2.00
902	45.10	215.31	21.31	1.98	0.29	0.89	181.91	52.09	234.00	4.000	No	No	2.00
903	45.15	213.85	21.49	1.98	0.29	0.89	180.46	52.41	232.87	4.000	No	No	2.00
904	45.20	212.05	21.71	1.98	0.29	0.89	178.99	52.84	231.84	4.000	No	No	2.00
905	45.25	210.12	21.96	1.99	0.29	0.89	176.86	53.21	230.07	4.000	No	No	2.00
906	45.30	208.04	22.22	1.99	0.29	0.89	175.04	53.66	228.70	4.000	No	No	2.00
907	45.35	206.23	22.52	1.99	0.29	0.89	173.20	54.19	227.38	4.000	No	No	2.00
908	45.40	204.69	22.85	2.00	0.30	0.89	171.84	54.84	226.69	4.000	No	No	2.00
909	45.45	203.43	23.21	2.00	0.30	0.89	170.81	55.63	226.43	4.000	No	No	2.00
910	45.50	202.70	23.44	2.01	0.30	0.89	169.72	56.04	225.75	4.000	No	No	2.00
911	45.55	202.59	23.47	2.01	0.30	0.89	169.76	56.11	225.87	4.000	No	No	2.00
912	45.60	203.21	23.28	2.00	0.30	0.89	170.33	55.72	226.06	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
913	45.65	204.10	23.00	2.00	0.30	0.89	171.14	55.14	226.28	4.000	No	No	2.00
914	45.70	204.99	22.80	2.00	0.30	0.89	171.88	54.72	226.60	4.000	No	No	2.00
915	45.75	205.81	22.64	2.00	0.30	0.89	172.49	54.41	226.89	4.000	No	No	2.00
916	45.80	206.70	22.46	1.99	0.30	0.89	173.09	54.02	227.11	4.000	No	No	2.00
917	45.85	207.49	22.12	1.99	0.30	0.89	174.01	53.23	227.23	4.000	No	No	2.00
918	45.90	208.14	21.53	1.98	0.30	0.89	174.21	51.60	225.80	4.000	No	No	2.00
919	45.95	208.40	20.66	1.97	0.30	0.88	174.21	49.04	223.26	4.000	No	No	2.00
920	46.00	208.46	19.57	1.96	0.30	0.88	173.82	45.61	219.43	4.000	No	No	2.00
921	46.05	208.14	18.23	1.94	0.31	0.88	173.15	41.10	214.25	4.000	No	No	2.00
922	46.10	207.68	16.80	1.92	0.32	0.88	171.86	35.91	207.77	3.017	No	No	2.00
923	46.15	207.15	15.14	1.90	0.33	0.87	170.75	29.55	200.30	1.924	No	No	2.00
924	46.20	207.36	13.57	1.88	0.34	0.87	169.69	23.30	192.99	1.303	No	No	1.39
925	46.25	208.33	12.02	1.86	0.35	0.87	170.27	17.19	187.46	1.000	No	No	1.08
926	46.30	210.67	10.78	1.85	0.35	0.86	171.34	12.47	183.81	0.851	No	No	0.92
927	46.35	213.60	9.67	1.83	0.35	0.86	174.24	8.67	182.91	0.819	No	No	0.88
928	46.40	217.34	8.63	1.82	0.35	0.86	176.73	5.56	182.29	0.798	No	No	0.86
929	46.45	220.91	7.58	1.81	0.35	0.86	180.24	3.07	183.32	0.833	No	No	0.90
930	46.50	224.61	6.36	1.79	0.35	0.86	182.89	1.15	184.04	0.859	No	No	0.93
931	46.55	227.82	5.11	1.78	0.35	0.86	186.00	0.25	186.24	0.946	No	No	1.02
932	46.60	230.78	3.80	1.76	0.35	0.86	188.46	0.02	188.48	1.048	No	No	1.13
933	46.65	232.99	2.68	1.75	0.34	0.86	190.67	0.00	190.67	1.162	No	No	1.25
934	46.70	234.26	1.72	1.73	0.34	0.86	191.82	0.00	191.82	1.229	No	No	1.32
935	46.75	234.70	0.78	1.72	0.34	0.86	191.74	0.00	191.74	1.225	No	No	1.31
936	46.80	234.70	0.00	1.71	0.34	0.86	191.66	0.00	191.66	1.220	No	No	1.31
937	46.85	234.70	0.00	1.70	0.34	0.86	191.59	0.00	191.59	1.215	No	No	1.30
938	46.90	234.57	0.00	1.68	0.34	0.86	191.51	0.00	191.51	1.211	No	No	1.30
939	46.95	233.63	0.00	1.67	0.34	0.86	191.08	0.00	191.08	1.186	No	No	1.27
940	47.00	231.40	0.00	1.66	0.34	0.86	188.78	0.00	188.78	1.063	No	No	1.14
941	47.05	227.32	0.00	1.65	0.35	0.86	185.16	0.00	185.16	0.902	No	No	0.97
942	47.10	221.14	0.00	1.66	0.36	0.86	179.67	0.00	179.67	0.717	No	No	0.77
943	47.15	213.26	0.00	1.68	0.37	0.85	171.67	0.00	171.67	0.533	No	No	0.58
944	47.20	204.49	0.07	1.71	0.38	0.85	163.50	0.00	163.50	4.000	Yes	No	2.00
945	47.25	195.41	2.68	1.75	0.39	0.84	155.71	0.00	155.71	4.000	Yes	No	2.00
946	47.30	186.26	5.65	1.78	0.41	0.84	147.07	0.47	147.54	4.000	Yes	No	2.00
947	47.35	175.48	9.97	1.84	0.41	0.84	139.85	8.71	148.57	4.000	Yes	No	2.00
948	47.40	163.92	15.14	1.90	0.39	0.84	129.78	26.05	155.84	4.000	Yes	No	2.00
949	47.45	150.98	21.45	1.98	0.38	0.85	121.01	43.53	164.54	4.000	Yes	No	2.00
950	47.50	138.23	27.96	2.06	0.38	0.85	110.29	54.57	164.87	4.000	Yes	No	2.00
951	47.55	125.91	34.83	2.15	0.39	0.84	99.62	61.23	160.86	4.000	Yes	No	2.00
952	47.60	114.57	41.94	2.24	0.39	0.84	90.80	65.27	156.08	4.000	Yes	No	2.00
953	47.65	106.12	48.30	2.32	0.41	0.83	82.10	66.91	149.01	4.000	Yes	No	2.00
954	47.70	100.59	53.89	2.39	0.41	0.83	78.56	68.52	147.08	4.000	Yes	No	2.00
955	47.75	98.14	57.88	2.44	0.41	0.83	77.02	69.60	146.62	4.000	Yes	No	2.00
956	47.80	96.75	61.34	2.48	0.41	0.83	76.05	70.46	146.50	4.000	Yes	No	2.00
957	47.85	95.75	63.91	2.51	0.41	0.83	75.13	70.95	146.08	4.000	Yes	No	2.00
958	47.90	95.51	65.73	2.53	0.41	0.83	74.49	71.26	145.75	4.000	Yes	No	2.00
959	47.95	97.24	65.93	2.54	0.41	0.83	75.41	71.58	146.99	0.270	No	No	0.29
960	48.00	100.39	65.09	2.53	0.40	0.83	79.45	72.51	151.96	0.302	No	No	0.33

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
961	48.05	104.45	63.28	2.50	0.40	0.84	82.37	72.83	155.21	0.327	No	No	0.35
962	48.10	106.59	61.93	2.49	0.39	0.84	85.61	73.34	158.95	0.361	No	No	0.39
963	48.15	106.99	61.07	2.48	0.39	0.84	84.75	72.83	157.58	0.348	No	No	0.38
964	48.20	104.22	61.74	2.48	0.39	0.84	83.26	72.62	155.87	0.333	No	No	0.36
965	48.25	100.01	63.33	2.50	0.40	0.83	78.45	71.73	150.18	0.290	No	No	0.31
966	48.30	93.91	66.23	2.54	0.41	0.83	73.99	71.25	145.24	0.260	No	No	0.28
967	48.35	87.69	69.52	2.58	0.42	0.82	67.80	70.26	138.06	0.226	No	No	0.25
968	48.40	81.23	73.50	2.63	0.43	0.82	62.83	0.00	62.83	4.000	No	Yes	2.00
969	48.45	76.48	77.13	2.68	0.44	0.81	57.86	0.00	57.86	4.000	No	Yes	2.00
970	48.50	73.37	80.28	2.72	0.45	0.81	56.02	0.00	56.02	4.000	No	Yes	2.00
971	48.55	72.59	81.83	2.74	0.45	0.81	55.15	0.00	55.15	4.000	No	Yes	2.00
972	48.60	73.49	82.00	2.74	0.45	0.81	55.89	0.00	55.89	4.000	Yes	Yes	2.00
973	48.65	76.28	80.26	2.72	0.44	0.81	58.15	0.00	58.15	4.000	Yes	Yes	2.00
974	48.70	81.36	76.96	2.67	0.43	0.82	61.90	0.00	61.90	4.000	Yes	Yes	2.00
975	48.75	88.11	72.21	2.62	0.42	0.82	68.31	0.00	68.31	4.000	Yes	Yes	2.00
976	48.80	96.50	66.67	2.55	0.41	0.83	74.78	71.59	146.37	4.000	Yes	No	2.00
977	48.85	104.19	61.09	2.48	0.40	0.83	82.69	72.25	154.94	4.000	Yes	No	2.00
978	48.90	110.71	56.14	2.41	0.39	0.83	87.46	71.85	159.31	4.000	Yes	No	2.00
979	48.95	113.99	52.51	2.37	0.38	0.83	91.00	71.29	162.30	4.000	Yes	No	2.00
980	49.00	114.88	50.35	2.34	0.39	0.83	90.72	70.20	160.92	4.000	Yes	No	2.00
981	49.05	113.12	50.00	2.34	0.39	0.83	89.44	69.70	159.14	0.363	No	No	0.39
982	49.10	110.32	50.93	2.35	0.39	0.83	86.34	69.32	155.65	4.000	Yes	No	2.00
983	49.15	106.45	53.17	2.38	0.40	0.83	83.51	69.56	153.07	4.000	Yes	No	2.00
984	49.20	102.97	55.82	2.41	0.41	0.82	79.61	69.57	149.18	4.000	Yes	No	2.00
985	49.25	99.99	58.90	2.45	0.41	0.82	77.59	70.11	147.70	4.000	Yes	No	2.00
986	49.30	98.58	61.27	2.48	0.41	0.82	76.02	70.43	146.45	4.000	Yes	No	2.00
987	49.35	98.15	62.97	2.50	0.41	0.82	76.10	70.96	147.07	4.000	Yes	No	2.00
988	49.40	98.96	63.14	2.50	0.41	0.82	76.46	71.11	147.57	0.274	No	No	0.30
989	49.45	100.29	62.29	2.49	0.41	0.82	77.98	71.29	149.28	4.000	Yes	No	2.00
990	49.50	102.24	60.34	2.47	0.40	0.82	79.32	71.06	150.38	4.000	Yes	No	2.00
991	49.55	103.75	58.21	2.44	0.40	0.82	81.20	70.87	152.07	4.000	Yes	No	2.00
992	49.60	104.70	55.93	2.41	0.40	0.82	81.56	70.14	151.70	4.000	Yes	No	2.00
993	49.65	105.55	54.10	2.39	0.40	0.82	81.48	69.40	150.87	4.000	Yes	No	2.00
994	49.70	106.91	52.78	2.37	0.40	0.82	83.12	69.29	152.41	4.000	Yes	No	2.00
995	49.75	109.29	51.94	2.36	0.40	0.82	84.80	69.37	154.17	0.319	No	No	0.35
996	49.80	110.81	51.43	2.36	0.39	0.83	87.35	69.82	157.18	0.344	No	No	0.37
997	49.85	110.25	50.91	2.35	0.39	0.82	86.82	69.44	156.26	0.336	No	No	0.36
998	49.90	108.66	50.69	2.35	0.40	0.82	83.21	68.38	151.59	0.300	No	No	0.32

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q_t :	Total cone resistance
FC:	Fines content (%)
I_c :	Soil behavior type index
m:	Stress exponent
C_N :	Overburden correction factor
q_{c1N} :	Normalized and adjusted cone resistance
Δq_{c1N} :	Cone resistance correction factor due to fines
$q_{c1N,cs}$:	Normalized and adjusted cone resistance
CRR _{7.5} :	Cyclic resistance ratio for $M_w=7.5$
FS:	Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
0.05	2.00	0.00	0.00	0.05	0.00	0.10	2.00	0.00	0.00	0.05	0.00
0.15	2.00	0.00	0.00	0.05	0.00	0.20	2.00	0.00	0.00	0.05	0.00
0.25	2.00	0.00	0.00	0.05	0.00	0.30	2.00	0.00	0.00	0.05	0.00
0.35	2.00	0.00	0.00	0.05	0.00	0.40	2.00	0.00	0.00	0.05	0.00
0.45	2.00	0.00	0.00	0.05	0.00	0.50	2.00	0.00	0.00	0.05	0.00
0.55	2.00	0.00	0.00	0.05	0.00	0.60	2.00	0.00	0.00	0.05	0.00
0.65	2.00	0.00	0.00	0.05	0.00	0.70	2.00	0.00	0.00	0.05	0.00
0.75	2.00	0.00	0.00	0.05	0.00	0.80	2.00	0.00	0.00	0.05	0.00
0.85	2.00	0.00	0.00	0.05	0.00	0.90	2.00	0.00	0.00	0.05	0.00
0.95	2.00	0.00	0.00	0.05	0.00	1.00	2.00	0.00	0.00	0.05	0.00
1.05	2.00	0.00	0.00	0.05	0.00	1.10	2.00	0.00	0.00	0.05	0.00
1.15	2.00	0.00	0.00	0.05	0.00	1.20	2.00	0.00	0.00	0.05	0.00
1.25	2.00	0.00	0.00	0.05	0.00	1.30	2.00	0.00	0.00	0.05	0.00
1.35	2.00	0.00	0.00	0.05	0.00	1.40	2.00	0.00	0.00	0.05	0.00
1.45	2.00	0.00	0.00	0.05	0.00	1.50	2.00	0.00	0.00	0.05	0.00
1.55	2.00	0.00	0.00	0.05	0.00	1.60	2.00	0.00	0.00	0.05	0.00
1.65	2.00	0.00	0.00	0.05	0.00	1.70	2.00	0.00	0.00	0.05	0.00
1.75	2.00	0.00	0.00	0.05	0.00	1.80	2.00	0.00	0.00	0.05	0.00
1.85	2.00	0.00	0.00	0.05	0.00	1.90	2.00	0.00	0.00	0.05	0.00
1.95	2.00	0.00	0.00	0.05	0.00	2.00	2.00	0.00	0.00	0.05	0.00
2.05	2.00	0.00	0.00	0.05	0.00	2.10	2.00	0.00	0.00	0.05	0.00
2.15	2.00	0.00	0.00	0.05	0.00	2.20	2.00	0.00	0.00	0.05	0.00
2.25	2.00	0.00	0.00	0.05	0.00	2.30	2.00	0.00	0.00	0.05	0.00
2.35	2.00	0.00	0.00	0.05	0.00	2.40	2.00	0.00	0.00	0.05	0.00
2.45	2.00	0.00	0.00	0.05	0.00	2.50	2.00	0.00	0.00	0.05	0.00
2.55	2.00	0.00	0.00	0.05	0.00	2.60	2.00	0.00	0.00	0.05	0.00
2.65	2.00	0.00	0.00	0.05	0.00	2.70	2.00	0.00	0.00	0.05	0.00
2.75	2.00	0.00	0.00	0.05	0.00	2.80	2.00	0.00	0.00	0.05	0.00
2.85	2.00	0.00	0.00	0.05	0.00	2.90	2.00	0.00	0.00	0.05	0.00
2.95	2.00	0.00	0.00	0.05	0.00	3.00	2.00	0.00	0.00	0.05	0.00
3.05	2.00	0.00	0.00	0.05	0.00	3.10	2.00	0.00	0.00	0.05	0.00
3.15	2.00	0.00	0.00	0.05	0.00	3.20	2.00	0.00	0.00	0.05	0.00
3.25	2.00	0.00	0.00	0.05	0.00	3.30	2.00	0.00	0.00	0.05	0.00
3.35	2.00	0.00	0.00	0.05	0.00	3.40	2.00	0.00	0.00	0.05	0.00
3.45	2.00	0.00	0.00	0.05	0.00	3.50	2.00	0.00	0.00	0.05	0.00
3.55	2.00	0.00	0.00	0.05	0.00	3.60	2.00	0.00	0.00	0.05	0.00
3.65	2.00	0.00	0.00	0.05	0.00	3.70	2.00	0.00	0.00	0.05	0.00
3.75	2.00	0.00	0.00	0.05	0.00	3.80	2.00	0.00	0.00	0.05	0.00
3.85	2.00	0.00	0.00	0.05	0.00	3.90	2.00	0.00	0.00	0.05	0.00
3.95	2.00	0.00	0.00	0.05	0.00	4.00	2.00	0.00	0.00	0.05	0.00
4.05	2.00	0.00	0.00	0.05	0.00	4.10	2.00	0.00	0.00	0.05	0.00
4.15	2.00	0.00	0.00	0.05	0.00	4.20	2.00	0.00	0.00	0.05	0.00
4.25	2.00	0.00	0.00	0.05	0.00	4.30	2.00	0.00	0.00	0.05	0.00
4.35	2.00	0.00	0.00	0.05	0.00	4.40	2.00	0.00	0.00	0.05	0.00
4.45	2.00	0.00	0.00	0.05	0.00	4.50	2.00	0.00	0.00	0.05	0.00
4.55	2.00	0.00	0.00	0.05	0.00	4.60	2.00	0.00	0.00	0.05	0.00
4.65	2.00	0.00	0.00	0.05	0.00	4.70	2.00	0.00	0.00	0.05	0.00
4.75	2.00	0.00	0.00	0.05	0.00	4.80	2.00	0.00	0.00	0.05	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
4.85	2.00	0.00	0.00	0.05	0.00	4.90	2.00	0.00	0.00	0.05	0.00
4.95	2.00	0.00	0.00	0.05	0.00	5.00	2.00	0.00	0.00	0.05	0.00
5.05	2.00	0.00	0.00	0.05	0.00	5.10	2.00	0.00	0.00	0.05	0.00
5.15	2.00	0.00	0.00	0.05	0.00	5.20	2.00	0.00	0.00	0.05	0.00
5.25	2.00	0.00	0.00	0.05	0.00	5.30	2.00	0.00	0.00	0.05	0.00
5.35	2.00	0.00	0.00	0.05	0.00	5.40	2.00	0.00	0.00	0.05	0.00
5.45	2.00	0.00	0.00	0.05	0.00	5.50	2.00	0.00	0.00	0.05	0.00
5.55	2.00	0.00	0.00	0.05	0.00	5.60	2.00	0.00	0.00	0.05	0.00
5.65	2.00	0.00	0.00	0.05	0.00	5.70	2.00	0.00	0.00	0.05	0.00
5.75	2.00	0.00	0.00	0.05	0.00	5.80	2.00	0.00	0.00	0.05	0.00
5.85	2.00	0.00	0.00	0.05	0.00	5.90	2.00	0.00	0.00	0.05	0.00
5.95	2.00	0.00	0.00	0.05	0.00	6.00	2.00	0.00	0.00	0.05	0.00
6.05	2.00	0.00	0.00	0.05	0.00	6.10	2.00	0.00	0.00	0.05	0.00
6.15	2.00	0.00	0.00	0.05	0.00	6.20	2.00	0.00	0.00	0.05	0.00
6.25	2.00	0.00	0.00	0.05	0.00	6.30	2.00	0.00	0.00	0.05	0.00
6.35	2.00	0.00	0.00	0.05	0.00	6.40	2.00	0.00	0.00	0.05	0.00
6.45	2.00	0.00	0.00	0.05	0.00	6.50	2.00	0.00	0.00	0.05	0.00
6.55	2.00	0.00	0.00	0.05	0.00	6.60	2.00	0.00	0.00	0.05	0.00
6.65	2.00	0.00	0.00	0.05	0.00	6.70	2.00	0.00	0.00	0.05	0.00
6.75	2.00	0.00	0.00	0.05	0.00	6.80	2.00	0.00	0.00	0.05	0.00
6.85	2.00	0.00	0.00	0.05	0.00	6.90	2.00	0.00	0.00	0.05	0.00
6.95	2.00	0.00	0.00	0.05	0.00	7.00	2.00	0.00	0.00	0.05	0.00
7.05	2.00	0.00	0.00	0.05	0.00	7.10	2.00	0.00	0.00	0.05	0.00
7.15	2.00	0.00	0.00	0.05	0.00	7.20	2.00	0.00	0.00	0.05	0.00
7.25	2.00	0.00	0.00	0.05	0.00	7.30	2.00	0.00	0.00	0.05	0.00
7.35	2.00	0.00	0.00	0.05	0.00	7.40	2.00	0.00	0.00	0.05	0.00
7.45	2.00	0.00	0.00	0.05	0.00	7.50	2.00	0.00	0.00	0.05	0.00
7.55	2.00	0.00	0.00	0.05	0.00	7.60	2.00	0.00	0.00	0.05	0.00
7.65	2.00	0.00	0.00	0.05	0.00	7.70	2.00	0.00	0.00	0.05	0.00
7.75	2.00	0.00	0.00	0.05	0.00	7.80	2.00	0.00	0.00	0.05	0.00
7.85	2.00	0.00	0.00	0.05	0.00	7.90	2.00	0.00	0.00	0.05	0.00
7.95	2.00	0.00	0.00	0.05	0.00	8.00	2.00	0.00	0.00	0.05	0.00
8.05	2.00	0.00	0.00	0.05	0.00	8.10	2.00	0.00	0.00	0.05	0.00
8.15	2.00	0.00	0.00	0.05	0.00	8.20	2.00	0.00	0.00	0.05	0.00
8.25	2.00	0.00	0.00	0.05	0.00	8.30	2.00	0.00	0.00	0.05	0.00
8.35	2.00	0.00	0.00	0.05	0.00	8.40	2.00	0.00	0.00	0.05	0.00
8.45	2.00	0.00	0.00	0.05	0.00	8.50	2.00	0.00	0.00	0.05	0.00
8.55	0.26	0.00	0.00	0.05	0.10	8.60	0.26	0.00	0.00	0.05	0.10
8.65	0.26	0.00	0.00	0.05	0.10	8.70	0.26	0.00	0.00	0.05	0.10
8.75	0.26	0.00	0.00	0.05	0.10	8.80	0.26	0.00	0.00	0.05	0.10
8.85	0.26	0.00	0.00	0.05	0.10	8.90	0.25	0.00	0.00	0.05	0.10
8.95	2.00	0.00	0.00	0.05	0.00	9.00	2.00	0.00	0.00	0.05	0.00
9.05	2.00	0.00	0.00	0.05	0.00	9.10	2.00	0.00	0.00	0.05	0.00
9.15	2.00	0.00	0.00	0.05	0.00	9.20	2.00	0.00	0.00	0.05	0.00
9.25	2.00	0.00	0.00	0.05	0.00	9.30	2.00	0.00	0.00	0.05	0.00
9.35	2.00	0.00	0.00	0.05	0.00	9.40	2.00	0.00	0.00	0.05	0.00
9.45	2.00	0.00	0.00	0.05	0.00	9.50	2.00	0.00	0.00	0.05	0.00
9.55	2.00	0.00	0.00	0.05	0.00	9.60	2.00	0.00	0.00	0.05	0.00

:: Liquefaction Potential Index calculation data ::

Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
9.65	2.00	0.00	0.00	0.05	0.00	9.70	2.00	0.00	0.00	0.05	0.00
9.75	2.00	0.00	0.00	0.05	0.00	9.80	2.00	0.00	0.00	0.05	0.00
9.85	2.00	0.00	0.00	0.05	0.00	9.90	2.00	0.00	0.00	0.05	0.00
9.95	2.00	0.00	0.00	0.05	0.00	10.00	2.00	0.00	0.00	0.05	0.00
10.05	2.00	0.00	0.00	0.05	0.00	10.10	2.00	0.00	0.00	0.05	0.00
10.15	2.00	0.00	0.00	0.05	0.00	10.20	2.00	0.00	0.00	0.05	0.00
10.25	2.00	0.00	0.00	0.05	0.00	10.30	2.00	0.00	0.00	0.05	0.00
10.35	0.22	0.78	0.28	0.05	0.10	10.40	0.21	0.79	0.28	0.05	0.10
10.45	0.21	0.79	0.28	0.05	0.10	10.50	0.21	0.79	0.28	0.05	0.10
10.55	0.21	0.79	0.28	0.05	0.10	10.60	0.21	0.79	0.28	0.05	0.10
10.65	0.21	0.79	0.28	0.05	0.10	10.70	0.21	0.79	0.28	0.05	0.10
10.75	0.21	0.79	0.28	0.05	0.10	10.80	0.21	0.79	0.28	0.05	0.10
10.85	0.21	0.79	0.28	0.05	0.10	10.90	0.20	0.80	0.28	0.05	0.10
10.95	0.21	0.79	0.28	0.05	0.10	11.00	0.21	0.79	0.28	0.05	0.10
11.05	0.21	0.79	0.28	0.05	0.10	11.10	0.21	0.79	0.28	0.05	0.10
11.15	0.20	0.80	0.28	0.05	0.10	11.20	0.20	0.80	0.28	0.05	0.10
11.25	0.20	0.80	0.28	0.05	0.10	11.30	0.20	0.80	0.28	0.05	0.10
11.35	0.20	0.80	0.28	0.05	0.10	11.40	0.20	0.80	0.28	0.05	0.10
11.45	0.20	0.80	0.28	0.05	0.10	11.50	2.00	0.00	0.00	0.05	0.00
11.55	2.00	0.00	0.00	0.05	0.00	11.60	2.00	0.00	0.00	0.05	0.00
11.65	2.00	0.00	0.00	0.05	0.00	11.70	2.00	0.00	0.00	0.05	0.00
11.75	2.00	0.00	0.00	0.05	0.00	11.80	2.00	0.00	0.00	0.05	0.00
11.85	2.00	0.00	0.00	0.05	0.00	11.90	2.00	0.00	0.00	0.05	0.00
11.95	2.00	0.00	0.00	0.05	0.00	12.00	0.18	0.82	0.27	0.05	0.10
12.05	2.00	0.00	0.00	0.05	0.00	12.10	2.00	0.00	0.00	0.05	0.00
12.15	2.00	0.00	0.00	0.05	0.00	12.20	2.00	0.00	0.00	0.05	0.00
12.25	2.00	0.00	0.00	0.05	0.00	12.30	2.00	0.00	0.00	0.05	0.00
12.35	2.00	0.00	0.00	0.05	0.00	12.40	0.19	0.81	0.27	0.05	0.10
12.45	2.00	0.00	0.00	0.05	0.00	12.50	2.00	0.00	0.00	0.05	0.00
12.55	2.00	0.00	0.00	0.05	0.00	12.60	2.00	0.00	0.00	0.05	0.00
12.65	2.00	0.00	0.00	0.05	0.00	12.70	2.00	0.00	0.00	0.05	0.00
12.75	2.00	0.00	0.00	0.05	0.00	12.80	2.00	0.00	0.00	0.05	0.00
12.85	2.00	0.00	0.00	0.05	0.00	12.90	2.00	0.00	0.00	0.05	0.00
12.95	2.00	0.00	0.00	0.05	0.00	13.00	2.00	0.00	0.00	0.05	0.00
13.05	2.00	0.00	0.00	0.05	0.00	13.10	2.00	0.00	0.00	0.05	0.00
13.15	2.00	0.00	0.00	0.05	0.00	13.20	2.00	0.00	0.00	0.05	0.00
13.25	2.00	0.00	0.00	0.05	0.00	13.30	2.00	0.00	0.00	0.05	0.00
13.35	2.00	0.00	0.00	0.05	0.00	13.40	2.00	0.00	0.00	0.05	0.00
13.45	2.00	0.00	0.00	0.05	0.00	13.50	2.00	0.00	0.00	0.05	0.00
13.55	2.00	0.00	0.00	0.05	0.00	13.60	2.00	0.00	0.00	0.05	0.00
13.65	2.00	0.00	0.00	0.05	0.00	13.70	2.00	0.00	0.00	0.05	0.00
13.75	2.00	0.00	0.00	0.05	0.00	13.80	2.00	0.00	0.00	0.05	0.00
13.85	2.00	0.00	0.00	0.05	0.00	13.90	2.00	0.00	0.00	0.05	0.00
13.95	2.00	0.00	0.00	0.05	0.00	14.00	2.00	0.00	0.00	0.05	0.00
14.05	2.00	0.00	0.00	0.05	0.00	14.10	2.00	0.00	0.00	0.05	0.00
14.15	2.00	0.00	0.00	0.05	0.00	14.20	2.00	0.00	0.00	0.05	0.00
14.25	2.00	0.00	0.00	0.05	0.00	14.30	2.00	0.00	0.00	0.05	0.00
14.35	2.00	0.00	0.00	0.05	0.00	14.40	2.00	0.00	0.00	0.05	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
14.45	2.00	0.00	0.00	0.05	0.00	14.50	2.00	0.00	0.00	0.05	0.00
14.55	2.00	0.00	0.00	0.05	0.00	14.60	2.00	0.00	0.00	0.05	0.00
14.65	2.00	0.00	0.00	0.05	0.00	14.70	2.00	0.00	0.00	0.05	0.00
14.75	2.00	0.00	0.00	0.05	0.00	14.80	2.00	0.00	0.00	0.05	0.00
14.85	2.00	0.00	0.00	0.05	0.00	14.90	2.00	0.00	0.00	0.05	0.00
14.95	2.00	0.00	0.00	0.05	0.00	15.00	2.00	0.00	0.00	0.05	0.00
15.05	2.00	0.00	0.00	0.05	0.00	15.10	2.00	0.00	0.00	0.05	0.00
15.15	2.00	0.00	0.00	0.05	0.00	15.20	2.00	0.00	0.00	0.05	0.00
15.25	2.00	0.00	0.00	0.05	0.00	15.30	2.00	0.00	0.00	0.05	0.00
15.35	2.00	0.00	0.00	0.05	0.00	15.40	2.00	0.00	0.00	0.05	0.00
15.45	2.00	0.00	0.00	0.05	0.00	15.50	2.00	0.00	0.00	0.05	0.00
15.55	2.00	0.00	0.00	0.05	0.00	15.60	2.00	0.00	0.00	0.05	0.00
15.65	2.00	0.00	0.00	0.05	0.00	15.70	2.00	0.00	0.00	0.05	0.00
15.75	2.00	0.00	0.00	0.05	0.00	15.80	2.00	0.00	0.00	0.05	0.00
15.85	2.00	0.00	0.00	0.05	0.00	15.90	2.00	0.00	0.00	0.05	0.00
15.95	2.00	0.00	0.00	0.05	0.00	16.00	2.00	0.00	0.00	0.05	0.00
16.05	2.00	0.00	0.00	0.05	0.00	16.10	0.17	0.83	0.26	0.05	0.10
16.15	0.17	0.83	0.27	0.05	0.10	16.20	2.00	0.00	0.00	0.05	0.00
16.25	2.00	0.00	0.00	0.05	0.00	16.30	2.00	0.00	0.00	0.05	0.00
16.35	2.00	0.00	0.00	0.05	0.00	16.40	2.00	0.00	0.00	0.05	0.00
16.45	2.00	0.00	0.00	0.05	0.00	16.50	2.00	0.00	0.00	0.05	0.00
16.55	2.00	0.00	0.00	0.05	0.00	16.60	2.00	0.00	0.00	0.05	0.00
16.65	2.00	0.00	0.00	0.05	0.00	16.70	2.00	0.00	0.00	0.05	0.00
16.75	2.00	0.00	0.00	0.05	0.00	16.80	2.00	0.00	0.00	0.05	0.00
16.85	2.00	0.00	0.00	0.05	0.00	16.90	2.00	0.00	0.00	0.05	0.00
16.95	2.00	0.00	0.00	0.05	0.00	17.00	2.00	0.00	0.00	0.05	0.00
17.05	2.00	0.00	0.00	0.05	0.00	17.10	2.00	0.00	0.00	0.05	0.00
17.15	2.00	0.00	0.00	0.05	0.00	17.20	2.00	0.00	0.00	0.05	0.00
17.25	2.00	0.00	0.00	0.05	0.00	17.30	2.00	0.00	0.00	0.05	0.00
17.35	2.00	0.00	0.00	0.05	0.00	17.40	2.00	0.00	0.00	0.05	0.00
17.45	2.00	0.00	0.00	0.05	0.00	17.50	2.00	0.00	0.00	0.05	0.00
17.55	0.18	0.82	0.27	0.05	0.09	17.60	2.00	0.00	0.00	0.05	0.00
17.65	2.00	0.00	0.00	0.05	0.00	17.70	2.00	0.00	0.00	0.05	0.00
17.75	2.00	0.00	0.00	0.05	0.00	17.80	2.00	0.00	0.00	0.05	0.00
17.85	2.00	0.00	0.00	0.05	0.00	17.90	2.00	0.00	0.00	0.05	0.00
17.95	2.00	0.00	0.00	0.05	0.00	18.00	2.00	0.00	0.00	0.05	0.00
18.05	2.00	0.00	0.00	0.05	0.00	18.10	2.00	0.00	0.00	0.05	0.00
18.15	2.00	0.00	0.00	0.05	0.00	18.20	2.00	0.00	0.00	0.05	0.00
18.25	2.00	0.00	0.00	0.05	0.00	18.30	2.00	0.00	0.00	0.05	0.00
18.35	2.00	0.00	0.00	0.05	0.00	18.40	2.00	0.00	0.00	0.05	0.00
18.45	2.00	0.00	0.00	0.05	0.00	18.50	2.00	0.00	0.00	0.05	0.00
18.55	2.00	0.00	0.00	0.05	0.00	18.60	2.00	0.00	0.00	0.05	0.00
18.65	2.00	0.00	0.00	0.05	0.00	18.70	2.00	0.00	0.00	0.05	0.00
18.75	2.00	0.00	0.00	0.05	0.00	18.80	2.00	0.00	0.00	0.05	0.00
18.85	2.00	0.00	0.00	0.05	0.00	18.90	2.00	0.00	0.00	0.05	0.00
18.95	2.00	0.00	0.00	0.05	0.00	19.00	2.00	0.00	0.00	0.05	0.00
19.05	2.00	0.00	0.00	0.05	0.00	19.10	2.00	0.00	0.00	0.05	0.00
19.15	2.00	0.00	0.00	0.05	0.00	19.20	2.00	0.00	0.00	0.05	0.00

:: Liquefaction Potential Index calculation data ::

Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
19.25	2.00	0.00	0.00	0.05	0.00	19.30	2.00	0.00	0.00	0.05	0.00
19.35	2.00	0.00	0.00	0.05	0.00	19.40	2.00	0.00	0.00	0.05	0.00
19.45	2.00	0.00	0.00	0.05	0.00	19.50	2.00	0.00	0.00	0.05	0.00
19.55	2.00	0.00	0.00	0.05	0.00	19.60	2.00	0.00	0.00	0.05	0.00
19.65	2.00	0.00	0.00	0.05	0.00	19.70	2.00	0.00	0.00	0.05	0.00
19.75	2.00	0.00	0.00	0.05	0.00	19.80	2.00	0.00	0.00	0.05	0.00
19.85	2.00	0.00	0.00	0.05	0.00	19.90	2.00	0.00	0.00	0.05	0.00
19.95	2.00	0.00	0.00	0.05	0.00	20.00	2.00	0.00	0.00	0.05	0.00
20.05	2.00	0.00	0.00	0.05	0.00	20.10	2.00	0.00	0.00	0.05	0.00
20.15	2.00	0.00	0.00	0.05	0.00	20.20	2.00	0.00	0.00	0.05	0.00
20.25	2.00	0.00	0.00	0.05	0.00	20.30	2.00	0.00	0.00	0.05	0.00
20.35	2.00	0.00	0.00	0.05	0.00	20.40	2.00	0.00	0.00	0.05	0.00
20.45	2.00	0.00	0.00	0.05	0.00	20.50	2.00	0.00	0.00	0.05	0.00
20.55	2.00	0.00	0.00	0.05	0.00	20.60	2.00	0.00	0.00	0.05	0.00
20.65	2.00	0.00	0.00	0.05	0.00	20.70	2.00	0.00	0.00	0.05	0.00
20.75	2.00	0.00	0.00	0.05	0.00	20.80	2.00	0.00	0.00	0.05	0.00
20.85	2.00	0.00	0.00	0.05	0.00	20.90	2.00	0.00	0.00	0.05	0.00
20.95	2.00	0.00	0.00	0.05	0.00	21.00	2.00	0.00	0.00	0.05	0.00
21.05	2.00	0.00	0.00	0.05	0.00	21.10	2.00	0.00	0.00	0.05	0.00
21.15	2.00	0.00	0.00	0.05	0.00	21.20	2.00	0.00	0.00	0.05	0.00
21.25	2.00	0.00	0.00	0.05	0.00	21.30	2.00	0.00	0.00	0.05	0.00
21.35	2.00	0.00	0.00	0.05	0.00	21.40	2.00	0.00	0.00	0.05	0.00
21.45	2.00	0.00	0.00	0.05	0.00	21.50	2.00	0.00	0.00	0.05	0.00
21.55	2.00	0.00	0.00	0.05	0.00	21.60	2.00	0.00	0.00	0.05	0.00
21.65	2.00	0.00	0.00	0.05	0.00	21.70	2.00	0.00	0.00	0.05	0.00
21.75	2.00	0.00	0.00	0.05	0.00	21.80	2.00	0.00	0.00	0.05	0.00
21.85	2.00	0.00	0.00	0.05	0.00	21.90	2.00	0.00	0.00	0.05	0.00
21.95	2.00	0.00	0.00	0.05	0.00	22.00	2.00	0.00	0.00	0.05	0.00
22.05	2.00	0.00	0.00	0.05	0.00	22.10	2.00	0.00	0.00	0.05	0.00
22.15	2.00	0.00	0.00	0.05	0.00	22.20	2.00	0.00	0.00	0.05	0.00
22.25	2.00	0.00	0.00	0.05	0.00	22.30	2.00	0.00	0.00	0.05	0.00
22.35	2.00	0.00	0.00	0.05	0.00	22.40	2.00	0.00	0.00	0.05	0.00
22.45	2.00	0.00	0.00	0.05	0.00	22.50	2.00	0.00	0.00	0.05	0.00
22.55	2.00	0.00	0.00	0.05	0.00	22.60	2.00	0.00	0.00	0.05	0.00
22.65	2.00	0.00	0.00	0.05	0.00	22.70	2.00	0.00	0.00	0.05	0.00
22.75	2.00	0.00	0.00	0.05	0.00	22.80	2.00	0.00	0.00	0.05	0.00
22.85	2.00	0.00	0.00	0.05	0.00	22.90	2.00	0.00	0.00	0.05	0.00
22.95	2.00	0.00	0.00	0.05	0.00	23.00	2.00	0.00	0.00	0.05	0.00
23.05	2.00	0.00	0.00	0.05	0.00	23.10	2.00	0.00	0.00	0.05	0.00
23.15	2.00	0.00	0.00	0.05	0.00	23.20	2.00	0.00	0.00	0.05	0.00
23.25	2.00	0.00	0.00	0.05	0.00	23.30	2.00	0.00	0.00	0.05	0.00
23.35	2.00	0.00	0.00	0.05	0.00	23.40	2.00	0.00	0.00	0.05	0.00
23.45	2.00	0.00	0.00	0.05	0.00	23.50	2.00	0.00	0.00	0.05	0.00
23.55	2.00	0.00	0.00	0.05	0.00	23.60	2.00	0.00	0.00	0.05	0.00
23.65	2.00	0.00	0.00	0.05	0.00	23.70	2.00	0.00	0.00	0.05	0.00
23.75	2.00	0.00	0.00	0.05	0.00	23.80	2.00	0.00	0.00	0.05	0.00
23.85	2.00	0.00	0.00	0.05	0.00	23.90	2.00	0.00	0.00	0.05	0.00
23.95	2.00	0.00	0.00	0.05	0.00	24.00	2.00	0.00	0.00	0.05	0.00

:: Liquefaction Potential Index calculation data ::

Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
24.05	2.00	0.00	0.00	0.05	0.00	24.10	2.00	0.00	0.00	0.05	0.00
24.15	2.00	0.00	0.00	0.05	0.00	24.20	2.00	0.00	0.00	0.05	0.00
24.25	2.00	0.00	0.00	0.05	0.00	24.30	2.00	0.00	0.00	0.05	0.00
24.35	2.00	0.00	0.00	0.05	0.00	24.40	2.00	0.00	0.00	0.05	0.00
24.45	2.00	0.00	0.00	0.05	0.00	24.50	2.00	0.00	0.00	0.05	0.00
24.55	2.00	0.00	0.00	0.05	0.00	24.60	2.00	0.00	0.00	0.05	0.00
24.65	2.00	0.00	0.00	0.05	0.00	24.70	2.00	0.00	0.00	0.05	0.00
24.75	2.00	0.00	0.00	0.05	0.00	24.80	2.00	0.00	0.00	0.05	0.00
24.85	2.00	0.00	0.00	0.05	0.00	24.90	2.00	0.00	0.00	0.05	0.00
24.95	2.00	0.00	0.00	0.05	0.00	25.00	2.00	0.00	0.00	0.05	0.00
25.05	2.00	0.00	0.00	0.05	0.00	25.10	2.00	0.00	0.00	0.05	0.00
25.15	2.00	0.00	0.00	0.05	0.00	25.20	2.00	0.00	0.00	0.05	0.00
25.25	0.19	0.81	0.27	0.05	0.08	25.30	0.19	0.81	0.27	0.05	0.08
25.35	0.19	0.81	0.27	0.05	0.08	25.40	0.19	0.81	0.27	0.05	0.08
25.45	0.19	0.81	0.27	0.05	0.08	25.50	0.19	0.81	0.28	0.05	0.08
25.55	0.20	0.80	0.28	0.05	0.07	25.60	0.20	0.80	0.28	0.05	0.07
25.65	0.21	0.79	0.28	0.05	0.07	25.70	0.22	0.78	0.28	0.05	0.07
25.75	0.22	0.78	0.29	0.05	0.07	25.80	0.23	0.77	0.29	0.05	0.07
25.85	0.24	0.76	0.29	0.05	0.07	25.90	0.25	0.75	0.30	0.05	0.07
25.95	0.27	0.73	0.31	0.05	0.07	26.00	0.26	0.74	0.30	0.05	0.07
26.05	0.24	0.76	0.30	0.05	0.07	26.10	0.23	0.77	0.29	0.05	0.07
26.15	0.22	0.78	0.29	0.05	0.07	26.20	0.23	0.77	0.29	0.05	0.07
26.25	0.23	0.77	0.29	0.05	0.07	26.30	2.00	0.00	0.00	0.05	0.00
26.35	2.00	0.00	0.00	0.05	0.00	26.40	2.00	0.00	0.00	0.05	0.00
26.45	2.00	0.00	0.00	0.05	0.00	26.50	2.00	0.00	0.00	0.05	0.00
26.55	2.00	0.00	0.00	0.05	0.00	26.60	2.00	0.00	0.00	0.05	0.00
26.65	2.00	0.00	0.00	0.05	0.00	26.70	2.00	0.00	0.00	0.05	0.00
26.75	2.00	0.00	0.00	0.05	0.00	26.80	2.00	0.00	0.00	0.05	0.00
26.85	2.00	0.00	0.00	0.05	0.00	26.90	2.00	0.00	0.00	0.05	0.00
26.95	2.00	0.00	0.00	0.05	0.00	27.00	2.00	0.00	0.00	0.05	0.00
27.05	2.00	0.00	0.00	0.05	0.00	27.10	2.00	0.00	0.00	0.05	0.00
27.15	2.00	0.00	0.00	0.05	0.00	27.20	2.00	0.00	0.00	0.05	0.00
27.25	2.00	0.00	0.00	0.05	0.00	27.30	2.00	0.00	0.00	0.05	0.00
27.35	2.00	0.00	0.00	0.05	0.00	27.40	2.00	0.00	0.00	0.05	0.00
27.45	2.00	0.00	0.00	0.05	0.00	27.50	2.00	0.00	0.00	0.05	0.00
27.55	2.00	0.00	0.00	0.05	0.00	27.60	2.00	0.00	0.00	0.05	0.00
27.65	2.00	0.00	0.00	0.05	0.00	27.70	2.00	0.00	0.00	0.05	0.00
27.75	2.00	0.00	0.00	0.05	0.00	27.80	2.00	0.00	0.00	0.05	0.00
27.85	2.00	0.00	0.00	0.05	0.00	27.90	2.00	0.00	0.00	0.05	0.00
27.95	2.00	0.00	0.00	0.05	0.00	28.00	2.00	0.00	0.00	0.05	0.00
28.05	0.17	0.83	0.27	0.05	0.07	28.10	0.17	0.83	0.27	0.05	0.07
28.15	0.17	0.83	0.26	0.05	0.07	28.20	0.16	0.84	0.26	0.05	0.07
28.25	2.00	0.00	0.00	0.05	0.00	28.30	2.00	0.00	0.00	0.05	0.00
28.35	2.00	0.00	0.00	0.05	0.00	28.40	2.00	0.00	0.00	0.05	0.00
28.45	2.00	0.00	0.00	0.05	0.00	28.50	2.00	0.00	0.00	0.05	0.00
28.55	2.00	0.00	0.00	0.05	0.00	28.60	2.00	0.00	0.00	0.05	0.00
28.65	2.00	0.00	0.00	0.05	0.00	28.70	2.00	0.00	0.00	0.05	0.00
28.75	2.00	0.00	0.00	0.05	0.00	28.80	2.00	0.00	0.00	0.05	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
28.85	2.00	0.00	0.00	0.05	0.00	28.90	2.00	0.00	0.00	0.05	0.00
28.95	2.00	0.00	0.00	0.05	0.00	29.00	2.00	0.00	0.00	0.05	0.00
29.05	2.00	0.00	0.00	0.05	0.00	29.10	2.00	0.00	0.00	0.05	0.00
29.15	2.00	0.00	0.00	0.05	0.00	29.20	2.00	0.00	0.00	0.05	0.00
29.25	2.00	0.00	0.00	0.05	0.00	29.30	2.00	0.00	0.00	0.05	0.00
29.35	2.00	0.00	0.00	0.05	0.00	29.40	2.00	0.00	0.00	0.05	0.00
29.45	2.00	0.00	0.00	0.05	0.00	29.50	2.00	0.00	0.00	0.05	0.00
29.55	2.00	0.00	0.00	0.05	0.00	29.60	2.00	0.00	0.00	0.05	0.00
29.65	2.00	0.00	0.00	0.05	0.00	29.70	2.00	0.00	0.00	0.05	0.00
29.75	2.00	0.00	0.00	0.05	0.00	29.80	2.00	0.00	0.00	0.05	0.00
29.85	2.00	0.00	0.00	0.05	0.00	29.90	2.00	0.00	0.00	0.05	0.00
29.95	2.00	0.00	0.00	0.05	0.00	30.00	2.00	0.00	0.00	0.05	0.00
30.05	2.00	0.00	0.00	0.05	0.00	30.10	2.00	0.00	0.00	0.05	0.00
30.15	2.00	0.00	0.00	0.05	0.00	30.20	2.00	0.00	0.00	0.05	0.00
30.25	2.00	0.00	0.00	0.05	0.00	30.30	2.00	0.00	0.00	0.05	0.00
30.35	2.00	0.00	0.00	0.05	0.00	30.40	2.00	0.00	0.00	0.05	0.00
30.45	2.00	0.00	0.00	0.05	0.00	30.50	2.00	0.00	0.00	0.05	0.00
30.55	2.00	0.00	0.00	0.05	0.00	30.60	2.00	0.00	0.00	0.05	0.00
30.65	2.00	0.00	0.00	0.05	0.00	30.70	2.00	0.00	0.00	0.05	0.00
30.75	2.00	0.00	0.00	0.05	0.00	30.80	2.00	0.00	0.00	0.05	0.00
30.85	2.00	0.00	0.00	0.05	0.00	30.90	2.00	0.00	0.00	0.05	0.00
30.95	2.00	0.00	0.00	0.05	0.00	31.00	2.00	0.00	0.00	0.05	0.00
31.05	2.00	0.00	0.00	0.05	0.00	31.10	2.00	0.00	0.00	0.05	0.00
31.15	2.00	0.00	0.00	0.05	0.00	31.20	2.00	0.00	0.00	0.05	0.00
31.25	0.47	0.53	0.45	0.05	0.04	31.30	0.59	0.41	0.62	0.05	0.03
31.35	0.82	0.00	0.00	0.05	0.01	31.40	1.18	0.00	0.00	0.05	0.00
31.45	1.98	0.00	0.00	0.05	0.00	31.50	2.00	0.00	0.00	0.05	0.00
31.55	2.00	0.00	0.00	0.05	0.00	31.60	2.00	0.00	0.00	0.05	0.00
31.65	2.00	0.00	0.00	0.05	0.00	31.70	2.00	0.00	0.00	0.05	0.00
31.75	2.00	0.00	0.00	0.05	0.00	31.80	2.00	0.00	0.00	0.05	0.00
31.85	2.00	0.00	0.00	0.05	0.00	31.90	2.00	0.00	0.00	0.05	0.00
31.95	2.00	0.00	0.00	0.05	0.00	32.00	2.00	0.00	0.00	0.05	0.00
32.05	2.00	0.00	0.00	0.05	0.00	32.10	2.00	0.00	0.00	0.05	0.00
32.15	2.00	0.00	0.00	0.05	0.00	32.20	2.00	0.00	0.00	0.05	0.00
32.25	2.00	0.00	0.00	0.05	0.00	32.30	2.00	0.00	0.00	0.05	0.00
32.35	2.00	0.00	0.00	0.05	0.00	32.40	2.00	0.00	0.00	0.05	0.00
32.45	2.00	0.00	0.00	0.05	0.00	32.50	2.00	0.00	0.00	0.05	0.00
32.55	2.00	0.00	0.00	0.05	0.00	32.60	2.00	0.00	0.00	0.05	0.00
32.65	2.00	0.00	0.00	0.05	0.00	32.70	2.00	0.00	0.00	0.05	0.00
32.75	2.00	0.00	0.00	0.05	0.00	32.80	2.00	0.00	0.00	0.05	0.00
32.85	2.00	0.00	0.00	0.05	0.00	32.90	2.00	0.00	0.00	0.05	0.00
32.95	2.00	0.00	0.00	0.05	0.00	33.00	2.00	0.00	0.00	0.05	0.00
33.05	2.00	0.00	0.00	0.05	0.00	33.10	2.00	0.00	0.00	0.05	0.00
33.15	2.00	0.00	0.00	0.05	0.00	33.20	2.00	0.00	0.00	0.05	0.00
33.25	2.00	0.00	0.00	0.05	0.00	33.30	2.00	0.00	0.00	0.05	0.00
33.35	2.00	0.00	0.00	0.05	0.00	33.40	2.00	0.00	0.00	0.05	0.00
33.45	2.00	0.00	0.00	0.05	0.00	33.50	2.00	0.00	0.00	0.05	0.00
33.55	2.00	0.00	0.00	0.05	0.00	33.60	2.00	0.00	0.00	0.05	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
33.65	2.00	0.00	0.00	0.05	0.00	33.70	2.00	0.00	0.00	0.05	0.00
33.75	2.00	0.00	0.00	0.05	0.00	33.80	2.00	0.00	0.00	0.05	0.00
33.85	1.95	0.00	0.00	0.05	0.00	33.90	1.79	0.00	0.00	0.05	0.00
33.95	1.60	0.00	0.00	0.05	0.00	34.00	1.44	0.00	0.00	0.05	0.00
34.05	1.23	0.00	0.00	0.05	0.00	34.10	1.17	0.00	0.00	0.05	0.00
34.15	1.13	0.00	0.00	0.05	0.00	34.20	1.09	0.00	0.00	0.05	0.00
34.25	1.07	0.00	0.00	0.05	0.00	34.30	1.04	0.00	0.00	0.05	0.00
34.35	1.07	0.00	0.00	0.05	0.00	34.40	1.13	0.00	0.00	0.05	0.00
34.45	1.21	0.00	0.00	0.05	0.00	34.50	1.30	0.00	0.00	0.05	0.00
34.55	1.44	0.00	0.00	0.05	0.00	34.60	1.58	0.00	0.00	0.05	0.00
34.65	1.80	0.00	0.00	0.05	0.00	34.70	2.00	0.00	0.00	0.05	0.00
34.75	2.00	0.00	0.00	0.05	0.00	34.80	2.00	0.00	0.00	0.05	0.00
34.85	2.00	0.00	0.00	0.05	0.00	34.90	2.00	0.00	0.00	0.05	0.00
34.95	2.00	0.00	0.00	0.05	0.00	35.00	2.00	0.00	0.00	0.05	0.00
35.05	2.00	0.00	0.00	0.05	0.00	35.10	2.00	0.00	0.00	0.05	0.00
35.15	2.00	0.00	0.00	0.05	0.00	35.20	2.00	0.00	0.00	0.05	0.00
35.25	2.00	0.00	0.00	0.05	0.00	35.30	2.00	0.00	0.00	0.05	0.00
35.35	2.00	0.00	0.00	0.05	0.00	35.40	2.00	0.00	0.00	0.05	0.00
35.45	2.00	0.00	0.00	0.05	0.00	35.50	2.00	0.00	0.00	0.05	0.00
35.55	2.00	0.00	0.00	0.05	0.00	35.60	2.00	0.00	0.00	0.05	0.00
35.65	2.00	0.00	0.00	0.05	0.00	35.70	2.00	0.00	0.00	0.05	0.00
35.75	2.00	0.00	0.00	0.05	0.00	35.80	2.00	0.00	0.00	0.05	0.00
35.85	2.00	0.00	0.00	0.05	0.00	35.90	2.00	0.00	0.00	0.05	0.00
35.95	2.00	0.00	0.00	0.05	0.00	36.00	2.00	0.00	0.00	0.05	0.00
36.05	2.00	0.00	0.00	0.05	0.00	36.10	2.00	0.00	0.00	0.05	0.00
36.15	2.00	0.00	0.00	0.05	0.00	36.20	2.00	0.00	0.00	0.05	0.00
36.25	2.00	0.00	0.00	0.05	0.00	36.30	2.00	0.00	0.00	0.05	0.00
36.35	2.00	0.00	0.00	0.05	0.00	36.40	2.00	0.00	0.00	0.05	0.00
36.45	1.45	0.00	0.00	0.05	0.00	36.50	1.06	0.00	0.00	0.05	0.00
36.55	0.69	0.31	0.87	0.05	0.02	36.60	0.62	0.38	0.68	0.05	0.03
36.65	0.57	0.43	0.58	0.05	0.03	36.70	0.67	0.33	0.79	0.05	0.02
36.75	0.73	0.00	0.00	0.05	0.02	36.80	2.00	0.00	0.00	0.05	0.00
36.85	2.00	0.00	0.00	0.05	0.00	36.90	2.00	0.00	0.00	0.05	0.00
36.95	2.00	0.00	0.00	0.05	0.00	37.00	2.00	0.00	0.00	0.05	0.00
37.05	2.00	0.00	0.00	0.05	0.00	37.10	2.00	0.00	0.00	0.05	0.00
37.15	2.00	0.00	0.00	0.05	0.00	37.20	2.00	0.00	0.00	0.05	0.00
37.25	2.00	0.00	0.00	0.05	0.00	37.30	2.00	0.00	0.00	0.05	0.00
37.35	2.00	0.00	0.00	0.05	0.00	37.40	2.00	0.00	0.00	0.05	0.00
37.45	2.00	0.00	0.00	0.05	0.00	37.50	2.00	0.00	0.00	0.05	0.00
37.55	2.00	0.00	0.00	0.05	0.00	37.60	2.00	0.00	0.00	0.05	0.00
37.65	2.00	0.00	0.00	0.05	0.00	37.70	2.00	0.00	0.00	0.05	0.00
37.75	2.00	0.00	0.00	0.05	0.00	37.80	2.00	0.00	0.00	0.05	0.00
37.85	2.00	0.00	0.00	0.05	0.00	37.90	2.00	0.00	0.00	0.05	0.00
37.95	2.00	0.00	0.00	0.05	0.00	38.00	2.00	0.00	0.00	0.05	0.00
38.05	2.00	0.00	0.00	0.05	0.00	38.10	2.00	0.00	0.00	0.05	0.00
38.15	2.00	0.00	0.00	0.05	0.00	38.20	2.00	0.00	0.00	0.05	0.00
38.25	2.00	0.00	0.00	0.05	0.00	38.30	2.00	0.00	0.00	0.05	0.00
38.35	2.00	0.00	0.00	0.05	0.00	38.40	2.00	0.00	0.00	0.05	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
38.45	0.30	0.70	0.32	0.05	0.04	38.50	0.30	0.70	0.32	0.05	0.04
38.55	0.29	0.71	0.32	0.05	0.04	38.60	0.29	0.71	0.31	0.05	0.04
38.65	0.28	0.72	0.31	0.05	0.04	38.70	0.27	0.73	0.31	0.05	0.05
38.75	0.27	0.73	0.31	0.05	0.05	38.80	0.27	0.73	0.31	0.05	0.05
38.85	0.28	0.72	0.31	0.05	0.04	38.90	0.29	0.71	0.32	0.05	0.04
38.95	0.30	0.70	0.32	0.05	0.04	39.00	0.30	0.70	0.32	0.05	0.04
39.05	0.31	0.69	0.33	0.05	0.04	39.10	2.00	0.00	0.00	0.05	0.00
39.15	2.00	0.00	0.00	0.05	0.00	39.20	2.00	0.00	0.00	0.05	0.00
39.25	2.00	0.00	0.00	0.05	0.00	39.30	2.00	0.00	0.00	0.05	0.00
39.35	2.00	0.00	0.00	0.05	0.00	39.40	2.00	0.00	0.00	0.05	0.00
39.45	2.00	0.00	0.00	0.05	0.00	39.50	2.00	0.00	0.00	0.05	0.00
39.55	2.00	0.00	0.00	0.05	0.00	39.60	2.00	0.00	0.00	0.05	0.00
39.65	0.18	0.82	0.27	0.05	0.05	39.70	2.00	0.00	0.00	0.05	0.00
39.75	2.00	0.00	0.00	0.05	0.00	39.80	2.00	0.00	0.00	0.05	0.00
39.85	2.00	0.00	0.00	0.05	0.00	39.90	2.00	0.00	0.00	0.05	0.00
39.95	2.00	0.00	0.00	0.05	0.00	40.00	2.00	0.00	0.00	0.05	0.00
40.05	2.00	0.00	0.00	0.05	0.00	40.10	2.00	0.00	0.00	0.05	0.00
40.15	0.21	0.79	0.28	0.05	0.05	40.20	0.21	0.79	0.28	0.05	0.05
40.25	0.21	0.79	0.28	0.05	0.05	40.30	0.20	0.80	0.28	0.05	0.05
40.35	0.20	0.80	0.28	0.05	0.05	40.40	0.20	0.80	0.28	0.05	0.05
40.45	0.20	0.80	0.28	0.05	0.05	40.50	0.19	0.81	0.27	0.05	0.05
40.55	0.19	0.81	0.27	0.05	0.05	40.60	2.00	0.00	0.00	0.05	0.00
40.65	2.00	0.00	0.00	0.05	0.00	40.70	2.00	0.00	0.00	0.05	0.00
40.75	2.00	0.00	0.00	0.05	0.00	40.80	2.00	0.00	0.00	0.05	0.00
40.85	2.00	0.00	0.00	0.05	0.00	40.90	2.00	0.00	0.00	0.05	0.00
40.95	2.00	0.00	0.00	0.05	0.00	41.00	2.00	0.00	0.00	0.05	0.00
41.05	2.00	0.00	0.00	0.05	0.00	41.10	2.00	0.00	0.00	0.05	0.00
41.15	2.00	0.00	0.00	0.05	0.00	41.20	2.00	0.00	0.00	0.05	0.00
41.25	2.00	0.00	0.00	0.05	0.00	41.30	2.00	0.00	0.00	0.05	0.00
41.35	2.00	0.00	0.00	0.05	0.00	41.40	2.00	0.00	0.00	0.05	0.00
41.45	2.00	0.00	0.00	0.05	0.00	41.50	2.00	0.00	0.00	0.05	0.00
41.55	2.00	0.00	0.00	0.05	0.00	41.60	0.29	0.71	0.32	0.05	0.04
41.65	2.00	0.00	0.00	0.05	0.00	41.70	2.00	0.00	0.00	0.05	0.00
41.75	2.00	0.00	0.00	0.05	0.00	41.80	2.00	0.00	0.00	0.05	0.00
41.85	2.00	0.00	0.00	0.05	0.00	41.90	2.00	0.00	0.00	0.05	0.00
41.95	2.00	0.00	0.00	0.05	0.00	42.00	2.00	0.00	0.00	0.05	0.00
42.05	2.00	0.00	0.00	0.05	0.00	42.10	2.00	0.00	0.00	0.05	0.00
42.15	2.00	0.00	0.00	0.05	0.00	42.20	2.00	0.00	0.00	0.05	0.00
42.25	2.00	0.00	0.00	0.05	0.00	42.30	2.00	0.00	0.00	0.05	0.00
42.35	2.00	0.00	0.00	0.05	0.00	42.40	2.00	0.00	0.00	0.05	0.00
42.45	2.00	0.00	0.00	0.05	0.00	42.50	2.00	0.00	0.00	0.05	0.00
42.55	2.00	0.00	0.00	0.05	0.00	42.60	2.00	0.00	0.00	0.05	0.00
42.65	2.00	0.00	0.00	0.05	0.00	42.70	2.00	0.00	0.00	0.05	0.00
42.75	2.00	0.00	0.00	0.05	0.00	42.80	2.00	0.00	0.00	0.05	0.00
42.85	2.00	0.00	0.00	0.05	0.00	42.90	2.00	0.00	0.00	0.05	0.00
42.95	2.00	0.00	0.00	0.05	0.00	43.00	2.00	0.00	0.00	0.05	0.00
43.05	2.00	0.00	0.00	0.05	0.00	43.10	2.00	0.00	0.00	0.05	0.00
43.15	2.00	0.00	0.00	0.05	0.00	43.20	2.00	0.00	0.00	0.05	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
43.25	2.00	0.00	0.00	0.05	0.00	43.30	0.21	0.79	0.28	0.05	0.04
43.35	2.00	0.00	0.00	0.05	0.00	43.40	2.00	0.00	0.00	0.05	0.00
43.45	2.00	0.00	0.00	0.05	0.00	43.50	2.00	0.00	0.00	0.05	0.00
43.55	2.00	0.00	0.00	0.05	0.00	43.60	2.00	0.00	0.00	0.05	0.00
43.65	2.00	0.00	0.00	0.05	0.00	43.70	0.19	0.81	0.27	0.05	0.04
43.75	2.00	0.00	0.00	0.05	0.00	43.80	2.00	0.00	0.00	0.05	0.00
43.85	2.00	0.00	0.00	0.05	0.00	43.90	2.00	0.00	0.00	0.05	0.00
43.95	2.00	0.00	0.00	0.05	0.00	44.00	2.00	0.00	0.00	0.05	0.00
44.05	2.00	0.00	0.00	0.05	0.00	44.10	2.00	0.00	0.00	0.05	0.00
44.15	2.00	0.00	0.00	0.05	0.00	44.20	2.00	0.00	0.00	0.05	0.00
44.25	2.00	0.00	0.00	0.05	0.00	44.30	2.00	0.00	0.00	0.05	0.00
44.35	2.00	0.00	0.00	0.05	0.00	44.40	2.00	0.00	0.00	0.05	0.00
44.45	2.00	0.00	0.00	0.05	0.00	44.50	2.00	0.00	0.00	0.05	0.00
44.55	2.00	0.00	0.00	0.05	0.00	44.60	2.00	0.00	0.00	0.05	0.00
44.65	2.00	0.00	0.00	0.05	0.00	44.70	2.00	0.00	0.00	0.05	0.00
44.75	2.00	0.00	0.00	0.05	0.00	44.80	2.00	0.00	0.00	0.05	0.00
44.85	2.00	0.00	0.00	0.05	0.00	44.90	2.00	0.00	0.00	0.05	0.00
44.95	2.00	0.00	0.00	0.05	0.00	45.00	2.00	0.00	0.00	0.05	0.00
45.05	2.00	0.00	0.00	0.05	0.00	45.10	2.00	0.00	0.00	0.05	0.00
45.15	2.00	0.00	0.00	0.05	0.00	45.20	2.00	0.00	0.00	0.05	0.00
45.25	2.00	0.00	0.00	0.05	0.00	45.30	2.00	0.00	0.00	0.05	0.00
45.35	2.00	0.00	0.00	0.05	0.00	45.40	2.00	0.00	0.00	0.05	0.00
45.45	2.00	0.00	0.00	0.05	0.00	45.50	2.00	0.00	0.00	0.05	0.00
45.55	2.00	0.00	0.00	0.05	0.00	45.60	2.00	0.00	0.00	0.05	0.00
45.65	2.00	0.00	0.00	0.05	0.00	45.70	2.00	0.00	0.00	0.05	0.00
45.75	2.00	0.00	0.00	0.05	0.00	45.80	2.00	0.00	0.00	0.05	0.00
45.85	2.00	0.00	0.00	0.05	0.00	45.90	2.00	0.00	0.00	0.05	0.00
45.95	2.00	0.00	0.00	0.05	0.00	46.00	2.00	0.00	0.00	0.05	0.00
46.05	2.00	0.00	0.00	0.05	0.00	46.10	2.00	0.00	0.00	0.05	0.00
46.15	2.00	0.00	0.00	0.05	0.00	46.20	1.39	0.00	0.00	0.05	0.00
46.25	1.08	0.00	0.00	0.05	0.00	46.30	0.92	0.00	0.00	0.05	0.00
46.35	0.88	0.00	0.00	0.05	0.01	46.40	0.86	0.00	0.00	0.05	0.01
46.45	0.90	0.00	0.00	0.05	0.00	46.50	0.93	0.00	0.00	0.05	0.00
46.55	1.02	0.00	0.00	0.05	0.00	46.60	1.13	0.00	0.00	0.05	0.00
46.65	1.25	0.00	0.00	0.05	0.00	46.70	1.32	0.00	0.00	0.05	0.00
46.75	1.31	0.00	0.00	0.05	0.00	46.80	1.31	0.00	0.00	0.05	0.00
46.85	1.30	0.00	0.00	0.05	0.00	46.90	1.30	0.00	0.00	0.05	0.00
46.95	1.27	0.00	0.00	0.05	0.00	47.00	1.14	0.00	0.00	0.05	0.00
47.05	0.97	0.00	0.00	0.05	0.00	47.10	0.77	0.00	0.00	0.05	0.01
47.15	0.58	0.42	0.59	0.05	0.02	47.20	2.00	0.00	0.00	0.05	0.00
47.25	2.00	0.00	0.00	0.05	0.00	47.30	2.00	0.00	0.00	0.05	0.00
47.35	2.00	0.00	0.00	0.05	0.00	47.40	2.00	0.00	0.00	0.05	0.00
47.45	2.00	0.00	0.00	0.05	0.00	47.50	2.00	0.00	0.00	0.05	0.00
47.55	2.00	0.00	0.00	0.05	0.00	47.60	2.00	0.00	0.00	0.05	0.00
47.65	2.00	0.00	0.00	0.05	0.00	47.70	2.00	0.00	0.00	0.05	0.00
47.75	2.00	0.00	0.00	0.05	0.00	47.80	2.00	0.00	0.00	0.05	0.00
47.85	2.00	0.00	0.00	0.05	0.00	47.90	2.00	0.00	0.00	0.05	0.00
47.95	0.29	0.71	0.32	0.05	0.03	48.00	0.33	0.67	0.34	0.05	0.03

:: Liquefaction Potential Index calculation data ::

Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
48.05	0.35	0.65	0.35	0.05	0.03	48.10	0.39	0.61	0.38	0.05	0.02
48.15	0.38	0.62	0.37	0.05	0.03	48.20	0.36	0.64	0.36	0.05	0.03
48.25	0.31	0.69	0.33	0.05	0.03	48.30	0.28	0.72	0.31	0.05	0.03
48.35	0.25	0.75	0.30	0.05	0.03	48.40	2.00	0.00	0.00	0.05	0.00
48.45	2.00	0.00	0.00	0.05	0.00	48.50	2.00	0.00	0.00	0.05	0.00
48.55	2.00	0.00	0.00	0.05	0.00	48.60	2.00	0.00	0.00	0.05	0.00
48.65	2.00	0.00	0.00	0.05	0.00	48.70	2.00	0.00	0.00	0.05	0.00
48.75	2.00	0.00	0.00	0.05	0.00	48.80	2.00	0.00	0.00	0.05	0.00
48.85	2.00	0.00	0.00	0.05	0.00	48.90	2.00	0.00	0.00	0.05	0.00
48.95	2.00	0.00	0.00	0.05	0.00	49.00	2.00	0.00	0.00	0.05	0.00
49.05	0.39	0.61	0.38	0.05	0.02	49.10	2.00	0.00	0.00	0.05	0.00
49.15	2.00	0.00	0.00	0.05	0.00	49.20	2.00	0.00	0.00	0.05	0.00
49.25	2.00	0.00	0.00	0.05	0.00	49.30	2.00	0.00	0.00	0.05	0.00
49.35	2.00	0.00	0.00	0.05	0.00	49.40	0.30	0.70	0.32	0.05	0.03
49.45	2.00	0.00	0.00	0.05	0.00	49.50	2.00	0.00	0.00	0.05	0.00
49.55	2.00	0.00	0.00	0.05	0.00	49.60	2.00	0.00	0.00	0.05	0.00
49.65	2.00	0.00	0.00	0.05	0.00	49.70	2.00	0.00	0.00	0.05	0.00
49.75	0.35	0.65	0.35	0.05	0.02	49.80	0.37	0.63	0.37	0.05	0.02
49.85	0.36	0.64	0.36	0.05	0.02	49.90	0.32	0.68	0.34	0.05	0.02

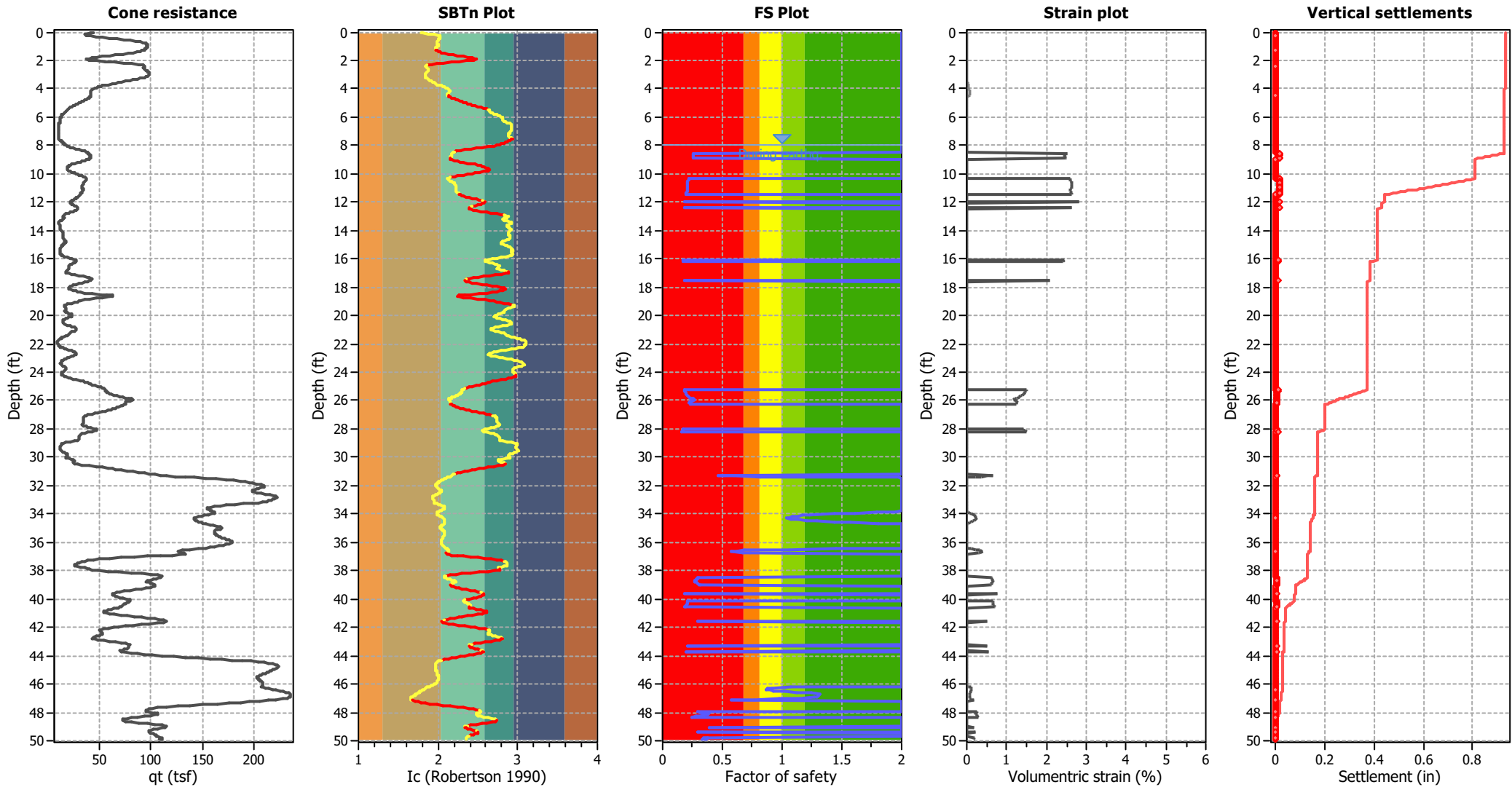
Overall liquefaction potential: 7.21LPI_{ISH} > 5.0 - Liquefaction manifestation is expected**Abbreviations**

FS: Calculated factor of safety for test point

d_z: Layer thickness (ft)

LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

- q_c : Total cone resistance (cone resistance q_c corrected for pore water effects)
- I_c : Soil Behaviour Type Index
- FS: Calculated Factor of Safety against liquefaction
- Volumetric strain: Post-liquefaction volumetric strain

:: Post-earthquake settlement of dry sands ::												
Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
0.05	1.78	72.27	1.00	72.27	14	386	0.56	0.000	0.00	13.69	0.00	0.000
0.10	1.81	67.76	1.00	67.76	13	377	0.56	0.001	0.00	13.69	0.00	0.000
0.15	1.88	61.39	1.00	61.39	12	370	0.56	0.001	0.00	13.69	0.00	0.000
0.20	1.95	58.70	1.27	74.67	15	390	0.56	0.002	0.00	13.69	0.00	0.000
0.25	2.00	60.20	1.31	78.78	16	425	0.56	0.002	0.00	13.69	0.00	0.000
0.30	2.02	66.92	1.32	88.36	19	481	0.56	0.002	0.00	13.69	0.00	0.000
0.35	2.02	75.73	1.32	100.32	21	548	0.56	0.002	0.00	13.69	0.00	0.000
0.40	2.02	86.34	1.32	114.07	24	621	0.55	0.002	0.00	13.69	0.00	0.000
0.45	2.02	96.83	1.32	127.85	27	696	0.55	0.002	0.00	13.69	0.00	0.000
0.50	2.01	108.03	1.31	142.01	30	770	0.55	0.002	0.00	13.69	0.00	0.000
0.55	2.00	118.43	1.31	155.26	32	840	0.54	0.002	0.00	13.69	0.00	0.000
0.60	2.00	129.00	1.30	168.33	35	906	0.54	0.002	0.00	13.69	0.00	0.000
0.65	1.99	137.96	1.30	179.52	37	964	0.53	0.002	0.00	13.69	0.00	0.000
0.70	1.99	145.10	1.30	188.52	39	1010	0.53	0.002	0.00	13.69	0.00	0.000
0.75	1.99	149.61	1.30	194.47	40	1043	0.53	0.002	0.00	13.69	0.00	0.000
0.80	1.99	152.23	1.30	198.25	41	1065	0.53	0.002	0.00	13.69	0.00	0.000
0.85	2.00	153.66	1.30	200.47	42	1079	0.53	0.003	0.00	13.69	0.00	0.000
0.90	2.00	154.39	1.31	201.72	42	1088	0.53	0.003	0.00	13.69	0.00	0.000
0.95	2.00	154.80	1.31	202.02	42	1088	0.53	0.003	0.00	13.69	0.00	0.000
1.00	1.99	154.84	1.30	201.51	42	1082	0.53	0.003	0.00	13.69	0.00	0.000
1.05	1.98	154.66	1.29	200.22	41	1069	0.53	0.003	0.00	13.69	0.00	0.000
1.10	1.98	154.13	1.29	198.56	41	1054	0.53	0.004	0.00	13.69	0.00	0.000
1.15	1.97	153.26	1.28	196.57	40	1038	0.53	0.004	0.00	13.69	0.00	0.000
1.20	1.97	152.02	1.28	194.83	40	1028	0.53	0.004	0.00	13.69	0.00	0.000
1.25	1.97	150.04	1.28	192.76	40	1020	0.53	0.004	0.00	13.69	0.00	0.000
1.30	1.98	147.38	1.29	190.63	0	0	0.53	0.000	0.00	13.69	0.00	0.000
1.35	2.00	143.34	1.31	187.31	0	0	0.53	0.000	0.00	13.69	0.00	0.000
1.40	2.02	138.61	1.33	183.81	0	0	0.53	0.000	0.00	13.69	0.00	0.000
1.45	2.05	132.63	1.36	179.81	0	0	0.53	0.000	0.00	13.69	0.00	0.000
1.50	2.09	125.48	1.40	175.83	0	0	0.53	0.000	0.00	13.69	0.00	0.000
1.55	2.13	116.85	1.47	172.30	0	0	0.54	0.000	0.00	13.69	0.00	0.000
1.60	2.19	106.47	1.59	168.91	0	0	0.54	0.000	0.00	13.69	0.00	0.000
1.65	2.25	96.04	1.75	168.09	0	0	0.54	0.000	0.00	13.69	0.00	0.000
1.70	2.31	85.53	1.97	168.23	0	0	0.55	0.000	0.00	13.69	0.00	0.000
1.75	2.37	77.02	2.23	171.49	0	0	0.55	0.000	0.00	13.69	0.00	0.000
1.80	2.42	69.49	2.50	173.94	0	0	0.55	0.000	0.00	13.69	0.00	0.000
1.85	2.47	64.14	2.75	176.62	0	0	0.55	0.000	0.00	13.69	0.00	0.000
1.90	2.49	60.39	2.91	175.70	0	0	0.56	0.000	0.00	13.69	0.00	0.000
1.95	2.48	60.83	2.86	174.16	0	0	0.56	0.000	0.00	13.69	0.00	0.000
2.00	2.44	65.45	2.58	169.03	0	0	0.55	0.000	0.00	13.69	0.00	0.000
2.05	2.36	75.85	2.17	164.65	0	0	0.55	0.000	0.00	13.69	0.00	0.000
2.10	2.26	88.90	1.79	159.30	0	0	0.55	0.000	0.00	13.69	0.00	0.000
2.15	2.16	103.88	1.53	158.98	0	0	0.54	0.000	0.00	13.69	0.00	0.000
2.20	2.07	118.36	1.37	162.65	0	0	0.54	0.000	0.00	13.69	0.00	0.000
2.25	1.98	131.51	1.29	169.92	0	0	0.54	0.000	0.00	13.69	0.00	0.000
2.30	1.91	142.01	1.24	176.62	0	0	0.54	0.000	0.00	13.69	0.00	0.000
2.35	1.86	148.18	1.21	179.31	0	0	0.54	0.000	0.00	13.69	0.00	0.000
2.40	1.84	150.68	1.19	179.81	0	0	0.54	0.000	0.00	13.69	0.00	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
2.45	1.84	150.58	1.19	179.54	35	867	0.54	0.013	0.01	13.69	0.01	0.000
2.50	1.85	149.82	1.20	180.14	35	876	0.54	0.013	0.01	13.69	0.01	0.000
2.55	1.87	149.62	1.21	181.47	36	890	0.54	0.013	0.01	13.69	0.01	0.000
2.60	1.88	150.05	1.22	183.19	36	905	0.54	0.013	0.01	13.69	0.01	0.000
2.65	1.88	151.28	1.22	185.06	37	916	0.54	0.013	0.01	13.69	0.01	0.000
2.70	1.88	152.70	1.22	186.47	37	921	0.54	0.013	0.01	13.69	0.01	0.000
2.75	1.87	154.29	1.22	187.55	37	922	0.54	0.013	0.01	13.69	0.01	0.000
2.80	1.86	155.63	1.21	188.16	37	920	0.54	0.014	0.01	13.69	0.01	0.000
2.85	1.85	156.80	1.20	188.52	37	917	0.54	0.014	0.01	13.69	0.01	0.000
2.90	1.84	157.68	1.20	188.59	37	913	0.54	0.014	0.01	13.69	0.01	0.000
2.95	1.84	158.15	1.19	188.33	37	909	0.54	0.015	0.01	13.69	0.01	0.000
3.00	1.84	158.12	1.19	187.86	37	905	0.54	0.015	0.01	13.69	0.01	0.000
3.05	1.84	157.39	1.19	186.98	37	901	0.54	0.016	0.01	13.69	0.01	0.000
3.10	1.84	156.09	1.19	185.74	36	896	0.54	0.016	0.01	13.69	0.01	0.000
3.15	1.84	153.59	1.19	183.41	36	887	0.54	0.017	0.01	13.69	0.01	0.000
3.20	1.85	150.16	1.20	180.17	35	875	0.54	0.018	0.01	13.69	0.01	0.000
3.25	1.86	145.06	1.21	175.26	35	856	0.54	0.019	0.01	13.69	0.01	0.000
3.30	1.87	139.50	1.22	169.81	34	836	0.55	0.020	0.01	13.69	0.01	0.000
3.35	1.89	133.24	1.23	163.52	33	813	0.55	0.022	0.01	13.69	0.01	0.000
3.40	1.90	127.21	1.24	157.37	32	790	0.55	0.024	0.01	13.69	0.01	0.000
3.45	1.92	121.20	1.25	151.16	30	768	0.55	0.026	0.02	13.69	0.01	0.000
3.50	1.93	115.48	1.26	145.18	29	746	0.55	0.028	0.02	13.69	0.02	0.000
3.55	1.95	110.32	1.27	139.76	28	726	0.55	0.031	0.02	13.69	0.02	0.000
3.60	1.96	105.14	1.28	134.31	28	705	0.55	0.033	0.02	13.69	0.02	0.000
3.65	1.98	100.10	1.29	129.02	27	685	0.55	0.037	0.03	13.69	0.02	0.000
3.70	2.00	94.74	1.30	123.55	26	665	0.55	0.041	0.03	13.69	0.03	0.000
3.75	2.02	89.85	1.32	118.80	25	647	0.55	0.045	0.03	13.69	0.03	0.000
3.80	2.04	85.55	1.35	115.11	24	636	0.55	0.048	0.04	13.69	0.03	0.000
3.85	2.06	81.81	1.37	112.24	24	626	0.55	0.052	0.04	13.69	0.04	0.000
3.90	2.09	78.55	1.40	110.01	24	618	0.55	0.055	0.04	13.69	0.04	0.000
3.95	2.11	75.42	1.43	107.67	23	608	0.55	0.059	0.05	13.69	0.04	0.000
4.00	2.12	72.79	1.45	105.57	23	598	0.55	0.064	0.05	13.69	0.05	0.000
4.05	2.13	70.41	1.47	103.50	23	587	0.55	0.069	0.06	13.69	0.05	0.000
4.10	2.14	68.61	1.49	101.91	22	578	0.55	0.075	0.07	13.69	0.06	0.000
4.15	2.15	67.37	1.49	100.69	22	571	0.55	0.080	0.07	13.69	0.06	0.000
4.20	2.15	66.77	1.50	99.85	22	566	0.55	0.084	0.07	13.69	0.07	0.000
4.25	2.14	66.59	1.49	99.01	22	561	0.55	0.088	0.08	13.69	0.07	0.000
4.30	2.13	66.58	1.47	98.16	22	556	0.55	0.093	0.09	13.69	0.08	0.000
4.35	2.13	66.58	1.46	97.18	21	550	0.55	0.099	0.09	13.69	0.08	0.000
4.40	2.12	66.57	1.45	96.68	21	547	0.55	0.104	0.10	13.69	0.09	0.001
4.45	2.12	66.57	1.45	96.66	21	547	0.55	0.106	0.10	13.69	0.09	0.001
4.50	2.13	66.47	1.47	97.46	21	552	0.55	0.105	0.10	13.69	0.09	0.001
4.55	2.14	66.16	1.49	98.49	0	0	0.55	0.000	0.00	13.69	0.00	0.000
4.60	2.16	65.37	1.52	99.55	0	0	0.55	0.000	0.00	13.69	0.00	0.000
4.65	2.18	64.12	1.56	100.22	0	0	0.55	0.000	0.00	13.69	0.00	0.000
4.70	2.20	62.28	1.61	100.57	0	0	0.55	0.000	0.00	13.69	0.00	0.000
4.75	2.22	60.26	1.68	101.16	0	0	0.55	0.000	0.00	13.69	0.00	0.000
4.80	2.25	57.96	1.76	101.80	0	0	0.55	0.000	0.00	13.69	0.00	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
4.85	2.28	55.79	1.84	102.75	0	0	0.55	0.000	0.00	13.69	0.00	0.000
4.90	2.30	53.51	1.93	103.16	0	0	0.56	0.000	0.00	13.69	0.00	0.000
4.95	2.32	51.31	2.01	103.36	0	0	0.56	0.000	0.00	13.69	0.00	0.000
5.00	2.35	49.10	2.11	103.71	0	0	0.56	0.000	0.00	13.69	0.00	0.000
5.05	2.37	46.84	2.23	104.56	0	0	0.56	0.000	0.00	13.69	0.00	0.000
5.10	2.40	44.67	2.39	106.54	0	0	0.56	0.000	0.00	13.69	0.00	0.000
5.15	2.44	42.37	2.57	108.83	0	0	0.56	0.000	0.00	13.69	0.00	0.000
5.20	2.47	40.19	2.79	111.95	0	0	0.56	0.000	0.00	13.69	0.00	0.000
5.25	2.51	37.95	3.03	114.88	0	0	0.56	0.000	0.00	13.69	0.00	0.000
5.30	2.54	35.94	3.29	118.08	0	0	0.56	0.000	0.00	13.69	0.00	0.000
5.35	2.57	34.17	3.53	120.73	0	0	0.56	0.000	0.00	13.69	0.00	0.000
5.40	2.60	32.71	3.76	122.93	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.45	2.62	31.51	3.94	124.14	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.50	2.64	30.36	4.09	124.08	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.55	2.65	29.43	4.17	122.80	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.60	2.65	28.63	4.22	120.72	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.65	2.65	27.83	4.25	118.31	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.70	2.66	26.82	4.34	116.50	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.75	2.68	25.38	4.53	115.07	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.80	2.71	23.97	4.79	114.86	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.85	2.74	22.59	5.09	115.07	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.90	2.76	21.64	5.37	116.24	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.95	2.78	20.94	5.61	117.53	0	0	0.56	0.000	0.00	0.00	0.00	0.000
6.00	2.79	20.62	5.78	119.14	0	0	0.56	0.000	0.00	0.00	0.00	0.000
6.05	2.80	20.48	5.88	120.42	0	0	0.56	0.000	0.00	0.00	0.00	0.000
6.10	2.81	20.48	5.93	121.49	0	0	0.56	0.000	0.00	0.00	0.00	0.000
6.15	2.81	20.48	5.97	122.32	0	0	0.56	0.000	0.00	0.00	0.00	0.000
6.20	2.81	20.47	6.03	123.35	0	0	0.56	0.000	0.00	0.00	0.00	0.000
6.25	2.82	20.47	6.10	124.76	0	0	0.56	0.000	0.00	0.00	0.00	0.000
6.30	2.83	20.34	6.22	126.53	0	0	0.56	0.000	0.00	0.00	0.00	0.000
6.35	2.85	19.80	6.45	127.73	0	0	0.56	0.000	0.00	0.00	0.00	0.000
6.40	2.87	18.92	6.79	128.39	0	0	0.56	0.000	0.00	0.00	0.00	0.000
6.45	2.90	17.77	7.19	127.85	0	0	0.56	0.000	0.00	0.00	0.00	0.000
6.50	2.92	17.03	7.49	127.50	0	0	0.56	0.000	0.00	0.00	0.00	0.000
6.55	2.93	16.63	7.63	126.85	0	0	0.56	0.000	0.00	0.00	0.00	0.000
6.60	2.93	16.61	7.62	126.49	0	0	0.56	0.000	0.00	0.00	0.00	0.000
6.65	2.92	16.60	7.57	125.68	0	0	0.56	0.000	0.00	0.00	0.00	0.000
6.70	2.92	16.60	7.52	124.89	0	0	0.56	0.000	0.00	0.00	0.00	0.000
6.75	2.92	16.59	7.49	124.30	0	0	0.56	0.000	0.00	0.00	0.00	0.000
6.80	2.92	16.59	7.47	123.96	0	0	0.56	0.000	0.00	0.00	0.00	0.000
6.85	2.92	16.59	7.46	123.73	0	0	0.56	0.000	0.00	0.00	0.00	0.000
6.90	2.92	16.58	7.43	123.25	0	0	0.57	0.000	0.00	0.00	0.00	0.000
6.95	2.91	16.58	7.39	122.48	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.00	2.91	16.57	7.32	121.37	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.05	2.90	16.57	7.26	120.24	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.10	2.90	16.56	7.18	118.94	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.15	2.89	16.56	7.10	117.64	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.20	2.89	16.55	7.02	116.22	0	0	0.57	0.000	0.00	0.00	0.00	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
7.25	2.88	16.55	6.98	115.47	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.30	2.88	16.54	6.98	115.48	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.35	2.89	16.54	7.08	117.10	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.40	2.90	16.54	7.23	119.55	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.45	2.92	16.53	7.44	122.97	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.50	2.93	16.61	7.61	126.44	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.55	2.93	17.10	7.66	130.95	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.60	2.92	18.02	7.53	135.71	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.65	2.90	19.46	7.24	140.90	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.70	2.88	20.86	6.93	144.59	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.75	2.86	22.20	6.63	147.22	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.80	2.84	23.33	6.38	148.74	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.85	2.82	24.42	6.13	149.67	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.90	2.80	25.56	5.87	149.97	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.95	2.78	26.75	5.55	148.47	0	0	0.57	0.000	0.00	0.00	0.00	0.000

Total estimated settlement: 0.01**Abbreviations**

Q_{tn}: Normalized cone resistance
 K_c: Fines correction factor
 Q_{tn,cs}: Equivalent clean sand normalized cone resistance
 G_{max}: Small strain shear modulus
 CSR: Soil cyclic stress ratio
 γ: Cyclic shear strain
 e_{vol(15)}: Volumetric strain after 15 cycles
 N_c: Equivalent number of cycles
 e_v: Volumetric strain
 Settle.: Calculated settlement

:: Post-earthquake settlement due to soil liquefaction ::

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
8.00	26.10	2.00	0.00	0.85	0.00	8.05	27.57	2.00	0.00	0.85	0.00
8.10	29.85	2.00	0.00	0.85	0.00	8.15	91.74	2.00	0.00	0.85	0.00
8.20	94.91	2.00	0.00	0.85	0.00	8.25	97.25	2.00	0.00	0.85	0.00
8.30	100.94	2.00	0.00	0.85	0.00	8.35	103.10	2.00	0.00	0.85	0.00
8.40	105.56	2.00	0.00	0.85	0.00	8.45	106.36	2.00	0.00	0.85	0.00
8.50	107.05	2.00	0.00	0.85	0.00	8.55	107.83	0.26	2.51	0.84	0.02
8.60	108.53	0.26	2.49	0.84	0.01	8.65	109.47	0.26	2.47	0.84	0.01
8.70	109.72	0.26	2.46	0.84	0.01	8.75	109.81	0.26	2.45	0.84	0.01
8.80	109.40	0.26	2.46	0.84	0.01	8.85	108.80	0.26	2.47	0.84	0.01
8.90	108.05	0.25	2.49	0.84	0.01	8.95	106.74	2.00	0.00	0.84	0.00
9.00	105.47	2.00	0.00	0.84	0.00	9.05	102.95	2.00	0.00	0.84	0.00
9.10	101.13	2.00	0.00	0.83	0.00	9.15	98.44	2.00	0.00	0.83	0.00
9.20	96.72	2.00	0.00	0.83	0.00	9.25	94.30	2.00	0.00	0.83	0.00
9.30	92.18	2.00	0.00	0.83	0.00	9.35	89.86	2.00	0.00	0.83	0.00
9.40	88.10	2.00	0.00	0.83	0.00	9.45	87.06	2.00	0.00	0.83	0.00
9.50	86.74	2.00	0.00	0.83	0.00	9.55	86.48	2.00	0.00	0.83	0.00
9.60	27.37	2.00	0.00	0.83	0.00	9.65	26.87	2.00	0.00	0.82	0.00
9.70	26.48	2.00	0.00	0.82	0.00	9.75	26.44	2.00	0.00	0.82	0.00
9.80	27.61	2.00	0.00	0.82	0.00	9.85	89.87	2.00	0.00	0.82	0.00
9.90	92.06	2.00	0.00	0.82	0.00	9.95	94.43	2.00	0.00	0.82	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
10.00	95.25	2.00	0.00	0.82	0.00	10.05	96.02	2.00	0.00	0.82	0.00
10.10	98.43	2.00	0.00	0.82	0.00	10.15	99.23	2.00	0.00	0.82	0.00
10.20	100.25	2.00	0.00	0.81	0.00	10.25	100.06	2.00	0.00	0.81	0.00
10.30	100.20	2.00	0.00	0.81	0.00	10.35	100.08	0.22	2.61	0.81	0.02
10.40	100.21	0.21	2.60	0.81	0.02	10.45	99.89	0.21	2.61	0.81	0.02
10.50	99.55	0.21	2.61	0.81	0.02	10.55	98.79	0.21	2.63	0.81	0.02
10.60	98.42	0.21	2.64	0.81	0.02	10.65	98.18	0.21	2.64	0.81	0.02
10.70	98.57	0.21	2.63	0.81	0.02	10.75	98.63	0.21	2.62	0.80	0.02
10.80	98.29	0.21	2.63	0.80	0.02	10.85	97.97	0.21	2.63	0.80	0.02
10.90	97.53	0.20	2.64	0.80	0.02	10.95	98.00	0.21	2.63	0.80	0.02
11.00	98.28	0.21	2.62	0.80	0.02	11.05	98.72	0.21	2.60	0.80	0.02
11.10	98.76	0.21	2.60	0.80	0.02	11.15	98.71	0.20	2.60	0.80	0.02
11.20	98.69	0.20	2.59	0.80	0.02	11.25	98.62	0.20	2.59	0.80	0.02
11.30	97.70	0.20	2.61	0.79	0.02	11.35	97.16	0.20	2.63	0.79	0.02
11.40	96.39	0.20	2.64	0.79	0.02	11.45	96.54	0.20	2.64	0.79	0.02
11.50	96.89	2.00	0.00	0.79	0.00	11.55	96.30	2.00	0.00	0.79	0.00
11.60	95.95	2.00	0.00	0.79	0.00	11.65	95.07	2.00	0.00	0.79	0.00
11.70	94.59	2.00	0.00	0.79	0.00	11.75	93.86	2.00	0.00	0.79	0.00
11.80	92.70	2.00	0.00	0.79	0.00	11.85	91.44	2.00	0.00	0.78	0.00
11.90	90.16	2.00	0.00	0.78	0.00	11.95	89.43	2.00	0.00	0.78	0.00
12.00	88.88	0.18	2.83	0.78	0.02	12.05	89.01	2.00	0.00	0.78	0.00
12.10	89.20	2.00	0.00	0.78	0.00	12.15	90.34	2.00	0.00	0.78	0.00
12.20	91.24	2.00	0.00	0.78	0.00	12.25	92.89	2.00	0.00	0.78	0.00
12.30	93.69	2.00	0.00	0.78	0.00	12.35	94.80	2.00	0.00	0.78	0.00
12.40	95.07	0.19	2.62	0.77	0.02	12.45	95.63	2.00	0.00	0.77	0.00
12.50	94.95	2.00	0.00	0.77	0.00	12.55	94.44	2.00	0.00	0.77	0.00
12.60	92.87	2.00	0.00	0.77	0.00	12.65	91.12	2.00	0.00	0.77	0.00
12.70	29.19	2.00	0.00	0.77	0.00	12.75	26.22	2.00	0.00	0.77	0.00
12.80	23.57	2.00	0.00	0.77	0.00	12.85	21.64	2.00	0.00	0.77	0.00
12.90	20.61	2.00	0.00	0.77	0.00	12.95	20.11	2.00	0.00	0.76	0.00
13.00	20.00	2.00	0.00	0.76	0.00	13.05	19.99	2.00	0.00	0.76	0.00
13.10	20.41	2.00	0.00	0.76	0.00	13.15	20.68	2.00	0.00	0.76	0.00
13.20	20.66	2.00	0.00	0.76	0.00	13.25	19.70	2.00	0.00	0.76	0.00
13.30	17.82	2.00	0.00	0.76	0.00	13.35	16.13	2.00	0.00	0.76	0.00
13.40	14.58	2.00	0.00	0.76	0.00	13.45	14.09	2.00	0.00	0.76	0.00
13.50	14.16	2.00	0.00	0.75	0.00	13.55	15.12	2.00	0.00	0.75	0.00
13.60	15.89	2.00	0.00	0.75	0.00	13.65	16.77	2.00	0.00	0.75	0.00
13.70	16.76	2.00	0.00	0.75	0.00	13.75	16.74	2.00	0.00	0.75	0.00
13.80	16.72	2.00	0.00	0.75	0.00	13.85	16.70	2.00	0.00	0.75	0.00
13.90	16.68	2.00	0.00	0.75	0.00	13.95	16.66	2.00	0.00	0.75	0.00
14.00	16.69	2.00	0.00	0.75	0.00	14.05	17.58	2.00	0.00	0.74	0.00
14.10	18.33	2.00	0.00	0.74	0.00	14.15	19.25	2.00	0.00	0.74	0.00
14.20	19.48	2.00	0.00	0.74	0.00	14.25	19.46	2.00	0.00	0.74	0.00
14.30	19.44	2.00	0.00	0.74	0.00	14.35	19.41	2.00	0.00	0.74	0.00
14.40	19.39	2.00	0.00	0.74	0.00	14.45	19.37	2.00	0.00	0.74	0.00
14.50	19.35	2.00	0.00	0.74	0.00	14.55	19.63	2.00	0.00	0.74	0.00
14.60	20.04	2.00	0.00	0.73	0.00	14.65	20.89	2.00	0.00	0.73	0.00
14.70	21.52	2.00	0.00	0.73	0.00	14.75	21.97	2.00	0.00	0.73	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
14.80	22.09	2.00	0.00	0.73	0.00	14.85	22.07	2.00	0.00	0.73	0.00
14.90	21.34	2.00	0.00	0.73	0.00	14.95	20.52	2.00	0.00	0.73	0.00
15.00	19.60	2.00	0.00	0.73	0.00	15.05	18.83	2.00	0.00	0.73	0.00
15.10	17.88	2.00	0.00	0.73	0.00	15.15	17.10	2.00	0.00	0.72	0.00
15.20	16.22	2.00	0.00	0.72	0.00	15.25	16.18	2.00	0.00	0.72	0.00
15.30	16.17	2.00	0.00	0.72	0.00	15.35	16.15	2.00	0.00	0.72	0.00
15.40	16.13	2.00	0.00	0.72	0.00	15.45	16.11	2.00	0.00	0.72	0.00
15.50	16.10	2.00	0.00	0.72	0.00	15.55	16.08	2.00	0.00	0.72	0.00
15.60	16.06	2.00	0.00	0.72	0.00	15.65	16.05	2.00	0.00	0.72	0.00
15.70	16.03	2.00	0.00	0.71	0.00	15.75	16.75	2.00	0.00	0.71	0.00
15.80	18.05	2.00	0.00	0.71	0.00	15.85	20.74	2.00	0.00	0.71	0.00
15.90	23.40	2.00	0.00	0.71	0.00	15.95	26.48	2.00	0.00	0.71	0.00
16.00	28.79	2.00	0.00	0.71	0.00	16.05	31.42	2.00	0.00	0.71	0.00
16.10	92.98	0.17	2.45	0.71	0.01	16.15	94.37	0.17	2.41	0.71	0.01
16.20	33.00	2.00	0.00	0.71	0.00	16.25	31.95	2.00	0.00	0.70	0.00
16.30	29.71	2.00	0.00	0.70	0.00	16.35	28.11	2.00	0.00	0.70	0.00
16.40	26.35	2.00	0.00	0.70	0.00	16.45	25.48	2.00	0.00	0.70	0.00
16.50	24.76	2.00	0.00	0.70	0.00	16.55	24.74	2.00	0.00	0.70	0.00
16.60	24.72	2.00	0.00	0.70	0.00	16.65	24.69	2.00	0.00	0.70	0.00
16.70	24.41	2.00	0.00	0.70	0.00	16.75	23.97	2.00	0.00	0.70	0.00
16.80	23.54	2.00	0.00	0.69	0.00	16.85	22.99	2.00	0.00	0.69	0.00
16.90	21.64	2.00	0.00	0.69	0.00	16.95	21.11	2.00	0.00	0.69	0.00
17.00	21.09	2.00	0.00	0.69	0.00	17.05	23.56	2.00	0.00	0.69	0.00
17.10	26.73	2.00	0.00	0.69	0.00	17.15	31.67	2.00	0.00	0.69	0.00
17.20	35.84	2.00	0.00	0.69	0.00	17.25	103.35	2.00	0.00	0.69	0.00
17.30	106.43	2.00	0.00	0.69	0.00	17.35	109.75	2.00	0.00	0.68	0.00
17.40	109.52	2.00	0.00	0.68	0.00	17.45	109.12	2.00	0.00	0.68	0.00
17.50	106.95	2.00	0.00	0.68	0.00	17.55	105.29	0.18	2.07	0.68	0.01
17.60	103.00	2.00	0.00	0.68	0.00	17.65	100.81	2.00	0.00	0.68	0.00
17.70	98.41	2.00	0.00	0.68	0.00	17.75	94.19	2.00	0.00	0.68	0.00
17.80	91.16	2.00	0.00	0.68	0.00	17.85	29.30	2.00	0.00	0.68	0.00
17.90	27.76	2.00	0.00	0.67	0.00	17.95	26.32	2.00	0.00	0.67	0.00
18.00	24.77	2.00	0.00	0.67	0.00	18.05	23.35	2.00	0.00	0.67	0.00
18.10	23.74	2.00	0.00	0.67	0.00	18.15	25.13	2.00	0.00	0.67	0.00
18.20	28.98	2.00	0.00	0.67	0.00	18.25	31.08	2.00	0.00	0.67	0.00
18.30	33.04	2.00	0.00	0.67	0.00	18.35	35.66	2.00	0.00	0.67	0.00
18.40	39.20	2.00	0.00	0.67	0.00	18.45	112.23	2.00	0.00	0.66	0.00
18.50	119.55	2.00	0.00	0.66	0.00	18.55	128.67	2.00	0.00	0.66	0.00
18.60	130.28	2.00	0.00	0.66	0.00	18.65	132.24	2.00	0.00	0.66	0.00
18.70	125.75	2.00	0.00	0.66	0.00	18.75	121.44	2.00	0.00	0.66	0.00
18.80	112.46	2.00	0.00	0.66	0.00	18.85	107.31	2.00	0.00	0.66	0.00
18.90	101.18	2.00	0.00	0.66	0.00	18.95	36.25	2.00	0.00	0.66	0.00
19.00	33.76	2.00	0.00	0.65	0.00	19.05	32.28	2.00	0.00	0.65	0.00
19.10	30.17	2.00	0.00	0.65	0.00	19.15	26.15	2.00	0.00	0.65	0.00
19.20	22.67	2.00	0.00	0.65	0.00	19.25	18.80	2.00	0.00	0.65	0.00
19.30	18.38	2.00	0.00	0.65	0.00	19.35	18.28	2.00	0.00	0.65	0.00
19.40	19.12	2.00	0.00	0.65	0.00	19.45	19.78	2.00	0.00	0.65	0.00
19.50	20.59	2.00	0.00	0.65	0.00	19.55	20.66	2.00	0.00	0.64	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
19.60	20.58	2.00	0.00	0.64	0.00	19.65	19.75	2.00	0.00	0.64	0.00
19.70	19.28	2.00	0.00	0.64	0.00	19.75	19.18	2.00	0.00	0.64	0.00
19.80	20.85	2.00	0.00	0.64	0.00	19.85	23.59	2.00	0.00	0.64	0.00
19.90	25.91	2.00	0.00	0.64	0.00	19.95	27.62	2.00	0.00	0.64	0.00
20.00	27.17	2.00	0.00	0.64	0.00	20.05	25.69	2.00	0.00	0.64	0.00
20.10	23.88	2.00	0.00	0.63	0.00	20.15	21.89	2.00	0.00	0.63	0.00
20.20	19.89	2.00	0.00	0.63	0.00	20.25	18.04	2.00	0.00	0.63	0.00
20.30	16.48	2.00	0.00	0.63	0.00	20.35	16.21	2.00	0.00	0.63	0.00
20.40	16.69	2.00	0.00	0.63	0.00	20.45	17.08	2.00	0.00	0.63	0.00
20.50	17.09	2.00	0.00	0.63	0.00	20.55	17.12	2.00	0.00	0.63	0.00
20.60	17.52	2.00	0.00	0.63	0.00	20.65	18.57	2.00	0.00	0.62	0.00
20.70	21.05	2.00	0.00	0.62	0.00	20.75	23.61	2.00	0.00	0.62	0.00
20.80	26.60	2.00	0.00	0.62	0.00	20.85	28.85	2.00	0.00	0.62	0.00
20.90	30.52	2.00	0.00	0.62	0.00	20.95	31.31	2.00	0.00	0.62	0.00
21.00	31.00	2.00	0.00	0.62	0.00	21.05	29.77	2.00	0.00	0.62	0.00
21.10	28.08	2.00	0.00	0.62	0.00	21.15	26.27	2.00	0.00	0.62	0.00
21.20	24.27	2.00	0.00	0.61	0.00	21.25	23.21	2.00	0.00	0.61	0.00
21.30	23.19	2.00	0.00	0.61	0.00	21.35	22.47	2.00	0.00	0.61	0.00
21.40	21.29	2.00	0.00	0.61	0.00	21.45	18.92	2.00	0.00	0.61	0.00
21.50	16.90	2.00	0.00	0.61	0.00	21.55	15.65	2.00	0.00	0.61	0.00
21.60	14.65	2.00	0.00	0.61	0.00	21.65	13.41	2.00	0.00	0.61	0.00
21.70	12.37	2.00	0.00	0.61	0.00	21.75	11.27	2.00	0.00	0.60	0.00
21.80	10.68	2.00	0.00	0.60	0.00	21.85	10.32	2.00	0.00	0.60	0.00
21.90	10.31	2.00	0.00	0.60	0.00	21.95	10.62	2.00	0.00	0.60	0.00
22.00	11.21	2.00	0.00	0.60	0.00	22.05	11.68	2.00	0.00	0.60	0.00
22.10	12.13	2.00	0.00	0.60	0.00	22.15	12.59	2.00	0.00	0.60	0.00
22.20	13.25	2.00	0.00	0.60	0.00	22.25	14.53	2.00	0.00	0.60	0.00
22.30	15.63	2.00	0.00	0.59	0.00	22.35	16.86	2.00	0.00	0.59	0.00
22.40	19.65	2.00	0.00	0.59	0.00	22.45	22.16	2.00	0.00	0.59	0.00
22.50	25.37	2.00	0.00	0.59	0.00	22.55	27.19	2.00	0.00	0.59	0.00
22.60	28.74	2.00	0.00	0.59	0.00	22.65	29.49	2.00	0.00	0.59	0.00
22.70	30.06	2.00	0.00	0.59	0.00	22.75	29.27	2.00	0.00	0.59	0.00
22.80	28.36	2.00	0.00	0.59	0.00	22.85	26.73	2.00	0.00	0.58	0.00
22.90	24.95	2.00	0.00	0.58	0.00	22.95	22.67	2.00	0.00	0.58	0.00
23.00	20.50	2.00	0.00	0.58	0.00	23.05	18.59	2.00	0.00	0.58	0.00
23.10	16.97	2.00	0.00	0.58	0.00	23.15	15.83	2.00	0.00	0.58	0.00
23.20	14.62	2.00	0.00	0.58	0.00	23.25	14.15	2.00	0.00	0.58	0.00
23.30	13.79	2.00	0.00	0.58	0.00	23.35	13.78	2.00	0.00	0.58	0.00
23.40	13.87	2.00	0.00	0.57	0.00	23.45	14.26	2.00	0.00	0.57	0.00
23.50	14.98	2.00	0.00	0.57	0.00	23.55	16.12	2.00	0.00	0.57	0.00
23.60	17.47	2.00	0.00	0.57	0.00	23.65	18.68	2.00	0.00	0.57	0.00
23.70	19.06	2.00	0.00	0.57	0.00	23.75	18.95	2.00	0.00	0.57	0.00
23.80	18.14	2.00	0.00	0.57	0.00	23.85	17.47	2.00	0.00	0.57	0.00
23.90	16.73	2.00	0.00	0.57	0.00	23.95	15.62	2.00	0.00	0.56	0.00
24.00	14.71	2.00	0.00	0.56	0.00	24.05	13.90	2.00	0.00	0.56	0.00
24.10	13.61	2.00	0.00	0.56	0.00	24.15	13.60	2.00	0.00	0.56	0.00
24.20	14.18	2.00	0.00	0.56	0.00	24.25	14.94	2.00	0.00	0.56	0.00
24.30	16.83	2.00	0.00	0.56	0.00	24.35	18.51	2.00	0.00	0.56	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
24.40	20.87	2.00	0.00	0.56	0.00	24.45	22.98	2.00	0.00	0.56	0.00
24.50	25.56	2.00	0.00	0.55	0.00	24.55	28.90	2.00	0.00	0.55	0.00
24.60	32.03	2.00	0.00	0.55	0.00	24.65	35.47	2.00	0.00	0.55	0.00
24.70	37.58	2.00	0.00	0.55	0.00	24.75	39.40	2.00	0.00	0.55	0.00
24.80	103.30	2.00	0.00	0.55	0.00	24.85	104.67	2.00	0.00	0.55	0.00
24.90	106.93	2.00	0.00	0.55	0.00	24.95	108.86	2.00	0.00	0.55	0.00
25.00	112.07	2.00	0.00	0.55	0.00	25.05	113.87	2.00	0.00	0.54	0.00
25.10	116.06	2.00	0.00	0.54	0.00	25.15	115.80	2.00	0.00	0.54	0.00
25.20	115.62	2.00	0.00	0.54	0.00	25.25	115.69	0.19	1.49	0.54	0.01
25.30	116.04	0.19	1.49	0.54	0.01	25.35	117.01	0.19	1.47	0.54	0.01
25.40	117.66	0.19	1.46	0.54	0.01	25.45	118.30	0.19	1.45	0.54	0.01
25.50	119.81	0.19	1.43	0.54	0.01	25.55	120.99	0.20	1.41	0.54	0.01
25.60	122.88	0.20	1.38	0.53	0.01	25.65	124.56	0.21	1.36	0.53	0.01
25.70	127.45	0.22	1.33	0.53	0.01	25.75	129.28	0.22	1.30	0.53	0.01
25.80	131.25	0.23	1.28	0.53	0.01	25.85	134.22	0.24	1.25	0.53	0.01
25.90	136.67	0.25	1.22	0.53	0.01	25.95	140.68	0.27	1.18	0.53	0.01
26.00	139.02	0.26	1.19	0.53	0.01	26.05	134.56	0.24	1.23	0.53	0.01
26.10	131.68	0.23	1.26	0.53	0.01	26.15	129.37	0.22	1.28	0.52	0.01
26.20	131.44	0.23	1.26	0.52	0.01	26.25	131.69	0.23	1.25	0.52	0.01
26.30	130.28	2.00	0.00	0.52	0.00	26.35	129.35	2.00	0.00	0.52	0.00
26.40	128.27	2.00	0.00	0.52	0.00	26.45	127.14	2.00	0.00	0.52	0.00
26.50	126.42	2.00	0.00	0.52	0.00	26.55	125.37	2.00	0.00	0.52	0.00
26.60	124.35	2.00	0.00	0.52	0.00	26.65	122.51	2.00	0.00	0.52	0.00
26.70	120.11	2.00	0.00	0.51	0.00	26.75	117.59	2.00	0.00	0.51	0.00
26.80	115.08	2.00	0.00	0.51	0.00	26.85	112.70	2.00	0.00	0.51	0.00
26.90	108.78	2.00	0.00	0.51	0.00	26.95	42.16	2.00	0.00	0.51	0.00
27.00	38.54	2.00	0.00	0.51	0.00	27.05	36.36	2.00	0.00	0.51	0.00
27.10	34.78	2.00	0.00	0.51	0.00	27.15	34.50	2.00	0.00	0.51	0.00
27.20	34.33	2.00	0.00	0.51	0.00	27.25	34.18	2.00	0.00	0.50	0.00
27.30	33.78	2.00	0.00	0.50	0.00	27.35	33.37	2.00	0.00	0.50	0.00
27.40	33.83	2.00	0.00	0.50	0.00	27.45	34.20	2.00	0.00	0.50	0.00
27.50	34.68	2.00	0.00	0.50	0.00	27.55	34.57	2.00	0.00	0.50	0.00
27.60	34.19	2.00	0.00	0.50	0.00	27.65	32.89	2.00	0.00	0.50	0.00
27.70	31.98	2.00	0.00	0.50	0.00	27.75	33.06	2.00	0.00	0.50	0.00
27.80	34.17	2.00	0.00	0.49	0.00	27.85	35.91	2.00	0.00	0.49	0.00
27.90	37.65	2.00	0.00	0.49	0.00	27.95	39.68	2.00	0.00	0.49	0.00
28.00	43.55	2.00	0.00	0.49	0.00	28.05	110.07	0.17	1.43	0.49	0.01
28.10	110.12	0.17	1.42	0.49	0.01	28.15	108.22	0.17	1.45	0.49	0.01
28.20	104.53	0.16	1.50	0.49	0.01	28.25	38.30	2.00	0.00	0.49	0.00
28.30	34.80	2.00	0.00	0.49	0.00	28.35	31.93	2.00	0.00	0.48	0.00
28.40	30.48	2.00	0.00	0.48	0.00	28.45	30.31	2.00	0.00	0.48	0.00
28.50	30.01	2.00	0.00	0.48	0.00	28.55	29.62	2.00	0.00	0.48	0.00
28.60	29.15	2.00	0.00	0.48	0.00	28.65	28.91	2.00	0.00	0.48	0.00
28.70	29.44	2.00	0.00	0.48	0.00	28.75	29.41	2.00	0.00	0.48	0.00
28.80	28.90	2.00	0.00	0.48	0.00	28.85	25.38	2.00	0.00	0.48	0.00
28.90	21.16	2.00	0.00	0.47	0.00	28.95	16.69	2.00	0.00	0.47	0.00
29.00	14.00	2.00	0.00	0.47	0.00	29.05	13.25	2.00	0.00	0.47	0.00
29.10	12.85	2.00	0.00	0.47	0.00	29.15	12.49	2.00	0.00	0.47	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
29.20	12.47	2.00	0.00	0.47	0.00	29.25	12.46	2.00	0.00	0.47	0.00
29.30	12.45	2.00	0.00	0.47	0.00	29.35	12.44	2.00	0.00	0.47	0.00
29.40	12.44	2.00	0.00	0.47	0.00	29.45	12.43	2.00	0.00	0.46	0.00
29.50	12.43	2.00	0.00	0.46	0.00	29.55	13.11	2.00	0.00	0.46	0.00
29.60	13.69	2.00	0.00	0.46	0.00	29.65	14.42	2.00	0.00	0.46	0.00
29.70	15.35	2.00	0.00	0.46	0.00	29.75	16.75	2.00	0.00	0.46	0.00
29.80	18.00	2.00	0.00	0.46	0.00	29.85	19.10	2.00	0.00	0.46	0.00
29.90	19.09	2.00	0.00	0.46	0.00	29.95	18.37	2.00	0.00	0.46	0.00
30.00	16.18	2.00	0.00	0.45	0.00	30.05	16.77	2.00	0.00	0.45	0.00
30.10	18.45	2.00	0.00	0.45	0.00	30.15	22.02	2.00	0.00	0.45	0.00
30.20	24.61	2.00	0.00	0.45	0.00	30.25	24.59	2.00	0.00	0.45	0.00
30.30	24.27	2.00	0.00	0.45	0.00	30.35	23.53	2.00	0.00	0.45	0.00
30.40	23.23	2.00	0.00	0.45	0.00	30.45	23.20	2.00	0.00	0.45	0.00
30.50	27.04	2.00	0.00	0.45	0.00	30.55	30.98	2.00	0.00	0.44	0.00
30.60	37.61	2.00	0.00	0.44	0.00	30.65	43.54	2.00	0.00	0.44	0.00
30.70	50.91	2.00	0.00	0.44	0.00	30.75	121.23	2.00	0.00	0.44	0.00
30.80	124.79	2.00	0.00	0.44	0.00	30.85	128.14	2.00	0.00	0.44	0.00
30.90	131.80	2.00	0.00	0.44	0.00	30.95	138.38	2.00	0.00	0.44	0.00
31.00	143.02	2.00	0.00	0.44	0.00	31.05	147.86	2.00	0.00	0.44	0.00
31.10	152.35	2.00	0.00	0.43	0.00	31.15	155.69	2.00	0.00	0.43	0.00
31.20	159.52	2.00	0.00	0.43	0.00	31.25	164.10	0.47	0.65	0.43	0.00
31.30	171.36	0.59	0.50	0.43	0.00	31.35	179.80	0.82	0.37	0.43	0.00
31.40	188.31	1.18	0.21	0.43	0.00	31.45	198.50	1.98	0.00	0.43	0.00
31.50	206.41	2.00	0.00	0.43	0.00	31.55	217.60	2.00	0.00	0.43	0.00
31.60	223.64	2.00	0.00	0.43	0.00	31.65	230.31	2.00	0.00	0.42	0.00
31.70	233.37	2.00	0.00	0.42	0.00	31.75	235.83	2.00	0.00	0.42	0.00
31.80	237.85	2.00	0.00	0.42	0.00	31.85	239.51	2.00	0.00	0.42	0.00
31.90	242.34	2.00	0.00	0.42	0.00	31.95	244.89	2.00	0.00	0.42	0.00
32.00	248.07	2.00	0.00	0.42	0.00	32.05	248.08	2.00	0.00	0.42	0.00
32.10	248.47	2.00	0.00	0.42	0.00	32.15	247.61	2.00	0.00	0.42	0.00
32.20	247.60	2.00	0.00	0.41	0.00	32.25	247.25	2.00	0.00	0.41	0.00
32.30	247.36	2.00	0.00	0.41	0.00	32.35	247.16	2.00	0.00	0.41	0.00
32.40	247.36	2.00	0.00	0.41	0.00	32.45	247.69	2.00	0.00	0.41	0.00
32.50	248.84	2.00	0.00	0.41	0.00	32.55	249.16	2.00	0.00	0.41	0.00
32.60	249.06	2.00	0.00	0.41	0.00	32.65	249.26	2.00	0.00	0.41	0.00
32.70	248.53	2.00	0.00	0.41	0.00	32.75	248.67	2.00	0.00	0.40	0.00
32.80	247.35	2.00	0.00	0.40	0.00	32.85	246.16	2.00	0.00	0.40	0.00
32.90	245.01	2.00	0.00	0.40	0.00	32.95	244.08	2.00	0.00	0.40	0.00
33.00	243.32	2.00	0.00	0.40	0.00	33.05	242.17	2.00	0.00	0.40	0.00
33.10	239.90	2.00	0.00	0.40	0.00	33.15	237.32	2.00	0.00	0.40	0.00
33.20	234.57	2.00	0.00	0.40	0.00	33.25	230.25	2.00	0.00	0.40	0.00
33.30	226.97	2.00	0.00	0.39	0.00	33.35	220.35	2.00	0.00	0.39	0.00
33.40	216.96	2.00	0.00	0.39	0.00	33.45	212.23	2.00	0.00	0.39	0.00
33.50	209.60	2.00	0.00	0.39	0.00	33.55	206.08	2.00	0.00	0.39	0.00
33.60	204.04	2.00	0.00	0.39	0.00	33.65	202.42	2.00	0.00	0.39	0.00
33.70	202.60	2.00	0.00	0.39	0.00	33.75	201.50	2.00	0.00	0.39	0.00
33.80	199.83	2.00	0.00	0.39	0.00	33.85	198.54	1.95	0.01	0.38	0.00
33.90	197.00	1.79	0.03	0.38	0.00	33.95	194.86	1.60	0.07	0.38	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
34.00	192.66	1.44	0.11	0.38	0.00	34.05	189.44	1.23	0.17	0.38	0.00
34.10	188.43	1.17	0.19	0.38	0.00	34.15	187.63	1.13	0.21	0.38	0.00
34.20	186.83	1.09	0.23	0.38	0.00	34.25	186.33	1.07	0.24	0.38	0.00
34.30	185.77	1.04	0.25	0.38	0.00	34.35	186.43	1.07	0.23	0.38	0.00
34.40	187.65	1.13	0.21	0.37	0.00	34.45	189.11	1.21	0.18	0.37	0.00
34.50	190.63	1.30	0.15	0.37	0.00	34.55	192.74	1.44	0.11	0.37	0.00
34.60	194.60	1.58	0.07	0.37	0.00	34.65	197.15	1.80	0.03	0.37	0.00
34.70	199.12	2.00	0.00	0.37	0.00	34.75	201.19	2.00	0.00	0.37	0.00
34.80	203.50	2.00	0.00	0.37	0.00	34.85	205.12	2.00	0.00	0.37	0.00
34.90	207.33	2.00	0.00	0.37	0.00	34.95	208.01	2.00	0.00	0.36	0.00
35.00	208.57	2.00	0.00	0.36	0.00	35.05	208.10	2.00	0.00	0.36	0.00
35.10	207.65	2.00	0.00	0.36	0.00	35.15	207.24	2.00	0.00	0.36	0.00
35.20	207.16	2.00	0.00	0.36	0.00	35.25	207.10	2.00	0.00	0.36	0.00
35.30	207.30	2.00	0.00	0.36	0.00	35.35	207.37	2.00	0.00	0.36	0.00
35.40	207.97	2.00	0.00	0.36	0.00	35.45	208.50	2.00	0.00	0.36	0.00
35.50	209.50	2.00	0.00	0.35	0.00	35.55	210.20	2.00	0.00	0.35	0.00
35.60	211.02	2.00	0.00	0.35	0.00	35.65	211.95	2.00	0.00	0.35	0.00
35.70	212.90	2.00	0.00	0.35	0.00	35.75	214.56	2.00	0.00	0.35	0.00
35.80	215.78	2.00	0.00	0.35	0.00	35.85	217.38	2.00	0.00	0.35	0.00
35.90	218.17	2.00	0.00	0.35	0.00	35.95	219.29	2.00	0.00	0.35	0.00
36.00	219.28	2.00	0.00	0.35	0.00	36.05	219.48	2.00	0.00	0.34	0.00
36.10	217.76	2.00	0.00	0.34	0.00	36.15	216.22	2.00	0.00	0.34	0.00
36.20	212.87	2.00	0.00	0.34	0.00	36.25	210.32	2.00	0.00	0.34	0.00
36.30	206.88	2.00	0.00	0.34	0.00	36.35	204.12	2.00	0.00	0.34	0.00
36.40	200.97	2.00	0.00	0.34	0.00	36.45	193.14	1.45	0.09	0.34	0.00
36.50	186.42	1.06	0.21	0.34	0.00	36.55	175.96	0.69	0.33	0.34	0.00
36.60	173.32	0.62	0.36	0.33	0.00	36.65	170.97	0.57	0.39	0.33	0.00
36.70	175.11	0.67	0.34	0.33	0.00	36.75	177.55	0.73	0.31	0.33	0.00
36.80	180.04	2.00	0.00	0.33	0.00	36.85	177.50	2.00	0.00	0.33	0.00
36.90	171.68	2.00	0.00	0.33	0.00	36.95	161.72	2.00	0.00	0.33	0.00
37.00	151.43	2.00	0.00	0.33	0.00	37.05	138.88	2.00	0.00	0.33	0.00
37.10	128.80	2.00	0.00	0.33	0.00	37.15	115.29	2.00	0.00	0.32	0.00
37.20	43.37	2.00	0.00	0.32	0.00	37.25	36.91	2.00	0.00	0.32	0.00
37.30	33.51	2.00	0.00	0.32	0.00	37.35	30.62	2.00	0.00	0.32	0.00
37.40	27.61	2.00	0.00	0.32	0.00	37.45	25.97	2.00	0.00	0.32	0.00
37.50	24.66	2.00	0.00	0.32	0.00	37.55	23.77	2.00	0.00	0.32	0.00
37.60	22.87	2.00	0.00	0.32	0.00	37.65	21.59	2.00	0.00	0.32	0.00
37.70	22.35	2.00	0.00	0.31	0.00	37.75	27.22	2.00	0.00	0.31	0.00
37.80	30.54	2.00	0.00	0.31	0.00	37.85	34.08	2.00	0.00	0.31	0.00
37.90	33.58	2.00	0.00	0.31	0.00	37.95	34.12	2.00	0.00	0.31	0.00
38.00	40.90	2.00	0.00	0.31	0.00	38.05	48.21	2.00	0.00	0.31	0.00
38.10	126.37	2.00	0.00	0.31	0.00	38.15	135.75	2.00	0.00	0.31	0.00
38.20	144.59	2.00	0.00	0.31	0.00	38.25	150.48	2.00	0.00	0.30	0.00
38.30	152.43	2.00	0.00	0.30	0.00	38.35	152.59	2.00	0.00	0.30	0.00
38.40	150.30	2.00	0.00	0.30	0.00	38.45	148.55	0.30	0.63	0.30	0.00
38.50	147.21	0.30	0.64	0.30	0.00	38.55	146.68	0.29	0.64	0.30	0.00
38.60	145.65	0.29	0.64	0.30	0.00	38.65	145.16	0.28	0.64	0.30	0.00
38.70	143.36	0.27	0.65	0.30	0.00	38.75	143.68	0.27	0.64	0.30	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
38.80	143.75	0.27	0.64	0.29	0.00	38.85	145.19	0.28	0.63	0.29	0.00
38.90	145.90	0.29	0.63	0.29	0.00	38.95	147.26	0.30	0.62	0.29	0.00
39.00	147.91	0.30	0.61	0.29	0.00	39.05	149.67	0.31	0.60	0.29	0.00
39.10	149.13	2.00	0.00	0.29	0.00	39.15	149.08	2.00	0.00	0.29	0.00
39.20	146.89	2.00	0.00	0.29	0.00	39.25	145.44	2.00	0.00	0.29	0.00
39.30	142.61	2.00	0.00	0.29	0.00	39.35	138.98	2.00	0.00	0.28	0.00
39.40	133.36	2.00	0.00	0.28	0.00	39.45	129.06	2.00	0.00	0.28	0.00
39.50	125.21	2.00	0.00	0.28	0.00	39.55	122.11	2.00	0.00	0.28	0.00
39.60	119.96	2.00	0.00	0.28	0.00	39.65	117.35	0.18	0.76	0.28	0.00
39.70	117.93	2.00	0.00	0.28	0.00	39.75	119.06	2.00	0.00	0.28	0.00
39.80	120.39	2.00	0.00	0.28	0.00	39.85	121.64	2.00	0.00	0.28	0.00
39.90	123.54	2.00	0.00	0.27	0.00	39.95	125.93	2.00	0.00	0.27	0.00
40.00	129.64	2.00	0.00	0.27	0.00	40.05	130.11	2.00	0.00	0.27	0.00
40.10	130.80	2.00	0.00	0.27	0.00	40.15	129.61	0.21	0.66	0.27	0.00
40.20	129.07	0.21	0.66	0.27	0.00	40.25	127.98	0.21	0.66	0.27	0.00
40.30	127.16	0.20	0.67	0.27	0.00	40.35	126.01	0.20	0.67	0.27	0.00
40.40	125.08	0.20	0.67	0.27	0.00	40.45	124.06	0.20	0.68	0.26	0.00
40.50	122.67	0.19	0.68	0.26	0.00	40.55	121.48	0.19	0.69	0.26	0.00
40.60	120.34	2.00	0.00	0.26	0.00	40.65	118.66	2.00	0.00	0.26	0.00
40.70	117.18	2.00	0.00	0.26	0.00	40.75	114.84	2.00	0.00	0.26	0.00
40.80	112.98	2.00	0.00	0.26	0.00	40.85	109.93	2.00	0.00	0.26	0.00
40.90	44.65	2.00	0.00	0.26	0.00	40.95	43.39	2.00	0.00	0.26	0.00
41.00	109.51	2.00	0.00	0.25	0.00	41.05	112.08	2.00	0.00	0.25	0.00
41.10	118.29	2.00	0.00	0.25	0.00	41.15	122.66	2.00	0.00	0.25	0.00
41.20	128.45	2.00	0.00	0.25	0.00	41.25	132.66	2.00	0.00	0.25	0.00
41.30	137.04	2.00	0.00	0.25	0.00	41.35	141.77	2.00	0.00	0.25	0.00
41.40	144.36	2.00	0.00	0.25	0.00	41.45	147.11	2.00	0.00	0.25	0.00
41.50	147.24	2.00	0.00	0.25	0.00	41.55	148.64	2.00	0.00	0.24	0.00
41.60	146.28	0.29	0.52	0.24	0.00	41.65	145.60	2.00	0.00	0.24	0.00
41.70	141.07	2.00	0.00	0.24	0.00	41.75	138.47	2.00	0.00	0.24	0.00
41.80	132.80	2.00	0.00	0.24	0.00	41.85	128.87	2.00	0.00	0.24	0.00
41.90	122.91	2.00	0.00	0.24	0.00	41.95	119.46	2.00	0.00	0.24	0.00
42.00	115.90	2.00	0.00	0.24	0.00	42.05	110.67	2.00	0.00	0.24	0.00
42.10	107.46	2.00	0.00	0.23	0.00	42.15	40.69	2.00	0.00	0.23	0.00
42.20	40.75	2.00	0.00	0.23	0.00	42.25	41.31	2.00	0.00	0.23	0.00
42.30	42.21	2.00	0.00	0.23	0.00	42.35	42.79	2.00	0.00	0.23	0.00
42.40	43.09	2.00	0.00	0.23	0.00	42.45	42.97	2.00	0.00	0.23	0.00
42.50	42.64	2.00	0.00	0.23	0.00	42.55	41.53	2.00	0.00	0.23	0.00
42.60	40.30	2.00	0.00	0.23	0.00	42.65	38.07	2.00	0.00	0.22	0.00
42.70	36.40	2.00	0.00	0.22	0.00	42.75	34.48	2.00	0.00	0.22	0.00
42.80	34.58	2.00	0.00	0.22	0.00	42.85	35.21	2.00	0.00	0.22	0.00
42.90	39.06	2.00	0.00	0.22	0.00	42.95	42.80	2.00	0.00	0.22	0.00
43.00	48.58	2.00	0.00	0.22	0.00	43.05	119.39	2.00	0.00	0.22	0.00
43.10	125.51	2.00	0.00	0.22	0.00	43.15	128.37	2.00	0.00	0.22	0.00
43.20	130.68	2.00	0.00	0.21	0.00	43.25	129.78	2.00	0.00	0.21	0.00
43.30	129.05	0.21	0.52	0.21	0.00	43.35	127.97	2.00	0.00	0.21	0.00
43.40	128.68	2.00	0.00	0.21	0.00	43.45	130.12	2.00	0.00	0.21	0.00
43.50	128.95	2.00	0.00	0.21	0.00	43.55	127.67	2.00	0.00	0.21	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
43.60	124.16	2.00	0.00	0.21	0.00	43.65	123.01	2.00	0.00	0.21	0.00
43.70	122.72	0.19	0.53	0.21	0.00	43.75	127.74	2.00	0.00	0.20	0.00
43.80	133.55	2.00	0.00	0.20	0.00	43.85	140.35	2.00	0.00	0.20	0.00
43.90	145.53	2.00	0.00	0.20	0.00	43.95	151.92	2.00	0.00	0.20	0.00
44.00	159.46	2.00	0.00	0.20	0.00	44.05	170.11	2.00	0.00	0.20	0.00
44.10	180.28	2.00	0.00	0.20	0.00	44.15	189.06	2.00	0.00	0.20	0.00
44.20	198.28	2.00	0.00	0.20	0.00	44.25	202.99	2.00	0.00	0.20	0.00
44.30	209.63	2.00	0.00	0.19	0.00	44.35	214.17	2.00	0.00	0.19	0.00
44.40	221.05	2.00	0.00	0.19	0.00	44.45	226.18	2.00	0.00	0.19	0.00
44.50	230.13	2.00	0.00	0.19	0.00	44.55	233.80	2.00	0.00	0.19	0.00
44.60	235.85	2.00	0.00	0.19	0.00	44.65	238.43	2.00	0.00	0.19	0.00
44.70	239.26	2.00	0.00	0.19	0.00	44.75	240.20	2.00	0.00	0.19	0.00
44.80	239.78	2.00	0.00	0.19	0.00	44.85	239.37	2.00	0.00	0.18	0.00
44.90	238.17	2.00	0.00	0.18	0.00	44.95	237.17	2.00	0.00	0.18	0.00
45.00	235.82	2.00	0.00	0.18	0.00	45.05	234.86	2.00	0.00	0.18	0.00
45.10	234.00	2.00	0.00	0.18	0.00	45.15	232.87	2.00	0.00	0.18	0.00
45.20	231.84	2.00	0.00	0.18	0.00	45.25	230.07	2.00	0.00	0.18	0.00
45.30	228.70	2.00	0.00	0.18	0.00	45.35	227.38	2.00	0.00	0.18	0.00
45.40	226.69	2.00	0.00	0.17	0.00	45.45	226.43	2.00	0.00	0.17	0.00
45.50	225.75	2.00	0.00	0.17	0.00	45.55	225.87	2.00	0.00	0.17	0.00
45.60	226.06	2.00	0.00	0.17	0.00	45.65	226.28	2.00	0.00	0.17	0.00
45.70	226.60	2.00	0.00	0.17	0.00	45.75	226.89	2.00	0.00	0.17	0.00
45.80	227.11	2.00	0.00	0.17	0.00	45.85	227.23	2.00	0.00	0.17	0.00
45.90	225.80	2.00	0.00	0.17	0.00	45.95	223.26	2.00	0.00	0.16	0.00
46.00	219.43	2.00	0.00	0.16	0.00	46.05	214.25	2.00	0.00	0.16	0.00
46.10	207.77	2.00	0.00	0.16	0.00	46.15	200.30	2.00	0.00	0.16	0.00
46.20	192.99	1.39	0.05	0.16	0.00	46.25	187.46	1.08	0.10	0.16	0.00
46.30	183.81	0.92	0.12	0.16	0.00	46.35	182.91	0.88	0.12	0.16	0.00
46.40	182.29	0.86	0.12	0.16	0.00	46.45	183.32	0.90	0.12	0.16	0.00
46.50	184.04	0.93	0.11	0.15	0.00	46.55	186.24	1.02	0.10	0.15	0.00
46.60	188.48	1.13	0.08	0.15	0.00	46.65	190.67	1.25	0.07	0.15	0.00
46.70	191.82	1.32	0.06	0.15	0.00	46.75	191.74	1.31	0.06	0.15	0.00
46.80	191.66	1.31	0.06	0.15	0.00	46.85	191.59	1.30	0.06	0.15	0.00
46.90	191.51	1.30	0.06	0.15	0.00	46.95	191.08	1.27	0.06	0.15	0.00
47.00	188.78	1.14	0.08	0.15	0.00	47.05	185.16	0.97	0.10	0.14	0.00
47.10	179.67	0.77	0.12	0.14	0.00	47.15	171.67	0.58	0.16	0.14	0.00
47.20	163.50	2.00	0.00	0.14	0.00	47.25	155.71	2.00	0.00	0.14	0.00
47.30	147.54	2.00	0.00	0.14	0.00	47.35	148.57	2.00	0.00	0.14	0.00
47.40	155.84	2.00	0.00	0.14	0.00	47.45	164.54	2.00	0.00	0.14	0.00
47.50	164.87	2.00	0.00	0.14	0.00	47.55	160.86	2.00	0.00	0.14	0.00
47.60	156.08	2.00	0.00	0.13	0.00	47.65	149.01	2.00	0.00	0.13	0.00
47.70	147.08	2.00	0.00	0.13	0.00	47.75	146.62	2.00	0.00	0.13	0.00
47.80	146.50	2.00	0.00	0.13	0.00	47.85	146.08	2.00	0.00	0.13	0.00
47.90	145.75	2.00	0.00	0.13	0.00	47.95	146.99	0.29	0.27	0.13	0.00
48.00	151.96	0.33	0.26	0.13	0.00	48.05	155.21	0.35	0.25	0.13	0.00
48.10	158.95	0.39	0.22	0.13	0.00	48.15	157.58	0.38	0.23	0.12	0.00
48.20	155.87	0.36	0.25	0.12	0.00	48.25	150.18	0.31	0.25	0.12	0.00
48.30	145.24	0.28	0.26	0.12	0.00	48.35	138.06	0.25	0.28	0.12	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
48.40	62.83	2.00	0.00	0.12	0.00	48.45	57.86	2.00	0.00	0.12	0.00
48.50	56.02	2.00	0.00	0.12	0.00	48.55	55.15	2.00	0.00	0.12	0.00
48.60	55.89	2.00	0.00	0.12	0.00	48.65	58.15	2.00	0.00	0.12	0.00
48.70	61.90	2.00	0.00	0.11	0.00	48.75	68.31	2.00	0.00	0.11	0.00
48.80	146.37	2.00	0.00	0.11	0.00	48.85	154.94	2.00	0.00	0.11	0.00
48.90	159.31	2.00	0.00	0.11	0.00	48.95	162.30	2.00	0.00	0.11	0.00
49.00	160.92	2.00	0.00	0.11	0.00	49.05	159.14	0.39	0.19	0.11	0.00
49.10	155.65	2.00	0.00	0.11	0.00	49.15	153.07	2.00	0.00	0.11	0.00
49.20	149.18	2.00	0.00	0.11	0.00	49.25	147.70	2.00	0.00	0.10	0.00
49.30	146.45	2.00	0.00	0.10	0.00	49.35	147.07	2.00	0.00	0.10	0.00
49.40	147.57	0.30	0.22	0.10	0.00	49.45	149.28	2.00	0.00	0.10	0.00
49.50	150.38	2.00	0.00	0.10	0.00	49.55	152.07	2.00	0.00	0.10	0.00
49.60	151.70	2.00	0.00	0.10	0.00	49.65	150.87	2.00	0.00	0.10	0.00
49.70	152.41	2.00	0.00	0.10	0.00	49.75	154.17	0.35	0.19	0.10	0.00
49.80	157.18	0.37	0.18	0.09	0.00	49.85	156.26	0.36	0.18	0.09	0.00
49.90	151.59	0.32	0.19	0.09	0.00						

Total estimated settlement: 0.93**Abbreviations**

$Q_{tn,cs}$:	Equivalent clean sand normalized cone resistance
FS:	Factor of safety against liquefaction
e_v (%):	Post-liquefaction volumetric strain
DF:	e_v depth weighting factor
Settlement:	Calculated settlement

:: Strength loss calculation Idriss & Boulanger (2008) ::

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.05	44.98	72.27	1.00	72.27	1.78	0.09	0.70
0.10	42.18	67.76	1.00	67.76	1.81	0.08	0.68
0.15	38.22	61.39	1.00	61.39	1.88	0.08	0.70
0.20	36.54	58.70	1.27	74.67	1.95	0.08	0.72
0.25	37.48	60.20	1.31	78.78	2.00	0.09	0.74
0.30	41.67	66.92	1.32	88.36	2.02	0.10	0.76
0.35	47.15	75.73	1.32	100.32	2.02	0.12	0.78
0.40	53.76	86.34	1.32	114.07	2.02	0.14	0.80
0.45	60.29	96.83	1.32	127.85	2.02	0.16	0.82
0.50	67.27	108.03	1.31	142.01	2.01	0.18	0.83
0.55	73.74	118.43	1.31	155.26	2.00	0.22	0.85
0.60	80.33	129.00	1.30	168.33	2.00	0.26	0.86
0.65	85.91	137.96	1.30	179.52	1.99	0.32	0.87
0.70	90.35	145.10	1.30	188.52	1.99	0.37	0.88
0.75	93.16	149.61	1.30	194.47	1.99	0.41	0.89
0.80	94.80	152.23	1.30	198.25	1.99	0.44	0.89
0.85	95.69	153.66	1.30	200.47	2.00	0.46	0.89
0.90	96.15	154.39	1.31	201.72	2.00	0.47	0.89
0.95	96.40	154.80	1.31	202.02	2.00	0.47	0.89
1.00	96.43	154.84	1.30	201.51	1.99	0.47	0.89
1.05	96.33	154.66	1.29	200.22	1.98	0.46	0.89
1.10	96.00	154.13	1.29	198.56	1.98	0.44	0.89
1.15	95.46	153.26	1.28	196.57	1.97	0.42	0.89
1.20	94.69	152.02	1.28	194.83	1.97	0.41	0.88
1.25	93.46	150.04	1.28	192.76	1.97	0.40	0.88
1.30	91.81	147.38	1.29	190.63	1.98	0.38	0.88
1.35	89.30	143.34	1.31	187.31	2.00	0.36	0.88
1.40	86.36	138.61	1.33	183.81	2.02	0.33	0.88
1.45	82.64	132.63	1.36	179.81	2.05	0.31	0.88
1.50	78.19	125.48	1.40	175.83	2.09	0.29	0.87
1.55	72.82	116.85	1.47	172.30	2.13	0.26	0.87
1.60	66.36	106.47	1.59	168.91	2.19	0.23	0.86
1.65	59.88	96.04	1.75	168.09	2.25	0.20	0.84
1.70	53.34	85.53	1.97	168.23	2.31	0.18	0.83
1.75	48.05	77.02	2.23	171.49	2.37	0.16	0.82
1.80	43.36	69.49	2.50	173.94	2.42	0.15	0.81
1.85	40.03	64.14	2.75	176.62	2.47	0.14	0.80
1.90	37.71	60.39	2.91	175.70	2.49	0.14	0.79
1.95	37.98	60.83	2.86	174.16	2.48	0.13	0.79
2.00	40.86	65.45	2.58	169.03	2.44	0.14	0.80
2.05	47.34	75.85	2.17	164.65	2.36	0.16	0.81
2.10	55.46	88.90	1.79	159.30	2.26	0.18	0.83
2.15	64.79	103.88	1.53	158.98	2.16	0.21	0.85
2.20	73.80	118.36	1.37	162.65	2.07	0.24	0.86
2.25	81.99	131.51	1.29	169.92	1.98	0.28	0.86
2.30	88.53	142.01	1.24	176.62	1.91	0.30	0.86
2.35	92.37	148.18	1.21	179.31	1.86	0.32	0.85
2.40	93.93	150.68	1.19	179.81	1.84	0.32	0.84

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
2.45	93.87	150.58	1.19	179.54	1.84	0.32	0.84
2.50	93.40	149.82	1.20	180.14	1.85	0.32	0.84
2.55	93.28	149.62	1.21	181.47	1.87	0.32	0.85
2.60	93.55	150.05	1.22	183.19	1.88	0.33	0.85
2.65	94.32	151.28	1.22	185.06	1.88	0.34	0.86
2.70	95.21	152.70	1.22	186.47	1.88	0.35	0.86
2.75	96.20	154.29	1.22	187.55	1.87	0.36	0.86
2.80	97.04	155.63	1.21	188.16	1.86	0.37	0.85
2.85	97.77	156.80	1.20	188.52	1.85	0.37	0.85
2.90	98.32	157.68	1.20	188.59	1.84	0.37	0.85
2.95	98.61	158.15	1.19	188.33	1.84	0.38	0.85
3.00	98.60	158.12	1.19	187.86	1.84	0.37	0.85
3.05	98.15	157.39	1.19	186.98	1.84	0.37	0.85
3.10	97.34	156.09	1.19	185.74	1.84	0.36	0.85
3.15	95.79	153.59	1.19	183.41	1.84	0.34	0.85
3.20	93.66	150.16	1.20	180.17	1.85	0.32	0.84
3.25	90.49	145.06	1.21	175.26	1.86	0.29	0.84
3.30	87.03	139.50	1.22	169.81	1.87	0.26	0.84
3.35	83.13	133.24	1.23	163.52	1.89	0.24	0.83
3.40	79.38	127.21	1.24	157.37	1.90	0.22	0.83
3.45	75.65	121.20	1.25	151.16	1.92	0.20	0.83
3.50	72.09	115.48	1.26	145.18	1.93	0.19	0.82
3.55	68.88	110.32	1.27	139.76	1.95	0.18	0.82
3.60	65.66	105.14	1.28	134.31	1.96	0.17	0.82
3.65	62.53	100.10	1.29	129.02	1.98	0.16	0.81
3.70	59.19	94.74	1.30	123.55	2.00	0.15	0.81
3.75	56.15	89.85	1.32	118.80	2.02	0.14	0.81
3.80	53.48	85.55	1.35	115.11	2.04	0.14	0.80
3.85	51.15	81.81	1.37	112.24	2.06	0.14	0.80
3.90	49.13	78.55	1.40	110.01	2.09	0.13	0.80
3.95	47.18	75.42	1.43	107.67	2.11	0.13	0.80
4.00	45.55	72.79	1.45	105.57	2.12	0.13	0.79
4.05	44.07	70.41	1.47	103.50	2.13	0.13	0.79
4.10	42.95	68.61	1.49	101.91	2.14	0.12	0.79
4.15	42.18	67.37	1.49	100.69	2.15	0.12	0.79
4.20	41.81	66.77	1.50	99.85	2.15	0.12	0.78
4.25	41.70	66.59	1.49	99.01	2.14	0.12	0.78
4.30	41.70	66.58	1.47	98.16	2.13	0.12	0.78
4.35	41.70	66.58	1.46	97.18	2.13	0.12	0.78
4.40	41.70	66.57	1.45	96.68	2.12	0.12	0.78
4.45	41.70	66.57	1.45	96.66	2.12	0.12	0.78
4.50	41.64	66.47	1.47	97.46	2.13	0.12	0.78
4.55	41.46	66.16	1.49	98.49	2.14	0.12	0.78
4.60	40.97	65.37	1.52	99.55	2.16	0.12	0.78
4.65	40.19	64.12	1.56	100.22	2.18	0.12	0.78
4.70	39.05	62.28	1.61	100.57	2.20	0.12	0.78
4.75	37.79	60.26	1.68	101.16	2.22	0.12	0.78
4.80	36.36	57.96	1.76	101.80	2.25	0.12	0.78

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
4.85	35.02	55.79	1.84	102.75	2.28	0.12	0.77
4.90	33.60	53.51	1.93	103.16	2.30	0.12	0.77
4.95	32.24	51.31	2.01	103.36	2.32	0.11	0.77
5.00	30.86	49.10	2.11	103.71	2.35	0.11	0.76
5.05	29.46	46.84	2.23	104.56	2.37	0.11	0.76
5.10	28.11	44.67	2.39	106.54	2.40	0.11	0.76
5.15	26.68	42.37	2.57	108.83	2.44	0.11	0.75
5.20	25.33	40.19	2.79	111.95	2.47	0.11	0.75
5.25	23.93	37.95	3.03	114.88	2.51	0.10	0.75
5.30	22.69	35.94	3.29	118.08	2.54	0.10	0.74
5.35	21.59	34.17	3.53	120.73	2.57	0.10	0.74
5.40	20.68	32.71	3.76	122.93	2.60	0.10	0.62
5.45	19.94	31.51	3.94	124.14	2.62	0.10	0.62
5.50	19.22	30.36	4.09	124.08	2.64	0.10	0.62
5.55	18.65	29.43	4.17	122.80	2.65	0.10	0.62
5.60	18.16	28.63	4.22	120.72	2.65	0.10	0.62
5.65	17.66	27.83	4.25	118.31	2.65	0.10	0.62
5.70	17.03	26.82	4.34	116.50	2.66	0.09	0.62
5.75	16.14	25.38	4.53	115.07	2.68	0.09	0.62
5.80	15.27	23.97	4.79	114.86	2.71	0.09	0.62
5.85	14.41	22.59	5.09	115.07	2.74	0.09	0.62
5.90	13.82	21.64	5.37	116.24	2.76	0.09	0.62
5.95	13.39	20.94	5.61	117.53	2.78	0.09	0.62
6.00	13.19	20.62	5.78	119.14	2.79	0.09	0.62
6.05	13.11	20.48	5.88	120.42	2.80	0.09	0.62
6.10	13.11	20.48	5.93	121.49	2.81	0.09	0.62
6.15	13.11	20.48	5.97	122.32	2.81	0.09	0.62
6.20	13.11	20.47	6.03	123.35	2.81	0.09	0.62
6.25	13.11	20.47	6.10	124.76	2.82	0.09	0.62
6.30	13.03	20.34	6.22	126.53	2.83	0.09	0.62
6.35	12.70	19.80	6.45	127.73	2.85	0.09	0.62
6.40	12.15	18.92	6.79	128.39	2.87	0.09	0.62
6.45	11.44	17.77	7.19	127.85	2.90	0.09	0.62
6.50	10.99	17.03	7.49	127.50	2.92	0.09	0.62
6.55	10.74	16.63	7.63	126.85	2.93	0.09	0.62
6.60	10.73	16.61	7.62	126.49	2.93	0.09	0.62
6.65	10.73	16.60	7.57	125.68	2.92	0.09	0.62
6.70	10.73	16.60	7.52	124.89	2.92	0.09	0.62
6.75	10.73	16.59	7.49	124.30	2.92	0.09	0.62
6.80	10.73	16.59	7.47	123.96	2.92	0.09	0.62
6.85	10.73	16.59	7.46	123.73	2.92	0.09	0.62
6.90	10.73	16.58	7.43	123.25	2.92	0.09	0.62
6.95	10.73	16.58	7.39	122.48	2.91	0.09	0.62
7.00	10.73	16.57	7.32	121.37	2.91	0.09	0.62
7.05	10.73	16.57	7.26	120.24	2.90	0.09	0.62
7.10	10.73	16.56	7.18	118.94	2.90	0.09	0.62
7.15	10.73	16.56	7.10	117.64	2.89	0.09	0.62
7.20	10.73	16.55	7.02	116.22	2.89	0.08	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
7.25	10.73	16.55	6.98	115.47	2.88	0.08	0.62
7.30	10.73	16.54	6.98	115.48	2.88	0.08	0.62
7.35	10.73	16.54	7.08	117.10	2.89	0.08	0.62
7.40	10.73	16.54	7.23	119.55	2.90	0.08	0.62
7.45	10.73	16.53	7.44	122.97	2.92	0.08	0.62
7.50	10.78	16.61	7.61	126.44	2.93	0.09	0.62
7.55	11.09	17.10	7.66	130.95	2.93	0.09	0.62
7.60	11.66	18.02	7.53	135.71	2.92	0.09	0.62
7.65	12.56	19.46	7.24	140.90	2.90	0.09	0.62
7.70	13.44	20.86	6.93	144.59	2.88	0.09	0.62
7.75	14.27	22.20	6.63	147.22	2.86	0.09	0.62
7.80	14.98	23.33	6.38	148.74	2.84	0.09	0.62
7.85	15.66	24.42	6.13	149.67	2.82	0.09	0.62
7.90	16.37	25.56	5.87	149.97	2.80	0.09	0.62
7.95	17.12	26.75	5.55	148.47	2.78	0.09	0.62
8.00	18.02	28.20	5.16	145.62	2.74	0.09	0.62
8.05	19.23	30.14	4.65	140.08	2.69	0.09	0.62
8.10	20.74	32.55	4.08	132.72	2.64	0.10	0.62
8.15	22.77	35.82	3.43	122.68	2.56	0.10	0.73
8.20	25.06	39.49	2.86	112.95	2.48	0.10	0.74
8.25	27.92	44.09	2.38	104.87	2.40	0.10	0.74
8.30	30.77	48.66	2.05	99.99	2.33	0.10	0.75
8.35	33.70	53.36	1.83	97.70	2.27	0.10	0.75
8.40	35.97	57.00	1.69	96.55	2.23	0.10	0.76
8.45	37.71	59.80	1.62	96.60	2.20	0.10	0.76
8.50	38.81	61.56	1.58	96.98	2.18	0.10	0.76
8.55	39.63	62.87	1.56	98.19	2.18	0.11	0.76
8.60	40.35	64.01	1.55	99.53	2.17	0.11	0.76
8.65	40.92	64.94	1.55	100.68	2.17	0.11	0.77
8.70	41.39	65.68	1.54	101.30	2.17	0.11	0.77
8.75	41.61	66.02	1.53	101.20	2.16	0.11	0.77
8.80	41.66	66.10	1.52	100.56	2.16	0.11	0.77
8.85	41.48	65.82	1.51	99.46	2.15	0.11	0.76
8.90	40.97	64.97	1.51	98.01	2.15	0.11	0.76
8.95	40.02	63.43	1.52	96.36	2.16	0.10	0.76
9.00	38.38	60.81	1.55	94.52	2.17	0.10	0.76
9.05	36.34	57.53	1.62	92.96	2.20	0.10	0.75
9.10	33.87	53.57	1.71	91.80	2.24	0.10	0.75
9.15	31.57	49.86	1.84	91.85	2.28	0.10	0.75
9.20	29.25	46.13	2.01	92.65	2.32	0.10	0.74
9.25	27.17	42.79	2.21	94.54	2.37	0.10	0.74
9.30	25.10	39.46	2.45	96.57	2.41	0.09	0.73
9.35	23.30	36.55	2.72	99.28	2.46	0.09	0.73
9.40	21.84	34.21	2.98	101.91	2.50	0.09	0.72
9.45	20.92	32.72	3.20	104.86	2.53	0.09	0.72
9.50	20.38	31.85	3.39	107.84	2.56	0.09	0.72
9.55	20.02	31.28	3.55	111.18	2.58	0.09	0.72
9.60	19.68	30.73	3.76	115.62	2.60	0.09	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.65	19.36	30.20	3.99	120.35	2.63	0.09	0.62
9.70	19.16	29.87	4.21	125.71	2.65	0.09	0.62
9.75	19.37	30.21	4.23	127.70	2.65	0.09	0.62
9.80	20.44	31.92	3.98	127.02	2.63	0.09	0.62
9.85	22.15	34.67	3.52	121.98	2.57	0.10	0.73
9.90	24.24	38.02	3.07	116.86	2.51	0.10	0.73
9.95	25.93	40.73	2.75	111.83	2.46	0.10	0.74
10.00	27.41	43.10	2.49	107.42	2.42	0.10	0.74
10.05	29.11	45.83	2.23	102.08	2.37	0.10	0.74
10.10	31.11	49.03	1.96	96.26	2.31	0.10	0.75
10.15	33.42	51.86	1.75	90.90	2.25	0.10	0.75
10.20	35.29	53.98	1.61	86.92	2.20	0.10	0.75
10.25	36.90	55.79	1.52	84.75	2.16	0.10	0.75
10.30	37.89	56.84	1.47	83.64	2.13	0.10	0.75
10.35	38.39	57.38	1.46	83.55	2.12	0.10	0.75
10.40	38.23	57.11	1.46	83.61	2.13	0.10	0.75
10.45	37.66	56.34	1.49	83.83	2.14	0.10	0.75
10.50	36.75	55.11	1.52	83.77	2.16	0.10	0.75
10.55	35.87	53.89	1.55	83.71	2.17	0.10	0.75
10.60	35.11	52.84	1.58	83.72	2.19	0.09	0.75
10.65	34.72	52.29	1.61	84.26	2.20	0.10	0.74
10.70	34.49	51.98	1.63	84.96	2.21	0.10	0.75
10.75	34.31	51.72	1.66	85.63	2.22	0.10	0.75
10.80	34.02	51.26	1.67	85.77	2.22	0.10	0.74
10.85	33.69	50.73	1.69	85.61	2.23	0.10	0.74
10.90	33.60	50.53	1.69	85.47	2.23	0.10	0.74
10.95	33.73	50.64	1.69	85.55	2.23	0.10	0.74
11.00	34.09	51.06	1.68	85.85	2.23	0.10	0.74
11.05	34.36	51.35	1.68	86.06	2.22	0.10	0.75
11.10	34.52	51.50	1.67	86.16	2.22	0.10	0.75
11.15	34.55	51.46	1.67	86.14	2.22	0.10	0.75
11.20	34.52	51.33	1.68	86.05	2.22	0.10	0.75
11.25	34.22	50.84	1.69	85.70	2.23	0.10	0.75
11.30	33.73	50.09	1.70	85.37	2.23	0.10	0.74
11.35	33.01	49.04	1.74	85.11	2.24	0.10	0.74
11.40	32.51	48.33	1.77	85.50	2.26	0.09	0.74
11.45	32.21	47.90	1.80	86.29	2.27	0.09	0.74
11.50	31.92	47.51	1.84	87.43	2.28	0.10	0.74
11.55	31.43	46.87	1.90	88.85	2.29	0.10	0.74
11.60	30.56	45.73	1.99	90.89	2.32	0.10	0.74
11.65	29.63	44.55	2.12	94.48	2.35	0.10	0.74
11.70	28.56	43.22	2.30	99.47	2.39	0.10	0.74
11.75	27.44	41.85	2.54	106.33	2.43	0.10	0.74
11.80	26.20	40.26	2.81	113.31	2.48	0.10	0.73
11.85	24.96	38.63	3.12	120.51	2.52	0.10	0.73
11.90	23.94	37.22	3.38	125.69	2.55	0.10	0.73
11.95	23.21	36.17	3.58	129.54	2.58	0.09	0.73
12.00	22.90	35.68	3.64	130.01	2.59	0.09	0.73

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
12.05	22.95	35.65	3.60	128.37	2.58	0.09	0.73
12.10	23.46	36.22	3.42	123.86	2.56	0.09	0.73
12.15	24.27	37.18	3.20	118.89	2.53	0.09	0.73
12.20	25.48	38.66	2.93	113.16	2.49	0.10	0.73
12.25	26.69	40.14	2.69	108.07	2.46	0.10	0.73
12.30	27.94	41.63	2.48	103.19	2.42	0.10	0.74
12.35	28.81	42.65	2.35	100.12	2.39	0.10	0.74
12.40	29.42	43.37	2.28	98.79	2.38	0.10	0.74
12.45	29.41	43.34	2.32	100.39	2.39	0.10	0.74
12.50	28.97	42.81	2.43	103.89	2.41	0.10	0.74
12.55	27.93	41.50	2.64	109.45	2.45	0.10	0.74
12.60	26.58	39.74	2.91	115.83	2.49	0.10	0.73
12.65	24.77	37.32	3.28	122.57	2.54	0.10	0.73
12.70	22.69	34.47	3.77	129.90	2.60	0.09	0.62
12.75	20.46	31.35	4.36	136.81	2.67	0.09	0.62
12.80	18.46	28.46	5.06	144.07	2.73	0.09	0.62
12.85	16.98	26.09	5.74	149.69	2.79	0.09	0.62
12.90	16.08	24.64	6.32	155.71	2.84	0.09	0.62
12.95	15.67	23.97	6.68	160.17	2.86	0.09	0.62
13.00	15.52	23.73	6.88	163.30	2.88	0.09	0.62
13.05	15.62	23.89	6.83	163.09	2.87	0.09	0.62
13.10	15.82	24.20	6.64	160.68	2.86	0.09	0.62
13.15	16.02	24.51	6.34	155.28	2.84	0.09	0.62
13.20	15.84	24.22	6.14	148.59	2.82	0.09	0.62
13.25	15.09	23.01	6.09	140.22	2.82	0.09	0.62
13.30	13.89	21.08	6.30	132.80	2.83	0.09	0.62
13.35	12.54	18.91	6.70	126.72	2.86	0.08	0.62
13.40	11.57	17.34	7.20	124.86	2.90	0.08	0.62
13.45	11.06	16.52	7.58	125.22	2.93	0.08	0.62
13.50	11.21	16.76	7.62	127.69	2.93	0.08	0.62
13.55	11.71	17.55	7.37	129.26	2.91	0.08	0.62
13.60	12.41	18.68	6.99	130.50	2.88	0.08	0.62
13.65	12.87	19.37	6.81	131.87	2.87	0.08	0.62
13.70	13.11	19.71	6.80	134.02	2.87	0.08	0.62
13.75	13.11	19.72	6.96	137.23	2.88	0.08	0.62
13.80	13.11	19.72	7.11	140.17	2.89	0.08	0.62
13.85	13.11	19.72	7.26	143.10	2.90	0.08	0.62
13.90	13.11	19.70	7.36	145.07	2.91	0.08	0.62
13.95	13.13	19.70	7.43	146.44	2.92	0.09	0.62
14.00	13.39	20.06	7.37	147.91	2.91	0.08	0.62
14.05	13.85	20.72	7.25	150.26	2.90	0.09	0.62
14.10	14.57	21.76	7.09	154.15	2.89	0.09	0.62
14.15	15.10	22.53	7.00	157.76	2.89	0.09	0.62
14.20	15.43	22.99	6.99	160.70	2.89	0.09	0.62
14.25	15.50	23.06	7.03	162.09	2.89	0.09	0.62
14.30	15.50	23.02	7.08	163.04	2.89	0.09	0.62
14.35	15.50	22.99	7.14	164.23	2.90	0.09	0.62
14.40	15.50	22.96	7.21	165.56	2.90	0.09	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
14.45	15.50	22.93	7.28	166.84	2.90	0.09	0.62
14.50	15.58	23.00	7.26	167.12	2.90	0.09	0.62
14.55	15.79	23.24	7.17	166.70	2.90	0.09	0.62
14.60	16.23	23.80	6.93	164.97	2.88	0.09	0.62
14.65	16.77	24.48	6.63	162.33	2.86	0.09	0.62
14.70	17.32	25.15	6.28	157.86	2.83	0.09	0.62
14.75	17.67	25.52	5.99	152.87	2.81	0.09	0.62
14.80	17.84	25.63	5.75	147.29	2.79	0.09	0.62
14.85	17.68	25.30	5.65	143.03	2.78	0.09	0.62
14.90	17.26	24.62	5.67	139.63	2.79	0.09	0.62
14.95	16.59	23.63	5.84	138.05	2.80	0.09	0.62
15.00	15.91	22.64	6.07	137.39	2.82	0.09	0.62
15.05	15.20	21.61	6.37	137.54	2.84	0.09	0.62
15.10	14.52	20.63	6.67	137.68	2.86	0.09	0.62
15.15	13.81	19.61	7.02	137.69	2.89	0.09	0.62
15.20	13.36	18.95	7.29	138.23	2.91	0.08	0.62
15.25	13.12	18.58	7.49	139.24	2.92	0.08	0.62
15.30	13.11	18.56	7.58	140.66	2.93	0.08	0.62
15.35	13.11	18.53	7.64	141.51	2.93	0.08	0.62
15.40	13.11	18.50	7.66	141.77	2.93	0.08	0.62
15.45	13.11	18.46	7.66	141.40	2.93	0.08	0.62
15.50	13.11	18.41	7.64	140.68	2.93	0.08	0.62
15.55	13.11	18.37	7.62	139.96	2.93	0.08	0.62
15.60	13.11	18.33	7.62	139.74	2.93	0.08	0.62
15.65	13.11	18.31	7.69	140.72	2.93	0.08	0.62
15.70	13.32	18.59	7.71	143.21	2.93	0.08	0.62
15.75	13.90	19.39	7.61	147.57	2.93	0.09	0.62
15.80	15.24	21.24	7.17	152.19	2.90	0.09	0.62
15.85	17.13	23.81	6.54	155.79	2.85	0.09	0.62
15.90	19.55	27.02	5.77	155.78	2.79	0.09	0.62
15.95	21.87	30.02	5.09	152.88	2.74	0.09	0.62
16.00	24.20	32.96	4.45	146.81	2.68	0.10	0.62
16.05	26.03	35.20	4.02	141.35	2.63	0.10	0.62
16.10	27.52	37.01	3.70	137.09	2.59	0.10	0.73
16.15	28.01	37.59	3.66	137.69	2.59	0.10	0.74
16.20	27.82	37.34	3.78	141.06	2.60	0.10	0.62
16.25	26.64	35.85	4.11	147.26	2.64	0.10	0.62
16.30	25.25	34.06	4.47	152.33	2.68	0.10	0.62
16.35	23.65	31.96	4.88	156.06	2.72	0.10	0.62
16.40	22.45	30.35	5.18	157.09	2.74	0.09	0.62
16.45	21.50	29.04	5.39	156.58	2.76	0.09	0.62
16.50	21.06	28.38	5.44	154.24	2.77	0.09	0.62
16.55	20.86	28.02	5.39	151.09	2.76	0.09	0.62
16.60	20.86	27.91	5.26	146.75	2.75	0.09	0.62
16.65	20.78	27.72	5.19	143.79	2.74	0.09	0.62
16.70	20.59	27.41	5.21	142.92	2.75	0.09	0.62
16.75	20.27	26.99	5.42	146.19	2.76	0.09	0.62
16.80	19.89	26.51	5.71	151.48	2.79	0.09	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
16.85	19.24	25.68	6.14	157.61	2.82	0.09	0.62
16.90	18.56	24.80	6.57	162.84	2.85	0.09	0.62
16.95	18.03	24.11	6.96	167.87	2.88	0.09	0.62
17.00	18.61	24.88	6.95	173.02	2.88	0.09	0.62
17.05	20.27	27.06	6.59	178.20	2.86	0.09	0.62
17.10	23.40	31.10	5.80	180.48	2.80	0.10	0.62
17.15	27.05	35.71	5.01	178.86	2.73	0.10	0.62
17.20	31.32	40.98	4.20	171.95	2.65	0.11	0.62
17.25	35.16	45.58	3.56	162.28	2.58	0.11	0.75
17.30	38.86	49.87	3.00	149.68	2.50	0.11	0.76
17.35	41.28	52.49	2.62	137.35	2.44	0.12	0.77
17.40	42.80	53.94	2.32	125.31	2.39	0.11	0.77
17.45	42.83	53.64	2.17	116.29	2.36	0.11	0.76
17.50	42.19	52.59	2.09	109.76	2.34	0.11	0.76
17.55	40.76	50.70	2.09	106.20	2.34	0.11	0.76
17.60	39.02	48.50	2.16	104.64	2.36	0.10	0.75
17.65	36.86	45.85	2.29	104.82	2.38	0.10	0.75
17.70	34.06	42.49	2.52	106.95	2.43	0.10	0.75
17.75	30.98	38.77	2.86	110.79	2.48	0.10	0.74
17.80	27.97	35.16	3.35	117.84	2.55	0.10	0.73
17.85	25.78	32.55	3.88	126.46	2.62	0.09	0.62
17.90	24.17	30.65	4.48	137.23	2.68	0.09	0.62
17.95	22.86	29.08	5.06	147.07	2.73	0.09	0.62
18.00	21.57	27.53	5.69	156.72	2.79	0.09	0.62
18.05	20.83	26.64	6.22	165.66	2.83	0.09	0.62
18.10	20.97	26.85	6.51	174.92	2.85	0.09	0.62
18.15	22.68	29.05	6.36	184.70	2.84	0.10	0.62
18.20	24.91	31.86	6.01	191.41	2.81	0.10	0.62
18.25	27.32	34.83	5.55	193.29	2.78	0.10	0.62
18.30	29.37	37.27	5.09	189.63	2.74	0.10	0.62
18.35	31.86	40.20	4.55	182.82	2.68	0.11	0.62
18.40	36.70	45.94	3.80	174.69	2.61	0.11	0.62
18.45	43.08	53.43	3.10	165.57	2.52	0.12	0.77
18.50	51.28	62.89	2.46	154.80	2.42	0.13	0.78
18.55	57.67	70.01	2.06	144.47	2.33	0.14	0.80
18.60	62.48	75.14	1.80	135.05	2.26	0.14	0.80
18.65	62.59	74.93	1.73	129.45	2.24	0.14	0.80
18.70	59.78	71.54	1.77	126.61	2.26	0.13	0.79
18.75	53.35	64.19	2.03	130.06	2.33	0.13	0.79
18.80	46.95	56.85	2.42	137.72	2.41	0.12	0.77
18.85	40.55	49.43	3.02	149.16	2.51	0.11	0.76
18.90	36.09	44.20	3.60	159.31	2.58	0.11	0.75
18.95	32.65	40.13	4.22	169.29	2.65	0.11	0.62
19.00	30.55	37.62	4.71	177.24	2.70	0.10	0.62
19.05	28.71	35.39	5.16	182.64	2.74	0.10	0.62
19.10	26.41	32.54	5.62	182.82	2.78	0.10	0.62
19.15	23.50	28.91	6.20	179.10	2.83	0.10	0.62
19.20	20.07	24.60	6.99	171.95	2.89	0.09	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
19.25	17.73	21.63	7.68	166.15	2.93	0.09	0.62
19.30	16.42	19.89	8.15	162.06	2.96	0.09	0.62
19.35	16.54	20.00	8.02	160.46	2.95	0.09	0.62
19.40	16.98	20.52	7.72	158.45	2.93	0.09	0.62
19.45	17.69	21.36	7.26	155.02	2.90	0.09	0.62
19.50	18.17	21.87	6.89	150.66	2.88	0.09	0.62
19.55	18.43	22.10	6.57	145.22	2.86	0.09	0.62
19.60	18.19	21.72	6.41	139.34	2.84	0.09	0.62
19.65	17.78	21.15	6.31	133.47	2.84	0.09	0.62
19.70	17.37	20.58	6.27	129.04	2.83	0.09	0.62
19.75	17.72	20.97	6.12	128.38	2.82	0.09	0.62
19.80	19.06	22.57	5.92	133.58	2.81	0.09	0.62
19.85	21.14	25.08	5.63	141.26	2.78	0.09	0.62
19.90	23.24	27.61	5.39	148.67	2.76	0.09	0.62
19.95	24.36	28.89	5.13	148.24	2.74	0.10	0.62
20.00	24.31	28.72	4.95	142.12	2.72	0.10	0.62
20.05	23.17	27.22	4.81	131.03	2.71	0.09	0.62
20.10	21.56	25.20	4.86	122.35	2.71	0.09	0.62
20.15	19.80	23.03	5.08	117.02	2.73	0.09	0.62
20.20	18.02	20.89	5.51	115.00	2.77	0.09	0.62
20.25	16.38	18.91	6.06	114.58	2.82	0.09	0.62
20.30	15.27	17.58	6.59	115.76	2.86	0.08	0.62
20.35	14.87	17.10	6.93	118.55	2.88	0.08	0.62
20.40	15.07	17.34	7.11	123.20	2.89	0.08	0.62
20.45	15.35	17.68	7.23	127.88	2.90	0.09	0.62
20.50	15.50	17.86	7.42	132.49	2.91	0.09	0.62
20.55	15.65	18.02	7.56	136.23	2.92	0.09	0.62
20.60	16.12	18.57	7.55	140.14	2.92	0.09	0.62
20.65	17.35	20.02	7.19	144.01	2.90	0.09	0.62
20.70	19.25	22.25	6.63	147.59	2.86	0.09	0.62
20.75	21.77	25.16	5.94	149.44	2.81	0.09	0.62
20.80	24.22	27.97	5.34	149.40	2.76	0.10	0.62
20.85	26.40	30.43	4.84	147.35	2.71	0.10	0.62
20.90	27.89	32.08	4.50	144.36	2.68	0.10	0.62
20.95	28.59	32.79	4.30	140.89	2.66	0.10	0.62
21.00	28.38	32.48	4.28	139.05	2.66	0.10	0.62
21.05	27.39	31.30	4.45	139.41	2.68	0.10	0.62
21.10	25.93	29.61	4.83	142.95	2.71	0.10	0.62
21.15	24.23	27.65	5.33	147.25	2.76	0.09	0.62
21.20	22.73	25.91	5.87	152.02	2.80	0.09	0.62
21.25	21.78	24.80	6.25	154.91	2.83	0.09	0.62
21.30	21.24	24.13	6.46	155.82	2.85	0.09	0.62
21.35	20.65	23.40	6.53	152.82	2.85	0.09	0.62
21.40	19.33	21.80	6.75	147.16	2.87	0.09	0.62
21.45	17.60	19.73	7.11	140.19	2.89	0.09	0.62
21.50	15.86	17.63	7.65	134.78	2.93	0.09	0.62
21.55	14.54	16.01	8.19	131.08	2.96	0.08	0.62
21.60	13.46	14.69	8.70	127.86	3.00	0.08	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
21.65	12.45	13.44	9.21	123.82	3.02	0.08	0.96
21.70	11.41	12.17	9.73	118.43	3.05	0.08	0.87
21.75	10.56	11.14	10.20	113.60	3.08	0.08	0.80
21.80	9.94	10.37	10.56	109.55	3.10	0.08	0.74
21.85	9.64	10.00	10.79	107.95	3.11	0.08	0.71
21.90	9.63	9.98	10.85	108.24	3.11	0.08	0.71
21.95	9.92	10.30	10.76	110.77	3.11	0.08	0.74
22.00	10.36	10.80	10.57	114.18	3.10	0.08	0.77
22.05	10.84	11.35	10.42	118.27	3.09	0.08	0.81
22.10	11.28	11.86	10.32	122.33	3.08	0.08	0.85
22.15	11.78	12.43	10.20	126.83	3.08	0.08	0.89
22.20	12.54	13.31	9.91	131.86	3.06	0.08	0.95
22.25	13.51	14.43	9.49	136.89	3.04	0.08	1.03
22.30	14.66	15.76	8.96	141.27	3.01	0.08	1.13
22.35	16.29	17.65	8.25	145.67	2.97	0.09	0.62
22.40	18.38	20.07	7.44	149.26	2.92	0.09	0.62
22.45	21.10	23.12	6.54	151.28	2.85	0.09	0.62
22.50	23.53	25.78	5.81	149.91	2.80	0.09	0.62
22.55	25.65	28.08	5.17	145.19	2.74	0.10	0.62
22.60	26.99	29.47	4.70	138.46	2.70	0.10	0.62
22.65	27.93	30.40	4.31	130.92	2.66	0.10	0.62
22.70	28.11	30.52	4.10	125.14	2.64	0.10	0.62
22.75	27.77	30.06	4.03	121.00	2.63	0.10	0.62
22.80	26.72	28.86	4.17	120.20	2.65	0.09	0.62
22.85	25.36	27.33	4.43	121.19	2.67	0.09	0.62
22.90	23.55	25.32	4.89	123.79	2.72	0.09	0.62
22.95	21.57	23.11	5.43	125.59	2.77	0.09	0.62
23.00	19.55	20.85	6.08	126.77	2.82	0.09	0.62
23.05	17.74	18.82	6.74	126.79	2.87	0.09	0.62
23.10	16.26	17.15	7.39	126.68	2.91	0.09	0.62
23.15	15.01	15.69	8.05	126.27	2.96	0.08	0.62
23.20	14.12	14.64	8.64	126.45	2.99	0.08	0.62
23.25	13.48	13.88	9.17	127.37	3.02	0.08	0.99
23.30	13.22	13.57	9.55	129.58	3.04	0.08	0.97
23.35	13.14	13.45	9.89	133.12	3.06	0.08	0.96
23.40	13.31	13.61	10.12	137.78	3.07	0.08	0.97
23.45	13.70	14.04	10.21	143.37	3.08	0.08	1.00
23.50	14.44	14.85	10.02	148.80	3.07	0.08	1.06
23.55	15.48	16.01	9.59	153.56	3.05	0.09	1.14
23.60	16.69	17.35	9.00	156.13	3.01	0.09	1.24
23.65	17.65	18.41	8.48	156.09	2.98	0.09	0.62
23.70	18.15	18.94	8.08	153.01	2.96	0.09	0.62
23.75	17.98	18.72	7.88	147.60	2.94	0.09	0.62
23.80	17.49	18.13	7.79	141.12	2.94	0.09	0.62
23.85	16.78	17.30	7.77	134.36	2.94	0.09	0.62
23.90	15.98	16.37	7.82	128.08	2.94	0.09	0.62
23.95	15.09	15.36	7.93	121.85	2.95	0.08	0.62
24.00	14.19	14.32	8.11	116.08	2.96	0.08	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
24.05	13.55	13.58	8.18	111.15	2.96	0.08	0.62
24.10	13.20	13.17	8.28	109.11	2.97	0.08	0.62
24.15	13.30	13.26	8.32	110.41	2.97	0.08	0.62
24.20	13.74	13.73	8.47	116.27	2.98	0.08	0.62
24.25	14.80	14.89	8.41	125.27	2.98	0.08	0.62
24.30	16.23	16.44	8.32	136.81	2.97	0.09	0.62
24.35	18.18	18.58	7.97	148.06	2.95	0.09	0.62
24.40	20.21	20.79	7.59	157.80	2.93	0.09	0.62
24.45	22.53	23.30	7.02	163.48	2.89	0.09	0.62
24.50	25.19	26.12	6.38	166.60	2.84	0.10	0.62
24.55	28.19	29.28	5.69	166.51	2.79	0.10	0.62
24.60	31.49	32.73	5.07	165.98	2.73	0.10	0.62
24.65	34.39	35.73	4.58	163.76	2.69	0.11	0.62
24.70	36.86	38.27	4.21	161.05	2.65	0.11	0.62
24.75	38.66	40.08	3.92	157.16	2.62	0.11	0.62
24.80	40.24	41.65	3.66	152.45	2.59	0.11	0.75
24.85	41.99	43.39	3.40	147.45	2.56	0.11	0.76
24.90	44.00	45.38	3.12	141.37	2.52	0.11	0.76
24.95	46.64	48.02	2.82	135.54	2.48	0.11	0.76
25.00	49.30	50.65	2.55	129.14	2.43	0.12	0.77
25.05	52.08	53.40	2.32	123.72	2.39	0.12	0.77
25.10	53.91	55.16	2.15	118.66	2.35	0.12	0.78
25.15	55.06	56.22	2.04	114.69	2.33	0.12	0.78
25.20	55.46	56.53	1.98	111.85	2.31	0.12	0.78
25.25	55.87	56.85	1.94	110.41	2.30	0.12	0.78
25.30	56.48	57.41	1.92	110.21	2.30	0.12	0.78
25.35	57.20	58.07	1.90	110.52	2.29	0.12	0.78
25.40	57.98	58.80	1.89	111.18	2.29	0.12	0.78
25.45	58.95	59.72	1.87	111.96	2.29	0.12	0.78
25.50	60.19	60.91	1.85	112.60	2.28	0.12	0.78
25.55	61.96	62.63	1.80	112.86	2.27	0.12	0.78
25.60	64.03	64.63	1.74	112.54	2.25	0.13	0.79
25.65	66.76	67.30	1.67	112.58	2.22	0.13	0.79
25.70	69.59	70.06	1.61	113.00	2.20	0.13	0.79
25.75	72.49	72.90	1.57	114.12	2.18	0.13	0.80
25.80	75.35	75.69	1.53	115.74	2.16	0.14	0.80
25.85	78.28	78.55	1.50	118.06	2.15	0.14	0.80
25.90	81.53	81.75	1.48	121.18	2.14	0.14	0.81
25.95	83.12	83.27	1.48	123.07	2.14	0.15	0.81
26.00	82.31	82.35	1.49	122.42	2.14	0.15	0.81
26.05	79.36	79.29	1.51	119.46	2.15	0.14	0.81
26.10	76.33	76.14	1.52	115.83	2.16	0.14	0.80
26.15	75.41	75.11	1.52	114.22	2.16	0.13	0.80
26.20	75.46	75.07	1.52	113.85	2.16	0.14	0.80
26.25	75.56	75.10	1.52	114.26	2.16	0.14	0.80
26.30	74.50	73.96	1.54	114.10	2.17	0.13	0.80
26.35	72.82	72.22	1.58	113.87	2.18	0.13	0.80
26.40	71.07	70.41	1.62	113.99	2.20	0.13	0.80

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
26.45	69.30	68.58	1.68	115.12	2.22	0.13	0.79
26.50	67.46	66.70	1.76	117.10	2.25	0.13	0.79
26.55	65.64	64.85	1.85	120.28	2.28	0.13	0.79
26.60	63.55	62.72	1.98	123.94	2.31	0.13	0.79
26.65	61.12	60.26	2.12	128.02	2.35	0.13	0.79
26.70	58.35	57.45	2.32	133.12	2.39	0.13	0.78
26.75	55.46	54.53	2.54	138.68	2.43	0.12	0.78
26.80	52.67	51.71	2.81	145.49	2.48	0.12	0.77
26.85	49.61	48.61	3.11	151.41	2.52	0.12	0.77
26.90	46.41	45.37	3.46	157.14	2.57	0.12	0.76
26.95	42.85	41.77	3.86	161.23	2.61	0.11	0.62
27.00	39.81	38.68	4.25	164.56	2.65	0.11	0.62
27.05	37.31	36.14	4.62	166.86	2.69	0.11	0.62
27.10	35.96	34.74	4.86	168.70	2.71	0.11	0.62
27.15	35.29	34.03	5.00	170.04	2.73	0.11	0.62
27.20	35.12	33.80	5.04	170.50	2.73	0.11	0.62
27.25	34.89	33.53	5.07	170.13	2.73	0.11	0.62
27.30	34.59	33.18	5.11	169.40	2.74	0.10	0.62
27.35	34.50	33.03	5.13	169.37	2.74	0.10	0.62
27.40	34.67	33.16	5.14	170.51	2.74	0.11	0.62
27.45	35.15	33.58	5.14	172.54	2.74	0.11	0.62
27.50	35.43	33.82	5.17	174.71	2.74	0.11	0.62
27.55	35.45	33.79	5.23	176.60	2.75	0.11	0.62
27.60	34.87	33.16	5.36	177.61	2.76	0.11	0.62
27.65	34.00	32.26	5.52	178.02	2.77	0.10	0.62
27.70	33.63	31.85	5.61	178.60	2.78	0.10	0.62
27.75	34.10	32.26	5.56	179.47	2.78	0.10	0.62
27.80	35.49	33.58	5.36	179.99	2.76	0.11	0.62
27.85	37.10	35.11	5.10	179.02	2.74	0.11	0.62
27.90	39.04	36.95	4.77	176.14	2.71	0.11	0.62
27.95	41.71	39.51	4.37	172.64	2.67	0.11	0.62
28.00	44.66	42.31	3.96	167.52	2.62	0.12	0.62
28.05	47.02	44.54	3.64	162.17	2.59	0.12	0.77
28.10	47.52	44.96	3.45	155.18	2.56	0.12	0.77
28.15	46.09	43.50	3.44	149.84	2.56	0.12	0.76
28.20	43.31	40.73	3.58	145.94	2.58	0.11	0.76
28.25	39.82	37.29	3.89	145.14	2.62	0.11	0.62
28.30	36.40	33.92	4.28	145.06	2.66	0.10	0.62
28.35	33.71	31.27	4.67	145.87	2.70	0.10	0.62
28.40	32.17	29.73	4.94	146.89	2.72	0.10	0.62
28.45	31.53	29.07	5.11	148.63	2.74	0.10	0.62
28.50	31.26	28.76	5.24	150.74	2.75	0.10	0.62
28.55	30.87	28.36	5.38	152.68	2.76	0.10	0.62
28.60	30.51	27.97	5.51	154.20	2.77	0.10	0.62
28.65	30.47	27.89	5.57	155.21	2.78	0.10	0.62
28.70	30.58	27.96	5.55	155.03	2.77	0.10	0.62
28.75	30.60	27.93	5.49	153.36	2.77	0.10	0.62
28.80	29.20	26.55	5.60	148.69	2.78	0.10	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
28.85	26.34	23.76	5.94	141.17	2.81	0.09	0.62
28.90	22.09	19.64	6.66	130.78	2.86	0.09	0.62
28.95	18.12	15.80	7.57	119.61	2.92	0.09	0.62
29.00	15.37	13.13	8.39	110.11	2.98	0.08	0.62
29.05	14.03	11.83	8.73	103.30	3.00	0.08	0.62
29.10	13.51	11.32	8.73	98.81	3.00	0.08	0.62
29.15	13.24	11.05	8.59	94.90	2.99	0.08	0.62
29.20	13.11	10.91	8.43	91.97	2.98	0.08	0.62
29.25	13.11	10.89	8.28	90.19	2.97	0.08	0.62
29.30	13.11	10.87	8.27	89.95	2.97	0.08	0.62
29.35	13.11	10.86	8.38	90.96	2.98	0.08	0.62
29.40	13.11	10.84	8.58	93.04	2.99	0.08	0.62
29.45	13.11	10.83	8.81	95.44	3.00	0.08	0.77
29.50	13.36	11.05	8.91	98.49	3.01	0.08	0.79
29.55	13.81	11.47	8.89	101.95	3.01	0.08	0.82
29.60	14.52	12.12	8.71	105.65	3.00	0.08	0.62
29.65	15.32	12.86	8.49	109.24	2.98	0.08	0.62
29.70	16.41	13.87	8.13	112.82	2.96	0.08	0.62
29.75	17.69	15.06	7.73	116.36	2.93	0.09	0.62
29.80	19.03	16.30	7.28	118.68	2.91	0.09	0.62
29.85	19.87	17.07	6.98	119.18	2.88	0.09	0.62
29.90	20.01	17.18	6.86	117.81	2.88	0.09	0.62
29.95	18.99	16.20	7.10	115.07	2.89	0.09	0.62
30.00	18.18	15.42	7.35	113.32	2.91	0.08	0.62
30.05	18.22	15.43	7.31	112.87	2.91	0.09	0.62
30.10	20.31	17.37	6.62	115.01	2.86	0.09	0.62
30.15	23.10	19.96	5.85	116.84	2.80	0.09	0.62
30.20	25.29	21.99	5.36	117.94	2.76	0.09	0.62
30.25	26.11	22.72	5.23	118.75	2.75	0.09	0.62
30.30	25.75	22.35	5.40	120.72	2.76	0.09	0.62
30.35	25.28	21.88	5.73	125.41	2.79	0.09	0.62
30.40	24.92	21.51	6.18	132.98	2.83	0.09	0.62
30.45	26.19	22.65	6.40	144.96	2.84	0.09	0.62
30.50	28.97	25.20	6.35	160.00	2.84	0.10	0.62
30.55	34.13	29.94	5.88	176.16	2.80	0.10	0.62
30.60	40.03	35.37	5.32	188.27	2.76	0.11	0.62
30.65	47.16	41.93	4.63	194.28	2.69	0.12	0.62
30.70	53.35	47.61	4.03	191.77	2.63	0.13	0.63
30.75	58.70	52.51	3.51	184.10	2.57	0.13	0.78
30.80	62.66	56.12	3.10	173.99	2.52	0.14	0.79
30.85	66.56	59.66	2.77	165.44	2.47	0.14	0.80
30.90	71.42	64.10	2.49	159.58	2.42	0.14	0.80
30.95	76.82	69.03	2.25	155.17	2.38	0.15	0.81
31.00	82.78	74.46	2.04	151.92	2.33	0.16	0.82
31.05	88.37	79.56	1.87	148.44	2.28	0.17	0.82
31.10	93.74	84.44	1.73	146.17	2.24	0.18	0.83
31.15	98.72	88.96	1.64	145.53	2.21	0.18	0.83
31.20	103.47	93.25	1.58	147.45	2.19	0.19	0.84

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
31.25	109.02	98.24	1.55	152.11	2.17	0.20	0.85
31.30	115.77	104.33	1.53	159.36	2.16	0.22	0.85
31.35	123.72	111.51	1.50	167.81	2.15	0.25	0.86
31.40	132.87	119.76	1.48	177.11	2.14	0.29	0.87
31.45	142.35	128.33	1.45	185.77	2.12	0.34	0.89
31.50	153.16	138.10	1.41	195.20	2.10	0.41	0.89
31.55	163.20	147.16	1.38	203.54	2.07	0.53	0.91
31.60	173.03	156.02	1.36	211.85	2.05	0.64	0.91
31.65	180.44	162.64	1.34	217.88	2.04	0.79	0.92
31.70	186.57	168.09	1.33	222.79	2.02	0.90	0.92
31.75	191.07	172.05	1.31	226.20	2.01	0.91	0.92
31.80	194.89	175.37	1.31	229.14	2.00	0.91	0.92
31.85	198.61	178.59	1.30	232.22	1.99	0.91	0.93
31.90	202.38	181.85	1.29	235.46	1.98	0.91	0.93
31.95	206.39	185.31	1.29	239.04	1.98	0.92	0.93
32.00	209.00	187.50	1.29	241.32	1.97	0.92	0.93
32.05	210.08	188.27	1.29	242.36	1.97	0.92	0.93
32.10	208.94	187.01	1.29	241.44	1.98	0.92	0.93
32.15	207.00	185.02	1.30	240.15	1.99	0.92	0.93
32.20	204.32	182.34	1.31	238.41	2.00	0.92	0.93
32.25	201.85	179.85	1.32	237.31	2.01	0.91	0.93
32.30	199.62	177.59	1.33	236.38	2.03	0.91	0.93
32.35	198.37	176.23	1.34	236.18	2.04	0.91	0.93
32.40	198.24	175.91	1.34	236.04	2.04	0.91	0.93
32.45	199.82	177.15	1.34	236.75	2.03	0.91	0.93
32.50	202.60	179.52	1.32	237.65	2.02	0.91	0.93
32.55	206.36	182.79	1.31	239.27	2.00	0.92	0.94
32.60	210.53	186.43	1.29	241.11	1.98	0.92	0.94
32.65	214.74	190.11	1.28	243.31	1.96	0.92	0.94
32.70	218.70	193.56	1.27	245.52	1.95	0.92	0.93
32.75	221.32	195.76	1.26	246.83	1.94	0.93	0.93
32.80	222.30	196.48	1.26	246.97	1.93	0.93	0.93
32.85	221.39	195.47	1.26	245.74	1.93	0.93	0.93
32.90	219.55	193.60	1.26	243.89	1.93	0.92	0.93
32.95	217.58	191.62	1.26	242.03	1.94	0.92	0.93
33.00	215.84	189.86	1.27	240.19	1.94	0.92	0.93
33.05	214.08	188.09	1.27	238.17	1.94	0.92	0.93
33.10	211.73	185.81	1.27	235.40	1.95	0.92	0.93
33.15	208.42	182.68	1.27	231.84	1.95	0.92	0.92
33.20	203.60	178.18	1.27	226.98	1.96	0.91	0.92
33.25	197.58	172.60	1.28	221.31	1.97	0.91	0.92
33.30	189.54	165.23	1.29	213.96	1.98	0.83	0.91
33.35	181.40	157.75	1.31	207.08	2.01	0.64	0.91
33.40	173.00	150.06	1.34	200.33	2.03	0.56	0.90
33.45	166.53	144.09	1.36	195.86	2.05	0.48	0.90
33.50	161.02	139.02	1.38	191.82	2.07	0.44	0.90
33.55	157.44	135.69	1.39	189.00	2.08	0.41	0.89
33.60	155.20	133.59	1.39	186.21	2.08	0.39	0.89

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
33.65	155.05	133.36	1.39	184.71	2.08	0.38	0.89
33.70	155.92	134.06	1.37	183.45	2.06	0.39	0.89
33.75	157.40	135.31	1.35	182.75	2.05	0.38	0.89
33.80	158.78	136.49	1.33	181.82	2.03	0.38	0.89
33.85	160.22	137.70	1.32	181.31	2.01	0.38	0.89
33.90	161.17	138.50	1.30	180.58	2.00	0.38	0.88
33.95	161.04	138.31	1.30	179.34	1.99	0.37	0.88
34.00	159.04	136.45	1.30	176.73	1.98	0.36	0.88
34.05	156.01	133.64	1.30	173.80	1.99	0.33	0.88
34.10	152.34	130.25	1.31	170.80	2.00	0.32	0.87
34.15	149.01	127.13	1.33	168.66	2.02	0.30	0.87
34.20	145.93	124.24	1.34	166.90	2.04	0.29	0.87
34.25	143.37	121.81	1.36	165.70	2.05	0.29	0.87
34.30	141.80	120.26	1.37	165.25	2.07	0.28	0.87
34.35	141.31	119.67	1.38	165.60	2.07	0.28	0.87
34.40	141.88	120.02	1.39	166.64	2.08	0.29	0.87
34.45	143.01	120.85	1.39	167.98	2.08	0.30	0.87
34.50	144.50	122.01	1.39	169.67	2.08	0.30	0.88
34.55	146.18	123.31	1.39	171.61	2.08	0.32	0.88
34.60	148.30	125.00	1.39	173.90	2.08	0.33	0.88
34.65	150.68	126.93	1.39	176.09	2.08	0.34	0.88
34.70	153.55	129.30	1.38	178.30	2.07	0.36	0.89
34.75	156.78	132.00	1.37	180.38	2.06	0.38	0.89
34.80	160.27	134.93	1.35	182.58	2.05	0.40	0.89
34.85	163.82	137.92	1.34	184.80	2.04	0.42	0.89
34.90	166.56	140.18	1.33	186.64	2.03	0.45	0.89
34.95	168.16	141.44	1.33	187.78	2.02	0.46	0.90
35.00	168.07	141.20	1.33	187.93	2.03	0.46	0.90
35.05	166.85	139.96	1.34	187.36	2.03	0.45	0.90
35.10	165.03	138.17	1.35	186.60	2.05	0.44	0.89
35.15	163.32	136.50	1.36	185.97	2.06	0.43	0.89
35.20	162.03	135.19	1.37	185.69	2.07	0.42	0.89
35.25	161.27	134.37	1.38	185.58	2.07	0.42	0.89
35.30	160.94	133.92	1.39	185.60	2.08	0.42	0.89
35.35	161.08	133.89	1.39	185.75	2.08	0.42	0.89
35.40	161.52	134.13	1.39	186.05	2.08	0.43	0.90
35.45	162.34	134.69	1.39	186.63	2.08	0.43	0.90
35.50	163.26	135.34	1.38	187.29	2.07	0.44	0.90
35.55	164.33	136.12	1.38	188.07	2.07	0.45	0.90
35.60	165.51	136.99	1.38	188.81	2.07	0.46	0.90
35.65	166.97	138.11	1.37	189.67	2.07	0.47	0.90
35.70	168.87	139.62	1.37	190.72	2.06	0.48	0.90
35.75	171.00	141.33	1.36	191.99	2.05	0.51	0.90
35.80	173.32	143.18	1.35	193.48	2.05	0.53	0.90
35.85	175.30	144.75	1.35	194.80	2.04	0.55	0.90
35.90	177.07	146.14	1.34	195.98	2.04	0.57	0.91
35.95	178.13	146.90	1.34	196.61	2.03	0.59	0.91
36.00	178.63	147.17	1.34	196.90	2.03	0.59	0.91

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
36.05	177.88	146.38	1.34	196.23	2.04	0.59	0.91
36.10	176.26	144.84	1.35	194.88	2.04	0.56	0.91
36.15	173.28	142.14	1.35	192.38	2.05	0.53	0.90
36.20	169.82	139.04	1.36	189.59	2.06	0.49	0.90
36.25	165.72	135.41	1.38	186.35	2.07	0.45	0.90
36.30	161.89	132.00	1.39	183.40	2.08	0.42	0.89
36.35	157.98	128.56	1.40	180.16	2.09	0.39	0.89
36.40	152.84	124.11	1.42	175.67	2.10	0.36	0.89
36.45	146.42	118.61	1.43	169.73	2.11	0.31	0.88
36.50	137.93	111.40	1.45	161.92	2.12	0.28	0.87
36.55	131.24	105.74	1.47	155.26	2.13	0.24	0.86
36.60	126.58	101.79	1.48	150.19	2.13	0.23	0.86
36.65	126.90	102.02	1.46	148.88	2.13	0.22	0.85
36.70	129.22	103.91	1.44	149.66	2.11	0.23	0.86
36.75	132.57	106.64	1.42	151.77	2.10	0.24	0.86
36.80	132.90	106.77	1.43	152.68	2.11	0.25	0.86
36.85	129.15	103.43	1.46	151.48	2.13	0.24	0.86
36.90	120.57	95.99	1.56	149.44	2.18	0.22	0.85
36.95	109.20	86.26	1.72	148.40	2.24	0.20	0.84
37.00	96.25	75.25	2.00	150.52	2.32	0.18	0.83
37.05	83.85	64.83	2.39	154.97	2.40	0.16	0.81
37.10	71.18	54.30	2.94	159.91	2.50	0.14	0.80
37.15	60.50	45.50	3.63	165.02	2.59	0.13	0.78
37.20	51.00	37.77	4.44	167.57	2.67	0.12	0.62
37.25	44.67	32.64	5.17	168.73	2.74	0.11	0.62
37.30	39.79	28.73	5.77	165.90	2.79	0.11	0.62
37.35	36.21	25.89	6.21	160.83	2.83	0.10	0.62
37.40	33.31	23.61	6.50	153.47	2.85	0.10	0.62
37.45	31.01	21.83	6.68	145.85	2.86	0.10	0.62
37.50	29.53	20.68	6.72	138.90	2.87	0.09	0.62
37.55	28.34	19.75	6.73	132.88	2.87	0.09	0.62
37.60	27.15	18.83	6.75	127.12	2.87	0.09	0.62
37.65	26.61	18.40	6.71	123.40	2.86	0.09	0.62
37.70	28.33	19.71	6.27	123.59	2.83	0.09	0.62
37.75	31.84	22.41	5.80	129.95	2.80	0.10	0.62
37.80	36.44	25.93	5.40	140.08	2.76	0.10	0.62
37.85	38.93	27.78	5.45	151.43	2.77	0.11	0.62
37.90	40.34	28.79	5.56	160.06	2.78	0.11	0.62
37.95	43.01	30.79	5.45	167.96	2.77	0.11	0.62
38.00	48.68	35.20	4.85	170.85	2.71	0.11	0.62
38.05	58.51	42.95	3.96	170.30	2.62	0.12	0.62
38.10	69.29	51.60	3.12	160.90	2.52	0.14	0.79
38.15	81.00	61.13	2.44	149.34	2.41	0.15	0.81
38.20	91.48	69.87	1.95	136.32	2.31	0.16	0.82
38.25	100.61	77.55	1.66	128.87	2.22	0.17	0.83
38.30	107.26	83.27	1.50	124.52	2.15	0.17	0.83
38.35	110.81	86.35	1.42	122.93	2.10	0.17	0.83
38.40	111.54	87.02	1.39	121.21	2.08	0.17	0.83

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
38.45	110.10	85.78	1.40	119.80	2.08	0.17	0.82
38.50	107.73	83.72	1.42	118.55	2.10	0.16	0.82
38.55	104.98	81.28	1.45	118.12	2.12	0.16	0.82
38.60	102.27	78.87	1.50	118.33	2.15	0.16	0.82
38.65	99.41	76.33	1.56	119.14	2.18	0.16	0.82
38.70	97.36	74.48	1.62	120.46	2.20	0.16	0.82
38.75	96.13	73.33	1.66	121.75	2.22	0.16	0.82
38.80	96.51	73.55	1.67	122.50	2.22	0.16	0.82
38.85	97.65	74.42	1.65	122.48	2.21	0.16	0.82
38.90	99.57	75.96	1.60	121.86	2.20	0.16	0.82
38.95	101.45	77.49	1.57	121.34	2.18	0.16	0.82
39.00	103.41	79.06	1.53	121.23	2.16	0.16	0.82
39.05	104.30	79.71	1.53	121.67	2.16	0.17	0.83
39.10	104.12	79.44	1.54	122.39	2.17	0.17	0.83
39.15	102.07	77.60	1.59	123.48	2.19	0.17	0.83
39.20	99.25	75.11	1.67	125.26	2.22	0.16	0.82
39.25	95.46	71.83	1.78	128.08	2.26	0.16	0.82
39.30	91.24	68.21	1.94	132.15	2.30	0.16	0.82
39.35	85.91	63.72	2.15	136.82	2.35	0.15	0.81
39.40	80.34	59.09	2.42	142.78	2.41	0.15	0.80
39.45	74.97	54.68	2.72	148.58	2.46	0.14	0.80
39.50	70.67	51.14	3.03	154.93	2.51	0.14	0.79
39.55	67.29	48.38	3.29	159.10	2.54	0.13	0.79
39.60	64.57	46.18	3.50	161.57	2.57	0.13	0.78
39.65	63.21	45.08	3.55	160.17	2.58	0.13	0.78
39.70	63.09	44.98	3.49	157.17	2.57	0.13	0.78
39.75	64.30	45.91	3.34	153.20	2.55	0.13	0.78
39.80	65.78	47.05	3.20	150.41	2.53	0.13	0.78
39.85	67.57	48.42	3.06	148.38	2.51	0.13	0.79
39.90	69.92	50.27	2.87	144.07	2.48	0.13	0.79
39.95	73.38	53.05	2.58	136.93	2.44	0.14	0.79
40.00	76.70	55.79	2.29	127.51	2.38	0.14	0.80
40.05	79.39	58.04	2.07	120.37	2.34	0.14	0.80
40.10	80.09	58.63	2.00	117.00	2.32	0.14	0.80
40.15	79.80	58.34	2.01	117.02	2.32	0.14	0.80
40.20	78.56	57.24	2.08	118.96	2.34	0.14	0.80
40.25	77.27	56.10	2.16	121.10	2.36	0.14	0.80
40.30	75.86	54.88	2.24	123.19	2.37	0.14	0.79
40.35	74.61	53.81	2.32	124.64	2.39	0.13	0.79
40.40	73.46	52.85	2.36	124.90	2.40	0.13	0.79
40.45	72.40	52.00	2.37	123.47	2.40	0.13	0.79
40.50	71.39	51.21	2.36	120.96	2.40	0.13	0.79
40.55	70.32	50.39	2.34	117.87	2.39	0.13	0.79
40.60	68.99	49.33	2.36	116.60	2.40	0.13	0.78
40.65	67.26	47.92	2.45	117.24	2.41	0.13	0.78
40.70	64.92	45.97	2.64	121.43	2.45	0.12	0.78
40.75	62.36	43.85	2.89	126.93	2.49	0.12	0.77
40.80	59.39	41.41	3.23	133.71	2.53	0.12	0.77

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
40.85	56.83	39.33	3.53	138.79	2.57	0.12	0.77
40.90	54.64	37.58	3.79	142.38	2.60	0.12	0.62
40.95	54.44	37.37	3.83	143.11	2.61	0.12	0.62
41.00	55.85	38.41	3.70	142.02	2.59	0.12	0.77
41.05	59.98	41.56	3.33	138.21	2.55	0.12	0.77
41.10	65.10	45.50	2.93	133.14	2.49	0.13	0.78
41.15	71.52	50.49	2.51	126.96	2.43	0.13	0.79
41.20	77.66	55.32	2.20	121.83	2.37	0.14	0.80
41.25	84.09	60.40	1.95	117.94	2.31	0.14	0.80
41.30	90.57	65.55	1.76	115.56	2.25	0.15	0.81
41.35	97.02	70.71	1.62	114.48	2.20	0.15	0.82
41.40	103.34	75.81	1.51	114.35	2.15	0.16	0.82
41.45	108.53	80.03	1.44	115.04	2.11	0.16	0.82
41.50	113.02	83.70	1.39	116.12	2.08	0.16	0.82
41.55	115.16	85.45	1.36	116.49	2.06	0.17	0.83
41.60	115.36	85.63	1.35	115.88	2.05	0.16	0.82
41.65	111.94	82.85	1.37	113.19	2.06	0.16	0.82
41.70	106.66	78.55	1.40	109.84	2.09	0.15	0.81
41.75	98.88	72.23	1.47	105.98	2.13	0.15	0.81
41.80	90.96	65.75	1.59	104.54	2.19	0.14	0.80
41.85	82.43	58.83	1.80	105.82	2.26	0.14	0.80
41.90	75.38	53.10	2.08	110.70	2.34	0.13	0.79
41.95	69.28	48.21	2.41	116.29	2.41	0.13	0.78
42.00	64.01	44.03	2.77	121.84	2.47	0.12	0.78
42.05	59.15	40.23	3.16	126.93	2.52	0.12	0.77
42.10	54.53	36.64	3.61	132.43	2.58	0.12	0.76
42.15	51.91	34.58	3.98	137.59	2.63	0.11	0.62
42.20	50.83	33.68	4.22	142.10	2.65	0.11	0.62
42.25	51.46	34.07	4.24	144.40	2.65	0.11	0.62
42.30	52.30	34.64	4.18	144.97	2.65	0.11	0.62
42.35	53.04	35.17	4.08	143.50	2.64	0.12	0.62
42.40	53.37	35.39	4.02	142.17	2.63	0.12	0.62
42.45	53.34	35.34	4.00	141.51	2.63	0.12	0.62
42.50	52.74	34.84	4.10	142.94	2.64	0.12	0.62
42.55	51.69	34.00	4.27	145.32	2.66	0.11	0.62
42.60	49.87	32.58	4.57	148.79	2.69	0.11	0.62
42.65	47.83	31.01	4.92	152.45	2.72	0.11	0.62
42.70	45.50	29.23	5.36	156.77	2.76	0.11	0.62
42.75	44.11	28.14	5.73	161.19	2.79	0.11	0.62
42.80	43.65	27.72	5.98	165.81	2.81	0.11	0.62
42.85	45.52	28.99	5.86	169.89	2.80	0.11	0.62
42.90	48.86	31.33	5.51	172.70	2.77	0.11	0.62
42.95	54.26	35.19	4.90	172.48	2.72	0.12	0.62
43.00	59.96	39.32	4.30	168.95	2.66	0.13	0.62
43.05	66.38	44.07	3.67	161.80	2.59	0.13	0.78
43.10	71.78	48.15	3.18	152.89	2.53	0.14	0.79
43.15	76.39	51.71	2.77	143.28	2.47	0.14	0.80
43.20	78.77	53.63	2.51	134.57	2.42	0.14	0.80

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
43.25	79.71	54.45	2.35	128.17	2.40	0.14	0.80
43.30	79.20	54.10	2.31	124.94	2.39	0.14	0.80
43.35	78.76	53.69	2.34	125.89	2.39	0.14	0.80
43.40	78.69	53.47	2.43	130.11	2.41	0.14	0.80
43.45	78.43	53.06	2.57	136.32	2.44	0.14	0.80
43.50	77.44	52.12	2.74	142.81	2.46	0.14	0.80
43.55	74.94	50.08	2.98	149.15	2.50	0.14	0.79
43.60	72.49	48.11	3.22	154.85	2.53	0.14	0.79
43.65	70.55	46.54	3.45	160.67	2.56	0.14	0.79
43.70	71.50	47.08	3.52	165.81	2.57	0.14	0.79
43.75	74.94	49.44	3.45	170.55	2.56	0.14	0.79
43.80	80.85	53.66	3.21	172.00	2.53	0.15	0.80
43.85	87.12	58.21	2.93	170.73	2.49	0.16	0.81
43.90	93.83	63.18	2.63	166.08	2.45	0.17	0.82
43.95	101.14	68.65	2.35	161.46	2.40	0.18	0.83
44.00	110.53	75.73	2.08	157.27	2.34	0.19	0.84
44.05	121.59	84.08	1.85	155.83	2.28	0.22	0.85
44.10	133.55	93.17	1.68	156.49	2.22	0.25	0.86
44.15	145.66	102.44	1.55	158.95	2.17	0.29	0.87
44.20	156.89	111.13	1.46	162.31	2.13	0.34	0.89
44.25	168.00	119.81	1.39	166.68	2.08	0.38	0.89
44.30	177.83	127.46	1.35	172.03	2.05	0.46	0.90
44.35	187.59	134.95	1.32	178.61	2.02	0.53	0.90
44.40	196.04	141.30	1.31	185.16	2.00	0.66	0.91
44.45	203.45	146.83	1.30	191.06	1.99	0.79	0.91
44.50	209.43	151.26	1.29	195.82	1.98	0.89	0.92
44.55	214.10	154.68	1.29	199.50	1.98	0.89	0.92
44.60	217.99	157.52	1.29	202.56	1.97	0.89	0.92
44.65	220.70	159.45	1.28	204.64	1.97	0.90	0.93
44.70	222.71	160.85	1.28	206.15	1.97	0.90	0.93
44.75	223.47	161.28	1.28	206.62	1.97	0.90	0.93
44.80	223.50	161.17	1.28	206.50	1.97	0.90	0.93
44.85	222.63	160.37	1.28	205.63	1.97	0.90	0.93
44.90	221.39	159.29	1.28	204.47	1.97	0.89	0.93
44.95	219.77	157.93	1.29	203.00	1.97	0.89	0.92
45.00	218.21	156.60	1.29	201.57	1.97	0.89	0.92
45.05	216.72	155.34	1.29	200.21	1.98	0.89	0.92
45.10	215.31	154.14	1.29	198.92	1.98	0.89	0.92
45.15	213.85	152.90	1.29	197.59	1.98	0.89	0.92
45.20	212.05	151.41	1.29	195.99	1.98	0.89	0.92
45.25	210.12	149.82	1.30	194.28	1.99	0.89	0.92
45.30	208.04	148.13	1.30	192.46	1.99	0.86	0.92
45.35	206.23	146.62	1.30	190.94	1.99	0.82	0.91
45.40	204.69	145.30	1.31	189.71	2.00	0.79	0.91
45.45	203.43	144.18	1.31	188.79	2.00	0.77	0.91
45.50	202.70	143.47	1.31	188.21	2.01	0.75	0.91
45.55	202.59	143.27	1.31	187.99	2.01	0.75	0.91
45.60	203.21	143.64	1.31	188.19	2.00	0.76	0.91

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
45.65	204.10	144.23	1.31	188.55	2.00	0.77	0.91
45.70	204.99	144.82	1.31	189.00	2.00	0.79	0.91
45.75	205.81	145.33	1.30	189.43	2.00	0.80	0.91
45.80	206.70	145.89	1.30	189.91	1.99	0.81	0.91
45.85	207.49	146.44	1.30	190.12	1.99	0.83	0.91
45.90	208.14	146.95	1.29	189.95	1.98	0.82	0.91
45.95	208.40	147.27	1.28	189.18	1.97	0.79	0.91
46.00	208.46	147.51	1.27	188.06	1.96	0.75	0.91
46.05	208.14	147.56	1.26	186.44	1.94	0.70	0.90
46.10	207.68	147.52	1.25	184.66	1.92	0.64	0.90
46.15	207.15	147.51	1.24	182.64	1.90	0.59	0.89
46.20	207.36	148.01	1.22	181.28	1.88	0.55	0.88
46.25	208.33	149.06	1.21	180.46	1.86	0.53	0.87
46.30	210.67	151.03	1.20	180.98	1.85	0.53	0.87
46.35	213.60	153.39	1.19	181.99	1.83	0.56	0.87
46.40	217.34	156.32	1.17	183.58	1.82	0.59	0.87
46.45	220.91	159.14	1.16	184.76	1.81	0.64	0.87
46.50	224.61	162.13	1.14	185.42	1.79	0.68	0.87
46.55	227.82	164.78	1.12	185.18	1.78	0.74	0.87
46.60	230.78	167.27	1.10	184.06	1.76	0.79	0.87
46.65	232.99	169.16	1.08	182.33	1.75	0.84	0.88
46.70	234.26	170.31	1.06	179.97	1.73	0.87	0.88
46.75	234.70	170.85	1.03	176.65	1.72	0.86	0.88
46.80	234.70	171.09	1.01	172.39	1.71	0.86	0.88
46.85	234.70	171.39	1.00	171.39	1.70	0.85	0.88
46.90	234.57	171.59	1.00	171.59	1.68	0.85	0.88
46.95	233.63	171.17	1.00	171.17	1.67	0.84	0.88
47.00	231.40	169.71	1.00	169.71	1.66	0.78	0.87
47.05	227.32	166.66	1.00	166.66	1.65	0.69	0.87
47.10	221.14	161.73	1.00	161.73	1.66	0.58	0.86
47.15	213.26	155.25	1.00	155.25	1.68	0.46	0.85
47.20	204.49	147.97	1.02	150.23	1.71	0.38	0.84
47.25	195.41	140.45	1.08	151.39	1.75	0.32	0.83
47.30	186.26	132.87	1.13	150.49	1.78	0.27	0.82
47.35	175.48	123.85	1.19	147.35	1.84	0.25	0.83
47.40	163.92	114.23	1.24	141.44	1.90	0.23	0.83
47.45	150.98	103.60	1.29	133.84	1.98	0.22	0.85
47.50	138.23	93.33	1.37	127.72	2.06	0.21	0.85
47.55	125.91	83.54	1.50	125.29	2.15	0.19	0.84
47.60	114.57	74.65	1.71	127.91	2.24	0.18	0.84
47.65	106.12	68.01	1.99	135.18	2.32	0.17	0.83
47.70	100.59	63.55	2.30	146.32	2.39	0.17	0.82
47.75	98.14	61.38	2.57	157.93	2.44	0.17	0.82
47.80	96.75	59.98	2.84	170.33	2.48	0.17	0.82
47.85	95.75	58.96	3.06	180.27	2.51	0.17	0.82
47.90	95.51	58.52	3.22	188.60	2.53	0.17	0.82
47.95	97.24	59.53	3.24	192.99	2.54	0.17	0.82
48.00	100.39	61.57	3.16	194.79	2.53	0.18	0.83

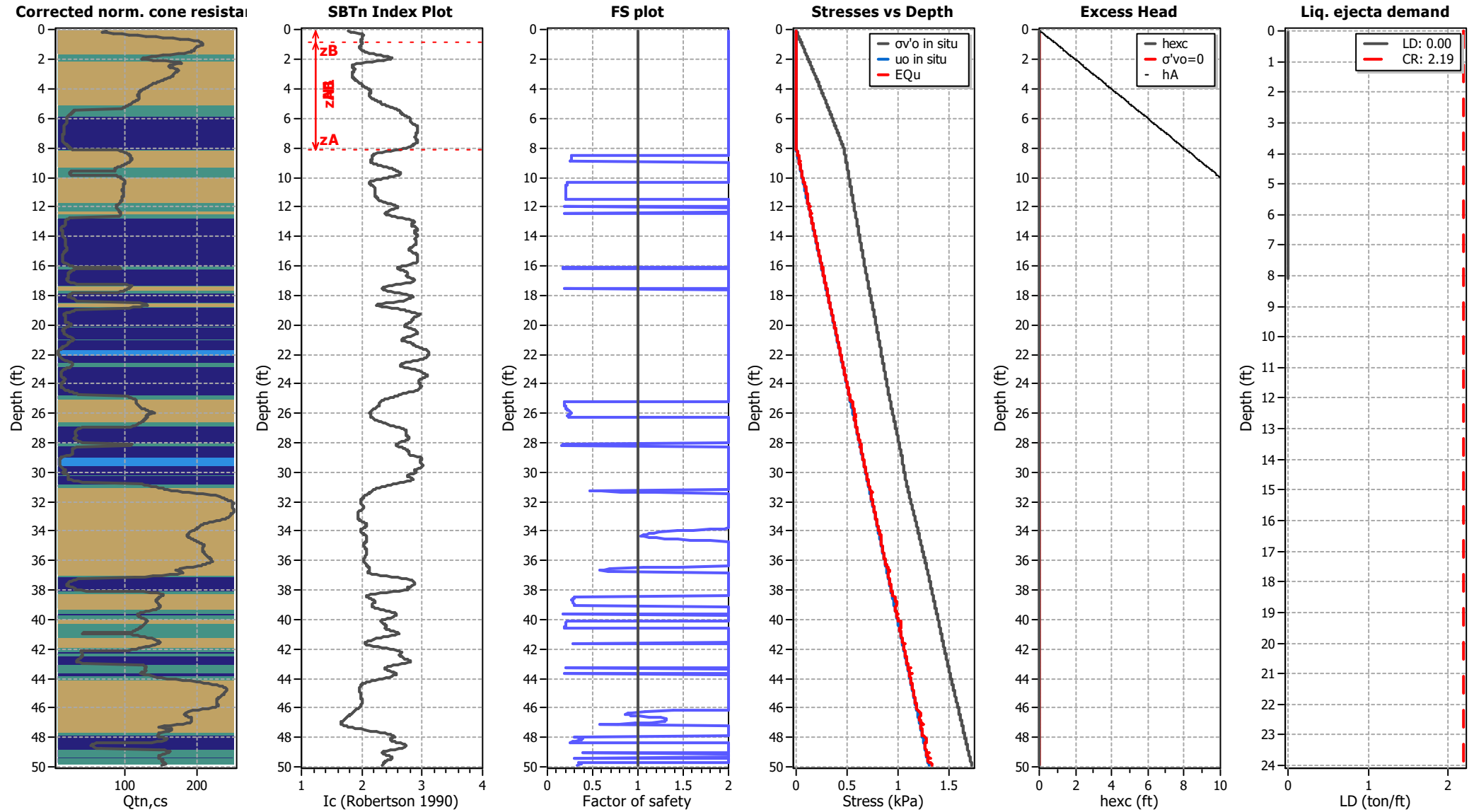
:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
48.05	104.45	64.31	3.00	193.12	2.50	0.19	0.83
48.10	106.59	65.79	2.89	190.05	2.49	0.20	0.84
48.15	106.99	66.10	2.82	186.27	2.48	0.20	0.84
48.20	104.22	64.19	2.87	184.38	2.48	0.19	0.83
48.25	100.01	61.25	3.01	184.19	2.50	0.18	0.83
48.30	93.91	56.98	3.27	186.32	2.54	0.17	0.82
48.35	87.69	52.66	3.60	189.36	2.58	0.16	0.81
48.40	81.23	48.17	4.03	194.16	2.63	0.15	0.66
48.45	76.48	44.84	4.47	200.28	2.68	0.14	0.65
48.50	73.37	42.61	4.88	207.76	2.72	0.14	0.64
48.55	72.59	41.95	5.09	213.46	2.74	0.14	0.64
48.60	73.49	42.43	5.11	216.91	2.74	0.14	0.64
48.65	76.28	44.22	4.87	215.57	2.72	0.15	0.65
48.70	81.36	47.58	4.45	211.56	2.67	0.15	0.66
48.75	88.11	52.18	3.88	202.68	2.62	0.16	0.68
48.80	96.50	57.97	3.31	191.96	2.55	0.17	0.82
48.85	104.19	63.46	2.82	178.92	2.48	0.19	0.83
48.90	110.71	68.23	2.45	167.17	2.41	0.20	0.84
48.95	113.99	70.82	2.22	157.06	2.37	0.20	0.84
49.00	114.88	71.66	2.09	150.09	2.34	0.20	0.84
49.05	113.12	70.53	2.08	146.41	2.34	0.19	0.84
49.10	110.32	68.53	2.13	145.75	2.35	0.19	0.83
49.15	106.45	65.67	2.26	148.28	2.38	0.18	0.83
49.20	102.97	63.02	2.43	153.06	2.41	0.17	0.83
49.25	99.99	60.66	2.65	160.67	2.45	0.17	0.82
49.30	98.58	59.41	2.83	168.36	2.48	0.17	0.82
49.35	98.15	58.85	2.98	175.16	2.50	0.17	0.82
49.40	98.96	59.27	2.99	177.28	2.50	0.17	0.82
49.45	100.29	60.15	2.92	175.55	2.49	0.18	0.83
49.50	102.24	61.57	2.76	169.89	2.47	0.18	0.83
49.55	103.75	62.76	2.60	162.96	2.44	0.18	0.83
49.60	104.70	63.62	2.44	154.97	2.41	0.18	0.83
49.65	105.55	64.37	2.32	149.05	2.39	0.18	0.83
49.70	106.91	65.36	2.23	146.04	2.37	0.18	0.83
49.75	109.29	66.93	2.18	146.21	2.36	0.18	0.83
49.80	110.81	67.91	2.15	146.33	2.36	0.19	0.84
49.85	110.25	67.58	2.13	143.64	2.35	0.19	0.84
49.90	108.66	66.55	2.11	140.65	2.35	0.18	0.83

Abbreviations

q_t :	Total cone resistance
K_c :	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c :	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

Ejecta Severity Estimation



LIQUEFACTION ANALYSIS REPORT

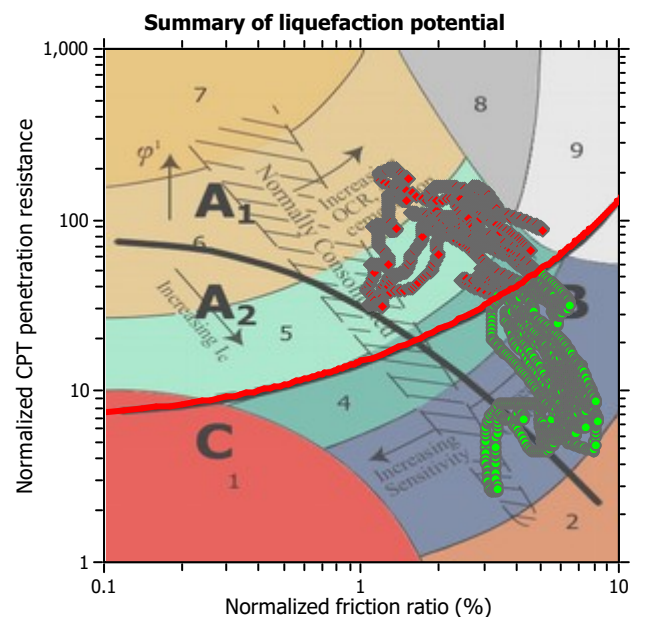
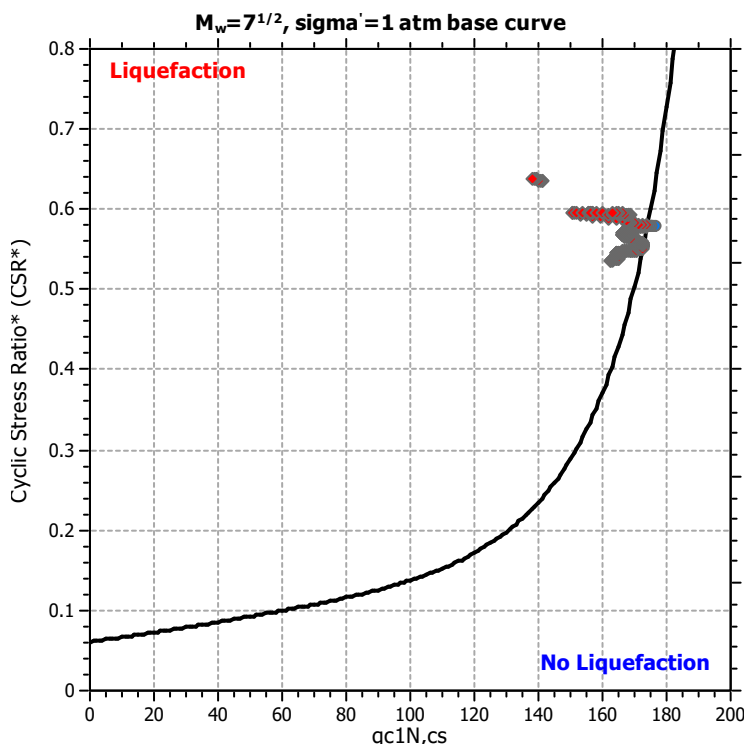
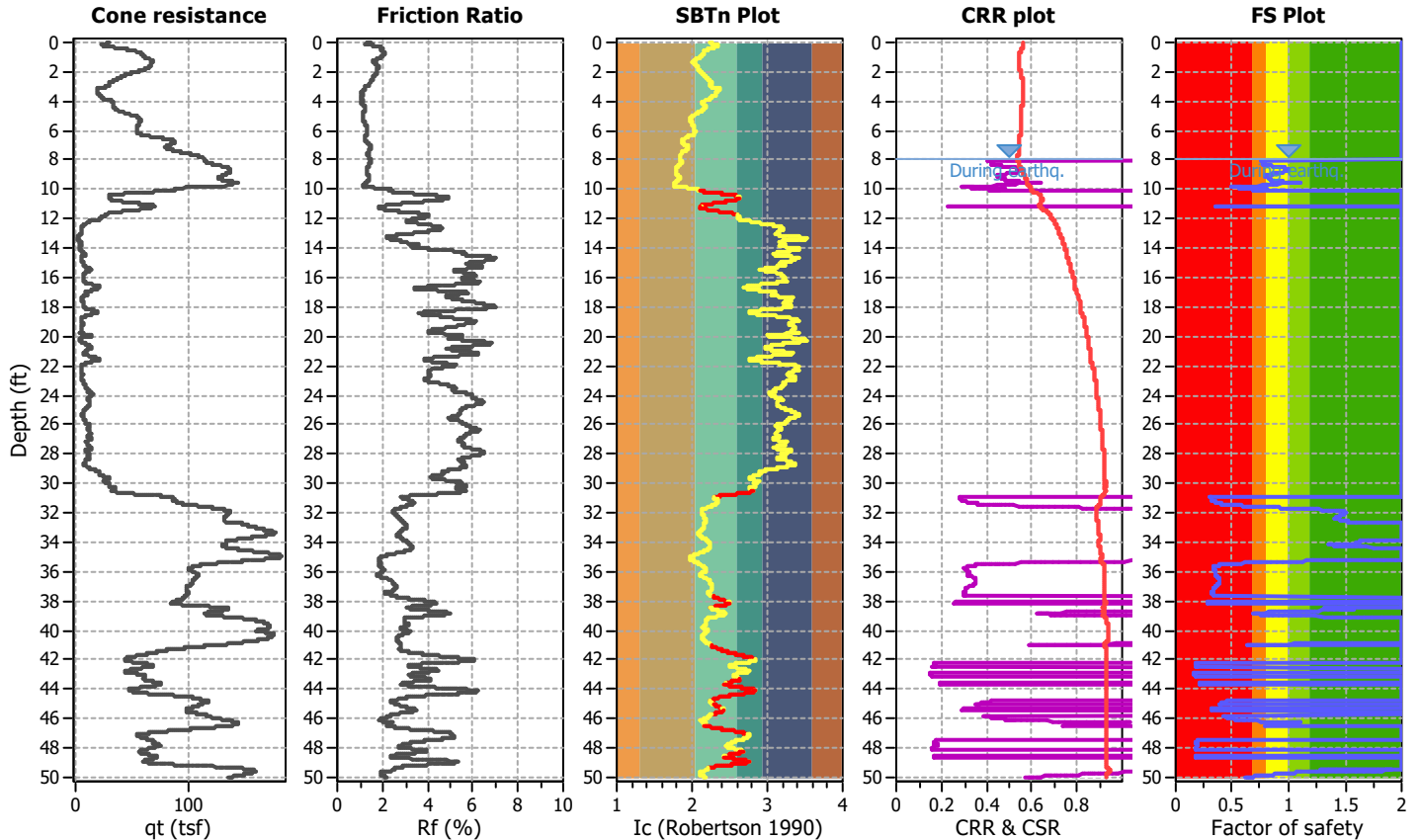
Project title : 21-483 Equestrian Estates

Location : Avenue 64 at Harrison Street, Thermal California

CPT file : CPT-2 B&I 2014

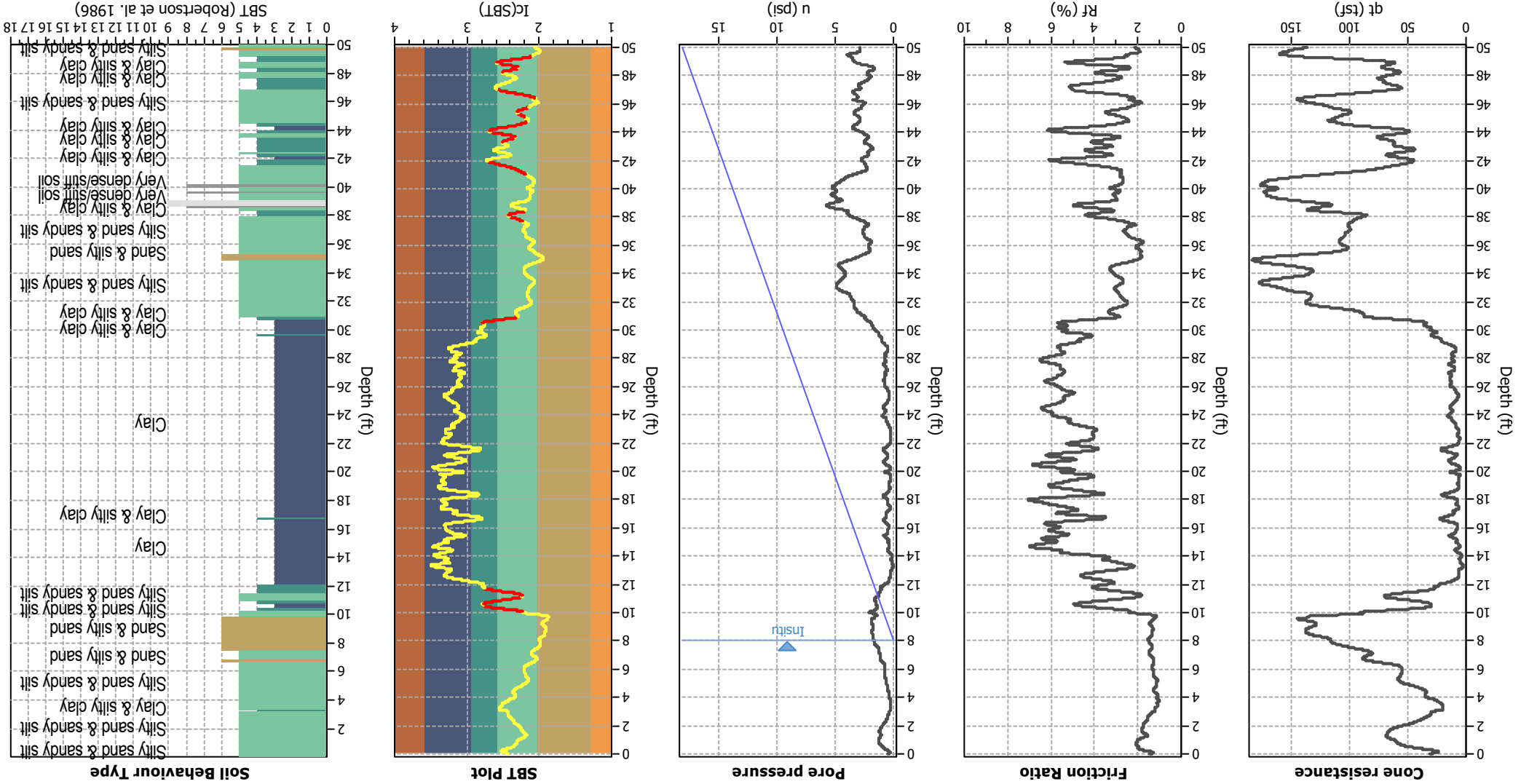
Input parameters and analysis data

Analysis method:	B&I (2014)	G.W.T. (in-situ):	8.00 ft	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	8.00 ft	Fill height:	N/A	Limit depth applied:	No
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth:	N/A
Earthquake magnitude M_w :	7.34	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.74	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		



Zone A₁: Cyclic liquefaction likely depending on size and duration of cyclic loading
 Zone A₂: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
 Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
 Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



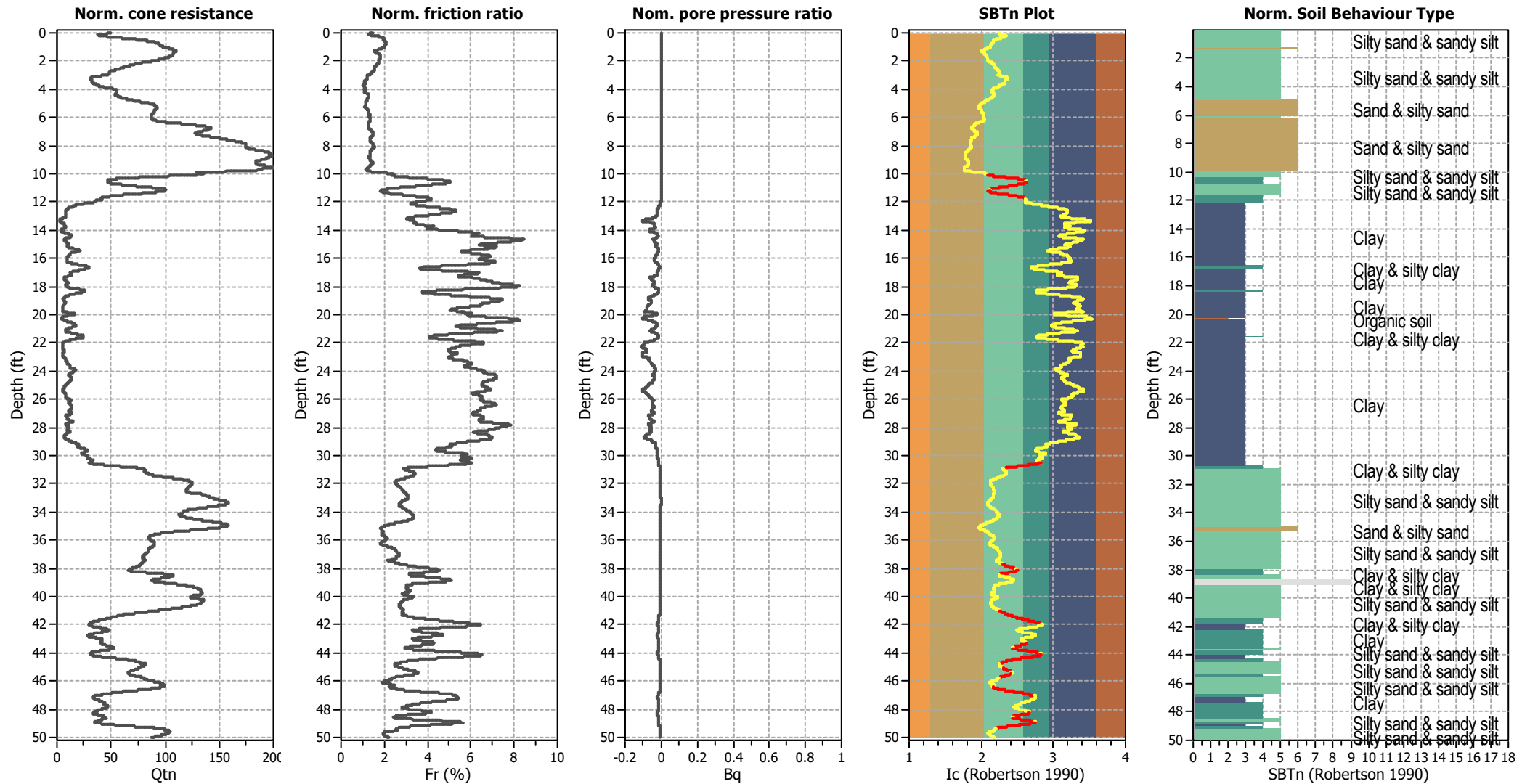
Input parameters and analysis data

Analysis method:	B&I (2014)
Fines correction method:	B&I (2014)
Points to test:	Based on Ic value
Earthquake magnitude M_w :	7.34
Peak ground acceleration:	0.74
Depth to water table (insitu):	8.00 ft

Depth to GWT (earthq.):	8.00 ft
Average results interval:	3
Ic cut-off value:	2.60
Unit weight calculation:	Based on SBT
Use fill:	No
Fill height:	N/A
Limit depth:	N/A
Limit depth applied:	No
Clay like behavior applied:	Sands only
K_p applied:	Yes
Transition detect. applied:	Yes
Fill weight:	N/A

SBT legend	
1. Sensitive fine grained	Red
2. Organic material	Green
3. Clay to silty clay	Blue
4. Clayey silt to silty	Orange
5. Silty sand to sandy silt	Light Green
6. Clean sand to silty sand	Light Blue
7. Gravely sand to sand	Dark Green
8. Very stiff sand to	Dark Blue
9. Very stiff fine grained	Dark Orange

CPT basic interpretation plots (normalized)



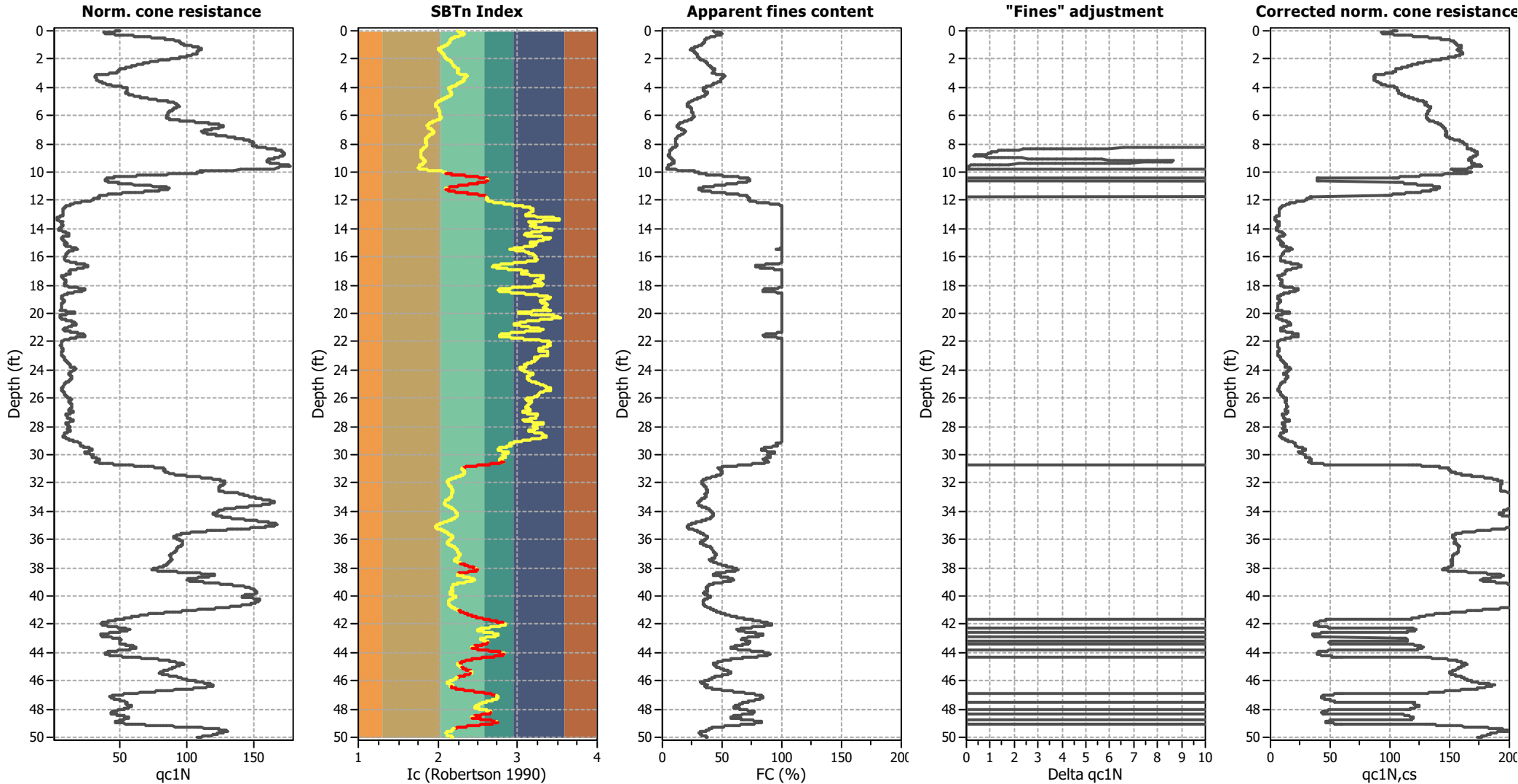
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	Yes
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

SBTn legend

1. Sensitive fine grained	4. Clayey silt to silty	7. Gravely sand to sand
2. Organic material	5. Silty sand to sandy silt	8. Very stiff sand to
3. Clay to silty clay	6. Clean sand to silty sand	9. Very stiff fine grained

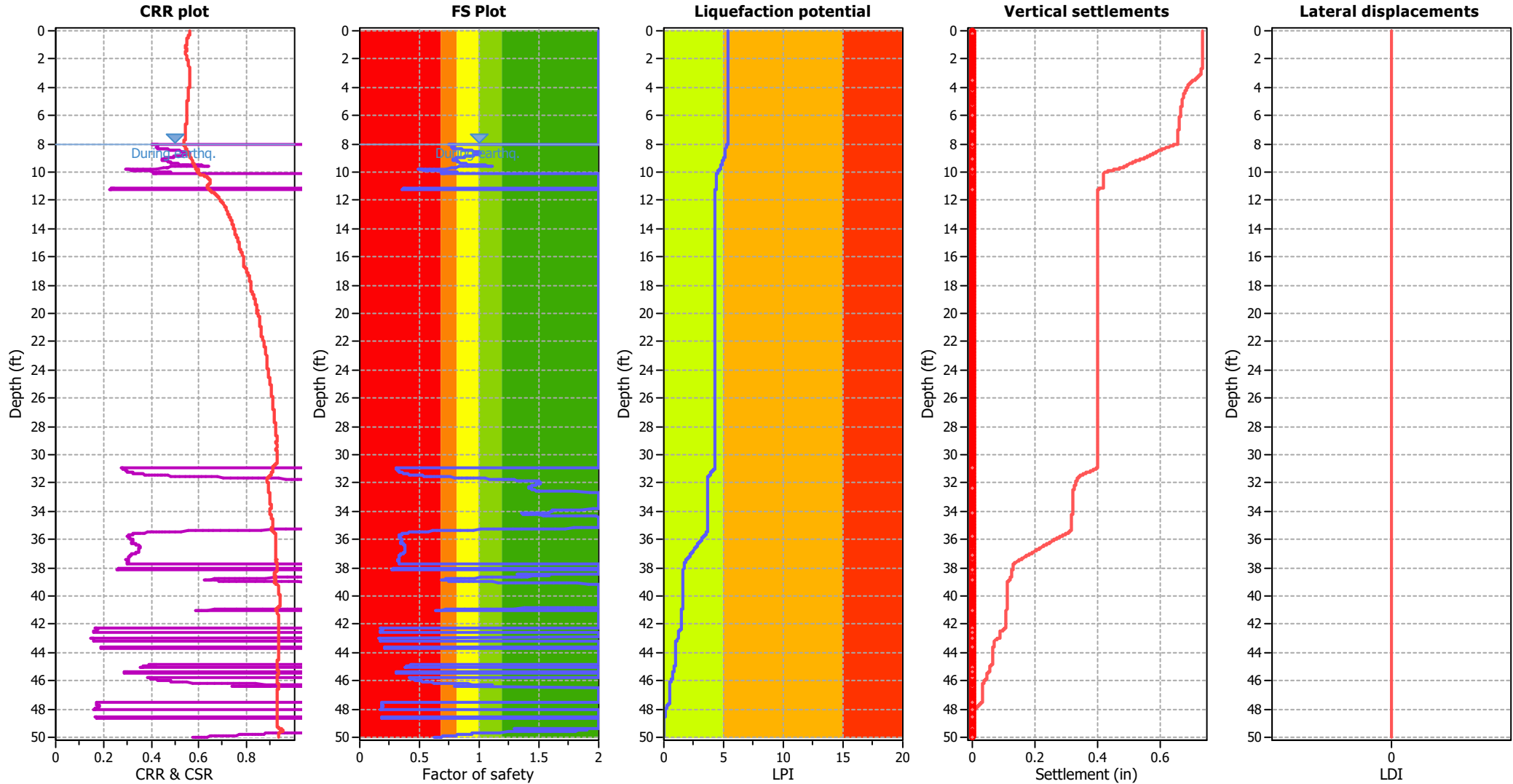
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on I_c value	I_c cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (earthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	Yes
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

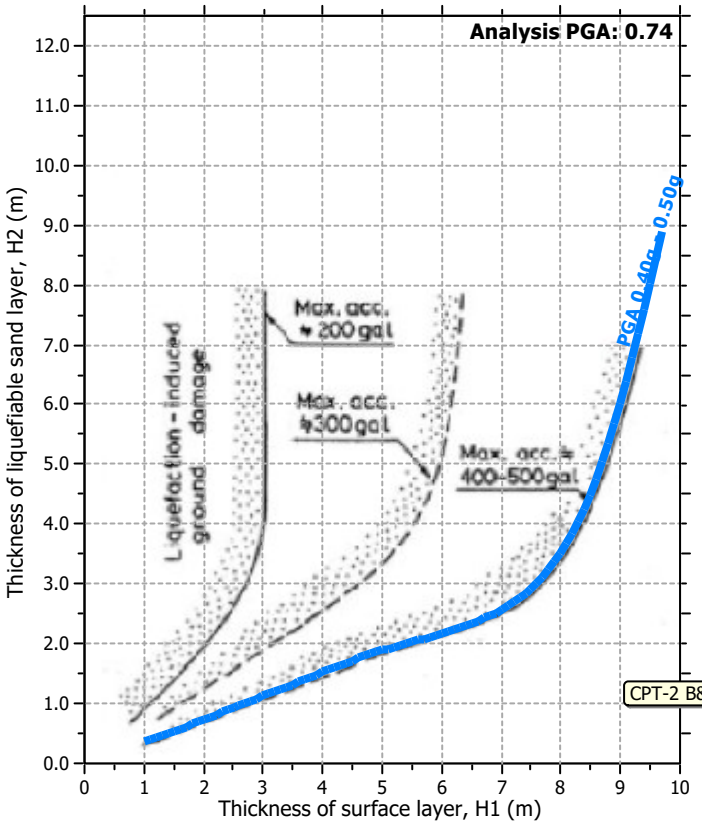
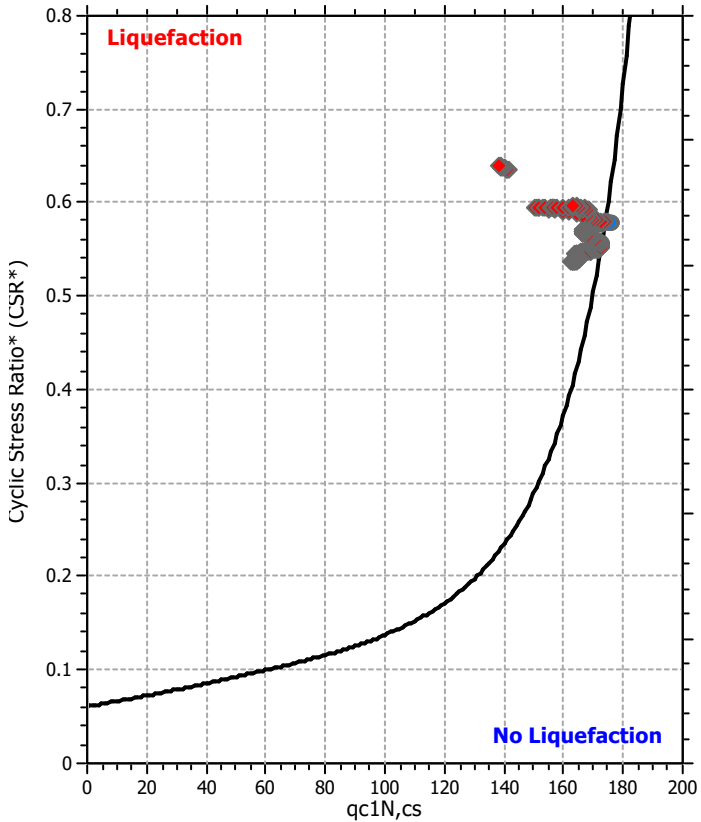
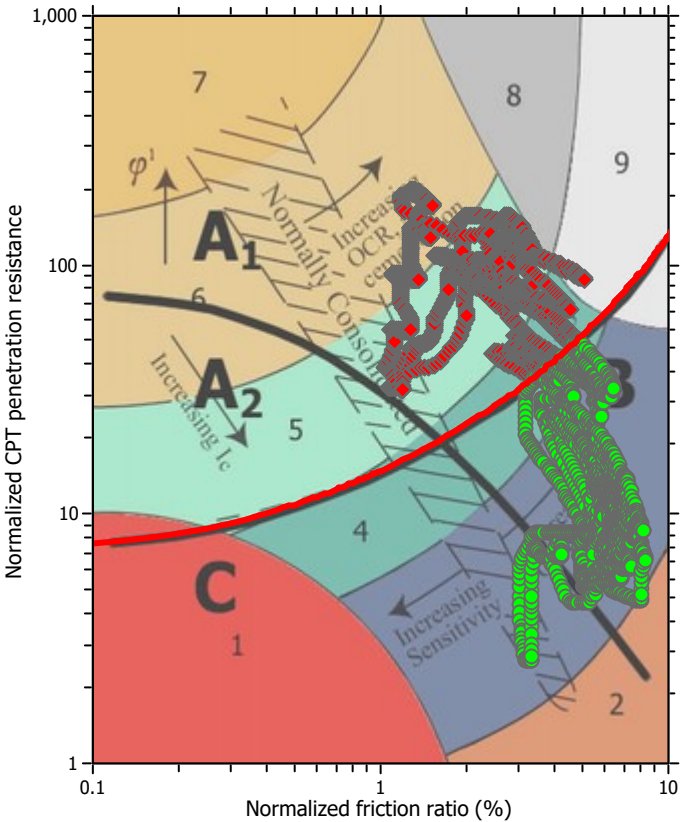
F.S. color scheme

Very high risk	Almost certain it will liquefy
High risk	Very likely to liquefy
Low risk	Liquefaction and no liq. are equally likely
	Unlike to liquefy
	Almost certain it will not liquefy

LPI color scheme

Very high risk
High risk
Low risk

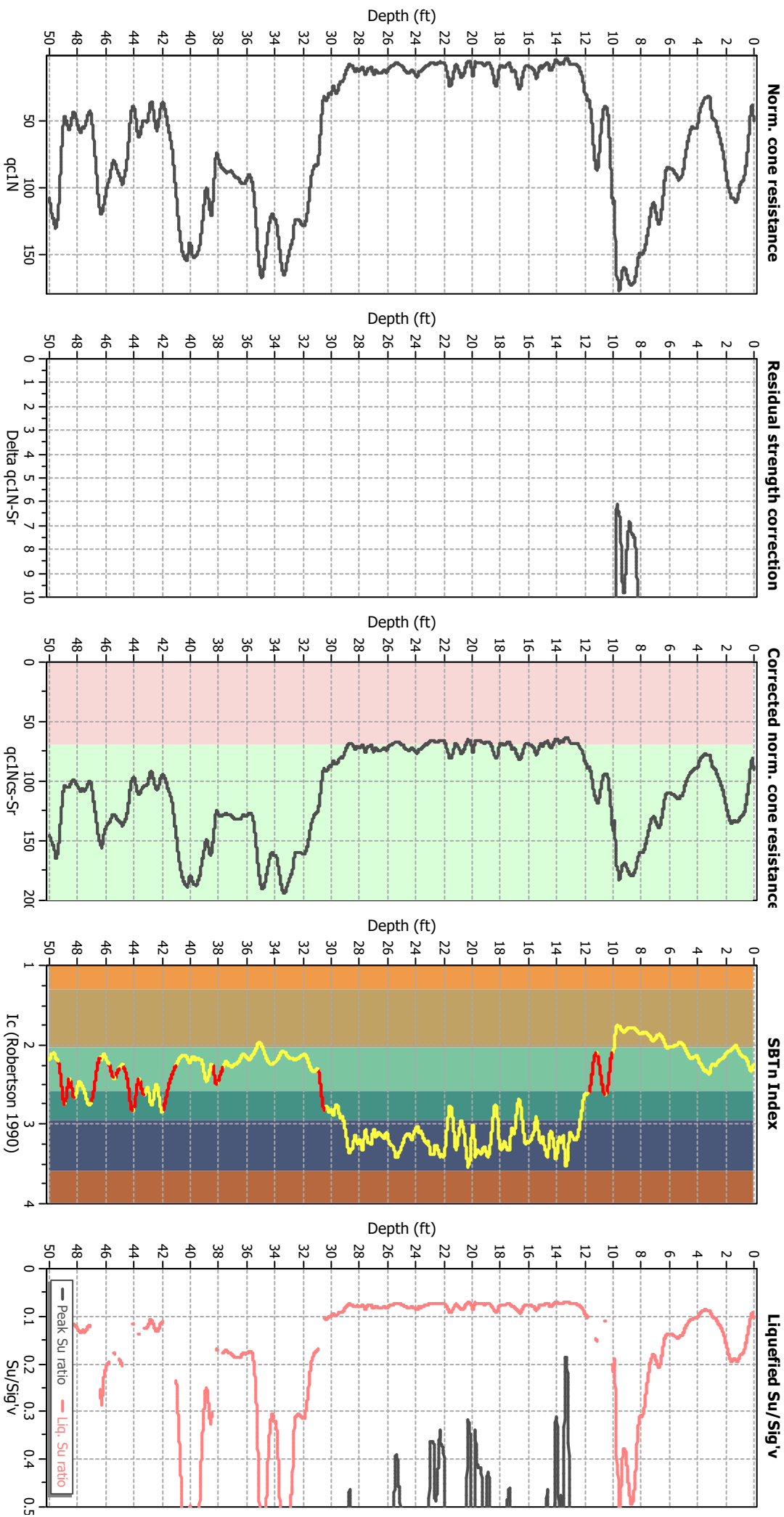
Liquefaction analysis summary plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on I_c value	I_c cut-off value:	2.60	K_o applied:	Yes
Earthquake magnitude M_w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

Check for strength loss plots (Idriss & Boulanger (2008))



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (ethq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	Yes
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (instn):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

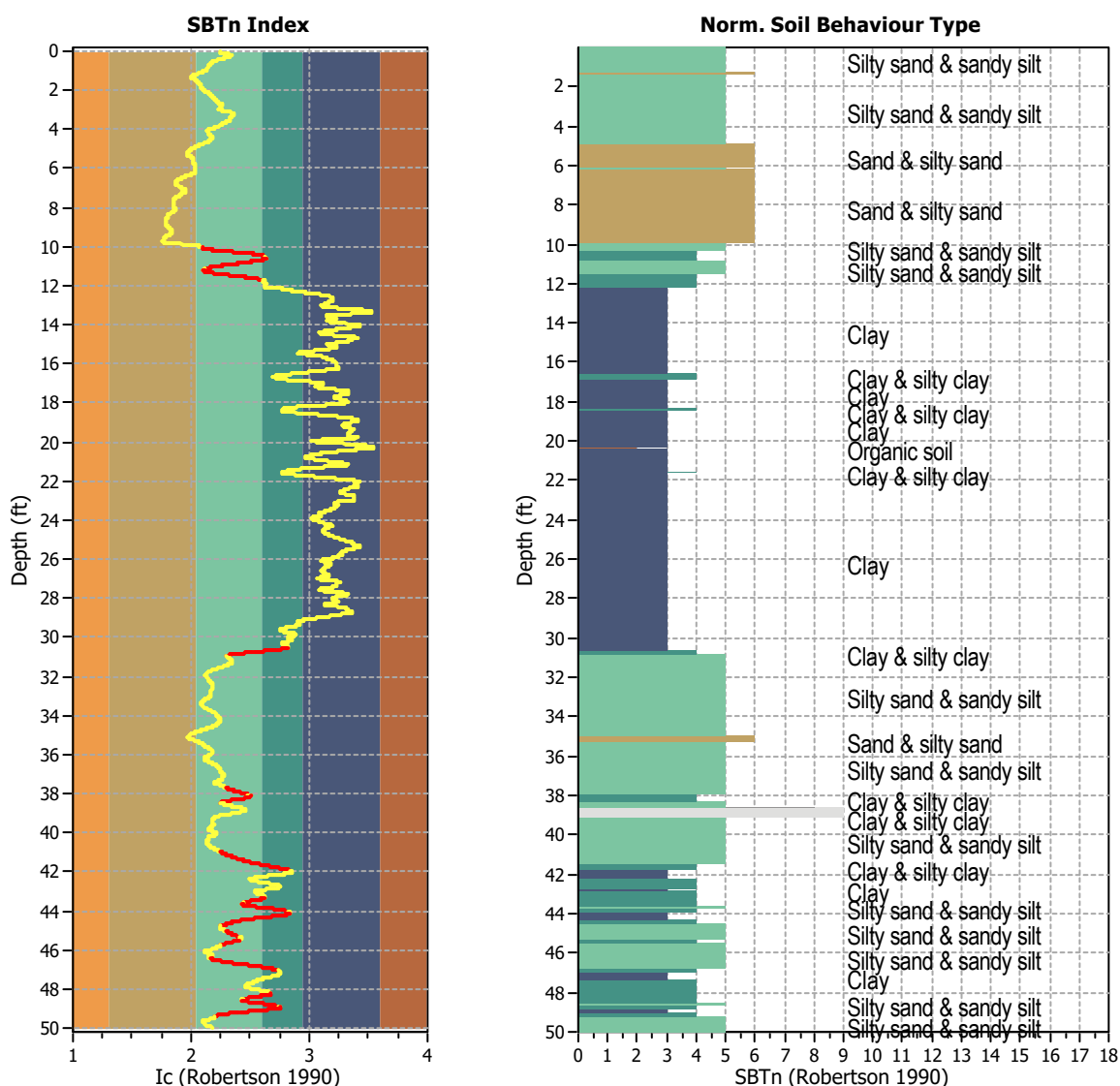
TRANSITION LAYER DETECTION ALGORITHM REPORT

Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vice-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between $1.80 < I_c < 3.0$) and a rate of change of I_c . Transitions typically occur when the rate of change of I_c is fast (i.e. ΔI_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties

I_c minimum check value: 1.70
 I_c maximum check value: 3.00
 I_c change ratio value: 0.0250
 Minimum number of points in layer: 4

General statistics

Total points in CPT file: 5000
 Total points excluded: 701
 Exclusion percentage: 14.02%
 Number of layers detected: 16

Transition layer No	Number of points	Depth	SBT _n number	SBT _n description
Transition layer 1	44	Start depth: 10.08 (ft)	5	Silty sand & sandy silt
		End depth: 10.51 (ft)	4	Clay & silty clay
Transition layer 2	52	Start depth: 10.62 (ft)	4	Clay & silty clay
		End depth: 11.13 (ft)	5	Silty sand & sandy silt
Transition layer 3	52	Start depth: 11.22 (ft)	5	Silty sand & sandy silt
		End depth: 11.73 (ft)	4	Clay & silty clay
Transition layer 4	43	Start depth: 30.53 (ft)	3	Clay
		End depth: 30.95 (ft)	5	Silty sand & sandy silt
Transition layer 5	36	Start depth: 37.71 (ft)	5	Silty sand & sandy silt
		End depth: 38.06 (ft)	4	Clay & silty clay
Transition layer 6	33	Start depth: 38.15 (ft)	4	Clay & silty clay
		End depth: 38.47 (ft)	5	Silty sand & sandy silt
Transition layer 7	94	Start depth: 41.02 (ft)	5	Silty sand & sandy silt
		End depth: 41.95 (ft)	3	Clay
Transition layer 8	27	Start depth: 43.34 (ft)	4	Clay & silty clay
		End depth: 43.60 (ft)	5	Silty sand & sandy silt
Transition layer 9	37	Start depth: 43.68 (ft)	5	Silty sand & sandy silt
		End depth: 44.04 (ft)	3	Clay
Transition layer 10	68	Start depth: 44.13 (ft)	3	Clay
		End depth: 44.80 (ft)	5	Silty sand & sandy silt
Transition layer 11	26	Start depth: 45.08 (ft)	5	Silty sand & sandy silt
		End depth: 45.33 (ft)	4	Clay & silty clay
Transition layer 12	27	Start depth: 45.50 (ft)	4	Clay & silty clay
		End depth: 45.76 (ft)	5	Silty sand & sandy silt
Transition layer 13	62	Start depth: 46.45 (ft)	5	Silty sand & sandy silt
		End depth: 47.06 (ft)	3	Clay
Transition layer 14	27	Start depth: 48.27 (ft)	4	Clay & silty clay
		End depth: 48.53 (ft)	5	Silty sand & sandy silt
Transition layer 15	28	Start depth: 48.62 (ft)	5	Silty sand & sandy silt
		End depth: 48.89 (ft)	3	Clay
Transition layer 16	45	Start depth: 48.96 (ft)	3	Clay
		End depth: 49.40 (ft)	5	Silty sand & sandy silt

Start depth: Depth where the transition layer begins

End depth: Depth where the transition layer ends

:: Field input data ::						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1	0.01	30.99	0.46	0.46	20.81	112.89
2	0.02	30.73	0.45	0.45	20.72	112.72
3	0.03	30.50	0.43	0.43	20.59	112.47
4	0.04	30.31	0.42	0.42	20.52	112.24
5	0.05	29.88	0.41	0.41	20.57	111.99
6	0.06	29.16	0.40	0.40	20.75	111.69
7	0.07	28.32	0.38	0.38	20.99	111.32
8	0.08	27.40	0.36	0.36	21.27	110.90
9	0.09	26.45	0.34	0.34	21.57	110.46
10	0.10	25.52	0.33	0.33	21.89	110.01
11	0.11	24.65	0.31	0.31	22.21	109.58
12	0.12	23.89	0.30	0.30	22.50	109.19
13	0.13	23.29	0.29	0.29	22.73	109.03
14	0.14	23.42	0.30	0.30	22.92	109.09
15	0.15	23.58	0.31	0.31	23.09	109.35
16	0.16	23.76	0.32	0.32	23.28	109.65
17	0.17	23.96	0.33	0.33	23.47	109.96
18	0.18	24.16	0.35	0.35	23.66	110.26
19	0.19	24.35	0.36	0.36	23.85	110.55
20	0.20	24.53	0.37	0.37	24.01	110.81
21	0.21	24.68	0.38	0.38	24.12	111.04
22	0.22	24.93	0.39	0.39	24.13	111.32
23	0.23	25.55	0.41	0.41	24.04	111.66
24	0.24	26.30	0.43	0.43	23.88	112.10
25	0.25	27.14	0.45	0.45	23.72	112.57
26	0.26	28.02	0.48	0.48	23.56	113.05
27	0.27	28.90	0.51	0.51	23.41	113.51
28	0.28	29.73	0.53	0.53	23.27	113.94
29	0.29	30.48	0.56	0.56	23.16	114.32
30	0.30	31.09	0.58	0.58	23.05	114.62
31	0.31	31.65	0.59	0.59	22.90	114.89
32	0.32	32.38	0.61	0.61	22.70	115.16
33	0.33	33.24	0.63	0.63	22.46	115.47
34	0.34	34.18	0.65	0.65	22.21	115.79
35	0.35	35.15	0.68	0.68	21.97	116.12
36	0.36	36.10	0.70	0.70	21.74	116.43
37	0.37	36.98	0.73	0.73	21.53	116.72
38	0.38	37.75	0.75	0.75	21.36	116.96
39	0.39	38.36	0.76	0.76	21.20	117.16
40	0.40	38.98	0.77	0.77	21.01	117.33
41	0.41	39.75	0.79	0.79	20.77	117.51
42	0.42	40.64	0.80	0.80	20.52	117.71
43	0.43	41.58	0.82	0.82	20.25	117.92
44	0.44	42.54	0.84	0.84	19.98	118.12
45	0.45	43.47	0.86	0.86	19.74	118.32
46	0.46	44.32	0.87	0.87	19.52	118.49
47	0.47	45.03	0.88	0.88	19.34	118.64
48	0.48	45.57	0.89	0.89	19.20	118.78

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
49	0.49	46.14	0.91	0.91	19.08	118.92
50	0.50	46.83	0.92	0.92	18.95	119.08
51	0.51	47.61	0.94	0.94	18.81	119.26
52	0.52	48.42	0.96	0.96	18.67	119.44
53	0.53	49.22	0.98	0.98	18.53	119.62
54	0.54	49.99	1.00	1.00	18.41	119.79
55	0.55	50.67	1.01	1.01	18.30	119.94
56	0.56	51.23	1.03	1.03	18.21	120.06
57	0.57	51.63	1.04	1.04	18.15	120.17
58	0.58	52.08	1.05	1.05	18.09	120.29
59	0.59	52.61	1.07	1.07	18.03	120.41
60	0.60	53.19	1.08	1.08	17.97	120.55
61	0.61	53.79	1.10	1.10	17.91	120.69
62	0.62	54.37	1.12	1.12	17.85	120.83
63	0.63	54.92	1.13	1.13	17.79	120.95
64	0.64	55.39	1.15	1.15	17.74	121.06
65	0.65	55.75	1.16	1.16	17.71	121.14
66	0.66	55.95	1.16	1.16	17.68	121.20
67	0.67	56.19	1.17	1.17	17.65	121.25
68	0.68	56.46	1.18	1.18	17.61	121.31
69	0.69	56.76	1.19	1.19	17.58	121.37
70	0.70	57.06	1.19	1.19	17.54	121.43
71	0.71	57.34	1.20	1.20	17.51	121.49
72	0.72	57.61	1.21	1.21	17.48	121.54
73	0.73	57.83	1.21	1.21	17.45	121.58
74	0.74	57.97	1.22	1.22	17.43	121.61
75	0.75	58.06	1.22	1.22	17.40	121.62
76	0.76	58.18	1.22	1.22	17.37	121.63
77	0.77	58.31	1.22	1.22	17.34	121.64
78	0.78	58.44	1.22	1.22	17.30	121.65
79	0.79	58.58	1.22	1.22	17.26	121.66
80	0.80	58.70	1.22	1.22	17.23	121.67
81	0.81	58.82	1.22	1.22	17.20	121.68
82	0.82	58.91	1.22	1.22	17.17	121.69
83	0.83	58.98	1.22	1.22	17.14	121.69
84	0.84	59.06	1.22	1.22	17.11	121.69
85	0.85	59.16	1.22	1.22	17.07	121.68
86	0.86	59.26	1.22	1.22	17.02	121.68
87	0.87	59.37	1.22	1.22	16.97	121.68
88	0.88	59.48	1.22	1.22	16.93	121.67
89	0.89	59.58	1.21	1.21	16.89	121.67
90	0.90	59.66	1.21	1.21	16.85	121.66
91	0.91	59.73	1.21	1.21	16.81	121.66
92	0.92	59.84	1.21	1.21	16.78	121.66
93	0.93	59.97	1.21	1.21	16.73	121.66
94	0.94	60.12	1.21	1.21	16.68	121.67
95	0.95	60.28	1.21	1.21	16.63	121.67
96	0.96	60.45	1.21	1.21	16.57	121.67

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
97	0.97	60.60	1.21	1.21	16.52	121.68
98	0.98	60.75	1.21	1.21	16.47	121.68
99	0.99	60.87	1.21	1.21	16.43	121.68
100	1.00	61.03	1.21	1.21	16.37	121.69
101	1.01	61.33	1.21	1.21	16.28	121.70
102	1.02	61.69	1.21	1.21	16.18	121.72
103	1.03	62.09	1.21	1.21	16.06	121.74
104	1.04	62.51	1.21	1.21	15.94	121.75
105	1.05	62.93	1.21	1.21	15.82	121.77
106	1.06	63.33	1.21	1.21	15.70	121.79
107	1.07	63.68	1.21	1.21	15.60	121.80
108	1.08	63.97	1.21	1.21	15.51	121.81
109	1.09	64.20	1.21	1.21	15.42	121.80
110	1.10	64.48	1.20	1.20	15.31	121.79
111	1.11	64.81	1.20	1.20	15.18	121.77
112	1.12	65.16	1.19	1.19	15.05	121.75
113	1.13	65.53	1.19	1.19	14.90	121.73
114	1.14	65.89	1.18	1.18	14.76	121.71
115	1.15	66.22	1.18	1.18	14.64	121.69
116	1.16	66.51	1.17	1.17	14.52	121.67
117	1.17	66.73	1.17	1.17	14.42	121.64
118	1.18	66.88	1.16	1.16	14.32	121.61
119	1.19	67.06	1.15	1.15	14.21	121.56
120	1.20	67.27	1.14	1.14	14.08	121.50
121	1.21	67.50	1.13	1.13	13.94	121.44
122	1.22	67.73	1.12	1.12	13.80	121.37
123	1.23	67.95	1.11	1.11	13.66	121.31
124	1.24	68.14	1.10	1.10	13.54	121.25
125	1.25	68.31	1.09	1.09	13.44	121.21
126	1.26	68.39	1.08	1.08	13.38	121.17
127	1.27	68.40	1.08	1.08	13.34	121.15
128	1.28	68.41	1.08	1.08	13.31	121.13
129	1.29	68.43	1.07	1.07	13.28	121.10
130	1.30	68.44	1.07	1.07	13.24	121.07
131	1.31	68.45	1.07	1.07	13.21	121.04
132	1.32	68.46	1.06	1.06	13.17	121.02
133	1.33	68.48	1.06	1.06	13.14	121.00
134	1.34	68.49	1.06	1.06	13.14	120.99
135	1.35	68.38	1.06	1.06	13.17	120.99
136	1.36	68.21	1.06	1.06	13.24	121.01
137	1.37	68.02	1.07	1.07	13.32	121.04
138	1.38	67.81	1.07	1.07	13.41	121.06
139	1.39	67.59	1.08	1.08	13.51	121.09
140	1.40	67.38	1.08	1.08	13.60	121.11
141	1.41	67.18	1.09	1.09	13.68	121.14
142	1.42	67.01	1.09	1.09	13.75	121.16
143	1.43	66.89	1.09	1.09	13.81	121.18
144	1.44	66.88	1.10	1.10	13.87	121.22

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
145	1.45	66.87	1.11	1.11	13.92	121.26
146	1.46	66.86	1.11	1.11	13.98	121.31
147	1.47	66.85	1.12	1.12	14.05	121.36
148	1.48	66.83	1.13	1.13	14.12	121.41
149	1.49	66.82	1.14	1.14	14.18	121.46
150	1.50	66.81	1.14	1.14	14.24	121.51
151	1.51	66.80	1.15	1.15	14.28	121.55
152	1.52	66.79	1.16	1.16	14.33	121.58
153	1.53	66.77	1.16	1.16	14.37	121.60
154	1.54	66.74	1.16	1.16	14.41	121.63
155	1.55	66.72	1.17	1.17	14.46	121.67
156	1.56	66.69	1.18	1.18	14.51	121.70
157	1.57	66.66	1.18	1.18	14.56	121.74
158	1.58	66.64	1.19	1.19	14.61	121.77
159	1.59	66.62	1.19	1.19	14.65	121.80
160	1.60	66.60	1.20	1.20	14.68	121.81
161	1.61	66.47	1.20	1.20	14.72	121.81
162	1.62	66.28	1.19	1.19	14.76	121.80
163	1.63	66.07	1.19	1.19	14.80	121.78
164	1.64	65.83	1.19	1.19	14.85	121.75
165	1.65	65.58	1.19	1.19	14.89	121.73
166	1.66	65.34	1.18	1.18	14.94	121.71
167	1.67	65.12	1.18	1.18	14.99	121.69
168	1.68	64.93	1.18	1.18	15.02	121.67
169	1.69	64.78	1.18	1.18	15.05	121.65
170	1.70	64.62	1.18	1.18	15.08	121.63
171	1.71	64.42	1.17	1.17	15.11	121.60
172	1.72	64.19	1.17	1.17	15.14	121.56
173	1.73	63.95	1.16	1.16	15.17	121.53
174	1.74	63.71	1.16	1.16	15.21	121.49
175	1.75	63.47	1.16	1.16	15.24	121.45
176	1.76	63.26	1.15	1.15	15.27	121.42
177	1.77	63.09	1.15	1.15	15.29	121.39
178	1.78	62.92	1.14	1.14	15.31	121.35
179	1.79	62.68	1.14	1.14	15.32	121.30
180	1.80	62.39	1.13	1.13	15.34	121.23
181	1.81	62.07	1.12	1.12	15.35	121.16
182	1.82	61.74	1.11	1.11	15.37	121.09
183	1.83	61.42	1.10	1.10	15.39	121.01
184	1.84	61.11	1.09	1.09	15.40	120.94
185	1.85	60.83	1.08	1.08	15.42	120.87
186	1.86	60.61	1.08	1.08	15.43	120.81
187	1.87	60.36	1.07	1.07	15.45	120.75
188	1.88	60.02	1.06	1.06	15.48	120.68
189	1.89	59.63	1.05	1.05	15.51	120.59
190	1.90	59.20	1.04	1.04	15.54	120.50
191	1.91	58.77	1.03	1.03	15.58	120.40
192	1.92	58.35	1.02	1.02	15.61	120.31

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
193	1.93	57.96	1.01	1.01	15.64	120.22
194	1.94	57.62	1.00	1.00	15.67	120.14
195	1.95	57.35	0.99	0.99	15.71	120.08
196	1.96	57.00	0.98	0.98	15.77	120.01
197	1.97	56.56	0.98	0.98	15.84	119.94
198	1.98	56.08	0.97	0.97	15.92	119.86
199	1.99	55.56	0.96	0.96	16.00	119.77
200	2.00	55.04	0.95	0.95	16.09	119.68
201	2.01	54.54	0.94	0.94	16.18	119.59
202	2.02	54.08	0.93	0.93	16.26	119.51
203	2.03	53.71	0.93	0.93	16.33	119.44
204	2.04	53.37	0.92	0.92	16.40	119.37
205	2.05	52.91	0.91	0.91	16.48	119.29
206	2.06	52.37	0.90	0.90	16.58	119.19
207	2.07	51.77	0.89	0.89	16.69	119.08
208	2.08	51.15	0.88	0.88	16.81	118.96
209	2.09	50.53	0.87	0.87	16.93	118.85
210	2.10	49.95	0.86	0.86	17.05	118.74
211	2.11	49.44	0.85	0.85	17.15	118.64
212	2.12	49.03	0.85	0.85	17.23	118.55
213	2.13	48.72	0.84	0.84	17.29	118.47
214	2.14	48.34	0.83	0.83	17.34	118.37
215	2.15	47.89	0.82	0.82	17.40	118.26
216	2.16	47.42	0.81	0.81	17.47	118.14
217	2.17	46.93	0.80	0.80	17.54	118.01
218	2.18	46.45	0.79	0.79	17.61	117.88
219	2.19	46.01	0.78	0.78	17.68	117.77
220	2.20	45.64	0.77	0.77	17.74	117.67
221	2.21	45.35	0.76	0.76	17.78	117.59
222	2.22	45.10	0.76	0.76	17.82	117.51
223	2.23	44.79	0.75	0.75	17.87	117.42
224	2.24	44.44	0.74	0.74	17.92	117.32
225	2.25	44.07	0.73	0.73	17.97	117.21
226	2.26	43.70	0.72	0.72	18.02	117.10
227	2.27	43.34	0.71	0.71	18.07	116.99
228	2.28	43.02	0.71	0.71	18.12	116.90
229	2.29	42.75	0.70	0.70	18.16	116.82
230	2.30	42.54	0.69	0.69	18.20	116.74
231	2.31	42.29	0.69	0.69	18.24	116.66
232	2.32	41.99	0.68	0.68	18.28	116.57
233	2.33	41.66	0.67	0.67	18.33	116.47
234	2.34	41.32	0.66	0.66	18.38	116.36
235	2.35	40.98	0.66	0.66	18.43	116.26
236	2.36	40.67	0.65	0.65	18.48	116.15
237	2.37	40.39	0.64	0.64	18.53	116.07
238	2.38	40.16	0.64	0.64	18.56	115.99
239	2.39	39.99	0.63	0.63	18.59	115.92
240	2.40	39.77	0.63	0.63	18.63	115.84

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
241	2.41	39.52	0.62	0.62	18.66	115.76
242	2.42	39.25	0.61	0.61	18.70	115.66
243	2.43	38.97	0.61	0.61	18.74	115.57
244	2.44	38.70	0.60	0.60	18.78	115.47
245	2.45	38.45	0.60	0.60	18.82	115.38
246	2.46	38.24	0.59	0.59	18.85	115.31
247	2.47	38.07	0.59	0.59	18.89	115.25
248	2.48	37.89	0.58	0.58	18.94	115.19
249	2.49	37.67	0.58	0.58	19.01	115.14
250	2.50	37.42	0.58	0.58	19.08	115.07
251	2.51	37.15	0.57	0.57	19.16	115.00
252	2.52	36.88	0.57	0.57	19.24	114.94
253	2.53	36.63	0.56	0.56	19.32	114.87
254	2.54	36.40	0.56	0.56	19.39	114.81
255	2.55	36.20	0.56	0.56	19.45	114.75
256	2.56	36.01	0.55	0.55	19.52	114.69
257	2.57	35.74	0.55	0.55	19.59	114.60
258	2.58	35.41	0.54	0.54	19.68	114.50
259	2.59	35.05	0.54	0.54	19.78	114.39
260	2.60	34.68	0.53	0.53	19.88	114.27
261	2.61	34.31	0.52	0.52	19.98	114.16
262	2.62	33.96	0.52	0.52	20.08	114.04
263	2.63	33.65	0.51	0.51	20.17	113.95
264	2.64	33.41	0.51	0.51	20.25	113.86
265	2.65	33.18	0.50	0.50	20.32	113.77
266	2.66	32.89	0.50	0.50	20.39	113.66
267	2.67	32.56	0.49	0.49	20.47	113.53
268	2.68	32.20	0.48	0.48	20.57	113.40
269	2.69	31.84	0.47	0.47	20.66	113.26
270	2.70	31.48	0.47	0.47	20.76	113.12
271	2.71	31.15	0.46	0.46	20.85	112.99
272	2.72	30.87	0.45	0.45	20.92	112.89
273	2.73	30.70	0.45	0.45	20.96	112.81
274	2.74	30.67	0.45	0.45	20.96	112.77
275	2.75	30.65	0.45	0.45	20.93	112.73
276	2.76	30.62	0.45	0.45	20.91	112.69
277	2.77	30.58	0.44	0.44	20.88	112.65
278	2.78	30.55	0.44	0.44	20.85	112.61
279	2.79	30.52	0.44	0.44	20.83	112.57
280	2.80	30.49	0.44	0.44	20.80	112.53
281	2.81	30.47	0.43	0.43	20.78	112.50
282	2.82	30.45	0.43	0.43	20.76	112.48
283	2.83	30.43	0.43	0.43	20.74	112.44
284	2.84	30.41	0.43	0.43	20.71	112.41
285	2.85	30.38	0.43	0.43	20.69	112.37
286	2.86	30.35	0.42	0.42	20.66	112.33
287	2.87	30.33	0.42	0.42	20.63	112.29
288	2.88	30.30	0.42	0.42	20.60	112.25

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
289	2.89	30.28	0.42	0.42	20.57	112.22
290	2.90	30.26	0.42	0.42	20.55	112.17
291	2.91	30.20	0.41	0.41	20.52	112.12
292	2.92	30.11	0.41	0.41	20.49	112.04
293	2.93	30.01	0.40	0.40	20.45	111.95
294	2.94	29.91	0.40	0.40	20.41	111.84
295	2.95	29.80	0.39	0.39	20.37	111.74
296	2.96	29.69	0.39	0.39	20.33	111.64
297	2.97	29.60	0.38	0.38	20.29	111.55
298	2.98	29.51	0.38	0.38	20.27	111.46
299	2.99	29.37	0.38	0.38	20.30	111.33
300	3.00	28.95	0.37	0.37	20.39	111.16
301	3.01	28.42	0.36	0.36	20.54	110.93
302	3.02	27.84	0.35	0.35	20.72	110.66
303	3.03	27.22	0.34	0.34	20.90	110.37
304	3.04	26.60	0.33	0.33	21.10	110.07
305	3.05	26.00	0.32	0.32	21.30	109.79
306	3.06	25.47	0.31	0.31	21.48	109.53
307	3.07	25.03	0.30	0.30	21.66	109.30
308	3.08	24.63	0.29	0.29	21.87	109.10
309	3.09	24.11	0.29	0.29	22.14	108.89
310	3.10	23.49	0.28	0.28	22.49	108.64
311	3.11	22.81	0.27	0.27	22.88	108.36
312	3.12	22.10	0.26	0.26	23.30	108.05
313	3.13	21.41	0.25	0.25	23.74	107.75
314	3.14	20.76	0.25	0.25	24.16	107.45
315	3.15	20.19	0.24	0.24	24.55	107.19
316	3.16	19.73	0.23	0.23	24.81	107.02
317	3.17	19.71	0.23	0.23	24.92	106.94
318	3.18	19.71	0.23	0.23	24.93	106.93
319	3.19	19.71	0.23	0.23	24.93	106.93
320	3.20	19.71	0.23	0.23	24.93	106.93
321	3.21	19.71	0.23	0.23	24.93	106.93
322	3.22	19.71	0.23	0.23	24.93	106.93
323	3.23	19.71	0.23	0.23	24.93	106.93
324	3.24	19.71	0.23	0.23	24.93	106.93
325	3.25	19.72	0.23	0.23	24.89	106.93
326	3.26	19.78	0.23	0.23	24.81	106.92
327	3.27	19.85	0.23	0.23	24.70	106.90
328	3.28	19.92	0.23	0.23	24.58	106.88
329	3.29	20.00	0.23	0.23	24.45	106.86
330	3.30	20.09	0.23	0.23	24.31	106.84
331	3.31	20.16	0.23	0.23	24.19	106.82
332	3.32	20.23	0.23	0.23	24.08	106.80
333	3.33	20.29	0.23	0.23	23.99	106.78
334	3.34	20.31	0.23	0.23	23.92	106.75
335	3.35	20.31	0.23	0.23	23.86	106.71
336	3.36	20.31	0.22	0.22	23.79	106.65

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
337	3.37	20.31	0.22	0.22	23.72	106.59
338	3.38	20.31	0.22	0.22	23.64	106.53
339	3.39	20.31	0.22	0.22	23.57	106.47
340	3.40	20.31	0.22	0.22	23.50	106.41
341	3.41	20.31	0.21	0.21	23.43	106.36
342	3.42	20.31	0.21	0.21	23.40	106.33
343	3.43	20.31	0.21	0.21	23.40	106.33
344	3.44	20.31	0.21	0.21	23.42	106.34
345	3.45	20.31	0.21	0.21	23.44	106.36
346	3.46	20.31	0.22	0.22	23.47	106.38
347	3.47	20.31	0.22	0.22	23.49	106.40
348	3.48	20.31	0.22	0.22	23.52	106.43
349	3.49	20.31	0.22	0.22	23.54	106.44
350	3.50	20.31	0.22	0.22	23.56	106.47
351	3.51	20.34	0.22	0.22	23.55	106.51
352	3.52	20.45	0.22	0.22	23.52	106.58
353	3.53	20.59	0.22	0.22	23.47	106.68
354	3.54	20.74	0.23	0.23	23.42	106.79
355	3.55	20.90	0.23	0.23	23.36	106.91
356	3.56	21.06	0.23	0.23	23.31	107.02
357	3.57	21.22	0.24	0.24	23.26	107.13
358	3.58	21.35	0.24	0.24	23.21	107.23
359	3.59	21.47	0.24	0.24	23.15	107.31
360	3.60	21.60	0.24	0.24	23.06	107.37
361	3.61	21.78	0.24	0.24	22.92	107.42
362	3.62	22.00	0.24	0.24	22.74	107.48
363	3.63	22.23	0.24	0.24	22.55	107.54
364	3.64	22.48	0.25	0.25	22.35	107.60
365	3.65	22.72	0.25	0.25	22.16	107.66
366	3.66	22.94	0.25	0.25	21.99	107.72
367	3.67	23.14	0.25	0.25	21.83	107.77
368	3.68	23.29	0.25	0.25	21.71	107.80
369	3.69	23.40	0.25	0.25	21.60	107.83
370	3.70	23.53	0.25	0.25	21.49	107.84
371	3.71	23.68	0.25	0.25	21.36	107.87
372	3.72	23.84	0.25	0.25	21.22	107.89
373	3.73	24.00	0.25	0.25	21.09	107.91
374	3.74	24.16	0.25	0.25	20.95	107.93
375	3.75	24.30	0.25	0.25	20.83	107.95
376	3.76	24.42	0.25	0.25	20.73	107.97
377	3.77	24.53	0.25	0.25	20.66	108.02
378	3.78	24.70	0.26	0.26	20.60	108.10
379	3.79	24.91	0.26	0.26	20.53	108.22
380	3.80	25.14	0.26	0.26	20.47	108.35
381	3.81	25.38	0.27	0.27	20.40	108.49
382	3.82	25.63	0.27	0.27	20.33	108.62
383	3.83	25.86	0.27	0.27	20.26	108.75
384	3.84	26.06	0.28	0.28	20.20	108.86

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
385	3.85	26.23	0.28	0.28	20.13	108.98
386	3.86	26.53	0.29	0.29	20.02	109.12
387	3.87	27.00	0.29	0.29	19.85	109.31
388	3.88	27.56	0.30	0.30	19.64	109.54
389	3.89	28.16	0.31	0.31	19.43	109.79
390	3.90	28.78	0.32	0.32	19.21	110.04
391	3.91	29.40	0.32	0.32	19.01	110.29
392	3.92	29.97	0.33	0.33	18.83	110.51
393	3.93	30.47	0.34	0.34	18.67	110.70
394	3.94	30.86	0.35	0.35	18.53	110.84
395	3.95	31.16	0.35	0.35	18.40	110.95
396	3.96	31.53	0.35	0.35	18.24	111.05
397	3.97	31.95	0.36	0.36	18.07	111.16
398	3.98	32.40	0.36	0.36	17.89	111.27
399	3.99	32.87	0.36	0.36	17.71	111.39
400	4.00	33.31	0.37	0.37	17.53	111.50
401	4.01	33.72	0.37	0.37	17.38	111.59
402	4.02	34.06	0.37	0.37	17.26	111.67
403	4.03	34.24	0.38	0.38	17.18	111.70
404	4.04	34.24	0.37	0.37	17.15	111.71
405	4.05	34.24	0.37	0.37	17.13	111.69
406	4.06	34.24	0.37	0.37	17.11	111.67
407	4.07	34.24	0.37	0.37	17.08	111.65
408	4.08	34.24	0.37	0.37	17.06	111.63
409	4.09	34.24	0.37	0.37	17.04	111.61
410	4.10	34.24	0.37	0.37	17.02	111.59
411	4.11	34.24	0.37	0.37	17.01	111.58
412	4.12	34.24	0.37	0.37	17.01	111.58
413	4.13	34.24	0.37	0.37	17.03	111.59
414	4.14	34.24	0.37	0.37	17.05	111.61
415	4.15	34.24	0.37	0.37	17.07	111.63
416	4.16	34.24	0.37	0.37	17.09	111.66
417	4.17	34.24	0.37	0.37	17.12	111.68
418	4.18	34.24	0.37	0.37	17.14	111.69
419	4.19	34.24	0.37	0.37	17.16	111.71
420	4.20	34.24	0.38	0.38	17.19	111.74
421	4.21	34.24	0.38	0.38	17.22	111.77
422	4.22	34.24	0.38	0.38	17.28	111.82
423	4.23	34.24	0.38	0.38	17.34	111.88
424	4.24	34.24	0.39	0.39	17.41	111.94
425	4.25	34.24	0.39	0.39	17.48	112.00
426	4.26	34.24	0.39	0.39	17.55	112.06
427	4.27	34.24	0.40	0.40	17.60	112.11
428	4.28	34.24	0.40	0.40	17.66	112.15
429	4.29	34.23	0.40	0.40	17.71	112.19
430	4.30	34.19	0.40	0.40	17.77	112.22
431	4.31	34.15	0.40	0.40	17.84	112.26
432	4.32	34.10	0.41	0.41	17.92	112.30

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
433	4.33	34.04	0.41	0.41	18.01	112.34
434	4.34	33.99	0.41	0.41	18.09	112.38
435	4.35	33.94	0.41	0.41	18.17	112.42
436	4.36	33.89	0.42	0.42	18.24	112.45
437	4.37	33.85	0.42	0.42	18.29	112.48
438	4.38	33.88	0.42	0.42	18.31	112.51
439	4.39	33.93	0.42	0.42	18.31	112.54
440	4.40	33.99	0.42	0.42	18.31	112.57
441	4.41	34.05	0.42	0.42	18.31	112.61
442	4.42	34.12	0.43	0.43	18.31	112.65
443	4.43	34.19	0.43	0.43	18.31	112.68
444	4.44	34.25	0.43	0.43	18.31	112.72
445	4.45	34.30	0.43	0.43	18.31	112.75
446	4.46	34.35	0.43	0.43	18.29	112.78
447	4.47	34.51	0.43	0.43	18.25	112.82
448	4.48	34.71	0.44	0.44	18.19	112.88
449	4.49	34.93	0.44	0.44	18.12	112.94
450	4.50	35.17	0.44	0.44	18.04	113.00
451	4.51	35.42	0.45	0.45	17.96	113.07
452	4.52	35.65	0.45	0.45	17.89	113.13
453	4.53	35.87	0.45	0.45	17.82	113.19
454	4.54	36.05	0.45	0.45	17.77	113.24
455	4.55	36.20	0.46	0.46	17.71	113.29
456	4.56	36.39	0.46	0.46	17.66	113.34
457	4.57	36.62	0.46	0.46	17.59	113.40
458	4.58	36.87	0.46	0.46	17.51	113.46
459	4.59	37.14	0.47	0.47	17.43	113.53
460	4.60	37.41	0.47	0.47	17.36	113.60
461	4.61	37.66	0.47	0.47	17.28	113.67
462	4.62	37.88	0.48	0.48	17.22	113.72
463	4.63	38.07	0.48	0.48	17.15	113.77
464	4.64	38.29	0.48	0.48	17.07	113.82
465	4.65	38.60	0.48	0.48	16.95	113.87
466	4.66	38.96	0.49	0.49	16.82	113.92
467	4.67	39.36	0.49	0.49	16.67	113.99
468	4.68	39.77	0.49	0.49	16.52	114.05
469	4.69	40.17	0.49	0.49	16.37	114.11
470	4.70	40.54	0.50	0.50	16.24	114.16
471	4.71	40.86	0.50	0.50	16.12	114.21
472	4.72	41.11	0.50	0.50	16.02	114.25
473	4.73	41.39	0.50	0.50	15.92	114.29
474	4.74	41.73	0.50	0.50	15.80	114.34
475	4.75	42.12	0.50	0.50	15.67	114.39
476	4.76	42.54	0.51	0.51	15.52	114.45
477	4.77	42.96	0.51	0.51	15.38	114.51
478	4.78	43.37	0.51	0.51	15.25	114.56
479	4.79	43.74	0.51	0.51	15.13	114.61
480	4.80	44.05	0.52	0.52	15.03	114.65

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
481	4.81	44.32	0.52	0.52	14.94	114.70
482	4.82	44.67	0.52	0.52	14.86	114.78
483	4.83	45.08	0.53	0.53	14.77	114.86
484	4.84	45.55	0.53	0.53	14.67	114.96
485	4.85	46.04	0.54	0.54	14.56	115.07
486	4.86	46.52	0.54	0.54	14.46	115.17
487	4.87	46.98	0.55	0.55	14.37	115.26
488	4.88	47.38	0.55	0.55	14.29	115.34
489	4.89	47.72	0.56	0.56	14.21	115.42
490	4.90	48.07	0.56	0.56	14.13	115.50
491	4.91	48.55	0.57	0.57	14.04	115.59
492	4.92	49.10	0.57	0.57	13.94	115.70
493	4.93	49.70	0.58	0.58	13.82	115.81
494	4.94	50.32	0.59	0.59	13.71	115.93
495	4.95	50.93	0.59	0.59	13.60	116.05
496	4.96	51.49	0.60	0.60	13.50	116.15
497	4.97	51.97	0.61	0.61	13.41	116.24
498	4.98	52.35	0.61	0.61	13.34	116.31
499	4.99	52.64	0.61	0.61	13.28	116.38
500	5.00	53.01	0.62	0.62	13.22	116.44
501	5.01	53.42	0.62	0.62	13.15	116.52
502	5.02	53.86	0.63	0.63	13.08	116.60
503	5.03	54.31	0.63	0.63	13.00	116.68
504	5.04	54.74	0.64	0.64	12.93	116.75
505	5.05	55.13	0.64	0.64	12.87	116.82
506	5.06	55.46	0.65	0.65	12.82	116.87
507	5.07	55.64	0.65	0.65	12.77	116.89
508	5.08	55.74	0.65	0.65	12.72	116.89
509	5.09	55.86	0.65	0.65	12.67	116.88
510	5.10	56.00	0.64	0.64	12.61	116.86
511	5.11	56.14	0.64	0.64	12.55	116.85
512	5.12	56.28	0.64	0.64	12.48	116.83
513	5.13	56.41	0.64	0.64	12.43	116.82
514	5.14	56.53	0.64	0.64	12.37	116.80
515	5.15	56.62	0.63	0.63	12.33	116.79
516	5.16	56.69	0.63	0.63	12.30	116.79
517	5.17	56.76	0.63	0.63	12.27	116.78
518	5.18	56.85	0.63	0.63	12.24	116.78
519	5.19	56.94	0.63	0.63	12.21	116.77
520	5.20	57.03	0.63	0.63	12.17	116.77
521	5.21	57.13	0.63	0.63	12.14	116.77
522	5.22	57.21	0.63	0.63	12.11	116.76
523	5.23	57.29	0.63	0.63	12.08	116.76
524	5.24	57.35	0.63	0.63	12.07	116.77
525	5.25	57.44	0.63	0.63	12.08	116.81
526	5.26	57.55	0.64	0.64	12.10	116.86
527	5.27	57.67	0.64	0.64	12.11	116.92
528	5.28	57.81	0.65	0.65	12.14	116.98

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
529	5.29	57.94	0.65	0.65	12.16	117.04
530	5.30	58.07	0.66	0.66	12.18	117.10
531	5.31	58.19	0.66	0.66	12.19	117.16
532	5.32	58.29	0.67	0.67	12.21	117.20
533	5.33	58.30	0.67	0.67	12.25	117.24
534	5.34	58.23	0.67	0.67	12.30	117.27
535	5.35	58.13	0.68	0.68	12.36	117.31
536	5.36	58.03	0.68	0.68	12.44	117.35
537	5.37	57.92	0.68	0.68	12.51	117.39
538	5.38	57.81	0.69	0.69	12.59	117.43
539	5.39	57.71	0.69	0.69	12.66	117.46
540	5.40	57.62	0.70	0.70	12.72	117.50
541	5.41	57.55	0.70	0.70	12.77	117.52
542	5.42	57.47	0.70	0.70	12.82	117.54
543	5.43	57.36	0.70	0.70	12.87	117.55
544	5.44	57.24	0.70	0.70	12.92	117.56
545	5.45	57.11	0.70	0.70	12.98	117.58
546	5.46	56.97	0.71	0.71	13.04	117.59
547	5.47	56.84	0.71	0.71	13.10	117.60
548	5.48	56.72	0.71	0.71	13.15	117.62
549	5.49	56.61	0.71	0.71	13.20	117.63
550	5.50	56.54	0.71	0.71	13.23	117.63
551	5.51	56.54	0.71	0.71	13.24	117.63
552	5.52	56.54	0.71	0.71	13.24	117.63
553	5.53	56.54	0.71	0.71	13.24	117.63
554	5.54	56.54	0.71	0.71	13.24	117.63
555	5.55	56.54	0.71	0.71	13.24	117.63
556	5.56	56.54	0.71	0.71	13.24	117.63
557	5.57	56.54	0.71	0.71	13.24	117.63
558	5.58	56.54	0.71	0.71	13.24	117.63
559	5.59	56.51	0.71	0.71	13.25	117.63
560	5.60	56.43	0.71	0.71	13.26	117.61
561	5.61	56.34	0.71	0.71	13.27	117.60
562	5.62	56.23	0.71	0.71	13.29	117.58
563	5.63	56.13	0.71	0.71	13.31	117.56
564	5.64	56.02	0.71	0.71	13.32	117.54
565	5.65	55.92	0.70	0.70	13.34	117.53
566	5.66	55.83	0.70	0.70	13.35	117.51
567	5.67	55.76	0.70	0.70	13.37	117.50
568	5.68	55.69	0.70	0.70	13.39	117.50
569	5.69	55.60	0.70	0.70	13.42	117.49
570	5.70	55.51	0.70	0.70	13.45	117.49
571	5.71	55.40	0.70	0.70	13.49	117.49
572	5.72	55.29	0.70	0.70	13.53	117.49
573	5.73	55.19	0.70	0.70	13.56	117.49
574	5.74	55.09	0.70	0.70	13.60	117.49
575	5.75	55.00	0.71	0.71	13.62	117.49
576	5.76	54.95	0.71	0.71	13.65	117.49

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
577	5.77	54.95	0.71	0.71	13.66	117.50
578	5.78	54.95	0.71	0.71	13.68	117.52
579	5.79	54.95	0.71	0.71	13.70	117.54
580	5.80	54.95	0.71	0.71	13.72	117.55
581	5.81	54.95	0.71	0.71	13.74	117.57
582	5.82	54.95	0.71	0.71	13.75	117.59
583	5.83	54.95	0.72	0.72	13.77	117.60
584	5.84	54.95	0.72	0.72	13.78	117.61
585	5.85	54.95	0.72	0.72	13.78	117.61
586	5.86	54.95	0.72	0.72	13.77	117.60
587	5.87	54.95	0.71	0.71	13.75	117.59
588	5.88	54.95	0.71	0.71	13.74	117.57
589	5.89	54.95	0.71	0.71	13.72	117.55
590	5.90	54.95	0.71	0.71	13.70	117.53
591	5.91	54.95	0.71	0.71	13.68	117.52
592	5.92	54.95	0.71	0.71	13.67	117.50
593	5.93	54.95	0.71	0.71	13.66	117.50
594	5.94	54.95	0.71	0.71	13.66	117.50
595	5.95	54.95	0.71	0.71	13.68	117.51
596	5.96	54.95	0.71	0.71	13.69	117.53
597	5.97	54.95	0.71	0.71	13.71	117.55
598	5.98	54.95	0.71	0.71	13.73	117.56
599	5.99	54.95	0.71	0.71	13.75	117.58
600	6.00	54.95	0.72	0.72	13.77	117.60
601	6.01	54.95	0.72	0.72	13.78	117.61
602	6.02	54.95	0.72	0.72	13.80	117.63
603	6.03	54.95	0.72	0.72	13.83	117.65
604	6.04	54.95	0.72	0.72	13.86	117.68
605	6.05	54.95	0.73	0.73	13.90	117.71
606	6.06	54.95	0.73	0.73	13.93	117.75
607	6.07	54.95	0.73	0.73	13.97	117.78
608	6.08	54.95	0.74	0.74	14.01	117.81
609	6.09	54.95	0.74	0.74	14.04	117.84
610	6.10	54.95	0.74	0.74	14.06	117.87
611	6.11	54.99	0.74	0.74	14.07	117.88
612	6.12	55.08	0.75	0.75	14.06	117.90
613	6.13	55.18	0.75	0.75	14.04	117.92
614	6.14	55.30	0.75	0.75	14.02	117.94
615	6.15	55.42	0.75	0.75	14.00	117.96
616	6.16	55.54	0.75	0.75	13.98	117.98
617	6.17	55.66	0.75	0.75	13.96	118.00
618	6.18	55.76	0.75	0.75	13.95	118.02
619	6.19	55.84	0.76	0.76	13.92	118.04
620	6.20	56.04	0.76	0.76	13.87	118.05
621	6.21	56.32	0.76	0.76	13.80	118.07
622	6.22	56.65	0.76	0.76	13.71	118.10
623	6.23	57.00	0.76	0.76	13.62	118.12
624	6.24	57.35	0.76	0.76	13.53	118.15

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
625	6.25	57.70	0.76	0.76	13.44	118.17
626	6.26	58.02	0.76	0.76	13.35	118.20
627	6.27	58.30	0.76	0.76	13.28	118.22
628	6.28	58.57	0.77	0.77	13.20	118.25
629	6.29	59.09	0.77	0.77	13.10	118.31
630	6.30	59.73	0.77	0.77	12.97	118.38
631	6.31	60.46	0.78	0.78	12.84	118.46
632	6.32	61.22	0.79	0.79	12.69	118.55
633	6.33	61.99	0.79	0.79	12.54	118.63
634	6.34	62.73	0.80	0.80	12.41	118.71
635	6.35	63.39	0.80	0.80	12.29	118.78
636	6.36	63.95	0.81	0.81	12.19	118.85
637	6.37	64.49	0.81	0.81	12.09	118.93
638	6.38	65.24	0.82	0.82	11.99	119.04
639	6.39	66.14	0.83	0.83	11.88	119.17
640	6.40	67.12	0.85	0.85	11.76	119.31
641	6.41	68.15	0.86	0.86	11.64	119.45
642	6.42	69.16	0.87	0.87	11.52	119.60
643	6.43	70.11	0.88	0.88	11.41	119.73
644	6.44	70.94	0.89	0.89	11.32	119.84
645	6.45	71.62	0.90	0.90	11.24	119.94
646	6.46	72.22	0.91	0.91	11.16	120.03
647	6.47	72.99	0.92	0.92	11.08	120.13
648	6.48	73.88	0.93	0.93	10.98	120.25
649	6.49	74.84	0.94	0.94	10.88	120.37
650	6.50	75.81	0.96	0.96	10.78	120.49
651	6.51	76.76	0.97	0.97	10.69	120.61
652	6.52	77.64	0.98	0.98	10.60	120.72
653	6.53	78.38	0.99	0.99	10.53	120.81
654	6.54	78.95	1.00	1.00	10.47	120.89
655	6.55	79.50	1.00	1.00	10.41	120.96
656	6.56	80.18	1.01	1.01	10.35	121.05
657	6.57	80.95	1.02	1.02	10.28	121.14
658	6.58	81.75	1.03	1.03	10.21	121.23
659	6.59	82.56	1.04	1.04	10.14	121.33
660	6.60	83.34	1.05	1.05	10.07	121.42
661	6.61	84.04	1.06	1.06	10.01	121.50
662	6.62	84.61	1.07	1.07	9.96	121.56
663	6.63	84.98	1.07	1.07	9.92	121.61
664	6.64	85.34	1.08	1.08	9.89	121.65
665	6.65	85.77	1.08	1.08	9.85	121.70
666	6.66	86.24	1.09	1.09	9.81	121.75
667	6.67	86.73	1.09	1.09	9.77	121.81
668	6.68	87.21	1.10	1.10	9.73	121.86
669	6.69	87.66	1.10	1.10	9.70	121.91
670	6.70	88.06	1.11	1.11	9.67	121.95
671	6.71	88.38	1.11	1.11	9.65	121.99
672	6.72	88.44	1.12	1.12	9.64	122.01

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
673	6.73	88.51	1.12	1.12	9.65	122.03
674	6.74	88.58	1.12	1.12	9.66	122.06
675	6.75	88.66	1.13	1.13	9.67	122.08
676	6.76	88.74	1.13	1.13	9.69	122.11
677	6.77	88.82	1.13	1.13	9.70	122.14
678	6.78	88.89	1.14	1.14	9.71	122.16
679	6.79	88.96	1.14	1.14	9.72	122.18
680	6.80	88.96	1.14	1.14	9.74	122.19
681	6.81	88.79	1.14	1.14	9.77	122.20
682	6.82	88.59	1.15	1.15	9.81	122.21
683	6.83	88.36	1.15	1.15	9.87	122.22
684	6.84	88.11	1.15	1.15	9.92	122.23
685	6.85	87.87	1.15	1.15	9.97	122.23
686	6.86	87.64	1.16	1.16	10.03	122.24
687	6.87	87.43	1.16	1.16	10.07	122.25
688	6.88	87.26	1.16	1.16	10.12	122.25
689	6.89	87.05	1.16	1.16	10.17	122.26
690	6.90	86.75	1.16	1.16	10.23	122.26
691	6.91	86.39	1.17	1.17	10.30	122.27
692	6.92	86.00	1.17	1.17	10.39	122.27
693	6.93	85.60	1.17	1.17	10.47	122.28
694	6.94	85.19	1.17	1.17	10.56	122.28
695	6.95	84.82	1.18	1.18	10.64	122.29
696	6.96	84.49	1.18	1.18	10.71	122.29
697	6.97	84.23	1.18	1.18	10.77	122.29
698	6.98	83.97	1.18	1.18	10.82	122.28
699	6.99	83.65	1.18	1.18	10.87	122.27
700	7.00	83.28	1.18	1.18	10.94	122.26
701	7.01	82.88	1.18	1.18	11.01	122.24
702	7.02	82.47	1.18	1.18	11.08	122.23
703	7.03	82.08	1.18	1.18	11.15	122.21
704	7.04	81.71	1.18	1.18	11.21	122.20
705	7.05	81.41	1.18	1.18	11.26	122.19
706	7.06	81.20	1.18	1.18	11.31	122.19
707	7.07	81.09	1.18	1.18	11.35	122.19
708	7.08	80.95	1.18	1.18	11.39	122.20
709	7.09	80.80	1.18	1.18	11.43	122.21
710	7.10	80.64	1.19	1.19	11.48	122.22
711	7.11	80.48	1.19	1.19	11.53	122.24
712	7.12	80.32	1.19	1.19	11.58	122.25
713	7.13	80.18	1.19	1.19	11.62	122.26
714	7.14	80.07	1.19	1.19	11.65	122.27
715	7.15	80.13	1.20	1.20	11.65	122.28
716	7.16	80.31	1.20	1.20	11.64	122.30
717	7.17	80.52	1.20	1.20	11.62	122.33
718	7.18	80.76	1.21	1.21	11.60	122.36
719	7.19	81.00	1.21	1.21	11.57	122.38
720	7.20	81.24	1.21	1.21	11.55	122.41

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
721	7.21	81.47	1.22	1.22	11.53	122.44
722	7.22	81.67	1.22	1.22	11.51	122.46
723	7.23	81.82	1.22	1.22	11.49	122.48
724	7.24	82.13	1.22	1.22	11.44	122.50
725	7.25	82.52	1.23	1.23	11.38	122.52
726	7.26	82.96	1.23	1.23	11.31	122.55
727	7.27	83.44	1.23	1.23	11.23	122.57
728	7.28	83.93	1.23	1.23	11.16	122.59
729	7.29	84.40	1.23	1.23	11.08	122.62
730	7.30	84.84	1.23	1.23	11.02	122.64
731	7.31	85.20	1.24	1.24	10.96	122.66
732	7.32	85.52	1.24	1.24	10.90	122.68
733	7.33	85.98	1.24	1.24	10.84	122.71
734	7.34	86.52	1.24	1.24	10.76	122.74
735	7.35	87.14	1.25	1.25	10.68	122.78
736	7.36	87.79	1.25	1.25	10.59	122.82
737	7.37	88.43	1.25	1.25	10.51	122.86
738	7.38	89.05	1.26	1.26	10.42	122.89
739	7.39	89.60	1.26	1.26	10.35	122.92
740	7.40	90.06	1.26	1.26	10.29	122.95
741	7.41	90.48	1.26	1.26	10.23	122.98
742	7.42	91.02	1.27	1.27	10.17	123.01
743	7.43	91.67	1.27	1.27	10.10	123.05
744	7.44	92.38	1.28	1.28	10.03	123.09
745	7.45	93.11	1.28	1.28	9.95	123.14
746	7.46	93.83	1.28	1.28	9.88	123.18
747	7.47	94.50	1.29	1.29	9.81	123.22
748	7.48	95.09	1.29	1.29	9.75	123.25
749	7.49	95.56	1.29	1.29	9.71	123.28
750	7.50	95.97	1.30	1.30	9.68	123.32
751	7.51	96.49	1.31	1.31	9.65	123.37
752	7.52	97.09	1.31	1.31	9.62	123.43
753	7.53	97.73	1.32	1.32	9.58	123.50
754	7.54	98.38	1.33	1.33	9.54	123.56
755	7.55	99.01	1.34	1.34	9.51	123.62
756	7.56	99.59	1.35	1.35	9.48	123.68
757	7.57	100.08	1.35	1.35	9.45	123.72
758	7.58	100.48	1.36	1.36	9.43	123.77
759	7.59	100.99	1.37	1.37	9.40	123.82
760	7.60	101.61	1.38	1.38	9.37	123.88
761	7.61	102.30	1.38	1.38	9.33	123.94
762	7.62	103.03	1.39	1.39	9.29	124.01
763	7.63	103.76	1.40	1.40	9.25	124.08
764	7.64	104.45	1.41	1.41	9.22	124.14
765	7.65	105.07	1.42	1.42	9.19	124.20
766	7.66	105.58	1.43	1.43	9.17	124.25
767	7.67	105.95	1.44	1.44	9.16	124.30
768	7.68	106.38	1.45	1.45	9.16	124.37

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
769	7.69	106.88	1.46	1.46	9.16	124.44
770	7.70	107.43	1.47	1.47	9.16	124.52
771	7.71	108.00	1.49	1.49	9.17	124.61
772	7.72	108.56	1.50	1.50	9.17	124.69
773	7.73	109.09	1.52	1.52	9.17	124.77
774	7.74	109.54	1.53	1.53	9.18	124.83
775	7.75	109.90	1.54	1.54	9.18	124.89
776	7.76	110.16	1.55	1.55	9.19	124.94
777	7.77	110.49	1.56	1.56	9.20	124.99
778	7.78	110.86	1.57	1.57	9.21	125.05
779	7.79	111.26	1.58	1.58	9.23	125.12
780	7.80	111.67	1.59	1.59	9.24	125.19
781	7.81	112.06	1.61	1.61	9.25	125.25
782	7.82	112.42	1.62	1.62	9.26	125.31
783	7.83	112.73	1.63	1.63	9.27	125.36
784	7.84	112.95	1.63	1.63	9.27	125.39
785	7.85	113.18	1.64	1.64	9.27	125.42
786	7.86	113.45	1.64	1.64	9.26	125.44
787	7.87	113.76	1.65	1.65	9.25	125.47
788	7.88	114.09	1.65	1.65	9.23	125.49
789	7.89	114.41	1.66	1.66	9.22	125.52
790	7.90	114.72	1.66	1.66	9.21	125.55
791	7.91	114.99	1.66	1.66	9.20	125.57
792	7.92	115.22	1.67	1.67	9.20	125.59
793	7.93	115.27	1.67	1.67	9.20	125.60
794	7.94	115.27	1.67	1.67	9.22	125.61
795	7.95	115.27	1.68	1.68	9.23	125.63
796	7.96	115.27	1.68	1.68	9.25	125.64
797	7.97	115.27	1.68	1.68	9.27	125.66
798	7.98	115.27	1.69	1.69	9.29	125.67
799	7.99	115.27	1.69	1.69	9.31	125.69
800	8.00	115.27	1.69	1.69	9.32	125.70
801	8.01	115.27	1.70	1.70	9.34	125.72
802	8.02	115.27	1.70	1.70	9.36	125.73
803	8.03	115.27	1.71	1.71	9.39	125.76
804	8.04	115.27	1.71	1.71	9.42	125.79
805	8.05	115.27	1.72	1.72	9.45	125.82
806	8.06	115.27	1.73	1.73	9.48	125.85
807	8.07	115.27	1.73	1.73	9.51	125.88
808	8.08	115.27	1.74	1.74	9.53	125.90
809	8.09	115.27	1.75	1.75	9.55	125.93
810	8.10	115.34	1.75	1.75	9.56	125.94
811	8.11	115.57	1.75	1.75	9.54	125.95
812	8.12	115.85	1.75	1.75	9.52	125.96
813	8.13	116.16	1.75	1.75	9.49	125.97
814	8.14	116.48	1.75	1.75	9.46	125.98
815	8.15	116.81	1.75	1.75	9.44	126.00
816	8.16	117.11	1.76	1.76	9.41	126.01

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
817	8.17	117.39	1.76	1.76	9.39	126.02
818	8.18	117.61	1.76	1.76	9.36	126.02
819	8.19	117.91	1.76	1.76	9.32	126.03
820	8.20	118.35	1.75	1.75	9.27	126.03
821	8.21	118.85	1.75	1.75	9.21	126.03
822	8.22	119.41	1.75	1.75	9.14	126.03
823	8.23	119.97	1.75	1.75	9.08	126.02
824	8.24	120.53	1.74	1.74	9.01	126.02
825	8.25	121.05	1.74	1.74	8.94	126.02
826	8.26	121.51	1.74	1.74	8.89	126.02
827	8.27	121.87	1.73	1.73	8.84	126.02
828	8.28	122.34	1.74	1.74	8.80	126.04
829	8.29	122.93	1.74	1.74	8.75	126.06
830	8.30	123.61	1.74	1.74	8.69	126.08
831	8.31	124.33	1.74	1.74	8.63	126.10
832	8.32	125.06	1.75	1.75	8.57	126.13
833	8.33	125.77	1.75	1.75	8.51	126.15
834	8.34	126.41	1.75	1.75	8.46	126.17
835	8.35	126.96	1.75	1.75	8.42	126.18
836	8.36	127.37	1.75	1.75	8.39	126.20
837	8.37	127.83	1.76	1.76	8.36	126.23
838	8.38	128.39	1.76	1.76	8.32	126.25
839	8.39	129.01	1.77	1.77	8.28	126.28
840	8.40	129.65	1.77	1.77	8.24	126.31
841	8.41	130.30	1.77	1.77	8.20	126.35
842	8.42	130.91	1.78	1.78	8.16	126.37
843	8.43	131.46	1.78	1.78	8.13	126.40
844	8.44	131.90	1.79	1.79	8.10	126.42
845	8.45	132.18	1.79	1.79	8.09	126.44
846	8.46	132.49	1.79	1.79	8.08	126.47
847	8.47	132.86	1.80	1.80	8.06	126.49
848	8.48	133.25	1.80	1.80	8.05	126.52
849	8.49	133.66	1.81	1.81	8.03	126.55
850	8.50	134.06	1.81	1.81	8.02	126.58
851	8.51	134.43	1.82	1.82	8.01	126.60
852	8.52	134.75	1.82	1.82	7.99	126.63
853	8.53	134.99	1.83	1.83	7.99	126.64
854	8.54	135.15	1.83	1.83	7.98	126.66
855	8.55	135.35	1.83	1.83	7.97	126.67
856	8.56	135.58	1.84	1.84	7.97	126.69
857	8.57	135.82	1.84	1.84	7.96	126.71
858	8.58	136.06	1.84	1.84	7.95	126.72
859	8.59	136.30	1.85	1.85	7.94	126.74
860	8.60	136.51	1.85	1.85	7.94	126.76
861	8.61	136.69	1.85	1.85	7.93	126.77
862	8.62	136.79	1.85	1.85	7.93	126.78
863	8.63	136.85	1.85	1.85	7.93	126.78
864	8.64	136.92	1.85	1.85	7.93	126.79

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
865	8.65	137.00	1.85	1.85	7.93	126.79
866	8.66	137.08	1.86	1.86	7.93	126.80
867	8.67	137.16	1.86	1.86	7.92	126.80
868	8.68	137.24	1.86	1.86	7.92	126.81
869	8.69	137.31	1.86	1.86	7.92	126.81
870	8.70	137.36	1.86	1.86	7.92	126.81
871	8.71	137.37	1.86	1.86	7.91	126.80
872	8.72	137.37	1.85	1.85	7.89	126.77
873	8.73	137.37	1.84	1.84	7.86	126.74
874	8.74	137.37	1.83	1.83	7.84	126.71
875	8.75	137.37	1.82	1.82	7.81	126.68
876	8.76	137.37	1.82	1.82	7.78	126.64
877	8.77	137.37	1.81	1.81	7.76	126.61
878	8.78	137.37	1.80	1.80	7.73	126.58
879	8.79	137.36	1.80	1.80	7.72	126.56
880	8.80	137.26	1.79	1.79	7.71	126.54
881	8.81	137.12	1.79	1.79	7.71	126.51
882	8.82	136.97	1.78	1.78	7.70	126.49
883	8.83	136.81	1.77	1.77	7.70	126.46
884	8.84	136.65	1.77	1.77	7.69	126.43
885	8.85	136.49	1.76	1.76	7.68	126.40
886	8.86	136.35	1.75	1.75	7.68	126.38
887	8.87	136.23	1.75	1.75	7.68	126.36
888	8.88	136.09	1.75	1.75	7.69	126.35
889	8.89	135.86	1.75	1.75	7.72	126.36
890	8.90	135.58	1.76	1.76	7.76	126.37
891	8.91	135.27	1.76	1.76	7.80	126.38
892	8.92	134.94	1.76	1.76	7.85	126.39
893	8.93	134.62	1.77	1.77	7.89	126.40
894	8.94	134.32	1.77	1.77	7.93	126.41
895	8.95	134.05	1.78	1.78	7.97	126.42
896	8.96	133.83	1.78	1.78	8.00	126.43
897	8.97	133.59	1.78	1.78	8.03	126.42
898	8.98	133.28	1.78	1.78	8.06	126.42
899	8.99	132.91	1.78	1.78	8.09	126.41
900	9.00	132.52	1.78	1.78	8.12	126.39
901	9.01	132.11	1.77	1.77	8.16	126.38
902	9.02	131.71	1.77	1.77	8.19	126.37
903	9.03	131.34	1.77	1.77	8.22	126.36
904	9.04	131.02	1.77	1.77	8.25	126.35
905	9.05	130.78	1.77	1.77	8.28	126.34
906	9.06	130.56	1.77	1.77	8.31	126.35
907	9.07	130.30	1.78	1.78	8.35	126.36
908	9.08	130.00	1.78	1.78	8.39	126.36
909	9.09	129.67	1.78	1.78	8.43	126.37
910	9.10	129.35	1.79	1.79	8.48	126.38
911	9.11	129.04	1.79	1.79	8.53	126.39
912	9.12	128.75	1.79	1.79	8.57	126.40

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
913	9.13	128.52	1.80	1.80	8.60	126.41
914	9.14	128.39	1.80	1.80	8.63	126.42
915	9.15	128.33	1.81	1.81	8.66	126.44
916	9.16	128.26	1.81	1.81	8.69	126.46
917	9.17	128.18	1.82	1.82	8.72	126.48
918	9.18	128.10	1.82	1.82	8.76	126.51
919	9.19	128.02	1.83	1.83	8.79	126.54
920	9.20	127.95	1.84	1.84	8.82	126.56
921	9.21	127.88	1.84	1.84	8.85	126.58
922	9.22	127.82	1.85	1.85	8.87	126.60
923	9.23	127.90	1.85	1.85	8.88	126.61
924	9.24	128.02	1.85	1.85	8.88	126.62
925	9.25	128.17	1.85	1.85	8.87	126.63
926	9.26	128.33	1.86	1.86	8.87	126.64
927	9.27	128.49	1.86	1.86	8.86	126.65
928	9.28	128.65	1.86	1.86	8.86	126.67
929	9.29	128.80	1.86	1.86	8.85	126.68
930	9.30	128.92	1.87	1.87	8.85	126.69
931	9.31	129.06	1.87	1.87	8.83	126.69
932	9.32	129.44	1.87	1.87	8.80	126.70
933	9.33	129.91	1.87	1.87	8.76	126.71
934	9.34	130.44	1.87	1.87	8.71	126.72
935	9.35	131.00	1.87	1.87	8.66	126.73
936	9.36	131.57	1.87	1.87	8.61	126.74
937	9.37	132.11	1.87	1.87	8.56	126.75
938	9.38	132.61	1.87	1.87	8.51	126.75
939	9.39	133.02	1.87	1.87	8.47	126.76
940	9.40	133.43	1.86	1.86	8.43	126.77
941	9.41	134.02	1.86	1.86	8.38	126.77
942	9.42	134.72	1.86	1.86	8.31	126.78
943	9.43	135.50	1.86	1.86	8.24	126.79
944	9.44	136.31	1.86	1.86	8.16	126.80
945	9.45	137.12	1.86	1.86	8.09	126.80
946	9.46	137.87	1.86	1.86	8.01	126.81
947	9.47	138.55	1.85	1.85	7.95	126.81
948	9.48	139.09	1.85	1.85	7.90	126.82
949	9.49	139.54	1.85	1.85	7.86	126.83
950	9.50	140.11	1.85	1.85	7.81	126.84
951	9.51	140.77	1.85	1.85	7.76	126.85
952	9.52	141.49	1.85	1.85	7.71	126.87
953	9.53	142.22	1.85	1.85	7.65	126.88
954	9.54	142.94	1.85	1.85	7.60	126.89
955	9.55	143.60	1.86	1.86	7.55	126.91
956	9.56	144.16	1.86	1.86	7.51	126.91
957	9.57	144.43	1.85	1.85	7.48	126.88
958	9.58	143.64	1.83	1.83	7.47	126.82
959	9.59	142.66	1.81	1.81	7.47	126.71
960	9.60	141.56	1.78	1.78	7.48	126.58

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
961	9.61	140.39	1.76	1.76	7.48	126.45
962	9.62	139.22	1.73	1.73	7.48	126.31
963	9.63	138.09	1.70	1.70	7.48	126.18
964	9.64	137.07	1.68	1.68	7.48	126.06
965	9.65	136.22	1.66	1.66	7.48	125.97
966	9.66	135.90	1.65	1.65	7.47	125.91
967	9.67	135.96	1.64	1.64	7.45	125.88
968	9.68	136.03	1.63	1.63	7.42	125.85
969	9.69	136.11	1.63	1.63	7.39	125.82
970	9.70	136.19	1.62	1.62	7.36	125.78
971	9.71	136.27	1.61	1.61	7.33	125.75
972	9.72	136.35	1.60	1.60	7.29	125.72
973	9.73	136.42	1.60	1.60	7.27	125.69
974	9.74	136.47	1.59	1.59	7.27	125.65
975	9.75	135.15	1.58	1.58	7.32	125.57
976	9.76	133.21	1.56	1.56	7.41	125.45
977	9.77	130.97	1.54	1.54	7.52	125.31
978	9.78	128.54	1.51	1.51	7.64	125.15
979	9.79	126.06	1.49	1.49	7.77	124.98
980	9.80	123.64	1.46	1.46	7.90	124.81
981	9.81	121.41	1.44	1.44	8.02	124.65
982	9.82	119.49	1.42	1.42	8.15	124.53
983	9.83	117.80	1.41	1.41	8.38	124.49
984	9.84	115.01	1.44	1.44	8.75	124.53
985	9.85	111.57	1.48	1.48	9.27	124.62
986	9.86	107.69	1.51	1.51	9.88	124.68
987	9.87	103.58	1.54	1.54	10.52	124.72
988	9.88	99.44	1.56	1.56	11.19	124.72
989	9.89	95.48	1.57	1.57	11.84	124.68
990	9.90	91.91	1.58	1.58	12.43	124.63
991	9.91	88.92	1.58	1.58	12.92	124.61
992	9.92	87.93	1.60	1.60	13.28	124.71
993	9.93	88.25	1.66	1.66	13.55	124.94
994	9.94	88.62	1.73	1.73	13.83	125.25
995	9.95	89.02	1.81	1.81	14.13	125.57
996	9.96	89.45	1.89	1.89	14.44	125.91
997	9.97	89.87	1.98	1.98	14.74	126.22
998	9.98	90.26	2.05	2.05	15.01	126.51
999	9.99	90.61	2.12	2.12	15.24	126.76
1000	10.00	90.89	2.18	2.18	15.39	126.89
1001	10.01	90.51	2.17	2.17	15.47	126.91
1002	10.02	89.92	2.15	2.15	15.50	126.83
1003	10.03	89.24	2.12	2.12	15.51	126.72
1004	10.04	88.51	2.09	2.09	15.53	126.61
1005	10.05	87.76	2.06	2.06	15.55	126.48
1006	10.06	87.03	2.03	2.03	15.57	126.37
1007	10.07	86.36	2.01	2.01	15.59	126.26
1008	10.08	85.79	1.99	1.99	15.62	126.16

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1009	10.09	85.12	1.97	1.97	15.72	126.04
1010	10.10	83.40	1.94	1.94	15.90	125.90
1011	10.11	81.28	1.90	1.90	16.17	125.70
1012	10.12	78.90	1.86	1.86	16.49	125.47
1013	10.13	76.38	1.82	1.82	16.83	125.21
1014	10.14	73.85	1.77	1.77	17.20	124.95
1015	10.15	71.43	1.73	1.73	17.56	124.68
1016	10.16	69.25	1.68	1.68	17.89	124.44
1017	10.17	67.43	1.65	1.65	18.22	124.24
1018	10.18	65.97	1.64	1.64	18.60	124.10
1019	10.19	64.19	1.63	1.63	19.08	124.00
1020	10.20	62.07	1.62	1.62	19.68	123.88
1021	10.21	59.74	1.61	1.61	20.36	123.74
1022	10.22	57.32	1.60	1.60	21.09	123.56
1023	10.23	54.92	1.58	1.58	21.83	123.37
1024	10.24	52.67	1.55	1.55	22.55	123.17
1025	10.25	50.70	1.53	1.53	23.21	122.97
1026	10.26	49.11	1.51	1.51	23.78	122.82
1027	10.27	47.96	1.51	1.51	24.34	122.70
1028	10.28	46.55	1.50	1.50	24.96	122.60
1029	10.29	44.93	1.49	1.49	25.70	122.47
1030	10.30	43.17	1.48	1.48	26.51	122.30
1031	10.31	41.38	1.46	1.46	27.41	122.11
1032	10.32	39.64	1.44	1.44	28.33	121.91
1033	10.33	38.04	1.42	1.42	29.21	121.70
1034	10.34	36.67	1.39	1.39	29.97	121.51
1035	10.35	35.74	1.38	1.38	30.56	121.39
1036	10.36	35.24	1.38	1.38	31.04	121.31
1037	10.37	34.63	1.38	1.38	31.51	121.26
1038	10.38	33.94	1.38	1.38	32.05	121.20
1039	10.39	33.21	1.37	1.37	32.63	121.13
1040	10.40	32.48	1.37	1.37	33.22	121.06
1041	10.41	31.79	1.36	1.36	33.79	120.98
1042	10.42	31.16	1.36	1.36	34.31	120.90
1043	10.43	30.64	1.35	1.35	34.72	120.85
1044	10.44	30.43	1.35	1.35	35.01	120.84
1045	10.45	30.37	1.36	1.36	35.20	120.87
1046	10.46	30.30	1.37	1.37	35.40	120.92
1047	10.47	30.22	1.39	1.39	35.61	120.98
1048	10.48	30.14	1.40	1.40	35.83	121.04
1049	10.49	30.06	1.41	1.41	36.04	121.09
1050	10.50	29.99	1.42	1.42	36.25	121.15
1051	10.51	29.92	1.43	1.43	36.42	121.19
1052	10.52	29.87	1.44	1.44	36.54	121.22
1053	10.53	29.86	1.44	1.44	36.63	121.25
1054	10.54	29.86	1.45	1.45	36.68	121.27
1055	10.55	29.86	1.45	1.45	36.74	121.30
1056	10.56	29.86	1.46	1.46	36.80	121.33

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1057	10.57	29.86	1.47	1.47	36.86	121.36
1058	10.58	29.86	1.47	1.47	36.92	121.39
1059	10.59	29.86	1.48	1.48	36.98	121.41
1060	10.60	29.86	1.48	1.48	37.01	121.44
1061	10.61	29.91	1.49	1.49	36.96	121.46
1062	10.62	30.13	1.49	1.49	36.81	121.49
1063	10.63	30.39	1.49	1.49	36.58	121.53
1064	10.64	30.68	1.49	1.49	36.32	121.57
1065	10.65	31.00	1.50	1.50	36.04	121.61
1066	10.66	31.31	1.50	1.50	35.77	121.65
1067	10.67	31.61	1.50	1.50	35.52	121.68
1068	10.68	31.87	1.51	1.51	35.29	121.71
1069	10.69	32.10	1.51	1.51	35.05	121.75
1070	10.70	32.43	1.51	1.51	34.75	121.80
1071	10.71	32.98	1.52	1.52	34.35	121.86
1072	10.72	33.62	1.53	1.53	33.85	121.94
1073	10.73	34.33	1.53	1.53	33.31	122.02
1074	10.74	35.06	1.54	1.54	32.76	122.10
1075	10.75	35.78	1.54	1.54	32.23	122.17
1076	10.76	36.46	1.55	1.55	31.74	122.23
1077	10.77	37.05	1.55	1.55	31.31	122.28
1078	10.78	37.52	1.55	1.55	30.91	122.34
1079	10.79	38.18	1.56	1.56	30.47	122.41
1080	10.80	39.03	1.57	1.57	29.97	122.49
1081	10.81	40.01	1.57	1.57	29.42	122.59
1082	10.82	41.06	1.58	1.58	28.84	122.68
1083	10.83	42.13	1.59	1.59	28.25	122.76
1084	10.84	43.17	1.59	1.59	27.70	122.84
1085	10.85	44.12	1.59	1.59	27.19	122.90
1086	10.86	44.93	1.59	1.59	26.76	122.95
1087	10.87	45.63	1.59	1.59	26.35	123.01
1088	10.88	46.64	1.60	1.60	25.91	123.09
1089	10.89	47.87	1.61	1.61	25.38	123.19
1090	10.90	49.25	1.62	1.62	24.80	123.29
1091	10.91	50.71	1.62	1.62	24.20	123.39
1092	10.92	52.17	1.63	1.63	23.61	123.47
1093	10.93	53.55	1.63	1.63	23.06	123.54
1094	10.94	54.80	1.63	1.63	22.58	123.60
1095	10.95	55.83	1.63	1.63	22.17	123.63
1096	10.96	56.64	1.62	1.62	21.81	123.66
1097	10.97	57.61	1.62	1.62	21.43	123.69
1098	10.98	58.75	1.61	1.61	20.99	123.71
1099	10.99	60.01	1.61	1.61	20.52	123.72
1100	11.00	61.31	1.60	1.60	20.03	123.73
1101	11.01	62.59	1.58	1.58	19.56	123.73
1102	11.02	63.79	1.57	1.57	19.12	123.72
1103	11.03	64.84	1.56	1.56	18.74	123.70
1104	11.04	65.68	1.55	1.55	18.45	123.68

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1105	11.05	66.10	1.54	1.54	18.21	123.64
1106	11.06	66.62	1.53	1.53	17.99	123.60
1107	11.07	67.21	1.51	1.51	17.73	123.55
1108	11.08	67.85	1.49	1.49	17.45	123.49
1109	11.09	68.51	1.47	1.47	17.17	123.42
1110	11.10	69.14	1.46	1.46	16.89	123.35
1111	11.11	69.71	1.44	1.44	16.64	123.29
1112	11.12	70.21	1.42	1.42	16.44	123.23
1113	11.13	70.45	1.41	1.41	16.30	123.16
1114	11.14	70.32	1.40	1.40	16.21	123.08
1115	11.15	70.16	1.38	1.38	16.14	122.98
1116	11.16	69.99	1.36	1.36	16.06	122.87
1117	11.17	69.81	1.34	1.34	15.97	122.75
1118	11.18	69.63	1.32	1.32	15.88	122.63
1119	11.19	69.45	1.30	1.30	15.79	122.51
1120	11.20	69.30	1.28	1.28	15.72	122.41
1121	11.21	69.17	1.26	1.26	15.68	122.32
1122	11.22	68.84	1.26	1.26	15.71	122.26
1123	11.23	68.28	1.25	1.25	15.80	122.21
1124	11.24	67.62	1.24	1.24	15.93	122.15
1125	11.25	66.89	1.24	1.24	16.07	122.08
1126	11.26	66.14	1.23	1.23	16.21	122.01
1127	11.27	65.41	1.22	1.22	16.36	121.94
1128	11.28	64.72	1.21	1.21	16.50	121.87
1129	11.29	64.12	1.21	1.21	16.62	121.81
1130	11.30	63.64	1.20	1.20	16.77	121.77
1131	11.31	62.93	1.20	1.20	16.96	121.74
1132	11.32	62.04	1.21	1.21	17.24	121.71
1133	11.33	61.01	1.21	1.21	17.55	121.68
1134	11.34	59.91	1.21	1.21	17.89	121.64
1135	11.35	58.79	1.21	1.21	18.25	121.59
1136	11.36	57.71	1.21	1.21	18.59	121.54
1137	11.37	56.72	1.21	1.21	18.91	121.49
1138	11.38	55.88	1.20	1.20	19.20	121.45
1139	11.39	55.13	1.20	1.20	19.51	121.40
1140	11.40	54.07	1.20	1.20	19.88	121.35
1141	11.41	52.77	1.20	1.20	20.34	121.28
1142	11.42	51.33	1.20	1.20	20.88	121.19
1143	11.43	49.81	1.19	1.19	21.44	121.08
1144	11.44	48.28	1.18	1.18	22.03	120.96
1145	11.45	46.84	1.18	1.18	22.59	120.84
1146	11.46	45.55	1.17	1.17	23.11	120.72
1147	11.47	44.48	1.16	1.16	23.57	120.62
1148	11.48	43.69	1.15	1.15	24.00	120.54
1149	11.49	42.75	1.15	1.15	24.47	120.46
1150	11.50	41.64	1.15	1.15	25.02	120.37
1151	11.51	40.44	1.14	1.14	25.64	120.26
1152	11.52	39.19	1.13	1.13	26.29	120.14

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1153	11.53	37.96	1.13	1.13	26.95	120.00
1154	11.54	36.82	1.11	1.11	27.57	119.87
1155	11.55	35.82	1.10	1.10	28.13	119.74
1156	11.56	35.03	1.10	1.10	28.61	119.64
1157	11.57	34.49	1.09	1.09	29.05	119.56
1158	11.58	33.81	1.09	1.09	29.52	119.50
1159	11.59	33.03	1.09	1.09	30.07	119.41
1160	11.60	32.20	1.08	1.08	30.67	119.32
1161	11.61	31.35	1.08	1.08	31.29	119.21
1162	11.62	30.54	1.07	1.07	31.90	119.10
1163	11.63	29.79	1.06	1.06	32.47	118.99
1164	11.64	29.16	1.05	1.05	32.95	118.90
1165	11.65	28.75	1.05	1.05	33.33	118.84
1166	11.66	28.48	1.05	1.05	33.65	118.80
1167	11.67	28.16	1.05	1.05	33.98	118.78
1168	11.68	27.80	1.05	1.05	34.35	118.76
1169	11.69	27.42	1.05	1.05	34.74	118.73
1170	11.70	27.05	1.05	1.05	35.14	118.70
1171	11.71	26.69	1.05	1.05	35.51	118.66
1172	11.72	26.37	1.05	1.05	35.86	118.63
1173	11.73	26.11	1.05	1.05	36.09	118.61
1174	11.74	26.10	1.05	1.05	36.19	118.63
1175	11.75	26.21	1.06	1.06	36.18	118.67
1176	11.76	26.33	1.07	1.07	36.13	118.72
1177	11.77	26.47	1.07	1.07	36.08	118.79
1178	11.78	26.61	1.08	1.08	36.03	118.85
1179	11.79	26.75	1.09	1.09	35.98	118.91
1180	11.80	26.88	1.10	1.10	35.94	118.96
1181	11.81	26.99	1.10	1.10	35.90	119.01
1182	11.82	27.07	1.11	1.11	35.92	118.99
1183	11.83	26.77	1.09	1.09	35.98	118.90
1184	11.84	26.41	1.07	1.07	36.10	118.72
1185	11.85	25.99	1.04	1.04	36.25	118.51
1186	11.86	25.54	1.02	1.02	36.41	118.29
1187	11.87	25.08	0.99	0.99	36.57	118.06
1188	11.88	24.64	0.96	0.96	36.74	117.83
1189	11.89	24.24	0.94	0.94	36.90	117.62
1190	11.90	23.90	0.92	0.92	37.01	117.45
1191	11.91	23.71	0.91	0.91	37.05	117.31
1192	11.92	23.63	0.90	0.90	37.00	117.19
1193	11.93	23.54	0.88	0.88	36.90	117.07
1194	11.94	23.44	0.87	0.87	36.79	116.93
1195	11.95	23.33	0.85	0.85	36.67	116.78
1196	11.96	23.22	0.84	0.84	36.54	116.63
1197	11.97	23.12	0.82	0.82	36.43	116.48
1198	11.98	23.03	0.81	0.81	36.32	116.35
1199	11.99	22.95	0.79	0.79	36.26	116.23
1200	12.00	22.78	0.78	0.78	36.25	116.08

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1201	12.01	22.51	0.76	0.76	36.29	115.89
1202	12.02	22.19	0.74	0.74	36.35	115.66
1203	12.03	21.84	0.72	0.72	36.42	115.41
1204	12.04	21.48	0.70	0.70	36.50	115.15
1205	12.05	21.13	0.68	0.68	36.57	114.89
1206	12.06	20.80	0.66	0.66	36.65	114.64
1207	12.07	20.52	0.64	0.64	36.72	114.42
1208	12.08	20.27	0.63	0.63	36.94	114.18
1209	12.09	19.64	0.61	0.61	37.35	113.88
1210	12.10	18.85	0.58	0.58	38.01	113.47
1211	12.11	17.95	0.55	0.55	38.82	112.99
1212	12.12	16.99	0.52	0.52	39.74	112.44
1213	12.13	16.01	0.49	0.49	40.76	111.86
1214	12.14	15.07	0.46	0.46	41.83	111.27
1215	12.15	14.21	0.44	0.44	42.91	110.70
1216	12.16	13.49	0.41	0.41	43.88	110.23
1217	12.17	13.08	0.40	0.40	44.61	109.93
1218	12.18	12.91	0.40	0.40	45.14	109.78
1219	12.19	12.70	0.40	0.40	45.63	109.70
1220	12.20	12.47	0.39	0.39	46.19	109.59
1221	12.21	12.23	0.39	0.39	46.78	109.48
1222	12.22	11.98	0.39	0.39	47.39	109.37
1223	12.23	11.75	0.38	0.38	47.98	109.26
1224	12.24	11.55	0.38	0.38	48.51	109.16
1225	12.25	11.38	0.38	0.38	48.99	109.07
1226	12.26	11.24	0.38	0.38	49.49	109.00
1227	12.27	11.05	0.37	0.37	50.06	108.92
1228	12.28	10.83	0.37	0.37	50.75	108.83
1229	12.29	10.60	0.37	0.37	51.52	108.73
1230	12.30	10.35	0.37	0.37	52.33	108.62
1231	12.31	10.11	0.36	0.36	53.14	108.50
1232	12.32	9.89	0.36	0.36	53.91	108.38
1233	12.33	9.70	0.36	0.36	54.60	108.28
1234	12.34	9.55	0.35	0.35	55.22	108.18
1235	12.35	9.39	0.35	0.35	55.85	108.08
1236	12.36	9.19	0.35	0.35	56.60	107.96
1237	12.37	8.96	0.34	0.34	57.47	107.82
1238	12.38	8.72	0.34	0.34	58.43	107.65
1239	12.39	8.48	0.33	0.33	59.43	107.48
1240	12.40	8.24	0.33	0.33	60.43	107.31
1241	12.41	8.03	0.33	0.33	61.36	107.14
1242	12.42	7.85	0.32	0.32	62.16	107.00
1243	12.43	7.72	0.32	0.32	62.83	106.88
1244	12.44	7.61	0.32	0.32	63.46	106.78
1245	12.45	7.47	0.31	0.31	64.16	106.67
1246	12.46	7.31	0.31	0.31	64.96	106.54
1247	12.47	7.15	0.31	0.31	65.82	106.40
1248	12.48	6.99	0.30	0.30	66.70	106.26

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1249	12.49	6.84	0.30	0.30	67.56	106.11
1250	12.50	6.70	0.29	0.29	68.34	105.98
1251	12.51	6.59	0.29	0.29	68.95	105.88
1252	12.52	6.53	0.29	0.29	69.43	105.80
1253	12.53	6.47	0.29	0.29	69.85	105.74
1254	12.54	6.40	0.29	0.29	70.31	105.67
1255	12.55	6.32	0.29	0.29	70.82	105.59
1256	12.56	6.24	0.28	0.28	71.35	105.50
1257	12.57	6.16	0.28	0.28	71.88	105.42
1258	12.58	6.08	0.28	0.28	72.38	105.34
1259	12.59	6.02	0.28	0.28	72.81	105.27
1260	12.60	5.97	0.28	0.28	73.07	105.23
1261	12.61	5.97	0.28	0.28	73.18	105.21
1262	12.62	5.97	0.28	0.28	73.18	105.21
1263	12.63	5.97	0.28	0.28	73.19	105.21
1264	12.64	5.97	0.28	0.28	73.19	105.21
1265	12.65	5.97	0.28	0.28	73.20	105.21
1266	12.66	5.97	0.28	0.28	73.20	105.21
1267	12.67	5.97	0.28	0.28	73.21	105.21
1268	12.68	5.97	0.28	0.28	73.20	105.21
1269	12.69	5.97	0.28	0.28	73.15	105.19
1270	12.70	5.97	0.27	0.27	73.06	105.16
1271	12.71	5.97	0.27	0.27	72.93	105.11
1272	12.72	5.97	0.27	0.27	72.79	105.06
1273	12.73	5.97	0.27	0.27	72.64	105.00
1274	12.74	5.97	0.27	0.27	72.49	104.94
1275	12.75	5.97	0.26	0.26	72.35	104.89
1276	12.76	5.97	0.26	0.26	72.22	104.84
1277	12.77	5.97	0.26	0.26	72.10	104.80
1278	12.78	5.97	0.26	0.26	71.96	104.74
1279	12.79	5.97	0.26	0.26	71.78	104.68
1280	12.80	5.97	0.25	0.25	71.56	104.59
1281	12.81	5.97	0.25	0.25	71.32	104.50
1282	12.82	5.97	0.25	0.25	71.07	104.41
1283	12.83	5.97	0.24	0.24	70.82	104.32
1284	12.84	5.97	0.24	0.24	70.59	104.23
1285	12.85	5.97	0.24	0.24	70.40	104.16
1286	12.86	5.97	0.24	0.24	70.21	104.09
1287	12.87	5.97	0.23	0.23	70.01	104.01
1288	12.88	5.97	0.23	0.23	69.77	103.92
1289	12.89	5.97	0.23	0.23	69.50	103.81
1290	12.90	5.97	0.22	0.22	69.21	103.70
1291	12.91	5.97	0.22	0.22	68.91	103.58
1292	12.92	5.97	0.22	0.22	68.62	103.47
1293	12.93	5.97	0.21	0.21	68.35	103.36
1294	12.94	5.97	0.21	0.21	68.12	103.27
1295	12.95	5.97	0.21	0.21	67.89	103.18
1296	12.96	5.97	0.21	0.21	67.62	103.08

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1297	12.97	5.97	0.20	0.20	67.31	102.95
1298	12.98	5.97	0.20	0.20	66.95	102.81
1299	12.99	5.97	0.19	0.19	66.57	102.65
1300	13.00	5.97	0.19	0.19	66.19	102.50
1301	13.01	5.97	0.19	0.19	65.83	102.35
1302	13.02	5.97	0.18	0.18	65.50	102.22
1303	13.03	5.97	0.18	0.18	65.38	102.06
1304	13.04	5.89	0.18	0.18	65.51	101.84
1305	13.05	5.76	0.17	0.17	65.92	101.54
1306	13.06	5.62	0.16	0.16	66.46	101.16
1307	13.07	5.46	0.15	0.15	67.07	100.75
1308	13.08	5.30	0.15	0.15	67.73	100.31
1309	13.09	5.14	0.14	0.14	68.42	99.87
1310	13.10	4.99	0.13	0.13	69.10	99.46
1311	13.11	4.86	0.13	0.13	69.73	99.08
1312	13.12	4.76	0.12	0.12	70.50	98.72
1313	13.13	4.60	0.12	0.12	71.53	98.30
1314	13.14	4.39	0.11	0.11	72.98	97.78
1315	13.15	4.17	0.10	0.10	74.77	97.16
1316	13.16	3.93	0.10	0.10	76.88	96.47
1317	13.17	3.68	0.09	0.09	79.26	95.73
1318	13.18	3.45	0.08	0.08	81.85	94.98
1319	13.19	3.24	0.08	0.08	84.48	94.27
1320	13.20	3.06	0.07	0.07	86.77	93.68
1321	13.21	2.96	0.07	0.07	88.47	93.25
1322	13.22	2.90	0.07	0.07	89.69	92.95
1323	13.23	2.83	0.06	0.06	90.85	92.67
1324	13.24	2.76	0.06	0.06	92.21	92.34
1325	13.25	2.67	0.06	0.06	93.71	91.99
1326	13.26	2.59	0.06	0.06	95.30	91.64
1327	13.27	2.52	0.05	0.05	96.89	91.29
1328	13.28	2.45	0.05	0.05	98.38	90.98
1329	13.29	2.40	0.05	0.05	100.00	90.79
1330	13.30	2.39	0.05	0.05	100.00	90.72
1331	13.31	2.39	0.05	0.05	100.00	90.75
1332	13.32	2.39	0.05	0.05	100.00	90.81
1333	13.33	2.39	0.05	0.05	100.00	90.87
1334	13.34	2.39	0.05	0.05	100.00	90.93
1335	13.35	2.39	0.05	0.05	100.00	90.99
1336	13.36	2.39	0.05	0.05	100.00	91.04
1337	13.37	2.39	0.05	0.05	100.00	91.12
1338	13.38	2.40	0.06	0.06	100.00	91.35
1339	13.39	2.51	0.06	0.06	98.38	91.78
1340	13.40	2.65	0.06	0.06	95.69	92.40
1341	13.41	2.80	0.07	0.07	92.96	93.07
1342	13.42	2.96	0.07	0.07	90.38	93.75
1343	13.43	3.12	0.08	0.08	88.05	94.40
1344	13.44	3.28	0.08	0.08	86.03	94.99

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1345	13.45	3.42	0.09	0.09	84.37	95.51
1346	13.46	3.54	0.09	0.09	82.94	95.96
1347	13.47	3.66	0.10	0.10	81.43	96.42
1348	13.48	3.84	0.10	0.10	79.67	96.94
1349	13.49	4.05	0.11	0.11	77.70	97.55
1350	13.50	4.28	0.12	0.12	75.73	98.19
1351	13.51	4.53	0.13	0.13	73.87	98.83
1352	13.52	4.77	0.14	0.14	72.19	99.43
1353	13.53	4.99	0.14	0.14	70.75	99.98
1354	13.54	5.19	0.15	0.15	69.59	100.44
1355	13.55	5.36	0.16	0.16	68.96	100.72
1356	13.56	5.35	0.16	0.16	68.85	100.83
1357	13.57	5.30	0.16	0.16	69.18	100.81
1358	13.58	5.25	0.16	0.16	69.62	100.76
1359	13.59	5.20	0.16	0.16	70.10	100.71
1360	13.60	5.15	0.16	0.16	70.59	100.65
1361	13.61	5.09	0.15	0.15	71.08	100.60
1362	13.62	5.05	0.15	0.15	71.54	100.55
1363	13.63	5.00	0.15	0.15	71.94	100.51
1364	13.64	4.98	0.15	0.15	72.29	100.53
1365	13.65	4.98	0.16	0.16	72.63	100.61
1366	13.66	4.98	0.16	0.16	73.00	100.75
1367	13.67	4.98	0.16	0.16	73.41	100.90
1368	13.68	4.98	0.17	0.17	73.84	101.06
1369	13.69	4.98	0.17	0.17	74.26	101.21
1370	13.70	4.98	0.17	0.17	74.66	101.36
1371	13.71	4.98	0.18	0.18	75.02	101.49
1372	13.72	4.98	0.18	0.18	75.18	101.61
1373	13.73	5.02	0.18	0.18	74.98	101.75
1374	13.74	5.12	0.19	0.19	74.41	101.94
1375	13.75	5.24	0.19	0.19	73.62	102.16
1376	13.76	5.37	0.19	0.19	72.78	102.40
1377	13.77	5.50	0.20	0.20	71.94	102.65
1378	13.78	5.64	0.20	0.20	71.14	102.88
1379	13.79	5.76	0.21	0.21	70.42	103.10
1380	13.80	5.87	0.21	0.21	69.80	103.29
1381	13.81	5.96	0.22	0.22	69.55	103.34
1382	13.82	5.88	0.21	0.21	69.67	103.23
1383	13.83	5.76	0.21	0.21	70.18	102.95
1384	13.84	5.61	0.20	0.20	70.84	102.61
1385	13.85	5.45	0.19	0.19	71.58	102.23
1386	13.86	5.29	0.18	0.18	72.38	101.84
1387	13.87	5.13	0.17	0.17	73.21	101.44
1388	13.88	4.98	0.17	0.17	74.01	101.07
1389	13.89	4.86	0.16	0.16	74.76	100.74
1390	13.90	4.76	0.16	0.16	75.59	100.49
1391	13.91	4.65	0.15	0.15	76.62	100.28
1392	13.92	4.51	0.15	0.15	77.95	100.06

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1393	13.93	4.36	0.15	0.15	79.53	99.80
1394	13.94	4.20	0.14	0.14	81.29	99.51
1395	13.95	4.04	0.14	0.14	83.18	99.20
1396	13.96	3.88	0.13	0.13	85.09	98.90
1397	13.97	3.74	0.13	0.13	86.93	98.61
1398	13.98	3.63	0.13	0.13	88.39	98.41
1399	13.99	3.58	0.13	0.13	89.35	98.36
1400	14.00	3.58	0.13	0.13	89.90	98.44
1401	14.01	3.58	0.13	0.13	90.34	98.58
1402	14.02	3.58	0.14	0.14	90.82	98.74
1403	14.03	3.58	0.14	0.14	91.32	98.90
1404	14.04	3.58	0.14	0.14	91.80	99.05
1405	14.05	3.58	0.14	0.14	92.24	99.19
1406	14.06	3.58	0.15	0.15	92.63	99.31
1407	14.07	3.58	0.15	0.15	92.59	99.51
1408	14.08	3.68	0.15	0.15	92.01	99.83
1409	14.09	3.80	0.16	0.16	90.93	100.30
1410	14.10	3.95	0.17	0.17	89.72	100.83
1411	14.11	4.11	0.19	0.19	88.52	101.39
1412	14.12	4.27	0.20	0.20	87.39	101.94
1413	14.13	4.43	0.21	0.21	86.37	102.45
1414	14.14	4.58	0.22	0.22	85.50	102.91
1415	14.15	4.70	0.23	0.23	84.76	103.30
1416	14.16	4.81	0.24	0.24	83.94	103.67
1417	14.17	4.98	0.25	0.25	82.94	104.08
1418	14.18	5.18	0.26	0.26	81.73	104.57
1419	14.19	5.41	0.28	0.28	80.45	105.09
1420	14.20	5.65	0.30	0.30	79.21	105.63
1421	14.21	5.90	0.32	0.32	78.06	106.15
1422	14.22	6.13	0.33	0.33	77.04	106.62
1423	14.23	6.34	0.35	0.35	76.18	107.04
1424	14.24	6.51	0.36	0.36	75.46	107.37
1425	14.25	6.66	0.37	0.37	74.72	107.66
1426	14.26	6.84	0.38	0.38	73.88	107.93
1427	14.27	7.05	0.39	0.39	72.92	108.23
1428	14.28	7.28	0.41	0.41	71.90	108.54
1429	14.29	7.53	0.42	0.42	70.90	108.86
1430	14.30	7.77	0.43	0.43	69.96	109.17
1431	14.31	7.99	0.45	0.45	69.12	109.45
1432	14.32	8.19	0.46	0.46	68.42	109.69
1433	14.33	8.35	0.47	0.47	67.87	109.87
1434	14.34	8.46	0.47	0.47	67.39	110.01
1435	14.35	8.59	0.48	0.48	66.92	110.14
1436	14.36	8.73	0.49	0.49	66.39	110.28
1437	14.37	8.89	0.49	0.49	65.83	110.44
1438	14.38	9.06	0.50	0.50	65.28	110.59
1439	14.39	9.21	0.51	0.51	64.75	110.74
1440	14.40	9.36	0.52	0.52	64.28	110.87

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1441	14.41	9.48	0.52	0.52	63.94	110.97
1442	14.42	9.54	0.52	0.52	63.88	111.03
1443	14.43	9.49	0.53	0.53	64.09	111.06
1444	14.44	9.42	0.53	0.53	64.52	111.07
1445	14.45	9.34	0.53	0.53	65.00	111.08
1446	14.46	9.26	0.53	0.53	65.50	111.09
1447	14.47	9.18	0.53	0.53	66.02	111.10
1448	14.48	9.10	0.54	0.54	66.51	111.10
1449	14.49	9.04	0.54	0.54	66.95	111.10
1450	14.50	8.98	0.54	0.54	67.46	111.07
1451	14.51	8.82	0.53	0.53	68.23	110.96
1452	14.52	8.54	0.52	0.52	69.37	110.76
1453	14.53	8.21	0.51	0.51	70.87	110.48
1454	14.54	7.84	0.50	0.50	72.61	110.15
1455	14.55	7.46	0.48	0.48	74.52	109.79
1456	14.56	7.09	0.46	0.46	76.54	109.41
1457	14.57	6.74	0.45	0.45	78.56	109.03
1458	14.58	6.43	0.43	0.43	80.44	108.67
1459	14.59	6.18	0.42	0.42	81.90	108.40
1460	14.60	6.07	0.41	0.41	83.01	108.18
1461	14.61	5.94	0.41	0.41	83.92	108.00
1462	14.62	5.80	0.40	0.40	84.98	107.79
1463	14.63	5.64	0.39	0.39	86.17	107.56
1464	14.64	5.47	0.38	0.38	87.43	107.32
1465	14.65	5.32	0.37	0.37	88.70	107.07
1466	14.66	5.17	0.36	0.36	89.92	106.84
1467	14.67	5.05	0.35	0.35	90.87	106.66
1468	14.68	5.00	0.35	0.35	91.13	106.62
1469	14.69	5.09	0.36	0.36	90.69	106.72
1470	14.70	5.21	0.36	0.36	89.75	106.91
1471	14.71	5.33	0.37	0.37	88.73	107.12
1472	14.72	5.47	0.38	0.38	87.69	107.33
1473	14.73	5.60	0.39	0.39	86.69	107.55
1474	14.74	5.73	0.40	0.40	85.77	107.74
1475	14.75	5.85	0.40	0.40	84.98	107.91
1476	14.76	5.94	0.41	0.41	84.42	108.03
1477	14.77	5.97	0.41	0.41	84.10	108.07
1478	14.78	5.97	0.41	0.41	83.96	108.06
1479	14.79	5.97	0.41	0.41	83.87	108.02
1480	14.80	5.97	0.40	0.40	83.76	107.98
1481	14.81	5.97	0.40	0.40	83.64	107.94
1482	14.82	5.97	0.40	0.40	83.53	107.90
1483	14.83	5.97	0.40	0.40	83.42	107.86
1484	14.84	5.97	0.39	0.39	83.33	107.83
1485	14.85	5.97	0.39	0.39	83.03	107.85
1486	14.86	6.07	0.40	0.40	82.44	107.93
1487	14.87	6.20	0.40	0.40	81.53	108.08
1488	14.88	6.35	0.41	0.41	80.51	108.25

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1489	14.89	6.51	0.42	0.42	79.45	108.42
1490	14.90	6.67	0.42	0.42	78.40	108.59
1491	14.91	6.83	0.43	0.43	77.42	108.74
1492	14.92	6.98	0.43	0.43	76.55	108.88
1493	14.93	7.10	0.44	0.44	75.82	109.00
1494	14.94	7.20	0.44	0.44	75.16	109.10
1495	14.95	7.31	0.44	0.44	74.49	109.20
1496	14.96	7.45	0.45	0.45	73.72	109.31
1497	14.97	7.60	0.45	0.45	72.87	109.44
1498	14.98	7.76	0.46	0.46	72.00	109.56
1499	14.99	7.92	0.46	0.46	71.14	109.68
1500	15.00	8.08	0.47	0.47	70.35	109.79
1501	15.01	8.22	0.47	0.47	69.66	109.89
1502	15.02	8.33	0.47	0.47	69.28	109.93
1503	15.03	8.29	0.47	0.47	69.33	109.88
1504	15.04	8.14	0.46	0.46	69.79	109.74
1505	15.05	7.98	0.45	0.45	70.46	109.55
1506	15.06	7.79	0.44	0.44	71.23	109.34
1507	15.07	7.60	0.43	0.43	72.05	109.12
1508	15.08	7.42	0.42	0.42	72.88	108.89
1509	15.09	7.24	0.41	0.41	73.69	108.67
1510	15.10	7.09	0.41	0.41	74.42	108.48
1511	15.11	6.97	0.40	0.40	74.87	108.41
1512	15.12	7.02	0.41	0.41	75.05	108.46
1513	15.13	7.08	0.42	0.42	75.00	108.63
1514	15.14	7.16	0.42	0.42	74.95	108.82
1515	15.15	7.24	0.44	0.44	74.89	109.02
1516	15.16	7.32	0.45	0.45	74.83	109.23
1517	15.17	7.40	0.46	0.46	74.78	109.42
1518	15.18	7.47	0.47	0.47	74.74	109.60
1519	15.19	7.53	0.48	0.48	74.62	109.77
1520	15.20	7.63	0.48	0.48	74.20	109.98
1521	15.21	7.86	0.50	0.50	73.43	110.26
1522	15.22	8.15	0.52	0.52	72.39	110.61
1523	15.23	8.47	0.54	0.54	71.29	111.00
1524	15.24	8.80	0.56	0.56	70.19	111.39
1525	15.25	9.14	0.59	0.59	69.16	111.76
1526	15.26	9.45	0.61	0.61	68.24	112.11
1527	15.27	9.74	0.63	0.63	67.46	112.41
1528	15.28	9.97	0.64	0.64	66.74	112.65
1529	15.29	10.20	0.66	0.66	65.96	112.87
1530	15.30	10.51	0.67	0.67	65.01	113.09
1531	15.31	10.87	0.69	0.69	63.90	113.34
1532	15.32	11.26	0.70	0.70	62.74	113.59
1533	15.33	11.67	0.72	0.72	61.59	113.84
1534	15.34	12.07	0.73	0.73	60.50	114.08
1535	15.35	12.44	0.75	0.75	59.53	114.29
1536	15.36	12.77	0.76	0.76	58.72	114.46

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1537	15.37	13.02	0.77	0.77	58.04	114.60
1538	15.38	13.24	0.78	0.78	57.40	114.72
1539	15.39	13.52	0.78	0.78	56.72	114.83
1540	15.40	13.83	0.79	0.79	55.95	114.96
1541	15.41	14.17	0.80	0.80	55.14	115.09
1542	15.42	14.51	0.81	0.81	54.35	115.22
1543	15.43	14.84	0.81	0.81	53.63	115.34
1544	15.44	15.14	0.82	0.82	52.99	115.44
1545	15.45	15.40	0.82	0.82	52.54	115.49
1546	15.46	15.44	0.82	0.82	52.44	115.44
1547	15.47	15.12	0.80	0.80	52.69	115.27
1548	15.48	14.74	0.78	0.78	53.18	115.00
1549	15.49	14.32	0.75	0.75	53.76	114.70
1550	15.50	13.87	0.73	0.73	54.39	114.37
1551	15.51	13.43	0.70	0.70	55.09	114.03
1552	15.52	13.01	0.68	0.68	55.79	113.70
1553	15.53	12.63	0.66	0.66	56.44	113.40
1554	15.54	12.32	0.64	0.64	57.05	113.15
1555	15.55	12.07	0.63	0.63	57.69	112.93
1556	15.56	11.76	0.61	0.61	58.44	112.71
1557	15.57	11.40	0.60	0.60	59.36	112.46
1558	15.58	11.01	0.58	0.58	60.41	112.17
1559	15.59	10.60	0.57	0.57	61.54	111.86
1560	15.60	10.20	0.55	0.55	62.72	111.54
1561	15.61	9.83	0.53	0.53	63.86	111.24
1562	15.62	9.50	0.52	0.52	64.91	110.96
1563	15.63	9.26	0.51	0.51	65.63	110.79
1564	15.64	9.23	0.51	0.51	66.07	110.72
1565	15.65	9.20	0.51	0.51	66.31	110.74
1566	15.66	9.16	0.51	0.51	66.59	110.75
1567	15.67	9.12	0.51	0.51	66.89	110.76
1568	15.68	9.08	0.51	0.51	67.19	110.78
1569	15.69	9.04	0.52	0.52	67.48	110.79
1570	15.70	9.00	0.52	0.52	67.75	110.80
1571	15.71	8.97	0.52	0.52	67.99	110.81
1572	15.72	8.94	0.52	0.52	68.24	110.80
1573	15.73	8.88	0.52	0.52	68.54	110.78
1574	15.74	8.81	0.52	0.52	68.91	110.75
1575	15.75	8.74	0.52	0.52	69.32	110.71
1576	15.76	8.66	0.51	0.51	69.75	110.67
1577	15.77	8.58	0.51	0.51	70.19	110.63
1578	15.78	8.50	0.51	0.51	70.61	110.59
1579	15.79	8.43	0.51	0.51	70.99	110.56
1580	15.80	8.37	0.51	0.51	71.30	110.52
1581	15.81	8.33	0.51	0.51	71.57	110.47
1582	15.82	8.26	0.50	0.50	71.84	110.41
1583	15.83	8.19	0.50	0.50	72.14	110.33
1584	15.84	8.11	0.50	0.50	72.48	110.24

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1585	15.85	8.03	0.49	0.49	72.83	110.16
1586	15.86	7.95	0.49	0.49	73.18	110.07
1587	15.87	7.88	0.48	0.48	73.51	109.98
1588	15.88	7.81	0.48	0.48	73.80	109.91
1589	15.89	7.76	0.48	0.48	74.02	109.83
1590	15.90	7.71	0.47	0.47	74.19	109.73
1591	15.91	7.64	0.46	0.46	74.35	109.61
1592	15.92	7.57	0.46	0.46	74.52	109.46
1593	15.93	7.49	0.45	0.45	74.72	109.30
1594	15.94	7.41	0.44	0.44	74.91	109.14
1595	15.95	7.33	0.43	0.43	75.11	108.98
1596	15.96	7.26	0.42	0.42	75.30	108.83
1597	15.97	7.20	0.42	0.42	75.43	108.72
1598	15.98	7.17	0.41	0.41	75.48	108.64
1599	15.99	7.17	0.41	0.41	75.44	108.60
1600	16.00	7.17	0.41	0.41	75.34	108.56
1601	16.01	7.17	0.41	0.41	75.23	108.52
1602	16.02	7.17	0.41	0.41	75.11	108.47
1603	16.03	7.17	0.40	0.40	74.99	108.43
1604	16.04	7.17	0.40	0.40	74.88	108.39
1605	16.05	7.17	0.40	0.40	74.78	108.35
1606	16.06	7.17	0.40	0.40	74.74	108.33
1607	16.07	7.17	0.40	0.40	74.77	108.33
1608	16.08	7.17	0.40	0.40	74.86	108.36
1609	16.09	7.17	0.40	0.40	74.98	108.40
1610	16.10	7.17	0.40	0.40	75.11	108.44
1611	16.11	7.17	0.41	0.41	75.24	108.48
1612	16.12	7.17	0.41	0.41	75.38	108.52
1613	16.13	7.17	0.41	0.41	75.50	108.55
1614	16.14	7.17	0.41	0.41	75.61	108.58
1615	16.15	7.17	0.41	0.41	75.73	108.62
1616	16.16	7.17	0.42	0.42	75.88	108.67
1617	16.17	7.17	0.42	0.42	76.07	108.73
1618	16.18	7.17	0.42	0.42	76.29	108.80
1619	16.19	7.17	0.43	0.43	76.52	108.87
1620	16.20	7.17	0.43	0.43	76.75	108.94
1621	16.21	7.17	0.44	0.44	76.98	109.01
1622	16.22	7.17	0.44	0.44	77.18	109.07
1623	16.23	7.17	0.44	0.44	77.21	109.16
1624	16.24	7.25	0.45	0.45	76.83	109.33
1625	16.25	7.48	0.47	0.47	76.00	109.61
1626	16.26	7.76	0.48	0.48	74.88	109.98
1627	16.27	8.07	0.51	0.51	73.70	110.38
1628	16.28	8.39	0.53	0.53	72.53	110.78
1629	16.29	8.72	0.55	0.55	71.45	111.16
1630	16.30	9.02	0.57	0.57	70.48	111.51
1631	16.31	9.29	0.59	0.59	69.66	111.81
1632	16.32	9.51	0.60	0.60	68.91	112.07

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1633	16.33	9.75	0.62	0.62	68.07	112.30
1634	16.34	10.06	0.63	0.63	67.05	112.55
1635	16.35	10.43	0.65	0.65	65.89	112.83
1636	16.36	10.82	0.67	0.67	64.69	113.11
1637	16.37	11.23	0.68	0.68	63.50	113.40
1638	16.38	11.63	0.70	0.70	62.40	113.66
1639	16.39	12.00	0.72	0.72	61.42	113.90
1640	16.40	12.32	0.73	0.73	60.60	114.09
1641	16.41	12.57	0.74	0.74	59.81	114.26
1642	16.42	12.89	0.75	0.75	58.93	114.42
1643	16.43	13.29	0.76	0.76	57.88	114.59
1644	16.44	13.74	0.77	0.77	56.72	114.77
1645	16.45	14.23	0.78	0.78	55.53	114.95
1646	16.46	14.71	0.79	0.79	54.36	115.12
1647	16.47	15.18	0.80	0.80	53.32	115.28
1648	16.48	15.61	0.81	0.81	52.40	115.40
1649	16.49	15.97	0.81	0.81	51.61	115.51
1650	16.50	16.32	0.82	0.82	50.81	115.65
1651	16.51	16.84	0.83	0.83	49.90	115.82
1652	16.52	17.47	0.84	0.84	48.83	116.02
1653	16.53	18.17	0.86	0.86	47.69	116.23
1654	16.54	18.90	0.87	0.87	46.53	116.42
1655	16.55	19.63	0.88	0.88	45.42	116.60
1656	16.56	20.31	0.89	0.89	44.40	116.75
1657	16.57	20.92	0.90	0.90	43.53	116.88
1658	16.58	21.42	0.90	0.90	42.90	116.93
1659	16.59	21.53	0.89	0.89	42.46	116.91
1660	16.60	21.58	0.88	0.88	42.14	116.81
1661	16.61	21.64	0.86	0.86	41.78	116.69
1662	16.62	21.71	0.85	0.85	41.40	116.55
1663	16.63	21.77	0.83	0.83	40.99	116.41
1664	16.64	21.83	0.81	0.81	40.60	116.26
1665	16.65	21.89	0.79	0.79	40.22	116.12
1666	16.66	21.94	0.78	0.78	39.92	115.99
1667	16.67	21.95	0.77	0.77	39.81	115.87
1668	16.68	21.68	0.76	0.76	39.89	115.74
1669	16.69	21.35	0.75	0.75	40.15	115.58
1670	16.70	20.97	0.73	0.73	40.44	115.40
1671	16.71	20.57	0.72	0.72	40.76	115.20
1672	16.72	20.16	0.70	0.70	41.10	114.99
1673	16.73	19.77	0.69	0.69	41.43	114.79
1674	16.74	19.42	0.67	0.67	41.74	114.61
1675	16.75	19.12	0.66	0.66	42.05	114.47
1676	16.76	18.89	0.66	0.66	42.44	114.38
1677	16.77	18.60	0.66	0.66	42.95	114.34
1678	16.78	18.27	0.66	0.66	43.60	114.32
1679	16.79	17.89	0.66	0.66	44.34	114.28
1680	16.80	17.50	0.66	0.66	45.11	114.23

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1681	16.81	17.12	0.66	0.66	45.89	114.18
1682	16.82	16.75	0.66	0.66	46.64	114.12
1683	16.83	16.43	0.66	0.66	47.32	114.06
1684	16.84	16.17	0.66	0.66	47.98	114.00
1685	16.85	15.82	0.66	0.66	48.77	113.92
1686	16.86	15.35	0.65	0.65	49.77	113.80
1687	16.87	14.80	0.65	0.65	50.99	113.64
1688	16.88	14.20	0.64	0.64	52.36	113.45
1689	16.89	13.59	0.63	0.63	53.82	113.24
1690	16.90	13.00	0.62	0.62	55.38	113.00
1691	16.91	12.44	0.61	0.61	56.90	112.77
1692	16.92	11.97	0.60	0.60	58.24	112.55
1693	16.93	11.63	0.59	0.59	59.29	112.40
1694	16.94	11.46	0.59	0.59	60.12	112.32
1695	16.95	11.26	0.59	0.59	60.91	112.26
1696	16.96	11.04	0.58	0.58	61.80	112.20
1697	16.97	10.79	0.58	0.58	62.78	112.12
1698	16.98	10.55	0.58	0.58	63.78	112.03
1699	16.99	10.32	0.58	0.58	64.76	111.95
1700	17.00	10.10	0.57	0.57	65.67	111.86
1701	17.01	9.93	0.57	0.57	66.31	111.80
1702	17.02	9.89	0.57	0.57	66.56	111.80
1703	17.03	9.98	0.58	0.58	66.42	111.86
1704	17.04	10.08	0.58	0.58	66.10	111.94
1705	17.05	10.20	0.59	0.59	65.74	112.04
1706	17.06	10.32	0.59	0.59	65.38	112.14
1707	17.07	10.44	0.60	0.60	65.02	112.23
1708	17.08	10.56	0.60	0.60	64.69	112.32
1709	17.09	10.66	0.61	0.61	64.40	112.40
1710	17.10	10.74	0.61	0.61	64.17	112.43
1711	17.11	10.75	0.61	0.61	63.95	112.41
1712	17.12	10.75	0.60	0.60	63.73	112.33
1713	17.13	10.75	0.59	0.59	63.46	112.23
1714	17.14	10.75	0.58	0.58	63.17	112.12
1715	17.15	10.75	0.57	0.57	62.87	112.00
1716	17.16	10.75	0.56	0.56	62.57	111.89
1717	17.17	10.75	0.56	0.56	62.29	111.78
1718	17.18	10.75	0.55	0.55	62.09	111.68
1719	17.19	10.72	0.54	0.54	62.15	111.53
1720	17.20	10.48	0.53	0.53	62.52	111.31
1721	17.21	10.19	0.51	0.51	63.18	110.99
1722	17.22	9.86	0.49	0.49	63.97	110.62
1723	17.23	9.51	0.47	0.47	64.86	110.22
1724	17.24	9.16	0.45	0.45	65.81	109.80
1725	17.25	8.82	0.43	0.43	66.78	109.38
1726	17.26	8.52	0.41	0.41	67.71	108.99
1727	17.27	8.26	0.40	0.40	68.58	108.66
1728	17.28	8.05	0.38	0.38	69.50	108.37

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1729	17.29	7.80	0.37	0.37	70.62	108.07
1730	17.30	7.49	0.36	0.36	72.03	107.71
1731	17.31	7.15	0.35	0.35	73.69	107.31
1732	17.32	6.80	0.33	0.33	75.55	106.86
1733	17.33	6.45	0.32	0.32	77.55	106.39
1734	17.34	6.13	0.30	0.30	79.58	105.92
1735	17.35	5.84	0.29	0.29	81.52	105.49
1736	17.36	5.60	0.28	0.28	82.86	105.21
1737	17.37	5.59	0.28	0.28	83.51	105.11
1738	17.38	5.61	0.28	0.28	83.56	105.17
1739	17.39	5.63	0.28	0.28	83.53	105.26
1740	17.40	5.66	0.29	0.29	83.50	105.35
1741	17.41	5.69	0.29	0.29	83.47	105.44
1742	17.42	5.71	0.29	0.29	83.44	105.53
1743	17.43	5.74	0.30	0.30	83.42	105.62
1744	17.44	5.76	0.30	0.30	83.40	105.69
1745	17.45	5.78	0.30	0.30	83.39	105.75
1746	17.46	5.79	0.30	0.30	83.39	105.82
1747	17.47	5.82	0.31	0.31	83.39	105.90
1748	17.48	5.84	0.31	0.31	83.38	106.00
1749	17.49	5.87	0.31	0.31	83.38	106.09
1750	17.50	5.90	0.32	0.32	83.38	106.19
1751	17.51	5.92	0.32	0.32	83.37	106.28
1752	17.52	5.95	0.32	0.32	83.37	106.37
1753	17.53	5.97	0.33	0.33	83.28	106.46
1754	17.54	6.02	0.33	0.33	82.99	106.61
1755	17.55	6.14	0.34	0.34	82.47	106.83
1756	17.56	6.29	0.35	0.35	81.79	107.10
1757	17.57	6.44	0.36	0.36	81.07	107.40
1758	17.58	6.60	0.38	0.38	80.36	107.71
1759	17.59	6.77	0.39	0.39	79.69	108.00
1760	17.60	6.92	0.40	0.40	79.09	108.27
1761	17.61	7.05	0.41	0.41	78.58	108.50
1762	17.62	7.16	0.42	0.42	78.14	108.70
1763	17.63	7.26	0.43	0.43	77.73	108.89
1764	17.64	7.38	0.44	0.44	77.26	109.10
1765	17.65	7.53	0.45	0.45	76.74	109.34
1766	17.66	7.69	0.46	0.46	76.19	109.59
1767	17.67	7.85	0.47	0.47	75.66	109.84
1768	17.68	8.01	0.49	0.49	75.16	110.08
1769	17.69	8.16	0.50	0.50	74.71	110.30
1770	17.70	8.28	0.51	0.51	74.38	110.47
1771	17.71	8.35	0.52	0.52	74.30	110.56
1772	17.72	8.30	0.51	0.51	74.47	110.57
1773	17.73	8.23	0.51	0.51	74.84	110.52
1774	17.74	8.15	0.51	0.51	75.27	110.46
1775	17.75	8.07	0.51	0.51	75.72	110.40
1776	17.76	7.99	0.50	0.50	76.17	110.34

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1777	17.77	7.91	0.50	0.50	76.62	110.28
1778	17.78	7.84	0.50	0.50	77.02	110.23
1779	17.79	7.79	0.50	0.50	77.38	110.18
1780	17.80	7.74	0.50	0.50	77.73	110.15
1781	17.81	7.68	0.50	0.50	78.13	110.11
1782	17.82	7.61	0.49	0.49	78.60	110.06
1783	17.83	7.53	0.49	0.49	79.12	110.01
1784	17.84	7.45	0.49	0.49	79.67	109.96
1785	17.85	7.37	0.49	0.49	80.22	109.90
1786	17.86	7.29	0.49	0.49	80.75	109.85
1787	17.87	7.22	0.48	0.48	81.21	109.80
1788	17.88	7.17	0.48	0.48	81.54	109.78
1789	17.89	7.17	0.49	0.49	81.76	109.79
1790	17.90	7.17	0.49	0.49	81.90	109.83
1791	17.91	7.17	0.49	0.49	82.05	109.87
1792	17.92	7.17	0.49	0.49	82.21	109.91
1793	17.93	7.17	0.50	0.50	82.37	109.96
1794	17.94	7.17	0.50	0.50	82.53	110.01
1795	17.95	7.17	0.50	0.50	82.68	110.05
1796	17.96	7.17	0.51	0.51	82.77	110.09
1797	17.97	7.18	0.51	0.51	82.67	110.14
1798	17.98	7.26	0.51	0.51	82.37	110.22
1799	17.99	7.35	0.52	0.52	81.89	110.32
1800	18.00	7.45	0.52	0.52	81.35	110.43
1801	18.01	7.56	0.53	0.53	80.80	110.55
1802	18.02	7.66	0.54	0.54	80.25	110.67
1803	18.03	7.77	0.54	0.54	79.74	110.78
1804	18.04	7.86	0.55	0.55	79.29	110.87
1805	18.05	7.94	0.55	0.55	78.70	110.99
1806	18.06	8.13	0.56	0.56	77.70	111.19
1807	18.07	8.47	0.58	0.58	76.20	111.47
1808	18.08	8.87	0.60	0.60	74.40	111.81
1809	18.09	9.31	0.62	0.62	72.53	112.16
1810	18.10	9.77	0.63	0.63	70.70	112.50
1811	18.11	10.23	0.65	0.65	69.00	112.82
1812	18.12	10.66	0.67	0.67	67.50	113.09
1813	18.13	11.03	0.68	0.68	66.24	113.32
1814	18.14	11.33	0.69	0.69	64.96	113.57
1815	18.15	11.86	0.72	0.72	63.46	113.88
1816	18.16	12.54	0.74	0.74	61.63	114.28
1817	18.17	13.33	0.77	0.77	59.64	114.70
1818	18.18	14.18	0.80	0.80	57.65	115.12
1819	18.19	15.05	0.83	0.83	55.76	115.51
1820	18.20	15.89	0.85	0.85	54.03	115.85
1821	18.21	16.67	0.87	0.87	52.59	116.13
1822	18.22	17.33	0.89	0.89	51.44	116.35
1823	18.23	17.78	0.90	0.90	50.57	116.47
1824	18.24	18.06	0.90	0.90	49.83	116.53

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1825	18.25	18.40	0.89	0.89	49.08	116.54
1826	18.26	18.78	0.89	0.89	48.24	116.55
1827	18.27	19.19	0.88	0.88	47.36	116.55
1828	18.28	19.59	0.87	0.87	46.49	116.54
1829	18.29	19.98	0.87	0.87	45.66	116.52
1830	18.30	20.33	0.86	0.86	44.92	116.49
1831	18.31	20.61	0.85	0.85	44.40	116.44
1832	18.32	20.60	0.84	0.84	44.13	116.32
1833	18.33	20.40	0.82	0.82	44.05	116.14
1834	18.34	20.15	0.79	0.79	44.04	115.91
1835	18.35	19.88	0.77	0.77	44.02	115.65
1836	18.36	19.60	0.74	0.74	44.00	115.38
1837	18.37	19.33	0.72	0.72	43.99	115.10
1838	18.38	19.07	0.70	0.70	43.97	114.84
1839	18.39	18.85	0.68	0.68	43.96	114.61
1840	18.40	18.67	0.66	0.66	44.09	114.42
1841	18.41	18.35	0.65	0.65	44.39	114.25
1842	18.42	17.95	0.64	0.64	44.91	114.07
1843	18.43	17.48	0.63	0.63	45.54	113.87
1844	18.44	16.98	0.62	0.62	46.24	113.64
1845	18.45	16.47	0.60	0.60	46.97	113.40
1846	18.46	15.98	0.59	0.59	47.72	113.15
1847	18.47	15.52	0.57	0.57	48.43	112.92
1848	18.48	15.14	0.56	0.56	49.07	112.72
1849	18.49	14.82	0.56	0.56	49.75	112.54
1850	18.50	14.42	0.55	0.55	50.57	112.37
1851	18.51	13.94	0.54	0.54	51.60	112.16
1852	18.52	13.40	0.53	0.53	52.81	111.91
1853	18.53	12.83	0.51	0.51	54.16	111.62
1854	18.54	12.25	0.50	0.50	55.64	111.32
1855	18.55	11.71	0.49	0.49	57.12	111.01
1856	18.56	11.22	0.47	0.47	58.53	110.71
1857	18.57	10.81	0.46	0.46	59.72	110.47
1858	18.58	10.55	0.46	0.46	60.74	110.26
1859	18.59	10.29	0.45	0.45	61.73	110.08
1860	18.60	9.97	0.44	0.44	62.86	109.88
1861	18.61	9.63	0.43	0.43	64.15	109.64
1862	18.62	9.27	0.42	0.42	65.55	109.37
1863	18.63	8.92	0.41	0.41	67.01	109.10
1864	18.64	8.59	0.40	0.40	68.43	108.83
1865	18.65	8.30	0.39	0.39	69.74	108.59
1866	18.66	8.07	0.38	0.38	70.82	108.39
1867	18.67	7.92	0.38	0.38	71.77	108.21
1868	18.68	7.74	0.37	0.37	72.73	108.05
1869	18.69	7.53	0.37	0.37	73.87	107.85
1870	18.70	7.30	0.36	0.36	75.14	107.62
1871	18.71	7.07	0.35	0.35	76.50	107.39
1872	18.72	6.85	0.34	0.34	77.87	107.15

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1873	18.73	6.64	0.34	0.34	79.18	106.92
1874	18.74	6.47	0.33	0.33	80.31	106.73
1875	18.75	6.35	0.33	0.33	81.22	106.60
1876	18.76	6.28	0.32	0.32	82.01	106.51
1877	18.77	6.18	0.32	0.32	82.82	106.44
1878	18.78	6.08	0.32	0.32	83.75	106.37
1879	18.79	5.97	0.32	0.32	84.75	106.28
1880	18.80	5.87	0.32	0.32	85.77	106.19
1881	18.81	5.76	0.32	0.32	86.76	106.10
1882	18.82	5.67	0.31	0.31	87.67	106.02
1883	18.83	5.60	0.31	0.31	88.36	105.97
1884	18.84	5.57	0.31	0.31	88.80	105.96
1885	18.85	5.57	0.31	0.31	89.06	106.01
1886	18.86	5.57	0.32	0.32	89.29	106.08
1887	18.87	5.57	0.32	0.32	89.54	106.15
1888	18.88	5.57	0.32	0.32	89.80	106.23
1889	18.89	5.57	0.33	0.33	90.05	106.30
1890	18.90	5.57	0.33	0.33	90.29	106.37
1891	18.91	5.57	0.33	0.33	90.49	106.43
1892	18.92	5.57	0.34	0.34	90.46	106.51
1893	18.93	5.64	0.34	0.34	90.15	106.62
1894	18.94	5.73	0.35	0.35	89.56	106.78
1895	18.95	5.83	0.35	0.35	88.91	106.96
1896	18.96	5.94	0.36	0.36	88.22	107.16
1897	18.97	6.04	0.37	0.37	87.55	107.35
1898	18.98	6.15	0.38	0.38	86.92	107.53
1899	18.99	6.25	0.38	0.38	86.36	107.70
1900	19.00	6.33	0.39	0.39	85.89	107.83
1901	19.01	6.39	0.39	0.39	85.42	107.94
1902	19.02	6.47	0.40	0.40	84.90	108.04
1903	19.03	6.56	0.40	0.40	84.28	108.15
1904	19.04	6.66	0.40	0.40	83.59	108.27
1905	19.05	6.77	0.41	0.41	82.88	108.39
1906	19.06	6.88	0.41	0.41	82.19	108.50
1907	19.07	6.98	0.42	0.42	81.55	108.61
1908	19.08	7.07	0.42	0.42	80.99	108.71
1909	19.09	7.15	0.42	0.42	80.59	108.77
1910	19.10	7.17	0.42	0.42	80.33	108.78
1911	19.11	7.17	0.42	0.42	80.18	108.74
1912	19.12	7.17	0.42	0.42	80.03	108.69
1913	19.13	7.17	0.41	0.41	79.87	108.63
1914	19.14	7.17	0.41	0.41	79.70	108.57
1915	19.15	7.17	0.41	0.41	79.53	108.52
1916	19.16	7.17	0.40	0.40	79.38	108.46
1917	19.17	7.17	0.40	0.40	79.25	108.41
1918	19.18	7.17	0.40	0.40	79.27	108.34
1919	19.19	7.10	0.39	0.39	79.46	108.24
1920	19.20	7.01	0.39	0.39	79.83	108.09

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1921	19.21	6.91	0.38	0.38	80.27	107.92
1922	19.22	6.80	0.37	0.37	80.76	107.73
1923	19.23	6.69	0.36	0.36	81.26	107.54
1924	19.24	6.59	0.36	0.36	81.76	107.35
1925	19.25	6.49	0.35	0.35	82.23	107.17
1926	19.26	6.41	0.34	0.34	82.65	107.02
1927	19.27	6.35	0.34	0.34	83.04	106.88
1928	19.28	6.27	0.33	0.33	83.47	106.73
1929	19.29	6.18	0.33	0.33	83.97	106.56
1930	19.30	6.08	0.32	0.32	84.55	106.36
1931	19.31	5.97	0.31	0.31	85.17	106.15
1932	19.32	5.86	0.31	0.31	85.82	105.94
1933	19.33	5.76	0.30	0.30	86.46	105.73
1934	19.34	5.67	0.29	0.29	87.04	105.55
1935	19.35	5.59	0.29	0.29	87.42	105.41
1936	19.36	5.57	0.29	0.29	87.54	105.31
1937	19.37	5.57	0.28	0.28	87.43	105.24
1938	19.38	5.57	0.28	0.28	87.22	105.17
1939	19.39	5.57	0.28	0.28	86.99	105.09
1940	19.40	5.57	0.27	0.27	86.75	105.01
1941	19.41	5.57	0.27	0.27	86.51	104.92
1942	19.42	5.57	0.27	0.27	86.29	104.85
1943	19.43	5.57	0.27	0.27	86.10	104.78
1944	19.44	5.57	0.26	0.26	85.93	104.72
1945	19.45	5.57	0.26	0.26	85.77	104.66
1946	19.46	5.57	0.26	0.26	85.58	104.59
1947	19.47	5.57	0.26	0.26	85.36	104.52
1948	19.48	5.57	0.25	0.25	85.12	104.43
1949	19.49	5.57	0.25	0.25	84.88	104.35
1950	19.50	5.57	0.25	0.25	84.64	104.26
1951	19.51	5.57	0.25	0.25	84.43	104.19
1952	19.52	5.57	0.24	0.24	84.25	104.12
1953	19.53	5.57	0.24	0.24	84.10	104.07
1954	19.54	5.57	0.24	0.24	83.97	104.02
1955	19.55	5.57	0.24	0.24	83.82	103.96
1956	19.56	5.57	0.24	0.24	83.66	103.90
1957	19.57	5.57	0.23	0.23	83.48	103.84
1958	19.58	5.57	0.23	0.23	83.30	103.77
1959	19.59	5.57	0.23	0.23	83.13	103.71
1960	19.60	5.57	0.23	0.23	82.99	103.66
1961	19.61	5.57	0.23	0.23	82.90	103.61
1962	19.62	5.57	0.23	0.23	82.88	103.58
1963	19.63	5.56	0.23	0.23	82.94	103.55
1964	19.64	5.55	0.22	0.22	83.01	103.52
1965	19.65	5.53	0.22	0.22	83.10	103.49
1966	19.66	5.52	0.22	0.22	83.18	103.45
1967	19.67	5.51	0.22	0.22	83.27	103.42
1968	19.68	5.49	0.22	0.22	83.35	103.38

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1969	19.69	5.48	0.22	0.22	83.43	103.36
1970	19.70	5.47	0.22	0.22	83.72	103.31
1971	19.71	5.40	0.22	0.22	84.29	103.24
1972	19.72	5.31	0.22	0.22	85.17	103.13
1973	19.73	5.21	0.21	0.21	86.21	103.01
1974	19.74	5.11	0.21	0.21	87.35	102.88
1975	19.75	5.00	0.21	0.21	88.54	102.74
1976	19.76	4.89	0.21	0.21	89.73	102.59
1977	19.77	4.80	0.20	0.20	90.85	102.46
1978	19.78	4.72	0.20	0.20	91.28	102.47
1979	19.79	4.82	0.21	0.21	90.03	102.86
1980	19.80	5.26	0.23	0.23	87.17	103.65
1981	19.81	5.78	0.26	0.26	83.57	104.70
1982	19.82	6.36	0.29	0.29	80.20	105.77
1983	19.83	6.96	0.33	0.33	77.21	106.81
1984	19.84	7.57	0.36	0.36	74.67	107.77
1985	19.85	8.14	0.40	0.40	72.59	108.62
1986	19.86	8.65	0.43	0.43	70.94	109.32
1987	19.87	9.07	0.46	0.46	69.59	109.92
1988	19.88	9.48	0.48	0.48	68.28	110.48
1989	19.89	10.02	0.52	0.52	66.86	111.08
1990	19.90	10.65	0.55	0.55	65.32	111.75
1991	19.91	11.33	0.60	0.60	63.82	112.44
1992	19.92	12.04	0.64	0.64	62.42	113.12
1993	19.93	12.73	0.69	0.69	61.18	113.75
1994	19.94	13.37	0.73	0.73	60.13	114.30
1995	19.95	13.93	0.77	0.77	59.33	114.75
1996	19.96	14.30	0.80	0.80	59.11	114.88
1997	19.97	13.84	0.77	0.77	59.47	114.70
1998	19.98	13.27	0.73	0.73	60.39	114.23
1999	19.99	12.61	0.68	0.68	61.52	113.67
2000	20.00	11.92	0.64	0.64	62.84	113.04
2001	20.01	11.21	0.59	0.59	64.32	112.37
2002	20.02	10.54	0.55	0.55	65.89	111.69
2003	20.03	9.92	0.51	0.51	67.48	111.04
2004	20.04	9.40	0.48	0.48	68.94	110.47
2005	20.05	9.02	0.46	0.46	70.34	109.96
2006	20.06	8.61	0.44	0.44	71.85	109.46
2007	20.07	8.12	0.41	0.41	73.72	108.86
2008	20.08	7.58	0.38	0.38	76.03	108.16
2009	20.09	7.01	0.35	0.35	78.76	107.38
2010	20.10	6.45	0.32	0.32	81.88	106.53
2011	20.11	5.91	0.29	0.29	85.28	105.67
2012	20.12	5.44	0.27	0.27	88.78	104.84
2013	20.13	5.05	0.25	0.25	91.54	104.25
2014	20.14	4.96	0.25	0.25	93.22	103.96
2015	20.15	4.94	0.25	0.25	93.90	103.94
2016	20.16	4.92	0.25	0.25	94.44	103.99

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2017	20.17	4.89	0.25	0.25	95.02	104.03
2018	20.18	4.87	0.25	0.25	95.63	104.07
2019	20.19	4.84	0.25	0.25	96.22	104.11
2020	20.20	4.81	0.26	0.26	96.77	104.15
2021	20.21	4.79	0.26	0.26	97.25	104.18
2022	20.22	4.78	0.26	0.26	97.71	104.21
2023	20.23	4.76	0.26	0.26	98.19	104.25
2024	20.24	4.74	0.26	0.26	98.77	104.31
2025	20.25	4.71	0.27	0.27	100.00	104.36
2026	20.26	4.68	0.27	0.27	100.00	104.42
2027	20.27	4.66	0.27	0.27	100.00	104.48
2028	20.28	4.63	0.27	0.27	100.00	104.54
2029	20.29	4.61	0.28	0.28	100.00	104.58
2030	20.30	4.59	0.28	0.28	100.00	104.67
2031	20.31	4.64	0.28	0.28	100.00	104.90
2032	20.32	4.82	0.30	0.30	100.00	105.27
2033	20.33	5.03	0.31	0.31	98.72	105.77
2034	20.34	5.26	0.33	0.33	96.87	106.30
2035	20.35	5.50	0.35	0.35	95.11	106.84
2036	20.36	5.75	0.37	0.37	93.50	107.35
2037	20.37	5.97	0.39	0.39	92.10	107.81
2038	20.38	6.18	0.41	0.41	90.94	108.21
2039	20.39	6.34	0.43	0.43	89.84	108.56
2040	20.40	6.54	0.44	0.44	88.58	108.91
2041	20.41	6.82	0.46	0.46	87.04	109.31
2042	20.42	7.13	0.48	0.48	85.33	109.76
2043	20.43	7.48	0.51	0.51	83.61	110.23
2044	20.44	7.83	0.53	0.53	81.98	110.69
2045	20.45	8.17	0.56	0.56	80.50	111.12
2046	20.46	8.49	0.58	0.58	79.22	111.51
2047	20.47	8.77	0.60	0.60	78.16	111.83
2048	20.48	8.99	0.62	0.62	77.17	112.10
2049	20.49	9.26	0.63	0.63	76.09	112.37
2050	20.50	9.59	0.65	0.65	74.82	112.66
2051	20.51	9.97	0.67	0.67	73.45	112.98
2052	20.52	10.37	0.69	0.69	72.06	113.31
2053	20.53	10.78	0.72	0.72	70.74	113.62
2054	20.54	11.17	0.74	0.74	69.53	113.91
2055	20.55	11.52	0.75	0.75	68.49	114.16
2056	20.56	11.82	0.77	0.77	67.67	114.35
2057	20.57	12.01	0.78	0.78	66.99	114.49
2058	20.58	12.19	0.78	0.78	66.37	114.58
2059	20.59	12.40	0.79	0.79	65.68	114.67
2060	20.60	12.63	0.79	0.79	64.94	114.77
2061	20.61	12.88	0.80	0.80	64.17	114.86
2062	20.62	13.12	0.80	0.80	63.43	114.95
2063	20.63	13.35	0.81	0.81	62.74	115.03
2064	20.64	13.55	0.81	0.81	62.14	115.10

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2065	20.65	13.71	0.81	0.81	61.62	115.15
2066	20.66	13.86	0.82	0.82	61.11	115.19
2067	20.67	14.05	0.82	0.82	60.53	115.23
2068	20.68	14.27	0.82	0.82	59.86	115.28
2069	20.69	14.51	0.82	0.82	59.15	115.32
2070	20.70	14.75	0.82	0.82	58.42	115.37
2071	20.71	14.99	0.82	0.82	57.72	115.40
2072	20.72	15.21	0.82	0.82	57.08	115.43
2073	20.73	15.40	0.82	0.82	56.55	115.45
2074	20.74	15.52	0.81	0.81	56.25	115.42
2075	20.75	15.44	0.80	0.80	56.12	115.34
2076	20.76	15.34	0.79	0.79	56.12	115.22
2077	20.77	15.22	0.78	0.78	56.12	115.07
2078	20.78	15.10	0.76	0.76	56.12	114.91
2079	20.79	14.98	0.75	0.75	56.11	114.75
2080	20.80	14.86	0.73	0.73	56.11	114.60
2081	20.81	14.76	0.72	0.72	56.11	114.46
2082	20.82	14.67	0.71	0.71	56.19	114.33
2083	20.83	14.51	0.70	0.70	56.47	114.20
2084	20.84	14.22	0.69	0.69	57.00	114.03
2085	20.85	13.87	0.68	0.68	57.74	113.83
2086	20.86	13.48	0.66	0.66	58.58	113.60
2087	20.87	13.07	0.65	0.65	59.50	113.35
2088	20.88	12.67	0.63	0.63	60.44	113.09
2089	20.89	12.29	0.61	0.61	61.37	112.84
2090	20.90	11.95	0.60	0.60	62.23	112.61
2091	20.91	11.68	0.59	0.59	62.97	112.44
2092	20.92	11.52	0.59	0.59	63.65	112.32
2093	20.93	11.33	0.58	0.58	64.37	112.24
2094	20.94	11.11	0.58	0.58	65.22	112.15
2095	20.95	10.87	0.58	0.58	66.15	112.05
2096	20.96	10.63	0.57	0.57	67.14	111.94
2097	20.97	10.39	0.57	0.57	68.12	111.83
2098	20.98	10.17	0.56	0.56	69.04	111.72
2099	20.99	9.98	0.56	0.56	69.86	111.62
2100	21.00	9.83	0.55	0.55	70.60	111.52
2101	21.01	9.67	0.55	0.55	71.36	111.41
2102	21.02	9.47	0.54	0.54	72.24	111.28
2103	21.03	9.24	0.54	0.54	73.27	111.12
2104	21.04	9.00	0.53	0.53	74.40	110.95
2105	21.05	8.75	0.52	0.52	75.57	110.76
2106	21.06	8.52	0.51	0.51	76.74	110.58
2107	21.07	8.31	0.50	0.50	77.83	110.41
2108	21.08	8.13	0.50	0.50	78.72	110.27
2109	21.09	8.03	0.49	0.49	79.39	110.15
2110	21.10	7.94	0.49	0.49	79.93	110.05
2111	21.11	7.83	0.48	0.48	80.48	109.94
2112	21.12	7.71	0.48	0.48	81.10	109.81

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2113	21.13	7.59	0.47	0.47	81.76	109.68
2114	21.14	7.47	0.46	0.46	82.43	109.54
2115	21.15	7.36	0.46	0.46	83.08	109.41
2116	21.16	7.26	0.45	0.45	83.67	109.30
2117	21.17	7.18	0.45	0.45	83.70	109.29
2118	21.18	7.34	0.46	0.46	83.02	109.41
2119	21.19	7.60	0.47	0.47	81.65	109.67
2120	21.20	7.89	0.48	0.48	80.06	109.96
2121	21.21	8.21	0.50	0.50	78.44	110.27
2122	21.22	8.53	0.51	0.51	76.86	110.57
2123	21.23	8.85	0.52	0.52	75.41	110.85
2124	21.24	9.14	0.54	0.54	74.14	111.10
2125	21.25	9.40	0.55	0.55	73.03	111.32
2126	21.26	9.63	0.56	0.56	71.75	111.58
2127	21.27	10.10	0.58	0.58	70.13	111.91
2128	21.28	10.68	0.60	0.60	68.14	112.34
2129	21.29	11.34	0.63	0.63	66.06	112.78
2130	21.30	12.03	0.65	0.65	64.01	113.21
2131	21.31	12.72	0.68	0.68	62.10	113.62
2132	21.32	13.39	0.70	0.70	60.39	113.98
2133	21.33	13.99	0.72	0.72	58.94	114.28
2134	21.34	14.49	0.73	0.73	57.81	114.50
2135	21.35	14.81	0.74	0.74	56.92	114.65
2136	21.36	15.10	0.75	0.75	56.11	114.75
2137	21.37	15.46	0.75	0.75	55.23	114.85
2138	21.38	15.85	0.75	0.75	54.28	114.94
2139	21.39	16.26	0.76	0.76	53.32	115.04
2140	21.40	16.66	0.76	0.76	52.41	115.12
2141	21.41	17.04	0.76	0.76	51.58	115.19
2142	21.42	17.37	0.76	0.76	50.86	115.24
2143	21.43	17.64	0.76	0.76	50.25	115.32
2144	21.44	17.95	0.77	0.77	49.67	115.42
2145	21.45	18.36	0.78	0.78	49.04	115.57
2146	21.46	18.84	0.79	0.79	48.34	115.73
2147	21.47	19.35	0.80	0.80	47.60	115.91
2148	21.48	19.87	0.82	0.82	46.87	116.08
2149	21.49	20.38	0.83	0.83	46.18	116.23
2150	21.50	20.85	0.84	0.84	45.56	116.37
2151	21.51	21.25	0.85	0.85	45.07	116.48
2152	21.52	21.50	0.85	0.85	44.77	116.54
2153	21.53	21.51	0.85	0.85	44.62	116.55
2154	21.54	21.53	0.85	0.85	44.57	116.53
2155	21.55	21.54	0.84	0.84	44.50	116.51
2156	21.56	21.56	0.84	0.84	44.43	116.49
2157	21.57	21.58	0.84	0.84	44.36	116.47
2158	21.58	21.59	0.83	0.83	44.29	116.45
2159	21.59	21.61	0.83	0.83	44.23	116.43
2160	21.60	21.62	0.83	0.83	44.28	116.38

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2161	21.61	21.37	0.82	0.82	44.55	116.27
2162	21.62	20.81	0.80	0.80	45.10	116.07
2163	21.63	20.14	0.78	0.78	45.85	115.81
2164	21.64	19.41	0.76	0.76	46.71	115.50
2165	21.65	18.65	0.74	0.74	47.66	115.17
2166	21.66	17.90	0.71	0.71	48.65	114.83
2167	21.67	17.20	0.69	0.69	49.62	114.49
2168	21.68	16.58	0.67	0.67	50.53	114.18
2169	21.69	16.09	0.65	0.65	51.32	113.94
2170	21.70	15.75	0.64	0.64	52.07	113.75
2171	21.71	15.34	0.63	0.63	52.89	113.58
2172	21.72	14.87	0.62	0.62	53.89	113.38
2173	21.73	14.36	0.61	0.61	55.02	113.15
2174	21.74	13.84	0.60	0.60	56.23	112.91
2175	21.75	13.33	0.58	0.58	57.45	112.65
2176	21.76	12.86	0.57	0.57	58.63	112.40
2177	21.77	12.46	0.56	0.56	59.67	112.18
2178	21.78	12.16	0.55	0.55	60.63	111.99
2179	21.79	11.85	0.54	0.54	61.61	111.78
2180	21.80	11.46	0.53	0.53	62.77	111.55
2181	21.81	11.03	0.52	0.52	64.13	111.27
2182	21.82	10.57	0.50	0.50	65.65	110.96
2183	21.83	10.11	0.49	0.49	67.27	110.63
2184	21.84	9.67	0.47	0.47	68.90	110.29
2185	21.85	9.28	0.46	0.46	70.47	109.97
2186	21.86	8.95	0.44	0.44	71.82	109.70
2187	21.87	8.72	0.43	0.43	73.02	109.46
2188	21.88	8.47	0.43	0.43	74.21	109.21
2189	21.89	8.18	0.41	0.41	75.62	108.93
2190	21.90	7.85	0.40	0.40	77.26	108.60
2191	21.91	7.52	0.39	0.39	79.07	108.24
2192	21.92	7.19	0.37	0.37	80.98	107.87
2193	21.93	6.88	0.36	0.36	82.90	107.50
2194	21.94	6.60	0.35	0.35	84.70	107.17
2195	21.95	6.38	0.34	0.34	86.02	106.91
2196	21.96	6.31	0.33	0.33	86.88	106.71
2197	21.97	6.22	0.33	0.33	87.41	106.54
2198	21.98	6.12	0.32	0.32	88.01	106.35
2199	21.99	6.02	0.31	0.31	88.67	106.15
2200	22.00	5.91	0.31	0.31	89.37	105.93
2201	22.01	5.80	0.30	0.30	90.07	105.72
2202	22.02	5.71	0.29	0.29	90.74	105.52
2203	22.03	5.62	0.29	0.29	91.28	105.36
2204	22.04	5.57	0.28	0.28	91.53	105.24
2205	22.05	5.57	0.28	0.28	91.50	105.16
2206	22.06	5.57	0.28	0.28	91.27	105.08
2207	22.07	5.57	0.27	0.27	91.01	104.99
2208	22.08	5.57	0.27	0.27	90.74	104.90

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2209	22.09	5.57	0.27	0.27	90.46	104.81
2210	22.10	5.57	0.26	0.26	90.19	104.72
2211	22.11	5.57	0.26	0.26	89.95	104.64
2212	22.12	5.57	0.26	0.26	89.75	104.57
2213	22.13	5.57	0.26	0.26	89.58	104.51
2214	22.14	5.57	0.25	0.25	89.40	104.45
2215	22.15	5.57	0.25	0.25	89.20	104.38
2216	22.16	5.57	0.25	0.25	88.97	104.30
2217	22.17	5.57	0.25	0.25	88.73	104.21
2218	22.18	5.57	0.24	0.24	88.50	104.13
2219	22.19	5.57	0.24	0.24	88.27	104.05
2220	22.20	5.57	0.24	0.24	88.08	103.99
2221	22.21	5.57	0.24	0.24	88.03	103.92
2222	22.22	5.54	0.23	0.23	88.15	103.83
2223	22.23	5.50	0.23	0.23	88.43	103.73
2224	22.24	5.45	0.23	0.23	88.76	103.61
2225	22.25	5.40	0.23	0.23	89.12	103.48
2226	22.26	5.34	0.22	0.22	89.50	103.34
2227	22.27	5.29	0.22	0.22	89.88	103.21
2228	22.28	5.24	0.22	0.22	90.23	103.09
2229	22.29	5.20	0.21	0.21	90.45	103.00
2230	22.30	5.19	0.21	0.21	90.32	103.00
2231	22.31	5.27	0.21	0.21	89.78	103.08
2232	22.32	5.36	0.22	0.22	88.93	103.23
2233	22.33	5.46	0.22	0.22	88.01	103.40
2234	22.34	5.57	0.23	0.23	87.07	103.57
2235	22.35	5.68	0.23	0.23	86.15	103.73
2236	22.36	5.78	0.23	0.23	85.31	103.89
2237	22.37	5.87	0.24	0.24	84.58	104.03
2238	22.38	5.95	0.24	0.24	84.03	104.13
2239	22.39	5.99	0.24	0.24	83.63	104.22
2240	22.40	6.03	0.24	0.24	83.32	104.29
2241	22.41	6.08	0.24	0.24	82.99	104.36
2242	22.42	6.13	0.25	0.25	82.64	104.44
2243	22.43	6.19	0.25	0.25	82.28	104.53
2244	22.44	6.24	0.25	0.25	81.93	104.61
2245	22.45	6.29	0.25	0.25	81.61	104.69
2246	22.46	6.34	0.25	0.25	81.33	104.75
2247	22.47	6.37	0.26	0.26	81.06	104.82
2248	22.48	6.42	0.26	0.26	80.76	104.90
2249	22.49	6.49	0.26	0.26	80.39	105.01
2250	22.50	6.56	0.26	0.26	79.96	105.13
2251	22.51	6.64	0.27	0.27	79.52	105.26
2252	22.52	6.72	0.27	0.27	79.07	105.38
2253	22.53	6.80	0.28	0.28	78.65	105.51
2254	22.54	6.87	0.28	0.28	78.28	105.62
2255	22.55	6.93	0.28	0.28	77.99	105.71
2256	22.56	6.97	0.28	0.28	77.84	105.76

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2257	22.57	6.97	0.28	0.28	77.81	105.78
2258	22.58	6.97	0.28	0.28	77.85	105.79
2259	22.59	6.97	0.28	0.28	77.89	105.80
2260	22.60	6.97	0.28	0.28	77.94	105.81
2261	22.61	6.97	0.29	0.29	77.98	105.82
2262	22.62	6.97	0.29	0.29	78.02	105.83
2263	22.63	6.97	0.29	0.29	78.06	105.84
2264	22.64	6.97	0.29	0.29	78.24	105.82
2265	22.65	6.89	0.28	0.28	78.69	105.72
2266	22.66	6.75	0.28	0.28	79.48	105.54
2267	22.67	6.58	0.27	0.27	80.52	105.30
2268	22.68	6.40	0.26	0.26	81.72	105.04
2269	22.69	6.21	0.26	0.26	83.02	104.75
2270	22.70	6.02	0.25	0.25	84.37	104.47
2271	22.71	5.85	0.24	0.24	85.70	104.19
2272	22.72	5.70	0.24	0.24	86.91	103.94
2273	22.73	5.57	0.23	0.23	87.68	103.78
2274	22.74	5.57	0.23	0.23	88.00	103.70
2275	22.75	5.57	0.23	0.23	87.96	103.69
2276	22.76	5.57	0.23	0.23	87.92	103.67
2277	22.77	5.57	0.23	0.23	87.86	103.64
2278	22.78	5.57	0.23	0.23	87.81	103.62
2279	22.79	5.57	0.23	0.23	87.76	103.60
2280	22.80	5.57	0.23	0.23	87.72	103.58
2281	22.81	5.57	0.23	0.23	87.68	103.56
2282	22.82	5.57	0.22	0.22	87.63	103.54
2283	22.83	5.57	0.22	0.22	87.58	103.52
2284	22.84	5.57	0.22	0.22	87.51	103.49
2285	22.85	5.57	0.22	0.22	87.42	103.46
2286	22.86	5.57	0.22	0.22	87.33	103.42
2287	22.87	5.57	0.22	0.22	87.25	103.39
2288	22.88	5.57	0.22	0.22	87.16	103.36
2289	22.89	5.57	0.22	0.22	87.09	103.33
2290	22.90	5.57	0.22	0.22	87.04	103.31
2291	22.91	5.57	0.22	0.22	87.02	103.30
2292	22.92	5.57	0.22	0.22	87.03	103.29
2293	22.93	5.57	0.22	0.22	87.05	103.29
2294	22.94	5.57	0.22	0.22	87.06	103.29
2295	22.95	5.57	0.22	0.22	87.07	103.29
2296	22.96	5.57	0.22	0.22	87.09	103.29
2297	22.97	5.57	0.22	0.22	87.10	103.29
2298	22.98	5.57	0.22	0.22	87.11	103.30
2299	22.99	5.58	0.22	0.22	86.66	103.41
2300	23.00	5.75	0.23	0.23	85.68	103.66
2301	23.01	5.97	0.24	0.24	84.15	104.06
2302	23.02	6.22	0.25	0.25	82.53	104.50
2303	23.03	6.49	0.26	0.26	80.92	104.95
2304	23.04	6.76	0.27	0.27	79.40	105.40

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2305	23.05	7.02	0.28	0.28	78.04	105.81
2306	23.06	7.26	0.30	0.30	76.87	106.18
2307	23.07	7.46	0.31	0.31	75.99	106.47
2308	23.08	7.59	0.31	0.31	75.43	106.69
2309	23.09	7.66	0.32	0.32	75.09	106.86
2310	23.10	7.76	0.32	0.32	74.83	107.04
2311	23.11	7.86	0.33	0.33	74.55	107.23
2312	23.12	7.97	0.34	0.34	74.26	107.43
2313	23.13	8.07	0.35	0.35	73.98	107.63
2314	23.14	8.18	0.35	0.35	73.72	107.81
2315	23.15	8.27	0.36	0.36	73.50	107.98
2316	23.16	8.34	0.37	0.37	73.41	108.09
2317	23.17	8.34	0.37	0.37	73.50	108.14
2318	23.18	8.30	0.37	0.37	73.78	108.15
2319	23.19	8.25	0.37	0.37	74.15	108.15
2320	23.20	8.20	0.37	0.37	74.56	108.15
2321	23.21	8.14	0.37	0.37	74.98	108.15
2322	23.22	8.09	0.37	0.37	75.40	108.14
2323	23.23	8.04	0.37	0.37	75.79	108.14
2324	23.24	8.00	0.37	0.37	76.12	108.14
2325	23.25	7.97	0.37	0.37	76.26	108.17
2326	23.26	8.04	0.38	0.38	76.18	108.26
2327	23.27	8.12	0.39	0.39	75.92	108.41
2328	23.28	8.22	0.39	0.39	75.63	108.58
2329	23.29	8.33	0.40	0.40	75.33	108.75
2330	23.30	8.44	0.41	0.41	75.03	108.93
2331	23.31	8.54	0.42	0.42	74.75	109.10
2332	23.32	8.64	0.42	0.42	74.50	109.25
2333	23.33	8.72	0.43	0.43	74.29	109.38
2334	23.34	8.78	0.44	0.44	74.10	109.49
2335	23.35	8.86	0.44	0.44	73.89	109.61
2336	23.36	8.95	0.45	0.45	73.66	109.75
2337	23.37	9.06	0.46	0.46	73.40	109.90
2338	23.38	9.16	0.46	0.46	73.14	110.06
2339	23.39	9.27	0.47	0.47	72.88	110.22
2340	23.40	9.37	0.48	0.48	72.64	110.37
2341	23.41	9.46	0.49	0.49	72.44	110.50
2342	23.42	9.54	0.49	0.49	72.25	110.60
2343	23.43	9.60	0.50	0.50	72.05	110.69
2344	23.44	9.69	0.50	0.50	71.80	110.78
2345	23.45	9.78	0.51	0.51	71.50	110.89
2346	23.46	9.89	0.51	0.51	71.19	111.00
2347	23.47	10.00	0.52	0.52	70.87	111.11
2348	23.48	10.10	0.53	0.53	70.56	111.22
2349	23.49	10.20	0.53	0.53	70.28	111.32
2350	23.50	10.29	0.54	0.54	70.04	111.41
2351	23.51	10.36	0.54	0.54	69.79	111.49
2352	23.52	10.45	0.55	0.55	69.47	111.57

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2353	23.53	10.58	0.55	0.55	69.07	111.66
2354	23.54	10.71	0.56	0.56	68.62	111.76
2355	23.55	10.86	0.56	0.56	68.15	111.87
2356	23.56	11.01	0.57	0.57	67.68	111.98
2357	23.57	11.15	0.57	0.57	67.23	112.09
2358	23.58	11.28	0.58	0.58	66.84	112.18
2359	23.59	11.39	0.58	0.58	66.52	112.25
2360	23.60	11.47	0.59	0.59	66.26	112.32
2361	23.61	11.55	0.59	0.59	66.04	112.38
2362	23.62	11.64	0.59	0.59	65.80	112.46
2363	23.63	11.75	0.60	0.60	65.54	112.54
2364	23.64	11.85	0.60	0.60	65.27	112.62
2365	23.65	11.96	0.61	0.61	65.00	112.70
2366	23.66	12.06	0.61	0.61	64.75	112.78
2367	23.67	12.15	0.62	0.62	64.53	112.85
2368	23.68	12.23	0.62	0.62	64.42	112.90
2369	23.69	12.23	0.62	0.62	64.44	112.92
2370	23.70	12.19	0.62	0.62	64.59	112.93
2371	23.71	12.16	0.63	0.63	64.79	112.94
2372	23.72	12.12	0.63	0.63	65.00	112.95
2373	23.73	12.08	0.63	0.63	65.22	112.96
2374	23.74	12.04	0.63	0.63	65.44	112.97
2375	23.75	12.00	0.63	0.63	65.64	112.98
2376	23.76	11.97	0.63	0.63	65.80	112.99
2377	23.77	11.97	0.64	0.64	65.72	113.09
2378	23.78	12.23	0.65	0.65	65.36	113.29
2379	23.79	12.56	0.68	0.68	64.75	113.59
2380	23.80	12.94	0.70	0.70	64.08	113.94
2381	23.81	13.34	0.73	0.73	63.40	114.29
2382	23.82	13.75	0.76	0.76	62.75	114.64
2383	23.83	14.14	0.79	0.79	62.16	114.97
2384	23.84	14.49	0.81	0.81	61.65	115.26
2385	23.85	14.79	0.83	0.83	61.26	115.49
2386	23.86	14.97	0.85	0.85	61.02	115.66
2387	23.87	15.09	0.86	0.86	60.86	115.79
2388	23.88	15.23	0.87	0.87	60.74	115.92
2389	23.89	15.38	0.89	0.89	60.61	116.06
2390	23.90	15.55	0.90	0.90	60.47	116.20
2391	23.91	15.71	0.92	0.92	60.33	116.35
2392	23.92	15.86	0.93	0.93	60.21	116.48
2393	23.93	15.99	0.94	0.94	60.10	116.60
2394	23.94	16.11	0.95	0.95	60.11	116.65
2395	23.95	15.98	0.95	0.95	60.29	116.62
2396	23.96	15.76	0.94	0.94	60.66	116.50
2397	23.97	15.49	0.92	0.92	61.13	116.34
2398	23.98	15.20	0.90	0.90	61.66	116.17
2399	23.99	14.90	0.89	0.89	62.21	115.99
2400	24.00	14.61	0.87	0.87	62.77	115.81

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2401	24.01	14.34	0.86	0.86	63.30	115.63
2402	24.02	14.10	0.84	0.84	63.77	115.48
2403	24.03	13.93	0.83	0.83	64.07	115.38
2404	24.04	13.90	0.83	0.83	64.24	115.32
2405	24.05	13.85	0.83	0.83	64.32	115.29
2406	24.06	13.80	0.82	0.82	64.41	115.25
2407	24.07	13.75	0.82	0.82	64.51	115.20
2408	24.08	13.69	0.81	0.81	64.60	115.15
2409	24.09	13.64	0.81	0.81	64.70	115.11
2410	24.10	13.60	0.81	0.81	64.79	115.07
2411	24.11	13.56	0.80	0.80	64.89	115.03
2412	24.12	13.49	0.80	0.80	65.08	114.97
2413	24.13	13.35	0.79	0.79	65.38	114.89
2414	24.14	13.19	0.78	0.78	65.77	114.79
2415	24.15	13.01	0.78	0.78	66.22	114.67
2416	24.16	12.82	0.77	0.77	66.70	114.55
2417	24.17	12.63	0.76	0.76	67.18	114.42
2418	24.18	12.45	0.75	0.75	67.64	114.30
2419	24.19	12.29	0.74	0.74	68.06	114.19
2420	24.20	12.17	0.73	0.73	68.44	114.10
2421	24.21	12.05	0.73	0.73	68.83	114.01
2422	24.22	11.90	0.72	0.72	69.28	113.92
2423	24.23	11.73	0.71	0.71	69.82	113.81
2424	24.24	11.55	0.71	0.71	70.41	113.69
2425	24.25	11.36	0.70	0.70	71.02	113.56
2426	24.26	11.17	0.69	0.69	71.64	113.43
2427	24.27	11.00	0.68	0.68	72.23	113.31
2428	24.28	10.85	0.67	0.67	72.72	113.22
2429	24.29	10.76	0.67	0.67	72.90	113.20
2430	24.30	10.89	0.68	0.68	72.77	113.28
2431	24.31	11.05	0.69	0.69	72.39	113.43
2432	24.32	11.22	0.70	0.70	71.96	113.61
2433	24.33	11.41	0.72	0.72	71.52	113.79
2434	24.34	11.60	0.73	0.73	71.09	113.97
2435	24.35	11.78	0.75	0.75	70.69	114.14
2436	24.36	11.95	0.76	0.76	70.33	114.30
2437	24.37	12.09	0.77	0.77	70.03	114.43
2438	24.38	12.20	0.78	0.78	69.76	114.54
2439	24.39	12.33	0.79	0.79	69.46	114.67
2440	24.40	12.50	0.80	0.80	69.12	114.81
2441	24.41	12.68	0.81	0.81	68.74	114.96
2442	24.42	12.87	0.83	0.83	68.36	115.12
2443	24.43	13.06	0.84	0.84	67.99	115.27
2444	24.44	13.23	0.85	0.85	67.65	115.41
2445	24.45	13.39	0.87	0.87	67.36	115.54
2446	24.46	13.52	0.88	0.88	67.17	115.62
2447	24.47	13.54	0.88	0.88	67.07	115.66
2448	24.48	13.54	0.88	0.88	67.05	115.65

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2449	24.49	13.54	0.87	0.87	67.04	115.65
2450	24.50	13.54	0.87	0.87	67.02	115.64
2451	24.51	13.54	0.87	0.87	67.01	115.63
2452	24.52	13.54	0.87	0.87	66.99	115.62
2453	24.53	13.54	0.87	0.87	66.98	115.61
2454	24.54	13.54	0.87	0.87	66.97	115.60
2455	24.55	13.53	0.87	0.87	67.00	115.57
2456	24.56	13.46	0.86	0.86	67.07	115.51
2457	24.57	13.37	0.85	0.85	67.19	115.42
2458	24.58	13.27	0.84	0.84	67.32	115.31
2459	24.59	13.16	0.83	0.83	67.46	115.20
2460	24.60	13.05	0.82	0.82	67.61	115.08
2461	24.61	12.95	0.81	0.81	67.75	114.97
2462	24.62	12.85	0.80	0.80	67.88	114.87
2463	24.63	12.77	0.79	0.79	67.99	114.78
2464	24.64	12.71	0.78	0.78	68.09	114.70
2465	24.65	12.63	0.78	0.78	68.21	114.60
2466	24.66	12.54	0.77	0.77	68.33	114.50
2467	24.67	12.43	0.76	0.76	68.48	114.38
2468	24.68	12.33	0.75	0.75	68.63	114.25
2469	24.69	12.22	0.74	0.74	68.78	114.13
2470	24.70	12.12	0.73	0.73	68.93	114.01
2471	24.71	12.03	0.72	0.72	69.06	113.90
2472	24.72	11.96	0.71	0.71	69.18	113.81
2473	24.73	11.89	0.70	0.70	69.31	113.73
2474	24.74	11.80	0.70	0.70	69.46	113.63
2475	24.75	11.71	0.69	0.69	69.63	113.52
2476	24.76	11.60	0.68	0.68	69.82	113.40
2477	24.77	11.49	0.67	0.67	70.02	113.27
2478	24.78	11.39	0.66	0.66	70.22	113.15
2479	24.79	11.29	0.65	0.65	70.41	113.03
2480	24.80	11.20	0.64	0.64	70.58	112.93
2481	24.81	11.13	0.64	0.64	70.82	112.82
2482	24.82	10.98	0.63	0.63	71.17	112.68
2483	24.83	10.80	0.61	0.61	71.65	112.51
2484	24.84	10.60	0.60	0.60	72.20	112.30
2485	24.85	10.39	0.59	0.59	72.82	112.08
2486	24.86	10.17	0.57	0.57	73.45	111.86
2487	24.87	9.96	0.56	0.56	74.09	111.63
2488	24.88	9.77	0.55	0.55	74.68	111.43
2489	24.89	9.62	0.54	0.54	75.16	111.27
2490	24.90	9.52	0.53	0.53	75.54	111.14
2491	24.91	9.44	0.53	0.53	75.84	111.03
2492	24.92	9.35	0.52	0.52	76.15	110.92
2493	24.93	9.25	0.51	0.51	76.51	110.80
2494	24.94	9.14	0.50	0.50	76.88	110.67
2495	24.95	9.03	0.50	0.50	77.26	110.53
2496	24.96	8.93	0.49	0.49	77.62	110.41

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2497	24.97	8.84	0.48	0.48	77.95	110.30
2498	24.98	8.77	0.48	0.48	78.25	110.20
2499	24.99	8.70	0.48	0.48	78.55	110.11
2500	25.00	8.62	0.47	0.47	78.89	110.00
2501	25.01	8.52	0.46	0.46	79.29	109.88
2502	25.02	8.41	0.46	0.46	79.74	109.75
2503	25.03	8.30	0.45	0.45	80.20	109.61
2504	25.04	8.20	0.44	0.44	80.67	109.48
2505	25.05	8.10	0.44	0.44	81.11	109.35
2506	25.06	8.02	0.43	0.43	81.49	109.24
2507	25.07	7.95	0.43	0.43	81.86	109.15
2508	25.08	7.88	0.43	0.43	82.25	109.05
2509	25.09	7.79	0.42	0.42	82.71	108.94
2510	25.10	7.69	0.42	0.42	83.25	108.81
2511	25.11	7.58	0.41	0.41	83.83	108.68
2512	25.12	7.47	0.40	0.40	84.43	108.54
2513	25.13	7.37	0.40	0.40	85.02	108.41
2514	25.14	7.27	0.39	0.39	85.56	108.28
2515	25.15	7.20	0.39	0.39	85.97	108.20
2516	25.16	7.17	0.39	0.39	86.21	108.15
2517	25.17	7.17	0.39	0.39	86.31	108.15
2518	25.18	7.17	0.39	0.39	86.35	108.16
2519	25.19	7.17	0.39	0.39	86.40	108.17
2520	25.20	7.17	0.39	0.39	86.46	108.18
2521	25.21	7.17	0.39	0.39	86.51	108.19
2522	25.22	7.17	0.39	0.39	86.56	108.21
2523	25.23	7.17	0.39	0.39	86.60	108.22
2524	25.24	7.17	0.39	0.39	86.75	108.19
2525	25.25	7.11	0.39	0.39	87.04	108.12
2526	25.26	7.02	0.38	0.38	87.51	107.99
2527	25.27	6.92	0.38	0.38	88.08	107.84
2528	25.28	6.82	0.37	0.37	88.72	107.68
2529	25.29	6.71	0.36	0.36	89.39	107.50
2530	25.30	6.60	0.36	0.36	90.06	107.33
2531	25.31	6.51	0.35	0.35	90.69	107.18
2532	25.32	6.42	0.35	0.35	91.22	107.04
2533	25.33	6.37	0.34	0.34	91.51	106.96
2534	25.34	6.37	0.34	0.34	91.57	106.91
2535	25.35	6.37	0.34	0.34	91.48	106.87
2536	25.36	6.37	0.34	0.34	91.38	106.84
2537	25.37	6.37	0.34	0.34	91.27	106.80
2538	25.38	6.37	0.33	0.33	91.15	106.76
2539	25.39	6.37	0.33	0.33	91.05	106.72
2540	25.40	6.37	0.33	0.33	90.95	106.69
2541	25.41	6.37	0.33	0.33	90.79	106.68
2542	25.42	6.41	0.33	0.33	90.43	106.71
2543	25.43	6.49	0.33	0.33	89.86	106.80
2544	25.44	6.58	0.34	0.34	89.13	106.91

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2545	25.45	6.69	0.34	0.34	88.34	107.03
2546	25.46	6.79	0.34	0.34	87.54	107.15
2547	25.47	6.90	0.35	0.35	86.77	107.27
2548	25.48	7.00	0.35	0.35	86.06	107.38
2549	25.49	7.09	0.36	0.36	85.46	107.47
2550	25.50	7.16	0.36	0.36	84.95	107.56
2551	25.51	7.23	0.36	0.36	84.47	107.64
2552	25.52	7.31	0.36	0.36	83.96	107.74
2553	25.53	7.41	0.37	0.37	83.38	107.86
2554	25.54	7.52	0.37	0.37	82.77	107.98
2555	25.55	7.63	0.38	0.38	82.15	108.11
2556	25.56	7.73	0.38	0.38	81.57	108.23
2557	25.57	7.83	0.39	0.39	81.05	108.33
2558	25.58	7.91	0.39	0.39	80.62	108.43
2559	25.59	7.98	0.39	0.39	80.28	108.52
2560	25.60	8.05	0.40	0.40	79.98	108.64
2561	25.61	8.14	0.41	0.41	79.67	108.79
2562	25.62	8.25	0.41	0.41	79.33	108.95
2563	25.63	8.35	0.42	0.42	78.98	109.12
2564	25.64	8.46	0.43	0.43	78.64	109.28
2565	25.65	8.56	0.44	0.44	78.32	109.44
2566	25.66	8.66	0.44	0.44	78.04	109.58
2567	25.67	8.73	0.45	0.45	77.86	109.69
2568	25.68	8.76	0.45	0.45	77.83	109.76
2569	25.69	8.76	0.46	0.46	77.92	109.81
2570	25.70	8.76	0.46	0.46	78.06	109.86
2571	25.71	8.76	0.46	0.46	78.22	109.91
2572	25.72	8.76	0.46	0.46	78.39	109.96
2573	25.73	8.76	0.47	0.47	78.55	110.01
2574	25.74	8.76	0.47	0.47	78.71	110.06
2575	25.75	8.76	0.47	0.47	78.84	110.10
2576	25.76	8.76	0.48	0.48	78.85	110.15
2577	25.77	8.82	0.48	0.48	78.71	110.23
2578	25.78	8.91	0.49	0.49	78.41	110.33
2579	25.79	9.01	0.49	0.49	78.06	110.45
2580	25.80	9.11	0.50	0.50	77.69	110.58
2581	25.81	9.22	0.51	0.51	77.33	110.71
2582	25.82	9.33	0.51	0.51	76.98	110.84
2583	25.83	9.43	0.52	0.52	76.67	110.95
2584	25.84	9.51	0.53	0.53	76.40	111.05
2585	25.85	9.57	0.53	0.53	76.17	111.14
2586	25.86	9.65	0.53	0.53	75.92	111.22
2587	25.87	9.74	0.54	0.54	75.63	111.32
2588	25.88	9.84	0.55	0.55	75.31	111.43
2589	25.89	9.95	0.55	0.55	74.98	111.55
2590	25.90	10.06	0.56	0.56	74.66	111.67
2591	25.91	10.16	0.57	0.57	74.35	111.78
2592	25.92	10.25	0.57	0.57	74.09	111.87

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2593	25.93	10.33	0.58	0.58	73.77	111.99
2594	25.94	10.48	0.59	0.59	73.27	112.15
2595	25.95	10.74	0.60	0.60	72.55	112.38
2596	25.96	11.05	0.62	0.62	71.67	112.67
2597	25.97	11.39	0.64	0.64	70.75	112.98
2598	25.98	11.75	0.66	0.66	69.85	113.28
2599	25.99	12.09	0.69	0.69	69.00	113.58
2600	26.00	12.42	0.70	0.70	68.24	113.85
2601	26.01	12.70	0.72	0.72	67.60	114.08
2602	26.02	12.93	0.74	0.74	67.18	114.24
2603	26.03	13.01	0.74	0.74	66.93	114.35
2604	26.04	13.09	0.75	0.75	66.78	114.43
2605	26.05	13.19	0.76	0.76	66.62	114.52
2606	26.06	13.30	0.76	0.76	66.45	114.62
2607	26.07	13.41	0.77	0.77	66.28	114.72
2608	26.08	13.51	0.78	0.78	66.12	114.81
2609	26.09	13.61	0.79	0.79	65.97	114.90
2610	26.10	13.69	0.79	0.79	65.89	114.96
2611	26.11	13.70	0.80	0.80	66.00	114.95
2612	26.12	13.53	0.79	0.79	66.32	114.88
2613	26.13	13.32	0.78	0.78	66.83	114.75
2614	26.14	13.09	0.77	0.77	67.41	114.61
2615	26.15	12.85	0.76	0.76	68.05	114.45
2616	26.16	12.61	0.74	0.74	68.70	114.29
2617	26.17	12.38	0.73	0.73	69.33	114.14
2618	26.18	12.17	0.72	0.72	69.92	113.99
2619	26.19	12.00	0.71	0.71	70.36	113.90
2620	26.20	11.95	0.71	0.71	70.62	113.86
2621	26.21	11.95	0.71	0.71	70.75	113.87
2622	26.22	11.95	0.72	0.72	70.85	113.90
2623	26.23	11.95	0.72	0.72	70.95	113.93
2624	26.24	11.95	0.72	0.72	71.06	113.97
2625	26.25	11.95	0.73	0.73	71.17	114.00
2626	26.26	11.95	0.73	0.73	71.27	114.03
2627	26.27	11.95	0.73	0.73	71.36	114.06
2628	26.28	11.95	0.74	0.74	71.38	114.10
2629	26.29	12.01	0.74	0.74	71.31	114.16
2630	26.30	12.10	0.75	0.75	71.16	114.25
2631	26.31	12.20	0.76	0.76	70.98	114.35
2632	26.32	12.31	0.77	0.77	70.79	114.46
2633	26.33	12.41	0.78	0.78	70.61	114.57
2634	26.34	12.52	0.79	0.79	70.43	114.67
2635	26.35	12.61	0.79	0.79	70.27	114.77
2636	26.36	12.70	0.80	0.80	70.13	114.85
2637	26.37	12.76	0.81	0.81	69.97	114.91
2638	26.38	12.84	0.81	0.81	69.77	114.96
2639	26.39	12.93	0.81	0.81	69.52	115.01
2640	26.40	13.03	0.82	0.82	69.25	115.07

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2641	26.41	13.14	0.82	0.82	68.95	115.13
2642	26.42	13.25	0.83	0.83	68.67	115.19
2643	26.43	13.35	0.83	0.83	68.39	115.25
2644	26.44	13.44	0.84	0.84	68.16	115.30
2645	26.45	13.52	0.84	0.84	67.98	115.33
2646	26.46	13.54	0.84	0.84	67.85	115.33
2647	26.47	13.54	0.83	0.83	67.75	115.30
2648	26.48	13.54	0.83	0.83	67.64	115.26
2649	26.49	13.54	0.82	0.82	67.53	115.22
2650	26.50	13.54	0.82	0.82	67.41	115.18
2651	26.51	13.54	0.81	0.81	67.29	115.13
2652	26.52	13.54	0.81	0.81	67.18	115.09
2653	26.53	13.54	0.81	0.81	67.08	115.05
2654	26.54	13.54	0.80	0.80	66.98	115.03
2655	26.55	13.57	0.80	0.80	66.86	115.03
2656	26.56	13.62	0.80	0.80	66.71	115.03
2657	26.57	13.67	0.80	0.80	66.54	115.04
2658	26.58	13.72	0.80	0.80	66.35	115.05
2659	26.59	13.77	0.80	0.80	66.16	115.06
2660	26.60	13.83	0.80	0.80	65.98	115.07
2661	26.61	13.87	0.80	0.80	65.82	115.07
2662	26.62	13.91	0.80	0.80	65.71	115.07
2663	26.63	13.92	0.80	0.80	65.70	115.05
2664	26.64	13.84	0.80	0.80	65.81	115.01
2665	26.65	13.75	0.79	0.79	66.00	114.94
2666	26.66	13.64	0.78	0.78	66.21	114.86
2667	26.67	13.54	0.78	0.78	66.44	114.78
2668	26.68	13.43	0.77	0.77	66.67	114.70
2669	26.69	13.33	0.76	0.76	66.89	114.62
2670	26.70	13.24	0.76	0.76	67.09	114.55
2671	26.71	13.16	0.75	0.75	67.28	114.48
2672	26.72	13.07	0.75	0.75	67.49	114.41
2673	26.73	12.95	0.74	0.74	67.75	114.31
2674	26.74	12.81	0.73	0.73	68.06	114.19
2675	26.75	12.65	0.72	0.72	68.40	114.05
2676	26.76	12.49	0.71	0.71	68.76	113.92
2677	26.77	12.33	0.70	0.70	69.13	113.78
2678	26.78	12.18	0.69	0.69	69.48	113.65
2679	26.79	12.05	0.68	0.68	69.78	113.53
2680	26.80	11.95	0.67	0.67	69.96	113.46
2681	26.81	11.95	0.67	0.67	70.01	113.41
2682	26.82	11.95	0.67	0.67	69.96	113.39
2683	26.83	11.95	0.67	0.67	69.90	113.37
2684	26.84	11.95	0.67	0.67	69.84	113.34
2685	26.85	11.95	0.66	0.66	69.77	113.32
2686	26.86	11.95	0.66	0.66	69.71	113.29
2687	26.87	11.95	0.66	0.66	69.65	113.27
2688	26.88	11.95	0.66	0.66	69.53	113.27

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2689	26.89	12.03	0.66	0.66	69.18	113.36
2690	26.90	12.32	0.68	0.68	68.55	113.54
2691	26.91	12.66	0.69	0.69	67.70	113.80
2692	26.92	13.05	0.71	0.71	66.79	114.08
2693	26.93	13.45	0.74	0.74	65.88	114.37
2694	26.94	13.86	0.76	0.76	65.01	114.65
2695	26.95	14.24	0.78	0.78	64.22	114.91
2696	26.96	14.58	0.80	0.80	63.54	115.13
2697	26.97	14.86	0.81	0.81	63.15	115.25
2698	26.98	14.83	0.81	0.81	63.10	115.26
2699	26.99	14.64	0.80	0.80	63.35	115.15
2700	27.00	14.43	0.78	0.78	63.73	114.99
2701	27.01	14.19	0.77	0.77	64.16	114.81
2702	27.02	13.94	0.75	0.75	64.62	114.62
2703	27.03	13.70	0.74	0.74	65.07	114.44
2704	27.04	13.48	0.72	0.72	65.51	114.27
2705	27.05	13.29	0.71	0.71	65.91	114.11
2706	27.06	13.13	0.70	0.70	66.42	113.93
2707	27.07	12.80	0.69	0.69	67.14	113.70
2708	27.08	12.38	0.66	0.66	68.16	113.39
2709	27.09	11.90	0.64	0.64	69.40	113.01
2710	27.10	11.40	0.61	0.61	70.81	112.60
2711	27.11	10.88	0.58	0.58	72.34	112.16
2712	27.12	10.38	0.56	0.56	73.94	111.71
2713	27.13	9.93	0.53	0.53	75.50	111.29
2714	27.14	9.55	0.51	0.51	76.76	110.96
2715	27.15	9.39	0.50	0.50	77.39	110.82
2716	27.16	9.48	0.51	0.51	77.40	110.86
2717	27.17	9.60	0.52	0.52	77.07	111.01
2718	27.18	9.73	0.53	0.53	76.71	111.18
2719	27.19	9.86	0.54	0.54	76.33	111.35
2720	27.20	10.00	0.55	0.55	75.97	111.51
2721	27.21	10.12	0.56	0.56	75.64	111.67
2722	27.22	10.24	0.57	0.57	75.35	111.81
2723	27.23	10.33	0.58	0.58	75.17	111.90
2724	27.24	10.35	0.58	0.58	75.08	111.95
2725	27.25	10.35	0.58	0.58	75.08	111.96
2726	27.26	10.35	0.58	0.58	75.10	111.97
2727	27.27	10.35	0.58	0.58	75.13	111.97
2728	27.28	10.35	0.58	0.58	75.15	111.97
2729	27.29	10.35	0.58	0.58	75.17	111.98
2730	27.30	10.35	0.58	0.58	75.19	111.98
2731	27.31	10.35	0.58	0.58	75.21	111.98
2732	27.32	10.35	0.58	0.58	75.22	111.98
2733	27.33	10.35	0.58	0.58	75.22	111.98
2734	27.34	10.35	0.58	0.58	75.21	111.97
2735	27.35	10.35	0.58	0.58	75.20	111.97
2736	27.36	10.35	0.58	0.58	75.18	111.96

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2737	27.37	10.35	0.58	0.58	75.17	111.95
2738	27.38	10.35	0.58	0.58	75.16	111.94
2739	27.39	10.35	0.58	0.58	75.15	111.94
2740	27.40	10.35	0.58	0.58	75.05	111.96
2741	27.41	10.44	0.58	0.58	74.68	112.06
2742	27.42	10.69	0.59	0.59	74.01	112.26
2743	27.43	10.99	0.61	0.61	73.10	112.53
2744	27.44	11.32	0.63	0.63	72.14	112.83
2745	27.45	11.67	0.65	0.65	71.18	113.13
2746	27.46	12.02	0.67	0.67	70.26	113.42
2747	27.47	12.36	0.69	0.69	69.44	113.69
2748	27.48	12.65	0.71	0.71	68.74	113.92
2749	27.49	12.89	0.72	0.72	68.17	114.12
2750	27.50	13.10	0.74	0.74	67.64	114.32
2751	27.51	13.37	0.75	0.75	67.10	114.53
2752	27.52	13.69	0.77	0.77	66.49	114.78
2753	27.53	14.03	0.80	0.80	65.86	115.04
2754	27.54	14.38	0.82	0.82	65.23	115.31
2755	27.55	14.73	0.84	0.84	64.64	115.57
2756	27.56	15.05	0.86	0.86	64.11	115.80
2757	27.57	15.33	0.88	0.88	63.69	115.99
2758	27.58	15.51	0.89	0.89	63.63	116.06
2759	27.59	15.28	0.89	0.89	63.93	116.02
2760	27.60	14.99	0.87	0.87	64.58	115.88
2761	27.61	14.67	0.86	0.86	65.34	115.72
2762	27.62	14.32	0.85	0.85	66.18	115.54
2763	27.63	13.97	0.83	0.83	67.06	115.35
2764	27.64	13.63	0.82	0.82	67.94	115.16
2765	27.65	13.32	0.80	0.80	68.75	114.99
2766	27.66	13.06	0.79	0.79	69.50	114.82
2767	27.67	12.82	0.78	0.78	70.30	114.64
2768	27.68	12.47	0.76	0.76	71.26	114.42
2769	27.69	12.05	0.74	0.74	72.48	114.13
2770	27.70	11.59	0.72	0.72	73.91	113.80
2771	27.71	11.10	0.69	0.69	75.50	113.44
2772	27.72	10.62	0.67	0.67	77.19	113.06
2773	27.73	10.16	0.64	0.64	78.90	112.68
2774	27.74	9.75	0.62	0.62	80.52	112.33
2775	27.75	9.42	0.60	0.60	81.67	112.09
2776	27.76	9.36	0.60	0.60	82.29	111.98
2777	27.77	9.36	0.60	0.60	82.46	111.98
2778	27.78	9.36	0.60	0.60	82.54	112.00
2779	27.79	9.36	0.60	0.60	82.63	112.02
2780	27.80	9.36	0.60	0.60	82.72	112.05
2781	27.81	9.36	0.61	0.61	82.80	112.07
2782	27.82	9.36	0.61	0.61	82.89	112.09
2783	27.83	9.36	0.61	0.61	82.93	112.12
2784	27.84	9.37	0.61	0.61	82.70	112.20

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2785	27.85	9.56	0.62	0.62	82.13	112.36
2786	27.86	9.80	0.64	0.64	81.25	112.59
2787	27.87	10.06	0.66	0.66	80.28	112.84
2788	27.88	10.34	0.68	0.68	79.29	113.10
2789	27.89	10.63	0.69	0.69	78.34	113.37
2790	27.90	10.90	0.71	0.71	77.46	113.61
2791	27.91	11.15	0.73	0.73	76.69	113.82
2792	27.92	11.36	0.74	0.74	76.09	113.99
2793	27.93	11.49	0.75	0.75	75.63	114.11
2794	27.94	11.59	0.76	0.76	75.23	114.20
2795	27.95	11.72	0.76	0.76	74.81	114.28
2796	27.96	11.86	0.77	0.77	74.35	114.38
2797	27.97	12.01	0.77	0.77	73.87	114.47
2798	27.98	12.16	0.78	0.78	73.41	114.56
2799	27.99	12.30	0.79	0.79	72.98	114.65
2800	28.00	12.42	0.79	0.79	72.61	114.73
2801	28.01	12.53	0.80	0.80	72.41	114.75
2802	28.02	12.47	0.79	0.79	72.41	114.71
2803	28.03	12.35	0.78	0.78	72.60	114.60
2804	28.04	12.22	0.77	0.77	72.85	114.46
2805	28.05	12.08	0.76	0.76	73.13	114.30
2806	28.06	11.93	0.74	0.74	73.42	114.14
2807	28.07	11.78	0.73	0.73	73.72	113.99
2808	28.08	11.64	0.72	0.72	74.00	113.84
2809	28.09	11.53	0.71	0.71	74.25	113.71
2810	28.10	11.44	0.70	0.70	74.47	113.59
2811	28.11	11.34	0.69	0.69	74.71	113.48
2812	28.12	11.22	0.68	0.68	74.98	113.34
2813	28.13	11.08	0.67	0.67	75.30	113.18
2814	28.14	10.93	0.66	0.66	75.64	113.01
2815	28.15	10.78	0.64	0.64	76.00	112.84
2816	28.16	10.64	0.63	0.63	76.35	112.67
2817	28.17	10.51	0.62	0.62	76.68	112.51
2818	28.18	10.40	0.61	0.61	76.80	112.42
2819	28.19	10.45	0.61	0.61	76.49	112.45
2820	28.20	10.71	0.62	0.62	75.71	112.61
2821	28.21	11.01	0.64	0.64	74.64	112.83
2822	28.22	11.35	0.65	0.65	73.50	113.08
2823	28.23	11.70	0.67	0.67	72.35	113.32
2824	28.24	12.05	0.68	0.68	71.27	113.56
2825	28.25	12.38	0.70	0.70	70.28	113.77
2826	28.26	12.67	0.71	0.71	69.45	113.95
2827	28.27	12.91	0.72	0.72	68.90	114.06
2828	28.28	12.94	0.72	0.72	68.60	114.10
2829	28.29	12.94	0.72	0.72	68.49	114.08
2830	28.30	12.94	0.71	0.71	68.40	114.05
2831	28.31	12.94	0.71	0.71	68.31	114.01
2832	28.32	12.94	0.71	0.71	68.21	113.97

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2833	28.33	12.94	0.70	0.70	68.11	113.93
2834	28.34	12.94	0.70	0.70	68.02	113.90
2835	28.35	12.94	0.70	0.70	67.97	113.86
2836	28.36	12.90	0.69	0.69	68.22	113.75
2837	28.37	12.59	0.68	0.68	68.83	113.56
2838	28.38	12.21	0.66	0.66	69.82	113.28
2839	28.39	11.78	0.63	0.63	71.00	112.94
2840	28.40	11.33	0.61	0.61	72.33	112.57
2841	28.41	10.87	0.59	0.59	73.76	112.18
2842	28.42	10.43	0.56	0.56	75.23	111.79
2843	28.43	10.03	0.54	0.54	76.64	111.42
2844	28.44	9.69	0.52	0.52	77.80	111.13
2845	28.45	9.52	0.52	0.52	78.61	110.95
2846	28.46	9.45	0.51	0.51	79.15	110.86
2847	28.47	9.35	0.51	0.51	79.62	110.79
2848	28.48	9.25	0.51	0.51	80.15	110.72
2849	28.49	9.14	0.50	0.50	80.72	110.64
2850	28.50	9.03	0.50	0.50	81.29	110.56
2851	28.51	8.93	0.50	0.50	81.83	110.48
2852	28.52	8.84	0.49	0.49	82.32	110.41
2853	28.53	8.77	0.49	0.49	82.65	110.36
2854	28.54	8.76	0.49	0.49	82.81	110.34
2855	28.55	8.76	0.49	0.49	82.83	110.34
2856	28.56	8.76	0.49	0.49	82.83	110.33
2857	28.57	8.76	0.49	0.49	82.83	110.33
2858	28.58	8.76	0.49	0.49	82.83	110.33
2859	28.59	8.76	0.49	0.49	82.83	110.32
2860	28.60	8.76	0.49	0.49	82.84	110.32
2861	28.61	8.76	0.49	0.49	82.86	110.31
2862	28.62	8.75	0.49	0.49	82.99	110.28
2863	28.63	8.68	0.48	0.48	83.26	110.21
2864	28.64	8.59	0.48	0.48	83.68	110.11
2865	28.65	8.49	0.47	0.47	84.16	109.99
2866	28.66	8.38	0.47	0.47	84.69	109.86
2867	28.67	8.27	0.46	0.46	85.22	109.74
2868	28.68	8.17	0.45	0.45	85.75	109.61
2869	28.69	8.07	0.45	0.45	86.24	109.50
2870	28.70	7.99	0.44	0.44	86.54	109.43
2871	28.71	8.01	0.44	0.44	86.52	109.46
2872	28.72	8.10	0.45	0.45	86.19	109.57
2873	28.73	8.22	0.46	0.46	85.69	109.73
2874	28.74	8.35	0.47	0.47	85.14	109.92
2875	28.75	8.49	0.48	0.48	84.59	110.10
2876	28.76	8.62	0.49	0.49	84.06	110.29
2877	28.77	8.75	0.50	0.50	83.58	110.45
2878	28.78	8.86	0.51	0.51	83.17	110.60
2879	28.79	8.95	0.51	0.51	82.65	110.76
2880	28.80	9.13	0.52	0.52	81.91	110.96

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2881	28.81	9.39	0.54	0.54	80.89	111.22
2882	28.82	9.68	0.56	0.56	79.73	111.51
2883	28.83	10.00	0.57	0.57	78.55	111.83
2884	28.84	10.33	0.59	0.59	77.40	112.14
2885	28.85	10.64	0.61	0.61	76.33	112.43
2886	28.86	10.94	0.63	0.63	75.40	112.69
2887	28.87	11.19	0.64	0.64	74.63	112.90
2888	28.88	11.38	0.65	0.65	73.99	113.06
2889	28.89	11.54	0.66	0.66	73.36	113.19
2890	28.90	11.74	0.67	0.67	72.67	113.32
2891	28.91	11.97	0.68	0.68	71.91	113.46
2892	28.92	12.21	0.68	0.68	71.12	113.60
2893	28.93	12.46	0.69	0.69	70.35	113.74
2894	28.94	12.69	0.70	0.70	69.63	113.86
2895	28.95	12.90	0.71	0.71	69.00	113.98
2896	28.96	13.08	0.71	0.71	68.42	114.08
2897	28.97	13.27	0.72	0.72	67.78	114.21
2898	28.98	13.57	0.73	0.73	67.01	114.36
2899	28.99	13.92	0.75	0.75	66.08	114.55
2900	29.00	14.31	0.76	0.76	65.10	114.75
2901	29.01	14.72	0.77	0.77	64.11	114.96
2902	29.02	15.12	0.79	0.79	63.17	115.15
2903	29.03	15.50	0.80	0.80	62.32	115.32
2904	29.04	15.83	0.81	0.81	61.59	115.47
2905	29.05	16.10	0.82	0.82	60.95	115.61
2906	29.06	16.40	0.83	0.83	60.32	115.76
2907	29.07	16.78	0.85	0.85	59.62	115.94
2908	29.08	17.22	0.86	0.86	58.82	116.14
2909	29.09	17.70	0.88	0.88	57.99	116.35
2910	29.10	18.19	0.90	0.90	57.17	116.57
2911	29.11	18.66	0.92	0.92	56.41	116.76
2912	29.12	19.10	0.93	0.93	55.72	116.94
2913	29.13	19.48	0.94	0.94	55.17	117.09
2914	29.14	19.74	0.95	0.95	54.76	117.19
2915	29.15	19.91	0.96	0.96	54.43	117.26
2916	29.16	20.11	0.96	0.96	54.12	117.33
2917	29.17	20.34	0.97	0.97	53.77	117.41
2918	29.18	20.58	0.98	0.98	53.41	117.48
2919	29.19	20.82	0.98	0.98	53.05	117.56
2920	29.20	21.06	0.99	0.99	52.71	117.63
2921	29.21	21.27	1.00	1.00	52.41	117.70
2922	29.22	21.44	1.00	1.00	52.21	117.74
2923	29.23	21.47	1.00	1.00	52.15	117.76
2924	29.24	21.41	1.00	1.00	52.21	117.75
2925	29.25	21.34	1.00	1.00	52.33	117.73
2926	29.26	21.26	1.00	1.00	52.46	117.71
2927	29.27	21.18	1.00	1.00	52.60	117.69
2928	29.28	21.10	0.99	0.99	52.74	117.67

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2929	29.29	21.03	0.99	0.99	52.87	117.65
2930	29.30	20.96	0.99	0.99	52.98	117.64
2931	29.31	20.91	0.99	0.99	53.03	117.63
2932	29.32	20.95	0.99	0.99	53.01	117.64
2933	29.33	21.02	0.99	0.99	52.92	117.65
2934	29.34	21.09	1.00	1.00	52.82	117.68
2935	29.35	21.17	1.00	1.00	52.70	117.70
2936	29.36	21.25	1.00	1.00	52.58	117.72
2937	29.37	21.33	1.00	1.00	52.46	117.74
2938	29.38	21.40	1.00	1.00	52.36	117.76
2939	29.39	21.46	1.00	1.00	52.24	117.78
2940	29.40	21.57	1.01	1.01	51.99	117.83
2941	29.41	21.90	1.01	1.01	51.56	117.90
2942	29.42	22.31	1.02	1.02	50.97	118.00
2943	29.43	22.77	1.03	1.03	50.32	118.11
2944	29.44	23.25	1.04	1.04	49.64	118.22
2945	29.45	23.74	1.05	1.05	48.97	118.33
2946	29.46	24.21	1.05	1.05	48.35	118.42
2947	29.47	24.62	1.06	1.06	47.80	118.50
2948	29.48	24.97	1.06	1.06	47.35	118.58
2949	29.49	25.26	1.07	1.07	46.97	118.66
2950	29.50	25.62	1.08	1.08	46.60	118.77
2951	29.51	26.05	1.10	1.10	46.19	118.89
2952	29.52	26.52	1.11	1.11	45.74	119.03
2953	29.53	27.00	1.12	1.12	45.29	119.16
2954	29.54	27.49	1.14	1.14	44.85	119.29
2955	29.55	27.94	1.15	1.15	44.46	119.41
2956	29.56	28.33	1.16	1.16	44.11	119.52
2957	29.57	28.65	1.17	1.17	43.89	119.60
2958	29.58	28.76	1.18	1.18	43.77	119.66
2959	29.59	28.89	1.19	1.19	43.73	119.73
2960	29.60	29.04	1.20	1.20	43.69	119.80
2961	29.61	29.20	1.21	1.21	43.65	119.88
2962	29.62	29.36	1.22	1.22	43.60	119.96
2963	29.63	29.52	1.23	1.23	43.56	120.04
2964	29.64	29.67	1.24	1.24	43.52	120.11
2965	29.65	29.79	1.25	1.25	43.51	120.16
2966	29.66	29.83	1.25	1.25	43.59	120.19
2967	29.67	29.66	1.26	1.26	43.77	120.20
2968	29.68	29.45	1.26	1.26	44.06	120.20
2969	29.69	29.22	1.26	1.26	44.37	120.20
2970	29.70	28.98	1.26	1.26	44.71	120.19
2971	29.71	28.74	1.26	1.26	45.05	120.18
2972	29.72	28.51	1.27	1.27	45.37	120.17
2973	29.73	28.30	1.27	1.27	45.67	120.17
2974	29.74	28.13	1.27	1.27	45.97	120.16
2975	29.75	27.89	1.27	1.27	46.35	120.15
2976	29.76	27.53	1.28	1.28	46.87	120.14

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
2977	29.77	27.10	1.28	1.28	47.51	120.12
2978	29.78	26.63	1.28	1.28	48.23	120.10
2979	29.79	26.14	1.29	1.29	48.97	120.07
2980	29.80	25.66	1.29	1.29	49.72	120.03
2981	29.81	25.21	1.29	1.29	50.43	119.99
2982	29.82	24.82	1.29	1.29	51.05	119.95
2983	29.83	24.50	1.29	1.29	51.41	119.96
2984	29.84	24.68	1.30	1.30	51.52	120.04
2985	29.85	24.94	1.32	1.32	51.40	120.17
2986	29.86	25.24	1.35	1.35	51.25	120.33
2987	29.87	25.56	1.37	1.37	51.10	120.49
2988	29.88	25.89	1.40	1.40	50.95	120.66
2989	29.89	26.20	1.42	1.42	50.80	120.82
2990	29.90	26.49	1.45	1.45	50.68	120.97
2991	29.91	26.74	1.47	1.47	50.55	121.09
2992	29.92	26.97	1.48	1.48	50.33	121.20
2993	29.93	27.37	1.50	1.50	49.99	121.31
2994	29.94	27.85	1.52	1.52	49.54	121.44
2995	29.95	28.38	1.54	1.54	49.04	121.58
2996	29.96	28.95	1.56	1.56	48.53	121.72
2997	29.97	29.52	1.58	1.58	48.02	121.86
2998	29.98	30.05	1.60	1.60	47.56	121.99
2999	29.99	30.54	1.61	1.61	47.15	122.11
3000	30.00	30.94	1.63	1.63	46.90	122.18
3001	30.01	31.00	1.63	1.63	46.85	122.23
3002	30.02	30.87	1.64	1.64	46.99	122.24
3003	30.03	30.73	1.64	1.64	47.22	122.25
3004	30.04	30.57	1.65	1.65	47.47	122.26
3005	30.05	30.41	1.65	1.65	47.72	122.27
3006	30.06	30.25	1.66	1.66	47.98	122.28
3007	30.07	30.10	1.66	1.66	48.21	122.28
3008	30.08	29.97	1.66	1.66	48.42	122.29
3009	30.09	29.87	1.67	1.67	48.55	122.30
3010	30.10	29.91	1.67	1.67	48.61	122.32
3011	30.11	29.98	1.68	1.68	48.62	122.36
3012	30.12	30.05	1.69	1.69	48.62	122.40
3013	30.13	30.13	1.70	1.70	48.62	122.45
3014	30.14	30.21	1.71	1.71	48.63	122.50
3015	30.15	30.29	1.72	1.72	48.63	122.54
3016	30.16	30.37	1.72	1.72	48.63	122.58
3017	30.17	30.43	1.73	1.73	48.61	122.62
3018	30.18	30.55	1.74	1.74	48.46	122.66
3019	30.19	30.89	1.74	1.74	48.18	122.72
3020	30.20	31.30	1.75	1.75	47.77	122.78
3021	30.21	31.76	1.76	1.76	47.31	122.85
3022	30.22	32.25	1.77	1.77	46.84	122.92
3023	30.23	32.73	1.78	1.78	46.37	122.99
3024	30.24	33.19	1.79	1.79	45.93	123.05

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3025	30.25	33.61	1.79	1.79	45.55	123.11
3026	30.26	33.95	1.80	1.80	45.26	123.15
3027	30.27	34.14	1.80	1.80	45.07	123.20
3028	30.28	34.33	1.81	1.81	44.94	123.24
3029	30.29	34.54	1.82	1.82	44.82	123.30
3030	30.30	34.78	1.83	1.83	44.68	123.36
3031	30.31	35.02	1.84	1.84	44.55	123.42
3032	30.32	35.26	1.85	1.85	44.41	123.48
3033	30.33	35.49	1.87	1.87	44.29	123.54
3034	30.34	35.68	1.87	1.87	44.18	123.59
3035	30.35	35.84	1.88	1.88	44.17	123.62
3036	30.36	35.73	1.89	1.89	44.26	123.64
3037	30.37	35.60	1.89	1.89	44.44	123.65
3038	30.38	35.45	1.90	1.90	44.66	123.67
3039	30.39	35.29	1.91	1.91	44.89	123.68
3040	30.40	35.13	1.91	1.91	45.12	123.70
3041	30.41	34.97	1.92	1.92	45.35	123.71
3042	30.42	34.83	1.92	1.92	45.55	123.72
3043	30.43	34.71	1.93	1.93	45.73	123.73
3044	30.44	34.59	1.93	1.93	45.89	123.72
3045	30.45	34.42	1.93	1.93	46.04	123.70
3046	30.46	34.22	1.92	1.92	46.22	123.67
3047	30.47	33.99	1.92	1.92	46.43	123.63
3048	30.48	33.74	1.91	1.91	46.64	123.59
3049	30.49	33.50	1.90	1.90	46.85	123.55
3050	30.50	33.27	1.90	1.90	47.06	123.51
3051	30.51	33.06	1.89	1.89	47.24	123.47
3052	30.52	32.89	1.89	1.89	47.30	123.47
3053	30.53	33.12	1.89	1.89	47.15	123.50
3054	30.54	33.61	1.91	1.91	46.79	123.58
3055	30.55	34.19	1.93	1.93	46.33	123.69
3056	30.56	34.82	1.95	1.95	45.83	123.80
3057	30.57	35.47	1.96	1.96	45.33	123.91
3058	30.58	36.11	1.98	1.98	44.84	124.02
3059	30.59	36.70	2.00	2.00	44.39	124.11
3060	30.60	37.22	2.01	2.01	44.01	124.19
3061	30.61	37.65	2.02	2.02	43.53	124.30
3062	30.62	38.69	2.05	2.05	42.90	124.45
3063	30.63	40.00	2.09	2.09	42.05	124.66
3064	30.64	41.50	2.13	2.13	41.11	124.88
3065	30.65	43.10	2.16	2.16	40.14	125.10
3066	30.66	44.73	2.20	2.20	39.19	125.31
3067	30.67	46.30	2.23	2.23	38.30	125.49
3068	30.68	47.73	2.26	2.26	37.52	125.65
3069	30.69	48.95	2.28	2.28	36.85	125.78
3070	30.70	49.98	2.29	2.29	36.23	125.90
3071	30.71	51.35	2.32	2.32	35.55	126.04
3072	30.72	53.01	2.35	2.35	34.76	126.20

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3073	30.73	54.86	2.37	2.37	33.90	126.36
3074	30.74	56.81	2.39	2.39	33.03	126.51
3075	30.75	58.75	2.41	2.41	32.17	126.65
3076	30.76	60.59	2.43	2.43	31.39	126.76
3077	30.77	62.23	2.44	2.44	30.70	126.86
3078	30.78	63.58	2.44	2.44	30.13	126.93
3079	30.79	64.75	2.45	2.45	29.58	126.99
3080	30.80	66.23	2.45	2.45	28.99	127.06
3081	30.81	67.96	2.45	2.45	28.32	127.12
3082	30.82	69.86	2.45	2.45	27.59	127.18
3083	30.83	71.81	2.44	2.44	26.85	127.23
3084	30.84	73.73	2.43	2.43	26.14	127.26
3085	30.85	75.51	2.42	2.42	25.48	127.28
3086	30.86	77.06	2.40	2.40	24.92	127.29
3087	30.87	78.27	2.39	2.39	24.52	127.30
3088	30.88	79.01	2.40	2.40	24.22	127.33
3089	30.89	79.93	2.40	2.40	23.98	127.37
3090	30.90	80.98	2.41	2.41	23.70	127.42
3091	30.91	82.10	2.41	2.41	23.40	127.47
3092	30.92	83.24	2.42	2.42	23.11	127.51
3093	30.93	84.34	2.42	2.42	22.82	127.56
3094	30.94	85.34	2.42	2.42	22.57	127.59
3095	30.95	86.18	2.42	2.42	22.38	127.62
3096	30.96	86.64	2.43	2.43	22.31	127.67
3097	30.97	86.76	2.45	2.45	22.33	127.73
3098	30.98	86.89	2.48	2.48	22.41	127.80
3099	30.99	87.05	2.51	2.51	22.51	127.89
3100	31.00	87.21	2.54	2.54	22.60	127.98
3101	31.01	87.37	2.57	2.57	22.70	128.07
3102	31.02	87.53	2.59	2.59	22.79	128.15
3103	31.03	87.66	2.62	2.62	22.87	128.22
3104	31.04	87.77	2.64	2.64	22.94	128.28
3105	31.05	87.76	2.65	2.65	23.01	128.32
3106	31.06	87.70	2.67	2.67	23.10	128.37
3107	31.07	87.63	2.69	2.69	23.20	128.41
3108	31.08	87.55	2.70	2.70	23.31	128.46
3109	31.09	87.47	2.72	2.72	23.42	128.51
3110	31.10	87.39	2.74	2.74	23.53	128.56
3111	31.11	87.31	2.76	2.76	23.63	128.60
3112	31.12	87.25	2.78	2.78	23.72	128.64
3113	31.13	87.21	2.79	2.79	23.78	128.68
3114	31.14	87.31	2.80	2.80	23.83	128.72
3115	31.15	87.45	2.82	2.82	23.88	128.77
3116	31.16	87.60	2.84	2.84	23.93	128.82
3117	31.17	87.76	2.86	2.86	23.98	128.88
3118	31.18	87.92	2.89	2.89	24.03	128.94
3119	31.19	88.08	2.91	2.91	24.08	129.00
3120	31.20	88.22	2.93	2.93	24.13	129.05

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3121	31.21	88.34	2.94	2.94	24.16	129.10
3122	31.22	88.49	2.95	2.95	24.18	129.14
3123	31.23	88.78	2.97	2.97	24.17	129.18
3124	31.24	89.13	2.98	2.98	24.15	129.23
3125	31.25	89.52	3.00	3.00	24.12	129.28
3126	31.26	89.92	3.02	3.02	24.10	129.34
3127	31.27	90.33	3.04	3.04	24.07	129.40
3128	31.28	90.71	3.06	3.06	24.05	129.45
3129	31.29	91.05	3.08	3.08	24.03	129.50
3130	31.30	91.33	3.09	3.09	24.00	129.53
3131	31.31	91.64	3.10	3.10	23.95	129.57
3132	31.32	92.08	3.11	3.11	23.88	129.60
3133	31.33	92.59	3.11	3.11	23.79	129.63
3134	31.34	93.14	3.12	3.12	23.69	129.67
3135	31.35	93.71	3.13	3.13	23.59	129.71
3136	31.36	94.27	3.14	3.14	23.49	129.74
3137	31.37	94.79	3.15	3.15	23.40	129.78
3138	31.38	95.24	3.16	3.16	23.32	129.81
3139	31.39	95.62	3.17	3.17	23.23	129.84
3140	31.40	96.31	3.18	3.18	23.12	129.88
3141	31.41	97.17	3.19	3.19	22.97	129.93
3142	31.42	98.15	3.21	3.21	22.80	129.99
3143	31.43	99.19	3.22	3.22	22.61	130.05
3144	31.44	100.25	3.24	3.24	22.43	130.11
3145	31.45	101.27	3.25	3.25	22.26	130.16
3146	31.46	102.19	3.26	3.26	22.10	130.21
3147	31.47	102.97	3.28	3.28	21.97	130.25
3148	31.48	103.64	3.28	3.28	21.84	130.29
3149	31.49	104.51	3.29	3.29	21.69	130.34
3150	31.50	105.55	3.31	3.31	21.52	130.39
3151	31.51	106.72	3.32	3.32	21.33	130.45
3152	31.52	107.93	3.34	3.34	21.13	130.50
3153	31.53	109.14	3.35	3.35	20.94	130.56
3154	31.54	110.29	3.36	3.36	20.76	130.61
3155	31.55	111.30	3.37	3.37	20.60	130.65
3156	31.56	112.13	3.38	3.38	20.46	130.69
3157	31.57	112.87	3.38	3.38	20.32	130.72
3158	31.58	113.81	3.39	3.39	20.17	130.76
3159	31.59	114.90	3.40	3.40	19.99	130.79
3160	31.60	116.09	3.40	3.40	19.80	130.83
3161	31.61	117.31	3.41	3.41	19.60	130.87
3162	31.62	118.50	3.41	3.41	19.41	130.90
3163	31.63	119.61	3.42	3.42	19.23	130.93
3164	31.64	120.57	3.42	3.42	19.08	130.96
3165	31.65	121.31	3.42	3.42	18.95	130.98
3166	31.66	122.01	3.42	3.42	18.81	130.99
3167	31.67	122.87	3.42	3.42	18.66	131.00
3168	31.68	123.85	3.41	3.41	18.48	131.00

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3169	31.69	124.90	3.40	3.40	18.29	131.01
3170	31.70	125.96	3.40	3.40	18.10	131.01
3171	31.71	126.97	3.39	3.39	17.92	131.02
3172	31.72	127.89	3.38	3.38	17.76	131.02
3173	31.73	128.67	3.38	3.38	17.63	131.02
3174	31.74	129.18	3.37	3.37	17.53	131.02
3175	31.75	129.65	3.37	3.37	17.44	131.02
3176	31.76	130.21	3.37	3.37	17.35	131.03
3177	31.77	130.83	3.36	3.36	17.24	131.03
3178	31.78	131.48	3.36	3.36	17.14	131.03
3179	31.79	132.13	3.35	3.35	17.03	131.04
3180	31.80	132.74	3.35	3.35	16.93	131.04
3181	31.81	133.28	3.35	3.35	16.85	131.04
3182	31.82	133.71	3.34	3.34	16.78	131.04
3183	31.83	133.99	3.34	3.34	16.74	131.05
3184	31.84	134.30	3.35	3.35	16.71	131.07
3185	31.85	134.67	3.35	3.35	16.67	131.09
3186	31.86	135.06	3.36	3.36	16.64	131.10
3187	31.87	135.47	3.37	3.37	16.60	131.12
3188	31.88	135.87	3.37	3.37	16.56	131.14
3189	31.89	136.24	3.38	3.38	16.53	131.16
3190	31.90	136.56	3.38	3.38	16.50	131.18
3191	31.91	136.77	3.38	3.38	16.49	131.19
3192	31.92	136.77	3.39	3.39	16.49	131.19
3193	31.93	136.77	3.39	3.39	16.50	131.20
3194	31.94	136.77	3.39	3.39	16.52	131.21
3195	31.95	136.77	3.40	3.40	16.53	131.22
3196	31.96	136.77	3.40	3.40	16.55	131.23
3197	31.97	136.77	3.41	3.41	16.56	131.24
3198	31.98	136.77	3.41	3.41	16.58	131.25
3199	31.99	136.77	3.41	3.41	16.59	131.25
3200	32.00	136.73	3.42	3.42	16.61	131.26
3201	32.01	136.61	3.42	3.42	16.65	131.27
3202	32.02	136.47	3.43	3.43	16.69	131.29
3203	32.03	136.32	3.44	3.44	16.74	131.30
3204	32.04	136.15	3.45	3.45	16.79	131.32
3205	32.05	135.99	3.46	3.46	16.84	131.33
3206	32.06	135.84	3.47	3.47	16.89	131.35
3207	32.07	135.71	3.47	3.47	16.93	131.36
3208	32.08	135.60	3.48	3.48	16.97	131.37
3209	32.09	135.50	3.49	3.49	17.01	131.38
3210	32.10	135.37	3.49	3.49	17.05	131.39
3211	32.11	135.23	3.50	3.50	17.09	131.41
3212	32.12	135.07	3.51	3.51	17.14	131.42
3213	32.13	134.90	3.52	3.52	17.19	131.44
3214	32.14	134.74	3.53	3.53	17.24	131.45
3215	32.15	134.60	3.53	3.53	17.29	131.46
3216	32.16	134.47	3.54	3.54	17.33	131.47

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3217	32.17	134.37	3.54	3.54	17.37	131.49
3218	32.18	134.26	3.55	3.55	17.40	131.50
3219	32.19	134.13	3.56	3.56	17.45	131.51
3220	32.20	133.98	3.57	3.57	17.49	131.52
3221	32.21	133.82	3.57	3.57	17.54	131.53
3222	32.22	133.65	3.58	3.58	17.59	131.55
3223	32.23	133.50	3.59	3.59	17.64	131.56
3224	32.24	133.36	3.60	3.60	17.69	131.57
3225	32.25	133.24	3.60	3.60	17.72	131.58
3226	32.26	133.17	3.61	3.61	17.75	131.59
3227	32.27	133.11	3.61	3.61	17.78	131.60
3228	32.28	133.04	3.62	3.62	17.81	131.61
3229	32.29	132.96	3.62	3.62	17.84	131.62
3230	32.30	132.88	3.63	3.63	17.87	131.63
3231	32.31	132.80	3.64	3.64	17.90	131.64
3232	32.32	132.72	3.64	3.64	17.93	131.65
3233	32.33	132.66	3.65	3.65	17.96	131.66
3234	32.34	132.60	3.65	3.65	17.98	131.67
3235	32.35	132.59	3.66	3.66	18.00	131.68
3236	32.36	132.59	3.66	3.66	18.03	131.69
3237	32.37	132.59	3.67	3.67	18.05	131.71
3238	32.38	132.59	3.68	3.68	18.08	131.72
3239	32.39	132.59	3.69	3.69	18.10	131.74
3240	32.40	132.59	3.70	3.70	18.13	131.76
3241	32.41	132.59	3.70	3.70	18.15	131.77
3242	32.42	132.59	3.71	3.71	18.17	131.78
3243	32.43	132.59	3.71	3.71	18.19	131.79
3244	32.44	132.59	3.72	3.72	18.21	131.81
3245	32.45	132.59	3.73	3.73	18.24	131.82
3246	32.46	132.59	3.73	3.73	18.26	131.83
3247	32.47	132.59	3.74	3.74	18.29	131.85
3248	32.48	132.59	3.75	3.75	18.31	131.87
3249	32.49	132.59	3.76	3.76	18.34	131.88
3250	32.50	132.59	3.77	3.77	18.36	131.90
3251	32.51	132.59	3.77	3.77	18.38	131.91
3252	32.52	132.62	3.78	3.78	18.40	131.92
3253	32.53	132.68	3.79	3.79	18.42	131.94
3254	32.54	132.75	3.80	3.80	18.43	131.96
3255	32.55	132.83	3.81	3.81	18.45	131.98
3256	32.56	132.91	3.82	3.82	18.47	132.00
3257	32.57	132.99	3.83	3.83	18.49	132.02
3258	32.58	133.06	3.84	3.84	18.51	132.04
3259	32.59	133.13	3.85	3.85	18.53	132.06
3260	32.60	133.19	3.85	3.85	18.53	132.09
3261	32.61	133.92	3.88	3.88	18.51	132.15
3262	32.62	134.97	3.92	3.92	18.46	132.23
3263	32.63	136.18	3.96	3.96	18.40	132.33
3264	32.64	137.49	4.01	4.01	18.34	132.44

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3265	32.65	138.84	4.06	4.06	18.27	132.55
3266	32.66	140.15	4.10	4.10	18.21	132.65
3267	32.67	141.35	4.15	4.15	18.16	132.75
3268	32.68	142.39	4.18	4.18	18.11	132.83
3269	32.69	143.19	4.21	4.21	18.07	132.90
3270	32.70	144.02	4.24	4.24	18.04	132.97
3271	32.71	145.05	4.28	4.28	17.99	133.05
3272	32.72	146.21	4.32	4.32	17.95	133.15
3273	32.73	147.43	4.37	4.37	17.90	133.24
3274	32.74	148.67	4.41	4.41	17.85	133.34
3275	32.75	149.84	4.46	4.46	17.80	133.43
3276	32.76	150.91	4.50	4.50	17.76	133.51
3277	32.77	151.80	4.53	4.53	17.74	133.57
3278	32.78	152.18	4.55	4.55	17.73	133.61
3279	32.79	152.31	4.57	4.57	17.75	133.64
3280	32.80	152.46	4.58	4.58	17.77	133.67
3281	32.81	152.63	4.60	4.60	17.80	133.71
3282	32.82	152.81	4.62	4.62	17.82	133.74
3283	32.83	152.98	4.64	4.64	17.85	133.77
3284	32.84	153.15	4.66	4.66	17.87	133.80
3285	32.85	153.29	4.68	4.68	17.89	133.83
3286	32.86	153.41	4.69	4.69	17.91	133.86
3287	32.87	153.68	4.70	4.70	17.91	133.88
3288	32.88	154.05	4.72	4.72	17.90	133.91
3289	32.89	154.48	4.73	4.73	17.89	133.94
3290	32.90	154.94	4.75	4.75	17.87	133.98
3291	32.91	155.41	4.77	4.77	17.86	134.02
3292	32.92	155.87	4.79	4.79	17.85	134.05
3293	32.93	156.30	4.81	4.81	17.84	134.08
3294	32.94	156.66	4.82	4.82	17.83	134.11
3295	32.95	156.96	4.83	4.83	17.81	134.13
3296	32.96	157.39	4.84	4.84	17.77	134.15
3297	32.97	157.91	4.85	4.85	17.73	134.17
3298	32.98	158.50	4.86	4.86	17.68	134.19
3299	32.99	159.13	4.87	4.87	17.62	134.22
3300	33.00	159.76	4.88	4.88	17.57	134.24
3301	33.01	160.36	4.88	4.88	17.52	134.26
3302	33.02	160.89	4.89	4.89	17.47	134.28
3303	33.03	161.34	4.90	4.90	17.43	134.29
3304	33.04	161.72	4.90	4.90	17.38	134.30
3305	33.05	162.20	4.90	4.90	17.33	134.31
3306	33.06	162.77	4.90	4.90	17.26	134.32
3307	33.07	163.40	4.90	4.90	17.18	134.33
3308	33.08	164.05	4.90	4.90	17.11	134.33
3309	33.09	164.69	4.89	4.89	17.03	134.34
3310	33.10	165.29	4.89	4.89	16.96	134.35
3311	33.11	165.82	4.89	4.89	16.90	134.35
3312	33.12	166.25	4.89	4.89	16.84	134.36

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3313	33.13	166.73	4.89	4.89	16.78	134.37
3314	33.14	167.34	4.89	4.89	16.72	134.38
3315	33.15	168.05	4.89	4.89	16.64	134.39
3316	33.16	168.82	4.89	4.89	16.56	134.40
3317	33.17	169.60	4.90	4.90	16.48	134.41
3318	33.18	170.36	4.90	4.90	16.40	134.43
3319	33.19	171.06	4.90	4.90	16.33	134.44
3320	33.20	171.66	4.90	4.90	16.26	134.45
3321	33.21	172.11	4.90	4.90	16.21	134.45
3322	33.22	172.55	4.90	4.90	16.16	134.46
3323	33.23	173.09	4.89	4.89	16.09	134.46
3324	33.24	173.71	4.89	4.89	16.02	134.46
3325	33.25	174.35	4.88	4.88	15.95	134.47
3326	33.26	175.00	4.88	4.88	15.87	134.47
3327	33.27	175.62	4.88	4.88	15.80	134.47
3328	33.28	176.18	4.87	4.87	15.74	134.47
3329	33.29	176.64	4.87	4.87	15.69	134.47
3330	33.30	176.82	4.86	4.86	15.65	134.47
3331	33.31	176.88	4.85	4.85	15.62	134.45
3332	33.32	176.95	4.84	4.84	15.59	134.43
3333	33.33	177.03	4.83	4.83	15.55	134.41
3334	33.34	177.11	4.81	4.81	15.51	134.39
3335	33.35	177.19	4.80	4.80	15.48	134.37
3336	33.36	177.27	4.78	4.78	15.44	134.35
3337	33.37	177.33	4.77	4.77	15.41	134.34
3338	33.38	177.39	4.76	4.76	15.39	134.32
3339	33.39	177.15	4.75	4.75	15.39	134.30
3340	33.40	176.83	4.74	4.74	15.40	134.28
3341	33.41	176.46	4.72	4.72	15.40	134.25
3342	33.42	176.06	4.71	4.71	15.41	134.22
3343	33.43	175.65	4.69	4.69	15.42	134.19
3344	33.44	175.26	4.67	4.67	15.43	134.16
3345	33.45	174.89	4.66	4.66	15.44	134.13
3346	33.46	174.58	4.65	4.65	15.44	134.11
3347	33.47	174.28	4.64	4.64	15.46	134.08
3348	33.48	173.72	4.62	4.62	15.48	134.05
3349	33.49	173.04	4.60	4.60	15.52	134.01
3350	33.50	172.27	4.58	4.58	15.56	133.97
3351	33.51	171.46	4.56	4.56	15.60	133.92
3352	33.52	170.65	4.54	4.54	15.64	133.88
3353	33.53	169.88	4.52	4.52	15.67	133.84
3354	33.54	169.19	4.50	4.50	15.71	133.80
3355	33.55	168.61	4.49	4.49	15.75	133.76
3356	33.56	168.01	4.48	4.48	15.80	133.73
3357	33.57	167.16	4.47	4.47	15.86	133.70
3358	33.58	166.16	4.45	4.45	15.95	133.67
3359	33.59	165.06	4.44	4.44	16.04	133.63
3360	33.60	163.92	4.42	4.42	16.14	133.59

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3361	33.61	162.80	4.41	4.41	16.23	133.55
3362	33.62	161.75	4.39	4.39	16.32	133.51
3363	33.63	160.83	4.38	4.38	16.40	133.48
3364	33.64	160.10	4.37	4.37	16.48	133.45
3365	33.65	159.33	4.37	4.37	16.56	133.42
3366	33.66	158.36	4.36	4.36	16.66	133.40
3367	33.67	157.24	4.35	4.35	16.78	133.37
3368	33.68	156.05	4.34	4.34	16.91	133.33
3369	33.69	154.82	4.33	4.33	17.04	133.30
3370	33.70	153.64	4.32	4.32	17.16	133.27
3371	33.71	152.56	4.32	4.32	17.28	133.23
3372	33.72	151.63	4.31	4.31	17.38	133.21
3373	33.73	150.92	4.30	4.30	17.47	133.18
3374	33.74	150.13	4.29	4.29	17.56	133.15
3375	33.75	149.17	4.28	4.28	17.66	133.12
3376	33.76	148.10	4.27	4.27	17.77	133.08
3377	33.77	146.97	4.25	4.25	17.89	133.04
3378	33.78	145.83	4.24	4.24	18.01	132.99
3379	33.79	144.75	4.22	4.22	18.12	132.95
3380	33.80	143.79	4.21	4.21	18.22	132.91
3381	33.81	142.99	4.20	4.20	18.31	132.88
3382	33.82	142.34	4.19	4.19	18.40	132.85
3383	33.83	141.55	4.18	4.18	18.49	132.82
3384	33.84	140.62	4.17	4.17	18.59	132.78
3385	33.85	139.60	4.16	4.16	18.71	132.74
3386	33.86	138.54	4.14	4.14	18.83	132.70
3387	33.87	137.50	4.13	4.13	18.95	132.66
3388	33.88	136.52	4.12	4.12	19.06	132.62
3389	33.89	135.67	4.11	4.11	19.16	132.58
3390	33.90	135.00	4.10	4.10	19.23	132.57
3391	33.91	134.92	4.10	4.10	19.28	132.56
3392	33.92	134.83	4.11	4.11	19.32	132.57
3393	33.93	134.73	4.12	4.12	19.36	132.59
3394	33.94	134.62	4.13	4.13	19.40	132.60
3395	33.95	134.51	4.14	4.14	19.45	132.62
3396	33.96	134.41	4.15	4.15	19.49	132.63
3397	33.97	134.31	4.15	4.15	19.53	132.64
3398	33.98	134.23	4.16	4.16	19.57	132.65
3399	33.99	134.17	4.17	4.17	19.60	132.67
3400	34.00	134.12	4.17	4.17	19.63	132.68
3401	34.01	134.05	4.18	4.18	19.67	132.69
3402	34.02	133.97	4.19	4.19	19.71	132.71
3403	34.03	133.89	4.20	4.20	19.75	132.72
3404	34.04	133.81	4.21	4.21	19.79	132.74
3405	34.05	133.73	4.22	4.22	19.83	132.75
3406	34.06	133.66	4.23	4.23	19.87	132.77
3407	34.07	133.61	4.24	4.24	19.91	132.77
3408	34.08	133.41	4.24	4.24	19.94	132.77

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3409	34.09	133.06	4.23	4.23	19.99	132.76
3410	34.10	132.65	4.23	4.23	20.04	132.74
3411	34.11	132.21	4.22	4.22	20.10	132.72
3412	34.12	131.74	4.22	4.22	20.16	132.70
3413	34.13	131.29	4.21	4.21	20.21	132.69
3414	34.14	130.87	4.20	4.20	20.27	132.67
3415	34.15	130.50	4.20	4.20	20.32	132.65
3416	34.16	130.21	4.19	4.19	20.35	132.65
3417	34.17	130.26	4.20	4.20	20.37	132.65
3418	34.18	130.32	4.21	4.21	20.39	132.67
3419	34.19	130.40	4.22	4.22	20.41	132.69
3420	34.20	130.48	4.23	4.23	20.43	132.71
3421	34.21	130.56	4.24	4.24	20.45	132.73
3422	34.22	130.64	4.25	4.25	20.46	132.75
3423	34.23	130.71	4.26	4.26	20.48	132.76
3424	34.24	130.77	4.27	4.27	20.50	132.78
3425	34.25	130.88	4.28	4.28	20.50	132.80
3426	34.26	131.17	4.29	4.29	20.50	132.83
3427	34.27	131.51	4.31	4.31	20.50	132.87
3428	34.28	131.90	4.33	4.33	20.49	132.91
3429	34.29	132.30	4.35	4.35	20.49	132.95
3430	34.30	132.71	4.38	4.38	20.48	132.99
3431	34.31	133.09	4.40	4.40	20.48	133.04
3432	34.32	133.43	4.41	4.41	20.47	133.07
3433	34.33	133.72	4.43	4.43	20.46	133.10
3434	34.34	134.13	4.44	4.44	20.43	133.14
3435	34.35	134.74	4.46	4.46	20.39	133.17
3436	34.36	135.46	4.48	4.48	20.33	133.22
3437	34.37	136.25	4.50	4.50	20.26	133.27
3438	34.38	137.06	4.53	4.53	20.20	133.32
3439	34.39	137.86	4.55	4.55	20.13	133.37
3440	34.40	138.61	4.57	4.57	20.07	133.41
3441	34.41	139.26	4.59	4.59	20.02	133.45
3442	34.42	139.77	4.60	4.60	19.97	133.49
3443	34.43	140.40	4.61	4.61	19.90	133.52
3444	34.44	141.19	4.63	4.63	19.83	133.56
3445	34.45	142.08	4.64	4.64	19.74	133.60
3446	34.46	143.05	4.66	4.66	19.64	133.64
3447	34.47	144.02	4.68	4.68	19.55	133.69
3448	34.48	144.97	4.70	4.70	19.46	133.73
3449	34.49	145.83	4.71	4.71	19.37	133.77
3450	34.50	146.56	4.73	4.73	19.30	133.80
3451	34.51	147.17	4.73	4.73	19.22	133.82
3452	34.52	147.97	4.74	4.74	19.12	133.84
3453	34.53	148.94	4.74	4.74	18.99	133.86
3454	34.54	150.02	4.74	4.74	18.85	133.88
3455	34.55	151.15	4.74	4.74	18.71	133.90
3456	34.56	152.28	4.75	4.75	18.56	133.92

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3457	34.57	153.36	4.75	4.75	18.42	133.94
3458	34.58	154.31	4.75	4.75	18.30	133.96
3459	34.59	155.10	4.75	4.75	18.19	133.97
3460	34.60	155.89	4.74	4.74	18.07	133.98
3461	34.61	156.93	4.74	4.74	17.93	133.99
3462	34.62	158.16	4.73	4.73	17.76	133.99
3463	34.63	159.51	4.72	4.72	17.57	134.00
3464	34.64	160.89	4.71	4.71	17.38	134.01
3465	34.65	162.25	4.70	4.70	17.19	134.01
3466	34.66	163.51	4.69	4.69	17.02	134.01
3467	34.67	164.61	4.68	4.68	16.87	134.01
3468	34.68	165.47	4.67	4.67	16.74	134.01
3469	34.69	166.21	4.65	4.65	16.60	133.99
3470	34.70	167.13	4.63	4.63	16.44	133.96
3471	34.71	168.18	4.60	4.60	16.25	133.93
3472	34.72	169.30	4.56	4.56	16.06	133.89
3473	34.73	170.44	4.53	4.53	15.86	133.86
3474	34.74	171.54	4.49	4.49	15.66	133.82
3475	34.75	172.54	4.46	4.46	15.49	133.78
3476	34.76	173.39	4.44	4.44	15.34	133.75
3477	34.77	173.99	4.41	4.41	15.21	133.71
3478	34.78	174.56	4.38	4.38	15.08	133.67
3479	34.79	175.26	4.35	4.35	14.93	133.63
3480	34.80	176.03	4.31	4.31	14.76	133.57
3481	34.81	176.84	4.27	4.27	14.59	133.51
3482	34.82	177.65	4.23	4.23	14.41	133.45
3483	34.83	178.41	4.19	4.19	14.25	133.39
3484	34.84	179.10	4.15	4.15	14.10	133.34
3485	34.85	179.65	4.12	4.12	13.98	133.29
3486	34.86	180.00	4.10	4.10	13.88	133.25
3487	34.87	180.37	4.07	4.07	13.78	133.21
3488	34.88	180.80	4.04	4.04	13.67	133.16
3489	34.89	181.28	4.00	4.00	13.54	133.11
3490	34.90	181.77	3.97	3.97	13.42	133.05
3491	34.91	182.24	3.93	3.93	13.29	132.99
3492	34.92	182.69	3.90	3.90	13.18	132.94
3493	34.93	183.08	3.87	3.87	13.08	132.89
3494	34.94	183.35	3.85	3.85	13.00	132.84
3495	34.95	183.14	3.82	3.82	12.93	132.78
3496	34.96	182.87	3.78	3.78	12.87	132.70
3497	34.97	182.57	3.74	3.74	12.79	132.62
3498	34.98	182.25	3.69	3.69	12.71	132.52
3499	34.99	181.93	3.64	3.64	12.63	132.42
3500	35.00	181.61	3.60	3.60	12.55	132.33
3501	35.01	181.33	3.56	3.56	12.47	132.24
3502	35.02	181.09	3.52	3.52	12.42	132.17
3503	35.03	180.74	3.50	3.50	12.38	132.10
3504	35.04	180.05	3.47	3.47	12.36	132.03

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3505	35.05	179.21	3.43	3.43	12.35	131.94
3506	35.06	178.28	3.39	3.39	12.34	131.85
3507	35.07	177.31	3.35	3.35	12.32	131.75
3508	35.08	176.34	3.31	3.31	12.31	131.65
3509	35.09	175.42	3.27	3.27	12.29	131.55
3510	35.10	174.61	3.24	3.24	12.28	131.47
3511	35.11	173.94	3.21	3.21	12.28	131.39
3512	35.12	173.13	3.19	3.19	12.30	131.33
3513	35.13	172.01	3.16	3.16	12.34	131.25
3514	35.14	170.70	3.14	3.14	12.38	131.17
3515	35.15	169.28	3.10	3.10	12.43	131.08
3516	35.16	167.81	3.07	3.07	12.49	130.98
3517	35.17	166.38	3.04	3.04	12.54	130.89
3518	35.18	165.04	3.01	3.01	12.59	130.80
3519	35.19	163.89	2.99	2.99	12.64	130.72
3520	35.20	162.95	2.97	2.97	12.70	130.65
3521	35.21	161.62	2.95	2.95	12.78	130.58
3522	35.22	159.96	2.93	2.93	12.88	130.51
3523	35.23	158.08	2.90	2.90	13.01	130.42
3524	35.24	156.07	2.88	2.88	13.14	130.32
3525	35.25	154.04	2.85	2.85	13.28	130.22
3526	35.26	152.08	2.82	2.82	13.42	130.12
3527	35.27	150.31	2.80	2.80	13.54	130.03
3528	35.28	148.81	2.78	2.78	13.65	129.95
3529	35.29	147.61	2.76	2.76	13.76	129.87
3530	35.30	146.16	2.74	2.74	13.86	129.79
3531	35.31	144.41	2.71	2.71	13.99	129.70
3532	35.32	142.47	2.69	2.69	14.14	129.59
3533	35.33	140.44	2.66	2.66	14.30	129.48
3534	35.34	138.43	2.63	2.63	14.45	129.37
3535	35.35	136.52	2.60	2.60	14.61	129.25
3536	35.36	134.83	2.57	2.57	14.74	129.16
3537	35.37	133.45	2.55	2.55	14.85	129.07
3538	35.38	132.34	2.53	2.53	14.95	128.97
3539	35.39	130.96	2.50	2.50	15.03	128.86
3540	35.40	129.36	2.47	2.47	15.13	128.74
3541	35.41	127.61	2.43	2.43	15.24	128.59
3542	35.42	125.82	2.39	2.39	15.36	128.45
3543	35.43	124.07	2.35	2.35	15.48	128.30
3544	35.44	122.45	2.32	2.32	15.59	128.16
3545	35.45	121.04	2.29	2.29	15.68	128.04
3546	35.46	119.97	2.27	2.27	15.75	127.94
3547	35.47	119.17	2.25	2.25	15.81	127.85
3548	35.48	118.17	2.22	2.22	15.87	127.75
3549	35.49	117.04	2.19	2.19	15.93	127.64
3550	35.50	115.83	2.16	2.16	16.00	127.51
3551	35.51	114.61	2.13	2.13	16.08	127.39
3552	35.52	113.44	2.11	2.11	16.15	127.26

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3553	35.53	112.38	2.08	2.08	16.21	127.15
3554	35.54	111.49	2.06	2.06	16.27	127.06
3555	35.55	110.92	2.05	2.05	16.32	127.00
3556	35.56	110.45	2.04	2.04	16.38	126.96
3557	35.57	109.89	2.03	2.03	16.44	126.92
3558	35.58	109.27	2.02	2.02	16.52	126.88
3559	35.59	108.62	2.02	2.02	16.59	126.84
3560	35.60	107.98	2.01	2.01	16.67	126.79
3561	35.61	107.37	2.00	2.00	16.75	126.75
3562	35.62	106.83	1.99	1.99	16.81	126.71
3563	35.63	106.39	1.99	1.99	16.87	126.69
3564	35.64	106.07	1.99	1.99	16.94	126.67
3565	35.65	105.70	1.99	1.99	17.03	126.68
3566	35.66	105.26	1.99	1.99	17.13	126.68
3567	35.67	104.78	2.00	2.00	17.24	126.68
3568	35.68	104.29	2.00	2.00	17.36	126.69
3569	35.69	103.82	2.01	2.01	17.47	126.69
3570	35.70	103.37	2.01	2.01	17.57	126.69
3571	35.71	102.99	2.01	2.01	17.66	126.69
3572	35.72	102.71	2.01	2.01	17.74	126.70
3573	35.73	102.55	2.02	2.02	17.81	126.71
3574	35.74	102.35	2.03	2.03	17.88	126.73
3575	35.75	102.12	2.03	2.03	17.97	126.75
3576	35.76	101.88	2.04	2.04	18.06	126.78
3577	35.77	101.64	2.05	2.05	18.15	126.80
3578	35.78	101.40	2.06	2.06	18.23	126.82
3579	35.79	101.19	2.07	2.07	18.31	126.84
3580	35.80	101.01	2.07	2.07	18.37	126.85
3581	35.81	100.96	2.07	2.07	18.41	126.87
3582	35.82	101.02	2.08	2.08	18.42	126.88
3583	35.83	101.09	2.08	2.08	18.43	126.90
3584	35.84	101.17	2.09	2.09	18.44	126.92
3585	35.85	101.25	2.09	2.09	18.45	126.93
3586	35.86	101.33	2.10	2.10	18.46	126.95
3587	35.87	101.41	2.10	2.10	18.47	126.97
3588	35.88	101.47	2.11	2.11	18.47	126.99
3589	35.89	101.53	2.11	2.11	18.47	127.00
3590	35.90	101.70	2.11	2.11	18.45	127.01
3591	35.91	101.95	2.11	2.11	18.40	127.01
3592	35.92	102.25	2.11	2.11	18.34	127.02
3593	35.93	102.56	2.11	2.11	18.28	127.03
3594	35.94	102.89	2.11	2.11	18.22	127.04
3595	35.95	103.21	2.11	2.11	18.16	127.04
3596	35.96	103.50	2.11	2.11	18.10	127.05
3597	35.97	103.76	2.11	2.11	18.06	127.06
3598	35.98	103.95	2.11	2.11	18.01	127.06
3599	35.99	104.17	2.11	2.11	17.95	127.05
3600	36.00	104.44	2.10	2.10	17.87	127.04

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3601	36.01	104.74	2.09	2.09	17.78	127.02
3602	36.02	105.06	2.09	2.09	17.69	127.01
3603	36.03	105.39	2.08	2.08	17.60	126.99
3604	36.04	105.70	2.07	2.07	17.51	126.97
3605	36.05	105.98	2.07	2.07	17.43	126.96
3606	36.06	106.22	2.06	2.06	17.36	126.94
3607	36.07	106.39	2.05	2.05	17.29	126.92
3608	36.08	106.56	2.04	2.04	17.20	126.89
3609	36.09	106.78	2.03	2.03	17.10	126.84
3610	36.10	107.01	2.01	2.01	16.99	126.79
3611	36.11	107.25	2.00	2.00	16.87	126.74
3612	36.12	107.49	1.98	1.98	16.75	126.69
3613	36.13	107.72	1.97	1.97	16.64	126.64
3614	36.14	107.92	1.96	1.96	16.54	126.60
3615	36.15	108.08	1.94	1.94	16.47	126.57
3616	36.16	108.15	1.94	1.94	16.43	126.54
3617	36.17	108.21	1.94	1.94	16.39	126.53
3618	36.18	108.29	1.93	1.93	16.36	126.51
3619	36.19	108.36	1.93	1.93	16.32	126.49
3620	36.20	108.45	1.92	1.92	16.28	126.48
3621	36.21	108.53	1.91	1.91	16.24	126.46
3622	36.22	108.60	1.91	1.91	16.21	126.44
3623	36.23	108.66	1.91	1.91	16.18	126.43
3624	36.24	108.70	1.90	1.90	16.18	126.43
3625	36.25	108.70	1.91	1.91	16.22	126.46
3626	36.26	108.70	1.92	1.92	16.27	126.50
3627	36.27	108.70	1.94	1.94	16.34	126.55
3628	36.28	108.70	1.95	1.95	16.41	126.60
3629	36.29	108.70	1.97	1.97	16.47	126.65
3630	36.30	108.70	1.98	1.98	16.54	126.70
3631	36.31	108.70	1.99	1.99	16.60	126.74
3632	36.32	108.70	2.00	2.00	16.65	126.78
3633	36.33	108.68	2.01	2.01	16.73	126.83
3634	36.34	108.62	2.03	2.03	16.83	126.90
3635	36.35	108.55	2.05	2.05	16.95	126.97
3636	36.36	108.47	2.08	2.08	17.08	127.06
3637	36.37	108.39	2.11	2.11	17.22	127.15
3638	36.38	108.31	2.13	2.13	17.35	127.23
3639	36.39	108.23	2.15	2.15	17.48	127.31
3640	36.40	108.17	2.18	2.18	17.59	127.38
3641	36.41	108.11	2.19	2.19	17.69	127.44
3642	36.42	107.97	2.21	2.21	17.80	127.50
3643	36.43	107.78	2.23	2.23	17.93	127.56
3644	36.44	107.56	2.25	2.25	18.08	127.63
3645	36.45	107.32	2.28	2.28	18.24	127.70
3646	36.46	107.08	2.30	2.30	18.40	127.77
3647	36.47	106.84	2.33	2.33	18.56	127.85
3648	36.48	106.62	2.35	2.35	18.70	127.91

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3649	36.49	106.43	2.37	2.37	18.82	127.96
3650	36.50	106.29	2.38	2.38	18.92	128.00
3651	36.51	106.12	2.39	2.39	19.01	128.04
3652	36.52	105.92	2.41	2.41	19.11	128.07
3653	36.53	105.69	2.42	2.42	19.22	128.11
3654	36.54	105.45	2.43	2.43	19.33	128.14
3655	36.55	105.20	2.45	2.45	19.44	128.18
3656	36.56	104.97	2.46	2.46	19.55	128.21
3657	36.57	104.76	2.47	2.47	19.65	128.24
3658	36.58	104.59	2.48	2.48	19.73	128.27
3659	36.59	104.50	2.49	2.49	19.79	128.29
3660	36.60	104.44	2.50	2.50	19.83	128.31
3661	36.61	104.37	2.50	2.50	19.88	128.32
3662	36.62	104.29	2.51	2.51	19.93	128.34
3663	36.63	104.21	2.52	2.52	19.98	128.37
3664	36.64	104.13	2.53	2.53	20.04	128.39
3665	36.65	104.05	2.53	2.53	20.09	128.41
3666	36.66	103.98	2.54	2.54	20.13	128.42
3667	36.67	103.93	2.55	2.55	20.16	128.43
3668	36.68	103.93	2.55	2.55	20.18	128.44
3669	36.69	103.93	2.55	2.55	20.20	128.45
3670	36.70	103.93	2.55	2.55	20.21	128.46
3671	36.71	103.93	2.56	2.56	20.23	128.47
3672	36.72	103.93	2.56	2.56	20.25	128.48
3673	36.73	103.93	2.56	2.56	20.26	128.49
3674	36.74	103.93	2.57	2.57	20.28	128.50
3675	36.75	103.93	2.57	2.57	20.29	128.50
3676	36.76	103.91	2.57	2.57	20.31	128.51
3677	36.77	103.86	2.57	2.57	20.33	128.52
3678	36.78	103.79	2.58	2.58	20.37	128.53
3679	36.79	103.72	2.58	2.58	20.40	128.54
3680	36.80	103.63	2.59	2.59	20.44	128.55
3681	36.81	103.55	2.59	2.59	20.48	128.56
3682	36.82	103.48	2.60	2.60	20.52	128.57
3683	36.83	103.41	2.60	2.60	20.55	128.58
3684	36.84	103.35	2.60	2.60	20.59	128.59
3685	36.85	103.27	2.61	2.61	20.63	128.60
3686	36.86	103.15	2.61	2.61	20.68	128.61
3687	36.87	103.01	2.62	2.62	20.75	128.63
3688	36.88	102.85	2.63	2.63	20.82	128.65
3689	36.89	102.69	2.64	2.64	20.90	128.67
3690	36.90	102.53	2.65	2.65	20.97	128.69
3691	36.91	102.38	2.66	2.66	21.04	128.71
3692	36.92	102.25	2.66	2.66	21.10	128.73
3693	36.93	102.14	2.67	2.67	21.15	128.73
3694	36.94	101.95	2.67	2.67	21.20	128.73
3695	36.95	101.69	2.67	2.67	21.25	128.72
3696	36.96	101.39	2.67	2.67	21.31	128.71

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3697	36.97	101.07	2.66	2.66	21.38	128.70
3698	36.98	100.75	2.66	2.66	21.44	128.68
3699	36.99	100.43	2.66	2.66	21.51	128.67
3700	37.00	100.14	2.66	2.66	21.57	128.66
3701	37.01	99.89	2.65	2.65	21.62	128.65
3702	37.02	99.72	2.65	2.65	21.64	128.63
3703	37.03	99.61	2.65	2.65	21.65	128.61
3704	37.04	99.47	2.64	2.64	21.65	128.58
3705	37.05	99.32	2.63	2.63	21.64	128.55
3706	37.06	99.16	2.62	2.62	21.63	128.52
3707	37.07	99.00	2.61	2.61	21.63	128.49
3708	37.08	98.84	2.60	2.60	21.62	128.45
3709	37.09	98.70	2.59	2.59	21.62	128.43
3710	37.10	98.59	2.58	2.58	21.60	128.40
3711	37.11	98.58	2.57	2.57	21.57	128.37
3712	37.12	98.64	2.56	2.56	21.51	128.34
3713	37.13	98.71	2.54	2.54	21.43	128.30
3714	37.14	98.79	2.53	2.53	21.34	128.26
3715	37.15	98.87	2.51	2.51	21.25	128.21
3716	37.16	98.95	2.49	2.49	21.16	128.17
3717	37.17	99.03	2.48	2.48	21.07	128.12
3718	37.18	99.09	2.46	2.46	21.00	128.08
3719	37.19	99.14	2.45	2.45	20.95	128.06
3720	37.20	99.15	2.45	2.45	20.94	128.05
3721	37.21	99.15	2.45	2.45	20.94	128.05
3722	37.22	99.15	2.45	2.45	20.94	128.05
3723	37.23	99.15	2.45	2.45	20.95	128.05
3724	37.24	99.15	2.46	2.46	20.95	128.06
3725	37.25	99.15	2.46	2.46	20.96	128.06
3726	37.26	99.15	2.46	2.46	20.96	128.06
3727	37.27	99.15	2.46	2.46	20.96	128.06
3728	37.28	99.17	2.45	2.45	20.93	128.05
3729	37.29	99.28	2.44	2.44	20.87	128.02
3730	37.30	99.42	2.43	2.43	20.77	127.98
3731	37.31	99.57	2.41	2.41	20.66	127.93
3732	37.32	99.74	2.39	2.39	20.54	127.88
3733	37.33	99.90	2.37	2.37	20.43	127.83
3734	37.34	100.05	2.36	2.36	20.31	127.78
3735	37.35	100.19	2.34	2.34	20.21	127.73
3736	37.36	100.31	2.33	2.33	20.12	127.69
3737	37.37	100.37	2.31	2.31	20.03	127.64
3738	37.38	100.43	2.29	2.29	19.91	127.57
3739	37.39	100.50	2.26	2.26	19.77	127.49
3740	37.40	100.58	2.23	2.23	19.62	127.39
3741	37.41	100.66	2.20	2.20	19.45	127.29
3742	37.42	100.74	2.17	2.17	19.29	127.20
3743	37.43	100.82	2.14	2.14	19.14	127.10
3744	37.44	100.88	2.12	2.12	19.01	127.02

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3745	37.45	100.94	2.10	2.10	18.97	126.99
3746	37.46	100.84	2.12	2.12	19.02	127.02
3747	37.47	100.71	2.14	2.14	19.17	127.10
3748	37.48	100.56	2.17	2.17	19.35	127.19
3749	37.49	100.40	2.20	2.20	19.54	127.30
3750	37.50	100.24	2.24	2.24	19.73	127.40
3751	37.51	100.08	2.27	2.27	19.91	127.49
3752	37.52	99.94	2.29	2.29	20.08	127.58
3753	37.53	99.81	2.32	2.32	20.22	127.65
3754	37.54	99.72	2.34	2.34	20.33	127.70
3755	37.55	99.60	2.35	2.35	20.43	127.74
3756	37.56	99.47	2.36	2.36	20.53	127.79
3757	37.57	99.31	2.38	2.38	20.65	127.84
3758	37.58	99.15	2.40	2.40	20.77	127.89
3759	37.59	98.99	2.42	2.42	20.89	127.94
3760	37.60	98.84	2.43	2.43	21.01	127.98
3761	37.61	98.70	2.45	2.45	21.11	128.02
3762	37.62	98.58	2.46	2.46	21.20	128.06
3763	37.63	98.49	2.47	2.47	21.28	128.09
3764	37.64	98.37	2.49	2.49	21.38	128.13
3765	37.65	98.22	2.50	2.50	21.48	128.17
3766	37.66	98.06	2.52	2.52	21.60	128.22
3767	37.67	97.90	2.54	2.54	21.72	128.26
3768	37.68	97.74	2.55	2.55	21.84	128.31
3769	37.69	97.59	2.57	2.57	21.95	128.35
3770	37.70	97.46	2.58	2.58	22.04	128.39
3771	37.71	97.36	2.60	2.60	22.15	128.43
3772	37.72	97.25	2.62	2.62	22.29	128.49
3773	37.73	97.12	2.66	2.66	22.47	128.58
3774	37.74	96.97	2.69	2.69	22.67	128.68
3775	37.75	96.81	2.73	2.73	22.89	128.79
3776	37.76	96.65	2.78	2.78	23.12	128.89
3777	37.77	96.49	2.82	2.82	23.33	128.99
3778	37.78	96.35	2.85	2.85	23.52	129.08
3779	37.79	96.23	2.88	2.88	23.69	129.15
3780	37.80	96.10	2.91	2.91	23.85	129.22
3781	37.81	95.87	2.93	2.93	24.02	129.28
3782	37.82	95.60	2.97	2.97	24.23	129.35
3783	37.83	95.29	3.00	3.00	24.46	129.43
3784	37.84	94.97	3.04	3.04	24.70	129.51
3785	37.85	94.64	3.08	3.08	24.94	129.59
3786	37.86	94.34	3.11	3.11	25.17	129.66
3787	37.87	94.06	3.14	3.14	25.37	129.73
3788	37.88	93.83	3.17	3.17	25.55	129.78
3789	37.89	93.61	3.19	3.19	25.74	129.84
3790	37.90	93.30	3.23	3.23	25.96	129.91
3791	37.91	92.94	3.27	3.27	26.22	129.99
3792	37.92	92.55	3.31	3.31	26.51	130.07

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3793	37.93	92.14	3.35	3.35	26.80	130.16
3794	37.94	91.74	3.40	3.40	27.09	130.24
3795	37.95	91.37	3.44	3.44	27.35	130.31
3796	37.96	91.04	3.47	3.47	27.58	130.37
3797	37.97	90.78	3.50	3.50	27.78	130.42
3798	37.98	90.47	3.51	3.51	27.97	130.46
3799	37.99	90.08	3.54	3.54	28.18	130.50
3800	38.00	89.63	3.56	3.56	28.41	130.54
3801	38.01	89.15	3.59	3.59	28.67	130.58
3802	38.02	88.66	3.62	3.62	28.93	130.62
3803	38.03	88.19	3.64	3.64	29.18	130.66
3804	38.04	87.76	3.67	3.67	29.41	130.69
3805	38.05	87.40	3.69	3.69	29.59	130.72
3806	38.06	87.14	3.70	3.70	29.74	130.74
3807	38.07	86.91	3.71	3.71	29.86	130.75
3808	38.08	86.63	3.71	3.71	29.98	130.75
3809	38.09	86.33	3.72	3.72	30.11	130.76
3810	38.10	86.00	3.73	3.73	30.25	130.77
3811	38.11	85.68	3.74	3.74	30.39	130.77
3812	38.12	85.37	3.74	3.74	30.53	130.78
3813	38.13	85.10	3.75	3.75	30.65	130.79
3814	38.14	84.87	3.76	3.76	30.70	130.80
3815	38.15	85.18	3.77	3.77	30.65	130.82
3816	38.16	85.86	3.78	3.78	30.51	130.87
3817	38.17	86.65	3.80	3.80	30.32	130.92
3818	38.18	87.52	3.81	3.81	30.11	130.97
3819	38.19	88.42	3.83	3.83	29.89	131.03
3820	38.20	89.30	3.85	3.85	29.68	131.09
3821	38.21	90.11	3.86	3.86	29.49	131.14
3822	38.22	90.83	3.88	3.88	29.32	131.18
3823	38.23	91.41	3.89	3.89	29.10	131.23
3824	38.24	92.82	3.90	3.90	28.78	131.29
3825	38.25	94.59	3.92	3.92	28.33	131.36
3826	38.26	96.61	3.93	3.93	27.82	131.44
3827	38.27	98.78	3.94	3.94	27.28	131.51
3828	38.28	100.97	3.95	3.95	26.75	131.59
3829	38.29	103.09	3.96	3.96	26.24	131.65
3830	38.30	105.03	3.96	3.96	25.78	131.70
3831	38.31	106.67	3.96	3.96	25.39	131.74
3832	38.32	108.01	3.96	3.96	25.03	131.77
3833	38.33	109.67	3.96	3.96	24.65	131.81
3834	38.34	111.67	3.96	3.96	24.20	131.85
3835	38.35	113.91	3.95	3.95	23.70	131.88
3836	38.36	116.26	3.94	3.94	23.18	131.91
3837	38.37	118.60	3.93	3.93	22.67	131.93
3838	38.38	120.82	3.91	3.91	22.19	131.95
3839	38.39	122.81	3.90	3.90	21.77	131.95
3840	38.40	124.44	3.88	3.88	21.46	131.97

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3841	38.41	125.50	3.90	3.90	21.26	132.02
3842	38.42	126.67	3.93	3.93	21.14	132.10
3843	38.43	128.04	3.97	3.97	21.03	132.20
3844	38.44	129.54	4.02	4.02	20.91	132.31
3845	38.45	131.09	4.06	4.06	20.78	132.42
3846	38.46	132.61	4.11	4.11	20.66	132.53
3847	38.47	134.02	4.15	4.15	20.55	132.63
3848	38.48	135.25	4.19	4.19	20.46	132.72
3849	38.49	136.18	4.22	4.22	20.46	132.81
3850	38.50	136.18	4.28	4.28	20.57	132.90
3851	38.51	136.18	4.35	4.35	20.77	133.03
3852	38.52	136.18	4.44	4.44	21.00	133.16
3853	38.53	136.18	4.53	4.53	21.24	133.31
3854	38.54	136.18	4.62	4.62	21.49	133.45
3855	38.55	136.18	4.71	4.71	21.72	133.59
3856	38.56	136.18	4.79	4.79	21.93	133.71
3857	38.57	136.18	4.85	4.85	22.11	133.80
3858	38.58	135.96	4.90	4.90	22.31	133.88
3859	38.59	135.27	4.95	4.95	22.54	133.94
3860	38.60	134.43	5.00	5.00	22.82	134.01
3861	38.61	133.51	5.06	5.06	23.14	134.07
3862	38.62	132.54	5.12	5.12	23.46	134.14
3863	38.63	131.57	5.18	5.18	23.79	134.21
3864	38.64	130.65	5.24	5.24	24.10	134.27
3865	38.65	129.83	5.28	5.28	24.37	134.32
3866	38.66	129.16	5.32	5.32	24.62	134.36
3867	38.67	128.47	5.35	5.35	24.86	134.40
3868	38.68	127.53	5.40	5.40	25.15	134.43
3869	38.69	126.45	5.44	5.44	25.48	134.48
3870	38.70	125.26	5.49	5.49	25.84	134.52
3871	38.71	124.04	5.54	5.54	26.21	134.56
3872	38.72	122.84	5.59	5.59	26.58	134.59
3873	38.73	121.73	5.63	5.63	26.92	134.63
3874	38.74	120.77	5.66	5.66	27.21	134.65
3875	38.75	120.02	5.69	5.69	27.43	134.66
3876	38.76	119.49	5.69	5.69	27.61	134.66
3877	38.77	118.83	5.70	5.70	27.77	134.66
3878	38.78	118.08	5.70	5.70	27.95	134.65
3879	38.79	117.28	5.71	5.71	28.15	134.64
3880	38.80	116.46	5.71	5.71	28.35	134.63
3881	38.81	115.68	5.72	5.72	28.54	134.62
3882	38.82	114.97	5.72	5.72	28.72	134.61
3883	38.83	114.36	5.72	5.72	28.84	134.60
3884	38.84	114.18	5.72	5.72	28.87	134.59
3885	38.85	114.47	5.70	5.70	28.80	134.57
3886	38.86	114.81	5.68	5.68	28.67	134.55
3887	38.87	115.20	5.66	5.66	28.52	134.53
3888	38.88	115.61	5.64	5.64	28.37	134.51

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3889	38.89	116.01	5.61	5.61	28.22	134.49
3890	38.90	116.39	5.59	5.59	28.07	134.47
3891	38.91	116.73	5.57	5.57	27.95	134.45
3892	38.92	117.01	5.55	5.55	27.80	134.43
3893	38.93	117.67	5.53	5.53	27.59	134.41
3894	38.94	118.66	5.49	5.49	27.29	134.38
3895	38.95	119.83	5.45	5.45	26.93	134.35
3896	38.96	121.09	5.40	5.40	26.55	134.31
3897	38.97	122.40	5.35	5.35	26.14	134.27
3898	38.98	123.67	5.30	5.30	25.75	134.23
3899	38.99	124.85	5.25	5.25	25.39	134.18
3900	39.00	125.88	5.21	5.21	25.07	134.14
3901	39.01	126.71	5.17	5.17	24.77	134.10
3902	39.02	127.77	5.13	5.13	24.46	134.06
3903	39.03	129.10	5.08	5.08	24.08	134.02
3904	39.04	130.60	5.02	5.02	23.65	133.96
3905	39.05	132.21	4.95	4.95	23.19	133.89
3906	39.06	133.84	4.88	4.88	22.72	133.82
3907	39.07	135.40	4.81	4.81	22.27	133.74
3908	39.08	136.82	4.74	4.74	21.86	133.66
3909	39.09	138.02	4.68	4.68	21.52	133.60
3910	39.10	138.92	4.65	4.65	21.26	133.56
3911	39.11	139.91	4.63	4.63	21.02	133.54
3912	39.12	141.09	4.61	4.61	20.77	133.52
3913	39.13	142.41	4.58	4.58	20.50	133.50
3914	39.14	143.79	4.55	4.55	20.21	133.47
3915	39.15	145.16	4.51	4.51	19.92	133.44
3916	39.16	146.46	4.48	4.48	19.65	133.41
3917	39.17	147.61	4.45	4.45	19.41	133.38
3918	39.18	148.55	4.43	4.43	19.24	133.37
3919	39.19	149.26	4.44	4.44	19.12	133.39
3920	39.20	150.14	4.46	4.46	19.05	133.43
3921	39.21	151.16	4.48	4.48	18.97	133.49
3922	39.22	152.27	4.51	4.51	18.89	133.55
3923	39.23	153.41	4.54	4.54	18.80	133.61
3924	39.24	154.53	4.56	4.56	18.72	133.67
3925	39.25	155.56	4.59	4.59	18.64	133.72
3926	39.26	156.45	4.61	4.61	18.58	133.77
3927	39.27	157.13	4.63	4.63	18.54	133.82
3928	39.28	157.67	4.65	4.65	18.52	133.87
3929	39.29	158.34	4.68	4.68	18.51	133.93
3930	39.30	159.09	4.72	4.72	18.51	134.00
3931	39.31	159.90	4.76	4.76	18.50	134.07
3932	39.32	160.71	4.80	4.80	18.49	134.14
3933	39.33	161.49	4.84	4.84	18.49	134.21
3934	39.34	162.20	4.88	4.88	18.48	134.28
3935	39.35	162.79	4.91	4.91	18.48	134.33
3936	39.36	163.21	4.93	4.93	18.46	134.36

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3937	39.37	163.62	4.94	4.94	18.44	134.39
3938	39.38	164.11	4.95	4.95	18.40	134.41
3939	39.39	164.65	4.96	4.96	18.37	134.44
3940	39.40	165.22	4.97	4.97	18.33	134.47
3941	39.41	165.78	4.99	4.99	18.29	134.49
3942	39.42	166.32	5.00	5.00	18.26	134.52
3943	39.43	166.79	5.01	5.01	18.23	134.54
3944	39.44	167.17	5.02	5.02	18.21	134.57
3945	39.45	167.44	5.04	5.04	18.20	134.59
3946	39.46	167.75	5.06	5.06	18.21	134.63
3947	39.47	168.12	5.08	5.08	18.22	134.66
3948	39.48	168.51	5.11	5.11	18.23	134.71
3949	39.49	168.92	5.13	5.13	18.24	134.75
3950	39.50	169.32	5.16	5.16	18.26	134.79
3951	39.51	169.69	5.18	5.18	18.27	134.83
3952	39.52	170.00	5.20	5.20	18.28	134.86
3953	39.53	170.23	5.22	5.22	18.29	134.89
3954	39.54	170.28	5.24	5.24	18.33	134.92
3955	39.55	170.35	5.26	5.26	18.37	134.95
3956	39.56	170.42	5.29	5.29	18.42	134.99
3957	39.57	170.51	5.31	5.31	18.47	135.03
3958	39.58	170.59	5.34	5.34	18.52	135.07
3959	39.59	170.66	5.37	5.37	18.57	135.10
3960	39.60	170.74	5.39	5.39	18.61	135.14
3961	39.61	170.79	5.41	5.41	18.64	135.16
3962	39.62	170.87	5.41	5.41	18.62	135.15
3963	39.63	170.98	5.38	5.38	18.56	135.12
3964	39.64	171.12	5.35	5.35	18.47	135.08
3965	39.65	171.28	5.31	5.31	18.37	135.03
3966	39.66	171.44	5.27	5.27	18.27	134.98
3967	39.67	171.60	5.23	5.23	18.17	134.93
3968	39.68	171.75	5.19	5.19	18.07	134.88
3969	39.69	171.89	5.16	5.16	17.98	134.83
3970	39.70	172.00	5.13	5.13	17.91	134.79
3971	39.71	172.10	5.11	5.11	17.84	134.76
3972	39.72	172.22	5.08	5.08	17.76	134.72
3973	39.73	172.37	5.04	5.04	17.68	134.67
3974	39.74	172.53	5.01	5.01	17.58	134.62
3975	39.75	172.69	4.97	4.97	17.48	134.57
3976	39.76	172.85	4.93	4.93	17.38	134.52
3977	39.77	173.00	4.90	4.90	17.29	134.47
3978	39.78	173.12	4.87	4.87	17.22	134.43
3979	39.79	173.17	4.85	4.85	17.19	134.41
3980	39.80	172.88	4.85	4.85	17.20	134.39
3981	39.81	172.52	4.85	4.85	17.24	134.39
3982	39.82	172.12	4.85	4.85	17.28	134.38
3983	39.83	171.69	4.85	4.85	17.33	134.37
3984	39.84	171.26	4.85	4.85	17.38	134.36

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
3985	39.85	170.84	4.84	4.84	17.43	134.36
3986	39.86	170.46	4.84	4.84	17.47	134.35
3987	39.87	170.15	4.84	4.84	17.52	134.34
3988	39.88	169.73	4.85	4.85	17.60	134.35
3989	39.89	169.02	4.86	4.86	17.71	134.36
3990	39.90	168.18	4.88	4.88	17.85	134.37
3991	39.91	167.24	4.90	4.90	18.00	134.38
3992	39.92	166.27	4.92	4.92	18.17	134.40
3993	39.93	165.30	4.94	4.94	18.33	134.41
3994	39.94	164.39	4.95	4.95	18.48	134.42
3995	39.95	163.59	4.97	4.97	18.62	134.43
3996	39.96	162.94	4.98	4.98	18.73	134.45
3997	39.97	162.70	5.00	5.00	18.84	134.47
3998	39.98	162.47	5.03	5.03	18.94	134.52
3999	39.99	162.20	5.07	5.07	19.07	134.57
4000	40.00	161.91	5.11	5.11	19.20	134.62
4001	40.01	161.61	5.16	5.16	19.34	134.68
4002	40.02	161.32	5.20	5.20	19.47	134.73
4003	40.03	161.05	5.23	5.23	19.59	134.78
4004	40.04	160.82	5.27	5.27	19.68	134.82
4005	40.05	160.78	5.29	5.29	19.70	134.84
4006	40.06	161.55	5.29	5.29	19.65	134.86
4007	40.07	162.49	5.29	5.29	19.53	134.88
4008	40.08	163.55	5.29	5.29	19.39	134.89
4009	40.09	164.68	5.29	5.29	19.25	134.91
4010	40.10	165.82	5.29	5.29	19.11	134.93
4011	40.11	166.91	5.29	5.29	18.97	134.94
4012	40.12	167.89	5.29	5.29	18.85	134.95
4013	40.13	168.71	5.29	5.29	18.74	134.96
4014	40.14	169.31	5.28	5.28	18.64	134.96
4015	40.15	169.96	5.26	5.26	18.52	134.94
4016	40.16	170.74	5.24	5.24	18.38	134.92
4017	40.17	171.60	5.21	5.21	18.22	134.90
4018	40.18	172.49	5.18	5.18	18.05	134.87
4019	40.19	173.37	5.15	5.15	17.89	134.85
4020	40.20	174.21	5.13	5.13	17.74	134.82
4021	40.21	174.94	5.10	5.10	17.61	134.80
4022	40.22	175.53	5.08	5.08	17.51	134.78
4023	40.23	175.60	5.07	5.07	17.46	134.76
4024	40.24	175.60	5.06	5.06	17.43	134.74
4025	40.25	175.60	5.04	5.04	17.40	134.72
4026	40.26	175.60	5.03	5.03	17.36	134.69
4027	40.27	175.60	5.01	5.01	17.33	134.67
4028	40.28	175.60	5.00	5.00	17.30	134.65
4029	40.29	175.60	4.98	4.98	17.27	134.63
4030	40.30	175.60	4.97	4.97	17.24	134.61
4031	40.31	175.58	4.96	4.96	17.22	134.59
4032	40.32	175.47	4.94	4.94	17.20	134.57

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4033	40.33	175.33	4.92	4.92	17.18	134.54
4034	40.34	175.18	4.90	4.90	17.15	134.51
4035	40.35	175.02	4.88	4.88	17.12	134.47
4036	40.36	174.86	4.86	4.86	17.10	134.44
4037	40.37	174.70	4.84	4.84	17.07	134.41
4038	40.38	174.56	4.82	4.82	17.05	134.38
4039	40.39	174.45	4.81	4.81	17.03	134.35
4040	40.40	174.30	4.79	4.79	17.02	134.33
4041	40.41	174.06	4.78	4.78	17.00	134.30
4042	40.42	173.77	4.75	4.75	16.99	134.26
4043	40.43	173.46	4.73	4.73	16.97	134.22
4044	40.44	173.14	4.70	4.70	16.95	134.17
4045	40.45	172.82	4.68	4.68	16.93	134.13
4046	40.46	172.51	4.66	4.66	16.91	134.09
4047	40.47	172.25	4.63	4.63	16.90	134.05
4048	40.48	172.03	4.62	4.62	16.89	134.03
4049	40.49	171.79	4.61	4.61	16.89	134.00
4050	40.50	171.47	4.59	4.59	16.90	133.98
4051	40.51	171.10	4.58	4.58	16.91	133.95
4052	40.52	170.70	4.56	4.56	16.92	133.92
4053	40.53	170.29	4.55	4.55	16.93	133.89
4054	40.54	169.90	4.53	4.53	16.94	133.86
4055	40.55	169.53	4.52	4.52	16.95	133.83
4056	40.56	169.22	4.50	4.50	16.96	133.80
4057	40.57	168.92	4.49	4.49	16.98	133.78
4058	40.58	168.37	4.48	4.48	17.00	133.74
4059	40.59	167.69	4.46	4.46	17.04	133.71
4060	40.60	166.93	4.44	4.44	17.09	133.66
4061	40.61	166.12	4.42	4.42	17.13	133.62
4062	40.62	165.31	4.40	4.40	17.18	133.57
4063	40.63	164.54	4.38	4.38	17.22	133.52
4064	40.64	163.84	4.36	4.36	17.26	133.48
4065	40.65	163.26	4.34	4.34	17.30	133.45
4066	40.66	162.69	4.33	4.33	17.34	133.41
4067	40.67	161.91	4.31	4.31	17.39	133.36
4068	40.68	160.99	4.28	4.28	17.44	133.31
4069	40.69	159.97	4.26	4.26	17.50	133.25
4070	40.70	158.92	4.23	4.23	17.57	133.18
4071	40.71	157.87	4.20	4.20	17.63	133.12
4072	40.72	156.89	4.17	4.17	17.69	133.06
4073	40.73	156.03	4.15	4.15	17.74	133.01
4074	40.74	155.34	4.13	4.13	17.80	132.97
4075	40.75	154.59	4.13	4.13	17.88	132.94
4076	40.76	153.63	4.12	4.12	17.99	132.91
4077	40.77	152.52	4.11	4.11	18.12	132.87
4078	40.78	151.32	4.10	4.10	18.25	132.84
4079	40.79	150.10	4.09	4.09	18.39	132.80
4080	40.80	148.91	4.08	4.08	18.53	132.76

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4081	40.81	147.82	4.07	4.07	18.65	132.72
4082	40.82	146.89	4.06	4.06	18.76	132.69
4083	40.83	146.12	4.05	4.05	18.86	132.65
4084	40.84	145.12	4.03	4.03	18.96	132.60
4085	40.85	143.90	4.01	4.01	19.08	132.54
4086	40.86	142.52	3.98	3.98	19.22	132.47
4087	40.87	141.07	3.95	3.95	19.36	132.40
4088	40.88	139.61	3.93	3.93	19.51	132.33
4089	40.89	138.22	3.90	3.90	19.65	132.25
4090	40.90	136.96	3.87	3.87	19.77	132.19
4091	40.91	135.92	3.85	3.85	19.88	132.12
4092	40.92	135.00	3.83	3.83	19.97	132.05
4093	40.93	133.80	3.79	3.79	20.05	131.95
4094	40.94	132.37	3.74	3.74	20.14	131.83
4095	40.95	130.80	3.69	3.69	20.24	131.70
4096	40.96	129.17	3.63	3.63	20.34	131.57
4097	40.97	127.57	3.58	3.58	20.45	131.43
4098	40.98	126.07	3.53	3.53	20.56	131.30
4099	40.99	124.75	3.48	3.48	20.65	131.19
4100	41.00	123.69	3.45	3.45	20.73	131.09
4101	41.01	122.72	3.42	3.42	20.82	131.00
4102	41.02	121.50	3.39	3.39	20.93	130.90
4103	41.03	120.09	3.34	3.34	21.05	130.78
4104	41.04	118.57	3.30	3.30	21.19	130.66
4105	41.05	117.02	3.26	3.26	21.33	130.53
4106	41.06	115.52	3.21	3.21	21.47	130.40
4107	41.07	114.15	3.17	3.17	21.60	130.28
4108	41.08	112.97	3.14	3.14	21.72	130.18
4109	41.09	112.02	3.11	3.11	21.84	130.08
4110	41.10	110.83	3.08	3.08	21.98	129.99
4111	41.11	109.38	3.05	3.05	22.15	129.87
4112	41.12	107.75	3.01	3.01	22.34	129.74
4113	41.13	106.03	2.96	2.96	22.55	129.60
4114	41.14	104.31	2.92	2.92	22.77	129.45
4115	41.15	102.67	2.88	2.88	22.98	129.31
4116	41.16	101.20	2.84	2.84	23.17	129.18
4117	41.17	99.98	2.81	2.81	23.33	129.07
4118	41.18	98.99	2.78	2.78	23.46	128.95
4119	41.19	97.78	2.74	2.74	23.59	128.81
4120	41.20	96.35	2.69	2.69	23.73	128.64
4121	41.21	94.78	2.63	2.63	23.89	128.46
4122	41.22	93.15	2.58	2.58	24.06	128.26
4123	41.23	91.55	2.52	2.52	24.23	128.07
4124	41.24	90.05	2.47	2.47	24.40	127.88
4125	41.25	88.73	2.43	2.43	24.55	127.72
4126	41.26	87.69	2.39	2.39	24.68	127.60
4127	41.27	87.07	2.38	2.38	24.82	127.52
4128	41.28	86.31	2.37	2.37	24.98	127.46

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4129	41.29	85.43	2.36	2.36	25.16	127.39
4130	41.30	84.50	2.34	2.34	25.36	127.31
4131	41.31	83.54	2.32	2.32	25.57	127.23
4132	41.32	82.61	2.31	2.31	25.77	127.16
4133	41.33	81.76	2.29	2.29	25.95	127.08
4134	41.34	81.04	2.28	2.28	26.12	127.02
4135	41.35	80.49	2.27	2.27	26.29	126.99
4136	41.36	79.93	2.27	2.27	26.49	126.96
4137	41.37	79.25	2.27	2.27	26.72	126.95
4138	41.38	78.48	2.28	2.28	26.99	126.93
4139	41.39	77.67	2.28	2.28	27.28	126.91
4140	41.40	76.86	2.28	2.28	27.57	126.89
4141	41.41	76.09	2.28	2.28	27.84	126.86
4142	41.42	75.40	2.28	2.28	28.09	126.84
4143	41.43	74.83	2.28	2.28	28.31	126.82
4144	41.44	74.37	2.28	2.28	28.52	126.81
4145	41.45	73.80	2.28	2.28	28.75	126.80
4146	41.46	73.14	2.28	2.28	29.02	126.78
4147	41.47	72.41	2.29	2.29	29.32	126.77
4148	41.48	71.66	2.29	2.29	29.63	126.75
4149	41.49	70.92	2.29	2.29	29.93	126.73
4150	41.50	70.23	2.29	2.29	30.22	126.71
4151	41.51	69.62	2.29	2.29	30.48	126.69
4152	41.52	69.14	2.29	2.29	30.73	126.68
4153	41.53	68.65	2.30	2.30	31.02	126.70
4154	41.54	68.03	2.32	2.32	31.38	126.72
4155	41.55	67.33	2.34	2.34	31.79	126.75
4156	41.56	66.57	2.35	2.35	32.24	126.77
4157	41.57	65.79	2.37	2.37	32.69	126.80
4158	41.58	65.05	2.39	2.39	33.14	126.82
4159	41.59	64.36	2.40	2.40	33.54	126.83
4160	41.60	63.78	2.41	2.41	33.89	126.84
4161	41.61	63.30	2.42	2.42	34.22	126.84
4162	41.62	62.69	2.42	2.42	34.56	126.83
4163	41.63	61.95	2.42	2.42	34.97	126.82
4164	41.64	61.13	2.43	2.43	35.42	126.80
4165	41.65	60.26	2.43	2.43	35.91	126.77
4166	41.66	59.39	2.44	2.44	36.39	126.75
4167	41.67	58.56	2.44	2.44	36.86	126.72
4168	41.68	57.82	2.44	2.44	37.29	126.69
4169	41.69	57.21	2.44	2.44	37.65	126.66
4170	41.70	56.73	2.44	2.44	38.00	126.64
4171	41.71	56.15	2.44	2.44	38.37	126.63
4172	41.72	55.46	2.45	2.45	38.81	126.61
4173	41.73	54.72	2.45	2.45	39.29	126.58
4174	41.74	53.94	2.45	2.45	39.79	126.55
4175	41.75	53.18	2.45	2.45	40.29	126.52
4176	41.76	52.47	2.45	2.45	40.76	126.49

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4177	41.77	51.85	2.45	2.45	41.18	126.46
4178	41.78	51.36	2.45	2.45	41.55	126.44
4179	41.79	50.95	2.45	2.45	41.93	126.43
4180	41.80	50.43	2.46	2.46	42.36	126.43
4181	41.81	49.83	2.47	2.47	42.85	126.43
4182	41.82	49.19	2.48	2.48	43.39	126.42
4183	41.83	48.54	2.49	2.49	43.93	126.41
4184	41.84	47.91	2.49	2.49	44.47	126.40
4185	41.85	47.33	2.50	2.50	44.96	126.38
4186	41.86	46.84	2.50	2.50	45.37	126.37
4187	41.87	46.52	2.51	2.51	45.72	126.38
4188	41.88	46.30	2.52	2.52	46.04	126.40
4189	41.89	46.02	2.54	2.54	46.40	126.44
4190	41.90	45.71	2.56	2.56	46.79	126.47
4191	41.91	45.39	2.58	2.58	47.21	126.51
4192	41.92	45.06	2.60	2.60	47.62	126.54
4193	41.93	44.76	2.61	2.61	48.02	126.57
4194	41.94	44.48	2.63	2.63	48.37	126.60
4195	41.95	44.26	2.64	2.64	48.61	126.62
4196	41.96	44.23	2.65	2.65	48.74	126.65
4197	41.97	44.29	2.66	2.66	48.77	126.67
4198	41.98	44.37	2.67	2.67	48.79	126.71
4199	41.99	44.44	2.68	2.68	48.80	126.74
4200	42.00	44.53	2.69	2.69	48.82	126.78
4201	42.01	44.61	2.70	2.70	48.83	126.81
4202	42.02	44.68	2.72	2.72	48.85	126.85
4203	42.03	44.75	2.72	2.72	48.86	126.88
4204	42.04	44.81	2.73	2.73	48.74	126.91
4205	42.05	45.28	2.74	2.74	48.46	126.94
4206	42.06	45.87	2.74	2.74	47.98	126.98
4207	42.07	46.54	2.74	2.74	47.44	127.02
4208	42.08	47.26	2.75	2.75	46.87	127.07
4209	42.09	47.99	2.75	2.75	46.29	127.11
4210	42.10	48.70	2.75	2.75	45.74	127.14
4211	42.11	49.35	2.75	2.75	45.24	127.17
4212	42.12	49.89	2.74	2.74	44.79	127.19
4213	42.13	50.41	2.74	2.74	44.30	127.21
4214	42.14	51.21	2.73	2.73	43.69	127.23
4215	42.15	52.18	2.72	2.72	42.93	127.24
4216	42.16	53.26	2.70	2.70	42.09	127.24
4217	42.17	54.40	2.68	2.68	41.22	127.24
4218	42.18	55.53	2.66	2.66	40.36	127.23
4219	42.19	56.60	2.63	2.63	39.54	127.20
4220	42.20	57.56	2.61	2.61	38.82	127.18
4221	42.21	58.34	2.59	2.59	38.23	127.15
4222	42.22	58.95	2.57	2.57	37.69	127.12
4223	42.23	59.70	2.55	2.55	37.14	127.09
4224	42.24	60.56	2.52	2.52	36.50	127.05

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4225	42.25	61.51	2.49	2.49	35.81	126.99
4226	42.26	62.49	2.46	2.46	35.10	126.93
4227	42.27	63.45	2.42	2.42	34.40	126.86
4228	42.28	64.34	2.38	2.38	33.75	126.79
4229	42.29	65.11	2.35	2.35	33.19	126.72
4230	42.30	65.71	2.33	2.33	32.78	126.67
4231	42.31	66.03	2.32	2.32	32.47	126.63
4232	42.32	66.42	2.30	2.30	32.22	126.61
4233	42.33	66.87	2.29	2.29	31.93	126.58
4234	42.34	67.35	2.27	2.27	31.61	126.54
4235	42.35	67.84	2.25	2.25	31.29	126.50
4236	42.36	68.31	2.24	2.24	30.99	126.46
4237	42.37	68.74	2.22	2.22	30.71	126.43
4238	42.38	69.11	2.21	2.21	30.51	126.39
4239	42.39	69.16	2.20	2.20	30.44	126.36
4240	42.40	68.79	2.19	2.19	30.51	126.33
4241	42.41	68.35	2.18	2.18	30.65	126.29
4242	42.42	67.85	2.18	2.18	30.82	126.24
4243	42.43	67.33	2.17	2.17	30.99	126.20
4244	42.44	66.81	2.16	2.16	31.16	126.15
4245	42.45	66.31	2.15	2.15	31.33	126.10
4246	42.46	65.87	2.14	2.14	31.47	126.06
4247	42.47	65.51	2.13	2.13	31.66	126.03
4248	42.48	65.00	2.14	2.14	31.93	126.02
4249	42.49	64.25	2.15	2.15	32.32	126.02
4250	42.50	63.38	2.16	2.16	32.80	126.02
4251	42.51	62.43	2.17	2.17	33.33	126.01
4252	42.52	61.46	2.18	2.18	33.87	126.00
4253	42.53	60.50	2.18	2.18	34.41	125.99
4254	42.54	59.61	2.19	2.19	34.92	125.97
4255	42.55	58.84	2.19	2.19	35.37	125.95
4256	42.56	58.23	2.19	2.19	35.77	125.94
4257	42.57	57.56	2.20	2.20	36.19	125.92
4258	42.58	56.73	2.20	2.20	36.69	125.89
4259	42.59	55.79	2.20	2.20	37.26	125.86
4260	42.60	54.78	2.20	2.20	37.88	125.82
4261	42.61	53.76	2.20	2.20	38.51	125.77
4262	42.62	52.78	2.20	2.20	39.13	125.72
4263	42.63	51.88	2.20	2.20	39.70	125.67
4264	42.64	51.13	2.19	2.19	40.17	125.61
4265	42.65	50.55	2.19	2.19	40.55	125.55
4266	42.66	49.92	2.16	2.16	40.88	125.45
4267	42.67	49.15	2.14	2.14	41.24	125.33
4268	42.68	48.30	2.11	2.11	41.65	125.19
4269	42.69	47.41	2.08	2.08	42.09	125.05
4270	42.70	46.52	2.05	2.05	42.53	124.90
4271	42.71	45.68	2.02	2.02	42.96	124.75
4272	42.72	44.93	2.00	2.00	43.36	124.62

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4273	42.73	44.32	1.97	1.97	43.60	124.51
4274	42.74	44.16	1.96	1.96	43.67	124.42
4275	42.75	44.10	1.94	1.94	43.57	124.34
4276	42.76	44.03	1.91	1.91	43.42	124.24
4277	42.77	43.95	1.89	1.89	43.26	124.14
4278	42.78	43.86	1.86	1.86	43.09	124.03
4279	42.79	43.79	1.83	1.83	42.92	123.92
4280	42.80	43.71	1.81	1.81	42.76	123.82
4281	42.81	43.65	1.79	1.79	42.61	123.74
4282	42.82	43.66	1.77	1.77	42.34	123.71
4283	42.83	44.35	1.78	1.78	41.89	123.73
4284	42.84	45.21	1.78	1.78	41.26	123.80
4285	42.85	46.19	1.79	1.79	40.54	123.87
4286	42.86	47.24	1.79	1.79	39.80	123.94
4287	42.87	48.29	1.79	1.79	39.05	124.00
4288	42.88	49.31	1.79	1.79	38.35	124.05
4289	42.89	50.23	1.79	1.79	37.72	124.09
4290	42.90	51.01	1.79	1.79	37.20	124.13
4291	42.91	51.66	1.79	1.79	36.75	124.18
4292	42.92	52.47	1.81	1.81	36.31	124.26
4293	42.93	53.45	1.82	1.82	35.82	124.35
4294	42.94	54.53	1.83	1.83	35.29	124.46
4295	42.95	55.67	1.85	1.85	34.74	124.56
4296	42.96	56.80	1.86	1.86	34.21	124.65
4297	42.97	57.87	1.87	1.87	33.71	124.74
4298	42.98	58.81	1.88	1.88	33.28	124.81
4299	42.99	59.58	1.88	1.88	32.99	124.87
4300	43.00	59.88	1.89	1.89	32.84	124.93
4301	43.01	60.13	1.91	1.91	32.80	124.99
4302	43.02	60.43	1.92	1.92	32.77	125.06
4303	43.03	60.74	1.94	1.94	32.74	125.14
4304	43.04	61.07	1.96	1.96	32.71	125.22
4305	43.05	61.39	1.98	1.98	32.69	125.30
4306	43.06	61.68	1.99	1.99	32.66	125.37
4307	43.07	61.94	2.01	2.01	32.65	125.43
4308	43.08	62.11	2.02	2.02	32.70	125.49
4309	43.09	62.06	2.04	2.04	32.84	125.57
4310	43.10	61.99	2.07	2.07	33.06	125.66
4311	43.11	61.92	2.10	2.10	33.31	125.76
4312	43.12	61.83	2.13	2.13	33.58	125.87
4313	43.13	61.75	2.16	2.16	33.84	125.97
4314	43.14	61.68	2.19	2.19	34.09	126.07
4315	43.15	61.60	2.22	2.22	34.32	126.16
4316	43.16	61.54	2.25	2.25	34.52	126.24
4317	43.17	61.50	2.27	2.27	34.70	126.31
4318	43.18	61.44	2.29	2.29	34.90	126.38
4319	43.19	61.37	2.32	2.32	35.13	126.47
4320	43.20	61.29	2.35	2.35	35.38	126.57

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4321	43.21	61.21	2.38	2.38	35.64	126.67
4322	43.22	61.13	2.42	2.42	35.90	126.76
4323	43.23	61.05	2.45	2.45	36.14	126.85
4324	43.24	60.99	2.48	2.48	36.35	126.93
4325	43.25	60.93	2.50	2.50	36.49	126.98
4326	43.26	60.95	2.51	2.51	36.57	127.02
4327	43.27	60.99	2.51	2.51	36.59	127.03
4328	43.28	61.04	2.52	2.52	36.60	127.05
4329	43.29	61.09	2.52	2.52	36.61	127.07
4330	43.30	61.15	2.53	2.53	36.62	127.09
4331	43.31	61.20	2.53	2.53	36.64	127.11
4332	43.32	61.25	2.54	2.54	36.65	127.13
4333	43.33	61.29	2.54	2.54	36.65	127.14
4334	43.34	61.35	2.55	2.55	36.58	127.14
4335	43.35	61.64	2.54	2.54	36.41	127.13
4336	43.36	61.99	2.52	2.52	36.15	127.11
4337	43.37	62.39	2.51	2.51	35.85	127.08
4338	43.38	62.82	2.49	2.49	35.54	127.05
4339	43.39	63.25	2.47	2.47	35.22	127.02
4340	43.40	63.66	2.46	2.46	34.91	126.98
4341	43.41	64.03	2.44	2.44	34.63	126.95
4342	43.42	64.35	2.43	2.43	34.38	126.93
4343	43.43	64.73	2.42	2.42	34.10	126.91
4344	43.44	65.38	2.41	2.41	33.75	126.91
4345	43.45	66.16	2.40	2.40	33.32	126.90
4346	43.46	67.02	2.39	2.39	32.84	126.89
4347	43.47	67.92	2.37	2.37	32.35	126.88
4348	43.48	68.82	2.36	2.36	31.86	126.86
4349	43.49	69.66	2.34	2.34	31.41	126.84
4350	43.50	70.40	2.32	2.32	31.01	126.82
4351	43.51	71.01	2.31	2.31	30.68	126.80
4352	43.52	71.45	2.30	2.30	30.40	126.78
4353	43.53	71.99	2.29	2.29	30.11	126.76
4354	43.54	72.62	2.28	2.28	29.78	126.74
4355	43.55	73.30	2.26	2.26	29.42	126.71
4356	43.56	74.00	2.24	2.24	29.05	126.68
4357	43.57	74.68	2.23	2.23	28.70	126.65
4358	43.58	75.31	2.21	2.21	28.37	126.62
4359	43.59	75.85	2.20	2.20	28.10	126.59
4360	43.60	76.22	2.18	2.18	27.93	126.56
4361	43.61	76.21	2.18	2.18	27.85	126.55
4362	43.62	76.21	2.18	2.18	27.83	126.53
4363	43.63	76.21	2.17	2.17	27.80	126.52
4364	43.64	76.21	2.17	2.17	27.78	126.50
4365	43.65	76.21	2.16	2.16	27.75	126.48
4366	43.66	76.21	2.16	2.16	27.72	126.46
4367	43.67	76.20	2.15	2.15	27.70	126.45
4368	43.68	76.20	2.15	2.15	27.72	126.44

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4369	43.69	75.97	2.15	2.15	27.86	126.45
4370	43.70	75.42	2.17	2.17	28.12	126.48
4371	43.71	74.76	2.19	2.19	28.48	126.52
4372	43.72	74.02	2.21	2.21	28.88	126.56
4373	43.73	73.26	2.23	2.23	29.29	126.60
4374	43.74	72.50	2.25	2.25	29.70	126.64
4375	43.75	71.79	2.26	2.26	30.09	126.67
4376	43.76	71.16	2.28	2.28	30.44	126.69
4377	43.77	70.65	2.29	2.29	30.80	126.72
4378	43.78	69.87	2.31	2.31	31.26	126.76
4379	43.79	68.81	2.34	2.34	31.86	126.80
4380	43.80	67.58	2.36	2.36	32.58	126.84
4381	43.81	66.25	2.39	2.39	33.35	126.88
4382	43.82	64.89	2.42	2.42	34.16	126.90
4383	43.83	63.56	2.44	2.44	34.95	126.92
4384	43.84	62.34	2.45	2.45	35.68	126.92
4385	43.85	61.28	2.47	2.47	36.32	126.92
4386	43.86	60.47	2.48	2.48	36.89	126.92
4387	43.87	59.68	2.50	2.50	37.48	126.94
4388	43.88	58.71	2.51	2.51	38.15	126.95
4389	43.89	57.61	2.53	2.53	38.92	126.96
4390	43.90	56.45	2.55	2.55	39.74	126.96
4391	43.91	55.27	2.57	2.57	40.58	126.96
4392	43.92	54.15	2.58	2.58	41.39	126.94
4393	43.93	53.14	2.59	2.59	42.13	126.92
4394	43.94	52.29	2.59	2.59	42.73	126.91
4395	43.95	51.81	2.60	2.60	43.22	126.92
4396	43.96	51.45	2.63	2.63	43.66	126.95
4397	43.97	51.03	2.65	2.65	44.14	127.00
4398	43.98	50.56	2.68	2.68	44.67	127.05
4399	43.99	50.07	2.71	2.71	45.22	127.10
4400	44.00	49.59	2.73	2.73	45.76	127.14
4401	44.01	49.14	2.75	2.75	46.27	127.18
4402	44.02	48.74	2.77	2.77	46.72	127.22
4403	44.03	48.41	2.79	2.79	47.04	127.26
4404	44.04	48.47	2.81	2.81	47.23	127.31
4405	44.05	48.59	2.84	2.84	47.34	127.39
4406	44.06	48.74	2.88	2.88	47.46	127.49
4407	44.07	48.90	2.92	2.92	47.58	127.59
4408	44.08	49.06	2.96	2.96	47.71	127.70
4409	44.09	49.22	2.99	2.99	47.83	127.80
4410	44.10	49.37	3.03	3.03	47.94	127.89
4411	44.11	49.49	3.06	3.06	48.01	127.97
4412	44.12	49.65	3.08	3.08	47.98	128.04
4413	44.13	50.09	3.10	3.10	47.83	128.11
4414	44.14	50.63	3.13	3.13	47.57	128.20
4415	44.15	51.24	3.16	3.16	47.28	128.29
4416	44.16	51.88	3.19	3.19	46.97	128.39

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4417	44.17	52.53	3.22	3.22	46.67	128.48
4418	44.18	53.15	3.24	3.24	46.38	128.57
4419	44.19	53.71	3.27	3.27	46.13	128.65
4420	44.20	54.18	3.29	3.29	45.85	128.73
4421	44.21	54.84	3.31	3.31	45.46	128.81
4422	44.22	55.95	3.33	3.33	44.89	128.91
4423	44.23	57.26	3.36	3.36	44.18	129.02
4424	44.24	58.70	3.39	3.39	43.41	129.14
4425	44.25	60.20	3.41	3.41	42.63	129.25
4426	44.26	61.68	3.44	3.44	41.88	129.36
4427	44.27	63.08	3.46	3.46	41.18	129.45
4428	44.28	64.30	3.47	3.47	40.59	129.52
4429	44.29	65.29	3.48	3.48	40.02	129.59
4430	44.30	66.52	3.49	3.49	39.41	129.66
4431	44.31	68.11	3.50	3.50	38.67	129.74
4432	44.32	69.95	3.51	3.51	37.83	129.82
4433	44.33	71.94	3.52	3.52	36.94	129.90
4434	44.34	73.97	3.52	3.52	36.04	129.97
4435	44.35	75.94	3.51	3.51	35.18	130.02
4436	44.36	77.76	3.50	3.50	34.40	130.06
4437	44.37	79.32	3.49	3.49	33.75	130.09
4438	44.38	80.52	3.48	3.48	33.20	130.12
4439	44.39	81.76	3.48	3.48	32.68	130.14
4440	44.40	83.29	3.48	3.48	32.11	130.18
4441	44.41	85.01	3.47	3.47	31.47	130.21
4442	44.42	86.83	3.46	3.46	30.80	130.23
4443	44.43	88.66	3.44	3.44	30.13	130.25
4444	44.44	90.40	3.42	3.42	29.50	130.26
4445	44.45	91.97	3.40	3.40	28.94	130.26
4446	44.46	93.28	3.38	3.38	28.48	130.25
4447	44.47	94.23	3.37	3.37	28.09	130.25
4448	44.48	95.30	3.36	3.36	27.71	130.25
4449	44.49	96.57	3.34	3.34	27.29	130.24
4450	44.50	97.96	3.32	3.32	26.83	130.23
4451	44.51	99.41	3.30	3.30	26.35	130.21
4452	44.52	100.84	3.27	3.27	25.87	130.19
4453	44.53	102.18	3.24	3.24	25.43	130.17
4454	44.54	103.36	3.22	3.22	25.05	130.14
4455	44.55	104.31	3.20	3.20	24.77	130.12
4456	44.56	104.60	3.19	3.19	24.58	130.09
4457	44.57	104.91	3.17	3.17	24.43	130.06
4458	44.58	105.26	3.15	3.15	24.27	130.02
4459	44.59	105.64	3.12	3.12	24.09	129.97
4460	44.60	106.03	3.10	3.10	23.91	129.93
4461	44.61	106.41	3.08	3.08	23.73	129.89
4462	44.62	106.76	3.06	3.06	23.57	129.84
4463	44.63	107.06	3.04	3.04	23.43	129.81
4464	44.64	107.35	3.03	3.03	23.29	129.79

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4465	44.65	107.86	3.02	3.02	23.15	129.78
4466	44.66	108.49	3.01	3.01	22.98	129.77
4467	44.67	109.20	3.00	3.00	22.79	129.76
4468	44.68	109.95	2.99	2.99	22.58	129.75
4469	44.69	110.70	2.98	2.98	22.38	129.74
4470	44.70	111.41	2.97	2.97	22.18	129.73
4471	44.71	112.05	2.96	2.96	22.01	129.72
4472	44.72	112.59	2.95	2.95	21.86	129.71
4473	44.73	113.03	2.94	2.94	21.72	129.70
4474	44.74	113.59	2.93	2.93	21.57	129.69
4475	44.75	114.24	2.92	2.92	21.39	129.67
4476	44.76	114.96	2.91	2.91	21.19	129.66
4477	44.77	115.71	2.89	2.89	20.99	129.64
4478	44.78	116.45	2.88	2.88	20.79	129.62
4479	44.79	117.14	2.87	2.87	20.61	129.60
4480	44.80	117.75	2.85	2.85	20.44	129.58
4481	44.81	118.23	2.84	2.84	20.35	129.56
4482	44.82	118.02	2.84	2.84	20.34	129.55
4483	44.83	117.70	2.84	2.84	20.39	129.54
4484	44.84	117.33	2.84	2.84	20.46	129.52
4485	44.85	116.93	2.84	2.84	20.53	129.51
4486	44.86	116.52	2.83	2.83	20.60	129.50
4487	44.87	116.12	2.83	2.83	20.67	129.48
4488	44.88	115.76	2.83	2.83	20.73	129.47
4489	44.89	115.45	2.83	2.83	20.79	129.46
4490	44.90	115.21	2.83	2.83	20.85	129.45
4491	44.91	114.93	2.83	2.83	20.92	129.45
4492	44.92	114.59	2.83	2.83	21.00	129.46
4493	44.93	114.21	2.84	2.84	21.10	129.46
4494	44.94	113.80	2.84	2.84	21.20	129.46
4495	44.95	113.40	2.85	2.85	21.30	129.46
4496	44.96	113.01	2.85	2.85	21.40	129.46
4497	44.97	112.66	2.85	2.85	21.49	129.47
4498	44.98	112.38	2.86	2.86	21.57	129.47
4499	44.99	112.17	2.86	2.86	21.65	129.48
4500	45.00	111.92	2.88	2.88	21.75	129.51
4501	45.01	111.64	2.89	2.89	21.87	129.54
4502	45.02	111.32	2.91	2.91	22.01	129.57
4503	45.03	111.00	2.92	2.92	22.14	129.60
4504	45.04	110.68	2.94	2.94	22.28	129.64
4505	45.05	110.38	2.95	2.95	22.40	129.66
4506	45.06	110.11	2.96	2.96	22.51	129.69
4507	45.07	109.90	2.98	2.98	22.61	129.71
4508	45.08	109.70	2.99	2.99	22.72	129.74
4509	45.09	109.44	3.00	3.00	22.84	129.77
4510	45.10	109.14	3.02	3.02	22.97	129.80
4511	45.11	108.82	3.04	3.04	23.12	129.84
4512	45.12	108.50	3.06	3.06	23.27	129.88

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4513	45.13	108.18	3.07	3.07	23.41	129.91
4514	45.14	107.89	3.09	3.09	23.54	129.94
4515	45.15	107.65	3.10	3.10	23.66	129.97
4516	45.16	107.43	3.11	3.11	23.78	129.99
4517	45.17	107.09	3.13	3.13	23.91	130.02
4518	45.18	106.68	3.15	3.15	24.07	130.05
4519	45.19	106.22	3.16	3.16	24.26	130.08
4520	45.20	105.73	3.18	3.18	24.45	130.11
4521	45.21	105.24	3.20	3.20	24.64	130.14
4522	45.22	104.78	3.22	3.22	24.83	130.17
4523	45.23	104.37	3.23	3.23	24.99	130.20
4524	45.24	104.03	3.25	3.25	25.13	130.22
4525	45.25	103.74	3.26	3.26	25.27	130.24
4526	45.26	103.37	3.27	3.27	25.43	130.26
4527	45.27	102.94	3.29	3.29	25.61	130.29
4528	45.28	102.47	3.31	3.31	25.81	130.33
4529	45.29	101.98	3.33	3.33	26.01	130.36
4530	45.30	101.50	3.35	3.35	26.21	130.39
4531	45.31	101.05	3.37	3.37	26.40	130.41
4532	45.32	100.66	3.38	3.38	26.57	130.44
4533	45.33	100.35	3.40	3.40	26.69	130.45
4534	45.34	100.14	3.40	3.40	26.79	130.46
4535	45.35	99.88	3.40	3.40	26.88	130.46
4536	45.36	99.58	3.41	3.41	26.98	130.46
4537	45.37	99.26	3.41	3.41	27.09	130.47
4538	45.38	98.93	3.42	3.42	27.19	130.47
4539	45.39	98.62	3.42	3.42	27.30	130.47
4540	45.40	98.33	3.42	3.42	27.40	130.47
4541	45.41	98.09	3.43	3.43	27.47	130.47
4542	45.42	97.98	3.43	3.43	27.47	130.46
4543	45.43	98.10	3.41	3.41	27.42	130.44
4544	45.44	98.23	3.40	3.40	27.32	130.41
4545	45.45	98.39	3.38	3.38	27.21	130.37
4546	45.46	98.55	3.36	3.36	27.09	130.33
4547	45.47	98.71	3.34	3.34	26.97	130.29
4548	45.48	98.86	3.32	3.32	26.86	130.26
4549	45.49	99.00	3.30	3.30	26.75	130.23
4550	45.50	99.12	3.29	3.29	26.64	130.20
4551	45.51	99.44	3.28	3.28	26.49	130.17
4552	45.52	99.99	3.26	3.26	26.27	130.14
4553	45.53	100.64	3.23	3.23	26.01	130.10
4554	45.54	101.35	3.20	3.20	25.72	130.06
4555	45.55	102.08	3.18	3.18	25.42	130.01
4556	45.56	102.80	3.15	3.15	25.12	129.96
4557	45.57	103.47	3.12	3.12	24.85	129.91
4558	45.58	104.06	3.09	3.09	24.61	129.87
4559	45.59	104.53	3.07	3.07	24.39	129.83
4560	45.60	105.10	3.06	3.06	24.18	129.80

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4561	45.61	105.81	3.04	3.04	23.93	129.77
4562	45.62	106.64	3.02	3.02	23.65	129.74
4563	45.63	107.52	2.99	2.99	23.34	129.69
4564	45.64	108.41	2.96	2.96	23.03	129.65
4565	45.65	109.28	2.94	2.94	22.73	129.60
4566	45.66	110.07	2.91	2.91	22.46	129.56
4567	45.67	110.74	2.89	2.89	22.24	129.52
4568	45.68	111.22	2.88	2.88	22.06	129.49
4569	45.69	111.68	2.86	2.86	21.90	129.47
4570	45.70	112.23	2.85	2.85	21.73	129.45
4571	45.71	112.84	2.84	2.84	21.54	129.43
4572	45.72	113.49	2.82	2.82	21.35	129.40
4573	45.73	114.14	2.80	2.80	21.15	129.37
4574	45.74	114.75	2.79	2.79	20.97	129.34
4575	45.75	115.30	2.77	2.77	20.80	129.32
4576	45.76	115.75	2.76	2.76	20.67	129.30
4577	45.77	116.01	2.76	2.76	20.58	129.28
4578	45.78	116.25	2.75	2.75	20.50	129.27
4579	45.79	116.54	2.74	2.74	20.42	129.26
4580	45.80	116.86	2.74	2.74	20.34	129.25
4581	45.81	117.18	2.73	2.73	20.25	129.24
4582	45.82	117.50	2.72	2.72	20.16	129.23
4583	45.83	117.80	2.72	2.72	20.08	129.21
4584	45.84	118.06	2.71	2.71	20.00	129.20
4585	45.85	118.27	2.70	2.70	19.93	129.19
4586	45.86	118.63	2.70	2.70	19.84	129.18
4587	45.87	119.09	2.69	2.69	19.72	129.17
4588	45.88	119.62	2.68	2.68	19.59	129.16
4589	45.89	120.18	2.67	2.67	19.45	129.14
4590	45.90	120.75	2.66	2.66	19.31	129.13
4591	45.91	121.30	2.65	2.65	19.17	129.11
4592	45.92	121.80	2.64	2.64	19.04	129.09
4593	45.93	122.22	2.63	2.63	18.93	129.08
4594	45.94	122.63	2.63	2.63	18.82	129.07
4595	45.95	123.26	2.62	2.62	18.69	129.07
4596	45.96	124.02	2.61	2.61	18.53	129.06
4597	45.97	124.87	2.61	2.61	18.35	129.05
4598	45.98	125.76	2.60	2.60	18.16	129.04
4599	45.99	126.65	2.59	2.59	17.98	129.03
4600	46.00	127.49	2.58	2.58	17.81	129.02
4601	46.01	128.25	2.57	2.57	17.65	129.01
4602	46.02	128.86	2.56	2.56	17.51	129.00
4603	46.03	129.40	2.55	2.55	17.38	128.99
4604	46.04	130.08	2.54	2.54	17.23	128.97
4605	46.05	130.87	2.53	2.53	17.05	128.94
4606	46.06	131.74	2.51	2.51	16.86	128.91
4607	46.07	132.64	2.49	2.49	16.66	128.88
4608	46.08	133.52	2.48	2.48	16.46	128.85

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4609	46.09	134.33	2.46	2.46	16.28	128.82
4610	46.10	135.04	2.45	2.45	16.12	128.79
4611	46.11	135.60	2.44	2.44	16.07	128.82
4612	46.12	136.07	2.48	2.48	16.11	128.92
4613	46.13	136.67	2.54	2.54	16.24	129.09
4614	46.14	137.34	2.60	2.60	16.39	129.29
4615	46.15	138.06	2.67	2.67	16.55	129.49
4616	46.16	138.80	2.75	2.75	16.71	129.69
4617	46.17	139.50	2.82	2.82	16.86	129.89
4618	46.18	140.14	2.88	2.88	16.99	130.06
4619	46.19	140.69	2.93	2.93	17.11	130.20
4620	46.20	141.09	2.98	2.98	17.23	130.34
4621	46.21	141.49	3.03	3.03	17.36	130.48
4622	46.22	141.97	3.10	3.10	17.51	130.64
4623	46.23	142.51	3.17	3.17	17.68	130.82
4624	46.24	143.08	3.25	3.25	17.86	131.01
4625	46.25	143.65	3.33	3.33	18.03	131.19
4626	46.26	144.18	3.41	3.41	18.19	131.36
4627	46.27	144.66	3.47	3.47	18.33	131.50
4628	46.28	145.05	3.53	3.53	18.41	131.59
4629	46.29	145.10	3.51	3.51	18.39	131.59
4630	46.30	145.04	3.47	3.47	18.28	131.51
4631	46.31	144.97	3.42	3.42	18.13	131.40
4632	46.32	144.89	3.36	3.36	17.97	131.28
4633	46.33	144.81	3.31	3.31	17.80	131.16
4634	46.34	144.73	3.25	3.25	17.63	131.03
4635	46.35	144.65	3.20	3.20	17.48	130.92
4636	46.36	144.59	3.15	3.15	17.35	130.82
4637	46.37	144.51	3.12	3.12	17.29	130.75
4638	46.38	143.98	3.12	3.12	17.30	130.71
4639	46.39	143.32	3.11	3.11	17.38	130.68
4640	46.40	142.56	3.10	3.10	17.47	130.66
4641	46.41	141.76	3.10	3.10	17.56	130.63
4642	46.42	140.95	3.09	3.09	17.66	130.60
4643	46.43	140.17	3.08	3.08	17.75	130.57
4644	46.44	139.45	3.08	3.08	17.84	130.54
4645	46.45	138.85	3.07	3.07	17.92	130.52
4646	46.46	138.25	3.07	3.07	18.05	130.51
4647	46.47	137.33	3.09	3.09	18.22	130.52
4648	46.48	136.21	3.10	3.10	18.45	130.54
4649	46.49	134.97	3.12	3.12	18.70	130.56
4650	46.50	133.68	3.14	3.14	18.97	130.57
4651	46.51	132.38	3.15	3.15	19.24	130.58
4652	46.52	131.16	3.16	3.16	19.49	130.59
4653	46.53	130.08	3.18	3.18	19.72	130.60
4654	46.54	129.19	3.19	3.19	19.93	130.60
4655	46.55	128.12	3.19	3.19	20.14	130.58
4656	46.56	126.66	3.18	3.18	20.39	130.55

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4657	46.57	124.95	3.18	3.18	20.69	130.51
4658	46.58	123.09	3.18	3.18	21.01	130.47
4659	46.59	121.18	3.17	3.17	21.36	130.41
4660	46.60	119.30	3.16	3.16	21.69	130.36
4661	46.61	117.57	3.15	3.15	22.01	130.31
4662	46.62	116.06	3.15	3.15	22.29	130.26
4663	46.63	114.87	3.14	3.14	22.58	130.24
4664	46.64	113.63	3.16	3.16	22.91	130.23
4665	46.65	112.09	3.18	3.18	23.33	130.25
4666	46.66	110.33	3.20	3.20	23.80	130.26
4667	46.67	108.46	3.22	3.22	24.32	130.27
4668	46.68	106.56	3.24	3.24	24.84	130.27
4669	46.69	104.74	3.26	3.26	25.35	130.26
4670	46.70	103.08	3.27	3.27	25.81	130.25
4671	46.71	101.69	3.28	3.28	26.22	130.24
4672	46.72	100.59	3.29	3.29	26.62	130.24
4673	46.73	99.30	3.32	3.32	27.07	130.26
4674	46.74	97.75	3.35	3.35	27.61	130.28
4675	46.75	96.03	3.37	3.37	28.22	130.30
4676	46.76	94.23	3.40	3.40	28.86	130.31
4677	46.77	92.43	3.42	3.42	29.50	130.31
4678	46.78	90.74	3.44	3.44	30.11	130.31
4679	46.79	89.24	3.46	3.46	30.65	130.30
4680	46.80	88.01	3.46	3.46	31.12	130.29
4681	46.81	87.03	3.48	3.48	31.56	130.28
4682	46.82	85.81	3.49	3.49	32.05	130.27
4683	46.83	84.38	3.50	3.50	32.61	130.26
4684	46.84	82.83	3.51	3.51	33.23	130.24
4685	46.85	81.24	3.52	3.52	33.88	130.21
4686	46.86	79.69	3.53	3.53	34.51	130.18
4687	46.87	78.25	3.53	3.53	35.11	130.14
4688	46.88	77.00	3.53	3.53	35.62	130.11
4689	46.89	76.03	3.53	3.53	36.05	130.06
4690	46.90	75.04	3.51	3.51	36.44	129.99
4691	46.91	73.81	3.48	3.48	36.86	129.89
4692	46.92	72.41	3.45	3.45	37.34	129.78
4693	46.93	70.92	3.41	3.41	37.87	129.65
4694	46.94	69.42	3.38	3.38	38.41	129.52
4695	46.95	67.98	3.34	3.34	38.94	129.39
4696	46.96	66.67	3.30	3.30	39.43	129.27
4697	46.97	65.56	3.27	3.27	39.84	129.16
4698	46.98	64.77	3.24	3.24	40.16	129.05
4699	46.99	63.94	3.20	3.20	40.44	128.93
4700	47.00	62.95	3.16	3.16	40.74	128.78
4701	47.01	61.85	3.10	3.10	41.08	128.62
4702	47.02	60.70	3.05	3.05	41.44	128.44
4703	47.03	59.56	2.99	2.99	41.82	128.26
4704	47.04	58.48	2.94	2.94	42.17	128.09

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4705	47.05	57.52	2.89	2.89	42.50	127.94
4706	47.06	56.75	2.86	2.86	42.74	127.83
4707	47.07	56.51	2.85	2.85	42.90	127.77
4708	47.08	56.33	2.84	2.84	43.01	127.75
4709	47.09	56.13	2.84	2.84	43.11	127.73
4710	47.10	55.91	2.83	2.83	43.23	127.71
4711	47.11	55.68	2.83	2.83	43.35	127.68
4712	47.12	55.45	2.82	2.82	43.47	127.66
4713	47.13	55.25	2.82	2.82	43.58	127.64
4714	47.14	55.07	2.81	2.81	43.67	127.62
4715	47.15	54.97	2.81	2.81	43.71	127.63
4716	47.16	55.19	2.83	2.83	43.70	127.66
4717	47.17	55.46	2.85	2.85	43.64	127.72
4718	47.18	55.76	2.87	2.87	43.58	127.79
4719	47.19	56.08	2.89	2.89	43.52	127.86
4720	47.20	56.41	2.92	2.92	43.45	127.94
4721	47.21	56.72	2.94	2.94	43.39	128.01
4722	47.22	57.00	2.96	2.96	43.33	128.07
4723	47.23	57.24	2.98	2.98	43.27	128.12
4724	47.24	57.50	2.99	2.99	43.14	128.16
4725	47.25	57.90	2.99	2.99	42.95	128.20
4726	47.26	58.38	3.00	3.00	42.69	128.23
4727	47.27	58.92	3.01	3.01	42.41	128.27
4728	47.28	59.47	3.02	3.02	42.11	128.31
4729	47.29	60.02	3.02	3.02	41.82	128.35
4730	47.30	60.54	3.03	3.03	41.55	128.39
4731	47.31	61.01	3.03	3.03	41.32	128.42
4732	47.32	61.38	3.04	3.04	41.10	128.44
4733	47.33	61.71	3.03	3.03	40.86	128.45
4734	47.34	62.13	3.02	3.02	40.57	128.44
4735	47.35	62.62	3.01	3.01	40.23	128.43
4736	47.36	63.15	3.00	3.00	39.86	128.42
4737	47.37	63.69	2.98	2.98	39.48	128.40
4738	47.38	64.22	2.97	2.97	39.11	128.38
4739	47.39	64.71	2.95	2.95	38.78	128.37
4740	47.40	65.13	2.94	2.94	38.48	128.35
4741	47.41	65.47	2.93	2.93	38.21	128.33
4742	47.42	65.86	2.91	2.91	37.92	128.31
4743	47.43	66.34	2.90	2.90	37.58	128.28
4744	47.44	66.88	2.87	2.87	37.18	128.25
4745	47.45	67.45	2.85	2.85	36.77	128.21
4746	47.46	68.03	2.82	2.82	36.35	128.16
4747	47.47	68.59	2.80	2.80	35.95	128.12
4748	47.48	69.09	2.78	2.78	35.58	128.08
4749	47.49	69.51	2.76	2.76	35.29	128.04
4750	47.50	69.71	2.74	2.74	35.06	127.98
4751	47.51	69.79	2.71	2.71	34.85	127.92
4752	47.52	69.89	2.68	2.68	34.62	127.83

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4753	47.53	69.99	2.64	2.64	34.37	127.74
4754	47.54	70.10	2.60	2.60	34.10	127.64
4755	47.55	70.21	2.56	2.56	33.84	127.53
4756	47.56	70.31	2.53	2.53	33.59	127.44
4757	47.57	70.40	2.50	2.50	33.36	127.35
4758	47.58	70.47	2.47	2.47	33.19	127.27
4759	47.59	70.39	2.45	2.45	33.06	127.19
4760	47.60	70.27	2.42	2.42	32.95	127.11
4761	47.61	70.12	2.39	2.39	32.82	127.00
4762	47.62	69.96	2.35	2.35	32.67	126.89
4763	47.63	69.80	2.32	2.32	32.52	126.77
4764	47.64	69.64	2.28	2.28	32.38	126.66
4765	47.65	69.49	2.25	2.25	32.24	126.55
4766	47.66	69.37	2.22	2.22	32.12	126.46
4767	47.67	69.36	2.20	2.20	31.98	126.42
4768	47.68	69.85	2.20	2.20	31.78	126.42
4769	47.69	70.46	2.21	2.21	31.54	126.44
4770	47.70	71.14	2.21	2.21	31.26	126.47
4771	47.71	71.87	2.21	2.21	30.96	126.49
4772	47.72	72.60	2.21	2.21	30.67	126.52
4773	47.73	73.30	2.21	2.21	30.39	126.54
4774	47.74	73.93	2.21	2.21	30.14	126.56
4775	47.75	74.46	2.21	2.21	29.94	126.57
4776	47.76	74.70	2.20	2.20	29.79	126.56
4777	47.77	74.79	2.19	2.19	29.66	126.53
4778	47.78	74.89	2.17	2.17	29.53	126.48
4779	47.79	75.01	2.16	2.16	29.38	126.42
4780	47.80	75.13	2.14	2.14	29.23	126.37
4781	47.81	75.25	2.12	2.12	29.07	126.31
4782	47.82	75.37	2.10	2.10	28.93	126.26
4783	47.83	75.47	2.09	2.09	28.80	126.21
4784	47.84	75.55	2.08	2.08	28.74	126.16
4785	47.85	75.17	2.06	2.06	28.76	126.10
4786	47.86	74.62	2.05	2.05	28.85	126.02
4787	47.87	73.98	2.03	2.03	28.97	125.93
4788	47.88	73.29	2.00	2.00	29.09	125.83
4789	47.89	72.59	1.98	1.98	29.23	125.73
4790	47.90	71.90	1.96	1.96	29.36	125.63
4791	47.91	71.27	1.94	1.94	29.48	125.53
4792	47.92	70.72	1.92	1.92	29.59	125.46
4793	47.93	70.33	1.91	1.91	29.74	125.43
4794	47.94	70.06	1.93	1.93	29.93	125.44
4795	47.95	69.73	1.95	1.95	30.19	125.49
4796	47.96	69.35	1.96	1.96	30.48	125.55
4797	47.97	68.95	1.98	1.98	30.78	125.61
4798	47.98	68.55	2.00	2.00	31.09	125.66
4799	47.99	68.17	2.02	2.02	31.38	125.71
4800	48.00	67.83	2.03	2.03	31.64	125.75

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4801	48.01	67.54	2.05	2.05	31.89	125.79
4802	48.02	67.20	2.06	2.06	32.18	125.83
4803	48.03	66.67	2.08	2.08	32.55	125.88
4804	48.04	66.03	2.10	2.10	32.99	125.93
4805	48.05	65.34	2.13	2.13	33.49	125.99
4806	48.06	64.61	2.15	2.15	34.00	126.04
4807	48.07	63.90	2.17	2.17	34.51	126.08
4808	48.08	63.23	2.19	2.19	34.99	126.12
4809	48.09	62.63	2.21	2.21	35.41	126.16
4810	48.10	62.16	2.22	2.22	35.76	126.18
4811	48.11	61.77	2.23	2.23	36.08	126.20
4812	48.12	61.29	2.24	2.24	36.41	126.21
4813	48.13	60.73	2.25	2.25	36.79	126.22
4814	48.14	60.12	2.26	2.26	37.21	126.23
4815	48.15	59.51	2.27	2.27	37.63	126.24
4816	48.16	58.91	2.28	2.28	38.04	126.24
4817	48.17	58.36	2.29	2.29	38.43	126.25
4818	48.18	57.88	2.29	2.29	38.74	126.25
4819	48.19	57.56	2.30	2.30	38.92	126.23
4820	48.20	57.41	2.28	2.28	38.99	126.19
4821	48.21	57.22	2.27	2.27	38.99	126.13
4822	48.22	57.01	2.25	2.25	38.99	126.06
4823	48.23	56.79	2.23	2.23	38.99	125.99
4824	48.24	56.57	2.21	2.21	38.99	125.91
4825	48.25	56.35	2.19	2.19	38.99	125.84
4826	48.26	56.16	2.17	2.17	38.99	125.78
4827	48.27	56.00	2.16	2.16	38.93	125.72
4828	48.28	56.09	2.14	2.14	38.75	125.66
4829	48.29	56.41	2.12	2.12	38.41	125.59
4830	48.30	56.78	2.09	2.09	37.96	125.51
4831	48.31	57.19	2.05	2.05	37.46	125.41
4832	48.32	57.62	2.02	2.02	36.94	125.30
4833	48.33	58.04	1.98	1.98	36.42	125.18
4834	48.34	58.43	1.95	1.95	35.94	125.07
4835	48.35	58.78	1.92	1.92	35.51	124.97
4836	48.36	59.06	1.89	1.89	35.11	124.90
4837	48.37	59.56	1.88	1.88	34.70	124.85
4838	48.38	60.22	1.86	1.86	34.22	124.80
4839	48.39	60.97	1.84	1.84	33.67	124.75
4840	48.40	61.79	1.82	1.82	33.07	124.69
4841	48.41	62.62	1.79	1.79	32.46	124.62
4842	48.42	63.43	1.76	1.76	31.87	124.55
4843	48.43	64.17	1.74	1.74	31.32	124.48
4844	48.44	64.81	1.72	1.72	30.87	124.41
4845	48.45	65.30	1.70	1.70	30.51	124.38
4846	48.46	65.82	1.70	1.70	30.20	124.37
4847	48.47	66.46	1.70	1.70	29.88	124.37
4848	48.48	67.18	1.69	1.69	29.53	124.37

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4849	48.49	67.94	1.68	1.68	29.15	124.37
4850	48.50	68.71	1.68	1.68	28.78	124.36
4851	48.51	69.43	1.67	1.67	28.43	124.36
4852	48.52	70.09	1.66	1.66	28.11	124.35
4853	48.53	70.63	1.65	1.65	27.89	124.35
4854	48.54	70.90	1.66	1.66	27.77	124.37
4855	48.55	71.09	1.67	1.67	27.74	124.41
4856	48.56	71.31	1.68	1.68	27.74	124.47
4857	48.57	71.55	1.69	1.69	27.74	124.53
4858	48.58	71.81	1.70	1.70	27.74	124.59
4859	48.59	72.06	1.72	1.72	27.74	124.65
4860	48.60	72.29	1.73	1.73	27.74	124.71
4861	48.61	72.50	1.74	1.74	27.74	124.76
4862	48.62	72.66	1.75	1.75	27.85	124.83
4863	48.63	72.41	1.78	1.78	28.11	124.94
4864	48.64	72.06	1.82	1.82	28.54	125.10
4865	48.65	71.66	1.87	1.87	29.04	125.27
4866	48.66	71.23	1.92	1.92	29.57	125.45
4867	48.67	70.79	1.97	1.97	30.11	125.63
4868	48.68	70.37	2.02	2.02	30.62	125.79
4869	48.69	69.98	2.06	2.06	31.09	125.93
4870	48.70	69.65	2.10	2.10	31.50	126.06
4871	48.71	69.36	2.14	2.14	31.96	126.20
4872	48.72	68.97	2.20	2.20	32.52	126.38
4873	48.73	68.49	2.27	2.27	33.21	126.60
4874	48.74	67.96	2.36	2.36	33.98	126.84
4875	48.75	67.39	2.44	2.44	34.78	127.07
4876	48.76	66.82	2.52	2.52	35.57	127.29
4877	48.77	66.28	2.60	2.60	36.31	127.49
4878	48.78	65.80	2.67	2.67	36.96	127.66
4879	48.79	65.40	2.73	2.73	37.51	127.79
4880	48.80	65.05	2.77	2.77	38.01	127.90
4881	48.81	64.61	2.81	2.81	38.52	128.01
4882	48.82	64.09	2.86	2.86	39.10	128.12
4883	48.83	63.52	2.92	2.92	39.74	128.24
4884	48.84	62.92	2.98	2.98	40.40	128.35
4885	48.85	62.34	3.03	3.03	41.05	128.46
4886	48.86	61.79	3.08	3.08	41.65	128.56
4887	48.87	61.32	3.12	3.12	42.17	128.64
4888	48.88	60.93	3.16	3.16	42.51	128.69
4889	48.89	60.92	3.17	3.17	42.70	128.73
4890	48.90	60.92	3.18	3.18	42.78	128.76
4891	48.91	60.92	3.19	3.19	42.86	128.79
4892	48.92	60.92	3.21	3.21	42.94	128.82
4893	48.93	60.92	3.22	3.22	43.03	128.86
4894	48.94	60.92	3.24	3.24	43.12	128.89
4895	48.95	60.92	3.25	3.25	43.19	128.92
4896	48.96	60.92	3.26	3.26	43.21	128.95

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4897	48.97	61.19	3.27	3.27	43.03	129.00
4898	48.98	62.26	3.30	3.30	42.60	129.08
4899	48.99	63.56	3.32	3.32	41.99	129.18
4900	49.00	65.02	3.35	3.35	41.31	129.29
4901	49.01	66.55	3.37	3.37	40.60	129.40
4902	49.02	68.09	3.39	3.39	39.91	129.50
4903	49.03	69.56	3.41	3.41	39.27	129.59
4904	49.04	70.87	3.42	3.42	38.70	129.67
4905	49.05	71.95	3.44	3.44	38.17	129.74
4906	49.06	73.25	3.45	3.45	37.58	129.82
4907	49.07	75.14	3.47	3.47	36.85	129.92
4908	49.08	77.36	3.49	3.49	35.99	130.03
4909	49.09	79.80	3.51	3.51	35.07	130.14
4910	49.10	82.32	3.52	3.52	34.14	130.24
4911	49.11	84.80	3.53	3.53	33.24	130.32
4912	49.12	87.12	3.53	3.53	32.41	130.39
4913	49.13	89.15	3.52	3.52	31.71	130.43
4914	49.14	90.76	3.52	3.52	31.09	130.49
4915	49.15	92.76	3.53	3.53	30.46	130.56
4916	49.16	95.28	3.55	3.55	29.74	130.65
4917	49.17	98.18	3.56	3.56	28.94	130.75
4918	49.18	101.28	3.57	3.57	28.10	130.84
4919	49.19	104.44	3.57	3.57	27.26	130.91
4920	49.20	107.49	3.56	3.56	26.47	130.97
4921	49.21	110.29	3.55	3.55	25.75	131.01
4922	49.22	112.67	3.54	3.54	25.16	131.04
4923	49.23	114.52	3.53	3.53	24.67	131.08
4924	49.24	116.61	3.54	3.54	24.21	131.14
4925	49.25	119.16	3.56	3.56	23.72	131.22
4926	49.26	122.00	3.57	3.57	23.17	131.29
4927	49.27	125.00	3.57	3.57	22.60	131.36
4928	49.28	127.99	3.58	3.58	22.05	131.43
4929	49.29	130.84	3.58	3.58	21.53	131.48
4930	49.30	133.38	3.57	3.57	21.07	131.52
4931	49.31	135.48	3.57	3.57	20.73	131.55
4932	49.32	136.79	3.58	3.58	20.48	131.60
4933	49.33	138.15	3.59	3.59	20.30	131.66
4934	49.34	139.74	3.61	3.61	20.11	131.72
4935	49.35	141.49	3.64	3.64	19.90	131.80
4936	49.36	143.30	3.66	3.66	19.69	131.88
4937	49.37	145.07	3.68	3.68	19.49	131.95
4938	49.38	146.73	3.70	3.70	19.30	132.01
4939	49.39	148.18	3.72	3.72	19.14	132.07
4940	49.40	149.32	3.73	3.73	19.04	132.13
4941	49.41	150.05	3.76	3.76	18.98	132.19
4942	49.42	150.96	3.79	3.79	18.95	132.27
4943	49.43	152.01	3.83	3.83	18.92	132.36
4944	49.44	153.13	3.88	3.88	18.89	132.46

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4945	49.45	154.27	3.92	3.92	18.85	132.56
4946	49.46	155.37	3.96	3.96	18.82	132.65
4947	49.47	156.38	4.00	4.00	18.79	132.74
4948	49.48	157.23	4.04	4.04	18.76	132.80
4949	49.49	157.74	4.04	4.04	18.68	132.81
4950	49.50	157.97	4.00	4.00	18.56	132.76
4951	49.51	158.25	3.95	3.95	18.38	132.67
4952	49.52	158.56	3.89	3.89	18.18	132.57
4953	49.53	158.88	3.83	3.83	17.97	132.47
4954	49.54	159.20	3.77	3.77	17.76	132.36
4955	49.55	159.51	3.72	3.72	17.56	132.25
4956	49.56	159.79	3.66	3.66	17.38	132.16
4957	49.57	160.01	3.62	3.62	17.22	132.06
4958	49.58	159.86	3.57	3.57	17.08	131.95
4959	49.59	159.50	3.51	3.51	16.93	131.81
4960	49.60	159.06	3.43	3.43	16.75	131.64
4961	49.61	158.59	3.34	3.34	16.55	131.45
4962	49.62	158.10	3.25	3.25	16.33	131.25
4963	49.63	157.62	3.16	3.16	16.12	131.04
4964	49.64	157.17	3.08	3.08	15.93	130.85
4965	49.65	156.79	3.01	3.01	15.75	130.68
4966	49.66	156.48	2.96	2.96	15.66	130.57
4967	49.67	156.11	2.95	2.95	15.64	130.52
4968	49.68	155.65	2.95	2.95	15.68	130.50
4969	49.69	155.13	2.94	2.94	15.73	130.48
4970	49.70	154.57	2.94	2.94	15.79	130.45
4971	49.71	154.00	2.93	2.93	15.84	130.43
4972	49.72	153.45	2.93	2.93	15.89	130.41
4973	49.73	152.94	2.92	2.92	15.94	130.39
4974	49.74	152.52	2.92	2.92	15.98	130.37
4975	49.75	152.20	2.91	2.91	16.01	130.35
4976	49.76	151.86	2.91	2.91	16.04	130.33
4977	49.77	151.44	2.90	2.90	16.07	130.30
4978	49.78	150.98	2.89	2.89	16.10	130.27
4979	49.79	150.49	2.88	2.88	16.14	130.24
4980	49.80	150.01	2.87	2.87	16.17	130.21
4981	49.81	149.55	2.86	2.86	16.20	130.18
4982	49.82	149.14	2.85	2.85	16.23	130.15
4983	49.83	148.80	2.85	2.85	16.28	130.14
4984	49.84	148.26	2.85	2.85	16.37	130.14
4985	49.85	147.46	2.86	2.86	16.50	130.15
4986	49.86	146.52	2.87	2.87	16.67	130.16
4987	49.87	145.49	2.89	2.89	16.86	130.17
4988	49.88	144.43	2.90	2.90	17.05	130.18
4989	49.89	143.39	2.91	2.91	17.24	130.19
4990	49.90	142.43	2.92	2.92	17.42	130.20
4991	49.91	141.59	2.93	2.93	17.57	130.21
4992	49.92	140.93	2.93	2.93	17.69	130.21

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
4993	49.93	140.41	2.93	2.93	17.80	130.21
4994	49.94	139.75	2.93	2.93	17.90	130.20
4995	49.95	139.00	2.93	2.93	18.02	130.18
4996	49.96	138.20	2.93	2.93	18.15	130.17
4997	49.97	137.38	2.94	2.94	18.27	130.16
4998	49.98	136.60	2.94	2.94	18.40	130.14
4999	49.99	135.88	2.93	2.93	18.51	130.13
5000	50.00	135.28	2.93	2.93	18.58	130.12

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q_c :	Measured cone resistance (tsf)
f_s :	Sleeve friction resistance (tsf)
u :	Pore pressure (tsf)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (pcf)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1	0.01	0.00	0.00	0.00	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
2	0.02	0.00	0.00	0.00	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
3	0.03	0.00	0.00	0.00	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
4	0.04	0.00	0.00	0.00	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
5	0.05	0.00	0.00	0.00	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
6	0.06	0.00	0.00	0.00	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
7	0.07	0.00	0.00	0.00	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
8	0.08	0.00	0.00	0.00	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
9	0.09	0.01	0.00	0.01	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
10	0.10	0.01	0.00	0.01	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
11	0.11	0.01	0.00	0.01	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
12	0.12	0.01	0.00	0.01	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
13	0.13	0.01	0.00	0.01	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
14	0.14	0.01	0.00	0.01	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
15	0.15	0.01	0.00	0.01	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
16	0.16	0.01	0.00	0.01	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
17	0.17	0.01	0.00	0.01	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
18	0.18	0.01	0.00	0.01	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
19	0.19	0.01	0.00	0.01	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
20	0.20	0.01	0.00	0.01	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
21	0.21	0.01	0.00	0.01	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
22	0.22	0.01	0.00	0.01	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
23	0.23	0.01	0.00	0.01	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
24	0.24	0.01	0.00	0.01	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
25	0.25	0.01	0.00	0.01	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
26	0.26	0.01	0.00	0.01	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
27	0.27	0.01	0.00	0.01	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
28	0.28	0.02	0.00	0.02	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
29	0.29	0.02	0.00	0.02	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
30	0.30	0.02	0.00	0.02	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
31	0.31	0.02	0.00	0.02	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
32	0.32	0.02	0.00	0.02	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
33	0.33	0.02	0.00	0.02	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
34	0.34	0.02	0.00	0.02	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
35	0.35	0.02	0.00	0.02	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
36	0.36	0.02	0.00	0.02	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
37	0.37	0.02	0.00	0.02	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
38	0.38	0.02	0.00	0.02	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
39	0.39	0.02	0.00	0.02	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
40	0.40	0.02	0.00	0.02	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
41	0.41	0.02	0.00	0.02	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
42	0.42	0.02	0.00	0.02	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
43	0.43	0.02	0.00	0.02	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
44	0.44	0.02	0.00	0.02	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
45	0.45	0.03	0.00	0.03	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
46	0.46	0.03	0.00	0.03	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
47	0.47	0.03	0.00	0.03	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
48	0.48	0.03	0.00	0.03	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
49	0.49	0.03	0.00	0.03	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
50	0.50	0.03	0.00	0.03	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
51	0.51	0.03	0.00	0.03	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
52	0.52	0.03	0.00	0.03	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
53	0.53	0.03	0.00	0.03	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
54	0.54	0.03	0.00	0.03	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
55	0.55	0.03	0.00	0.03	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
56	0.56	0.03	0.00	0.03	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
57	0.57	0.03	0.00	0.03	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
58	0.58	0.03	0.00	0.03	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
59	0.59	0.03	0.00	0.03	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
60	0.60	0.03	0.00	0.03	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
61	0.61	0.04	0.00	0.04	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
62	0.62	0.04	0.00	0.04	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
63	0.63	0.04	0.00	0.04	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
64	0.64	0.04	0.00	0.04	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
65	0.65	0.04	0.00	0.04	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
66	0.66	0.04	0.00	0.04	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
67	0.67	0.04	0.00	0.04	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
68	0.68	0.04	0.00	0.04	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
69	0.69	0.04	0.00	0.04	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
70	0.70	0.04	0.00	0.04	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
71	0.71	0.04	0.00	0.04	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
72	0.72	0.04	0.00	0.04	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
73	0.73	0.04	0.00	0.04	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
74	0.74	0.04	0.00	0.04	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
75	0.75	0.04	0.00	0.04	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
76	0.76	0.04	0.00	0.04	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
77	0.77	0.04	0.00	0.04	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
78	0.78	0.05	0.00	0.05	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
79	0.79	0.05	0.00	0.05	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
80	0.80	0.05	0.00	0.05	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
81	0.81	0.05	0.00	0.05	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
82	0.82	0.05	0.00	0.05	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
83	0.83	0.05	0.00	0.05	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
84	0.84	0.05	0.00	0.05	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
85	0.85	0.05	0.00	0.05	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
86	0.86	0.05	0.00	0.05	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
87	0.87	0.05	0.00	0.05	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
88	0.88	0.05	0.00	0.05	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
89	0.89	0.05	0.00	0.05	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
90	0.90	0.05	0.00	0.05	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
91	0.91	0.05	0.00	0.05	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
92	0.92	0.05	0.00	0.05	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
93	0.93	0.05	0.00	0.05	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
94	0.94	0.06	0.00	0.06	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
95	0.95	0.06	0.00	0.06	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
96	0.96	0.06	0.00	0.06	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
97	0.97	0.06	0.00	0.06	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
98	0.98	0.06	0.00	0.06	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
99	0.99	0.06	0.00	0.06	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
100	1.00	0.06	0.00	0.06	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
101	1.01	0.06	0.00	0.06	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
102	1.02	0.06	0.00	0.06	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
103	1.03	0.06	0.00	0.06	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
104	1.04	0.06	0.00	0.06	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
105	1.05	0.06	0.00	0.06	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
106	1.06	0.06	0.00	0.06	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
107	1.07	0.06	0.00	0.06	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
108	1.08	0.06	0.00	0.06	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
109	1.09	0.06	0.00	0.06	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
110	1.10	0.06	0.00	0.06	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
111	1.11	0.07	0.00	0.07	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
112	1.12	0.07	0.00	0.07	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
113	1.13	0.07	0.00	0.07	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
114	1.14	0.07	0.00	0.07	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
115	1.15	0.07	0.00	0.07	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
116	1.16	0.07	0.00	0.07	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
117	1.17	0.07	0.00	0.07	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
118	1.18	0.07	0.00	0.07	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
119	1.19	0.07	0.00	0.07	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
120	1.20	0.07	0.00	0.07	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
121	1.21	0.07	0.00	0.07	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
122	1.22	0.07	0.00	0.07	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
123	1.23	0.07	0.00	0.07	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
124	1.24	0.07	0.00	0.07	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
125	1.25	0.07	0.00	0.07	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
126	1.26	0.07	0.00	0.07	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
127	1.27	0.08	0.00	0.08	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
128	1.28	0.08	0.00	0.08	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
129	1.29	0.08	0.00	0.08	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
130	1.30	0.08	0.00	0.08	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
131	1.31	0.08	0.00	0.08	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
132	1.32	0.08	0.00	0.08	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
133	1.33	0.08	0.00	0.08	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
134	1.34	0.08	0.00	0.08	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
135	1.35	0.08	0.00	0.08	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
136	1.36	0.08	0.00	0.08	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
137	1.37	0.08	0.00	0.08	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
138	1.38	0.08	0.00	0.08	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
139	1.39	0.08	0.00	0.08	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
140	1.40	0.08	0.00	0.08	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
141	1.41	0.08	0.00	0.08	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
142	1.42	0.08	0.00	0.08	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
143	1.43	0.08	0.00	0.08	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
144	1.44	0.09	0.00	0.09	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
145	1.45	0.09	0.00	0.09	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
146	1.46	0.09	0.00	0.09	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
147	1.47	0.09	0.00	0.09	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
148	1.48	0.09	0.00	0.09	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
149	1.49	0.09	0.00	0.09	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
150	1.50	0.09	0.00	0.09	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
151	1.51	0.09	0.00	0.09	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
152	1.52	0.09	0.00	0.09	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
153	1.53	0.09	0.00	0.09	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
154	1.54	0.09	0.00	0.09	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
155	1.55	0.09	0.00	0.09	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
156	1.56	0.09	0.00	0.09	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
157	1.57	0.09	0.00	0.09	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
158	1.58	0.09	0.00	0.09	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
159	1.59	0.09	0.00	0.09	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
160	1.60	0.10	0.00	0.10	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
161	1.61	0.10	0.00	0.10	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
162	1.62	0.10	0.00	0.10	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
163	1.63	0.10	0.00	0.10	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
164	1.64	0.10	0.00	0.10	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
165	1.65	0.10	0.00	0.10	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
166	1.66	0.10	0.00	0.10	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
167	1.67	0.10	0.00	0.10	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
168	1.68	0.10	0.00	0.10	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
169	1.69	0.10	0.00	0.10	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
170	1.70	0.10	0.00	0.10	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
171	1.71	0.10	0.00	0.10	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
172	1.72	0.10	0.00	0.10	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
173	1.73	0.10	0.00	0.10	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
174	1.74	0.10	0.00	0.10	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
175	1.75	0.10	0.00	0.10	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
176	1.76	0.10	0.00	0.10	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
177	1.77	0.11	0.00	0.11	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
178	1.78	0.11	0.00	0.11	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
179	1.79	0.11	0.00	0.11	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
180	1.80	0.11	0.00	0.11	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
181	1.81	0.11	0.00	0.11	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
182	1.82	0.11	0.00	0.11	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
183	1.83	0.11	0.00	0.11	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
184	1.84	0.11	0.00	0.11	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
185	1.85	0.11	0.00	0.11	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
186	1.86	0.11	0.00	0.11	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
187	1.87	0.11	0.00	0.11	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
188	1.88	0.11	0.00	0.11	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
189	1.89	0.11	0.00	0.11	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
190	1.90	0.11	0.00	0.11	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
191	1.91	0.11	0.00	0.11	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
192	1.92	0.11	0.00	0.11	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
193	1.93	0.12	0.00	0.12	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
194	1.94	0.12	0.00	0.12	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
195	1.95	0.12	0.00	0.12	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
196	1.96	0.12	0.00	0.12	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
197	1.97	0.12	0.00	0.12	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
198	1.98	0.12	0.00	0.12	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
199	1.99	0.12	0.00	0.12	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
200	2.00	0.12	0.00	0.12	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
201	2.01	0.12	0.00	0.12	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
202	2.02	0.12	0.00	0.12	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
203	2.03	0.12	0.00	0.12	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
204	2.04	0.12	0.00	0.12	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
205	2.05	0.12	0.00	0.12	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
206	2.06	0.12	0.00	0.12	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
207	2.07	0.12	0.00	0.12	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
208	2.08	0.12	0.00	0.12	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
209	2.09	0.12	0.00	0.12	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
210	2.10	0.13	0.00	0.13	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
211	2.11	0.13	0.00	0.13	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
212	2.12	0.13	0.00	0.13	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
213	2.13	0.13	0.00	0.13	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
214	2.14	0.13	0.00	0.13	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
215	2.15	0.13	0.00	0.13	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
216	2.16	0.13	0.00	0.13	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
217	2.17	0.13	0.00	0.13	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
218	2.18	0.13	0.00	0.13	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
219	2.19	0.13	0.00	0.13	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
220	2.20	0.13	0.00	0.13	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
221	2.21	0.13	0.00	0.13	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
222	2.22	0.13	0.00	0.13	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
223	2.23	0.13	0.00	0.13	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
224	2.24	0.13	0.00	0.13	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
225	2.25	0.13	0.00	0.13	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
226	2.26	0.13	0.00	0.13	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
227	2.27	0.14	0.00	0.14	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
228	2.28	0.14	0.00	0.14	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
229	2.29	0.14	0.00	0.14	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
230	2.30	0.14	0.00	0.14	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
231	2.31	0.14	0.00	0.14	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
232	2.32	0.14	0.00	0.14	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
233	2.33	0.14	0.00	0.14	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
234	2.34	0.14	0.00	0.14	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
235	2.35	0.14	0.00	0.14	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
236	2.36	0.14	0.00	0.14	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
237	2.37	0.14	0.00	0.14	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
238	2.38	0.14	0.00	0.14	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
239	2.39	0.14	0.00	0.14	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
240	2.40	0.14	0.00	0.14	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
241	2.41	0.14	0.00	0.14	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
242	2.42	0.14	0.00	0.14	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
243	2.43	0.14	0.00	0.14	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
244	2.44	0.15	0.00	0.15	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
245	2.45	0.15	0.00	0.15	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
246	2.46	0.15	0.00	0.15	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
247	2.47	0.15	0.00	0.15	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
248	2.48	0.15	0.00	0.15	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
249	2.49	0.15	0.00	0.15	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
250	2.50	0.15	0.00	0.15	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
251	2.51	0.15	0.00	0.15	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
252	2.52	0.15	0.00	0.15	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
253	2.53	0.15	0.00	0.15	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
254	2.54	0.15	0.00	0.15	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
255	2.55	0.15	0.00	0.15	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
256	2.56	0.15	0.00	0.15	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
257	2.57	0.15	0.00	0.15	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
258	2.58	0.15	0.00	0.15	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
259	2.59	0.15	0.00	0.15	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
260	2.60	0.15	0.00	0.15	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
261	2.61	0.15	0.00	0.15	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
262	2.62	0.16	0.00	0.16	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
263	2.63	0.16	0.00	0.16	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
264	2.64	0.16	0.00	0.16	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
265	2.65	0.16	0.00	0.16	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
266	2.66	0.16	0.00	0.16	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
267	2.67	0.16	0.00	0.16	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
268	2.68	0.16	0.00	0.16	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
269	2.69	0.16	0.00	0.16	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
270	2.70	0.16	0.00	0.16	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
271	2.71	0.16	0.00	0.16	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
272	2.72	0.16	0.00	0.16	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
273	2.73	0.16	0.00	0.16	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
274	2.74	0.16	0.00	0.16	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
275	2.75	0.16	0.00	0.16	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
276	2.76	0.16	0.00	0.16	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
277	2.77	0.16	0.00	0.16	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
278	2.78	0.16	0.00	0.16	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
279	2.79	0.17	0.00	0.17	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
280	2.80	0.17	0.00	0.17	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
281	2.81	0.17	0.00	0.17	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
282	2.82	0.17	0.00	0.17	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
283	2.83	0.17	0.00	0.17	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
284	2.84	0.17	0.00	0.17	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
285	2.85	0.17	0.00	0.17	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
286	2.86	0.17	0.00	0.17	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
287	2.87	0.17	0.00	0.17	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
288	2.88	0.17	0.00	0.17	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
289	2.89	0.17	0.00	0.17	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
290	2.90	0.17	0.00	0.17	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
291	2.91	0.17	0.00	0.17	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
292	2.92	0.17	0.00	0.17	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
293	2.93	0.17	0.00	0.17	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
294	2.94	0.17	0.00	0.17	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
295	2.95	0.17	0.00	0.17	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
296	2.96	0.17	0.00	0.17	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
297	2.97	0.18	0.00	0.18	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
298	2.98	0.18	0.00	0.18	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
299	2.99	0.18	0.00	0.18	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
300	3.00	0.18	0.00	0.18	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
301	3.01	0.18	0.00	0.18	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
302	3.02	0.18	0.00	0.18	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
303	3.03	0.18	0.00	0.18	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
304	3.04	0.18	0.00	0.18	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
305	3.05	0.18	0.00	0.18	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
306	3.06	0.18	0.00	0.18	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
307	3.07	0.18	0.00	0.18	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
308	3.08	0.18	0.00	0.18	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
309	3.09	0.18	0.00	0.18	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
310	3.10	0.18	0.00	0.18	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
311	3.11	0.18	0.00	0.18	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
312	3.12	0.18	0.00	0.18	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
313	3.13	0.18	0.00	0.18	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
314	3.14	0.18	0.00	0.18	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
315	3.15	0.19	0.00	0.19	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
316	3.16	0.19	0.00	0.19	1.00	0.480	1.04	0.461	1.10	1.30	2.000	No
317	3.17	0.19	0.00	0.19	1.00	0.480	1.04	0.461	1.10	1.30	2.000	No
318	3.18	0.19	0.00	0.19	1.00	0.480	1.04	0.461	1.10	1.30	2.000	No
319	3.19	0.19	0.00	0.19	1.00	0.480	1.04	0.461	1.10	1.30	2.000	No
320	3.20	0.19	0.00	0.19	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
321	3.21	0.19	0.00	0.19	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
322	3.22	0.19	0.00	0.19	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
323	3.23	0.19	0.00	0.19	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
324	3.24	0.19	0.00	0.19	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
325	3.25	0.19	0.00	0.19	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
326	3.26	0.19	0.00	0.19	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
327	3.27	0.19	0.00	0.19	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
328	3.28	0.19	0.00	0.19	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
329	3.29	0.19	0.00	0.19	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
330	3.30	0.19	0.00	0.19	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
331	3.31	0.19	0.00	0.19	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
332	3.32	0.19	0.00	0.19	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
333	3.33	0.19	0.00	0.19	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
334	3.34	0.20	0.00	0.20	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
335	3.35	0.20	0.00	0.20	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
336	3.36	0.20	0.00	0.20	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
337	3.37	0.20	0.00	0.20	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
338	3.38	0.20	0.00	0.20	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
339	3.39	0.20	0.00	0.20	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
340	3.40	0.20	0.00	0.20	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
341	3.41	0.20	0.00	0.20	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
342	3.42	0.20	0.00	0.20	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
343	3.43	0.20	0.00	0.20	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
344	3.44	0.20	0.00	0.20	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
345	3.45	0.20	0.00	0.20	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
346	3.46	0.20	0.00	0.20	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
347	3.47	0.20	0.00	0.20	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
348	3.48	0.20	0.00	0.20	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
349	3.49	0.20	0.00	0.20	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
350	3.50	0.20	0.00	0.20	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
351	3.51	0.20	0.00	0.20	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
352	3.52	0.20	0.00	0.20	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
353	3.53	0.21	0.00	0.21	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
354	3.54	0.21	0.00	0.21	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
355	3.55	0.21	0.00	0.21	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
356	3.56	0.21	0.00	0.21	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
357	3.57	0.21	0.00	0.21	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
358	3.58	0.21	0.00	0.21	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
359	3.59	0.21	0.00	0.21	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
360	3.60	0.21	0.00	0.21	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
361	3.61	0.21	0.00	0.21	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
362	3.62	0.21	0.00	0.21	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
363	3.63	0.21	0.00	0.21	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
364	3.64	0.21	0.00	0.21	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
365	3.65	0.21	0.00	0.21	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
366	3.66	0.21	0.00	0.21	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
367	3.67	0.21	0.00	0.21	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
368	3.68	0.21	0.00	0.21	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
369	3.69	0.21	0.00	0.21	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
370	3.70	0.21	0.00	0.21	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
371	3.71	0.22	0.00	0.22	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
372	3.72	0.22	0.00	0.22	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
373	3.73	0.22	0.00	0.22	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
374	3.74	0.22	0.00	0.22	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
375	3.75	0.22	0.00	0.22	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
376	3.76	0.22	0.00	0.22	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
377	3.77	0.22	0.00	0.22	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
378	3.78	0.22	0.00	0.22	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
379	3.79	0.22	0.00	0.22	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
380	3.80	0.22	0.00	0.22	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
381	3.81	0.22	0.00	0.22	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
382	3.82	0.22	0.00	0.22	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
383	3.83	0.22	0.00	0.22	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
384	3.84	0.22	0.00	0.22	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
385	3.85	0.22	0.00	0.22	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
386	3.86	0.22	0.00	0.22	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
387	3.87	0.22	0.00	0.22	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
388	3.88	0.22	0.00	0.22	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
389	3.89	0.22	0.00	0.22	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
390	3.90	0.23	0.00	0.23	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
391	3.91	0.23	0.00	0.23	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
392	3.92	0.23	0.00	0.23	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
393	3.93	0.23	0.00	0.23	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
394	3.94	0.23	0.00	0.23	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
395	3.95	0.23	0.00	0.23	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
396	3.96	0.23	0.00	0.23	1.00	0.479	1.04	0.460	1.10	1.30	2.000	No
397	3.97	0.23	0.00	0.23	1.00	0.479	1.04	0.460	1.10	1.30	2.000	No
398	3.98	0.23	0.00	0.23	1.00	0.479	1.04	0.460	1.10	1.30	2.000	No
399	3.99	0.23	0.00	0.23	1.00	0.479	1.04	0.460	1.10	1.30	2.000	No
400	4.00	0.23	0.00	0.23	1.00	0.479	1.04	0.460	1.10	1.30	2.000	No
401	4.01	0.23	0.00	0.23	1.00	0.479	1.04	0.460	1.10	1.30	2.000	No
402	4.02	0.23	0.00	0.23	1.00	0.479	1.04	0.460	1.10	1.30	2.000	No
403	4.03	0.23	0.00	0.23	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
404	4.04	0.23	0.00	0.23	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
405	4.05	0.23	0.00	0.23	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
406	4.06	0.23	0.00	0.23	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
407	4.07	0.23	0.00	0.23	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
408	4.08	0.24	0.00	0.24	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
409	4.09	0.24	0.00	0.24	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
410	4.10	0.24	0.00	0.24	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
411	4.11	0.24	0.00	0.24	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
412	4.12	0.24	0.00	0.24	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
413	4.13	0.24	0.00	0.24	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
414	4.14	0.24	0.00	0.24	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
415	4.15	0.24	0.00	0.24	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
416	4.16	0.24	0.00	0.24	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
417	4.17	0.24	0.00	0.24	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
418	4.18	0.24	0.00	0.24	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
419	4.19	0.24	0.00	0.24	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
420	4.20	0.24	0.00	0.24	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
421	4.21	0.24	0.00	0.24	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
422	4.22	0.24	0.00	0.24	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
423	4.23	0.24	0.00	0.24	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
424	4.24	0.24	0.00	0.24	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
425	4.25	0.24	0.00	0.24	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
426	4.26	0.25	0.00	0.25	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
427	4.27	0.25	0.00	0.25	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
428	4.28	0.25	0.00	0.25	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
429	4.29	0.25	0.00	0.25	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
430	4.30	0.25	0.00	0.25	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
431	4.31	0.25	0.00	0.25	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
432	4.32	0.25	0.00	0.25	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
433	4.33	0.25	0.00	0.25	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
434	4.34	0.25	0.00	0.25	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
435	4.35	0.25	0.00	0.25	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
436	4.36	0.25	0.00	0.25	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
437	4.37	0.25	0.00	0.25	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
438	4.38	0.25	0.00	0.25	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
439	4.39	0.25	0.00	0.25	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
440	4.40	0.25	0.00	0.25	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
441	4.41	0.25	0.00	0.25	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
442	4.42	0.25	0.00	0.25	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
443	4.43	0.26	0.00	0.26	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
444	4.44	0.26	0.00	0.26	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
445	4.45	0.26	0.00	0.26	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
446	4.46	0.26	0.00	0.26	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
447	4.47	0.26	0.00	0.26	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
448	4.48	0.26	0.00	0.26	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
449	4.49	0.26	0.00	0.26	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
450	4.50	0.26	0.00	0.26	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
451	4.51	0.26	0.00	0.26	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
452	4.52	0.26	0.00	0.26	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
453	4.53	0.26	0.00	0.26	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
454	4.54	0.26	0.00	0.26	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
455	4.55	0.26	0.00	0.26	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
456	4.56	0.26	0.00	0.26	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
457	4.57	0.26	0.00	0.26	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
458	4.58	0.26	0.00	0.26	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
459	4.59	0.26	0.00	0.26	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
460	4.60	0.26	0.00	0.26	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
461	4.61	0.27	0.00	0.27	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
462	4.62	0.27	0.00	0.27	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
463	4.63	0.27	0.00	0.27	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
464	4.64	0.27	0.00	0.27	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
465	4.65	0.27	0.00	0.27	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
466	4.66	0.27	0.00	0.27	0.99	0.479	1.04	0.459	1.10	1.30	2.000	No
467	4.67	0.27	0.00	0.27	0.99	0.479	1.04	0.459	1.10	1.30	2.000	No
468	4.68	0.27	0.00	0.27	0.99	0.479	1.04	0.459	1.10	1.30	2.000	No
469	4.69	0.27	0.00	0.27	0.99	0.479	1.04	0.459	1.10	1.30	2.000	No
470	4.70	0.27	0.00	0.27	0.99	0.479	1.04	0.459	1.10	1.30	2.000	No
471	4.71	0.27	0.00	0.27	0.99	0.479	1.04	0.459	1.10	1.30	2.000	No
472	4.72	0.27	0.00	0.27	0.99	0.479	1.04	0.459	1.10	1.30	2.000	No
473	4.73	0.27	0.00	0.27	0.99	0.478	1.04	0.459	1.10	1.30	2.000	No
474	4.74	0.27	0.00	0.27	0.99	0.478	1.04	0.459	1.10	1.30	2.000	No
475	4.75	0.27	0.00	0.27	0.99	0.478	1.04	0.459	1.10	1.30	2.000	No
476	4.76	0.27	0.00	0.27	0.99	0.478	1.04	0.459	1.10	1.30	2.000	No
477	4.77	0.27	0.00	0.27	0.99	0.478	1.04	0.459	1.10	1.30	2.000	No
478	4.78	0.27	0.00	0.27	0.99	0.478	1.04	0.459	1.10	1.30	2.000	No
479	4.79	0.28	0.00	0.28	0.99	0.478	1.04	0.459	1.10	1.30	2.000	No
480	4.80	0.28	0.00	0.28	0.99	0.478	1.04	0.459	1.10	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
481	4.81	0.28	0.00	0.28	0.99	0.478	1.04	0.459	1.10	1.30	2.000	No
482	4.82	0.28	0.00	0.28	0.99	0.478	1.04	0.459	1.10	1.30	2.000	No
483	4.83	0.28	0.00	0.28	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
484	4.84	0.28	0.00	0.28	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
485	4.85	0.28	0.00	0.28	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
486	4.86	0.28	0.00	0.28	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
487	4.87	0.28	0.00	0.28	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
488	4.88	0.28	0.00	0.28	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
489	4.89	0.28	0.00	0.28	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
490	4.90	0.28	0.00	0.28	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
491	4.91	0.28	0.00	0.28	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
492	4.92	0.28	0.00	0.28	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
493	4.93	0.28	0.00	0.28	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
494	4.94	0.28	0.00	0.28	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
495	4.95	0.28	0.00	0.28	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
496	4.96	0.29	0.00	0.29	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
497	4.97	0.29	0.00	0.29	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
498	4.98	0.29	0.00	0.29	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
499	4.99	0.29	0.00	0.29	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
500	5.00	0.29	0.00	0.29	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
501	5.01	0.29	0.00	0.29	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
502	5.02	0.29	0.00	0.29	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
503	5.03	0.29	0.00	0.29	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
504	5.04	0.29	0.00	0.29	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
505	5.05	0.29	0.00	0.29	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
506	5.06	0.29	0.00	0.29	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
507	5.07	0.29	0.00	0.29	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
508	5.08	0.29	0.00	0.29	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
509	5.09	0.29	0.00	0.29	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
510	5.10	0.29	0.00	0.29	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
511	5.11	0.29	0.00	0.29	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
512	5.12	0.29	0.00	0.29	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
513	5.13	0.30	0.00	0.30	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
514	5.14	0.30	0.00	0.30	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
515	5.15	0.30	0.00	0.30	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
516	5.16	0.30	0.00	0.30	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
517	5.17	0.30	0.00	0.30	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
518	5.18	0.30	0.00	0.30	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
519	5.19	0.30	0.00	0.30	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
520	5.20	0.30	0.00	0.30	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
521	5.21	0.30	0.00	0.30	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
522	5.22	0.30	0.00	0.30	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
523	5.23	0.30	0.00	0.30	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
524	5.24	0.30	0.00	0.30	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
525	5.25	0.30	0.00	0.30	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
526	5.26	0.30	0.00	0.30	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
527	5.27	0.30	0.00	0.30	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
528	5.28	0.30	0.00	0.30	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
529	5.29	0.30	0.00	0.30	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
530	5.30	0.31	0.00	0.31	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
531	5.31	0.31	0.00	0.31	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
532	5.32	0.31	0.00	0.31	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
533	5.33	0.31	0.00	0.31	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
534	5.34	0.31	0.00	0.31	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
535	5.35	0.31	0.00	0.31	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
536	5.36	0.31	0.00	0.31	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
537	5.37	0.31	0.00	0.31	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
538	5.38	0.31	0.00	0.31	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
539	5.39	0.31	0.00	0.31	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
540	5.40	0.31	0.00	0.31	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
541	5.41	0.31	0.00	0.31	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
542	5.42	0.31	0.00	0.31	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
543	5.43	0.31	0.00	0.31	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
544	5.44	0.31	0.00	0.31	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
545	5.45	0.31	0.00	0.31	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
546	5.46	0.31	0.00	0.31	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
547	5.47	0.32	0.00	0.32	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
548	5.48	0.32	0.00	0.32	0.99	0.477	1.04	0.458	1.10	1.30	2.000	No
549	5.49	0.32	0.00	0.32	0.99	0.477	1.04	0.458	1.10	1.30	2.000	No
550	5.50	0.32	0.00	0.32	0.99	0.477	1.04	0.458	1.10	1.30	2.000	No
551	5.51	0.32	0.00	0.32	0.99	0.477	1.04	0.458	1.10	1.30	2.000	No
552	5.52	0.32	0.00	0.32	0.99	0.477	1.04	0.458	1.10	1.30	2.000	No
553	5.53	0.32	0.00	0.32	0.99	0.477	1.04	0.458	1.10	1.30	2.000	No
554	5.54	0.32	0.00	0.32	0.99	0.477	1.04	0.458	1.10	1.30	2.000	No
555	5.55	0.32	0.00	0.32	0.99	0.477	1.04	0.458	1.10	1.30	2.000	No
556	5.56	0.32	0.00	0.32	0.99	0.477	1.04	0.458	1.10	1.30	2.000	No
557	5.57	0.32	0.00	0.32	0.99	0.477	1.04	0.458	1.10	1.30	2.000	No
558	5.58	0.32	0.00	0.32	0.99	0.477	1.04	0.458	1.10	1.30	2.000	No
559	5.59	0.32	0.00	0.32	0.99	0.477	1.04	0.458	1.10	1.30	2.000	No
560	5.60	0.32	0.00	0.32	0.99	0.477	1.04	0.458	1.10	1.30	2.000	No
561	5.61	0.32	0.00	0.32	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
562	5.62	0.32	0.00	0.32	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
563	5.63	0.32	0.00	0.32	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
564	5.64	0.33	0.00	0.33	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
565	5.65	0.33	0.00	0.33	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
566	5.66	0.33	0.00	0.33	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
567	5.67	0.33	0.00	0.33	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
568	5.68	0.33	0.00	0.33	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
569	5.69	0.33	0.00	0.33	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
570	5.70	0.33	0.00	0.33	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
571	5.71	0.33	0.00	0.33	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
572	5.72	0.33	0.00	0.33	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
573	5.73	0.33	0.00	0.33	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
574	5.74	0.33	0.00	0.33	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
575	5.75	0.33	0.00	0.33	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
576	5.76	0.33	0.00	0.33	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
577	5.77	0.33	0.00	0.33	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
578	5.78	0.33	0.00	0.33	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
579	5.79	0.33	0.00	0.33	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
580	5.80	0.33	0.00	0.33	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
581	5.81	0.34	0.00	0.34	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
582	5.82	0.34	0.00	0.34	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
583	5.83	0.34	0.00	0.34	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
584	5.84	0.34	0.00	0.34	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
585	5.85	0.34	0.00	0.34	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
586	5.86	0.34	0.00	0.34	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
587	5.87	0.34	0.00	0.34	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
588	5.88	0.34	0.00	0.34	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
589	5.89	0.34	0.00	0.34	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
590	5.90	0.34	0.00	0.34	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
591	5.91	0.34	0.00	0.34	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
592	5.92	0.34	0.00	0.34	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
593	5.93	0.34	0.00	0.34	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
594	5.94	0.34	0.00	0.34	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
595	5.95	0.34	0.00	0.34	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
596	5.96	0.34	0.00	0.34	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
597	5.97	0.34	0.00	0.34	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
598	5.98	0.35	0.00	0.35	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
599	5.99	0.35	0.00	0.35	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
600	6.00	0.35	0.00	0.35	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
601	6.01	0.35	0.00	0.35	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
602	6.02	0.35	0.00	0.35	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
603	6.03	0.35	0.00	0.35	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
604	6.04	0.35	0.00	0.35	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
605	6.05	0.35	0.00	0.35	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
606	6.06	0.35	0.00	0.35	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
607	6.07	0.35	0.00	0.35	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
608	6.08	0.35	0.00	0.35	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
609	6.09	0.35	0.00	0.35	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
610	6.10	0.35	0.00	0.35	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
611	6.11	0.35	0.00	0.35	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
612	6.12	0.35	0.00	0.35	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
613	6.13	0.35	0.00	0.35	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
614	6.14	0.35	0.00	0.35	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
615	6.15	0.36	0.00	0.36	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
616	6.16	0.36	0.00	0.36	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
617	6.17	0.36	0.00	0.36	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
618	6.18	0.36	0.00	0.36	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
619	6.19	0.36	0.00	0.36	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
620	6.20	0.36	0.00	0.36	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
621	6.21	0.36	0.00	0.36	0.99	0.476	1.04	0.457	1.10	1.30	2.000	No
622	6.22	0.36	0.00	0.36	0.99	0.476	1.04	0.457	1.10	1.30	2.000	No
623	6.23	0.36	0.00	0.36	0.99	0.476	1.04	0.457	1.10	1.30	2.000	No
624	6.24	0.36	0.00	0.36	0.99	0.476	1.04	0.457	1.10	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
625	6.25	0.36	0.00	0.36	0.99	0.476	1.04	0.457	1.10	1.30	2.000	No
626	6.26	0.36	0.00	0.36	0.99	0.476	1.04	0.457	1.10	1.30	2.000	No
627	6.27	0.36	0.00	0.36	0.99	0.476	1.04	0.457	1.10	1.30	2.000	No
628	6.28	0.36	0.00	0.36	0.99	0.476	1.04	0.457	1.10	1.30	2.000	No
629	6.29	0.36	0.00	0.36	0.99	0.476	1.04	0.457	1.10	1.30	2.000	No
630	6.30	0.36	0.00	0.36	0.99	0.476	1.04	0.457	1.10	1.30	2.000	No
631	6.31	0.36	0.00	0.36	0.99	0.476	1.04	0.457	1.10	1.30	2.000	No
632	6.32	0.37	0.00	0.37	0.99	0.476	1.04	0.457	1.10	1.30	2.000	No
633	6.33	0.37	0.00	0.37	0.99	0.476	1.04	0.457	1.10	1.30	2.000	No
634	6.34	0.37	0.00	0.37	0.99	0.476	1.04	0.457	1.10	1.30	2.000	No
635	6.35	0.37	0.00	0.37	0.99	0.476	1.04	0.457	1.10	1.30	2.000	No
636	6.36	0.37	0.00	0.37	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
637	6.37	0.37	0.00	0.37	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
638	6.38	0.37	0.00	0.37	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
639	6.39	0.37	0.00	0.37	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
640	6.40	0.37	0.00	0.37	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
641	6.41	0.37	0.00	0.37	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
642	6.42	0.37	0.00	0.37	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
643	6.43	0.37	0.00	0.37	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
644	6.44	0.37	0.00	0.37	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
645	6.45	0.37	0.00	0.37	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
646	6.46	0.37	0.00	0.37	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
647	6.47	0.37	0.00	0.37	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
648	6.48	0.37	0.00	0.37	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
649	6.49	0.38	0.00	0.38	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
650	6.50	0.38	0.00	0.38	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
651	6.51	0.38	0.00	0.38	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
652	6.52	0.38	0.00	0.38	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
653	6.53	0.38	0.00	0.38	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
654	6.54	0.38	0.00	0.38	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
655	6.55	0.38	0.00	0.38	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
656	6.56	0.38	0.00	0.38	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
657	6.57	0.38	0.00	0.38	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
658	6.58	0.38	0.00	0.38	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
659	6.59	0.38	0.00	0.38	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
660	6.60	0.38	0.00	0.38	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
661	6.61	0.38	0.00	0.38	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
662	6.62	0.38	0.00	0.38	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
663	6.63	0.38	0.00	0.38	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
664	6.64	0.38	0.00	0.38	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
665	6.65	0.38	0.00	0.38	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
666	6.66	0.39	0.00	0.39	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
667	6.67	0.39	0.00	0.39	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
668	6.68	0.39	0.00	0.39	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
669	6.69	0.39	0.00	0.39	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
670	6.70	0.39	0.00	0.39	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
671	6.71	0.39	0.00	0.39	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
672	6.72	0.39	0.00	0.39	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
673	6.73	0.39	0.00	0.39	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
674	6.74	0.39	0.00	0.39	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
675	6.75	0.39	0.00	0.39	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
676	6.76	0.39	0.00	0.39	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
677	6.77	0.39	0.00	0.39	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
678	6.78	0.39	0.00	0.39	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
679	6.79	0.39	0.00	0.39	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
680	6.80	0.39	0.00	0.39	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
681	6.81	0.39	0.00	0.39	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
682	6.82	0.40	0.00	0.40	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
683	6.83	0.40	0.00	0.40	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
684	6.84	0.40	0.00	0.40	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
685	6.85	0.40	0.00	0.40	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
686	6.86	0.40	0.00	0.40	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
687	6.87	0.40	0.00	0.40	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
688	6.88	0.40	0.00	0.40	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
689	6.89	0.40	0.00	0.40	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
690	6.90	0.40	0.00	0.40	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
691	6.91	0.40	0.00	0.40	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
692	6.92	0.40	0.00	0.40	0.99	0.475	1.04	0.456	1.10	1.30	2.000	No
693	6.93	0.40	0.00	0.40	0.99	0.475	1.04	0.456	1.10	1.30	2.000	No
694	6.94	0.40	0.00	0.40	0.99	0.475	1.04	0.456	1.10	1.30	2.000	No
695	6.95	0.40	0.00	0.40	0.99	0.475	1.04	0.456	1.10	1.30	2.000	No
696	6.96	0.40	0.00	0.40	0.99	0.475	1.04	0.456	1.10	1.30	2.000	No
697	6.97	0.40	0.00	0.40	0.99	0.475	1.04	0.456	1.10	1.30	2.000	No
698	6.98	0.41	0.00	0.41	0.99	0.475	1.04	0.456	1.10	1.30	2.000	No
699	6.99	0.41	0.00	0.41	0.99	0.475	1.04	0.456	1.10	1.30	2.000	No
700	7.00	0.41	0.00	0.41	0.99	0.475	1.04	0.456	1.10	1.30	2.000	No
701	7.01	0.41	0.00	0.41	0.99	0.475	1.04	0.456	1.10	1.30	2.000	No
702	7.02	0.41	0.00	0.41	0.99	0.475	1.04	0.456	1.10	1.30	2.000	No
703	7.03	0.41	0.00	0.41	0.99	0.475	1.04	0.456	1.10	1.30	2.000	No
704	7.04	0.41	0.00	0.41	0.99	0.475	1.04	0.456	1.10	1.30	2.000	No
705	7.05	0.41	0.00	0.41	0.99	0.475	1.04	0.456	1.10	1.30	2.000	No
706	7.06	0.41	0.00	0.41	0.99	0.475	1.04	0.456	1.10	1.30	2.000	No
707	7.07	0.41	0.00	0.41	0.99	0.475	1.04	0.456	1.10	1.30	2.000	No
708	7.08	0.41	0.00	0.41	0.99	0.475	1.04	0.456	1.10	1.30	2.000	No
709	7.09	0.41	0.00	0.41	0.99	0.475	1.04	0.456	1.10	1.30	2.000	No
710	7.10	0.41	0.00	0.41	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
711	7.11	0.41	0.00	0.41	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
712	7.12	0.41	0.00	0.41	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
713	7.13	0.41	0.00	0.41	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
714	7.14	0.41	0.00	0.41	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
715	7.15	0.42	0.00	0.42	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
716	7.16	0.42	0.00	0.42	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
717	7.17	0.42	0.00	0.42	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
718	7.18	0.42	0.00	0.42	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
719	7.19	0.42	0.00	0.42	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
720	7.20	0.42	0.00	0.42	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
721	7.21	0.42	0.00	0.42	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
722	7.22	0.42	0.00	0.42	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
723	7.23	0.42	0.00	0.42	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
724	7.24	0.42	0.00	0.42	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
725	7.25	0.42	0.00	0.42	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
726	7.26	0.42	0.00	0.42	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
727	7.27	0.42	0.00	0.42	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
728	7.28	0.42	0.00	0.42	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
729	7.29	0.42	0.00	0.42	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
730	7.30	0.42	0.00	0.42	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
731	7.31	0.43	0.00	0.43	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
732	7.32	0.43	0.00	0.43	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
733	7.33	0.43	0.00	0.43	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
734	7.34	0.43	0.00	0.43	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
735	7.35	0.43	0.00	0.43	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
736	7.36	0.43	0.00	0.43	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
737	7.37	0.43	0.00	0.43	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
738	7.38	0.43	0.00	0.43	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
739	7.39	0.43	0.00	0.43	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
740	7.40	0.43	0.00	0.43	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
741	7.41	0.43	0.00	0.43	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
742	7.42	0.43	0.00	0.43	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
743	7.43	0.43	0.00	0.43	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
744	7.44	0.43	0.00	0.43	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
745	7.45	0.43	0.00	0.43	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
746	7.46	0.43	0.00	0.43	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
747	7.47	0.44	0.00	0.44	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
748	7.48	0.44	0.00	0.44	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
749	7.49	0.44	0.00	0.44	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
750	7.50	0.44	0.00	0.44	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
751	7.51	0.44	0.00	0.44	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
752	7.52	0.44	0.00	0.44	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
753	7.53	0.44	0.00	0.44	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
754	7.54	0.44	0.00	0.44	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
755	7.55	0.44	0.00	0.44	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
756	7.56	0.44	0.00	0.44	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
757	7.57	0.44	0.00	0.44	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
758	7.58	0.44	0.00	0.44	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
759	7.59	0.44	0.00	0.44	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
760	7.60	0.44	0.00	0.44	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
761	7.61	0.44	0.00	0.44	0.99	0.474	1.04	0.455	1.10	1.30	2.000	No
762	7.62	0.44	0.00	0.44	0.99	0.474	1.04	0.455	1.10	1.30	2.000	No
763	7.63	0.45	0.00	0.45	0.99	0.474	1.04	0.455	1.10	1.30	2.000	No
764	7.64	0.45	0.00	0.45	0.99	0.474	1.04	0.455	1.10	1.30	2.000	No
765	7.65	0.45	0.00	0.45	0.99	0.474	1.04	0.455	1.10	1.30	2.000	No
766	7.66	0.45	0.00	0.45	0.99	0.474	1.04	0.455	1.10	1.30	2.000	No
767	7.67	0.45	0.00	0.45	0.99	0.474	1.04	0.455	1.10	1.30	2.000	No
768	7.68	0.45	0.00	0.45	0.99	0.474	1.04	0.455	1.10	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
769	7.69	0.45	0.00	0.45	0.99	0.474	1.04	0.455	1.10	1.30	2.000	No
770	7.70	0.45	0.00	0.45	0.99	0.474	1.04	0.455	1.10	1.30	2.000	No
771	7.71	0.45	0.00	0.45	0.99	0.474	1.04	0.455	1.10	1.30	2.000	No
772	7.72	0.45	0.00	0.45	0.99	0.474	1.04	0.455	1.10	1.30	2.000	No
773	7.73	0.45	0.00	0.45	0.99	0.474	1.04	0.455	1.10	1.30	2.000	No
774	7.74	0.45	0.00	0.45	0.99	0.474	1.04	0.455	1.10	1.30	2.000	No
775	7.75	0.45	0.00	0.45	0.99	0.474	1.04	0.455	1.10	1.30	2.000	No
776	7.76	0.45	0.00	0.45	0.99	0.474	1.04	0.455	1.10	1.30	2.000	No
777	7.77	0.45	0.00	0.45	0.99	0.474	1.04	0.455	1.10	1.30	2.000	No
778	7.78	0.45	0.00	0.45	0.99	0.474	1.04	0.455	1.10	1.30	2.000	No
779	7.79	0.46	0.00	0.46	0.99	0.474	1.04	0.455	1.10	1.30	2.000	No
780	7.80	0.46	0.00	0.46	0.99	0.474	1.04	0.455	1.10	1.30	2.000	No
781	7.81	0.46	0.00	0.46	0.99	0.474	1.04	0.455	1.10	1.30	2.000	No
782	7.82	0.46	0.00	0.46	0.99	0.474	1.04	0.454	1.10	1.30	2.000	No
783	7.83	0.46	0.00	0.46	0.99	0.474	1.04	0.454	1.10	1.30	2.000	No
784	7.84	0.46	0.00	0.46	0.99	0.474	1.04	0.454	1.10	1.30	2.000	No
785	7.85	0.46	0.00	0.46	0.99	0.474	1.04	0.454	1.10	1.30	2.000	No
786	7.86	0.46	0.00	0.46	0.99	0.474	1.04	0.454	1.10	1.30	2.000	No
787	7.87	0.46	0.00	0.46	0.99	0.474	1.04	0.454	1.10	1.30	2.000	No
788	7.88	0.46	0.00	0.46	0.99	0.474	1.04	0.454	1.10	1.30	2.000	No
789	7.89	0.46	0.00	0.46	0.99	0.474	1.04	0.454	1.10	1.30	2.000	No
790	7.90	0.46	0.00	0.46	0.99	0.474	1.04	0.454	1.10	1.30	2.000	No
791	7.91	0.46	0.00	0.46	0.99	0.474	1.04	0.454	1.10	1.30	2.000	No
792	7.92	0.46	0.00	0.46	0.99	0.474	1.04	0.454	1.10	1.30	2.000	No
793	7.93	0.46	0.00	0.46	0.99	0.474	1.04	0.454	1.10	1.30	2.000	No
794	7.94	0.46	0.00	0.46	0.99	0.474	1.04	0.454	1.10	1.30	2.000	No
795	7.95	0.47	0.00	0.47	0.99	0.474	1.04	0.454	1.10	1.30	2.000	No
796	7.96	0.47	0.00	0.47	0.99	0.474	1.04	0.454	1.10	1.30	2.000	No
797	7.97	0.47	0.00	0.47	0.99	0.474	1.04	0.454	1.10	1.30	2.000	No
798	7.98	0.47	0.00	0.47	0.99	0.474	1.04	0.454	1.10	1.30	2.000	No
799	7.99	0.47	0.00	0.47	0.99	0.474	1.04	0.454	1.10	1.30	2.000	No
800	8.00	0.47	0.00	0.47	0.99	0.474	1.04	0.454	1.10	1.30	2.000	No
801	8.01	0.47	0.00	0.47	0.99	0.474	1.04	0.455	1.10	1.30	0.536	No
802	8.02	0.47	0.00	0.47	0.99	0.475	1.04	0.455	1.10	1.30	0.537	No
803	8.03	0.47	0.00	0.47	0.99	0.475	1.04	0.455	1.10	1.30	0.537	No
804	8.04	0.47	0.00	0.47	0.99	0.475	1.04	0.455	1.10	1.30	0.537	No
805	8.05	0.47	0.00	0.47	0.99	0.475	1.04	0.456	1.10	1.30	0.537	No
806	8.06	0.47	0.00	0.47	0.99	0.476	1.04	0.456	1.10	1.30	0.538	No
807	8.07	0.47	0.00	0.47	0.99	0.476	1.04	0.456	1.10	1.30	0.538	No
808	8.08	0.47	0.00	0.47	0.99	0.476	1.04	0.457	1.10	1.30	0.538	No
809	8.09	0.47	0.00	0.47	0.99	0.477	1.04	0.457	1.10	1.30	0.538	No
810	8.10	0.47	0.00	0.47	0.98	0.477	1.04	0.457	1.10	1.30	0.539	No
811	8.11	0.48	0.00	0.47	0.98	0.477	1.04	0.457	1.10	1.30	0.539	No
812	8.12	0.48	0.00	0.47	0.98	0.478	1.04	0.458	1.10	1.30	0.539	No
813	8.13	0.48	0.00	0.47	0.98	0.478	1.04	0.458	1.10	1.30	0.540	No
814	8.14	0.48	0.00	0.47	0.98	0.478	1.04	0.458	1.10	1.30	0.540	No
815	8.15	0.48	0.00	0.47	0.98	0.478	1.04	0.459	1.10	1.30	0.540	No
816	8.16	0.48	0.00	0.47	0.98	0.479	1.04	0.459	1.10	1.30	0.541	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
817	8.17	0.48	0.01	0.47	0.98	0.479	1.04	0.459	1.10	1.30	0.541	No
818	8.18	0.48	0.01	0.47	0.98	0.479	1.04	0.459	1.10	1.30	0.541	No
819	8.19	0.48	0.01	0.47	0.98	0.480	1.04	0.460	1.10	1.30	0.542	No
820	8.20	0.48	0.01	0.47	0.98	0.480	1.04	0.460	1.10	1.30	0.542	No
821	8.21	0.48	0.01	0.47	0.98	0.480	1.04	0.460	1.10	1.30	0.542	No
822	8.22	0.48	0.01	0.48	0.98	0.480	1.04	0.460	1.10	1.30	0.543	No
823	8.23	0.48	0.01	0.48	0.98	0.481	1.04	0.461	1.10	1.30	0.543	No
824	8.24	0.48	0.01	0.48	0.98	0.481	1.04	0.461	1.10	1.30	0.543	No
825	8.25	0.48	0.01	0.48	0.98	0.481	1.04	0.461	1.10	1.30	0.544	No
826	8.26	0.48	0.01	0.48	0.98	0.482	1.04	0.462	1.10	1.30	0.544	No
827	8.27	0.49	0.01	0.48	0.98	0.482	1.04	0.462	1.10	1.30	0.545	No
828	8.28	0.49	0.01	0.48	0.98	0.482	1.04	0.462	1.10	1.30	0.545	No
829	8.29	0.49	0.01	0.48	0.98	0.482	1.04	0.462	1.10	1.30	0.545	No
830	8.30	0.49	0.01	0.48	0.98	0.483	1.04	0.463	1.10	1.30	0.545	No
831	8.31	0.49	0.01	0.48	0.98	0.483	1.04	0.463	1.10	1.30	0.546	No
832	8.32	0.49	0.01	0.48	0.98	0.483	1.04	0.463	1.10	1.30	0.546	No
833	8.33	0.49	0.01	0.48	0.98	0.484	1.04	0.464	1.10	1.30	0.546	No
834	8.34	0.49	0.01	0.48	0.98	0.484	1.04	0.464	1.10	1.30	0.546	No
835	8.35	0.49	0.01	0.48	0.98	0.484	1.04	0.464	1.10	1.30	0.546	No
836	8.36	0.49	0.01	0.48	0.98	0.484	1.04	0.464	1.10	1.30	0.547	No
837	8.37	0.49	0.01	0.48	0.98	0.485	1.04	0.465	1.10	1.30	0.547	No
838	8.38	0.49	0.01	0.48	0.98	0.485	1.04	0.465	1.10	1.30	0.547	No
839	8.39	0.49	0.01	0.48	0.98	0.485	1.04	0.465	1.10	1.30	0.547	No
840	8.40	0.49	0.01	0.48	0.98	0.486	1.04	0.465	1.10	1.30	0.547	No
841	8.41	0.49	0.01	0.48	0.98	0.486	1.04	0.466	1.10	1.30	0.548	No
842	8.42	0.49	0.01	0.48	0.98	0.486	1.04	0.466	1.10	1.30	0.548	No
843	8.43	0.50	0.01	0.48	0.98	0.486	1.04	0.466	1.10	1.30	0.548	No
844	8.44	0.50	0.01	0.48	0.98	0.487	1.04	0.467	1.10	1.30	0.548	No
845	8.45	0.50	0.01	0.48	0.98	0.487	1.04	0.467	1.10	1.30	0.548	No
846	8.46	0.50	0.01	0.48	0.98	0.487	1.04	0.467	1.10	1.30	0.549	No
847	8.47	0.50	0.01	0.48	0.98	0.488	1.04	0.467	1.10	1.30	0.549	No
848	8.48	0.50	0.01	0.48	0.98	0.488	1.04	0.468	1.10	1.30	0.549	No
849	8.49	0.50	0.02	0.48	0.98	0.488	1.04	0.468	1.10	1.30	0.549	No
850	8.50	0.50	0.02	0.48	0.98	0.488	1.04	0.468	1.10	1.30	0.549	No
851	8.51	0.50	0.02	0.48	0.98	0.489	1.04	0.468	1.10	1.30	0.549	No
852	8.52	0.50	0.02	0.48	0.98	0.489	1.04	0.469	1.10	1.30	0.550	No
853	8.53	0.50	0.02	0.49	0.98	0.489	1.04	0.469	1.10	1.30	0.550	No
854	8.54	0.50	0.02	0.49	0.98	0.490	1.04	0.469	1.10	1.30	0.550	No
855	8.55	0.50	0.02	0.49	0.98	0.490	1.04	0.469	1.10	1.30	0.550	No
856	8.56	0.50	0.02	0.49	0.98	0.490	1.04	0.470	1.10	1.30	0.551	No
857	8.57	0.50	0.02	0.49	0.98	0.490	1.04	0.470	1.10	1.30	0.551	No
858	8.58	0.50	0.02	0.49	0.98	0.491	1.04	0.470	1.10	1.30	0.551	No
859	8.59	0.51	0.02	0.49	0.98	0.491	1.04	0.471	1.10	1.30	0.551	No
860	8.60	0.51	0.02	0.49	0.98	0.491	1.04	0.471	1.10	1.30	0.552	No
861	8.61	0.51	0.02	0.49	0.98	0.491	1.04	0.471	1.10	1.30	0.552	No
862	8.62	0.51	0.02	0.49	0.98	0.492	1.04	0.471	1.10	1.30	0.552	No
863	8.63	0.51	0.02	0.49	0.98	0.492	1.04	0.472	1.10	1.30	0.552	No
864	8.64	0.51	0.02	0.49	0.98	0.492	1.04	0.472	1.10	1.30	0.553	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
865	8.65	0.51	0.02	0.49	0.98	0.493	1.04	0.472	1.10	1.30	0.553	No
866	8.66	0.51	0.02	0.49	0.98	0.493	1.04	0.472	1.10	1.30	0.553	No
867	8.67	0.51	0.02	0.49	0.98	0.493	1.04	0.473	1.10	1.30	0.554	No
868	8.68	0.51	0.02	0.49	0.98	0.493	1.04	0.473	1.10	1.30	0.554	No
869	8.69	0.51	0.02	0.49	0.98	0.494	1.04	0.473	1.10	1.30	0.554	No
870	8.70	0.51	0.02	0.49	0.98	0.494	1.04	0.473	1.10	1.30	0.554	No
871	8.71	0.51	0.02	0.49	0.98	0.494	1.04	0.474	1.10	1.30	0.555	No
872	8.72	0.51	0.02	0.49	0.98	0.494	1.04	0.474	1.10	1.30	0.555	No
873	8.73	0.51	0.02	0.49	0.98	0.495	1.04	0.474	1.10	1.30	0.555	No
874	8.74	0.51	0.02	0.49	0.98	0.495	1.04	0.474	1.10	1.30	0.556	No
875	8.75	0.52	0.02	0.49	0.98	0.495	1.04	0.475	1.10	1.30	0.556	No
876	8.76	0.52	0.02	0.49	0.98	0.496	1.04	0.475	1.10	1.30	0.556	No
877	8.77	0.52	0.02	0.49	0.98	0.496	1.04	0.475	1.10	1.30	0.557	No
878	8.78	0.52	0.02	0.49	0.98	0.496	1.04	0.475	1.10	1.30	0.557	No
879	8.79	0.52	0.02	0.49	0.98	0.496	1.04	0.476	1.10	1.30	0.557	No
880	8.80	0.52	0.02	0.49	0.98	0.497	1.04	0.476	1.10	1.30	0.558	No
881	8.81	0.52	0.03	0.49	0.98	0.497	1.04	0.476	1.10	1.30	0.558	No
882	8.82	0.52	0.03	0.49	0.98	0.497	1.04	0.477	1.10	1.30	0.559	No
883	8.83	0.52	0.03	0.49	0.98	0.497	1.04	0.477	1.10	1.30	0.559	No
884	8.84	0.52	0.03	0.50	0.98	0.498	1.04	0.477	1.10	1.30	0.559	No
885	8.85	0.52	0.03	0.50	0.98	0.498	1.04	0.477	1.10	1.30	0.560	No
886	8.86	0.52	0.03	0.50	0.98	0.498	1.04	0.478	1.10	1.30	0.560	No
887	8.87	0.52	0.03	0.50	0.98	0.498	1.04	0.478	1.10	1.30	0.561	No
888	8.88	0.52	0.03	0.50	0.98	0.499	1.04	0.478	1.10	1.30	0.561	No
889	8.89	0.52	0.03	0.50	0.98	0.499	1.04	0.478	1.10	1.30	0.561	No
890	8.90	0.53	0.03	0.50	0.98	0.499	1.04	0.479	1.10	1.30	0.562	No
891	8.91	0.53	0.03	0.50	0.98	0.500	1.04	0.479	1.10	1.30	0.562	No
892	8.92	0.53	0.03	0.50	0.98	0.500	1.04	0.479	1.10	1.30	0.563	No
893	8.93	0.53	0.03	0.50	0.98	0.500	1.04	0.479	1.10	1.30	0.563	No
894	8.94	0.53	0.03	0.50	0.98	0.500	1.04	0.480	1.10	1.30	0.563	No
895	8.95	0.53	0.03	0.50	0.98	0.501	1.04	0.480	1.10	1.30	0.564	No
896	8.96	0.53	0.03	0.50	0.98	0.501	1.04	0.480	1.10	1.30	0.564	No
897	8.97	0.53	0.03	0.50	0.98	0.501	1.04	0.480	1.10	1.30	0.564	No
898	8.98	0.53	0.03	0.50	0.98	0.501	1.04	0.481	1.10	1.30	0.565	No
899	8.99	0.53	0.03	0.50	0.98	0.502	1.04	0.481	1.10	1.30	0.565	No
900	9.00	0.53	0.03	0.50	0.98	0.502	1.04	0.481	1.10	1.30	0.566	No
901	9.01	0.53	0.03	0.50	0.98	0.502	1.04	0.481	1.10	1.30	0.566	No
902	9.02	0.53	0.03	0.50	0.98	0.502	1.04	0.482	1.10	1.30	0.566	No
903	9.03	0.53	0.03	0.50	0.98	0.503	1.04	0.482	1.10	1.30	0.567	No
904	9.04	0.53	0.03	0.50	0.98	0.503	1.04	0.482	1.10	1.30	0.567	No
905	9.05	0.53	0.03	0.50	0.98	0.503	1.04	0.482	1.10	1.30	0.568	No
906	9.06	0.54	0.03	0.50	0.98	0.503	1.04	0.483	1.10	1.30	0.568	No
907	9.07	0.54	0.03	0.50	0.98	0.504	1.04	0.483	1.10	1.30	0.568	No
908	9.08	0.54	0.03	0.50	0.98	0.504	1.04	0.483	1.10	1.30	0.569	No
909	9.09	0.54	0.03	0.50	0.98	0.504	1.04	0.483	1.10	1.30	0.569	No
910	9.10	0.54	0.03	0.50	0.98	0.504	1.04	0.484	1.10	1.30	0.569	No
911	9.11	0.54	0.03	0.50	0.98	0.505	1.04	0.484	1.10	1.30	0.569	No
912	9.12	0.54	0.03	0.50	0.98	0.505	1.04	0.484	1.10	1.30	0.570	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
913	9.13	0.54	0.04	0.50	0.98	0.505	1.04	0.484	1.10	1.30	0.570	No
914	9.14	0.54	0.04	0.50	0.98	0.505	1.04	0.484	1.10	1.30	0.570	No
915	9.15	0.54	0.04	0.50	0.98	0.506	1.04	0.485	1.10	1.30	0.571	No
916	9.16	0.54	0.04	0.51	0.98	0.506	1.04	0.485	1.10	1.30	0.571	No
917	9.17	0.54	0.04	0.51	0.98	0.506	1.04	0.485	1.10	1.30	0.571	No
918	9.18	0.54	0.04	0.51	0.98	0.507	1.04	0.485	1.10	1.30	0.571	No
919	9.19	0.54	0.04	0.51	0.98	0.507	1.04	0.486	1.10	1.30	0.571	No
920	9.20	0.54	0.04	0.51	0.98	0.507	1.04	0.486	1.10	1.30	0.572	No
921	9.21	0.54	0.04	0.51	0.98	0.507	1.04	0.486	1.10	1.30	0.572	No
922	9.22	0.55	0.04	0.51	0.98	0.508	1.04	0.486	1.10	1.30	0.572	No
923	9.23	0.55	0.04	0.51	0.98	0.508	1.04	0.487	1.10	1.30	0.572	No
924	9.24	0.55	0.04	0.51	0.98	0.508	1.04	0.487	1.10	1.30	0.572	No
925	9.25	0.55	0.04	0.51	0.98	0.508	1.04	0.487	1.10	1.30	0.573	No
926	9.26	0.55	0.04	0.51	0.98	0.509	1.04	0.487	1.10	1.30	0.573	No
927	9.27	0.55	0.04	0.51	0.98	0.509	1.04	0.488	1.10	1.30	0.573	No
928	9.28	0.55	0.04	0.51	0.98	0.509	1.04	0.488	1.10	1.30	0.573	No
929	9.29	0.55	0.04	0.51	0.98	0.509	1.04	0.488	1.10	1.30	0.574	No
930	9.30	0.55	0.04	0.51	0.98	0.510	1.04	0.488	1.10	1.30	0.574	No
931	9.31	0.55	0.04	0.51	0.98	0.510	1.04	0.489	1.10	1.30	0.574	No
932	9.32	0.55	0.04	0.51	0.98	0.510	1.04	0.489	1.10	1.30	0.575	No
933	9.33	0.55	0.04	0.51	0.98	0.510	1.04	0.489	1.10	1.30	0.575	No
934	9.34	0.55	0.04	0.51	0.98	0.511	1.04	0.489	1.10	1.30	0.575	No
935	9.35	0.55	0.04	0.51	0.98	0.511	1.04	0.490	1.10	1.30	0.575	No
936	9.36	0.55	0.04	0.51	0.98	0.511	1.04	0.490	1.10	1.30	0.575	No
937	9.37	0.55	0.04	0.51	0.98	0.511	1.04	0.490	1.10	1.30	0.576	No
938	9.38	0.56	0.04	0.51	0.98	0.511	1.04	0.490	1.10	1.30	0.576	No
939	9.39	0.56	0.04	0.51	0.98	0.512	1.04	0.490	1.10	1.30	0.576	No
940	9.40	0.56	0.04	0.51	0.98	0.512	1.04	0.491	1.10	1.30	0.576	No
941	9.41	0.56	0.04	0.51	0.98	0.512	1.04	0.491	1.10	1.30	0.577	No
942	9.42	0.56	0.04	0.51	0.98	0.512	1.04	0.491	1.10	1.30	0.577	No
943	9.43	0.56	0.04	0.51	0.98	0.513	1.04	0.491	1.10	1.30	0.577	No
944	9.44	0.56	0.04	0.51	0.98	0.513	1.04	0.492	1.10	1.30	0.577	No
945	9.45	0.56	0.05	0.51	0.98	0.513	1.04	0.492	1.10	1.30	0.577	No
946	9.46	0.56	0.05	0.51	0.98	0.513	1.04	0.492	1.10	1.30	0.577	No
947	9.47	0.56	0.05	0.52	0.98	0.514	1.04	0.492	1.10	1.30	0.577	No
948	9.48	0.56	0.05	0.52	0.98	0.514	1.04	0.493	1.10	1.30	0.577	No
949	9.49	0.56	0.05	0.52	0.98	0.514	1.04	0.493	1.10	1.30	0.577	No
950	9.50	0.56	0.05	0.52	0.98	0.514	1.04	0.493	1.10	1.30	0.577	No
951	9.51	0.56	0.05	0.52	0.98	0.515	1.04	0.493	1.10	1.30	0.577	No
952	9.52	0.56	0.05	0.52	0.98	0.515	1.04	0.494	1.10	1.30	0.577	No
953	9.53	0.56	0.05	0.52	0.98	0.515	1.04	0.494	1.10	1.30	0.577	No
954	9.54	0.57	0.05	0.52	0.98	0.515	1.04	0.494	1.10	1.30	0.577	No
955	9.55	0.57	0.05	0.52	0.98	0.516	1.04	0.494	1.10	1.30	0.577	No
956	9.56	0.57	0.05	0.52	0.98	0.516	1.04	0.494	1.10	1.30	0.577	No
957	9.57	0.57	0.05	0.52	0.98	0.516	1.04	0.495	1.10	1.30	0.578	No
958	9.58	0.57	0.05	0.52	0.98	0.516	1.04	0.495	1.10	1.30	0.578	No
959	9.59	0.57	0.05	0.52	0.98	0.517	1.04	0.495	1.10	1.30	0.579	No
960	9.60	0.57	0.05	0.52	0.98	0.517	1.04	0.495	1.10	1.30	0.580	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
961	9.61	0.57	0.05	0.52	0.98	0.517	1.04	0.496	1.10	1.30	0.581	No
962	9.62	0.57	0.05	0.52	0.98	0.517	1.04	0.496	1.10	1.30	0.582	No
963	9.63	0.57	0.05	0.52	0.98	0.518	1.04	0.496	1.10	1.30	0.582	No
964	9.64	0.57	0.05	0.52	0.98	0.518	1.04	0.496	1.10	1.30	0.583	No
965	9.65	0.57	0.05	0.52	0.98	0.518	1.04	0.496	1.10	1.30	0.584	No
966	9.66	0.57	0.05	0.52	0.98	0.518	1.04	0.497	1.10	1.30	0.584	No
967	9.67	0.57	0.05	0.52	0.98	0.518	1.04	0.497	1.10	1.30	0.584	No
968	9.68	0.57	0.05	0.52	0.98	0.519	1.04	0.497	1.10	1.30	0.585	No
969	9.69	0.58	0.05	0.52	0.98	0.519	1.04	0.497	1.10	1.30	0.585	No
970	9.70	0.58	0.05	0.52	0.98	0.519	1.04	0.498	1.10	1.30	0.585	No
971	9.71	0.58	0.05	0.52	0.98	0.519	1.04	0.498	1.10	1.30	0.585	No
972	9.72	0.58	0.05	0.52	0.98	0.520	1.04	0.498	1.10	1.30	0.586	No
973	9.73	0.58	0.05	0.52	0.98	0.520	1.04	0.498	1.10	1.30	0.586	No
974	9.74	0.58	0.05	0.52	0.98	0.520	1.04	0.499	1.10	1.30	0.586	No
975	9.75	0.58	0.05	0.52	0.98	0.520	1.04	0.499	1.10	1.30	0.587	No
976	9.76	0.58	0.05	0.52	0.98	0.521	1.04	0.499	1.10	1.30	0.588	No
977	9.77	0.58	0.06	0.52	0.98	0.521	1.04	0.499	1.10	1.30	0.589	No
978	9.78	0.58	0.06	0.53	0.98	0.521	1.04	0.499	1.10	1.30	0.591	No
979	9.79	0.58	0.06	0.53	0.98	0.521	1.04	0.500	1.10	1.30	0.592	No
980	9.80	0.58	0.06	0.53	0.98	0.522	1.04	0.500	1.10	1.30	0.593	No
981	9.81	0.58	0.06	0.53	0.98	0.522	1.04	0.500	1.10	1.30	0.594	No
982	9.82	0.58	0.06	0.53	0.98	0.522	1.04	0.500	1.10	1.30	0.595	No
983	9.83	0.58	0.06	0.53	0.98	0.522	1.04	0.501	1.10	1.30	0.595	No
984	9.84	0.58	0.06	0.53	0.98	0.522	1.04	0.501	1.10	1.30	0.596	No
985	9.85	0.59	0.06	0.53	0.98	0.523	1.04	0.501	1.10	1.30	0.595	No
986	9.86	0.59	0.06	0.53	0.98	0.523	1.04	0.501	1.10	1.30	0.595	No
987	9.87	0.59	0.06	0.53	0.98	0.523	1.04	0.501	1.10	1.30	0.595	No
988	9.88	0.59	0.06	0.53	0.98	0.523	1.04	0.502	1.10	1.30	0.594	No
989	9.89	0.59	0.06	0.53	0.98	0.524	1.04	0.502	1.10	1.30	0.595	No
990	9.90	0.59	0.06	0.53	0.98	0.524	1.04	0.502	1.10	1.30	0.595	No
991	9.91	0.59	0.06	0.53	0.98	0.524	1.04	0.502	1.10	1.30	0.596	No
992	9.92	0.59	0.06	0.53	0.98	0.524	1.04	0.503	1.10	1.30	0.596	No
993	9.93	0.59	0.06	0.53	0.98	0.525	1.04	0.503	1.10	1.30	0.595	No
994	9.94	0.59	0.06	0.53	0.98	0.525	1.04	0.503	1.10	1.30	0.595	No
995	9.95	0.59	0.06	0.53	0.98	0.525	1.04	0.503	1.10	1.30	0.594	No
996	9.96	0.59	0.06	0.53	0.98	0.525	1.04	0.503	1.10	1.30	0.594	No
997	9.97	0.59	0.06	0.53	0.98	0.525	1.04	0.504	1.10	1.30	0.593	No
998	9.98	0.59	0.06	0.53	0.98	0.526	1.04	0.504	1.10	1.30	0.593	No
999	9.99	0.59	0.06	0.53	0.98	0.526	1.04	0.504	1.10	1.30	0.593	No
1000	10.00	0.59	0.06	0.53	0.98	0.526	1.04	0.504	1.10	1.30	0.593	No
1001	10.01	0.60	0.06	0.53	0.98	0.526	1.04	0.504	1.10	1.30	0.593	No
1002	10.02	0.60	0.06	0.53	0.98	0.527	1.04	0.505	1.10	1.30	0.593	No
1003	10.03	0.60	0.06	0.53	0.98	0.527	1.04	0.505	1.10	1.30	0.594	No
1004	10.04	0.60	0.06	0.53	0.98	0.527	1.04	0.505	1.10	1.30	0.595	No
1005	10.05	0.60	0.06	0.53	0.98	0.527	1.04	0.505	1.10	1.30	0.595	No
1006	10.06	0.60	0.06	0.53	0.98	0.527	1.04	0.506	1.10	1.30	0.596	No
1007	10.07	0.60	0.06	0.53	0.98	0.528	1.04	0.506	1.10	1.30	0.597	No
1008	10.08	0.60	0.06	0.53	0.98	0.528	1.04	0.506	1.10	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
1009	10.09	0.60	0.07	0.53	0.98	0.528	1.04	0.506	1.10	1.30	2.000	Yes
1010	10.10	0.60	0.07	0.54	0.98	0.528	1.04	0.506	1.10	1.30	2.000	Yes
1011	10.11	0.60	0.07	0.54	0.98	0.529	1.04	0.507	1.10	1.30	2.000	Yes
1012	10.12	0.60	0.07	0.54	0.98	0.529	1.04	0.507	1.10	1.30	2.000	Yes
1013	10.13	0.60	0.07	0.54	0.98	0.529	1.04	0.507	1.10	1.30	2.000	Yes
1014	10.14	0.60	0.07	0.54	0.98	0.529	1.04	0.507	1.10	1.30	2.000	Yes
1015	10.15	0.60	0.07	0.54	0.98	0.529	1.04	0.507	1.10	1.30	2.000	Yes
1016	10.16	0.60	0.07	0.54	0.98	0.530	1.04	0.508	1.10	1.30	2.000	Yes
1017	10.17	0.61	0.07	0.54	0.98	0.530	1.04	0.508	1.10	1.30	2.000	Yes
1018	10.18	0.61	0.07	0.54	0.98	0.530	1.04	0.508	1.10	1.30	2.000	Yes
1019	10.19	0.61	0.07	0.54	0.98	0.530	1.04	0.508	1.10	1.30	2.000	Yes
1020	10.20	0.61	0.07	0.54	0.98	0.531	1.04	0.509	1.10	1.30	2.000	Yes
1021	10.21	0.61	0.07	0.54	0.98	0.531	1.04	0.509	1.10	1.30	2.000	Yes
1022	10.22	0.61	0.07	0.54	0.98	0.531	1.04	0.509	1.09	1.30	2.000	Yes
1023	10.23	0.61	0.07	0.54	0.98	0.531	1.04	0.509	1.09	1.30	2.000	Yes
1024	10.24	0.61	0.07	0.54	0.98	0.531	1.04	0.509	1.09	1.30	2.000	Yes
1025	10.25	0.61	0.07	0.54	0.98	0.532	1.04	0.510	1.09	1.30	2.000	Yes
1026	10.26	0.61	0.07	0.54	0.98	0.532	1.04	0.510	1.09	1.30	2.000	Yes
1027	10.27	0.61	0.07	0.54	0.98	0.532	1.04	0.510	1.09	1.30	2.000	Yes
1028	10.28	0.61	0.07	0.54	0.98	0.532	1.04	0.510	1.09	1.30	2.000	Yes
1029	10.29	0.61	0.07	0.54	0.98	0.533	1.04	0.510	1.08	1.30	2.000	Yes
1030	10.30	0.61	0.07	0.54	0.98	0.533	1.04	0.511	1.08	1.30	2.000	Yes
1031	10.31	0.61	0.07	0.54	0.98	0.533	1.04	0.511	1.08	1.30	2.000	Yes
1032	10.32	0.61	0.07	0.54	0.98	0.533	1.04	0.511	1.08	1.30	2.000	Yes
1033	10.33	0.61	0.07	0.54	0.98	0.533	1.04	0.511	1.08	1.30	2.000	Yes
1034	10.34	0.62	0.07	0.54	0.98	0.534	1.04	0.511	1.08	1.30	2.000	Yes
1035	10.35	0.62	0.07	0.54	0.98	0.534	1.04	0.512	1.08	1.30	2.000	Yes
1036	10.36	0.62	0.07	0.54	0.98	0.534	1.04	0.512	1.08	1.30	2.000	Yes
1037	10.37	0.62	0.07	0.54	0.98	0.534	1.04	0.512	1.08	1.30	2.000	Yes
1038	10.38	0.62	0.07	0.54	0.98	0.534	1.04	0.512	1.07	1.30	2.000	Yes
1039	10.39	0.62	0.07	0.54	0.98	0.535	1.04	0.513	1.07	1.30	2.000	Yes
1040	10.40	0.62	0.07	0.54	0.98	0.535	1.04	0.513	1.07	1.30	2.000	Yes
1041	10.41	0.62	0.08	0.54	0.98	0.535	1.04	0.513	1.07	1.30	2.000	Yes
1042	10.42	0.62	0.08	0.54	0.98	0.535	1.04	0.513	1.07	1.30	2.000	Yes
1043	10.43	0.62	0.08	0.55	0.98	0.536	1.04	0.513	1.07	1.30	2.000	Yes
1044	10.44	0.62	0.08	0.55	0.98	0.536	1.04	0.514	1.07	1.30	2.000	Yes
1045	10.45	0.62	0.08	0.55	0.98	0.536	1.04	0.514	1.07	1.30	2.000	Yes
1046	10.46	0.62	0.08	0.55	0.98	0.536	1.04	0.514	1.07	1.30	2.000	Yes
1047	10.47	0.62	0.08	0.55	0.98	0.536	1.04	0.514	1.07	1.30	2.000	Yes
1048	10.48	0.62	0.08	0.55	0.98	0.537	1.04	0.514	1.07	1.30	2.000	Yes
1049	10.49	0.62	0.08	0.55	0.98	0.537	1.04	0.515	1.07	1.30	2.000	Yes
1050	10.50	0.63	0.08	0.55	0.98	0.537	1.04	0.515	1.07	1.30	2.000	Yes
1051	10.51	0.63	0.08	0.55	0.98	0.537	1.04	0.515	1.07	1.30	2.000	Yes
1052	10.52	0.63	0.08	0.55	0.98	0.538	1.04	0.515	1.07	1.30	0.643	No
1053	10.53	0.63	0.08	0.55	0.98	0.538	1.04	0.515	1.07	1.30	0.643	No
1054	10.54	0.63	0.08	0.55	0.98	0.538	1.04	0.516	1.07	1.30	0.644	No
1055	10.55	0.63	0.08	0.55	0.98	0.538	1.04	0.516	1.07	1.30	0.644	No
1056	10.56	0.63	0.08	0.55	0.98	0.538	1.04	0.516	1.07	1.30	0.644	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1057	10.57	0.63	0.08	0.55	0.98	0.539	1.04	0.516	1.07	1.30	0.645	No
1058	10.58	0.63	0.08	0.55	0.98	0.539	1.04	0.516	1.07	1.30	0.645	No
1059	10.59	0.63	0.08	0.55	0.98	0.539	1.04	0.517	1.07	1.30	0.645	No
1060	10.60	0.63	0.08	0.55	0.98	0.539	1.04	0.517	1.07	1.30	0.645	No
1061	10.61	0.63	0.08	0.55	0.98	0.539	1.04	0.517	1.07	1.30	0.646	No
1062	10.62	0.63	0.08	0.55	0.98	0.540	1.04	0.517	1.07	1.30	2.000	Yes
1063	10.63	0.63	0.08	0.55	0.98	0.540	1.04	0.517	1.07	1.30	2.000	Yes
1064	10.64	0.63	0.08	0.55	0.98	0.540	1.04	0.518	1.07	1.30	2.000	Yes
1065	10.65	0.63	0.08	0.55	0.98	0.540	1.04	0.518	1.07	1.30	2.000	Yes
1066	10.66	0.63	0.08	0.55	0.98	0.540	1.04	0.518	1.07	1.30	2.000	Yes
1067	10.67	0.64	0.08	0.55	0.98	0.541	1.04	0.518	1.07	1.30	2.000	Yes
1068	10.68	0.64	0.08	0.55	0.98	0.541	1.04	0.518	1.07	1.30	2.000	Yes
1069	10.69	0.64	0.08	0.55	0.98	0.541	1.04	0.519	1.07	1.30	2.000	Yes
1070	10.70	0.64	0.08	0.55	0.98	0.541	1.04	0.519	1.07	1.30	2.000	Yes
1071	10.71	0.64	0.08	0.55	0.98	0.542	1.04	0.519	1.07	1.30	2.000	Yes
1072	10.72	0.64	0.08	0.55	0.98	0.542	1.04	0.519	1.07	1.30	2.000	Yes
1073	10.73	0.64	0.09	0.55	0.98	0.542	1.04	0.519	1.07	1.30	2.000	Yes
1074	10.74	0.64	0.09	0.55	0.98	0.542	1.04	0.520	1.07	1.30	2.000	Yes
1075	10.75	0.64	0.09	0.55	0.98	0.542	1.04	0.520	1.07	1.30	2.000	Yes
1076	10.76	0.64	0.09	0.55	0.98	0.543	1.04	0.520	1.07	1.30	2.000	Yes
1077	10.77	0.64	0.09	0.56	0.98	0.543	1.04	0.520	1.07	1.30	2.000	Yes
1078	10.78	0.64	0.09	0.56	0.98	0.543	1.04	0.520	1.07	1.30	2.000	Yes
1079	10.79	0.64	0.09	0.56	0.98	0.543	1.04	0.521	1.08	1.30	2.000	Yes
1080	10.80	0.64	0.09	0.56	0.98	0.543	1.04	0.521	1.08	1.30	2.000	Yes
1081	10.81	0.64	0.09	0.56	0.98	0.544	1.04	0.521	1.08	1.30	2.000	Yes
1082	10.82	0.64	0.09	0.56	0.98	0.544	1.04	0.521	1.08	1.30	2.000	Yes
1083	10.83	0.65	0.09	0.56	0.98	0.544	1.04	0.521	1.08	1.30	2.000	Yes
1084	10.84	0.65	0.09	0.56	0.98	0.544	1.04	0.522	1.08	1.30	2.000	Yes
1085	10.85	0.65	0.09	0.56	0.98	0.544	1.04	0.522	1.08	1.30	2.000	Yes
1086	10.86	0.65	0.09	0.56	0.98	0.545	1.04	0.522	1.08	1.30	2.000	Yes
1087	10.87	0.65	0.09	0.56	0.98	0.545	1.04	0.522	1.08	1.30	2.000	Yes
1088	10.88	0.65	0.09	0.56	0.98	0.545	1.04	0.522	1.08	1.30	2.000	Yes
1089	10.89	0.65	0.09	0.56	0.98	0.545	1.04	0.523	1.08	1.30	2.000	Yes
1090	10.90	0.65	0.09	0.56	0.98	0.545	1.04	0.523	1.08	1.30	2.000	Yes
1091	10.91	0.65	0.09	0.56	0.98	0.546	1.04	0.523	1.08	1.30	2.000	Yes
1092	10.92	0.65	0.09	0.56	0.98	0.546	1.04	0.523	1.08	1.30	2.000	Yes
1093	10.93	0.65	0.09	0.56	0.98	0.546	1.04	0.523	1.09	1.30	2.000	Yes
1094	10.94	0.65	0.09	0.56	0.98	0.546	1.04	0.524	1.09	1.30	2.000	Yes
1095	10.95	0.65	0.09	0.56	0.98	0.546	1.04	0.524	1.09	1.30	2.000	Yes
1096	10.96	0.65	0.09	0.56	0.98	0.547	1.04	0.524	1.09	1.30	2.000	Yes
1097	10.97	0.65	0.09	0.56	0.98	0.547	1.04	0.524	1.09	1.30	2.000	Yes
1098	10.98	0.65	0.09	0.56	0.98	0.547	1.04	0.524	1.09	1.30	2.000	Yes
1099	10.99	0.66	0.09	0.56	0.98	0.547	1.04	0.524	1.09	1.30	2.000	Yes
1100	11.00	0.66	0.09	0.56	0.98	0.547	1.04	0.525	1.09	1.30	2.000	Yes
1101	11.01	0.66	0.09	0.56	0.98	0.548	1.04	0.525	1.09	1.30	2.000	Yes
1102	11.02	0.66	0.09	0.56	0.98	0.548	1.04	0.525	1.09	1.30	2.000	Yes
1103	11.03	0.66	0.09	0.56	0.98	0.548	1.04	0.525	1.09	1.30	2.000	Yes
1104	11.04	0.66	0.09	0.56	0.98	0.548	1.04	0.525	1.09	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1105	11.05	0.66	0.10	0.56	0.98	0.548	1.04	0.526	1.09	1.30	2.000	Yes
1106	11.06	0.66	0.10	0.56	0.98	0.549	1.04	0.526	1.09	1.30	2.000	Yes
1107	11.07	0.66	0.10	0.56	0.98	0.549	1.04	0.526	1.09	1.30	2.000	Yes
1108	11.08	0.66	0.10	0.56	0.98	0.549	1.04	0.526	1.09	1.30	2.000	Yes
1109	11.09	0.66	0.10	0.57	0.98	0.549	1.04	0.526	1.09	1.30	2.000	Yes
1110	11.10	0.66	0.10	0.57	0.98	0.549	1.04	0.527	1.09	1.30	2.000	Yes
1111	11.11	0.66	0.10	0.57	0.98	0.550	1.04	0.527	1.09	1.30	2.000	Yes
1112	11.12	0.66	0.10	0.57	0.98	0.550	1.04	0.527	1.09	1.30	2.000	Yes
1113	11.13	0.66	0.10	0.57	0.98	0.550	1.04	0.527	1.09	1.30	2.000	Yes
1114	11.14	0.66	0.10	0.57	0.98	0.550	1.04	0.527	1.09	1.30	0.635	No
1115	11.15	0.67	0.10	0.57	0.98	0.550	1.04	0.528	1.09	1.30	0.635	No
1116	11.16	0.67	0.10	0.57	0.98	0.551	1.04	0.528	1.09	1.30	0.636	No
1117	11.17	0.67	0.10	0.57	0.98	0.551	1.04	0.528	1.09	1.30	0.637	No
1118	11.18	0.67	0.10	0.57	0.98	0.551	1.04	0.528	1.09	1.30	0.637	No
1119	11.19	0.67	0.10	0.57	0.97	0.551	1.04	0.528	1.09	1.30	0.638	No
1120	11.20	0.67	0.10	0.57	0.97	0.551	1.04	0.528	1.09	1.30	0.639	No
1121	11.21	0.67	0.10	0.57	0.97	0.552	1.04	0.529	1.09	1.30	0.639	No
1122	11.22	0.67	0.10	0.57	0.97	0.552	1.04	0.529	1.09	1.30	2.000	Yes
1123	11.23	0.67	0.10	0.57	0.97	0.552	1.04	0.529	1.09	1.30	2.000	Yes
1124	11.24	0.67	0.10	0.57	0.97	0.552	1.04	0.529	1.09	1.30	2.000	Yes
1125	11.25	0.67	0.10	0.57	0.97	0.552	1.04	0.529	1.09	1.30	2.000	Yes
1126	11.26	0.67	0.10	0.57	0.97	0.553	1.04	0.530	1.09	1.30	2.000	Yes
1127	11.27	0.67	0.10	0.57	0.97	0.553	1.04	0.530	1.09	1.30	2.000	Yes
1128	11.28	0.67	0.10	0.57	0.97	0.553	1.04	0.530	1.09	1.30	2.000	Yes
1129	11.29	0.67	0.10	0.57	0.97	0.553	1.04	0.530	1.09	1.30	2.000	Yes
1130	11.30	0.67	0.10	0.57	0.97	0.553	1.04	0.530	1.09	1.30	2.000	Yes
1131	11.31	0.67	0.10	0.57	0.97	0.553	1.04	0.530	1.09	1.30	2.000	Yes
1132	11.32	0.68	0.10	0.57	0.97	0.554	1.04	0.531	1.08	1.30	2.000	Yes
1133	11.33	0.68	0.10	0.57	0.97	0.554	1.04	0.531	1.08	1.30	2.000	Yes
1134	11.34	0.68	0.10	0.57	0.97	0.554	1.04	0.531	1.08	1.30	2.000	Yes
1135	11.35	0.68	0.10	0.57	0.97	0.554	1.04	0.531	1.08	1.30	2.000	Yes
1136	11.36	0.68	0.10	0.57	0.97	0.554	1.04	0.531	1.08	1.30	2.000	Yes
1137	11.37	0.68	0.11	0.57	0.97	0.555	1.04	0.532	1.08	1.30	2.000	Yes
1138	11.38	0.68	0.11	0.57	0.97	0.555	1.04	0.532	1.08	1.30	2.000	Yes
1139	11.39	0.68	0.11	0.57	0.97	0.555	1.04	0.532	1.08	1.30	2.000	Yes
1140	11.40	0.68	0.11	0.57	0.97	0.555	1.04	0.532	1.08	1.30	2.000	Yes
1141	11.41	0.68	0.11	0.57	0.97	0.555	1.04	0.532	1.08	1.30	2.000	Yes
1142	11.42	0.68	0.11	0.57	0.97	0.556	1.04	0.533	1.08	1.30	2.000	Yes
1143	11.43	0.68	0.11	0.58	0.97	0.556	1.04	0.533	1.08	1.30	2.000	Yes
1144	11.44	0.68	0.11	0.58	0.97	0.556	1.04	0.533	1.08	1.30	2.000	Yes
1145	11.45	0.68	0.11	0.58	0.97	0.556	1.04	0.533	1.08	1.30	2.000	Yes
1146	11.46	0.68	0.11	0.58	0.97	0.556	1.04	0.533	1.07	1.30	2.000	Yes
1147	11.47	0.68	0.11	0.58	0.97	0.557	1.04	0.533	1.07	1.30	2.000	Yes
1148	11.48	0.69	0.11	0.58	0.97	0.557	1.04	0.534	1.07	1.30	2.000	Yes
1149	11.49	0.69	0.11	0.58	0.97	0.557	1.04	0.534	1.07	1.30	2.000	Yes
1150	11.50	0.69	0.11	0.58	0.97	0.557	1.04	0.534	1.07	1.30	2.000	Yes
1151	11.51	0.69	0.11	0.58	0.97	0.557	1.04	0.534	1.07	1.30	2.000	Yes
1152	11.52	0.69	0.11	0.58	0.97	0.557	1.04	0.534	1.07	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
1153	11.53	0.69	0.11	0.58	0.97	0.558	1.04	0.535	1.07	1.30	2.000	Yes
1154	11.54	0.69	0.11	0.58	0.97	0.558	1.04	0.535	1.07	1.30	2.000	Yes
1155	11.55	0.69	0.11	0.58	0.97	0.558	1.04	0.535	1.07	1.30	2.000	Yes
1156	11.56	0.69	0.11	0.58	0.97	0.558	1.04	0.535	1.07	1.30	2.000	Yes
1157	11.57	0.69	0.11	0.58	0.97	0.558	1.04	0.535	1.07	1.30	2.000	Yes
1158	11.58	0.69	0.11	0.58	0.97	0.559	1.04	0.535	1.07	1.30	2.000	Yes
1159	11.59	0.69	0.11	0.58	0.97	0.559	1.04	0.536	1.07	1.30	2.000	Yes
1160	11.60	0.69	0.11	0.58	0.97	0.559	1.04	0.536	1.06	1.30	2.000	Yes
1161	11.61	0.69	0.11	0.58	0.97	0.559	1.04	0.536	1.06	1.30	2.000	Yes
1162	11.62	0.69	0.11	0.58	0.97	0.559	1.04	0.536	1.06	1.30	2.000	Yes
1163	11.63	0.69	0.11	0.58	0.97	0.560	1.04	0.536	1.06	1.30	2.000	Yes
1164	11.64	0.69	0.11	0.58	0.97	0.560	1.04	0.536	1.06	1.30	2.000	Yes
1165	11.65	0.70	0.11	0.58	0.97	0.560	1.04	0.537	1.06	1.30	2.000	Yes
1166	11.66	0.70	0.11	0.58	0.97	0.560	1.04	0.537	1.06	1.30	2.000	Yes
1167	11.67	0.70	0.11	0.58	0.97	0.560	1.04	0.537	1.06	1.30	2.000	Yes
1168	11.68	0.70	0.11	0.58	0.97	0.560	1.04	0.537	1.06	1.30	2.000	Yes
1169	11.69	0.70	0.12	0.58	0.97	0.561	1.04	0.537	1.06	1.30	2.000	Yes
1170	11.70	0.70	0.12	0.58	0.97	0.561	1.04	0.538	1.06	1.30	2.000	Yes
1171	11.71	0.70	0.12	0.58	0.97	0.561	1.04	0.538	1.06	1.30	2.000	Yes
1172	11.72	0.70	0.12	0.58	0.97	0.561	1.04	0.538	1.06	1.30	2.000	Yes
1173	11.73	0.70	0.12	0.58	0.97	0.561	1.04	0.538	1.06	1.30	2.000	Yes
1174	11.74	0.70	0.12	0.58	0.97	0.562	1.04	0.538	1.06	1.30	0.680	No
1175	11.75	0.70	0.12	0.58	0.97	0.562	1.04	0.538	1.06	1.30	0.680	No
1176	11.76	0.70	0.12	0.58	0.97	0.562	1.04	0.539	1.06	1.30	0.680	No
1177	11.77	0.70	0.12	0.58	0.97	0.562	1.04	0.539	1.06	1.30	0.680	No
1178	11.78	0.70	0.12	0.59	0.97	0.562	1.04	0.539	1.06	1.30	0.681	No
1179	11.79	0.70	0.12	0.59	0.97	0.563	1.04	0.539	1.06	1.30	0.681	No
1180	11.80	0.70	0.12	0.59	0.97	0.563	1.04	0.539	1.06	1.30	0.681	No
1181	11.81	0.70	0.12	0.59	0.97	0.563	1.04	0.540	1.06	1.30	0.681	No
1182	11.82	0.71	0.12	0.59	0.97	0.563	1.04	0.540	1.06	1.30	0.681	No
1183	11.83	0.71	0.12	0.59	0.97	0.563	1.04	0.540	1.06	1.30	0.682	No
1184	11.84	0.71	0.12	0.59	0.97	0.563	1.04	0.540	1.06	1.30	0.682	No
1185	11.85	0.71	0.12	0.59	0.97	0.564	1.04	0.540	1.06	1.30	0.683	No
1186	11.86	0.71	0.12	0.59	0.97	0.564	1.04	0.540	1.06	1.30	0.683	No
1187	11.87	0.71	0.12	0.59	0.97	0.564	1.04	0.541	1.06	1.30	0.684	No
1188	11.88	0.71	0.12	0.59	0.97	0.564	1.04	0.541	1.06	1.30	0.685	No
1189	11.89	0.71	0.12	0.59	0.97	0.564	1.04	0.541	1.06	1.30	0.685	No
1190	11.90	0.71	0.12	0.59	0.97	0.565	1.04	0.541	1.06	1.30	0.686	No
1191	11.91	0.71	0.12	0.59	0.97	0.565	1.04	0.541	1.06	1.30	0.686	No
1192	11.92	0.71	0.12	0.59	0.97	0.565	1.04	0.541	1.06	1.30	0.686	No
1193	11.93	0.71	0.12	0.59	0.97	0.565	1.04	0.542	1.06	1.30	0.687	No
1194	11.94	0.71	0.12	0.59	0.97	0.565	1.04	0.542	1.06	1.30	0.687	No
1195	11.95	0.71	0.12	0.59	0.97	0.565	1.04	0.542	1.06	1.30	0.687	No
1196	11.96	0.71	0.12	0.59	0.97	0.566	1.04	0.542	1.06	1.30	0.688	No
1197	11.97	0.71	0.12	0.59	0.97	0.566	1.04	0.542	1.06	1.30	0.688	No
1198	11.98	0.71	0.12	0.59	0.97	0.566	1.04	0.542	1.06	1.30	0.688	No
1199	11.99	0.72	0.12	0.59	0.97	0.566	1.04	0.543	1.06	1.30	0.689	No
1200	12.00	0.72	0.12	0.59	0.97	0.566	1.04	0.543	1.06	1.30	0.689	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
1201	12.01	0.72	0.13	0.59	0.97	0.567	1.04	0.543	1.06	1.30	0.689	No
1202	12.02	0.72	0.13	0.59	0.97	0.567	1.04	0.543	1.06	1.30	0.690	No
1203	12.03	0.72	0.13	0.59	0.97	0.567	1.04	0.543	1.06	1.30	0.690	No
1204	12.04	0.72	0.13	0.59	0.97	0.567	1.04	0.544	1.06	1.30	0.691	No
1205	12.05	0.72	0.13	0.59	0.97	0.567	1.04	0.544	1.06	1.30	0.691	No
1206	12.06	0.72	0.13	0.59	0.97	0.567	1.04	0.544	1.06	1.30	0.692	No
1207	12.07	0.72	0.13	0.59	0.97	0.568	1.04	0.544	1.05	1.30	0.692	No
1208	12.08	0.72	0.13	0.59	0.97	0.568	1.04	0.544	1.05	1.30	0.693	No
1209	12.09	0.72	0.13	0.59	0.97	0.568	1.04	0.544	1.05	1.30	0.693	No
1210	12.10	0.72	0.13	0.59	0.97	0.568	1.04	0.545	1.05	1.30	0.694	No
1211	12.11	0.72	0.13	0.59	0.97	0.568	1.04	0.545	1.05	1.30	0.695	No
1212	12.12	0.72	0.13	0.59	0.97	0.569	1.04	0.545	1.05	1.30	0.695	No
1213	12.13	0.72	0.13	0.59	0.97	0.569	1.04	0.545	1.05	1.30	0.696	No
1214	12.14	0.72	0.13	0.59	0.97	0.569	1.04	0.545	1.05	1.30	0.697	No
1215	12.15	0.72	0.13	0.60	0.97	0.569	1.04	0.545	1.05	1.30	0.698	No
1216	12.16	0.73	0.13	0.60	0.97	0.569	1.04	0.546	1.05	1.30	0.698	No
1217	12.17	0.73	0.13	0.60	0.97	0.569	1.04	0.546	1.05	1.30	0.699	No
1218	12.18	0.73	0.13	0.60	0.97	0.570	1.04	0.546	1.05	1.30	0.699	No
1219	12.19	0.73	0.13	0.60	0.97	0.570	1.04	0.546	1.05	1.30	0.700	No
1220	12.20	0.73	0.13	0.60	0.97	0.570	1.04	0.546	1.05	1.30	0.700	No
1221	12.21	0.73	0.13	0.60	0.97	0.570	1.04	0.547	1.05	1.30	0.700	No
1222	12.22	0.73	0.13	0.60	0.97	0.570	1.04	0.547	1.05	1.30	0.701	No
1223	12.23	0.73	0.13	0.60	0.97	0.571	1.04	0.547	1.05	1.30	0.701	No
1224	12.24	0.73	0.13	0.60	0.97	0.571	1.04	0.547	1.05	1.30	0.701	No
1225	12.25	0.73	0.13	0.60	0.97	0.571	1.04	0.547	1.05	1.30	0.702	No
1226	12.26	0.73	0.13	0.60	0.97	0.571	1.04	0.547	1.05	1.30	0.702	No
1227	12.27	0.73	0.13	0.60	0.97	0.571	1.04	0.548	1.05	1.30	0.702	No
1228	12.28	0.73	0.13	0.60	0.97	0.571	1.04	0.548	1.05	1.30	0.703	No
1229	12.29	0.73	0.13	0.60	0.97	0.572	1.04	0.548	1.05	1.30	0.703	No
1230	12.30	0.73	0.13	0.60	0.97	0.572	1.04	0.548	1.05	1.30	0.703	No
1231	12.31	0.73	0.13	0.60	0.97	0.572	1.04	0.548	1.05	1.30	0.704	No
1232	12.32	0.73	0.13	0.60	0.97	0.572	1.04	0.548	1.05	1.30	0.704	No
1233	12.33	0.73	0.14	0.60	0.97	0.572	1.04	0.549	1.05	1.30	0.704	No
1234	12.34	0.73	0.14	0.60	0.97	0.573	1.04	0.549	1.05	1.30	0.705	No
1235	12.35	0.74	0.14	0.60	0.97	0.573	1.04	0.549	1.05	1.30	0.705	No
1236	12.36	0.74	0.14	0.60	0.97	0.573	1.04	0.549	1.05	1.30	0.705	No
1237	12.37	0.74	0.14	0.60	0.97	0.573	1.04	0.549	1.05	1.30	0.706	No
1238	12.38	0.74	0.14	0.60	0.97	0.573	1.04	0.549	1.05	1.30	0.706	No
1239	12.39	0.74	0.14	0.60	0.97	0.573	1.04	0.550	1.05	1.30	0.707	No
1240	12.40	0.74	0.14	0.60	0.97	0.574	1.04	0.550	1.05	1.30	0.707	No
1241	12.41	0.74	0.14	0.60	0.97	0.574	1.04	0.550	1.05	1.30	0.707	No
1242	12.42	0.74	0.14	0.60	0.97	0.574	1.04	0.550	1.05	1.30	0.708	No
1243	12.43	0.74	0.14	0.60	0.97	0.574	1.04	0.550	1.05	1.30	0.708	No
1244	12.44	0.74	0.14	0.60	0.97	0.574	1.04	0.551	1.05	1.30	0.708	No
1245	12.45	0.74	0.14	0.60	0.97	0.575	1.04	0.551	1.05	1.30	0.709	No
1246	12.46	0.74	0.14	0.60	0.97	0.575	1.04	0.551	1.05	1.30	0.709	No
1247	12.47	0.74	0.14	0.60	0.97	0.575	1.04	0.551	1.05	1.30	0.709	No
1248	12.48	0.74	0.14	0.60	0.97	0.575	1.04	0.551	1.05	1.30	0.710	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1249	12.49	0.74	0.14	0.60	0.97	0.575	1.04	0.551	1.05	1.30	0.710	No
1250	12.50	0.74	0.14	0.60	0.97	0.575	1.04	0.552	1.05	1.30	0.710	No
1251	12.51	0.74	0.14	0.60	0.97	0.576	1.04	0.552	1.05	1.30	0.711	No
1252	12.52	0.74	0.14	0.60	0.97	0.576	1.04	0.552	1.05	1.30	0.711	No
1253	12.53	0.75	0.14	0.60	0.97	0.576	1.04	0.552	1.05	1.30	0.711	No
1254	12.54	0.75	0.14	0.60	0.97	0.576	1.04	0.552	1.05	1.30	0.711	No
1255	12.55	0.75	0.14	0.60	0.97	0.576	1.04	0.552	1.05	1.30	0.712	No
1256	12.56	0.75	0.14	0.60	0.97	0.577	1.04	0.553	1.05	1.30	0.712	No
1257	12.57	0.75	0.14	0.60	0.97	0.577	1.04	0.553	1.04	1.30	0.712	No
1258	12.58	0.75	0.14	0.60	0.97	0.577	1.04	0.553	1.04	1.30	0.713	No
1259	12.59	0.75	0.14	0.61	0.97	0.577	1.04	0.553	1.04	1.30	0.713	No
1260	12.60	0.75	0.14	0.61	0.97	0.577	1.04	0.553	1.04	1.30	0.713	No
1261	12.61	0.75	0.14	0.61	0.97	0.577	1.04	0.553	1.04	1.30	0.713	No
1262	12.62	0.75	0.14	0.61	0.97	0.578	1.04	0.554	1.04	1.30	0.714	No
1263	12.63	0.75	0.14	0.61	0.97	0.578	1.04	0.554	1.04	1.30	0.714	No
1264	12.64	0.75	0.14	0.61	0.97	0.578	1.04	0.554	1.04	1.30	0.714	No
1265	12.65	0.75	0.15	0.61	0.97	0.578	1.04	0.554	1.04	1.30	0.714	No
1266	12.66	0.75	0.15	0.61	0.97	0.578	1.04	0.554	1.04	1.30	0.715	No
1267	12.67	0.75	0.15	0.61	0.97	0.579	1.04	0.555	1.04	1.30	0.715	No
1268	12.68	0.75	0.15	0.61	0.97	0.579	1.04	0.555	1.04	1.30	0.715	No
1269	12.69	0.75	0.15	0.61	0.97	0.579	1.04	0.555	1.04	1.30	0.715	No
1270	12.70	0.75	0.15	0.61	0.97	0.579	1.04	0.555	1.04	1.30	0.716	No
1271	12.71	0.75	0.15	0.61	0.97	0.579	1.04	0.555	1.04	1.30	0.716	No
1272	12.72	0.76	0.15	0.61	0.97	0.579	1.04	0.555	1.04	1.30	0.716	No
1273	12.73	0.76	0.15	0.61	0.97	0.580	1.04	0.556	1.04	1.30	0.716	No
1274	12.74	0.76	0.15	0.61	0.97	0.580	1.04	0.556	1.04	1.30	0.717	No
1275	12.75	0.76	0.15	0.61	0.97	0.580	1.04	0.556	1.04	1.30	0.717	No
1276	12.76	0.76	0.15	0.61	0.97	0.580	1.04	0.556	1.04	1.30	0.717	No
1277	12.77	0.76	0.15	0.61	0.97	0.580	1.04	0.556	1.04	1.30	0.717	No
1278	12.78	0.76	0.15	0.61	0.97	0.581	1.04	0.556	1.04	1.30	0.717	No
1279	12.79	0.76	0.15	0.61	0.97	0.581	1.04	0.557	1.04	1.30	0.718	No
1280	12.80	0.76	0.15	0.61	0.97	0.581	1.04	0.557	1.04	1.30	0.718	No
1281	12.81	0.76	0.15	0.61	0.97	0.581	1.04	0.557	1.04	1.30	0.718	No
1282	12.82	0.76	0.15	0.61	0.97	0.581	1.04	0.557	1.04	1.30	0.718	No
1283	12.83	0.76	0.15	0.61	0.97	0.581	1.04	0.557	1.04	1.30	0.719	No
1284	12.84	0.76	0.15	0.61	0.97	0.582	1.04	0.557	1.04	1.30	0.719	No
1285	12.85	0.76	0.15	0.61	0.97	0.582	1.04	0.558	1.04	1.30	0.719	No
1286	12.86	0.76	0.15	0.61	0.97	0.582	1.04	0.558	1.04	1.30	0.719	No
1287	12.87	0.76	0.15	0.61	0.97	0.582	1.04	0.558	1.04	1.30	0.720	No
1288	12.88	0.76	0.15	0.61	0.97	0.582	1.04	0.558	1.04	1.30	0.720	No
1289	12.89	0.76	0.15	0.61	0.97	0.582	1.04	0.558	1.04	1.30	0.720	No
1290	12.90	0.76	0.15	0.61	0.97	0.583	1.04	0.558	1.04	1.30	0.720	No
1291	12.91	0.76	0.15	0.61	0.97	0.583	1.04	0.559	1.04	1.30	0.721	No
1292	12.92	0.77	0.15	0.61	0.97	0.583	1.04	0.559	1.04	1.30	0.721	No
1293	12.93	0.77	0.15	0.61	0.97	0.583	1.04	0.559	1.04	1.30	0.721	No
1294	12.94	0.77	0.15	0.61	0.97	0.583	1.04	0.559	1.04	1.30	0.721	No
1295	12.95	0.77	0.15	0.61	0.97	0.584	1.04	0.559	1.04	1.30	0.722	No
1296	12.96	0.77	0.15	0.61	0.97	0.584	1.04	0.559	1.04	1.30	0.722	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
1297	12.97	0.77	0.16	0.61	0.97	0.584	1.04	0.560	1.04	1.30	0.722	No
1298	12.98	0.77	0.16	0.61	0.97	0.584	1.04	0.560	1.04	1.30	0.722	No
1299	12.99	0.77	0.16	0.61	0.97	0.584	1.04	0.560	1.04	1.30	0.722	No
1300	13.00	0.77	0.16	0.61	0.97	0.584	1.04	0.560	1.04	1.30	0.723	No
1301	13.01	0.77	0.16	0.61	0.97	0.585	1.04	0.560	1.04	1.30	0.723	No
1302	13.02	0.77	0.16	0.61	0.97	0.585	1.04	0.560	1.04	1.30	0.723	No
1303	13.03	0.77	0.16	0.61	0.97	0.585	1.04	0.561	1.04	1.30	0.723	No
1304	13.04	0.77	0.16	0.61	0.97	0.585	1.04	0.561	1.04	1.30	0.724	No
1305	13.05	0.77	0.16	0.61	0.97	0.585	1.04	0.561	1.04	1.30	0.724	No
1306	13.06	0.77	0.16	0.61	0.97	0.585	1.04	0.561	1.04	1.30	0.724	No
1307	13.07	0.77	0.16	0.62	0.97	0.586	1.04	0.561	1.04	1.30	0.725	No
1308	13.08	0.77	0.16	0.62	0.97	0.586	1.04	0.562	1.04	1.30	0.725	No
1309	13.09	0.77	0.16	0.62	0.97	0.586	1.04	0.562	1.04	1.30	0.725	No
1310	13.10	0.77	0.16	0.62	0.97	0.586	1.04	0.562	1.04	1.30	0.726	No
1311	13.11	0.78	0.16	0.62	0.97	0.586	1.04	0.562	1.04	1.30	0.726	No
1312	13.12	0.78	0.16	0.62	0.97	0.587	1.04	0.562	1.04	1.30	0.726	No
1313	13.13	0.78	0.16	0.62	0.97	0.587	1.04	0.562	1.04	1.30	0.727	No
1314	13.14	0.78	0.16	0.62	0.97	0.587	1.04	0.563	1.04	1.30	0.727	No
1315	13.15	0.78	0.16	0.62	0.97	0.587	1.04	0.563	1.04	1.30	0.727	No
1316	13.16	0.78	0.16	0.62	0.97	0.587	1.04	0.563	1.04	1.30	0.728	No
1317	13.17	0.78	0.16	0.62	0.97	0.587	1.04	0.563	1.04	1.30	0.728	No
1318	13.18	0.78	0.16	0.62	0.97	0.588	1.04	0.563	1.04	1.30	0.728	No
1319	13.19	0.78	0.16	0.62	0.97	0.588	1.04	0.563	1.04	1.30	0.729	No
1320	13.20	0.78	0.16	0.62	0.97	0.588	1.04	0.564	1.04	1.30	0.729	No
1321	13.21	0.78	0.16	0.62	0.97	0.588	1.04	0.564	1.04	1.30	0.729	No
1322	13.22	0.78	0.16	0.62	0.97	0.588	1.04	0.564	1.04	1.30	0.730	No
1323	13.23	0.78	0.16	0.62	0.97	0.589	1.04	0.564	1.04	1.30	0.730	No
1324	13.24	0.78	0.16	0.62	0.97	0.589	1.04	0.564	1.04	1.30	0.730	No
1325	13.25	0.78	0.16	0.62	0.97	0.589	1.04	0.564	1.04	1.30	0.730	No
1326	13.26	0.78	0.16	0.62	0.97	0.589	1.04	0.565	1.04	1.30	0.731	No
1327	13.27	0.78	0.16	0.62	0.97	0.589	1.04	0.565	1.04	1.30	0.731	No
1328	13.28	0.78	0.16	0.62	0.97	0.589	1.04	0.565	1.04	1.30	0.731	No
1329	13.29	0.78	0.17	0.62	0.97	0.590	1.04	0.565	1.04	1.30	0.732	No
1330	13.30	0.78	0.17	0.62	0.97	0.590	1.04	0.565	1.04	1.30	0.732	No
1331	13.31	0.78	0.17	0.62	0.97	0.590	1.04	0.566	1.04	1.30	0.732	No
1332	13.32	0.79	0.17	0.62	0.97	0.590	1.04	0.566	1.04	1.30	0.732	No
1333	13.33	0.79	0.17	0.62	0.97	0.590	1.04	0.566	1.04	1.30	0.733	No
1334	13.34	0.79	0.17	0.62	0.97	0.591	1.04	0.566	1.04	1.30	0.733	No
1335	13.35	0.79	0.17	0.62	0.97	0.591	1.04	0.566	1.04	1.30	0.733	No
1336	13.36	0.79	0.17	0.62	0.97	0.591	1.04	0.566	1.04	1.30	0.733	No
1337	13.37	0.79	0.17	0.62	0.97	0.591	1.04	0.567	1.04	1.30	0.734	No
1338	13.38	0.79	0.17	0.62	0.97	0.591	1.04	0.567	1.04	1.30	0.734	No
1339	13.39	0.79	0.17	0.62	0.97	0.591	1.04	0.567	1.04	1.30	0.734	No
1340	13.40	0.79	0.17	0.62	0.97	0.592	1.04	0.567	1.04	1.30	0.734	No
1341	13.41	0.79	0.17	0.62	0.97	0.592	1.04	0.567	1.04	1.30	0.734	No
1342	13.42	0.79	0.17	0.62	0.97	0.592	1.04	0.567	1.04	1.30	0.734	No
1343	13.43	0.79	0.17	0.62	0.97	0.592	1.04	0.568	1.04	1.30	0.735	No
1344	13.44	0.79	0.17	0.62	0.97	0.592	1.04	0.568	1.04	1.30	0.735	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1345	13.45	0.79	0.17	0.62	0.97	0.593	1.04	0.568	1.04	1.30	0.735	No
1346	13.46	0.79	0.17	0.62	0.97	0.593	1.04	0.568	1.04	1.30	0.735	No
1347	13.47	0.79	0.17	0.62	0.97	0.593	1.04	0.568	1.04	1.30	0.735	No
1348	13.48	0.79	0.17	0.62	0.97	0.593	1.04	0.568	1.04	1.30	0.735	No
1349	13.49	0.79	0.17	0.62	0.97	0.593	1.04	0.569	1.04	1.30	0.735	No
1350	13.50	0.79	0.17	0.62	0.97	0.593	1.04	0.569	1.04	1.30	0.736	No
1351	13.51	0.79	0.17	0.62	0.97	0.594	1.04	0.569	1.04	1.30	0.736	No
1352	13.52	0.79	0.17	0.62	0.97	0.594	1.04	0.569	1.04	1.30	0.736	No
1353	13.53	0.79	0.17	0.62	0.97	0.594	1.04	0.569	1.04	1.30	0.736	No
1354	13.54	0.80	0.17	0.62	0.97	0.594	1.04	0.569	1.04	1.30	0.736	No
1355	13.55	0.80	0.17	0.62	0.97	0.594	1.04	0.570	1.04	1.30	0.736	No
1356	13.56	0.80	0.17	0.62	0.97	0.594	1.04	0.570	1.04	1.30	0.736	No
1357	13.57	0.80	0.17	0.62	0.97	0.595	1.04	0.570	1.04	1.30	0.737	No
1358	13.58	0.80	0.17	0.62	0.97	0.595	1.04	0.570	1.04	1.30	0.737	No
1359	13.59	0.80	0.17	0.62	0.97	0.595	1.04	0.570	1.04	1.30	0.737	No
1360	13.60	0.80	0.17	0.62	0.97	0.595	1.04	0.570	1.04	1.30	0.737	No
1361	13.61	0.80	0.18	0.62	0.97	0.595	1.04	0.571	1.04	1.30	0.738	No
1362	13.62	0.80	0.18	0.62	0.97	0.596	1.04	0.571	1.04	1.30	0.738	No
1363	13.63	0.80	0.18	0.62	0.97	0.596	1.04	0.571	1.04	1.30	0.738	No
1364	13.64	0.80	0.18	0.62	0.97	0.596	1.04	0.571	1.04	1.30	0.738	No
1365	13.65	0.80	0.18	0.62	0.97	0.596	1.04	0.571	1.04	1.30	0.739	No
1366	13.66	0.80	0.18	0.62	0.97	0.596	1.04	0.571	1.04	1.30	0.739	No
1367	13.67	0.80	0.18	0.63	0.97	0.596	1.04	0.572	1.04	1.30	0.739	No
1368	13.68	0.80	0.18	0.63	0.97	0.597	1.04	0.572	1.04	1.30	0.739	No
1369	13.69	0.80	0.18	0.63	0.97	0.597	1.04	0.572	1.04	1.30	0.740	No
1370	13.70	0.80	0.18	0.63	0.97	0.597	1.04	0.572	1.04	1.30	0.740	No
1371	13.71	0.80	0.18	0.63	0.97	0.597	1.04	0.572	1.04	1.30	0.740	No
1372	13.72	0.80	0.18	0.63	0.97	0.597	1.04	0.572	1.04	1.30	0.740	No
1373	13.73	0.81	0.18	0.63	0.97	0.597	1.04	0.573	1.04	1.30	0.740	No
1374	13.74	0.81	0.18	0.63	0.97	0.598	1.04	0.573	1.04	1.30	0.741	No
1375	13.75	0.81	0.18	0.63	0.97	0.598	1.04	0.573	1.04	1.30	0.741	No
1376	13.76	0.81	0.18	0.63	0.97	0.598	1.04	0.573	1.04	1.30	0.741	No
1377	13.77	0.81	0.18	0.63	0.97	0.598	1.04	0.573	1.04	1.30	0.741	No
1378	13.78	0.81	0.18	0.63	0.97	0.598	1.04	0.573	1.04	1.30	0.741	No
1379	13.79	0.81	0.18	0.63	0.97	0.598	1.04	0.574	1.04	1.30	0.741	No
1380	13.80	0.81	0.18	0.63	0.97	0.599	1.04	0.574	1.04	1.30	0.742	No
1381	13.81	0.81	0.18	0.63	0.97	0.599	1.04	0.574	1.04	1.30	0.742	No
1382	13.82	0.81	0.18	0.63	0.97	0.599	1.04	0.574	1.04	1.30	0.742	No
1383	13.83	0.81	0.18	0.63	0.97	0.599	1.04	0.574	1.04	1.30	0.742	No
1384	13.84	0.81	0.18	0.63	0.97	0.599	1.04	0.574	1.04	1.30	0.743	No
1385	13.85	0.81	0.18	0.63	0.97	0.599	1.04	0.574	1.04	1.30	0.743	No
1386	13.86	0.81	0.18	0.63	0.97	0.600	1.04	0.575	1.04	1.30	0.743	No
1387	13.87	0.81	0.18	0.63	0.97	0.600	1.04	0.575	1.04	1.30	0.744	No
1388	13.88	0.81	0.18	0.63	0.97	0.600	1.04	0.575	1.04	1.30	0.744	No
1389	13.89	0.81	0.18	0.63	0.97	0.600	1.04	0.575	1.04	1.30	0.744	No
1390	13.90	0.81	0.18	0.63	0.97	0.600	1.04	0.575	1.04	1.30	0.744	No
1391	13.91	0.81	0.18	0.63	0.97	0.600	1.04	0.575	1.04	1.30	0.745	No
1392	13.92	0.81	0.18	0.63	0.97	0.601	1.04	0.576	1.04	1.30	0.745	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1393	13.93	0.82	0.19	0.63	0.97	0.601	1.04	0.576	1.04	1.30	0.745	No
1394	13.94	0.82	0.19	0.63	0.97	0.601	1.04	0.576	1.04	1.30	0.746	No
1395	13.95	0.82	0.19	0.63	0.97	0.601	1.04	0.576	1.04	1.30	0.746	No
1396	13.96	0.82	0.19	0.63	0.97	0.601	1.04	0.576	1.04	1.30	0.746	No
1397	13.97	0.82	0.19	0.63	0.97	0.601	1.04	0.576	1.04	1.30	0.746	No
1398	13.98	0.82	0.19	0.63	0.97	0.602	1.04	0.577	1.04	1.30	0.747	No
1399	13.99	0.82	0.19	0.63	0.97	0.602	1.04	0.577	1.04	1.30	0.747	No
1400	14.00	0.82	0.19	0.63	0.97	0.602	1.04	0.577	1.04	1.30	0.747	No
1401	14.01	0.82	0.19	0.63	0.97	0.602	1.04	0.577	1.04	1.30	0.747	No
1402	14.02	0.82	0.19	0.63	0.97	0.602	1.04	0.577	1.04	1.30	0.748	No
1403	14.03	0.82	0.19	0.63	0.97	0.602	1.04	0.577	1.04	1.30	0.748	No
1404	14.04	0.82	0.19	0.63	0.97	0.603	1.04	0.578	1.04	1.30	0.748	No
1405	14.05	0.82	0.19	0.63	0.96	0.603	1.04	0.578	1.04	1.30	0.748	No
1406	14.06	0.82	0.19	0.63	0.96	0.603	1.04	0.578	1.04	1.30	0.749	No
1407	14.07	0.82	0.19	0.63	0.96	0.603	1.04	0.578	1.04	1.30	0.749	No
1408	14.08	0.82	0.19	0.63	0.96	0.603	1.04	0.578	1.04	1.30	0.749	No
1409	14.09	0.82	0.19	0.63	0.96	0.603	1.04	0.578	1.04	1.30	0.749	No
1410	14.10	0.82	0.19	0.63	0.96	0.604	1.04	0.578	1.04	1.30	0.749	No
1411	14.11	0.82	0.19	0.63	0.96	0.604	1.04	0.579	1.04	1.30	0.749	No
1412	14.12	0.82	0.19	0.63	0.96	0.604	1.04	0.579	1.04	1.30	0.750	No
1413	14.13	0.83	0.19	0.63	0.96	0.604	1.04	0.579	1.04	1.30	0.750	No
1414	14.14	0.83	0.19	0.63	0.96	0.604	1.04	0.579	1.04	1.30	0.750	No
1415	14.15	0.83	0.19	0.63	0.96	0.604	1.04	0.579	1.04	1.30	0.750	No
1416	14.16	0.83	0.19	0.63	0.96	0.604	1.04	0.579	1.04	1.30	0.750	No
1417	14.17	0.83	0.19	0.63	0.96	0.605	1.04	0.580	1.04	1.30	0.750	No
1418	14.18	0.83	0.19	0.63	0.96	0.605	1.04	0.580	1.04	1.30	0.750	No
1419	14.19	0.83	0.19	0.64	0.96	0.605	1.04	0.580	1.04	1.30	0.750	No
1420	14.20	0.83	0.19	0.64	0.96	0.605	1.04	0.580	1.04	1.30	0.751	No
1421	14.21	0.83	0.19	0.64	0.96	0.605	1.04	0.580	1.04	1.30	0.751	No
1422	14.22	0.83	0.19	0.64	0.96	0.605	1.04	0.580	1.04	1.30	0.751	No
1423	14.23	0.83	0.19	0.64	0.96	0.606	1.04	0.580	1.04	1.30	0.751	No
1424	14.24	0.83	0.19	0.64	0.96	0.606	1.04	0.581	1.04	1.30	0.751	No
1425	14.25	0.83	0.20	0.64	0.96	0.606	1.04	0.581	1.04	1.30	0.751	No
1426	14.26	0.83	0.20	0.64	0.96	0.606	1.04	0.581	1.04	1.30	0.751	No
1427	14.27	0.83	0.20	0.64	0.96	0.606	1.04	0.581	1.04	1.30	0.751	No
1428	14.28	0.83	0.20	0.64	0.96	0.606	1.04	0.581	1.04	1.30	0.751	No
1429	14.29	0.83	0.20	0.64	0.96	0.607	1.04	0.581	1.04	1.30	0.751	No
1430	14.30	0.83	0.20	0.64	0.96	0.607	1.04	0.581	1.04	1.30	0.752	No
1431	14.31	0.83	0.20	0.64	0.96	0.607	1.04	0.582	1.04	1.30	0.752	No
1432	14.32	0.84	0.20	0.64	0.96	0.607	1.04	0.582	1.04	1.30	0.752	No
1433	14.33	0.84	0.20	0.64	0.96	0.607	1.04	0.582	1.04	1.30	0.752	No
1434	14.34	0.84	0.20	0.64	0.96	0.607	1.04	0.582	1.04	1.30	0.752	No
1435	14.35	0.84	0.20	0.64	0.96	0.607	1.04	0.582	1.04	1.30	0.752	No
1436	14.36	0.84	0.20	0.64	0.96	0.608	1.04	0.582	1.04	1.30	0.752	No
1437	14.37	0.84	0.20	0.64	0.96	0.608	1.04	0.582	1.04	1.30	0.752	No
1438	14.38	0.84	0.20	0.64	0.96	0.608	1.04	0.583	1.04	1.30	0.752	No
1439	14.39	0.84	0.20	0.64	0.96	0.608	1.04	0.583	1.04	1.30	0.753	No
1440	14.40	0.84	0.20	0.64	0.96	0.608	1.04	0.583	1.04	1.30	0.753	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
1441	14.41	0.84	0.20	0.64	0.96	0.608	1.04	0.583	1.04	1.30	0.753	No
1442	14.42	0.84	0.20	0.64	0.96	0.608	1.04	0.583	1.04	1.30	0.753	No
1443	14.43	0.84	0.20	0.64	0.96	0.609	1.04	0.583	1.04	1.30	0.753	No
1444	14.44	0.84	0.20	0.64	0.96	0.609	1.04	0.583	1.04	1.30	0.754	No
1445	14.45	0.84	0.20	0.64	0.96	0.609	1.04	0.584	1.04	1.30	0.754	No
1446	14.46	0.84	0.20	0.64	0.96	0.609	1.04	0.584	1.04	1.30	0.754	No
1447	14.47	0.84	0.20	0.64	0.96	0.609	1.04	0.584	1.04	1.30	0.754	No
1448	14.48	0.84	0.20	0.64	0.96	0.609	1.04	0.584	1.04	1.30	0.755	No
1449	14.49	0.84	0.20	0.64	0.96	0.609	1.04	0.584	1.04	1.30	0.755	No
1450	14.50	0.85	0.20	0.64	0.96	0.610	1.04	0.584	1.04	1.30	0.755	No
1451	14.51	0.85	0.20	0.64	0.96	0.610	1.04	0.584	1.04	1.30	0.755	No
1452	14.52	0.85	0.20	0.64	0.96	0.610	1.04	0.585	1.04	1.30	0.756	No
1453	14.53	0.85	0.20	0.64	0.96	0.610	1.04	0.585	1.04	1.30	0.756	No
1454	14.54	0.85	0.20	0.64	0.96	0.610	1.04	0.585	1.04	1.30	0.756	No
1455	14.55	0.85	0.20	0.64	0.96	0.610	1.04	0.585	1.04	1.30	0.757	No
1456	14.56	0.85	0.20	0.64	0.96	0.611	1.04	0.585	1.04	1.30	0.757	No
1457	14.57	0.85	0.20	0.64	0.96	0.611	1.04	0.585	1.04	1.30	0.758	No
1458	14.58	0.85	0.21	0.64	0.96	0.611	1.04	0.585	1.04	1.30	0.758	No
1459	14.59	0.85	0.21	0.64	0.96	0.611	1.04	0.586	1.04	1.30	0.758	No
1460	14.60	0.85	0.21	0.64	0.96	0.611	1.04	0.586	1.04	1.30	0.759	No
1461	14.61	0.85	0.21	0.65	0.96	0.611	1.04	0.586	1.04	1.30	0.759	No
1462	14.62	0.85	0.21	0.65	0.96	0.611	1.04	0.586	1.04	1.30	0.759	No
1463	14.63	0.85	0.21	0.65	0.96	0.612	1.04	0.586	1.04	1.30	0.759	No
1464	14.64	0.85	0.21	0.65	0.96	0.612	1.04	0.586	1.04	1.30	0.760	No
1465	14.65	0.85	0.21	0.65	0.96	0.612	1.04	0.586	1.04	1.30	0.760	No
1466	14.66	0.85	0.21	0.65	0.96	0.612	1.04	0.587	1.04	1.30	0.760	No
1467	14.67	0.85	0.21	0.65	0.96	0.612	1.04	0.587	1.04	1.30	0.761	No
1468	14.68	0.86	0.21	0.65	0.96	0.612	1.04	0.587	1.04	1.30	0.761	No
1469	14.69	0.86	0.21	0.65	0.96	0.612	1.04	0.587	1.04	1.30	0.761	No
1470	14.70	0.86	0.21	0.65	0.96	0.613	1.04	0.587	1.04	1.30	0.761	No
1471	14.71	0.86	0.21	0.65	0.96	0.613	1.04	0.587	1.04	1.30	0.761	No
1472	14.72	0.86	0.21	0.65	0.96	0.613	1.04	0.587	1.04	1.30	0.761	No
1473	14.73	0.86	0.21	0.65	0.96	0.613	1.04	0.588	1.04	1.30	0.762	No
1474	14.74	0.86	0.21	0.65	0.96	0.613	1.04	0.588	1.04	1.30	0.762	No
1475	14.75	0.86	0.21	0.65	0.96	0.613	1.04	0.588	1.04	1.30	0.762	No
1476	14.76	0.86	0.21	0.65	0.96	0.613	1.04	0.588	1.04	1.30	0.762	No
1477	14.77	0.86	0.21	0.65	0.96	0.614	1.04	0.588	1.04	1.30	0.762	No
1478	14.78	0.86	0.21	0.65	0.96	0.614	1.04	0.588	1.04	1.30	0.762	No
1479	14.79	0.86	0.21	0.65	0.96	0.614	1.04	0.588	1.04	1.30	0.763	No
1480	14.80	0.86	0.21	0.65	0.96	0.614	1.04	0.589	1.04	1.30	0.763	No
1481	14.81	0.86	0.21	0.65	0.96	0.614	1.04	0.589	1.04	1.30	0.763	No
1482	14.82	0.86	0.21	0.65	0.96	0.614	1.04	0.589	1.04	1.30	0.763	No
1483	14.83	0.86	0.21	0.65	0.96	0.614	1.04	0.589	1.04	1.30	0.763	No
1484	14.84	0.86	0.21	0.65	0.96	0.615	1.04	0.589	1.04	1.30	0.764	No
1485	14.85	0.86	0.21	0.65	0.96	0.615	1.04	0.589	1.04	1.30	0.764	No
1486	14.86	0.86	0.21	0.65	0.96	0.615	1.04	0.589	1.04	1.30	0.764	No
1487	14.87	0.87	0.21	0.65	0.96	0.615	1.04	0.590	1.04	1.30	0.764	No
1488	14.88	0.87	0.21	0.65	0.96	0.615	1.04	0.590	1.04	1.30	0.764	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1489	14.89	0.87	0.21	0.65	0.96	0.615	1.04	0.590	1.04	1.30	0.764	No
1490	14.90	0.87	0.22	0.65	0.96	0.616	1.04	0.590	1.04	1.30	0.764	No
1491	14.91	0.87	0.22	0.65	0.96	0.616	1.04	0.590	1.04	1.30	0.765	No
1492	14.92	0.87	0.22	0.65	0.96	0.616	1.04	0.590	1.04	1.30	0.765	No
1493	14.93	0.87	0.22	0.65	0.96	0.616	1.04	0.590	1.04	1.30	0.765	No
1494	14.94	0.87	0.22	0.65	0.96	0.616	1.04	0.590	1.04	1.30	0.765	No
1495	14.95	0.87	0.22	0.65	0.96	0.616	1.04	0.591	1.04	1.30	0.765	No
1496	14.96	0.87	0.22	0.65	0.96	0.616	1.04	0.591	1.04	1.30	0.765	No
1497	14.97	0.87	0.22	0.65	0.96	0.617	1.04	0.591	1.04	1.30	0.765	No
1498	14.98	0.87	0.22	0.65	0.96	0.617	1.04	0.591	1.04	1.30	0.765	No
1499	14.99	0.87	0.22	0.65	0.96	0.617	1.04	0.591	1.04	1.30	0.766	No
1500	15.00	0.87	0.22	0.65	0.96	0.617	1.04	0.591	1.04	1.30	0.766	No
1501	15.01	0.87	0.22	0.65	0.96	0.617	1.04	0.591	1.04	1.30	0.766	No
1502	15.02	0.87	0.22	0.65	0.96	0.617	1.04	0.592	1.04	1.30	0.766	No
1503	15.03	0.87	0.22	0.65	0.96	0.617	1.04	0.592	1.04	1.30	0.766	No
1504	15.04	0.87	0.22	0.65	0.96	0.617	1.04	0.592	1.04	1.30	0.766	No
1505	15.05	0.88	0.22	0.66	0.96	0.618	1.04	0.592	1.04	1.30	0.767	No
1506	15.06	0.88	0.22	0.66	0.96	0.618	1.04	0.592	1.04	1.30	0.767	No
1507	15.07	0.88	0.22	0.66	0.96	0.618	1.04	0.592	1.04	1.30	0.767	No
1508	15.08	0.88	0.22	0.66	0.96	0.618	1.04	0.592	1.04	1.30	0.768	No
1509	15.09	0.88	0.22	0.66	0.96	0.618	1.04	0.593	1.04	1.30	0.768	No
1510	15.10	0.88	0.22	0.66	0.96	0.618	1.04	0.593	1.04	1.30	0.768	No
1511	15.11	0.88	0.22	0.66	0.96	0.618	1.04	0.593	1.04	1.30	0.768	No
1512	15.12	0.88	0.22	0.66	0.96	0.619	1.04	0.593	1.04	1.30	0.769	No
1513	15.13	0.88	0.22	0.66	0.96	0.619	1.04	0.593	1.04	1.30	0.769	No
1514	15.14	0.88	0.22	0.66	0.96	0.619	1.04	0.593	1.04	1.30	0.769	No
1515	15.15	0.88	0.22	0.66	0.96	0.619	1.04	0.593	1.04	1.30	0.769	No
1516	15.16	0.88	0.22	0.66	0.96	0.619	1.04	0.593	1.04	1.30	0.769	No
1517	15.17	0.88	0.22	0.66	0.96	0.619	1.04	0.594	1.04	1.30	0.769	No
1518	15.18	0.88	0.22	0.66	0.96	0.619	1.04	0.594	1.04	1.30	0.770	No
1519	15.19	0.88	0.22	0.66	0.96	0.620	1.04	0.594	1.04	1.30	0.770	No
1520	15.20	0.88	0.22	0.66	0.96	0.620	1.04	0.594	1.04	1.30	0.770	No
1521	15.21	0.88	0.22	0.66	0.96	0.620	1.04	0.594	1.04	1.30	0.770	No
1522	15.22	0.88	0.23	0.66	0.96	0.620	1.04	0.594	1.04	1.30	0.770	No
1523	15.23	0.88	0.23	0.66	0.96	0.620	1.04	0.594	1.04	1.30	0.770	No
1524	15.24	0.89	0.23	0.66	0.96	0.620	1.04	0.595	1.04	1.30	0.770	No
1525	15.25	0.89	0.23	0.66	0.96	0.620	1.04	0.595	1.04	1.30	0.770	No
1526	15.26	0.89	0.23	0.66	0.96	0.621	1.04	0.595	1.04	1.30	0.770	No
1527	15.27	0.89	0.23	0.66	0.96	0.621	1.04	0.595	1.04	1.30	0.770	No
1528	15.28	0.89	0.23	0.66	0.96	0.621	1.04	0.595	1.04	1.30	0.770	No
1529	15.29	0.89	0.23	0.66	0.96	0.621	1.04	0.595	1.04	1.30	0.770	No
1530	15.30	0.89	0.23	0.66	0.96	0.621	1.04	0.595	1.04	1.30	0.770	No
1531	15.31	0.89	0.23	0.66	0.96	0.621	1.04	0.595	1.04	1.30	0.770	No
1532	15.32	0.89	0.23	0.66	0.96	0.621	1.04	0.596	1.04	1.30	0.770	No
1533	15.33	0.89	0.23	0.66	0.96	0.621	1.04	0.596	1.04	1.30	0.770	No
1534	15.34	0.89	0.23	0.66	0.96	0.622	1.04	0.596	1.04	1.30	0.770	No
1535	15.35	0.89	0.23	0.66	0.96	0.622	1.04	0.596	1.04	1.30	0.770	No
1536	15.36	0.89	0.23	0.66	0.96	0.622	1.04	0.596	1.04	1.30	0.770	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1537	15.37	0.89	0.23	0.66	0.96	0.622	1.04	0.596	1.04	1.30	0.770	No
1538	15.38	0.89	0.23	0.66	0.96	0.622	1.04	0.596	1.04	1.30	0.770	No
1539	15.39	0.89	0.23	0.66	0.96	0.622	1.04	0.596	1.04	1.30	0.770	No
1540	15.40	0.89	0.23	0.66	0.96	0.622	1.04	0.597	1.04	1.30	0.770	No
1541	15.41	0.90	0.23	0.66	0.96	0.623	1.04	0.597	1.04	1.30	0.770	No
1542	15.42	0.90	0.23	0.66	0.96	0.623	1.04	0.597	1.04	1.30	0.770	No
1543	15.43	0.90	0.23	0.66	0.96	0.623	1.04	0.597	1.04	1.30	0.770	No
1544	15.44	0.90	0.23	0.66	0.96	0.623	1.04	0.597	1.04	1.30	0.770	No
1545	15.45	0.90	0.23	0.67	0.96	0.623	1.04	0.597	1.04	1.30	0.770	No
1546	15.46	0.90	0.23	0.67	0.96	0.623	1.04	0.597	1.04	1.30	0.771	No
1547	15.47	0.90	0.23	0.67	0.96	0.623	1.04	0.597	1.04	1.30	0.771	No
1548	15.48	0.90	0.23	0.67	0.96	0.623	1.04	0.598	1.04	1.30	0.771	No
1549	15.49	0.90	0.23	0.67	0.96	0.624	1.04	0.598	1.04	1.30	0.772	No
1550	15.50	0.90	0.23	0.67	0.96	0.624	1.04	0.598	1.04	1.30	0.772	No
1551	15.51	0.90	0.23	0.67	0.96	0.624	1.04	0.598	1.04	1.30	0.773	No
1552	15.52	0.90	0.23	0.67	0.96	0.624	1.04	0.598	1.04	1.30	0.773	No
1553	15.53	0.90	0.23	0.67	0.96	0.624	1.04	0.598	1.04	1.30	0.773	No
1554	15.54	0.90	0.24	0.67	0.96	0.624	1.04	0.598	1.04	1.30	0.774	No
1555	15.55	0.90	0.24	0.67	0.96	0.624	1.04	0.598	1.04	1.30	0.774	No
1556	15.56	0.90	0.24	0.67	0.96	0.624	1.04	0.599	1.04	1.30	0.774	No
1557	15.57	0.90	0.24	0.67	0.96	0.625	1.04	0.599	1.04	1.30	0.775	No
1558	15.58	0.90	0.24	0.67	0.96	0.625	1.04	0.599	1.04	1.30	0.775	No
1559	15.59	0.91	0.24	0.67	0.96	0.625	1.04	0.599	1.04	1.30	0.776	No
1560	15.60	0.91	0.24	0.67	0.96	0.625	1.04	0.599	1.04	1.30	0.776	No
1561	15.61	0.91	0.24	0.67	0.96	0.625	1.04	0.599	1.04	1.30	0.776	No
1562	15.62	0.91	0.24	0.67	0.96	0.625	1.04	0.599	1.04	1.30	0.777	No
1563	15.63	0.91	0.24	0.67	0.96	0.625	1.04	0.599	1.04	1.30	0.777	No
1564	15.64	0.91	0.24	0.67	0.96	0.626	1.04	0.600	1.04	1.30	0.777	No
1565	15.65	0.91	0.24	0.67	0.96	0.626	1.04	0.600	1.04	1.30	0.777	No
1566	15.66	0.91	0.24	0.67	0.96	0.626	1.04	0.600	1.04	1.30	0.778	No
1567	15.67	0.91	0.24	0.67	0.96	0.626	1.04	0.600	1.04	1.30	0.778	No
1568	15.68	0.91	0.24	0.67	0.96	0.626	1.04	0.600	1.04	1.30	0.778	No
1569	15.69	0.91	0.24	0.67	0.96	0.626	1.04	0.600	1.04	1.30	0.778	No
1570	15.70	0.91	0.24	0.67	0.96	0.626	1.04	0.600	1.04	1.30	0.778	No
1571	15.71	0.91	0.24	0.67	0.96	0.626	1.04	0.600	1.04	1.30	0.779	No
1572	15.72	0.91	0.24	0.67	0.96	0.627	1.04	0.601	1.04	1.30	0.779	No
1573	15.73	0.91	0.24	0.67	0.96	0.627	1.04	0.601	1.04	1.30	0.779	No
1574	15.74	0.91	0.24	0.67	0.96	0.627	1.04	0.601	1.04	1.30	0.779	No
1575	15.75	0.91	0.24	0.67	0.96	0.627	1.04	0.601	1.04	1.30	0.780	No
1576	15.76	0.91	0.24	0.67	0.96	0.627	1.04	0.601	1.04	1.30	0.780	No
1577	15.77	0.92	0.24	0.67	0.96	0.627	1.04	0.601	1.04	1.30	0.780	No
1578	15.78	0.92	0.24	0.67	0.96	0.627	1.04	0.601	1.04	1.30	0.780	No
1579	15.79	0.92	0.24	0.67	0.96	0.627	1.04	0.601	1.04	1.30	0.780	No
1580	15.80	0.92	0.24	0.67	0.96	0.628	1.04	0.602	1.04	1.30	0.781	No
1581	15.81	0.92	0.24	0.67	0.96	0.628	1.04	0.602	1.04	1.30	0.781	No
1582	15.82	0.92	0.24	0.67	0.96	0.628	1.04	0.602	1.04	1.30	0.781	No
1583	15.83	0.92	0.24	0.67	0.96	0.628	1.04	0.602	1.04	1.30	0.781	No
1584	15.84	0.92	0.24	0.67	0.96	0.628	1.04	0.602	1.04	1.30	0.782	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1585	15.85	0.92	0.24	0.67	0.96	0.628	1.04	0.602	1.04	1.30	0.782	No
1586	15.86	0.92	0.25	0.68	0.96	0.628	1.04	0.602	1.04	1.30	0.782	No
1587	15.87	0.92	0.25	0.68	0.96	0.628	1.04	0.602	1.04	1.30	0.782	No
1588	15.88	0.92	0.25	0.68	0.96	0.629	1.04	0.603	1.04	1.30	0.782	No
1589	15.89	0.92	0.25	0.68	0.96	0.629	1.04	0.603	1.04	1.30	0.783	No
1590	15.90	0.92	0.25	0.68	0.96	0.629	1.04	0.603	1.04	1.30	0.783	No
1591	15.91	0.92	0.25	0.68	0.96	0.629	1.04	0.603	1.04	1.30	0.783	No
1592	15.92	0.92	0.25	0.68	0.96	0.629	1.04	0.603	1.04	1.30	0.783	No
1593	15.93	0.92	0.25	0.68	0.96	0.629	1.04	0.603	1.04	1.30	0.783	No
1594	15.94	0.92	0.25	0.68	0.96	0.629	1.04	0.603	1.04	1.30	0.784	No
1595	15.95	0.93	0.25	0.68	0.96	0.630	1.04	0.603	1.04	1.30	0.784	No
1596	15.96	0.93	0.25	0.68	0.96	0.630	1.04	0.604	1.04	1.30	0.784	No
1597	15.97	0.93	0.25	0.68	0.96	0.630	1.04	0.604	1.04	1.30	0.784	No
1598	15.98	0.93	0.25	0.68	0.96	0.630	1.04	0.604	1.04	1.30	0.785	No
1599	15.99	0.93	0.25	0.68	0.96	0.630	1.04	0.604	1.04	1.30	0.785	No
1600	16.00	0.93	0.25	0.68	0.96	0.630	1.04	0.604	1.04	1.30	0.785	No
1601	16.01	0.93	0.25	0.68	0.96	0.630	1.04	0.604	1.04	1.30	0.785	No
1602	16.02	0.93	0.25	0.68	0.96	0.630	1.04	0.604	1.04	1.30	0.785	No
1603	16.03	0.93	0.25	0.68	0.96	0.631	1.04	0.604	1.04	1.30	0.785	No
1604	16.04	0.93	0.25	0.68	0.96	0.631	1.04	0.604	1.04	1.30	0.786	No
1605	16.05	0.93	0.25	0.68	0.96	0.631	1.04	0.605	1.04	1.30	0.786	No
1606	16.06	0.93	0.25	0.68	0.96	0.631	1.04	0.605	1.04	1.30	0.786	No
1607	16.07	0.93	0.25	0.68	0.96	0.631	1.04	0.605	1.04	1.30	0.786	No
1608	16.08	0.93	0.25	0.68	0.96	0.631	1.04	0.605	1.04	1.30	0.786	No
1609	16.09	0.93	0.25	0.68	0.96	0.631	1.04	0.605	1.04	1.30	0.787	No
1610	16.10	0.93	0.25	0.68	0.96	0.631	1.04	0.605	1.04	1.30	0.787	No
1611	16.11	0.93	0.25	0.68	0.96	0.632	1.04	0.605	1.04	1.30	0.787	No
1612	16.12	0.93	0.25	0.68	0.96	0.632	1.04	0.605	1.04	1.30	0.787	No
1613	16.13	0.94	0.25	0.68	0.96	0.632	1.04	0.606	1.04	1.30	0.787	No
1614	16.14	0.94	0.25	0.68	0.96	0.632	1.04	0.606	1.04	1.30	0.787	No
1615	16.15	0.94	0.25	0.68	0.96	0.632	1.04	0.606	1.04	1.30	0.788	No
1616	16.16	0.94	0.25	0.68	0.96	0.632	1.04	0.606	1.04	1.30	0.788	No
1617	16.17	0.94	0.25	0.68	0.96	0.632	1.04	0.606	1.04	1.30	0.788	No
1618	16.18	0.94	0.26	0.68	0.96	0.632	1.04	0.606	1.04	1.30	0.788	No
1619	16.19	0.94	0.26	0.68	0.96	0.633	1.04	0.606	1.04	1.30	0.788	No
1620	16.20	0.94	0.26	0.68	0.96	0.633	1.04	0.606	1.04	1.30	0.789	No
1621	16.21	0.94	0.26	0.68	0.96	0.633	1.04	0.607	1.04	1.30	0.789	No
1622	16.22	0.94	0.26	0.68	0.96	0.633	1.04	0.607	1.04	1.30	0.789	No
1623	16.23	0.94	0.26	0.68	0.96	0.633	1.04	0.607	1.04	1.30	0.789	No
1624	16.24	0.94	0.26	0.68	0.96	0.633	1.04	0.607	1.04	1.30	0.789	No
1625	16.25	0.94	0.26	0.68	0.96	0.633	1.04	0.607	1.04	1.30	0.789	No
1626	16.26	0.94	0.26	0.68	0.96	0.633	1.04	0.607	1.04	1.30	0.789	No
1627	16.27	0.94	0.26	0.68	0.96	0.634	1.04	0.607	1.04	1.30	0.789	No
1628	16.28	0.94	0.26	0.68	0.96	0.634	1.04	0.607	1.04	1.30	0.789	No
1629	16.29	0.94	0.26	0.69	0.96	0.634	1.04	0.608	1.04	1.30	0.789	No
1630	16.30	0.94	0.26	0.69	0.96	0.634	1.04	0.608	1.04	1.30	0.789	No
1631	16.31	0.94	0.26	0.69	0.96	0.634	1.04	0.608	1.04	1.30	0.789	No
1632	16.32	0.95	0.26	0.69	0.96	0.634	1.04	0.608	1.04	1.30	0.789	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1633	16.33	0.95	0.26	0.69	0.96	0.634	1.04	0.608	1.04	1.30	0.790	No
1634	16.34	0.95	0.26	0.69	0.96	0.634	1.04	0.608	1.04	1.30	0.790	No
1635	16.35	0.95	0.26	0.69	0.96	0.635	1.04	0.608	1.04	1.30	0.790	No
1636	16.36	0.95	0.26	0.69	0.96	0.635	1.04	0.608	1.04	1.30	0.790	No
1637	16.37	0.95	0.26	0.69	0.96	0.635	1.04	0.608	1.04	1.30	0.789	No
1638	16.38	0.95	0.26	0.69	0.96	0.635	1.04	0.609	1.04	1.30	0.789	No
1639	16.39	0.95	0.26	0.69	0.96	0.635	1.04	0.609	1.04	1.30	0.789	No
1640	16.40	0.95	0.26	0.69	0.96	0.635	1.04	0.609	1.04	1.30	0.789	No
1641	16.41	0.95	0.26	0.69	0.96	0.635	1.04	0.609	1.04	1.30	0.789	No
1642	16.42	0.95	0.26	0.69	0.96	0.635	1.04	0.609	1.04	1.30	0.789	No
1643	16.43	0.95	0.26	0.69	0.96	0.636	1.04	0.609	1.04	1.30	0.789	No
1644	16.44	0.95	0.26	0.69	0.96	0.636	1.04	0.609	1.04	1.30	0.789	No
1645	16.45	0.95	0.26	0.69	0.96	0.636	1.04	0.609	1.04	1.30	0.789	No
1646	16.46	0.95	0.26	0.69	0.96	0.636	1.04	0.609	1.04	1.30	0.789	No
1647	16.47	0.95	0.26	0.69	0.96	0.636	1.04	0.610	1.04	1.30	0.789	No
1648	16.48	0.95	0.26	0.69	0.96	0.636	1.04	0.610	1.04	1.30	0.789	No
1649	16.49	0.96	0.26	0.69	0.96	0.636	1.04	0.610	1.04	1.30	0.789	No
1650	16.50	0.96	0.27	0.69	0.96	0.636	1.04	0.610	1.04	1.30	0.789	No
1651	16.51	0.96	0.27	0.69	0.96	0.636	1.04	0.610	1.04	1.30	0.789	No
1652	16.52	0.96	0.27	0.69	0.96	0.637	1.04	0.610	1.04	1.30	0.789	No
1653	16.53	0.96	0.27	0.69	0.96	0.637	1.04	0.610	1.04	1.30	0.789	No
1654	16.54	0.96	0.27	0.69	0.96	0.637	1.04	0.610	1.04	1.30	0.789	No
1655	16.55	0.96	0.27	0.69	0.96	0.637	1.04	0.610	1.04	1.30	0.788	No
1656	16.56	0.96	0.27	0.69	0.96	0.637	1.04	0.611	1.04	1.30	0.788	No
1657	16.57	0.96	0.27	0.69	0.96	0.637	1.04	0.611	1.04	1.30	0.788	No
1658	16.58	0.96	0.27	0.69	0.96	0.637	1.04	0.611	1.04	1.30	0.788	No
1659	16.59	0.96	0.27	0.69	0.96	0.637	1.04	0.611	1.04	1.30	0.788	No
1660	16.60	0.96	0.27	0.69	0.96	0.637	1.04	0.611	1.04	1.30	0.788	No
1661	16.61	0.96	0.27	0.69	0.96	0.638	1.04	0.611	1.04	1.30	0.789	No
1662	16.62	0.96	0.27	0.69	0.96	0.638	1.04	0.611	1.04	1.30	0.789	No
1663	16.63	0.96	0.27	0.69	0.96	0.638	1.04	0.611	1.04	1.30	0.789	No
1664	16.64	0.96	0.27	0.69	0.96	0.638	1.04	0.611	1.04	1.30	0.789	No
1665	16.65	0.96	0.27	0.69	0.96	0.638	1.04	0.612	1.04	1.30	0.789	No
1666	16.66	0.97	0.27	0.69	0.96	0.638	1.04	0.612	1.04	1.30	0.789	No
1667	16.67	0.97	0.27	0.70	0.96	0.638	1.04	0.612	1.04	1.30	0.790	No
1668	16.68	0.97	0.27	0.70	0.96	0.638	1.04	0.612	1.04	1.30	0.790	No
1669	16.69	0.97	0.27	0.70	0.96	0.638	1.04	0.612	1.04	1.30	0.790	No
1670	16.70	0.97	0.27	0.70	0.96	0.639	1.04	0.612	1.04	1.30	0.791	No
1671	16.71	0.97	0.27	0.70	0.96	0.639	1.04	0.612	1.04	1.30	0.791	No
1672	16.72	0.97	0.27	0.70	0.96	0.639	1.04	0.612	1.04	1.30	0.791	No
1673	16.73	0.97	0.27	0.70	0.95	0.639	1.04	0.612	1.04	1.30	0.792	No
1674	16.74	0.97	0.27	0.70	0.95	0.639	1.04	0.612	1.04	1.30	0.792	No
1675	16.75	0.97	0.27	0.70	0.95	0.639	1.04	0.613	1.04	1.30	0.792	No
1676	16.76	0.97	0.27	0.70	0.95	0.639	1.04	0.613	1.04	1.30	0.793	No
1677	16.77	0.97	0.27	0.70	0.95	0.639	1.04	0.613	1.04	1.30	0.793	No
1678	16.78	0.97	0.27	0.70	0.95	0.639	1.04	0.613	1.04	1.30	0.793	No
1679	16.79	0.97	0.27	0.70	0.95	0.640	1.04	0.613	1.04	1.30	0.794	No
1680	16.80	0.97	0.27	0.70	0.95	0.640	1.04	0.613	1.04	1.30	0.794	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
1681	16.81	0.97	0.27	0.70	0.95	0.640	1.04	0.613	1.04	1.30	0.794	No
1682	16.82	0.97	0.28	0.70	0.95	0.640	1.04	0.613	1.04	1.30	0.794	No
1683	16.83	0.97	0.28	0.70	0.95	0.640	1.04	0.613	1.04	1.30	0.795	No
1684	16.84	0.98	0.28	0.70	0.95	0.640	1.04	0.614	1.04	1.30	0.795	No
1685	16.85	0.98	0.28	0.70	0.95	0.640	1.04	0.614	1.04	1.30	0.795	No
1686	16.86	0.98	0.28	0.70	0.95	0.640	1.04	0.614	1.04	1.30	0.796	No
1687	16.87	0.98	0.28	0.70	0.95	0.640	1.04	0.614	1.04	1.30	0.796	No
1688	16.88	0.98	0.28	0.70	0.95	0.641	1.04	0.614	1.04	1.30	0.797	No
1689	16.89	0.98	0.28	0.70	0.95	0.641	1.04	0.614	1.04	1.30	0.797	No
1690	16.90	0.98	0.28	0.70	0.95	0.641	1.04	0.614	1.04	1.30	0.797	No
1691	16.91	0.98	0.28	0.70	0.95	0.641	1.04	0.614	1.04	1.30	0.798	No
1692	16.92	0.98	0.28	0.70	0.95	0.641	1.04	0.614	1.04	1.30	0.798	No
1693	16.93	0.98	0.28	0.70	0.95	0.641	1.04	0.615	1.04	1.30	0.799	No
1694	16.94	0.98	0.28	0.70	0.95	0.641	1.04	0.615	1.03	1.30	0.799	No
1695	16.95	0.98	0.28	0.70	0.95	0.641	1.04	0.615	1.03	1.30	0.799	No
1696	16.96	0.98	0.28	0.70	0.95	0.641	1.04	0.615	1.03	1.30	0.799	No
1697	16.97	0.98	0.28	0.70	0.95	0.642	1.04	0.615	1.03	1.30	0.800	No
1698	16.98	0.98	0.28	0.70	0.95	0.642	1.04	0.615	1.03	1.30	0.800	No
1699	16.99	0.98	0.28	0.70	0.95	0.642	1.04	0.615	1.03	1.30	0.800	No
1700	17.00	0.98	0.28	0.70	0.95	0.642	1.04	0.615	1.03	1.30	0.801	No
1701	17.01	0.98	0.28	0.70	0.95	0.642	1.04	0.615	1.03	1.30	0.801	No
1702	17.02	0.99	0.28	0.70	0.95	0.642	1.04	0.616	1.03	1.30	0.801	No
1703	17.03	0.99	0.28	0.70	0.95	0.642	1.04	0.616	1.03	1.30	0.801	No
1704	17.04	0.99	0.28	0.70	0.95	0.642	1.04	0.616	1.03	1.30	0.801	No
1705	17.05	0.99	0.28	0.70	0.95	0.643	1.04	0.616	1.03	1.30	0.801	No
1706	17.06	0.99	0.28	0.71	0.95	0.643	1.04	0.616	1.03	1.30	0.801	No
1707	17.07	0.99	0.28	0.71	0.95	0.643	1.04	0.616	1.03	1.30	0.802	No
1708	17.08	0.99	0.28	0.71	0.95	0.643	1.04	0.616	1.03	1.30	0.802	No
1709	17.09	0.99	0.28	0.71	0.95	0.643	1.04	0.616	1.03	1.30	0.802	No
1710	17.10	0.99	0.28	0.71	0.95	0.643	1.04	0.616	1.03	1.30	0.802	No
1711	17.11	0.99	0.28	0.71	0.95	0.643	1.04	0.616	1.03	1.30	0.802	No
1712	17.12	0.99	0.28	0.71	0.95	0.643	1.04	0.617	1.03	1.30	0.802	No
1713	17.13	0.99	0.28	0.71	0.95	0.643	1.04	0.617	1.03	1.30	0.802	No
1714	17.14	0.99	0.29	0.71	0.95	0.644	1.04	0.617	1.03	1.30	0.803	No
1715	17.15	0.99	0.29	0.71	0.95	0.644	1.04	0.617	1.03	1.30	0.803	No
1716	17.16	0.99	0.29	0.71	0.95	0.644	1.04	0.617	1.03	1.30	0.803	No
1717	17.17	0.99	0.29	0.71	0.95	0.644	1.04	0.617	1.03	1.30	0.803	No
1718	17.18	0.99	0.29	0.71	0.95	0.644	1.04	0.617	1.03	1.30	0.803	No
1719	17.19	1.00	0.29	0.71	0.95	0.644	1.04	0.617	1.03	1.30	0.803	No
1720	17.20	1.00	0.29	0.71	0.95	0.644	1.04	0.617	1.03	1.30	0.804	No
1721	17.21	1.00	0.29	0.71	0.95	0.644	1.04	0.618	1.03	1.30	0.804	No
1722	17.22	1.00	0.29	0.71	0.95	0.644	1.04	0.618	1.03	1.30	0.804	No
1723	17.23	1.00	0.29	0.71	0.95	0.645	1.04	0.618	1.03	1.30	0.805	No
1724	17.24	1.00	0.29	0.71	0.95	0.645	1.04	0.618	1.03	1.30	0.805	No
1725	17.25	1.00	0.29	0.71	0.95	0.645	1.04	0.618	1.03	1.30	0.805	No
1726	17.26	1.00	0.29	0.71	0.95	0.645	1.04	0.618	1.03	1.30	0.806	No
1727	17.27	1.00	0.29	0.71	0.95	0.645	1.04	0.618	1.03	1.30	0.806	No
1728	17.28	1.00	0.29	0.71	0.95	0.645	1.04	0.618	1.03	1.30	0.806	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
1729	17.29	1.00	0.29	0.71	0.95	0.645	1.04	0.618	1.03	1.30	0.806	No
1730	17.30	1.00	0.29	0.71	0.95	0.645	1.04	0.619	1.03	1.30	0.807	No
1731	17.31	1.00	0.29	0.71	0.95	0.645	1.04	0.619	1.03	1.30	0.807	No
1732	17.32	1.00	0.29	0.71	0.95	0.646	1.04	0.619	1.03	1.30	0.807	No
1733	17.33	1.00	0.29	0.71	0.95	0.646	1.04	0.619	1.03	1.30	0.808	No
1734	17.34	1.00	0.29	0.71	0.95	0.646	1.04	0.619	1.03	1.30	0.808	No
1735	17.35	1.00	0.29	0.71	0.95	0.646	1.04	0.619	1.03	1.30	0.808	No
1736	17.36	1.00	0.29	0.71	0.95	0.646	1.04	0.619	1.03	1.30	0.809	No
1737	17.37	1.00	0.29	0.71	0.95	0.646	1.04	0.619	1.03	1.30	0.809	No
1738	17.38	1.01	0.29	0.71	0.95	0.646	1.04	0.619	1.03	1.30	0.809	No
1739	17.39	1.01	0.29	0.71	0.95	0.646	1.04	0.620	1.03	1.30	0.809	No
1740	17.40	1.01	0.29	0.71	0.95	0.646	1.04	0.620	1.03	1.30	0.809	No
1741	17.41	1.01	0.29	0.71	0.95	0.647	1.04	0.620	1.03	1.30	0.809	No
1742	17.42	1.01	0.29	0.71	0.95	0.647	1.04	0.620	1.03	1.30	0.809	No
1743	17.43	1.01	0.29	0.71	0.95	0.647	1.04	0.620	1.03	1.30	0.810	No
1744	17.44	1.01	0.29	0.71	0.95	0.647	1.04	0.620	1.03	1.30	0.810	No
1745	17.45	1.01	0.29	0.71	0.95	0.647	1.04	0.620	1.03	1.30	0.810	No
1746	17.46	1.01	0.30	0.71	0.95	0.647	1.04	0.620	1.03	1.30	0.810	No
1747	17.47	1.01	0.30	0.71	0.95	0.647	1.04	0.620	1.03	1.30	0.810	No
1748	17.48	1.01	0.30	0.71	0.95	0.647	1.04	0.621	1.03	1.30	0.810	No
1749	17.49	1.01	0.30	0.72	0.95	0.648	1.04	0.621	1.03	1.30	0.811	No
1750	17.50	1.01	0.30	0.72	0.95	0.648	1.04	0.621	1.03	1.30	0.811	No
1751	17.51	1.01	0.30	0.72	0.95	0.648	1.04	0.621	1.03	1.30	0.811	No
1752	17.52	1.01	0.30	0.72	0.95	0.648	1.04	0.621	1.03	1.30	0.811	No
1753	17.53	1.01	0.30	0.72	0.95	0.648	1.04	0.621	1.03	1.30	0.811	No
1754	17.54	1.01	0.30	0.72	0.95	0.648	1.04	0.621	1.03	1.30	0.811	No
1755	17.55	1.01	0.30	0.72	0.95	0.648	1.04	0.621	1.03	1.30	0.811	No
1756	17.56	1.01	0.30	0.72	0.95	0.648	1.04	0.621	1.03	1.30	0.812	No
1757	17.57	1.02	0.30	0.72	0.95	0.648	1.04	0.622	1.03	1.30	0.812	No
1758	17.58	1.02	0.30	0.72	0.95	0.649	1.04	0.622	1.03	1.30	0.812	No
1759	17.59	1.02	0.30	0.72	0.95	0.649	1.04	0.622	1.03	1.30	0.812	No
1760	17.60	1.02	0.30	0.72	0.95	0.649	1.04	0.622	1.03	1.30	0.812	No
1761	17.61	1.02	0.30	0.72	0.95	0.649	1.04	0.622	1.03	1.30	0.812	No
1762	17.62	1.02	0.30	0.72	0.95	0.649	1.04	0.622	1.03	1.30	0.812	No
1763	17.63	1.02	0.30	0.72	0.95	0.649	1.04	0.622	1.03	1.30	0.812	No
1764	17.64	1.02	0.30	0.72	0.95	0.649	1.04	0.622	1.03	1.30	0.812	No
1765	17.65	1.02	0.30	0.72	0.95	0.649	1.04	0.622	1.03	1.30	0.812	No
1766	17.66	1.02	0.30	0.72	0.95	0.649	1.04	0.622	1.03	1.30	0.812	No
1767	17.67	1.02	0.30	0.72	0.95	0.650	1.04	0.623	1.03	1.30	0.813	No
1768	17.68	1.02	0.30	0.72	0.95	0.650	1.04	0.623	1.03	1.30	0.813	No
1769	17.69	1.02	0.30	0.72	0.95	0.650	1.04	0.623	1.03	1.30	0.813	No
1770	17.70	1.02	0.30	0.72	0.95	0.650	1.04	0.623	1.03	1.30	0.813	No
1771	17.71	1.02	0.30	0.72	0.95	0.650	1.04	0.623	1.03	1.30	0.813	No
1772	17.72	1.02	0.30	0.72	0.95	0.650	1.04	0.623	1.03	1.30	0.813	No
1773	17.73	1.02	0.30	0.72	0.95	0.650	1.04	0.623	1.03	1.30	0.813	No
1774	17.74	1.02	0.30	0.72	0.95	0.650	1.04	0.623	1.03	1.30	0.814	No
1775	17.75	1.03	0.30	0.72	0.95	0.650	1.04	0.623	1.03	1.30	0.814	No
1776	17.76	1.03	0.30	0.72	0.95	0.651	1.04	0.624	1.03	1.30	0.814	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1777	17.77	1.03	0.30	0.72	0.95	0.651	1.04	0.624	1.03	1.30	0.814	No
1778	17.78	1.03	0.31	0.72	0.95	0.651	1.04	0.624	1.03	1.30	0.814	No
1779	17.79	1.03	0.31	0.72	0.95	0.651	1.04	0.624	1.03	1.30	0.814	No
1780	17.80	1.03	0.31	0.72	0.95	0.651	1.04	0.624	1.03	1.30	0.815	No
1781	17.81	1.03	0.31	0.72	0.95	0.651	1.04	0.624	1.03	1.30	0.815	No
1782	17.82	1.03	0.31	0.72	0.95	0.651	1.04	0.624	1.03	1.30	0.815	No
1783	17.83	1.03	0.31	0.72	0.95	0.651	1.04	0.624	1.03	1.30	0.815	No
1784	17.84	1.03	0.31	0.72	0.95	0.651	1.04	0.624	1.03	1.30	0.815	No
1785	17.85	1.03	0.31	0.72	0.95	0.651	1.04	0.624	1.03	1.30	0.816	No
1786	17.86	1.03	0.31	0.72	0.95	0.652	1.04	0.625	1.03	1.30	0.816	No
1787	17.87	1.03	0.31	0.72	0.95	0.652	1.04	0.625	1.03	1.30	0.816	No
1788	17.88	1.03	0.31	0.72	0.95	0.652	1.04	0.625	1.03	1.30	0.816	No
1789	17.89	1.03	0.31	0.72	0.95	0.652	1.04	0.625	1.03	1.30	0.816	No
1790	17.90	1.03	0.31	0.72	0.95	0.652	1.04	0.625	1.03	1.30	0.816	No
1791	17.91	1.03	0.31	0.72	0.95	0.652	1.04	0.625	1.03	1.30	0.817	No
1792	17.92	1.03	0.31	0.73	0.95	0.652	1.04	0.625	1.03	1.30	0.817	No
1793	17.93	1.04	0.31	0.73	0.95	0.652	1.04	0.625	1.03	1.30	0.817	No
1794	17.94	1.04	0.31	0.73	0.95	0.652	1.04	0.625	1.03	1.30	0.817	No
1795	17.95	1.04	0.31	0.73	0.95	0.653	1.04	0.625	1.03	1.30	0.817	No
1796	17.96	1.04	0.31	0.73	0.95	0.653	1.04	0.626	1.03	1.30	0.817	No
1797	17.97	1.04	0.31	0.73	0.95	0.653	1.04	0.626	1.03	1.30	0.818	No
1798	17.98	1.04	0.31	0.73	0.95	0.653	1.04	0.626	1.03	1.30	0.818	No
1799	17.99	1.04	0.31	0.73	0.95	0.653	1.04	0.626	1.03	1.30	0.818	No
1800	18.00	1.04	0.31	0.73	0.95	0.653	1.04	0.626	1.03	1.30	0.818	No
1801	18.01	1.04	0.31	0.73	0.95	0.653	1.04	0.626	1.03	1.30	0.818	No
1802	18.02	1.04	0.31	0.73	0.95	0.653	1.04	0.626	1.03	1.30	0.818	No
1803	18.03	1.04	0.31	0.73	0.95	0.653	1.04	0.626	1.03	1.30	0.818	No
1804	18.04	1.04	0.31	0.73	0.95	0.653	1.04	0.626	1.03	1.30	0.818	No
1805	18.05	1.04	0.31	0.73	0.95	0.654	1.04	0.626	1.03	1.30	0.818	No
1806	18.06	1.04	0.31	0.73	0.95	0.654	1.04	0.627	1.03	1.30	0.818	No
1807	18.07	1.04	0.31	0.73	0.95	0.654	1.04	0.627	1.03	1.30	0.818	No
1808	18.08	1.04	0.31	0.73	0.95	0.654	1.04	0.627	1.03	1.30	0.818	No
1809	18.09	1.04	0.31	0.73	0.95	0.654	1.04	0.627	1.03	1.30	0.818	No
1810	18.10	1.04	0.32	0.73	0.95	0.654	1.04	0.627	1.03	1.30	0.818	No
1811	18.11	1.05	0.32	0.73	0.95	0.654	1.04	0.627	1.03	1.30	0.818	No
1812	18.12	1.05	0.32	0.73	0.95	0.654	1.04	0.627	1.03	1.30	0.818	No
1813	18.13	1.05	0.32	0.73	0.95	0.654	1.04	0.627	1.03	1.30	0.818	No
1814	18.14	1.05	0.32	0.73	0.95	0.654	1.04	0.627	1.03	1.30	0.818	No
1815	18.15	1.05	0.32	0.73	0.95	0.655	1.04	0.627	1.03	1.30	0.818	No
1816	18.16	1.05	0.32	0.73	0.95	0.655	1.04	0.627	1.03	1.30	0.818	No
1817	18.17	1.05	0.32	0.73	0.95	0.655	1.04	0.628	1.03	1.30	0.818	No
1818	18.18	1.05	0.32	0.73	0.95	0.655	1.04	0.628	1.03	1.30	0.817	No
1819	18.19	1.05	0.32	0.73	0.95	0.655	1.04	0.628	1.03	1.30	0.817	No
1820	18.20	1.05	0.32	0.73	0.95	0.655	1.04	0.628	1.03	1.30	0.817	No
1821	18.21	1.05	0.32	0.73	0.95	0.655	1.04	0.628	1.03	1.30	0.817	No
1822	18.22	1.05	0.32	0.73	0.95	0.655	1.04	0.628	1.03	1.30	0.817	No
1823	18.23	1.05	0.32	0.73	0.95	0.655	1.04	0.628	1.03	1.30	0.817	No
1824	18.24	1.05	0.32	0.73	0.95	0.655	1.04	0.628	1.03	1.30	0.817	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1825	18.25	1.05	0.32	0.73	0.95	0.656	1.04	0.628	1.03	1.30	0.817	No
1826	18.26	1.05	0.32	0.73	0.95	0.656	1.04	0.628	1.03	1.30	0.817	No
1827	18.27	1.05	0.32	0.73	0.95	0.656	1.04	0.628	1.03	1.30	0.817	No
1828	18.28	1.05	0.32	0.73	0.95	0.656	1.04	0.629	1.03	1.30	0.816	No
1829	18.29	1.06	0.32	0.73	0.95	0.656	1.04	0.629	1.03	1.30	0.816	No
1830	18.30	1.06	0.32	0.73	0.95	0.656	1.04	0.629	1.03	1.30	0.816	No
1831	18.31	1.06	0.32	0.74	0.95	0.656	1.04	0.629	1.03	1.30	0.817	No
1832	18.32	1.06	0.32	0.74	0.95	0.656	1.04	0.629	1.03	1.30	0.817	No
1833	18.33	1.06	0.32	0.74	0.95	0.656	1.04	0.629	1.03	1.30	0.817	No
1834	18.34	1.06	0.32	0.74	0.95	0.656	1.04	0.629	1.03	1.30	0.817	No
1835	18.35	1.06	0.32	0.74	0.95	0.656	1.04	0.629	1.03	1.30	0.817	No
1836	18.36	1.06	0.32	0.74	0.95	0.657	1.04	0.629	1.03	1.30	0.818	No
1837	18.37	1.06	0.32	0.74	0.95	0.657	1.04	0.629	1.03	1.30	0.818	No
1838	18.38	1.06	0.32	0.74	0.95	0.657	1.04	0.629	1.03	1.30	0.818	No
1839	18.39	1.06	0.32	0.74	0.95	0.657	1.04	0.630	1.03	1.30	0.819	No
1840	18.40	1.06	0.32	0.74	0.95	0.657	1.04	0.630	1.03	1.30	0.819	No
1841	18.41	1.06	0.32	0.74	0.95	0.657	1.04	0.630	1.03	1.30	0.819	No
1842	18.42	1.06	0.33	0.74	0.95	0.657	1.04	0.630	1.03	1.30	0.819	No
1843	18.43	1.06	0.33	0.74	0.95	0.657	1.04	0.630	1.03	1.30	0.820	No
1844	18.44	1.06	0.33	0.74	0.95	0.657	1.04	0.630	1.03	1.30	0.820	No
1845	18.45	1.06	0.33	0.74	0.95	0.657	1.04	0.630	1.03	1.30	0.821	No
1846	18.46	1.07	0.33	0.74	0.95	0.658	1.04	0.630	1.03	1.30	0.821	No
1847	18.47	1.07	0.33	0.74	0.95	0.658	1.04	0.630	1.03	1.30	0.821	No
1848	18.48	1.07	0.33	0.74	0.95	0.658	1.04	0.630	1.03	1.30	0.822	No
1849	18.49	1.07	0.33	0.74	0.95	0.658	1.04	0.630	1.03	1.30	0.822	No
1850	18.50	1.07	0.33	0.74	0.95	0.658	1.04	0.631	1.03	1.30	0.822	No
1851	18.51	1.07	0.33	0.74	0.95	0.658	1.04	0.631	1.03	1.30	0.822	No
1852	18.52	1.07	0.33	0.74	0.95	0.658	1.04	0.631	1.03	1.30	0.823	No
1853	18.53	1.07	0.33	0.74	0.95	0.658	1.04	0.631	1.03	1.30	0.823	No
1854	18.54	1.07	0.33	0.74	0.95	0.658	1.04	0.631	1.03	1.30	0.824	No
1855	18.55	1.07	0.33	0.74	0.95	0.658	1.04	0.631	1.03	1.30	0.824	No
1856	18.56	1.07	0.33	0.74	0.95	0.658	1.04	0.631	1.03	1.30	0.824	No
1857	18.57	1.07	0.33	0.74	0.95	0.659	1.04	0.631	1.03	1.30	0.825	No
1858	18.58	1.07	0.33	0.74	0.95	0.659	1.04	0.631	1.03	1.30	0.825	No
1859	18.59	1.07	0.33	0.74	0.95	0.659	1.04	0.631	1.03	1.30	0.825	No
1860	18.60	1.07	0.33	0.74	0.95	0.659	1.04	0.632	1.03	1.30	0.825	No
1861	18.61	1.07	0.33	0.74	0.95	0.659	1.04	0.632	1.03	1.30	0.826	No
1862	18.62	1.07	0.33	0.74	0.95	0.659	1.04	0.632	1.03	1.30	0.826	No
1863	18.63	1.07	0.33	0.74	0.95	0.659	1.04	0.632	1.03	1.30	0.826	No
1864	18.64	1.08	0.33	0.74	0.95	0.659	1.04	0.632	1.03	1.30	0.827	No
1865	18.65	1.08	0.33	0.74	0.95	0.659	1.04	0.632	1.03	1.30	0.827	No
1866	18.66	1.08	0.33	0.74	0.95	0.659	1.04	0.632	1.03	1.30	0.827	No
1867	18.67	1.08	0.33	0.74	0.95	0.660	1.04	0.632	1.03	1.30	0.827	No
1868	18.68	1.08	0.33	0.74	0.95	0.660	1.04	0.632	1.03	1.30	0.828	No
1869	18.69	1.08	0.33	0.74	0.95	0.660	1.04	0.632	1.03	1.30	0.828	No
1870	18.70	1.08	0.33	0.74	0.95	0.660	1.04	0.632	1.03	1.30	0.828	No
1871	18.71	1.08	0.33	0.74	0.95	0.660	1.04	0.633	1.03	1.30	0.828	No
1872	18.72	1.08	0.33	0.75	0.95	0.660	1.04	0.633	1.03	1.30	0.829	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
1873	18.73	1.08	0.33	0.75	0.95	0.660	1.04	0.633	1.03	1.30	0.829	No
1874	18.74	1.08	0.34	0.75	0.95	0.660	1.04	0.633	1.03	1.30	0.829	No
1875	18.75	1.08	0.34	0.75	0.95	0.660	1.04	0.633	1.03	1.30	0.829	No
1876	18.76	1.08	0.34	0.75	0.95	0.660	1.04	0.633	1.03	1.30	0.829	No
1877	18.77	1.08	0.34	0.75	0.95	0.661	1.04	0.633	1.03	1.30	0.830	No
1878	18.78	1.08	0.34	0.75	0.95	0.661	1.04	0.633	1.03	1.30	0.830	No
1879	18.79	1.08	0.34	0.75	0.95	0.661	1.04	0.633	1.03	1.30	0.830	No
1880	18.80	1.08	0.34	0.75	0.95	0.661	1.04	0.633	1.03	1.30	0.830	No
1881	18.81	1.08	0.34	0.75	0.95	0.661	1.04	0.634	1.03	1.30	0.830	No
1882	18.82	1.08	0.34	0.75	0.95	0.661	1.04	0.634	1.03	1.30	0.831	No
1883	18.83	1.09	0.34	0.75	0.95	0.661	1.04	0.634	1.03	1.30	0.831	No
1884	18.84	1.09	0.34	0.75	0.95	0.661	1.04	0.634	1.03	1.30	0.831	No
1885	18.85	1.09	0.34	0.75	0.95	0.661	1.04	0.634	1.03	1.30	0.831	No
1886	18.86	1.09	0.34	0.75	0.95	0.662	1.04	0.634	1.03	1.30	0.831	No
1887	18.87	1.09	0.34	0.75	0.95	0.662	1.04	0.634	1.03	1.30	0.831	No
1888	18.88	1.09	0.34	0.75	0.95	0.662	1.04	0.634	1.03	1.30	0.831	No
1889	18.89	1.09	0.34	0.75	0.95	0.662	1.04	0.634	1.03	1.30	0.832	No
1890	18.90	1.09	0.34	0.75	0.95	0.662	1.04	0.634	1.03	1.30	0.832	No
1891	18.91	1.09	0.34	0.75	0.95	0.662	1.04	0.635	1.03	1.30	0.832	No
1892	18.92	1.09	0.34	0.75	0.95	0.662	1.04	0.635	1.03	1.30	0.832	No
1893	18.93	1.09	0.34	0.75	0.95	0.662	1.04	0.635	1.03	1.30	0.832	No
1894	18.94	1.09	0.34	0.75	0.95	0.662	1.04	0.635	1.03	1.30	0.832	No
1895	18.95	1.09	0.34	0.75	0.95	0.662	1.04	0.635	1.03	1.30	0.832	No
1896	18.96	1.09	0.34	0.75	0.95	0.663	1.04	0.635	1.03	1.30	0.832	No
1897	18.97	1.09	0.34	0.75	0.95	0.663	1.04	0.635	1.03	1.30	0.833	No
1898	18.98	1.09	0.34	0.75	0.95	0.663	1.04	0.635	1.03	1.30	0.833	No
1899	18.99	1.09	0.34	0.75	0.95	0.663	1.04	0.635	1.03	1.30	0.833	No
1900	19.00	1.09	0.34	0.75	0.95	0.663	1.04	0.635	1.03	1.30	0.833	No
1901	19.01	1.10	0.34	0.75	0.95	0.663	1.04	0.635	1.03	1.30	0.833	No
1902	19.02	1.10	0.34	0.75	0.95	0.663	1.04	0.636	1.03	1.30	0.833	No
1903	19.03	1.10	0.34	0.75	0.95	0.663	1.04	0.636	1.03	1.30	0.833	No
1904	19.04	1.10	0.34	0.75	0.95	0.663	1.04	0.636	1.03	1.30	0.833	No
1905	19.05	1.10	0.34	0.75	0.95	0.663	1.04	0.636	1.03	1.30	0.833	No
1906	19.06	1.10	0.35	0.75	0.95	0.664	1.04	0.636	1.03	1.30	0.834	No
1907	19.07	1.10	0.35	0.75	0.95	0.664	1.04	0.636	1.03	1.30	0.834	No
1908	19.08	1.10	0.35	0.75	0.95	0.664	1.04	0.636	1.03	1.30	0.834	No
1909	19.09	1.10	0.35	0.75	0.95	0.664	1.04	0.636	1.03	1.30	0.834	No
1910	19.10	1.10	0.35	0.75	0.95	0.664	1.04	0.636	1.03	1.30	0.834	No
1911	19.11	1.10	0.35	0.75	0.95	0.664	1.04	0.636	1.03	1.30	0.834	No
1912	19.12	1.10	0.35	0.75	0.95	0.664	1.04	0.636	1.03	1.30	0.834	No
1913	19.13	1.10	0.35	0.75	0.95	0.664	1.04	0.637	1.03	1.30	0.834	No
1914	19.14	1.10	0.35	0.75	0.95	0.664	1.04	0.637	1.03	1.30	0.835	No
1915	19.15	1.10	0.35	0.75	0.95	0.664	1.04	0.637	1.03	1.30	0.835	No
1916	19.16	1.10	0.35	0.76	0.95	0.664	1.04	0.637	1.03	1.30	0.835	No
1917	19.17	1.10	0.35	0.76	0.95	0.665	1.04	0.637	1.03	1.30	0.835	No
1918	19.18	1.10	0.35	0.76	0.95	0.665	1.04	0.637	1.03	1.30	0.835	No
1919	19.19	1.10	0.35	0.76	0.95	0.665	1.04	0.637	1.03	1.30	0.835	No
1920	19.20	1.11	0.35	0.76	0.95	0.665	1.04	0.637	1.03	1.30	0.835	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1921	19.21	1.11	0.35	0.76	0.95	0.665	1.04	0.637	1.03	1.30	0.836	No
1922	19.22	1.11	0.35	0.76	0.95	0.665	1.04	0.637	1.03	1.30	0.836	No
1923	19.23	1.11	0.35	0.76	0.95	0.665	1.04	0.638	1.03	1.30	0.836	No
1924	19.24	1.11	0.35	0.76	0.95	0.665	1.04	0.638	1.03	1.30	0.836	No
1925	19.25	1.11	0.35	0.76	0.95	0.665	1.04	0.638	1.03	1.30	0.836	No
1926	19.26	1.11	0.35	0.76	0.95	0.665	1.04	0.638	1.03	1.30	0.837	No
1927	19.27	1.11	0.35	0.76	0.94	0.666	1.04	0.638	1.03	1.30	0.837	No
1928	19.28	1.11	0.35	0.76	0.94	0.666	1.04	0.638	1.03	1.30	0.837	No
1929	19.29	1.11	0.35	0.76	0.94	0.666	1.04	0.638	1.03	1.30	0.837	No
1930	19.30	1.11	0.35	0.76	0.94	0.666	1.04	0.638	1.03	1.30	0.837	No
1931	19.31	1.11	0.35	0.76	0.94	0.666	1.04	0.638	1.03	1.30	0.837	No
1932	19.32	1.11	0.35	0.76	0.94	0.666	1.04	0.638	1.03	1.30	0.838	No
1933	19.33	1.11	0.35	0.76	0.94	0.666	1.04	0.638	1.03	1.30	0.838	No
1934	19.34	1.11	0.35	0.76	0.94	0.666	1.04	0.639	1.03	1.30	0.838	No
1935	19.35	1.11	0.35	0.76	0.94	0.666	1.04	0.639	1.03	1.30	0.838	No
1936	19.36	1.11	0.35	0.76	0.94	0.666	1.04	0.639	1.03	1.30	0.838	No
1937	19.37	1.11	0.35	0.76	0.94	0.667	1.04	0.639	1.03	1.30	0.838	No
1938	19.38	1.11	0.36	0.76	0.94	0.667	1.04	0.639	1.03	1.30	0.839	No
1939	19.39	1.12	0.36	0.76	0.94	0.667	1.04	0.639	1.03	1.30	0.839	No
1940	19.40	1.12	0.36	0.76	0.94	0.667	1.04	0.639	1.03	1.30	0.839	No
1941	19.41	1.12	0.36	0.76	0.94	0.667	1.04	0.639	1.03	1.30	0.839	No
1942	19.42	1.12	0.36	0.76	0.94	0.667	1.04	0.639	1.03	1.30	0.839	No
1943	19.43	1.12	0.36	0.76	0.94	0.667	1.04	0.639	1.03	1.30	0.839	No
1944	19.44	1.12	0.36	0.76	0.94	0.667	1.04	0.639	1.03	1.30	0.839	No
1945	19.45	1.12	0.36	0.76	0.94	0.667	1.04	0.640	1.03	1.30	0.840	No
1946	19.46	1.12	0.36	0.76	0.94	0.667	1.04	0.640	1.03	1.30	0.840	No
1947	19.47	1.12	0.36	0.76	0.94	0.667	1.04	0.640	1.03	1.30	0.840	No
1948	19.48	1.12	0.36	0.76	0.94	0.668	1.04	0.640	1.03	1.30	0.840	No
1949	19.49	1.12	0.36	0.76	0.94	0.668	1.04	0.640	1.03	1.30	0.840	No
1950	19.50	1.12	0.36	0.76	0.94	0.668	1.04	0.640	1.03	1.30	0.840	No
1951	19.51	1.12	0.36	0.76	0.94	0.668	1.04	0.640	1.03	1.30	0.840	No
1952	19.52	1.12	0.36	0.76	0.94	0.668	1.04	0.640	1.03	1.30	0.841	No
1953	19.53	1.12	0.36	0.76	0.94	0.668	1.04	0.640	1.03	1.30	0.841	No
1954	19.54	1.12	0.36	0.76	0.94	0.668	1.04	0.640	1.03	1.30	0.841	No
1955	19.55	1.12	0.36	0.76	0.94	0.668	1.04	0.641	1.03	1.30	0.841	No
1956	19.56	1.12	0.36	0.76	0.94	0.668	1.04	0.641	1.03	1.30	0.841	No
1957	19.57	1.12	0.36	0.76	0.94	0.668	1.04	0.641	1.03	1.30	0.841	No
1958	19.58	1.13	0.36	0.76	0.94	0.669	1.04	0.641	1.03	1.30	0.841	No
1959	19.59	1.13	0.36	0.76	0.94	0.669	1.04	0.641	1.03	1.30	0.842	No
1960	19.60	1.13	0.36	0.76	0.94	0.669	1.04	0.641	1.03	1.30	0.842	No
1961	19.61	1.13	0.36	0.76	0.94	0.669	1.04	0.641	1.03	1.30	0.842	No
1962	19.62	1.13	0.36	0.76	0.94	0.669	1.04	0.641	1.03	1.30	0.842	No
1963	19.63	1.13	0.36	0.77	0.94	0.669	1.04	0.641	1.03	1.30	0.842	No
1964	19.64	1.13	0.36	0.77	0.94	0.669	1.04	0.641	1.03	1.30	0.842	No
1965	19.65	1.13	0.36	0.77	0.94	0.669	1.04	0.641	1.03	1.30	0.842	No
1966	19.66	1.13	0.36	0.77	0.94	0.669	1.04	0.642	1.03	1.30	0.843	No
1967	19.67	1.13	0.36	0.77	0.94	0.669	1.04	0.642	1.03	1.30	0.843	No
1968	19.68	1.13	0.36	0.77	0.94	0.670	1.04	0.642	1.03	1.30	0.843	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
1969	19.69	1.13	0.36	0.77	0.94	0.670	1.04	0.642	1.03	1.30	0.843	No
1970	19.70	1.13	0.37	0.77	0.94	0.670	1.04	0.642	1.03	1.30	0.843	No
1971	19.71	1.13	0.37	0.77	0.94	0.670	1.04	0.642	1.03	1.30	0.843	No
1972	19.72	1.13	0.37	0.77	0.94	0.670	1.04	0.642	1.03	1.30	0.843	No
1973	19.73	1.13	0.37	0.77	0.94	0.670	1.04	0.642	1.03	1.30	0.844	No
1974	19.74	1.13	0.37	0.77	0.94	0.670	1.04	0.642	1.03	1.30	0.844	No
1975	19.75	1.13	0.37	0.77	0.94	0.670	1.04	0.642	1.03	1.30	0.844	No
1976	19.76	1.13	0.37	0.77	0.94	0.670	1.04	0.643	1.03	1.30	0.844	No
1977	19.77	1.14	0.37	0.77	0.94	0.670	1.04	0.643	1.03	1.30	0.844	No
1978	19.78	1.14	0.37	0.77	0.94	0.671	1.04	0.643	1.02	1.30	0.845	No
1979	19.79	1.14	0.37	0.77	0.94	0.671	1.04	0.643	1.02	1.30	0.845	No
1980	19.80	1.14	0.37	0.77	0.94	0.671	1.04	0.643	1.03	1.30	0.845	No
1981	19.81	1.14	0.37	0.77	0.94	0.671	1.04	0.643	1.03	1.30	0.845	No
1982	19.82	1.14	0.37	0.77	0.94	0.671	1.04	0.643	1.03	1.30	0.844	No
1983	19.83	1.14	0.37	0.77	0.94	0.671	1.04	0.643	1.03	1.30	0.844	No
1984	19.84	1.14	0.37	0.77	0.94	0.671	1.04	0.643	1.03	1.30	0.844	No
1985	19.85	1.14	0.37	0.77	0.94	0.671	1.04	0.643	1.03	1.30	0.844	No
1986	19.86	1.14	0.37	0.77	0.94	0.671	1.04	0.643	1.03	1.30	0.844	No
1987	19.87	1.14	0.37	0.77	0.94	0.671	1.04	0.643	1.03	1.30	0.844	No
1988	19.88	1.14	0.37	0.77	0.94	0.671	1.04	0.644	1.03	1.30	0.844	No
1989	19.89	1.14	0.37	0.77	0.94	0.672	1.04	0.644	1.03	1.30	0.844	No
1990	19.90	1.14	0.37	0.77	0.94	0.672	1.04	0.644	1.03	1.30	0.844	No
1991	19.91	1.14	0.37	0.77	0.94	0.672	1.04	0.644	1.03	1.30	0.844	No
1992	19.92	1.14	0.37	0.77	0.94	0.672	1.04	0.644	1.03	1.30	0.843	No
1993	19.93	1.14	0.37	0.77	0.94	0.672	1.04	0.644	1.03	1.30	0.843	No
1994	19.94	1.14	0.37	0.77	0.94	0.672	1.04	0.644	1.03	1.30	0.843	No
1995	19.95	1.15	0.37	0.77	0.94	0.672	1.04	0.644	1.03	1.30	0.843	No
1996	19.96	1.15	0.37	0.77	0.94	0.672	1.04	0.644	1.03	1.30	0.843	No
1997	19.97	1.15	0.37	0.77	0.94	0.672	1.04	0.644	1.03	1.30	0.843	No
1998	19.98	1.15	0.37	0.77	0.94	0.672	1.04	0.644	1.03	1.30	0.844	No
1999	19.99	1.15	0.37	0.77	0.94	0.672	1.04	0.644	1.03	1.30	0.844	No
2000	20.00	1.15	0.37	0.77	0.94	0.672	1.04	0.645	1.03	1.30	0.845	No
2001	20.01	1.15	0.37	0.77	0.94	0.673	1.04	0.645	1.03	1.30	0.845	No
2002	20.02	1.15	0.38	0.77	0.94	0.673	1.04	0.645	1.03	1.30	0.845	No
2003	20.03	1.15	0.38	0.77	0.94	0.673	1.04	0.645	1.03	1.30	0.846	No
2004	20.04	1.15	0.38	0.77	0.94	0.673	1.04	0.645	1.03	1.30	0.846	No
2005	20.05	1.15	0.38	0.77	0.94	0.673	1.04	0.645	1.03	1.30	0.846	No
2006	20.06	1.15	0.38	0.77	0.94	0.673	1.04	0.645	1.03	1.30	0.847	No
2007	20.07	1.15	0.38	0.78	0.94	0.673	1.04	0.645	1.03	1.30	0.847	No
2008	20.08	1.15	0.38	0.78	0.94	0.673	1.04	0.645	1.03	1.30	0.847	No
2009	20.09	1.15	0.38	0.78	0.94	0.673	1.04	0.645	1.02	1.30	0.848	No
2010	20.10	1.15	0.38	0.78	0.94	0.673	1.04	0.645	1.02	1.30	0.848	No
2011	20.11	1.15	0.38	0.78	0.94	0.673	1.04	0.645	1.02	1.30	0.848	No
2012	20.12	1.15	0.38	0.78	0.94	0.673	1.04	0.646	1.02	1.30	0.849	No
2013	20.13	1.15	0.38	0.78	0.94	0.674	1.04	0.646	1.02	1.30	0.849	No
2014	20.14	1.16	0.38	0.78	0.94	0.674	1.04	0.646	1.02	1.30	0.849	No
2015	20.15	1.16	0.38	0.78	0.94	0.674	1.04	0.646	1.02	1.30	0.849	No
2016	20.16	1.16	0.38	0.78	0.94	0.674	1.04	0.646	1.02	1.30	0.849	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
2017	20.17	1.16	0.38	0.78	0.94	0.674	1.04	0.646	1.02	1.30	0.850	No
2018	20.18	1.16	0.38	0.78	0.94	0.674	1.04	0.646	1.02	1.30	0.850	No
2019	20.19	1.16	0.38	0.78	0.94	0.674	1.04	0.646	1.02	1.30	0.850	No
2020	20.20	1.16	0.38	0.78	0.94	0.674	1.04	0.646	1.02	1.30	0.850	No
2021	20.21	1.16	0.38	0.78	0.94	0.674	1.04	0.646	1.02	1.30	0.850	No
2022	20.22	1.16	0.38	0.78	0.94	0.674	1.04	0.646	1.02	1.30	0.850	No
2023	20.23	1.16	0.38	0.78	0.94	0.675	1.04	0.646	1.02	1.30	0.850	No
2024	20.24	1.16	0.38	0.78	0.94	0.675	1.04	0.647	1.02	1.30	0.851	No
2025	20.25	1.16	0.38	0.78	0.94	0.675	1.04	0.647	1.02	1.30	0.851	No
2026	20.26	1.16	0.38	0.78	0.94	0.675	1.04	0.647	1.02	1.30	0.851	No
2027	20.27	1.16	0.38	0.78	0.94	0.675	1.04	0.647	1.02	1.30	0.851	No
2028	20.28	1.16	0.38	0.78	0.94	0.675	1.04	0.647	1.02	1.30	0.851	No
2029	20.29	1.16	0.38	0.78	0.94	0.675	1.04	0.647	1.02	1.30	0.851	No
2030	20.30	1.16	0.38	0.78	0.94	0.675	1.04	0.647	1.02	1.30	0.851	No
2031	20.31	1.16	0.38	0.78	0.94	0.675	1.04	0.647	1.02	1.30	0.852	No
2032	20.32	1.16	0.38	0.78	0.94	0.675	1.04	0.647	1.02	1.30	0.852	No
2033	20.33	1.17	0.38	0.78	0.94	0.675	1.04	0.647	1.02	1.30	0.852	No
2034	20.34	1.17	0.39	0.78	0.94	0.676	1.04	0.647	1.02	1.30	0.852	No
2035	20.35	1.17	0.39	0.78	0.94	0.676	1.04	0.648	1.02	1.30	0.852	No
2036	20.36	1.17	0.39	0.78	0.94	0.676	1.04	0.648	1.02	1.30	0.852	No
2037	20.37	1.17	0.39	0.78	0.94	0.676	1.04	0.648	1.02	1.30	0.852	No
2038	20.38	1.17	0.39	0.78	0.94	0.676	1.04	0.648	1.02	1.30	0.852	No
2039	20.39	1.17	0.39	0.78	0.94	0.676	1.04	0.648	1.02	1.30	0.852	No
2040	20.40	1.17	0.39	0.78	0.94	0.676	1.04	0.648	1.02	1.30	0.852	No
2041	20.41	1.17	0.39	0.78	0.94	0.676	1.04	0.648	1.02	1.30	0.852	No
2042	20.42	1.17	0.39	0.78	0.94	0.676	1.04	0.648	1.02	1.30	0.852	No
2043	20.43	1.17	0.39	0.78	0.94	0.676	1.04	0.648	1.02	1.30	0.852	No
2044	20.44	1.17	0.39	0.78	0.94	0.676	1.04	0.648	1.02	1.30	0.852	No
2045	20.45	1.17	0.39	0.78	0.94	0.676	1.04	0.648	1.02	1.30	0.852	No
2046	20.46	1.17	0.39	0.78	0.94	0.677	1.04	0.648	1.02	1.30	0.852	No
2047	20.47	1.17	0.39	0.78	0.94	0.677	1.04	0.648	1.02	1.30	0.852	No
2048	20.48	1.17	0.39	0.78	0.94	0.677	1.04	0.649	1.02	1.30	0.852	No
2049	20.49	1.17	0.39	0.78	0.94	0.677	1.04	0.649	1.02	1.30	0.852	No
2050	20.50	1.17	0.39	0.78	0.94	0.677	1.04	0.649	1.02	1.30	0.852	No
2051	20.51	1.18	0.39	0.78	0.94	0.677	1.04	0.649	1.02	1.30	0.852	No
2052	20.52	1.18	0.39	0.79	0.94	0.677	1.04	0.649	1.02	1.30	0.852	No
2053	20.53	1.18	0.39	0.79	0.94	0.677	1.04	0.649	1.02	1.30	0.852	No
2054	20.54	1.18	0.39	0.79	0.94	0.677	1.04	0.649	1.03	1.30	0.852	No
2055	20.55	1.18	0.39	0.79	0.94	0.677	1.04	0.649	1.03	1.30	0.852	No
2056	20.56	1.18	0.39	0.79	0.94	0.677	1.04	0.649	1.03	1.30	0.852	No
2057	20.57	1.18	0.39	0.79	0.94	0.677	1.04	0.649	1.03	1.30	0.852	No
2058	20.58	1.18	0.39	0.79	0.94	0.677	1.04	0.649	1.03	1.30	0.852	No
2059	20.59	1.18	0.39	0.79	0.94	0.678	1.04	0.649	1.03	1.30	0.852	No
2060	20.60	1.18	0.39	0.79	0.94	0.678	1.04	0.649	1.03	1.30	0.852	No
2061	20.61	1.18	0.39	0.79	0.94	0.678	1.04	0.650	1.03	1.30	0.852	No
2062	20.62	1.18	0.39	0.79	0.94	0.678	1.04	0.650	1.03	1.30	0.852	No
2063	20.63	1.18	0.39	0.79	0.94	0.678	1.04	0.650	1.03	1.30	0.852	No
2064	20.64	1.18	0.39	0.79	0.94	0.678	1.04	0.650	1.03	1.30	0.852	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
2065	20.65	1.18	0.39	0.79	0.94	0.678	1.04	0.650	1.03	1.30	0.852	No
2066	20.66	1.18	0.39	0.79	0.94	0.678	1.04	0.650	1.03	1.30	0.852	No
2067	20.67	1.18	0.40	0.79	0.94	0.678	1.04	0.650	1.03	1.30	0.852	No
2068	20.68	1.19	0.40	0.79	0.94	0.678	1.04	0.650	1.03	1.30	0.852	No
2069	20.69	1.19	0.40	0.79	0.94	0.678	1.04	0.650	1.03	1.30	0.852	No
2070	20.70	1.19	0.40	0.79	0.94	0.678	1.04	0.650	1.03	1.30	0.852	No
2071	20.71	1.19	0.40	0.79	0.94	0.678	1.04	0.650	1.03	1.30	0.852	No
2072	20.72	1.19	0.40	0.79	0.94	0.678	1.04	0.650	1.03	1.30	0.852	No
2073	20.73	1.19	0.40	0.79	0.94	0.679	1.04	0.650	1.03	1.30	0.852	No
2074	20.74	1.19	0.40	0.79	0.94	0.679	1.04	0.650	1.03	1.30	0.852	No
2075	20.75	1.19	0.40	0.79	0.94	0.679	1.04	0.651	1.03	1.30	0.853	No
2076	20.76	1.19	0.40	0.79	0.94	0.679	1.04	0.651	1.03	1.30	0.853	No
2077	20.77	1.19	0.40	0.79	0.94	0.679	1.04	0.651	1.03	1.30	0.853	No
2078	20.78	1.19	0.40	0.79	0.94	0.679	1.04	0.651	1.03	1.30	0.853	No
2079	20.79	1.19	0.40	0.79	0.94	0.679	1.04	0.651	1.03	1.30	0.853	No
2080	20.80	1.19	0.40	0.79	0.94	0.679	1.04	0.651	1.03	1.30	0.853	No
2081	20.81	1.19	0.40	0.79	0.94	0.679	1.04	0.651	1.03	1.30	0.854	No
2082	20.82	1.19	0.40	0.79	0.94	0.679	1.04	0.651	1.03	1.30	0.854	No
2083	20.83	1.19	0.40	0.79	0.94	0.679	1.04	0.651	1.03	1.30	0.854	No
2084	20.84	1.19	0.40	0.79	0.94	0.679	1.04	0.651	1.03	1.30	0.854	No
2085	20.85	1.19	0.40	0.79	0.94	0.679	1.04	0.651	1.02	1.30	0.854	No
2086	20.86	1.20	0.40	0.79	0.94	0.679	1.04	0.651	1.02	1.30	0.855	No
2087	20.87	1.20	0.40	0.79	0.94	0.680	1.04	0.651	1.02	1.30	0.855	No
2088	20.88	1.20	0.40	0.79	0.94	0.680	1.04	0.651	1.02	1.30	0.855	No
2089	20.89	1.20	0.40	0.79	0.94	0.680	1.04	0.651	1.02	1.30	0.856	No
2090	20.90	1.20	0.40	0.80	0.94	0.680	1.04	0.652	1.02	1.30	0.856	No
2091	20.91	1.20	0.40	0.80	0.94	0.680	1.04	0.652	1.02	1.30	0.856	No
2092	20.92	1.20	0.40	0.80	0.94	0.680	1.04	0.652	1.02	1.30	0.856	No
2093	20.93	1.20	0.40	0.80	0.94	0.680	1.04	0.652	1.02	1.30	0.856	No
2094	20.94	1.20	0.40	0.80	0.94	0.680	1.04	0.652	1.02	1.30	0.857	No
2095	20.95	1.20	0.40	0.80	0.94	0.680	1.04	0.652	1.02	1.30	0.857	No
2096	20.96	1.20	0.40	0.80	0.94	0.680	1.04	0.652	1.02	1.30	0.857	No
2097	20.97	1.20	0.40	0.80	0.94	0.680	1.04	0.652	1.02	1.30	0.857	No
2098	20.98	1.20	0.40	0.80	0.94	0.680	1.04	0.652	1.02	1.30	0.857	No
2099	20.99	1.20	0.41	0.80	0.94	0.680	1.04	0.652	1.02	1.30	0.858	No
2100	21.00	1.20	0.41	0.80	0.94	0.681	1.04	0.652	1.02	1.30	0.858	No
2101	21.01	1.20	0.41	0.80	0.94	0.681	1.04	0.652	1.02	1.30	0.858	No
2102	21.02	1.20	0.41	0.80	0.94	0.681	1.04	0.652	1.02	1.30	0.858	No
2103	21.03	1.20	0.41	0.80	0.94	0.681	1.04	0.653	1.02	1.30	0.858	No
2104	21.04	1.21	0.41	0.80	0.94	0.681	1.04	0.653	1.02	1.30	0.859	No
2105	21.05	1.21	0.41	0.80	0.94	0.681	1.04	0.653	1.02	1.30	0.859	No
2106	21.06	1.21	0.41	0.80	0.94	0.681	1.04	0.653	1.02	1.30	0.859	No
2107	21.07	1.21	0.41	0.80	0.94	0.681	1.04	0.653	1.02	1.30	0.859	No
2108	21.08	1.21	0.41	0.80	0.94	0.681	1.04	0.653	1.02	1.30	0.859	No
2109	21.09	1.21	0.41	0.80	0.94	0.681	1.04	0.653	1.02	1.30	0.860	No
2110	21.10	1.21	0.41	0.80	0.94	0.681	1.04	0.653	1.02	1.30	0.860	No
2111	21.11	1.21	0.41	0.80	0.94	0.681	1.04	0.653	1.02	1.30	0.860	No
2112	21.12	1.21	0.41	0.80	0.94	0.681	1.04	0.653	1.02	1.30	0.860	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
2113	21.13	1.21	0.41	0.80	0.94	0.682	1.04	0.653	1.02	1.30	0.860	No
2114	21.14	1.21	0.41	0.80	0.94	0.682	1.04	0.653	1.02	1.30	0.860	No
2115	21.15	1.21	0.41	0.80	0.94	0.682	1.04	0.653	1.02	1.30	0.860	No
2116	21.16	1.21	0.41	0.80	0.94	0.682	1.04	0.653	1.02	1.30	0.861	No
2117	21.17	1.21	0.41	0.80	0.94	0.682	1.04	0.654	1.02	1.30	0.861	No
2118	21.18	1.21	0.41	0.80	0.94	0.682	1.04	0.654	1.02	1.30	0.861	No
2119	21.19	1.21	0.41	0.80	0.94	0.682	1.04	0.654	1.02	1.30	0.861	No
2120	21.20	1.21	0.41	0.80	0.94	0.682	1.04	0.654	1.02	1.30	0.861	No
2121	21.21	1.21	0.41	0.80	0.94	0.682	1.04	0.654	1.02	1.30	0.861	No
2122	21.22	1.22	0.41	0.80	0.94	0.682	1.04	0.654	1.02	1.30	0.861	No
2123	21.23	1.22	0.41	0.80	0.94	0.682	1.04	0.654	1.02	1.30	0.861	No
2124	21.24	1.22	0.41	0.80	0.94	0.682	1.04	0.654	1.02	1.30	0.861	No
2125	21.25	1.22	0.41	0.80	0.94	0.682	1.04	0.654	1.02	1.30	0.861	No
2126	21.26	1.22	0.41	0.80	0.94	0.683	1.04	0.654	1.02	1.30	0.861	No
2127	21.27	1.22	0.41	0.80	0.94	0.683	1.04	0.654	1.02	1.30	0.861	No
2128	21.28	1.22	0.41	0.80	0.94	0.683	1.04	0.654	1.02	1.30	0.861	No
2129	21.29	1.22	0.41	0.80	0.94	0.683	1.04	0.654	1.02	1.30	0.861	No
2130	21.30	1.22	0.41	0.80	0.94	0.683	1.04	0.654	1.02	1.30	0.860	No
2131	21.31	1.22	0.42	0.81	0.94	0.683	1.04	0.655	1.02	1.30	0.860	No
2132	21.32	1.22	0.42	0.81	0.94	0.683	1.04	0.655	1.02	1.30	0.860	No
2133	21.33	1.22	0.42	0.81	0.94	0.683	1.04	0.655	1.02	1.30	0.860	No
2134	21.34	1.22	0.42	0.81	0.94	0.683	1.04	0.655	1.02	1.30	0.860	No
2135	21.35	1.22	0.42	0.81	0.94	0.683	1.04	0.655	1.02	1.30	0.860	No
2136	21.36	1.22	0.42	0.81	0.94	0.683	1.04	0.655	1.02	1.30	0.860	No
2137	21.37	1.22	0.42	0.81	0.94	0.683	1.04	0.655	1.02	1.30	0.860	No
2138	21.38	1.22	0.42	0.81	0.94	0.683	1.04	0.655	1.02	1.30	0.860	No
2139	21.39	1.22	0.42	0.81	0.94	0.683	1.04	0.655	1.02	1.30	0.860	No
2140	21.40	1.23	0.42	0.81	0.94	0.684	1.04	0.655	1.02	1.30	0.860	No
2141	21.41	1.23	0.42	0.81	0.94	0.684	1.04	0.655	1.02	1.30	0.860	No
2142	21.42	1.23	0.42	0.81	0.94	0.684	1.04	0.655	1.02	1.30	0.860	No
2143	21.43	1.23	0.42	0.81	0.94	0.684	1.04	0.655	1.02	1.30	0.860	No
2144	21.44	1.23	0.42	0.81	0.94	0.684	1.04	0.655	1.02	1.30	0.860	No
2145	21.45	1.23	0.42	0.81	0.94	0.684	1.04	0.655	1.02	1.30	0.860	No
2146	21.46	1.23	0.42	0.81	0.94	0.684	1.04	0.656	1.02	1.30	0.860	No
2147	21.47	1.23	0.42	0.81	0.94	0.684	1.04	0.656	1.02	1.30	0.860	No
2148	21.48	1.23	0.42	0.81	0.94	0.684	1.04	0.656	1.02	1.30	0.859	No
2149	21.49	1.23	0.42	0.81	0.94	0.684	1.04	0.656	1.02	1.30	0.859	No
2150	21.50	1.23	0.42	0.81	0.94	0.684	1.04	0.656	1.02	1.30	0.859	No
2151	21.51	1.23	0.42	0.81	0.94	0.684	1.04	0.656	1.02	1.30	0.859	No
2152	21.52	1.23	0.42	0.81	0.94	0.684	1.04	0.656	1.02	1.30	0.859	No
2153	21.53	1.23	0.42	0.81	0.94	0.684	1.04	0.656	1.02	1.30	0.859	No
2154	21.54	1.23	0.42	0.81	0.94	0.684	1.04	0.656	1.02	1.30	0.859	No
2155	21.55	1.23	0.42	0.81	0.94	0.684	1.04	0.656	1.02	1.30	0.860	No
2156	21.56	1.23	0.42	0.81	0.94	0.685	1.04	0.656	1.02	1.30	0.860	No
2157	21.57	1.24	0.42	0.81	0.94	0.685	1.04	0.656	1.02	1.30	0.860	No
2158	21.58	1.24	0.42	0.81	0.94	0.685	1.04	0.656	1.02	1.30	0.860	No
2159	21.59	1.24	0.42	0.81	0.94	0.685	1.04	0.656	1.02	1.30	0.860	No
2160	21.60	1.24	0.42	0.81	0.94	0.685	1.04	0.656	1.02	1.30	0.860	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
2161	21.61	1.24	0.42	0.81	0.94	0.685	1.04	0.656	1.02	1.30	0.860	No
2162	21.62	1.24	0.42	0.81	0.94	0.685	1.04	0.656	1.02	1.30	0.861	No
2163	21.63	1.24	0.43	0.81	0.94	0.685	1.04	0.657	1.02	1.30	0.861	No
2164	21.64	1.24	0.43	0.81	0.94	0.685	1.04	0.657	1.02	1.30	0.861	No
2165	21.65	1.24	0.43	0.81	0.94	0.685	1.04	0.657	1.02	1.30	0.862	No
2166	21.66	1.24	0.43	0.81	0.94	0.685	1.04	0.657	1.02	1.30	0.862	No
2167	21.67	1.24	0.43	0.81	0.94	0.685	1.04	0.657	1.02	1.30	0.863	No
2168	21.68	1.24	0.43	0.81	0.94	0.685	1.04	0.657	1.02	1.30	0.863	No
2169	21.69	1.24	0.43	0.82	0.94	0.685	1.04	0.657	1.02	1.30	0.863	No
2170	21.70	1.24	0.43	0.82	0.93	0.685	1.04	0.657	1.02	1.30	0.863	No
2171	21.71	1.24	0.43	0.82	0.93	0.686	1.04	0.657	1.02	1.30	0.864	No
2172	21.72	1.24	0.43	0.82	0.93	0.686	1.04	0.657	1.02	1.30	0.864	No
2173	21.73	1.24	0.43	0.82	0.93	0.686	1.04	0.657	1.02	1.30	0.864	No
2174	21.74	1.25	0.43	0.82	0.93	0.686	1.04	0.657	1.02	1.30	0.864	No
2175	21.75	1.25	0.43	0.82	0.93	0.686	1.04	0.657	1.02	1.30	0.865	No
2176	21.76	1.25	0.43	0.82	0.93	0.686	1.04	0.657	1.02	1.30	0.865	No
2177	21.77	1.25	0.43	0.82	0.93	0.686	1.04	0.657	1.02	1.30	0.865	No
2178	21.78	1.25	0.43	0.82	0.93	0.686	1.04	0.658	1.02	1.30	0.866	No
2179	21.79	1.25	0.43	0.82	0.93	0.686	1.04	0.658	1.02	1.30	0.866	No
2180	21.80	1.25	0.43	0.82	0.93	0.686	1.04	0.658	1.02	1.30	0.866	No
2181	21.81	1.25	0.43	0.82	0.93	0.686	1.04	0.658	1.02	1.30	0.866	No
2182	21.82	1.25	0.43	0.82	0.93	0.686	1.04	0.658	1.02	1.30	0.867	No
2183	21.83	1.25	0.43	0.82	0.93	0.686	1.04	0.658	1.02	1.30	0.867	No
2184	21.84	1.25	0.43	0.82	0.93	0.686	1.04	0.658	1.02	1.30	0.867	No
2185	21.85	1.25	0.43	0.82	0.93	0.687	1.04	0.658	1.02	1.30	0.867	No
2186	21.86	1.25	0.43	0.82	0.93	0.687	1.04	0.658	1.02	1.30	0.868	No
2187	21.87	1.25	0.43	0.82	0.93	0.687	1.04	0.658	1.02	1.30	0.868	No
2188	21.88	1.25	0.43	0.82	0.93	0.687	1.04	0.658	1.02	1.30	0.868	No
2189	21.89	1.25	0.43	0.82	0.93	0.687	1.04	0.658	1.02	1.30	0.868	No
2190	21.90	1.25	0.43	0.82	0.93	0.687	1.04	0.658	1.02	1.30	0.868	No
2191	21.91	1.25	0.43	0.82	0.93	0.687	1.04	0.658	1.02	1.30	0.869	No
2192	21.92	1.26	0.43	0.82	0.93	0.687	1.04	0.658	1.02	1.30	0.869	No
2193	21.93	1.26	0.43	0.82	0.93	0.687	1.04	0.659	1.02	1.30	0.869	No
2194	21.94	1.26	0.43	0.82	0.93	0.687	1.04	0.659	1.02	1.30	0.869	No
2195	21.95	1.26	0.44	0.82	0.93	0.687	1.04	0.659	1.02	1.30	0.870	No
2196	21.96	1.26	0.44	0.82	0.93	0.687	1.04	0.659	1.02	1.30	0.870	No
2197	21.97	1.26	0.44	0.82	0.93	0.687	1.04	0.659	1.02	1.30	0.870	No
2198	21.98	1.26	0.44	0.82	0.93	0.687	1.04	0.659	1.02	1.30	0.870	No
2199	21.99	1.26	0.44	0.82	0.93	0.688	1.04	0.659	1.02	1.30	0.870	No
2200	22.00	1.26	0.44	0.82	0.93	0.688	1.04	0.659	1.02	1.30	0.870	No
2201	22.01	1.26	0.44	0.82	0.93	0.688	1.04	0.659	1.02	1.30	0.870	No
2202	22.02	1.26	0.44	0.82	0.93	0.688	1.04	0.659	1.02	1.30	0.871	No
2203	22.03	1.26	0.44	0.82	0.93	0.688	1.04	0.659	1.02	1.30	0.871	No
2204	22.04	1.26	0.44	0.82	0.93	0.688	1.04	0.659	1.02	1.30	0.871	No
2205	22.05	1.26	0.44	0.82	0.93	0.688	1.04	0.659	1.02	1.30	0.871	No
2206	22.06	1.26	0.44	0.82	0.93	0.688	1.04	0.660	1.02	1.30	0.871	No
2207	22.07	1.26	0.44	0.82	0.93	0.688	1.04	0.660	1.02	1.30	0.871	No
2208	22.08	1.26	0.44	0.82	0.93	0.688	1.04	0.660	1.02	1.30	0.871	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
2209	22.09	1.26	0.44	0.82	0.93	0.688	1.04	0.660	1.02	1.30	0.871	No
2210	22.10	1.26	0.44	0.82	0.93	0.688	1.04	0.660	1.02	1.30	0.872	No
2211	22.11	1.27	0.44	0.82	0.93	0.688	1.04	0.660	1.02	1.30	0.872	No
2212	22.12	1.27	0.44	0.83	0.93	0.689	1.04	0.660	1.02	1.30	0.872	No
2213	22.13	1.27	0.44	0.83	0.93	0.689	1.04	0.660	1.02	1.30	0.872	No
2214	22.14	1.27	0.44	0.83	0.93	0.689	1.04	0.660	1.02	1.30	0.872	No
2215	22.15	1.27	0.44	0.83	0.93	0.689	1.04	0.660	1.02	1.30	0.872	No
2216	22.16	1.27	0.44	0.83	0.93	0.689	1.04	0.660	1.02	1.30	0.872	No
2217	22.17	1.27	0.44	0.83	0.93	0.689	1.04	0.660	1.02	1.30	0.872	No
2218	22.18	1.27	0.44	0.83	0.93	0.689	1.04	0.660	1.02	1.30	0.872	No
2219	22.19	1.27	0.44	0.83	0.93	0.689	1.04	0.660	1.02	1.30	0.873	No
2220	22.20	1.27	0.44	0.83	0.93	0.689	1.04	0.661	1.02	1.30	0.873	No
2221	22.21	1.27	0.44	0.83	0.93	0.689	1.04	0.661	1.02	1.30	0.873	No
2222	22.22	1.27	0.44	0.83	0.93	0.689	1.04	0.661	1.02	1.30	0.873	No
2223	22.23	1.27	0.44	0.83	0.93	0.689	1.04	0.661	1.02	1.30	0.873	No
2224	22.24	1.27	0.44	0.83	0.93	0.689	1.04	0.661	1.02	1.30	0.873	No
2225	22.25	1.27	0.44	0.83	0.93	0.690	1.04	0.661	1.02	1.30	0.873	No
2226	22.26	1.27	0.44	0.83	0.93	0.690	1.04	0.661	1.02	1.30	0.873	No
2227	22.27	1.27	0.45	0.83	0.93	0.690	1.04	0.661	1.02	1.30	0.874	No
2228	22.28	1.27	0.45	0.83	0.93	0.690	1.04	0.661	1.02	1.30	0.874	No
2229	22.29	1.27	0.45	0.83	0.93	0.690	1.04	0.661	1.02	1.30	0.874	No
2230	22.30	1.28	0.45	0.83	0.93	0.690	1.04	0.661	1.02	1.30	0.874	No
2231	22.31	1.28	0.45	0.83	0.93	0.690	1.04	0.661	1.02	1.30	0.874	No
2232	22.32	1.28	0.45	0.83	0.93	0.690	1.04	0.661	1.02	1.30	0.874	No
2233	22.33	1.28	0.45	0.83	0.93	0.690	1.04	0.662	1.02	1.30	0.874	No
2234	22.34	1.28	0.45	0.83	0.93	0.690	1.04	0.662	1.02	1.30	0.874	No
2235	22.35	1.28	0.45	0.83	0.93	0.690	1.04	0.662	1.02	1.30	0.874	No
2236	22.36	1.28	0.45	0.83	0.93	0.690	1.04	0.662	1.02	1.30	0.874	No
2237	22.37	1.28	0.45	0.83	0.93	0.690	1.04	0.662	1.02	1.30	0.875	No
2238	22.38	1.28	0.45	0.83	0.93	0.691	1.04	0.662	1.02	1.30	0.875	No
2239	22.39	1.28	0.45	0.83	0.93	0.691	1.04	0.662	1.02	1.30	0.875	No
2240	22.40	1.28	0.45	0.83	0.93	0.691	1.04	0.662	1.02	1.30	0.875	No
2241	22.41	1.28	0.45	0.83	0.93	0.691	1.04	0.662	1.02	1.30	0.875	No
2242	22.42	1.28	0.45	0.83	0.93	0.691	1.04	0.662	1.02	1.30	0.875	No
2243	22.43	1.28	0.45	0.83	0.93	0.691	1.04	0.662	1.02	1.30	0.875	No
2244	22.44	1.28	0.45	0.83	0.93	0.691	1.04	0.662	1.02	1.30	0.875	No
2245	22.45	1.28	0.45	0.83	0.93	0.691	1.04	0.662	1.02	1.30	0.875	No
2246	22.46	1.28	0.45	0.83	0.93	0.691	1.04	0.662	1.02	1.30	0.875	No
2247	22.47	1.28	0.45	0.83	0.93	0.691	1.04	0.663	1.02	1.30	0.876	No
2248	22.48	1.28	0.45	0.83	0.93	0.691	1.04	0.663	1.02	1.30	0.876	No
2249	22.49	1.28	0.45	0.83	0.93	0.691	1.04	0.663	1.02	1.30	0.876	No
2250	22.50	1.29	0.45	0.83	0.93	0.691	1.04	0.663	1.02	1.30	0.876	No
2251	22.51	1.29	0.45	0.83	0.93	0.692	1.04	0.663	1.02	1.30	0.876	No
2252	22.52	1.29	0.45	0.83	0.93	0.692	1.04	0.663	1.02	1.30	0.876	No
2253	22.53	1.29	0.45	0.83	0.93	0.692	1.04	0.663	1.02	1.30	0.876	No
2254	22.54	1.29	0.45	0.83	0.93	0.692	1.04	0.663	1.02	1.30	0.876	No
2255	22.55	1.29	0.45	0.83	0.93	0.692	1.04	0.663	1.02	1.30	0.876	No
2256	22.56	1.29	0.45	0.83	0.93	0.692	1.04	0.663	1.02	1.30	0.876	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
2257	22.57	1.29	0.45	0.83	0.93	0.692	1.04	0.663	1.02	1.30	0.876	No
2258	22.58	1.29	0.45	0.83	0.93	0.692	1.04	0.663	1.02	1.30	0.877	No
2259	22.59	1.29	0.46	0.83	0.93	0.692	1.04	0.663	1.02	1.30	0.877	No
2260	22.60	1.29	0.46	0.84	0.93	0.692	1.04	0.663	1.02	1.30	0.877	No
2261	22.61	1.29	0.46	0.84	0.93	0.692	1.04	0.664	1.02	1.30	0.877	No
2262	22.62	1.29	0.46	0.84	0.93	0.692	1.04	0.664	1.02	1.30	0.877	No
2263	22.63	1.29	0.46	0.84	0.93	0.692	1.04	0.664	1.02	1.30	0.877	No
2264	22.64	1.29	0.46	0.84	0.93	0.692	1.04	0.664	1.02	1.30	0.877	No
2265	22.65	1.29	0.46	0.84	0.93	0.693	1.04	0.664	1.02	1.30	0.877	No
2266	22.66	1.29	0.46	0.84	0.93	0.693	1.04	0.664	1.02	1.30	0.878	No
2267	22.67	1.29	0.46	0.84	0.93	0.693	1.04	0.664	1.02	1.30	0.878	No
2268	22.68	1.29	0.46	0.84	0.93	0.693	1.04	0.664	1.02	1.30	0.878	No
2269	22.69	1.30	0.46	0.84	0.93	0.693	1.04	0.664	1.02	1.30	0.878	No
2270	22.70	1.30	0.46	0.84	0.93	0.693	1.04	0.664	1.02	1.30	0.878	No
2271	22.71	1.30	0.46	0.84	0.93	0.693	1.04	0.664	1.02	1.30	0.878	No
2272	22.72	1.30	0.46	0.84	0.93	0.693	1.04	0.664	1.02	1.30	0.879	No
2273	22.73	1.30	0.46	0.84	0.93	0.693	1.04	0.664	1.02	1.30	0.879	No
2274	22.74	1.30	0.46	0.84	0.93	0.693	1.04	0.664	1.02	1.30	0.879	No
2275	22.75	1.30	0.46	0.84	0.93	0.693	1.04	0.665	1.02	1.30	0.879	No
2276	22.76	1.30	0.46	0.84	0.93	0.693	1.04	0.665	1.02	1.30	0.879	No
2277	22.77	1.30	0.46	0.84	0.93	0.693	1.04	0.665	1.02	1.30	0.879	No
2278	22.78	1.30	0.46	0.84	0.93	0.694	1.04	0.665	1.02	1.30	0.879	No
2279	22.79	1.30	0.46	0.84	0.93	0.694	1.04	0.665	1.02	1.30	0.879	No
2280	22.80	1.30	0.46	0.84	0.93	0.694	1.04	0.665	1.02	1.30	0.879	No
2281	22.81	1.30	0.46	0.84	0.93	0.694	1.04	0.665	1.02	1.30	0.880	No
2282	22.82	1.30	0.46	0.84	0.93	0.694	1.04	0.665	1.02	1.30	0.880	No
2283	22.83	1.30	0.46	0.84	0.93	0.694	1.04	0.665	1.02	1.30	0.880	No
2284	22.84	1.30	0.46	0.84	0.93	0.694	1.04	0.665	1.02	1.30	0.880	No
2285	22.85	1.30	0.46	0.84	0.93	0.694	1.04	0.665	1.02	1.30	0.880	No
2286	22.86	1.30	0.46	0.84	0.93	0.694	1.04	0.665	1.02	1.30	0.880	No
2287	22.87	1.30	0.46	0.84	0.93	0.694	1.04	0.665	1.02	1.30	0.880	No
2288	22.88	1.31	0.46	0.84	0.93	0.694	1.04	0.665	1.02	1.30	0.880	No
2289	22.89	1.31	0.46	0.84	0.93	0.694	1.04	0.665	1.02	1.30	0.880	No
2290	22.90	1.31	0.46	0.84	0.93	0.694	1.04	0.666	1.02	1.30	0.881	No
2291	22.91	1.31	0.47	0.84	0.93	0.694	1.04	0.666	1.02	1.30	0.881	No
2292	22.92	1.31	0.47	0.84	0.93	0.695	1.04	0.666	1.02	1.30	0.881	No
2293	22.93	1.31	0.47	0.84	0.93	0.695	1.04	0.666	1.02	1.30	0.881	No
2294	22.94	1.31	0.47	0.84	0.93	0.695	1.04	0.666	1.02	1.30	0.881	No
2295	22.95	1.31	0.47	0.84	0.93	0.695	1.04	0.666	1.02	1.30	0.881	No
2296	22.96	1.31	0.47	0.84	0.93	0.695	1.04	0.666	1.02	1.30	0.881	No
2297	22.97	1.31	0.47	0.84	0.93	0.695	1.04	0.666	1.02	1.30	0.881	No
2298	22.98	1.31	0.47	0.84	0.93	0.695	1.04	0.666	1.02	1.30	0.881	No
2299	22.99	1.31	0.47	0.84	0.93	0.695	1.04	0.666	1.02	1.30	0.882	No
2300	23.00	1.31	0.47	0.84	0.93	0.695	1.04	0.666	1.02	1.30	0.882	No
2301	23.01	1.31	0.47	0.84	0.93	0.695	1.04	0.666	1.02	1.30	0.882	No
2302	23.02	1.31	0.47	0.84	0.93	0.695	1.04	0.666	1.02	1.30	0.882	No
2303	23.03	1.31	0.47	0.84	0.93	0.695	1.04	0.666	1.02	1.30	0.882	No
2304	23.04	1.31	0.47	0.84	0.93	0.695	1.04	0.667	1.02	1.30	0.882	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
2305	23.05	1.31	0.47	0.84	0.93	0.696	1.04	0.667	1.02	1.30	0.882	No
2306	23.06	1.31	0.47	0.84	0.93	0.696	1.04	0.667	1.02	1.30	0.882	No
2307	23.07	1.32	0.47	0.85	0.93	0.696	1.04	0.667	1.02	1.30	0.882	No
2308	23.08	1.32	0.47	0.85	0.93	0.696	1.04	0.667	1.02	1.30	0.882	No
2309	23.09	1.32	0.47	0.85	0.93	0.696	1.04	0.667	1.02	1.30	0.882	No
2310	23.10	1.32	0.47	0.85	0.93	0.696	1.04	0.667	1.02	1.30	0.882	No
2311	23.11	1.32	0.47	0.85	0.93	0.696	1.04	0.667	1.02	1.30	0.882	No
2312	23.12	1.32	0.47	0.85	0.93	0.696	1.04	0.667	1.02	1.30	0.882	No
2313	23.13	1.32	0.47	0.85	0.93	0.696	1.04	0.667	1.02	1.30	0.882	No
2314	23.14	1.32	0.47	0.85	0.93	0.696	1.04	0.667	1.02	1.30	0.882	No
2315	23.15	1.32	0.47	0.85	0.93	0.696	1.04	0.667	1.02	1.30	0.882	No
2316	23.16	1.32	0.47	0.85	0.93	0.696	1.04	0.667	1.02	1.30	0.882	No
2317	23.17	1.32	0.47	0.85	0.93	0.696	1.04	0.667	1.02	1.30	0.883	No
2318	23.18	1.32	0.47	0.85	0.93	0.696	1.04	0.667	1.02	1.30	0.883	No
2319	23.19	1.32	0.47	0.85	0.93	0.696	1.04	0.668	1.02	1.30	0.883	No
2320	23.20	1.32	0.47	0.85	0.93	0.696	1.04	0.668	1.02	1.30	0.883	No
2321	23.21	1.32	0.47	0.85	0.93	0.697	1.04	0.668	1.02	1.30	0.883	No
2322	23.22	1.32	0.47	0.85	0.93	0.697	1.04	0.668	1.02	1.30	0.883	No
2323	23.23	1.32	0.48	0.85	0.93	0.697	1.04	0.668	1.02	1.30	0.883	No
2324	23.24	1.32	0.48	0.85	0.93	0.697	1.04	0.668	1.02	1.30	0.883	No
2325	23.25	1.32	0.48	0.85	0.93	0.697	1.04	0.668	1.02	1.30	0.883	No
2326	23.26	1.33	0.48	0.85	0.93	0.697	1.04	0.668	1.02	1.30	0.884	No
2327	23.27	1.33	0.48	0.85	0.93	0.697	1.04	0.668	1.02	1.30	0.884	No
2328	23.28	1.33	0.48	0.85	0.93	0.697	1.04	0.668	1.02	1.30	0.884	No
2329	23.29	1.33	0.48	0.85	0.93	0.697	1.04	0.668	1.02	1.30	0.884	No
2330	23.30	1.33	0.48	0.85	0.93	0.697	1.04	0.668	1.02	1.30	0.884	No
2331	23.31	1.33	0.48	0.85	0.93	0.697	1.04	0.668	1.02	1.30	0.884	No
2332	23.32	1.33	0.48	0.85	0.93	0.697	1.04	0.668	1.02	1.30	0.884	No
2333	23.33	1.33	0.48	0.85	0.93	0.697	1.04	0.668	1.02	1.30	0.884	No
2334	23.34	1.33	0.48	0.85	0.93	0.697	1.04	0.668	1.02	1.30	0.884	No
2335	23.35	1.33	0.48	0.85	0.93	0.697	1.04	0.668	1.02	1.30	0.884	No
2336	23.36	1.33	0.48	0.85	0.93	0.698	1.04	0.669	1.02	1.30	0.884	No
2337	23.37	1.33	0.48	0.85	0.93	0.698	1.04	0.669	1.02	1.30	0.884	No
2338	23.38	1.33	0.48	0.85	0.93	0.698	1.04	0.669	1.02	1.30	0.884	No
2339	23.39	1.33	0.48	0.85	0.93	0.698	1.04	0.669	1.02	1.30	0.884	No
2340	23.40	1.33	0.48	0.85	0.93	0.698	1.04	0.669	1.02	1.30	0.885	No
2341	23.41	1.33	0.48	0.85	0.93	0.698	1.04	0.669	1.02	1.30	0.885	No
2342	23.42	1.33	0.48	0.85	0.93	0.698	1.04	0.669	1.02	1.30	0.885	No
2343	23.43	1.33	0.48	0.85	0.93	0.698	1.04	0.669	1.02	1.30	0.885	No
2344	23.44	1.34	0.48	0.85	0.93	0.698	1.04	0.669	1.02	1.30	0.885	No
2345	23.45	1.34	0.48	0.85	0.93	0.698	1.04	0.669	1.02	1.30	0.885	No
2346	23.46	1.34	0.48	0.85	0.93	0.698	1.04	0.669	1.02	1.30	0.885	No
2347	23.47	1.34	0.48	0.85	0.93	0.698	1.04	0.669	1.02	1.30	0.885	No
2348	23.48	1.34	0.48	0.85	0.93	0.698	1.04	0.669	1.02	1.30	0.885	No
2349	23.49	1.34	0.48	0.85	0.93	0.698	1.04	0.669	1.02	1.30	0.885	No
2350	23.50	1.34	0.48	0.86	0.93	0.698	1.04	0.669	1.02	1.30	0.885	No
2351	23.51	1.34	0.48	0.86	0.93	0.698	1.04	0.669	1.02	1.30	0.885	No
2352	23.52	1.34	0.48	0.86	0.93	0.698	1.04	0.669	1.02	1.30	0.885	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
2353	23.53	1.34	0.48	0.86	0.93	0.699	1.04	0.670	1.02	1.30	0.885	No
2354	23.54	1.34	0.48	0.86	0.93	0.699	1.04	0.670	1.02	1.30	0.885	No
2355	23.55	1.34	0.49	0.86	0.93	0.699	1.04	0.670	1.02	1.30	0.885	No
2356	23.56	1.34	0.49	0.86	0.93	0.699	1.04	0.670	1.02	1.30	0.886	No
2357	23.57	1.34	0.49	0.86	0.93	0.699	1.04	0.670	1.02	1.30	0.886	No
2358	23.58	1.34	0.49	0.86	0.93	0.699	1.04	0.670	1.02	1.30	0.886	No
2359	23.59	1.34	0.49	0.86	0.93	0.699	1.04	0.670	1.02	1.30	0.886	No
2360	23.60	1.34	0.49	0.86	0.93	0.699	1.04	0.670	1.02	1.30	0.886	No
2361	23.61	1.34	0.49	0.86	0.93	0.699	1.04	0.670	1.02	1.30	0.886	No
2362	23.62	1.35	0.49	0.86	0.93	0.699	1.04	0.670	1.02	1.30	0.886	No
2363	23.63	1.35	0.49	0.86	0.93	0.699	1.04	0.670	1.02	1.30	0.886	No
2364	23.64	1.35	0.49	0.86	0.93	0.699	1.04	0.670	1.02	1.30	0.886	No
2365	23.65	1.35	0.49	0.86	0.93	0.699	1.04	0.670	1.02	1.30	0.886	No
2366	23.66	1.35	0.49	0.86	0.93	0.699	1.04	0.670	1.02	1.30	0.886	No
2367	23.67	1.35	0.49	0.86	0.93	0.699	1.04	0.670	1.02	1.30	0.886	No
2368	23.68	1.35	0.49	0.86	0.93	0.699	1.04	0.670	1.02	1.30	0.886	No
2369	23.69	1.35	0.49	0.86	0.93	0.699	1.04	0.670	1.02	1.30	0.886	No
2370	23.70	1.35	0.49	0.86	0.93	0.699	1.04	0.670	1.02	1.30	0.886	No
2371	23.71	1.35	0.49	0.86	0.93	0.700	1.04	0.670	1.02	1.30	0.887	No
2372	23.72	1.35	0.49	0.86	0.93	0.700	1.04	0.671	1.02	1.30	0.887	No
2373	23.73	1.35	0.49	0.86	0.93	0.700	1.04	0.671	1.02	1.30	0.887	No
2374	23.74	1.35	0.49	0.86	0.93	0.700	1.04	0.671	1.02	1.30	0.887	No
2375	23.75	1.35	0.49	0.86	0.93	0.700	1.04	0.671	1.02	1.30	0.887	No
2376	23.76	1.35	0.49	0.86	0.93	0.700	1.04	0.671	1.02	1.30	0.887	No
2377	23.77	1.35	0.49	0.86	0.93	0.700	1.04	0.671	1.02	1.30	0.887	No
2378	23.78	1.35	0.49	0.86	0.93	0.700	1.04	0.671	1.02	1.30	0.887	No
2379	23.79	1.35	0.49	0.86	0.93	0.700	1.04	0.671	1.02	1.30	0.887	No
2380	23.80	1.36	0.49	0.86	0.93	0.700	1.04	0.671	1.02	1.30	0.887	No
2381	23.81	1.36	0.49	0.86	0.93	0.700	1.04	0.671	1.02	1.30	0.887	No
2382	23.82	1.36	0.49	0.86	0.93	0.700	1.04	0.671	1.02	1.30	0.887	No
2383	23.83	1.36	0.49	0.86	0.93	0.700	1.04	0.671	1.02	1.30	0.887	No
2384	23.84	1.36	0.49	0.86	0.93	0.700	1.04	0.671	1.02	1.30	0.887	No
2385	23.85	1.36	0.49	0.86	0.93	0.700	1.04	0.671	1.02	1.30	0.887	No
2386	23.86	1.36	0.49	0.86	0.93	0.700	1.04	0.671	1.02	1.30	0.887	No
2387	23.87	1.36	0.50	0.86	0.93	0.700	1.04	0.671	1.02	1.30	0.887	No
2388	23.88	1.36	0.50	0.86	0.93	0.700	1.04	0.671	1.02	1.30	0.887	No
2389	23.89	1.36	0.50	0.86	0.93	0.700	1.04	0.671	1.02	1.30	0.887	No
2390	23.90	1.36	0.50	0.87	0.93	0.701	1.04	0.671	1.02	1.30	0.887	No
2391	23.91	1.36	0.50	0.87	0.93	0.701	1.04	0.671	1.02	1.30	0.887	No
2392	23.92	1.36	0.50	0.87	0.93	0.701	1.04	0.672	1.02	1.30	0.887	No
2393	23.93	1.36	0.50	0.87	0.93	0.701	1.04	0.672	1.02	1.30	0.887	No
2394	23.94	1.36	0.50	0.87	0.93	0.701	1.04	0.672	1.02	1.30	0.887	No
2395	23.95	1.36	0.50	0.87	0.93	0.701	1.04	0.672	1.02	1.30	0.887	No
2396	23.96	1.36	0.50	0.87	0.93	0.701	1.04	0.672	1.02	1.30	0.887	No
2397	23.97	1.37	0.50	0.87	0.93	0.701	1.04	0.672	1.02	1.30	0.888	No
2398	23.98	1.37	0.50	0.87	0.93	0.701	1.04	0.672	1.02	1.30	0.888	No
2399	23.99	1.37	0.50	0.87	0.93	0.701	1.04	0.672	1.02	1.30	0.888	No
2400	24.00	1.37	0.50	0.87	0.93	0.701	1.04	0.672	1.02	1.30	0.888	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
2401	24.01	1.37	0.50	0.87	0.93	0.701	1.04	0.672	1.02	1.30	0.888	No
2402	24.02	1.37	0.50	0.87	0.93	0.701	1.04	0.672	1.02	1.30	0.889	No
2403	24.03	1.37	0.50	0.87	0.93	0.701	1.04	0.672	1.02	1.30	0.889	No
2404	24.04	1.37	0.50	0.87	0.93	0.701	1.04	0.672	1.02	1.30	0.889	No
2405	24.05	1.37	0.50	0.87	0.92	0.701	1.04	0.672	1.02	1.30	0.889	No
2406	24.06	1.37	0.50	0.87	0.92	0.701	1.04	0.672	1.02	1.30	0.889	No
2407	24.07	1.37	0.50	0.87	0.92	0.701	1.04	0.672	1.02	1.30	0.889	No
2408	24.08	1.37	0.50	0.87	0.92	0.701	1.04	0.672	1.02	1.30	0.889	No
2409	24.09	1.37	0.50	0.87	0.92	0.701	1.04	0.672	1.02	1.30	0.889	No
2410	24.10	1.37	0.50	0.87	0.92	0.701	1.04	0.672	1.02	1.30	0.889	No
2411	24.11	1.37	0.50	0.87	0.92	0.702	1.04	0.672	1.02	1.30	0.890	No
2412	24.12	1.37	0.50	0.87	0.92	0.702	1.04	0.672	1.02	1.30	0.890	No
2413	24.13	1.37	0.50	0.87	0.92	0.702	1.04	0.672	1.02	1.30	0.890	No
2414	24.14	1.38	0.50	0.87	0.92	0.702	1.04	0.673	1.02	1.30	0.890	No
2415	24.15	1.38	0.50	0.87	0.92	0.702	1.04	0.673	1.02	1.30	0.890	No
2416	24.16	1.38	0.50	0.87	0.92	0.702	1.04	0.673	1.02	1.30	0.890	No
2417	24.17	1.38	0.50	0.87	0.92	0.702	1.04	0.673	1.02	1.30	0.890	No
2418	24.18	1.38	0.50	0.87	0.92	0.702	1.04	0.673	1.02	1.30	0.890	No
2419	24.19	1.38	0.51	0.87	0.92	0.702	1.04	0.673	1.02	1.30	0.891	No
2420	24.20	1.38	0.51	0.87	0.92	0.702	1.04	0.673	1.02	1.30	0.891	No
2421	24.21	1.38	0.51	0.87	0.92	0.702	1.04	0.673	1.02	1.30	0.891	No
2422	24.22	1.38	0.51	0.87	0.92	0.702	1.04	0.673	1.02	1.30	0.891	No
2423	24.23	1.38	0.51	0.87	0.92	0.702	1.04	0.673	1.02	1.30	0.891	No
2424	24.24	1.38	0.51	0.87	0.92	0.702	1.04	0.673	1.02	1.30	0.891	No
2425	24.25	1.38	0.51	0.87	0.92	0.702	1.04	0.673	1.02	1.30	0.891	No
2426	24.26	1.38	0.51	0.87	0.92	0.702	1.04	0.673	1.02	1.30	0.892	No
2427	24.27	1.38	0.51	0.87	0.92	0.702	1.04	0.673	1.02	1.30	0.892	No
2428	24.28	1.38	0.51	0.88	0.92	0.702	1.04	0.673	1.02	1.30	0.892	No
2429	24.29	1.38	0.51	0.88	0.92	0.702	1.04	0.673	1.02	1.30	0.892	No
2430	24.30	1.38	0.51	0.88	0.92	0.702	1.04	0.673	1.02	1.30	0.892	No
2431	24.31	1.38	0.51	0.88	0.92	0.703	1.04	0.673	1.02	1.30	0.892	No
2432	24.32	1.39	0.51	0.88	0.92	0.703	1.04	0.673	1.02	1.30	0.892	No
2433	24.33	1.39	0.51	0.88	0.92	0.703	1.04	0.673	1.02	1.30	0.892	No
2434	24.34	1.39	0.51	0.88	0.92	0.703	1.04	0.673	1.02	1.30	0.892	No
2435	24.35	1.39	0.51	0.88	0.92	0.703	1.04	0.674	1.02	1.30	0.892	No
2436	24.36	1.39	0.51	0.88	0.92	0.703	1.04	0.674	1.02	1.30	0.892	No
2437	24.37	1.39	0.51	0.88	0.92	0.703	1.04	0.674	1.02	1.30	0.892	No
2438	24.38	1.39	0.51	0.88	0.92	0.703	1.04	0.674	1.02	1.30	0.892	No
2439	24.39	1.39	0.51	0.88	0.92	0.703	1.04	0.674	1.02	1.30	0.892	No
2440	24.40	1.39	0.51	0.88	0.92	0.703	1.04	0.674	1.02	1.30	0.892	No
2441	24.41	1.39	0.51	0.88	0.92	0.703	1.04	0.674	1.02	1.30	0.892	No
2442	24.42	1.39	0.51	0.88	0.92	0.703	1.04	0.674	1.02	1.30	0.892	No
2443	24.43	1.39	0.51	0.88	0.92	0.703	1.04	0.674	1.02	1.30	0.892	No
2444	24.44	1.39	0.51	0.88	0.92	0.703	1.04	0.674	1.02	1.30	0.892	No
2445	24.45	1.39	0.51	0.88	0.92	0.703	1.04	0.674	1.02	1.30	0.892	No
2446	24.46	1.39	0.51	0.88	0.92	0.703	1.04	0.674	1.02	1.30	0.892	No
2447	24.47	1.39	0.51	0.88	0.92	0.703	1.04	0.674	1.02	1.30	0.893	No
2448	24.48	1.39	0.51	0.88	0.92	0.703	1.04	0.674	1.02	1.30	0.893	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
2449	24.49	1.40	0.51	0.88	0.92	0.703	1.04	0.674	1.02	1.30	0.893	No
2450	24.50	1.40	0.51	0.88	0.92	0.703	1.04	0.674	1.02	1.30	0.893	No
2451	24.51	1.40	0.52	0.88	0.92	0.703	1.04	0.674	1.02	1.30	0.893	No
2452	24.52	1.40	0.52	0.88	0.92	0.704	1.04	0.674	1.02	1.30	0.893	No
2453	24.53	1.40	0.52	0.88	0.92	0.704	1.04	0.674	1.02	1.30	0.893	No
2454	24.54	1.40	0.52	0.88	0.92	0.704	1.04	0.674	1.02	1.30	0.893	No
2455	24.55	1.40	0.52	0.88	0.92	0.704	1.04	0.674	1.02	1.30	0.893	No
2456	24.56	1.40	0.52	0.88	0.92	0.704	1.04	0.674	1.02	1.30	0.893	No
2457	24.57	1.40	0.52	0.88	0.92	0.704	1.04	0.675	1.02	1.30	0.893	No
2458	24.58	1.40	0.52	0.88	0.92	0.704	1.04	0.675	1.02	1.30	0.894	No
2459	24.59	1.40	0.52	0.88	0.92	0.704	1.04	0.675	1.02	1.30	0.894	No
2460	24.60	1.40	0.52	0.88	0.92	0.704	1.04	0.675	1.02	1.30	0.894	No
2461	24.61	1.40	0.52	0.88	0.92	0.704	1.04	0.675	1.02	1.30	0.894	No
2462	24.62	1.40	0.52	0.88	0.92	0.704	1.04	0.675	1.02	1.30	0.894	No
2463	24.63	1.40	0.52	0.88	0.92	0.704	1.04	0.675	1.02	1.30	0.894	No
2464	24.64	1.40	0.52	0.88	0.92	0.704	1.04	0.675	1.02	1.30	0.894	No
2465	24.65	1.40	0.52	0.88	0.92	0.704	1.04	0.675	1.02	1.30	0.894	No
2466	24.66	1.40	0.52	0.89	0.92	0.704	1.04	0.675	1.02	1.30	0.894	No
2467	24.67	1.41	0.52	0.89	0.92	0.704	1.04	0.675	1.02	1.30	0.895	No
2468	24.68	1.41	0.52	0.89	0.92	0.704	1.04	0.675	1.02	1.30	0.895	No
2469	24.69	1.41	0.52	0.89	0.92	0.704	1.04	0.675	1.01	1.30	0.895	No
2470	24.70	1.41	0.52	0.89	0.92	0.704	1.04	0.675	1.01	1.30	0.895	No
2471	24.71	1.41	0.52	0.89	0.92	0.704	1.04	0.675	1.01	1.30	0.895	No
2472	24.72	1.41	0.52	0.89	0.92	0.704	1.04	0.675	1.01	1.30	0.895	No
2473	24.73	1.41	0.52	0.89	0.92	0.704	1.04	0.675	1.01	1.30	0.895	No
2474	24.74	1.41	0.52	0.89	0.92	0.705	1.04	0.675	1.01	1.30	0.895	No
2475	24.75	1.41	0.52	0.89	0.92	0.705	1.04	0.675	1.01	1.30	0.895	No
2476	24.76	1.41	0.52	0.89	0.92	0.705	1.04	0.675	1.01	1.30	0.896	No
2477	24.77	1.41	0.52	0.89	0.92	0.705	1.04	0.675	1.01	1.30	0.896	No
2478	24.78	1.41	0.52	0.89	0.92	0.705	1.04	0.675	1.01	1.30	0.896	No
2479	24.79	1.41	0.52	0.89	0.92	0.705	1.04	0.675	1.01	1.30	0.896	No
2480	24.80	1.41	0.52	0.89	0.92	0.705	1.04	0.676	1.01	1.30	0.896	No
2481	24.81	1.41	0.52	0.89	0.92	0.705	1.04	0.676	1.01	1.30	0.896	No
2482	24.82	1.41	0.52	0.89	0.92	0.705	1.04	0.676	1.01	1.30	0.896	No
2483	24.83	1.41	0.53	0.89	0.92	0.705	1.04	0.676	1.01	1.30	0.896	No
2484	24.84	1.42	0.53	0.89	0.92	0.705	1.04	0.676	1.01	1.30	0.897	No
2485	24.85	1.42	0.53	0.89	0.92	0.705	1.04	0.676	1.01	1.30	0.897	No
2486	24.86	1.42	0.53	0.89	0.92	0.705	1.04	0.676	1.01	1.30	0.897	No
2487	24.87	1.42	0.53	0.89	0.92	0.705	1.04	0.676	1.01	1.30	0.897	No
2488	24.88	1.42	0.53	0.89	0.92	0.705	1.04	0.676	1.01	1.30	0.897	No
2489	24.89	1.42	0.53	0.89	0.92	0.705	1.04	0.676	1.01	1.30	0.897	No
2490	24.90	1.42	0.53	0.89	0.92	0.705	1.04	0.676	1.01	1.30	0.897	No
2491	24.91	1.42	0.53	0.89	0.92	0.705	1.04	0.676	1.01	1.30	0.897	No
2492	24.92	1.42	0.53	0.89	0.92	0.705	1.04	0.676	1.01	1.30	0.898	No
2493	24.93	1.42	0.53	0.89	0.92	0.705	1.04	0.676	1.01	1.30	0.898	No
2494	24.94	1.42	0.53	0.89	0.92	0.706	1.04	0.676	1.01	1.30	0.898	No
2495	24.95	1.42	0.53	0.89	0.92	0.706	1.04	0.676	1.01	1.30	0.898	No
2496	24.96	1.42	0.53	0.89	0.92	0.706	1.04	0.676	1.01	1.30	0.898	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
2497	24.97	1.42	0.53	0.89	0.92	0.706	1.04	0.676	1.01	1.30	0.898	No
2498	24.98	1.42	0.53	0.89	0.92	0.706	1.04	0.676	1.01	1.30	0.898	No
2499	24.99	1.42	0.53	0.89	0.92	0.706	1.04	0.676	1.01	1.30	0.898	No
2500	25.00	1.42	0.53	0.89	0.92	0.706	1.04	0.676	1.01	1.30	0.898	No
2501	25.01	1.42	0.53	0.89	0.92	0.706	1.04	0.677	1.01	1.30	0.899	No
2502	25.02	1.43	0.53	0.89	0.92	0.706	1.04	0.677	1.01	1.30	0.899	No
2503	25.03	1.43	0.53	0.89	0.92	0.706	1.04	0.677	1.01	1.30	0.899	No
2504	25.04	1.43	0.53	0.89	0.92	0.706	1.04	0.677	1.01	1.30	0.899	No
2505	25.05	1.43	0.53	0.89	0.92	0.706	1.04	0.677	1.01	1.30	0.899	No
2506	25.06	1.43	0.53	0.90	0.92	0.706	1.04	0.677	1.01	1.30	0.899	No
2507	25.07	1.43	0.53	0.90	0.92	0.706	1.04	0.677	1.01	1.30	0.899	No
2508	25.08	1.43	0.53	0.90	0.92	0.706	1.04	0.677	1.01	1.30	0.899	No
2509	25.09	1.43	0.53	0.90	0.92	0.706	1.04	0.677	1.01	1.30	0.899	No
2510	25.10	1.43	0.53	0.90	0.92	0.706	1.04	0.677	1.01	1.30	0.900	No
2511	25.11	1.43	0.53	0.90	0.92	0.706	1.04	0.677	1.01	1.30	0.900	No
2512	25.12	1.43	0.53	0.90	0.92	0.706	1.04	0.677	1.01	1.30	0.900	No
2513	25.13	1.43	0.53	0.90	0.92	0.706	1.04	0.677	1.01	1.30	0.900	No
2514	25.14	1.43	0.53	0.90	0.92	0.707	1.04	0.677	1.01	1.30	0.900	No
2515	25.15	1.43	0.54	0.90	0.92	0.707	1.04	0.677	1.01	1.30	0.900	No
2516	25.16	1.43	0.54	0.90	0.92	0.707	1.04	0.677	1.01	1.30	0.900	No
2517	25.17	1.43	0.54	0.90	0.92	0.707	1.04	0.677	1.01	1.30	0.900	No
2518	25.18	1.43	0.54	0.90	0.92	0.707	1.04	0.677	1.01	1.30	0.900	No
2519	25.19	1.43	0.54	0.90	0.92	0.707	1.04	0.677	1.01	1.30	0.900	No
2520	25.20	1.43	0.54	0.90	0.92	0.707	1.04	0.677	1.01	1.30	0.901	No
2521	25.21	1.44	0.54	0.90	0.92	0.707	1.04	0.678	1.01	1.30	0.901	No
2522	25.22	1.44	0.54	0.90	0.92	0.707	1.04	0.678	1.01	1.30	0.901	No
2523	25.23	1.44	0.54	0.90	0.92	0.707	1.04	0.678	1.01	1.30	0.901	No
2524	25.24	1.44	0.54	0.90	0.92	0.707	1.04	0.678	1.01	1.30	0.901	No
2525	25.25	1.44	0.54	0.90	0.92	0.707	1.04	0.678	1.01	1.30	0.901	No
2526	25.26	1.44	0.54	0.90	0.92	0.707	1.04	0.678	1.01	1.30	0.901	No
2527	25.27	1.44	0.54	0.90	0.92	0.707	1.04	0.678	1.01	1.30	0.901	No
2528	25.28	1.44	0.54	0.90	0.92	0.707	1.04	0.678	1.01	1.30	0.901	No
2529	25.29	1.44	0.54	0.90	0.92	0.707	1.04	0.678	1.01	1.30	0.901	No
2530	25.30	1.44	0.54	0.90	0.92	0.707	1.04	0.678	1.01	1.30	0.902	No
2531	25.31	1.44	0.54	0.90	0.92	0.707	1.04	0.678	1.01	1.30	0.902	No
2532	25.32	1.44	0.54	0.90	0.92	0.707	1.04	0.678	1.01	1.30	0.902	No
2533	25.33	1.44	0.54	0.90	0.92	0.708	1.04	0.678	1.01	1.30	0.902	No
2534	25.34	1.44	0.54	0.90	0.92	0.708	1.04	0.678	1.01	1.30	0.902	No
2535	25.35	1.44	0.54	0.90	0.92	0.708	1.04	0.678	1.01	1.30	0.902	No
2536	25.36	1.44	0.54	0.90	0.92	0.708	1.04	0.678	1.01	1.30	0.902	No
2537	25.37	1.44	0.54	0.90	0.92	0.708	1.04	0.678	1.01	1.30	0.902	No
2538	25.38	1.44	0.54	0.90	0.92	0.708	1.04	0.678	1.01	1.30	0.902	No
2539	25.39	1.45	0.54	0.90	0.92	0.708	1.04	0.678	1.01	1.30	0.902	No
2540	25.40	1.45	0.54	0.90	0.92	0.708	1.04	0.679	1.01	1.30	0.902	No
2541	25.41	1.45	0.54	0.90	0.92	0.708	1.04	0.679	1.01	1.30	0.903	No
2542	25.42	1.45	0.54	0.90	0.92	0.708	1.04	0.679	1.01	1.30	0.903	No
2543	25.43	1.45	0.54	0.90	0.92	0.708	1.04	0.679	1.01	1.30	0.903	No
2544	25.44	1.45	0.54	0.90	0.92	0.708	1.04	0.679	1.01	1.30	0.903	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
2545	25.45	1.45	0.54	0.90	0.92	0.708	1.04	0.679	1.01	1.30	0.903	No
2546	25.46	1.45	0.54	0.90	0.92	0.708	1.04	0.679	1.01	1.30	0.903	No
2547	25.47	1.45	0.55	0.90	0.92	0.708	1.04	0.679	1.01	1.30	0.903	No
2548	25.48	1.45	0.55	0.90	0.92	0.708	1.04	0.679	1.01	1.30	0.903	No
2549	25.49	1.45	0.55	0.90	0.92	0.708	1.04	0.679	1.01	1.30	0.903	No
2550	25.50	1.45	0.55	0.91	0.92	0.708	1.04	0.679	1.01	1.30	0.903	No
2551	25.51	1.45	0.55	0.91	0.92	0.709	1.04	0.679	1.01	1.30	0.903	No
2552	25.52	1.45	0.55	0.91	0.92	0.709	1.04	0.679	1.01	1.30	0.903	No
2553	25.53	1.45	0.55	0.91	0.92	0.709	1.04	0.679	1.01	1.30	0.903	No
2554	25.54	1.45	0.55	0.91	0.92	0.709	1.04	0.679	1.01	1.30	0.903	No
2555	25.55	1.45	0.55	0.91	0.92	0.709	1.04	0.679	1.01	1.30	0.903	No
2556	25.56	1.45	0.55	0.91	0.92	0.709	1.04	0.679	1.01	1.30	0.903	No
2557	25.57	1.45	0.55	0.91	0.92	0.709	1.04	0.679	1.01	1.30	0.904	No
2558	25.58	1.46	0.55	0.91	0.92	0.709	1.04	0.679	1.01	1.30	0.904	No
2559	25.59	1.46	0.55	0.91	0.92	0.709	1.04	0.679	1.01	1.30	0.904	No
2560	25.60	1.46	0.55	0.91	0.92	0.709	1.04	0.680	1.01	1.30	0.904	No
2561	25.61	1.46	0.55	0.91	0.92	0.709	1.04	0.680	1.01	1.30	0.904	No
2562	25.62	1.46	0.55	0.91	0.92	0.709	1.04	0.680	1.01	1.30	0.904	No
2563	25.63	1.46	0.55	0.91	0.92	0.709	1.04	0.680	1.01	1.30	0.904	No
2564	25.64	1.46	0.55	0.91	0.92	0.709	1.04	0.680	1.01	1.30	0.904	No
2565	25.65	1.46	0.55	0.91	0.92	0.709	1.04	0.680	1.01	1.30	0.904	No
2566	25.66	1.46	0.55	0.91	0.92	0.709	1.04	0.680	1.01	1.30	0.904	No
2567	25.67	1.46	0.55	0.91	0.92	0.709	1.04	0.680	1.01	1.30	0.904	No
2568	25.68	1.46	0.55	0.91	0.92	0.709	1.04	0.680	1.01	1.30	0.904	No
2569	25.69	1.46	0.55	0.91	0.92	0.709	1.04	0.680	1.01	1.30	0.904	No
2570	25.70	1.46	0.55	0.91	0.92	0.709	1.04	0.680	1.01	1.30	0.904	No
2571	25.71	1.46	0.55	0.91	0.92	0.709	1.04	0.680	1.01	1.30	0.904	No
2572	25.72	1.46	0.55	0.91	0.92	0.710	1.04	0.680	1.01	1.30	0.904	No
2573	25.73	1.46	0.55	0.91	0.92	0.710	1.04	0.680	1.01	1.30	0.905	No
2574	25.74	1.46	0.55	0.91	0.92	0.710	1.04	0.680	1.01	1.30	0.905	No
2575	25.75	1.46	0.55	0.91	0.92	0.710	1.04	0.680	1.01	1.30	0.905	No
2576	25.76	1.47	0.55	0.91	0.92	0.710	1.04	0.680	1.01	1.30	0.905	No
2577	25.77	1.47	0.55	0.91	0.92	0.710	1.04	0.680	1.01	1.30	0.905	No
2578	25.78	1.47	0.55	0.91	0.92	0.710	1.04	0.680	1.01	1.30	0.905	No
2579	25.79	1.47	0.56	0.91	0.92	0.710	1.04	0.680	1.01	1.30	0.905	No
2580	25.80	1.47	0.56	0.91	0.92	0.710	1.04	0.680	1.01	1.30	0.905	No
2581	25.81	1.47	0.56	0.91	0.92	0.710	1.04	0.680	1.01	1.30	0.905	No
2582	25.82	1.47	0.56	0.91	0.92	0.710	1.04	0.681	1.01	1.30	0.905	No
2583	25.83	1.47	0.56	0.91	0.92	0.710	1.04	0.681	1.01	1.30	0.905	No
2584	25.84	1.47	0.56	0.91	0.92	0.710	1.04	0.681	1.01	1.30	0.905	No
2585	25.85	1.47	0.56	0.91	0.92	0.710	1.04	0.681	1.01	1.30	0.905	No
2586	25.86	1.47	0.56	0.91	0.92	0.710	1.04	0.681	1.01	1.30	0.905	No
2587	25.87	1.47	0.56	0.91	0.92	0.710	1.04	0.681	1.01	1.30	0.905	No
2588	25.88	1.47	0.56	0.91	0.92	0.710	1.04	0.681	1.01	1.30	0.905	No
2589	25.89	1.47	0.56	0.91	0.92	0.710	1.04	0.681	1.01	1.30	0.905	No
2590	25.90	1.47	0.56	0.91	0.92	0.710	1.04	0.681	1.01	1.30	0.906	No
2591	25.91	1.47	0.56	0.91	0.92	0.710	1.04	0.681	1.01	1.30	0.906	No
2592	25.92	1.47	0.56	0.92	0.92	0.710	1.04	0.681	1.01	1.30	0.906	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
2593	25.93	1.47	0.56	0.92	0.92	0.710	1.04	0.681	1.01	1.30	0.906	No
2594	25.94	1.48	0.56	0.92	0.92	0.711	1.04	0.681	1.01	1.30	0.906	No
2595	25.95	1.48	0.56	0.92	0.92	0.711	1.04	0.681	1.01	1.30	0.906	No
2596	25.96	1.48	0.56	0.92	0.92	0.711	1.04	0.681	1.01	1.30	0.906	No
2597	25.97	1.48	0.56	0.92	0.92	0.711	1.04	0.681	1.01	1.30	0.906	No
2598	25.98	1.48	0.56	0.92	0.92	0.711	1.04	0.681	1.01	1.30	0.906	No
2599	25.99	1.48	0.56	0.92	0.92	0.711	1.04	0.681	1.01	1.30	0.906	No
2600	26.00	1.48	0.56	0.92	0.92	0.711	1.04	0.681	1.01	1.30	0.906	No
2601	26.01	1.48	0.56	0.92	0.92	0.711	1.04	0.681	1.01	1.30	0.906	No
2602	26.02	1.48	0.56	0.92	0.92	0.711	1.04	0.681	1.01	1.30	0.906	No
2603	26.03	1.48	0.56	0.92	0.92	0.711	1.04	0.681	1.01	1.30	0.906	No
2604	26.04	1.48	0.56	0.92	0.92	0.711	1.04	0.681	1.01	1.30	0.906	No
2605	26.05	1.48	0.56	0.92	0.92	0.711	1.04	0.681	1.01	1.30	0.906	No
2606	26.06	1.48	0.56	0.92	0.92	0.711	1.04	0.681	1.01	1.30	0.906	No
2607	26.07	1.48	0.56	0.92	0.92	0.711	1.04	0.682	1.01	1.30	0.906	No
2608	26.08	1.48	0.56	0.92	0.92	0.711	1.04	0.682	1.01	1.30	0.906	No
2609	26.09	1.48	0.56	0.92	0.92	0.711	1.04	0.682	1.01	1.30	0.906	No
2610	26.10	1.48	0.56	0.92	0.92	0.711	1.04	0.682	1.01	1.30	0.906	No
2611	26.11	1.48	0.57	0.92	0.92	0.711	1.04	0.682	1.01	1.30	0.906	No
2612	26.12	1.49	0.57	0.92	0.92	0.711	1.04	0.682	1.01	1.30	0.906	No
2613	26.13	1.49	0.57	0.92	0.92	0.711	1.04	0.682	1.01	1.30	0.906	No
2614	26.14	1.49	0.57	0.92	0.92	0.711	1.04	0.682	1.01	1.30	0.906	No
2615	26.15	1.49	0.57	0.92	0.92	0.711	1.04	0.682	1.01	1.30	0.907	No
2616	26.16	1.49	0.57	0.92	0.92	0.711	1.04	0.682	1.01	1.30	0.907	No
2617	26.17	1.49	0.57	0.92	0.92	0.711	1.04	0.682	1.01	1.30	0.907	No
2618	26.18	1.49	0.57	0.92	0.92	0.711	1.04	0.682	1.01	1.30	0.907	No
2619	26.19	1.49	0.57	0.92	0.92	0.711	1.04	0.682	1.01	1.30	0.907	No
2620	26.20	1.49	0.57	0.92	0.92	0.712	1.04	0.682	1.01	1.30	0.907	No
2621	26.21	1.49	0.57	0.92	0.92	0.712	1.04	0.682	1.01	1.30	0.907	No
2622	26.22	1.49	0.57	0.92	0.92	0.712	1.04	0.682	1.01	1.30	0.907	No
2623	26.23	1.49	0.57	0.92	0.92	0.712	1.04	0.682	1.01	1.30	0.907	No
2624	26.24	1.49	0.57	0.92	0.92	0.712	1.04	0.682	1.01	1.30	0.907	No
2625	26.25	1.49	0.57	0.92	0.92	0.712	1.04	0.682	1.01	1.30	0.908	No
2626	26.26	1.49	0.57	0.92	0.92	0.712	1.04	0.682	1.01	1.30	0.908	No
2627	26.27	1.49	0.57	0.92	0.92	0.712	1.04	0.682	1.01	1.30	0.908	No
2628	26.28	1.49	0.57	0.92	0.92	0.712	1.04	0.682	1.01	1.30	0.908	No
2629	26.29	1.50	0.57	0.92	0.92	0.712	1.04	0.682	1.01	1.30	0.908	No
2630	26.30	1.50	0.57	0.92	0.92	0.712	1.04	0.682	1.01	1.30	0.908	No
2631	26.31	1.50	0.57	0.93	0.92	0.712	1.04	0.682	1.01	1.30	0.908	No
2632	26.32	1.50	0.57	0.93	0.92	0.712	1.04	0.682	1.01	1.30	0.908	No
2633	26.33	1.50	0.57	0.93	0.91	0.712	1.04	0.682	1.01	1.30	0.908	No
2634	26.34	1.50	0.57	0.93	0.91	0.712	1.04	0.682	1.01	1.30	0.908	No
2635	26.35	1.50	0.57	0.93	0.91	0.712	1.04	0.683	1.01	1.30	0.908	No
2636	26.36	1.50	0.57	0.93	0.91	0.712	1.04	0.683	1.01	1.30	0.908	No
2637	26.37	1.50	0.57	0.93	0.91	0.712	1.04	0.683	1.01	1.30	0.908	No
2638	26.38	1.50	0.57	0.93	0.91	0.712	1.04	0.683	1.01	1.30	0.908	No
2639	26.39	1.50	0.57	0.93	0.91	0.712	1.04	0.683	1.01	1.30	0.908	No
2640	26.40	1.50	0.57	0.93	0.91	0.712	1.04	0.683	1.01	1.30	0.908	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
2641	26.41	1.50	0.57	0.93	0.91	0.712	1.04	0.683	1.01	1.30	0.908	No
2642	26.42	1.50	0.57	0.93	0.91	0.712	1.04	0.683	1.01	1.30	0.908	No
2643	26.43	1.50	0.58	0.93	0.91	0.712	1.04	0.683	1.01	1.30	0.908	No
2644	26.44	1.50	0.58	0.93	0.91	0.712	1.04	0.683	1.01	1.30	0.908	No
2645	26.45	1.50	0.58	0.93	0.91	0.712	1.04	0.683	1.01	1.30	0.908	No
2646	26.46	1.50	0.58	0.93	0.91	0.713	1.04	0.683	1.01	1.30	0.909	No
2647	26.47	1.51	0.58	0.93	0.91	0.713	1.04	0.683	1.01	1.30	0.909	No
2648	26.48	1.51	0.58	0.93	0.91	0.713	1.04	0.683	1.01	1.30	0.909	No
2649	26.49	1.51	0.58	0.93	0.91	0.713	1.04	0.683	1.01	1.30	0.909	No
2650	26.50	1.51	0.58	0.93	0.91	0.713	1.04	0.683	1.01	1.30	0.909	No
2651	26.51	1.51	0.58	0.93	0.91	0.713	1.04	0.683	1.01	1.30	0.909	No
2652	26.52	1.51	0.58	0.93	0.91	0.713	1.04	0.683	1.01	1.30	0.909	No
2653	26.53	1.51	0.58	0.93	0.91	0.713	1.04	0.683	1.01	1.30	0.909	No
2654	26.54	1.51	0.58	0.93	0.91	0.713	1.04	0.683	1.01	1.30	0.909	No
2655	26.55	1.51	0.58	0.93	0.91	0.713	1.04	0.683	1.01	1.30	0.909	No
2656	26.56	1.51	0.58	0.93	0.91	0.713	1.04	0.683	1.01	1.30	0.909	No
2657	26.57	1.51	0.58	0.93	0.91	0.713	1.04	0.683	1.01	1.30	0.909	No
2658	26.58	1.51	0.58	0.93	0.91	0.713	1.04	0.683	1.01	1.30	0.909	No
2659	26.59	1.51	0.58	0.93	0.91	0.713	1.04	0.683	1.01	1.30	0.909	No
2660	26.60	1.51	0.58	0.93	0.91	0.713	1.04	0.683	1.01	1.30	0.909	No
2661	26.61	1.51	0.58	0.93	0.91	0.713	1.04	0.683	1.01	1.30	0.909	No
2662	26.62	1.51	0.58	0.93	0.91	0.713	1.04	0.683	1.01	1.30	0.909	No
2663	26.63	1.51	0.58	0.93	0.91	0.713	1.04	0.683	1.01	1.30	0.910	No
2664	26.64	1.52	0.58	0.93	0.91	0.713	1.04	0.684	1.01	1.30	0.910	No
2665	26.65	1.52	0.58	0.93	0.91	0.713	1.04	0.684	1.01	1.30	0.910	No
2666	26.66	1.52	0.58	0.93	0.91	0.713	1.04	0.684	1.01	1.30	0.910	No
2667	26.67	1.52	0.58	0.93	0.91	0.713	1.04	0.684	1.01	1.30	0.910	No
2668	26.68	1.52	0.58	0.93	0.91	0.713	1.04	0.684	1.01	1.30	0.910	No
2669	26.69	1.52	0.58	0.94	0.91	0.713	1.04	0.684	1.01	1.30	0.910	No
2670	26.70	1.52	0.58	0.94	0.91	0.713	1.04	0.684	1.01	1.30	0.910	No
2671	26.71	1.52	0.58	0.94	0.91	0.713	1.04	0.684	1.01	1.30	0.910	No
2672	26.72	1.52	0.58	0.94	0.91	0.713	1.04	0.684	1.01	1.30	0.910	No
2673	26.73	1.52	0.58	0.94	0.91	0.713	1.04	0.684	1.01	1.30	0.910	No
2674	26.74	1.52	0.58	0.94	0.91	0.713	1.04	0.684	1.01	1.30	0.911	No
2675	26.75	1.52	0.59	0.94	0.91	0.714	1.04	0.684	1.01	1.30	0.911	No
2676	26.76	1.52	0.59	0.94	0.91	0.714	1.04	0.684	1.01	1.30	0.911	No
2677	26.77	1.52	0.59	0.94	0.91	0.714	1.04	0.684	1.01	1.30	0.911	No
2678	26.78	1.52	0.59	0.94	0.91	0.714	1.04	0.684	1.01	1.30	0.911	No
2679	26.79	1.52	0.59	0.94	0.91	0.714	1.04	0.684	1.01	1.30	0.911	No
2680	26.80	1.52	0.59	0.94	0.91	0.714	1.04	0.684	1.01	1.30	0.911	No
2681	26.81	1.53	0.59	0.94	0.91	0.714	1.04	0.684	1.01	1.30	0.911	No
2682	26.82	1.53	0.59	0.94	0.91	0.714	1.04	0.684	1.01	1.30	0.911	No
2683	26.83	1.53	0.59	0.94	0.91	0.714	1.04	0.684	1.01	1.30	0.911	No
2684	26.84	1.53	0.59	0.94	0.91	0.714	1.04	0.684	1.01	1.30	0.911	No
2685	26.85	1.53	0.59	0.94	0.91	0.714	1.04	0.684	1.01	1.30	0.912	No
2686	26.86	1.53	0.59	0.94	0.91	0.714	1.04	0.684	1.01	1.30	0.912	No
2687	26.87	1.53	0.59	0.94	0.91	0.714	1.04	0.684	1.01	1.30	0.912	No
2688	26.88	1.53	0.59	0.94	0.91	0.714	1.04	0.684	1.01	1.30	0.912	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
2689	26.89	1.53	0.59	0.94	0.91	0.714	1.04	0.684	1.01	1.30	0.912	No
2690	26.90	1.53	0.59	0.94	0.91	0.714	1.04	0.684	1.01	1.30	0.912	No
2691	26.91	1.53	0.59	0.94	0.91	0.714	1.04	0.684	1.01	1.30	0.912	No
2692	26.92	1.53	0.59	0.94	0.91	0.714	1.04	0.684	1.01	1.30	0.912	No
2693	26.93	1.53	0.59	0.94	0.91	0.714	1.04	0.685	1.01	1.30	0.912	No
2694	26.94	1.53	0.59	0.94	0.91	0.714	1.04	0.685	1.01	1.30	0.912	No
2695	26.95	1.53	0.59	0.94	0.91	0.714	1.04	0.685	1.01	1.30	0.912	No
2696	26.96	1.53	0.59	0.94	0.91	0.714	1.04	0.685	1.01	1.30	0.912	No
2697	26.97	1.53	0.59	0.94	0.91	0.714	1.04	0.685	1.01	1.30	0.912	No
2698	26.98	1.53	0.59	0.94	0.91	0.714	1.04	0.685	1.01	1.30	0.912	No
2699	26.99	1.54	0.59	0.94	0.91	0.714	1.04	0.685	1.01	1.30	0.912	No
2700	27.00	1.54	0.59	0.94	0.91	0.714	1.04	0.685	1.01	1.30	0.912	No
2701	27.01	1.54	0.59	0.94	0.91	0.714	1.04	0.685	1.01	1.30	0.912	No
2702	27.02	1.54	0.59	0.94	0.91	0.714	1.04	0.685	1.01	1.30	0.912	No
2703	27.03	1.54	0.59	0.94	0.91	0.715	1.04	0.685	1.01	1.30	0.912	No
2704	27.04	1.54	0.59	0.94	0.91	0.715	1.04	0.685	1.01	1.30	0.912	No
2705	27.05	1.54	0.59	0.94	0.91	0.715	1.04	0.685	1.01	1.30	0.913	No
2706	27.06	1.54	0.59	0.94	0.91	0.715	1.04	0.685	1.01	1.30	0.913	No
2707	27.07	1.54	0.59	0.94	0.91	0.715	1.04	0.685	1.01	1.30	0.913	No
2708	27.08	1.54	0.60	0.95	0.91	0.715	1.04	0.685	1.01	1.30	0.913	No
2709	27.09	1.54	0.60	0.95	0.91	0.715	1.04	0.685	1.01	1.30	0.913	No
2710	27.10	1.54	0.60	0.95	0.91	0.715	1.04	0.685	1.01	1.30	0.913	No
2711	27.11	1.54	0.60	0.95	0.91	0.715	1.04	0.685	1.01	1.30	0.914	No
2712	27.12	1.54	0.60	0.95	0.91	0.715	1.04	0.685	1.01	1.30	0.914	No
2713	27.13	1.54	0.60	0.95	0.91	0.715	1.04	0.685	1.01	1.30	0.914	No
2714	27.14	1.54	0.60	0.95	0.91	0.715	1.04	0.685	1.01	1.30	0.914	No
2715	27.15	1.54	0.60	0.95	0.91	0.715	1.04	0.685	1.01	1.30	0.914	No
2716	27.16	1.54	0.60	0.95	0.91	0.715	1.04	0.685	1.01	1.30	0.914	No
2717	27.17	1.55	0.60	0.95	0.91	0.715	1.04	0.685	1.01	1.30	0.914	No
2718	27.18	1.55	0.60	0.95	0.91	0.715	1.04	0.685	1.01	1.30	0.914	No
2719	27.19	1.55	0.60	0.95	0.91	0.715	1.04	0.685	1.01	1.30	0.914	No
2720	27.20	1.55	0.60	0.95	0.91	0.715	1.04	0.685	1.01	1.30	0.914	No
2721	27.21	1.55	0.60	0.95	0.91	0.715	1.04	0.685	1.01	1.30	0.914	No
2722	27.22	1.55	0.60	0.95	0.91	0.715	1.04	0.685	1.01	1.30	0.914	No
2723	27.23	1.55	0.60	0.95	0.91	0.715	1.04	0.686	1.01	1.30	0.914	No
2724	27.24	1.55	0.60	0.95	0.91	0.715	1.04	0.686	1.01	1.30	0.915	No
2725	27.25	1.55	0.60	0.95	0.91	0.715	1.04	0.686	1.01	1.30	0.915	No
2726	27.26	1.55	0.60	0.95	0.91	0.715	1.04	0.686	1.01	1.30	0.915	No
2727	27.27	1.55	0.60	0.95	0.91	0.715	1.04	0.686	1.01	1.30	0.915	No
2728	27.28	1.55	0.60	0.95	0.91	0.715	1.04	0.686	1.01	1.30	0.915	No
2729	27.29	1.55	0.60	0.95	0.91	0.715	1.04	0.686	1.01	1.30	0.915	No
2730	27.30	1.55	0.60	0.95	0.91	0.715	1.04	0.686	1.01	1.30	0.915	No
2731	27.31	1.55	0.60	0.95	0.91	0.716	1.04	0.686	1.01	1.30	0.915	No
2732	27.32	1.55	0.60	0.95	0.91	0.716	1.04	0.686	1.01	1.30	0.915	No
2733	27.33	1.55	0.60	0.95	0.91	0.716	1.04	0.686	1.01	1.30	0.915	No
2734	27.34	1.55	0.60	0.95	0.91	0.716	1.04	0.686	1.01	1.30	0.915	No
2735	27.35	1.56	0.60	0.95	0.91	0.716	1.04	0.686	1.01	1.30	0.915	No
2736	27.36	1.56	0.60	0.95	0.91	0.716	1.04	0.686	1.01	1.30	0.915	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
2737	27.37	1.56	0.60	0.95	0.91	0.716	1.04	0.686	1.01	1.30	0.915	No
2738	27.38	1.56	0.60	0.95	0.91	0.716	1.04	0.686	1.01	1.30	0.915	No
2739	27.39	1.56	0.60	0.95	0.91	0.716	1.04	0.686	1.01	1.30	0.916	No
2740	27.40	1.56	0.61	0.95	0.91	0.716	1.04	0.686	1.01	1.30	0.916	No
2741	27.41	1.56	0.61	0.95	0.91	0.716	1.04	0.686	1.01	1.30	0.916	No
2742	27.42	1.56	0.61	0.95	0.91	0.716	1.04	0.686	1.01	1.30	0.916	No
2743	27.43	1.56	0.61	0.95	0.91	0.716	1.04	0.686	1.01	1.30	0.916	No
2744	27.44	1.56	0.61	0.95	0.91	0.716	1.04	0.686	1.01	1.30	0.916	No
2745	27.45	1.56	0.61	0.95	0.91	0.716	1.04	0.686	1.01	1.30	0.916	No
2746	27.46	1.56	0.61	0.95	0.91	0.716	1.04	0.686	1.01	1.30	0.916	No
2747	27.47	1.56	0.61	0.95	0.91	0.716	1.04	0.686	1.01	1.30	0.916	No
2748	27.48	1.56	0.61	0.96	0.91	0.716	1.04	0.686	1.01	1.30	0.916	No
2749	27.49	1.56	0.61	0.96	0.91	0.716	1.04	0.686	1.01	1.30	0.916	No
2750	27.50	1.56	0.61	0.96	0.91	0.716	1.04	0.686	1.01	1.30	0.916	No
2751	27.51	1.56	0.61	0.96	0.91	0.716	1.04	0.686	1.01	1.30	0.916	No
2752	27.52	1.57	0.61	0.96	0.91	0.716	1.04	0.686	1.01	1.30	0.916	No
2753	27.53	1.57	0.61	0.96	0.91	0.716	1.04	0.687	1.01	1.30	0.916	No
2754	27.54	1.57	0.61	0.96	0.91	0.716	1.04	0.687	1.01	1.30	0.915	No
2755	27.55	1.57	0.61	0.96	0.91	0.716	1.04	0.687	1.01	1.30	0.915	No
2756	27.56	1.57	0.61	0.96	0.91	0.716	1.04	0.687	1.01	1.30	0.915	No
2757	27.57	1.57	0.61	0.96	0.91	0.716	1.04	0.687	1.01	1.30	0.915	No
2758	27.58	1.57	0.61	0.96	0.91	0.716	1.04	0.687	1.01	1.30	0.915	No
2759	27.59	1.57	0.61	0.96	0.91	0.716	1.04	0.687	1.01	1.30	0.916	No
2760	27.60	1.57	0.61	0.96	0.91	0.716	1.04	0.687	1.01	1.30	0.916	No
2761	27.61	1.57	0.61	0.96	0.91	0.717	1.04	0.687	1.01	1.30	0.916	No
2762	27.62	1.57	0.61	0.96	0.91	0.717	1.04	0.687	1.01	1.30	0.916	No
2763	27.63	1.57	0.61	0.96	0.91	0.717	1.04	0.687	1.01	1.30	0.916	No
2764	27.64	1.57	0.61	0.96	0.91	0.717	1.04	0.687	1.01	1.30	0.916	No
2765	27.65	1.57	0.61	0.96	0.91	0.717	1.04	0.687	1.01	1.30	0.916	No
2766	27.66	1.57	0.61	0.96	0.91	0.717	1.04	0.687	1.01	1.30	0.917	No
2767	27.67	1.57	0.61	0.96	0.91	0.717	1.04	0.687	1.01	1.30	0.917	No
2768	27.68	1.57	0.61	0.96	0.91	0.717	1.04	0.687	1.01	1.30	0.917	No
2769	27.69	1.57	0.61	0.96	0.91	0.717	1.04	0.687	1.01	1.30	0.917	No
2770	27.70	1.58	0.61	0.96	0.91	0.717	1.04	0.687	1.01	1.30	0.917	No
2771	27.71	1.58	0.61	0.96	0.91	0.717	1.04	0.687	1.01	1.30	0.917	No
2772	27.72	1.58	0.62	0.96	0.91	0.717	1.04	0.687	1.01	1.30	0.917	No
2773	27.73	1.58	0.62	0.96	0.91	0.717	1.04	0.687	1.01	1.30	0.918	No
2774	27.74	1.58	0.62	0.96	0.91	0.717	1.04	0.687	1.01	1.30	0.918	No
2775	27.75	1.58	0.62	0.96	0.91	0.717	1.04	0.687	1.01	1.30	0.918	No
2776	27.76	1.58	0.62	0.96	0.91	0.717	1.04	0.687	1.01	1.30	0.918	No
2777	27.77	1.58	0.62	0.96	0.91	0.717	1.04	0.687	1.01	1.30	0.918	No
2778	27.78	1.58	0.62	0.96	0.91	0.717	1.04	0.687	1.01	1.30	0.918	No
2779	27.79	1.58	0.62	0.96	0.91	0.717	1.04	0.687	1.01	1.30	0.918	No
2780	27.80	1.58	0.62	0.96	0.91	0.717	1.04	0.687	1.01	1.30	0.918	No
2781	27.81	1.58	0.62	0.96	0.91	0.717	1.04	0.687	1.01	1.30	0.918	No
2782	27.82	1.58	0.62	0.96	0.91	0.717	1.04	0.687	1.01	1.30	0.918	No
2783	27.83	1.58	0.62	0.96	0.91	0.717	1.04	0.687	1.01	1.30	0.918	No
2784	27.84	1.58	0.62	0.96	0.91	0.717	1.04	0.687	1.01	1.30	0.919	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
2785	27.85	1.58	0.62	0.96	0.91	0.717	1.04	0.687	1.01	1.30	0.919	No
2786	27.86	1.58	0.62	0.96	0.91	0.717	1.04	0.688	1.01	1.30	0.919	No
2787	27.87	1.59	0.62	0.97	0.91	0.717	1.04	0.688	1.01	1.30	0.919	No
2788	27.88	1.59	0.62	0.97	0.91	0.717	1.04	0.688	1.01	1.30	0.919	No
2789	27.89	1.59	0.62	0.97	0.91	0.717	1.04	0.688	1.01	1.30	0.919	No
2790	27.90	1.59	0.62	0.97	0.91	0.717	1.04	0.688	1.01	1.30	0.919	No
2791	27.91	1.59	0.62	0.97	0.91	0.717	1.04	0.688	1.01	1.30	0.919	No
2792	27.92	1.59	0.62	0.97	0.91	0.718	1.04	0.688	1.01	1.30	0.919	No
2793	27.93	1.59	0.62	0.97	0.91	0.718	1.04	0.688	1.01	1.30	0.919	No
2794	27.94	1.59	0.62	0.97	0.91	0.718	1.04	0.688	1.01	1.30	0.919	No
2795	27.95	1.59	0.62	0.97	0.91	0.718	1.04	0.688	1.01	1.30	0.919	No
2796	27.96	1.59	0.62	0.97	0.91	0.718	1.04	0.688	1.01	1.30	0.919	No
2797	27.97	1.59	0.62	0.97	0.91	0.718	1.04	0.688	1.01	1.30	0.919	No
2798	27.98	1.59	0.62	0.97	0.91	0.718	1.04	0.688	1.01	1.30	0.919	No
2799	27.99	1.59	0.62	0.97	0.91	0.718	1.04	0.688	1.01	1.30	0.919	No
2800	28.00	1.59	0.62	0.97	0.91	0.718	1.04	0.688	1.01	1.30	0.919	No
2801	28.01	1.59	0.62	0.97	0.91	0.718	1.04	0.688	1.01	1.30	0.919	No
2802	28.02	1.59	0.62	0.97	0.91	0.718	1.04	0.688	1.01	1.30	0.919	No
2803	28.03	1.59	0.62	0.97	0.91	0.718	1.04	0.688	1.01	1.30	0.919	No
2804	28.04	1.59	0.63	0.97	0.91	0.718	1.04	0.688	1.01	1.30	0.919	No
2805	28.05	1.60	0.63	0.97	0.91	0.718	1.04	0.688	1.01	1.30	0.919	No
2806	28.06	1.60	0.63	0.97	0.91	0.718	1.04	0.688	1.01	1.30	0.919	No
2807	28.07	1.60	0.63	0.97	0.91	0.718	1.04	0.688	1.01	1.30	0.919	No
2808	28.08	1.60	0.63	0.97	0.91	0.718	1.04	0.688	1.01	1.30	0.919	No
2809	28.09	1.60	0.63	0.97	0.91	0.718	1.04	0.688	1.01	1.30	0.919	No
2810	28.10	1.60	0.63	0.97	0.91	0.718	1.04	0.688	1.01	1.30	0.920	No
2811	28.11	1.60	0.63	0.97	0.91	0.718	1.04	0.688	1.01	1.30	0.920	No
2812	28.12	1.60	0.63	0.97	0.91	0.718	1.04	0.688	1.01	1.30	0.920	No
2813	28.13	1.60	0.63	0.97	0.91	0.718	1.04	0.688	1.01	1.30	0.920	No
2814	28.14	1.60	0.63	0.97	0.91	0.718	1.04	0.688	1.01	1.30	0.920	No
2815	28.15	1.60	0.63	0.97	0.91	0.718	1.04	0.688	1.01	1.30	0.920	No
2816	28.16	1.60	0.63	0.97	0.91	0.718	1.04	0.688	1.01	1.30	0.920	No
2817	28.17	1.60	0.63	0.97	0.91	0.718	1.04	0.688	1.01	1.30	0.920	No
2818	28.18	1.60	0.63	0.97	0.91	0.718	1.04	0.688	1.01	1.30	0.920	No
2819	28.19	1.60	0.63	0.97	0.91	0.718	1.04	0.688	1.01	1.30	0.920	No
2820	28.20	1.60	0.63	0.97	0.91	0.718	1.04	0.689	1.01	1.30	0.920	No
2821	28.21	1.60	0.63	0.97	0.91	0.718	1.04	0.689	1.01	1.30	0.920	No
2822	28.22	1.60	0.63	0.97	0.91	0.718	1.04	0.689	1.01	1.30	0.920	No
2823	28.23	1.61	0.63	0.97	0.91	0.718	1.04	0.689	1.01	1.30	0.920	No
2824	28.24	1.61	0.63	0.97	0.91	0.718	1.04	0.689	1.01	1.30	0.920	No
2825	28.25	1.61	0.63	0.97	0.91	0.718	1.04	0.689	1.01	1.30	0.920	No
2826	28.26	1.61	0.63	0.98	0.91	0.719	1.04	0.689	1.01	1.30	0.920	No
2827	28.27	1.61	0.63	0.98	0.91	0.719	1.04	0.689	1.01	1.30	0.920	No
2828	28.28	1.61	0.63	0.98	0.91	0.719	1.04	0.689	1.01	1.30	0.920	No
2829	28.29	1.61	0.63	0.98	0.91	0.719	1.04	0.689	1.01	1.30	0.920	No
2830	28.30	1.61	0.63	0.98	0.91	0.719	1.04	0.689	1.01	1.30	0.920	No
2831	28.31	1.61	0.63	0.98	0.91	0.719	1.04	0.689	1.01	1.30	0.920	No
2832	28.32	1.61	0.63	0.98	0.91	0.719	1.04	0.689	1.01	1.30	0.921	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
2833	28.33	1.61	0.63	0.98	0.91	0.719	1.04	0.689	1.01	1.30	0.921	No
2834	28.34	1.61	0.63	0.98	0.91	0.719	1.04	0.689	1.01	1.30	0.921	No
2835	28.35	1.61	0.63	0.98	0.91	0.719	1.04	0.689	1.01	1.30	0.921	No
2836	28.36	1.61	0.64	0.98	0.91	0.719	1.04	0.689	1.01	1.30	0.921	No
2837	28.37	1.61	0.64	0.98	0.91	0.719	1.04	0.689	1.01	1.30	0.921	No
2838	28.38	1.61	0.64	0.98	0.91	0.719	1.04	0.689	1.01	1.30	0.921	No
2839	28.39	1.61	0.64	0.98	0.91	0.719	1.04	0.689	1.01	1.30	0.921	No
2840	28.40	1.62	0.64	0.98	0.91	0.719	1.04	0.689	1.01	1.30	0.921	No
2841	28.41	1.62	0.64	0.98	0.91	0.719	1.04	0.689	1.01	1.30	0.922	No
2842	28.42	1.62	0.64	0.98	0.91	0.719	1.04	0.689	1.01	1.30	0.922	No
2843	28.43	1.62	0.64	0.98	0.91	0.719	1.04	0.689	1.01	1.30	0.922	No
2844	28.44	1.62	0.64	0.98	0.91	0.719	1.04	0.689	1.01	1.30	0.922	No
2845	28.45	1.62	0.64	0.98	0.91	0.719	1.04	0.689	1.01	1.30	0.922	No
2846	28.46	1.62	0.64	0.98	0.91	0.719	1.04	0.689	1.01	1.30	0.922	No
2847	28.47	1.62	0.64	0.98	0.91	0.719	1.04	0.689	1.01	1.30	0.922	No
2848	28.48	1.62	0.64	0.98	0.91	0.719	1.04	0.689	1.01	1.30	0.922	No
2849	28.49	1.62	0.64	0.98	0.91	0.719	1.04	0.689	1.01	1.30	0.922	No
2850	28.50	1.62	0.64	0.98	0.91	0.719	1.04	0.689	1.01	1.30	0.922	No
2851	28.51	1.62	0.64	0.98	0.91	0.719	1.04	0.689	1.01	1.30	0.923	No
2852	28.52	1.62	0.64	0.98	0.91	0.719	1.04	0.689	1.01	1.30	0.923	No
2853	28.53	1.62	0.64	0.98	0.91	0.719	1.04	0.689	1.01	1.30	0.923	No
2854	28.54	1.62	0.64	0.98	0.91	0.719	1.04	0.689	1.01	1.30	0.923	No
2855	28.55	1.62	0.64	0.98	0.90	0.719	1.04	0.690	1.01	1.30	0.923	No
2856	28.56	1.62	0.64	0.98	0.90	0.719	1.04	0.690	1.01	1.30	0.923	No
2857	28.57	1.62	0.64	0.98	0.90	0.719	1.04	0.690	1.01	1.30	0.923	No
2858	28.58	1.63	0.64	0.98	0.90	0.720	1.04	0.690	1.01	1.30	0.923	No
2859	28.59	1.63	0.64	0.98	0.90	0.720	1.04	0.690	1.01	1.30	0.923	No
2860	28.60	1.63	0.64	0.98	0.90	0.720	1.04	0.690	1.01	1.30	0.923	No
2861	28.61	1.63	0.64	0.98	0.90	0.720	1.04	0.690	1.01	1.30	0.923	No
2862	28.62	1.63	0.64	0.98	0.90	0.720	1.04	0.690	1.01	1.30	0.923	No
2863	28.63	1.63	0.64	0.98	0.90	0.720	1.04	0.690	1.01	1.30	0.923	No
2864	28.64	1.63	0.64	0.98	0.90	0.720	1.04	0.690	1.01	1.30	0.923	No
2865	28.65	1.63	0.64	0.98	0.90	0.720	1.04	0.690	1.01	1.30	0.923	No
2866	28.66	1.63	0.64	0.98	0.90	0.720	1.04	0.690	1.01	1.30	0.924	No
2867	28.67	1.63	0.64	0.99	0.90	0.720	1.04	0.690	1.01	1.30	0.924	No
2868	28.68	1.63	0.65	0.99	0.90	0.720	1.04	0.690	1.01	1.30	0.924	No
2869	28.69	1.63	0.65	0.99	0.90	0.720	1.04	0.690	1.01	1.30	0.924	No
2870	28.70	1.63	0.65	0.99	0.90	0.720	1.04	0.690	1.01	1.30	0.924	No
2871	28.71	1.63	0.65	0.99	0.90	0.720	1.04	0.690	1.01	1.30	0.924	No
2872	28.72	1.63	0.65	0.99	0.90	0.720	1.04	0.690	1.01	1.30	0.924	No
2873	28.73	1.63	0.65	0.99	0.90	0.720	1.04	0.690	1.01	1.30	0.924	No
2874	28.74	1.63	0.65	0.99	0.90	0.720	1.04	0.690	1.01	1.30	0.924	No
2875	28.75	1.63	0.65	0.99	0.90	0.720	1.04	0.690	1.01	1.30	0.924	No
2876	28.76	1.64	0.65	0.99	0.90	0.720	1.04	0.690	1.01	1.30	0.924	No
2877	28.77	1.64	0.65	0.99	0.90	0.720	1.04	0.690	1.01	1.30	0.924	No
2878	28.78	1.64	0.65	0.99	0.90	0.720	1.04	0.690	1.01	1.30	0.924	No
2879	28.79	1.64	0.65	0.99	0.90	0.720	1.04	0.690	1.01	1.30	0.924	No
2880	28.80	1.64	0.65	0.99	0.90	0.720	1.04	0.690	1.01	1.30	0.924	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
2881	28.81	1.64	0.65	0.99	0.90	0.720	1.04	0.690	1.01	1.30	0.924	No
2882	28.82	1.64	0.65	0.99	0.90	0.720	1.04	0.690	1.01	1.30	0.924	No
2883	28.83	1.64	0.65	0.99	0.90	0.720	1.04	0.690	1.01	1.30	0.924	No
2884	28.84	1.64	0.65	0.99	0.90	0.720	1.04	0.690	1.01	1.30	0.924	No
2885	28.85	1.64	0.65	0.99	0.90	0.720	1.04	0.690	1.01	1.30	0.924	No
2886	28.86	1.64	0.65	0.99	0.90	0.720	1.04	0.690	1.01	1.30	0.924	No
2887	28.87	1.64	0.65	0.99	0.90	0.720	1.04	0.691	1.01	1.30	0.924	No
2888	28.88	1.64	0.65	0.99	0.90	0.720	1.04	0.691	1.01	1.30	0.924	No
2889	28.89	1.64	0.65	0.99	0.90	0.720	1.04	0.691	1.01	1.30	0.924	No
2890	28.90	1.64	0.65	0.99	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2891	28.91	1.64	0.65	0.99	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2892	28.92	1.64	0.65	0.99	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2893	28.93	1.64	0.65	0.99	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2894	28.94	1.65	0.65	0.99	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2895	28.95	1.65	0.65	0.99	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2896	28.96	1.65	0.65	0.99	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2897	28.97	1.65	0.65	0.99	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2898	28.98	1.65	0.65	0.99	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2899	28.99	1.65	0.65	0.99	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2900	29.00	1.65	0.66	0.99	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2901	29.01	1.65	0.66	0.99	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2902	29.02	1.65	0.66	0.99	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2903	29.03	1.65	0.66	0.99	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2904	29.04	1.65	0.66	0.99	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2905	29.05	1.65	0.66	0.99	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2906	29.06	1.65	0.66	0.99	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2907	29.07	1.65	0.66	1.00	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2908	29.08	1.65	0.66	1.00	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2909	29.09	1.65	0.66	1.00	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2910	29.10	1.65	0.66	1.00	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2911	29.11	1.65	0.66	1.00	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2912	29.12	1.66	0.66	1.00	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2913	29.13	1.66	0.66	1.00	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2914	29.14	1.66	0.66	1.00	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2915	29.15	1.66	0.66	1.00	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2916	29.16	1.66	0.66	1.00	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2917	29.17	1.66	0.66	1.00	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2918	29.18	1.66	0.66	1.00	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2919	29.19	1.66	0.66	1.00	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2920	29.20	1.66	0.66	1.00	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2921	29.21	1.66	0.66	1.00	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2922	29.22	1.66	0.66	1.00	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2923	29.23	1.66	0.66	1.00	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2924	29.24	1.66	0.66	1.00	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2925	29.25	1.66	0.66	1.00	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2926	29.26	1.66	0.66	1.00	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2927	29.27	1.66	0.66	1.00	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2928	29.28	1.66	0.66	1.00	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
2929	29.29	1.67	0.66	1.00	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2930	29.30	1.67	0.66	1.00	0.90	0.721	1.04	0.691	1.01	1.30	0.924	No
2931	29.31	1.67	0.66	1.00	0.90	0.721	1.04	0.691	1.00	1.30	0.924	No
2932	29.32	1.67	0.67	1.00	0.90	0.721	1.04	0.691	1.00	1.30	0.924	No
2933	29.33	1.67	0.67	1.00	0.90	0.721	1.04	0.691	1.00	1.30	0.924	No
2934	29.34	1.67	0.67	1.00	0.90	0.721	1.04	0.691	1.00	1.30	0.924	No
2935	29.35	1.67	0.67	1.00	0.90	0.721	1.04	0.692	1.00	1.30	0.924	No
2936	29.36	1.67	0.67	1.00	0.90	0.721	1.04	0.692	1.00	1.30	0.924	No
2937	29.37	1.67	0.67	1.00	0.90	0.722	1.04	0.692	1.00	1.30	0.924	No
2938	29.38	1.67	0.67	1.00	0.90	0.722	1.04	0.692	1.00	1.30	0.924	No
2939	29.39	1.67	0.67	1.00	0.90	0.722	1.04	0.692	1.00	1.30	0.925	No
2940	29.40	1.67	0.67	1.00	0.90	0.722	1.04	0.692	1.00	1.30	0.925	No
2941	29.41	1.67	0.67	1.00	0.90	0.722	1.04	0.692	1.00	1.30	0.925	No
2942	29.42	1.67	0.67	1.00	0.90	0.722	1.04	0.692	1.00	1.30	0.924	No
2943	29.43	1.67	0.67	1.01	0.90	0.722	1.04	0.692	1.00	1.30	0.924	No
2944	29.44	1.67	0.67	1.01	0.90	0.722	1.04	0.692	1.00	1.30	0.924	No
2945	29.45	1.67	0.67	1.01	0.90	0.722	1.04	0.692	1.00	1.30	0.924	No
2946	29.46	1.68	0.67	1.01	0.90	0.722	1.04	0.692	1.00	1.30	0.924	No
2947	29.47	1.68	0.67	1.01	0.90	0.722	1.04	0.692	1.00	1.30	0.924	No
2948	29.48	1.68	0.67	1.01	0.90	0.722	1.04	0.692	1.00	1.30	0.924	No
2949	29.49	1.68	0.67	1.01	0.90	0.722	1.04	0.692	1.00	1.30	0.924	No
2950	29.50	1.68	0.67	1.01	0.90	0.722	1.04	0.692	1.00	1.30	0.924	No
2951	29.51	1.68	0.67	1.01	0.90	0.722	1.04	0.692	1.00	1.30	0.924	No
2952	29.52	1.68	0.67	1.01	0.90	0.722	1.04	0.692	1.00	1.30	0.924	No
2953	29.53	1.68	0.67	1.01	0.90	0.722	1.04	0.692	1.00	1.30	0.924	No
2954	29.54	1.68	0.67	1.01	0.90	0.722	1.04	0.692	1.00	1.30	0.924	No
2955	29.55	1.68	0.67	1.01	0.90	0.722	1.04	0.692	1.00	1.30	0.924	No
2956	29.56	1.68	0.67	1.01	0.90	0.722	1.04	0.692	1.00	1.30	0.924	No
2957	29.57	1.68	0.67	1.01	0.90	0.722	1.04	0.692	1.00	1.30	0.924	No
2958	29.58	1.68	0.67	1.01	0.90	0.722	1.04	0.692	1.00	1.30	0.924	No
2959	29.59	1.68	0.67	1.01	0.90	0.722	1.04	0.692	1.00	1.30	0.924	No
2960	29.60	1.68	0.67	1.01	0.90	0.722	1.04	0.692	1.00	1.30	0.924	No
2961	29.61	1.68	0.67	1.01	0.90	0.722	1.04	0.692	1.00	1.30	0.924	No
2962	29.62	1.69	0.67	1.01	0.90	0.722	1.04	0.692	1.00	1.30	0.924	No
2963	29.63	1.69	0.67	1.01	0.90	0.722	1.04	0.692	1.00	1.30	0.924	No
2964	29.64	1.69	0.68	1.01	0.90	0.722	1.04	0.692	1.00	1.30	0.924	No
2965	29.65	1.69	0.68	1.01	0.90	0.722	1.04	0.692	1.00	1.30	0.924	No
2966	29.66	1.69	0.68	1.01	0.90	0.722	1.04	0.692	1.00	1.30	0.924	No
2967	29.67	1.69	0.68	1.01	0.90	0.722	1.04	0.692	1.00	1.30	0.924	No
2968	29.68	1.69	0.68	1.01	0.90	0.722	1.04	0.692	1.00	1.30	0.924	No
2969	29.69	1.69	0.68	1.01	0.90	0.722	1.04	0.692	1.00	1.30	0.924	No
2970	29.70	1.69	0.68	1.01	0.90	0.722	1.04	0.692	1.00	1.30	0.924	No
2971	29.71	1.69	0.68	1.01	0.90	0.722	1.04	0.692	1.00	1.30	0.924	No
2972	29.72	1.69	0.68	1.01	0.90	0.722	1.04	0.692	1.00	1.30	0.924	No
2973	29.73	1.69	0.68	1.01	0.90	0.722	1.04	0.692	1.00	1.30	0.924	No
2974	29.74	1.69	0.68	1.01	0.90	0.722	1.04	0.692	1.00	1.30	0.924	No
2975	29.75	1.69	0.68	1.01	0.90	0.722	1.04	0.692	1.00	1.30	0.925	No
2976	29.76	1.69	0.68	1.01	0.90	0.722	1.04	0.692	1.00	1.30	0.925	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
2977	29.77	1.69	0.68	1.01	0.90	0.722	1.04	0.692	1.00	1.30	0.925	No
2978	29.78	1.69	0.68	1.02	0.90	0.722	1.04	0.692	1.00	1.30	0.925	No
2979	29.79	1.70	0.68	1.02	0.90	0.722	1.04	0.692	1.00	1.30	0.925	No
2980	29.80	1.70	0.68	1.02	0.90	0.722	1.04	0.692	1.00	1.30	0.925	No
2981	29.81	1.70	0.68	1.02	0.90	0.722	1.04	0.692	1.00	1.30	0.925	No
2982	29.82	1.70	0.68	1.02	0.90	0.722	1.04	0.692	1.00	1.30	0.926	No
2983	29.83	1.70	0.68	1.02	0.90	0.722	1.04	0.692	1.00	1.30	0.926	No
2984	29.84	1.70	0.68	1.02	0.90	0.722	1.04	0.692	1.00	1.30	0.926	No
2985	29.85	1.70	0.68	1.02	0.90	0.722	1.04	0.692	1.00	1.30	0.926	No
2986	29.86	1.70	0.68	1.02	0.90	0.722	1.04	0.692	1.00	1.30	0.926	No
2987	29.87	1.70	0.68	1.02	0.90	0.722	1.04	0.692	1.00	1.30	0.926	No
2988	29.88	1.70	0.68	1.02	0.90	0.722	1.04	0.692	1.00	1.30	0.926	No
2989	29.89	1.70	0.68	1.02	0.90	0.722	1.04	0.692	1.00	1.30	0.926	No
2990	29.90	1.70	0.68	1.02	0.90	0.722	1.04	0.692	1.00	1.30	0.925	No
2991	29.91	1.70	0.68	1.02	0.90	0.722	1.04	0.692	1.00	1.30	0.925	No
2992	29.92	1.70	0.68	1.02	0.90	0.722	1.04	0.692	1.00	1.30	0.925	No
2993	29.93	1.70	0.68	1.02	0.90	0.722	1.04	0.692	1.00	1.30	0.925	No
2994	29.94	1.70	0.68	1.02	0.90	0.722	1.04	0.692	1.00	1.30	0.925	No
2995	29.95	1.70	0.68	1.02	0.90	0.722	1.04	0.692	1.00	1.30	0.925	No
2996	29.96	1.71	0.69	1.02	0.90	0.722	1.04	0.692	1.00	1.30	0.925	No
2997	29.97	1.71	0.69	1.02	0.90	0.722	1.04	0.692	1.00	1.30	0.925	No
2998	29.98	1.71	0.69	1.02	0.90	0.722	1.04	0.692	1.00	1.30	0.925	No
2999	29.99	1.71	0.69	1.02	0.90	0.722	1.04	0.692	1.00	1.30	0.925	No
3000	30.00	1.71	0.69	1.02	0.90	0.722	1.04	0.692	1.00	1.30	0.925	No
3001	30.01	1.71	0.69	1.02	0.90	0.722	1.04	0.692	1.00	1.30	0.925	No
3002	30.02	1.71	0.69	1.02	0.90	0.722	1.04	0.692	1.00	1.30	0.925	No
3003	30.03	1.71	0.69	1.02	0.90	0.722	1.04	0.692	1.00	1.30	0.925	No
3004	30.04	1.71	0.69	1.02	0.90	0.722	1.04	0.692	1.00	1.30	0.925	No
3005	30.05	1.71	0.69	1.02	0.90	0.722	1.04	0.692	1.00	1.30	0.925	No
3006	30.06	1.71	0.69	1.02	0.90	0.722	1.04	0.692	1.00	1.30	0.925	No
3007	30.07	1.71	0.69	1.02	0.90	0.722	1.04	0.692	1.00	1.30	0.925	No
3008	30.08	1.71	0.69	1.02	0.90	0.722	1.04	0.692	1.00	1.30	0.925	No
3009	30.09	1.71	0.69	1.02	0.90	0.723	1.04	0.692	1.00	1.30	0.925	No
3010	30.10	1.71	0.69	1.02	0.90	0.723	1.04	0.693	1.00	1.30	0.925	No
3011	30.11	1.71	0.69	1.02	0.90	0.723	1.04	0.693	1.00	1.30	0.925	No
3012	30.12	1.72	0.69	1.03	0.90	0.723	1.04	0.693	1.00	1.30	0.925	No
3013	30.13	1.72	0.69	1.03	0.90	0.723	1.04	0.693	1.00	1.30	0.925	No
3014	30.14	1.72	0.69	1.03	0.90	0.723	1.04	0.693	1.00	1.30	0.925	No
3015	30.15	1.72	0.69	1.03	0.90	0.723	1.04	0.693	1.00	1.30	0.925	No
3016	30.16	1.72	0.69	1.03	0.90	0.723	1.04	0.693	1.00	1.30	0.925	No
3017	30.17	1.72	0.69	1.03	0.90	0.723	1.04	0.693	1.00	1.30	0.926	No
3018	30.18	1.72	0.69	1.03	0.90	0.723	1.04	0.693	1.00	1.30	0.926	No
3019	30.19	1.72	0.69	1.03	0.90	0.723	1.04	0.693	1.00	1.30	0.925	No
3020	30.20	1.72	0.69	1.03	0.90	0.723	1.04	0.693	1.00	1.30	0.925	No
3021	30.21	1.72	0.69	1.03	0.90	0.723	1.04	0.693	1.00	1.30	0.925	No
3022	30.22	1.72	0.69	1.03	0.90	0.723	1.04	0.693	1.00	1.30	0.925	No
3023	30.23	1.72	0.69	1.03	0.90	0.723	1.04	0.693	1.00	1.30	0.925	No
3024	30.24	1.72	0.69	1.03	0.90	0.723	1.04	0.693	1.00	1.30	0.925	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
3025	30.25	1.72	0.69	1.03	0.90	0.723	1.04	0.693	1.00	1.30	0.925	No
3026	30.26	1.72	0.69	1.03	0.90	0.723	1.04	0.693	1.00	1.30	0.925	No
3027	30.27	1.72	0.69	1.03	0.90	0.723	1.04	0.693	1.00	1.30	0.925	No
3028	30.28	1.73	0.70	1.03	0.90	0.723	1.04	0.693	1.00	1.30	0.925	No
3029	30.29	1.73	0.70	1.03	0.90	0.723	1.04	0.693	1.00	1.30	0.925	No
3030	30.30	1.73	0.70	1.03	0.90	0.723	1.04	0.693	1.00	1.30	0.925	No
3031	30.31	1.73	0.70	1.03	0.90	0.723	1.04	0.693	1.00	1.30	0.925	No
3032	30.32	1.73	0.70	1.03	0.90	0.723	1.04	0.693	1.00	1.30	0.925	No
3033	30.33	1.73	0.70	1.03	0.90	0.723	1.04	0.693	1.00	1.30	0.925	No
3034	30.34	1.73	0.70	1.03	0.90	0.723	1.04	0.693	1.00	1.30	0.925	No
3035	30.35	1.73	0.70	1.03	0.90	0.723	1.04	0.693	1.00	1.30	0.925	No
3036	30.36	1.73	0.70	1.03	0.90	0.723	1.04	0.693	1.00	1.30	0.925	No
3037	30.37	1.73	0.70	1.03	0.90	0.723	1.04	0.693	1.00	1.30	0.925	No
3038	30.38	1.73	0.70	1.03	0.90	0.723	1.04	0.693	1.00	1.30	0.925	No
3039	30.39	1.73	0.70	1.03	0.90	0.723	1.04	0.693	1.00	1.30	0.925	No
3040	30.40	1.73	0.70	1.03	0.90	0.723	1.04	0.693	1.00	1.30	0.925	No
3041	30.41	1.73	0.70	1.03	0.90	0.723	1.04	0.693	1.00	1.30	0.925	No
3042	30.42	1.73	0.70	1.03	0.90	0.723	1.04	0.693	1.00	1.30	0.925	No
3043	30.43	1.73	0.70	1.03	0.90	0.723	1.04	0.693	1.00	1.30	0.925	No
3044	30.44	1.74	0.70	1.03	0.90	0.723	1.04	0.693	1.00	1.30	0.925	No
3045	30.45	1.74	0.70	1.04	0.90	0.723	1.04	0.693	1.00	1.30	0.925	No
3046	30.46	1.74	0.70	1.04	0.90	0.723	1.04	0.693	1.00	1.30	0.926	No
3047	30.47	1.74	0.70	1.04	0.90	0.723	1.04	0.693	1.00	1.30	0.926	No
3048	30.48	1.74	0.70	1.04	0.90	0.723	1.04	0.693	1.00	1.30	0.926	No
3049	30.49	1.74	0.70	1.04	0.90	0.723	1.04	0.693	1.00	1.30	0.926	No
3050	30.50	1.74	0.70	1.04	0.90	0.723	1.04	0.693	1.00	1.30	0.926	No
3051	30.51	1.74	0.70	1.04	0.90	0.723	1.04	0.693	1.00	1.30	0.926	No
3052	30.52	1.74	0.70	1.04	0.90	0.723	1.04	0.693	1.00	1.30	0.926	No
3053	30.53	1.74	0.70	1.04	0.90	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3054	30.54	1.74	0.70	1.04	0.90	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3055	30.55	1.74	0.70	1.04	0.90	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3056	30.56	1.74	0.70	1.04	0.90	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3057	30.57	1.74	0.70	1.04	0.90	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3058	30.58	1.74	0.70	1.04	0.90	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3059	30.59	1.74	0.70	1.04	0.90	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3060	30.60	1.74	0.71	1.04	0.90	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3061	30.61	1.75	0.71	1.04	0.90	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3062	30.62	1.75	0.71	1.04	0.90	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3063	30.63	1.75	0.71	1.04	0.90	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3064	30.64	1.75	0.71	1.04	0.90	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3065	30.65	1.75	0.71	1.04	0.90	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3066	30.66	1.75	0.71	1.04	0.90	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3067	30.67	1.75	0.71	1.04	0.90	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3068	30.68	1.75	0.71	1.04	0.90	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3069	30.69	1.75	0.71	1.04	0.90	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3070	30.70	1.75	0.71	1.04	0.90	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3071	30.71	1.75	0.71	1.04	0.90	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3072	30.72	1.75	0.71	1.04	0.90	0.723	1.04	0.693	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
3073	30.73	1.75	0.71	1.04	0.89	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3074	30.74	1.75	0.71	1.04	0.89	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3075	30.75	1.75	0.71	1.04	0.89	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3076	30.76	1.76	0.71	1.04	0.89	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3077	30.77	1.76	0.71	1.05	0.89	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3078	30.78	1.76	0.71	1.05	0.89	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3079	30.79	1.76	0.71	1.05	0.89	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3080	30.80	1.76	0.71	1.05	0.89	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3081	30.81	1.76	0.71	1.05	0.89	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3082	30.82	1.76	0.71	1.05	0.89	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3083	30.83	1.76	0.71	1.05	0.89	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3084	30.84	1.76	0.71	1.05	0.89	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3085	30.85	1.76	0.71	1.05	0.89	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3086	30.86	1.76	0.71	1.05	0.89	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3087	30.87	1.76	0.71	1.05	0.89	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3088	30.88	1.76	0.71	1.05	0.89	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3089	30.89	1.76	0.71	1.05	0.89	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3090	30.90	1.76	0.71	1.05	0.89	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3091	30.91	1.76	0.71	1.05	0.89	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3092	30.92	1.77	0.72	1.05	0.89	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3093	30.93	1.77	0.72	1.05	0.89	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3094	30.94	1.77	0.72	1.05	0.89	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3095	30.95	1.77	0.72	1.05	0.89	0.723	1.04	0.693	1.00	1.30	2.000	Yes
3096	30.96	1.77	0.72	1.05	0.89	0.723	1.04	0.693	1.00	1.30	0.907	No
3097	30.97	1.77	0.72	1.05	0.89	0.723	1.04	0.693	1.00	1.30	0.907	No
3098	30.98	1.77	0.72	1.05	0.89	0.723	1.04	0.693	1.00	1.30	0.907	No
3099	30.99	1.77	0.72	1.05	0.89	0.723	1.04	0.693	1.00	1.30	0.907	No
3100	31.00	1.77	0.72	1.05	0.89	0.723	1.04	0.693	1.00	1.30	0.907	No
3101	31.01	1.77	0.72	1.05	0.89	0.723	1.04	0.693	1.00	1.30	0.907	No
3102	31.02	1.77	0.72	1.05	0.89	0.723	1.04	0.693	1.00	1.30	0.907	No
3103	31.03	1.77	0.72	1.05	0.89	0.723	1.04	0.693	1.00	1.30	0.906	No
3104	31.04	1.77	0.72	1.05	0.89	0.723	1.04	0.693	1.00	1.30	0.906	No
3105	31.05	1.77	0.72	1.05	0.89	0.723	1.04	0.693	1.00	1.30	0.906	No
3106	31.06	1.77	0.72	1.05	0.89	0.723	1.04	0.693	1.00	1.30	0.906	No
3107	31.07	1.77	0.72	1.05	0.89	0.723	1.04	0.693	1.00	1.30	0.906	No
3108	31.08	1.78	0.72	1.06	0.89	0.723	1.04	0.693	1.00	1.30	0.907	No
3109	31.09	1.78	0.72	1.06	0.89	0.723	1.04	0.693	1.00	1.30	0.907	No
3110	31.10	1.78	0.72	1.06	0.89	0.723	1.04	0.693	1.00	1.30	0.907	No
3111	31.11	1.78	0.72	1.06	0.89	0.723	1.04	0.693	1.00	1.30	0.907	No
3112	31.12	1.78	0.72	1.06	0.89	0.723	1.04	0.693	1.00	1.30	0.907	No
3113	31.13	1.78	0.72	1.06	0.89	0.723	1.04	0.693	1.00	1.30	0.907	No
3114	31.14	1.78	0.72	1.06	0.89	0.723	1.04	0.693	1.00	1.30	0.907	No
3115	31.15	1.78	0.72	1.06	0.89	0.723	1.04	0.693	1.00	1.30	0.907	No
3116	31.16	1.78	0.72	1.06	0.89	0.723	1.04	0.693	1.00	1.30	0.907	No
3117	31.17	1.78	0.72	1.06	0.89	0.723	1.04	0.693	1.00	1.30	0.906	No
3118	31.18	1.78	0.72	1.06	0.89	0.723	1.04	0.693	1.00	1.30	0.906	No
3119	31.19	1.78	0.72	1.06	0.89	0.723	1.04	0.693	1.00	1.30	0.906	No
3120	31.20	1.78	0.72	1.06	0.89	0.723	1.04	0.693	1.00	1.30	0.906	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
3121	31.21	1.78	0.72	1.06	0.89	0.723	1.04	0.693	1.00	1.30	0.906	No
3122	31.22	1.78	0.72	1.06	0.89	0.723	1.04	0.693	1.00	1.30	0.906	No
3123	31.23	1.79	0.72	1.06	0.89	0.723	1.04	0.693	1.00	1.30	0.906	No
3124	31.24	1.79	0.73	1.06	0.89	0.723	1.04	0.693	1.00	1.30	0.906	No
3125	31.25	1.79	0.73	1.06	0.89	0.723	1.04	0.693	1.00	1.30	0.906	No
3126	31.26	1.79	0.73	1.06	0.89	0.723	1.04	0.693	1.00	1.30	0.905	No
3127	31.27	1.79	0.73	1.06	0.89	0.723	1.04	0.693	1.00	1.30	0.905	No
3128	31.28	1.79	0.73	1.06	0.89	0.723	1.04	0.693	1.00	1.30	0.905	No
3129	31.29	1.79	0.73	1.06	0.89	0.723	1.04	0.693	1.00	1.30	0.905	No
3130	31.30	1.79	0.73	1.06	0.89	0.723	1.04	0.693	1.00	1.30	0.905	No
3131	31.31	1.79	0.73	1.06	0.89	0.723	1.04	0.693	1.00	1.30	0.905	No
3132	31.32	1.79	0.73	1.06	0.89	0.723	1.04	0.693	1.00	1.30	0.904	No
3133	31.33	1.79	0.73	1.06	0.89	0.723	1.04	0.693	1.00	1.30	0.904	No
3134	31.34	1.79	0.73	1.06	0.89	0.723	1.04	0.693	1.00	1.30	0.904	No
3135	31.35	1.79	0.73	1.06	0.89	0.723	1.04	0.693	1.00	1.30	0.904	No
3136	31.36	1.79	0.73	1.06	0.89	0.723	1.04	0.693	1.00	1.30	0.903	No
3137	31.37	1.79	0.73	1.07	0.89	0.723	1.04	0.693	1.00	1.30	0.903	No
3138	31.38	1.79	0.73	1.07	0.89	0.723	1.04	0.693	1.00	1.30	0.903	No
3139	31.39	1.80	0.73	1.07	0.89	0.723	1.04	0.693	1.00	1.30	0.903	No
3140	31.40	1.80	0.73	1.07	0.89	0.723	1.04	0.693	1.00	1.30	0.902	No
3141	31.41	1.80	0.73	1.07	0.89	0.723	1.04	0.693	1.00	1.30	0.902	No
3142	31.42	1.80	0.73	1.07	0.89	0.723	1.04	0.693	1.00	1.30	0.901	No
3143	31.43	1.80	0.73	1.07	0.89	0.723	1.04	0.693	1.00	1.30	0.901	No
3144	31.44	1.80	0.73	1.07	0.89	0.723	1.04	0.693	1.00	1.30	0.900	No
3145	31.45	1.80	0.73	1.07	0.89	0.723	1.04	0.693	1.00	1.30	0.899	No
3146	31.46	1.80	0.73	1.07	0.89	0.723	1.04	0.693	1.00	1.30	0.899	No
3147	31.47	1.80	0.73	1.07	0.89	0.723	1.04	0.693	1.00	1.30	0.899	No
3148	31.48	1.80	0.73	1.07	0.89	0.723	1.04	0.693	1.00	1.30	0.898	No
3149	31.49	1.80	0.73	1.07	0.89	0.723	1.04	0.693	1.00	1.30	0.898	No
3150	31.50	1.80	0.73	1.07	0.89	0.723	1.04	0.693	1.00	1.30	0.897	No
3151	31.51	1.80	0.73	1.07	0.89	0.723	1.04	0.693	1.00	1.30	0.896	No
3152	31.52	1.80	0.73	1.07	0.89	0.723	1.04	0.693	1.00	1.30	0.896	No
3153	31.53	1.80	0.73	1.07	0.89	0.723	1.04	0.693	1.00	1.30	0.895	No
3154	31.54	1.81	0.73	1.07	0.89	0.723	1.04	0.693	1.00	1.30	0.894	No
3155	31.55	1.81	0.73	1.07	0.89	0.723	1.04	0.693	1.00	1.30	0.894	No
3156	31.56	1.81	0.74	1.07	0.89	0.723	1.04	0.693	1.00	1.30	0.893	No
3157	31.57	1.81	0.74	1.07	0.89	0.723	1.04	0.693	1.00	1.30	0.893	No
3158	31.58	1.81	0.74	1.07	0.89	0.723	1.04	0.693	1.00	1.30	0.892	No
3159	31.59	1.81	0.74	1.07	0.89	0.723	1.04	0.693	1.00	1.30	0.892	No
3160	31.60	1.81	0.74	1.07	0.89	0.723	1.04	0.693	1.00	1.30	0.891	No
3161	31.61	1.81	0.74	1.07	0.89	0.723	1.04	0.693	1.00	1.30	0.890	No
3162	31.62	1.81	0.74	1.07	0.89	0.723	1.04	0.693	1.00	1.30	0.890	No
3163	31.63	1.81	0.74	1.07	0.89	0.723	1.04	0.693	1.00	1.30	0.889	No
3164	31.64	1.81	0.74	1.07	0.89	0.723	1.04	0.693	1.00	1.30	0.889	No
3165	31.65	1.81	0.74	1.07	0.89	0.723	1.04	0.693	1.00	1.30	0.888	No
3166	31.66	1.81	0.74	1.07	0.89	0.723	1.04	0.693	1.00	1.30	0.888	No
3167	31.67	1.81	0.74	1.08	0.89	0.723	1.04	0.693	1.00	1.30	0.887	No
3168	31.68	1.81	0.74	1.08	0.89	0.723	1.04	0.693	1.00	1.30	0.887	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
3169	31.69	1.82	0.74	1.08	0.89	0.723	1.04	0.693	1.00	1.30	0.886	No
3170	31.70	1.82	0.74	1.08	0.89	0.723	1.04	0.693	1.00	1.30	0.886	No
3171	31.71	1.82	0.74	1.08	0.89	0.723	1.04	0.693	1.00	1.30	0.886	No
3172	31.72	1.82	0.74	1.08	0.89	0.723	1.04	0.693	1.00	1.30	0.886	No
3173	31.73	1.82	0.74	1.08	0.89	0.723	1.04	0.693	1.00	1.30	0.886	No
3174	31.74	1.82	0.74	1.08	0.89	0.723	1.04	0.693	1.00	1.30	0.886	No
3175	31.75	1.82	0.74	1.08	0.89	0.723	1.04	0.693	1.00	1.30	0.886	No
3176	31.76	1.82	0.74	1.08	0.89	0.723	1.04	0.693	1.00	1.30	0.886	No
3177	31.77	1.82	0.74	1.08	0.89	0.723	1.04	0.693	1.00	1.30	0.886	No
3178	31.78	1.82	0.74	1.08	0.89	0.723	1.04	0.692	1.00	1.30	0.886	No
3179	31.79	1.82	0.74	1.08	0.89	0.722	1.04	0.692	1.00	1.30	0.886	No
3180	31.80	1.82	0.74	1.08	0.89	0.722	1.04	0.692	1.00	1.30	0.886	No
3181	31.81	1.82	0.74	1.08	0.89	0.722	1.04	0.692	1.00	1.30	0.886	No
3182	31.82	1.82	0.74	1.08	0.89	0.722	1.04	0.692	1.00	1.30	0.886	No
3183	31.83	1.82	0.74	1.08	0.89	0.722	1.04	0.692	0.99	1.30	0.886	No
3184	31.84	1.82	0.74	1.08	0.89	0.722	1.04	0.692	0.99	1.30	0.887	No
3185	31.85	1.83	0.74	1.08	0.89	0.722	1.04	0.692	0.99	1.30	0.887	No
3186	31.86	1.83	0.74	1.08	0.89	0.722	1.04	0.692	0.99	1.30	0.887	No
3187	31.87	1.83	0.74	1.08	0.89	0.722	1.04	0.692	0.99	1.30	0.887	No
3188	31.88	1.83	0.75	1.08	0.89	0.722	1.04	0.692	0.99	1.30	0.887	No
3189	31.89	1.83	0.75	1.08	0.89	0.722	1.04	0.692	0.99	1.30	0.887	No
3190	31.90	1.83	0.75	1.08	0.89	0.722	1.04	0.692	0.99	1.30	0.887	No
3191	31.91	1.83	0.75	1.08	0.89	0.722	1.04	0.692	0.99	1.30	0.887	No
3192	31.92	1.83	0.75	1.08	0.89	0.722	1.04	0.692	0.99	1.30	0.887	No
3193	31.93	1.83	0.75	1.08	0.89	0.722	1.04	0.692	0.99	1.30	0.887	No
3194	31.94	1.83	0.75	1.08	0.89	0.722	1.04	0.692	0.99	1.30	0.887	No
3195	31.95	1.83	0.75	1.08	0.89	0.722	1.04	0.692	0.99	1.30	0.887	No
3196	31.96	1.83	0.75	1.09	0.89	0.722	1.04	0.692	0.99	1.30	0.887	No
3197	31.97	1.83	0.75	1.09	0.89	0.722	1.04	0.692	0.99	1.30	0.887	No
3198	31.98	1.83	0.75	1.09	0.89	0.722	1.04	0.692	0.99	1.30	0.887	No
3199	31.99	1.83	0.75	1.09	0.89	0.722	1.04	0.692	0.99	1.30	0.888	No
3200	32.00	1.84	0.75	1.09	0.89	0.722	1.04	0.692	0.99	1.30	0.888	No
3201	32.01	1.84	0.75	1.09	0.89	0.722	1.04	0.692	0.99	1.30	0.888	No
3202	32.02	1.84	0.75	1.09	0.89	0.722	1.04	0.692	0.99	1.30	0.888	No
3203	32.03	1.84	0.75	1.09	0.89	0.722	1.04	0.692	0.99	1.30	0.888	No
3204	32.04	1.84	0.75	1.09	0.89	0.722	1.04	0.692	0.99	1.30	0.888	No
3205	32.05	1.84	0.75	1.09	0.89	0.722	1.04	0.692	0.99	1.30	0.888	No
3206	32.06	1.84	0.75	1.09	0.89	0.722	1.04	0.692	0.99	1.30	0.888	No
3207	32.07	1.84	0.75	1.09	0.89	0.722	1.04	0.692	0.99	1.30	0.888	No
3208	32.08	1.84	0.75	1.09	0.89	0.722	1.04	0.692	0.99	1.30	0.888	No
3209	32.09	1.84	0.75	1.09	0.89	0.722	1.04	0.692	0.99	1.30	0.888	No
3210	32.10	1.84	0.75	1.09	0.89	0.722	1.04	0.692	0.99	1.30	0.888	No
3211	32.11	1.84	0.75	1.09	0.89	0.722	1.04	0.692	0.99	1.30	0.888	No
3212	32.12	1.84	0.75	1.09	0.89	0.722	1.04	0.692	0.99	1.30	0.888	No
3213	32.13	1.84	0.75	1.09	0.89	0.722	1.04	0.692	0.99	1.30	0.888	No
3214	32.14	1.84	0.75	1.09	0.89	0.722	1.04	0.692	0.99	1.30	0.888	No
3215	32.15	1.85	0.75	1.09	0.89	0.722	1.04	0.692	0.99	1.30	0.888	No
3216	32.16	1.85	0.75	1.09	0.89	0.722	1.04	0.692	0.99	1.30	0.888	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
3217	32.17	1.85	0.75	1.09	0.89	0.722	1.04	0.692	0.99	1.30	0.889	No
3218	32.18	1.85	0.75	1.09	0.89	0.722	1.04	0.692	0.99	1.30	0.889	No
3219	32.19	1.85	0.75	1.09	0.89	0.722	1.04	0.692	0.99	1.30	0.889	No
3220	32.20	1.85	0.76	1.09	0.89	0.722	1.04	0.692	0.99	1.30	0.889	No
3221	32.21	1.85	0.76	1.09	0.89	0.722	1.04	0.692	0.99	1.30	0.889	No
3222	32.22	1.85	0.76	1.09	0.89	0.722	1.04	0.692	0.99	1.30	0.889	No
3223	32.23	1.85	0.76	1.09	0.89	0.722	1.04	0.692	0.99	1.30	0.889	No
3224	32.24	1.85	0.76	1.09	0.89	0.722	1.04	0.692	0.99	1.30	0.889	No
3225	32.25	1.85	0.76	1.10	0.89	0.722	1.04	0.692	0.99	1.30	0.889	No
3226	32.26	1.85	0.76	1.10	0.89	0.722	1.04	0.692	0.99	1.30	0.889	No
3227	32.27	1.85	0.76	1.10	0.89	0.722	1.04	0.692	0.99	1.30	0.889	No
3228	32.28	1.85	0.76	1.10	0.89	0.722	1.04	0.692	0.99	1.30	0.889	No
3229	32.29	1.85	0.76	1.10	0.89	0.722	1.04	0.692	0.99	1.30	0.889	No
3230	32.30	1.86	0.76	1.10	0.89	0.722	1.04	0.692	0.99	1.30	0.889	No
3231	32.31	1.86	0.76	1.10	0.89	0.722	1.04	0.692	0.99	1.30	0.889	No
3232	32.32	1.86	0.76	1.10	0.89	0.722	1.04	0.692	0.99	1.30	0.889	No
3233	32.33	1.86	0.76	1.10	0.89	0.722	1.04	0.692	0.99	1.30	0.889	No
3234	32.34	1.86	0.76	1.10	0.89	0.722	1.04	0.692	0.99	1.30	0.889	No
3235	32.35	1.86	0.76	1.10	0.89	0.722	1.04	0.692	0.99	1.30	0.889	No
3236	32.36	1.86	0.76	1.10	0.89	0.722	1.04	0.692	0.99	1.30	0.890	No
3237	32.37	1.86	0.76	1.10	0.89	0.722	1.04	0.692	0.99	1.30	0.890	No
3238	32.38	1.86	0.76	1.10	0.89	0.722	1.04	0.692	0.99	1.30	0.890	No
3239	32.39	1.86	0.76	1.10	0.89	0.722	1.04	0.692	0.99	1.30	0.890	No
3240	32.40	1.86	0.76	1.10	0.89	0.722	1.04	0.692	0.99	1.30	0.890	No
3241	32.41	1.86	0.76	1.10	0.89	0.722	1.04	0.692	0.99	1.30	0.890	No
3242	32.42	1.86	0.76	1.10	0.89	0.722	1.04	0.692	0.99	1.30	0.890	No
3243	32.43	1.86	0.76	1.10	0.89	0.722	1.04	0.692	0.99	1.30	0.890	No
3244	32.44	1.86	0.76	1.10	0.89	0.722	1.04	0.692	0.99	1.30	0.890	No
3245	32.45	1.86	0.76	1.10	0.89	0.722	1.04	0.692	0.99	1.30	0.890	No
3246	32.46	1.87	0.76	1.10	0.89	0.722	1.04	0.692	0.99	1.30	0.890	No
3247	32.47	1.87	0.76	1.10	0.89	0.722	1.04	0.692	0.99	1.30	0.890	No
3248	32.48	1.87	0.76	1.10	0.89	0.722	1.04	0.692	0.99	1.30	0.890	No
3249	32.49	1.87	0.76	1.10	0.89	0.722	1.04	0.692	0.99	1.30	0.890	No
3250	32.50	1.87	0.76	1.10	0.89	0.722	1.04	0.692	0.99	1.30	0.890	No
3251	32.51	1.87	0.76	1.10	0.89	0.722	1.04	0.692	0.99	1.30	0.890	No
3252	32.52	1.87	0.77	1.10	0.89	0.722	1.04	0.692	0.99	1.30	0.890	No
3253	32.53	1.87	0.77	1.10	0.89	0.722	1.04	0.692	0.99	1.30	0.891	No
3254	32.54	1.87	0.77	1.11	0.89	0.722	1.04	0.692	0.99	1.30	0.891	No
3255	32.55	1.87	0.77	1.11	0.89	0.722	1.04	0.692	0.99	1.30	0.891	No
3256	32.56	1.87	0.77	1.11	0.89	0.722	1.04	0.692	0.99	1.30	0.891	No
3257	32.57	1.87	0.77	1.11	0.89	0.722	1.04	0.692	0.99	1.30	0.891	No
3258	32.58	1.87	0.77	1.11	0.89	0.722	1.04	0.692	0.99	1.30	0.891	No
3259	32.59	1.87	0.77	1.11	0.89	0.722	1.04	0.692	0.99	1.30	0.891	No
3260	32.60	1.87	0.77	1.11	0.89	0.722	1.04	0.692	0.99	1.30	0.891	No
3261	32.61	1.88	0.77	1.11	0.89	0.722	1.04	0.692	0.99	1.30	0.891	No
3262	32.62	1.88	0.77	1.11	0.89	0.722	1.04	0.692	0.99	1.30	0.891	No
3263	32.63	1.88	0.77	1.11	0.89	0.722	1.04	0.692	0.99	1.30	0.892	No
3264	32.64	1.88	0.77	1.11	0.89	0.722	1.04	0.692	0.99	1.30	0.892	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
3265	32.65	1.88	0.77	1.11	0.89	0.722	1.04	0.692	0.99	1.30	0.892	No
3266	32.66	1.88	0.77	1.11	0.89	0.722	1.04	0.692	0.99	1.30	0.892	No
3267	32.67	1.88	0.77	1.11	0.89	0.722	1.04	0.692	0.99	1.30	0.892	No
3268	32.68	1.88	0.77	1.11	0.89	0.722	1.04	0.692	0.99	1.30	0.893	No
3269	32.69	1.88	0.77	1.11	0.89	0.722	1.04	0.692	0.99	1.30	0.893	No
3270	32.70	1.88	0.77	1.11	0.89	0.722	1.04	0.692	0.99	1.30	0.893	No
3271	32.71	1.88	0.77	1.11	0.89	0.722	1.04	0.692	0.99	1.30	0.893	No
3272	32.72	1.88	0.77	1.11	0.89	0.722	1.04	0.692	0.99	1.30	0.894	No
3273	32.73	1.88	0.77	1.11	0.89	0.722	1.04	0.692	0.99	1.30	0.894	No
3274	32.74	1.88	0.77	1.11	0.89	0.722	1.04	0.692	0.99	1.30	0.894	No
3275	32.75	1.88	0.77	1.11	0.89	0.722	1.04	0.692	0.98	1.30	0.894	No
3276	32.76	1.89	0.77	1.11	0.89	0.722	1.04	0.692	0.98	1.30	0.894	No
3277	32.77	1.89	0.77	1.11	0.89	0.722	1.04	0.692	0.98	1.30	0.894	No
3278	32.78	1.89	0.77	1.11	0.89	0.722	1.04	0.692	0.98	1.30	0.895	No
3279	32.79	1.89	0.77	1.11	0.89	0.721	1.04	0.692	0.98	1.30	0.895	No
3280	32.80	1.89	0.77	1.11	0.89	0.721	1.04	0.692	0.98	1.30	0.895	No
3281	32.81	1.89	0.77	1.11	0.89	0.721	1.04	0.691	0.98	1.30	0.895	No
3282	32.82	1.89	0.77	1.12	0.89	0.721	1.04	0.691	0.98	1.30	0.895	No
3283	32.83	1.89	0.77	1.12	0.89	0.721	1.04	0.691	0.98	1.30	0.895	No
3284	32.84	1.89	0.78	1.12	0.89	0.721	1.04	0.691	0.98	1.30	0.895	No
3285	32.85	1.89	0.78	1.12	0.89	0.721	1.04	0.691	0.98	1.30	0.895	No
3286	32.86	1.89	0.78	1.12	0.88	0.721	1.04	0.691	0.98	1.30	0.895	No
3287	32.87	1.89	0.78	1.12	0.88	0.721	1.04	0.691	0.98	1.30	0.895	No
3288	32.88	1.89	0.78	1.12	0.88	0.721	1.04	0.691	0.98	1.30	0.895	No
3289	32.89	1.89	0.78	1.12	0.88	0.721	1.04	0.691	0.98	1.30	0.895	No
3290	32.90	1.89	0.78	1.12	0.88	0.721	1.04	0.691	0.98	1.30	0.895	No
3291	32.91	1.90	0.78	1.12	0.88	0.721	1.04	0.691	0.98	1.30	0.895	No
3292	32.92	1.90	0.78	1.12	0.88	0.721	1.04	0.691	0.98	1.30	0.896	No
3293	32.93	1.90	0.78	1.12	0.88	0.721	1.04	0.691	0.98	1.30	0.896	No
3294	32.94	1.90	0.78	1.12	0.88	0.721	1.04	0.691	0.98	1.30	0.896	No
3295	32.95	1.90	0.78	1.12	0.88	0.721	1.04	0.691	0.98	1.30	0.896	No
3296	32.96	1.90	0.78	1.12	0.88	0.721	1.04	0.691	0.98	1.30	0.896	No
3297	32.97	1.90	0.78	1.12	0.88	0.721	1.04	0.691	0.98	1.30	0.896	No
3298	32.98	1.90	0.78	1.12	0.88	0.721	1.04	0.691	0.98	1.30	0.896	No
3299	32.99	1.90	0.78	1.12	0.88	0.721	1.04	0.691	0.98	1.30	0.896	No
3300	33.00	1.90	0.78	1.12	0.88	0.721	1.04	0.691	0.98	1.30	0.896	No
3301	33.01	1.90	0.78	1.12	0.88	0.721	1.04	0.691	0.98	1.30	0.896	No
3302	33.02	1.90	0.78	1.12	0.88	0.721	1.04	0.691	0.98	1.30	0.896	No
3303	33.03	1.90	0.78	1.12	0.88	0.721	1.04	0.691	0.98	1.30	0.896	No
3304	33.04	1.90	0.78	1.12	0.88	0.721	1.04	0.691	0.98	1.30	0.896	No
3305	33.05	1.90	0.78	1.12	0.88	0.721	1.04	0.691	0.98	1.30	0.896	No
3306	33.06	1.91	0.78	1.12	0.88	0.721	1.04	0.691	0.98	1.30	0.896	No
3307	33.07	1.91	0.78	1.12	0.88	0.721	1.04	0.691	0.98	1.30	0.897	No
3308	33.08	1.91	0.78	1.12	0.88	0.721	1.04	0.691	0.98	1.30	0.897	No
3309	33.09	1.91	0.78	1.12	0.88	0.721	1.04	0.691	0.98	1.30	0.897	No
3310	33.10	1.91	0.78	1.13	0.88	0.721	1.04	0.691	0.98	1.30	0.897	No
3311	33.11	1.91	0.78	1.13	0.88	0.721	1.04	0.691	0.98	1.30	0.897	No
3312	33.12	1.91	0.78	1.13	0.88	0.721	1.04	0.691	0.98	1.30	0.897	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
3313	33.13	1.91	0.78	1.13	0.88	0.721	1.04	0.691	0.98	1.30	0.897	No
3314	33.14	1.91	0.78	1.13	0.88	0.721	1.04	0.691	0.98	1.30	0.897	No
3315	33.15	1.91	0.78	1.13	0.88	0.721	1.04	0.691	0.98	1.30	0.897	No
3316	33.16	1.91	0.78	1.13	0.88	0.721	1.04	0.691	0.98	1.30	0.897	No
3317	33.17	1.91	0.79	1.13	0.88	0.721	1.04	0.691	0.98	1.30	0.897	No
3318	33.18	1.91	0.79	1.13	0.88	0.721	1.04	0.691	0.98	1.30	0.897	No
3319	33.19	1.91	0.79	1.13	0.88	0.721	1.04	0.691	0.98	1.30	0.897	No
3320	33.20	1.91	0.79	1.13	0.88	0.721	1.04	0.691	0.98	1.30	0.897	No
3321	33.21	1.92	0.79	1.13	0.88	0.721	1.04	0.691	0.98	1.30	0.898	No
3322	33.22	1.92	0.79	1.13	0.88	0.721	1.04	0.691	0.98	1.30	0.898	No
3323	33.23	1.92	0.79	1.13	0.88	0.721	1.04	0.691	0.98	1.30	0.898	No
3324	33.24	1.92	0.79	1.13	0.88	0.721	1.04	0.691	0.98	1.30	0.898	No
3325	33.25	1.92	0.79	1.13	0.88	0.721	1.04	0.691	0.98	1.30	0.898	No
3326	33.26	1.92	0.79	1.13	0.88	0.721	1.04	0.691	0.98	1.30	0.898	No
3327	33.27	1.92	0.79	1.13	0.88	0.721	1.04	0.691	0.98	1.30	0.898	No
3328	33.28	1.92	0.79	1.13	0.88	0.721	1.04	0.691	0.98	1.30	0.898	No
3329	33.29	1.92	0.79	1.13	0.88	0.721	1.04	0.691	0.98	1.30	0.898	No
3330	33.30	1.92	0.79	1.13	0.88	0.721	1.04	0.691	0.98	1.30	0.898	No
3331	33.31	1.92	0.79	1.13	0.88	0.721	1.04	0.691	0.98	1.30	0.898	No
3332	33.32	1.92	0.79	1.13	0.88	0.721	1.04	0.691	0.98	1.30	0.898	No
3333	33.33	1.92	0.79	1.13	0.88	0.721	1.04	0.691	0.98	1.30	0.898	No
3334	33.34	1.92	0.79	1.13	0.88	0.721	1.04	0.691	0.98	1.30	0.898	No
3335	33.35	1.93	0.79	1.13	0.88	0.721	1.04	0.691	0.98	1.30	0.898	No
3336	33.36	1.93	0.79	1.13	0.88	0.721	1.04	0.691	0.98	1.30	0.899	No
3337	33.37	1.93	0.79	1.13	0.88	0.721	1.04	0.691	0.98	1.30	0.899	No
3338	33.38	1.93	0.79	1.14	0.88	0.721	1.04	0.691	0.98	1.30	0.899	No
3339	33.39	1.93	0.79	1.14	0.88	0.721	1.04	0.691	0.98	1.30	0.899	No
3340	33.40	1.93	0.79	1.14	0.88	0.721	1.04	0.691	0.98	1.30	0.899	No
3341	33.41	1.93	0.79	1.14	0.88	0.721	1.04	0.691	0.98	1.30	0.899	No
3342	33.42	1.93	0.79	1.14	0.88	0.721	1.04	0.691	0.98	1.30	0.899	No
3343	33.43	1.93	0.79	1.14	0.88	0.721	1.04	0.691	0.98	1.30	0.899	No
3344	33.44	1.93	0.79	1.14	0.88	0.721	1.04	0.691	0.98	1.30	0.899	No
3345	33.45	1.93	0.79	1.14	0.88	0.720	1.04	0.691	0.98	1.30	0.899	No
3346	33.46	1.93	0.79	1.14	0.88	0.720	1.04	0.691	0.98	1.30	0.899	No
3347	33.47	1.93	0.79	1.14	0.88	0.720	1.04	0.691	0.98	1.30	0.899	No
3348	33.48	1.93	0.79	1.14	0.88	0.720	1.04	0.691	0.98	1.30	0.899	No
3349	33.49	1.93	0.80	1.14	0.88	0.720	1.04	0.691	0.98	1.30	0.899	No
3350	33.50	1.94	0.80	1.14	0.88	0.720	1.04	0.690	0.98	1.30	0.899	No
3351	33.51	1.94	0.80	1.14	0.88	0.720	1.04	0.690	0.98	1.30	0.900	No
3352	33.52	1.94	0.80	1.14	0.88	0.720	1.04	0.690	0.98	1.30	0.900	No
3353	33.53	1.94	0.80	1.14	0.88	0.720	1.04	0.690	0.98	1.30	0.900	No
3354	33.54	1.94	0.80	1.14	0.88	0.720	1.04	0.690	0.98	1.30	0.900	No
3355	33.55	1.94	0.80	1.14	0.88	0.720	1.04	0.690	0.98	1.30	0.900	No
3356	33.56	1.94	0.80	1.14	0.88	0.720	1.04	0.690	0.98	1.30	0.900	No
3357	33.57	1.94	0.80	1.14	0.88	0.720	1.04	0.690	0.98	1.30	0.900	No
3358	33.58	1.94	0.80	1.14	0.88	0.720	1.04	0.690	0.98	1.30	0.900	No
3359	33.59	1.94	0.80	1.14	0.88	0.720	1.04	0.690	0.98	1.30	0.900	No
3360	33.60	1.94	0.80	1.14	0.88	0.720	1.04	0.690	0.98	1.30	0.900	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
3361	33.61	1.94	0.80	1.14	0.88	0.720	1.04	0.690	0.98	1.30	0.900	No
3362	33.62	1.94	0.80	1.14	0.88	0.720	1.04	0.690	0.98	1.30	0.900	No
3363	33.63	1.94	0.80	1.14	0.88	0.720	1.04	0.690	0.98	1.30	0.900	No
3364	33.64	1.94	0.80	1.14	0.88	0.720	1.04	0.690	0.98	1.30	0.900	No
3365	33.65	1.95	0.80	1.14	0.88	0.720	1.04	0.690	0.98	1.30	0.900	No
3366	33.66	1.95	0.80	1.15	0.88	0.720	1.04	0.690	0.98	1.30	0.901	No
3367	33.67	1.95	0.80	1.15	0.88	0.720	1.04	0.690	0.98	1.30	0.901	No
3368	33.68	1.95	0.80	1.15	0.88	0.720	1.04	0.690	0.98	1.30	0.901	No
3369	33.69	1.95	0.80	1.15	0.88	0.720	1.04	0.690	0.98	1.30	0.901	No
3370	33.70	1.95	0.80	1.15	0.88	0.720	1.04	0.690	0.98	1.30	0.901	No
3371	33.71	1.95	0.80	1.15	0.88	0.720	1.04	0.690	0.98	1.30	0.901	No
3372	33.72	1.95	0.80	1.15	0.88	0.720	1.04	0.690	0.98	1.30	0.901	No
3373	33.73	1.95	0.80	1.15	0.88	0.720	1.04	0.690	0.98	1.30	0.901	No
3374	33.74	1.95	0.80	1.15	0.88	0.720	1.04	0.690	0.98	1.30	0.901	No
3375	33.75	1.95	0.80	1.15	0.88	0.720	1.04	0.690	0.98	1.30	0.900	No
3376	33.76	1.95	0.80	1.15	0.88	0.720	1.04	0.690	0.98	1.30	0.900	No
3377	33.77	1.95	0.80	1.15	0.88	0.720	1.04	0.690	0.98	1.30	0.900	No
3378	33.78	1.95	0.80	1.15	0.88	0.720	1.04	0.690	0.98	1.30	0.900	No
3379	33.79	1.95	0.80	1.15	0.88	0.720	1.04	0.690	0.98	1.30	0.900	No
3380	33.80	1.96	0.80	1.15	0.88	0.720	1.04	0.690	0.98	1.30	0.899	No
3381	33.81	1.96	0.81	1.15	0.88	0.720	1.04	0.690	0.98	1.30	0.899	No
3382	33.82	1.96	0.81	1.15	0.88	0.720	1.04	0.690	0.98	1.30	0.899	No
3383	33.83	1.96	0.81	1.15	0.88	0.720	1.04	0.690	0.98	1.30	0.899	No
3384	33.84	1.96	0.81	1.15	0.88	0.720	1.04	0.690	0.98	1.30	0.899	No
3385	33.85	1.96	0.81	1.15	0.88	0.720	1.04	0.690	0.98	1.30	0.899	No
3386	33.86	1.96	0.81	1.15	0.88	0.720	1.04	0.690	0.98	1.30	0.899	No
3387	33.87	1.96	0.81	1.15	0.88	0.720	1.04	0.690	0.98	1.30	0.898	No
3388	33.88	1.96	0.81	1.15	0.88	0.720	1.04	0.690	0.98	1.30	0.898	No
3389	33.89	1.96	0.81	1.15	0.88	0.720	1.04	0.690	0.98	1.30	0.898	No
3390	33.90	1.96	0.81	1.15	0.88	0.720	1.04	0.690	0.98	1.30	0.898	No
3391	33.91	1.96	0.81	1.15	0.88	0.720	1.04	0.690	0.98	1.30	0.898	No
3392	33.92	1.96	0.81	1.15	0.88	0.720	1.04	0.690	0.98	1.30	0.898	No
3393	33.93	1.96	0.81	1.15	0.88	0.720	1.04	0.690	0.98	1.30	0.898	No
3394	33.94	1.96	0.81	1.16	0.88	0.720	1.04	0.690	0.98	1.30	0.898	No
3395	33.95	1.97	0.81	1.16	0.88	0.720	1.04	0.690	0.98	1.30	0.898	No
3396	33.96	1.97	0.81	1.16	0.88	0.720	1.04	0.690	0.98	1.30	0.898	No
3397	33.97	1.97	0.81	1.16	0.88	0.720	1.04	0.690	0.98	1.30	0.898	No
3398	33.98	1.97	0.81	1.16	0.88	0.720	1.04	0.690	0.98	1.30	0.898	No
3399	33.99	1.97	0.81	1.16	0.88	0.720	1.04	0.690	0.98	1.30	0.899	No
3400	34.00	1.97	0.81	1.16	0.88	0.720	1.04	0.690	0.98	1.30	0.899	No
3401	34.01	1.97	0.81	1.16	0.88	0.720	1.04	0.690	0.98	1.30	0.899	No
3402	34.02	1.97	0.81	1.16	0.88	0.720	1.04	0.690	0.98	1.30	0.899	No
3403	34.03	1.97	0.81	1.16	0.88	0.720	1.04	0.690	0.98	1.30	0.899	No
3404	34.04	1.97	0.81	1.16	0.88	0.720	1.04	0.690	0.98	1.30	0.899	No
3405	34.05	1.97	0.81	1.16	0.88	0.720	1.04	0.690	0.98	1.30	0.899	No
3406	34.06	1.97	0.81	1.16	0.88	0.720	1.04	0.690	0.98	1.30	0.899	No
3407	34.07	1.97	0.81	1.16	0.88	0.720	1.04	0.690	0.98	1.30	0.899	No
3408	34.08	1.97	0.81	1.16	0.88	0.720	1.04	0.690	0.98	1.30	0.899	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
3409	34.09	1.97	0.81	1.16	0.88	0.720	1.04	0.690	0.98	1.30	0.899	No
3410	34.10	1.98	0.81	1.16	0.88	0.720	1.04	0.690	0.98	1.30	0.899	No
3411	34.11	1.98	0.81	1.16	0.88	0.720	1.04	0.690	0.98	1.30	0.899	No
3412	34.12	1.98	0.81	1.16	0.88	0.719	1.04	0.690	0.98	1.30	0.899	No
3413	34.13	1.98	0.82	1.16	0.88	0.719	1.04	0.690	0.98	1.30	0.899	No
3414	34.14	1.98	0.82	1.16	0.88	0.719	1.04	0.690	0.98	1.30	0.899	No
3415	34.15	1.98	0.82	1.16	0.88	0.719	1.04	0.690	0.98	1.30	0.899	No
3416	34.16	1.98	0.82	1.16	0.88	0.719	1.04	0.690	0.98	1.30	0.899	No
3417	34.17	1.98	0.82	1.16	0.88	0.719	1.04	0.690	0.98	1.30	0.899	No
3418	34.18	1.98	0.82	1.16	0.88	0.719	1.04	0.690	0.98	1.30	0.899	No
3419	34.19	1.98	0.82	1.16	0.88	0.719	1.04	0.690	0.98	1.30	0.899	No
3420	34.20	1.98	0.82	1.16	0.88	0.719	1.04	0.689	0.98	1.30	0.899	No
3421	34.21	1.98	0.82	1.16	0.88	0.719	1.04	0.689	0.98	1.30	0.899	No
3422	34.22	1.98	0.82	1.16	0.88	0.719	1.04	0.689	0.98	1.30	0.899	No
3423	34.23	1.98	0.82	1.17	0.88	0.719	1.04	0.689	0.98	1.30	0.899	No
3424	34.24	1.98	0.82	1.17	0.88	0.719	1.04	0.689	0.98	1.30	0.899	No
3425	34.25	1.99	0.82	1.17	0.88	0.719	1.04	0.689	0.98	1.30	0.899	No
3426	34.26	1.99	0.82	1.17	0.88	0.719	1.04	0.689	0.98	1.30	0.899	No
3427	34.27	1.99	0.82	1.17	0.88	0.719	1.04	0.689	0.98	1.30	0.899	No
3428	34.28	1.99	0.82	1.17	0.88	0.719	1.04	0.689	0.98	1.30	0.900	No
3429	34.29	1.99	0.82	1.17	0.88	0.719	1.04	0.689	0.98	1.30	0.900	No
3430	34.30	1.99	0.82	1.17	0.88	0.719	1.04	0.689	0.98	1.30	0.900	No
3431	34.31	1.99	0.82	1.17	0.88	0.719	1.04	0.689	0.98	1.30	0.900	No
3432	34.32	1.99	0.82	1.17	0.88	0.719	1.04	0.689	0.98	1.30	0.900	No
3433	34.33	1.99	0.82	1.17	0.88	0.719	1.04	0.689	0.98	1.30	0.900	No
3434	34.34	1.99	0.82	1.17	0.88	0.719	1.04	0.689	0.97	1.30	0.901	No
3435	34.35	1.99	0.82	1.17	0.88	0.719	1.04	0.689	0.97	1.30	0.901	No
3436	34.36	1.99	0.82	1.17	0.88	0.719	1.04	0.689	0.97	1.30	0.901	No
3437	34.37	1.99	0.82	1.17	0.88	0.719	1.04	0.689	0.97	1.30	0.901	No
3438	34.38	1.99	0.82	1.17	0.88	0.719	1.04	0.689	0.97	1.30	0.902	No
3439	34.39	1.99	0.82	1.17	0.88	0.719	1.04	0.689	0.97	1.30	0.902	No
3440	34.40	1.99	0.82	1.17	0.88	0.719	1.04	0.689	0.97	1.30	0.902	No
3441	34.41	2.00	0.82	1.17	0.88	0.719	1.04	0.689	0.97	1.30	0.902	No
3442	34.42	2.00	0.82	1.17	0.88	0.719	1.04	0.689	0.97	1.30	0.902	No
3443	34.43	2.00	0.82	1.17	0.88	0.719	1.04	0.689	0.97	1.30	0.903	No
3444	34.44	2.00	0.82	1.17	0.88	0.719	1.04	0.689	0.97	1.30	0.903	No
3445	34.45	2.00	0.83	1.17	0.88	0.719	1.04	0.689	0.97	1.30	0.903	No
3446	34.46	2.00	0.83	1.17	0.88	0.719	1.04	0.689	0.97	1.30	0.904	No
3447	34.47	2.00	0.83	1.17	0.88	0.719	1.04	0.689	0.97	1.30	0.904	No
3448	34.48	2.00	0.83	1.17	0.88	0.719	1.04	0.689	0.97	1.30	0.904	No
3449	34.49	2.00	0.83	1.17	0.88	0.719	1.04	0.689	0.97	1.30	0.905	No
3450	34.50	2.00	0.83	1.17	0.88	0.719	1.04	0.689	0.97	1.30	0.905	No
3451	34.51	2.00	0.83	1.18	0.88	0.719	1.04	0.689	0.97	1.30	0.905	No
3452	34.52	2.00	0.83	1.18	0.88	0.719	1.04	0.689	0.97	1.30	0.906	No
3453	34.53	2.00	0.83	1.18	0.88	0.719	1.04	0.689	0.97	1.30	0.906	No
3454	34.54	2.00	0.83	1.18	0.88	0.719	1.04	0.689	0.97	1.30	0.906	No
3455	34.55	2.01	0.83	1.18	0.88	0.719	1.04	0.689	0.97	1.30	0.906	No
3456	34.56	2.01	0.83	1.18	0.88	0.719	1.04	0.689	0.97	1.30	0.906	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
3457	34.57	2.01	0.83	1.18	0.88	0.719	1.04	0.689	0.97	1.30	0.907	No
3458	34.58	2.01	0.83	1.18	0.88	0.719	1.04	0.689	0.97	1.30	0.907	No
3459	34.59	2.01	0.83	1.18	0.88	0.719	1.04	0.689	0.97	1.30	0.907	No
3460	34.60	2.01	0.83	1.18	0.88	0.719	1.04	0.689	0.97	1.30	0.907	No
3461	34.61	2.01	0.83	1.18	0.88	0.719	1.04	0.689	0.97	1.30	0.907	No
3462	34.62	2.01	0.83	1.18	0.88	0.719	1.04	0.689	0.97	1.30	0.907	No
3463	34.63	2.01	0.83	1.18	0.88	0.719	1.04	0.689	0.97	1.30	0.907	No
3464	34.64	2.01	0.83	1.18	0.88	0.719	1.04	0.689	0.97	1.30	0.907	No
3465	34.65	2.01	0.83	1.18	0.88	0.719	1.04	0.689	0.97	1.30	0.907	No
3466	34.66	2.01	0.83	1.18	0.88	0.719	1.04	0.689	0.97	1.30	0.907	No
3467	34.67	2.01	0.83	1.18	0.88	0.719	1.04	0.689	0.97	1.30	0.907	No
3468	34.68	2.01	0.83	1.18	0.88	0.719	1.04	0.689	0.97	1.30	0.907	No
3469	34.69	2.01	0.83	1.18	0.88	0.719	1.04	0.689	0.97	1.30	0.907	No
3470	34.70	2.02	0.83	1.18	0.88	0.719	1.04	0.689	0.97	1.30	0.907	No
3471	34.71	2.02	0.83	1.18	0.88	0.719	1.04	0.689	0.97	1.30	0.907	No
3472	34.72	2.02	0.83	1.18	0.88	0.718	1.04	0.689	0.97	1.30	0.907	No
3473	34.73	2.02	0.83	1.18	0.88	0.718	1.04	0.689	0.97	1.30	0.908	No
3474	34.74	2.02	0.83	1.18	0.88	0.718	1.04	0.689	0.97	1.30	0.908	No
3475	34.75	2.02	0.83	1.18	0.88	0.718	1.04	0.689	0.97	1.30	0.908	No
3476	34.76	2.02	0.83	1.18	0.88	0.718	1.04	0.689	0.97	1.30	0.908	No
3477	34.77	2.02	0.84	1.18	0.88	0.718	1.04	0.689	0.97	1.30	0.908	No
3478	34.78	2.02	0.84	1.18	0.88	0.718	1.04	0.689	0.97	1.30	0.908	No
3479	34.79	2.02	0.84	1.19	0.88	0.718	1.04	0.689	0.97	1.30	0.908	No
3480	34.80	2.02	0.84	1.19	0.88	0.718	1.04	0.689	0.97	1.30	0.908	No
3481	34.81	2.02	0.84	1.19	0.88	0.718	1.04	0.689	0.97	1.30	0.908	No
3482	34.82	2.02	0.84	1.19	0.88	0.718	1.04	0.688	0.97	1.30	0.908	No
3483	34.83	2.02	0.84	1.19	0.88	0.718	1.04	0.688	0.97	1.30	0.908	No
3484	34.84	2.02	0.84	1.19	0.88	0.718	1.04	0.688	0.97	1.30	0.908	No
3485	34.85	2.03	0.84	1.19	0.88	0.718	1.04	0.688	0.97	1.30	0.908	No
3486	34.86	2.03	0.84	1.19	0.88	0.718	1.04	0.688	0.97	1.30	0.908	No
3487	34.87	2.03	0.84	1.19	0.88	0.718	1.04	0.688	0.97	1.30	0.908	No
3488	34.88	2.03	0.84	1.19	0.88	0.718	1.04	0.688	0.97	1.30	0.908	No
3489	34.89	2.03	0.84	1.19	0.88	0.718	1.04	0.688	0.97	1.30	0.909	No
3490	34.90	2.03	0.84	1.19	0.88	0.718	1.04	0.688	0.96	1.30	0.909	No
3491	34.91	2.03	0.84	1.19	0.88	0.718	1.04	0.688	0.96	1.30	0.909	No
3492	34.92	2.03	0.84	1.19	0.88	0.718	1.04	0.688	0.96	1.30	0.909	No
3493	34.93	2.03	0.84	1.19	0.88	0.718	1.04	0.688	0.96	1.30	0.909	No
3494	34.94	2.03	0.84	1.19	0.88	0.718	1.04	0.688	0.96	1.30	0.909	No
3495	34.95	2.03	0.84	1.19	0.88	0.718	1.04	0.688	0.96	1.30	0.909	No
3496	34.96	2.03	0.84	1.19	0.88	0.718	1.04	0.688	0.96	1.30	0.909	No
3497	34.97	2.03	0.84	1.19	0.87	0.718	1.04	0.688	0.96	1.30	0.909	No
3498	34.98	2.03	0.84	1.19	0.87	0.718	1.04	0.688	0.96	1.30	0.909	No
3499	34.99	2.03	0.84	1.19	0.87	0.718	1.04	0.688	0.96	1.30	0.909	No
3500	35.00	2.04	0.84	1.19	0.87	0.718	1.04	0.688	0.96	1.30	0.909	No
3501	35.01	2.04	0.84	1.19	0.87	0.718	1.04	0.688	0.96	1.30	0.909	No
3502	35.02	2.04	0.84	1.19	0.87	0.718	1.04	0.688	0.96	1.30	0.909	No
3503	35.03	2.04	0.84	1.19	0.87	0.718	1.04	0.688	0.96	1.30	0.909	No
3504	35.04	2.04	0.84	1.19	0.87	0.718	1.04	0.688	0.96	1.30	0.909	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
3505	35.05	2.04	0.84	1.19	0.87	0.718	1.04	0.688	0.96	1.30	0.910	No
3506	35.06	2.04	0.84	1.19	0.87	0.718	1.04	0.688	0.96	1.30	0.910	No
3507	35.07	2.04	0.84	1.20	0.87	0.718	1.04	0.688	0.96	1.30	0.909	No
3508	35.08	2.04	0.84	1.20	0.87	0.718	1.04	0.688	0.96	1.30	0.909	No
3509	35.09	2.04	0.85	1.20	0.87	0.718	1.04	0.688	0.96	1.30	0.908	No
3510	35.10	2.04	0.85	1.20	0.87	0.718	1.04	0.688	0.97	1.30	0.908	No
3511	35.11	2.04	0.85	1.20	0.87	0.718	1.04	0.688	0.97	1.30	0.908	No
3512	35.12	2.04	0.85	1.20	0.87	0.718	1.04	0.688	0.97	1.30	0.907	No
3513	35.13	2.04	0.85	1.20	0.87	0.718	1.04	0.688	0.97	1.30	0.907	No
3514	35.14	2.04	0.85	1.20	0.87	0.718	1.04	0.688	0.97	1.30	0.907	No
3515	35.15	2.04	0.85	1.20	0.87	0.718	1.04	0.688	0.97	1.30	0.907	No
3516	35.16	2.05	0.85	1.20	0.87	0.718	1.04	0.688	0.97	1.30	0.906	No
3517	35.17	2.05	0.85	1.20	0.87	0.718	1.04	0.688	0.97	1.30	0.906	No
3518	35.18	2.05	0.85	1.20	0.87	0.718	1.04	0.688	0.97	1.30	0.905	No
3519	35.19	2.05	0.85	1.20	0.87	0.718	1.04	0.688	0.97	1.30	0.905	No
3520	35.20	2.05	0.85	1.20	0.87	0.718	1.04	0.688	0.97	1.30	0.905	No
3521	35.21	2.05	0.85	1.20	0.87	0.718	1.04	0.688	0.97	1.30	0.905	No
3522	35.22	2.05	0.85	1.20	0.87	0.718	1.04	0.688	0.97	1.30	0.905	No
3523	35.23	2.05	0.85	1.20	0.87	0.718	1.04	0.688	0.97	1.30	0.904	No
3524	35.24	2.05	0.85	1.20	0.87	0.718	1.04	0.688	0.97	1.30	0.904	No
3525	35.25	2.05	0.85	1.20	0.87	0.718	1.04	0.688	0.97	1.30	0.904	No
3526	35.26	2.05	0.85	1.20	0.87	0.718	1.04	0.688	0.97	1.30	0.903	No
3527	35.27	2.05	0.85	1.20	0.87	0.718	1.04	0.688	0.97	1.30	0.903	No
3528	35.28	2.05	0.85	1.20	0.87	0.718	1.04	0.688	0.97	1.30	0.903	No
3529	35.29	2.05	0.85	1.20	0.87	0.718	1.04	0.688	0.97	1.30	0.902	No
3530	35.30	2.05	0.85	1.20	0.87	0.718	1.04	0.688	0.97	1.30	0.902	No
3531	35.31	2.06	0.85	1.20	0.87	0.718	1.04	0.688	0.97	1.30	0.903	No
3532	35.32	2.06	0.85	1.20	0.87	0.718	1.04	0.688	0.97	1.30	0.903	No
3533	35.33	2.06	0.85	1.20	0.87	0.718	1.04	0.688	0.97	1.30	0.904	No
3534	35.34	2.06	0.85	1.20	0.87	0.718	1.04	0.688	0.97	1.30	0.905	No
3535	35.35	2.06	0.85	1.20	0.87	0.718	1.04	0.688	0.97	1.30	0.906	No
3536	35.36	2.06	0.85	1.20	0.87	0.717	1.04	0.688	0.97	1.30	0.906	No
3537	35.37	2.06	0.85	1.21	0.87	0.717	1.04	0.688	0.97	1.30	0.907	No
3538	35.38	2.06	0.85	1.21	0.87	0.717	1.04	0.688	0.97	1.30	0.907	No
3539	35.39	2.06	0.85	1.21	0.87	0.717	1.04	0.688	0.97	1.30	0.908	No
3540	35.40	2.06	0.85	1.21	0.87	0.717	1.04	0.688	0.97	1.30	0.909	No
3541	35.41	2.06	0.86	1.21	0.87	0.717	1.04	0.688	0.97	1.30	0.910	No
3542	35.42	2.06	0.86	1.21	0.87	0.717	1.04	0.688	0.97	1.30	0.910	No
3543	35.43	2.06	0.86	1.21	0.87	0.717	1.04	0.688	0.97	1.30	0.911	No
3544	35.44	2.06	0.86	1.21	0.87	0.717	1.04	0.688	0.98	1.30	0.912	No
3545	35.45	2.06	0.86	1.21	0.87	0.717	1.04	0.688	0.98	1.30	0.912	No
3546	35.46	2.07	0.86	1.21	0.87	0.717	1.04	0.688	0.98	1.30	0.913	No
3547	35.47	2.07	0.86	1.21	0.87	0.717	1.04	0.688	0.98	1.30	0.913	No
3548	35.48	2.07	0.86	1.21	0.87	0.717	1.04	0.688	0.98	1.30	0.914	No
3549	35.49	2.07	0.86	1.21	0.87	0.717	1.04	0.688	0.98	1.30	0.914	No
3550	35.50	2.07	0.86	1.21	0.87	0.717	1.04	0.688	0.98	1.30	0.915	No
3551	35.51	2.07	0.86	1.21	0.87	0.717	1.04	0.688	0.98	1.30	0.915	No
3552	35.52	2.07	0.86	1.21	0.87	0.717	1.04	0.688	0.98	1.30	0.916	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
3553	35.53	2.07	0.86	1.21	0.87	0.717	1.04	0.687	0.98	1.30	0.916	No
3554	35.54	2.07	0.86	1.21	0.87	0.717	1.04	0.687	0.98	1.30	0.916	No
3555	35.55	2.07	0.86	1.21	0.87	0.717	1.04	0.687	0.98	1.30	0.917	No
3556	35.56	2.07	0.86	1.21	0.87	0.717	1.04	0.687	0.98	1.30	0.917	No
3557	35.57	2.07	0.86	1.21	0.87	0.717	1.04	0.687	0.98	1.30	0.917	No
3558	35.58	2.07	0.86	1.21	0.87	0.717	1.04	0.687	0.98	1.30	0.917	No
3559	35.59	2.07	0.86	1.21	0.87	0.717	1.04	0.687	0.98	1.30	0.918	No
3560	35.60	2.07	0.86	1.21	0.87	0.717	1.04	0.687	0.98	1.30	0.918	No
3561	35.61	2.07	0.86	1.21	0.87	0.717	1.04	0.687	0.98	1.30	0.918	No
3562	35.62	2.08	0.86	1.21	0.87	0.717	1.04	0.687	0.98	1.30	0.918	No
3563	35.63	2.08	0.86	1.21	0.87	0.717	1.04	0.687	0.98	1.30	0.918	No
3564	35.64	2.08	0.86	1.21	0.87	0.717	1.04	0.687	0.98	1.30	0.918	No
3565	35.65	2.08	0.86	1.21	0.87	0.717	1.04	0.687	0.98	1.30	0.919	No
3566	35.66	2.08	0.86	1.21	0.87	0.717	1.04	0.687	0.98	1.30	0.919	No
3567	35.67	2.08	0.86	1.22	0.87	0.717	1.04	0.687	0.98	1.30	0.919	No
3568	35.68	2.08	0.86	1.22	0.87	0.717	1.04	0.687	0.98	1.30	0.919	No
3569	35.69	2.08	0.86	1.22	0.87	0.717	1.04	0.687	0.98	1.30	0.919	No
3570	35.70	2.08	0.86	1.22	0.87	0.717	1.04	0.687	0.98	1.30	0.919	No
3571	35.71	2.08	0.86	1.22	0.87	0.717	1.04	0.687	0.98	1.30	0.919	No
3572	35.72	2.08	0.86	1.22	0.87	0.717	1.04	0.687	0.98	1.30	0.919	No
3573	35.73	2.08	0.87	1.22	0.87	0.717	1.04	0.687	0.98	1.30	0.919	No
3574	35.74	2.08	0.87	1.22	0.87	0.717	1.04	0.687	0.98	1.30	0.919	No
3575	35.75	2.08	0.87	1.22	0.87	0.717	1.04	0.687	0.98	1.30	0.919	No
3576	35.76	2.08	0.87	1.22	0.87	0.717	1.04	0.687	0.98	1.30	0.920	No
3577	35.77	2.08	0.87	1.22	0.87	0.717	1.04	0.687	0.98	1.30	0.920	No
3578	35.78	2.09	0.87	1.22	0.87	0.717	1.04	0.687	0.98	1.30	0.920	No
3579	35.79	2.09	0.87	1.22	0.87	0.717	1.04	0.687	0.98	1.30	0.920	No
3580	35.80	2.09	0.87	1.22	0.87	0.717	1.04	0.687	0.98	1.30	0.920	No
3581	35.81	2.09	0.87	1.22	0.87	0.717	1.04	0.687	0.98	1.30	0.920	No
3582	35.82	2.09	0.87	1.22	0.87	0.717	1.04	0.687	0.98	1.30	0.920	No
3583	35.83	2.09	0.87	1.22	0.87	0.717	1.04	0.687	0.98	1.30	0.920	No
3584	35.84	2.09	0.87	1.22	0.87	0.717	1.04	0.687	0.98	1.30	0.920	No
3585	35.85	2.09	0.87	1.22	0.87	0.717	1.04	0.687	0.98	1.30	0.920	No
3586	35.86	2.09	0.87	1.22	0.87	0.717	1.04	0.687	0.98	1.30	0.920	No
3587	35.87	2.09	0.87	1.22	0.87	0.717	1.04	0.687	0.98	1.30	0.920	No
3588	35.88	2.09	0.87	1.22	0.87	0.717	1.04	0.687	0.98	1.30	0.920	No
3589	35.89	2.09	0.87	1.22	0.87	0.717	1.04	0.687	0.98	1.30	0.920	No
3590	35.90	2.09	0.87	1.22	0.87	0.717	1.04	0.687	0.98	1.30	0.920	No
3591	35.91	2.09	0.87	1.22	0.87	0.717	1.04	0.687	0.98	1.30	0.920	No
3592	35.92	2.09	0.87	1.22	0.87	0.717	1.04	0.687	0.98	1.30	0.920	No
3593	35.93	2.09	0.87	1.22	0.87	0.717	1.04	0.687	0.98	1.30	0.920	No
3594	35.94	2.10	0.87	1.22	0.87	0.717	1.04	0.687	0.98	1.30	0.920	No
3595	35.95	2.10	0.87	1.22	0.87	0.717	1.04	0.687	0.98	1.30	0.919	No
3596	35.96	2.10	0.87	1.22	0.87	0.717	1.04	0.687	0.98	1.30	0.919	No
3597	35.97	2.10	0.87	1.22	0.87	0.717	1.04	0.687	0.98	1.30	0.919	No
3598	35.98	2.10	0.87	1.23	0.87	0.717	1.04	0.687	0.98	1.30	0.919	No
3599	35.99	2.10	0.87	1.23	0.87	0.717	1.04	0.687	0.98	1.30	0.919	No
3600	36.00	2.10	0.87	1.23	0.87	0.717	1.04	0.687	0.98	1.30	0.919	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
3601	36.01	2.10	0.87	1.23	0.87	0.717	1.04	0.687	0.98	1.30	0.919	No
3602	36.02	2.10	0.87	1.23	0.87	0.717	1.04	0.687	0.98	1.30	0.919	No
3603	36.03	2.10	0.87	1.23	0.87	0.717	1.04	0.687	0.98	1.30	0.919	No
3604	36.04	2.10	0.87	1.23	0.87	0.717	1.04	0.687	0.98	1.30	0.919	No
3605	36.05	2.10	0.88	1.23	0.87	0.717	1.04	0.687	0.98	1.30	0.919	No
3606	36.06	2.10	0.88	1.23	0.87	0.717	1.04	0.687	0.98	1.30	0.919	No
3607	36.07	2.10	0.88	1.23	0.87	0.717	1.04	0.687	0.98	1.30	0.919	No
3608	36.08	2.10	0.88	1.23	0.87	0.717	1.04	0.687	0.98	1.30	0.919	No
3609	36.09	2.11	0.88	1.23	0.87	0.717	1.04	0.687	0.98	1.30	0.919	No
3610	36.10	2.11	0.88	1.23	0.87	0.717	1.04	0.687	0.98	1.30	0.919	No
3611	36.11	2.11	0.88	1.23	0.87	0.717	1.04	0.687	0.98	1.30	0.919	No
3612	36.12	2.11	0.88	1.23	0.87	0.717	1.04	0.687	0.97	1.30	0.920	No
3613	36.13	2.11	0.88	1.23	0.87	0.717	1.04	0.687	0.97	1.30	0.920	No
3614	36.14	2.11	0.88	1.23	0.87	0.717	1.04	0.687	0.97	1.30	0.920	No
3615	36.15	2.11	0.88	1.23	0.87	0.717	1.04	0.687	0.97	1.30	0.920	No
3616	36.16	2.11	0.88	1.23	0.87	0.717	1.04	0.687	0.97	1.30	0.920	No
3617	36.17	2.11	0.88	1.23	0.87	0.717	1.04	0.687	0.97	1.30	0.920	No
3618	36.18	2.11	0.88	1.23	0.87	0.717	1.04	0.687	0.97	1.30	0.920	No
3619	36.19	2.11	0.88	1.23	0.87	0.717	1.04	0.687	0.97	1.30	0.920	No
3620	36.20	2.11	0.88	1.23	0.87	0.717	1.04	0.687	0.97	1.30	0.920	No
3621	36.21	2.11	0.88	1.23	0.87	0.717	1.04	0.687	0.97	1.30	0.920	No
3622	36.22	2.11	0.88	1.23	0.87	0.717	1.04	0.687	0.97	1.30	0.920	No
3623	36.23	2.11	0.88	1.23	0.87	0.717	1.04	0.687	0.97	1.30	0.920	No
3624	36.24	2.11	0.88	1.23	0.87	0.716	1.04	0.687	0.97	1.30	0.920	No
3625	36.25	2.12	0.88	1.23	0.87	0.716	1.04	0.687	0.97	1.30	0.920	No
3626	36.26	2.12	0.88	1.23	0.87	0.716	1.04	0.687	0.97	1.30	0.920	No
3627	36.27	2.12	0.88	1.23	0.87	0.716	1.04	0.687	0.97	1.30	0.920	No
3628	36.28	2.12	0.88	1.23	0.87	0.716	1.04	0.687	0.97	1.30	0.920	No
3629	36.29	2.12	0.88	1.24	0.87	0.716	1.04	0.687	0.97	1.30	0.920	No
3630	36.30	2.12	0.88	1.24	0.87	0.716	1.04	0.687	0.97	1.30	0.920	No
3631	36.31	2.12	0.88	1.24	0.87	0.716	1.04	0.687	0.97	1.30	0.920	No
3632	36.32	2.12	0.88	1.24	0.87	0.716	1.04	0.687	0.97	1.30	0.920	No
3633	36.33	2.12	0.88	1.24	0.87	0.716	1.04	0.687	0.97	1.30	0.920	No
3634	36.34	2.12	0.88	1.24	0.87	0.716	1.04	0.687	0.97	1.30	0.920	No
3635	36.35	2.12	0.88	1.24	0.87	0.716	1.04	0.687	0.97	1.30	0.920	No
3636	36.36	2.12	0.88	1.24	0.87	0.716	1.04	0.687	0.97	1.30	0.920	No
3637	36.37	2.12	0.89	1.24	0.87	0.716	1.04	0.687	0.97	1.30	0.919	No
3638	36.38	2.12	0.89	1.24	0.87	0.716	1.04	0.687	0.97	1.30	0.919	No
3639	36.39	2.12	0.89	1.24	0.87	0.716	1.04	0.687	0.97	1.30	0.919	No
3640	36.40	2.12	0.89	1.24	0.87	0.716	1.04	0.687	0.97	1.30	0.919	No
3641	36.41	2.13	0.89	1.24	0.87	0.716	1.04	0.687	0.97	1.30	0.919	No
3642	36.42	2.13	0.89	1.24	0.87	0.716	1.04	0.687	0.97	1.30	0.919	No
3643	36.43	2.13	0.89	1.24	0.87	0.716	1.04	0.687	0.97	1.30	0.919	No
3644	36.44	2.13	0.89	1.24	0.87	0.716	1.04	0.687	0.97	1.30	0.919	No
3645	36.45	2.13	0.89	1.24	0.87	0.716	1.04	0.686	0.97	1.30	0.919	No
3646	36.46	2.13	0.89	1.24	0.87	0.716	1.04	0.686	0.97	1.30	0.919	No
3647	36.47	2.13	0.89	1.24	0.87	0.716	1.04	0.686	0.97	1.30	0.919	No
3648	36.48	2.13	0.89	1.24	0.87	0.716	1.04	0.686	0.97	1.30	0.919	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
3649	36.49	2.13	0.89	1.24	0.87	0.716	1.04	0.686	0.97	1.30	0.919	No
3650	36.50	2.13	0.89	1.24	0.87	0.716	1.04	0.686	0.97	1.30	0.919	No
3651	36.51	2.13	0.89	1.24	0.87	0.716	1.04	0.686	0.97	1.30	0.919	No
3652	36.52	2.13	0.89	1.24	0.87	0.716	1.04	0.686	0.97	1.30	0.919	No
3653	36.53	2.13	0.89	1.24	0.87	0.716	1.04	0.686	0.97	1.30	0.919	No
3654	36.54	2.13	0.89	1.24	0.87	0.716	1.04	0.686	0.97	1.30	0.919	No
3655	36.55	2.13	0.89	1.24	0.87	0.716	1.04	0.686	0.97	1.30	0.919	No
3656	36.56	2.13	0.89	1.24	0.87	0.716	1.04	0.686	0.97	1.30	0.919	No
3657	36.57	2.14	0.89	1.24	0.87	0.716	1.04	0.686	0.97	1.30	0.920	No
3658	36.58	2.14	0.89	1.24	0.87	0.716	1.04	0.686	0.97	1.30	0.920	No
3659	36.59	2.14	0.89	1.24	0.87	0.716	1.04	0.686	0.97	1.30	0.920	No
3660	36.60	2.14	0.89	1.25	0.87	0.716	1.04	0.686	0.97	1.30	0.920	No
3661	36.61	2.14	0.89	1.25	0.87	0.716	1.04	0.686	0.97	1.30	0.920	No
3662	36.62	2.14	0.89	1.25	0.87	0.716	1.04	0.686	0.97	1.30	0.920	No
3663	36.63	2.14	0.89	1.25	0.87	0.716	1.04	0.686	0.97	1.30	0.920	No
3664	36.64	2.14	0.89	1.25	0.87	0.716	1.04	0.686	0.97	1.30	0.920	No
3665	36.65	2.14	0.89	1.25	0.87	0.716	1.04	0.686	0.97	1.30	0.920	No
3666	36.66	2.14	0.89	1.25	0.87	0.716	1.04	0.686	0.97	1.30	0.920	No
3667	36.67	2.14	0.89	1.25	0.87	0.716	1.04	0.686	0.97	1.30	0.920	No
3668	36.68	2.14	0.89	1.25	0.87	0.716	1.04	0.686	0.97	1.30	0.920	No
3669	36.69	2.14	0.90	1.25	0.87	0.716	1.04	0.686	0.97	1.30	0.920	No
3670	36.70	2.14	0.90	1.25	0.87	0.716	1.04	0.686	0.97	1.30	0.920	No
3671	36.71	2.14	0.90	1.25	0.87	0.716	1.04	0.686	0.97	1.30	0.920	No
3672	36.72	2.15	0.90	1.25	0.87	0.716	1.04	0.686	0.97	1.30	0.920	No
3673	36.73	2.15	0.90	1.25	0.87	0.716	1.04	0.686	0.97	1.30	0.920	No
3674	36.74	2.15	0.90	1.25	0.87	0.716	1.04	0.686	0.97	1.30	0.920	No
3675	36.75	2.15	0.90	1.25	0.87	0.716	1.04	0.686	0.97	1.30	0.920	No
3676	36.76	2.15	0.90	1.25	0.87	0.716	1.04	0.686	0.97	1.30	0.920	No
3677	36.77	2.15	0.90	1.25	0.87	0.716	1.04	0.686	0.97	1.30	0.920	No
3678	36.78	2.15	0.90	1.25	0.87	0.716	1.04	0.686	0.97	1.30	0.920	No
3679	36.79	2.15	0.90	1.25	0.87	0.716	1.04	0.686	0.97	1.30	0.920	No
3680	36.80	2.15	0.90	1.25	0.87	0.716	1.04	0.686	0.97	1.30	0.920	No
3681	36.81	2.15	0.90	1.25	0.87	0.716	1.04	0.686	0.97	1.30	0.920	No
3682	36.82	2.15	0.90	1.25	0.87	0.716	1.04	0.686	0.97	1.30	0.920	No
3683	36.83	2.15	0.90	1.25	0.87	0.716	1.04	0.686	0.97	1.30	0.920	No
3684	36.84	2.15	0.90	1.25	0.87	0.716	1.04	0.686	0.97	1.30	0.920	No
3685	36.85	2.15	0.90	1.25	0.87	0.716	1.04	0.686	0.97	1.30	0.920	No
3686	36.86	2.15	0.90	1.25	0.87	0.716	1.04	0.686	0.97	1.30	0.920	No
3687	36.87	2.15	0.90	1.25	0.87	0.716	1.04	0.686	0.97	1.30	0.920	No
3688	36.88	2.16	0.90	1.25	0.87	0.716	1.04	0.686	0.97	1.30	0.920	No
3689	36.89	2.16	0.90	1.25	0.87	0.716	1.04	0.686	0.97	1.30	0.921	No
3690	36.90	2.16	0.90	1.26	0.87	0.716	1.04	0.686	0.97	1.30	0.921	No
3691	36.91	2.16	0.90	1.26	0.87	0.716	1.04	0.686	0.97	1.30	0.921	No
3692	36.92	2.16	0.90	1.26	0.87	0.716	1.04	0.686	0.97	1.30	0.921	No
3693	36.93	2.16	0.90	1.26	0.87	0.716	1.04	0.686	0.97	1.30	0.921	No
3694	36.94	2.16	0.90	1.26	0.87	0.716	1.04	0.686	0.97	1.30	0.921	No
3695	36.95	2.16	0.90	1.26	0.87	0.716	1.04	0.686	0.97	1.30	0.921	No
3696	36.96	2.16	0.90	1.26	0.87	0.715	1.04	0.686	0.97	1.30	0.921	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
3697	36.97	2.16	0.90	1.26	0.87	0.715	1.04	0.686	0.97	1.30	0.921	No
3698	36.98	2.16	0.90	1.26	0.87	0.715	1.04	0.686	0.97	1.30	0.921	No
3699	36.99	2.16	0.90	1.26	0.87	0.715	1.04	0.686	0.97	1.30	0.921	No
3700	37.00	2.16	0.90	1.26	0.87	0.715	1.04	0.686	0.97	1.30	0.922	No
3701	37.01	2.16	0.91	1.26	0.87	0.715	1.04	0.686	0.97	1.30	0.922	No
3702	37.02	2.16	0.91	1.26	0.87	0.715	1.04	0.686	0.97	1.30	0.922	No
3703	37.03	2.17	0.91	1.26	0.87	0.715	1.04	0.686	0.97	1.30	0.922	No
3704	37.04	2.17	0.91	1.26	0.87	0.715	1.04	0.686	0.97	1.30	0.922	No
3705	37.05	2.17	0.91	1.26	0.87	0.715	1.04	0.686	0.97	1.30	0.922	No
3706	37.06	2.17	0.91	1.26	0.86	0.715	1.04	0.686	0.97	1.30	0.922	No
3707	37.07	2.17	0.91	1.26	0.86	0.715	1.04	0.686	0.97	1.30	0.922	No
3708	37.08	2.17	0.91	1.26	0.86	0.715	1.04	0.686	0.97	1.30	0.922	No
3709	37.09	2.17	0.91	1.26	0.86	0.715	1.04	0.686	0.97	1.30	0.922	No
3710	37.10	2.17	0.91	1.26	0.86	0.715	1.04	0.686	0.97	1.30	0.922	No
3711	37.11	2.17	0.91	1.26	0.86	0.715	1.04	0.686	0.97	1.30	0.922	No
3712	37.12	2.17	0.91	1.26	0.86	0.715	1.04	0.686	0.97	1.30	0.922	No
3713	37.13	2.17	0.91	1.26	0.86	0.715	1.04	0.686	0.97	1.30	0.922	No
3714	37.14	2.17	0.91	1.26	0.86	0.715	1.04	0.686	0.97	1.30	0.923	No
3715	37.15	2.17	0.91	1.26	0.86	0.715	1.04	0.685	0.97	1.30	0.923	No
3716	37.16	2.17	0.91	1.26	0.86	0.715	1.04	0.685	0.97	1.30	0.923	No
3717	37.17	2.17	0.91	1.26	0.86	0.715	1.04	0.685	0.97	1.30	0.923	No
3718	37.18	2.17	0.91	1.26	0.86	0.715	1.04	0.685	0.97	1.30	0.923	No
3719	37.19	2.18	0.91	1.26	0.86	0.715	1.04	0.685	0.97	1.30	0.923	No
3720	37.20	2.18	0.91	1.26	0.86	0.715	1.04	0.685	0.97	1.30	0.923	No
3721	37.21	2.18	0.91	1.27	0.86	0.715	1.04	0.685	0.97	1.30	0.923	No
3722	37.22	2.18	0.91	1.27	0.86	0.715	1.04	0.685	0.97	1.30	0.923	No
3723	37.23	2.18	0.91	1.27	0.86	0.715	1.04	0.685	0.97	1.30	0.923	No
3724	37.24	2.18	0.91	1.27	0.86	0.715	1.04	0.685	0.97	1.30	0.923	No
3725	37.25	2.18	0.91	1.27	0.86	0.715	1.04	0.685	0.97	1.30	0.923	No
3726	37.26	2.18	0.91	1.27	0.86	0.715	1.04	0.685	0.97	1.30	0.923	No
3727	37.27	2.18	0.91	1.27	0.86	0.715	1.04	0.685	0.97	1.30	0.923	No
3728	37.28	2.18	0.91	1.27	0.86	0.715	1.04	0.685	0.97	1.30	0.923	No
3729	37.29	2.18	0.91	1.27	0.86	0.715	1.04	0.685	0.97	1.30	0.923	No
3730	37.30	2.18	0.91	1.27	0.86	0.715	1.04	0.685	0.97	1.30	0.923	No
3731	37.31	2.18	0.91	1.27	0.86	0.715	1.04	0.685	0.97	1.30	0.923	No
3732	37.32	2.18	0.91	1.27	0.86	0.715	1.04	0.685	0.97	1.30	0.923	No
3733	37.33	2.18	0.92	1.27	0.86	0.715	1.04	0.685	0.97	1.30	0.923	No
3734	37.34	2.18	0.92	1.27	0.86	0.715	1.04	0.685	0.97	1.30	0.923	No
3735	37.35	2.19	0.92	1.27	0.86	0.715	1.04	0.685	0.97	1.30	0.923	No
3736	37.36	2.19	0.92	1.27	0.86	0.715	1.04	0.685	0.97	1.30	0.923	No
3737	37.37	2.19	0.92	1.27	0.86	0.715	1.04	0.685	0.97	1.30	0.923	No
3738	37.38	2.19	0.92	1.27	0.86	0.715	1.04	0.685	0.97	1.30	0.923	No
3739	37.39	2.19	0.92	1.27	0.86	0.715	1.04	0.685	0.97	1.30	0.923	No
3740	37.40	2.19	0.92	1.27	0.86	0.715	1.04	0.685	0.97	1.30	0.923	No
3741	37.41	2.19	0.92	1.27	0.86	0.715	1.04	0.685	0.97	1.30	0.923	No
3742	37.42	2.19	0.92	1.27	0.86	0.715	1.04	0.685	0.97	1.30	0.924	No
3743	37.43	2.19	0.92	1.27	0.86	0.715	1.04	0.685	0.97	1.30	0.924	No
3744	37.44	2.19	0.92	1.27	0.86	0.715	1.04	0.685	0.97	1.30	0.924	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
3745	37.45	2.19	0.92	1.27	0.86	0.715	1.04	0.685	0.97	1.30	0.924	No
3746	37.46	2.19	0.92	1.27	0.86	0.715	1.04	0.685	0.97	1.30	0.924	No
3747	37.47	2.19	0.92	1.27	0.86	0.715	1.04	0.685	0.97	1.30	0.924	No
3748	37.48	2.19	0.92	1.27	0.86	0.715	1.04	0.685	0.97	1.30	0.924	No
3749	37.49	2.19	0.92	1.27	0.86	0.715	1.04	0.685	0.97	1.30	0.924	No
3750	37.50	2.20	0.92	1.27	0.86	0.715	1.04	0.685	0.97	1.30	0.924	No
3751	37.51	2.20	0.92	1.28	0.86	0.715	1.04	0.685	0.97	1.30	0.924	No
3752	37.52	2.20	0.92	1.28	0.86	0.715	1.04	0.685	0.97	1.30	0.924	No
3753	37.53	2.20	0.92	1.28	0.86	0.715	1.04	0.685	0.97	1.30	0.924	No
3754	37.54	2.20	0.92	1.28	0.86	0.715	1.04	0.685	0.97	1.30	0.924	No
3755	37.55	2.20	0.92	1.28	0.86	0.715	1.04	0.685	0.97	1.30	0.924	No
3756	37.56	2.20	0.92	1.28	0.86	0.715	1.04	0.685	0.97	1.30	0.924	No
3757	37.57	2.20	0.92	1.28	0.86	0.715	1.04	0.685	0.97	1.30	0.924	No
3758	37.58	2.20	0.92	1.28	0.86	0.715	1.04	0.685	0.97	1.30	0.924	No
3759	37.59	2.20	0.92	1.28	0.86	0.715	1.04	0.685	0.97	1.30	0.924	No
3760	37.60	2.20	0.92	1.28	0.86	0.715	1.04	0.685	0.97	1.30	0.924	No
3761	37.61	2.20	0.92	1.28	0.86	0.715	1.04	0.685	0.97	1.30	0.924	No
3762	37.62	2.20	0.92	1.28	0.86	0.714	1.04	0.685	0.97	1.30	0.924	No
3763	37.63	2.20	0.92	1.28	0.86	0.714	1.04	0.685	0.97	1.30	0.924	No
3764	37.64	2.20	0.92	1.28	0.86	0.714	1.04	0.685	0.97	1.30	0.924	No
3765	37.65	2.20	0.93	1.28	0.86	0.714	1.04	0.685	0.97	1.30	0.924	No
3766	37.66	2.21	0.93	1.28	0.86	0.714	1.04	0.685	0.97	1.30	0.924	No
3767	37.67	2.21	0.93	1.28	0.86	0.714	1.04	0.685	0.97	1.30	0.924	No
3768	37.68	2.21	0.93	1.28	0.86	0.714	1.04	0.685	0.97	1.30	0.924	No
3769	37.69	2.21	0.93	1.28	0.86	0.714	1.04	0.685	0.97	1.30	0.924	No
3770	37.70	2.21	0.93	1.28	0.86	0.714	1.04	0.685	0.97	1.30	0.924	No
3771	37.71	2.21	0.93	1.28	0.86	0.714	1.04	0.685	0.97	1.30	2.000	Yes
3772	37.72	2.21	0.93	1.28	0.86	0.714	1.04	0.685	0.97	1.30	2.000	Yes
3773	37.73	2.21	0.93	1.28	0.86	0.714	1.04	0.685	0.97	1.30	2.000	Yes
3774	37.74	2.21	0.93	1.28	0.86	0.714	1.04	0.685	0.97	1.30	2.000	Yes
3775	37.75	2.21	0.93	1.28	0.86	0.714	1.04	0.685	0.97	1.30	2.000	Yes
3776	37.76	2.21	0.93	1.28	0.86	0.714	1.04	0.685	0.97	1.30	2.000	Yes
3777	37.77	2.21	0.93	1.28	0.86	0.714	1.04	0.685	0.97	1.30	2.000	Yes
3778	37.78	2.21	0.93	1.28	0.86	0.714	1.04	0.685	0.97	1.30	2.000	Yes
3779	37.79	2.21	0.93	1.28	0.86	0.714	1.04	0.685	0.97	1.30	2.000	Yes
3780	37.80	2.21	0.93	1.28	0.86	0.714	1.04	0.685	0.97	1.30	2.000	Yes
3781	37.81	2.22	0.93	1.28	0.86	0.714	1.04	0.685	0.97	1.30	2.000	Yes
3782	37.82	2.22	0.93	1.29	0.86	0.714	1.04	0.685	0.97	1.30	2.000	Yes
3783	37.83	2.22	0.93	1.29	0.86	0.714	1.04	0.684	0.97	1.30	2.000	Yes
3784	37.84	2.22	0.93	1.29	0.86	0.714	1.04	0.684	0.97	1.30	2.000	Yes
3785	37.85	2.22	0.93	1.29	0.86	0.714	1.04	0.684	0.97	1.30	2.000	Yes
3786	37.86	2.22	0.93	1.29	0.86	0.714	1.04	0.684	0.97	1.30	2.000	Yes
3787	37.87	2.22	0.93	1.29	0.86	0.714	1.04	0.684	0.97	1.30	2.000	Yes
3788	37.88	2.22	0.93	1.29	0.86	0.714	1.04	0.684	0.97	1.30	2.000	Yes
3789	37.89	2.22	0.93	1.29	0.86	0.714	1.04	0.684	0.97	1.30	2.000	Yes
3790	37.90	2.22	0.93	1.29	0.86	0.714	1.04	0.684	0.97	1.30	2.000	Yes
3791	37.91	2.22	0.93	1.29	0.86	0.714	1.04	0.684	0.97	1.30	2.000	Yes
3792	37.92	2.22	0.93	1.29	0.86	0.714	1.04	0.684	0.97	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
3793	37.93	2.22	0.93	1.29	0.86	0.714	1.04	0.684	0.97	1.30	2.000	Yes
3794	37.94	2.22	0.93	1.29	0.86	0.714	1.04	0.684	0.97	1.30	2.000	Yes
3795	37.95	2.22	0.93	1.29	0.86	0.714	1.04	0.684	0.97	1.30	2.000	Yes
3796	37.96	2.22	0.93	1.29	0.86	0.714	1.04	0.684	0.97	1.30	2.000	Yes
3797	37.97	2.23	0.94	1.29	0.86	0.714	1.04	0.684	0.97	1.30	2.000	Yes
3798	37.98	2.23	0.94	1.29	0.86	0.714	1.04	0.684	0.97	1.30	2.000	Yes
3799	37.99	2.23	0.94	1.29	0.86	0.714	1.04	0.684	0.97	1.30	2.000	Yes
3800	38.00	2.23	0.94	1.29	0.86	0.714	1.04	0.684	0.97	1.30	2.000	Yes
3801	38.01	2.23	0.94	1.29	0.86	0.714	1.04	0.684	0.97	1.30	2.000	Yes
3802	38.02	2.23	0.94	1.29	0.86	0.714	1.04	0.684	0.97	1.30	2.000	Yes
3803	38.03	2.23	0.94	1.29	0.86	0.714	1.04	0.684	0.97	1.30	2.000	Yes
3804	38.04	2.23	0.94	1.29	0.86	0.714	1.04	0.684	0.97	1.30	2.000	Yes
3805	38.05	2.23	0.94	1.29	0.86	0.714	1.04	0.684	0.97	1.30	2.000	Yes
3806	38.06	2.23	0.94	1.29	0.86	0.714	1.04	0.684	0.97	1.30	2.000	Yes
3807	38.07	2.23	0.94	1.29	0.86	0.714	1.04	0.684	0.97	1.30	0.926	No
3808	38.08	2.23	0.94	1.29	0.86	0.714	1.04	0.684	0.97	1.30	0.926	No
3809	38.09	2.23	0.94	1.29	0.86	0.714	1.04	0.684	0.97	1.30	0.926	No
3810	38.10	2.23	0.94	1.29	0.86	0.714	1.04	0.684	0.97	1.30	0.927	No
3811	38.11	2.23	0.94	1.30	0.86	0.714	1.04	0.684	0.97	1.30	0.927	No
3812	38.12	2.24	0.94	1.30	0.86	0.714	1.04	0.684	0.97	1.30	0.927	No
3813	38.13	2.24	0.94	1.30	0.86	0.714	1.04	0.684	0.97	1.30	0.927	No
3814	38.14	2.24	0.94	1.30	0.86	0.714	1.04	0.684	0.97	1.30	0.927	No
3815	38.15	2.24	0.94	1.30	0.86	0.714	1.04	0.684	0.97	1.30	2.000	Yes
3816	38.16	2.24	0.94	1.30	0.86	0.714	1.04	0.684	0.97	1.30	2.000	Yes
3817	38.17	2.24	0.94	1.30	0.86	0.713	1.04	0.684	0.97	1.30	2.000	Yes
3818	38.18	2.24	0.94	1.30	0.86	0.713	1.04	0.684	0.97	1.30	2.000	Yes
3819	38.19	2.24	0.94	1.30	0.86	0.713	1.04	0.684	0.97	1.30	2.000	Yes
3820	38.20	2.24	0.94	1.30	0.86	0.713	1.04	0.684	0.97	1.30	2.000	Yes
3821	38.21	2.24	0.94	1.30	0.86	0.713	1.04	0.684	0.97	1.30	2.000	Yes
3822	38.22	2.24	0.94	1.30	0.86	0.713	1.04	0.684	0.97	1.30	2.000	Yes
3823	38.23	2.24	0.94	1.30	0.86	0.713	1.04	0.684	0.97	1.30	2.000	Yes
3824	38.24	2.24	0.94	1.30	0.86	0.713	1.04	0.684	0.97	1.30	2.000	Yes
3825	38.25	2.24	0.94	1.30	0.86	0.713	1.04	0.684	0.97	1.30	2.000	Yes
3826	38.26	2.24	0.94	1.30	0.86	0.713	1.04	0.684	0.97	1.30	2.000	Yes
3827	38.27	2.25	0.94	1.30	0.86	0.713	1.04	0.684	0.96	1.30	2.000	Yes
3828	38.28	2.25	0.94	1.30	0.86	0.713	1.04	0.684	0.96	1.30	2.000	Yes
3829	38.29	2.25	0.95	1.30	0.86	0.713	1.04	0.684	0.96	1.30	2.000	Yes
3830	38.30	2.25	0.95	1.30	0.86	0.713	1.04	0.684	0.96	1.30	2.000	Yes
3831	38.31	2.25	0.95	1.30	0.86	0.713	1.04	0.684	0.96	1.30	2.000	Yes
3832	38.32	2.25	0.95	1.30	0.86	0.713	1.04	0.684	0.96	1.30	2.000	Yes
3833	38.33	2.25	0.95	1.30	0.86	0.713	1.04	0.684	0.96	1.30	2.000	Yes
3834	38.34	2.25	0.95	1.30	0.86	0.713	1.04	0.684	0.96	1.30	2.000	Yes
3835	38.35	2.25	0.95	1.30	0.86	0.713	1.04	0.684	0.96	1.30	2.000	Yes
3836	38.36	2.25	0.95	1.30	0.86	0.713	1.04	0.683	0.96	1.30	2.000	Yes
3837	38.37	2.25	0.95	1.30	0.86	0.713	1.04	0.683	0.96	1.30	2.000	Yes
3838	38.38	2.25	0.95	1.30	0.86	0.713	1.04	0.683	0.96	1.30	2.000	Yes
3839	38.39	2.25	0.95	1.30	0.86	0.713	1.04	0.683	0.96	1.30	2.000	Yes
3840	38.40	2.25	0.95	1.31	0.86	0.713	1.04	0.683	0.96	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
3841	38.41	2.25	0.95	1.31	0.86	0.713	1.04	0.683	0.95	1.30	2.000	Yes
3842	38.42	2.25	0.95	1.31	0.86	0.713	1.04	0.683	0.95	1.30	2.000	Yes
3843	38.43	2.26	0.95	1.31	0.86	0.713	1.04	0.683	0.95	1.30	2.000	Yes
3844	38.44	2.26	0.95	1.31	0.86	0.713	1.04	0.683	0.95	1.30	2.000	Yes
3845	38.45	2.26	0.95	1.31	0.86	0.713	1.04	0.683	0.95	1.30	2.000	Yes
3846	38.46	2.26	0.95	1.31	0.86	0.713	1.04	0.683	0.95	1.30	2.000	Yes
3847	38.47	2.26	0.95	1.31	0.86	0.713	1.04	0.683	0.95	1.30	2.000	Yes
3848	38.48	2.26	0.95	1.31	0.86	0.713	1.04	0.683	0.95	1.30	0.917	No
3849	38.49	2.26	0.95	1.31	0.86	0.713	1.04	0.683	0.95	1.30	0.917	No
3850	38.50	2.26	0.95	1.31	0.86	0.713	1.04	0.683	0.95	1.30	0.917	No
3851	38.51	2.26	0.95	1.31	0.86	0.713	1.04	0.683	0.95	1.30	0.918	No
3852	38.52	2.26	0.95	1.31	0.86	0.713	1.04	0.683	0.95	1.30	0.918	No
3853	38.53	2.26	0.95	1.31	0.86	0.713	1.04	0.683	0.95	1.30	0.918	No
3854	38.54	2.26	0.95	1.31	0.86	0.713	1.04	0.683	0.95	1.30	0.918	No
3855	38.55	2.26	0.95	1.31	0.86	0.713	1.04	0.683	0.95	1.30	0.919	No
3856	38.56	2.26	0.95	1.31	0.86	0.713	1.04	0.683	0.95	1.30	0.919	No
3857	38.57	2.26	0.95	1.31	0.86	0.713	1.04	0.683	0.95	1.30	0.919	No
3858	38.58	2.27	0.95	1.31	0.86	0.713	1.04	0.683	0.95	1.30	0.919	No
3859	38.59	2.27	0.95	1.31	0.86	0.713	1.04	0.683	0.95	1.30	0.919	No
3860	38.60	2.27	0.95	1.31	0.86	0.713	1.04	0.683	0.95	1.30	0.918	No
3861	38.61	2.27	0.96	1.31	0.86	0.713	1.04	0.683	0.95	1.30	0.918	No
3862	38.62	2.27	0.96	1.31	0.86	0.713	1.04	0.683	0.95	1.30	0.918	No
3863	38.63	2.27	0.96	1.31	0.86	0.712	1.04	0.683	0.95	1.30	0.917	No
3864	38.64	2.27	0.96	1.31	0.86	0.712	1.04	0.683	0.95	1.30	0.917	No
3865	38.65	2.27	0.96	1.31	0.86	0.712	1.04	0.683	0.95	1.30	0.917	No
3866	38.66	2.27	0.96	1.31	0.86	0.712	1.04	0.683	0.95	1.30	0.916	No
3867	38.67	2.27	0.96	1.31	0.86	0.712	1.04	0.683	0.95	1.30	0.916	No
3868	38.68	2.27	0.96	1.32	0.86	0.712	1.04	0.683	0.95	1.30	0.916	No
3869	38.69	2.27	0.96	1.32	0.86	0.712	1.04	0.683	0.95	1.30	0.915	No
3870	38.70	2.27	0.96	1.32	0.86	0.712	1.04	0.683	0.95	1.30	0.915	No
3871	38.71	2.27	0.96	1.32	0.86	0.712	1.04	0.683	0.95	1.30	0.915	No
3872	38.72	2.27	0.96	1.32	0.86	0.712	1.04	0.683	0.95	1.30	0.915	No
3873	38.73	2.28	0.96	1.32	0.86	0.712	1.04	0.683	0.95	1.30	0.916	No
3874	38.74	2.28	0.96	1.32	0.86	0.712	1.04	0.683	0.95	1.30	0.916	No
3875	38.75	2.28	0.96	1.32	0.86	0.712	1.04	0.683	0.95	1.30	0.916	No
3876	38.76	2.28	0.96	1.32	0.86	0.712	1.04	0.683	0.95	1.30	0.916	No
3877	38.77	2.28	0.96	1.32	0.86	0.712	1.04	0.683	0.95	1.30	0.917	No
3878	38.78	2.28	0.96	1.32	0.86	0.712	1.04	0.683	0.95	1.30	0.917	No
3879	38.79	2.28	0.96	1.32	0.86	0.712	1.04	0.683	0.95	1.30	0.917	No
3880	38.80	2.28	0.96	1.32	0.86	0.712	1.04	0.682	0.95	1.30	0.918	No
3881	38.81	2.28	0.96	1.32	0.86	0.712	1.04	0.682	0.95	1.30	0.918	No
3882	38.82	2.28	0.96	1.32	0.86	0.712	1.04	0.682	0.95	1.30	0.918	No
3883	38.83	2.28	0.96	1.32	0.86	0.712	1.04	0.682	0.95	1.30	0.918	No
3884	38.84	2.28	0.96	1.32	0.86	0.712	1.04	0.682	0.95	1.30	0.918	No
3885	38.85	2.28	0.96	1.32	0.86	0.712	1.04	0.682	0.95	1.30	0.918	No
3886	38.86	2.28	0.96	1.32	0.86	0.712	1.04	0.682	0.95	1.30	0.918	No
3887	38.87	2.29	0.96	1.32	0.86	0.712	1.04	0.682	0.95	1.30	0.918	No
3888	38.88	2.29	0.96	1.32	0.86	0.712	1.04	0.682	0.95	1.30	0.918	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
3889	38.89	2.29	0.96	1.32	0.86	0.712	1.04	0.682	0.95	1.30	0.918	No
3890	38.90	2.29	0.96	1.32	0.86	0.712	1.04	0.682	0.95	1.30	0.918	No
3891	38.91	2.29	0.96	1.32	0.86	0.712	1.04	0.682	0.95	1.30	0.918	No
3892	38.92	2.29	0.96	1.32	0.86	0.712	1.04	0.682	0.95	1.30	0.918	No
3893	38.93	2.29	0.97	1.32	0.86	0.712	1.04	0.682	0.95	1.30	0.918	No
3894	38.94	2.29	0.97	1.32	0.86	0.712	1.04	0.682	0.95	1.30	0.917	No
3895	38.95	2.29	0.97	1.32	0.86	0.712	1.04	0.682	0.95	1.30	0.917	No
3896	38.96	2.29	0.97	1.33	0.86	0.712	1.04	0.682	0.95	1.30	0.917	No
3897	38.97	2.29	0.97	1.33	0.86	0.712	1.04	0.682	0.95	1.30	0.916	No
3898	38.98	2.29	0.97	1.33	0.86	0.712	1.04	0.682	0.95	1.30	0.916	No
3899	38.99	2.29	0.97	1.33	0.86	0.712	1.04	0.682	0.95	1.30	0.916	No
3900	39.00	2.29	0.97	1.33	0.86	0.712	1.04	0.682	0.95	1.30	0.916	No
3901	39.01	2.29	0.97	1.33	0.86	0.712	1.04	0.682	0.95	1.30	0.916	No
3902	39.02	2.30	0.97	1.33	0.86	0.712	1.04	0.682	0.95	1.30	0.916	No
3903	39.03	2.30	0.97	1.33	0.86	0.711	1.04	0.682	0.95	1.30	0.917	No
3904	39.04	2.30	0.97	1.33	0.86	0.711	1.04	0.682	0.95	1.30	0.918	No
3905	39.05	2.30	0.97	1.33	0.86	0.711	1.04	0.682	0.95	1.30	0.918	No
3906	39.06	2.30	0.97	1.33	0.86	0.711	1.04	0.682	0.94	1.30	0.919	No
3907	39.07	2.30	0.97	1.33	0.86	0.711	1.04	0.682	0.94	1.30	0.920	No
3908	39.08	2.30	0.97	1.33	0.86	0.711	1.04	0.682	0.94	1.30	0.920	No
3909	39.09	2.30	0.97	1.33	0.86	0.711	1.04	0.682	0.94	1.30	0.921	No
3910	39.10	2.30	0.97	1.33	0.86	0.711	1.04	0.682	0.94	1.30	0.921	No
3911	39.11	2.30	0.97	1.33	0.86	0.711	1.04	0.682	0.94	1.30	0.922	No
3912	39.12	2.30	0.97	1.33	0.85	0.711	1.04	0.682	0.94	1.30	0.923	No
3913	39.13	2.30	0.97	1.33	0.85	0.711	1.04	0.682	0.94	1.30	0.923	No
3914	39.14	2.30	0.97	1.33	0.85	0.711	1.04	0.682	0.94	1.30	0.924	No
3915	39.15	2.30	0.97	1.33	0.85	0.711	1.04	0.682	0.94	1.30	0.925	No
3916	39.16	2.30	0.97	1.33	0.85	0.711	1.04	0.682	0.94	1.30	0.925	No
3917	39.17	2.31	0.97	1.33	0.85	0.711	1.04	0.682	0.94	1.30	0.926	No
3918	39.18	2.31	0.97	1.33	0.85	0.711	1.04	0.682	0.94	1.30	0.927	No
3919	39.19	2.31	0.97	1.33	0.85	0.711	1.04	0.682	0.94	1.30	0.927	No
3920	39.20	2.31	0.97	1.33	0.85	0.711	1.04	0.682	0.94	1.30	0.928	No
3921	39.21	2.31	0.97	1.33	0.85	0.711	1.04	0.682	0.93	1.30	0.928	No
3922	39.22	2.31	0.97	1.33	0.85	0.711	1.04	0.682	0.93	1.30	0.929	No
3923	39.23	2.31	0.97	1.33	0.85	0.711	1.04	0.681	0.93	1.30	0.930	No
3924	39.24	2.31	0.97	1.34	0.85	0.711	1.04	0.681	0.93	1.30	0.931	No
3925	39.25	2.31	0.98	1.34	0.85	0.711	1.04	0.681	0.93	1.30	0.932	No
3926	39.26	2.31	0.98	1.34	0.85	0.711	1.04	0.681	0.93	1.30	0.933	No
3927	39.27	2.31	0.98	1.34	0.85	0.711	1.04	0.681	0.93	1.30	0.933	No
3928	39.28	2.31	0.98	1.34	0.85	0.711	1.04	0.681	0.93	1.30	0.933	No
3929	39.29	2.31	0.98	1.34	0.85	0.711	1.04	0.681	0.93	1.30	0.933	No
3930	39.30	2.31	0.98	1.34	0.85	0.711	1.04	0.681	0.93	1.30	0.933	No
3931	39.31	2.31	0.98	1.34	0.85	0.711	1.04	0.681	0.93	1.30	0.933	No
3932	39.32	2.32	0.98	1.34	0.85	0.711	1.04	0.681	0.93	1.30	0.933	No
3933	39.33	2.32	0.98	1.34	0.85	0.711	1.04	0.681	0.93	1.30	0.934	No
3934	39.34	2.32	0.98	1.34	0.85	0.711	1.04	0.681	0.93	1.30	0.934	No
3935	39.35	2.32	0.98	1.34	0.85	0.711	1.04	0.681	0.93	1.30	0.934	No
3936	39.36	2.32	0.98	1.34	0.85	0.711	1.04	0.681	0.93	1.30	0.934	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
3937	39.37	2.32	0.98	1.34	0.85	0.711	1.04	0.681	0.93	1.30	0.934	No
3938	39.38	2.32	0.98	1.34	0.85	0.711	1.04	0.681	0.93	1.30	0.934	No
3939	39.39	2.32	0.98	1.34	0.85	0.711	1.04	0.681	0.93	1.30	0.934	No
3940	39.40	2.32	0.98	1.34	0.85	0.711	1.04	0.681	0.93	1.30	0.934	No
3941	39.41	2.32	0.98	1.34	0.85	0.711	1.04	0.681	0.93	1.30	0.934	No
3942	39.42	2.32	0.98	1.34	0.85	0.711	1.04	0.681	0.93	1.30	0.934	No
3943	39.43	2.32	0.98	1.34	0.85	0.711	1.04	0.681	0.93	1.30	0.934	No
3944	39.44	2.32	0.98	1.34	0.85	0.710	1.04	0.681	0.93	1.30	0.934	No
3945	39.45	2.32	0.98	1.34	0.85	0.710	1.04	0.681	0.93	1.30	0.934	No
3946	39.46	2.32	0.98	1.34	0.85	0.710	1.04	0.681	0.93	1.30	0.934	No
3947	39.47	2.33	0.98	1.34	0.85	0.710	1.04	0.681	0.93	1.30	0.934	No
3948	39.48	2.33	0.98	1.34	0.85	0.710	1.04	0.681	0.93	1.30	0.934	No
3949	39.49	2.33	0.98	1.34	0.85	0.710	1.04	0.681	0.93	1.30	0.934	No
3950	39.50	2.33	0.98	1.34	0.85	0.710	1.04	0.681	0.93	1.30	0.934	No
3951	39.51	2.33	0.98	1.34	0.85	0.710	1.04	0.681	0.93	1.30	0.934	No
3952	39.52	2.33	0.98	1.35	0.85	0.710	1.04	0.681	0.93	1.30	0.934	No
3953	39.53	2.33	0.98	1.35	0.85	0.710	1.04	0.681	0.93	1.30	0.934	No
3954	39.54	2.33	0.98	1.35	0.85	0.710	1.04	0.681	0.93	1.30	0.935	No
3955	39.55	2.33	0.98	1.35	0.85	0.710	1.04	0.681	0.93	1.30	0.935	No
3956	39.56	2.33	0.98	1.35	0.85	0.710	1.04	0.681	0.93	1.30	0.935	No
3957	39.57	2.33	0.98	1.35	0.85	0.710	1.04	0.681	0.93	1.30	0.935	No
3958	39.58	2.33	0.99	1.35	0.85	0.710	1.04	0.681	0.93	1.30	0.935	No
3959	39.59	2.33	0.99	1.35	0.85	0.710	1.04	0.681	0.93	1.30	0.935	No
3960	39.60	2.33	0.99	1.35	0.85	0.710	1.04	0.681	0.93	1.30	0.935	No
3961	39.61	2.33	0.99	1.35	0.85	0.710	1.04	0.681	0.93	1.30	0.935	No
3962	39.62	2.34	0.99	1.35	0.85	0.710	1.04	0.681	0.93	1.30	0.935	No
3963	39.63	2.34	0.99	1.35	0.85	0.710	1.04	0.680	0.93	1.30	0.935	No
3964	39.64	2.34	0.99	1.35	0.85	0.710	1.04	0.680	0.93	1.30	0.935	No
3965	39.65	2.34	0.99	1.35	0.85	0.710	1.04	0.680	0.93	1.30	0.935	No
3966	39.66	2.34	0.99	1.35	0.85	0.710	1.04	0.680	0.93	1.30	0.935	No
3967	39.67	2.34	0.99	1.35	0.85	0.710	1.04	0.680	0.93	1.30	0.935	No
3968	39.68	2.34	0.99	1.35	0.85	0.710	1.04	0.680	0.93	1.30	0.935	No
3969	39.69	2.34	0.99	1.35	0.85	0.710	1.04	0.680	0.93	1.30	0.935	No
3970	39.70	2.34	0.99	1.35	0.85	0.710	1.04	0.680	0.93	1.30	0.935	No
3971	39.71	2.34	0.99	1.35	0.85	0.710	1.04	0.680	0.93	1.30	0.935	No
3972	39.72	2.34	0.99	1.35	0.85	0.710	1.04	0.680	0.93	1.30	0.935	No
3973	39.73	2.34	0.99	1.35	0.85	0.710	1.04	0.680	0.93	1.30	0.935	No
3974	39.74	2.34	0.99	1.35	0.85	0.710	1.04	0.680	0.93	1.30	0.935	No
3975	39.75	2.34	0.99	1.35	0.85	0.710	1.04	0.680	0.93	1.30	0.935	No
3976	39.76	2.34	0.99	1.35	0.85	0.710	1.04	0.680	0.93	1.30	0.936	No
3977	39.77	2.35	0.99	1.35	0.85	0.710	1.04	0.680	0.93	1.30	0.936	No
3978	39.78	2.35	0.99	1.35	0.85	0.710	1.04	0.680	0.93	1.30	0.936	No
3979	39.79	2.35	0.99	1.36	0.85	0.710	1.04	0.680	0.93	1.30	0.936	No
3980	39.80	2.35	0.99	1.36	0.85	0.710	1.04	0.680	0.93	1.30	0.936	No
3981	39.81	2.35	0.99	1.36	0.85	0.710	1.04	0.680	0.93	1.30	0.936	No
3982	39.82	2.35	0.99	1.36	0.85	0.709	1.04	0.680	0.93	1.30	0.936	No
3983	39.83	2.35	0.99	1.36	0.85	0.709	1.04	0.680	0.93	1.30	0.936	No
3984	39.84	2.35	0.99	1.36	0.85	0.709	1.04	0.680	0.93	1.30	0.936	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
3985	39.85	2.35	0.99	1.36	0.85	0.709	1.04	0.680	0.93	1.30	0.936	No
3986	39.86	2.35	0.99	1.36	0.85	0.709	1.04	0.680	0.93	1.30	0.936	No
3987	39.87	2.35	0.99	1.36	0.85	0.709	1.04	0.680	0.93	1.30	0.936	No
3988	39.88	2.35	0.99	1.36	0.85	0.709	1.04	0.680	0.93	1.30	0.936	No
3989	39.89	2.35	0.99	1.36	0.85	0.709	1.04	0.680	0.93	1.30	0.936	No
3990	39.90	2.35	1.00	1.36	0.85	0.709	1.04	0.680	0.92	1.30	0.936	No
3991	39.91	2.35	1.00	1.36	0.85	0.709	1.04	0.680	0.92	1.30	0.936	No
3992	39.92	2.36	1.00	1.36	0.85	0.709	1.04	0.680	0.92	1.30	0.936	No
3993	39.93	2.36	1.00	1.36	0.85	0.709	1.04	0.680	0.92	1.30	0.936	No
3994	39.94	2.36	1.00	1.36	0.85	0.709	1.04	0.680	0.92	1.30	0.936	No
3995	39.95	2.36	1.00	1.36	0.85	0.709	1.04	0.680	0.92	1.30	0.936	No
3996	39.96	2.36	1.00	1.36	0.85	0.709	1.04	0.680	0.92	1.30	0.936	No
3997	39.97	2.36	1.00	1.36	0.85	0.709	1.04	0.680	0.92	1.30	0.936	No
3998	39.98	2.36	1.00	1.36	0.85	0.709	1.04	0.680	0.92	1.30	0.937	No
3999	39.99	2.36	1.00	1.36	0.85	0.709	1.04	0.680	0.92	1.30	0.937	No
4000	40.00	2.36	1.00	1.36	0.85	0.709	1.04	0.680	0.92	1.30	0.937	No
4001	40.01	2.36	1.00	1.36	0.85	0.709	1.04	0.680	0.92	1.30	0.937	No
4002	40.02	2.36	1.00	1.36	0.85	0.709	1.04	0.680	0.92	1.30	0.937	No
4003	40.03	2.36	1.00	1.36	0.85	0.709	1.04	0.679	0.92	1.30	0.937	No
4004	40.04	2.36	1.00	1.36	0.85	0.709	1.04	0.679	0.92	1.30	0.937	No
4005	40.05	2.36	1.00	1.36	0.85	0.709	1.04	0.679	0.92	1.30	0.937	No
4006	40.06	2.37	1.00	1.36	0.85	0.709	1.04	0.679	0.92	1.30	0.937	No
4007	40.07	2.37	1.00	1.37	0.85	0.709	1.04	0.679	0.92	1.30	0.937	No
4008	40.08	2.37	1.00	1.37	0.85	0.709	1.04	0.679	0.92	1.30	0.937	No
4009	40.09	2.37	1.00	1.37	0.85	0.709	1.04	0.679	0.92	1.30	0.937	No
4010	40.10	2.37	1.00	1.37	0.85	0.709	1.04	0.679	0.92	1.30	0.937	No
4011	40.11	2.37	1.00	1.37	0.85	0.709	1.04	0.679	0.92	1.30	0.937	No
4012	40.12	2.37	1.00	1.37	0.85	0.709	1.04	0.679	0.92	1.30	0.937	No
4013	40.13	2.37	1.00	1.37	0.85	0.709	1.04	0.679	0.92	1.30	0.937	No
4014	40.14	2.37	1.00	1.37	0.85	0.709	1.04	0.679	0.92	1.30	0.937	No
4015	40.15	2.37	1.00	1.37	0.85	0.709	1.04	0.679	0.92	1.30	0.937	No
4016	40.16	2.37	1.00	1.37	0.85	0.709	1.04	0.679	0.92	1.30	0.937	No
4017	40.17	2.37	1.00	1.37	0.85	0.709	1.04	0.679	0.92	1.30	0.937	No
4018	40.18	2.37	1.00	1.37	0.85	0.709	1.04	0.679	0.92	1.30	0.937	No
4019	40.19	2.37	1.00	1.37	0.85	0.709	1.04	0.679	0.92	1.30	0.938	No
4020	40.20	2.37	1.00	1.37	0.85	0.708	1.04	0.679	0.92	1.30	0.938	No
4021	40.21	2.38	1.00	1.37	0.85	0.708	1.04	0.679	0.92	1.30	0.938	No
4022	40.22	2.38	1.01	1.37	0.85	0.708	1.04	0.679	0.92	1.30	0.938	No
4023	40.23	2.38	1.01	1.37	0.85	0.708	1.04	0.679	0.92	1.30	0.938	No
4024	40.24	2.38	1.01	1.37	0.85	0.708	1.04	0.679	0.92	1.30	0.938	No
4025	40.25	2.38	1.01	1.37	0.85	0.708	1.04	0.679	0.92	1.30	0.938	No
4026	40.26	2.38	1.01	1.37	0.85	0.708	1.04	0.679	0.92	1.30	0.938	No
4027	40.27	2.38	1.01	1.37	0.85	0.708	1.04	0.679	0.92	1.30	0.938	No
4028	40.28	2.38	1.01	1.37	0.85	0.708	1.04	0.679	0.92	1.30	0.938	No
4029	40.29	2.38	1.01	1.37	0.85	0.708	1.04	0.679	0.92	1.30	0.938	No
4030	40.30	2.38	1.01	1.37	0.85	0.708	1.04	0.679	0.92	1.30	0.938	No
4031	40.31	2.38	1.01	1.37	0.85	0.708	1.04	0.679	0.92	1.30	0.938	No
4032	40.32	2.38	1.01	1.37	0.85	0.708	1.04	0.679	0.92	1.30	0.938	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
4033	40.33	2.38	1.01	1.37	0.85	0.708	1.04	0.679	0.92	1.30	0.938	No
4034	40.34	2.38	1.01	1.37	0.85	0.708	1.04	0.679	0.92	1.30	0.938	No
4035	40.35	2.38	1.01	1.38	0.85	0.708	1.04	0.679	0.92	1.30	0.938	No
4036	40.36	2.39	1.01	1.38	0.85	0.708	1.04	0.679	0.92	1.30	0.938	No
4037	40.37	2.39	1.01	1.38	0.85	0.708	1.04	0.679	0.92	1.30	0.938	No
4038	40.38	2.39	1.01	1.38	0.85	0.708	1.04	0.679	0.92	1.30	0.938	No
4039	40.39	2.39	1.01	1.38	0.85	0.708	1.04	0.679	0.92	1.30	0.938	No
4040	40.40	2.39	1.01	1.38	0.85	0.708	1.04	0.679	0.92	1.30	0.938	No
4041	40.41	2.39	1.01	1.38	0.85	0.708	1.04	0.679	0.92	1.30	0.938	No
4042	40.42	2.39	1.01	1.38	0.85	0.708	1.04	0.679	0.92	1.30	0.939	No
4043	40.43	2.39	1.01	1.38	0.85	0.708	1.04	0.678	0.92	1.30	0.939	No
4044	40.44	2.39	1.01	1.38	0.85	0.708	1.04	0.678	0.92	1.30	0.939	No
4045	40.45	2.39	1.01	1.38	0.85	0.708	1.04	0.678	0.92	1.30	0.939	No
4046	40.46	2.39	1.01	1.38	0.85	0.708	1.04	0.678	0.92	1.30	0.939	No
4047	40.47	2.39	1.01	1.38	0.85	0.708	1.04	0.678	0.92	1.30	0.939	No
4048	40.48	2.39	1.01	1.38	0.85	0.708	1.04	0.678	0.92	1.30	0.939	No
4049	40.49	2.39	1.01	1.38	0.85	0.708	1.04	0.678	0.92	1.30	0.939	No
4050	40.50	2.39	1.01	1.38	0.85	0.708	1.04	0.678	0.92	1.30	0.939	No
4051	40.51	2.40	1.01	1.38	0.85	0.708	1.04	0.678	0.92	1.30	0.939	No
4052	40.52	2.40	1.01	1.38	0.85	0.708	1.04	0.678	0.92	1.30	0.939	No
4053	40.53	2.40	1.01	1.38	0.85	0.708	1.04	0.678	0.92	1.30	0.939	No
4054	40.54	2.40	1.02	1.38	0.85	0.708	1.04	0.678	0.92	1.30	0.939	No
4055	40.55	2.40	1.02	1.38	0.85	0.708	1.04	0.678	0.92	1.30	0.939	No
4056	40.56	2.40	1.02	1.38	0.85	0.708	1.04	0.678	0.92	1.30	0.939	No
4057	40.57	2.40	1.02	1.38	0.85	0.708	1.04	0.678	0.92	1.30	0.939	No
4058	40.58	2.40	1.02	1.38	0.85	0.707	1.04	0.678	0.92	1.30	0.939	No
4059	40.59	2.40	1.02	1.38	0.85	0.707	1.04	0.678	0.92	1.30	0.939	No
4060	40.60	2.40	1.02	1.38	0.85	0.707	1.04	0.678	0.92	1.30	0.939	No
4061	40.61	2.40	1.02	1.38	0.85	0.707	1.04	0.678	0.92	1.30	0.939	No
4062	40.62	2.40	1.02	1.38	0.85	0.707	1.04	0.678	0.92	1.30	0.939	No
4063	40.63	2.40	1.02	1.39	0.85	0.707	1.04	0.678	0.92	1.30	0.939	No
4064	40.64	2.40	1.02	1.39	0.85	0.707	1.04	0.678	0.92	1.30	0.940	No
4065	40.65	2.40	1.02	1.39	0.85	0.707	1.04	0.678	0.92	1.30	0.940	No
4066	40.66	2.41	1.02	1.39	0.85	0.707	1.04	0.678	0.92	1.30	0.940	No
4067	40.67	2.41	1.02	1.39	0.85	0.707	1.04	0.678	0.92	1.30	0.940	No
4068	40.68	2.41	1.02	1.39	0.85	0.707	1.04	0.678	0.92	1.30	0.939	No
4069	40.69	2.41	1.02	1.39	0.85	0.707	1.04	0.678	0.92	1.30	0.938	No
4070	40.70	2.41	1.02	1.39	0.85	0.707	1.04	0.678	0.92	1.30	0.937	No
4071	40.71	2.41	1.02	1.39	0.85	0.707	1.04	0.678	0.92	1.30	0.936	No
4072	40.72	2.41	1.02	1.39	0.85	0.707	1.04	0.678	0.92	1.30	0.935	No
4073	40.73	2.41	1.02	1.39	0.85	0.707	1.04	0.678	0.92	1.30	0.935	No
4074	40.74	2.41	1.02	1.39	0.85	0.707	1.04	0.678	0.92	1.30	0.934	No
4075	40.75	2.41	1.02	1.39	0.85	0.707	1.04	0.678	0.92	1.30	0.933	No
4076	40.76	2.41	1.02	1.39	0.85	0.707	1.04	0.678	0.93	1.30	0.933	No
4077	40.77	2.41	1.02	1.39	0.85	0.707	1.04	0.678	0.93	1.30	0.932	No
4078	40.78	2.41	1.02	1.39	0.85	0.707	1.04	0.678	0.93	1.30	0.931	No
4079	40.79	2.41	1.02	1.39	0.85	0.707	1.04	0.678	0.93	1.30	0.930	No
4080	40.80	2.41	1.02	1.39	0.85	0.707	1.04	0.678	0.93	1.30	0.930	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
4081	40.81	2.42	1.02	1.39	0.85	0.707	1.04	0.678	0.93	1.30	0.929	No
4082	40.82	2.42	1.02	1.39	0.85	0.707	1.04	0.678	0.93	1.30	0.928	No
4083	40.83	2.42	1.02	1.39	0.85	0.707	1.04	0.677	0.93	1.30	0.928	No
4084	40.84	2.42	1.02	1.39	0.85	0.707	1.04	0.677	0.93	1.30	0.927	No
4085	40.85	2.42	1.02	1.39	0.85	0.707	1.04	0.677	0.93	1.30	0.926	No
4086	40.86	2.42	1.03	1.39	0.85	0.707	1.04	0.677	0.93	1.30	0.925	No
4087	40.87	2.42	1.03	1.39	0.85	0.707	1.04	0.677	0.93	1.30	0.924	No
4088	40.88	2.42	1.03	1.39	0.85	0.707	1.04	0.677	0.93	1.30	0.923	No
4089	40.89	2.42	1.03	1.39	0.85	0.707	1.04	0.677	0.94	1.30	0.922	No
4090	40.90	2.42	1.03	1.39	0.85	0.707	1.04	0.677	0.94	1.30	0.922	No
4091	40.91	2.42	1.03	1.40	0.85	0.707	1.04	0.677	0.94	1.30	0.921	No
4092	40.92	2.42	1.03	1.40	0.85	0.707	1.04	0.677	0.94	1.30	0.921	No
4093	40.93	2.42	1.03	1.40	0.85	0.707	1.04	0.677	0.94	1.30	0.920	No
4094	40.94	2.42	1.03	1.40	0.85	0.707	1.04	0.677	0.94	1.30	0.921	No
4095	40.95	2.42	1.03	1.40	0.85	0.707	1.04	0.677	0.94	1.30	0.921	No
4096	40.96	2.43	1.03	1.40	0.85	0.707	1.04	0.677	0.94	1.30	0.921	No
4097	40.97	2.43	1.03	1.40	0.85	0.707	1.04	0.677	0.94	1.30	0.922	No
4098	40.98	2.43	1.03	1.40	0.85	0.706	1.04	0.677	0.94	1.30	0.922	No
4099	40.99	2.43	1.03	1.40	0.85	0.706	1.04	0.677	0.94	1.30	0.922	No
4100	41.00	2.43	1.03	1.40	0.85	0.706	1.04	0.677	0.94	1.30	0.923	No
4101	41.01	2.43	1.03	1.40	0.85	0.706	1.04	0.677	0.94	1.30	0.923	No
4102	41.02	2.43	1.03	1.40	0.85	0.706	1.04	0.677	0.94	1.30	2.000	Yes
4103	41.03	2.43	1.03	1.40	0.85	0.706	1.04	0.677	0.95	1.30	2.000	Yes
4104	41.04	2.43	1.03	1.40	0.85	0.706	1.04	0.677	0.95	1.30	2.000	Yes
4105	41.05	2.43	1.03	1.40	0.85	0.706	1.04	0.677	0.95	1.30	2.000	Yes
4106	41.06	2.43	1.03	1.40	0.85	0.706	1.04	0.677	0.95	1.30	2.000	Yes
4107	41.07	2.43	1.03	1.40	0.85	0.706	1.04	0.677	0.95	1.30	2.000	Yes
4108	41.08	2.43	1.03	1.40	0.85	0.706	1.04	0.677	0.95	1.30	2.000	Yes
4109	41.09	2.43	1.03	1.40	0.85	0.706	1.04	0.677	0.95	1.30	2.000	Yes
4110	41.10	2.43	1.03	1.40	0.85	0.706	1.04	0.677	0.95	1.30	2.000	Yes
4111	41.11	2.44	1.03	1.40	0.85	0.706	1.04	0.677	0.95	1.30	2.000	Yes
4112	41.12	2.44	1.03	1.40	0.85	0.706	1.04	0.677	0.95	1.30	2.000	Yes
4113	41.13	2.44	1.03	1.40	0.85	0.706	1.04	0.677	0.95	1.30	2.000	Yes
4114	41.14	2.44	1.03	1.40	0.85	0.706	1.04	0.677	0.95	1.30	2.000	Yes
4115	41.15	2.44	1.03	1.40	0.85	0.706	1.04	0.677	0.95	1.30	2.000	Yes
4116	41.16	2.44	1.03	1.40	0.85	0.706	1.04	0.677	0.95	1.30	2.000	Yes
4117	41.17	2.44	1.03	1.40	0.85	0.706	1.04	0.677	0.95	1.30	2.000	Yes
4118	41.18	2.44	1.04	1.40	0.84	0.706	1.04	0.677	0.95	1.30	2.000	Yes
4119	41.19	2.44	1.04	1.40	0.84	0.706	1.04	0.677	0.95	1.30	2.000	Yes
4120	41.20	2.44	1.04	1.40	0.84	0.706	1.04	0.677	0.96	1.30	2.000	Yes
4121	41.21	2.44	1.04	1.41	0.84	0.706	1.04	0.677	0.96	1.30	2.000	Yes
4122	41.22	2.44	1.04	1.41	0.84	0.706	1.04	0.677	0.96	1.30	2.000	Yes
4123	41.23	2.44	1.04	1.41	0.84	0.706	1.04	0.677	0.96	1.30	2.000	Yes
4124	41.24	2.44	1.04	1.41	0.84	0.706	1.04	0.677	0.96	1.30	2.000	Yes
4125	41.25	2.44	1.04	1.41	0.84	0.706	1.04	0.677	0.96	1.30	2.000	Yes
4126	41.26	2.44	1.04	1.41	0.84	0.706	1.04	0.677	0.96	1.30	2.000	Yes
4127	41.27	2.45	1.04	1.41	0.84	0.706	1.04	0.677	0.96	1.30	2.000	Yes
4128	41.28	2.45	1.04	1.41	0.84	0.706	1.04	0.677	0.96	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
4129	41.29	2.45	1.04	1.41	0.84	0.706	1.04	0.676	0.96	1.30	2.000	Yes
4130	41.30	2.45	1.04	1.41	0.84	0.706	1.04	0.676	0.96	1.30	2.000	Yes
4131	41.31	2.45	1.04	1.41	0.84	0.706	1.04	0.676	0.96	1.30	2.000	Yes
4132	41.32	2.45	1.04	1.41	0.84	0.706	1.04	0.676	0.96	1.30	2.000	Yes
4133	41.33	2.45	1.04	1.41	0.84	0.706	1.04	0.676	0.96	1.30	2.000	Yes
4134	41.34	2.45	1.04	1.41	0.84	0.706	1.04	0.676	0.96	1.30	2.000	Yes
4135	41.35	2.45	1.04	1.41	0.84	0.706	1.04	0.676	0.96	1.30	2.000	Yes
4136	41.36	2.45	1.04	1.41	0.84	0.706	1.04	0.676	0.96	1.30	2.000	Yes
4137	41.37	2.45	1.04	1.41	0.84	0.706	1.04	0.676	0.96	1.30	2.000	Yes
4138	41.38	2.45	1.04	1.41	0.84	0.706	1.04	0.676	0.96	1.30	2.000	Yes
4139	41.39	2.45	1.04	1.41	0.84	0.706	1.04	0.676	0.96	1.30	2.000	Yes
4140	41.40	2.45	1.04	1.41	0.84	0.706	1.04	0.676	0.96	1.30	2.000	Yes
4141	41.41	2.45	1.04	1.41	0.84	0.706	1.04	0.676	0.96	1.30	2.000	Yes
4142	41.42	2.45	1.04	1.41	0.84	0.706	1.04	0.676	0.96	1.30	2.000	Yes
4143	41.43	2.46	1.04	1.41	0.84	0.706	1.04	0.676	0.96	1.30	2.000	Yes
4144	41.44	2.46	1.04	1.41	0.84	0.706	1.04	0.676	0.96	1.30	2.000	Yes
4145	41.45	2.46	1.04	1.41	0.84	0.705	1.04	0.676	0.96	1.30	2.000	Yes
4146	41.46	2.46	1.04	1.41	0.84	0.705	1.04	0.676	0.96	1.30	2.000	Yes
4147	41.47	2.46	1.04	1.41	0.84	0.705	1.04	0.676	0.96	1.30	2.000	Yes
4148	41.48	2.46	1.04	1.41	0.84	0.705	1.04	0.676	0.96	1.30	2.000	Yes
4149	41.49	2.46	1.04	1.41	0.84	0.705	1.04	0.676	0.96	1.30	2.000	Yes
4150	41.50	2.46	1.05	1.41	0.84	0.705	1.04	0.676	0.96	1.30	2.000	Yes
4151	41.51	2.46	1.05	1.42	0.84	0.705	1.04	0.676	0.96	1.30	2.000	Yes
4152	41.52	2.46	1.05	1.42	0.84	0.705	1.04	0.676	0.96	1.30	2.000	Yes
4153	41.53	2.46	1.05	1.42	0.84	0.705	1.04	0.676	0.96	1.30	2.000	Yes
4154	41.54	2.46	1.05	1.42	0.84	0.705	1.04	0.676	0.96	1.30	2.000	Yes
4155	41.55	2.46	1.05	1.42	0.84	0.705	1.04	0.676	0.96	1.30	2.000	Yes
4156	41.56	2.46	1.05	1.42	0.84	0.705	1.04	0.676	0.96	1.30	2.000	Yes
4157	41.57	2.46	1.05	1.42	0.84	0.705	1.04	0.676	0.96	1.30	2.000	Yes
4158	41.58	2.46	1.05	1.42	0.84	0.705	1.04	0.676	0.96	1.30	2.000	Yes
4159	41.59	2.47	1.05	1.42	0.84	0.705	1.04	0.676	0.96	1.30	2.000	Yes
4160	41.60	2.47	1.05	1.42	0.84	0.705	1.04	0.676	0.96	1.30	2.000	Yes
4161	41.61	2.47	1.05	1.42	0.84	0.705	1.04	0.676	0.96	1.30	2.000	Yes
4162	41.62	2.47	1.05	1.42	0.84	0.705	1.04	0.676	0.96	1.30	2.000	Yes
4163	41.63	2.47	1.05	1.42	0.84	0.705	1.04	0.676	0.96	1.30	2.000	Yes
4164	41.64	2.47	1.05	1.42	0.84	0.705	1.04	0.676	0.96	1.30	2.000	Yes
4165	41.65	2.47	1.05	1.42	0.84	0.705	1.04	0.676	0.96	1.30	2.000	Yes
4166	41.66	2.47	1.05	1.42	0.84	0.705	1.04	0.676	0.97	1.30	2.000	Yes
4167	41.67	2.47	1.05	1.42	0.84	0.705	1.04	0.676	0.97	1.30	2.000	Yes
4168	41.68	2.47	1.05	1.42	0.84	0.705	1.04	0.676	0.97	1.30	2.000	Yes
4169	41.69	2.47	1.05	1.42	0.84	0.705	1.04	0.676	0.97	1.30	2.000	Yes
4170	41.70	2.47	1.05	1.42	0.84	0.705	1.04	0.676	0.97	1.30	2.000	Yes
4171	41.71	2.47	1.05	1.42	0.84	0.705	1.04	0.676	0.97	1.30	2.000	Yes
4172	41.72	2.47	1.05	1.42	0.84	0.705	1.04	0.676	0.97	1.30	2.000	Yes
4173	41.73	2.47	1.05	1.42	0.84	0.705	1.04	0.676	0.97	1.30	2.000	Yes
4174	41.74	2.48	1.05	1.42	0.84	0.705	1.04	0.676	0.97	1.30	2.000	Yes
4175	41.75	2.48	1.05	1.42	0.84	0.705	1.04	0.676	0.97	1.30	2.000	Yes
4176	41.76	2.48	1.05	1.42	0.84	0.705	1.04	0.676	0.97	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
4177	41.77	2.48	1.05	1.42	0.84	0.705	1.04	0.676	0.97	1.30	2.000	Yes
4178	41.78	2.48	1.05	1.42	0.84	0.705	1.04	0.676	0.97	1.30	2.000	Yes
4179	41.79	2.48	1.05	1.42	0.84	0.705	1.04	0.676	0.97	1.30	2.000	Yes
4180	41.80	2.48	1.05	1.42	0.84	0.705	1.04	0.676	0.97	1.30	2.000	Yes
4181	41.81	2.48	1.05	1.42	0.84	0.705	1.04	0.676	0.97	1.30	2.000	Yes
4182	41.82	2.48	1.06	1.42	0.84	0.705	1.04	0.675	0.97	1.30	2.000	Yes
4183	41.83	2.48	1.06	1.43	0.84	0.705	1.04	0.675	0.97	1.30	2.000	Yes
4184	41.84	2.48	1.06	1.43	0.84	0.705	1.04	0.675	0.97	1.30	2.000	Yes
4185	41.85	2.48	1.06	1.43	0.84	0.705	1.04	0.675	0.97	1.30	2.000	Yes
4186	41.86	2.48	1.06	1.43	0.84	0.705	1.04	0.675	0.97	1.30	2.000	Yes
4187	41.87	2.48	1.06	1.43	0.84	0.705	1.04	0.675	0.97	1.30	2.000	Yes
4188	41.88	2.48	1.06	1.43	0.84	0.705	1.04	0.675	0.97	1.30	2.000	Yes
4189	41.89	2.48	1.06	1.43	0.84	0.705	1.04	0.675	0.97	1.30	2.000	Yes
4190	41.90	2.49	1.06	1.43	0.84	0.705	1.04	0.675	0.97	1.30	2.000	Yes
4191	41.91	2.49	1.06	1.43	0.84	0.705	1.04	0.675	0.97	1.30	2.000	Yes
4192	41.92	2.49	1.06	1.43	0.84	0.705	1.04	0.675	0.97	1.30	2.000	Yes
4193	41.93	2.49	1.06	1.43	0.84	0.705	1.04	0.675	0.97	1.30	2.000	Yes
4194	41.94	2.49	1.06	1.43	0.84	0.705	1.04	0.675	0.97	1.30	2.000	Yes
4195	41.95	2.49	1.06	1.43	0.84	0.705	1.04	0.675	0.97	1.30	2.000	Yes
4196	41.96	2.49	1.06	1.43	0.84	0.704	1.04	0.675	0.97	1.30	0.933	No
4197	41.97	2.49	1.06	1.43	0.84	0.704	1.04	0.675	0.97	1.30	0.933	No
4198	41.98	2.49	1.06	1.43	0.84	0.704	1.04	0.675	0.97	1.30	0.933	No
4199	41.99	2.49	1.06	1.43	0.84	0.704	1.04	0.675	0.97	1.30	0.933	No
4200	42.00	2.49	1.06	1.43	0.84	0.704	1.04	0.675	0.97	1.30	0.933	No
4201	42.01	2.49	1.06	1.43	0.84	0.704	1.04	0.675	0.97	1.30	0.933	No
4202	42.02	2.49	1.06	1.43	0.84	0.704	1.04	0.675	0.97	1.30	0.933	No
4203	42.03	2.49	1.06	1.43	0.84	0.704	1.04	0.675	0.97	1.30	0.933	No
4204	42.04	2.49	1.06	1.43	0.84	0.704	1.04	0.675	0.97	1.30	0.933	No
4205	42.05	2.49	1.06	1.43	0.84	0.704	1.04	0.675	0.97	1.30	0.933	No
4206	42.06	2.50	1.06	1.43	0.84	0.704	1.04	0.675	0.97	1.30	0.933	No
4207	42.07	2.50	1.06	1.43	0.84	0.704	1.04	0.675	0.97	1.30	0.933	No
4208	42.08	2.50	1.06	1.43	0.84	0.704	1.04	0.675	0.97	1.30	0.933	No
4209	42.09	2.50	1.06	1.43	0.84	0.704	1.04	0.675	0.97	1.30	0.933	No
4210	42.10	2.50	1.06	1.43	0.84	0.704	1.04	0.675	0.97	1.30	0.933	No
4211	42.11	2.50	1.06	1.43	0.84	0.704	1.04	0.675	0.97	1.30	0.933	No
4212	42.12	2.50	1.06	1.43	0.84	0.704	1.04	0.675	0.97	1.30	0.933	No
4213	42.13	2.50	1.06	1.43	0.84	0.704	1.04	0.675	0.97	1.30	0.933	No
4214	42.14	2.50	1.07	1.44	0.84	0.704	1.04	0.675	0.97	1.30	0.933	No
4215	42.15	2.50	1.07	1.44	0.84	0.704	1.04	0.675	0.97	1.30	0.933	No
4216	42.16	2.50	1.07	1.44	0.84	0.704	1.04	0.675	0.97	1.30	0.933	No
4217	42.17	2.50	1.07	1.44	0.84	0.704	1.04	0.675	0.96	1.30	0.933	No
4218	42.18	2.50	1.07	1.44	0.84	0.704	1.04	0.675	0.96	1.30	0.933	No
4219	42.19	2.50	1.07	1.44	0.84	0.704	1.04	0.675	0.96	1.30	0.932	No
4220	42.20	2.50	1.07	1.44	0.84	0.704	1.04	0.675	0.96	1.30	0.932	No
4221	42.21	2.50	1.07	1.44	0.84	0.704	1.04	0.675	0.96	1.30	0.932	No
4222	42.22	2.51	1.07	1.44	0.84	0.704	1.04	0.675	0.96	1.30	0.932	No
4223	42.23	2.51	1.07	1.44	0.84	0.704	1.04	0.675	0.96	1.30	0.932	No
4224	42.24	2.51	1.07	1.44	0.84	0.704	1.04	0.675	0.96	1.30	0.932	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
4225	42.25	2.51	1.07	1.44	0.84	0.704	1.04	0.675	0.96	1.30	0.932	No
4226	42.26	2.51	1.07	1.44	0.84	0.704	1.04	0.675	0.96	1.30	0.932	No
4227	42.27	2.51	1.07	1.44	0.84	0.704	1.04	0.675	0.96	1.30	0.932	No
4228	42.28	2.51	1.07	1.44	0.84	0.704	1.04	0.675	0.96	1.30	0.932	No
4229	42.29	2.51	1.07	1.44	0.84	0.704	1.04	0.675	0.96	1.30	0.932	No
4230	42.30	2.51	1.07	1.44	0.84	0.704	1.04	0.675	0.96	1.30	0.932	No
4231	42.31	2.51	1.07	1.44	0.84	0.704	1.04	0.675	0.96	1.30	0.932	No
4232	42.32	2.51	1.07	1.44	0.84	0.704	1.04	0.675	0.96	1.30	0.932	No
4233	42.33	2.51	1.07	1.44	0.84	0.704	1.04	0.675	0.96	1.30	0.932	No
4234	42.34	2.51	1.07	1.44	0.84	0.704	1.04	0.674	0.96	1.30	0.932	No
4235	42.35	2.51	1.07	1.44	0.84	0.704	1.04	0.674	0.96	1.30	0.932	No
4236	42.36	2.51	1.07	1.44	0.84	0.704	1.04	0.674	0.96	1.30	0.932	No
4237	42.37	2.52	1.07	1.44	0.84	0.704	1.04	0.674	0.96	1.30	0.932	No
4238	42.38	2.52	1.07	1.44	0.84	0.704	1.04	0.674	0.96	1.30	0.932	No
4239	42.39	2.52	1.07	1.44	0.84	0.704	1.04	0.674	0.96	1.30	0.932	No
4240	42.40	2.52	1.07	1.44	0.84	0.704	1.04	0.674	0.96	1.30	0.932	No
4241	42.41	2.52	1.07	1.44	0.84	0.704	1.04	0.674	0.96	1.30	0.932	No
4242	42.42	2.52	1.07	1.44	0.84	0.704	1.04	0.674	0.96	1.30	0.932	No
4243	42.43	2.52	1.07	1.44	0.84	0.704	1.04	0.674	0.96	1.30	0.932	No
4244	42.44	2.52	1.07	1.44	0.84	0.704	1.04	0.674	0.96	1.30	0.932	No
4245	42.45	2.52	1.07	1.45	0.84	0.703	1.04	0.674	0.96	1.30	0.932	No
4246	42.46	2.52	1.08	1.45	0.84	0.703	1.04	0.674	0.96	1.30	0.932	No
4247	42.47	2.52	1.08	1.45	0.84	0.703	1.04	0.674	0.96	1.30	0.932	No
4248	42.48	2.52	1.08	1.45	0.84	0.703	1.04	0.674	0.96	1.30	0.932	No
4249	42.49	2.52	1.08	1.45	0.84	0.703	1.04	0.674	0.96	1.30	0.932	No
4250	42.50	2.52	1.08	1.45	0.84	0.703	1.04	0.674	0.96	1.30	0.932	No
4251	42.51	2.52	1.08	1.45	0.84	0.703	1.04	0.674	0.96	1.30	0.932	No
4252	42.52	2.52	1.08	1.45	0.84	0.703	1.04	0.674	0.96	1.30	0.932	No
4253	42.53	2.53	1.08	1.45	0.84	0.703	1.04	0.674	0.96	1.30	0.932	No
4254	42.54	2.53	1.08	1.45	0.84	0.703	1.04	0.674	0.96	1.30	0.932	No
4255	42.55	2.53	1.08	1.45	0.84	0.703	1.04	0.674	0.96	1.30	0.932	No
4256	42.56	2.53	1.08	1.45	0.84	0.703	1.04	0.674	0.96	1.30	0.932	No
4257	42.57	2.53	1.08	1.45	0.84	0.703	1.04	0.674	0.96	1.30	0.932	No
4258	42.58	2.53	1.08	1.45	0.84	0.703	1.04	0.674	0.96	1.30	0.932	No
4259	42.59	2.53	1.08	1.45	0.84	0.703	1.04	0.674	0.96	1.30	0.932	No
4260	42.60	2.53	1.08	1.45	0.84	0.703	1.04	0.674	0.96	1.30	0.933	No
4261	42.61	2.53	1.08	1.45	0.84	0.703	1.04	0.674	0.96	1.30	0.933	No
4262	42.62	2.53	1.08	1.45	0.84	0.703	1.04	0.674	0.96	1.30	0.933	No
4263	42.63	2.53	1.08	1.45	0.84	0.703	1.04	0.674	0.96	1.30	0.933	No
4264	42.64	2.53	1.08	1.45	0.84	0.703	1.04	0.674	0.96	1.30	0.933	No
4265	42.65	2.53	1.08	1.45	0.84	0.703	1.04	0.674	0.97	1.30	0.933	No
4266	42.66	2.53	1.08	1.45	0.84	0.703	1.04	0.674	0.97	1.30	0.933	No
4267	42.67	2.53	1.08	1.45	0.84	0.703	1.04	0.674	0.97	1.30	0.933	No
4268	42.68	2.53	1.08	1.45	0.84	0.703	1.04	0.674	0.97	1.30	0.933	No
4269	42.69	2.54	1.08	1.45	0.84	0.703	1.04	0.674	0.97	1.30	0.933	No
4270	42.70	2.54	1.08	1.45	0.84	0.703	1.04	0.674	0.97	1.30	0.933	No
4271	42.71	2.54	1.08	1.45	0.84	0.703	1.04	0.674	0.97	1.30	0.933	No
4272	42.72	2.54	1.08	1.45	0.84	0.703	1.04	0.674	0.97	1.30	0.933	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
4273	42.73	2.54	1.08	1.45	0.84	0.703	1.04	0.674	0.97	1.30	0.933	No
4274	42.74	2.54	1.08	1.45	0.84	0.703	1.04	0.674	0.97	1.30	0.933	No
4275	42.75	2.54	1.08	1.45	0.84	0.703	1.04	0.674	0.97	1.30	0.933	No
4276	42.76	2.54	1.08	1.46	0.84	0.703	1.04	0.674	0.97	1.30	0.933	No
4277	42.77	2.54	1.08	1.46	0.84	0.703	1.04	0.674	0.97	1.30	0.933	No
4278	42.78	2.54	1.09	1.46	0.84	0.703	1.04	0.674	0.97	1.30	0.933	No
4279	42.79	2.54	1.09	1.46	0.84	0.703	1.04	0.674	0.97	1.30	0.933	No
4280	42.80	2.54	1.09	1.46	0.84	0.703	1.04	0.674	0.97	1.30	0.933	No
4281	42.81	2.54	1.09	1.46	0.84	0.703	1.04	0.674	0.97	1.30	0.933	No
4282	42.82	2.54	1.09	1.46	0.84	0.703	1.04	0.674	0.97	1.30	0.933	No
4283	42.83	2.54	1.09	1.46	0.84	0.703	1.04	0.674	0.97	1.30	0.933	No
4284	42.84	2.54	1.09	1.46	0.84	0.703	1.04	0.674	0.97	1.30	0.933	No
4285	42.85	2.55	1.09	1.46	0.84	0.703	1.04	0.674	0.97	1.30	0.933	No
4286	42.86	2.55	1.09	1.46	0.84	0.703	1.04	0.674	0.97	1.30	0.933	No
4287	42.87	2.55	1.09	1.46	0.84	0.703	1.04	0.674	0.97	1.30	0.933	No
4288	42.88	2.55	1.09	1.46	0.84	0.703	1.04	0.673	0.97	1.30	0.933	No
4289	42.89	2.55	1.09	1.46	0.84	0.703	1.04	0.673	0.96	1.30	0.933	No
4290	42.90	2.55	1.09	1.46	0.84	0.703	1.04	0.673	0.96	1.30	0.933	No
4291	42.91	2.55	1.09	1.46	0.84	0.703	1.04	0.673	0.96	1.30	0.933	No
4292	42.92	2.55	1.09	1.46	0.84	0.703	1.04	0.673	0.96	1.30	0.933	No
4293	42.93	2.55	1.09	1.46	0.84	0.703	1.04	0.673	0.96	1.30	0.933	No
4294	42.94	2.55	1.09	1.46	0.84	0.703	1.04	0.673	0.96	1.30	0.932	No
4295	42.95	2.55	1.09	1.46	0.84	0.703	1.04	0.673	0.96	1.30	0.932	No
4296	42.96	2.55	1.09	1.46	0.84	0.703	1.04	0.673	0.96	1.30	0.932	No
4297	42.97	2.55	1.09	1.46	0.84	0.702	1.04	0.673	0.96	1.30	0.932	No
4298	42.98	2.55	1.09	1.46	0.84	0.702	1.04	0.673	0.96	1.30	0.932	No
4299	42.99	2.55	1.09	1.46	0.84	0.702	1.04	0.673	0.96	1.30	0.932	No
4300	43.00	2.55	1.09	1.46	0.84	0.702	1.04	0.673	0.96	1.30	0.932	No
4301	43.01	2.56	1.09	1.46	0.84	0.702	1.04	0.673	0.96	1.30	0.932	No
4302	43.02	2.56	1.09	1.46	0.84	0.702	1.04	0.673	0.96	1.30	0.932	No
4303	43.03	2.56	1.09	1.46	0.84	0.702	1.04	0.673	0.96	1.30	0.932	No
4304	43.04	2.56	1.09	1.46	0.84	0.702	1.04	0.673	0.96	1.30	0.932	No
4305	43.05	2.56	1.09	1.46	0.84	0.702	1.04	0.673	0.96	1.30	0.932	No
4306	43.06	2.56	1.09	1.46	0.84	0.702	1.04	0.673	0.96	1.30	0.932	No
4307	43.07	2.56	1.09	1.46	0.84	0.702	1.04	0.673	0.96	1.30	0.932	No
4308	43.08	2.56	1.09	1.46	0.84	0.702	1.04	0.673	0.96	1.30	0.932	No
4309	43.09	2.56	1.09	1.47	0.84	0.702	1.04	0.673	0.96	1.30	0.932	No
4310	43.10	2.56	1.10	1.47	0.84	0.702	1.04	0.673	0.96	1.30	0.932	No
4311	43.11	2.56	1.10	1.47	0.84	0.702	1.04	0.673	0.96	1.30	0.932	No
4312	43.12	2.56	1.10	1.47	0.84	0.702	1.04	0.673	0.96	1.30	0.932	No
4313	43.13	2.56	1.10	1.47	0.84	0.702	1.04	0.673	0.96	1.30	0.932	No
4314	43.14	2.56	1.10	1.47	0.84	0.702	1.04	0.673	0.96	1.30	0.932	No
4315	43.15	2.56	1.10	1.47	0.84	0.702	1.04	0.673	0.96	1.30	0.932	No
4316	43.16	2.56	1.10	1.47	0.84	0.702	1.04	0.673	0.96	1.30	0.932	No
4317	43.17	2.57	1.10	1.47	0.84	0.702	1.04	0.673	0.96	1.30	0.932	No
4318	43.18	2.57	1.10	1.47	0.84	0.702	1.04	0.673	0.96	1.30	0.932	No
4319	43.19	2.57	1.10	1.47	0.84	0.702	1.04	0.673	0.96	1.30	0.932	No
4320	43.20	2.57	1.10	1.47	0.84	0.702	1.04	0.673	0.96	1.30	0.932	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
4321	43.21	2.57	1.10	1.47	0.84	0.702	1.04	0.673	0.96	1.30	0.932	No
4322	43.22	2.57	1.10	1.47	0.84	0.702	1.04	0.673	0.96	1.30	0.932	No
4323	43.23	2.57	1.10	1.47	0.83	0.702	1.04	0.673	0.96	1.30	0.932	No
4324	43.24	2.57	1.10	1.47	0.83	0.702	1.04	0.673	0.96	1.30	0.932	No
4325	43.25	2.57	1.10	1.47	0.83	0.702	1.04	0.673	0.96	1.30	0.932	No
4326	43.26	2.57	1.10	1.47	0.83	0.702	1.04	0.673	0.96	1.30	0.932	No
4327	43.27	2.57	1.10	1.47	0.83	0.702	1.04	0.673	0.96	1.30	0.932	No
4328	43.28	2.57	1.10	1.47	0.83	0.702	1.04	0.673	0.96	1.30	0.932	No
4329	43.29	2.57	1.10	1.47	0.83	0.702	1.04	0.673	0.96	1.30	0.932	No
4330	43.30	2.57	1.10	1.47	0.83	0.702	1.04	0.673	0.96	1.30	0.932	No
4331	43.31	2.57	1.10	1.47	0.83	0.702	1.04	0.673	0.96	1.30	0.932	No
4332	43.32	2.57	1.10	1.47	0.83	0.702	1.04	0.673	0.96	1.30	0.932	No
4333	43.33	2.58	1.10	1.47	0.83	0.702	1.04	0.673	0.96	1.30	0.932	No
4334	43.34	2.58	1.10	1.47	0.83	0.702	1.04	0.673	0.96	1.30	2.000	Yes
4335	43.35	2.58	1.10	1.47	0.83	0.702	1.04	0.673	0.96	1.30	2.000	Yes
4336	43.36	2.58	1.10	1.47	0.83	0.702	1.04	0.673	0.96	1.30	2.000	Yes
4337	43.37	2.58	1.10	1.47	0.83	0.702	1.04	0.673	0.96	1.30	2.000	Yes
4338	43.38	2.58	1.10	1.47	0.83	0.702	1.04	0.672	0.96	1.30	2.000	Yes
4339	43.39	2.58	1.10	1.47	0.83	0.702	1.04	0.672	0.96	1.30	2.000	Yes
4340	43.40	2.58	1.10	1.48	0.83	0.702	1.04	0.672	0.96	1.30	2.000	Yes
4341	43.41	2.58	1.10	1.48	0.83	0.702	1.04	0.672	0.96	1.30	2.000	Yes
4342	43.42	2.58	1.11	1.48	0.83	0.702	1.04	0.672	0.96	1.30	2.000	Yes
4343	43.43	2.58	1.11	1.48	0.83	0.702	1.04	0.672	0.96	1.30	2.000	Yes
4344	43.44	2.58	1.11	1.48	0.83	0.702	1.04	0.672	0.96	1.30	2.000	Yes
4345	43.45	2.58	1.11	1.48	0.83	0.701	1.04	0.672	0.96	1.30	2.000	Yes
4346	43.46	2.58	1.11	1.48	0.83	0.701	1.04	0.672	0.96	1.30	2.000	Yes
4347	43.47	2.58	1.11	1.48	0.83	0.701	1.04	0.672	0.96	1.30	2.000	Yes
4348	43.48	2.58	1.11	1.48	0.83	0.701	1.04	0.672	0.96	1.30	2.000	Yes
4349	43.49	2.59	1.11	1.48	0.83	0.701	1.04	0.672	0.96	1.30	2.000	Yes
4350	43.50	2.59	1.11	1.48	0.83	0.701	1.04	0.672	0.96	1.30	2.000	Yes
4351	43.51	2.59	1.11	1.48	0.83	0.701	1.04	0.672	0.96	1.30	2.000	Yes
4352	43.52	2.59	1.11	1.48	0.83	0.701	1.04	0.672	0.96	1.30	2.000	Yes
4353	43.53	2.59	1.11	1.48	0.83	0.701	1.04	0.672	0.96	1.30	2.000	Yes
4354	43.54	2.59	1.11	1.48	0.83	0.701	1.04	0.672	0.96	1.30	2.000	Yes
4355	43.55	2.59	1.11	1.48	0.83	0.701	1.04	0.672	0.96	1.30	2.000	Yes
4356	43.56	2.59	1.11	1.48	0.83	0.701	1.04	0.672	0.96	1.30	2.000	Yes
4357	43.57	2.59	1.11	1.48	0.83	0.701	1.04	0.672	0.96	1.30	2.000	Yes
4358	43.58	2.59	1.11	1.48	0.83	0.701	1.04	0.672	0.96	1.30	2.000	Yes
4359	43.59	2.59	1.11	1.48	0.83	0.701	1.04	0.672	0.96	1.30	2.000	Yes
4360	43.60	2.59	1.11	1.48	0.83	0.701	1.04	0.672	0.96	1.30	2.000	Yes
4361	43.61	2.59	1.11	1.48	0.83	0.701	1.04	0.672	0.96	1.30	0.932	No
4362	43.62	2.59	1.11	1.48	0.83	0.701	1.04	0.672	0.96	1.30	0.932	No
4363	43.63	2.59	1.11	1.48	0.83	0.701	1.04	0.672	0.96	1.30	0.932	No
4364	43.64	2.59	1.11	1.48	0.83	0.701	1.04	0.672	0.96	1.30	0.932	No
4365	43.65	2.60	1.11	1.48	0.83	0.701	1.04	0.672	0.96	1.30	0.932	No
4366	43.66	2.60	1.11	1.48	0.83	0.701	1.04	0.672	0.96	1.30	0.932	No
4367	43.67	2.60	1.11	1.48	0.83	0.701	1.04	0.672	0.96	1.30	0.932	No
4368	43.68	2.60	1.11	1.48	0.83	0.701	1.04	0.672	0.96	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
4369	43.69	2.60	1.11	1.48	0.83	0.701	1.04	0.672	0.96	1.30	2.000	Yes
4370	43.70	2.60	1.11	1.48	0.83	0.701	1.04	0.672	0.96	1.30	2.000	Yes
4371	43.71	2.60	1.11	1.49	0.83	0.701	1.04	0.672	0.96	1.30	2.000	Yes
4372	43.72	2.60	1.11	1.49	0.83	0.701	1.04	0.672	0.96	1.30	2.000	Yes
4373	43.73	2.60	1.11	1.49	0.83	0.701	1.04	0.672	0.96	1.30	2.000	Yes
4374	43.74	2.60	1.12	1.49	0.83	0.701	1.04	0.672	0.96	1.30	2.000	Yes
4375	43.75	2.60	1.12	1.49	0.83	0.701	1.04	0.672	0.96	1.30	2.000	Yes
4376	43.76	2.60	1.12	1.49	0.83	0.701	1.04	0.672	0.96	1.30	2.000	Yes
4377	43.77	2.60	1.12	1.49	0.83	0.701	1.04	0.672	0.96	1.30	2.000	Yes
4378	43.78	2.60	1.12	1.49	0.83	0.701	1.04	0.672	0.96	1.30	2.000	Yes
4379	43.79	2.60	1.12	1.49	0.83	0.701	1.04	0.672	0.96	1.30	2.000	Yes
4380	43.80	2.61	1.12	1.49	0.83	0.701	1.04	0.672	0.96	1.30	2.000	Yes
4381	43.81	2.61	1.12	1.49	0.83	0.701	1.04	0.672	0.96	1.30	2.000	Yes
4382	43.82	2.61	1.12	1.49	0.83	0.701	1.04	0.672	0.96	1.30	2.000	Yes
4383	43.83	2.61	1.12	1.49	0.83	0.701	1.04	0.672	0.96	1.30	2.000	Yes
4384	43.84	2.61	1.12	1.49	0.83	0.701	1.04	0.672	0.96	1.30	2.000	Yes
4385	43.85	2.61	1.12	1.49	0.83	0.701	1.04	0.672	0.96	1.30	2.000	Yes
4386	43.86	2.61	1.12	1.49	0.83	0.701	1.04	0.671	0.96	1.30	2.000	Yes
4387	43.87	2.61	1.12	1.49	0.83	0.701	1.04	0.671	0.96	1.30	2.000	Yes
4388	43.88	2.61	1.12	1.49	0.83	0.701	1.04	0.671	0.96	1.30	2.000	Yes
4389	43.89	2.61	1.12	1.49	0.83	0.701	1.04	0.671	0.96	1.30	2.000	Yes
4390	43.90	2.61	1.12	1.49	0.83	0.700	1.04	0.671	0.96	1.30	2.000	Yes
4391	43.91	2.61	1.12	1.49	0.83	0.700	1.04	0.671	0.96	1.30	2.000	Yes
4392	43.92	2.61	1.12	1.49	0.83	0.700	1.04	0.671	0.96	1.30	2.000	Yes
4393	43.93	2.61	1.12	1.49	0.83	0.700	1.04	0.671	0.96	1.30	2.000	Yes
4394	43.94	2.61	1.12	1.49	0.83	0.700	1.04	0.671	0.96	1.30	2.000	Yes
4395	43.95	2.61	1.12	1.49	0.83	0.700	1.04	0.671	0.96	1.30	2.000	Yes
4396	43.96	2.62	1.12	1.49	0.83	0.700	1.04	0.671	0.96	1.30	2.000	Yes
4397	43.97	2.62	1.12	1.49	0.83	0.700	1.04	0.671	0.96	1.30	2.000	Yes
4398	43.98	2.62	1.12	1.49	0.83	0.700	1.04	0.671	0.96	1.30	2.000	Yes
4399	43.99	2.62	1.12	1.49	0.83	0.700	1.04	0.671	0.96	1.30	2.000	Yes
4400	44.00	2.62	1.12	1.49	0.83	0.700	1.04	0.671	0.96	1.30	2.000	Yes
4401	44.01	2.62	1.12	1.49	0.83	0.700	1.04	0.671	0.96	1.30	2.000	Yes
4402	44.02	2.62	1.12	1.50	0.83	0.700	1.04	0.671	0.96	1.30	2.000	Yes
4403	44.03	2.62	1.12	1.50	0.83	0.700	1.04	0.671	0.96	1.30	2.000	Yes
4404	44.04	2.62	1.12	1.50	0.83	0.700	1.04	0.671	0.96	1.30	2.000	Yes
4405	44.05	2.62	1.12	1.50	0.83	0.700	1.04	0.671	0.96	1.30	0.932	No
4406	44.06	2.62	1.13	1.50	0.83	0.700	1.04	0.671	0.96	1.30	0.932	No
4407	44.07	2.62	1.13	1.50	0.83	0.700	1.04	0.671	0.96	1.30	0.932	No
4408	44.08	2.62	1.13	1.50	0.83	0.700	1.04	0.671	0.96	1.30	0.932	No
4409	44.09	2.62	1.13	1.50	0.83	0.700	1.04	0.671	0.96	1.30	0.932	No
4410	44.10	2.62	1.13	1.50	0.83	0.700	1.04	0.671	0.96	1.30	0.932	No
4411	44.11	2.62	1.13	1.50	0.83	0.700	1.04	0.671	0.96	1.30	0.932	No
4412	44.12	2.63	1.13	1.50	0.83	0.700	1.04	0.671	0.96	1.30	0.932	No
4413	44.13	2.63	1.13	1.50	0.83	0.700	1.04	0.671	0.96	1.30	2.000	Yes
4414	44.14	2.63	1.13	1.50	0.83	0.700	1.04	0.671	0.96	1.30	2.000	Yes
4415	44.15	2.63	1.13	1.50	0.83	0.700	1.04	0.671	0.96	1.30	2.000	Yes
4416	44.16	2.63	1.13	1.50	0.83	0.700	1.04	0.671	0.96	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
4417	44.17	2.63	1.13	1.50	0.83	0.700	1.04	0.671	0.96	1.30	2.000	Yes
4418	44.18	2.63	1.13	1.50	0.83	0.700	1.04	0.671	0.96	1.30	2.000	Yes
4419	44.19	2.63	1.13	1.50	0.83	0.700	1.04	0.671	0.96	1.30	2.000	Yes
4420	44.20	2.63	1.13	1.50	0.83	0.700	1.04	0.671	0.96	1.30	2.000	Yes
4421	44.21	2.63	1.13	1.50	0.83	0.700	1.04	0.671	0.96	1.30	2.000	Yes
4422	44.22	2.63	1.13	1.50	0.83	0.700	1.04	0.671	0.96	1.30	2.000	Yes
4423	44.23	2.63	1.13	1.50	0.83	0.700	1.04	0.671	0.96	1.30	2.000	Yes
4424	44.24	2.63	1.13	1.50	0.83	0.700	1.04	0.671	0.96	1.30	2.000	Yes
4425	44.25	2.63	1.13	1.50	0.83	0.700	1.04	0.671	0.96	1.30	2.000	Yes
4426	44.26	2.63	1.13	1.50	0.83	0.700	1.04	0.671	0.96	1.30	2.000	Yes
4427	44.27	2.64	1.13	1.50	0.83	0.700	1.04	0.671	0.96	1.30	2.000	Yes
4428	44.28	2.64	1.13	1.50	0.83	0.700	1.04	0.671	0.96	1.30	2.000	Yes
4429	44.29	2.64	1.13	1.50	0.83	0.700	1.04	0.671	0.96	1.30	2.000	Yes
4430	44.30	2.64	1.13	1.50	0.83	0.700	1.04	0.670	0.96	1.30	2.000	Yes
4431	44.31	2.64	1.13	1.50	0.83	0.700	1.04	0.670	0.96	1.30	2.000	Yes
4432	44.32	2.64	1.13	1.51	0.83	0.699	1.04	0.670	0.95	1.30	2.000	Yes
4433	44.33	2.64	1.13	1.51	0.83	0.699	1.04	0.670	0.95	1.30	2.000	Yes
4434	44.34	2.64	1.13	1.51	0.83	0.699	1.04	0.670	0.95	1.30	2.000	Yes
4435	44.35	2.64	1.13	1.51	0.83	0.699	1.04	0.670	0.95	1.30	2.000	Yes
4436	44.36	2.64	1.13	1.51	0.83	0.699	1.04	0.670	0.95	1.30	2.000	Yes
4437	44.37	2.64	1.13	1.51	0.83	0.699	1.04	0.670	0.95	1.30	2.000	Yes
4438	44.38	2.64	1.14	1.51	0.83	0.699	1.04	0.670	0.95	1.30	2.000	Yes
4439	44.39	2.64	1.14	1.51	0.83	0.699	1.04	0.670	0.95	1.30	2.000	Yes
4440	44.40	2.64	1.14	1.51	0.83	0.699	1.04	0.670	0.95	1.30	2.000	Yes
4441	44.41	2.64	1.14	1.51	0.83	0.699	1.04	0.670	0.95	1.30	2.000	Yes
4442	44.42	2.64	1.14	1.51	0.83	0.699	1.04	0.670	0.95	1.30	2.000	Yes
4443	44.43	2.65	1.14	1.51	0.83	0.699	1.04	0.670	0.95	1.30	2.000	Yes
4444	44.44	2.65	1.14	1.51	0.83	0.699	1.04	0.670	0.95	1.30	2.000	Yes
4445	44.45	2.65	1.14	1.51	0.83	0.699	1.04	0.670	0.95	1.30	2.000	Yes
4446	44.46	2.65	1.14	1.51	0.83	0.699	1.04	0.670	0.95	1.30	2.000	Yes
4447	44.47	2.65	1.14	1.51	0.83	0.699	1.04	0.670	0.94	1.30	2.000	Yes
4448	44.48	2.65	1.14	1.51	0.83	0.699	1.04	0.670	0.94	1.30	2.000	Yes
4449	44.49	2.65	1.14	1.51	0.83	0.699	1.04	0.670	0.94	1.30	2.000	Yes
4450	44.50	2.65	1.14	1.51	0.83	0.699	1.04	0.670	0.94	1.30	2.000	Yes
4451	44.51	2.65	1.14	1.51	0.83	0.699	1.04	0.670	0.94	1.30	2.000	Yes
4452	44.52	2.65	1.14	1.51	0.83	0.699	1.04	0.670	0.94	1.30	2.000	Yes
4453	44.53	2.65	1.14	1.51	0.83	0.699	1.04	0.670	0.94	1.30	2.000	Yes
4454	44.54	2.65	1.14	1.51	0.83	0.699	1.04	0.670	0.94	1.30	2.000	Yes
4455	44.55	2.65	1.14	1.51	0.83	0.699	1.04	0.670	0.94	1.30	2.000	Yes
4456	44.56	2.65	1.14	1.51	0.83	0.699	1.04	0.670	0.94	1.30	2.000	Yes
4457	44.57	2.65	1.14	1.51	0.83	0.699	1.04	0.670	0.94	1.30	2.000	Yes
4458	44.58	2.66	1.14	1.51	0.83	0.699	1.04	0.670	0.94	1.30	2.000	Yes
4459	44.59	2.66	1.14	1.51	0.83	0.699	1.04	0.670	0.94	1.30	2.000	Yes
4460	44.60	2.66	1.14	1.51	0.83	0.699	1.04	0.670	0.94	1.30	2.000	Yes
4461	44.61	2.66	1.14	1.51	0.83	0.699	1.04	0.670	0.94	1.30	2.000	Yes
4462	44.62	2.66	1.14	1.52	0.83	0.699	1.04	0.670	0.94	1.30	2.000	Yes
4463	44.63	2.66	1.14	1.52	0.83	0.699	1.04	0.670	0.94	1.30	2.000	Yes
4464	44.64	2.66	1.14	1.52	0.83	0.699	1.04	0.670	0.94	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
4465	44.65	2.66	1.14	1.52	0.83	0.699	1.04	0.670	0.94	1.30	2.000	Yes
4466	44.66	2.66	1.14	1.52	0.83	0.699	1.04	0.670	0.94	1.30	2.000	Yes
4467	44.67	2.66	1.14	1.52	0.83	0.699	1.04	0.670	0.94	1.30	2.000	Yes
4468	44.68	2.66	1.14	1.52	0.83	0.699	1.04	0.670	0.94	1.30	2.000	Yes
4469	44.69	2.66	1.14	1.52	0.83	0.699	1.04	0.670	0.94	1.30	2.000	Yes
4470	44.70	2.66	1.15	1.52	0.83	0.698	1.04	0.669	0.94	1.30	2.000	Yes
4471	44.71	2.66	1.15	1.52	0.83	0.698	1.04	0.669	0.94	1.30	2.000	Yes
4472	44.72	2.66	1.15	1.52	0.83	0.698	1.04	0.669	0.94	1.30	2.000	Yes
4473	44.73	2.66	1.15	1.52	0.83	0.698	1.04	0.669	0.94	1.30	2.000	Yes
4474	44.74	2.67	1.15	1.52	0.83	0.698	1.04	0.669	0.94	1.30	2.000	Yes
4475	44.75	2.67	1.15	1.52	0.83	0.698	1.04	0.669	0.94	1.30	2.000	Yes
4476	44.76	2.67	1.15	1.52	0.83	0.698	1.04	0.669	0.94	1.30	2.000	Yes
4477	44.77	2.67	1.15	1.52	0.83	0.698	1.04	0.669	0.94	1.30	2.000	Yes
4478	44.78	2.67	1.15	1.52	0.83	0.698	1.04	0.669	0.93	1.30	2.000	Yes
4479	44.79	2.67	1.15	1.52	0.83	0.698	1.04	0.669	0.93	1.30	2.000	Yes
4480	44.80	2.67	1.15	1.52	0.83	0.698	1.04	0.669	0.93	1.30	2.000	Yes
4481	44.81	2.67	1.15	1.52	0.83	0.698	1.04	0.669	0.93	1.30	0.929	No
4482	44.82	2.67	1.15	1.52	0.83	0.698	1.04	0.669	0.93	1.30	0.929	No
4483	44.83	2.67	1.15	1.52	0.83	0.698	1.04	0.669	0.93	1.30	0.929	No
4484	44.84	2.67	1.15	1.52	0.83	0.698	1.04	0.669	0.93	1.30	0.929	No
4485	44.85	2.67	1.15	1.52	0.83	0.698	1.04	0.669	0.93	1.30	0.929	No
4486	44.86	2.67	1.15	1.52	0.83	0.698	1.04	0.669	0.93	1.30	0.929	No
4487	44.87	2.67	1.15	1.52	0.83	0.698	1.04	0.669	0.93	1.30	0.929	No
4488	44.88	2.67	1.15	1.52	0.83	0.698	1.04	0.669	0.93	1.30	0.929	No
4489	44.89	2.68	1.15	1.52	0.83	0.698	1.04	0.669	0.94	1.30	0.929	No
4490	44.90	2.68	1.15	1.52	0.83	0.698	1.04	0.669	0.94	1.30	0.929	No
4491	44.91	2.68	1.15	1.53	0.83	0.698	1.04	0.669	0.94	1.30	0.929	No
4492	44.92	2.68	1.15	1.53	0.83	0.698	1.04	0.669	0.94	1.30	0.929	No
4493	44.93	2.68	1.15	1.53	0.83	0.698	1.04	0.669	0.94	1.30	0.929	No
4494	44.94	2.68	1.15	1.53	0.83	0.698	1.04	0.669	0.94	1.30	0.929	No
4495	44.95	2.68	1.15	1.53	0.83	0.698	1.04	0.669	0.94	1.30	0.929	No
4496	44.96	2.68	1.15	1.53	0.83	0.698	1.04	0.669	0.94	1.30	0.929	No
4497	44.97	2.68	1.15	1.53	0.83	0.698	1.04	0.669	0.94	1.30	0.929	No
4498	44.98	2.68	1.15	1.53	0.83	0.698	1.04	0.669	0.94	1.30	0.929	No
4499	44.99	2.68	1.15	1.53	0.83	0.698	1.04	0.669	0.94	1.30	0.930	No
4500	45.00	2.68	1.15	1.53	0.83	0.698	1.04	0.669	0.94	1.30	0.930	No
4501	45.01	2.68	1.15	1.53	0.83	0.698	1.04	0.669	0.94	1.30	0.930	No
4502	45.02	2.68	1.16	1.53	0.83	0.698	1.04	0.669	0.94	1.30	0.930	No
4503	45.03	2.68	1.16	1.53	0.83	0.698	1.04	0.669	0.94	1.30	0.930	No
4504	45.04	2.69	1.16	1.53	0.83	0.698	1.04	0.669	0.94	1.30	0.930	No
4505	45.05	2.69	1.16	1.53	0.83	0.698	1.04	0.669	0.94	1.30	0.930	No
4506	45.06	2.69	1.16	1.53	0.83	0.698	1.04	0.669	0.94	1.30	0.930	No
4507	45.07	2.69	1.16	1.53	0.83	0.698	1.04	0.669	0.94	1.30	0.930	No
4508	45.08	2.69	1.16	1.53	0.83	0.698	1.04	0.669	0.94	1.30	2.000	Yes
4509	45.09	2.69	1.16	1.53	0.83	0.697	1.04	0.669	0.94	1.30	2.000	Yes
4510	45.10	2.69	1.16	1.53	0.83	0.697	1.04	0.668	0.94	1.30	2.000	Yes
4511	45.11	2.69	1.16	1.53	0.83	0.697	1.04	0.668	0.94	1.30	2.000	Yes
4512	45.12	2.69	1.16	1.53	0.83	0.697	1.04	0.668	0.94	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
4513	45.13	2.69	1.16	1.53	0.83	0.697	1.04	0.668	0.94	1.30	2.000	Yes
4514	45.14	2.69	1.16	1.53	0.83	0.697	1.04	0.668	0.94	1.30	2.000	Yes
4515	45.15	2.69	1.16	1.53	0.83	0.697	1.04	0.668	0.94	1.30	2.000	Yes
4516	45.16	2.69	1.16	1.53	0.83	0.697	1.04	0.668	0.94	1.30	2.000	Yes
4517	45.17	2.69	1.16	1.53	0.83	0.697	1.04	0.668	0.94	1.30	2.000	Yes
4518	45.18	2.69	1.16	1.53	0.83	0.697	1.04	0.668	0.94	1.30	2.000	Yes
4519	45.19	2.69	1.16	1.53	0.83	0.697	1.04	0.668	0.94	1.30	2.000	Yes
4520	45.20	2.70	1.16	1.53	0.83	0.697	1.04	0.668	0.94	1.30	2.000	Yes
4521	45.21	2.70	1.16	1.54	0.83	0.697	1.04	0.668	0.94	1.30	2.000	Yes
4522	45.22	2.70	1.16	1.54	0.83	0.697	1.04	0.668	0.94	1.30	2.000	Yes
4523	45.23	2.70	1.16	1.54	0.83	0.697	1.04	0.668	0.94	1.30	2.000	Yes
4524	45.24	2.70	1.16	1.54	0.83	0.697	1.04	0.668	0.94	1.30	2.000	Yes
4525	45.25	2.70	1.16	1.54	0.83	0.697	1.04	0.668	0.94	1.30	2.000	Yes
4526	45.26	2.70	1.16	1.54	0.83	0.697	1.04	0.668	0.94	1.30	2.000	Yes
4527	45.27	2.70	1.16	1.54	0.82	0.697	1.04	0.668	0.94	1.30	2.000	Yes
4528	45.28	2.70	1.16	1.54	0.82	0.697	1.04	0.668	0.94	1.30	2.000	Yes
4529	45.29	2.70	1.16	1.54	0.82	0.697	1.04	0.668	0.94	1.30	2.000	Yes
4530	45.30	2.70	1.16	1.54	0.82	0.697	1.04	0.668	0.94	1.30	2.000	Yes
4531	45.31	2.70	1.16	1.54	0.82	0.697	1.04	0.668	0.94	1.30	2.000	Yes
4532	45.32	2.70	1.16	1.54	0.82	0.697	1.04	0.668	0.94	1.30	2.000	Yes
4533	45.33	2.70	1.16	1.54	0.82	0.697	1.04	0.668	0.94	1.30	2.000	Yes
4534	45.34	2.70	1.17	1.54	0.82	0.697	1.04	0.668	0.94	1.30	0.930	No
4535	45.35	2.71	1.17	1.54	0.82	0.697	1.04	0.668	0.94	1.30	0.930	No
4536	45.36	2.71	1.17	1.54	0.82	0.697	1.04	0.668	0.94	1.30	0.930	No
4537	45.37	2.71	1.17	1.54	0.82	0.697	1.04	0.668	0.94	1.30	0.930	No
4538	45.38	2.71	1.17	1.54	0.82	0.697	1.04	0.668	0.94	1.30	0.930	No
4539	45.39	2.71	1.17	1.54	0.82	0.697	1.04	0.668	0.94	1.30	0.930	No
4540	45.40	2.71	1.17	1.54	0.82	0.697	1.04	0.668	0.94	1.30	0.930	No
4541	45.41	2.71	1.17	1.54	0.82	0.697	1.04	0.668	0.94	1.30	0.930	No
4542	45.42	2.71	1.17	1.54	0.82	0.697	1.04	0.668	0.94	1.30	0.930	No
4543	45.43	2.71	1.17	1.54	0.82	0.697	1.04	0.668	0.94	1.30	0.930	No
4544	45.44	2.71	1.17	1.54	0.82	0.697	1.04	0.668	0.94	1.30	0.930	No
4545	45.45	2.71	1.17	1.54	0.82	0.697	1.04	0.668	0.94	1.30	0.930	No
4546	45.46	2.71	1.17	1.54	0.82	0.696	1.04	0.668	0.94	1.30	0.930	No
4547	45.47	2.71	1.17	1.54	0.82	0.696	1.04	0.668	0.94	1.30	0.930	No
4548	45.48	2.71	1.17	1.54	0.82	0.696	1.04	0.668	0.94	1.30	0.930	No
4549	45.49	2.71	1.17	1.54	0.82	0.696	1.04	0.667	0.94	1.30	0.930	No
4550	45.50	2.71	1.17	1.54	0.82	0.696	1.04	0.667	0.94	1.30	2.000	Yes
4551	45.51	2.72	1.17	1.55	0.82	0.696	1.04	0.667	0.94	1.30	2.000	Yes
4552	45.52	2.72	1.17	1.55	0.82	0.696	1.04	0.667	0.94	1.30	2.000	Yes
4553	45.53	2.72	1.17	1.55	0.82	0.696	1.04	0.667	0.94	1.30	2.000	Yes
4554	45.54	2.72	1.17	1.55	0.82	0.696	1.04	0.667	0.94	1.30	2.000	Yes
4555	45.55	2.72	1.17	1.55	0.82	0.696	1.04	0.667	0.94	1.30	2.000	Yes
4556	45.56	2.72	1.17	1.55	0.82	0.696	1.04	0.667	0.94	1.30	2.000	Yes
4557	45.57	2.72	1.17	1.55	0.82	0.696	1.04	0.667	0.94	1.30	2.000	Yes
4558	45.58	2.72	1.17	1.55	0.82	0.696	1.04	0.667	0.94	1.30	2.000	Yes
4559	45.59	2.72	1.17	1.55	0.82	0.696	1.04	0.667	0.94	1.30	2.000	Yes
4560	45.60	2.72	1.17	1.55	0.82	0.696	1.04	0.667	0.94	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
4561	45.61	2.72	1.17	1.55	0.82	0.696	1.04	0.667	0.94	1.30	2.000	Yes
4562	45.62	2.72	1.17	1.55	0.82	0.696	1.04	0.667	0.94	1.30	2.000	Yes
4563	45.63	2.72	1.17	1.55	0.82	0.696	1.04	0.667	0.94	1.30	2.000	Yes
4564	45.64	2.72	1.17	1.55	0.82	0.696	1.04	0.667	0.94	1.30	2.000	Yes
4565	45.65	2.72	1.17	1.55	0.82	0.696	1.04	0.667	0.93	1.30	2.000	Yes
4566	45.66	2.73	1.17	1.55	0.82	0.696	1.04	0.667	0.93	1.30	2.000	Yes
4567	45.67	2.73	1.18	1.55	0.82	0.696	1.04	0.667	0.93	1.30	2.000	Yes
4568	45.68	2.73	1.18	1.55	0.82	0.696	1.04	0.667	0.93	1.30	2.000	Yes
4569	45.69	2.73	1.18	1.55	0.82	0.696	1.04	0.667	0.93	1.30	2.000	Yes
4570	45.70	2.73	1.18	1.55	0.82	0.696	1.04	0.667	0.93	1.30	2.000	Yes
4571	45.71	2.73	1.18	1.55	0.82	0.696	1.04	0.667	0.93	1.30	2.000	Yes
4572	45.72	2.73	1.18	1.55	0.82	0.696	1.04	0.667	0.93	1.30	2.000	Yes
4573	45.73	2.73	1.18	1.55	0.82	0.696	1.04	0.667	0.93	1.30	2.000	Yes
4574	45.74	2.73	1.18	1.55	0.82	0.696	1.04	0.667	0.93	1.30	2.000	Yes
4575	45.75	2.73	1.18	1.55	0.82	0.696	1.04	0.667	0.93	1.30	2.000	Yes
4576	45.76	2.73	1.18	1.55	0.82	0.696	1.04	0.667	0.93	1.30	2.000	Yes
4577	45.77	2.73	1.18	1.55	0.82	0.696	1.04	0.667	0.93	1.30	0.930	No
4578	45.78	2.73	1.18	1.55	0.82	0.696	1.04	0.667	0.93	1.30	0.930	No
4579	45.79	2.73	1.18	1.55	0.82	0.696	1.04	0.667	0.93	1.30	0.930	No
4580	45.80	2.73	1.18	1.56	0.82	0.696	1.04	0.667	0.93	1.30	0.930	No
4581	45.81	2.74	1.18	1.56	0.82	0.696	1.04	0.667	0.93	1.30	0.930	No
4582	45.82	2.74	1.18	1.56	0.82	0.696	1.04	0.667	0.93	1.30	0.930	No
4583	45.83	2.74	1.18	1.56	0.82	0.695	1.04	0.667	0.93	1.30	0.930	No
4584	45.84	2.74	1.18	1.56	0.82	0.695	1.04	0.667	0.93	1.30	0.930	No
4585	45.85	2.74	1.18	1.56	0.82	0.695	1.04	0.667	0.93	1.30	0.930	No
4586	45.86	2.74	1.18	1.56	0.82	0.695	1.04	0.667	0.93	1.30	0.930	No
4587	45.87	2.74	1.18	1.56	0.82	0.695	1.04	0.667	0.93	1.30	0.930	No
4588	45.88	2.74	1.18	1.56	0.82	0.695	1.04	0.666	0.93	1.30	0.930	No
4589	45.89	2.74	1.18	1.56	0.82	0.695	1.04	0.666	0.93	1.30	0.930	No
4590	45.90	2.74	1.18	1.56	0.82	0.695	1.04	0.666	0.93	1.30	0.930	No
4591	45.91	2.74	1.18	1.56	0.82	0.695	1.04	0.666	0.93	1.30	0.930	No
4592	45.92	2.74	1.18	1.56	0.82	0.695	1.04	0.666	0.93	1.30	0.930	No
4593	45.93	2.74	1.18	1.56	0.82	0.695	1.04	0.666	0.93	1.30	0.930	No
4594	45.94	2.74	1.18	1.56	0.82	0.695	1.04	0.666	0.93	1.30	0.930	No
4595	45.95	2.74	1.18	1.56	0.82	0.695	1.04	0.666	0.93	1.30	0.930	No
4596	45.96	2.74	1.18	1.56	0.82	0.695	1.04	0.666	0.93	1.30	0.930	No
4597	45.97	2.75	1.18	1.56	0.82	0.695	1.04	0.666	0.93	1.30	0.930	No
4598	45.98	2.75	1.18	1.56	0.82	0.695	1.04	0.666	0.93	1.30	0.930	No
4599	45.99	2.75	1.19	1.56	0.82	0.695	1.04	0.666	0.93	1.30	0.930	No
4600	46.00	2.75	1.19	1.56	0.82	0.695	1.04	0.666	0.93	1.30	0.930	No
4601	46.01	2.75	1.19	1.56	0.82	0.695	1.04	0.666	0.93	1.30	0.930	No
4602	46.02	2.75	1.19	1.56	0.82	0.695	1.04	0.666	0.93	1.30	0.930	No
4603	46.03	2.75	1.19	1.56	0.82	0.695	1.04	0.666	0.93	1.30	0.930	No
4604	46.04	2.75	1.19	1.56	0.82	0.695	1.04	0.666	0.93	1.30	0.930	No
4605	46.05	2.75	1.19	1.56	0.82	0.695	1.04	0.666	0.93	1.30	0.930	No
4606	46.06	2.75	1.19	1.56	0.82	0.695	1.04	0.666	0.93	1.30	0.930	No
4607	46.07	2.75	1.19	1.56	0.82	0.695	1.04	0.666	0.93	1.30	0.930	No
4608	46.08	2.75	1.19	1.56	0.82	0.695	1.04	0.666	0.92	1.30	0.930	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
4609	46.09	2.75	1.19	1.56	0.82	0.695	1.04	0.666	0.92	1.30	0.930	No
4610	46.10	2.75	1.19	1.57	0.82	0.695	1.04	0.666	0.92	1.30	0.930	No
4611	46.11	2.75	1.19	1.57	0.82	0.695	1.04	0.666	0.92	1.30	0.930	No
4612	46.12	2.76	1.19	1.57	0.82	0.695	1.04	0.666	0.92	1.30	0.930	No
4613	46.13	2.76	1.19	1.57	0.82	0.695	1.04	0.666	0.92	1.30	0.930	No
4614	46.14	2.76	1.19	1.57	0.82	0.695	1.04	0.666	0.92	1.30	0.930	No
4615	46.15	2.76	1.19	1.57	0.82	0.695	1.04	0.666	0.92	1.30	0.930	No
4616	46.16	2.76	1.19	1.57	0.82	0.695	1.04	0.666	0.92	1.30	0.930	No
4617	46.17	2.76	1.19	1.57	0.82	0.695	1.04	0.666	0.92	1.30	0.930	No
4618	46.18	2.76	1.19	1.57	0.82	0.695	1.04	0.666	0.92	1.30	0.930	No
4619	46.19	2.76	1.19	1.57	0.82	0.695	1.04	0.666	0.92	1.30	0.930	No
4620	46.20	2.76	1.19	1.57	0.82	0.695	1.04	0.666	0.92	1.30	0.930	No
4621	46.21	2.76	1.19	1.57	0.82	0.694	1.04	0.666	0.92	1.30	0.930	No
4622	46.22	2.76	1.19	1.57	0.82	0.694	1.04	0.666	0.91	1.30	0.930	No
4623	46.23	2.76	1.19	1.57	0.82	0.694	1.04	0.666	0.91	1.30	0.930	No
4624	46.24	2.76	1.19	1.57	0.82	0.694	1.04	0.666	0.91	1.30	0.931	No
4625	46.25	2.76	1.19	1.57	0.82	0.694	1.04	0.666	0.91	1.30	0.931	No
4626	46.26	2.76	1.19	1.57	0.82	0.694	1.04	0.666	0.91	1.30	0.931	No
4627	46.27	2.76	1.19	1.57	0.82	0.694	1.04	0.665	0.91	1.30	0.932	No
4628	46.28	2.77	1.19	1.57	0.82	0.694	1.04	0.665	0.91	1.30	0.933	No
4629	46.29	2.77	1.19	1.57	0.82	0.694	1.04	0.665	0.91	1.30	0.933	No
4630	46.30	2.77	1.19	1.57	0.82	0.694	1.04	0.665	0.91	1.30	0.932	No
4631	46.31	2.77	1.20	1.57	0.82	0.694	1.04	0.665	0.91	1.30	0.932	No
4632	46.32	2.77	1.20	1.57	0.82	0.694	1.04	0.665	0.91	1.30	0.931	No
4633	46.33	2.77	1.20	1.57	0.82	0.694	1.04	0.665	0.91	1.30	0.931	No
4634	46.34	2.77	1.20	1.57	0.82	0.694	1.04	0.665	0.91	1.30	0.931	No
4635	46.35	2.77	1.20	1.57	0.82	0.694	1.04	0.665	0.91	1.30	0.931	No
4636	46.36	2.77	1.20	1.57	0.82	0.694	1.04	0.665	0.91	1.30	0.931	No
4637	46.37	2.77	1.20	1.57	0.82	0.694	1.04	0.665	0.91	1.30	0.931	No
4638	46.38	2.77	1.20	1.57	0.82	0.694	1.04	0.665	0.91	1.30	0.931	No
4639	46.39	2.77	1.20	1.57	0.82	0.694	1.04	0.665	0.91	1.30	0.931	No
4640	46.40	2.77	1.20	1.58	0.82	0.694	1.04	0.665	0.91	1.30	0.931	No
4641	46.41	2.77	1.20	1.58	0.82	0.694	1.04	0.665	0.91	1.30	0.930	No
4642	46.42	2.77	1.20	1.58	0.82	0.694	1.04	0.665	0.91	1.30	0.930	No
4643	46.43	2.78	1.20	1.58	0.82	0.694	1.04	0.665	0.91	1.30	0.930	No
4644	46.44	2.78	1.20	1.58	0.82	0.694	1.04	0.665	0.92	1.30	0.930	No
4645	46.45	2.78	1.20	1.58	0.82	0.694	1.04	0.665	0.92	1.30	2.000	Yes
4646	46.46	2.78	1.20	1.58	0.82	0.694	1.04	0.665	0.92	1.30	2.000	Yes
4647	46.47	2.78	1.20	1.58	0.82	0.694	1.04	0.665	0.92	1.30	2.000	Yes
4648	46.48	2.78	1.20	1.58	0.82	0.694	1.04	0.665	0.92	1.30	2.000	Yes
4649	46.49	2.78	1.20	1.58	0.82	0.694	1.04	0.665	0.92	1.30	2.000	Yes
4650	46.50	2.78	1.20	1.58	0.82	0.694	1.04	0.665	0.92	1.30	2.000	Yes
4651	46.51	2.78	1.20	1.58	0.82	0.694	1.04	0.665	0.92	1.30	2.000	Yes
4652	46.52	2.78	1.20	1.58	0.82	0.694	1.04	0.665	0.92	1.30	2.000	Yes
4653	46.53	2.78	1.20	1.58	0.82	0.694	1.04	0.665	0.92	1.30	2.000	Yes
4654	46.54	2.78	1.20	1.58	0.82	0.694	1.04	0.665	0.92	1.30	2.000	Yes
4655	46.55	2.78	1.20	1.58	0.82	0.694	1.04	0.665	0.92	1.30	2.000	Yes
4656	46.56	2.78	1.20	1.58	0.82	0.693	1.04	0.665	0.92	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
4657	46.57	2.78	1.20	1.58	0.82	0.693	1.04	0.665	0.92	1.30	2.000	Yes
4658	46.58	2.79	1.20	1.58	0.82	0.693	1.04	0.665	0.92	1.30	2.000	Yes
4659	46.59	2.79	1.20	1.58	0.82	0.693	1.04	0.665	0.92	1.30	2.000	Yes
4660	46.60	2.79	1.20	1.58	0.82	0.693	1.04	0.665	0.93	1.30	2.000	Yes
4661	46.61	2.79	1.20	1.58	0.82	0.693	1.04	0.665	0.93	1.30	2.000	Yes
4662	46.62	2.79	1.20	1.58	0.82	0.693	1.04	0.665	0.93	1.30	2.000	Yes
4663	46.63	2.79	1.21	1.58	0.82	0.693	1.04	0.664	0.93	1.30	2.000	Yes
4664	46.64	2.79	1.21	1.58	0.82	0.693	1.04	0.664	0.93	1.30	2.000	Yes
4665	46.65	2.79	1.21	1.58	0.82	0.693	1.04	0.664	0.93	1.30	2.000	Yes
4666	46.66	2.79	1.21	1.58	0.82	0.693	1.04	0.664	0.93	1.30	2.000	Yes
4667	46.67	2.79	1.21	1.58	0.82	0.693	1.04	0.664	0.93	1.30	2.000	Yes
4668	46.68	2.79	1.21	1.58	0.82	0.693	1.04	0.664	0.93	1.30	2.000	Yes
4669	46.69	2.79	1.21	1.59	0.82	0.693	1.04	0.664	0.93	1.30	2.000	Yes
4670	46.70	2.79	1.21	1.59	0.82	0.693	1.04	0.664	0.93	1.30	2.000	Yes
4671	46.71	2.79	1.21	1.59	0.82	0.693	1.04	0.664	0.93	1.30	2.000	Yes
4672	46.72	2.79	1.21	1.59	0.82	0.693	1.04	0.664	0.94	1.30	2.000	Yes
4673	46.73	2.79	1.21	1.59	0.82	0.693	1.04	0.664	0.94	1.30	2.000	Yes
4674	46.74	2.80	1.21	1.59	0.82	0.693	1.04	0.664	0.94	1.30	2.000	Yes
4675	46.75	2.80	1.21	1.59	0.82	0.693	1.04	0.664	0.94	1.30	2.000	Yes
4676	46.76	2.80	1.21	1.59	0.82	0.693	1.04	0.664	0.94	1.30	2.000	Yes
4677	46.77	2.80	1.21	1.59	0.82	0.693	1.04	0.664	0.94	1.30	2.000	Yes
4678	46.78	2.80	1.21	1.59	0.82	0.693	1.04	0.664	0.94	1.30	2.000	Yes
4679	46.79	2.80	1.21	1.59	0.82	0.693	1.04	0.664	0.94	1.30	2.000	Yes
4680	46.80	2.80	1.21	1.59	0.82	0.693	1.04	0.664	0.94	1.30	2.000	Yes
4681	46.81	2.80	1.21	1.59	0.82	0.693	1.04	0.664	0.94	1.30	2.000	Yes
4682	46.82	2.80	1.21	1.59	0.82	0.693	1.04	0.664	0.94	1.30	2.000	Yes
4683	46.83	2.80	1.21	1.59	0.82	0.693	1.04	0.664	0.94	1.30	2.000	Yes
4684	46.84	2.80	1.21	1.59	0.82	0.693	1.04	0.664	0.94	1.30	2.000	Yes
4685	46.85	2.80	1.21	1.59	0.82	0.693	1.04	0.664	0.94	1.30	2.000	Yes
4686	46.86	2.80	1.21	1.59	0.82	0.693	1.04	0.664	0.94	1.30	2.000	Yes
4687	46.87	2.80	1.21	1.59	0.82	0.693	1.04	0.664	0.94	1.30	2.000	Yes
4688	46.88	2.80	1.21	1.59	0.82	0.693	1.04	0.664	0.95	1.30	2.000	Yes
4689	46.89	2.81	1.21	1.59	0.82	0.693	1.04	0.664	0.95	1.30	2.000	Yes
4690	46.90	2.81	1.21	1.59	0.82	0.693	1.04	0.664	0.95	1.30	2.000	Yes
4691	46.91	2.81	1.21	1.59	0.82	0.693	1.04	0.664	0.95	1.30	2.000	Yes
4692	46.92	2.81	1.21	1.59	0.82	0.692	1.04	0.664	0.95	1.30	2.000	Yes
4693	46.93	2.81	1.21	1.59	0.82	0.692	1.04	0.664	0.95	1.30	2.000	Yes
4694	46.94	2.81	1.21	1.59	0.82	0.692	1.04	0.664	0.95	1.30	2.000	Yes
4695	46.95	2.81	1.22	1.59	0.82	0.692	1.04	0.664	0.95	1.30	2.000	Yes
4696	46.96	2.81	1.22	1.59	0.82	0.692	1.04	0.664	0.95	1.30	2.000	Yes
4697	46.97	2.81	1.22	1.59	0.82	0.692	1.04	0.664	0.95	1.30	2.000	Yes
4698	46.98	2.81	1.22	1.59	0.82	0.692	1.04	0.664	0.95	1.30	2.000	Yes
4699	46.99	2.81	1.22	1.60	0.82	0.692	1.04	0.664	0.95	1.30	2.000	Yes
4700	47.00	2.81	1.22	1.60	0.82	0.692	1.04	0.664	0.95	1.30	2.000	Yes
4701	47.01	2.81	1.22	1.60	0.82	0.692	1.04	0.663	0.95	1.30	2.000	Yes
4702	47.02	2.81	1.22	1.60	0.82	0.692	1.04	0.663	0.95	1.30	2.000	Yes
4703	47.03	2.81	1.22	1.60	0.82	0.692	1.04	0.663	0.95	1.30	2.000	Yes
4704	47.04	2.81	1.22	1.60	0.82	0.692	1.04	0.663	0.95	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
4705	47.05	2.82	1.22	1.60	0.82	0.692	1.04	0.663	0.95	1.30	2.000	Yes
4706	47.06	2.82	1.22	1.60	0.82	0.692	1.04	0.663	0.95	1.30	2.000	Yes
4707	47.07	2.82	1.22	1.60	0.82	0.692	1.04	0.663	0.95	1.30	0.928	No
4708	47.08	2.82	1.22	1.60	0.82	0.692	1.04	0.663	0.95	1.30	0.928	No
4709	47.09	2.82	1.22	1.60	0.82	0.692	1.04	0.663	0.95	1.30	0.928	No
4710	47.10	2.82	1.22	1.60	0.82	0.692	1.04	0.663	0.95	1.30	0.928	No
4711	47.11	2.82	1.22	1.60	0.82	0.692	1.04	0.663	0.95	1.30	0.928	No
4712	47.12	2.82	1.22	1.60	0.82	0.692	1.04	0.663	0.95	1.30	0.928	No
4713	47.13	2.82	1.22	1.60	0.82	0.692	1.04	0.663	0.95	1.30	0.928	No
4714	47.14	2.82	1.22	1.60	0.82	0.692	1.04	0.663	0.95	1.30	0.928	No
4715	47.15	2.82	1.22	1.60	0.82	0.692	1.04	0.663	0.95	1.30	0.928	No
4716	47.16	2.82	1.22	1.60	0.82	0.692	1.04	0.663	0.95	1.30	0.928	No
4717	47.17	2.82	1.22	1.60	0.82	0.692	1.04	0.663	0.95	1.30	0.928	No
4718	47.18	2.82	1.22	1.60	0.82	0.692	1.04	0.663	0.95	1.30	0.928	No
4719	47.19	2.82	1.22	1.60	0.82	0.692	1.04	0.663	0.95	1.30	0.928	No
4720	47.20	2.83	1.22	1.60	0.82	0.692	1.04	0.663	0.95	1.30	0.928	No
4721	47.21	2.83	1.22	1.60	0.82	0.692	1.04	0.663	0.95	1.30	0.928	No
4722	47.22	2.83	1.22	1.60	0.82	0.692	1.04	0.663	0.95	1.30	0.928	No
4723	47.23	2.83	1.22	1.60	0.82	0.692	1.04	0.663	0.95	1.30	0.928	No
4724	47.24	2.83	1.22	1.60	0.82	0.692	1.04	0.663	0.95	1.30	0.928	No
4725	47.25	2.83	1.22	1.60	0.82	0.692	1.04	0.663	0.95	1.30	0.928	No
4726	47.26	2.83	1.22	1.60	0.82	0.692	1.04	0.663	0.95	1.30	0.928	No
4727	47.27	2.83	1.23	1.60	0.82	0.692	1.04	0.663	0.95	1.30	0.928	No
4728	47.28	2.83	1.23	1.60	0.82	0.692	1.04	0.663	0.95	1.30	0.928	No
4729	47.29	2.83	1.23	1.61	0.82	0.692	1.04	0.663	0.95	1.30	0.928	No
4730	47.30	2.83	1.23	1.61	0.82	0.691	1.04	0.663	0.95	1.30	0.928	No
4731	47.31	2.83	1.23	1.61	0.82	0.691	1.04	0.663	0.95	1.30	0.928	No
4732	47.32	2.83	1.23	1.61	0.81	0.691	1.04	0.663	0.95	1.30	0.928	No
4733	47.33	2.83	1.23	1.61	0.81	0.691	1.04	0.663	0.95	1.30	0.928	No
4734	47.34	2.83	1.23	1.61	0.81	0.691	1.04	0.663	0.95	1.30	0.928	No
4735	47.35	2.83	1.23	1.61	0.81	0.691	1.04	0.663	0.95	1.30	0.928	No
4736	47.36	2.84	1.23	1.61	0.81	0.691	1.04	0.663	0.95	1.30	0.928	No
4737	47.37	2.84	1.23	1.61	0.81	0.691	1.04	0.663	0.95	1.30	0.928	No
4738	47.38	2.84	1.23	1.61	0.81	0.691	1.04	0.663	0.95	1.30	0.928	No
4739	47.39	2.84	1.23	1.61	0.81	0.691	1.04	0.663	0.95	1.30	0.928	No
4740	47.40	2.84	1.23	1.61	0.81	0.691	1.04	0.662	0.95	1.30	0.929	No
4741	47.41	2.84	1.23	1.61	0.81	0.691	1.04	0.662	0.95	1.30	0.929	No
4742	47.42	2.84	1.23	1.61	0.81	0.691	1.04	0.662	0.95	1.30	0.929	No
4743	47.43	2.84	1.23	1.61	0.81	0.691	1.04	0.662	0.95	1.30	0.929	No
4744	47.44	2.84	1.23	1.61	0.81	0.691	1.04	0.662	0.95	1.30	0.929	No
4745	47.45	2.84	1.23	1.61	0.81	0.691	1.04	0.662	0.95	1.30	0.929	No
4746	47.46	2.84	1.23	1.61	0.81	0.691	1.04	0.662	0.95	1.30	0.929	No
4747	47.47	2.84	1.23	1.61	0.81	0.691	1.04	0.662	0.95	1.30	0.929	No
4748	47.48	2.84	1.23	1.61	0.81	0.691	1.04	0.662	0.95	1.30	0.929	No
4749	47.49	2.84	1.23	1.61	0.81	0.691	1.04	0.662	0.95	1.30	0.929	No
4750	47.50	2.84	1.23	1.61	0.81	0.691	1.04	0.662	0.95	1.30	0.929	No
4751	47.51	2.85	1.23	1.61	0.81	0.691	1.04	0.662	0.95	1.30	0.929	No
4752	47.52	2.85	1.23	1.61	0.81	0.691	1.04	0.662	0.95	1.30	0.929	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
4753	47.53	2.85	1.23	1.61	0.81	0.691	1.04	0.662	0.95	1.30	0.929	No
4754	47.54	2.85	1.23	1.61	0.81	0.691	1.04	0.662	0.95	1.30	0.929	No
4755	47.55	2.85	1.23	1.61	0.81	0.691	1.04	0.662	0.95	1.30	0.929	No
4756	47.56	2.85	1.23	1.61	0.81	0.691	1.04	0.662	0.95	1.30	0.929	No
4757	47.57	2.85	1.23	1.61	0.81	0.691	1.04	0.662	0.95	1.30	0.929	No
4758	47.58	2.85	1.23	1.61	0.81	0.691	1.04	0.662	0.95	1.30	0.928	No
4759	47.59	2.85	1.24	1.61	0.81	0.691	1.04	0.662	0.95	1.30	0.928	No
4760	47.60	2.85	1.24	1.62	0.81	0.691	1.04	0.662	0.95	1.30	0.928	No
4761	47.61	2.85	1.24	1.62	0.81	0.691	1.04	0.662	0.95	1.30	0.928	No
4762	47.62	2.85	1.24	1.62	0.81	0.691	1.04	0.662	0.95	1.30	0.928	No
4763	47.63	2.85	1.24	1.62	0.81	0.691	1.04	0.662	0.95	1.30	0.928	No
4764	47.64	2.85	1.24	1.62	0.81	0.691	1.04	0.662	0.95	1.30	0.928	No
4765	47.65	2.85	1.24	1.62	0.81	0.691	1.04	0.662	0.95	1.30	0.928	No
4766	47.66	2.85	1.24	1.62	0.81	0.691	1.04	0.662	0.95	1.30	0.928	No
4767	47.67	2.86	1.24	1.62	0.81	0.691	1.04	0.662	0.95	1.30	0.928	No
4768	47.68	2.86	1.24	1.62	0.81	0.690	1.04	0.662	0.95	1.30	0.928	No
4769	47.69	2.86	1.24	1.62	0.81	0.690	1.04	0.662	0.95	1.30	0.928	No
4770	47.70	2.86	1.24	1.62	0.81	0.690	1.04	0.662	0.95	1.30	0.928	No
4771	47.71	2.86	1.24	1.62	0.81	0.690	1.04	0.662	0.95	1.30	0.928	No
4772	47.72	2.86	1.24	1.62	0.81	0.690	1.04	0.662	0.95	1.30	0.928	No
4773	47.73	2.86	1.24	1.62	0.81	0.690	1.04	0.662	0.95	1.30	0.928	No
4774	47.74	2.86	1.24	1.62	0.81	0.690	1.04	0.662	0.95	1.30	0.928	No
4775	47.75	2.86	1.24	1.62	0.81	0.690	1.04	0.662	0.95	1.30	0.928	No
4776	47.76	2.86	1.24	1.62	0.81	0.690	1.04	0.662	0.95	1.30	0.928	No
4777	47.77	2.86	1.24	1.62	0.81	0.690	1.04	0.662	0.95	1.30	0.928	No
4778	47.78	2.86	1.24	1.62	0.81	0.690	1.04	0.662	0.95	1.30	0.928	No
4779	47.79	2.86	1.24	1.62	0.81	0.690	1.04	0.662	0.95	1.30	0.928	No
4780	47.80	2.86	1.24	1.62	0.81	0.690	1.04	0.662	0.95	1.30	0.928	No
4781	47.81	2.86	1.24	1.62	0.81	0.690	1.04	0.661	0.95	1.30	0.928	No
4782	47.82	2.86	1.24	1.62	0.81	0.690	1.04	0.661	0.95	1.30	0.928	No
4783	47.83	2.87	1.24	1.62	0.81	0.690	1.04	0.661	0.95	1.30	0.928	No
4784	47.84	2.87	1.24	1.62	0.81	0.690	1.04	0.661	0.94	1.30	0.928	No
4785	47.85	2.87	1.24	1.62	0.81	0.690	1.04	0.661	0.95	1.30	0.928	No
4786	47.86	2.87	1.24	1.62	0.81	0.690	1.04	0.661	0.95	1.30	0.928	No
4787	47.87	2.87	1.24	1.62	0.81	0.690	1.04	0.661	0.95	1.30	0.928	No
4788	47.88	2.87	1.24	1.62	0.81	0.690	1.04	0.661	0.95	1.30	0.928	No
4789	47.89	2.87	1.24	1.62	0.81	0.690	1.04	0.661	0.95	1.30	0.928	No
4790	47.90	2.87	1.24	1.62	0.81	0.690	1.04	0.661	0.95	1.30	0.928	No
4791	47.91	2.87	1.25	1.63	0.81	0.690	1.04	0.661	0.95	1.30	0.928	No
4792	47.92	2.87	1.25	1.63	0.81	0.690	1.04	0.661	0.95	1.30	0.928	No
4793	47.93	2.87	1.25	1.63	0.81	0.690	1.04	0.661	0.95	1.30	0.928	No
4794	47.94	2.87	1.25	1.63	0.81	0.690	1.04	0.661	0.95	1.30	0.928	No
4795	47.95	2.87	1.25	1.63	0.81	0.690	1.04	0.661	0.95	1.30	0.928	No
4796	47.96	2.87	1.25	1.63	0.81	0.690	1.04	0.661	0.95	1.30	0.928	No
4797	47.97	2.87	1.25	1.63	0.81	0.690	1.04	0.661	0.95	1.30	0.928	No
4798	47.98	2.87	1.25	1.63	0.81	0.690	1.04	0.661	0.95	1.30	0.928	No
4799	47.99	2.88	1.25	1.63	0.81	0.690	1.04	0.661	0.95	1.30	0.928	No
4800	48.00	2.88	1.25	1.63	0.81	0.690	1.04	0.661	0.95	1.30	0.928	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
4801	48.01	2.88	1.25	1.63	0.81	0.690	1.04	0.661	0.95	1.30	0.928	No
4802	48.02	2.88	1.25	1.63	0.81	0.690	1.04	0.661	0.95	1.30	0.928	No
4803	48.03	2.88	1.25	1.63	0.81	0.690	1.04	0.661	0.95	1.30	0.928	No
4804	48.04	2.88	1.25	1.63	0.81	0.690	1.04	0.661	0.95	1.30	0.928	No
4805	48.05	2.88	1.25	1.63	0.81	0.690	1.04	0.661	0.95	1.30	0.928	No
4806	48.06	2.88	1.25	1.63	0.81	0.690	1.04	0.661	0.95	1.30	0.928	No
4807	48.07	2.88	1.25	1.63	0.81	0.690	1.04	0.661	0.95	1.30	0.928	No
4808	48.08	2.88	1.25	1.63	0.81	0.689	1.04	0.661	0.95	1.30	0.928	No
4809	48.09	2.88	1.25	1.63	0.81	0.689	1.04	0.661	0.95	1.30	0.928	No
4810	48.10	2.88	1.25	1.63	0.81	0.689	1.04	0.661	0.95	1.30	0.927	No
4811	48.11	2.88	1.25	1.63	0.81	0.689	1.04	0.661	0.95	1.30	0.927	No
4812	48.12	2.88	1.25	1.63	0.81	0.689	1.04	0.661	0.95	1.30	0.927	No
4813	48.13	2.88	1.25	1.63	0.81	0.689	1.04	0.661	0.95	1.30	0.927	No
4814	48.14	2.88	1.25	1.63	0.81	0.689	1.04	0.661	0.95	1.30	0.927	No
4815	48.15	2.89	1.25	1.63	0.81	0.689	1.04	0.661	0.95	1.30	0.927	No
4816	48.16	2.89	1.25	1.63	0.81	0.689	1.04	0.661	0.95	1.30	0.927	No
4817	48.17	2.89	1.25	1.63	0.81	0.689	1.04	0.661	0.95	1.30	0.927	No
4818	48.18	2.89	1.25	1.63	0.81	0.689	1.04	0.661	0.95	1.30	0.927	No
4819	48.19	2.89	1.25	1.63	0.81	0.689	1.04	0.661	0.95	1.30	0.927	No
4820	48.20	2.89	1.25	1.63	0.81	0.689	1.04	0.661	0.95	1.30	0.927	No
4821	48.21	2.89	1.25	1.63	0.81	0.689	1.04	0.661	0.95	1.30	0.927	No
4822	48.22	2.89	1.25	1.64	0.81	0.689	1.04	0.661	0.95	1.30	0.927	No
4823	48.23	2.89	1.26	1.64	0.81	0.689	1.04	0.660	0.95	1.30	0.927	No
4824	48.24	2.89	1.26	1.64	0.81	0.689	1.04	0.660	0.95	1.30	0.927	No
4825	48.25	2.89	1.26	1.64	0.81	0.689	1.04	0.660	0.95	1.30	0.927	No
4826	48.26	2.89	1.26	1.64	0.81	0.689	1.04	0.660	0.95	1.30	0.927	No
4827	48.27	2.89	1.26	1.64	0.81	0.689	1.04	0.660	0.95	1.30	2.000	Yes
4828	48.28	2.89	1.26	1.64	0.81	0.689	1.04	0.660	0.95	1.30	2.000	Yes
4829	48.29	2.89	1.26	1.64	0.81	0.689	1.04	0.660	0.95	1.30	2.000	Yes
4830	48.30	2.89	1.26	1.64	0.81	0.689	1.04	0.660	0.95	1.30	2.000	Yes
4831	48.31	2.90	1.26	1.64	0.81	0.689	1.04	0.660	0.95	1.30	2.000	Yes
4832	48.32	2.90	1.26	1.64	0.81	0.689	1.04	0.660	0.95	1.30	2.000	Yes
4833	48.33	2.90	1.26	1.64	0.81	0.689	1.04	0.660	0.95	1.30	2.000	Yes
4834	48.34	2.90	1.26	1.64	0.81	0.689	1.04	0.660	0.95	1.30	2.000	Yes
4835	48.35	2.90	1.26	1.64	0.81	0.689	1.04	0.660	0.95	1.30	2.000	Yes
4836	48.36	2.90	1.26	1.64	0.81	0.689	1.04	0.660	0.95	1.30	2.000	Yes
4837	48.37	2.90	1.26	1.64	0.81	0.689	1.04	0.660	0.95	1.30	2.000	Yes
4838	48.38	2.90	1.26	1.64	0.81	0.689	1.04	0.660	0.95	1.30	2.000	Yes
4839	48.39	2.90	1.26	1.64	0.81	0.689	1.04	0.660	0.95	1.30	2.000	Yes
4840	48.40	2.90	1.26	1.64	0.81	0.689	1.04	0.660	0.95	1.30	2.000	Yes
4841	48.41	2.90	1.26	1.64	0.81	0.689	1.04	0.660	0.95	1.30	2.000	Yes
4842	48.42	2.90	1.26	1.64	0.81	0.689	1.04	0.660	0.95	1.30	2.000	Yes
4843	48.43	2.90	1.26	1.64	0.81	0.689	1.04	0.660	0.95	1.30	2.000	Yes
4844	48.44	2.90	1.26	1.64	0.81	0.689	1.04	0.660	0.95	1.30	2.000	Yes
4845	48.45	2.90	1.26	1.64	0.81	0.689	1.04	0.660	0.95	1.30	2.000	Yes
4846	48.46	2.90	1.26	1.64	0.81	0.689	1.04	0.660	0.95	1.30	2.000	Yes
4847	48.47	2.91	1.26	1.64	0.81	0.689	1.04	0.660	0.95	1.30	2.000	Yes
4848	48.48	2.91	1.26	1.64	0.81	0.688	1.04	0.660	0.95	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
4849	48.49	2.91	1.26	1.64	0.81	0.688	1.04	0.660	0.95	1.30	2.000	Yes
4850	48.50	2.91	1.26	1.64	0.81	0.688	1.04	0.660	0.95	1.30	2.000	Yes
4851	48.51	2.91	1.26	1.64	0.81	0.688	1.04	0.660	0.95	1.30	2.000	Yes
4852	48.52	2.91	1.26	1.64	0.81	0.688	1.04	0.660	0.95	1.30	2.000	Yes
4853	48.53	2.91	1.26	1.64	0.81	0.688	1.04	0.660	0.95	1.30	2.000	Yes
4854	48.54	2.91	1.26	1.65	0.81	0.688	1.04	0.660	0.95	1.30	0.927	No
4855	48.55	2.91	1.27	1.65	0.81	0.688	1.04	0.660	0.95	1.30	0.927	No
4856	48.56	2.91	1.27	1.65	0.81	0.688	1.04	0.660	0.95	1.30	0.927	No
4857	48.57	2.91	1.27	1.65	0.81	0.688	1.04	0.660	0.95	1.30	0.927	No
4858	48.58	2.91	1.27	1.65	0.81	0.688	1.04	0.660	0.95	1.30	0.927	No
4859	48.59	2.91	1.27	1.65	0.81	0.688	1.04	0.660	0.95	1.30	0.927	No
4860	48.60	2.91	1.27	1.65	0.81	0.688	1.04	0.660	0.95	1.30	0.927	No
4861	48.61	2.91	1.27	1.65	0.81	0.688	1.04	0.660	0.95	1.30	0.927	No
4862	48.62	2.91	1.27	1.65	0.81	0.688	1.04	0.660	0.94	1.30	2.000	Yes
4863	48.63	2.92	1.27	1.65	0.81	0.688	1.04	0.660	0.94	1.30	2.000	Yes
4864	48.64	2.92	1.27	1.65	0.81	0.688	1.04	0.660	0.94	1.30	2.000	Yes
4865	48.65	2.92	1.27	1.65	0.81	0.688	1.04	0.660	0.95	1.30	2.000	Yes
4866	48.66	2.92	1.27	1.65	0.81	0.688	1.04	0.659	0.95	1.30	2.000	Yes
4867	48.67	2.92	1.27	1.65	0.81	0.688	1.04	0.659	0.95	1.30	2.000	Yes
4868	48.68	2.92	1.27	1.65	0.81	0.688	1.04	0.659	0.95	1.30	2.000	Yes
4869	48.69	2.92	1.27	1.65	0.81	0.688	1.04	0.659	0.95	1.30	2.000	Yes
4870	48.70	2.92	1.27	1.65	0.81	0.688	1.04	0.659	0.95	1.30	2.000	Yes
4871	48.71	2.92	1.27	1.65	0.81	0.688	1.04	0.659	0.95	1.30	2.000	Yes
4872	48.72	2.92	1.27	1.65	0.81	0.688	1.04	0.659	0.95	1.30	2.000	Yes
4873	48.73	2.92	1.27	1.65	0.81	0.688	1.04	0.659	0.95	1.30	2.000	Yes
4874	48.74	2.92	1.27	1.65	0.81	0.688	1.04	0.659	0.95	1.30	2.000	Yes
4875	48.75	2.92	1.27	1.65	0.81	0.688	1.04	0.659	0.95	1.30	2.000	Yes
4876	48.76	2.92	1.27	1.65	0.81	0.688	1.04	0.659	0.95	1.30	2.000	Yes
4877	48.77	2.92	1.27	1.65	0.81	0.688	1.04	0.659	0.95	1.30	2.000	Yes
4878	48.78	2.93	1.27	1.65	0.81	0.688	1.04	0.659	0.95	1.30	2.000	Yes
4879	48.79	2.93	1.27	1.65	0.81	0.688	1.04	0.659	0.95	1.30	2.000	Yes
4880	48.80	2.93	1.27	1.65	0.81	0.688	1.04	0.659	0.95	1.30	2.000	Yes
4881	48.81	2.93	1.27	1.65	0.81	0.688	1.04	0.659	0.95	1.30	2.000	Yes
4882	48.82	2.93	1.27	1.65	0.81	0.688	1.04	0.659	0.95	1.30	2.000	Yes
4883	48.83	2.93	1.27	1.65	0.81	0.688	1.04	0.659	0.95	1.30	2.000	Yes
4884	48.84	2.93	1.27	1.65	0.81	0.688	1.04	0.659	0.95	1.30	2.000	Yes
4885	48.85	2.93	1.27	1.65	0.81	0.688	1.04	0.659	0.95	1.30	2.000	Yes
4886	48.86	2.93	1.27	1.66	0.81	0.688	1.04	0.659	0.95	1.30	2.000	Yes
4887	48.87	2.93	1.28	1.66	0.81	0.687	1.04	0.659	0.95	1.30	2.000	Yes
4888	48.88	2.93	1.28	1.66	0.81	0.687	1.04	0.659	0.95	1.30	2.000	Yes
4889	48.89	2.93	1.28	1.66	0.81	0.687	1.04	0.659	0.95	1.30	2.000	Yes
4890	48.90	2.93	1.28	1.66	0.81	0.687	1.04	0.659	0.95	1.30	0.927	No
4891	48.91	2.93	1.28	1.66	0.81	0.687	1.04	0.659	0.95	1.30	0.927	No
4892	48.92	2.93	1.28	1.66	0.81	0.687	1.04	0.659	0.95	1.30	0.927	No
4893	48.93	2.93	1.28	1.66	0.81	0.687	1.04	0.659	0.95	1.30	0.926	No
4894	48.94	2.94	1.28	1.66	0.81	0.687	1.04	0.659	0.95	1.30	0.926	No
4895	48.95	2.94	1.28	1.66	0.81	0.687	1.04	0.659	0.95	1.30	0.926	No
4896	48.96	2.94	1.28	1.66	0.81	0.687	1.04	0.659	0.95	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
4897	48.97	2.94	1.28	1.66	0.81	0.687	1.04	0.659	0.95	1.30	2.000	Yes
4898	48.98	2.94	1.28	1.66	0.81	0.687	1.04	0.659	0.95	1.30	2.000	Yes
4899	48.99	2.94	1.28	1.66	0.81	0.687	1.04	0.659	0.95	1.30	2.000	Yes
4900	49.00	2.94	1.28	1.66	0.81	0.687	1.04	0.659	0.95	1.30	2.000	Yes
4901	49.01	2.94	1.28	1.66	0.81	0.687	1.04	0.659	0.94	1.30	2.000	Yes
4902	49.02	2.94	1.28	1.66	0.81	0.687	1.04	0.659	0.94	1.30	2.000	Yes
4903	49.03	2.94	1.28	1.66	0.81	0.687	1.04	0.659	0.94	1.30	2.000	Yes
4904	49.04	2.94	1.28	1.66	0.81	0.687	1.04	0.658	0.94	1.30	2.000	Yes
4905	49.05	2.94	1.28	1.66	0.81	0.687	1.04	0.658	0.94	1.30	2.000	Yes
4906	49.06	2.94	1.28	1.66	0.81	0.687	1.04	0.658	0.94	1.30	2.000	Yes
4907	49.07	2.94	1.28	1.66	0.81	0.687	1.04	0.658	0.94	1.30	2.000	Yes
4908	49.08	2.94	1.28	1.66	0.81	0.687	1.04	0.658	0.94	1.30	2.000	Yes
4909	49.09	2.94	1.28	1.66	0.81	0.687	1.04	0.658	0.94	1.30	2.000	Yes
4910	49.10	2.95	1.28	1.66	0.81	0.687	1.04	0.658	0.94	1.30	2.000	Yes
4911	49.11	2.95	1.28	1.66	0.81	0.687	1.04	0.658	0.94	1.30	2.000	Yes
4912	49.12	2.95	1.28	1.66	0.81	0.687	1.04	0.658	0.94	1.30	2.000	Yes
4913	49.13	2.95	1.28	1.66	0.81	0.687	1.04	0.658	0.93	1.30	2.000	Yes
4914	49.14	2.95	1.28	1.66	0.81	0.687	1.04	0.658	0.93	1.30	2.000	Yes
4915	49.15	2.95	1.28	1.67	0.81	0.687	1.04	0.658	0.93	1.30	2.000	Yes
4916	49.16	2.95	1.28	1.67	0.81	0.687	1.04	0.658	0.93	1.30	2.000	Yes
4917	49.17	2.95	1.28	1.67	0.81	0.687	1.04	0.658	0.93	1.30	2.000	Yes
4918	49.18	2.95	1.28	1.67	0.81	0.687	1.04	0.658	0.93	1.30	2.000	Yes
4919	49.19	2.95	1.29	1.67	0.81	0.687	1.04	0.658	0.93	1.30	2.000	Yes
4920	49.20	2.95	1.29	1.67	0.81	0.687	1.04	0.658	0.92	1.30	2.000	Yes
4921	49.21	2.95	1.29	1.67	0.81	0.687	1.04	0.658	0.92	1.30	2.000	Yes
4922	49.22	2.95	1.29	1.67	0.81	0.686	1.04	0.658	0.92	1.30	2.000	Yes
4923	49.23	2.95	1.29	1.67	0.81	0.686	1.04	0.658	0.92	1.30	2.000	Yes
4924	49.24	2.95	1.29	1.67	0.81	0.686	1.04	0.658	0.92	1.30	2.000	Yes
4925	49.25	2.96	1.29	1.67	0.81	0.686	1.04	0.658	0.92	1.30	2.000	Yes
4926	49.26	2.96	1.29	1.67	0.81	0.686	1.04	0.658	0.91	1.30	2.000	Yes
4927	49.27	2.96	1.29	1.67	0.81	0.686	1.04	0.658	0.91	1.30	2.000	Yes
4928	49.28	2.96	1.29	1.67	0.81	0.686	1.04	0.658	0.91	1.30	2.000	Yes
4929	49.29	2.96	1.29	1.67	0.81	0.686	1.04	0.658	0.91	1.30	2.000	Yes
4930	49.30	2.96	1.29	1.67	0.81	0.686	1.04	0.658	0.91	1.30	2.000	Yes
4931	49.31	2.96	1.29	1.67	0.81	0.686	1.04	0.658	0.90	1.30	2.000	Yes
4932	49.32	2.96	1.29	1.67	0.81	0.686	1.04	0.658	0.90	1.30	2.000	Yes
4933	49.33	2.96	1.29	1.67	0.81	0.686	1.04	0.658	0.90	1.30	2.000	Yes
4934	49.34	2.96	1.29	1.67	0.81	0.686	1.04	0.658	0.90	1.30	2.000	Yes
4935	49.35	2.96	1.29	1.67	0.81	0.686	1.04	0.658	0.90	1.30	2.000	Yes
4936	49.36	2.96	1.29	1.67	0.81	0.686	1.04	0.658	0.90	1.30	2.000	Yes
4937	49.37	2.96	1.29	1.67	0.80	0.686	1.04	0.658	0.90	1.30	2.000	Yes
4938	49.38	2.96	1.29	1.67	0.80	0.686	1.04	0.657	0.89	1.30	2.000	Yes
4939	49.39	2.96	1.29	1.67	0.80	0.686	1.04	0.657	0.89	1.30	2.000	Yes
4940	49.40	2.97	1.29	1.67	0.80	0.686	1.04	0.657	0.89	1.30	2.000	Yes
4941	49.41	2.97	1.29	1.67	0.80	0.686	1.04	0.657	0.89	1.30	0.940	No
4942	49.42	2.97	1.29	1.67	0.80	0.686	1.04	0.657	0.89	1.30	0.942	No
4943	49.43	2.97	1.29	1.67	0.80	0.686	1.04	0.657	0.89	1.30	0.943	No
4944	49.44	2.97	1.29	1.68	0.80	0.686	1.04	0.657	0.89	1.30	0.945	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
4945	49.45	2.97	1.29	1.68	0.80	0.686	1.04	0.657	0.88	1.30	0.946	No
4946	49.46	2.97	1.29	1.68	0.80	0.686	1.04	0.657	0.88	1.30	0.948	No
4947	49.47	2.97	1.29	1.68	0.80	0.686	1.04	0.657	0.88	1.30	0.949	No
4948	49.48	2.97	1.29	1.68	0.80	0.686	1.04	0.657	0.88	1.30	0.951	No
4949	49.49	2.97	1.29	1.68	0.80	0.686	1.04	0.657	0.88	1.30	0.951	No
4950	49.50	2.97	1.29	1.68	0.80	0.686	1.04	0.657	0.88	1.30	0.951	No
4951	49.51	2.97	1.30	1.68	0.80	0.686	1.04	0.657	0.88	1.30	0.951	No
4952	49.52	2.97	1.30	1.68	0.80	0.686	1.04	0.657	0.88	1.30	0.950	No
4953	49.53	2.97	1.30	1.68	0.80	0.685	1.04	0.657	0.88	1.30	0.950	No
4954	49.54	2.97	1.30	1.68	0.80	0.685	1.04	0.657	0.88	1.30	0.950	No
4955	49.55	2.98	1.30	1.68	0.80	0.685	1.04	0.657	0.88	1.30	0.949	No
4956	49.56	2.98	1.30	1.68	0.80	0.685	1.04	0.657	0.88	1.30	0.949	No
4957	49.57	2.98	1.30	1.68	0.80	0.685	1.04	0.657	0.88	1.30	0.949	No
4958	49.58	2.98	1.30	1.68	0.80	0.685	1.04	0.657	0.88	1.30	0.948	No
4959	49.59	2.98	1.30	1.68	0.80	0.685	1.04	0.657	0.88	1.30	0.946	No
4960	49.60	2.98	1.30	1.68	0.80	0.685	1.04	0.657	0.89	1.30	0.945	No
4961	49.61	2.98	1.30	1.68	0.80	0.685	1.04	0.657	0.89	1.30	0.943	No
4962	49.62	2.98	1.30	1.68	0.80	0.685	1.04	0.657	0.89	1.30	0.941	No
4963	49.63	2.98	1.30	1.68	0.80	0.685	1.04	0.657	0.89	1.30	0.940	No
4964	49.64	2.98	1.30	1.68	0.80	0.685	1.04	0.657	0.89	1.30	0.938	No
4965	49.65	2.98	1.30	1.68	0.80	0.685	1.04	0.657	0.89	1.30	0.937	No
4966	49.66	2.98	1.30	1.68	0.80	0.685	1.04	0.657	0.89	1.30	0.936	No
4967	49.67	2.98	1.30	1.68	0.80	0.685	1.04	0.657	0.89	1.30	0.935	No
4968	49.68	2.98	1.30	1.68	0.80	0.685	1.04	0.657	0.89	1.30	0.935	No
4969	49.69	2.98	1.30	1.68	0.80	0.685	1.04	0.657	0.89	1.30	0.934	No
4970	49.70	2.99	1.30	1.68	0.80	0.685	1.04	0.657	0.90	1.30	0.934	No
4971	49.71	2.99	1.30	1.68	0.80	0.685	1.04	0.656	0.90	1.30	0.934	No
4972	49.72	2.99	1.30	1.68	0.80	0.685	1.04	0.656	0.90	1.30	0.934	No
4973	49.73	2.99	1.30	1.69	0.80	0.685	1.04	0.656	0.90	1.30	0.934	No
4974	49.74	2.99	1.30	1.69	0.80	0.685	1.04	0.656	0.90	1.30	0.934	No
4975	49.75	2.99	1.30	1.69	0.80	0.685	1.04	0.656	0.90	1.30	0.934	No
4976	49.76	2.99	1.30	1.69	0.80	0.685	1.04	0.656	0.90	1.30	0.934	No
4977	49.77	2.99	1.30	1.69	0.80	0.685	1.04	0.656	0.90	1.30	0.934	No
4978	49.78	2.99	1.30	1.69	0.80	0.685	1.04	0.656	0.90	1.30	0.934	No
4979	49.79	2.99	1.30	1.69	0.80	0.685	1.04	0.656	0.90	1.30	0.933	No
4980	49.80	2.99	1.30	1.69	0.80	0.685	1.04	0.656	0.90	1.30	0.933	No
4981	49.81	2.99	1.30	1.69	0.80	0.685	1.04	0.656	0.90	1.30	0.933	No
4982	49.82	2.99	1.30	1.69	0.80	0.685	1.04	0.656	0.90	1.30	0.933	No
4983	49.83	2.99	1.31	1.69	0.80	0.685	1.04	0.656	0.90	1.30	0.933	No
4984	49.84	2.99	1.31	1.69	0.80	0.685	1.04	0.656	0.90	1.30	0.933	No
4985	49.85	2.99	1.31	1.69	0.80	0.685	1.04	0.656	0.90	1.30	0.933	No
4986	49.86	3.00	1.31	1.69	0.80	0.684	1.04	0.656	0.90	1.30	0.933	No
4987	49.87	3.00	1.31	1.69	0.80	0.684	1.04	0.656	0.90	1.30	0.933	No
4988	49.88	3.00	1.31	1.69	0.80	0.684	1.04	0.656	0.90	1.30	0.933	No
4989	49.89	3.00	1.31	1.69	0.80	0.684	1.04	0.656	0.90	1.30	0.932	No
4990	49.90	3.00	1.31	1.69	0.80	0.684	1.04	0.656	0.90	1.30	0.932	No
4991	49.91	3.00	1.31	1.69	0.80	0.684	1.04	0.656	0.90	1.30	0.932	No
4992	49.92	3.00	1.31	1.69	0.80	0.684	1.04	0.656	0.90	1.30	0.932	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
4993	49.93	3.00	1.31	1.69	0.80	0.684	1.04	0.656	0.90	1.30	0.932	No
4994	49.94	3.00	1.31	1.69	0.80	0.684	1.04	0.656	0.90	1.30	0.932	No
4995	49.95	3.00	1.31	1.69	0.80	0.684	1.04	0.656	0.90	1.30	0.932	No
4996	49.96	3.00	1.31	1.69	0.80	0.684	1.04	0.656	0.90	1.30	0.932	No
4997	49.97	3.00	1.31	1.69	0.80	0.684	1.04	0.656	0.91	1.30	0.932	No
4998	49.98	3.00	1.31	1.69	0.80	0.684	1.04	0.656	0.91	1.30	0.932	No
4999	49.99	3.00	1.31	1.69	0.80	0.684	1.04	0.656	0.91	1.30	0.931	No
5000	50.00	3.00	1.31	1.69	0.80	0.684	1.04	0.656	0.91	1.30	0.931	No

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
σ_v :	Total overburden pressure at test point (tsf)
u_0 :	Water pressure at test point (tsf)
σ_v' :	Effective overburden pressure based on GWT during earthquake (tsf)
r_d :	Nonlinear shear mass factor
CSR:	Cyclic Stress Ratio
MSF:	Magnitude Scaling Factor
CSR_{eq} :	CSR adjusted for M=7.5
K_σ :	Effective overburden stress factor
CSR*:	CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1	0.01	30.91	43.23	2.25	0.49	1.70	49.79	55.90	105.68	4.000	No	No	2.00
2	0.02	30.75	43.01	2.25	0.49	1.70	49.37	55.68	105.05	4.000	No	No	2.00
3	0.03	30.52	42.71	2.25	0.49	1.70	49.01	55.41	104.41	4.000	No	No	2.00
4	0.04	30.24	42.57	2.24	0.49	1.70	48.70	55.25	103.95	4.000	No	No	2.00
5	0.05	29.79	42.68	2.25	0.49	1.70	48.00	55.14	103.14	4.000	No	No	2.00
6	0.06	29.13	43.07	2.25	0.49	1.70	46.85	55.08	101.93	4.000	No	No	2.00
7	0.07	28.30	43.62	2.26	0.50	1.70	45.50	55.04	100.54	4.000	No	No	2.00
8	0.08	27.40	44.25	2.27	0.50	1.70	44.03	55.00	99.03	4.000	No	No	2.00
9	0.09	26.46	44.93	2.27	0.50	1.70	42.50	54.97	97.47	4.000	No	No	2.00
10	0.10	25.55	45.63	2.28	0.51	1.70	41.00	54.93	95.94	4.000	No	No	2.00
11	0.11	24.69	46.33	2.29	0.51	1.70	39.60	54.91	94.51	4.000	No	No	2.00
12	0.12	23.95	46.96	2.30	0.51	1.70	38.38	54.88	93.26	4.000	No	No	2.00
13	0.13	23.54	47.46	2.31	0.52	1.70	37.43	54.86	92.28	4.000	No	No	2.00
14	0.14	23.44	47.86	2.31	0.51	1.70	37.63	55.09	92.72	4.000	No	No	2.00
15	0.15	23.59	48.22	2.32	0.51	1.70	37.89	55.31	93.19	4.000	No	No	2.00
16	0.16	23.77	48.61	2.32	0.51	1.70	38.18	55.55	93.73	4.000	No	No	2.00
17	0.17	23.97	49.03	2.33	0.51	1.70	38.50	55.81	94.30	4.000	No	No	2.00
18	0.18	24.16	49.43	2.33	0.51	1.70	38.81	56.06	94.87	4.000	No	No	2.00
19	0.19	24.35	49.81	2.34	0.51	1.70	39.12	56.30	95.42	4.000	No	No	2.00
20	0.20	24.52	50.15	2.34	0.51	1.70	39.41	56.51	95.91	4.000	No	No	2.00
21	0.21	24.72	50.38	2.34	0.51	1.70	39.65	56.66	96.31	4.000	No	No	2.00
22	0.22	25.06	50.40	2.34	0.51	1.70	40.06	56.78	96.83	4.000	No	No	2.00
23	0.23	25.60	50.21	2.34	0.50	1.70	41.05	56.96	98.02	4.000	No	No	2.00
24	0.24	26.34	49.88	2.34	0.50	1.70	42.26	57.15	99.41	4.000	No	No	2.00
25	0.25	27.16	49.54	2.33	0.50	1.70	43.60	57.37	100.97	4.000	No	No	2.00
26	0.26	28.03	49.20	2.33	0.49	1.70	45.02	57.60	102.61	4.000	No	No	2.00
27	0.27	28.89	48.89	2.32	0.49	1.70	46.43	57.83	104.26	4.000	No	No	2.00
28	0.28	29.71	48.61	2.32	0.49	1.70	47.77	58.06	105.83	4.000	No	No	2.00
29	0.29	30.44	48.37	2.32	0.48	1.70	48.97	58.27	107.24	4.000	No	No	2.00
30	0.30	31.08	48.13	2.31	0.48	1.70	49.95	58.42	108.37	4.000	No	No	2.00
31	0.31	31.72	47.81	2.31	0.48	1.70	50.85	58.51	109.36	4.000	No	No	2.00
32	0.32	32.43	47.38	2.30	0.48	1.70	52.03	58.61	110.64	4.000	No	No	2.00
33	0.33	33.28	46.87	2.30	0.47	1.70	53.41	58.72	112.13	4.000	No	No	2.00
34	0.34	34.20	46.33	2.29	0.47	1.70	54.91	58.85	113.76	4.000	No	No	2.00
35	0.35	35.15	45.79	2.28	0.47	1.70	56.47	58.97	115.44	4.000	No	No	2.00
36	0.36	36.09	45.29	2.28	0.46	1.70	58.00	59.10	117.10	4.000	No	No	2.00
37	0.37	36.95	44.84	2.27	0.46	1.70	59.42	59.22	118.64	4.000	No	No	2.00
38	0.38	37.71	44.46	2.27	0.46	1.70	60.66	59.33	119.98	4.000	No	No	2.00
39	0.39	38.38	44.09	2.26	0.45	1.70	61.63	59.36	121.00	4.000	No	No	2.00
40	0.40	39.04	43.66	2.26	0.45	1.70	62.63	59.37	121.99	4.000	No	No	2.00
41	0.41	39.80	43.14	2.25	0.45	1.70	63.87	59.37	123.24	4.000	No	No	2.00
42	0.42	40.67	42.55	2.24	0.45	1.70	65.29	59.36	124.65	4.000	No	No	2.00
43	0.43	41.60	41.94	2.24	0.45	1.70	66.81	59.35	126.16	4.000	No	No	2.00
44	0.44	42.55	41.33	2.23	0.44	1.70	68.35	59.33	127.68	4.000	No	No	2.00
45	0.45	43.46	40.75	2.22	0.44	1.70	69.84	59.30	129.15	4.000	No	No	2.00
46	0.46	44.29	40.24	2.22	0.44	1.70	71.20	59.27	130.47	4.000	No	No	2.00
47	0.47	44.98	39.82	2.21	0.44	1.70	72.35	59.25	131.60	4.000	No	No	2.00
48	0.48	45.59	39.49	2.21	0.43	1.70	73.21	59.22	132.43	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
49	0.49	46.19	39.20	2.20	0.43	1.70	74.13	59.22	133.35	4.000	No	No	2.00
50	0.50	46.87	38.90	2.20	0.43	1.70	75.25	59.25	134.50	4.000	No	No	2.00
51	0.51	47.63	38.57	2.19	0.43	1.70	76.49	59.29	135.78	4.000	No	No	2.00
52	0.52	48.43	38.23	2.19	0.43	1.70	77.79	59.33	137.11	4.000	No	No	2.00
53	0.53	49.22	37.89	2.19	0.42	1.70	79.09	59.36	138.45	4.000	No	No	2.00
54	0.54	49.98	37.59	2.18	0.42	1.70	80.32	59.39	139.71	4.000	No	No	2.00
55	0.55	50.65	37.32	2.18	0.42	1.70	81.41	59.42	140.84	4.000	No	No	2.00
56	0.56	51.19	37.11	2.18	0.42	1.70	82.32	59.46	141.77	4.000	No	No	2.00
57	0.57	51.66	36.95	2.17	0.42	1.70	82.94	59.46	142.41	4.000	No	No	2.00
58	0.58	52.12	36.82	2.17	0.41	1.70	83.67	59.51	143.19	4.000	No	No	2.00
59	0.59	52.64	36.67	2.17	0.41	1.70	84.53	59.58	144.11	4.000	No	No	2.00
60	0.60	53.21	36.52	2.17	0.41	1.70	85.46	59.66	145.11	4.000	No	No	2.00
61	0.61	53.80	36.36	2.17	0.41	1.70	86.42	59.73	146.15	4.000	No	No	2.00
62	0.62	54.37	36.21	2.17	0.41	1.70	87.36	59.81	147.17	4.000	No	No	2.00
63	0.63	54.91	36.07	2.16	0.41	1.70	88.23	59.88	148.11	4.000	No	No	2.00
64	0.64	55.37	35.96	2.16	0.41	1.70	88.99	59.95	148.94	4.000	No	No	2.00
65	0.65	55.71	35.87	2.16	0.40	1.70	89.58	60.00	149.57	4.000	No	No	2.00
66	0.66	55.98	35.79	2.16	0.40	1.70	89.89	59.99	149.88	4.000	No	No	2.00
67	0.67	56.22	35.72	2.16	0.40	1.70	90.28	60.01	150.29	4.000	No	No	2.00
68	0.68	56.49	35.64	2.16	0.40	1.70	90.72	60.03	150.75	4.000	No	No	2.00
69	0.69	56.78	35.55	2.16	0.40	1.70	91.19	60.06	151.25	4.000	No	No	2.00
70	0.70	57.07	35.46	2.16	0.40	1.70	91.67	60.08	151.75	4.000	No	No	2.00
71	0.71	57.35	35.38	2.15	0.40	1.70	92.13	60.10	152.23	4.000	No	No	2.00
72	0.72	57.61	35.30	2.15	0.40	1.70	92.55	60.12	152.68	4.000	No	No	2.00
73	0.73	57.82	35.24	2.15	0.40	1.70	92.91	60.14	153.05	4.000	No	No	2.00
74	0.74	57.97	35.18	2.15	0.40	1.70	93.13	60.13	153.26	4.000	No	No	2.00
75	0.75	58.09	35.11	2.15	0.40	1.70	93.29	60.10	153.38	4.000	No	No	2.00
76	0.76	58.20	35.03	2.15	0.40	1.70	93.47	60.06	153.53	4.000	No	No	2.00
77	0.77	58.33	34.94	2.15	0.40	1.70	93.68	60.02	153.70	4.000	No	No	2.00
78	0.78	58.46	34.85	2.15	0.40	1.70	93.90	59.97	153.87	4.000	No	No	2.00
79	0.79	58.59	34.76	2.15	0.40	1.70	94.11	59.93	154.04	4.000	No	No	2.00
80	0.80	58.72	34.67	2.15	0.40	1.70	94.32	59.88	154.20	4.000	No	No	2.00
81	0.81	58.83	34.60	2.14	0.40	1.70	94.50	59.85	154.35	4.000	No	No	2.00
82	0.82	58.92	34.53	2.14	0.40	1.70	94.65	59.81	154.45	4.000	No	No	2.00
83	0.83	59.00	34.45	2.14	0.40	1.70	94.76	59.75	154.51	4.000	No	No	2.00
84	0.84	59.08	34.36	2.14	0.40	1.70	94.89	59.69	154.58	4.000	No	No	2.00
85	0.85	59.18	34.26	2.14	0.40	1.70	95.05	59.61	154.66	4.000	No	No	2.00
86	0.86	59.28	34.14	2.14	0.40	1.70	95.22	59.53	154.75	4.000	No	No	2.00
87	0.87	59.39	34.02	2.14	0.40	1.70	95.39	59.44	154.83	4.000	No	No	2.00
88	0.88	59.49	33.91	2.14	0.40	1.70	95.56	59.35	154.91	4.000	No	No	2.00
89	0.89	59.59	33.80	2.13	0.40	1.70	95.72	59.27	154.99	4.000	No	No	2.00
90	0.90	59.68	33.70	2.13	0.40	1.70	95.86	59.20	155.06	4.000	No	No	2.00
91	0.91	59.76	33.62	2.13	0.39	1.70	95.97	59.13	155.10	4.000	No	No	2.00
92	0.92	59.87	33.52	2.13	0.39	1.70	96.14	59.06	155.20	4.000	No	No	2.00
93	0.93	60.00	33.41	2.13	0.39	1.70	96.35	58.98	155.33	4.000	No	No	2.00
94	0.94	60.14	33.28	2.13	0.39	1.70	96.60	58.88	155.48	4.000	No	No	2.00
95	0.95	60.30	33.14	2.13	0.39	1.70	96.85	58.78	155.64	4.000	No	No	2.00
96	0.96	60.46	32.99	2.12	0.39	1.70	97.12	58.68	155.80	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
97	0.97	60.62	32.86	2.12	0.39	1.70	97.37	58.58	155.95	4.000	No	No	2.00
98	0.98	60.76	32.74	2.12	0.39	1.70	97.60	58.49	156.08	4.000	No	No	2.00
99	0.99	60.90	32.61	2.12	0.39	1.70	97.79	58.39	156.18	4.000	No	No	2.00
100	1.00	61.09	32.46	2.12	0.39	1.70	98.05	58.26	156.30	4.000	No	No	2.00
101	1.01	61.36	32.24	2.12	0.39	1.70	98.53	58.11	156.64	4.000	No	No	2.00
102	1.02	61.72	31.97	2.11	0.39	1.70	99.11	57.90	157.01	4.000	No	No	2.00
103	1.03	62.12	31.66	2.11	0.39	1.70	99.76	57.66	157.42	4.000	No	No	2.00
104	1.04	62.53	31.34	2.10	0.39	1.70	100.44	57.40	157.84	4.000	No	No	2.00
105	1.05	62.94	31.02	2.10	0.39	1.70	101.11	57.13	158.25	4.000	No	No	2.00
106	1.06	63.33	30.72	2.10	0.39	1.70	101.75	56.87	158.62	4.000	No	No	2.00
107	1.07	63.68	30.45	2.09	0.39	1.70	102.32	56.64	158.95	4.000	No	No	2.00
108	1.08	63.97	30.21	2.09	0.39	1.70	102.78	56.41	159.18	4.000	No	No	2.00
109	1.09	64.23	29.96	2.09	0.39	1.70	103.14	56.14	159.28	4.000	No	No	2.00
110	1.10	64.51	29.67	2.08	0.39	1.70	103.60	55.82	159.42	4.000	No	No	2.00
111	1.11	64.83	29.33	2.08	0.39	1.70	104.12	55.44	159.56	4.000	No	No	2.00
112	1.12	65.18	28.95	2.07	0.39	1.70	104.69	55.00	159.70	4.000	No	No	2.00
113	1.13	65.54	28.56	2.07	0.39	1.70	105.28	54.54	159.82	4.000	No	No	2.00
114	1.14	65.90	28.18	2.06	0.39	1.70	105.86	54.07	159.93	4.000	No	No	2.00
115	1.15	66.22	27.82	2.06	0.39	1.70	106.39	53.61	160.01	4.000	No	No	2.00
116	1.16	66.50	27.51	2.06	0.39	1.70	106.86	53.21	160.06	4.000	No	No	2.00
117	1.17	66.72	27.24	2.05	0.39	1.70	107.21	52.83	160.03	4.000	No	No	2.00
118	1.18	66.91	26.96	2.05	0.39	1.70	107.45	52.41	159.86	4.000	No	No	2.00
119	1.19	67.09	26.64	2.05	0.39	1.70	107.75	51.92	159.67	4.000	No	No	2.00
120	1.20	67.30	26.27	2.04	0.39	1.70	108.09	51.35	159.43	4.000	No	No	2.00
121	1.21	67.52	25.87	2.04	0.39	1.70	108.45	50.71	159.16	4.000	No	No	2.00
122	1.22	67.74	25.47	2.03	0.39	1.70	108.81	50.05	158.86	4.000	No	No	2.00
123	1.23	67.96	25.07	2.03	0.39	1.70	109.16	49.38	158.54	4.000	No	No	2.00
124	1.24	68.15	24.72	2.02	0.39	1.70	109.48	48.75	158.24	4.000	No	No	2.00
125	1.25	68.30	24.43	2.02	0.39	1.70	109.75	48.25	158.01	4.000	No	No	2.00
126	1.26	68.38	24.25	2.02	0.39	1.70	109.88	47.91	157.79	4.000	No	No	2.00
127	1.27	68.42	24.14	2.01	0.39	1.70	109.90	47.70	157.59	4.000	No	No	2.00
128	1.28	68.43	24.05	2.01	0.39	1.70	109.91	47.53	157.44	4.000	No	No	2.00
129	1.29	68.44	23.96	2.01	0.39	1.70	109.93	47.34	157.27	4.000	No	No	2.00
130	1.30	68.45	23.86	2.01	0.39	1.70	109.96	47.14	157.09	4.000	No	No	2.00
131	1.31	68.47	23.76	2.01	0.39	1.70	109.98	46.93	156.91	4.000	No	No	2.00
132	1.32	68.48	23.66	2.01	0.39	1.70	110.00	46.74	156.74	4.000	No	No	2.00
133	1.33	68.49	23.57	2.01	0.39	1.70	110.02	46.57	156.59	4.000	No	No	2.00
134	1.34	68.46	23.56	2.01	0.39	1.70	110.03	46.55	156.58	4.000	No	No	2.00
135	1.35	68.38	23.65	2.01	0.39	1.70	109.87	46.70	156.57	4.000	No	No	2.00
136	1.36	68.22	23.85	2.01	0.39	1.70	109.60	47.06	156.65	4.000	No	No	2.00
137	1.37	68.03	24.09	2.01	0.39	1.70	109.28	47.50	156.78	4.000	No	No	2.00
138	1.38	67.82	24.36	2.02	0.39	1.70	108.94	47.96	156.91	4.000	No	No	2.00
139	1.39	67.61	24.63	2.02	0.39	1.70	108.60	48.43	157.03	4.000	No	No	2.00
140	1.40	67.40	24.89	2.02	0.39	1.70	108.25	48.88	157.13	4.000	No	No	2.00
141	1.41	67.21	25.14	2.03	0.39	1.70	107.94	49.28	157.22	4.000	No	No	2.00
142	1.42	67.05	25.34	2.03	0.39	1.70	107.67	49.62	157.28	4.000	No	No	2.00
143	1.43	66.95	25.51	2.03	0.39	1.70	107.47	49.89	157.37	4.000	No	No	2.00
144	1.44	66.90	25.66	2.03	0.39	1.70	107.46	50.16	157.62	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
145	1.45	66.89	25.82	2.04	0.39	1.70	107.44	50.44	157.88	4.000	No	No	2.00
146	1.46	66.88	26.00	2.04	0.39	1.70	107.42	50.75	158.17	4.000	No	No	2.00
147	1.47	66.86	26.18	2.04	0.39	1.70	107.40	51.08	158.48	4.000	No	No	2.00
148	1.48	66.85	26.37	2.04	0.39	1.70	107.38	51.40	158.78	4.000	No	No	2.00
149	1.49	66.84	26.55	2.04	0.39	1.70	107.36	51.70	159.06	4.000	No	No	2.00
150	1.50	66.83	26.71	2.05	0.39	1.70	107.34	51.97	159.31	4.000	No	No	2.00
151	1.51	66.82	26.85	2.05	0.39	1.70	107.32	52.20	159.52	4.000	No	No	2.00
152	1.52	66.80	26.96	2.05	0.39	1.70	107.30	52.39	159.69	4.000	No	No	2.00
153	1.53	66.78	27.07	2.05	0.39	1.70	107.27	52.56	159.83	4.000	No	No	2.00
154	1.54	66.76	27.19	2.05	0.39	1.70	107.23	52.76	159.99	4.000	No	No	2.00
155	1.55	66.73	27.33	2.05	0.39	1.70	107.19	52.98	160.17	4.000	No	No	2.00
156	1.56	66.71	27.47	2.06	0.39	1.70	107.15	53.20	160.35	4.000	No	No	2.00
157	1.57	66.68	27.61	2.06	0.39	1.70	107.11	53.42	160.52	4.000	No	No	2.00
158	1.58	66.66	27.74	2.06	0.39	1.70	107.07	53.62	160.68	4.000	No	No	2.00
159	1.59	66.64	27.86	2.06	0.39	1.70	107.03	53.80	160.83	4.000	No	No	2.00
160	1.60	66.58	27.96	2.06	0.39	1.70	107.00	53.95	160.95	4.000	No	No	2.00
161	1.61	66.47	28.05	2.06	0.39	1.70	106.80	54.05	160.85	4.000	No	No	2.00
162	1.62	66.29	28.15	2.06	0.39	1.70	106.50	54.16	160.65	4.000	No	No	2.00
163	1.63	66.08	28.27	2.07	0.39	1.70	106.14	54.27	160.41	4.000	No	No	2.00
164	1.64	65.84	28.40	2.07	0.39	1.70	105.76	54.39	160.15	4.000	No	No	2.00
165	1.65	65.60	28.53	2.07	0.39	1.70	105.37	54.52	159.89	4.000	No	No	2.00
166	1.66	65.37	28.66	2.07	0.39	1.70	104.99	54.64	159.62	4.000	No	No	2.00
167	1.67	65.15	28.78	2.07	0.39	1.70	104.63	54.75	159.38	4.000	No	No	2.00
168	1.68	64.96	28.89	2.07	0.39	1.70	104.32	54.84	159.16	4.000	No	No	2.00
169	1.69	64.80	28.97	2.07	0.39	1.70	104.08	54.91	159.00	4.000	No	No	2.00
170	1.70	64.63	29.04	2.08	0.39	1.70	103.82	54.97	158.79	4.000	No	No	2.00
171	1.71	64.43	29.12	2.08	0.39	1.70	103.50	55.01	158.51	4.000	No	No	2.00
172	1.72	64.21	29.20	2.08	0.39	1.70	103.14	55.06	158.20	4.000	No	No	2.00
173	1.73	63.97	29.29	2.08	0.39	1.70	102.75	55.12	157.87	4.000	No	No	2.00
174	1.74	63.73	29.39	2.08	0.39	1.70	102.36	55.17	157.53	4.000	No	No	2.00
175	1.75	63.50	29.47	2.08	0.39	1.70	101.98	55.22	157.20	4.000	No	No	2.00
176	1.76	63.29	29.55	2.08	0.39	1.70	101.64	55.27	156.91	4.000	No	No	2.00
177	1.77	63.11	29.62	2.08	0.39	1.70	101.36	55.30	156.66	4.000	No	No	2.00
178	1.78	62.91	29.67	2.08	0.39	1.70	101.08	55.31	156.40	4.000	No	No	2.00
179	1.79	62.68	29.70	2.08	0.39	1.70	100.70	55.29	155.99	4.000	No	No	2.00
180	1.80	62.40	29.74	2.08	0.39	1.70	100.24	55.25	155.48	4.000	No	No	2.00
181	1.81	62.09	29.78	2.08	0.40	1.70	99.73	55.20	154.93	4.000	No	No	2.00
182	1.82	61.76	29.83	2.09	0.40	1.70	99.20	55.16	154.35	4.000	No	No	2.00
183	1.83	61.44	29.87	2.09	0.40	1.70	98.67	55.11	153.78	4.000	No	No	2.00
184	1.84	61.13	29.92	2.09	0.40	1.70	98.18	55.07	153.24	4.000	No	No	2.00
185	1.85	60.87	29.95	2.09	0.40	1.70	97.74	55.03	152.77	4.000	No	No	2.00
186	1.86	60.62	30.00	2.09	0.40	1.70	97.38	55.01	152.40	4.000	No	No	2.00
187	1.87	60.34	30.05	2.09	0.40	1.70	96.97	55.00	151.97	4.000	No	No	2.00
188	1.88	60.02	30.12	2.09	0.40	1.70	96.43	54.98	151.41	4.000	No	No	2.00
189	1.89	59.63	30.20	2.09	0.40	1.70	95.80	54.96	150.76	4.000	No	No	2.00
190	1.90	59.22	30.29	2.09	0.40	1.70	95.12	54.94	150.06	4.000	No	No	2.00
191	1.91	58.79	30.38	2.09	0.40	1.70	94.42	54.92	149.35	4.000	No	No	2.00
192	1.92	58.37	30.48	2.09	0.41	1.70	93.74	54.91	148.65	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
193	1.93	57.99	30.56	2.09	0.41	1.70	93.11	54.89	148.00	4.000	No	No	2.00
194	1.94	57.65	30.64	2.10	0.41	1.70	92.57	54.88	147.45	4.000	No	No	2.00
195	1.95	57.33	30.74	2.10	0.41	1.70	92.13	54.92	147.05	4.000	No	No	2.00
196	1.96	56.98	30.88	2.10	0.41	1.70	91.57	54.98	146.55	4.000	No	No	2.00
197	1.97	56.56	31.07	2.10	0.41	1.70	90.88	55.07	145.95	4.000	No	No	2.00
198	1.98	56.08	31.29	2.10	0.41	1.70	90.09	55.17	145.26	4.000	No	No	2.00
199	1.99	55.57	31.52	2.11	0.41	1.70	89.26	55.27	144.53	4.000	No	No	2.00
200	2.00	55.06	31.75	2.11	0.41	1.70	88.42	55.38	143.80	4.000	No	No	2.00
201	2.01	54.57	31.98	2.11	0.41	1.70	87.62	55.47	143.09	4.000	No	No	2.00
202	2.02	54.12	32.18	2.11	0.42	1.70	86.89	55.56	142.45	4.000	No	No	2.00
203	2.03	53.73	32.37	2.12	0.42	1.70	86.29	55.63	141.92	4.000	No	No	2.00
204	2.04	53.34	32.55	2.12	0.42	1.70	85.74	55.73	141.47	4.000	No	No	2.00
205	2.05	52.90	32.76	2.12	0.42	1.70	85.01	55.81	140.82	4.000	No	No	2.00
206	2.06	52.37	33.02	2.13	0.42	1.70	84.14	55.90	140.04	4.000	No	No	2.00
207	2.07	51.78	33.31	2.13	0.42	1.70	83.18	56.00	139.18	4.000	No	No	2.00
208	2.08	51.17	33.61	2.13	0.42	1.70	82.18	56.10	138.28	4.000	No	No	2.00
209	2.09	50.56	33.92	2.14	0.42	1.70	81.19	56.19	137.38	4.000	No	No	2.00
210	2.10	49.99	34.21	2.14	0.43	1.70	80.26	56.28	136.54	4.000	No	No	2.00
211	2.11	49.49	34.47	2.14	0.43	1.70	79.43	56.36	135.79	4.000	No	No	2.00
212	2.12	49.07	34.67	2.15	0.43	1.70	78.77	56.40	135.17	4.000	No	No	2.00
213	2.13	48.71	34.82	2.15	0.43	1.70	78.27	56.44	134.71	4.000	No	No	2.00
214	2.14	48.33	34.96	2.15	0.43	1.70	77.66	56.43	134.09	4.000	No	No	2.00
215	2.15	47.89	35.11	2.15	0.43	1.70	76.95	56.42	133.37	4.000	No	No	2.00
216	2.16	47.43	35.28	2.15	0.43	1.70	76.18	56.41	132.59	4.000	No	No	2.00
217	2.17	46.94	35.46	2.16	0.43	1.70	75.40	56.40	131.79	4.000	No	No	2.00
218	2.18	46.48	35.64	2.16	0.44	1.70	74.63	56.38	131.02	4.000	No	No	2.00
219	2.19	46.05	35.80	2.16	0.44	1.70	73.93	56.37	130.30	4.000	No	No	2.00
220	2.20	45.68	35.94	2.16	0.44	1.70	73.32	56.36	129.68	4.000	No	No	2.00
221	2.21	45.37	36.06	2.16	0.44	1.70	72.86	56.35	129.22	4.000	No	No	2.00
222	2.22	45.09	36.16	2.16	0.44	1.70	72.46	56.35	128.81	4.000	No	No	2.00
223	2.23	44.79	36.26	2.17	0.44	1.70	71.96	56.33	128.29	4.000	No	No	2.00
224	2.24	44.44	36.38	2.17	0.44	1.70	71.40	56.30	127.70	4.000	No	No	2.00
225	2.25	44.08	36.51	2.17	0.44	1.70	70.80	56.28	127.08	4.000	No	No	2.00
226	2.26	43.71	36.64	2.17	0.44	1.70	70.20	56.25	126.46	4.000	No	No	2.00
227	2.27	43.36	36.77	2.17	0.45	1.70	69.63	56.23	125.86	4.000	No	No	2.00
228	2.28	43.04	36.89	2.17	0.45	1.70	69.11	56.21	125.32	4.000	No	No	2.00
229	2.29	42.78	36.99	2.17	0.45	1.70	68.68	56.19	124.87	4.000	No	No	2.00
230	2.30	42.53	37.08	2.18	0.45	1.70	68.34	56.18	124.53	4.000	No	No	2.00
231	2.31	42.28	37.17	2.18	0.45	1.70	67.94	56.17	124.11	4.000	No	No	2.00
232	2.32	41.99	37.28	2.18	0.45	1.70	67.46	56.14	123.60	4.000	No	No	2.00
233	2.33	41.67	37.40	2.18	0.45	1.70	66.94	56.12	123.05	4.000	No	No	2.00
234	2.34	41.33	37.52	2.18	0.45	1.70	66.39	56.09	122.48	4.000	No	No	2.00
235	2.35	41.00	37.65	2.18	0.45	1.70	65.84	56.06	121.91	4.000	No	No	2.00
236	2.36	40.69	37.77	2.18	0.45	1.70	65.33	56.04	121.37	4.000	No	No	2.00
237	2.37	40.41	37.88	2.19	0.45	1.70	64.88	56.02	120.90	4.000	No	No	2.00
238	2.38	40.19	37.97	2.19	0.46	1.70	64.52	56.00	120.52	4.000	No	No	2.00
239	2.39	39.98	38.04	2.19	0.46	1.70	64.24	55.99	120.23	4.000	No	No	2.00
240	2.40	39.77	38.12	2.19	0.46	1.70	63.89	55.97	119.86	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
241	2.41	39.52	38.20	2.19	0.46	1.70	63.49	55.94	119.43	4.000	No	No	2.00
242	2.42	39.25	38.29	2.19	0.46	1.70	63.06	55.90	118.96	4.000	No	No	2.00
243	2.43	38.98	38.39	2.19	0.46	1.70	62.61	55.87	118.48	4.000	No	No	2.00
244	2.44	38.72	38.49	2.19	0.46	1.70	62.18	55.84	118.02	4.000	No	No	2.00
245	2.45	38.47	38.58	2.19	0.46	1.70	61.78	55.81	117.59	4.000	No	No	2.00
246	2.46	38.26	38.66	2.20	0.46	1.70	61.44	55.79	117.23	4.000	No	No	2.00
247	2.47	38.08	38.75	2.20	0.46	1.70	61.17	55.80	116.97	4.000	No	No	2.00
248	2.48	37.89	38.87	2.20	0.46	1.70	60.88	55.82	116.69	4.000	No	No	2.00
249	2.49	37.67	39.03	2.20	0.46	1.70	60.52	55.84	116.36	4.000	No	No	2.00
250	2.50	37.42	39.20	2.20	0.46	1.70	60.12	55.87	115.99	4.000	No	No	2.00
251	2.51	37.16	39.39	2.20	0.47	1.70	59.69	55.91	115.59	4.000	No	No	2.00
252	2.52	36.90	39.59	2.21	0.47	1.70	59.26	55.94	115.20	4.000	No	No	2.00
253	2.53	36.64	39.77	2.21	0.47	1.70	58.85	55.97	114.81	4.000	No	No	2.00
254	2.54	36.42	39.94	2.21	0.47	1.70	58.48	55.99	114.47	4.000	No	No	2.00
255	2.55	36.21	40.09	2.21	0.47	1.70	58.17	56.02	114.19	4.000	No	No	2.00
256	2.56	35.99	40.24	2.22	0.47	1.70	57.86	56.05	113.90	4.000	No	No	2.00
257	2.57	35.73	40.41	2.22	0.47	1.70	57.41	56.05	113.47	4.000	No	No	2.00
258	2.58	35.41	40.61	2.22	0.47	1.70	56.89	56.06	112.95	4.000	No	No	2.00
259	2.59	35.05	40.84	2.22	0.47	1.70	56.31	56.07	112.38	4.000	No	No	2.00
260	2.60	34.68	41.09	2.23	0.47	1.70	55.71	56.08	111.79	4.000	No	No	2.00
261	2.61	34.32	41.33	2.23	0.47	1.70	55.12	56.09	111.21	4.000	No	No	2.00
262	2.62	33.98	41.56	2.23	0.48	1.70	54.56	56.10	110.66	4.000	No	No	2.00
263	2.63	33.68	41.77	2.23	0.48	1.70	54.07	56.10	110.17	4.000	No	No	2.00
264	2.64	33.42	41.94	2.24	0.48	1.70	53.67	56.11	109.78	4.000	No	No	2.00
265	2.65	33.17	42.09	2.24	0.48	1.70	53.31	56.11	109.42	4.000	No	No	2.00
266	2.66	32.89	42.26	2.24	0.48	1.70	52.85	56.10	108.95	4.000	No	No	2.00
267	2.67	32.56	42.45	2.24	0.48	1.70	52.31	56.08	108.39	4.000	No	No	2.00
268	2.68	32.21	42.66	2.25	0.48	1.70	51.74	56.06	107.80	4.000	No	No	2.00
269	2.69	31.85	42.88	2.25	0.48	1.70	51.15	56.04	107.19	4.000	No	No	2.00
270	2.70	31.50	43.10	2.25	0.48	1.70	50.58	56.02	106.60	4.000	No	No	2.00
271	2.71	31.17	43.30	2.25	0.49	1.70	50.05	56.01	106.06	4.000	No	No	2.00
272	2.72	30.91	43.47	2.26	0.49	1.70	49.60	55.98	105.58	4.000	No	No	2.00
273	2.73	30.75	43.55	2.26	0.49	1.70	49.32	55.96	105.27	4.000	No	No	2.00
274	2.74	30.68	43.55	2.26	0.49	1.70	49.28	55.95	105.23	4.000	No	No	2.00
275	2.75	30.65	43.50	2.26	0.49	1.70	49.24	55.91	105.15	4.000	No	No	2.00
276	2.76	30.62	43.44	2.26	0.49	1.70	49.19	55.87	105.06	4.000	No	No	2.00
277	2.77	30.59	43.38	2.25	0.49	1.70	49.14	55.82	104.96	4.000	No	No	2.00
278	2.78	30.56	43.32	2.25	0.49	1.70	49.08	55.77	104.86	4.000	No	No	2.00
279	2.79	30.53	43.26	2.25	0.49	1.70	49.03	55.73	104.76	4.000	No	No	2.00
280	2.80	30.50	43.20	2.25	0.49	1.70	48.99	55.69	104.68	4.000	No	No	2.00
281	2.81	30.48	43.16	2.25	0.49	1.70	48.95	55.65	104.60	4.000	No	No	2.00
282	2.82	30.46	43.11	2.25	0.49	1.70	48.92	55.62	104.54	4.000	No	No	2.00
283	2.83	30.44	43.06	2.25	0.49	1.70	48.89	55.58	104.47	4.000	No	No	2.00
284	2.84	30.41	43.00	2.25	0.49	1.70	48.85	55.54	104.39	4.000	No	No	2.00
285	2.85	30.39	42.94	2.25	0.49	1.70	48.81	55.49	104.30	4.000	No	No	2.00
286	2.86	30.36	42.87	2.25	0.49	1.70	48.77	55.44	104.21	4.000	No	No	2.00
287	2.87	30.33	42.80	2.25	0.49	1.70	48.73	55.39	104.12	4.000	No	No	2.00
288	2.88	30.31	42.73	2.25	0.49	1.70	48.69	55.34	104.03	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
289	2.89	30.29	42.68	2.25	0.49	1.70	48.65	55.30	103.95	4.000	No	No	2.00
290	2.90	30.25	42.62	2.25	0.49	1.70	48.62	55.26	103.89	4.000	No	No	2.00
291	2.91	30.20	42.57	2.24	0.49	1.70	48.52	55.21	103.72	4.000	No	No	2.00
292	2.92	30.11	42.49	2.24	0.49	1.70	48.38	55.13	103.51	4.000	No	No	2.00
293	2.93	30.02	42.41	2.24	0.49	1.70	48.22	55.04	103.26	4.000	No	No	2.00
294	2.94	29.91	42.32	2.24	0.49	1.70	48.05	54.94	103.00	4.000	No	No	2.00
295	2.95	29.81	42.22	2.24	0.49	1.70	47.88	54.85	102.72	4.000	No	No	2.00
296	2.96	29.70	42.13	2.24	0.49	1.70	47.71	54.75	102.46	4.000	No	No	2.00
297	2.97	29.61	42.04	2.24	0.49	1.70	47.55	54.66	102.21	4.000	No	No	2.00
298	2.98	29.50	41.99	2.24	0.49	1.70	47.42	54.60	102.02	4.000	No	No	2.00
299	2.99	29.28	42.06	2.24	0.49	1.70	47.19	54.58	101.78	4.000	No	No	2.00
300	3.00	28.92	42.27	2.24	0.50	1.70	46.51	54.54	101.04	4.000	No	No	2.00
301	3.01	28.41	42.61	2.25	0.50	1.70	45.67	54.52	100.19	4.000	No	No	2.00
302	3.02	27.83	43.00	2.25	0.50	1.70	44.72	54.51	99.23	4.000	No	No	2.00
303	3.03	27.22	43.43	2.26	0.50	1.70	43.73	54.50	98.22	4.000	No	No	2.00
304	3.04	26.61	43.88	2.26	0.50	1.70	42.73	54.48	97.21	4.000	No	No	2.00
305	3.05	26.03	44.32	2.27	0.51	1.70	41.78	54.47	96.25	4.000	No	No	2.00
306	3.06	25.51	44.73	2.27	0.51	1.70	40.92	54.46	95.39	4.000	No	No	2.00
307	3.07	25.05	45.12	2.28	0.51	1.70	40.21	54.48	94.70	4.000	No	No	2.00
308	3.08	24.59	45.59	2.28	0.51	1.70	39.57	54.55	94.12	4.000	No	No	2.00
309	3.09	24.08	46.18	2.29	0.51	1.70	38.73	54.61	93.35	4.000	No	No	2.00
310	3.10	23.47	46.92	2.30	0.52	1.70	37.74	54.70	92.44	4.000	No	No	2.00
311	3.11	22.80	47.76	2.31	0.52	1.70	36.65	54.79	91.43	4.000	No	No	2.00
312	3.12	22.11	48.67	2.32	0.52	1.70	35.51	54.87	90.39	4.000	No	No	2.00
313	3.13	21.43	49.58	2.33	0.52	1.70	34.40	54.95	89.35	4.000	No	No	2.00
314	3.14	20.79	50.47	2.34	0.53	1.70	33.35	55.02	88.38	4.000	No	No	2.00
315	3.15	20.23	51.28	2.35	0.53	1.70	32.43	55.08	87.51	4.000	No	No	2.00
316	3.16	19.88	51.79	2.36	0.53	1.70	31.70	55.07	86.77	4.000	No	No	2.00
317	3.17	19.72	52.03	2.36	0.53	1.70	31.67	55.15	86.81	4.000	No	No	2.00
318	3.18	19.71	52.04	2.36	0.53	1.70	31.67	55.15	86.82	4.000	No	No	2.00
319	3.19	19.71	52.04	2.36	0.53	1.70	31.67	55.15	86.82	4.000	No	No	2.00
320	3.20	19.71	52.04	2.36	0.53	1.70	31.67	55.15	86.82	4.000	No	No	2.00
321	3.21	19.71	52.04	2.36	0.53	1.70	31.67	55.15	86.82	4.000	No	No	2.00
322	3.22	19.71	52.05	2.36	0.53	1.70	31.67	55.15	86.82	4.000	No	No	2.00
323	3.23	19.71	52.05	2.36	0.53	1.70	31.67	55.15	86.82	4.000	No	No	2.00
324	3.24	19.72	52.03	2.36	0.53	1.70	31.67	55.15	86.82	4.000	No	No	2.00
325	3.25	19.74	51.96	2.36	0.53	1.70	31.69	55.13	86.81	4.000	No	No	2.00
326	3.26	19.79	51.80	2.36	0.53	1.70	31.78	55.10	86.87	4.000	No	No	2.00
327	3.27	19.85	51.58	2.36	0.53	1.70	31.89	55.04	86.93	4.000	No	No	2.00
328	3.28	19.93	51.32	2.35	0.53	1.70	32.01	54.98	87.00	4.000	No	No	2.00
329	3.29	20.01	51.05	2.35	0.53	1.70	32.14	54.92	87.06	4.000	No	No	2.00
330	3.30	20.09	50.78	2.35	0.53	1.70	32.27	54.85	87.12	4.000	No	No	2.00
331	3.31	20.16	50.53	2.34	0.53	1.70	32.39	54.79	87.18	4.000	No	No	2.00
332	3.32	20.23	50.29	2.34	0.53	1.70	32.51	54.73	87.24	4.000	No	No	2.00
333	3.33	20.28	50.11	2.34	0.53	1.70	32.60	54.68	87.28	4.000	No	No	2.00
334	3.34	20.30	49.97	2.34	0.53	1.70	32.63	54.64	87.26	4.000	No	No	2.00
335	3.35	20.31	49.84	2.34	0.53	1.70	32.63	54.59	87.21	4.000	No	No	2.00
336	3.36	20.31	49.70	2.33	0.53	1.70	32.63	54.53	87.16	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
337	3.37	20.31	49.55	2.33	0.53	1.70	32.63	54.47	87.10	4.000	No	No	2.00
338	3.38	20.31	49.39	2.33	0.53	1.70	32.63	54.41	87.03	4.000	No	No	2.00
339	3.39	20.31	49.23	2.33	0.53	1.70	32.63	54.34	86.97	4.000	No	No	2.00
340	3.40	20.31	49.08	2.33	0.53	1.70	32.63	54.28	86.91	4.000	No	No	2.00
341	3.41	20.31	48.95	2.32	0.53	1.70	32.63	54.23	86.86	4.000	No	No	2.00
342	3.42	20.31	48.88	2.32	0.53	1.70	32.63	54.20	86.83	4.000	No	No	2.00
343	3.43	20.31	48.87	2.32	0.53	1.70	32.63	54.20	86.83	4.000	No	No	2.00
344	3.44	20.31	48.91	2.32	0.53	1.70	32.63	54.22	86.84	4.000	No	No	2.00
345	3.45	20.31	48.96	2.32	0.53	1.70	32.63	54.24	86.86	4.000	No	No	2.00
346	3.46	20.31	49.02	2.33	0.53	1.70	32.63	54.26	86.89	4.000	No	No	2.00
347	3.47	20.31	49.07	2.33	0.53	1.70	32.63	54.28	86.91	4.000	No	No	2.00
348	3.48	20.31	49.13	2.33	0.53	1.70	32.63	54.30	86.93	4.000	No	No	2.00
349	3.49	20.31	49.18	2.33	0.53	1.70	32.63	54.32	86.95	4.000	No	No	2.00
350	3.50	20.32	49.21	2.33	0.53	1.70	32.63	54.34	86.96	4.000	No	No	2.00
351	3.51	20.37	49.20	2.33	0.53	1.70	32.67	54.34	87.02	4.000	No	No	2.00
352	3.52	20.46	49.13	2.33	0.53	1.70	32.85	54.37	87.22	4.000	No	No	2.00
353	3.53	20.59	49.03	2.33	0.53	1.70	33.07	54.38	87.46	4.000	No	No	2.00
354	3.54	20.75	48.92	2.32	0.53	1.70	33.32	54.40	87.72	4.000	No	No	2.00
355	3.55	20.90	48.80	2.32	0.53	1.70	33.58	54.42	88.00	4.000	No	No	2.00
356	3.56	21.06	48.68	2.32	0.53	1.70	33.84	54.44	88.28	4.000	No	No	2.00
357	3.57	21.22	48.57	2.32	0.52	1.70	34.09	54.46	88.55	4.000	No	No	2.00
358	3.58	21.35	48.48	2.32	0.52	1.70	34.31	54.48	88.79	4.000	No	No	2.00
359	3.59	21.48	48.35	2.32	0.52	1.70	34.49	54.48	88.97	4.000	No	No	2.00
360	3.60	21.62	48.15	2.31	0.52	1.70	34.70	54.45	89.15	4.000	No	No	2.00
361	3.61	21.79	47.85	2.31	0.52	1.70	34.99	54.39	89.39	4.000	No	No	2.00
362	3.62	22.01	47.47	2.31	0.52	1.70	35.34	54.32	89.66	4.000	No	No	2.00
363	3.63	22.24	47.06	2.30	0.52	1.70	35.72	54.24	89.95	4.000	No	No	2.00
364	3.64	22.48	46.63	2.30	0.52	1.70	36.11	54.15	90.26	4.000	No	No	2.00
365	3.65	22.71	46.22	2.29	0.52	1.70	36.50	54.06	90.55	4.000	No	No	2.00
366	3.66	22.93	45.83	2.29	0.52	1.70	36.86	53.97	90.83	4.000	No	No	2.00
367	3.67	23.13	45.50	2.28	0.52	1.70	37.17	53.89	91.06	4.000	No	No	2.00
368	3.68	23.28	45.23	2.28	0.52	1.70	37.42	53.83	91.25	4.000	No	No	2.00
369	3.69	23.41	44.99	2.27	0.52	1.70	37.59	53.75	91.34	4.000	No	No	2.00
370	3.70	23.54	44.74	2.27	0.52	1.70	37.80	53.68	91.48	4.000	No	No	2.00
371	3.71	23.68	44.46	2.27	0.52	1.70	38.04	53.60	91.64	4.000	No	No	2.00
372	3.72	23.84	44.15	2.26	0.52	1.70	38.30	53.51	91.80	4.000	No	No	2.00
373	3.73	24.00	43.84	2.26	0.52	1.70	38.56	53.41	91.97	4.000	No	No	2.00
374	3.74	24.15	43.54	2.26	0.52	1.70	38.81	53.32	92.13	4.000	No	No	2.00
375	3.75	24.30	43.27	2.25	0.52	1.70	39.04	53.23	92.27	4.000	No	No	2.00
376	3.76	24.42	43.05	2.25	0.52	1.70	39.24	53.16	92.40	4.000	No	No	2.00
377	3.77	24.56	42.87	2.25	0.52	1.70	39.42	53.11	92.53	4.000	No	No	2.00
378	3.78	24.72	42.73	2.25	0.51	1.70	39.69	53.11	92.80	4.000	No	No	2.00
379	3.79	24.92	42.59	2.24	0.51	1.70	40.02	53.11	93.13	4.000	No	No	2.00
380	3.80	25.15	42.44	2.24	0.51	1.70	40.39	53.11	93.51	4.000	No	No	2.00
381	3.81	25.39	42.27	2.24	0.51	1.70	40.78	53.12	93.90	4.000	No	No	2.00
382	3.82	25.63	42.12	2.24	0.51	1.70	41.17	53.13	94.30	4.000	No	No	2.00
383	3.83	25.85	41.97	2.24	0.51	1.70	41.54	53.13	94.68	4.000	No	No	2.00
384	3.84	26.06	41.84	2.24	0.51	1.70	41.88	53.14	95.02	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
385	3.85	26.28	41.67	2.23	0.51	1.70	42.15	53.11	95.26	4.000	No	No	2.00
386	3.86	26.59	41.40	2.23	0.51	1.70	42.63	53.07	95.70	4.000	No	No	2.00
387	3.87	27.04	41.01	2.23	0.51	1.70	43.39	53.02	96.41	4.000	No	No	2.00
388	3.88	27.58	40.54	2.22	0.50	1.70	44.27	52.95	97.22	4.000	No	No	2.00
389	3.89	28.17	40.03	2.21	0.50	1.70	45.24	52.86	98.10	4.000	No	No	2.00
390	3.90	28.78	39.52	2.21	0.50	1.70	46.24	52.77	99.02	4.000	No	No	2.00
391	3.91	29.39	39.04	2.20	0.50	1.70	47.23	52.68	99.91	4.000	No	No	2.00
392	3.92	29.95	38.60	2.19	0.50	1.70	48.15	52.60	100.75	4.000	No	No	2.00
393	3.93	30.44	38.22	2.19	0.49	1.70	48.95	52.52	101.47	4.000	No	No	2.00
394	3.94	30.83	37.90	2.19	0.49	1.70	49.58	52.44	102.02	4.000	No	No	2.00
395	3.95	31.19	37.57	2.18	0.49	1.70	50.06	52.31	102.36	4.000	No	No	2.00
396	3.96	31.55	37.19	2.18	0.49	1.70	50.65	52.16	102.82	4.000	No	No	2.00
397	3.97	31.97	36.77	2.17	0.49	1.70	51.33	52.00	103.33	4.000	No	No	2.00
398	3.98	32.41	36.31	2.17	0.49	1.70	52.06	51.81	103.87	4.000	No	No	2.00
399	3.99	32.87	35.86	2.16	0.49	1.70	52.80	51.61	104.42	4.000	No	No	2.00
400	4.00	33.30	35.43	2.16	0.49	1.70	53.52	51.42	104.94	4.000	No	No	2.00
401	4.01	33.70	35.04	2.15	0.49	1.70	54.17	51.24	105.41	4.000	No	No	2.00
402	4.02	34.01	34.74	2.15	0.49	1.70	54.73	51.10	105.82	4.000	No	No	2.00
403	4.03	34.19	34.55	2.14	0.49	1.70	55.02	51.00	106.01	4.000	No	No	2.00
404	4.04	34.25	34.46	2.14	0.49	1.70	55.02	50.92	105.93	4.000	No	No	2.00
405	4.05	34.25	34.41	2.14	0.49	1.70	55.02	50.87	105.89	4.000	No	No	2.00
406	4.06	34.25	34.36	2.14	0.49	1.70	55.02	50.82	105.84	4.000	No	No	2.00
407	4.07	34.25	34.30	2.14	0.49	1.70	55.02	50.77	105.79	4.000	No	No	2.00
408	4.08	34.25	34.24	2.14	0.49	1.70	55.02	50.72	105.74	4.000	No	No	2.00
409	4.09	34.25	34.19	2.14	0.49	1.70	55.02	50.67	105.69	4.000	No	No	2.00
410	4.10	34.25	34.14	2.14	0.49	1.70	55.02	50.63	105.64	4.000	No	No	2.00
411	4.11	34.25	34.11	2.14	0.49	1.70	55.02	50.60	105.62	4.000	No	No	2.00
412	4.12	34.25	34.12	2.14	0.49	1.70	55.02	50.61	105.63	4.000	No	No	2.00
413	4.13	34.25	34.16	2.14	0.49	1.70	55.02	50.65	105.66	4.000	No	No	2.00
414	4.14	34.25	34.21	2.14	0.49	1.70	55.02	50.69	105.71	4.000	No	No	2.00
415	4.15	34.25	34.27	2.14	0.49	1.70	55.02	50.75	105.76	4.000	No	No	2.00
416	4.16	34.25	34.33	2.14	0.49	1.70	55.02	50.80	105.82	4.000	No	No	2.00
417	4.17	34.25	34.39	2.14	0.49	1.70	55.02	50.85	105.87	4.000	No	No	2.00
418	4.18	34.25	34.44	2.14	0.49	1.70	55.02	50.90	105.92	4.000	No	No	2.00
419	4.19	34.25	34.49	2.14	0.49	1.70	55.02	50.94	105.96	4.000	No	No	2.00
420	4.20	34.25	34.56	2.14	0.49	1.70	55.02	51.00	106.02	4.000	No	No	2.00
421	4.21	34.25	34.66	2.15	0.48	1.70	55.02	51.09	106.11	4.000	No	No	2.00
422	4.22	34.25	34.80	2.15	0.48	1.70	55.02	51.21	106.23	4.000	No	No	2.00
423	4.23	34.25	34.96	2.15	0.48	1.70	55.02	51.35	106.37	4.000	No	No	2.00
424	4.24	34.25	35.13	2.15	0.48	1.70	55.02	51.50	106.52	4.000	No	No	2.00
425	4.25	34.25	35.30	2.15	0.48	1.70	55.02	51.65	106.66	4.000	No	No	2.00
426	4.26	34.25	35.46	2.16	0.48	1.70	55.02	51.78	106.80	4.000	No	No	2.00
427	4.27	34.25	35.61	2.16	0.48	1.70	55.02	51.91	106.93	4.000	No	No	2.00
428	4.28	34.25	35.74	2.16	0.48	1.70	55.02	52.02	107.04	4.000	No	No	2.00
429	4.29	34.23	35.87	2.16	0.48	1.70	55.00	52.12	107.12	4.000	No	No	2.00
430	4.30	34.20	36.02	2.16	0.48	1.70	54.94	52.23	107.17	4.000	No	No	2.00
431	4.31	34.15	36.20	2.16	0.48	1.70	54.86	52.36	107.22	4.000	No	No	2.00
432	4.32	34.10	36.40	2.17	0.48	1.70	54.78	52.50	107.28	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
433	4.33	34.05	36.60	2.17	0.48	1.70	54.69	52.64	107.34	4.000	No	No	2.00
434	4.34	33.99	36.81	2.17	0.48	1.70	54.61	52.79	107.39	4.000	No	No	2.00
435	4.35	33.94	37.00	2.18	0.48	1.70	54.52	52.92	107.44	4.000	No	No	2.00
436	4.36	33.90	37.18	2.18	0.48	1.70	54.45	53.04	107.49	4.000	No	No	2.00
437	4.37	33.88	37.29	2.18	0.48	1.70	54.39	53.11	107.50	4.000	No	No	2.00
438	4.38	33.89	37.35	2.18	0.48	1.70	54.43	53.16	107.59	4.000	No	No	2.00
439	4.39	33.94	37.36	2.18	0.48	1.70	54.51	53.19	107.70	4.000	No	No	2.00
440	4.40	33.99	37.36	2.18	0.48	1.70	54.60	53.21	107.82	4.000	No	No	2.00
441	4.41	34.06	37.36	2.18	0.48	1.70	54.71	53.24	107.95	4.000	No	No	2.00
442	4.42	34.13	37.36	2.18	0.48	1.70	54.82	53.26	108.08	4.000	No	No	2.00
443	4.43	34.19	37.36	2.18	0.48	1.70	54.93	53.28	108.21	4.000	No	No	2.00
444	4.44	34.25	37.36	2.18	0.48	1.70	55.03	53.31	108.33	4.000	No	No	2.00
445	4.45	34.31	37.35	2.18	0.48	1.70	55.11	53.32	108.44	4.000	No	No	2.00
446	4.46	34.39	37.31	2.18	0.48	1.70	55.19	53.31	108.50	4.000	No	No	2.00
447	4.47	34.53	37.21	2.18	0.48	1.70	55.44	53.29	108.74	4.000	No	No	2.00
448	4.48	34.72	37.05	2.18	0.48	1.70	55.76	53.24	109.01	4.000	No	No	2.00
449	4.49	34.94	36.88	2.17	0.48	1.70	56.12	53.19	109.31	4.000	No	No	2.00
450	4.50	35.18	36.69	2.17	0.48	1.70	56.51	53.13	109.64	4.000	No	No	2.00
451	4.51	35.42	36.50	2.17	0.48	1.70	56.90	53.07	109.97	4.000	No	No	2.00
452	4.52	35.65	36.32	2.17	0.48	1.70	57.28	53.01	110.29	4.000	No	No	2.00
453	4.53	35.86	36.16	2.16	0.48	1.70	57.62	52.96	110.58	4.000	No	No	2.00
454	4.54	36.04	36.02	2.16	0.48	1.70	57.91	52.91	110.82	4.000	No	No	2.00
455	4.55	36.22	35.88	2.16	0.47	1.70	58.16	52.85	111.01	4.000	No	No	2.00
456	4.56	36.41	35.74	2.16	0.47	1.70	58.46	52.80	111.26	4.000	No	No	2.00
457	4.57	36.63	35.57	2.16	0.47	1.70	58.83	52.74	111.57	4.000	No	No	2.00
458	4.58	36.88	35.38	2.15	0.47	1.70	59.24	52.67	111.91	4.000	No	No	2.00
459	4.59	37.15	35.18	2.15	0.47	1.70	59.67	52.60	112.27	4.000	No	No	2.00
460	4.60	37.41	34.99	2.15	0.47	1.70	60.10	52.52	112.62	4.000	No	No	2.00
461	4.61	37.66	34.81	2.15	0.47	1.70	60.50	52.45	112.95	4.000	No	No	2.00
462	4.62	37.88	34.65	2.15	0.47	1.70	60.86	52.39	113.25	4.000	No	No	2.00
463	4.63	38.09	34.48	2.14	0.47	1.70	61.16	52.30	113.46	4.000	No	No	2.00
464	4.64	38.33	34.26	2.14	0.47	1.70	61.52	52.18	113.70	4.000	No	No	2.00
465	4.65	38.63	33.97	2.14	0.47	1.70	62.02	52.02	114.04	4.000	No	No	2.00
466	4.66	38.98	33.62	2.13	0.47	1.70	62.60	51.81	114.42	4.000	No	No	2.00
467	4.67	39.37	33.24	2.13	0.47	1.70	63.24	51.59	114.82	4.000	No	No	2.00
468	4.68	39.77	32.85	2.12	0.47	1.70	63.89	51.34	115.23	4.000	No	No	2.00
469	4.69	40.16	32.48	2.12	0.47	1.70	64.53	51.09	115.63	4.000	No	No	2.00
470	4.70	40.53	32.13	2.11	0.46	1.70	65.13	50.86	115.98	4.000	No	No	2.00
471	4.71	40.84	31.83	2.11	0.46	1.70	65.64	50.65	116.29	4.000	No	No	2.00
472	4.72	41.13	31.56	2.11	0.46	1.70	66.05	50.45	116.50	4.000	No	No	2.00
473	4.73	41.42	31.29	2.10	0.46	1.70	66.49	50.24	116.73	4.000	No	No	2.00
474	4.74	41.75	30.98	2.10	0.46	1.70	67.05	50.00	117.05	4.000	No	No	2.00
475	4.75	42.14	30.62	2.10	0.46	1.70	67.68	49.72	117.40	4.000	No	No	2.00
476	4.76	42.55	30.24	2.09	0.46	1.70	68.35	49.42	117.76	4.000	No	No	2.00
477	4.77	42.96	29.86	2.09	0.46	1.70	69.03	49.10	118.12	4.000	No	No	2.00
478	4.78	43.36	29.50	2.08	0.46	1.70	69.68	48.78	118.46	4.000	No	No	2.00
479	4.79	43.73	29.17	2.08	0.46	1.70	70.27	48.49	118.76	4.000	No	No	2.00
480	4.80	44.04	28.89	2.07	0.46	1.70	70.78	48.23	119.01	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
481	4.81	44.35	28.66	2.07	0.46	1.70	71.20	48.01	119.21	4.000	No	No	2.00
482	4.82	44.70	28.44	2.07	0.46	1.70	71.76	47.82	119.58	4.000	No	No	2.00
483	4.83	45.11	28.19	2.06	0.46	1.70	72.43	47.61	120.05	4.000	No	No	2.00
484	4.84	45.56	27.91	2.06	0.46	1.70	73.18	47.38	120.56	4.000	No	No	2.00
485	4.85	46.04	27.62	2.06	0.45	1.70	73.96	47.13	121.09	4.000	No	No	2.00
486	4.86	46.52	27.34	2.05	0.45	1.70	74.74	46.88	121.62	4.000	No	No	2.00
487	4.87	46.97	27.08	2.05	0.45	1.70	75.48	46.63	122.11	4.000	No	No	2.00
488	4.88	47.37	26.85	2.05	0.45	1.70	76.13	46.41	122.54	4.000	No	No	2.00
489	4.89	47.73	26.64	2.05	0.45	1.70	76.66	46.20	122.86	4.000	No	No	2.00
490	4.90	48.12	26.42	2.04	0.45	1.70	77.23	45.97	123.20	4.000	No	No	2.00
491	4.91	48.58	26.16	2.04	0.45	1.70	78.00	45.70	123.70	4.000	No	No	2.00
492	4.92	49.12	25.86	2.04	0.45	1.70	78.89	45.39	124.27	4.000	No	No	2.00
493	4.93	49.72	25.54	2.03	0.45	1.70	79.85	45.03	124.89	4.000	No	No	2.00
494	4.94	50.32	25.21	2.03	0.45	1.70	80.85	44.66	125.51	4.000	No	No	2.00
495	4.95	50.92	24.89	2.02	0.45	1.70	81.82	44.29	126.11	4.000	No	No	2.00
496	4.96	51.47	24.60	2.02	0.44	1.70	82.72	43.94	126.66	4.000	No	No	2.00
497	4.97	51.94	24.35	2.02	0.44	1.70	83.50	43.64	127.14	4.000	No	No	2.00
498	4.98	52.33	24.15	2.01	0.44	1.70	84.10	43.39	127.49	4.000	No	No	2.00
499	4.99	52.67	23.98	2.01	0.44	1.70	84.57	43.14	127.72	4.000	No	No	2.00
500	5.00	53.03	23.80	2.01	0.44	1.70	85.16	42.91	128.07	4.000	No	No	2.00
501	5.01	53.44	23.59	2.01	0.44	1.70	85.83	42.63	128.46	4.000	No	No	2.00
502	5.02	53.87	23.37	2.00	0.44	1.70	86.54	42.33	128.87	4.000	No	No	2.00
503	5.03	54.31	23.16	2.00	0.44	1.70	87.26	42.03	129.29	4.000	No	No	2.00
504	5.04	54.74	22.95	2.00	0.44	1.70	87.95	41.73	129.68	4.000	No	No	2.00
505	5.05	55.12	22.76	2.00	0.44	1.70	88.57	41.46	130.04	4.000	No	No	2.00
506	5.06	55.42	22.61	2.00	0.44	1.70	89.10	41.23	130.33	4.000	No	No	2.00
507	5.07	55.62	22.47	1.99	0.44	1.70	89.40	41.00	130.39	4.000	No	No	2.00
508	5.08	55.76	22.33	1.99	0.44	1.70	89.56	40.74	130.30	4.000	No	No	2.00
509	5.09	55.88	22.17	1.99	0.44	1.70	89.75	40.43	130.19	4.000	No	No	2.00
510	5.10	56.01	21.99	1.99	0.44	1.70	89.97	40.09	130.06	4.000	No	No	2.00
511	5.11	56.15	21.80	1.99	0.44	1.70	90.20	39.73	129.92	4.000	No	No	2.00
512	5.12	56.29	21.61	1.98	0.44	1.70	90.42	39.36	129.78	4.000	No	No	2.00
513	5.13	56.42	21.44	1.98	0.44	1.70	90.63	39.01	129.64	4.000	No	No	2.00
514	5.14	56.53	21.28	1.98	0.44	1.70	90.82	38.69	129.51	4.000	No	No	2.00
515	5.15	56.62	21.16	1.98	0.44	1.70	90.97	38.45	129.42	4.000	No	No	2.00
516	5.16	56.70	21.06	1.98	0.44	1.70	91.08	38.25	129.32	4.000	No	No	2.00
517	5.17	56.77	20.98	1.97	0.44	1.70	91.19	38.07	129.27	4.000	No	No	2.00
518	5.18	56.86	20.88	1.97	0.44	1.70	91.33	37.88	129.21	4.000	No	No	2.00
519	5.19	56.95	20.78	1.97	0.44	1.70	91.48	37.66	129.14	4.000	No	No	2.00
520	5.20	57.04	20.67	1.97	0.44	1.70	91.63	37.44	129.07	4.000	No	No	2.00
521	5.21	57.13	20.57	1.97	0.44	1.70	91.78	37.22	129.00	4.000	No	No	2.00
522	5.22	57.22	20.47	1.97	0.44	1.70	91.92	37.02	128.94	4.000	No	No	2.00
523	5.23	57.29	20.39	1.97	0.44	1.70	92.04	36.85	128.89	4.000	No	No	2.00
524	5.24	57.37	20.36	1.97	0.44	1.70	92.14	36.79	128.93	4.000	No	No	2.00
525	5.25	57.45	20.38	1.97	0.44	1.70	92.28	36.85	129.13	4.000	No	No	2.00
526	5.26	57.56	20.43	1.97	0.44	1.70	92.46	36.99	129.45	4.000	No	No	2.00
527	5.27	57.69	20.49	1.97	0.44	1.70	92.66	37.16	129.82	4.000	No	No	2.00
528	5.28	57.82	20.55	1.97	0.44	1.70	92.88	37.34	130.22	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
529	5.29	57.95	20.62	1.97	0.44	1.70	93.09	37.52	130.61	4.000	No	No	2.00
530	5.30	58.08	20.68	1.97	0.44	1.70	93.30	37.69	130.99	4.000	No	No	2.00
531	5.31	58.19	20.73	1.97	0.44	1.70	93.49	37.84	131.33	4.000	No	No	2.00
532	5.32	58.27	20.79	1.97	0.43	1.70	93.65	38.01	131.66	4.000	No	No	2.00
533	5.33	58.28	20.90	1.97	0.43	1.70	93.67	38.24	131.91	4.000	No	No	2.00
534	5.34	58.23	21.05	1.98	0.43	1.70	93.55	38.57	132.12	4.000	No	No	2.00
535	5.35	58.14	21.25	1.98	0.43	1.70	93.40	39.00	132.39	4.000	No	No	2.00
536	5.36	58.04	21.47	1.98	0.43	1.70	93.23	39.46	132.69	4.000	No	No	2.00
537	5.37	57.93	21.70	1.98	0.43	1.70	93.06	39.94	132.99	4.000	No	No	2.00
538	5.38	57.82	21.93	1.99	0.43	1.70	92.88	40.40	133.28	4.000	No	No	2.00
539	5.39	57.73	22.14	1.99	0.43	1.70	92.62	40.81	133.43	4.000	No	No	2.00
540	5.40	57.64	22.33	1.99	0.43	1.70	92.38	41.17	133.55	4.000	No	No	2.00
541	5.41	57.56	22.48	1.99	0.43	1.69	92.18	41.46	133.63	4.000	No	No	2.00
542	5.42	57.47	22.62	2.00	0.43	1.69	91.97	41.70	133.68	4.000	No	No	2.00
543	5.43	57.37	22.76	2.00	0.43	1.69	91.73	41.95	133.69	4.000	No	No	2.00
544	5.44	57.25	22.92	2.00	0.43	1.69	91.47	42.23	133.70	4.000	No	No	2.00
545	5.45	57.12	23.09	2.00	0.43	1.69	91.18	42.53	133.72	4.000	No	No	2.00
546	5.46	56.99	23.27	2.00	0.43	1.69	90.89	42.84	133.73	4.000	No	No	2.00
547	5.47	56.86	23.44	2.01	0.43	1.69	90.61	43.13	133.74	4.000	No	No	2.00
548	5.48	56.74	23.60	2.01	0.43	1.69	90.35	43.39	133.74	4.000	No	No	2.00
549	5.49	56.64	23.73	2.01	0.43	1.68	90.12	43.61	133.72	4.000	No	No	2.00
550	5.50	56.58	23.81	2.01	0.43	1.68	89.94	43.73	133.67	4.000	No	No	2.00
551	5.51	56.55	23.85	2.01	0.43	1.68	89.88	43.78	133.66	4.000	No	No	2.00
552	5.52	56.55	23.85	2.01	0.43	1.68	89.82	43.77	133.59	4.000	No	No	2.00
553	5.53	56.55	23.85	2.01	0.43	1.68	89.77	43.76	133.53	4.000	No	No	2.00
554	5.54	56.55	23.85	2.01	0.43	1.68	89.71	43.75	133.46	4.000	No	No	2.00
555	5.55	56.55	23.85	2.01	0.43	1.68	89.65	43.75	133.40	4.000	No	No	2.00
556	5.56	56.55	23.85	2.01	0.43	1.68	89.60	43.74	133.34	4.000	No	No	2.00
557	5.57	56.55	23.85	2.01	0.43	1.68	89.54	43.73	133.27	4.000	No	No	2.00
558	5.58	56.54	23.85	2.01	0.43	1.67	89.49	43.73	133.22	4.000	No	No	2.00
559	5.59	56.50	23.87	2.01	0.43	1.67	89.39	43.75	133.13	4.000	No	No	2.00
560	5.60	56.44	23.90	2.01	0.43	1.67	89.22	43.78	133.00	4.000	No	No	2.00
561	5.61	56.34	23.95	2.01	0.43	1.67	89.03	43.83	132.86	4.000	No	No	2.00
562	5.62	56.24	24.00	2.01	0.43	1.67	88.83	43.89	132.71	4.000	No	No	2.00
563	5.63	56.14	24.05	2.01	0.43	1.67	88.62	43.94	132.56	4.000	No	No	2.00
564	5.64	56.03	24.10	2.01	0.43	1.67	88.41	44.00	132.41	4.000	No	No	2.00
565	5.65	55.93	24.14	2.01	0.43	1.67	88.21	44.06	132.26	4.000	No	No	2.00
566	5.66	55.84	24.19	2.01	0.44	1.67	88.02	44.10	132.13	4.000	No	No	2.00
567	5.67	55.77	24.23	2.02	0.44	1.67	87.86	44.16	132.02	4.000	No	No	2.00
568	5.68	55.69	24.29	2.02	0.44	1.67	87.71	44.25	131.95	4.000	No	No	2.00
569	5.69	55.61	24.38	2.02	0.44	1.67	87.52	44.36	131.88	4.000	No	No	2.00
570	5.70	55.51	24.47	2.02	0.44	1.66	87.31	44.50	131.82	4.000	No	No	2.00
571	5.71	55.41	24.58	2.02	0.44	1.66	87.09	44.65	131.75	4.000	No	No	2.00
572	5.72	55.30	24.69	2.02	0.44	1.66	86.87	44.81	131.68	4.000	No	No	2.00
573	5.73	55.20	24.79	2.02	0.44	1.66	86.65	44.96	131.61	4.000	No	No	2.00
574	5.74	55.10	24.89	2.02	0.44	1.66	86.45	45.09	131.54	4.000	No	No	2.00
575	5.75	55.02	24.97	2.02	0.44	1.66	86.26	45.20	131.46	4.000	No	No	2.00
576	5.76	54.98	25.03	2.03	0.44	1.66	86.12	45.28	131.41	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
577	5.77	54.96	25.08	2.03	0.44	1.66	86.06	45.36	131.42	4.000	No	No	2.00
578	5.78	54.96	25.13	2.03	0.44	1.66	85.99	45.43	131.42	4.000	No	No	2.00
579	5.79	54.96	25.18	2.03	0.44	1.65	85.93	45.50	131.43	4.000	No	No	2.00
580	5.80	54.96	25.23	2.03	0.44	1.65	85.86	45.59	131.45	4.000	No	No	2.00
581	5.81	54.96	25.29	2.03	0.44	1.65	85.80	45.67	131.47	4.000	No	No	2.00
582	5.82	54.96	25.34	2.03	0.44	1.65	85.73	45.75	131.48	4.000	No	No	2.00
583	5.83	54.96	25.39	2.03	0.44	1.65	85.67	45.82	131.49	4.000	No	No	2.00
584	5.84	54.96	25.42	2.03	0.44	1.65	85.61	45.86	131.47	4.000	No	No	2.00
585	5.85	54.96	25.42	2.03	0.44	1.65	85.56	45.85	131.41	4.000	No	No	2.00
586	5.86	54.96	25.39	2.03	0.44	1.65	85.51	45.79	131.31	4.000	No	No	2.00
587	5.87	54.96	25.34	2.03	0.44	1.65	85.47	45.70	131.18	4.000	No	No	2.00
588	5.88	54.96	25.29	2.03	0.44	1.65	85.43	45.61	131.04	4.000	No	No	2.00
589	5.89	54.96	25.24	2.03	0.44	1.64	85.40	45.51	130.91	4.000	No	No	2.00
590	5.90	54.96	25.18	2.03	0.44	1.64	85.36	45.41	130.77	4.000	No	No	2.00
591	5.91	54.96	25.13	2.03	0.44	1.64	85.32	45.32	130.63	4.000	No	No	2.00
592	5.92	54.96	25.09	2.03	0.44	1.64	85.28	45.23	130.51	4.000	No	No	2.00
593	5.93	54.96	25.07	2.03	0.44	1.64	85.23	45.19	130.42	4.000	No	No	2.00
594	5.94	54.96	25.08	2.03	0.44	1.64	85.18	45.20	130.38	4.000	No	No	2.00
595	5.95	54.96	25.12	2.03	0.44	1.64	85.12	45.26	130.38	4.000	No	No	2.00
596	5.96	54.96	25.17	2.03	0.44	1.64	85.05	45.34	130.39	4.000	No	No	2.00
597	5.97	54.96	25.22	2.03	0.44	1.64	84.99	45.42	130.41	4.000	No	No	2.00
598	5.98	54.96	25.28	2.03	0.44	1.64	84.92	45.50	130.43	4.000	No	No	2.00
599	5.99	54.96	25.33	2.03	0.44	1.63	84.86	45.58	130.44	4.000	No	No	2.00
600	6.00	54.96	25.38	2.03	0.44	1.63	84.80	45.66	130.45	4.000	No	No	2.00
601	6.01	54.96	25.43	2.03	0.44	1.63	84.74	45.72	130.46	4.000	No	No	2.00
602	6.02	54.96	25.48	2.03	0.44	1.63	84.67	45.80	130.47	4.000	No	No	2.00
603	6.03	54.96	25.55	2.03	0.44	1.63	84.61	45.90	130.51	4.000	No	No	2.00
604	6.04	54.96	25.64	2.03	0.44	1.63	84.54	46.04	130.58	4.000	No	No	2.00
605	6.05	54.96	25.74	2.03	0.44	1.62	84.27	46.16	130.44	4.000	No	No	2.00
606	6.06	54.96	25.85	2.04	0.44	1.62	84.20	46.33	130.52	4.000	No	No	2.00
607	6.07	54.96	25.96	2.04	0.44	1.62	84.12	46.49	130.61	4.000	No	No	2.00
608	6.08	54.96	26.06	2.04	0.44	1.62	84.04	46.64	130.69	4.000	No	No	2.00
609	6.09	54.96	26.16	2.04	0.44	1.62	83.97	46.78	130.75	4.000	No	No	2.00
610	6.10	54.97	26.22	2.04	0.44	1.62	83.91	46.86	130.77	4.000	No	No	2.00
611	6.11	55.02	26.23	2.04	0.44	1.61	83.90	46.89	130.79	4.000	No	No	2.00
612	6.12	55.09	26.21	2.04	0.44	1.61	83.97	46.86	130.83	4.000	No	No	2.00
613	6.13	55.20	26.16	2.04	0.44	1.61	84.06	46.80	130.86	4.000	No	No	2.00
614	6.14	55.31	26.10	2.04	0.44	1.61	84.17	46.73	130.90	4.000	No	No	2.00
615	6.15	55.43	26.05	2.04	0.44	1.61	84.29	46.66	130.95	4.000	No	No	2.00
616	6.16	55.55	25.99	2.04	0.44	1.61	84.40	46.59	130.99	4.000	No	No	2.00
617	6.17	55.66	25.94	2.04	0.44	1.61	84.51	46.52	131.03	4.000	No	No	2.00
618	6.18	55.76	25.89	2.04	0.44	1.61	84.59	46.46	131.06	4.000	No	No	2.00
619	6.19	55.89	25.81	2.04	0.44	1.60	84.66	46.35	131.01	4.000	No	No	2.00
620	6.20	56.08	25.68	2.03	0.44	1.60	84.90	46.16	131.06	4.000	No	No	2.00
621	6.21	56.35	25.47	2.03	0.44	1.60	85.25	45.88	131.13	4.000	No	No	2.00
622	6.22	56.67	25.22	2.03	0.44	1.60	85.67	45.54	131.21	4.000	No	No	2.00
623	6.23	57.01	24.96	2.02	0.44	1.60	86.12	45.16	131.29	4.000	No	No	2.00
624	6.24	57.36	24.69	2.02	0.43	1.60	86.59	44.77	131.36	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
625	6.25	57.71	24.43	2.02	0.43	1.60	87.04	44.38	131.42	4.000	No	No	2.00
626	6.26	58.02	24.19	2.01	0.43	1.59	87.46	44.01	131.47	4.000	No	No	2.00
627	6.27	58.31	23.97	2.01	0.43	1.59	87.81	43.68	131.48	4.000	No	No	2.00
628	6.28	58.66	23.74	2.01	0.43	1.59	88.15	43.29	131.44	4.000	No	No	2.00
629	6.29	59.14	23.45	2.01	0.43	1.59	88.83	42.85	131.68	4.000	No	No	2.00
630	6.30	59.77	23.08	2.00	0.43	1.59	89.69	42.27	131.95	4.000	No	No	2.00
631	6.31	60.48	22.66	2.00	0.43	1.59	90.66	41.59	132.25	4.000	No	No	2.00
632	6.32	61.24	22.23	1.99	0.43	1.58	91.69	40.85	132.54	4.000	No	No	2.00
633	6.33	61.99	21.79	1.98	0.43	1.58	92.72	40.09	132.82	4.000	No	No	2.00
634	6.34	62.72	21.38	1.98	0.43	1.58	93.71	39.34	133.06	4.000	No	No	2.00
635	6.35	63.37	21.02	1.98	0.43	1.58	94.60	38.65	133.25	4.000	No	No	2.00
636	6.36	63.96	20.71	1.97	0.43	1.58	95.34	38.04	133.38	4.000	No	No	2.00
637	6.37	64.57	20.42	1.97	0.43	1.58	96.05	37.47	133.52	4.000	No	No	2.00
638	6.38	65.30	20.12	1.96	0.43	1.57	97.03	36.89	133.92	4.000	No	No	2.00
639	6.39	66.18	19.77	1.96	0.43	1.57	98.20	36.20	134.40	4.000	No	No	2.00
640	6.40	67.15	19.40	1.95	0.43	1.57	99.50	35.43	134.92	4.000	No	No	2.00
641	6.41	68.15	19.01	1.95	0.43	1.57	100.84	34.62	135.46	4.000	No	No	2.00
642	6.42	69.15	18.64	1.95	0.43	1.56	102.17	33.80	135.97	4.000	No	No	2.00
643	6.43	70.08	18.29	1.94	0.43	1.56	103.41	33.02	136.43	4.000	No	No	2.00
644	6.44	70.90	18.00	1.94	0.42	1.56	104.49	32.33	136.82	4.000	No	No	2.00
645	6.45	71.61	17.74	1.93	0.42	1.56	105.36	31.72	137.08	4.000	No	No	2.00
646	6.46	72.29	17.50	1.93	0.42	1.56	106.15	31.12	137.26	4.000	No	No	2.00
647	6.47	73.05	17.24	1.93	0.42	1.55	107.14	30.46	137.60	4.000	No	No	2.00
648	6.48	73.92	16.93	1.92	0.42	1.55	108.28	29.70	137.98	4.000	No	No	2.00
649	6.49	74.86	16.61	1.92	0.42	1.55	109.53	28.87	138.39	4.000	No	No	2.00
650	6.50	75.82	16.29	1.92	0.42	1.55	110.80	28.01	138.81	4.000	No	No	2.00
651	6.51	76.75	15.98	1.91	0.42	1.54	112.03	27.17	139.20	4.000	No	No	2.00
652	6.52	77.61	15.70	1.91	0.42	1.54	113.15	26.39	139.54	4.000	No	No	2.00
653	6.53	78.34	15.46	1.91	0.42	1.54	114.11	25.73	139.83	4.000	No	No	2.00
654	6.54	78.96	15.26	1.90	0.42	1.54	114.82	25.15	139.97	4.000	No	No	2.00
655	6.55	79.56	15.07	1.90	0.42	1.54	115.52	24.59	140.11	4.000	No	No	2.00
656	6.56	80.23	14.86	1.90	0.42	1.54	116.38	23.98	140.36	4.000	No	No	2.00
657	6.57	80.98	14.63	1.90	0.42	1.53	117.35	23.29	140.64	4.000	No	No	2.00
658	6.58	81.77	14.38	1.89	0.42	1.53	118.38	22.55	140.93	4.000	No	No	2.00
659	6.59	82.57	14.14	1.89	0.42	1.53	119.41	21.82	141.22	4.000	No	No	2.00
660	6.60	83.33	13.91	1.89	0.42	1.53	120.39	21.11	141.50	4.000	No	No	2.00
661	6.61	84.01	13.71	1.88	0.42	1.53	121.26	20.48	141.74	4.000	No	No	2.00
662	6.62	84.56	13.55	1.88	0.42	1.53	121.97	19.98	141.95	4.000	No	No	2.00
663	6.63	85.00	13.42	1.88	0.42	1.52	122.41	19.57	141.98	4.000	No	No	2.00
664	6.64	85.38	13.31	1.88	0.42	1.52	122.84	19.21	142.05	4.000	No	No	2.00
665	6.65	85.80	13.19	1.88	0.42	1.52	123.34	18.83	142.17	4.000	No	No	2.00
666	6.66	86.26	13.05	1.88	0.41	1.52	123.91	18.40	142.31	4.000	No	No	2.00
667	6.67	86.74	12.91	1.87	0.41	1.52	124.49	17.96	142.46	4.000	No	No	2.00
668	6.68	87.22	12.78	1.87	0.41	1.52	125.07	17.53	142.60	4.000	No	No	2.00
669	6.69	87.66	12.65	1.87	0.41	1.52	125.61	17.13	142.74	4.000	No	No	2.00
670	6.70	88.05	12.55	1.87	0.41	1.51	126.07	16.78	142.85	4.000	No	No	2.00
671	6.71	88.31	12.48	1.87	0.41	1.51	126.41	16.59	143.00	4.000	No	No	2.00
672	6.72	88.46	12.47	1.87	0.41	1.51	126.43	16.54	142.97	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
673	6.73	88.53	12.50	1.87	0.41	1.51	126.42	16.64	143.06	4.000	No	No	2.00
674	6.74	88.60	12.53	1.87	0.41	1.51	126.42	16.76	143.18	4.000	No	No	2.00
675	6.75	88.68	12.57	1.87	0.41	1.51	126.42	16.89	143.32	4.000	No	No	2.00
676	6.76	88.76	12.61	1.87	0.41	1.51	126.43	17.03	143.46	4.000	No	No	2.00
677	6.77	88.84	12.65	1.87	0.41	1.51	126.43	17.16	143.59	4.000	No	No	2.00
678	6.78	88.91	12.68	1.87	0.41	1.50	126.43	17.28	143.70	4.000	No	No	2.00
679	6.79	88.95	12.72	1.87	0.41	1.50	126.41	17.40	143.82	4.000	No	No	2.00
680	6.80	88.92	12.79	1.87	0.41	1.50	126.31	17.63	143.94	4.000	No	No	2.00
681	6.81	88.79	12.90	1.87	0.41	1.50	125.98	18.00	143.98	4.000	No	No	2.00
682	6.82	88.59	13.06	1.88	0.41	1.50	125.59	18.52	144.11	4.000	No	No	2.00
683	6.83	88.37	13.23	1.88	0.41	1.50	125.15	19.10	144.25	4.000	No	No	2.00
684	6.84	88.13	13.42	1.88	0.41	1.50	124.70	19.71	144.41	4.000	No	No	2.00
685	6.85	87.89	13.60	1.88	0.41	1.50	124.25	20.31	144.56	4.000	No	No	2.00
686	6.86	87.66	13.78	1.88	0.41	1.49	123.81	20.89	144.70	4.000	No	No	2.00
687	6.87	87.46	13.93	1.89	0.41	1.49	123.42	21.40	144.82	4.000	No	No	2.00
688	6.88	87.26	14.08	1.89	0.41	1.49	123.07	21.88	144.95	4.000	No	No	2.00
689	6.89	87.04	14.25	1.89	0.41	1.49	122.68	22.42	145.10	4.000	No	No	2.00
690	6.90	86.75	14.45	1.89	0.41	1.49	122.15	23.08	145.23	4.000	No	No	2.00
691	6.91	86.40	14.71	1.90	0.41	1.49	121.54	23.88	145.42	4.000	No	No	2.00
692	6.92	86.01	14.98	1.90	0.41	1.49	120.87	24.74	145.62	4.000	No	No	2.00
693	6.93	85.61	15.27	1.90	0.41	1.49	120.19	25.63	145.82	4.000	No	No	2.00
694	6.94	85.22	15.55	1.91	0.41	1.48	119.52	26.49	146.00	4.000	No	No	2.00
695	6.95	84.85	15.81	1.91	0.41	1.48	118.89	27.28	146.16	4.000	No	No	2.00
696	6.96	84.53	16.04	1.91	0.41	1.48	118.33	27.96	146.29	4.000	No	No	2.00
697	6.97	84.25	16.23	1.92	0.41	1.48	117.87	28.51	146.38	4.000	No	No	2.00
698	6.98	83.97	16.40	1.92	0.41	1.48	117.43	29.01	146.44	4.000	No	No	2.00
699	6.99	83.65	16.58	1.92	0.41	1.48	116.91	29.52	146.43	4.000	No	No	2.00
700	7.00	83.29	16.79	1.92	0.41	1.48	116.32	30.10	146.42	4.000	No	No	2.00
701	7.01	82.89	17.01	1.93	0.41	1.48	115.70	30.71	146.41	4.000	No	No	2.00
702	7.02	82.49	17.24	1.93	0.41	1.48	115.06	31.33	146.40	4.000	No	No	2.00
703	7.03	82.10	17.46	1.93	0.41	1.48	114.45	31.92	146.37	4.000	No	No	2.00
704	7.04	81.75	17.66	1.93	0.41	1.47	113.88	32.46	146.34	4.000	No	No	2.00
705	7.05	81.46	17.83	1.94	0.41	1.47	113.39	32.89	146.29	4.000	No	No	2.00
706	7.06	81.25	17.97	1.94	0.41	1.47	113.04	33.25	146.29	4.000	No	No	2.00
707	7.07	81.10	18.09	1.94	0.41	1.47	112.80	33.57	146.38	4.000	No	No	2.00
708	7.08	80.96	18.23	1.94	0.41	1.47	112.53	33.91	146.44	4.000	No	No	2.00
709	7.09	80.81	18.37	1.94	0.41	1.47	112.24	34.29	146.53	4.000	No	No	2.00
710	7.10	80.66	18.53	1.94	0.41	1.47	111.93	34.68	146.61	4.000	No	No	2.00
711	7.11	80.50	18.68	1.95	0.41	1.47	111.63	35.07	146.69	4.000	No	No	2.00
712	7.12	80.34	18.83	1.95	0.41	1.47	111.33	35.43	146.76	4.000	No	No	2.00
713	7.13	80.21	18.96	1.95	0.41	1.47	111.07	35.75	146.82	4.000	No	No	2.00
714	7.14	80.14	19.04	1.95	0.41	1.46	110.85	35.95	146.79	4.000	No	No	2.00
715	7.15	80.19	19.06	1.95	0.41	1.46	110.85	36.00	146.85	4.000	No	No	2.00
716	7.16	80.34	19.02	1.95	0.41	1.46	111.02	35.92	146.94	4.000	No	No	2.00
717	7.17	80.55	18.96	1.95	0.41	1.46	111.24	35.78	147.01	4.000	No	No	2.00
718	7.18	80.78	18.89	1.95	0.41	1.46	111.48	35.62	147.10	4.000	No	No	2.00
719	7.19	81.02	18.81	1.95	0.41	1.46	111.74	35.45	147.19	4.000	No	No	2.00
720	7.20	81.26	18.74	1.95	0.41	1.46	111.99	35.29	147.27	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
721	7.21	81.48	18.68	1.95	0.41	1.46	112.22	35.13	147.35	4.000	No	No	2.00
722	7.22	81.67	18.62	1.95	0.41	1.46	112.41	35.00	147.41	4.000	No	No	2.00
723	7.23	81.89	18.53	1.94	0.41	1.46	112.57	34.78	147.35	4.000	No	No	2.00
724	7.24	82.17	18.40	1.94	0.41	1.45	112.92	34.45	147.36	4.000	No	No	2.00
725	7.25	82.55	18.20	1.94	0.41	1.45	113.39	33.95	147.34	4.000	No	No	2.00
726	7.26	82.99	17.98	1.94	0.41	1.45	113.94	33.37	147.31	4.000	No	No	2.00
727	7.27	83.46	17.74	1.93	0.41	1.45	114.54	32.74	147.28	4.000	No	No	2.00
728	7.28	83.94	17.49	1.93	0.41	1.45	115.15	32.09	147.23	4.000	No	No	2.00
729	7.29	84.41	17.25	1.93	0.41	1.45	115.74	31.45	147.18	4.000	No	No	2.00
730	7.30	84.83	17.04	1.93	0.41	1.45	116.27	30.85	147.12	4.000	No	No	2.00
731	7.31	85.21	16.85	1.92	0.41	1.45	116.72	30.32	147.05	4.000	No	No	2.00
732	7.32	85.59	16.66	1.92	0.41	1.45	117.12	29.80	146.92	4.000	No	No	2.00
733	7.33	86.03	16.46	1.92	0.41	1.45	117.67	29.23	146.89	4.000	No	No	2.00
734	7.34	86.56	16.22	1.92	0.41	1.45	118.35	28.53	146.88	4.000	No	No	2.00
735	7.35	87.17	15.95	1.91	0.41	1.45	119.12	27.74	146.87	4.000	No	No	2.00
736	7.36	87.80	15.66	1.91	0.41	1.45	119.94	26.90	146.84	4.000	No	No	2.00
737	7.37	88.44	15.38	1.90	0.41	1.44	120.76	26.04	146.80	4.000	No	No	2.00
738	7.38	89.05	15.11	1.90	0.41	1.44	121.54	25.22	146.76	4.000	No	No	2.00
739	7.39	89.59	14.87	1.90	0.41	1.44	122.23	24.47	146.70	4.000	No	No	2.00
740	7.40	90.06	14.66	1.90	0.41	1.44	122.80	23.81	146.61	4.000	No	No	2.00
741	7.41	90.54	14.45	1.89	0.41	1.44	123.32	23.16	146.48	4.000	No	No	2.00
742	7.42	91.08	14.26	1.89	0.41	1.44	123.99	22.56	146.54	4.000	No	No	2.00
743	7.43	91.71	14.03	1.89	0.41	1.44	124.78	21.84	146.62	4.000	No	No	2.00
744	7.44	92.41	13.78	1.88	0.41	1.44	125.65	21.05	146.70	4.000	No	No	2.00
745	7.45	93.13	13.53	1.88	0.41	1.44	126.56	20.22	146.78	4.000	No	No	2.00
746	7.46	93.83	13.28	1.88	0.41	1.44	127.45	19.41	146.86	4.000	No	No	2.00
747	7.47	94.49	13.04	1.88	0.41	1.44	128.28	18.65	146.92	4.000	No	No	2.00
748	7.48	95.07	12.84	1.87	0.41	1.44	128.99	17.99	146.98	4.000	No	No	2.00
749	7.49	95.56	12.70	1.87	0.41	1.43	129.54	17.51	147.04	4.000	No	No	2.00
750	7.50	96.03	12.58	1.87	0.41	1.43	130.00	17.14	147.14	4.000	No	No	2.00
751	7.51	96.54	12.48	1.87	0.41	1.43	130.58	16.82	147.40	4.000	No	No	2.00
752	7.52	97.13	12.37	1.87	0.41	1.43	131.26	16.45	147.71	4.000	No	No	2.00
753	7.53	97.75	12.24	1.87	0.41	1.43	131.98	16.05	148.04	4.000	No	No	2.00
754	7.54	98.39	12.12	1.86	0.40	1.43	132.72	15.65	148.37	4.000	No	No	2.00
755	7.55	99.01	12.00	1.86	0.40	1.43	133.43	15.27	148.69	4.000	No	No	2.00
756	7.56	99.58	11.89	1.86	0.40	1.42	134.07	14.92	148.99	4.000	No	No	2.00
757	7.57	100.07	11.80	1.86	0.40	1.42	134.61	14.63	149.24	4.000	No	No	2.00
758	7.58	100.54	11.72	1.86	0.40	1.42	135.04	14.36	149.39	4.000	No	No	2.00
759	7.59	101.05	11.62	1.86	0.40	1.42	135.60	14.06	149.65	4.000	No	No	2.00
760	7.60	101.65	11.51	1.86	0.40	1.42	136.29	13.69	149.98	4.000	No	No	2.00
761	7.61	102.33	11.38	1.85	0.40	1.42	137.07	13.28	150.35	4.000	No	No	2.00
762	7.62	103.05	11.24	1.85	0.40	1.42	137.89	12.85	150.73	4.000	No	No	2.00
763	7.63	103.77	11.11	1.85	0.40	1.41	138.71	12.42	151.13	4.000	No	No	2.00
764	7.64	104.45	10.98	1.85	0.40	1.41	139.48	12.02	151.50	4.000	No	No	2.00
765	7.65	105.05	10.88	1.85	0.40	1.41	140.16	11.68	151.84	4.000	No	No	2.00
766	7.66	105.55	10.80	1.85	0.40	1.41	140.70	11.46	152.15	4.000	No	No	2.00
767	7.67	105.99	10.77	1.85	0.40	1.41	141.06	11.37	152.42	4.000	No	No	2.00
768	7.68	106.42	10.78	1.85	0.40	1.41	141.47	11.39	152.85	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
769	7.69	106.92	10.79	1.85	0.40	1.41	141.95	11.44	153.39	4.000	No	No	2.00
770	7.70	107.46	10.80	1.85	0.40	1.40	142.49	11.50	153.98	4.000	No	No	2.00
771	7.71	108.02	10.81	1.85	0.39	1.40	143.04	11.55	154.59	4.000	No	No	2.00
772	7.72	108.57	10.82	1.85	0.39	1.40	143.59	11.61	155.19	4.000	No	No	2.00
773	7.73	109.09	10.83	1.85	0.39	1.40	144.09	11.66	155.75	4.000	No	No	2.00
774	7.74	109.53	10.84	1.85	0.39	1.40	144.51	11.72	156.24	4.000	No	No	2.00
775	7.75	109.89	10.86	1.85	0.39	1.39	144.83	11.80	156.63	4.000	No	No	2.00
776	7.76	110.21	10.89	1.85	0.39	1.39	145.04	11.91	156.94	4.000	No	No	2.00
777	7.77	110.53	10.93	1.85	0.39	1.39	145.31	12.05	157.36	4.000	No	No	2.00
778	7.78	110.89	10.97	1.85	0.39	1.39	145.63	12.20	157.83	4.000	No	No	2.00
779	7.79	111.29	11.01	1.85	0.39	1.39	145.98	12.36	158.34	4.000	No	No	2.00
780	7.80	111.69	11.05	1.85	0.39	1.39	146.33	12.53	158.86	4.000	No	No	2.00
781	7.81	112.07	11.10	1.85	0.39	1.38	146.67	12.69	159.36	4.000	No	No	2.00
782	7.82	112.43	11.14	1.85	0.39	1.38	146.97	12.84	159.81	4.000	No	No	2.00
783	7.83	112.72	11.17	1.85	0.39	1.38	147.22	12.96	160.18	4.000	No	No	2.00
784	7.84	112.98	11.17	1.85	0.39	1.38	147.40	12.99	160.39	4.000	No	No	2.00
785	7.85	113.22	11.16	1.85	0.39	1.38	147.59	12.94	160.53	4.000	No	No	2.00
786	7.86	113.49	11.12	1.85	0.39	1.38	147.84	12.83	160.68	4.000	No	No	2.00
787	7.87	113.79	11.08	1.85	0.38	1.38	148.14	12.70	160.84	4.000	No	No	2.00
788	7.88	114.11	11.04	1.85	0.38	1.38	148.45	12.56	161.01	4.000	No	No	2.00
789	7.89	114.43	11.00	1.85	0.38	1.38	148.76	12.42	161.18	4.000	No	No	2.00
790	7.90	114.73	10.96	1.85	0.38	1.37	149.05	12.29	161.34	4.000	No	No	2.00
791	7.91	115.00	10.92	1.85	0.38	1.37	149.30	12.18	161.48	4.000	No	No	2.00
792	7.92	115.18	10.91	1.85	0.38	1.37	149.48	12.15	161.64	4.000	No	No	2.00
793	7.93	115.28	10.93	1.85	0.38	1.37	149.47	12.22	161.69	4.000	No	No	2.00
794	7.94	115.30	10.98	1.85	0.38	1.37	149.38	12.39	161.76	4.000	No	No	2.00
795	7.95	115.30	11.04	1.85	0.38	1.37	149.28	12.60	161.88	4.000	No	No	2.00
796	7.96	115.30	11.11	1.85	0.38	1.37	149.18	12.83	162.01	4.000	No	No	2.00
797	7.97	115.30	11.17	1.85	0.38	1.37	149.08	13.06	162.14	4.000	No	No	2.00
798	7.98	115.30	11.24	1.85	0.38	1.37	148.98	13.29	162.27	4.000	No	No	2.00
799	7.99	115.30	11.30	1.85	0.38	1.37	148.88	13.51	162.39	4.000	No	No	2.00
800	8.00	115.30	11.36	1.85	0.38	1.37	148.78	13.71	162.49	4.000	No	No	2.00
801	8.01	115.30	11.42	1.86	0.38	1.37	148.72	13.91	162.63	0.400	No	No	0.75
802	8.02	115.30	11.48	1.86	0.38	1.36	148.65	14.15	162.80	0.402	No	No	0.75
803	8.03	115.30	11.57	1.86	0.38	1.36	148.57	14.47	163.04	0.405	No	No	0.75
804	8.04	115.30	11.68	1.86	0.38	1.36	148.48	14.83	163.31	0.409	No	No	0.76
805	8.05	115.30	11.78	1.86	0.38	1.36	148.38	15.22	163.60	0.412	No	No	0.77
806	8.06	115.30	11.89	1.86	0.38	1.36	148.29	15.61	163.90	0.416	No	No	0.77
807	8.07	115.30	12.00	1.86	0.38	1.36	148.20	15.99	164.19	0.419	No	No	0.78
808	8.08	115.30	12.09	1.86	0.38	1.36	148.11	16.34	164.45	0.423	No	No	0.79
809	8.09	115.32	12.16	1.86	0.38	1.36	148.04	16.58	164.62	0.425	No	No	0.79
810	8.10	115.42	12.17	1.86	0.38	1.36	148.08	16.63	164.71	0.426	No	No	0.79
811	8.11	115.61	12.13	1.86	0.38	1.36	148.32	16.47	164.80	0.427	No	No	0.79
812	8.12	115.89	12.04	1.86	0.38	1.36	148.64	16.18	164.82	0.427	No	No	0.79
813	8.13	116.19	11.95	1.86	0.38	1.36	148.99	15.85	164.84	0.428	No	No	0.79
814	8.14	116.51	11.85	1.86	0.38	1.36	149.36	15.50	164.87	0.428	No	No	0.79
815	8.15	116.83	11.75	1.86	0.38	1.36	149.73	15.16	164.89	0.428	No	No	0.79
816	8.16	117.13	11.66	1.86	0.38	1.36	150.08	14.83	164.92	0.429	No	No	0.79

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
817	8.17	117.40	11.57	1.86	0.38	1.36	150.39	14.55	164.94	0.429	No	No	0.79
818	8.18	117.66	11.48	1.86	0.38	1.36	150.65	14.23	164.88	0.428	No	No	0.79
819	8.19	117.98	11.36	1.85	0.38	1.36	151.01	13.79	164.80	0.427	No	No	0.79
820	8.20	118.40	11.18	1.85	0.38	1.35	151.54	13.18	164.72	0.426	No	No	0.79
821	8.21	118.89	10.96	1.85	0.38	1.35	152.18	12.43	164.61	0.425	No	No	0.78
822	8.22	119.44	10.72	1.85	0.38	1.35	152.87	11.63	164.49	0.423	No	No	0.78
823	8.23	120.00	10.48	1.84	0.38	1.35	153.58	10.80	164.38	0.422	No	No	0.78
824	8.24	120.55	10.24	1.84	0.38	1.35	154.27	10.01	164.28	0.421	No	No	0.77
825	8.25	121.06	10.01	1.84	0.38	1.35	154.91	9.29	164.20	0.420	No	No	0.77
826	8.26	121.50	9.82	1.84	0.38	1.35	155.46	8.68	164.14	0.419	No	No	0.77
827	8.27	121.93	9.65	1.83	0.38	1.35	155.90	8.17	164.07	0.418	No	No	0.77
828	8.28	122.41	9.49	1.83	0.38	1.35	156.45	7.68	164.14	0.419	No	No	0.77
829	8.29	122.99	9.32	1.83	0.38	1.35	157.14	7.16	164.30	0.421	No	No	0.77
830	8.30	123.65	9.11	1.83	0.38	1.35	157.92	6.57	164.50	0.423	No	No	0.78
831	8.31	124.36	8.89	1.82	0.38	1.35	158.76	5.97	164.73	0.426	No	No	0.78
832	8.32	125.08	8.67	1.82	0.38	1.35	159.60	5.38	164.99	0.430	No	No	0.79
833	8.33	125.77	8.45	1.82	0.38	1.35	160.41	4.84	165.26	0.433	No	No	0.79
834	8.34	126.40	8.26	1.82	0.38	1.35	161.14	4.38	165.52	0.437	No	No	0.80
835	8.35	126.94	8.10	1.81	0.38	1.35	161.74	4.01	165.75	0.440	No	No	0.80
836	8.36	127.41	7.99	1.81	0.38	1.35	162.19	3.76	165.95	0.442	No	No	0.81
837	8.37	127.89	7.87	1.81	0.38	1.35	162.69	3.51	166.20	0.446	No	No	0.82
838	8.38	128.43	7.74	1.81	0.38	1.35	163.29	3.24	166.53	0.451	No	No	0.82
839	8.39	129.04	7.60	1.81	0.38	1.34	163.96	2.96	166.91	0.456	No	No	0.83
840	8.40	129.68	7.45	1.81	0.37	1.34	164.66	2.67	167.33	0.462	No	No	0.84
841	8.41	130.31	7.29	1.80	0.37	1.34	165.35	2.41	167.76	0.468	No	No	0.86
842	8.42	130.92	7.15	1.80	0.37	1.34	166.00	2.17	168.17	0.475	No	No	0.87
843	8.43	131.45	7.03	1.80	0.37	1.34	166.58	1.97	168.55	0.481	No	No	0.88
844	8.44	131.87	6.94	1.80	0.37	1.34	167.03	1.84	168.87	0.486	No	No	0.89
845	8.45	132.22	6.87	1.80	0.37	1.34	167.31	1.74	169.05	0.489	No	No	0.89
846	8.46	132.54	6.83	1.80	0.37	1.34	167.61	1.68	169.29	0.492	No	No	0.90
847	8.47	132.89	6.78	1.80	0.37	1.34	167.97	1.61	169.59	0.497	No	No	0.91
848	8.48	133.28	6.72	1.80	0.37	1.34	168.37	1.54	169.91	0.503	No	No	0.92
849	8.49	133.68	6.67	1.80	0.37	1.34	168.77	1.47	170.24	0.508	No	No	0.93
850	8.50	134.07	6.61	1.80	0.37	1.34	169.17	1.40	170.57	0.514	No	No	0.94
851	8.51	134.44	6.56	1.79	0.37	1.33	169.54	1.34	170.88	0.519	No	No	0.94
852	8.52	134.75	6.52	1.79	0.37	1.33	169.85	1.29	171.14	0.524	No	No	0.95
853	8.53	134.99	6.49	1.79	0.37	1.33	170.08	1.26	171.33	0.527	No	No	0.96
854	8.54	135.19	6.47	1.79	0.37	1.33	170.21	1.23	171.44	0.529	No	No	0.96
855	8.55	135.39	6.44	1.79	0.37	1.33	170.39	1.20	171.59	0.532	No	No	0.97
856	8.56	135.61	6.42	1.79	0.37	1.33	170.60	1.17	171.77	0.535	No	No	0.97
857	8.57	135.85	6.39	1.79	0.37	1.33	170.82	1.14	171.96	0.539	No	No	0.98
858	8.58	136.09	6.36	1.79	0.37	1.33	171.05	1.11	172.16	0.542	No	No	0.98
859	8.59	136.32	6.33	1.79	0.37	1.33	171.27	1.08	172.35	0.546	No	No	0.99
860	8.60	136.53	6.31	1.79	0.37	1.33	171.46	1.05	172.51	0.549	No	No	1.00
861	8.61	136.69	6.29	1.79	0.37	1.33	171.62	1.03	172.65	0.552	No	No	1.00
862	8.62	136.81	6.28	1.79	0.37	1.33	171.69	1.02	172.72	0.553	No	No	1.00
863	8.63	136.88	6.27	1.79	0.37	1.33	171.72	1.02	172.74	0.554	No	No	1.00
864	8.64	136.95	6.27	1.79	0.37	1.33	171.76	1.02	172.78	0.554	No	No	1.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
865	8.65	137.03	6.27	1.79	0.37	1.33	171.81	1.01	172.82	0.555	No	No	1.00
866	8.66	137.11	6.26	1.79	0.37	1.33	171.86	1.01	172.87	0.556	No	No	1.01
867	8.67	137.19	6.26	1.79	0.37	1.33	171.91	1.00	172.91	0.557	No	No	1.01
868	8.68	137.26	6.25	1.79	0.37	1.33	171.96	1.00	172.96	0.558	No	No	1.01
869	8.69	137.33	6.25	1.79	0.37	1.33	171.99	1.00	172.99	0.558	No	No	1.01
870	8.70	137.37	6.23	1.79	0.37	1.33	172.02	0.98	173.00	0.559	No	No	1.01
871	8.71	137.40	6.19	1.79	0.37	1.32	172.00	0.94	172.94	0.558	No	No	1.01
872	8.72	137.40	6.12	1.79	0.37	1.32	171.98	0.87	172.85	0.556	No	No	1.00
873	8.73	137.40	6.02	1.79	0.37	1.32	171.96	0.78	172.74	0.554	No	No	1.00
874	8.74	137.40	5.92	1.79	0.37	1.32	171.94	0.70	172.64	0.552	No	No	0.99
875	8.75	137.40	5.81	1.79	0.37	1.32	171.92	0.62	172.54	0.550	No	No	0.99
876	8.76	137.40	5.71	1.78	0.37	1.32	171.90	0.54	172.44	0.548	No	No	0.98
877	8.77	137.40	5.61	1.78	0.37	1.32	171.87	0.48	172.36	0.546	No	No	0.98
878	8.78	137.39	5.53	1.78	0.37	1.32	171.85	0.43	172.28	0.545	No	No	0.98
879	8.79	137.36	5.48	1.78	0.37	1.32	171.81	0.40	172.21	0.544	No	No	0.97
880	8.80	137.27	5.45	1.78	0.37	1.32	171.67	0.39	172.05	0.540	No	No	0.97
881	8.81	137.14	5.43	1.78	0.37	1.32	171.50	0.38	171.87	0.537	No	No	0.96
882	8.82	136.99	5.41	1.78	0.37	1.32	171.31	0.36	171.67	0.533	No	No	0.95
883	8.83	136.84	5.38	1.78	0.37	1.32	171.11	0.35	171.46	0.530	No	No	0.95
884	8.84	136.68	5.36	1.78	0.37	1.32	170.90	0.34	171.24	0.526	No	No	0.94
885	8.85	136.52	5.33	1.78	0.37	1.32	170.71	0.33	171.04	0.522	No	No	0.93
886	8.86	136.38	5.31	1.78	0.37	1.32	170.53	0.32	170.85	0.519	No	No	0.93
887	8.87	136.25	5.31	1.78	0.37	1.32	170.37	0.32	170.69	0.516	No	No	0.92
888	8.88	136.09	5.36	1.78	0.37	1.32	170.19	0.34	170.53	0.513	No	No	0.91
889	8.89	135.87	5.47	1.78	0.37	1.32	169.90	0.40	170.30	0.509	No	No	0.91
890	8.90	135.59	5.62	1.78	0.37	1.32	169.56	0.48	170.04	0.505	No	No	0.90
891	8.91	135.29	5.79	1.78	0.37	1.32	169.19	0.59	169.78	0.500	No	No	0.89
892	8.92	134.97	5.96	1.79	0.37	1.32	168.79	0.72	169.51	0.496	No	No	0.88
893	8.93	134.65	6.13	1.79	0.37	1.32	168.39	0.87	169.27	0.492	No	No	0.87
894	8.94	134.35	6.29	1.79	0.37	1.32	168.02	1.03	169.05	0.488	No	No	0.87
895	8.95	134.09	6.44	1.79	0.37	1.32	167.67	1.19	168.86	0.485	No	No	0.86
896	8.96	133.85	6.56	1.79	0.37	1.32	167.39	1.32	168.71	0.483	No	No	0.86
897	8.97	133.59	6.66	1.80	0.37	1.32	167.09	1.45	168.54	0.480	No	No	0.85
898	8.98	133.29	6.76	1.80	0.37	1.32	166.70	1.59	168.29	0.476	No	No	0.84
899	8.99	132.93	6.88	1.80	0.37	1.32	166.26	1.75	168.01	0.472	No	No	0.84
900	9.00	132.54	7.00	1.80	0.37	1.32	165.78	1.93	167.71	0.468	No	No	0.83
901	9.01	132.14	7.13	1.80	0.37	1.32	165.29	2.13	167.42	0.463	No	No	0.82
902	9.02	131.75	7.26	1.80	0.38	1.32	164.81	2.34	167.14	0.459	No	No	0.81
903	9.03	131.38	7.37	1.80	0.38	1.32	164.35	2.54	166.89	0.456	No	No	0.80
904	9.04	131.07	7.48	1.81	0.38	1.32	163.95	2.73	166.68	0.453	No	No	0.80
905	9.05	130.81	7.58	1.81	0.38	1.32	163.63	2.92	166.55	0.451	No	No	0.79
906	9.06	130.57	7.70	1.81	0.38	1.32	163.34	3.15	166.49	0.450	No	No	0.79
907	9.07	130.31	7.84	1.81	0.38	1.32	162.98	3.44	166.42	0.449	No	No	0.79
908	9.08	130.01	8.00	1.81	0.38	1.32	162.58	3.78	166.35	0.448	No	No	0.79
909	9.09	129.70	8.16	1.81	0.38	1.32	162.14	4.16	166.30	0.447	No	No	0.79
910	9.10	129.38	8.33	1.82	0.38	1.32	161.71	4.56	166.27	0.447	No	No	0.79
911	9.11	129.07	8.50	1.82	0.38	1.32	161.28	4.96	166.24	0.447	No	No	0.78
912	9.12	128.79	8.64	1.82	0.38	1.32	160.89	5.34	166.23	0.446	No	No	0.78

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
913	9.13	128.58	8.77	1.82	0.38	1.32	160.56	5.66	166.22	0.446	No	No	0.78
914	9.14	128.44	8.87	1.82	0.38	1.32	160.35	5.95	166.30	0.447	No	No	0.78
915	9.15	128.35	8.97	1.82	0.38	1.32	160.22	6.23	166.44	0.449	No	No	0.79
916	9.16	128.29	9.08	1.83	0.38	1.32	160.06	6.54	166.60	0.452	No	No	0.79
917	9.17	128.21	9.21	1.83	0.38	1.32	159.89	6.90	166.79	0.454	No	No	0.80
918	9.18	128.13	9.33	1.83	0.38	1.32	159.72	7.27	166.99	0.457	No	No	0.80
919	9.19	128.05	9.46	1.83	0.38	1.32	159.54	7.65	167.19	0.460	No	No	0.81
920	9.20	127.98	9.58	1.83	0.37	1.32	159.38	8.01	167.39	0.463	No	No	0.81
921	9.21	127.91	9.68	1.83	0.37	1.32	159.22	8.34	167.57	0.466	No	No	0.81
922	9.22	127.89	9.75	1.83	0.37	1.32	159.10	8.55	167.66	0.467	No	No	0.82
923	9.23	127.94	9.78	1.83	0.37	1.32	159.13	8.64	167.78	0.469	No	No	0.82
924	9.24	128.06	9.77	1.83	0.37	1.32	159.24	8.62	167.86	0.470	No	No	0.82
925	9.25	128.20	9.75	1.83	0.37	1.32	159.37	8.57	167.94	0.471	No	No	0.82
926	9.26	128.36	9.74	1.83	0.37	1.32	159.51	8.51	168.03	0.472	No	No	0.82
927	9.27	128.52	9.72	1.83	0.37	1.31	159.66	8.46	168.12	0.474	No	No	0.83
928	9.28	128.67	9.70	1.83	0.37	1.31	159.81	8.40	168.21	0.475	No	No	0.83
929	9.29	128.82	9.68	1.83	0.37	1.31	159.94	8.35	168.29	0.477	No	No	0.83
930	9.30	128.95	9.66	1.83	0.37	1.31	160.05	8.30	168.35	0.477	No	No	0.83
931	9.31	129.17	9.61	1.83	0.37	1.31	160.18	8.13	168.31	0.477	No	No	0.83
932	9.32	129.49	9.51	1.83	0.37	1.31	160.59	7.82	168.42	0.478	No	No	0.83
933	9.33	129.95	9.35	1.83	0.37	1.31	161.13	7.36	168.49	0.480	No	No	0.83
934	9.34	130.47	9.18	1.83	0.37	1.31	161.73	6.85	168.58	0.481	No	No	0.84
935	9.35	131.03	8.99	1.82	0.37	1.31	162.37	6.31	168.68	0.483	No	No	0.84
936	9.36	131.59	8.80	1.82	0.37	1.31	163.01	5.79	168.81	0.485	No	No	0.84
937	9.37	132.12	8.62	1.82	0.37	1.31	163.63	5.31	168.94	0.487	No	No	0.85
938	9.38	132.61	8.45	1.82	0.37	1.31	164.18	4.90	169.07	0.489	No	No	0.85
939	9.39	133.04	8.31	1.82	0.37	1.31	164.63	4.53	169.16	0.490	No	No	0.85
940	9.40	133.51	8.14	1.81	0.37	1.31	165.08	4.15	169.23	0.491	No	No	0.85
941	9.41	134.08	7.95	1.81	0.37	1.31	165.74	3.70	169.44	0.495	No	No	0.86
942	9.42	134.77	7.70	1.81	0.37	1.31	166.52	3.19	169.71	0.499	No	No	0.87
943	9.43	135.54	7.43	1.81	0.37	1.31	167.38	2.67	170.05	0.505	No	No	0.88
944	9.44	136.33	7.15	1.80	0.37	1.31	168.27	2.18	170.45	0.512	No	No	0.89
945	9.45	137.13	6.86	1.80	0.37	1.31	169.14	1.74	170.89	0.519	No	No	0.90
946	9.46	137.87	6.60	1.79	0.37	1.30	169.96	1.39	171.34	0.527	No	No	0.91
947	9.47	138.53	6.37	1.79	0.37	1.30	170.66	1.12	171.78	0.535	No	No	0.93
948	9.48	139.09	6.18	1.79	0.37	1.30	171.22	0.92	172.15	0.542	No	No	0.94
949	9.49	139.61	6.01	1.79	0.37	1.30	171.69	0.77	172.46	0.548	No	No	0.95
950	9.50	140.17	5.84	1.79	0.37	1.30	172.27	0.64	172.90	0.557	No	No	0.96
951	9.51	140.82	5.64	1.78	0.37	1.30	172.94	0.50	173.44	0.567	No	No	0.98
952	9.52	141.52	5.43	1.78	0.36	1.30	173.67	0.38	174.05	0.580	No	No	1.00
953	9.53	142.24	5.22	1.78	0.36	1.30	174.41	0.28	174.69	0.593	No	No	1.03
954	9.54	142.94	5.00	1.78	0.36	1.30	175.12	0.20	175.33	0.607	No	No	1.05
955	9.55	143.59	4.81	1.77	0.36	1.30	175.78	0.14	175.93	0.621	No	No	1.08
956	9.56	144.09	4.65	1.77	0.36	1.29	176.34	0.11	176.45	0.633	No	No	1.10
957	9.57	144.10	4.56	1.77	0.36	1.29	176.58	0.09	176.67	0.639	No	No	1.11
958	9.58	143.60	4.52	1.77	0.36	1.29	175.73	0.08	175.82	0.619	No	No	1.07
959	9.59	142.65	4.53	1.77	0.36	1.30	174.69	0.08	174.78	0.595	No	No	1.03
960	9.60	141.56	4.53	1.77	0.37	1.30	173.52	0.09	173.61	0.571	No	No	0.98

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
961	9.61	140.42	4.54	1.77	0.37	1.30	172.28	0.09	172.37	0.546	No	No	0.94
962	9.62	139.26	4.54	1.77	0.37	1.30	171.03	0.09	171.11	0.523	No	No	0.90
963	9.63	138.15	4.55	1.77	0.37	1.30	169.82	0.09	169.91	0.503	No	No	0.86
964	9.64	137.15	4.56	1.77	0.37	1.30	168.73	0.09	168.82	0.485	No	No	0.83
965	9.65	136.42	4.56	1.77	0.37	1.30	167.81	0.09	167.90	0.470	No	No	0.81
966	9.66	136.05	4.52	1.77	0.37	1.30	167.45	0.08	167.53	0.465	No	No	0.80
967	9.67	135.99	4.44	1.77	0.37	1.30	167.48	0.07	167.55	0.465	No	No	0.80
968	9.68	136.06	4.33	1.77	0.37	1.30	167.53	0.05	167.58	0.466	No	No	0.80
969	9.69	136.14	4.20	1.77	0.37	1.30	167.58	0.04	167.62	0.466	No	No	0.80
970	9.70	136.22	4.07	1.76	0.37	1.30	167.63	0.03	167.66	0.467	No	No	0.80
971	9.71	136.29	3.94	1.76	0.37	1.30	167.69	0.02	167.71	0.468	No	No	0.80
972	9.72	136.37	3.82	1.76	0.37	1.30	167.73	0.02	167.75	0.468	No	No	0.80
973	9.73	136.43	3.72	1.76	0.37	1.30	167.77	0.01	167.78	0.469	No	No	0.80
974	9.74	136.04	3.73	1.76	0.37	1.30	167.80	0.01	167.81	0.469	No	No	0.80
975	9.75	134.97	3.91	1.76	0.38	1.30	166.39	0.02	166.41	0.449	No	No	0.76
976	9.76	133.13	4.26	1.77	0.38	1.31	164.33	0.05	164.37	0.422	No	No	0.72
977	9.77	130.93	4.70	1.77	0.38	1.31	161.94	0.11	162.05	0.394	No	No	0.67
978	9.78	128.55	5.18	1.78	0.39	1.31	159.33	0.25	159.58	0.367	No	No	0.62
979	9.79	126.10	5.67	1.78	0.39	1.31	156.65	0.50	157.14	0.344	No	No	0.58
980	9.80	123.73	6.17	1.79	0.39	1.32	154.00	0.87	154.87	0.325	No	No	0.55
981	9.81	121.54	6.63	1.80	0.40	1.32	151.53	1.35	152.88	0.309	No	No	0.52
982	9.82	119.59	7.10	1.80	0.40	1.32	149.36	1.99	151.35	0.298	No	No	0.50
983	9.83	117.46	7.95	1.81	0.40	1.32	147.31	3.51	150.82	0.294	No	No	0.49
984	9.84	114.82	9.30	1.83	0.40	1.32	143.81	6.83	150.64	0.293	No	No	0.49
985	9.85	111.45	11.18	1.85	0.40	1.32	139.27	12.69	151.96	0.302	No	No	0.51
986	9.86	107.64	13.26	1.88	0.40	1.32	134.11	19.79	153.89	0.317	No	No	0.53
987	9.87	103.59	15.43	1.91	0.39	1.31	128.71	26.94	155.65	0.331	No	No	0.56
988	9.88	99.52	17.59	1.93	0.39	1.31	123.39	33.30	156.70	0.340	No	No	0.57
989	9.89	95.63	19.63	1.96	0.39	1.31	118.42	38.51	156.94	0.342	No	No	0.58
990	9.90	92.13	21.46	1.98	0.39	1.31	114.02	42.51	156.53	0.339	No	No	0.57
991	9.91	89.61	22.91	2.00	0.39	1.31	110.40	45.22	155.62	0.331	No	No	0.56
992	9.92	88.39	23.97	2.01	0.39	1.31	109.07	47.22	156.29	0.337	No	No	0.57
993	9.93	88.29	24.77	2.02	0.39	1.31	109.22	48.81	158.03	0.352	No	No	0.59
994	9.94	88.65	25.57	2.03	0.39	1.31	109.44	50.35	159.79	0.370	No	No	0.62
995	9.95	89.05	26.42	2.04	0.38	1.30	109.70	51.91	161.62	0.389	No	No	0.65
996	9.96	89.47	27.28	2.05	0.38	1.30	109.99	53.42	163.41	0.410	No	No	0.69
997	9.97	89.89	28.10	2.06	0.38	1.30	110.28	54.80	165.08	0.431	No	No	0.73
998	9.98	90.28	28.84	2.07	0.38	1.30	110.57	56.01	166.57	0.451	No	No	0.76
999	9.99	90.62	29.48	2.08	0.37	1.29	110.82	57.00	167.83	0.469	No	No	0.79
1000	10.00	90.70	29.89	2.09	0.37	1.29	111.04	57.64	168.68	0.483	No	No	0.81
1001	10.01	90.47	30.10	2.09	0.37	1.29	110.58	57.85	168.43	0.479	No	No	0.81
1002	10.02	89.92	30.16	2.09	0.37	1.29	109.92	57.79	167.71	0.468	No	No	0.79
1003	10.03	89.25	30.21	2.09	0.38	1.29	109.16	57.70	166.87	0.455	No	No	0.77
1004	10.04	88.54	30.26	2.09	0.38	1.30	108.35	57.61	165.96	0.443	No	No	0.74
1005	10.05	87.80	30.32	2.09	0.38	1.30	107.51	57.52	165.03	0.430	No	No	0.72
1006	10.06	87.08	30.37	2.09	0.38	1.30	106.70	57.42	164.12	0.419	No	No	0.70
1007	10.07	86.42	30.42	2.09	0.38	1.30	105.95	57.34	163.29	0.408	No	No	0.68
1008	10.08	85.78	30.50	2.09	0.38	1.30	105.29	57.32	162.61	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1009	10.09	84.79	30.76	2.10	0.38	1.30	104.51	57.49	162.00	4.000	Yes	No	2.00
1010	10.10	83.29	31.24	2.10	0.39	1.30	102.56	57.71	160.28	4.000	Yes	No	2.00
1011	10.11	81.22	31.95	2.11	0.39	1.30	100.16	58.10	158.26	4.000	Yes	No	2.00
1012	10.12	78.88	32.77	2.12	0.39	1.31	97.45	58.50	155.95	4.000	Yes	No	2.00
1013	10.13	76.41	33.66	2.13	0.40	1.31	94.58	58.87	153.45	4.000	Yes	No	2.00
1014	10.14	73.91	34.59	2.14	0.40	1.31	91.68	59.20	150.89	4.000	Yes	No	2.00
1015	10.15	71.54	35.49	2.16	0.41	1.32	88.90	59.48	148.39	4.000	Yes	No	2.00
1016	10.16	69.39	36.33	2.17	0.41	1.32	86.39	59.70	146.09	4.000	Yes	No	2.00
1017	10.17	67.57	37.13	2.18	0.41	1.32	84.29	59.93	144.22	4.000	Yes	No	2.00
1018	10.18	65.89	38.05	2.19	0.42	1.32	82.57	60.31	142.88	4.000	Yes	No	2.00
1019	10.19	64.10	39.21	2.20	0.42	1.33	80.47	60.74	141.21	4.000	Yes	No	2.00
1020	10.20	62.02	40.63	2.22	0.42	1.33	77.99	61.20	139.18	4.000	Yes	No	2.00
1021	10.21	59.73	42.20	2.24	0.43	1.33	75.30	61.62	136.92	4.000	Yes	No	2.00
1022	10.22	57.35	43.85	2.26	0.43	1.34	72.44	61.94	134.38	4.000	Yes	No	2.00
1023	10.23	54.99	45.49	2.28	0.44	1.34	69.61	62.18	131.79	4.000	Yes	No	2.00
1024	10.24	52.79	47.06	2.30	0.44	1.34	66.95	62.33	129.28	4.000	Yes	No	2.00
1025	10.25	50.85	48.46	2.32	0.44	1.35	64.60	62.41	127.00	4.000	Yes	No	2.00
1026	10.26	49.28	49.68	2.33	0.45	1.35	62.70	62.47	125.17	4.000	Yes	No	2.00
1027	10.27	47.90	50.84	2.35	0.45	1.35	61.32	62.61	123.93	4.000	Yes	No	2.00
1028	10.28	46.50	52.11	2.36	0.45	1.36	59.62	62.69	122.31	4.000	Yes	No	2.00
1029	10.29	44.91	53.58	2.38	0.46	1.36	57.66	62.73	120.40	4.000	Yes	No	2.00
1030	10.30	43.18	55.19	2.40	0.46	1.36	55.55	62.74	118.29	4.000	Yes	No	2.00
1031	10.31	41.42	56.95	2.42	0.46	1.36	53.38	62.74	116.12	4.000	Yes	No	2.00
1032	10.32	39.71	58.69	2.45	0.47	1.37	51.27	62.70	113.97	4.000	Yes	No	2.00
1033	10.33	38.14	60.32	2.47	0.47	1.37	49.32	62.63	111.95	4.000	Yes	No	2.00
1034	10.34	36.84	61.71	2.48	0.48	1.37	47.64	62.55	110.19	4.000	Yes	No	2.00
1035	10.35	35.90	62.78	2.50	0.48	1.38	46.49	62.50	109.00	4.000	Yes	No	2.00
1036	10.36	35.22	63.64	2.51	0.48	1.38	45.87	62.54	108.41	4.000	Yes	No	2.00
1037	10.37	34.62	64.48	2.52	0.48	1.38	45.11	62.53	107.64	4.000	Yes	No	2.00
1038	10.38	33.95	65.42	2.53	0.48	1.38	44.26	62.51	106.77	4.000	Yes	No	2.00
1039	10.39	33.23	66.42	2.54	0.49	1.38	43.36	62.48	105.84	4.000	Yes	No	2.00
1040	10.40	32.51	67.43	2.56	0.49	1.38	42.45	62.45	104.89	4.000	Yes	No	2.00
1041	10.41	31.83	68.40	2.57	0.49	1.38	41.58	62.40	103.98	4.000	Yes	No	2.00
1042	10.42	31.21	69.28	2.58	0.49	1.38	40.78	62.35	103.13	4.000	Yes	No	2.00
1043	10.43	30.76	69.95	2.59	0.49	1.39	40.13	62.30	102.43	4.000	Yes	No	2.00
1044	10.44	30.50	70.42	2.59	0.49	1.39	39.87	62.31	102.18	4.000	Yes	No	2.00
1045	10.45	30.39	70.75	2.60	0.49	1.39	39.78	62.35	102.13	4.000	Yes	No	2.00
1046	10.46	30.32	71.07	2.60	0.49	1.39	39.68	0.00	39.68	4.000	Yes	Yes	2.00
1047	10.47	30.24	71.41	2.61	0.49	1.39	39.57	0.00	39.57	4.000	Yes	Yes	2.00
1048	10.48	30.16	71.77	2.61	0.49	1.39	39.46	0.00	39.46	4.000	Yes	Yes	2.00
1049	10.49	30.08	72.12	2.61	0.49	1.39	39.35	0.00	39.35	4.000	Yes	Yes	2.00
1050	10.50	30.01	72.44	2.62	0.49	1.38	39.24	0.00	39.24	4.000	Yes	Yes	2.00
1051	10.51	29.94	72.73	2.62	0.49	1.38	39.15	0.00	39.15	4.000	Yes	Yes	2.00
1052	10.52	29.90	72.93	2.62	0.49	1.38	39.08	0.00	39.08	4.000	No	Yes	2.00
1053	10.53	29.89	73.05	2.63	0.49	1.38	39.06	0.00	39.06	4.000	No	Yes	2.00
1054	10.54	29.88	73.14	2.63	0.49	1.38	39.05	0.00	39.05	4.000	No	Yes	2.00
1055	10.55	29.88	73.23	2.63	0.49	1.38	39.04	0.00	39.04	4.000	No	Yes	2.00
1056	10.56	29.88	73.33	2.63	0.49	1.38	39.03	0.00	39.03	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1057	10.57	29.88	73.43	2.63	0.49	1.38	39.02	0.00	39.02	4.000	No	Yes	2.00
1058	10.58	29.88	73.53	2.63	0.49	1.38	39.01	0.00	39.01	4.000	No	Yes	2.00
1059	10.59	29.88	73.62	2.63	0.49	1.38	39.00	0.00	39.00	4.000	No	Yes	2.00
1060	10.60	29.90	73.67	2.63	0.49	1.38	38.99	0.00	38.99	4.000	No	Yes	2.00
1061	10.61	29.99	73.58	2.63	0.49	1.38	39.04	0.00	39.04	4.000	No	Yes	2.00
1062	10.62	30.16	73.35	2.63	0.49	1.38	39.29	0.00	39.29	4.000	Yes	Yes	2.00
1063	10.63	30.42	72.97	2.62	0.49	1.38	39.60	0.00	39.60	4.000	Yes	Yes	2.00
1064	10.64	30.71	72.56	2.62	0.49	1.38	39.95	0.00	39.95	4.000	Yes	Yes	2.00
1065	10.65	31.02	72.12	2.61	0.49	1.38	40.32	0.00	40.32	4.000	Yes	Yes	2.00
1066	10.66	31.32	71.68	2.61	0.49	1.38	40.71	0.00	40.71	4.000	Yes	Yes	2.00
1067	10.67	31.62	71.26	2.60	0.49	1.37	41.07	0.00	41.07	4.000	Yes	Yes	2.00
1068	10.68	31.88	70.89	2.60	0.49	1.37	41.39	62.85	104.23	4.000	Yes	No	2.00
1069	10.69	32.16	70.50	2.59	0.49	1.37	41.65	62.85	104.50	4.000	Yes	No	2.00
1070	10.70	32.52	70.00	2.59	0.49	1.37	42.05	62.87	104.92	4.000	Yes	No	2.00
1071	10.71	33.03	69.33	2.58	0.49	1.37	42.70	62.92	105.62	4.000	Yes	No	2.00
1072	10.72	33.66	68.50	2.57	0.48	1.37	43.48	62.97	106.45	4.000	Yes	No	2.00
1073	10.73	34.36	67.59	2.56	0.48	1.37	44.32	63.02	107.34	4.000	Yes	No	2.00
1074	10.74	35.08	66.65	2.55	0.48	1.36	45.20	63.07	108.27	4.000	Yes	No	2.00
1075	10.75	35.79	65.73	2.53	0.48	1.36	46.06	63.10	109.17	4.000	Yes	No	2.00
1076	10.76	36.45	64.87	2.52	0.48	1.36	46.87	63.13	110.00	4.000	Yes	No	2.00
1077	10.77	37.03	64.12	2.51	0.48	1.36	47.57	63.15	110.72	4.000	Yes	No	2.00
1078	10.78	37.61	63.40	2.51	0.47	1.36	48.14	63.13	111.26	4.000	Yes	No	2.00
1079	10.79	38.27	62.62	2.50	0.47	1.36	48.92	63.15	112.07	4.000	Yes	No	2.00
1080	10.80	39.10	61.71	2.48	0.47	1.35	49.93	63.19	113.12	4.000	Yes	No	2.00
1081	10.81	40.06	60.71	2.47	0.47	1.35	51.08	63.24	114.32	4.000	Yes	No	2.00
1082	10.82	41.09	59.63	2.46	0.47	1.35	52.33	63.28	115.60	4.000	Yes	No	2.00
1083	10.83	42.14	58.54	2.44	0.46	1.35	53.59	63.30	116.89	4.000	Yes	No	2.00
1084	10.84	43.16	57.49	2.43	0.46	1.34	54.81	63.31	118.12	4.000	Yes	No	2.00
1085	10.85	44.09	56.52	2.42	0.46	1.34	55.93	63.30	119.23	4.000	Yes	No	2.00
1086	10.86	44.92	55.69	2.41	0.46	1.34	56.88	63.28	120.16	4.000	Yes	No	2.00
1087	10.87	45.76	54.89	2.40	0.46	1.34	57.70	63.22	120.92	4.000	Yes	No	2.00
1088	10.88	46.74	54.01	2.39	0.45	1.34	58.88	63.22	122.10	4.000	Yes	No	2.00
1089	10.89	47.95	52.96	2.37	0.45	1.33	60.32	63.21	123.52	4.000	Yes	No	2.00
1090	10.90	49.30	51.79	2.36	0.45	1.33	61.92	63.17	125.09	4.000	Yes	No	2.00
1091	10.91	50.73	50.56	2.34	0.44	1.33	63.61	63.10	126.72	4.000	Yes	No	2.00
1092	10.92	52.17	49.33	2.33	0.44	1.32	65.31	63.00	128.30	4.000	Yes	No	2.00
1093	10.93	53.53	48.16	2.31	0.44	1.32	66.92	62.87	129.78	4.000	Yes	No	2.00
1094	10.94	54.75	47.12	2.30	0.44	1.32	68.36	62.72	131.07	4.000	Yes	No	2.00
1095	10.95	55.78	46.24	2.29	0.43	1.32	69.54	62.56	132.11	4.000	Yes	No	2.00
1096	10.96	56.72	45.44	2.28	0.43	1.32	70.47	62.37	132.84	4.000	Yes	No	2.00
1097	10.97	57.69	44.60	2.27	0.43	1.31	71.59	62.17	133.77	4.000	Yes	No	2.00
1098	10.98	58.81	43.63	2.26	0.43	1.31	72.91	61.93	134.84	4.000	Yes	No	2.00
1099	10.99	60.05	42.56	2.24	0.43	1.31	74.36	61.62	135.98	4.000	Yes	No	2.00
1100	11.00	61.33	41.45	2.23	0.43	1.31	75.86	61.25	137.11	4.000	Yes	No	2.00
1101	11.01	62.59	40.34	2.22	0.42	1.31	77.34	60.83	138.18	4.000	Yes	No	2.00
1102	11.02	63.77	39.30	2.20	0.42	1.31	78.72	60.39	139.12	4.000	Yes	No	2.00
1103	11.03	64.79	38.39	2.19	0.42	1.30	79.93	59.96	139.90	4.000	Yes	No	2.00
1104	11.04	65.56	37.69	2.18	0.42	1.30	80.89	59.62	140.51	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1105	11.05	66.15	37.11	2.18	0.42	1.30	81.38	59.24	140.62	4.000	Yes	No	2.00
1106	11.06	66.67	36.56	2.17	0.42	1.30	81.98	58.89	140.88	4.000	Yes	No	2.00
1107	11.07	67.25	35.92	2.16	0.42	1.30	82.62	58.46	141.08	4.000	Yes	No	2.00
1108	11.08	67.88	35.23	2.15	0.42	1.30	83.36	57.98	141.34	4.000	Yes	No	2.00
1109	11.09	68.52	34.52	2.14	0.42	1.30	84.12	57.45	141.57	4.000	Yes	No	2.00
1110	11.10	69.14	33.82	2.14	0.42	1.30	84.86	56.90	141.76	4.000	Yes	No	2.00
1111	11.11	69.71	33.17	2.13	0.42	1.30	85.53	56.37	141.90	4.000	Yes	No	2.00
1112	11.12	70.14	32.65	2.12	0.42	1.30	86.11	55.91	142.02	4.000	Yes	No	2.00
1113	11.13	70.34	32.29	2.12	0.42	1.30	86.39	55.57	141.96	4.000	Yes	No	2.00
1114	11.14	70.33	32.06	2.11	0.42	1.30	86.25	55.27	141.53	0.242	No	No	0.38
1115	11.15	70.18	31.87	2.11	0.42	1.30	86.08	55.02	141.10	0.240	No	No	0.38
1116	11.16	70.01	31.65	2.11	0.42	1.30	85.90	54.72	140.62	0.237	No	No	0.37
1117	11.17	69.83	31.42	2.11	0.42	1.30	85.70	54.41	140.11	0.235	No	No	0.37
1118	11.18	69.65	31.18	2.10	0.42	1.30	85.57	54.10	139.66	0.233	No	No	0.37
1119	11.19	69.48	30.96	2.10	0.42	1.30	85.38	53.79	139.16	0.231	No	No	0.36
1120	11.20	69.33	30.75	2.10	0.42	1.30	85.21	53.50	138.71	0.229	No	No	0.36
1121	11.21	69.12	30.66	2.10	0.42	1.30	85.06	53.36	138.42	0.228	No	No	0.36
1122	11.22	68.78	30.73	2.10	0.42	1.30	84.67	53.36	138.03	4.000	Yes	No	2.00
1123	11.23	68.26	30.98	2.10	0.43	1.30	84.00	53.53	137.53	4.000	Yes	No	2.00
1124	11.24	67.61	31.31	2.10	0.43	1.30	83.22	53.76	136.98	4.000	Yes	No	2.00
1125	11.25	66.90	31.68	2.11	0.43	1.30	82.36	54.01	136.38	4.000	Yes	No	2.00
1126	11.26	66.17	32.06	2.11	0.43	1.30	81.48	54.27	135.74	4.000	Yes	No	2.00
1127	11.27	65.44	32.44	2.12	0.43	1.30	80.61	54.50	135.11	4.000	Yes	No	2.00
1128	11.28	64.77	32.80	2.12	0.43	1.30	79.79	54.72	134.51	4.000	Yes	No	2.00
1129	11.29	64.18	33.11	2.13	0.43	1.31	79.08	54.90	133.98	4.000	Yes	No	2.00
1130	11.30	63.58	33.49	2.13	0.43	1.31	78.50	55.17	133.67	4.000	Yes	No	2.00
1131	11.31	62.89	34.00	2.14	0.43	1.31	77.65	55.50	133.15	4.000	Yes	No	2.00
1132	11.32	62.01	34.69	2.15	0.43	1.31	76.58	55.94	132.52	4.000	Yes	No	2.00
1133	11.33	61.00	35.48	2.16	0.44	1.31	75.36	56.41	131.77	4.000	Yes	No	2.00
1134	11.34	59.92	36.33	2.17	0.44	1.31	74.05	56.87	130.92	4.000	Yes	No	2.00
1135	11.35	58.82	37.20	2.18	0.44	1.31	72.72	57.30	130.02	4.000	Yes	No	2.00
1136	11.36	57.76	38.04	2.19	0.44	1.31	71.44	57.68	129.12	4.000	Yes	No	2.00
1137	11.37	56.79	38.80	2.20	0.44	1.31	70.27	58.00	128.26	4.000	Yes	No	2.00
1138	11.38	55.93	39.49	2.21	0.44	1.31	69.26	58.27	127.53	4.000	Yes	No	2.00
1139	11.39	55.04	40.22	2.22	0.44	1.31	68.37	58.57	126.94	4.000	Yes	No	2.00
1140	11.40	54.01	41.08	2.23	0.45	1.31	67.11	58.86	125.97	4.000	Yes	No	2.00
1141	11.41	52.74	42.16	2.24	0.45	1.31	65.57	59.19	124.76	4.000	Yes	No	2.00
1142	11.42	51.32	43.37	2.25	0.45	1.32	63.86	59.50	123.36	4.000	Yes	No	2.00
1143	11.43	49.82	44.64	2.27	0.45	1.32	62.06	59.78	121.84	4.000	Yes	No	2.00
1144	11.44	48.33	45.92	2.29	0.46	1.32	60.26	60.01	120.28	4.000	Yes	No	2.00
1145	11.45	46.91	47.16	2.30	0.46	1.32	58.55	60.20	118.75	4.000	Yes	No	2.00
1146	11.46	45.64	48.27	2.32	0.46	1.32	57.02	60.33	117.35	4.000	Yes	No	2.00
1147	11.47	44.59	49.23	2.33	0.46	1.33	55.75	60.43	116.18	4.000	Yes	No	2.00
1148	11.48	43.66	50.13	2.34	0.47	1.33	54.79	60.57	115.37	4.000	Yes	No	2.00
1149	11.49	42.71	51.10	2.35	0.47	1.33	53.67	60.68	114.34	4.000	Yes	No	2.00
1150	11.50	41.62	52.22	2.37	0.47	1.33	52.34	60.77	113.12	4.000	Yes	No	2.00
1151	11.51	40.44	53.46	2.38	0.47	1.33	50.90	60.85	111.75	4.000	Yes	No	2.00
1152	11.52	39.21	54.76	2.40	0.48	1.33	49.40	60.91	110.31	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1153	11.53	38.00	56.04	2.41	0.48	1.34	47.93	60.94	108.87	4.000	Yes	No	2.00
1154	11.54	36.88	57.25	2.43	0.48	1.34	46.56	60.95	107.51	4.000	Yes	No	2.00
1155	11.55	35.91	58.31	2.44	0.48	1.34	45.35	60.94	106.29	4.000	Yes	No	2.00
1156	11.56	35.13	59.21	2.45	0.49	1.34	44.40	60.94	105.34	4.000	Yes	No	2.00
1157	11.57	34.46	60.03	2.46	0.49	1.34	43.74	60.99	104.72	4.000	Yes	No	2.00
1158	11.58	33.79	60.90	2.47	0.49	1.34	42.91	60.99	103.90	4.000	Yes	No	2.00
1159	11.59	33.03	61.90	2.49	0.49	1.34	41.95	60.99	102.93	4.000	Yes	No	2.00
1160	11.60	32.21	62.98	2.50	0.49	1.35	40.94	60.97	101.91	4.000	Yes	No	2.00
1161	11.61	31.38	64.08	2.51	0.50	1.35	39.91	60.95	100.87	4.000	Yes	No	2.00
1162	11.62	30.58	65.15	2.53	0.50	1.35	38.92	60.92	99.84	4.000	Yes	No	2.00
1163	11.63	29.84	66.14	2.54	0.50	1.35	38.01	60.88	98.90	4.000	Yes	No	2.00
1164	11.64	29.25	66.97	2.55	0.50	1.35	37.24	60.84	98.08	4.000	Yes	No	2.00
1165	11.65	28.81	67.61	2.56	0.50	1.35	36.74	60.83	97.57	4.000	Yes	No	2.00
1166	11.66	28.48	68.15	2.56	0.50	1.35	36.40	60.85	97.26	4.000	Yes	No	2.00
1167	11.67	28.16	68.71	2.57	0.51	1.35	36.00	60.85	96.85	4.000	Yes	No	2.00
1168	11.68	27.81	69.33	2.58	0.51	1.35	35.56	60.84	96.40	4.000	Yes	No	2.00
1169	11.69	27.44	69.98	2.59	0.51	1.35	35.09	60.84	95.93	4.000	Yes	No	2.00
1170	11.70	27.07	70.64	2.60	0.51	1.35	34.62	60.83	95.45	4.000	Yes	No	2.00
1171	11.71	26.72	71.26	2.60	0.51	1.35	34.17	0.00	34.17	4.000	Yes	Yes	2.00
1172	11.72	26.40	71.81	2.61	0.51	1.36	33.77	0.00	33.77	4.000	Yes	Yes	2.00
1173	11.73	26.21	72.19	2.61	0.51	1.36	33.44	0.00	33.44	4.000	Yes	Yes	2.00
1174	11.74	26.15	72.35	2.62	0.51	1.36	33.43	0.00	33.43	4.000	No	Yes	2.00
1175	11.75	26.23	72.33	2.62	0.51	1.35	33.55	0.00	33.55	4.000	No	Yes	2.00
1176	11.76	26.35	72.26	2.62	0.51	1.35	33.69	0.00	33.69	4.000	No	Yes	2.00
1177	11.77	26.49	72.18	2.61	0.51	1.35	33.85	0.00	33.85	4.000	No	Yes	2.00
1178	11.78	26.63	72.10	2.61	0.51	1.35	34.01	0.00	34.01	4.000	No	Yes	2.00
1179	11.79	26.76	72.02	2.61	0.51	1.35	34.18	0.00	34.18	4.000	No	Yes	2.00
1180	11.80	26.89	71.95	2.61	0.51	1.35	34.33	0.00	34.33	4.000	No	Yes	2.00
1181	11.81	26.99	71.89	2.61	0.51	1.35	34.46	0.00	34.46	4.000	No	Yes	2.00
1182	11.82	26.96	71.91	2.61	0.51	1.35	34.54	0.00	34.54	4.000	No	Yes	2.00
1183	11.83	26.76	72.02	2.61	0.51	1.35	34.18	0.00	34.18	4.000	No	Yes	2.00
1184	11.84	26.40	72.22	2.62	0.51	1.35	33.72	0.00	33.72	4.000	No	Yes	2.00
1185	11.85	25.99	72.45	2.62	0.51	1.35	33.20	0.00	33.20	4.000	No	Yes	2.00
1186	11.86	25.55	72.70	2.62	0.51	1.35	32.65	0.00	32.65	4.000	No	Yes	2.00
1187	11.87	25.10	72.97	2.62	0.51	1.35	32.09	0.00	32.09	4.000	No	Yes	2.00
1188	11.88	24.67	73.24	2.63	0.52	1.35	31.55	0.00	31.55	4.000	No	Yes	2.00
1189	11.89	24.27	73.49	2.63	0.52	1.36	31.05	0.00	31.05	4.000	No	Yes	2.00
1190	11.90	23.96	73.67	2.63	0.52	1.36	30.63	0.00	30.63	4.000	No	Yes	2.00
1191	11.91	23.76	73.73	2.63	0.52	1.36	30.39	0.00	30.39	4.000	No	Yes	2.00
1192	11.92	23.64	73.66	2.63	0.52	1.36	30.29	0.00	30.29	4.000	No	Yes	2.00
1193	11.93	23.55	73.50	2.63	0.52	1.36	30.17	0.00	30.17	4.000	No	Yes	2.00
1194	11.94	23.45	73.32	2.63	0.52	1.36	30.04	0.00	30.04	4.000	No	Yes	2.00
1195	11.95	23.34	73.12	2.63	0.52	1.36	29.90	0.00	29.90	4.000	No	Yes	2.00
1196	11.96	23.23	72.92	2.62	0.52	1.36	29.77	0.00	29.77	4.000	No	Yes	2.00
1197	11.97	23.13	72.73	2.62	0.52	1.36	29.64	0.00	29.64	4.000	No	Yes	2.00
1198	11.98	23.04	72.56	2.62	0.52	1.36	29.52	0.00	29.52	4.000	No	Yes	2.00
1199	11.99	22.93	72.46	2.62	0.52	1.36	29.42	0.00	29.42	4.000	No	Yes	2.00
1200	12.00	22.76	72.45	2.62	0.52	1.36	29.20	0.00	29.20	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1201	12.01	22.50	72.52	2.62	0.53	1.36	28.87	0.00	28.87	4.000	No	Yes	2.00
1202	12.02	22.19	72.62	2.62	0.53	1.36	28.47	0.00	28.47	4.000	No	Yes	2.00
1203	12.03	21.85	72.73	2.62	0.53	1.36	28.04	0.00	28.04	4.000	No	Yes	2.00
1204	12.04	21.49	72.85	2.62	0.53	1.36	27.59	0.00	27.59	4.000	No	Yes	2.00
1205	12.05	21.15	72.97	2.62	0.53	1.36	27.16	0.00	27.16	4.000	No	Yes	2.00
1206	12.06	20.83	73.09	2.63	0.53	1.36	26.75	0.00	26.75	4.000	No	Yes	2.00
1207	12.07	20.54	73.21	2.63	0.53	1.36	26.40	0.00	26.40	4.000	No	Yes	2.00
1208	12.08	20.15	73.56	2.63	0.53	1.36	26.09	0.00	26.09	4.000	No	Yes	2.00
1209	12.09	19.60	74.21	2.64	0.54	1.36	25.30	0.00	25.30	4.000	No	Yes	2.00
1210	12.10	18.82	75.25	2.65	0.54	1.36	24.32	0.00	24.32	4.000	No	Yes	2.00
1211	12.11	17.94	76.50	2.67	0.54	1.37	23.19	0.00	23.19	4.000	No	Yes	2.00
1212	12.12	16.99	77.92	2.69	0.55	1.37	21.99	0.00	21.99	4.000	No	Yes	2.00
1213	12.13	16.03	79.46	2.71	0.55	1.37	20.76	0.00	20.76	4.000	No	Yes	2.00
1214	12.14	15.10	81.05	2.73	0.55	1.37	19.58	0.00	19.58	4.000	No	Yes	2.00
1215	12.15	14.26	82.62	2.75	0.56	1.38	18.50	0.00	18.50	4.000	No	Yes	2.00
1216	12.16	13.60	84.03	2.76	0.56	1.38	17.58	0.00	17.58	4.000	No	Yes	2.00
1217	12.17	13.17	85.06	2.78	0.56	1.38	17.06	0.00	17.06	4.000	No	Yes	2.00
1218	12.18	12.90	85.81	2.79	0.56	1.38	16.84	0.00	16.84	4.000	No	Yes	2.00
1219	12.19	12.70	86.50	2.79	0.56	1.38	16.57	0.00	16.57	4.000	No	Yes	2.00
1220	12.20	12.47	87.27	2.80	0.56	1.38	16.27	0.00	16.27	4.000	No	Yes	2.00
1221	12.21	12.23	88.09	2.81	0.56	1.38	15.96	0.00	15.96	4.000	No	Yes	2.00
1222	12.22	11.99	88.92	2.82	0.56	1.38	15.64	0.00	15.64	4.000	No	Yes	2.00
1223	12.23	11.77	89.71	2.83	0.56	1.38	15.35	0.00	15.35	4.000	No	Yes	2.00
1224	12.24	11.57	90.43	2.84	0.57	1.38	15.09	0.00	15.09	4.000	No	Yes	2.00
1225	12.25	11.40	91.07	2.85	0.57	1.38	14.87	0.00	14.87	4.000	No	Yes	2.00
1226	12.26	11.23	91.73	2.86	0.57	1.38	14.68	0.00	14.68	4.000	No	Yes	2.00
1227	12.27	11.05	92.49	2.87	0.57	1.38	14.44	0.00	14.44	4.000	No	Yes	2.00
1228	12.28	10.83	93.39	2.88	0.57	1.38	14.16	0.00	14.16	4.000	No	Yes	2.00
1229	12.29	10.60	94.39	2.89	0.57	1.38	13.85	0.00	13.85	4.000	No	Yes	2.00
1230	12.30	10.36	95.43	2.91	0.57	1.38	13.53	0.00	13.53	4.000	No	Yes	2.00
1231	12.31	10.12	96.46	2.92	0.57	1.38	13.23	0.00	13.23	4.000	No	Yes	2.00
1232	12.32	9.90	97.43	2.93	0.57	1.38	12.94	0.00	12.94	4.000	No	Yes	2.00
1233	12.33	9.72	98.28	2.94	0.57	1.38	12.69	0.00	12.69	4.000	No	Yes	2.00
1234	12.34	9.55	99.05	2.95	0.57	1.38	12.49	0.00	12.49	4.000	No	Yes	2.00
1235	12.35	9.38	99.83	2.96	0.57	1.38	12.28	0.00	12.28	4.000	No	Yes	2.00
1236	12.36	9.18	100.00	2.97	0.57	1.39	12.03	0.00	12.03	4.000	No	Yes	2.00
1237	12.37	8.96	100.00	2.98	0.58	1.39	11.74	0.00	11.74	4.000	No	Yes	2.00
1238	12.38	8.72	100.00	3.00	0.58	1.39	11.43	0.00	11.43	4.000	No	Yes	2.00
1239	12.39	8.48	100.00	3.01	0.58	1.39	11.11	0.00	11.11	4.000	No	Yes	2.00
1240	12.40	8.25	100.00	3.03	0.58	1.39	10.81	0.00	10.81	4.000	No	Yes	2.00
1241	12.41	8.04	100.00	3.04	0.58	1.39	10.53	0.00	10.53	4.000	No	Yes	2.00
1242	12.42	7.87	100.00	3.05	0.58	1.39	10.30	0.00	10.30	4.000	No	Yes	2.00
1243	12.43	7.73	100.00	3.06	0.58	1.39	10.14	0.00	10.14	4.000	No	Yes	2.00
1244	12.44	7.60	100.00	3.07	0.58	1.39	9.99	0.00	9.99	4.000	No	Yes	2.00
1245	12.45	7.47	100.00	3.08	0.58	1.39	9.81	0.00	9.81	4.000	No	Yes	2.00
1246	12.46	7.32	100.00	3.09	0.58	1.39	9.61	0.00	9.61	4.000	No	Yes	2.00
1247	12.47	7.16	100.00	3.10	0.58	1.39	9.39	0.00	9.39	4.000	No	Yes	2.00
1248	12.48	7.00	100.00	3.12	0.59	1.39	9.19	0.00	9.19	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1249	12.49	6.85	100.00	3.13	0.59	1.39	8.99	0.00	8.99	4.000	No	Yes	2.00
1250	12.50	6.71	100.00	3.14	0.59	1.39	8.81	0.00	8.81	4.000	No	Yes	2.00
1251	12.51	6.61	100.00	3.15	0.59	1.39	8.67	0.00	8.67	4.000	No	Yes	2.00
1252	12.52	6.53	100.00	3.15	0.59	1.39	8.59	0.00	8.59	4.000	No	Yes	2.00
1253	12.53	6.47	100.00	3.16	0.59	1.39	8.50	0.00	8.50	4.000	No	Yes	2.00
1254	12.54	6.40	100.00	3.17	0.59	1.39	8.41	0.00	8.41	4.000	No	Yes	2.00
1255	12.55	6.32	100.00	3.17	0.59	1.39	8.30	0.00	8.30	4.000	No	Yes	2.00
1256	12.56	6.24	100.00	3.18	0.59	1.39	8.20	0.00	8.20	4.000	No	Yes	2.00
1257	12.57	6.16	100.00	3.19	0.59	1.39	8.09	0.00	8.09	4.000	No	Yes	2.00
1258	12.58	6.09	100.00	3.19	0.59	1.39	8.00	0.00	8.00	4.000	No	Yes	2.00
1259	12.59	6.03	100.00	3.20	0.59	1.39	7.91	0.00	7.91	4.000	No	Yes	2.00
1260	12.60	5.99	100.00	3.20	0.59	1.39	7.85	0.00	7.85	4.000	No	Yes	2.00
1261	12.61	5.98	100.00	3.20	0.59	1.39	7.85	0.00	7.85	4.000	No	Yes	2.00
1262	12.62	5.98	100.00	3.20	0.59	1.39	7.85	0.00	7.85	4.000	No	Yes	2.00
1263	12.63	5.98	100.00	3.20	0.59	1.39	7.85	0.00	7.85	4.000	No	Yes	2.00
1264	12.64	5.98	100.00	3.20	0.59	1.39	7.85	0.00	7.85	4.000	No	Yes	2.00
1265	12.65	5.98	100.00	3.20	0.59	1.39	7.84	0.00	7.84	4.000	No	Yes	2.00
1266	12.66	5.98	100.00	3.20	0.59	1.39	7.84	0.00	7.84	4.000	No	Yes	2.00
1267	12.67	5.98	100.00	3.20	0.59	1.39	7.84	0.00	7.84	4.000	No	Yes	2.00
1268	12.68	5.98	100.00	3.20	0.59	1.39	7.84	0.00	7.84	4.000	No	Yes	2.00
1269	12.69	5.98	100.00	3.20	0.59	1.39	7.84	0.00	7.84	4.000	No	Yes	2.00
1270	12.70	5.98	100.00	3.20	0.59	1.39	7.84	0.00	7.84	4.000	No	Yes	2.00
1271	12.71	5.98	100.00	3.20	0.59	1.39	7.83	0.00	7.83	4.000	No	Yes	2.00
1272	12.72	5.98	100.00	3.20	0.59	1.39	7.83	0.00	7.83	4.000	No	Yes	2.00
1273	12.73	5.98	100.00	3.20	0.59	1.39	7.83	0.00	7.83	4.000	No	Yes	2.00
1274	12.74	5.98	100.00	3.19	0.59	1.39	7.83	0.00	7.83	4.000	No	Yes	2.00
1275	12.75	5.98	100.00	3.19	0.59	1.39	7.83	0.00	7.83	4.000	No	Yes	2.00
1276	12.76	5.98	100.00	3.19	0.59	1.39	7.83	0.00	7.83	4.000	No	Yes	2.00
1277	12.77	5.98	100.00	3.19	0.59	1.39	7.82	0.00	7.82	4.000	No	Yes	2.00
1278	12.78	5.98	100.00	3.19	0.59	1.39	7.82	0.00	7.82	4.000	No	Yes	2.00
1279	12.79	5.98	100.00	3.18	0.59	1.39	7.82	0.00	7.82	4.000	No	Yes	2.00
1280	12.80	5.98	100.00	3.18	0.59	1.39	7.82	0.00	7.82	4.000	No	Yes	2.00
1281	12.81	5.98	100.00	3.18	0.59	1.39	7.82	0.00	7.82	4.000	No	Yes	2.00
1282	12.82	5.98	100.00	3.18	0.59	1.38	7.82	0.00	7.82	4.000	No	Yes	2.00
1283	12.83	5.98	100.00	3.17	0.59	1.38	7.82	0.00	7.82	4.000	No	Yes	2.00
1284	12.84	5.98	100.00	3.17	0.59	1.38	7.81	0.00	7.81	4.000	No	Yes	2.00
1285	12.85	5.98	100.00	3.17	0.59	1.38	7.81	0.00	7.81	4.000	No	Yes	2.00
1286	12.86	5.98	100.00	3.16	0.59	1.38	7.81	0.00	7.81	4.000	No	Yes	2.00
1287	12.87	5.98	100.00	3.16	0.59	1.38	7.81	0.00	7.81	4.000	No	Yes	2.00
1288	12.88	5.98	100.00	3.16	0.59	1.38	7.81	0.00	7.81	4.000	No	Yes	2.00
1289	12.89	5.98	100.00	3.15	0.59	1.38	7.81	0.00	7.81	4.000	No	Yes	2.00
1290	12.90	5.98	100.00	3.15	0.59	1.38	7.80	0.00	7.80	4.000	No	Yes	2.00
1291	12.91	5.98	100.00	3.15	0.59	1.38	7.80	0.00	7.80	4.000	No	Yes	2.00
1292	12.92	5.98	100.00	3.14	0.59	1.38	7.80	0.00	7.80	4.000	No	Yes	2.00
1293	12.93	5.98	100.00	3.14	0.59	1.38	7.80	0.00	7.80	4.000	No	Yes	2.00
1294	12.94	5.98	100.00	3.14	0.59	1.38	7.80	0.00	7.80	4.000	No	Yes	2.00
1295	12.95	5.98	100.00	3.13	0.59	1.38	7.80	0.00	7.80	4.000	No	Yes	2.00
1296	12.96	5.98	100.00	3.13	0.59	1.38	7.80	0.00	7.80	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1297	12.97	5.98	100.00	3.12	0.59	1.38	7.79	0.00	7.79	4.000	No	Yes	2.00
1298	12.98	5.98	100.00	3.12	0.59	1.38	7.79	0.00	7.79	4.000	No	Yes	2.00
1299	12.99	5.98	100.00	3.12	0.59	1.38	7.79	0.00	7.79	4.000	No	Yes	2.00
1300	13.00	5.98	100.00	3.11	0.59	1.38	7.79	0.00	7.79	4.000	No	Yes	2.00
1301	13.01	5.98	100.00	3.10	0.59	1.38	7.79	0.00	7.79	4.000	No	Yes	2.00
1302	13.02	5.98	100.00	3.10	0.59	1.38	7.79	0.00	7.79	4.000	No	Yes	2.00
1303	13.03	5.95	100.00	3.10	0.59	1.38	7.78	0.00	7.78	4.000	No	Yes	2.00
1304	13.04	5.88	100.00	3.10	0.59	1.38	7.68	0.00	7.68	4.000	No	Yes	2.00
1305	13.05	5.76	100.00	3.11	0.59	1.38	7.52	0.00	7.52	4.000	No	Yes	2.00
1306	13.06	5.62	100.00	3.11	0.59	1.38	7.33	0.00	7.33	4.000	No	Yes	2.00
1307	13.07	5.46	100.00	3.12	0.59	1.38	7.12	0.00	7.12	4.000	No	Yes	2.00
1308	13.08	5.30	100.00	3.13	0.59	1.38	6.91	0.00	6.91	4.000	No	Yes	2.00
1309	13.09	5.14	100.00	3.14	0.60	1.38	6.71	0.00	6.71	4.000	No	Yes	2.00
1310	13.10	5.00	100.00	3.15	0.60	1.38	6.52	0.00	6.52	4.000	No	Yes	2.00
1311	13.11	4.87	100.00	3.16	0.60	1.38	6.35	0.00	6.35	4.000	No	Yes	2.00
1312	13.12	4.74	100.00	3.17	0.60	1.38	6.21	0.00	6.21	4.000	No	Yes	2.00
1313	13.13	4.58	100.00	3.18	0.60	1.38	6.00	0.00	6.00	4.000	No	Yes	2.00
1314	13.14	4.39	100.00	3.20	0.60	1.38	5.74	0.00	5.74	4.000	No	Yes	2.00
1315	13.15	4.16	100.00	3.22	0.60	1.38	5.45	0.00	5.45	4.000	No	Yes	2.00
1316	13.16	3.93	100.00	3.25	0.60	1.38	5.13	0.00	5.13	4.000	No	Yes	2.00
1317	13.17	3.69	100.00	3.28	0.60	1.38	4.82	0.00	4.82	4.000	No	Yes	2.00
1318	13.18	3.46	100.00	3.31	0.60	1.39	4.52	0.00	4.52	4.000	No	Yes	2.00
1319	13.19	3.25	100.00	3.34	0.61	1.39	4.24	0.00	4.24	4.000	No	Yes	2.00
1320	13.20	3.09	100.00	3.37	0.61	1.39	4.01	0.00	4.01	4.000	No	Yes	2.00
1321	13.21	2.98	100.00	3.39	0.61	1.39	3.88	0.00	3.88	4.000	No	Yes	2.00
1322	13.22	2.90	100.00	3.40	0.61	1.39	3.81	0.00	3.81	4.000	No	Yes	2.00
1323	13.23	2.83	100.00	3.41	0.61	1.39	3.71	0.00	3.71	4.000	No	Yes	2.00
1324	13.24	2.76	100.00	3.43	0.61	1.39	3.61	0.00	3.61	4.000	No	Yes	2.00
1325	13.25	2.68	100.00	3.44	0.61	1.39	3.51	0.00	3.51	4.000	No	Yes	2.00
1326	13.26	2.60	100.00	3.46	0.61	1.39	3.40	0.00	3.40	4.000	No	Yes	2.00
1327	13.27	2.52	100.00	3.48	0.61	1.39	3.30	0.00	3.30	4.000	No	Yes	2.00
1328	13.28	2.46	100.00	3.49	0.61	1.39	3.21	0.00	3.21	4.000	No	Yes	2.00
1329	13.29	2.41	100.00	3.51	0.61	1.39	3.14	0.00	3.14	4.000	No	Yes	2.00
1330	13.30	2.39	100.00	3.51	0.61	1.39	3.13	0.00	3.13	4.000	No	Yes	2.00
1331	13.31	2.39	100.00	3.51	0.61	1.39	3.13	0.00	3.13	4.000	No	Yes	2.00
1332	13.32	2.39	100.00	3.52	0.61	1.39	3.13	0.00	3.13	4.000	No	Yes	2.00
1333	13.33	2.39	100.00	3.52	0.61	1.39	3.13	0.00	3.13	4.000	No	Yes	2.00
1334	13.34	2.39	100.00	3.52	0.61	1.39	3.13	0.00	3.13	4.000	No	Yes	2.00
1335	13.35	2.39	100.00	3.52	0.61	1.39	3.13	0.00	3.13	4.000	No	Yes	2.00
1336	13.36	2.39	100.00	3.52	0.61	1.39	3.13	0.00	3.13	4.000	No	Yes	2.00
1337	13.37	2.40	100.00	3.52	0.61	1.39	3.13	0.00	3.13	4.000	No	Yes	2.00
1338	13.38	2.44	100.00	3.51	0.61	1.39	3.15	0.00	3.15	4.000	No	Yes	2.00
1339	13.39	2.52	100.00	3.49	0.61	1.39	3.29	0.00	3.29	4.000	No	Yes	2.00
1340	13.40	2.65	100.00	3.47	0.61	1.38	3.47	0.00	3.47	4.000	No	Yes	2.00
1341	13.41	2.80	100.00	3.44	0.61	1.38	3.66	0.00	3.66	4.000	No	Yes	2.00
1342	13.42	2.96	100.00	3.41	0.61	1.38	3.87	0.00	3.87	4.000	No	Yes	2.00
1343	13.43	3.12	100.00	3.38	0.61	1.38	4.08	0.00	4.08	4.000	No	Yes	2.00
1344	13.44	3.28	100.00	3.36	0.61	1.38	4.28	0.00	4.28	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1345	13.45	3.41	100.00	3.34	0.60	1.38	4.46	0.00	4.46	4.000	No	Yes	2.00
1346	13.46	3.54	100.00	3.32	0.60	1.38	4.61	0.00	4.61	4.000	No	Yes	2.00
1347	13.47	3.68	100.00	3.30	0.60	1.38	4.77	0.00	4.77	4.000	No	Yes	2.00
1348	13.48	3.85	100.00	3.28	0.60	1.38	5.00	0.00	5.00	4.000	No	Yes	2.00
1349	13.49	4.06	100.00	3.26	0.60	1.38	5.27	0.00	5.27	4.000	No	Yes	2.00
1350	13.50	4.29	100.00	3.23	0.60	1.38	5.57	0.00	5.57	4.000	No	Yes	2.00
1351	13.51	4.53	100.00	3.21	0.60	1.37	5.88	0.00	5.88	4.000	No	Yes	2.00
1352	13.52	4.76	100.00	3.19	0.60	1.37	6.19	0.00	6.19	4.000	No	Yes	2.00
1353	13.53	4.99	100.00	3.17	0.60	1.37	6.48	0.00	6.48	4.000	No	Yes	2.00
1354	13.54	5.18	100.00	3.16	0.60	1.37	6.73	0.00	6.73	4.000	No	Yes	2.00
1355	13.55	5.30	100.00	3.15	0.59	1.37	6.94	0.00	6.94	4.000	No	Yes	2.00
1356	13.56	5.34	100.00	3.15	0.59	1.37	6.92	0.00	6.92	4.000	No	Yes	2.00
1357	13.57	5.30	100.00	3.15	0.59	1.37	6.87	0.00	6.87	4.000	No	Yes	2.00
1358	13.58	5.26	100.00	3.16	0.60	1.37	6.80	0.00	6.80	4.000	No	Yes	2.00
1359	13.59	5.20	100.00	3.16	0.60	1.37	6.74	0.00	6.74	4.000	No	Yes	2.00
1360	13.60	5.15	100.00	3.17	0.60	1.37	6.66	0.00	6.66	4.000	No	Yes	2.00
1361	13.61	5.10	100.00	3.18	0.60	1.37	6.60	0.00	6.60	4.000	No	Yes	2.00
1362	13.62	5.05	100.00	3.18	0.60	1.37	6.53	0.00	6.53	4.000	No	Yes	2.00
1363	13.63	5.01	100.00	3.19	0.60	1.37	6.48	0.00	6.48	4.000	No	Yes	2.00
1364	13.64	4.99	100.00	3.19	0.60	1.37	6.44	0.00	6.44	4.000	No	Yes	2.00
1365	13.65	4.98	100.00	3.20	0.60	1.37	6.44	0.00	6.44	4.000	No	Yes	2.00
1366	13.66	4.98	100.00	3.20	0.60	1.37	6.44	0.00	6.44	4.000	No	Yes	2.00
1367	13.67	4.98	100.00	3.21	0.60	1.37	6.44	0.00	6.44	4.000	No	Yes	2.00
1368	13.68	4.98	100.00	3.21	0.60	1.37	6.44	0.00	6.44	4.000	No	Yes	2.00
1369	13.69	4.98	100.00	3.22	0.60	1.37	6.44	0.00	6.44	4.000	No	Yes	2.00
1370	13.70	4.98	100.00	3.22	0.60	1.37	6.44	0.00	6.44	4.000	No	Yes	2.00
1371	13.71	4.98	100.00	3.23	0.60	1.37	6.43	0.00	6.43	4.000	No	Yes	2.00
1372	13.72	4.99	100.00	3.23	0.60	1.37	6.43	0.00	6.43	4.000	No	Yes	2.00
1373	13.73	5.04	100.00	3.23	0.60	1.37	6.49	0.00	6.49	4.000	No	Yes	2.00
1374	13.74	5.13	100.00	3.22	0.60	1.37	6.61	0.00	6.61	4.000	No	Yes	2.00
1375	13.75	5.24	100.00	3.21	0.60	1.37	6.76	0.00	6.76	4.000	No	Yes	2.00
1376	13.76	5.37	100.00	3.20	0.59	1.37	6.93	0.00	6.93	4.000	No	Yes	2.00
1377	13.77	5.51	100.00	3.19	0.59	1.36	7.10	0.00	7.10	4.000	No	Yes	2.00
1378	13.78	5.64	100.00	3.18	0.59	1.36	7.27	0.00	7.27	4.000	No	Yes	2.00
1379	13.79	5.76	100.00	3.17	0.59	1.36	7.42	0.00	7.42	4.000	No	Yes	2.00
1380	13.80	5.87	100.00	3.16	0.59	1.36	7.56	0.00	7.56	4.000	No	Yes	2.00
1381	13.81	5.91	100.00	3.15	0.59	1.36	7.67	0.00	7.67	4.000	No	Yes	2.00
1382	13.82	5.87	100.00	3.16	0.59	1.36	7.57	0.00	7.57	4.000	No	Yes	2.00
1383	13.83	5.75	100.00	3.16	0.59	1.36	7.41	0.00	7.41	4.000	No	Yes	2.00
1384	13.84	5.61	100.00	3.17	0.59	1.36	7.22	0.00	7.22	4.000	No	Yes	2.00
1385	13.85	5.45	100.00	3.18	0.59	1.36	7.02	0.00	7.02	4.000	No	Yes	2.00
1386	13.86	5.29	100.00	3.19	0.60	1.36	6.81	0.00	6.81	4.000	No	Yes	2.00
1387	13.87	5.13	100.00	3.20	0.60	1.36	6.61	0.00	6.61	4.000	No	Yes	2.00
1388	13.88	4.99	100.00	3.21	0.60	1.36	6.42	0.00	6.42	4.000	No	Yes	2.00
1389	13.89	4.87	100.00	3.22	0.60	1.36	6.26	0.00	6.26	4.000	No	Yes	2.00
1390	13.90	4.76	100.00	3.23	0.60	1.36	6.13	0.00	6.13	4.000	No	Yes	2.00
1391	13.91	4.64	100.00	3.25	0.60	1.36	5.99	0.00	5.99	4.000	No	Yes	2.00
1392	13.92	4.51	100.00	3.26	0.60	1.36	5.82	0.00	5.82	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1393	13.93	4.36	100.00	3.28	0.60	1.36	5.62	0.00	5.62	4.000	No	Yes	2.00
1394	13.94	4.20	100.00	3.30	0.60	1.36	5.42	0.00	5.42	4.000	No	Yes	2.00
1395	13.95	4.04	100.00	3.33	0.60	1.37	5.21	0.00	5.21	4.000	No	Yes	2.00
1396	13.96	3.89	100.00	3.35	0.60	1.37	5.01	0.00	5.01	4.000	No	Yes	2.00
1397	13.97	3.75	100.00	3.37	0.60	1.37	4.83	0.00	4.83	4.000	No	Yes	2.00
1398	13.98	3.65	100.00	3.39	0.60	1.37	4.68	0.00	4.68	4.000	No	Yes	2.00
1399	13.99	3.60	100.00	3.40	0.60	1.37	4.63	0.00	4.63	4.000	No	Yes	2.00
1400	14.00	3.59	100.00	3.40	0.60	1.37	4.63	0.00	4.63	4.000	No	Yes	2.00
1401	14.01	3.59	100.00	3.41	0.60	1.37	4.63	0.00	4.63	4.000	No	Yes	2.00
1402	14.02	3.59	100.00	3.41	0.60	1.37	4.62	0.00	4.62	4.000	No	Yes	2.00
1403	14.03	3.59	100.00	3.42	0.60	1.37	4.62	0.00	4.62	4.000	No	Yes	2.00
1404	14.04	3.59	100.00	3.42	0.60	1.36	4.62	0.00	4.62	4.000	No	Yes	2.00
1405	14.05	3.59	100.00	3.43	0.60	1.36	4.62	0.00	4.62	4.000	No	Yes	2.00
1406	14.06	3.59	100.00	3.43	0.60	1.36	4.62	0.00	4.62	4.000	No	Yes	2.00
1407	14.07	3.62	100.00	3.43	0.60	1.36	4.62	0.00	4.62	4.000	No	Yes	2.00
1408	14.08	3.69	100.00	3.43	0.60	1.36	4.74	0.00	4.74	4.000	No	Yes	2.00
1409	14.09	3.81	100.00	3.41	0.60	1.36	4.90	0.00	4.90	4.000	No	Yes	2.00
1410	14.10	3.96	100.00	3.40	0.60	1.36	5.09	0.00	5.09	4.000	No	Yes	2.00
1411	14.11	4.12	100.00	3.39	0.60	1.36	5.29	0.00	5.29	4.000	No	Yes	2.00
1412	14.12	4.28	100.00	3.37	0.60	1.36	5.50	0.00	5.50	4.000	No	Yes	2.00
1413	14.13	4.43	100.00	3.36	0.60	1.36	5.70	0.00	5.70	4.000	No	Yes	2.00
1414	14.14	4.57	100.00	3.35	0.60	1.36	5.88	0.00	5.88	4.000	No	Yes	2.00
1415	14.15	4.70	100.00	3.34	0.60	1.36	6.04	0.00	6.04	4.000	No	Yes	2.00
1416	14.16	4.83	100.00	3.33	0.60	1.36	6.17	0.00	6.17	4.000	No	Yes	2.00
1417	14.17	4.99	100.00	3.32	0.60	1.36	6.38	0.00	6.38	4.000	No	Yes	2.00
1418	14.18	5.19	100.00	3.31	0.60	1.36	6.64	0.00	6.64	4.000	No	Yes	2.00
1419	14.19	5.42	100.00	3.29	0.59	1.35	6.93	0.00	6.93	4.000	No	Yes	2.00
1420	14.20	5.66	100.00	3.28	0.59	1.35	7.23	0.00	7.23	4.000	No	Yes	2.00
1421	14.21	5.90	100.00	3.26	0.59	1.35	7.54	0.00	7.54	4.000	No	Yes	2.00
1422	14.22	6.13	100.00	3.25	0.59	1.35	7.83	0.00	7.83	4.000	No	Yes	2.00
1423	14.23	6.33	100.00	3.24	0.59	1.35	8.09	0.00	8.09	4.000	No	Yes	2.00
1424	14.24	6.51	100.00	3.23	0.59	1.35	8.30	0.00	8.30	4.000	No	Yes	2.00
1425	14.25	6.67	100.00	3.22	0.59	1.35	8.48	0.00	8.48	4.000	No	Yes	2.00
1426	14.26	6.85	100.00	3.21	0.59	1.35	8.71	0.00	8.71	4.000	No	Yes	2.00
1427	14.27	7.06	100.00	3.20	0.59	1.35	8.97	0.00	8.97	4.000	No	Yes	2.00
1428	14.28	7.29	100.00	3.19	0.59	1.35	9.26	0.00	9.26	4.000	No	Yes	2.00
1429	14.29	7.53	100.00	3.17	0.58	1.34	9.57	0.00	9.57	4.000	No	Yes	2.00
1430	14.30	7.77	100.00	3.16	0.58	1.34	9.86	0.00	9.86	4.000	No	Yes	2.00
1431	14.31	7.99	100.00	3.15	0.58	1.34	10.14	0.00	10.14	4.000	No	Yes	2.00
1432	14.32	8.19	100.00	3.14	0.58	1.34	10.39	0.00	10.39	4.000	No	Yes	2.00
1433	14.33	8.34	100.00	3.13	0.58	1.34	10.58	0.00	10.58	4.000	No	Yes	2.00
1434	14.34	8.47	100.00	3.13	0.58	1.34	10.71	0.00	10.71	4.000	No	Yes	2.00
1435	14.35	8.60	100.00	3.12	0.58	1.34	10.87	0.00	10.87	4.000	No	Yes	2.00
1436	14.36	8.74	100.00	3.11	0.58	1.34	11.05	0.00	11.05	4.000	No	Yes	2.00
1437	14.37	8.90	100.00	3.10	0.58	1.34	11.24	0.00	11.24	4.000	No	Yes	2.00
1438	14.38	9.06	100.00	3.10	0.58	1.34	11.44	0.00	11.44	4.000	No	Yes	2.00
1439	14.39	9.22	100.00	3.09	0.58	1.34	11.63	0.00	11.63	4.000	No	Yes	2.00
1440	14.40	9.36	100.00	3.08	0.58	1.34	11.81	0.00	11.81	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1441	14.41	9.47	100.00	3.08	0.57	1.33	11.96	0.00	11.96	4.000	No	Yes	2.00
1442	14.42	9.51	100.00	3.08	0.57	1.33	12.03	0.00	12.03	4.000	No	Yes	2.00
1443	14.43	9.49	100.00	3.08	0.57	1.33	11.96	0.00	11.96	4.000	No	Yes	2.00
1444	14.44	9.42	100.00	3.09	0.58	1.33	11.88	0.00	11.88	4.000	No	Yes	2.00
1445	14.45	9.35	100.00	3.09	0.58	1.33	11.78	0.00	11.78	4.000	No	Yes	2.00
1446	14.46	9.27	100.00	3.10	0.58	1.33	11.68	0.00	11.68	4.000	No	Yes	2.00
1447	14.47	9.19	100.00	3.11	0.58	1.33	11.58	0.00	11.58	4.000	No	Yes	2.00
1448	14.48	9.11	100.00	3.11	0.58	1.33	11.48	0.00	11.48	4.000	No	Yes	2.00
1449	14.49	9.05	100.00	3.12	0.58	1.33	11.39	0.00	11.39	4.000	No	Yes	2.00
1450	14.50	8.95	100.00	3.13	0.58	1.33	11.32	0.00	11.32	4.000	No	Yes	2.00
1451	14.51	8.79	100.00	3.14	0.58	1.33	11.12	0.00	11.12	4.000	No	Yes	2.00
1452	14.52	8.53	100.00	3.15	0.58	1.33	10.77	0.00	10.77	4.000	No	Yes	2.00
1453	14.53	8.20	100.00	3.17	0.58	1.34	10.35	0.00	10.35	4.000	No	Yes	2.00
1454	14.54	7.84	100.00	3.20	0.58	1.34	9.90	0.00	9.90	4.000	No	Yes	2.00
1455	14.55	7.47	100.00	3.22	0.58	1.34	9.43	0.00	9.43	4.000	No	Yes	2.00
1456	14.56	7.10	100.00	3.24	0.59	1.34	8.96	0.00	8.96	4.000	No	Yes	2.00
1457	14.57	6.76	100.00	3.27	0.59	1.34	8.52	0.00	8.52	4.000	No	Yes	2.00
1458	14.58	6.45	100.00	3.29	0.59	1.34	8.14	0.00	8.14	4.000	No	Yes	2.00
1459	14.59	6.23	100.00	3.31	0.59	1.34	7.83	0.00	7.83	4.000	No	Yes	2.00
1460	14.60	6.07	100.00	3.32	0.59	1.34	7.69	0.00	7.69	4.000	No	Yes	2.00
1461	14.61	5.94	100.00	3.33	0.59	1.34	7.53	0.00	7.53	4.000	No	Yes	2.00
1462	14.62	5.80	100.00	3.35	0.59	1.34	7.34	0.00	7.34	4.000	No	Yes	2.00
1463	14.63	5.64	100.00	3.36	0.59	1.34	7.14	0.00	7.14	4.000	No	Yes	2.00
1464	14.64	5.48	100.00	3.37	0.59	1.34	6.94	0.00	6.94	4.000	No	Yes	2.00
1465	14.65	5.33	100.00	3.39	0.60	1.34	6.74	0.00	6.74	4.000	No	Yes	2.00
1466	14.66	5.18	100.00	3.40	0.60	1.34	6.56	0.00	6.56	4.000	No	Yes	2.00
1467	14.67	5.08	100.00	3.41	0.60	1.34	6.40	0.00	6.40	4.000	No	Yes	2.00
1468	14.68	5.05	100.00	3.42	0.60	1.34	6.34	0.00	6.34	4.000	No	Yes	2.00
1469	14.69	5.11	100.00	3.41	0.60	1.34	6.46	0.00	6.46	4.000	No	Yes	2.00
1470	14.70	5.22	100.00	3.40	0.60	1.34	6.60	0.00	6.60	4.000	No	Yes	2.00
1471	14.71	5.34	100.00	3.39	0.60	1.34	6.76	0.00	6.76	4.000	No	Yes	2.00
1472	14.72	5.48	100.00	3.38	0.59	1.34	6.92	0.00	6.92	4.000	No	Yes	2.00
1473	14.73	5.61	100.00	3.37	0.59	1.34	7.09	0.00	7.09	4.000	No	Yes	2.00
1474	14.74	5.73	100.00	3.36	0.59	1.34	7.25	0.00	7.25	4.000	No	Yes	2.00
1475	14.75	5.85	100.00	3.35	0.59	1.34	7.39	0.00	7.39	4.000	No	Yes	2.00
1476	14.76	5.93	100.00	3.34	0.59	1.34	7.51	0.00	7.51	4.000	No	Yes	2.00
1477	14.77	5.97	100.00	3.34	0.59	1.34	7.54	0.00	7.54	4.000	No	Yes	2.00
1478	14.78	5.98	100.00	3.33	0.59	1.34	7.54	0.00	7.54	4.000	No	Yes	2.00
1479	14.79	5.98	100.00	3.33	0.59	1.34	7.54	0.00	7.54	4.000	No	Yes	2.00
1480	14.80	5.98	100.00	3.33	0.59	1.34	7.54	0.00	7.54	4.000	No	Yes	2.00
1481	14.81	5.98	100.00	3.33	0.59	1.33	7.54	0.00	7.54	4.000	No	Yes	2.00
1482	14.82	5.98	100.00	3.33	0.59	1.33	7.53	0.00	7.53	4.000	No	Yes	2.00
1483	14.83	5.98	100.00	3.33	0.59	1.33	7.53	0.00	7.53	4.000	No	Yes	2.00
1484	14.84	5.98	100.00	3.33	0.59	1.33	7.53	0.00	7.53	4.000	No	Yes	2.00
1485	14.85	6.01	100.00	3.32	0.59	1.33	7.53	0.00	7.53	4.000	No	Yes	2.00
1486	14.86	6.09	100.00	3.32	0.59	1.33	7.65	0.00	7.65	4.000	No	Yes	2.00
1487	14.87	6.21	100.00	3.31	0.59	1.33	7.81	0.00	7.81	4.000	No	Yes	2.00
1488	14.88	6.36	100.00	3.29	0.59	1.33	7.99	0.00	7.99	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1489	14.89	6.52	100.00	3.28	0.59	1.33	8.19	0.00	8.19	4.000	No	Yes	2.00
1490	14.90	6.68	100.00	3.27	0.59	1.33	8.39	0.00	8.39	4.000	No	Yes	2.00
1491	14.91	6.83	100.00	3.26	0.59	1.33	8.58	0.00	8.58	4.000	No	Yes	2.00
1492	14.92	6.98	100.00	3.24	0.59	1.33	8.76	0.00	8.76	4.000	No	Yes	2.00
1493	14.93	7.10	100.00	3.24	0.59	1.33	8.91	0.00	8.91	4.000	No	Yes	2.00
1494	14.94	7.21	100.00	3.23	0.59	1.33	9.03	0.00	9.03	4.000	No	Yes	2.00
1495	14.95	7.32	100.00	3.22	0.59	1.33	9.17	0.00	9.17	4.000	No	Yes	2.00
1496	14.96	7.46	100.00	3.21	0.58	1.33	9.33	0.00	9.33	4.000	No	Yes	2.00
1497	14.97	7.61	100.00	3.20	0.58	1.33	9.52	0.00	9.52	4.000	No	Yes	2.00
1498	14.98	7.77	100.00	3.19	0.58	1.32	9.72	0.00	9.72	4.000	No	Yes	2.00
1499	14.99	7.93	100.00	3.18	0.58	1.32	9.91	0.00	9.91	4.000	No	Yes	2.00
1500	15.00	8.08	100.00	3.17	0.58	1.32	10.10	0.00	10.10	4.000	No	Yes	2.00
1501	15.01	8.21	100.00	3.16	0.58	1.32	10.27	0.00	10.27	4.000	No	Yes	2.00
1502	15.02	8.28	100.00	3.15	0.58	1.32	10.41	0.00	10.41	4.000	No	Yes	2.00
1503	15.03	8.26	100.00	3.15	0.58	1.32	10.35	0.00	10.35	4.000	No	Yes	2.00
1504	15.04	8.14	100.00	3.16	0.58	1.32	10.17	0.00	10.17	4.000	No	Yes	2.00
1505	15.05	7.98	100.00	3.17	0.58	1.32	9.97	0.00	9.97	4.000	No	Yes	2.00
1506	15.06	7.80	100.00	3.18	0.58	1.32	9.74	0.00	9.74	4.000	No	Yes	2.00
1507	15.07	7.61	100.00	3.19	0.58	1.32	9.50	0.00	9.50	4.000	No	Yes	2.00
1508	15.08	7.43	100.00	3.20	0.59	1.32	9.27	0.00	9.27	4.000	No	Yes	2.00
1509	15.09	7.26	100.00	3.21	0.59	1.32	9.06	0.00	9.06	4.000	No	Yes	2.00
1510	15.10	7.11	100.00	3.22	0.59	1.32	8.87	0.00	8.87	4.000	No	Yes	2.00
1511	15.11	7.03	100.00	3.22	0.59	1.32	8.72	0.00	8.72	4.000	No	Yes	2.00
1512	15.12	7.03	100.00	3.23	0.59	1.32	8.78	0.00	8.78	4.000	No	Yes	2.00
1513	15.13	7.09	100.00	3.23	0.59	1.32	8.86	0.00	8.86	4.000	No	Yes	2.00
1514	15.14	7.17	100.00	3.22	0.59	1.32	8.95	0.00	8.95	4.000	No	Yes	2.00
1515	15.15	7.25	100.00	3.22	0.59	1.32	9.04	0.00	9.04	4.000	No	Yes	2.00
1516	15.16	7.33	100.00	3.22	0.59	1.32	9.14	0.00	9.14	4.000	No	Yes	2.00
1517	15.17	7.40	100.00	3.22	0.59	1.32	9.24	0.00	9.24	4.000	No	Yes	2.00
1518	15.18	7.47	100.00	3.22	0.58	1.32	9.32	0.00	9.32	4.000	No	Yes	2.00
1519	15.19	7.55	100.00	3.22	0.58	1.32	9.39	0.00	9.39	4.000	No	Yes	2.00
1520	15.20	7.68	100.00	3.22	0.58	1.32	9.51	0.00	9.51	4.000	No	Yes	2.00
1521	15.21	7.89	100.00	3.21	0.58	1.32	9.80	0.00	9.80	4.000	No	Yes	2.00
1522	15.22	8.17	100.00	3.19	0.58	1.32	10.14	0.00	10.14	4.000	No	Yes	2.00
1523	15.23	8.48	100.00	3.18	0.58	1.32	10.53	0.00	10.53	4.000	No	Yes	2.00
1524	15.24	8.81	100.00	3.16	0.58	1.31	10.93	0.00	10.93	4.000	No	Yes	2.00
1525	15.25	9.14	100.00	3.15	0.58	1.31	11.34	0.00	11.34	4.000	No	Yes	2.00
1526	15.26	9.45	100.00	3.14	0.58	1.31	11.72	0.00	11.72	4.000	No	Yes	2.00
1527	15.27	9.73	100.00	3.13	0.57	1.31	12.07	0.00	12.07	4.000	No	Yes	2.00
1528	15.28	9.98	100.00	3.12	0.57	1.31	12.35	0.00	12.35	4.000	No	Yes	2.00
1529	15.29	10.24	100.00	3.11	0.57	1.31	12.62	0.00	12.62	4.000	No	Yes	2.00
1530	15.30	10.54	100.00	3.09	0.57	1.31	12.99	0.00	12.99	4.000	No	Yes	2.00
1531	15.31	10.89	100.00	3.08	0.57	1.31	13.42	0.00	13.42	4.000	No	Yes	2.00
1532	15.32	11.28	100.00	3.06	0.57	1.31	13.89	0.00	13.89	4.000	No	Yes	2.00
1533	15.33	11.68	100.00	3.05	0.57	1.30	14.38	0.00	14.38	4.000	No	Yes	2.00
1534	15.34	12.07	100.00	3.03	0.56	1.30	14.86	0.00	14.86	4.000	No	Yes	2.00
1535	15.35	12.44	100.00	3.02	0.56	1.30	15.30	0.00	15.30	4.000	No	Yes	2.00
1536	15.36	12.75	100.00	3.00	0.56	1.30	15.69	0.00	15.69	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1537	15.37	13.02	100.00	2.99	0.56	1.30	15.99	0.00	15.99	4.000	No	Yes	2.00
1538	15.38	13.27	100.00	2.98	0.56	1.30	16.25	0.00	16.25	4.000	No	Yes	2.00
1539	15.39	13.54	100.00	2.97	0.56	1.30	16.57	0.00	16.57	4.000	No	Yes	2.00
1540	15.40	13.85	99.95	2.96	0.56	1.30	16.94	0.00	16.94	4.000	No	Yes	2.00
1541	15.41	14.18	98.96	2.95	0.56	1.30	17.34	0.00	17.34	4.000	No	Yes	2.00
1542	15.42	14.52	97.97	2.94	0.55	1.29	17.75	0.00	17.75	4.000	No	Yes	2.00
1543	15.43	14.84	97.07	2.93	0.55	1.29	18.14	0.00	18.14	4.000	No	Yes	2.00
1544	15.44	15.14	96.27	2.92	0.55	1.29	18.49	0.00	18.49	4.000	No	Yes	2.00
1545	15.45	15.34	95.70	2.91	0.55	1.29	18.79	0.00	18.79	4.000	No	Yes	2.00
1546	15.46	15.33	95.57	2.91	0.55	1.29	18.84	0.00	18.84	4.000	No	Yes	2.00
1547	15.47	15.11	95.89	2.91	0.55	1.29	18.46	0.00	18.46	4.000	No	Yes	2.00
1548	15.48	14.74	96.51	2.92	0.55	1.29	18.01	0.00	18.01	4.000	No	Yes	2.00
1549	15.49	14.32	97.23	2.93	0.56	1.29	17.50	0.00	17.50	4.000	No	Yes	2.00
1550	15.50	13.88	98.03	2.94	0.56	1.29	16.96	0.00	16.96	4.000	No	Yes	2.00
1551	15.51	13.45	98.89	2.95	0.56	1.29	16.43	0.00	16.43	4.000	No	Yes	2.00
1552	15.52	13.03	99.75	2.96	0.56	1.30	15.92	0.00	15.92	4.000	No	Yes	2.00
1553	15.53	12.66	100.00	2.97	0.56	1.30	15.47	0.00	15.47	4.000	No	Yes	2.00
1554	15.54	12.35	100.00	2.98	0.56	1.30	15.09	0.00	15.09	4.000	No	Yes	2.00
1555	15.55	12.06	100.00	2.99	0.56	1.30	14.79	0.00	14.79	4.000	No	Yes	2.00
1556	15.56	11.75	100.00	3.00	0.57	1.30	14.42	0.00	14.42	4.000	No	Yes	2.00
1557	15.57	11.40	100.00	3.01	0.57	1.30	13.99	0.00	13.99	4.000	No	Yes	2.00
1558	15.58	11.01	100.00	3.03	0.57	1.30	13.51	0.00	13.51	4.000	No	Yes	2.00
1559	15.59	10.61	100.00	3.04	0.57	1.30	13.02	0.00	13.02	4.000	No	Yes	2.00
1560	15.60	10.22	100.00	3.06	0.57	1.30	12.54	0.00	12.54	4.000	No	Yes	2.00
1561	15.61	9.85	100.00	3.08	0.57	1.30	12.09	0.00	12.09	4.000	No	Yes	2.00
1562	15.62	9.54	100.00	3.09	0.58	1.30	11.69	0.00	11.69	4.000	No	Yes	2.00
1563	15.63	9.34	100.00	3.10	0.58	1.30	11.39	0.00	11.39	4.000	No	Yes	2.00
1564	15.64	9.24	100.00	3.11	0.58	1.30	11.36	0.00	11.36	4.000	No	Yes	2.00
1565	15.65	9.20	100.00	3.11	0.58	1.30	11.32	0.00	11.32	4.000	No	Yes	2.00
1566	15.66	9.17	100.00	3.12	0.58	1.30	11.27	0.00	11.27	4.000	No	Yes	2.00
1567	15.67	9.13	100.00	3.12	0.58	1.30	11.22	0.00	11.22	4.000	No	Yes	2.00
1568	15.68	9.09	100.00	3.12	0.58	1.30	11.17	0.00	11.17	4.000	No	Yes	2.00
1569	15.69	9.05	100.00	3.13	0.58	1.30	11.12	0.00	11.12	4.000	No	Yes	2.00
1570	15.70	9.01	100.00	3.13	0.58	1.30	11.07	0.00	11.07	4.000	No	Yes	2.00
1571	15.71	8.98	100.00	3.13	0.58	1.30	11.03	0.00	11.03	4.000	No	Yes	2.00
1572	15.72	8.94	100.00	3.14	0.58	1.30	10.99	0.00	10.99	4.000	No	Yes	2.00
1573	15.73	8.89	100.00	3.14	0.58	1.30	10.92	0.00	10.92	4.000	No	Yes	2.00
1574	15.74	8.82	100.00	3.15	0.58	1.30	10.83	0.00	10.83	4.000	No	Yes	2.00
1575	15.75	8.74	100.00	3.15	0.58	1.30	10.74	0.00	10.74	4.000	No	Yes	2.00
1576	15.76	8.66	100.00	3.16	0.58	1.30	10.64	0.00	10.64	4.000	No	Yes	2.00
1577	15.77	8.58	100.00	3.16	0.58	1.30	10.54	0.00	10.54	4.000	No	Yes	2.00
1578	15.78	8.51	100.00	3.17	0.58	1.30	10.44	0.00	10.44	4.000	No	Yes	2.00
1579	15.79	8.44	100.00	3.17	0.58	1.30	10.36	0.00	10.36	4.000	No	Yes	2.00
1580	15.80	8.38	100.00	3.18	0.58	1.30	10.29	0.00	10.29	4.000	No	Yes	2.00
1581	15.81	8.33	100.00	3.18	0.58	1.30	10.23	0.00	10.23	4.000	No	Yes	2.00
1582	15.82	8.27	100.00	3.19	0.58	1.30	10.15	0.00	10.15	4.000	No	Yes	2.00
1583	15.83	8.20	100.00	3.19	0.58	1.30	10.06	0.00	10.06	4.000	No	Yes	2.00
1584	15.84	8.12	100.00	3.19	0.58	1.30	9.96	0.00	9.96	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1585	15.85	8.04	100.00	3.20	0.58	1.30	9.86	0.00	9.86	4.000	No	Yes	2.00
1586	15.86	7.96	100.00	3.20	0.58	1.30	9.77	0.00	9.77	4.000	No	Yes	2.00
1587	15.87	7.89	100.00	3.21	0.58	1.30	9.67	0.00	9.67	4.000	No	Yes	2.00
1588	15.88	7.82	100.00	3.21	0.58	1.30	9.59	0.00	9.59	4.000	No	Yes	2.00
1589	15.89	7.77	100.00	3.21	0.58	1.30	9.53	0.00	9.53	4.000	No	Yes	2.00
1590	15.90	7.71	100.00	3.22	0.58	1.30	9.47	0.00	9.47	4.000	No	Yes	2.00
1591	15.91	7.65	100.00	3.22	0.58	1.30	9.38	0.00	9.38	4.000	No	Yes	2.00
1592	15.92	7.57	100.00	3.22	0.59	1.30	9.29	0.00	9.29	4.000	No	Yes	2.00
1593	15.93	7.49	100.00	3.22	0.59	1.30	9.19	0.00	9.19	4.000	No	Yes	2.00
1594	15.94	7.41	100.00	3.22	0.59	1.30	9.09	0.00	9.09	4.000	No	Yes	2.00
1595	15.95	7.34	100.00	3.23	0.59	1.30	9.00	0.00	9.00	4.000	No	Yes	2.00
1596	15.96	7.27	100.00	3.23	0.59	1.30	8.91	0.00	8.91	4.000	No	Yes	2.00
1597	15.97	7.21	100.00	3.23	0.59	1.30	8.83	0.00	8.83	4.000	No	Yes	2.00
1598	15.98	7.18	100.00	3.23	0.59	1.30	8.80	0.00	8.80	4.000	No	Yes	2.00
1599	15.99	7.17	100.00	3.23	0.59	1.30	8.79	0.00	8.79	4.000	No	Yes	2.00
1600	16.00	7.17	100.00	3.23	0.59	1.30	8.79	0.00	8.79	4.000	No	Yes	2.00
1601	16.01	7.17	100.00	3.23	0.59	1.30	8.79	0.00	8.79	4.000	No	Yes	2.00
1602	16.02	7.17	100.00	3.23	0.59	1.30	8.79	0.00	8.79	4.000	No	Yes	2.00
1603	16.03	7.17	100.00	3.23	0.59	1.30	8.79	0.00	8.79	4.000	No	Yes	2.00
1604	16.04	7.17	100.00	3.22	0.59	1.30	8.79	0.00	8.79	4.000	No	Yes	2.00
1605	16.05	7.17	100.00	3.22	0.59	1.30	8.78	0.00	8.78	4.000	No	Yes	2.00
1606	16.06	7.17	100.00	3.22	0.59	1.30	8.78	0.00	8.78	4.000	No	Yes	2.00
1607	16.07	7.17	100.00	3.22	0.59	1.30	8.78	0.00	8.78	4.000	No	Yes	2.00
1608	16.08	7.17	100.00	3.22	0.59	1.30	8.78	0.00	8.78	4.000	No	Yes	2.00
1609	16.09	7.17	100.00	3.23	0.59	1.30	8.78	0.00	8.78	4.000	No	Yes	2.00
1610	16.10	7.17	100.00	3.23	0.59	1.30	8.78	0.00	8.78	4.000	No	Yes	2.00
1611	16.11	7.17	100.00	3.23	0.59	1.30	8.77	0.00	8.77	4.000	No	Yes	2.00
1612	16.12	7.17	100.00	3.23	0.59	1.30	8.77	0.00	8.77	4.000	No	Yes	2.00
1613	16.13	7.17	100.00	3.23	0.59	1.29	8.77	0.00	8.77	4.000	No	Yes	2.00
1614	16.14	7.17	100.00	3.23	0.59	1.29	8.77	0.00	8.77	4.000	No	Yes	2.00
1615	16.15	7.17	100.00	3.23	0.59	1.29	8.77	0.00	8.77	4.000	No	Yes	2.00
1616	16.16	7.17	100.00	3.24	0.59	1.29	8.77	0.00	8.77	4.000	No	Yes	2.00
1617	16.17	7.17	100.00	3.24	0.59	1.29	8.76	0.00	8.76	4.000	No	Yes	2.00
1618	16.18	7.17	100.00	3.24	0.59	1.29	8.76	0.00	8.76	4.000	No	Yes	2.00
1619	16.19	7.17	100.00	3.24	0.59	1.29	8.76	0.00	8.76	4.000	No	Yes	2.00
1620	16.20	7.17	100.00	3.25	0.59	1.29	8.76	0.00	8.76	4.000	No	Yes	2.00
1621	16.21	7.17	100.00	3.25	0.59	1.29	8.76	0.00	8.76	4.000	No	Yes	2.00
1622	16.22	7.17	100.00	3.25	0.59	1.29	8.76	0.00	8.76	4.000	No	Yes	2.00
1623	16.23	7.20	100.00	3.25	0.59	1.29	8.75	0.00	8.75	4.000	No	Yes	2.00
1624	16.24	7.31	100.00	3.25	0.59	1.29	8.85	0.00	8.85	4.000	No	Yes	2.00
1625	16.25	7.50	100.00	3.24	0.59	1.29	9.13	0.00	9.13	4.000	No	Yes	2.00
1626	16.26	7.78	100.00	3.22	0.58	1.29	9.46	0.00	9.46	4.000	No	Yes	2.00
1627	16.27	8.08	100.00	3.21	0.58	1.29	9.83	0.00	9.83	4.000	No	Yes	2.00
1628	16.28	8.40	100.00	3.19	0.58	1.29	10.21	0.00	10.21	4.000	No	Yes	2.00
1629	16.29	8.72	100.00	3.18	0.58	1.29	10.60	0.00	10.60	4.000	No	Yes	2.00
1630	16.30	9.02	100.00	3.17	0.58	1.29	10.96	0.00	10.96	4.000	No	Yes	2.00
1631	16.31	9.28	100.00	3.16	0.58	1.28	11.28	0.00	11.28	4.000	No	Yes	2.00
1632	16.32	9.53	100.00	3.15	0.58	1.28	11.54	0.00	11.54	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1633	16.33	9.78	100.00	3.14	0.58	1.28	11.82	0.00	11.82	4.000	No	Yes	2.00
1634	16.34	10.09	100.00	3.12	0.57	1.28	12.19	0.00	12.19	4.000	No	Yes	2.00
1635	16.35	10.44	100.00	3.11	0.57	1.28	12.62	0.00	12.62	4.000	No	Yes	2.00
1636	16.36	10.83	100.00	3.09	0.57	1.28	13.08	0.00	13.08	4.000	No	Yes	2.00
1637	16.37	11.23	100.00	3.07	0.57	1.28	13.56	0.00	13.56	4.000	No	Yes	2.00
1638	16.38	11.63	100.00	3.06	0.57	1.28	14.03	0.00	14.03	4.000	No	Yes	2.00
1639	16.39	11.99	100.00	3.04	0.57	1.28	14.46	0.00	14.46	4.000	No	Yes	2.00
1640	16.40	12.30	100.00	3.03	0.56	1.27	14.84	0.00	14.84	4.000	No	Yes	2.00
1641	16.41	12.60	100.00	3.02	0.56	1.27	15.14	0.00	15.14	4.000	No	Yes	2.00
1642	16.42	12.93	100.00	3.01	0.56	1.27	15.51	0.00	15.51	4.000	No	Yes	2.00
1643	16.43	13.32	100.00	2.99	0.56	1.27	15.98	0.00	15.98	4.000	No	Yes	2.00
1644	16.44	13.76	100.00	2.97	0.56	1.27	16.50	0.00	16.50	4.000	No	Yes	2.00
1645	16.45	14.24	99.43	2.96	0.56	1.27	17.06	0.00	17.06	4.000	No	Yes	2.00
1646	16.46	14.72	97.99	2.94	0.55	1.27	17.63	0.00	17.63	4.000	No	Yes	2.00
1647	16.47	15.18	96.68	2.92	0.55	1.27	18.18	0.00	18.18	4.000	No	Yes	2.00
1648	16.48	15.60	95.52	2.91	0.55	1.27	18.67	0.00	18.67	4.000	No	Yes	2.00
1649	16.49	15.98	94.51	2.89	0.55	1.26	19.09	0.00	19.09	4.000	No	Yes	2.00
1650	16.50	16.39	93.47	2.88	0.55	1.26	19.49	0.00	19.49	4.000	No	Yes	2.00
1651	16.51	16.89	92.28	2.87	0.55	1.26	20.10	0.00	20.10	4.000	No	Yes	2.00
1652	16.52	17.51	90.86	2.85	0.55	1.26	20.83	0.00	20.83	4.000	No	Yes	2.00
1653	16.53	18.19	89.32	2.83	0.54	1.26	21.64	0.00	21.64	4.000	No	Yes	2.00
1654	16.54	18.91	87.74	2.81	0.54	1.26	22.48	0.00	22.48	4.000	No	Yes	2.00
1655	16.55	19.63	86.20	2.79	0.54	1.26	23.31	0.00	23.31	4.000	No	Yes	2.00
1656	16.56	20.30	84.77	2.77	0.54	1.26	24.10	0.00	24.10	4.000	No	Yes	2.00
1657	16.57	20.90	83.52	2.76	0.53	1.25	24.80	0.00	24.80	4.000	No	Yes	2.00
1658	16.58	21.30	82.61	2.75	0.53	1.25	25.36	0.00	25.36	4.000	No	Yes	2.00
1659	16.59	21.52	81.97	2.74	0.53	1.25	25.49	0.00	25.49	4.000	No	Yes	2.00
1660	16.60	21.60	81.50	2.73	0.53	1.25	25.55	0.00	25.55	4.000	No	Yes	2.00
1661	16.61	21.66	80.98	2.72	0.53	1.25	25.61	0.00	25.61	4.000	No	Yes	2.00
1662	16.62	21.72	80.41	2.72	0.53	1.25	25.68	0.00	25.68	4.000	No	Yes	2.00
1663	16.63	21.78	79.81	2.71	0.53	1.25	25.75	0.00	25.75	4.000	No	Yes	2.00
1664	16.64	21.84	79.21	2.70	0.53	1.25	25.82	0.00	25.82	4.000	No	Yes	2.00
1665	16.65	21.90	78.65	2.70	0.53	1.25	25.89	0.00	25.89	4.000	No	Yes	2.00
1666	16.66	21.94	78.19	2.69	0.53	1.25	25.94	0.00	25.94	4.000	No	Yes	2.00
1667	16.67	21.87	78.02	2.69	0.53	1.25	25.94	0.00	25.94	4.000	No	Yes	2.00
1668	16.68	21.67	78.15	2.69	0.53	1.25	25.63	0.00	25.63	4.000	No	Yes	2.00
1669	16.69	21.34	78.53	2.69	0.53	1.25	25.24	0.00	25.24	4.000	No	Yes	2.00
1670	16.70	20.97	78.98	2.70	0.54	1.25	24.80	0.00	24.80	4.000	No	Yes	2.00
1671	16.71	20.58	79.47	2.71	0.54	1.25	24.34	0.00	24.34	4.000	No	Yes	2.00
1672	16.72	20.18	79.97	2.71	0.54	1.25	23.86	0.00	23.86	4.000	No	Yes	2.00
1673	16.73	19.79	80.46	2.72	0.54	1.25	23.41	0.00	23.41	4.000	No	Yes	2.00
1674	16.74	19.45	80.92	2.72	0.54	1.25	23.00	0.00	23.00	4.000	No	Yes	2.00
1675	16.75	19.15	81.38	2.73	0.54	1.25	22.65	0.00	22.65	4.000	No	Yes	2.00
1676	16.76	18.88	81.94	2.74	0.54	1.25	22.38	0.00	22.38	4.000	No	Yes	2.00
1677	16.77	18.59	82.69	2.75	0.54	1.25	22.05	0.00	22.05	4.000	No	Yes	2.00
1678	16.78	18.26	83.63	2.76	0.54	1.25	21.65	0.00	21.65	4.000	No	Yes	2.00
1679	16.79	17.90	84.67	2.77	0.55	1.25	21.22	0.00	21.22	4.000	No	Yes	2.00
1680	16.80	17.51	85.77	2.78	0.55	1.25	20.76	0.00	20.76	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1681	16.81	17.13	86.86	2.80	0.55	1.26	20.31	0.00	20.31	4.000	No	Yes	2.00
1682	16.82	16.78	87.90	2.81	0.55	1.26	19.88	0.00	19.88	4.000	No	Yes	2.00
1683	16.83	16.46	88.82	2.82	0.55	1.26	19.50	0.00	19.50	4.000	No	Yes	2.00
1684	16.84	16.15	89.72	2.83	0.55	1.26	19.19	0.00	19.19	4.000	No	Yes	2.00
1685	16.85	15.79	90.77	2.85	0.55	1.26	18.78	0.00	18.78	4.000	No	Yes	2.00
1686	16.86	15.33	92.11	2.86	0.55	1.26	18.23	0.00	18.23	4.000	No	Yes	2.00
1687	16.87	14.79	93.70	2.88	0.56	1.26	17.59	0.00	17.59	4.000	No	Yes	2.00
1688	16.88	14.21	95.46	2.91	0.56	1.26	16.89	0.00	16.89	4.000	No	Yes	2.00
1689	16.89	13.61	97.31	2.93	0.56	1.26	16.18	0.00	16.18	4.000	No	Yes	2.00
1690	16.90	13.02	99.25	2.95	0.56	1.26	15.48	0.00	15.48	4.000	No	Yes	2.00
1691	16.91	12.48	100.00	2.98	0.56	1.26	14.83	0.00	14.83	4.000	No	Yes	2.00
1692	16.92	12.02	100.00	3.00	0.57	1.26	14.27	0.00	14.27	4.000	No	Yes	2.00
1693	16.93	11.69	100.00	3.01	0.57	1.26	13.87	0.00	13.87	4.000	No	Yes	2.00
1694	16.94	11.46	100.00	3.02	0.57	1.26	13.68	0.00	13.68	4.000	No	Yes	2.00
1695	16.95	11.26	100.00	3.04	0.57	1.26	13.44	0.00	13.44	4.000	No	Yes	2.00
1696	16.96	11.04	100.00	3.05	0.57	1.26	13.17	0.00	13.17	4.000	No	Yes	2.00
1697	16.97	10.80	100.00	3.06	0.57	1.26	12.89	0.00	12.89	4.000	No	Yes	2.00
1698	16.98	10.56	100.00	3.08	0.57	1.26	12.60	0.00	12.60	4.000	No	Yes	2.00
1699	16.99	10.33	100.00	3.09	0.57	1.26	12.32	0.00	12.32	4.000	No	Yes	2.00
1700	17.00	10.12	100.00	3.10	0.57	1.26	12.07	0.00	12.07	4.000	No	Yes	2.00
1701	17.01	9.98	100.00	3.11	0.58	1.26	11.86	0.00	11.86	4.000	No	Yes	2.00
1702	17.02	9.94	100.00	3.11	0.58	1.26	11.82	0.00	11.82	4.000	No	Yes	2.00
1703	17.03	9.99	100.00	3.11	0.57	1.26	11.92	0.00	11.92	4.000	No	Yes	2.00
1704	17.04	10.10	100.00	3.11	0.57	1.26	12.04	0.00	12.04	4.000	No	Yes	2.00
1705	17.05	10.21	100.00	3.10	0.57	1.26	12.17	0.00	12.17	4.000	No	Yes	2.00
1706	17.06	10.33	100.00	3.10	0.57	1.26	12.31	0.00	12.31	4.000	No	Yes	2.00
1707	17.07	10.45	100.00	3.09	0.57	1.26	12.45	0.00	12.45	4.000	No	Yes	2.00
1708	17.08	10.56	100.00	3.09	0.57	1.26	12.58	0.00	12.58	4.000	No	Yes	2.00
1709	17.09	10.66	100.00	3.09	0.57	1.26	12.70	0.00	12.70	4.000	No	Yes	2.00
1710	17.10	10.73	100.00	3.08	0.57	1.26	12.79	0.00	12.79	4.000	No	Yes	2.00
1711	17.11	10.76	100.00	3.08	0.57	1.26	12.80	0.00	12.80	4.000	No	Yes	2.00
1712	17.12	10.76	100.00	3.08	0.57	1.26	12.80	0.00	12.80	4.000	No	Yes	2.00
1713	17.13	10.76	100.00	3.07	0.57	1.26	12.80	0.00	12.80	4.000	No	Yes	2.00
1714	17.14	10.76	100.00	3.07	0.57	1.26	12.79	0.00	12.79	4.000	No	Yes	2.00
1715	17.15	10.76	100.00	3.06	0.57	1.26	12.79	0.00	12.79	4.000	No	Yes	2.00
1716	17.16	10.76	100.00	3.06	0.57	1.26	12.79	0.00	12.79	4.000	No	Yes	2.00
1717	17.17	10.76	100.00	3.06	0.57	1.26	12.79	0.00	12.79	4.000	No	Yes	2.00
1718	17.18	10.75	100.00	3.05	0.57	1.26	12.78	0.00	12.78	4.000	No	Yes	2.00
1719	17.19	10.66	100.00	3.05	0.57	1.26	12.74	0.00	12.74	4.000	No	Yes	2.00
1720	17.20	10.47	100.00	3.06	0.57	1.26	12.46	0.00	12.46	4.000	No	Yes	2.00
1721	17.21	10.18	100.00	3.07	0.57	1.26	12.12	0.00	12.12	4.000	No	Yes	2.00
1722	17.22	9.86	100.00	3.08	0.58	1.26	11.73	0.00	11.73	4.000	No	Yes	2.00
1723	17.23	9.52	100.00	3.09	0.58	1.26	11.32	0.00	11.32	4.000	No	Yes	2.00
1724	17.24	9.17	100.00	3.10	0.58	1.26	10.91	0.00	10.91	4.000	No	Yes	2.00
1725	17.25	8.84	100.00	3.12	0.58	1.26	10.51	0.00	10.51	4.000	No	Yes	2.00
1726	17.26	8.54	100.00	3.13	0.58	1.26	10.15	0.00	10.15	4.000	No	Yes	2.00
1727	17.27	8.28	100.00	3.14	0.58	1.26	9.85	0.00	9.85	4.000	No	Yes	2.00
1728	17.28	8.04	100.00	3.15	0.58	1.26	9.61	0.00	9.61	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1729	17.29	7.79	100.00	3.17	0.59	1.26	9.30	0.00	9.30	4.000	No	Yes	2.00
1730	17.30	7.49	100.00	3.19	0.59	1.26	8.94	0.00	8.94	4.000	No	Yes	2.00
1731	17.31	7.15	100.00	3.21	0.59	1.26	8.54	0.00	8.54	4.000	No	Yes	2.00
1732	17.32	6.81	100.00	3.23	0.59	1.26	8.12	0.00	8.12	4.000	No	Yes	2.00
1733	17.33	6.46	100.00	3.26	0.59	1.26	7.71	0.00	7.71	4.000	No	Yes	2.00
1734	17.34	6.14	100.00	3.28	0.59	1.26	7.32	0.00	7.32	4.000	No	Yes	2.00
1735	17.35	5.86	100.00	3.31	0.59	1.27	6.98	0.00	6.98	4.000	No	Yes	2.00
1736	17.36	5.68	100.00	3.32	0.60	1.27	6.70	0.00	6.70	4.000	No	Yes	2.00
1737	17.37	5.60	100.00	3.33	0.60	1.27	6.68	0.00	6.68	4.000	No	Yes	2.00
1738	17.38	5.62	100.00	3.33	0.60	1.27	6.71	0.00	6.71	4.000	No	Yes	2.00
1739	17.39	5.64	100.00	3.33	0.60	1.27	6.74	0.00	6.74	4.000	No	Yes	2.00
1740	17.40	5.67	100.00	3.33	0.60	1.26	6.77	0.00	6.77	4.000	No	Yes	2.00
1741	17.41	5.69	100.00	3.33	0.60	1.26	6.80	0.00	6.80	4.000	No	Yes	2.00
1742	17.42	5.72	100.00	3.33	0.59	1.26	6.83	0.00	6.83	4.000	No	Yes	2.00
1743	17.43	5.74	100.00	3.33	0.59	1.26	6.86	0.00	6.86	4.000	No	Yes	2.00
1744	17.44	5.76	100.00	3.33	0.59	1.26	6.88	0.00	6.88	4.000	No	Yes	2.00
1745	17.45	5.78	100.00	3.33	0.59	1.26	6.90	0.00	6.90	4.000	No	Yes	2.00
1746	17.46	5.80	100.00	3.33	0.59	1.26	6.92	0.00	6.92	4.000	No	Yes	2.00
1747	17.47	5.82	100.00	3.33	0.59	1.26	6.94	0.00	6.94	4.000	No	Yes	2.00
1748	17.48	5.85	100.00	3.33	0.59	1.26	6.97	0.00	6.97	4.000	No	Yes	2.00
1749	17.49	5.87	100.00	3.33	0.59	1.26	7.00	0.00	7.00	4.000	No	Yes	2.00
1750	17.50	5.90	100.00	3.33	0.59	1.26	7.03	0.00	7.03	4.000	No	Yes	2.00
1751	17.51	5.93	100.00	3.33	0.59	1.26	7.06	0.00	7.06	4.000	No	Yes	2.00
1752	17.52	5.95	100.00	3.33	0.59	1.26	7.09	0.00	7.09	4.000	No	Yes	2.00
1753	17.53	5.98	100.00	3.33	0.59	1.26	7.11	0.00	7.11	4.000	No	Yes	2.00
1754	17.54	6.05	100.00	3.32	0.59	1.26	7.18	0.00	7.18	4.000	No	Yes	2.00
1755	17.55	6.16	100.00	3.32	0.59	1.26	7.32	0.00	7.32	4.000	No	Yes	2.00
1756	17.56	6.30	100.00	3.31	0.59	1.26	7.48	0.00	7.48	4.000	No	Yes	2.00
1757	17.57	6.45	100.00	3.30	0.59	1.26	7.67	0.00	7.67	4.000	No	Yes	2.00
1758	17.58	6.61	100.00	3.29	0.59	1.26	7.85	0.00	7.85	4.000	No	Yes	2.00
1759	17.59	6.77	100.00	3.28	0.59	1.26	8.04	0.00	8.04	4.000	No	Yes	2.00
1760	17.60	6.92	100.00	3.28	0.59	1.26	8.22	0.00	8.22	4.000	No	Yes	2.00
1761	17.61	7.05	100.00	3.27	0.59	1.26	8.37	0.00	8.37	4.000	No	Yes	2.00
1762	17.62	7.16	100.00	3.26	0.59	1.26	8.50	0.00	8.50	4.000	No	Yes	2.00
1763	17.63	7.27	100.00	3.26	0.59	1.26	8.61	0.00	8.61	4.000	No	Yes	2.00
1764	17.64	7.40	100.00	3.25	0.59	1.26	8.76	0.00	8.76	4.000	No	Yes	2.00
1765	17.65	7.54	100.00	3.25	0.59	1.25	8.93	0.00	8.93	4.000	No	Yes	2.00
1766	17.66	7.70	100.00	3.24	0.59	1.25	9.12	0.00	9.12	4.000	No	Yes	2.00
1767	17.67	7.86	100.00	3.23	0.59	1.25	9.30	0.00	9.30	4.000	No	Yes	2.00
1768	17.68	8.02	100.00	3.23	0.58	1.25	9.49	0.00	9.49	4.000	No	Yes	2.00
1769	17.69	8.16	100.00	3.22	0.58	1.25	9.66	0.00	9.66	4.000	No	Yes	2.00
1770	17.70	8.27	100.00	3.22	0.58	1.25	9.80	0.00	9.80	4.000	No	Yes	2.00
1771	17.71	8.32	100.00	3.22	0.58	1.25	9.88	0.00	9.88	4.000	No	Yes	2.00
1772	17.72	8.30	100.00	3.22	0.58	1.25	9.81	0.00	9.81	4.000	No	Yes	2.00
1773	17.73	8.23	100.00	3.22	0.58	1.25	9.73	0.00	9.73	4.000	No	Yes	2.00
1774	17.74	8.16	100.00	3.23	0.58	1.25	9.64	0.00	9.64	4.000	No	Yes	2.00
1775	17.75	8.08	100.00	3.23	0.58	1.25	9.54	0.00	9.54	4.000	No	Yes	2.00
1776	17.76	8.00	100.00	3.24	0.58	1.25	9.45	0.00	9.45	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1777	17.77	7.92	100.00	3.25	0.58	1.25	9.36	0.00	9.36	4.000	No	Yes	2.00
1778	17.78	7.85	100.00	3.25	0.59	1.25	9.27	0.00	9.27	4.000	No	Yes	2.00
1779	17.79	7.80	100.00	3.26	0.59	1.25	9.20	0.00	9.20	4.000	No	Yes	2.00
1780	17.80	7.74	100.00	3.26	0.59	1.25	9.14	0.00	9.14	4.000	No	Yes	2.00
1781	17.81	7.68	100.00	3.26	0.59	1.25	9.07	0.00	9.07	4.000	No	Yes	2.00
1782	17.82	7.61	100.00	3.27	0.59	1.25	8.99	0.00	8.99	4.000	No	Yes	2.00
1783	17.83	7.53	100.00	3.28	0.59	1.25	8.90	0.00	8.90	4.000	No	Yes	2.00
1784	17.84	7.45	100.00	3.28	0.59	1.25	8.80	0.00	8.80	4.000	No	Yes	2.00
1785	17.85	7.38	100.00	3.29	0.59	1.25	8.70	0.00	8.70	4.000	No	Yes	2.00
1786	17.86	7.30	100.00	3.30	0.59	1.25	8.61	0.00	8.61	4.000	No	Yes	2.00
1787	17.87	7.24	100.00	3.30	0.59	1.25	8.54	0.00	8.54	4.000	No	Yes	2.00
1788	17.88	7.19	100.00	3.31	0.59	1.25	8.47	0.00	8.47	4.000	No	Yes	2.00
1789	17.89	7.18	100.00	3.31	0.59	1.25	8.47	0.00	8.47	4.000	No	Yes	2.00
1790	17.90	7.17	100.00	3.31	0.59	1.25	8.46	0.00	8.46	4.000	No	Yes	2.00
1791	17.91	7.17	100.00	3.31	0.59	1.25	8.46	0.00	8.46	4.000	No	Yes	2.00
1792	17.92	7.17	100.00	3.31	0.59	1.25	8.46	0.00	8.46	4.000	No	Yes	2.00
1793	17.93	7.17	100.00	3.32	0.59	1.25	8.46	0.00	8.46	4.000	No	Yes	2.00
1794	17.94	7.17	100.00	3.32	0.59	1.25	8.46	0.00	8.46	4.000	No	Yes	2.00
1795	17.95	7.17	100.00	3.32	0.59	1.25	8.46	0.00	8.46	4.000	No	Yes	2.00
1796	17.96	7.18	100.00	3.32	0.59	1.25	8.45	0.00	8.45	4.000	No	Yes	2.00
1797	17.97	7.21	100.00	3.32	0.59	1.25	8.47	0.00	8.47	4.000	No	Yes	2.00
1798	17.98	7.27	100.00	3.32	0.59	1.25	8.55	0.00	8.55	4.000	No	Yes	2.00
1799	17.99	7.36	100.00	3.31	0.59	1.25	8.66	0.00	8.66	4.000	No	Yes	2.00
1800	18.00	7.46	100.00	3.30	0.59	1.25	8.77	0.00	8.77	4.000	No	Yes	2.00
1801	18.01	7.56	100.00	3.30	0.59	1.25	8.90	0.00	8.90	4.000	No	Yes	2.00
1802	18.02	7.67	100.00	3.29	0.59	1.25	9.02	0.00	9.02	4.000	No	Yes	2.00
1803	18.03	7.77	100.00	3.28	0.59	1.25	9.14	0.00	9.14	4.000	No	Yes	2.00
1804	18.04	7.86	100.00	3.28	0.59	1.24	9.25	0.00	9.25	4.000	No	Yes	2.00
1805	18.05	7.98	100.00	3.27	0.58	1.24	9.33	0.00	9.33	4.000	No	Yes	2.00
1806	18.06	8.18	100.00	3.26	0.58	1.24	9.55	0.00	9.55	4.000	No	Yes	2.00
1807	18.07	8.50	100.00	3.24	0.58	1.24	9.94	0.00	9.94	4.000	No	Yes	2.00
1808	18.08	8.89	100.00	3.22	0.58	1.24	10.41	0.00	10.41	4.000	No	Yes	2.00
1809	18.09	9.33	100.00	3.19	0.58	1.24	10.92	0.00	10.92	4.000	No	Yes	2.00
1810	18.10	9.78	100.00	3.17	0.58	1.24	11.45	0.00	11.45	4.000	No	Yes	2.00
1811	18.11	10.23	100.00	3.15	0.57	1.24	11.97	0.00	11.97	4.000	No	Yes	2.00
1812	18.12	10.65	100.00	3.13	0.57	1.24	12.46	0.00	12.46	4.000	No	Yes	2.00
1813	18.13	11.01	100.00	3.11	0.57	1.24	12.88	0.00	12.88	4.000	No	Yes	2.00
1814	18.14	11.42	100.00	3.09	0.57	1.24	13.23	0.00	13.23	4.000	No	Yes	2.00
1815	18.15	11.92	100.00	3.07	0.57	1.23	13.82	0.00	13.82	4.000	No	Yes	2.00
1816	18.16	12.59	100.00	3.05	0.56	1.23	14.61	0.00	14.61	4.000	No	Yes	2.00
1817	18.17	13.36	100.00	3.02	0.56	1.23	15.51	0.00	15.51	4.000	No	Yes	2.00
1818	18.18	14.20	100.00	2.99	0.56	1.23	16.47	0.00	16.47	4.000	No	Yes	2.00
1819	18.19	15.06	99.71	2.96	0.55	1.23	17.45	0.00	17.45	4.000	No	Yes	2.00
1820	18.20	15.88	97.57	2.93	0.55	1.23	18.41	0.00	18.41	4.000	No	Yes	2.00
1821	18.21	16.64	95.75	2.91	0.55	1.22	19.28	0.00	19.28	4.000	No	Yes	2.00
1822	18.22	17.27	94.28	2.89	0.55	1.22	20.03	0.00	20.03	4.000	No	Yes	2.00
1823	18.23	17.74	93.15	2.88	0.55	1.22	20.53	0.00	20.53	4.000	No	Yes	2.00
1824	18.24	18.09	92.19	2.86	0.54	1.22	20.84	0.00	20.84	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1825	18.25	18.43	91.19	2.85	0.54	1.22	21.23	0.00	21.23	4.000	No	Yes	2.00
1826	18.26	18.80	90.07	2.84	0.54	1.22	21.65	0.00	21.65	4.000	No	Yes	2.00
1827	18.27	19.20	88.88	2.82	0.54	1.22	22.11	0.00	22.11	4.000	No	Yes	2.00
1828	18.28	19.60	87.68	2.81	0.54	1.22	22.56	0.00	22.56	4.000	No	Yes	2.00
1829	18.29	19.98	86.53	2.79	0.54	1.22	22.99	0.00	22.99	4.000	No	Yes	2.00
1830	18.30	20.32	85.50	2.78	0.54	1.22	23.38	0.00	23.38	4.000	No	Yes	2.00
1831	18.31	20.53	84.77	2.77	0.54	1.22	23.69	0.00	23.69	4.000	No	Yes	2.00
1832	18.32	20.55	84.37	2.77	0.54	1.22	23.68	0.00	23.68	4.000	No	Yes	2.00
1833	18.33	20.40	84.27	2.77	0.54	1.22	23.44	0.00	23.44	4.000	No	Yes	2.00
1834	18.34	20.15	84.25	2.77	0.54	1.22	23.17	0.00	23.17	4.000	No	Yes	2.00
1835	18.35	19.89	84.22	2.77	0.54	1.22	22.86	0.00	22.86	4.000	No	Yes	2.00
1836	18.36	19.62	84.20	2.76	0.54	1.22	22.54	0.00	22.54	4.000	No	Yes	2.00
1837	18.37	19.34	84.18	2.76	0.54	1.22	22.23	0.00	22.23	4.000	No	Yes	2.00
1838	18.38	19.09	84.16	2.76	0.54	1.22	21.94	0.00	21.94	4.000	No	Yes	2.00
1839	18.39	18.87	84.14	2.76	0.54	1.22	21.68	0.00	21.68	4.000	No	Yes	2.00
1840	18.40	18.63	84.32	2.77	0.54	1.22	21.48	0.00	21.48	4.000	No	Yes	2.00
1841	18.41	18.33	84.75	2.77	0.55	1.22	21.12	0.00	21.12	4.000	No	Yes	2.00
1842	18.42	17.94	85.49	2.78	0.55	1.22	20.66	0.00	20.66	4.000	No	Yes	2.00
1843	18.43	17.48	86.37	2.79	0.55	1.22	20.13	0.00	20.13	4.000	No	Yes	2.00
1844	18.44	16.99	87.34	2.80	0.55	1.22	19.56	0.00	19.56	4.000	No	Yes	2.00
1845	18.45	16.48	88.35	2.82	0.55	1.22	18.98	0.00	18.98	4.000	No	Yes	2.00
1846	18.46	16.00	89.36	2.83	0.55	1.22	18.42	0.00	18.42	4.000	No	Yes	2.00
1847	18.47	15.55	90.32	2.84	0.56	1.22	17.90	0.00	17.90	4.000	No	Yes	2.00
1848	18.48	15.17	91.18	2.85	0.56	1.22	17.46	0.00	17.46	4.000	No	Yes	2.00
1849	18.49	14.80	92.08	2.86	0.56	1.22	17.10	0.00	17.10	4.000	No	Yes	2.00
1850	18.50	14.40	93.15	2.88	0.56	1.22	16.65	0.00	16.65	4.000	No	Yes	2.00
1851	18.51	13.93	94.49	2.89	0.56	1.22	16.10	0.00	16.10	4.000	No	Yes	2.00
1852	18.52	13.39	96.03	2.91	0.56	1.22	15.48	0.00	15.48	4.000	No	Yes	2.00
1853	18.53	12.83	97.74	2.93	0.56	1.22	14.82	0.00	14.82	4.000	No	Yes	2.00
1854	18.54	12.27	99.57	2.96	0.57	1.22	14.17	0.00	14.17	4.000	No	Yes	2.00
1855	18.55	11.73	100.00	2.98	0.57	1.22	13.55	0.00	13.55	4.000	No	Yes	2.00
1856	18.56	11.25	100.00	3.00	0.57	1.23	12.99	0.00	12.99	4.000	No	Yes	2.00
1857	18.57	10.87	100.00	3.02	0.57	1.23	12.53	0.00	12.53	4.000	No	Yes	2.00
1858	18.58	10.56	100.00	3.03	0.57	1.23	12.23	0.00	12.23	4.000	No	Yes	2.00
1859	18.59	10.28	100.00	3.05	0.57	1.23	11.92	0.00	11.92	4.000	No	Yes	2.00
1860	18.60	9.97	100.00	3.06	0.58	1.23	11.56	0.00	11.56	4.000	No	Yes	2.00
1861	18.61	9.63	100.00	3.08	0.58	1.23	11.16	0.00	11.16	4.000	No	Yes	2.00
1862	18.62	9.28	100.00	3.10	0.58	1.23	10.75	0.00	10.75	4.000	No	Yes	2.00
1863	18.63	8.93	100.00	3.12	0.58	1.23	10.35	0.00	10.35	4.000	No	Yes	2.00
1864	18.64	8.61	100.00	3.14	0.58	1.23	9.97	0.00	9.97	4.000	No	Yes	2.00
1865	18.65	8.32	100.00	3.16	0.58	1.23	9.64	0.00	9.64	4.000	No	Yes	2.00
1866	18.66	8.10	100.00	3.17	0.58	1.23	9.37	0.00	9.37	4.000	No	Yes	2.00
1867	18.67	7.91	100.00	3.18	0.59	1.23	9.20	0.00	9.20	4.000	No	Yes	2.00
1868	18.68	7.73	100.00	3.20	0.59	1.23	8.99	0.00	8.99	4.000	No	Yes	2.00
1869	18.69	7.53	100.00	3.21	0.59	1.23	8.74	0.00	8.74	4.000	No	Yes	2.00
1870	18.70	7.30	100.00	3.23	0.59	1.23	8.48	0.00	8.48	4.000	No	Yes	2.00
1871	18.71	7.08	100.00	3.24	0.59	1.23	8.22	0.00	8.22	4.000	No	Yes	2.00
1872	18.72	6.86	100.00	3.26	0.59	1.23	7.96	0.00	7.96	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1873	18.73	6.66	100.00	3.28	0.59	1.23	7.72	0.00	7.72	4.000	No	Yes	2.00
1874	18.74	6.49	100.00	3.29	0.59	1.23	7.52	0.00	7.52	4.000	No	Yes	2.00
1875	18.75	6.37	100.00	3.30	0.59	1.23	7.39	0.00	7.39	4.000	No	Yes	2.00
1876	18.76	6.28	100.00	3.31	0.59	1.23	7.30	0.00	7.30	4.000	No	Yes	2.00
1877	18.77	6.19	100.00	3.32	0.59	1.23	7.19	0.00	7.19	4.000	No	Yes	2.00
1878	18.78	6.09	100.00	3.33	0.59	1.23	7.07	0.00	7.07	4.000	No	Yes	2.00
1879	18.79	5.98	100.00	3.34	0.59	1.23	6.95	0.00	6.95	4.000	No	Yes	2.00
1880	18.80	5.87	100.00	3.36	0.59	1.23	6.82	0.00	6.82	4.000	No	Yes	2.00
1881	18.81	5.77	100.00	3.37	0.60	1.23	6.70	0.00	6.70	4.000	No	Yes	2.00
1882	18.82	5.68	100.00	3.38	0.60	1.23	6.59	0.00	6.59	4.000	No	Yes	2.00
1883	18.83	5.62	100.00	3.38	0.60	1.23	6.51	0.00	6.51	4.000	No	Yes	2.00
1884	18.84	5.59	100.00	3.39	0.60	1.23	6.48	0.00	6.48	4.000	No	Yes	2.00
1885	18.85	5.58	100.00	3.39	0.60	1.23	6.48	0.00	6.48	4.000	No	Yes	2.00
1886	18.86	5.58	100.00	3.40	0.60	1.23	6.48	0.00	6.48	4.000	No	Yes	2.00
1887	18.87	5.58	100.00	3.40	0.60	1.23	6.48	0.00	6.48	4.000	No	Yes	2.00
1888	18.88	5.58	100.00	3.40	0.60	1.23	6.48	0.00	6.48	4.000	No	Yes	2.00
1889	18.89	5.58	100.00	3.40	0.60	1.23	6.47	0.00	6.47	4.000	No	Yes	2.00
1890	18.90	5.58	100.00	3.41	0.60	1.23	6.47	0.00	6.47	4.000	No	Yes	2.00
1891	18.91	5.58	100.00	3.41	0.60	1.23	6.47	0.00	6.47	4.000	No	Yes	2.00
1892	18.92	5.60	100.00	3.41	0.60	1.23	6.47	0.00	6.47	4.000	No	Yes	2.00
1893	18.93	5.65	100.00	3.41	0.60	1.23	6.55	0.00	6.55	4.000	No	Yes	2.00
1894	18.94	5.74	100.00	3.40	0.60	1.23	6.65	0.00	6.65	4.000	No	Yes	2.00
1895	18.95	5.84	100.00	3.39	0.60	1.23	6.76	0.00	6.76	4.000	No	Yes	2.00
1896	18.96	5.94	100.00	3.38	0.59	1.23	6.88	0.00	6.88	4.000	No	Yes	2.00
1897	18.97	6.05	100.00	3.38	0.59	1.23	7.01	0.00	7.01	4.000	No	Yes	2.00
1898	18.98	6.15	100.00	3.37	0.59	1.23	7.12	0.00	7.12	4.000	No	Yes	2.00
1899	18.99	6.25	100.00	3.36	0.59	1.23	7.23	0.00	7.23	4.000	No	Yes	2.00
1900	19.00	6.33	100.00	3.36	0.59	1.23	7.33	0.00	7.33	4.000	No	Yes	2.00
1901	19.01	6.40	100.00	3.35	0.59	1.22	7.40	0.00	7.40	4.000	No	Yes	2.00
1902	19.02	6.48	100.00	3.35	0.59	1.22	7.48	0.00	7.48	4.000	No	Yes	2.00
1903	19.03	6.57	100.00	3.34	0.59	1.22	7.59	0.00	7.59	4.000	No	Yes	2.00
1904	19.04	6.67	100.00	3.33	0.59	1.22	7.70	0.00	7.70	4.000	No	Yes	2.00
1905	19.05	6.78	100.00	3.32	0.59	1.22	7.83	0.00	7.83	4.000	No	Yes	2.00
1906	19.06	6.88	100.00	3.31	0.59	1.22	7.95	0.00	7.95	4.000	No	Yes	2.00
1907	19.07	6.98	100.00	3.31	0.59	1.22	8.06	0.00	8.06	4.000	No	Yes	2.00
1908	19.08	7.07	100.00	3.30	0.59	1.22	8.17	0.00	8.17	4.000	No	Yes	2.00
1909	19.09	7.13	100.00	3.29	0.59	1.22	8.25	0.00	8.25	4.000	No	Yes	2.00
1910	19.10	7.17	100.00	3.29	0.59	1.22	8.27	0.00	8.27	4.000	No	Yes	2.00
1911	19.11	7.17	100.00	3.29	0.59	1.22	8.27	0.00	8.27	4.000	No	Yes	2.00
1912	19.12	7.17	100.00	3.29	0.59	1.22	8.27	0.00	8.27	4.000	No	Yes	2.00
1913	19.13	7.17	100.00	3.29	0.59	1.22	8.27	0.00	8.27	4.000	No	Yes	2.00
1914	19.14	7.17	100.00	3.28	0.59	1.22	8.27	0.00	8.27	4.000	No	Yes	2.00
1915	19.15	7.17	100.00	3.28	0.59	1.22	8.27	0.00	8.27	4.000	No	Yes	2.00
1916	19.16	7.17	100.00	3.28	0.59	1.22	8.26	0.00	8.26	4.000	No	Yes	2.00
1917	19.17	7.17	100.00	3.28	0.59	1.22	8.26	0.00	8.26	4.000	No	Yes	2.00
1918	19.18	7.15	100.00	3.28	0.59	1.22	8.26	0.00	8.26	4.000	No	Yes	2.00
1919	19.19	7.10	100.00	3.28	0.59	1.22	8.18	0.00	8.18	4.000	No	Yes	2.00
1920	19.20	7.01	100.00	3.29	0.59	1.22	8.08	0.00	8.08	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1921	19.21	6.91	100.00	3.29	0.59	1.22	7.96	0.00	7.96	4.000	No	Yes	2.00
1922	19.22	6.81	100.00	3.30	0.59	1.22	7.84	0.00	7.84	4.000	No	Yes	2.00
1923	19.23	6.70	100.00	3.30	0.59	1.22	7.71	0.00	7.71	4.000	No	Yes	2.00
1924	19.24	6.60	100.00	3.31	0.59	1.22	7.59	0.00	7.59	4.000	No	Yes	2.00
1925	19.25	6.50	100.00	3.31	0.59	1.22	7.48	0.00	7.48	4.000	No	Yes	2.00
1926	19.26	6.42	100.00	3.32	0.59	1.22	7.39	0.00	7.39	4.000	No	Yes	2.00
1927	19.27	6.35	100.00	3.32	0.59	1.22	7.31	0.00	7.31	4.000	No	Yes	2.00
1928	19.28	6.27	100.00	3.33	0.59	1.22	7.23	0.00	7.23	4.000	No	Yes	2.00
1929	19.29	6.18	100.00	3.33	0.59	1.22	7.12	0.00	7.12	4.000	No	Yes	2.00
1930	19.30	6.08	100.00	3.34	0.59	1.22	7.00	0.00	7.00	4.000	No	Yes	2.00
1931	19.31	5.97	100.00	3.35	0.59	1.22	6.88	0.00	6.88	4.000	No	Yes	2.00
1932	19.32	5.87	100.00	3.36	0.60	1.22	6.75	0.00	6.75	4.000	No	Yes	2.00
1933	19.33	5.77	100.00	3.36	0.60	1.22	6.64	0.00	6.64	4.000	No	Yes	2.00
1934	19.34	5.68	100.00	3.37	0.60	1.22	6.53	0.00	6.53	4.000	No	Yes	2.00
1935	19.35	5.62	100.00	3.37	0.60	1.22	6.44	0.00	6.44	4.000	No	Yes	2.00
1936	19.36	5.58	100.00	3.38	0.60	1.22	6.42	0.00	6.42	4.000	No	Yes	2.00
1937	19.37	5.58	100.00	3.37	0.60	1.22	6.42	0.00	6.42	4.000	No	Yes	2.00
1938	19.38	5.58	100.00	3.37	0.60	1.22	6.42	0.00	6.42	4.000	No	Yes	2.00
1939	19.39	5.58	100.00	3.37	0.60	1.22	6.42	0.00	6.42	4.000	No	Yes	2.00
1940	19.40	5.58	100.00	3.37	0.60	1.22	6.42	0.00	6.42	4.000	No	Yes	2.00
1941	19.41	5.58	100.00	3.36	0.60	1.22	6.42	0.00	6.42	4.000	No	Yes	2.00
1942	19.42	5.58	100.00	3.36	0.60	1.22	6.41	0.00	6.41	4.000	No	Yes	2.00
1943	19.43	5.58	100.00	3.36	0.60	1.22	6.41	0.00	6.41	4.000	No	Yes	2.00
1944	19.44	5.58	100.00	3.36	0.60	1.22	6.41	0.00	6.41	4.000	No	Yes	2.00
1945	19.45	5.58	100.00	3.36	0.60	1.22	6.41	0.00	6.41	4.000	No	Yes	2.00
1946	19.46	5.58	100.00	3.35	0.60	1.22	6.41	0.00	6.41	4.000	No	Yes	2.00
1947	19.47	5.58	100.00	3.35	0.60	1.22	6.41	0.00	6.41	4.000	No	Yes	2.00
1948	19.48	5.58	100.00	3.35	0.60	1.22	6.41	0.00	6.41	4.000	No	Yes	2.00
1949	19.49	5.58	100.00	3.35	0.60	1.22	6.41	0.00	6.41	4.000	No	Yes	2.00
1950	19.50	5.58	100.00	3.34	0.60	1.22	6.41	0.00	6.41	4.000	No	Yes	2.00
1951	19.51	5.58	100.00	3.34	0.60	1.22	6.41	0.00	6.41	4.000	No	Yes	2.00
1952	19.52	5.58	100.00	3.34	0.60	1.22	6.40	0.00	6.40	4.000	No	Yes	2.00
1953	19.53	5.58	100.00	3.34	0.60	1.22	6.40	0.00	6.40	4.000	No	Yes	2.00
1954	19.54	5.58	100.00	3.33	0.60	1.22	6.40	0.00	6.40	4.000	No	Yes	2.00
1955	19.55	5.58	100.00	3.33	0.60	1.21	6.40	0.00	6.40	4.000	No	Yes	2.00
1956	19.56	5.58	100.00	3.33	0.60	1.21	6.40	0.00	6.40	4.000	No	Yes	2.00
1957	19.57	5.58	100.00	3.33	0.60	1.21	6.40	0.00	6.40	4.000	No	Yes	2.00
1958	19.58	5.58	100.00	3.33	0.60	1.21	6.40	0.00	6.40	4.000	No	Yes	2.00
1959	19.59	5.58	100.00	3.32	0.60	1.21	6.40	0.00	6.40	4.000	No	Yes	2.00
1960	19.60	5.58	100.00	3.32	0.60	1.21	6.40	0.00	6.40	4.000	No	Yes	2.00
1961	19.61	5.58	100.00	3.32	0.60	1.21	6.39	0.00	6.39	4.000	No	Yes	2.00
1962	19.62	5.57	100.00	3.32	0.60	1.21	6.39	0.00	6.39	4.000	No	Yes	2.00
1963	19.63	5.56	100.00	3.32	0.60	1.21	6.37	0.00	6.37	4.000	No	Yes	2.00
1964	19.64	5.55	100.00	3.32	0.60	1.21	6.36	0.00	6.36	4.000	No	Yes	2.00
1965	19.65	5.54	100.00	3.32	0.60	1.21	6.34	0.00	6.34	4.000	No	Yes	2.00
1966	19.66	5.52	100.00	3.33	0.60	1.21	6.33	0.00	6.33	4.000	No	Yes	2.00
1967	19.67	5.51	100.00	3.33	0.60	1.21	6.31	0.00	6.31	4.000	No	Yes	2.00
1968	19.68	5.50	100.00	3.33	0.60	1.21	6.30	0.00	6.30	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1969	19.69	5.49	100.00	3.33	0.60	1.21	6.28	0.00	6.28	4.000	No	Yes	2.00
1970	19.70	5.45	100.00	3.33	0.60	1.21	6.27	0.00	6.27	4.000	No	Yes	2.00
1971	19.71	5.40	100.00	3.34	0.60	1.21	6.19	0.00	6.19	4.000	No	Yes	2.00
1972	19.72	5.31	100.00	3.35	0.60	1.21	6.09	0.00	6.09	4.000	No	Yes	2.00
1973	19.73	5.21	100.00	3.36	0.60	1.21	5.97	0.00	5.97	4.000	No	Yes	2.00
1974	19.74	5.11	100.00	3.37	0.60	1.21	5.85	0.00	5.85	4.000	No	Yes	2.00
1975	19.75	5.00	100.00	3.39	0.60	1.21	5.72	0.00	5.72	4.000	No	Yes	2.00
1976	19.76	4.90	100.00	3.40	0.60	1.21	5.61	0.00	5.61	4.000	No	Yes	2.00
1977	19.77	4.81	100.00	3.41	0.60	1.21	5.50	0.00	5.50	4.000	No	Yes	2.00
1978	19.78	4.78	100.00	3.42	0.60	1.21	5.40	0.00	5.40	4.000	No	Yes	2.00
1979	19.79	4.93	100.00	3.40	0.60	1.21	5.52	0.00	5.52	4.000	No	Yes	2.00
1980	19.80	5.29	100.00	3.37	0.60	1.21	6.01	0.00	6.01	4.000	No	Yes	2.00
1981	19.81	5.80	100.00	3.33	0.60	1.21	6.60	0.00	6.60	4.000	No	Yes	2.00
1982	19.82	6.37	100.00	3.29	0.59	1.21	7.26	0.00	7.26	4.000	No	Yes	2.00
1983	19.83	6.97	100.00	3.25	0.59	1.21	7.95	0.00	7.95	4.000	No	Yes	2.00
1984	19.84	7.56	100.00	3.22	0.59	1.21	8.63	0.00	8.63	4.000	No	Yes	2.00
1985	19.85	8.13	100.00	3.19	0.59	1.20	9.27	0.00	9.27	4.000	No	Yes	2.00
1986	19.86	8.63	100.00	3.17	0.58	1.20	9.84	0.00	9.84	4.000	No	Yes	2.00
1987	19.87	9.07	100.00	3.16	0.58	1.20	10.31	0.00	10.31	4.000	No	Yes	2.00
1988	19.88	9.53	100.00	3.14	0.58	1.20	10.77	0.00	10.77	4.000	No	Yes	2.00
1989	19.89	10.06	100.00	3.12	0.58	1.20	11.37	0.00	11.37	4.000	No	Yes	2.00
1990	19.90	10.68	100.00	3.10	0.57	1.20	12.07	0.00	12.07	4.000	No	Yes	2.00
1991	19.91	11.35	100.00	3.08	0.57	1.20	12.84	0.00	12.84	4.000	No	Yes	2.00
1992	19.92	12.04	100.00	3.06	0.57	1.20	13.62	0.00	13.62	4.000	No	Yes	2.00
1993	19.93	12.72	100.00	3.04	0.57	1.20	14.38	0.00	14.38	4.000	No	Yes	2.00
1994	19.94	13.36	100.00	3.02	0.56	1.19	15.09	0.00	15.09	4.000	No	Yes	2.00
1995	19.95	13.88	100.00	3.01	0.56	1.19	15.71	0.00	15.71	4.000	No	Yes	2.00
1996	19.96	14.03	100.00	3.01	0.56	1.19	16.12	0.00	16.12	4.000	No	Yes	2.00
1997	19.97	13.81	100.00	3.01	0.56	1.19	15.60	0.00	15.60	4.000	No	Yes	2.00
1998	19.98	13.25	100.00	3.03	0.56	1.19	14.96	0.00	14.96	4.000	No	Yes	2.00
1999	19.99	12.61	100.00	3.04	0.57	1.19	14.24	0.00	14.24	4.000	No	Yes	2.00
2000	20.00	11.92	100.00	3.06	0.57	1.20	13.46	0.00	13.46	4.000	No	Yes	2.00
2001	20.01	11.23	100.00	3.08	0.57	1.20	12.68	0.00	12.68	4.000	No	Yes	2.00
2002	20.02	10.56	100.00	3.11	0.57	1.20	11.92	0.00	11.92	4.000	No	Yes	2.00
2003	20.03	9.96	100.00	3.13	0.58	1.20	11.23	0.00	11.23	4.000	No	Yes	2.00
2004	20.04	9.45	100.00	3.15	0.58	1.20	10.64	0.00	10.64	4.000	No	Yes	2.00
2005	20.05	9.01	100.00	3.17	0.58	1.20	10.21	0.00	10.21	4.000	No	Yes	2.00
2006	20.06	8.59	100.00	3.19	0.58	1.20	9.76	0.00	9.76	4.000	No	Yes	2.00
2007	20.07	8.11	100.00	3.21	0.59	1.20	9.21	0.00	9.21	4.000	No	Yes	2.00
2008	20.08	7.58	100.00	3.24	0.59	1.20	8.60	0.00	8.60	4.000	No	Yes	2.00
2009	20.09	7.02	100.00	3.27	0.59	1.20	7.96	0.00	7.96	4.000	No	Yes	2.00
2010	20.10	6.46	100.00	3.31	0.59	1.20	7.32	0.00	7.32	4.000	No	Yes	2.00
2011	20.11	5.94	100.00	3.35	0.60	1.20	6.72	0.00	6.72	4.000	No	Yes	2.00
2012	20.12	5.47	100.00	3.39	0.60	1.20	6.18	0.00	6.18	4.000	No	Yes	2.00
2013	20.13	5.15	100.00	3.42	0.60	1.20	5.75	0.00	5.75	4.000	No	Yes	2.00
2014	20.14	4.99	100.00	3.44	0.60	1.20	5.65	0.00	5.65	4.000	No	Yes	2.00
2015	20.15	4.95	100.00	3.45	0.60	1.20	5.62	0.00	5.62	4.000	No	Yes	2.00
2016	20.16	4.92	100.00	3.45	0.60	1.20	5.60	0.00	5.60	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
2017	20.17	4.90	100.00	3.46	0.60	1.20	5.56	0.00	5.56	4.000	No	Yes	2.00
2018	20.18	4.87	100.00	3.46	0.60	1.20	5.53	0.00	5.53	4.000	No	Yes	2.00
2019	20.19	4.84	100.00	3.47	0.60	1.20	5.50	0.00	5.50	4.000	No	Yes	2.00
2020	20.20	4.82	100.00	3.48	0.60	1.20	5.47	0.00	5.47	4.000	No	Yes	2.00
2021	20.21	4.80	100.00	3.48	0.60	1.20	5.45	0.00	5.45	4.000	No	Yes	2.00
2022	20.22	4.78	100.00	3.49	0.60	1.20	5.43	0.00	5.43	4.000	No	Yes	2.00
2023	20.23	4.76	100.00	3.49	0.60	1.20	5.41	0.00	5.41	4.000	No	Yes	2.00
2024	20.24	4.74	100.00	3.50	0.60	1.20	5.38	0.00	5.38	4.000	No	Yes	2.00
2025	20.25	4.71	100.00	3.51	0.60	1.20	5.35	0.00	5.35	4.000	No	Yes	2.00
2026	20.26	4.69	100.00	3.51	0.60	1.20	5.32	0.00	5.32	4.000	No	Yes	2.00
2027	20.27	4.66	100.00	3.52	0.60	1.20	5.29	0.00	5.29	4.000	No	Yes	2.00
2028	20.28	4.64	100.00	3.53	0.60	1.20	5.26	0.00	5.26	4.000	No	Yes	2.00
2029	20.29	4.61	100.00	3.53	0.60	1.20	5.23	0.00	5.23	4.000	No	Yes	2.00
2030	20.30	4.62	100.00	3.54	0.60	1.20	5.21	0.00	5.21	4.000	No	Yes	2.00
2031	20.31	4.69	100.00	3.53	0.60	1.20	5.27	0.00	5.27	4.000	No	Yes	2.00
2032	20.32	4.83	100.00	3.52	0.60	1.20	5.47	0.00	5.47	4.000	No	Yes	2.00
2033	20.33	5.04	100.00	3.50	0.60	1.20	5.70	0.00	5.70	4.000	No	Yes	2.00
2034	20.34	5.27	100.00	3.48	0.60	1.20	5.96	0.00	5.96	4.000	No	Yes	2.00
2035	20.35	5.51	100.00	3.46	0.60	1.20	6.24	0.00	6.24	4.000	No	Yes	2.00
2036	20.36	5.75	100.00	3.44	0.60	1.20	6.51	0.00	6.51	4.000	No	Yes	2.00
2037	20.37	5.97	100.00	3.43	0.60	1.20	6.76	0.00	6.76	4.000	No	Yes	2.00
2038	20.38	6.17	100.00	3.41	0.59	1.20	6.99	0.00	6.99	4.000	No	Yes	2.00
2039	20.39	6.36	100.00	3.40	0.59	1.20	7.17	0.00	7.17	4.000	No	Yes	2.00
2040	20.40	6.57	100.00	3.39	0.59	1.20	7.40	0.00	7.40	4.000	No	Yes	2.00
2041	20.41	6.84	100.00	3.37	0.59	1.20	7.70	0.00	7.70	4.000	No	Yes	2.00
2042	20.42	7.15	100.00	3.35	0.59	1.19	8.05	0.00	8.05	4.000	No	Yes	2.00
2043	20.43	7.49	100.00	3.33	0.59	1.19	8.43	0.00	8.43	4.000	No	Yes	2.00
2044	20.44	7.83	100.00	3.31	0.59	1.19	8.83	0.00	8.83	4.000	No	Yes	2.00
2045	20.45	8.17	100.00	3.29	0.59	1.19	9.21	0.00	9.21	4.000	No	Yes	2.00
2046	20.46	8.49	100.00	3.28	0.58	1.19	9.56	0.00	9.56	4.000	No	Yes	2.00
2047	20.47	8.76	100.00	3.26	0.58	1.19	9.87	0.00	9.87	4.000	No	Yes	2.00
2048	20.48	9.01	100.00	3.25	0.58	1.19	10.11	0.00	10.11	4.000	No	Yes	2.00
2049	20.49	9.29	100.00	3.24	0.58	1.19	10.41	0.00	10.41	4.000	No	Yes	2.00
2050	20.50	9.62	100.00	3.22	0.58	1.19	10.78	0.00	10.78	4.000	No	Yes	2.00
2051	20.51	9.99	100.00	3.21	0.58	1.19	11.20	0.00	11.20	4.000	No	Yes	2.00
2052	20.52	10.38	100.00	3.19	0.58	1.19	11.64	0.00	11.64	4.000	No	Yes	2.00
2053	20.53	10.78	100.00	3.17	0.57	1.19	12.09	0.00	12.09	4.000	No	Yes	2.00
2054	20.54	11.17	100.00	3.15	0.57	1.19	12.52	0.00	12.52	4.000	No	Yes	2.00
2055	20.55	11.51	100.00	3.14	0.57	1.19	12.90	0.00	12.90	4.000	No	Yes	2.00
2056	20.56	11.80	100.00	3.13	0.57	1.18	13.23	0.00	13.23	4.000	No	Yes	2.00
2057	20.57	12.02	100.00	3.12	0.57	1.18	13.44	0.00	13.44	4.000	No	Yes	2.00
2058	20.58	12.21	100.00	3.11	0.57	1.18	13.63	0.00	13.63	4.000	No	Yes	2.00
2059	20.59	12.42	100.00	3.10	0.57	1.18	13.86	0.00	13.86	4.000	No	Yes	2.00
2060	20.60	12.65	100.00	3.09	0.57	1.18	14.12	0.00	14.12	4.000	No	Yes	2.00
2061	20.61	12.89	100.00	3.08	0.57	1.18	14.38	0.00	14.38	4.000	No	Yes	2.00
2062	20.62	13.13	100.00	3.07	0.56	1.18	14.65	0.00	14.65	4.000	No	Yes	2.00
2063	20.63	13.35	100.00	3.06	0.56	1.18	14.89	0.00	14.89	4.000	No	Yes	2.00
2064	20.64	13.55	100.00	3.05	0.56	1.18	15.11	0.00	15.11	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
2065	20.65	13.72	100.00	3.05	0.56	1.18	15.29	0.00	15.29	4.000	No	Yes	2.00
2066	20.66	13.89	100.00	3.04	0.56	1.18	15.45	0.00	15.45	4.000	No	Yes	2.00
2067	20.67	14.07	100.00	3.03	0.56	1.18	15.65	0.00	15.65	4.000	No	Yes	2.00
2068	20.68	14.29	100.00	3.02	0.56	1.18	15.89	0.00	15.89	4.000	No	Yes	2.00
2069	20.69	14.52	100.00	3.01	0.56	1.18	16.15	0.00	16.15	4.000	No	Yes	2.00
2070	20.70	14.76	100.00	3.00	0.56	1.18	16.41	0.00	16.41	4.000	No	Yes	2.00
2071	20.71	15.00	100.00	2.99	0.56	1.18	16.67	0.00	16.67	4.000	No	Yes	2.00
2072	20.72	15.21	100.00	2.98	0.56	1.18	16.91	0.00	16.91	4.000	No	Yes	2.00
2073	20.73	15.39	100.00	2.97	0.56	1.18	17.11	0.00	17.11	4.000	No	Yes	2.00
2074	20.74	15.46	100.00	2.97	0.56	1.18	17.24	0.00	17.24	4.000	No	Yes	2.00
2075	20.75	15.44	100.00	2.96	0.56	1.18	17.15	0.00	17.15	4.000	No	Yes	2.00
2076	20.76	15.34	100.00	2.96	0.56	1.18	17.03	0.00	17.03	4.000	No	Yes	2.00
2077	20.77	15.23	100.00	2.96	0.56	1.18	16.91	0.00	16.91	4.000	No	Yes	2.00
2078	20.78	15.11	100.00	2.96	0.56	1.18	16.77	0.00	16.77	4.000	No	Yes	2.00
2079	20.79	14.99	100.00	2.96	0.56	1.18	16.64	0.00	16.64	4.000	No	Yes	2.00
2080	20.80	14.88	100.00	2.96	0.56	1.17	16.51	0.00	16.51	4.000	No	Yes	2.00
2081	20.81	14.77	100.00	2.96	0.56	1.17	16.39	0.00	16.39	4.000	No	Yes	2.00
2082	20.82	14.66	100.00	2.97	0.56	1.17	16.29	0.00	16.29	4.000	No	Yes	2.00
2083	20.83	14.48	100.00	2.97	0.56	1.17	16.11	0.00	16.11	4.000	No	Yes	2.00
2084	20.84	14.21	100.00	2.98	0.56	1.17	15.79	0.00	15.79	4.000	No	Yes	2.00
2085	20.85	13.86	100.00	2.99	0.56	1.18	15.40	0.00	15.40	4.000	No	Yes	2.00
2086	20.86	13.48	100.00	3.00	0.56	1.18	14.97	0.00	14.97	4.000	No	Yes	2.00
2087	20.87	13.08	100.00	3.01	0.57	1.18	14.53	0.00	14.53	4.000	No	Yes	2.00
2088	20.88	12.69	100.00	3.03	0.57	1.18	14.08	0.00	14.08	4.000	No	Yes	2.00
2089	20.89	12.31	100.00	3.04	0.57	1.18	13.67	0.00	13.67	4.000	No	Yes	2.00
2090	20.90	11.98	100.00	3.05	0.57	1.18	13.30	0.00	13.30	4.000	No	Yes	2.00
2091	20.91	11.73	100.00	3.06	0.57	1.18	13.00	0.00	13.00	4.000	No	Yes	2.00
2092	20.92	11.52	100.00	3.07	0.57	1.18	12.81	0.00	12.81	4.000	No	Yes	2.00
2093	20.93	11.33	100.00	3.08	0.57	1.18	12.60	0.00	12.60	4.000	No	Yes	2.00
2094	20.94	11.11	100.00	3.10	0.57	1.18	12.36	0.00	12.36	4.000	No	Yes	2.00
2095	20.95	10.88	100.00	3.11	0.57	1.18	12.10	0.00	12.10	4.000	No	Yes	2.00
2096	20.96	10.64	100.00	3.12	0.58	1.18	11.82	0.00	11.82	4.000	No	Yes	2.00
2097	20.97	10.40	100.00	3.14	0.58	1.18	11.56	0.00	11.56	4.000	No	Yes	2.00
2098	20.98	10.19	100.00	3.15	0.58	1.18	11.32	0.00	11.32	4.000	No	Yes	2.00
2099	20.99	10.00	100.00	3.16	0.58	1.18	11.11	0.00	11.11	4.000	No	Yes	2.00
2100	21.00	9.83	100.00	3.17	0.58	1.18	10.94	0.00	10.94	4.000	No	Yes	2.00
2101	21.01	9.66	100.00	3.18	0.58	1.18	10.76	0.00	10.76	4.000	No	Yes	2.00
2102	21.02	9.46	100.00	3.19	0.58	1.18	10.54	0.00	10.54	4.000	No	Yes	2.00
2103	21.03	9.24	100.00	3.20	0.58	1.18	10.28	0.00	10.28	4.000	No	Yes	2.00
2104	21.04	9.00	100.00	3.22	0.58	1.18	10.02	0.00	10.02	4.000	No	Yes	2.00
2105	21.05	8.76	100.00	3.23	0.58	1.18	9.75	0.00	9.75	4.000	No	Yes	2.00
2106	21.06	8.53	100.00	3.25	0.58	1.18	9.49	0.00	9.49	4.000	No	Yes	2.00
2107	21.07	8.33	100.00	3.26	0.59	1.18	9.25	0.00	9.25	4.000	No	Yes	2.00
2108	21.08	8.16	100.00	3.27	0.59	1.18	9.06	0.00	9.06	4.000	No	Yes	2.00
2109	21.09	8.04	100.00	3.28	0.59	1.18	8.94	0.00	8.94	4.000	No	Yes	2.00
2110	21.10	7.94	100.00	3.29	0.59	1.18	8.84	0.00	8.84	4.000	No	Yes	2.00
2111	21.11	7.83	100.00	3.29	0.59	1.18	8.72	0.00	8.72	4.000	No	Yes	2.00
2112	21.12	7.72	100.00	3.30	0.59	1.18	8.59	0.00	8.59	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
2113	21.13	7.60	100.00	3.31	0.59	1.18	8.45	0.00	8.45	4.000	No	Yes	2.00
2114	21.14	7.48	100.00	3.32	0.59	1.18	8.32	0.00	8.32	4.000	No	Yes	2.00
2115	21.15	7.37	100.00	3.32	0.59	1.18	8.19	0.00	8.19	4.000	No	Yes	2.00
2116	21.16	7.27	100.00	3.33	0.59	1.18	8.08	0.00	8.08	4.000	No	Yes	2.00
2117	21.17	7.27	100.00	3.33	0.59	1.18	7.99	0.00	7.99	4.000	No	Yes	2.00
2118	21.18	7.38	100.00	3.32	0.59	1.18	8.17	0.00	8.17	4.000	No	Yes	2.00
2119	21.19	7.62	100.00	3.31	0.59	1.18	8.45	0.00	8.45	4.000	No	Yes	2.00
2120	21.20	7.91	100.00	3.29	0.59	1.18	8.77	0.00	8.77	4.000	No	Yes	2.00
2121	21.21	8.22	100.00	3.27	0.59	1.18	9.12	0.00	9.12	4.000	No	Yes	2.00
2122	21.22	8.54	100.00	3.25	0.58	1.18	9.48	0.00	9.48	4.000	No	Yes	2.00
2123	21.23	8.85	100.00	3.23	0.58	1.17	9.82	0.00	9.82	4.000	No	Yes	2.00
2124	21.24	9.14	100.00	3.21	0.58	1.17	10.14	0.00	10.14	4.000	No	Yes	2.00
2125	21.25	9.40	100.00	3.20	0.58	1.17	10.42	0.00	10.42	4.000	No	Yes	2.00
2126	21.26	9.72	100.00	3.18	0.58	1.17	10.68	0.00	10.68	4.000	No	Yes	2.00
2127	21.27	10.15	100.00	3.16	0.58	1.17	11.19	0.00	11.19	4.000	No	Yes	2.00
2128	21.28	10.72	100.00	3.14	0.58	1.17	11.82	0.00	11.82	4.000	No	Yes	2.00
2129	21.29	11.36	100.00	3.11	0.57	1.17	12.53	0.00	12.53	4.000	No	Yes	2.00
2130	21.30	12.04	100.00	3.08	0.57	1.17	13.28	0.00	13.28	4.000	No	Yes	2.00
2131	21.31	12.72	100.00	3.05	0.57	1.17	14.04	0.00	14.04	4.000	No	Yes	2.00
2132	21.32	13.38	100.00	3.03	0.56	1.17	14.76	0.00	14.76	4.000	No	Yes	2.00
2133	21.33	13.97	100.00	3.01	0.56	1.17	15.41	0.00	15.41	4.000	No	Yes	2.00
2134	21.34	14.44	100.00	2.99	0.56	1.16	15.95	0.00	15.95	4.000	No	Yes	2.00
2135	21.35	14.81	100.00	2.98	0.56	1.16	16.29	0.00	16.29	4.000	No	Yes	2.00
2136	21.36	15.13	100.00	2.96	0.56	1.16	16.61	0.00	16.61	4.000	No	Yes	2.00
2137	21.37	15.48	99.07	2.95	0.56	1.16	16.99	0.00	16.99	4.000	No	Yes	2.00
2138	21.38	15.87	97.89	2.94	0.56	1.16	17.41	0.00	17.41	4.000	No	Yes	2.00
2139	21.39	16.27	96.68	2.92	0.55	1.16	17.85	0.00	17.85	4.000	No	Yes	2.00
2140	21.40	16.66	95.53	2.91	0.55	1.16	18.28	0.00	18.28	4.000	No	Yes	2.00
2141	21.41	17.03	94.46	2.89	0.55	1.16	18.69	0.00	18.69	4.000	No	Yes	2.00
2142	21.42	17.36	93.53	2.88	0.55	1.16	19.04	0.00	19.04	4.000	No	Yes	2.00
2143	21.43	17.66	92.73	2.87	0.55	1.16	19.33	0.00	19.33	4.000	No	Yes	2.00
2144	21.44	17.99	91.97	2.86	0.55	1.16	19.67	0.00	19.67	4.000	No	Yes	2.00
2145	21.45	18.39	91.14	2.85	0.55	1.16	20.10	0.00	20.10	4.000	No	Yes	2.00
2146	21.46	18.86	90.20	2.84	0.55	1.16	20.61	0.00	20.61	4.000	No	Yes	2.00
2147	21.47	19.36	89.21	2.83	0.54	1.16	21.16	0.00	21.16	4.000	No	Yes	2.00
2148	21.48	19.88	88.21	2.82	0.54	1.16	21.72	0.00	21.72	4.000	No	Yes	2.00
2149	21.49	20.38	87.26	2.80	0.54	1.16	22.26	0.00	22.26	4.000	No	Yes	2.00
2150	21.50	20.84	86.40	2.79	0.54	1.16	22.76	0.00	22.76	4.000	No	Yes	2.00
2151	21.51	21.21	85.71	2.78	0.54	1.15	23.19	0.00	23.19	4.000	No	Yes	2.00
2152	21.52	21.44	85.28	2.78	0.54	1.15	23.45	0.00	23.45	4.000	No	Yes	2.00
2153	21.53	21.53	85.08	2.78	0.54	1.15	23.46	0.00	23.46	4.000	No	Yes	2.00
2154	21.54	21.54	85.00	2.77	0.54	1.15	23.47	0.00	23.47	4.000	No	Yes	2.00
2155	21.55	21.56	84.91	2.77	0.54	1.15	23.49	0.00	23.49	4.000	No	Yes	2.00
2156	21.56	21.57	84.81	2.77	0.54	1.15	23.50	0.00	23.50	4.000	No	Yes	2.00
2157	21.57	21.59	84.71	2.77	0.54	1.15	23.51	0.00	23.51	4.000	No	Yes	2.00
2158	21.58	21.60	84.61	2.77	0.54	1.15	23.52	0.00	23.52	4.000	No	Yes	2.00
2159	21.59	21.62	84.52	2.77	0.54	1.15	23.54	0.00	23.54	4.000	No	Yes	2.00
2160	21.60	21.54	84.59	2.77	0.54	1.15	23.54	0.00	23.54	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
2161	21.61	21.27	84.98	2.77	0.54	1.15	23.27	0.00	23.27	4.000	No	Yes	2.00
2162	21.62	20.78	85.75	2.78	0.54	1.15	22.67	0.00	22.67	4.000	No	Yes	2.00
2163	21.63	20.13	86.80	2.80	0.54	1.15	21.95	0.00	21.95	4.000	No	Yes	2.00
2164	21.64	19.41	87.99	2.81	0.54	1.15	21.17	0.00	21.17	4.000	No	Yes	2.00
2165	21.65	18.67	89.29	2.83	0.55	1.15	20.35	0.00	20.35	4.000	No	Yes	2.00
2166	21.66	17.93	90.62	2.85	0.55	1.15	19.54	0.00	19.54	4.000	No	Yes	2.00
2167	21.67	17.24	91.91	2.86	0.55	1.16	18.78	0.00	18.78	4.000	No	Yes	2.00
2168	21.68	16.63	93.10	2.88	0.55	1.16	18.11	0.00	18.11	4.000	No	Yes	2.00
2169	21.69	16.15	94.12	2.89	0.56	1.16	17.57	0.00	17.57	4.000	No	Yes	2.00
2170	21.70	15.73	95.10	2.90	0.56	1.16	17.21	0.00	17.21	4.000	No	Yes	2.00
2171	21.71	15.33	96.14	2.91	0.56	1.16	16.76	0.00	16.76	4.000	No	Yes	2.00
2172	21.72	14.86	97.40	2.93	0.56	1.16	16.25	0.00	16.25	4.000	No	Yes	2.00
2173	21.73	14.36	98.81	2.95	0.56	1.16	15.70	0.00	15.70	4.000	No	Yes	2.00
2174	21.74	13.85	100.00	2.97	0.56	1.16	15.13	0.00	15.13	4.000	No	Yes	2.00
2175	21.75	13.35	100.00	2.98	0.56	1.16	14.58	0.00	14.58	4.000	No	Yes	2.00
2176	21.76	12.89	100.00	3.00	0.57	1.16	14.08	0.00	14.08	4.000	No	Yes	2.00
2177	21.77	12.50	100.00	3.02	0.57	1.16	13.64	0.00	13.64	4.000	No	Yes	2.00
2178	21.78	12.16	100.00	3.03	0.57	1.16	13.31	0.00	13.31	4.000	No	Yes	2.00
2179	21.79	11.83	100.00	3.05	0.57	1.16	12.97	0.00	12.97	4.000	No	Yes	2.00
2180	21.80	11.45	100.00	3.06	0.57	1.16	12.55	0.00	12.55	4.000	No	Yes	2.00
2181	21.81	11.03	100.00	3.08	0.57	1.16	12.08	0.00	12.08	4.000	No	Yes	2.00
2182	21.82	10.58	100.00	3.10	0.58	1.16	11.58	0.00	11.58	4.000	No	Yes	2.00
2183	21.83	10.12	100.00	3.12	0.58	1.16	11.08	0.00	11.08	4.000	No	Yes	2.00
2184	21.84	9.69	100.00	3.15	0.58	1.16	10.61	0.00	10.61	4.000	No	Yes	2.00
2185	21.85	9.31	100.00	3.17	0.58	1.16	10.18	0.00	10.18	4.000	No	Yes	2.00
2186	21.86	8.99	100.00	3.18	0.58	1.16	9.82	0.00	9.82	4.000	No	Yes	2.00
2187	21.87	8.72	100.00	3.20	0.58	1.16	9.57	0.00	9.57	4.000	No	Yes	2.00
2188	21.88	8.46	100.00	3.22	0.59	1.16	9.30	0.00	9.30	4.000	No	Yes	2.00
2189	21.89	8.17	100.00	3.23	0.59	1.16	8.97	0.00	8.97	4.000	No	Yes	2.00
2190	21.90	7.86	100.00	3.25	0.59	1.16	8.62	0.00	8.62	4.000	No	Yes	2.00
2191	21.91	7.53	100.00	3.28	0.59	1.16	8.25	0.00	8.25	4.000	No	Yes	2.00
2192	21.92	7.20	100.00	3.30	0.59	1.16	7.89	0.00	7.89	4.000	No	Yes	2.00
2193	21.93	6.89	100.00	3.32	0.59	1.16	7.55	0.00	7.55	4.000	No	Yes	2.00
2194	21.94	6.63	100.00	3.34	0.59	1.16	7.25	0.00	7.25	4.000	No	Yes	2.00
2195	21.95	6.44	100.00	3.36	0.59	1.16	7.01	0.00	7.01	4.000	No	Yes	2.00
2196	21.96	6.31	100.00	3.37	0.59	1.16	6.93	0.00	6.93	4.000	No	Yes	2.00
2197	21.97	6.22	100.00	3.37	0.59	1.16	6.83	0.00	6.83	4.000	No	Yes	2.00
2198	21.98	6.12	100.00	3.38	0.60	1.16	6.72	0.00	6.72	4.000	No	Yes	2.00
2199	21.99	6.02	100.00	3.39	0.60	1.16	6.61	0.00	6.61	4.000	No	Yes	2.00
2200	22.00	5.91	100.00	3.40	0.60	1.16	6.49	0.00	6.49	4.000	No	Yes	2.00
2201	22.01	5.81	100.00	3.40	0.60	1.16	6.37	0.00	6.37	4.000	No	Yes	2.00
2202	22.02	5.71	100.00	3.41	0.60	1.16	6.27	0.00	6.27	4.000	No	Yes	2.00
2203	22.03	5.64	100.00	3.42	0.60	1.16	6.17	0.00	6.17	4.000	No	Yes	2.00
2204	22.04	5.59	100.00	3.42	0.60	1.16	6.12	0.00	6.12	4.000	No	Yes	2.00
2205	22.05	5.58	100.00	3.42	0.60	1.16	6.12	0.00	6.12	4.000	No	Yes	2.00
2206	22.06	5.58	100.00	3.42	0.60	1.16	6.12	0.00	6.12	4.000	No	Yes	2.00
2207	22.07	5.58	100.00	3.41	0.60	1.16	6.12	0.00	6.12	4.000	No	Yes	2.00
2208	22.08	5.58	100.00	3.41	0.60	1.16	6.12	0.00	6.12	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
2209	22.09	5.58	100.00	3.41	0.60	1.16	6.12	0.00	6.12	4.000	No	Yes	2.00
2210	22.10	5.58	100.00	3.41	0.60	1.16	6.11	0.00	6.11	4.000	No	Yes	2.00
2211	22.11	5.58	100.00	3.40	0.60	1.16	6.11	0.00	6.11	4.000	No	Yes	2.00
2212	22.12	5.58	100.00	3.40	0.60	1.16	6.11	0.00	6.11	4.000	No	Yes	2.00
2213	22.13	5.58	100.00	3.40	0.60	1.16	6.11	0.00	6.11	4.000	No	Yes	2.00
2214	22.14	5.58	100.00	3.40	0.60	1.16	6.11	0.00	6.11	4.000	No	Yes	2.00
2215	22.15	5.58	100.00	3.39	0.60	1.16	6.11	0.00	6.11	4.000	No	Yes	2.00
2216	22.16	5.58	100.00	3.39	0.60	1.16	6.11	0.00	6.11	4.000	No	Yes	2.00
2217	22.17	5.58	100.00	3.39	0.60	1.16	6.11	0.00	6.11	4.000	No	Yes	2.00
2218	22.18	5.58	100.00	3.39	0.60	1.16	6.11	0.00	6.11	4.000	No	Yes	2.00
2219	22.19	5.58	100.00	3.38	0.60	1.16	6.11	0.00	6.11	4.000	No	Yes	2.00
2220	22.20	5.58	100.00	3.38	0.60	1.16	6.11	0.00	6.11	4.000	No	Yes	2.00
2221	22.21	5.57	100.00	3.38	0.60	1.16	6.10	0.00	6.10	4.000	No	Yes	2.00
2222	22.22	5.54	100.00	3.38	0.60	1.16	6.07	0.00	6.07	4.000	No	Yes	2.00
2223	22.23	5.50	100.00	3.39	0.60	1.16	6.02	0.00	6.02	4.000	No	Yes	2.00
2224	22.24	5.45	100.00	3.39	0.60	1.16	5.97	0.00	5.97	4.000	No	Yes	2.00
2225	22.25	5.40	100.00	3.39	0.60	1.16	5.91	0.00	5.91	4.000	No	Yes	2.00
2226	22.26	5.35	100.00	3.40	0.60	1.16	5.85	0.00	5.85	4.000	No	Yes	2.00
2227	22.27	5.29	100.00	3.40	0.60	1.16	5.79	0.00	5.79	4.000	No	Yes	2.00
2228	22.28	5.25	100.00	3.41	0.60	1.16	5.74	0.00	5.74	4.000	No	Yes	2.00
2229	22.29	5.21	100.00	3.41	0.60	1.16	5.69	0.00	5.69	4.000	No	Yes	2.00
2230	22.30	5.22	100.00	3.41	0.60	1.16	5.68	0.00	5.68	4.000	No	Yes	2.00
2231	22.31	5.28	100.00	3.40	0.60	1.16	5.76	0.00	5.76	4.000	No	Yes	2.00
2232	22.32	5.37	100.00	3.39	0.60	1.16	5.86	0.00	5.86	4.000	No	Yes	2.00
2233	22.33	5.47	100.00	3.38	0.60	1.16	5.97	0.00	5.97	4.000	No	Yes	2.00
2234	22.34	5.57	100.00	3.37	0.60	1.16	6.09	0.00	6.09	4.000	No	Yes	2.00
2235	22.35	5.68	100.00	3.36	0.60	1.16	6.21	0.00	6.21	4.000	No	Yes	2.00
2236	22.36	5.78	100.00	3.35	0.60	1.16	6.32	0.00	6.32	4.000	No	Yes	2.00
2237	22.37	5.87	100.00	3.34	0.60	1.16	6.42	0.00	6.42	4.000	No	Yes	2.00
2238	22.38	5.94	100.00	3.34	0.60	1.16	6.50	0.00	6.50	4.000	No	Yes	2.00
2239	22.39	6.00	100.00	3.33	0.60	1.16	6.54	0.00	6.54	4.000	No	Yes	2.00
2240	22.40	6.04	100.00	3.33	0.60	1.15	6.59	0.00	6.59	4.000	No	Yes	2.00
2241	22.41	6.09	100.00	3.32	0.60	1.15	6.64	0.00	6.64	4.000	No	Yes	2.00
2242	22.42	6.14	100.00	3.32	0.60	1.15	6.69	0.00	6.69	4.000	No	Yes	2.00
2243	22.43	6.19	100.00	3.31	0.60	1.15	6.75	0.00	6.75	4.000	No	Yes	2.00
2244	22.44	6.24	100.00	3.31	0.60	1.15	6.81	0.00	6.81	4.000	No	Yes	2.00
2245	22.45	6.29	100.00	3.31	0.59	1.15	6.86	0.00	6.86	4.000	No	Yes	2.00
2246	22.46	6.34	100.00	3.30	0.59	1.15	6.91	0.00	6.91	4.000	No	Yes	2.00
2247	22.47	6.38	100.00	3.30	0.59	1.15	6.94	0.00	6.94	4.000	No	Yes	2.00
2248	22.48	6.43	100.00	3.30	0.59	1.15	7.00	0.00	7.00	4.000	No	Yes	2.00
2249	22.49	6.49	100.00	3.29	0.59	1.15	7.07	0.00	7.07	4.000	No	Yes	2.00
2250	22.50	6.57	100.00	3.29	0.59	1.15	7.15	0.00	7.15	4.000	No	Yes	2.00
2251	22.51	6.64	100.00	3.28	0.59	1.15	7.23	0.00	7.23	4.000	No	Yes	2.00
2252	22.52	6.73	100.00	3.28	0.59	1.15	7.32	0.00	7.32	4.000	No	Yes	2.00
2253	22.53	6.80	100.00	3.27	0.59	1.15	7.40	0.00	7.40	4.000	No	Yes	2.00
2254	22.54	6.87	100.00	3.27	0.59	1.15	7.48	0.00	7.48	4.000	No	Yes	2.00
2255	22.55	6.93	100.00	3.26	0.59	1.15	7.54	0.00	7.54	4.000	No	Yes	2.00
2256	22.56	6.96	100.00	3.26	0.59	1.15	7.58	0.00	7.58	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
2257	22.57	6.97	100.00	3.26	0.59	1.15	7.58	0.00	7.58	4.000	No	Yes	2.00
2258	22.58	6.97	100.00	3.26	0.59	1.15	7.58	0.00	7.58	4.000	No	Yes	2.00
2259	22.59	6.97	100.00	3.26	0.59	1.15	7.58	0.00	7.58	4.000	No	Yes	2.00
2260	22.60	6.97	100.00	3.26	0.59	1.15	7.58	0.00	7.58	4.000	No	Yes	2.00
2261	22.61	6.97	100.00	3.26	0.59	1.15	7.57	0.00	7.57	4.000	No	Yes	2.00
2262	22.62	6.97	100.00	3.26	0.59	1.15	7.57	0.00	7.57	4.000	No	Yes	2.00
2263	22.63	6.97	100.00	3.26	0.59	1.15	7.57	0.00	7.57	4.000	No	Yes	2.00
2264	22.64	6.95	100.00	3.27	0.59	1.15	7.57	0.00	7.57	4.000	No	Yes	2.00
2265	22.65	6.87	100.00	3.27	0.59	1.15	7.49	0.00	7.49	4.000	No	Yes	2.00
2266	22.66	6.75	100.00	3.28	0.59	1.15	7.33	0.00	7.33	4.000	No	Yes	2.00
2267	22.67	6.58	100.00	3.29	0.59	1.15	7.15	0.00	7.15	4.000	No	Yes	2.00
2268	22.68	6.40	100.00	3.31	0.59	1.15	6.95	0.00	6.95	4.000	No	Yes	2.00
2269	22.69	6.21	100.00	3.32	0.60	1.15	6.75	0.00	6.75	4.000	No	Yes	2.00
2270	22.70	6.03	100.00	3.34	0.60	1.15	6.54	0.00	6.54	4.000	No	Yes	2.00
2271	22.71	5.86	100.00	3.35	0.60	1.15	6.35	0.00	6.35	4.000	No	Yes	2.00
2272	22.72	5.71	100.00	3.37	0.60	1.15	6.19	0.00	6.19	4.000	No	Yes	2.00
2273	22.73	5.62	100.00	3.38	0.60	1.15	6.06	0.00	6.06	4.000	No	Yes	2.00
2274	22.74	5.58	100.00	3.38	0.60	1.15	6.06	0.00	6.06	4.000	No	Yes	2.00
2275	22.75	5.58	100.00	3.38	0.60	1.15	6.06	0.00	6.06	4.000	No	Yes	2.00
2276	22.76	5.58	100.00	3.38	0.60	1.15	6.05	0.00	6.05	4.000	No	Yes	2.00
2277	22.77	5.58	100.00	3.38	0.60	1.15	6.05	0.00	6.05	4.000	No	Yes	2.00
2278	22.78	5.58	100.00	3.38	0.60	1.15	6.05	0.00	6.05	4.000	No	Yes	2.00
2279	22.79	5.58	100.00	3.38	0.60	1.15	6.05	0.00	6.05	4.000	No	Yes	2.00
2280	22.80	5.58	100.00	3.38	0.60	1.15	6.05	0.00	6.05	4.000	No	Yes	2.00
2281	22.81	5.58	100.00	3.38	0.60	1.15	6.05	0.00	6.05	4.000	No	Yes	2.00
2282	22.82	5.58	100.00	3.38	0.60	1.15	6.05	0.00	6.05	4.000	No	Yes	2.00
2283	22.83	5.58	100.00	3.38	0.60	1.15	6.05	0.00	6.05	4.000	No	Yes	2.00
2284	22.84	5.58	100.00	3.38	0.60	1.15	6.05	0.00	6.05	4.000	No	Yes	2.00
2285	22.85	5.58	100.00	3.37	0.60	1.15	6.05	0.00	6.05	4.000	No	Yes	2.00
2286	22.86	5.58	100.00	3.37	0.60	1.15	6.05	0.00	6.05	4.000	No	Yes	2.00
2287	22.87	5.58	100.00	3.37	0.60	1.15	6.04	0.00	6.04	4.000	No	Yes	2.00
2288	22.88	5.58	100.00	3.37	0.60	1.15	6.04	0.00	6.04	4.000	No	Yes	2.00
2289	22.89	5.58	100.00	3.37	0.60	1.15	6.04	0.00	6.04	4.000	No	Yes	2.00
2290	22.90	5.58	100.00	3.37	0.60	1.15	6.04	0.00	6.04	4.000	No	Yes	2.00
2291	22.91	5.58	100.00	3.37	0.60	1.15	6.04	0.00	6.04	4.000	No	Yes	2.00
2292	22.92	5.58	100.00	3.37	0.60	1.15	6.04	0.00	6.04	4.000	No	Yes	2.00
2293	22.93	5.58	100.00	3.37	0.60	1.15	6.04	0.00	6.04	4.000	No	Yes	2.00
2294	22.94	5.58	100.00	3.37	0.60	1.15	6.04	0.00	6.04	4.000	No	Yes	2.00
2295	22.95	5.58	100.00	3.37	0.60	1.15	6.04	0.00	6.04	4.000	No	Yes	2.00
2296	22.96	5.58	100.00	3.37	0.60	1.15	6.04	0.00	6.04	4.000	No	Yes	2.00
2297	22.97	5.58	100.00	3.37	0.60	1.15	6.04	0.00	6.04	4.000	No	Yes	2.00
2298	22.98	5.58	100.00	3.37	0.60	1.15	6.04	0.00	6.04	4.000	No	Yes	2.00
2299	22.99	5.64	100.00	3.37	0.60	1.15	6.04	0.00	6.04	4.000	No	Yes	2.00
2300	23.00	5.77	100.00	3.35	0.60	1.15	6.22	0.00	6.22	4.000	No	Yes	2.00
2301	23.01	5.98	100.00	3.34	0.60	1.14	6.46	0.00	6.46	4.000	No	Yes	2.00
2302	23.02	6.23	100.00	3.32	0.60	1.14	6.72	0.00	6.72	4.000	No	Yes	2.00
2303	23.03	6.49	100.00	3.30	0.59	1.14	7.01	0.00	7.01	4.000	No	Yes	2.00
2304	23.04	6.76	100.00	3.28	0.59	1.14	7.30	0.00	7.30	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
2305	23.05	7.02	100.00	3.26	0.59	1.14	7.58	0.00	7.58	4.000	No	Yes	2.00
2306	23.06	7.25	100.00	3.25	0.59	1.14	7.84	0.00	7.84	4.000	No	Yes	2.00
2307	23.07	7.44	100.00	3.24	0.59	1.14	8.05	0.00	8.05	4.000	No	Yes	2.00
2308	23.08	7.58	100.00	3.23	0.59	1.14	8.19	0.00	8.19	4.000	No	Yes	2.00
2309	23.09	7.67	100.00	3.23	0.59	1.14	8.27	0.00	8.27	4.000	No	Yes	2.00
2310	23.10	7.76	100.00	3.22	0.59	1.14	8.36	0.00	8.36	4.000	No	Yes	2.00
2311	23.11	7.87	100.00	3.22	0.59	1.14	8.47	0.00	8.47	4.000	No	Yes	2.00
2312	23.12	7.97	100.00	3.22	0.59	1.14	8.59	0.00	8.59	4.000	No	Yes	2.00
2313	23.13	8.08	100.00	3.21	0.59	1.14	8.70	0.00	8.70	4.000	No	Yes	2.00
2314	23.14	8.18	100.00	3.21	0.59	1.14	8.81	0.00	8.81	4.000	No	Yes	2.00
2315	23.15	8.27	100.00	3.21	0.59	1.14	8.91	0.00	8.91	4.000	No	Yes	2.00
2316	23.16	8.32	100.00	3.21	0.59	1.14	8.98	0.00	8.98	4.000	No	Yes	2.00
2317	23.17	8.33	100.00	3.21	0.59	1.14	8.98	0.00	8.98	4.000	No	Yes	2.00
2318	23.18	8.30	100.00	3.21	0.59	1.14	8.93	0.00	8.93	4.000	No	Yes	2.00
2319	23.19	8.25	100.00	3.21	0.59	1.14	8.88	0.00	8.88	4.000	No	Yes	2.00
2320	23.20	8.20	100.00	3.22	0.59	1.14	8.82	0.00	8.82	4.000	No	Yes	2.00
2321	23.21	8.15	100.00	3.23	0.59	1.14	8.76	0.00	8.76	4.000	No	Yes	2.00
2322	23.22	8.10	100.00	3.23	0.59	1.14	8.70	0.00	8.70	4.000	No	Yes	2.00
2323	23.23	8.05	100.00	3.24	0.59	1.14	8.65	0.00	8.65	4.000	No	Yes	2.00
2324	23.24	8.01	100.00	3.24	0.59	1.14	8.60	0.00	8.60	4.000	No	Yes	2.00
2325	23.25	8.00	100.00	3.24	0.59	1.14	8.57	0.00	8.57	4.000	No	Yes	2.00
2326	23.26	8.05	100.00	3.24	0.59	1.14	8.64	0.00	8.64	4.000	No	Yes	2.00
2327	23.27	8.13	100.00	3.24	0.59	1.14	8.73	0.00	8.73	4.000	No	Yes	2.00
2328	23.28	8.23	100.00	3.23	0.59	1.14	8.84	0.00	8.84	4.000	No	Yes	2.00
2329	23.29	8.34	100.00	3.23	0.59	1.14	8.95	0.00	8.95	4.000	No	Yes	2.00
2330	23.30	8.44	100.00	3.23	0.59	1.14	9.07	0.00	9.07	4.000	No	Yes	2.00
2331	23.31	8.55	100.00	3.22	0.59	1.14	9.18	0.00	9.18	4.000	No	Yes	2.00
2332	23.32	8.64	100.00	3.22	0.59	1.14	9.28	0.00	9.28	4.000	No	Yes	2.00
2333	23.33	8.72	100.00	3.22	0.58	1.14	9.36	0.00	9.36	4.000	No	Yes	2.00
2334	23.34	8.79	100.00	3.21	0.58	1.14	9.43	0.00	9.43	4.000	No	Yes	2.00
2335	23.35	8.87	100.00	3.21	0.58	1.14	9.51	0.00	9.51	4.000	No	Yes	2.00
2336	23.36	8.96	100.00	3.21	0.58	1.14	9.60	0.00	9.60	4.000	No	Yes	2.00
2337	23.37	9.06	100.00	3.21	0.58	1.13	9.71	0.00	9.71	4.000	No	Yes	2.00
2338	23.38	9.17	100.00	3.20	0.58	1.13	9.83	0.00	9.83	4.000	No	Yes	2.00
2339	23.39	9.28	100.00	3.20	0.58	1.13	9.94	0.00	9.94	4.000	No	Yes	2.00
2340	23.40	9.38	100.00	3.20	0.58	1.13	10.05	0.00	10.05	4.000	No	Yes	2.00
2341	23.41	9.47	100.00	3.19	0.58	1.13	10.14	0.00	10.14	4.000	No	Yes	2.00
2342	23.42	9.54	100.00	3.19	0.58	1.13	10.22	0.00	10.22	4.000	No	Yes	2.00
2343	23.43	9.62	100.00	3.19	0.58	1.13	10.29	0.00	10.29	4.000	No	Yes	2.00
2344	23.44	9.70	100.00	3.18	0.58	1.13	10.37	0.00	10.37	4.000	No	Yes	2.00
2345	23.45	9.79	100.00	3.18	0.58	1.13	10.47	0.00	10.47	4.000	No	Yes	2.00
2346	23.46	9.90	100.00	3.18	0.58	1.13	10.58	0.00	10.58	4.000	No	Yes	2.00
2347	23.47	10.00	100.00	3.17	0.58	1.13	10.70	0.00	10.70	4.000	No	Yes	2.00
2348	23.48	10.11	100.00	3.17	0.58	1.13	10.81	0.00	10.81	4.000	No	Yes	2.00
2349	23.49	10.21	100.00	3.16	0.58	1.13	10.91	0.00	10.91	4.000	No	Yes	2.00
2350	23.50	10.29	100.00	3.16	0.58	1.13	11.00	0.00	11.00	4.000	No	Yes	2.00
2351	23.51	10.38	100.00	3.16	0.58	1.13	11.07	0.00	11.07	4.000	No	Yes	2.00
2352	23.52	10.47	100.00	3.15	0.58	1.13	11.17	0.00	11.17	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
2353	23.53	10.59	100.00	3.15	0.58	1.13	11.30	0.00	11.30	4.000	No	Yes	2.00
2354	23.54	10.72	100.00	3.14	0.58	1.13	11.44	0.00	11.44	4.000	No	Yes	2.00
2355	23.55	10.87	100.00	3.14	0.58	1.13	11.60	0.00	11.60	4.000	No	Yes	2.00
2356	23.56	11.02	100.00	3.13	0.58	1.13	11.75	0.00	11.75	4.000	No	Yes	2.00
2357	23.57	11.16	100.00	3.12	0.57	1.13	11.90	0.00	11.90	4.000	No	Yes	2.00
2358	23.58	11.29	100.00	3.12	0.57	1.13	12.04	0.00	12.04	4.000	No	Yes	2.00
2359	23.59	11.39	100.00	3.11	0.57	1.13	12.15	0.00	12.15	4.000	No	Yes	2.00
2360	23.60	11.48	100.00	3.11	0.57	1.13	12.23	0.00	12.23	4.000	No	Yes	2.00
2361	23.61	11.56	100.00	3.11	0.57	1.13	12.31	0.00	12.31	4.000	No	Yes	2.00
2362	23.62	11.66	100.00	3.10	0.57	1.13	12.41	0.00	12.41	4.000	No	Yes	2.00
2363	23.63	11.76	100.00	3.10	0.57	1.13	12.51	0.00	12.51	4.000	No	Yes	2.00
2364	23.64	11.86	100.00	3.10	0.57	1.13	12.63	0.00	12.63	4.000	No	Yes	2.00
2365	23.65	11.97	100.00	3.09	0.57	1.13	12.74	0.00	12.74	4.000	No	Yes	2.00
2366	23.66	12.07	100.00	3.09	0.57	1.13	12.84	0.00	12.84	4.000	No	Yes	2.00
2367	23.67	12.16	100.00	3.09	0.57	1.13	12.94	0.00	12.94	4.000	No	Yes	2.00
2368	23.68	12.21	100.00	3.09	0.57	1.13	13.01	0.00	13.01	4.000	No	Yes	2.00
2369	23.69	12.23	100.00	3.09	0.57	1.13	13.01	0.00	13.01	4.000	No	Yes	2.00
2370	23.70	12.20	100.00	3.09	0.57	1.13	12.97	0.00	12.97	4.000	No	Yes	2.00
2371	23.71	12.17	100.00	3.09	0.57	1.13	12.93	0.00	12.93	4.000	No	Yes	2.00
2372	23.72	12.13	100.00	3.09	0.57	1.13	12.89	0.00	12.89	4.000	No	Yes	2.00
2373	23.73	12.09	100.00	3.10	0.57	1.13	12.84	0.00	12.84	4.000	No	Yes	2.00
2374	23.74	12.05	100.00	3.10	0.57	1.13	12.80	0.00	12.80	4.000	No	Yes	2.00
2375	23.75	12.01	100.00	3.10	0.57	1.12	12.76	0.00	12.76	4.000	No	Yes	2.00
2376	23.76	11.99	100.00	3.10	0.57	1.12	12.72	0.00	12.72	4.000	No	Yes	2.00
2377	23.77	12.06	100.00	3.10	0.57	1.12	12.72	0.00	12.72	4.000	No	Yes	2.00
2378	23.78	12.26	100.00	3.10	0.57	1.12	12.99	0.00	12.99	4.000	No	Yes	2.00
2379	23.79	12.59	100.00	3.09	0.57	1.12	13.34	0.00	13.34	4.000	No	Yes	2.00
2380	23.80	12.96	100.00	3.08	0.57	1.12	13.73	0.00	13.73	4.000	No	Yes	2.00
2381	23.81	13.35	100.00	3.07	0.57	1.12	14.15	0.00	14.15	4.000	No	Yes	2.00
2382	23.82	13.75	100.00	3.06	0.57	1.12	14.58	0.00	14.58	4.000	No	Yes	2.00
2383	23.83	14.14	100.00	3.05	0.56	1.12	14.98	0.00	14.98	4.000	No	Yes	2.00
2384	23.84	14.49	100.00	3.05	0.56	1.12	15.35	0.00	15.35	4.000	No	Yes	2.00
2385	23.85	14.77	100.00	3.04	0.56	1.12	15.67	0.00	15.67	4.000	No	Yes	2.00
2386	23.86	14.96	100.00	3.04	0.56	1.12	15.85	0.00	15.85	4.000	No	Yes	2.00
2387	23.87	15.11	100.00	3.03	0.56	1.12	15.97	0.00	15.97	4.000	No	Yes	2.00
2388	23.88	15.25	100.00	3.03	0.56	1.12	16.11	0.00	16.11	4.000	No	Yes	2.00
2389	23.89	15.40	100.00	3.03	0.56	1.12	16.27	0.00	16.27	4.000	No	Yes	2.00
2390	23.90	15.56	100.00	3.03	0.56	1.12	16.44	0.00	16.44	4.000	No	Yes	2.00
2391	23.91	15.72	100.00	3.03	0.56	1.12	16.60	0.00	16.60	4.000	No	Yes	2.00
2392	23.92	15.87	100.00	3.03	0.56	1.12	16.76	0.00	16.76	4.000	No	Yes	2.00
2393	23.93	16.00	100.00	3.02	0.56	1.12	16.90	0.00	16.90	4.000	No	Yes	2.00
2394	23.94	16.04	100.00	3.02	0.56	1.12	17.01	0.00	17.01	4.000	No	Yes	2.00
2395	23.95	15.96	100.00	3.03	0.56	1.12	16.88	0.00	16.88	4.000	No	Yes	2.00
2396	23.96	15.76	100.00	3.03	0.56	1.12	16.64	0.00	16.64	4.000	No	Yes	2.00
2397	23.97	15.49	100.00	3.04	0.56	1.12	16.36	0.00	16.36	4.000	No	Yes	2.00
2398	23.98	15.21	100.00	3.05	0.56	1.12	16.05	0.00	16.05	4.000	No	Yes	2.00
2399	23.99	14.91	100.00	3.05	0.56	1.12	15.74	0.00	15.74	4.000	No	Yes	2.00
2400	24.00	14.63	100.00	3.06	0.56	1.12	15.43	0.00	15.43	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
2401	24.01	14.36	100.00	3.07	0.56	1.12	15.15	0.00	15.15	4.000	No	Yes	2.00
2402	24.02	14.14	100.00	3.08	0.56	1.12	14.90	0.00	14.90	4.000	No	Yes	2.00
2403	24.03	13.99	100.00	3.08	0.56	1.12	14.72	0.00	14.72	4.000	No	Yes	2.00
2404	24.04	13.91	100.00	3.08	0.56	1.12	14.68	0.00	14.68	4.000	No	Yes	2.00
2405	24.05	13.86	100.00	3.08	0.56	1.12	14.63	0.00	14.63	4.000	No	Yes	2.00
2406	24.06	13.81	100.00	3.09	0.57	1.12	14.57	0.00	14.57	4.000	No	Yes	2.00
2407	24.07	13.76	100.00	3.09	0.57	1.12	14.52	0.00	14.52	4.000	No	Yes	2.00
2408	24.08	13.71	100.00	3.09	0.57	1.12	14.46	0.00	14.46	4.000	No	Yes	2.00
2409	24.09	13.66	100.00	3.09	0.57	1.12	14.40	0.00	14.40	4.000	No	Yes	2.00
2410	24.10	13.61	100.00	3.09	0.57	1.12	14.35	0.00	14.35	4.000	No	Yes	2.00
2411	24.11	13.56	100.00	3.09	0.57	1.12	14.30	0.00	14.30	4.000	No	Yes	2.00
2412	24.12	13.48	100.00	3.09	0.57	1.12	14.23	0.00	14.23	4.000	No	Yes	2.00
2413	24.13	13.35	100.00	3.10	0.57	1.12	14.09	0.00	14.09	4.000	No	Yes	2.00
2414	24.14	13.19	100.00	3.10	0.57	1.12	13.91	0.00	13.91	4.000	No	Yes	2.00
2415	24.15	13.02	100.00	3.11	0.57	1.12	13.72	0.00	13.72	4.000	No	Yes	2.00
2416	24.16	12.83	100.00	3.12	0.57	1.12	13.52	0.00	13.52	4.000	No	Yes	2.00
2417	24.17	12.64	100.00	3.12	0.57	1.12	13.32	0.00	13.32	4.000	No	Yes	2.00
2418	24.18	12.47	100.00	3.13	0.57	1.12	13.14	0.00	13.14	4.000	No	Yes	2.00
2419	24.19	12.32	100.00	3.14	0.57	1.12	12.97	0.00	12.97	4.000	No	Yes	2.00
2420	24.20	12.18	100.00	3.14	0.57	1.12	12.83	0.00	12.83	4.000	No	Yes	2.00
2421	24.21	12.05	100.00	3.15	0.57	1.12	12.71	0.00	12.71	4.000	No	Yes	2.00
2422	24.22	11.91	100.00	3.15	0.57	1.12	12.55	0.00	12.55	4.000	No	Yes	2.00
2423	24.23	11.74	100.00	3.16	0.57	1.12	12.37	0.00	12.37	4.000	No	Yes	2.00
2424	24.24	11.56	100.00	3.17	0.57	1.12	12.18	0.00	12.18	4.000	No	Yes	2.00
2425	24.25	11.37	100.00	3.17	0.57	1.12	11.98	0.00	11.98	4.000	No	Yes	2.00
2426	24.26	11.19	100.00	3.18	0.58	1.12	11.78	0.00	11.78	4.000	No	Yes	2.00
2427	24.27	11.02	100.00	3.19	0.58	1.12	11.60	0.00	11.60	4.000	No	Yes	2.00
2428	24.28	10.88	100.00	3.20	0.58	1.12	11.44	0.00	11.44	4.000	No	Yes	2.00
2429	24.29	10.85	100.00	3.20	0.58	1.12	11.35	0.00	11.35	4.000	No	Yes	2.00
2430	24.30	10.91	100.00	3.20	0.58	1.12	11.48	0.00	11.48	4.000	No	Yes	2.00
2431	24.31	11.06	100.00	3.19	0.58	1.11	11.64	0.00	11.64	4.000	No	Yes	2.00
2432	24.32	11.24	100.00	3.19	0.58	1.11	11.82	0.00	11.82	4.000	No	Yes	2.00
2433	24.33	11.42	100.00	3.18	0.57	1.11	12.02	0.00	12.02	4.000	No	Yes	2.00
2434	24.34	11.61	100.00	3.18	0.57	1.11	12.21	0.00	12.21	4.000	No	Yes	2.00
2435	24.35	11.79	100.00	3.17	0.57	1.11	12.40	0.00	12.40	4.000	No	Yes	2.00
2436	24.36	11.95	100.00	3.17	0.57	1.11	12.57	0.00	12.57	4.000	No	Yes	2.00
2437	24.37	12.09	100.00	3.16	0.57	1.11	12.71	0.00	12.71	4.000	No	Yes	2.00
2438	24.38	12.22	100.00	3.16	0.57	1.11	12.83	0.00	12.83	4.000	No	Yes	2.00
2439	24.39	12.35	100.00	3.15	0.57	1.11	12.97	0.00	12.97	4.000	No	Yes	2.00
2440	24.40	12.52	100.00	3.15	0.57	1.11	13.14	0.00	13.14	4.000	No	Yes	2.00
2441	24.41	12.69	100.00	3.14	0.57	1.11	13.32	0.00	13.32	4.000	No	Yes	2.00
2442	24.42	12.88	100.00	3.14	0.57	1.11	13.52	0.00	13.52	4.000	No	Yes	2.00
2443	24.43	13.07	100.00	3.13	0.57	1.11	13.71	0.00	13.71	4.000	No	Yes	2.00
2444	24.44	13.24	100.00	3.13	0.57	1.11	13.89	0.00	13.89	4.000	No	Yes	2.00
2445	24.45	13.39	100.00	3.13	0.57	1.11	14.05	0.00	14.05	4.000	No	Yes	2.00
2446	24.46	13.50	100.00	3.12	0.57	1.11	14.18	0.00	14.18	4.000	No	Yes	2.00
2447	24.47	13.54	100.00	3.12	0.57	1.11	14.20	0.00	14.20	4.000	No	Yes	2.00
2448	24.48	13.55	100.00	3.12	0.57	1.11	14.20	0.00	14.20	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
2449	24.49	13.55	100.00	3.12	0.57	1.11	14.20	0.00	14.20	4.000	No	Yes	2.00
2450	24.50	13.55	100.00	3.12	0.57	1.11	14.19	0.00	14.19	4.000	No	Yes	2.00
2451	24.51	13.55	100.00	3.12	0.57	1.11	14.19	0.00	14.19	4.000	No	Yes	2.00
2452	24.52	13.55	100.00	3.12	0.57	1.11	14.19	0.00	14.19	4.000	No	Yes	2.00
2453	24.53	13.55	100.00	3.12	0.57	1.11	14.19	0.00	14.19	4.000	No	Yes	2.00
2454	24.54	13.55	100.00	3.12	0.57	1.11	14.18	0.00	14.18	4.000	No	Yes	2.00
2455	24.55	13.52	100.00	3.12	0.57	1.11	14.17	0.00	14.17	4.000	No	Yes	2.00
2456	24.56	13.46	100.00	3.12	0.57	1.11	14.09	0.00	14.09	4.000	No	Yes	2.00
2457	24.57	13.38	100.00	3.12	0.57	1.11	14.00	0.00	14.00	4.000	No	Yes	2.00
2458	24.58	13.28	100.00	3.13	0.57	1.11	13.89	0.00	13.89	4.000	No	Yes	2.00
2459	24.59	13.17	100.00	3.13	0.57	1.11	13.78	0.00	13.78	4.000	No	Yes	2.00
2460	24.60	13.06	100.00	3.13	0.57	1.11	13.66	0.00	13.66	4.000	No	Yes	2.00
2461	24.61	12.96	100.00	3.13	0.57	1.11	13.55	0.00	13.55	4.000	No	Yes	2.00
2462	24.62	12.87	100.00	3.13	0.57	1.11	13.45	0.00	13.45	4.000	No	Yes	2.00
2463	24.63	12.79	100.00	3.13	0.57	1.11	13.37	0.00	13.37	4.000	No	Yes	2.00
2464	24.64	12.72	100.00	3.14	0.57	1.11	13.30	0.00	13.30	4.000	No	Yes	2.00
2465	24.65	12.64	100.00	3.14	0.57	1.11	13.22	0.00	13.22	4.000	No	Yes	2.00
2466	24.66	12.55	100.00	3.14	0.57	1.11	13.12	0.00	13.12	4.000	No	Yes	2.00
2467	24.67	12.44	100.00	3.14	0.57	1.11	13.01	0.00	13.01	4.000	No	Yes	2.00
2468	24.68	12.34	100.00	3.14	0.57	1.11	12.89	0.00	12.89	4.000	No	Yes	2.00
2469	24.69	12.23	100.00	3.14	0.57	1.11	12.78	0.00	12.78	4.000	No	Yes	2.00
2470	24.70	12.13	100.00	3.15	0.57	1.11	12.67	0.00	12.67	4.000	No	Yes	2.00
2471	24.71	12.04	100.00	3.15	0.57	1.11	12.58	0.00	12.58	4.000	No	Yes	2.00
2472	24.72	11.97	100.00	3.15	0.57	1.11	12.50	0.00	12.50	4.000	No	Yes	2.00
2473	24.73	11.89	100.00	3.15	0.57	1.11	12.43	0.00	12.43	4.000	No	Yes	2.00
2474	24.74	11.81	100.00	3.15	0.57	1.11	12.34	0.00	12.34	4.000	No	Yes	2.00
2475	24.75	11.71	100.00	3.16	0.57	1.11	12.24	0.00	12.24	4.000	No	Yes	2.00
2476	24.76	11.61	100.00	3.16	0.57	1.11	12.13	0.00	12.13	4.000	No	Yes	2.00
2477	24.77	11.50	100.00	3.16	0.57	1.11	12.01	0.00	12.01	4.000	No	Yes	2.00
2478	24.78	11.40	100.00	3.16	0.57	1.11	11.90	0.00	11.90	4.000	No	Yes	2.00
2479	24.79	11.30	100.00	3.17	0.58	1.11	11.80	0.00	11.80	4.000	No	Yes	2.00
2480	24.80	11.22	100.00	3.17	0.58	1.11	11.71	0.00	11.71	4.000	No	Yes	2.00
2481	24.81	11.11	100.00	3.17	0.58	1.11	11.63	0.00	11.63	4.000	No	Yes	2.00
2482	24.82	10.98	100.00	3.18	0.58	1.11	11.47	0.00	11.47	4.000	No	Yes	2.00
2483	24.83	10.80	100.00	3.18	0.58	1.11	11.29	0.00	11.29	4.000	No	Yes	2.00
2484	24.84	10.60	100.00	3.19	0.58	1.11	11.07	0.00	11.07	4.000	No	Yes	2.00
2485	24.85	10.39	100.00	3.20	0.58	1.11	10.85	0.00	10.85	4.000	No	Yes	2.00
2486	24.86	10.18	100.00	3.21	0.58	1.11	10.62	0.00	10.62	4.000	No	Yes	2.00
2487	24.87	9.98	100.00	3.21	0.58	1.11	10.41	0.00	10.41	4.000	No	Yes	2.00
2488	24.88	9.79	100.00	3.22	0.58	1.11	10.21	0.00	10.21	4.000	No	Yes	2.00
2489	24.89	9.65	100.00	3.23	0.58	1.11	10.05	0.00	10.05	4.000	No	Yes	2.00
2490	24.90	9.54	100.00	3.23	0.58	1.11	9.95	0.00	9.95	4.000	No	Yes	2.00
2491	24.91	9.45	100.00	3.24	0.58	1.11	9.86	0.00	9.86	4.000	No	Yes	2.00
2492	24.92	9.35	100.00	3.24	0.58	1.10	9.76	0.00	9.76	4.000	No	Yes	2.00
2493	24.93	9.25	100.00	3.24	0.58	1.10	9.65	0.00	9.65	4.000	No	Yes	2.00
2494	24.94	9.14	100.00	3.25	0.58	1.10	9.54	0.00	9.54	4.000	No	Yes	2.00
2495	24.95	9.04	100.00	3.25	0.58	1.10	9.43	0.00	9.43	4.000	No	Yes	2.00
2496	24.96	8.94	100.00	3.26	0.58	1.10	9.32	0.00	9.32	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
2497	24.97	8.85	100.00	3.26	0.59	1.10	9.23	0.00	9.23	4.000	No	Yes	2.00
2498	24.98	8.78	100.00	3.27	0.59	1.10	9.15	0.00	9.15	4.000	No	Yes	2.00
2499	24.99	8.70	100.00	3.27	0.59	1.10	9.08	0.00	9.08	4.000	No	Yes	2.00
2500	25.00	8.62	100.00	3.27	0.59	1.10	8.99	0.00	8.99	4.000	No	Yes	2.00
2501	25.01	8.52	100.00	3.28	0.59	1.10	8.89	0.00	8.89	4.000	No	Yes	2.00
2502	25.02	8.42	100.00	3.28	0.59	1.10	8.78	0.00	8.78	4.000	No	Yes	2.00
2503	25.03	8.31	100.00	3.29	0.59	1.10	8.66	0.00	8.66	4.000	No	Yes	2.00
2504	25.04	8.21	100.00	3.30	0.59	1.10	8.55	0.00	8.55	4.000	No	Yes	2.00
2505	25.05	8.11	100.00	3.30	0.59	1.10	8.45	0.00	8.45	4.000	No	Yes	2.00
2506	25.06	8.03	100.00	3.31	0.59	1.10	8.36	0.00	8.36	4.000	No	Yes	2.00
2507	25.07	7.96	100.00	3.31	0.59	1.10	8.29	0.00	8.29	4.000	No	Yes	2.00
2508	25.08	7.88	100.00	3.31	0.59	1.10	8.21	0.00	8.21	4.000	No	Yes	2.00
2509	25.09	7.79	100.00	3.32	0.59	1.10	8.12	0.00	8.12	4.000	No	Yes	2.00
2510	25.10	7.69	100.00	3.33	0.59	1.10	8.01	0.00	8.01	4.000	No	Yes	2.00
2511	25.11	7.58	100.00	3.33	0.59	1.10	7.90	0.00	7.90	4.000	No	Yes	2.00
2512	25.12	7.48	100.00	3.34	0.59	1.10	7.79	0.00	7.79	4.000	No	Yes	2.00
2513	25.13	7.38	100.00	3.35	0.59	1.10	7.68	0.00	7.68	4.000	No	Yes	2.00
2514	25.14	7.28	100.00	3.35	0.59	1.10	7.58	0.00	7.58	4.000	No	Yes	2.00
2515	25.15	7.22	100.00	3.36	0.59	1.10	7.50	0.00	7.50	4.000	No	Yes	2.00
2516	25.16	7.18	100.00	3.36	0.59	1.10	7.47	0.00	7.47	4.000	No	Yes	2.00
2517	25.17	7.17	100.00	3.36	0.59	1.10	7.47	0.00	7.47	4.000	No	Yes	2.00
2518	25.18	7.17	100.00	3.36	0.59	1.10	7.47	0.00	7.47	4.000	No	Yes	2.00
2519	25.19	7.17	100.00	3.36	0.59	1.10	7.46	0.00	7.46	4.000	No	Yes	2.00
2520	25.20	7.17	100.00	3.36	0.59	1.10	7.46	0.00	7.46	4.000	No	Yes	2.00
2521	25.21	7.17	100.00	3.36	0.59	1.10	7.46	0.00	7.46	4.000	No	Yes	2.00
2522	25.22	7.17	100.00	3.36	0.59	1.10	7.46	0.00	7.46	4.000	No	Yes	2.00
2523	25.23	7.17	100.00	3.36	0.59	1.10	7.46	0.00	7.46	4.000	No	Yes	2.00
2524	25.24	7.15	100.00	3.37	0.59	1.10	7.46	0.00	7.46	4.000	No	Yes	2.00
2525	25.25	7.10	100.00	3.37	0.59	1.10	7.40	0.00	7.40	4.000	No	Yes	2.00
2526	25.26	7.02	100.00	3.38	0.59	1.10	7.31	0.00	7.31	4.000	No	Yes	2.00
2527	25.27	6.93	100.00	3.38	0.59	1.10	7.20	0.00	7.20	4.000	No	Yes	2.00
2528	25.28	6.82	100.00	3.39	0.59	1.10	7.09	0.00	7.09	4.000	No	Yes	2.00
2529	25.29	6.72	100.00	3.40	0.59	1.10	6.98	0.00	6.98	4.000	No	Yes	2.00
2530	25.30	6.61	100.00	3.40	0.59	1.10	6.87	0.00	6.87	4.000	No	Yes	2.00
2531	25.31	6.52	100.00	3.41	0.60	1.10	6.77	0.00	6.77	4.000	No	Yes	2.00
2532	25.32	6.44	100.00	3.42	0.60	1.10	6.68	0.00	6.68	4.000	No	Yes	2.00
2533	25.33	6.39	100.00	3.42	0.60	1.10	6.63	0.00	6.63	4.000	No	Yes	2.00
2534	25.34	6.38	100.00	3.42	0.60	1.10	6.62	0.00	6.62	4.000	No	Yes	2.00
2535	25.35	6.38	100.00	3.42	0.60	1.10	6.62	0.00	6.62	4.000	No	Yes	2.00
2536	25.36	6.38	100.00	3.42	0.60	1.10	6.62	0.00	6.62	4.000	No	Yes	2.00
2537	25.37	6.38	100.00	3.42	0.60	1.10	6.62	0.00	6.62	4.000	No	Yes	2.00
2538	25.38	6.38	100.00	3.42	0.60	1.10	6.62	0.00	6.62	4.000	No	Yes	2.00
2539	25.39	6.38	100.00	3.42	0.60	1.10	6.62	0.00	6.62	4.000	No	Yes	2.00
2540	25.40	6.38	100.00	3.41	0.60	1.10	6.62	0.00	6.62	4.000	No	Yes	2.00
2541	25.41	6.39	100.00	3.41	0.60	1.10	6.62	0.00	6.62	4.000	No	Yes	2.00
2542	25.42	6.43	100.00	3.41	0.60	1.10	6.65	0.00	6.65	4.000	No	Yes	2.00
2543	25.43	6.50	100.00	3.40	0.60	1.10	6.74	0.00	6.74	4.000	No	Yes	2.00
2544	25.44	6.59	100.00	3.39	0.59	1.10	6.83	0.00	6.83	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
2545	25.45	6.69	100.00	3.38	0.59	1.10	6.94	0.00	6.94	4.000	No	Yes	2.00
2546	25.46	6.80	100.00	3.38	0.59	1.10	7.05	0.00	7.05	4.000	No	Yes	2.00
2547	25.47	6.90	100.00	3.37	0.59	1.10	7.16	0.00	7.16	4.000	No	Yes	2.00
2548	25.48	7.00	100.00	3.36	0.59	1.10	7.26	0.00	7.26	4.000	No	Yes	2.00
2549	25.49	7.09	100.00	3.35	0.59	1.10	7.35	0.00	7.35	4.000	No	Yes	2.00
2550	25.50	7.17	100.00	3.35	0.59	1.10	7.43	0.00	7.43	4.000	No	Yes	2.00
2551	25.51	7.24	100.00	3.34	0.59	1.10	7.49	0.00	7.49	4.000	No	Yes	2.00
2552	25.52	7.32	100.00	3.33	0.59	1.10	7.58	0.00	7.58	4.000	No	Yes	2.00
2553	25.53	7.42	100.00	3.33	0.59	1.10	7.68	0.00	7.68	4.000	No	Yes	2.00
2554	25.54	7.53	100.00	3.32	0.59	1.10	7.79	0.00	7.79	4.000	No	Yes	2.00
2555	25.55	7.63	100.00	3.31	0.59	1.10	7.90	0.00	7.90	4.000	No	Yes	2.00
2556	25.56	7.74	100.00	3.31	0.59	1.10	8.01	0.00	8.01	4.000	No	Yes	2.00
2557	25.57	7.83	100.00	3.30	0.59	1.10	8.11	0.00	8.11	4.000	No	Yes	2.00
2558	25.58	7.91	100.00	3.29	0.59	1.10	8.19	0.00	8.19	4.000	No	Yes	2.00
2559	25.59	7.99	100.00	3.29	0.59	1.09	8.26	0.00	8.26	4.000	No	Yes	2.00
2560	25.60	8.06	100.00	3.29	0.59	1.09	8.33	0.00	8.33	4.000	No	Yes	2.00
2561	25.61	8.15	100.00	3.28	0.59	1.09	8.42	0.00	8.42	4.000	No	Yes	2.00
2562	25.62	8.25	100.00	3.28	0.59	1.09	8.53	0.00	8.53	4.000	No	Yes	2.00
2563	25.63	8.36	100.00	3.27	0.59	1.09	8.64	0.00	8.64	4.000	No	Yes	2.00
2564	25.64	8.47	100.00	3.27	0.59	1.09	8.75	0.00	8.75	4.000	No	Yes	2.00
2565	25.65	8.57	100.00	3.27	0.59	1.09	8.85	0.00	8.85	4.000	No	Yes	2.00
2566	25.66	8.66	100.00	3.26	0.59	1.09	8.95	0.00	8.95	4.000	No	Yes	2.00
2567	25.67	8.72	100.00	3.26	0.59	1.09	9.02	0.00	9.02	4.000	No	Yes	2.00
2568	25.68	8.76	100.00	3.26	0.59	1.09	9.05	0.00	9.05	4.000	No	Yes	2.00
2569	25.69	8.77	100.00	3.26	0.59	1.09	9.05	0.00	9.05	4.000	No	Yes	2.00
2570	25.70	8.77	100.00	3.26	0.59	1.09	9.05	0.00	9.05	4.000	No	Yes	2.00
2571	25.71	8.77	100.00	3.27	0.59	1.09	9.04	0.00	9.04	4.000	No	Yes	2.00
2572	25.72	8.77	100.00	3.27	0.59	1.09	9.04	0.00	9.04	4.000	No	Yes	2.00
2573	25.73	8.77	100.00	3.27	0.59	1.09	9.04	0.00	9.04	4.000	No	Yes	2.00
2574	25.74	8.77	100.00	3.27	0.59	1.09	9.04	0.00	9.04	4.000	No	Yes	2.00
2575	25.75	8.77	100.00	3.27	0.59	1.09	9.04	0.00	9.04	4.000	No	Yes	2.00
2576	25.76	8.79	100.00	3.27	0.59	1.09	9.04	0.00	9.04	4.000	No	Yes	2.00
2577	25.77	8.84	100.00	3.27	0.59	1.09	9.10	0.00	9.10	4.000	No	Yes	2.00
2578	25.78	8.92	100.00	3.27	0.59	1.09	9.19	0.00	9.19	4.000	No	Yes	2.00
2579	25.79	9.02	100.00	3.26	0.59	1.09	9.29	0.00	9.29	4.000	No	Yes	2.00
2580	25.80	9.12	100.00	3.26	0.58	1.09	9.40	0.00	9.40	4.000	No	Yes	2.00
2581	25.81	9.23	100.00	3.25	0.58	1.09	9.51	0.00	9.51	4.000	No	Yes	2.00
2582	25.82	9.33	100.00	3.25	0.58	1.09	9.61	0.00	9.61	4.000	No	Yes	2.00
2583	25.83	9.43	100.00	3.25	0.58	1.09	9.71	0.00	9.71	4.000	No	Yes	2.00
2584	25.84	9.51	100.00	3.24	0.58	1.09	9.79	0.00	9.79	4.000	No	Yes	2.00
2585	25.85	9.58	100.00	3.24	0.58	1.09	9.86	0.00	9.86	4.000	No	Yes	2.00
2586	25.86	9.66	100.00	3.24	0.58	1.09	9.93	0.00	9.93	4.000	No	Yes	2.00
2587	25.87	9.75	100.00	3.23	0.58	1.09	10.02	0.00	10.02	4.000	No	Yes	2.00
2588	25.88	9.85	100.00	3.23	0.58	1.09	10.13	0.00	10.13	4.000	No	Yes	2.00
2589	25.89	9.96	100.00	3.23	0.58	1.09	10.24	0.00	10.24	4.000	No	Yes	2.00
2590	25.90	10.06	100.00	3.22	0.58	1.09	10.34	0.00	10.34	4.000	No	Yes	2.00
2591	25.91	10.16	100.00	3.22	0.58	1.09	10.45	0.00	10.45	4.000	No	Yes	2.00
2592	25.92	10.25	100.00	3.21	0.58	1.09	10.54	0.00	10.54	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
2593	25.93	10.36	100.00	3.21	0.58	1.09	10.62	0.00	10.62	4.000	No	Yes	2.00
2594	25.94	10.53	100.00	3.20	0.58	1.09	10.77	0.00	10.77	4.000	No	Yes	2.00
2595	25.95	10.77	100.00	3.19	0.58	1.09	11.04	0.00	11.04	4.000	No	Yes	2.00
2596	25.96	11.07	100.00	3.18	0.58	1.09	11.35	0.00	11.35	4.000	No	Yes	2.00
2597	25.97	11.41	100.00	3.17	0.58	1.09	11.70	0.00	11.70	4.000	No	Yes	2.00
2598	25.98	11.75	100.00	3.16	0.57	1.09	12.06	0.00	12.06	4.000	No	Yes	2.00
2599	25.99	12.10	100.00	3.15	0.57	1.09	12.41	0.00	12.41	4.000	No	Yes	2.00
2600	26.00	12.42	100.00	3.14	0.57	1.09	12.74	0.00	12.74	4.000	No	Yes	2.00
2601	26.01	12.70	100.00	3.13	0.57	1.08	13.03	0.00	13.03	4.000	No	Yes	2.00
2602	26.02	12.89	100.00	3.12	0.57	1.08	13.26	0.00	13.26	4.000	No	Yes	2.00
2603	26.03	13.02	100.00	3.12	0.57	1.08	13.33	0.00	13.33	4.000	No	Yes	2.00
2604	26.04	13.11	100.00	3.12	0.57	1.08	13.42	0.00	13.42	4.000	No	Yes	2.00
2605	26.05	13.20	100.00	3.12	0.57	1.08	13.51	0.00	13.51	4.000	No	Yes	2.00
2606	26.06	13.31	100.00	3.11	0.57	1.08	13.62	0.00	13.62	4.000	No	Yes	2.00
2607	26.07	13.42	100.00	3.11	0.57	1.08	13.73	0.00	13.73	4.000	No	Yes	2.00
2608	26.08	13.52	100.00	3.11	0.57	1.08	13.83	0.00	13.83	4.000	No	Yes	2.00
2609	26.09	13.61	100.00	3.11	0.57	1.08	13.93	0.00	13.93	4.000	No	Yes	2.00
2610	26.10	13.68	100.00	3.11	0.57	1.08	14.01	0.00	14.01	4.000	No	Yes	2.00
2611	26.11	13.65	100.00	3.11	0.57	1.08	14.01	0.00	14.01	4.000	No	Yes	2.00
2612	26.12	13.53	100.00	3.11	0.57	1.08	13.84	0.00	13.84	4.000	No	Yes	2.00
2613	26.13	13.33	100.00	3.12	0.57	1.08	13.63	0.00	13.63	4.000	No	Yes	2.00
2614	26.14	13.10	100.00	3.13	0.57	1.08	13.39	0.00	13.39	4.000	No	Yes	2.00
2615	26.15	12.86	100.00	3.13	0.57	1.08	13.15	0.00	13.15	4.000	No	Yes	2.00
2616	26.16	12.62	100.00	3.14	0.57	1.08	12.90	0.00	12.90	4.000	No	Yes	2.00
2617	26.17	12.39	100.00	3.15	0.57	1.08	12.66	0.00	12.66	4.000	No	Yes	2.00
2618	26.18	12.19	100.00	3.16	0.57	1.08	12.45	0.00	12.45	4.000	No	Yes	2.00
2619	26.19	12.05	100.00	3.17	0.57	1.08	12.27	0.00	12.27	4.000	No	Yes	2.00
2620	26.20	11.97	100.00	3.17	0.57	1.08	12.22	0.00	12.22	4.000	No	Yes	2.00
2621	26.21	11.96	100.00	3.17	0.57	1.08	12.21	0.00	12.21	4.000	No	Yes	2.00
2622	26.22	11.96	100.00	3.17	0.57	1.08	12.21	0.00	12.21	4.000	No	Yes	2.00
2623	26.23	11.96	100.00	3.17	0.57	1.08	12.21	0.00	12.21	4.000	No	Yes	2.00
2624	26.24	11.96	100.00	3.17	0.57	1.08	12.21	0.00	12.21	4.000	No	Yes	2.00
2625	26.25	11.96	100.00	3.18	0.57	1.08	12.21	0.00	12.21	4.000	No	Yes	2.00
2626	26.26	11.96	100.00	3.18	0.57	1.08	12.20	0.00	12.20	4.000	No	Yes	2.00
2627	26.27	11.96	100.00	3.18	0.57	1.08	12.20	0.00	12.20	4.000	No	Yes	2.00
2628	26.28	11.98	100.00	3.18	0.57	1.08	12.20	0.00	12.20	4.000	No	Yes	2.00
2629	26.29	12.03	100.00	3.18	0.57	1.08	12.27	0.00	12.27	4.000	No	Yes	2.00
2630	26.30	12.11	100.00	3.18	0.57	1.08	12.35	0.00	12.35	4.000	No	Yes	2.00
2631	26.31	12.21	100.00	3.17	0.57	1.08	12.45	0.00	12.45	4.000	No	Yes	2.00
2632	26.32	12.32	100.00	3.17	0.57	1.08	12.56	0.00	12.56	4.000	No	Yes	2.00
2633	26.33	12.42	100.00	3.17	0.57	1.08	12.67	0.00	12.67	4.000	No	Yes	2.00
2634	26.34	12.53	100.00	3.17	0.57	1.08	12.77	0.00	12.77	4.000	No	Yes	2.00
2635	26.35	12.62	100.00	3.16	0.57	1.08	12.87	0.00	12.87	4.000	No	Yes	2.00
2636	26.36	12.70	100.00	3.16	0.57	1.08	12.95	0.00	12.95	4.000	No	Yes	2.00
2637	26.37	12.78	100.00	3.16	0.57	1.08	13.01	0.00	13.01	4.000	No	Yes	2.00
2638	26.38	12.85	100.00	3.16	0.57	1.08	13.08	0.00	13.08	4.000	No	Yes	2.00
2639	26.39	12.94	100.00	3.15	0.57	1.08	13.17	0.00	13.17	4.000	No	Yes	2.00
2640	26.40	13.04	100.00	3.15	0.57	1.08	13.28	0.00	13.28	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
2641	26.41	13.15	100.00	3.15	0.57	1.08	13.38	0.00	13.38	4.000	No	Yes	2.00
2642	26.42	13.26	100.00	3.14	0.57	1.08	13.49	0.00	13.49	4.000	No	Yes	2.00
2643	26.43	13.36	100.00	3.14	0.57	1.08	13.59	0.00	13.59	4.000	No	Yes	2.00
2644	26.44	13.45	100.00	3.14	0.57	1.08	13.68	0.00	13.68	4.000	No	Yes	2.00
2645	26.45	13.51	100.00	3.13	0.57	1.08	13.76	0.00	13.76	4.000	No	Yes	2.00
2646	26.46	13.54	100.00	3.13	0.57	1.08	13.78	0.00	13.78	4.000	No	Yes	2.00
2647	26.47	13.55	100.00	3.13	0.57	1.08	13.77	0.00	13.77	4.000	No	Yes	2.00
2648	26.48	13.55	100.00	3.13	0.57	1.08	13.77	0.00	13.77	4.000	No	Yes	2.00
2649	26.49	13.55	100.00	3.13	0.57	1.08	13.77	0.00	13.77	4.000	No	Yes	2.00
2650	26.50	13.55	100.00	3.13	0.57	1.08	13.77	0.00	13.77	4.000	No	Yes	2.00
2651	26.51	13.55	100.00	3.12	0.57	1.08	13.76	0.00	13.76	4.000	No	Yes	2.00
2652	26.52	13.55	100.00	3.12	0.57	1.08	13.76	0.00	13.76	4.000	No	Yes	2.00
2653	26.53	13.55	100.00	3.12	0.57	1.08	13.76	0.00	13.76	4.000	No	Yes	2.00
2654	26.54	13.56	100.00	3.12	0.57	1.08	13.76	0.00	13.76	4.000	No	Yes	2.00
2655	26.55	13.59	100.00	3.12	0.57	1.08	13.79	0.00	13.79	4.000	No	Yes	2.00
2656	26.56	13.63	100.00	3.12	0.57	1.07	13.83	0.00	13.83	4.000	No	Yes	2.00
2657	26.57	13.68	100.00	3.11	0.57	1.07	13.88	0.00	13.88	4.000	No	Yes	2.00
2658	26.58	13.73	100.00	3.11	0.57	1.07	13.93	0.00	13.93	4.000	No	Yes	2.00
2659	26.59	13.78	100.00	3.11	0.57	1.07	13.98	0.00	13.98	4.000	No	Yes	2.00
2660	26.60	13.84	100.00	3.11	0.57	1.07	14.04	0.00	14.04	4.000	No	Yes	2.00
2661	26.61	13.88	100.00	3.10	0.57	1.07	14.08	0.00	14.08	4.000	No	Yes	2.00
2662	26.62	13.91	100.00	3.10	0.57	1.07	14.12	0.00	14.12	4.000	No	Yes	2.00
2663	26.63	13.90	100.00	3.10	0.57	1.07	14.12	0.00	14.12	4.000	No	Yes	2.00
2664	26.64	13.85	100.00	3.10	0.57	1.07	14.04	0.00	14.04	4.000	No	Yes	2.00
2665	26.65	13.76	100.00	3.11	0.57	1.07	13.95	0.00	13.95	4.000	No	Yes	2.00
2666	26.66	13.65	100.00	3.11	0.57	1.07	13.84	0.00	13.84	4.000	No	Yes	2.00
2667	26.67	13.55	100.00	3.11	0.57	1.07	13.73	0.00	13.73	4.000	No	Yes	2.00
2668	26.68	13.44	100.00	3.12	0.57	1.07	13.62	0.00	13.62	4.000	No	Yes	2.00
2669	26.69	13.34	100.00	3.12	0.57	1.07	13.51	0.00	13.51	4.000	No	Yes	2.00
2670	26.70	13.25	100.00	3.12	0.57	1.07	13.42	0.00	13.42	4.000	No	Yes	2.00
2671	26.71	13.17	100.00	3.12	0.57	1.07	13.34	0.00	13.34	4.000	No	Yes	2.00
2672	26.72	13.07	100.00	3.13	0.57	1.07	13.25	0.00	13.25	4.000	No	Yes	2.00
2673	26.73	12.95	100.00	3.13	0.57	1.07	13.12	0.00	13.12	4.000	No	Yes	2.00
2674	26.74	12.81	100.00	3.14	0.57	1.07	12.98	0.00	12.98	4.000	No	Yes	2.00
2675	26.75	12.66	100.00	3.14	0.57	1.07	12.82	0.00	12.82	4.000	No	Yes	2.00
2676	26.76	12.50	100.00	3.14	0.57	1.07	12.65	0.00	12.65	4.000	No	Yes	2.00
2677	26.77	12.34	100.00	3.15	0.57	1.07	12.49	0.00	12.49	4.000	No	Yes	2.00
2678	26.78	12.19	100.00	3.15	0.57	1.07	12.34	0.00	12.34	4.000	No	Yes	2.00
2679	26.79	12.07	100.00	3.16	0.57	1.07	12.20	0.00	12.20	4.000	No	Yes	2.00
2680	26.80	11.99	100.00	3.16	0.57	1.07	12.10	0.00	12.10	4.000	No	Yes	2.00
2681	26.81	11.96	100.00	3.16	0.57	1.07	12.10	0.00	12.10	4.000	No	Yes	2.00
2682	26.82	11.96	100.00	3.16	0.57	1.07	12.10	0.00	12.10	4.000	No	Yes	2.00
2683	26.83	11.96	100.00	3.16	0.57	1.07	12.09	0.00	12.09	4.000	No	Yes	2.00
2684	26.84	11.95	100.00	3.16	0.57	1.07	12.09	0.00	12.09	4.000	No	Yes	2.00
2685	26.85	11.95	100.00	3.16	0.57	1.07	12.09	0.00	12.09	4.000	No	Yes	2.00
2686	26.86	11.95	100.00	3.16	0.57	1.07	12.09	0.00	12.09	4.000	No	Yes	2.00
2687	26.87	11.95	100.00	3.16	0.57	1.07	12.09	0.00	12.09	4.000	No	Yes	2.00
2688	26.88	11.98	100.00	3.15	0.57	1.07	12.08	0.00	12.08	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
2689	26.89	12.11	100.00	3.15	0.57	1.07	12.17	0.00	12.17	4.000	No	Yes	2.00
2690	26.90	12.35	100.00	3.14	0.57	1.07	12.45	0.00	12.45	4.000	No	Yes	2.00
2691	26.91	12.68	100.00	3.13	0.57	1.07	12.80	0.00	12.80	4.000	No	Yes	2.00
2692	26.92	13.06	100.00	3.12	0.57	1.07	13.18	0.00	13.18	4.000	No	Yes	2.00
2693	26.93	13.46	100.00	3.11	0.57	1.07	13.59	0.00	13.59	4.000	No	Yes	2.00
2694	26.94	13.86	100.00	3.09	0.57	1.07	13.99	0.00	13.99	4.000	No	Yes	2.00
2695	26.95	14.24	100.00	3.08	0.57	1.07	14.37	0.00	14.37	4.000	No	Yes	2.00
2696	26.96	14.57	100.00	3.07	0.56	1.07	14.72	0.00	14.72	4.000	No	Yes	2.00
2697	26.97	14.77	100.00	3.07	0.56	1.07	15.00	0.00	15.00	4.000	No	Yes	2.00
2698	26.98	14.79	100.00	3.07	0.56	1.07	14.96	0.00	14.96	4.000	No	Yes	2.00
2699	26.99	14.64	100.00	3.07	0.56	1.07	14.77	0.00	14.77	4.000	No	Yes	2.00
2700	27.00	14.43	100.00	3.08	0.57	1.07	14.55	0.00	14.55	4.000	No	Yes	2.00
2701	27.01	14.20	100.00	3.08	0.57	1.07	14.31	0.00	14.31	4.000	No	Yes	2.00
2702	27.02	13.96	100.00	3.09	0.57	1.07	14.06	0.00	14.06	4.000	No	Yes	2.00
2703	27.03	13.72	100.00	3.09	0.57	1.07	13.82	0.00	13.82	4.000	No	Yes	2.00
2704	27.04	13.50	100.00	3.10	0.57	1.07	13.59	0.00	13.59	4.000	No	Yes	2.00
2705	27.05	13.31	100.00	3.11	0.57	1.07	13.40	0.00	13.40	4.000	No	Yes	2.00
2706	27.06	13.08	100.00	3.11	0.57	1.07	13.24	0.00	13.24	4.000	No	Yes	2.00
2707	27.07	12.78	100.00	3.12	0.57	1.07	12.90	0.00	12.90	4.000	No	Yes	2.00
2708	27.08	12.37	100.00	3.14	0.57	1.07	12.48	0.00	12.48	4.000	No	Yes	2.00
2709	27.09	11.90	100.00	3.15	0.57	1.07	12.00	0.00	12.00	4.000	No	Yes	2.00
2710	27.10	11.40	100.00	3.17	0.58	1.07	11.49	0.00	11.49	4.000	No	Yes	2.00
2711	27.11	10.90	100.00	3.19	0.58	1.07	10.97	0.00	10.97	4.000	No	Yes	2.00
2712	27.12	10.41	100.00	3.21	0.58	1.07	10.47	0.00	10.47	4.000	No	Yes	2.00
2713	27.13	9.96	100.00	3.23	0.58	1.07	10.02	0.00	10.02	4.000	No	Yes	2.00
2714	27.14	9.63	100.00	3.25	0.58	1.07	9.63	0.00	9.63	4.000	No	Yes	2.00
2715	27.15	9.48	100.00	3.26	0.58	1.07	9.47	0.00	9.47	4.000	No	Yes	2.00
2716	27.16	9.50	100.00	3.26	0.58	1.07	9.56	0.00	9.56	4.000	No	Yes	2.00
2717	27.17	9.61	100.00	3.25	0.58	1.07	9.68	0.00	9.68	4.000	No	Yes	2.00
2718	27.18	9.74	100.00	3.25	0.58	1.07	9.80	0.00	9.80	4.000	No	Yes	2.00
2719	27.19	9.87	100.00	3.24	0.58	1.07	9.94	0.00	9.94	4.000	No	Yes	2.00
2720	27.20	10.00	100.00	3.24	0.58	1.07	10.07	0.00	10.07	4.000	No	Yes	2.00
2721	27.21	10.13	100.00	3.23	0.58	1.07	10.20	0.00	10.20	4.000	No	Yes	2.00
2722	27.22	10.24	100.00	3.23	0.58	1.07	10.31	0.00	10.31	4.000	No	Yes	2.00
2723	27.23	10.32	100.00	3.23	0.58	1.07	10.40	0.00	10.40	4.000	No	Yes	2.00
2724	27.24	10.35	100.00	3.23	0.58	1.07	10.42	0.00	10.42	4.000	No	Yes	2.00
2725	27.25	10.36	100.00	3.23	0.58	1.07	10.42	0.00	10.42	4.000	No	Yes	2.00
2726	27.26	10.36	100.00	3.23	0.58	1.06	10.42	0.00	10.42	4.000	No	Yes	2.00
2727	27.27	10.36	100.00	3.23	0.58	1.06	10.42	0.00	10.42	4.000	No	Yes	2.00
2728	27.28	10.36	100.00	3.23	0.58	1.06	10.42	0.00	10.42	4.000	No	Yes	2.00
2729	27.29	10.36	100.00	3.23	0.58	1.06	10.41	0.00	10.41	4.000	No	Yes	2.00
2730	27.30	10.36	100.00	3.23	0.58	1.06	10.41	0.00	10.41	4.000	No	Yes	2.00
2731	27.31	10.36	100.00	3.23	0.58	1.06	10.41	0.00	10.41	4.000	No	Yes	2.00
2732	27.32	10.36	100.00	3.23	0.58	1.06	10.41	0.00	10.41	4.000	No	Yes	2.00
2733	27.33	10.36	100.00	3.23	0.58	1.06	10.41	0.00	10.41	4.000	No	Yes	2.00
2734	27.34	10.36	100.00	3.23	0.58	1.06	10.41	0.00	10.41	4.000	No	Yes	2.00
2735	27.35	10.36	100.00	3.23	0.58	1.06	10.40	0.00	10.40	4.000	No	Yes	2.00
2736	27.36	10.36	100.00	3.23	0.58	1.06	10.40	0.00	10.40	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
2737	27.37	10.36	100.00	3.23	0.58	1.06	10.40	0.00	10.40	4.000	No	Yes	2.00
2738	27.38	10.36	100.00	3.23	0.58	1.06	10.40	0.00	10.40	4.000	No	Yes	2.00
2739	27.39	10.36	100.00	3.23	0.58	1.06	10.40	0.00	10.40	4.000	No	Yes	2.00
2740	27.40	10.39	100.00	3.23	0.58	1.06	10.40	0.00	10.40	4.000	No	Yes	2.00
2741	27.41	10.50	100.00	3.22	0.58	1.06	10.48	0.00	10.48	4.000	No	Yes	2.00
2742	27.42	10.71	100.00	3.21	0.58	1.06	10.73	0.00	10.73	4.000	No	Yes	2.00
2743	27.43	11.01	100.00	3.20	0.58	1.06	11.03	0.00	11.03	4.000	No	Yes	2.00
2744	27.44	11.34	100.00	3.19	0.58	1.06	11.36	0.00	11.36	4.000	No	Yes	2.00
2745	27.45	11.68	100.00	3.18	0.58	1.06	11.71	0.00	11.71	4.000	No	Yes	2.00
2746	27.46	12.03	100.00	3.16	0.57	1.06	12.06	0.00	12.06	4.000	No	Yes	2.00
2747	27.47	12.35	100.00	3.15	0.57	1.06	12.39	0.00	12.39	4.000	No	Yes	2.00
2748	27.48	12.64	100.00	3.14	0.57	1.06	12.68	0.00	12.68	4.000	No	Yes	2.00
2749	27.49	12.89	100.00	3.14	0.57	1.06	12.92	0.00	12.92	4.000	No	Yes	2.00
2750	27.50	13.13	100.00	3.13	0.57	1.06	13.12	0.00	13.12	4.000	No	Yes	2.00
2751	27.51	13.40	100.00	3.12	0.57	1.06	13.39	0.00	13.39	4.000	No	Yes	2.00
2752	27.52	13.71	100.00	3.11	0.57	1.06	13.70	0.00	13.70	4.000	No	Yes	2.00
2753	27.53	14.05	100.00	3.11	0.57	1.06	14.04	0.00	14.04	4.000	No	Yes	2.00
2754	27.54	14.39	100.00	3.10	0.57	1.06	14.39	0.00	14.39	4.000	No	Yes	2.00
2755	27.55	14.73	100.00	3.09	0.56	1.06	14.73	0.00	14.73	4.000	No	Yes	2.00
2756	27.56	15.05	100.00	3.08	0.56	1.06	15.05	0.00	15.05	4.000	No	Yes	2.00
2757	27.57	15.31	100.00	3.08	0.56	1.06	15.32	0.00	15.32	4.000	No	Yes	2.00
2758	27.58	15.39	100.00	3.07	0.56	1.06	15.50	0.00	15.50	4.000	No	Yes	2.00
2759	27.59	15.28	100.00	3.08	0.56	1.06	15.27	0.00	15.27	4.000	No	Yes	2.00
2760	27.60	14.99	100.00	3.09	0.56	1.06	14.98	0.00	14.98	4.000	No	Yes	2.00
2761	27.61	14.67	100.00	3.10	0.56	1.06	14.66	0.00	14.66	4.000	No	Yes	2.00
2762	27.62	14.33	100.00	3.11	0.57	1.06	14.31	0.00	14.31	4.000	No	Yes	2.00
2763	27.63	13.98	100.00	3.12	0.57	1.06	13.96	0.00	13.96	4.000	No	Yes	2.00
2764	27.64	13.65	100.00	3.13	0.57	1.06	13.62	0.00	13.62	4.000	No	Yes	2.00
2765	27.65	13.35	100.00	3.14	0.57	1.06	13.31	0.00	13.31	4.000	No	Yes	2.00
2766	27.66	13.08	100.00	3.15	0.57	1.06	13.05	0.00	13.05	4.000	No	Yes	2.00
2767	27.67	12.79	100.00	3.16	0.57	1.06	12.81	0.00	12.81	4.000	No	Yes	2.00
2768	27.68	12.46	100.00	3.18	0.57	1.06	12.46	0.00	12.46	4.000	No	Yes	2.00
2769	27.69	12.05	100.00	3.19	0.57	1.06	12.04	0.00	12.04	4.000	No	Yes	2.00
2770	27.70	11.59	100.00	3.21	0.58	1.06	11.58	0.00	11.58	4.000	No	Yes	2.00
2771	27.71	11.11	100.00	3.23	0.58	1.06	11.09	0.00	11.09	4.000	No	Yes	2.00
2772	27.72	10.63	100.00	3.25	0.58	1.06	10.61	0.00	10.61	4.000	No	Yes	2.00
2773	27.73	10.18	100.00	3.27	0.58	1.06	10.15	0.00	10.15	4.000	No	Yes	2.00
2774	27.74	9.79	100.00	3.29	0.58	1.06	9.74	0.00	9.74	4.000	No	Yes	2.00
2775	27.75	9.52	100.00	3.31	0.58	1.06	9.41	0.00	9.41	4.000	No	Yes	2.00
2776	27.76	9.39	100.00	3.31	0.58	1.06	9.35	0.00	9.35	4.000	No	Yes	2.00
2777	27.77	9.37	100.00	3.32	0.58	1.06	9.35	0.00	9.35	4.000	No	Yes	2.00
2778	27.78	9.37	100.00	3.32	0.58	1.06	9.34	0.00	9.34	4.000	No	Yes	2.00
2779	27.79	9.37	100.00	3.32	0.58	1.06	9.34	0.00	9.34	4.000	No	Yes	2.00
2780	27.80	9.37	100.00	3.32	0.58	1.06	9.34	0.00	9.34	4.000	No	Yes	2.00
2781	27.81	9.37	100.00	3.32	0.58	1.06	9.34	0.00	9.34	4.000	No	Yes	2.00
2782	27.82	9.37	100.00	3.32	0.58	1.06	9.34	0.00	9.34	4.000	No	Yes	2.00
2783	27.83	9.37	100.00	3.32	0.58	1.06	9.34	0.00	9.34	4.000	No	Yes	2.00
2784	27.84	9.44	100.00	3.32	0.58	1.06	9.35	0.00	9.35	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
2785	27.85	9.59	100.00	3.31	0.58	1.06	9.54	0.00	9.54	4.000	No	Yes	2.00
2786	27.86	9.81	100.00	3.30	0.58	1.06	9.77	0.00	9.77	4.000	No	Yes	2.00
2787	27.87	10.07	100.00	3.29	0.58	1.06	10.03	0.00	10.03	4.000	No	Yes	2.00
2788	27.88	10.35	100.00	3.28	0.58	1.05	10.31	0.00	10.31	4.000	No	Yes	2.00
2789	27.89	10.63	100.00	3.27	0.58	1.05	10.59	0.00	10.59	4.000	No	Yes	2.00
2790	27.90	10.90	100.00	3.26	0.58	1.05	10.86	0.00	10.86	4.000	No	Yes	2.00
2791	27.91	11.14	100.00	3.25	0.58	1.05	11.10	0.00	11.10	4.000	No	Yes	2.00
2792	27.92	11.34	100.00	3.24	0.58	1.05	11.31	0.00	11.31	4.000	No	Yes	2.00
2793	27.93	11.49	100.00	3.23	0.58	1.05	11.44	0.00	11.44	4.000	No	Yes	2.00
2794	27.94	11.61	100.00	3.23	0.58	1.05	11.54	0.00	11.54	4.000	No	Yes	2.00
2795	27.95	11.74	100.00	3.22	0.58	1.05	11.67	0.00	11.67	4.000	No	Yes	2.00
2796	27.96	11.88	100.00	3.22	0.58	1.05	11.81	0.00	11.81	4.000	No	Yes	2.00
2797	27.97	12.02	100.00	3.21	0.57	1.05	11.95	0.00	11.95	4.000	No	Yes	2.00
2798	27.98	12.17	100.00	3.21	0.57	1.05	12.10	0.00	12.10	4.000	No	Yes	2.00
2799	27.99	12.31	100.00	3.20	0.57	1.05	12.23	0.00	12.23	4.000	No	Yes	2.00
2800	28.00	12.43	100.00	3.20	0.57	1.05	12.35	0.00	12.35	4.000	No	Yes	2.00
2801	28.01	12.48	100.00	3.19	0.57	1.05	12.45	0.00	12.45	4.000	No	Yes	2.00
2802	28.02	12.46	100.00	3.19	0.57	1.05	12.39	0.00	12.39	4.000	No	Yes	2.00
2803	28.03	12.36	100.00	3.19	0.57	1.05	12.28	0.00	12.28	4.000	No	Yes	2.00
2804	28.04	12.23	100.00	3.20	0.57	1.05	12.14	0.00	12.14	4.000	No	Yes	2.00
2805	28.05	12.08	100.00	3.20	0.57	1.05	12.00	0.00	12.00	4.000	No	Yes	2.00
2806	28.06	11.94	100.00	3.21	0.58	1.05	11.85	0.00	11.85	4.000	No	Yes	2.00
2807	28.07	11.79	100.00	3.21	0.58	1.05	11.70	0.00	11.70	4.000	No	Yes	2.00
2808	28.08	11.66	100.00	3.21	0.58	1.05	11.57	0.00	11.57	4.000	No	Yes	2.00
2809	28.09	11.55	100.00	3.22	0.58	1.05	11.45	0.00	11.45	4.000	No	Yes	2.00
2810	28.10	11.44	100.00	3.22	0.58	1.05	11.36	0.00	11.36	4.000	No	Yes	2.00
2811	28.11	11.34	100.00	3.22	0.58	1.05	11.26	0.00	11.26	4.000	No	Yes	2.00
2812	28.12	11.22	100.00	3.23	0.58	1.05	11.14	0.00	11.14	4.000	No	Yes	2.00
2813	28.13	11.08	100.00	3.23	0.58	1.05	11.00	0.00	11.00	4.000	No	Yes	2.00
2814	28.14	10.94	100.00	3.23	0.58	1.05	10.85	0.00	10.85	4.000	No	Yes	2.00
2815	28.15	10.79	100.00	3.24	0.58	1.05	10.70	0.00	10.70	4.000	No	Yes	2.00
2816	28.16	10.65	100.00	3.24	0.58	1.05	10.56	0.00	10.56	4.000	No	Yes	2.00
2817	28.17	10.52	100.00	3.25	0.58	1.05	10.43	0.00	10.43	4.000	No	Yes	2.00
2818	28.18	10.46	100.00	3.25	0.58	1.05	10.32	0.00	10.32	4.000	No	Yes	2.00
2819	28.19	10.53	100.00	3.24	0.58	1.05	10.37	0.00	10.37	4.000	No	Yes	2.00
2820	28.20	10.73	100.00	3.23	0.58	1.05	10.62	0.00	10.62	4.000	No	Yes	2.00
2821	28.21	11.03	100.00	3.22	0.58	1.05	10.92	0.00	10.92	4.000	No	Yes	2.00
2822	28.22	11.36	100.00	3.21	0.58	1.05	11.25	0.00	11.25	4.000	No	Yes	2.00
2823	28.23	11.71	100.00	3.19	0.58	1.05	11.59	0.00	11.59	4.000	No	Yes	2.00
2824	28.24	12.05	100.00	3.18	0.57	1.05	11.94	0.00	11.94	4.000	No	Yes	2.00
2825	28.25	12.37	100.00	3.16	0.57	1.05	12.26	0.00	12.26	4.000	No	Yes	2.00
2826	28.26	12.66	100.00	3.15	0.57	1.05	12.55	0.00	12.55	4.000	No	Yes	2.00
2827	28.27	12.85	100.00	3.15	0.57	1.05	12.78	0.00	12.78	4.000	No	Yes	2.00
2828	28.28	12.94	100.00	3.14	0.57	1.05	12.81	0.00	12.81	4.000	No	Yes	2.00
2829	28.29	12.95	100.00	3.14	0.57	1.05	12.81	0.00	12.81	4.000	No	Yes	2.00
2830	28.30	12.95	100.00	3.14	0.57	1.05	12.81	0.00	12.81	4.000	No	Yes	2.00
2831	28.31	12.95	100.00	3.14	0.57	1.05	12.81	0.00	12.81	4.000	No	Yes	2.00
2832	28.32	12.95	100.00	3.14	0.57	1.05	12.80	0.00	12.80	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
2833	28.33	12.95	100.00	3.14	0.57	1.05	12.80	0.00	12.80	4.000	No	Yes	2.00
2834	28.34	12.95	100.00	3.13	0.57	1.05	12.80	0.00	12.80	4.000	No	Yes	2.00
2835	28.35	12.94	100.00	3.13	0.57	1.05	12.80	0.00	12.80	4.000	No	Yes	2.00
2836	28.36	12.82	100.00	3.14	0.57	1.05	12.76	0.00	12.76	4.000	No	Yes	2.00
2837	28.37	12.58	100.00	3.15	0.57	1.05	12.45	0.00	12.45	4.000	No	Yes	2.00
2838	28.38	12.21	100.00	3.16	0.57	1.05	12.08	0.00	12.08	4.000	No	Yes	2.00
2839	28.39	11.78	100.00	3.17	0.58	1.05	11.65	0.00	11.65	4.000	No	Yes	2.00
2840	28.40	11.34	100.00	3.19	0.58	1.05	11.20	0.00	11.20	4.000	No	Yes	2.00
2841	28.41	10.88	100.00	3.21	0.58	1.05	10.74	0.00	10.74	4.000	No	Yes	2.00
2842	28.42	10.45	100.00	3.23	0.58	1.05	10.31	0.00	10.31	4.000	No	Yes	2.00
2843	28.43	10.06	100.00	3.25	0.58	1.05	9.91	0.00	9.91	4.000	No	Yes	2.00
2844	28.44	9.76	100.00	3.26	0.58	1.05	9.58	0.00	9.58	4.000	No	Yes	2.00
2845	28.45	9.56	100.00	3.27	0.58	1.05	9.41	0.00	9.41	4.000	No	Yes	2.00
2846	28.46	9.45	100.00	3.28	0.58	1.05	9.34	0.00	9.34	4.000	No	Yes	2.00
2847	28.47	9.36	100.00	3.28	0.59	1.05	9.24	0.00	9.24	4.000	No	Yes	2.00
2848	28.48	9.25	100.00	3.29	0.59	1.05	9.14	0.00	9.14	4.000	No	Yes	2.00
2849	28.49	9.15	100.00	3.30	0.59	1.05	9.03	0.00	9.03	4.000	No	Yes	2.00
2850	28.50	9.04	100.00	3.30	0.59	1.05	8.92	0.00	8.92	4.000	No	Yes	2.00
2851	28.51	8.94	100.00	3.31	0.59	1.05	8.82	0.00	8.82	4.000	No	Yes	2.00
2852	28.52	8.85	100.00	3.31	0.59	1.05	8.73	0.00	8.73	4.000	No	Yes	2.00
2853	28.53	8.80	100.00	3.32	0.59	1.04	8.66	0.00	8.66	4.000	No	Yes	2.00
2854	28.54	8.77	100.00	3.32	0.59	1.04	8.65	0.00	8.65	4.000	No	Yes	2.00
2855	28.55	8.77	100.00	3.32	0.59	1.04	8.65	0.00	8.65	4.000	No	Yes	2.00
2856	28.56	8.77	100.00	3.32	0.59	1.04	8.65	0.00	8.65	4.000	No	Yes	2.00
2857	28.57	8.77	100.00	3.32	0.59	1.04	8.65	0.00	8.65	4.000	No	Yes	2.00
2858	28.58	8.77	100.00	3.32	0.59	1.04	8.64	0.00	8.64	4.000	No	Yes	2.00
2859	28.59	8.77	100.00	3.32	0.59	1.04	8.64	0.00	8.64	4.000	No	Yes	2.00
2860	28.60	8.77	100.00	3.32	0.59	1.04	8.64	0.00	8.64	4.000	No	Yes	2.00
2861	28.61	8.76	100.00	3.32	0.59	1.04	8.64	0.00	8.64	4.000	No	Yes	2.00
2862	28.62	8.74	100.00	3.32	0.59	1.04	8.63	0.00	8.63	4.000	No	Yes	2.00
2863	28.63	8.68	100.00	3.33	0.59	1.04	8.56	0.00	8.56	4.000	No	Yes	2.00
2864	28.64	8.59	100.00	3.33	0.59	1.04	8.47	0.00	8.47	4.000	No	Yes	2.00
2865	28.65	8.49	100.00	3.34	0.59	1.04	8.37	0.00	8.37	4.000	No	Yes	2.00
2866	28.66	8.38	100.00	3.34	0.59	1.04	8.26	0.00	8.26	4.000	No	Yes	2.00
2867	28.67	8.28	100.00	3.35	0.59	1.04	8.15	0.00	8.15	4.000	No	Yes	2.00
2868	28.68	8.18	100.00	3.36	0.59	1.04	8.05	0.00	8.05	4.000	No	Yes	2.00
2869	28.69	8.08	100.00	3.36	0.59	1.04	7.96	0.00	7.96	4.000	No	Yes	2.00
2870	28.70	8.03	100.00	3.36	0.59	1.04	7.88	0.00	7.88	4.000	No	Yes	2.00
2871	28.71	8.04	100.00	3.36	0.59	1.04	7.89	0.00	7.89	4.000	No	Yes	2.00
2872	28.72	8.12	100.00	3.36	0.59	1.04	7.98	0.00	7.98	4.000	No	Yes	2.00
2873	28.73	8.23	100.00	3.35	0.59	1.04	8.10	0.00	8.10	4.000	No	Yes	2.00
2874	28.74	8.36	100.00	3.35	0.59	1.04	8.22	0.00	8.22	4.000	No	Yes	2.00
2875	28.75	8.49	100.00	3.34	0.59	1.04	8.36	0.00	8.36	4.000	No	Yes	2.00
2876	28.76	8.63	100.00	3.34	0.59	1.04	8.49	0.00	8.49	4.000	No	Yes	2.00
2877	28.77	8.75	100.00	3.33	0.59	1.04	8.61	0.00	8.61	4.000	No	Yes	2.00
2878	28.78	8.86	100.00	3.32	0.59	1.04	8.72	0.00	8.72	4.000	No	Yes	2.00
2879	28.79	8.99	100.00	3.32	0.59	1.04	8.80	0.00	8.80	4.000	No	Yes	2.00
2880	28.80	9.16	100.00	3.31	0.59	1.04	8.99	0.00	8.99	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
2881	28.81	9.41	100.00	3.30	0.59	1.04	9.23	0.00	9.23	4.000	No	Yes	2.00
2882	28.82	9.70	100.00	3.28	0.58	1.04	9.52	0.00	9.52	4.000	No	Yes	2.00
2883	28.83	10.01	100.00	3.27	0.58	1.04	9.83	0.00	9.83	4.000	No	Yes	2.00
2884	28.84	10.33	100.00	3.26	0.58	1.04	10.15	0.00	10.15	4.000	No	Yes	2.00
2885	28.85	10.64	100.00	3.24	0.58	1.04	10.46	0.00	10.46	4.000	No	Yes	2.00
2886	28.86	10.93	100.00	3.23	0.58	1.04	10.74	0.00	10.74	4.000	No	Yes	2.00
2887	28.87	11.18	100.00	3.22	0.58	1.04	10.99	0.00	10.99	4.000	No	Yes	2.00
2888	28.88	11.38	100.00	3.21	0.58	1.04	11.17	0.00	11.17	4.000	No	Yes	2.00
2889	28.89	11.56	100.00	3.20	0.58	1.04	11.33	0.00	11.33	4.000	No	Yes	2.00
2890	28.90	11.76	100.00	3.20	0.58	1.04	11.53	0.00	11.53	4.000	No	Yes	2.00
2891	28.91	11.99	100.00	3.19	0.58	1.04	11.75	0.00	11.75	4.000	No	Yes	2.00
2892	28.92	12.22	100.00	3.18	0.57	1.04	11.98	0.00	11.98	4.000	No	Yes	2.00
2893	28.93	12.46	100.00	3.17	0.57	1.04	12.22	0.00	12.22	4.000	No	Yes	2.00
2894	28.94	12.69	100.00	3.16	0.57	1.04	12.45	0.00	12.45	4.000	No	Yes	2.00
2895	28.95	12.90	100.00	3.15	0.57	1.04	12.65	0.00	12.65	4.000	No	Yes	2.00
2896	28.96	13.09	100.00	3.14	0.57	1.04	12.82	0.00	12.82	4.000	No	Yes	2.00
2897	28.97	13.32	100.00	3.13	0.57	1.04	13.01	0.00	13.01	4.000	No	Yes	2.00
2898	28.98	13.60	100.00	3.12	0.57	1.04	13.30	0.00	13.30	4.000	No	Yes	2.00
2899	28.99	13.95	100.00	3.11	0.57	1.04	13.64	0.00	13.64	4.000	No	Yes	2.00
2900	29.00	14.33	100.00	3.09	0.57	1.04	14.02	0.00	14.02	4.000	No	Yes	2.00
2901	29.01	14.73	100.00	3.08	0.57	1.04	14.42	0.00	14.42	4.000	No	Yes	2.00
2902	29.02	15.13	100.00	3.07	0.56	1.04	14.81	0.00	14.81	4.000	No	Yes	2.00
2903	29.03	15.50	100.00	3.06	0.56	1.04	15.17	0.00	15.17	4.000	No	Yes	2.00
2904	29.04	15.82	100.00	3.05	0.56	1.04	15.49	0.00	15.49	4.000	No	Yes	2.00
2905	29.05	16.12	100.00	3.04	0.56	1.04	15.75	0.00	15.75	4.000	No	Yes	2.00
2906	29.06	16.44	100.00	3.03	0.56	1.04	16.04	0.00	16.04	4.000	No	Yes	2.00
2907	29.07	16.81	100.00	3.02	0.56	1.03	16.41	0.00	16.41	4.000	No	Yes	2.00
2908	29.08	17.25	100.00	3.00	0.56	1.03	16.84	0.00	16.84	4.000	No	Yes	2.00
2909	29.09	17.72	100.00	2.99	0.56	1.03	17.30	0.00	17.30	4.000	No	Yes	2.00
2910	29.10	18.20	100.00	2.98	0.55	1.03	17.78	0.00	17.78	4.000	No	Yes	2.00
2911	29.11	18.67	100.00	2.97	0.55	1.03	18.24	0.00	18.24	4.000	No	Yes	2.00
2912	29.12	19.09	99.67	2.96	0.55	1.03	18.66	0.00	18.66	4.000	No	Yes	2.00
2913	29.13	19.45	98.99	2.95	0.55	1.03	19.02	0.00	19.02	4.000	No	Yes	2.00
2914	29.14	19.72	98.48	2.94	0.55	1.03	19.27	0.00	19.27	4.000	No	Yes	2.00
2915	29.15	19.93	98.07	2.94	0.55	1.03	19.43	0.00	19.43	4.000	No	Yes	2.00
2916	29.16	20.13	97.69	2.93	0.55	1.03	19.63	0.00	19.63	4.000	No	Yes	2.00
2917	29.17	20.36	97.25	2.93	0.55	1.03	19.85	0.00	19.85	4.000	No	Yes	2.00
2918	29.18	20.60	96.79	2.92	0.55	1.03	20.08	0.00	20.08	4.000	No	Yes	2.00
2919	29.19	20.83	96.34	2.92	0.55	1.03	20.31	0.00	20.31	4.000	No	Yes	2.00
2920	29.20	21.06	95.91	2.91	0.54	1.03	20.54	0.00	20.54	4.000	No	Yes	2.00
2921	29.21	21.27	95.53	2.91	0.54	1.03	20.74	0.00	20.74	4.000	No	Yes	2.00
2922	29.22	21.41	95.27	2.90	0.54	1.03	20.90	0.00	20.90	4.000	No	Yes	2.00
2923	29.23	21.46	95.19	2.90	0.54	1.03	20.93	0.00	20.93	4.000	No	Yes	2.00
2924	29.24	21.42	95.27	2.90	0.54	1.03	20.87	0.00	20.87	4.000	No	Yes	2.00
2925	29.25	21.36	95.43	2.91	0.54	1.03	20.80	0.00	20.80	4.000	No	Yes	2.00
2926	29.26	21.28	95.60	2.91	0.54	1.03	20.72	0.00	20.72	4.000	No	Yes	2.00
2927	29.27	21.20	95.77	2.91	0.54	1.03	20.64	0.00	20.64	4.000	No	Yes	2.00
2928	29.28	21.12	95.95	2.91	0.54	1.03	20.56	0.00	20.56	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
2929	29.29	21.05	96.11	2.91	0.55	1.03	20.48	0.00	20.48	4.000	No	Yes	2.00
2930	29.30	20.98	96.25	2.92	0.55	1.03	20.41	0.00	20.41	4.000	No	Yes	2.00
2931	29.31	20.95	96.32	2.92	0.55	1.03	20.36	0.00	20.36	4.000	No	Yes	2.00
2932	29.32	20.97	96.29	2.92	0.55	1.03	20.40	0.00	20.40	4.000	No	Yes	2.00
2933	29.33	21.03	96.18	2.91	0.55	1.03	20.46	0.00	20.46	4.000	No	Yes	2.00
2934	29.34	21.11	96.04	2.91	0.54	1.03	20.52	0.00	20.52	4.000	No	Yes	2.00
2935	29.35	21.18	95.90	2.91	0.54	1.03	20.60	0.00	20.60	4.000	No	Yes	2.00
2936	29.36	21.26	95.74	2.91	0.54	1.03	20.67	0.00	20.67	4.000	No	Yes	2.00
2937	29.37	21.34	95.60	2.91	0.54	1.03	20.75	0.00	20.75	4.000	No	Yes	2.00
2938	29.38	21.41	95.46	2.91	0.54	1.03	20.82	0.00	20.82	4.000	No	Yes	2.00
2939	29.39	21.49	95.31	2.90	0.54	1.03	20.87	0.00	20.87	4.000	No	Yes	2.00
2940	29.40	21.66	94.99	2.90	0.54	1.03	20.97	0.00	20.97	4.000	No	Yes	2.00
2941	29.41	21.94	94.44	2.89	0.54	1.03	21.29	0.00	21.29	4.000	No	Yes	2.00
2942	29.42	22.34	93.68	2.88	0.54	1.03	21.68	0.00	21.68	4.000	No	Yes	2.00
2943	29.43	22.79	92.82	2.87	0.54	1.03	22.12	0.00	22.12	4.000	No	Yes	2.00
2944	29.44	23.27	91.93	2.86	0.54	1.03	22.59	0.00	22.59	4.000	No	Yes	2.00
2945	29.45	23.75	91.05	2.85	0.54	1.03	23.06	0.00	23.06	4.000	No	Yes	2.00
2946	29.46	24.20	90.21	2.84	0.54	1.03	23.50	0.00	23.50	4.000	No	Yes	2.00
2947	29.47	24.61	89.47	2.83	0.54	1.03	23.90	0.00	23.90	4.000	No	Yes	2.00
2948	29.48	24.97	88.87	2.82	0.53	1.03	24.24	0.00	24.24	4.000	No	Yes	2.00
2949	29.49	25.30	88.35	2.82	0.53	1.03	24.51	0.00	24.51	4.000	No	Yes	2.00
2950	29.50	25.66	87.84	2.81	0.53	1.03	24.86	0.00	24.86	4.000	No	Yes	2.00
2951	29.51	26.08	87.27	2.80	0.53	1.03	25.27	0.00	25.27	4.000	No	Yes	2.00
2952	29.52	26.54	86.65	2.80	0.53	1.03	25.72	0.00	25.72	4.000	No	Yes	2.00
2953	29.53	27.02	86.02	2.79	0.53	1.03	26.19	0.00	26.19	4.000	No	Yes	2.00
2954	29.54	27.49	85.41	2.78	0.53	1.03	26.65	0.00	26.65	4.000	No	Yes	2.00
2955	29.55	27.94	84.84	2.77	0.53	1.03	27.08	0.00	27.08	4.000	No	Yes	2.00
2956	29.56	28.32	84.36	2.77	0.53	1.03	27.46	0.00	27.46	4.000	No	Yes	2.00
2957	29.57	28.60	84.04	2.76	0.52	1.03	27.76	0.00	27.76	4.000	No	Yes	2.00
2958	29.58	28.79	83.87	2.76	0.52	1.03	27.86	0.00	27.86	4.000	No	Yes	2.00
2959	29.59	28.92	83.81	2.76	0.52	1.02	27.99	0.00	27.99	4.000	No	Yes	2.00
2960	29.60	29.06	83.76	2.76	0.52	1.02	28.12	0.00	28.12	4.000	No	Yes	2.00
2961	29.61	29.22	83.69	2.76	0.52	1.02	28.27	0.00	28.27	4.000	No	Yes	2.00
2962	29.62	29.38	83.63	2.76	0.52	1.02	28.43	0.00	28.43	4.000	No	Yes	2.00
2963	29.63	29.54	83.57	2.76	0.52	1.02	28.57	0.00	28.57	4.000	No	Yes	2.00
2964	29.64	29.68	83.51	2.76	0.52	1.02	28.71	0.00	28.71	4.000	No	Yes	2.00
2965	29.65	29.78	83.49	2.76	0.52	1.02	28.83	0.00	28.83	4.000	No	Yes	2.00
2966	29.66	29.78	83.61	2.76	0.52	1.02	28.85	0.00	28.85	4.000	No	Yes	2.00
2967	29.67	29.66	83.87	2.76	0.52	1.02	28.69	0.00	28.69	4.000	No	Yes	2.00
2968	29.68	29.46	84.28	2.77	0.52	1.02	28.49	0.00	28.49	4.000	No	Yes	2.00
2969	29.69	29.24	84.73	2.77	0.52	1.02	28.26	0.00	28.26	4.000	No	Yes	2.00
2970	29.70	29.00	85.20	2.78	0.52	1.02	28.02	0.00	28.02	4.000	No	Yes	2.00
2971	29.71	28.76	85.68	2.78	0.52	1.02	27.79	0.00	27.79	4.000	No	Yes	2.00
2972	29.72	28.53	86.14	2.79	0.52	1.02	27.56	0.00	27.56	4.000	No	Yes	2.00
2973	29.73	28.33	86.55	2.79	0.53	1.02	27.35	0.00	27.35	4.000	No	Yes	2.00
2974	29.74	28.12	86.96	2.80	0.53	1.02	27.18	0.00	27.18	4.000	No	Yes	2.00
2975	29.75	27.87	87.49	2.81	0.53	1.02	26.95	0.00	26.95	4.000	No	Yes	2.00
2976	29.76	27.53	88.21	2.82	0.53	1.02	26.60	0.00	26.60	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
2977	29.77	27.10	89.08	2.83	0.53	1.02	26.18	0.00	26.18	4.000	No	Yes	2.00
2978	29.78	26.64	90.05	2.84	0.53	1.02	25.72	0.00	25.72	4.000	No	Yes	2.00
2979	29.79	26.16	91.05	2.85	0.53	1.02	25.25	0.00	25.25	4.000	No	Yes	2.00
2980	29.80	25.69	92.04	2.86	0.53	1.02	24.78	0.00	24.78	4.000	No	Yes	2.00
2981	29.81	25.25	92.97	2.87	0.53	1.02	24.35	0.00	24.35	4.000	No	Yes	2.00
2982	29.82	24.86	93.78	2.88	0.53	1.02	23.96	0.00	23.96	4.000	No	Yes	2.00
2983	29.83	24.69	94.25	2.89	0.53	1.02	23.66	0.00	23.66	4.000	No	Yes	2.00
2984	29.84	24.73	94.38	2.89	0.53	1.02	23.83	0.00	23.83	4.000	No	Yes	2.00
2985	29.85	24.98	94.23	2.89	0.53	1.02	24.08	0.00	24.08	4.000	No	Yes	2.00
2986	29.86	25.27	94.04	2.89	0.53	1.02	24.36	0.00	24.36	4.000	No	Yes	2.00
2987	29.87	25.58	93.84	2.89	0.53	1.02	24.66	0.00	24.66	4.000	No	Yes	2.00
2988	29.88	25.90	93.64	2.88	0.53	1.02	24.97	0.00	24.97	4.000	No	Yes	2.00
2989	29.89	26.21	93.46	2.88	0.53	1.02	25.27	0.00	25.27	4.000	No	Yes	2.00
2990	29.90	26.50	93.29	2.88	0.53	1.02	25.54	0.00	25.54	4.000	No	Yes	2.00
2991	29.91	26.75	93.12	2.88	0.53	1.02	25.78	0.00	25.78	4.000	No	Yes	2.00
2992	29.92	27.05	92.84	2.87	0.53	1.02	26.00	0.00	26.00	4.000	No	Yes	2.00
2993	29.93	27.42	92.40	2.87	0.53	1.02	26.37	0.00	26.37	4.000	No	Yes	2.00
2994	29.94	27.89	91.80	2.86	0.53	1.02	26.83	0.00	26.83	4.000	No	Yes	2.00
2995	29.95	28.41	91.14	2.85	0.52	1.02	27.34	0.00	27.34	4.000	No	Yes	2.00
2996	29.96	28.97	90.45	2.84	0.52	1.02	27.88	0.00	27.88	4.000	No	Yes	2.00
2997	29.97	29.53	89.78	2.83	0.52	1.02	28.42	0.00	28.42	4.000	No	Yes	2.00
2998	29.98	30.06	89.14	2.83	0.52	1.02	28.94	0.00	28.94	4.000	No	Yes	2.00
2999	29.99	30.53	88.58	2.82	0.52	1.02	29.40	0.00	29.40	4.000	No	Yes	2.00
3000	30.00	30.85	88.24	2.82	0.52	1.02	29.78	0.00	29.78	4.000	No	Yes	2.00
3001	30.01	30.96	88.18	2.81	0.52	1.02	29.83	0.00	29.83	4.000	No	Yes	2.00
3002	30.02	30.89	88.37	2.82	0.52	1.02	29.70	0.00	29.70	4.000	No	Yes	2.00
3003	30.03	30.75	88.68	2.82	0.52	1.02	29.56	0.00	29.56	4.000	No	Yes	2.00
3004	30.04	30.60	89.02	2.83	0.52	1.02	29.41	0.00	29.41	4.000	No	Yes	2.00
3005	30.05	30.44	89.37	2.83	0.52	1.02	29.25	0.00	29.25	4.000	No	Yes	2.00
3006	30.06	30.28	89.71	2.83	0.52	1.02	29.09	0.00	29.09	4.000	No	Yes	2.00
3007	30.07	30.13	90.03	2.84	0.52	1.02	28.94	0.00	28.94	4.000	No	Yes	2.00
3008	30.08	30.00	90.31	2.84	0.52	1.02	28.81	0.00	28.81	4.000	No	Yes	2.00
3009	30.09	29.94	90.49	2.84	0.52	1.02	28.71	0.00	28.71	4.000	No	Yes	2.00
3010	30.10	29.94	90.57	2.84	0.52	1.02	28.75	0.00	28.75	4.000	No	Yes	2.00
3011	30.11	30.01	90.57	2.84	0.52	1.02	28.81	0.00	28.81	4.000	No	Yes	2.00
3012	30.12	30.08	90.58	2.84	0.52	1.02	28.87	0.00	28.87	4.000	No	Yes	2.00
3013	30.13	30.16	90.58	2.84	0.52	1.02	28.95	0.00	28.95	4.000	No	Yes	2.00
3014	30.14	30.24	90.59	2.84	0.52	1.02	29.02	0.00	29.02	4.000	No	Yes	2.00
3015	30.15	30.32	90.59	2.84	0.52	1.02	29.09	0.00	29.09	4.000	No	Yes	2.00
3016	30.16	30.39	90.60	2.84	0.52	1.02	29.15	0.00	29.15	4.000	No	Yes	2.00
3017	30.17	30.47	90.56	2.84	0.52	1.02	29.21	0.00	29.21	4.000	No	Yes	2.00
3018	30.18	30.65	90.37	2.84	0.52	1.02	29.32	0.00	29.32	4.000	No	Yes	2.00
3019	30.19	30.94	89.98	2.84	0.52	1.02	29.64	0.00	29.64	4.000	No	Yes	2.00
3020	30.20	31.34	89.43	2.83	0.52	1.02	30.03	0.00	30.03	4.000	No	Yes	2.00
3021	30.21	31.80	88.81	2.82	0.51	1.02	30.47	0.00	30.47	4.000	No	Yes	2.00
3022	30.22	32.27	88.16	2.81	0.51	1.01	30.93	0.00	30.93	4.000	No	Yes	2.00
3023	30.23	32.75	87.52	2.81	0.51	1.01	31.39	0.00	31.39	4.000	No	Yes	2.00
3024	30.24	33.20	86.91	2.80	0.51	1.01	31.82	0.00	31.82	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3025	30.25	33.61	86.38	2.79	0.51	1.01	32.22	0.00	32.22	4.000	No	Yes	2.00
3026	30.26	33.93	85.98	2.79	0.51	1.01	32.54	0.00	32.54	4.000	No	Yes	2.00
3027	30.27	34.16	85.71	2.78	0.51	1.01	32.72	0.00	32.72	4.000	No	Yes	2.00
3028	30.28	34.36	85.53	2.78	0.51	1.01	32.89	0.00	32.89	4.000	No	Yes	2.00
3029	30.29	34.57	85.36	2.78	0.51	1.01	33.09	0.00	33.09	4.000	No	Yes	2.00
3030	30.30	34.81	85.17	2.78	0.51	1.01	33.31	0.00	33.31	4.000	No	Yes	2.00
3031	30.31	35.05	84.97	2.77	0.51	1.01	33.54	0.00	33.54	4.000	No	Yes	2.00
3032	30.32	35.28	84.78	2.77	0.51	1.01	33.76	0.00	33.76	4.000	No	Yes	2.00
3033	30.33	35.50	84.61	2.77	0.51	1.01	33.97	0.00	33.97	4.000	No	Yes	2.00
3034	30.34	35.69	84.46	2.77	0.50	1.01	34.15	0.00	34.15	4.000	No	Yes	2.00
3035	30.35	35.78	84.44	2.77	0.50	1.01	34.29	0.00	34.29	4.000	No	Yes	2.00
3036	30.36	35.75	84.56	2.77	0.50	1.01	34.19	0.00	34.19	4.000	No	Yes	2.00
3037	30.37	35.62	84.83	2.77	0.51	1.01	34.06	0.00	34.06	4.000	No	Yes	2.00
3038	30.38	35.48	85.13	2.78	0.51	1.01	33.91	0.00	33.91	4.000	No	Yes	2.00
3039	30.39	35.32	85.45	2.78	0.51	1.01	33.76	0.00	33.76	4.000	No	Yes	2.00
3040	30.40	35.16	85.78	2.78	0.51	1.01	33.60	0.00	33.60	4.000	No	Yes	2.00
3041	30.41	35.00	86.10	2.79	0.51	1.01	33.44	0.00	33.44	4.000	No	Yes	2.00
3042	30.42	34.86	86.39	2.79	0.51	1.01	33.30	0.00	33.30	4.000	No	Yes	2.00
3043	30.43	34.74	86.63	2.80	0.51	1.01	33.18	0.00	33.18	4.000	No	Yes	2.00
3044	30.44	34.60	86.85	2.80	0.51	1.01	33.06	0.00	33.06	4.000	No	Yes	2.00
3045	30.45	34.44	87.07	2.80	0.51	1.01	32.90	0.00	32.90	4.000	No	Yes	2.00
3046	30.46	34.24	87.32	2.80	0.51	1.01	32.69	0.00	32.69	4.000	No	Yes	2.00
3047	30.47	34.01	87.60	2.81	0.51	1.01	32.47	0.00	32.47	4.000	No	Yes	2.00
3048	30.48	33.77	87.89	2.81	0.51	1.01	32.23	0.00	32.23	4.000	No	Yes	2.00
3049	30.49	33.53	88.18	2.81	0.51	1.01	32.00	0.00	32.00	4.000	No	Yes	2.00
3050	30.50	33.31	88.47	2.82	0.51	1.01	31.77	0.00	31.77	4.000	No	Yes	2.00
3051	30.51	33.10	88.72	2.82	0.51	1.01	31.57	0.00	31.57	4.000	No	Yes	2.00
3052	30.52	33.05	88.79	2.82	0.51	1.01	31.40	0.00	31.40	4.000	No	Yes	2.00
3053	30.53	33.24	88.59	2.82	0.51	1.01	31.61	0.00	31.61	4.000	Yes	Yes	2.00
3054	30.54	33.67	88.10	2.81	0.51	1.01	32.08	0.00	32.08	4.000	Yes	Yes	2.00
3055	30.55	34.23	87.47	2.81	0.51	1.01	32.62	0.00	32.62	4.000	Yes	Yes	2.00
3056	30.56	34.85	86.77	2.80	0.51	1.01	33.22	0.00	33.22	4.000	Yes	Yes	2.00
3057	30.57	35.49	86.07	2.79	0.51	1.01	33.83	0.00	33.83	4.000	Yes	Yes	2.00
3058	30.58	36.12	85.38	2.78	0.50	1.01	34.44	0.00	34.44	4.000	Yes	Yes	2.00
3059	30.59	36.71	84.75	2.77	0.50	1.01	35.00	0.00	35.00	4.000	Yes	Yes	2.00
3060	30.60	37.22	84.21	2.77	0.50	1.01	35.49	0.00	35.49	4.000	Yes	Yes	2.00
3061	30.61	37.88	83.53	2.76	0.50	1.01	35.89	0.00	35.89	4.000	Yes	Yes	2.00
3062	30.62	38.81	82.61	2.75	0.50	1.01	36.87	0.00	36.87	4.000	Yes	Yes	2.00
3063	30.63	40.09	81.37	2.73	0.49	1.01	38.11	0.00	38.11	4.000	Yes	Yes	2.00
3064	30.64	41.56	79.98	2.71	0.49	1.01	39.53	0.00	39.53	4.000	Yes	Yes	2.00
3065	30.65	43.14	78.52	2.69	0.49	1.01	41.05	0.00	41.05	4.000	Yes	Yes	2.00
3066	30.66	44.74	77.08	2.68	0.48	1.01	42.59	0.00	42.59	4.000	Yes	Yes	2.00
3067	30.67	46.29	75.70	2.66	0.48	1.01	44.08	0.00	44.08	4.000	Yes	Yes	2.00
3068	30.68	47.69	74.47	2.64	0.48	1.01	45.44	0.00	45.44	4.000	Yes	Yes	2.00
3069	30.69	48.92	73.42	2.63	0.47	1.01	46.59	0.00	46.59	4.000	Yes	Yes	2.00
3070	30.70	50.13	72.41	2.62	0.47	1.01	47.56	0.00	47.56	4.000	Yes	Yes	2.00
3071	30.71	51.48	71.31	2.60	0.47	1.01	48.86	0.00	48.86	4.000	Yes	Yes	2.00
3072	30.72	53.11	70.01	2.59	0.47	1.01	50.43	65.31	115.73	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3073	30.73	54.93	68.58	2.57	0.46	1.01	52.17	65.51	117.69	4.000	Yes	No	2.00
3074	30.74	56.84	67.10	2.55	0.46	1.01	54.01	65.71	119.72	4.000	Yes	No	2.00
3075	30.75	58.75	65.63	2.53	0.45	1.01	55.85	65.89	121.73	4.000	Yes	No	2.00
3076	30.76	60.56	64.25	2.52	0.45	1.01	57.59	66.04	123.63	4.000	Yes	No	2.00
3077	30.77	62.17	63.04	2.50	0.45	1.01	59.14	66.16	125.30	4.000	Yes	No	2.00
3078	30.78	63.55	62.00	2.49	0.44	1.01	60.41	66.23	126.64	4.000	Yes	No	2.00
3079	30.79	64.89	61.00	2.48	0.44	1.01	61.51	66.26	127.76	4.000	Yes	No	2.00
3080	30.80	66.35	59.92	2.46	0.44	1.00	62.90	66.33	129.23	4.000	Yes	No	2.00
3081	30.81	68.05	58.66	2.45	0.44	1.00	64.54	66.39	130.93	4.000	Yes	No	2.00
3082	30.82	69.91	57.28	2.43	0.43	1.00	66.33	66.43	132.75	4.000	Yes	No	2.00
3083	30.83	71.83	55.86	2.41	0.43	1.00	68.17	66.44	134.61	4.000	Yes	No	2.00
3084	30.84	73.72	54.46	2.39	0.43	1.00	69.98	66.41	136.39	4.000	Yes	No	2.00
3085	30.85	75.47	53.16	2.38	0.42	1.00	71.66	66.35	138.01	4.000	Yes	No	2.00
3086	30.86	76.98	52.03	2.36	0.42	1.00	73.12	66.28	139.40	4.000	Yes	No	2.00
3087	30.87	78.15	51.20	2.35	0.42	1.00	74.26	66.22	140.48	4.000	Yes	No	2.00
3088	30.88	79.10	50.59	2.34	0.42	1.00	74.94	66.13	141.07	4.000	Yes	No	2.00
3089	30.89	80.00	50.08	2.34	0.42	1.00	75.81	66.12	141.93	4.000	Yes	No	2.00
3090	30.90	81.04	49.50	2.33	0.42	1.00	76.79	66.11	142.90	4.000	Yes	No	2.00
3091	30.91	82.14	48.88	2.32	0.41	1.00	77.85	66.08	143.93	4.000	Yes	No	2.00
3092	30.92	83.26	48.25	2.32	0.41	1.00	78.91	66.05	144.96	4.000	Yes	No	2.00
3093	30.93	84.34	47.65	2.31	0.41	1.00	79.94	66.00	145.95	4.000	Yes	No	2.00
3094	30.94	85.32	47.10	2.30	0.41	1.00	80.88	65.96	146.84	4.000	Yes	No	2.00
3095	30.95	86.09	46.70	2.30	0.41	1.00	81.67	65.94	147.61	4.000	Yes	No	2.00
3096	30.96	86.56	46.53	2.29	0.41	1.00	82.10	65.96	148.05	0.277	No	No	0.30
3097	30.97	86.80	46.59	2.29	0.41	1.00	82.19	66.01	148.21	0.277	No	No	0.31
3098	30.98	86.94	46.77	2.30	0.41	1.00	82.31	66.14	148.46	0.279	No	No	0.31
3099	30.99	87.09	46.97	2.30	0.41	1.00	82.45	66.29	148.74	0.281	No	No	0.31
3100	31.00	87.25	47.18	2.30	0.40	1.00	82.59	66.44	149.03	0.283	No	No	0.31
3101	31.01	87.41	47.38	2.30	0.40	1.00	82.74	66.59	149.32	0.284	No	No	0.31
3102	31.02	87.56	47.58	2.31	0.40	1.00	82.87	66.73	149.59	0.286	No	No	0.32
3103	31.03	87.69	47.75	2.31	0.40	1.00	82.99	66.85	149.84	0.288	No	No	0.32
3104	31.04	87.77	47.90	2.31	0.40	1.00	83.08	66.95	150.04	0.289	No	No	0.32
3105	31.05	87.78	48.06	2.31	0.40	1.00	83.06	67.03	150.09	0.289	No	No	0.32
3106	31.06	87.74	48.24	2.32	0.40	1.00	82.99	67.11	150.10	0.290	No	No	0.32
3107	31.07	87.66	48.45	2.32	0.40	1.00	82.91	67.20	150.11	0.290	No	No	0.32
3108	31.08	87.59	48.68	2.32	0.40	1.00	82.83	67.29	150.12	0.290	No	No	0.32
3109	31.09	87.51	48.92	2.32	0.40	1.00	82.74	67.39	150.13	0.290	No	No	0.32
3110	31.10	87.43	49.15	2.33	0.40	1.00	82.66	67.48	150.14	0.290	No	No	0.32
3111	31.11	87.36	49.36	2.33	0.40	1.00	82.58	67.56	150.14	0.290	No	No	0.32
3112	31.12	87.30	49.54	2.33	0.40	1.00	82.50	67.64	150.14	0.290	No	No	0.32
3113	31.13	87.30	49.68	2.33	0.40	1.00	82.45	67.69	150.14	0.290	No	No	0.32
3114	31.14	87.36	49.78	2.33	0.40	1.00	82.54	67.76	150.31	0.291	No	No	0.32
3115	31.15	87.49	49.88	2.34	0.40	1.00	82.66	67.84	150.50	0.292	No	No	0.32
3116	31.16	87.64	49.98	2.34	0.40	1.00	82.79	67.92	150.71	0.294	No	No	0.32
3117	31.17	87.80	50.09	2.34	0.40	1.00	82.93	68.01	150.94	0.295	No	No	0.33
3118	31.18	87.96	50.20	2.34	0.40	1.00	83.07	68.10	151.18	0.297	No	No	0.33
3119	31.19	88.11	50.31	2.34	0.40	1.00	83.21	68.19	151.40	0.298	No	No	0.33
3120	31.20	88.25	50.40	2.34	0.40	1.00	83.34	68.27	151.61	0.300	No	No	0.33

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3121	31.21	88.39	50.47	2.34	0.40	1.00	83.44	68.33	151.77	0.301	No	No	0.33
3122	31.22	88.58	50.50	2.34	0.40	1.00	83.57	68.38	151.95	0.302	No	No	0.33
3123	31.23	88.84	50.48	2.34	0.40	1.00	83.84	68.44	152.28	0.305	No	No	0.34
3124	31.24	89.19	50.43	2.34	0.40	1.00	84.15	68.50	152.66	0.307	No	No	0.34
3125	31.25	89.57	50.38	2.34	0.40	1.00	84.51	68.57	153.08	0.311	No	No	0.34
3126	31.26	89.96	50.33	2.34	0.40	1.00	84.88	68.65	153.53	0.314	No	No	0.35
3127	31.27	90.36	50.28	2.34	0.40	1.00	85.25	68.72	153.97	0.317	No	No	0.35
3128	31.28	90.74	50.23	2.34	0.40	1.00	85.60	68.79	154.39	0.321	No	No	0.35
3129	31.29	91.07	50.19	2.34	0.40	1.00	85.91	68.85	154.76	0.324	No	No	0.36
3130	31.30	91.38	50.13	2.34	0.40	1.00	86.16	68.89	155.05	0.326	No	No	0.36
3131	31.31	91.73	50.03	2.34	0.39	1.00	86.45	68.92	155.37	0.329	No	No	0.36
3132	31.32	92.15	49.88	2.34	0.39	1.00	86.86	68.95	155.80	0.332	No	No	0.37
3133	31.33	92.65	49.69	2.33	0.39	1.00	87.32	68.98	156.31	0.337	No	No	0.37
3134	31.34	93.19	49.48	2.33	0.39	1.00	87.84	69.01	156.85	0.342	No	No	0.38
3135	31.35	93.75	49.27	2.33	0.39	1.00	88.36	69.05	157.41	0.347	No	No	0.38
3136	31.36	94.30	49.07	2.33	0.39	1.00	88.88	69.08	157.96	0.352	No	No	0.39
3137	31.37	94.81	48.88	2.32	0.39	1.00	89.36	69.11	158.46	0.356	No	No	0.39
3138	31.38	95.26	48.71	2.32	0.39	1.00	89.77	69.13	158.90	0.361	No	No	0.40
3139	31.39	95.77	48.52	2.32	0.39	1.00	90.12	69.12	159.23	0.364	No	No	0.40
3140	31.40	96.41	48.28	2.32	0.39	1.00	90.76	69.16	159.91	0.371	No	No	0.41
3141	31.41	97.25	47.96	2.31	0.39	1.00	91.56	69.19	160.75	0.380	No	No	0.42
3142	31.42	98.22	47.59	2.31	0.38	1.00	92.47	69.23	161.70	0.390	No	No	0.43
3143	31.43	99.24	47.20	2.30	0.38	1.00	93.44	69.26	162.71	0.401	No	No	0.45
3144	31.44	100.28	46.81	2.30	0.38	1.00	94.43	69.30	163.73	0.414	No	No	0.46
3145	31.45	101.28	46.43	2.29	0.38	1.00	95.38	69.32	164.70	0.426	No	No	0.47
3146	31.46	102.19	46.09	2.29	0.38	1.00	96.24	69.34	165.58	0.437	No	No	0.49
3147	31.47	102.98	45.80	2.28	0.38	1.00	96.96	69.35	166.31	0.447	No	No	0.50
3148	31.48	103.75	45.51	2.28	0.38	1.00	97.58	69.33	166.91	0.456	No	No	0.51
3149	31.49	104.61	45.19	2.28	0.38	1.00	98.39	69.34	167.73	0.468	No	No	0.52
3150	31.50	105.64	44.81	2.27	0.37	1.00	99.36	69.35	168.71	0.483	No	No	0.54
3151	31.51	106.78	44.39	2.27	0.37	1.00	100.45	69.35	169.79	0.501	No	No	0.56
3152	31.52	107.98	43.95	2.26	0.37	1.00	101.58	69.34	170.92	0.520	No	No	0.58
3153	31.53	109.17	43.51	2.26	0.37	1.00	102.71	69.33	172.04	0.540	No	No	0.60
3154	31.54	110.29	43.10	2.25	0.37	1.00	103.78	69.31	173.09	0.560	No	No	0.63
3155	31.55	111.29	42.74	2.25	0.37	1.00	104.72	69.29	174.01	0.579	No	No	0.65
3156	31.56	112.15	42.42	2.24	0.36	1.00	105.49	69.25	174.74	0.595	No	No	0.67
3157	31.57	112.98	42.11	2.24	0.36	1.00	106.17	69.19	175.36	0.608	No	No	0.68
3158	31.58	113.91	41.75	2.23	0.36	1.00	107.04	69.14	176.18	0.627	No	No	0.70
3159	31.59	114.98	41.34	2.23	0.36	1.00	108.06	69.07	177.13	0.650	No	No	0.73
3160	31.60	116.15	40.89	2.22	0.36	1.00	109.17	68.99	178.16	0.676	No	No	0.76
3161	31.61	117.35	40.43	2.22	0.36	0.99	110.31	68.89	179.20	0.704	No	No	0.79
3162	31.62	118.52	39.98	2.21	0.36	0.99	111.42	68.79	180.21	0.733	No	No	0.82
3163	31.63	119.61	39.56	2.21	0.36	0.99	112.45	68.69	181.14	0.761	No	No	0.86
3164	31.64	120.55	39.20	2.20	0.35	0.99	113.34	68.59	181.93	0.786	No	No	0.88
3165	31.65	121.35	38.89	2.20	0.35	0.99	114.03	68.47	182.50	0.805	No	No	0.91
3166	31.66	122.11	38.56	2.19	0.35	0.99	114.67	68.33	183.00	0.822	No	No	0.93
3167	31.67	122.96	38.19	2.19	0.35	0.99	115.47	68.18	183.65	0.845	No	No	0.95
3168	31.68	123.93	37.76	2.18	0.35	0.99	116.38	67.99	184.38	0.872	No	No	0.98

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3169	31.69	124.95	37.31	2.18	0.35	0.99	117.35	67.78	185.14	0.901	No	No	1.02
3170	31.70	125.99	36.84	2.17	0.35	0.99	118.34	67.55	185.89	0.932	No	No	1.05
3171	31.71	126.99	36.40	2.17	0.35	0.99	119.28	67.32	186.60	0.962	No	No	1.09
3172	31.72	127.89	36.00	2.16	0.35	0.99	120.13	67.09	187.23	0.989	No	No	1.12
3173	31.73	128.63	35.67	2.16	0.35	0.99	120.85	66.91	187.76	1.014	No	No	1.14
3174	31.74	129.22	35.41	2.16	0.35	0.99	121.32	66.74	188.06	1.028	No	No	1.16
3175	31.75	129.73	35.20	2.15	0.35	0.99	121.75	66.60	188.34	1.041	No	No	1.18
3176	31.76	130.28	34.97	2.15	0.34	0.99	122.26	66.46	188.72	1.060	No	No	1.20
3177	31.77	130.89	34.71	2.15	0.34	0.99	122.83	66.30	189.13	1.080	No	No	1.22
3178	31.78	131.53	34.44	2.14	0.34	0.99	123.43	66.12	189.55	1.102	No	No	1.24
3179	31.79	132.16	34.17	2.14	0.34	0.99	124.02	65.94	189.96	1.124	No	No	1.27
3180	31.80	132.76	33.92	2.14	0.34	0.99	124.58	65.76	190.35	1.144	No	No	1.29
3181	31.81	133.29	33.70	2.13	0.34	0.99	125.08	65.60	190.68	1.163	No	No	1.31
3182	31.82	133.71	33.53	2.13	0.34	0.99	125.48	65.49	190.97	1.179	No	No	1.33
3183	31.83	134.05	33.42	2.13	0.34	0.99	125.72	65.41	191.13	1.188	No	No	1.34
3184	31.84	134.37	33.34	2.13	0.34	0.99	126.00	65.37	191.37	1.203	No	No	1.36
3185	31.85	134.73	33.25	2.13	0.34	0.99	126.33	65.34	191.67	1.220	No	No	1.38
3186	31.86	135.12	33.16	2.13	0.34	0.99	126.69	65.30	191.99	1.239	No	No	1.40
3187	31.87	135.52	33.06	2.13	0.34	0.99	127.06	65.25	192.31	1.260	No	No	1.42
3188	31.88	135.91	32.97	2.12	0.34	0.99	127.42	65.21	192.63	1.280	No	No	1.44
3189	31.89	136.27	32.88	2.12	0.34	0.99	127.75	65.18	192.93	1.299	No	No	1.46
3190	31.90	136.57	32.81	2.12	0.34	0.99	128.04	65.15	193.19	1.316	No	No	1.48
3191	31.91	136.75	32.78	2.12	0.34	0.99	128.23	65.15	193.38	1.329	No	No	1.50
3192	31.92	136.82	32.78	2.12	0.34	0.99	128.22	65.15	193.37	1.328	No	No	1.50
3193	31.93	136.82	32.82	2.12	0.34	0.99	128.20	65.19	193.39	1.330	No	No	1.50
3194	31.94	136.82	32.85	2.12	0.34	0.99	128.19	65.23	193.42	1.332	No	No	1.50
3195	31.95	136.82	32.89	2.12	0.34	0.99	128.18	65.28	193.46	1.334	No	No	1.50
3196	31.96	136.82	32.93	2.12	0.34	0.99	128.16	65.33	193.49	1.336	No	No	1.51
3197	31.97	136.82	32.97	2.12	0.34	0.99	128.15	65.37	193.52	1.338	No	No	1.51
3198	31.98	136.82	33.00	2.13	0.34	0.99	128.14	65.41	193.55	1.340	No	No	1.51
3199	31.99	136.81	33.04	2.13	0.34	0.99	128.12	65.46	193.58	1.342	No	No	1.51
3200	32.00	136.75	33.10	2.13	0.34	0.99	128.07	65.52	193.59	1.343	No	No	1.51
3201	32.01	136.65	33.19	2.13	0.34	0.99	127.94	65.61	193.55	1.340	No	No	1.51
3202	32.02	136.52	33.30	2.13	0.34	0.99	127.80	65.72	193.51	1.338	No	No	1.51
3203	32.03	136.36	33.43	2.13	0.34	0.99	127.64	65.84	193.48	1.335	No	No	1.50
3204	32.04	136.20	33.56	2.13	0.34	0.99	127.47	65.96	193.44	1.332	No	No	1.50
3205	32.05	136.05	33.69	2.13	0.34	0.99	127.31	66.09	193.39	1.330	No	No	1.50
3206	32.06	135.90	33.81	2.14	0.34	0.99	127.15	66.20	193.35	1.327	No	No	1.49
3207	32.07	135.76	33.92	2.14	0.34	0.99	127.01	66.30	193.31	1.324	No	No	1.49
3208	32.08	135.65	34.02	2.14	0.34	0.99	126.90	66.39	193.28	1.322	No	No	1.49
3209	32.09	135.54	34.11	2.14	0.34	0.99	126.79	66.48	193.26	1.321	No	No	1.49
3210	32.10	135.42	34.21	2.14	0.34	0.99	126.66	66.57	193.22	1.318	No	No	1.48
3211	32.11	135.27	34.33	2.14	0.34	0.99	126.51	66.67	193.18	1.315	No	No	1.48
3212	32.12	135.12	34.45	2.14	0.34	0.99	126.34	66.78	193.13	1.312	No	No	1.48
3213	32.13	134.96	34.58	2.14	0.34	0.99	126.18	66.90	193.07	1.308	No	No	1.47
3214	32.14	134.80	34.71	2.15	0.34	0.99	126.02	67.00	193.02	1.305	No	No	1.47
3215	32.15	134.66	34.82	2.15	0.34	0.99	125.86	67.10	192.97	1.301	No	No	1.46
3216	32.16	134.53	34.92	2.15	0.34	0.99	125.73	67.19	192.92	1.298	No	No	1.46

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3217	32.17	134.42	35.02	2.15	0.34	0.99	125.63	67.27	192.89	1.297	No	No	1.46
3218	32.18	134.31	35.11	2.15	0.34	0.99	125.51	67.35	192.86	1.294	No	No	1.46
3219	32.19	134.17	35.21	2.15	0.34	0.99	125.37	67.43	192.80	1.291	No	No	1.45
3220	32.20	134.03	35.33	2.15	0.34	0.99	125.22	67.53	192.75	1.287	No	No	1.45
3221	32.21	133.87	35.46	2.16	0.34	0.99	125.05	67.63	192.68	1.283	No	No	1.44
3222	32.22	133.71	35.58	2.16	0.34	0.99	124.89	67.73	192.62	1.279	No	No	1.44
3223	32.23	133.55	35.70	2.16	0.34	0.99	124.73	67.83	192.56	1.275	No	No	1.43
3224	32.24	133.42	35.81	2.16	0.34	0.99	124.58	67.91	192.50	1.271	No	No	1.43
3225	32.25	133.31	35.90	2.16	0.34	0.99	124.46	67.98	192.44	1.268	No	No	1.43
3226	32.26	133.22	35.98	2.16	0.34	0.99	124.38	68.04	192.42	1.266	No	No	1.42
3227	32.27	133.16	36.04	2.16	0.34	0.99	124.31	68.10	192.41	1.265	No	No	1.42
3228	32.28	133.09	36.11	2.16	0.34	0.99	124.23	68.16	192.38	1.264	No	No	1.42
3229	32.29	133.01	36.19	2.16	0.34	0.99	124.14	68.22	192.36	1.263	No	No	1.42
3230	32.30	132.93	36.27	2.17	0.34	0.99	124.05	68.28	192.34	1.261	No	No	1.42
3231	32.31	132.85	36.35	2.17	0.34	0.99	123.96	68.35	192.31	1.259	No	No	1.42
3232	32.32	132.78	36.43	2.17	0.34	0.99	123.88	68.40	192.28	1.258	No	No	1.41
3233	32.33	132.71	36.49	2.17	0.34	0.99	123.80	68.46	192.26	1.256	No	No	1.41
3234	32.34	132.67	36.55	2.17	0.34	0.99	123.74	68.50	192.24	1.255	No	No	1.41
3235	32.35	132.65	36.60	2.17	0.34	0.99	123.72	68.55	192.27	1.257	No	No	1.41
3236	32.36	132.65	36.65	2.17	0.34	0.99	123.71	68.60	192.31	1.259	No	No	1.42
3237	32.37	132.65	36.71	2.17	0.34	0.99	123.69	68.66	192.35	1.262	No	No	1.42
3238	32.38	132.65	36.78	2.17	0.34	0.99	123.68	68.72	192.40	1.265	No	No	1.42
3239	32.39	132.65	36.84	2.17	0.34	0.99	123.67	68.79	192.46	1.269	No	No	1.43
3240	32.40	132.65	36.91	2.17	0.34	0.99	123.66	68.85	192.50	1.272	No	No	1.43
3241	32.41	132.65	36.97	2.17	0.34	0.99	123.64	68.91	192.55	1.274	No	No	1.43
3242	32.42	132.65	37.02	2.18	0.34	0.99	123.63	68.96	192.59	1.277	No	No	1.43
3243	32.43	132.65	37.07	2.18	0.34	0.99	123.62	69.00	192.62	1.279	No	No	1.44
3244	32.44	132.65	37.11	2.18	0.34	0.99	123.60	69.05	192.65	1.281	No	No	1.44
3245	32.45	132.65	37.17	2.18	0.34	0.99	123.59	69.10	192.69	1.283	No	No	1.44
3246	32.46	132.65	37.23	2.18	0.34	0.99	123.58	69.16	192.73	1.286	No	No	1.45
3247	32.47	132.65	37.29	2.18	0.34	0.99	123.57	69.22	192.78	1.289	No	No	1.45
3248	32.48	132.65	37.36	2.18	0.34	0.99	123.55	69.28	192.83	1.292	No	No	1.45
3249	32.49	132.65	37.42	2.18	0.34	0.99	123.54	69.34	192.88	1.295	No	No	1.46
3250	32.50	132.65	37.48	2.18	0.34	0.99	123.53	69.39	192.92	1.298	No	No	1.46
3251	32.51	132.66	37.52	2.18	0.34	0.99	123.51	69.43	192.95	1.300	No	No	1.46
3252	32.52	132.69	37.57	2.18	0.34	0.99	123.52	69.48	193.00	1.304	No	No	1.46
3253	32.53	132.74	37.61	2.18	0.34	0.99	123.57	69.53	193.09	1.310	No	No	1.47
3254	32.54	132.81	37.65	2.18	0.34	0.99	123.62	69.58	193.20	1.317	No	No	1.48
3255	32.55	132.88	37.70	2.18	0.34	0.99	123.68	69.64	193.32	1.325	No	No	1.49
3256	32.56	132.96	37.75	2.18	0.34	0.99	123.74	69.71	193.45	1.333	No	No	1.50
3257	32.57	133.04	37.80	2.18	0.34	0.99	123.81	69.77	193.58	1.342	No	No	1.51
3258	32.58	133.12	37.85	2.19	0.34	0.98	123.87	69.83	193.69	1.350	No	No	1.52
3259	32.59	133.18	37.89	2.19	0.34	0.98	123.92	69.88	193.80	1.357	No	No	1.52
3260	32.60	133.47	37.89	2.19	0.34	0.98	123.95	69.89	193.84	1.360	No	No	1.53
3261	32.61	134.08	37.83	2.19	0.34	0.98	124.63	69.99	194.61	1.415	No	No	1.59
3262	32.62	135.08	37.71	2.18	0.34	0.98	125.60	70.10	195.70	1.497	No	No	1.68
3263	32.63	136.27	37.57	2.18	0.33	0.98	126.73	70.22	196.95	1.600	No	No	1.79
3264	32.64	137.56	37.41	2.18	0.33	0.98	127.94	70.36	198.30	1.721	No	No	1.93

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3265	32.65	138.88	37.26	2.18	0.33	0.98	129.19	70.49	199.68	1.858	No	No	2.00
3266	32.66	140.17	37.11	2.18	0.33	0.98	130.41	70.62	201.03	2.006	No	No	2.00
3267	32.67	141.35	36.98	2.17	0.33	0.98	131.52	70.74	202.27	2.155	No	No	2.00
3268	32.68	142.37	36.87	2.17	0.33	0.98	132.48	70.85	203.33	2.295	No	No	2.00
3269	32.69	143.26	36.77	2.17	0.32	0.98	133.22	70.92	204.14	2.409	No	No	2.00
3270	32.70	144.15	36.68	2.17	0.32	0.98	133.99	71.00	204.99	2.536	No	No	2.00
3271	32.71	145.15	36.58	2.17	0.32	0.98	134.94	71.11	206.05	2.707	No	No	2.00
3272	32.72	146.29	36.46	2.17	0.32	0.98	136.02	71.23	207.25	2.918	No	No	2.00
3273	32.73	147.50	36.34	2.17	0.32	0.98	137.15	71.36	208.51	3.165	No	No	2.00
3274	32.74	148.71	36.22	2.17	0.32	0.98	138.30	71.49	209.79	3.440	No	No	2.00
3275	32.75	149.87	36.11	2.16	0.32	0.98	139.39	71.62	211.01	3.731	No	No	2.00
3276	32.76	150.92	36.01	2.16	0.31	0.98	140.38	71.73	212.11	4.000	No	No	2.00
3277	32.77	151.69	35.94	2.16	0.31	0.98	141.20	71.85	213.04	4.000	No	No	2.00
3278	32.78	152.16	35.93	2.16	0.31	0.98	141.55	71.91	213.46	4.000	No	No	2.00
3279	32.79	152.39	35.97	2.16	0.31	0.98	141.65	71.97	213.63	4.000	No	No	2.00
3280	32.80	152.54	36.02	2.16	0.31	0.98	141.78	72.07	213.85	4.000	No	No	2.00
3281	32.81	152.70	36.09	2.16	0.31	0.98	141.93	72.17	214.10	4.000	No	No	2.00
3282	32.82	152.88	36.15	2.16	0.31	0.98	142.08	72.28	214.36	4.000	No	No	2.00
3283	32.83	153.05	36.22	2.17	0.31	0.98	142.23	72.39	214.62	4.000	No	No	2.00
3284	32.84	153.21	36.28	2.17	0.31	0.98	142.37	72.49	214.86	4.000	No	No	2.00
3285	32.85	153.35	36.33	2.17	0.31	0.98	142.49	72.58	215.07	4.000	No	No	2.00
3286	32.86	153.53	36.36	2.17	0.31	0.98	142.59	72.63	215.22	4.000	No	No	2.00
3287	32.87	153.78	36.36	2.17	0.31	0.98	142.83	72.69	215.52	4.000	No	No	2.00
3288	32.88	154.14	36.34	2.17	0.31	0.98	143.17	72.74	215.91	4.000	No	No	2.00
3289	32.89	154.56	36.31	2.17	0.31	0.98	143.55	72.80	216.35	4.000	No	No	2.00
3290	32.90	155.01	36.28	2.17	0.31	0.98	143.97	72.86	216.83	4.000	No	No	2.00
3291	32.91	155.48	36.25	2.17	0.31	0.98	144.40	72.92	217.32	4.000	No	No	2.00
3292	32.92	155.93	36.22	2.17	0.31	0.98	144.82	72.98	217.80	4.000	No	No	2.00
3293	32.93	156.35	36.19	2.16	0.31	0.98	145.20	73.04	218.24	4.000	No	No	2.00
3294	32.94	156.71	36.16	2.16	0.31	0.98	145.53	73.08	218.61	4.000	No	No	2.00
3295	32.95	157.07	36.11	2.16	0.31	0.98	145.80	73.09	218.89	4.000	No	No	2.00
3296	32.96	157.49	36.03	2.16	0.30	0.98	146.19	73.08	219.27	4.000	No	No	2.00
3297	32.97	158.01	35.92	2.16	0.30	0.98	146.67	73.06	219.73	4.000	No	No	2.00
3298	32.98	158.59	35.79	2.16	0.30	0.98	147.20	73.04	220.24	4.000	No	No	2.00
3299	32.99	159.20	35.65	2.16	0.30	0.98	147.78	73.01	220.78	4.000	No	No	2.00
3300	33.00	159.82	35.52	2.16	0.30	0.98	148.35	72.98	221.33	4.000	No	No	2.00
3301	33.01	160.41	35.39	2.15	0.30	0.98	148.90	72.95	221.84	4.000	No	No	2.00
3302	33.02	160.94	35.27	2.15	0.30	0.98	149.39	72.92	222.31	4.000	No	No	2.00
3303	33.03	161.39	35.17	2.15	0.30	0.98	149.80	72.88	222.68	4.000	No	No	2.00
3304	33.04	161.83	35.05	2.15	0.30	0.98	150.14	72.82	222.96	4.000	No	No	2.00
3305	33.05	162.30	34.91	2.15	0.30	0.98	150.57	72.75	223.32	4.000	No	No	2.00
3306	33.06	162.86	34.74	2.15	0.30	0.98	151.09	72.65	223.74	4.000	No	No	2.00
3307	33.07	163.48	34.56	2.14	0.30	0.98	151.66	72.55	224.21	4.000	No	No	2.00
3308	33.08	164.12	34.36	2.14	0.30	0.98	152.25	72.43	224.68	4.000	No	No	2.00
3309	33.09	164.75	34.17	2.14	0.30	0.98	152.84	72.31	225.15	4.000	No	No	2.00
3310	33.10	165.34	33.98	2.14	0.30	0.98	153.39	72.20	225.59	4.000	No	No	2.00
3311	33.11	165.86	33.83	2.14	0.30	0.98	153.87	72.10	225.97	4.000	No	No	2.00
3312	33.12	166.34	33.68	2.13	0.30	0.98	154.26	71.99	226.25	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3313	33.13	166.84	33.54	2.13	0.30	0.98	154.69	71.90	226.59	4.000	No	No	2.00
3314	33.14	167.45	33.37	2.13	0.30	0.98	155.25	71.79	227.05	4.000	No	No	2.00
3315	33.15	168.14	33.18	2.13	0.29	0.98	155.90	71.67	227.58	4.000	No	No	2.00
3316	33.16	168.89	32.97	2.12	0.29	0.98	156.61	71.53	228.14	4.000	No	No	2.00
3317	33.17	169.66	32.76	2.12	0.29	0.98	157.32	71.39	228.71	4.000	No	No	2.00
3318	33.18	170.41	32.55	2.12	0.29	0.98	158.02	71.24	229.26	4.000	No	No	2.00
3319	33.19	171.09	32.36	2.12	0.29	0.98	158.66	71.11	229.76	4.000	No	No	2.00
3320	33.20	171.68	32.20	2.11	0.29	0.98	159.20	70.99	230.19	4.000	No	No	2.00
3321	33.21	172.17	32.05	2.11	0.29	0.98	159.61	70.86	230.47	4.000	No	No	2.00
3322	33.22	172.65	31.91	2.11	0.29	0.98	160.01	70.74	230.75	4.000	No	No	2.00
3323	33.23	173.19	31.75	2.11	0.29	0.98	160.50	70.59	231.10	4.000	No	No	2.00
3324	33.24	173.79	31.56	2.11	0.29	0.98	161.06	70.43	231.49	4.000	No	No	2.00
3325	33.25	174.42	31.36	2.10	0.29	0.98	161.65	70.25	231.90	4.000	No	No	2.00
3326	33.26	175.06	31.16	2.10	0.29	0.98	162.24	70.07	232.31	4.000	No	No	2.00
3327	33.27	175.67	30.98	2.10	0.29	0.98	162.80	69.89	232.69	4.000	No	No	2.00
3328	33.28	176.21	30.81	2.10	0.29	0.98	163.31	69.72	233.03	4.000	No	No	2.00
3329	33.29	176.62	30.67	2.10	0.29	0.98	163.73	69.59	233.32	4.000	No	No	2.00
3330	33.30	176.85	30.57	2.09	0.29	0.98	163.88	69.46	233.35	4.000	No	No	2.00
3331	33.31	176.95	30.49	2.09	0.29	0.98	163.92	69.34	233.26	4.000	No	No	2.00
3332	33.32	177.02	30.41	2.09	0.29	0.98	163.97	69.21	233.18	4.000	No	No	2.00
3333	33.33	177.10	30.31	2.09	0.29	0.98	164.03	69.06	233.09	4.000	No	No	2.00
3334	33.34	177.18	30.21	2.09	0.29	0.98	164.09	68.91	232.99	4.000	No	No	2.00
3335	33.35	177.26	30.11	2.09	0.29	0.98	164.15	68.75	232.90	4.000	No	No	2.00
3336	33.36	177.33	30.02	2.09	0.29	0.98	164.20	68.61	232.81	4.000	No	No	2.00
3337	33.37	177.40	29.94	2.09	0.29	0.98	164.24	68.48	232.72	4.000	No	No	2.00
3338	33.38	177.36	29.89	2.09	0.29	0.98	164.28	68.41	232.69	4.000	No	No	2.00
3339	33.39	177.19	29.88	2.09	0.29	0.98	164.04	68.34	232.38	4.000	No	No	2.00
3340	33.40	176.88	29.89	2.09	0.29	0.98	163.72	68.31	232.03	4.000	No	No	2.00
3341	33.41	176.52	29.92	2.09	0.29	0.98	163.36	68.27	231.62	4.000	No	No	2.00
3342	33.42	176.12	29.94	2.09	0.29	0.98	162.97	68.23	231.19	4.000	No	No	2.00
3343	33.43	175.72	29.96	2.09	0.29	0.98	162.57	68.18	230.75	4.000	No	No	2.00
3344	33.44	175.33	29.98	2.09	0.29	0.98	162.18	68.14	230.32	4.000	No	No	2.00
3345	33.45	174.98	30.00	2.09	0.29	0.98	161.83	68.10	229.93	4.000	No	No	2.00
3346	33.46	174.65	30.03	2.09	0.29	0.98	161.52	68.08	229.60	4.000	No	No	2.00
3347	33.47	174.26	30.07	2.09	0.29	0.98	161.22	68.09	229.30	4.000	No	No	2.00
3348	33.48	173.74	30.13	2.09	0.29	0.98	160.68	68.08	228.76	4.000	No	No	2.00
3349	33.49	173.07	30.22	2.09	0.29	0.98	160.02	68.10	228.12	4.000	No	No	2.00
3350	33.50	172.32	30.32	2.09	0.29	0.98	159.29	68.11	227.40	4.000	No	No	2.00
3351	33.51	171.53	30.43	2.09	0.30	0.98	158.52	68.13	226.65	4.000	No	No	2.00
3352	33.52	170.73	30.54	2.09	0.30	0.98	157.74	68.14	225.89	4.000	No	No	2.00
3353	33.53	169.97	30.64	2.10	0.30	0.98	157.00	68.16	225.16	4.000	No	No	2.00
3354	33.54	169.29	30.74	2.10	0.30	0.98	156.34	68.17	224.51	4.000	No	No	2.00
3355	33.55	168.67	30.83	2.10	0.30	0.98	155.79	68.21	224.00	4.000	No	No	2.00
3356	33.56	167.99	30.97	2.10	0.30	0.98	155.21	68.29	223.50	4.000	No	No	2.00
3357	33.57	167.18	31.14	2.10	0.30	0.98	154.40	68.40	222.80	4.000	No	No	2.00
3358	33.58	166.19	31.36	2.10	0.30	0.98	153.45	68.54	221.99	4.000	No	No	2.00
3359	33.59	165.11	31.61	2.11	0.30	0.98	152.41	68.68	221.09	4.000	No	No	2.00
3360	33.60	163.99	31.86	2.11	0.30	0.98	151.33	68.82	220.15	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3361	33.61	162.89	32.11	2.11	0.30	0.98	150.26	68.96	219.22	4.000	No	No	2.00
3362	33.62	161.86	32.34	2.12	0.31	0.98	149.27	69.08	218.35	4.000	No	No	2.00
3363	33.63	160.96	32.55	2.12	0.31	0.98	148.39	69.18	217.57	4.000	No	No	2.00
3364	33.64	160.15	32.75	2.12	0.31	0.98	147.69	69.30	216.99	4.000	No	No	2.00
3365	33.65	159.32	32.96	2.12	0.31	0.98	146.96	69.44	216.40	4.000	No	No	2.00
3366	33.66	158.37	33.22	2.13	0.31	0.98	146.04	69.59	215.63	4.000	No	No	2.00
3367	33.67	157.28	33.53	2.13	0.31	0.98	144.99	69.76	214.74	4.000	No	No	2.00
3368	33.68	156.10	33.85	2.14	0.31	0.98	143.86	69.93	213.78	4.000	No	No	2.00
3369	33.69	154.90	34.18	2.14	0.31	0.98	142.70	70.09	212.79	4.000	No	No	2.00
3370	33.70	153.74	34.51	2.14	0.31	0.98	141.58	70.24	211.82	3.943	No	No	2.00
3371	33.71	152.67	34.80	2.15	0.32	0.97	140.56	70.37	210.93	3.711	No	No	2.00
3372	33.72	151.76	35.06	2.15	0.32	0.97	139.68	70.47	210.15	3.524	No	No	2.00
3373	33.73	150.96	35.28	2.15	0.32	0.97	139.00	70.58	209.58	3.393	No	No	2.00
3374	33.74	150.13	35.50	2.16	0.32	0.97	138.25	70.66	208.92	3.248	No	No	2.00
3375	33.75	149.19	35.74	2.16	0.32	0.97	137.34	70.74	208.08	3.078	No	No	2.00
3376	33.76	148.14	36.02	2.16	0.32	0.97	136.33	70.82	207.15	2.900	No	No	2.00
3377	33.77	147.03	36.31	2.17	0.32	0.97	135.26	70.90	206.16	2.725	No	No	2.00
3378	33.78	145.91	36.61	2.17	0.32	0.97	134.19	70.97	205.16	2.562	No	No	2.00
3379	33.79	144.85	36.89	2.17	0.32	0.97	133.17	71.03	204.20	2.417	No	No	2.00
3380	33.80	143.90	37.14	2.18	0.33	0.97	132.25	71.08	203.33	2.295	No	No	2.00
3381	33.81	143.10	37.36	2.18	0.33	0.97	131.49	71.13	202.62	2.200	No	No	2.00
3382	33.82	142.35	37.56	2.18	0.33	0.97	130.88	71.19	202.07	2.130	No	No	2.00
3383	33.83	141.56	37.78	2.18	0.33	0.97	130.13	71.24	201.36	2.045	No	No	2.00
3384	33.84	140.65	38.04	2.19	0.33	0.97	129.25	71.28	200.53	1.949	No	No	2.00
3385	33.85	139.64	38.32	2.19	0.33	0.97	128.28	71.32	199.60	1.850	No	No	2.00
3386	33.86	138.60	38.61	2.20	0.33	0.97	127.28	71.36	198.65	1.754	No	No	1.95
3387	33.87	137.58	38.89	2.20	0.33	0.97	126.30	71.40	197.70	1.666	No	No	1.85
3388	33.88	136.62	39.16	2.20	0.33	0.97	125.38	71.43	196.81	1.587	No	No	1.77
3389	33.89	135.79	39.40	2.20	0.33	0.97	124.57	71.45	196.02	1.523	No	No	1.70
3390	33.90	135.25	39.57	2.21	0.34	0.97	123.93	71.44	195.37	1.472	No	No	1.64
3391	33.91	134.97	39.68	2.21	0.34	0.97	123.84	71.53	195.37	1.472	No	No	1.64
3392	33.92	134.88	39.77	2.21	0.34	0.97	123.75	71.58	195.34	1.469	No	No	1.64
3393	33.93	134.79	39.87	2.21	0.34	0.97	123.65	71.64	195.29	1.466	No	No	1.63
3394	33.94	134.68	39.97	2.21	0.34	0.97	123.54	71.71	195.25	1.462	No	No	1.63
3395	33.95	134.58	40.08	2.21	0.34	0.97	123.42	71.78	195.20	1.458	No	No	1.62
3396	33.96	134.47	40.18	2.21	0.34	0.97	123.31	71.84	195.15	1.455	No	No	1.62
3397	33.97	134.38	40.28	2.22	0.34	0.97	123.21	71.89	195.11	1.451	No	No	1.62
3398	33.98	134.30	40.36	2.22	0.34	0.97	123.12	71.94	195.07	1.448	No	No	1.61
3399	33.99	134.23	40.43	2.22	0.34	0.97	123.06	71.99	195.05	1.447	No	No	1.61
3400	34.00	134.17	40.51	2.22	0.34	0.97	122.99	72.04	195.03	1.446	No	No	1.61
3401	34.01	134.10	40.59	2.22	0.34	0.97	122.92	72.09	195.01	1.444	No	No	1.61
3402	34.02	134.03	40.69	2.22	0.34	0.97	122.83	72.15	194.98	1.442	No	No	1.60
3403	34.03	133.95	40.79	2.22	0.34	0.97	122.74	72.21	194.96	1.440	No	No	1.60
3404	34.04	133.87	40.89	2.22	0.34	0.97	122.66	72.28	194.93	1.439	No	No	1.60
3405	34.05	133.79	40.98	2.22	0.34	0.97	122.57	72.33	194.91	1.437	No	No	1.60
3406	34.06	133.73	41.07	2.23	0.34	0.97	122.50	72.39	194.88	1.435	No	No	1.60
3407	34.07	133.62	41.15	2.23	0.34	0.97	122.43	72.43	194.87	1.434	No	No	1.59
3408	34.08	133.42	41.23	2.23	0.34	0.97	122.24	72.46	194.69	1.421	No	No	1.58

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3409	34.09	133.10	41.33	2.23	0.34	0.97	121.90	72.46	194.36	1.396	No	No	1.55
3410	34.10	132.70	41.45	2.23	0.34	0.97	121.51	72.46	193.97	1.369	No	No	1.52
3411	34.11	132.26	41.59	2.23	0.34	0.97	121.08	72.46	193.54	1.340	No	No	1.49
3412	34.12	131.81	41.72	2.23	0.34	0.97	120.64	72.46	193.10	1.310	No	No	1.46
3413	34.13	131.36	41.86	2.24	0.34	0.97	120.21	72.46	192.67	1.282	No	No	1.43
3414	34.14	130.95	41.99	2.24	0.34	0.97	119.80	72.46	192.26	1.256	No	No	1.40
3415	34.15	130.58	42.10	2.24	0.34	0.97	119.44	72.46	191.90	1.234	No	No	1.37
3416	34.16	130.38	42.17	2.24	0.34	0.97	119.16	72.45	191.61	1.217	No	No	1.35
3417	34.17	130.32	42.23	2.24	0.34	0.97	119.19	72.50	191.70	1.222	No	No	1.36
3418	34.18	130.39	42.26	2.24	0.34	0.97	119.24	72.54	191.78	1.227	No	No	1.37
3419	34.19	130.46	42.30	2.24	0.34	0.97	119.30	72.59	191.89	1.233	No	No	1.37
3420	34.20	130.54	42.35	2.24	0.34	0.97	119.36	72.64	192.00	1.240	No	No	1.38
3421	34.21	130.62	42.39	2.24	0.34	0.97	119.43	72.68	192.11	1.247	No	No	1.39
3422	34.22	130.70	42.43	2.24	0.34	0.97	119.49	72.73	192.22	1.254	No	No	1.39
3423	34.23	130.77	42.47	2.24	0.34	0.97	119.54	72.78	192.32	1.260	No	No	1.40
3424	34.24	130.85	42.50	2.24	0.34	0.97	119.59	72.81	192.40	1.265	No	No	1.41
3425	34.25	131.00	42.52	2.24	0.34	0.97	119.68	72.84	192.53	1.273	No	No	1.42
3426	34.26	131.25	42.52	2.24	0.34	0.97	119.93	72.91	192.84	1.293	No	No	1.44
3427	34.27	131.59	42.51	2.24	0.34	0.97	120.24	72.98	193.22	1.318	No	No	1.47
3428	34.28	131.96	42.50	2.24	0.34	0.97	120.59	73.05	193.64	1.346	No	No	1.50
3429	34.29	132.36	42.49	2.24	0.34	0.97	120.95	73.14	194.09	1.377	No	No	1.53
3430	34.30	132.76	42.47	2.24	0.34	0.97	121.32	73.22	194.54	1.409	No	No	1.57
3431	34.31	133.14	42.46	2.24	0.34	0.97	121.66	73.29	194.96	1.440	No	No	1.60
3432	34.32	133.48	42.45	2.24	0.34	0.97	121.97	73.36	195.34	1.469	No	No	1.63
3433	34.33	133.82	42.43	2.24	0.34	0.97	122.22	73.40	195.63	1.491	No	No	1.66
3434	34.34	134.26	42.36	2.24	0.33	0.97	122.59	73.45	196.04	1.524	No	No	1.69
3435	34.35	134.84	42.25	2.24	0.33	0.97	123.15	73.50	196.65	1.575	No	No	1.75
3436	34.36	135.55	42.12	2.24	0.33	0.97	123.81	73.56	197.37	1.636	No	No	1.82
3437	34.37	136.32	41.97	2.24	0.33	0.97	124.53	73.62	198.15	1.707	No	No	1.89
3438	34.38	137.12	41.82	2.24	0.33	0.97	125.28	73.68	198.95	1.784	No	No	1.98
3439	34.39	137.91	41.67	2.23	0.33	0.97	126.01	73.74	199.74	1.865	No	No	2.00
3440	34.40	138.64	41.53	2.23	0.33	0.97	126.69	73.79	200.48	1.944	No	No	2.00
3441	34.41	139.28	41.41	2.23	0.33	0.97	127.28	73.84	201.12	2.016	No	No	2.00
3442	34.42	139.88	41.29	2.23	0.33	0.97	127.75	73.85	201.60	2.073	No	No	2.00
3443	34.43	140.52	41.14	2.23	0.33	0.97	128.32	73.87	202.19	2.145	No	No	2.00
3444	34.44	141.29	40.96	2.22	0.33	0.97	129.04	73.90	202.93	2.241	No	No	2.00
3445	34.45	142.17	40.76	2.22	0.32	0.97	129.86	73.92	203.78	2.357	No	No	2.00
3446	34.46	143.12	40.53	2.22	0.32	0.97	130.74	73.94	204.68	2.489	No	No	2.00
3447	34.47	144.08	40.31	2.22	0.32	0.97	131.64	73.96	205.60	2.633	No	No	2.00
3448	34.48	145.01	40.09	2.21	0.32	0.97	132.50	73.98	206.48	2.781	No	No	2.00
3449	34.49	145.85	39.90	2.21	0.32	0.97	133.29	73.99	207.28	2.925	No	No	2.00
3450	34.50	146.58	39.72	2.21	0.32	0.97	133.96	74.00	207.95	3.052	No	No	2.00
3451	34.51	147.30	39.53	2.21	0.32	0.97	134.51	73.95	208.46	3.155	No	No	2.00
3452	34.52	148.09	39.29	2.20	0.32	0.97	135.24	73.90	209.15	3.298	No	No	2.00
3453	34.53	149.04	38.99	2.20	0.32	0.97	136.13	73.83	209.96	3.480	No	No	2.00
3454	34.54	150.10	38.66	2.20	0.32	0.97	137.12	73.75	210.87	3.696	No	No	2.00
3455	34.55	151.22	38.31	2.19	0.31	0.97	138.16	73.65	211.81	3.939	No	No	2.00
3456	34.56	152.33	37.96	2.19	0.31	0.97	139.20	73.54	212.74	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3457	34.57	153.39	37.62	2.18	0.31	0.97	140.19	73.43	213.62	4.000	No	No	2.00
3458	34.58	154.32	37.33	2.18	0.31	0.97	141.06	73.33	214.39	4.000	No	No	2.00
3459	34.59	155.17	37.06	2.18	0.31	0.97	141.78	73.21	214.98	4.000	No	No	2.00
3460	34.60	156.04	36.77	2.17	0.31	0.97	142.49	73.06	215.55	4.000	No	No	2.00
3461	34.61	157.06	36.41	2.17	0.31	0.97	143.46	72.89	216.34	4.000	No	No	2.00
3462	34.62	158.27	35.99	2.16	0.31	0.97	144.58	72.67	217.26	4.000	No	No	2.00
3463	34.63	159.59	35.53	2.16	0.31	0.97	145.82	72.42	218.23	4.000	No	No	2.00
3464	34.64	160.95	35.05	2.15	0.30	0.97	147.09	72.14	219.22	4.000	No	No	2.00
3465	34.65	162.28	34.58	2.14	0.30	0.97	148.33	71.84	220.17	4.000	No	No	2.00
3466	34.66	163.52	34.14	2.14	0.30	0.97	149.49	71.54	221.04	4.000	No	No	2.00
3467	34.67	164.60	33.76	2.13	0.30	0.97	150.50	71.27	221.77	4.000	No	No	2.00
3468	34.68	165.50	33.42	2.13	0.30	0.97	151.28	70.99	222.27	4.000	No	No	2.00
3469	34.69	166.34	33.06	2.13	0.30	0.97	151.95	70.65	222.60	4.000	No	No	2.00
3470	34.70	167.24	32.65	2.12	0.30	0.97	152.79	70.26	223.05	4.000	No	No	2.00
3471	34.71	168.27	32.17	2.11	0.30	0.97	153.74	69.78	223.53	4.000	No	No	2.00
3472	34.72	169.37	31.65	2.11	0.30	0.97	154.77	69.24	224.01	4.000	No	No	2.00
3473	34.73	170.49	31.12	2.10	0.30	0.97	155.80	68.66	224.46	4.000	No	No	2.00
3474	34.74	171.57	30.61	2.10	0.30	0.97	156.80	68.06	224.86	4.000	No	No	2.00
3475	34.75	172.55	30.14	2.09	0.30	0.97	157.71	67.49	225.20	4.000	No	No	2.00
3476	34.76	173.37	29.74	2.08	0.30	0.97	158.47	66.98	225.46	4.000	No	No	2.00
3477	34.77	174.04	29.39	2.08	0.30	0.97	159.01	66.49	225.50	4.000	No	No	2.00
3478	34.78	174.67	29.03	2.08	0.30	0.97	159.52	65.98	225.50	4.000	No	No	2.00
3479	34.79	175.35	28.63	2.07	0.30	0.97	160.14	65.38	225.53	4.000	No	No	2.00
3480	34.80	176.10	28.17	2.06	0.30	0.97	160.83	64.69	225.52	4.000	No	No	2.00
3481	34.81	176.90	27.69	2.06	0.30	0.97	161.56	63.92	225.47	4.000	No	No	2.00
3482	34.82	177.69	27.20	2.05	0.30	0.97	162.28	63.11	225.39	4.000	No	No	2.00
3483	34.83	178.45	26.74	2.05	0.30	0.97	162.96	62.31	225.27	4.000	No	No	2.00
3484	34.84	179.11	26.32	2.04	0.30	0.97	163.57	61.56	225.13	4.000	No	No	2.00
3485	34.85	179.64	25.98	2.04	0.30	0.97	164.06	60.94	225.00	4.000	No	No	2.00
3486	34.86	180.06	25.69	2.03	0.30	0.97	164.35	60.37	224.72	4.000	No	No	2.00
3487	34.87	180.45	25.41	2.03	0.30	0.97	164.67	59.82	224.49	4.000	No	No	2.00
3488	34.88	180.87	25.09	2.03	0.30	0.97	165.05	59.17	224.22	4.000	No	No	2.00
3489	34.89	181.34	24.74	2.02	0.30	0.97	165.46	58.44	223.90	4.000	No	No	2.00
3490	34.90	181.82	24.37	2.02	0.30	0.97	165.88	57.66	223.54	4.000	No	No	2.00
3491	34.91	182.29	24.01	2.01	0.30	0.97	166.29	56.87	223.16	4.000	No	No	2.00
3492	34.92	182.73	23.67	2.01	0.30	0.97	166.67	56.11	222.79	4.000	No	No	2.00
3493	34.93	183.09	23.38	2.00	0.30	0.97	167.00	55.44	222.44	4.000	No	No	2.00
3494	34.94	183.24	23.15	2.00	0.30	0.97	167.23	54.89	222.13	4.000	No	No	2.00
3495	34.95	183.18	22.95	2.00	0.30	0.96	167.00	54.36	221.36	4.000	No	No	2.00
3496	34.96	182.92	22.76	2.00	0.30	0.96	166.73	53.81	220.54	4.000	No	No	2.00
3497	34.97	182.62	22.54	1.99	0.30	0.96	166.42	53.18	219.59	4.000	No	No	2.00
3498	34.98	182.30	22.29	1.99	0.31	0.96	166.08	52.48	218.57	4.000	No	No	2.00
3499	34.99	181.98	22.05	1.99	0.31	0.96	165.75	51.76	217.51	4.000	No	No	2.00
3500	35.00	181.67	21.80	1.99	0.31	0.96	165.42	51.06	216.48	4.000	No	No	2.00
3501	35.01	181.39	21.58	1.98	0.31	0.96	165.12	50.40	215.52	4.000	No	No	2.00
3502	35.02	181.10	21.41	1.98	0.31	0.96	164.87	49.88	214.75	4.000	No	No	2.00
3503	35.03	180.67	21.30	1.98	0.31	0.96	164.52	49.53	214.05	4.000	No	No	2.00
3504	35.04	180.05	21.24	1.98	0.31	0.96	163.85	49.27	213.12	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3505	35.05	179.23	21.21	1.98	0.31	0.96	163.05	49.04	212.09	4.000	No	No	2.00
3506	35.06	178.32	21.16	1.98	0.32	0.96	162.16	48.79	210.96	3.718	No	No	2.00
3507	35.07	177.36	21.12	1.98	0.32	0.96	161.23	48.53	209.76	3.434	No	No	2.00
3508	35.08	176.41	21.07	1.98	0.32	0.96	160.31	48.27	208.58	3.178	No	No	2.00
3509	35.09	175.50	21.03	1.98	0.32	0.96	159.43	48.03	207.46	2.957	No	No	2.00
3510	35.10	174.70	20.99	1.97	0.32	0.96	158.65	47.81	206.46	2.777	No	No	2.00
3511	35.11	173.94	20.99	1.97	0.32	0.96	158.01	47.72	205.73	2.654	No	No	2.00
3512	35.12	173.07	21.05	1.98	0.32	0.96	157.24	47.76	205.00	2.537	No	No	2.00
3513	35.13	171.99	21.16	1.98	0.32	0.96	156.18	47.92	204.10	2.403	No	No	2.00
3514	35.14	170.71	21.30	1.98	0.33	0.96	154.96	48.13	203.09	2.262	No	No	2.00
3515	35.15	169.31	21.46	1.98	0.33	0.96	153.62	48.36	201.99	2.120	No	No	2.00
3516	35.16	167.87	21.62	1.98	0.33	0.96	152.25	48.60	200.85	1.985	No	No	2.00
3517	35.17	166.45	21.79	1.98	0.33	0.96	150.90	48.83	199.73	1.863	No	No	2.00
3518	35.18	165.15	21.94	1.99	0.33	0.96	149.66	49.04	198.69	1.759	No	No	1.94
3519	35.19	164.00	22.08	1.99	0.33	0.96	148.57	49.23	197.80	1.675	No	No	1.85
3520	35.20	162.86	22.25	1.99	0.33	0.96	147.69	49.53	197.23	1.624	No	No	1.79
3521	35.21	161.55	22.49	1.99	0.33	0.96	146.45	49.93	196.39	1.553	No	No	1.72
3522	35.22	159.93	22.81	2.00	0.34	0.96	144.91	50.48	195.39	1.473	No	No	1.63
3523	35.23	158.08	23.18	2.00	0.34	0.96	143.17	51.08	194.25	1.389	No	No	1.54
3524	35.24	156.11	23.57	2.01	0.34	0.96	141.30	51.70	193.01	1.304	No	No	1.44
3525	35.25	154.11	23.98	2.01	0.34	0.96	139.42	52.31	191.73	1.224	No	No	1.35
3526	35.26	152.18	24.38	2.02	0.34	0.96	137.61	52.87	190.47	1.151	No	No	1.27
3527	35.27	150.44	24.74	2.02	0.34	0.96	135.96	53.36	189.31	1.090	No	No	1.21
3528	35.28	148.95	25.05	2.03	0.35	0.96	134.57	53.77	188.33	1.041	No	No	1.15
3529	35.29	147.56	25.35	2.03	0.35	0.96	133.45	54.17	187.62	1.007	No	No	1.12
3530	35.30	146.10	25.66	2.03	0.35	0.96	132.10	54.55	186.65	0.964	No	No	1.07
3531	35.31	144.39	26.03	2.04	0.35	0.96	130.48	54.97	185.45	0.914	No	No	1.01
3532	35.32	142.48	26.44	2.04	0.35	0.96	128.69	55.42	184.11	0.862	No	No	0.95
3533	35.33	140.49	26.88	2.05	0.35	0.96	126.81	55.88	182.69	0.811	No	No	0.90
3534	35.34	138.50	27.32	2.05	0.36	0.96	124.94	56.30	181.25	0.765	No	No	0.84
3535	35.35	136.63	27.74	2.06	0.36	0.95	123.18	56.69	179.87	0.723	No	No	0.80
3536	35.36	134.97	28.12	2.06	0.36	0.95	121.61	57.02	178.63	0.689	No	No	0.76
3537	35.37	133.57	28.42	2.07	0.36	0.95	120.33	57.26	177.60	0.662	No	No	0.73
3538	35.38	132.29	28.68	2.07	0.36	0.95	119.30	57.46	176.76	0.641	No	No	0.71
3539	35.39	130.92	28.91	2.07	0.36	0.95	118.02	57.58	175.60	0.614	No	No	0.68
3540	35.40	129.35	29.18	2.08	0.37	0.95	116.53	57.70	174.23	0.584	No	No	0.64
3541	35.41	127.63	29.48	2.08	0.37	0.95	114.92	57.83	172.74	0.554	No	No	0.61
3542	35.42	125.87	29.80	2.08	0.37	0.95	113.26	57.95	171.21	0.525	No	No	0.58
3543	35.43	124.15	30.11	2.09	0.37	0.95	111.64	58.07	169.71	0.499	No	No	0.55
3544	35.44	122.55	30.40	2.09	0.37	0.95	110.14	58.17	168.31	0.477	No	No	0.52
3545	35.45	121.19	30.66	2.10	0.38	0.95	108.83	58.25	167.09	0.459	No	No	0.50
3546	35.46	120.09	30.85	2.10	0.38	0.95	107.84	58.31	166.15	0.445	No	No	0.49
3547	35.47	119.14	31.01	2.10	0.38	0.95	107.09	58.37	165.46	0.436	No	No	0.48
3548	35.48	118.16	31.16	2.10	0.38	0.95	106.17	58.37	164.53	0.424	No	No	0.46
3549	35.49	117.05	31.33	2.10	0.38	0.95	105.11	58.37	163.48	0.411	No	No	0.45
3550	35.50	115.86	31.51	2.11	0.38	0.95	104.00	58.37	162.36	0.397	No	No	0.43
3551	35.51	114.66	31.70	2.11	0.39	0.95	102.87	58.37	161.23	0.385	No	No	0.42
3552	35.52	113.51	31.89	2.11	0.39	0.95	101.78	58.37	160.15	0.373	No	No	0.41

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3553	35.53	112.47	32.06	2.11	0.39	0.95	100.80	58.37	159.16	0.363	No	No	0.40
3554	35.54	111.62	32.21	2.12	0.39	0.95	99.97	58.37	158.34	0.355	No	No	0.39
3555	35.55	110.98	32.34	2.12	0.39	0.95	99.44	58.42	157.86	0.351	No	No	0.38
3556	35.56	110.45	32.49	2.12	0.39	0.95	99.00	58.50	157.50	0.347	No	No	0.38
3557	35.57	109.90	32.66	2.12	0.39	0.95	98.48	58.59	157.07	0.343	No	No	0.37
3558	35.58	109.29	32.85	2.12	0.39	0.95	97.90	58.69	156.59	0.339	No	No	0.37
3559	35.59	108.65	33.05	2.13	0.39	0.95	97.30	58.78	156.08	0.335	No	No	0.36
3560	35.60	108.02	33.25	2.13	0.39	0.95	96.70	58.88	155.58	0.331	No	No	0.36
3561	35.61	107.42	33.44	2.13	0.40	0.95	96.14	58.97	155.10	0.327	No	No	0.36
3562	35.62	106.89	33.61	2.13	0.40	0.95	95.63	59.04	154.68	0.323	No	No	0.35
3563	35.63	106.46	33.77	2.13	0.40	0.95	95.22	59.13	154.35	0.320	No	No	0.35
3564	35.64	106.08	33.95	2.14	0.40	0.95	94.93	59.26	154.19	0.319	No	No	0.35
3565	35.65	105.70	34.17	2.14	0.40	0.95	94.58	59.42	153.99	0.318	No	No	0.35
3566	35.66	105.27	34.43	2.14	0.40	0.95	94.17	59.60	153.77	0.316	No	No	0.34
3567	35.67	104.81	34.71	2.15	0.40	0.95	93.73	59.79	153.52	0.314	No	No	0.34
3568	35.68	104.33	35.00	2.15	0.40	0.95	93.28	59.98	153.26	0.312	No	No	0.34
3569	35.69	103.86	35.28	2.15	0.40	0.95	92.84	60.16	153.00	0.310	No	No	0.34
3570	35.70	103.42	35.54	2.16	0.40	0.95	92.43	60.32	152.75	0.308	No	No	0.34
3571	35.71	103.06	35.76	2.16	0.40	0.95	92.07	60.46	152.53	0.307	No	No	0.33
3572	35.72	102.78	35.95	2.16	0.40	0.95	91.81	60.58	152.38	0.305	No	No	0.33
3573	35.73	102.57	36.12	2.16	0.40	0.95	91.65	60.71	152.36	0.305	No	No	0.33
3574	35.74	102.37	36.30	2.17	0.40	0.95	91.46	60.84	152.30	0.305	No	No	0.33
3575	35.75	102.15	36.51	2.17	0.40	0.95	91.25	60.98	152.23	0.304	No	No	0.33
3576	35.76	101.91	36.73	2.17	0.40	0.95	91.02	61.13	152.15	0.304	No	No	0.33
3577	35.77	101.67	36.95	2.17	0.40	0.95	90.79	61.28	152.07	0.303	No	No	0.33
3578	35.78	101.44	37.16	2.18	0.40	0.95	90.57	61.42	151.99	0.303	No	No	0.33
3579	35.79	101.23	37.35	2.18	0.40	0.94	90.37	61.54	151.91	0.302	No	No	0.33
3580	35.80	101.09	37.50	2.18	0.40	0.94	90.20	61.63	151.83	0.301	No	No	0.33
3581	35.81	101.03	37.59	2.18	0.40	0.94	90.14	61.69	151.84	0.301	No	No	0.33
3582	35.82	101.05	37.62	2.18	0.40	0.94	90.19	61.74	151.92	0.302	No	No	0.33
3583	35.83	101.12	37.64	2.18	0.40	0.94	90.24	61.77	152.01	0.303	No	No	0.33
3584	35.84	101.20	37.67	2.18	0.40	0.94	90.31	61.80	152.11	0.303	No	No	0.33
3585	35.85	101.28	37.69	2.18	0.40	0.94	90.37	61.83	152.21	0.304	No	No	0.33
3586	35.86	101.36	37.71	2.18	0.40	0.94	90.44	61.87	152.30	0.305	No	No	0.33
3587	35.87	101.43	37.73	2.18	0.40	0.94	90.50	61.90	152.40	0.306	No	No	0.33
3588	35.88	101.50	37.75	2.18	0.40	0.94	90.55	61.93	152.48	0.306	No	No	0.33
3589	35.89	101.60	37.74	2.18	0.40	0.94	90.59	61.93	152.52	0.306	No	No	0.33
3590	35.90	101.76	37.68	2.18	0.40	0.94	90.74	61.91	152.65	0.307	No	No	0.33
3591	35.91	102.00	37.57	2.18	0.40	0.94	90.96	61.87	152.82	0.309	No	No	0.34
3592	35.92	102.29	37.43	2.18	0.40	0.94	91.21	61.81	153.02	0.310	No	No	0.34
3593	35.93	102.60	37.28	2.18	0.40	0.94	91.49	61.74	153.23	0.312	No	No	0.34
3594	35.94	102.92	37.13	2.18	0.40	0.94	91.77	61.67	153.45	0.313	No	No	0.34
3595	35.95	103.23	36.98	2.17	0.40	0.94	92.05	61.60	153.66	0.315	No	No	0.34
3596	35.96	103.52	36.85	2.17	0.40	0.94	92.31	61.54	153.85	0.316	No	No	0.34
3597	35.97	103.77	36.73	2.17	0.40	0.94	92.53	61.48	154.01	0.318	No	No	0.35
3598	35.98	103.99	36.61	2.17	0.40	0.94	92.70	61.40	154.10	0.318	No	No	0.35
3599	35.99	104.22	36.46	2.17	0.40	0.94	92.89	61.31	154.19	0.319	No	No	0.35
3600	36.00	104.48	36.27	2.17	0.40	0.94	93.12	61.19	154.30	0.320	No	No	0.35

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3601	36.01	104.78	36.06	2.16	0.40	0.94	93.38	61.04	154.42	0.321	No	No	0.35
3602	36.02	105.10	35.83	2.16	0.40	0.94	93.66	60.89	154.55	0.322	No	No	0.35
3603	36.03	105.42	35.60	2.16	0.40	0.94	93.94	60.73	154.67	0.323	No	No	0.35
3604	36.04	105.72	35.37	2.15	0.40	0.94	94.21	60.57	154.78	0.324	No	No	0.35
3605	36.05	106.00	35.17	2.15	0.40	0.94	94.46	60.42	154.88	0.325	No	No	0.35
3606	36.06	106.23	35.00	2.15	0.40	0.94	94.66	60.29	154.95	0.325	No	No	0.35
3607	36.07	106.42	34.81	2.15	0.40	0.94	94.80	60.14	154.93	0.325	No	No	0.35
3608	36.08	106.60	34.60	2.15	0.40	0.94	94.94	59.95	154.90	0.325	No	No	0.35
3609	36.09	106.81	34.34	2.14	0.40	0.94	95.12	59.72	154.84	0.324	No	No	0.35
3610	36.10	107.04	34.06	2.14	0.40	0.94	95.32	59.46	154.78	0.324	No	No	0.35
3611	36.11	107.28	33.76	2.13	0.40	0.94	95.52	59.18	154.71	0.323	No	No	0.35
3612	36.12	107.52	33.46	2.13	0.40	0.94	95.73	58.90	154.62	0.323	No	No	0.35
3613	36.13	107.74	33.17	2.13	0.40	0.94	95.92	58.62	154.54	0.322	No	No	0.35
3614	36.14	107.94	32.92	2.12	0.40	0.94	96.09	58.37	154.46	0.321	No	No	0.35
3615	36.15	108.08	32.74	2.12	0.40	0.94	96.22	58.19	154.41	0.321	No	No	0.35
3616	36.16	108.18	32.61	2.12	0.40	0.94	96.26	58.06	154.32	0.320	No	No	0.35
3617	36.17	108.24	32.53	2.12	0.40	0.94	96.31	57.97	154.28	0.320	No	No	0.35
3618	36.18	108.32	32.44	2.12	0.40	0.94	96.36	57.88	154.24	0.320	No	No	0.35
3619	36.19	108.39	32.34	2.12	0.40	0.94	96.42	57.77	154.20	0.319	No	No	0.35
3620	36.20	108.47	32.24	2.12	0.40	0.94	96.49	57.67	154.15	0.319	No	No	0.35
3621	36.21	108.55	32.14	2.11	0.40	0.94	96.54	57.56	154.11	0.319	No	No	0.35
3622	36.22	108.62	32.05	2.11	0.40	0.94	96.60	57.47	154.06	0.318	No	No	0.35
3623	36.23	108.68	31.98	2.11	0.40	0.94	96.64	57.39	154.04	0.318	No	No	0.35
3624	36.24	108.72	31.99	2.11	0.40	0.94	96.67	57.40	154.08	0.318	No	No	0.35
3625	36.25	108.73	32.07	2.11	0.40	0.94	96.66	57.50	154.17	0.319	No	No	0.35
3626	36.26	108.73	32.22	2.12	0.40	0.94	96.66	57.68	154.34	0.320	No	No	0.35
3627	36.27	108.73	32.38	2.12	0.40	0.94	96.65	57.87	154.53	0.322	No	No	0.35
3628	36.28	108.73	32.56	2.12	0.40	0.94	96.65	58.08	154.73	0.323	No	No	0.35
3629	36.29	108.73	32.74	2.12	0.40	0.94	96.64	58.28	154.93	0.325	No	No	0.35
3630	36.30	108.73	32.91	2.12	0.40	0.94	96.64	58.48	155.11	0.327	No	No	0.36
3631	36.31	108.73	33.06	2.13	0.39	0.94	96.63	58.65	155.28	0.328	No	No	0.36
3632	36.32	108.72	33.21	2.13	0.39	0.94	96.63	58.81	155.44	0.329	No	No	0.36
3633	36.33	108.70	33.39	2.13	0.39	0.94	96.60	59.02	155.61	0.331	No	No	0.36
3634	36.34	108.64	33.64	2.13	0.39	0.94	96.54	59.28	155.82	0.333	No	No	0.36
3635	36.35	108.58	33.95	2.14	0.39	0.94	96.47	59.60	156.07	0.335	No	No	0.36
3636	36.36	108.50	34.29	2.14	0.39	0.94	96.40	59.95	156.35	0.337	No	No	0.37
3637	36.37	108.42	34.64	2.15	0.39	0.94	96.32	60.29	156.62	0.339	No	No	0.37
3638	36.38	108.34	34.98	2.15	0.39	0.94	96.25	60.63	156.88	0.342	No	No	0.37
3639	36.39	108.27	35.30	2.15	0.39	0.94	96.18	60.93	157.11	0.344	No	No	0.37
3640	36.40	108.20	35.57	2.16	0.39	0.94	96.11	61.20	157.31	0.346	No	No	0.38
3641	36.41	108.12	35.83	2.16	0.39	0.94	96.06	61.43	157.49	0.347	No	No	0.38
3642	36.42	107.99	36.09	2.16	0.39	0.94	95.93	61.66	157.59	0.348	No	No	0.38
3643	36.43	107.81	36.41	2.17	0.39	0.94	95.75	61.93	157.68	0.349	No	No	0.38
3644	36.44	107.59	36.78	2.17	0.39	0.94	95.55	62.22	157.77	0.350	No	No	0.38
3645	36.45	107.35	37.17	2.18	0.39	0.94	95.33	62.53	157.86	0.351	No	No	0.38
3646	36.46	107.11	37.56	2.18	0.39	0.94	95.10	62.83	157.94	0.351	No	No	0.38
3647	36.47	106.88	37.95	2.19	0.39	0.94	94.88	63.12	158.00	0.352	No	No	0.38
3648	36.48	106.67	38.29	2.19	0.39	0.94	94.68	63.37	158.05	0.353	No	No	0.38

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3649	36.49	106.48	38.59	2.19	0.39	0.94	94.50	63.58	158.08	0.353	No	No	0.38
3650	36.50	106.31	38.83	2.20	0.39	0.94	94.36	63.75	158.11	0.353	No	No	0.38
3651	36.51	106.14	39.05	2.20	0.39	0.94	94.21	63.89	158.10	0.353	No	No	0.38
3652	36.52	105.94	39.27	2.20	0.39	0.94	94.02	64.03	158.05	0.352	No	No	0.38
3653	36.53	105.72	39.53	2.21	0.39	0.94	93.80	64.18	157.99	0.352	No	No	0.38
3654	36.54	105.48	39.80	2.21	0.39	0.94	93.58	64.34	157.92	0.351	No	No	0.38
3655	36.55	105.24	40.07	2.21	0.39	0.94	93.35	64.50	157.85	0.351	No	No	0.38
3656	36.56	105.02	40.32	2.22	0.39	0.94	93.13	64.65	157.78	0.350	No	No	0.38
3657	36.57	104.81	40.55	2.22	0.39	0.94	92.93	64.78	157.71	0.349	No	No	0.38
3658	36.58	104.65	40.73	2.22	0.39	0.94	92.77	64.87	157.64	0.349	No	No	0.38
3659	36.59	104.54	40.87	2.22	0.39	0.94	92.68	64.95	157.63	0.349	No	No	0.38
3660	36.60	104.47	40.98	2.22	0.39	0.94	92.62	65.02	157.63	0.349	No	No	0.38
3661	36.61	104.40	41.09	2.23	0.39	0.94	92.54	65.08	157.62	0.349	No	No	0.38
3662	36.62	104.32	41.21	2.23	0.39	0.94	92.46	65.15	157.61	0.348	No	No	0.38
3663	36.63	104.24	41.33	2.23	0.39	0.94	92.38	65.22	157.60	0.348	No	No	0.38
3664	36.64	104.16	41.45	2.23	0.39	0.94	92.30	65.29	157.59	0.348	No	No	0.38
3665	36.65	104.09	41.57	2.23	0.39	0.94	92.22	65.35	157.58	0.348	No	No	0.38
3666	36.66	104.02	41.67	2.23	0.39	0.94	92.15	65.41	157.57	0.348	No	No	0.38
3667	36.67	103.98	41.74	2.23	0.39	0.94	92.10	65.45	157.55	0.348	No	No	0.38
3668	36.68	103.96	41.79	2.23	0.39	0.94	92.08	65.48	157.56	0.348	No	No	0.38
3669	36.69	103.96	41.82	2.24	0.39	0.94	92.07	65.50	157.58	0.348	No	No	0.38
3670	36.70	103.96	41.86	2.24	0.39	0.94	92.07	65.52	157.59	0.348	No	No	0.38
3671	36.71	103.96	41.89	2.24	0.39	0.94	92.06	65.55	157.61	0.348	No	No	0.38
3672	36.72	103.96	41.93	2.24	0.39	0.94	92.05	65.57	157.62	0.348	No	No	0.38
3673	36.73	103.96	41.97	2.24	0.39	0.94	92.04	65.60	157.64	0.349	No	No	0.38
3674	36.74	103.96	42.00	2.24	0.39	0.94	92.03	65.62	157.65	0.349	No	No	0.38
3675	36.75	103.96	42.04	2.24	0.39	0.94	92.02	65.64	157.66	0.349	No	No	0.38
3676	36.76	103.94	42.08	2.24	0.39	0.94	92.00	65.67	157.67	0.349	No	No	0.38
3677	36.77	103.89	42.14	2.24	0.39	0.94	91.94	65.69	157.63	0.349	No	No	0.38
3678	36.78	103.83	42.21	2.24	0.39	0.94	91.87	65.73	157.60	0.348	No	No	0.38
3679	36.79	103.75	42.29	2.24	0.39	0.94	91.79	65.77	157.56	0.348	No	No	0.38
3680	36.80	103.67	42.38	2.24	0.39	0.94	91.71	65.81	157.52	0.348	No	No	0.38
3681	36.81	103.59	42.47	2.24	0.39	0.94	91.63	65.85	157.48	0.347	No	No	0.38
3682	36.82	103.52	42.56	2.24	0.39	0.94	91.55	65.89	157.44	0.347	No	No	0.38
3683	36.83	103.45	42.63	2.25	0.39	0.94	91.48	65.92	157.40	0.346	No	No	0.38
3684	36.84	103.38	42.71	2.25	0.39	0.94	91.42	65.96	157.38	0.346	No	No	0.38
3685	36.85	103.30	42.80	2.25	0.39	0.94	91.34	66.00	157.34	0.346	No	No	0.38
3686	36.86	103.18	42.93	2.25	0.39	0.94	91.22	66.06	157.28	0.345	No	No	0.38
3687	36.87	103.04	43.08	2.25	0.39	0.94	91.09	66.13	157.21	0.345	No	No	0.37
3688	36.88	102.89	43.24	2.25	0.39	0.94	90.94	66.20	157.13	0.344	No	No	0.37
3689	36.89	102.73	43.41	2.26	0.39	0.94	90.78	66.27	157.05	0.343	No	No	0.37
3690	36.90	102.57	43.58	2.26	0.39	0.94	90.63	66.34	156.97	0.343	No	No	0.37
3691	36.91	102.42	43.74	2.26	0.39	0.94	90.48	66.41	156.89	0.342	No	No	0.37
3692	36.92	102.29	43.87	2.26	0.39	0.94	90.35	66.47	156.82	0.341	No	No	0.37
3693	36.93	102.15	43.99	2.26	0.39	0.93	90.25	66.52	156.77	0.341	No	No	0.37
3694	36.94	101.96	44.10	2.26	0.39	0.93	90.07	66.54	156.60	0.339	No	No	0.37
3695	36.95	101.72	44.22	2.27	0.39	0.93	89.82	66.55	156.38	0.337	No	No	0.37
3696	36.96	101.42	44.35	2.27	0.39	0.93	89.55	66.57	156.11	0.335	No	No	0.36

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3697	36.97	101.11	44.49	2.27	0.39	0.93	89.25	66.58	155.83	0.333	No	No	0.36
3698	36.98	100.79	44.64	2.27	0.39	0.93	88.94	66.60	155.54	0.330	No	No	0.36
3699	36.99	100.48	44.78	2.27	0.39	0.93	88.65	66.61	155.26	0.328	No	No	0.36
3700	37.00	100.19	44.92	2.27	0.40	0.93	88.38	66.62	155.00	0.326	No	No	0.35
3701	37.01	99.96	45.02	2.28	0.40	0.93	88.14	66.63	154.77	0.324	No	No	0.35
3702	37.02	99.78	45.08	2.28	0.40	0.93	87.98	66.62	154.60	0.322	No	No	0.35
3703	37.03	99.64	45.10	2.28	0.40	0.93	87.87	66.60	154.47	0.321	No	No	0.35
3704	37.04	99.51	45.09	2.28	0.40	0.93	87.73	66.56	154.30	0.320	No	No	0.35
3705	37.05	99.36	45.07	2.28	0.40	0.93	87.58	66.52	154.10	0.318	No	No	0.35
3706	37.06	99.20	45.06	2.28	0.40	0.93	87.43	66.47	153.90	0.317	No	No	0.34
3707	37.07	99.04	45.05	2.28	0.40	0.93	87.27	66.42	153.69	0.315	No	No	0.34
3708	37.08	98.89	45.03	2.28	0.40	0.93	87.12	66.37	153.49	0.314	No	No	0.34
3709	37.09	98.75	45.02	2.28	0.40	0.93	86.98	66.33	153.32	0.312	No	No	0.34
3710	37.10	98.66	44.99	2.27	0.40	0.93	86.87	66.28	153.15	0.311	No	No	0.34
3711	37.11	98.64	44.91	2.27	0.40	0.93	86.85	66.23	153.08	0.311	No	No	0.34
3712	37.12	98.68	44.78	2.27	0.40	0.93	86.89	66.16	153.05	0.310	No	No	0.34
3713	37.13	98.75	44.60	2.27	0.40	0.93	86.95	66.07	153.01	0.310	No	No	0.34
3714	37.14	98.83	44.41	2.27	0.40	0.93	87.01	65.96	152.97	0.310	No	No	0.34
3715	37.15	98.91	44.20	2.27	0.40	0.93	87.07	65.85	152.92	0.309	No	No	0.34
3716	37.16	98.98	44.00	2.26	0.40	0.93	87.13	65.74	152.86	0.309	No	No	0.33
3717	37.17	99.06	43.81	2.26	0.40	0.93	87.18	65.63	152.81	0.309	No	No	0.33
3718	37.18	99.12	43.65	2.26	0.40	0.93	87.23	65.53	152.77	0.308	No	No	0.33
3719	37.19	99.16	43.54	2.26	0.40	0.93	87.27	65.48	152.75	0.308	No	No	0.33
3720	37.20	99.18	43.50	2.26	0.40	0.93	87.26	65.45	152.71	0.308	No	No	0.33
3721	37.21	99.18	43.51	2.26	0.40	0.93	87.25	65.45	152.70	0.308	No	No	0.33
3722	37.22	99.18	43.52	2.26	0.40	0.93	87.24	65.46	152.70	0.308	No	No	0.33
3723	37.23	99.18	43.53	2.26	0.40	0.93	87.23	65.46	152.70	0.308	No	No	0.33
3724	37.24	99.18	43.55	2.26	0.40	0.93	87.22	65.47	152.69	0.308	No	No	0.33
3725	37.25	99.18	43.56	2.26	0.40	0.93	87.21	65.47	152.69	0.308	No	No	0.33
3726	37.26	99.18	43.57	2.26	0.40	0.93	87.21	65.48	152.68	0.308	No	No	0.33
3727	37.27	99.19	43.56	2.26	0.40	0.93	87.20	65.47	152.67	0.308	No	No	0.33
3728	37.28	99.24	43.50	2.26	0.40	0.93	87.21	65.43	152.64	0.307	No	No	0.33
3729	37.29	99.33	43.35	2.25	0.40	0.93	87.30	65.36	152.66	0.307	No	No	0.33
3730	37.30	99.46	43.13	2.25	0.40	0.93	87.41	65.24	152.65	0.307	No	No	0.33
3731	37.31	99.61	42.88	2.25	0.40	0.93	87.53	65.11	152.64	0.307	No	No	0.33
3732	37.32	99.77	42.61	2.25	0.40	0.93	87.67	64.96	152.63	0.307	No	No	0.33
3733	37.33	99.93	42.35	2.24	0.40	0.93	87.80	64.81	152.61	0.307	No	No	0.33
3734	37.34	100.08	42.09	2.24	0.40	0.93	87.93	64.67	152.59	0.307	No	No	0.33
3735	37.35	100.22	41.86	2.24	0.40	0.93	88.04	64.53	152.57	0.307	No	No	0.33
3736	37.36	100.32	41.65	2.23	0.40	0.93	88.13	64.41	152.54	0.307	No	No	0.33
3737	37.37	100.40	41.43	2.23	0.40	0.93	88.18	64.26	152.44	0.306	No	No	0.33
3738	37.38	100.47	41.16	2.23	0.40	0.93	88.22	64.08	152.29	0.305	No	No	0.33
3739	37.39	100.54	40.83	2.22	0.40	0.93	88.27	63.85	152.11	0.303	No	No	0.33
3740	37.40	100.62	40.47	2.22	0.40	0.93	88.32	63.59	151.91	0.302	No	No	0.33
3741	37.41	100.69	40.09	2.21	0.40	0.93	88.38	63.32	151.70	0.300	No	No	0.33
3742	37.42	100.77	39.71	2.21	0.40	0.93	88.43	63.04	151.47	0.299	No	No	0.32
3743	37.43	100.85	39.35	2.20	0.40	0.93	88.48	62.77	151.25	0.297	No	No	0.32
3744	37.44	100.91	39.04	2.20	0.40	0.93	88.53	62.53	151.05	0.296	No	No	0.32

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3745	37.45	100.92	38.94	2.20	0.40	0.93	88.56	62.46	151.02	0.296	No	No	0.32
3746	37.46	100.86	39.07	2.20	0.40	0.93	88.47	62.54	151.01	0.296	No	No	0.32
3747	37.47	100.74	39.43	2.21	0.40	0.93	88.35	62.80	151.15	0.297	No	No	0.32
3748	37.48	100.59	39.85	2.21	0.40	0.93	88.21	63.09	151.31	0.298	No	No	0.32
3749	37.49	100.43	40.29	2.22	0.40	0.93	88.07	63.40	151.47	0.299	No	No	0.32
3750	37.50	100.27	40.74	2.22	0.40	0.93	87.92	63.69	151.62	0.300	No	No	0.32
3751	37.51	100.12	41.16	2.23	0.40	0.93	87.78	63.97	151.75	0.301	No	No	0.33
3752	37.52	99.98	41.55	2.23	0.40	0.93	87.64	64.22	151.86	0.302	No	No	0.33
3753	37.53	99.86	41.87	2.24	0.40	0.93	87.53	64.41	151.94	0.302	No	No	0.33
3754	37.54	99.75	42.13	2.24	0.40	0.93	87.44	64.57	152.01	0.303	No	No	0.33
3755	37.55	99.63	42.35	2.24	0.40	0.93	87.33	64.70	152.03	0.303	No	No	0.33
3756	37.56	99.50	42.59	2.24	0.40	0.93	87.20	64.83	152.03	0.303	No	No	0.33
3757	37.57	99.35	42.85	2.25	0.40	0.93	87.06	64.97	152.03	0.303	No	No	0.33
3758	37.58	99.19	43.13	2.25	0.40	0.93	86.91	65.12	152.02	0.303	No	No	0.33
3759	37.59	99.03	43.40	2.26	0.40	0.93	86.76	65.26	152.02	0.303	No	No	0.33
3760	37.60	98.88	43.66	2.26	0.40	0.93	86.61	65.39	152.00	0.303	No	No	0.33
3761	37.61	98.74	43.90	2.26	0.40	0.93	86.48	65.51	151.99	0.303	No	No	0.33
3762	37.62	98.62	44.10	2.26	0.40	0.93	86.37	65.61	151.98	0.302	No	No	0.33
3763	37.63	98.51	44.28	2.27	0.40	0.93	86.28	65.70	151.98	0.302	No	No	0.33
3764	37.64	98.39	44.49	2.27	0.40	0.93	86.16	65.80	151.96	0.302	No	No	0.33
3765	37.65	98.25	44.73	2.27	0.40	0.93	86.03	65.91	151.94	0.302	No	No	0.33
3766	37.66	98.10	44.98	2.27	0.40	0.93	85.88	66.03	151.91	0.302	No	No	0.33
3767	37.67	97.94	45.25	2.28	0.40	0.93	85.73	66.15	151.88	0.302	No	No	0.33
3768	37.68	97.78	45.51	2.28	0.40	0.93	85.58	66.26	151.84	0.302	No	No	0.33
3769	37.69	97.64	45.75	2.28	0.40	0.93	85.44	66.37	151.81	0.301	No	No	0.33
3770	37.70	97.51	45.96	2.29	0.40	0.93	85.31	66.46	151.77	0.301	No	No	0.33
3771	37.71	97.39	46.19	2.29	0.40	0.93	85.21	66.57	151.78	4.000	Yes	No	2.00
3772	37.72	97.28	46.49	2.29	0.40	0.93	85.12	66.71	151.83	4.000	Yes	No	2.00
3773	37.73	97.16	46.88	2.30	0.40	0.93	84.99	66.90	151.89	4.000	Yes	No	2.00
3774	37.74	97.01	47.33	2.30	0.40	0.93	84.86	67.11	151.97	4.000	Yes	No	2.00
3775	37.75	96.85	47.80	2.31	0.40	0.93	84.71	67.32	152.03	4.000	Yes	No	2.00
3776	37.76	96.69	48.27	2.32	0.40	0.93	84.56	67.53	152.09	4.000	Yes	No	2.00
3777	37.77	96.54	48.73	2.32	0.40	0.93	84.42	67.73	152.14	4.000	Yes	No	2.00
3778	37.78	96.40	49.13	2.33	0.40	0.93	84.28	67.90	152.18	4.000	Yes	No	2.00
3779	37.79	96.27	49.49	2.33	0.40	0.93	84.17	68.05	152.21	4.000	Yes	No	2.00
3780	37.80	96.11	49.82	2.34	0.40	0.93	84.05	68.18	152.23	4.000	Yes	No	2.00
3781	37.81	95.90	50.18	2.34	0.40	0.93	83.84	68.30	152.14	4.000	Yes	No	2.00
3782	37.82	95.63	50.61	2.35	0.40	0.93	83.59	68.44	152.02	4.000	Yes	No	2.00
3783	37.83	95.33	51.08	2.35	0.40	0.93	83.31	68.58	151.89	4.000	Yes	No	2.00
3784	37.84	95.01	51.58	2.36	0.40	0.92	83.01	68.73	151.74	4.000	Yes	No	2.00
3785	37.85	94.69	52.06	2.36	0.40	0.92	82.71	68.87	151.58	4.000	Yes	No	2.00
3786	37.86	94.39	52.52	2.37	0.40	0.92	82.43	68.99	151.43	4.000	Yes	No	2.00
3787	37.87	94.12	52.93	2.37	0.40	0.92	82.18	69.10	151.28	4.000	Yes	No	2.00
3788	37.88	93.88	53.29	2.38	0.40	0.92	81.97	69.20	151.17	4.000	Yes	No	2.00
3789	37.89	93.63	53.67	2.38	0.40	0.92	81.76	69.30	151.06	4.000	Yes	No	2.00
3790	37.90	93.33	54.11	2.39	0.40	0.92	81.48	69.40	150.88	4.000	Yes	No	2.00
3791	37.91	92.98	54.63	2.40	0.40	0.92	81.15	69.52	150.67	4.000	Yes	No	2.00
3792	37.92	92.59	55.19	2.40	0.40	0.92	80.79	69.65	150.44	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3793	37.93	92.19	55.76	2.41	0.40	0.92	80.42	69.76	150.19	4.000	Yes	No	2.00
3794	37.94	91.80	56.31	2.42	0.40	0.92	80.06	69.87	149.93	4.000	Yes	No	2.00
3795	37.95	91.43	56.82	2.42	0.40	0.92	79.72	69.97	149.69	4.000	Yes	No	2.00
3796	37.96	91.12	57.27	2.43	0.40	0.92	79.42	70.05	149.47	4.000	Yes	No	2.00
3797	37.97	90.82	57.64	2.43	0.40	0.92	79.18	70.11	149.30	4.000	Yes	No	2.00
3798	37.98	90.50	58.00	2.44	0.40	0.92	78.89	70.16	149.06	4.000	Yes	No	2.00
3799	37.99	90.11	58.40	2.44	0.41	0.92	78.54	70.20	148.74	4.000	Yes	No	2.00
3800	38.00	89.67	58.84	2.45	0.41	0.92	78.13	70.24	148.37	4.000	Yes	No	2.00
3801	38.01	89.20	59.32	2.45	0.41	0.92	77.69	70.27	147.97	4.000	Yes	No	2.00
3802	38.02	88.72	59.80	2.46	0.41	0.92	77.25	70.31	147.55	4.000	Yes	No	2.00
3803	38.03	88.26	60.26	2.47	0.41	0.92	76.82	70.34	147.15	4.000	Yes	No	2.00
3804	38.04	87.84	60.68	2.47	0.41	0.92	76.42	70.36	146.78	4.000	Yes	No	2.00
3805	38.05	87.48	61.03	2.48	0.41	0.92	76.09	70.37	146.46	4.000	Yes	No	2.00
3806	38.06	87.20	61.29	2.48	0.41	0.92	75.85	70.39	146.24	4.000	Yes	No	2.00
3807	38.07	86.95	61.51	2.48	0.41	0.92	75.64	70.39	146.03	0.265	No	No	0.29
3808	38.08	86.68	61.73	2.48	0.41	0.92	75.38	70.39	145.77	0.263	No	No	0.28
3809	38.09	86.37	61.97	2.49	0.41	0.92	75.10	70.38	145.48	0.262	No	No	0.28
3810	38.10	86.06	62.22	2.49	0.41	0.92	74.80	70.37	145.17	0.260	No	No	0.28
3811	38.11	85.74	62.48	2.49	0.41	0.92	74.50	70.36	144.87	0.258	No	No	0.28
3812	38.12	85.44	62.72	2.50	0.41	0.92	74.22	70.35	144.57	0.257	No	No	0.28
3813	38.13	85.17	62.93	2.50	0.41	0.92	73.97	70.34	144.31	0.255	No	No	0.28
3814	38.14	85.10	63.03	2.50	0.41	0.92	73.76	70.31	144.07	0.254	No	No	0.27
3815	38.15	85.36	62.95	2.50	0.41	0.92	74.03	70.36	144.40	4.000	Yes	No	2.00
3816	38.16	85.95	62.69	2.50	0.41	0.92	74.63	70.46	145.09	4.000	Yes	No	2.00
3817	38.17	86.73	62.34	2.49	0.41	0.92	75.33	70.56	145.89	4.000	Yes	No	2.00
3818	38.18	87.59	61.96	2.49	0.41	0.92	76.10	70.66	146.76	4.000	Yes	No	2.00
3819	38.19	88.47	61.57	2.48	0.41	0.92	76.89	70.77	147.66	4.000	Yes	No	2.00
3820	38.20	89.33	61.19	2.48	0.41	0.92	77.67	70.87	148.54	4.000	Yes	No	2.00
3821	38.21	90.14	60.84	2.47	0.40	0.92	78.40	70.96	149.36	4.000	Yes	No	2.00
3822	38.22	90.84	60.53	2.47	0.40	0.92	79.03	71.04	150.07	4.000	Yes	No	2.00
3823	38.23	91.74	60.12	2.46	0.40	0.92	79.54	71.05	150.60	4.000	Yes	No	2.00
3824	38.24	93.00	59.52	2.46	0.40	0.92	80.80	71.21	152.01	4.000	Yes	No	2.00
3825	38.25	94.73	58.68	2.45	0.40	0.92	82.38	71.37	153.74	4.000	Yes	No	2.00
3826	38.26	96.72	57.72	2.43	0.39	0.92	84.18	71.53	155.71	4.000	Yes	No	2.00
3827	38.27	98.84	56.70	2.42	0.39	0.92	86.12	71.69	157.81	4.000	Yes	No	2.00
3828	38.28	101.01	55.66	2.41	0.39	0.92	88.09	71.83	159.92	4.000	Yes	No	2.00
3829	38.29	103.09	54.66	2.40	0.38	0.92	89.99	71.95	161.93	4.000	Yes	No	2.00
3830	38.30	104.99	53.76	2.38	0.38	0.92	91.72	72.04	163.76	4.000	Yes	No	2.00
3831	38.31	106.63	52.98	2.37	0.38	0.92	93.19	72.09	165.28	4.000	Yes	No	2.00
3832	38.32	108.17	52.25	2.37	0.38	0.92	94.38	72.09	166.47	4.000	Yes	No	2.00
3833	38.33	109.84	51.46	2.36	0.38	0.92	95.87	72.12	167.98	4.000	Yes	No	2.00
3834	38.34	111.81	50.54	2.34	0.37	0.93	97.67	72.14	169.81	4.000	Yes	No	2.00
3835	38.35	114.00	49.50	2.33	0.37	0.93	99.67	72.15	171.82	4.000	Yes	No	2.00
3836	38.36	116.31	48.41	2.32	0.37	0.93	101.79	72.11	173.90	4.000	Yes	No	2.00
3837	38.37	118.62	47.32	2.30	0.36	0.93	103.89	72.04	175.94	4.000	Yes	No	2.00
3838	38.38	120.80	46.28	2.29	0.36	0.93	105.89	71.94	177.83	4.000	Yes	No	2.00
3839	38.39	122.75	45.35	2.28	0.36	0.93	107.67	71.81	179.48	4.000	Yes	No	2.00
3840	38.40	124.30	44.67	2.27	0.36	0.93	109.14	71.74	180.87	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3841	38.41	125.59	44.23	2.27	0.35	0.93	110.08	71.68	181.76	4.000	Yes	No	2.00
3842	38.42	126.79	43.97	2.26	0.35	0.93	111.14	71.76	182.90	4.000	Yes	No	2.00
3843	38.43	128.14	43.71	2.26	0.35	0.93	112.38	71.90	184.28	4.000	Yes	No	2.00
3844	38.44	129.62	43.43	2.26	0.35	0.93	113.74	72.04	185.78	4.000	Yes	No	2.00
3845	38.45	131.14	43.15	2.25	0.35	0.93	115.14	72.19	187.32	4.000	Yes	No	2.00
3846	38.46	132.63	42.88	2.25	0.34	0.93	116.51	72.33	188.84	4.000	Yes	No	2.00
3847	38.47	134.02	42.63	2.25	0.34	0.93	117.79	72.46	190.25	4.000	Yes	No	2.00
3848	38.48	135.21	42.43	2.24	0.34	0.93	118.90	72.58	191.48	1.209	No	No	1.32
3849	38.49	135.93	42.43	2.24	0.34	0.93	119.74	72.80	192.54	1.274	No	No	1.39
3850	38.50	136.24	42.67	2.25	0.34	0.93	119.74	72.97	192.71	1.285	No	No	1.40
3851	38.51	136.24	43.13	2.25	0.34	0.93	119.74	73.32	193.06	1.307	No	No	1.42
3852	38.52	136.24	43.65	2.26	0.34	0.93	119.74	73.70	193.44	1.333	No	No	1.45
3853	38.53	136.24	44.19	2.26	0.34	0.93	119.74	74.09	193.83	1.360	No	No	1.48
3854	38.54	136.24	44.73	2.27	0.34	0.93	119.75	74.47	194.22	1.386	No	No	1.51
3855	38.55	136.25	45.25	2.28	0.34	0.93	119.75	74.82	194.57	1.412	No	No	1.54
3856	38.56	136.25	45.71	2.28	0.34	0.93	119.75	75.13	194.87	1.434	No	No	1.56
3857	38.57	136.17	46.11	2.29	0.34	0.93	119.75	75.39	195.14	1.454	No	No	1.58
3858	38.58	135.87	46.54	2.29	0.34	0.93	119.54	75.61	195.15	1.455	No	No	1.58
3859	38.59	135.29	47.04	2.30	0.34	0.93	118.91	75.76	194.67	1.419	No	No	1.54
3860	38.60	134.48	47.64	2.31	0.34	0.93	118.14	75.94	194.08	1.377	No	No	1.50
3861	38.61	133.57	48.31	2.32	0.34	0.93	117.30	76.12	193.41	1.331	No	No	1.45
3862	38.62	132.61	49.01	2.33	0.34	0.93	116.41	76.28	192.69	1.283	No	No	1.40
3863	38.63	131.66	49.70	2.33	0.34	0.93	115.52	76.43	191.95	1.237	No	No	1.35
3864	38.64	130.76	50.34	2.34	0.34	0.93	114.68	76.56	191.24	1.195	No	No	1.30
3865	38.65	129.95	50.90	2.35	0.34	0.93	113.93	76.66	190.58	1.158	No	No	1.26
3866	38.66	129.23	51.40	2.36	0.34	0.93	113.31	76.75	190.06	1.129	No	No	1.23
3867	38.67	128.46	51.91	2.36	0.34	0.93	112.67	76.83	189.50	1.100	No	No	1.20
3868	38.68	127.56	52.48	2.37	0.35	0.93	111.82	76.89	188.70	1.059	No	No	1.16
3869	38.69	126.49	53.15	2.38	0.35	0.93	110.82	76.94	187.76	1.014	No	No	1.11
3870	38.70	125.33	53.87	2.39	0.35	0.93	109.74	76.98	186.72	0.967	No	No	1.06
3871	38.71	124.13	54.61	2.40	0.35	0.93	108.62	77.01	185.63	0.921	No	No	1.01
3872	38.72	122.95	55.33	2.40	0.35	0.93	107.53	77.02	184.55	0.879	No	No	0.96
3873	38.73	121.86	55.99	2.41	0.35	0.93	106.51	77.02	183.53	0.841	No	No	0.92
3874	38.74	120.92	56.55	2.42	0.35	0.93	105.63	77.01	182.64	0.810	No	No	0.88
3875	38.75	120.17	56.98	2.42	0.35	0.93	104.94	76.99	181.93	0.786	No	No	0.86
3876	38.76	119.53	57.31	2.43	0.36	0.92	104.45	76.99	181.44	0.771	No	No	0.84
3877	38.77	118.88	57.62	2.43	0.36	0.92	103.84	76.94	180.78	0.750	No	No	0.82
3878	38.78	118.14	57.97	2.44	0.36	0.92	103.15	76.89	180.04	0.728	No	No	0.79
3879	38.79	117.35	58.34	2.44	0.36	0.92	102.41	76.82	179.24	0.705	No	No	0.77
3880	38.80	116.55	58.72	2.45	0.36	0.92	101.67	76.76	178.42	0.683	No	No	0.74
3881	38.81	115.79	59.08	2.45	0.36	0.92	100.95	76.69	177.64	0.663	No	No	0.72
3882	38.82	115.09	59.41	2.46	0.36	0.92	100.29	76.62	176.92	0.645	No	No	0.70
3883	38.83	114.58	59.64	2.46	0.36	0.92	99.74	76.55	176.29	0.630	No	No	0.69
3884	38.84	114.42	59.69	2.46	0.36	0.92	99.56	76.52	176.08	0.625	No	No	0.68
3885	38.85	114.57	59.56	2.46	0.36	0.92	99.81	76.54	176.35	0.631	No	No	0.69
3886	38.86	114.91	59.32	2.45	0.36	0.92	100.11	76.54	176.65	0.638	No	No	0.70
3887	38.87	115.29	59.05	2.45	0.36	0.92	100.45	76.54	176.99	0.646	No	No	0.70
3888	38.88	115.69	58.76	2.45	0.36	0.92	100.80	76.53	177.33	0.655	No	No	0.71

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3889	38.89	116.08	58.47	2.44	0.36	0.92	101.16	76.52	177.68	0.664	No	No	0.72
3890	38.90	116.46	58.20	2.44	0.36	0.92	101.49	76.51	178.00	0.672	No	No	0.73
3891	38.91	116.79	57.96	2.44	0.36	0.92	101.79	76.50	178.29	0.680	No	No	0.74
3892	38.92	117.22	57.68	2.43	0.36	0.92	102.03	76.46	178.49	0.685	No	No	0.75
3893	38.93	117.86	57.28	2.43	0.36	0.92	102.61	76.47	179.08	0.701	No	No	0.76
3894	38.94	118.80	56.71	2.42	0.36	0.92	103.50	76.49	179.99	0.727	No	No	0.79
3895	38.95	119.94	56.02	2.41	0.36	0.92	104.54	76.49	181.03	0.758	No	No	0.83
3896	38.96	121.18	55.26	2.40	0.35	0.92	105.67	76.49	182.16	0.794	No	No	0.87
3897	38.97	122.46	54.47	2.39	0.35	0.92	106.84	76.46	183.30	0.833	No	No	0.91
3898	38.98	123.72	53.69	2.38	0.35	0.92	107.98	76.42	184.40	0.873	No	No	0.95
3899	38.99	124.88	52.97	2.37	0.35	0.92	109.03	76.37	185.40	0.912	No	No	1.00
3900	39.00	125.89	52.33	2.37	0.35	0.92	109.95	76.31	186.26	0.947	No	No	1.03
3901	39.01	126.86	51.73	2.36	0.35	0.92	110.68	76.21	186.89	0.975	No	No	1.06
3902	39.02	127.93	51.08	2.35	0.35	0.92	111.63	76.14	187.77	1.014	No	No	1.11
3903	39.03	129.23	50.30	2.34	0.34	0.92	112.82	76.04	188.86	1.067	No	No	1.16
3904	39.04	130.71	49.40	2.33	0.34	0.92	114.17	75.91	190.08	1.130	No	No	1.23
3905	39.05	132.29	48.43	2.32	0.34	0.93	115.61	75.74	191.35	1.201	No	No	1.31
3906	39.06	133.89	47.43	2.31	0.34	0.93	117.07	75.53	192.59	1.277	No	No	1.39
3907	39.07	135.42	46.45	2.29	0.34	0.93	118.47	75.28	193.75	1.354	No	No	1.47
3908	39.08	136.82	45.56	2.28	0.34	0.93	119.74	75.03	194.76	1.426	No	No	1.55
3909	39.09	137.99	44.82	2.27	0.34	0.93	120.80	74.80	195.60	1.489	No	No	1.62
3910	39.10	139.01	44.22	2.27	0.33	0.93	121.60	74.58	196.18	1.536	No	No	1.67
3911	39.11	140.04	43.70	2.26	0.33	0.93	122.48	74.43	196.91	1.596	No	No	1.73
3912	39.12	141.20	43.14	2.25	0.33	0.93	123.55	74.28	197.82	1.677	No	No	1.82
3913	39.13	142.50	42.51	2.24	0.33	0.93	124.73	74.09	198.82	1.771	No	No	1.92
3914	39.14	143.85	41.85	2.24	0.33	0.93	125.96	73.87	199.84	1.874	No	No	2.00
3915	39.15	145.20	41.18	2.23	0.33	0.93	127.19	73.63	200.82	1.982	No	No	2.00
3916	39.16	146.47	40.55	2.22	0.33	0.93	128.35	73.38	201.73	2.088	No	No	2.00
3917	39.17	147.60	39.99	2.21	0.33	0.93	129.38	73.14	202.51	2.186	No	No	2.00
3918	39.18	148.54	39.58	2.21	0.33	0.93	130.22	72.97	203.18	2.274	No	No	2.00
3919	39.19	149.38	39.31	2.20	0.32	0.93	130.86	72.87	203.73	2.349	No	No	2.00
3920	39.20	150.25	39.13	2.20	0.32	0.93	131.64	72.89	204.54	2.467	No	No	2.00
3921	39.21	151.26	38.94	2.20	0.32	0.93	132.57	72.94	205.50	2.617	No	No	2.00
3922	39.22	152.35	38.74	2.20	0.32	0.93	133.57	72.98	206.55	2.793	No	No	2.00
3923	39.23	153.47	38.54	2.19	0.32	0.93	134.60	73.03	207.63	2.991	No	No	2.00
3924	39.24	154.56	38.34	2.19	0.32	0.93	135.61	73.07	208.69	3.200	No	No	2.00
3925	39.25	155.58	38.15	2.19	0.32	0.93	136.55	73.11	209.66	3.410	No	No	2.00
3926	39.26	156.45	38.00	2.19	0.32	0.93	137.35	73.15	210.50	3.607	No	No	2.00
3927	39.27	157.15	37.91	2.19	0.32	0.93	137.97	73.20	211.17	3.771	No	No	2.00
3928	39.28	157.78	37.86	2.19	0.31	0.93	138.45	73.27	211.72	3.914	No	No	2.00
3929	39.29	158.43	37.85	2.19	0.31	0.93	139.05	73.40	212.45	4.000	No	No	2.00
3930	39.30	159.18	37.83	2.19	0.31	0.93	139.74	73.54	213.28	4.000	No	No	2.00
3931	39.31	159.97	37.82	2.19	0.31	0.93	140.47	73.69	214.16	4.000	No	No	2.00
3932	39.32	160.77	37.80	2.18	0.31	0.93	141.21	73.85	215.06	4.000	No	No	2.00
3933	39.33	161.53	37.78	2.18	0.31	0.93	141.92	74.00	215.92	4.000	No	No	2.00
3934	39.34	162.23	37.77	2.18	0.31	0.93	142.56	74.14	216.70	4.000	No	No	2.00
3935	39.35	162.80	37.75	2.18	0.31	0.93	143.10	74.25	217.35	4.000	No	No	2.00
3936	39.36	163.28	37.72	2.18	0.31	0.93	143.47	74.30	217.77	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3937	39.37	163.71	37.66	2.18	0.31	0.93	143.84	74.32	218.16	4.000	No	No	2.00
3938	39.38	164.20	37.58	2.18	0.31	0.93	144.27	74.34	218.62	4.000	No	No	2.00
3939	39.39	164.73	37.49	2.18	0.31	0.93	144.76	74.36	219.12	4.000	No	No	2.00
3940	39.40	165.29	37.40	2.18	0.30	0.93	145.27	74.38	219.66	4.000	No	No	2.00
3941	39.41	165.84	37.31	2.18	0.30	0.93	145.78	74.40	220.18	4.000	No	No	2.00
3942	39.42	166.37	37.22	2.18	0.30	0.93	146.26	74.42	220.68	4.000	No	No	2.00
3943	39.43	166.83	37.15	2.18	0.30	0.93	146.68	74.44	221.12	4.000	No	No	2.00
3944	39.44	167.20	37.11	2.18	0.30	0.93	147.02	74.47	221.49	4.000	No	No	2.00
3945	39.45	167.53	37.09	2.18	0.30	0.93	147.25	74.51	221.77	4.000	No	No	2.00
3946	39.46	167.84	37.11	2.18	0.30	0.93	147.53	74.60	222.13	4.000	No	No	2.00
3947	39.47	168.20	37.14	2.18	0.30	0.93	147.88	74.71	222.59	4.000	No	No	2.00
3948	39.48	168.59	37.16	2.18	0.30	0.93	148.24	74.82	223.06	4.000	No	No	2.00
3949	39.49	168.99	37.19	2.18	0.30	0.93	148.60	74.93	223.54	4.000	No	No	2.00
3950	39.50	169.38	37.22	2.18	0.30	0.93	148.96	75.05	224.01	4.000	No	No	2.00
3951	39.51	169.74	37.24	2.18	0.30	0.93	149.29	75.15	224.44	4.000	No	No	2.00
3952	39.52	170.05	37.27	2.18	0.30	0.93	149.58	75.24	224.82	4.000	No	No	2.00
3953	39.53	170.25	37.31	2.18	0.30	0.93	149.78	75.34	225.12	4.000	No	No	2.00
3954	39.54	170.36	37.39	2.18	0.30	0.93	149.82	75.43	225.25	4.000	No	No	2.00
3955	39.55	170.43	37.49	2.18	0.30	0.93	149.87	75.55	225.43	4.000	No	No	2.00
3956	39.56	170.50	37.61	2.18	0.30	0.93	149.94	75.69	225.63	4.000	No	No	2.00
3957	39.57	170.58	37.73	2.18	0.30	0.93	150.00	75.84	225.85	4.000	No	No	2.00
3958	39.58	170.66	37.86	2.19	0.30	0.93	150.07	75.99	226.06	4.000	No	No	2.00
3959	39.59	170.74	37.98	2.19	0.30	0.93	150.14	76.13	226.27	4.000	No	No	2.00
3960	39.60	170.81	38.09	2.19	0.30	0.93	150.20	76.26	226.46	4.000	No	No	2.00
3961	39.61	170.88	38.14	2.19	0.30	0.93	150.24	76.33	226.57	4.000	No	No	2.00
3962	39.62	170.96	38.10	2.19	0.30	0.93	150.29	76.30	226.59	4.000	No	No	2.00
3963	39.63	171.07	37.96	2.19	0.30	0.93	150.38	76.17	226.56	4.000	No	No	2.00
3964	39.64	171.21	37.75	2.18	0.30	0.93	150.49	75.97	226.46	4.000	No	No	2.00
3965	39.65	171.36	37.51	2.18	0.30	0.93	150.61	75.74	226.35	4.000	No	No	2.00
3966	39.66	171.52	37.25	2.18	0.30	0.93	150.74	75.50	226.23	4.000	No	No	2.00
3967	39.67	171.67	37.00	2.18	0.30	0.93	150.86	75.25	226.11	4.000	No	No	2.00
3968	39.68	171.82	36.76	2.17	0.30	0.93	150.98	75.01	225.99	4.000	No	No	2.00
3969	39.69	171.95	36.55	2.17	0.30	0.93	151.08	74.80	225.87	4.000	No	No	2.00
3970	39.70	172.07	36.37	2.17	0.30	0.93	151.16	74.61	225.76	4.000	No	No	2.00
3971	39.71	172.18	36.20	2.16	0.30	0.93	151.23	74.43	225.65	4.000	No	No	2.00
3972	39.72	172.30	36.01	2.16	0.30	0.93	151.32	74.23	225.55	4.000	No	No	2.00
3973	39.73	172.45	35.79	2.16	0.30	0.93	151.43	74.00	225.43	4.000	No	No	2.00
3974	39.74	172.60	35.55	2.16	0.30	0.93	151.55	73.74	225.30	4.000	No	No	2.00
3975	39.75	172.76	35.30	2.15	0.30	0.93	151.68	73.47	225.15	4.000	No	No	2.00
3976	39.76	172.92	35.06	2.15	0.30	0.93	151.80	73.20	225.00	4.000	No	No	2.00
3977	39.77	173.06	34.83	2.15	0.30	0.93	151.91	72.95	224.86	4.000	No	No	2.00
3978	39.78	173.17	34.65	2.15	0.30	0.93	152.00	72.74	224.74	4.000	No	No	2.00
3979	39.79	173.13	34.57	2.14	0.30	0.93	152.03	72.65	224.68	4.000	No	No	2.00
3980	39.80	172.93	34.59	2.14	0.30	0.93	151.75	72.61	224.36	4.000	No	No	2.00
3981	39.81	172.58	34.70	2.15	0.30	0.93	151.41	72.67	224.07	4.000	No	No	2.00
3982	39.82	172.18	34.81	2.15	0.30	0.93	151.03	72.72	223.75	4.000	No	No	2.00
3983	39.83	171.76	34.93	2.15	0.30	0.93	150.62	72.78	223.41	4.000	No	No	2.00
3984	39.84	171.33	35.06	2.15	0.30	0.93	150.21	72.84	223.06	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
3985	39.85	170.92	35.17	2.15	0.30	0.93	149.82	72.90	222.72	4.000	No	No	2.00
3986	39.86	170.55	35.28	2.15	0.30	0.93	149.47	72.95	222.41	4.000	No	No	2.00
3987	39.87	170.19	35.40	2.16	0.30	0.93	149.17	73.03	222.19	4.000	No	No	2.00
3988	39.88	169.71	35.59	2.16	0.30	0.93	148.78	73.16	221.94	4.000	No	No	2.00
3989	39.89	169.05	35.86	2.16	0.30	0.93	148.12	73.33	221.46	4.000	No	No	2.00
3990	39.90	168.22	36.21	2.17	0.30	0.93	147.35	73.56	220.90	4.000	No	No	2.00
3991	39.91	167.30	36.60	2.17	0.30	0.93	146.49	73.80	220.28	4.000	No	No	2.00
3992	39.92	166.34	37.00	2.18	0.30	0.93	145.59	74.03	219.62	4.000	No	No	2.00
3993	39.93	165.39	37.40	2.18	0.31	0.93	144.70	74.25	218.96	4.000	No	No	2.00
3994	39.94	164.50	37.77	2.18	0.31	0.93	143.87	74.45	218.32	4.000	No	No	2.00
3995	39.95	163.71	38.10	2.19	0.31	0.93	143.13	74.61	217.74	4.000	No	No	2.00
3996	39.96	163.15	38.37	2.19	0.31	0.93	142.53	74.75	217.27	4.000	No	No	2.00
3997	39.97	162.77	38.62	2.20	0.31	0.93	142.30	74.94	217.24	4.000	No	No	2.00
3998	39.98	162.53	38.88	2.20	0.31	0.93	142.09	75.14	217.23	4.000	No	No	2.00
3999	39.99	162.26	39.18	2.20	0.31	0.93	141.84	75.37	217.21	4.000	No	No	2.00
4000	40.00	161.98	39.49	2.21	0.31	0.93	141.57	75.61	217.18	4.000	No	No	2.00
4001	40.01	161.68	39.81	2.21	0.31	0.93	141.30	75.84	217.14	4.000	No	No	2.00
4002	40.02	161.40	40.12	2.21	0.31	0.93	141.03	76.07	217.10	4.000	No	No	2.00
4003	40.03	161.14	40.41	2.22	0.31	0.92	140.78	76.27	217.05	4.000	No	No	2.00
4004	40.04	160.96	40.63	2.22	0.31	0.92	140.56	76.41	216.98	4.000	No	No	2.00
4005	40.05	161.13	40.68	2.22	0.31	0.92	140.52	76.45	216.97	4.000	No	No	2.00
4006	40.06	161.68	40.55	2.22	0.31	0.92	141.21	76.50	217.71	4.000	No	No	2.00
4007	40.07	162.61	40.27	2.22	0.31	0.93	142.06	76.45	218.51	4.000	No	No	2.00
4008	40.08	163.65	39.95	2.21	0.30	0.93	143.02	76.39	219.41	4.000	No	No	2.00
4009	40.09	164.76	39.61	2.21	0.30	0.93	144.04	76.31	220.35	4.000	No	No	2.00
4010	40.10	165.88	39.27	2.20	0.30	0.93	145.06	76.23	221.30	4.000	No	No	2.00
4011	40.11	166.95	38.94	2.20	0.30	0.93	146.05	76.15	222.20	4.000	No	No	2.00
4012	40.12	167.91	38.65	2.20	0.30	0.93	146.93	76.07	223.00	4.000	No	No	2.00
4013	40.13	168.71	38.40	2.19	0.30	0.93	147.67	75.98	223.65	4.000	No	No	2.00
4014	40.14	169.40	38.14	2.19	0.30	0.93	148.20	75.85	224.04	4.000	No	No	2.00
4015	40.15	170.08	37.85	2.19	0.30	0.93	148.78	75.68	224.46	4.000	No	No	2.00
4016	40.16	170.84	37.51	2.18	0.30	0.93	149.47	75.48	224.95	4.000	No	No	2.00
4017	40.17	171.68	37.13	2.18	0.30	0.93	150.23	75.24	225.47	4.000	No	No	2.00
4018	40.18	172.56	36.73	2.17	0.30	0.93	151.03	74.98	226.01	4.000	No	No	2.00
4019	40.19	173.43	36.33	2.17	0.30	0.93	151.82	74.71	226.53	4.000	No	No	2.00
4020	40.20	174.25	35.95	2.16	0.30	0.93	152.55	74.44	227.00	4.000	No	No	2.00
4021	40.21	174.97	35.62	2.16	0.29	0.93	153.20	74.20	227.40	4.000	No	No	2.00
4022	40.22	175.43	35.39	2.15	0.29	0.93	153.73	74.04	227.77	4.000	No	No	2.00
4023	40.23	175.65	35.25	2.15	0.29	0.93	153.77	73.88	227.64	4.000	No	No	2.00
4024	40.24	175.67	35.17	2.15	0.29	0.93	153.75	73.78	227.53	4.000	No	No	2.00
4025	40.25	175.67	35.09	2.15	0.29	0.93	153.73	73.68	227.42	4.000	No	No	2.00
4026	40.26	175.67	35.01	2.15	0.29	0.93	153.71	73.57	227.29	4.000	No	No	2.00
4027	40.27	175.67	34.92	2.15	0.30	0.93	153.70	73.46	227.16	4.000	No	No	2.00
4028	40.28	175.67	34.84	2.15	0.30	0.93	153.68	73.35	227.03	4.000	No	No	2.00
4029	40.29	175.67	34.76	2.15	0.30	0.93	153.66	73.25	226.91	4.000	No	No	2.00
4030	40.30	175.66	34.69	2.15	0.30	0.93	153.64	73.16	226.81	4.000	No	No	2.00
4031	40.31	175.62	34.64	2.15	0.30	0.93	153.61	73.09	226.70	4.000	No	No	2.00
4032	40.32	175.53	34.59	2.14	0.30	0.93	153.49	73.00	226.49	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4033	40.33	175.40	34.54	2.14	0.30	0.93	153.35	72.90	226.25	4.000	No	No	2.00
4034	40.34	175.25	34.47	2.14	0.30	0.93	153.19	72.78	225.97	4.000	No	No	2.00
4035	40.35	175.09	34.41	2.14	0.30	0.93	153.02	72.66	225.68	4.000	No	No	2.00
4036	40.36	174.93	34.34	2.14	0.30	0.92	152.86	72.54	225.39	4.000	No	No	2.00
4037	40.37	174.78	34.27	2.14	0.30	0.92	152.70	72.42	225.11	4.000	No	No	2.00
4038	40.38	174.64	34.21	2.14	0.30	0.92	152.55	72.31	224.86	4.000	No	No	2.00
4039	40.39	174.50	34.17	2.14	0.30	0.92	152.42	72.22	224.65	4.000	No	No	2.00
4040	40.40	174.34	34.13	2.14	0.30	0.92	152.27	72.14	224.41	4.000	No	No	2.00
4041	40.41	174.11	34.09	2.14	0.30	0.92	152.03	72.04	224.07	4.000	No	No	2.00
4042	40.42	173.83	34.05	2.14	0.30	0.92	151.75	71.92	223.68	4.000	No	No	2.00
4043	40.43	173.53	34.01	2.14	0.30	0.92	151.45	71.80	223.25	4.000	No	No	2.00
4044	40.44	173.21	33.96	2.14	0.30	0.92	151.13	71.66	222.80	4.000	No	No	2.00
4045	40.45	172.89	33.91	2.14	0.30	0.92	150.82	71.53	222.35	4.000	No	No	2.00
4046	40.46	172.59	33.87	2.14	0.30	0.92	150.52	71.41	221.93	4.000	No	No	2.00
4047	40.47	172.33	33.83	2.14	0.30	0.92	150.26	71.30	221.56	4.000	No	No	2.00
4048	40.48	172.09	33.81	2.14	0.30	0.92	150.05	71.23	221.28	4.000	No	No	2.00
4049	40.49	171.83	33.81	2.14	0.30	0.92	149.81	71.18	220.98	4.000	No	No	2.00
4050	40.50	171.52	33.83	2.14	0.30	0.92	149.50	71.14	220.64	4.000	No	No	2.00
4051	40.51	171.15	33.85	2.14	0.30	0.92	149.14	71.09	220.24	4.000	No	No	2.00
4052	40.52	170.76	33.88	2.14	0.30	0.92	148.76	71.04	219.81	4.000	No	No	2.00
4053	40.53	170.36	33.91	2.14	0.30	0.92	148.38	70.99	219.37	4.000	No	No	2.00
4054	40.54	169.97	33.93	2.14	0.31	0.92	148.00	70.94	218.94	4.000	No	No	2.00
4055	40.55	169.61	33.96	2.14	0.31	0.92	147.65	70.90	218.55	4.000	No	No	2.00
4056	40.56	169.29	33.99	2.14	0.31	0.92	147.35	70.87	218.22	4.000	No	No	2.00
4057	40.57	168.90	34.03	2.14	0.31	0.92	147.06	70.86	217.92	4.000	No	No	2.00
4058	40.58	168.39	34.10	2.14	0.31	0.92	146.54	70.83	217.38	4.000	No	No	2.00
4059	40.59	167.73	34.20	2.14	0.31	0.92	145.91	70.82	216.73	4.000	No	No	2.00
4060	40.60	166.98	34.31	2.14	0.31	0.92	145.20	70.80	216.00	4.000	No	No	2.00
4061	40.61	166.18	34.42	2.14	0.31	0.92	144.45	70.78	215.23	4.000	No	No	2.00
4062	40.62	165.39	34.54	2.14	0.31	0.92	143.69	70.75	214.45	4.000	No	No	2.00
4063	40.63	164.62	34.66	2.15	0.31	0.92	142.97	70.73	213.71	4.000	No	No	2.00
4064	40.64	163.94	34.76	2.15	0.31	0.92	142.32	70.71	213.03	4.000	No	No	2.00
4065	40.65	163.33	34.85	2.15	0.31	0.92	141.78	70.70	212.48	4.000	No	No	2.00
4066	40.66	162.68	34.95	2.15	0.31	0.92	141.25	70.70	211.96	3.978	No	No	2.00
4067	40.67	161.93	35.06	2.15	0.31	0.92	140.53	70.67	211.20	3.780	No	No	2.00
4068	40.68	161.02	35.20	2.15	0.32	0.92	139.67	70.64	210.32	3.562	No	No	2.00
4069	40.69	160.02	35.35	2.15	0.32	0.92	138.73	70.61	209.34	3.340	No	No	2.00
4070	40.70	158.98	35.51	2.16	0.32	0.92	137.76	70.57	208.33	3.127	No	No	2.00
4071	40.71	157.95	35.67	2.16	0.32	0.92	136.77	70.53	207.30	2.928	No	No	2.00
4072	40.72	156.99	35.82	2.16	0.32	0.92	135.87	70.49	206.36	2.759	No	No	2.00
4073	40.73	156.15	35.96	2.16	0.32	0.92	135.07	70.46	205.53	2.621	No	No	2.00
4074	40.74	155.38	36.11	2.16	0.32	0.92	134.43	70.48	204.91	2.524	No	No	2.00
4075	40.75	154.58	36.30	2.17	0.32	0.92	133.74	70.54	204.28	2.428	No	No	2.00
4076	40.76	153.64	36.57	2.17	0.33	0.92	132.86	70.62	203.48	2.314	No	No	2.00
4077	40.77	152.55	36.87	2.17	0.33	0.91	131.84	70.71	202.55	2.191	No	No	2.00
4078	40.78	151.37	37.21	2.18	0.33	0.91	130.75	70.80	201.55	2.067	No	No	2.00
4079	40.79	150.17	37.55	2.18	0.33	0.91	129.64	70.89	200.52	1.949	No	No	2.00
4080	40.80	149.00	37.88	2.19	0.33	0.91	128.56	70.96	199.52	1.841	No	No	1.98

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4081	40.81	147.93	38.18	2.19	0.33	0.91	127.56	71.03	198.59	1.749	No	No	1.88
4082	40.82	147.00	38.45	2.19	0.33	0.91	126.71	71.08	197.78	1.673	No	No	1.80
4083	40.83	146.10	38.69	2.20	0.33	0.91	126.00	71.14	197.14	1.616	No	No	1.74
4084	40.84	145.10	38.93	2.20	0.34	0.91	125.09	71.14	196.23	1.540	No	No	1.66
4085	40.85	143.90	39.21	2.20	0.34	0.91	123.97	71.14	195.11	1.451	No	No	1.57
4086	40.86	142.55	39.53	2.21	0.34	0.91	122.72	71.12	193.84	1.360	No	No	1.47
4087	40.87	141.12	39.87	2.21	0.34	0.91	121.39	71.10	192.50	1.271	No	No	1.38
4088	40.88	139.69	40.21	2.22	0.34	0.91	120.07	71.08	191.15	1.189	No	No	1.29
4089	40.89	138.32	40.54	2.22	0.34	0.91	118.80	71.05	189.85	1.118	No	No	1.21
4090	40.90	137.09	40.84	2.22	0.35	0.91	117.66	71.02	188.68	1.058	No	No	1.15
4091	40.91	136.02	41.08	2.23	0.35	0.91	116.72	70.99	187.70	1.011	No	No	1.10
4092	40.92	134.96	41.29	2.23	0.35	0.91	115.87	70.94	186.82	0.971	No	No	1.06
4093	40.93	133.78	41.47	2.23	0.35	0.91	114.78	70.82	185.60	0.920	No	No	1.00
4094	40.94	132.38	41.68	2.23	0.35	0.91	113.48	70.67	184.14	0.863	No	No	0.94
4095	40.95	130.83	41.91	2.24	0.35	0.91	112.05	70.49	182.55	0.807	No	No	0.88
4096	40.96	129.23	42.16	2.24	0.36	0.91	110.58	70.32	180.90	0.754	No	No	0.82
4097	40.97	127.66	42.41	2.24	0.36	0.91	109.12	70.14	179.27	0.706	No	No	0.77
4098	40.98	126.18	42.64	2.25	0.36	0.90	107.76	69.98	177.74	0.665	No	No	0.72
4099	40.99	124.89	42.85	2.25	0.36	0.90	106.57	69.83	176.40	0.632	No	No	0.69
4100	41.00	123.77	43.05	2.25	0.36	0.90	105.61	69.73	175.34	0.608	No	No	0.66
4101	41.01	122.69	43.25	2.25	0.37	0.90	104.73	69.66	174.39	0.587	No	No	0.64
4102	41.02	121.48	43.49	2.26	0.37	0.90	103.63	69.54	173.17	4.000	Yes	No	2.00
4103	41.03	120.10	43.77	2.26	0.37	0.90	102.36	69.42	171.77	4.000	Yes	No	2.00
4104	41.04	118.61	44.07	2.26	0.37	0.90	100.99	69.28	170.27	4.000	Yes	No	2.00
4105	41.05	117.09	44.39	2.27	0.37	0.90	99.60	69.13	168.74	4.000	Yes	No	2.00
4106	41.06	115.61	44.70	2.27	0.38	0.90	98.25	68.99	167.25	4.000	Yes	No	2.00
4107	41.07	114.26	44.99	2.27	0.38	0.90	97.02	68.87	165.88	4.000	Yes	No	2.00
4108	41.08	113.09	45.25	2.28	0.38	0.90	95.96	68.76	164.72	4.000	Yes	No	2.00
4109	41.09	111.98	45.51	2.28	0.38	0.90	95.10	68.70	163.80	4.000	Yes	No	2.00
4110	41.10	110.78	45.81	2.29	0.38	0.90	94.04	68.61	162.65	4.000	Yes	No	2.00
4111	41.11	109.36	46.19	2.29	0.39	0.90	92.74	68.50	161.24	4.000	Yes	No	2.00
4112	41.12	107.76	46.61	2.30	0.39	0.90	91.29	68.37	159.66	4.000	Yes	No	2.00
4113	41.13	106.07	47.07	2.30	0.39	0.90	89.76	68.24	158.00	4.000	Yes	No	2.00
4114	41.14	104.38	47.53	2.31	0.39	0.89	88.23	68.09	156.32	4.000	Yes	No	2.00
4115	41.15	102.77	47.98	2.31	0.40	0.89	86.77	67.96	154.73	4.000	Yes	No	2.00
4116	41.16	101.32	48.39	2.32	0.40	0.89	85.46	67.83	153.29	4.000	Yes	No	2.00
4117	41.17	100.10	48.73	2.32	0.40	0.89	84.38	67.72	152.10	4.000	Yes	No	2.00
4118	41.18	98.96	49.01	2.33	0.40	0.89	83.50	67.63	151.13	4.000	Yes	No	2.00
4119	41.19	97.75	49.27	2.33	0.40	0.89	82.42	67.48	149.90	4.000	Yes	No	2.00
4120	41.20	96.34	49.57	2.33	0.41	0.89	81.15	67.29	148.45	4.000	Yes	No	2.00
4121	41.21	94.80	49.90	2.34	0.41	0.89	79.77	67.08	146.85	4.000	Yes	No	2.00
4122	41.22	93.20	50.25	2.34	0.41	0.89	78.33	66.87	145.20	4.000	Yes	No	2.00
4123	41.23	91.62	50.61	2.35	0.41	0.89	76.91	66.66	143.57	4.000	Yes	No	2.00
4124	41.24	90.15	50.95	2.35	0.42	0.89	75.59	66.46	142.05	4.000	Yes	No	2.00
4125	41.25	88.86	51.26	2.35	0.42	0.89	74.43	66.29	140.72	4.000	Yes	No	2.00
4126	41.26	87.86	51.54	2.36	0.42	0.89	73.51	66.17	139.67	4.000	Yes	No	2.00
4127	41.27	87.06	51.82	2.36	0.42	0.89	72.96	66.14	139.10	4.000	Yes	No	2.00
4128	41.28	86.30	52.14	2.36	0.42	0.89	72.29	66.10	138.39	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4129	41.29	85.45	52.51	2.37	0.42	0.89	71.52	66.05	137.57	4.000	Yes	No	2.00
4130	41.30	84.52	52.91	2.37	0.43	0.89	70.70	65.99	136.69	4.000	Yes	No	2.00
4131	41.31	83.58	53.32	2.38	0.43	0.88	69.86	65.93	135.79	4.000	Yes	No	2.00
4132	41.32	82.67	53.73	2.38	0.43	0.88	69.05	65.87	134.92	4.000	Yes	No	2.00
4133	41.33	81.84	54.10	2.39	0.43	0.88	68.30	65.82	134.12	4.000	Yes	No	2.00
4134	41.34	81.13	54.43	2.39	0.43	0.88	67.67	65.77	133.44	4.000	Yes	No	2.00
4135	41.35	80.52	54.76	2.40	0.43	0.88	67.19	65.77	132.95	4.000	Yes	No	2.00
4136	41.36	79.92	55.15	2.40	0.43	0.88	66.70	65.77	132.47	4.000	Yes	No	2.00
4137	41.37	79.25	55.61	2.41	0.43	0.88	66.10	65.78	131.88	4.000	Yes	No	2.00
4138	41.38	78.50	56.14	2.41	0.44	0.88	65.43	65.78	131.21	4.000	Yes	No	2.00
4139	41.39	77.70	56.69	2.42	0.44	0.88	64.72	65.78	130.51	4.000	Yes	No	2.00
4140	41.40	76.91	57.24	2.43	0.44	0.88	64.02	65.78	129.79	4.000	Yes	No	2.00
4141	41.41	76.15	57.77	2.43	0.44	0.88	63.35	65.77	129.11	4.000	Yes	No	2.00
4142	41.42	75.47	58.24	2.44	0.44	0.88	62.75	65.75	128.50	4.000	Yes	No	2.00
4143	41.43	74.90	58.65	2.45	0.44	0.88	62.25	65.75	127.99	4.000	Yes	No	2.00
4144	41.44	74.37	59.04	2.45	0.44	0.88	61.85	65.76	127.60	4.000	Yes	No	2.00
4145	41.45	73.80	59.47	2.46	0.44	0.88	61.36	65.75	127.11	4.000	Yes	No	2.00
4146	41.46	73.15	59.97	2.46	0.44	0.88	60.78	65.75	126.52	4.000	Yes	No	2.00
4147	41.47	72.44	60.52	2.47	0.45	0.88	60.15	65.73	125.88	4.000	Yes	No	2.00
4148	41.48	71.70	61.09	2.48	0.45	0.88	59.49	65.72	125.21	4.000	Yes	No	2.00
4149	41.49	70.97	61.65	2.48	0.45	0.88	58.85	65.69	124.55	4.000	Yes	No	2.00
4150	41.50	70.29	62.17	2.49	0.45	0.88	58.25	65.67	123.92	4.000	Yes	No	2.00
4151	41.51	69.70	62.63	2.50	0.45	0.88	57.73	65.65	123.38	4.000	Yes	No	2.00
4152	41.52	69.17	63.08	2.50	0.45	0.88	57.31	65.65	122.96	4.000	Yes	No	2.00
4153	41.53	68.64	63.60	2.51	0.45	0.88	56.88	65.67	122.55	4.000	Yes	No	2.00
4154	41.54	68.04	64.23	2.52	0.45	0.88	56.35	65.68	122.03	4.000	Yes	No	2.00
4155	41.55	67.34	64.96	2.52	0.45	0.88	55.74	65.69	121.43	4.000	Yes	No	2.00
4156	41.56	66.60	65.74	2.53	0.46	0.88	55.08	65.70	120.78	4.000	Yes	No	2.00
4157	41.57	65.84	66.53	2.54	0.46	0.88	54.42	65.69	120.11	4.000	Yes	No	2.00
4158	41.58	65.10	67.29	2.55	0.46	0.87	53.77	65.68	119.46	4.000	Yes	No	2.00
4159	41.59	64.43	67.98	2.56	0.46	0.87	53.18	65.67	118.85	4.000	Yes	No	2.00
4160	41.60	63.85	68.57	2.57	0.46	0.87	52.68	65.66	118.34	4.000	Yes	No	2.00
4161	41.61	63.29	69.11	2.58	0.46	0.87	52.27	65.65	117.92	4.000	Yes	No	2.00
4162	41.62	62.68	69.69	2.58	0.46	0.87	51.74	65.62	117.37	4.000	Yes	No	2.00
4163	41.63	61.96	70.36	2.59	0.46	0.87	51.11	65.58	116.69	4.000	Yes	No	2.00
4164	41.64	61.15	71.11	2.60	0.46	0.87	50.40	0.00	50.40	4.000	Yes	Yes	2.00
4165	41.65	60.29	71.89	2.61	0.47	0.87	49.65	0.00	49.65	4.000	Yes	Yes	2.00
4166	41.66	59.44	72.68	2.62	0.47	0.87	48.91	0.00	48.91	4.000	Yes	Yes	2.00
4167	41.67	58.62	73.44	2.63	0.47	0.87	48.20	0.00	48.20	4.000	Yes	Yes	2.00
4168	41.68	57.90	74.11	2.64	0.47	0.87	47.57	0.00	47.57	4.000	Yes	Yes	2.00
4169	41.69	57.29	74.68	2.65	0.47	0.87	47.04	0.00	47.04	4.000	Yes	Yes	2.00
4170	41.70	56.73	75.23	2.65	0.47	0.87	46.63	0.00	46.63	4.000	Yes	Yes	2.00
4171	41.71	56.15	75.81	2.66	0.47	0.87	46.13	0.00	46.13	4.000	Yes	Yes	2.00
4172	41.72	55.48	76.49	2.67	0.48	0.87	45.55	0.00	45.55	4.000	Yes	Yes	2.00
4173	41.73	54.74	77.23	2.68	0.48	0.87	44.91	0.00	44.91	4.000	Yes	Yes	2.00
4174	41.74	53.98	78.00	2.69	0.48	0.87	44.25	0.00	44.25	4.000	Yes	Yes	2.00
4175	41.75	53.24	78.76	2.70	0.48	0.87	43.60	0.00	43.60	4.000	Yes	Yes	2.00
4176	41.76	52.54	79.47	2.71	0.48	0.87	43.00	0.00	43.00	4.000	Yes	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4177	41.77	51.93	80.08	2.71	0.48	0.87	42.47	0.00	42.47	4.000	Yes	Yes	2.00
4178	41.78	51.42	80.63	2.72	0.48	0.87	42.05	0.00	42.05	4.000	Yes	Yes	2.00
4179	41.79	50.95	81.19	2.73	0.48	0.87	41.70	0.00	41.70	4.000	Yes	Yes	2.00
4180	41.80	50.44	81.82	2.74	0.49	0.87	41.25	0.00	41.25	4.000	Yes	Yes	2.00
4181	41.81	49.85	82.54	2.74	0.49	0.87	40.75	0.00	40.75	4.000	Yes	Yes	2.00
4182	41.82	49.22	83.32	2.75	0.49	0.86	40.20	0.00	40.20	4.000	Yes	Yes	2.00
4183	41.83	48.58	84.10	2.76	0.49	0.86	39.65	0.00	39.65	4.000	Yes	Yes	2.00
4184	41.84	47.96	84.86	2.77	0.49	0.86	39.11	0.00	39.11	4.000	Yes	Yes	2.00
4185	41.85	47.40	85.55	2.78	0.49	0.86	38.63	0.00	38.63	4.000	Yes	Yes	2.00
4186	41.86	46.94	86.13	2.79	0.49	0.86	38.21	0.00	38.21	4.000	Yes	Yes	2.00
4187	41.87	46.59	86.62	2.80	0.49	0.86	37.94	0.00	37.94	4.000	Yes	Yes	2.00
4188	41.88	46.32	87.07	2.80	0.49	0.86	37.75	0.00	37.75	4.000	Yes	Yes	2.00
4189	41.89	46.05	87.56	2.81	0.49	0.86	37.51	0.00	37.51	4.000	Yes	Yes	2.00
4190	41.90	45.74	88.10	2.81	0.50	0.86	37.25	0.00	37.25	4.000	Yes	Yes	2.00
4191	41.91	45.42	88.67	2.82	0.50	0.86	36.97	0.00	36.97	4.000	Yes	Yes	2.00
4192	41.92	45.11	89.24	2.83	0.50	0.86	36.70	0.00	36.70	4.000	Yes	Yes	2.00
4193	41.93	44.81	89.77	2.83	0.50	0.86	36.44	0.00	36.44	4.000	Yes	Yes	2.00
4194	41.94	44.54	90.24	2.84	0.50	0.86	36.21	0.00	36.21	4.000	Yes	Yes	2.00
4195	41.95	44.36	90.56	2.84	0.50	0.86	36.01	0.00	36.01	4.000	Yes	Yes	2.00
4196	41.96	44.30	90.73	2.85	0.50	0.86	35.99	0.00	35.99	4.000	No	Yes	2.00
4197	41.97	44.34	90.78	2.85	0.50	0.86	36.04	0.00	36.04	4.000	No	Yes	2.00
4198	41.98	44.41	90.80	2.85	0.50	0.86	36.09	0.00	36.09	4.000	No	Yes	2.00
4199	41.99	44.48	90.82	2.85	0.50	0.86	36.15	0.00	36.15	4.000	No	Yes	2.00
4200	42.00	44.56	90.84	2.85	0.50	0.86	36.22	0.00	36.22	4.000	No	Yes	2.00
4201	42.01	44.64	90.87	2.85	0.50	0.86	36.28	0.00	36.28	4.000	No	Yes	2.00
4202	42.02	44.72	90.88	2.85	0.50	0.86	36.34	0.00	36.34	4.000	No	Yes	2.00
4203	42.03	44.78	90.90	2.85	0.50	0.86	36.39	0.00	36.39	4.000	No	Yes	2.00
4204	42.04	44.98	90.74	2.85	0.50	0.86	36.44	0.00	36.44	4.000	No	Yes	2.00
4205	42.05	45.36	90.36	2.84	0.50	0.86	36.83	0.00	36.83	4.000	No	Yes	2.00
4206	42.06	45.93	89.72	2.83	0.49	0.86	37.32	0.00	37.32	4.000	No	Yes	2.00
4207	42.07	46.60	88.99	2.82	0.49	0.86	37.87	0.00	37.87	4.000	No	Yes	2.00
4208	42.08	47.30	88.20	2.82	0.49	0.86	38.47	0.00	38.47	4.000	No	Yes	2.00
4209	42.09	48.02	87.41	2.81	0.49	0.86	39.08	0.00	39.08	4.000	No	Yes	2.00
4210	42.10	48.72	86.64	2.80	0.49	0.86	39.68	0.00	39.68	4.000	No	Yes	2.00
4211	42.11	49.35	85.95	2.79	0.49	0.86	40.21	0.00	40.21	4.000	No	Yes	2.00
4212	42.12	49.92	85.32	2.78	0.49	0.86	40.67	0.00	40.67	4.000	No	Yes	2.00
4213	42.13	50.55	84.62	2.77	0.48	0.86	41.10	0.00	41.10	4.000	No	Yes	2.00
4214	42.14	51.31	83.75	2.76	0.48	0.86	41.77	0.00	41.77	4.000	No	Yes	2.00
4215	42.15	52.26	82.66	2.75	0.48	0.86	42.58	0.00	42.58	4.000	No	Yes	2.00
4216	42.16	53.32	81.44	2.73	0.48	0.86	43.48	0.00	43.48	4.000	No	Yes	2.00
4217	42.17	54.43	80.15	2.71	0.48	0.86	44.43	0.00	44.43	4.000	No	Yes	2.00
4218	42.18	55.55	78.85	2.70	0.48	0.86	45.38	0.00	45.38	4.000	No	Yes	2.00
4219	42.19	56.60	77.62	2.68	0.47	0.87	46.28	0.00	46.28	4.000	No	Yes	2.00
4220	42.20	57.54	76.51	2.67	0.47	0.87	47.09	0.00	47.09	4.000	No	Yes	2.00
4221	42.21	58.32	75.59	2.66	0.47	0.87	47.74	0.00	47.74	4.000	No	Yes	2.00
4222	42.22	59.04	74.74	2.65	0.47	0.87	48.25	0.00	48.25	4.000	No	Yes	2.00
4223	42.23	59.77	73.87	2.64	0.47	0.87	48.87	0.00	48.87	4.000	No	Yes	2.00
4224	42.24	60.63	72.86	2.62	0.47	0.87	49.60	0.00	49.60	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4225	42.25	61.56	71.74	2.61	0.46	0.87	50.40	0.00	50.40	4.000	No	Yes	2.00
4226	42.26	62.52	70.57	2.59	0.46	0.87	51.22	65.66	116.87	0.165	No	No	0.18
4227	42.27	63.46	69.41	2.58	0.46	0.87	52.02	65.65	117.67	0.166	No	No	0.18
4228	42.28	64.33	68.32	2.57	0.46	0.87	52.77	65.63	118.40	0.168	No	No	0.18
4229	42.29	65.09	67.37	2.55	0.46	0.87	53.42	65.60	119.03	0.169	No	No	0.18
4230	42.30	65.65	66.67	2.55	0.46	0.87	53.93	65.58	119.51	0.170	No	No	0.18
4231	42.31	66.09	66.15	2.54	0.46	0.87	54.19	65.54	119.72	0.171	No	No	0.18
4232	42.32	66.47	65.71	2.53	0.46	0.87	54.51	65.52	120.04	0.172	No	No	0.18
4233	42.33	66.92	65.20	2.53	0.46	0.87	54.89	65.51	120.40	0.172	No	No	0.18
4234	42.34	67.39	64.65	2.52	0.46	0.87	55.29	65.48	120.78	0.173	No	No	0.19
4235	42.35	67.87	64.09	2.51	0.45	0.87	55.70	65.46	121.16	0.174	No	No	0.19
4236	42.36	68.33	63.54	2.51	0.45	0.87	56.09	65.43	121.52	0.175	No	No	0.19
4237	42.37	68.75	63.05	2.50	0.45	0.87	56.45	65.40	121.85	0.176	No	No	0.19
4238	42.38	69.04	62.69	2.50	0.45	0.87	56.75	65.39	122.14	0.176	No	No	0.19
4239	42.39	69.05	62.57	2.49	0.45	0.87	56.80	65.37	122.17	0.176	No	No	0.19
4240	42.40	68.80	62.69	2.50	0.45	0.87	56.47	65.31	121.78	0.175	No	No	0.19
4241	42.41	68.36	62.95	2.50	0.45	0.87	56.09	65.27	121.35	0.174	No	No	0.19
4242	42.42	67.87	63.24	2.50	0.46	0.87	55.66	65.22	120.88	0.173	No	No	0.19
4243	42.43	67.36	63.54	2.51	0.46	0.87	55.21	65.18	120.38	0.172	No	No	0.18
4244	42.44	66.85	63.85	2.51	0.46	0.87	54.76	65.13	119.89	0.171	No	No	0.18
4245	42.45	66.36	64.14	2.51	0.46	0.87	54.33	65.08	119.41	0.170	No	No	0.18
4246	42.46	65.93	64.41	2.52	0.46	0.87	53.95	65.04	118.99	0.169	No	No	0.18
4247	42.47	65.49	64.73	2.52	0.46	0.87	53.64	65.03	118.67	0.169	No	No	0.18
4248	42.48	64.95	65.20	2.53	0.46	0.87	53.20	65.02	118.22	0.168	No	No	0.18
4249	42.49	64.24	65.88	2.54	0.46	0.87	52.56	65.01	117.57	0.166	No	No	0.18
4250	42.50	63.39	66.71	2.55	0.46	0.87	51.82	64.99	116.81	0.165	No	No	0.18
4251	42.51	62.46	67.61	2.56	0.46	0.86	51.02	64.96	115.98	0.163	No	No	0.17
4252	42.52	61.49	68.54	2.57	0.47	0.86	50.18	64.92	115.11	0.161	No	No	0.17
4253	42.53	60.55	69.44	2.58	0.47	0.86	49.37	64.88	114.25	0.160	No	No	0.17
4254	42.54	59.68	70.28	2.59	0.47	0.86	48.62	64.84	113.45	0.158	No	No	0.17
4255	42.55	58.92	71.01	2.60	0.47	0.86	47.96	0.00	47.96	4.000	No	Yes	2.00
4256	42.56	58.24	71.68	2.61	0.47	0.86	47.44	0.00	47.44	4.000	No	Yes	2.00
4257	42.57	57.54	72.36	2.62	0.47	0.86	46.88	0.00	46.88	4.000	No	Yes	2.00
4258	42.58	56.73	73.16	2.63	0.48	0.86	46.17	0.00	46.17	4.000	No	Yes	2.00
4259	42.59	55.80	74.07	2.64	0.48	0.86	45.37	0.00	45.37	4.000	No	Yes	2.00
4260	42.60	54.81	75.04	2.65	0.48	0.86	44.52	0.00	44.52	4.000	No	Yes	2.00
4261	42.61	53.80	76.03	2.66	0.48	0.86	43.66	0.00	43.66	4.000	No	Yes	2.00
4262	42.62	52.84	76.99	2.67	0.48	0.86	42.83	0.00	42.83	4.000	No	Yes	2.00
4263	42.63	51.96	77.86	2.69	0.48	0.86	42.08	0.00	42.08	4.000	No	Yes	2.00
4264	42.64	51.22	78.57	2.69	0.49	0.86	41.44	0.00	41.44	4.000	No	Yes	2.00
4265	42.65	50.56	79.14	2.70	0.49	0.86	40.96	0.00	40.96	4.000	No	Yes	2.00
4266	42.66	49.90	79.64	2.71	0.49	0.86	40.42	0.00	40.42	4.000	No	Yes	2.00
4267	42.67	49.15	80.18	2.71	0.49	0.86	39.77	0.00	39.77	4.000	No	Yes	2.00
4268	42.68	48.32	80.78	2.72	0.49	0.86	39.06	0.00	39.06	4.000	No	Yes	2.00
4269	42.69	47.44	81.43	2.73	0.49	0.86	38.31	0.00	38.31	4.000	No	Yes	2.00
4270	42.70	46.56	82.08	2.74	0.50	0.85	37.57	0.00	37.57	4.000	No	Yes	2.00
4271	42.71	45.74	82.70	2.75	0.50	0.85	36.86	0.00	36.86	4.000	No	Yes	2.00
4272	42.72	45.01	83.27	2.75	0.50	0.85	36.24	0.00	36.24	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4273	42.73	44.50	83.62	2.76	0.50	0.85	35.73	0.00	35.73	4.000	No	Yes	2.00
4274	42.74	44.22	83.72	2.76	0.50	0.85	35.59	0.00	35.59	4.000	No	Yes	2.00
4275	42.75	44.12	83.58	2.76	0.50	0.85	35.53	0.00	35.53	4.000	No	Yes	2.00
4276	42.76	44.05	83.37	2.75	0.50	0.85	35.47	0.00	35.47	4.000	No	Yes	2.00
4277	42.77	43.97	83.13	2.75	0.50	0.85	35.40	0.00	35.40	4.000	No	Yes	2.00
4278	42.78	43.89	82.88	2.75	0.50	0.85	35.32	0.00	35.32	4.000	No	Yes	2.00
4279	42.79	43.81	82.64	2.75	0.50	0.85	35.25	0.00	35.25	4.000	No	Yes	2.00
4280	42.80	43.74	82.41	2.74	0.50	0.85	35.19	0.00	35.19	4.000	No	Yes	2.00
4281	42.81	43.70	82.19	2.74	0.50	0.85	35.13	0.00	35.13	4.000	No	Yes	2.00
4282	42.82	43.91	81.80	2.73	0.50	0.85	35.13	0.00	35.13	4.000	No	Yes	2.00
4283	42.83	44.43	81.14	2.73	0.50	0.85	35.70	0.00	35.70	4.000	No	Yes	2.00
4284	42.84	45.28	80.20	2.72	0.50	0.85	36.41	0.00	36.41	4.000	No	Yes	2.00
4285	42.85	46.24	79.14	2.70	0.50	0.85	37.22	0.00	37.22	4.000	No	Yes	2.00
4286	42.86	47.26	78.01	2.69	0.50	0.85	38.08	0.00	38.08	4.000	No	Yes	2.00
4287	42.87	48.30	76.87	2.67	0.49	0.85	38.95	0.00	38.95	4.000	No	Yes	2.00
4288	42.88	49.30	75.78	2.66	0.49	0.85	39.79	0.00	39.79	4.000	No	Yes	2.00
4289	42.89	50.21	74.79	2.65	0.49	0.85	40.56	0.00	40.56	4.000	No	Yes	2.00
4290	42.90	50.99	73.97	2.64	0.49	0.85	41.21	0.00	41.21	4.000	No	Yes	2.00
4291	42.91	51.74	73.25	2.63	0.49	0.85	41.74	0.00	41.74	4.000	No	Yes	2.00
4292	42.92	52.55	72.55	2.62	0.49	0.86	42.41	0.00	42.41	4.000	No	Yes	2.00
4293	42.93	53.51	71.76	2.61	0.48	0.86	43.23	0.00	43.23	4.000	No	Yes	2.00
4294	42.94	54.58	70.89	2.60	0.48	0.86	44.13	63.65	107.78	0.149	No	No	0.16
4295	42.95	55.69	69.98	2.59	0.48	0.86	45.08	63.74	108.82	0.150	No	No	0.16
4296	42.96	56.80	69.09	2.58	0.48	0.86	46.02	63.83	109.85	0.152	No	No	0.16
4297	42.97	57.85	68.26	2.57	0.48	0.86	46.91	63.92	110.82	0.154	No	No	0.16
4298	42.98	58.78	67.53	2.56	0.47	0.86	47.70	63.98	111.68	0.155	No	No	0.17
4299	42.99	59.45	67.04	2.55	0.47	0.86	48.34	64.06	112.40	0.156	No	No	0.17
4300	43.00	59.89	66.78	2.55	0.47	0.86	48.59	64.07	112.66	0.157	No	No	0.17
4301	43.01	60.17	66.71	2.55	0.47	0.86	48.79	64.11	112.91	0.157	No	No	0.17
4302	43.02	60.46	66.66	2.55	0.47	0.86	49.04	64.17	113.21	0.158	No	No	0.17
4303	43.03	60.77	66.61	2.55	0.47	0.86	49.30	64.24	113.54	0.158	No	No	0.17
4304	43.04	61.09	66.56	2.54	0.47	0.86	49.57	64.30	113.87	0.159	No	No	0.17
4305	43.05	61.41	66.51	2.54	0.47	0.86	49.83	64.37	114.20	0.160	No	No	0.17
4306	43.06	61.70	66.47	2.54	0.47	0.86	50.08	64.43	114.51	0.160	No	No	0.17
4307	43.07	61.94	66.45	2.54	0.47	0.86	50.29	64.48	114.77	0.161	No	No	0.17
4308	43.08	62.06	66.54	2.54	0.47	0.86	50.43	64.55	114.98	0.161	No	No	0.17
4309	43.09	62.08	66.78	2.55	0.47	0.86	50.38	64.59	114.97	0.161	No	No	0.17
4310	43.10	62.02	67.16	2.55	0.47	0.86	50.32	64.66	114.98	0.161	No	No	0.17
4311	43.11	61.94	67.59	2.56	0.47	0.86	50.26	64.74	114.99	0.161	No	No	0.17
4312	43.12	61.87	68.03	2.56	0.47	0.86	50.19	64.82	115.00	0.161	No	No	0.17
4313	43.13	61.79	68.48	2.57	0.47	0.86	50.12	64.89	115.01	0.161	No	No	0.17
4314	43.14	61.71	68.91	2.57	0.47	0.86	50.05	64.97	115.01	0.161	No	No	0.17
4315	43.15	61.64	69.29	2.58	0.47	0.86	49.99	65.03	115.01	0.161	No	No	0.17
4316	43.16	61.58	69.61	2.58	0.47	0.86	49.93	65.08	115.01	0.161	No	No	0.17
4317	43.17	61.53	69.92	2.59	0.47	0.86	49.89	65.13	115.02	0.161	No	No	0.17
4318	43.18	61.47	70.24	2.59	0.47	0.86	49.84	65.18	115.02	0.161	No	No	0.17
4319	43.19	61.40	70.62	2.60	0.47	0.86	49.77	65.24	115.02	0.161	No	No	0.17
4320	43.20	61.32	71.03	2.60	0.47	0.86	49.71	0.00	49.71	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4321	43.21	61.24	71.46	2.61	0.47	0.86	49.63	0.00	49.63	4.000	No	Yes	2.00
4322	43.22	61.17	71.88	2.61	0.47	0.86	49.56	0.00	49.56	4.000	No	Yes	2.00
4323	43.23	61.09	72.27	2.62	0.47	0.86	49.50	0.00	49.50	4.000	No	Yes	2.00
4324	43.24	61.03	72.61	2.62	0.47	0.86	49.44	0.00	49.44	4.000	No	Yes	2.00
4325	43.25	60.99	72.84	2.62	0.47	0.86	49.39	0.00	49.39	4.000	No	Yes	2.00
4326	43.26	60.99	72.96	2.62	0.47	0.86	49.40	0.00	49.40	4.000	No	Yes	2.00
4327	43.27	61.03	73.00	2.62	0.47	0.86	49.43	0.00	49.43	4.000	No	Yes	2.00
4328	43.28	61.08	73.01	2.63	0.47	0.86	49.46	0.00	49.46	4.000	No	Yes	2.00
4329	43.29	61.13	73.03	2.63	0.47	0.86	49.50	0.00	49.50	4.000	No	Yes	2.00
4330	43.30	61.18	73.05	2.63	0.47	0.86	49.54	0.00	49.54	4.000	No	Yes	2.00
4331	43.31	61.23	73.07	2.63	0.47	0.86	49.58	0.00	49.58	4.000	No	Yes	2.00
4332	43.32	61.28	73.09	2.63	0.47	0.86	49.62	0.00	49.62	4.000	No	Yes	2.00
4333	43.33	61.33	73.10	2.63	0.47	0.86	49.65	0.00	49.65	4.000	No	Yes	2.00
4334	43.34	61.46	72.98	2.62	0.47	0.86	49.70	0.00	49.70	4.000	Yes	Yes	2.00
4335	43.35	61.70	72.71	2.62	0.47	0.86	49.93	0.00	49.93	4.000	Yes	Yes	2.00
4336	43.36	62.04	72.29	2.62	0.46	0.86	50.22	0.00	50.22	4.000	Yes	Yes	2.00
4337	43.37	62.44	71.81	2.61	0.46	0.86	50.55	0.00	50.55	4.000	Yes	Yes	2.00
4338	43.38	62.85	71.29	2.60	0.46	0.86	50.90	0.00	50.90	4.000	Yes	Yes	2.00
4339	43.39	63.28	70.77	2.60	0.46	0.86	51.26	65.71	116.97	4.000	Yes	No	2.00
4340	43.40	63.68	70.26	2.59	0.46	0.86	51.60	65.70	117.30	4.000	Yes	No	2.00
4341	43.41	64.05	69.80	2.59	0.46	0.86	51.91	65.70	117.60	4.000	Yes	No	2.00
4342	43.42	64.40	69.38	2.58	0.46	0.86	52.16	65.68	117.84	4.000	Yes	No	2.00
4343	43.43	64.86	68.91	2.57	0.46	0.86	52.48	65.67	118.15	4.000	Yes	No	2.00
4344	43.44	65.46	68.32	2.57	0.46	0.86	53.02	65.70	118.72	4.000	Yes	No	2.00
4345	43.45	66.23	67.59	2.56	0.46	0.86	53.67	65.73	119.40	4.000	Yes	No	2.00
4346	43.46	67.07	66.79	2.55	0.46	0.86	54.39	65.75	120.14	4.000	Yes	No	2.00
4347	43.47	67.96	65.94	2.54	0.46	0.86	55.15	65.76	120.91	4.000	Yes	No	2.00
4348	43.48	68.83	65.09	2.53	0.45	0.86	55.89	65.77	121.66	4.000	Yes	No	2.00
4349	43.49	69.66	64.29	2.52	0.45	0.86	56.60	65.77	122.36	4.000	Yes	No	2.00
4350	43.50	70.39	63.58	2.51	0.45	0.86	57.22	65.76	122.98	4.000	Yes	No	2.00
4351	43.51	70.99	63.00	2.50	0.45	0.86	57.72	65.75	123.47	4.000	Yes	No	2.00
4352	43.52	71.52	62.49	2.49	0.45	0.86	58.09	65.71	123.80	4.000	Yes	No	2.00
4353	43.53	72.06	61.97	2.49	0.45	0.86	58.54	65.70	124.23	4.000	Yes	No	2.00
4354	43.54	72.67	61.37	2.48	0.45	0.86	59.06	65.67	124.74	4.000	Yes	No	2.00
4355	43.55	73.34	60.71	2.47	0.45	0.86	59.63	65.64	125.28	4.000	Yes	No	2.00
4356	43.56	74.03	60.04	2.46	0.45	0.86	60.21	65.61	125.82	4.000	Yes	No	2.00
4357	43.57	74.70	59.38	2.45	0.44	0.86	60.78	65.57	126.35	4.000	Yes	No	2.00
4358	43.58	75.31	58.76	2.45	0.44	0.86	61.31	65.52	126.83	4.000	Yes	No	2.00
4359	43.59	75.83	58.25	2.44	0.44	0.86	61.76	65.48	127.24	4.000	Yes	No	2.00
4360	43.60	76.13	57.93	2.44	0.44	0.86	62.06	65.46	127.52	4.000	Yes	No	2.00
4361	43.61	76.25	57.78	2.43	0.44	0.86	62.05	65.41	127.46	0.190	No	No	0.20
4362	43.62	76.24	57.74	2.43	0.44	0.86	62.04	65.40	127.44	0.190	No	No	0.20
4363	43.63	76.24	57.69	2.43	0.44	0.86	62.03	65.38	127.41	0.190	No	No	0.20
4364	43.64	76.24	57.64	2.43	0.44	0.86	62.02	65.36	127.38	0.190	No	No	0.20
4365	43.65	76.24	57.59	2.43	0.44	0.86	62.01	65.34	127.35	0.190	No	No	0.20
4366	43.66	76.24	57.53	2.43	0.44	0.86	62.01	65.32	127.32	0.190	No	No	0.20
4367	43.67	76.24	57.49	2.43	0.44	0.86	62.00	65.30	127.30	0.190	No	No	0.20
4368	43.68	76.16	57.53	2.43	0.44	0.86	61.99	65.31	127.30	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4369	43.69	75.90	57.79	2.43	0.44	0.86	61.79	65.34	127.14	4.000	Yes	No	2.00
4370	43.70	75.41	58.29	2.44	0.44	0.86	61.32	65.37	126.69	4.000	Yes	No	2.00
4371	43.71	74.76	58.96	2.45	0.45	0.86	60.75	65.43	126.18	4.000	Yes	No	2.00
4372	43.72	74.04	59.71	2.46	0.45	0.86	60.13	65.48	125.62	4.000	Yes	No	2.00
4373	43.73	73.29	60.47	2.47	0.45	0.86	59.48	65.53	125.01	4.000	Yes	No	2.00
4374	43.74	72.55	61.23	2.48	0.45	0.86	58.84	65.57	124.41	4.000	Yes	No	2.00
4375	43.75	71.85	61.94	2.49	0.45	0.86	58.23	65.60	123.83	4.000	Yes	No	2.00
4376	43.76	71.23	62.56	2.49	0.45	0.86	57.70	65.62	123.32	4.000	Yes	No	2.00
4377	43.77	70.59	63.21	2.50	0.45	0.86	57.27	65.67	122.94	4.000	Yes	No	2.00
4378	43.78	69.81	64.02	2.51	0.45	0.86	56.60	65.70	122.30	4.000	Yes	No	2.00
4379	43.79	68.79	65.08	2.53	0.45	0.86	55.71	65.71	121.42	4.000	Yes	No	2.00
4380	43.80	67.58	66.33	2.54	0.46	0.86	54.67	65.72	120.38	4.000	Yes	No	2.00
4381	43.81	66.27	67.66	2.56	0.46	0.86	53.55	65.70	119.25	4.000	Yes	No	2.00
4382	43.82	64.93	69.01	2.58	0.46	0.85	52.40	65.67	118.07	4.000	Yes	No	2.00
4383	43.83	63.63	70.33	2.59	0.46	0.85	51.28	65.62	116.91	4.000	Yes	No	2.00
4384	43.84	62.43	71.53	2.61	0.47	0.85	50.25	0.00	50.25	4.000	Yes	Yes	2.00
4385	43.85	61.40	72.56	2.62	0.47	0.85	49.37	0.00	49.37	4.000	Yes	Yes	2.00
4386	43.86	60.52	73.48	2.63	0.47	0.85	48.69	0.00	48.69	4.000	Yes	Yes	2.00
4387	43.87	59.66	74.41	2.64	0.47	0.85	48.02	0.00	48.02	4.000	Yes	Yes	2.00
4388	43.88	58.71	75.47	2.66	0.47	0.85	47.21	0.00	47.21	4.000	Yes	Yes	2.00
4389	43.89	57.63	76.66	2.67	0.47	0.85	46.29	0.00	46.29	4.000	Yes	Yes	2.00
4390	43.90	56.48	77.92	2.69	0.48	0.85	45.31	0.00	45.31	4.000	Yes	Yes	2.00
4391	43.91	55.33	79.19	2.70	0.48	0.85	44.33	0.00	44.33	4.000	Yes	Yes	2.00
4392	43.92	54.22	80.40	2.72	0.48	0.85	43.40	0.00	43.40	4.000	Yes	Yes	2.00
4393	43.93	53.23	81.49	2.73	0.48	0.85	42.55	0.00	42.55	4.000	Yes	Yes	2.00
4394	43.94	52.45	82.37	2.74	0.48	0.85	41.84	0.00	41.84	4.000	Yes	Yes	2.00
4395	43.95	51.89	83.08	2.75	0.48	0.85	41.44	0.00	41.44	4.000	Yes	Yes	2.00
4396	43.96	51.47	83.71	2.76	0.49	0.85	41.14	0.00	41.14	4.000	Yes	Yes	2.00
4397	43.97	51.05	84.40	2.77	0.49	0.85	40.79	0.00	40.79	4.000	Yes	Yes	2.00
4398	43.98	50.59	85.14	2.78	0.49	0.85	40.40	0.00	40.40	4.000	Yes	Yes	2.00
4399	43.99	50.11	85.92	2.79	0.49	0.85	39.99	0.00	39.99	4.000	Yes	Yes	2.00
4400	44.00	49.64	86.67	2.80	0.49	0.84	39.59	0.00	39.59	4.000	Yes	Yes	2.00
4401	44.01	49.19	87.38	2.80	0.49	0.84	39.21	0.00	39.21	4.000	Yes	Yes	2.00
4402	44.02	48.80	88.00	2.81	0.49	0.84	38.87	0.00	38.87	4.000	Yes	Yes	2.00
4403	44.03	48.58	88.44	2.82	0.49	0.84	38.60	0.00	38.60	4.000	Yes	Yes	2.00
4404	44.04	48.53	88.70	2.82	0.49	0.84	38.64	0.00	38.64	4.000	Yes	Yes	2.00
4405	44.05	48.64	88.86	2.82	0.49	0.84	38.75	0.00	38.75	4.000	No	Yes	2.00
4406	44.06	48.79	89.01	2.83	0.49	0.84	38.86	0.00	38.86	4.000	No	Yes	2.00
4407	44.07	48.94	89.18	2.83	0.49	0.84	38.99	0.00	38.99	4.000	No	Yes	2.00
4408	44.08	49.11	89.35	2.83	0.49	0.84	39.13	0.00	39.13	4.000	No	Yes	2.00
4409	44.09	49.26	89.52	2.83	0.49	0.84	39.26	0.00	39.26	4.000	No	Yes	2.00
4410	44.10	49.41	89.66	2.83	0.49	0.84	39.37	0.00	39.37	4.000	No	Yes	2.00
4411	44.11	49.55	89.76	2.83	0.49	0.84	39.47	0.00	39.47	4.000	No	Yes	2.00
4412	44.12	49.79	89.72	2.83	0.49	0.84	39.60	0.00	39.60	4.000	No	Yes	2.00
4413	44.13	50.17	89.51	2.83	0.49	0.84	39.96	0.00	39.96	4.000	Yes	Yes	2.00
4414	44.14	50.70	89.16	2.83	0.49	0.84	40.40	0.00	40.40	4.000	Yes	Yes	2.00
4415	44.15	51.30	88.76	2.82	0.48	0.84	40.90	0.00	40.90	4.000	Yes	Yes	2.00
4416	44.16	51.93	88.35	2.82	0.48	0.84	41.43	0.00	41.43	4.000	Yes	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4417	44.17	52.57	87.93	2.81	0.48	0.85	41.96	0.00	41.96	4.000	Yes	Yes	2.00
4418	44.18	53.18	87.54	2.81	0.48	0.85	42.47	0.00	42.47	4.000	Yes	Yes	2.00
4419	44.19	53.73	87.19	2.80	0.48	0.85	42.93	0.00	42.93	4.000	Yes	Yes	2.00
4420	44.20	54.29	86.80	2.80	0.48	0.85	43.32	0.00	43.32	4.000	Yes	Yes	2.00
4421	44.21	55.04	86.25	2.79	0.48	0.85	43.86	0.00	43.86	4.000	Yes	Yes	2.00
4422	44.22	56.06	85.45	2.78	0.47	0.85	44.78	0.00	44.78	4.000	Yes	Yes	2.00
4423	44.23	57.35	84.45	2.77	0.47	0.85	45.86	0.00	45.86	4.000	Yes	Yes	2.00
4424	44.24	58.77	83.35	2.75	0.47	0.85	47.06	0.00	47.06	4.000	Yes	Yes	2.00
4425	44.25	60.24	82.23	2.74	0.47	0.85	48.31	0.00	48.31	4.000	Yes	Yes	2.00
4426	44.26	61.70	81.12	2.73	0.46	0.85	49.54	0.00	49.54	4.000	Yes	Yes	2.00
4427	44.27	63.07	80.09	2.71	0.46	0.85	50.70	0.00	50.70	4.000	Yes	Yes	2.00
4428	44.28	64.27	79.20	2.70	0.46	0.85	51.73	0.00	51.73	4.000	Yes	Yes	2.00
4429	44.29	65.42	78.35	2.69	0.46	0.85	52.55	0.00	52.55	4.000	Yes	Yes	2.00
4430	44.30	66.69	77.42	2.68	0.45	0.85	53.57	0.00	53.57	4.000	Yes	Yes	2.00
4431	44.31	68.24	76.28	2.67	0.45	0.85	54.91	0.00	54.91	4.000	Yes	Yes	2.00
4432	44.32	70.05	74.97	2.65	0.45	0.85	56.45	0.00	56.45	4.000	Yes	Yes	2.00
4433	44.33	72.01	73.55	2.63	0.44	0.85	58.12	0.00	58.12	4.000	Yes	Yes	2.00
4434	44.34	74.00	72.11	2.61	0.44	0.86	59.83	0.00	59.83	4.000	Yes	Yes	2.00
4435	44.35	75.94	70.71	2.60	0.44	0.86	61.50	68.69	130.18	4.000	Yes	No	2.00
4436	44.36	77.73	69.42	2.58	0.43	0.86	63.03	68.85	131.88	4.000	Yes	No	2.00
4437	44.37	79.25	68.33	2.57	0.43	0.86	64.35	68.98	133.33	4.000	Yes	No	2.00
4438	44.38	80.58	67.40	2.55	0.43	0.86	65.35	69.05	134.41	4.000	Yes	No	2.00
4439	44.39	81.91	66.50	2.54	0.43	0.86	66.41	69.14	135.54	4.000	Yes	No	2.00
4440	44.40	83.41	65.51	2.53	0.43	0.86	67.70	69.26	136.96	4.000	Yes	No	2.00
4441	44.41	85.09	64.39	2.52	0.42	0.86	69.16	69.38	138.54	4.000	Yes	No	2.00
4442	44.42	86.88	63.20	2.50	0.42	0.86	70.70	69.49	140.20	4.000	Yes	No	2.00
4443	44.43	88.68	62.01	2.49	0.42	0.86	72.26	69.59	141.84	4.000	Yes	No	2.00
4444	44.44	90.39	60.86	2.47	0.41	0.86	73.74	69.66	143.40	4.000	Yes	No	2.00
4445	44.45	91.93	59.82	2.46	0.41	0.86	75.08	69.71	144.79	4.000	Yes	No	2.00
4446	44.46	93.21	58.97	2.45	0.41	0.86	76.19	69.74	145.93	4.000	Yes	No	2.00
4447	44.47	94.32	58.24	2.44	0.41	0.86	77.00	69.71	146.71	4.000	Yes	No	2.00
4448	44.48	95.42	57.52	2.43	0.41	0.86	77.90	69.72	147.62	4.000	Yes	No	2.00
4449	44.49	96.66	56.71	2.42	0.41	0.87	78.98	69.72	148.71	4.000	Yes	No	2.00
4450	44.50	98.03	55.81	2.41	0.40	0.87	80.17	69.72	149.89	4.000	Yes	No	2.00
4451	44.51	99.45	54.87	2.40	0.40	0.87	81.41	69.69	151.10	4.000	Yes	No	2.00
4452	44.52	100.86	53.94	2.39	0.40	0.87	82.63	69.65	152.27	4.000	Yes	No	2.00
4453	44.53	102.17	53.06	2.38	0.40	0.87	83.77	69.59	153.36	4.000	Yes	No	2.00
4454	44.54	103.33	52.29	2.37	0.40	0.87	84.77	69.52	154.29	4.000	Yes	No	2.00
4455	44.55	104.13	51.72	2.36	0.40	0.87	85.58	69.48	155.06	4.000	Yes	No	2.00
4456	44.56	104.65	51.32	2.35	0.40	0.87	85.82	69.36	155.18	4.000	Yes	No	2.00
4457	44.57	104.97	51.02	2.35	0.39	0.87	86.07	69.29	155.36	4.000	Yes	No	2.00
4458	44.58	105.32	50.69	2.35	0.39	0.87	86.37	69.21	155.58	4.000	Yes	No	2.00
4459	44.59	105.69	50.32	2.34	0.39	0.87	86.68	69.12	155.80	4.000	Yes	No	2.00
4460	44.60	106.08	49.94	2.34	0.39	0.87	87.01	69.02	156.03	4.000	Yes	No	2.00
4461	44.61	106.45	49.57	2.33	0.39	0.87	87.32	68.92	156.25	4.000	Yes	No	2.00
4462	44.62	106.79	49.23	2.33	0.39	0.87	87.61	68.83	156.44	4.000	Yes	No	2.00
4463	44.63	107.10	48.94	2.32	0.39	0.87	87.86	68.74	156.60	4.000	Yes	No	2.00
4464	44.64	107.47	48.65	2.32	0.39	0.87	88.09	68.66	156.75	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4465	44.65	107.94	48.35	2.32	0.39	0.87	88.53	68.61	157.14	4.000	Yes	No	2.00
4466	44.66	108.56	47.98	2.31	0.39	0.87	89.06	68.55	157.61	4.000	Yes	No	2.00
4467	44.67	109.26	47.57	2.31	0.39	0.87	89.66	68.49	158.14	4.000	Yes	No	2.00
4468	44.68	109.99	47.13	2.30	0.39	0.87	90.29	68.41	158.70	4.000	Yes	No	2.00
4469	44.69	110.73	46.69	2.30	0.39	0.87	90.93	68.32	159.25	4.000	Yes	No	2.00
4470	44.70	111.43	46.26	2.29	0.39	0.87	91.53	68.23	159.77	4.000	Yes	No	2.00
4471	44.71	112.06	45.89	2.29	0.39	0.87	92.08	68.15	160.23	4.000	Yes	No	2.00
4472	44.72	112.60	45.56	2.28	0.39	0.87	92.53	68.07	160.60	4.000	Yes	No	2.00
4473	44.73	113.11	45.25	2.28	0.39	0.87	92.90	67.98	160.88	4.000	Yes	No	2.00
4474	44.74	113.66	44.91	2.27	0.39	0.87	93.37	67.89	161.26	4.000	Yes	No	2.00
4475	44.75	114.31	44.52	2.27	0.39	0.87	93.92	67.78	161.70	4.000	Yes	No	2.00
4476	44.76	115.02	44.08	2.26	0.38	0.87	94.53	67.66	162.19	4.000	Yes	No	2.00
4477	44.77	115.75	43.63	2.26	0.38	0.87	95.17	67.52	162.68	4.000	Yes	No	2.00
4478	44.78	116.48	43.18	2.25	0.38	0.87	95.79	67.37	163.16	4.000	Yes	No	2.00
4479	44.79	117.15	42.75	2.25	0.38	0.87	96.37	67.22	163.60	4.000	Yes	No	2.00
4480	44.80	117.75	42.38	2.24	0.38	0.87	96.89	67.09	163.97	4.000	Yes	No	2.00
4481	44.81	118.04	42.18	2.24	0.38	0.87	97.30	67.05	164.35	0.421	No	No	0.45
4482	44.82	118.02	42.15	2.24	0.38	0.87	97.10	66.98	164.07	0.418	No	No	0.45
4483	44.83	117.72	42.27	2.24	0.38	0.87	96.81	66.99	163.80	0.415	No	No	0.45
4484	44.84	117.36	42.42	2.24	0.38	0.87	96.48	67.02	163.50	0.411	No	No	0.44
4485	44.85	116.96	42.58	2.24	0.38	0.87	96.13	67.04	163.17	0.407	No	No	0.44
4486	44.86	116.56	42.74	2.25	0.38	0.87	95.76	67.06	162.83	0.403	No	No	0.43
4487	44.87	116.18	42.90	2.25	0.38	0.87	95.41	67.09	162.50	0.399	No	No	0.43
4488	44.88	115.82	43.05	2.25	0.38	0.87	95.09	67.10	162.20	0.396	No	No	0.43
4489	44.89	115.52	43.17	2.25	0.38	0.87	94.82	67.12	161.94	0.393	No	No	0.42
4490	44.90	115.24	43.31	2.25	0.38	0.87	94.60	67.16	161.76	0.391	No	No	0.42
4491	44.91	114.95	43.46	2.26	0.39	0.87	94.35	67.20	161.55	0.388	No	No	0.42
4492	44.92	114.61	43.66	2.26	0.39	0.87	94.05	67.25	161.30	0.386	No	No	0.41
4493	44.93	114.24	43.87	2.26	0.39	0.87	93.71	67.31	161.02	0.382	No	No	0.41
4494	44.94	113.84	44.10	2.26	0.39	0.87	93.36	67.37	160.72	0.379	No	No	0.41
4495	44.95	113.44	44.33	2.27	0.39	0.87	93.00	67.42	160.42	0.376	No	No	0.40
4496	44.96	113.06	44.54	2.27	0.39	0.87	92.66	67.48	160.14	0.373	No	No	0.40
4497	44.97	112.72	44.74	2.27	0.39	0.87	92.35	67.52	159.88	0.370	No	No	0.40
4498	44.98	112.44	44.91	2.27	0.39	0.87	92.10	67.57	159.67	0.368	No	No	0.40
4499	44.99	112.20	45.10	2.28	0.39	0.87	91.91	67.64	159.55	0.367	No	No	0.39
4500	45.00	111.95	45.32	2.28	0.39	0.87	91.70	67.72	159.42	0.366	No	No	0.39
4501	45.01	111.67	45.59	2.28	0.39	0.87	91.45	67.81	159.26	0.364	No	No	0.39
4502	45.02	111.36	45.88	2.29	0.39	0.87	91.18	67.92	159.09	0.363	No	No	0.39
4503	45.03	111.04	46.18	2.29	0.39	0.87	90.89	68.02	158.91	0.361	No	No	0.39
4504	45.04	110.73	46.47	2.29	0.39	0.87	90.61	68.12	158.73	0.359	No	No	0.39
4505	45.05	110.43	46.74	2.30	0.39	0.87	90.35	68.21	158.56	0.357	No	No	0.38
4506	45.06	110.17	46.98	2.30	0.39	0.87	90.12	68.28	158.40	0.356	No	No	0.38
4507	45.07	109.95	47.20	2.30	0.39	0.87	89.93	68.35	158.29	0.355	No	No	0.38
4508	45.08	109.72	47.42	2.31	0.39	0.87	89.75	68.43	158.18	4.000	Yes	No	2.00
4509	45.09	109.47	47.67	2.31	0.39	0.87	89.53	68.51	158.04	4.000	Yes	No	2.00
4510	45.10	109.18	47.97	2.31	0.39	0.87	89.27	68.60	157.87	4.000	Yes	No	2.00
4511	45.11	108.87	48.28	2.32	0.39	0.87	88.99	68.69	157.68	4.000	Yes	No	2.00
4512	45.12	108.55	48.60	2.32	0.39	0.87	88.70	68.79	157.49	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4513	45.13	108.24	48.90	2.32	0.39	0.86	88.43	68.87	157.30	4.000	Yes	No	2.00
4514	45.14	107.95	49.18	2.33	0.39	0.86	88.18	68.95	157.12	4.000	Yes	No	2.00
4515	45.15	107.70	49.42	2.33	0.39	0.86	87.96	69.02	156.97	4.000	Yes	No	2.00
4516	45.16	107.43	49.67	2.33	0.39	0.86	87.76	69.09	156.85	4.000	Yes	No	2.00
4517	45.17	107.11	49.95	2.34	0.39	0.86	87.47	69.15	156.61	4.000	Yes	No	2.00
4518	45.18	106.71	50.29	2.34	0.39	0.86	87.11	69.22	156.33	4.000	Yes	No	2.00
4519	45.19	106.25	50.67	2.35	0.39	0.86	86.71	69.29	156.00	4.000	Yes	No	2.00
4520	45.20	105.78	51.06	2.35	0.39	0.86	86.29	69.37	155.66	4.000	Yes	No	2.00
4521	45.21	105.30	51.46	2.36	0.40	0.86	85.87	69.44	155.30	4.000	Yes	No	2.00
4522	45.22	104.84	51.83	2.36	0.40	0.86	85.46	69.50	154.97	4.000	Yes	No	2.00
4523	45.23	104.44	52.16	2.36	0.40	0.86	85.10	69.55	154.66	4.000	Yes	No	2.00
4524	45.24	104.09	52.45	2.37	0.40	0.86	84.80	69.60	154.41	4.000	Yes	No	2.00
4525	45.25	103.76	52.74	2.37	0.40	0.86	84.55	69.66	154.21	4.000	Yes	No	2.00
4526	45.26	103.40	53.05	2.38	0.40	0.86	84.23	69.70	153.94	4.000	Yes	No	2.00
4527	45.27	102.97	53.41	2.38	0.40	0.86	83.86	69.76	153.62	4.000	Yes	No	2.00
4528	45.28	102.51	53.81	2.39	0.40	0.86	83.45	69.81	153.26	4.000	Yes	No	2.00
4529	45.29	102.03	54.21	2.39	0.40	0.86	83.02	69.87	152.89	4.000	Yes	No	2.00
4530	45.30	101.56	54.61	2.40	0.40	0.86	82.61	69.91	152.52	4.000	Yes	No	2.00
4531	45.31	101.12	54.99	2.40	0.40	0.86	82.22	69.96	152.17	4.000	Yes	No	2.00
4532	45.32	100.73	55.31	2.40	0.40	0.86	81.88	69.99	151.87	4.000	Yes	No	2.00
4533	45.33	100.43	55.55	2.41	0.40	0.86	81.60	70.01	151.61	4.000	Yes	No	2.00
4534	45.34	100.17	55.74	2.41	0.40	0.86	81.42	70.03	151.45	0.299	No	No	0.32
4535	45.35	99.91	55.91	2.41	0.40	0.86	81.19	70.03	151.22	0.297	No	No	0.32
4536	45.36	99.62	56.11	2.41	0.40	0.86	80.93	70.03	150.96	0.295	No	No	0.32
4537	45.37	99.31	56.31	2.42	0.40	0.86	80.64	70.03	150.68	0.293	No	No	0.32
4538	45.38	98.99	56.52	2.42	0.40	0.86	80.36	70.03	150.39	0.291	No	No	0.31
4539	45.39	98.68	56.73	2.42	0.40	0.86	80.08	70.03	150.11	0.290	No	No	0.31
4540	45.40	98.39	56.91	2.42	0.40	0.86	79.83	70.03	149.86	0.288	No	No	0.31
4541	45.41	98.18	57.04	2.43	0.40	0.86	79.61	70.02	149.63	0.286	No	No	0.31
4542	45.42	98.10	57.06	2.43	0.40	0.86	79.51	70.00	149.51	0.286	No	No	0.31
4543	45.43	98.15	56.96	2.42	0.40	0.86	79.60	69.99	149.59	0.286	No	No	0.31
4544	45.44	98.29	56.77	2.42	0.40	0.86	79.71	69.94	149.65	0.287	No	No	0.31
4545	45.45	98.44	56.55	2.42	0.40	0.86	79.83	69.90	149.73	0.287	No	No	0.31
4546	45.46	98.60	56.32	2.42	0.40	0.86	79.96	69.85	149.81	0.288	No	No	0.31
4547	45.47	98.76	56.09	2.41	0.40	0.86	80.09	69.80	149.88	0.288	No	No	0.31
4548	45.48	98.91	55.87	2.41	0.40	0.86	80.21	69.75	149.96	0.289	No	No	0.31
4549	45.49	99.04	55.67	2.41	0.40	0.86	80.32	69.70	150.02	0.289	No	No	0.31
4550	45.50	99.23	55.45	2.41	0.40	0.86	80.40	69.64	150.04	4.000	Yes	No	2.00
4551	45.51	99.56	55.15	2.40	0.40	0.86	80.67	69.60	150.27	4.000	Yes	No	2.00
4552	45.52	100.07	54.73	2.40	0.40	0.86	81.13	69.56	150.69	4.000	Yes	No	2.00
4553	45.53	100.71	54.21	2.39	0.40	0.86	81.67	69.50	151.17	4.000	Yes	No	2.00
4554	45.54	101.40	53.63	2.38	0.40	0.86	82.27	69.42	151.69	4.000	Yes	No	2.00
4555	45.55	102.12	53.03	2.38	0.40	0.86	82.88	69.33	152.21	4.000	Yes	No	2.00
4556	45.56	102.83	52.43	2.37	0.40	0.86	83.49	69.24	152.72	4.000	Yes	No	2.00
4557	45.57	103.49	51.87	2.36	0.40	0.86	84.05	69.14	153.19	4.000	Yes	No	2.00
4558	45.58	104.06	51.38	2.35	0.40	0.86	84.54	69.05	153.58	4.000	Yes	No	2.00
4559	45.59	104.60	50.94	2.35	0.40	0.86	84.92	68.95	153.87	4.000	Yes	No	2.00
4560	45.60	105.19	50.50	2.34	0.40	0.86	85.40	68.86	154.26	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4561	45.61	105.89	49.98	2.34	0.40	0.86	86.00	68.78	154.78	4.000	Yes	No	2.00
4562	45.62	106.70	49.39	2.33	0.39	0.86	86.69	68.67	155.36	4.000	Yes	No	2.00
4563	45.63	107.56	48.75	2.32	0.39	0.86	87.44	68.54	155.97	4.000	Yes	No	2.00
4564	45.64	108.44	48.10	2.31	0.39	0.86	88.19	68.39	156.58	4.000	Yes	No	2.00
4565	45.65	109.29	47.46	2.31	0.39	0.86	88.91	68.23	157.15	4.000	Yes	No	2.00
4566	45.66	110.07	46.87	2.30	0.39	0.86	89.58	68.08	157.65	4.000	Yes	No	2.00
4567	45.67	110.72	46.38	2.29	0.39	0.86	90.14	67.94	158.08	4.000	Yes	No	2.00
4568	45.68	111.25	45.99	2.29	0.39	0.86	90.54	67.82	158.36	4.000	Yes	No	2.00
4569	45.69	111.75	45.64	2.28	0.39	0.86	90.92	67.71	158.63	4.000	Yes	No	2.00
4570	45.70	112.29	45.28	2.28	0.39	0.86	91.38	67.60	158.98	4.000	Yes	No	2.00
4571	45.71	112.90	44.86	2.27	0.39	0.86	91.89	67.48	159.38	4.000	Yes	No	2.00
4572	45.72	113.53	44.43	2.27	0.39	0.86	92.44	67.35	159.78	4.000	Yes	No	2.00
4573	45.73	114.17	43.99	2.26	0.39	0.86	92.98	67.20	160.18	4.000	Yes	No	2.00
4574	45.74	114.77	43.57	2.26	0.39	0.86	93.49	67.06	160.54	4.000	Yes	No	2.00
4575	45.75	115.31	43.19	2.25	0.39	0.86	93.95	66.92	160.87	4.000	Yes	No	2.00
4576	45.76	115.73	42.91	2.25	0.39	0.86	94.32	66.82	161.14	4.000	Yes	No	2.00
4577	45.77	116.04	42.69	2.25	0.39	0.86	94.53	66.72	161.25	0.385	No	No	0.41
4578	45.78	116.31	42.52	2.24	0.39	0.86	94.73	66.65	161.38	0.386	No	No	0.42
4579	45.79	116.59	42.34	2.24	0.39	0.86	94.96	66.58	161.55	0.388	No	No	0.42
4580	45.80	116.90	42.14	2.24	0.39	0.86	95.22	66.51	161.73	0.390	No	No	0.42
4581	45.81	117.22	41.94	2.24	0.38	0.86	95.49	66.42	161.91	0.392	No	No	0.42
4582	45.82	117.53	41.73	2.23	0.38	0.86	95.75	66.34	162.09	0.394	No	No	0.42
4583	45.83	117.83	41.54	2.23	0.38	0.86	96.00	66.26	162.26	0.396	No	No	0.43
4584	45.84	118.08	41.38	2.23	0.38	0.86	96.21	66.19	162.40	0.398	No	No	0.43
4585	45.85	118.36	41.20	2.23	0.38	0.86	96.38	66.10	162.48	0.399	No	No	0.43
4586	45.86	118.70	40.99	2.22	0.38	0.86	96.68	66.02	162.70	0.401	No	No	0.43
4587	45.87	119.15	40.72	2.22	0.38	0.86	97.06	65.91	162.97	0.404	No	No	0.44
4588	45.88	119.67	40.42	2.22	0.38	0.86	97.50	65.78	163.27	0.408	No	No	0.44
4589	45.89	120.22	40.08	2.21	0.38	0.86	97.96	65.63	163.59	0.412	No	No	0.44
4590	45.90	120.78	39.74	2.21	0.38	0.86	98.44	65.47	163.91	0.416	No	No	0.45
4591	45.91	121.32	39.41	2.21	0.38	0.86	98.90	65.31	164.21	0.420	No	No	0.45
4592	45.92	121.81	39.11	2.20	0.38	0.86	99.31	65.16	164.47	0.423	No	No	0.45
4593	45.93	122.26	38.85	2.20	0.38	0.86	99.66	65.02	164.69	0.426	No	No	0.46
4594	45.94	122.74	38.58	2.19	0.38	0.86	100.00	64.87	164.87	0.428	No	No	0.46
4595	45.95	123.34	38.26	2.19	0.38	0.86	100.53	64.72	165.25	0.433	No	No	0.47
4596	45.96	124.09	37.88	2.19	0.38	0.86	101.16	64.53	165.70	0.439	No	No	0.47
4597	45.97	124.92	37.45	2.18	0.38	0.86	101.88	64.31	166.19	0.446	No	No	0.48
4598	45.98	125.80	37.00	2.17	0.38	0.86	102.63	64.06	166.69	0.453	No	No	0.49
4599	45.99	126.67	36.54	2.17	0.38	0.86	103.37	63.80	167.18	0.460	No	No	0.49
4600	46.00	127.50	36.11	2.16	0.38	0.86	104.08	63.54	167.62	0.466	No	No	0.50
4601	46.01	128.24	35.72	2.16	0.38	0.86	104.71	63.30	168.01	0.472	No	No	0.51
4602	46.02	128.87	35.39	2.15	0.38	0.86	105.22	63.07	168.29	0.477	No	No	0.51
4603	46.03	129.48	35.05	2.15	0.37	0.86	105.66	62.82	168.48	0.479	No	No	0.52
4604	46.04	130.15	34.67	2.15	0.37	0.86	106.23	62.54	168.77	0.484	No	No	0.52
4605	46.05	130.93	34.22	2.14	0.37	0.86	106.89	62.19	169.08	0.489	No	No	0.53
4606	46.06	131.79	33.72	2.13	0.37	0.86	107.61	61.80	169.41	0.494	No	No	0.53
4607	46.07	132.67	33.21	2.13	0.37	0.86	108.35	61.37	169.72	0.499	No	No	0.54
4608	46.08	133.53	32.70	2.12	0.37	0.86	109.08	60.92	169.99	0.504	No	No	0.54

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4609	46.09	134.33	32.23	2.12	0.37	0.86	109.75	60.48	170.23	0.508	No	No	0.55
4610	46.10	135.03	31.82	2.11	0.37	0.86	110.34	60.10	170.43	0.511	No	No	0.55
4611	46.11	135.61	31.68	2.11	0.37	0.86	110.81	60.01	170.82	0.518	No	No	0.56
4612	46.12	136.15	31.79	2.11	0.37	0.86	111.23	60.25	171.47	0.530	No	No	0.57
4613	46.13	136.73	32.14	2.11	0.37	0.87	111.77	60.81	172.58	0.550	No	No	0.59
4614	46.14	137.40	32.53	2.12	0.37	0.87	112.40	61.43	173.82	0.575	No	No	0.62
4615	46.15	138.11	32.94	2.12	0.37	0.87	113.06	62.07	175.13	0.603	No	No	0.65
4616	46.16	138.83	33.35	2.13	0.36	0.87	113.74	62.70	176.44	0.633	No	No	0.68
4617	46.17	139.52	33.73	2.13	0.36	0.87	114.43	63.30	177.73	0.665	No	No	0.72
4618	46.18	140.15	34.07	2.14	0.36	0.87	115.02	63.83	178.85	0.695	No	No	0.75
4619	46.19	140.68	34.37	2.14	0.36	0.87	115.52	64.28	179.80	0.721	No	No	0.78
4620	46.20	141.13	34.66	2.15	0.36	0.87	115.89	64.69	180.57	0.744	No	No	0.80
4621	46.21	141.56	34.99	2.15	0.36	0.87	116.26	65.14	181.40	0.769	No	No	0.83
4622	46.22	142.04	35.38	2.15	0.35	0.87	116.72	65.66	182.37	0.801	No	No	0.86
4623	46.23	142.57	35.80	2.16	0.35	0.87	117.22	66.23	183.45	0.838	No	No	0.90
4624	46.24	143.13	36.24	2.17	0.35	0.87	117.75	66.80	184.55	0.879	No	No	0.94
4625	46.25	143.69	36.67	2.17	0.35	0.87	118.28	67.36	185.64	0.921	No	No	0.99
4626	46.26	144.21	37.06	2.18	0.35	0.87	118.78	67.87	186.65	0.964	No	No	1.04
4627	46.27	144.68	37.41	2.18	0.35	0.87	119.22	68.32	187.54	1.004	No	No	1.08
4628	46.28	144.99	37.58	2.18	0.35	0.87	119.57	68.57	188.14	1.032	No	No	1.11
4629	46.29	145.11	37.54	2.18	0.35	0.87	119.60	68.53	188.13	1.031	No	No	1.11
4630	46.30	145.08	37.27	2.18	0.35	0.87	119.52	68.25	187.77	1.014	No	No	1.09
4631	46.31	145.01	36.91	2.17	0.35	0.87	119.42	67.87	187.29	0.992	No	No	1.07
4632	46.32	144.93	36.52	2.17	0.35	0.87	119.31	67.44	186.75	0.968	No	No	1.04
4633	46.33	144.85	36.10	2.16	0.35	0.87	119.20	66.99	186.18	0.944	No	No	1.01
4634	46.34	144.77	35.68	2.16	0.35	0.87	119.08	66.53	185.61	0.920	No	No	0.99
4635	46.35	144.70	35.30	2.15	0.35	0.87	118.98	66.08	185.06	0.898	No	No	0.97
4636	46.36	144.63	34.96	2.15	0.35	0.87	118.88	65.70	184.58	0.880	No	No	0.95
4637	46.37	144.40	34.82	2.15	0.35	0.87	118.79	65.51	184.30	0.869	No	No	0.93
4638	46.38	143.98	34.85	2.15	0.35	0.87	118.31	65.44	183.75	0.849	No	No	0.91
4639	46.39	143.33	35.05	2.15	0.35	0.87	117.72	65.53	183.25	0.831	No	No	0.89
4640	46.40	142.59	35.27	2.15	0.35	0.87	117.06	65.62	182.68	0.811	No	No	0.87
4641	46.41	141.80	35.50	2.16	0.35	0.87	116.35	65.71	182.06	0.791	No	No	0.85
4642	46.42	141.00	35.75	2.16	0.36	0.87	115.63	65.80	181.44	0.770	No	No	0.83
4643	46.43	140.23	35.98	2.16	0.36	0.87	114.94	65.89	180.83	0.752	No	No	0.81
4644	46.44	139.53	36.19	2.16	0.36	0.87	114.31	65.96	180.28	0.735	No	No	0.79
4645	46.45	138.90	36.41	2.17	0.36	0.87	113.78	66.06	179.84	4.000	Yes	No	2.00
4646	46.46	138.19	36.71	2.17	0.36	0.87	113.26	66.24	179.50	4.000	Yes	No	2.00
4647	46.47	137.31	37.14	2.18	0.36	0.87	112.46	66.48	178.93	4.000	Yes	No	2.00
4648	46.48	136.22	37.69	2.18	0.36	0.87	111.49	66.78	178.27	4.000	Yes	No	2.00
4649	46.49	135.00	38.31	2.19	0.36	0.87	110.42	67.10	177.52	4.000	Yes	No	2.00
4650	46.50	133.72	38.95	2.20	0.36	0.86	109.27	67.39	176.66	4.000	Yes	No	2.00
4651	46.51	132.45	39.58	2.21	0.36	0.86	108.15	67.67	175.82	4.000	Yes	No	2.00
4652	46.52	131.25	40.18	2.21	0.37	0.86	107.09	67.92	175.01	4.000	Yes	No	2.00
4653	46.53	130.19	40.71	2.22	0.37	0.86	106.15	68.11	174.26	4.000	Yes	No	2.00
4654	46.54	129.18	41.19	2.23	0.37	0.86	105.38	68.30	173.68	4.000	Yes	No	2.00
4655	46.55	128.04	41.69	2.23	0.37	0.86	104.46	68.45	172.91	4.000	Yes	No	2.00
4656	46.56	126.62	42.26	2.24	0.37	0.86	103.18	68.56	171.74	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4657	46.57	124.94	42.94	2.25	0.37	0.86	101.70	68.68	170.38	4.000	Yes	No	2.00
4658	46.58	123.12	43.68	2.26	0.37	0.86	100.09	68.79	168.87	4.000	Yes	No	2.00
4659	46.59	121.23	44.44	2.27	0.38	0.86	98.43	68.87	167.30	4.000	Yes	No	2.00
4660	46.60	119.39	45.19	2.28	0.38	0.86	96.81	68.94	165.75	4.000	Yes	No	2.00
4661	46.61	117.69	45.89	2.29	0.38	0.86	95.31	68.98	164.29	4.000	Yes	No	2.00
4662	46.62	116.21	46.50	2.29	0.38	0.86	94.00	69.01	163.01	4.000	Yes	No	2.00
4663	46.63	114.90	47.12	2.30	0.38	0.86	92.98	69.10	162.08	4.000	Yes	No	2.00
4664	46.64	113.58	47.83	2.31	0.39	0.86	91.92	69.22	161.14	4.000	Yes	No	2.00
4665	46.65	112.06	48.72	2.32	0.39	0.86	90.59	69.35	159.94	4.000	Yes	No	2.00
4666	46.66	110.34	49.72	2.33	0.39	0.85	89.08	69.46	158.55	4.000	Yes	No	2.00
4667	46.67	108.49	50.79	2.35	0.39	0.85	87.48	69.56	157.04	4.000	Yes	No	2.00
4668	46.68	106.63	51.86	2.36	0.39	0.85	85.86	69.62	155.48	4.000	Yes	No	2.00
4669	46.69	104.84	52.88	2.37	0.40	0.85	84.30	69.65	153.95	4.000	Yes	No	2.00
4670	46.70	103.22	53.81	2.39	0.40	0.85	82.89	69.66	152.55	4.000	Yes	No	2.00
4671	46.71	101.83	54.62	2.40	0.40	0.85	81.69	69.67	151.36	4.000	Yes	No	2.00
4672	46.72	100.57	55.41	2.41	0.40	0.85	80.76	69.72	150.48	4.000	Yes	No	2.00
4673	46.73	99.26	56.29	2.42	0.40	0.85	79.66	69.75	149.41	4.000	Yes	No	2.00
4674	46.74	97.74	57.33	2.43	0.41	0.85	78.34	69.77	148.11	4.000	Yes	No	2.00
4675	46.75	96.05	58.48	2.44	0.41	0.85	76.88	69.76	146.64	4.000	Yes	No	2.00
4676	46.76	94.28	59.67	2.46	0.41	0.85	75.35	69.73	145.08	4.000	Yes	No	2.00
4677	46.77	92.52	60.85	2.47	0.41	0.85	73.83	69.68	143.51	4.000	Yes	No	2.00
4678	46.78	90.85	61.96	2.49	0.42	0.84	72.40	69.61	142.01	4.000	Yes	No	2.00
4679	46.79	89.38	62.94	2.50	0.42	0.84	71.13	69.54	140.66	4.000	Yes	No	2.00
4680	46.80	88.14	63.78	2.51	0.42	0.84	70.09	69.48	139.57	4.000	Yes	No	2.00
4681	46.81	87.00	64.56	2.52	0.42	0.84	69.26	69.45	138.71	4.000	Yes	No	2.00
4682	46.82	85.79	65.41	2.53	0.42	0.84	68.22	69.38	137.61	4.000	Yes	No	2.00
4683	46.83	84.39	66.39	2.54	0.43	0.84	67.02	69.29	136.31	4.000	Yes	No	2.00
4684	46.84	82.87	67.45	2.56	0.43	0.84	65.72	69.17	134.90	4.000	Yes	No	2.00
4685	46.85	81.31	68.54	2.57	0.43	0.84	64.39	69.04	133.43	4.000	Yes	No	2.00
4686	46.86	79.78	69.60	2.58	0.43	0.84	63.08	68.91	131.99	4.000	Yes	No	2.00
4687	46.87	78.37	70.59	2.59	0.44	0.84	61.88	68.77	130.65	4.000	Yes	No	2.00
4688	46.88	77.15	71.44	2.61	0.44	0.84	60.83	0.00	60.83	4.000	Yes	Yes	2.00
4689	46.89	76.07	72.13	2.61	0.44	0.84	60.02	0.00	60.02	4.000	Yes	Yes	2.00
4690	46.90	75.01	72.76	2.62	0.44	0.83	59.18	0.00	59.18	4.000	Yes	Yes	2.00
4691	46.91	73.80	73.43	2.63	0.44	0.83	58.16	0.00	58.16	4.000	Yes	Yes	2.00
4692	46.92	72.43	74.20	2.64	0.45	0.83	56.99	0.00	56.99	4.000	Yes	Yes	2.00
4693	46.93	70.97	75.02	2.65	0.45	0.83	55.75	0.00	55.75	4.000	Yes	Yes	2.00
4694	46.94	69.49	75.87	2.66	0.45	0.83	54.50	0.00	54.50	4.000	Yes	Yes	2.00
4695	46.95	68.07	76.70	2.67	0.46	0.83	53.31	0.00	53.31	4.000	Yes	Yes	2.00
4696	46.96	66.78	77.45	2.68	0.46	0.83	52.22	0.00	52.22	4.000	Yes	Yes	2.00
4697	46.97	65.71	78.07	2.69	0.46	0.83	51.31	0.00	51.31	4.000	Yes	Yes	2.00
4698	46.98	64.81	78.56	2.69	0.46	0.83	50.65	0.00	50.65	4.000	Yes	Yes	2.00
4699	46.99	63.93	78.98	2.70	0.46	0.83	49.97	0.00	49.97	4.000	Yes	Yes	2.00
4700	47.00	62.96	79.43	2.71	0.47	0.83	49.15	0.00	49.15	4.000	Yes	Yes	2.00
4701	47.01	61.88	79.94	2.71	0.47	0.83	48.24	0.00	48.24	4.000	Yes	Yes	2.00
4702	47.02	60.75	80.48	2.72	0.47	0.82	47.29	0.00	47.29	4.000	Yes	Yes	2.00
4703	47.03	59.62	81.03	2.73	0.47	0.82	46.36	0.00	46.36	4.000	Yes	Yes	2.00
4704	47.04	58.56	81.56	2.73	0.47	0.82	45.47	0.00	45.47	4.000	Yes	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4705	47.05	57.63	82.03	2.74	0.48	0.82	44.69	0.00	44.69	4.000	Yes	Yes	2.00
4706	47.06	56.97	82.38	2.74	0.48	0.82	44.05	0.00	44.05	4.000	Yes	Yes	2.00
4707	47.07	56.57	82.62	2.75	0.48	0.82	43.85	0.00	43.85	4.000	No	Yes	2.00
4708	47.08	56.36	82.77	2.75	0.48	0.82	43.71	0.00	43.71	4.000	No	Yes	2.00
4709	47.09	56.16	82.92	2.75	0.48	0.82	43.53	0.00	43.53	4.000	No	Yes	2.00
4710	47.10	55.94	83.09	2.75	0.48	0.82	43.35	0.00	43.35	4.000	No	Yes	2.00
4711	47.11	55.72	83.27	2.75	0.48	0.82	43.16	0.00	43.16	4.000	No	Yes	2.00
4712	47.12	55.50	83.44	2.76	0.48	0.82	42.98	0.00	42.98	4.000	No	Yes	2.00
4713	47.13	55.30	83.59	2.76	0.48	0.82	42.80	0.00	42.80	4.000	No	Yes	2.00
4714	47.14	55.14	83.72	2.76	0.48	0.82	42.66	0.00	42.66	4.000	No	Yes	2.00
4715	47.15	55.12	83.78	2.76	0.48	0.82	42.57	0.00	42.57	4.000	No	Yes	2.00
4716	47.16	55.25	83.76	2.76	0.48	0.82	42.74	0.00	42.74	4.000	No	Yes	2.00
4717	47.17	55.51	83.68	2.76	0.48	0.82	42.96	0.00	42.96	4.000	No	Yes	2.00
4718	47.18	55.81	83.59	2.76	0.48	0.82	43.20	0.00	43.20	4.000	No	Yes	2.00
4719	47.19	56.13	83.50	2.76	0.48	0.82	43.46	0.00	43.46	4.000	No	Yes	2.00
4720	47.20	56.45	83.41	2.76	0.48	0.82	43.72	0.00	43.72	4.000	No	Yes	2.00
4721	47.21	56.75	83.32	2.75	0.48	0.82	43.97	0.00	43.97	4.000	No	Yes	2.00
4722	47.22	57.03	83.24	2.75	0.48	0.82	44.19	0.00	44.19	4.000	No	Yes	2.00
4723	47.23	57.29	83.14	2.75	0.48	0.82	44.38	0.00	44.38	4.000	No	Yes	2.00
4724	47.24	57.59	82.96	2.75	0.48	0.82	44.58	0.00	44.58	4.000	No	Yes	2.00
4725	47.25	57.97	82.68	2.75	0.48	0.82	44.91	0.00	44.91	4.000	No	Yes	2.00
4726	47.26	58.44	82.31	2.74	0.47	0.82	45.29	0.00	45.29	4.000	No	Yes	2.00
4727	47.27	58.97	81.89	2.74	0.47	0.82	45.72	0.00	45.72	4.000	No	Yes	2.00
4728	47.28	59.51	81.46	2.73	0.47	0.82	46.17	0.00	46.17	4.000	No	Yes	2.00
4729	47.29	60.06	81.04	2.73	0.47	0.82	46.61	0.00	46.61	4.000	No	Yes	2.00
4730	47.30	60.57	80.64	2.72	0.47	0.82	47.03	0.00	47.03	4.000	No	Yes	2.00
4731	47.31	61.02	80.29	2.72	0.47	0.82	47.40	0.00	47.40	4.000	No	Yes	2.00
4732	47.32	61.41	79.96	2.71	0.47	0.82	47.70	0.00	47.70	4.000	No	Yes	2.00
4733	47.33	61.78	79.60	2.71	0.47	0.82	47.97	0.00	47.97	4.000	No	Yes	2.00
4734	47.34	62.20	79.17	2.70	0.47	0.82	48.31	0.00	48.31	4.000	No	Yes	2.00
4735	47.35	62.68	78.66	2.70	0.47	0.82	48.70	0.00	48.70	4.000	No	Yes	2.00
4736	47.36	63.20	78.10	2.69	0.47	0.82	49.12	0.00	49.12	4.000	No	Yes	2.00
4737	47.37	63.73	77.52	2.68	0.46	0.82	49.56	0.00	49.56	4.000	No	Yes	2.00
4738	47.38	64.25	76.96	2.67	0.46	0.82	49.99	0.00	49.99	4.000	No	Yes	2.00
4739	47.39	64.73	76.44	2.67	0.46	0.82	50.38	0.00	50.38	4.000	No	Yes	2.00
4740	47.40	65.15	75.99	2.66	0.46	0.82	50.72	0.00	50.72	4.000	No	Yes	2.00
4741	47.41	65.53	75.56	2.66	0.46	0.82	50.99	0.00	50.99	4.000	No	Yes	2.00
4742	47.42	65.93	75.11	2.65	0.46	0.82	51.30	0.00	51.30	4.000	No	Yes	2.00
4743	47.43	66.40	74.57	2.64	0.46	0.82	51.68	0.00	51.68	4.000	No	Yes	2.00
4744	47.44	66.93	73.95	2.64	0.46	0.82	52.12	0.00	52.12	4.000	No	Yes	2.00
4745	47.45	67.50	73.28	2.63	0.46	0.82	52.58	0.00	52.58	4.000	No	Yes	2.00
4746	47.46	68.07	72.61	2.62	0.46	0.83	53.05	0.00	53.05	4.000	No	Yes	2.00
4747	47.47	68.61	71.96	2.61	0.46	0.83	53.50	0.00	53.50	4.000	No	Yes	2.00
4748	47.48	69.10	71.37	2.60	0.46	0.83	53.90	0.00	53.90	4.000	No	Yes	2.00
4749	47.49	69.48	70.89	2.60	0.46	0.83	54.24	66.60	120.85	0.173	No	No	0.19
4750	47.50	69.71	70.51	2.59	0.46	0.83	54.40	66.57	120.97	0.174	No	No	0.19
4751	47.51	69.84	70.16	2.59	0.46	0.83	54.46	66.52	120.97	0.174	No	No	0.19
4752	47.52	69.93	69.79	2.58	0.45	0.83	54.52	66.46	120.98	0.174	No	No	0.19

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4753	47.53	70.03	69.37	2.58	0.45	0.83	54.60	66.39	120.99	0.174	No	No	0.19
4754	47.54	70.14	68.92	2.57	0.45	0.83	54.68	66.31	120.99	0.174	No	No	0.19
4755	47.55	70.24	68.48	2.57	0.45	0.83	54.76	66.24	121.00	0.174	No	No	0.19
4756	47.56	70.34	68.05	2.56	0.45	0.83	54.83	66.16	121.00	0.174	No	No	0.19
4757	47.57	70.43	67.68	2.56	0.45	0.83	54.90	66.10	120.99	0.174	No	No	0.19
4758	47.58	70.45	67.39	2.55	0.45	0.83	54.95	66.05	120.99	0.174	No	No	0.19
4759	47.59	70.41	67.16	2.55	0.46	0.82	54.88	65.97	120.85	0.173	No	No	0.19
4760	47.60	70.29	66.96	2.55	0.46	0.82	54.77	65.89	120.66	0.173	No	No	0.19
4761	47.61	70.15	66.74	2.55	0.46	0.82	54.64	65.80	120.44	0.172	No	No	0.19
4762	47.62	69.99	66.49	2.54	0.46	0.82	54.50	65.71	120.20	0.172	No	No	0.19
4763	47.63	69.83	66.24	2.54	0.46	0.82	54.35	65.60	119.96	0.171	No	No	0.18
4764	47.64	69.67	65.99	2.54	0.46	0.82	54.21	65.50	119.72	0.171	No	No	0.18
4765	47.65	69.53	65.75	2.53	0.46	0.82	54.09	65.41	119.50	0.170	No	No	0.18
4766	47.66	69.44	65.54	2.53	0.46	0.82	53.97	65.33	119.30	0.170	No	No	0.18
4767	47.67	69.56	65.28	2.53	0.46	0.82	53.96	65.26	119.22	0.170	No	No	0.18
4768	47.68	69.92	64.95	2.52	0.46	0.82	54.36	65.29	119.65	0.171	No	No	0.18
4769	47.69	70.52	64.51	2.52	0.46	0.82	54.85	65.32	120.17	0.172	No	No	0.19
4770	47.70	71.19	64.02	2.51	0.46	0.82	55.40	65.36	120.76	0.173	No	No	0.19
4771	47.71	71.90	63.50	2.51	0.45	0.82	55.99	65.39	121.38	0.175	No	No	0.19
4772	47.72	72.62	62.97	2.50	0.45	0.82	56.58	65.42	122.00	0.176	No	No	0.19
4773	47.73	73.31	62.47	2.49	0.45	0.83	57.15	65.44	122.59	0.177	No	No	0.19
4774	47.74	73.93	62.02	2.49	0.45	0.83	57.66	65.46	123.13	0.179	No	No	0.19
4775	47.75	74.39	61.66	2.48	0.45	0.83	58.09	65.48	123.57	0.180	No	No	0.19
4776	47.76	74.68	61.39	2.48	0.45	0.83	58.28	65.46	123.74	0.180	No	No	0.19
4777	47.77	74.82	61.16	2.48	0.45	0.83	58.35	65.41	123.76	0.180	No	No	0.19
4778	47.78	74.93	60.91	2.47	0.45	0.83	58.42	65.36	123.79	0.180	No	No	0.19
4779	47.79	75.04	60.64	2.47	0.45	0.83	58.51	65.31	123.82	0.180	No	No	0.19
4780	47.80	75.16	60.35	2.47	0.45	0.83	58.60	65.25	123.85	0.181	No	No	0.19
4781	47.81	75.28	60.07	2.46	0.45	0.83	58.69	65.19	123.88	0.181	No	No	0.19
4782	47.82	75.39	59.80	2.46	0.45	0.83	58.78	65.13	123.91	0.181	No	No	0.19
4783	47.83	75.49	59.56	2.46	0.45	0.83	58.85	65.08	123.93	0.181	No	No	0.19
4784	47.84	75.42	59.45	2.46	0.45	0.83	58.91	65.07	123.98	0.181	No	No	0.19
4785	47.85	75.14	59.48	2.46	0.45	0.82	58.60	64.99	123.58	0.180	No	No	0.19
4786	47.86	74.62	59.66	2.46	0.45	0.82	58.14	64.91	123.05	0.179	No	No	0.19
4787	47.87	73.99	59.87	2.46	0.45	0.82	57.60	64.83	122.43	0.177	No	No	0.19
4788	47.88	73.31	60.11	2.46	0.45	0.82	57.03	64.74	121.77	0.175	No	No	0.19
4789	47.89	72.62	60.35	2.47	0.45	0.82	56.45	64.64	121.09	0.174	No	No	0.19
4790	47.90	71.94	60.59	2.47	0.46	0.82	55.88	64.55	120.43	0.172	No	No	0.19
4791	47.91	71.32	60.82	2.47	0.46	0.82	55.35	64.47	119.82	0.171	No	No	0.18
4792	47.92	70.80	61.03	2.48	0.46	0.82	54.90	64.40	119.31	0.170	No	No	0.18
4793	47.93	70.40	61.29	2.48	0.46	0.82	54.58	64.39	118.96	0.169	No	No	0.18
4794	47.94	70.07	61.64	2.48	0.46	0.82	54.35	64.42	118.78	0.169	No	No	0.18
4795	47.95	69.74	62.11	2.49	0.46	0.82	54.08	64.47	118.55	0.168	No	No	0.18
4796	47.96	69.37	62.63	2.50	0.46	0.82	53.77	64.53	118.30	0.168	No	No	0.18
4797	47.97	68.98	63.18	2.50	0.46	0.82	53.45	64.58	118.03	0.167	No	No	0.18
4798	47.98	68.59	63.72	2.51	0.46	0.82	53.12	64.63	117.75	0.167	No	No	0.18
4799	47.99	68.21	64.24	2.52	0.46	0.82	52.81	64.67	117.48	0.166	No	No	0.18
4800	48.00	67.88	64.70	2.52	0.46	0.82	52.52	64.71	117.23	0.166	No	No	0.18

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4801	48.01	67.55	65.14	2.53	0.46	0.82	52.29	64.75	117.04	0.165	No	No	0.18
4802	48.02	67.16	65.64	2.53	0.46	0.82	52.01	64.79	116.80	0.165	No	No	0.18
4803	48.03	66.66	66.27	2.54	0.46	0.82	51.57	64.81	116.39	0.164	No	No	0.18
4804	48.04	66.04	67.04	2.55	0.46	0.82	51.06	64.84	115.90	0.163	No	No	0.18
4805	48.05	65.36	67.88	2.56	0.47	0.82	50.49	64.87	115.36	0.162	No	No	0.17
4806	48.06	64.65	68.75	2.57	0.47	0.82	49.91	64.89	114.80	0.161	No	No	0.17
4807	48.07	63.94	69.60	2.58	0.47	0.82	49.32	64.90	114.23	0.160	No	No	0.17
4808	48.08	63.28	70.40	2.59	0.47	0.82	48.78	64.91	113.69	0.159	No	No	0.17
4809	48.09	62.70	71.09	2.60	0.47	0.82	48.30	0.00	48.30	4.000	No	Yes	2.00
4810	48.10	62.22	71.66	2.61	0.47	0.82	47.91	0.00	47.91	4.000	No	Yes	2.00
4811	48.11	61.77	72.18	2.61	0.47	0.82	47.59	0.00	47.59	4.000	No	Yes	2.00
4812	48.12	61.29	72.71	2.62	0.47	0.81	47.20	0.00	47.20	4.000	No	Yes	2.00
4813	48.13	60.75	73.32	2.63	0.47	0.81	46.74	0.00	46.74	4.000	No	Yes	2.00
4814	48.14	60.15	73.98	2.64	0.47	0.81	46.25	0.00	46.25	4.000	No	Yes	2.00
4815	48.15	59.55	74.65	2.65	0.48	0.81	45.75	0.00	45.75	4.000	No	Yes	2.00
4816	48.16	58.96	75.30	2.65	0.48	0.81	45.27	0.00	45.27	4.000	No	Yes	2.00
4817	48.17	58.42	75.90	2.66	0.48	0.81	44.82	0.00	44.82	4.000	No	Yes	2.00
4818	48.18	57.97	76.38	2.67	0.48	0.81	44.44	0.00	44.44	4.000	No	Yes	2.00
4819	48.19	57.65	76.66	2.67	0.48	0.81	44.18	0.00	44.18	4.000	No	Yes	2.00
4820	48.20	57.43	76.77	2.67	0.48	0.81	44.05	0.00	44.05	4.000	No	Yes	2.00
4821	48.21	57.25	76.77	2.67	0.48	0.81	43.89	0.00	43.89	4.000	No	Yes	2.00
4822	48.22	57.04	76.77	2.67	0.48	0.81	43.72	0.00	43.72	4.000	No	Yes	2.00
4823	48.23	56.82	76.77	2.67	0.48	0.81	43.53	0.00	43.53	4.000	No	Yes	2.00
4824	48.24	56.60	76.77	2.67	0.48	0.81	43.35	0.00	43.35	4.000	No	Yes	2.00
4825	48.25	56.39	76.77	2.67	0.48	0.81	43.17	0.00	43.17	4.000	No	Yes	2.00
4826	48.26	56.20	76.77	2.67	0.48	0.81	43.01	0.00	43.01	4.000	No	Yes	2.00
4827	48.27	56.11	76.68	2.67	0.48	0.81	42.88	0.00	42.88	4.000	Yes	Yes	2.00
4828	48.28	56.20	76.39	2.67	0.48	0.81	42.95	0.00	42.95	4.000	Yes	Yes	2.00
4829	48.29	56.46	75.87	2.66	0.48	0.81	43.19	0.00	43.19	4.000	Yes	Yes	2.00
4830	48.30	56.82	75.17	2.65	0.48	0.81	43.48	0.00	43.48	4.000	Yes	Yes	2.00
4831	48.31	57.23	74.38	2.64	0.48	0.81	43.81	0.00	43.81	4.000	Yes	Yes	2.00
4832	48.32	57.64	73.56	2.63	0.48	0.81	44.14	0.00	44.14	4.000	Yes	Yes	2.00
4833	48.33	58.06	72.73	2.62	0.48	0.81	44.47	0.00	44.47	4.000	Yes	Yes	2.00
4834	48.34	58.45	71.94	2.61	0.48	0.81	44.78	0.00	44.78	4.000	Yes	Yes	2.00
4835	48.35	58.79	71.25	2.60	0.48	0.81	45.05	0.00	45.05	4.000	Yes	Yes	2.00
4836	48.36	59.16	70.60	2.60	0.48	0.81	45.27	63.92	109.19	4.000	Yes	No	2.00
4837	48.37	59.64	69.92	2.59	0.48	0.81	45.66	63.90	109.56	4.000	Yes	No	2.00
4838	48.38	60.28	69.12	2.58	0.48	0.81	46.18	63.89	110.07	4.000	Yes	No	2.00
4839	48.39	61.02	68.19	2.56	0.48	0.81	46.78	63.86	110.64	4.000	Yes	No	2.00
4840	48.40	61.82	67.17	2.55	0.47	0.81	47.43	63.83	111.25	4.000	Yes	No	2.00
4841	48.41	62.64	66.12	2.54	0.47	0.81	48.09	63.78	111.86	4.000	Yes	No	2.00
4842	48.42	63.43	65.09	2.53	0.47	0.81	48.73	63.72	112.45	4.000	Yes	No	2.00
4843	48.43	64.16	64.14	2.51	0.47	0.81	49.32	63.65	112.97	4.000	Yes	No	2.00
4844	48.44	64.78	63.33	2.50	0.47	0.81	49.82	63.59	113.41	4.000	Yes	No	2.00
4845	48.45	65.33	62.69	2.50	0.47	0.81	50.21	63.53	113.74	4.000	Yes	No	2.00
4846	48.46	65.88	62.13	2.49	0.47	0.81	50.62	63.50	114.13	4.000	Yes	No	2.00
4847	48.47	66.51	61.55	2.48	0.47	0.81	51.14	63.49	114.62	4.000	Yes	No	2.00
4848	48.48	67.22	60.91	2.47	0.47	0.81	51.71	63.47	115.18	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4849	48.49	67.97	60.22	2.47	0.47	0.81	52.32	63.45	115.76	4.000	Yes	No	2.00
4850	48.50	68.72	59.52	2.46	0.46	0.82	52.93	63.41	116.34	4.000	Yes	No	2.00
4851	48.51	69.43	58.86	2.45	0.46	0.82	53.51	63.38	116.89	4.000	Yes	No	2.00
4852	48.52	70.07	58.27	2.44	0.46	0.82	54.03	63.34	117.37	4.000	Yes	No	2.00
4853	48.53	70.56	57.85	2.44	0.46	0.82	54.46	63.33	117.79	4.000	Yes	No	2.00
4854	48.54	70.90	57.62	2.43	0.46	0.82	54.68	63.32	117.99	0.167	No	No	0.18
4855	48.55	71.12	57.57	2.43	0.46	0.82	54.83	63.34	118.16	0.167	No	No	0.18
4856	48.56	71.34	57.57	2.43	0.46	0.82	55.00	63.39	118.39	0.168	No	No	0.18
4857	48.57	71.58	57.56	2.43	0.46	0.82	55.20	63.44	118.64	0.168	No	No	0.18
4858	48.58	71.83	57.56	2.43	0.46	0.82	55.40	63.50	118.90	0.169	No	No	0.18
4859	48.59	72.08	57.56	2.43	0.46	0.82	55.60	63.55	119.15	0.170	No	No	0.18
4860	48.60	72.31	57.56	2.43	0.46	0.82	55.79	63.60	119.39	0.170	No	No	0.18
4861	48.61	72.51	57.56	2.43	0.46	0.82	55.95	63.65	119.60	0.171	No	No	0.18
4862	48.62	72.55	57.78	2.43	0.46	0.82	56.08	63.75	119.84	4.000	Yes	No	2.00
4863	48.63	72.40	58.27	2.44	0.46	0.82	55.88	63.86	119.74	4.000	Yes	No	2.00
4864	48.64	72.07	59.08	2.45	0.46	0.82	55.60	64.03	119.63	4.000	Yes	No	2.00
4865	48.65	71.68	60.01	2.46	0.46	0.82	55.28	64.22	119.50	4.000	Yes	No	2.00
4866	48.66	71.26	60.99	2.47	0.46	0.82	54.94	64.40	119.34	4.000	Yes	No	2.00
4867	48.67	70.83	61.97	2.49	0.46	0.82	54.59	64.58	119.17	4.000	Yes	No	2.00
4868	48.68	70.41	62.89	2.50	0.46	0.82	54.25	64.73	118.98	4.000	Yes	No	2.00
4869	48.69	70.03	63.72	2.51	0.46	0.82	53.93	64.86	118.79	4.000	Yes	No	2.00
4870	48.70	69.69	64.46	2.52	0.46	0.82	53.66	64.97	118.64	4.000	Yes	No	2.00
4871	48.71	69.36	65.26	2.53	0.46	0.82	53.44	65.10	118.54	4.000	Yes	No	2.00
4872	48.72	68.97	66.22	2.54	0.46	0.81	53.12	65.25	118.37	4.000	Yes	No	2.00
4873	48.73	68.51	67.42	2.56	0.46	0.81	52.74	65.41	118.16	4.000	Yes	No	2.00
4874	48.74	67.98	68.72	2.57	0.46	0.81	52.31	65.58	117.89	4.000	Yes	No	2.00
4875	48.75	67.43	70.05	2.59	0.46	0.81	51.86	65.73	117.59	4.000	Yes	No	2.00
4876	48.76	66.87	71.35	2.60	0.46	0.81	51.40	0.00	51.40	4.000	Yes	Yes	2.00
4877	48.77	66.34	72.55	2.62	0.46	0.81	50.97	0.00	50.97	4.000	Yes	Yes	2.00
4878	48.78	65.87	73.60	2.63	0.46	0.81	50.58	0.00	50.58	4.000	Yes	Yes	2.00
4879	48.79	65.46	74.46	2.64	0.46	0.81	50.25	0.00	50.25	4.000	Yes	Yes	2.00
4880	48.80	65.06	75.24	2.65	0.46	0.81	49.97	0.00	49.97	4.000	Yes	Yes	2.00
4881	48.81	64.62	76.04	2.66	0.47	0.81	49.61	0.00	49.61	4.000	Yes	Yes	2.00
4882	48.82	64.11	76.95	2.67	0.47	0.81	49.19	0.00	49.19	4.000	Yes	Yes	2.00
4883	48.83	63.55	77.92	2.69	0.47	0.81	48.73	0.00	48.73	4.000	Yes	Yes	2.00
4884	48.84	62.97	78.92	2.70	0.47	0.81	48.25	0.00	48.25	4.000	Yes	Yes	2.00
4885	48.85	62.40	79.89	2.71	0.47	0.81	47.78	0.00	47.78	4.000	Yes	Yes	2.00
4886	48.86	61.86	80.78	2.72	0.47	0.81	47.34	0.00	47.34	4.000	Yes	Yes	2.00
4887	48.87	61.39	81.55	2.73	0.47	0.81	46.95	0.00	46.95	4.000	Yes	Yes	2.00
4888	48.88	61.10	82.05	2.74	0.47	0.81	46.64	0.00	46.64	4.000	Yes	Yes	2.00
4889	48.89	60.97	82.33	2.74	0.47	0.81	46.63	0.00	46.63	4.000	Yes	Yes	2.00
4890	48.90	60.97	82.43	2.74	0.47	0.81	46.62	0.00	46.62	4.000	No	Yes	2.00
4891	48.91	60.97	82.55	2.74	0.47	0.81	46.62	0.00	46.62	4.000	No	Yes	2.00
4892	48.92	60.97	82.68	2.75	0.47	0.81	46.61	0.00	46.61	4.000	No	Yes	2.00
4893	48.93	60.97	82.80	2.75	0.47	0.81	46.61	0.00	46.61	4.000	No	Yes	2.00
4894	48.94	60.97	82.93	2.75	0.47	0.81	46.61	0.00	46.61	4.000	No	Yes	2.00
4895	48.95	60.97	83.04	2.75	0.47	0.81	46.60	0.00	46.60	4.000	No	Yes	2.00
4896	48.96	61.06	83.07	2.75	0.47	0.81	46.60	0.00	46.60	4.000	Yes	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4897	48.97	61.50	82.80	2.75	0.47	0.81	46.81	0.00	46.81	4.000	Yes	Yes	2.00
4898	48.98	62.38	82.18	2.74	0.47	0.81	47.66	0.00	47.66	4.000	Yes	Yes	2.00
4899	48.99	63.66	81.28	2.73	0.47	0.81	48.71	0.00	48.71	4.000	Yes	Yes	2.00
4900	49.00	65.09	80.27	2.72	0.46	0.81	49.88	0.00	49.88	4.000	Yes	Yes	2.00
4901	49.01	66.60	79.22	2.70	0.46	0.81	51.12	0.00	51.12	4.000	Yes	Yes	2.00
4902	49.02	68.12	78.18	2.69	0.46	0.81	52.37	0.00	52.37	4.000	Yes	Yes	2.00
4903	49.03	69.55	77.19	2.68	0.45	0.81	53.55	0.00	53.55	4.000	Yes	Yes	2.00
4904	49.04	70.84	76.32	2.67	0.45	0.82	54.61	0.00	54.61	4.000	Yes	Yes	2.00
4905	49.05	72.07	75.50	2.66	0.45	0.82	55.49	0.00	55.49	4.000	Yes	Yes	2.00
4906	49.06	73.50	74.57	2.64	0.45	0.82	56.54	0.00	56.54	4.000	Yes	Yes	2.00
4907	49.07	75.30	73.42	2.63	0.44	0.82	58.08	0.00	58.08	4.000	Yes	Yes	2.00
4908	49.08	77.48	72.03	2.61	0.44	0.82	59.90	0.00	59.90	4.000	Yes	Yes	2.00
4909	49.09	79.88	70.53	2.59	0.44	0.82	61.90	68.76	130.66	4.000	Yes	No	2.00
4910	49.10	82.36	68.98	2.57	0.43	0.82	63.97	69.02	132.99	4.000	Yes	No	2.00
4911	49.11	84.80	67.46	2.56	0.43	0.82	66.01	69.26	135.27	4.000	Yes	No	2.00
4912	49.12	87.08	66.05	2.54	0.43	0.82	67.92	69.46	137.38	4.000	Yes	No	2.00
4913	49.13	89.06	64.82	2.52	0.42	0.83	69.60	69.62	139.22	4.000	Yes	No	2.00
4914	49.14	90.94	63.72	2.51	0.42	0.83	70.93	69.70	140.63	4.000	Yes	No	2.00
4915	49.15	92.99	62.59	2.49	0.42	0.83	72.59	69.85	142.44	4.000	Yes	No	2.00
4916	49.16	95.46	61.30	2.48	0.41	0.83	74.69	70.06	144.75	4.000	Yes	No	2.00
4917	49.17	98.30	59.83	2.46	0.41	0.83	77.10	70.28	147.38	4.000	Yes	No	2.00
4918	49.18	101.35	58.25	2.44	0.40	0.83	79.70	70.47	150.17	4.000	Yes	No	2.00
4919	49.19	104.46	56.66	2.42	0.40	0.83	82.34	70.63	152.98	4.000	Yes	No	2.00
4920	49.20	107.46	55.11	2.40	0.39	0.84	84.91	70.74	155.65	4.000	Yes	No	2.00
4921	49.21	110.20	53.70	2.38	0.39	0.84	87.26	70.80	158.07	4.000	Yes	No	2.00
4922	49.22	112.54	52.51	2.37	0.39	0.84	89.27	70.83	160.09	4.000	Yes	No	2.00
4923	49.23	114.65	51.51	2.36	0.39	0.84	90.82	70.79	161.61	4.000	Yes	No	2.00
4924	49.24	116.81	50.57	2.34	0.38	0.84	92.59	70.81	163.40	4.000	Yes	No	2.00
4925	49.25	119.31	49.54	2.33	0.38	0.84	94.75	70.87	165.62	4.000	Yes	No	2.00
4926	49.26	122.10	48.39	2.32	0.38	0.84	97.17	70.89	168.06	4.000	Yes	No	2.00
4927	49.27	125.05	47.18	2.30	0.37	0.84	99.71	70.88	170.59	4.000	Yes	No	2.00
4928	49.28	127.99	45.97	2.29	0.37	0.85	102.31	70.83	173.14	4.000	Yes	No	2.00
4929	49.29	130.79	44.83	2.27	0.36	0.85	104.74	70.72	175.46	4.000	Yes	No	2.00
4930	49.30	133.29	43.81	2.26	0.36	0.85	106.91	70.59	177.50	4.000	Yes	No	2.00
4931	49.31	135.27	43.03	2.25	0.36	0.85	108.71	70.49	179.20	4.000	Yes	No	2.00
4932	49.32	136.86	42.47	2.24	0.36	0.85	109.82	70.36	180.18	4.000	Yes	No	2.00
4933	49.33	138.28	42.05	2.24	0.36	0.85	110.98	70.33	181.32	4.000	Yes	No	2.00
4934	49.34	139.85	41.61	2.23	0.35	0.85	112.36	70.34	182.70	4.000	Yes	No	2.00
4935	49.35	141.56	41.14	2.23	0.35	0.85	113.87	70.33	184.20	4.000	Yes	No	2.00
4936	49.36	143.34	40.65	2.22	0.35	0.85	115.43	70.32	185.75	4.000	Yes	No	2.00
4937	49.37	145.09	40.17	2.21	0.35	0.85	116.96	70.29	187.26	4.000	Yes	No	2.00
4938	49.38	146.71	39.73	2.21	0.35	0.85	118.40	70.26	188.66	4.000	Yes	No	2.00
4939	49.39	148.13	39.35	2.20	0.34	0.85	119.65	70.23	189.87	4.000	Yes	No	2.00
4940	49.40	149.24	39.10	2.20	0.34	0.85	120.64	70.24	190.88	4.000	Yes	No	2.00
4941	49.41	150.17	38.96	2.20	0.34	0.86	121.27	70.26	191.53	1.212	No	No	1.29
4942	49.42	151.06	38.89	2.20	0.34	0.86	122.07	70.39	192.47	1.269	No	No	1.35
4943	49.43	152.09	38.82	2.20	0.34	0.86	122.99	70.54	193.54	1.339	No	No	1.42
4944	49.44	153.19	38.74	2.20	0.34	0.86	123.98	70.71	194.68	1.420	No	No	1.50

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4945	49.45	154.31	38.66	2.20	0.34	0.86	124.98	70.87	195.85	1.509	No	No	1.60
4946	49.46	155.40	38.59	2.19	0.33	0.86	125.95	71.03	196.98	1.603	No	No	1.69
4947	49.47	156.38	38.52	2.19	0.33	0.86	126.84	71.18	198.02	1.695	No	No	1.79
4948	49.48	157.18	38.44	2.19	0.33	0.86	127.59	71.28	198.87	1.776	No	No	1.87
4949	49.49	157.71	38.26	2.19	0.33	0.86	128.03	71.21	199.24	1.812	No	No	1.91
4950	49.50	158.05	37.95	2.19	0.33	0.86	128.20	70.95	199.15	1.804	No	No	1.90
4951	49.51	158.32	37.53	2.18	0.33	0.86	128.40	70.58	198.97	1.786	No	No	1.88
4952	49.52	158.62	37.04	2.18	0.33	0.86	128.62	70.14	198.76	1.765	No	No	1.86
4953	49.53	158.94	36.53	2.17	0.33	0.86	128.86	69.65	198.51	1.741	No	No	1.83
4954	49.54	159.25	36.00	2.16	0.33	0.86	129.09	69.15	198.23	1.715	No	No	1.81
4955	49.55	159.55	35.50	2.16	0.33	0.86	129.31	68.64	197.95	1.688	No	No	1.78
4956	49.56	159.82	35.05	2.15	0.33	0.86	129.50	68.17	197.67	1.663	No	No	1.75
4957	49.57	159.94	34.66	2.15	0.33	0.86	129.65	67.76	197.41	1.640	No	No	1.73
4958	49.58	159.84	34.30	2.14	0.33	0.86	129.47	67.29	196.76	1.584	No	No	1.67
4959	49.59	159.52	33.90	2.14	0.34	0.86	129.09	66.74	195.82	1.507	No	No	1.59
4960	49.60	159.10	33.44	2.13	0.34	0.86	128.64	66.07	194.71	1.422	No	No	1.50
4961	49.61	158.63	32.92	2.12	0.34	0.85	128.14	65.31	193.46	1.334	No	No	1.41
4962	49.62	158.15	32.38	2.12	0.34	0.85	127.63	64.50	192.13	1.248	No	No	1.33
4963	49.63	157.68	31.83	2.11	0.34	0.85	127.13	63.66	190.79	1.169	No	No	1.24
4964	49.64	157.24	31.31	2.10	0.34	0.85	126.66	62.85	189.50	1.099	No	No	1.17
4965	49.65	156.86	30.85	2.10	0.35	0.85	126.24	62.12	188.36	1.042	No	No	1.11
4966	49.66	156.50	30.60	2.10	0.35	0.85	125.92	61.69	187.61	1.007	No	No	1.08
4967	49.67	156.12	30.55	2.09	0.35	0.85	125.58	61.55	187.12	0.985	No	No	1.05
4968	49.68	155.67	30.66	2.10	0.35	0.85	125.17	61.63	186.80	0.971	No	No	1.04
4969	49.69	155.16	30.80	2.10	0.35	0.85	124.71	61.72	186.44	0.955	No	No	1.02
4970	49.70	154.60	30.94	2.10	0.35	0.85	124.22	61.82	186.04	0.938	No	No	1.00
4971	49.71	154.04	31.08	2.10	0.35	0.85	123.72	61.92	185.64	0.922	No	No	0.99
4972	49.72	153.50	31.22	2.10	0.35	0.85	123.24	62.01	185.25	0.906	No	No	0.97
4973	49.73	153.01	31.35	2.10	0.35	0.85	122.80	62.09	184.90	0.892	No	No	0.95
4974	49.74	152.60	31.45	2.11	0.35	0.85	122.43	62.16	184.59	0.880	No	No	0.94
4975	49.75	152.23	31.54	2.11	0.35	0.85	122.14	62.21	184.36	0.871	No	No	0.93
4976	49.76	151.87	31.61	2.11	0.35	0.85	121.84	62.25	184.08	0.861	No	No	0.92
4977	49.77	151.47	31.69	2.11	0.35	0.85	121.47	62.27	183.74	0.848	No	No	0.91
4978	49.78	151.01	31.77	2.11	0.35	0.85	121.06	62.30	183.35	0.835	No	No	0.89
4979	49.79	150.53	31.86	2.11	0.35	0.85	120.63	62.32	182.95	0.820	No	No	0.88
4980	49.80	150.06	31.95	2.11	0.35	0.85	120.20	62.35	182.55	0.807	No	No	0.86
4981	49.81	149.60	32.03	2.11	0.35	0.85	119.79	62.37	182.16	0.794	No	No	0.85
4982	49.82	149.20	32.11	2.11	0.35	0.85	119.43	62.39	181.82	0.783	No	No	0.84
4983	49.83	148.77	32.24	2.12	0.35	0.85	119.13	62.50	181.63	0.777	No	No	0.83
4984	49.84	148.21	32.46	2.12	0.36	0.85	118.67	62.69	181.36	0.768	No	No	0.82
4985	49.85	147.45	32.82	2.12	0.36	0.85	117.99	62.99	180.98	0.756	No	No	0.81
4986	49.86	146.53	33.26	2.13	0.36	0.85	117.19	63.35	180.54	0.743	No	No	0.80
4987	49.87	145.52	33.74	2.13	0.36	0.85	116.33	63.73	180.06	0.728	No	No	0.78
4988	49.88	144.48	34.23	2.14	0.36	0.85	115.43	64.10	179.53	0.713	No	No	0.76
4989	49.89	143.46	34.71	2.15	0.36	0.85	114.55	64.44	178.99	0.698	No	No	0.75
4990	49.90	142.51	35.15	2.15	0.36	0.84	113.73	64.74	178.47	0.684	No	No	0.73
4991	49.91	141.69	35.53	2.16	0.36	0.84	113.02	64.99	178.01	0.672	No	No	0.72
4992	49.92	141.02	35.84	2.16	0.36	0.84	112.46	65.18	177.63	0.663	No	No	0.71

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
4993	49.93	140.40	36.09	2.16	0.36	0.84	112.01	65.34	177.35	0.655	No	No	0.70
4994	49.94	139.76	36.35	2.17	0.36	0.84	111.44	65.47	176.91	0.644	No	No	0.69
4995	49.95	139.02	36.64	2.17	0.36	0.84	110.80	65.61	176.40	0.632	No	No	0.68
4996	49.96	138.23	36.95	2.17	0.36	0.84	110.11	65.75	175.86	0.620	No	No	0.66
4997	49.97	137.43	37.26	2.18	0.36	0.84	109.41	65.89	175.30	0.607	No	No	0.65
4998	49.98	136.66	37.56	2.18	0.36	0.84	108.74	66.02	174.76	0.595	No	No	0.64
4999	49.99	135.96	37.84	2.19	0.37	0.84	108.12	66.13	174.25	0.584	No	No	0.63
5000	50.00	135.52	38.02	2.19	0.37	0.84	107.60	66.17	173.76	0.574	No	No	0.62

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q_t :	Total cone resistance
FC:	Fines content (%)
I_c :	Soil behavior type index
m:	Stress exponent
C_N :	Overburden correction factor
q_{c1N} :	Normalized and adjusted cone resistance
Δq_{c1N} :	Cone resistance correction factor due to fines
$q_{c1N,cs}$:	Normalized and adjusted cone resistance
CRR _{7.5} :	Cyclic resistance ratio for $M_w=7.5$
FS:	Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
0.01	2.00	0.00	0.00	0.01	0.00	0.02	2.00	0.00	0.00	0.01	0.00
0.03	2.00	0.00	0.00	0.01	0.00	0.04	2.00	0.00	0.00	0.01	0.00
0.05	2.00	0.00	0.00	0.01	0.00	0.06	2.00	0.00	0.00	0.01	0.00
0.07	2.00	0.00	0.00	0.01	0.00	0.08	2.00	0.00	0.00	0.01	0.00
0.09	2.00	0.00	0.00	0.01	0.00	0.10	2.00	0.00	0.00	0.01	0.00
0.11	2.00	0.00	0.00	0.01	0.00	0.12	2.00	0.00	0.00	0.01	0.00
0.13	2.00	0.00	0.00	0.01	0.00	0.14	2.00	0.00	0.00	0.01	0.00
0.15	2.00	0.00	0.00	0.01	0.00	0.16	2.00	0.00	0.00	0.01	0.00
0.17	2.00	0.00	0.00	0.01	0.00	0.18	2.00	0.00	0.00	0.01	0.00
0.19	2.00	0.00	0.00	0.01	0.00	0.20	2.00	0.00	0.00	0.01	0.00
0.21	2.00	0.00	0.00	0.01	0.00	0.22	2.00	0.00	0.00	0.01	0.00
0.23	2.00	0.00	0.00	0.01	0.00	0.24	2.00	0.00	0.00	0.01	0.00
0.25	2.00	0.00	0.00	0.01	0.00	0.26	2.00	0.00	0.00	0.01	0.00
0.27	2.00	0.00	0.00	0.01	0.00	0.28	2.00	0.00	0.00	0.01	0.00
0.29	2.00	0.00	0.00	0.01	0.00	0.30	2.00	0.00	0.00	0.01	0.00
0.31	2.00	0.00	0.00	0.01	0.00	0.32	2.00	0.00	0.00	0.01	0.00
0.33	2.00	0.00	0.00	0.01	0.00	0.34	2.00	0.00	0.00	0.01	0.00
0.35	2.00	0.00	0.00	0.01	0.00	0.36	2.00	0.00	0.00	0.01	0.00
0.37	2.00	0.00	0.00	0.01	0.00	0.38	2.00	0.00	0.00	0.01	0.00
0.39	2.00	0.00	0.00	0.01	0.00	0.40	2.00	0.00	0.00	0.01	0.00
0.41	2.00	0.00	0.00	0.01	0.00	0.42	2.00	0.00	0.00	0.01	0.00
0.43	2.00	0.00	0.00	0.01	0.00	0.44	2.00	0.00	0.00	0.01	0.00
0.45	2.00	0.00	0.00	0.01	0.00	0.46	2.00	0.00	0.00	0.01	0.00
0.47	2.00	0.00	0.00	0.01	0.00	0.48	2.00	0.00	0.00	0.01	0.00
0.49	2.00	0.00	0.00	0.01	0.00	0.50	2.00	0.00	0.00	0.01	0.00
0.51	2.00	0.00	0.00	0.01	0.00	0.52	2.00	0.00	0.00	0.01	0.00
0.53	2.00	0.00	0.00	0.01	0.00	0.54	2.00	0.00	0.00	0.01	0.00
0.55	2.00	0.00	0.00	0.01	0.00	0.56	2.00	0.00	0.00	0.01	0.00
0.57	2.00	0.00	0.00	0.01	0.00	0.58	2.00	0.00	0.00	0.01	0.00
0.59	2.00	0.00	0.00	0.01	0.00	0.60	2.00	0.00	0.00	0.01	0.00
0.61	2.00	0.00	0.00	0.01	0.00	0.62	2.00	0.00	0.00	0.01	0.00
0.63	2.00	0.00	0.00	0.01	0.00	0.64	2.00	0.00	0.00	0.01	0.00
0.65	2.00	0.00	0.00	0.01	0.00	0.66	2.00	0.00	0.00	0.01	0.00
0.67	2.00	0.00	0.00	0.01	0.00	0.68	2.00	0.00	0.00	0.01	0.00
0.69	2.00	0.00	0.00	0.01	0.00	0.70	2.00	0.00	0.00	0.01	0.00
0.71	2.00	0.00	0.00	0.01	0.00	0.72	2.00	0.00	0.00	0.01	0.00
0.73	2.00	0.00	0.00	0.01	0.00	0.74	2.00	0.00	0.00	0.01	0.00
0.75	2.00	0.00	0.00	0.01	0.00	0.76	2.00	0.00	0.00	0.01	0.00
0.77	2.00	0.00	0.00	0.01	0.00	0.78	2.00	0.00	0.00	0.01	0.00
0.79	2.00	0.00	0.00	0.01	0.00	0.80	2.00	0.00	0.00	0.01	0.00
0.81	2.00	0.00	0.00	0.01	0.00	0.82	2.00	0.00	0.00	0.01	0.00
0.83	2.00	0.00	0.00	0.01	0.00	0.84	2.00	0.00	0.00	0.01	0.00
0.85	2.00	0.00	0.00	0.01	0.00	0.86	2.00	0.00	0.00	0.01	0.00
0.87	2.00	0.00	0.00	0.01	0.00	0.88	2.00	0.00	0.00	0.01	0.00
0.89	2.00	0.00	0.00	0.01	0.00	0.90	2.00	0.00	0.00	0.01	0.00
0.91	2.00	0.00	0.00	0.01	0.00	0.92	2.00	0.00	0.00	0.01	0.00
0.93	2.00	0.00	0.00	0.01	0.00	0.94	2.00	0.00	0.00	0.01	0.00
0.95	2.00	0.00	0.00	0.01	0.00	0.96	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
0.97	2.00	0.00	0.00	0.01	0.00	0.98	2.00	0.00	0.00	0.01	0.00
0.99	2.00	0.00	0.00	0.01	0.00	1.00	2.00	0.00	0.00	0.01	0.00
1.01	2.00	0.00	0.00	0.01	0.00	1.02	2.00	0.00	0.00	0.01	0.00
1.03	2.00	0.00	0.00	0.01	0.00	1.04	2.00	0.00	0.00	0.01	0.00
1.05	2.00	0.00	0.00	0.01	0.00	1.06	2.00	0.00	0.00	0.01	0.00
1.07	2.00	0.00	0.00	0.01	0.00	1.08	2.00	0.00	0.00	0.01	0.00
1.09	2.00	0.00	0.00	0.01	0.00	1.10	2.00	0.00	0.00	0.01	0.00
1.11	2.00	0.00	0.00	0.01	0.00	1.12	2.00	0.00	0.00	0.01	0.00
1.13	2.00	0.00	0.00	0.01	0.00	1.14	2.00	0.00	0.00	0.01	0.00
1.15	2.00	0.00	0.00	0.01	0.00	1.16	2.00	0.00	0.00	0.01	0.00
1.17	2.00	0.00	0.00	0.01	0.00	1.18	2.00	0.00	0.00	0.01	0.00
1.19	2.00	0.00	0.00	0.01	0.00	1.20	2.00	0.00	0.00	0.01	0.00
1.21	2.00	0.00	0.00	0.01	0.00	1.22	2.00	0.00	0.00	0.01	0.00
1.23	2.00	0.00	0.00	0.01	0.00	1.24	2.00	0.00	0.00	0.01	0.00
1.25	2.00	0.00	0.00	0.01	0.00	1.26	2.00	0.00	0.00	0.01	0.00
1.27	2.00	0.00	0.00	0.01	0.00	1.28	2.00	0.00	0.00	0.01	0.00
1.29	2.00	0.00	0.00	0.01	0.00	1.30	2.00	0.00	0.00	0.01	0.00
1.31	2.00	0.00	0.00	0.01	0.00	1.32	2.00	0.00	0.00	0.01	0.00
1.33	2.00	0.00	0.00	0.01	0.00	1.34	2.00	0.00	0.00	0.01	0.00
1.35	2.00	0.00	0.00	0.01	0.00	1.36	2.00	0.00	0.00	0.01	0.00
1.37	2.00	0.00	0.00	0.01	0.00	1.38	2.00	0.00	0.00	0.01	0.00
1.39	2.00	0.00	0.00	0.01	0.00	1.40	2.00	0.00	0.00	0.01	0.00
1.41	2.00	0.00	0.00	0.01	0.00	1.42	2.00	0.00	0.00	0.01	0.00
1.43	2.00	0.00	0.00	0.01	0.00	1.44	2.00	0.00	0.00	0.01	0.00
1.45	2.00	0.00	0.00	0.01	0.00	1.46	2.00	0.00	0.00	0.01	0.00
1.47	2.00	0.00	0.00	0.01	0.00	1.48	2.00	0.00	0.00	0.01	0.00
1.49	2.00	0.00	0.00	0.01	0.00	1.50	2.00	0.00	0.00	0.01	0.00
1.51	2.00	0.00	0.00	0.01	0.00	1.52	2.00	0.00	0.00	0.01	0.00
1.53	2.00	0.00	0.00	0.01	0.00	1.54	2.00	0.00	0.00	0.01	0.00
1.55	2.00	0.00	0.00	0.01	0.00	1.56	2.00	0.00	0.00	0.01	0.00
1.57	2.00	0.00	0.00	0.01	0.00	1.58	2.00	0.00	0.00	0.01	0.00
1.59	2.00	0.00	0.00	0.01	0.00	1.60	2.00	0.00	0.00	0.01	0.00
1.61	2.00	0.00	0.00	0.01	0.00	1.62	2.00	0.00	0.00	0.01	0.00
1.63	2.00	0.00	0.00	0.01	0.00	1.64	2.00	0.00	0.00	0.01	0.00
1.65	2.00	0.00	0.00	0.01	0.00	1.66	2.00	0.00	0.00	0.01	0.00
1.67	2.00	0.00	0.00	0.01	0.00	1.68	2.00	0.00	0.00	0.01	0.00
1.69	2.00	0.00	0.00	0.01	0.00	1.70	2.00	0.00	0.00	0.01	0.00
1.71	2.00	0.00	0.00	0.01	0.00	1.72	2.00	0.00	0.00	0.01	0.00
1.73	2.00	0.00	0.00	0.01	0.00	1.74	2.00	0.00	0.00	0.01	0.00
1.75	2.00	0.00	0.00	0.01	0.00	1.76	2.00	0.00	0.00	0.01	0.00
1.77	2.00	0.00	0.00	0.01	0.00	1.78	2.00	0.00	0.00	0.01	0.00
1.79	2.00	0.00	0.00	0.01	0.00	1.80	2.00	0.00	0.00	0.01	0.00
1.81	2.00	0.00	0.00	0.01	0.00	1.82	2.00	0.00	0.00	0.01	0.00
1.83	2.00	0.00	0.00	0.01	0.00	1.84	2.00	0.00	0.00	0.01	0.00
1.85	2.00	0.00	0.00	0.01	0.00	1.86	2.00	0.00	0.00	0.01	0.00
1.87	2.00	0.00	0.00	0.01	0.00	1.88	2.00	0.00	0.00	0.01	0.00
1.89	2.00	0.00	0.00	0.01	0.00	1.90	2.00	0.00	0.00	0.01	0.00
1.91	2.00	0.00	0.00	0.01	0.00	1.92	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
1.93	2.00	0.00	0.00	0.01	0.00	1.94	2.00	0.00	0.00	0.01	0.00
1.95	2.00	0.00	0.00	0.01	0.00	1.96	2.00	0.00	0.00	0.01	0.00
1.97	2.00	0.00	0.00	0.01	0.00	1.98	2.00	0.00	0.00	0.01	0.00
1.99	2.00	0.00	0.00	0.01	0.00	2.00	2.00	0.00	0.00	0.01	0.00
2.01	2.00	0.00	0.00	0.01	0.00	2.02	2.00	0.00	0.00	0.01	0.00
2.03	2.00	0.00	0.00	0.01	0.00	2.04	2.00	0.00	0.00	0.01	0.00
2.05	2.00	0.00	0.00	0.01	0.00	2.06	2.00	0.00	0.00	0.01	0.00
2.07	2.00	0.00	0.00	0.01	0.00	2.08	2.00	0.00	0.00	0.01	0.00
2.09	2.00	0.00	0.00	0.01	0.00	2.10	2.00	0.00	0.00	0.01	0.00
2.11	2.00	0.00	0.00	0.01	0.00	2.12	2.00	0.00	0.00	0.01	0.00
2.13	2.00	0.00	0.00	0.01	0.00	2.14	2.00	0.00	0.00	0.01	0.00
2.15	2.00	0.00	0.00	0.01	0.00	2.16	2.00	0.00	0.00	0.01	0.00
2.17	2.00	0.00	0.00	0.01	0.00	2.18	2.00	0.00	0.00	0.01	0.00
2.19	2.00	0.00	0.00	0.01	0.00	2.20	2.00	0.00	0.00	0.01	0.00
2.21	2.00	0.00	0.00	0.01	0.00	2.22	2.00	0.00	0.00	0.01	0.00
2.23	2.00	0.00	0.00	0.01	0.00	2.24	2.00	0.00	0.00	0.01	0.00
2.25	2.00	0.00	0.00	0.01	0.00	2.26	2.00	0.00	0.00	0.01	0.00
2.27	2.00	0.00	0.00	0.01	0.00	2.28	2.00	0.00	0.00	0.01	0.00
2.29	2.00	0.00	0.00	0.01	0.00	2.30	2.00	0.00	0.00	0.01	0.00
2.31	2.00	0.00	0.00	0.01	0.00	2.32	2.00	0.00	0.00	0.01	0.00
2.33	2.00	0.00	0.00	0.01	0.00	2.34	2.00	0.00	0.00	0.01	0.00
2.35	2.00	0.00	0.00	0.01	0.00	2.36	2.00	0.00	0.00	0.01	0.00
2.37	2.00	0.00	0.00	0.01	0.00	2.38	2.00	0.00	0.00	0.01	0.00
2.39	2.00	0.00	0.00	0.01	0.00	2.40	2.00	0.00	0.00	0.01	0.00
2.41	2.00	0.00	0.00	0.01	0.00	2.42	2.00	0.00	0.00	0.01	0.00
2.43	2.00	0.00	0.00	0.01	0.00	2.44	2.00	0.00	0.00	0.01	0.00
2.45	2.00	0.00	0.00	0.01	0.00	2.46	2.00	0.00	0.00	0.01	0.00
2.47	2.00	0.00	0.00	0.01	0.00	2.48	2.00	0.00	0.00	0.01	0.00
2.49	2.00	0.00	0.00	0.01	0.00	2.50	2.00	0.00	0.00	0.01	0.00
2.51	2.00	0.00	0.00	0.01	0.00	2.52	2.00	0.00	0.00	0.01	0.00
2.53	2.00	0.00	0.00	0.01	0.00	2.54	2.00	0.00	0.00	0.01	0.00
2.55	2.00	0.00	0.00	0.01	0.00	2.56	2.00	0.00	0.00	0.01	0.00
2.57	2.00	0.00	0.00	0.01	0.00	2.58	2.00	0.00	0.00	0.01	0.00
2.59	2.00	0.00	0.00	0.01	0.00	2.60	2.00	0.00	0.00	0.01	0.00
2.61	2.00	0.00	0.00	0.01	0.00	2.62	2.00	0.00	0.00	0.01	0.00
2.63	2.00	0.00	0.00	0.01	0.00	2.64	2.00	0.00	0.00	0.01	0.00
2.65	2.00	0.00	0.00	0.01	0.00	2.66	2.00	0.00	0.00	0.01	0.00
2.67	2.00	0.00	0.00	0.01	0.00	2.68	2.00	0.00	0.00	0.01	0.00
2.69	2.00	0.00	0.00	0.01	0.00	2.70	2.00	0.00	0.00	0.01	0.00
2.71	2.00	0.00	0.00	0.01	0.00	2.72	2.00	0.00	0.00	0.01	0.00
2.73	2.00	0.00	0.00	0.01	0.00	2.74	2.00	0.00	0.00	0.01	0.00
2.75	2.00	0.00	0.00	0.01	0.00	2.76	2.00	0.00	0.00	0.01	0.00
2.77	2.00	0.00	0.00	0.01	0.00	2.78	2.00	0.00	0.00	0.01	0.00
2.79	2.00	0.00	0.00	0.01	0.00	2.80	2.00	0.00	0.00	0.01	0.00
2.81	2.00	0.00	0.00	0.01	0.00	2.82	2.00	0.00	0.00	0.01	0.00
2.83	2.00	0.00	0.00	0.01	0.00	2.84	2.00	0.00	0.00	0.01	0.00
2.85	2.00	0.00	0.00	0.01	0.00	2.86	2.00	0.00	0.00	0.01	0.00
2.87	2.00	0.00	0.00	0.01	0.00	2.88	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
2.89	2.00	0.00	0.00	0.01	0.00	2.90	2.00	0.00	0.00	0.01	0.00
2.91	2.00	0.00	0.00	0.01	0.00	2.92	2.00	0.00	0.00	0.01	0.00
2.93	2.00	0.00	0.00	0.01	0.00	2.94	2.00	0.00	0.00	0.01	0.00
2.95	2.00	0.00	0.00	0.01	0.00	2.96	2.00	0.00	0.00	0.01	0.00
2.97	2.00	0.00	0.00	0.01	0.00	2.98	2.00	0.00	0.00	0.01	0.00
2.99	2.00	0.00	0.00	0.01	0.00	3.00	2.00	0.00	0.00	0.01	0.00
3.01	2.00	0.00	0.00	0.01	0.00	3.02	2.00	0.00	0.00	0.01	0.00
3.03	2.00	0.00	0.00	0.01	0.00	3.04	2.00	0.00	0.00	0.01	0.00
3.05	2.00	0.00	0.00	0.01	0.00	3.06	2.00	0.00	0.00	0.01	0.00
3.07	2.00	0.00	0.00	0.01	0.00	3.08	2.00	0.00	0.00	0.01	0.00
3.09	2.00	0.00	0.00	0.01	0.00	3.10	2.00	0.00	0.00	0.01	0.00
3.11	2.00	0.00	0.00	0.01	0.00	3.12	2.00	0.00	0.00	0.01	0.00
3.13	2.00	0.00	0.00	0.01	0.00	3.14	2.00	0.00	0.00	0.01	0.00
3.15	2.00	0.00	0.00	0.01	0.00	3.16	2.00	0.00	0.00	0.01	0.00
3.17	2.00	0.00	0.00	0.01	0.00	3.18	2.00	0.00	0.00	0.01	0.00
3.19	2.00	0.00	0.00	0.01	0.00	3.20	2.00	0.00	0.00	0.01	0.00
3.21	2.00	0.00	0.00	0.01	0.00	3.22	2.00	0.00	0.00	0.01	0.00
3.23	2.00	0.00	0.00	0.01	0.00	3.24	2.00	0.00	0.00	0.01	0.00
3.25	2.00	0.00	0.00	0.01	0.00	3.26	2.00	0.00	0.00	0.01	0.00
3.27	2.00	0.00	0.00	0.01	0.00	3.28	2.00	0.00	0.00	0.01	0.00
3.29	2.00	0.00	0.00	0.01	0.00	3.30	2.00	0.00	0.00	0.01	0.00
3.31	2.00	0.00	0.00	0.01	0.00	3.32	2.00	0.00	0.00	0.01	0.00
3.33	2.00	0.00	0.00	0.01	0.00	3.34	2.00	0.00	0.00	0.01	0.00
3.35	2.00	0.00	0.00	0.01	0.00	3.36	2.00	0.00	0.00	0.01	0.00
3.37	2.00	0.00	0.00	0.01	0.00	3.38	2.00	0.00	0.00	0.01	0.00
3.39	2.00	0.00	0.00	0.01	0.00	3.40	2.00	0.00	0.00	0.01	0.00
3.41	2.00	0.00	0.00	0.01	0.00	3.42	2.00	0.00	0.00	0.01	0.00
3.43	2.00	0.00	0.00	0.01	0.00	3.44	2.00	0.00	0.00	0.01	0.00
3.45	2.00	0.00	0.00	0.01	0.00	3.46	2.00	0.00	0.00	0.01	0.00
3.47	2.00	0.00	0.00	0.01	0.00	3.48	2.00	0.00	0.00	0.01	0.00
3.49	2.00	0.00	0.00	0.01	0.00	3.50	2.00	0.00	0.00	0.01	0.00
3.51	2.00	0.00	0.00	0.01	0.00	3.52	2.00	0.00	0.00	0.01	0.00
3.53	2.00	0.00	0.00	0.01	0.00	3.54	2.00	0.00	0.00	0.01	0.00
3.55	2.00	0.00	0.00	0.01	0.00	3.56	2.00	0.00	0.00	0.01	0.00
3.57	2.00	0.00	0.00	0.01	0.00	3.58	2.00	0.00	0.00	0.01	0.00
3.59	2.00	0.00	0.00	0.01	0.00	3.60	2.00	0.00	0.00	0.01	0.00
3.61	2.00	0.00	0.00	0.01	0.00	3.62	2.00	0.00	0.00	0.01	0.00
3.63	2.00	0.00	0.00	0.01	0.00	3.64	2.00	0.00	0.00	0.01	0.00
3.65	2.00	0.00	0.00	0.01	0.00	3.66	2.00	0.00	0.00	0.01	0.00
3.67	2.00	0.00	0.00	0.01	0.00	3.68	2.00	0.00	0.00	0.01	0.00
3.69	2.00	0.00	0.00	0.01	0.00	3.70	2.00	0.00	0.00	0.01	0.00
3.71	2.00	0.00	0.00	0.01	0.00	3.72	2.00	0.00	0.00	0.01	0.00
3.73	2.00	0.00	0.00	0.01	0.00	3.74	2.00	0.00	0.00	0.01	0.00
3.75	2.00	0.00	0.00	0.01	0.00	3.76	2.00	0.00	0.00	0.01	0.00
3.77	2.00	0.00	0.00	0.01	0.00	3.78	2.00	0.00	0.00	0.01	0.00
3.79	2.00	0.00	0.00	0.01	0.00	3.80	2.00	0.00	0.00	0.01	0.00
3.81	2.00	0.00	0.00	0.01	0.00	3.82	2.00	0.00	0.00	0.01	0.00
3.83	2.00	0.00	0.00	0.01	0.00	3.84	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
3.85	2.00	0.00	0.00	0.01	0.00	3.86	2.00	0.00	0.00	0.01	0.00
3.87	2.00	0.00	0.00	0.01	0.00	3.88	2.00	0.00	0.00	0.01	0.00
3.89	2.00	0.00	0.00	0.01	0.00	3.90	2.00	0.00	0.00	0.01	0.00
3.91	2.00	0.00	0.00	0.01	0.00	3.92	2.00	0.00	0.00	0.01	0.00
3.93	2.00	0.00	0.00	0.01	0.00	3.94	2.00	0.00	0.00	0.01	0.00
3.95	2.00	0.00	0.00	0.01	0.00	3.96	2.00	0.00	0.00	0.01	0.00
3.97	2.00	0.00	0.00	0.01	0.00	3.98	2.00	0.00	0.00	0.01	0.00
3.99	2.00	0.00	0.00	0.01	0.00	4.00	2.00	0.00	0.00	0.01	0.00
4.01	2.00	0.00	0.00	0.01	0.00	4.02	2.00	0.00	0.00	0.01	0.00
4.03	2.00	0.00	0.00	0.01	0.00	4.04	2.00	0.00	0.00	0.01	0.00
4.05	2.00	0.00	0.00	0.01	0.00	4.06	2.00	0.00	0.00	0.01	0.00
4.07	2.00	0.00	0.00	0.01	0.00	4.08	2.00	0.00	0.00	0.01	0.00
4.09	2.00	0.00	0.00	0.01	0.00	4.10	2.00	0.00	0.00	0.01	0.00
4.11	2.00	0.00	0.00	0.01	0.00	4.12	2.00	0.00	0.00	0.01	0.00
4.13	2.00	0.00	0.00	0.01	0.00	4.14	2.00	0.00	0.00	0.01	0.00
4.15	2.00	0.00	0.00	0.01	0.00	4.16	2.00	0.00	0.00	0.01	0.00
4.17	2.00	0.00	0.00	0.01	0.00	4.18	2.00	0.00	0.00	0.01	0.00
4.19	2.00	0.00	0.00	0.01	0.00	4.20	2.00	0.00	0.00	0.01	0.00
4.21	2.00	0.00	0.00	0.01	0.00	4.22	2.00	0.00	0.00	0.01	0.00
4.23	2.00	0.00	0.00	0.01	0.00	4.24	2.00	0.00	0.00	0.01	0.00
4.25	2.00	0.00	0.00	0.01	0.00	4.26	2.00	0.00	0.00	0.01	0.00
4.27	2.00	0.00	0.00	0.01	0.00	4.28	2.00	0.00	0.00	0.01	0.00
4.29	2.00	0.00	0.00	0.01	0.00	4.30	2.00	0.00	0.00	0.01	0.00
4.31	2.00	0.00	0.00	0.01	0.00	4.32	2.00	0.00	0.00	0.01	0.00
4.33	2.00	0.00	0.00	0.01	0.00	4.34	2.00	0.00	0.00	0.01	0.00
4.35	2.00	0.00	0.00	0.01	0.00	4.36	2.00	0.00	0.00	0.01	0.00
4.37	2.00	0.00	0.00	0.01	0.00	4.38	2.00	0.00	0.00	0.01	0.00
4.39	2.00	0.00	0.00	0.01	0.00	4.40	2.00	0.00	0.00	0.01	0.00
4.41	2.00	0.00	0.00	0.01	0.00	4.42	2.00	0.00	0.00	0.01	0.00
4.43	2.00	0.00	0.00	0.01	0.00	4.44	2.00	0.00	0.00	0.01	0.00
4.45	2.00	0.00	0.00	0.01	0.00	4.46	2.00	0.00	0.00	0.01	0.00
4.47	2.00	0.00	0.00	0.01	0.00	4.48	2.00	0.00	0.00	0.01	0.00
4.49	2.00	0.00	0.00	0.01	0.00	4.50	2.00	0.00	0.00	0.01	0.00
4.51	2.00	0.00	0.00	0.01	0.00	4.52	2.00	0.00	0.00	0.01	0.00
4.53	2.00	0.00	0.00	0.01	0.00	4.54	2.00	0.00	0.00	0.01	0.00
4.55	2.00	0.00	0.00	0.01	0.00	4.56	2.00	0.00	0.00	0.01	0.00
4.57	2.00	0.00	0.00	0.01	0.00	4.58	2.00	0.00	0.00	0.01	0.00
4.59	2.00	0.00	0.00	0.01	0.00	4.60	2.00	0.00	0.00	0.01	0.00
4.61	2.00	0.00	0.00	0.01	0.00	4.62	2.00	0.00	0.00	0.01	0.00
4.63	2.00	0.00	0.00	0.01	0.00	4.64	2.00	0.00	0.00	0.01	0.00
4.65	2.00	0.00	0.00	0.01	0.00	4.66	2.00	0.00	0.00	0.01	0.00
4.67	2.00	0.00	0.00	0.01	0.00	4.68	2.00	0.00	0.00	0.01	0.00
4.69	2.00	0.00	0.00	0.01	0.00	4.70	2.00	0.00	0.00	0.01	0.00
4.71	2.00	0.00	0.00	0.01	0.00	4.72	2.00	0.00	0.00	0.01	0.00
4.73	2.00	0.00	0.00	0.01	0.00	4.74	2.00	0.00	0.00	0.01	0.00
4.75	2.00	0.00	0.00	0.01	0.00	4.76	2.00	0.00	0.00	0.01	0.00
4.77	2.00	0.00	0.00	0.01	0.00	4.78	2.00	0.00	0.00	0.01	0.00
4.79	2.00	0.00	0.00	0.01	0.00	4.80	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
4.81	2.00	0.00	0.00	0.01	0.00	4.82	2.00	0.00	0.00	0.01	0.00
4.83	2.00	0.00	0.00	0.01	0.00	4.84	2.00	0.00	0.00	0.01	0.00
4.85	2.00	0.00	0.00	0.01	0.00	4.86	2.00	0.00	0.00	0.01	0.00
4.87	2.00	0.00	0.00	0.01	0.00	4.88	2.00	0.00	0.00	0.01	0.00
4.89	2.00	0.00	0.00	0.01	0.00	4.90	2.00	0.00	0.00	0.01	0.00
4.91	2.00	0.00	0.00	0.01	0.00	4.92	2.00	0.00	0.00	0.01	0.00
4.93	2.00	0.00	0.00	0.01	0.00	4.94	2.00	0.00	0.00	0.01	0.00
4.95	2.00	0.00	0.00	0.01	0.00	4.96	2.00	0.00	0.00	0.01	0.00
4.97	2.00	0.00	0.00	0.01	0.00	4.98	2.00	0.00	0.00	0.01	0.00
4.99	2.00	0.00	0.00	0.01	0.00	5.00	2.00	0.00	0.00	0.01	0.00
5.01	2.00	0.00	0.00	0.01	0.00	5.02	2.00	0.00	0.00	0.01	0.00
5.03	2.00	0.00	0.00	0.01	0.00	5.04	2.00	0.00	0.00	0.01	0.00
5.05	2.00	0.00	0.00	0.01	0.00	5.06	2.00	0.00	0.00	0.01	0.00
5.07	2.00	0.00	0.00	0.01	0.00	5.08	2.00	0.00	0.00	0.01	0.00
5.09	2.00	0.00	0.00	0.01	0.00	5.10	2.00	0.00	0.00	0.01	0.00
5.11	2.00	0.00	0.00	0.01	0.00	5.12	2.00	0.00	0.00	0.01	0.00
5.13	2.00	0.00	0.00	0.01	0.00	5.14	2.00	0.00	0.00	0.01	0.00
5.15	2.00	0.00	0.00	0.01	0.00	5.16	2.00	0.00	0.00	0.01	0.00
5.17	2.00	0.00	0.00	0.01	0.00	5.18	2.00	0.00	0.00	0.01	0.00
5.19	2.00	0.00	0.00	0.01	0.00	5.20	2.00	0.00	0.00	0.01	0.00
5.21	2.00	0.00	0.00	0.01	0.00	5.22	2.00	0.00	0.00	0.01	0.00
5.23	2.00	0.00	0.00	0.01	0.00	5.24	2.00	0.00	0.00	0.01	0.00
5.25	2.00	0.00	0.00	0.01	0.00	5.26	2.00	0.00	0.00	0.01	0.00
5.27	2.00	0.00	0.00	0.01	0.00	5.28	2.00	0.00	0.00	0.01	0.00
5.29	2.00	0.00	0.00	0.01	0.00	5.30	2.00	0.00	0.00	0.01	0.00
5.31	2.00	0.00	0.00	0.01	0.00	5.32	2.00	0.00	0.00	0.01	0.00
5.33	2.00	0.00	0.00	0.01	0.00	5.34	2.00	0.00	0.00	0.01	0.00
5.35	2.00	0.00	0.00	0.01	0.00	5.36	2.00	0.00	0.00	0.01	0.00
5.37	2.00	0.00	0.00	0.01	0.00	5.38	2.00	0.00	0.00	0.01	0.00
5.39	2.00	0.00	0.00	0.01	0.00	5.40	2.00	0.00	0.00	0.01	0.00
5.41	2.00	0.00	0.00	0.01	0.00	5.42	2.00	0.00	0.00	0.01	0.00
5.43	2.00	0.00	0.00	0.01	0.00	5.44	2.00	0.00	0.00	0.01	0.00
5.45	2.00	0.00	0.00	0.01	0.00	5.46	2.00	0.00	0.00	0.01	0.00
5.47	2.00	0.00	0.00	0.01	0.00	5.48	2.00	0.00	0.00	0.01	0.00
5.49	2.00	0.00	0.00	0.01	0.00	5.50	2.00	0.00	0.00	0.01	0.00
5.51	2.00	0.00	0.00	0.01	0.00	5.52	2.00	0.00	0.00	0.01	0.00
5.53	2.00	0.00	0.00	0.01	0.00	5.54	2.00	0.00	0.00	0.01	0.00
5.55	2.00	0.00	0.00	0.01	0.00	5.56	2.00	0.00	0.00	0.01	0.00
5.57	2.00	0.00	0.00	0.01	0.00	5.58	2.00	0.00	0.00	0.01	0.00
5.59	2.00	0.00	0.00	0.01	0.00	5.60	2.00	0.00	0.00	0.01	0.00
5.61	2.00	0.00	0.00	0.01	0.00	5.62	2.00	0.00	0.00	0.01	0.00
5.63	2.00	0.00	0.00	0.01	0.00	5.64	2.00	0.00	0.00	0.01	0.00
5.65	2.00	0.00	0.00	0.01	0.00	5.66	2.00	0.00	0.00	0.01	0.00
5.67	2.00	0.00	0.00	0.01	0.00	5.68	2.00	0.00	0.00	0.01	0.00
5.69	2.00	0.00	0.00	0.01	0.00	5.70	2.00	0.00	0.00	0.01	0.00
5.71	2.00	0.00	0.00	0.01	0.00	5.72	2.00	0.00	0.00	0.01	0.00
5.73	2.00	0.00	0.00	0.01	0.00	5.74	2.00	0.00	0.00	0.01	0.00
5.75	2.00	0.00	0.00	0.01	0.00	5.76	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
5.77	2.00	0.00	0.00	0.01	0.00	5.78	2.00	0.00	0.00	0.01	0.00
5.79	2.00	0.00	0.00	0.01	0.00	5.80	2.00	0.00	0.00	0.01	0.00
5.81	2.00	0.00	0.00	0.01	0.00	5.82	2.00	0.00	0.00	0.01	0.00
5.83	2.00	0.00	0.00	0.01	0.00	5.84	2.00	0.00	0.00	0.01	0.00
5.85	2.00	0.00	0.00	0.01	0.00	5.86	2.00	0.00	0.00	0.01	0.00
5.87	2.00	0.00	0.00	0.01	0.00	5.88	2.00	0.00	0.00	0.01	0.00
5.89	2.00	0.00	0.00	0.01	0.00	5.90	2.00	0.00	0.00	0.01	0.00
5.91	2.00	0.00	0.00	0.01	0.00	5.92	2.00	0.00	0.00	0.01	0.00
5.93	2.00	0.00	0.00	0.01	0.00	5.94	2.00	0.00	0.00	0.01	0.00
5.95	2.00	0.00	0.00	0.01	0.00	5.96	2.00	0.00	0.00	0.01	0.00
5.97	2.00	0.00	0.00	0.01	0.00	5.98	2.00	0.00	0.00	0.01	0.00
5.99	2.00	0.00	0.00	0.01	0.00	6.00	2.00	0.00	0.00	0.01	0.00
6.01	2.00	0.00	0.00	0.01	0.00	6.02	2.00	0.00	0.00	0.01	0.00
6.03	2.00	0.00	0.00	0.01	0.00	6.04	2.00	0.00	0.00	0.01	0.00
6.05	2.00	0.00	0.00	0.01	0.00	6.06	2.00	0.00	0.00	0.01	0.00
6.07	2.00	0.00	0.00	0.01	0.00	6.08	2.00	0.00	0.00	0.01	0.00
6.09	2.00	0.00	0.00	0.01	0.00	6.10	2.00	0.00	0.00	0.01	0.00
6.11	2.00	0.00	0.00	0.01	0.00	6.12	2.00	0.00	0.00	0.01	0.00
6.13	2.00	0.00	0.00	0.01	0.00	6.14	2.00	0.00	0.00	0.01	0.00
6.15	2.00	0.00	0.00	0.01	0.00	6.16	2.00	0.00	0.00	0.01	0.00
6.17	2.00	0.00	0.00	0.01	0.00	6.18	2.00	0.00	0.00	0.01	0.00
6.19	2.00	0.00	0.00	0.01	0.00	6.20	2.00	0.00	0.00	0.01	0.00
6.21	2.00	0.00	0.00	0.01	0.00	6.22	2.00	0.00	0.00	0.01	0.00
6.23	2.00	0.00	0.00	0.01	0.00	6.24	2.00	0.00	0.00	0.01	0.00
6.25	2.00	0.00	0.00	0.01	0.00	6.26	2.00	0.00	0.00	0.01	0.00
6.27	2.00	0.00	0.00	0.01	0.00	6.28	2.00	0.00	0.00	0.01	0.00
6.29	2.00	0.00	0.00	0.01	0.00	6.30	2.00	0.00	0.00	0.01	0.00
6.31	2.00	0.00	0.00	0.01	0.00	6.32	2.00	0.00	0.00	0.01	0.00
6.33	2.00	0.00	0.00	0.01	0.00	6.34	2.00	0.00	0.00	0.01	0.00
6.35	2.00	0.00	0.00	0.01	0.00	6.36	2.00	0.00	0.00	0.01	0.00
6.37	2.00	0.00	0.00	0.01	0.00	6.38	2.00	0.00	0.00	0.01	0.00
6.39	2.00	0.00	0.00	0.01	0.00	6.40	2.00	0.00	0.00	0.01	0.00
6.41	2.00	0.00	0.00	0.01	0.00	6.42	2.00	0.00	0.00	0.01	0.00
6.43	2.00	0.00	0.00	0.01	0.00	6.44	2.00	0.00	0.00	0.01	0.00
6.45	2.00	0.00	0.00	0.01	0.00	6.46	2.00	0.00	0.00	0.01	0.00
6.47	2.00	0.00	0.00	0.01	0.00	6.48	2.00	0.00	0.00	0.01	0.00
6.49	2.00	0.00	0.00	0.01	0.00	6.50	2.00	0.00	0.00	0.01	0.00
6.51	2.00	0.00	0.00	0.01	0.00	6.52	2.00	0.00	0.00	0.01	0.00
6.53	2.00	0.00	0.00	0.01	0.00	6.54	2.00	0.00	0.00	0.01	0.00
6.55	2.00	0.00	0.00	0.01	0.00	6.56	2.00	0.00	0.00	0.01	0.00
6.57	2.00	0.00	0.00	0.01	0.00	6.58	2.00	0.00	0.00	0.01	0.00
6.59	2.00	0.00	0.00	0.01	0.00	6.60	2.00	0.00	0.00	0.01	0.00
6.61	2.00	0.00	0.00	0.01	0.00	6.62	2.00	0.00	0.00	0.01	0.00
6.63	2.00	0.00	0.00	0.01	0.00	6.64	2.00	0.00	0.00	0.01	0.00
6.65	2.00	0.00	0.00	0.01	0.00	6.66	2.00	0.00	0.00	0.01	0.00
6.67	2.00	0.00	0.00	0.01	0.00	6.68	2.00	0.00	0.00	0.01	0.00
6.69	2.00	0.00	0.00	0.01	0.00	6.70	2.00	0.00	0.00	0.01	0.00
6.71	2.00	0.00	0.00	0.01	0.00	6.72	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
6.73	2.00	0.00	0.00	0.01	0.00	6.74	2.00	0.00	0.00	0.01	0.00
6.75	2.00	0.00	0.00	0.01	0.00	6.76	2.00	0.00	0.00	0.01	0.00
6.77	2.00	0.00	0.00	0.01	0.00	6.78	2.00	0.00	0.00	0.01	0.00
6.79	2.00	0.00	0.00	0.01	0.00	6.80	2.00	0.00	0.00	0.01	0.00
6.81	2.00	0.00	0.00	0.01	0.00	6.82	2.00	0.00	0.00	0.01	0.00
6.83	2.00	0.00	0.00	0.01	0.00	6.84	2.00	0.00	0.00	0.01	0.00
6.85	2.00	0.00	0.00	0.01	0.00	6.86	2.00	0.00	0.00	0.01	0.00
6.87	2.00	0.00	0.00	0.01	0.00	6.88	2.00	0.00	0.00	0.01	0.00
6.89	2.00	0.00	0.00	0.01	0.00	6.90	2.00	0.00	0.00	0.01	0.00
6.91	2.00	0.00	0.00	0.01	0.00	6.92	2.00	0.00	0.00	0.01	0.00
6.93	2.00	0.00	0.00	0.01	0.00	6.94	2.00	0.00	0.00	0.01	0.00
6.95	2.00	0.00	0.00	0.01	0.00	6.96	2.00	0.00	0.00	0.01	0.00
6.97	2.00	0.00	0.00	0.01	0.00	6.98	2.00	0.00	0.00	0.01	0.00
6.99	2.00	0.00	0.00	0.01	0.00	7.00	2.00	0.00	0.00	0.01	0.00
7.01	2.00	0.00	0.00	0.01	0.00	7.02	2.00	0.00	0.00	0.01	0.00
7.03	2.00	0.00	0.00	0.01	0.00	7.04	2.00	0.00	0.00	0.01	0.00
7.05	2.00	0.00	0.00	0.01	0.00	7.06	2.00	0.00	0.00	0.01	0.00
7.07	2.00	0.00	0.00	0.01	0.00	7.08	2.00	0.00	0.00	0.01	0.00
7.09	2.00	0.00	0.00	0.01	0.00	7.10	2.00	0.00	0.00	0.01	0.00
7.11	2.00	0.00	0.00	0.01	0.00	7.12	2.00	0.00	0.00	0.01	0.00
7.13	2.00	0.00	0.00	0.01	0.00	7.14	2.00	0.00	0.00	0.01	0.00
7.15	2.00	0.00	0.00	0.01	0.00	7.16	2.00	0.00	0.00	0.01	0.00
7.17	2.00	0.00	0.00	0.01	0.00	7.18	2.00	0.00	0.00	0.01	0.00
7.19	2.00	0.00	0.00	0.01	0.00	7.20	2.00	0.00	0.00	0.01	0.00
7.21	2.00	0.00	0.00	0.01	0.00	7.22	2.00	0.00	0.00	0.01	0.00
7.23	2.00	0.00	0.00	0.01	0.00	7.24	2.00	0.00	0.00	0.01	0.00
7.25	2.00	0.00	0.00	0.01	0.00	7.26	2.00	0.00	0.00	0.01	0.00
7.27	2.00	0.00	0.00	0.01	0.00	7.28	2.00	0.00	0.00	0.01	0.00
7.29	2.00	0.00	0.00	0.01	0.00	7.30	2.00	0.00	0.00	0.01	0.00
7.31	2.00	0.00	0.00	0.01	0.00	7.32	2.00	0.00	0.00	0.01	0.00
7.33	2.00	0.00	0.00	0.01	0.00	7.34	2.00	0.00	0.00	0.01	0.00
7.35	2.00	0.00	0.00	0.01	0.00	7.36	2.00	0.00	0.00	0.01	0.00
7.37	2.00	0.00	0.00	0.01	0.00	7.38	2.00	0.00	0.00	0.01	0.00
7.39	2.00	0.00	0.00	0.01	0.00	7.40	2.00	0.00	0.00	0.01	0.00
7.41	2.00	0.00	0.00	0.01	0.00	7.42	2.00	0.00	0.00	0.01	0.00
7.43	2.00	0.00	0.00	0.01	0.00	7.44	2.00	0.00	0.00	0.01	0.00
7.45	2.00	0.00	0.00	0.01	0.00	7.46	2.00	0.00	0.00	0.01	0.00
7.47	2.00	0.00	0.00	0.01	0.00	7.48	2.00	0.00	0.00	0.01	0.00
7.49	2.00	0.00	0.00	0.01	0.00	7.50	2.00	0.00	0.00	0.01	0.00
7.51	2.00	0.00	0.00	0.01	0.00	7.52	2.00	0.00	0.00	0.01	0.00
7.53	2.00	0.00	0.00	0.01	0.00	7.54	2.00	0.00	0.00	0.01	0.00
7.55	2.00	0.00	0.00	0.01	0.00	7.56	2.00	0.00	0.00	0.01	0.00
7.57	2.00	0.00	0.00	0.01	0.00	7.58	2.00	0.00	0.00	0.01	0.00
7.59	2.00	0.00	0.00	0.01	0.00	7.60	2.00	0.00	0.00	0.01	0.00
7.61	2.00	0.00	0.00	0.01	0.00	7.62	2.00	0.00	0.00	0.01	0.00
7.63	2.00	0.00	0.00	0.01	0.00	7.64	2.00	0.00	0.00	0.01	0.00
7.65	2.00	0.00	0.00	0.01	0.00	7.66	2.00	0.00	0.00	0.01	0.00
7.67	2.00	0.00	0.00	0.01	0.00	7.68	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
7.69	2.00	0.00	0.00	0.01	0.00	7.70	2.00	0.00	0.00	0.01	0.00
7.71	2.00	0.00	0.00	0.01	0.00	7.72	2.00	0.00	0.00	0.01	0.00
7.73	2.00	0.00	0.00	0.01	0.00	7.74	2.00	0.00	0.00	0.01	0.00
7.75	2.00	0.00	0.00	0.01	0.00	7.76	2.00	0.00	0.00	0.01	0.00
7.77	2.00	0.00	0.00	0.01	0.00	7.78	2.00	0.00	0.00	0.01	0.00
7.79	2.00	0.00	0.00	0.01	0.00	7.80	2.00	0.00	0.00	0.01	0.00
7.81	2.00	0.00	0.00	0.01	0.00	7.82	2.00	0.00	0.00	0.01	0.00
7.83	2.00	0.00	0.00	0.01	0.00	7.84	2.00	0.00	0.00	0.01	0.00
7.85	2.00	0.00	0.00	0.01	0.00	7.86	2.00	0.00	0.00	0.01	0.00
7.87	2.00	0.00	0.00	0.01	0.00	7.88	2.00	0.00	0.00	0.01	0.00
7.89	2.00	0.00	0.00	0.01	0.00	7.90	2.00	0.00	0.00	0.01	0.00
7.91	2.00	0.00	0.00	0.01	0.00	7.92	2.00	0.00	0.00	0.01	0.00
7.93	2.00	0.00	0.00	0.01	0.00	7.94	2.00	0.00	0.00	0.01	0.00
7.95	2.00	0.00	0.00	0.01	0.00	7.96	2.00	0.00	0.00	0.01	0.00
7.97	2.00	0.00	0.00	0.01	0.00	7.98	2.00	0.00	0.00	0.01	0.00
7.99	2.00	0.00	0.00	0.01	0.00	8.00	2.00	0.00	0.00	0.01	0.00
8.01	0.75	0.00	0.00	0.01	0.01	8.02	0.75	0.00	0.00	0.01	0.01
8.03	0.75	0.00	0.00	0.01	0.01	8.04	0.76	0.00	0.00	0.01	0.01
8.05	0.77	0.00	0.00	0.01	0.01	8.06	0.77	0.00	0.00	0.01	0.01
8.07	0.78	0.00	0.00	0.01	0.01	8.08	0.79	0.00	0.00	0.01	0.01
8.09	0.79	0.00	0.00	0.01	0.01	8.10	0.79	0.00	0.00	0.01	0.01
8.11	0.79	0.00	0.00	0.01	0.01	8.12	0.79	0.00	0.00	0.01	0.01
8.13	0.79	0.00	0.00	0.01	0.01	8.14	0.79	0.00	0.00	0.01	0.01
8.15	0.79	0.00	0.00	0.01	0.01	8.16	0.79	0.00	0.00	0.01	0.01
8.17	0.79	0.00	0.00	0.01	0.01	8.18	0.79	0.00	0.00	0.01	0.01
8.19	0.79	0.00	0.00	0.01	0.01	8.20	0.79	0.00	0.00	0.01	0.01
8.21	0.78	0.00	0.00	0.01	0.01	8.22	0.78	0.00	0.00	0.01	0.01
8.23	0.78	0.00	0.00	0.01	0.01	8.24	0.77	0.00	0.00	0.01	0.01
8.25	0.77	0.00	0.00	0.01	0.01	8.26	0.77	0.00	0.00	0.01	0.01
8.27	0.77	0.00	0.00	0.01	0.01	8.28	0.77	0.00	0.00	0.01	0.01
8.29	0.77	0.00	0.00	0.01	0.01	8.30	0.78	0.00	0.00	0.01	0.01
8.31	0.78	0.00	0.00	0.01	0.01	8.32	0.79	0.00	0.00	0.01	0.01
8.33	0.79	0.00	0.00	0.01	0.01	8.34	0.80	0.00	0.00	0.01	0.01
8.35	0.80	0.00	0.00	0.01	0.01	8.36	0.81	0.00	0.00	0.01	0.01
8.37	0.82	0.00	0.00	0.01	0.00	8.38	0.82	0.00	0.00	0.01	0.00
8.39	0.83	0.00	0.00	0.01	0.00	8.40	0.84	0.00	0.00	0.01	0.00
8.41	0.86	0.00	0.00	0.01	0.00	8.42	0.87	0.00	0.00	0.01	0.00
8.43	0.88	0.00	0.00	0.01	0.00	8.44	0.89	0.00	0.00	0.01	0.00
8.45	0.89	0.00	0.00	0.01	0.00	8.46	0.90	0.00	0.00	0.01	0.00
8.47	0.91	0.00	0.00	0.01	0.00	8.48	0.92	0.00	0.00	0.01	0.00
8.49	0.93	0.00	0.00	0.01	0.00	8.50	0.94	0.00	0.00	0.01	0.00
8.51	0.94	0.00	0.00	0.01	0.00	8.52	0.95	0.00	0.00	0.01	0.00
8.53	0.96	0.00	0.00	0.01	0.00	8.54	0.96	0.00	0.00	0.01	0.00
8.55	0.97	0.00	0.00	0.01	0.00	8.56	0.97	0.00	0.00	0.01	0.00
8.57	0.98	0.00	0.00	0.01	0.00	8.58	0.98	0.00	0.00	0.01	0.00
8.59	0.99	0.00	0.00	0.01	0.00	8.60	1.00	0.00	0.00	0.01	0.00
8.61	1.00	0.00	0.00	0.01	0.00	8.62	1.00	0.00	0.00	0.01	0.00
8.63	1.00	0.00	0.00	0.01	0.00	8.64	1.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
8.65	1.00	0.00	0.00	0.01	0.00	8.66	1.01	0.00	0.00	0.01	0.00
8.67	1.01	0.00	0.00	0.01	0.00	8.68	1.01	0.00	0.00	0.01	0.00
8.69	1.01	0.00	0.00	0.01	0.00	8.70	1.01	0.00	0.00	0.01	0.00
8.71	1.01	0.00	0.00	0.01	0.00	8.72	1.00	0.00	0.00	0.01	0.00
8.73	1.00	0.00	0.00	0.01	0.00	8.74	0.99	0.00	0.00	0.01	0.00
8.75	0.99	0.00	0.00	0.01	0.00	8.76	0.98	0.00	0.00	0.01	0.00
8.77	0.98	0.00	0.00	0.01	0.00	8.78	0.98	0.00	0.00	0.01	0.00
8.79	0.97	0.00	0.00	0.01	0.00	8.80	0.97	0.00	0.00	0.01	0.00
8.81	0.96	0.00	0.00	0.01	0.00	8.82	0.95	0.00	0.00	0.01	0.00
8.83	0.95	0.00	0.00	0.01	0.00	8.84	0.94	0.00	0.00	0.01	0.00
8.85	0.93	0.00	0.00	0.01	0.00	8.86	0.93	0.00	0.00	0.01	0.00
8.87	0.92	0.00	0.00	0.01	0.00	8.88	0.91	0.00	0.00	0.01	0.00
8.89	0.91	0.00	0.00	0.01	0.00	8.90	0.90	0.00	0.00	0.01	0.00
8.91	0.89	0.00	0.00	0.01	0.00	8.92	0.88	0.00	0.00	0.01	0.00
8.93	0.87	0.00	0.00	0.01	0.00	8.94	0.87	0.00	0.00	0.01	0.00
8.95	0.86	0.00	0.00	0.01	0.00	8.96	0.86	0.00	0.00	0.01	0.00
8.97	0.85	0.00	0.00	0.01	0.00	8.98	0.84	0.00	0.00	0.01	0.00
8.99	0.84	0.00	0.00	0.01	0.00	9.00	0.83	0.00	0.00	0.01	0.00
9.01	0.82	0.00	0.00	0.01	0.00	9.02	0.81	0.00	0.00	0.01	0.00
9.03	0.80	0.00	0.00	0.01	0.01	9.04	0.80	0.00	0.00	0.01	0.01
9.05	0.79	0.00	0.00	0.01	0.01	9.06	0.79	0.00	0.00	0.01	0.01
9.07	0.79	0.00	0.00	0.01	0.01	9.08	0.79	0.00	0.00	0.01	0.01
9.09	0.79	0.00	0.00	0.01	0.01	9.10	0.79	0.00	0.00	0.01	0.01
9.11	0.78	0.00	0.00	0.01	0.01	9.12	0.78	0.00	0.00	0.01	0.01
9.13	0.78	0.00	0.00	0.01	0.01	9.14	0.78	0.00	0.00	0.01	0.01
9.15	0.79	0.00	0.00	0.01	0.01	9.16	0.79	0.00	0.00	0.01	0.01
9.17	0.80	0.00	0.00	0.01	0.01	9.18	0.80	0.00	0.00	0.01	0.01
9.19	0.81	0.00	0.00	0.01	0.01	9.20	0.81	0.00	0.00	0.01	0.00
9.21	0.81	0.00	0.00	0.01	0.00	9.22	0.82	0.00	0.00	0.01	0.00
9.23	0.82	0.00	0.00	0.01	0.00	9.24	0.82	0.00	0.00	0.01	0.00
9.25	0.82	0.00	0.00	0.01	0.00	9.26	0.82	0.00	0.00	0.01	0.00
9.27	0.83	0.00	0.00	0.01	0.00	9.28	0.83	0.00	0.00	0.01	0.00
9.29	0.83	0.00	0.00	0.01	0.00	9.30	0.83	0.00	0.00	0.01	0.00
9.31	0.83	0.00	0.00	0.01	0.00	9.32	0.83	0.00	0.00	0.01	0.00
9.33	0.83	0.00	0.00	0.01	0.00	9.34	0.84	0.00	0.00	0.01	0.00
9.35	0.84	0.00	0.00	0.01	0.00	9.36	0.84	0.00	0.00	0.01	0.00
9.37	0.85	0.00	0.00	0.01	0.00	9.38	0.85	0.00	0.00	0.01	0.00
9.39	0.85	0.00	0.00	0.01	0.00	9.40	0.85	0.00	0.00	0.01	0.00
9.41	0.86	0.00	0.00	0.01	0.00	9.42	0.87	0.00	0.00	0.01	0.00
9.43	0.88	0.00	0.00	0.01	0.00	9.44	0.89	0.00	0.00	0.01	0.00
9.45	0.90	0.00	0.00	0.01	0.00	9.46	0.91	0.00	0.00	0.01	0.00
9.47	0.93	0.00	0.00	0.01	0.00	9.48	0.94	0.00	0.00	0.01	0.00
9.49	0.95	0.00	0.00	0.01	0.00	9.50	0.96	0.00	0.00	0.01	0.00
9.51	0.98	0.00	0.00	0.01	0.00	9.52	1.00	0.00	0.00	0.01	0.00
9.53	1.03	0.00	0.00	0.01	0.00	9.54	1.05	0.00	0.00	0.01	0.00
9.55	1.08	0.00	0.00	0.01	0.00	9.56	1.10	0.00	0.00	0.01	0.00
9.57	1.11	0.00	0.00	0.01	0.00	9.58	1.07	0.00	0.00	0.01	0.00
9.59	1.03	0.00	0.00	0.01	0.00	9.60	0.98	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
9.61	0.94	0.00	0.00	0.01	0.00	9.62	0.90	0.00	0.00	0.01	0.00
9.63	0.86	0.00	0.00	0.01	0.00	9.64	0.83	0.00	0.00	0.01	0.00
9.65	0.81	0.00	0.00	0.01	0.01	9.66	0.80	0.00	0.00	0.01	0.01
9.67	0.80	0.00	0.00	0.01	0.01	9.68	0.80	0.00	0.00	0.01	0.01
9.69	0.80	0.00	0.00	0.01	0.01	9.70	0.80	0.00	0.00	0.01	0.01
9.71	0.80	0.00	0.00	0.01	0.01	9.72	0.80	0.00	0.00	0.01	0.01
9.73	0.80	0.00	0.00	0.01	0.01	9.74	0.80	0.00	0.00	0.01	0.01
9.75	0.76	0.00	0.00	0.01	0.01	9.76	0.72	0.00	0.00	0.01	0.01
9.77	0.67	0.00	0.00	0.01	0.01	9.78	0.62	0.00	0.00	0.01	0.01
9.79	0.58	0.00	0.00	0.01	0.01	9.80	0.55	0.00	0.00	0.01	0.01
9.81	0.52	0.00	0.00	0.01	0.01	9.82	0.50	0.00	0.00	0.01	0.01
9.83	0.49	0.00	0.00	0.01	0.01	9.84	0.49	0.00	0.00	0.01	0.01
9.85	0.51	0.00	0.00	0.01	0.01	9.86	0.53	0.00	0.00	0.01	0.01
9.87	0.56	0.00	0.00	0.01	0.01	9.88	0.57	0.00	0.00	0.01	0.01
9.89	0.58	0.00	0.00	0.01	0.01	9.90	0.57	0.00	0.00	0.01	0.01
9.91	0.56	0.00	0.00	0.01	0.01	9.92	0.57	0.00	0.00	0.01	0.01
9.93	0.59	0.00	0.00	0.01	0.01	9.94	0.62	0.00	0.00	0.01	0.01
9.95	0.65	0.00	0.00	0.01	0.01	9.96	0.69	0.00	0.00	0.01	0.01
9.97	0.73	0.00	0.00	0.01	0.01	9.98	0.76	0.00	0.00	0.01	0.01
9.99	0.79	0.00	0.00	0.01	0.01	10.00	0.81	0.00	0.00	0.01	0.00
10.01	0.81	0.00	0.00	0.01	0.00	10.02	0.79	0.00	0.00	0.01	0.01
10.03	0.77	0.00	0.00	0.01	0.01	10.04	0.74	0.00	0.00	0.01	0.01
10.05	0.72	0.00	0.00	0.01	0.01	10.06	0.70	0.00	0.00	0.01	0.01
10.07	0.68	0.00	0.00	0.01	0.01	10.08	2.00	0.00	0.00	0.01	0.00
10.09	2.00	0.00	0.00	0.01	0.00	10.10	2.00	0.00	0.00	0.01	0.00
10.11	2.00	0.00	0.00	0.01	0.00	10.12	2.00	0.00	0.00	0.01	0.00
10.13	2.00	0.00	0.00	0.01	0.00	10.14	2.00	0.00	0.00	0.01	0.00
10.15	2.00	0.00	0.00	0.01	0.00	10.16	2.00	0.00	0.00	0.01	0.00
10.17	2.00	0.00	0.00	0.01	0.00	10.18	2.00	0.00	0.00	0.01	0.00
10.19	2.00	0.00	0.00	0.01	0.00	10.20	2.00	0.00	0.00	0.01	0.00
10.21	2.00	0.00	0.00	0.01	0.00	10.22	2.00	0.00	0.00	0.01	0.00
10.23	2.00	0.00	0.00	0.01	0.00	10.24	2.00	0.00	0.00	0.01	0.00
10.25	2.00	0.00	0.00	0.01	0.00	10.26	2.00	0.00	0.00	0.01	0.00
10.27	2.00	0.00	0.00	0.01	0.00	10.28	2.00	0.00	0.00	0.01	0.00
10.29	2.00	0.00	0.00	0.01	0.00	10.30	2.00	0.00	0.00	0.01	0.00
10.31	2.00	0.00	0.00	0.01	0.00	10.32	2.00	0.00	0.00	0.01	0.00
10.33	2.00	0.00	0.00	0.01	0.00	10.34	2.00	0.00	0.00	0.01	0.00
10.35	2.00	0.00	0.00	0.01	0.00	10.36	2.00	0.00	0.00	0.01	0.00
10.37	2.00	0.00	0.00	0.01	0.00	10.38	2.00	0.00	0.00	0.01	0.00
10.39	2.00	0.00	0.00	0.01	0.00	10.40	2.00	0.00	0.00	0.01	0.00
10.41	2.00	0.00	0.00	0.01	0.00	10.42	2.00	0.00	0.00	0.01	0.00
10.43	2.00	0.00	0.00	0.01	0.00	10.44	2.00	0.00	0.00	0.01	0.00
10.45	2.00	0.00	0.00	0.01	0.00	10.46	2.00	0.00	0.00	0.01	0.00
10.47	2.00	0.00	0.00	0.01	0.00	10.48	2.00	0.00	0.00	0.01	0.00
10.49	2.00	0.00	0.00	0.01	0.00	10.50	2.00	0.00	0.00	0.01	0.00
10.51	2.00	0.00	0.00	0.01	0.00	10.52	2.00	0.00	0.00	0.01	0.00
10.53	2.00	0.00	0.00	0.01	0.00	10.54	2.00	0.00	0.00	0.01	0.00
10.55	2.00	0.00	0.00	0.01	0.00	10.56	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
10.57	2.00	0.00	0.00	0.01	0.00	10.58	2.00	0.00	0.00	0.01	0.00
10.59	2.00	0.00	0.00	0.01	0.00	10.60	2.00	0.00	0.00	0.01	0.00
10.61	2.00	0.00	0.00	0.01	0.00	10.62	2.00	0.00	0.00	0.01	0.00
10.63	2.00	0.00	0.00	0.01	0.00	10.64	2.00	0.00	0.00	0.01	0.00
10.65	2.00	0.00	0.00	0.01	0.00	10.66	2.00	0.00	0.00	0.01	0.00
10.67	2.00	0.00	0.00	0.01	0.00	10.68	2.00	0.00	0.00	0.01	0.00
10.69	2.00	0.00	0.00	0.01	0.00	10.70	2.00	0.00	0.00	0.01	0.00
10.71	2.00	0.00	0.00	0.01	0.00	10.72	2.00	0.00	0.00	0.01	0.00
10.73	2.00	0.00	0.00	0.01	0.00	10.74	2.00	0.00	0.00	0.01	0.00
10.75	2.00	0.00	0.00	0.01	0.00	10.76	2.00	0.00	0.00	0.01	0.00
10.77	2.00	0.00	0.00	0.01	0.00	10.78	2.00	0.00	0.00	0.01	0.00
10.79	2.00	0.00	0.00	0.01	0.00	10.80	2.00	0.00	0.00	0.01	0.00
10.81	2.00	0.00	0.00	0.01	0.00	10.82	2.00	0.00	0.00	0.01	0.00
10.83	2.00	0.00	0.00	0.01	0.00	10.84	2.00	0.00	0.00	0.01	0.00
10.85	2.00	0.00	0.00	0.01	0.00	10.86	2.00	0.00	0.00	0.01	0.00
10.87	2.00	0.00	0.00	0.01	0.00	10.88	2.00	0.00	0.00	0.01	0.00
10.89	2.00	0.00	0.00	0.01	0.00	10.90	2.00	0.00	0.00	0.01	0.00
10.91	2.00	0.00	0.00	0.01	0.00	10.92	2.00	0.00	0.00	0.01	0.00
10.93	2.00	0.00	0.00	0.01	0.00	10.94	2.00	0.00	0.00	0.01	0.00
10.95	2.00	0.00	0.00	0.01	0.00	10.96	2.00	0.00	0.00	0.01	0.00
10.97	2.00	0.00	0.00	0.01	0.00	10.98	2.00	0.00	0.00	0.01	0.00
10.99	2.00	0.00	0.00	0.01	0.00	11.00	2.00	0.00	0.00	0.01	0.00
11.01	2.00	0.00	0.00	0.01	0.00	11.02	2.00	0.00	0.00	0.01	0.00
11.03	2.00	0.00	0.00	0.01	0.00	11.04	2.00	0.00	0.00	0.01	0.00
11.05	2.00	0.00	0.00	0.01	0.00	11.06	2.00	0.00	0.00	0.01	0.00
11.07	2.00	0.00	0.00	0.01	0.00	11.08	2.00	0.00	0.00	0.01	0.00
11.09	2.00	0.00	0.00	0.01	0.00	11.10	2.00	0.00	0.00	0.01	0.00
11.11	2.00	0.00	0.00	0.01	0.00	11.12	2.00	0.00	0.00	0.01	0.00
11.13	2.00	0.00	0.00	0.01	0.00	11.14	0.38	0.00	0.00	0.01	0.02
11.15	0.38	0.00	0.00	0.01	0.02	11.16	0.37	0.00	0.00	0.01	0.02
11.17	0.37	0.00	0.00	0.01	0.02	11.18	0.37	0.00	0.00	0.01	0.02
11.19	0.36	0.00	0.00	0.01	0.02	11.20	0.36	0.00	0.00	0.01	0.02
11.21	0.36	0.00	0.00	0.01	0.02	11.22	2.00	0.00	0.00	0.01	0.00
11.23	2.00	0.00	0.00	0.01	0.00	11.24	2.00	0.00	0.00	0.01	0.00
11.25	2.00	0.00	0.00	0.01	0.00	11.26	2.00	0.00	0.00	0.01	0.00
11.27	2.00	0.00	0.00	0.01	0.00	11.28	2.00	0.00	0.00	0.01	0.00
11.29	2.00	0.00	0.00	0.01	0.00	11.30	2.00	0.00	0.00	0.01	0.00
11.31	2.00	0.00	0.00	0.01	0.00	11.32	2.00	0.00	0.00	0.01	0.00
11.33	2.00	0.00	0.00	0.01	0.00	11.34	2.00	0.00	0.00	0.01	0.00
11.35	2.00	0.00	0.00	0.01	0.00	11.36	2.00	0.00	0.00	0.01	0.00
11.37	2.00	0.00	0.00	0.01	0.00	11.38	2.00	0.00	0.00	0.01	0.00
11.39	2.00	0.00	0.00	0.01	0.00	11.40	2.00	0.00	0.00	0.01	0.00
11.41	2.00	0.00	0.00	0.01	0.00	11.42	2.00	0.00	0.00	0.01	0.00
11.43	2.00	0.00	0.00	0.01	0.00	11.44	2.00	0.00	0.00	0.01	0.00
11.45	2.00	0.00	0.00	0.01	0.00	11.46	2.00	0.00	0.00	0.01	0.00
11.47	2.00	0.00	0.00	0.01	0.00	11.48	2.00	0.00	0.00	0.01	0.00
11.49	2.00	0.00	0.00	0.01	0.00	11.50	2.00	0.00	0.00	0.01	0.00
11.51	2.00	0.00	0.00	0.01	0.00	11.52	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
11.53	2.00	0.00	0.00	0.01	0.00	11.54	2.00	0.00	0.00	0.01	0.00
11.55	2.00	0.00	0.00	0.01	0.00	11.56	2.00	0.00	0.00	0.01	0.00
11.57	2.00	0.00	0.00	0.01	0.00	11.58	2.00	0.00	0.00	0.01	0.00
11.59	2.00	0.00	0.00	0.01	0.00	11.60	2.00	0.00	0.00	0.01	0.00
11.61	2.00	0.00	0.00	0.01	0.00	11.62	2.00	0.00	0.00	0.01	0.00
11.63	2.00	0.00	0.00	0.01	0.00	11.64	2.00	0.00	0.00	0.01	0.00
11.65	2.00	0.00	0.00	0.01	0.00	11.66	2.00	0.00	0.00	0.01	0.00
11.67	2.00	0.00	0.00	0.01	0.00	11.68	2.00	0.00	0.00	0.01	0.00
11.69	2.00	0.00	0.00	0.01	0.00	11.70	2.00	0.00	0.00	0.01	0.00
11.71	2.00	0.00	0.00	0.01	0.00	11.72	2.00	0.00	0.00	0.01	0.00
11.73	2.00	0.00	0.00	0.01	0.00	11.74	2.00	0.00	0.00	0.01	0.00
11.75	2.00	0.00	0.00	0.01	0.00	11.76	2.00	0.00	0.00	0.01	0.00
11.77	2.00	0.00	0.00	0.01	0.00	11.78	2.00	0.00	0.00	0.01	0.00
11.79	2.00	0.00	0.00	0.01	0.00	11.80	2.00	0.00	0.00	0.01	0.00
11.81	2.00	0.00	0.00	0.01	0.00	11.82	2.00	0.00	0.00	0.01	0.00
11.83	2.00	0.00	0.00	0.01	0.00	11.84	2.00	0.00	0.00	0.01	0.00
11.85	2.00	0.00	0.00	0.01	0.00	11.86	2.00	0.00	0.00	0.01	0.00
11.87	2.00	0.00	0.00	0.01	0.00	11.88	2.00	0.00	0.00	0.01	0.00
11.89	2.00	0.00	0.00	0.01	0.00	11.90	2.00	0.00	0.00	0.01	0.00
11.91	2.00	0.00	0.00	0.01	0.00	11.92	2.00	0.00	0.00	0.01	0.00
11.93	2.00	0.00	0.00	0.01	0.00	11.94	2.00	0.00	0.00	0.01	0.00
11.95	2.00	0.00	0.00	0.01	0.00	11.96	2.00	0.00	0.00	0.01	0.00
11.97	2.00	0.00	0.00	0.01	0.00	11.98	2.00	0.00	0.00	0.01	0.00
11.99	2.00	0.00	0.00	0.01	0.00	12.00	2.00	0.00	0.00	0.01	0.00
12.01	2.00	0.00	0.00	0.01	0.00	12.02	2.00	0.00	0.00	0.01	0.00
12.03	2.00	0.00	0.00	0.01	0.00	12.04	2.00	0.00	0.00	0.01	0.00
12.05	2.00	0.00	0.00	0.01	0.00	12.06	2.00	0.00	0.00	0.01	0.00
12.07	2.00	0.00	0.00	0.01	0.00	12.08	2.00	0.00	0.00	0.01	0.00
12.09	2.00	0.00	0.00	0.01	0.00	12.10	2.00	0.00	0.00	0.01	0.00
12.11	2.00	0.00	0.00	0.01	0.00	12.12	2.00	0.00	0.00	0.01	0.00
12.13	2.00	0.00	0.00	0.01	0.00	12.14	2.00	0.00	0.00	0.01	0.00
12.15	2.00	0.00	0.00	0.01	0.00	12.16	2.00	0.00	0.00	0.01	0.00
12.17	2.00	0.00	0.00	0.01	0.00	12.18	2.00	0.00	0.00	0.01	0.00
12.19	2.00	0.00	0.00	0.01	0.00	12.20	2.00	0.00	0.00	0.01	0.00
12.21	2.00	0.00	0.00	0.01	0.00	12.22	2.00	0.00	0.00	0.01	0.00
12.23	2.00	0.00	0.00	0.01	0.00	12.24	2.00	0.00	0.00	0.01	0.00
12.25	2.00	0.00	0.00	0.01	0.00	12.26	2.00	0.00	0.00	0.01	0.00
12.27	2.00	0.00	0.00	0.01	0.00	12.28	2.00	0.00	0.00	0.01	0.00
12.29	2.00	0.00	0.00	0.01	0.00	12.30	2.00	0.00	0.00	0.01	0.00
12.31	2.00	0.00	0.00	0.01	0.00	12.32	2.00	0.00	0.00	0.01	0.00
12.33	2.00	0.00	0.00	0.01	0.00	12.34	2.00	0.00	0.00	0.01	0.00
12.35	2.00	0.00	0.00	0.01	0.00	12.36	2.00	0.00	0.00	0.01	0.00
12.37	2.00	0.00	0.00	0.01	0.00	12.38	2.00	0.00	0.00	0.01	0.00
12.39	2.00	0.00	0.00	0.01	0.00	12.40	2.00	0.00	0.00	0.01	0.00
12.41	2.00	0.00	0.00	0.01	0.00	12.42	2.00	0.00	0.00	0.01	0.00
12.43	2.00	0.00	0.00	0.01	0.00	12.44	2.00	0.00	0.00	0.01	0.00
12.45	2.00	0.00	0.00	0.01	0.00	12.46	2.00	0.00	0.00	0.01	0.00
12.47	2.00	0.00	0.00	0.01	0.00	12.48	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
12.49	2.00	0.00	0.00	0.01	0.00	12.50	2.00	0.00	0.00	0.01	0.00
12.51	2.00	0.00	0.00	0.01	0.00	12.52	2.00	0.00	0.00	0.01	0.00
12.53	2.00	0.00	0.00	0.01	0.00	12.54	2.00	0.00	0.00	0.01	0.00
12.55	2.00	0.00	0.00	0.01	0.00	12.56	2.00	0.00	0.00	0.01	0.00
12.57	2.00	0.00	0.00	0.01	0.00	12.58	2.00	0.00	0.00	0.01	0.00
12.59	2.00	0.00	0.00	0.01	0.00	12.60	2.00	0.00	0.00	0.01	0.00
12.61	2.00	0.00	0.00	0.01	0.00	12.62	2.00	0.00	0.00	0.01	0.00
12.63	2.00	0.00	0.00	0.01	0.00	12.64	2.00	0.00	0.00	0.01	0.00
12.65	2.00	0.00	0.00	0.01	0.00	12.66	2.00	0.00	0.00	0.01	0.00
12.67	2.00	0.00	0.00	0.01	0.00	12.68	2.00	0.00	0.00	0.01	0.00
12.69	2.00	0.00	0.00	0.01	0.00	12.70	2.00	0.00	0.00	0.01	0.00
12.71	2.00	0.00	0.00	0.01	0.00	12.72	2.00	0.00	0.00	0.01	0.00
12.73	2.00	0.00	0.00	0.01	0.00	12.74	2.00	0.00	0.00	0.01	0.00
12.75	2.00	0.00	0.00	0.01	0.00	12.76	2.00	0.00	0.00	0.01	0.00
12.77	2.00	0.00	0.00	0.01	0.00	12.78	2.00	0.00	0.00	0.01	0.00
12.79	2.00	0.00	0.00	0.01	0.00	12.80	2.00	0.00	0.00	0.01	0.00
12.81	2.00	0.00	0.00	0.01	0.00	12.82	2.00	0.00	0.00	0.01	0.00
12.83	2.00	0.00	0.00	0.01	0.00	12.84	2.00	0.00	0.00	0.01	0.00
12.85	2.00	0.00	0.00	0.01	0.00	12.86	2.00	0.00	0.00	0.01	0.00
12.87	2.00	0.00	0.00	0.01	0.00	12.88	2.00	0.00	0.00	0.01	0.00
12.89	2.00	0.00	0.00	0.01	0.00	12.90	2.00	0.00	0.00	0.01	0.00
12.91	2.00	0.00	0.00	0.01	0.00	12.92	2.00	0.00	0.00	0.01	0.00
12.93	2.00	0.00	0.00	0.01	0.00	12.94	2.00	0.00	0.00	0.01	0.00
12.95	2.00	0.00	0.00	0.01	0.00	12.96	2.00	0.00	0.00	0.01	0.00
12.97	2.00	0.00	0.00	0.01	0.00	12.98	2.00	0.00	0.00	0.01	0.00
12.99	2.00	0.00	0.00	0.01	0.00	13.00	2.00	0.00	0.00	0.01	0.00
13.01	2.00	0.00	0.00	0.01	0.00	13.02	2.00	0.00	0.00	0.01	0.00
13.03	2.00	0.00	0.00	0.01	0.00	13.04	2.00	0.00	0.00	0.01	0.00
13.05	2.00	0.00	0.00	0.01	0.00	13.06	2.00	0.00	0.00	0.01	0.00
13.07	2.00	0.00	0.00	0.01	0.00	13.08	2.00	0.00	0.00	0.01	0.00
13.09	2.00	0.00	0.00	0.01	0.00	13.10	2.00	0.00	0.00	0.01	0.00
13.11	2.00	0.00	0.00	0.01	0.00	13.12	2.00	0.00	0.00	0.01	0.00
13.13	2.00	0.00	0.00	0.01	0.00	13.14	2.00	0.00	0.00	0.01	0.00
13.15	2.00	0.00	0.00	0.01	0.00	13.16	2.00	0.00	0.00	0.01	0.00
13.17	2.00	0.00	0.00	0.01	0.00	13.18	2.00	0.00	0.00	0.01	0.00
13.19	2.00	0.00	0.00	0.01	0.00	13.20	2.00	0.00	0.00	0.01	0.00
13.21	2.00	0.00	0.00	0.01	0.00	13.22	2.00	0.00	0.00	0.01	0.00
13.23	2.00	0.00	0.00	0.01	0.00	13.24	2.00	0.00	0.00	0.01	0.00
13.25	2.00	0.00	0.00	0.01	0.00	13.26	2.00	0.00	0.00	0.01	0.00
13.27	2.00	0.00	0.00	0.01	0.00	13.28	2.00	0.00	0.00	0.01	0.00
13.29	2.00	0.00	0.00	0.01	0.00	13.30	2.00	0.00	0.00	0.01	0.00
13.31	2.00	0.00	0.00	0.01	0.00	13.32	2.00	0.00	0.00	0.01	0.00
13.33	2.00	0.00	0.00	0.01	0.00	13.34	2.00	0.00	0.00	0.01	0.00
13.35	2.00	0.00	0.00	0.01	0.00	13.36	2.00	0.00	0.00	0.01	0.00
13.37	2.00	0.00	0.00	0.01	0.00	13.38	2.00	0.00	0.00	0.01	0.00
13.39	2.00	0.00	0.00	0.01	0.00	13.40	2.00	0.00	0.00	0.01	0.00
13.41	2.00	0.00	0.00	0.01	0.00	13.42	2.00	0.00	0.00	0.01	0.00
13.43	2.00	0.00	0.00	0.01	0.00	13.44	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
13.45	2.00	0.00	0.00	0.01	0.00	13.46	2.00	0.00	0.00	0.01	0.00
13.47	2.00	0.00	0.00	0.01	0.00	13.48	2.00	0.00	0.00	0.01	0.00
13.49	2.00	0.00	0.00	0.01	0.00	13.50	2.00	0.00	0.00	0.01	0.00
13.51	2.00	0.00	0.00	0.01	0.00	13.52	2.00	0.00	0.00	0.01	0.00
13.53	2.00	0.00	0.00	0.01	0.00	13.54	2.00	0.00	0.00	0.01	0.00
13.55	2.00	0.00	0.00	0.01	0.00	13.56	2.00	0.00	0.00	0.01	0.00
13.57	2.00	0.00	0.00	0.01	0.00	13.58	2.00	0.00	0.00	0.01	0.00
13.59	2.00	0.00	0.00	0.01	0.00	13.60	2.00	0.00	0.00	0.01	0.00
13.61	2.00	0.00	0.00	0.01	0.00	13.62	2.00	0.00	0.00	0.01	0.00
13.63	2.00	0.00	0.00	0.01	0.00	13.64	2.00	0.00	0.00	0.01	0.00
13.65	2.00	0.00	0.00	0.01	0.00	13.66	2.00	0.00	0.00	0.01	0.00
13.67	2.00	0.00	0.00	0.01	0.00	13.68	2.00	0.00	0.00	0.01	0.00
13.69	2.00	0.00	0.00	0.01	0.00	13.70	2.00	0.00	0.00	0.01	0.00
13.71	2.00	0.00	0.00	0.01	0.00	13.72	2.00	0.00	0.00	0.01	0.00
13.73	2.00	0.00	0.00	0.01	0.00	13.74	2.00	0.00	0.00	0.01	0.00
13.75	2.00	0.00	0.00	0.01	0.00	13.76	2.00	0.00	0.00	0.01	0.00
13.77	2.00	0.00	0.00	0.01	0.00	13.78	2.00	0.00	0.00	0.01	0.00
13.79	2.00	0.00	0.00	0.01	0.00	13.80	2.00	0.00	0.00	0.01	0.00
13.81	2.00	0.00	0.00	0.01	0.00	13.82	2.00	0.00	0.00	0.01	0.00
13.83	2.00	0.00	0.00	0.01	0.00	13.84	2.00	0.00	0.00	0.01	0.00
13.85	2.00	0.00	0.00	0.01	0.00	13.86	2.00	0.00	0.00	0.01	0.00
13.87	2.00	0.00	0.00	0.01	0.00	13.88	2.00	0.00	0.00	0.01	0.00
13.89	2.00	0.00	0.00	0.01	0.00	13.90	2.00	0.00	0.00	0.01	0.00
13.91	2.00	0.00	0.00	0.01	0.00	13.92	2.00	0.00	0.00	0.01	0.00
13.93	2.00	0.00	0.00	0.01	0.00	13.94	2.00	0.00	0.00	0.01	0.00
13.95	2.00	0.00	0.00	0.01	0.00	13.96	2.00	0.00	0.00	0.01	0.00
13.97	2.00	0.00	0.00	0.01	0.00	13.98	2.00	0.00	0.00	0.01	0.00
13.99	2.00	0.00	0.00	0.01	0.00	14.00	2.00	0.00	0.00	0.01	0.00
14.01	2.00	0.00	0.00	0.01	0.00	14.02	2.00	0.00	0.00	0.01	0.00
14.03	2.00	0.00	0.00	0.01	0.00	14.04	2.00	0.00	0.00	0.01	0.00
14.05	2.00	0.00	0.00	0.01	0.00	14.06	2.00	0.00	0.00	0.01	0.00
14.07	2.00	0.00	0.00	0.01	0.00	14.08	2.00	0.00	0.00	0.01	0.00
14.09	2.00	0.00	0.00	0.01	0.00	14.10	2.00	0.00	0.00	0.01	0.00
14.11	2.00	0.00	0.00	0.01	0.00	14.12	2.00	0.00	0.00	0.01	0.00
14.13	2.00	0.00	0.00	0.01	0.00	14.14	2.00	0.00	0.00	0.01	0.00
14.15	2.00	0.00	0.00	0.01	0.00	14.16	2.00	0.00	0.00	0.01	0.00
14.17	2.00	0.00	0.00	0.01	0.00	14.18	2.00	0.00	0.00	0.01	0.00
14.19	2.00	0.00	0.00	0.01	0.00	14.20	2.00	0.00	0.00	0.01	0.00
14.21	2.00	0.00	0.00	0.01	0.00	14.22	2.00	0.00	0.00	0.01	0.00
14.23	2.00	0.00	0.00	0.01	0.00	14.24	2.00	0.00	0.00	0.01	0.00
14.25	2.00	0.00	0.00	0.01	0.00	14.26	2.00	0.00	0.00	0.01	0.00
14.27	2.00	0.00	0.00	0.01	0.00	14.28	2.00	0.00	0.00	0.01	0.00
14.29	2.00	0.00	0.00	0.01	0.00	14.30	2.00	0.00	0.00	0.01	0.00
14.31	2.00	0.00	0.00	0.01	0.00	14.32	2.00	0.00	0.00	0.01	0.00
14.33	2.00	0.00	0.00	0.01	0.00	14.34	2.00	0.00	0.00	0.01	0.00
14.35	2.00	0.00	0.00	0.01	0.00	14.36	2.00	0.00	0.00	0.01	0.00
14.37	2.00	0.00	0.00	0.01	0.00	14.38	2.00	0.00	0.00	0.01	0.00
14.39	2.00	0.00	0.00	0.01	0.00	14.40	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
14.41	2.00	0.00	0.00	0.01	0.00	14.42	2.00	0.00	0.00	0.01	0.00
14.43	2.00	0.00	0.00	0.01	0.00	14.44	2.00	0.00	0.00	0.01	0.00
14.45	2.00	0.00	0.00	0.01	0.00	14.46	2.00	0.00	0.00	0.01	0.00
14.47	2.00	0.00	0.00	0.01	0.00	14.48	2.00	0.00	0.00	0.01	0.00
14.49	2.00	0.00	0.00	0.01	0.00	14.50	2.00	0.00	0.00	0.01	0.00
14.51	2.00	0.00	0.00	0.01	0.00	14.52	2.00	0.00	0.00	0.01	0.00
14.53	2.00	0.00	0.00	0.01	0.00	14.54	2.00	0.00	0.00	0.01	0.00
14.55	2.00	0.00	0.00	0.01	0.00	14.56	2.00	0.00	0.00	0.01	0.00
14.57	2.00	0.00	0.00	0.01	0.00	14.58	2.00	0.00	0.00	0.01	0.00
14.59	2.00	0.00	0.00	0.01	0.00	14.60	2.00	0.00	0.00	0.01	0.00
14.61	2.00	0.00	0.00	0.01	0.00	14.62	2.00	0.00	0.00	0.01	0.00
14.63	2.00	0.00	0.00	0.01	0.00	14.64	2.00	0.00	0.00	0.01	0.00
14.65	2.00	0.00	0.00	0.01	0.00	14.66	2.00	0.00	0.00	0.01	0.00
14.67	2.00	0.00	0.00	0.01	0.00	14.68	2.00	0.00	0.00	0.01	0.00
14.69	2.00	0.00	0.00	0.01	0.00	14.70	2.00	0.00	0.00	0.01	0.00
14.71	2.00	0.00	0.00	0.01	0.00	14.72	2.00	0.00	0.00	0.01	0.00
14.73	2.00	0.00	0.00	0.01	0.00	14.74	2.00	0.00	0.00	0.01	0.00
14.75	2.00	0.00	0.00	0.01	0.00	14.76	2.00	0.00	0.00	0.01	0.00
14.77	2.00	0.00	0.00	0.01	0.00	14.78	2.00	0.00	0.00	0.01	0.00
14.79	2.00	0.00	0.00	0.01	0.00	14.80	2.00	0.00	0.00	0.01	0.00
14.81	2.00	0.00	0.00	0.01	0.00	14.82	2.00	0.00	0.00	0.01	0.00
14.83	2.00	0.00	0.00	0.01	0.00	14.84	2.00	0.00	0.00	0.01	0.00
14.85	2.00	0.00	0.00	0.01	0.00	14.86	2.00	0.00	0.00	0.01	0.00
14.87	2.00	0.00	0.00	0.01	0.00	14.88	2.00	0.00	0.00	0.01	0.00
14.89	2.00	0.00	0.00	0.01	0.00	14.90	2.00	0.00	0.00	0.01	0.00
14.91	2.00	0.00	0.00	0.01	0.00	14.92	2.00	0.00	0.00	0.01	0.00
14.93	2.00	0.00	0.00	0.01	0.00	14.94	2.00	0.00	0.00	0.01	0.00
14.95	2.00	0.00	0.00	0.01	0.00	14.96	2.00	0.00	0.00	0.01	0.00
14.97	2.00	0.00	0.00	0.01	0.00	14.98	2.00	0.00	0.00	0.01	0.00
14.99	2.00	0.00	0.00	0.01	0.00	15.00	2.00	0.00	0.00	0.01	0.00
15.01	2.00	0.00	0.00	0.01	0.00	15.02	2.00	0.00	0.00	0.01	0.00
15.03	2.00	0.00	0.00	0.01	0.00	15.04	2.00	0.00	0.00	0.01	0.00
15.05	2.00	0.00	0.00	0.01	0.00	15.06	2.00	0.00	0.00	0.01	0.00
15.07	2.00	0.00	0.00	0.01	0.00	15.08	2.00	0.00	0.00	0.01	0.00
15.09	2.00	0.00	0.00	0.01	0.00	15.10	2.00	0.00	0.00	0.01	0.00
15.11	2.00	0.00	0.00	0.01	0.00	15.12	2.00	0.00	0.00	0.01	0.00
15.13	2.00	0.00	0.00	0.01	0.00	15.14	2.00	0.00	0.00	0.01	0.00
15.15	2.00	0.00	0.00	0.01	0.00	15.16	2.00	0.00	0.00	0.01	0.00
15.17	2.00	0.00	0.00	0.01	0.00	15.18	2.00	0.00	0.00	0.01	0.00
15.19	2.00	0.00	0.00	0.01	0.00	15.20	2.00	0.00	0.00	0.01	0.00
15.21	2.00	0.00	0.00	0.01	0.00	15.22	2.00	0.00	0.00	0.01	0.00
15.23	2.00	0.00	0.00	0.01	0.00	15.24	2.00	0.00	0.00	0.01	0.00
15.25	2.00	0.00	0.00	0.01	0.00	15.26	2.00	0.00	0.00	0.01	0.00
15.27	2.00	0.00	0.00	0.01	0.00	15.28	2.00	0.00	0.00	0.01	0.00
15.29	2.00	0.00	0.00	0.01	0.00	15.30	2.00	0.00	0.00	0.01	0.00
15.31	2.00	0.00	0.00	0.01	0.00	15.32	2.00	0.00	0.00	0.01	0.00
15.33	2.00	0.00	0.00	0.01	0.00	15.34	2.00	0.00	0.00	0.01	0.00
15.35	2.00	0.00	0.00	0.01	0.00	15.36	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
15.37	2.00	0.00	0.00	0.01	0.00	15.38	2.00	0.00	0.00	0.01	0.00
15.39	2.00	0.00	0.00	0.01	0.00	15.40	2.00	0.00	0.00	0.01	0.00
15.41	2.00	0.00	0.00	0.01	0.00	15.42	2.00	0.00	0.00	0.01	0.00
15.43	2.00	0.00	0.00	0.01	0.00	15.44	2.00	0.00	0.00	0.01	0.00
15.45	2.00	0.00	0.00	0.01	0.00	15.46	2.00	0.00	0.00	0.01	0.00
15.47	2.00	0.00	0.00	0.01	0.00	15.48	2.00	0.00	0.00	0.01	0.00
15.49	2.00	0.00	0.00	0.01	0.00	15.50	2.00	0.00	0.00	0.01	0.00
15.51	2.00	0.00	0.00	0.01	0.00	15.52	2.00	0.00	0.00	0.01	0.00
15.53	2.00	0.00	0.00	0.01	0.00	15.54	2.00	0.00	0.00	0.01	0.00
15.55	2.00	0.00	0.00	0.01	0.00	15.56	2.00	0.00	0.00	0.01	0.00
15.57	2.00	0.00	0.00	0.01	0.00	15.58	2.00	0.00	0.00	0.01	0.00
15.59	2.00	0.00	0.00	0.01	0.00	15.60	2.00	0.00	0.00	0.01	0.00
15.61	2.00	0.00	0.00	0.01	0.00	15.62	2.00	0.00	0.00	0.01	0.00
15.63	2.00	0.00	0.00	0.01	0.00	15.64	2.00	0.00	0.00	0.01	0.00
15.65	2.00	0.00	0.00	0.01	0.00	15.66	2.00	0.00	0.00	0.01	0.00
15.67	2.00	0.00	0.00	0.01	0.00	15.68	2.00	0.00	0.00	0.01	0.00
15.69	2.00	0.00	0.00	0.01	0.00	15.70	2.00	0.00	0.00	0.01	0.00
15.71	2.00	0.00	0.00	0.01	0.00	15.72	2.00	0.00	0.00	0.01	0.00
15.73	2.00	0.00	0.00	0.01	0.00	15.74	2.00	0.00	0.00	0.01	0.00
15.75	2.00	0.00	0.00	0.01	0.00	15.76	2.00	0.00	0.00	0.01	0.00
15.77	2.00	0.00	0.00	0.01	0.00	15.78	2.00	0.00	0.00	0.01	0.00
15.79	2.00	0.00	0.00	0.01	0.00	15.80	2.00	0.00	0.00	0.01	0.00
15.81	2.00	0.00	0.00	0.01	0.00	15.82	2.00	0.00	0.00	0.01	0.00
15.83	2.00	0.00	0.00	0.01	0.00	15.84	2.00	0.00	0.00	0.01	0.00
15.85	2.00	0.00	0.00	0.01	0.00	15.86	2.00	0.00	0.00	0.01	0.00
15.87	2.00	0.00	0.00	0.01	0.00	15.88	2.00	0.00	0.00	0.01	0.00
15.89	2.00	0.00	0.00	0.01	0.00	15.90	2.00	0.00	0.00	0.01	0.00
15.91	2.00	0.00	0.00	0.01	0.00	15.92	2.00	0.00	0.00	0.01	0.00
15.93	2.00	0.00	0.00	0.01	0.00	15.94	2.00	0.00	0.00	0.01	0.00
15.95	2.00	0.00	0.00	0.01	0.00	15.96	2.00	0.00	0.00	0.01	0.00
15.97	2.00	0.00	0.00	0.01	0.00	15.98	2.00	0.00	0.00	0.01	0.00
15.99	2.00	0.00	0.00	0.01	0.00	16.00	2.00	0.00	0.00	0.01	0.00
16.01	2.00	0.00	0.00	0.01	0.00	16.02	2.00	0.00	0.00	0.01	0.00
16.03	2.00	0.00	0.00	0.01	0.00	16.04	2.00	0.00	0.00	0.01	0.00
16.05	2.00	0.00	0.00	0.01	0.00	16.06	2.00	0.00	0.00	0.01	0.00
16.07	2.00	0.00	0.00	0.01	0.00	16.08	2.00	0.00	0.00	0.01	0.00
16.09	2.00	0.00	0.00	0.01	0.00	16.10	2.00	0.00	0.00	0.01	0.00
16.11	2.00	0.00	0.00	0.01	0.00	16.12	2.00	0.00	0.00	0.01	0.00
16.13	2.00	0.00	0.00	0.01	0.00	16.14	2.00	0.00	0.00	0.01	0.00
16.15	2.00	0.00	0.00	0.01	0.00	16.16	2.00	0.00	0.00	0.01	0.00
16.17	2.00	0.00	0.00	0.01	0.00	16.18	2.00	0.00	0.00	0.01	0.00
16.19	2.00	0.00	0.00	0.01	0.00	16.20	2.00	0.00	0.00	0.01	0.00
16.21	2.00	0.00	0.00	0.01	0.00	16.22	2.00	0.00	0.00	0.01	0.00
16.23	2.00	0.00	0.00	0.01	0.00	16.24	2.00	0.00	0.00	0.01	0.00
16.25	2.00	0.00	0.00	0.01	0.00	16.26	2.00	0.00	0.00	0.01	0.00
16.27	2.00	0.00	0.00	0.01	0.00	16.28	2.00	0.00	0.00	0.01	0.00
16.29	2.00	0.00	0.00	0.01	0.00	16.30	2.00	0.00	0.00	0.01	0.00
16.31	2.00	0.00	0.00	0.01	0.00	16.32	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
16.33	2.00	0.00	0.00	0.01	0.00	16.34	2.00	0.00	0.00	0.01	0.00
16.35	2.00	0.00	0.00	0.01	0.00	16.36	2.00	0.00	0.00	0.01	0.00
16.37	2.00	0.00	0.00	0.01	0.00	16.38	2.00	0.00	0.00	0.01	0.00
16.39	2.00	0.00	0.00	0.01	0.00	16.40	2.00	0.00	0.00	0.01	0.00
16.41	2.00	0.00	0.00	0.01	0.00	16.42	2.00	0.00	0.00	0.01	0.00
16.43	2.00	0.00	0.00	0.01	0.00	16.44	2.00	0.00	0.00	0.01	0.00
16.45	2.00	0.00	0.00	0.01	0.00	16.46	2.00	0.00	0.00	0.01	0.00
16.47	2.00	0.00	0.00	0.01	0.00	16.48	2.00	0.00	0.00	0.01	0.00
16.49	2.00	0.00	0.00	0.01	0.00	16.50	2.00	0.00	0.00	0.01	0.00
16.51	2.00	0.00	0.00	0.01	0.00	16.52	2.00	0.00	0.00	0.01	0.00
16.53	2.00	0.00	0.00	0.01	0.00	16.54	2.00	0.00	0.00	0.01	0.00
16.55	2.00	0.00	0.00	0.01	0.00	16.56	2.00	0.00	0.00	0.01	0.00
16.57	2.00	0.00	0.00	0.01	0.00	16.58	2.00	0.00	0.00	0.01	0.00
16.59	2.00	0.00	0.00	0.01	0.00	16.60	2.00	0.00	0.00	0.01	0.00
16.61	2.00	0.00	0.00	0.01	0.00	16.62	2.00	0.00	0.00	0.01	0.00
16.63	2.00	0.00	0.00	0.01	0.00	16.64	2.00	0.00	0.00	0.01	0.00
16.65	2.00	0.00	0.00	0.01	0.00	16.66	2.00	0.00	0.00	0.01	0.00
16.67	2.00	0.00	0.00	0.01	0.00	16.68	2.00	0.00	0.00	0.01	0.00
16.69	2.00	0.00	0.00	0.01	0.00	16.70	2.00	0.00	0.00	0.01	0.00
16.71	2.00	0.00	0.00	0.01	0.00	16.72	2.00	0.00	0.00	0.01	0.00
16.73	2.00	0.00	0.00	0.01	0.00	16.74	2.00	0.00	0.00	0.01	0.00
16.75	2.00	0.00	0.00	0.01	0.00	16.76	2.00	0.00	0.00	0.01	0.00
16.77	2.00	0.00	0.00	0.01	0.00	16.78	2.00	0.00	0.00	0.01	0.00
16.79	2.00	0.00	0.00	0.01	0.00	16.80	2.00	0.00	0.00	0.01	0.00
16.81	2.00	0.00	0.00	0.01	0.00	16.82	2.00	0.00	0.00	0.01	0.00
16.83	2.00	0.00	0.00	0.01	0.00	16.84	2.00	0.00	0.00	0.01	0.00
16.85	2.00	0.00	0.00	0.01	0.00	16.86	2.00	0.00	0.00	0.01	0.00
16.87	2.00	0.00	0.00	0.01	0.00	16.88	2.00	0.00	0.00	0.01	0.00
16.89	2.00	0.00	0.00	0.01	0.00	16.90	2.00	0.00	0.00	0.01	0.00
16.91	2.00	0.00	0.00	0.01	0.00	16.92	2.00	0.00	0.00	0.01	0.00
16.93	2.00	0.00	0.00	0.01	0.00	16.94	2.00	0.00	0.00	0.01	0.00
16.95	2.00	0.00	0.00	0.01	0.00	16.96	2.00	0.00	0.00	0.01	0.00
16.97	2.00	0.00	0.00	0.01	0.00	16.98	2.00	0.00	0.00	0.01	0.00
16.99	2.00	0.00	0.00	0.01	0.00	17.00	2.00	0.00	0.00	0.01	0.00
17.01	2.00	0.00	0.00	0.01	0.00	17.02	2.00	0.00	0.00	0.01	0.00
17.03	2.00	0.00	0.00	0.01	0.00	17.04	2.00	0.00	0.00	0.01	0.00
17.05	2.00	0.00	0.00	0.01	0.00	17.06	2.00	0.00	0.00	0.01	0.00
17.07	2.00	0.00	0.00	0.01	0.00	17.08	2.00	0.00	0.00	0.01	0.00
17.09	2.00	0.00	0.00	0.01	0.00	17.10	2.00	0.00	0.00	0.01	0.00
17.11	2.00	0.00	0.00	0.01	0.00	17.12	2.00	0.00	0.00	0.01	0.00
17.13	2.00	0.00	0.00	0.01	0.00	17.14	2.00	0.00	0.00	0.01	0.00
17.15	2.00	0.00	0.00	0.01	0.00	17.16	2.00	0.00	0.00	0.01	0.00
17.17	2.00	0.00	0.00	0.01	0.00	17.18	2.00	0.00	0.00	0.01	0.00
17.19	2.00	0.00	0.00	0.01	0.00	17.20	2.00	0.00	0.00	0.01	0.00
17.21	2.00	0.00	0.00	0.01	0.00	17.22	2.00	0.00	0.00	0.01	0.00
17.23	2.00	0.00	0.00	0.01	0.00	17.24	2.00	0.00	0.00	0.01	0.00
17.25	2.00	0.00	0.00	0.01	0.00	17.26	2.00	0.00	0.00	0.01	0.00
17.27	2.00	0.00	0.00	0.01	0.00	17.28	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
17.29	2.00	0.00	0.00	0.01	0.00	17.30	2.00	0.00	0.00	0.01	0.00
17.31	2.00	0.00	0.00	0.01	0.00	17.32	2.00	0.00	0.00	0.01	0.00
17.33	2.00	0.00	0.00	0.01	0.00	17.34	2.00	0.00	0.00	0.01	0.00
17.35	2.00	0.00	0.00	0.01	0.00	17.36	2.00	0.00	0.00	0.01	0.00
17.37	2.00	0.00	0.00	0.01	0.00	17.38	2.00	0.00	0.00	0.01	0.00
17.39	2.00	0.00	0.00	0.01	0.00	17.40	2.00	0.00	0.00	0.01	0.00
17.41	2.00	0.00	0.00	0.01	0.00	17.42	2.00	0.00	0.00	0.01	0.00
17.43	2.00	0.00	0.00	0.01	0.00	17.44	2.00	0.00	0.00	0.01	0.00
17.45	2.00	0.00	0.00	0.01	0.00	17.46	2.00	0.00	0.00	0.01	0.00
17.47	2.00	0.00	0.00	0.01	0.00	17.48	2.00	0.00	0.00	0.01	0.00
17.49	2.00	0.00	0.00	0.01	0.00	17.50	2.00	0.00	0.00	0.01	0.00
17.51	2.00	0.00	0.00	0.01	0.00	17.52	2.00	0.00	0.00	0.01	0.00
17.53	2.00	0.00	0.00	0.01	0.00	17.54	2.00	0.00	0.00	0.01	0.00
17.55	2.00	0.00	0.00	0.01	0.00	17.56	2.00	0.00	0.00	0.01	0.00
17.57	2.00	0.00	0.00	0.01	0.00	17.58	2.00	0.00	0.00	0.01	0.00
17.59	2.00	0.00	0.00	0.01	0.00	17.60	2.00	0.00	0.00	0.01	0.00
17.61	2.00	0.00	0.00	0.01	0.00	17.62	2.00	0.00	0.00	0.01	0.00
17.63	2.00	0.00	0.00	0.01	0.00	17.64	2.00	0.00	0.00	0.01	0.00
17.65	2.00	0.00	0.00	0.01	0.00	17.66	2.00	0.00	0.00	0.01	0.00
17.67	2.00	0.00	0.00	0.01	0.00	17.68	2.00	0.00	0.00	0.01	0.00
17.69	2.00	0.00	0.00	0.01	0.00	17.70	2.00	0.00	0.00	0.01	0.00
17.71	2.00	0.00	0.00	0.01	0.00	17.72	2.00	0.00	0.00	0.01	0.00
17.73	2.00	0.00	0.00	0.01	0.00	17.74	2.00	0.00	0.00	0.01	0.00
17.75	2.00	0.00	0.00	0.01	0.00	17.76	2.00	0.00	0.00	0.01	0.00
17.77	2.00	0.00	0.00	0.01	0.00	17.78	2.00	0.00	0.00	0.01	0.00
17.79	2.00	0.00	0.00	0.01	0.00	17.80	2.00	0.00	0.00	0.01	0.00
17.81	2.00	0.00	0.00	0.01	0.00	17.82	2.00	0.00	0.00	0.01	0.00
17.83	2.00	0.00	0.00	0.01	0.00	17.84	2.00	0.00	0.00	0.01	0.00
17.85	2.00	0.00	0.00	0.01	0.00	17.86	2.00	0.00	0.00	0.01	0.00
17.87	2.00	0.00	0.00	0.01	0.00	17.88	2.00	0.00	0.00	0.01	0.00
17.89	2.00	0.00	0.00	0.01	0.00	17.90	2.00	0.00	0.00	0.01	0.00
17.91	2.00	0.00	0.00	0.01	0.00	17.92	2.00	0.00	0.00	0.01	0.00
17.93	2.00	0.00	0.00	0.01	0.00	17.94	2.00	0.00	0.00	0.01	0.00
17.95	2.00	0.00	0.00	0.01	0.00	17.96	2.00	0.00	0.00	0.01	0.00
17.97	2.00	0.00	0.00	0.01	0.00	17.98	2.00	0.00	0.00	0.01	0.00
17.99	2.00	0.00	0.00	0.01	0.00	18.00	2.00	0.00	0.00	0.01	0.00
18.01	2.00	0.00	0.00	0.01	0.00	18.02	2.00	0.00	0.00	0.01	0.00
18.03	2.00	0.00	0.00	0.01	0.00	18.04	2.00	0.00	0.00	0.01	0.00
18.05	2.00	0.00	0.00	0.01	0.00	18.06	2.00	0.00	0.00	0.01	0.00
18.07	2.00	0.00	0.00	0.01	0.00	18.08	2.00	0.00	0.00	0.01	0.00
18.09	2.00	0.00	0.00	0.01	0.00	18.10	2.00	0.00	0.00	0.01	0.00
18.11	2.00	0.00	0.00	0.01	0.00	18.12	2.00	0.00	0.00	0.01	0.00
18.13	2.00	0.00	0.00	0.01	0.00	18.14	2.00	0.00	0.00	0.01	0.00
18.15	2.00	0.00	0.00	0.01	0.00	18.16	2.00	0.00	0.00	0.01	0.00
18.17	2.00	0.00	0.00	0.01	0.00	18.18	2.00	0.00	0.00	0.01	0.00
18.19	2.00	0.00	0.00	0.01	0.00	18.20	2.00	0.00	0.00	0.01	0.00
18.21	2.00	0.00	0.00	0.01	0.00	18.22	2.00	0.00	0.00	0.01	0.00
18.23	2.00	0.00	0.00	0.01	0.00	18.24	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
18.25	2.00	0.00	0.00	0.01	0.00	18.26	2.00	0.00	0.00	0.01	0.00
18.27	2.00	0.00	0.00	0.01	0.00	18.28	2.00	0.00	0.00	0.01	0.00
18.29	2.00	0.00	0.00	0.01	0.00	18.30	2.00	0.00	0.00	0.01	0.00
18.31	2.00	0.00	0.00	0.01	0.00	18.32	2.00	0.00	0.00	0.01	0.00
18.33	2.00	0.00	0.00	0.01	0.00	18.34	2.00	0.00	0.00	0.01	0.00
18.35	2.00	0.00	0.00	0.01	0.00	18.36	2.00	0.00	0.00	0.01	0.00
18.37	2.00	0.00	0.00	0.01	0.00	18.38	2.00	0.00	0.00	0.01	0.00
18.39	2.00	0.00	0.00	0.01	0.00	18.40	2.00	0.00	0.00	0.01	0.00
18.41	2.00	0.00	0.00	0.01	0.00	18.42	2.00	0.00	0.00	0.01	0.00
18.43	2.00	0.00	0.00	0.01	0.00	18.44	2.00	0.00	0.00	0.01	0.00
18.45	2.00	0.00	0.00	0.01	0.00	18.46	2.00	0.00	0.00	0.01	0.00
18.47	2.00	0.00	0.00	0.01	0.00	18.48	2.00	0.00	0.00	0.01	0.00
18.49	2.00	0.00	0.00	0.01	0.00	18.50	2.00	0.00	0.00	0.01	0.00
18.51	2.00	0.00	0.00	0.01	0.00	18.52	2.00	0.00	0.00	0.01	0.00
18.53	2.00	0.00	0.00	0.01	0.00	18.54	2.00	0.00	0.00	0.01	0.00
18.55	2.00	0.00	0.00	0.01	0.00	18.56	2.00	0.00	0.00	0.01	0.00
18.57	2.00	0.00	0.00	0.01	0.00	18.58	2.00	0.00	0.00	0.01	0.00
18.59	2.00	0.00	0.00	0.01	0.00	18.60	2.00	0.00	0.00	0.01	0.00
18.61	2.00	0.00	0.00	0.01	0.00	18.62	2.00	0.00	0.00	0.01	0.00
18.63	2.00	0.00	0.00	0.01	0.00	18.64	2.00	0.00	0.00	0.01	0.00
18.65	2.00	0.00	0.00	0.01	0.00	18.66	2.00	0.00	0.00	0.01	0.00
18.67	2.00	0.00	0.00	0.01	0.00	18.68	2.00	0.00	0.00	0.01	0.00
18.69	2.00	0.00	0.00	0.01	0.00	18.70	2.00	0.00	0.00	0.01	0.00
18.71	2.00	0.00	0.00	0.01	0.00	18.72	2.00	0.00	0.00	0.01	0.00
18.73	2.00	0.00	0.00	0.01	0.00	18.74	2.00	0.00	0.00	0.01	0.00
18.75	2.00	0.00	0.00	0.01	0.00	18.76	2.00	0.00	0.00	0.01	0.00
18.77	2.00	0.00	0.00	0.01	0.00	18.78	2.00	0.00	0.00	0.01	0.00
18.79	2.00	0.00	0.00	0.01	0.00	18.80	2.00	0.00	0.00	0.01	0.00
18.81	2.00	0.00	0.00	0.01	0.00	18.82	2.00	0.00	0.00	0.01	0.00
18.83	2.00	0.00	0.00	0.01	0.00	18.84	2.00	0.00	0.00	0.01	0.00
18.85	2.00	0.00	0.00	0.01	0.00	18.86	2.00	0.00	0.00	0.01	0.00
18.87	2.00	0.00	0.00	0.01	0.00	18.88	2.00	0.00	0.00	0.01	0.00
18.89	2.00	0.00	0.00	0.01	0.00	18.90	2.00	0.00	0.00	0.01	0.00
18.91	2.00	0.00	0.00	0.01	0.00	18.92	2.00	0.00	0.00	0.01	0.00
18.93	2.00	0.00	0.00	0.01	0.00	18.94	2.00	0.00	0.00	0.01	0.00
18.95	2.00	0.00	0.00	0.01	0.00	18.96	2.00	0.00	0.00	0.01	0.00
18.97	2.00	0.00	0.00	0.01	0.00	18.98	2.00	0.00	0.00	0.01	0.00
18.99	2.00	0.00	0.00	0.01	0.00	19.00	2.00	0.00	0.00	0.01	0.00
19.01	2.00	0.00	0.00	0.01	0.00	19.02	2.00	0.00	0.00	0.01	0.00
19.03	2.00	0.00	0.00	0.01	0.00	19.04	2.00	0.00	0.00	0.01	0.00
19.05	2.00	0.00	0.00	0.01	0.00	19.06	2.00	0.00	0.00	0.01	0.00
19.07	2.00	0.00	0.00	0.01	0.00	19.08	2.00	0.00	0.00	0.01	0.00
19.09	2.00	0.00	0.00	0.01	0.00	19.10	2.00	0.00	0.00	0.01	0.00
19.11	2.00	0.00	0.00	0.01	0.00	19.12	2.00	0.00	0.00	0.01	0.00
19.13	2.00	0.00	0.00	0.01	0.00	19.14	2.00	0.00	0.00	0.01	0.00
19.15	2.00	0.00	0.00	0.01	0.00	19.16	2.00	0.00	0.00	0.01	0.00
19.17	2.00	0.00	0.00	0.01	0.00	19.18	2.00	0.00	0.00	0.01	0.00
19.19	2.00	0.00	0.00	0.01	0.00	19.20	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
19.21	2.00	0.00	0.00	0.01	0.00	19.22	2.00	0.00	0.00	0.01	0.00
19.23	2.00	0.00	0.00	0.01	0.00	19.24	2.00	0.00	0.00	0.01	0.00
19.25	2.00	0.00	0.00	0.01	0.00	19.26	2.00	0.00	0.00	0.01	0.00
19.27	2.00	0.00	0.00	0.01	0.00	19.28	2.00	0.00	0.00	0.01	0.00
19.29	2.00	0.00	0.00	0.01	0.00	19.30	2.00	0.00	0.00	0.01	0.00
19.31	2.00	0.00	0.00	0.01	0.00	19.32	2.00	0.00	0.00	0.01	0.00
19.33	2.00	0.00	0.00	0.01	0.00	19.34	2.00	0.00	0.00	0.01	0.00
19.35	2.00	0.00	0.00	0.01	0.00	19.36	2.00	0.00	0.00	0.01	0.00
19.37	2.00	0.00	0.00	0.01	0.00	19.38	2.00	0.00	0.00	0.01	0.00
19.39	2.00	0.00	0.00	0.01	0.00	19.40	2.00	0.00	0.00	0.01	0.00
19.41	2.00	0.00	0.00	0.01	0.00	19.42	2.00	0.00	0.00	0.01	0.00
19.43	2.00	0.00	0.00	0.01	0.00	19.44	2.00	0.00	0.00	0.01	0.00
19.45	2.00	0.00	0.00	0.01	0.00	19.46	2.00	0.00	0.00	0.01	0.00
19.47	2.00	0.00	0.00	0.01	0.00	19.48	2.00	0.00	0.00	0.01	0.00
19.49	2.00	0.00	0.00	0.01	0.00	19.50	2.00	0.00	0.00	0.01	0.00
19.51	2.00	0.00	0.00	0.01	0.00	19.52	2.00	0.00	0.00	0.01	0.00
19.53	2.00	0.00	0.00	0.01	0.00	19.54	2.00	0.00	0.00	0.01	0.00
19.55	2.00	0.00	0.00	0.01	0.00	19.56	2.00	0.00	0.00	0.01	0.00
19.57	2.00	0.00	0.00	0.01	0.00	19.58	2.00	0.00	0.00	0.01	0.00
19.59	2.00	0.00	0.00	0.01	0.00	19.60	2.00	0.00	0.00	0.01	0.00
19.61	2.00	0.00	0.00	0.01	0.00	19.62	2.00	0.00	0.00	0.01	0.00
19.63	2.00	0.00	0.00	0.01	0.00	19.64	2.00	0.00	0.00	0.01	0.00
19.65	2.00	0.00	0.00	0.01	0.00	19.66	2.00	0.00	0.00	0.01	0.00
19.67	2.00	0.00	0.00	0.01	0.00	19.68	2.00	0.00	0.00	0.01	0.00
19.69	2.00	0.00	0.00	0.01	0.00	19.70	2.00	0.00	0.00	0.01	0.00
19.71	2.00	0.00	0.00	0.01	0.00	19.72	2.00	0.00	0.00	0.01	0.00
19.73	2.00	0.00	0.00	0.01	0.00	19.74	2.00	0.00	0.00	0.01	0.00
19.75	2.00	0.00	0.00	0.01	0.00	19.76	2.00	0.00	0.00	0.01	0.00
19.77	2.00	0.00	0.00	0.01	0.00	19.78	2.00	0.00	0.00	0.01	0.00
19.79	2.00	0.00	0.00	0.01	0.00	19.80	2.00	0.00	0.00	0.01	0.00
19.81	2.00	0.00	0.00	0.01	0.00	19.82	2.00	0.00	0.00	0.01	0.00
19.83	2.00	0.00	0.00	0.01	0.00	19.84	2.00	0.00	0.00	0.01	0.00
19.85	2.00	0.00	0.00	0.01	0.00	19.86	2.00	0.00	0.00	0.01	0.00
19.87	2.00	0.00	0.00	0.01	0.00	19.88	2.00	0.00	0.00	0.01	0.00
19.89	2.00	0.00	0.00	0.01	0.00	19.90	2.00	0.00	0.00	0.01	0.00
19.91	2.00	0.00	0.00	0.01	0.00	19.92	2.00	0.00	0.00	0.01	0.00
19.93	2.00	0.00	0.00	0.01	0.00	19.94	2.00	0.00	0.00	0.01	0.00
19.95	2.00	0.00	0.00	0.01	0.00	19.96	2.00	0.00	0.00	0.01	0.00
19.97	2.00	0.00	0.00	0.01	0.00	19.98	2.00	0.00	0.00	0.01	0.00
19.99	2.00	0.00	0.00	0.01	0.00	20.00	2.00	0.00	0.00	0.01	0.00
20.01	2.00	0.00	0.00	0.01	0.00	20.02	2.00	0.00	0.00	0.01	0.00
20.03	2.00	0.00	0.00	0.01	0.00	20.04	2.00	0.00	0.00	0.01	0.00
20.05	2.00	0.00	0.00	0.01	0.00	20.06	2.00	0.00	0.00	0.01	0.00
20.07	2.00	0.00	0.00	0.01	0.00	20.08	2.00	0.00	0.00	0.01	0.00
20.09	2.00	0.00	0.00	0.01	0.00	20.10	2.00	0.00	0.00	0.01	0.00
20.11	2.00	0.00	0.00	0.01	0.00	20.12	2.00	0.00	0.00	0.01	0.00
20.13	2.00	0.00	0.00	0.01	0.00	20.14	2.00	0.00	0.00	0.01	0.00
20.15	2.00	0.00	0.00	0.01	0.00	20.16	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
20.17	2.00	0.00	0.00	0.01	0.00	20.18	2.00	0.00	0.00	0.01	0.00
20.19	2.00	0.00	0.00	0.01	0.00	20.20	2.00	0.00	0.00	0.01	0.00
20.21	2.00	0.00	0.00	0.01	0.00	20.22	2.00	0.00	0.00	0.01	0.00
20.23	2.00	0.00	0.00	0.01	0.00	20.24	2.00	0.00	0.00	0.01	0.00
20.25	2.00	0.00	0.00	0.01	0.00	20.26	2.00	0.00	0.00	0.01	0.00
20.27	2.00	0.00	0.00	0.01	0.00	20.28	2.00	0.00	0.00	0.01	0.00
20.29	2.00	0.00	0.00	0.01	0.00	20.30	2.00	0.00	0.00	0.01	0.00
20.31	2.00	0.00	0.00	0.01	0.00	20.32	2.00	0.00	0.00	0.01	0.00
20.33	2.00	0.00	0.00	0.01	0.00	20.34	2.00	0.00	0.00	0.01	0.00
20.35	2.00	0.00	0.00	0.01	0.00	20.36	2.00	0.00	0.00	0.01	0.00
20.37	2.00	0.00	0.00	0.01	0.00	20.38	2.00	0.00	0.00	0.01	0.00
20.39	2.00	0.00	0.00	0.01	0.00	20.40	2.00	0.00	0.00	0.01	0.00
20.41	2.00	0.00	0.00	0.01	0.00	20.42	2.00	0.00	0.00	0.01	0.00
20.43	2.00	0.00	0.00	0.01	0.00	20.44	2.00	0.00	0.00	0.01	0.00
20.45	2.00	0.00	0.00	0.01	0.00	20.46	2.00	0.00	0.00	0.01	0.00
20.47	2.00	0.00	0.00	0.01	0.00	20.48	2.00	0.00	0.00	0.01	0.00
20.49	2.00	0.00	0.00	0.01	0.00	20.50	2.00	0.00	0.00	0.01	0.00
20.51	2.00	0.00	0.00	0.01	0.00	20.52	2.00	0.00	0.00	0.01	0.00
20.53	2.00	0.00	0.00	0.01	0.00	20.54	2.00	0.00	0.00	0.01	0.00
20.55	2.00	0.00	0.00	0.01	0.00	20.56	2.00	0.00	0.00	0.01	0.00
20.57	2.00	0.00	0.00	0.01	0.00	20.58	2.00	0.00	0.00	0.01	0.00
20.59	2.00	0.00	0.00	0.01	0.00	20.60	2.00	0.00	0.00	0.01	0.00
20.61	2.00	0.00	0.00	0.01	0.00	20.62	2.00	0.00	0.00	0.01	0.00
20.63	2.00	0.00	0.00	0.01	0.00	20.64	2.00	0.00	0.00	0.01	0.00
20.65	2.00	0.00	0.00	0.01	0.00	20.66	2.00	0.00	0.00	0.01	0.00
20.67	2.00	0.00	0.00	0.01	0.00	20.68	2.00	0.00	0.00	0.01	0.00
20.69	2.00	0.00	0.00	0.01	0.00	20.70	2.00	0.00	0.00	0.01	0.00
20.71	2.00	0.00	0.00	0.01	0.00	20.72	2.00	0.00	0.00	0.01	0.00
20.73	2.00	0.00	0.00	0.01	0.00	20.74	2.00	0.00	0.00	0.01	0.00
20.75	2.00	0.00	0.00	0.01	0.00	20.76	2.00	0.00	0.00	0.01	0.00
20.77	2.00	0.00	0.00	0.01	0.00	20.78	2.00	0.00	0.00	0.01	0.00
20.79	2.00	0.00	0.00	0.01	0.00	20.80	2.00	0.00	0.00	0.01	0.00
20.81	2.00	0.00	0.00	0.01	0.00	20.82	2.00	0.00	0.00	0.01	0.00
20.83	2.00	0.00	0.00	0.01	0.00	20.84	2.00	0.00	0.00	0.01	0.00
20.85	2.00	0.00	0.00	0.01	0.00	20.86	2.00	0.00	0.00	0.01	0.00
20.87	2.00	0.00	0.00	0.01	0.00	20.88	2.00	0.00	0.00	0.01	0.00
20.89	2.00	0.00	0.00	0.01	0.00	20.90	2.00	0.00	0.00	0.01	0.00
20.91	2.00	0.00	0.00	0.01	0.00	20.92	2.00	0.00	0.00	0.01	0.00
20.93	2.00	0.00	0.00	0.01	0.00	20.94	2.00	0.00	0.00	0.01	0.00
20.95	2.00	0.00	0.00	0.01	0.00	20.96	2.00	0.00	0.00	0.01	0.00
20.97	2.00	0.00	0.00	0.01	0.00	20.98	2.00	0.00	0.00	0.01	0.00
20.99	2.00	0.00	0.00	0.01	0.00	21.00	2.00	0.00	0.00	0.01	0.00
21.01	2.00	0.00	0.00	0.01	0.00	21.02	2.00	0.00	0.00	0.01	0.00
21.03	2.00	0.00	0.00	0.01	0.00	21.04	2.00	0.00	0.00	0.01	0.00
21.05	2.00	0.00	0.00	0.01	0.00	21.06	2.00	0.00	0.00	0.01	0.00
21.07	2.00	0.00	0.00	0.01	0.00	21.08	2.00	0.00	0.00	0.01	0.00
21.09	2.00	0.00	0.00	0.01	0.00	21.10	2.00	0.00	0.00	0.01	0.00
21.11	2.00	0.00	0.00	0.01	0.00	21.12	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
21.13	2.00	0.00	0.00	0.01	0.00	21.14	2.00	0.00	0.00	0.01	0.00
21.15	2.00	0.00	0.00	0.01	0.00	21.16	2.00	0.00	0.00	0.01	0.00
21.17	2.00	0.00	0.00	0.01	0.00	21.18	2.00	0.00	0.00	0.01	0.00
21.19	2.00	0.00	0.00	0.01	0.00	21.20	2.00	0.00	0.00	0.01	0.00
21.21	2.00	0.00	0.00	0.01	0.00	21.22	2.00	0.00	0.00	0.01	0.00
21.23	2.00	0.00	0.00	0.01	0.00	21.24	2.00	0.00	0.00	0.01	0.00
21.25	2.00	0.00	0.00	0.01	0.00	21.26	2.00	0.00	0.00	0.01	0.00
21.27	2.00	0.00	0.00	0.01	0.00	21.28	2.00	0.00	0.00	0.01	0.00
21.29	2.00	0.00	0.00	0.01	0.00	21.30	2.00	0.00	0.00	0.01	0.00
21.31	2.00	0.00	0.00	0.01	0.00	21.32	2.00	0.00	0.00	0.01	0.00
21.33	2.00	0.00	0.00	0.01	0.00	21.34	2.00	0.00	0.00	0.01	0.00
21.35	2.00	0.00	0.00	0.01	0.00	21.36	2.00	0.00	0.00	0.01	0.00
21.37	2.00	0.00	0.00	0.01	0.00	21.38	2.00	0.00	0.00	0.01	0.00
21.39	2.00	0.00	0.00	0.01	0.00	21.40	2.00	0.00	0.00	0.01	0.00
21.41	2.00	0.00	0.00	0.01	0.00	21.42	2.00	0.00	0.00	0.01	0.00
21.43	2.00	0.00	0.00	0.01	0.00	21.44	2.00	0.00	0.00	0.01	0.00
21.45	2.00	0.00	0.00	0.01	0.00	21.46	2.00	0.00	0.00	0.01	0.00
21.47	2.00	0.00	0.00	0.01	0.00	21.48	2.00	0.00	0.00	0.01	0.00
21.49	2.00	0.00	0.00	0.01	0.00	21.50	2.00	0.00	0.00	0.01	0.00
21.51	2.00	0.00	0.00	0.01	0.00	21.52	2.00	0.00	0.00	0.01	0.00
21.53	2.00	0.00	0.00	0.01	0.00	21.54	2.00	0.00	0.00	0.01	0.00
21.55	2.00	0.00	0.00	0.01	0.00	21.56	2.00	0.00	0.00	0.01	0.00
21.57	2.00	0.00	0.00	0.01	0.00	21.58	2.00	0.00	0.00	0.01	0.00
21.59	2.00	0.00	0.00	0.01	0.00	21.60	2.00	0.00	0.00	0.01	0.00
21.61	2.00	0.00	0.00	0.01	0.00	21.62	2.00	0.00	0.00	0.01	0.00
21.63	2.00	0.00	0.00	0.01	0.00	21.64	2.00	0.00	0.00	0.01	0.00
21.65	2.00	0.00	0.00	0.01	0.00	21.66	2.00	0.00	0.00	0.01	0.00
21.67	2.00	0.00	0.00	0.01	0.00	21.68	2.00	0.00	0.00	0.01	0.00
21.69	2.00	0.00	0.00	0.01	0.00	21.70	2.00	0.00	0.00	0.01	0.00
21.71	2.00	0.00	0.00	0.01	0.00	21.72	2.00	0.00	0.00	0.01	0.00
21.73	2.00	0.00	0.00	0.01	0.00	21.74	2.00	0.00	0.00	0.01	0.00
21.75	2.00	0.00	0.00	0.01	0.00	21.76	2.00	0.00	0.00	0.01	0.00
21.77	2.00	0.00	0.00	0.01	0.00	21.78	2.00	0.00	0.00	0.01	0.00
21.79	2.00	0.00	0.00	0.01	0.00	21.80	2.00	0.00	0.00	0.01	0.00
21.81	2.00	0.00	0.00	0.01	0.00	21.82	2.00	0.00	0.00	0.01	0.00
21.83	2.00	0.00	0.00	0.01	0.00	21.84	2.00	0.00	0.00	0.01	0.00
21.85	2.00	0.00	0.00	0.01	0.00	21.86	2.00	0.00	0.00	0.01	0.00
21.87	2.00	0.00	0.00	0.01	0.00	21.88	2.00	0.00	0.00	0.01	0.00
21.89	2.00	0.00	0.00	0.01	0.00	21.90	2.00	0.00	0.00	0.01	0.00
21.91	2.00	0.00	0.00	0.01	0.00	21.92	2.00	0.00	0.00	0.01	0.00
21.93	2.00	0.00	0.00	0.01	0.00	21.94	2.00	0.00	0.00	0.01	0.00
21.95	2.00	0.00	0.00	0.01	0.00	21.96	2.00	0.00	0.00	0.01	0.00
21.97	2.00	0.00	0.00	0.01	0.00	21.98	2.00	0.00	0.00	0.01	0.00
21.99	2.00	0.00	0.00	0.01	0.00	22.00	2.00	0.00	0.00	0.01	0.00
22.01	2.00	0.00	0.00	0.01	0.00	22.02	2.00	0.00	0.00	0.01	0.00
22.03	2.00	0.00	0.00	0.01	0.00	22.04	2.00	0.00	0.00	0.01	0.00
22.05	2.00	0.00	0.00	0.01	0.00	22.06	2.00	0.00	0.00	0.01	0.00
22.07	2.00	0.00	0.00	0.01	0.00	22.08	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
22.09	2.00	0.00	0.00	0.01	0.00	22.10	2.00	0.00	0.00	0.01	0.00
22.11	2.00	0.00	0.00	0.01	0.00	22.12	2.00	0.00	0.00	0.01	0.00
22.13	2.00	0.00	0.00	0.01	0.00	22.14	2.00	0.00	0.00	0.01	0.00
22.15	2.00	0.00	0.00	0.01	0.00	22.16	2.00	0.00	0.00	0.01	0.00
22.17	2.00	0.00	0.00	0.01	0.00	22.18	2.00	0.00	0.00	0.01	0.00
22.19	2.00	0.00	0.00	0.01	0.00	22.20	2.00	0.00	0.00	0.01	0.00
22.21	2.00	0.00	0.00	0.01	0.00	22.22	2.00	0.00	0.00	0.01	0.00
22.23	2.00	0.00	0.00	0.01	0.00	22.24	2.00	0.00	0.00	0.01	0.00
22.25	2.00	0.00	0.00	0.01	0.00	22.26	2.00	0.00	0.00	0.01	0.00
22.27	2.00	0.00	0.00	0.01	0.00	22.28	2.00	0.00	0.00	0.01	0.00
22.29	2.00	0.00	0.00	0.01	0.00	22.30	2.00	0.00	0.00	0.01	0.00
22.31	2.00	0.00	0.00	0.01	0.00	22.32	2.00	0.00	0.00	0.01	0.00
22.33	2.00	0.00	0.00	0.01	0.00	22.34	2.00	0.00	0.00	0.01	0.00
22.35	2.00	0.00	0.00	0.01	0.00	22.36	2.00	0.00	0.00	0.01	0.00
22.37	2.00	0.00	0.00	0.01	0.00	22.38	2.00	0.00	0.00	0.01	0.00
22.39	2.00	0.00	0.00	0.01	0.00	22.40	2.00	0.00	0.00	0.01	0.00
22.41	2.00	0.00	0.00	0.01	0.00	22.42	2.00	0.00	0.00	0.01	0.00
22.43	2.00	0.00	0.00	0.01	0.00	22.44	2.00	0.00	0.00	0.01	0.00
22.45	2.00	0.00	0.00	0.01	0.00	22.46	2.00	0.00	0.00	0.01	0.00
22.47	2.00	0.00	0.00	0.01	0.00	22.48	2.00	0.00	0.00	0.01	0.00
22.49	2.00	0.00	0.00	0.01	0.00	22.50	2.00	0.00	0.00	0.01	0.00
22.51	2.00	0.00	0.00	0.01	0.00	22.52	2.00	0.00	0.00	0.01	0.00
22.53	2.00	0.00	0.00	0.01	0.00	22.54	2.00	0.00	0.00	0.01	0.00
22.55	2.00	0.00	0.00	0.01	0.00	22.56	2.00	0.00	0.00	0.01	0.00
22.57	2.00	0.00	0.00	0.01	0.00	22.58	2.00	0.00	0.00	0.01	0.00
22.59	2.00	0.00	0.00	0.01	0.00	22.60	2.00	0.00	0.00	0.01	0.00
22.61	2.00	0.00	0.00	0.01	0.00	22.62	2.00	0.00	0.00	0.01	0.00
22.63	2.00	0.00	0.00	0.01	0.00	22.64	2.00	0.00	0.00	0.01	0.00
22.65	2.00	0.00	0.00	0.01	0.00	22.66	2.00	0.00	0.00	0.01	0.00
22.67	2.00	0.00	0.00	0.01	0.00	22.68	2.00	0.00	0.00	0.01	0.00
22.69	2.00	0.00	0.00	0.01	0.00	22.70	2.00	0.00	0.00	0.01	0.00
22.71	2.00	0.00	0.00	0.01	0.00	22.72	2.00	0.00	0.00	0.01	0.00
22.73	2.00	0.00	0.00	0.01	0.00	22.74	2.00	0.00	0.00	0.01	0.00
22.75	2.00	0.00	0.00	0.01	0.00	22.76	2.00	0.00	0.00	0.01	0.00
22.77	2.00	0.00	0.00	0.01	0.00	22.78	2.00	0.00	0.00	0.01	0.00
22.79	2.00	0.00	0.00	0.01	0.00	22.80	2.00	0.00	0.00	0.01	0.00
22.81	2.00	0.00	0.00	0.01	0.00	22.82	2.00	0.00	0.00	0.01	0.00
22.83	2.00	0.00	0.00	0.01	0.00	22.84	2.00	0.00	0.00	0.01	0.00
22.85	2.00	0.00	0.00	0.01	0.00	22.86	2.00	0.00	0.00	0.01	0.00
22.87	2.00	0.00	0.00	0.01	0.00	22.88	2.00	0.00	0.00	0.01	0.00
22.89	2.00	0.00	0.00	0.01	0.00	22.90	2.00	0.00	0.00	0.01	0.00
22.91	2.00	0.00	0.00	0.01	0.00	22.92	2.00	0.00	0.00	0.01	0.00
22.93	2.00	0.00	0.00	0.01	0.00	22.94	2.00	0.00	0.00	0.01	0.00
22.95	2.00	0.00	0.00	0.01	0.00	22.96	2.00	0.00	0.00	0.01	0.00
22.97	2.00	0.00	0.00	0.01	0.00	22.98	2.00	0.00	0.00	0.01	0.00
22.99	2.00	0.00	0.00	0.01	0.00	23.00	2.00	0.00	0.00	0.01	0.00
23.01	2.00	0.00	0.00	0.01	0.00	23.02	2.00	0.00	0.00	0.01	0.00
23.03	2.00	0.00	0.00	0.01	0.00	23.04	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
23.05	2.00	0.00	0.00	0.01	0.00	23.06	2.00	0.00	0.00	0.01	0.00
23.07	2.00	0.00	0.00	0.01	0.00	23.08	2.00	0.00	0.00	0.01	0.00
23.09	2.00	0.00	0.00	0.01	0.00	23.10	2.00	0.00	0.00	0.01	0.00
23.11	2.00	0.00	0.00	0.01	0.00	23.12	2.00	0.00	0.00	0.01	0.00
23.13	2.00	0.00	0.00	0.01	0.00	23.14	2.00	0.00	0.00	0.01	0.00
23.15	2.00	0.00	0.00	0.01	0.00	23.16	2.00	0.00	0.00	0.01	0.00
23.17	2.00	0.00	0.00	0.01	0.00	23.18	2.00	0.00	0.00	0.01	0.00
23.19	2.00	0.00	0.00	0.01	0.00	23.20	2.00	0.00	0.00	0.01	0.00
23.21	2.00	0.00	0.00	0.01	0.00	23.22	2.00	0.00	0.00	0.01	0.00
23.23	2.00	0.00	0.00	0.01	0.00	23.24	2.00	0.00	0.00	0.01	0.00
23.25	2.00	0.00	0.00	0.01	0.00	23.26	2.00	0.00	0.00	0.01	0.00
23.27	2.00	0.00	0.00	0.01	0.00	23.28	2.00	0.00	0.00	0.01	0.00
23.29	2.00	0.00	0.00	0.01	0.00	23.30	2.00	0.00	0.00	0.01	0.00
23.31	2.00	0.00	0.00	0.01	0.00	23.32	2.00	0.00	0.00	0.01	0.00
23.33	2.00	0.00	0.00	0.01	0.00	23.34	2.00	0.00	0.00	0.01	0.00
23.35	2.00	0.00	0.00	0.01	0.00	23.36	2.00	0.00	0.00	0.01	0.00
23.37	2.00	0.00	0.00	0.01	0.00	23.38	2.00	0.00	0.00	0.01	0.00
23.39	2.00	0.00	0.00	0.01	0.00	23.40	2.00	0.00	0.00	0.01	0.00
23.41	2.00	0.00	0.00	0.01	0.00	23.42	2.00	0.00	0.00	0.01	0.00
23.43	2.00	0.00	0.00	0.01	0.00	23.44	2.00	0.00	0.00	0.01	0.00
23.45	2.00	0.00	0.00	0.01	0.00	23.46	2.00	0.00	0.00	0.01	0.00
23.47	2.00	0.00	0.00	0.01	0.00	23.48	2.00	0.00	0.00	0.01	0.00
23.49	2.00	0.00	0.00	0.01	0.00	23.50	2.00	0.00	0.00	0.01	0.00
23.51	2.00	0.00	0.00	0.01	0.00	23.52	2.00	0.00	0.00	0.01	0.00
23.53	2.00	0.00	0.00	0.01	0.00	23.54	2.00	0.00	0.00	0.01	0.00
23.55	2.00	0.00	0.00	0.01	0.00	23.56	2.00	0.00	0.00	0.01	0.00
23.57	2.00	0.00	0.00	0.01	0.00	23.58	2.00	0.00	0.00	0.01	0.00
23.59	2.00	0.00	0.00	0.01	0.00	23.60	2.00	0.00	0.00	0.01	0.00
23.61	2.00	0.00	0.00	0.01	0.00	23.62	2.00	0.00	0.00	0.01	0.00
23.63	2.00	0.00	0.00	0.01	0.00	23.64	2.00	0.00	0.00	0.01	0.00
23.65	2.00	0.00	0.00	0.01	0.00	23.66	2.00	0.00	0.00	0.01	0.00
23.67	2.00	0.00	0.00	0.01	0.00	23.68	2.00	0.00	0.00	0.01	0.00
23.69	2.00	0.00	0.00	0.01	0.00	23.70	2.00	0.00	0.00	0.01	0.00
23.71	2.00	0.00	0.00	0.01	0.00	23.72	2.00	0.00	0.00	0.01	0.00
23.73	2.00	0.00	0.00	0.01	0.00	23.74	2.00	0.00	0.00	0.01	0.00
23.75	2.00	0.00	0.00	0.01	0.00	23.76	2.00	0.00	0.00	0.01	0.00
23.77	2.00	0.00	0.00	0.01	0.00	23.78	2.00	0.00	0.00	0.01	0.00
23.79	2.00	0.00	0.00	0.01	0.00	23.80	2.00	0.00	0.00	0.01	0.00
23.81	2.00	0.00	0.00	0.01	0.00	23.82	2.00	0.00	0.00	0.01	0.00
23.83	2.00	0.00	0.00	0.01	0.00	23.84	2.00	0.00	0.00	0.01	0.00
23.85	2.00	0.00	0.00	0.01	0.00	23.86	2.00	0.00	0.00	0.01	0.00
23.87	2.00	0.00	0.00	0.01	0.00	23.88	2.00	0.00	0.00	0.01	0.00
23.89	2.00	0.00	0.00	0.01	0.00	23.90	2.00	0.00	0.00	0.01	0.00
23.91	2.00	0.00	0.00	0.01	0.00	23.92	2.00	0.00	0.00	0.01	0.00
23.93	2.00	0.00	0.00	0.01	0.00	23.94	2.00	0.00	0.00	0.01	0.00
23.95	2.00	0.00	0.00	0.01	0.00	23.96	2.00	0.00	0.00	0.01	0.00
23.97	2.00	0.00	0.00	0.01	0.00	23.98	2.00	0.00	0.00	0.01	0.00
23.99	2.00	0.00	0.00	0.01	0.00	24.00	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
24.01	2.00	0.00	0.00	0.01	0.00	24.02	2.00	0.00	0.00	0.01	0.00
24.03	2.00	0.00	0.00	0.01	0.00	24.04	2.00	0.00	0.00	0.01	0.00
24.05	2.00	0.00	0.00	0.01	0.00	24.06	2.00	0.00	0.00	0.01	0.00
24.07	2.00	0.00	0.00	0.01	0.00	24.08	2.00	0.00	0.00	0.01	0.00
24.09	2.00	0.00	0.00	0.01	0.00	24.10	2.00	0.00	0.00	0.01	0.00
24.11	2.00	0.00	0.00	0.01	0.00	24.12	2.00	0.00	0.00	0.01	0.00
24.13	2.00	0.00	0.00	0.01	0.00	24.14	2.00	0.00	0.00	0.01	0.00
24.15	2.00	0.00	0.00	0.01	0.00	24.16	2.00	0.00	0.00	0.01	0.00
24.17	2.00	0.00	0.00	0.01	0.00	24.18	2.00	0.00	0.00	0.01	0.00
24.19	2.00	0.00	0.00	0.01	0.00	24.20	2.00	0.00	0.00	0.01	0.00
24.21	2.00	0.00	0.00	0.01	0.00	24.22	2.00	0.00	0.00	0.01	0.00
24.23	2.00	0.00	0.00	0.01	0.00	24.24	2.00	0.00	0.00	0.01	0.00
24.25	2.00	0.00	0.00	0.01	0.00	24.26	2.00	0.00	0.00	0.01	0.00
24.27	2.00	0.00	0.00	0.01	0.00	24.28	2.00	0.00	0.00	0.01	0.00
24.29	2.00	0.00	0.00	0.01	0.00	24.30	2.00	0.00	0.00	0.01	0.00
24.31	2.00	0.00	0.00	0.01	0.00	24.32	2.00	0.00	0.00	0.01	0.00
24.33	2.00	0.00	0.00	0.01	0.00	24.34	2.00	0.00	0.00	0.01	0.00
24.35	2.00	0.00	0.00	0.01	0.00	24.36	2.00	0.00	0.00	0.01	0.00
24.37	2.00	0.00	0.00	0.01	0.00	24.38	2.00	0.00	0.00	0.01	0.00
24.39	2.00	0.00	0.00	0.01	0.00	24.40	2.00	0.00	0.00	0.01	0.00
24.41	2.00	0.00	0.00	0.01	0.00	24.42	2.00	0.00	0.00	0.01	0.00
24.43	2.00	0.00	0.00	0.01	0.00	24.44	2.00	0.00	0.00	0.01	0.00
24.45	2.00	0.00	0.00	0.01	0.00	24.46	2.00	0.00	0.00	0.01	0.00
24.47	2.00	0.00	0.00	0.01	0.00	24.48	2.00	0.00	0.00	0.01	0.00
24.49	2.00	0.00	0.00	0.01	0.00	24.50	2.00	0.00	0.00	0.01	0.00
24.51	2.00	0.00	0.00	0.01	0.00	24.52	2.00	0.00	0.00	0.01	0.00
24.53	2.00	0.00	0.00	0.01	0.00	24.54	2.00	0.00	0.00	0.01	0.00
24.55	2.00	0.00	0.00	0.01	0.00	24.56	2.00	0.00	0.00	0.01	0.00
24.57	2.00	0.00	0.00	0.01	0.00	24.58	2.00	0.00	0.00	0.01	0.00
24.59	2.00	0.00	0.00	0.01	0.00	24.60	2.00	0.00	0.00	0.01	0.00
24.61	2.00	0.00	0.00	0.01	0.00	24.62	2.00	0.00	0.00	0.01	0.00
24.63	2.00	0.00	0.00	0.01	0.00	24.64	2.00	0.00	0.00	0.01	0.00
24.65	2.00	0.00	0.00	0.01	0.00	24.66	2.00	0.00	0.00	0.01	0.00
24.67	2.00	0.00	0.00	0.01	0.00	24.68	2.00	0.00	0.00	0.01	0.00
24.69	2.00	0.00	0.00	0.01	0.00	24.70	2.00	0.00	0.00	0.01	0.00
24.71	2.00	0.00	0.00	0.01	0.00	24.72	2.00	0.00	0.00	0.01	0.00
24.73	2.00	0.00	0.00	0.01	0.00	24.74	2.00	0.00	0.00	0.01	0.00
24.75	2.00	0.00	0.00	0.01	0.00	24.76	2.00	0.00	0.00	0.01	0.00
24.77	2.00	0.00	0.00	0.01	0.00	24.78	2.00	0.00	0.00	0.01	0.00
24.79	2.00	0.00	0.00	0.01	0.00	24.80	2.00	0.00	0.00	0.01	0.00
24.81	2.00	0.00	0.00	0.01	0.00	24.82	2.00	0.00	0.00	0.01	0.00
24.83	2.00	0.00	0.00	0.01	0.00	24.84	2.00	0.00	0.00	0.01	0.00
24.85	2.00	0.00	0.00	0.01	0.00	24.86	2.00	0.00	0.00	0.01	0.00
24.87	2.00	0.00	0.00	0.01	0.00	24.88	2.00	0.00	0.00	0.01	0.00
24.89	2.00	0.00	0.00	0.01	0.00	24.90	2.00	0.00	0.00	0.01	0.00
24.91	2.00	0.00	0.00	0.01	0.00	24.92	2.00	0.00	0.00	0.01	0.00
24.93	2.00	0.00	0.00	0.01	0.00	24.94	2.00	0.00	0.00	0.01	0.00
24.95	2.00	0.00	0.00	0.01	0.00	24.96	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
24.97	2.00	0.00	0.00	0.01	0.00	24.98	2.00	0.00	0.00	0.01	0.00
24.99	2.00	0.00	0.00	0.01	0.00	25.00	2.00	0.00	0.00	0.01	0.00
25.01	2.00	0.00	0.00	0.01	0.00	25.02	2.00	0.00	0.00	0.01	0.00
25.03	2.00	0.00	0.00	0.01	0.00	25.04	2.00	0.00	0.00	0.01	0.00
25.05	2.00	0.00	0.00	0.01	0.00	25.06	2.00	0.00	0.00	0.01	0.00
25.07	2.00	0.00	0.00	0.01	0.00	25.08	2.00	0.00	0.00	0.01	0.00
25.09	2.00	0.00	0.00	0.01	0.00	25.10	2.00	0.00	0.00	0.01	0.00
25.11	2.00	0.00	0.00	0.01	0.00	25.12	2.00	0.00	0.00	0.01	0.00
25.13	2.00	0.00	0.00	0.01	0.00	25.14	2.00	0.00	0.00	0.01	0.00
25.15	2.00	0.00	0.00	0.01	0.00	25.16	2.00	0.00	0.00	0.01	0.00
25.17	2.00	0.00	0.00	0.01	0.00	25.18	2.00	0.00	0.00	0.01	0.00
25.19	2.00	0.00	0.00	0.01	0.00	25.20	2.00	0.00	0.00	0.01	0.00
25.21	2.00	0.00	0.00	0.01	0.00	25.22	2.00	0.00	0.00	0.01	0.00
25.23	2.00	0.00	0.00	0.01	0.00	25.24	2.00	0.00	0.00	0.01	0.00
25.25	2.00	0.00	0.00	0.01	0.00	25.26	2.00	0.00	0.00	0.01	0.00
25.27	2.00	0.00	0.00	0.01	0.00	25.28	2.00	0.00	0.00	0.01	0.00
25.29	2.00	0.00	0.00	0.01	0.00	25.30	2.00	0.00	0.00	0.01	0.00
25.31	2.00	0.00	0.00	0.01	0.00	25.32	2.00	0.00	0.00	0.01	0.00
25.33	2.00	0.00	0.00	0.01	0.00	25.34	2.00	0.00	0.00	0.01	0.00
25.35	2.00	0.00	0.00	0.01	0.00	25.36	2.00	0.00	0.00	0.01	0.00
25.37	2.00	0.00	0.00	0.01	0.00	25.38	2.00	0.00	0.00	0.01	0.00
25.39	2.00	0.00	0.00	0.01	0.00	25.40	2.00	0.00	0.00	0.01	0.00
25.41	2.00	0.00	0.00	0.01	0.00	25.42	2.00	0.00	0.00	0.01	0.00
25.43	2.00	0.00	0.00	0.01	0.00	25.44	2.00	0.00	0.00	0.01	0.00
25.45	2.00	0.00	0.00	0.01	0.00	25.46	2.00	0.00	0.00	0.01	0.00
25.47	2.00	0.00	0.00	0.01	0.00	25.48	2.00	0.00	0.00	0.01	0.00
25.49	2.00	0.00	0.00	0.01	0.00	25.50	2.00	0.00	0.00	0.01	0.00
25.51	2.00	0.00	0.00	0.01	0.00	25.52	2.00	0.00	0.00	0.01	0.00
25.53	2.00	0.00	0.00	0.01	0.00	25.54	2.00	0.00	0.00	0.01	0.00
25.55	2.00	0.00	0.00	0.01	0.00	25.56	2.00	0.00	0.00	0.01	0.00
25.57	2.00	0.00	0.00	0.01	0.00	25.58	2.00	0.00	0.00	0.01	0.00
25.59	2.00	0.00	0.00	0.01	0.00	25.60	2.00	0.00	0.00	0.01	0.00
25.61	2.00	0.00	0.00	0.01	0.00	25.62	2.00	0.00	0.00	0.01	0.00
25.63	2.00	0.00	0.00	0.01	0.00	25.64	2.00	0.00	0.00	0.01	0.00
25.65	2.00	0.00	0.00	0.01	0.00	25.66	2.00	0.00	0.00	0.01	0.00
25.67	2.00	0.00	0.00	0.01	0.00	25.68	2.00	0.00	0.00	0.01	0.00
25.69	2.00	0.00	0.00	0.01	0.00	25.70	2.00	0.00	0.00	0.01	0.00
25.71	2.00	0.00	0.00	0.01	0.00	25.72	2.00	0.00	0.00	0.01	0.00
25.73	2.00	0.00	0.00	0.01	0.00	25.74	2.00	0.00	0.00	0.01	0.00
25.75	2.00	0.00	0.00	0.01	0.00	25.76	2.00	0.00	0.00	0.01	0.00
25.77	2.00	0.00	0.00	0.01	0.00	25.78	2.00	0.00	0.00	0.01	0.00
25.79	2.00	0.00	0.00	0.01	0.00	25.80	2.00	0.00	0.00	0.01	0.00
25.81	2.00	0.00	0.00	0.01	0.00	25.82	2.00	0.00	0.00	0.01	0.00
25.83	2.00	0.00	0.00	0.01	0.00	25.84	2.00	0.00	0.00	0.01	0.00
25.85	2.00	0.00	0.00	0.01	0.00	25.86	2.00	0.00	0.00	0.01	0.00
25.87	2.00	0.00	0.00	0.01	0.00	25.88	2.00	0.00	0.00	0.01	0.00
25.89	2.00	0.00	0.00	0.01	0.00	25.90	2.00	0.00	0.00	0.01	0.00
25.91	2.00	0.00	0.00	0.01	0.00	25.92	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
25.93	2.00	0.00	0.00	0.01	0.00	25.94	2.00	0.00	0.00	0.01	0.00
25.95	2.00	0.00	0.00	0.01	0.00	25.96	2.00	0.00	0.00	0.01	0.00
25.97	2.00	0.00	0.00	0.01	0.00	25.98	2.00	0.00	0.00	0.01	0.00
25.99	2.00	0.00	0.00	0.01	0.00	26.00	2.00	0.00	0.00	0.01	0.00
26.01	2.00	0.00	0.00	0.01	0.00	26.02	2.00	0.00	0.00	0.01	0.00
26.03	2.00	0.00	0.00	0.01	0.00	26.04	2.00	0.00	0.00	0.01	0.00
26.05	2.00	0.00	0.00	0.01	0.00	26.06	2.00	0.00	0.00	0.01	0.00
26.07	2.00	0.00	0.00	0.01	0.00	26.08	2.00	0.00	0.00	0.01	0.00
26.09	2.00	0.00	0.00	0.01	0.00	26.10	2.00	0.00	0.00	0.01	0.00
26.11	2.00	0.00	0.00	0.01	0.00	26.12	2.00	0.00	0.00	0.01	0.00
26.13	2.00	0.00	0.00	0.01	0.00	26.14	2.00	0.00	0.00	0.01	0.00
26.15	2.00	0.00	0.00	0.01	0.00	26.16	2.00	0.00	0.00	0.01	0.00
26.17	2.00	0.00	0.00	0.01	0.00	26.18	2.00	0.00	0.00	0.01	0.00
26.19	2.00	0.00	0.00	0.01	0.00	26.20	2.00	0.00	0.00	0.01	0.00
26.21	2.00	0.00	0.00	0.01	0.00	26.22	2.00	0.00	0.00	0.01	0.00
26.23	2.00	0.00	0.00	0.01	0.00	26.24	2.00	0.00	0.00	0.01	0.00
26.25	2.00	0.00	0.00	0.01	0.00	26.26	2.00	0.00	0.00	0.01	0.00
26.27	2.00	0.00	0.00	0.01	0.00	26.28	2.00	0.00	0.00	0.01	0.00
26.29	2.00	0.00	0.00	0.01	0.00	26.30	2.00	0.00	0.00	0.01	0.00
26.31	2.00	0.00	0.00	0.01	0.00	26.32	2.00	0.00	0.00	0.01	0.00
26.33	2.00	0.00	0.00	0.01	0.00	26.34	2.00	0.00	0.00	0.01	0.00
26.35	2.00	0.00	0.00	0.01	0.00	26.36	2.00	0.00	0.00	0.01	0.00
26.37	2.00	0.00	0.00	0.01	0.00	26.38	2.00	0.00	0.00	0.01	0.00
26.39	2.00	0.00	0.00	0.01	0.00	26.40	2.00	0.00	0.00	0.01	0.00
26.41	2.00	0.00	0.00	0.01	0.00	26.42	2.00	0.00	0.00	0.01	0.00
26.43	2.00	0.00	0.00	0.01	0.00	26.44	2.00	0.00	0.00	0.01	0.00
26.45	2.00	0.00	0.00	0.01	0.00	26.46	2.00	0.00	0.00	0.01	0.00
26.47	2.00	0.00	0.00	0.01	0.00	26.48	2.00	0.00	0.00	0.01	0.00
26.49	2.00	0.00	0.00	0.01	0.00	26.50	2.00	0.00	0.00	0.01	0.00
26.51	2.00	0.00	0.00	0.01	0.00	26.52	2.00	0.00	0.00	0.01	0.00
26.53	2.00	0.00	0.00	0.01	0.00	26.54	2.00	0.00	0.00	0.01	0.00
26.55	2.00	0.00	0.00	0.01	0.00	26.56	2.00	0.00	0.00	0.01	0.00
26.57	2.00	0.00	0.00	0.01	0.00	26.58	2.00	0.00	0.00	0.01	0.00
26.59	2.00	0.00	0.00	0.01	0.00	26.60	2.00	0.00	0.00	0.01	0.00
26.61	2.00	0.00	0.00	0.01	0.00	26.62	2.00	0.00	0.00	0.01	0.00
26.63	2.00	0.00	0.00	0.01	0.00	26.64	2.00	0.00	0.00	0.01	0.00
26.65	2.00	0.00	0.00	0.01	0.00	26.66	2.00	0.00	0.00	0.01	0.00
26.67	2.00	0.00	0.00	0.01	0.00	26.68	2.00	0.00	0.00	0.01	0.00
26.69	2.00	0.00	0.00	0.01	0.00	26.70	2.00	0.00	0.00	0.01	0.00
26.71	2.00	0.00	0.00	0.01	0.00	26.72	2.00	0.00	0.00	0.01	0.00
26.73	2.00	0.00	0.00	0.01	0.00	26.74	2.00	0.00	0.00	0.01	0.00
26.75	2.00	0.00	0.00	0.01	0.00	26.76	2.00	0.00	0.00	0.01	0.00
26.77	2.00	0.00	0.00	0.01	0.00	26.78	2.00	0.00	0.00	0.01	0.00
26.79	2.00	0.00	0.00	0.01	0.00	26.80	2.00	0.00	0.00	0.01	0.00
26.81	2.00	0.00	0.00	0.01	0.00	26.82	2.00	0.00	0.00	0.01	0.00
26.83	2.00	0.00	0.00	0.01	0.00	26.84	2.00	0.00	0.00	0.01	0.00
26.85	2.00	0.00	0.00	0.01	0.00	26.86	2.00	0.00	0.00	0.01	0.00
26.87	2.00	0.00	0.00	0.01	0.00	26.88	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
26.89	2.00	0.00	0.00	0.01	0.00	26.90	2.00	0.00	0.00	0.01	0.00
26.91	2.00	0.00	0.00	0.01	0.00	26.92	2.00	0.00	0.00	0.01	0.00
26.93	2.00	0.00	0.00	0.01	0.00	26.94	2.00	0.00	0.00	0.01	0.00
26.95	2.00	0.00	0.00	0.01	0.00	26.96	2.00	0.00	0.00	0.01	0.00
26.97	2.00	0.00	0.00	0.01	0.00	26.98	2.00	0.00	0.00	0.01	0.00
26.99	2.00	0.00	0.00	0.01	0.00	27.00	2.00	0.00	0.00	0.01	0.00
27.01	2.00	0.00	0.00	0.01	0.00	27.02	2.00	0.00	0.00	0.01	0.00
27.03	2.00	0.00	0.00	0.01	0.00	27.04	2.00	0.00	0.00	0.01	0.00
27.05	2.00	0.00	0.00	0.01	0.00	27.06	2.00	0.00	0.00	0.01	0.00
27.07	2.00	0.00	0.00	0.01	0.00	27.08	2.00	0.00	0.00	0.01	0.00
27.09	2.00	0.00	0.00	0.01	0.00	27.10	2.00	0.00	0.00	0.01	0.00
27.11	2.00	0.00	0.00	0.01	0.00	27.12	2.00	0.00	0.00	0.01	0.00
27.13	2.00	0.00	0.00	0.01	0.00	27.14	2.00	0.00	0.00	0.01	0.00
27.15	2.00	0.00	0.00	0.01	0.00	27.16	2.00	0.00	0.00	0.01	0.00
27.17	2.00	0.00	0.00	0.01	0.00	27.18	2.00	0.00	0.00	0.01	0.00
27.19	2.00	0.00	0.00	0.01	0.00	27.20	2.00	0.00	0.00	0.01	0.00
27.21	2.00	0.00	0.00	0.01	0.00	27.22	2.00	0.00	0.00	0.01	0.00
27.23	2.00	0.00	0.00	0.01	0.00	27.24	2.00	0.00	0.00	0.01	0.00
27.25	2.00	0.00	0.00	0.01	0.00	27.26	2.00	0.00	0.00	0.01	0.00
27.27	2.00	0.00	0.00	0.01	0.00	27.28	2.00	0.00	0.00	0.01	0.00
27.29	2.00	0.00	0.00	0.01	0.00	27.30	2.00	0.00	0.00	0.01	0.00
27.31	2.00	0.00	0.00	0.01	0.00	27.32	2.00	0.00	0.00	0.01	0.00
27.33	2.00	0.00	0.00	0.01	0.00	27.34	2.00	0.00	0.00	0.01	0.00
27.35	2.00	0.00	0.00	0.01	0.00	27.36	2.00	0.00	0.00	0.01	0.00
27.37	2.00	0.00	0.00	0.01	0.00	27.38	2.00	0.00	0.00	0.01	0.00
27.39	2.00	0.00	0.00	0.01	0.00	27.40	2.00	0.00	0.00	0.01	0.00
27.41	2.00	0.00	0.00	0.01	0.00	27.42	2.00	0.00	0.00	0.01	0.00
27.43	2.00	0.00	0.00	0.01	0.00	27.44	2.00	0.00	0.00	0.01	0.00
27.45	2.00	0.00	0.00	0.01	0.00	27.46	2.00	0.00	0.00	0.01	0.00
27.47	2.00	0.00	0.00	0.01	0.00	27.48	2.00	0.00	0.00	0.01	0.00
27.49	2.00	0.00	0.00	0.01	0.00	27.50	2.00	0.00	0.00	0.01	0.00
27.51	2.00	0.00	0.00	0.01	0.00	27.52	2.00	0.00	0.00	0.01	0.00
27.53	2.00	0.00	0.00	0.01	0.00	27.54	2.00	0.00	0.00	0.01	0.00
27.55	2.00	0.00	0.00	0.01	0.00	27.56	2.00	0.00	0.00	0.01	0.00
27.57	2.00	0.00	0.00	0.01	0.00	27.58	2.00	0.00	0.00	0.01	0.00
27.59	2.00	0.00	0.00	0.01	0.00	27.60	2.00	0.00	0.00	0.01	0.00
27.61	2.00	0.00	0.00	0.01	0.00	27.62	2.00	0.00	0.00	0.01	0.00
27.63	2.00	0.00	0.00	0.01	0.00	27.64	2.00	0.00	0.00	0.01	0.00
27.65	2.00	0.00	0.00	0.01	0.00	27.66	2.00	0.00	0.00	0.01	0.00
27.67	2.00	0.00	0.00	0.01	0.00	27.68	2.00	0.00	0.00	0.01	0.00
27.69	2.00	0.00	0.00	0.01	0.00	27.70	2.00	0.00	0.00	0.01	0.00
27.71	2.00	0.00	0.00	0.01	0.00	27.72	2.00	0.00	0.00	0.01	0.00
27.73	2.00	0.00	0.00	0.01	0.00	27.74	2.00	0.00	0.00	0.01	0.00
27.75	2.00	0.00	0.00	0.01	0.00	27.76	2.00	0.00	0.00	0.01	0.00
27.77	2.00	0.00	0.00	0.01	0.00	27.78	2.00	0.00	0.00	0.01	0.00
27.79	2.00	0.00	0.00	0.01	0.00	27.80	2.00	0.00	0.00	0.01	0.00
27.81	2.00	0.00	0.00	0.01	0.00	27.82	2.00	0.00	0.00	0.01	0.00
27.83	2.00	0.00	0.00	0.01	0.00	27.84	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
27.85	2.00	0.00	0.00	0.01	0.00	27.86	2.00	0.00	0.00	0.01	0.00
27.87	2.00	0.00	0.00	0.01	0.00	27.88	2.00	0.00	0.00	0.01	0.00
27.89	2.00	0.00	0.00	0.01	0.00	27.90	2.00	0.00	0.00	0.01	0.00
27.91	2.00	0.00	0.00	0.01	0.00	27.92	2.00	0.00	0.00	0.01	0.00
27.93	2.00	0.00	0.00	0.01	0.00	27.94	2.00	0.00	0.00	0.01	0.00
27.95	2.00	0.00	0.00	0.01	0.00	27.96	2.00	0.00	0.00	0.01	0.00
27.97	2.00	0.00	0.00	0.01	0.00	27.98	2.00	0.00	0.00	0.01	0.00
27.99	2.00	0.00	0.00	0.01	0.00	28.00	2.00	0.00	0.00	0.01	0.00
28.01	2.00	0.00	0.00	0.01	0.00	28.02	2.00	0.00	0.00	0.01	0.00
28.03	2.00	0.00	0.00	0.01	0.00	28.04	2.00	0.00	0.00	0.01	0.00
28.05	2.00	0.00	0.00	0.01	0.00	28.06	2.00	0.00	0.00	0.01	0.00
28.07	2.00	0.00	0.00	0.01	0.00	28.08	2.00	0.00	0.00	0.01	0.00
28.09	2.00	0.00	0.00	0.01	0.00	28.10	2.00	0.00	0.00	0.01	0.00
28.11	2.00	0.00	0.00	0.01	0.00	28.12	2.00	0.00	0.00	0.01	0.00
28.13	2.00	0.00	0.00	0.01	0.00	28.14	2.00	0.00	0.00	0.01	0.00
28.15	2.00	0.00	0.00	0.01	0.00	28.16	2.00	0.00	0.00	0.01	0.00
28.17	2.00	0.00	0.00	0.01	0.00	28.18	2.00	0.00	0.00	0.01	0.00
28.19	2.00	0.00	0.00	0.01	0.00	28.20	2.00	0.00	0.00	0.01	0.00
28.21	2.00	0.00	0.00	0.01	0.00	28.22	2.00	0.00	0.00	0.01	0.00
28.23	2.00	0.00	0.00	0.01	0.00	28.24	2.00	0.00	0.00	0.01	0.00
28.25	2.00	0.00	0.00	0.01	0.00	28.26	2.00	0.00	0.00	0.01	0.00
28.27	2.00	0.00	0.00	0.01	0.00	28.28	2.00	0.00	0.00	0.01	0.00
28.29	2.00	0.00	0.00	0.01	0.00	28.30	2.00	0.00	0.00	0.01	0.00
28.31	2.00	0.00	0.00	0.01	0.00	28.32	2.00	0.00	0.00	0.01	0.00
28.33	2.00	0.00	0.00	0.01	0.00	28.34	2.00	0.00	0.00	0.01	0.00
28.35	2.00	0.00	0.00	0.01	0.00	28.36	2.00	0.00	0.00	0.01	0.00
28.37	2.00	0.00	0.00	0.01	0.00	28.38	2.00	0.00	0.00	0.01	0.00
28.39	2.00	0.00	0.00	0.01	0.00	28.40	2.00	0.00	0.00	0.01	0.00
28.41	2.00	0.00	0.00	0.01	0.00	28.42	2.00	0.00	0.00	0.01	0.00
28.43	2.00	0.00	0.00	0.01	0.00	28.44	2.00	0.00	0.00	0.01	0.00
28.45	2.00	0.00	0.00	0.01	0.00	28.46	2.00	0.00	0.00	0.01	0.00
28.47	2.00	0.00	0.00	0.01	0.00	28.48	2.00	0.00	0.00	0.01	0.00
28.49	2.00	0.00	0.00	0.01	0.00	28.50	2.00	0.00	0.00	0.01	0.00
28.51	2.00	0.00	0.00	0.01	0.00	28.52	2.00	0.00	0.00	0.01	0.00
28.53	2.00	0.00	0.00	0.01	0.00	28.54	2.00	0.00	0.00	0.01	0.00
28.55	2.00	0.00	0.00	0.01	0.00	28.56	2.00	0.00	0.00	0.01	0.00
28.57	2.00	0.00	0.00	0.01	0.00	28.58	2.00	0.00	0.00	0.01	0.00
28.59	2.00	0.00	0.00	0.01	0.00	28.60	2.00	0.00	0.00	0.01	0.00
28.61	2.00	0.00	0.00	0.01	0.00	28.62	2.00	0.00	0.00	0.01	0.00
28.63	2.00	0.00	0.00	0.01	0.00	28.64	2.00	0.00	0.00	0.01	0.00
28.65	2.00	0.00	0.00	0.01	0.00	28.66	2.00	0.00	0.00	0.01	0.00
28.67	2.00	0.00	0.00	0.01	0.00	28.68	2.00	0.00	0.00	0.01	0.00
28.69	2.00	0.00	0.00	0.01	0.00	28.70	2.00	0.00	0.00	0.01	0.00
28.71	2.00	0.00	0.00	0.01	0.00	28.72	2.00	0.00	0.00	0.01	0.00
28.73	2.00	0.00	0.00	0.01	0.00	28.74	2.00	0.00	0.00	0.01	0.00
28.75	2.00	0.00	0.00	0.01	0.00	28.76	2.00	0.00	0.00	0.01	0.00
28.77	2.00	0.00	0.00	0.01	0.00	28.78	2.00	0.00	0.00	0.01	0.00
28.79	2.00	0.00	0.00	0.01	0.00	28.80	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
28.81	2.00	0.00	0.00	0.01	0.00	28.82	2.00	0.00	0.00	0.01	0.00
28.83	2.00	0.00	0.00	0.01	0.00	28.84	2.00	0.00	0.00	0.01	0.00
28.85	2.00	0.00	0.00	0.01	0.00	28.86	2.00	0.00	0.00	0.01	0.00
28.87	2.00	0.00	0.00	0.01	0.00	28.88	2.00	0.00	0.00	0.01	0.00
28.89	2.00	0.00	0.00	0.01	0.00	28.90	2.00	0.00	0.00	0.01	0.00
28.91	2.00	0.00	0.00	0.01	0.00	28.92	2.00	0.00	0.00	0.01	0.00
28.93	2.00	0.00	0.00	0.01	0.00	28.94	2.00	0.00	0.00	0.01	0.00
28.95	2.00	0.00	0.00	0.01	0.00	28.96	2.00	0.00	0.00	0.01	0.00
28.97	2.00	0.00	0.00	0.01	0.00	28.98	2.00	0.00	0.00	0.01	0.00
28.99	2.00	0.00	0.00	0.01	0.00	29.00	2.00	0.00	0.00	0.01	0.00
29.01	2.00	0.00	0.00	0.01	0.00	29.02	2.00	0.00	0.00	0.01	0.00
29.03	2.00	0.00	0.00	0.01	0.00	29.04	2.00	0.00	0.00	0.01	0.00
29.05	2.00	0.00	0.00	0.01	0.00	29.06	2.00	0.00	0.00	0.01	0.00
29.07	2.00	0.00	0.00	0.01	0.00	29.08	2.00	0.00	0.00	0.01	0.00
29.09	2.00	0.00	0.00	0.01	0.00	29.10	2.00	0.00	0.00	0.01	0.00
29.11	2.00	0.00	0.00	0.01	0.00	29.12	2.00	0.00	0.00	0.01	0.00
29.13	2.00	0.00	0.00	0.01	0.00	29.14	2.00	0.00	0.00	0.01	0.00
29.15	2.00	0.00	0.00	0.01	0.00	29.16	2.00	0.00	0.00	0.01	0.00
29.17	2.00	0.00	0.00	0.01	0.00	29.18	2.00	0.00	0.00	0.01	0.00
29.19	2.00	0.00	0.00	0.01	0.00	29.20	2.00	0.00	0.00	0.01	0.00
29.21	2.00	0.00	0.00	0.01	0.00	29.22	2.00	0.00	0.00	0.01	0.00
29.23	2.00	0.00	0.00	0.01	0.00	29.24	2.00	0.00	0.00	0.01	0.00
29.25	2.00	0.00	0.00	0.01	0.00	29.26	2.00	0.00	0.00	0.01	0.00
29.27	2.00	0.00	0.00	0.01	0.00	29.28	2.00	0.00	0.00	0.01	0.00
29.29	2.00	0.00	0.00	0.01	0.00	29.30	2.00	0.00	0.00	0.01	0.00
29.31	2.00	0.00	0.00	0.01	0.00	29.32	2.00	0.00	0.00	0.01	0.00
29.33	2.00	0.00	0.00	0.01	0.00	29.34	2.00	0.00	0.00	0.01	0.00
29.35	2.00	0.00	0.00	0.01	0.00	29.36	2.00	0.00	0.00	0.01	0.00
29.37	2.00	0.00	0.00	0.01	0.00	29.38	2.00	0.00	0.00	0.01	0.00
29.39	2.00	0.00	0.00	0.01	0.00	29.40	2.00	0.00	0.00	0.01	0.00
29.41	2.00	0.00	0.00	0.01	0.00	29.42	2.00	0.00	0.00	0.01	0.00
29.43	2.00	0.00	0.00	0.01	0.00	29.44	2.00	0.00	0.00	0.01	0.00
29.45	2.00	0.00	0.00	0.01	0.00	29.46	2.00	0.00	0.00	0.01	0.00
29.47	2.00	0.00	0.00	0.01	0.00	29.48	2.00	0.00	0.00	0.01	0.00
29.49	2.00	0.00	0.00	0.01	0.00	29.50	2.00	0.00	0.00	0.01	0.00
29.51	2.00	0.00	0.00	0.01	0.00	29.52	2.00	0.00	0.00	0.01	0.00
29.53	2.00	0.00	0.00	0.01	0.00	29.54	2.00	0.00	0.00	0.01	0.00
29.55	2.00	0.00	0.00	0.01	0.00	29.56	2.00	0.00	0.00	0.01	0.00
29.57	2.00	0.00	0.00	0.01	0.00	29.58	2.00	0.00	0.00	0.01	0.00
29.59	2.00	0.00	0.00	0.01	0.00	29.60	2.00	0.00	0.00	0.01	0.00
29.61	2.00	0.00	0.00	0.01	0.00	29.62	2.00	0.00	0.00	0.01	0.00
29.63	2.00	0.00	0.00	0.01	0.00	29.64	2.00	0.00	0.00	0.01	0.00
29.65	2.00	0.00	0.00	0.01	0.00	29.66	2.00	0.00	0.00	0.01	0.00
29.67	2.00	0.00	0.00	0.01	0.00	29.68	2.00	0.00	0.00	0.01	0.00
29.69	2.00	0.00	0.00	0.01	0.00	29.70	2.00	0.00	0.00	0.01	0.00
29.71	2.00	0.00	0.00	0.01	0.00	29.72	2.00	0.00	0.00	0.01	0.00
29.73	2.00	0.00	0.00	0.01	0.00	29.74	2.00	0.00	0.00	0.01	0.00
29.75	2.00	0.00	0.00	0.01	0.00	29.76	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
29.77	2.00	0.00	0.00	0.01	0.00	29.78	2.00	0.00	0.00	0.01	0.00
29.79	2.00	0.00	0.00	0.01	0.00	29.80	2.00	0.00	0.00	0.01	0.00
29.81	2.00	0.00	0.00	0.01	0.00	29.82	2.00	0.00	0.00	0.01	0.00
29.83	2.00	0.00	0.00	0.01	0.00	29.84	2.00	0.00	0.00	0.01	0.00
29.85	2.00	0.00	0.00	0.01	0.00	29.86	2.00	0.00	0.00	0.01	0.00
29.87	2.00	0.00	0.00	0.01	0.00	29.88	2.00	0.00	0.00	0.01	0.00
29.89	2.00	0.00	0.00	0.01	0.00	29.90	2.00	0.00	0.00	0.01	0.00
29.91	2.00	0.00	0.00	0.01	0.00	29.92	2.00	0.00	0.00	0.01	0.00
29.93	2.00	0.00	0.00	0.01	0.00	29.94	2.00	0.00	0.00	0.01	0.00
29.95	2.00	0.00	0.00	0.01	0.00	29.96	2.00	0.00	0.00	0.01	0.00
29.97	2.00	0.00	0.00	0.01	0.00	29.98	2.00	0.00	0.00	0.01	0.00
29.99	2.00	0.00	0.00	0.01	0.00	30.00	2.00	0.00	0.00	0.01	0.00
30.01	2.00	0.00	0.00	0.01	0.00	30.02	2.00	0.00	0.00	0.01	0.00
30.03	2.00	0.00	0.00	0.01	0.00	30.04	2.00	0.00	0.00	0.01	0.00
30.05	2.00	0.00	0.00	0.01	0.00	30.06	2.00	0.00	0.00	0.01	0.00
30.07	2.00	0.00	0.00	0.01	0.00	30.08	2.00	0.00	0.00	0.01	0.00
30.09	2.00	0.00	0.00	0.01	0.00	30.10	2.00	0.00	0.00	0.01	0.00
30.11	2.00	0.00	0.00	0.01	0.00	30.12	2.00	0.00	0.00	0.01	0.00
30.13	2.00	0.00	0.00	0.01	0.00	30.14	2.00	0.00	0.00	0.01	0.00
30.15	2.00	0.00	0.00	0.01	0.00	30.16	2.00	0.00	0.00	0.01	0.00
30.17	2.00	0.00	0.00	0.01	0.00	30.18	2.00	0.00	0.00	0.01	0.00
30.19	2.00	0.00	0.00	0.01	0.00	30.20	2.00	0.00	0.00	0.01	0.00
30.21	2.00	0.00	0.00	0.01	0.00	30.22	2.00	0.00	0.00	0.01	0.00
30.23	2.00	0.00	0.00	0.01	0.00	30.24	2.00	0.00	0.00	0.01	0.00
30.25	2.00	0.00	0.00	0.01	0.00	30.26	2.00	0.00	0.00	0.01	0.00
30.27	2.00	0.00	0.00	0.01	0.00	30.28	2.00	0.00	0.00	0.01	0.00
30.29	2.00	0.00	0.00	0.01	0.00	30.30	2.00	0.00	0.00	0.01	0.00
30.31	2.00	0.00	0.00	0.01	0.00	30.32	2.00	0.00	0.00	0.01	0.00
30.33	2.00	0.00	0.00	0.01	0.00	30.34	2.00	0.00	0.00	0.01	0.00
30.35	2.00	0.00	0.00	0.01	0.00	30.36	2.00	0.00	0.00	0.01	0.00
30.37	2.00	0.00	0.00	0.01	0.00	30.38	2.00	0.00	0.00	0.01	0.00
30.39	2.00	0.00	0.00	0.01	0.00	30.40	2.00	0.00	0.00	0.01	0.00
30.41	2.00	0.00	0.00	0.01	0.00	30.42	2.00	0.00	0.00	0.01	0.00
30.43	2.00	0.00	0.00	0.01	0.00	30.44	2.00	0.00	0.00	0.01	0.00
30.45	2.00	0.00	0.00	0.01	0.00	30.46	2.00	0.00	0.00	0.01	0.00
30.47	2.00	0.00	0.00	0.01	0.00	30.48	2.00	0.00	0.00	0.01	0.00
30.49	2.00	0.00	0.00	0.01	0.00	30.50	2.00	0.00	0.00	0.01	0.00
30.51	2.00	0.00	0.00	0.01	0.00	30.52	2.00	0.00	0.00	0.01	0.00
30.53	2.00	0.00	0.00	0.01	0.00	30.54	2.00	0.00	0.00	0.01	0.00
30.55	2.00	0.00	0.00	0.01	0.00	30.56	2.00	0.00	0.00	0.01	0.00
30.57	2.00	0.00	0.00	0.01	0.00	30.58	2.00	0.00	0.00	0.01	0.00
30.59	2.00	0.00	0.00	0.01	0.00	30.60	2.00	0.00	0.00	0.01	0.00
30.61	2.00	0.00	0.00	0.01	0.00	30.62	2.00	0.00	0.00	0.01	0.00
30.63	2.00	0.00	0.00	0.01	0.00	30.64	2.00	0.00	0.00	0.01	0.00
30.65	2.00	0.00	0.00	0.01	0.00	30.66	2.00	0.00	0.00	0.01	0.00
30.67	2.00	0.00	0.00	0.01	0.00	30.68	2.00	0.00	0.00	0.01	0.00
30.69	2.00	0.00	0.00	0.01	0.00	30.70	2.00	0.00	0.00	0.01	0.00
30.71	2.00	0.00	0.00	0.01	0.00	30.72	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
30.73	2.00	0.00	0.00	0.01	0.00	30.74	2.00	0.00	0.00	0.01	0.00
30.75	2.00	0.00	0.00	0.01	0.00	30.76	2.00	0.00	0.00	0.01	0.00
30.77	2.00	0.00	0.00	0.01	0.00	30.78	2.00	0.00	0.00	0.01	0.00
30.79	2.00	0.00	0.00	0.01	0.00	30.80	2.00	0.00	0.00	0.01	0.00
30.81	2.00	0.00	0.00	0.01	0.00	30.82	2.00	0.00	0.00	0.01	0.00
30.83	2.00	0.00	0.00	0.01	0.00	30.84	2.00	0.00	0.00	0.01	0.00
30.85	2.00	0.00	0.00	0.01	0.00	30.86	2.00	0.00	0.00	0.01	0.00
30.87	2.00	0.00	0.00	0.01	0.00	30.88	2.00	0.00	0.00	0.01	0.00
30.89	2.00	0.00	0.00	0.01	0.00	30.90	2.00	0.00	0.00	0.01	0.00
30.91	2.00	0.00	0.00	0.01	0.00	30.92	2.00	0.00	0.00	0.01	0.00
30.93	2.00	0.00	0.00	0.01	0.00	30.94	2.00	0.00	0.00	0.01	0.00
30.95	2.00	0.00	0.00	0.01	0.00	30.96	0.30	0.00	0.00	0.01	0.01
30.97	0.31	0.00	0.00	0.01	0.01	30.98	0.31	0.00	0.00	0.01	0.01
30.99	0.31	0.00	0.00	0.01	0.01	31.00	0.31	0.00	0.00	0.01	0.01
31.01	0.31	0.00	0.00	0.01	0.01	31.02	0.32	0.00	0.00	0.01	0.01
31.03	0.32	0.00	0.00	0.01	0.01	31.04	0.32	0.00	0.00	0.01	0.01
31.05	0.32	0.00	0.00	0.01	0.01	31.06	0.32	0.00	0.00	0.01	0.01
31.07	0.32	0.00	0.00	0.01	0.01	31.08	0.32	0.00	0.00	0.01	0.01
31.09	0.32	0.00	0.00	0.01	0.01	31.10	0.32	0.00	0.00	0.01	0.01
31.11	0.32	0.00	0.00	0.01	0.01	31.12	0.32	0.00	0.00	0.01	0.01
31.13	0.32	0.00	0.00	0.01	0.01	31.14	0.32	0.00	0.00	0.01	0.01
31.15	0.32	0.00	0.00	0.01	0.01	31.16	0.32	0.00	0.00	0.01	0.01
31.17	0.33	0.00	0.00	0.01	0.01	31.18	0.33	0.00	0.00	0.01	0.01
31.19	0.33	0.00	0.00	0.01	0.01	31.20	0.33	0.00	0.00	0.01	0.01
31.21	0.33	0.00	0.00	0.01	0.01	31.22	0.33	0.00	0.00	0.01	0.01
31.23	0.34	0.00	0.00	0.01	0.01	31.24	0.34	0.00	0.00	0.01	0.01
31.25	0.34	0.00	0.00	0.01	0.01	31.26	0.35	0.00	0.00	0.01	0.01
31.27	0.35	0.00	0.00	0.01	0.01	31.28	0.35	0.00	0.00	0.01	0.01
31.29	0.36	0.00	0.00	0.01	0.01	31.30	0.36	0.00	0.00	0.01	0.01
31.31	0.36	0.00	0.00	0.01	0.01	31.32	0.37	0.00	0.00	0.01	0.01
31.33	0.37	0.00	0.00	0.01	0.01	31.34	0.38	0.00	0.00	0.01	0.01
31.35	0.38	0.00	0.00	0.01	0.01	31.36	0.39	0.00	0.00	0.01	0.01
31.37	0.39	0.00	0.00	0.01	0.01	31.38	0.40	0.00	0.00	0.01	0.01
31.39	0.40	0.00	0.00	0.01	0.01	31.40	0.41	0.00	0.00	0.01	0.01
31.41	0.42	0.00	0.00	0.01	0.01	31.42	0.43	0.00	0.00	0.01	0.01
31.43	0.45	0.00	0.00	0.01	0.01	31.44	0.46	0.00	0.00	0.01	0.01
31.45	0.47	0.00	0.00	0.01	0.01	31.46	0.49	0.00	0.00	0.01	0.01
31.47	0.50	0.00	0.00	0.01	0.01	31.48	0.51	0.00	0.00	0.01	0.01
31.49	0.52	0.00	0.00	0.01	0.01	31.50	0.54	0.00	0.00	0.01	0.01
31.51	0.56	0.00	0.00	0.01	0.01	31.52	0.58	0.00	0.00	0.01	0.01
31.53	0.60	0.00	0.00	0.01	0.01	31.54	0.63	0.00	0.00	0.01	0.01
31.55	0.65	0.00	0.00	0.01	0.01	31.56	0.67	0.00	0.00	0.01	0.01
31.57	0.68	0.00	0.00	0.01	0.01	31.58	0.70	0.00	0.00	0.01	0.00
31.59	0.73	0.00	0.00	0.01	0.00	31.60	0.76	0.00	0.00	0.01	0.00
31.61	0.79	0.00	0.00	0.01	0.00	31.62	0.82	0.00	0.00	0.01	0.00
31.63	0.86	0.00	0.00	0.01	0.00	31.64	0.88	0.00	0.00	0.01	0.00
31.65	0.91	0.00	0.00	0.01	0.00	31.66	0.93	0.00	0.00	0.01	0.00
31.67	0.95	0.00	0.00	0.01	0.00	31.68	0.98	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
31.69	1.02	0.00	0.00	0.01	0.00	31.70	1.05	0.00	0.00	0.01	0.00
31.71	1.09	0.00	0.00	0.01	0.00	31.72	1.12	0.00	0.00	0.01	0.00
31.73	1.14	0.00	0.00	0.01	0.00	31.74	1.16	0.00	0.00	0.01	0.00
31.75	1.18	0.00	0.00	0.01	0.00	31.76	1.20	0.00	0.00	0.01	0.00
31.77	1.22	0.00	0.00	0.01	0.00	31.78	1.24	0.00	0.00	0.01	0.00
31.79	1.27	0.00	0.00	0.01	0.00	31.80	1.29	0.00	0.00	0.01	0.00
31.81	1.31	0.00	0.00	0.01	0.00	31.82	1.33	0.00	0.00	0.01	0.00
31.83	1.34	0.00	0.00	0.01	0.00	31.84	1.36	0.00	0.00	0.01	0.00
31.85	1.38	0.00	0.00	0.01	0.00	31.86	1.40	0.00	0.00	0.01	0.00
31.87	1.42	0.00	0.00	0.01	0.00	31.88	1.44	0.00	0.00	0.01	0.00
31.89	1.46	0.00	0.00	0.01	0.00	31.90	1.48	0.00	0.00	0.01	0.00
31.91	1.50	0.00	0.00	0.01	0.00	31.92	1.50	0.00	0.00	0.01	0.00
31.93	1.50	0.00	0.00	0.01	0.00	31.94	1.50	0.00	0.00	0.01	0.00
31.95	1.50	0.00	0.00	0.01	0.00	31.96	1.51	0.00	0.00	0.01	0.00
31.97	1.51	0.00	0.00	0.01	0.00	31.98	1.51	0.00	0.00	0.01	0.00
31.99	1.51	0.00	0.00	0.01	0.00	32.00	1.51	0.00	0.00	0.01	0.00
32.01	1.51	0.00	0.00	0.01	0.00	32.02	1.51	0.00	0.00	0.01	0.00
32.03	1.50	0.00	0.00	0.01	0.00	32.04	1.50	0.00	0.00	0.01	0.00
32.05	1.50	0.00	0.00	0.01	0.00	32.06	1.49	0.00	0.00	0.01	0.00
32.07	1.49	0.00	0.00	0.01	0.00	32.08	1.49	0.00	0.00	0.01	0.00
32.09	1.49	0.00	0.00	0.01	0.00	32.10	1.48	0.00	0.00	0.01	0.00
32.11	1.48	0.00	0.00	0.01	0.00	32.12	1.48	0.00	0.00	0.01	0.00
32.13	1.47	0.00	0.00	0.01	0.00	32.14	1.47	0.00	0.00	0.01	0.00
32.15	1.46	0.00	0.00	0.01	0.00	32.16	1.46	0.00	0.00	0.01	0.00
32.17	1.46	0.00	0.00	0.01	0.00	32.18	1.46	0.00	0.00	0.01	0.00
32.19	1.45	0.00	0.00	0.01	0.00	32.20	1.45	0.00	0.00	0.01	0.00
32.21	1.44	0.00	0.00	0.01	0.00	32.22	1.44	0.00	0.00	0.01	0.00
32.23	1.43	0.00	0.00	0.01	0.00	32.24	1.43	0.00	0.00	0.01	0.00
32.25	1.43	0.00	0.00	0.01	0.00	32.26	1.42	0.00	0.00	0.01	0.00
32.27	1.42	0.00	0.00	0.01	0.00	32.28	1.42	0.00	0.00	0.01	0.00
32.29	1.42	0.00	0.00	0.01	0.00	32.30	1.42	0.00	0.00	0.01	0.00
32.31	1.42	0.00	0.00	0.01	0.00	32.32	1.41	0.00	0.00	0.01	0.00
32.33	1.41	0.00	0.00	0.01	0.00	32.34	1.41	0.00	0.00	0.01	0.00
32.35	1.41	0.00	0.00	0.01	0.00	32.36	1.42	0.00	0.00	0.01	0.00
32.37	1.42	0.00	0.00	0.01	0.00	32.38	1.42	0.00	0.00	0.01	0.00
32.39	1.43	0.00	0.00	0.01	0.00	32.40	1.43	0.00	0.00	0.01	0.00
32.41	1.43	0.00	0.00	0.01	0.00	32.42	1.43	0.00	0.00	0.01	0.00
32.43	1.44	0.00	0.00	0.01	0.00	32.44	1.44	0.00	0.00	0.01	0.00
32.45	1.44	0.00	0.00	0.01	0.00	32.46	1.45	0.00	0.00	0.01	0.00
32.47	1.45	0.00	0.00	0.01	0.00	32.48	1.45	0.00	0.00	0.01	0.00
32.49	1.46	0.00	0.00	0.01	0.00	32.50	1.46	0.00	0.00	0.01	0.00
32.51	1.46	0.00	0.00	0.01	0.00	32.52	1.46	0.00	0.00	0.01	0.00
32.53	1.47	0.00	0.00	0.01	0.00	32.54	1.48	0.00	0.00	0.01	0.00
32.55	1.49	0.00	0.00	0.01	0.00	32.56	1.50	0.00	0.00	0.01	0.00
32.57	1.51	0.00	0.00	0.01	0.00	32.58	1.52	0.00	0.00	0.01	0.00
32.59	1.52	0.00	0.00	0.01	0.00	32.60	1.53	0.00	0.00	0.01	0.00
32.61	1.59	0.00	0.00	0.01	0.00	32.62	1.68	0.00	0.00	0.01	0.00
32.63	1.79	0.00	0.00	0.01	0.00	32.64	1.93	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
32.65	2.00	0.00	0.00	0.01	0.00	32.66	2.00	0.00	0.00	0.01	0.00
32.67	2.00	0.00	0.00	0.01	0.00	32.68	2.00	0.00	0.00	0.01	0.00
32.69	2.00	0.00	0.00	0.01	0.00	32.70	2.00	0.00	0.00	0.01	0.00
32.71	2.00	0.00	0.00	0.01	0.00	32.72	2.00	0.00	0.00	0.01	0.00
32.73	2.00	0.00	0.00	0.01	0.00	32.74	2.00	0.00	0.00	0.01	0.00
32.75	2.00	0.00	0.00	0.01	0.00	32.76	2.00	0.00	0.00	0.01	0.00
32.77	2.00	0.00	0.00	0.01	0.00	32.78	2.00	0.00	0.00	0.01	0.00
32.79	2.00	0.00	0.00	0.01	0.00	32.80	2.00	0.00	0.00	0.01	0.00
32.81	2.00	0.00	0.00	0.01	0.00	32.82	2.00	0.00	0.00	0.01	0.00
32.83	2.00	0.00	0.00	0.01	0.00	32.84	2.00	0.00	0.00	0.01	0.00
32.85	2.00	0.00	0.00	0.01	0.00	32.86	2.00	0.00	0.00	0.01	0.00
32.87	2.00	0.00	0.00	0.01	0.00	32.88	2.00	0.00	0.00	0.01	0.00
32.89	2.00	0.00	0.00	0.01	0.00	32.90	2.00	0.00	0.00	0.01	0.00
32.91	2.00	0.00	0.00	0.01	0.00	32.92	2.00	0.00	0.00	0.01	0.00
32.93	2.00	0.00	0.00	0.01	0.00	32.94	2.00	0.00	0.00	0.01	0.00
32.95	2.00	0.00	0.00	0.01	0.00	32.96	2.00	0.00	0.00	0.01	0.00
32.97	2.00	0.00	0.00	0.01	0.00	32.98	2.00	0.00	0.00	0.01	0.00
32.99	2.00	0.00	0.00	0.01	0.00	33.00	2.00	0.00	0.00	0.01	0.00
33.01	2.00	0.00	0.00	0.01	0.00	33.02	2.00	0.00	0.00	0.01	0.00
33.03	2.00	0.00	0.00	0.01	0.00	33.04	2.00	0.00	0.00	0.01	0.00
33.05	2.00	0.00	0.00	0.01	0.00	33.06	2.00	0.00	0.00	0.01	0.00
33.07	2.00	0.00	0.00	0.01	0.00	33.08	2.00	0.00	0.00	0.01	0.00
33.09	2.00	0.00	0.00	0.01	0.00	33.10	2.00	0.00	0.00	0.01	0.00
33.11	2.00	0.00	0.00	0.01	0.00	33.12	2.00	0.00	0.00	0.01	0.00
33.13	2.00	0.00	0.00	0.01	0.00	33.14	2.00	0.00	0.00	0.01	0.00
33.15	2.00	0.00	0.00	0.01	0.00	33.16	2.00	0.00	0.00	0.01	0.00
33.17	2.00	0.00	0.00	0.01	0.00	33.18	2.00	0.00	0.00	0.01	0.00
33.19	2.00	0.00	0.00	0.01	0.00	33.20	2.00	0.00	0.00	0.01	0.00
33.21	2.00	0.00	0.00	0.01	0.00	33.22	2.00	0.00	0.00	0.01	0.00
33.23	2.00	0.00	0.00	0.01	0.00	33.24	2.00	0.00	0.00	0.01	0.00
33.25	2.00	0.00	0.00	0.01	0.00	33.26	2.00	0.00	0.00	0.01	0.00
33.27	2.00	0.00	0.00	0.01	0.00	33.28	2.00	0.00	0.00	0.01	0.00
33.29	2.00	0.00	0.00	0.01	0.00	33.30	2.00	0.00	0.00	0.01	0.00
33.31	2.00	0.00	0.00	0.01	0.00	33.32	2.00	0.00	0.00	0.01	0.00
33.33	2.00	0.00	0.00	0.01	0.00	33.34	2.00	0.00	0.00	0.01	0.00
33.35	2.00	0.00	0.00	0.01	0.00	33.36	2.00	0.00	0.00	0.01	0.00
33.37	2.00	0.00	0.00	0.01	0.00	33.38	2.00	0.00	0.00	0.01	0.00
33.39	2.00	0.00	0.00	0.01	0.00	33.40	2.00	0.00	0.00	0.01	0.00
33.41	2.00	0.00	0.00	0.01	0.00	33.42	2.00	0.00	0.00	0.01	0.00
33.43	2.00	0.00	0.00	0.01	0.00	33.44	2.00	0.00	0.00	0.01	0.00
33.45	2.00	0.00	0.00	0.01	0.00	33.46	2.00	0.00	0.00	0.01	0.00
33.47	2.00	0.00	0.00	0.01	0.00	33.48	2.00	0.00	0.00	0.01	0.00
33.49	2.00	0.00	0.00	0.01	0.00	33.50	2.00	0.00	0.00	0.01	0.00
33.51	2.00	0.00	0.00	0.01	0.00	33.52	2.00	0.00	0.00	0.01	0.00
33.53	2.00	0.00	0.00	0.01	0.00	33.54	2.00	0.00	0.00	0.01	0.00
33.55	2.00	0.00	0.00	0.01	0.00	33.56	2.00	0.00	0.00	0.01	0.00
33.57	2.00	0.00	0.00	0.01	0.00	33.58	2.00	0.00	0.00	0.01	0.00
33.59	2.00	0.00	0.00	0.01	0.00	33.60	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
33.61	2.00	0.00	0.00	0.01	0.00	33.62	2.00	0.00	0.00	0.01	0.00
33.63	2.00	0.00	0.00	0.01	0.00	33.64	2.00	0.00	0.00	0.01	0.00
33.65	2.00	0.00	0.00	0.01	0.00	33.66	2.00	0.00	0.00	0.01	0.00
33.67	2.00	0.00	0.00	0.01	0.00	33.68	2.00	0.00	0.00	0.01	0.00
33.69	2.00	0.00	0.00	0.01	0.00	33.70	2.00	0.00	0.00	0.01	0.00
33.71	2.00	0.00	0.00	0.01	0.00	33.72	2.00	0.00	0.00	0.01	0.00
33.73	2.00	0.00	0.00	0.01	0.00	33.74	2.00	0.00	0.00	0.01	0.00
33.75	2.00	0.00	0.00	0.01	0.00	33.76	2.00	0.00	0.00	0.01	0.00
33.77	2.00	0.00	0.00	0.01	0.00	33.78	2.00	0.00	0.00	0.01	0.00
33.79	2.00	0.00	0.00	0.01	0.00	33.80	2.00	0.00	0.00	0.01	0.00
33.81	2.00	0.00	0.00	0.01	0.00	33.82	2.00	0.00	0.00	0.01	0.00
33.83	2.00	0.00	0.00	0.01	0.00	33.84	2.00	0.00	0.00	0.01	0.00
33.85	2.00	0.00	0.00	0.01	0.00	33.86	1.95	0.00	0.00	0.01	0.00
33.87	1.85	0.00	0.00	0.01	0.00	33.88	1.77	0.00	0.00	0.01	0.00
33.89	1.70	0.00	0.00	0.01	0.00	33.90	1.64	0.00	0.00	0.01	0.00
33.91	1.64	0.00	0.00	0.01	0.00	33.92	1.64	0.00	0.00	0.01	0.00
33.93	1.63	0.00	0.00	0.01	0.00	33.94	1.63	0.00	0.00	0.01	0.00
33.95	1.62	0.00	0.00	0.01	0.00	33.96	1.62	0.00	0.00	0.01	0.00
33.97	1.62	0.00	0.00	0.01	0.00	33.98	1.61	0.00	0.00	0.01	0.00
33.99	1.61	0.00	0.00	0.01	0.00	34.00	1.61	0.00	0.00	0.01	0.00
34.01	1.61	0.00	0.00	0.01	0.00	34.02	1.60	0.00	0.00	0.01	0.00
34.03	1.60	0.00	0.00	0.01	0.00	34.04	1.60	0.00	0.00	0.01	0.00
34.05	1.60	0.00	0.00	0.01	0.00	34.06	1.60	0.00	0.00	0.01	0.00
34.07	1.59	0.00	0.00	0.01	0.00	34.08	1.58	0.00	0.00	0.01	0.00
34.09	1.55	0.00	0.00	0.01	0.00	34.10	1.52	0.00	0.00	0.01	0.00
34.11	1.49	0.00	0.00	0.01	0.00	34.12	1.46	0.00	0.00	0.01	0.00
34.13	1.43	0.00	0.00	0.01	0.00	34.14	1.40	0.00	0.00	0.01	0.00
34.15	1.37	0.00	0.00	0.01	0.00	34.16	1.35	0.00	0.00	0.01	0.00
34.17	1.36	0.00	0.00	0.01	0.00	34.18	1.37	0.00	0.00	0.01	0.00
34.19	1.37	0.00	0.00	0.01	0.00	34.20	1.38	0.00	0.00	0.01	0.00
34.21	1.39	0.00	0.00	0.01	0.00	34.22	1.39	0.00	0.00	0.01	0.00
34.23	1.40	0.00	0.00	0.01	0.00	34.24	1.41	0.00	0.00	0.01	0.00
34.25	1.42	0.00	0.00	0.01	0.00	34.26	1.44	0.00	0.00	0.01	0.00
34.27	1.47	0.00	0.00	0.01	0.00	34.28	1.50	0.00	0.00	0.01	0.00
34.29	1.53	0.00	0.00	0.01	0.00	34.30	1.57	0.00	0.00	0.01	0.00
34.31	1.60	0.00	0.00	0.01	0.00	34.32	1.63	0.00	0.00	0.01	0.00
34.33	1.66	0.00	0.00	0.01	0.00	34.34	1.69	0.00	0.00	0.01	0.00
34.35	1.75	0.00	0.00	0.01	0.00	34.36	1.82	0.00	0.00	0.01	0.00
34.37	1.89	0.00	0.00	0.01	0.00	34.38	1.98	0.00	0.00	0.01	0.00
34.39	2.00	0.00	0.00	0.01	0.00	34.40	2.00	0.00	0.00	0.01	0.00
34.41	2.00	0.00	0.00	0.01	0.00	34.42	2.00	0.00	0.00	0.01	0.00
34.43	2.00	0.00	0.00	0.01	0.00	34.44	2.00	0.00	0.00	0.01	0.00
34.45	2.00	0.00	0.00	0.01	0.00	34.46	2.00	0.00	0.00	0.01	0.00
34.47	2.00	0.00	0.00	0.01	0.00	34.48	2.00	0.00	0.00	0.01	0.00
34.49	2.00	0.00	0.00	0.01	0.00	34.50	2.00	0.00	0.00	0.01	0.00
34.51	2.00	0.00	0.00	0.01	0.00	34.52	2.00	0.00	0.00	0.01	0.00
34.53	2.00	0.00	0.00	0.01	0.00	34.54	2.00	0.00	0.00	0.01	0.00
34.55	2.00	0.00	0.00	0.01	0.00	34.56	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
34.57	2.00	0.00	0.00	0.01	0.00	34.58	2.00	0.00	0.00	0.01	0.00
34.59	2.00	0.00	0.00	0.01	0.00	34.60	2.00	0.00	0.00	0.01	0.00
34.61	2.00	0.00	0.00	0.01	0.00	34.62	2.00	0.00	0.00	0.01	0.00
34.63	2.00	0.00	0.00	0.01	0.00	34.64	2.00	0.00	0.00	0.01	0.00
34.65	2.00	0.00	0.00	0.01	0.00	34.66	2.00	0.00	0.00	0.01	0.00
34.67	2.00	0.00	0.00	0.01	0.00	34.68	2.00	0.00	0.00	0.01	0.00
34.69	2.00	0.00	0.00	0.01	0.00	34.70	2.00	0.00	0.00	0.01	0.00
34.71	2.00	0.00	0.00	0.01	0.00	34.72	2.00	0.00	0.00	0.01	0.00
34.73	2.00	0.00	0.00	0.01	0.00	34.74	2.00	0.00	0.00	0.01	0.00
34.75	2.00	0.00	0.00	0.01	0.00	34.76	2.00	0.00	0.00	0.01	0.00
34.77	2.00	0.00	0.00	0.01	0.00	34.78	2.00	0.00	0.00	0.01	0.00
34.79	2.00	0.00	0.00	0.01	0.00	34.80	2.00	0.00	0.00	0.01	0.00
34.81	2.00	0.00	0.00	0.01	0.00	34.82	2.00	0.00	0.00	0.01	0.00
34.83	2.00	0.00	0.00	0.01	0.00	34.84	2.00	0.00	0.00	0.01	0.00
34.85	2.00	0.00	0.00	0.01	0.00	34.86	2.00	0.00	0.00	0.01	0.00
34.87	2.00	0.00	0.00	0.01	0.00	34.88	2.00	0.00	0.00	0.01	0.00
34.89	2.00	0.00	0.00	0.01	0.00	34.90	2.00	0.00	0.00	0.01	0.00
34.91	2.00	0.00	0.00	0.01	0.00	34.92	2.00	0.00	0.00	0.01	0.00
34.93	2.00	0.00	0.00	0.01	0.00	34.94	2.00	0.00	0.00	0.01	0.00
34.95	2.00	0.00	0.00	0.01	0.00	34.96	2.00	0.00	0.00	0.01	0.00
34.97	2.00	0.00	0.00	0.01	0.00	34.98	2.00	0.00	0.00	0.01	0.00
34.99	2.00	0.00	0.00	0.01	0.00	35.00	2.00	0.00	0.00	0.01	0.00
35.01	2.00	0.00	0.00	0.01	0.00	35.02	2.00	0.00	0.00	0.01	0.00
35.03	2.00	0.00	0.00	0.01	0.00	35.04	2.00	0.00	0.00	0.01	0.00
35.05	2.00	0.00	0.00	0.01	0.00	35.06	2.00	0.00	0.00	0.01	0.00
35.07	2.00	0.00	0.00	0.01	0.00	35.08	2.00	0.00	0.00	0.01	0.00
35.09	2.00	0.00	0.00	0.01	0.00	35.10	2.00	0.00	0.00	0.01	0.00
35.11	2.00	0.00	0.00	0.01	0.00	35.12	2.00	0.00	0.00	0.01	0.00
35.13	2.00	0.00	0.00	0.01	0.00	35.14	2.00	0.00	0.00	0.01	0.00
35.15	2.00	0.00	0.00	0.01	0.00	35.16	2.00	0.00	0.00	0.01	0.00
35.17	2.00	0.00	0.00	0.01	0.00	35.18	1.94	0.00	0.00	0.01	0.00
35.19	1.85	0.00	0.00	0.01	0.00	35.20	1.79	0.00	0.00	0.01	0.00
35.21	1.72	0.00	0.00	0.01	0.00	35.22	1.63	0.00	0.00	0.01	0.00
35.23	1.54	0.00	0.00	0.01	0.00	35.24	1.44	0.00	0.00	0.01	0.00
35.25	1.35	0.00	0.00	0.01	0.00	35.26	1.27	0.00	0.00	0.01	0.00
35.27	1.21	0.00	0.00	0.01	0.00	35.28	1.15	0.00	0.00	0.01	0.00
35.29	1.12	0.00	0.00	0.01	0.00	35.30	1.07	0.00	0.00	0.01	0.00
35.31	1.01	0.00	0.00	0.01	0.00	35.32	0.95	0.00	0.00	0.01	0.00
35.33	0.90	0.00	0.00	0.01	0.00	35.34	0.84	0.00	0.00	0.01	0.00
35.35	0.80	0.00	0.00	0.01	0.00	35.36	0.76	0.00	0.00	0.01	0.00
35.37	0.73	0.00	0.00	0.01	0.00	35.38	0.71	0.00	0.00	0.01	0.00
35.39	0.68	0.00	0.00	0.01	0.00	35.40	0.64	0.00	0.00	0.01	0.01
35.41	0.61	0.00	0.00	0.01	0.01	35.42	0.58	0.00	0.00	0.01	0.01
35.43	0.55	0.00	0.00	0.01	0.01	35.44	0.52	0.00	0.00	0.01	0.01
35.45	0.50	0.00	0.00	0.01	0.01	35.46	0.49	0.00	0.00	0.01	0.01
35.47	0.48	0.00	0.00	0.01	0.01	35.48	0.46	0.00	0.00	0.01	0.01
35.49	0.45	0.00	0.00	0.01	0.01	35.50	0.43	0.00	0.00	0.01	0.01
35.51	0.42	0.00	0.00	0.01	0.01	35.52	0.41	0.00	0.00	0.01	0.01

:: Liquefaction Potential Index calculation data ::

Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
35.53	0.40	0.00	0.00	0.01	0.01	35.54	0.39	0.00	0.00	0.01	0.01
35.55	0.38	0.00	0.00	0.01	0.01	35.56	0.38	0.00	0.00	0.01	0.01
35.57	0.37	0.00	0.00	0.01	0.01	35.58	0.37	0.00	0.00	0.01	0.01
35.59	0.36	0.00	0.00	0.01	0.01	35.60	0.36	0.00	0.00	0.01	0.01
35.61	0.36	0.00	0.00	0.01	0.01	35.62	0.35	0.00	0.00	0.01	0.01
35.63	0.35	0.00	0.00	0.01	0.01	35.64	0.35	0.00	0.00	0.01	0.01
35.65	0.35	0.00	0.00	0.01	0.01	35.66	0.34	0.00	0.00	0.01	0.01
35.67	0.34	0.00	0.00	0.01	0.01	35.68	0.34	0.00	0.00	0.01	0.01
35.69	0.34	0.00	0.00	0.01	0.01	35.70	0.34	0.00	0.00	0.01	0.01
35.71	0.33	0.00	0.00	0.01	0.01	35.72	0.33	0.00	0.00	0.01	0.01
35.73	0.33	0.00	0.00	0.01	0.01	35.74	0.33	0.00	0.00	0.01	0.01
35.75	0.33	0.00	0.00	0.01	0.01	35.76	0.33	0.00	0.00	0.01	0.01
35.77	0.33	0.00	0.00	0.01	0.01	35.78	0.33	0.00	0.00	0.01	0.01
35.79	0.33	0.00	0.00	0.01	0.01	35.80	0.33	0.00	0.00	0.01	0.01
35.81	0.33	0.00	0.00	0.01	0.01	35.82	0.33	0.00	0.00	0.01	0.01
35.83	0.33	0.00	0.00	0.01	0.01	35.84	0.33	0.00	0.00	0.01	0.01
35.85	0.33	0.00	0.00	0.01	0.01	35.86	0.33	0.00	0.00	0.01	0.01
35.87	0.33	0.00	0.00	0.01	0.01	35.88	0.33	0.00	0.00	0.01	0.01
35.89	0.33	0.00	0.00	0.01	0.01	35.90	0.33	0.00	0.00	0.01	0.01
35.91	0.34	0.00	0.00	0.01	0.01	35.92	0.34	0.00	0.00	0.01	0.01
35.93	0.34	0.00	0.00	0.01	0.01	35.94	0.34	0.00	0.00	0.01	0.01
35.95	0.34	0.00	0.00	0.01	0.01	35.96	0.34	0.00	0.00	0.01	0.01
35.97	0.35	0.00	0.00	0.01	0.01	35.98	0.35	0.00	0.00	0.01	0.01
35.99	0.35	0.00	0.00	0.01	0.01	36.00	0.35	0.00	0.00	0.01	0.01
36.01	0.35	0.00	0.00	0.01	0.01	36.02	0.35	0.00	0.00	0.01	0.01
36.03	0.35	0.00	0.00	0.01	0.01	36.04	0.35	0.00	0.00	0.01	0.01
36.05	0.35	0.00	0.00	0.01	0.01	36.06	0.35	0.00	0.00	0.01	0.01
36.07	0.35	0.00	0.00	0.01	0.01	36.08	0.35	0.00	0.00	0.01	0.01
36.09	0.35	0.00	0.00	0.01	0.01	36.10	0.35	0.00	0.00	0.01	0.01
36.11	0.35	0.00	0.00	0.01	0.01	36.12	0.35	0.00	0.00	0.01	0.01
36.13	0.35	0.00	0.00	0.01	0.01	36.14	0.35	0.00	0.00	0.01	0.01
36.15	0.35	0.00	0.00	0.01	0.01	36.16	0.35	0.00	0.00	0.01	0.01
36.17	0.35	0.00	0.00	0.01	0.01	36.18	0.35	0.00	0.00	0.01	0.01
36.19	0.35	0.00	0.00	0.01	0.01	36.20	0.35	0.00	0.00	0.01	0.01
36.21	0.35	0.00	0.00	0.01	0.01	36.22	0.35	0.00	0.00	0.01	0.01
36.23	0.35	0.00	0.00	0.01	0.01	36.24	0.35	0.00	0.00	0.01	0.01
36.25	0.35	0.00	0.00	0.01	0.01	36.26	0.35	0.00	0.00	0.01	0.01
36.27	0.35	0.00	0.00	0.01	0.01	36.28	0.35	0.00	0.00	0.01	0.01
36.29	0.35	0.00	0.00	0.01	0.01	36.30	0.36	0.00	0.00	0.01	0.01
36.31	0.36	0.00	0.00	0.01	0.01	36.32	0.36	0.00	0.00	0.01	0.01
36.33	0.36	0.00	0.00	0.01	0.01	36.34	0.36	0.00	0.00	0.01	0.01
36.35	0.36	0.00	0.00	0.01	0.01	36.36	0.37	0.00	0.00	0.01	0.01
36.37	0.37	0.00	0.00	0.01	0.01	36.38	0.37	0.00	0.00	0.01	0.01
36.39	0.37	0.00	0.00	0.01	0.01	36.40	0.38	0.00	0.00	0.01	0.01
36.41	0.38	0.00	0.00	0.01	0.01	36.42	0.38	0.00	0.00	0.01	0.01
36.43	0.38	0.00	0.00	0.01	0.01	36.44	0.38	0.00	0.00	0.01	0.01
36.45	0.38	0.00	0.00	0.01	0.01	36.46	0.38	0.00	0.00	0.01	0.01
36.47	0.38	0.00	0.00	0.01	0.01	36.48	0.38	0.00	0.00	0.01	0.01

:: Liquefaction Potential Index calculation data ::

Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
36.49	0.38	0.00	0.00	0.01	0.01	36.50	0.38	0.00	0.00	0.01	0.01
36.51	0.38	0.00	0.00	0.01	0.01	36.52	0.38	0.00	0.00	0.01	0.01
36.53	0.38	0.00	0.00	0.01	0.01	36.54	0.38	0.00	0.00	0.01	0.01
36.55	0.38	0.00	0.00	0.01	0.01	36.56	0.38	0.00	0.00	0.01	0.01
36.57	0.38	0.00	0.00	0.01	0.01	36.58	0.38	0.00	0.00	0.01	0.01
36.59	0.38	0.00	0.00	0.01	0.01	36.60	0.38	0.00	0.00	0.01	0.01
36.61	0.38	0.00	0.00	0.01	0.01	36.62	0.38	0.00	0.00	0.01	0.01
36.63	0.38	0.00	0.00	0.01	0.01	36.64	0.38	0.00	0.00	0.01	0.01
36.65	0.38	0.00	0.00	0.01	0.01	36.66	0.38	0.00	0.00	0.01	0.01
36.67	0.38	0.00	0.00	0.01	0.01	36.68	0.38	0.00	0.00	0.01	0.01
36.69	0.38	0.00	0.00	0.01	0.01	36.70	0.38	0.00	0.00	0.01	0.01
36.71	0.38	0.00	0.00	0.01	0.01	36.72	0.38	0.00	0.00	0.01	0.01
36.73	0.38	0.00	0.00	0.01	0.01	36.74	0.38	0.00	0.00	0.01	0.01
36.75	0.38	0.00	0.00	0.01	0.01	36.76	0.38	0.00	0.00	0.01	0.01
36.77	0.38	0.00	0.00	0.01	0.01	36.78	0.38	0.00	0.00	0.01	0.01
36.79	0.38	0.00	0.00	0.01	0.01	36.80	0.38	0.00	0.00	0.01	0.01
36.81	0.38	0.00	0.00	0.01	0.01	36.82	0.38	0.00	0.00	0.01	0.01
36.83	0.38	0.00	0.00	0.01	0.01	36.84	0.38	0.00	0.00	0.01	0.01
36.85	0.38	0.00	0.00	0.01	0.01	36.86	0.38	0.00	0.00	0.01	0.01
36.87	0.37	0.00	0.00	0.01	0.01	36.88	0.37	0.00	0.00	0.01	0.01
36.89	0.37	0.00	0.00	0.01	0.01	36.90	0.37	0.00	0.00	0.01	0.01
36.91	0.37	0.00	0.00	0.01	0.01	36.92	0.37	0.00	0.00	0.01	0.01
36.93	0.37	0.00	0.00	0.01	0.01	36.94	0.37	0.00	0.00	0.01	0.01
36.95	0.37	0.00	0.00	0.01	0.01	36.96	0.36	0.00	0.00	0.01	0.01
36.97	0.36	0.00	0.00	0.01	0.01	36.98	0.36	0.00	0.00	0.01	0.01
36.99	0.36	0.00	0.00	0.01	0.01	37.00	0.35	0.00	0.00	0.01	0.01
37.01	0.35	0.00	0.00	0.01	0.01	37.02	0.35	0.00	0.00	0.01	0.01
37.03	0.35	0.00	0.00	0.01	0.01	37.04	0.35	0.00	0.00	0.01	0.01
37.05	0.35	0.00	0.00	0.01	0.01	37.06	0.34	0.00	0.00	0.01	0.01
37.07	0.34	0.00	0.00	0.01	0.01	37.08	0.34	0.00	0.00	0.01	0.01
37.09	0.34	0.00	0.00	0.01	0.01	37.10	0.34	0.00	0.00	0.01	0.01
37.11	0.34	0.00	0.00	0.01	0.01	37.12	0.34	0.00	0.00	0.01	0.01
37.13	0.34	0.00	0.00	0.01	0.01	37.14	0.34	0.00	0.00	0.01	0.01
37.15	0.34	0.00	0.00	0.01	0.01	37.16	0.33	0.00	0.00	0.01	0.01
37.17	0.33	0.00	0.00	0.01	0.01	37.18	0.33	0.00	0.00	0.01	0.01
37.19	0.33	0.00	0.00	0.01	0.01	37.20	0.33	0.00	0.00	0.01	0.01
37.21	0.33	0.00	0.00	0.01	0.01	37.22	0.33	0.00	0.00	0.01	0.01
37.23	0.33	0.00	0.00	0.01	0.01	37.24	0.33	0.00	0.00	0.01	0.01
37.25	0.33	0.00	0.00	0.01	0.01	37.26	0.33	0.00	0.00	0.01	0.01
37.27	0.33	0.00	0.00	0.01	0.01	37.28	0.33	0.00	0.00	0.01	0.01
37.29	0.33	0.00	0.00	0.01	0.01	37.30	0.33	0.00	0.00	0.01	0.01
37.31	0.33	0.00	0.00	0.01	0.01	37.32	0.33	0.00	0.00	0.01	0.01
37.33	0.33	0.00	0.00	0.01	0.01	37.34	0.33	0.00	0.00	0.01	0.01
37.35	0.33	0.00	0.00	0.01	0.01	37.36	0.33	0.00	0.00	0.01	0.01
37.37	0.33	0.00	0.00	0.01	0.01	37.38	0.33	0.00	0.00	0.01	0.01
37.39	0.33	0.00	0.00	0.01	0.01	37.40	0.33	0.00	0.00	0.01	0.01
37.41	0.33	0.00	0.00	0.01	0.01	37.42	0.32	0.00	0.00	0.01	0.01
37.43	0.32	0.00	0.00	0.01	0.01	37.44	0.32	0.00	0.00	0.01	0.01

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
37.45	0.32	0.00	0.00	0.01	0.01	37.46	0.32	0.00	0.00	0.01	0.01
37.47	0.32	0.00	0.00	0.01	0.01	37.48	0.32	0.00	0.00	0.01	0.01
37.49	0.32	0.00	0.00	0.01	0.01	37.50	0.32	0.00	0.00	0.01	0.01
37.51	0.33	0.00	0.00	0.01	0.01	37.52	0.33	0.00	0.00	0.01	0.01
37.53	0.33	0.00	0.00	0.01	0.01	37.54	0.33	0.00	0.00	0.01	0.01
37.55	0.33	0.00	0.00	0.01	0.01	37.56	0.33	0.00	0.00	0.01	0.01
37.57	0.33	0.00	0.00	0.01	0.01	37.58	0.33	0.00	0.00	0.01	0.01
37.59	0.33	0.00	0.00	0.01	0.01	37.60	0.33	0.00	0.00	0.01	0.01
37.61	0.33	0.00	0.00	0.01	0.01	37.62	0.33	0.00	0.00	0.01	0.01
37.63	0.33	0.00	0.00	0.01	0.01	37.64	0.33	0.00	0.00	0.01	0.01
37.65	0.33	0.00	0.00	0.01	0.01	37.66	0.33	0.00	0.00	0.01	0.01
37.67	0.33	0.00	0.00	0.01	0.01	37.68	0.33	0.00	0.00	0.01	0.01
37.69	0.33	0.00	0.00	0.01	0.01	37.70	0.33	0.00	0.00	0.01	0.01
37.71	2.00	0.00	0.00	0.01	0.00	37.72	2.00	0.00	0.00	0.01	0.00
37.73	2.00	0.00	0.00	0.01	0.00	37.74	2.00	0.00	0.00	0.01	0.00
37.75	2.00	0.00	0.00	0.01	0.00	37.76	2.00	0.00	0.00	0.01	0.00
37.77	2.00	0.00	0.00	0.01	0.00	37.78	2.00	0.00	0.00	0.01	0.00
37.79	2.00	0.00	0.00	0.01	0.00	37.80	2.00	0.00	0.00	0.01	0.00
37.81	2.00	0.00	0.00	0.01	0.00	37.82	2.00	0.00	0.00	0.01	0.00
37.83	2.00	0.00	0.00	0.01	0.00	37.84	2.00	0.00	0.00	0.01	0.00
37.85	2.00	0.00	0.00	0.01	0.00	37.86	2.00	0.00	0.00	0.01	0.00
37.87	2.00	0.00	0.00	0.01	0.00	37.88	2.00	0.00	0.00	0.01	0.00
37.89	2.00	0.00	0.00	0.01	0.00	37.90	2.00	0.00	0.00	0.01	0.00
37.91	2.00	0.00	0.00	0.01	0.00	37.92	2.00	0.00	0.00	0.01	0.00
37.93	2.00	0.00	0.00	0.01	0.00	37.94	2.00	0.00	0.00	0.01	0.00
37.95	2.00	0.00	0.00	0.01	0.00	37.96	2.00	0.00	0.00	0.01	0.00
37.97	2.00	0.00	0.00	0.01	0.00	37.98	2.00	0.00	0.00	0.01	0.00
37.99	2.00	0.00	0.00	0.01	0.00	38.00	2.00	0.00	0.00	0.01	0.00
38.01	2.00	0.00	0.00	0.01	0.00	38.02	2.00	0.00	0.00	0.01	0.00
38.03	2.00	0.00	0.00	0.01	0.00	38.04	2.00	0.00	0.00	0.01	0.00
38.05	2.00	0.00	0.00	0.01	0.00	38.06	2.00	0.00	0.00	0.01	0.00
38.07	0.29	0.00	0.00	0.01	0.01	38.08	0.28	0.00	0.00	0.01	0.01
38.09	0.28	0.00	0.00	0.01	0.01	38.10	0.28	0.00	0.00	0.01	0.01
38.11	0.28	0.00	0.00	0.01	0.01	38.12	0.28	0.00	0.00	0.01	0.01
38.13	0.28	0.00	0.00	0.01	0.01	38.14	0.27	0.00	0.00	0.01	0.01
38.15	2.00	0.00	0.00	0.01	0.00	38.16	2.00	0.00	0.00	0.01	0.00
38.17	2.00	0.00	0.00	0.01	0.00	38.18	2.00	0.00	0.00	0.01	0.00
38.19	2.00	0.00	0.00	0.01	0.00	38.20	2.00	0.00	0.00	0.01	0.00
38.21	2.00	0.00	0.00	0.01	0.00	38.22	2.00	0.00	0.00	0.01	0.00
38.23	2.00	0.00	0.00	0.01	0.00	38.24	2.00	0.00	0.00	0.01	0.00
38.25	2.00	0.00	0.00	0.01	0.00	38.26	2.00	0.00	0.00	0.01	0.00
38.27	2.00	0.00	0.00	0.01	0.00	38.28	2.00	0.00	0.00	0.01	0.00
38.29	2.00	0.00	0.00	0.01	0.00	38.30	2.00	0.00	0.00	0.01	0.00
38.31	2.00	0.00	0.00	0.01	0.00	38.32	2.00	0.00	0.00	0.01	0.00
38.33	2.00	0.00	0.00	0.01	0.00	38.34	2.00	0.00	0.00	0.01	0.00
38.35	2.00	0.00	0.00	0.01	0.00	38.36	2.00	0.00	0.00	0.01	0.00
38.37	2.00	0.00	0.00	0.01	0.00	38.38	2.00	0.00	0.00	0.01	0.00
38.39	2.00	0.00	0.00	0.01	0.00	38.40	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
38.41	2.00	0.00	0.00	0.01	0.00	38.42	2.00	0.00	0.00	0.01	0.00
38.43	2.00	0.00	0.00	0.01	0.00	38.44	2.00	0.00	0.00	0.01	0.00
38.45	2.00	0.00	0.00	0.01	0.00	38.46	2.00	0.00	0.00	0.01	0.00
38.47	2.00	0.00	0.00	0.01	0.00	38.48	1.32	0.00	0.00	0.01	0.00
38.49	1.39	0.00	0.00	0.01	0.00	38.50	1.40	0.00	0.00	0.01	0.00
38.51	1.42	0.00	0.00	0.01	0.00	38.52	1.45	0.00	0.00	0.01	0.00
38.53	1.48	0.00	0.00	0.01	0.00	38.54	1.51	0.00	0.00	0.01	0.00
38.55	1.54	0.00	0.00	0.01	0.00	38.56	1.56	0.00	0.00	0.01	0.00
38.57	1.58	0.00	0.00	0.01	0.00	38.58	1.58	0.00	0.00	0.01	0.00
38.59	1.54	0.00	0.00	0.01	0.00	38.60	1.50	0.00	0.00	0.01	0.00
38.61	1.45	0.00	0.00	0.01	0.00	38.62	1.40	0.00	0.00	0.01	0.00
38.63	1.35	0.00	0.00	0.01	0.00	38.64	1.30	0.00	0.00	0.01	0.00
38.65	1.26	0.00	0.00	0.01	0.00	38.66	1.23	0.00	0.00	0.01	0.00
38.67	1.20	0.00	0.00	0.01	0.00	38.68	1.16	0.00	0.00	0.01	0.00
38.69	1.11	0.00	0.00	0.01	0.00	38.70	1.06	0.00	0.00	0.01	0.00
38.71	1.01	0.00	0.00	0.01	0.00	38.72	0.96	0.00	0.00	0.01	0.00
38.73	0.92	0.00	0.00	0.01	0.00	38.74	0.88	0.00	0.00	0.01	0.00
38.75	0.86	0.00	0.00	0.01	0.00	38.76	0.84	0.00	0.00	0.01	0.00
38.77	0.82	0.00	0.00	0.01	0.00	38.78	0.79	0.00	0.00	0.01	0.00
38.79	0.77	0.00	0.00	0.01	0.00	38.80	0.74	0.00	0.00	0.01	0.00
38.81	0.72	0.00	0.00	0.01	0.00	38.82	0.70	0.00	0.00	0.01	0.00
38.83	0.69	0.00	0.00	0.01	0.00	38.84	0.68	0.00	0.00	0.01	0.00
38.85	0.69	0.00	0.00	0.01	0.00	38.86	0.70	0.00	0.00	0.01	0.00
38.87	0.70	0.00	0.00	0.01	0.00	38.88	0.71	0.00	0.00	0.01	0.00
38.89	0.72	0.00	0.00	0.01	0.00	38.90	0.73	0.00	0.00	0.01	0.00
38.91	0.74	0.00	0.00	0.01	0.00	38.92	0.75	0.00	0.00	0.01	0.00
38.93	0.76	0.00	0.00	0.01	0.00	38.94	0.79	0.00	0.00	0.01	0.00
38.95	0.83	0.00	0.00	0.01	0.00	38.96	0.87	0.00	0.00	0.01	0.00
38.97	0.91	0.00	0.00	0.01	0.00	38.98	0.95	0.00	0.00	0.01	0.00
38.99	1.00	0.00	0.00	0.01	0.00	39.00	1.03	0.00	0.00	0.01	0.00
39.01	1.06	0.00	0.00	0.01	0.00	39.02	1.11	0.00	0.00	0.01	0.00
39.03	1.16	0.00	0.00	0.01	0.00	39.04	1.23	0.00	0.00	0.01	0.00
39.05	1.31	0.00	0.00	0.01	0.00	39.06	1.39	0.00	0.00	0.01	0.00
39.07	1.47	0.00	0.00	0.01	0.00	39.08	1.55	0.00	0.00	0.01	0.00
39.09	1.62	0.00	0.00	0.01	0.00	39.10	1.67	0.00	0.00	0.01	0.00
39.11	1.73	0.00	0.00	0.01	0.00	39.12	1.82	0.00	0.00	0.01	0.00
39.13	1.92	0.00	0.00	0.01	0.00	39.14	2.00	0.00	0.00	0.01	0.00
39.15	2.00	0.00	0.00	0.01	0.00	39.16	2.00	0.00	0.00	0.01	0.00
39.17	2.00	0.00	0.00	0.01	0.00	39.18	2.00	0.00	0.00	0.01	0.00
39.19	2.00	0.00	0.00	0.01	0.00	39.20	2.00	0.00	0.00	0.01	0.00
39.21	2.00	0.00	0.00	0.01	0.00	39.22	2.00	0.00	0.00	0.01	0.00
39.23	2.00	0.00	0.00	0.01	0.00	39.24	2.00	0.00	0.00	0.01	0.00
39.25	2.00	0.00	0.00	0.01	0.00	39.26	2.00	0.00	0.00	0.01	0.00
39.27	2.00	0.00	0.00	0.01	0.00	39.28	2.00	0.00	0.00	0.01	0.00
39.29	2.00	0.00	0.00	0.01	0.00	39.30	2.00	0.00	0.00	0.01	0.00
39.31	2.00	0.00	0.00	0.01	0.00	39.32	2.00	0.00	0.00	0.01	0.00
39.33	2.00	0.00	0.00	0.01	0.00	39.34	2.00	0.00	0.00	0.01	0.00
39.35	2.00	0.00	0.00	0.01	0.00	39.36	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
39.37	2.00	0.00	0.00	0.01	0.00	39.38	2.00	0.00	0.00	0.01	0.00
39.39	2.00	0.00	0.00	0.01	0.00	39.40	2.00	0.00	0.00	0.01	0.00
39.41	2.00	0.00	0.00	0.01	0.00	39.42	2.00	0.00	0.00	0.01	0.00
39.43	2.00	0.00	0.00	0.01	0.00	39.44	2.00	0.00	0.00	0.01	0.00
39.45	2.00	0.00	0.00	0.01	0.00	39.46	2.00	0.00	0.00	0.01	0.00
39.47	2.00	0.00	0.00	0.01	0.00	39.48	2.00	0.00	0.00	0.01	0.00
39.49	2.00	0.00	0.00	0.01	0.00	39.50	2.00	0.00	0.00	0.01	0.00
39.51	2.00	0.00	0.00	0.01	0.00	39.52	2.00	0.00	0.00	0.01	0.00
39.53	2.00	0.00	0.00	0.01	0.00	39.54	2.00	0.00	0.00	0.01	0.00
39.55	2.00	0.00	0.00	0.01	0.00	39.56	2.00	0.00	0.00	0.01	0.00
39.57	2.00	0.00	0.00	0.01	0.00	39.58	2.00	0.00	0.00	0.01	0.00
39.59	2.00	0.00	0.00	0.01	0.00	39.60	2.00	0.00	0.00	0.01	0.00
39.61	2.00	0.00	0.00	0.01	0.00	39.62	2.00	0.00	0.00	0.01	0.00
39.63	2.00	0.00	0.00	0.01	0.00	39.64	2.00	0.00	0.00	0.01	0.00
39.65	2.00	0.00	0.00	0.01	0.00	39.66	2.00	0.00	0.00	0.01	0.00
39.67	2.00	0.00	0.00	0.01	0.00	39.68	2.00	0.00	0.00	0.01	0.00
39.69	2.00	0.00	0.00	0.01	0.00	39.70	2.00	0.00	0.00	0.01	0.00
39.71	2.00	0.00	0.00	0.01	0.00	39.72	2.00	0.00	0.00	0.01	0.00
39.73	2.00	0.00	0.00	0.01	0.00	39.74	2.00	0.00	0.00	0.01	0.00
39.75	2.00	0.00	0.00	0.01	0.00	39.76	2.00	0.00	0.00	0.01	0.00
39.77	2.00	0.00	0.00	0.01	0.00	39.78	2.00	0.00	0.00	0.01	0.00
39.79	2.00	0.00	0.00	0.01	0.00	39.80	2.00	0.00	0.00	0.01	0.00
39.81	2.00	0.00	0.00	0.01	0.00	39.82	2.00	0.00	0.00	0.01	0.00
39.83	2.00	0.00	0.00	0.01	0.00	39.84	2.00	0.00	0.00	0.01	0.00
39.85	2.00	0.00	0.00	0.01	0.00	39.86	2.00	0.00	0.00	0.01	0.00
39.87	2.00	0.00	0.00	0.01	0.00	39.88	2.00	0.00	0.00	0.01	0.00
39.89	2.00	0.00	0.00	0.01	0.00	39.90	2.00	0.00	0.00	0.01	0.00
39.91	2.00	0.00	0.00	0.01	0.00	39.92	2.00	0.00	0.00	0.01	0.00
39.93	2.00	0.00	0.00	0.01	0.00	39.94	2.00	0.00	0.00	0.01	0.00
39.95	2.00	0.00	0.00	0.01	0.00	39.96	2.00	0.00	0.00	0.01	0.00
39.97	2.00	0.00	0.00	0.01	0.00	39.98	2.00	0.00	0.00	0.01	0.00
39.99	2.00	0.00	0.00	0.01	0.00	40.00	2.00	0.00	0.00	0.01	0.00
40.01	2.00	0.00	0.00	0.01	0.00	40.02	2.00	0.00	0.00	0.01	0.00
40.03	2.00	0.00	0.00	0.01	0.00	40.04	2.00	0.00	0.00	0.01	0.00
40.05	2.00	0.00	0.00	0.01	0.00	40.06	2.00	0.00	0.00	0.01	0.00
40.07	2.00	0.00	0.00	0.01	0.00	40.08	2.00	0.00	0.00	0.01	0.00
40.09	2.00	0.00	0.00	0.01	0.00	40.10	2.00	0.00	0.00	0.01	0.00
40.11	2.00	0.00	0.00	0.01	0.00	40.12	2.00	0.00	0.00	0.01	0.00
40.13	2.00	0.00	0.00	0.01	0.00	40.14	2.00	0.00	0.00	0.01	0.00
40.15	2.00	0.00	0.00	0.01	0.00	40.16	2.00	0.00	0.00	0.01	0.00
40.17	2.00	0.00	0.00	0.01	0.00	40.18	2.00	0.00	0.00	0.01	0.00
40.19	2.00	0.00	0.00	0.01	0.00	40.20	2.00	0.00	0.00	0.01	0.00
40.21	2.00	0.00	0.00	0.01	0.00	40.22	2.00	0.00	0.00	0.01	0.00
40.23	2.00	0.00	0.00	0.01	0.00	40.24	2.00	0.00	0.00	0.01	0.00
40.25	2.00	0.00	0.00	0.01	0.00	40.26	2.00	0.00	0.00	0.01	0.00
40.27	2.00	0.00	0.00	0.01	0.00	40.28	2.00	0.00	0.00	0.01	0.00
40.29	2.00	0.00	0.00	0.01	0.00	40.30	2.00	0.00	0.00	0.01	0.00
40.31	2.00	0.00	0.00	0.01	0.00	40.32	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
40.33	2.00	0.00	0.00	0.01	0.00	40.34	2.00	0.00	0.00	0.01	0.00
40.35	2.00	0.00	0.00	0.01	0.00	40.36	2.00	0.00	0.00	0.01	0.00
40.37	2.00	0.00	0.00	0.01	0.00	40.38	2.00	0.00	0.00	0.01	0.00
40.39	2.00	0.00	0.00	0.01	0.00	40.40	2.00	0.00	0.00	0.01	0.00
40.41	2.00	0.00	0.00	0.01	0.00	40.42	2.00	0.00	0.00	0.01	0.00
40.43	2.00	0.00	0.00	0.01	0.00	40.44	2.00	0.00	0.00	0.01	0.00
40.45	2.00	0.00	0.00	0.01	0.00	40.46	2.00	0.00	0.00	0.01	0.00
40.47	2.00	0.00	0.00	0.01	0.00	40.48	2.00	0.00	0.00	0.01	0.00
40.49	2.00	0.00	0.00	0.01	0.00	40.50	2.00	0.00	0.00	0.01	0.00
40.51	2.00	0.00	0.00	0.01	0.00	40.52	2.00	0.00	0.00	0.01	0.00
40.53	2.00	0.00	0.00	0.01	0.00	40.54	2.00	0.00	0.00	0.01	0.00
40.55	2.00	0.00	0.00	0.01	0.00	40.56	2.00	0.00	0.00	0.01	0.00
40.57	2.00	0.00	0.00	0.01	0.00	40.58	2.00	0.00	0.00	0.01	0.00
40.59	2.00	0.00	0.00	0.01	0.00	40.60	2.00	0.00	0.00	0.01	0.00
40.61	2.00	0.00	0.00	0.01	0.00	40.62	2.00	0.00	0.00	0.01	0.00
40.63	2.00	0.00	0.00	0.01	0.00	40.64	2.00	0.00	0.00	0.01	0.00
40.65	2.00	0.00	0.00	0.01	0.00	40.66	2.00	0.00	0.00	0.01	0.00
40.67	2.00	0.00	0.00	0.01	0.00	40.68	2.00	0.00	0.00	0.01	0.00
40.69	2.00	0.00	0.00	0.01	0.00	40.70	2.00	0.00	0.00	0.01	0.00
40.71	2.00	0.00	0.00	0.01	0.00	40.72	2.00	0.00	0.00	0.01	0.00
40.73	2.00	0.00	0.00	0.01	0.00	40.74	2.00	0.00	0.00	0.01	0.00
40.75	2.00	0.00	0.00	0.01	0.00	40.76	2.00	0.00	0.00	0.01	0.00
40.77	2.00	0.00	0.00	0.01	0.00	40.78	2.00	0.00	0.00	0.01	0.00
40.79	2.00	0.00	0.00	0.01	0.00	40.80	1.98	0.00	0.00	0.01	0.00
40.81	1.88	0.00	0.00	0.01	0.00	40.82	1.80	0.00	0.00	0.01	0.00
40.83	1.74	0.00	0.00	0.01	0.00	40.84	1.66	0.00	0.00	0.01	0.00
40.85	1.57	0.00	0.00	0.01	0.00	40.86	1.47	0.00	0.00	0.01	0.00
40.87	1.38	0.00	0.00	0.01	0.00	40.88	1.29	0.00	0.00	0.01	0.00
40.89	1.21	0.00	0.00	0.01	0.00	40.90	1.15	0.00	0.00	0.01	0.00
40.91	1.10	0.00	0.00	0.01	0.00	40.92	1.06	0.00	0.00	0.01	0.00
40.93	1.00	0.00	0.00	0.01	0.00	40.94	0.94	0.00	0.00	0.01	0.00
40.95	0.88	0.00	0.00	0.01	0.00	40.96	0.82	0.00	0.00	0.01	0.00
40.97	0.77	0.00	0.00	0.01	0.00	40.98	0.72	0.00	0.00	0.01	0.00
40.99	0.69	0.00	0.00	0.01	0.00	41.00	0.66	0.00	0.00	0.01	0.00
41.01	0.64	0.00	0.00	0.01	0.00	41.02	2.00	0.00	0.00	0.01	0.00
41.03	2.00	0.00	0.00	0.01	0.00	41.04	2.00	0.00	0.00	0.01	0.00
41.05	2.00	0.00	0.00	0.01	0.00	41.06	2.00	0.00	0.00	0.01	0.00
41.07	2.00	0.00	0.00	0.01	0.00	41.08	2.00	0.00	0.00	0.01	0.00
41.09	2.00	0.00	0.00	0.01	0.00	41.10	2.00	0.00	0.00	0.01	0.00
41.11	2.00	0.00	0.00	0.01	0.00	41.12	2.00	0.00	0.00	0.01	0.00
41.13	2.00	0.00	0.00	0.01	0.00	41.14	2.00	0.00	0.00	0.01	0.00
41.15	2.00	0.00	0.00	0.01	0.00	41.16	2.00	0.00	0.00	0.01	0.00
41.17	2.00	0.00	0.00	0.01	0.00	41.18	2.00	0.00	0.00	0.01	0.00
41.19	2.00	0.00	0.00	0.01	0.00	41.20	2.00	0.00	0.00	0.01	0.00
41.21	2.00	0.00	0.00	0.01	0.00	41.22	2.00	0.00	0.00	0.01	0.00
41.23	2.00	0.00	0.00	0.01	0.00	41.24	2.00	0.00	0.00	0.01	0.00
41.25	2.00	0.00	0.00	0.01	0.00	41.26	2.00	0.00	0.00	0.01	0.00
41.27	2.00	0.00	0.00	0.01	0.00	41.28	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
41.29	2.00	0.00	0.00	0.01	0.00	41.30	2.00	0.00	0.00	0.01	0.00
41.31	2.00	0.00	0.00	0.01	0.00	41.32	2.00	0.00	0.00	0.01	0.00
41.33	2.00	0.00	0.00	0.01	0.00	41.34	2.00	0.00	0.00	0.01	0.00
41.35	2.00	0.00	0.00	0.01	0.00	41.36	2.00	0.00	0.00	0.01	0.00
41.37	2.00	0.00	0.00	0.01	0.00	41.38	2.00	0.00	0.00	0.01	0.00
41.39	2.00	0.00	0.00	0.01	0.00	41.40	2.00	0.00	0.00	0.01	0.00
41.41	2.00	0.00	0.00	0.01	0.00	41.42	2.00	0.00	0.00	0.01	0.00
41.43	2.00	0.00	0.00	0.01	0.00	41.44	2.00	0.00	0.00	0.01	0.00
41.45	2.00	0.00	0.00	0.01	0.00	41.46	2.00	0.00	0.00	0.01	0.00
41.47	2.00	0.00	0.00	0.01	0.00	41.48	2.00	0.00	0.00	0.01	0.00
41.49	2.00	0.00	0.00	0.01	0.00	41.50	2.00	0.00	0.00	0.01	0.00
41.51	2.00	0.00	0.00	0.01	0.00	41.52	2.00	0.00	0.00	0.01	0.00
41.53	2.00	0.00	0.00	0.01	0.00	41.54	2.00	0.00	0.00	0.01	0.00
41.55	2.00	0.00	0.00	0.01	0.00	41.56	2.00	0.00	0.00	0.01	0.00
41.57	2.00	0.00	0.00	0.01	0.00	41.58	2.00	0.00	0.00	0.01	0.00
41.59	2.00	0.00	0.00	0.01	0.00	41.60	2.00	0.00	0.00	0.01	0.00
41.61	2.00	0.00	0.00	0.01	0.00	41.62	2.00	0.00	0.00	0.01	0.00
41.63	2.00	0.00	0.00	0.01	0.00	41.64	2.00	0.00	0.00	0.01	0.00
41.65	2.00	0.00	0.00	0.01	0.00	41.66	2.00	0.00	0.00	0.01	0.00
41.67	2.00	0.00	0.00	0.01	0.00	41.68	2.00	0.00	0.00	0.01	0.00
41.69	2.00	0.00	0.00	0.01	0.00	41.70	2.00	0.00	0.00	0.01	0.00
41.71	2.00	0.00	0.00	0.01	0.00	41.72	2.00	0.00	0.00	0.01	0.00
41.73	2.00	0.00	0.00	0.01	0.00	41.74	2.00	0.00	0.00	0.01	0.00
41.75	2.00	0.00	0.00	0.01	0.00	41.76	2.00	0.00	0.00	0.01	0.00
41.77	2.00	0.00	0.00	0.01	0.00	41.78	2.00	0.00	0.00	0.01	0.00
41.79	2.00	0.00	0.00	0.01	0.00	41.80	2.00	0.00	0.00	0.01	0.00
41.81	2.00	0.00	0.00	0.01	0.00	41.82	2.00	0.00	0.00	0.01	0.00
41.83	2.00	0.00	0.00	0.01	0.00	41.84	2.00	0.00	0.00	0.01	0.00
41.85	2.00	0.00	0.00	0.01	0.00	41.86	2.00	0.00	0.00	0.01	0.00
41.87	2.00	0.00	0.00	0.01	0.00	41.88	2.00	0.00	0.00	0.01	0.00
41.89	2.00	0.00	0.00	0.01	0.00	41.90	2.00	0.00	0.00	0.01	0.00
41.91	2.00	0.00	0.00	0.01	0.00	41.92	2.00	0.00	0.00	0.01	0.00
41.93	2.00	0.00	0.00	0.01	0.00	41.94	2.00	0.00	0.00	0.01	0.00
41.95	2.00	0.00	0.00	0.01	0.00	41.96	2.00	0.00	0.00	0.01	0.00
41.97	2.00	0.00	0.00	0.01	0.00	41.98	2.00	0.00	0.00	0.01	0.00
41.99	2.00	0.00	0.00	0.01	0.00	42.00	2.00	0.00	0.00	0.01	0.00
42.01	2.00	0.00	0.00	0.01	0.00	42.02	2.00	0.00	0.00	0.01	0.00
42.03	2.00	0.00	0.00	0.01	0.00	42.04	2.00	0.00	0.00	0.01	0.00
42.05	2.00	0.00	0.00	0.01	0.00	42.06	2.00	0.00	0.00	0.01	0.00
42.07	2.00	0.00	0.00	0.01	0.00	42.08	2.00	0.00	0.00	0.01	0.00
42.09	2.00	0.00	0.00	0.01	0.00	42.10	2.00	0.00	0.00	0.01	0.00
42.11	2.00	0.00	0.00	0.01	0.00	42.12	2.00	0.00	0.00	0.01	0.00
42.13	2.00	0.00	0.00	0.01	0.00	42.14	2.00	0.00	0.00	0.01	0.00
42.15	2.00	0.00	0.00	0.01	0.00	42.16	2.00	0.00	0.00	0.01	0.00
42.17	2.00	0.00	0.00	0.01	0.00	42.18	2.00	0.00	0.00	0.01	0.00
42.19	2.00	0.00	0.00	0.01	0.00	42.20	2.00	0.00	0.00	0.01	0.00
42.21	2.00	0.00	0.00	0.01	0.00	42.22	2.00	0.00	0.00	0.01	0.00
42.23	2.00	0.00	0.00	0.01	0.00	42.24	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
42.25	2.00	0.00	0.00	0.01	0.00	42.26	0.18	0.82	0.27	0.01	0.01
42.27	0.18	0.82	0.27	0.01	0.01	42.28	0.18	0.82	0.27	0.01	0.01
42.29	0.18	0.82	0.27	0.01	0.01	42.30	0.18	0.82	0.27	0.01	0.01
42.31	0.18	0.82	0.27	0.01	0.01	42.32	0.18	0.82	0.27	0.01	0.01
42.33	0.18	0.82	0.27	0.01	0.01	42.34	0.19	0.81	0.27	0.01	0.01
42.35	0.19	0.81	0.27	0.01	0.01	42.36	0.19	0.81	0.27	0.01	0.01
42.37	0.19	0.81	0.27	0.01	0.01	42.38	0.19	0.81	0.27	0.01	0.01
42.39	0.19	0.81	0.27	0.01	0.01	42.40	0.19	0.81	0.27	0.01	0.01
42.41	0.19	0.81	0.27	0.01	0.01	42.42	0.19	0.81	0.27	0.01	0.01
42.43	0.18	0.82	0.27	0.01	0.01	42.44	0.18	0.82	0.27	0.01	0.01
42.45	0.18	0.82	0.27	0.01	0.01	42.46	0.18	0.82	0.27	0.01	0.01
42.47	0.18	0.82	0.27	0.01	0.01	42.48	0.18	0.82	0.27	0.01	0.01
42.49	0.18	0.82	0.27	0.01	0.01	42.50	0.18	0.82	0.27	0.01	0.01
42.51	0.17	0.83	0.27	0.01	0.01	42.52	0.17	0.83	0.27	0.01	0.01
42.53	0.17	0.83	0.27	0.01	0.01	42.54	0.17	0.83	0.27	0.01	0.01
42.55	2.00	0.00	0.00	0.01	0.00	42.56	2.00	0.00	0.00	0.01	0.00
42.57	2.00	0.00	0.00	0.01	0.00	42.58	2.00	0.00	0.00	0.01	0.00
42.59	2.00	0.00	0.00	0.01	0.00	42.60	2.00	0.00	0.00	0.01	0.00
42.61	2.00	0.00	0.00	0.01	0.00	42.62	2.00	0.00	0.00	0.01	0.00
42.63	2.00	0.00	0.00	0.01	0.00	42.64	2.00	0.00	0.00	0.01	0.00
42.65	2.00	0.00	0.00	0.01	0.00	42.66	2.00	0.00	0.00	0.01	0.00
42.67	2.00	0.00	0.00	0.01	0.00	42.68	2.00	0.00	0.00	0.01	0.00
42.69	2.00	0.00	0.00	0.01	0.00	42.70	2.00	0.00	0.00	0.01	0.00
42.71	2.00	0.00	0.00	0.01	0.00	42.72	2.00	0.00	0.00	0.01	0.00
42.73	2.00	0.00	0.00	0.01	0.00	42.74	2.00	0.00	0.00	0.01	0.00
42.75	2.00	0.00	0.00	0.01	0.00	42.76	2.00	0.00	0.00	0.01	0.00
42.77	2.00	0.00	0.00	0.01	0.00	42.78	2.00	0.00	0.00	0.01	0.00
42.79	2.00	0.00	0.00	0.01	0.00	42.80	2.00	0.00	0.00	0.01	0.00
42.81	2.00	0.00	0.00	0.01	0.00	42.82	2.00	0.00	0.00	0.01	0.00
42.83	2.00	0.00	0.00	0.01	0.00	42.84	2.00	0.00	0.00	0.01	0.00
42.85	2.00	0.00	0.00	0.01	0.00	42.86	2.00	0.00	0.00	0.01	0.00
42.87	2.00	0.00	0.00	0.01	0.00	42.88	2.00	0.00	0.00	0.01	0.00
42.89	2.00	0.00	0.00	0.01	0.00	42.90	2.00	0.00	0.00	0.01	0.00
42.91	2.00	0.00	0.00	0.01	0.00	42.92	2.00	0.00	0.00	0.01	0.00
42.93	2.00	0.00	0.00	0.01	0.00	42.94	0.16	0.84	0.26	0.01	0.01
42.95	0.16	0.84	0.26	0.01	0.01	42.96	0.16	0.84	0.26	0.01	0.01
42.97	0.16	0.84	0.26	0.01	0.01	42.98	0.17	0.83	0.26	0.01	0.01
42.99	0.17	0.83	0.26	0.01	0.01	43.00	0.17	0.83	0.27	0.01	0.01
43.01	0.17	0.83	0.27	0.01	0.01	43.02	0.17	0.83	0.27	0.01	0.01
43.03	0.17	0.83	0.27	0.01	0.01	43.04	0.17	0.83	0.27	0.01	0.01
43.05	0.17	0.83	0.27	0.01	0.01	43.06	0.17	0.83	0.27	0.01	0.01
43.07	0.17	0.83	0.27	0.01	0.01	43.08	0.17	0.83	0.27	0.01	0.01
43.09	0.17	0.83	0.27	0.01	0.01	43.10	0.17	0.83	0.27	0.01	0.01
43.11	0.17	0.83	0.27	0.01	0.01	43.12	0.17	0.83	0.27	0.01	0.01
43.13	0.17	0.83	0.27	0.01	0.01	43.14	0.17	0.83	0.27	0.01	0.01
43.15	0.17	0.83	0.27	0.01	0.01	43.16	0.17	0.83	0.27	0.01	0.01
43.17	0.17	0.83	0.27	0.01	0.01	43.18	0.17	0.83	0.27	0.01	0.01
43.19	0.17	0.83	0.27	0.01	0.01	43.20	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
43.21	2.00	0.00	0.00	0.01	0.00	43.22	2.00	0.00	0.00	0.01	0.00
43.23	2.00	0.00	0.00	0.01	0.00	43.24	2.00	0.00	0.00	0.01	0.00
43.25	2.00	0.00	0.00	0.01	0.00	43.26	2.00	0.00	0.00	0.01	0.00
43.27	2.00	0.00	0.00	0.01	0.00	43.28	2.00	0.00	0.00	0.01	0.00
43.29	2.00	0.00	0.00	0.01	0.00	43.30	2.00	0.00	0.00	0.01	0.00
43.31	2.00	0.00	0.00	0.01	0.00	43.32	2.00	0.00	0.00	0.01	0.00
43.33	2.00	0.00	0.00	0.01	0.00	43.34	2.00	0.00	0.00	0.01	0.00
43.35	2.00	0.00	0.00	0.01	0.00	43.36	2.00	0.00	0.00	0.01	0.00
43.37	2.00	0.00	0.00	0.01	0.00	43.38	2.00	0.00	0.00	0.01	0.00
43.39	2.00	0.00	0.00	0.01	0.00	43.40	2.00	0.00	0.00	0.01	0.00
43.41	2.00	0.00	0.00	0.01	0.00	43.42	2.00	0.00	0.00	0.01	0.00
43.43	2.00	0.00	0.00	0.01	0.00	43.44	2.00	0.00	0.00	0.01	0.00
43.45	2.00	0.00	0.00	0.01	0.00	43.46	2.00	0.00	0.00	0.01	0.00
43.47	2.00	0.00	0.00	0.01	0.00	43.48	2.00	0.00	0.00	0.01	0.00
43.49	2.00	0.00	0.00	0.01	0.00	43.50	2.00	0.00	0.00	0.01	0.00
43.51	2.00	0.00	0.00	0.01	0.00	43.52	2.00	0.00	0.00	0.01	0.00
43.53	2.00	0.00	0.00	0.01	0.00	43.54	2.00	0.00	0.00	0.01	0.00
43.55	2.00	0.00	0.00	0.01	0.00	43.56	2.00	0.00	0.00	0.01	0.00
43.57	2.00	0.00	0.00	0.01	0.00	43.58	2.00	0.00	0.00	0.01	0.00
43.59	2.00	0.00	0.00	0.01	0.00	43.60	2.00	0.00	0.00	0.01	0.00
43.61	0.20	0.80	0.28	0.01	0.01	43.62	0.20	0.80	0.28	0.01	0.01
43.63	0.20	0.80	0.28	0.01	0.01	43.64	0.20	0.80	0.28	0.01	0.01
43.65	0.20	0.80	0.28	0.01	0.01	43.66	0.20	0.80	0.28	0.01	0.01
43.67	0.20	0.80	0.28	0.01	0.01	43.68	2.00	0.00	0.00	0.01	0.00
43.69	2.00	0.00	0.00	0.01	0.00	43.70	2.00	0.00	0.00	0.01	0.00
43.71	2.00	0.00	0.00	0.01	0.00	43.72	2.00	0.00	0.00	0.01	0.00
43.73	2.00	0.00	0.00	0.01	0.00	43.74	2.00	0.00	0.00	0.01	0.00
43.75	2.00	0.00	0.00	0.01	0.00	43.76	2.00	0.00	0.00	0.01	0.00
43.77	2.00	0.00	0.00	0.01	0.00	43.78	2.00	0.00	0.00	0.01	0.00
43.79	2.00	0.00	0.00	0.01	0.00	43.80	2.00	0.00	0.00	0.01	0.00
43.81	2.00	0.00	0.00	0.01	0.00	43.82	2.00	0.00	0.00	0.01	0.00
43.83	2.00	0.00	0.00	0.01	0.00	43.84	2.00	0.00	0.00	0.01	0.00
43.85	2.00	0.00	0.00	0.01	0.00	43.86	2.00	0.00	0.00	0.01	0.00
43.87	2.00	0.00	0.00	0.01	0.00	43.88	2.00	0.00	0.00	0.01	0.00
43.89	2.00	0.00	0.00	0.01	0.00	43.90	2.00	0.00	0.00	0.01	0.00
43.91	2.00	0.00	0.00	0.01	0.00	43.92	2.00	0.00	0.00	0.01	0.00
43.93	2.00	0.00	0.00	0.01	0.00	43.94	2.00	0.00	0.00	0.01	0.00
43.95	2.00	0.00	0.00	0.01	0.00	43.96	2.00	0.00	0.00	0.01	0.00
43.97	2.00	0.00	0.00	0.01	0.00	43.98	2.00	0.00	0.00	0.01	0.00
43.99	2.00	0.00	0.00	0.01	0.00	44.00	2.00	0.00	0.00	0.01	0.00
44.01	2.00	0.00	0.00	0.01	0.00	44.02	2.00	0.00	0.00	0.01	0.00
44.03	2.00	0.00	0.00	0.01	0.00	44.04	2.00	0.00	0.00	0.01	0.00
44.05	2.00	0.00	0.00	0.01	0.00	44.06	2.00	0.00	0.00	0.01	0.00
44.07	2.00	0.00	0.00	0.01	0.00	44.08	2.00	0.00	0.00	0.01	0.00
44.09	2.00	0.00	0.00	0.01	0.00	44.10	2.00	0.00	0.00	0.01	0.00
44.11	2.00	0.00	0.00	0.01	0.00	44.12	2.00	0.00	0.00	0.01	0.00
44.13	2.00	0.00	0.00	0.01	0.00	44.14	2.00	0.00	0.00	0.01	0.00
44.15	2.00	0.00	0.00	0.01	0.00	44.16	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
44.17	2.00	0.00	0.00	0.01	0.00	44.18	2.00	0.00	0.00	0.01	0.00
44.19	2.00	0.00	0.00	0.01	0.00	44.20	2.00	0.00	0.00	0.01	0.00
44.21	2.00	0.00	0.00	0.01	0.00	44.22	2.00	0.00	0.00	0.01	0.00
44.23	2.00	0.00	0.00	0.01	0.00	44.24	2.00	0.00	0.00	0.01	0.00
44.25	2.00	0.00	0.00	0.01	0.00	44.26	2.00	0.00	0.00	0.01	0.00
44.27	2.00	0.00	0.00	0.01	0.00	44.28	2.00	0.00	0.00	0.01	0.00
44.29	2.00	0.00	0.00	0.01	0.00	44.30	2.00	0.00	0.00	0.01	0.00
44.31	2.00	0.00	0.00	0.01	0.00	44.32	2.00	0.00	0.00	0.01	0.00
44.33	2.00	0.00	0.00	0.01	0.00	44.34	2.00	0.00	0.00	0.01	0.00
44.35	2.00	0.00	0.00	0.01	0.00	44.36	2.00	0.00	0.00	0.01	0.00
44.37	2.00	0.00	0.00	0.01	0.00	44.38	2.00	0.00	0.00	0.01	0.00
44.39	2.00	0.00	0.00	0.01	0.00	44.40	2.00	0.00	0.00	0.01	0.00
44.41	2.00	0.00	0.00	0.01	0.00	44.42	2.00	0.00	0.00	0.01	0.00
44.43	2.00	0.00	0.00	0.01	0.00	44.44	2.00	0.00	0.00	0.01	0.00
44.45	2.00	0.00	0.00	0.01	0.00	44.46	2.00	0.00	0.00	0.01	0.00
44.47	2.00	0.00	0.00	0.01	0.00	44.48	2.00	0.00	0.00	0.01	0.00
44.49	2.00	0.00	0.00	0.01	0.00	44.50	2.00	0.00	0.00	0.01	0.00
44.51	2.00	0.00	0.00	0.01	0.00	44.52	2.00	0.00	0.00	0.01	0.00
44.53	2.00	0.00	0.00	0.01	0.00	44.54	2.00	0.00	0.00	0.01	0.00
44.55	2.00	0.00	0.00	0.01	0.00	44.56	2.00	0.00	0.00	0.01	0.00
44.57	2.00	0.00	0.00	0.01	0.00	44.58	2.00	0.00	0.00	0.01	0.00
44.59	2.00	0.00	0.00	0.01	0.00	44.60	2.00	0.00	0.00	0.01	0.00
44.61	2.00	0.00	0.00	0.01	0.00	44.62	2.00	0.00	0.00	0.01	0.00
44.63	2.00	0.00	0.00	0.01	0.00	44.64	2.00	0.00	0.00	0.01	0.00
44.65	2.00	0.00	0.00	0.01	0.00	44.66	2.00	0.00	0.00	0.01	0.00
44.67	2.00	0.00	0.00	0.01	0.00	44.68	2.00	0.00	0.00	0.01	0.00
44.69	2.00	0.00	0.00	0.01	0.00	44.70	2.00	0.00	0.00	0.01	0.00
44.71	2.00	0.00	0.00	0.01	0.00	44.72	2.00	0.00	0.00	0.01	0.00
44.73	2.00	0.00	0.00	0.01	0.00	44.74	2.00	0.00	0.00	0.01	0.00
44.75	2.00	0.00	0.00	0.01	0.00	44.76	2.00	0.00	0.00	0.01	0.00
44.77	2.00	0.00	0.00	0.01	0.00	44.78	2.00	0.00	0.00	0.01	0.00
44.79	2.00	0.00	0.00	0.01	0.00	44.80	2.00	0.00	0.00	0.01	0.00
44.81	0.45	0.00	0.00	0.01	0.01	44.82	0.45	0.00	0.00	0.01	0.01
44.83	0.45	0.00	0.00	0.01	0.01	44.84	0.44	0.00	0.00	0.01	0.01
44.85	0.44	0.00	0.00	0.01	0.01	44.86	0.43	0.00	0.00	0.01	0.01
44.87	0.43	0.00	0.00	0.01	0.01	44.88	0.43	0.00	0.00	0.01	0.01
44.89	0.42	0.00	0.00	0.01	0.01	44.90	0.42	0.00	0.00	0.01	0.01
44.91	0.42	0.00	0.00	0.01	0.01	44.92	0.41	0.00	0.00	0.01	0.01
44.93	0.41	0.00	0.00	0.01	0.01	44.94	0.41	0.00	0.00	0.01	0.01
44.95	0.40	0.00	0.00	0.01	0.01	44.96	0.40	0.00	0.00	0.01	0.01
44.97	0.40	0.00	0.00	0.01	0.01	44.98	0.40	0.00	0.00	0.01	0.01
44.99	0.39	0.00	0.00	0.01	0.01	45.00	0.39	0.00	0.00	0.01	0.01
45.01	0.39	0.00	0.00	0.01	0.01	45.02	0.39	0.00	0.00	0.01	0.01
45.03	0.39	0.00	0.00	0.01	0.01	45.04	0.39	0.00	0.00	0.01	0.01
45.05	0.38	0.00	0.00	0.01	0.01	45.06	0.38	0.00	0.00	0.01	0.01
45.07	0.38	0.00	0.00	0.01	0.01	45.08	2.00	0.00	0.00	0.01	0.00
45.09	2.00	0.00	0.00	0.01	0.00	45.10	2.00	0.00	0.00	0.01	0.00
45.11	2.00	0.00	0.00	0.01	0.00	45.12	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
45.13	2.00	0.00	0.00	0.01	0.00	45.14	2.00	0.00	0.00	0.01	0.00
45.15	2.00	0.00	0.00	0.01	0.00	45.16	2.00	0.00	0.00	0.01	0.00
45.17	2.00	0.00	0.00	0.01	0.00	45.18	2.00	0.00	0.00	0.01	0.00
45.19	2.00	0.00	0.00	0.01	0.00	45.20	2.00	0.00	0.00	0.01	0.00
45.21	2.00	0.00	0.00	0.01	0.00	45.22	2.00	0.00	0.00	0.01	0.00
45.23	2.00	0.00	0.00	0.01	0.00	45.24	2.00	0.00	0.00	0.01	0.00
45.25	2.00	0.00	0.00	0.01	0.00	45.26	2.00	0.00	0.00	0.01	0.00
45.27	2.00	0.00	0.00	0.01	0.00	45.28	2.00	0.00	0.00	0.01	0.00
45.29	2.00	0.00	0.00	0.01	0.00	45.30	2.00	0.00	0.00	0.01	0.00
45.31	2.00	0.00	0.00	0.01	0.00	45.32	2.00	0.00	0.00	0.01	0.00
45.33	2.00	0.00	0.00	0.01	0.00	45.34	0.32	0.00	0.00	0.01	0.01
45.35	0.32	0.00	0.00	0.01	0.01	45.36	0.32	0.00	0.00	0.01	0.01
45.37	0.32	0.00	0.00	0.01	0.01	45.38	0.31	0.00	0.00	0.01	0.01
45.39	0.31	0.00	0.00	0.01	0.01	45.40	0.31	0.00	0.00	0.01	0.01
45.41	0.31	0.00	0.00	0.01	0.01	45.42	0.31	0.00	0.00	0.01	0.01
45.43	0.31	0.00	0.00	0.01	0.01	45.44	0.31	0.00	0.00	0.01	0.01
45.45	0.31	0.00	0.00	0.01	0.01	45.46	0.31	0.00	0.00	0.01	0.01
45.47	0.31	0.00	0.00	0.01	0.01	45.48	0.31	0.00	0.00	0.01	0.01
45.49	0.31	0.00	0.00	0.01	0.01	45.50	2.00	0.00	0.00	0.01	0.00
45.51	2.00	0.00	0.00	0.01	0.00	45.52	2.00	0.00	0.00	0.01	0.00
45.53	2.00	0.00	0.00	0.01	0.00	45.54	2.00	0.00	0.00	0.01	0.00
45.55	2.00	0.00	0.00	0.01	0.00	45.56	2.00	0.00	0.00	0.01	0.00
45.57	2.00	0.00	0.00	0.01	0.00	45.58	2.00	0.00	0.00	0.01	0.00
45.59	2.00	0.00	0.00	0.01	0.00	45.60	2.00	0.00	0.00	0.01	0.00
45.61	2.00	0.00	0.00	0.01	0.00	45.62	2.00	0.00	0.00	0.01	0.00
45.63	2.00	0.00	0.00	0.01	0.00	45.64	2.00	0.00	0.00	0.01	0.00
45.65	2.00	0.00	0.00	0.01	0.00	45.66	2.00	0.00	0.00	0.01	0.00
45.67	2.00	0.00	0.00	0.01	0.00	45.68	2.00	0.00	0.00	0.01	0.00
45.69	2.00	0.00	0.00	0.01	0.00	45.70	2.00	0.00	0.00	0.01	0.00
45.71	2.00	0.00	0.00	0.01	0.00	45.72	2.00	0.00	0.00	0.01	0.00
45.73	2.00	0.00	0.00	0.01	0.00	45.74	2.00	0.00	0.00	0.01	0.00
45.75	2.00	0.00	0.00	0.01	0.00	45.76	2.00	0.00	0.00	0.01	0.00
45.77	0.41	0.00	0.00	0.01	0.01	45.78	0.42	0.00	0.00	0.01	0.01
45.79	0.42	0.00	0.00	0.01	0.01	45.80	0.42	0.00	0.00	0.01	0.01
45.81	0.42	0.00	0.00	0.01	0.01	45.82	0.42	0.00	0.00	0.01	0.01
45.83	0.43	0.00	0.00	0.01	0.01	45.84	0.43	0.00	0.00	0.01	0.01
45.85	0.43	0.00	0.00	0.01	0.01	45.86	0.43	0.00	0.00	0.01	0.01
45.87	0.44	0.00	0.00	0.01	0.01	45.88	0.44	0.00	0.00	0.01	0.01
45.89	0.44	0.00	0.00	0.01	0.01	45.90	0.45	0.00	0.00	0.01	0.01
45.91	0.45	0.00	0.00	0.01	0.01	45.92	0.45	0.00	0.00	0.01	0.00
45.93	0.46	0.00	0.00	0.01	0.00	45.94	0.46	0.00	0.00	0.01	0.00
45.95	0.47	0.00	0.00	0.01	0.00	45.96	0.47	0.00	0.00	0.01	0.00
45.97	0.48	0.00	0.00	0.01	0.00	45.98	0.49	0.00	0.00	0.01	0.00
45.99	0.49	0.00	0.00	0.01	0.00	46.00	0.50	0.00	0.00	0.01	0.00
46.01	0.51	0.00	0.00	0.01	0.00	46.02	0.51	0.00	0.00	0.01	0.00
46.03	0.52	0.00	0.00	0.01	0.00	46.04	0.52	0.00	0.00	0.01	0.00
46.05	0.53	0.00	0.00	0.01	0.00	46.06	0.53	0.00	0.00	0.01	0.00
46.07	0.54	0.00	0.00	0.01	0.00	46.08	0.54	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
46.09	0.55	0.00	0.00	0.01	0.00	46.10	0.55	0.00	0.00	0.01	0.00
46.11	0.56	0.00	0.00	0.01	0.00	46.12	0.57	0.00	0.00	0.01	0.00
46.13	0.59	0.00	0.00	0.01	0.00	46.14	0.62	0.00	0.00	0.01	0.00
46.15	0.65	0.00	0.00	0.01	0.00	46.16	0.68	0.00	0.00	0.01	0.00
46.17	0.72	0.00	0.00	0.01	0.00	46.18	0.75	0.00	0.00	0.01	0.00
46.19	0.78	0.00	0.00	0.01	0.00	46.20	0.80	0.00	0.00	0.01	0.00
46.21	0.83	0.00	0.00	0.01	0.00	46.22	0.86	0.00	0.00	0.01	0.00
46.23	0.90	0.00	0.00	0.01	0.00	46.24	0.94	0.00	0.00	0.01	0.00
46.25	0.99	0.00	0.00	0.01	0.00	46.26	1.04	0.00	0.00	0.01	0.00
46.27	1.08	0.00	0.00	0.01	0.00	46.28	1.11	0.00	0.00	0.01	0.00
46.29	1.11	0.00	0.00	0.01	0.00	46.30	1.09	0.00	0.00	0.01	0.00
46.31	1.07	0.00	0.00	0.01	0.00	46.32	1.04	0.00	0.00	0.01	0.00
46.33	1.01	0.00	0.00	0.01	0.00	46.34	0.99	0.00	0.00	0.01	0.00
46.35	0.97	0.00	0.00	0.01	0.00	46.36	0.95	0.00	0.00	0.01	0.00
46.37	0.93	0.00	0.00	0.01	0.00	46.38	0.91	0.00	0.00	0.01	0.00
46.39	0.89	0.00	0.00	0.01	0.00	46.40	0.87	0.00	0.00	0.01	0.00
46.41	0.85	0.00	0.00	0.01	0.00	46.42	0.83	0.00	0.00	0.01	0.00
46.43	0.81	0.00	0.00	0.01	0.00	46.44	0.79	0.00	0.00	0.01	0.00
46.45	2.00	0.00	0.00	0.01	0.00	46.46	2.00	0.00	0.00	0.01	0.00
46.47	2.00	0.00	0.00	0.01	0.00	46.48	2.00	0.00	0.00	0.01	0.00
46.49	2.00	0.00	0.00	0.01	0.00	46.50	2.00	0.00	0.00	0.01	0.00
46.51	2.00	0.00	0.00	0.01	0.00	46.52	2.00	0.00	0.00	0.01	0.00
46.53	2.00	0.00	0.00	0.01	0.00	46.54	2.00	0.00	0.00	0.01	0.00
46.55	2.00	0.00	0.00	0.01	0.00	46.56	2.00	0.00	0.00	0.01	0.00
46.57	2.00	0.00	0.00	0.01	0.00	46.58	2.00	0.00	0.00	0.01	0.00
46.59	2.00	0.00	0.00	0.01	0.00	46.60	2.00	0.00	0.00	0.01	0.00
46.61	2.00	0.00	0.00	0.01	0.00	46.62	2.00	0.00	0.00	0.01	0.00
46.63	2.00	0.00	0.00	0.01	0.00	46.64	2.00	0.00	0.00	0.01	0.00
46.65	2.00	0.00	0.00	0.01	0.00	46.66	2.00	0.00	0.00	0.01	0.00
46.67	2.00	0.00	0.00	0.01	0.00	46.68	2.00	0.00	0.00	0.01	0.00
46.69	2.00	0.00	0.00	0.01	0.00	46.70	2.00	0.00	0.00	0.01	0.00
46.71	2.00	0.00	0.00	0.01	0.00	46.72	2.00	0.00	0.00	0.01	0.00
46.73	2.00	0.00	0.00	0.01	0.00	46.74	2.00	0.00	0.00	0.01	0.00
46.75	2.00	0.00	0.00	0.01	0.00	46.76	2.00	0.00	0.00	0.01	0.00
46.77	2.00	0.00	0.00	0.01	0.00	46.78	2.00	0.00	0.00	0.01	0.00
46.79	2.00	0.00	0.00	0.01	0.00	46.80	2.00	0.00	0.00	0.01	0.00
46.81	2.00	0.00	0.00	0.01	0.00	46.82	2.00	0.00	0.00	0.01	0.00
46.83	2.00	0.00	0.00	0.01	0.00	46.84	2.00	0.00	0.00	0.01	0.00
46.85	2.00	0.00	0.00	0.01	0.00	46.86	2.00	0.00	0.00	0.01	0.00
46.87	2.00	0.00	0.00	0.01	0.00	46.88	2.00	0.00	0.00	0.01	0.00
46.89	2.00	0.00	0.00	0.01	0.00	46.90	2.00	0.00	0.00	0.01	0.00
46.91	2.00	0.00	0.00	0.01	0.00	46.92	2.00	0.00	0.00	0.01	0.00
46.93	2.00	0.00	0.00	0.01	0.00	46.94	2.00	0.00	0.00	0.01	0.00
46.95	2.00	0.00	0.00	0.01	0.00	46.96	2.00	0.00	0.00	0.01	0.00
46.97	2.00	0.00	0.00	0.01	0.00	46.98	2.00	0.00	0.00	0.01	0.00
46.99	2.00	0.00	0.00	0.01	0.00	47.00	2.00	0.00	0.00	0.01	0.00
47.01	2.00	0.00	0.00	0.01	0.00	47.02	2.00	0.00	0.00	0.01	0.00
47.03	2.00	0.00	0.00	0.01	0.00	47.04	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
47.05	2.00	0.00	0.00	0.01	0.00	47.06	2.00	0.00	0.00	0.01	0.00
47.07	2.00	0.00	0.00	0.01	0.00	47.08	2.00	0.00	0.00	0.01	0.00
47.09	2.00	0.00	0.00	0.01	0.00	47.10	2.00	0.00	0.00	0.01	0.00
47.11	2.00	0.00	0.00	0.01	0.00	47.12	2.00	0.00	0.00	0.01	0.00
47.13	2.00	0.00	0.00	0.01	0.00	47.14	2.00	0.00	0.00	0.01	0.00
47.15	2.00	0.00	0.00	0.01	0.00	47.16	2.00	0.00	0.00	0.01	0.00
47.17	2.00	0.00	0.00	0.01	0.00	47.18	2.00	0.00	0.00	0.01	0.00
47.19	2.00	0.00	0.00	0.01	0.00	47.20	2.00	0.00	0.00	0.01	0.00
47.21	2.00	0.00	0.00	0.01	0.00	47.22	2.00	0.00	0.00	0.01	0.00
47.23	2.00	0.00	0.00	0.01	0.00	47.24	2.00	0.00	0.00	0.01	0.00
47.25	2.00	0.00	0.00	0.01	0.00	47.26	2.00	0.00	0.00	0.01	0.00
47.27	2.00	0.00	0.00	0.01	0.00	47.28	2.00	0.00	0.00	0.01	0.00
47.29	2.00	0.00	0.00	0.01	0.00	47.30	2.00	0.00	0.00	0.01	0.00
47.31	2.00	0.00	0.00	0.01	0.00	47.32	2.00	0.00	0.00	0.01	0.00
47.33	2.00	0.00	0.00	0.01	0.00	47.34	2.00	0.00	0.00	0.01	0.00
47.35	2.00	0.00	0.00	0.01	0.00	47.36	2.00	0.00	0.00	0.01	0.00
47.37	2.00	0.00	0.00	0.01	0.00	47.38	2.00	0.00	0.00	0.01	0.00
47.39	2.00	0.00	0.00	0.01	0.00	47.40	2.00	0.00	0.00	0.01	0.00
47.41	2.00	0.00	0.00	0.01	0.00	47.42	2.00	0.00	0.00	0.01	0.00
47.43	2.00	0.00	0.00	0.01	0.00	47.44	2.00	0.00	0.00	0.01	0.00
47.45	2.00	0.00	0.00	0.01	0.00	47.46	2.00	0.00	0.00	0.01	0.00
47.47	2.00	0.00	0.00	0.01	0.00	47.48	2.00	0.00	0.00	0.01	0.00
47.49	0.19	0.81	0.27	0.01	0.01	47.50	0.19	0.81	0.27	0.01	0.01
47.51	0.19	0.81	0.27	0.01	0.01	47.52	0.19	0.81	0.27	0.01	0.01
47.53	0.19	0.81	0.27	0.01	0.01	47.54	0.19	0.81	0.27	0.01	0.01
47.55	0.19	0.81	0.27	0.01	0.01	47.56	0.19	0.81	0.27	0.01	0.01
47.57	0.19	0.81	0.27	0.01	0.01	47.58	0.19	0.81	0.27	0.01	0.01
47.59	0.19	0.81	0.27	0.01	0.01	47.60	0.19	0.81	0.27	0.01	0.01
47.61	0.19	0.81	0.27	0.01	0.01	47.62	0.19	0.81	0.27	0.01	0.01
47.63	0.18	0.82	0.27	0.01	0.01	47.64	0.18	0.82	0.27	0.01	0.01
47.65	0.18	0.82	0.27	0.01	0.01	47.66	0.18	0.82	0.27	0.01	0.01
47.67	0.18	0.82	0.27	0.01	0.01	47.68	0.18	0.82	0.27	0.01	0.01
47.69	0.19	0.81	0.27	0.01	0.01	47.70	0.19	0.81	0.27	0.01	0.01
47.71	0.19	0.81	0.27	0.01	0.01	47.72	0.19	0.81	0.27	0.01	0.01
47.73	0.19	0.81	0.27	0.01	0.01	47.74	0.19	0.81	0.27	0.01	0.01
47.75	0.19	0.81	0.27	0.01	0.01	47.76	0.19	0.81	0.27	0.01	0.01
47.77	0.19	0.81	0.27	0.01	0.01	47.78	0.19	0.81	0.27	0.01	0.01
47.79	0.19	0.81	0.27	0.01	0.01	47.80	0.19	0.81	0.27	0.01	0.01
47.81	0.19	0.81	0.27	0.01	0.01	47.82	0.19	0.81	0.27	0.01	0.01
47.83	0.19	0.81	0.27	0.01	0.01	47.84	0.19	0.81	0.27	0.01	0.01
47.85	0.19	0.81	0.27	0.01	0.01	47.86	0.19	0.81	0.27	0.01	0.01
47.87	0.19	0.81	0.27	0.01	0.01	47.88	0.19	0.81	0.27	0.01	0.01
47.89	0.19	0.81	0.27	0.01	0.01	47.90	0.19	0.81	0.27	0.01	0.01
47.91	0.18	0.82	0.27	0.01	0.01	47.92	0.18	0.82	0.27	0.01	0.01
47.93	0.18	0.82	0.27	0.01	0.01	47.94	0.18	0.82	0.27	0.01	0.01
47.95	0.18	0.82	0.27	0.01	0.01	47.96	0.18	0.82	0.27	0.01	0.01
47.97	0.18	0.82	0.27	0.01	0.01	47.98	0.18	0.82	0.27	0.01	0.01
47.99	0.18	0.82	0.27	0.01	0.01	48.00	0.18	0.82	0.27	0.01	0.01

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
48.01	0.18	0.82	0.27	0.01	0.01	48.02	0.18	0.82	0.27	0.01	0.01
48.03	0.18	0.82	0.27	0.01	0.01	48.04	0.18	0.82	0.27	0.01	0.01
48.05	0.17	0.83	0.27	0.01	0.01	48.06	0.17	0.83	0.27	0.01	0.01
48.07	0.17	0.83	0.27	0.01	0.01	48.08	0.17	0.83	0.27	0.01	0.01
48.09	2.00	0.00	0.00	0.01	0.00	48.10	2.00	0.00	0.00	0.01	0.00
48.11	2.00	0.00	0.00	0.01	0.00	48.12	2.00	0.00	0.00	0.01	0.00
48.13	2.00	0.00	0.00	0.01	0.00	48.14	2.00	0.00	0.00	0.01	0.00
48.15	2.00	0.00	0.00	0.01	0.00	48.16	2.00	0.00	0.00	0.01	0.00
48.17	2.00	0.00	0.00	0.01	0.00	48.18	2.00	0.00	0.00	0.01	0.00
48.19	2.00	0.00	0.00	0.01	0.00	48.20	2.00	0.00	0.00	0.01	0.00
48.21	2.00	0.00	0.00	0.01	0.00	48.22	2.00	0.00	0.00	0.01	0.00
48.23	2.00	0.00	0.00	0.01	0.00	48.24	2.00	0.00	0.00	0.01	0.00
48.25	2.00	0.00	0.00	0.01	0.00	48.26	2.00	0.00	0.00	0.01	0.00
48.27	2.00	0.00	0.00	0.01	0.00	48.28	2.00	0.00	0.00	0.01	0.00
48.29	2.00	0.00	0.00	0.01	0.00	48.30	2.00	0.00	0.00	0.01	0.00
48.31	2.00	0.00	0.00	0.01	0.00	48.32	2.00	0.00	0.00	0.01	0.00
48.33	2.00	0.00	0.00	0.01	0.00	48.34	2.00	0.00	0.00	0.01	0.00
48.35	2.00	0.00	0.00	0.01	0.00	48.36	2.00	0.00	0.00	0.01	0.00
48.37	2.00	0.00	0.00	0.01	0.00	48.38	2.00	0.00	0.00	0.01	0.00
48.39	2.00	0.00	0.00	0.01	0.00	48.40	2.00	0.00	0.00	0.01	0.00
48.41	2.00	0.00	0.00	0.01	0.00	48.42	2.00	0.00	0.00	0.01	0.00
48.43	2.00	0.00	0.00	0.01	0.00	48.44	2.00	0.00	0.00	0.01	0.00
48.45	2.00	0.00	0.00	0.01	0.00	48.46	2.00	0.00	0.00	0.01	0.00
48.47	2.00	0.00	0.00	0.01	0.00	48.48	2.00	0.00	0.00	0.01	0.00
48.49	2.00	0.00	0.00	0.01	0.00	48.50	2.00	0.00	0.00	0.01	0.00
48.51	2.00	0.00	0.00	0.01	0.00	48.52	2.00	0.00	0.00	0.01	0.00
48.53	2.00	0.00	0.00	0.01	0.00	48.54	0.18	0.82	0.27	0.01	0.01
48.55	0.18	0.82	0.27	0.01	0.01	48.56	0.18	0.82	0.27	0.01	0.01
48.57	0.18	0.82	0.27	0.01	0.01	48.58	0.18	0.82	0.27	0.01	0.01
48.59	0.18	0.82	0.27	0.01	0.01	48.60	0.18	0.82	0.27	0.01	0.01
48.61	0.18	0.82	0.27	0.01	0.01	48.62	2.00	0.00	0.00	0.01	0.00
48.63	2.00	0.00	0.00	0.01	0.00	48.64	2.00	0.00	0.00	0.01	0.00
48.65	2.00	0.00	0.00	0.01	0.00	48.66	2.00	0.00	0.00	0.01	0.00
48.67	2.00	0.00	0.00	0.01	0.00	48.68	2.00	0.00	0.00	0.01	0.00
48.69	2.00	0.00	0.00	0.01	0.00	48.70	2.00	0.00	0.00	0.01	0.00
48.71	2.00	0.00	0.00	0.01	0.00	48.72	2.00	0.00	0.00	0.01	0.00
48.73	2.00	0.00	0.00	0.01	0.00	48.74	2.00	0.00	0.00	0.01	0.00
48.75	2.00	0.00	0.00	0.01	0.00	48.76	2.00	0.00	0.00	0.01	0.00
48.77	2.00	0.00	0.00	0.01	0.00	48.78	2.00	0.00	0.00	0.01	0.00
48.79	2.00	0.00	0.00	0.01	0.00	48.80	2.00	0.00	0.00	0.01	0.00
48.81	2.00	0.00	0.00	0.01	0.00	48.82	2.00	0.00	0.00	0.01	0.00
48.83	2.00	0.00	0.00	0.01	0.00	48.84	2.00	0.00	0.00	0.01	0.00
48.85	2.00	0.00	0.00	0.01	0.00	48.86	2.00	0.00	0.00	0.01	0.00
48.87	2.00	0.00	0.00	0.01	0.00	48.88	2.00	0.00	0.00	0.01	0.00
48.89	2.00	0.00	0.00	0.01	0.00	48.90	2.00	0.00	0.00	0.01	0.00
48.91	2.00	0.00	0.00	0.01	0.00	48.92	2.00	0.00	0.00	0.01	0.00
48.93	2.00	0.00	0.00	0.01	0.00	48.94	2.00	0.00	0.00	0.01	0.00
48.95	2.00	0.00	0.00	0.01	0.00	48.96	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
48.97	2.00	0.00	0.00	0.01	0.00	48.98	2.00	0.00	0.00	0.01	0.00
48.99	2.00	0.00	0.00	0.01	0.00	49.00	2.00	0.00	0.00	0.01	0.00
49.01	2.00	0.00	0.00	0.01	0.00	49.02	2.00	0.00	0.00	0.01	0.00
49.03	2.00	0.00	0.00	0.01	0.00	49.04	2.00	0.00	0.00	0.01	0.00
49.05	2.00	0.00	0.00	0.01	0.00	49.06	2.00	0.00	0.00	0.01	0.00
49.07	2.00	0.00	0.00	0.01	0.00	49.08	2.00	0.00	0.00	0.01	0.00
49.09	2.00	0.00	0.00	0.01	0.00	49.10	2.00	0.00	0.00	0.01	0.00
49.11	2.00	0.00	0.00	0.01	0.00	49.12	2.00	0.00	0.00	0.01	0.00
49.13	2.00	0.00	0.00	0.01	0.00	49.14	2.00	0.00	0.00	0.01	0.00
49.15	2.00	0.00	0.00	0.01	0.00	49.16	2.00	0.00	0.00	0.01	0.00
49.17	2.00	0.00	0.00	0.01	0.00	49.18	2.00	0.00	0.00	0.01	0.00
49.19	2.00	0.00	0.00	0.01	0.00	49.20	2.00	0.00	0.00	0.01	0.00
49.21	2.00	0.00	0.00	0.01	0.00	49.22	2.00	0.00	0.00	0.01	0.00
49.23	2.00	0.00	0.00	0.01	0.00	49.24	2.00	0.00	0.00	0.01	0.00
49.25	2.00	0.00	0.00	0.01	0.00	49.26	2.00	0.00	0.00	0.01	0.00
49.27	2.00	0.00	0.00	0.01	0.00	49.28	2.00	0.00	0.00	0.01	0.00
49.29	2.00	0.00	0.00	0.01	0.00	49.30	2.00	0.00	0.00	0.01	0.00
49.31	2.00	0.00	0.00	0.01	0.00	49.32	2.00	0.00	0.00	0.01	0.00
49.33	2.00	0.00	0.00	0.01	0.00	49.34	2.00	0.00	0.00	0.01	0.00
49.35	2.00	0.00	0.00	0.01	0.00	49.36	2.00	0.00	0.00	0.01	0.00
49.37	2.00	0.00	0.00	0.01	0.00	49.38	2.00	0.00	0.00	0.01	0.00
49.39	2.00	0.00	0.00	0.01	0.00	49.40	2.00	0.00	0.00	0.01	0.00
49.41	1.29	0.00	0.00	0.01	0.00	49.42	1.35	0.00	0.00	0.01	0.00
49.43	1.42	0.00	0.00	0.01	0.00	49.44	1.50	0.00	0.00	0.01	0.00
49.45	1.60	0.00	0.00	0.01	0.00	49.46	1.69	0.00	0.00	0.01	0.00
49.47	1.79	0.00	0.00	0.01	0.00	49.48	1.87	0.00	0.00	0.01	0.00
49.49	1.91	0.00	0.00	0.01	0.00	49.50	1.90	0.00	0.00	0.01	0.00
49.51	1.88	0.00	0.00	0.01	0.00	49.52	1.86	0.00	0.00	0.01	0.00
49.53	1.83	0.00	0.00	0.01	0.00	49.54	1.81	0.00	0.00	0.01	0.00
49.55	1.78	0.00	0.00	0.01	0.00	49.56	1.75	0.00	0.00	0.01	0.00
49.57	1.73	0.00	0.00	0.01	0.00	49.58	1.67	0.00	0.00	0.01	0.00
49.59	1.59	0.00	0.00	0.01	0.00	49.60	1.50	0.00	0.00	0.01	0.00
49.61	1.41	0.00	0.00	0.01	0.00	49.62	1.33	0.00	0.00	0.01	0.00
49.63	1.24	0.00	0.00	0.01	0.00	49.64	1.17	0.00	0.00	0.01	0.00
49.65	1.11	0.00	0.00	0.01	0.00	49.66	1.08	0.00	0.00	0.01	0.00
49.67	1.05	0.00	0.00	0.01	0.00	49.68	1.04	0.00	0.00	0.01	0.00
49.69	1.02	0.00	0.00	0.01	0.00	49.70	1.00	0.00	0.00	0.01	0.00
49.71	0.99	0.00	0.00	0.01	0.00	49.72	0.97	0.00	0.00	0.01	0.00
49.73	0.95	0.00	0.00	0.01	0.00	49.74	0.94	0.00	0.00	0.01	0.00
49.75	0.93	0.00	0.00	0.01	0.00	49.76	0.92	0.00	0.00	0.01	0.00
49.77	0.91	0.00	0.00	0.01	0.00	49.78	0.89	0.00	0.00	0.01	0.00
49.79	0.88	0.00	0.00	0.01	0.00	49.80	0.86	0.00	0.00	0.01	0.00
49.81	0.85	0.00	0.00	0.01	0.00	49.82	0.84	0.00	0.00	0.01	0.00
49.83	0.83	0.00	0.00	0.01	0.00	49.84	0.82	0.00	0.00	0.01	0.00
49.85	0.81	0.00	0.00	0.01	0.00	49.86	0.80	0.00	0.00	0.01	0.00
49.87	0.78	0.00	0.00	0.01	0.00	49.88	0.76	0.00	0.00	0.01	0.00
49.89	0.75	0.00	0.00	0.01	0.00	49.90	0.73	0.00	0.00	0.01	0.00
49.91	0.72	0.00	0.00	0.01	0.00	49.92	0.71	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
49.93	0.70	0.00	0.00	0.01	0.00	49.94	0.69	0.00	0.00	0.01	0.00
49.95	0.68	0.00	0.00	0.01	0.00	49.96	0.66	0.00	0.00	0.01	0.00
49.97	0.65	0.00	0.00	0.01	0.00	49.98	0.64	0.00	0.00	0.01	0.00
49.99	0.63	0.00	0.00	0.01	0.00	50.00	0.62	0.00	0.00	0.01	0.00

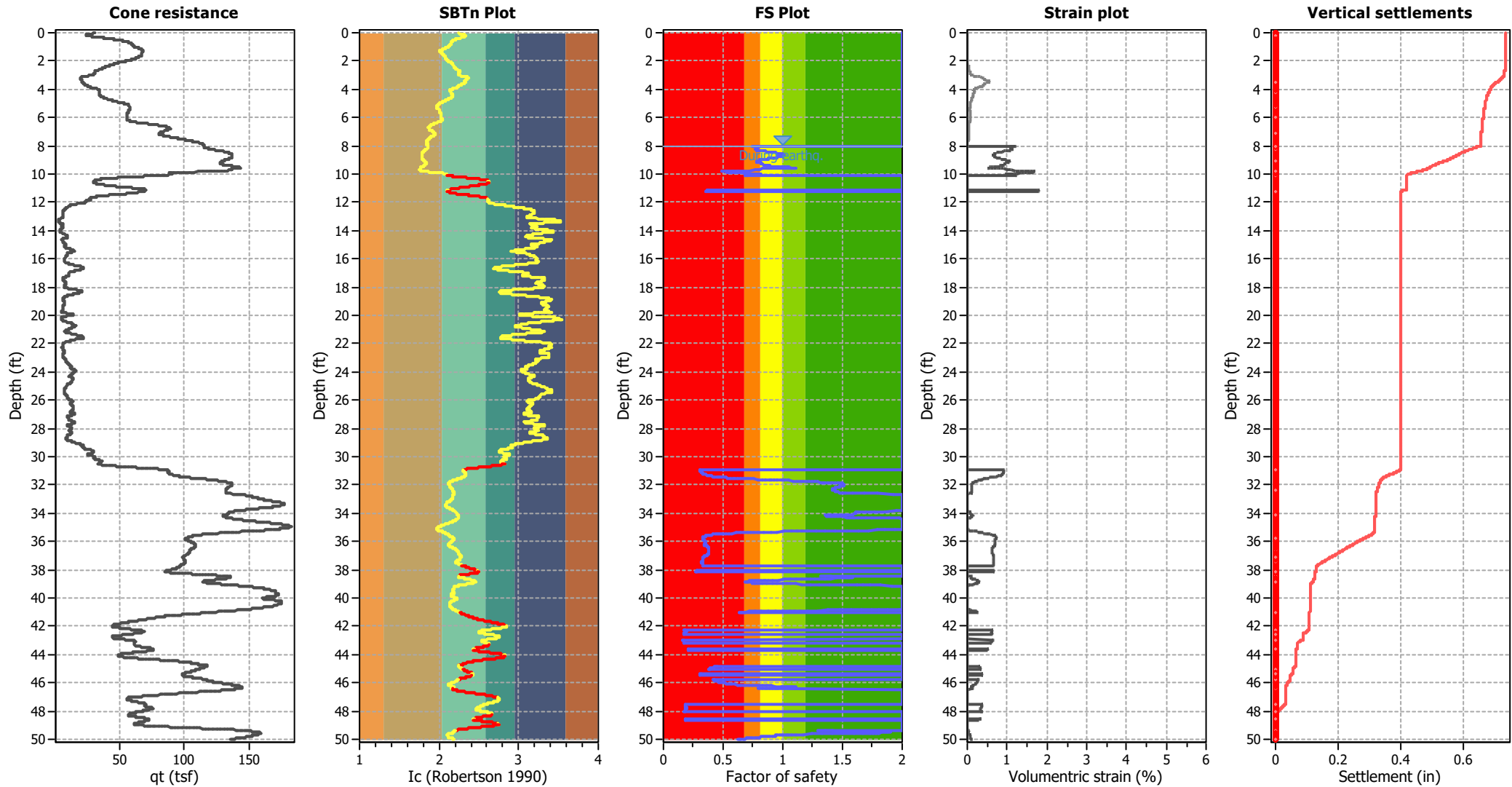
Overall liquefaction potential: 5.36LPI_{ISH} > 5.0 - Liquefaction manifestation is expected**Abbreviations**

FS: Calculated factor of safety for test point

d_z: Layer thickness (ft)

LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

- q_c : Total cone resistance (cone resistance q_c corrected for pore water effects)
- I_c : Soil Behaviour Type Index
- FS: Calculated Factor of Safety against liquefaction
- Volumetric strain: Post-liquefaction volumetric strain

:: Post-earthquake settlement of dry sands ::												
Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
0.01	2.25	49.66	1.76	87.50	20	482	0.56	0.000	0.00	13.69	0.00	0.000
0.02	2.25	49.40	1.75	86.63	20	478	0.56	0.000	0.00	13.69	0.00	0.000
0.03	2.25	49.03	1.74	85.42	20	472	0.56	0.000	0.00	13.69	0.00	0.000
0.04	2.24	48.58	1.74	84.36	19	467	0.56	0.000	0.00	13.69	0.00	0.000
0.05	2.25	47.86	1.74	83.32	19	461	0.56	0.000	0.00	13.69	0.00	0.000
0.06	2.25	46.79	1.76	82.16	19	453	0.56	0.000	0.00	13.69	0.00	0.000
0.07	2.26	45.46	1.78	80.81	19	444	0.56	0.000	0.00	13.69	0.00	0.000
0.08	2.27	44.01	1.80	79.35	18	434	0.56	0.001	0.00	13.69	0.00	0.000
0.09	2.27	42.51	1.83	77.86	18	424	0.56	0.001	0.00	13.69	0.00	0.000
0.10	2.28	41.03	1.86	76.42	18	414	0.56	0.001	0.00	13.69	0.00	0.000
0.11	2.29	39.66	1.89	75.09	18	405	0.56	0.001	0.00	13.69	0.00	0.000
0.12	2.30	38.47	1.92	73.96	17	396	0.56	0.001	0.00	13.69	0.00	0.000
0.13	2.31	37.81	1.95	73.58	17	393	0.56	0.001	0.00	13.69	0.00	0.000
0.14	2.31	37.64	1.97	74.00	17	393	0.56	0.001	0.00	13.69	0.00	0.000
0.15	2.32	37.89	1.98	75.16	18	398	0.56	0.001	0.00	13.69	0.00	0.000
0.16	2.32	38.18	2.00	76.49	18	404	0.56	0.001	0.00	13.69	0.00	0.000
0.17	2.33	38.49	2.02	77.92	19	410	0.56	0.001	0.00	13.69	0.00	0.000
0.18	2.33	38.80	2.05	79.38	19	416	0.56	0.001	0.00	13.69	0.00	0.000
0.19	2.34	39.11	2.07	80.78	19	422	0.56	0.002	0.00	13.69	0.00	0.000
0.20	2.34	39.38	2.08	82.07	20	427	0.56	0.002	0.00	13.69	0.00	0.000
0.21	2.34	39.69	2.10	83.21	20	432	0.56	0.002	0.00	13.69	0.00	0.000
0.22	2.34	40.24	2.10	84.40	20	438	0.56	0.002	0.00	13.69	0.00	0.000
0.23	2.34	41.11	2.09	85.80	21	446	0.56	0.002	0.00	13.69	0.00	0.000
0.24	2.34	42.29	2.07	87.52	21	456	0.56	0.002	0.00	13.69	0.00	0.000
0.25	2.33	43.61	2.05	89.46	21	468	0.56	0.002	0.00	13.69	0.00	0.000
0.26	2.33	45.00	2.03	91.52	22	480	0.56	0.002	0.00	13.69	0.00	0.000
0.27	2.32	46.39	2.02	93.59	22	493	0.56	0.002	0.00	13.69	0.00	0.000
0.28	2.32	47.71	2.00	95.56	23	505	0.56	0.002	0.00	13.69	0.00	0.000
0.29	2.32	48.88	1.99	97.33	23	515	0.56	0.002	0.00	13.69	0.00	0.000
0.30	2.31	49.91	1.98	98.77	23	524	0.56	0.002	0.00	13.69	0.00	0.000
0.31	2.31	50.93	1.96	99.99	24	532	0.56	0.002	0.00	13.69	0.00	0.000
0.32	2.30	52.08	1.94	101.16	24	540	0.56	0.002	0.00	13.69	0.00	0.000
0.33	2.30	53.44	1.92	102.50	24	550	0.56	0.002	0.00	13.69	0.00	0.000
0.34	2.29	54.91	1.89	103.98	24	560	0.56	0.002	0.00	13.69	0.00	0.000
0.35	2.28	56.44	1.87	105.51	25	571	0.56	0.002	0.00	13.69	0.00	0.000
0.36	2.28	57.94	1.85	107.04	25	581	0.56	0.002	0.00	13.69	0.00	0.000
0.37	2.27	59.34	1.83	108.47	25	591	0.56	0.002	0.00	13.69	0.00	0.000
0.38	2.27	60.55	1.81	109.72	25	600	0.56	0.002	0.00	13.69	0.00	0.000
0.39	2.26	61.62	1.80	110.71	26	607	0.56	0.002	0.00	13.69	0.00	0.000
0.40	2.26	62.69	1.78	111.55	26	613	0.56	0.002	0.00	13.69	0.00	0.000
0.41	2.25	63.91	1.76	112.40	26	620	0.56	0.002	0.00	13.69	0.00	0.000
0.42	2.24	65.31	1.74	113.38	26	627	0.56	0.002	0.00	13.69	0.00	0.000
0.43	2.24	66.80	1.71	114.44	26	636	0.56	0.002	0.00	13.69	0.00	0.000
0.44	2.23	68.32	1.69	115.54	26	644	0.56	0.002	0.00	13.69	0.00	0.000
0.45	2.22	69.78	1.67	116.61	27	652	0.55	0.002	0.00	13.69	0.00	0.000
0.46	2.22	71.11	1.65	117.60	27	659	0.55	0.002	0.00	13.69	0.00	0.000
0.47	2.21	72.23	1.64	118.47	27	665	0.55	0.002	0.00	13.69	0.00	0.000
0.48	2.21	73.21	1.63	119.29	27	670	0.55	0.002	0.00	13.69	0.00	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
0.49	2.20	74.17	1.62	120.18	27	676	0.55	0.002	0.00	13.69	0.00	0.000
0.50	2.20	75.26	1.61	121.24	27	683	0.55	0.002	0.00	13.69	0.00	0.000
0.51	2.19	76.48	1.60	122.43	28	690	0.55	0.002	0.00	13.69	0.00	0.000
0.52	2.19	77.76	1.59	123.68	28	698	0.55	0.003	0.00	13.69	0.00	0.000
0.53	2.19	79.04	1.58	124.94	28	705	0.55	0.003	0.00	13.69	0.00	0.000
0.54	2.18	80.25	1.57	126.14	28	713	0.55	0.003	0.00	13.69	0.00	0.000
0.55	2.18	81.32	1.56	127.21	28	719	0.55	0.003	0.00	13.69	0.00	0.000
0.56	2.18	82.20	1.56	128.11	29	725	0.55	0.003	0.00	13.69	0.00	0.000
0.57	2.17	82.95	1.55	128.92	29	729	0.55	0.003	0.00	13.69	0.00	0.000
0.58	2.17	83.69	1.55	129.76	29	734	0.55	0.003	0.00	13.69	0.00	0.000
0.59	2.17	84.52	1.55	130.72	29	740	0.55	0.003	0.00	13.69	0.00	0.000
0.60	2.17	85.44	1.54	131.78	29	746	0.55	0.003	0.00	13.69	0.00	0.000
0.61	2.17	86.38	1.54	132.87	30	753	0.55	0.003	0.00	13.69	0.00	0.000
0.62	2.17	87.30	1.53	133.95	30	759	0.55	0.003	0.00	13.69	0.00	0.000
0.63	2.16	88.16	1.53	134.95	30	765	0.55	0.003	0.00	13.69	0.00	0.000
0.64	2.16	88.90	1.53	135.81	30	770	0.55	0.003	0.00	13.69	0.00	0.000
0.65	2.16	89.45	1.53	136.45	30	773	0.55	0.003	0.00	13.69	0.00	0.000
0.66	2.16	89.88	1.52	136.93	30	776	0.55	0.003	0.00	13.69	0.00	0.000
0.67	2.16	90.26	1.52	137.34	30	778	0.55	0.003	0.00	13.69	0.00	0.000
0.68	2.16	90.69	1.52	137.81	31	781	0.55	0.003	0.00	13.69	0.00	0.000
0.69	2.16	91.16	1.52	138.31	31	784	0.55	0.003	0.00	13.69	0.00	0.000
0.70	2.16	91.63	1.52	138.83	31	787	0.55	0.003	0.00	13.69	0.00	0.000
0.71	2.15	92.08	1.51	139.32	31	790	0.55	0.003	0.00	13.69	0.00	0.000
0.72	2.15	92.49	1.51	139.77	31	792	0.55	0.003	0.00	13.69	0.00	0.000
0.73	2.15	92.82	1.51	140.12	31	794	0.55	0.003	0.00	13.69	0.00	0.000
0.74	2.15	93.07	1.51	140.35	31	796	0.55	0.003	0.00	13.69	0.00	0.000
0.75	2.15	93.25	1.51	140.48	31	796	0.55	0.003	0.00	13.69	0.00	0.000
0.76	2.15	93.44	1.50	140.58	31	797	0.55	0.003	0.00	13.69	0.00	0.000
0.77	2.15	93.64	1.50	140.68	31	798	0.55	0.003	0.00	13.69	0.00	0.000
0.78	2.15	93.85	1.50	140.79	31	798	0.55	0.003	0.00	13.69	0.00	0.000
0.79	2.15	94.06	1.50	140.90	31	799	0.55	0.003	0.00	13.69	0.00	0.000
0.80	2.15	94.26	1.50	141.01	31	800	0.55	0.003	0.00	13.69	0.00	0.000
0.81	2.14	94.44	1.49	141.11	31	800	0.55	0.004	0.00	13.69	0.00	0.000
0.82	2.14	94.59	1.49	141.17	31	800	0.55	0.004	0.00	13.69	0.00	0.000
0.83	2.14	94.72	1.49	141.20	31	801	0.55	0.004	0.00	13.69	0.00	0.000
0.84	2.14	94.85	1.49	141.20	31	801	0.55	0.004	0.00	13.69	0.00	0.000
0.85	2.14	95.00	1.49	141.19	31	801	0.55	0.004	0.00	13.69	0.00	0.000
0.86	2.14	95.17	1.48	141.18	31	800	0.55	0.004	0.00	13.69	0.00	0.000
0.87	2.14	95.34	1.48	141.18	31	800	0.55	0.004	0.00	13.69	0.00	0.000
0.88	2.14	95.50	1.48	141.17	31	800	0.55	0.004	0.00	13.69	0.00	0.000
0.89	2.13	95.66	1.48	141.17	31	800	0.55	0.004	0.00	13.69	0.00	0.000
0.90	2.13	95.79	1.47	141.17	31	800	0.55	0.004	0.00	13.69	0.00	0.000
0.91	2.13	95.93	1.47	141.19	31	800	0.55	0.004	0.00	13.69	0.00	0.000
0.92	2.13	96.10	1.47	141.22	31	800	0.55	0.004	0.00	13.69	0.00	0.000
0.93	2.13	96.30	1.47	141.29	31	801	0.55	0.004	0.00	13.69	0.00	0.000
0.94	2.13	96.54	1.46	141.36	31	801	0.55	0.004	0.00	13.69	0.00	0.000
0.95	2.13	96.79	1.46	141.44	31	801	0.55	0.004	0.00	13.69	0.00	0.000
0.96	2.12	97.05	1.46	141.52	31	802	0.55	0.004	0.00	13.69	0.00	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
0.97	2.12	97.30	1.46	141.60	31	802	0.55	0.004	0.00	13.69	0.00	0.000
0.98	2.12	97.52	1.45	141.68	31	802	0.55	0.004	0.00	13.69	0.00	0.000
0.99	2.12	97.74	1.45	141.76	31	802	0.55	0.004	0.00	13.69	0.00	0.000
1.00	2.12	98.05	1.45	141.89	31	803	0.55	0.005	0.00	13.69	0.00	0.000
1.01	2.12	98.49	1.44	142.10	31	804	0.55	0.005	0.00	13.69	0.00	0.000
1.02	2.11	99.07	1.44	142.38	31	805	0.55	0.005	0.00	13.69	0.00	0.000
1.03	2.11	99.70	1.43	142.70	31	806	0.55	0.005	0.00	13.69	0.00	0.000
1.04	2.10	100.37	1.43	143.04	31	808	0.55	0.005	0.00	13.69	0.00	0.000
1.05	2.10	101.03	1.42	143.38	31	809	0.55	0.005	0.00	13.69	0.00	0.000
1.06	2.10	101.65	1.41	143.71	31	810	0.55	0.005	0.00	13.69	0.00	0.000
1.07	2.09	102.21	1.41	144.00	31	811	0.55	0.005	0.00	13.69	0.00	0.000
1.08	2.09	102.67	1.40	144.22	31	811	0.55	0.005	0.00	13.69	0.00	0.000
1.09	2.09	103.10	1.40	144.38	31	812	0.55	0.005	0.00	13.69	0.00	0.000
1.10	2.08	103.54	1.40	144.49	31	811	0.55	0.005	0.00	13.69	0.00	0.000
1.11	2.08	104.06	1.39	144.62	31	811	0.55	0.005	0.00	13.69	0.00	0.000
1.12	2.07	104.62	1.38	144.77	31	811	0.55	0.005	0.00	13.69	0.00	0.000
1.13	2.07	105.20	1.38	144.92	31	810	0.55	0.005	0.00	13.69	0.00	0.000
1.14	2.06	105.76	1.37	145.09	31	809	0.55	0.005	0.00	13.69	0.00	0.000
1.15	2.06	106.29	1.37	145.25	31	809	0.55	0.005	0.00	13.69	0.00	0.000
1.16	2.06	106.74	1.36	145.38	31	808	0.55	0.005	0.00	13.69	0.00	0.000
1.17	2.05	107.09	1.36	145.44	31	807	0.55	0.005	0.00	13.69	0.00	0.000
1.18	2.05	107.38	1.35	145.43	31	806	0.55	0.006	0.00	13.69	0.00	0.000
1.19	2.05	107.67	1.35	145.36	31	804	0.55	0.006	0.00	13.69	0.00	0.000
1.20	2.04	108.01	1.35	145.28	31	802	0.55	0.006	0.00	13.69	0.00	0.000
1.21	2.04	108.36	1.34	145.21	31	800	0.55	0.006	0.00	13.69	0.00	0.000
1.22	2.03	108.72	1.34	145.14	31	797	0.55	0.006	0.00	13.69	0.00	0.000
1.23	2.03	109.06	1.33	145.08	31	795	0.55	0.006	0.00	13.69	0.00	0.000
1.24	2.02	109.37	1.33	145.03	30	792	0.55	0.006	0.00	13.69	0.00	0.000
1.25	2.02	109.61	1.32	144.99	30	791	0.55	0.006	0.00	13.69	0.00	0.000
1.26	2.02	109.75	1.32	144.95	30	789	0.55	0.006	0.00	13.69	0.00	0.000
1.27	2.01	109.80	1.32	144.88	30	788	0.55	0.006	0.00	13.69	0.00	0.000
1.28	2.01	109.82	1.32	144.80	30	787	0.55	0.006	0.00	13.69	0.00	0.000
1.29	2.01	109.84	1.32	144.70	30	786	0.55	0.006	0.00	13.69	0.00	0.000
1.30	2.01	109.86	1.32	144.61	30	785	0.55	0.006	0.00	13.69	0.00	0.000
1.31	2.01	109.88	1.32	144.51	30	784	0.55	0.007	0.00	13.69	0.00	0.000
1.32	2.01	109.90	1.31	144.42	30	783	0.55	0.007	0.00	13.69	0.00	0.000
1.33	2.01	109.91	1.31	144.34	30	782	0.55	0.007	0.00	13.69	0.00	0.000
1.34	2.01	109.87	1.31	144.27	30	782	0.55	0.007	0.00	13.69	0.00	0.000
1.35	2.01	109.73	1.31	144.19	30	782	0.55	0.007	0.00	13.69	0.00	0.000
1.36	2.01	109.48	1.32	144.10	30	782	0.55	0.007	0.00	13.69	0.00	0.000
1.37	2.01	109.17	1.32	143.99	30	783	0.55	0.007	0.00	13.69	0.00	0.000
1.38	2.02	108.83	1.32	143.87	30	784	0.55	0.007	0.00	13.69	0.00	0.000
1.39	2.02	108.49	1.33	143.75	30	785	0.55	0.007	0.00	13.69	0.00	0.000
1.40	2.02	108.15	1.33	143.64	30	786	0.55	0.007	0.00	13.69	0.00	0.000
1.41	2.03	107.84	1.33	143.54	30	787	0.55	0.007	0.00	13.69	0.00	0.000
1.42	2.03	107.58	1.33	143.46	30	787	0.55	0.007	0.00	13.69	0.00	0.000
1.43	2.03	107.42	1.34	143.47	30	788	0.55	0.007	0.00	13.69	0.00	0.000
1.44	2.03	107.35	1.34	143.57	30	789	0.55	0.007	0.00	13.69	0.00	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
1.45	2.04	107.33	1.34	143.75	30	791	0.55	0.007	0.00	13.69	0.00	0.000
1.46	2.04	107.31	1.34	143.97	30	793	0.55	0.007	0.00	13.69	0.00	0.000
1.47	2.04	107.29	1.34	144.19	30	796	0.55	0.007	0.00	13.69	0.00	0.000
1.48	2.04	107.26	1.35	144.43	31	798	0.55	0.007	0.00	13.69	0.00	0.000
1.49	2.04	107.24	1.35	144.65	31	800	0.55	0.007	0.00	13.69	0.00	0.000
1.50	2.05	107.22	1.35	144.86	31	802	0.55	0.007	0.00	13.69	0.00	0.000
1.51	2.05	107.20	1.35	145.03	31	803	0.55	0.008	0.00	13.69	0.00	0.000
1.52	2.05	107.18	1.35	145.16	31	805	0.55	0.008	0.00	13.69	0.00	0.000
1.53	2.05	107.15	1.36	145.28	31	806	0.55	0.008	0.00	13.69	0.00	0.000
1.54	2.05	107.11	1.36	145.42	31	807	0.55	0.008	0.00	13.69	0.00	0.000
1.55	2.05	107.07	1.36	145.56	31	808	0.55	0.008	0.00	13.69	0.00	0.000
1.56	2.06	107.03	1.36	145.72	31	810	0.54	0.008	0.00	13.69	0.00	0.000
1.57	2.06	106.98	1.36	145.87	31	811	0.54	0.008	0.00	13.69	0.00	0.000
1.58	2.06	106.94	1.37	146.02	31	813	0.54	0.008	0.00	13.69	0.00	0.000
1.59	2.06	106.91	1.37	146.15	31	814	0.54	0.008	0.00	13.69	0.00	0.000
1.60	2.06	106.82	1.37	146.19	31	815	0.54	0.008	0.00	13.69	0.00	0.000
1.61	2.06	106.64	1.37	146.09	31	814	0.54	0.008	0.00	13.69	0.00	0.000
1.62	2.06	106.35	1.37	145.86	31	814	0.54	0.008	0.00	13.69	0.00	0.000
1.63	2.07	106.00	1.37	145.57	31	812	0.54	0.008	0.00	13.69	0.00	0.000
1.64	2.07	105.63	1.38	145.26	31	811	0.55	0.008	0.00	13.69	0.00	0.000
1.65	2.07	105.24	1.38	144.94	31	810	0.55	0.008	0.00	13.69	0.00	0.000
1.66	2.07	104.86	1.38	144.63	31	809	0.55	0.008	0.00	13.69	0.00	0.000
1.67	2.07	104.51	1.38	144.35	31	808	0.55	0.008	0.01	13.69	0.00	0.000
1.68	2.07	104.21	1.38	144.10	31	807	0.55	0.009	0.01	13.69	0.00	0.000
1.69	2.07	103.94	1.38	143.86	31	806	0.55	0.009	0.01	13.69	0.00	0.000
1.70	2.08	103.67	1.39	143.60	31	804	0.55	0.009	0.01	13.69	0.00	0.000
1.71	2.08	103.35	1.39	143.28	31	803	0.55	0.009	0.01	13.69	0.00	0.000
1.72	2.08	102.99	1.39	142.93	31	801	0.55	0.009	0.01	13.69	0.00	0.000
1.73	2.08	102.61	1.39	142.55	31	799	0.55	0.009	0.01	13.69	0.01	0.000
1.74	2.08	102.22	1.39	142.16	31	797	0.55	0.009	0.01	13.69	0.01	0.000
1.75	2.08	101.85	1.39	141.80	30	796	0.55	0.009	0.01	13.69	0.01	0.000
1.76	2.08	101.52	1.39	141.47	30	794	0.55	0.009	0.01	13.69	0.01	0.000
1.77	2.08	101.22	1.39	141.16	30	793	0.55	0.009	0.01	13.69	0.01	0.000
1.78	2.08	100.90	1.40	140.80	30	791	0.55	0.010	0.01	13.69	0.01	0.000
1.79	2.08	100.53	1.40	140.34	30	788	0.55	0.010	0.01	13.69	0.01	0.000
1.80	2.08	100.08	1.40	139.77	30	785	0.55	0.010	0.01	13.69	0.01	0.000
1.81	2.08	99.58	1.40	139.14	30	782	0.55	0.010	0.01	13.69	0.01	0.000
1.82	2.09	99.05	1.40	138.49	30	778	0.55	0.010	0.01	13.69	0.01	0.000
1.83	2.09	98.53	1.40	137.83	30	775	0.55	0.010	0.01	13.69	0.01	0.000
1.84	2.09	98.04	1.40	137.22	30	771	0.55	0.010	0.01	13.69	0.01	0.000
1.85	2.09	97.61	1.40	136.68	29	768	0.55	0.010	0.01	13.69	0.01	0.000
1.86	2.09	97.21	1.40	136.19	29	766	0.55	0.011	0.01	13.69	0.01	0.000
1.87	2.09	96.77	1.40	135.66	29	763	0.55	0.011	0.01	13.69	0.01	0.000
1.88	2.09	96.24	1.40	135.03	29	760	0.55	0.011	0.01	13.69	0.01	0.000
1.89	2.09	95.63	1.40	134.30	29	756	0.55	0.011	0.01	13.69	0.01	0.000
1.90	2.09	94.96	1.41	133.51	29	751	0.55	0.011	0.01	13.69	0.01	0.000
1.91	2.09	94.27	1.41	132.70	29	747	0.55	0.011	0.01	13.69	0.01	0.000
1.92	2.09	93.60	1.41	131.91	28	743	0.55	0.012	0.01	13.69	0.01	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
1.93	2.09	92.98	1.41	131.18	28	739	0.55	0.012	0.01	13.69	0.01	0.000
1.94	2.10	92.44	1.41	130.56	28	736	0.55	0.012	0.01	13.69	0.01	0.000
1.95	2.10	91.93	1.41	130.00	28	733	0.55	0.012	0.01	13.69	0.01	0.000
1.96	2.10	91.36	1.42	129.43	28	730	0.55	0.012	0.01	13.69	0.01	0.000
1.97	2.10	90.68	1.42	128.78	28	727	0.55	0.013	0.01	13.69	0.01	0.000
1.98	2.10	89.91	1.42	128.04	28	723	0.55	0.013	0.01	13.69	0.01	0.000
1.99	2.11	89.09	1.43	127.26	28	719	0.55	0.013	0.01	13.69	0.01	0.000
2.00	2.11	88.27	1.43	126.48	27	715	0.55	0.013	0.01	13.69	0.01	0.000
2.01	2.11	87.47	1.44	125.74	27	711	0.55	0.013	0.01	13.69	0.01	0.000
2.02	2.11	86.76	1.44	125.07	27	707	0.55	0.014	0.01	13.69	0.01	0.000
2.03	2.12	86.13	1.45	124.48	27	704	0.55	0.014	0.01	13.69	0.01	0.000
2.04	2.12	85.51	1.45	123.90	27	701	0.55	0.014	0.01	13.69	0.01	0.000
2.05	2.12	84.79	1.45	123.23	27	698	0.55	0.014	0.01	13.69	0.01	0.000
2.06	2.13	83.94	1.46	122.45	27	694	0.55	0.015	0.01	13.69	0.01	0.000
2.07	2.13	82.99	1.46	121.58	27	689	0.55	0.015	0.01	13.69	0.01	0.000
2.08	2.13	82.01	1.47	120.68	26	684	0.55	0.015	0.01	13.69	0.01	0.000
2.09	2.14	81.03	1.48	119.80	26	679	0.55	0.016	0.01	13.69	0.01	0.000
2.10	2.14	80.11	1.49	118.97	26	675	0.55	0.016	0.01	13.69	0.01	0.000
2.11	2.14	79.30	1.49	118.24	26	670	0.55	0.016	0.01	13.69	0.01	0.000
2.12	2.15	78.64	1.50	117.63	26	667	0.55	0.016	0.01	13.69	0.01	0.000
2.13	2.15	78.05	1.50	117.03	26	664	0.55	0.017	0.01	13.69	0.01	0.000
2.14	2.15	77.44	1.50	116.37	26	660	0.55	0.017	0.01	13.69	0.01	0.000
2.15	2.15	76.74	1.51	115.61	26	655	0.55	0.017	0.01	13.69	0.01	0.000
2.16	2.15	75.99	1.51	114.79	25	651	0.55	0.018	0.01	13.69	0.01	0.000
2.17	2.16	75.21	1.52	113.96	25	646	0.55	0.018	0.01	13.69	0.01	0.000
2.18	2.16	74.46	1.52	113.14	25	641	0.55	0.019	0.01	13.69	0.01	0.000
2.19	2.16	73.77	1.52	112.40	25	637	0.55	0.019	0.01	13.69	0.01	0.000
2.20	2.16	73.18	1.53	111.76	25	633	0.55	0.019	0.02	13.69	0.01	0.000
2.21	2.16	72.69	1.53	111.23	25	630	0.55	0.020	0.02	13.69	0.01	0.000
2.22	2.16	72.23	1.53	110.72	25	627	0.55	0.020	0.02	13.69	0.01	0.000
2.23	2.17	71.74	1.54	110.17	24	624	0.55	0.020	0.02	13.69	0.01	0.000
2.24	2.17	71.19	1.54	109.55	24	620	0.56	0.021	0.02	13.69	0.02	0.000
2.25	2.17	70.60	1.54	108.89	24	617	0.56	0.021	0.02	13.69	0.02	0.000
2.26	2.17	70.01	1.55	108.23	24	613	0.56	0.022	0.02	13.69	0.02	0.000
2.27	2.17	69.45	1.55	107.59	24	609	0.56	0.022	0.02	13.69	0.02	0.000
2.28	2.17	68.94	1.55	107.02	24	606	0.56	0.023	0.02	13.69	0.02	0.000
2.29	2.17	68.51	1.56	106.54	24	603	0.56	0.023	0.02	13.69	0.02	0.000
2.30	2.18	68.12	1.56	106.10	24	600	0.56	0.024	0.02	13.69	0.02	0.000
2.31	2.18	67.71	1.56	105.64	24	597	0.56	0.024	0.02	13.69	0.02	0.000
2.32	2.18	67.24	1.56	105.11	23	594	0.56	0.024	0.02	13.69	0.02	0.000
2.33	2.18	66.72	1.57	104.52	23	591	0.56	0.025	0.02	13.69	0.02	0.000
2.34	2.18	66.18	1.57	103.91	23	587	0.56	0.025	0.02	13.69	0.02	0.000
2.35	2.18	65.65	1.57	103.31	23	584	0.56	0.026	0.02	13.69	0.02	0.000
2.36	2.18	65.14	1.58	102.75	23	580	0.56	0.027	0.02	13.69	0.02	0.000
2.37	2.19	64.70	1.58	102.25	23	577	0.56	0.027	0.02	13.69	0.02	0.000
2.38	2.19	64.34	1.58	101.84	23	575	0.56	0.028	0.02	13.69	0.02	0.000
2.39	2.19	64.01	1.59	101.45	23	573	0.56	0.028	0.02	13.69	0.02	0.000
2.40	2.19	63.66	1.59	101.05	23	570	0.56	0.029	0.02	13.69	0.02	0.000

:: Post-earthquake settlement of dry sands :: (continued)												
Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
2.41	2.19	63.26	1.59	100.58	23	567	0.56	0.029	0.03	13.69	0.02	0.000
2.42	2.19	62.84	1.59	100.07	22	564	0.56	0.030	0.03	13.69	0.02	0.000
2.43	2.19	62.40	1.60	99.55	22	561	0.56	0.030	0.03	13.69	0.02	0.000
2.44	2.19	61.97	1.60	99.05	22	558	0.56	0.031	0.03	13.69	0.03	0.000
2.45	2.19	61.58	1.60	98.59	22	556	0.56	0.032	0.03	13.69	0.03	0.000
2.46	2.20	61.24	1.60	98.20	22	553	0.56	0.032	0.03	13.69	0.03	0.000
2.47	2.20	60.94	1.61	97.89	22	551	0.56	0.033	0.03	13.69	0.03	0.000
2.48	2.20	60.63	1.61	97.62	22	550	0.56	0.033	0.03	13.69	0.03	0.000
2.49	2.20	60.28	1.61	97.34	22	548	0.56	0.034	0.03	13.69	0.03	0.000
2.50	2.20	59.88	1.62	97.03	22	546	0.56	0.034	0.03	13.69	0.03	0.000
2.51	2.20	59.46	1.63	96.71	22	543	0.56	0.035	0.03	13.69	0.03	0.000
2.52	2.21	59.04	1.63	96.38	22	541	0.56	0.036	0.03	13.69	0.03	0.000
2.53	2.21	58.63	1.64	96.07	22	539	0.56	0.036	0.03	13.69	0.03	0.000
2.54	2.21	58.27	1.64	95.79	22	537	0.56	0.037	0.03	13.69	0.03	0.000
2.55	2.21	57.94	1.65	95.53	22	535	0.56	0.038	0.03	13.69	0.03	0.000
2.56	2.22	57.58	1.65	95.23	22	533	0.56	0.038	0.03	13.69	0.03	0.000
2.57	2.22	57.15	1.66	94.85	22	531	0.56	0.039	0.04	13.69	0.03	0.000
2.58	2.22	56.64	1.67	94.39	21	528	0.56	0.040	0.04	13.69	0.03	0.000
2.59	2.22	56.07	1.67	93.88	21	524	0.56	0.041	0.04	13.69	0.03	0.000
2.60	2.23	55.48	1.68	93.36	21	521	0.56	0.042	0.04	13.69	0.04	0.000
2.61	2.23	54.89	1.69	92.84	21	517	0.56	0.043	0.04	13.69	0.04	0.000
2.62	2.23	54.34	1.70	92.36	21	514	0.56	0.045	0.04	13.69	0.04	0.000
2.63	2.23	53.86	1.71	91.94	21	511	0.56	0.046	0.04	13.69	0.04	0.000
2.64	2.24	53.44	1.71	91.56	21	509	0.56	0.047	0.04	13.69	0.04	0.000
2.65	2.24	53.04	1.72	91.17	21	506	0.56	0.048	0.05	13.69	0.04	0.000
2.66	2.24	52.58	1.73	90.71	21	503	0.56	0.049	0.05	13.69	0.04	0.000
2.67	2.24	52.06	1.73	90.18	21	499	0.56	0.051	0.05	13.69	0.04	0.000
2.68	2.25	51.49	1.74	89.61	21	496	0.56	0.052	0.05	13.69	0.05	0.000
2.69	2.25	50.91	1.75	89.02	20	492	0.56	0.054	0.05	13.69	0.05	0.000
2.70	2.25	50.34	1.76	88.46	20	488	0.56	0.056	0.05	13.69	0.05	0.000
2.71	2.25	49.83	1.77	87.95	20	484	0.56	0.057	0.06	13.69	0.05	0.000
2.72	2.26	49.41	1.77	87.52	20	482	0.56	0.059	0.06	13.69	0.05	0.000
2.73	2.26	49.15	1.77	87.22	20	480	0.56	0.060	0.06	13.69	0.05	0.000
2.74	2.26	49.03	1.77	87.01	20	479	0.56	0.061	0.06	13.69	0.06	0.000
2.75	2.26	48.98	1.77	86.84	20	478	0.56	0.062	0.06	13.69	0.06	0.000
2.76	2.26	48.93	1.77	86.64	20	477	0.56	0.063	0.06	13.69	0.06	0.000
2.77	2.25	48.88	1.77	86.43	20	476	0.56	0.064	0.06	13.69	0.06	0.000
2.78	2.25	48.83	1.77	86.21	20	475	0.56	0.065	0.07	13.69	0.06	0.000
2.79	2.25	48.78	1.76	86.01	20	474	0.56	0.066	0.07	13.69	0.06	0.000
2.80	2.25	48.74	1.76	85.83	20	473	0.56	0.066	0.07	13.69	0.06	0.000
2.81	2.25	48.70	1.76	85.68	20	472	0.56	0.067	0.07	13.69	0.06	0.000
2.82	2.25	48.66	1.76	85.53	20	472	0.56	0.068	0.07	13.69	0.06	0.000
2.83	2.25	48.63	1.76	85.38	20	471	0.56	0.069	0.07	13.69	0.06	0.000
2.84	2.25	48.59	1.75	85.20	20	470	0.56	0.070	0.07	13.69	0.06	0.000
2.85	2.25	48.55	1.75	85.00	20	469	0.56	0.071	0.07	13.69	0.07	0.000
2.86	2.25	48.51	1.75	84.80	20	468	0.56	0.072	0.07	13.69	0.07	0.000
2.87	2.25	48.46	1.75	84.59	19	467	0.56	0.073	0.08	13.69	0.07	0.000
2.88	2.25	48.42	1.74	84.40	19	467	0.56	0.074	0.08	13.69	0.07	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
2.89	2.25	48.39	1.74	84.24	19	466	0.56	0.075	0.08	13.69	0.07	0.000
2.90	2.25	48.33	1.74	84.04	19	465	0.56	0.076	0.08	13.69	0.07	0.000
2.91	2.24	48.24	1.74	83.78	19	464	0.56	0.077	0.08	13.69	0.07	0.000
2.92	2.24	48.11	1.73	83.41	19	462	0.56	0.079	0.08	13.69	0.08	0.000
2.93	2.24	47.95	1.73	82.99	19	460	0.56	0.081	0.09	13.69	0.08	0.000
2.94	2.24	47.78	1.73	82.53	19	457	0.56	0.083	0.09	13.69	0.08	0.000
2.95	2.24	47.61	1.72	82.06	19	455	0.56	0.085	0.09	13.69	0.08	0.000
2.96	2.24	47.44	1.72	81.61	19	453	0.56	0.087	0.09	13.69	0.09	0.000
2.97	2.24	47.29	1.72	81.20	19	451	0.56	0.089	0.10	13.69	0.09	0.000
2.98	2.24	47.11	1.72	80.81	19	449	0.56	0.092	0.10	13.69	0.09	0.000
2.99	2.24	46.76	1.72	80.33	18	446	0.56	0.094	0.10	13.69	0.09	0.000
3.00	2.24	46.18	1.73	79.69	18	442	0.56	0.099	0.11	13.69	0.10	0.000
3.01	2.25	45.35	1.74	78.84	18	436	0.56	0.105	0.12	13.69	0.11	0.000
3.02	2.25	44.43	1.75	77.90	18	430	0.56	0.112	0.13	13.69	0.12	0.000
3.03	2.26	43.45	1.77	76.91	18	423	0.56	0.120	0.14	13.69	0.13	0.000
3.04	2.26	42.47	1.79	75.93	18	417	0.56	0.129	0.15	13.69	0.14	0.000
3.05	2.27	41.53	1.81	75.00	17	410	0.56	0.139	0.16	13.69	0.15	0.000
3.06	2.27	40.69	1.82	74.18	17	405	0.56	0.149	0.18	13.69	0.16	0.000
3.07	2.28	39.95	1.84	73.51	17	400	0.56	0.158	0.19	13.69	0.17	0.000
3.08	2.28	39.22	1.86	72.96	17	395	0.56	0.168	0.20	13.69	0.18	0.000
3.09	2.29	38.40	1.89	72.44	17	391	0.56	0.179	0.22	13.69	0.20	0.000
3.10	2.30	37.42	1.92	71.88	17	385	0.56	0.192	0.24	13.69	0.21	0.000
3.11	2.31	36.35	1.96	71.28	17	379	0.56	0.209	0.26	13.69	0.23	0.000
3.12	2.32	35.23	2.01	70.67	17	373	0.56	0.229	0.28	13.69	0.26	0.000
3.13	2.33	34.13	2.05	70.09	17	367	0.56	0.251	0.31	13.69	0.28	0.000
3.14	2.34	33.10	2.10	69.56	17	361	0.56	0.275	0.34	13.69	0.31	0.000
3.15	2.35	32.20	2.15	69.11	17	355	0.56	0.299	0.37	13.69	0.34	0.000
3.16	2.36	31.64	2.18	68.84	17	352	0.56	0.317	0.40	13.69	0.36	0.000
3.17	2.36	31.38	2.19	68.72	17	350	0.56	0.327	0.41	13.69	0.37	0.000
3.18	2.36	31.37	2.19	68.71	17	350	0.56	0.330	0.41	13.69	0.37	0.000
3.19	2.36	31.37	2.19	68.71	17	350	0.56	0.332	0.42	13.69	0.38	0.000
3.20	2.36	31.37	2.19	68.71	17	350	0.56	0.335	0.42	13.69	0.38	0.000
3.21	2.36	31.37	2.19	68.71	17	350	0.56	0.338	0.42	13.69	0.38	0.000
3.22	2.36	31.37	2.19	68.71	17	350	0.56	0.340	0.42	13.69	0.38	0.000
3.23	2.36	31.37	2.19	68.71	17	350	0.56	0.343	0.43	13.69	0.39	0.000
3.24	2.36	31.37	2.19	68.70	17	350	0.56	0.346	0.43	13.69	0.39	0.000
3.25	2.36	31.41	2.19	68.64	17	350	0.56	0.348	0.44	13.69	0.39	0.000
3.26	2.36	31.48	2.18	68.52	17	350	0.56	0.351	0.44	13.69	0.40	0.000
3.27	2.36	31.59	2.16	68.34	16	350	0.56	0.354	0.45	13.69	0.40	0.000
3.28	2.35	31.71	2.15	68.14	16	350	0.56	0.358	0.45	13.69	0.41	0.000
3.29	2.35	31.84	2.13	67.93	16	350	0.56	0.361	0.46	13.69	0.41	0.000
3.30	2.35	31.96	2.12	67.72	16	350	0.56	0.364	0.47	13.69	0.42	0.001
3.31	2.34	32.08	2.10	67.52	16	350	0.56	0.368	0.47	13.69	0.43	0.001
3.32	2.34	32.19	2.09	67.34	16	350	0.56	0.371	0.48	13.69	0.43	0.001
3.33	2.34	32.27	2.08	67.17	16	349	0.56	0.375	0.49	13.69	0.44	0.001
3.34	2.34	32.31	2.07	67.00	16	349	0.56	0.380	0.50	13.69	0.45	0.001
3.35	2.34	32.32	2.07	66.80	16	348	0.56	0.386	0.51	13.69	0.46	0.001
3.36	2.33	32.32	2.06	66.56	16	348	0.56	0.394	0.52	13.69	0.47	0.001

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
3.37	2.33	32.32	2.05	66.30	16	347	0.56	0.403	0.53	13.69	0.48	0.001
3.38	2.33	32.31	2.04	66.02	16	346	0.56	0.411	0.55	13.69	0.49	0.001
3.39	2.33	32.31	2.03	65.75	16	345	0.56	0.420	0.56	13.69	0.51	0.001
3.40	2.33	32.31	2.03	65.50	16	344	0.56	0.429	0.58	13.69	0.52	0.001
3.41	2.32	32.31	2.02	65.28	16	344	0.56	0.438	0.59	13.69	0.53	0.001
3.42	2.32	32.31	2.02	65.16	15	343	0.56	0.444	0.60	13.69	0.54	0.001
3.43	2.32	32.31	2.02	65.14	15	343	0.56	0.448	0.61	13.69	0.55	0.001
3.44	2.32	32.31	2.02	65.21	16	343	0.56	0.449	0.61	13.69	0.55	0.001
3.45	2.32	32.31	2.02	65.30	16	344	0.56	0.451	0.61	13.69	0.55	0.001
3.46	2.33	32.31	2.02	65.39	16	344	0.56	0.452	0.61	13.69	0.55	0.001
3.47	2.33	32.31	2.03	65.48	16	344	0.56	0.453	0.61	13.69	0.55	0.001
3.48	2.33	32.31	2.03	65.57	16	344	0.56	0.454	0.61	13.69	0.55	0.001
3.49	2.33	32.30	2.03	65.65	16	345	0.56	0.456	0.61	13.69	0.55	0.001
3.50	2.33	32.32	2.03	65.73	16	345	0.56	0.457	0.61	13.69	0.55	0.001
3.51	2.33	32.39	2.03	65.86	16	346	0.56	0.455	0.61	13.69	0.55	0.001
3.52	2.33	32.54	2.03	66.06	16	347	0.56	0.449	0.60	13.69	0.54	0.001
3.53	2.33	32.76	2.02	66.32	16	349	0.56	0.440	0.58	13.69	0.53	0.001
3.54	2.32	33.00	2.02	66.62	16	351	0.56	0.430	0.57	13.69	0.51	0.001
3.55	2.32	33.25	2.01	66.93	16	353	0.56	0.419	0.55	13.69	0.50	0.001
3.56	2.32	33.51	2.01	67.25	16	355	0.56	0.409	0.54	13.69	0.48	0.001
3.57	2.32	33.75	2.00	67.55	16	357	0.56	0.400	0.52	13.69	0.47	0.001
3.58	2.32	33.97	2.00	67.82	16	358	0.56	0.392	0.51	13.69	0.46	0.001
3.59	2.32	34.17	1.99	68.01	16	360	0.56	0.386	0.50	13.69	0.45	0.001
3.60	2.31	34.40	1.98	68.11	16	361	0.56	0.382	0.49	13.69	0.44	0.001
3.61	2.31	34.68	1.97	68.15	16	362	0.56	0.378	0.49	13.69	0.44	0.001
3.62	2.31	35.02	1.95	68.18	16	364	0.56	0.373	0.48	13.69	0.43	0.001
3.63	2.30	35.39	1.93	68.20	16	365	0.56	0.368	0.48	13.69	0.43	0.001
3.64	2.30	35.77	1.91	68.24	16	367	0.56	0.362	0.47	13.69	0.42	0.001
3.65	2.29	36.15	1.89	68.27	16	368	0.56	0.357	0.47	13.69	0.42	0.001
3.66	2.29	36.51	1.87	68.31	16	369	0.56	0.353	0.46	13.69	0.41	0.000
3.67	2.28	36.81	1.86	68.34	16	371	0.56	0.349	0.46	13.69	0.41	0.000
3.68	2.28	37.06	1.84	68.36	16	371	0.56	0.347	0.46	13.69	0.41	0.000
3.69	2.27	37.27	1.83	68.35	16	372	0.56	0.346	0.46	13.69	0.41	0.000
3.70	2.27	37.47	1.82	68.33	16	373	0.56	0.346	0.46	13.69	0.41	0.000
3.71	2.27	37.70	1.81	68.31	16	373	0.56	0.345	0.46	13.69	0.41	0.000
3.72	2.26	37.96	1.80	68.29	16	374	0.56	0.344	0.46	13.69	0.41	0.000
3.73	2.26	38.21	1.79	68.27	16	375	0.56	0.343	0.46	13.69	0.41	0.000
3.74	2.26	38.46	1.77	68.25	16	375	0.56	0.342	0.46	13.69	0.41	0.000
3.75	2.25	38.69	1.76	68.23	16	376	0.56	0.342	0.46	13.69	0.41	0.000
3.76	2.25	38.89	1.76	68.25	16	377	0.56	0.341	0.46	13.69	0.41	0.000
3.77	2.25	39.10	1.75	68.37	16	378	0.56	0.338	0.45	13.69	0.40	0.000
3.78	2.25	39.36	1.74	68.61	16	379	0.56	0.333	0.44	13.69	0.40	0.000
3.79	2.24	39.69	1.74	68.97	16	382	0.56	0.325	0.43	13.69	0.38	0.000
3.80	2.24	40.05	1.73	69.36	16	384	0.56	0.316	0.42	13.69	0.37	0.000
3.81	2.24	40.44	1.73	69.78	16	387	0.56	0.307	0.40	13.69	0.36	0.000
3.82	2.24	40.82	1.72	70.20	16	390	0.56	0.298	0.39	13.69	0.35	0.000
3.83	2.24	41.18	1.71	70.60	16	392	0.56	0.290	0.37	13.69	0.33	0.000
3.84	2.24	41.51	1.71	70.96	16	394	0.56	0.284	0.36	13.69	0.33	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
3.85	2.23	41.87	1.70	71.32	16	397	0.56	0.277	0.35	13.69	0.32	0.000
3.86	2.23	42.37	1.69	71.77	16	400	0.56	0.268	0.34	13.69	0.30	0.000
3.87	2.23	43.08	1.68	72.38	16	404	0.56	0.256	0.32	13.69	0.29	0.000
3.88	2.22	43.95	1.66	73.12	17	409	0.56	0.243	0.30	13.69	0.27	0.000
3.89	2.21	44.90	1.65	73.95	17	415	0.56	0.229	0.28	13.69	0.25	0.000
3.90	2.21	45.88	1.63	74.82	17	420	0.56	0.216	0.26	13.69	0.24	0.000
3.91	2.20	46.85	1.62	75.68	17	426	0.56	0.204	0.25	13.69	0.22	0.000
3.92	2.19	47.75	1.60	76.49	17	431	0.56	0.194	0.23	13.69	0.21	0.000
3.93	2.19	48.54	1.59	77.20	17	435	0.56	0.186	0.22	13.69	0.20	0.000
3.94	2.19	49.17	1.58	77.74	17	439	0.56	0.181	0.21	13.69	0.19	0.000
3.95	2.18	49.74	1.57	78.16	17	442	0.56	0.177	0.21	13.69	0.19	0.000
3.96	2.18	50.32	1.56	78.54	18	444	0.56	0.173	0.20	13.69	0.18	0.000
3.97	2.17	50.99	1.55	78.99	18	447	0.56	0.169	0.20	13.69	0.18	0.000
3.98	2.17	51.71	1.54	79.47	18	450	0.56	0.165	0.19	13.69	0.17	0.000
3.99	2.16	52.43	1.53	79.97	18	453	0.56	0.161	0.19	13.69	0.17	0.000
4.00	2.16	53.14	1.51	80.47	18	456	0.56	0.158	0.18	13.69	0.16	0.000
4.01	2.15	53.78	1.50	80.92	18	459	0.56	0.155	0.18	13.69	0.16	0.000
4.02	2.15	54.28	1.50	81.27	18	461	0.56	0.153	0.17	13.69	0.15	0.000
4.03	2.14	54.56	1.49	81.46	18	462	0.56	0.152	0.17	13.69	0.15	0.000
4.04	2.14	54.65	1.49	81.48	18	462	0.56	0.153	0.17	13.69	0.15	0.000
4.05	2.14	54.65	1.49	81.42	18	462	0.56	0.154	0.18	13.69	0.16	0.000
4.06	2.14	54.65	1.49	81.35	18	461	0.56	0.156	0.18	13.69	0.16	0.000
4.07	2.14	54.65	1.49	81.27	18	461	0.56	0.157	0.18	13.69	0.16	0.000
4.08	2.14	54.65	1.49	81.20	18	460	0.56	0.159	0.18	13.69	0.16	0.000
4.09	2.14	54.65	1.48	81.13	18	460	0.56	0.160	0.18	13.69	0.16	0.000
4.10	2.14	54.65	1.48	81.06	18	460	0.56	0.162	0.19	13.69	0.16	0.000
4.11	2.14	54.64	1.48	81.03	18	459	0.56	0.163	0.19	13.69	0.17	0.000
4.12	2.14	54.64	1.48	81.04	18	459	0.56	0.164	0.19	13.69	0.17	0.000
4.13	2.14	54.64	1.48	81.09	18	460	0.56	0.164	0.19	13.69	0.17	0.000
4.14	2.14	54.64	1.49	81.15	18	460	0.56	0.164	0.19	13.69	0.17	0.000
4.15	2.14	54.64	1.49	81.22	18	461	0.56	0.165	0.19	13.69	0.17	0.000
4.16	2.14	54.64	1.49	81.30	18	461	0.56	0.165	0.19	13.69	0.17	0.000
4.17	2.14	54.64	1.49	81.37	18	461	0.56	0.165	0.19	13.69	0.17	0.000
4.18	2.14	54.64	1.49	81.44	18	462	0.56	0.165	0.19	13.69	0.17	0.000
4.19	2.14	54.64	1.49	81.50	18	462	0.56	0.166	0.19	13.69	0.17	0.000
4.20	2.14	54.64	1.49	81.58	18	463	0.56	0.166	0.19	13.69	0.17	0.000
4.21	2.15	54.64	1.50	81.71	18	463	0.56	0.166	0.19	13.69	0.17	0.000
4.22	2.15	54.64	1.50	81.89	18	464	0.56	0.165	0.19	13.69	0.17	0.000
4.23	2.15	54.63	1.50	82.10	18	465	0.56	0.164	0.18	13.69	0.16	0.000
4.24	2.15	54.63	1.51	82.33	18	467	0.56	0.163	0.18	13.69	0.16	0.000
4.25	2.15	54.63	1.51	82.55	18	468	0.56	0.162	0.18	13.69	0.16	0.000
4.26	2.16	54.63	1.52	82.78	18	469	0.56	0.161	0.18	13.69	0.16	0.000
4.27	2.16	54.63	1.52	82.98	18	470	0.56	0.160	0.18	13.69	0.16	0.000
4.28	2.16	54.62	1.52	83.15	18	471	0.56	0.160	0.18	13.69	0.16	0.000
4.29	2.16	54.60	1.53	83.29	18	472	0.56	0.160	0.18	13.69	0.16	0.000
4.30	2.16	54.54	1.53	83.42	19	473	0.56	0.159	0.17	13.69	0.15	0.000
4.31	2.16	54.47	1.53	83.56	19	473	0.56	0.159	0.17	13.69	0.15	0.000
4.32	2.17	54.39	1.54	83.71	19	474	0.56	0.159	0.17	13.69	0.15	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
4.33	2.17	54.30	1.54	83.88	19	475	0.56	0.159	0.17	13.69	0.15	0.000
4.34	2.17	54.22	1.55	84.05	19	476	0.56	0.158	0.17	13.69	0.15	0.000
4.35	2.18	54.13	1.56	84.21	19	476	0.56	0.158	0.17	13.69	0.15	0.000
4.36	2.18	54.06	1.56	84.36	19	477	0.56	0.158	0.17	13.69	0.15	0.000
4.37	2.18	54.03	1.56	84.48	19	478	0.56	0.158	0.17	13.69	0.15	0.000
4.38	2.18	54.05	1.57	84.60	19	478	0.56	0.158	0.17	13.69	0.15	0.000
4.39	2.18	54.12	1.57	84.72	19	479	0.56	0.158	0.17	13.69	0.15	0.000
4.40	2.18	54.21	1.57	84.87	19	480	0.56	0.157	0.17	13.69	0.15	0.000
4.41	2.18	54.31	1.57	85.03	19	481	0.56	0.157	0.17	13.69	0.15	0.000
4.42	2.18	54.42	1.57	85.19	19	482	0.56	0.156	0.17	13.69	0.15	0.000
4.43	2.18	54.52	1.57	85.35	19	483	0.56	0.156	0.17	13.69	0.15	0.000
4.44	2.18	54.62	1.57	85.50	19	483	0.56	0.156	0.16	13.69	0.14	0.000
4.45	2.18	54.71	1.57	85.63	19	484	0.56	0.155	0.16	13.69	0.14	0.000
4.46	2.18	54.85	1.56	85.78	19	485	0.56	0.155	0.16	13.69	0.14	0.000
4.47	2.18	55.06	1.56	85.97	19	486	0.56	0.154	0.16	13.69	0.14	0.000
4.48	2.18	55.37	1.56	86.21	19	488	0.56	0.153	0.16	13.69	0.14	0.000
4.49	2.17	55.73	1.55	86.49	19	489	0.56	0.151	0.16	13.69	0.14	0.000
4.50	2.17	56.11	1.55	86.80	19	491	0.56	0.150	0.16	13.69	0.14	0.000
4.51	2.17	56.49	1.54	87.11	19	493	0.56	0.148	0.15	13.69	0.14	0.000
4.52	2.17	56.86	1.54	87.40	19	495	0.56	0.146	0.15	13.69	0.13	0.000
4.53	2.16	57.20	1.53	87.68	19	497	0.56	0.145	0.15	13.69	0.13	0.000
4.54	2.16	57.49	1.53	87.91	20	498	0.56	0.144	0.15	13.69	0.13	0.000
4.55	2.16	57.77	1.53	88.14	20	499	0.56	0.143	0.15	13.69	0.13	0.000
4.56	2.16	58.07	1.52	88.39	20	501	0.56	0.142	0.15	13.69	0.13	0.000
4.57	2.16	58.43	1.52	88.69	20	503	0.56	0.141	0.14	13.69	0.13	0.000
4.58	2.15	58.83	1.51	89.02	20	505	0.56	0.139	0.14	13.69	0.12	0.000
4.59	2.15	59.26	1.51	89.37	20	507	0.56	0.138	0.14	13.69	0.12	0.000
4.60	2.15	59.68	1.50	89.72	20	509	0.56	0.136	0.14	13.69	0.12	0.000
4.61	2.15	60.07	1.50	90.06	20	511	0.56	0.135	0.14	13.69	0.12	0.000
4.62	2.15	60.43	1.50	90.35	20	512	0.56	0.134	0.13	13.69	0.12	0.000
4.63	2.14	60.76	1.49	90.62	20	514	0.56	0.133	0.13	13.69	0.12	0.000
4.64	2.14	61.15	1.49	90.88	20	515	0.56	0.132	0.13	13.69	0.12	0.000
4.65	2.14	61.63	1.48	91.18	20	517	0.56	0.131	0.13	13.69	0.11	0.000
4.66	2.13	62.20	1.47	91.54	20	519	0.56	0.129	0.13	13.69	0.11	0.000
4.67	2.13	62.82	1.46	91.94	20	521	0.56	0.128	0.13	13.69	0.11	0.000
4.68	2.12	63.46	1.46	92.36	20	523	0.55	0.126	0.13	13.69	0.11	0.000
4.69	2.12	64.09	1.45	92.77	20	525	0.55	0.125	0.12	13.69	0.11	0.000
4.70	2.11	64.68	1.44	93.16	20	527	0.55	0.124	0.12	13.69	0.11	0.000
4.71	2.11	65.18	1.43	93.51	20	529	0.55	0.123	0.12	13.69	0.11	0.000
4.72	2.11	65.64	1.43	93.82	20	530	0.55	0.122	0.12	13.69	0.10	0.000
4.73	2.10	66.10	1.42	94.15	20	531	0.55	0.121	0.12	13.69	0.10	0.000
4.74	2.10	66.65	1.42	94.53	20	533	0.55	0.121	0.12	13.69	0.10	0.000
4.75	2.10	67.26	1.41	94.97	21	535	0.55	0.119	0.12	13.69	0.10	0.000
4.76	2.09	67.92	1.41	95.44	21	537	0.55	0.118	0.11	13.69	0.10	0.000
4.77	2.09	68.59	1.40	95.93	21	539	0.55	0.117	0.11	13.69	0.10	0.000
4.78	2.08	69.23	1.39	96.41	21	541	0.55	0.116	0.11	13.69	0.10	0.000
4.79	2.08	69.81	1.39	96.84	21	543	0.55	0.115	0.11	13.69	0.10	0.000
4.80	2.07	70.32	1.38	97.24	21	544	0.55	0.114	0.11	13.69	0.10	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
4.81	2.07	70.81	1.38	97.67	21	546	0.55	0.113	0.11	13.69	0.09	0.000
4.82	2.07	71.37	1.38	98.18	21	548	0.55	0.112	0.11	13.69	0.09	0.000
4.83	2.06	72.02	1.37	98.81	21	551	0.55	0.110	0.10	13.69	0.09	0.000
4.84	2.06	72.76	1.37	99.52	21	554	0.55	0.108	0.10	13.69	0.09	0.000
4.85	2.06	73.53	1.36	100.27	21	558	0.55	0.106	0.10	13.69	0.09	0.000
4.86	2.05	74.29	1.36	101.01	21	561	0.55	0.105	0.10	13.69	0.08	0.000
4.87	2.05	75.01	1.36	101.72	22	564	0.55	0.103	0.09	13.69	0.08	0.000
4.88	2.05	75.65	1.35	102.35	22	567	0.55	0.102	0.09	13.69	0.08	0.000
4.89	2.05	76.24	1.35	102.92	22	569	0.55	0.100	0.09	13.69	0.08	0.000
4.90	2.04	76.86	1.35	103.54	22	572	0.55	0.099	0.09	13.69	0.08	0.000
4.91	2.04	77.60	1.34	104.27	22	575	0.55	0.098	0.09	13.69	0.08	0.000
4.92	2.04	78.47	1.34	105.14	22	579	0.55	0.096	0.08	13.69	0.07	0.000
4.93	2.03	79.42	1.34	106.09	22	583	0.55	0.094	0.08	13.69	0.07	0.000
4.94	2.03	80.40	1.33	107.08	23	587	0.55	0.092	0.08	13.69	0.07	0.000
4.95	2.02	81.35	1.33	108.04	23	591	0.55	0.090	0.08	13.69	0.07	0.000
4.96	2.02	82.24	1.32	108.94	23	595	0.55	0.088	0.08	13.69	0.07	0.000
4.97	2.02	83.00	1.32	109.71	23	598	0.55	0.087	0.07	13.69	0.06	0.000
4.98	2.01	83.61	1.32	110.34	23	600	0.55	0.086	0.07	13.69	0.06	0.000
4.99	2.01	84.17	1.32	110.90	23	603	0.55	0.086	0.07	13.69	0.06	0.000
5.00	2.01	84.74	1.32	111.49	23	605	0.55	0.085	0.07	13.69	0.06	0.000
5.01	2.01	85.39	1.31	112.16	23	608	0.55	0.084	0.07	13.69	0.06	0.000
5.02	2.00	86.09	1.31	112.88	24	611	0.55	0.083	0.07	13.69	0.06	0.000
5.03	2.00	86.80	1.31	113.60	24	613	0.55	0.082	0.07	13.69	0.06	0.000
5.04	2.00	87.47	1.31	114.30	24	616	0.55	0.081	0.07	13.69	0.06	0.000
5.05	2.00	88.09	1.30	114.93	24	619	0.55	0.080	0.06	13.69	0.06	0.000
5.06	2.00	88.57	1.30	115.42	24	621	0.55	0.080	0.06	13.69	0.06	0.000
5.07	1.99	88.90	1.30	115.73	24	622	0.55	0.080	0.06	13.69	0.06	0.000
5.08	1.99	89.12	1.30	115.89	24	622	0.55	0.080	0.06	13.69	0.06	0.000
5.09	1.99	89.31	1.30	115.99	24	621	0.55	0.080	0.06	13.69	0.06	0.000
5.10	1.99	89.52	1.30	116.11	24	621	0.55	0.081	0.06	13.69	0.06	0.000
5.11	1.99	89.74	1.30	116.23	24	621	0.55	0.081	0.06	13.69	0.06	0.000
5.12	1.98	89.96	1.29	116.36	24	621	0.55	0.082	0.07	13.69	0.06	0.000
5.13	1.98	90.17	1.29	116.47	24	620	0.55	0.082	0.07	13.69	0.06	0.000
5.14	1.98	90.35	1.29	116.58	24	620	0.55	0.082	0.07	13.69	0.06	0.000
5.15	1.98	90.50	1.29	116.66	24	620	0.55	0.083	0.07	13.69	0.06	0.000
5.16	1.98	90.62	1.29	116.74	24	620	0.55	0.083	0.07	13.69	0.06	0.000
5.17	1.97	90.74	1.29	116.82	24	620	0.55	0.084	0.07	13.69	0.06	0.000
5.18	1.97	90.87	1.29	116.91	24	620	0.55	0.084	0.07	13.69	0.06	0.000
5.19	1.97	91.01	1.29	117.01	24	620	0.55	0.084	0.07	13.69	0.06	0.000
5.20	1.97	91.16	1.28	117.12	24	620	0.55	0.085	0.07	13.69	0.06	0.000
5.21	1.97	91.31	1.28	117.22	24	620	0.55	0.085	0.07	13.69	0.06	0.000
5.22	1.97	91.44	1.28	117.31	24	619	0.55	0.085	0.07	13.69	0.06	0.000
5.23	1.97	91.56	1.28	117.40	24	619	0.55	0.086	0.07	13.69	0.06	0.000
5.24	1.97	91.68	1.28	117.52	24	620	0.55	0.086	0.07	13.69	0.06	0.000
5.25	1.97	91.82	1.28	117.72	24	621	0.55	0.085	0.07	13.69	0.06	0.000
5.26	1.97	92.00	1.28	117.98	24	623	0.55	0.085	0.07	13.69	0.06	0.000
5.27	1.97	92.19	1.28	118.29	24	625	0.55	0.084	0.07	13.69	0.06	0.000
5.28	1.97	92.40	1.28	118.61	24	627	0.55	0.084	0.07	13.69	0.06	0.000

:: Post-earthquake settlement of dry sands :: (continued)												
Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
5.29	1.97	92.62	1.28	118.94	24	629	0.55	0.083	0.07	13.69	0.06	0.000
5.30	1.97	92.82	1.28	119.25	25	631	0.55	0.083	0.06	13.69	0.06	0.000
5.31	1.97	93.01	1.29	119.53	25	633	0.55	0.082	0.06	13.69	0.06	0.000
5.32	1.97	93.13	1.29	119.74	25	634	0.55	0.082	0.06	13.69	0.06	0.000
5.33	1.97	93.15	1.29	119.85	25	635	0.55	0.082	0.06	13.69	0.05	0.000
5.34	1.98	93.06	1.29	119.87	25	636	0.55	0.081	0.06	13.69	0.05	0.000
5.35	1.98	92.91	1.29	119.86	25	637	0.55	0.081	0.06	13.69	0.05	0.000
5.36	1.98	92.75	1.29	119.84	25	638	0.55	0.081	0.06	13.69	0.05	0.000
5.37	1.98	92.58	1.29	119.82	25	639	0.55	0.081	0.06	13.69	0.05	0.000
5.38	1.99	92.41	1.30	119.80	25	641	0.55	0.081	0.06	13.69	0.05	0.000
5.39	1.99	92.24	1.30	119.78	25	642	0.55	0.081	0.06	13.69	0.05	0.000
5.40	1.99	92.10	1.30	119.77	25	643	0.55	0.081	0.06	13.69	0.05	0.000
5.41	1.99	91.97	1.30	119.74	25	643	0.55	0.081	0.06	13.69	0.05	0.000
5.42	2.00	91.83	1.30	119.68	25	644	0.55	0.081	0.06	13.69	0.05	0.000
5.43	2.00	91.67	1.30	119.60	25	644	0.55	0.081	0.06	13.69	0.05	0.000
5.44	2.00	91.48	1.31	119.50	25	644	0.55	0.081	0.06	13.69	0.05	0.000
5.45	2.00	91.27	1.31	119.39	25	644	0.55	0.081	0.06	13.69	0.05	0.000
5.46	2.00	91.05	1.31	119.28	25	645	0.55	0.081	0.06	13.69	0.05	0.000
5.47	2.01	90.84	1.31	119.17	25	645	0.55	0.082	0.06	13.69	0.05	0.000
5.48	2.01	90.65	1.31	119.07	25	645	0.55	0.082	0.06	13.69	0.05	0.000
5.49	2.01	90.48	1.31	118.99	25	645	0.55	0.082	0.06	13.69	0.05	0.000
5.50	2.01	90.39	1.32	118.94	25	646	0.55	0.082	0.06	13.69	0.05	0.000
5.51	2.01	90.35	1.32	118.92	25	646	0.55	0.083	0.06	13.69	0.05	0.000
5.52	2.01	90.35	1.32	118.92	25	646	0.55	0.083	0.06	13.69	0.06	0.000
5.53	2.01	90.35	1.32	118.92	25	646	0.55	0.083	0.06	13.69	0.06	0.000
5.54	2.01	90.35	1.32	118.91	25	646	0.55	0.083	0.06	13.69	0.06	0.000
5.55	2.01	90.34	1.32	118.91	25	646	0.55	0.084	0.06	13.69	0.06	0.000
5.56	2.01	90.34	1.32	118.91	25	646	0.55	0.084	0.06	13.69	0.06	0.000
5.57	2.01	90.34	1.32	118.91	25	646	0.55	0.084	0.06	13.69	0.06	0.000
5.58	2.01	90.33	1.32	118.89	25	646	0.55	0.085	0.07	13.69	0.06	0.000
5.59	2.01	90.27	1.32	118.83	25	645	0.55	0.085	0.07	13.69	0.06	0.000
5.60	2.01	90.16	1.32	118.72	25	645	0.55	0.086	0.07	13.69	0.06	0.000
5.61	2.01	90.01	1.32	118.57	25	644	0.55	0.086	0.07	13.69	0.06	0.000
5.62	2.01	89.84	1.32	118.40	25	644	0.55	0.087	0.07	13.69	0.06	0.000
5.63	2.01	89.67	1.32	118.22	25	643	0.55	0.087	0.07	13.69	0.06	0.000
5.64	2.01	89.50	1.32	118.05	25	642	0.55	0.088	0.07	13.69	0.06	0.000
5.65	2.01	89.34	1.32	117.88	25	641	0.55	0.089	0.07	13.69	0.06	0.000
5.66	2.01	89.20	1.32	117.74	25	641	0.55	0.089	0.07	13.69	0.06	0.000
5.67	2.02	89.07	1.32	117.62	25	640	0.55	0.090	0.07	13.69	0.06	0.000
5.68	2.02	88.95	1.32	117.52	25	640	0.55	0.090	0.07	13.69	0.06	0.000
5.69	2.02	88.82	1.32	117.43	25	640	0.55	0.091	0.07	13.69	0.06	0.000
5.70	2.02	88.66	1.32	117.32	25	640	0.55	0.091	0.07	13.69	0.06	0.000
5.71	2.02	88.50	1.32	117.21	25	640	0.55	0.091	0.07	13.69	0.06	0.000
5.72	2.02	88.32	1.33	117.09	25	640	0.55	0.092	0.07	13.69	0.06	0.000
5.73	2.02	88.16	1.33	116.97	25	639	0.55	0.092	0.07	13.69	0.06	0.000
5.74	2.02	88.00	1.33	116.87	25	639	0.55	0.093	0.07	13.69	0.06	0.000
5.75	2.02	87.87	1.33	116.78	25	639	0.55	0.093	0.07	13.69	0.06	0.000
5.76	2.03	87.80	1.33	116.75	25	639	0.55	0.093	0.07	13.69	0.06	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
5.77	2.03	87.76	1.33	116.76	25	640	0.55	0.093	0.07	13.69	0.06	0.000
5.78	2.03	87.76	1.33	116.80	25	640	0.55	0.094	0.07	13.69	0.06	0.000
5.79	2.03	87.76	1.33	116.86	25	641	0.55	0.094	0.07	13.69	0.06	0.000
5.80	2.03	87.76	1.33	116.91	25	641	0.55	0.094	0.07	13.69	0.06	0.000
5.81	2.03	87.76	1.33	116.97	25	642	0.55	0.094	0.07	13.69	0.06	0.000
5.82	2.03	87.76	1.33	117.03	25	642	0.55	0.094	0.07	13.69	0.06	0.000
5.83	2.03	87.76	1.33	117.08	25	643	0.55	0.094	0.07	13.69	0.06	0.000
5.84	2.03	87.76	1.33	117.11	25	643	0.55	0.094	0.07	13.69	0.06	0.000
5.85	2.03	87.76	1.33	117.11	25	643	0.55	0.094	0.07	13.69	0.06	0.000
5.86	2.03	87.76	1.33	117.07	25	643	0.55	0.095	0.07	13.69	0.06	0.000
5.87	2.03	87.76	1.33	117.02	25	642	0.55	0.095	0.07	13.69	0.06	0.000
5.88	2.03	87.75	1.33	116.97	25	642	0.55	0.096	0.07	13.69	0.06	0.000
5.89	2.03	87.75	1.33	116.91	25	641	0.55	0.097	0.08	13.69	0.06	0.000
5.90	2.03	87.75	1.33	116.85	25	640	0.55	0.097	0.08	13.69	0.07	0.000
5.91	2.03	87.75	1.33	116.79	25	640	0.55	0.098	0.08	13.69	0.07	0.000
5.92	2.03	87.75	1.33	116.74	25	639	0.55	0.098	0.08	13.69	0.07	0.000
5.93	2.03	87.75	1.33	116.72	25	639	0.55	0.099	0.08	13.69	0.07	0.000
5.94	2.03	87.75	1.33	116.73	25	639	0.55	0.099	0.08	13.69	0.07	0.000
5.95	2.03	87.75	1.33	116.78	25	640	0.55	0.099	0.08	13.69	0.07	0.000
5.96	2.03	87.75	1.33	116.83	25	640	0.55	0.099	0.08	13.69	0.07	0.000
5.97	2.03	87.75	1.33	116.88	25	641	0.55	0.099	0.08	13.69	0.07	0.000
5.98	2.03	87.75	1.33	116.94	25	641	0.55	0.099	0.08	13.69	0.07	0.000
5.99	2.03	87.74	1.33	117.00	25	642	0.55	0.099	0.08	13.69	0.07	0.000
6.00	2.03	87.74	1.33	117.05	25	642	0.55	0.100	0.08	13.69	0.07	0.000
6.01	2.03	87.74	1.33	117.10	25	643	0.55	0.100	0.08	13.69	0.07	0.000
6.02	2.03	87.74	1.34	117.15	25	643	0.55	0.100	0.08	13.69	0.07	0.000
6.03	2.03	87.74	1.34	117.23	25	644	0.55	0.100	0.08	13.69	0.07	0.000
6.04	2.03	87.74	1.34	117.32	25	645	0.55	0.099	0.08	13.69	0.07	0.000
6.05	2.03	87.74	1.34	117.43	25	646	0.55	0.099	0.08	13.69	0.07	0.000
6.06	2.04	87.74	1.34	117.55	25	647	0.55	0.099	0.08	13.69	0.07	0.000
6.07	2.04	87.74	1.34	117.67	25	648	0.55	0.099	0.08	13.69	0.06	0.000
6.08	2.04	87.74	1.34	117.79	25	649	0.55	0.099	0.08	13.69	0.06	0.000
6.09	2.04	87.74	1.34	117.89	25	650	0.55	0.098	0.08	13.69	0.06	0.000
6.10	2.04	87.76	1.34	117.99	25	651	0.55	0.098	0.08	13.69	0.06	0.000
6.11	2.04	87.82	1.34	118.09	25	652	0.55	0.098	0.08	13.69	0.06	0.000
6.12	2.04	87.95	1.34	118.23	25	652	0.55	0.098	0.08	13.69	0.06	0.000
6.13	2.04	88.11	1.34	118.40	25	653	0.55	0.098	0.08	13.69	0.06	0.000
6.14	2.04	88.30	1.34	118.58	25	654	0.55	0.098	0.07	13.69	0.06	0.000
6.15	2.04	88.49	1.34	118.78	25	655	0.55	0.098	0.07	13.69	0.06	0.000
6.16	2.04	88.68	1.34	118.97	25	656	0.55	0.098	0.07	13.69	0.06	0.000
6.17	2.04	88.86	1.34	119.15	25	656	0.55	0.098	0.07	13.69	0.06	0.000
6.18	2.04	89.01	1.34	119.31	25	657	0.55	0.098	0.07	13.69	0.06	0.000
6.19	2.04	89.22	1.34	119.49	25	658	0.55	0.098	0.07	13.69	0.06	0.000
6.20	2.03	89.52	1.34	119.74	25	659	0.55	0.098	0.07	13.69	0.06	0.000
6.21	2.03	89.95	1.34	120.09	25	660	0.55	0.097	0.07	13.69	0.06	0.000
6.22	2.03	90.46	1.33	120.51	25	661	0.55	0.097	0.07	13.69	0.06	0.000
6.23	2.02	91.02	1.33	120.95	25	662	0.55	0.097	0.07	13.69	0.06	0.000
6.24	2.02	91.58	1.33	121.41	25	663	0.55	0.097	0.07	13.69	0.06	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
6.25	2.02	92.13	1.32	121.87	26	664	0.55	0.096	0.07	13.69	0.06	0.000
6.26	2.01	92.64	1.32	122.28	26	666	0.55	0.096	0.07	13.69	0.06	0.000
6.27	2.01	93.10	1.32	122.67	26	667	0.55	0.096	0.07	13.69	0.06	0.000
6.28	2.01	93.67	1.32	123.18	26	668	0.55	0.095	0.07	13.69	0.06	0.000
6.29	2.01	94.44	1.31	123.89	26	671	0.55	0.095	0.07	13.69	0.06	0.000
6.30	2.00	95.45	1.31	124.84	26	674	0.55	0.093	0.07	13.69	0.06	0.000
6.31	2.00	96.59	1.30	125.93	26	677	0.55	0.092	0.07	13.69	0.06	0.000
6.32	1.99	97.80	1.30	127.08	26	681	0.55	0.091	0.07	13.69	0.06	0.000
6.33	1.98	99.02	1.30	128.24	27	685	0.55	0.089	0.06	13.69	0.05	0.000
6.34	1.98	100.18	1.29	129.35	27	688	0.55	0.088	0.06	13.69	0.05	0.000
6.35	1.98	101.22	1.29	130.36	27	692	0.55	0.087	0.06	13.69	0.05	0.000
6.36	1.97	102.16	1.28	131.28	27	695	0.55	0.086	0.06	13.69	0.05	0.000
6.37	1.97	103.15	1.28	132.28	27	698	0.55	0.085	0.06	13.69	0.05	0.000
6.38	1.96	104.32	1.28	133.50	27	703	0.55	0.083	0.06	13.69	0.05	0.000
6.39	1.96	105.73	1.28	134.98	28	708	0.55	0.081	0.06	13.69	0.05	0.000
6.40	1.95	107.29	1.27	136.62	28	715	0.55	0.079	0.05	13.69	0.05	0.000
6.41	1.95	108.90	1.27	138.32	28	721	0.55	0.078	0.05	13.69	0.04	0.000
6.42	1.95	110.50	1.27	140.00	29	727	0.55	0.076	0.05	13.69	0.04	0.000
6.43	1.94	112.00	1.26	141.58	29	733	0.55	0.074	0.05	13.69	0.04	0.000
6.44	1.94	113.32	1.26	142.96	29	738	0.55	0.073	0.05	13.69	0.04	0.000
6.45	1.93	114.45	1.26	144.15	29	743	0.55	0.072	0.05	13.69	0.04	0.000
6.46	1.93	115.55	1.26	145.30	29	747	0.55	0.071	0.04	13.69	0.04	0.000
6.47	1.93	116.76	1.26	146.57	30	751	0.55	0.070	0.04	13.69	0.04	0.000
6.48	1.92	118.16	1.25	148.03	30	757	0.55	0.068	0.04	13.69	0.04	0.000
6.49	1.92	119.67	1.25	149.61	30	763	0.55	0.067	0.04	13.69	0.03	0.000
6.50	1.92	121.21	1.25	151.22	30	768	0.55	0.066	0.04	13.69	0.03	0.000
6.51	1.91	122.71	1.25	152.77	31	774	0.55	0.064	0.04	13.69	0.03	0.000
6.52	1.91	124.08	1.24	154.20	31	779	0.55	0.063	0.04	13.69	0.03	0.000
6.53	1.91	125.25	1.24	155.41	31	784	0.55	0.063	0.04	13.69	0.03	0.000
6.54	1.90	126.25	1.24	156.44	31	788	0.55	0.062	0.04	13.69	0.03	0.000
6.55	1.90	127.22	1.24	157.43	32	791	0.55	0.061	0.04	13.69	0.03	0.000
6.56	1.90	128.28	1.24	158.53	32	795	0.55	0.061	0.03	13.69	0.03	0.000
6.57	1.90	129.49	1.23	159.77	32	800	0.55	0.060	0.03	13.69	0.03	0.000
6.58	1.89	130.76	1.23	161.07	32	804	0.55	0.059	0.03	13.69	0.03	0.000
6.59	1.89	132.04	1.23	162.37	32	809	0.55	0.058	0.03	13.69	0.03	0.000
6.60	1.89	133.26	1.23	163.61	33	814	0.55	0.057	0.03	13.69	0.03	0.000
6.61	1.88	134.36	1.23	164.72	33	818	0.55	0.057	0.03	13.69	0.03	0.000
6.62	1.88	135.24	1.22	165.61	33	821	0.55	0.056	0.03	13.69	0.03	0.000
6.63	1.88	135.94	1.22	166.31	33	824	0.55	0.056	0.03	13.69	0.03	0.000
6.64	1.88	136.56	1.22	166.93	33	826	0.55	0.056	0.03	13.69	0.03	0.000
6.65	1.88	137.23	1.22	167.61	33	828	0.55	0.055	0.03	13.69	0.03	0.000
6.66	1.88	137.97	1.22	168.35	33	831	0.55	0.055	0.03	13.69	0.03	0.000
6.67	1.87	138.74	1.22	169.11	34	834	0.55	0.055	0.03	13.69	0.02	0.000
6.68	1.87	139.50	1.22	169.87	34	837	0.55	0.054	0.03	13.69	0.02	0.000
6.69	1.87	140.21	1.22	170.58	34	839	0.54	0.054	0.03	13.69	0.02	0.000
6.70	1.87	140.84	1.22	171.19	34	842	0.54	0.054	0.03	13.69	0.02	0.000
6.71	1.87	141.26	1.21	171.62	34	843	0.54	0.054	0.03	13.69	0.02	0.000
6.72	1.87	141.50	1.21	171.90	34	844	0.54	0.054	0.03	13.69	0.02	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
6.73	1.87	141.60	1.22	172.07	34	846	0.54	0.054	0.03	13.69	0.02	0.000
6.74	1.87	141.72	1.22	172.25	34	847	0.54	0.054	0.03	13.69	0.02	0.000
6.75	1.87	141.85	1.22	172.46	34	848	0.54	0.053	0.03	13.69	0.02	0.000
6.76	1.87	141.97	1.22	172.66	34	849	0.54	0.053	0.03	13.69	0.02	0.000
6.77	1.87	142.10	1.22	172.86	34	850	0.54	0.053	0.03	13.69	0.02	0.000
6.78	1.87	142.21	1.22	173.04	34	852	0.54	0.053	0.03	13.69	0.02	0.000
6.79	1.87	142.28	1.22	173.18	34	853	0.54	0.053	0.03	13.69	0.02	0.000
6.80	1.87	142.23	1.22	173.20	34	853	0.54	0.053	0.03	13.69	0.02	0.000
6.81	1.87	142.03	1.22	173.10	34	853	0.54	0.053	0.03	13.69	0.02	0.000
6.82	1.88	141.70	1.22	172.90	34	854	0.54	0.054	0.03	13.69	0.02	0.000
6.83	1.88	141.34	1.22	172.68	34	854	0.54	0.054	0.03	13.69	0.02	0.000
6.84	1.88	140.96	1.22	172.44	34	854	0.54	0.054	0.03	13.69	0.02	0.000
6.85	1.88	140.57	1.22	172.20	34	854	0.54	0.054	0.03	13.69	0.02	0.000
6.86	1.88	140.20	1.23	171.96	34	854	0.54	0.054	0.03	13.69	0.02	0.000
6.87	1.89	139.87	1.23	171.75	34	854	0.54	0.054	0.03	13.69	0.02	0.000
6.88	1.89	139.56	1.23	171.54	34	854	0.54	0.054	0.03	13.69	0.02	0.000
6.89	1.89	139.20	1.23	171.29	34	854	0.54	0.054	0.03	13.69	0.02	0.000
6.90	1.89	138.73	1.23	170.97	34	854	0.54	0.054	0.03	13.69	0.02	0.000
6.91	1.90	138.17	1.23	170.56	34	854	0.54	0.055	0.03	13.69	0.02	0.000
6.92	1.90	137.55	1.24	170.12	34	854	0.54	0.055	0.03	13.69	0.02	0.000
6.93	1.90	136.91	1.24	169.65	34	854	0.54	0.055	0.03	13.69	0.02	0.000
6.94	1.91	136.27	1.24	169.18	34	854	0.54	0.055	0.03	13.69	0.02	0.000
6.95	1.91	135.68	1.24	168.73	34	854	0.54	0.055	0.03	13.69	0.02	0.000
6.96	1.91	135.16	1.25	168.34	34	854	0.54	0.055	0.03	13.69	0.02	0.000
6.97	1.92	134.70	1.25	167.98	34	853	0.54	0.056	0.03	13.69	0.02	0.000
6.98	1.92	134.25	1.25	167.61	34	853	0.54	0.056	0.03	13.69	0.02	0.000
6.99	1.92	133.74	1.25	167.17	34	852	0.54	0.056	0.03	13.69	0.03	0.000
7.00	1.92	133.16	1.25	166.67	34	851	0.54	0.056	0.03	13.69	0.03	0.000
7.01	1.93	132.52	1.25	166.12	34	850	0.54	0.057	0.03	13.69	0.03	0.000
7.02	1.93	131.88	1.26	165.56	34	849	0.54	0.057	0.03	13.69	0.03	0.000
7.03	1.93	131.26	1.26	165.01	33	848	0.54	0.057	0.03	13.69	0.03	0.000
7.04	1.93	130.69	1.26	164.51	33	847	0.54	0.058	0.03	13.69	0.03	0.000
7.05	1.94	130.22	1.26	164.11	33	846	0.54	0.058	0.03	13.69	0.03	0.000
7.06	1.94	129.88	1.26	163.83	33	846	0.54	0.058	0.03	13.69	0.03	0.000
7.07	1.94	129.64	1.26	163.66	33	846	0.54	0.058	0.03	13.69	0.03	0.000
7.08	1.94	129.42	1.26	163.52	33	846	0.54	0.059	0.03	13.69	0.03	0.000
7.09	1.94	129.18	1.26	163.37	33	846	0.54	0.059	0.03	13.69	0.03	0.000
7.10	1.94	128.92	1.27	163.22	33	847	0.54	0.059	0.03	13.69	0.03	0.000
7.11	1.95	128.66	1.27	163.06	33	847	0.54	0.059	0.03	13.69	0.03	0.000
7.12	1.95	128.42	1.27	162.91	33	848	0.54	0.059	0.03	13.69	0.03	0.000
7.13	1.95	128.20	1.27	162.77	33	848	0.54	0.059	0.03	13.69	0.03	0.000
7.14	1.95	128.10	1.27	162.73	33	848	0.54	0.059	0.03	13.69	0.03	0.000
7.15	1.95	128.16	1.27	162.83	33	849	0.54	0.059	0.03	13.69	0.03	0.000
7.16	1.95	128.40	1.27	163.10	33	850	0.54	0.059	0.03	13.69	0.03	0.000
7.17	1.95	128.74	1.27	163.46	33	851	0.54	0.059	0.03	13.69	0.03	0.000
7.18	1.95	129.11	1.27	163.85	33	853	0.54	0.059	0.03	13.69	0.03	0.000
7.19	1.95	129.50	1.27	164.26	34	855	0.54	0.059	0.03	13.69	0.03	0.000
7.20	1.95	129.88	1.27	164.66	34	856	0.54	0.058	0.03	13.69	0.03	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
7.21	1.95	130.23	1.27	165.04	34	857	0.54	0.058	0.03	13.69	0.03	0.000
7.22	1.95	130.54	1.27	165.37	34	859	0.54	0.058	0.03	13.69	0.03	0.000
7.23	1.94	130.89	1.27	165.72	34	860	0.54	0.058	0.03	13.69	0.03	0.000
7.24	1.94	131.34	1.26	166.14	34	861	0.54	0.058	0.03	13.69	0.03	0.000
7.25	1.94	131.95	1.26	166.70	34	862	0.54	0.058	0.03	13.69	0.03	0.000
7.26	1.94	132.66	1.26	167.34	34	864	0.54	0.058	0.03	13.69	0.03	0.000
7.27	1.93	133.41	1.26	168.03	34	865	0.54	0.058	0.03	13.69	0.03	0.000
7.28	1.93	134.18	1.26	168.73	34	867	0.54	0.058	0.03	13.69	0.03	0.000
7.29	1.93	134.93	1.26	169.40	34	869	0.54	0.057	0.03	13.69	0.03	0.000
7.30	1.93	135.61	1.25	170.02	34	870	0.54	0.057	0.03	13.69	0.02	0.000
7.31	1.92	136.21	1.25	170.56	34	871	0.54	0.057	0.03	13.69	0.02	0.000
7.32	1.92	136.82	1.25	171.12	35	873	0.54	0.057	0.03	13.69	0.02	0.000
7.33	1.92	137.53	1.25	171.77	35	874	0.54	0.057	0.03	13.69	0.02	0.000
7.34	1.92	138.39	1.25	172.57	35	876	0.54	0.057	0.03	13.69	0.02	0.000
7.35	1.91	139.36	1.24	173.47	35	879	0.54	0.056	0.03	13.69	0.02	0.000
7.36	1.91	140.38	1.24	174.41	35	881	0.54	0.056	0.03	13.69	0.02	0.000
7.37	1.90	141.40	1.24	175.35	35	884	0.54	0.056	0.03	13.69	0.02	0.000
7.38	1.90	142.38	1.24	176.23	35	886	0.54	0.056	0.03	13.69	0.02	0.000
7.39	1.90	143.24	1.24	177.02	35	888	0.54	0.055	0.03	13.69	0.02	0.000
7.40	1.90	144.01	1.23	177.71	36	890	0.54	0.055	0.03	13.69	0.02	0.000
7.41	1.89	144.77	1.23	178.40	36	892	0.54	0.055	0.03	13.69	0.02	0.000
7.42	1.89	145.42	1.23	178.96	36	894	0.54	0.055	0.03	13.69	0.02	0.000
7.43	1.89	146.18	1.23	179.61	36	897	0.54	0.055	0.03	13.69	0.02	0.000
7.44	1.88	147.02	1.23	180.33	36	900	0.54	0.054	0.03	13.69	0.02	0.000
7.45	1.88	147.89	1.22	181.07	36	904	0.54	0.054	0.03	13.69	0.02	0.000
7.46	1.88	148.74	1.22	181.79	36	907	0.54	0.053	0.03	13.69	0.02	0.000
7.47	1.88	149.53	1.22	182.44	36	910	0.54	0.053	0.03	13.69	0.02	0.000
7.48	1.87	150.20	1.22	182.98	36	913	0.54	0.053	0.03	13.69	0.02	0.000
7.49	1.87	150.76	1.22	183.47	36	915	0.54	0.053	0.03	13.69	0.02	0.000
7.50	1.87	151.31	1.22	183.98	36	918	0.54	0.052	0.03	13.69	0.02	0.000
7.51	1.87	151.94	1.21	184.60	37	922	0.54	0.052	0.03	13.69	0.02	0.000
7.52	1.87	152.67	1.21	185.33	37	926	0.54	0.051	0.02	13.69	0.02	0.000
7.53	1.87	153.46	1.21	186.11	37	930	0.54	0.051	0.02	13.69	0.02	0.000
7.54	1.86	154.27	1.21	186.91	37	934	0.54	0.050	0.02	13.69	0.02	0.000
7.55	1.86	155.04	1.21	187.67	37	938	0.54	0.050	0.02	13.69	0.02	0.000
7.56	1.86	155.74	1.21	188.36	37	942	0.54	0.050	0.02	13.69	0.02	0.000
7.57	1.86	156.33	1.21	188.93	37	945	0.54	0.049	0.02	13.69	0.02	0.000
7.58	1.86	156.89	1.21	189.48	37	948	0.54	0.049	0.02	13.69	0.02	0.000
7.59	1.86	157.50	1.21	190.08	38	952	0.54	0.049	0.02	13.69	0.02	0.000
7.60	1.86	158.26	1.21	190.81	38	956	0.54	0.048	0.02	13.69	0.02	0.000
7.61	1.85	159.11	1.20	191.64	38	960	0.54	0.048	0.02	13.69	0.02	0.000
7.62	1.85	160.02	1.20	192.51	38	965	0.54	0.047	0.02	13.69	0.02	0.000
7.63	1.85	160.92	1.20	193.39	38	970	0.54	0.047	0.02	13.69	0.02	0.000
7.64	1.85	161.77	1.20	194.20	38	974	0.54	0.047	0.02	13.69	0.02	0.000
7.65	1.85	162.51	1.20	194.92	38	978	0.54	0.046	0.02	13.69	0.02	0.000
7.66	1.85	163.12	1.20	195.52	38	982	0.54	0.046	0.02	13.69	0.02	0.000
7.67	1.85	163.65	1.20	196.10	39	985	0.54	0.046	0.02	13.69	0.02	0.000
7.68	1.85	164.19	1.20	196.76	39	989	0.54	0.045	0.02	13.69	0.02	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
7.69	1.85	164.84	1.20	197.55	39	994	0.54	0.045	0.02	13.69	0.02	0.000
7.70	1.85	165.56	1.20	198.43	39	999	0.54	0.044	0.02	13.69	0.02	0.000
7.71	1.85	166.30	1.20	199.34	39	1005	0.54	0.044	0.02	13.69	0.02	0.000
7.72	1.85	167.03	1.20	200.24	39	1010	0.54	0.044	0.02	13.69	0.02	0.000
7.73	1.85	167.70	1.20	201.06	40	1015	0.54	0.043	0.02	13.69	0.02	0.000
7.74	1.85	168.27	1.20	201.76	40	1019	0.54	0.043	0.02	13.69	0.02	0.000
7.75	1.85	168.71	1.20	202.32	40	1023	0.54	0.043	0.02	13.69	0.02	0.000
7.76	1.85	169.08	1.20	202.82	40	1026	0.54	0.042	0.02	13.69	0.02	0.000
7.77	1.85	169.47	1.20	203.35	40	1030	0.54	0.042	0.02	13.69	0.02	0.000
7.78	1.85	169.94	1.20	203.98	40	1034	0.54	0.042	0.02	13.69	0.01	0.000
7.79	1.85	170.44	1.20	204.66	40	1038	0.54	0.042	0.02	13.69	0.01	0.000
7.80	1.85	170.95	1.20	205.35	40	1043	0.54	0.041	0.02	13.69	0.01	0.000
7.81	1.85	171.44	1.20	206.01	41	1047	0.54	0.041	0.02	13.69	0.01	0.000
7.82	1.85	171.88	1.20	206.60	41	1051	0.54	0.041	0.02	13.69	0.01	0.000
7.83	1.85	172.22	1.20	207.07	41	1055	0.54	0.040	0.02	13.69	0.01	0.000
7.84	1.85	172.48	1.20	207.40	41	1057	0.54	0.040	0.02	13.69	0.01	0.000
7.85	1.85	172.71	1.20	207.64	41	1059	0.54	0.040	0.02	13.69	0.01	0.000
7.86	1.85	172.97	1.20	207.90	41	1061	0.54	0.040	0.02	13.69	0.01	0.000
7.87	1.85	173.28	1.20	208.19	41	1063	0.54	0.040	0.02	13.69	0.01	0.000
7.88	1.85	173.60	1.20	208.50	41	1065	0.54	0.040	0.02	13.69	0.01	0.000
7.89	1.85	173.93	1.20	208.82	41	1068	0.54	0.040	0.02	13.69	0.01	0.000
7.90	1.85	174.23	1.20	209.11	41	1070	0.54	0.040	0.02	13.69	0.01	0.000
7.91	1.85	174.48	1.20	209.35	41	1072	0.54	0.040	0.02	13.69	0.01	0.000
7.92	1.85	174.62	1.20	209.50	41	1073	0.54	0.040	0.02	13.69	0.01	0.000
7.93	1.85	174.65	1.20	209.57	41	1074	0.54	0.040	0.02	13.69	0.01	0.000
7.94	1.85	174.58	1.20	209.57	41	1075	0.54	0.040	0.02	13.69	0.01	0.000
7.95	1.85	174.49	1.20	209.57	41	1076	0.54	0.040	0.02	13.69	0.01	0.000
7.96	1.85	174.40	1.20	209.58	41	1078	0.54	0.040	0.02	13.69	0.01	0.000
7.97	1.85	174.31	1.20	209.59	41	1079	0.54	0.040	0.02	13.69	0.01	0.000
7.98	1.85	174.23	1.20	209.61	41	1080	0.54	0.040	0.02	13.69	0.01	0.000
7.99	1.85	174.14	1.20	209.61	41	1081	0.54	0.040	0.02	13.69	0.01	0.000

Total estimated settlement: 0.08**Abbreviations**

Q_{tn}: Normalized cone resistance
 K_c: Fines correction factor
 Q_{tn,cs}: Equivalent clean sand normalized cone resistance
 G_{max}: Small strain shear modulus
 CSR: Soil cyclic stress ratio
 γ: Cyclic shear strain
 e_{vol(15)}: Volumetric strain after 15 cycles
 N_c: Equivalent number of cycles
 e_v: Volumetric strain
 Settle.: Calculated settlement

:: Post-earthquake settlement due to soil liquefaction ::

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
8.00	162.49	2.00	0.00	0.85	0.00	8.01	162.63	0.75	1.22	0.85	0.00
8.02	162.80	0.75	1.21	0.85	0.00	8.03	163.04	0.75	1.19	0.85	0.00
8.04	163.31	0.76	1.17	0.85	0.00	8.05	163.60	0.77	1.15	0.85	0.00
8.06	163.90	0.77	1.13	0.85	0.00	8.07	164.19	0.78	1.11	0.85	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
8.08	164.45	0.79	1.10	0.85	0.00	8.09	164.62	0.79	1.08	0.85	0.00
8.10	164.71	0.79	1.08	0.85	0.00	8.11	164.80	0.79	1.07	0.85	0.00
8.12	164.82	0.79	1.07	0.85	0.00	8.13	164.84	0.79	1.07	0.85	0.00
8.14	164.87	0.79	1.07	0.85	0.00	8.15	164.89	0.79	1.07	0.85	0.00
8.16	164.92	0.79	1.07	0.85	0.00	8.17	164.94	0.79	1.07	0.85	0.00
8.18	164.88	0.79	1.07	0.85	0.00	8.19	164.80	0.79	1.08	0.85	0.00
8.20	164.72	0.79	1.09	0.85	0.00	8.21	164.61	0.78	1.10	0.85	0.00
8.22	164.49	0.78	1.11	0.85	0.00	8.23	164.38	0.78	1.11	0.85	0.00
8.24	164.28	0.77	1.12	0.85	0.00	8.25	164.20	0.77	1.13	0.85	0.00
8.26	164.14	0.77	1.13	0.85	0.00	8.27	164.07	0.77	1.14	0.85	0.00
8.28	164.14	0.77	1.14	0.85	0.00	8.29	164.30	0.77	1.13	0.85	0.00
8.30	164.50	0.78	1.11	0.85	0.00	8.31	164.73	0.78	1.10	0.85	0.00
8.32	164.99	0.79	1.08	0.85	0.00	8.33	165.26	0.79	1.06	0.85	0.00
8.34	165.52	0.80	1.04	0.85	0.00	8.35	165.75	0.80	1.03	0.85	0.00
8.36	165.95	0.81	1.02	0.85	0.00	8.37	166.20	0.82	1.00	0.85	0.00
8.38	166.53	0.82	0.98	0.85	0.00	8.39	166.91	0.83	0.96	0.85	0.00
8.40	167.33	0.84	0.93	0.85	0.00	8.41	167.76	0.86	0.91	0.85	0.00
8.42	168.17	0.87	0.88	0.85	0.00	8.43	168.55	0.88	0.86	0.85	0.00
8.44	168.87	0.89	0.84	0.85	0.00	8.45	169.05	0.89	0.83	0.85	0.00
8.46	169.29	0.90	0.82	0.85	0.00	8.47	169.59	0.91	0.80	0.85	0.00
8.48	169.91	0.92	0.79	0.85	0.00	8.49	170.24	0.93	0.77	0.85	0.00
8.50	170.57	0.94	0.75	0.85	0.00	8.51	170.88	0.94	0.74	0.85	0.00
8.52	171.14	0.95	0.72	0.85	0.00	8.53	171.33	0.96	0.71	0.84	0.00
8.54	171.44	0.96	0.71	0.84	0.00	8.55	171.59	0.97	0.70	0.84	0.00
8.56	171.77	0.97	0.69	0.84	0.00	8.57	171.96	0.98	0.68	0.84	0.00
8.58	172.16	0.98	0.67	0.84	0.00	8.59	172.35	0.99	0.66	0.84	0.00
8.60	172.51	1.00	0.66	0.84	0.00	8.61	172.65	1.00	0.65	0.84	0.00
8.62	172.72	1.00	0.65	0.84	0.00	8.63	172.74	1.00	0.65	0.84	0.00
8.64	172.78	1.00	0.65	0.84	0.00	8.65	172.82	1.00	0.64	0.84	0.00
8.66	172.87	1.01	0.64	0.84	0.00	8.67	172.91	1.01	0.64	0.84	0.00
8.68	172.96	1.01	0.64	0.84	0.00	8.69	172.99	1.01	0.64	0.84	0.00
8.70	173.00	1.01	0.64	0.84	0.00	8.71	172.94	1.01	0.64	0.84	0.00
8.72	172.85	1.00	0.65	0.84	0.00	8.73	172.74	1.00	0.65	0.84	0.00
8.74	172.64	0.99	0.66	0.84	0.00	8.75	172.54	0.99	0.66	0.84	0.00
8.76	172.44	0.98	0.67	0.84	0.00	8.77	172.36	0.98	0.67	0.84	0.00
8.78	172.28	0.98	0.68	0.84	0.00	8.79	172.21	0.97	0.68	0.84	0.00
8.80	172.05	0.97	0.69	0.84	0.00	8.81	171.87	0.96	0.70	0.84	0.00
8.82	171.67	0.95	0.71	0.84	0.00	8.83	171.46	0.95	0.72	0.84	0.00
8.84	171.24	0.94	0.74	0.84	0.00	8.85	171.04	0.93	0.75	0.84	0.00
8.86	170.85	0.93	0.76	0.84	0.00	8.87	170.69	0.92	0.77	0.84	0.00
8.88	170.53	0.91	0.78	0.84	0.00	8.89	170.30	0.91	0.79	0.84	0.00
8.90	170.04	0.90	0.81	0.84	0.00	8.91	169.78	0.89	0.82	0.84	0.00
8.92	169.51	0.88	0.84	0.84	0.00	8.93	169.27	0.87	0.85	0.84	0.00
8.94	169.05	0.87	0.86	0.84	0.00	8.95	168.86	0.86	0.88	0.84	0.00
8.96	168.71	0.86	0.89	0.84	0.00	8.97	168.54	0.85	0.90	0.84	0.00
8.98	168.29	0.84	0.91	0.84	0.00	8.99	168.01	0.84	0.93	0.84	0.00
9.00	167.71	0.83	0.95	0.84	0.00	9.01	167.42	0.82	0.97	0.84	0.00
9.02	167.14	0.81	0.99	0.84	0.00	9.03	166.89	0.80	1.00	0.84	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
9.04	166.68	0.80	1.02	0.84	0.00	9.05	166.55	0.79	1.03	0.84	0.00
9.06	166.49	0.79	1.03	0.84	0.00	9.07	166.42	0.79	1.04	0.84	0.00
9.08	166.35	0.79	1.04	0.83	0.00	9.09	166.30	0.79	1.05	0.83	0.00
9.10	166.27	0.79	1.05	0.83	0.00	9.11	166.24	0.78	1.05	0.83	0.00
9.12	166.23	0.78	1.05	0.83	0.00	9.13	166.22	0.78	1.06	0.83	0.00
9.14	166.30	0.78	1.05	0.83	0.00	9.15	166.44	0.79	1.04	0.83	0.00
9.16	166.60	0.79	1.03	0.83	0.00	9.17	166.79	0.80	1.02	0.83	0.00
9.18	166.99	0.80	1.01	0.83	0.00	9.19	167.19	0.81	0.99	0.83	0.00
9.20	167.39	0.81	0.98	0.83	0.00	9.21	167.57	0.81	0.97	0.83	0.00
9.22	167.66	0.82	0.97	0.83	0.00	9.23	167.78	0.82	0.96	0.83	0.00
9.24	167.86	0.82	0.96	0.83	0.00	9.25	167.94	0.82	0.95	0.83	0.00
9.26	168.03	0.82	0.95	0.83	0.00	9.27	168.12	0.83	0.94	0.83	0.00
9.28	168.21	0.83	0.94	0.83	0.00	9.29	168.29	0.83	0.93	0.83	0.00
9.30	168.35	0.83	0.93	0.83	0.00	9.31	168.31	0.83	0.93	0.83	0.00
9.32	168.42	0.83	0.92	0.83	0.00	9.33	168.49	0.83	0.92	0.83	0.00
9.34	168.58	0.84	0.92	0.83	0.00	9.35	168.68	0.84	0.91	0.83	0.00
9.36	168.81	0.84	0.90	0.83	0.00	9.37	168.94	0.85	0.90	0.83	0.00
9.38	169.07	0.85	0.89	0.83	0.00	9.39	169.16	0.85	0.88	0.83	0.00
9.40	169.23	0.85	0.88	0.83	0.00	9.41	169.44	0.86	0.87	0.83	0.00
9.42	169.71	0.87	0.85	0.83	0.00	9.43	170.05	0.88	0.83	0.83	0.00
9.44	170.45	0.89	0.81	0.83	0.00	9.45	170.89	0.90	0.79	0.83	0.00
9.46	171.34	0.91	0.76	0.83	0.00	9.47	171.78	0.93	0.74	0.83	0.00
9.48	172.15	0.94	0.72	0.83	0.00	9.49	172.46	0.95	0.71	0.83	0.00
9.50	172.90	0.96	0.68	0.83	0.00	9.51	173.44	0.98	0.66	0.83	0.00
9.52	174.05	1.00	0.63	0.83	0.00	9.53	174.69	1.03	0.60	0.83	0.00
9.54	175.33	1.05	0.57	0.83	0.00	9.55	175.93	1.08	0.54	0.83	0.00
9.56	176.45	1.10	0.52	0.83	0.00	9.57	176.67	1.11	0.51	0.83	0.00
9.58	175.82	1.07	0.55	0.83	0.00	9.59	174.78	1.03	0.59	0.83	0.00
9.60	173.61	0.98	0.65	0.83	0.00	9.61	172.37	0.94	0.72	0.83	0.00
9.62	171.11	0.90	0.78	0.83	0.00	9.63	169.91	0.86	0.85	0.82	0.00
9.64	168.82	0.83	0.92	0.82	0.00	9.65	167.90	0.81	0.98	0.82	0.00
9.66	167.53	0.80	1.00	0.82	0.00	9.67	167.55	0.80	1.00	0.82	0.00
9.68	167.58	0.80	1.00	0.82	0.00	9.69	167.62	0.80	1.00	0.82	0.00
9.70	167.66	0.80	0.99	0.82	0.00	9.71	167.71	0.80	0.99	0.82	0.00
9.72	167.75	0.80	0.99	0.82	0.00	9.73	167.78	0.80	0.99	0.82	0.00
9.74	167.81	0.80	0.99	0.82	0.00	9.75	166.41	0.76	1.08	0.82	0.00
9.76	164.37	0.72	1.22	0.82	0.00	9.77	162.05	0.67	1.32	0.82	0.00
9.78	159.58	0.62	1.44	0.82	0.00	9.79	157.14	0.58	1.56	0.82	0.00
9.80	154.87	0.55	1.64	0.82	0.00	9.81	152.88	0.52	1.67	0.82	0.00
9.82	151.35	0.50	1.69	0.82	0.00	9.83	150.82	0.49	1.69	0.82	0.00
9.84	150.64	0.49	1.70	0.82	0.00	9.85	151.96	0.51	1.68	0.82	0.00
9.86	153.89	0.53	1.65	0.82	0.00	9.87	155.65	0.56	1.63	0.82	0.00
9.88	156.70	0.57	1.58	0.82	0.00	9.89	156.94	0.58	1.57	0.82	0.00
9.90	156.53	0.57	1.59	0.82	0.00	9.91	155.62	0.56	1.63	0.82	0.00
9.92	156.29	0.57	1.60	0.82	0.00	9.93	158.03	0.59	1.51	0.82	0.00
9.94	159.79	0.62	1.42	0.82	0.00	9.95	161.62	0.65	1.34	0.82	0.00
9.96	163.41	0.69	1.26	0.82	0.00	9.97	165.08	0.73	1.19	0.82	0.00
9.98	166.57	0.76	1.08	0.82	0.00	9.99	167.83	0.79	1.00	0.82	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
10.00	168.68	0.81	0.94	0.82	0.00	10.01	168.43	0.81	0.96	0.82	0.00
10.02	167.71	0.79	1.01	0.82	0.00	10.03	166.87	0.77	1.06	0.82	0.00
10.04	165.96	0.74	1.13	0.82	0.00	10.05	165.03	0.72	1.19	0.82	0.00
10.06	164.12	0.70	1.23	0.82	0.00	10.07	163.29	0.68	1.26	0.82	0.00
10.08	162.61	2.00	0.00	0.82	0.00	10.09	162.00	2.00	0.00	0.82	0.00
10.10	160.28	2.00	0.00	0.82	0.00	10.11	158.26	2.00	0.00	0.82	0.00
10.12	155.95	2.00	0.00	0.82	0.00	10.13	153.45	2.00	0.00	0.82	0.00
10.14	150.89	2.00	0.00	0.82	0.00	10.15	148.39	2.00	0.00	0.82	0.00
10.16	146.09	2.00	0.00	0.82	0.00	10.17	144.22	2.00	0.00	0.82	0.00
10.18	142.88	2.00	0.00	0.81	0.00	10.19	141.21	2.00	0.00	0.81	0.00
10.20	139.18	2.00	0.00	0.81	0.00	10.21	136.92	2.00	0.00	0.81	0.00
10.22	134.38	2.00	0.00	0.81	0.00	10.23	131.79	2.00	0.00	0.81	0.00
10.24	129.28	2.00	0.00	0.81	0.00	10.25	127.00	2.00	0.00	0.81	0.00
10.26	125.17	2.00	0.00	0.81	0.00	10.27	123.93	2.00	0.00	0.81	0.00
10.28	122.31	2.00	0.00	0.81	0.00	10.29	120.40	2.00	0.00	0.81	0.00
10.30	118.29	2.00	0.00	0.81	0.00	10.31	116.12	2.00	0.00	0.81	0.00
10.32	113.97	2.00	0.00	0.81	0.00	10.33	111.95	2.00	0.00	0.81	0.00
10.34	110.19	2.00	0.00	0.81	0.00	10.35	109.00	2.00	0.00	0.81	0.00
10.36	108.41	2.00	0.00	0.81	0.00	10.37	107.64	2.00	0.00	0.81	0.00
10.38	106.77	2.00	0.00	0.81	0.00	10.39	105.84	2.00	0.00	0.81	0.00
10.40	104.89	2.00	0.00	0.81	0.00	10.41	103.98	2.00	0.00	0.81	0.00
10.42	103.13	2.00	0.00	0.81	0.00	10.43	102.43	2.00	0.00	0.81	0.00
10.44	102.18	2.00	0.00	0.81	0.00	10.45	102.13	2.00	0.00	0.81	0.00
10.46	39.68	2.00	0.00	0.81	0.00	10.47	39.57	2.00	0.00	0.81	0.00
10.48	39.46	2.00	0.00	0.81	0.00	10.49	39.35	2.00	0.00	0.81	0.00
10.50	39.24	2.00	0.00	0.81	0.00	10.51	39.15	2.00	0.00	0.81	0.00
10.52	39.08	2.00	0.00	0.81	0.00	10.53	39.06	2.00	0.00	0.81	0.00
10.54	39.05	2.00	0.00	0.81	0.00	10.55	39.04	2.00	0.00	0.81	0.00
10.56	39.03	2.00	0.00	0.81	0.00	10.57	39.02	2.00	0.00	0.81	0.00
10.58	39.01	2.00	0.00	0.81	0.00	10.59	39.00	2.00	0.00	0.81	0.00
10.60	38.99	2.00	0.00	0.81	0.00	10.61	39.04	2.00	0.00	0.81	0.00
10.62	39.29	2.00	0.00	0.81	0.00	10.63	39.60	2.00	0.00	0.81	0.00
10.64	39.95	2.00	0.00	0.81	0.00	10.65	40.32	2.00	0.00	0.81	0.00
10.66	40.71	2.00	0.00	0.81	0.00	10.67	41.07	2.00	0.00	0.81	0.00
10.68	104.23	2.00	0.00	0.81	0.00	10.69	104.50	2.00	0.00	0.81	0.00
10.70	104.92	2.00	0.00	0.81	0.00	10.71	105.62	2.00	0.00	0.81	0.00
10.72	106.45	2.00	0.00	0.81	0.00	10.73	107.34	2.00	0.00	0.80	0.00
10.74	108.27	2.00	0.00	0.80	0.00	10.75	109.17	2.00	0.00	0.80	0.00
10.76	110.00	2.00	0.00	0.80	0.00	10.77	110.72	2.00	0.00	0.80	0.00
10.78	111.26	2.00	0.00	0.80	0.00	10.79	112.07	2.00	0.00	0.80	0.00
10.80	113.12	2.00	0.00	0.80	0.00	10.81	114.32	2.00	0.00	0.80	0.00
10.82	115.60	2.00	0.00	0.80	0.00	10.83	116.89	2.00	0.00	0.80	0.00
10.84	118.12	2.00	0.00	0.80	0.00	10.85	119.23	2.00	0.00	0.80	0.00
10.86	120.16	2.00	0.00	0.80	0.00	10.87	120.92	2.00	0.00	0.80	0.00
10.88	122.10	2.00	0.00	0.80	0.00	10.89	123.52	2.00	0.00	0.80	0.00
10.90	125.09	2.00	0.00	0.80	0.00	10.91	126.72	2.00	0.00	0.80	0.00
10.92	128.30	2.00	0.00	0.80	0.00	10.93	129.78	2.00	0.00	0.80	0.00
10.94	131.07	2.00	0.00	0.80	0.00	10.95	132.11	2.00	0.00	0.80	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
10.96	132.84	2.00	0.00	0.80	0.00	10.97	133.77	2.00	0.00	0.80	0.00
10.98	134.84	2.00	0.00	0.80	0.00	10.99	135.98	2.00	0.00	0.80	0.00
11.00	137.11	2.00	0.00	0.80	0.00	11.01	138.18	2.00	0.00	0.80	0.00
11.02	139.12	2.00	0.00	0.80	0.00	11.03	139.90	2.00	0.00	0.80	0.00
11.04	140.51	2.00	0.00	0.80	0.00	11.05	140.62	2.00	0.00	0.80	0.00
11.06	140.88	2.00	0.00	0.80	0.00	11.07	141.08	2.00	0.00	0.80	0.00
11.08	141.34	2.00	0.00	0.80	0.00	11.09	141.57	2.00	0.00	0.80	0.00
11.10	141.76	2.00	0.00	0.80	0.00	11.11	141.90	2.00	0.00	0.80	0.00
11.12	142.02	2.00	0.00	0.80	0.00	11.13	141.96	2.00	0.00	0.80	0.00
11.14	141.53	0.38	1.77	0.80	0.00	11.15	141.10	0.38	1.77	0.80	0.00
11.16	140.62	0.37	1.78	0.80	0.00	11.17	140.11	0.37	1.79	0.80	0.00
11.18	139.66	0.37	1.79	0.80	0.00	11.19	139.16	0.36	1.80	0.80	0.00
11.20	138.71	0.36	1.80	0.80	0.00	11.21	138.42	0.36	1.81	0.80	0.00
11.22	138.03	2.00	0.00	0.80	0.00	11.23	137.53	2.00	0.00	0.80	0.00
11.24	136.98	2.00	0.00	0.80	0.00	11.25	136.38	2.00	0.00	0.80	0.00
11.26	135.74	2.00	0.00	0.80	0.00	11.27	135.11	2.00	0.00	0.80	0.00
11.28	134.51	2.00	0.00	0.79	0.00	11.29	133.98	2.00	0.00	0.79	0.00
11.30	133.67	2.00	0.00	0.79	0.00	11.31	133.15	2.00	0.00	0.79	0.00
11.32	132.52	2.00	0.00	0.79	0.00	11.33	131.77	2.00	0.00	0.79	0.00
11.34	130.92	2.00	0.00	0.79	0.00	11.35	130.02	2.00	0.00	0.79	0.00
11.36	129.12	2.00	0.00	0.79	0.00	11.37	128.26	2.00	0.00	0.79	0.00
11.38	127.53	2.00	0.00	0.79	0.00	11.39	126.94	2.00	0.00	0.79	0.00
11.40	125.97	2.00	0.00	0.79	0.00	11.41	124.76	2.00	0.00	0.79	0.00
11.42	123.36	2.00	0.00	0.79	0.00	11.43	121.84	2.00	0.00	0.79	0.00
11.44	120.28	2.00	0.00	0.79	0.00	11.45	118.75	2.00	0.00	0.79	0.00
11.46	117.35	2.00	0.00	0.79	0.00	11.47	116.18	2.00	0.00	0.79	0.00
11.48	115.37	2.00	0.00	0.79	0.00	11.49	114.34	2.00	0.00	0.79	0.00
11.50	113.12	2.00	0.00	0.79	0.00	11.51	111.75	2.00	0.00	0.79	0.00
11.52	110.31	2.00	0.00	0.79	0.00	11.53	108.87	2.00	0.00	0.79	0.00
11.54	107.51	2.00	0.00	0.79	0.00	11.55	106.29	2.00	0.00	0.79	0.00
11.56	105.34	2.00	0.00	0.79	0.00	11.57	104.72	2.00	0.00	0.79	0.00
11.58	103.90	2.00	0.00	0.79	0.00	11.59	102.93	2.00	0.00	0.79	0.00
11.60	101.91	2.00	0.00	0.79	0.00	11.61	100.87	2.00	0.00	0.79	0.00
11.62	99.84	2.00	0.00	0.79	0.00	11.63	98.90	2.00	0.00	0.79	0.00
11.64	98.08	2.00	0.00	0.79	0.00	11.65	97.57	2.00	0.00	0.79	0.00
11.66	97.26	2.00	0.00	0.79	0.00	11.67	96.85	2.00	0.00	0.79	0.00
11.68	96.40	2.00	0.00	0.79	0.00	11.69	95.93	2.00	0.00	0.79	0.00
11.70	95.45	2.00	0.00	0.79	0.00	11.71	34.17	2.00	0.00	0.79	0.00
11.72	33.77	2.00	0.00	0.79	0.00	11.73	33.44	2.00	0.00	0.79	0.00
11.74	33.43	2.00	0.00	0.79	0.00	11.75	33.55	2.00	0.00	0.79	0.00
11.76	33.69	2.00	0.00	0.79	0.00	11.77	33.85	2.00	0.00	0.79	0.00
11.78	34.01	2.00	0.00	0.79	0.00	11.79	34.18	2.00	0.00	0.79	0.00
11.80	34.33	2.00	0.00	0.79	0.00	11.81	34.46	2.00	0.00	0.79	0.00
11.82	34.54	2.00	0.00	0.79	0.00	11.83	34.18	2.00	0.00	0.78	0.00
11.84	33.72	2.00	0.00	0.78	0.00	11.85	33.20	2.00	0.00	0.78	0.00
11.86	32.65	2.00	0.00	0.78	0.00	11.87	32.09	2.00	0.00	0.78	0.00
11.88	31.55	2.00	0.00	0.78	0.00	11.89	31.05	2.00	0.00	0.78	0.00
11.90	30.63	2.00	0.00	0.78	0.00	11.91	30.39	2.00	0.00	0.78	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
11.92	30.29	2.00	0.00	0.78	0.00	11.93	30.17	2.00	0.00	0.78	0.00
11.94	30.04	2.00	0.00	0.78	0.00	11.95	29.90	2.00	0.00	0.78	0.00
11.96	29.77	2.00	0.00	0.78	0.00	11.97	29.64	2.00	0.00	0.78	0.00
11.98	29.52	2.00	0.00	0.78	0.00	11.99	29.42	2.00	0.00	0.78	0.00
12.00	29.20	2.00	0.00	0.78	0.00	12.01	28.87	2.00	0.00	0.78	0.00
12.02	28.47	2.00	0.00	0.78	0.00	12.03	28.04	2.00	0.00	0.78	0.00
12.04	27.59	2.00	0.00	0.78	0.00	12.05	27.16	2.00	0.00	0.78	0.00
12.06	26.75	2.00	0.00	0.78	0.00	12.07	26.40	2.00	0.00	0.78	0.00
12.08	26.09	2.00	0.00	0.78	0.00	12.09	25.30	2.00	0.00	0.78	0.00
12.10	24.32	2.00	0.00	0.78	0.00	12.11	23.19	2.00	0.00	0.78	0.00
12.12	21.99	2.00	0.00	0.78	0.00	12.13	20.76	2.00	0.00	0.78	0.00
12.14	19.58	2.00	0.00	0.78	0.00	12.15	18.50	2.00	0.00	0.78	0.00
12.16	17.58	2.00	0.00	0.78	0.00	12.17	17.06	2.00	0.00	0.78	0.00
12.18	16.84	2.00	0.00	0.78	0.00	12.19	16.57	2.00	0.00	0.78	0.00
12.20	16.27	2.00	0.00	0.78	0.00	12.21	15.96	2.00	0.00	0.78	0.00
12.22	15.64	2.00	0.00	0.78	0.00	12.23	15.35	2.00	0.00	0.78	0.00
12.24	15.09	2.00	0.00	0.78	0.00	12.25	14.87	2.00	0.00	0.78	0.00
12.26	14.68	2.00	0.00	0.78	0.00	12.27	14.44	2.00	0.00	0.78	0.00
12.28	14.16	2.00	0.00	0.78	0.00	12.29	13.85	2.00	0.00	0.78	0.00
12.30	13.53	2.00	0.00	0.78	0.00	12.31	13.23	2.00	0.00	0.78	0.00
12.32	12.94	2.00	0.00	0.78	0.00	12.33	12.69	2.00	0.00	0.78	0.00
12.34	12.49	2.00	0.00	0.78	0.00	12.35	12.28	2.00	0.00	0.78	0.00
12.36	12.03	2.00	0.00	0.78	0.00	12.37	11.74	2.00	0.00	0.78	0.00
12.38	11.43	2.00	0.00	0.77	0.00	12.39	11.11	2.00	0.00	0.77	0.00
12.40	10.81	2.00	0.00	0.77	0.00	12.41	10.53	2.00	0.00	0.77	0.00
12.42	10.30	2.00	0.00	0.77	0.00	12.43	10.14	2.00	0.00	0.77	0.00
12.44	9.99	2.00	0.00	0.77	0.00	12.45	9.81	2.00	0.00	0.77	0.00
12.46	9.61	2.00	0.00	0.77	0.00	12.47	9.39	2.00	0.00	0.77	0.00
12.48	9.19	2.00	0.00	0.77	0.00	12.49	8.99	2.00	0.00	0.77	0.00
12.50	8.81	2.00	0.00	0.77	0.00	12.51	8.67	2.00	0.00	0.77	0.00
12.52	8.59	2.00	0.00	0.77	0.00	12.53	8.50	2.00	0.00	0.77	0.00
12.54	8.41	2.00	0.00	0.77	0.00	12.55	8.30	2.00	0.00	0.77	0.00
12.56	8.20	2.00	0.00	0.77	0.00	12.57	8.09	2.00	0.00	0.77	0.00
12.58	8.00	2.00	0.00	0.77	0.00	12.59	7.91	2.00	0.00	0.77	0.00
12.60	7.85	2.00	0.00	0.77	0.00	12.61	7.85	2.00	0.00	0.77	0.00
12.62	7.85	2.00	0.00	0.77	0.00	12.63	7.85	2.00	0.00	0.77	0.00
12.64	7.85	2.00	0.00	0.77	0.00	12.65	7.84	2.00	0.00	0.77	0.00
12.66	7.84	2.00	0.00	0.77	0.00	12.67	7.84	2.00	0.00	0.77	0.00
12.68	7.84	2.00	0.00	0.77	0.00	12.69	7.84	2.00	0.00	0.77	0.00
12.70	7.84	2.00	0.00	0.77	0.00	12.71	7.83	2.00	0.00	0.77	0.00
12.72	7.83	2.00	0.00	0.77	0.00	12.73	7.83	2.00	0.00	0.77	0.00
12.74	7.83	2.00	0.00	0.77	0.00	12.75	7.83	2.00	0.00	0.77	0.00
12.76	7.83	2.00	0.00	0.77	0.00	12.77	7.82	2.00	0.00	0.77	0.00
12.78	7.82	2.00	0.00	0.77	0.00	12.79	7.82	2.00	0.00	0.77	0.00
12.80	7.82	2.00	0.00	0.77	0.00	12.81	7.82	2.00	0.00	0.77	0.00
12.82	7.82	2.00	0.00	0.77	0.00	12.83	7.82	2.00	0.00	0.77	0.00
12.84	7.81	2.00	0.00	0.77	0.00	12.85	7.81	2.00	0.00	0.77	0.00
12.86	7.81	2.00	0.00	0.77	0.00	12.87	7.81	2.00	0.00	0.77	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
12.88	7.81	2.00	0.00	0.77	0.00	12.89	7.81	2.00	0.00	0.77	0.00
12.90	7.80	2.00	0.00	0.77	0.00	12.91	7.80	2.00	0.00	0.77	0.00
12.92	7.80	2.00	0.00	0.77	0.00	12.93	7.80	2.00	0.00	0.76	0.00
12.94	7.80	2.00	0.00	0.76	0.00	12.95	7.80	2.00	0.00	0.76	0.00
12.96	7.80	2.00	0.00	0.76	0.00	12.97	7.79	2.00	0.00	0.76	0.00
12.98	7.79	2.00	0.00	0.76	0.00	12.99	7.79	2.00	0.00	0.76	0.00
13.00	7.79	2.00	0.00	0.76	0.00	13.01	7.79	2.00	0.00	0.76	0.00
13.02	7.79	2.00	0.00	0.76	0.00	13.03	7.78	2.00	0.00	0.76	0.00
13.04	7.68	2.00	0.00	0.76	0.00	13.05	7.52	2.00	0.00	0.76	0.00
13.06	7.33	2.00	0.00	0.76	0.00	13.07	7.12	2.00	0.00	0.76	0.00
13.08	6.91	2.00	0.00	0.76	0.00	13.09	6.71	2.00	0.00	0.76	0.00
13.10	6.52	2.00	0.00	0.76	0.00	13.11	6.35	2.00	0.00	0.76	0.00
13.12	6.21	2.00	0.00	0.76	0.00	13.13	6.00	2.00	0.00	0.76	0.00
13.14	5.74	2.00	0.00	0.76	0.00	13.15	5.45	2.00	0.00	0.76	0.00
13.16	5.13	2.00	0.00	0.76	0.00	13.17	4.82	2.00	0.00	0.76	0.00
13.18	4.52	2.00	0.00	0.76	0.00	13.19	4.24	2.00	0.00	0.76	0.00
13.20	4.01	2.00	0.00	0.76	0.00	13.21	3.88	2.00	0.00	0.76	0.00
13.22	3.81	2.00	0.00	0.76	0.00	13.23	3.71	2.00	0.00	0.76	0.00
13.24	3.61	2.00	0.00	0.76	0.00	13.25	3.51	2.00	0.00	0.76	0.00
13.26	3.40	2.00	0.00	0.76	0.00	13.27	3.30	2.00	0.00	0.76	0.00
13.28	3.21	2.00	0.00	0.76	0.00	13.29	3.14	2.00	0.00	0.76	0.00
13.30	3.13	2.00	0.00	0.76	0.00	13.31	3.13	2.00	0.00	0.76	0.00
13.32	3.13	2.00	0.00	0.76	0.00	13.33	3.13	2.00	0.00	0.76	0.00
13.34	3.13	2.00	0.00	0.76	0.00	13.35	3.13	2.00	0.00	0.76	0.00
13.36	3.13	2.00	0.00	0.76	0.00	13.37	3.13	2.00	0.00	0.76	0.00
13.38	3.15	2.00	0.00	0.76	0.00	13.39	3.29	2.00	0.00	0.76	0.00
13.40	3.47	2.00	0.00	0.76	0.00	13.41	3.66	2.00	0.00	0.76	0.00
13.42	3.87	2.00	0.00	0.76	0.00	13.43	4.08	2.00	0.00	0.76	0.00
13.44	4.28	2.00	0.00	0.76	0.00	13.45	4.46	2.00	0.00	0.76	0.00
13.46	4.61	2.00	0.00	0.76	0.00	13.47	4.77	2.00	0.00	0.76	0.00
13.48	5.00	2.00	0.00	0.75	0.00	13.49	5.27	2.00	0.00	0.75	0.00
13.50	5.57	2.00	0.00	0.75	0.00	13.51	5.88	2.00	0.00	0.75	0.00
13.52	6.19	2.00	0.00	0.75	0.00	13.53	6.48	2.00	0.00	0.75	0.00
13.54	6.73	2.00	0.00	0.75	0.00	13.55	6.94	2.00	0.00	0.75	0.00
13.56	6.92	2.00	0.00	0.75	0.00	13.57	6.87	2.00	0.00	0.75	0.00
13.58	6.80	2.00	0.00	0.75	0.00	13.59	6.74	2.00	0.00	0.75	0.00
13.60	6.66	2.00	0.00	0.75	0.00	13.61	6.60	2.00	0.00	0.75	0.00
13.62	6.53	2.00	0.00	0.75	0.00	13.63	6.48	2.00	0.00	0.75	0.00
13.64	6.44	2.00	0.00	0.75	0.00	13.65	6.44	2.00	0.00	0.75	0.00
13.66	6.44	2.00	0.00	0.75	0.00	13.67	6.44	2.00	0.00	0.75	0.00
13.68	6.44	2.00	0.00	0.75	0.00	13.69	6.44	2.00	0.00	0.75	0.00
13.70	6.44	2.00	0.00	0.75	0.00	13.71	6.43	2.00	0.00	0.75	0.00
13.72	6.43	2.00	0.00	0.75	0.00	13.73	6.49	2.00	0.00	0.75	0.00
13.74	6.61	2.00	0.00	0.75	0.00	13.75	6.76	2.00	0.00	0.75	0.00
13.76	6.93	2.00	0.00	0.75	0.00	13.77	7.10	2.00	0.00	0.75	0.00
13.78	7.27	2.00	0.00	0.75	0.00	13.79	7.42	2.00	0.00	0.75	0.00
13.80	7.56	2.00	0.00	0.75	0.00	13.81	7.67	2.00	0.00	0.75	0.00
13.82	7.57	2.00	0.00	0.75	0.00	13.83	7.41	2.00	0.00	0.75	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
13.84	7.22	2.00	0.00	0.75	0.00	13.85	7.02	2.00	0.00	0.75	0.00
13.86	6.81	2.00	0.00	0.75	0.00	13.87	6.61	2.00	0.00	0.75	0.00
13.88	6.42	2.00	0.00	0.75	0.00	13.89	6.26	2.00	0.00	0.75	0.00
13.90	6.13	2.00	0.00	0.75	0.00	13.91	5.99	2.00	0.00	0.75	0.00
13.92	5.82	2.00	0.00	0.75	0.00	13.93	5.62	2.00	0.00	0.75	0.00
13.94	5.42	2.00	0.00	0.75	0.00	13.95	5.21	2.00	0.00	0.75	0.00
13.96	5.01	2.00	0.00	0.75	0.00	13.97	4.83	2.00	0.00	0.75	0.00
13.98	4.68	2.00	0.00	0.75	0.00	13.99	4.63	2.00	0.00	0.75	0.00
14.00	4.63	2.00	0.00	0.75	0.00	14.01	4.63	2.00	0.00	0.75	0.00
14.02	4.62	2.00	0.00	0.75	0.00	14.03	4.62	2.00	0.00	0.74	0.00
14.04	4.62	2.00	0.00	0.74	0.00	14.05	4.62	2.00	0.00	0.74	0.00
14.06	4.62	2.00	0.00	0.74	0.00	14.07	4.62	2.00	0.00	0.74	0.00
14.08	4.74	2.00	0.00	0.74	0.00	14.09	4.90	2.00	0.00	0.74	0.00
14.10	5.09	2.00	0.00	0.74	0.00	14.11	5.29	2.00	0.00	0.74	0.00
14.12	5.50	2.00	0.00	0.74	0.00	14.13	5.70	2.00	0.00	0.74	0.00
14.14	5.88	2.00	0.00	0.74	0.00	14.15	6.04	2.00	0.00	0.74	0.00
14.16	6.17	2.00	0.00	0.74	0.00	14.17	6.38	2.00	0.00	0.74	0.00
14.18	6.64	2.00	0.00	0.74	0.00	14.19	6.93	2.00	0.00	0.74	0.00
14.20	7.23	2.00	0.00	0.74	0.00	14.21	7.54	2.00	0.00	0.74	0.00
14.22	7.83	2.00	0.00	0.74	0.00	14.23	8.09	2.00	0.00	0.74	0.00
14.24	8.30	2.00	0.00	0.74	0.00	14.25	8.48	2.00	0.00	0.74	0.00
14.26	8.71	2.00	0.00	0.74	0.00	14.27	8.97	2.00	0.00	0.74	0.00
14.28	9.26	2.00	0.00	0.74	0.00	14.29	9.57	2.00	0.00	0.74	0.00
14.30	9.86	2.00	0.00	0.74	0.00	14.31	10.14	2.00	0.00	0.74	0.00
14.32	10.39	2.00	0.00	0.74	0.00	14.33	10.58	2.00	0.00	0.74	0.00
14.34	10.71	2.00	0.00	0.74	0.00	14.35	10.87	2.00	0.00	0.74	0.00
14.36	11.05	2.00	0.00	0.74	0.00	14.37	11.24	2.00	0.00	0.74	0.00
14.38	11.44	2.00	0.00	0.74	0.00	14.39	11.63	2.00	0.00	0.74	0.00
14.40	11.81	2.00	0.00	0.74	0.00	14.41	11.96	2.00	0.00	0.74	0.00
14.42	12.03	2.00	0.00	0.74	0.00	14.43	11.96	2.00	0.00	0.74	0.00
14.44	11.88	2.00	0.00	0.74	0.00	14.45	11.78	2.00	0.00	0.74	0.00
14.46	11.68	2.00	0.00	0.74	0.00	14.47	11.58	2.00	0.00	0.74	0.00
14.48	11.48	2.00	0.00	0.74	0.00	14.49	11.39	2.00	0.00	0.74	0.00
14.50	11.32	2.00	0.00	0.74	0.00	14.51	11.12	2.00	0.00	0.74	0.00
14.52	10.77	2.00	0.00	0.74	0.00	14.53	10.35	2.00	0.00	0.74	0.00
14.54	9.90	2.00	0.00	0.74	0.00	14.55	9.43	2.00	0.00	0.74	0.00
14.56	8.96	2.00	0.00	0.74	0.00	14.57	8.52	2.00	0.00	0.74	0.00
14.58	8.14	2.00	0.00	0.73	0.00	14.59	7.83	2.00	0.00	0.73	0.00
14.60	7.69	2.00	0.00	0.73	0.00	14.61	7.53	2.00	0.00	0.73	0.00
14.62	7.34	2.00	0.00	0.73	0.00	14.63	7.14	2.00	0.00	0.73	0.00
14.64	6.94	2.00	0.00	0.73	0.00	14.65	6.74	2.00	0.00	0.73	0.00
14.66	6.56	2.00	0.00	0.73	0.00	14.67	6.40	2.00	0.00	0.73	0.00
14.68	6.34	2.00	0.00	0.73	0.00	14.69	6.46	2.00	0.00	0.73	0.00
14.70	6.60	2.00	0.00	0.73	0.00	14.71	6.76	2.00	0.00	0.73	0.00
14.72	6.92	2.00	0.00	0.73	0.00	14.73	7.09	2.00	0.00	0.73	0.00
14.74	7.25	2.00	0.00	0.73	0.00	14.75	7.39	2.00	0.00	0.73	0.00
14.76	7.51	2.00	0.00	0.73	0.00	14.77	7.54	2.00	0.00	0.73	0.00
14.78	7.54	2.00	0.00	0.73	0.00	14.79	7.54	2.00	0.00	0.73	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
14.80	7.54	2.00	0.00	0.73	0.00	14.81	7.54	2.00	0.00	0.73	0.00
14.82	7.53	2.00	0.00	0.73	0.00	14.83	7.53	2.00	0.00	0.73	0.00
14.84	7.53	2.00	0.00	0.73	0.00	14.85	7.53	2.00	0.00	0.73	0.00
14.86	7.65	2.00	0.00	0.73	0.00	14.87	7.81	2.00	0.00	0.73	0.00
14.88	7.99	2.00	0.00	0.73	0.00	14.89	8.19	2.00	0.00	0.73	0.00
14.90	8.39	2.00	0.00	0.73	0.00	14.91	8.58	2.00	0.00	0.73	0.00
14.92	8.76	2.00	0.00	0.73	0.00	14.93	8.91	2.00	0.00	0.73	0.00
14.94	9.03	2.00	0.00	0.73	0.00	14.95	9.17	2.00	0.00	0.73	0.00
14.96	9.33	2.00	0.00	0.73	0.00	14.97	9.52	2.00	0.00	0.73	0.00
14.98	9.72	2.00	0.00	0.73	0.00	14.99	9.91	2.00	0.00	0.73	0.00
15.00	10.10	2.00	0.00	0.73	0.00	15.01	10.27	2.00	0.00	0.73	0.00
15.02	10.41	2.00	0.00	0.73	0.00	15.03	10.35	2.00	0.00	0.73	0.00
15.04	10.17	2.00	0.00	0.73	0.00	15.05	9.97	2.00	0.00	0.73	0.00
15.06	9.74	2.00	0.00	0.73	0.00	15.07	9.50	2.00	0.00	0.73	0.00
15.08	9.27	2.00	0.00	0.73	0.00	15.09	9.06	2.00	0.00	0.73	0.00
15.10	8.87	2.00	0.00	0.73	0.00	15.11	8.72	2.00	0.00	0.73	0.00
15.12	8.78	2.00	0.00	0.73	0.00	15.13	8.86	2.00	0.00	0.72	0.00
15.14	8.95	2.00	0.00	0.72	0.00	15.15	9.04	2.00	0.00	0.72	0.00
15.16	9.14	2.00	0.00	0.72	0.00	15.17	9.24	2.00	0.00	0.72	0.00
15.18	9.32	2.00	0.00	0.72	0.00	15.19	9.39	2.00	0.00	0.72	0.00
15.20	9.51	2.00	0.00	0.72	0.00	15.21	9.80	2.00	0.00	0.72	0.00
15.22	10.14	2.00	0.00	0.72	0.00	15.23	10.53	2.00	0.00	0.72	0.00
15.24	10.93	2.00	0.00	0.72	0.00	15.25	11.34	2.00	0.00	0.72	0.00
15.26	11.72	2.00	0.00	0.72	0.00	15.27	12.07	2.00	0.00	0.72	0.00
15.28	12.35	2.00	0.00	0.72	0.00	15.29	12.62	2.00	0.00	0.72	0.00
15.30	12.99	2.00	0.00	0.72	0.00	15.31	13.42	2.00	0.00	0.72	0.00
15.32	13.89	2.00	0.00	0.72	0.00	15.33	14.38	2.00	0.00	0.72	0.00
15.34	14.86	2.00	0.00	0.72	0.00	15.35	15.30	2.00	0.00	0.72	0.00
15.36	15.69	2.00	0.00	0.72	0.00	15.37	15.99	2.00	0.00	0.72	0.00
15.38	16.25	2.00	0.00	0.72	0.00	15.39	16.57	2.00	0.00	0.72	0.00
15.40	16.94	2.00	0.00	0.72	0.00	15.41	17.34	2.00	0.00	0.72	0.00
15.42	17.75	2.00	0.00	0.72	0.00	15.43	18.14	2.00	0.00	0.72	0.00
15.44	18.49	2.00	0.00	0.72	0.00	15.45	18.79	2.00	0.00	0.72	0.00
15.46	18.84	2.00	0.00	0.72	0.00	15.47	18.46	2.00	0.00	0.72	0.00
15.48	18.01	2.00	0.00	0.72	0.00	15.49	17.50	2.00	0.00	0.72	0.00
15.50	16.96	2.00	0.00	0.72	0.00	15.51	16.43	2.00	0.00	0.72	0.00
15.52	15.92	2.00	0.00	0.72	0.00	15.53	15.47	2.00	0.00	0.72	0.00
15.54	15.09	2.00	0.00	0.72	0.00	15.55	14.79	2.00	0.00	0.72	0.00
15.56	14.42	2.00	0.00	0.72	0.00	15.57	13.99	2.00	0.00	0.72	0.00
15.58	13.51	2.00	0.00	0.72	0.00	15.59	13.02	2.00	0.00	0.72	0.00
15.60	12.54	2.00	0.00	0.72	0.00	15.61	12.09	2.00	0.00	0.72	0.00
15.62	11.69	2.00	0.00	0.72	0.00	15.63	11.39	2.00	0.00	0.72	0.00
15.64	11.36	2.00	0.00	0.72	0.00	15.65	11.32	2.00	0.00	0.72	0.00
15.66	11.27	2.00	0.00	0.72	0.00	15.67	11.22	2.00	0.00	0.72	0.00
15.68	11.17	2.00	0.00	0.71	0.00	15.69	11.12	2.00	0.00	0.71	0.00
15.70	11.07	2.00	0.00	0.71	0.00	15.71	11.03	2.00	0.00	0.71	0.00
15.72	10.99	2.00	0.00	0.71	0.00	15.73	10.92	2.00	0.00	0.71	0.00
15.74	10.83	2.00	0.00	0.71	0.00	15.75	10.74	2.00	0.00	0.71	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
15.76	10.64	2.00	0.00	0.71	0.00	15.77	10.54	2.00	0.00	0.71	0.00
15.78	10.44	2.00	0.00	0.71	0.00	15.79	10.36	2.00	0.00	0.71	0.00
15.80	10.29	2.00	0.00	0.71	0.00	15.81	10.23	2.00	0.00	0.71	0.00
15.82	10.15	2.00	0.00	0.71	0.00	15.83	10.06	2.00	0.00	0.71	0.00
15.84	9.96	2.00	0.00	0.71	0.00	15.85	9.86	2.00	0.00	0.71	0.00
15.86	9.77	2.00	0.00	0.71	0.00	15.87	9.67	2.00	0.00	0.71	0.00
15.88	9.59	2.00	0.00	0.71	0.00	15.89	9.53	2.00	0.00	0.71	0.00
15.90	9.47	2.00	0.00	0.71	0.00	15.91	9.38	2.00	0.00	0.71	0.00
15.92	9.29	2.00	0.00	0.71	0.00	15.93	9.19	2.00	0.00	0.71	0.00
15.94	9.09	2.00	0.00	0.71	0.00	15.95	9.00	2.00	0.00	0.71	0.00
15.96	8.91	2.00	0.00	0.71	0.00	15.97	8.83	2.00	0.00	0.71	0.00
15.98	8.80	2.00	0.00	0.71	0.00	15.99	8.79	2.00	0.00	0.71	0.00
16.00	8.79	2.00	0.00	0.71	0.00	16.01	8.79	2.00	0.00	0.71	0.00
16.02	8.79	2.00	0.00	0.71	0.00	16.03	8.79	2.00	0.00	0.71	0.00
16.04	8.79	2.00	0.00	0.71	0.00	16.05	8.78	2.00	0.00	0.71	0.00
16.06	8.78	2.00	0.00	0.71	0.00	16.07	8.78	2.00	0.00	0.71	0.00
16.08	8.78	2.00	0.00	0.71	0.00	16.09	8.78	2.00	0.00	0.71	0.00
16.10	8.78	2.00	0.00	0.71	0.00	16.11	8.77	2.00	0.00	0.71	0.00
16.12	8.77	2.00	0.00	0.71	0.00	16.13	8.77	2.00	0.00	0.71	0.00
16.14	8.77	2.00	0.00	0.71	0.00	16.15	8.77	2.00	0.00	0.71	0.00
16.16	8.77	2.00	0.00	0.71	0.00	16.17	8.76	2.00	0.00	0.71	0.00
16.18	8.76	2.00	0.00	0.71	0.00	16.19	8.76	2.00	0.00	0.71	0.00
16.20	8.76	2.00	0.00	0.71	0.00	16.21	8.76	2.00	0.00	0.71	0.00
16.22	8.76	2.00	0.00	0.71	0.00	16.23	8.75	2.00	0.00	0.70	0.00
16.24	8.85	2.00	0.00	0.70	0.00	16.25	9.13	2.00	0.00	0.70	0.00
16.26	9.46	2.00	0.00	0.70	0.00	16.27	9.83	2.00	0.00	0.70	0.00
16.28	10.21	2.00	0.00	0.70	0.00	16.29	10.60	2.00	0.00	0.70	0.00
16.30	10.96	2.00	0.00	0.70	0.00	16.31	11.28	2.00	0.00	0.70	0.00
16.32	11.54	2.00	0.00	0.70	0.00	16.33	11.82	2.00	0.00	0.70	0.00
16.34	12.19	2.00	0.00	0.70	0.00	16.35	12.62	2.00	0.00	0.70	0.00
16.36	13.08	2.00	0.00	0.70	0.00	16.37	13.56	2.00	0.00	0.70	0.00
16.38	14.03	2.00	0.00	0.70	0.00	16.39	14.46	2.00	0.00	0.70	0.00
16.40	14.84	2.00	0.00	0.70	0.00	16.41	15.14	2.00	0.00	0.70	0.00
16.42	15.51	2.00	0.00	0.70	0.00	16.43	15.98	2.00	0.00	0.70	0.00
16.44	16.50	2.00	0.00	0.70	0.00	16.45	17.06	2.00	0.00	0.70	0.00
16.46	17.63	2.00	0.00	0.70	0.00	16.47	18.18	2.00	0.00	0.70	0.00
16.48	18.67	2.00	0.00	0.70	0.00	16.49	19.09	2.00	0.00	0.70	0.00
16.50	19.49	2.00	0.00	0.70	0.00	16.51	20.10	2.00	0.00	0.70	0.00
16.52	20.83	2.00	0.00	0.70	0.00	16.53	21.64	2.00	0.00	0.70	0.00
16.54	22.48	2.00	0.00	0.70	0.00	16.55	23.31	2.00	0.00	0.70	0.00
16.56	24.10	2.00	0.00	0.70	0.00	16.57	24.80	2.00	0.00	0.70	0.00
16.58	25.36	2.00	0.00	0.70	0.00	16.59	25.49	2.00	0.00	0.70	0.00
16.60	25.55	2.00	0.00	0.70	0.00	16.61	25.61	2.00	0.00	0.70	0.00
16.62	25.68	2.00	0.00	0.70	0.00	16.63	25.75	2.00	0.00	0.70	0.00
16.64	25.82	2.00	0.00	0.70	0.00	16.65	25.89	2.00	0.00	0.70	0.00
16.66	25.94	2.00	0.00	0.70	0.00	16.67	25.94	2.00	0.00	0.70	0.00
16.68	25.63	2.00	0.00	0.70	0.00	16.69	25.24	2.00	0.00	0.70	0.00
16.70	24.80	2.00	0.00	0.70	0.00	16.71	24.34	2.00	0.00	0.70	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
16.72	23.86	2.00	0.00	0.70	0.00	16.73	23.41	2.00	0.00	0.70	0.00
16.74	23.00	2.00	0.00	0.70	0.00	16.75	22.65	2.00	0.00	0.70	0.00
16.76	22.38	2.00	0.00	0.70	0.00	16.77	22.05	2.00	0.00	0.70	0.00
16.78	21.65	2.00	0.00	0.69	0.00	16.79	21.22	2.00	0.00	0.69	0.00
16.80	20.76	2.00	0.00	0.69	0.00	16.81	20.31	2.00	0.00	0.69	0.00
16.82	19.88	2.00	0.00	0.69	0.00	16.83	19.50	2.00	0.00	0.69	0.00
16.84	19.19	2.00	0.00	0.69	0.00	16.85	18.78	2.00	0.00	0.69	0.00
16.86	18.23	2.00	0.00	0.69	0.00	16.87	17.59	2.00	0.00	0.69	0.00
16.88	16.89	2.00	0.00	0.69	0.00	16.89	16.18	2.00	0.00	0.69	0.00
16.90	15.48	2.00	0.00	0.69	0.00	16.91	14.83	2.00	0.00	0.69	0.00
16.92	14.27	2.00	0.00	0.69	0.00	16.93	13.87	2.00	0.00	0.69	0.00
16.94	13.68	2.00	0.00	0.69	0.00	16.95	13.44	2.00	0.00	0.69	0.00
16.96	13.17	2.00	0.00	0.69	0.00	16.97	12.89	2.00	0.00	0.69	0.00
16.98	12.60	2.00	0.00	0.69	0.00	16.99	12.32	2.00	0.00	0.69	0.00
17.00	12.07	2.00	0.00	0.69	0.00	17.01	11.86	2.00	0.00	0.69	0.00
17.02	11.82	2.00	0.00	0.69	0.00	17.03	11.92	2.00	0.00	0.69	0.00
17.04	12.04	2.00	0.00	0.69	0.00	17.05	12.17	2.00	0.00	0.69	0.00
17.06	12.31	2.00	0.00	0.69	0.00	17.07	12.45	2.00	0.00	0.69	0.00
17.08	12.58	2.00	0.00	0.69	0.00	17.09	12.70	2.00	0.00	0.69	0.00
17.10	12.79	2.00	0.00	0.69	0.00	17.11	12.80	2.00	0.00	0.69	0.00
17.12	12.80	2.00	0.00	0.69	0.00	17.13	12.80	2.00	0.00	0.69	0.00
17.14	12.79	2.00	0.00	0.69	0.00	17.15	12.79	2.00	0.00	0.69	0.00
17.16	12.79	2.00	0.00	0.69	0.00	17.17	12.79	2.00	0.00	0.69	0.00
17.18	12.78	2.00	0.00	0.69	0.00	17.19	12.74	2.00	0.00	0.69	0.00
17.20	12.46	2.00	0.00	0.69	0.00	17.21	12.12	2.00	0.00	0.69	0.00
17.22	11.73	2.00	0.00	0.69	0.00	17.23	11.32	2.00	0.00	0.69	0.00
17.24	10.91	2.00	0.00	0.69	0.00	17.25	10.51	2.00	0.00	0.69	0.00
17.26	10.15	2.00	0.00	0.69	0.00	17.27	9.85	2.00	0.00	0.69	0.00
17.28	9.61	2.00	0.00	0.69	0.00	17.29	9.30	2.00	0.00	0.69	0.00
17.30	8.94	2.00	0.00	0.69	0.00	17.31	8.54	2.00	0.00	0.69	0.00
17.32	8.12	2.00	0.00	0.69	0.00	17.33	7.71	2.00	0.00	0.68	0.00
17.34	7.32	2.00	0.00	0.68	0.00	17.35	6.98	2.00	0.00	0.68	0.00
17.36	6.70	2.00	0.00	0.68	0.00	17.37	6.68	2.00	0.00	0.68	0.00
17.38	6.71	2.00	0.00	0.68	0.00	17.39	6.74	2.00	0.00	0.68	0.00
17.40	6.77	2.00	0.00	0.68	0.00	17.41	6.80	2.00	0.00	0.68	0.00
17.42	6.83	2.00	0.00	0.68	0.00	17.43	6.86	2.00	0.00	0.68	0.00
17.44	6.88	2.00	0.00	0.68	0.00	17.45	6.90	2.00	0.00	0.68	0.00
17.46	6.92	2.00	0.00	0.68	0.00	17.47	6.94	2.00	0.00	0.68	0.00
17.48	6.97	2.00	0.00	0.68	0.00	17.49	7.00	2.00	0.00	0.68	0.00
17.50	7.03	2.00	0.00	0.68	0.00	17.51	7.06	2.00	0.00	0.68	0.00
17.52	7.09	2.00	0.00	0.68	0.00	17.53	7.11	2.00	0.00	0.68	0.00
17.54	7.18	2.00	0.00	0.68	0.00	17.55	7.32	2.00	0.00	0.68	0.00
17.56	7.48	2.00	0.00	0.68	0.00	17.57	7.67	2.00	0.00	0.68	0.00
17.58	7.85	2.00	0.00	0.68	0.00	17.59	8.04	2.00	0.00	0.68	0.00
17.60	8.22	2.00	0.00	0.68	0.00	17.61	8.37	2.00	0.00	0.68	0.00
17.62	8.50	2.00	0.00	0.68	0.00	17.63	8.61	2.00	0.00	0.68	0.00
17.64	8.76	2.00	0.00	0.68	0.00	17.65	8.93	2.00	0.00	0.68	0.00
17.66	9.12	2.00	0.00	0.68	0.00	17.67	9.30	2.00	0.00	0.68	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
17.68	9.49	2.00	0.00	0.68	0.00	17.69	9.66	2.00	0.00	0.68	0.00
17.70	9.80	2.00	0.00	0.68	0.00	17.71	9.88	2.00	0.00	0.68	0.00
17.72	9.81	2.00	0.00	0.68	0.00	17.73	9.73	2.00	0.00	0.68	0.00
17.74	9.64	2.00	0.00	0.68	0.00	17.75	9.54	2.00	0.00	0.68	0.00
17.76	9.45	2.00	0.00	0.68	0.00	17.77	9.36	2.00	0.00	0.68	0.00
17.78	9.27	2.00	0.00	0.68	0.00	17.79	9.20	2.00	0.00	0.68	0.00
17.80	9.14	2.00	0.00	0.68	0.00	17.81	9.07	2.00	0.00	0.68	0.00
17.82	8.99	2.00	0.00	0.68	0.00	17.83	8.90	2.00	0.00	0.68	0.00
17.84	8.80	2.00	0.00	0.68	0.00	17.85	8.70	2.00	0.00	0.68	0.00
17.86	8.61	2.00	0.00	0.68	0.00	17.87	8.54	2.00	0.00	0.68	0.00
17.88	8.47	2.00	0.00	0.67	0.00	17.89	8.47	2.00	0.00	0.67	0.00
17.90	8.46	2.00	0.00	0.67	0.00	17.91	8.46	2.00	0.00	0.67	0.00
17.92	8.46	2.00	0.00	0.67	0.00	17.93	8.46	2.00	0.00	0.67	0.00
17.94	8.46	2.00	0.00	0.67	0.00	17.95	8.46	2.00	0.00	0.67	0.00
17.96	8.45	2.00	0.00	0.67	0.00	17.97	8.47	2.00	0.00	0.67	0.00
17.98	8.55	2.00	0.00	0.67	0.00	17.99	8.66	2.00	0.00	0.67	0.00
18.00	8.77	2.00	0.00	0.67	0.00	18.01	8.90	2.00	0.00	0.67	0.00
18.02	9.02	2.00	0.00	0.67	0.00	18.03	9.14	2.00	0.00	0.67	0.00
18.04	9.25	2.00	0.00	0.67	0.00	18.05	9.33	2.00	0.00	0.67	0.00
18.06	9.55	2.00	0.00	0.67	0.00	18.07	9.94	2.00	0.00	0.67	0.00
18.08	10.41	2.00	0.00	0.67	0.00	18.09	10.92	2.00	0.00	0.67	0.00
18.10	11.45	2.00	0.00	0.67	0.00	18.11	11.97	2.00	0.00	0.67	0.00
18.12	12.46	2.00	0.00	0.67	0.00	18.13	12.88	2.00	0.00	0.67	0.00
18.14	13.23	2.00	0.00	0.67	0.00	18.15	13.82	2.00	0.00	0.67	0.00
18.16	14.61	2.00	0.00	0.67	0.00	18.17	15.51	2.00	0.00	0.67	0.00
18.18	16.47	2.00	0.00	0.67	0.00	18.19	17.45	2.00	0.00	0.67	0.00
18.20	18.41	2.00	0.00	0.67	0.00	18.21	19.28	2.00	0.00	0.67	0.00
18.22	20.03	2.00	0.00	0.67	0.00	18.23	20.53	2.00	0.00	0.67	0.00
18.24	20.84	2.00	0.00	0.67	0.00	18.25	21.23	2.00	0.00	0.67	0.00
18.26	21.65	2.00	0.00	0.67	0.00	18.27	22.11	2.00	0.00	0.67	0.00
18.28	22.56	2.00	0.00	0.67	0.00	18.29	22.99	2.00	0.00	0.67	0.00
18.30	23.38	2.00	0.00	0.67	0.00	18.31	23.69	2.00	0.00	0.67	0.00
18.32	23.68	2.00	0.00	0.67	0.00	18.33	23.44	2.00	0.00	0.67	0.00
18.34	23.17	2.00	0.00	0.67	0.00	18.35	22.86	2.00	0.00	0.67	0.00
18.36	22.54	2.00	0.00	0.67	0.00	18.37	22.23	2.00	0.00	0.67	0.00
18.38	21.94	2.00	0.00	0.67	0.00	18.39	21.68	2.00	0.00	0.67	0.00
18.40	21.48	2.00	0.00	0.67	0.00	18.41	21.12	2.00	0.00	0.67	0.00
18.42	20.66	2.00	0.00	0.67	0.00	18.43	20.13	2.00	0.00	0.66	0.00
18.44	19.56	2.00	0.00	0.66	0.00	18.45	18.98	2.00	0.00	0.66	0.00
18.46	18.42	2.00	0.00	0.66	0.00	18.47	17.90	2.00	0.00	0.66	0.00
18.48	17.46	2.00	0.00	0.66	0.00	18.49	17.10	2.00	0.00	0.66	0.00
18.50	16.65	2.00	0.00	0.66	0.00	18.51	16.10	2.00	0.00	0.66	0.00
18.52	15.48	2.00	0.00	0.66	0.00	18.53	14.82	2.00	0.00	0.66	0.00
18.54	14.17	2.00	0.00	0.66	0.00	18.55	13.55	2.00	0.00	0.66	0.00
18.56	12.99	2.00	0.00	0.66	0.00	18.57	12.53	2.00	0.00	0.66	0.00
18.58	12.23	2.00	0.00	0.66	0.00	18.59	11.92	2.00	0.00	0.66	0.00
18.60	11.56	2.00	0.00	0.66	0.00	18.61	11.16	2.00	0.00	0.66	0.00
18.62	10.75	2.00	0.00	0.66	0.00	18.63	10.35	2.00	0.00	0.66	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
18.64	9.97	2.00	0.00	0.66	0.00	18.65	9.64	2.00	0.00	0.66	0.00
18.66	9.37	2.00	0.00	0.66	0.00	18.67	9.20	2.00	0.00	0.66	0.00
18.68	8.99	2.00	0.00	0.66	0.00	18.69	8.74	2.00	0.00	0.66	0.00
18.70	8.48	2.00	0.00	0.66	0.00	18.71	8.22	2.00	0.00	0.66	0.00
18.72	7.96	2.00	0.00	0.66	0.00	18.73	7.72	2.00	0.00	0.66	0.00
18.74	7.52	2.00	0.00	0.66	0.00	18.75	7.39	2.00	0.00	0.66	0.00
18.76	7.30	2.00	0.00	0.66	0.00	18.77	7.19	2.00	0.00	0.66	0.00
18.78	7.07	2.00	0.00	0.66	0.00	18.79	6.95	2.00	0.00	0.66	0.00
18.80	6.82	2.00	0.00	0.66	0.00	18.81	6.70	2.00	0.00	0.66	0.00
18.82	6.59	2.00	0.00	0.66	0.00	18.83	6.51	2.00	0.00	0.66	0.00
18.84	6.48	2.00	0.00	0.66	0.00	18.85	6.48	2.00	0.00	0.66	0.00
18.86	6.48	2.00	0.00	0.66	0.00	18.87	6.48	2.00	0.00	0.66	0.00
18.88	6.48	2.00	0.00	0.66	0.00	18.89	6.47	2.00	0.00	0.66	0.00
18.90	6.47	2.00	0.00	0.66	0.00	18.91	6.47	2.00	0.00	0.66	0.00
18.92	6.47	2.00	0.00	0.66	0.00	18.93	6.55	2.00	0.00	0.66	0.00
18.94	6.65	2.00	0.00	0.66	0.00	18.95	6.76	2.00	0.00	0.66	0.00
18.96	6.88	2.00	0.00	0.66	0.00	18.97	7.01	2.00	0.00	0.66	0.00
18.98	7.12	2.00	0.00	0.65	0.00	18.99	7.23	2.00	0.00	0.65	0.00
19.00	7.33	2.00	0.00	0.65	0.00	19.01	7.40	2.00	0.00	0.65	0.00
19.02	7.48	2.00	0.00	0.65	0.00	19.03	7.59	2.00	0.00	0.65	0.00
19.04	7.70	2.00	0.00	0.65	0.00	19.05	7.83	2.00	0.00	0.65	0.00
19.06	7.95	2.00	0.00	0.65	0.00	19.07	8.06	2.00	0.00	0.65	0.00
19.08	8.17	2.00	0.00	0.65	0.00	19.09	8.25	2.00	0.00	0.65	0.00
19.10	8.27	2.00	0.00	0.65	0.00	19.11	8.27	2.00	0.00	0.65	0.00
19.12	8.27	2.00	0.00	0.65	0.00	19.13	8.27	2.00	0.00	0.65	0.00
19.14	8.27	2.00	0.00	0.65	0.00	19.15	8.27	2.00	0.00	0.65	0.00
19.16	8.26	2.00	0.00	0.65	0.00	19.17	8.26	2.00	0.00	0.65	0.00
19.18	8.26	2.00	0.00	0.65	0.00	19.19	8.18	2.00	0.00	0.65	0.00
19.20	8.08	2.00	0.00	0.65	0.00	19.21	7.96	2.00	0.00	0.65	0.00
19.22	7.84	2.00	0.00	0.65	0.00	19.23	7.71	2.00	0.00	0.65	0.00
19.24	7.59	2.00	0.00	0.65	0.00	19.25	7.48	2.00	0.00	0.65	0.00
19.26	7.39	2.00	0.00	0.65	0.00	19.27	7.31	2.00	0.00	0.65	0.00
19.28	7.23	2.00	0.00	0.65	0.00	19.29	7.12	2.00	0.00	0.65	0.00
19.30	7.00	2.00	0.00	0.65	0.00	19.31	6.88	2.00	0.00	0.65	0.00
19.32	6.75	2.00	0.00	0.65	0.00	19.33	6.64	2.00	0.00	0.65	0.00
19.34	6.53	2.00	0.00	0.65	0.00	19.35	6.44	2.00	0.00	0.65	0.00
19.36	6.42	2.00	0.00	0.65	0.00	19.37	6.42	2.00	0.00	0.65	0.00
19.38	6.42	2.00	0.00	0.65	0.00	19.39	6.42	2.00	0.00	0.65	0.00
19.40	6.42	2.00	0.00	0.65	0.00	19.41	6.42	2.00	0.00	0.65	0.00
19.42	6.41	2.00	0.00	0.65	0.00	19.43	6.41	2.00	0.00	0.65	0.00
19.44	6.41	2.00	0.00	0.65	0.00	19.45	6.41	2.00	0.00	0.65	0.00
19.46	6.41	2.00	0.00	0.65	0.00	19.47	6.41	2.00	0.00	0.65	0.00
19.48	6.41	2.00	0.00	0.65	0.00	19.49	6.41	2.00	0.00	0.65	0.00
19.50	6.41	2.00	0.00	0.65	0.00	19.51	6.41	2.00	0.00	0.65	0.00
19.52	6.40	2.00	0.00	0.65	0.00	19.53	6.40	2.00	0.00	0.64	0.00
19.54	6.40	2.00	0.00	0.64	0.00	19.55	6.40	2.00	0.00	0.64	0.00
19.56	6.40	2.00	0.00	0.64	0.00	19.57	6.40	2.00	0.00	0.64	0.00
19.58	6.40	2.00	0.00	0.64	0.00	19.59	6.40	2.00	0.00	0.64	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
19.60	6.40	2.00	0.00	0.64	0.00	19.61	6.39	2.00	0.00	0.64	0.00
19.62	6.39	2.00	0.00	0.64	0.00	19.63	6.37	2.00	0.00	0.64	0.00
19.64	6.36	2.00	0.00	0.64	0.00	19.65	6.34	2.00	0.00	0.64	0.00
19.66	6.33	2.00	0.00	0.64	0.00	19.67	6.31	2.00	0.00	0.64	0.00
19.68	6.30	2.00	0.00	0.64	0.00	19.69	6.28	2.00	0.00	0.64	0.00
19.70	6.27	2.00	0.00	0.64	0.00	19.71	6.19	2.00	0.00	0.64	0.00
19.72	6.09	2.00	0.00	0.64	0.00	19.73	5.97	2.00	0.00	0.64	0.00
19.74	5.85	2.00	0.00	0.64	0.00	19.75	5.72	2.00	0.00	0.64	0.00
19.76	5.61	2.00	0.00	0.64	0.00	19.77	5.50	2.00	0.00	0.64	0.00
19.78	5.40	2.00	0.00	0.64	0.00	19.79	5.52	2.00	0.00	0.64	0.00
19.80	6.01	2.00	0.00	0.64	0.00	19.81	6.60	2.00	0.00	0.64	0.00
19.82	7.26	2.00	0.00	0.64	0.00	19.83	7.95	2.00	0.00	0.64	0.00
19.84	8.63	2.00	0.00	0.64	0.00	19.85	9.27	2.00	0.00	0.64	0.00
19.86	9.84	2.00	0.00	0.64	0.00	19.87	10.31	2.00	0.00	0.64	0.00
19.88	10.77	2.00	0.00	0.64	0.00	19.89	11.37	2.00	0.00	0.64	0.00
19.90	12.07	2.00	0.00	0.64	0.00	19.91	12.84	2.00	0.00	0.64	0.00
19.92	13.62	2.00	0.00	0.64	0.00	19.93	14.38	2.00	0.00	0.64	0.00
19.94	15.09	2.00	0.00	0.64	0.00	19.95	15.71	2.00	0.00	0.64	0.00
19.96	16.12	2.00	0.00	0.64	0.00	19.97	15.60	2.00	0.00	0.64	0.00
19.98	14.96	2.00	0.00	0.64	0.00	19.99	14.24	2.00	0.00	0.64	0.00
20.00	13.46	2.00	0.00	0.64	0.00	20.01	12.68	2.00	0.00	0.64	0.00
20.02	11.92	2.00	0.00	0.64	0.00	20.03	11.23	2.00	0.00	0.64	0.00
20.04	10.64	2.00	0.00	0.64	0.00	20.05	10.21	2.00	0.00	0.64	0.00
20.06	9.76	2.00	0.00	0.64	0.00	20.07	9.21	2.00	0.00	0.64	0.00
20.08	8.60	2.00	0.00	0.63	0.00	20.09	7.96	2.00	0.00	0.63	0.00
20.10	7.32	2.00	0.00	0.63	0.00	20.11	6.72	2.00	0.00	0.63	0.00
20.12	6.18	2.00	0.00	0.63	0.00	20.13	5.75	2.00	0.00	0.63	0.00
20.14	5.65	2.00	0.00	0.63	0.00	20.15	5.62	2.00	0.00	0.63	0.00
20.16	5.60	2.00	0.00	0.63	0.00	20.17	5.56	2.00	0.00	0.63	0.00
20.18	5.53	2.00	0.00	0.63	0.00	20.19	5.50	2.00	0.00	0.63	0.00
20.20	5.47	2.00	0.00	0.63	0.00	20.21	5.45	2.00	0.00	0.63	0.00
20.22	5.43	2.00	0.00	0.63	0.00	20.23	5.41	2.00	0.00	0.63	0.00
20.24	5.38	2.00	0.00	0.63	0.00	20.25	5.35	2.00	0.00	0.63	0.00
20.26	5.32	2.00	0.00	0.63	0.00	20.27	5.29	2.00	0.00	0.63	0.00
20.28	5.26	2.00	0.00	0.63	0.00	20.29	5.23	2.00	0.00	0.63	0.00
20.30	5.21	2.00	0.00	0.63	0.00	20.31	5.27	2.00	0.00	0.63	0.00
20.32	5.47	2.00	0.00	0.63	0.00	20.33	5.70	2.00	0.00	0.63	0.00
20.34	5.96	2.00	0.00	0.63	0.00	20.35	6.24	2.00	0.00	0.63	0.00
20.36	6.51	2.00	0.00	0.63	0.00	20.37	6.76	2.00	0.00	0.63	0.00
20.38	6.99	2.00	0.00	0.63	0.00	20.39	7.17	2.00	0.00	0.63	0.00
20.40	7.40	2.00	0.00	0.63	0.00	20.41	7.70	2.00	0.00	0.63	0.00
20.42	8.05	2.00	0.00	0.63	0.00	20.43	8.43	2.00	0.00	0.63	0.00
20.44	8.83	2.00	0.00	0.63	0.00	20.45	9.21	2.00	0.00	0.63	0.00
20.46	9.56	2.00	0.00	0.63	0.00	20.47	9.87	2.00	0.00	0.63	0.00
20.48	10.11	2.00	0.00	0.63	0.00	20.49	10.41	2.00	0.00	0.63	0.00
20.50	10.78	2.00	0.00	0.63	0.00	20.51	11.20	2.00	0.00	0.63	0.00
20.52	11.64	2.00	0.00	0.63	0.00	20.53	12.09	2.00	0.00	0.63	0.00
20.54	12.52	2.00	0.00	0.63	0.00	20.55	12.90	2.00	0.00	0.63	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
20.56	13.23	2.00	0.00	0.63	0.00	20.57	13.44	2.00	0.00	0.63	0.00
20.58	13.63	2.00	0.00	0.63	0.00	20.59	13.86	2.00	0.00	0.63	0.00
20.60	14.12	2.00	0.00	0.63	0.00	20.61	14.38	2.00	0.00	0.63	0.00
20.62	14.65	2.00	0.00	0.63	0.00	20.63	14.89	2.00	0.00	0.62	0.00
20.64	15.11	2.00	0.00	0.62	0.00	20.65	15.29	2.00	0.00	0.62	0.00
20.66	15.45	2.00	0.00	0.62	0.00	20.67	15.65	2.00	0.00	0.62	0.00
20.68	15.89	2.00	0.00	0.62	0.00	20.69	16.15	2.00	0.00	0.62	0.00
20.70	16.41	2.00	0.00	0.62	0.00	20.71	16.67	2.00	0.00	0.62	0.00
20.72	16.91	2.00	0.00	0.62	0.00	20.73	17.11	2.00	0.00	0.62	0.00
20.74	17.24	2.00	0.00	0.62	0.00	20.75	17.15	2.00	0.00	0.62	0.00
20.76	17.03	2.00	0.00	0.62	0.00	20.77	16.91	2.00	0.00	0.62	0.00
20.78	16.77	2.00	0.00	0.62	0.00	20.79	16.64	2.00	0.00	0.62	0.00
20.80	16.51	2.00	0.00	0.62	0.00	20.81	16.39	2.00	0.00	0.62	0.00
20.82	16.29	2.00	0.00	0.62	0.00	20.83	16.11	2.00	0.00	0.62	0.00
20.84	15.79	2.00	0.00	0.62	0.00	20.85	15.40	2.00	0.00	0.62	0.00
20.86	14.97	2.00	0.00	0.62	0.00	20.87	14.53	2.00	0.00	0.62	0.00
20.88	14.08	2.00	0.00	0.62	0.00	20.89	13.67	2.00	0.00	0.62	0.00
20.90	13.30	2.00	0.00	0.62	0.00	20.91	13.00	2.00	0.00	0.62	0.00
20.92	12.81	2.00	0.00	0.62	0.00	20.93	12.60	2.00	0.00	0.62	0.00
20.94	12.36	2.00	0.00	0.62	0.00	20.95	12.10	2.00	0.00	0.62	0.00
20.96	11.82	2.00	0.00	0.62	0.00	20.97	11.56	2.00	0.00	0.62	0.00
20.98	11.32	2.00	0.00	0.62	0.00	20.99	11.11	2.00	0.00	0.62	0.00
21.00	10.94	2.00	0.00	0.62	0.00	21.01	10.76	2.00	0.00	0.62	0.00
21.02	10.54	2.00	0.00	0.62	0.00	21.03	10.28	2.00	0.00	0.62	0.00
21.04	10.02	2.00	0.00	0.62	0.00	21.05	9.75	2.00	0.00	0.62	0.00
21.06	9.49	2.00	0.00	0.62	0.00	21.07	9.25	2.00	0.00	0.62	0.00
21.08	9.06	2.00	0.00	0.62	0.00	21.09	8.94	2.00	0.00	0.62	0.00
21.10	8.84	2.00	0.00	0.62	0.00	21.11	8.72	2.00	0.00	0.62	0.00
21.12	8.59	2.00	0.00	0.62	0.00	21.13	8.45	2.00	0.00	0.62	0.00
21.14	8.32	2.00	0.00	0.62	0.00	21.15	8.19	2.00	0.00	0.62	0.00
21.16	8.08	2.00	0.00	0.62	0.00	21.17	7.99	2.00	0.00	0.62	0.00
21.18	8.17	2.00	0.00	0.61	0.00	21.19	8.45	2.00	0.00	0.61	0.00
21.20	8.77	2.00	0.00	0.61	0.00	21.21	9.12	2.00	0.00	0.61	0.00
21.22	9.48	2.00	0.00	0.61	0.00	21.23	9.82	2.00	0.00	0.61	0.00
21.24	10.14	2.00	0.00	0.61	0.00	21.25	10.42	2.00	0.00	0.61	0.00
21.26	10.68	2.00	0.00	0.61	0.00	21.27	11.19	2.00	0.00	0.61	0.00
21.28	11.82	2.00	0.00	0.61	0.00	21.29	12.53	2.00	0.00	0.61	0.00
21.30	13.28	2.00	0.00	0.61	0.00	21.31	14.04	2.00	0.00	0.61	0.00
21.32	14.76	2.00	0.00	0.61	0.00	21.33	15.41	2.00	0.00	0.61	0.00
21.34	15.95	2.00	0.00	0.61	0.00	21.35	16.29	2.00	0.00	0.61	0.00
21.36	16.61	2.00	0.00	0.61	0.00	21.37	16.99	2.00	0.00	0.61	0.00
21.38	17.41	2.00	0.00	0.61	0.00	21.39	17.85	2.00	0.00	0.61	0.00
21.40	18.28	2.00	0.00	0.61	0.00	21.41	18.69	2.00	0.00	0.61	0.00
21.42	19.04	2.00	0.00	0.61	0.00	21.43	19.33	2.00	0.00	0.61	0.00
21.44	19.67	2.00	0.00	0.61	0.00	21.45	20.10	2.00	0.00	0.61	0.00
21.46	20.61	2.00	0.00	0.61	0.00	21.47	21.16	2.00	0.00	0.61	0.00
21.48	21.72	2.00	0.00	0.61	0.00	21.49	22.26	2.00	0.00	0.61	0.00
21.50	22.76	2.00	0.00	0.61	0.00	21.51	23.19	2.00	0.00	0.61	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
21.52	23.45	2.00	0.00	0.61	0.00	21.53	23.46	2.00	0.00	0.61	0.00
21.54	23.47	2.00	0.00	0.61	0.00	21.55	23.49	2.00	0.00	0.61	0.00
21.56	23.50	2.00	0.00	0.61	0.00	21.57	23.51	2.00	0.00	0.61	0.00
21.58	23.52	2.00	0.00	0.61	0.00	21.59	23.54	2.00	0.00	0.61	0.00
21.60	23.54	2.00	0.00	0.61	0.00	21.61	23.27	2.00	0.00	0.61	0.00
21.62	22.67	2.00	0.00	0.61	0.00	21.63	21.95	2.00	0.00	0.61	0.00
21.64	21.17	2.00	0.00	0.61	0.00	21.65	20.35	2.00	0.00	0.61	0.00
21.66	19.54	2.00	0.00	0.61	0.00	21.67	18.78	2.00	0.00	0.61	0.00
21.68	18.11	2.00	0.00	0.61	0.00	21.69	17.57	2.00	0.00	0.61	0.00
21.70	17.21	2.00	0.00	0.61	0.00	21.71	16.76	2.00	0.00	0.61	0.00
21.72	16.25	2.00	0.00	0.61	0.00	21.73	15.70	2.00	0.00	0.60	0.00
21.74	15.13	2.00	0.00	0.60	0.00	21.75	14.58	2.00	0.00	0.60	0.00
21.76	14.08	2.00	0.00	0.60	0.00	21.77	13.64	2.00	0.00	0.60	0.00
21.78	13.31	2.00	0.00	0.60	0.00	21.79	12.97	2.00	0.00	0.60	0.00
21.80	12.55	2.00	0.00	0.60	0.00	21.81	12.08	2.00	0.00	0.60	0.00
21.82	11.58	2.00	0.00	0.60	0.00	21.83	11.08	2.00	0.00	0.60	0.00
21.84	10.61	2.00	0.00	0.60	0.00	21.85	10.18	2.00	0.00	0.60	0.00
21.86	9.82	2.00	0.00	0.60	0.00	21.87	9.57	2.00	0.00	0.60	0.00
21.88	9.30	2.00	0.00	0.60	0.00	21.89	8.97	2.00	0.00	0.60	0.00
21.90	8.62	2.00	0.00	0.60	0.00	21.91	8.25	2.00	0.00	0.60	0.00
21.92	7.89	2.00	0.00	0.60	0.00	21.93	7.55	2.00	0.00	0.60	0.00
21.94	7.25	2.00	0.00	0.60	0.00	21.95	7.01	2.00	0.00	0.60	0.00
21.96	6.93	2.00	0.00	0.60	0.00	21.97	6.83	2.00	0.00	0.60	0.00
21.98	6.72	2.00	0.00	0.60	0.00	21.99	6.61	2.00	0.00	0.60	0.00
22.00	6.49	2.00	0.00	0.60	0.00	22.01	6.37	2.00	0.00	0.60	0.00
22.02	6.27	2.00	0.00	0.60	0.00	22.03	6.17	2.00	0.00	0.60	0.00
22.04	6.12	2.00	0.00	0.60	0.00	22.05	6.12	2.00	0.00	0.60	0.00
22.06	6.12	2.00	0.00	0.60	0.00	22.07	6.12	2.00	0.00	0.60	0.00
22.08	6.12	2.00	0.00	0.60	0.00	22.09	6.12	2.00	0.00	0.60	0.00
22.10	6.11	2.00	0.00	0.60	0.00	22.11	6.11	2.00	0.00	0.60	0.00
22.12	6.11	2.00	0.00	0.60	0.00	22.13	6.11	2.00	0.00	0.60	0.00
22.14	6.11	2.00	0.00	0.60	0.00	22.15	6.11	2.00	0.00	0.60	0.00
22.16	6.11	2.00	0.00	0.60	0.00	22.17	6.11	2.00	0.00	0.60	0.00
22.18	6.11	2.00	0.00	0.60	0.00	22.19	6.11	2.00	0.00	0.60	0.00
22.20	6.11	2.00	0.00	0.60	0.00	22.21	6.10	2.00	0.00	0.60	0.00
22.22	6.07	2.00	0.00	0.60	0.00	22.23	6.02	2.00	0.00	0.60	0.00
22.24	5.97	2.00	0.00	0.60	0.00	22.25	5.91	2.00	0.00	0.60	0.00
22.26	5.85	2.00	0.00	0.60	0.00	22.27	5.79	2.00	0.00	0.60	0.00
22.28	5.74	2.00	0.00	0.59	0.00	22.29	5.69	2.00	0.00	0.59	0.00
22.30	5.68	2.00	0.00	0.59	0.00	22.31	5.76	2.00	0.00	0.59	0.00
22.32	5.86	2.00	0.00	0.59	0.00	22.33	5.97	2.00	0.00	0.59	0.00
22.34	6.09	2.00	0.00	0.59	0.00	22.35	6.21	2.00	0.00	0.59	0.00
22.36	6.32	2.00	0.00	0.59	0.00	22.37	6.42	2.00	0.00	0.59	0.00
22.38	6.50	2.00	0.00	0.59	0.00	22.39	6.54	2.00	0.00	0.59	0.00
22.40	6.59	2.00	0.00	0.59	0.00	22.41	6.64	2.00	0.00	0.59	0.00
22.42	6.69	2.00	0.00	0.59	0.00	22.43	6.75	2.00	0.00	0.59	0.00
22.44	6.81	2.00	0.00	0.59	0.00	22.45	6.86	2.00	0.00	0.59	0.00
22.46	6.91	2.00	0.00	0.59	0.00	22.47	6.94	2.00	0.00	0.59	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
22.48	7.00	2.00	0.00	0.59	0.00	22.49	7.07	2.00	0.00	0.59	0.00
22.50	7.15	2.00	0.00	0.59	0.00	22.51	7.23	2.00	0.00	0.59	0.00
22.52	7.32	2.00	0.00	0.59	0.00	22.53	7.40	2.00	0.00	0.59	0.00
22.54	7.48	2.00	0.00	0.59	0.00	22.55	7.54	2.00	0.00	0.59	0.00
22.56	7.58	2.00	0.00	0.59	0.00	22.57	7.58	2.00	0.00	0.59	0.00
22.58	7.58	2.00	0.00	0.59	0.00	22.59	7.58	2.00	0.00	0.59	0.00
22.60	7.58	2.00	0.00	0.59	0.00	22.61	7.57	2.00	0.00	0.59	0.00
22.62	7.57	2.00	0.00	0.59	0.00	22.63	7.57	2.00	0.00	0.59	0.00
22.64	7.57	2.00	0.00	0.59	0.00	22.65	7.49	2.00	0.00	0.59	0.00
22.66	7.33	2.00	0.00	0.59	0.00	22.67	7.15	2.00	0.00	0.59	0.00
22.68	6.95	2.00	0.00	0.59	0.00	22.69	6.75	2.00	0.00	0.59	0.00
22.70	6.54	2.00	0.00	0.59	0.00	22.71	6.35	2.00	0.00	0.59	0.00
22.72	6.19	2.00	0.00	0.59	0.00	22.73	6.06	2.00	0.00	0.59	0.00
22.74	6.06	2.00	0.00	0.59	0.00	22.75	6.06	2.00	0.00	0.59	0.00
22.76	6.05	2.00	0.00	0.59	0.00	22.77	6.05	2.00	0.00	0.59	0.00
22.78	6.05	2.00	0.00	0.59	0.00	22.79	6.05	2.00	0.00	0.59	0.00
22.80	6.05	2.00	0.00	0.59	0.00	22.81	6.05	2.00	0.00	0.59	0.00
22.82	6.05	2.00	0.00	0.59	0.00	22.83	6.05	2.00	0.00	0.58	0.00
22.84	6.05	2.00	0.00	0.58	0.00	22.85	6.05	2.00	0.00	0.58	0.00
22.86	6.05	2.00	0.00	0.58	0.00	22.87	6.04	2.00	0.00	0.58	0.00
22.88	6.04	2.00	0.00	0.58	0.00	22.89	6.04	2.00	0.00	0.58	0.00
22.90	6.04	2.00	0.00	0.58	0.00	22.91	6.04	2.00	0.00	0.58	0.00
22.92	6.04	2.00	0.00	0.58	0.00	22.93	6.04	2.00	0.00	0.58	0.00
22.94	6.04	2.00	0.00	0.58	0.00	22.95	6.04	2.00	0.00	0.58	0.00
22.96	6.04	2.00	0.00	0.58	0.00	22.97	6.04	2.00	0.00	0.58	0.00
22.98	6.04	2.00	0.00	0.58	0.00	22.99	6.04	2.00	0.00	0.58	0.00
23.00	6.22	2.00	0.00	0.58	0.00	23.01	6.46	2.00	0.00	0.58	0.00
23.02	6.72	2.00	0.00	0.58	0.00	23.03	7.01	2.00	0.00	0.58	0.00
23.04	7.30	2.00	0.00	0.58	0.00	23.05	7.58	2.00	0.00	0.58	0.00
23.06	7.84	2.00	0.00	0.58	0.00	23.07	8.05	2.00	0.00	0.58	0.00
23.08	8.19	2.00	0.00	0.58	0.00	23.09	8.27	2.00	0.00	0.58	0.00
23.10	8.36	2.00	0.00	0.58	0.00	23.11	8.47	2.00	0.00	0.58	0.00
23.12	8.59	2.00	0.00	0.58	0.00	23.13	8.70	2.00	0.00	0.58	0.00
23.14	8.81	2.00	0.00	0.58	0.00	23.15	8.91	2.00	0.00	0.58	0.00
23.16	8.98	2.00	0.00	0.58	0.00	23.17	8.98	2.00	0.00	0.58	0.00
23.18	8.93	2.00	0.00	0.58	0.00	23.19	8.88	2.00	0.00	0.58	0.00
23.20	8.82	2.00	0.00	0.58	0.00	23.21	8.76	2.00	0.00	0.58	0.00
23.22	8.70	2.00	0.00	0.58	0.00	23.23	8.65	2.00	0.00	0.58	0.00
23.24	8.60	2.00	0.00	0.58	0.00	23.25	8.57	2.00	0.00	0.58	0.00
23.26	8.64	2.00	0.00	0.58	0.00	23.27	8.73	2.00	0.00	0.58	0.00
23.28	8.84	2.00	0.00	0.58	0.00	23.29	8.95	2.00	0.00	0.58	0.00
23.30	9.07	2.00	0.00	0.58	0.00	23.31	9.18	2.00	0.00	0.58	0.00
23.32	9.28	2.00	0.00	0.58	0.00	23.33	9.36	2.00	0.00	0.58	0.00
23.34	9.43	2.00	0.00	0.58	0.00	23.35	9.51	2.00	0.00	0.58	0.00
23.36	9.60	2.00	0.00	0.58	0.00	23.37	9.71	2.00	0.00	0.58	0.00
23.38	9.83	2.00	0.00	0.57	0.00	23.39	9.94	2.00	0.00	0.57	0.00
23.40	10.05	2.00	0.00	0.57	0.00	23.41	10.14	2.00	0.00	0.57	0.00
23.42	10.22	2.00	0.00	0.57	0.00	23.43	10.29	2.00	0.00	0.57	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
23.44	10.37	2.00	0.00	0.57	0.00	23.45	10.47	2.00	0.00	0.57	0.00
23.46	10.58	2.00	0.00	0.57	0.00	23.47	10.70	2.00	0.00	0.57	0.00
23.48	10.81	2.00	0.00	0.57	0.00	23.49	10.91	2.00	0.00	0.57	0.00
23.50	11.00	2.00	0.00	0.57	0.00	23.51	11.07	2.00	0.00	0.57	0.00
23.52	11.17	2.00	0.00	0.57	0.00	23.53	11.30	2.00	0.00	0.57	0.00
23.54	11.44	2.00	0.00	0.57	0.00	23.55	11.60	2.00	0.00	0.57	0.00
23.56	11.75	2.00	0.00	0.57	0.00	23.57	11.90	2.00	0.00	0.57	0.00
23.58	12.04	2.00	0.00	0.57	0.00	23.59	12.15	2.00	0.00	0.57	0.00
23.60	12.23	2.00	0.00	0.57	0.00	23.61	12.31	2.00	0.00	0.57	0.00
23.62	12.41	2.00	0.00	0.57	0.00	23.63	12.51	2.00	0.00	0.57	0.00
23.64	12.63	2.00	0.00	0.57	0.00	23.65	12.74	2.00	0.00	0.57	0.00
23.66	12.84	2.00	0.00	0.57	0.00	23.67	12.94	2.00	0.00	0.57	0.00
23.68	13.01	2.00	0.00	0.57	0.00	23.69	13.01	2.00	0.00	0.57	0.00
23.70	12.97	2.00	0.00	0.57	0.00	23.71	12.93	2.00	0.00	0.57	0.00
23.72	12.89	2.00	0.00	0.57	0.00	23.73	12.84	2.00	0.00	0.57	0.00
23.74	12.80	2.00	0.00	0.57	0.00	23.75	12.76	2.00	0.00	0.57	0.00
23.76	12.72	2.00	0.00	0.57	0.00	23.77	12.72	2.00	0.00	0.57	0.00
23.78	12.99	2.00	0.00	0.57	0.00	23.79	13.34	2.00	0.00	0.57	0.00
23.80	13.73	2.00	0.00	0.57	0.00	23.81	14.15	2.00	0.00	0.57	0.00
23.82	14.58	2.00	0.00	0.57	0.00	23.83	14.98	2.00	0.00	0.57	0.00
23.84	15.35	2.00	0.00	0.57	0.00	23.85	15.67	2.00	0.00	0.57	0.00
23.86	15.85	2.00	0.00	0.57	0.00	23.87	15.97	2.00	0.00	0.57	0.00
23.88	16.11	2.00	0.00	0.57	0.00	23.89	16.27	2.00	0.00	0.57	0.00
23.90	16.44	2.00	0.00	0.57	0.00	23.91	16.60	2.00	0.00	0.57	0.00
23.92	16.76	2.00	0.00	0.57	0.00	23.93	16.90	2.00	0.00	0.56	0.00
23.94	17.01	2.00	0.00	0.56	0.00	23.95	16.88	2.00	0.00	0.56	0.00
23.96	16.64	2.00	0.00	0.56	0.00	23.97	16.36	2.00	0.00	0.56	0.00
23.98	16.05	2.00	0.00	0.56	0.00	23.99	15.74	2.00	0.00	0.56	0.00
24.00	15.43	2.00	0.00	0.56	0.00	24.01	15.15	2.00	0.00	0.56	0.00
24.02	14.90	2.00	0.00	0.56	0.00	24.03	14.72	2.00	0.00	0.56	0.00
24.04	14.68	2.00	0.00	0.56	0.00	24.05	14.63	2.00	0.00	0.56	0.00
24.06	14.57	2.00	0.00	0.56	0.00	24.07	14.52	2.00	0.00	0.56	0.00
24.08	14.46	2.00	0.00	0.56	0.00	24.09	14.40	2.00	0.00	0.56	0.00
24.10	14.35	2.00	0.00	0.56	0.00	24.11	14.30	2.00	0.00	0.56	0.00
24.12	14.23	2.00	0.00	0.56	0.00	24.13	14.09	2.00	0.00	0.56	0.00
24.14	13.91	2.00	0.00	0.56	0.00	24.15	13.72	2.00	0.00	0.56	0.00
24.16	13.52	2.00	0.00	0.56	0.00	24.17	13.32	2.00	0.00	0.56	0.00
24.18	13.14	2.00	0.00	0.56	0.00	24.19	12.97	2.00	0.00	0.56	0.00
24.20	12.83	2.00	0.00	0.56	0.00	24.21	12.71	2.00	0.00	0.56	0.00
24.22	12.55	2.00	0.00	0.56	0.00	24.23	12.37	2.00	0.00	0.56	0.00
24.24	12.18	2.00	0.00	0.56	0.00	24.25	11.98	2.00	0.00	0.56	0.00
24.26	11.78	2.00	0.00	0.56	0.00	24.27	11.60	2.00	0.00	0.56	0.00
24.28	11.44	2.00	0.00	0.56	0.00	24.29	11.35	2.00	0.00	0.56	0.00
24.30	11.48	2.00	0.00	0.56	0.00	24.31	11.64	2.00	0.00	0.56	0.00
24.32	11.82	2.00	0.00	0.56	0.00	24.33	12.02	2.00	0.00	0.56	0.00
24.34	12.21	2.00	0.00	0.56	0.00	24.35	12.40	2.00	0.00	0.56	0.00
24.36	12.57	2.00	0.00	0.56	0.00	24.37	12.71	2.00	0.00	0.56	0.00
24.38	12.83	2.00	0.00	0.56	0.00	24.39	12.97	2.00	0.00	0.56	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
24.40	13.14	2.00	0.00	0.56	0.00	24.41	13.32	2.00	0.00	0.56	0.00
24.42	13.52	2.00	0.00	0.56	0.00	24.43	13.71	2.00	0.00	0.56	0.00
24.44	13.89	2.00	0.00	0.56	0.00	24.45	14.05	2.00	0.00	0.56	0.00
24.46	14.18	2.00	0.00	0.56	0.00	24.47	14.20	2.00	0.00	0.56	0.00
24.48	14.20	2.00	0.00	0.55	0.00	24.49	14.20	2.00	0.00	0.55	0.00
24.50	14.19	2.00	0.00	0.55	0.00	24.51	14.19	2.00	0.00	0.55	0.00
24.52	14.19	2.00	0.00	0.55	0.00	24.53	14.19	2.00	0.00	0.55	0.00
24.54	14.18	2.00	0.00	0.55	0.00	24.55	14.17	2.00	0.00	0.55	0.00
24.56	14.09	2.00	0.00	0.55	0.00	24.57	14.00	2.00	0.00	0.55	0.00
24.58	13.89	2.00	0.00	0.55	0.00	24.59	13.78	2.00	0.00	0.55	0.00
24.60	13.66	2.00	0.00	0.55	0.00	24.61	13.55	2.00	0.00	0.55	0.00
24.62	13.45	2.00	0.00	0.55	0.00	24.63	13.37	2.00	0.00	0.55	0.00
24.64	13.30	2.00	0.00	0.55	0.00	24.65	13.22	2.00	0.00	0.55	0.00
24.66	13.12	2.00	0.00	0.55	0.00	24.67	13.01	2.00	0.00	0.55	0.00
24.68	12.89	2.00	0.00	0.55	0.00	24.69	12.78	2.00	0.00	0.55	0.00
24.70	12.67	2.00	0.00	0.55	0.00	24.71	12.58	2.00	0.00	0.55	0.00
24.72	12.50	2.00	0.00	0.55	0.00	24.73	12.43	2.00	0.00	0.55	0.00
24.74	12.34	2.00	0.00	0.55	0.00	24.75	12.24	2.00	0.00	0.55	0.00
24.76	12.13	2.00	0.00	0.55	0.00	24.77	12.01	2.00	0.00	0.55	0.00
24.78	11.90	2.00	0.00	0.55	0.00	24.79	11.80	2.00	0.00	0.55	0.00
24.80	11.71	2.00	0.00	0.55	0.00	24.81	11.63	2.00	0.00	0.55	0.00
24.82	11.47	2.00	0.00	0.55	0.00	24.83	11.29	2.00	0.00	0.55	0.00
24.84	11.07	2.00	0.00	0.55	0.00	24.85	10.85	2.00	0.00	0.55	0.00
24.86	10.62	2.00	0.00	0.55	0.00	24.87	10.41	2.00	0.00	0.55	0.00
24.88	10.21	2.00	0.00	0.55	0.00	24.89	10.05	2.00	0.00	0.55	0.00
24.90	9.95	2.00	0.00	0.55	0.00	24.91	9.86	2.00	0.00	0.55	0.00
24.92	9.76	2.00	0.00	0.55	0.00	24.93	9.65	2.00	0.00	0.55	0.00
24.94	9.54	2.00	0.00	0.55	0.00	24.95	9.43	2.00	0.00	0.55	0.00
24.96	9.32	2.00	0.00	0.55	0.00	24.97	9.23	2.00	0.00	0.55	0.00
24.98	9.15	2.00	0.00	0.55	0.00	24.99	9.08	2.00	0.00	0.55	0.00
25.00	8.99	2.00	0.00	0.55	0.00	25.01	8.89	2.00	0.00	0.55	0.00
25.02	8.78	2.00	0.00	0.55	0.00	25.03	8.66	2.00	0.00	0.54	0.00
25.04	8.55	2.00	0.00	0.54	0.00	25.05	8.45	2.00	0.00	0.54	0.00
25.06	8.36	2.00	0.00	0.54	0.00	25.07	8.29	2.00	0.00	0.54	0.00
25.08	8.21	2.00	0.00	0.54	0.00	25.09	8.12	2.00	0.00	0.54	0.00
25.10	8.01	2.00	0.00	0.54	0.00	25.11	7.90	2.00	0.00	0.54	0.00
25.12	7.79	2.00	0.00	0.54	0.00	25.13	7.68	2.00	0.00	0.54	0.00
25.14	7.58	2.00	0.00	0.54	0.00	25.15	7.50	2.00	0.00	0.54	0.00
25.16	7.47	2.00	0.00	0.54	0.00	25.17	7.47	2.00	0.00	0.54	0.00
25.18	7.47	2.00	0.00	0.54	0.00	25.19	7.46	2.00	0.00	0.54	0.00
25.20	7.46	2.00	0.00	0.54	0.00	25.21	7.46	2.00	0.00	0.54	0.00
25.22	7.46	2.00	0.00	0.54	0.00	25.23	7.46	2.00	0.00	0.54	0.00
25.24	7.46	2.00	0.00	0.54	0.00	25.25	7.40	2.00	0.00	0.54	0.00
25.26	7.31	2.00	0.00	0.54	0.00	25.27	7.20	2.00	0.00	0.54	0.00
25.28	7.09	2.00	0.00	0.54	0.00	25.29	6.98	2.00	0.00	0.54	0.00
25.30	6.87	2.00	0.00	0.54	0.00	25.31	6.77	2.00	0.00	0.54	0.00
25.32	6.68	2.00	0.00	0.54	0.00	25.33	6.63	2.00	0.00	0.54	0.00
25.34	6.62	2.00	0.00	0.54	0.00	25.35	6.62	2.00	0.00	0.54	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
25.36	6.62	2.00	0.00	0.54	0.00	25.37	6.62	2.00	0.00	0.54	0.00
25.38	6.62	2.00	0.00	0.54	0.00	25.39	6.62	2.00	0.00	0.54	0.00
25.40	6.62	2.00	0.00	0.54	0.00	25.41	6.62	2.00	0.00	0.54	0.00
25.42	6.65	2.00	0.00	0.54	0.00	25.43	6.74	2.00	0.00	0.54	0.00
25.44	6.83	2.00	0.00	0.54	0.00	25.45	6.94	2.00	0.00	0.54	0.00
25.46	7.05	2.00	0.00	0.54	0.00	25.47	7.16	2.00	0.00	0.54	0.00
25.48	7.26	2.00	0.00	0.54	0.00	25.49	7.35	2.00	0.00	0.54	0.00
25.50	7.43	2.00	0.00	0.54	0.00	25.51	7.49	2.00	0.00	0.54	0.00
25.52	7.58	2.00	0.00	0.54	0.00	25.53	7.68	2.00	0.00	0.54	0.00
25.54	7.79	2.00	0.00	0.54	0.00	25.55	7.90	2.00	0.00	0.54	0.00
25.56	8.01	2.00	0.00	0.54	0.00	25.57	8.11	2.00	0.00	0.54	0.00
25.58	8.19	2.00	0.00	0.53	0.00	25.59	8.26	2.00	0.00	0.53	0.00
25.60	8.33	2.00	0.00	0.53	0.00	25.61	8.42	2.00	0.00	0.53	0.00
25.62	8.53	2.00	0.00	0.53	0.00	25.63	8.64	2.00	0.00	0.53	0.00
25.64	8.75	2.00	0.00	0.53	0.00	25.65	8.85	2.00	0.00	0.53	0.00
25.66	8.95	2.00	0.00	0.53	0.00	25.67	9.02	2.00	0.00	0.53	0.00
25.68	9.05	2.00	0.00	0.53	0.00	25.69	9.05	2.00	0.00	0.53	0.00
25.70	9.05	2.00	0.00	0.53	0.00	25.71	9.04	2.00	0.00	0.53	0.00
25.72	9.04	2.00	0.00	0.53	0.00	25.73	9.04	2.00	0.00	0.53	0.00
25.74	9.04	2.00	0.00	0.53	0.00	25.75	9.04	2.00	0.00	0.53	0.00
25.76	9.04	2.00	0.00	0.53	0.00	25.77	9.10	2.00	0.00	0.53	0.00
25.78	9.19	2.00	0.00	0.53	0.00	25.79	9.29	2.00	0.00	0.53	0.00
25.80	9.40	2.00	0.00	0.53	0.00	25.81	9.51	2.00	0.00	0.53	0.00
25.82	9.61	2.00	0.00	0.53	0.00	25.83	9.71	2.00	0.00	0.53	0.00
25.84	9.79	2.00	0.00	0.53	0.00	25.85	9.86	2.00	0.00	0.53	0.00
25.86	9.93	2.00	0.00	0.53	0.00	25.87	10.02	2.00	0.00	0.53	0.00
25.88	10.13	2.00	0.00	0.53	0.00	25.89	10.24	2.00	0.00	0.53	0.00
25.90	10.34	2.00	0.00	0.53	0.00	25.91	10.45	2.00	0.00	0.53	0.00
25.92	10.54	2.00	0.00	0.53	0.00	25.93	10.62	2.00	0.00	0.53	0.00
25.94	10.77	2.00	0.00	0.53	0.00	25.95	11.04	2.00	0.00	0.53	0.00
25.96	11.35	2.00	0.00	0.53	0.00	25.97	11.70	2.00	0.00	0.53	0.00
25.98	12.06	2.00	0.00	0.53	0.00	25.99	12.41	2.00	0.00	0.53	0.00
26.00	12.74	2.00	0.00	0.53	0.00	26.01	13.03	2.00	0.00	0.53	0.00
26.02	13.26	2.00	0.00	0.53	0.00	26.03	13.33	2.00	0.00	0.53	0.00
26.04	13.42	2.00	0.00	0.53	0.00	26.05	13.51	2.00	0.00	0.53	0.00
26.06	13.62	2.00	0.00	0.53	0.00	26.07	13.73	2.00	0.00	0.53	0.00
26.08	13.83	2.00	0.00	0.53	0.00	26.09	13.93	2.00	0.00	0.53	0.00
26.10	14.01	2.00	0.00	0.53	0.00	26.11	14.01	2.00	0.00	0.53	0.00
26.12	13.84	2.00	0.00	0.53	0.00	26.13	13.63	2.00	0.00	0.52	0.00
26.14	13.39	2.00	0.00	0.52	0.00	26.15	13.15	2.00	0.00	0.52	0.00
26.16	12.90	2.00	0.00	0.52	0.00	26.17	12.66	2.00	0.00	0.52	0.00
26.18	12.45	2.00	0.00	0.52	0.00	26.19	12.27	2.00	0.00	0.52	0.00
26.20	12.22	2.00	0.00	0.52	0.00	26.21	12.21	2.00	0.00	0.52	0.00
26.22	12.21	2.00	0.00	0.52	0.00	26.23	12.21	2.00	0.00	0.52	0.00
26.24	12.21	2.00	0.00	0.52	0.00	26.25	12.21	2.00	0.00	0.52	0.00
26.26	12.20	2.00	0.00	0.52	0.00	26.27	12.20	2.00	0.00	0.52	0.00
26.28	12.20	2.00	0.00	0.52	0.00	26.29	12.27	2.00	0.00	0.52	0.00
26.30	12.35	2.00	0.00	0.52	0.00	26.31	12.45	2.00	0.00	0.52	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
26.32	12.56	2.00	0.00	0.52	0.00	26.33	12.67	2.00	0.00	0.52	0.00
26.34	12.77	2.00	0.00	0.52	0.00	26.35	12.87	2.00	0.00	0.52	0.00
26.36	12.95	2.00	0.00	0.52	0.00	26.37	13.01	2.00	0.00	0.52	0.00
26.38	13.08	2.00	0.00	0.52	0.00	26.39	13.17	2.00	0.00	0.52	0.00
26.40	13.28	2.00	0.00	0.52	0.00	26.41	13.38	2.00	0.00	0.52	0.00
26.42	13.49	2.00	0.00	0.52	0.00	26.43	13.59	2.00	0.00	0.52	0.00
26.44	13.68	2.00	0.00	0.52	0.00	26.45	13.76	2.00	0.00	0.52	0.00
26.46	13.78	2.00	0.00	0.52	0.00	26.47	13.77	2.00	0.00	0.52	0.00
26.48	13.77	2.00	0.00	0.52	0.00	26.49	13.77	2.00	0.00	0.52	0.00
26.50	13.77	2.00	0.00	0.52	0.00	26.51	13.76	2.00	0.00	0.52	0.00
26.52	13.76	2.00	0.00	0.52	0.00	26.53	13.76	2.00	0.00	0.52	0.00
26.54	13.76	2.00	0.00	0.52	0.00	26.55	13.79	2.00	0.00	0.52	0.00
26.56	13.83	2.00	0.00	0.52	0.00	26.57	13.88	2.00	0.00	0.52	0.00
26.58	13.93	2.00	0.00	0.52	0.00	26.59	13.98	2.00	0.00	0.52	0.00
26.60	14.04	2.00	0.00	0.52	0.00	26.61	14.08	2.00	0.00	0.52	0.00
26.62	14.12	2.00	0.00	0.52	0.00	26.63	14.12	2.00	0.00	0.52	0.00
26.64	14.04	2.00	0.00	0.52	0.00	26.65	13.95	2.00	0.00	0.52	0.00
26.66	13.84	2.00	0.00	0.52	0.00	26.67	13.73	2.00	0.00	0.52	0.00
26.68	13.62	2.00	0.00	0.51	0.00	26.69	13.51	2.00	0.00	0.51	0.00
26.70	13.42	2.00	0.00	0.51	0.00	26.71	13.34	2.00	0.00	0.51	0.00
26.72	13.25	2.00	0.00	0.51	0.00	26.73	13.12	2.00	0.00	0.51	0.00
26.74	12.98	2.00	0.00	0.51	0.00	26.75	12.82	2.00	0.00	0.51	0.00
26.76	12.65	2.00	0.00	0.51	0.00	26.77	12.49	2.00	0.00	0.51	0.00
26.78	12.34	2.00	0.00	0.51	0.00	26.79	12.20	2.00	0.00	0.51	0.00
26.80	12.10	2.00	0.00	0.51	0.00	26.81	12.10	2.00	0.00	0.51	0.00
26.82	12.10	2.00	0.00	0.51	0.00	26.83	12.09	2.00	0.00	0.51	0.00
26.84	12.09	2.00	0.00	0.51	0.00	26.85	12.09	2.00	0.00	0.51	0.00
26.86	12.09	2.00	0.00	0.51	0.00	26.87	12.09	2.00	0.00	0.51	0.00
26.88	12.08	2.00	0.00	0.51	0.00	26.89	12.17	2.00	0.00	0.51	0.00
26.90	12.45	2.00	0.00	0.51	0.00	26.91	12.80	2.00	0.00	0.51	0.00
26.92	13.18	2.00	0.00	0.51	0.00	26.93	13.59	2.00	0.00	0.51	0.00
26.94	13.99	2.00	0.00	0.51	0.00	26.95	14.37	2.00	0.00	0.51	0.00
26.96	14.72	2.00	0.00	0.51	0.00	26.97	15.00	2.00	0.00	0.51	0.00
26.98	14.96	2.00	0.00	0.51	0.00	26.99	14.77	2.00	0.00	0.51	0.00
27.00	14.55	2.00	0.00	0.51	0.00	27.01	14.31	2.00	0.00	0.51	0.00
27.02	14.06	2.00	0.00	0.51	0.00	27.03	13.82	2.00	0.00	0.51	0.00
27.04	13.59	2.00	0.00	0.51	0.00	27.05	13.40	2.00	0.00	0.51	0.00
27.06	13.24	2.00	0.00	0.51	0.00	27.07	12.90	2.00	0.00	0.51	0.00
27.08	12.48	2.00	0.00	0.51	0.00	27.09	12.00	2.00	0.00	0.51	0.00
27.10	11.49	2.00	0.00	0.51	0.00	27.11	10.97	2.00	0.00	0.51	0.00
27.12	10.47	2.00	0.00	0.51	0.00	27.13	10.02	2.00	0.00	0.51	0.00
27.14	9.63	2.00	0.00	0.51	0.00	27.15	9.47	2.00	0.00	0.51	0.00
27.16	9.56	2.00	0.00	0.51	0.00	27.17	9.68	2.00	0.00	0.51	0.00
27.18	9.80	2.00	0.00	0.51	0.00	27.19	9.94	2.00	0.00	0.51	0.00
27.20	10.07	2.00	0.00	0.51	0.00	27.21	10.20	2.00	0.00	0.51	0.00
27.22	10.31	2.00	0.00	0.51	0.00	27.23	10.40	2.00	0.00	0.50	0.00
27.24	10.42	2.00	0.00	0.50	0.00	27.25	10.42	2.00	0.00	0.50	0.00
27.26	10.42	2.00	0.00	0.50	0.00	27.27	10.42	2.00	0.00	0.50	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
27.28	10.42	2.00	0.00	0.50	0.00	27.29	10.41	2.00	0.00	0.50	0.00
27.30	10.41	2.00	0.00	0.50	0.00	27.31	10.41	2.00	0.00	0.50	0.00
27.32	10.41	2.00	0.00	0.50	0.00	27.33	10.41	2.00	0.00	0.50	0.00
27.34	10.41	2.00	0.00	0.50	0.00	27.35	10.40	2.00	0.00	0.50	0.00
27.36	10.40	2.00	0.00	0.50	0.00	27.37	10.40	2.00	0.00	0.50	0.00
27.38	10.40	2.00	0.00	0.50	0.00	27.39	10.40	2.00	0.00	0.50	0.00
27.40	10.40	2.00	0.00	0.50	0.00	27.41	10.48	2.00	0.00	0.50	0.00
27.42	10.73	2.00	0.00	0.50	0.00	27.43	11.03	2.00	0.00	0.50	0.00
27.44	11.36	2.00	0.00	0.50	0.00	27.45	11.71	2.00	0.00	0.50	0.00
27.46	12.06	2.00	0.00	0.50	0.00	27.47	12.39	2.00	0.00	0.50	0.00
27.48	12.68	2.00	0.00	0.50	0.00	27.49	12.92	2.00	0.00	0.50	0.00
27.50	13.12	2.00	0.00	0.50	0.00	27.51	13.39	2.00	0.00	0.50	0.00
27.52	13.70	2.00	0.00	0.50	0.00	27.53	14.04	2.00	0.00	0.50	0.00
27.54	14.39	2.00	0.00	0.50	0.00	27.55	14.73	2.00	0.00	0.50	0.00
27.56	15.05	2.00	0.00	0.50	0.00	27.57	15.32	2.00	0.00	0.50	0.00
27.58	15.50	2.00	0.00	0.50	0.00	27.59	15.27	2.00	0.00	0.50	0.00
27.60	14.98	2.00	0.00	0.50	0.00	27.61	14.66	2.00	0.00	0.50	0.00
27.62	14.31	2.00	0.00	0.50	0.00	27.63	13.96	2.00	0.00	0.50	0.00
27.64	13.62	2.00	0.00	0.50	0.00	27.65	13.31	2.00	0.00	0.50	0.00
27.66	13.05	2.00	0.00	0.50	0.00	27.67	12.81	2.00	0.00	0.50	0.00
27.68	12.46	2.00	0.00	0.50	0.00	27.69	12.04	2.00	0.00	0.50	0.00
27.70	11.58	2.00	0.00	0.50	0.00	27.71	11.09	2.00	0.00	0.50	0.00
27.72	10.61	2.00	0.00	0.50	0.00	27.73	10.15	2.00	0.00	0.50	0.00
27.74	9.74	2.00	0.00	0.50	0.00	27.75	9.41	2.00	0.00	0.50	0.00
27.76	9.35	2.00	0.00	0.50	0.00	27.77	9.35	2.00	0.00	0.50	0.00
27.78	9.34	2.00	0.00	0.49	0.00	27.79	9.34	2.00	0.00	0.49	0.00
27.80	9.34	2.00	0.00	0.49	0.00	27.81	9.34	2.00	0.00	0.49	0.00
27.82	9.34	2.00	0.00	0.49	0.00	27.83	9.34	2.00	0.00	0.49	0.00
27.84	9.35	2.00	0.00	0.49	0.00	27.85	9.54	2.00	0.00	0.49	0.00
27.86	9.77	2.00	0.00	0.49	0.00	27.87	10.03	2.00	0.00	0.49	0.00
27.88	10.31	2.00	0.00	0.49	0.00	27.89	10.59	2.00	0.00	0.49	0.00
27.90	10.86	2.00	0.00	0.49	0.00	27.91	11.10	2.00	0.00	0.49	0.00
27.92	11.31	2.00	0.00	0.49	0.00	27.93	11.44	2.00	0.00	0.49	0.00
27.94	11.54	2.00	0.00	0.49	0.00	27.95	11.67	2.00	0.00	0.49	0.00
27.96	11.81	2.00	0.00	0.49	0.00	27.97	11.95	2.00	0.00	0.49	0.00
27.98	12.10	2.00	0.00	0.49	0.00	27.99	12.23	2.00	0.00	0.49	0.00
28.00	12.35	2.00	0.00	0.49	0.00	28.01	12.45	2.00	0.00	0.49	0.00
28.02	12.39	2.00	0.00	0.49	0.00	28.03	12.28	2.00	0.00	0.49	0.00
28.04	12.14	2.00	0.00	0.49	0.00	28.05	12.00	2.00	0.00	0.49	0.00
28.06	11.85	2.00	0.00	0.49	0.00	28.07	11.70	2.00	0.00	0.49	0.00
28.08	11.57	2.00	0.00	0.49	0.00	28.09	11.45	2.00	0.00	0.49	0.00
28.10	11.36	2.00	0.00	0.49	0.00	28.11	11.26	2.00	0.00	0.49	0.00
28.12	11.14	2.00	0.00	0.49	0.00	28.13	11.00	2.00	0.00	0.49	0.00
28.14	10.85	2.00	0.00	0.49	0.00	28.15	10.70	2.00	0.00	0.49	0.00
28.16	10.56	2.00	0.00	0.49	0.00	28.17	10.43	2.00	0.00	0.49	0.00
28.18	10.32	2.00	0.00	0.49	0.00	28.19	10.37	2.00	0.00	0.49	0.00
28.20	10.62	2.00	0.00	0.49	0.00	28.21	10.92	2.00	0.00	0.49	0.00
28.22	11.25	2.00	0.00	0.49	0.00	28.23	11.59	2.00	0.00	0.49	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
28.24	11.94	2.00	0.00	0.49	0.00	28.25	12.26	2.00	0.00	0.49	0.00
28.26	12.55	2.00	0.00	0.49	0.00	28.27	12.78	2.00	0.00	0.49	0.00
28.28	12.81	2.00	0.00	0.49	0.00	28.29	12.81	2.00	0.00	0.49	0.00
28.30	12.81	2.00	0.00	0.49	0.00	28.31	12.81	2.00	0.00	0.49	0.00
28.32	12.80	2.00	0.00	0.49	0.00	28.33	12.80	2.00	0.00	0.48	0.00
28.34	12.80	2.00	0.00	0.48	0.00	28.35	12.80	2.00	0.00	0.48	0.00
28.36	12.76	2.00	0.00	0.48	0.00	28.37	12.45	2.00	0.00	0.48	0.00
28.38	12.08	2.00	0.00	0.48	0.00	28.39	11.65	2.00	0.00	0.48	0.00
28.40	11.20	2.00	0.00	0.48	0.00	28.41	10.74	2.00	0.00	0.48	0.00
28.42	10.31	2.00	0.00	0.48	0.00	28.43	9.91	2.00	0.00	0.48	0.00
28.44	9.58	2.00	0.00	0.48	0.00	28.45	9.41	2.00	0.00	0.48	0.00
28.46	9.34	2.00	0.00	0.48	0.00	28.47	9.24	2.00	0.00	0.48	0.00
28.48	9.14	2.00	0.00	0.48	0.00	28.49	9.03	2.00	0.00	0.48	0.00
28.50	8.92	2.00	0.00	0.48	0.00	28.51	8.82	2.00	0.00	0.48	0.00
28.52	8.73	2.00	0.00	0.48	0.00	28.53	8.66	2.00	0.00	0.48	0.00
28.54	8.65	2.00	0.00	0.48	0.00	28.55	8.65	2.00	0.00	0.48	0.00
28.56	8.65	2.00	0.00	0.48	0.00	28.57	8.65	2.00	0.00	0.48	0.00
28.58	8.64	2.00	0.00	0.48	0.00	28.59	8.64	2.00	0.00	0.48	0.00
28.60	8.64	2.00	0.00	0.48	0.00	28.61	8.64	2.00	0.00	0.48	0.00
28.62	8.63	2.00	0.00	0.48	0.00	28.63	8.56	2.00	0.00	0.48	0.00
28.64	8.47	2.00	0.00	0.48	0.00	28.65	8.37	2.00	0.00	0.48	0.00
28.66	8.26	2.00	0.00	0.48	0.00	28.67	8.15	2.00	0.00	0.48	0.00
28.68	8.05	2.00	0.00	0.48	0.00	28.69	7.96	2.00	0.00	0.48	0.00
28.70	7.88	2.00	0.00	0.48	0.00	28.71	7.89	2.00	0.00	0.48	0.00
28.72	7.98	2.00	0.00	0.48	0.00	28.73	8.10	2.00	0.00	0.48	0.00
28.74	8.22	2.00	0.00	0.48	0.00	28.75	8.36	2.00	0.00	0.48	0.00
28.76	8.49	2.00	0.00	0.48	0.00	28.77	8.61	2.00	0.00	0.48	0.00
28.78	8.72	2.00	0.00	0.48	0.00	28.79	8.80	2.00	0.00	0.48	0.00
28.80	8.99	2.00	0.00	0.48	0.00	28.81	9.23	2.00	0.00	0.48	0.00
28.82	9.52	2.00	0.00	0.48	0.00	28.83	9.83	2.00	0.00	0.48	0.00
28.84	10.15	2.00	0.00	0.48	0.00	28.85	10.46	2.00	0.00	0.48	0.00
28.86	10.74	2.00	0.00	0.48	0.00	28.87	10.99	2.00	0.00	0.48	0.00
28.88	11.17	2.00	0.00	0.47	0.00	28.89	11.33	2.00	0.00	0.47	0.00
28.90	11.53	2.00	0.00	0.47	0.00	28.91	11.75	2.00	0.00	0.47	0.00
28.92	11.98	2.00	0.00	0.47	0.00	28.93	12.22	2.00	0.00	0.47	0.00
28.94	12.45	2.00	0.00	0.47	0.00	28.95	12.65	2.00	0.00	0.47	0.00
28.96	12.82	2.00	0.00	0.47	0.00	28.97	13.01	2.00	0.00	0.47	0.00
28.98	13.30	2.00	0.00	0.47	0.00	28.99	13.64	2.00	0.00	0.47	0.00
29.00	14.02	2.00	0.00	0.47	0.00	29.01	14.42	2.00	0.00	0.47	0.00
29.02	14.81	2.00	0.00	0.47	0.00	29.03	15.17	2.00	0.00	0.47	0.00
29.04	15.49	2.00	0.00	0.47	0.00	29.05	15.75	2.00	0.00	0.47	0.00
29.06	16.04	2.00	0.00	0.47	0.00	29.07	16.41	2.00	0.00	0.47	0.00
29.08	16.84	2.00	0.00	0.47	0.00	29.09	17.30	2.00	0.00	0.47	0.00
29.10	17.78	2.00	0.00	0.47	0.00	29.11	18.24	2.00	0.00	0.47	0.00
29.12	18.66	2.00	0.00	0.47	0.00	29.13	19.02	2.00	0.00	0.47	0.00
29.14	19.27	2.00	0.00	0.47	0.00	29.15	19.43	2.00	0.00	0.47	0.00
29.16	19.63	2.00	0.00	0.47	0.00	29.17	19.85	2.00	0.00	0.47	0.00
29.18	20.08	2.00	0.00	0.47	0.00	29.19	20.31	2.00	0.00	0.47	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
29.20	20.54	2.00	0.00	0.47	0.00	29.21	20.74	2.00	0.00	0.47	0.00
29.22	20.90	2.00	0.00	0.47	0.00	29.23	20.93	2.00	0.00	0.47	0.00
29.24	20.87	2.00	0.00	0.47	0.00	29.25	20.80	2.00	0.00	0.47	0.00
29.26	20.72	2.00	0.00	0.47	0.00	29.27	20.64	2.00	0.00	0.47	0.00
29.28	20.56	2.00	0.00	0.47	0.00	29.29	20.48	2.00	0.00	0.47	0.00
29.30	20.41	2.00	0.00	0.47	0.00	29.31	20.36	2.00	0.00	0.47	0.00
29.32	20.40	2.00	0.00	0.47	0.00	29.33	20.46	2.00	0.00	0.47	0.00
29.34	20.52	2.00	0.00	0.47	0.00	29.35	20.60	2.00	0.00	0.47	0.00
29.36	20.67	2.00	0.00	0.47	0.00	29.37	20.75	2.00	0.00	0.47	0.00
29.38	20.82	2.00	0.00	0.47	0.00	29.39	20.87	2.00	0.00	0.47	0.00
29.40	20.97	2.00	0.00	0.47	0.00	29.41	21.29	2.00	0.00	0.47	0.00
29.42	21.68	2.00	0.00	0.47	0.00	29.43	22.12	2.00	0.00	0.46	0.00
29.44	22.59	2.00	0.00	0.46	0.00	29.45	23.06	2.00	0.00	0.46	0.00
29.46	23.50	2.00	0.00	0.46	0.00	29.47	23.90	2.00	0.00	0.46	0.00
29.48	24.24	2.00	0.00	0.46	0.00	29.49	24.51	2.00	0.00	0.46	0.00
29.50	24.86	2.00	0.00	0.46	0.00	29.51	25.27	2.00	0.00	0.46	0.00
29.52	25.72	2.00	0.00	0.46	0.00	29.53	26.19	2.00	0.00	0.46	0.00
29.54	26.65	2.00	0.00	0.46	0.00	29.55	27.08	2.00	0.00	0.46	0.00
29.56	27.46	2.00	0.00	0.46	0.00	29.57	27.76	2.00	0.00	0.46	0.00
29.58	27.86	2.00	0.00	0.46	0.00	29.59	27.99	2.00	0.00	0.46	0.00
29.60	28.12	2.00	0.00	0.46	0.00	29.61	28.27	2.00	0.00	0.46	0.00
29.62	28.43	2.00	0.00	0.46	0.00	29.63	28.57	2.00	0.00	0.46	0.00
29.64	28.71	2.00	0.00	0.46	0.00	29.65	28.83	2.00	0.00	0.46	0.00
29.66	28.85	2.00	0.00	0.46	0.00	29.67	28.69	2.00	0.00	0.46	0.00
29.68	28.49	2.00	0.00	0.46	0.00	29.69	28.26	2.00	0.00	0.46	0.00
29.70	28.02	2.00	0.00	0.46	0.00	29.71	27.79	2.00	0.00	0.46	0.00
29.72	27.56	2.00	0.00	0.46	0.00	29.73	27.35	2.00	0.00	0.46	0.00
29.74	27.18	2.00	0.00	0.46	0.00	29.75	26.95	2.00	0.00	0.46	0.00
29.76	26.60	2.00	0.00	0.46	0.00	29.77	26.18	2.00	0.00	0.46	0.00
29.78	25.72	2.00	0.00	0.46	0.00	29.79	25.25	2.00	0.00	0.46	0.00
29.80	24.78	2.00	0.00	0.46	0.00	29.81	24.35	2.00	0.00	0.46	0.00
29.82	23.96	2.00	0.00	0.46	0.00	29.83	23.66	2.00	0.00	0.46	0.00
29.84	23.83	2.00	0.00	0.46	0.00	29.85	24.08	2.00	0.00	0.46	0.00
29.86	24.36	2.00	0.00	0.46	0.00	29.87	24.66	2.00	0.00	0.46	0.00
29.88	24.97	2.00	0.00	0.46	0.00	29.89	25.27	2.00	0.00	0.46	0.00
29.90	25.54	2.00	0.00	0.46	0.00	29.91	25.78	2.00	0.00	0.46	0.00
29.92	26.00	2.00	0.00	0.46	0.00	29.93	26.37	2.00	0.00	0.46	0.00
29.94	26.83	2.00	0.00	0.46	0.00	29.95	27.34	2.00	0.00	0.46	0.00
29.96	27.88	2.00	0.00	0.46	0.00	29.97	28.42	2.00	0.00	0.46	0.00
29.98	28.94	2.00	0.00	0.45	0.00	29.99	29.40	2.00	0.00	0.45	0.00
30.00	29.78	2.00	0.00	0.45	0.00	30.01	29.83	2.00	0.00	0.45	0.00
30.02	29.70	2.00	0.00	0.45	0.00	30.03	29.56	2.00	0.00	0.45	0.00
30.04	29.41	2.00	0.00	0.45	0.00	30.05	29.25	2.00	0.00	0.45	0.00
30.06	29.09	2.00	0.00	0.45	0.00	30.07	28.94	2.00	0.00	0.45	0.00
30.08	28.81	2.00	0.00	0.45	0.00	30.09	28.71	2.00	0.00	0.45	0.00
30.10	28.75	2.00	0.00	0.45	0.00	30.11	28.81	2.00	0.00	0.45	0.00
30.12	28.87	2.00	0.00	0.45	0.00	30.13	28.95	2.00	0.00	0.45	0.00
30.14	29.02	2.00	0.00	0.45	0.00	30.15	29.09	2.00	0.00	0.45	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
30.16	29.15	2.00	0.00	0.45	0.00	30.17	29.21	2.00	0.00	0.45	0.00
30.18	29.32	2.00	0.00	0.45	0.00	30.19	29.64	2.00	0.00	0.45	0.00
30.20	30.03	2.00	0.00	0.45	0.00	30.21	30.47	2.00	0.00	0.45	0.00
30.22	30.93	2.00	0.00	0.45	0.00	30.23	31.39	2.00	0.00	0.45	0.00
30.24	31.82	2.00	0.00	0.45	0.00	30.25	32.22	2.00	0.00	0.45	0.00
30.26	32.54	2.00	0.00	0.45	0.00	30.27	32.72	2.00	0.00	0.45	0.00
30.28	32.89	2.00	0.00	0.45	0.00	30.29	33.09	2.00	0.00	0.45	0.00
30.30	33.31	2.00	0.00	0.45	0.00	30.31	33.54	2.00	0.00	0.45	0.00
30.32	33.76	2.00	0.00	0.45	0.00	30.33	33.97	2.00	0.00	0.45	0.00
30.34	34.15	2.00	0.00	0.45	0.00	30.35	34.29	2.00	0.00	0.45	0.00
30.36	34.19	2.00	0.00	0.45	0.00	30.37	34.06	2.00	0.00	0.45	0.00
30.38	33.91	2.00	0.00	0.45	0.00	30.39	33.76	2.00	0.00	0.45	0.00
30.40	33.60	2.00	0.00	0.45	0.00	30.41	33.44	2.00	0.00	0.45	0.00
30.42	33.30	2.00	0.00	0.45	0.00	30.43	33.18	2.00	0.00	0.45	0.00
30.44	33.06	2.00	0.00	0.45	0.00	30.45	32.90	2.00	0.00	0.45	0.00
30.46	32.69	2.00	0.00	0.45	0.00	30.47	32.47	2.00	0.00	0.45	0.00
30.48	32.23	2.00	0.00	0.45	0.00	30.49	32.00	2.00	0.00	0.45	0.00
30.50	31.77	2.00	0.00	0.45	0.00	30.51	31.57	2.00	0.00	0.45	0.00
30.52	31.40	2.00	0.00	0.45	0.00	30.53	31.61	2.00	0.00	0.44	0.00
30.54	32.08	2.00	0.00	0.44	0.00	30.55	32.62	2.00	0.00	0.44	0.00
30.56	33.22	2.00	0.00	0.44	0.00	30.57	33.83	2.00	0.00	0.44	0.00
30.58	34.44	2.00	0.00	0.44	0.00	30.59	35.00	2.00	0.00	0.44	0.00
30.60	35.49	2.00	0.00	0.44	0.00	30.61	35.89	2.00	0.00	0.44	0.00
30.62	36.87	2.00	0.00	0.44	0.00	30.63	38.11	2.00	0.00	0.44	0.00
30.64	39.53	2.00	0.00	0.44	0.00	30.65	41.05	2.00	0.00	0.44	0.00
30.66	42.59	2.00	0.00	0.44	0.00	30.67	44.08	2.00	0.00	0.44	0.00
30.68	45.44	2.00	0.00	0.44	0.00	30.69	46.59	2.00	0.00	0.44	0.00
30.70	47.56	2.00	0.00	0.44	0.00	30.71	48.86	2.00	0.00	0.44	0.00
30.72	115.73	2.00	0.00	0.44	0.00	30.73	117.69	2.00	0.00	0.44	0.00
30.74	119.72	2.00	0.00	0.44	0.00	30.75	121.73	2.00	0.00	0.44	0.00
30.76	123.63	2.00	0.00	0.44	0.00	30.77	125.30	2.00	0.00	0.44	0.00
30.78	126.64	2.00	0.00	0.44	0.00	30.79	127.76	2.00	0.00	0.44	0.00
30.80	129.23	2.00	0.00	0.44	0.00	30.81	130.93	2.00	0.00	0.44	0.00
30.82	132.75	2.00	0.00	0.44	0.00	30.83	134.61	2.00	0.00	0.44	0.00
30.84	136.39	2.00	0.00	0.44	0.00	30.85	138.01	2.00	0.00	0.44	0.00
30.86	139.40	2.00	0.00	0.44	0.00	30.87	140.48	2.00	0.00	0.44	0.00
30.88	141.07	2.00	0.00	0.44	0.00	30.89	141.93	2.00	0.00	0.44	0.00
30.90	142.90	2.00	0.00	0.44	0.00	30.91	143.93	2.00	0.00	0.44	0.00
30.92	144.96	2.00	0.00	0.44	0.00	30.93	145.95	2.00	0.00	0.44	0.00
30.94	146.84	2.00	0.00	0.44	0.00	30.95	147.61	2.00	0.00	0.44	0.00
30.96	148.05	0.30	0.92	0.44	0.00	30.97	148.21	0.31	0.92	0.44	0.00
30.98	148.46	0.31	0.92	0.44	0.00	30.99	148.74	0.31	0.91	0.44	0.00
31.00	149.03	0.31	0.91	0.44	0.00	31.01	149.32	0.31	0.91	0.44	0.00
31.02	149.59	0.32	0.91	0.44	0.00	31.03	149.84	0.32	0.91	0.44	0.00
31.04	150.04	0.32	0.90	0.44	0.00	31.05	150.09	0.32	0.90	0.44	0.00
31.06	150.10	0.32	0.90	0.44	0.00	31.07	150.11	0.32	0.90	0.44	0.00
31.08	150.12	0.32	0.90	0.43	0.00	31.09	150.13	0.32	0.90	0.43	0.00
31.10	150.14	0.32	0.90	0.43	0.00	31.11	150.14	0.32	0.90	0.43	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
31.12	150.14	0.32	0.90	0.43	0.00	31.13	150.14	0.32	0.90	0.43	0.00
31.14	150.31	0.32	0.90	0.43	0.00	31.15	150.50	0.32	0.90	0.43	0.00
31.16	150.71	0.32	0.89	0.43	0.00	31.17	150.94	0.33	0.89	0.43	0.00
31.18	151.18	0.33	0.89	0.43	0.00	31.19	151.40	0.33	0.89	0.43	0.00
31.20	151.61	0.33	0.89	0.43	0.00	31.21	151.77	0.33	0.89	0.43	0.00
31.22	151.95	0.33	0.88	0.43	0.00	31.23	152.28	0.34	0.88	0.43	0.00
31.24	152.66	0.34	0.88	0.43	0.00	31.25	153.08	0.34	0.88	0.43	0.00
31.26	153.53	0.35	0.87	0.43	0.00	31.27	153.97	0.35	0.87	0.43	0.00
31.28	154.39	0.35	0.87	0.43	0.00	31.29	154.76	0.36	0.86	0.43	0.00
31.30	155.05	0.36	0.86	0.43	0.00	31.31	155.37	0.36	0.86	0.43	0.00
31.32	155.80	0.37	0.86	0.43	0.00	31.33	156.31	0.37	0.84	0.43	0.00
31.34	156.85	0.38	0.83	0.43	0.00	31.35	157.41	0.38	0.81	0.43	0.00
31.36	157.96	0.39	0.80	0.43	0.00	31.37	158.46	0.39	0.78	0.43	0.00
31.38	158.90	0.40	0.77	0.43	0.00	31.39	159.23	0.40	0.76	0.43	0.00
31.40	159.91	0.41	0.74	0.43	0.00	31.41	160.75	0.42	0.72	0.43	0.00
31.42	161.70	0.43	0.70	0.43	0.00	31.43	162.71	0.45	0.67	0.43	0.00
31.44	163.73	0.46	0.65	0.43	0.00	31.45	164.70	0.47	0.63	0.43	0.00
31.46	165.58	0.49	0.61	0.43	0.00	31.47	166.31	0.50	0.59	0.43	0.00
31.48	166.91	0.51	0.58	0.43	0.00	31.49	167.73	0.52	0.57	0.43	0.00
31.50	168.71	0.54	0.55	0.43	0.00	31.51	169.79	0.56	0.53	0.43	0.00
31.52	170.92	0.58	0.51	0.43	0.00	31.53	172.04	0.60	0.49	0.43	0.00
31.54	173.09	0.63	0.47	0.43	0.00	31.55	174.01	0.65	0.45	0.43	0.00
31.56	174.74	0.67	0.44	0.43	0.00	31.57	175.36	0.68	0.43	0.43	0.00
31.58	176.18	0.70	0.42	0.43	0.00	31.59	177.13	0.73	0.40	0.43	0.00
31.60	178.16	0.76	0.39	0.43	0.00	31.61	179.20	0.79	0.38	0.43	0.00
31.62	180.21	0.82	0.36	0.43	0.00	31.63	181.14	0.86	0.35	0.42	0.00
31.64	181.93	0.88	0.34	0.42	0.00	31.65	182.50	0.91	0.33	0.42	0.00
31.66	183.00	0.93	0.33	0.42	0.00	31.67	183.65	0.95	0.32	0.42	0.00
31.68	184.38	0.98	0.31	0.42	0.00	31.69	185.14	1.02	0.29	0.42	0.00
31.70	185.89	1.05	0.27	0.42	0.00	31.71	186.60	1.09	0.25	0.42	0.00
31.72	187.23	1.12	0.24	0.42	0.00	31.73	187.76	1.14	0.23	0.42	0.00
31.74	188.06	1.16	0.22	0.42	0.00	31.75	188.34	1.18	0.21	0.42	0.00
31.76	188.72	1.20	0.20	0.42	0.00	31.77	189.13	1.22	0.20	0.42	0.00
31.78	189.55	1.24	0.19	0.42	0.00	31.79	189.96	1.27	0.18	0.42	0.00
31.80	190.35	1.29	0.17	0.42	0.00	31.81	190.68	1.31	0.16	0.42	0.00
31.82	190.97	1.33	0.15	0.42	0.00	31.83	191.13	1.34	0.15	0.42	0.00
31.84	191.37	1.36	0.15	0.42	0.00	31.85	191.67	1.38	0.14	0.42	0.00
31.86	191.99	1.40	0.13	0.42	0.00	31.87	192.31	1.42	0.13	0.42	0.00
31.88	192.63	1.44	0.12	0.42	0.00	31.89	192.93	1.46	0.11	0.42	0.00
31.90	193.19	1.48	0.11	0.42	0.00	31.91	193.38	1.50	0.10	0.42	0.00
31.92	193.37	1.50	0.10	0.42	0.00	31.93	193.39	1.50	0.10	0.42	0.00
31.94	193.42	1.50	0.10	0.42	0.00	31.95	193.46	1.50	0.10	0.42	0.00
31.96	193.49	1.51	0.10	0.42	0.00	31.97	193.52	1.51	0.10	0.42	0.00
31.98	193.55	1.51	0.10	0.42	0.00	31.99	193.58	1.51	0.10	0.42	0.00
32.00	193.59	1.51	0.10	0.42	0.00	32.01	193.55	1.51	0.10	0.42	0.00
32.02	193.51	1.51	0.10	0.42	0.00	32.03	193.48	1.50	0.10	0.42	0.00
32.04	193.44	1.50	0.10	0.42	0.00	32.05	193.39	1.50	0.10	0.42	0.00
32.06	193.35	1.49	0.10	0.42	0.00	32.07	193.31	1.49	0.10	0.42	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
32.08	193.28	1.49	0.11	0.42	0.00	32.09	193.26	1.49	0.11	0.42	0.00
32.10	193.22	1.48	0.11	0.42	0.00	32.11	193.18	1.48	0.11	0.42	0.00
32.12	193.13	1.48	0.11	0.42	0.00	32.13	193.07	1.47	0.11	0.42	0.00
32.14	193.02	1.47	0.11	0.42	0.00	32.15	192.97	1.46	0.11	0.42	0.00
32.16	192.92	1.46	0.11	0.42	0.00	32.17	192.89	1.46	0.11	0.42	0.00
32.18	192.86	1.46	0.11	0.41	0.00	32.19	192.80	1.45	0.11	0.41	0.00
32.20	192.75	1.45	0.12	0.41	0.00	32.21	192.68	1.44	0.12	0.41	0.00
32.22	192.62	1.44	0.12	0.41	0.00	32.23	192.56	1.43	0.12	0.41	0.00
32.24	192.50	1.43	0.12	0.41	0.00	32.25	192.44	1.43	0.12	0.41	0.00
32.26	192.42	1.42	0.12	0.41	0.00	32.27	192.41	1.42	0.12	0.41	0.00
32.28	192.38	1.42	0.12	0.41	0.00	32.29	192.36	1.42	0.12	0.41	0.00
32.30	192.34	1.42	0.12	0.41	0.00	32.31	192.31	1.42	0.12	0.41	0.00
32.32	192.28	1.41	0.13	0.41	0.00	32.33	192.26	1.41	0.13	0.41	0.00
32.34	192.24	1.41	0.13	0.41	0.00	32.35	192.27	1.41	0.13	0.41	0.00
32.36	192.31	1.42	0.12	0.41	0.00	32.37	192.35	1.42	0.12	0.41	0.00
32.38	192.40	1.42	0.12	0.41	0.00	32.39	192.46	1.43	0.12	0.41	0.00
32.40	192.50	1.43	0.12	0.41	0.00	32.41	192.55	1.43	0.12	0.41	0.00
32.42	192.59	1.43	0.12	0.41	0.00	32.43	192.62	1.44	0.12	0.41	0.00
32.44	192.65	1.44	0.12	0.41	0.00	32.45	192.69	1.44	0.12	0.41	0.00
32.46	192.73	1.45	0.12	0.41	0.00	32.47	192.78	1.45	0.11	0.41	0.00
32.48	192.83	1.45	0.11	0.41	0.00	32.49	192.88	1.46	0.11	0.41	0.00
32.50	192.92	1.46	0.11	0.41	0.00	32.51	192.95	1.46	0.11	0.41	0.00
32.52	193.00	1.46	0.11	0.41	0.00	32.53	193.09	1.47	0.11	0.41	0.00
32.54	193.20	1.48	0.11	0.41	0.00	32.55	193.32	1.49	0.10	0.41	0.00
32.56	193.45	1.50	0.10	0.41	0.00	32.57	193.58	1.51	0.10	0.41	0.00
32.58	193.69	1.52	0.10	0.41	0.00	32.59	193.80	1.52	0.09	0.41	0.00
32.60	193.84	1.53	0.09	0.41	0.00	32.61	194.61	1.59	0.08	0.41	0.00
32.62	195.70	1.68	0.06	0.41	0.00	32.63	196.95	1.79	0.04	0.41	0.00
32.64	198.30	1.93	0.01	0.41	0.00	32.65	199.68	2.00	0.00	0.41	0.00
32.66	201.03	2.00	0.00	0.41	0.00	32.67	202.27	2.00	0.00	0.41	0.00
32.68	203.33	2.00	0.00	0.41	0.00	32.69	204.14	2.00	0.00	0.41	0.00
32.70	204.99	2.00	0.00	0.41	0.00	32.71	206.05	2.00	0.00	0.41	0.00
32.72	207.25	2.00	0.00	0.41	0.00	32.73	208.51	2.00	0.00	0.40	0.00
32.74	209.79	2.00	0.00	0.40	0.00	32.75	211.01	2.00	0.00	0.40	0.00
32.76	212.11	2.00	0.00	0.40	0.00	32.77	213.04	2.00	0.00	0.40	0.00
32.78	213.46	2.00	0.00	0.40	0.00	32.79	213.63	2.00	0.00	0.40	0.00
32.80	213.85	2.00	0.00	0.40	0.00	32.81	214.10	2.00	0.00	0.40	0.00
32.82	214.36	2.00	0.00	0.40	0.00	32.83	214.62	2.00	0.00	0.40	0.00
32.84	214.86	2.00	0.00	0.40	0.00	32.85	215.07	2.00	0.00	0.40	0.00
32.86	215.22	2.00	0.00	0.40	0.00	32.87	215.52	2.00	0.00	0.40	0.00
32.88	215.91	2.00	0.00	0.40	0.00	32.89	216.35	2.00	0.00	0.40	0.00
32.90	216.83	2.00	0.00	0.40	0.00	32.91	217.32	2.00	0.00	0.40	0.00
32.92	217.80	2.00	0.00	0.40	0.00	32.93	218.24	2.00	0.00	0.40	0.00
32.94	218.61	2.00	0.00	0.40	0.00	32.95	218.89	2.00	0.00	0.40	0.00
32.96	219.27	2.00	0.00	0.40	0.00	32.97	219.73	2.00	0.00	0.40	0.00
32.98	220.24	2.00	0.00	0.40	0.00	32.99	220.78	2.00	0.00	0.40	0.00
33.00	221.33	2.00	0.00	0.40	0.00	33.01	221.84	2.00	0.00	0.40	0.00
33.02	222.31	2.00	0.00	0.40	0.00	33.03	222.68	2.00	0.00	0.40	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
33.04	222.96	2.00	0.00	0.40	0.00	33.05	223.32	2.00	0.00	0.40	0.00
33.06	223.74	2.00	0.00	0.40	0.00	33.07	224.21	2.00	0.00	0.40	0.00
33.08	224.68	2.00	0.00	0.40	0.00	33.09	225.15	2.00	0.00	0.40	0.00
33.10	225.59	2.00	0.00	0.40	0.00	33.11	225.97	2.00	0.00	0.40	0.00
33.12	226.25	2.00	0.00	0.40	0.00	33.13	226.59	2.00	0.00	0.40	0.00
33.14	227.05	2.00	0.00	0.40	0.00	33.15	227.58	2.00	0.00	0.40	0.00
33.16	228.14	2.00	0.00	0.40	0.00	33.17	228.71	2.00	0.00	0.40	0.00
33.18	229.26	2.00	0.00	0.40	0.00	33.19	229.76	2.00	0.00	0.40	0.00
33.20	230.19	2.00	0.00	0.40	0.00	33.21	230.47	2.00	0.00	0.40	0.00
33.22	230.75	2.00	0.00	0.40	0.00	33.23	231.10	2.00	0.00	0.40	0.00
33.24	231.49	2.00	0.00	0.40	0.00	33.25	231.90	2.00	0.00	0.40	0.00
33.26	232.31	2.00	0.00	0.40	0.00	33.27	232.69	2.00	0.00	0.40	0.00
33.28	233.03	2.00	0.00	0.39	0.00	33.29	233.32	2.00	0.00	0.39	0.00
33.30	233.35	2.00	0.00	0.39	0.00	33.31	233.26	2.00	0.00	0.39	0.00
33.32	233.18	2.00	0.00	0.39	0.00	33.33	233.09	2.00	0.00	0.39	0.00
33.34	232.99	2.00	0.00	0.39	0.00	33.35	232.90	2.00	0.00	0.39	0.00
33.36	232.81	2.00	0.00	0.39	0.00	33.37	232.72	2.00	0.00	0.39	0.00
33.38	232.69	2.00	0.00	0.39	0.00	33.39	232.38	2.00	0.00	0.39	0.00
33.40	232.03	2.00	0.00	0.39	0.00	33.41	231.62	2.00	0.00	0.39	0.00
33.42	231.19	2.00	0.00	0.39	0.00	33.43	230.75	2.00	0.00	0.39	0.00
33.44	230.32	2.00	0.00	0.39	0.00	33.45	229.93	2.00	0.00	0.39	0.00
33.46	229.60	2.00	0.00	0.39	0.00	33.47	229.30	2.00	0.00	0.39	0.00
33.48	228.76	2.00	0.00	0.39	0.00	33.49	228.12	2.00	0.00	0.39	0.00
33.50	227.40	2.00	0.00	0.39	0.00	33.51	226.65	2.00	0.00	0.39	0.00
33.52	225.89	2.00	0.00	0.39	0.00	33.53	225.16	2.00	0.00	0.39	0.00
33.54	224.51	2.00	0.00	0.39	0.00	33.55	224.00	2.00	0.00	0.39	0.00
33.56	223.50	2.00	0.00	0.39	0.00	33.57	222.80	2.00	0.00	0.39	0.00
33.58	221.99	2.00	0.00	0.39	0.00	33.59	221.09	2.00	0.00	0.39	0.00
33.60	220.15	2.00	0.00	0.39	0.00	33.61	219.22	2.00	0.00	0.39	0.00
33.62	218.35	2.00	0.00	0.39	0.00	33.63	217.57	2.00	0.00	0.39	0.00
33.64	216.99	2.00	0.00	0.39	0.00	33.65	216.40	2.00	0.00	0.39	0.00
33.66	215.63	2.00	0.00	0.39	0.00	33.67	214.74	2.00	0.00	0.39	0.00
33.68	213.78	2.00	0.00	0.39	0.00	33.69	212.79	2.00	0.00	0.39	0.00
33.70	211.82	2.00	0.00	0.39	0.00	33.71	210.93	2.00	0.00	0.39	0.00
33.72	210.15	2.00	0.00	0.39	0.00	33.73	209.58	2.00	0.00	0.39	0.00
33.74	208.92	2.00	0.00	0.39	0.00	33.75	208.08	2.00	0.00	0.39	0.00
33.76	207.15	2.00	0.00	0.39	0.00	33.77	206.16	2.00	0.00	0.39	0.00
33.78	205.16	2.00	0.00	0.39	0.00	33.79	204.20	2.00	0.00	0.39	0.00
33.80	203.33	2.00	0.00	0.39	0.00	33.81	202.62	2.00	0.00	0.39	0.00
33.82	202.07	2.00	0.00	0.39	0.00	33.83	201.36	2.00	0.00	0.38	0.00
33.84	200.53	2.00	0.00	0.38	0.00	33.85	199.60	2.00	0.00	0.38	0.00
33.86	198.65	1.95	0.01	0.38	0.00	33.87	197.70	1.85	0.02	0.38	0.00
33.88	196.81	1.77	0.04	0.38	0.00	33.89	196.02	1.70	0.05	0.38	0.00
33.90	195.37	1.64	0.06	0.38	0.00	33.91	195.37	1.64	0.06	0.38	0.00
33.92	195.34	1.64	0.06	0.38	0.00	33.93	195.29	1.63	0.06	0.38	0.00
33.94	195.25	1.63	0.07	0.38	0.00	33.95	195.20	1.62	0.07	0.38	0.00
33.96	195.15	1.62	0.07	0.38	0.00	33.97	195.11	1.62	0.07	0.38	0.00
33.98	195.07	1.61	0.07	0.38	0.00	33.99	195.05	1.61	0.07	0.38	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
34.00	195.03	1.61	0.07	0.38	0.00	34.01	195.01	1.61	0.07	0.38	0.00
34.02	194.98	1.60	0.07	0.38	0.00	34.03	194.96	1.60	0.07	0.38	0.00
34.04	194.93	1.60	0.07	0.38	0.00	34.05	194.91	1.60	0.07	0.38	0.00
34.06	194.88	1.60	0.07	0.38	0.00	34.07	194.87	1.59	0.07	0.38	0.00
34.08	194.69	1.58	0.07	0.38	0.00	34.09	194.36	1.55	0.08	0.38	0.00
34.10	193.97	1.52	0.09	0.38	0.00	34.11	193.54	1.49	0.10	0.38	0.00
34.12	193.10	1.46	0.10	0.38	0.00	34.13	192.67	1.43	0.11	0.38	0.00
34.14	192.26	1.40	0.12	0.38	0.00	34.15	191.90	1.37	0.13	0.38	0.00
34.16	191.61	1.35	0.13	0.38	0.00	34.17	191.70	1.36	0.13	0.38	0.00
34.18	191.78	1.37	0.13	0.38	0.00	34.19	191.89	1.37	0.13	0.38	0.00
34.20	192.00	1.38	0.12	0.38	0.00	34.21	192.11	1.39	0.12	0.38	0.00
34.22	192.22	1.39	0.12	0.38	0.00	34.23	192.32	1.40	0.12	0.38	0.00
34.24	192.40	1.41	0.12	0.38	0.00	34.25	192.53	1.42	0.11	0.38	0.00
34.26	192.84	1.44	0.11	0.38	0.00	34.27	193.22	1.47	0.10	0.38	0.00
34.28	193.64	1.50	0.09	0.38	0.00	34.29	194.09	1.53	0.09	0.38	0.00
34.30	194.54	1.57	0.08	0.38	0.00	34.31	194.96	1.60	0.07	0.38	0.00
34.32	195.34	1.63	0.06	0.38	0.00	34.33	195.63	1.66	0.06	0.38	0.00
34.34	196.04	1.69	0.05	0.38	0.00	34.35	196.65	1.75	0.04	0.38	0.00
34.36	197.37	1.82	0.03	0.38	0.00	34.37	198.15	1.89	0.02	0.38	0.00
34.38	198.95	1.98	0.00	0.37	0.00	34.39	199.74	2.00	0.00	0.37	0.00
34.40	200.48	2.00	0.00	0.37	0.00	34.41	201.12	2.00	0.00	0.37	0.00
34.42	201.60	2.00	0.00	0.37	0.00	34.43	202.19	2.00	0.00	0.37	0.00
34.44	202.93	2.00	0.00	0.37	0.00	34.45	203.78	2.00	0.00	0.37	0.00
34.46	204.68	2.00	0.00	0.37	0.00	34.47	205.60	2.00	0.00	0.37	0.00
34.48	206.48	2.00	0.00	0.37	0.00	34.49	207.28	2.00	0.00	0.37	0.00
34.50	207.95	2.00	0.00	0.37	0.00	34.51	208.46	2.00	0.00	0.37	0.00
34.52	209.15	2.00	0.00	0.37	0.00	34.53	209.96	2.00	0.00	0.37	0.00
34.54	210.87	2.00	0.00	0.37	0.00	34.55	211.81	2.00	0.00	0.37	0.00
34.56	212.74	2.00	0.00	0.37	0.00	34.57	213.62	2.00	0.00	0.37	0.00
34.58	214.39	2.00	0.00	0.37	0.00	34.59	214.98	2.00	0.00	0.37	0.00
34.60	215.55	2.00	0.00	0.37	0.00	34.61	216.34	2.00	0.00	0.37	0.00
34.62	217.26	2.00	0.00	0.37	0.00	34.63	218.23	2.00	0.00	0.37	0.00
34.64	219.22	2.00	0.00	0.37	0.00	34.65	220.17	2.00	0.00	0.37	0.00
34.66	221.04	2.00	0.00	0.37	0.00	34.67	221.77	2.00	0.00	0.37	0.00
34.68	222.27	2.00	0.00	0.37	0.00	34.69	222.60	2.00	0.00	0.37	0.00
34.70	223.05	2.00	0.00	0.37	0.00	34.71	223.53	2.00	0.00	0.37	0.00
34.72	224.01	2.00	0.00	0.37	0.00	34.73	224.46	2.00	0.00	0.37	0.00
34.74	224.86	2.00	0.00	0.37	0.00	34.75	225.20	2.00	0.00	0.37	0.00
34.76	225.46	2.00	0.00	0.37	0.00	34.77	225.50	2.00	0.00	0.37	0.00
34.78	225.50	2.00	0.00	0.37	0.00	34.79	225.53	2.00	0.00	0.37	0.00
34.80	225.52	2.00	0.00	0.37	0.00	34.81	225.47	2.00	0.00	0.37	0.00
34.82	225.39	2.00	0.00	0.37	0.00	34.83	225.27	2.00	0.00	0.37	0.00
34.84	225.13	2.00	0.00	0.37	0.00	34.85	225.00	2.00	0.00	0.37	0.00
34.86	224.72	2.00	0.00	0.37	0.00	34.87	224.49	2.00	0.00	0.37	0.00
34.88	224.22	2.00	0.00	0.37	0.00	34.89	223.90	2.00	0.00	0.37	0.00
34.90	223.54	2.00	0.00	0.37	0.00	34.91	223.16	2.00	0.00	0.37	0.00
34.92	222.79	2.00	0.00	0.37	0.00	34.93	222.44	2.00	0.00	0.36	0.00
34.94	222.13	2.00	0.00	0.36	0.00	34.95	221.36	2.00	0.00	0.36	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
34.96	220.54	2.00	0.00	0.36	0.00	34.97	219.59	2.00	0.00	0.36	0.00
34.98	218.57	2.00	0.00	0.36	0.00	34.99	217.51	2.00	0.00	0.36	0.00
35.00	216.48	2.00	0.00	0.36	0.00	35.01	215.52	2.00	0.00	0.36	0.00
35.02	214.75	2.00	0.00	0.36	0.00	35.03	214.05	2.00	0.00	0.36	0.00
35.04	213.12	2.00	0.00	0.36	0.00	35.05	212.09	2.00	0.00	0.36	0.00
35.06	210.96	2.00	0.00	0.36	0.00	35.07	209.76	2.00	0.00	0.36	0.00
35.08	208.58	2.00	0.00	0.36	0.00	35.09	207.46	2.00	0.00	0.36	0.00
35.10	206.46	2.00	0.00	0.36	0.00	35.11	205.73	2.00	0.00	0.36	0.00
35.12	205.00	2.00	0.00	0.36	0.00	35.13	204.10	2.00	0.00	0.36	0.00
35.14	203.09	2.00	0.00	0.36	0.00	35.15	201.99	2.00	0.00	0.36	0.00
35.16	200.85	2.00	0.00	0.36	0.00	35.17	199.73	2.00	0.00	0.36	0.00
35.18	198.69	1.94	0.01	0.36	0.00	35.19	197.80	1.85	0.02	0.36	0.00
35.20	197.23	1.79	0.03	0.36	0.00	35.21	196.39	1.72	0.04	0.36	0.00
35.22	195.39	1.63	0.06	0.36	0.00	35.23	194.25	1.54	0.08	0.36	0.00
35.24	193.01	1.44	0.10	0.36	0.00	35.25	191.73	1.35	0.12	0.36	0.00
35.26	190.47	1.27	0.15	0.36	0.00	35.27	189.31	1.21	0.17	0.36	0.00
35.28	188.33	1.15	0.19	0.36	0.00	35.29	187.62	1.12	0.20	0.36	0.00
35.30	186.65	1.07	0.22	0.36	0.00	35.31	185.45	1.01	0.25	0.36	0.00
35.32	184.11	0.95	0.26	0.36	0.00	35.33	182.69	0.90	0.28	0.36	0.00
35.34	181.25	0.84	0.29	0.36	0.00	35.35	179.87	0.80	0.31	0.36	0.00
35.36	178.63	0.76	0.32	0.36	0.00	35.37	177.60	0.73	0.33	0.36	0.00
35.38	176.76	0.71	0.34	0.36	0.00	35.39	175.60	0.68	0.36	0.36	0.00
35.40	174.23	0.64	0.38	0.36	0.00	35.41	172.74	0.61	0.40	0.36	0.00
35.42	171.21	0.58	0.42	0.36	0.00	35.43	169.71	0.55	0.44	0.36	0.00
35.44	168.31	0.52	0.46	0.36	0.00	35.45	167.09	0.50	0.48	0.36	0.00
35.46	166.15	0.49	0.50	0.36	0.00	35.47	165.46	0.48	0.51	0.36	0.00
35.48	164.53	0.46	0.52	0.35	0.00	35.49	163.48	0.45	0.54	0.35	0.00
35.50	162.36	0.43	0.56	0.35	0.00	35.51	161.23	0.42	0.59	0.35	0.00
35.52	160.15	0.41	0.61	0.35	0.00	35.53	159.16	0.40	0.63	0.35	0.00
35.54	158.34	0.39	0.65	0.35	0.00	35.55	157.86	0.38	0.66	0.35	0.00
35.56	157.50	0.38	0.66	0.35	0.00	35.57	157.07	0.37	0.67	0.35	0.00
35.58	156.59	0.37	0.68	0.35	0.00	35.59	156.08	0.36	0.70	0.35	0.00
35.60	155.58	0.36	0.70	0.35	0.00	35.61	155.10	0.36	0.70	0.35	0.00
35.62	154.68	0.35	0.71	0.35	0.00	35.63	154.35	0.35	0.71	0.35	0.00
35.64	154.19	0.35	0.71	0.35	0.00	35.65	153.99	0.35	0.71	0.35	0.00
35.66	153.77	0.34	0.71	0.35	0.00	35.67	153.52	0.34	0.71	0.35	0.00
35.68	153.26	0.34	0.71	0.35	0.00	35.69	153.00	0.34	0.71	0.35	0.00
35.70	152.75	0.34	0.71	0.35	0.00	35.71	152.53	0.33	0.71	0.35	0.00
35.72	152.38	0.33	0.71	0.35	0.00	35.73	152.36	0.33	0.71	0.35	0.00
35.74	152.30	0.33	0.71	0.35	0.00	35.75	152.23	0.33	0.71	0.35	0.00
35.76	152.15	0.33	0.71	0.35	0.00	35.77	152.07	0.33	0.71	0.35	0.00
35.78	151.99	0.33	0.71	0.35	0.00	35.79	151.91	0.33	0.71	0.35	0.00
35.80	151.83	0.33	0.71	0.35	0.00	35.81	151.84	0.33	0.71	0.35	0.00
35.82	151.92	0.33	0.71	0.35	0.00	35.83	152.01	0.33	0.71	0.35	0.00
35.84	152.11	0.33	0.71	0.35	0.00	35.85	152.21	0.33	0.71	0.35	0.00
35.86	152.30	0.33	0.71	0.35	0.00	35.87	152.40	0.33	0.71	0.35	0.00
35.88	152.48	0.33	0.71	0.35	0.00	35.89	152.52	0.33	0.71	0.35	0.00
35.90	152.65	0.33	0.71	0.35	0.00	35.91	152.82	0.34	0.71	0.35	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
35.92	153.02	0.34	0.70	0.35	0.00	35.93	153.23	0.34	0.70	0.35	0.00
35.94	153.45	0.34	0.70	0.35	0.00	35.95	153.66	0.34	0.70	0.35	0.00
35.96	153.85	0.34	0.70	0.35	0.00	35.97	154.01	0.35	0.70	0.35	0.00
35.98	154.10	0.35	0.70	0.35	0.00	35.99	154.19	0.35	0.70	0.35	0.00
36.00	154.30	0.35	0.69	0.35	0.00	36.01	154.42	0.35	0.69	0.35	0.00
36.02	154.55	0.35	0.69	0.35	0.00	36.03	154.67	0.35	0.69	0.34	0.00
36.04	154.78	0.35	0.69	0.34	0.00	36.05	154.88	0.35	0.69	0.34	0.00
36.06	154.95	0.35	0.69	0.34	0.00	36.07	154.93	0.35	0.69	0.34	0.00
36.08	154.90	0.35	0.69	0.34	0.00	36.09	154.84	0.35	0.69	0.34	0.00
36.10	154.78	0.35	0.69	0.34	0.00	36.11	154.71	0.35	0.69	0.34	0.00
36.12	154.62	0.35	0.69	0.34	0.00	36.13	154.54	0.35	0.69	0.34	0.00
36.14	154.46	0.35	0.69	0.34	0.00	36.15	154.41	0.35	0.69	0.34	0.00
36.16	154.32	0.35	0.69	0.34	0.00	36.17	154.28	0.35	0.69	0.34	0.00
36.18	154.24	0.35	0.69	0.34	0.00	36.19	154.20	0.35	0.69	0.34	0.00
36.20	154.15	0.35	0.69	0.34	0.00	36.21	154.11	0.35	0.69	0.34	0.00
36.22	154.06	0.35	0.69	0.34	0.00	36.23	154.04	0.35	0.69	0.34	0.00
36.24	154.08	0.35	0.69	0.34	0.00	36.25	154.17	0.35	0.69	0.34	0.00
36.26	154.34	0.35	0.68	0.34	0.00	36.27	154.53	0.35	0.68	0.34	0.00
36.28	154.73	0.35	0.68	0.34	0.00	36.29	154.93	0.35	0.68	0.34	0.00
36.30	155.11	0.36	0.68	0.34	0.00	36.31	155.28	0.36	0.68	0.34	0.00
36.32	155.44	0.36	0.68	0.34	0.00	36.33	155.61	0.36	0.68	0.34	0.00
36.34	155.82	0.36	0.67	0.34	0.00	36.35	156.07	0.36	0.67	0.34	0.00
36.36	156.35	0.37	0.66	0.34	0.00	36.37	156.62	0.37	0.66	0.34	0.00
36.38	156.88	0.37	0.65	0.34	0.00	36.39	157.11	0.37	0.64	0.34	0.00
36.40	157.31	0.38	0.64	0.34	0.00	36.41	157.49	0.38	0.64	0.34	0.00
36.42	157.59	0.38	0.63	0.34	0.00	36.43	157.68	0.38	0.63	0.34	0.00
36.44	157.77	0.38	0.63	0.34	0.00	36.45	157.86	0.38	0.63	0.34	0.00
36.46	157.94	0.38	0.62	0.34	0.00	36.47	158.00	0.38	0.62	0.34	0.00
36.48	158.05	0.38	0.62	0.34	0.00	36.49	158.08	0.38	0.62	0.34	0.00
36.50	158.11	0.38	0.62	0.34	0.00	36.51	158.10	0.38	0.62	0.34	0.00
36.52	158.05	0.38	0.62	0.34	0.00	36.53	157.99	0.38	0.62	0.34	0.00
36.54	157.92	0.38	0.62	0.34	0.00	36.55	157.85	0.38	0.62	0.34	0.00
36.56	157.78	0.38	0.62	0.34	0.00	36.57	157.71	0.38	0.63	0.34	0.00
36.58	157.64	0.38	0.63	0.33	0.00	36.59	157.63	0.38	0.63	0.33	0.00
36.60	157.63	0.38	0.63	0.33	0.00	36.61	157.62	0.38	0.63	0.33	0.00
36.62	157.61	0.38	0.63	0.33	0.00	36.63	157.60	0.38	0.63	0.33	0.00
36.64	157.59	0.38	0.63	0.33	0.00	36.65	157.58	0.38	0.63	0.33	0.00
36.66	157.57	0.38	0.63	0.33	0.00	36.67	157.55	0.38	0.63	0.33	0.00
36.68	157.56	0.38	0.62	0.33	0.00	36.69	157.58	0.38	0.62	0.33	0.00
36.70	157.59	0.38	0.62	0.33	0.00	36.71	157.61	0.38	0.62	0.33	0.00
36.72	157.62	0.38	0.62	0.33	0.00	36.73	157.64	0.38	0.62	0.33	0.00
36.74	157.65	0.38	0.62	0.33	0.00	36.75	157.66	0.38	0.62	0.33	0.00
36.76	157.67	0.38	0.62	0.33	0.00	36.77	157.63	0.38	0.62	0.33	0.00
36.78	157.60	0.38	0.62	0.33	0.00	36.79	157.56	0.38	0.62	0.33	0.00
36.80	157.52	0.38	0.62	0.33	0.00	36.81	157.48	0.38	0.62	0.33	0.00
36.82	157.44	0.38	0.62	0.33	0.00	36.83	157.40	0.38	0.62	0.33	0.00
36.84	157.38	0.38	0.62	0.33	0.00	36.85	157.34	0.38	0.62	0.33	0.00
36.86	157.28	0.38	0.62	0.33	0.00	36.87	157.21	0.37	0.63	0.33	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
36.88	157.13	0.37	0.63	0.33	0.00	36.89	157.05	0.37	0.63	0.33	0.00
36.90	156.97	0.37	0.63	0.33	0.00	36.91	156.89	0.37	0.63	0.33	0.00
36.92	156.82	0.37	0.63	0.33	0.00	36.93	156.77	0.37	0.63	0.33	0.00
36.94	156.60	0.37	0.64	0.33	0.00	36.95	156.38	0.37	0.64	0.33	0.00
36.96	156.11	0.36	0.65	0.33	0.00	36.97	155.83	0.36	0.65	0.33	0.00
36.98	155.54	0.36	0.65	0.33	0.00	36.99	155.26	0.36	0.65	0.33	0.00
37.00	155.00	0.35	0.65	0.33	0.00	37.01	154.77	0.35	0.66	0.33	0.00
37.02	154.60	0.35	0.66	0.33	0.00	37.03	154.47	0.35	0.66	0.33	0.00
37.04	154.30	0.35	0.66	0.33	0.00	37.05	154.10	0.35	0.66	0.33	0.00
37.06	153.90	0.34	0.66	0.33	0.00	37.07	153.69	0.34	0.66	0.33	0.00
37.08	153.49	0.34	0.66	0.33	0.00	37.09	153.32	0.34	0.66	0.33	0.00
37.10	153.15	0.34	0.66	0.33	0.00	37.11	153.08	0.34	0.66	0.33	0.00
37.12	153.05	0.34	0.66	0.33	0.00	37.13	153.01	0.34	0.66	0.32	0.00
37.14	152.97	0.34	0.66	0.32	0.00	37.15	152.92	0.34	0.66	0.32	0.00
37.16	152.86	0.33	0.66	0.32	0.00	37.17	152.81	0.33	0.66	0.32	0.00
37.18	152.77	0.33	0.66	0.32	0.00	37.19	152.75	0.33	0.66	0.32	0.00
37.20	152.71	0.33	0.66	0.32	0.00	37.21	152.70	0.33	0.66	0.32	0.00
37.22	152.70	0.33	0.66	0.32	0.00	37.23	152.70	0.33	0.66	0.32	0.00
37.24	152.69	0.33	0.66	0.32	0.00	37.25	152.69	0.33	0.66	0.32	0.00
37.26	152.68	0.33	0.66	0.32	0.00	37.27	152.67	0.33	0.66	0.32	0.00
37.28	152.64	0.33	0.66	0.32	0.00	37.29	152.66	0.33	0.66	0.32	0.00
37.30	152.65	0.33	0.65	0.32	0.00	37.31	152.64	0.33	0.65	0.32	0.00
37.32	152.63	0.33	0.65	0.32	0.00	37.33	152.61	0.33	0.65	0.32	0.00
37.34	152.59	0.33	0.65	0.32	0.00	37.35	152.57	0.33	0.65	0.32	0.00
37.36	152.54	0.33	0.65	0.32	0.00	37.37	152.44	0.33	0.65	0.32	0.00
37.38	152.29	0.33	0.65	0.32	0.00	37.39	152.11	0.33	0.65	0.32	0.00
37.40	151.91	0.33	0.65	0.32	0.00	37.41	151.70	0.33	0.66	0.32	0.00
37.42	151.47	0.32	0.66	0.32	0.00	37.43	151.25	0.32	0.66	0.32	0.00
37.44	151.05	0.32	0.66	0.32	0.00	37.45	151.02	0.32	0.66	0.32	0.00
37.46	151.01	0.32	0.66	0.32	0.00	37.47	151.15	0.32	0.66	0.32	0.00
37.48	151.31	0.32	0.65	0.32	0.00	37.49	151.47	0.32	0.65	0.32	0.00
37.50	151.62	0.32	0.65	0.32	0.00	37.51	151.75	0.33	0.65	0.32	0.00
37.52	151.86	0.33	0.65	0.32	0.00	37.53	151.94	0.33	0.65	0.32	0.00
37.54	152.01	0.33	0.65	0.32	0.00	37.55	152.03	0.33	0.65	0.32	0.00
37.56	152.03	0.33	0.65	0.32	0.00	37.57	152.03	0.33	0.65	0.32	0.00
37.58	152.02	0.33	0.65	0.32	0.00	37.59	152.02	0.33	0.65	0.32	0.00
37.60	152.00	0.33	0.65	0.32	0.00	37.61	151.99	0.33	0.65	0.32	0.00
37.62	151.98	0.33	0.65	0.32	0.00	37.63	151.98	0.33	0.65	0.32	0.00
37.64	151.96	0.33	0.65	0.32	0.00	37.65	151.94	0.33	0.65	0.32	0.00
37.66	151.91	0.33	0.64	0.32	0.00	37.67	151.88	0.33	0.64	0.32	0.00
37.68	151.84	0.33	0.64	0.31	0.00	37.69	151.81	0.33	0.64	0.31	0.00
37.70	151.77	0.33	0.64	0.31	0.00	37.71	151.78	2.00	0.00	0.31	0.00
37.72	151.83	2.00	0.00	0.31	0.00	37.73	151.89	2.00	0.00	0.31	0.00
37.74	151.97	2.00	0.00	0.31	0.00	37.75	152.03	2.00	0.00	0.31	0.00
37.76	152.09	2.00	0.00	0.31	0.00	37.77	152.14	2.00	0.00	0.31	0.00
37.78	152.18	2.00	0.00	0.31	0.00	37.79	152.21	2.00	0.00	0.31	0.00
37.80	152.23	2.00	0.00	0.31	0.00	37.81	152.14	2.00	0.00	0.31	0.00
37.82	152.02	2.00	0.00	0.31	0.00	37.83	151.89	2.00	0.00	0.31	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
37.84	151.74	2.00	0.00	0.31	0.00	37.85	151.58	2.00	0.00	0.31	0.00
37.86	151.43	2.00	0.00	0.31	0.00	37.87	151.28	2.00	0.00	0.31	0.00
37.88	151.17	2.00	0.00	0.31	0.00	37.89	151.06	2.00	0.00	0.31	0.00
37.90	150.88	2.00	0.00	0.31	0.00	37.91	150.67	2.00	0.00	0.31	0.00
37.92	150.44	2.00	0.00	0.31	0.00	37.93	150.19	2.00	0.00	0.31	0.00
37.94	149.93	2.00	0.00	0.31	0.00	37.95	149.69	2.00	0.00	0.31	0.00
37.96	149.47	2.00	0.00	0.31	0.00	37.97	149.30	2.00	0.00	0.31	0.00
37.98	149.06	2.00	0.00	0.31	0.00	37.99	148.74	2.00	0.00	0.31	0.00
38.00	148.37	2.00	0.00	0.31	0.00	38.01	147.97	2.00	0.00	0.31	0.00
38.02	147.55	2.00	0.00	0.31	0.00	38.03	147.15	2.00	0.00	0.31	0.00
38.04	146.78	2.00	0.00	0.31	0.00	38.05	146.46	2.00	0.00	0.31	0.00
38.06	146.24	2.00	0.00	0.31	0.00	38.07	146.03	0.29	0.66	0.31	0.00
38.08	145.77	0.28	0.66	0.31	0.00	38.09	145.48	0.28	0.66	0.31	0.00
38.10	145.17	0.28	0.66	0.31	0.00	38.11	144.87	0.28	0.66	0.31	0.00
38.12	144.57	0.28	0.66	0.31	0.00	38.13	144.31	0.28	0.67	0.31	0.00
38.14	144.07	0.27	0.67	0.31	0.00	38.15	144.40	2.00	0.00	0.31	0.00
38.16	145.09	2.00	0.00	0.31	0.00	38.17	145.89	2.00	0.00	0.31	0.00
38.18	146.76	2.00	0.00	0.31	0.00	38.19	147.66	2.00	0.00	0.31	0.00
38.20	148.54	2.00	0.00	0.31	0.00	38.21	149.36	2.00	0.00	0.31	0.00
38.22	150.07	2.00	0.00	0.31	0.00	38.23	150.60	2.00	0.00	0.30	0.00
38.24	152.01	2.00	0.00	0.30	0.00	38.25	153.74	2.00	0.00	0.30	0.00
38.26	155.71	2.00	0.00	0.30	0.00	38.27	157.81	2.00	0.00	0.30	0.00
38.28	159.92	2.00	0.00	0.30	0.00	38.29	161.93	2.00	0.00	0.30	0.00
38.30	163.76	2.00	0.00	0.30	0.00	38.31	165.28	2.00	0.00	0.30	0.00
38.32	166.47	2.00	0.00	0.30	0.00	38.33	167.98	2.00	0.00	0.30	0.00
38.34	169.81	2.00	0.00	0.30	0.00	38.35	171.82	2.00	0.00	0.30	0.00
38.36	173.90	2.00	0.00	0.30	0.00	38.37	175.94	2.00	0.00	0.30	0.00
38.38	177.83	2.00	0.00	0.30	0.00	38.39	179.48	2.00	0.00	0.30	0.00
38.40	180.87	2.00	0.00	0.30	0.00	38.41	181.76	2.00	0.00	0.30	0.00
38.42	182.90	2.00	0.00	0.30	0.00	38.43	184.28	2.00	0.00	0.30	0.00
38.44	185.78	2.00	0.00	0.30	0.00	38.45	187.32	2.00	0.00	0.30	0.00
38.46	188.84	2.00	0.00	0.30	0.00	38.47	190.25	2.00	0.00	0.30	0.00
38.48	191.48	1.32	0.11	0.30	0.00	38.49	192.54	1.39	0.10	0.30	0.00
38.50	192.71	1.40	0.09	0.30	0.00	38.51	193.06	1.42	0.09	0.30	0.00
38.52	193.44	1.45	0.08	0.30	0.00	38.53	193.83	1.48	0.08	0.30	0.00
38.54	194.22	1.51	0.07	0.30	0.00	38.55	194.57	1.54	0.07	0.30	0.00
38.56	194.87	1.56	0.06	0.30	0.00	38.57	195.14	1.58	0.06	0.30	0.00
38.58	195.15	1.58	0.06	0.30	0.00	38.59	194.67	1.54	0.07	0.30	0.00
38.60	194.08	1.50	0.07	0.30	0.00	38.61	193.41	1.45	0.08	0.30	0.00
38.62	192.69	1.40	0.09	0.30	0.00	38.63	191.95	1.35	0.10	0.30	0.00
38.64	191.24	1.30	0.12	0.30	0.00	38.65	190.58	1.26	0.13	0.30	0.00
38.66	190.06	1.23	0.13	0.30	0.00	38.67	189.50	1.20	0.14	0.30	0.00
38.68	188.70	1.16	0.15	0.30	0.00	38.69	187.76	1.11	0.17	0.30	0.00
38.70	186.72	1.06	0.19	0.30	0.00	38.71	185.63	1.01	0.21	0.30	0.00
38.72	184.55	0.96	0.21	0.30	0.00	38.73	183.53	0.92	0.22	0.30	0.00
38.74	182.64	0.88	0.23	0.30	0.00	38.75	181.93	0.86	0.24	0.30	0.00
38.76	181.44	0.84	0.24	0.30	0.00	38.77	180.78	0.82	0.25	0.30	0.00
38.78	180.04	0.79	0.25	0.29	0.00	38.79	179.24	0.77	0.26	0.29	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
38.80	178.42	0.74	0.27	0.29	0.00	38.81	177.64	0.72	0.27	0.29	0.00
38.82	176.92	0.70	0.28	0.29	0.00	38.83	176.29	0.69	0.29	0.29	0.00
38.84	176.08	0.68	0.29	0.29	0.00	38.85	176.35	0.69	0.29	0.29	0.00
38.86	176.65	0.70	0.28	0.29	0.00	38.87	176.99	0.70	0.28	0.29	0.00
38.88	177.33	0.71	0.28	0.29	0.00	38.89	177.68	0.72	0.27	0.29	0.00
38.90	178.00	0.73	0.27	0.29	0.00	38.91	178.29	0.74	0.27	0.29	0.00
38.92	178.49	0.75	0.26	0.29	0.00	38.93	179.08	0.76	0.26	0.29	0.00
38.94	179.99	0.79	0.25	0.29	0.00	38.95	181.03	0.83	0.24	0.29	0.00
38.96	182.16	0.87	0.23	0.29	0.00	38.97	183.30	0.91	0.22	0.29	0.00
38.98	184.40	0.95	0.21	0.29	0.00	38.99	185.40	1.00	0.20	0.29	0.00
39.00	186.26	1.03	0.19	0.29	0.00	39.01	186.89	1.06	0.18	0.29	0.00
39.02	187.77	1.11	0.17	0.29	0.00	39.03	188.86	1.16	0.15	0.29	0.00
39.04	190.08	1.23	0.13	0.29	0.00	39.05	191.35	1.31	0.11	0.29	0.00
39.06	192.59	1.39	0.09	0.29	0.00	39.07	193.75	1.47	0.08	0.29	0.00
39.08	194.76	1.55	0.06	0.29	0.00	39.09	195.60	1.62	0.05	0.29	0.00
39.10	196.18	1.67	0.04	0.29	0.00	39.11	196.91	1.73	0.03	0.29	0.00
39.12	197.82	1.82	0.02	0.29	0.00	39.13	198.82	1.92	0.01	0.29	0.00
39.14	199.84	2.00	0.00	0.29	0.00	39.15	200.82	2.00	0.00	0.29	0.00
39.16	201.73	2.00	0.00	0.29	0.00	39.17	202.51	2.00	0.00	0.29	0.00
39.18	203.18	2.00	0.00	0.29	0.00	39.19	203.73	2.00	0.00	0.29	0.00
39.20	204.54	2.00	0.00	0.29	0.00	39.21	205.50	2.00	0.00	0.29	0.00
39.22	206.55	2.00	0.00	0.29	0.00	39.23	207.63	2.00	0.00	0.29	0.00
39.24	208.69	2.00	0.00	0.29	0.00	39.25	209.66	2.00	0.00	0.29	0.00
39.26	210.50	2.00	0.00	0.29	0.00	39.27	211.17	2.00	0.00	0.29	0.00
39.28	211.72	2.00	0.00	0.29	0.00	39.29	212.45	2.00	0.00	0.29	0.00
39.30	213.28	2.00	0.00	0.29	0.00	39.31	214.16	2.00	0.00	0.29	0.00
39.32	215.06	2.00	0.00	0.29	0.00	39.33	215.92	2.00	0.00	0.28	0.00
39.34	216.70	2.00	0.00	0.28	0.00	39.35	217.35	2.00	0.00	0.28	0.00
39.36	217.77	2.00	0.00	0.28	0.00	39.37	218.16	2.00	0.00	0.28	0.00
39.38	218.62	2.00	0.00	0.28	0.00	39.39	219.12	2.00	0.00	0.28	0.00
39.40	219.66	2.00	0.00	0.28	0.00	39.41	220.18	2.00	0.00	0.28	0.00
39.42	220.68	2.00	0.00	0.28	0.00	39.43	221.12	2.00	0.00	0.28	0.00
39.44	221.49	2.00	0.00	0.28	0.00	39.45	221.77	2.00	0.00	0.28	0.00
39.46	222.13	2.00	0.00	0.28	0.00	39.47	222.59	2.00	0.00	0.28	0.00
39.48	223.06	2.00	0.00	0.28	0.00	39.49	223.54	2.00	0.00	0.28	0.00
39.50	224.01	2.00	0.00	0.28	0.00	39.51	224.44	2.00	0.00	0.28	0.00
39.52	224.82	2.00	0.00	0.28	0.00	39.53	225.12	2.00	0.00	0.28	0.00
39.54	225.25	2.00	0.00	0.28	0.00	39.55	225.43	2.00	0.00	0.28	0.00
39.56	225.63	2.00	0.00	0.28	0.00	39.57	225.85	2.00	0.00	0.28	0.00
39.58	226.06	2.00	0.00	0.28	0.00	39.59	226.27	2.00	0.00	0.28	0.00
39.60	226.46	2.00	0.00	0.28	0.00	39.61	226.57	2.00	0.00	0.28	0.00
39.62	226.59	2.00	0.00	0.28	0.00	39.63	226.56	2.00	0.00	0.28	0.00
39.64	226.46	2.00	0.00	0.28	0.00	39.65	226.35	2.00	0.00	0.28	0.00
39.66	226.23	2.00	0.00	0.28	0.00	39.67	226.11	2.00	0.00	0.28	0.00
39.68	225.99	2.00	0.00	0.28	0.00	39.69	225.87	2.00	0.00	0.28	0.00
39.70	225.76	2.00	0.00	0.28	0.00	39.71	225.65	2.00	0.00	0.28	0.00
39.72	225.55	2.00	0.00	0.28	0.00	39.73	225.43	2.00	0.00	0.28	0.00
39.74	225.30	2.00	0.00	0.28	0.00	39.75	225.15	2.00	0.00	0.28	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
39.76	225.00	2.00	0.00	0.28	0.00	39.77	224.86	2.00	0.00	0.28	0.00
39.78	224.74	2.00	0.00	0.28	0.00	39.79	224.68	2.00	0.00	0.28	0.00
39.80	224.36	2.00	0.00	0.28	0.00	39.81	224.07	2.00	0.00	0.28	0.00
39.82	223.75	2.00	0.00	0.28	0.00	39.83	223.41	2.00	0.00	0.28	0.00
39.84	223.06	2.00	0.00	0.28	0.00	39.85	222.72	2.00	0.00	0.28	0.00
39.86	222.41	2.00	0.00	0.28	0.00	39.87	222.19	2.00	0.00	0.28	0.00
39.88	221.94	2.00	0.00	0.27	0.00	39.89	221.46	2.00	0.00	0.27	0.00
39.90	220.90	2.00	0.00	0.27	0.00	39.91	220.28	2.00	0.00	0.27	0.00
39.92	219.62	2.00	0.00	0.27	0.00	39.93	218.96	2.00	0.00	0.27	0.00
39.94	218.32	2.00	0.00	0.27	0.00	39.95	217.74	2.00	0.00	0.27	0.00
39.96	217.27	2.00	0.00	0.27	0.00	39.97	217.24	2.00	0.00	0.27	0.00
39.98	217.23	2.00	0.00	0.27	0.00	39.99	217.21	2.00	0.00	0.27	0.00
40.00	217.18	2.00	0.00	0.27	0.00	40.01	217.14	2.00	0.00	0.27	0.00
40.02	217.10	2.00	0.00	0.27	0.00	40.03	217.05	2.00	0.00	0.27	0.00
40.04	216.98	2.00	0.00	0.27	0.00	40.05	216.97	2.00	0.00	0.27	0.00
40.06	217.71	2.00	0.00	0.27	0.00	40.07	218.51	2.00	0.00	0.27	0.00
40.08	219.41	2.00	0.00	0.27	0.00	40.09	220.35	2.00	0.00	0.27	0.00
40.10	221.30	2.00	0.00	0.27	0.00	40.11	222.20	2.00	0.00	0.27	0.00
40.12	223.00	2.00	0.00	0.27	0.00	40.13	223.65	2.00	0.00	0.27	0.00
40.14	224.04	2.00	0.00	0.27	0.00	40.15	224.46	2.00	0.00	0.27	0.00
40.16	224.95	2.00	0.00	0.27	0.00	40.17	225.47	2.00	0.00	0.27	0.00
40.18	226.01	2.00	0.00	0.27	0.00	40.19	226.53	2.00	0.00	0.27	0.00
40.20	227.00	2.00	0.00	0.27	0.00	40.21	227.40	2.00	0.00	0.27	0.00
40.22	227.77	2.00	0.00	0.27	0.00	40.23	227.64	2.00	0.00	0.27	0.00
40.24	227.53	2.00	0.00	0.27	0.00	40.25	227.42	2.00	0.00	0.27	0.00
40.26	227.29	2.00	0.00	0.27	0.00	40.27	227.16	2.00	0.00	0.27	0.00
40.28	227.03	2.00	0.00	0.27	0.00	40.29	226.91	2.00	0.00	0.27	0.00
40.30	226.81	2.00	0.00	0.27	0.00	40.31	226.70	2.00	0.00	0.27	0.00
40.32	226.49	2.00	0.00	0.27	0.00	40.33	226.25	2.00	0.00	0.27	0.00
40.34	225.97	2.00	0.00	0.27	0.00	40.35	225.68	2.00	0.00	0.27	0.00
40.36	225.39	2.00	0.00	0.27	0.00	40.37	225.11	2.00	0.00	0.27	0.00
40.38	224.86	2.00	0.00	0.27	0.00	40.39	224.65	2.00	0.00	0.27	0.00
40.40	224.41	2.00	0.00	0.27	0.00	40.41	224.07	2.00	0.00	0.27	0.00
40.42	223.68	2.00	0.00	0.27	0.00	40.43	223.25	2.00	0.00	0.26	0.00
40.44	222.80	2.00	0.00	0.26	0.00	40.45	222.35	2.00	0.00	0.26	0.00
40.46	221.93	2.00	0.00	0.26	0.00	40.47	221.56	2.00	0.00	0.26	0.00
40.48	221.28	2.00	0.00	0.26	0.00	40.49	220.98	2.00	0.00	0.26	0.00
40.50	220.64	2.00	0.00	0.26	0.00	40.51	220.24	2.00	0.00	0.26	0.00
40.52	219.81	2.00	0.00	0.26	0.00	40.53	219.37	2.00	0.00	0.26	0.00
40.54	218.94	2.00	0.00	0.26	0.00	40.55	218.55	2.00	0.00	0.26	0.00
40.56	218.22	2.00	0.00	0.26	0.00	40.57	217.92	2.00	0.00	0.26	0.00
40.58	217.38	2.00	0.00	0.26	0.00	40.59	216.73	2.00	0.00	0.26	0.00
40.60	216.00	2.00	0.00	0.26	0.00	40.61	215.23	2.00	0.00	0.26	0.00
40.62	214.45	2.00	0.00	0.26	0.00	40.63	213.71	2.00	0.00	0.26	0.00
40.64	213.03	2.00	0.00	0.26	0.00	40.65	212.48	2.00	0.00	0.26	0.00
40.66	211.96	2.00	0.00	0.26	0.00	40.67	211.20	2.00	0.00	0.26	0.00
40.68	210.32	2.00	0.00	0.26	0.00	40.69	209.34	2.00	0.00	0.26	0.00
40.70	208.33	2.00	0.00	0.26	0.00	40.71	207.30	2.00	0.00	0.26	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
40.72	206.36	2.00	0.00	0.26	0.00	40.73	205.53	2.00	0.00	0.26	0.00
40.74	204.91	2.00	0.00	0.26	0.00	40.75	204.28	2.00	0.00	0.26	0.00
40.76	203.48	2.00	0.00	0.26	0.00	40.77	202.55	2.00	0.00	0.26	0.00
40.78	201.55	2.00	0.00	0.26	0.00	40.79	200.52	2.00	0.00	0.26	0.00
40.80	199.52	1.98	0.00	0.26	0.00	40.81	198.59	1.88	0.01	0.26	0.00
40.82	197.78	1.80	0.02	0.26	0.00	40.83	197.14	1.74	0.03	0.26	0.00
40.84	196.23	1.66	0.04	0.26	0.00	40.85	195.11	1.57	0.05	0.26	0.00
40.86	193.84	1.47	0.07	0.26	0.00	40.87	192.50	1.38	0.08	0.26	0.00
40.88	191.15	1.29	0.10	0.26	0.00	40.89	189.85	1.21	0.12	0.26	0.00
40.90	188.68	1.15	0.14	0.26	0.00	40.91	187.70	1.10	0.15	0.26	0.00
40.92	186.82	1.06	0.16	0.26	0.00	40.93	185.60	1.00	0.18	0.26	0.00
40.94	184.14	0.94	0.19	0.26	0.00	40.95	182.55	0.88	0.20	0.26	0.00
40.96	180.90	0.82	0.21	0.26	0.00	40.97	179.27	0.77	0.22	0.26	0.00
40.98	177.74	0.72	0.24	0.25	0.00	40.99	176.40	0.69	0.25	0.25	0.00
41.00	175.34	0.66	0.26	0.25	0.00	41.01	174.39	0.64	0.27	0.25	0.00
41.02	173.17	2.00	0.00	0.25	0.00	41.03	171.77	2.00	0.00	0.25	0.00
41.04	170.27	2.00	0.00	0.25	0.00	41.05	168.74	2.00	0.00	0.25	0.00
41.06	167.25	2.00	0.00	0.25	0.00	41.07	165.88	2.00	0.00	0.25	0.00
41.08	164.72	2.00	0.00	0.25	0.00	41.09	163.80	2.00	0.00	0.25	0.00
41.10	162.65	2.00	0.00	0.25	0.00	41.11	161.24	2.00	0.00	0.25	0.00
41.12	159.66	2.00	0.00	0.25	0.00	41.13	158.00	2.00	0.00	0.25	0.00
41.14	156.32	2.00	0.00	0.25	0.00	41.15	154.73	2.00	0.00	0.25	0.00
41.16	153.29	2.00	0.00	0.25	0.00	41.17	152.10	2.00	0.00	0.25	0.00
41.18	151.13	2.00	0.00	0.25	0.00	41.19	149.90	2.00	0.00	0.25	0.00
41.20	148.45	2.00	0.00	0.25	0.00	41.21	146.85	2.00	0.00	0.25	0.00
41.22	145.20	2.00	0.00	0.25	0.00	41.23	143.57	2.00	0.00	0.25	0.00
41.24	142.05	2.00	0.00	0.25	0.00	41.25	140.72	2.00	0.00	0.25	0.00
41.26	139.67	2.00	0.00	0.25	0.00	41.27	139.10	2.00	0.00	0.25	0.00
41.28	138.39	2.00	0.00	0.25	0.00	41.29	137.57	2.00	0.00	0.25	0.00
41.30	136.69	2.00	0.00	0.25	0.00	41.31	135.79	2.00	0.00	0.25	0.00
41.32	134.92	2.00	0.00	0.25	0.00	41.33	134.12	2.00	0.00	0.25	0.00
41.34	133.44	2.00	0.00	0.25	0.00	41.35	132.95	2.00	0.00	0.25	0.00
41.36	132.47	2.00	0.00	0.25	0.00	41.37	131.88	2.00	0.00	0.25	0.00
41.38	131.21	2.00	0.00	0.25	0.00	41.39	130.51	2.00	0.00	0.25	0.00
41.40	129.79	2.00	0.00	0.25	0.00	41.41	129.11	2.00	0.00	0.25	0.00
41.42	128.50	2.00	0.00	0.25	0.00	41.43	127.99	2.00	0.00	0.25	0.00
41.44	127.60	2.00	0.00	0.25	0.00	41.45	127.11	2.00	0.00	0.25	0.00
41.46	126.52	2.00	0.00	0.25	0.00	41.47	125.88	2.00	0.00	0.25	0.00
41.48	125.21	2.00	0.00	0.25	0.00	41.49	124.55	2.00	0.00	0.25	0.00
41.50	123.92	2.00	0.00	0.25	0.00	41.51	123.38	2.00	0.00	0.25	0.00
41.52	122.96	2.00	0.00	0.25	0.00	41.53	122.55	2.00	0.00	0.24	0.00
41.54	122.03	2.00	0.00	0.24	0.00	41.55	121.43	2.00	0.00	0.24	0.00
41.56	120.78	2.00	0.00	0.24	0.00	41.57	120.11	2.00	0.00	0.24	0.00
41.58	119.46	2.00	0.00	0.24	0.00	41.59	118.85	2.00	0.00	0.24	0.00
41.60	118.34	2.00	0.00	0.24	0.00	41.61	117.92	2.00	0.00	0.24	0.00
41.62	117.37	2.00	0.00	0.24	0.00	41.63	116.69	2.00	0.00	0.24	0.00
41.64	50.40	2.00	0.00	0.24	0.00	41.65	49.65	2.00	0.00	0.24	0.00
41.66	48.91	2.00	0.00	0.24	0.00	41.67	48.20	2.00	0.00	0.24	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
41.68	47.57	2.00	0.00	0.24	0.00	41.69	47.04	2.00	0.00	0.24	0.00
41.70	46.63	2.00	0.00	0.24	0.00	41.71	46.13	2.00	0.00	0.24	0.00
41.72	45.55	2.00	0.00	0.24	0.00	41.73	44.91	2.00	0.00	0.24	0.00
41.74	44.25	2.00	0.00	0.24	0.00	41.75	43.60	2.00	0.00	0.24	0.00
41.76	43.00	2.00	0.00	0.24	0.00	41.77	42.47	2.00	0.00	0.24	0.00
41.78	42.05	2.00	0.00	0.24	0.00	41.79	41.70	2.00	0.00	0.24	0.00
41.80	41.25	2.00	0.00	0.24	0.00	41.81	40.75	2.00	0.00	0.24	0.00
41.82	40.20	2.00	0.00	0.24	0.00	41.83	39.65	2.00	0.00	0.24	0.00
41.84	39.11	2.00	0.00	0.24	0.00	41.85	38.63	2.00	0.00	0.24	0.00
41.86	38.21	2.00	0.00	0.24	0.00	41.87	37.94	2.00	0.00	0.24	0.00
41.88	37.75	2.00	0.00	0.24	0.00	41.89	37.51	2.00	0.00	0.24	0.00
41.90	37.25	2.00	0.00	0.24	0.00	41.91	36.97	2.00	0.00	0.24	0.00
41.92	36.70	2.00	0.00	0.24	0.00	41.93	36.44	2.00	0.00	0.24	0.00
41.94	36.21	2.00	0.00	0.24	0.00	41.95	36.01	2.00	0.00	0.24	0.00
41.96	35.99	2.00	0.00	0.24	0.00	41.97	36.04	2.00	0.00	0.24	0.00
41.98	36.09	2.00	0.00	0.24	0.00	41.99	36.15	2.00	0.00	0.24	0.00
42.00	36.22	2.00	0.00	0.24	0.00	42.01	36.28	2.00	0.00	0.24	0.00
42.02	36.34	2.00	0.00	0.24	0.00	42.03	36.39	2.00	0.00	0.24	0.00
42.04	36.44	2.00	0.00	0.24	0.00	42.05	36.83	2.00	0.00	0.24	0.00
42.06	37.32	2.00	0.00	0.24	0.00	42.07	37.87	2.00	0.00	0.24	0.00
42.08	38.47	2.00	0.00	0.23	0.00	42.09	39.08	2.00	0.00	0.23	0.00
42.10	39.68	2.00	0.00	0.23	0.00	42.11	40.21	2.00	0.00	0.23	0.00
42.12	40.67	2.00	0.00	0.23	0.00	42.13	41.10	2.00	0.00	0.23	0.00
42.14	41.77	2.00	0.00	0.23	0.00	42.15	42.58	2.00	0.00	0.23	0.00
42.16	43.48	2.00	0.00	0.23	0.00	42.17	44.43	2.00	0.00	0.23	0.00
42.18	45.38	2.00	0.00	0.23	0.00	42.19	46.28	2.00	0.00	0.23	0.00
42.20	47.09	2.00	0.00	0.23	0.00	42.21	47.74	2.00	0.00	0.23	0.00
42.22	48.25	2.00	0.00	0.23	0.00	42.23	48.87	2.00	0.00	0.23	0.00
42.24	49.60	2.00	0.00	0.23	0.00	42.25	50.40	2.00	0.00	0.23	0.00
42.26	116.87	0.18	0.63	0.23	0.00	42.27	117.67	0.18	0.63	0.23	0.00
42.28	118.40	0.18	0.62	0.23	0.00	42.29	119.03	0.18	0.62	0.23	0.00
42.30	119.51	0.18	0.62	0.23	0.00	42.31	119.72	0.18	0.61	0.23	0.00
42.32	120.04	0.18	0.61	0.23	0.00	42.33	120.40	0.18	0.61	0.23	0.00
42.34	120.78	0.19	0.61	0.23	0.00	42.35	121.16	0.19	0.60	0.23	0.00
42.36	121.52	0.19	0.60	0.23	0.00	42.37	121.85	0.19	0.60	0.23	0.00
42.38	122.14	0.19	0.60	0.23	0.00	42.39	122.17	0.19	0.60	0.23	0.00
42.40	121.78	0.19	0.60	0.23	0.00	42.41	121.35	0.19	0.60	0.23	0.00
42.42	120.88	0.19	0.60	0.23	0.00	42.43	120.38	0.18	0.60	0.23	0.00
42.44	119.89	0.18	0.61	0.23	0.00	42.45	119.41	0.18	0.61	0.23	0.00
42.46	118.99	0.18	0.61	0.23	0.00	42.47	118.67	0.18	0.61	0.23	0.00
42.48	118.22	0.18	0.61	0.23	0.00	42.49	117.57	0.18	0.62	0.23	0.00
42.50	116.81	0.18	0.62	0.23	0.00	42.51	115.98	0.17	0.63	0.23	0.00
42.52	115.11	0.17	0.63	0.23	0.00	42.53	114.25	0.17	0.63	0.23	0.00
42.54	113.45	0.17	0.64	0.23	0.00	42.55	47.96	2.00	0.00	0.23	0.00
42.56	47.44	2.00	0.00	0.23	0.00	42.57	46.88	2.00	0.00	0.23	0.00
42.58	46.17	2.00	0.00	0.23	0.00	42.59	45.37	2.00	0.00	0.23	0.00
42.60	44.52	2.00	0.00	0.23	0.00	42.61	43.66	2.00	0.00	0.23	0.00
42.62	42.83	2.00	0.00	0.23	0.00	42.63	42.08	2.00	0.00	0.22	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
42.64	41.44	2.00	0.00	0.22	0.00	42.65	40.96	2.00	0.00	0.22	0.00
42.66	40.42	2.00	0.00	0.22	0.00	42.67	39.77	2.00	0.00	0.22	0.00
42.68	39.06	2.00	0.00	0.22	0.00	42.69	38.31	2.00	0.00	0.22	0.00
42.70	37.57	2.00	0.00	0.22	0.00	42.71	36.86	2.00	0.00	0.22	0.00
42.72	36.24	2.00	0.00	0.22	0.00	42.73	35.73	2.00	0.00	0.22	0.00
42.74	35.59	2.00	0.00	0.22	0.00	42.75	35.53	2.00	0.00	0.22	0.00
42.76	35.47	2.00	0.00	0.22	0.00	42.77	35.40	2.00	0.00	0.22	0.00
42.78	35.32	2.00	0.00	0.22	0.00	42.79	35.25	2.00	0.00	0.22	0.00
42.80	35.19	2.00	0.00	0.22	0.00	42.81	35.13	2.00	0.00	0.22	0.00
42.82	35.13	2.00	0.00	0.22	0.00	42.83	35.70	2.00	0.00	0.22	0.00
42.84	36.41	2.00	0.00	0.22	0.00	42.85	37.22	2.00	0.00	0.22	0.00
42.86	38.08	2.00	0.00	0.22	0.00	42.87	38.95	2.00	0.00	0.22	0.00
42.88	39.79	2.00	0.00	0.22	0.00	42.89	40.56	2.00	0.00	0.22	0.00
42.90	41.21	2.00	0.00	0.22	0.00	42.91	41.74	2.00	0.00	0.22	0.00
42.92	42.41	2.00	0.00	0.22	0.00	42.93	43.23	2.00	0.00	0.22	0.00
42.94	107.78	0.16	0.65	0.22	0.00	42.95	108.82	0.16	0.65	0.22	0.00
42.96	109.85	0.16	0.64	0.22	0.00	42.97	110.82	0.16	0.63	0.22	0.00
42.98	111.68	0.17	0.63	0.22	0.00	42.99	112.40	0.17	0.62	0.22	0.00
43.00	112.66	0.17	0.62	0.22	0.00	43.01	112.91	0.17	0.62	0.22	0.00
43.02	113.21	0.17	0.62	0.22	0.00	43.03	113.54	0.17	0.61	0.22	0.00
43.04	113.87	0.17	0.61	0.22	0.00	43.05	114.20	0.17	0.61	0.22	0.00
43.06	114.51	0.17	0.61	0.22	0.00	43.07	114.77	0.17	0.60	0.22	0.00
43.08	114.98	0.17	0.60	0.22	0.00	43.09	114.97	0.17	0.60	0.22	0.00
43.10	114.98	0.17	0.60	0.22	0.00	43.11	114.99	0.17	0.60	0.22	0.00
43.12	115.00	0.17	0.60	0.22	0.00	43.13	115.01	0.17	0.60	0.22	0.00
43.14	115.01	0.17	0.60	0.22	0.00	43.15	115.01	0.17	0.60	0.22	0.00
43.16	115.01	0.17	0.60	0.22	0.00	43.17	115.02	0.17	0.60	0.22	0.00
43.18	115.02	0.17	0.60	0.21	0.00	43.19	115.02	0.17	0.60	0.21	0.00
43.20	49.71	2.00	0.00	0.21	0.00	43.21	49.63	2.00	0.00	0.21	0.00
43.22	49.56	2.00	0.00	0.21	0.00	43.23	49.50	2.00	0.00	0.21	0.00
43.24	49.44	2.00	0.00	0.21	0.00	43.25	49.39	2.00	0.00	0.21	0.00
43.26	49.40	2.00	0.00	0.21	0.00	43.27	49.43	2.00	0.00	0.21	0.00
43.28	49.46	2.00	0.00	0.21	0.00	43.29	49.50	2.00	0.00	0.21	0.00
43.30	49.54	2.00	0.00	0.21	0.00	43.31	49.58	2.00	0.00	0.21	0.00
43.32	49.62	2.00	0.00	0.21	0.00	43.33	49.65	2.00	0.00	0.21	0.00
43.34	49.70	2.00	0.00	0.21	0.00	43.35	49.93	2.00	0.00	0.21	0.00
43.36	50.22	2.00	0.00	0.21	0.00	43.37	50.55	2.00	0.00	0.21	0.00
43.38	50.90	2.00	0.00	0.21	0.00	43.39	116.97	2.00	0.00	0.21	0.00
43.40	117.30	2.00	0.00	0.21	0.00	43.41	117.60	2.00	0.00	0.21	0.00
43.42	117.84	2.00	0.00	0.21	0.00	43.43	118.15	2.00	0.00	0.21	0.00
43.44	118.72	2.00	0.00	0.21	0.00	43.45	119.40	2.00	0.00	0.21	0.00
43.46	120.14	2.00	0.00	0.21	0.00	43.47	120.91	2.00	0.00	0.21	0.00
43.48	121.66	2.00	0.00	0.21	0.00	43.49	122.36	2.00	0.00	0.21	0.00
43.50	122.98	2.00	0.00	0.21	0.00	43.51	123.47	2.00	0.00	0.21	0.00
43.52	123.80	2.00	0.00	0.21	0.00	43.53	124.23	2.00	0.00	0.21	0.00
43.54	124.74	2.00	0.00	0.21	0.00	43.55	125.28	2.00	0.00	0.21	0.00
43.56	125.82	2.00	0.00	0.21	0.00	43.57	126.35	2.00	0.00	0.21	0.00
43.58	126.83	2.00	0.00	0.21	0.00	43.59	127.24	2.00	0.00	0.21	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
43.60	127.52	2.00	0.00	0.21	0.00	43.61	127.46	0.20	0.52	0.21	0.00
43.62	127.44	0.20	0.51	0.21	0.00	43.63	127.41	0.20	0.51	0.21	0.00
43.64	127.38	0.20	0.51	0.21	0.00	43.65	127.35	0.20	0.51	0.21	0.00
43.66	127.32	0.20	0.51	0.21	0.00	43.67	127.30	0.20	0.51	0.21	0.00
43.68	127.30	2.00	0.00	0.21	0.00	43.69	127.14	2.00	0.00	0.21	0.00
43.70	126.69	2.00	0.00	0.21	0.00	43.71	126.18	2.00	0.00	0.21	0.00
43.72	125.62	2.00	0.00	0.21	0.00	43.73	125.01	2.00	0.00	0.20	0.00
43.74	124.41	2.00	0.00	0.20	0.00	43.75	123.83	2.00	0.00	0.20	0.00
43.76	123.32	2.00	0.00	0.20	0.00	43.77	122.94	2.00	0.00	0.20	0.00
43.78	122.30	2.00	0.00	0.20	0.00	43.79	121.42	2.00	0.00	0.20	0.00
43.80	120.38	2.00	0.00	0.20	0.00	43.81	119.25	2.00	0.00	0.20	0.00
43.82	118.07	2.00	0.00	0.20	0.00	43.83	116.91	2.00	0.00	0.20	0.00
43.84	50.25	2.00	0.00	0.20	0.00	43.85	49.37	2.00	0.00	0.20	0.00
43.86	48.69	2.00	0.00	0.20	0.00	43.87	48.02	2.00	0.00	0.20	0.00
43.88	47.21	2.00	0.00	0.20	0.00	43.89	46.29	2.00	0.00	0.20	0.00
43.90	45.31	2.00	0.00	0.20	0.00	43.91	44.33	2.00	0.00	0.20	0.00
43.92	43.40	2.00	0.00	0.20	0.00	43.93	42.55	2.00	0.00	0.20	0.00
43.94	41.84	2.00	0.00	0.20	0.00	43.95	41.44	2.00	0.00	0.20	0.00
43.96	41.14	2.00	0.00	0.20	0.00	43.97	40.79	2.00	0.00	0.20	0.00
43.98	40.40	2.00	0.00	0.20	0.00	43.99	39.99	2.00	0.00	0.20	0.00
44.00	39.59	2.00	0.00	0.20	0.00	44.01	39.21	2.00	0.00	0.20	0.00
44.02	38.87	2.00	0.00	0.20	0.00	44.03	38.60	2.00	0.00	0.20	0.00
44.04	38.64	2.00	0.00	0.20	0.00	44.05	38.75	2.00	0.00	0.20	0.00
44.06	38.86	2.00	0.00	0.20	0.00	44.07	38.99	2.00	0.00	0.20	0.00
44.08	39.13	2.00	0.00	0.20	0.00	44.09	39.26	2.00	0.00	0.20	0.00
44.10	39.37	2.00	0.00	0.20	0.00	44.11	39.47	2.00	0.00	0.20	0.00
44.12	39.60	2.00	0.00	0.20	0.00	44.13	39.96	2.00	0.00	0.20	0.00
44.14	40.40	2.00	0.00	0.20	0.00	44.15	40.90	2.00	0.00	0.20	0.00
44.16	41.43	2.00	0.00	0.20	0.00	44.17	41.96	2.00	0.00	0.20	0.00
44.18	42.47	2.00	0.00	0.20	0.00	44.19	42.93	2.00	0.00	0.20	0.00
44.20	43.32	2.00	0.00	0.20	0.00	44.21	43.86	2.00	0.00	0.20	0.00
44.22	44.78	2.00	0.00	0.20	0.00	44.23	45.86	2.00	0.00	0.20	0.00
44.24	47.06	2.00	0.00	0.20	0.00	44.25	48.31	2.00	0.00	0.20	0.00
44.26	49.54	2.00	0.00	0.20	0.00	44.27	50.70	2.00	0.00	0.20	0.00
44.28	51.73	2.00	0.00	0.19	0.00	44.29	52.55	2.00	0.00	0.19	0.00
44.30	53.57	2.00	0.00	0.19	0.00	44.31	54.91	2.00	0.00	0.19	0.00
44.32	56.45	2.00	0.00	0.19	0.00	44.33	58.12	2.00	0.00	0.19	0.00
44.34	59.83	2.00	0.00	0.19	0.00	44.35	130.18	2.00	0.00	0.19	0.00
44.36	131.88	2.00	0.00	0.19	0.00	44.37	133.33	2.00	0.00	0.19	0.00
44.38	134.41	2.00	0.00	0.19	0.00	44.39	135.54	2.00	0.00	0.19	0.00
44.40	136.96	2.00	0.00	0.19	0.00	44.41	138.54	2.00	0.00	0.19	0.00
44.42	140.20	2.00	0.00	0.19	0.00	44.43	141.84	2.00	0.00	0.19	0.00
44.44	143.40	2.00	0.00	0.19	0.00	44.45	144.79	2.00	0.00	0.19	0.00
44.46	145.93	2.00	0.00	0.19	0.00	44.47	146.71	2.00	0.00	0.19	0.00
44.48	147.62	2.00	0.00	0.19	0.00	44.49	148.71	2.00	0.00	0.19	0.00
44.50	149.89	2.00	0.00	0.19	0.00	44.51	151.10	2.00	0.00	0.19	0.00
44.52	152.27	2.00	0.00	0.19	0.00	44.53	153.36	2.00	0.00	0.19	0.00
44.54	154.29	2.00	0.00	0.19	0.00	44.55	155.06	2.00	0.00	0.19	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
44.56	155.18	2.00	0.00	0.19	0.00	44.57	155.36	2.00	0.00	0.19	0.00
44.58	155.58	2.00	0.00	0.19	0.00	44.59	155.80	2.00	0.00	0.19	0.00
44.60	156.03	2.00	0.00	0.19	0.00	44.61	156.25	2.00	0.00	0.19	0.00
44.62	156.44	2.00	0.00	0.19	0.00	44.63	156.60	2.00	0.00	0.19	0.00
44.64	156.75	2.00	0.00	0.19	0.00	44.65	157.14	2.00	0.00	0.19	0.00
44.66	157.61	2.00	0.00	0.19	0.00	44.67	158.14	2.00	0.00	0.19	0.00
44.68	158.70	2.00	0.00	0.19	0.00	44.69	159.25	2.00	0.00	0.19	0.00
44.70	159.77	2.00	0.00	0.19	0.00	44.71	160.23	2.00	0.00	0.19	0.00
44.72	160.60	2.00	0.00	0.19	0.00	44.73	160.88	2.00	0.00	0.19	0.00
44.74	161.26	2.00	0.00	0.19	0.00	44.75	161.70	2.00	0.00	0.19	0.00
44.76	162.19	2.00	0.00	0.19	0.00	44.77	162.68	2.00	0.00	0.19	0.00
44.78	163.16	2.00	0.00	0.19	0.00	44.79	163.60	2.00	0.00	0.19	0.00
44.80	163.97	2.00	0.00	0.19	0.00	44.81	164.35	0.45	0.28	0.19	0.00
44.82	164.07	0.45	0.28	0.19	0.00	44.83	163.80	0.45	0.28	0.18	0.00
44.84	163.50	0.44	0.28	0.18	0.00	44.85	163.17	0.44	0.29	0.18	0.00
44.86	162.83	0.43	0.29	0.18	0.00	44.87	162.50	0.43	0.29	0.18	0.00
44.88	162.20	0.43	0.29	0.18	0.00	44.89	161.94	0.42	0.30	0.18	0.00
44.90	161.76	0.42	0.30	0.18	0.00	44.91	161.55	0.42	0.30	0.18	0.00
44.92	161.30	0.41	0.30	0.18	0.00	44.93	161.02	0.41	0.31	0.18	0.00
44.94	160.72	0.41	0.31	0.18	0.00	44.95	160.42	0.40	0.31	0.18	0.00
44.96	160.14	0.40	0.31	0.18	0.00	44.97	159.88	0.40	0.32	0.18	0.00
44.98	159.67	0.40	0.32	0.18	0.00	44.99	159.55	0.39	0.32	0.18	0.00
45.00	159.42	0.39	0.32	0.18	0.00	45.01	159.26	0.39	0.32	0.18	0.00
45.02	159.09	0.39	0.32	0.18	0.00	45.03	158.91	0.39	0.32	0.18	0.00
45.04	158.73	0.39	0.33	0.18	0.00	45.05	158.56	0.38	0.33	0.18	0.00
45.06	158.40	0.38	0.33	0.18	0.00	45.07	158.29	0.38	0.33	0.18	0.00
45.08	158.18	2.00	0.00	0.18	0.00	45.09	158.04	2.00	0.00	0.18	0.00
45.10	157.87	2.00	0.00	0.18	0.00	45.11	157.68	2.00	0.00	0.18	0.00
45.12	157.49	2.00	0.00	0.18	0.00	45.13	157.30	2.00	0.00	0.18	0.00
45.14	157.12	2.00	0.00	0.18	0.00	45.15	156.97	2.00	0.00	0.18	0.00
45.16	156.85	2.00	0.00	0.18	0.00	45.17	156.61	2.00	0.00	0.18	0.00
45.18	156.33	2.00	0.00	0.18	0.00	45.19	156.00	2.00	0.00	0.18	0.00
45.20	155.66	2.00	0.00	0.18	0.00	45.21	155.30	2.00	0.00	0.18	0.00
45.22	154.97	2.00	0.00	0.18	0.00	45.23	154.66	2.00	0.00	0.18	0.00
45.24	154.41	2.00	0.00	0.18	0.00	45.25	154.21	2.00	0.00	0.18	0.00
45.26	153.94	2.00	0.00	0.18	0.00	45.27	153.62	2.00	0.00	0.18	0.00
45.28	153.26	2.00	0.00	0.18	0.00	45.29	152.89	2.00	0.00	0.18	0.00
45.30	152.52	2.00	0.00	0.18	0.00	45.31	152.17	2.00	0.00	0.18	0.00
45.32	151.87	2.00	0.00	0.18	0.00	45.33	151.61	2.00	0.00	0.18	0.00
45.34	151.45	0.32	0.36	0.18	0.00	45.35	151.22	0.32	0.36	0.18	0.00
45.36	150.96	0.32	0.36	0.18	0.00	45.37	150.68	0.32	0.36	0.18	0.00
45.38	150.39	0.31	0.36	0.17	0.00	45.39	150.11	0.31	0.36	0.17	0.00
45.40	149.86	0.31	0.36	0.17	0.00	45.41	149.63	0.31	0.36	0.17	0.00
45.42	149.51	0.31	0.36	0.17	0.00	45.43	149.59	0.31	0.36	0.17	0.00
45.44	149.65	0.31	0.36	0.17	0.00	45.45	149.73	0.31	0.36	0.17	0.00
45.46	149.81	0.31	0.36	0.17	0.00	45.47	149.88	0.31	0.36	0.17	0.00
45.48	149.96	0.31	0.36	0.17	0.00	45.49	150.02	0.31	0.36	0.17	0.00
45.50	150.04	2.00	0.00	0.17	0.00	45.51	150.27	2.00	0.00	0.17	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
45.52	150.69	2.00	0.00	0.17	0.00	45.53	151.17	2.00	0.00	0.17	0.00
45.54	151.69	2.00	0.00	0.17	0.00	45.55	152.21	2.00	0.00	0.17	0.00
45.56	152.72	2.00	0.00	0.17	0.00	45.57	153.19	2.00	0.00	0.17	0.00
45.58	153.58	2.00	0.00	0.17	0.00	45.59	153.87	2.00	0.00	0.17	0.00
45.60	154.26	2.00	0.00	0.17	0.00	45.61	154.78	2.00	0.00	0.17	0.00
45.62	155.36	2.00	0.00	0.17	0.00	45.63	155.97	2.00	0.00	0.17	0.00
45.64	156.58	2.00	0.00	0.17	0.00	45.65	157.15	2.00	0.00	0.17	0.00
45.66	157.65	2.00	0.00	0.17	0.00	45.67	158.08	2.00	0.00	0.17	0.00
45.68	158.36	2.00	0.00	0.17	0.00	45.69	158.63	2.00	0.00	0.17	0.00
45.70	158.98	2.00	0.00	0.17	0.00	45.71	159.38	2.00	0.00	0.17	0.00
45.72	159.78	2.00	0.00	0.17	0.00	45.73	160.18	2.00	0.00	0.17	0.00
45.74	160.54	2.00	0.00	0.17	0.00	45.75	160.87	2.00	0.00	0.17	0.00
45.76	161.14	2.00	0.00	0.17	0.00	45.77	161.25	0.41	0.28	0.17	0.00
45.78	161.38	0.42	0.28	0.17	0.00	45.79	161.55	0.42	0.27	0.17	0.00
45.80	161.73	0.42	0.27	0.17	0.00	45.81	161.91	0.42	0.27	0.17	0.00
45.82	162.09	0.42	0.27	0.17	0.00	45.83	162.26	0.43	0.27	0.17	0.00
45.84	162.40	0.43	0.26	0.17	0.00	45.85	162.48	0.43	0.26	0.17	0.00
45.86	162.70	0.43	0.26	0.17	0.00	45.87	162.97	0.44	0.26	0.17	0.00
45.88	163.27	0.44	0.26	0.17	0.00	45.89	163.59	0.44	0.25	0.17	0.00
45.90	163.91	0.45	0.25	0.17	0.00	45.91	164.21	0.45	0.25	0.17	0.00
45.92	164.47	0.45	0.24	0.17	0.00	45.93	164.69	0.46	0.24	0.16	0.00
45.94	164.87	0.46	0.24	0.16	0.00	45.95	165.25	0.47	0.24	0.16	0.00
45.96	165.70	0.47	0.23	0.16	0.00	45.97	166.19	0.48	0.23	0.16	0.00
45.98	166.69	0.49	0.23	0.16	0.00	45.99	167.18	0.49	0.22	0.16	0.00
46.00	167.62	0.50	0.22	0.16	0.00	46.01	168.01	0.51	0.21	0.16	0.00
46.02	168.29	0.51	0.21	0.16	0.00	46.03	168.48	0.52	0.21	0.16	0.00
46.04	168.77	0.52	0.21	0.16	0.00	46.05	169.08	0.53	0.21	0.16	0.00
46.06	169.41	0.53	0.20	0.16	0.00	46.07	169.72	0.54	0.20	0.16	0.00
46.08	169.99	0.54	0.20	0.16	0.00	46.09	170.23	0.55	0.20	0.16	0.00
46.10	170.43	0.55	0.19	0.16	0.00	46.11	170.82	0.56	0.19	0.16	0.00
46.12	171.47	0.57	0.19	0.16	0.00	46.13	172.58	0.59	0.18	0.16	0.00
46.14	173.82	0.62	0.17	0.16	0.00	46.15	175.13	0.65	0.16	0.16	0.00
46.16	176.44	0.68	0.16	0.16	0.00	46.17	177.73	0.72	0.15	0.16	0.00
46.18	178.85	0.75	0.14	0.16	0.00	46.19	179.80	0.78	0.14	0.16	0.00
46.20	180.57	0.80	0.13	0.16	0.00	46.21	181.40	0.83	0.13	0.16	0.00
46.22	182.37	0.86	0.13	0.16	0.00	46.23	183.45	0.90	0.12	0.16	0.00
46.24	184.55	0.94	0.12	0.16	0.00	46.25	185.64	0.99	0.11	0.16	0.00
46.26	186.65	1.04	0.10	0.16	0.00	46.27	187.54	1.08	0.10	0.16	0.00
46.28	188.14	1.11	0.09	0.16	0.00	46.29	188.13	1.11	0.09	0.16	0.00
46.30	187.77	1.09	0.09	0.16	0.00	46.31	187.29	1.07	0.10	0.16	0.00
46.32	186.75	1.04	0.10	0.16	0.00	46.33	186.18	1.01	0.11	0.16	0.00
46.34	185.61	0.99	0.11	0.16	0.00	46.35	185.06	0.97	0.11	0.16	0.00
46.36	184.58	0.95	0.11	0.16	0.00	46.37	184.30	0.93	0.11	0.16	0.00
46.38	183.75	0.91	0.12	0.16	0.00	46.39	183.25	0.89	0.12	0.16	0.00
46.40	182.68	0.87	0.12	0.16	0.00	46.41	182.06	0.85	0.12	0.16	0.00
46.42	181.44	0.83	0.13	0.16	0.00	46.43	180.83	0.81	0.13	0.16	0.00
46.44	180.28	0.79	0.13	0.16	0.00	46.45	179.84	2.00	0.00	0.16	0.00
46.46	179.50	2.00	0.00	0.16	0.00	46.47	178.93	2.00	0.00	0.16	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
46.48	178.27	2.00	0.00	0.15	0.00	46.49	177.52	2.00	0.00	0.15	0.00
46.50	176.66	2.00	0.00	0.15	0.00	46.51	175.82	2.00	0.00	0.15	0.00
46.52	175.01	2.00	0.00	0.15	0.00	46.53	174.26	2.00	0.00	0.15	0.00
46.54	173.68	2.00	0.00	0.15	0.00	46.55	172.91	2.00	0.00	0.15	0.00
46.56	171.74	2.00	0.00	0.15	0.00	46.57	170.38	2.00	0.00	0.15	0.00
46.58	168.87	2.00	0.00	0.15	0.00	46.59	167.30	2.00	0.00	0.15	0.00
46.60	165.75	2.00	0.00	0.15	0.00	46.61	164.29	2.00	0.00	0.15	0.00
46.62	163.01	2.00	0.00	0.15	0.00	46.63	162.08	2.00	0.00	0.15	0.00
46.64	161.14	2.00	0.00	0.15	0.00	46.65	159.94	2.00	0.00	0.15	0.00
46.66	158.55	2.00	0.00	0.15	0.00	46.67	157.04	2.00	0.00	0.15	0.00
46.68	155.48	2.00	0.00	0.15	0.00	46.69	153.95	2.00	0.00	0.15	0.00
46.70	152.55	2.00	0.00	0.15	0.00	46.71	151.36	2.00	0.00	0.15	0.00
46.72	150.48	2.00	0.00	0.15	0.00	46.73	149.41	2.00	0.00	0.15	0.00
46.74	148.11	2.00	0.00	0.15	0.00	46.75	146.64	2.00	0.00	0.15	0.00
46.76	145.08	2.00	0.00	0.15	0.00	46.77	143.51	2.00	0.00	0.15	0.00
46.78	142.01	2.00	0.00	0.15	0.00	46.79	140.66	2.00	0.00	0.15	0.00
46.80	139.57	2.00	0.00	0.15	0.00	46.81	138.71	2.00	0.00	0.15	0.00
46.82	137.61	2.00	0.00	0.15	0.00	46.83	136.31	2.00	0.00	0.15	0.00
46.84	134.90	2.00	0.00	0.15	0.00	46.85	133.43	2.00	0.00	0.15	0.00
46.86	131.99	2.00	0.00	0.15	0.00	46.87	130.65	2.00	0.00	0.15	0.00
46.88	60.83	2.00	0.00	0.15	0.00	46.89	60.02	2.00	0.00	0.15	0.00
46.90	59.18	2.00	0.00	0.15	0.00	46.91	58.16	2.00	0.00	0.15	0.00
46.92	56.99	2.00	0.00	0.15	0.00	46.93	55.75	2.00	0.00	0.15	0.00
46.94	54.50	2.00	0.00	0.15	0.00	46.95	53.31	2.00	0.00	0.15	0.00
46.96	52.22	2.00	0.00	0.15	0.00	46.97	51.31	2.00	0.00	0.15	0.00
46.98	50.65	2.00	0.00	0.15	0.00	46.99	49.97	2.00	0.00	0.15	0.00
47.00	49.15	2.00	0.00	0.15	0.00	47.01	48.24	2.00	0.00	0.15	0.00
47.02	47.29	2.00	0.00	0.15	0.00	47.03	46.36	2.00	0.00	0.14	0.00
47.04	45.47	2.00	0.00	0.14	0.00	47.05	44.69	2.00	0.00	0.14	0.00
47.06	44.05	2.00	0.00	0.14	0.00	47.07	43.85	2.00	0.00	0.14	0.00
47.08	43.71	2.00	0.00	0.14	0.00	47.09	43.53	2.00	0.00	0.14	0.00
47.10	43.35	2.00	0.00	0.14	0.00	47.11	43.16	2.00	0.00	0.14	0.00
47.12	42.98	2.00	0.00	0.14	0.00	47.13	42.80	2.00	0.00	0.14	0.00
47.14	42.66	2.00	0.00	0.14	0.00	47.15	42.57	2.00	0.00	0.14	0.00
47.16	42.74	2.00	0.00	0.14	0.00	47.17	42.96	2.00	0.00	0.14	0.00
47.18	43.20	2.00	0.00	0.14	0.00	47.19	43.46	2.00	0.00	0.14	0.00
47.20	43.72	2.00	0.00	0.14	0.00	47.21	43.97	2.00	0.00	0.14	0.00
47.22	44.19	2.00	0.00	0.14	0.00	47.23	44.38	2.00	0.00	0.14	0.00
47.24	44.58	2.00	0.00	0.14	0.00	47.25	44.91	2.00	0.00	0.14	0.00
47.26	45.29	2.00	0.00	0.14	0.00	47.27	45.72	2.00	0.00	0.14	0.00
47.28	46.17	2.00	0.00	0.14	0.00	47.29	46.61	2.00	0.00	0.14	0.00
47.30	47.03	2.00	0.00	0.14	0.00	47.31	47.40	2.00	0.00	0.14	0.00
47.32	47.70	2.00	0.00	0.14	0.00	47.33	47.97	2.00	0.00	0.14	0.00
47.34	48.31	2.00	0.00	0.14	0.00	47.35	48.70	2.00	0.00	0.14	0.00
47.36	49.12	2.00	0.00	0.14	0.00	47.37	49.56	2.00	0.00	0.14	0.00
47.38	49.99	2.00	0.00	0.14	0.00	47.39	50.38	2.00	0.00	0.14	0.00
47.40	50.72	2.00	0.00	0.14	0.00	47.41	50.99	2.00	0.00	0.14	0.00
47.42	51.30	2.00	0.00	0.14	0.00	47.43	51.68	2.00	0.00	0.14	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
47.44	52.12	2.00	0.00	0.14	0.00	47.45	52.58	2.00	0.00	0.14	0.00
47.46	53.05	2.00	0.00	0.14	0.00	47.47	53.50	2.00	0.00	0.14	0.00
47.48	53.90	2.00	0.00	0.14	0.00	47.49	120.85	0.19	0.36	0.14	0.00
47.50	120.97	0.19	0.36	0.14	0.00	47.51	120.97	0.19	0.36	0.14	0.00
47.52	120.98	0.19	0.36	0.14	0.00	47.53	120.99	0.19	0.36	0.14	0.00
47.54	120.99	0.19	0.36	0.14	0.00	47.55	121.00	0.19	0.36	0.14	0.00
47.56	121.00	0.19	0.36	0.14	0.00	47.57	120.99	0.19	0.36	0.14	0.00
47.58	120.99	0.19	0.36	0.13	0.00	47.59	120.85	0.19	0.36	0.13	0.00
47.60	120.66	0.19	0.36	0.13	0.00	47.61	120.44	0.19	0.36	0.13	0.00
47.62	120.20	0.19	0.36	0.13	0.00	47.63	119.96	0.18	0.36	0.13	0.00
47.64	119.72	0.18	0.36	0.13	0.00	47.65	119.50	0.18	0.36	0.13	0.00
47.66	119.30	0.18	0.36	0.13	0.00	47.67	119.22	0.18	0.36	0.13	0.00
47.68	119.65	0.18	0.35	0.13	0.00	47.69	120.17	0.19	0.35	0.13	0.00
47.70	120.76	0.19	0.35	0.13	0.00	47.71	121.38	0.19	0.35	0.13	0.00
47.72	122.00	0.19	0.35	0.13	0.00	47.73	122.59	0.19	0.34	0.13	0.00
47.74	123.13	0.19	0.34	0.13	0.00	47.75	123.57	0.19	0.34	0.13	0.00
47.76	123.74	0.19	0.34	0.13	0.00	47.77	123.76	0.19	0.34	0.13	0.00
47.78	123.79	0.19	0.34	0.13	0.00	47.79	123.82	0.19	0.34	0.13	0.00
47.80	123.85	0.19	0.34	0.13	0.00	47.81	123.88	0.19	0.34	0.13	0.00
47.82	123.91	0.19	0.33	0.13	0.00	47.83	123.93	0.19	0.33	0.13	0.00
47.84	123.98	0.19	0.33	0.13	0.00	47.85	123.58	0.19	0.33	0.13	0.00
47.86	123.05	0.19	0.34	0.13	0.00	47.87	122.43	0.19	0.34	0.13	0.00
47.88	121.77	0.19	0.34	0.13	0.00	47.89	121.09	0.19	0.34	0.13	0.00
47.90	120.43	0.19	0.34	0.13	0.00	47.91	119.82	0.18	0.34	0.13	0.00
47.92	119.31	0.18	0.34	0.13	0.00	47.93	118.96	0.18	0.34	0.13	0.00
47.94	118.78	0.18	0.34	0.13	0.00	47.95	118.55	0.18	0.34	0.13	0.00
47.96	118.30	0.18	0.35	0.13	0.00	47.97	118.03	0.18	0.35	0.13	0.00
47.98	117.75	0.18	0.35	0.13	0.00	47.99	117.48	0.18	0.35	0.13	0.00
48.00	117.23	0.18	0.35	0.13	0.00	48.01	117.04	0.18	0.35	0.13	0.00
48.02	116.80	0.18	0.35	0.13	0.00	48.03	116.39	0.18	0.35	0.13	0.00
48.04	115.90	0.18	0.35	0.13	0.00	48.05	115.36	0.17	0.35	0.13	0.00
48.06	114.80	0.17	0.35	0.13	0.00	48.07	114.23	0.17	0.35	0.13	0.00
48.08	113.69	0.17	0.35	0.13	0.00	48.09	48.30	2.00	0.00	0.13	0.00
48.10	47.91	2.00	0.00	0.13	0.00	48.11	47.59	2.00	0.00	0.13	0.00
48.12	47.20	2.00	0.00	0.13	0.00	48.13	46.74	2.00	0.00	0.12	0.00
48.14	46.25	2.00	0.00	0.12	0.00	48.15	45.75	2.00	0.00	0.12	0.00
48.16	45.27	2.00	0.00	0.12	0.00	48.17	44.82	2.00	0.00	0.12	0.00
48.18	44.44	2.00	0.00	0.12	0.00	48.19	44.18	2.00	0.00	0.12	0.00
48.20	44.05	2.00	0.00	0.12	0.00	48.21	43.89	2.00	0.00	0.12	0.00
48.22	43.72	2.00	0.00	0.12	0.00	48.23	43.53	2.00	0.00	0.12	0.00
48.24	43.35	2.00	0.00	0.12	0.00	48.25	43.17	2.00	0.00	0.12	0.00
48.26	43.01	2.00	0.00	0.12	0.00	48.27	42.88	2.00	0.00	0.12	0.00
48.28	42.95	2.00	0.00	0.12	0.00	48.29	43.19	2.00	0.00	0.12	0.00
48.30	43.48	2.00	0.00	0.12	0.00	48.31	43.81	2.00	0.00	0.12	0.00
48.32	44.14	2.00	0.00	0.12	0.00	48.33	44.47	2.00	0.00	0.12	0.00
48.34	44.78	2.00	0.00	0.12	0.00	48.35	45.05	2.00	0.00	0.12	0.00
48.36	109.19	2.00	0.00	0.12	0.00	48.37	109.56	2.00	0.00	0.12	0.00
48.38	110.07	2.00	0.00	0.12	0.00	48.39	110.64	2.00	0.00	0.12	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
48.40	111.25	2.00	0.00	0.12	0.00	48.41	111.86	2.00	0.00	0.12	0.00
48.42	112.45	2.00	0.00	0.12	0.00	48.43	112.97	2.00	0.00	0.12	0.00
48.44	113.41	2.00	0.00	0.12	0.00	48.45	113.74	2.00	0.00	0.12	0.00
48.46	114.13	2.00	0.00	0.12	0.00	48.47	114.62	2.00	0.00	0.12	0.00
48.48	115.18	2.00	0.00	0.12	0.00	48.49	115.76	2.00	0.00	0.12	0.00
48.50	116.34	2.00	0.00	0.12	0.00	48.51	116.89	2.00	0.00	0.12	0.00
48.52	117.37	2.00	0.00	0.12	0.00	48.53	117.79	2.00	0.00	0.12	0.00
48.54	117.99	0.18	0.32	0.12	0.00	48.55	118.16	0.18	0.32	0.12	0.00
48.56	118.39	0.18	0.32	0.12	0.00	48.57	118.64	0.18	0.31	0.12	0.00
48.58	118.90	0.18	0.31	0.12	0.00	48.59	119.15	0.18	0.31	0.12	0.00
48.60	119.39	0.18	0.31	0.12	0.00	48.61	119.60	0.18	0.31	0.12	0.00
48.62	119.84	2.00	0.00	0.12	0.00	48.63	119.74	2.00	0.00	0.12	0.00
48.64	119.63	2.00	0.00	0.12	0.00	48.65	119.50	2.00	0.00	0.12	0.00
48.66	119.34	2.00	0.00	0.12	0.00	48.67	119.17	2.00	0.00	0.12	0.00
48.68	118.98	2.00	0.00	0.11	0.00	48.69	118.79	2.00	0.00	0.11	0.00
48.70	118.64	2.00	0.00	0.11	0.00	48.71	118.54	2.00	0.00	0.11	0.00
48.72	118.37	2.00	0.00	0.11	0.00	48.73	118.16	2.00	0.00	0.11	0.00
48.74	117.89	2.00	0.00	0.11	0.00	48.75	117.59	2.00	0.00	0.11	0.00
48.76	51.40	2.00	0.00	0.11	0.00	48.77	50.97	2.00	0.00	0.11	0.00
48.78	50.58	2.00	0.00	0.11	0.00	48.79	50.25	2.00	0.00	0.11	0.00
48.80	49.97	2.00	0.00	0.11	0.00	48.81	49.61	2.00	0.00	0.11	0.00
48.82	49.19	2.00	0.00	0.11	0.00	48.83	48.73	2.00	0.00	0.11	0.00
48.84	48.25	2.00	0.00	0.11	0.00	48.85	47.78	2.00	0.00	0.11	0.00
48.86	47.34	2.00	0.00	0.11	0.00	48.87	46.95	2.00	0.00	0.11	0.00
48.88	46.64	2.00	0.00	0.11	0.00	48.89	46.63	2.00	0.00	0.11	0.00
48.90	46.62	2.00	0.00	0.11	0.00	48.91	46.62	2.00	0.00	0.11	0.00
48.92	46.61	2.00	0.00	0.11	0.00	48.93	46.61	2.00	0.00	0.11	0.00
48.94	46.61	2.00	0.00	0.11	0.00	48.95	46.60	2.00	0.00	0.11	0.00
48.96	46.60	2.00	0.00	0.11	0.00	48.97	46.81	2.00	0.00	0.11	0.00
48.98	47.66	2.00	0.00	0.11	0.00	48.99	48.71	2.00	0.00	0.11	0.00
49.00	49.88	2.00	0.00	0.11	0.00	49.01	51.12	2.00	0.00	0.11	0.00
49.02	52.37	2.00	0.00	0.11	0.00	49.03	53.55	2.00	0.00	0.11	0.00
49.04	54.61	2.00	0.00	0.11	0.00	49.05	55.49	2.00	0.00	0.11	0.00
49.06	56.54	2.00	0.00	0.11	0.00	49.07	58.08	2.00	0.00	0.11	0.00
49.08	59.90	2.00	0.00	0.11	0.00	49.09	130.66	2.00	0.00	0.11	0.00
49.10	132.99	2.00	0.00	0.11	0.00	49.11	135.27	2.00	0.00	0.11	0.00
49.12	137.38	2.00	0.00	0.11	0.00	49.13	139.22	2.00	0.00	0.11	0.00
49.14	140.63	2.00	0.00	0.11	0.00	49.15	142.44	2.00	0.00	0.11	0.00
49.16	144.75	2.00	0.00	0.11	0.00	49.17	147.38	2.00	0.00	0.11	0.00
49.18	150.17	2.00	0.00	0.11	0.00	49.19	152.98	2.00	0.00	0.11	0.00
49.20	155.65	2.00	0.00	0.11	0.00	49.21	158.07	2.00	0.00	0.11	0.00
49.22	160.09	2.00	0.00	0.11	0.00	49.23	161.61	2.00	0.00	0.10	0.00
49.24	163.40	2.00	0.00	0.10	0.00	49.25	165.62	2.00	0.00	0.10	0.00
49.26	168.06	2.00	0.00	0.10	0.00	49.27	170.59	2.00	0.00	0.10	0.00
49.28	173.14	2.00	0.00	0.10	0.00	49.29	175.46	2.00	0.00	0.10	0.00
49.30	177.50	2.00	0.00	0.10	0.00	49.31	179.20	2.00	0.00	0.10	0.00
49.32	180.18	2.00	0.00	0.10	0.00	49.33	181.32	2.00	0.00	0.10	0.00
49.34	182.70	2.00	0.00	0.10	0.00	49.35	184.20	2.00	0.00	0.10	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
49.36	185.75	2.00	0.00	0.10	0.00	49.37	187.26	2.00	0.00	0.10	0.00
49.38	188.66	2.00	0.00	0.10	0.00	49.39	189.87	2.00	0.00	0.10	0.00
49.40	190.88	2.00	0.00	0.10	0.00	49.41	191.53	1.29	0.04	0.10	0.00
49.42	192.47	1.35	0.04	0.10	0.00	49.43	193.54	1.42	0.03	0.10	0.00
49.44	194.68	1.50	0.02	0.10	0.00	49.45	195.85	1.60	0.02	0.10	0.00
49.46	196.98	1.69	0.01	0.10	0.00	49.47	198.02	1.79	0.01	0.10	0.00
49.48	198.87	1.87	0.01	0.10	0.00	49.49	199.24	1.91	0.00	0.10	0.00
49.50	199.15	1.90	0.00	0.10	0.00	49.51	198.97	1.88	0.00	0.10	0.00
49.52	198.76	1.86	0.01	0.10	0.00	49.53	198.51	1.83	0.01	0.10	0.00
49.54	198.23	1.81	0.01	0.10	0.00	49.55	197.95	1.78	0.01	0.10	0.00
49.56	197.67	1.75	0.01	0.10	0.00	49.57	197.41	1.73	0.01	0.10	0.00
49.58	196.76	1.67	0.01	0.10	0.00	49.59	195.82	1.59	0.02	0.10	0.00
49.60	194.71	1.50	0.02	0.10	0.00	49.61	193.46	1.41	0.03	0.10	0.00
49.62	192.13	1.33	0.04	0.10	0.00	49.63	190.79	1.24	0.04	0.10	0.00
49.64	189.50	1.17	0.05	0.10	0.00	49.65	188.36	1.11	0.06	0.10	0.00
49.66	187.61	1.08	0.06	0.10	0.00	49.67	187.12	1.05	0.06	0.10	0.00
49.68	186.80	1.04	0.06	0.10	0.00	49.69	186.44	1.02	0.07	0.10	0.00
49.70	186.04	1.00	0.07	0.10	0.00	49.71	185.64	0.99	0.07	0.10	0.00
49.72	185.25	0.97	0.07	0.10	0.00	49.73	184.90	0.95	0.07	0.10	0.00
49.74	184.59	0.94	0.07	0.10	0.00	49.75	184.36	0.93	0.07	0.10	0.00
49.76	184.08	0.92	0.07	0.10	0.00	49.77	183.74	0.91	0.07	0.10	0.00
49.78	183.35	0.89	0.07	0.09	0.00	49.79	182.95	0.88	0.07	0.09	0.00
49.80	182.55	0.86	0.07	0.09	0.00	49.81	182.16	0.85	0.07	0.09	0.00
49.82	181.82	0.84	0.08	0.09	0.00	49.83	181.63	0.83	0.08	0.09	0.00
49.84	181.36	0.82	0.08	0.09	0.00	49.85	180.98	0.81	0.08	0.09	0.00
49.86	180.54	0.80	0.08	0.09	0.00	49.87	180.06	0.78	0.08	0.09	0.00
49.88	179.53	0.76	0.08	0.09	0.00	49.89	178.99	0.75	0.08	0.09	0.00
49.90	178.47	0.73	0.08	0.09	0.00	49.91	178.01	0.72	0.09	0.09	0.00
49.92	177.63	0.71	0.09	0.09	0.00	49.93	177.35	0.70	0.09	0.09	0.00
49.94	176.91	0.69	0.09	0.09	0.00	49.95	176.40	0.68	0.09	0.09	0.00
49.96	175.86	0.66	0.09	0.09	0.00	49.97	175.30	0.65	0.09	0.09	0.00
49.98	174.76	0.64	0.09	0.09	0.00	49.99	174.25	0.63	0.10	0.09	0.00
50.00	173.76	0.62	0.10	0.09	0.00						

Total estimated settlement: 0.66**Abbreviations**

$Q_{tn,cs}$:	Equivalent clean sand normalized cone resistance
FS:	Factor of safety against liquefaction
e_v (%):	Post-liquefaction volumetric strain
DF:	e_v depth weighting factor
Settlement:	Calculated settlement

:: Strength loss calculation Idriss & Boulanger (2008) ::

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.01	30.91	49.66	1.76	87.50	2.25	0.10	0.76
0.02	30.75	49.40	1.75	86.63	2.25	0.10	0.76
0.03	30.52	49.03	1.74	85.42	2.25	0.10	0.76
0.04	30.24	48.58	1.74	84.36	2.24	0.10	0.76
0.05	29.79	47.86	1.74	83.32	2.25	0.10	0.75
0.06	29.13	46.79	1.76	82.16	2.25	0.10	0.75
0.07	28.30	45.46	1.78	80.81	2.26	0.10	0.75
0.08	27.40	44.01	1.80	79.35	2.27	0.10	0.75
0.09	26.46	42.51	1.83	77.86	2.27	0.10	0.74
0.10	25.55	41.03	1.86	76.42	2.28	0.09	0.74
0.11	24.69	39.66	1.89	75.09	2.29	0.09	0.74
0.12	23.95	38.47	1.92	73.96	2.30	0.09	0.74
0.13	23.54	37.81	1.95	73.58	2.31	0.09	0.73
0.14	23.44	37.64	1.97	74.00	2.31	0.09	0.73
0.15	23.59	37.89	1.98	75.16	2.32	0.09	0.73
0.16	23.77	38.18	2.00	76.49	2.32	0.09	0.74
0.17	23.97	38.49	2.02	77.92	2.33	0.09	0.74
0.18	24.16	38.80	2.05	79.38	2.33	0.09	0.74
0.19	24.35	39.11	2.07	80.78	2.34	0.10	0.74
0.20	24.52	39.38	2.08	82.07	2.34	0.10	0.74
0.21	24.72	39.69	2.10	83.21	2.34	0.10	0.74
0.22	25.06	40.24	2.10	84.40	2.34	0.10	0.74
0.23	25.60	41.11	2.09	85.80	2.34	0.10	0.74
0.24	26.34	42.29	2.07	87.52	2.34	0.10	0.75
0.25	27.16	43.61	2.05	89.46	2.33	0.10	0.75
0.26	28.03	45.00	2.03	91.52	2.33	0.10	0.75
0.27	28.89	46.39	2.02	93.59	2.32	0.11	0.76
0.28	29.71	47.71	2.00	95.56	2.32	0.11	0.76
0.29	30.44	48.88	1.99	97.33	2.32	0.11	0.76
0.30	31.08	49.91	1.98	98.77	2.31	0.11	0.76
0.31	31.72	50.93	1.96	99.99	2.31	0.11	0.76
0.32	32.43	52.08	1.94	101.16	2.30	0.11	0.77
0.33	33.28	53.44	1.92	102.50	2.30	0.11	0.77
0.34	34.20	54.91	1.89	103.98	2.29	0.12	0.77
0.35	35.15	56.44	1.87	105.51	2.28	0.12	0.78
0.36	36.09	57.94	1.85	107.04	2.28	0.12	0.78
0.37	36.95	59.34	1.83	108.47	2.27	0.12	0.78
0.38	37.71	60.55	1.81	109.72	2.27	0.12	0.78
0.39	38.38	61.62	1.80	110.71	2.26	0.12	0.78
0.40	39.04	62.69	1.78	111.55	2.26	0.13	0.79
0.41	39.80	63.91	1.76	112.40	2.25	0.13	0.79
0.42	40.67	65.31	1.74	113.38	2.24	0.13	0.79
0.43	41.60	66.80	1.71	114.44	2.24	0.13	0.79
0.44	42.55	68.32	1.69	115.54	2.23	0.13	0.79
0.45	43.46	69.78	1.67	116.61	2.22	0.13	0.80
0.46	44.29	71.11	1.65	117.60	2.22	0.14	0.80
0.47	44.98	72.23	1.64	118.47	2.21	0.14	0.80
0.48	45.59	73.21	1.63	119.29	2.21	0.14	0.80

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.49	46.19	74.17	1.62	120.18	2.20	0.14	0.80
0.50	46.87	75.26	1.61	121.24	2.20	0.14	0.81
0.51	47.63	76.48	1.60	122.43	2.19	0.14	0.81
0.52	48.43	77.76	1.59	123.68	2.19	0.15	0.81
0.53	49.22	79.04	1.58	124.94	2.19	0.15	0.81
0.54	49.98	80.25	1.57	126.14	2.18	0.15	0.81
0.55	50.65	81.32	1.56	127.21	2.18	0.15	0.81
0.56	51.19	82.20	1.56	128.11	2.18	0.15	0.82
0.57	51.66	82.95	1.55	128.92	2.17	0.15	0.82
0.58	52.12	83.69	1.55	129.76	2.17	0.16	0.82
0.59	52.64	84.52	1.55	130.72	2.17	0.16	0.82
0.60	53.21	85.44	1.54	131.78	2.17	0.16	0.82
0.61	53.80	86.38	1.54	132.87	2.17	0.16	0.82
0.62	54.37	87.30	1.53	133.95	2.17	0.16	0.82
0.63	54.91	88.16	1.53	134.95	2.16	0.16	0.82
0.64	55.37	88.90	1.53	135.81	2.16	0.17	0.83
0.65	55.71	89.45	1.53	136.45	2.16	0.17	0.83
0.66	55.98	89.88	1.52	136.93	2.16	0.17	0.83
0.67	56.22	90.26	1.52	137.34	2.16	0.17	0.83
0.68	56.49	90.69	1.52	137.81	2.16	0.17	0.83
0.69	56.78	91.16	1.52	138.31	2.16	0.17	0.83
0.70	57.07	91.63	1.52	138.83	2.16	0.17	0.83
0.71	57.35	92.08	1.51	139.32	2.15	0.17	0.83
0.72	57.61	92.49	1.51	139.77	2.15	0.17	0.83
0.73	57.82	92.82	1.51	140.12	2.15	0.17	0.83
0.74	57.97	93.07	1.51	140.35	2.15	0.18	0.83
0.75	58.09	93.25	1.51	140.48	2.15	0.18	0.83
0.76	58.20	93.44	1.50	140.58	2.15	0.18	0.83
0.77	58.33	93.64	1.50	140.68	2.15	0.18	0.83
0.78	58.46	93.85	1.50	140.79	2.15	0.18	0.83
0.79	58.59	94.06	1.50	140.90	2.15	0.18	0.83
0.80	58.72	94.26	1.50	141.01	2.15	0.18	0.83
0.81	58.83	94.44	1.49	141.11	2.14	0.18	0.83
0.82	58.92	94.59	1.49	141.17	2.14	0.18	0.83
0.83	59.00	94.72	1.49	141.20	2.14	0.18	0.83
0.84	59.08	94.85	1.49	141.20	2.14	0.18	0.83
0.85	59.18	95.00	1.49	141.19	2.14	0.18	0.83
0.86	59.28	95.17	1.48	141.18	2.14	0.18	0.83
0.87	59.39	95.34	1.48	141.18	2.14	0.18	0.83
0.88	59.49	95.50	1.48	141.17	2.14	0.18	0.83
0.89	59.59	95.66	1.48	141.17	2.13	0.18	0.83
0.90	59.68	95.79	1.47	141.17	2.13	0.18	0.83
0.91	59.76	95.93	1.47	141.19	2.13	0.18	0.83
0.92	59.87	96.10	1.47	141.22	2.13	0.18	0.83
0.93	60.00	96.30	1.47	141.29	2.13	0.18	0.83
0.94	60.14	96.54	1.46	141.36	2.13	0.18	0.83
0.95	60.30	96.79	1.46	141.44	2.13	0.18	0.83
0.96	60.46	97.05	1.46	141.52	2.12	0.18	0.83

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.97	60.62	97.30	1.46	141.60	2.12	0.18	0.83
0.98	60.76	97.52	1.45	141.68	2.12	0.18	0.84
0.99	60.90	97.74	1.45	141.76	2.12	0.18	0.84
1.00	61.09	98.05	1.45	141.89	2.12	0.18	0.84
1.01	61.36	98.49	1.44	142.10	2.12	0.18	0.84
1.02	61.72	99.07	1.44	142.38	2.11	0.18	0.84
1.03	62.12	99.70	1.43	142.70	2.11	0.18	0.84
1.04	62.53	100.37	1.43	143.04	2.10	0.19	0.84
1.05	62.94	101.03	1.42	143.38	2.10	0.19	0.84
1.06	63.33	101.65	1.41	143.71	2.10	0.19	0.84
1.07	63.68	102.21	1.41	144.00	2.09	0.19	0.84
1.08	63.97	102.67	1.40	144.22	2.09	0.19	0.84
1.09	64.23	103.10	1.40	144.38	2.09	0.19	0.84
1.10	64.51	103.54	1.40	144.49	2.08	0.19	0.84
1.11	64.83	104.06	1.39	144.62	2.08	0.19	0.84
1.12	65.18	104.62	1.38	144.77	2.07	0.19	0.84
1.13	65.54	105.20	1.38	144.92	2.07	0.19	0.84
1.14	65.90	105.76	1.37	145.09	2.06	0.19	0.84
1.15	66.22	106.29	1.37	145.25	2.06	0.19	0.84
1.16	66.50	106.74	1.36	145.38	2.06	0.19	0.84
1.17	66.72	107.09	1.36	145.44	2.05	0.19	0.84
1.18	66.91	107.38	1.35	145.43	2.05	0.19	0.84
1.19	67.09	107.67	1.35	145.36	2.05	0.19	0.84
1.20	67.30	108.01	1.35	145.28	2.04	0.19	0.84
1.21	67.52	108.36	1.34	145.21	2.04	0.19	0.84
1.22	67.74	108.72	1.34	145.14	2.03	0.19	0.84
1.23	67.96	109.06	1.33	145.08	2.03	0.19	0.84
1.24	68.15	109.37	1.33	145.03	2.02	0.19	0.84
1.25	68.30	109.61	1.32	144.99	2.02	0.19	0.84
1.26	68.38	109.75	1.32	144.95	2.02	0.19	0.84
1.27	68.42	109.80	1.32	144.88	2.01	0.19	0.84
1.28	68.43	109.82	1.32	144.80	2.01	0.19	0.84
1.29	68.44	109.84	1.32	144.70	2.01	0.19	0.84
1.30	68.45	109.86	1.32	144.61	2.01	0.19	0.84
1.31	68.47	109.88	1.32	144.51	2.01	0.19	0.84
1.32	68.48	109.90	1.31	144.42	2.01	0.19	0.84
1.33	68.49	109.91	1.31	144.34	2.01	0.19	0.84
1.34	68.46	109.87	1.31	144.27	2.01	0.19	0.84
1.35	68.38	109.73	1.31	144.19	2.01	0.19	0.84
1.36	68.22	109.48	1.32	144.10	2.01	0.19	0.84
1.37	68.03	109.17	1.32	143.99	2.01	0.19	0.84
1.38	67.82	108.83	1.32	143.87	2.02	0.19	0.84
1.39	67.61	108.49	1.33	143.75	2.02	0.19	0.84
1.40	67.40	108.15	1.33	143.64	2.02	0.19	0.84
1.41	67.21	107.84	1.33	143.54	2.03	0.19	0.84
1.42	67.05	107.58	1.33	143.46	2.03	0.19	0.84
1.43	66.95	107.42	1.34	143.47	2.03	0.19	0.84
1.44	66.90	107.35	1.34	143.57	2.03	0.19	0.84

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
1.45	66.89	107.33	1.34	143.75	2.04	0.19	0.84
1.46	66.88	107.31	1.34	143.97	2.04	0.19	0.84
1.47	66.86	107.29	1.34	144.19	2.04	0.19	0.84
1.48	66.85	107.26	1.35	144.43	2.04	0.19	0.84
1.49	66.84	107.24	1.35	144.65	2.04	0.19	0.84
1.50	66.83	107.22	1.35	144.86	2.05	0.19	0.84
1.51	66.82	107.20	1.35	145.03	2.05	0.19	0.84
1.52	66.80	107.18	1.35	145.16	2.05	0.19	0.84
1.53	66.78	107.15	1.36	145.28	2.05	0.19	0.84
1.54	66.76	107.11	1.36	145.42	2.05	0.19	0.84
1.55	66.73	107.07	1.36	145.56	2.05	0.19	0.84
1.56	66.71	107.03	1.36	145.72	2.06	0.19	0.84
1.57	66.68	106.98	1.36	145.87	2.06	0.19	0.84
1.58	66.66	106.94	1.37	146.02	2.06	0.20	0.84
1.59	66.64	106.91	1.37	146.15	2.06	0.20	0.84
1.60	66.58	106.82	1.37	146.19	2.06	0.20	0.84
1.61	66.47	106.64	1.37	146.09	2.06	0.20	0.84
1.62	66.29	106.35	1.37	145.86	2.06	0.19	0.84
1.63	66.08	106.00	1.37	145.57	2.07	0.19	0.84
1.64	65.84	105.63	1.38	145.26	2.07	0.19	0.84
1.65	65.60	105.24	1.38	144.94	2.07	0.19	0.84
1.66	65.37	104.86	1.38	144.63	2.07	0.19	0.84
1.67	65.15	104.51	1.38	144.35	2.07	0.19	0.84
1.68	64.96	104.21	1.38	144.10	2.07	0.19	0.84
1.69	64.80	103.94	1.38	143.86	2.07	0.19	0.84
1.70	64.63	103.67	1.39	143.60	2.08	0.19	0.84
1.71	64.43	103.35	1.39	143.28	2.08	0.19	0.84
1.72	64.21	102.99	1.39	142.93	2.08	0.19	0.84
1.73	63.97	102.61	1.39	142.55	2.08	0.19	0.84
1.74	63.73	102.22	1.39	142.16	2.08	0.19	0.84
1.75	63.50	101.85	1.39	141.80	2.08	0.19	0.84
1.76	63.29	101.52	1.39	141.47	2.08	0.18	0.84
1.77	63.11	101.22	1.39	141.16	2.08	0.18	0.84
1.78	62.91	100.90	1.40	140.80	2.08	0.18	0.84
1.79	62.68	100.53	1.40	140.34	2.08	0.18	0.83
1.80	62.40	100.08	1.40	139.77	2.08	0.18	0.83
1.81	62.09	99.58	1.40	139.14	2.08	0.18	0.83
1.82	61.76	99.05	1.40	138.49	2.09	0.18	0.83
1.83	61.44	98.53	1.40	137.83	2.09	0.18	0.83
1.84	61.13	98.04	1.40	137.22	2.09	0.18	0.83
1.85	60.87	97.61	1.40	136.68	2.09	0.17	0.83
1.86	60.62	97.21	1.40	136.19	2.09	0.17	0.83
1.87	60.34	96.77	1.40	135.66	2.09	0.17	0.83
1.88	60.02	96.24	1.40	135.03	2.09	0.17	0.83
1.89	59.63	95.63	1.40	134.30	2.09	0.17	0.83
1.90	59.22	94.96	1.41	133.51	2.09	0.17	0.83
1.91	58.79	94.27	1.41	132.70	2.09	0.17	0.83
1.92	58.37	93.60	1.41	131.91	2.09	0.17	0.83

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
1.93	57.99	92.98	1.41	131.18	2.09	0.16	0.82
1.94	57.65	92.44	1.41	130.56	2.10	0.16	0.82
1.95	57.33	91.93	1.41	130.00	2.10	0.16	0.82
1.96	56.98	91.36	1.42	129.43	2.10	0.16	0.82
1.97	56.56	90.68	1.42	128.78	2.10	0.16	0.82
1.98	56.08	89.91	1.42	128.04	2.10	0.16	0.82
1.99	55.57	89.09	1.43	127.26	2.11	0.16	0.82
2.00	55.06	88.27	1.43	126.48	2.11	0.16	0.82
2.01	54.57	87.47	1.44	125.74	2.11	0.16	0.82
2.02	54.12	86.76	1.44	125.07	2.11	0.15	0.82
2.03	53.73	86.13	1.45	124.48	2.12	0.15	0.82
2.04	53.34	85.51	1.45	123.90	2.12	0.15	0.82
2.05	52.90	84.79	1.45	123.23	2.12	0.15	0.81
2.06	52.37	83.94	1.46	122.45	2.13	0.15	0.81
2.07	51.78	82.99	1.46	121.58	2.13	0.15	0.81
2.08	51.17	82.01	1.47	120.68	2.13	0.15	0.81
2.09	50.56	81.03	1.48	119.80	2.14	0.15	0.81
2.10	49.99	80.11	1.49	118.97	2.14	0.14	0.81
2.11	49.49	79.30	1.49	118.24	2.14	0.14	0.81
2.12	49.07	78.64	1.50	117.63	2.15	0.14	0.81
2.13	48.71	78.05	1.50	117.03	2.15	0.14	0.81
2.14	48.33	77.44	1.50	116.37	2.15	0.14	0.80
2.15	47.89	76.74	1.51	115.61	2.15	0.14	0.80
2.16	47.43	75.99	1.51	114.79	2.15	0.14	0.80
2.17	46.94	75.21	1.52	113.96	2.16	0.14	0.80
2.18	46.48	74.46	1.52	113.14	2.16	0.14	0.80
2.19	46.05	73.77	1.52	112.40	2.16	0.13	0.80
2.20	45.68	73.18	1.53	111.76	2.16	0.13	0.80
2.21	45.37	72.69	1.53	111.23	2.16	0.13	0.80
2.22	45.09	72.23	1.53	110.72	2.16	0.13	0.80
2.23	44.79	71.74	1.54	110.17	2.17	0.13	0.80
2.24	44.44	71.19	1.54	109.55	2.17	0.13	0.79
2.25	44.08	70.60	1.54	108.89	2.17	0.13	0.79
2.26	43.71	70.01	1.55	108.23	2.17	0.13	0.79
2.27	43.36	69.45	1.55	107.59	2.17	0.13	0.79
2.28	43.04	68.94	1.55	107.02	2.17	0.13	0.79
2.29	42.78	68.51	1.56	106.54	2.17	0.13	0.79
2.30	42.53	68.12	1.56	106.10	2.18	0.13	0.79
2.31	42.28	67.71	1.56	105.64	2.18	0.13	0.79
2.32	41.99	67.24	1.56	105.11	2.18	0.13	0.79
2.33	41.67	66.72	1.57	104.52	2.18	0.12	0.79
2.34	41.33	66.18	1.57	103.91	2.18	0.12	0.79
2.35	41.00	65.65	1.57	103.31	2.18	0.12	0.79
2.36	40.69	65.14	1.58	102.75	2.18	0.12	0.79
2.37	40.41	64.70	1.58	102.25	2.19	0.12	0.78
2.38	40.19	64.34	1.58	101.84	2.19	0.12	0.78
2.39	39.98	64.01	1.59	101.45	2.19	0.12	0.78
2.40	39.77	63.66	1.59	101.05	2.19	0.12	0.78

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
2.41	39.52	63.26	1.59	100.58	2.19	0.12	0.78
2.42	39.25	62.84	1.59	100.07	2.19	0.12	0.78
2.43	38.98	62.40	1.60	99.55	2.19	0.12	0.78
2.44	38.72	61.97	1.60	99.05	2.19	0.12	0.78
2.45	38.47	61.58	1.60	98.59	2.19	0.12	0.78
2.46	38.26	61.24	1.60	98.20	2.20	0.12	0.78
2.47	38.08	60.94	1.61	97.89	2.20	0.12	0.78
2.48	37.89	60.63	1.61	97.62	2.20	0.12	0.78
2.49	37.67	60.28	1.61	97.34	2.20	0.12	0.78
2.50	37.42	59.88	1.62	97.03	2.20	0.12	0.78
2.51	37.16	59.46	1.63	96.71	2.20	0.12	0.78
2.52	36.90	59.04	1.63	96.38	2.21	0.12	0.77
2.53	36.64	58.63	1.64	96.07	2.21	0.11	0.77
2.54	36.42	58.27	1.64	95.79	2.21	0.11	0.77
2.55	36.21	57.94	1.65	95.53	2.21	0.11	0.77
2.56	35.99	57.58	1.65	95.23	2.22	0.11	0.77
2.57	35.73	57.15	1.66	94.85	2.22	0.11	0.77
2.58	35.41	56.64	1.67	94.39	2.22	0.11	0.77
2.59	35.05	56.07	1.67	93.88	2.22	0.11	0.77
2.60	34.68	55.48	1.68	93.36	2.23	0.11	0.77
2.61	34.32	54.89	1.69	92.84	2.23	0.11	0.77
2.62	33.98	54.34	1.70	92.36	2.23	0.11	0.77
2.63	33.68	53.86	1.71	91.94	2.23	0.11	0.77
2.64	33.42	53.44	1.71	91.56	2.24	0.11	0.77
2.65	33.17	53.04	1.72	91.17	2.24	0.11	0.77
2.66	32.89	52.58	1.73	90.71	2.24	0.11	0.76
2.67	32.56	52.06	1.73	90.18	2.24	0.11	0.76
2.68	32.21	51.49	1.74	89.61	2.25	0.11	0.76
2.69	31.85	50.91	1.75	89.02	2.25	0.11	0.76
2.70	31.50	50.34	1.76	88.46	2.25	0.11	0.76
2.71	31.17	49.83	1.77	87.95	2.25	0.11	0.76
2.72	30.91	49.41	1.77	87.52	2.26	0.10	0.76
2.73	30.75	49.15	1.77	87.22	2.26	0.10	0.76
2.74	30.68	49.03	1.77	87.01	2.26	0.10	0.76
2.75	30.65	48.98	1.77	86.84	2.26	0.10	0.76
2.76	30.62	48.93	1.77	86.64	2.26	0.10	0.76
2.77	30.59	48.88	1.77	86.43	2.25	0.10	0.76
2.78	30.56	48.83	1.77	86.21	2.25	0.10	0.76
2.79	30.53	48.78	1.76	86.01	2.25	0.10	0.76
2.80	30.50	48.74	1.76	85.83	2.25	0.10	0.76
2.81	30.48	48.70	1.76	85.68	2.25	0.10	0.76
2.82	30.46	48.66	1.76	85.53	2.25	0.10	0.76
2.83	30.44	48.63	1.76	85.38	2.25	0.10	0.76
2.84	30.41	48.59	1.75	85.20	2.25	0.10	0.76
2.85	30.39	48.55	1.75	85.00	2.25	0.10	0.76
2.86	30.36	48.51	1.75	84.80	2.25	0.10	0.76
2.87	30.33	48.46	1.75	84.59	2.25	0.10	0.76
2.88	30.31	48.42	1.74	84.40	2.25	0.10	0.76

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
2.89	30.29	48.39	1.74	84.24	2.25	0.10	0.76
2.90	30.25	48.33	1.74	84.04	2.25	0.10	0.76
2.91	30.20	48.24	1.74	83.78	2.24	0.10	0.75
2.92	30.11	48.11	1.73	83.41	2.24	0.10	0.75
2.93	30.02	47.95	1.73	82.99	2.24	0.10	0.75
2.94	29.91	47.78	1.73	82.53	2.24	0.10	0.75
2.95	29.81	47.61	1.72	82.06	2.24	0.10	0.75
2.96	29.70	47.44	1.72	81.61	2.24	0.10	0.75
2.97	29.61	47.29	1.72	81.20	2.24	0.10	0.75
2.98	29.50	47.11	1.72	80.81	2.24	0.10	0.75
2.99	29.28	46.76	1.72	80.33	2.24	0.10	0.75
3.00	28.92	46.18	1.73	79.69	2.24	0.10	0.75
3.01	28.41	45.35	1.74	78.84	2.25	0.10	0.75
3.02	27.83	44.43	1.75	77.90	2.25	0.10	0.75
3.03	27.22	43.45	1.77	76.91	2.26	0.10	0.74
3.04	26.61	42.47	1.79	75.93	2.26	0.10	0.74
3.05	26.03	41.53	1.81	75.00	2.27	0.09	0.74
3.06	25.51	40.69	1.82	74.18	2.27	0.09	0.74
3.07	25.05	39.95	1.84	73.51	2.28	0.09	0.74
3.08	24.59	39.22	1.86	72.96	2.28	0.09	0.74
3.09	24.08	38.40	1.89	72.44	2.29	0.09	0.74
3.10	23.47	37.42	1.92	71.88	2.30	0.09	0.73
3.11	22.80	36.35	1.96	71.28	2.31	0.09	0.73
3.12	22.11	35.23	2.01	70.67	2.32	0.09	0.73
3.13	21.43	34.13	2.05	70.09	2.33	0.09	0.73
3.14	20.79	33.10	2.10	69.56	2.34	0.09	0.73
3.15	20.23	32.20	2.15	69.11	2.35	0.09	0.72
3.16	19.88	31.64	2.18	68.84	2.36	0.09	0.72
3.17	19.72	31.38	2.19	68.72	2.36	0.09	0.72
3.18	19.71	31.37	2.19	68.71	2.36	0.09	0.72
3.19	19.71	31.37	2.19	68.71	2.36	0.09	0.72
3.20	19.71	31.37	2.19	68.71	2.36	0.09	0.72
3.21	19.71	31.37	2.19	68.71	2.36	0.09	0.72
3.22	19.71	31.37	2.19	68.71	2.36	0.09	0.72
3.23	19.71	31.37	2.19	68.71	2.36	0.09	0.72
3.24	19.72	31.37	2.19	68.70	2.36	0.09	0.72
3.25	19.74	31.41	2.19	68.64	2.36	0.09	0.72
3.26	19.79	31.48	2.18	68.52	2.36	0.09	0.72
3.27	19.85	31.59	2.16	68.34	2.36	0.09	0.72
3.28	19.93	31.71	2.15	68.14	2.35	0.09	0.72
3.29	20.01	31.84	2.13	67.93	2.35	0.09	0.72
3.30	20.09	31.96	2.12	67.72	2.35	0.09	0.72
3.31	20.16	32.08	2.10	67.52	2.34	0.09	0.72
3.32	20.23	32.19	2.09	67.34	2.34	0.09	0.72
3.33	20.28	32.27	2.08	67.17	2.34	0.09	0.72
3.34	20.30	32.31	2.07	67.00	2.34	0.09	0.72
3.35	20.31	32.32	2.07	66.80	2.34	0.09	0.72
3.36	20.31	32.32	2.06	66.56	2.33	0.09	0.72

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
3.37	20.31	32.32	2.05	66.30	2.33	0.09	0.72
3.38	20.31	32.31	2.04	66.02	2.33	0.09	0.72
3.39	20.31	32.31	2.03	65.75	2.33	0.09	0.72
3.40	20.31	32.31	2.03	65.50	2.33	0.09	0.72
3.41	20.31	32.31	2.02	65.28	2.32	0.09	0.72
3.42	20.31	32.31	2.02	65.16	2.32	0.09	0.72
3.43	20.31	32.31	2.02	65.14	2.32	0.09	0.72
3.44	20.31	32.31	2.02	65.21	2.32	0.09	0.72
3.45	20.31	32.31	2.02	65.30	2.32	0.09	0.72
3.46	20.31	32.31	2.02	65.39	2.33	0.09	0.72
3.47	20.31	32.31	2.03	65.48	2.33	0.09	0.72
3.48	20.31	32.31	2.03	65.57	2.33	0.09	0.72
3.49	20.31	32.30	2.03	65.65	2.33	0.09	0.72
3.50	20.32	32.32	2.03	65.73	2.33	0.09	0.72
3.51	20.37	32.39	2.03	65.86	2.33	0.09	0.72
3.52	20.46	32.54	2.03	66.06	2.33	0.09	0.72
3.53	20.59	32.76	2.02	66.32	2.33	0.09	0.72
3.54	20.75	33.00	2.02	66.62	2.32	0.09	0.72
3.55	20.90	33.25	2.01	66.93	2.32	0.09	0.72
3.56	21.06	33.51	2.01	67.25	2.32	0.09	0.73
3.57	21.22	33.75	2.00	67.55	2.32	0.09	0.73
3.58	21.35	33.97	2.00	67.82	2.32	0.09	0.73
3.59	21.48	34.17	1.99	68.01	2.32	0.09	0.73
3.60	21.62	34.40	1.98	68.11	2.31	0.09	0.73
3.61	21.79	34.68	1.97	68.15	2.31	0.09	0.73
3.62	22.01	35.02	1.95	68.18	2.31	0.09	0.73
3.63	22.24	35.39	1.93	68.20	2.30	0.09	0.73
3.64	22.48	35.77	1.91	68.24	2.30	0.09	0.73
3.65	22.71	36.15	1.89	68.27	2.29	0.09	0.73
3.66	22.93	36.51	1.87	68.31	2.29	0.09	0.73
3.67	23.13	36.81	1.86	68.34	2.28	0.09	0.73
3.68	23.28	37.06	1.84	68.36	2.28	0.09	0.73
3.69	23.41	37.27	1.83	68.35	2.27	0.09	0.73
3.70	23.54	37.47	1.82	68.33	2.27	0.09	0.73
3.71	23.68	37.70	1.81	68.31	2.27	0.09	0.73
3.72	23.84	37.96	1.80	68.29	2.26	0.09	0.73
3.73	24.00	38.21	1.79	68.27	2.26	0.09	0.73
3.74	24.15	38.46	1.77	68.25	2.26	0.09	0.73
3.75	24.30	38.69	1.76	68.23	2.25	0.09	0.73
3.76	24.42	38.89	1.76	68.25	2.25	0.09	0.73
3.77	24.56	39.10	1.75	68.37	2.25	0.09	0.73
3.78	24.72	39.36	1.74	68.61	2.25	0.09	0.73
3.79	24.92	39.69	1.74	68.97	2.24	0.09	0.73
3.80	25.15	40.05	1.73	69.36	2.24	0.09	0.74
3.81	25.39	40.44	1.73	69.78	2.24	0.09	0.74
3.82	25.63	40.82	1.72	70.20	2.24	0.09	0.74
3.83	25.85	41.18	1.71	70.60	2.24	0.09	0.74
3.84	26.06	41.51	1.71	70.96	2.24	0.09	0.74

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
3.85	26.28	41.87	1.70	71.32	2.23	0.09	0.74
3.86	26.59	42.37	1.69	71.77	2.23	0.09	0.74
3.87	27.04	43.08	1.68	72.38	2.23	0.09	0.74
3.88	27.58	43.95	1.66	73.12	2.22	0.09	0.74
3.89	28.17	44.90	1.65	73.95	2.21	0.10	0.74
3.90	28.78	45.88	1.63	74.82	2.21	0.10	0.75
3.91	29.39	46.85	1.62	75.68	2.20	0.10	0.75
3.92	29.95	47.75	1.60	76.49	2.19	0.10	0.75
3.93	30.44	48.54	1.59	77.20	2.19	0.10	0.75
3.94	30.83	49.17	1.58	77.74	2.19	0.10	0.75
3.95	31.19	49.74	1.57	78.16	2.18	0.10	0.75
3.96	31.55	50.32	1.56	78.54	2.18	0.10	0.75
3.97	31.97	50.99	1.55	78.99	2.17	0.10	0.75
3.98	32.41	51.71	1.54	79.47	2.17	0.10	0.76
3.99	32.87	52.43	1.53	79.97	2.16	0.10	0.76
4.00	33.30	53.14	1.51	80.47	2.16	0.10	0.76
4.01	33.70	53.78	1.50	80.92	2.15	0.10	0.76
4.02	34.01	54.28	1.50	81.27	2.15	0.10	0.76
4.03	34.19	54.56	1.49	81.46	2.14	0.10	0.76
4.04	34.25	54.65	1.49	81.48	2.14	0.10	0.76
4.05	34.25	54.65	1.49	81.42	2.14	0.10	0.76
4.06	34.25	54.65	1.49	81.35	2.14	0.10	0.76
4.07	34.25	54.65	1.49	81.27	2.14	0.10	0.76
4.08	34.25	54.65	1.49	81.20	2.14	0.10	0.76
4.09	34.25	54.65	1.48	81.13	2.14	0.10	0.76
4.10	34.25	54.65	1.48	81.06	2.14	0.10	0.76
4.11	34.25	54.64	1.48	81.03	2.14	0.10	0.76
4.12	34.25	54.64	1.48	81.04	2.14	0.10	0.76
4.13	34.25	54.64	1.48	81.09	2.14	0.10	0.76
4.14	34.25	54.64	1.49	81.15	2.14	0.10	0.76
4.15	34.25	54.64	1.49	81.22	2.14	0.10	0.76
4.16	34.25	54.64	1.49	81.30	2.14	0.10	0.76
4.17	34.25	54.64	1.49	81.37	2.14	0.10	0.76
4.18	34.25	54.64	1.49	81.44	2.14	0.10	0.76
4.19	34.25	54.64	1.49	81.50	2.14	0.10	0.76
4.20	34.25	54.64	1.49	81.58	2.14	0.10	0.76
4.21	34.25	54.64	1.50	81.71	2.15	0.10	0.76
4.22	34.25	54.64	1.50	81.89	2.15	0.10	0.76
4.23	34.25	54.63	1.50	82.10	2.15	0.10	0.76
4.24	34.25	54.63	1.51	82.33	2.15	0.10	0.76
4.25	34.25	54.63	1.51	82.55	2.15	0.10	0.76
4.26	34.25	54.63	1.52	82.78	2.16	0.10	0.76
4.27	34.25	54.63	1.52	82.98	2.16	0.10	0.76
4.28	34.25	54.62	1.52	83.15	2.16	0.10	0.76
4.29	34.23	54.60	1.53	83.29	2.16	0.10	0.76
4.30	34.20	54.54	1.53	83.42	2.16	0.10	0.76
4.31	34.15	54.47	1.53	83.56	2.16	0.10	0.76
4.32	34.10	54.39	1.54	83.71	2.17	0.10	0.76

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
4.33	34.05	54.30	1.54	83.88	2.17	0.10	0.76
4.34	33.99	54.22	1.55	84.05	2.17	0.10	0.76
4.35	33.94	54.13	1.56	84.21	2.18	0.11	0.76
4.36	33.90	54.06	1.56	84.36	2.18	0.11	0.76
4.37	33.88	54.03	1.56	84.48	2.18	0.11	0.76
4.38	33.89	54.05	1.57	84.60	2.18	0.11	0.76
4.39	33.94	54.12	1.57	84.72	2.18	0.11	0.76
4.40	33.99	54.21	1.57	84.87	2.18	0.11	0.76
4.41	34.06	54.31	1.57	85.03	2.18	0.11	0.76
4.42	34.13	54.42	1.57	85.19	2.18	0.11	0.76
4.43	34.19	54.52	1.57	85.35	2.18	0.11	0.76
4.44	34.25	54.62	1.57	85.50	2.18	0.11	0.76
4.45	34.31	54.71	1.57	85.63	2.18	0.11	0.76
4.46	34.39	54.85	1.56	85.78	2.18	0.11	0.76
4.47	34.53	55.06	1.56	85.97	2.18	0.11	0.76
4.48	34.72	55.37	1.56	86.21	2.18	0.11	0.76
4.49	34.94	55.73	1.55	86.49	2.17	0.11	0.76
4.50	35.18	56.11	1.55	86.80	2.17	0.11	0.77
4.51	35.42	56.49	1.54	87.11	2.17	0.11	0.77
4.52	35.65	56.86	1.54	87.40	2.17	0.11	0.77
4.53	35.86	57.20	1.53	87.68	2.16	0.11	0.77
4.54	36.04	57.49	1.53	87.91	2.16	0.11	0.77
4.55	36.22	57.77	1.53	88.14	2.16	0.11	0.77
4.56	36.41	58.07	1.52	88.39	2.16	0.11	0.77
4.57	36.63	58.43	1.52	88.69	2.16	0.11	0.77
4.58	36.88	58.83	1.51	89.02	2.15	0.11	0.77
4.59	37.15	59.26	1.51	89.37	2.15	0.11	0.77
4.60	37.41	59.68	1.50	89.72	2.15	0.11	0.77
4.61	37.66	60.07	1.50	90.06	2.15	0.11	0.77
4.62	37.88	60.43	1.50	90.35	2.15	0.11	0.77
4.63	38.09	60.76	1.49	90.62	2.14	0.11	0.77
4.64	38.33	61.15	1.49	90.88	2.14	0.11	0.77
4.65	38.63	61.63	1.48	91.18	2.14	0.11	0.77
4.66	38.98	62.20	1.47	91.54	2.13	0.11	0.77
4.67	39.37	62.82	1.46	91.94	2.13	0.11	0.77
4.68	39.77	63.46	1.46	92.36	2.12	0.11	0.77
4.69	40.16	64.09	1.45	92.77	2.12	0.11	0.78
4.70	40.53	64.68	1.44	93.16	2.11	0.11	0.78
4.71	40.84	65.18	1.43	93.51	2.11	0.12	0.78
4.72	41.13	65.64	1.43	93.82	2.11	0.12	0.78
4.73	41.42	66.10	1.42	94.15	2.10	0.12	0.78
4.74	41.75	66.65	1.42	94.53	2.10	0.12	0.78
4.75	42.14	67.26	1.41	94.97	2.10	0.12	0.78
4.76	42.55	67.92	1.41	95.44	2.09	0.12	0.78
4.77	42.96	68.59	1.40	95.93	2.09	0.12	0.78
4.78	43.36	69.23	1.39	96.41	2.08	0.12	0.78
4.79	43.73	69.81	1.39	96.84	2.08	0.12	0.78
4.80	44.04	70.32	1.38	97.24	2.07	0.12	0.78

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
4.81	44.35	70.81	1.38	97.67	2.07	0.12	0.78
4.82	44.70	71.37	1.38	98.18	2.07	0.12	0.78
4.83	45.11	72.02	1.37	98.81	2.06	0.12	0.78
4.84	45.56	72.76	1.37	99.52	2.06	0.12	0.78
4.85	46.04	73.53	1.36	100.27	2.06	0.12	0.78
4.86	46.52	74.29	1.36	101.01	2.05	0.12	0.79
4.87	46.97	75.01	1.36	101.72	2.05	0.12	0.79
4.88	47.37	75.65	1.35	102.35	2.05	0.12	0.79
4.89	47.73	76.24	1.35	102.92	2.05	0.12	0.79
4.90	48.12	76.86	1.35	103.54	2.04	0.13	0.79
4.91	48.58	77.60	1.34	104.27	2.04	0.13	0.79
4.92	49.12	78.47	1.34	105.14	2.04	0.13	0.79
4.93	49.72	79.42	1.34	106.09	2.03	0.13	0.79
4.94	50.32	80.40	1.33	107.08	2.03	0.13	0.79
4.95	50.92	81.35	1.33	108.04	2.02	0.13	0.79
4.96	51.47	82.24	1.32	108.94	2.02	0.13	0.79
4.97	51.94	83.00	1.32	109.71	2.02	0.13	0.79
4.98	52.33	83.61	1.32	110.34	2.01	0.13	0.79
4.99	52.67	84.17	1.32	110.90	2.01	0.13	0.79
5.00	53.03	84.74	1.32	111.49	2.01	0.13	0.80
5.01	53.44	85.39	1.31	112.16	2.01	0.14	0.80
5.02	53.87	86.09	1.31	112.88	2.00	0.14	0.80
5.03	54.31	86.80	1.31	113.60	2.00	0.14	0.80
5.04	54.74	87.47	1.31	114.30	2.00	0.14	0.80
5.05	55.12	88.09	1.30	114.93	2.00	0.14	0.80
5.06	55.42	88.57	1.30	115.42	2.00	0.14	0.80
5.07	55.62	88.90	1.30	115.73	1.99	0.14	0.80
5.08	55.76	89.12	1.30	115.89	1.99	0.14	0.80
5.09	55.88	89.31	1.30	115.99	1.99	0.14	0.80
5.10	56.01	89.52	1.30	116.11	1.99	0.14	0.80
5.11	56.15	89.74	1.30	116.23	1.99	0.14	0.80
5.12	56.29	89.96	1.29	116.36	1.98	0.14	0.80
5.13	56.42	90.17	1.29	116.47	1.98	0.14	0.80
5.14	56.53	90.35	1.29	116.58	1.98	0.14	0.80
5.15	56.62	90.50	1.29	116.66	1.98	0.14	0.80
5.16	56.70	90.62	1.29	116.74	1.98	0.14	0.80
5.17	56.77	90.74	1.29	116.82	1.97	0.14	0.80
5.18	56.86	90.87	1.29	116.91	1.97	0.14	0.80
5.19	56.95	91.01	1.29	117.01	1.97	0.14	0.80
5.20	57.04	91.16	1.28	117.12	1.97	0.14	0.80
5.21	57.13	91.31	1.28	117.22	1.97	0.14	0.80
5.22	57.22	91.44	1.28	117.31	1.97	0.14	0.80
5.23	57.29	91.56	1.28	117.40	1.97	0.14	0.80
5.24	57.37	91.68	1.28	117.52	1.97	0.14	0.80
5.25	57.45	91.82	1.28	117.72	1.97	0.14	0.80
5.26	57.56	92.00	1.28	117.98	1.97	0.14	0.80
5.27	57.69	92.19	1.28	118.29	1.97	0.14	0.80
5.28	57.82	92.40	1.28	118.61	1.97	0.14	0.80

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
5.29	57.95	92.62	1.28	118.94	1.97	0.14	0.80
5.30	58.08	92.82	1.28	119.25	1.97	0.14	0.80
5.31	58.19	93.01	1.29	119.53	1.97	0.14	0.80
5.32	58.27	93.13	1.29	119.74	1.97	0.14	0.80
5.33	58.28	93.15	1.29	119.85	1.97	0.14	0.80
5.34	58.23	93.06	1.29	119.87	1.98	0.15	0.80
5.35	58.14	92.91	1.29	119.86	1.98	0.15	0.80
5.36	58.04	92.75	1.29	119.84	1.98	0.15	0.80
5.37	57.93	92.58	1.29	119.82	1.98	0.15	0.80
5.38	57.82	92.41	1.30	119.80	1.99	0.15	0.80
5.39	57.73	92.24	1.30	119.78	1.99	0.15	0.80
5.40	57.64	92.10	1.30	119.77	1.99	0.15	0.80
5.41	57.56	91.97	1.30	119.74	1.99	0.15	0.80
5.42	57.47	91.83	1.30	119.68	2.00	0.15	0.80
5.43	57.37	91.67	1.30	119.60	2.00	0.14	0.80
5.44	57.25	91.48	1.31	119.50	2.00	0.14	0.80
5.45	57.12	91.27	1.31	119.39	2.00	0.14	0.80
5.46	56.99	91.05	1.31	119.28	2.00	0.14	0.80
5.47	56.86	90.84	1.31	119.17	2.01	0.14	0.80
5.48	56.74	90.65	1.31	119.07	2.01	0.14	0.80
5.49	56.64	90.48	1.31	118.99	2.01	0.14	0.80
5.50	56.58	90.39	1.32	118.94	2.01	0.14	0.80
5.51	56.55	90.35	1.32	118.92	2.01	0.14	0.80
5.52	56.55	90.35	1.32	118.92	2.01	0.14	0.80
5.53	56.55	90.35	1.32	118.92	2.01	0.14	0.80
5.54	56.55	90.35	1.32	118.91	2.01	0.14	0.80
5.55	56.55	90.34	1.32	118.91	2.01	0.14	0.80
5.56	56.55	90.34	1.32	118.91	2.01	0.14	0.80
5.57	56.55	90.34	1.32	118.91	2.01	0.14	0.80
5.58	56.54	90.33	1.32	118.89	2.01	0.14	0.80
5.59	56.50	90.27	1.32	118.83	2.01	0.14	0.80
5.60	56.44	90.16	1.32	118.72	2.01	0.14	0.80
5.61	56.34	90.01	1.32	118.57	2.01	0.14	0.80
5.62	56.24	89.84	1.32	118.40	2.01	0.14	0.80
5.63	56.14	89.67	1.32	118.22	2.01	0.14	0.80
5.64	56.03	89.50	1.32	118.05	2.01	0.14	0.80
5.65	55.93	89.34	1.32	117.88	2.01	0.14	0.80
5.66	55.84	89.20	1.32	117.74	2.01	0.14	0.80
5.67	55.77	89.07	1.32	117.62	2.02	0.14	0.80
5.68	55.69	88.95	1.32	117.52	2.02	0.14	0.80
5.69	55.61	88.82	1.32	117.43	2.02	0.14	0.80
5.70	55.51	88.66	1.32	117.32	2.02	0.14	0.80
5.71	55.41	88.50	1.32	117.21	2.02	0.14	0.80
5.72	55.30	88.32	1.33	117.09	2.02	0.14	0.80
5.73	55.20	88.16	1.33	116.97	2.02	0.14	0.80
5.74	55.10	88.00	1.33	116.87	2.02	0.14	0.80
5.75	55.02	87.87	1.33	116.78	2.02	0.14	0.80
5.76	54.98	87.80	1.33	116.75	2.03	0.14	0.80

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
5.77	54.96	87.76	1.33	116.76	2.03	0.14	0.80
5.78	54.96	87.76	1.33	116.80	2.03	0.14	0.80
5.79	54.96	87.76	1.33	116.86	2.03	0.14	0.80
5.80	54.96	87.76	1.33	116.91	2.03	0.14	0.80
5.81	54.96	87.76	1.33	116.97	2.03	0.14	0.80
5.82	54.96	87.76	1.33	117.03	2.03	0.14	0.80
5.83	54.96	87.76	1.33	117.08	2.03	0.14	0.80
5.84	54.96	87.76	1.33	117.11	2.03	0.14	0.80
5.85	54.96	87.76	1.33	117.11	2.03	0.14	0.80
5.86	54.96	87.76	1.33	117.07	2.03	0.14	0.80
5.87	54.96	87.76	1.33	117.02	2.03	0.14	0.80
5.88	54.96	87.75	1.33	116.97	2.03	0.14	0.80
5.89	54.96	87.75	1.33	116.91	2.03	0.14	0.80
5.90	54.96	87.75	1.33	116.85	2.03	0.14	0.80
5.91	54.96	87.75	1.33	116.79	2.03	0.14	0.80
5.92	54.96	87.75	1.33	116.74	2.03	0.14	0.80
5.93	54.96	87.75	1.33	116.72	2.03	0.14	0.80
5.94	54.96	87.75	1.33	116.73	2.03	0.14	0.80
5.95	54.96	87.75	1.33	116.78	2.03	0.14	0.80
5.96	54.96	87.75	1.33	116.83	2.03	0.14	0.80
5.97	54.96	87.75	1.33	116.88	2.03	0.14	0.80
5.98	54.96	87.75	1.33	116.94	2.03	0.14	0.80
5.99	54.96	87.74	1.33	117.00	2.03	0.14	0.80
6.00	54.96	87.74	1.33	117.05	2.03	0.14	0.80
6.01	54.96	87.74	1.33	117.10	2.03	0.14	0.80
6.02	54.96	87.74	1.34	117.15	2.03	0.14	0.80
6.03	54.96	87.74	1.34	117.23	2.03	0.14	0.80
6.04	54.96	87.74	1.34	117.32	2.03	0.14	0.80
6.05	54.96	87.74	1.34	117.43	2.03	0.14	0.80
6.06	54.96	87.74	1.34	117.55	2.04	0.14	0.80
6.07	54.96	87.74	1.34	117.67	2.04	0.14	0.80
6.08	54.96	87.74	1.34	117.79	2.04	0.14	0.80
6.09	54.96	87.74	1.34	117.89	2.04	0.14	0.80
6.10	54.97	87.76	1.34	117.99	2.04	0.14	0.80
6.11	55.02	87.82	1.34	118.09	2.04	0.14	0.80
6.12	55.09	87.95	1.34	118.23	2.04	0.14	0.80
6.13	55.20	88.11	1.34	118.40	2.04	0.14	0.80
6.14	55.31	88.30	1.34	118.58	2.04	0.14	0.80
6.15	55.43	88.49	1.34	118.78	2.04	0.14	0.80
6.16	55.55	88.68	1.34	118.97	2.04	0.14	0.80
6.17	55.66	88.86	1.34	119.15	2.04	0.14	0.80
6.18	55.76	89.01	1.34	119.31	2.04	0.14	0.80
6.19	55.89	89.22	1.34	119.49	2.04	0.14	0.80
6.20	56.08	89.52	1.34	119.74	2.03	0.14	0.80
6.21	56.35	89.95	1.34	120.09	2.03	0.14	0.80
6.22	56.67	90.46	1.33	120.51	2.03	0.14	0.80
6.23	57.01	91.02	1.33	120.95	2.02	0.14	0.80
6.24	57.36	91.58	1.33	121.41	2.02	0.14	0.80

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
6.25	57.71	92.13	1.32	121.87	2.02	0.14	0.80
6.26	58.02	92.64	1.32	122.28	2.01	0.14	0.80
6.27	58.31	93.10	1.32	122.67	2.01	0.14	0.80
6.28	58.66	93.67	1.32	123.18	2.01	0.14	0.80
6.29	59.14	94.44	1.31	123.89	2.01	0.14	0.80
6.30	59.77	95.45	1.31	124.84	2.00	0.14	0.80
6.31	60.48	96.59	1.30	125.93	2.00	0.14	0.80
6.32	61.24	97.80	1.30	127.08	1.99	0.14	0.80
6.33	61.99	99.02	1.30	128.24	1.98	0.14	0.80
6.34	62.72	100.18	1.29	129.35	1.98	0.15	0.80
6.35	63.37	101.22	1.29	130.36	1.98	0.15	0.80
6.36	63.96	102.16	1.28	131.28	1.97	0.15	0.80
6.37	64.57	103.15	1.28	132.28	1.97	0.15	0.80
6.38	65.30	104.32	1.28	133.50	1.96	0.15	0.80
6.39	66.18	105.73	1.28	134.98	1.96	0.15	0.80
6.40	67.15	107.29	1.27	136.62	1.95	0.15	0.81
6.41	68.15	108.90	1.27	138.32	1.95	0.16	0.81
6.42	69.15	110.50	1.27	140.00	1.95	0.16	0.81
6.43	70.08	112.00	1.26	141.58	1.94	0.16	0.81
6.44	70.90	113.32	1.26	142.96	1.94	0.16	0.81
6.45	71.61	114.45	1.26	144.15	1.93	0.16	0.81
6.46	72.29	115.55	1.26	145.30	1.93	0.16	0.81
6.47	73.05	116.76	1.26	146.57	1.93	0.17	0.81
6.48	73.92	118.16	1.25	148.03	1.92	0.17	0.81
6.49	74.86	119.67	1.25	149.61	1.92	0.17	0.81
6.50	75.82	121.21	1.25	151.22	1.92	0.17	0.81
6.51	76.75	122.71	1.25	152.77	1.91	0.17	0.81
6.52	77.61	124.08	1.24	154.20	1.91	0.18	0.81
6.53	78.34	125.25	1.24	155.41	1.91	0.18	0.81
6.54	78.96	126.25	1.24	156.44	1.90	0.18	0.81
6.55	79.56	127.22	1.24	157.43	1.90	0.18	0.81
6.56	80.23	128.28	1.24	158.53	1.90	0.18	0.81
6.57	80.98	129.49	1.23	159.77	1.90	0.19	0.81
6.58	81.77	130.76	1.23	161.07	1.89	0.19	0.81
6.59	82.57	132.04	1.23	162.37	1.89	0.19	0.81
6.60	83.33	133.26	1.23	163.61	1.89	0.19	0.82
6.61	84.01	134.36	1.23	164.72	1.88	0.19	0.82
6.62	84.56	135.24	1.22	165.61	1.88	0.20	0.82
6.63	85.00	135.94	1.22	166.31	1.88	0.20	0.82
6.64	85.38	136.56	1.22	166.93	1.88	0.20	0.82
6.65	85.80	137.23	1.22	167.61	1.88	0.20	0.82
6.66	86.26	137.97	1.22	168.35	1.88	0.20	0.82
6.67	86.74	138.74	1.22	169.11	1.87	0.20	0.82
6.68	87.22	139.50	1.22	169.87	1.87	0.20	0.82
6.69	87.66	140.21	1.22	170.58	1.87	0.21	0.82
6.70	88.05	140.84	1.22	171.19	1.87	0.21	0.82
6.71	88.31	141.26	1.21	171.62	1.87	0.21	0.82
6.72	88.46	141.50	1.21	171.90	1.87	0.21	0.82

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
6.73	88.53	141.60	1.22	172.07	1.87	0.21	0.82
6.74	88.60	141.72	1.22	172.25	1.87	0.21	0.82
6.75	88.68	141.85	1.22	172.46	1.87	0.21	0.82
6.76	88.76	141.97	1.22	172.66	1.87	0.21	0.82
6.77	88.84	142.10	1.22	172.86	1.87	0.21	0.82
6.78	88.91	142.21	1.22	173.04	1.87	0.21	0.82
6.79	88.95	142.28	1.22	173.18	1.87	0.21	0.82
6.80	88.92	142.23	1.22	173.20	1.87	0.21	0.82
6.81	88.79	142.03	1.22	173.10	1.87	0.21	0.82
6.82	88.59	141.70	1.22	172.90	1.88	0.21	0.82
6.83	88.37	141.34	1.22	172.68	1.88	0.21	0.82
6.84	88.13	140.96	1.22	172.44	1.88	0.20	0.82
6.85	87.89	140.57	1.22	172.20	1.88	0.20	0.82
6.86	87.66	140.20	1.23	171.96	1.88	0.20	0.82
6.87	87.46	139.87	1.23	171.75	1.89	0.20	0.82
6.88	87.26	139.56	1.23	171.54	1.89	0.20	0.82
6.89	87.04	139.20	1.23	171.29	1.89	0.20	0.82
6.90	86.75	138.73	1.23	170.97	1.89	0.20	0.82
6.91	86.40	138.17	1.23	170.56	1.90	0.20	0.82
6.92	86.01	137.55	1.24	170.12	1.90	0.20	0.82
6.93	85.61	136.91	1.24	169.65	1.90	0.20	0.82
6.94	85.22	136.27	1.24	169.18	1.91	0.19	0.82
6.95	84.85	135.68	1.24	168.73	1.91	0.19	0.82
6.96	84.53	135.16	1.25	168.34	1.91	0.19	0.82
6.97	84.25	134.70	1.25	167.98	1.92	0.19	0.82
6.98	83.97	134.25	1.25	167.61	1.92	0.19	0.82
6.99	83.65	133.74	1.25	167.17	1.92	0.19	0.82
7.00	83.29	133.16	1.25	166.67	1.92	0.19	0.82
7.01	82.89	132.52	1.25	166.12	1.93	0.19	0.82
7.02	82.49	131.88	1.26	165.56	1.93	0.19	0.82
7.03	82.10	131.26	1.26	165.01	1.93	0.19	0.82
7.04	81.75	130.69	1.26	164.51	1.93	0.18	0.82
7.05	81.46	130.22	1.26	164.11	1.94	0.18	0.82
7.06	81.25	129.88	1.26	163.83	1.94	0.18	0.82
7.07	81.10	129.64	1.26	163.66	1.94	0.18	0.82
7.08	80.96	129.42	1.26	163.52	1.94	0.18	0.82
7.09	80.81	129.18	1.26	163.37	1.94	0.18	0.82
7.10	80.66	128.92	1.27	163.22	1.94	0.18	0.82
7.11	80.50	128.66	1.27	163.06	1.95	0.18	0.82
7.12	80.34	128.42	1.27	162.91	1.95	0.18	0.82
7.13	80.21	128.20	1.27	162.77	1.95	0.18	0.82
7.14	80.14	128.10	1.27	162.73	1.95	0.18	0.82
7.15	80.19	128.16	1.27	162.83	1.95	0.18	0.82
7.16	80.34	128.40	1.27	163.10	1.95	0.18	0.82
7.17	80.55	128.74	1.27	163.46	1.95	0.18	0.82
7.18	80.78	129.11	1.27	163.85	1.95	0.18	0.82
7.19	81.02	129.50	1.27	164.26	1.95	0.18	0.82
7.20	81.26	129.88	1.27	164.66	1.95	0.18	0.82

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
7.21	81.48	130.23	1.27	165.04	1.95	0.18	0.82
7.22	81.67	130.54	1.27	165.37	1.95	0.18	0.82
7.23	81.89	130.89	1.27	165.72	1.94	0.18	0.82
7.24	82.17	131.34	1.26	166.14	1.94	0.18	0.82
7.25	82.55	131.95	1.26	166.70	1.94	0.18	0.82
7.26	82.99	132.66	1.26	167.34	1.94	0.19	0.82
7.27	83.46	133.41	1.26	168.03	1.93	0.19	0.82
7.28	83.94	134.18	1.26	168.73	1.93	0.19	0.82
7.29	84.41	134.93	1.26	169.40	1.93	0.19	0.82
7.30	84.83	135.61	1.25	170.02	1.93	0.19	0.82
7.31	85.21	136.21	1.25	170.56	1.92	0.19	0.82
7.32	85.59	136.82	1.25	171.12	1.92	0.19	0.82
7.33	86.03	137.53	1.25	171.77	1.92	0.19	0.82
7.34	86.56	138.39	1.25	172.57	1.92	0.19	0.82
7.35	87.17	139.36	1.24	173.47	1.91	0.19	0.82
7.36	87.80	140.38	1.24	174.41	1.91	0.20	0.82
7.37	88.44	141.40	1.24	175.35	1.90	0.20	0.82
7.38	89.05	142.38	1.24	176.23	1.90	0.20	0.82
7.39	89.59	143.24	1.24	177.02	1.90	0.20	0.82
7.40	90.06	144.01	1.23	177.71	1.90	0.20	0.82
7.41	90.54	144.77	1.23	178.40	1.89	0.20	0.82
7.42	91.08	145.42	1.23	178.96	1.89	0.20	0.82
7.43	91.71	146.18	1.23	179.61	1.89	0.21	0.82
7.44	92.41	147.02	1.23	180.33	1.88	0.21	0.82
7.45	93.13	147.89	1.22	181.07	1.88	0.21	0.82
7.46	93.83	148.74	1.22	181.79	1.88	0.21	0.82
7.47	94.49	149.53	1.22	182.44	1.88	0.22	0.82
7.48	95.07	150.20	1.22	182.98	1.87	0.22	0.82
7.49	95.56	150.76	1.22	183.47	1.87	0.22	0.82
7.50	96.03	151.31	1.22	183.98	1.87	0.22	0.82
7.51	96.54	151.94	1.21	184.60	1.87	0.22	0.82
7.52	97.13	152.67	1.21	185.33	1.87	0.22	0.82
7.53	97.75	153.46	1.21	186.11	1.87	0.23	0.82
7.54	98.39	154.27	1.21	186.91	1.86	0.23	0.82
7.55	99.01	155.04	1.21	187.67	1.86	0.23	0.83
7.56	99.58	155.74	1.21	188.36	1.86	0.23	0.83
7.57	100.07	156.33	1.21	188.93	1.86	0.24	0.83
7.58	100.54	156.89	1.21	189.48	1.86	0.24	0.83
7.59	101.05	157.50	1.21	190.08	1.86	0.24	0.83
7.60	101.65	158.26	1.21	190.81	1.86	0.24	0.83
7.61	102.33	159.11	1.20	191.64	1.85	0.24	0.83
7.62	103.05	160.02	1.20	192.51	1.85	0.25	0.83
7.63	103.77	160.92	1.20	193.39	1.85	0.25	0.83
7.64	104.45	161.77	1.20	194.20	1.85	0.25	0.83
7.65	105.05	162.51	1.20	194.92	1.85	0.26	0.83
7.66	105.55	163.12	1.20	195.52	1.85	0.26	0.83
7.67	105.99	163.65	1.20	196.10	1.85	0.26	0.83
7.68	106.42	164.19	1.20	196.76	1.85	0.26	0.83

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
7.69	106.92	164.84	1.20	197.55	1.85	0.27	0.83
7.70	107.46	165.56	1.20	198.43	1.85	0.27	0.83
7.71	108.02	166.30	1.20	199.34	1.85	0.27	0.83
7.72	108.57	167.03	1.20	200.24	1.85	0.27	0.83
7.73	109.09	167.70	1.20	201.06	1.85	0.28	0.83
7.74	109.53	168.27	1.20	201.76	1.85	0.28	0.84
7.75	109.89	168.71	1.20	202.32	1.85	0.28	0.84
7.76	110.21	169.08	1.20	202.82	1.85	0.28	0.84
7.77	110.53	169.47	1.20	203.35	1.85	0.28	0.84
7.78	110.89	169.94	1.20	203.98	1.85	0.29	0.84
7.79	111.29	170.44	1.20	204.66	1.85	0.29	0.84
7.80	111.69	170.95	1.20	205.35	1.85	0.29	0.84
7.81	112.07	171.44	1.20	206.01	1.85	0.29	0.84
7.82	112.43	171.88	1.20	206.60	1.85	0.30	0.84
7.83	112.72	172.22	1.20	207.07	1.85	0.30	0.84
7.84	112.98	172.48	1.20	207.40	1.85	0.30	0.84
7.85	113.22	172.71	1.20	207.64	1.85	0.30	0.84
7.86	113.49	172.97	1.20	207.90	1.85	0.30	0.84
7.87	113.79	173.28	1.20	208.19	1.85	0.30	0.84
7.88	114.11	173.60	1.20	208.50	1.85	0.30	0.84
7.89	114.43	173.93	1.20	208.82	1.85	0.31	0.84
7.90	114.73	174.23	1.20	209.11	1.85	0.31	0.84
7.91	115.00	174.48	1.20	209.35	1.85	0.31	0.84
7.92	115.18	174.62	1.20	209.50	1.85	0.31	0.84
7.93	115.28	174.65	1.20	209.57	1.85	0.31	0.84
7.94	115.30	174.58	1.20	209.57	1.85	0.31	0.84
7.95	115.30	174.49	1.20	209.57	1.85	0.31	0.84
7.96	115.30	174.40	1.20	209.58	1.85	0.31	0.84
7.97	115.30	174.31	1.20	209.59	1.85	0.31	0.84
7.98	115.30	174.23	1.20	209.61	1.85	0.31	0.84
7.99	115.30	174.14	1.20	209.61	1.85	0.31	0.84
8.00	115.30	174.04	1.20	209.59	1.85	0.31	0.84
8.01	115.30	174.01	1.20	209.65	1.86	0.31	0.84
8.02	115.30	173.99	1.21	209.75	1.86	0.31	0.84
8.03	115.30	173.99	1.21	209.89	1.86	0.31	0.84
8.04	115.30	173.99	1.21	210.06	1.86	0.31	0.84
8.05	115.30	173.99	1.21	210.25	1.86	0.31	0.84
8.06	115.30	174.00	1.21	210.44	1.86	0.31	0.85
8.07	115.30	174.00	1.21	210.61	1.86	0.31	0.85
8.08	115.30	174.00	1.21	210.77	1.86	0.31	0.85
8.09	115.32	174.01	1.21	210.90	1.86	0.31	0.85
8.10	115.42	174.11	1.21	211.03	1.86	0.31	0.85
8.11	115.61	174.30	1.21	211.19	1.86	0.31	0.85
8.12	115.89	174.59	1.21	211.40	1.86	0.31	0.85
8.13	116.19	174.92	1.21	211.64	1.86	0.31	0.85
8.14	116.51	175.27	1.21	211.90	1.86	0.32	0.85
8.15	116.83	175.61	1.21	212.15	1.86	0.32	0.85
8.16	117.13	175.94	1.21	212.38	1.86	0.32	0.85

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
8.17	117.40	176.22	1.21	212.58	1.86	0.32	0.85
8.18	117.66	176.49	1.21	212.75	1.86	0.32	0.85
8.19	117.98	176.82	1.20	212.93	1.85	0.32	0.85
8.20	118.40	177.26	1.20	213.15	1.85	0.33	0.85
8.21	118.89	177.79	1.20	213.40	1.85	0.33	0.85
8.22	119.44	178.38	1.20	213.67	1.85	0.33	0.85
8.23	120.00	178.99	1.20	213.94	1.84	0.34	0.85
8.24	120.55	179.58	1.19	214.19	1.84	0.34	0.85
8.25	121.06	180.12	1.19	214.40	1.84	0.34	0.85
8.26	121.50	180.59	1.19	214.57	1.84	0.35	0.85
8.27	121.93	181.05	1.19	214.78	1.83	0.35	0.85
8.28	122.41	181.58	1.18	215.08	1.83	0.35	0.85
8.29	122.99	182.26	1.18	215.51	1.83	0.36	0.85
8.30	123.65	183.04	1.18	216.00	1.83	0.36	0.85
8.31	124.36	183.87	1.18	216.50	1.82	0.37	0.85
8.32	125.08	184.72	1.17	217.01	1.82	0.37	0.85
8.33	125.77	185.53	1.17	217.47	1.82	0.38	0.85
8.34	126.40	186.26	1.17	217.88	1.82	0.39	0.85
8.35	126.94	186.87	1.17	218.21	1.81	0.39	0.85
8.36	127.41	187.28	1.17	218.42	1.81	0.39	0.85
8.37	127.89	187.83	1.16	218.77	1.81	0.40	0.85
8.38	128.43	188.47	1.16	219.20	1.81	0.40	0.85
8.39	129.04	189.20	1.16	219.68	1.81	0.41	0.85
8.40	129.68	189.96	1.16	220.18	1.81	0.41	0.85
8.41	130.31	190.71	1.16	220.66	1.80	0.42	0.85
8.42	130.92	191.42	1.16	221.11	1.80	0.43	0.85
8.43	131.45	192.05	1.15	221.49	1.80	0.43	0.85
8.44	131.87	192.53	1.15	221.80	1.80	0.44	0.85
8.45	132.22	192.92	1.15	222.08	1.80	0.44	0.85
8.46	132.54	193.28	1.15	222.37	1.80	0.44	0.85
8.47	132.89	193.70	1.15	222.71	1.80	0.45	0.85
8.48	133.28	194.16	1.15	223.08	1.80	0.45	0.85
8.49	133.68	194.63	1.15	223.47	1.80	0.46	0.85
8.50	134.07	195.10	1.15	223.85	1.80	0.46	0.85
8.51	134.44	195.52	1.15	224.19	1.79	0.46	0.85
8.52	134.75	195.88	1.15	224.48	1.79	0.47	0.85
8.53	134.99	196.14	1.15	224.69	1.79	0.47	0.85
8.54	135.19	196.34	1.15	224.85	1.79	0.47	0.85
8.55	135.39	196.54	1.14	225.01	1.79	0.47	0.85
8.56	135.61	196.77	1.14	225.20	1.79	0.48	0.85
8.57	135.85	197.02	1.14	225.40	1.79	0.48	0.85
8.58	136.09	197.28	1.14	225.61	1.79	0.48	0.86
8.59	136.32	197.52	1.14	225.80	1.79	0.48	0.86
8.60	136.53	197.74	1.14	225.98	1.79	0.49	0.86
8.61	136.69	197.89	1.14	226.10	1.79	0.49	0.86
8.62	136.81	197.98	1.14	226.17	1.79	0.49	0.86
8.63	136.88	198.02	1.14	226.20	1.79	0.49	0.86
8.64	136.95	198.05	1.14	226.22	1.79	0.49	0.86

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
8.65	137.03	198.08	1.14	226.25	1.79	0.49	0.86
8.66	137.11	198.12	1.14	226.29	1.79	0.49	0.86
8.67	137.19	198.16	1.14	226.32	1.79	0.49	0.86
8.68	137.26	198.20	1.14	226.35	1.79	0.49	0.86
8.69	137.33	198.22	1.14	226.37	1.79	0.49	0.86
8.70	137.37	198.20	1.14	226.29	1.79	0.49	0.86
8.71	137.40	198.13	1.14	226.08	1.79	0.49	0.86
8.72	137.40	198.01	1.14	225.72	1.79	0.49	0.86
8.73	137.40	197.88	1.14	225.28	1.79	0.49	0.86
8.74	137.40	197.73	1.14	224.81	1.79	0.49	0.86
8.75	137.40	197.59	1.14	224.31	1.79	0.49	0.86
8.76	137.40	197.44	1.13	223.82	1.78	0.49	0.86
8.77	137.40	197.30	1.13	223.36	1.78	0.49	0.86
8.78	137.39	197.17	1.13	222.95	1.78	0.49	0.86
8.79	137.36	197.01	1.13	222.60	1.78	0.49	0.86
8.80	137.27	196.79	1.13	222.26	1.78	0.48	0.86
8.81	137.14	196.52	1.13	221.90	1.78	0.48	0.85
8.82	136.99	196.23	1.13	221.49	1.78	0.48	0.85
8.83	136.84	195.91	1.13	221.05	1.78	0.48	0.85
8.84	136.68	195.60	1.13	220.61	1.78	0.47	0.85
8.85	136.52	195.29	1.13	220.19	1.78	0.47	0.85
8.86	136.38	195.01	1.13	219.80	1.78	0.47	0.85
8.87	136.25	194.75	1.13	219.51	1.78	0.47	0.85
8.88	136.09	194.48	1.13	219.37	1.78	0.46	0.85
8.89	135.87	194.18	1.13	219.37	1.78	0.46	0.85
8.90	135.59	193.82	1.13	219.44	1.78	0.46	0.85
8.91	135.29	193.43	1.13	219.51	1.78	0.45	0.85
8.92	134.97	193.03	1.14	219.57	1.79	0.45	0.85
8.93	134.65	192.62	1.14	219.62	1.79	0.45	0.85
8.94	134.35	192.24	1.14	219.66	1.79	0.44	0.85
8.95	134.09	191.89	1.14	219.67	1.79	0.44	0.85
8.96	133.85	191.55	1.15	219.62	1.79	0.44	0.85
8.97	133.59	191.19	1.15	219.49	1.80	0.44	0.85
8.98	133.29	190.75	1.15	219.28	1.80	0.43	0.85
8.99	132.93	190.25	1.15	219.01	1.80	0.43	0.85
9.00	132.54	189.71	1.15	218.73	1.80	0.42	0.85
9.01	132.14	189.15	1.15	218.43	1.80	0.42	0.85
9.02	131.75	188.61	1.16	218.13	1.80	0.42	0.85
9.03	131.38	188.10	1.16	217.84	1.80	0.41	0.85
9.04	131.07	187.66	1.16	217.59	1.81	0.41	0.85
9.05	130.81	187.29	1.16	217.42	1.81	0.41	0.85
9.06	130.57	186.95	1.16	217.32	1.81	0.40	0.85
9.07	130.31	186.60	1.16	217.26	1.81	0.40	0.85
9.08	130.01	186.22	1.17	217.19	1.81	0.40	0.85
9.09	129.70	185.81	1.17	217.12	1.81	0.39	0.85
9.10	129.38	185.39	1.17	217.03	1.82	0.39	0.85
9.11	129.07	184.99	1.17	216.93	1.82	0.39	0.85
9.12	128.79	184.62	1.17	216.84	1.82	0.39	0.85

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.13	128.58	184.33	1.18	216.77	1.82	0.38	0.85
9.14	128.44	184.13	1.18	216.77	1.82	0.38	0.85
9.15	128.35	184.01	1.18	216.85	1.82	0.38	0.85
9.16	128.29	183.92	1.18	216.98	1.83	0.38	0.85
9.17	128.21	183.82	1.18	217.13	1.83	0.38	0.85
9.18	128.13	183.72	1.18	217.28	1.83	0.38	0.85
9.19	128.05	183.62	1.18	217.43	1.83	0.38	0.85
9.20	127.98	183.53	1.19	217.56	1.83	0.38	0.85
9.21	127.91	183.44	1.19	217.67	1.83	0.38	0.85
9.22	127.89	183.39	1.19	217.76	1.83	0.38	0.85
9.23	127.94	183.41	1.19	217.84	1.83	0.38	0.85
9.24	128.06	183.51	1.19	217.94	1.83	0.38	0.85
9.25	128.20	183.64	1.19	218.06	1.83	0.38	0.85
9.26	128.36	183.79	1.19	218.19	1.83	0.38	0.85
9.27	128.52	183.94	1.19	218.34	1.83	0.38	0.85
9.28	128.67	184.09	1.19	218.47	1.83	0.38	0.85
9.29	128.82	184.22	1.19	218.60	1.83	0.38	0.85
9.30	128.95	184.34	1.19	218.70	1.83	0.39	0.85
9.31	129.17	184.54	1.19	218.83	1.83	0.39	0.85
9.32	129.49	184.88	1.18	219.02	1.83	0.39	0.85
9.33	129.95	185.37	1.18	219.28	1.83	0.39	0.85
9.34	130.47	185.94	1.18	219.57	1.83	0.40	0.85
9.35	131.03	186.54	1.18	219.87	1.82	0.40	0.85
9.36	131.59	187.16	1.18	220.17	1.82	0.41	0.85
9.37	132.12	187.74	1.17	220.44	1.82	0.41	0.85
9.38	132.61	188.26	1.17	220.66	1.82	0.42	0.85
9.39	133.04	188.72	1.17	220.86	1.82	0.42	0.85
9.40	133.51	189.21	1.17	221.05	1.81	0.42	0.85
9.41	134.08	189.82	1.17	221.28	1.81	0.43	0.85
9.42	134.77	190.58	1.16	221.55	1.81	0.44	0.85
9.43	135.54	191.42	1.16	221.84	1.81	0.44	0.85
9.44	136.33	192.30	1.15	222.10	1.80	0.45	0.85
9.45	137.13	193.17	1.15	222.34	1.80	0.46	0.85
9.46	137.87	193.98	1.15	222.52	1.79	0.47	0.85
9.47	138.53	194.68	1.14	222.66	1.79	0.48	0.85
9.48	139.09	195.27	1.14	222.78	1.79	0.48	0.86
9.49	139.61	195.83	1.14	222.91	1.79	0.49	0.86
9.50	140.17	196.44	1.14	223.09	1.79	0.49	0.86
9.51	140.82	197.16	1.13	223.29	1.78	0.50	0.86
9.52	141.52	197.93	1.13	223.49	1.78	0.51	0.86
9.53	142.24	198.73	1.13	223.68	1.78	0.52	0.86
9.54	142.94	199.50	1.12	223.84	1.78	0.53	0.86
9.55	143.59	200.21	1.12	223.97	1.77	0.54	0.86
9.56	144.09	200.73	1.12	223.99	1.77	0.55	0.86
9.57	144.10	200.62	1.11	223.54	1.77	0.55	0.86
9.58	143.60	199.83	1.11	222.54	1.77	0.53	0.86
9.59	142.65	198.43	1.11	221.00	1.77	0.52	0.86
9.60	141.56	196.86	1.11	219.26	1.77	0.50	0.86

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.61	140.42	195.19	1.11	217.43	1.77	0.49	0.86
9.62	139.26	193.52	1.11	215.59	1.77	0.47	0.85
9.63	138.15	191.91	1.11	213.82	1.77	0.45	0.85
9.64	137.15	190.46	1.11	212.23	1.77	0.44	0.85
9.65	136.42	189.38	1.11	211.01	1.77	0.43	0.85
9.66	136.05	188.78	1.11	210.21	1.77	0.43	0.85
9.67	135.99	188.58	1.11	209.72	1.77	0.43	0.85
9.68	136.06	188.54	1.11	209.30	1.77	0.43	0.85
9.69	136.14	188.51	1.11	208.84	1.77	0.43	0.85
9.70	136.22	188.48	1.11	208.36	1.76	0.43	0.85
9.71	136.29	188.44	1.10	207.87	1.76	0.43	0.85
9.72	136.37	188.41	1.10	207.40	1.76	0.43	0.85
9.73	136.43	188.37	1.10	206.97	1.76	0.43	0.85
9.74	136.04	187.77	1.10	206.37	1.76	0.43	0.85
9.75	134.97	186.34	1.10	205.43	1.76	0.41	0.85
9.76	133.13	183.95	1.11	204.00	1.77	0.39	0.85
9.77	130.93	181.10	1.12	202.24	1.77	0.37	0.84
9.78	128.55	178.01	1.12	200.25	1.78	0.35	0.84
9.79	126.10	174.85	1.13	198.11	1.78	0.33	0.84
9.80	123.73	171.76	1.14	195.93	1.79	0.32	0.83
9.81	121.54	168.91	1.15	193.85	1.80	0.30	0.83
9.82	119.59	166.40	1.15	192.09	1.80	0.29	0.83
9.83	117.46	163.83	1.17	190.99	1.81	0.28	0.83
9.84	114.82	160.79	1.18	190.11	1.83	0.27	0.83
9.85	111.45	156.97	1.20	188.76	1.85	0.25	0.83
9.86	107.64	152.58	1.22	186.46	1.88	0.24	0.83
9.87	103.59	147.83	1.24	183.38	1.91	0.23	0.83
9.88	99.52	142.95	1.26	179.87	1.93	0.21	0.84
9.89	95.63	138.21	1.28	176.28	1.96	0.20	0.84
9.90	92.13	133.87	1.29	172.95	1.98	0.20	0.84
9.91	89.61	130.77	1.31	170.81	2.00	0.19	0.83
9.92	88.39	129.38	1.32	170.46	2.01	0.19	0.84
9.93	88.29	129.60	1.33	171.93	2.02	0.19	0.84
9.94	88.65	130.42	1.34	174.28	2.03	0.20	0.84
9.95	89.05	131.33	1.35	176.92	2.04	0.20	0.84
9.96	89.47	132.27	1.36	179.73	2.05	0.20	0.84
9.97	89.89	133.19	1.37	182.56	2.06	0.21	0.85
9.98	90.28	134.04	1.38	185.25	2.07	0.21	0.85
9.99	90.62	134.78	1.39	187.66	2.08	0.21	0.85
10.00	90.70	135.03	1.40	188.93	2.09	0.22	0.85
10.01	90.47	134.72	1.40	188.99	2.09	0.21	0.85
10.02	89.92	133.87	1.40	187.93	2.09	0.21	0.85
10.03	89.25	132.84	1.40	186.60	2.09	0.21	0.85
10.04	88.54	131.73	1.41	185.16	2.09	0.21	0.85
10.05	87.80	130.60	1.41	183.70	2.09	0.20	0.85
10.06	87.08	129.50	1.41	182.27	2.09	0.20	0.85
10.07	86.42	128.49	1.41	180.96	2.09	0.20	0.84
10.08	85.78	127.51	1.41	179.77	2.09	0.20	0.84

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
10.09	84.79	126.08	1.41	178.33	2.10	0.20	0.84
10.10	83.29	123.98	1.42	176.44	2.10	0.19	0.84
10.11	81.22	121.10	1.44	174.01	2.11	0.19	0.84
10.12	78.88	117.85	1.45	171.31	2.12	0.18	0.83
10.13	76.41	114.41	1.47	168.50	2.13	0.18	0.83
10.14	73.91	110.93	1.49	165.71	2.14	0.17	0.83
10.15	71.54	107.60	1.52	163.11	2.16	0.17	0.82
10.16	69.39	104.59	1.54	160.80	2.17	0.16	0.82
10.17	67.57	102.05	1.56	159.10	2.18	0.16	0.82
10.18	65.89	99.73	1.59	158.11	2.19	0.16	0.82
10.19	64.10	97.32	1.62	157.71	2.20	0.15	0.81
10.20	62.02	94.53	1.67	157.57	2.22	0.15	0.81
10.21	59.73	91.42	1.72	157.50	2.24	0.15	0.81
10.22	57.35	88.16	1.79	157.52	2.26	0.14	0.80
10.23	54.99	84.91	1.86	157.61	2.28	0.14	0.80
10.24	52.79	81.84	1.93	157.75	2.30	0.14	0.80
10.25	50.85	79.12	2.00	157.91	2.32	0.13	0.79
10.26	49.28	76.91	2.06	158.31	2.33	0.13	0.79
10.27	47.90	74.97	2.12	159.07	2.35	0.13	0.79
10.28	46.50	73.03	2.19	160.25	2.36	0.13	0.79
10.29	44.91	70.78	2.28	161.63	2.38	0.13	0.78
10.30	43.18	68.35	2.39	163.08	2.40	0.12	0.78
10.31	41.42	65.56	2.51	164.29	2.42	0.12	0.78
10.32	39.71	62.81	2.63	165.36	2.45	0.12	0.77
10.33	38.14	60.29	2.76	166.27	2.47	0.12	0.77
10.34	36.84	58.19	2.87	167.01	2.48	0.12	0.77
10.35	35.90	56.69	2.96	167.77	2.50	0.12	0.76
10.36	35.22	55.59	3.03	168.68	2.51	0.11	0.76
10.37	34.62	54.63	3.11	169.81	2.52	0.11	0.76
10.38	33.95	53.55	3.19	171.04	2.53	0.11	0.76
10.39	33.23	52.40	3.29	172.29	2.54	0.11	0.76
10.40	32.51	51.24	3.39	173.49	2.56	0.11	0.76
10.41	31.83	50.14	3.48	174.58	2.57	0.11	0.76
10.42	31.21	49.15	3.57	175.51	2.58	0.11	0.75
10.43	30.76	48.43	3.64	176.32	2.59	0.11	0.75
10.44	30.50	48.00	3.69	177.16	2.59	0.11	0.75
10.45	30.39	47.82	3.73	178.17	2.60	0.11	0.75
10.46	30.32	47.71	3.76	179.37	2.60	0.11	0.62
10.47	30.24	47.59	3.80	180.69	2.61	0.11	0.62
10.48	30.16	47.46	3.84	182.05	2.61	0.11	0.62
10.49	30.08	47.33	3.87	183.39	2.61	0.11	0.62
10.50	30.01	47.21	3.91	184.64	2.62	0.11	0.62
10.51	29.94	47.11	3.94	185.72	2.62	0.11	0.62
10.52	29.90	47.04	3.97	186.51	2.62	0.11	0.62
10.53	29.89	47.01	3.98	187.08	2.63	0.11	0.62
10.54	29.88	47.01	3.99	187.52	2.63	0.11	0.62
10.55	29.88	47.00	4.00	188.01	2.63	0.11	0.62
10.56	29.88	47.00	4.01	188.54	2.63	0.11	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
10.57	29.88	47.00	4.02	189.09	2.63	0.11	0.62
10.58	29.88	47.00	4.03	189.61	2.63	0.11	0.62
10.59	29.88	47.00	4.04	190.09	2.63	0.11	0.62
10.60	29.90	47.03	4.05	190.46	2.63	0.11	0.62
10.61	29.99	47.16	4.04	190.56	2.63	0.11	0.62
10.62	30.16	47.44	4.01	190.40	2.63	0.11	0.62
10.63	30.42	47.86	3.97	190.03	2.62	0.11	0.62
10.64	30.71	48.32	3.92	189.60	2.62	0.11	0.62
10.65	31.02	48.81	3.87	189.14	2.61	0.11	0.62
10.66	31.32	49.31	3.83	188.66	2.61	0.11	0.62
10.67	31.62	49.78	3.78	188.18	2.60	0.11	0.62
10.68	31.88	50.20	3.74	187.75	2.60	0.11	0.76
10.69	32.16	50.64	3.70	187.32	2.59	0.11	0.76
10.70	32.52	51.23	3.65	186.81	2.59	0.11	0.76
10.71	33.03	52.05	3.58	186.12	2.58	0.11	0.76
10.72	33.66	53.06	3.49	185.25	2.57	0.11	0.76
10.73	34.36	54.17	3.40	184.23	2.56	0.11	0.76
10.74	35.08	55.33	3.31	183.12	2.55	0.12	0.76
10.75	35.79	56.47	3.22	181.97	2.53	0.12	0.76
10.76	36.45	57.53	3.14	180.86	2.52	0.12	0.77
10.77	37.03	58.46	3.08	179.84	2.51	0.12	0.77
10.78	37.61	59.39	3.01	178.97	2.51	0.12	0.77
10.79	38.27	60.45	2.95	178.11	2.50	0.12	0.77
10.80	39.10	61.69	2.87	177.05	2.48	0.12	0.77
10.81	40.06	63.00	2.79	175.70	2.47	0.12	0.77
10.82	41.09	64.41	2.70	174.19	2.46	0.12	0.78
10.83	42.14	65.84	2.62	172.60	2.44	0.12	0.78
10.84	43.16	67.21	2.54	171.01	2.43	0.13	0.78
10.85	44.09	68.46	2.48	169.53	2.42	0.13	0.78
10.86	44.92	69.55	2.42	168.27	2.41	0.13	0.78
10.87	45.76	70.67	2.37	167.22	2.40	0.13	0.78
10.88	46.74	71.98	2.31	166.26	2.39	0.13	0.79
10.89	47.95	73.60	2.24	165.23	2.37	0.13	0.79
10.90	49.30	75.41	2.18	164.06	2.36	0.13	0.79
10.91	50.73	77.31	2.11	162.81	2.34	0.13	0.79
10.92	52.17	79.19	2.04	161.56	2.33	0.14	0.80
10.93	53.53	80.97	1.98	160.38	2.31	0.14	0.80
10.94	54.75	82.55	1.93	159.32	2.30	0.14	0.80
10.95	55.78	83.86	1.89	158.45	2.29	0.14	0.80
10.96	56.72	85.05	1.85	157.65	2.28	0.14	0.80
10.97	57.69	86.27	1.82	156.83	2.27	0.14	0.80
10.98	58.81	87.68	1.78	155.90	2.26	0.14	0.81
10.99	60.05	89.22	1.74	154.93	2.24	0.15	0.81
11.00	61.33	90.80	1.70	153.95	2.23	0.15	0.81
11.01	62.59	92.35	1.66	153.04	2.22	0.15	0.81
11.02	63.77	93.77	1.62	152.24	2.20	0.15	0.81
11.03	64.79	95.00	1.60	151.57	2.19	0.15	0.81
11.04	65.56	95.86	1.57	150.97	2.18	0.15	0.81

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
11.05	66.15	96.53	1.56	150.44	2.18	0.15	0.81
11.06	66.67	97.08	1.54	149.85	2.17	0.15	0.81
11.07	67.25	97.72	1.53	149.20	2.16	0.15	0.81
11.08	67.88	98.40	1.51	148.52	2.15	0.15	0.82
11.09	68.52	99.09	1.49	147.86	2.14	0.15	0.82
11.10	69.14	99.75	1.48	147.25	2.14	0.15	0.82
11.11	69.71	100.34	1.46	146.71	2.13	0.15	0.82
11.12	70.14	100.78	1.45	146.24	2.12	0.15	0.82
11.13	70.34	100.93	1.44	145.71	2.12	0.15	0.82
11.14	70.33	100.80	1.44	145.06	2.11	0.15	0.82
11.15	70.18	100.49	1.44	144.23	2.11	0.15	0.81
11.16	70.01	100.14	1.43	143.31	2.11	0.15	0.81
11.17	69.83	99.78	1.43	142.35	2.11	0.15	0.81
11.18	69.65	99.41	1.42	141.39	2.10	0.15	0.81
11.19	69.48	99.07	1.42	140.48	2.10	0.15	0.81
11.20	69.33	98.75	1.41	139.67	2.10	0.15	0.81
11.21	69.12	98.40	1.41	139.00	2.10	0.15	0.81
11.22	68.78	97.89	1.41	138.41	2.10	0.15	0.81
11.23	68.26	97.18	1.42	137.84	2.10	0.15	0.81
11.24	67.61	96.31	1.42	137.21	2.10	0.14	0.81
11.25	66.90	95.36	1.43	136.52	2.11	0.14	0.81
11.26	66.17	94.37	1.44	135.81	2.11	0.14	0.81
11.27	65.44	93.40	1.45	135.12	2.12	0.14	0.81
11.28	64.77	92.49	1.45	134.49	2.12	0.14	0.81
11.29	64.18	91.69	1.46	133.94	2.13	0.14	0.80
11.30	63.58	90.90	1.47	133.53	2.13	0.14	0.80
11.31	62.89	90.00	1.48	133.22	2.14	0.14	0.80
11.32	62.01	88.88	1.50	132.99	2.15	0.14	0.80
11.33	61.00	87.59	1.52	132.75	2.16	0.14	0.80
11.34	59.92	86.20	1.54	132.53	2.17	0.14	0.80
11.35	58.82	84.78	1.56	132.34	2.18	0.13	0.80
11.36	57.76	83.40	1.58	132.19	2.19	0.13	0.80
11.37	56.79	82.14	1.61	132.07	2.20	0.13	0.80
11.38	55.93	81.01	1.63	132.01	2.21	0.13	0.79
11.39	55.04	79.86	1.65	132.01	2.22	0.13	0.79
11.40	54.01	78.51	1.68	132.10	2.23	0.13	0.79
11.41	52.74	76.85	1.72	132.29	2.24	0.13	0.79
11.42	51.32	74.99	1.77	132.54	2.25	0.13	0.79
11.43	49.82	73.04	1.82	132.89	2.27	0.13	0.79
11.44	48.33	71.06	1.88	133.24	2.29	0.12	0.78
11.45	46.91	69.16	1.93	133.61	2.30	0.12	0.78
11.46	45.64	67.45	1.99	133.96	2.32	0.12	0.78
11.47	44.59	66.03	2.03	134.36	2.33	0.12	0.78
11.48	43.66	64.77	2.08	134.89	2.34	0.12	0.78
11.49	42.71	63.50	2.14	135.63	2.35	0.12	0.77
11.50	41.62	62.03	2.20	136.53	2.37	0.12	0.77
11.51	40.44	60.43	2.28	137.52	2.38	0.12	0.77
11.52	39.21	58.76	2.36	138.54	2.40	0.11	0.77

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
11.53	38.00	57.10	2.44	139.52	2.41	0.11	0.76
11.54	36.88	55.55	2.53	140.41	2.43	0.11	0.76
11.55	35.91	54.20	2.60	141.17	2.44	0.11	0.76
11.56	35.13	53.12	2.67	141.90	2.45	0.11	0.76
11.57	34.46	52.19	2.73	142.72	2.46	0.11	0.76
11.58	33.79	51.26	2.80	143.73	2.47	0.11	0.76
11.59	33.03	50.20	2.89	144.85	2.49	0.11	0.75
11.60	32.21	49.06	2.98	146.03	2.50	0.11	0.75
11.61	31.38	47.90	3.07	147.17	2.51	0.11	0.75
11.62	30.58	46.76	3.17	148.23	2.53	0.11	0.75
11.63	29.84	45.73	3.26	149.15	2.54	0.10	0.75
11.64	29.25	44.88	3.34	149.91	2.55	0.10	0.74
11.65	28.81	44.26	3.40	150.61	2.56	0.10	0.74
11.66	28.48	43.78	3.46	151.36	2.56	0.10	0.74
11.67	28.16	43.34	3.51	152.23	2.57	0.10	0.74
11.68	27.81	42.83	3.58	153.20	2.58	0.10	0.74
11.69	27.44	42.31	3.64	154.19	2.59	0.10	0.74
11.70	27.07	41.78	3.71	155.15	2.60	0.10	0.74
11.71	26.72	41.28	3.78	156.04	2.60	0.10	0.62
11.72	26.40	40.83	3.84	156.81	2.61	0.10	0.62
11.73	26.21	40.54	3.88	157.39	2.61	0.10	0.62
11.74	26.15	40.46	3.90	157.79	2.62	0.10	0.62
11.75	26.23	40.56	3.90	158.11	2.62	0.10	0.62
11.76	26.35	40.73	3.89	158.44	2.62	0.10	0.62
11.77	26.49	40.91	3.88	158.81	2.61	0.10	0.62
11.78	26.63	41.10	3.87	159.18	2.61	0.10	0.62
11.79	26.76	41.29	3.86	159.55	2.61	0.10	0.62
11.80	26.89	41.47	3.86	159.90	2.61	0.10	0.62
11.81	26.99	41.61	3.85	160.18	2.61	0.10	0.62
11.82	26.96	41.54	3.85	159.99	2.61	0.10	0.62
11.83	26.76	41.23	3.86	159.27	2.61	0.10	0.62
11.84	26.40	40.66	3.89	157.99	2.62	0.10	0.62
11.85	25.99	40.02	3.91	156.52	2.62	0.10	0.62
11.86	25.55	39.33	3.94	154.96	2.62	0.10	0.62
11.87	25.10	38.63	3.97	153.38	2.62	0.10	0.62
11.88	24.67	37.96	4.00	151.85	2.63	0.10	0.62
11.89	24.27	37.34	4.03	150.47	2.63	0.10	0.62
11.90	23.96	36.85	4.05	149.28	2.63	0.10	0.62
11.91	23.76	36.52	4.06	148.17	2.63	0.10	0.62
11.92	23.64	36.31	4.05	147.00	2.63	0.10	0.62
11.93	23.55	36.13	4.03	145.62	2.63	0.10	0.62
11.94	23.45	35.94	4.01	144.09	2.63	0.10	0.62
11.95	23.34	35.74	3.99	142.49	2.63	0.10	0.62
11.96	23.23	35.53	3.96	140.88	2.62	0.10	0.62
11.97	23.13	35.34	3.94	139.37	2.62	0.10	0.62
11.98	23.04	35.17	3.92	138.02	2.62	0.10	0.62
11.99	22.93	34.97	3.91	136.83	2.62	0.10	0.62
12.00	22.76	34.68	3.91	135.64	2.62	0.09	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
12.01	22.50	34.27	3.92	134.29	2.62	0.09	0.62
12.02	22.19	33.77	3.93	132.72	2.62	0.09	0.62
12.03	21.85	33.23	3.94	131.01	2.62	0.09	0.62
12.04	21.49	32.67	3.96	129.26	2.62	0.09	0.62
12.05	21.15	32.13	3.97	127.54	2.62	0.09	0.62
12.06	20.83	31.62	3.98	125.96	2.63	0.09	0.62
12.07	20.54	31.17	4.00	124.59	2.63	0.09	0.62
12.08	20.15	30.57	4.04	123.43	2.63	0.09	0.62
12.09	19.60	29.74	4.11	122.33	2.64	0.09	0.62
12.10	18.82	28.59	4.24	121.12	2.65	0.09	0.62
12.11	17.94	27.27	4.39	119.69	2.67	0.09	0.62
12.12	16.99	25.86	4.57	118.11	2.69	0.09	0.62
12.13	16.03	24.43	4.77	116.44	2.71	0.09	0.62
12.14	15.10	23.04	4.98	114.76	2.73	0.09	0.62
12.15	14.26	21.75	5.20	113.13	2.75	0.08	0.62
12.16	13.60	20.69	5.40	111.78	2.76	0.08	0.62
12.17	13.17	19.99	5.56	111.06	2.78	0.08	0.62
12.18	12.90	19.57	5.67	110.92	2.79	0.08	0.62
12.19	12.70	19.24	5.77	111.07	2.79	0.08	0.62
12.20	12.47	18.87	5.89	111.22	2.80	0.08	0.62
12.21	12.23	18.48	6.02	111.35	2.81	0.08	0.62
12.22	11.99	18.10	6.16	111.45	2.82	0.08	0.62
12.23	11.77	17.74	6.29	111.52	2.83	0.08	0.62
12.24	11.57	17.41	6.41	111.56	2.84	0.08	0.62
12.25	11.40	17.14	6.51	111.63	2.85	0.08	0.62
12.26	11.23	16.87	6.63	111.77	2.86	0.08	0.62
12.27	11.05	16.57	6.76	111.99	2.87	0.08	0.62
12.28	10.83	16.23	6.92	112.23	2.88	0.08	0.62
12.29	10.60	15.85	7.09	112.46	2.89	0.08	0.62
12.30	10.36	15.46	7.28	112.64	2.91	0.08	0.62
12.31	10.12	15.09	7.48	112.77	2.92	0.08	0.62
12.32	9.90	14.73	7.66	112.86	2.93	0.08	0.62
12.33	9.72	14.43	7.82	112.90	2.94	0.08	0.62
12.34	9.55	14.16	7.97	112.90	2.95	0.08	0.62
12.35	9.38	13.89	8.13	112.88	2.96	0.08	0.62
12.36	9.18	13.57	8.31	112.82	2.97	0.08	0.62
12.37	8.96	13.21	8.53	112.71	2.98	0.08	0.62
12.38	8.72	12.83	8.77	112.54	3.00	0.08	0.62
12.39	8.48	12.45	9.02	112.31	3.01	0.08	0.92
12.40	8.25	12.07	9.28	112.04	3.03	0.08	0.89
12.41	8.04	11.74	9.52	111.74	3.04	0.08	0.87
12.42	7.87	11.46	9.73	111.48	3.05	0.08	0.85
12.43	7.73	11.23	9.90	111.26	3.06	0.08	0.83
12.44	7.60	11.03	10.07	111.08	3.07	0.08	0.81
12.45	7.47	10.81	10.26	110.89	3.08	0.08	0.80
12.46	7.32	10.56	10.47	110.64	3.09	0.08	0.78
12.47	7.16	10.31	10.71	110.36	3.10	0.08	0.76
12.48	7.00	10.05	10.95	110.03	3.12	0.08	0.74

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
12.49	6.85	9.81	11.18	109.70	3.13	0.08	0.72
12.50	6.71	9.59	11.40	109.38	3.14	0.08	0.71
12.51	6.61	9.43	11.57	109.12	3.15	0.08	0.69
12.52	6.53	9.30	11.71	108.93	3.15	0.08	0.69
12.53	6.47	9.20	11.83	108.77	3.16	0.08	0.68
12.54	6.40	9.08	11.96	108.59	3.17	0.08	0.67
12.55	6.32	8.96	12.10	108.39	3.17	0.08	0.66
12.56	6.24	8.83	12.26	108.17	3.18	0.07	0.65
12.57	6.16	8.70	12.41	107.95	3.19	0.07	0.64
12.58	6.09	8.58	12.55	107.73	3.19	0.07	0.63
12.59	6.03	8.48	12.68	107.54	3.20	0.07	0.62
12.60	5.99	8.42	12.75	107.43	3.20	0.07	0.62
12.61	5.98	8.40	12.79	107.38	3.20	0.07	0.62
12.62	5.98	8.40	12.79	107.38	3.20	0.07	0.62
12.63	5.98	8.40	12.79	107.38	3.20	0.07	0.62
12.64	5.98	8.40	12.79	107.38	3.20	0.07	0.62
12.65	5.98	8.40	12.79	107.38	3.20	0.07	0.62
12.66	5.98	8.39	12.79	107.38	3.20	0.07	0.62
12.67	5.98	8.39	12.79	107.39	3.20	0.07	0.62
12.68	5.98	8.39	12.79	107.35	3.20	0.07	0.61
12.69	5.98	8.39	12.78	107.23	3.20	0.07	0.61
12.70	5.98	8.39	12.75	107.00	3.20	0.07	0.61
12.71	5.98	8.39	12.71	106.67	3.20	0.07	0.61
12.72	5.98	8.39	12.67	106.31	3.20	0.07	0.61
12.73	5.98	8.39	12.63	105.93	3.20	0.07	0.61
12.74	5.98	8.39	12.59	105.56	3.19	0.07	0.61
12.75	5.98	8.39	12.54	105.20	3.19	0.07	0.61
12.76	5.98	8.39	12.51	104.88	3.19	0.07	0.61
12.77	5.98	8.38	12.47	104.57	3.19	0.07	0.61
12.78	5.98	8.38	12.43	104.21	3.19	0.07	0.61
12.79	5.98	8.38	12.38	103.76	3.18	0.07	0.61
12.80	5.98	8.38	12.31	103.22	3.18	0.07	0.61
12.81	5.98	8.38	12.25	102.63	3.18	0.07	0.61
12.82	5.98	8.38	12.17	102.02	3.18	0.07	0.61
12.83	5.98	8.38	12.10	101.42	3.17	0.07	0.61
12.84	5.98	8.38	12.04	100.86	3.17	0.07	0.61
12.85	5.98	8.38	11.98	100.38	3.17	0.07	0.61
12.86	5.98	8.38	11.93	99.93	3.16	0.07	0.61
12.87	5.98	8.38	11.87	99.44	3.16	0.07	0.61
12.88	5.98	8.37	11.81	98.87	3.16	0.07	0.61
12.89	5.98	8.37	11.73	98.21	3.15	0.07	0.61
12.90	5.98	8.37	11.65	97.51	3.15	0.07	0.61
12.91	5.98	8.37	11.56	96.79	3.15	0.07	0.61
12.92	5.98	8.37	11.48	96.10	3.14	0.07	0.61
12.93	5.98	8.37	11.41	95.47	3.14	0.07	0.61
12.94	5.98	8.37	11.34	94.91	3.14	0.07	0.61
12.95	5.98	8.37	11.28	94.36	3.13	0.07	0.61
12.96	5.98	8.37	11.20	93.74	3.13	0.07	0.61

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
12.97	5.98	8.37	11.12	93.00	3.12	0.07	0.61
12.98	5.98	8.37	11.02	92.16	3.12	0.07	0.61
12.99	5.98	8.36	10.91	91.28	3.12	0.07	0.61
13.00	5.98	8.36	10.81	90.40	3.11	0.07	0.61
13.01	5.98	8.36	10.71	89.56	3.10	0.07	0.61
13.02	5.98	8.36	10.62	88.81	3.10	0.07	0.61
13.03	5.95	8.32	10.59	88.06	3.10	0.07	0.60
13.04	5.88	8.21	10.62	87.17	3.10	0.07	0.59
13.05	5.76	8.01	10.73	86.03	3.11	0.07	0.58
13.06	5.62	7.78	10.88	84.68	3.11	0.07	0.56
13.07	5.46	7.53	11.05	83.21	3.12	0.07	0.54
13.08	5.30	7.27	11.23	81.69	3.13	0.07	0.53
13.09	5.14	7.02	11.42	80.21	3.14	0.07	0.51
13.10	5.00	6.79	11.61	78.83	3.15	0.07	0.49
13.11	4.87	6.58	11.79	77.64	3.16	0.07	0.48
13.12	4.74	6.37	12.01	76.51	3.17	0.07	0.46
13.13	4.58	6.12	12.31	75.29	3.18	0.07	0.44
13.14	4.39	5.80	12.73	73.82	3.20	0.07	0.42
13.15	4.16	5.44	13.25	72.12	3.22	0.07	0.39
13.16	3.93	5.06	13.89	70.26	3.25	0.07	0.36
13.17	3.69	4.67	14.62	68.32	3.28	0.07	0.34
13.18	3.46	4.30	15.43	66.41	3.31	0.07	0.31
13.19	3.25	3.97	16.28	64.62	3.34	0.07	0.29
13.20	3.09	3.71	17.04	63.17	3.37	0.07	0.27
13.21	2.98	3.53	17.61	62.14	3.39	0.07	0.25
13.22	2.90	3.41	18.03	61.42	3.40	0.07	0.25
13.23	2.83	3.30	18.43	60.73	3.41	0.07	0.24
13.24	2.76	3.17	18.91	59.96	3.43	0.07	0.23
13.25	2.68	3.04	19.44	59.14	3.44	0.07	0.22
13.26	2.60	2.91	20.01	58.32	3.46	0.07	0.21
13.27	2.52	2.79	20.59	57.53	3.48	0.07	0.20
13.28	2.46	2.69	21.15	56.83	3.49	0.07	0.19
13.29	2.41	2.62	21.55	56.40	3.51	0.07	0.19
13.30	2.39	2.58	21.77	56.25	3.51	0.07	0.19
13.31	2.39	2.58	21.85	56.35	3.51	0.07	0.19
13.32	2.39	2.58	21.92	56.51	3.52	0.07	0.19
13.33	2.39	2.58	21.99	56.68	3.52	0.07	0.19
13.34	2.39	2.58	22.06	56.85	3.52	0.07	0.18
13.35	2.39	2.58	22.13	57.02	3.52	0.07	0.18
13.36	2.39	2.58	22.20	57.17	3.52	0.07	0.18
13.37	2.40	2.58	22.21	57.36	3.52	0.07	0.19
13.38	2.44	2.65	21.86	57.92	3.51	0.07	0.19
13.39	2.52	2.79	21.15	58.95	3.49	0.07	0.20
13.40	2.65	3.00	20.15	60.43	3.47	0.07	0.21
13.41	2.80	3.24	19.17	62.07	3.44	0.07	0.23
13.42	2.96	3.49	18.27	63.78	3.41	0.07	0.25
13.43	3.12	3.75	17.47	65.46	3.38	0.07	0.27
13.44	3.28	3.99	16.79	67.04	3.36	0.07	0.29

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
13.45	3.41	4.21	16.25	68.45	3.34	0.07	0.30
13.46	3.54	4.42	15.78	69.69	3.32	0.07	0.32
13.47	3.68	4.64	15.30	70.96	3.30	0.07	0.33
13.48	3.85	4.91	14.75	72.42	3.28	0.07	0.35
13.49	4.06	5.24	14.14	74.14	3.26	0.07	0.37
13.50	4.29	5.61	13.54	76.00	3.23	0.07	0.40
13.51	4.53	6.00	12.99	77.89	3.21	0.07	0.43
13.52	4.76	6.38	12.50	79.71	3.19	0.07	0.46
13.53	4.99	6.74	12.08	81.39	3.17	0.07	0.48
13.54	5.18	7.05	11.75	82.84	3.16	0.07	0.50
13.55	5.30	7.23	11.58	83.75	3.15	0.07	0.52
13.56	5.34	7.29	11.54	84.16	3.15	0.07	0.52
13.57	5.30	7.23	11.64	84.17	3.15	0.07	0.52
13.58	5.26	7.15	11.76	84.12	3.16	0.07	0.51
13.59	5.20	7.07	11.90	84.06	3.16	0.07	0.50
13.60	5.15	6.98	12.04	83.99	3.17	0.07	0.50
13.61	5.10	6.89	12.18	83.92	3.18	0.07	0.49
13.62	5.05	6.81	12.31	83.85	3.18	0.07	0.49
13.63	5.01	6.75	12.43	83.82	3.19	0.07	0.48
13.64	4.99	6.71	12.53	84.00	3.19	0.07	0.48
13.65	4.98	6.69	12.62	84.44	3.20	0.07	0.48
13.66	4.98	6.69	12.73	85.13	3.20	0.07	0.48
13.67	4.98	6.68	12.85	85.90	3.21	0.07	0.48
13.68	4.98	6.68	12.98	86.70	3.21	0.07	0.48
13.69	4.98	6.68	13.10	87.51	3.22	0.07	0.48
13.70	4.98	6.67	13.22	88.27	3.22	0.07	0.48
13.71	4.98	6.67	13.33	88.94	3.23	0.07	0.48
13.72	4.99	6.69	13.38	89.53	3.23	0.07	0.48
13.73	5.04	6.77	13.32	90.10	3.23	0.07	0.48
13.74	5.13	6.90	13.15	90.73	3.22	0.07	0.49
13.75	5.24	7.08	12.91	91.47	3.21	0.07	0.51
13.76	5.37	7.28	12.67	92.28	3.20	0.07	0.52
13.77	5.51	7.49	12.42	93.10	3.19	0.07	0.54
13.78	5.64	7.70	12.19	93.90	3.18	0.07	0.55
13.79	5.76	7.89	11.99	94.63	3.17	0.07	0.56
13.80	5.87	8.06	11.81	95.27	3.16	0.07	0.58
13.81	5.91	8.12	11.74	95.39	3.15	0.07	0.58
13.82	5.87	8.06	11.78	94.90	3.16	0.07	0.58
13.83	5.75	7.87	11.92	93.77	3.16	0.07	0.56
13.84	5.61	7.63	12.11	92.40	3.17	0.07	0.55
13.85	5.45	7.38	12.32	90.92	3.18	0.07	0.53
13.86	5.29	7.12	12.55	89.39	3.19	0.07	0.51
13.87	5.13	6.87	12.79	87.90	3.20	0.07	0.49
13.88	4.99	6.64	13.03	86.52	3.21	0.07	0.47
13.89	4.87	6.44	13.25	85.37	3.22	0.07	0.46
13.90	4.76	6.26	13.50	84.53	3.23	0.07	0.45
13.91	4.64	6.08	13.81	83.92	3.25	0.07	0.43
13.92	4.51	5.86	14.22	83.35	3.26	0.07	0.42

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
13.93	4.36	5.62	14.70	82.68	3.28	0.07	0.40
13.94	4.20	5.37	15.26	81.92	3.30	0.07	0.38
13.95	4.04	5.11	15.86	81.10	3.33	0.07	0.37
13.96	3.89	4.87	16.48	80.27	3.35	0.07	0.35
13.97	3.75	4.65	17.09	79.48	3.37	0.07	0.33
13.98	3.65	4.49	17.58	78.97	3.39	0.07	0.32
13.99	3.60	4.41	17.91	78.91	3.40	0.07	0.31
14.00	3.59	4.38	18.10	79.31	3.40	0.07	0.31
14.01	3.59	4.38	18.25	79.94	3.41	0.07	0.31
14.02	3.59	4.38	18.42	80.64	3.41	0.07	0.31
14.03	3.59	4.38	18.59	81.35	3.42	0.07	0.31
14.04	3.59	4.37	18.76	82.05	3.42	0.07	0.31
14.05	3.59	4.37	18.92	82.70	3.43	0.07	0.31
14.06	3.59	4.37	19.06	83.27	3.43	0.07	0.31
14.07	3.62	4.42	19.04	84.08	3.43	0.07	0.32
14.08	3.69	4.53	18.84	85.34	3.43	0.07	0.32
14.09	3.81	4.72	18.46	87.16	3.41	0.07	0.34
14.10	3.96	4.95	18.04	89.29	3.40	0.07	0.35
14.11	4.12	5.19	17.63	91.58	3.39	0.07	0.37
14.12	4.28	5.45	17.25	93.91	3.37	0.07	0.39
14.13	4.43	5.69	16.91	96.17	3.36	0.07	0.41
14.14	4.57	5.91	16.62	98.23	3.35	0.07	0.42
14.15	4.70	6.11	16.37	100.02	3.34	0.07	0.44
14.16	4.83	6.32	16.11	101.74	3.33	0.07	0.45
14.17	4.99	6.56	15.78	103.62	3.32	0.07	0.47
14.18	5.19	6.88	15.39	105.86	3.31	0.07	0.49
14.19	5.42	7.23	14.99	108.37	3.29	0.07	0.52
14.20	5.66	7.60	14.60	110.99	3.28	0.07	0.54
14.21	5.90	7.97	14.25	113.61	3.26	0.07	0.57
14.22	6.13	8.33	13.94	116.08	3.25	0.07	0.59
14.23	6.33	8.65	13.68	118.29	3.24	0.07	0.62
14.24	6.51	8.92	13.46	120.06	3.23	0.08	0.64
14.25	6.67	9.18	13.24	121.52	3.22	0.08	0.66
14.26	6.85	9.46	12.99	122.85	3.21	0.08	0.68
14.27	7.06	9.78	12.71	124.30	3.20	0.08	0.70
14.28	7.29	10.14	12.41	125.87	3.19	0.08	0.72
14.29	7.53	10.51	12.13	127.46	3.17	0.08	0.75
14.30	7.77	10.88	11.86	128.99	3.16	0.08	0.78
14.31	7.99	11.22	11.62	130.40	3.15	0.08	0.80
14.32	8.19	11.52	11.42	131.60	3.14	0.08	0.82
14.33	8.34	11.76	11.27	132.50	3.13	0.08	0.84
14.34	8.47	11.96	11.14	133.18	3.13	0.08	0.85
14.35	8.60	12.15	11.01	133.76	3.12	0.08	0.87
14.36	8.74	12.37	10.86	134.41	3.11	0.08	0.88
14.37	8.90	12.61	10.71	135.10	3.10	0.08	0.90
14.38	9.06	12.86	10.56	135.78	3.10	0.08	0.92
14.39	9.22	13.09	10.42	136.42	3.09	0.08	0.94
14.40	9.36	13.31	10.29	137.00	3.08	0.08	0.95

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
14.41	9.47	13.48	10.20	137.48	3.08	0.08	0.96
14.42	9.51	13.54	10.18	137.87	3.08	0.08	0.97
14.43	9.49	13.50	10.24	138.25	3.08	0.08	0.96
14.44	9.42	13.39	10.35	138.65	3.09	0.08	0.96
14.45	9.35	13.27	10.48	139.09	3.09	0.08	0.95
14.46	9.27	13.14	10.62	139.54	3.10	0.08	0.94
14.47	9.19	13.01	10.76	139.97	3.11	0.08	0.93
14.48	9.11	12.88	10.90	140.36	3.11	0.08	0.92
14.49	9.05	12.77	11.02	140.70	3.12	0.08	0.91
14.50	8.95	12.62	11.16	140.80	3.13	0.08	0.90
14.51	8.79	12.35	11.37	140.49	3.14	0.08	0.88
14.52	8.53	11.95	11.69	139.70	3.15	0.08	0.85
14.53	8.20	11.43	12.12	138.56	3.17	0.08	0.82
14.54	7.84	10.87	12.62	137.17	3.20	0.08	0.78
14.55	7.47	10.28	13.18	135.57	3.22	0.08	0.73
14.56	7.10	9.71	13.79	133.84	3.24	0.08	0.69
14.57	6.76	9.17	14.40	132.06	3.27	0.08	0.65
14.58	6.45	8.70	14.99	130.38	3.29	0.07	0.62
14.59	6.23	8.35	15.45	129.06	3.31	0.07	0.60
14.60	6.07	8.10	15.81	128.02	3.32	0.07	0.58
14.61	5.94	7.90	16.10	127.12	3.33	0.07	0.56
14.62	5.80	7.67	16.45	126.07	3.35	0.07	0.55
14.63	5.64	7.42	16.84	124.92	3.36	0.07	0.53
14.64	5.48	7.17	17.26	123.70	3.37	0.07	0.51
14.65	5.33	6.92	17.69	122.49	3.39	0.07	0.49
14.66	5.18	6.70	18.11	121.34	3.40	0.07	0.48
14.67	5.08	6.53	18.44	120.47	3.41	0.07	0.47
14.68	5.05	6.49	18.53	120.25	3.42	0.07	0.46
14.69	5.11	6.57	18.37	120.70	3.41	0.07	0.47
14.70	5.22	6.74	18.05	121.64	3.40	0.07	0.48
14.71	5.34	6.93	17.70	122.67	3.39	0.07	0.50
14.72	5.48	7.13	17.35	123.73	3.38	0.07	0.51
14.73	5.61	7.33	17.01	124.77	3.37	0.07	0.52
14.74	5.73	7.53	16.71	125.73	3.36	0.07	0.54
14.75	5.85	7.70	16.45	126.58	3.35	0.07	0.55
14.76	5.93	7.82	16.26	127.12	3.34	0.07	0.56
14.77	5.97	7.88	16.16	127.28	3.34	0.07	0.56
14.78	5.98	7.89	16.11	127.11	3.33	0.07	0.56
14.79	5.98	7.88	16.08	126.80	3.33	0.07	0.56
14.80	5.98	7.88	16.05	126.45	3.33	0.07	0.56
14.81	5.98	7.88	16.01	126.10	3.33	0.07	0.56
14.82	5.98	7.87	15.97	125.75	3.33	0.07	0.56
14.83	5.98	7.87	15.94	125.43	3.33	0.07	0.56
14.84	5.98	7.87	15.91	125.14	3.33	0.07	0.56
14.85	6.01	7.91	15.81	125.13	3.32	0.07	0.57
14.86	6.09	8.03	15.62	125.42	3.32	0.07	0.57
14.87	6.21	8.22	15.33	126.02	3.31	0.07	0.59
14.88	6.36	8.44	15.01	126.69	3.29	0.07	0.60

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
14.89	6.52	8.68	14.68	127.37	3.28	0.07	0.62
14.90	6.68	8.92	14.35	128.03	3.27	0.08	0.64
14.91	6.83	9.15	14.05	128.63	3.26	0.08	0.65
14.92	6.98	9.37	13.79	129.14	3.24	0.08	0.67
14.93	7.10	9.55	13.57	129.55	3.24	0.08	0.68
14.94	7.21	9.71	13.37	129.90	3.23	0.08	0.69
14.95	7.32	9.89	13.17	130.23	3.22	0.08	0.71
14.96	7.46	10.09	12.94	130.58	3.21	0.08	0.72
14.97	7.61	10.32	12.70	130.95	3.20	0.08	0.74
14.98	7.77	10.55	12.44	131.31	3.19	0.08	0.75
14.99	7.93	10.79	12.20	131.63	3.18	0.08	0.77
15.00	8.08	11.02	11.97	131.90	3.17	0.08	0.79
15.01	8.21	11.22	11.77	132.12	3.16	0.08	0.80
15.02	8.28	11.32	11.67	132.11	3.15	0.08	0.81
15.03	8.26	11.28	11.68	131.77	3.15	0.08	0.81
15.04	8.14	11.10	11.81	131.06	3.16	0.08	0.79
15.05	7.98	10.84	12.00	130.11	3.17	0.08	0.77
15.06	7.80	10.56	12.22	129.06	3.18	0.08	0.75
15.07	7.61	10.27	12.46	127.95	3.19	0.08	0.73
15.08	7.43	9.99	12.70	126.83	3.20	0.08	0.71
15.09	7.26	9.72	12.94	125.76	3.21	0.08	0.69
15.10	7.11	9.49	13.15	124.81	3.22	0.08	0.68
15.11	7.03	9.37	13.29	124.51	3.22	0.08	0.67
15.12	7.03	9.37	13.34	124.93	3.23	0.08	0.67
15.13	7.09	9.46	13.32	126.03	3.23	0.08	0.68
15.14	7.17	9.57	13.31	127.31	3.22	0.08	0.68
15.15	7.25	9.68	13.29	128.69	3.22	0.08	0.69
15.16	7.33	9.80	13.27	130.08	3.22	0.08	0.70
15.17	7.40	9.91	13.26	131.43	3.22	0.08	0.71
15.18	7.47	10.02	13.25	132.67	3.22	0.08	0.72
15.19	7.55	10.13	13.21	133.79	3.22	0.08	0.72
15.20	7.68	10.32	13.09	135.08	3.22	0.08	0.74
15.21	7.89	10.63	12.86	136.71	3.21	0.08	0.76
15.22	8.17	11.05	12.56	138.73	3.19	0.08	0.79
15.23	8.48	11.52	12.24	140.96	3.18	0.08	0.82
15.24	8.81	12.01	11.92	143.25	3.16	0.08	0.86
15.25	9.14	12.51	11.63	145.49	3.15	0.08	0.89
15.26	9.45	12.97	11.37	147.58	3.14	0.08	0.93
15.27	9.73	13.39	11.16	149.40	3.13	0.08	0.96
15.28	9.98	13.76	10.96	150.84	3.12	0.08	0.98
15.29	10.24	14.14	10.75	151.99	3.11	0.08	1.01
15.30	10.54	14.59	10.49	153.01	3.09	0.08	1.04
15.31	10.89	15.12	10.19	154.06	3.08	0.08	1.08
15.32	11.28	15.70	9.88	155.12	3.06	0.08	1.12
15.33	11.68	16.30	9.58	156.11	3.05	0.08	1.16
15.34	12.07	16.88	9.30	156.99	3.03	0.08	1.21
15.35	12.44	17.43	9.05	157.72	3.02	0.08	1.24
15.36	12.75	17.90	8.84	158.29	3.00	0.08	1.28

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
15.37	13.02	18.30	8.67	158.66	2.99	0.08	0.62
15.38	13.27	18.67	8.51	158.89	2.98	0.09	0.62
15.39	13.54	19.06	8.34	159.04	2.97	0.09	0.62
15.40	13.85	19.52	8.15	159.15	2.96	0.09	0.62
15.41	14.18	20.01	7.96	159.21	2.95	0.09	0.62
15.42	14.52	20.51	7.76	159.20	2.94	0.09	0.62
15.43	14.84	20.95	7.59	159.01	2.93	0.09	0.62
15.44	15.14	21.34	7.44	158.78	2.92	0.09	0.62
15.45	15.34	21.61	7.33	158.46	2.91	0.09	0.62
15.46	15.33	21.58	7.31	157.78	2.91	0.09	0.62
15.47	15.11	21.26	7.37	156.64	2.91	0.09	0.62
15.48	14.74	20.72	7.49	155.11	2.92	0.09	0.62
15.49	14.32	20.12	7.62	153.37	2.93	0.09	0.62
15.50	13.88	19.49	7.77	151.49	2.94	0.09	0.62
15.51	13.45	18.82	7.94	149.51	2.95	0.09	0.62
15.52	13.03	18.19	8.11	147.60	2.96	0.08	0.62
15.53	12.66	17.63	8.27	145.87	2.97	0.08	0.62
15.54	12.35	17.15	8.42	144.50	2.98	0.08	0.62
15.55	12.06	16.71	8.58	143.44	2.99	0.08	0.62
15.56	11.75	16.25	8.77	142.51	3.00	0.08	0.62
15.57	11.40	15.71	9.01	141.45	3.01	0.08	1.12
15.58	11.01	15.12	9.27	140.22	3.03	0.08	1.08
15.59	10.61	14.52	9.57	138.88	3.04	0.08	1.04
15.60	10.22	13.92	9.88	137.48	3.06	0.08	0.99
15.61	9.85	13.37	10.18	136.11	3.08	0.08	0.95
15.62	9.54	12.89	10.46	134.86	3.09	0.08	0.92
15.63	9.34	12.59	10.66	134.15	3.10	0.08	0.90
15.64	9.24	12.43	10.78	133.96	3.11	0.08	0.89
15.65	9.20	12.38	10.84	134.21	3.11	0.08	0.88
15.66	9.17	12.32	10.92	134.50	3.12	0.08	0.88
15.67	9.13	12.25	11.00	134.80	3.12	0.08	0.88
15.68	9.09	12.19	11.08	135.10	3.12	0.08	0.87
15.69	9.05	12.13	11.16	135.38	3.13	0.08	0.87
15.70	9.01	12.07	11.24	135.63	3.13	0.08	0.86
15.71	8.98	12.02	11.30	135.82	3.13	0.08	0.86
15.72	8.94	11.95	11.37	135.92	3.14	0.08	0.85
15.73	8.89	11.87	11.46	135.95	3.14	0.08	0.85
15.74	8.82	11.76	11.56	135.95	3.15	0.08	0.84
15.75	8.74	11.64	11.68	135.93	3.15	0.08	0.83
15.76	8.66	11.52	11.80	135.90	3.16	0.08	0.82
15.77	8.58	11.40	11.92	135.87	3.16	0.08	0.81
15.78	8.51	11.28	12.04	135.83	3.17	0.08	0.81
15.79	8.44	11.17	12.15	135.78	3.17	0.08	0.80
15.80	8.38	11.08	12.24	135.67	3.18	0.08	0.79
15.81	8.33	11.00	12.32	135.46	3.18	0.08	0.79
15.82	8.27	10.90	12.40	135.13	3.19	0.08	0.78
15.83	8.20	10.79	12.48	134.71	3.19	0.08	0.77
15.84	8.12	10.67	12.58	134.26	3.19	0.08	0.76

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
15.85	8.04	10.55	12.68	133.79	3.20	0.08	0.75
15.86	7.96	10.43	12.79	133.32	3.20	0.08	0.74
15.87	7.89	10.31	12.88	132.88	3.21	0.08	0.74
15.88	7.82	10.22	12.97	132.49	3.21	0.08	0.73
15.89	7.77	10.13	13.03	132.01	3.21	0.08	0.72
15.90	7.71	10.04	13.08	131.37	3.22	0.08	0.72
15.91	7.65	9.94	13.13	130.52	3.22	0.08	0.71
15.92	7.57	9.83	13.18	129.54	3.22	0.08	0.70
15.93	7.49	9.71	13.24	128.51	3.22	0.08	0.69
15.94	7.41	9.58	13.30	127.45	3.22	0.08	0.68
15.95	7.34	9.47	13.36	126.44	3.23	0.08	0.68
15.96	7.27	9.36	13.41	125.52	3.23	0.08	0.67
15.97	7.21	9.28	13.45	124.78	3.23	0.08	0.66
15.98	7.18	9.23	13.47	124.26	3.23	0.08	0.66
15.99	7.17	9.21	13.45	123.90	3.23	0.08	0.66
16.00	7.17	9.21	13.42	123.58	3.23	0.08	0.66
16.01	7.17	9.20	13.39	123.22	3.23	0.08	0.66
16.02	7.17	9.20	13.36	122.84	3.23	0.08	0.66
16.03	7.17	9.19	13.32	122.47	3.23	0.08	0.66
16.04	7.17	9.19	13.29	122.11	3.22	0.08	0.66
16.05	7.17	9.19	13.26	121.79	3.22	0.08	0.66
16.06	7.17	9.18	13.25	121.62	3.22	0.08	0.66
16.07	7.17	9.18	13.25	121.64	3.22	0.08	0.66
16.08	7.17	9.17	13.28	121.85	3.22	0.08	0.66
16.09	7.17	9.17	13.32	122.13	3.23	0.08	0.65
16.10	7.17	9.17	13.36	122.43	3.23	0.08	0.65
16.11	7.17	9.16	13.40	122.74	3.23	0.08	0.65
16.12	7.17	9.16	13.44	123.05	3.23	0.08	0.65
16.13	7.17	9.15	13.47	123.33	3.23	0.08	0.65
16.14	7.17	9.15	13.50	123.58	3.23	0.08	0.65
16.15	7.17	9.15	13.54	123.86	3.23	0.08	0.65
16.16	7.17	9.14	13.59	124.22	3.24	0.08	0.65
16.17	7.17	9.14	13.64	124.70	3.24	0.08	0.65
16.18	7.17	9.14	13.71	125.25	3.24	0.08	0.65
16.19	7.17	9.13	13.78	125.84	3.24	0.08	0.65
16.20	7.17	9.13	13.85	126.43	3.25	0.08	0.65
16.21	7.17	9.12	13.92	126.99	3.25	0.08	0.65
16.22	7.17	9.12	13.98	127.50	3.25	0.08	0.65
16.23	7.20	9.16	13.99	128.08	3.25	0.08	0.65
16.24	7.31	9.30	13.87	129.09	3.25	0.08	0.66
16.25	7.50	9.59	13.62	130.64	3.24	0.08	0.68
16.26	7.78	9.99	13.29	132.67	3.22	0.08	0.71
16.27	8.08	10.43	12.94	134.89	3.21	0.08	0.74
16.28	8.40	10.89	12.60	137.16	3.19	0.08	0.78
16.29	8.72	11.35	12.28	139.37	3.18	0.08	0.81
16.30	9.02	11.78	12.01	141.42	3.17	0.08	0.84
16.31	9.28	12.16	11.77	143.20	3.16	0.08	0.87
16.32	9.53	12.51	11.56	144.64	3.15	0.08	0.89

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
16.33	9.78	12.88	11.33	145.88	3.14	0.08	0.92
16.34	10.09	13.32	11.04	147.08	3.12	0.08	0.95
16.35	10.44	13.83	10.73	148.37	3.11	0.08	0.99
16.36	10.83	14.39	10.40	149.69	3.09	0.08	1.03
16.37	11.23	14.97	10.08	150.96	3.07	0.08	1.07
16.38	11.63	15.53	9.79	152.10	3.06	0.08	1.11
16.39	11.99	16.05	9.54	153.09	3.04	0.08	1.15
16.40	12.30	16.51	9.32	153.87	3.03	0.08	1.18
16.41	12.60	16.93	9.12	154.42	3.02	0.08	1.21
16.42	12.93	17.40	8.90	154.78	3.01	0.08	1.24
16.43	13.32	17.96	8.63	155.01	2.99	0.08	0.62
16.44	13.76	18.60	8.34	155.16	2.97	0.09	0.62
16.45	14.24	19.28	8.05	155.18	2.96	0.09	0.62
16.46	14.72	19.96	7.77	155.07	2.94	0.09	0.62
16.47	15.18	20.58	7.52	154.71	2.92	0.09	0.62
16.48	15.60	21.13	7.30	154.26	2.91	0.09	0.62
16.49	15.98	21.62	7.12	153.86	2.89	0.09	0.62
16.50	16.39	22.16	6.93	153.57	2.88	0.09	0.62
16.51	16.89	22.82	6.72	153.35	2.87	0.09	0.62
16.52	17.51	23.62	6.48	153.05	2.85	0.09	0.62
16.53	18.19	24.52	6.22	152.57	2.83	0.09	0.62
16.54	18.91	25.45	5.97	151.89	2.81	0.09	0.62
16.55	19.63	26.37	5.73	151.05	2.79	0.09	0.62
16.56	20.30	27.23	5.51	150.11	2.77	0.09	0.62
16.57	20.90	27.99	5.33	149.16	2.76	0.09	0.62
16.58	21.30	28.49	5.20	148.14	2.75	0.09	0.62
16.59	21.52	28.75	5.11	146.91	2.74	0.09	0.62
16.60	21.60	28.82	5.04	145.35	2.73	0.09	0.62
16.61	21.66	28.86	4.97	143.49	2.72	0.09	0.62
16.62	21.72	28.90	4.89	141.45	2.72	0.09	0.62
16.63	21.78	28.95	4.81	139.33	2.71	0.09	0.62
16.64	21.84	28.99	4.73	137.23	2.70	0.09	0.62
16.65	21.90	29.02	4.66	135.28	2.70	0.09	0.62
16.66	21.94	29.04	4.60	133.61	2.69	0.09	0.62
16.67	21.87	28.92	4.58	132.44	2.69	0.09	0.62
16.68	21.67	28.64	4.60	131.63	2.69	0.09	0.62
16.69	21.34	28.20	4.65	131.01	2.69	0.09	0.62
16.70	20.97	27.70	4.70	130.30	2.70	0.09	0.62
16.71	20.58	27.17	4.77	129.54	2.71	0.09	0.62
16.72	20.18	26.63	4.83	128.76	2.71	0.09	0.62
16.73	19.79	26.12	4.90	128.01	2.72	0.09	0.62
16.74	19.45	25.65	4.96	127.32	2.72	0.09	0.62
16.75	19.15	25.25	5.03	126.92	2.73	0.09	0.62
16.76	18.88	24.89	5.10	127.07	2.74	0.09	0.62
16.77	18.59	24.52	5.21	127.78	2.75	0.09	0.62
16.78	18.26	24.10	5.35	128.83	2.76	0.09	0.62
16.79	17.90	23.63	5.50	129.93	2.77	0.09	0.62
16.80	17.51	23.14	5.66	131.02	2.78	0.09	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
16.81	17.13	22.64	5.83	132.04	2.80	0.09	0.62
16.82	16.78	22.18	5.99	132.93	2.81	0.09	0.62
16.83	16.46	21.76	6.14	133.67	2.82	0.09	0.62
16.84	16.15	21.36	6.29	134.32	2.83	0.09	0.62
16.85	15.79	20.88	6.46	134.99	2.85	0.09	0.62
16.86	15.33	20.28	6.69	135.72	2.86	0.09	0.62
16.87	14.79	19.58	6.97	136.46	2.88	0.09	0.62
16.88	14.21	18.80	7.29	137.09	2.91	0.09	0.62
16.89	13.61	18.01	7.64	137.54	2.93	0.08	0.62
16.90	13.02	17.17	8.01	137.62	2.95	0.08	0.62
16.91	12.48	16.39	8.39	137.50	2.98	0.08	0.62
16.92	12.02	15.74	8.72	137.27	3.00	0.08	0.62
16.93	11.69	15.26	8.99	137.19	3.01	0.08	1.09
16.94	11.46	14.92	9.20	137.31	3.02	0.08	1.07
16.95	11.26	14.64	9.40	137.62	3.04	0.08	1.05
16.96	11.04	14.31	9.64	137.92	3.05	0.08	1.02
16.97	10.80	13.97	9.89	138.18	3.06	0.08	1.00
16.98	10.56	13.62	10.16	138.37	3.08	0.08	0.97
16.99	10.33	13.29	10.42	138.49	3.09	0.08	0.95
17.00	10.12	12.99	10.67	138.54	3.10	0.08	0.93
17.01	9.98	12.78	10.84	138.59	3.11	0.08	0.91
17.02	9.94	12.72	10.91	138.74	3.11	0.08	0.91
17.03	9.99	12.79	10.87	139.03	3.11	0.08	0.91
17.04	10.10	12.93	10.78	139.42	3.11	0.08	0.92
17.05	10.21	13.09	10.69	139.85	3.10	0.08	0.93
17.06	10.33	13.25	10.59	140.29	3.10	0.08	0.95
17.07	10.45	13.41	10.49	140.71	3.09	0.08	0.96
17.08	10.56	13.57	10.40	141.11	3.09	0.08	0.97
17.09	10.66	13.70	10.32	141.45	3.09	0.08	0.98
17.10	10.73	13.79	10.26	141.47	3.08	0.08	0.98
17.11	10.76	13.82	10.20	141.07	3.08	0.08	0.99
17.12	10.76	13.82	10.14	140.23	3.08	0.08	0.99
17.13	10.76	13.82	10.07	139.19	3.07	0.08	0.99
17.14	10.76	13.81	10.00	138.07	3.07	0.08	0.99
17.15	10.76	13.81	9.92	136.90	3.06	0.08	0.99
17.16	10.76	13.80	9.84	135.76	3.06	0.08	0.99
17.17	10.76	13.79	9.76	134.70	3.06	0.08	0.99
17.18	10.75	13.77	9.71	133.75	3.05	0.08	0.98
17.19	10.66	13.64	9.73	132.69	3.05	0.08	0.97
17.20	10.47	13.37	9.82	131.34	3.06	0.08	0.95
17.21	10.18	12.96	10.00	129.60	3.07	0.08	0.93
17.22	9.86	12.50	10.21	127.61	3.08	0.08	0.89
17.23	9.52	12.01	10.45	125.47	3.09	0.08	0.86
17.24	9.17	11.52	10.70	123.28	3.10	0.08	0.82
17.25	8.84	11.05	10.97	121.16	3.12	0.08	0.79
17.26	8.54	10.62	11.23	119.22	3.13	0.08	0.76
17.27	8.28	10.26	11.47	117.62	3.14	0.08	0.73
17.28	8.04	9.91	11.73	116.28	3.15	0.08	0.71

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
17.29	7.79	9.55	12.05	115.02	3.17	0.08	0.68
17.30	7.49	9.12	12.45	113.58	3.19	0.08	0.65
17.31	7.15	8.65	12.93	111.90	3.21	0.08	0.62
17.32	6.81	8.16	13.49	110.07	3.23	0.07	0.58
17.33	6.46	7.68	14.09	108.16	3.26	0.07	0.55
17.34	6.14	7.22	14.72	106.27	3.28	0.07	0.52
17.35	5.86	6.82	15.33	104.53	3.31	0.07	0.49
17.36	5.68	6.56	15.76	103.44	3.32	0.07	0.47
17.37	5.60	6.46	15.97	103.09	3.33	0.07	0.46
17.38	5.62	6.47	15.98	103.40	3.33	0.07	0.46
17.39	5.64	6.50	15.98	103.84	3.33	0.07	0.46
17.40	5.67	6.53	15.97	104.31	3.33	0.07	0.47
17.41	5.69	6.57	15.96	104.80	3.33	0.07	0.47
17.42	5.72	6.60	15.95	105.28	3.33	0.07	0.47
17.43	5.74	6.63	15.94	105.72	3.33	0.07	0.47
17.44	5.76	6.66	15.93	106.09	3.33	0.07	0.48
17.45	5.78	6.68	15.93	106.44	3.33	0.07	0.48
17.46	5.80	6.71	15.93	106.82	3.33	0.07	0.48
17.47	5.82	6.73	15.93	107.26	3.33	0.07	0.48
17.48	5.85	6.77	15.93	107.77	3.33	0.07	0.48
17.49	5.87	6.80	15.93	108.31	3.33	0.07	0.49
17.50	5.90	6.84	15.92	108.85	3.33	0.07	0.49
17.51	5.93	6.87	15.92	109.36	3.33	0.07	0.49
17.52	5.95	6.90	15.92	109.83	3.33	0.07	0.49
17.53	5.98	6.94	15.89	110.34	3.33	0.07	0.50
17.54	6.05	7.03	15.80	111.10	3.32	0.07	0.50
17.55	6.16	7.18	15.63	112.20	3.32	0.07	0.51
17.56	6.30	7.37	15.42	113.60	3.31	0.07	0.53
17.57	6.45	7.58	15.19	115.13	3.30	0.07	0.54
17.58	6.61	7.80	14.96	116.72	3.29	0.07	0.56
17.59	6.77	8.02	14.75	118.29	3.28	0.07	0.57
17.60	6.92	8.22	14.57	119.75	3.28	0.07	0.59
17.61	7.05	8.40	14.41	121.03	3.27	0.08	0.60
17.62	7.16	8.55	14.28	122.12	3.26	0.08	0.61
17.63	7.27	8.71	14.15	123.18	3.26	0.08	0.62
17.64	7.40	8.88	14.00	124.34	3.25	0.08	0.63
17.65	7.54	9.08	13.85	125.67	3.25	0.08	0.65
17.66	7.70	9.29	13.68	127.11	3.24	0.08	0.66
17.67	7.86	9.51	13.52	128.57	3.23	0.08	0.68
17.68	8.02	9.72	13.37	129.99	3.23	0.08	0.69
17.69	8.16	9.92	13.24	131.29	3.22	0.08	0.71
17.70	8.27	10.07	13.14	132.32	3.22	0.08	0.72
17.71	8.32	10.13	13.12	132.88	3.22	0.08	0.72
17.72	8.30	10.10	13.17	133.00	3.22	0.08	0.72
17.73	8.23	10.00	13.28	132.83	3.22	0.08	0.71
17.74	8.16	9.90	13.40	132.64	3.23	0.08	0.71
17.75	8.08	9.78	13.54	132.43	3.23	0.08	0.70
17.76	8.00	9.67	13.68	132.21	3.24	0.08	0.69

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
17.77	7.92	9.56	13.81	131.99	3.25	0.08	0.68
17.78	7.85	9.46	13.93	131.79	3.25	0.08	0.68
17.79	7.80	9.37	14.04	131.62	3.26	0.08	0.67
17.80	7.74	9.29	14.15	131.49	3.26	0.08	0.66
17.81	7.68	9.21	14.27	131.39	3.26	0.08	0.66
17.82	7.61	9.11	14.42	131.28	3.27	0.08	0.65
17.83	7.53	9.00	14.58	131.15	3.28	0.08	0.64
17.84	7.45	8.88	14.75	131.00	3.28	0.08	0.63
17.85	7.38	8.77	14.92	130.84	3.29	0.08	0.63
17.86	7.30	8.66	15.08	130.69	3.30	0.08	0.62
17.87	7.24	8.57	15.23	130.54	3.30	0.08	0.61
17.88	7.19	8.51	15.34	130.51	3.31	0.08	0.61
17.89	7.18	8.48	15.41	130.64	3.31	0.08	0.61
17.90	7.17	8.47	15.45	130.93	3.31	0.08	0.61
17.91	7.17	8.47	15.50	131.28	3.31	0.08	0.61
17.92	7.17	8.47	15.55	131.66	3.31	0.08	0.60
17.93	7.17	8.46	15.60	132.05	3.32	0.08	0.60
17.94	7.17	8.46	15.65	132.42	3.32	0.08	0.60
17.95	7.17	8.46	15.70	132.76	3.32	0.08	0.60
17.96	7.18	8.46	15.73	133.06	3.32	0.08	0.60
17.97	7.21	8.50	15.70	133.39	3.32	0.08	0.61
17.98	7.27	8.58	15.60	133.79	3.32	0.08	0.61
17.99	7.36	8.70	15.45	134.31	3.31	0.08	0.62
18.00	7.46	8.83	15.28	134.88	3.30	0.08	0.63
18.01	7.56	8.97	15.10	135.47	3.30	0.08	0.64
18.02	7.67	9.11	14.93	136.06	3.29	0.08	0.65
18.03	7.77	9.25	14.77	136.61	3.28	0.08	0.66
18.04	7.86	9.37	14.63	137.10	3.28	0.08	0.67
18.05	7.98	9.53	14.45	137.69	3.27	0.08	0.68
18.06	8.18	9.80	14.14	138.61	3.26	0.08	0.70
18.07	8.50	10.23	13.68	139.95	3.24	0.08	0.73
18.08	8.89	10.77	13.14	141.52	3.22	0.08	0.77
18.09	9.33	11.36	12.60	143.10	3.19	0.08	0.81
18.10	9.78	11.98	12.07	144.56	3.17	0.08	0.86
18.11	10.23	12.59	11.59	145.85	3.15	0.08	0.90
18.12	10.65	13.15	11.17	146.90	3.13	0.08	0.94
18.13	11.01	13.65	10.82	147.72	3.11	0.08	0.98
18.14	11.42	14.19	10.47	148.65	3.09	0.08	1.01
18.15	11.92	14.88	10.07	149.86	3.07	0.08	1.06
18.16	12.59	15.79	9.59	151.38	3.05	0.08	1.13
18.17	13.36	16.84	9.08	152.88	3.02	0.08	1.20
18.18	14.20	17.98	8.57	154.16	2.99	0.09	0.62
18.19	15.06	19.14	8.11	155.13	2.96	0.09	0.62
18.20	15.88	20.26	7.69	155.77	2.93	0.09	0.62
18.21	16.64	21.24	7.34	155.96	2.91	0.09	0.62
18.22	17.27	22.03	7.08	155.87	2.89	0.09	0.62
18.23	17.74	22.61	6.87	155.38	2.88	0.09	0.62
18.24	18.09	23.04	6.70	154.49	2.86	0.09	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
18.25	18.43	23.44	6.53	153.18	2.85	0.09	0.62
18.26	18.80	23.89	6.35	151.63	2.84	0.09	0.62
18.27	19.20	24.37	6.15	149.89	2.82	0.09	0.62
18.28	19.60	24.84	5.96	148.05	2.81	0.09	0.62
18.29	19.98	25.29	5.78	146.19	2.79	0.09	0.62
18.30	20.32	25.69	5.62	144.46	2.78	0.09	0.62
18.31	20.53	25.92	5.51	142.91	2.77	0.09	0.62
18.32	20.55	25.93	5.45	141.43	2.77	0.09	0.62
18.33	20.40	25.71	5.44	139.82	2.77	0.09	0.62
18.34	20.15	25.38	5.44	137.95	2.77	0.09	0.62
18.35	19.89	25.02	5.43	135.90	2.77	0.09	0.62
18.36	19.62	24.64	5.43	133.77	2.76	0.09	0.62
18.37	19.34	24.27	5.43	131.69	2.76	0.09	0.62
18.38	19.09	23.93	5.42	129.75	2.76	0.09	0.62
18.39	18.87	23.62	5.42	128.05	2.76	0.09	0.62
18.40	18.63	23.30	5.45	126.92	2.77	0.09	0.62
18.41	18.33	22.92	5.51	126.28	2.77	0.09	0.62
18.42	17.94	22.41	5.62	125.98	2.78	0.09	0.62
18.43	17.48	21.83	5.75	125.63	2.79	0.09	0.62
18.44	16.99	21.20	5.91	125.21	2.80	0.09	0.62
18.45	16.48	20.56	6.07	124.73	2.82	0.09	0.62
18.46	16.00	19.94	6.23	124.23	2.83	0.09	0.62
18.47	15.55	19.37	6.39	123.73	2.84	0.09	0.62
18.48	15.17	18.88	6.53	123.32	2.85	0.08	0.62
18.49	14.80	18.41	6.69	123.09	2.86	0.08	0.62
18.50	14.40	17.90	6.87	123.02	2.88	0.08	0.62
18.51	13.93	17.29	7.11	123.01	2.89	0.08	0.62
18.52	13.39	16.61	7.40	122.88	2.91	0.08	0.62
18.53	12.83	15.88	7.72	122.59	2.93	0.08	0.62
18.54	12.27	15.11	8.08	122.08	2.96	0.08	0.62
18.55	11.73	14.39	8.44	121.46	2.98	0.08	0.62
18.56	11.25	13.73	8.79	120.78	3.00	0.08	0.98
18.57	10.87	13.21	9.10	120.18	3.02	0.08	0.94
18.58	10.56	12.79	9.36	119.69	3.03	0.08	0.91
18.59	10.28	12.40	9.62	119.27	3.05	0.08	0.89
18.60	9.97	11.98	9.91	118.77	3.06	0.08	0.86
18.61	9.63	11.52	10.26	118.15	3.08	0.08	0.82
18.62	9.28	11.04	10.64	117.43	3.10	0.08	0.79
18.63	8.93	10.57	11.03	116.62	3.12	0.08	0.76
18.64	8.61	10.13	11.43	115.78	3.14	0.08	0.72
18.65	8.32	9.75	11.80	114.98	3.16	0.08	0.70
18.66	8.10	9.44	12.10	114.31	3.17	0.08	0.67
18.67	7.91	9.19	12.38	113.74	3.18	0.08	0.66
18.68	7.73	8.94	12.66	113.18	3.20	0.08	0.64
18.69	7.53	8.66	12.99	112.50	3.21	0.08	0.62
18.70	7.30	8.36	13.37	111.72	3.23	0.08	0.60
18.71	7.08	8.05	13.77	110.88	3.24	0.07	0.58
18.72	6.86	7.75	14.19	110.01	3.26	0.07	0.55

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
18.73	6.66	7.48	14.59	109.18	3.28	0.07	0.53
18.74	6.49	7.26	14.95	108.48	3.29	0.07	0.52
18.75	6.37	7.09	15.24	108.03	3.30	0.07	0.51
18.76	6.28	6.96	15.49	107.80	3.31	0.07	0.50
18.77	6.19	6.84	15.75	107.68	3.32	0.07	0.49
18.78	6.09	6.70	16.04	107.52	3.33	0.07	0.48
18.79	5.98	6.56	16.37	107.33	3.34	0.07	0.47
18.80	5.87	6.41	16.71	107.11	3.36	0.07	0.46
18.81	5.77	6.27	17.04	106.89	3.37	0.07	0.45
18.82	5.68	6.15	17.34	106.66	3.38	0.07	0.44
18.83	5.62	6.06	17.57	106.56	3.38	0.07	0.43
18.84	5.59	6.02	17.72	106.67	3.39	0.07	0.43
18.85	5.58	6.01	17.81	106.98	3.39	0.07	0.43
18.86	5.58	6.00	17.89	107.42	3.40	0.07	0.43
18.87	5.58	6.00	17.98	107.89	3.40	0.07	0.43
18.88	5.58	6.00	18.07	108.38	3.40	0.07	0.43
18.89	5.58	6.00	18.15	108.86	3.40	0.07	0.43
18.90	5.58	5.99	18.23	109.30	3.41	0.07	0.43
18.91	5.58	5.99	18.31	109.68	3.41	0.07	0.43
18.92	5.60	6.02	18.29	110.12	3.41	0.07	0.43
18.93	5.65	6.09	18.19	110.70	3.41	0.07	0.43
18.94	5.74	6.20	17.99	111.47	3.40	0.07	0.44
18.95	5.84	6.33	17.76	112.35	3.39	0.07	0.45
18.96	5.94	6.46	17.53	113.28	3.38	0.07	0.46
18.97	6.05	6.60	17.30	114.23	3.38	0.07	0.47
18.98	6.15	6.74	17.09	115.14	3.37	0.07	0.48
18.99	6.25	6.86	16.90	115.96	3.36	0.07	0.49
19.00	6.33	6.96	16.75	116.63	3.36	0.07	0.50
19.01	6.40	7.06	16.59	117.15	3.35	0.07	0.50
19.02	6.48	7.16	16.42	117.58	3.35	0.07	0.51
19.03	6.57	7.28	16.22	118.01	3.34	0.07	0.52
19.04	6.67	7.41	15.99	118.48	3.33	0.07	0.53
19.05	6.78	7.55	15.76	118.97	3.32	0.07	0.54
19.06	6.88	7.68	15.54	119.44	3.31	0.07	0.55
19.07	6.98	7.82	15.34	119.87	3.31	0.07	0.56
19.08	7.07	7.93	15.16	120.25	3.30	0.07	0.57
19.09	7.13	8.01	15.03	120.44	3.29	0.07	0.57
19.10	7.17	8.05	14.95	120.38	3.29	0.08	0.57
19.11	7.17	8.06	14.91	120.08	3.29	0.08	0.58
19.12	7.17	8.05	14.86	119.66	3.29	0.08	0.58
19.13	7.17	8.05	14.81	119.20	3.29	0.08	0.57
19.14	7.17	8.05	14.76	118.73	3.28	0.08	0.57
19.15	7.17	8.04	14.71	118.27	3.28	0.07	0.57
19.16	7.17	8.04	14.66	117.83	3.28	0.07	0.57
19.17	7.17	8.04	14.62	117.44	3.28	0.07	0.57
19.18	7.15	8.00	14.62	116.99	3.28	0.07	0.57
19.19	7.10	7.93	14.68	116.40	3.28	0.07	0.57
19.20	7.01	7.81	14.80	115.61	3.29	0.07	0.56

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
19.21	6.91	7.68	14.94	114.70	3.29	0.07	0.55
19.22	6.81	7.54	15.09	113.72	3.30	0.07	0.54
19.23	6.70	7.39	15.25	112.73	3.30	0.07	0.53
19.24	6.60	7.25	15.41	111.76	3.31	0.07	0.52
19.25	6.50	7.13	15.56	110.88	3.31	0.07	0.51
19.26	6.42	7.02	15.69	110.12	3.32	0.07	0.50
19.27	6.35	6.92	15.82	109.42	3.32	0.07	0.49
19.28	6.27	6.81	15.95	108.68	3.33	0.07	0.49
19.29	6.18	6.69	16.12	107.83	3.33	0.07	0.48
19.30	6.08	6.55	16.31	106.87	3.34	0.07	0.47
19.31	5.97	6.41	16.51	105.86	3.35	0.07	0.46
19.32	5.87	6.27	16.72	104.85	3.36	0.07	0.45
19.33	5.77	6.13	16.93	103.89	3.36	0.07	0.44
19.34	5.68	6.01	17.13	103.02	3.37	0.07	0.43
19.35	5.62	5.93	17.26	102.35	3.37	0.07	0.42
19.36	5.58	5.89	17.30	101.84	3.38	0.07	0.42
19.37	5.58	5.88	17.26	101.42	3.37	0.07	0.42
19.38	5.58	5.87	17.19	100.97	3.37	0.07	0.42
19.39	5.58	5.87	17.11	100.48	3.37	0.07	0.42
19.40	5.58	5.87	17.03	99.97	3.37	0.07	0.42
19.41	5.58	5.87	16.95	99.46	3.36	0.07	0.42
19.42	5.58	5.86	16.88	98.99	3.36	0.07	0.42
19.43	5.58	5.86	16.82	98.58	3.36	0.07	0.42
19.44	5.58	5.86	16.76	98.22	3.36	0.07	0.42
19.45	5.58	5.86	16.71	97.86	3.36	0.07	0.42
19.46	5.58	5.85	16.64	97.45	3.35	0.07	0.42
19.47	5.58	5.85	16.57	96.99	3.35	0.07	0.42
19.48	5.58	5.85	16.49	96.49	3.35	0.07	0.42
19.49	5.58	5.85	16.41	95.98	3.35	0.07	0.42
19.50	5.58	5.85	16.34	95.49	3.34	0.07	0.42
19.51	5.58	5.84	16.27	95.04	3.34	0.07	0.42
19.52	5.58	5.84	16.21	94.66	3.34	0.07	0.42
19.53	5.58	5.84	16.16	94.35	3.34	0.07	0.42
19.54	5.58	5.84	16.12	94.06	3.33	0.07	0.42
19.55	5.58	5.83	16.07	93.75	3.33	0.07	0.42
19.56	5.58	5.83	16.02	93.39	3.33	0.07	0.42
19.57	5.58	5.83	15.96	93.02	3.33	0.07	0.42
19.58	5.58	5.83	15.90	92.65	3.33	0.07	0.42
19.59	5.58	5.82	15.85	92.30	3.32	0.07	0.42
19.60	5.58	5.82	15.80	91.98	3.32	0.07	0.42
19.61	5.58	5.82	15.77	91.74	3.32	0.07	0.42
19.62	5.57	5.81	15.77	91.57	3.32	0.07	0.41
19.63	5.56	5.79	15.78	91.44	3.32	0.07	0.41
19.64	5.55	5.78	15.81	91.30	3.32	0.07	0.41
19.65	5.54	5.76	15.83	91.15	3.32	0.07	0.41
19.66	5.52	5.74	15.86	91.00	3.33	0.07	0.41
19.67	5.51	5.72	15.89	90.85	3.33	0.07	0.41
19.68	5.50	5.70	15.92	90.71	3.33	0.07	0.41

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
19.69	5.49	5.68	15.94	90.59	3.33	0.07	0.41
19.70	5.45	5.64	16.04	90.44	3.33	0.07	0.40
19.71	5.40	5.56	16.22	90.24	3.34	0.07	0.40
19.72	5.31	5.45	16.51	89.96	3.35	0.07	0.39
19.73	5.21	5.32	16.85	89.63	3.36	0.07	0.38
19.74	5.11	5.18	17.23	89.26	3.37	0.07	0.37
19.75	5.00	5.04	17.64	88.86	3.39	0.07	0.36
19.76	4.90	4.90	18.04	88.46	3.40	0.07	0.35
19.77	4.81	4.78	18.43	88.07	3.41	0.07	0.34
19.78	4.78	4.75	18.58	88.19	3.42	0.07	0.34
19.79	4.93	4.94	18.15	89.69	3.40	0.07	0.35
19.80	5.29	5.40	17.17	92.76	3.37	0.07	0.39
19.81	5.80	6.06	15.99	96.96	3.33	0.07	0.43
19.82	6.37	6.80	14.91	101.47	3.29	0.07	0.49
19.83	6.97	7.58	13.99	106.03	3.25	0.07	0.54
19.84	7.56	8.35	13.23	110.45	3.22	0.08	0.60
19.85	8.13	9.08	12.61	114.52	3.19	0.08	0.65
19.86	8.63	9.73	12.14	118.07	3.17	0.08	0.69
19.87	9.07	10.30	11.75	121.09	3.16	0.08	0.74
19.88	9.53	10.89	11.39	123.99	3.14	0.08	0.78
19.89	10.06	11.57	10.99	127.15	3.12	0.08	0.83
19.90	10.68	12.37	10.57	130.76	3.10	0.08	0.88
19.91	11.35	13.24	10.17	134.60	3.08	0.08	0.95
19.92	12.04	14.13	9.80	138.47	3.06	0.08	1.01
19.93	12.72	15.01	9.47	142.19	3.04	0.08	1.07
19.94	13.36	15.82	9.20	145.59	3.02	0.08	1.13
19.95	13.88	16.49	9.00	148.37	3.01	0.08	1.18
19.96	14.03	16.69	8.94	149.20	3.01	0.09	1.19
19.97	13.81	16.39	9.03	148.08	3.01	0.08	1.17
19.98	13.25	15.66	9.27	145.14	3.03	0.08	1.12
19.99	12.61	14.82	9.56	141.75	3.04	0.08	1.06
20.00	11.92	13.93	9.91	138.06	3.06	0.08	1.00
20.01	11.23	13.03	10.30	134.24	3.08	0.08	0.93
20.02	10.56	12.16	10.73	130.49	3.11	0.08	0.87
20.03	9.96	11.38	11.16	126.99	3.13	0.08	0.81
20.04	9.45	10.72	11.57	124.02	3.15	0.08	0.77
20.05	9.01	10.15	11.97	121.46	3.17	0.08	0.73
20.06	8.59	9.60	12.40	118.99	3.19	0.08	0.69
20.07	8.11	8.98	12.94	116.18	3.21	0.08	0.64
20.08	7.58	8.28	13.63	112.93	3.24	0.08	0.59
20.09	7.02	7.56	14.46	109.37	3.27	0.07	0.54
20.10	6.46	6.84	15.44	105.66	3.31	0.07	0.49
20.11	5.94	6.16	16.55	101.97	3.35	0.07	0.44
20.12	5.47	5.56	17.72	98.53	3.39	0.07	0.40
20.13	5.15	5.15	18.67	96.18	3.42	0.07	0.37
20.14	4.99	4.94	19.26	95.10	3.44	0.07	0.35
20.15	4.95	4.88	19.51	95.15	3.45	0.07	0.35
20.16	4.92	4.85	19.70	95.46	3.45	0.07	0.35

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
20.17	4.90	4.81	19.91	95.78	3.46	0.07	0.34
20.18	4.87	4.77	20.13	96.11	3.46	0.07	0.34
20.19	4.84	4.74	20.35	96.42	3.47	0.07	0.34
20.20	4.82	4.71	20.55	96.70	3.48	0.07	0.34
20.21	4.80	4.68	20.73	96.94	3.48	0.07	0.33
20.22	4.78	4.65	20.90	97.19	3.49	0.07	0.33
20.23	4.76	4.63	21.08	97.48	3.49	0.07	0.33
20.24	4.74	4.60	21.29	97.85	3.50	0.07	0.33
20.25	4.71	4.56	21.54	98.27	3.51	0.07	0.33
20.26	4.69	4.53	21.81	98.70	3.51	0.07	0.32
20.27	4.66	4.49	22.08	99.13	3.52	0.07	0.32
20.28	4.64	4.46	22.34	99.53	3.53	0.07	0.32
20.29	4.61	4.42	22.58	99.88	3.53	0.07	0.32
20.30	4.62	4.43	22.68	100.39	3.54	0.07	0.32
20.31	4.69	4.52	22.47	101.47	3.53	0.07	0.32
20.32	4.83	4.70	21.96	103.24	3.52	0.07	0.34
20.33	5.04	4.96	21.27	105.60	3.50	0.07	0.35
20.34	5.27	5.26	20.59	108.19	3.48	0.07	0.38
20.35	5.51	5.56	19.94	110.87	3.46	0.07	0.40
20.36	5.75	5.86	19.36	113.51	3.44	0.07	0.42
20.37	5.97	6.15	18.87	115.97	3.43	0.07	0.44
20.38	6.17	6.40	18.46	118.14	3.41	0.07	0.46
20.39	6.36	6.64	18.08	120.04	3.40	0.07	0.47
20.40	6.57	6.91	17.65	121.93	3.39	0.07	0.49
20.41	6.84	7.24	17.13	124.06	3.37	0.07	0.52
20.42	7.15	7.64	16.56	126.48	3.35	0.07	0.55
20.43	7.49	8.07	16.00	129.05	3.33	0.08	0.58
20.44	7.83	8.51	15.48	131.63	3.31	0.08	0.61
20.45	8.17	8.94	15.01	134.09	3.29	0.08	0.64
20.46	8.49	9.33	14.61	136.30	3.28	0.08	0.67
20.47	8.76	9.68	14.28	138.17	3.26	0.08	0.69
20.48	9.01	10.00	13.98	139.74	3.25	0.08	0.71
20.49	9.29	10.34	13.65	141.19	3.24	0.08	0.74
20.50	9.62	10.76	13.27	142.74	3.22	0.08	0.77
20.51	9.99	11.23	12.86	144.42	3.21	0.08	0.80
20.52	10.38	11.73	12.46	146.12	3.19	0.08	0.84
20.53	10.78	12.23	12.08	147.75	3.17	0.08	0.87
20.54	11.17	12.71	11.74	149.23	3.15	0.08	0.91
20.55	11.51	13.15	11.44	150.51	3.14	0.08	0.94
20.56	11.80	13.50	11.21	151.44	3.13	0.08	0.96
20.57	12.02	13.78	11.03	151.99	3.12	0.08	0.98
20.58	12.21	14.02	10.86	152.25	3.11	0.08	1.00
20.59	12.42	14.28	10.67	152.38	3.10	0.08	1.02
20.60	12.65	14.57	10.47	152.49	3.09	0.08	1.04
20.61	12.89	14.86	10.26	152.56	3.08	0.08	1.06
20.62	13.13	15.16	10.06	152.59	3.07	0.08	1.08
20.63	13.35	15.44	9.88	152.57	3.06	0.08	1.10
20.64	13.55	15.68	9.73	152.53	3.05	0.08	1.12

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
20.65	13.72	15.90	9.59	152.43	3.05	0.08	1.14
20.66	13.89	16.10	9.46	152.25	3.04	0.08	1.15
20.67	14.07	16.33	9.31	151.97	3.03	0.08	1.17
20.68	14.29	16.60	9.13	151.61	3.02	0.08	1.19
20.69	14.52	16.89	8.95	151.17	3.01	0.09	1.21
20.70	14.76	17.19	8.77	150.67	3.00	0.09	0.62
20.71	15.00	17.48	8.59	150.14	2.99	0.09	0.62
20.72	15.21	17.74	8.43	149.60	2.98	0.09	0.62
20.73	15.39	17.96	8.30	149.09	2.97	0.09	0.62
20.74	15.46	18.05	8.23	148.46	2.97	0.09	0.62
20.75	15.44	18.01	8.20	147.64	2.96	0.09	0.62
20.76	15.34	17.88	8.20	146.55	2.96	0.09	0.62
20.77	15.23	17.73	8.19	145.33	2.96	0.09	0.62
20.78	15.11	17.58	8.19	144.03	2.96	0.09	0.62
20.79	14.99	17.42	8.19	142.72	2.96	0.09	0.62
20.80	14.88	17.27	8.19	141.47	2.96	0.09	0.62
20.81	14.77	17.13	8.19	140.34	2.96	0.09	0.62
20.82	14.66	16.98	8.21	139.41	2.97	0.09	0.62
20.83	14.48	16.74	8.28	138.66	2.97	0.09	0.62
20.84	14.21	16.40	8.41	137.97	2.98	0.08	0.62
20.85	13.86	15.96	8.60	137.19	2.99	0.08	0.62
20.86	13.48	15.47	8.81	136.27	3.00	0.08	1.11
20.87	13.08	14.96	9.04	135.27	3.01	0.08	1.07
20.88	12.69	14.46	9.28	134.23	3.03	0.08	1.03
20.89	12.31	13.99	9.52	133.20	3.04	0.08	1.00
20.90	11.98	13.57	9.75	132.24	3.05	0.08	0.97
20.91	11.73	13.24	9.94	131.61	3.06	0.08	0.95
20.92	11.52	12.97	10.12	131.32	3.07	0.08	0.93
20.93	11.33	12.73	10.32	131.30	3.08	0.08	0.91
20.94	11.11	12.45	10.54	131.28	3.10	0.08	0.89
20.95	10.88	12.15	10.80	131.22	3.11	0.08	0.87
20.96	10.64	11.85	11.07	131.11	3.12	0.08	0.85
20.97	10.40	11.55	11.34	130.94	3.14	0.08	0.82
20.98	10.19	11.27	11.60	130.75	3.15	0.08	0.81
20.99	10.00	11.03	11.83	130.54	3.16	0.08	0.79
21.00	9.83	10.82	12.04	130.28	3.17	0.08	0.77
21.01	9.66	10.60	12.26	129.95	3.18	0.08	0.76
21.02	9.46	10.35	12.51	129.51	3.19	0.08	0.74
21.03	9.24	10.07	12.81	128.97	3.20	0.08	0.72
21.04	9.00	9.76	13.14	128.35	3.22	0.08	0.70
21.05	8.76	9.46	13.49	127.67	3.23	0.08	0.68
21.06	8.53	9.17	13.85	126.97	3.25	0.08	0.66
21.07	8.33	8.91	14.18	126.29	3.26	0.08	0.64
21.08	8.16	8.70	14.45	125.71	3.27	0.08	0.62
21.09	8.04	8.54	14.66	125.20	3.28	0.08	0.61
21.10	7.94	8.41	14.83	124.72	3.29	0.08	0.60
21.11	7.83	8.28	15.00	124.17	3.29	0.08	0.59
21.12	7.72	8.13	15.20	123.56	3.30	0.08	0.58

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
21.13	7.60	7.98	15.41	122.92	3.31	0.08	0.57
21.14	7.48	7.83	15.62	122.27	3.32	0.08	0.56
21.15	7.37	7.69	15.83	121.65	3.32	0.07	0.55
21.16	7.27	7.56	16.02	121.09	3.33	0.07	0.54
21.17	7.27	7.55	16.03	121.02	3.33	0.07	0.54
21.18	7.38	7.69	15.81	121.55	3.32	0.07	0.55
21.19	7.62	7.98	15.37	122.68	3.31	0.08	0.57
21.20	7.91	8.34	14.87	124.00	3.29	0.08	0.60
21.21	8.22	8.73	14.36	125.35	3.27	0.08	0.62
21.22	8.54	9.12	13.88	126.65	3.25	0.08	0.65
21.23	8.85	9.51	13.45	127.84	3.23	0.08	0.68
21.24	9.14	9.86	13.07	128.86	3.21	0.08	0.70
21.25	9.40	10.18	12.74	129.75	3.20	0.08	0.73
21.26	9.72	10.58	12.37	130.84	3.18	0.08	0.76
21.27	10.15	11.11	11.91	132.25	3.16	0.08	0.79
21.28	10.72	11.81	11.35	133.99	3.14	0.08	0.84
21.29	11.36	12.60	10.77	135.74	3.11	0.08	0.90
21.30	12.04	13.44	10.22	137.37	3.08	0.08	0.96
21.31	12.72	14.29	9.71	138.77	3.05	0.08	1.02
21.32	13.38	15.09	9.27	139.91	3.03	0.08	1.08
21.33	13.97	15.82	8.90	140.77	3.01	0.08	1.13
21.34	14.44	16.40	8.62	141.29	2.99	0.08	0.62
21.35	14.81	16.86	8.39	141.46	2.98	0.09	0.62
21.36	15.13	17.25	8.19	141.33	2.96	0.09	0.62
21.37	15.48	17.68	7.98	141.01	2.95	0.09	0.62
21.38	15.87	18.14	7.75	140.59	2.94	0.09	0.62
21.39	16.27	18.63	7.52	140.07	2.92	0.09	0.62
21.40	16.66	19.09	7.30	139.41	2.91	0.09	0.62
21.41	17.03	19.52	7.11	138.70	2.89	0.09	0.62
21.42	17.36	19.89	6.94	138.03	2.88	0.09	0.62
21.43	17.66	20.24	6.80	137.61	2.87	0.09	0.62
21.44	17.99	20.62	6.67	137.48	2.86	0.09	0.62
21.45	18.39	21.08	6.53	137.58	2.85	0.09	0.62
21.46	18.86	21.62	6.37	137.69	2.84	0.09	0.62
21.47	19.36	22.20	6.20	137.75	2.83	0.09	0.62
21.48	19.88	22.79	6.04	137.76	2.82	0.09	0.62
21.49	20.38	23.37	5.89	137.72	2.80	0.09	0.62
21.50	20.84	23.90	5.76	137.64	2.79	0.09	0.62
21.51	21.21	24.32	5.65	137.52	2.78	0.09	0.62
21.52	21.44	24.57	5.59	137.36	2.78	0.09	0.62
21.53	21.53	24.67	5.56	137.15	2.78	0.09	0.62
21.54	21.54	24.68	5.55	136.88	2.77	0.09	0.62
21.55	21.56	24.68	5.53	136.57	2.77	0.09	0.62
21.56	21.57	24.69	5.52	136.25	2.77	0.09	0.62
21.57	21.59	24.70	5.50	135.92	2.77	0.09	0.62
21.58	21.60	24.70	5.49	135.61	2.77	0.09	0.62
21.59	21.62	24.71	5.48	135.32	2.77	0.09	0.62
21.60	21.54	24.61	5.49	135.05	2.77	0.09	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
21.61	21.27	24.29	5.54	134.69	2.77	0.09	0.62
21.62	20.78	23.71	5.66	134.21	2.78	0.09	0.62
21.63	20.13	22.94	5.82	133.56	2.80	0.09	0.62
21.64	19.41	22.10	6.01	132.79	2.81	0.09	0.62
21.65	18.67	21.22	6.22	131.92	2.83	0.09	0.62
21.66	17.93	20.35	6.44	130.98	2.85	0.09	0.62
21.67	17.24	19.53	6.66	130.02	2.86	0.09	0.62
21.68	16.63	18.81	6.86	129.12	2.88	0.09	0.62
21.69	16.15	18.24	7.05	128.50	2.89	0.09	0.62
21.70	15.73	17.74	7.22	128.15	2.90	0.09	0.62
21.71	15.33	17.26	7.42	128.01	2.91	0.09	0.62
21.72	14.86	16.69	7.65	127.76	2.93	0.08	0.62
21.73	14.36	16.07	7.93	127.38	2.95	0.08	0.62
21.74	13.85	15.44	8.22	126.91	2.97	0.08	0.62
21.75	13.35	14.82	8.52	126.35	2.98	0.08	0.62
21.76	12.89	14.26	8.82	125.74	3.00	0.08	1.02
21.77	12.50	13.78	9.09	125.16	3.02	0.08	0.98
21.78	12.16	13.36	9.33	124.62	3.03	0.08	0.95
21.79	11.83	12.94	9.59	124.05	3.05	0.08	0.92
21.80	11.45	12.47	9.89	123.36	3.06	0.08	0.89
21.81	11.03	11.95	10.25	122.50	3.08	0.08	0.85
21.82	10.58	11.40	10.66	121.49	3.10	0.08	0.81
21.83	10.12	10.84	11.10	120.36	3.12	0.08	0.77
21.84	9.69	10.31	11.56	119.18	3.15	0.08	0.74
21.85	9.31	9.83	12.00	118.02	3.17	0.08	0.70
21.86	8.99	9.44	12.39	117.00	3.18	0.08	0.67
21.87	8.72	9.11	12.74	116.07	3.20	0.08	0.65
21.88	8.46	8.79	13.09	115.12	3.22	0.08	0.63
21.89	8.17	8.44	13.51	114.00	3.23	0.08	0.60
21.90	7.86	8.05	14.00	112.71	3.25	0.08	0.57
21.91	7.53	7.64	14.56	111.28	3.28	0.07	0.55
21.92	7.20	7.24	15.16	109.78	3.30	0.07	0.52
21.93	6.89	6.87	15.77	108.30	3.32	0.07	0.49
21.94	6.63	6.54	16.36	106.94	3.34	0.07	0.47
21.95	6.44	6.31	16.79	105.86	3.36	0.07	0.45
21.96	6.31	6.15	17.08	104.99	3.37	0.07	0.44
21.97	6.22	6.04	17.25	104.21	3.37	0.07	0.43
21.98	6.12	5.92	17.46	103.32	3.38	0.07	0.42
21.99	6.02	5.79	17.68	102.36	3.39	0.07	0.41
22.00	5.91	5.66	17.92	101.38	3.40	0.07	0.40
22.01	5.81	5.53	18.16	100.42	3.40	0.07	0.39
22.02	5.71	5.41	18.39	99.54	3.41	0.07	0.39
22.03	5.64	5.32	18.58	98.80	3.42	0.07	0.38
22.04	5.59	5.26	18.67	98.23	3.42	0.07	0.38
22.05	5.58	5.24	18.66	97.78	3.42	0.07	0.37
22.06	5.58	5.24	18.58	97.32	3.42	0.07	0.37
22.07	5.58	5.24	18.49	96.82	3.41	0.07	0.37
22.08	5.58	5.23	18.39	96.28	3.41	0.07	0.37

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
22.09	5.58	5.23	18.29	95.73	3.41	0.07	0.37
22.10	5.58	5.23	18.20	95.21	3.41	0.07	0.37
22.11	5.58	5.23	18.12	94.74	3.40	0.07	0.37
22.12	5.58	5.23	18.05	94.34	3.40	0.07	0.37
22.13	5.58	5.22	17.99	93.99	3.40	0.07	0.37
22.14	5.58	5.22	17.93	93.64	3.40	0.07	0.37
22.15	5.58	5.22	17.86	93.24	3.39	0.07	0.37
22.16	5.58	5.22	17.78	92.80	3.39	0.07	0.37
22.17	5.58	5.22	17.70	92.34	3.39	0.07	0.37
22.18	5.58	5.21	17.62	91.89	3.39	0.07	0.37
22.19	5.58	5.21	17.55	91.46	3.38	0.07	0.37
22.20	5.58	5.21	17.48	91.08	3.38	0.07	0.37
22.21	5.57	5.20	17.46	90.74	3.38	0.07	0.37
22.22	5.54	5.16	17.50	90.37	3.38	0.07	0.37
22.23	5.50	5.11	17.60	89.94	3.39	0.07	0.37
22.24	5.45	5.05	17.71	89.44	3.39	0.07	0.36
22.25	5.40	4.98	17.84	88.90	3.39	0.07	0.36
22.26	5.35	4.92	17.96	88.36	3.40	0.07	0.35
22.27	5.29	4.85	18.09	87.83	3.40	0.07	0.35
22.28	5.25	4.80	18.21	87.34	3.41	0.07	0.34
22.29	5.21	4.76	18.29	86.98	3.41	0.07	0.34
22.30	5.22	4.76	18.24	86.93	3.41	0.07	0.34
22.31	5.28	4.83	18.06	87.19	3.40	0.07	0.34
22.32	5.37	4.93	17.77	87.67	3.39	0.07	0.35
22.33	5.47	5.05	17.46	88.21	3.38	0.07	0.36
22.34	5.57	5.18	17.14	88.76	3.37	0.07	0.37
22.35	5.68	5.31	16.83	89.31	3.36	0.07	0.38
22.36	5.78	5.42	16.56	89.82	3.35	0.07	0.39
22.37	5.87	5.53	16.32	90.26	3.34	0.07	0.40
22.38	5.94	5.62	16.14	90.61	3.34	0.07	0.40
22.39	6.00	5.68	16.01	90.88	3.33	0.07	0.41
22.40	6.04	5.73	15.91	91.11	3.33	0.07	0.41
22.41	6.09	5.78	15.80	91.37	3.32	0.07	0.41
22.42	6.14	5.84	15.69	91.65	3.32	0.07	0.42
22.43	6.19	5.90	15.57	91.94	3.31	0.07	0.42
22.44	6.24	5.97	15.46	92.22	3.31	0.07	0.43
22.45	6.29	6.02	15.36	92.49	3.31	0.07	0.43
22.46	6.34	6.07	15.27	92.71	3.30	0.07	0.43
22.47	6.38	6.12	15.18	92.95	3.30	0.07	0.44
22.48	6.43	6.18	15.09	93.25	3.30	0.07	0.44
22.49	6.49	6.25	14.97	93.63	3.29	0.07	0.45
22.50	6.57	6.34	14.84	94.07	3.29	0.07	0.45
22.51	6.64	6.43	14.70	94.54	3.28	0.07	0.46
22.52	6.73	6.53	14.56	95.02	3.28	0.07	0.47
22.53	6.80	6.62	14.43	95.48	3.27	0.07	0.47
22.54	6.87	6.70	14.32	95.89	3.27	0.07	0.48
22.55	6.93	6.76	14.23	96.22	3.26	0.07	0.48
22.56	6.96	6.80	14.18	96.42	3.26	0.07	0.49

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
22.57	6.97	6.81	14.17	96.52	3.26	0.07	0.49
22.58	6.97	6.81	14.18	96.56	3.26	0.07	0.49
22.59	6.97	6.81	14.20	96.62	3.26	0.07	0.49
22.60	6.97	6.80	14.21	96.68	3.26	0.07	0.49
22.61	6.97	6.80	14.22	96.73	3.26	0.07	0.49
22.62	6.97	6.80	14.24	96.79	3.26	0.07	0.49
22.63	6.97	6.80	14.25	96.83	3.26	0.07	0.49
22.64	6.95	6.76	14.30	96.74	3.27	0.07	0.48
22.65	6.87	6.67	14.44	96.39	3.27	0.07	0.48
22.66	6.75	6.52	14.69	95.73	3.28	0.07	0.47
22.67	6.58	6.32	15.01	94.87	3.29	0.07	0.45
22.68	6.40	6.10	15.39	93.91	3.31	0.07	0.44
22.69	6.21	5.88	15.81	92.89	3.32	0.07	0.42
22.70	6.03	5.65	16.25	91.86	3.34	0.07	0.40
22.71	5.86	5.45	16.68	90.88	3.35	0.07	0.39
22.72	5.71	5.27	17.09	90.00	3.37	0.07	0.38
22.73	5.62	5.16	17.34	89.43	3.38	0.07	0.37
22.74	5.58	5.11	17.45	89.12	3.38	0.07	0.36
22.75	5.58	5.10	17.44	89.02	3.38	0.07	0.36
22.76	5.58	5.10	17.43	88.91	3.38	0.07	0.36
22.77	5.58	5.10	17.41	88.79	3.38	0.07	0.36
22.78	5.58	5.10	17.39	88.66	3.38	0.07	0.36
22.79	5.58	5.10	17.37	88.54	3.38	0.07	0.36
22.80	5.58	5.09	17.36	88.43	3.38	0.07	0.36
22.81	5.58	5.09	17.34	88.33	3.38	0.07	0.36
22.82	5.58	5.09	17.33	88.22	3.38	0.07	0.36
22.83	5.58	5.09	17.31	88.10	3.38	0.07	0.36
22.84	5.58	5.09	17.29	87.94	3.38	0.07	0.36
22.85	5.58	5.09	17.26	87.77	3.37	0.07	0.36
22.86	5.58	5.08	17.23	87.58	3.37	0.07	0.36
22.87	5.58	5.08	17.20	87.40	3.37	0.07	0.36
22.88	5.58	5.08	17.17	87.22	3.37	0.07	0.36
22.89	5.58	5.08	17.15	87.07	3.37	0.07	0.36
22.90	5.58	5.08	17.13	86.96	3.37	0.07	0.36
22.91	5.58	5.07	17.12	86.90	3.37	0.07	0.36
22.92	5.58	5.07	17.13	86.88	3.37	0.07	0.36
22.93	5.58	5.07	17.13	86.87	3.37	0.07	0.36
22.94	5.58	5.07	17.14	86.86	3.37	0.07	0.36
22.95	5.58	5.07	17.14	86.85	3.37	0.07	0.36
22.96	5.58	5.07	17.15	86.84	3.37	0.07	0.36
22.97	5.58	5.06	17.15	86.84	3.37	0.07	0.36
22.98	5.58	5.06	17.15	86.84	3.37	0.07	0.36
22.99	5.64	5.13	17.00	87.24	3.37	0.07	0.37
23.00	5.77	5.28	16.68	88.13	3.35	0.07	0.38
23.01	5.98	5.54	16.18	89.56	3.34	0.07	0.40
23.02	6.23	5.82	15.65	91.17	3.32	0.07	0.42
23.03	6.49	6.13	15.14	92.86	3.30	0.07	0.44
23.04	6.76	6.45	14.66	94.55	3.28	0.07	0.46

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
23.05	7.02	6.75	14.24	96.14	3.26	0.07	0.48
23.06	7.25	7.03	13.89	97.57	3.25	0.07	0.50
23.07	7.44	7.25	13.62	98.73	3.24	0.07	0.52
23.08	7.58	7.41	13.45	99.63	3.23	0.07	0.53
23.09	7.67	7.52	13.35	100.40	3.23	0.08	0.54
23.10	7.76	7.62	13.27	101.20	3.22	0.08	0.54
23.11	7.87	7.74	13.19	102.10	3.22	0.08	0.55
23.12	7.97	7.86	13.10	103.05	3.22	0.08	0.56
23.13	8.08	7.99	13.02	103.99	3.21	0.08	0.57
23.14	8.18	8.10	12.94	104.88	3.21	0.08	0.58
23.15	8.27	8.21	12.88	105.68	3.21	0.08	0.59
23.16	8.32	8.27	12.85	106.25	3.21	0.08	0.59
23.17	8.33	8.28	12.88	106.58	3.21	0.08	0.59
23.18	8.30	8.24	12.96	106.75	3.21	0.08	0.59
23.19	8.25	8.18	13.07	106.88	3.21	0.08	0.58
23.20	8.20	8.11	13.19	107.03	3.22	0.08	0.58
23.21	8.15	8.05	13.32	107.17	3.23	0.08	0.57
23.22	8.10	7.98	13.44	107.30	3.23	0.08	0.57
23.23	8.05	7.92	13.56	107.42	3.24	0.08	0.57
23.24	8.01	7.87	13.66	107.53	3.24	0.08	0.56
23.25	8.00	7.87	13.70	107.79	3.24	0.08	0.56
23.26	8.05	7.91	13.68	108.26	3.24	0.08	0.57
23.27	8.13	8.01	13.60	108.98	3.24	0.08	0.57
23.28	8.23	8.13	13.51	109.80	3.23	0.08	0.58
23.29	8.34	8.25	13.42	110.69	3.23	0.08	0.59
23.30	8.44	8.37	13.33	111.58	3.23	0.08	0.60
23.31	8.55	8.49	13.25	112.44	3.22	0.08	0.61
23.32	8.64	8.59	13.17	113.22	3.22	0.08	0.61
23.33	8.72	8.69	13.11	113.89	3.22	0.08	0.62
23.34	8.79	8.77	13.06	114.49	3.21	0.08	0.63
23.35	8.87	8.86	13.00	115.12	3.21	0.08	0.63
23.36	8.96	8.96	12.93	115.84	3.21	0.08	0.64
23.37	9.06	9.08	12.85	116.65	3.21	0.08	0.65
23.38	9.17	9.20	12.77	117.51	3.20	0.08	0.66
23.39	9.28	9.32	12.70	118.35	3.20	0.08	0.67
23.40	9.38	9.43	12.63	119.15	3.20	0.08	0.67
23.41	9.47	9.54	12.57	119.86	3.19	0.08	0.68
23.42	9.54	9.62	12.52	120.43	3.19	0.08	0.69
23.43	9.62	9.71	12.46	120.90	3.19	0.08	0.69
23.44	9.70	9.80	12.38	121.34	3.18	0.08	0.70
23.45	9.79	9.91	12.30	121.84	3.18	0.08	0.71
23.46	9.90	10.02	12.21	122.38	3.18	0.08	0.72
23.47	10.00	10.15	12.12	122.93	3.17	0.08	0.72
23.48	10.11	10.26	12.03	123.47	3.17	0.08	0.73
23.49	10.21	10.37	11.95	123.97	3.16	0.08	0.74
23.50	10.29	10.47	11.88	124.40	3.16	0.08	0.75
23.51	10.38	10.56	11.81	124.76	3.16	0.08	0.75
23.52	10.47	10.67	11.72	125.09	3.15	0.08	0.76

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
23.53	10.59	10.81	11.61	125.45	3.15	0.08	0.77
23.54	10.72	10.96	11.48	125.86	3.14	0.08	0.78
23.55	10.87	11.13	11.35	126.28	3.14	0.08	0.79
23.56	11.02	11.29	11.22	126.70	3.13	0.08	0.81
23.57	11.16	11.46	11.09	127.10	3.12	0.08	0.82
23.58	11.29	11.60	10.99	127.45	3.12	0.08	0.83
23.59	11.39	11.72	10.90	127.74	3.11	0.08	0.84
23.60	11.48	11.82	10.83	128.00	3.11	0.08	0.84
23.61	11.56	11.91	10.77	128.27	3.11	0.08	0.85
23.62	11.66	12.02	10.70	128.59	3.10	0.08	0.86
23.63	11.76	12.13	10.63	128.95	3.10	0.08	0.87
23.64	11.86	12.25	10.56	129.32	3.10	0.08	0.87
23.65	11.97	12.37	10.48	129.68	3.09	0.08	0.88
23.66	12.07	12.48	10.42	130.02	3.09	0.08	0.89
23.67	12.16	12.58	10.36	130.32	3.09	0.08	0.90
23.68	12.21	12.64	10.33	130.55	3.09	0.08	0.90
23.69	12.23	12.65	10.34	130.74	3.09	0.08	0.90
23.70	12.20	12.62	10.38	130.91	3.09	0.08	0.90
23.71	12.17	12.57	10.43	131.10	3.09	0.08	0.90
23.72	12.13	12.52	10.49	131.31	3.09	0.08	0.89
23.73	12.09	12.47	10.55	131.53	3.10	0.08	0.89
23.74	12.05	12.42	10.60	131.73	3.10	0.08	0.89
23.75	12.01	12.38	10.66	131.92	3.10	0.08	0.88
23.76	11.99	12.34	10.70	132.11	3.10	0.08	0.88
23.77	12.06	12.43	10.68	132.73	3.10	0.08	0.89
23.78	12.26	12.65	10.58	133.90	3.10	0.08	0.90
23.79	12.59	13.03	10.42	135.68	3.09	0.08	0.93
23.80	12.96	13.45	10.24	137.70	3.08	0.08	0.96
23.81	13.35	13.90	10.06	139.83	3.07	0.08	0.99
23.82	13.75	14.36	9.89	141.98	3.06	0.08	1.03
23.83	14.14	14.80	9.73	144.03	3.05	0.08	1.06
23.84	14.49	15.20	9.60	145.88	3.05	0.08	1.09
23.85	14.77	15.52	9.50	147.36	3.04	0.08	1.11
23.86	14.96	15.74	9.43	148.48	3.04	0.08	1.12
23.87	15.11	15.91	9.39	149.39	3.03	0.08	1.14
23.88	15.25	16.06	9.36	150.31	3.03	0.09	1.15
23.89	15.40	16.23	9.33	151.34	3.03	0.09	1.16
23.90	15.56	16.41	9.29	152.43	3.03	0.09	1.17
23.91	15.72	16.59	9.25	153.50	3.03	0.09	1.18
23.92	15.87	16.75	9.22	154.52	3.03	0.09	1.20
23.93	16.00	16.90	9.20	155.42	3.02	0.09	1.21
23.94	16.04	16.94	9.20	155.86	3.02	0.09	1.21
23.95	15.96	16.85	9.24	155.74	3.03	0.09	1.20
23.96	15.76	16.60	9.34	155.06	3.03	0.09	1.19
23.97	15.49	16.29	9.46	154.17	3.04	0.09	1.16
23.98	15.21	15.96	9.60	153.18	3.05	0.08	1.14
23.99	14.91	15.61	9.74	152.14	3.05	0.08	1.12
24.00	14.63	15.28	9.89	151.11	3.06	0.08	1.09

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
24.01	14.36	14.97	10.03	150.13	3.07	0.08	1.07
24.02	14.14	14.70	10.15	149.29	3.08	0.08	1.05
24.03	13.99	14.53	10.24	148.71	3.08	0.08	1.04
24.04	13.91	14.43	10.28	148.33	3.08	0.08	1.03
24.05	13.86	14.37	10.30	148.07	3.08	0.08	1.03
24.06	13.81	14.31	10.33	147.78	3.09	0.08	1.02
24.07	13.76	14.24	10.35	147.47	3.09	0.08	1.02
24.08	13.71	14.18	10.38	147.15	3.09	0.08	1.01
24.09	13.66	14.11	10.40	146.85	3.09	0.08	1.01
24.10	13.61	14.06	10.43	146.57	3.09	0.08	1.00
24.11	13.56	13.99	10.46	146.31	3.09	0.08	1.00
24.12	13.48	13.89	10.51	145.98	3.09	0.08	0.99
24.13	13.35	13.75	10.59	145.56	3.10	0.08	0.98
24.14	13.19	13.56	10.69	145.01	3.10	0.08	0.97
24.15	13.02	13.35	10.82	144.40	3.11	0.08	0.95
24.16	12.83	13.13	10.95	143.75	3.12	0.08	0.94
24.17	12.64	12.92	11.08	143.10	3.12	0.08	0.92
24.18	12.47	12.71	11.21	142.47	3.13	0.08	0.91
24.19	12.32	12.53	11.33	141.90	3.14	0.08	0.89
24.20	12.18	12.37	11.43	141.43	3.14	0.08	0.88
24.21	12.05	12.22	11.54	141.01	3.15	0.08	0.87
24.22	11.91	12.05	11.67	140.58	3.15	0.08	0.86
24.23	11.74	11.85	11.82	140.08	3.16	0.08	0.85
24.24	11.56	11.64	11.98	139.52	3.17	0.08	0.83
24.25	11.37	11.42	12.16	138.93	3.17	0.08	0.82
24.26	11.19	11.21	12.34	138.34	3.18	0.08	0.80
24.27	11.02	11.01	12.51	137.78	3.19	0.08	0.79
24.28	10.88	10.85	12.65	137.32	3.20	0.08	0.78
24.29	10.85	10.81	12.70	137.31	3.20	0.08	0.77
24.30	10.91	10.88	12.67	137.79	3.20	0.08	0.78
24.31	11.06	11.05	12.56	138.72	3.19	0.08	0.79
24.32	11.24	11.24	12.43	139.77	3.19	0.08	0.80
24.33	11.42	11.45	12.30	140.89	3.18	0.08	0.82
24.34	11.61	11.66	12.18	142.00	3.18	0.08	0.83
24.35	11.79	11.86	12.06	143.07	3.17	0.08	0.85
24.36	11.95	12.04	11.96	144.03	3.17	0.08	0.86
24.37	12.09	12.19	11.88	144.83	3.16	0.08	0.87
24.38	12.22	12.34	11.80	145.56	3.16	0.08	0.88
24.39	12.35	12.49	11.72	146.32	3.15	0.08	0.89
24.40	12.52	12.67	11.62	147.18	3.15	0.08	0.90
24.41	12.69	12.87	11.51	148.14	3.14	0.08	0.92
24.42	12.88	13.07	11.41	149.14	3.14	0.08	0.93
24.43	13.07	13.28	11.31	150.12	3.13	0.08	0.95
24.44	13.24	13.47	11.21	151.04	3.13	0.08	0.96
24.45	13.39	13.64	11.13	151.85	3.13	0.08	0.97
24.46	13.50	13.75	11.08	152.35	3.12	0.08	0.98
24.47	13.54	13.80	11.05	152.55	3.12	0.08	0.99
24.48	13.55	13.81	11.05	152.50	3.12	0.08	0.99

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
24.49	13.55	13.80	11.04	152.39	3.12	0.08	0.99
24.50	13.55	13.80	11.04	152.28	3.12	0.08	0.99
24.51	13.55	13.79	11.03	152.16	3.12	0.08	0.99
24.52	13.55	13.79	11.03	152.05	3.12	0.08	0.98
24.53	13.55	13.78	11.02	151.94	3.12	0.08	0.98
24.54	13.55	13.77	11.02	151.83	3.12	0.08	0.98
24.55	13.52	13.74	11.03	151.55	3.12	0.08	0.98
24.56	13.46	13.67	11.05	151.06	3.12	0.08	0.98
24.57	13.38	13.57	11.08	150.34	3.12	0.08	0.97
24.58	13.28	13.45	11.12	149.52	3.13	0.08	0.96
24.59	13.17	13.32	11.16	148.66	3.13	0.08	0.95
24.60	13.06	13.20	11.20	147.79	3.13	0.08	0.94
24.61	12.96	13.08	11.24	146.96	3.13	0.08	0.93
24.62	12.87	12.97	11.27	146.20	3.13	0.08	0.93
24.63	12.79	12.88	11.30	145.55	3.13	0.08	0.92
24.64	12.72	12.79	11.33	144.93	3.14	0.08	0.91
24.65	12.64	12.69	11.36	144.26	3.14	0.08	0.91
24.66	12.55	12.58	11.40	143.47	3.14	0.08	0.90
24.67	12.44	12.47	11.44	142.60	3.14	0.08	0.89
24.68	12.34	12.34	11.48	141.70	3.14	0.08	0.88
24.69	12.23	12.22	11.53	140.80	3.14	0.08	0.87
24.70	12.13	12.10	11.57	139.96	3.15	0.08	0.86
24.71	12.04	12.00	11.60	139.22	3.15	0.08	0.86
24.72	11.97	11.91	11.64	138.58	3.15	0.08	0.85
24.73	11.89	11.82	11.67	137.98	3.15	0.08	0.84
24.74	11.81	11.72	11.72	137.33	3.15	0.08	0.84
24.75	11.71	11.61	11.77	136.59	3.16	0.08	0.83
24.76	11.61	11.49	11.82	135.78	3.16	0.08	0.82
24.77	11.50	11.36	11.88	134.95	3.16	0.08	0.81
24.78	11.40	11.24	11.93	134.14	3.16	0.08	0.80
24.79	11.30	11.13	11.98	133.40	3.17	0.08	0.80
24.80	11.22	11.03	12.03	132.74	3.17	0.08	0.79
24.81	11.11	10.91	12.10	132.06	3.17	0.08	0.78
24.82	10.98	10.76	12.20	131.26	3.18	0.08	0.77
24.83	10.80	10.56	12.34	130.26	3.18	0.08	0.75
24.84	10.60	10.33	12.50	129.12	3.19	0.08	0.74
24.85	10.39	10.09	12.68	127.90	3.20	0.08	0.72
24.86	10.18	9.84	12.87	126.66	3.21	0.08	0.70
24.87	9.98	9.61	13.05	125.46	3.21	0.08	0.69
24.88	9.79	9.40	13.23	124.37	3.22	0.08	0.67
24.89	9.65	9.23	13.37	123.49	3.23	0.08	0.66
24.90	9.54	9.11	13.48	122.80	3.23	0.08	0.65
24.91	9.45	9.00	13.57	122.23	3.24	0.08	0.64
24.92	9.35	8.90	13.67	121.62	3.24	0.08	0.64
24.93	9.25	8.78	13.78	120.95	3.24	0.08	0.63
24.94	9.14	8.66	13.89	120.24	3.25	0.08	0.62
24.95	9.04	8.54	14.00	119.54	3.25	0.08	0.61
24.96	8.94	8.42	14.12	118.88	3.26	0.08	0.60

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
24.97	8.85	8.32	14.22	118.29	3.26	0.08	0.59
24.98	8.78	8.23	14.31	117.79	3.27	0.08	0.59
24.99	8.70	8.15	14.40	117.31	3.27	0.08	0.58
25.00	8.62	8.05	14.50	116.78	3.27	0.08	0.58
25.01	8.52	7.94	14.63	116.17	3.28	0.08	0.57
25.02	8.42	7.82	14.77	115.51	3.28	0.08	0.56
25.03	8.31	7.70	14.91	114.83	3.29	0.08	0.55
25.04	8.21	7.58	15.06	114.16	3.30	0.08	0.54
25.05	8.11	7.47	15.20	113.54	3.30	0.08	0.53
25.06	8.03	7.38	15.32	113.00	3.31	0.08	0.53
25.07	7.96	7.29	15.44	112.54	3.31	0.08	0.52
25.08	7.88	7.20	15.56	112.08	3.31	0.07	0.51
25.09	7.79	7.10	15.71	111.57	3.32	0.07	0.51
25.10	7.69	6.99	15.88	110.99	3.33	0.07	0.50
25.11	7.58	6.87	16.07	110.37	3.33	0.07	0.49
25.12	7.48	6.75	16.27	109.74	3.34	0.07	0.48
25.13	7.38	6.63	16.46	109.13	3.35	0.07	0.47
25.14	7.28	6.53	16.64	108.57	3.35	0.07	0.47
25.15	7.22	6.45	16.77	108.17	3.36	0.07	0.46
25.16	7.18	6.41	16.85	107.98	3.36	0.07	0.46
25.17	7.17	6.39	16.88	107.96	3.36	0.07	0.46
25.18	7.17	6.39	16.90	108.03	3.36	0.07	0.46
25.19	7.17	6.39	16.92	108.10	3.36	0.07	0.46
25.20	7.17	6.39	16.93	108.17	3.36	0.07	0.46
25.21	7.17	6.39	16.95	108.24	3.36	0.07	0.46
25.22	7.17	6.38	16.97	108.31	3.36	0.07	0.46
25.23	7.17	6.38	16.98	108.37	3.36	0.07	0.46
25.24	7.15	6.36	17.03	108.26	3.37	0.07	0.45
25.25	7.10	6.30	17.13	107.92	3.37	0.07	0.45
25.26	7.02	6.21	17.29	107.32	3.38	0.07	0.44
25.27	6.93	6.10	17.48	106.61	3.38	0.07	0.44
25.28	6.82	5.98	17.70	105.83	3.39	0.07	0.43
25.29	6.72	5.86	17.93	105.03	3.40	0.07	0.42
25.30	6.61	5.74	18.16	104.25	3.40	0.07	0.41
25.31	6.52	5.63	18.38	103.52	3.41	0.07	0.40
25.32	6.44	5.55	18.56	102.92	3.42	0.07	0.40
25.33	6.39	5.49	18.66	102.51	3.42	0.07	0.39
25.34	6.38	5.47	18.68	102.23	3.42	0.07	0.39
25.35	6.38	5.47	18.65	102.02	3.42	0.07	0.39
25.36	6.38	5.47	18.61	101.79	3.42	0.07	0.39
25.37	6.38	5.47	18.58	101.54	3.42	0.07	0.39
25.38	6.38	5.46	18.54	101.29	3.42	0.07	0.39
25.39	6.38	5.46	18.50	101.05	3.42	0.07	0.39
25.40	6.38	5.46	18.47	100.84	3.41	0.07	0.39
25.41	6.39	5.47	18.41	100.73	3.41	0.07	0.39
25.42	6.43	5.51	18.29	100.82	3.41	0.07	0.39
25.43	6.50	5.59	18.09	101.10	3.40	0.07	0.40
25.44	6.59	5.69	17.84	101.50	3.39	0.07	0.41

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
25.45	6.69	5.80	17.57	101.93	3.38	0.07	0.41
25.46	6.80	5.92	17.30	102.36	3.38	0.07	0.42
25.47	6.90	6.03	17.04	102.78	3.37	0.07	0.43
25.48	7.00	6.14	16.80	103.16	3.36	0.07	0.44
25.49	7.09	6.23	16.60	103.49	3.35	0.07	0.45
25.50	7.17	6.31	16.44	103.79	3.35	0.07	0.45
25.51	7.24	6.39	16.28	104.11	3.34	0.07	0.46
25.52	7.32	6.49	16.11	104.50	3.33	0.07	0.46
25.53	7.42	6.59	15.93	104.94	3.33	0.07	0.47
25.54	7.53	6.70	15.73	105.42	3.32	0.07	0.48
25.55	7.63	6.82	15.53	105.90	3.31	0.07	0.49
25.56	7.74	6.93	15.35	106.35	3.31	0.07	0.50
25.57	7.83	7.03	15.18	106.77	3.30	0.07	0.50
25.58	7.91	7.12	15.04	107.13	3.29	0.07	0.51
25.59	7.99	7.20	14.94	107.56	3.29	0.07	0.51
25.60	8.06	7.28	14.84	108.11	3.29	0.08	0.52
25.61	8.15	7.38	14.75	108.81	3.28	0.08	0.53
25.62	8.25	7.49	14.64	109.61	3.28	0.08	0.53
25.63	8.36	7.60	14.53	110.45	3.27	0.08	0.54
25.64	8.47	7.71	14.43	111.30	3.27	0.08	0.55
25.65	8.57	7.82	14.33	112.10	3.27	0.08	0.56
25.66	8.66	7.92	14.24	112.82	3.26	0.08	0.57
25.67	8.72	7.99	14.19	113.38	3.26	0.08	0.57
25.68	8.76	8.03	14.18	113.79	3.26	0.08	0.57
25.69	8.77	8.03	14.20	114.10	3.26	0.08	0.57
25.70	8.77	8.03	14.25	114.43	3.26	0.08	0.57
25.71	8.77	8.03	14.30	114.79	3.27	0.08	0.57
25.72	8.77	8.02	14.35	115.16	3.27	0.08	0.57
25.73	8.77	8.02	14.40	115.53	3.27	0.08	0.57
25.74	8.77	8.02	14.45	115.87	3.27	0.08	0.57
25.75	8.77	8.02	14.49	116.16	3.27	0.08	0.57
25.76	8.79	8.04	14.49	116.48	3.27	0.08	0.57
25.77	8.84	8.09	14.45	116.88	3.27	0.08	0.58
25.78	8.92	8.18	14.36	117.40	3.27	0.08	0.58
25.79	9.02	8.28	14.25	118.01	3.26	0.08	0.59
25.80	9.12	8.39	14.14	118.66	3.26	0.08	0.60
25.81	9.23	8.51	14.03	119.32	3.25	0.08	0.61
25.82	9.33	8.62	13.92	119.96	3.25	0.08	0.62
25.83	9.43	8.72	13.82	120.54	3.25	0.08	0.62
25.84	9.51	8.81	13.74	121.03	3.24	0.08	0.63
25.85	9.58	8.88	13.67	121.47	3.24	0.08	0.63
25.86	9.66	8.97	13.60	121.91	3.24	0.08	0.64
25.87	9.75	9.06	13.51	122.42	3.23	0.08	0.65
25.88	9.85	9.17	13.42	122.99	3.23	0.08	0.65
25.89	9.96	9.28	13.32	123.59	3.23	0.08	0.66
25.90	10.06	9.39	13.22	124.19	3.22	0.08	0.67
25.91	10.16	9.50	13.13	124.75	3.22	0.08	0.68
25.92	10.25	9.60	13.05	125.26	3.21	0.08	0.69

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
25.93	10.36	9.71	12.96	125.83	3.21	0.08	0.69
25.94	10.53	9.89	12.81	126.67	3.20	0.08	0.71
25.95	10.77	10.15	12.60	127.88	3.19	0.08	0.72
25.96	11.07	10.48	12.35	129.37	3.18	0.08	0.75
25.97	11.41	10.84	12.08	130.97	3.17	0.08	0.77
25.98	11.75	11.21	11.83	132.62	3.16	0.08	0.80
25.99	12.10	11.58	11.59	134.20	3.15	0.08	0.83
26.00	12.42	11.93	11.37	135.66	3.14	0.08	0.85
26.01	12.70	12.23	11.20	136.92	3.13	0.08	0.87
26.02	12.89	12.44	11.08	137.82	3.12	0.08	0.89
26.03	13.02	12.57	11.01	138.45	3.12	0.08	0.90
26.04	13.11	12.66	10.97	138.94	3.12	0.08	0.90
26.05	13.20	12.77	10.93	139.49	3.12	0.08	0.91
26.06	13.31	12.88	10.88	140.09	3.11	0.08	0.92
26.07	13.42	12.99	10.83	140.70	3.11	0.08	0.93
26.08	13.52	13.10	10.79	141.28	3.11	0.08	0.94
26.09	13.61	13.20	10.75	141.82	3.11	0.08	0.94
26.10	13.68	13.26	10.73	142.20	3.11	0.08	0.95
26.11	13.65	13.22	10.76	142.23	3.11	0.08	0.94
26.12	13.53	13.09	10.84	141.90	3.11	0.08	0.93
26.13	13.33	12.86	10.98	141.28	3.12	0.08	0.92
26.14	13.10	12.61	11.14	140.57	3.13	0.08	0.90
26.15	12.86	12.35	11.32	139.80	3.13	0.08	0.88
26.16	12.62	12.09	11.50	139.01	3.14	0.08	0.86
26.17	12.39	11.84	11.68	138.25	3.15	0.08	0.85
26.18	12.19	11.61	11.85	137.54	3.16	0.08	0.83
26.19	12.05	11.45	11.97	137.08	3.17	0.08	0.82
26.20	11.97	11.37	12.05	136.93	3.17	0.08	0.81
26.21	11.96	11.34	12.08	137.08	3.17	0.08	0.81
26.22	11.96	11.34	12.11	137.35	3.17	0.08	0.81
26.23	11.96	11.34	12.14	137.65	3.17	0.08	0.81
26.24	11.96	11.33	12.17	137.96	3.17	0.08	0.81
26.25	11.96	11.33	12.20	138.26	3.18	0.08	0.81
26.26	11.96	11.33	12.23	138.55	3.18	0.08	0.81
26.27	11.96	11.32	12.26	138.79	3.18	0.08	0.81
26.28	11.98	11.34	12.26	139.09	3.18	0.08	0.81
26.29	12.03	11.39	12.24	139.50	3.18	0.08	0.81
26.30	12.11	11.48	12.20	140.07	3.18	0.08	0.82
26.31	12.21	11.58	12.15	140.73	3.17	0.08	0.83
26.32	12.32	11.69	12.10	141.43	3.17	0.08	0.84
26.33	12.42	11.80	12.04	142.15	3.17	0.08	0.84
26.34	12.53	11.91	11.99	142.85	3.17	0.08	0.85
26.35	12.62	12.01	11.95	143.48	3.16	0.08	0.86
26.36	12.70	12.09	11.91	143.99	3.16	0.08	0.86
26.37	12.78	12.17	11.86	144.35	3.16	0.08	0.87
26.38	12.85	12.25	11.81	144.60	3.16	0.08	0.87
26.39	12.94	12.34	11.73	144.83	3.15	0.08	0.88
26.40	13.04	12.45	11.66	145.07	3.15	0.08	0.89

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
26.41	13.15	12.56	11.57	145.33	3.15	0.08	0.90
26.42	13.26	12.67	11.49	145.58	3.14	0.08	0.90
26.43	13.36	12.77	11.42	145.81	3.14	0.08	0.91
26.44	13.45	12.86	11.35	146.02	3.14	0.08	0.92
26.45	13.51	12.93	11.30	146.09	3.13	0.08	0.92
26.46	13.54	12.96	11.26	145.97	3.13	0.08	0.93
26.47	13.55	12.96	11.24	145.65	3.13	0.08	0.93
26.48	13.55	12.96	11.21	145.23	3.13	0.08	0.93
26.49	13.55	12.95	11.18	144.76	3.13	0.08	0.93
26.50	13.55	12.95	11.14	144.28	3.13	0.08	0.92
26.51	13.55	12.94	11.11	143.80	3.12	0.08	0.92
26.52	13.55	12.94	11.08	143.36	3.12	0.08	0.92
26.53	13.55	12.94	11.05	142.97	3.12	0.08	0.92
26.54	13.56	12.94	11.03	142.70	3.12	0.08	0.92
26.55	13.59	12.97	10.99	142.55	3.12	0.08	0.93
26.56	13.63	13.01	10.95	142.46	3.12	0.08	0.93
26.57	13.68	13.06	10.90	142.37	3.11	0.08	0.93
26.58	13.73	13.11	10.85	142.27	3.11	0.08	0.94
26.59	13.78	13.16	10.80	142.16	3.11	0.08	0.94
26.60	13.84	13.21	10.75	142.06	3.11	0.08	0.94
26.61	13.88	13.26	10.71	141.96	3.10	0.08	0.95
26.62	13.91	13.29	10.68	141.84	3.10	0.08	0.95
26.63	13.90	13.27	10.68	141.65	3.10	0.08	0.95
26.64	13.85	13.20	10.70	141.35	3.10	0.08	0.94
26.65	13.76	13.10	10.76	140.95	3.11	0.08	0.94
26.66	13.65	12.99	10.81	140.50	3.11	0.08	0.93
26.67	13.55	12.87	10.88	140.03	3.11	0.08	0.92
26.68	13.44	12.76	10.94	139.55	3.12	0.08	0.91
26.69	13.34	12.64	11.00	139.10	3.12	0.08	0.90
26.70	13.25	12.54	11.06	138.69	3.12	0.08	0.90
26.71	13.17	12.45	11.11	138.29	3.12	0.08	0.89
26.72	13.07	12.34	11.17	137.83	3.13	0.08	0.88
26.73	12.95	12.21	11.24	137.24	3.13	0.08	0.87
26.74	12.81	12.06	11.32	136.53	3.14	0.08	0.86
26.75	12.66	11.89	11.42	135.76	3.14	0.08	0.85
26.76	12.50	11.71	11.52	134.95	3.14	0.08	0.84
26.77	12.34	11.54	11.62	134.15	3.15	0.08	0.82
26.78	12.19	11.38	11.72	133.41	3.15	0.08	0.81
26.79	12.07	11.24	11.81	132.75	3.16	0.08	0.80
26.80	11.99	11.16	11.86	132.30	3.16	0.08	0.80
26.81	11.96	11.12	11.87	132.00	3.16	0.08	0.79
26.82	11.96	11.11	11.86	131.79	3.16	0.08	0.79
26.83	11.96	11.11	11.84	131.56	3.16	0.08	0.79
26.84	11.95	11.11	11.82	131.32	3.16	0.08	0.79
26.85	11.95	11.10	11.80	131.06	3.16	0.08	0.79
26.86	11.95	11.10	11.79	130.82	3.16	0.08	0.79
26.87	11.95	11.10	11.77	130.60	3.16	0.08	0.79
26.88	11.98	11.12	11.74	130.53	3.15	0.08	0.79

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
26.89	12.11	11.25	11.64	130.92	3.15	0.08	0.80
26.90	12.35	11.50	11.46	131.80	3.14	0.08	0.82
26.91	12.68	11.86	11.22	133.09	3.13	0.08	0.85
26.92	13.06	12.26	10.97	134.49	3.12	0.08	0.88
26.93	13.46	12.68	10.72	135.92	3.11	0.08	0.91
26.94	13.86	13.09	10.49	137.32	3.09	0.08	0.94
26.95	14.24	13.49	10.28	138.61	3.08	0.08	0.96
26.96	14.57	13.84	10.09	139.73	3.07	0.08	0.99
26.97	14.77	14.05	9.99	140.34	3.07	0.08	1.00
26.98	14.79	14.06	9.98	140.30	3.07	0.08	1.00
26.99	14.64	13.90	10.04	139.64	3.07	0.08	0.99
27.00	14.43	13.67	10.15	138.72	3.08	0.08	0.98
27.01	14.20	13.42	10.26	137.70	3.08	0.08	0.96
27.02	13.96	13.16	10.38	136.65	3.09	0.08	0.94
27.03	13.72	12.91	10.51	135.60	3.09	0.08	0.92
27.04	13.50	12.67	10.62	134.62	3.10	0.08	0.91
27.05	13.31	12.46	10.73	133.76	3.11	0.08	0.89
27.06	13.08	12.22	10.87	132.81	3.11	0.08	0.87
27.07	12.78	11.89	11.07	131.63	3.12	0.08	0.85
27.08	12.37	11.46	11.35	130.06	3.14	0.08	0.82
27.09	11.90	10.96	11.70	128.21	3.15	0.08	0.78
27.10	11.40	10.43	12.10	126.17	3.17	0.08	0.74
27.11	10.90	9.89	12.54	124.02	3.19	0.08	0.71
27.12	10.41	9.37	13.01	121.88	3.21	0.08	0.67
27.13	9.96	8.90	13.47	119.86	3.23	0.08	0.64
27.14	9.63	8.54	13.85	118.32	3.25	0.08	0.61
27.15	9.48	8.38	14.04	117.69	3.26	0.08	0.60
27.16	9.50	8.40	14.05	117.95	3.26	0.08	0.60
27.17	9.61	8.51	13.95	118.73	3.25	0.08	0.61
27.18	9.74	8.64	13.84	119.60	3.25	0.08	0.62
27.19	9.87	8.78	13.72	120.52	3.24	0.08	0.63
27.20	10.00	8.92	13.62	121.43	3.24	0.08	0.64
27.21	10.13	9.05	13.52	122.29	3.23	0.08	0.65
27.22	10.24	9.16	13.43	123.05	3.23	0.08	0.65
27.23	10.32	9.24	13.37	123.57	3.23	0.08	0.66
27.24	10.35	9.28	13.35	123.83	3.23	0.08	0.66
27.25	10.36	9.28	13.35	123.89	3.23	0.08	0.66
27.26	10.36	9.28	13.35	123.91	3.23	0.08	0.66
27.27	10.36	9.28	13.36	123.93	3.23	0.08	0.66
27.28	10.36	9.27	13.37	123.95	3.23	0.08	0.66
27.29	10.36	9.27	13.37	123.97	3.23	0.08	0.66
27.30	10.36	9.27	13.38	123.99	3.23	0.08	0.66
27.31	10.36	9.26	13.39	124.00	3.23	0.08	0.66
27.32	10.36	9.26	13.39	123.99	3.23	0.08	0.66
27.33	10.36	9.26	13.39	123.95	3.23	0.08	0.66
27.34	10.36	9.25	13.39	123.89	3.23	0.08	0.66
27.35	10.36	9.25	13.38	123.81	3.23	0.08	0.66
27.36	10.36	9.25	13.38	123.73	3.23	0.08	0.66

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
27.37	10.36	9.25	13.37	123.65	3.23	0.08	0.66
27.38	10.36	9.24	13.37	123.58	3.23	0.08	0.66
27.39	10.36	9.24	13.37	123.50	3.23	0.08	0.66
27.40	10.39	9.27	13.34	123.58	3.23	0.08	0.66
27.41	10.50	9.38	13.23	124.08	3.22	0.08	0.67
27.42	10.71	9.60	13.03	125.06	3.21	0.08	0.69
27.43	11.01	9.91	12.76	126.43	3.20	0.08	0.71
27.44	11.34	10.25	12.48	127.93	3.19	0.08	0.73
27.45	11.68	10.61	12.21	129.46	3.18	0.08	0.76
27.46	12.03	10.96	11.94	130.97	3.16	0.08	0.78
27.47	12.35	11.30	11.71	132.36	3.15	0.08	0.81
27.48	12.64	11.60	11.51	133.57	3.14	0.08	0.83
27.49	12.89	11.86	11.35	134.63	3.14	0.08	0.85
27.50	13.13	12.11	11.21	135.70	3.13	0.08	0.86
27.51	13.40	12.38	11.06	136.91	3.12	0.08	0.88
27.52	13.71	12.70	10.89	138.33	3.11	0.08	0.91
27.53	14.05	13.05	10.72	139.85	3.11	0.08	0.93
27.54	14.39	13.41	10.55	141.40	3.10	0.08	0.96
27.55	14.73	13.76	10.39	142.91	3.09	0.08	0.98
27.56	15.05	14.08	10.25	144.29	3.08	0.08	1.01
27.57	15.31	14.35	10.13	145.44	3.08	0.08	1.03
27.58	15.39	14.43	10.12	145.96	3.07	0.08	1.03
27.59	15.28	14.31	10.20	145.89	3.08	0.08	1.02
27.60	14.99	14.01	10.37	145.30	3.09	0.08	1.00
27.61	14.67	13.67	10.58	144.60	3.10	0.08	0.98
27.62	14.33	13.31	10.81	143.82	3.11	0.08	0.95
27.63	13.98	12.94	11.05	142.98	3.12	0.08	0.92
27.64	13.65	12.59	11.29	142.14	3.13	0.08	0.90
27.65	13.35	12.27	11.52	141.34	3.14	0.08	0.88
27.66	13.08	11.99	11.73	140.58	3.15	0.08	0.86
27.67	12.79	11.69	11.95	139.71	3.16	0.08	0.83
27.68	12.46	11.33	12.23	138.59	3.18	0.08	0.81
27.69	12.05	10.90	12.58	137.16	3.19	0.08	0.78
27.70	11.59	10.42	13.00	135.49	3.21	0.08	0.74
27.71	11.11	9.92	13.47	133.66	3.23	0.08	0.71
27.72	10.63	9.42	13.98	131.75	3.25	0.08	0.67
27.73	10.18	8.95	14.51	129.85	3.27	0.08	0.64
27.74	9.79	8.53	15.01	128.09	3.29	0.08	0.61
27.75	9.52	8.25	15.38	126.91	3.31	0.08	0.59
27.76	9.39	8.11	15.58	126.37	3.31	0.08	0.58
27.77	9.37	8.09	15.63	126.41	3.32	0.08	0.58
27.78	9.37	8.09	15.65	126.58	3.32	0.08	0.58
27.79	9.37	8.08	15.68	126.77	3.32	0.08	0.58
27.80	9.37	8.08	15.71	126.96	3.32	0.08	0.58
27.81	9.37	8.08	15.74	127.15	3.32	0.08	0.58
27.82	9.37	8.08	15.77	127.32	3.32	0.08	0.58
27.83	9.37	8.08	15.78	127.50	3.32	0.08	0.58
27.84	9.44	8.15	15.71	127.96	3.32	0.08	0.58

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
27.85	9.59	8.30	15.52	128.79	3.31	0.08	0.59
27.86	9.81	8.53	15.24	130.02	3.30	0.08	0.61
27.87	10.07	8.80	14.94	131.40	3.29	0.08	0.63
27.88	10.35	9.08	14.63	132.84	3.28	0.08	0.65
27.89	10.63	9.37	14.33	134.27	3.27	0.08	0.67
27.90	10.90	9.64	14.06	135.62	3.26	0.08	0.69
27.91	11.14	9.89	13.83	136.82	3.25	0.08	0.71
27.92	11.34	10.09	13.65	137.75	3.24	0.08	0.72
27.93	11.49	10.24	13.51	138.39	3.23	0.08	0.73
27.94	11.61	10.37	13.39	138.82	3.23	0.08	0.74
27.95	11.74	10.49	13.27	139.21	3.22	0.08	0.75
27.96	11.88	10.63	13.13	139.63	3.22	0.08	0.76
27.97	12.02	10.78	12.99	140.06	3.21	0.08	0.77
27.98	12.17	10.93	12.85	140.48	3.21	0.08	0.78
27.99	12.31	11.07	12.73	140.86	3.20	0.08	0.79
28.00	12.43	11.19	12.62	141.20	3.20	0.08	0.80
28.01	12.48	11.24	12.56	141.24	3.19	0.08	0.80
28.02	12.46	11.22	12.56	140.88	3.19	0.08	0.80
28.03	12.36	11.11	12.62	140.12	3.19	0.08	0.79
28.04	12.23	10.97	12.69	139.17	3.20	0.08	0.78
28.05	12.08	10.82	12.77	138.14	3.20	0.08	0.77
28.06	11.94	10.66	12.86	137.08	3.21	0.08	0.76
28.07	11.79	10.51	12.94	136.04	3.21	0.08	0.75
28.08	11.66	10.37	13.03	135.08	3.21	0.08	0.74
28.09	11.55	10.25	13.10	134.25	3.22	0.08	0.73
28.10	11.44	10.14	13.17	133.50	3.22	0.08	0.72
28.11	11.34	10.03	13.24	132.74	3.22	0.08	0.72
28.12	11.22	9.90	13.32	131.87	3.23	0.08	0.71
28.13	11.08	9.76	13.41	130.88	3.23	0.08	0.70
28.14	10.94	9.61	13.52	129.83	3.23	0.08	0.69
28.15	10.79	9.45	13.62	128.76	3.24	0.08	0.68
28.16	10.65	9.30	13.73	127.74	3.24	0.08	0.66
28.17	10.52	9.17	13.83	126.81	3.25	0.08	0.66
28.18	10.46	9.10	13.87	126.23	3.25	0.08	0.65
28.19	10.53	9.17	13.77	126.27	3.24	0.08	0.65
28.20	10.73	9.38	13.54	126.92	3.23	0.08	0.67
28.21	11.03	9.68	13.22	127.92	3.22	0.08	0.69
28.22	11.36	10.02	12.88	129.00	3.21	0.08	0.72
28.23	11.71	10.37	12.55	130.07	3.19	0.08	0.74
28.24	12.05	10.72	12.23	131.09	3.18	0.08	0.77
28.25	12.37	11.05	11.95	132.00	3.16	0.08	0.79
28.26	12.66	11.34	11.71	132.77	3.15	0.08	0.81
28.27	12.85	11.52	11.56	133.20	3.15	0.08	0.82
28.28	12.94	11.61	11.47	133.27	3.14	0.08	0.83
28.29	12.95	11.62	11.45	133.02	3.14	0.08	0.83
28.30	12.95	11.62	11.42	132.69	3.14	0.08	0.83
28.31	12.95	11.62	11.39	132.33	3.14	0.08	0.83
28.32	12.95	11.61	11.36	131.96	3.14	0.08	0.83

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
28.33	12.95	11.61	11.34	131.60	3.14	0.08	0.83
28.34	12.95	11.60	11.31	131.26	3.13	0.08	0.83
28.35	12.94	11.59	11.30	130.93	3.13	0.08	0.83
28.36	12.82	11.46	11.37	130.34	3.14	0.08	0.82
28.37	12.58	11.21	11.54	129.37	3.15	0.08	0.80
28.38	12.21	10.83	11.82	127.96	3.16	0.08	0.77
28.39	11.78	10.39	12.15	126.32	3.17	0.08	0.74
28.40	11.34	9.93	12.54	124.52	3.19	0.08	0.71
28.41	10.88	9.47	12.96	122.64	3.21	0.08	0.68
28.42	10.45	9.02	13.39	120.79	3.23	0.08	0.64
28.43	10.06	8.62	13.82	119.05	3.25	0.08	0.62
28.44	9.76	8.31	14.17	117.71	3.26	0.08	0.59
28.45	9.56	8.11	14.42	116.89	3.27	0.08	0.58
28.46	9.45	7.99	14.58	116.50	3.28	0.08	0.57
28.47	9.36	7.89	14.73	116.25	3.28	0.08	0.56
28.48	9.25	7.78	14.90	115.98	3.29	0.08	0.56
28.49	9.15	7.67	15.08	115.69	3.30	0.08	0.55
28.50	9.04	7.56	15.26	115.39	3.30	0.08	0.54
28.51	8.94	7.46	15.43	115.10	3.31	0.08	0.53
28.52	8.85	7.37	15.59	114.83	3.31	0.08	0.53
28.53	8.80	7.31	15.69	114.65	3.32	0.08	0.52
28.54	8.77	7.28	15.74	114.55	3.32	0.08	0.52
28.55	8.77	7.27	15.75	114.51	3.32	0.08	0.52
28.56	8.77	7.27	15.75	114.48	3.32	0.08	0.52
28.57	8.77	7.27	15.75	114.45	3.32	0.08	0.52
28.58	8.77	7.26	15.75	114.42	3.32	0.08	0.52
28.59	8.77	7.26	15.75	114.38	3.32	0.08	0.52
28.60	8.77	7.26	15.75	114.35	3.32	0.08	0.52
28.61	8.76	7.25	15.76	114.31	3.32	0.08	0.52
28.62	8.74	7.22	15.80	114.13	3.32	0.08	0.52
28.63	8.68	7.16	15.89	113.80	3.33	0.08	0.51
28.64	8.59	7.07	16.02	113.30	3.33	0.08	0.51
28.65	8.49	6.97	16.18	112.73	3.34	0.08	0.50
28.66	8.38	6.86	16.35	112.13	3.34	0.07	0.49
28.67	8.28	6.75	16.53	111.52	3.35	0.07	0.48
28.68	8.18	6.64	16.70	110.92	3.36	0.07	0.47
28.69	8.08	6.55	16.86	110.39	3.36	0.07	0.47
28.70	8.03	6.49	16.96	110.09	3.36	0.07	0.46
28.71	8.04	6.50	16.96	110.20	3.36	0.07	0.46
28.72	8.12	6.57	16.85	110.76	3.36	0.07	0.47
28.73	8.23	6.69	16.68	111.57	3.35	0.07	0.48
28.74	8.36	6.82	16.50	112.47	3.35	0.07	0.49
28.75	8.49	6.95	16.32	113.41	3.34	0.08	0.50
28.76	8.63	7.08	16.15	114.33	3.34	0.08	0.51
28.77	8.75	7.20	15.99	115.19	3.33	0.08	0.51
28.78	8.86	7.31	15.86	115.95	3.32	0.08	0.52
28.79	8.99	7.44	15.69	116.73	3.32	0.08	0.53
28.80	9.16	7.62	15.45	117.70	3.31	0.08	0.54

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
28.81	9.41	7.86	15.13	118.95	3.30	0.08	0.56
28.82	9.70	8.15	14.77	120.39	3.28	0.08	0.58
28.83	10.01	8.47	14.40	121.91	3.27	0.08	0.60
28.84	10.33	8.79	14.05	123.44	3.26	0.08	0.63
28.85	10.64	9.10	13.72	124.89	3.24	0.08	0.65
28.86	10.93	9.39	13.44	126.20	3.23	0.08	0.67
28.87	11.18	9.63	13.21	127.27	3.22	0.08	0.69
28.88	11.38	9.83	13.02	128.03	3.21	0.08	0.70
28.89	11.56	10.02	12.84	128.59	3.20	0.08	0.72
28.90	11.76	10.21	12.64	129.06	3.20	0.08	0.73
28.91	11.99	10.44	12.42	129.57	3.19	0.08	0.75
28.92	12.22	10.67	12.19	130.09	3.18	0.08	0.76
28.93	12.46	10.91	11.97	130.58	3.17	0.08	0.78
28.94	12.69	11.14	11.76	131.03	3.16	0.08	0.80
28.95	12.90	11.34	11.59	131.41	3.15	0.08	0.81
28.96	13.09	11.53	11.42	131.77	3.14	0.08	0.82
28.97	13.32	11.76	11.25	132.22	3.13	0.08	0.84
28.98	13.60	12.04	11.03	132.80	3.12	0.08	0.86
28.99	13.95	12.38	10.78	133.50	3.11	0.08	0.88
29.00	14.33	12.77	10.51	134.21	3.09	0.08	0.91
29.01	14.73	13.17	10.25	134.90	3.08	0.08	0.94
29.02	15.13	13.56	10.00	135.54	3.07	0.08	0.97
29.03	15.50	13.93	9.77	136.08	3.06	0.08	0.99
29.04	15.82	14.25	9.58	136.53	3.05	0.08	1.02
29.05	16.12	14.55	9.42	136.97	3.04	0.08	1.04
29.06	16.44	14.86	9.25	137.50	3.03	0.08	1.06
29.07	16.81	15.23	9.07	138.17	3.02	0.09	1.09
29.08	17.25	15.66	8.87	138.93	3.00	0.09	1.12
29.09	17.72	16.13	8.66	139.70	2.99	0.09	0.62
29.10	18.20	16.61	8.46	140.44	2.98	0.09	0.62
29.11	18.67	17.07	8.27	141.12	2.97	0.09	0.62
29.12	19.09	17.50	8.10	141.70	2.96	0.09	0.62
29.13	19.45	17.85	7.96	142.15	2.95	0.09	0.62
29.14	19.72	18.12	7.86	142.44	2.94	0.09	0.62
29.15	19.93	18.32	7.78	142.62	2.94	0.09	0.62
29.16	20.13	18.52	7.71	142.75	2.93	0.09	0.62
29.17	20.36	18.74	7.63	142.88	2.93	0.09	0.62
29.18	20.60	18.97	7.54	143.01	2.92	0.09	0.62
29.19	20.83	19.20	7.45	143.13	2.92	0.09	0.62
29.20	21.06	19.43	7.37	143.23	2.91	0.09	0.62
29.21	21.27	19.63	7.30	143.31	2.91	0.09	0.62
29.22	21.41	19.76	7.26	143.36	2.90	0.09	0.62
29.23	21.46	19.80	7.24	143.39	2.90	0.09	0.62
29.24	21.42	19.76	7.26	143.40	2.90	0.09	0.62
29.25	21.36	19.69	7.28	143.41	2.91	0.09	0.62
29.26	21.28	19.61	7.31	143.41	2.91	0.09	0.62
29.27	21.20	19.52	7.35	143.42	2.91	0.09	0.62
29.28	21.12	19.43	7.38	143.42	2.91	0.09	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
29.29	21.05	19.35	7.41	143.42	2.91	0.09	0.62
29.30	20.98	19.28	7.44	143.42	2.92	0.09	0.62
29.31	20.95	19.25	7.45	143.42	2.92	0.09	0.62
29.32	20.97	19.26	7.44	143.42	2.92	0.09	0.62
29.33	21.03	19.32	7.42	143.41	2.91	0.09	0.62
29.34	21.11	19.39	7.40	143.41	2.91	0.09	0.62
29.35	21.18	19.46	7.37	143.41	2.91	0.09	0.62
29.36	21.26	19.53	7.34	143.41	2.91	0.09	0.62
29.37	21.34	19.60	7.32	143.40	2.91	0.09	0.62
29.38	21.41	19.67	7.29	143.39	2.91	0.09	0.62
29.39	21.49	19.74	7.26	143.38	2.90	0.09	0.62
29.40	21.66	19.90	7.20	143.37	2.90	0.09	0.62
29.41	21.94	20.18	7.10	143.34	2.89	0.09	0.62
29.42	22.34	20.57	6.97	143.27	2.88	0.09	0.62
29.43	22.79	21.00	6.82	143.15	2.87	0.09	0.62
29.44	23.27	21.47	6.66	142.98	2.86	0.09	0.62
29.45	23.75	21.93	6.51	142.76	2.85	0.09	0.62
29.46	24.20	22.37	6.37	142.51	2.84	0.09	0.62
29.47	24.61	22.77	6.25	142.25	2.83	0.09	0.62
29.48	24.97	23.11	6.15	142.09	2.82	0.09	0.62
29.49	25.30	23.43	6.07	142.09	2.82	0.09	0.62
29.50	25.66	23.77	5.98	142.27	2.81	0.09	0.62
29.51	26.08	24.18	5.89	142.53	2.80	0.09	0.62
29.52	26.54	24.63	5.80	142.80	2.80	0.09	0.62
29.53	27.02	25.09	5.70	143.05	2.79	0.10	0.62
29.54	27.49	25.55	5.61	143.29	2.78	0.10	0.62
29.55	27.94	25.98	5.52	143.49	2.77	0.10	0.62
29.56	28.32	26.35	5.45	143.65	2.77	0.10	0.62
29.57	28.60	26.61	5.41	143.85	2.76	0.10	0.62
29.58	28.79	26.79	5.38	144.14	2.76	0.10	0.62
29.59	28.92	26.91	5.37	144.57	2.76	0.10	0.62
29.60	29.06	27.04	5.36	145.06	2.76	0.10	0.62
29.61	29.22	27.19	5.35	145.60	2.76	0.10	0.62
29.62	29.38	27.34	5.35	146.14	2.76	0.10	0.62
29.63	29.54	27.49	5.34	146.67	2.76	0.10	0.62
29.64	29.68	27.62	5.33	147.16	2.76	0.10	0.62
29.65	29.78	27.71	5.33	147.58	2.76	0.10	0.62
29.66	29.78	27.70	5.34	147.98	2.76	0.10	0.62
29.67	29.66	27.58	5.38	148.42	2.76	0.10	0.62
29.68	29.46	27.38	5.44	148.94	2.77	0.10	0.62
29.69	29.24	27.15	5.51	149.52	2.77	0.10	0.62
29.70	29.00	26.91	5.58	150.11	2.78	0.10	0.62
29.71	28.76	26.67	5.65	150.69	2.78	0.10	0.62
29.72	28.53	26.44	5.72	151.23	2.79	0.10	0.62
29.73	28.33	26.23	5.78	151.70	2.79	0.10	0.62
29.74	28.12	26.03	5.85	152.18	2.80	0.10	0.62
29.75	27.87	25.77	5.93	152.81	2.81	0.10	0.62
29.76	27.53	25.43	6.04	153.67	2.82	0.10	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
29.77	27.10	25.01	6.18	154.68	2.83	0.10	0.62
29.78	26.64	24.55	6.34	155.74	2.84	0.10	0.62
29.79	26.16	24.08	6.51	156.76	2.85	0.10	0.62
29.80	25.69	23.61	6.68	157.71	2.86	0.09	0.62
29.81	25.25	23.17	6.84	158.53	2.87	0.09	0.62
29.82	24.86	22.79	6.99	159.19	2.88	0.09	0.62
29.83	24.69	22.61	7.07	159.85	2.89	0.09	0.62
29.84	24.73	22.65	7.09	160.64	2.89	0.09	0.62
29.85	24.98	22.88	7.07	161.67	2.89	0.09	0.62
29.86	25.27	23.16	7.03	162.86	2.89	0.09	0.62
29.87	25.58	23.46	7.00	164.15	2.89	0.10	0.62
29.88	25.90	23.77	6.96	165.46	2.88	0.10	0.62
29.89	26.21	24.07	6.93	166.72	2.88	0.10	0.62
29.90	26.50	24.34	6.90	167.88	2.88	0.10	0.62
29.91	26.75	24.58	6.87	168.83	2.88	0.10	0.62
29.92	27.05	24.86	6.82	169.50	2.87	0.10	0.62
29.93	27.42	25.21	6.74	169.97	2.87	0.10	0.62
29.94	27.89	25.66	6.64	170.36	2.86	0.10	0.62
29.95	28.41	26.17	6.53	170.77	2.85	0.10	0.62
29.96	28.97	26.70	6.41	171.17	2.84	0.10	0.62
29.97	29.53	27.24	6.30	171.53	2.83	0.10	0.62
29.98	30.06	27.74	6.19	171.85	2.83	0.10	0.62
29.99	30.53	28.20	6.10	172.11	2.82	0.10	0.62
30.00	30.85	28.49	6.05	172.36	2.82	0.10	0.62
30.01	30.96	28.59	6.04	172.67	2.81	0.10	0.62
30.02	30.89	28.52	6.07	173.11	2.82	0.10	0.62
30.03	30.75	28.37	6.12	173.64	2.82	0.10	0.62
30.04	30.60	28.22	6.17	174.21	2.83	0.10	0.62
30.05	30.44	28.05	6.23	174.80	2.83	0.10	0.62
30.06	30.28	27.89	6.29	175.37	2.83	0.10	0.62
30.07	30.13	27.74	6.34	175.89	2.84	0.10	0.62
30.08	30.00	27.61	6.39	176.33	2.84	0.10	0.62
30.09	29.94	27.54	6.42	176.70	2.84	0.10	0.62
30.10	29.94	27.54	6.43	177.04	2.84	0.10	0.62
30.11	30.01	27.59	6.43	177.41	2.84	0.10	0.62
30.12	30.08	27.65	6.43	177.84	2.84	0.10	0.62
30.13	30.16	27.72	6.43	178.29	2.84	0.10	0.62
30.14	30.24	27.79	6.43	178.76	2.84	0.10	0.62
30.15	30.32	27.86	6.43	179.21	2.84	0.10	0.62
30.16	30.39	27.92	6.43	179.63	2.84	0.10	0.62
30.17	30.47	27.99	6.43	179.94	2.84	0.10	0.62
30.18	30.65	28.15	6.40	180.05	2.84	0.10	0.62
30.19	30.94	28.42	6.33	179.98	2.84	0.10	0.62
30.20	31.34	28.81	6.24	179.78	2.83	0.10	0.62
30.21	31.80	29.24	6.14	179.51	2.82	0.10	0.62
30.22	32.27	29.69	6.04	179.21	2.81	0.10	0.62
30.23	32.75	30.14	5.93	178.86	2.81	0.10	0.62
30.24	33.20	30.57	5.84	178.51	2.80	0.10	0.62

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
30.25	33.61	30.95	5.76	178.16	2.79	0.10	0.62
30.26	33.93	31.25	5.69	177.94	2.79	0.10	0.62
30.27	34.16	31.47	5.65	177.92	2.78	0.10	0.62
30.28	34.36	31.65	5.63	178.10	2.78	0.10	0.62
30.29	34.57	31.84	5.60	178.36	2.78	0.10	0.62
30.30	34.81	32.06	5.57	178.65	2.78	0.11	0.62
30.31	35.05	32.28	5.54	178.95	2.77	0.11	0.62
30.32	35.28	32.50	5.51	179.24	2.77	0.11	0.62
30.33	35.50	32.70	5.49	179.50	2.77	0.11	0.62
30.34	35.69	32.88	5.47	179.73	2.77	0.11	0.62
30.35	35.78	32.95	5.46	180.02	2.77	0.11	0.62
30.36	35.75	32.91	5.48	180.43	2.77	0.11	0.62
30.37	35.62	32.78	5.52	181.00	2.77	0.11	0.62
30.38	35.48	32.63	5.57	181.65	2.78	0.11	0.62
30.39	35.32	32.47	5.62	182.33	2.78	0.11	0.62
30.40	35.16	32.31	5.67	183.02	2.78	0.11	0.62
30.41	35.00	32.15	5.71	183.68	2.79	0.11	0.62
30.42	34.86	32.00	5.76	184.27	2.79	0.11	0.62
30.43	34.74	31.87	5.80	184.73	2.80	0.11	0.62
30.44	34.60	31.73	5.83	184.99	2.80	0.11	0.62
30.45	34.44	31.57	5.86	185.10	2.80	0.11	0.62
30.46	34.24	31.36	5.90	185.12	2.80	0.10	0.62
30.47	34.01	31.13	5.95	185.13	2.81	0.10	0.62
30.48	33.77	30.90	5.99	185.15	2.81	0.10	0.62
30.49	33.53	30.66	6.04	185.15	2.81	0.10	0.62
30.50	33.31	30.43	6.08	185.15	2.82	0.10	0.62
30.51	33.10	30.23	6.13	185.14	2.82	0.10	0.62
30.52	33.05	30.17	6.14	185.15	2.82	0.10	0.62
30.53	33.24	30.34	6.10	185.19	2.82	0.10	0.62
30.54	33.67	30.74	6.03	185.26	2.81	0.10	0.62
30.55	34.23	31.27	5.93	185.32	2.81	0.10	0.62
30.56	34.85	31.86	5.82	185.34	2.80	0.11	0.62
30.57	35.49	32.46	5.71	185.33	2.79	0.11	0.62
30.58	36.12	33.06	5.60	185.28	2.78	0.11	0.62
30.59	36.71	33.61	5.51	185.20	2.77	0.11	0.62
30.60	37.22	34.09	5.43	185.10	2.77	0.11	0.62
30.61	37.88	34.71	5.33	185.05	2.76	0.11	0.62
30.62	38.81	35.59	5.20	185.03	2.75	0.11	0.62
30.63	40.09	36.81	5.03	184.98	2.73	0.11	0.62
30.64	41.56	38.20	4.84	184.77	2.71	0.11	0.62
30.65	43.14	39.70	4.64	184.39	2.69	0.11	0.62
30.66	44.74	41.22	4.46	183.83	2.68	0.12	0.62
30.67	46.29	42.68	4.29	183.15	2.66	0.12	0.62
30.68	47.69	44.02	4.14	182.40	2.64	0.12	0.62
30.69	48.92	45.18	4.02	181.68	2.63	0.12	0.62
30.70	50.13	46.32	3.91	180.98	2.62	0.12	0.62
30.71	51.48	47.60	3.79	180.20	2.60	0.12	0.62
30.72	53.11	49.13	3.65	179.22	2.59	0.13	0.78

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
30.73	54.93	50.86	3.50	178.00	2.57	0.13	0.78
30.74	56.84	52.66	3.35	176.59	2.55	0.13	0.78
30.75	58.75	54.47	3.21	175.06	2.53	0.13	0.79
30.76	60.56	56.18	3.09	173.50	2.52	0.13	0.79
30.77	62.17	57.69	2.98	172.03	2.50	0.14	0.79
30.78	63.55	59.00	2.89	170.72	2.49	0.14	0.79
30.79	64.89	60.25	2.81	169.44	2.48	0.14	0.80
30.80	66.35	61.62	2.73	168.00	2.46	0.14	0.80
30.81	68.05	63.23	2.63	166.29	2.45	0.14	0.80
30.82	69.91	64.98	2.53	164.38	2.43	0.15	0.80
30.83	71.83	66.79	2.43	162.36	2.41	0.15	0.81
30.84	73.72	68.56	2.34	160.34	2.39	0.15	0.81
30.85	75.47	70.21	2.26	158.46	2.38	0.15	0.81
30.86	76.98	71.63	2.19	156.82	2.36	0.15	0.81
30.87	78.15	72.72	2.14	155.76	2.35	0.16	0.81
30.88	79.10	73.61	2.11	155.15	2.34	0.16	0.81
30.89	80.00	74.45	2.08	154.86	2.34	0.16	0.82
30.90	81.04	75.41	2.05	154.52	2.33	0.16	0.82
30.91	82.14	76.44	2.02	154.17	2.32	0.16	0.82
30.92	83.26	77.48	1.99	153.82	2.32	0.16	0.82
30.93	84.34	78.48	1.96	153.49	2.31	0.16	0.82
30.94	85.32	79.40	1.93	153.19	2.30	0.17	0.82
30.95	86.09	80.11	1.91	153.04	2.30	0.17	0.82
30.96	86.56	80.53	1.90	153.25	2.29	0.17	0.82
30.97	86.80	80.74	1.91	153.83	2.29	0.17	0.82
30.98	86.94	80.85	1.91	154.72	2.30	0.17	0.82
30.99	87.09	80.97	1.92	155.72	2.30	0.17	0.83
31.00	87.25	81.11	1.93	156.77	2.30	0.17	0.83
31.01	87.41	81.24	1.94	157.82	2.30	0.17	0.83
31.02	87.56	81.36	1.95	158.82	2.31	0.17	0.83
31.03	87.69	81.47	1.96	159.70	2.31	0.17	0.83
31.04	87.77	81.52	1.97	160.42	2.31	0.17	0.83
31.05	87.78	81.51	1.98	161.03	2.31	0.17	0.83
31.06	87.74	81.45	1.98	161.64	2.32	0.17	0.83
31.07	87.66	81.36	2.00	162.33	2.32	0.17	0.83
31.08	87.59	81.27	2.01	163.09	2.32	0.17	0.83
31.09	87.51	81.17	2.02	163.88	2.32	0.17	0.83
31.10	87.43	81.08	2.03	164.65	2.33	0.17	0.83
31.11	87.36	80.99	2.04	165.36	2.33	0.17	0.83
31.12	87.30	80.91	2.05	165.98	2.33	0.17	0.83
31.13	87.30	80.89	2.06	166.52	2.33	0.17	0.83
31.14	87.36	80.93	2.06	167.06	2.33	0.17	0.83
31.15	87.49	81.03	2.07	167.66	2.34	0.17	0.83
31.16	87.64	81.15	2.07	168.36	2.34	0.18	0.83
31.17	87.80	81.28	2.08	169.11	2.34	0.18	0.83
31.18	87.96	81.41	2.09	169.86	2.34	0.18	0.83
31.19	88.11	81.54	2.09	170.59	2.34	0.18	0.83
31.20	88.25	81.65	2.10	171.26	2.34	0.18	0.83

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
31.21	88.39	81.76	2.10	171.80	2.34	0.18	0.83
31.22	88.58	81.91	2.10	172.24	2.34	0.18	0.83
31.23	88.84	82.14	2.10	172.64	2.34	0.18	0.83
31.24	89.19	82.44	2.10	173.07	2.34	0.18	0.83
31.25	89.57	82.78	2.10	173.55	2.34	0.18	0.83
31.26	89.96	83.14	2.09	174.06	2.34	0.18	0.83
31.27	90.36	83.49	2.09	174.56	2.34	0.18	0.83
31.28	90.74	83.82	2.09	175.04	2.34	0.18	0.83
31.29	91.07	84.11	2.09	175.46	2.34	0.18	0.83
31.30	91.38	84.39	2.08	175.75	2.34	0.18	0.83
31.31	91.73	84.69	2.08	175.92	2.34	0.19	0.83
31.32	92.15	85.07	2.07	176.00	2.34	0.19	0.83
31.33	92.65	85.51	2.06	176.08	2.33	0.19	0.84
31.34	93.19	86.00	2.05	176.16	2.33	0.19	0.84
31.35	93.75	86.51	2.04	176.24	2.33	0.19	0.84
31.36	94.30	87.00	2.03	176.32	2.33	0.19	0.84
31.37	94.81	87.46	2.02	176.40	2.32	0.19	0.84
31.38	95.26	87.86	2.01	176.46	2.32	0.19	0.84
31.39	95.77	88.32	2.00	176.52	2.32	0.19	0.84
31.40	96.41	88.90	1.99	176.60	2.32	0.19	0.84
31.41	97.25	89.67	1.97	176.70	2.31	0.20	0.84
31.42	98.22	90.55	1.95	176.82	2.31	0.20	0.84
31.43	99.24	91.49	1.93	176.95	2.30	0.20	0.84
31.44	100.28	92.45	1.92	177.09	2.30	0.20	0.84
31.45	101.28	93.36	1.90	177.22	2.29	0.21	0.85
31.46	102.19	94.19	1.88	177.34	2.29	0.21	0.85
31.47	102.98	94.91	1.87	177.45	2.28	0.21	0.85
31.48	103.75	95.61	1.86	177.55	2.28	0.21	0.85
31.49	104.61	96.40	1.84	177.66	2.28	0.21	0.85
31.50	105.64	97.34	1.83	177.81	2.27	0.22	0.85
31.51	106.78	98.39	1.81	177.97	2.27	0.22	0.85
31.52	107.98	99.49	1.79	178.16	2.26	0.22	0.85
31.53	109.17	100.58	1.77	178.35	2.26	0.23	0.86
31.54	110.29	101.61	1.76	178.53	2.25	0.23	0.86
31.55	111.29	102.52	1.74	178.70	2.25	0.23	0.86
31.56	112.15	103.30	1.73	178.83	2.24	0.23	0.86
31.57	112.98	104.06	1.72	178.92	2.24	0.24	0.86
31.58	113.91	104.90	1.71	179.01	2.23	0.24	0.86
31.59	114.98	105.88	1.69	179.12	2.23	0.24	0.86
31.60	116.15	106.95	1.68	179.25	2.22	0.25	0.86
31.61	117.35	108.05	1.66	179.39	2.22	0.25	0.86
31.62	118.52	109.12	1.65	179.54	2.21	0.25	0.86
31.63	119.61	110.12	1.63	179.69	2.21	0.26	0.87
31.64	120.55	110.97	1.62	179.81	2.20	0.26	0.87
31.65	121.35	111.69	1.61	179.88	2.20	0.26	0.87
31.66	122.11	112.38	1.60	179.88	2.19	0.26	0.87
31.67	122.96	113.15	1.59	179.84	2.19	0.27	0.87
31.68	123.93	114.03	1.58	179.82	2.18	0.27	0.87

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
31.69	124.95	114.96	1.56	179.80	2.18	0.27	0.87
31.70	125.99	115.91	1.55	179.80	2.17	0.28	0.87
31.71	126.99	116.82	1.54	179.81	2.17	0.28	0.87
31.72	127.89	117.64	1.53	179.83	2.16	0.28	0.87
31.73	128.63	118.30	1.52	179.86	2.16	0.28	0.87
31.74	129.22	118.82	1.51	179.89	2.16	0.29	0.87
31.75	129.73	119.28	1.51	179.94	2.15	0.29	0.87
31.76	130.28	119.76	1.50	180.00	2.15	0.29	0.87
31.77	130.89	120.31	1.50	180.07	2.15	0.29	0.87
31.78	131.53	120.88	1.49	180.16	2.14	0.29	0.88
31.79	132.16	121.44	1.48	180.25	2.14	0.29	0.88
31.80	132.76	121.97	1.48	180.34	2.14	0.30	0.88
31.81	133.29	122.44	1.47	180.42	2.13	0.30	0.88
31.82	133.71	122.80	1.47	180.51	2.13	0.30	0.88
31.83	134.05	123.10	1.47	180.63	2.13	0.30	0.88
31.84	134.37	123.36	1.47	180.81	2.13	0.30	0.88
31.85	134.73	123.67	1.46	181.03	2.13	0.30	0.88
31.86	135.12	124.01	1.46	181.27	2.13	0.31	0.88
31.87	135.52	124.35	1.46	181.52	2.13	0.31	0.88
31.88	135.91	124.69	1.46	181.76	2.12	0.31	0.88
31.89	136.27	125.00	1.46	181.98	2.12	0.31	0.88
31.90	136.57	125.25	1.45	182.16	2.12	0.31	0.88
31.91	136.75	125.39	1.45	182.28	2.12	0.31	0.88
31.92	136.82	125.43	1.45	182.35	2.12	0.31	0.88
31.93	136.82	125.40	1.45	182.39	2.12	0.31	0.88
31.94	136.82	125.37	1.46	182.45	2.12	0.31	0.88
31.95	136.82	125.34	1.46	182.50	2.12	0.31	0.88
31.96	136.82	125.31	1.46	182.56	2.12	0.31	0.88
31.97	136.82	125.28	1.46	182.62	2.12	0.31	0.88
31.98	136.82	125.25	1.46	182.67	2.13	0.31	0.88
31.99	136.81	125.21	1.46	182.71	2.13	0.31	0.88
32.00	136.75	125.13	1.46	182.75	2.13	0.31	0.88
32.01	136.65	125.00	1.46	182.81	2.13	0.31	0.88
32.02	136.52	124.84	1.46	182.88	2.13	0.31	0.88
32.03	136.36	124.67	1.47	182.97	2.13	0.31	0.88
32.04	136.20	124.49	1.47	183.07	2.13	0.31	0.88
32.05	136.05	124.31	1.47	183.16	2.13	0.31	0.88
32.06	135.90	124.15	1.48	183.25	2.14	0.31	0.88
32.07	135.76	123.99	1.48	183.33	2.14	0.31	0.88
32.08	135.65	123.86	1.48	183.39	2.14	0.31	0.88
32.09	135.54	123.72	1.48	183.45	2.14	0.31	0.88
32.10	135.42	123.58	1.49	183.53	2.14	0.31	0.88
32.11	135.27	123.41	1.49	183.62	2.14	0.31	0.88
32.12	135.12	123.24	1.49	183.72	2.14	0.31	0.88
32.13	134.96	123.06	1.49	183.82	2.14	0.31	0.88
32.14	134.80	122.89	1.50	183.93	2.15	0.31	0.88
32.15	134.66	122.72	1.50	184.02	2.15	0.31	0.88
32.16	134.53	122.58	1.50	184.10	2.15	0.31	0.88

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
32.17	134.42	122.44	1.50	184.17	2.15	0.31	0.88
32.18	134.31	122.31	1.51	184.24	2.15	0.31	0.88
32.19	134.17	122.16	1.51	184.33	2.15	0.31	0.88
32.20	134.03	121.99	1.51	184.43	2.15	0.31	0.88
32.21	133.87	121.81	1.52	184.54	2.16	0.31	0.88
32.22	133.71	121.63	1.52	184.66	2.16	0.31	0.88
32.23	133.55	121.46	1.52	184.77	2.16	0.31	0.88
32.24	133.42	121.30	1.52	184.87	2.16	0.31	0.88
32.25	133.31	121.17	1.53	184.95	2.16	0.31	0.88
32.26	133.22	121.06	1.53	185.01	2.16	0.31	0.88
32.27	133.16	120.97	1.53	185.08	2.16	0.31	0.88
32.28	133.09	120.88	1.53	185.16	2.16	0.31	0.88
32.29	133.01	120.78	1.53	185.25	2.16	0.31	0.88
32.30	132.93	120.68	1.54	185.34	2.17	0.31	0.88
32.31	132.85	120.57	1.54	185.44	2.17	0.31	0.88
32.32	132.78	120.47	1.54	185.53	2.17	0.31	0.88
32.33	132.71	120.38	1.54	185.60	2.17	0.31	0.88
32.34	132.67	120.32	1.54	185.68	2.17	0.31	0.88
32.35	132.65	120.27	1.54	185.77	2.17	0.31	0.88
32.36	132.65	120.24	1.55	185.89	2.17	0.31	0.88
32.37	132.65	120.21	1.55	186.04	2.17	0.31	0.88
32.38	132.65	120.18	1.55	186.20	2.17	0.31	0.88
32.39	132.65	120.15	1.55	186.37	2.17	0.31	0.88
32.40	132.65	120.12	1.55	186.54	2.17	0.31	0.88
32.41	132.65	120.09	1.55	186.69	2.17	0.31	0.88
32.42	132.65	120.06	1.56	186.81	2.18	0.31	0.88
32.43	132.65	120.03	1.56	186.92	2.18	0.31	0.88
32.44	132.65	120.00	1.56	187.04	2.18	0.31	0.88
32.45	132.65	119.97	1.56	187.17	2.18	0.31	0.88
32.46	132.65	119.94	1.56	187.33	2.18	0.31	0.88
32.47	132.65	119.91	1.56	187.50	2.18	0.31	0.88
32.48	132.65	119.88	1.57	187.67	2.18	0.31	0.88
32.49	132.65	119.85	1.57	187.83	2.18	0.31	0.88
32.50	132.65	119.82	1.57	187.98	2.18	0.31	0.88
32.51	132.66	119.80	1.57	188.11	2.18	0.31	0.88
32.52	132.69	119.80	1.57	188.24	2.18	0.31	0.88
32.53	132.74	119.81	1.57	188.41	2.18	0.31	0.88
32.54	132.81	119.85	1.57	188.61	2.18	0.31	0.88
32.55	132.88	119.89	1.58	188.84	2.18	0.31	0.88
32.56	132.96	119.93	1.58	189.09	2.18	0.31	0.88
32.57	133.04	119.98	1.58	189.32	2.18	0.31	0.88
32.58	133.12	120.01	1.58	189.55	2.19	0.31	0.88
32.59	133.18	120.04	1.58	189.74	2.19	0.31	0.88
32.60	133.47	120.28	1.58	190.10	2.19	0.31	0.88
32.61	134.08	120.81	1.58	190.74	2.19	0.32	0.88
32.62	135.08	121.70	1.58	191.72	2.18	0.32	0.88
32.63	136.27	122.76	1.57	192.90	2.18	0.33	0.88
32.64	137.56	123.91	1.57	194.17	2.18	0.34	0.89

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
32.65	138.88	125.10	1.56	195.49	2.18	0.35	0.89
32.66	140.17	126.25	1.56	196.76	2.18	0.36	0.89
32.67	141.35	127.30	1.55	197.94	2.17	0.37	0.89
32.68	142.37	128.20	1.55	198.95	2.17	0.37	0.89
32.69	143.26	128.98	1.55	199.83	2.17	0.38	0.89
32.70	144.15	129.77	1.55	200.72	2.17	0.39	0.89
32.71	145.15	130.66	1.54	201.73	2.17	0.39	0.89
32.72	146.29	131.67	1.54	202.89	2.17	0.40	0.89
32.73	147.50	132.74	1.54	204.11	2.17	0.41	0.90
32.74	148.71	133.82	1.53	205.35	2.17	0.43	0.90
32.75	149.87	134.84	1.53	206.53	2.16	0.44	0.90
32.76	150.92	135.77	1.53	207.59	2.16	0.45	0.90
32.77	151.69	136.45	1.53	208.40	2.16	0.46	0.90
32.78	152.16	136.84	1.53	208.96	2.16	0.46	0.90
32.79	152.39	137.01	1.53	209.34	2.16	0.46	0.90
32.80	152.54	137.11	1.53	209.70	2.16	0.46	0.90
32.81	152.70	137.23	1.53	210.11	2.16	0.47	0.90
32.82	152.88	137.35	1.53	210.53	2.16	0.47	0.90
32.83	153.05	137.47	1.53	210.95	2.17	0.47	0.90
32.84	153.21	137.58	1.54	211.34	2.17	0.47	0.90
32.85	153.35	137.68	1.54	211.68	2.17	0.48	0.90
32.86	153.53	137.81	1.54	211.98	2.17	0.48	0.90
32.87	153.78	138.00	1.54	212.29	2.17	0.48	0.90
32.88	154.14	138.30	1.54	212.66	2.17	0.49	0.90
32.89	154.56	138.65	1.54	213.09	2.17	0.49	0.90
32.90	155.01	139.03	1.54	213.56	2.17	0.50	0.90
32.91	155.48	139.42	1.54	214.04	2.17	0.50	0.90
32.92	155.93	139.79	1.53	214.50	2.17	0.51	0.91
32.93	156.35	140.14	1.53	214.93	2.16	0.51	0.91
32.94	156.71	140.44	1.53	215.28	2.16	0.52	0.91
32.95	157.07	140.74	1.53	215.56	2.16	0.52	0.91
32.96	157.49	141.09	1.53	215.80	2.16	0.52	0.91
32.97	158.01	141.52	1.53	216.06	2.16	0.53	0.91
32.98	158.59	142.02	1.52	216.35	2.16	0.54	0.91
32.99	159.20	142.55	1.52	216.66	2.16	0.54	0.91
33.00	159.82	143.08	1.52	216.98	2.16	0.55	0.91
33.01	160.41	143.58	1.51	217.28	2.15	0.56	0.91
33.02	160.94	144.03	1.51	217.55	2.15	0.57	0.91
33.03	161.39	144.41	1.51	217.75	2.15	0.57	0.91
33.04	161.83	144.78	1.51	217.90	2.15	0.57	0.91
33.05	162.30	145.18	1.50	218.02	2.15	0.58	0.91
33.06	162.86	145.66	1.50	218.14	2.15	0.59	0.91
33.07	163.48	146.19	1.49	218.28	2.14	0.59	0.91
33.08	164.12	146.74	1.49	218.43	2.14	0.60	0.91
33.09	164.75	147.29	1.48	218.59	2.14	0.61	0.91
33.10	165.34	147.80	1.48	218.73	2.14	0.62	0.91
33.11	165.86	148.24	1.48	218.85	2.14	0.62	0.91
33.12	166.34	148.64	1.47	218.98	2.13	0.63	0.91

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
33.13	166.84	149.07	1.47	219.14	2.13	0.63	0.91
33.14	167.45	149.59	1.47	219.35	2.13	0.64	0.91
33.15	168.14	150.19	1.46	219.61	2.13	0.65	0.91
33.16	168.89	150.85	1.46	219.89	2.12	0.66	0.92
33.17	169.66	151.51	1.45	220.19	2.12	0.67	0.92
33.18	170.41	152.16	1.45	220.48	2.12	0.69	0.92
33.19	171.09	152.75	1.45	220.74	2.12	0.70	0.92
33.20	171.68	153.25	1.44	220.96	2.11	0.70	0.92
33.21	172.17	153.67	1.44	221.13	2.11	0.71	0.92
33.22	172.65	154.08	1.44	221.27	2.11	0.72	0.92
33.23	173.19	154.53	1.43	221.43	2.11	0.73	0.92
33.24	173.79	155.05	1.43	221.61	2.11	0.73	0.92
33.25	174.42	155.59	1.43	221.81	2.10	0.74	0.92
33.26	175.06	156.14	1.42	222.01	2.10	0.75	0.92
33.27	175.67	156.66	1.42	222.20	2.10	0.76	0.92
33.28	176.21	157.13	1.42	222.38	2.10	0.77	0.92
33.29	176.62	157.46	1.41	222.47	2.10	0.78	0.92
33.30	176.85	157.64	1.41	222.44	2.09	0.78	0.92
33.31	176.95	157.70	1.41	222.30	2.09	0.78	0.92
33.32	177.02	157.73	1.41	222.10	2.09	0.78	0.92
33.33	177.10	157.77	1.41	221.89	2.09	0.78	0.92
33.34	177.18	157.81	1.40	221.67	2.09	0.78	0.92
33.35	177.26	157.85	1.40	221.46	2.09	0.78	0.92
33.36	177.33	157.89	1.40	221.25	2.09	0.78	0.92
33.37	177.40	157.92	1.40	221.07	2.09	0.78	0.92
33.38	177.36	157.85	1.40	220.85	2.09	0.78	0.92
33.39	177.19	157.66	1.40	220.56	2.09	0.77	0.92
33.40	176.88	157.34	1.40	220.16	2.09	0.76	0.92
33.41	176.52	156.98	1.40	219.71	2.09	0.75	0.92
33.42	176.12	156.59	1.40	219.22	2.09	0.74	0.92
33.43	175.72	156.19	1.40	218.73	2.09	0.73	0.92
33.44	175.33	155.81	1.40	218.25	2.09	0.73	0.92
33.45	174.98	155.45	1.40	217.80	2.09	0.72	0.92
33.46	174.65	155.12	1.40	217.40	2.09	0.71	0.92
33.47	174.26	154.73	1.40	216.97	2.09	0.71	0.92
33.48	173.74	154.23	1.40	216.44	2.09	0.69	0.92
33.49	173.07	153.59	1.40	215.78	2.09	0.68	0.92
33.50	172.32	152.88	1.41	215.04	2.09	0.67	0.91
33.51	171.53	152.12	1.41	214.27	2.09	0.65	0.91
33.52	170.73	151.37	1.41	213.50	2.09	0.64	0.91
33.53	169.97	150.65	1.41	212.76	2.10	0.63	0.91
33.54	169.29	150.00	1.41	212.10	2.10	0.62	0.91
33.55	168.67	149.40	1.42	211.52	2.10	0.61	0.91
33.56	167.99	148.76	1.42	210.96	2.10	0.60	0.91
33.57	167.18	147.98	1.42	210.35	2.10	0.59	0.91
33.58	166.19	147.06	1.43	209.65	2.10	0.58	0.91
33.59	165.11	146.05	1.43	208.88	2.11	0.56	0.91
33.60	163.99	145.00	1.44	208.09	2.11	0.55	0.91

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
33.61	162.89	143.96	1.44	207.31	2.11	0.53	0.91
33.62	161.86	143.00	1.44	206.59	2.12	0.52	0.91
33.63	160.96	142.15	1.45	205.96	2.12	0.51	0.91
33.64	160.15	141.38	1.45	205.43	2.12	0.51	0.90
33.65	159.32	140.60	1.46	204.94	2.12	0.50	0.90
33.66	158.37	139.71	1.46	204.42	2.13	0.49	0.90
33.67	157.28	138.68	1.47	203.83	2.13	0.48	0.90
33.68	156.10	137.58	1.48	203.20	2.14	0.47	0.90
33.69	154.90	136.46	1.48	202.58	2.14	0.46	0.90
33.70	153.74	135.38	1.49	201.98	2.14	0.45	0.90
33.71	152.67	134.38	1.50	201.44	2.15	0.44	0.90
33.72	151.76	133.53	1.51	200.97	2.15	0.43	0.90
33.73	150.96	132.77	1.51	200.54	2.15	0.43	0.90
33.74	150.13	131.99	1.52	200.10	2.16	0.42	0.90
33.75	149.19	131.11	1.52	199.58	2.16	0.41	0.90
33.76	148.14	130.13	1.53	199.01	2.16	0.40	0.89
33.77	147.03	129.09	1.54	198.41	2.17	0.40	0.89
33.78	145.91	128.06	1.54	197.83	2.17	0.39	0.89
33.79	144.85	127.07	1.55	197.27	2.17	0.38	0.89
33.80	143.90	126.18	1.56	196.78	2.18	0.37	0.89
33.81	143.10	125.43	1.57	196.36	2.18	0.37	0.89
33.82	142.35	124.73	1.57	195.98	2.18	0.36	0.89
33.83	141.56	123.99	1.58	195.60	2.18	0.36	0.89
33.84	140.65	123.13	1.58	195.16	2.19	0.35	0.89
33.85	139.64	122.20	1.59	194.69	2.19	0.35	0.89
33.86	138.60	121.23	1.60	194.21	2.20	0.34	0.89
33.87	137.58	120.28	1.61	193.74	2.20	0.34	0.88
33.88	136.62	119.40	1.62	193.30	2.20	0.33	0.88
33.89	135.79	118.62	1.63	192.93	2.20	0.33	0.88
33.90	135.25	118.11	1.63	192.73	2.21	0.32	0.88
33.91	134.97	117.82	1.64	192.72	2.21	0.32	0.88
33.92	134.88	117.71	1.64	192.87	2.21	0.32	0.88
33.93	134.79	117.60	1.64	193.05	2.21	0.32	0.88
33.94	134.68	117.47	1.65	193.25	2.21	0.32	0.88
33.95	134.58	117.34	1.65	193.45	2.21	0.32	0.88
33.96	134.47	117.22	1.65	193.65	2.21	0.32	0.88
33.97	134.38	117.10	1.66	193.83	2.22	0.32	0.88
33.98	134.30	117.00	1.66	193.98	2.22	0.32	0.88
33.99	134.23	116.91	1.66	194.12	2.22	0.32	0.88
34.00	134.17	116.83	1.66	194.27	2.22	0.32	0.88
34.01	134.10	116.74	1.67	194.46	2.22	0.32	0.88
34.02	134.03	116.64	1.67	194.67	2.22	0.32	0.88
34.03	133.95	116.54	1.67	194.90	2.22	0.32	0.88
34.04	133.87	116.43	1.68	195.13	2.22	0.32	0.88
34.05	133.79	116.33	1.68	195.34	2.22	0.32	0.88
34.06	133.73	116.24	1.68	195.54	2.23	0.32	0.88
34.07	133.62	116.12	1.68	195.64	2.23	0.32	0.88
34.08	133.42	115.91	1.69	195.64	2.23	0.32	0.88

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
34.09	133.10	115.59	1.69	195.52	2.23	0.32	0.88
34.10	132.70	115.21	1.70	195.37	2.23	0.32	0.88
34.11	132.26	114.79	1.70	195.20	2.23	0.31	0.88
34.12	131.81	114.35	1.71	195.03	2.23	0.31	0.88
34.13	131.36	113.93	1.71	194.86	2.24	0.31	0.88
34.14	130.95	113.53	1.72	194.70	2.24	0.31	0.88
34.15	130.58	113.18	1.72	194.56	2.24	0.31	0.88
34.16	130.38	112.97	1.72	194.53	2.24	0.30	0.88
34.17	130.32	112.89	1.72	194.61	2.24	0.30	0.88
34.18	130.39	112.92	1.73	194.81	2.24	0.30	0.88
34.19	130.46	112.95	1.73	195.05	2.24	0.31	0.88
34.20	130.54	112.99	1.73	195.30	2.24	0.31	0.88
34.21	130.62	113.03	1.73	195.55	2.24	0.31	0.88
34.22	130.70	113.07	1.73	195.80	2.24	0.31	0.88
34.23	130.77	113.11	1.73	196.03	2.24	0.31	0.88
34.24	130.85	113.15	1.73	196.23	2.24	0.31	0.88
34.25	131.00	113.26	1.73	196.48	2.24	0.31	0.88
34.26	131.25	113.45	1.73	196.81	2.24	0.31	0.88
34.27	131.59	113.72	1.73	197.24	2.24	0.31	0.88
34.28	131.96	114.02	1.73	197.72	2.24	0.31	0.88
34.29	132.36	114.35	1.73	198.23	2.24	0.32	0.88
34.30	132.76	114.67	1.73	198.74	2.24	0.32	0.88
34.31	133.14	114.97	1.73	199.22	2.24	0.32	0.88
34.32	133.48	115.24	1.73	199.64	2.24	0.32	0.88
34.33	133.82	115.52	1.73	200.01	2.24	0.33	0.88
34.34	134.26	115.88	1.73	200.35	2.24	0.33	0.88
34.35	134.84	116.37	1.72	200.73	2.24	0.33	0.88
34.36	135.55	116.97	1.72	201.17	2.24	0.34	0.88
34.37	136.32	117.62	1.71	201.66	2.24	0.34	0.88
34.38	137.12	118.31	1.71	202.16	2.24	0.35	0.89
34.39	137.91	118.98	1.70	202.66	2.23	0.35	0.89
34.40	138.64	119.60	1.70	203.12	2.23	0.35	0.89
34.41	139.28	120.13	1.69	203.52	2.23	0.36	0.89
34.42	139.88	120.63	1.69	203.86	2.23	0.36	0.89
34.43	140.52	121.18	1.68	204.16	2.23	0.37	0.89
34.44	141.29	121.83	1.68	204.50	2.22	0.37	0.89
34.45	142.17	122.59	1.67	204.89	2.22	0.38	0.89
34.46	143.12	123.40	1.66	205.31	2.22	0.38	0.89
34.47	144.08	124.22	1.66	205.74	2.22	0.39	0.89
34.48	145.01	125.02	1.65	206.16	2.21	0.40	0.89
34.49	145.85	125.74	1.64	206.54	2.21	0.40	0.89
34.50	146.58	126.36	1.64	206.85	2.21	0.41	0.90
34.51	147.30	126.97	1.63	207.05	2.21	0.41	0.90
34.52	148.09	127.65	1.62	207.19	2.20	0.42	0.90
34.53	149.04	128.47	1.61	207.32	2.20	0.43	0.90
34.54	150.10	129.39	1.60	207.48	2.20	0.43	0.90
34.55	151.22	130.35	1.59	207.65	2.19	0.44	0.90
34.56	152.33	131.32	1.58	207.83	2.19	0.45	0.90

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
34.57	153.39	132.23	1.57	208.00	2.18	0.46	0.90
34.58	154.32	133.04	1.56	208.16	2.18	0.47	0.90
34.59	155.17	133.77	1.56	208.29	2.18	0.48	0.90
34.60	156.04	134.52	1.55	208.38	2.17	0.48	0.90
34.61	157.06	135.40	1.54	208.47	2.17	0.49	0.90
34.62	158.27	136.46	1.53	208.59	2.16	0.50	0.90
34.63	159.59	137.61	1.52	208.73	2.16	0.51	0.91
34.64	160.95	138.80	1.51	208.90	2.15	0.53	0.91
34.65	162.28	139.97	1.49	209.08	2.14	0.54	0.91
34.66	163.52	141.05	1.48	209.26	2.14	0.55	0.91
34.67	164.60	141.99	1.47	209.43	2.13	0.56	0.91
34.68	165.50	142.77	1.47	209.49	2.13	0.57	0.91
34.69	166.34	143.49	1.46	209.46	2.13	0.58	0.91
34.70	167.24	144.28	1.45	209.35	2.12	0.58	0.91
34.71	168.27	145.19	1.44	209.25	2.11	0.59	0.91
34.72	169.37	146.16	1.43	209.16	2.11	0.60	0.91
34.73	170.49	147.14	1.42	209.10	2.10	0.61	0.91
34.74	171.57	148.09	1.41	209.06	2.10	0.62	0.91
34.75	172.55	148.96	1.40	209.05	2.09	0.63	0.91
34.76	173.37	149.67	1.40	209.03	2.08	0.64	0.91
34.77	174.04	150.25	1.39	208.97	2.08	0.64	0.91
34.78	174.67	150.79	1.39	208.86	2.08	0.65	0.91
34.79	175.35	151.39	1.38	208.71	2.07	0.65	0.91
34.80	176.10	152.06	1.37	208.58	2.06	0.66	0.91
34.81	176.90	152.76	1.36	208.46	2.06	0.66	0.91
34.82	177.69	153.46	1.36	208.35	2.05	0.67	0.91
34.83	178.45	154.12	1.35	208.27	2.05	0.67	0.91
34.84	179.11	154.71	1.35	208.21	2.04	0.68	0.91
34.85	179.64	155.17	1.34	208.14	2.04	0.68	0.91
34.86	180.06	155.53	1.34	208.07	2.03	0.68	0.91
34.87	180.45	155.85	1.33	207.96	2.03	0.68	0.91
34.88	180.87	156.22	1.33	207.85	2.03	0.68	0.91
34.89	181.34	156.63	1.33	207.74	2.02	0.68	0.91
34.90	181.82	157.05	1.32	207.63	2.02	0.68	0.91
34.91	182.29	157.46	1.32	207.53	2.01	0.68	0.91
34.92	182.73	157.83	1.31	207.45	2.01	0.68	0.91
34.93	183.09	158.15	1.31	207.36	2.00	0.69	0.91
34.94	183.24	158.27	1.31	207.14	2.00	0.68	0.91
34.95	183.18	158.19	1.31	206.72	2.00	0.68	0.91
34.96	182.92	157.95	1.30	206.09	2.00	0.67	0.91
34.97	182.62	157.68	1.30	205.38	1.99	0.65	0.91
34.98	182.30	157.40	1.30	204.62	1.99	0.64	0.91
34.99	181.98	157.11	1.30	203.86	1.99	0.63	0.91
35.00	181.67	156.83	1.30	203.13	1.99	0.62	0.90
35.01	181.39	156.57	1.29	202.47	1.98	0.61	0.90
35.02	181.10	156.30	1.29	201.86	1.98	0.60	0.90
35.03	180.67	155.91	1.29	201.19	1.98	0.59	0.90
35.04	180.05	155.33	1.29	200.37	1.98	0.58	0.90

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
35.05	179.23	154.59	1.29	199.36	1.98	0.57	0.90
35.06	178.32	153.77	1.29	198.24	1.98	0.55	0.90
35.07	177.36	152.91	1.29	197.06	1.98	0.53	0.90
35.08	176.41	152.05	1.29	195.89	1.98	0.52	0.90
35.09	175.50	151.24	1.29	194.79	1.98	0.51	0.89
35.10	174.70	150.51	1.29	193.81	1.97	0.50	0.89
35.11	173.94	149.82	1.29	192.91	1.97	0.49	0.89
35.12	173.07	149.03	1.29	191.97	1.98	0.48	0.89
35.13	171.99	148.05	1.29	190.86	1.98	0.47	0.89
35.14	170.71	146.89	1.29	189.56	1.98	0.45	0.89
35.15	169.31	145.63	1.29	188.15	1.98	0.44	0.89
35.16	167.87	144.33	1.29	186.69	1.98	0.43	0.89
35.17	166.45	143.06	1.30	185.27	1.98	0.41	0.89
35.18	165.15	141.88	1.30	183.96	1.99	0.40	0.89
35.19	164.00	140.85	1.30	182.81	1.99	0.39	0.88
35.20	162.86	139.81	1.30	181.70	1.99	0.39	0.88
35.21	161.55	138.63	1.30	180.49	1.99	0.38	0.88
35.22	159.93	137.16	1.31	179.03	2.00	0.37	0.88
35.23	158.08	135.50	1.31	177.38	2.00	0.35	0.88
35.24	156.11	133.73	1.31	175.62	2.01	0.34	0.88
35.25	154.11	131.93	1.32	173.85	2.01	0.33	0.88
35.26	152.18	130.21	1.32	172.15	2.02	0.32	0.88
35.27	150.44	128.64	1.33	170.62	2.02	0.31	0.88
35.28	148.95	127.30	1.33	169.31	2.03	0.31	0.87
35.29	147.56	126.05	1.33	168.10	2.03	0.30	0.87
35.30	146.10	124.73	1.34	166.82	2.03	0.29	0.87
35.31	144.39	123.20	1.34	165.34	2.04	0.29	0.87
35.32	142.48	121.50	1.35	163.70	2.04	0.28	0.87
35.33	140.49	119.72	1.35	162.00	2.05	0.27	0.87
35.34	138.50	117.94	1.36	160.33	2.05	0.26	0.87
35.35	136.63	116.27	1.37	158.76	2.06	0.26	0.86
35.36	134.97	114.79	1.37	157.37	2.06	0.25	0.86
35.37	133.57	113.54	1.38	156.18	2.07	0.25	0.86
35.38	132.29	112.39	1.38	155.03	2.07	0.24	0.86
35.39	130.92	111.17	1.38	153.76	2.07	0.24	0.86
35.40	129.35	109.77	1.39	152.30	2.08	0.23	0.86
35.41	127.63	108.25	1.39	150.72	2.08	0.23	0.86
35.42	125.87	106.69	1.40	149.11	2.08	0.22	0.85
35.43	124.15	105.16	1.40	147.54	2.09	0.22	0.85
35.44	122.55	103.75	1.41	146.09	2.09	0.21	0.85
35.45	121.19	102.54	1.41	144.84	2.10	0.21	0.85
35.46	120.09	101.56	1.42	143.83	2.10	0.21	0.85
35.47	119.14	100.71	1.42	142.91	2.10	0.21	0.85
35.48	118.16	99.84	1.42	141.95	2.10	0.20	0.85
35.49	117.05	98.85	1.42	140.86	2.10	0.20	0.84
35.50	115.86	97.80	1.43	139.70	2.11	0.20	0.84
35.51	114.66	96.74	1.43	138.54	2.11	0.19	0.84
35.52	113.51	95.72	1.44	137.42	2.11	0.19	0.84

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
35.53	112.47	94.80	1.44	136.41	2.11	0.19	0.84
35.54	111.62	94.04	1.44	135.61	2.12	0.19	0.84
35.55	110.98	93.47	1.44	135.04	2.12	0.19	0.84
35.56	110.45	92.98	1.45	134.62	2.12	0.18	0.84
35.57	109.90	92.48	1.45	134.22	2.12	0.18	0.84
35.58	109.29	91.93	1.46	133.78	2.12	0.18	0.84
35.59	108.65	91.35	1.46	133.32	2.13	0.18	0.84
35.60	108.02	90.78	1.46	132.87	2.13	0.18	0.83
35.61	107.42	90.24	1.47	132.45	2.13	0.18	0.83
35.62	106.89	89.76	1.47	132.08	2.13	0.18	0.83
35.63	106.46	89.36	1.48	131.81	2.13	0.18	0.83
35.64	106.08	89.01	1.48	131.66	2.14	0.18	0.83
35.65	105.70	88.66	1.48	131.58	2.14	0.18	0.83
35.66	105.27	88.25	1.49	131.51	2.14	0.18	0.83
35.67	104.81	87.82	1.50	131.45	2.15	0.18	0.83
35.68	104.33	87.38	1.50	131.39	2.15	0.18	0.83
35.69	103.86	86.94	1.51	131.33	2.15	0.17	0.83
35.70	103.42	86.54	1.52	131.28	2.16	0.17	0.83
35.71	103.06	86.19	1.52	131.24	2.16	0.17	0.83
35.72	102.78	85.93	1.53	131.25	2.16	0.17	0.83
35.73	102.57	85.72	1.53	131.31	2.16	0.17	0.83
35.74	102.37	85.53	1.54	131.43	2.17	0.17	0.83
35.75	102.15	85.31	1.54	131.56	2.17	0.17	0.83
35.76	101.91	85.08	1.55	131.71	2.17	0.17	0.83
35.77	101.67	84.84	1.55	131.85	2.17	0.17	0.83
35.78	101.44	84.62	1.56	132.00	2.18	0.17	0.83
35.79	101.23	84.41	1.57	132.13	2.18	0.17	0.83
35.80	101.09	84.26	1.57	132.24	2.18	0.17	0.83
35.81	101.03	84.19	1.57	132.34	2.18	0.17	0.83
35.82	101.05	84.19	1.57	132.44	2.18	0.17	0.83
35.83	101.12	84.23	1.57	132.55	2.18	0.17	0.83
35.84	101.20	84.28	1.57	132.67	2.18	0.17	0.83
35.85	101.28	84.33	1.57	132.81	2.18	0.17	0.83
35.86	101.36	84.38	1.58	132.94	2.18	0.17	0.83
35.87	101.43	84.42	1.58	133.06	2.18	0.17	0.83
35.88	101.50	84.46	1.58	133.17	2.18	0.17	0.83
35.89	101.60	84.53	1.58	133.24	2.18	0.17	0.83
35.90	101.76	84.65	1.57	133.29	2.18	0.17	0.83
35.91	102.00	84.84	1.57	133.33	2.18	0.17	0.83
35.92	102.29	85.08	1.57	133.37	2.18	0.17	0.83
35.93	102.60	85.33	1.56	133.41	2.18	0.18	0.83
35.94	102.92	85.60	1.56	133.46	2.18	0.18	0.83
35.95	103.23	85.85	1.56	133.51	2.17	0.18	0.83
35.96	103.52	86.09	1.55	133.55	2.17	0.18	0.83
35.97	103.77	86.29	1.55	133.59	2.17	0.18	0.83
35.98	103.99	86.47	1.54	133.58	2.17	0.18	0.83
35.99	104.22	86.66	1.54	133.52	2.17	0.18	0.83
36.00	104.48	86.87	1.54	133.42	2.17	0.18	0.83

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
36.01	104.78	87.12	1.53	133.31	2.16	0.18	0.83
36.02	105.10	87.39	1.52	133.21	2.16	0.18	0.83
36.03	105.42	87.65	1.52	133.10	2.16	0.18	0.83
36.04	105.72	87.91	1.51	133.00	2.15	0.18	0.83
36.05	106.00	88.14	1.51	132.91	2.15	0.18	0.83
36.06	106.23	88.32	1.50	132.81	2.15	0.18	0.83
36.07	106.42	88.48	1.50	132.66	2.15	0.18	0.83
36.08	106.60	88.64	1.49	132.44	2.15	0.18	0.83
36.09	106.81	88.81	1.49	132.17	2.14	0.18	0.83
36.10	107.04	89.01	1.48	131.87	2.14	0.18	0.83
36.11	107.28	89.21	1.47	131.57	2.13	0.18	0.83
36.12	107.52	89.41	1.47	131.27	2.13	0.18	0.83
36.13	107.74	89.60	1.46	131.00	2.13	0.18	0.83
36.14	107.94	89.77	1.46	130.76	2.12	0.18	0.83
36.15	108.08	89.88	1.45	130.58	2.12	0.18	0.83
36.16	108.18	89.96	1.45	130.46	2.12	0.18	0.83
36.17	108.24	90.00	1.45	130.37	2.12	0.18	0.83
36.18	108.32	90.05	1.45	130.28	2.12	0.18	0.83
36.19	108.39	90.10	1.44	130.18	2.12	0.18	0.83
36.20	108.47	90.16	1.44	130.07	2.12	0.18	0.83
36.21	108.55	90.22	1.44	129.97	2.11	0.18	0.83
36.22	108.62	90.27	1.44	129.88	2.11	0.18	0.83
36.23	108.68	90.30	1.44	129.81	2.11	0.18	0.83
36.24	108.72	90.31	1.44	129.84	2.11	0.18	0.83
36.25	108.73	90.30	1.44	129.97	2.11	0.18	0.83
36.26	108.73	90.28	1.44	130.20	2.12	0.18	0.83
36.27	108.73	90.25	1.45	130.46	2.12	0.18	0.83
36.28	108.73	90.22	1.45	130.75	2.12	0.18	0.83
36.29	108.73	90.19	1.45	131.03	2.12	0.18	0.83
36.30	108.73	90.16	1.46	131.31	2.12	0.18	0.83
36.31	108.73	90.13	1.46	131.56	2.13	0.18	0.83
36.32	108.72	90.10	1.46	131.79	2.13	0.18	0.83
36.33	108.70	90.04	1.47	132.08	2.13	0.18	0.83
36.34	108.64	89.97	1.47	132.46	2.13	0.18	0.83
36.35	108.58	89.87	1.48	132.94	2.14	0.18	0.84
36.36	108.50	89.77	1.49	133.48	2.14	0.18	0.84
36.37	108.42	89.66	1.50	134.04	2.15	0.18	0.84
36.38	108.34	89.55	1.50	134.61	2.15	0.18	0.84
36.39	108.27	89.45	1.51	135.16	2.15	0.18	0.84
36.40	108.20	89.36	1.52	135.64	2.16	0.18	0.84
36.41	108.12	89.25	1.52	136.05	2.16	0.18	0.84
36.42	107.99	89.11	1.53	136.45	2.16	0.18	0.84
36.43	107.81	88.91	1.54	136.89	2.17	0.19	0.84
36.44	107.59	88.69	1.55	137.41	2.17	0.19	0.84
36.45	107.35	88.45	1.56	137.99	2.18	0.19	0.84
36.46	107.11	88.20	1.57	138.59	2.18	0.19	0.84
36.47	106.88	87.96	1.58	139.18	2.19	0.19	0.84
36.48	106.67	87.74	1.59	139.74	2.19	0.19	0.84

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
36.49	106.48	87.55	1.60	140.20	2.19	0.19	0.84
36.50	106.31	87.38	1.61	140.56	2.20	0.19	0.84
36.51	106.14	87.20	1.62	140.86	2.20	0.19	0.84
36.52	105.94	87.00	1.62	141.16	2.20	0.19	0.84
36.53	105.72	86.78	1.63	141.50	2.21	0.19	0.84
36.54	105.48	86.54	1.64	141.87	2.21	0.19	0.84
36.55	105.24	86.31	1.65	142.25	2.21	0.19	0.84
36.56	105.02	86.08	1.66	142.61	2.22	0.19	0.84
36.57	104.81	85.87	1.66	142.93	2.22	0.19	0.84
36.58	104.65	85.71	1.67	143.19	2.22	0.19	0.84
36.59	104.54	85.59	1.68	143.39	2.22	0.19	0.84
36.60	104.47	85.51	1.68	143.56	2.22	0.19	0.84
36.61	104.40	85.42	1.68	143.75	2.23	0.19	0.84
36.62	104.32	85.33	1.69	143.96	2.23	0.19	0.84
36.63	104.24	85.24	1.69	144.17	2.23	0.19	0.84
36.64	104.16	85.15	1.70	144.39	2.23	0.19	0.84
36.65	104.09	85.06	1.70	144.59	2.23	0.19	0.84
36.66	104.02	84.98	1.70	144.77	2.23	0.19	0.84
36.67	103.98	84.93	1.71	144.89	2.23	0.19	0.84
36.68	103.96	84.89	1.71	144.98	2.23	0.19	0.84
36.69	103.96	84.87	1.71	145.04	2.24	0.19	0.84
36.70	103.96	84.85	1.71	145.12	2.24	0.19	0.84
36.71	103.96	84.83	1.71	145.20	2.24	0.19	0.84
36.72	103.96	84.81	1.71	145.28	2.24	0.19	0.84
36.73	103.96	84.79	1.71	145.36	2.24	0.19	0.84
36.74	103.96	84.77	1.72	145.43	2.24	0.19	0.84
36.75	103.96	84.74	1.72	145.49	2.24	0.19	0.84
36.76	103.94	84.70	1.72	145.56	2.24	0.19	0.84
36.77	103.89	84.65	1.72	145.64	2.24	0.19	0.84
36.78	103.83	84.57	1.72	145.74	2.24	0.19	0.84
36.79	103.75	84.48	1.73	145.86	2.24	0.19	0.84
36.80	103.67	84.39	1.73	145.98	2.24	0.19	0.84
36.81	103.59	84.30	1.73	146.11	2.24	0.19	0.84
36.82	103.52	84.22	1.74	146.23	2.24	0.19	0.84
36.83	103.45	84.14	1.74	146.33	2.25	0.19	0.84
36.84	103.38	84.06	1.74	146.44	2.25	0.19	0.84
36.85	103.30	83.96	1.75	146.57	2.25	0.19	0.84
36.86	103.18	83.84	1.75	146.76	2.25	0.19	0.84
36.87	103.04	83.70	1.76	146.99	2.25	0.19	0.84
36.88	102.89	83.54	1.76	147.26	2.25	0.19	0.84
36.89	102.73	83.38	1.77	147.53	2.26	0.19	0.84
36.90	102.57	83.22	1.78	147.80	2.26	0.19	0.84
36.91	102.42	83.07	1.78	148.05	2.26	0.19	0.84
36.92	102.29	82.94	1.79	148.28	2.26	0.19	0.84
36.93	102.15	82.79	1.79	148.41	2.26	0.19	0.84
36.94	101.96	82.61	1.80	148.46	2.26	0.19	0.84
36.95	101.72	82.38	1.80	148.44	2.27	0.18	0.84
36.96	101.42	82.11	1.81	148.41	2.27	0.18	0.84

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
36.97	101.11	81.83	1.81	148.38	2.27	0.18	0.83
36.98	100.79	81.54	1.82	148.35	2.27	0.18	0.83
36.99	100.48	81.25	1.83	148.33	2.27	0.18	0.83
37.00	100.19	80.99	1.83	148.30	2.27	0.18	0.83
37.01	99.96	80.77	1.84	148.27	2.28	0.18	0.83
37.02	99.78	80.60	1.84	148.16	2.28	0.18	0.83
37.03	99.64	80.47	1.84	147.97	2.28	0.18	0.83
37.04	99.51	80.34	1.84	147.70	2.28	0.18	0.83
37.05	99.36	80.20	1.84	147.40	2.28	0.18	0.83
37.06	99.20	80.05	1.84	147.08	2.28	0.18	0.83
37.07	99.04	79.91	1.84	146.76	2.28	0.18	0.83
37.08	98.89	79.76	1.84	146.45	2.28	0.18	0.83
37.09	98.75	79.64	1.84	146.18	2.28	0.18	0.83
37.10	98.66	79.55	1.83	145.91	2.27	0.18	0.83
37.11	98.64	79.52	1.83	145.59	2.27	0.18	0.83
37.12	98.68	79.54	1.83	145.19	2.27	0.18	0.83
37.13	98.75	79.60	1.82	144.70	2.27	0.18	0.83
37.14	98.83	79.66	1.81	144.16	2.27	0.18	0.83
37.15	98.91	79.72	1.80	143.60	2.27	0.18	0.83
37.16	98.98	79.78	1.79	143.05	2.26	0.18	0.83
37.17	99.06	79.84	1.79	142.54	2.26	0.18	0.83
37.18	99.12	79.88	1.78	142.09	2.26	0.18	0.83
37.19	99.16	79.91	1.77	141.81	2.26	0.18	0.83
37.20	99.18	79.91	1.77	141.68	2.26	0.18	0.83
37.21	99.18	79.89	1.77	141.67	2.26	0.18	0.83
37.22	99.18	79.88	1.77	141.68	2.26	0.18	0.83
37.23	99.18	79.86	1.77	141.68	2.26	0.18	0.83
37.24	99.18	79.84	1.77	141.69	2.26	0.18	0.83
37.25	99.18	79.82	1.78	141.69	2.26	0.18	0.83
37.26	99.18	79.81	1.78	141.70	2.26	0.18	0.83
37.27	99.19	79.80	1.78	141.67	2.26	0.18	0.83
37.28	99.24	79.82	1.77	141.50	2.26	0.18	0.83
37.29	99.33	79.89	1.77	141.16	2.25	0.18	0.83
37.30	99.46	80.00	1.76	140.66	2.25	0.18	0.83
37.31	99.61	80.12	1.75	140.10	2.25	0.18	0.83
37.32	99.77	80.25	1.74	139.52	2.25	0.18	0.83
37.33	99.93	80.39	1.73	138.94	2.24	0.18	0.83
37.34	100.08	80.51	1.72	138.39	2.24	0.18	0.83
37.35	100.22	80.62	1.71	137.90	2.24	0.18	0.83
37.36	100.32	80.71	1.70	137.43	2.23	0.18	0.83
37.37	100.40	80.78	1.69	136.90	2.23	0.17	0.83
37.38	100.47	80.83	1.69	136.23	2.23	0.17	0.83
37.39	100.54	80.90	1.67	135.42	2.22	0.17	0.83
37.40	100.62	80.97	1.66	134.54	2.22	0.17	0.83
37.41	100.69	81.04	1.65	133.64	2.21	0.17	0.83
37.42	100.77	81.12	1.64	132.76	2.21	0.17	0.83
37.43	100.85	81.19	1.63	131.94	2.20	0.17	0.83
37.44	100.91	81.25	1.62	131.23	2.20	0.17	0.83

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
37.45	100.92	81.24	1.61	130.97	2.20	0.17	0.83
37.46	100.86	81.17	1.62	131.19	2.20	0.17	0.83
37.47	100.74	81.03	1.63	131.87	2.21	0.17	0.83
37.48	100.59	80.86	1.64	132.69	2.21	0.17	0.83
37.49	100.43	80.68	1.66	133.58	2.22	0.17	0.83
37.50	100.27	80.51	1.67	134.50	2.22	0.17	0.83
37.51	100.12	80.33	1.69	135.40	2.23	0.17	0.83
37.52	99.98	80.17	1.70	136.23	2.23	0.17	0.83
37.53	99.86	80.03	1.71	136.92	2.24	0.17	0.83
37.54	99.75	79.91	1.72	137.46	2.24	0.17	0.83
37.55	99.63	79.78	1.73	137.91	2.24	0.17	0.83
37.56	99.50	79.64	1.74	138.37	2.24	0.17	0.83
37.57	99.35	79.48	1.75	138.90	2.25	0.17	0.83
37.58	99.19	79.31	1.76	139.46	2.25	0.17	0.83
37.59	99.03	79.15	1.77	140.02	2.26	0.17	0.83
37.60	98.88	78.99	1.78	140.55	2.26	0.17	0.83
37.61	98.74	78.85	1.79	141.04	2.26	0.18	0.83
37.62	98.62	78.72	1.80	141.45	2.26	0.18	0.83
37.63	98.51	78.60	1.80	141.84	2.27	0.18	0.83
37.64	98.39	78.47	1.81	142.28	2.27	0.18	0.83
37.65	98.25	78.32	1.82	142.79	2.27	0.18	0.83
37.66	98.10	78.16	1.83	143.35	2.27	0.18	0.83
37.67	97.94	78.00	1.85	143.94	2.28	0.18	0.83
37.68	97.78	77.83	1.86	144.52	2.28	0.18	0.83
37.69	97.64	77.68	1.87	145.06	2.28	0.18	0.83
37.70	97.51	77.55	1.88	145.54	2.29	0.18	0.83
37.71	97.39	77.42	1.89	146.12	2.29	0.18	0.83
37.72	97.28	77.29	1.90	146.93	2.29	0.18	0.83
37.73	97.16	77.15	1.92	148.05	2.30	0.18	0.83
37.74	97.01	76.98	1.94	149.35	2.30	0.18	0.83
37.75	96.85	76.80	1.96	150.76	2.31	0.18	0.83
37.76	96.69	76.62	1.99	152.19	2.32	0.18	0.83
37.77	96.54	76.45	2.01	153.59	2.32	0.18	0.83
37.78	96.40	76.29	2.03	154.87	2.33	0.18	0.83
37.79	96.27	76.14	2.05	155.97	2.33	0.18	0.83
37.80	96.11	75.98	2.07	156.97	2.34	0.18	0.83
37.81	95.90	75.76	2.09	158.01	2.34	0.18	0.83
37.82	95.63	75.50	2.11	159.22	2.35	0.18	0.83
37.83	95.33	75.21	2.14	160.59	2.35	0.18	0.83
37.84	95.01	74.90	2.16	162.03	2.36	0.18	0.83
37.85	94.69	74.59	2.19	163.48	2.36	0.18	0.83
37.86	94.39	74.30	2.22	164.85	2.37	0.18	0.83
37.87	94.12	74.04	2.24	166.08	2.37	0.18	0.83
37.88	93.88	73.80	2.27	167.19	2.38	0.18	0.83
37.89	93.63	73.56	2.29	168.35	2.38	0.18	0.83
37.90	93.33	73.27	2.32	169.72	2.39	0.18	0.83
37.91	92.98	72.94	2.35	171.36	2.40	0.18	0.83
37.92	92.59	72.57	2.39	173.15	2.40	0.18	0.83

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)'/σ'_v}	S _{u(peak)'/σ'_v}
37.93	92.19	72.20	2.42	175.01	2.41	0.18	0.83
37.94	91.80	71.83	2.46	176.83	2.42	0.18	0.83
37.95	91.43	71.48	2.50	178.52	2.42	0.18	0.83
37.96	91.12	71.18	2.53	179.99	2.43	0.18	0.83
37.97	90.82	70.90	2.56	181.19	2.43	0.18	0.83
37.98	90.50	70.60	2.58	182.28	2.44	0.18	0.83
37.99	90.11	70.25	2.61	183.41	2.44	0.18	0.83
38.00	89.67	69.86	2.64	184.70	2.45	0.17	0.82
38.01	89.20	69.43	2.68	186.09	2.45	0.17	0.82
38.02	88.72	69.00	2.72	187.49	2.46	0.17	0.82
38.03	88.26	68.59	2.75	188.84	2.47	0.17	0.82
38.04	87.84	68.20	2.79	190.06	2.47	0.17	0.82
38.05	87.48	67.89	2.81	191.05	2.48	0.17	0.82
38.06	87.20	67.63	2.84	191.76	2.48	0.17	0.82
38.07	86.95	67.40	2.85	192.30	2.48	0.17	0.82
38.08	86.68	67.15	2.87	192.80	2.48	0.17	0.82
38.09	86.37	66.88	2.89	193.37	2.49	0.17	0.82
38.10	86.06	66.59	2.91	193.96	2.49	0.17	0.82
38.11	85.74	66.31	2.93	194.55	2.49	0.17	0.82
38.12	85.44	66.04	2.95	195.10	2.50	0.17	0.82
38.13	85.17	65.80	2.97	195.59	2.50	0.17	0.82
38.14	85.10	65.72	2.98	195.91	2.50	0.17	0.82
38.15	85.36	65.92	2.97	196.03	2.50	0.17	0.82
38.16	85.95	66.39	2.95	195.97	2.50	0.17	0.82
38.17	86.73	67.01	2.92	195.84	2.49	0.17	0.82
38.18	87.59	67.70	2.89	195.70	2.49	0.17	0.82
38.19	88.47	68.40	2.86	195.55	2.48	0.17	0.82
38.20	89.33	69.10	2.83	195.39	2.48	0.18	0.82
38.21	90.14	69.75	2.80	195.24	2.47	0.18	0.83
38.22	90.84	70.31	2.77	195.09	2.47	0.18	0.83
38.23	91.74	71.04	2.74	194.78	2.46	0.18	0.83
38.24	93.00	72.06	2.70	194.22	2.46	0.18	0.83
38.25	94.73	73.48	2.63	193.37	2.45	0.19	0.83
38.26	96.72	75.11	2.56	192.37	2.43	0.19	0.83
38.27	98.84	76.86	2.49	191.26	2.42	0.19	0.84
38.28	101.01	78.64	2.42	190.12	2.41	0.20	0.84
38.29	103.09	80.36	2.35	188.99	2.40	0.20	0.84
38.30	104.99	81.93	2.29	187.95	2.38	0.21	0.84
38.31	106.63	83.28	2.25	187.06	2.37	0.21	0.85
38.32	108.17	84.55	2.20	186.22	2.37	0.21	0.85
38.33	109.84	85.93	2.16	185.34	2.36	0.22	0.85
38.34	111.81	87.56	2.10	184.32	2.34	0.22	0.85
38.35	114.00	89.39	2.05	183.19	2.33	0.23	0.85
38.36	116.31	91.32	1.99	182.02	2.32	0.23	0.86
38.37	118.62	93.24	1.94	180.87	2.30	0.24	0.86
38.38	120.80	95.07	1.89	179.81	2.29	0.25	0.86
38.39	122.75	96.70	1.85	178.89	2.28	0.25	0.86
38.40	124.30	98.00	1.82	178.43	2.27	0.26	0.87

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
38.41	125.59	99.05	1.80	178.53	2.27	0.26	0.87
38.42	126.79	100.02	1.79	179.19	2.26	0.26	0.87
38.43	128.14	101.11	1.78	180.10	2.26	0.27	0.87
38.44	129.62	102.30	1.77	181.09	2.26	0.28	0.87
38.45	131.14	103.53	1.76	182.13	2.25	0.28	0.87
38.46	132.63	104.73	1.75	183.14	2.25	0.29	0.87
38.47	134.02	105.85	1.74	184.09	2.25	0.30	0.88
38.48	135.21	106.81	1.73	184.93	2.24	0.30	0.88
38.49	135.93	107.36	1.73	185.92	2.24	0.31	0.88
38.50	136.24	107.56	1.74	187.22	2.25	0.31	0.88
38.51	136.24	107.49	1.76	189.00	2.25	0.31	0.88
38.52	136.24	107.41	1.78	191.06	2.26	0.31	0.88
38.53	136.24	107.33	1.80	193.28	2.26	0.32	0.88
38.54	136.24	107.25	1.82	195.55	2.27	0.32	0.88
38.55	136.25	107.17	1.85	197.76	2.28	0.32	0.88
38.56	136.25	107.10	1.87	199.79	2.28	0.32	0.88
38.57	136.17	106.97	1.88	201.49	2.29	0.33	0.88
38.58	135.87	106.66	1.90	202.97	2.29	0.33	0.88
38.59	135.29	106.12	1.93	204.41	2.30	0.32	0.88
38.60	134.48	105.38	1.96	206.05	2.31	0.32	0.88
38.61	133.57	104.56	1.99	207.89	2.32	0.32	0.88
38.62	132.61	103.70	2.02	209.85	2.33	0.31	0.88
38.63	131.66	102.85	2.06	211.80	2.33	0.31	0.88
38.64	130.76	102.04	2.09	213.67	2.34	0.31	0.88
38.65	129.95	101.32	2.13	215.32	2.35	0.31	0.88
38.66	129.23	100.67	2.15	216.77	2.36	0.30	0.88
38.67	128.46	99.99	2.18	218.20	2.36	0.30	0.88
38.68	127.56	99.19	2.22	219.82	2.37	0.30	0.87
38.69	126.49	98.25	2.26	221.71	2.38	0.29	0.87
38.70	125.33	97.24	2.30	223.77	2.39	0.29	0.87
38.71	124.13	96.19	2.35	225.89	2.40	0.28	0.87
38.72	122.95	95.17	2.40	227.96	2.40	0.28	0.87
38.73	121.86	94.22	2.44	229.87	2.41	0.28	0.87
38.74	120.92	93.40	2.48	231.50	2.42	0.27	0.87
38.75	120.17	92.75	2.51	232.64	2.42	0.27	0.87
38.76	119.53	92.19	2.53	233.43	2.43	0.27	0.87
38.77	118.88	91.63	2.55	234.03	2.43	0.27	0.87
38.78	118.14	91.00	2.58	234.71	2.44	0.26	0.86
38.79	117.35	90.32	2.61	235.43	2.44	0.26	0.86
38.80	116.55	89.63	2.63	236.16	2.45	0.26	0.86
38.81	115.79	88.97	2.66	236.85	2.45	0.26	0.86
38.82	115.09	88.37	2.69	237.47	2.46	0.25	0.86
38.83	114.58	87.94	2.70	237.85	2.46	0.25	0.86
38.84	114.42	87.78	2.71	237.76	2.46	0.25	0.86
38.85	114.57	87.89	2.70	237.19	2.46	0.25	0.86
38.86	114.91	88.16	2.68	236.27	2.45	0.25	0.86
38.87	115.29	88.46	2.66	235.25	2.45	0.25	0.86
38.88	115.69	88.78	2.64	234.17	2.45	0.25	0.86

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
38.89	116.08	89.09	2.62	233.10	2.44	0.25	0.86
38.90	116.46	89.39	2.60	232.08	2.44	0.26	0.86
38.91	116.79	89.65	2.58	231.18	2.44	0.26	0.86
38.92	117.22	89.99	2.56	230.20	2.43	0.26	0.86
38.93	117.86	90.51	2.53	228.95	2.43	0.26	0.86
38.94	118.80	91.28	2.49	227.25	2.42	0.26	0.86
38.95	119.94	92.22	2.44	225.21	2.41	0.27	0.87
38.96	121.18	93.25	2.39	222.97	2.40	0.27	0.87
38.97	122.46	94.31	2.34	220.65	2.39	0.27	0.87
38.98	123.72	95.35	2.29	218.38	2.38	0.28	0.87
38.99	124.88	96.32	2.25	216.27	2.37	0.28	0.87
39.00	125.89	97.16	2.21	214.43	2.37	0.29	0.87
39.01	126.86	97.96	2.17	212.76	2.36	0.29	0.87
39.02	127.93	98.85	2.13	211.04	2.35	0.29	0.87
39.03	129.23	99.94	2.09	209.04	2.34	0.30	0.87
39.04	130.71	101.18	2.04	206.78	2.33	0.30	0.88
39.05	132.29	102.50	1.99	204.38	2.32	0.31	0.88
39.06	133.89	103.85	1.94	201.98	2.31	0.31	0.88
39.07	135.42	105.15	1.90	199.70	2.29	0.32	0.88
39.08	136.82	106.33	1.86	197.67	2.28	0.32	0.88
39.09	137.99	107.32	1.83	196.07	2.27	0.33	0.88
39.10	139.01	108.18	1.80	194.96	2.27	0.33	0.88
39.11	140.04	109.03	1.78	194.17	2.26	0.33	0.88
39.12	141.20	110.00	1.76	193.45	2.25	0.34	0.88
39.13	142.50	111.07	1.73	192.67	2.24	0.34	0.89
39.14	143.85	112.21	1.71	191.87	2.24	0.35	0.89
39.15	145.20	113.33	1.69	191.11	2.23	0.36	0.89
39.16	146.47	114.40	1.66	190.41	2.22	0.36	0.89
39.17	147.60	115.34	1.65	189.82	2.21	0.37	0.89
39.18	148.54	116.11	1.63	189.53	2.21	0.37	0.89
39.19	149.38	116.79	1.62	189.63	2.20	0.38	0.89
39.20	150.25	117.48	1.62	190.08	2.20	0.38	0.89
39.21	151.26	118.28	1.61	190.69	2.20	0.39	0.89
39.22	152.35	119.15	1.61	191.35	2.20	0.40	0.89
39.23	153.47	120.04	1.60	192.04	2.19	0.41	0.89
39.24	154.56	120.91	1.59	192.71	2.19	0.42	0.90
39.25	155.58	121.71	1.59	193.33	2.19	0.42	0.90
39.26	156.45	122.40	1.58	193.87	2.19	0.43	0.90
39.27	157.15	122.95	1.58	194.40	2.19	0.44	0.90
39.28	157.78	123.43	1.58	195.00	2.19	0.44	0.90
39.29	158.43	123.92	1.58	195.73	2.19	0.45	0.90
39.30	159.18	124.49	1.58	196.56	2.19	0.46	0.90
39.31	159.97	125.09	1.58	197.46	2.19	0.47	0.90
39.32	160.77	125.70	1.58	198.36	2.18	0.48	0.90
39.33	161.53	126.29	1.58	199.23	2.18	0.48	0.90
39.34	162.23	126.81	1.58	200.01	2.18	0.49	0.90
39.35	162.80	127.24	1.58	200.63	2.18	0.50	0.90
39.36	163.28	127.60	1.58	201.06	2.18	0.51	0.91

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
39.37	163.71	127.93	1.57	201.36	2.18	0.51	0.91
39.38	164.20	128.29	1.57	201.65	2.18	0.52	0.91
39.39	164.73	128.70	1.57	201.97	2.18	0.52	0.91
39.40	165.29	129.13	1.57	202.30	2.18	0.53	0.91
39.41	165.84	129.56	1.56	202.64	2.18	0.53	0.91
39.42	166.37	129.96	1.56	202.96	2.18	0.54	0.91
39.43	166.83	130.31	1.56	203.23	2.18	0.55	0.91
39.44	167.20	130.58	1.56	203.50	2.18	0.55	0.91
39.45	167.53	130.81	1.56	203.82	2.18	0.56	0.91
39.46	167.84	131.03	1.56	204.22	2.18	0.56	0.91
39.47	168.20	131.29	1.56	204.71	2.18	0.57	0.91
39.48	168.59	131.56	1.56	205.24	2.18	0.57	0.91
39.49	168.99	131.85	1.56	205.79	2.18	0.58	0.91
39.50	169.38	132.13	1.56	206.32	2.18	0.59	0.91
39.51	169.74	132.38	1.56	206.81	2.18	0.59	0.91
39.52	170.05	132.59	1.56	207.23	2.18	0.60	0.91
39.53	170.25	132.71	1.56	207.59	2.18	0.60	0.91
39.54	170.36	132.77	1.57	207.95	2.18	0.60	0.91
39.55	170.43	132.77	1.57	208.35	2.18	0.61	0.91
39.56	170.50	132.79	1.57	208.82	2.18	0.61	0.91
39.57	170.58	132.80	1.58	209.32	2.18	0.61	0.91
39.58	170.66	132.82	1.58	209.82	2.19	0.62	0.91
39.59	170.74	132.83	1.58	210.30	2.19	0.62	0.91
39.60	170.81	132.85	1.59	210.74	2.19	0.62	0.91
39.61	170.88	132.86	1.59	210.99	2.19	0.62	0.91
39.62	170.96	132.90	1.59	210.91	2.19	0.62	0.91
39.63	171.07	132.99	1.58	210.48	2.19	0.62	0.91
39.64	171.21	133.10	1.58	209.83	2.18	0.62	0.91
39.65	171.36	133.23	1.57	209.12	2.18	0.62	0.91
39.66	171.52	133.36	1.56	208.38	2.18	0.62	0.91
39.67	171.67	133.50	1.56	207.66	2.18	0.62	0.91
39.68	171.82	133.63	1.55	206.99	2.17	0.62	0.91
39.69	171.95	133.74	1.54	206.39	2.17	0.61	0.91
39.70	172.07	133.83	1.54	205.89	2.17	0.61	0.91
39.71	172.18	133.91	1.53	205.41	2.16	0.61	0.91
39.72	172.30	134.01	1.53	204.91	2.16	0.61	0.91
39.73	172.45	134.13	1.52	204.34	2.16	0.61	0.91
39.74	172.60	134.26	1.52	203.73	2.16	0.61	0.91
39.75	172.76	134.40	1.51	203.10	2.15	0.61	0.91
39.76	172.92	134.54	1.51	202.50	2.15	0.60	0.91
39.77	173.06	134.66	1.50	201.95	2.15	0.60	0.91
39.78	173.17	134.74	1.50	201.49	2.15	0.60	0.91
39.79	173.13	134.70	1.49	201.17	2.14	0.60	0.91
39.80	172.93	134.51	1.49	200.96	2.14	0.60	0.91
39.81	172.58	134.19	1.50	200.81	2.15	0.59	0.91
39.82	172.18	133.83	1.50	200.64	2.15	0.59	0.91
39.83	171.76	133.45	1.50	200.46	2.15	0.58	0.91
39.84	171.33	133.07	1.51	200.28	2.15	0.58	0.91

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
39.85	170.92	132.70	1.51	200.11	2.15	0.57	0.91
39.86	170.55	132.37	1.51	199.96	2.15	0.57	0.91
39.87	170.19	132.03	1.51	199.85	2.16	0.56	0.91
39.88	169.71	131.60	1.52	199.80	2.16	0.56	0.91
39.89	169.05	131.01	1.53	199.83	2.16	0.55	0.91
39.90	168.22	130.28	1.53	199.90	2.17	0.55	0.91
39.91	167.30	129.47	1.54	199.99	2.17	0.54	0.91
39.92	166.34	128.63	1.56	200.10	2.18	0.53	0.91
39.93	165.39	127.80	1.57	200.22	2.18	0.52	0.91
39.94	164.50	127.02	1.58	200.34	2.18	0.51	0.91
39.95	163.71	126.32	1.59	200.46	2.19	0.50	0.91
39.96	163.15	125.82	1.59	200.67	2.19	0.50	0.90
39.97	162.77	125.46	1.60	201.04	2.20	0.50	0.90
39.98	162.53	125.20	1.61	201.62	2.20	0.50	0.90
39.99	162.26	124.92	1.62	202.31	2.20	0.50	0.90
40.00	161.98	124.63	1.63	203.08	2.21	0.50	0.90
40.01	161.68	124.33	1.64	203.87	2.21	0.50	0.90
40.02	161.40	124.03	1.65	204.66	2.21	0.50	0.90
40.03	161.14	123.76	1.66	205.38	2.22	0.50	0.90
40.04	160.96	123.56	1.67	205.98	2.22	0.50	0.90
40.05	161.13	123.66	1.67	206.34	2.22	0.50	0.90
40.06	161.68	124.08	1.66	206.51	2.22	0.50	0.91
40.07	162.61	124.82	1.65	206.55	2.22	0.51	0.91
40.08	163.65	125.66	1.64	206.62	2.21	0.52	0.91
40.09	164.76	126.55	1.63	206.69	2.21	0.54	0.91
40.10	165.88	127.44	1.62	206.77	2.20	0.55	0.91
40.11	166.95	128.30	1.61	206.86	2.20	0.56	0.91
40.12	167.91	129.07	1.60	206.94	2.20	0.57	0.91
40.13	168.71	129.71	1.60	206.96	2.19	0.58	0.91
40.14	169.40	130.26	1.59	206.86	2.19	0.59	0.91
40.15	170.08	130.80	1.58	206.62	2.19	0.59	0.91
40.16	170.84	131.43	1.57	206.31	2.18	0.60	0.91
40.17	171.68	132.12	1.56	205.98	2.18	0.61	0.91
40.18	172.56	132.84	1.55	205.64	2.17	0.62	0.91
40.19	173.43	133.56	1.54	205.33	2.17	0.62	0.91
40.20	174.25	134.23	1.53	205.04	2.16	0.63	0.91
40.21	174.97	134.82	1.52	204.80	2.16	0.64	0.91
40.22	175.43	135.19	1.51	204.58	2.15	0.65	0.92
40.23	175.65	135.36	1.51	204.37	2.15	0.65	0.92
40.24	175.67	135.36	1.51	204.12	2.15	0.64	0.91
40.25	175.67	135.35	1.51	203.84	2.15	0.64	0.91
40.26	175.67	135.34	1.50	203.55	2.15	0.64	0.91
40.27	175.67	135.32	1.50	203.24	2.15	0.64	0.91
40.28	175.67	135.31	1.50	202.95	2.15	0.64	0.91
40.29	175.67	135.30	1.50	202.67	2.15	0.63	0.91
40.30	175.66	135.27	1.50	202.43	2.15	0.63	0.91
40.31	175.62	135.22	1.50	202.18	2.15	0.63	0.91
40.32	175.53	135.13	1.49	201.89	2.14	0.63	0.91

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
40.33	175.40	135.01	1.49	201.53	2.14	0.63	0.91
40.34	175.25	134.88	1.49	201.13	2.14	0.62	0.91
40.35	175.09	134.74	1.49	200.71	2.14	0.62	0.91
40.36	174.93	134.60	1.49	200.29	2.14	0.61	0.91
40.37	174.78	134.46	1.49	199.89	2.14	0.61	0.91
40.38	174.64	134.34	1.49	199.52	2.14	0.60	0.91
40.39	174.50	134.22	1.48	199.19	2.14	0.60	0.91
40.40	174.34	134.06	1.48	198.85	2.14	0.60	0.91
40.41	174.11	133.87	1.48	198.45	2.14	0.59	0.91
40.42	173.83	133.63	1.48	197.97	2.14	0.59	0.91
40.43	173.53	133.37	1.48	197.45	2.14	0.58	0.91
40.44	173.21	133.11	1.48	196.91	2.14	0.58	0.91
40.45	172.89	132.84	1.48	196.37	2.14	0.57	0.91
40.46	172.59	132.59	1.48	195.87	2.14	0.56	0.91
40.47	172.33	132.37	1.48	195.43	2.14	0.56	0.91
40.48	172.09	132.16	1.48	195.06	2.14	0.56	0.91
40.49	171.83	131.93	1.48	194.72	2.14	0.55	0.91
40.50	171.52	131.65	1.48	194.38	2.14	0.55	0.91
40.51	171.15	131.34	1.48	193.99	2.14	0.54	0.91
40.52	170.76	131.01	1.48	193.58	2.14	0.54	0.91
40.53	170.36	130.67	1.48	193.15	2.14	0.53	0.91
40.54	169.97	130.33	1.48	192.74	2.14	0.53	0.91
40.55	169.61	130.02	1.48	192.35	2.14	0.52	0.91
40.56	169.29	129.74	1.48	192.01	2.14	0.52	0.91
40.57	168.90	129.41	1.48	191.65	2.14	0.51	0.91
40.58	168.39	128.97	1.48	191.21	2.14	0.51	0.90
40.59	167.73	128.42	1.48	190.67	2.14	0.50	0.90
40.60	166.98	127.79	1.49	190.07	2.14	0.49	0.90
40.61	166.18	127.13	1.49	189.43	2.14	0.48	0.90
40.62	165.39	126.47	1.49	188.79	2.14	0.47	0.90
40.63	164.62	125.83	1.50	188.18	2.15	0.47	0.90
40.64	163.94	125.26	1.50	187.63	2.15	0.46	0.90
40.65	163.33	124.75	1.50	187.14	2.15	0.45	0.90
40.66	162.68	124.21	1.50	186.63	2.15	0.45	0.90
40.67	161.93	123.58	1.51	186.02	2.15	0.44	0.90
40.68	161.02	122.83	1.51	185.31	2.15	0.43	0.90
40.69	160.02	122.01	1.51	184.53	2.15	0.42	0.90
40.70	158.98	121.15	1.52	183.72	2.16	0.41	0.90
40.71	157.95	120.31	1.52	182.92	2.16	0.41	0.89
40.72	156.99	119.52	1.52	182.18	2.16	0.40	0.89
40.73	156.15	118.82	1.53	181.52	2.16	0.39	0.89
40.74	155.38	118.18	1.53	181.01	2.16	0.39	0.89
40.75	154.58	117.51	1.54	180.58	2.17	0.38	0.89
40.76	153.64	116.72	1.54	180.19	2.17	0.38	0.89
40.77	152.55	115.81	1.55	179.74	2.17	0.37	0.89
40.78	151.37	114.83	1.56	179.28	2.18	0.36	0.89
40.79	150.17	113.83	1.57	178.81	2.18	0.35	0.89
40.80	149.00	112.86	1.58	178.36	2.19	0.35	0.89

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
40.81	147.93	111.97	1.59	177.96	2.19	0.34	0.89
40.82	147.00	111.20	1.60	177.60	2.19	0.34	0.88
40.83	146.10	110.45	1.60	177.19	2.20	0.33	0.88
40.84	145.10	109.62	1.61	176.69	2.20	0.33	0.88
40.85	143.90	108.64	1.62	176.06	2.20	0.32	0.88
40.86	142.55	107.53	1.63	175.36	2.21	0.31	0.88
40.87	141.12	106.37	1.64	174.62	2.21	0.31	0.88
40.88	139.69	105.20	1.65	173.89	2.22	0.30	0.88
40.89	138.32	104.08	1.66	173.21	2.22	0.29	0.88
40.90	137.09	103.08	1.67	172.59	2.22	0.29	0.87
40.91	136.02	102.21	1.68	171.99	2.23	0.28	0.87
40.92	134.96	101.35	1.69	171.27	2.23	0.28	0.87
40.93	133.78	100.40	1.70	170.33	2.23	0.27	0.87
40.94	132.38	99.28	1.70	169.17	2.23	0.27	0.87
40.95	130.83	98.06	1.71	167.91	2.24	0.26	0.87
40.96	129.23	96.78	1.72	166.61	2.24	0.26	0.87
40.97	127.66	95.53	1.73	165.33	2.24	0.25	0.86
40.98	126.18	94.35	1.74	164.13	2.25	0.24	0.86
40.99	124.89	93.32	1.75	163.09	2.25	0.24	0.86
41.00	123.77	92.43	1.76	162.22	2.25	0.24	0.86
41.01	122.69	91.56	1.76	161.42	2.25	0.23	0.86
41.02	121.48	90.60	1.77	160.58	2.26	0.23	0.86
41.03	120.10	89.50	1.78	159.62	2.26	0.23	0.85
41.04	118.61	88.31	1.80	158.60	2.26	0.22	0.85
41.05	117.09	87.10	1.81	157.56	2.27	0.22	0.85
41.06	115.61	85.92	1.82	156.55	2.27	0.21	0.85
41.07	114.26	84.85	1.83	155.64	2.27	0.21	0.85
41.08	113.09	83.91	1.85	154.86	2.28	0.21	0.85
41.09	111.98	83.03	1.86	154.18	2.28	0.20	0.84
41.10	110.78	82.07	1.87	153.50	2.29	0.20	0.84
41.11	109.36	80.94	1.89	152.73	2.29	0.20	0.84
41.12	107.76	79.67	1.91	151.88	2.30	0.19	0.84
41.13	106.07	78.32	1.93	150.99	2.30	0.19	0.84
41.14	104.38	76.98	1.95	150.10	2.31	0.19	0.84
41.15	102.77	75.70	1.97	149.27	2.31	0.18	0.83
41.16	101.32	74.56	1.99	148.53	2.32	0.18	0.83
41.17	100.10	73.58	2.01	147.84	2.32	0.18	0.83
41.18	98.96	72.68	2.02	147.07	2.33	0.18	0.83
41.19	97.75	71.73	2.04	146.12	2.33	0.17	0.83
41.20	96.34	70.63	2.05	144.97	2.33	0.17	0.82
41.21	94.80	69.42	2.07	143.73	2.34	0.17	0.82
41.22	93.20	68.18	2.09	142.44	2.34	0.16	0.82
41.23	91.62	66.94	2.11	141.18	2.35	0.16	0.82
41.24	90.15	65.79	2.13	140.01	2.35	0.16	0.82
41.25	88.86	64.79	2.15	138.99	2.35	0.16	0.81
41.26	87.86	64.01	2.16	138.33	2.36	0.16	0.81
41.27	87.06	63.36	2.18	137.96	2.36	0.15	0.81
41.28	86.30	62.76	2.20	137.83	2.36	0.15	0.81

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
41.29	85.45	62.08	2.22	137.68	2.37	0.15	0.81
41.30	84.52	61.34	2.24	137.53	2.37	0.15	0.81
41.31	83.58	60.59	2.27	137.37	2.38	0.15	0.81
41.32	82.67	59.86	2.29	137.22	2.38	0.15	0.81
41.33	81.84	59.20	2.32	137.09	2.39	0.15	0.80
41.34	81.13	58.63	2.34	137.01	2.39	0.15	0.80
41.35	80.52	58.14	2.36	137.11	2.40	0.15	0.80
41.36	79.92	57.65	2.38	137.41	2.40	0.14	0.80
41.37	79.25	57.11	2.41	137.87	2.41	0.14	0.80
41.38	78.50	56.49	2.45	138.40	2.41	0.14	0.80
41.39	77.70	55.85	2.49	138.94	2.42	0.14	0.80
41.40	76.91	55.21	2.53	139.49	2.43	0.14	0.80
41.41	76.15	54.59	2.56	140.01	2.43	0.14	0.80
41.42	75.47	54.05	2.60	140.47	2.44	0.14	0.80
41.43	74.90	53.58	2.63	140.88	2.45	0.14	0.80
41.44	74.37	53.15	2.66	141.31	2.45	0.14	0.79
41.45	73.80	52.69	2.69	141.81	2.46	0.14	0.79
41.46	73.15	52.16	2.73	142.41	2.46	0.14	0.79
41.47	72.44	51.59	2.77	143.07	2.47	0.14	0.79
41.48	71.70	50.99	2.82	143.74	2.48	0.14	0.79
41.49	70.97	50.40	2.86	144.39	2.48	0.14	0.79
41.50	70.29	49.86	2.91	144.99	2.49	0.13	0.79
41.51	69.70	49.38	2.95	145.51	2.50	0.13	0.79
41.52	69.17	48.95	2.99	146.15	2.50	0.13	0.79
41.53	68.64	48.52	3.03	147.02	2.51	0.13	0.79
41.54	68.04	48.02	3.09	148.23	2.52	0.13	0.79
41.55	67.34	47.46	3.15	149.59	2.52	0.13	0.79
41.56	66.60	46.85	3.22	151.04	2.53	0.13	0.78
41.57	65.84	46.23	3.30	152.49	2.54	0.13	0.78
41.58	65.10	45.64	3.37	153.87	2.55	0.13	0.78
41.59	64.43	45.10	3.44	155.10	2.56	0.13	0.78
41.60	63.85	44.63	3.50	156.13	2.57	0.13	0.78
41.61	63.29	44.18	3.55	157.01	2.58	0.13	0.78
41.62	62.68	43.69	3.61	157.87	2.58	0.13	0.78
41.63	61.96	43.12	3.68	158.82	2.59	0.13	0.78
41.64	61.15	42.47	3.76	159.86	2.60	0.13	0.63
41.65	60.29	41.80	3.85	160.92	2.61	0.13	0.62
41.66	59.44	41.13	3.94	161.95	2.62	0.12	0.62
41.67	58.62	40.49	4.02	162.89	2.63	0.12	0.62
41.68	57.90	39.92	4.10	163.71	2.64	0.12	0.62
41.69	57.29	39.44	4.17	164.40	2.65	0.12	0.62
41.70	56.73	39.00	4.23	165.09	2.65	0.12	0.62
41.71	56.15	38.54	4.30	165.87	2.66	0.12	0.62
41.72	55.48	38.01	4.39	166.77	2.67	0.12	0.62
41.73	54.74	37.44	4.48	167.71	2.68	0.12	0.62
41.74	53.98	36.85	4.58	168.65	2.69	0.12	0.62
41.75	53.24	36.27	4.68	169.54	2.70	0.12	0.62
41.76	52.54	35.72	4.77	170.33	2.71	0.12	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
41.77	51.93	35.25	4.85	170.99	2.71	0.12	0.62
41.78	51.42	34.85	4.92	171.65	2.72	0.12	0.62
41.79	50.95	34.48	5.00	172.42	2.73	0.12	0.62
41.80	50.44	34.08	5.09	173.39	2.74	0.12	0.62
41.81	49.85	33.62	5.19	174.47	2.74	0.12	0.62
41.82	49.22	33.13	5.30	175.58	2.75	0.12	0.62
41.83	48.58	32.63	5.41	176.67	2.76	0.11	0.62
41.84	47.96	32.15	5.53	177.67	2.77	0.11	0.62
41.85	47.40	31.71	5.63	178.55	2.78	0.11	0.62
41.86	46.94	31.35	5.72	179.29	2.79	0.11	0.62
41.87	46.59	31.08	5.79	180.05	2.80	0.11	0.62
41.88	46.32	30.86	5.86	180.93	2.80	0.11	0.62
41.89	46.05	30.64	5.94	182.00	2.81	0.11	0.62
41.90	45.74	30.40	6.03	183.18	2.81	0.11	0.62
41.91	45.42	30.14	6.12	184.38	2.82	0.11	0.62
41.92	45.11	29.89	6.21	185.57	2.83	0.11	0.62
41.93	44.81	29.65	6.30	186.66	2.83	0.11	0.62
41.94	44.54	29.43	6.37	187.62	2.84	0.11	0.62
41.95	44.36	29.30	6.43	188.36	2.84	0.11	0.62
41.96	44.30	29.25	6.46	188.87	2.85	0.11	0.62
41.97	44.34	29.27	6.47	189.23	2.85	0.11	0.62
41.98	44.41	29.31	6.47	189.60	2.85	0.11	0.62
41.99	44.48	29.36	6.47	190.01	2.85	0.11	0.62
42.00	44.56	29.41	6.48	190.43	2.85	0.11	0.62
42.01	44.64	29.45	6.48	190.84	2.85	0.11	0.62
42.02	44.72	29.50	6.48	191.23	2.85	0.11	0.62
42.03	44.78	29.54	6.49	191.55	2.85	0.11	0.62
42.04	44.98	29.67	6.46	191.60	2.85	0.11	0.62
42.05	45.36	29.92	6.39	191.34	2.84	0.11	0.62
42.06	45.93	30.34	6.29	190.81	2.83	0.11	0.62
42.07	46.60	30.83	6.17	190.18	2.82	0.11	0.62
42.08	47.30	31.35	6.04	189.44	2.82	0.11	0.62
42.09	48.02	31.89	5.92	188.65	2.81	0.11	0.62
42.10	48.72	32.40	5.80	187.83	2.80	0.12	0.62
42.11	49.35	32.87	5.69	187.04	2.79	0.12	0.62
42.12	49.92	33.29	5.60	186.28	2.78	0.12	0.62
42.13	50.55	33.76	5.49	185.34	2.77	0.12	0.62
42.14	51.31	34.33	5.36	184.09	2.76	0.12	0.62
42.15	52.26	35.04	5.21	182.43	2.75	0.12	0.62
42.16	53.32	35.84	5.03	180.46	2.73	0.12	0.62
42.17	54.43	36.69	4.86	178.27	2.71	0.12	0.62
42.18	55.55	37.54	4.69	175.95	2.70	0.12	0.62
42.19	56.60	38.34	4.53	173.63	2.68	0.12	0.62
42.20	57.54	39.06	4.39	171.48	2.67	0.12	0.62
42.21	58.32	39.67	4.28	169.63	2.66	0.12	0.62
42.22	59.04	40.21	4.18	167.91	2.65	0.12	0.62
42.23	59.77	40.78	4.07	166.11	2.64	0.13	0.62
42.24	60.63	41.44	3.96	163.98	2.62	0.13	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
42.25	61.56	42.16	3.83	161.59	2.61	0.13	0.63
42.26	62.52	42.91	3.71	159.04	2.59	0.13	0.78
42.27	63.46	43.65	3.58	156.47	2.58	0.13	0.78
42.28	64.33	44.34	3.47	154.02	2.57	0.13	0.78
42.29	65.09	44.93	3.38	151.86	2.55	0.13	0.78
42.30	65.65	45.37	3.31	150.28	2.55	0.13	0.78
42.31	66.09	45.71	3.26	149.13	2.54	0.13	0.78
42.32	66.47	46.01	3.22	148.19	2.53	0.13	0.78
42.33	66.92	46.35	3.17	147.11	2.53	0.13	0.78
42.34	67.39	46.72	3.12	145.95	2.52	0.13	0.78
42.35	67.87	47.10	3.07	144.75	2.51	0.13	0.78
42.36	68.33	47.46	3.03	143.59	2.51	0.13	0.79
42.37	68.75	47.78	2.98	142.53	2.50	0.13	0.79
42.38	69.04	48.00	2.95	141.71	2.50	0.13	0.79
42.39	69.05	48.02	2.94	141.26	2.49	0.13	0.79
42.40	68.80	47.81	2.95	141.14	2.50	0.13	0.79
42.41	68.36	47.47	2.97	141.18	2.50	0.13	0.78
42.42	67.87	47.09	3.00	141.22	2.50	0.13	0.78
42.43	67.36	46.69	3.03	141.26	2.51	0.13	0.78
42.44	66.85	46.29	3.05	141.30	2.51	0.13	0.78
42.45	66.36	45.91	3.08	141.33	2.51	0.13	0.78
42.46	65.93	45.57	3.10	141.36	2.52	0.13	0.78
42.47	65.49	45.23	3.13	141.60	2.52	0.13	0.78
42.48	64.95	44.80	3.17	142.19	2.53	0.13	0.78
42.49	64.24	44.23	3.24	143.19	2.54	0.13	0.78
42.50	63.39	43.56	3.32	144.42	2.55	0.13	0.78
42.51	62.46	42.82	3.40	145.73	2.56	0.13	0.78
42.52	61.49	42.07	3.50	147.05	2.57	0.12	0.77
42.53	60.55	41.34	3.59	148.30	2.58	0.12	0.77
42.54	59.68	40.65	3.68	149.43	2.59	0.12	0.77
42.55	58.92	40.06	3.75	150.39	2.60	0.12	0.62
42.56	58.24	39.53	3.83	151.23	2.61	0.12	0.62
42.57	57.54	38.98	3.90	152.10	2.62	0.12	0.62
42.58	56.73	38.35	3.99	153.09	2.63	0.12	0.62
42.59	55.80	37.64	4.10	154.18	2.64	0.12	0.62
42.60	54.81	36.88	4.21	155.29	2.65	0.12	0.62
42.61	53.80	36.11	4.33	156.36	2.66	0.12	0.62
42.62	52.84	35.37	4.45	157.33	2.67	0.12	0.62
42.63	51.96	34.70	4.56	158.17	2.69	0.12	0.62
42.64	51.22	34.13	4.65	158.75	2.69	0.12	0.62
42.65	50.56	33.64	4.73	158.95	2.70	0.11	0.62
42.66	49.90	33.14	4.79	158.80	2.71	0.11	0.62
42.67	49.15	32.58	4.86	158.45	2.71	0.11	0.62
42.68	48.32	31.96	4.94	158.05	2.72	0.11	0.62
42.69	47.44	31.31	5.03	157.60	2.73	0.11	0.62
42.70	46.56	30.67	5.12	157.13	2.74	0.11	0.62
42.71	45.74	30.06	5.21	156.67	2.75	0.11	0.62
42.72	45.01	29.51	5.29	156.23	2.75	0.11	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
42.73	44.50	29.14	5.34	155.73	2.76	0.11	0.62
42.74	44.22	28.94	5.36	155.05	2.76	0.11	0.62
42.75	44.12	28.87	5.34	154.10	2.76	0.11	0.62
42.76	44.05	28.82	5.31	152.96	2.75	0.11	0.62
42.77	43.97	28.77	5.27	151.71	2.75	0.11	0.62
42.78	43.89	28.72	5.24	150.42	2.75	0.11	0.62
42.79	43.81	28.67	5.20	149.16	2.75	0.11	0.62
42.80	43.74	28.62	5.17	147.99	2.74	0.11	0.62
42.81	43.70	28.59	5.14	146.98	2.74	0.11	0.62
42.82	43.91	28.75	5.08	146.19	2.73	0.11	0.62
42.83	44.43	29.14	4.99	145.52	2.73	0.11	0.62
42.84	45.28	29.76	4.87	144.82	2.72	0.11	0.62
42.85	46.24	30.47	4.72	143.96	2.70	0.11	0.62
42.86	47.26	31.24	4.58	142.99	2.69	0.11	0.62
42.87	48.30	32.01	4.43	141.92	2.67	0.11	0.62
42.88	49.30	32.76	4.30	140.84	2.66	0.11	0.62
42.89	50.21	33.43	4.18	139.80	2.65	0.11	0.62
42.90	50.99	34.02	4.08	138.96	2.64	0.11	0.62
42.91	51.74	34.57	4.00	138.37	2.63	0.11	0.62
42.92	52.55	35.17	3.92	137.97	2.62	0.11	0.62
42.93	53.51	35.89	3.83	137.61	2.61	0.12	0.62
42.94	54.58	36.68	3.74	137.18	2.60	0.12	0.76
42.95	55.69	37.51	3.64	136.69	2.59	0.12	0.76
42.96	56.80	38.34	3.55	136.18	2.58	0.12	0.77
42.97	57.85	39.12	3.47	135.66	2.57	0.12	0.77
42.98	58.78	39.81	3.40	135.19	2.56	0.12	0.77
42.99	59.45	40.31	3.35	134.95	2.55	0.12	0.77
43.00	59.89	40.63	3.32	135.01	2.55	0.12	0.77
43.01	60.17	40.83	3.32	135.37	2.55	0.12	0.77
43.02	60.46	41.02	3.31	135.84	2.55	0.12	0.77
43.03	60.77	41.24	3.31	136.36	2.55	0.12	0.77
43.04	61.09	41.46	3.30	136.89	2.54	0.12	0.77
43.05	61.41	41.68	3.30	137.41	2.54	0.12	0.77
43.06	61.70	41.88	3.29	137.90	2.54	0.12	0.77
43.07	61.94	42.04	3.29	138.34	2.54	0.12	0.77
43.08	62.06	42.12	3.30	138.96	2.54	0.12	0.77
43.09	62.08	42.10	3.32	139.89	2.55	0.12	0.77
43.10	62.02	42.02	3.36	141.17	2.55	0.12	0.77
43.11	61.94	41.94	3.40	142.62	2.56	0.12	0.77
43.12	61.87	41.84	3.45	144.15	2.56	0.12	0.77
43.13	61.79	41.75	3.49	145.70	2.57	0.12	0.77
43.14	61.71	41.66	3.53	147.18	2.57	0.12	0.77
43.15	61.64	41.58	3.57	148.51	2.58	0.12	0.77
43.16	61.58	41.51	3.61	149.65	2.58	0.12	0.77
43.17	61.53	41.44	3.64	150.72	2.59	0.12	0.77
43.18	61.47	41.37	3.67	151.88	2.59	0.13	0.77
43.19	61.40	41.29	3.71	153.24	2.60	0.13	0.77
43.20	61.32	41.20	3.76	154.74	2.60	0.13	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
43.21	61.24	41.11	3.80	156.30	2.61	0.13	0.62
43.22	61.17	41.02	3.85	157.84	2.61	0.13	0.62
43.23	61.09	40.93	3.89	159.28	2.62	0.13	0.62
43.24	61.03	40.85	3.93	160.55	2.62	0.13	0.62
43.25	60.99	40.80	3.96	161.42	2.62	0.13	0.62
43.26	60.99	40.79	3.97	161.91	2.62	0.13	0.62
43.27	61.03	40.80	3.97	162.12	2.62	0.13	0.62
43.28	61.08	40.83	3.98	162.30	2.63	0.13	0.62
43.29	61.13	40.85	3.98	162.49	2.63	0.13	0.62
43.30	61.18	40.88	3.98	162.69	2.63	0.13	0.62
43.31	61.23	40.91	3.98	162.89	2.63	0.13	0.62
43.32	61.28	40.93	3.98	163.07	2.63	0.13	0.62
43.33	61.33	40.96	3.98	163.19	2.63	0.13	0.62
43.34	61.46	41.05	3.97	162.99	2.62	0.13	0.62
43.35	61.70	41.22	3.94	162.43	2.62	0.13	0.63
43.36	62.04	41.48	3.89	161.49	2.62	0.13	0.63
43.37	62.44	41.77	3.84	160.42	2.61	0.13	0.63
43.38	62.85	42.09	3.78	159.27	2.60	0.13	0.63
43.39	63.28	42.41	3.73	158.09	2.60	0.13	0.78
43.40	63.68	42.72	3.67	156.94	2.59	0.13	0.78
43.41	64.05	43.00	3.63	155.89	2.59	0.13	0.78
43.42	64.40	43.27	3.58	154.97	2.58	0.13	0.78
43.43	64.86	43.61	3.53	154.07	2.57	0.13	0.78
43.44	65.46	44.06	3.47	153.06	2.57	0.13	0.78
43.45	66.23	44.64	3.40	151.84	2.56	0.13	0.78
43.46	67.07	45.28	3.32	150.47	2.55	0.13	0.78
43.47	67.96	45.95	3.24	149.00	2.54	0.13	0.78
43.48	68.83	46.62	3.16	147.52	2.53	0.13	0.79
43.49	69.66	47.26	3.09	146.10	2.52	0.13	0.79
43.50	70.39	47.81	3.03	144.83	2.51	0.13	0.79
43.51	70.99	48.27	2.98	143.78	2.50	0.13	0.79
43.52	71.52	48.67	2.93	142.85	2.49	0.13	0.79
43.53	72.06	49.09	2.89	141.91	2.49	0.14	0.79
43.54	72.67	49.56	2.84	140.83	2.48	0.14	0.79
43.55	73.34	50.07	2.79	139.65	2.47	0.14	0.79
43.56	74.03	50.60	2.74	138.43	2.46	0.14	0.79
43.57	74.70	51.12	2.68	137.22	2.45	0.14	0.79
43.58	75.31	51.60	2.64	136.11	2.45	0.14	0.79
43.59	75.83	51.99	2.60	135.17	2.44	0.14	0.79
43.60	76.13	52.22	2.58	134.56	2.44	0.14	0.79
43.61	76.25	52.31	2.57	134.22	2.43	0.14	0.79
43.62	76.24	52.30	2.56	134.04	2.43	0.14	0.79
43.63	76.24	52.30	2.56	133.83	2.43	0.14	0.79
43.64	76.24	52.29	2.56	133.61	2.43	0.14	0.79
43.65	76.24	52.28	2.55	133.39	2.43	0.14	0.79
43.66	76.24	52.27	2.55	133.18	2.43	0.14	0.79
43.67	76.24	52.27	2.54	132.99	2.43	0.14	0.79
43.68	76.16	52.20	2.55	132.99	2.43	0.14	0.79

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
43.69	75.90	51.98	2.57	133.40	2.43	0.14	0.79
43.70	75.41	51.59	2.60	134.27	2.44	0.14	0.79
43.71	74.76	51.06	2.65	135.47	2.45	0.14	0.79
43.72	74.04	50.48	2.71	136.79	2.46	0.14	0.79
43.73	73.29	49.88	2.77	138.16	2.47	0.14	0.79
43.74	72.55	49.28	2.83	139.50	2.48	0.14	0.79
43.75	71.85	48.73	2.89	140.75	2.49	0.13	0.79
43.76	71.23	48.23	2.94	141.84	2.49	0.13	0.79
43.77	70.59	47.72	3.00	143.01	2.50	0.13	0.79
43.78	69.81	47.10	3.07	144.49	2.51	0.13	0.79
43.79	68.79	46.29	3.16	146.44	2.53	0.13	0.79
43.80	67.58	45.35	3.28	148.70	2.54	0.13	0.78
43.81	66.27	44.33	3.41	151.08	2.56	0.13	0.78
43.82	64.93	43.30	3.54	153.44	2.58	0.13	0.78
43.83	63.63	42.29	3.68	155.65	2.59	0.13	0.78
43.84	62.43	41.37	3.81	157.60	2.61	0.13	0.63
43.85	61.40	40.58	3.92	159.24	2.62	0.13	0.62
43.86	60.52	39.90	4.03	160.74	2.63	0.12	0.62
43.87	59.66	39.24	4.14	162.33	2.64	0.12	0.62
43.88	58.71	38.51	4.26	164.16	2.66	0.12	0.62
43.89	57.63	37.69	4.41	166.16	2.67	0.12	0.62
43.90	56.48	36.82	4.57	168.17	2.69	0.12	0.62
43.91	55.33	35.95	4.73	170.09	2.70	0.12	0.62
43.92	54.22	35.12	4.89	171.83	2.72	0.12	0.62
43.93	53.23	34.37	5.04	173.30	2.73	0.12	0.62
43.94	52.45	33.79	5.17	174.52	2.74	0.12	0.62
43.95	51.89	33.36	5.27	175.69	2.75	0.12	0.62
43.96	51.47	33.04	5.36	176.99	2.76	0.12	0.62
43.97	51.05	32.71	5.46	178.52	2.77	0.12	0.62
43.98	50.59	32.35	5.57	180.17	2.78	0.12	0.62
43.99	50.11	31.98	5.69	181.83	2.79	0.12	0.62
44.00	49.64	31.62	5.80	183.44	2.80	0.12	0.62
44.01	49.19	31.27	5.91	184.90	2.80	0.11	0.62
44.02	48.80	30.97	6.01	186.14	2.81	0.11	0.62
44.03	48.58	30.79	6.08	187.20	2.82	0.11	0.62
44.04	48.53	30.74	6.12	188.21	2.82	0.11	0.62
44.05	48.64	30.80	6.15	189.32	2.82	0.11	0.62
44.06	48.79	30.88	6.17	190.62	2.83	0.11	0.62
44.07	48.94	30.97	6.20	192.01	2.83	0.11	0.62
44.08	49.11	31.06	6.23	193.44	2.83	0.12	0.62
44.09	49.26	31.15	6.25	194.83	2.83	0.12	0.62
44.10	49.41	31.23	6.28	196.12	2.83	0.12	0.62
44.11	49.55	31.32	6.30	197.19	2.83	0.12	0.62
44.12	49.79	31.47	6.29	197.93	2.83	0.12	0.62
44.13	50.17	31.72	6.25	198.43	2.83	0.12	0.62
44.14	50.70	32.09	6.20	198.85	2.83	0.12	0.62
44.15	51.30	32.50	6.13	199.31	2.82	0.12	0.62
44.16	51.93	32.94	6.07	199.79	2.82	0.12	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
44.17	52.57	33.38	6.00	200.25	2.81	0.12	0.62
44.18	53.18	33.80	5.94	200.68	2.81	0.12	0.62
44.19	53.73	34.18	5.88	201.07	2.80	0.12	0.62
44.20	54.29	34.58	5.82	201.31	2.80	0.12	0.62
44.21	55.04	35.10	5.74	201.35	2.79	0.12	0.62
44.22	56.06	35.82	5.62	201.16	2.78	0.12	0.62
44.23	57.35	36.74	5.47	200.80	2.77	0.12	0.62
44.24	58.77	37.75	5.31	200.30	2.75	0.13	0.62
44.25	60.24	38.81	5.14	199.66	2.74	0.13	0.62
44.26	61.70	39.85	4.99	198.92	2.73	0.13	0.62
44.27	63.07	40.84	4.85	198.13	2.71	0.13	0.63
44.28	64.27	41.70	4.73	197.36	2.70	0.13	0.63
44.29	65.42	42.53	4.62	196.57	2.69	0.13	0.63
44.30	66.69	43.45	4.50	195.63	2.68	0.14	0.64
44.31	68.24	44.58	4.36	194.41	2.67	0.14	0.64
44.32	70.05	45.90	4.20	192.86	2.65	0.14	0.65
44.33	72.01	47.33	4.04	191.04	2.63	0.14	0.65
44.34	74.00	48.80	3.87	189.02	2.61	0.14	0.66
44.35	75.94	50.23	3.72	186.92	2.60	0.15	0.80
44.36	77.73	51.55	3.59	184.87	2.58	0.15	0.80
44.37	79.25	52.69	3.47	183.06	2.57	0.15	0.80
44.38	80.58	53.67	3.38	181.54	2.55	0.15	0.81
44.39	81.91	54.66	3.30	180.14	2.54	0.15	0.81
44.40	83.41	55.77	3.20	178.61	2.53	0.16	0.81
44.41	85.09	57.03	3.10	176.84	2.52	0.16	0.81
44.42	86.88	58.37	3.00	174.89	2.50	0.16	0.81
44.43	88.68	59.73	2.89	172.88	2.49	0.16	0.82
44.44	90.39	61.02	2.80	170.90	2.47	0.17	0.82
44.45	91.93	62.19	2.72	169.09	2.46	0.17	0.82
44.46	93.21	63.16	2.65	167.59	2.45	0.17	0.82
44.47	94.32	64.00	2.60	166.31	2.44	0.17	0.82
44.48	95.42	64.83	2.55	165.10	2.43	0.17	0.82
44.49	96.66	65.77	2.49	163.74	2.42	0.17	0.83
44.50	98.03	66.82	2.43	162.22	2.41	0.18	0.83
44.51	99.45	67.91	2.37	160.64	2.40	0.18	0.83
44.52	100.86	68.99	2.31	159.07	2.39	0.18	0.83
44.53	102.17	70.01	2.25	157.60	2.38	0.18	0.83
44.54	103.33	70.90	2.20	156.30	2.37	0.18	0.83
44.55	104.13	71.52	2.17	155.32	2.36	0.19	0.83
44.56	104.65	71.92	2.15	154.54	2.35	0.19	0.83
44.57	104.97	72.17	2.13	153.85	2.35	0.19	0.83
44.58	105.32	72.44	2.11	153.07	2.35	0.19	0.83
44.59	105.69	72.74	2.09	152.23	2.34	0.19	0.83
44.60	106.08	73.04	2.07	151.38	2.34	0.19	0.83
44.61	106.45	73.33	2.05	150.55	2.33	0.19	0.84
44.62	106.79	73.61	2.04	149.79	2.33	0.19	0.84
44.63	107.10	73.85	2.02	149.15	2.32	0.19	0.84
44.64	107.47	74.13	2.01	148.66	2.32	0.19	0.84

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
44.65	107.94	74.49	1.99	148.23	2.32	0.19	0.84
44.66	108.56	74.96	1.97	147.81	2.31	0.19	0.84
44.67	109.26	75.49	1.95	147.33	2.31	0.19	0.84
44.68	109.99	76.05	1.93	146.83	2.30	0.19	0.84
44.69	110.73	76.62	1.91	146.34	2.30	0.19	0.84
44.70	111.43	77.16	1.89	145.87	2.29	0.19	0.84
44.71	112.06	77.64	1.87	145.46	2.29	0.19	0.84
44.72	112.60	78.05	1.86	145.10	2.28	0.20	0.84
44.73	113.11	78.44	1.85	144.77	2.28	0.20	0.84
44.74	113.66	78.87	1.83	144.41	2.27	0.20	0.84
44.75	114.31	79.36	1.81	143.99	2.27	0.20	0.84
44.76	115.02	79.91	1.80	143.55	2.26	0.20	0.84
44.77	115.75	80.48	1.78	143.09	2.26	0.20	0.84
44.78	116.48	81.05	1.76	142.65	2.25	0.20	0.84
44.79	117.15	81.58	1.74	142.25	2.25	0.20	0.84
44.80	117.75	82.04	1.73	141.90	2.24	0.20	0.85
44.81	118.04	82.26	1.72	141.67	2.24	0.20	0.85
44.82	118.02	82.23	1.72	141.54	2.24	0.20	0.85
44.83	117.72	81.99	1.73	141.48	2.24	0.20	0.84
44.84	117.36	81.69	1.73	141.42	2.24	0.20	0.84
44.85	116.96	81.37	1.74	141.36	2.24	0.20	0.84
44.86	116.56	81.05	1.74	141.30	2.25	0.20	0.84
44.87	116.18	80.74	1.75	141.24	2.25	0.20	0.84
44.88	115.82	80.45	1.76	141.19	2.25	0.20	0.84
44.89	115.52	80.20	1.76	141.16	2.25	0.20	0.84
44.90	115.24	79.97	1.77	141.17	2.25	0.20	0.84
44.91	114.95	79.73	1.77	141.24	2.26	0.20	0.84
44.92	114.61	79.45	1.78	141.35	2.26	0.20	0.84
44.93	114.24	79.14	1.79	141.48	2.26	0.20	0.84
44.94	113.84	78.81	1.80	141.62	2.26	0.19	0.84
44.95	113.44	78.48	1.81	141.77	2.27	0.19	0.84
44.96	113.06	78.17	1.82	141.91	2.27	0.19	0.84
44.97	112.72	77.89	1.82	142.03	2.27	0.19	0.84
44.98	112.44	77.65	1.83	142.18	2.27	0.19	0.84
44.99	112.20	77.44	1.84	142.41	2.28	0.19	0.84
45.00	111.95	77.22	1.85	142.76	2.28	0.19	0.84
45.01	111.67	76.97	1.86	143.19	2.28	0.19	0.84
45.02	111.36	76.70	1.87	143.67	2.29	0.19	0.84
45.03	111.04	76.42	1.89	144.18	2.29	0.19	0.84
45.04	110.73	76.15	1.90	144.68	2.29	0.19	0.84
45.05	110.43	75.89	1.91	145.14	2.30	0.19	0.84
45.06	110.17	75.66	1.92	145.55	2.30	0.19	0.84
45.07	109.95	75.46	1.93	145.93	2.30	0.19	0.84
45.08	109.72	75.26	1.94	146.34	2.31	0.19	0.84
45.09	109.47	75.03	1.96	146.82	2.31	0.19	0.84
45.10	109.18	74.77	1.97	147.39	2.31	0.19	0.84
45.11	108.87	74.50	1.99	148.00	2.32	0.19	0.84
45.12	108.55	74.22	2.00	148.62	2.32	0.19	0.84

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
45.13	108.24	73.95	2.02	149.23	2.32	0.19	0.84
45.14	107.95	73.70	2.03	149.78	2.33	0.19	0.84
45.15	107.70	73.48	2.05	150.27	2.33	0.19	0.84
45.16	107.43	73.24	2.06	150.74	2.33	0.19	0.84
45.17	107.11	72.97	2.07	151.26	2.34	0.19	0.84
45.18	106.71	72.63	2.09	151.88	2.34	0.19	0.84
45.19	106.25	72.25	2.11	152.59	2.35	0.19	0.83
45.20	105.78	71.85	2.13	153.34	2.35	0.19	0.83
45.21	105.30	71.46	2.16	154.09	2.36	0.19	0.83
45.22	104.84	71.08	2.18	154.81	2.36	0.19	0.83
45.23	104.44	70.74	2.20	155.45	2.36	0.18	0.83
45.24	104.09	70.45	2.21	156.01	2.37	0.18	0.83
45.25	103.76	70.17	2.23	156.58	2.37	0.18	0.83
45.26	103.40	69.87	2.25	157.22	2.38	0.18	0.83
45.27	102.97	69.51	2.27	157.98	2.38	0.18	0.83
45.28	102.51	69.13	2.30	158.81	2.39	0.18	0.83
45.29	102.03	68.74	2.32	159.67	2.39	0.18	0.83
45.30	101.56	68.35	2.35	160.52	2.40	0.18	0.83
45.31	101.12	67.98	2.37	161.31	2.40	0.18	0.83
45.32	100.73	67.67	2.39	162.00	2.40	0.18	0.83
45.33	100.43	67.41	2.41	162.49	2.41	0.18	0.83
45.34	100.17	67.20	2.42	162.83	2.41	0.18	0.83
45.35	99.91	66.99	2.43	163.09	2.41	0.18	0.83
45.36	99.62	66.75	2.45	163.39	2.41	0.18	0.83
45.37	99.31	66.50	2.46	163.71	2.42	0.18	0.83
45.38	98.99	66.24	2.48	164.03	2.42	0.18	0.83
45.39	98.68	65.99	2.49	164.34	2.42	0.18	0.83
45.40	98.39	65.76	2.50	164.63	2.42	0.18	0.83
45.41	98.18	65.58	2.51	164.80	2.43	0.18	0.83
45.42	98.10	65.51	2.51	164.70	2.43	0.18	0.83
45.43	98.15	65.55	2.51	164.31	2.42	0.18	0.83
45.44	98.29	65.65	2.49	163.68	2.42	0.18	0.83
45.45	98.44	65.77	2.48	162.98	2.42	0.18	0.83
45.46	98.60	65.89	2.46	162.24	2.42	0.18	0.83
45.47	98.76	66.01	2.45	161.50	2.41	0.18	0.83
45.48	98.91	66.13	2.43	160.79	2.41	0.18	0.83
45.49	99.04	66.23	2.42	160.16	2.41	0.18	0.83
45.50	99.23	66.38	2.40	159.54	2.41	0.18	0.83
45.51	99.56	66.63	2.38	158.82	2.40	0.18	0.83
45.52	100.07	67.01	2.36	157.89	2.40	0.18	0.83
45.53	100.71	67.50	2.32	156.77	2.39	0.18	0.83
45.54	101.40	68.04	2.29	155.55	2.38	0.18	0.83
45.55	102.12	68.60	2.25	154.28	2.38	0.18	0.83
45.56	102.83	69.14	2.21	153.04	2.37	0.18	0.83
45.57	103.49	69.66	2.18	151.88	2.36	0.18	0.83
45.58	104.06	70.10	2.15	150.87	2.35	0.18	0.83
45.59	104.60	70.52	2.13	150.02	2.35	0.18	0.83
45.60	105.19	70.97	2.10	149.23	2.34	0.18	0.83

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
45.61	105.89	71.51	2.07	148.37	2.34	0.18	0.83
45.62	106.70	72.13	2.04	147.40	2.33	0.18	0.83
45.63	107.56	72.80	2.01	146.36	2.32	0.19	0.83
45.64	108.44	73.49	1.98	145.31	2.31	0.19	0.84
45.65	109.29	74.15	1.95	144.31	2.31	0.19	0.84
45.66	110.07	74.75	1.92	143.41	2.30	0.19	0.84
45.67	110.72	75.26	1.90	142.67	2.29	0.19	0.84
45.68	111.25	75.67	1.88	142.11	2.29	0.19	0.84
45.69	111.75	76.05	1.86	141.66	2.28	0.19	0.84
45.70	112.29	76.47	1.85	141.20	2.28	0.19	0.84
45.71	112.90	76.93	1.83	140.70	2.27	0.19	0.84
45.72	113.53	77.42	1.81	140.17	2.27	0.19	0.84
45.73	114.17	77.92	1.79	139.66	2.26	0.19	0.84
45.74	114.77	78.38	1.78	139.18	2.26	0.19	0.84
45.75	115.31	78.80	1.76	138.75	2.25	0.19	0.84
45.76	115.73	79.12	1.75	138.43	2.25	0.20	0.84
45.77	116.04	79.36	1.74	138.20	2.25	0.20	0.84
45.78	116.31	79.55	1.74	138.03	2.24	0.20	0.84
45.79	116.59	79.76	1.73	137.85	2.24	0.20	0.84
45.80	116.90	79.99	1.72	137.65	2.24	0.20	0.84
45.81	117.22	80.23	1.71	137.46	2.24	0.20	0.84
45.82	117.53	80.47	1.71	137.26	2.23	0.20	0.84
45.83	117.83	80.69	1.70	137.08	2.23	0.20	0.84
45.84	118.08	80.88	1.69	136.93	2.23	0.20	0.84
45.85	118.36	81.09	1.69	136.78	2.23	0.20	0.84
45.86	118.70	81.34	1.68	136.62	2.22	0.20	0.84
45.87	119.15	81.68	1.67	136.44	2.22	0.20	0.84
45.88	119.67	82.08	1.66	136.23	2.22	0.20	0.84
45.89	120.22	82.52	1.65	136.03	2.21	0.20	0.84
45.90	120.78	82.95	1.64	135.82	2.21	0.20	0.85
45.91	121.32	83.36	1.63	135.62	2.21	0.20	0.85
45.92	121.81	83.74	1.62	135.45	2.20	0.20	0.85
45.93	122.26	84.08	1.61	135.31	2.20	0.20	0.85
45.94	122.74	84.45	1.60	135.21	2.19	0.20	0.85
45.95	123.34	84.90	1.59	135.14	2.19	0.20	0.85
45.96	124.09	85.48	1.58	135.08	2.19	0.21	0.85
45.97	124.92	86.12	1.57	135.03	2.18	0.21	0.85
45.98	125.80	86.79	1.56	134.99	2.17	0.21	0.85
45.99	126.67	87.47	1.54	134.96	2.17	0.21	0.85
46.00	127.50	88.11	1.53	134.95	2.16	0.21	0.85
46.01	128.24	88.68	1.52	134.94	2.16	0.21	0.85
46.02	128.87	89.16	1.51	134.93	2.15	0.21	0.85
46.03	129.48	89.64	1.50	134.90	2.15	0.21	0.85
46.04	130.15	90.16	1.50	134.86	2.15	0.21	0.85
46.05	130.93	90.77	1.49	134.82	2.14	0.21	0.85
46.06	131.79	91.45	1.47	134.80	2.13	0.22	0.85
46.07	132.67	92.14	1.46	134.79	2.13	0.22	0.85
46.08	133.53	92.83	1.45	134.79	2.12	0.22	0.85

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
46.09	134.33	93.46	1.44	134.81	2.12	0.22	0.85
46.10	135.03	94.01	1.43	134.85	2.11	0.22	0.85
46.11	135.61	94.43	1.43	135.19	2.11	0.22	0.85
46.12	136.15	94.78	1.43	135.90	2.11	0.22	0.85
46.13	136.73	95.12	1.44	137.04	2.11	0.23	0.86
46.14	137.40	95.50	1.45	138.35	2.12	0.23	0.86
46.15	138.11	95.92	1.46	139.76	2.12	0.23	0.86
46.16	138.83	96.34	1.47	141.22	2.13	0.24	0.86
46.17	139.52	96.75	1.47	142.63	2.13	0.24	0.86
46.18	140.15	97.11	1.48	143.92	2.14	0.25	0.86
46.19	140.68	97.42	1.49	145.03	2.14	0.25	0.86
46.20	141.13	97.66	1.50	146.07	2.15	0.25	0.87
46.21	141.56	97.89	1.50	147.18	2.15	0.26	0.87
46.22	142.04	98.14	1.51	148.49	2.15	0.26	0.87
46.23	142.57	98.42	1.52	149.96	2.16	0.26	0.87
46.24	143.13	98.71	1.54	151.53	2.17	0.27	0.87
46.25	143.69	99.01	1.55	153.10	2.17	0.27	0.87
46.26	144.21	99.29	1.56	154.61	2.18	0.28	0.87
46.27	144.68	99.53	1.57	155.96	2.18	0.28	0.87
46.28	144.99	99.70	1.57	156.70	2.18	0.29	0.87
46.29	145.11	99.78	1.57	156.70	2.18	0.29	0.87
46.30	145.08	99.79	1.56	155.97	2.18	0.28	0.87
46.31	145.01	99.79	1.55	154.98	2.17	0.28	0.87
46.32	144.93	99.79	1.54	153.91	2.17	0.28	0.87
46.33	144.85	99.79	1.53	152.82	2.16	0.28	0.87
46.34	144.77	99.80	1.52	151.77	2.16	0.27	0.87
46.35	144.70	99.80	1.51	150.80	2.15	0.27	0.87
46.36	144.63	99.80	1.50	149.98	2.15	0.27	0.87
46.37	144.40	99.65	1.50	149.41	2.15	0.27	0.87
46.38	143.98	99.33	1.50	149.01	2.15	0.27	0.87
46.39	143.33	98.82	1.50	148.71	2.15	0.26	0.87
46.40	142.59	98.24	1.51	148.37	2.15	0.26	0.87
46.41	141.80	97.63	1.52	148.02	2.16	0.26	0.87
46.42	141.00	97.00	1.52	147.67	2.16	0.26	0.87
46.43	140.23	96.40	1.53	147.33	2.16	0.25	0.87
46.44	139.53	95.86	1.53	147.02	2.16	0.25	0.86
46.45	138.90	95.36	1.54	146.79	2.17	0.25	0.86
46.46	138.19	94.79	1.55	146.69	2.17	0.25	0.86
46.47	137.31	94.08	1.56	146.70	2.18	0.25	0.86
46.48	136.22	93.20	1.57	146.79	2.18	0.24	0.86
46.49	135.00	92.23	1.59	146.91	2.19	0.24	0.86
46.50	133.72	91.21	1.61	147.07	2.20	0.24	0.86
46.51	132.45	90.20	1.63	147.25	2.21	0.24	0.86
46.52	131.25	89.25	1.65	147.44	2.21	0.23	0.86
46.53	130.19	88.40	1.67	147.62	2.22	0.23	0.86
46.54	129.18	87.59	1.69	147.72	2.23	0.23	0.86
46.55	128.04	86.70	1.70	147.75	2.23	0.23	0.86
46.56	126.62	85.61	1.73	147.70	2.24	0.22	0.85

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
46.57	124.94	84.33	1.75	147.65	2.25	0.22	0.85
46.58	123.12	82.94	1.78	147.62	2.26	0.22	0.85
46.59	121.23	81.50	1.81	147.62	2.27	0.21	0.85
46.60	119.39	80.11	1.84	147.64	2.28	0.21	0.85
46.61	117.69	78.82	1.87	147.67	2.29	0.20	0.85
46.62	116.21	77.70	1.90	147.73	2.29	0.20	0.84
46.63	114.90	76.70	1.93	148.04	2.30	0.20	0.84
46.64	113.58	75.67	1.96	148.66	2.31	0.20	0.84
46.65	112.06	74.50	2.01	149.65	2.32	0.20	0.84
46.66	110.34	73.17	2.06	150.79	2.33	0.19	0.84
46.67	108.49	71.75	2.12	152.02	2.35	0.19	0.84
46.68	106.63	70.33	2.18	153.29	2.36	0.19	0.83
46.69	104.84	68.97	2.24	154.51	2.37	0.18	0.83
46.70	103.22	67.74	2.30	155.62	2.39	0.18	0.83
46.71	101.83	66.69	2.35	156.64	2.40	0.18	0.83
46.72	100.57	65.73	2.40	157.79	2.41	0.18	0.83
46.73	99.26	64.72	2.46	159.23	2.42	0.18	0.83
46.74	97.74	63.56	2.53	161.00	2.43	0.17	0.82
46.75	96.05	62.28	2.62	162.96	2.44	0.17	0.82
46.76	94.28	60.94	2.71	164.98	2.46	0.17	0.82
46.77	92.52	59.62	2.80	166.95	2.47	0.17	0.82
46.78	90.85	58.38	2.89	168.76	2.49	0.16	0.82
46.79	89.38	57.28	2.97	170.34	2.50	0.16	0.81
46.80	88.14	56.36	3.05	171.68	2.51	0.16	0.81
46.81	87.00	55.51	3.12	172.98	2.52	0.16	0.81
46.82	85.79	54.61	3.19	174.40	2.53	0.16	0.81
46.83	84.39	53.58	3.29	176.01	2.54	0.16	0.81
46.84	82.87	52.46	3.39	177.71	2.56	0.15	0.81
46.85	81.31	51.32	3.50	179.40	2.57	0.15	0.80
46.86	79.78	50.21	3.60	180.98	2.58	0.15	0.80
46.87	78.37	49.18	3.71	182.38	2.59	0.15	0.80
46.88	77.15	48.30	3.80	183.51	2.61	0.15	0.66
46.89	76.07	47.53	3.88	184.22	2.61	0.14	0.66
46.90	75.01	46.77	3.95	184.58	2.62	0.14	0.65
46.91	73.80	45.92	4.02	184.71	2.63	0.14	0.65
46.92	72.43	44.95	4.11	184.82	2.64	0.14	0.65
46.93	70.97	43.93	4.21	184.90	2.65	0.14	0.64
46.94	69.49	42.90	4.31	184.93	2.66	0.14	0.64
46.95	68.07	41.91	4.41	184.91	2.67	0.13	0.64
46.96	66.78	41.01	4.51	184.85	2.68	0.13	0.63
46.97	65.71	40.27	4.59	184.69	2.69	0.13	0.63
46.98	64.81	39.64	4.65	184.31	2.69	0.13	0.63
46.99	63.93	39.04	4.70	183.67	2.70	0.13	0.63
47.00	62.96	38.38	4.76	182.81	2.71	0.13	0.62
47.01	61.88	37.64	4.83	181.84	2.71	0.13	0.62
47.02	60.75	36.87	4.90	180.82	2.72	0.13	0.62
47.03	59.62	36.11	4.98	179.78	2.73	0.12	0.62
47.04	58.56	35.40	5.05	178.79	2.73	0.12	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
47.05	57.63	34.76	5.12	177.90	2.74	0.12	0.62
47.06	56.97	34.31	5.17	177.30	2.74	0.12	0.62
47.07	56.57	34.04	5.20	177.00	2.75	0.12	0.62
47.08	56.36	33.89	5.22	176.95	2.75	0.12	0.62
47.09	56.16	33.74	5.24	176.94	2.75	0.12	0.62
47.10	55.94	33.59	5.27	176.93	2.75	0.12	0.62
47.11	55.72	33.43	5.29	176.92	2.75	0.12	0.62
47.12	55.50	33.27	5.32	176.91	2.76	0.12	0.62
47.13	55.30	33.12	5.34	176.90	2.76	0.12	0.62
47.14	55.14	33.01	5.36	176.90	2.76	0.12	0.62
47.15	55.12	32.99	5.37	177.04	2.76	0.12	0.62
47.16	55.25	33.06	5.36	177.36	2.76	0.12	0.62
47.17	55.51	33.22	5.35	177.86	2.76	0.12	0.62
47.18	55.81	33.41	5.34	178.43	2.76	0.12	0.62
47.19	56.13	33.61	5.33	179.03	2.76	0.12	0.62
47.20	56.45	33.81	5.31	179.65	2.76	0.12	0.62
47.21	56.75	34.00	5.30	180.23	2.75	0.12	0.62
47.22	57.03	34.17	5.29	180.76	2.75	0.12	0.62
47.23	57.29	34.34	5.28	181.13	2.75	0.12	0.62
47.24	57.59	34.53	5.25	181.27	2.75	0.12	0.62
47.25	57.97	34.78	5.21	181.18	2.75	0.12	0.62
47.26	58.44	35.10	5.16	180.98	2.74	0.12	0.62
47.27	58.97	35.45	5.10	180.74	2.74	0.12	0.62
47.28	59.51	35.82	5.04	180.47	2.73	0.12	0.62
47.29	60.06	36.19	4.98	180.19	2.73	0.12	0.62
47.30	60.57	36.53	4.93	179.92	2.72	0.13	0.62
47.31	61.02	36.83	4.88	179.67	2.72	0.13	0.62
47.32	61.41	37.10	4.83	179.32	2.71	0.13	0.62
47.33	61.78	37.35	4.79	178.78	2.71	0.13	0.62
47.34	62.20	37.64	4.73	177.98	2.70	0.13	0.62
47.35	62.68	37.97	4.66	177.02	2.70	0.13	0.62
47.36	63.20	38.34	4.59	175.95	2.69	0.13	0.62
47.37	63.73	38.71	4.52	174.84	2.68	0.13	0.62
47.38	64.25	39.08	4.45	173.73	2.67	0.13	0.63
47.39	64.73	39.42	4.38	172.68	2.67	0.13	0.63
47.40	65.15	39.71	4.33	171.75	2.66	0.13	0.63
47.41	65.53	39.98	4.27	170.86	2.66	0.13	0.63
47.42	65.93	40.26	4.22	169.87	2.65	0.13	0.63
47.43	66.40	40.60	4.15	168.66	2.64	0.13	0.63
47.44	66.93	40.98	4.08	167.28	2.64	0.13	0.63
47.45	67.50	41.38	4.01	165.78	2.63	0.13	0.63
47.46	68.07	41.80	3.93	164.25	2.62	0.13	0.64
47.47	68.61	42.19	3.86	162.75	2.61	0.13	0.64
47.48	69.10	42.55	3.79	161.37	2.60	0.13	0.64
47.49	69.48	42.82	3.74	160.19	2.60	0.13	0.78
47.50	69.71	43.00	3.70	159.07	2.59	0.13	0.78
47.51	69.84	43.10	3.66	157.88	2.59	0.13	0.78
47.52	69.93	43.18	3.62	156.48	2.58	0.13	0.78

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
47.53	70.03	43.27	3.58	154.93	2.58	0.13	0.78
47.54	70.14	43.37	3.53	153.31	2.57	0.13	0.78
47.55	70.24	43.47	3.49	151.69	2.57	0.13	0.78
47.56	70.34	43.56	3.45	150.16	2.56	0.13	0.78
47.57	70.43	43.64	3.41	148.81	2.56	0.13	0.78
47.58	70.45	43.68	3.38	147.68	2.55	0.13	0.78
47.59	70.41	43.66	3.36	146.66	2.55	0.13	0.78
47.60	70.29	43.59	3.34	145.61	2.55	0.13	0.78
47.61	70.15	43.51	3.32	144.39	2.55	0.13	0.78
47.62	69.99	43.42	3.29	143.08	2.54	0.13	0.78
47.63	69.83	43.33	3.27	141.73	2.54	0.13	0.78
47.64	69.67	43.25	3.25	140.42	2.54	0.13	0.78
47.65	69.53	43.16	3.23	139.21	2.53	0.13	0.78
47.66	69.44	43.11	3.21	138.19	2.53	0.13	0.78
47.67	69.56	43.21	3.18	137.47	2.53	0.13	0.78
47.68	69.92	43.46	3.15	136.96	2.52	0.13	0.78
47.69	70.52	43.88	3.11	136.54	2.52	0.13	0.78
47.70	71.19	44.35	3.07	136.05	2.51	0.13	0.78
47.71	71.90	44.85	3.02	135.53	2.51	0.13	0.79
47.72	72.62	45.36	2.98	134.99	2.50	0.13	0.79
47.73	73.31	45.84	2.93	134.48	2.49	0.13	0.79
47.74	73.93	46.28	2.90	134.00	2.49	0.13	0.79
47.75	74.39	46.61	2.87	133.57	2.48	0.13	0.79
47.76	74.68	46.81	2.84	133.10	2.48	0.13	0.79
47.77	74.82	46.92	2.82	132.52	2.48	0.13	0.79
47.78	74.93	47.00	2.80	131.83	2.47	0.13	0.79
47.79	75.04	47.09	2.78	131.06	2.47	0.13	0.79
47.80	75.16	47.19	2.76	130.25	2.47	0.13	0.79
47.81	75.28	47.28	2.74	129.46	2.46	0.13	0.79
47.82	75.39	47.37	2.72	128.71	2.46	0.13	0.79
47.83	75.49	47.45	2.70	128.05	2.46	0.13	0.79
47.84	75.42	47.41	2.69	127.54	2.46	0.13	0.79
47.85	75.14	47.22	2.69	127.13	2.46	0.13	0.79
47.86	74.62	46.85	2.71	126.77	2.46	0.13	0.79
47.87	73.99	46.41	2.72	126.36	2.46	0.13	0.79
47.88	73.31	45.94	2.74	125.92	2.46	0.13	0.79
47.89	72.62	45.45	2.76	125.47	2.47	0.13	0.78
47.90	71.94	44.98	2.78	125.03	2.47	0.13	0.78
47.91	71.32	44.55	2.80	124.63	2.47	0.13	0.78
47.92	70.80	44.18	2.81	124.34	2.48	0.13	0.78
47.93	70.40	43.89	2.84	124.45	2.48	0.13	0.78
47.94	70.07	43.63	2.86	124.99	2.48	0.13	0.78
47.95	69.74	43.37	2.90	125.92	2.49	0.13	0.78
47.96	69.37	43.08	2.95	126.96	2.50	0.13	0.78
47.97	68.98	42.77	2.99	128.05	2.50	0.13	0.78
47.98	68.59	42.46	3.04	129.14	2.51	0.13	0.78
47.99	68.21	42.17	3.09	130.18	2.52	0.13	0.78
48.00	67.88	41.90	3.13	131.11	2.52	0.13	0.78

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
48.01	67.55	41.65	3.17	131.96	2.53	0.13	0.78
48.02	67.16	41.35	3.21	132.93	2.53	0.13	0.78
48.03	66.66	40.96	3.27	134.12	2.54	0.13	0.78
48.04	66.04	40.49	3.35	135.57	2.55	0.13	0.78
48.05	65.36	39.98	3.43	137.14	2.56	0.12	0.78
48.06	64.65	39.45	3.52	138.74	2.57	0.12	0.77
48.07	63.94	38.92	3.60	140.30	2.58	0.12	0.77
48.08	63.28	38.43	3.69	141.73	2.59	0.12	0.77
48.09	62.70	38.00	3.76	142.96	2.60	0.12	0.62
48.10	62.22	37.64	3.82	143.94	2.61	0.12	0.62
48.11	61.77	37.31	3.88	144.80	2.61	0.12	0.62
48.12	61.29	36.96	3.94	145.65	2.62	0.12	0.62
48.13	60.75	36.56	4.01	146.61	2.63	0.12	0.62
48.14	60.15	36.13	4.09	147.62	2.64	0.12	0.62
48.15	59.55	35.69	4.16	148.63	2.65	0.12	0.62
48.16	58.96	35.26	4.24	149.60	2.65	0.12	0.62
48.17	58.42	34.87	4.31	150.46	2.66	0.12	0.62
48.18	57.97	34.55	4.37	151.11	2.67	0.12	0.62
48.19	57.65	34.33	4.41	151.32	2.67	0.12	0.62
48.20	57.43	34.17	4.42	151.11	2.67	0.12	0.62
48.21	57.25	34.05	4.42	150.57	2.67	0.12	0.62
48.22	57.04	33.91	4.42	149.97	2.67	0.12	0.62
48.23	56.82	33.77	4.42	149.33	2.67	0.12	0.62
48.24	56.60	33.62	4.42	148.69	2.67	0.12	0.62
48.25	56.39	33.49	4.42	148.07	2.67	0.12	0.62
48.26	56.20	33.36	4.42	147.52	2.67	0.12	0.62
48.27	56.11	33.31	4.41	146.91	2.67	0.12	0.62
48.28	56.20	33.37	4.38	146.00	2.67	0.12	0.62
48.29	56.46	33.56	4.31	144.68	2.66	0.12	0.62
48.30	56.82	33.83	4.23	142.99	2.65	0.12	0.62
48.31	57.23	34.14	4.13	141.10	2.64	0.12	0.62
48.32	57.64	34.45	4.04	139.09	2.63	0.12	0.62
48.33	58.06	34.77	3.94	137.08	2.62	0.12	0.62
48.34	58.45	35.06	3.86	135.17	2.61	0.12	0.62
48.35	58.79	35.32	3.78	133.47	2.60	0.12	0.62
48.36	59.16	35.60	3.71	132.05	2.60	0.12	0.76
48.37	59.64	35.94	3.64	130.76	2.59	0.12	0.77
48.38	60.28	36.40	3.56	129.40	2.58	0.12	0.77
48.39	61.02	36.94	3.46	127.82	2.56	0.12	0.77
48.40	61.82	37.52	3.36	126.07	2.55	0.12	0.77
48.41	62.64	38.11	3.26	124.25	2.54	0.12	0.77
48.42	63.43	38.70	3.16	122.45	2.53	0.12	0.77
48.43	64.16	39.23	3.08	120.77	2.51	0.12	0.77
48.44	64.78	39.69	3.01	119.36	2.50	0.12	0.77
48.45	65.33	40.09	2.95	118.35	2.50	0.12	0.77
48.46	65.88	40.48	2.90	117.60	2.49	0.12	0.77
48.47	66.51	40.93	2.86	116.94	2.48	0.12	0.77
48.48	67.22	41.43	2.80	116.20	2.47	0.12	0.77

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
48.49	67.97	41.97	2.75	115.40	2.47	0.12	0.78
48.50	68.72	42.51	2.70	114.59	2.46	0.12	0.78
48.51	69.43	43.02	2.65	113.81	2.45	0.12	0.78
48.52	70.07	43.48	2.60	113.11	2.44	0.12	0.78
48.53	70.56	43.83	2.57	112.65	2.44	0.12	0.78
48.54	70.90	44.06	2.55	112.53	2.43	0.13	0.78
48.55	71.12	44.20	2.55	112.72	2.43	0.13	0.78
48.56	71.34	44.34	2.55	113.06	2.43	0.13	0.78
48.57	71.58	44.48	2.55	113.43	2.43	0.13	0.78
48.58	71.83	44.64	2.55	113.82	2.43	0.13	0.78
48.59	72.08	44.79	2.55	114.20	2.43	0.13	0.78
48.60	72.31	44.93	2.55	114.55	2.43	0.13	0.78
48.61	72.51	45.05	2.55	114.87	2.43	0.13	0.78
48.62	72.55	45.05	2.57	115.56	2.43	0.13	0.78
48.63	72.40	44.90	2.60	116.81	2.44	0.13	0.78
48.64	72.07	44.60	2.66	118.74	2.45	0.13	0.78
48.65	71.68	44.25	2.73	120.98	2.46	0.13	0.78
48.66	71.26	43.88	2.81	123.37	2.47	0.13	0.78
48.67	70.83	43.51	2.89	125.80	2.49	0.13	0.78
48.68	70.41	43.15	2.97	128.13	2.50	0.13	0.78
48.69	70.03	42.82	3.04	130.25	2.51	0.13	0.78
48.70	69.69	42.54	3.11	132.15	2.52	0.13	0.78
48.71	69.36	42.24	3.18	134.30	2.53	0.13	0.78
48.72	68.97	41.91	3.27	137.01	2.54	0.13	0.78
48.73	68.51	41.50	3.38	140.44	2.56	0.13	0.78
48.74	67.98	41.04	3.51	144.22	2.57	0.13	0.78
48.75	67.43	40.57	3.65	148.14	2.59	0.13	0.78
48.76	66.87	40.10	3.79	151.99	2.60	0.13	0.63
48.77	66.34	39.66	3.92	155.57	2.62	0.13	0.63
48.78	65.87	39.27	4.04	158.72	2.63	0.13	0.63
48.79	65.46	38.93	4.14	161.30	2.64	0.13	0.63
48.80	65.06	38.62	4.24	163.55	2.65	0.13	0.63
48.81	64.62	38.27	4.33	165.79	2.66	0.13	0.62
48.82	64.11	37.88	4.44	168.31	2.67	0.13	0.62
48.83	63.55	37.44	4.57	171.01	2.69	0.13	0.62
48.84	62.97	37.00	4.70	173.75	2.70	0.13	0.62
48.85	62.40	36.56	4.82	176.37	2.71	0.13	0.62
48.86	61.86	36.16	4.94	178.76	2.72	0.13	0.62
48.87	61.39	35.80	5.05	180.80	2.73	0.13	0.62
48.88	61.10	35.58	5.12	182.16	2.74	0.12	0.62
48.89	60.97	35.47	5.16	182.98	2.74	0.13	0.62
48.90	60.97	35.45	5.17	183.44	2.74	0.13	0.62
48.91	60.97	35.44	5.19	183.94	2.74	0.13	0.62
48.92	60.97	35.42	5.21	184.48	2.75	0.13	0.62
48.93	60.97	35.40	5.23	185.04	2.75	0.13	0.62
48.94	60.97	35.38	5.24	185.57	2.75	0.13	0.62
48.95	60.97	35.37	5.26	186.06	2.75	0.13	0.62
48.96	61.06	35.41	5.26	186.42	2.75	0.13	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
48.97	61.50	35.70	5.23	186.54	2.75	0.13	0.62
48.98	62.38	36.27	5.14	186.41	2.74	0.13	0.62
48.99	63.66	37.12	5.01	186.06	2.73	0.13	0.62
49.00	65.09	38.07	4.88	185.60	2.72	0.13	0.63
49.01	66.60	39.07	4.74	185.02	2.70	0.13	0.63
49.02	68.12	40.08	4.60	184.37	2.69	0.13	0.63
49.03	69.55	41.04	4.47	183.67	2.68	0.13	0.64
49.04	70.84	41.91	4.37	182.98	2.67	0.14	0.64
49.05	72.07	42.73	4.27	182.31	2.66	0.14	0.64
49.06	73.50	43.69	4.16	181.55	2.64	0.14	0.65
49.07	75.30	44.91	4.02	180.58	2.63	0.14	0.65
49.08	77.48	46.39	3.87	179.31	2.61	0.14	0.66
49.09	79.88	48.03	3.70	177.78	2.59	0.15	0.80
49.10	82.36	49.73	3.54	176.05	2.57	0.15	0.80
49.11	84.80	51.42	3.39	174.21	2.56	0.15	0.81
49.12	87.08	53.00	3.25	172.39	2.54	0.16	0.81
49.13	89.06	54.38	3.14	170.72	2.52	0.16	0.81
49.14	90.94	55.69	3.04	169.35	2.51	0.16	0.81
49.15	92.99	57.11	2.94	168.13	2.49	0.16	0.82
49.16	95.46	58.83	2.84	166.88	2.48	0.17	0.82
49.17	98.30	60.82	2.72	165.39	2.46	0.17	0.82
49.18	101.35	62.97	2.60	163.72	2.44	0.18	0.83
49.19	104.46	65.17	2.49	161.97	2.42	0.18	0.83
49.20	107.46	67.30	2.38	160.25	2.40	0.19	0.83
49.21	110.20	69.27	2.29	158.65	2.38	0.19	0.84
49.22	112.54	70.95	2.22	157.36	2.37	0.20	0.84
49.23	114.65	72.46	2.16	156.48	2.36	0.20	0.84
49.24	116.81	74.00	2.11	155.90	2.34	0.21	0.84
49.25	119.31	75.77	2.05	155.43	2.33	0.21	0.85
49.26	122.10	77.77	1.99	154.93	2.32	0.22	0.85
49.27	125.05	79.89	1.93	154.43	2.30	0.22	0.85
49.28	127.99	82.02	1.88	153.98	2.29	0.23	0.86
49.29	130.79	84.06	1.83	153.61	2.27	0.24	0.86
49.30	133.29	85.88	1.79	153.30	2.26	0.24	0.86
49.31	135.27	87.32	1.75	153.19	2.25	0.25	0.86
49.32	136.86	88.46	1.73	153.30	2.24	0.25	0.86
49.33	138.28	89.46	1.72	153.64	2.24	0.26	0.87
49.34	139.85	90.57	1.70	154.10	2.23	0.26	0.87
49.35	141.56	91.79	1.68	154.62	2.23	0.27	0.87
49.36	143.34	93.05	1.67	155.17	2.22	0.28	0.87
49.37	145.09	94.29	1.65	155.72	2.21	0.28	0.87
49.38	146.71	95.44	1.64	156.25	2.21	0.29	0.87
49.39	148.13	96.44	1.62	156.72	2.20	0.29	0.88
49.40	149.24	97.21	1.62	157.21	2.20	0.30	0.88
49.41	150.17	97.85	1.61	157.80	2.20	0.30	0.88
49.42	151.06	98.44	1.61	158.56	2.20	0.31	0.88
49.43	152.09	99.12	1.61	159.43	2.20	0.31	0.88
49.44	153.19	99.85	1.61	160.37	2.20	0.32	0.88

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
49.45	154.31	100.60	1.60	161.32	2.20	0.33	0.88
49.46	155.40	101.32	1.60	162.25	2.19	0.33	0.88
49.47	156.38	101.97	1.60	163.09	2.19	0.34	0.88
49.48	157.18	102.50	1.60	163.67	2.19	0.34	0.89
49.49	157.71	102.88	1.59	163.72	2.19	0.35	0.89
49.50	158.05	103.15	1.58	163.24	2.19	0.35	0.89
49.51	158.32	103.41	1.57	162.37	2.18	0.34	0.89
49.52	158.62	103.70	1.56	161.43	2.18	0.34	0.89
49.53	158.94	104.01	1.54	160.46	2.17	0.34	0.89
49.54	159.25	104.33	1.53	159.51	2.16	0.34	0.88
49.55	159.55	104.63	1.52	158.62	2.16	0.34	0.88
49.56	159.82	104.89	1.50	157.85	2.15	0.34	0.88
49.57	159.94	105.04	1.50	157.10	2.15	0.34	0.88
49.58	159.84	105.05	1.49	156.21	2.14	0.33	0.88
49.59	159.52	104.91	1.48	155.07	2.14	0.33	0.88
49.60	159.10	104.71	1.47	153.70	2.13	0.32	0.88
49.61	158.63	104.50	1.46	152.23	2.12	0.31	0.88
49.62	158.15	104.28	1.45	150.74	2.12	0.31	0.88
49.63	157.68	104.08	1.43	149.30	2.11	0.30	0.88
49.64	157.24	103.88	1.42	147.99	2.10	0.30	0.88
49.65	156.86	103.71	1.42	146.87	2.10	0.29	0.87
49.66	156.50	103.51	1.41	146.12	2.10	0.29	0.87
49.67	156.12	103.25	1.41	145.65	2.09	0.28	0.87
49.68	155.67	102.91	1.41	145.38	2.10	0.28	0.87
49.69	155.16	102.52	1.42	145.07	2.10	0.28	0.87
49.70	154.60	102.10	1.42	144.74	2.10	0.28	0.87
49.71	154.04	101.67	1.42	144.40	2.10	0.28	0.87
49.72	153.50	101.26	1.42	144.08	2.10	0.28	0.87
49.73	153.01	100.88	1.43	143.79	2.10	0.27	0.87
49.74	152.60	100.56	1.43	143.53	2.11	0.27	0.87
49.75	152.23	100.29	1.43	143.30	2.11	0.27	0.87
49.76	151.87	100.01	1.43	143.05	2.11	0.27	0.87
49.77	151.47	99.71	1.43	142.75	2.11	0.27	0.87
49.78	151.01	99.37	1.43	142.43	2.11	0.27	0.87
49.79	150.53	99.01	1.44	142.09	2.11	0.26	0.87
49.80	150.06	98.65	1.44	141.75	2.11	0.26	0.87
49.81	149.60	98.32	1.44	141.43	2.11	0.26	0.87
49.82	149.20	98.01	1.44	141.15	2.11	0.26	0.87
49.83	148.77	97.68	1.44	140.92	2.12	0.26	0.87
49.84	148.21	97.24	1.45	140.73	2.12	0.26	0.87
49.85	147.45	96.64	1.45	140.57	2.12	0.26	0.87
49.86	146.53	95.92	1.46	140.41	2.13	0.25	0.87
49.87	145.52	95.13	1.47	140.25	2.13	0.25	0.86
49.88	144.48	94.31	1.49	140.10	2.14	0.25	0.86
49.89	143.46	93.52	1.50	139.97	2.15	0.25	0.86
49.90	142.51	92.78	1.51	139.86	2.15	0.25	0.86
49.91	141.69	92.14	1.52	139.77	2.16	0.24	0.86
49.92	141.02	91.61	1.52	139.67	2.16	0.24	0.86

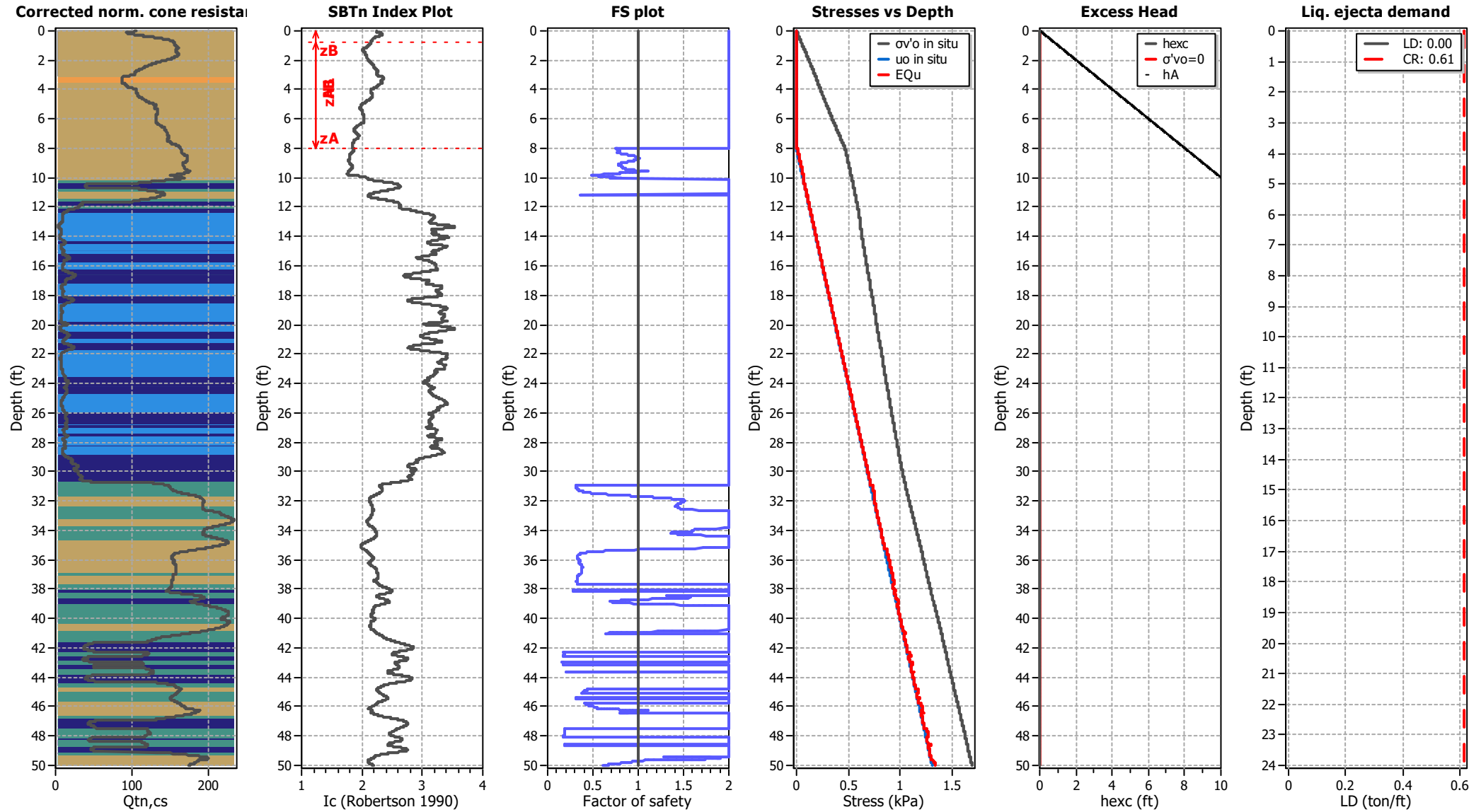
:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
49.93	140.40	91.14	1.53	139.56	2.16	0.24	0.86
49.94	139.76	90.65	1.54	139.40	2.17	0.24	0.86
49.95	139.02	90.08	1.55	139.24	2.17	0.24	0.86
49.96	138.23	89.48	1.55	139.06	2.17	0.24	0.86
49.97	137.43	88.88	1.56	138.89	2.18	0.23	0.86
49.98	136.66	88.29	1.57	138.74	2.18	0.23	0.86
49.99	135.96	87.76	1.58	138.60	2.19	0.23	0.86
50.00	135.52	87.42	1.58	138.51	2.19	0.23	0.86

Abbreviations

q_t :	Total cone resistance
K_c :	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c :	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

Ejecta Severity Estimation



LIQUEFACTION ANALYSIS REPORT

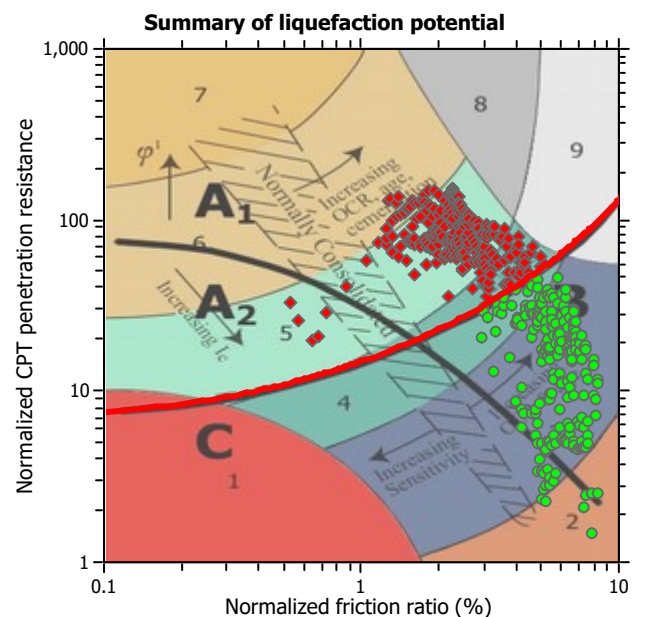
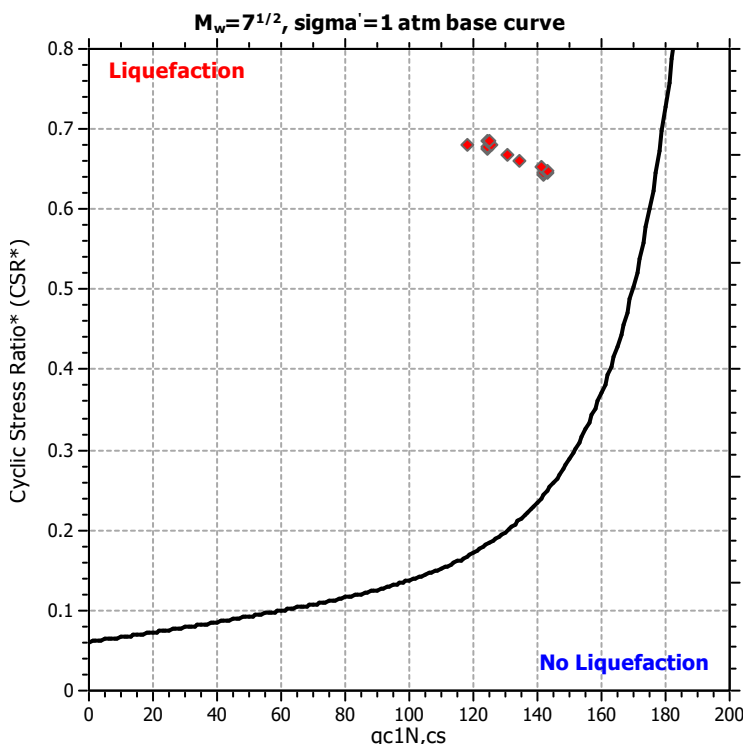
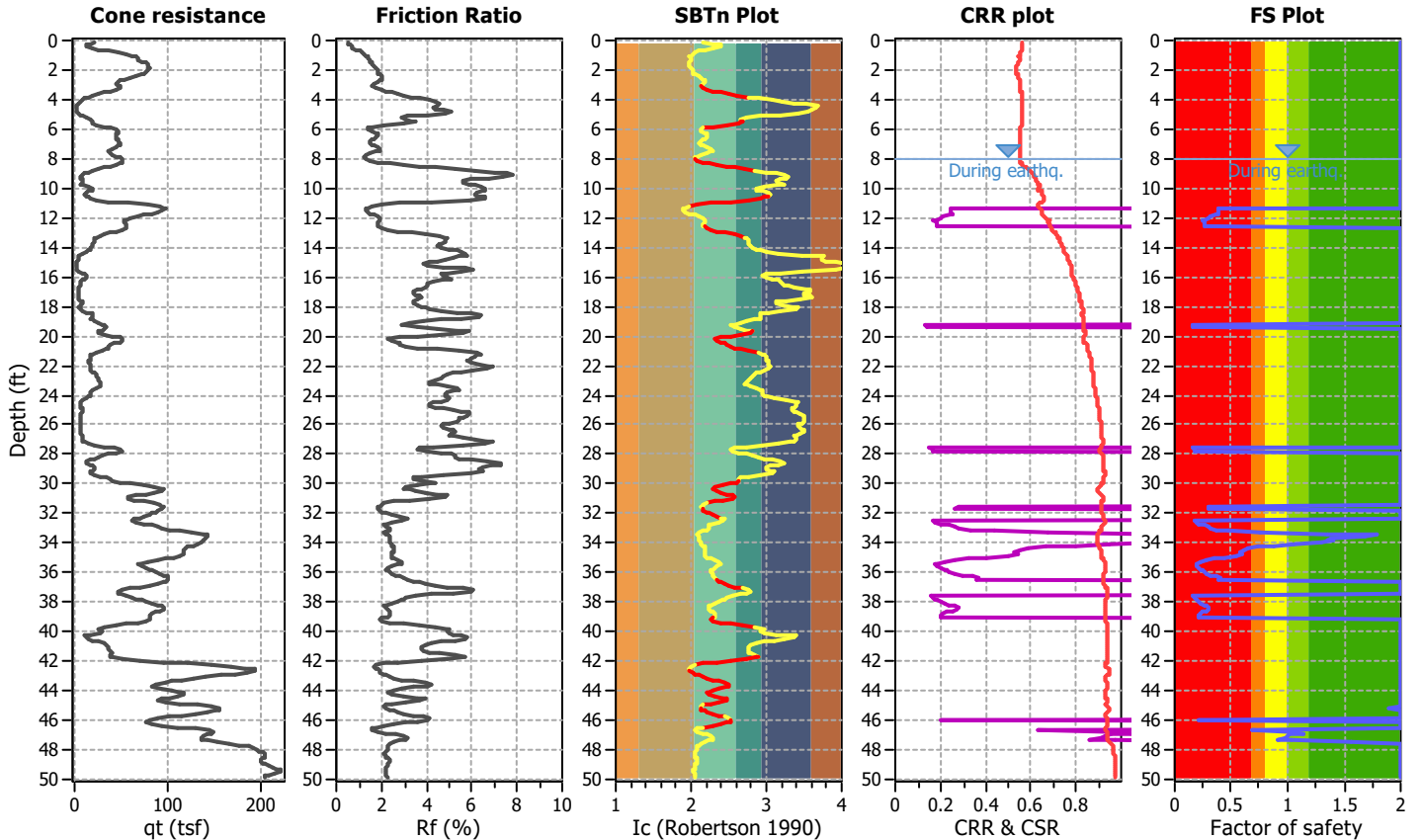
Project title : 21-483 Equestrian Estates

Location : Avenue 64 at Harrison Street, Thermal California

CPT file : CPT-3 B&I 2014

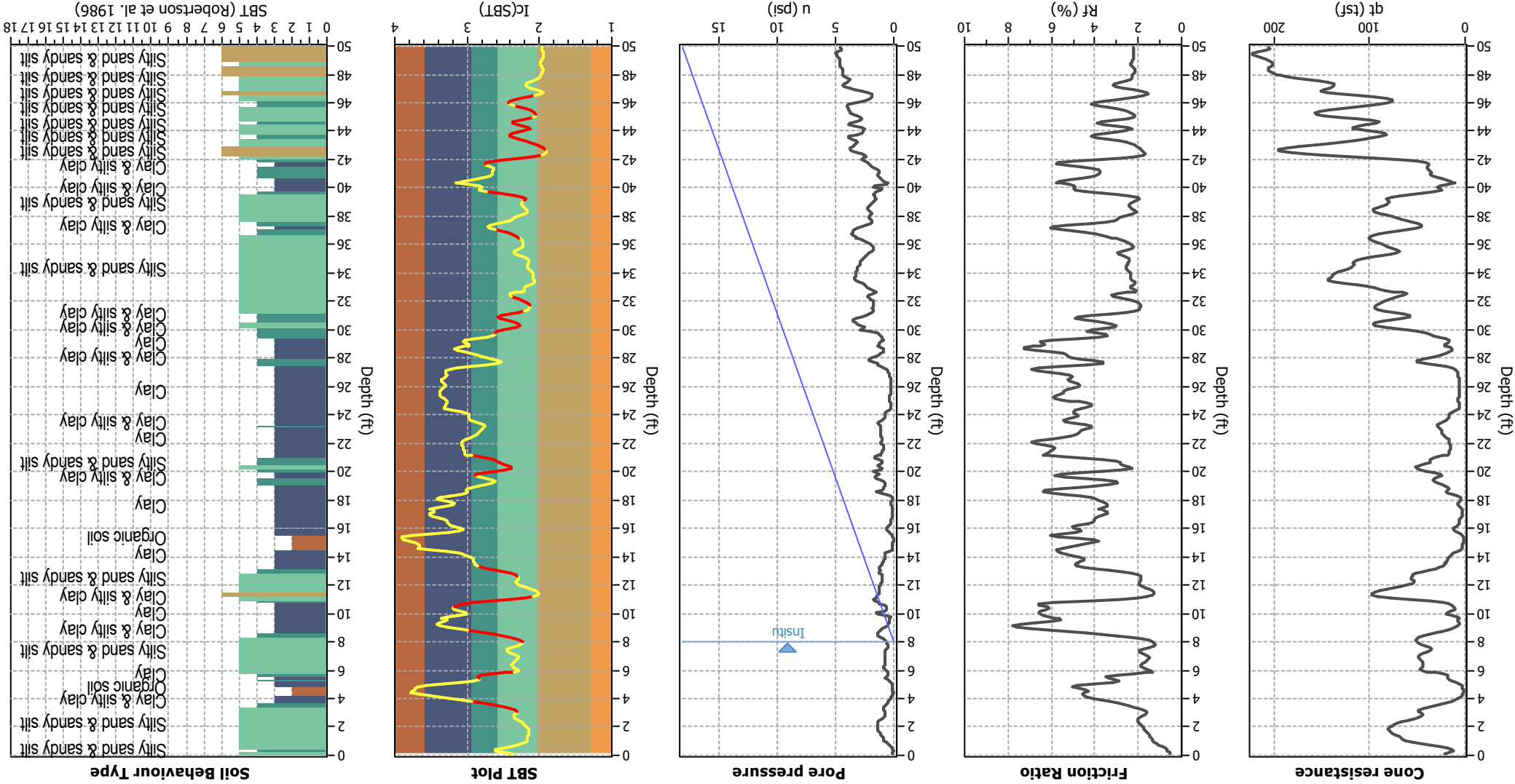
Input parameters and analysis data

Analysis method:	B&I (2014)	G.W.T. (in-situ):	8.00 ft	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	8.00 ft	Fill height:	N/A	Limit depth applied:	No
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth:	N/A
Earthquake magnitude M_w :	7.34	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.74	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		

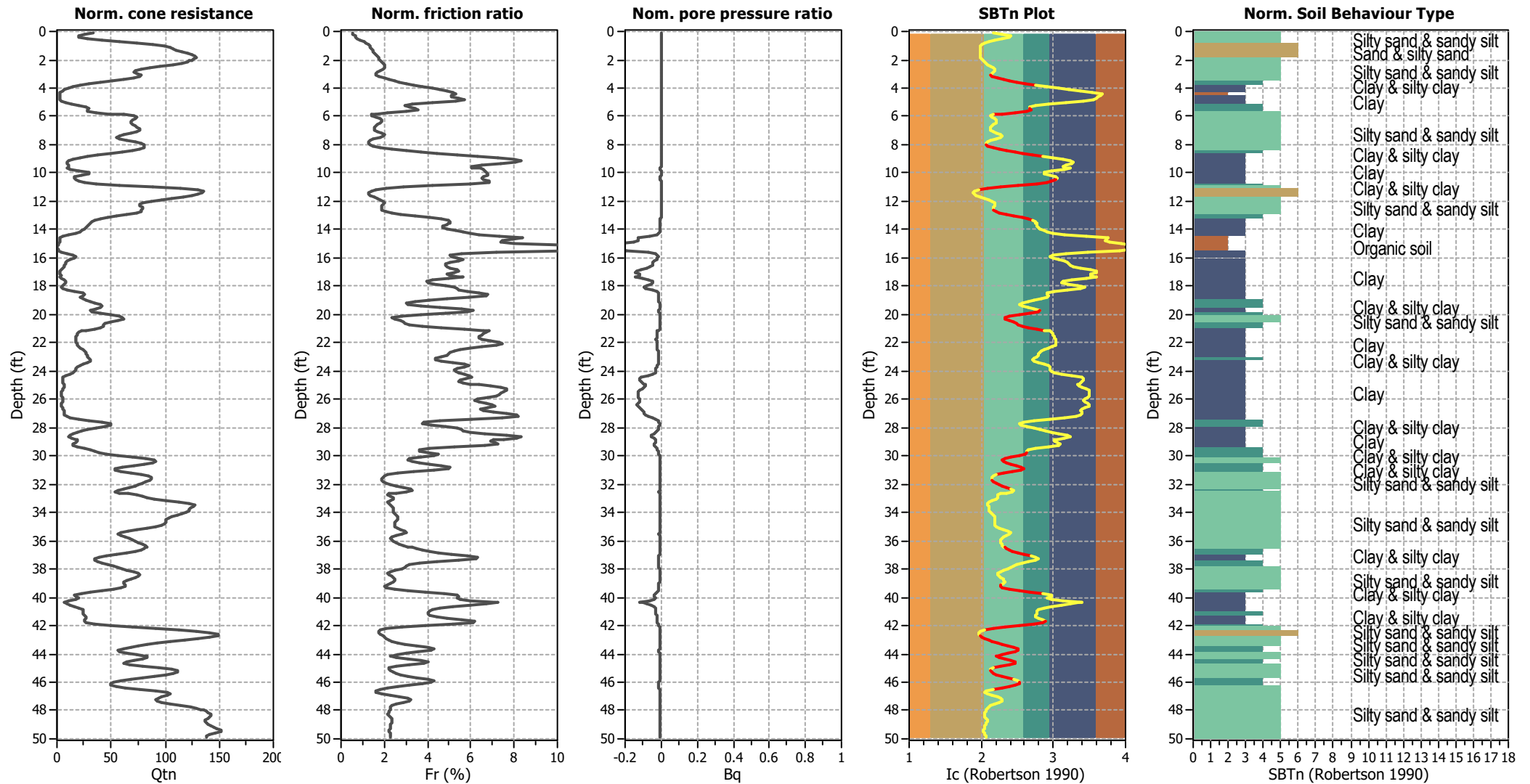


Zone A₁: Cyclic liquefaction likely depending on size and duration of cyclic loading
 Zone A₂: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
 Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
 Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



CPT basic interpretation plots (normalized)



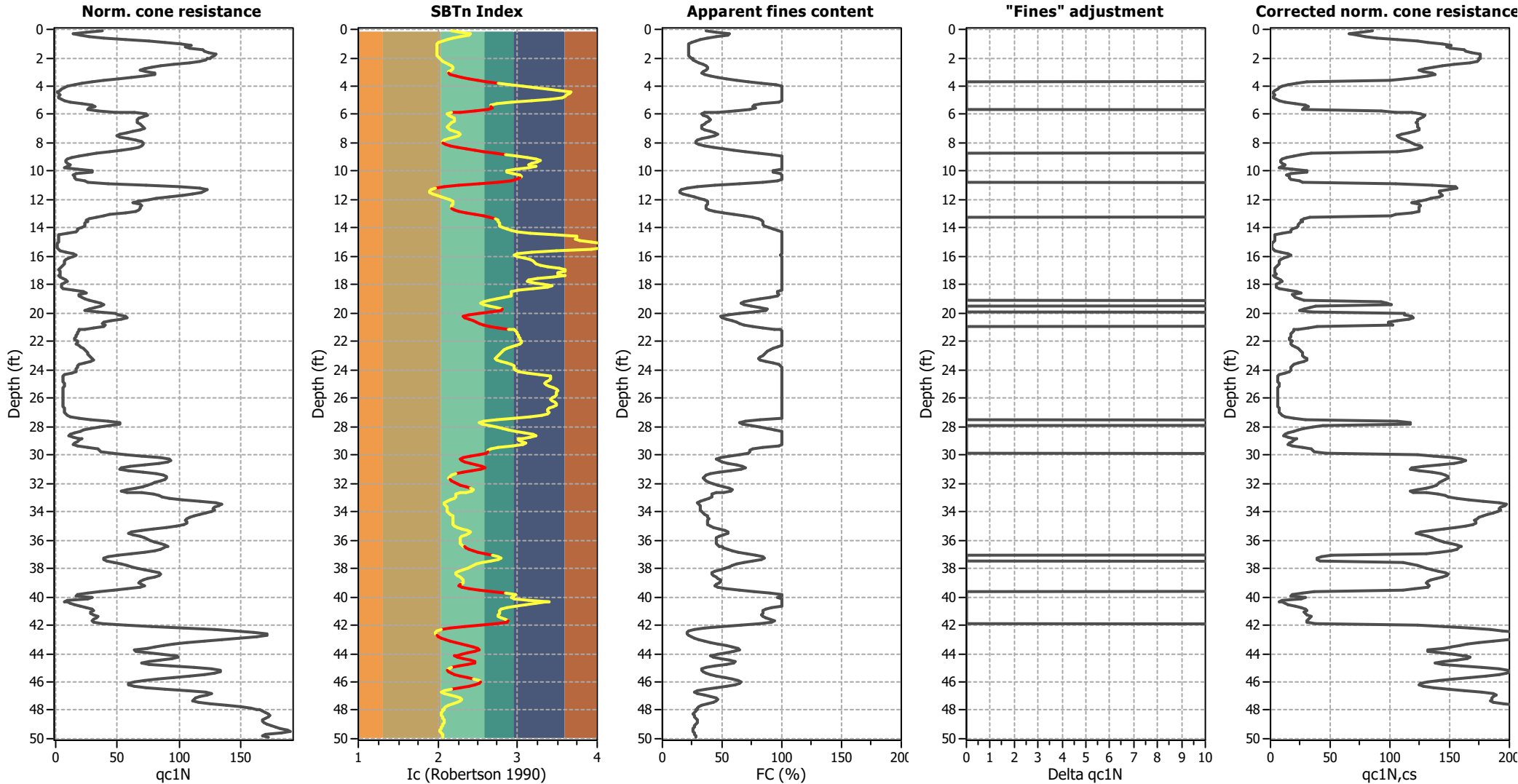
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	Yes
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

SBTn legend

1. Sensitive fine grained	4. Clayey silt to silty	7. Gravely sand to sand
2. Organic material	5. Silty sand to sandy silt	8. Very stiff sand to
3. Clay to silty clay	6. Clean sand to silty sand	9. Very stiff fine grained

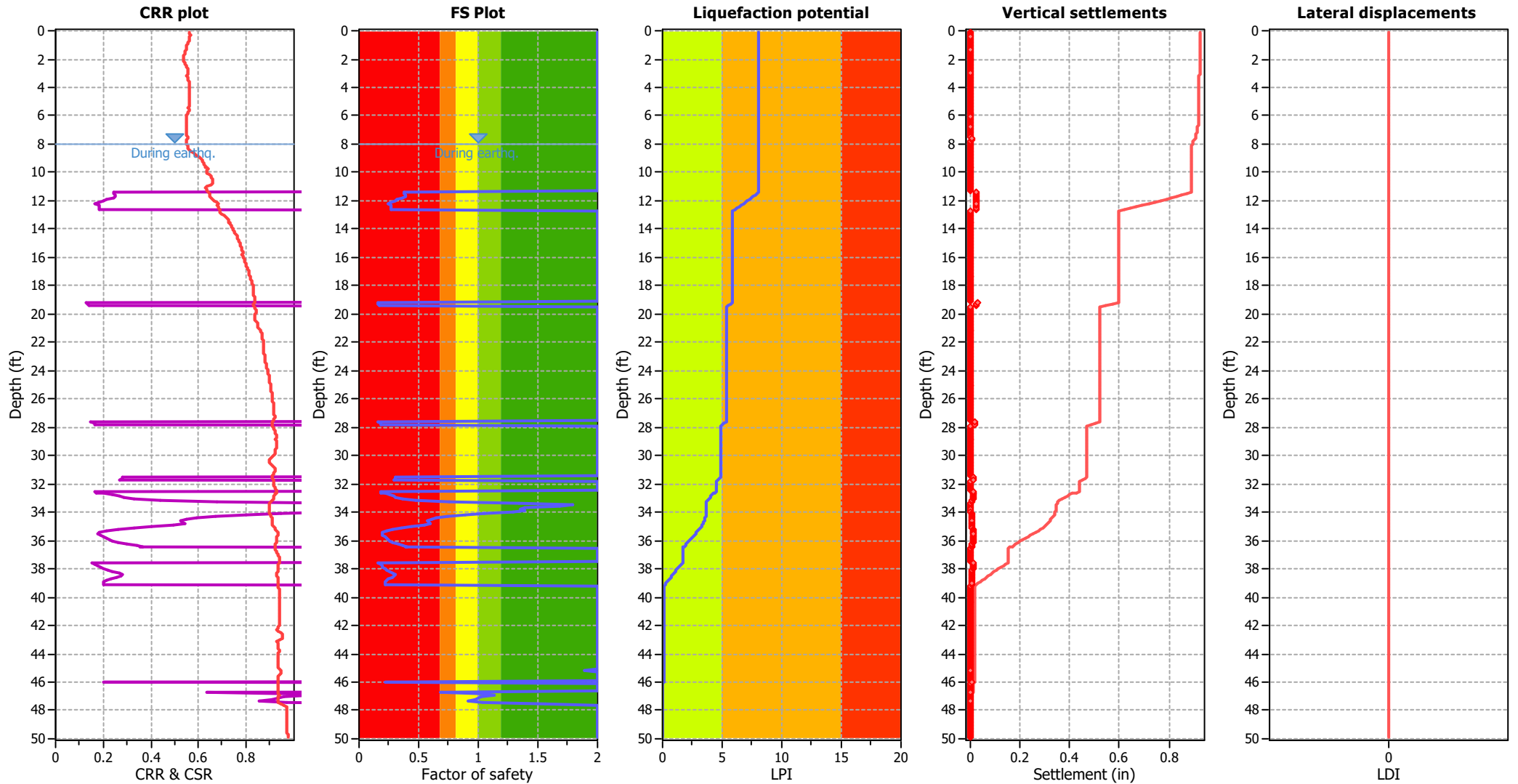
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _σ applied:	Yes
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (earthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	Yes
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

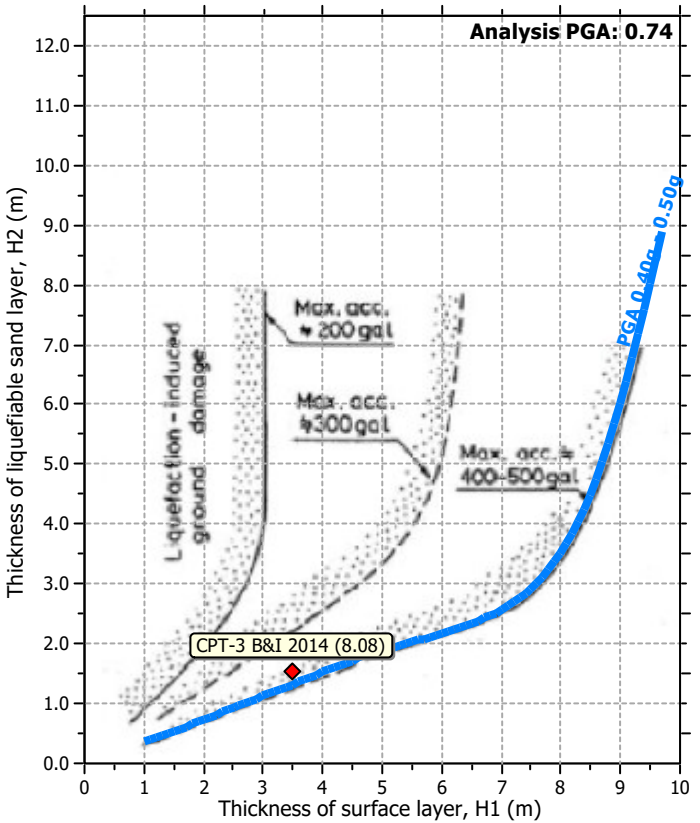
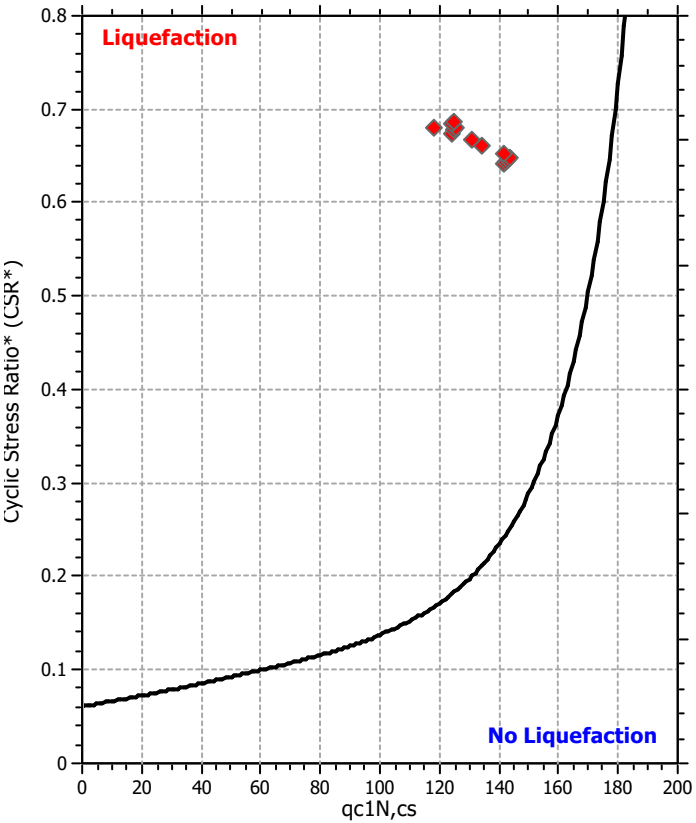
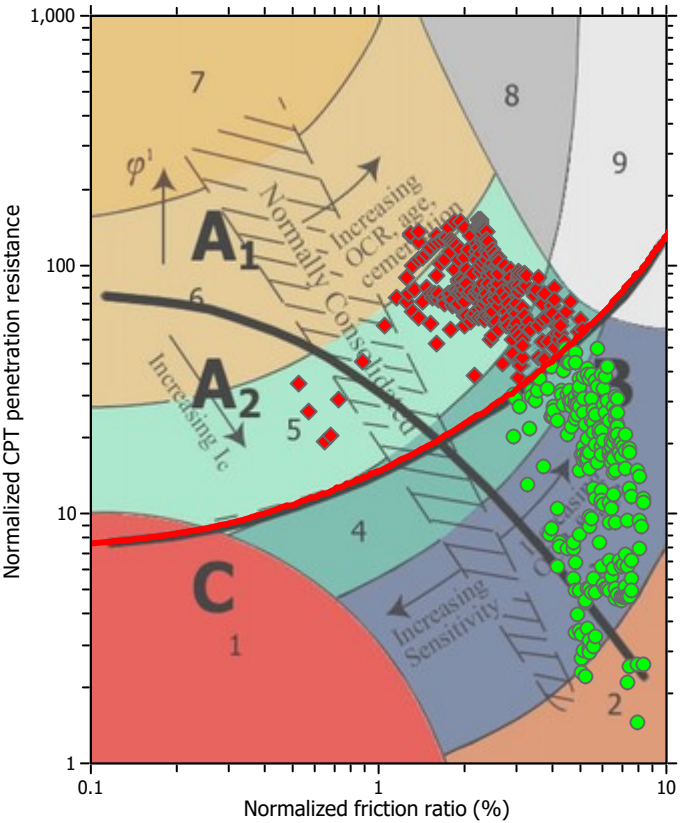
F.S. color scheme

Red	Almost certain it will liquefy
Orange	Very likely to liquefy
Yellow	Liquefaction and no liq. are equally likely
Light Green	Unlike to liquefy
Dark Green	Almost certain it will not liquefy

LPI color scheme

Red	Very high risk
Orange	High risk
Yellow	Low risk

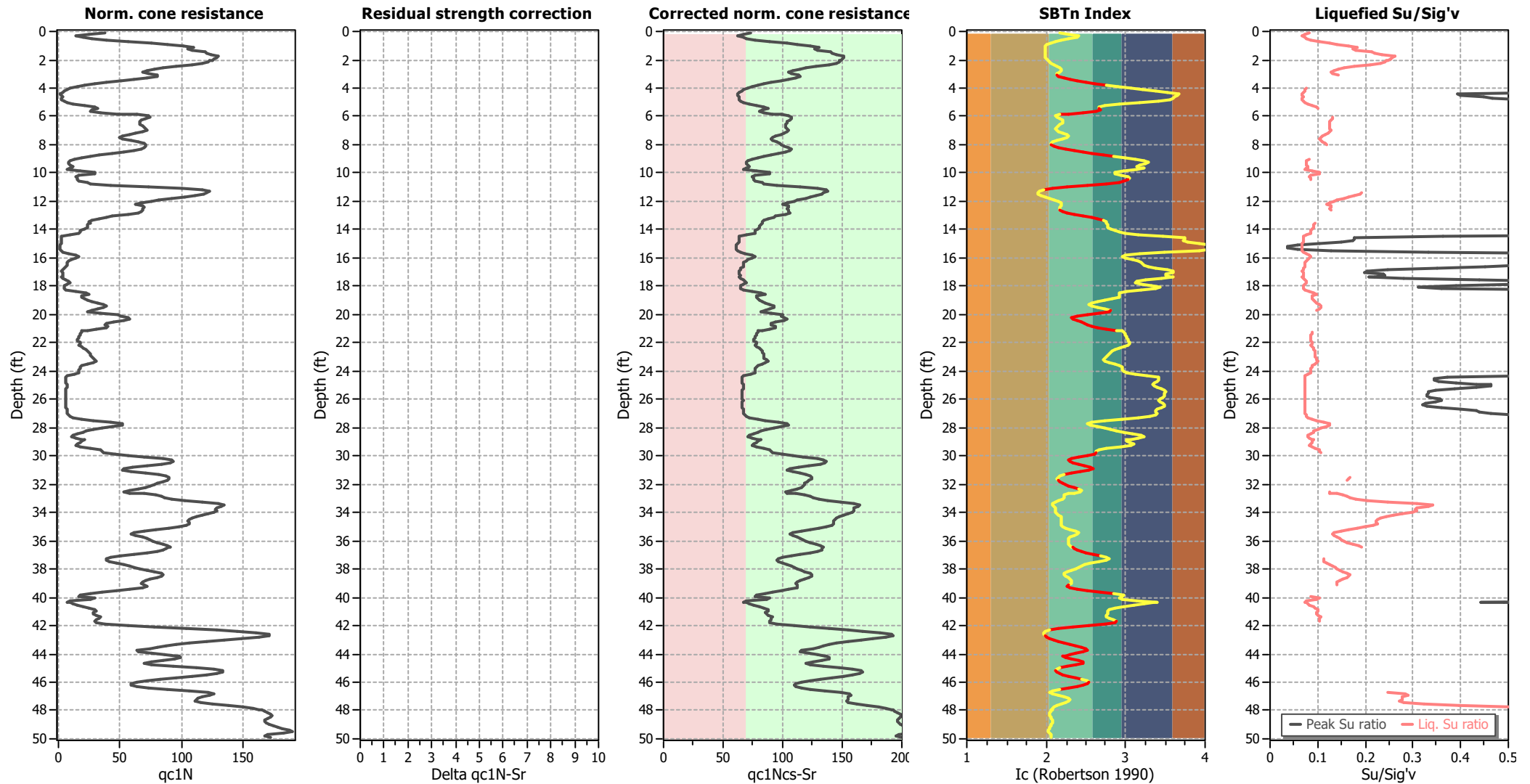
Liquefaction analysis summary plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{ϕ} applied:	Yes
Earthquake magnitude M_w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

Check for strength loss plots (Idriss & Boulanger (2008))



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on I_c value	I_c cut-off value:	2.60	K_g applied:	Yes
Earthquake magnitude M_w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

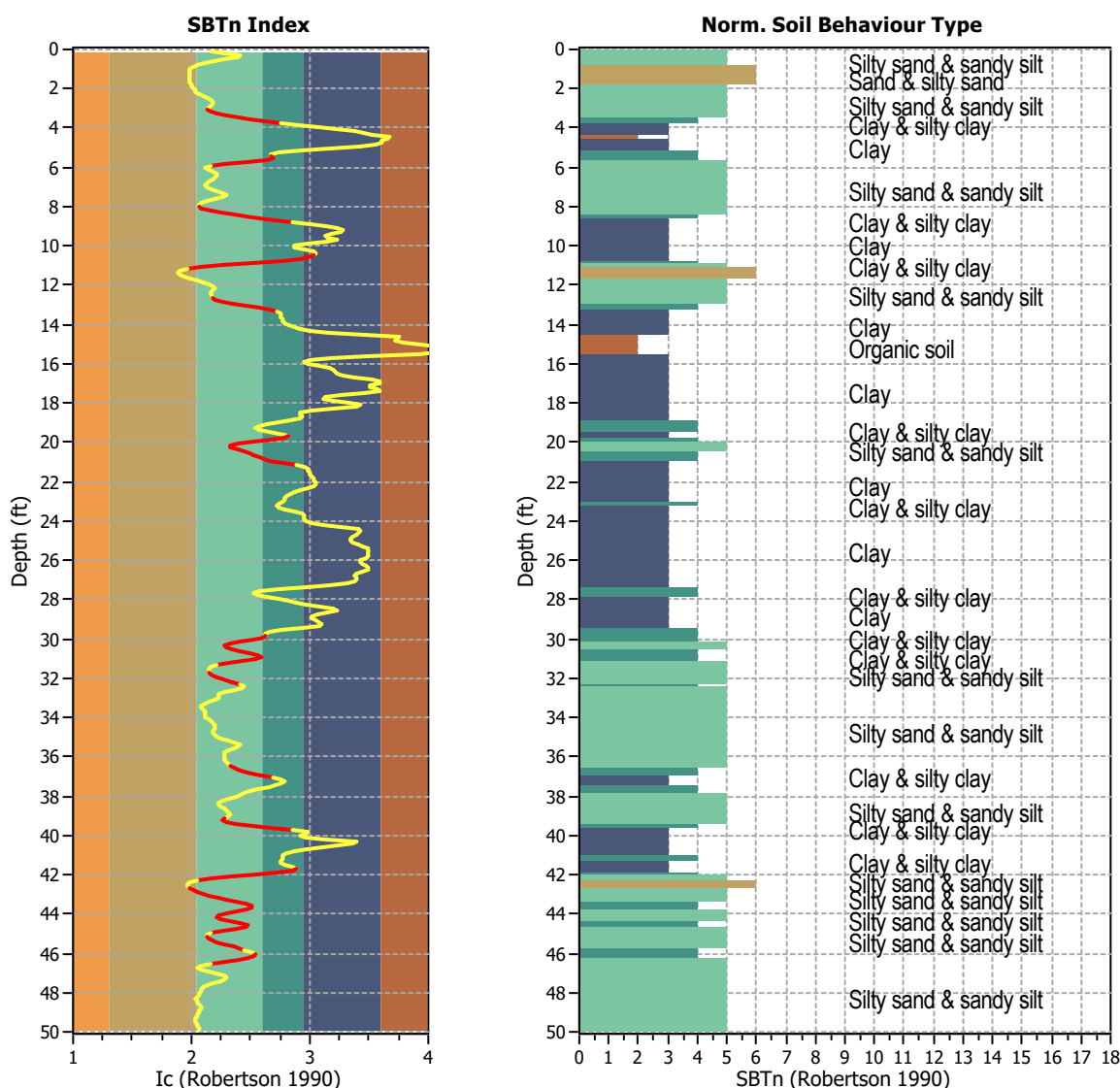
TRANSITION LAYER DETECTION ALGORITHM REPORT

Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vice-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between $1.80 < I_c < 3.0$) and a rate of change of I_c . Transitions typically occur when the rate of change of I_c is fast (i.e. ΔI_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties

I_c minimum check value: 1.70
 I_c maximum check value: 3.00
 I_c change ratio value: 0.0250
 Minimum number of points in layer: 4

General statistics

Total points in CPT file: 499
 Total points excluded: 136
 Exclusion percentage: 27.25%
 Number of layers detected: 20

Transition layer No	Number of points	Depth	SBT _n number	SBT _n description
Transition layer 1	8	Start depth: 3.20 (ft)	5	Silty sand & sandy silt
		End depth: 3.90 (ft)	3	Clay
Transition layer 2	6	Start depth: 5.50 (ft)	4	Clay & silty clay
		End depth: 6.00 (ft)	5	Silty sand & sandy silt
Transition layer 3	9	Start depth: 8.10 (ft)	5	Silty sand & sandy silt
		End depth: 8.90 (ft)	3	Clay
Transition layer 4	8	Start depth: 10.60 (ft)	3	Clay
		End depth: 11.30 (ft)	6	Sand & silty sand
Transition layer 5	8	Start depth: 12.70 (ft)	5	Silty sand & sandy silt
		End depth: 13.40 (ft)	3	Clay
Transition layer 6	5	Start depth: 19.80 (ft)	3	Clay
		End depth: 20.20 (ft)	5	Silty sand & sandy silt
Transition layer 7	10	Start depth: 20.30 (ft)	5	Silty sand & sandy silt
		End depth: 21.20 (ft)	3	Clay
Transition layer 8	5	Start depth: 29.90 (ft)	4	Clay & silty clay
		End depth: 30.30 (ft)	5	Silty sand & sandy silt
Transition layer 9	6	Start depth: 30.40 (ft)	5	Silty sand & sandy silt
		End depth: 30.90 (ft)	4	Clay & silty clay
Transition layer 10	6	Start depth: 30.90 (ft)	4	Clay & silty clay
		End depth: 31.40 (ft)	5	Silty sand & sandy silt
Transition layer 11	7	Start depth: 31.80 (ft)	5	Silty sand & sandy silt
		End depth: 32.40 (ft)	4	Clay & silty clay
Transition layer 12	7	Start depth: 36.60 (ft)	5	Silty sand & sandy silt
		End depth: 37.20 (ft)	3	Clay
Transition layer 13	7	Start depth: 39.20 (ft)	5	Silty sand & sandy silt
		End depth: 39.80 (ft)	3	Clay
Transition layer 14	7	Start depth: 41.80 (ft)	3	Clay
		End depth: 42.40 (ft)	6	Sand & silty sand
Transition layer 15	9	Start depth: 42.80 (ft)	5	Silty sand & sandy silt
		End depth: 43.60 (ft)	4	Clay & silty clay
Transition layer 16	5	Start depth: 43.70 (ft)	4	Clay & silty clay
		End depth: 44.10 (ft)	5	Silty sand & sandy silt
Transition layer 17	5	Start depth: 44.20 (ft)	5	Silty sand & sandy silt
		End depth: 44.60 (ft)	4	Clay & silty clay
Transition layer 18	5	Start depth: 44.70 (ft)	4	Clay & silty clay
		End depth: 45.10 (ft)	5	Silty sand & sandy silt
Transition layer 19	7	Start depth: 45.30 (ft)	5	Silty sand & sandy silt
		End depth: 45.90 (ft)	4	Clay & silty clay
Transition layer 20	6	Start depth: 46.10 (ft)	4	Clay & silty clay
		End depth: 46.60 (ft)	5	Silty sand & sandy silt

Start depth: Depth where the transition layer begins
End depth: Depth where the transition layer ends

:: Field input data ::						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1	0.10	23.36	0.12	0.12	17.83	101.47
2	0.20	15.35	0.09	0.09	21.79	99.44
3	0.30	9.12	0.06	0.06	26.67	97.83
4	0.40	12.40	0.08	0.08	26.34	98.63
5	0.50	17.04	0.11	0.11	21.91	102.39
6	0.60	24.34	0.19	0.19	18.71	107.27
7	0.70	35.40	0.37	0.37	16.23	111.74
8	0.80	47.10	0.55	0.55	14.50	114.99
9	0.90	54.87	0.67	0.67	13.34	117.32
10	1.00	63.20	0.84	0.84	12.70	118.85
11	1.10	67.85	0.94	0.94	12.58	119.69
12	1.20	65.14	0.92	0.92	12.65	120.11
13	1.30	67.16	0.98	0.98	12.64	120.62
14	1.40	74.04	1.11	1.11	12.51	121.31
15	1.50	75.01	1.17	1.17	12.41	122.00
16	1.60	77.31	1.25	1.25	12.45	122.55
17	1.70	80.96	1.35	1.35	12.55	122.99
18	1.80	80.02	1.38	1.38	12.76	123.26
19	1.90	78.73	1.39	1.39	13.11	123.32
20	2.00	77.42	1.40	1.40	13.44	123.34
21	2.10	76.40	1.41	1.41	13.70	123.32
22	2.20	75.47	1.40	1.40	14.01	123.24
23	2.30	72.92	1.39	1.39	14.60	123.05
24	2.40	67.65	1.36	1.36	15.61	122.55
25	2.50	59.20	1.22	1.22	16.83	121.67
26	2.60	52.57	1.06	1.06	17.84	120.48
27	2.70	48.33	0.93	0.93	18.40	119.25
28	2.80	44.75	0.81	0.81	18.53	118.13
29	2.90	42.83	0.72	0.72	18.03	117.34
30	3.00	45.35	0.70	0.70	17.11	117.26
31	3.10	49.63	0.76	0.76	16.74	117.86
32	3.20	49.85	0.87	0.87	17.59	118.47
33	3.30	44.82	0.90	0.90	19.62	118.56
34	3.40	38.54	0.86	0.86	22.48	117.98
35	3.50	31.85	0.79	0.79	26.01	116.81
36	3.60	24.55	0.67	0.67	30.44	115.19
37	3.70	18.60	0.55	0.55	36.14	113.20
38	3.80	13.62	0.46	0.46	43.30	110.98
39	3.90	9.43	0.36	0.36	52.32	108.44
40	4.00	6.42	0.27	0.27	63.31	105.43
41	4.10	4.27	0.19	0.19	74.49	102.53
42	4.20	3.51	0.16	0.16	87.16	99.28
43	4.30	2.12	0.10	0.10	100.00	95.74
44	4.40	1.20	0.05	0.05	100.00	92.31
45	4.50	1.57	0.07	0.07	100.00	92.34
46	4.60	2.27	0.10	0.10	100.00	93.69
47	4.70	1.85	0.09	0.09	100.00	94.63
48	4.80	1.86	0.10	0.10	100.00	96.45

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
49	4.90	3.12	0.16	0.16	91.67	99.04
50	5.00	4.25	0.19	0.19	71.52	102.50
51	5.10	7.69	0.26	0.26	53.83	105.75
52	5.20	13.10	0.35	0.35	42.86	109.38
53	5.30	18.16	0.52	0.52	38.64	112.46
54	5.40	19.86	0.70	0.70	38.62	113.89
55	5.50	17.23	0.64	0.64	39.65	113.78
56	5.60	16.35	0.51	0.51	36.99	112.89
57	5.70	21.19	0.47	0.47	29.30	112.56
58	5.80	30.23	0.46	0.46	21.94	113.21
59	5.90	39.59	0.50	0.50	17.75	114.53
60	6.00	46.17	0.62	0.62	16.50	116.08
61	6.10	47.46	0.75	0.75	17.05	117.39
62	6.20	45.94	0.83	0.83	18.27	118.03
63	6.30	43.81	0.84	0.84	19.22	118.12
64	6.40	42.74	0.81	0.81	19.43	117.90
65	6.50	43.21	0.78	0.78	18.99	117.59
66	6.60	43.90	0.74	0.74	18.24	117.35
67	6.70	45.19	0.72	0.72	17.45	117.18
68	6.80	46.56	0.71	0.71	16.74	117.15
69	6.90	47.97	0.71	0.71	16.35	117.28
70	7.00	48.76	0.74	0.74	16.59	117.54
71	7.10	47.05	0.78	0.78	17.64	117.77
72	7.20	43.20	0.80	0.80	19.34	117.76
73	7.30	39.14	0.80	0.80	21.10	117.31
74	7.40	35.23	0.71	0.71	22.06	116.41
75	7.50	33.45	0.60	0.60	21.34	115.36
76	7.60	35.99	0.53	0.53	19.14	114.64
77	7.70	40.66	0.51	0.51	16.78	114.68
78	7.80	45.60	0.55	0.55	15.26	115.28
79	7.90	49.24	0.61	0.61	14.66	116.07
80	8.00	50.61	0.66	0.66	14.73	116.83
81	8.10	51.17	0.72	0.72	15.50	117.70
82	8.20	50.93	0.86	0.86	17.61	119.23
83	8.30	49.16	1.18	1.18	20.70	120.65
84	8.40	44.49	1.36	1.36	24.54	121.54
85	8.50	38.38	1.42	1.42	28.99	121.57
86	8.60	31.10	1.40	1.40	34.36	120.92
87	8.70	23.78	1.27	1.27	41.13	119.79
88	8.80	17.85	1.13	1.13	49.06	118.19
89	8.90	13.17	0.96	0.96	58.09	116.18
90	9.00	9.32	0.74	0.74	67.49	113.66
91	9.10	6.86	0.53	0.53	75.82	111.11
92	9.20	6.02	0.45	0.45	79.62	109.24
93	9.30	6.09	0.42	0.42	77.36	108.59
94	9.40	6.95	0.41	0.41	71.71	108.75
95	9.50	8.10	0.44	0.44	68.18	108.92
96	9.60	7.66	0.42	0.42	69.18	108.64

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
97	9.70	6.25	0.38	0.38	74.97	107.42
98	9.80	4.87	0.31	0.31	68.91	110.04
99	9.90	12.65	0.78	0.78	56.97	115.26
100	10.00	21.85	1.43	1.43	49.86	118.94
101	10.10	21.86	1.48	1.48	50.15	118.92
102	10.20	12.25	0.78	0.78	54.98	116.47
103	10.30	9.79	0.61	0.61	60.87	113.31
104	10.40	10.78	0.66	0.66	61.69	112.77
105	10.50	10.84	0.66	0.66	60.38	113.47
106	10.60	11.83	0.75	0.75	57.20	115.64
107	10.70	17.45	1.22	1.22	53.13	117.59
108	10.80	19.39	1.25	1.25	44.01	120.15
109	10.90	32.59	1.60	1.60	31.45	122.14
110	11.00	57.58	1.73	1.73	21.31	123.67
111	11.10	80.88	1.54	1.54	15.27	124.21
112	11.20	94.33	1.46	1.46	12.00	123.96
113	11.30	98.49	1.33	1.33	10.60	123.48
114	11.40	96.60	1.19	1.19	10.11	122.98
115	11.50	95.04	1.19	1.19	10.33	122.66
116	11.60	89.85	1.21	1.21	11.17	122.64
117	11.70	82.57	1.24	1.24	12.52	122.62
118	11.80	74.95	1.27	1.27	14.18	122.36
119	11.90	65.44	1.21	1.21	15.84	121.96
120	12.00	60.20	1.17	1.17	17.35	121.28
121	12.10	54.00	1.07	1.07	18.45	120.51
122	12.20	49.56	0.96	0.96	18.71	120.08
123	12.30	54.68	1.02	1.02	18.39	120.02
124	12.40	55.98	1.03	1.03	17.93	120.26
125	12.50	55.38	1.02	1.02	17.89	120.27
126	12.60	55.38	1.02	1.02	18.19	120.31
127	12.70	54.30	1.06	1.06	19.05	120.67
128	12.80	52.80	1.20	1.20	21.01	121.07
129	12.90	46.00	1.28	1.28	24.35	120.97
130	13.00	34.79	1.18	1.18	28.83	120.69
131	13.10	31.32	1.27	1.27	33.91	120.12
132	13.20	26.15	1.23	1.23	38.00	119.58
133	13.30	21.95	1.09	1.09	41.51	118.57
134	13.40	20.08	0.97	0.97	43.16	117.83
135	13.50	20.69	0.99	0.99	43.62	117.47
136	13.60	20.11	0.98	0.98	43.83	117.28
137	13.70	19.22	0.91	0.91	44.19	116.73
138	13.80	18.46	0.82	0.82	44.26	116.20
139	13.90	18.46	0.81	0.81	44.97	115.81
140	14.00	17.17	0.81	0.81	47.14	115.35
141	14.10	14.45	0.73	0.73	50.20	114.88
142	14.20	13.85	0.74	0.74	52.99	114.58
143	14.30	13.76	0.78	0.78	58.23	113.08
144	14.40	7.30	0.43	0.43	69.93	109.42

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
145	14.50	2.41	0.14	0.14	95.36	103.06
146	14.60	2.41	0.13	0.13	100.00	97.61
147	14.70	2.41	0.12	0.12	100.00	97.15
148	14.80	2.41	0.12	0.12	100.00	96.67
149	14.90	2.41	0.11	0.11	100.00	95.24
150	15.00	1.75	0.07	0.07	100.00	92.65
151	15.10	1.20	0.04	0.04	100.00	89.56
152	15.20	1.20	0.05	0.05	100.00	88.55
153	15.30	1.20	0.06	0.06	100.00	89.83
154	15.40	1.20	0.07	0.07	100.00	92.56
155	15.50	1.77	0.11	0.11	100.00	96.70
156	15.60	3.16	0.19	0.19	97.54	102.42
157	15.70	6.83	0.35	0.35	70.95	107.31
158	15.80	11.33	0.50	0.50	58.36	110.80
159	15.90	13.58	0.62	0.62	55.16	112.33
160	16.00	11.74	0.61	0.61	57.92	111.99
161	16.10	8.82	0.46	0.46	64.07	110.14
162	16.20	7.21	0.33	0.33	69.92	107.42
163	16.30	6.02	0.25	0.25	72.58	105.37
164	16.40	6.02	0.24	0.24	73.94	104.36
165	16.50	6.02	0.24	0.24	75.28	103.93
166	16.60	5.35	0.22	0.22	79.64	102.79
167	16.70	4.18	0.16	0.16	87.94	100.72
168	16.80	3.23	0.12	0.12	100.00	97.98
169	16.90	2.46	0.09	0.09	100.00	96.40
170	17.00	3.01	0.10	0.10	100.00	95.88
171	17.10	3.09	0.10	0.10	100.00	97.00
172	17.20	3.58	0.12	0.12	100.00	97.44
173	17.30	3.19	0.12	0.12	100.00	97.13
174	17.40	2.45	0.10	0.10	100.00	96.99
175	17.50	3.29	0.12	0.12	94.68	98.71
176	17.60	5.31	0.18	0.18	77.57	101.73
177	17.70	7.05	0.23	0.23	67.97	104.11
178	17.80	7.83	0.27	0.27	66.97	104.70
179	17.90	6.23	0.23	0.23	72.97	103.59
180	18.00	4.20	0.16	0.16	83.57	101.67
181	18.10	4.01	0.16	0.16	92.49	100.34
182	18.20	4.01	0.16	0.16	88.41	101.80
183	18.30	5.63	0.25	0.25	72.28	107.19
184	18.40	12.16	0.60	0.60	59.39	113.37
185	18.50	19.22	1.13	1.13	53.00	117.76
186	18.60	21.87	1.46	1.46	52.73	118.89
187	18.70	16.04	1.05	1.05	53.75	118.30
188	18.80	16.26	0.91	0.91	52.97	116.65
189	18.90	18.16	0.84	0.84	48.03	116.20
190	19.00	20.82	0.81	0.81	42.67	116.19
191	19.10	24.12	0.79	0.79	37.63	116.44
192	19.20	28.37	0.80	0.80	33.73	117.05

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
193	19.30	32.47	0.90	0.90	32.34	118.37
194	19.40	34.48	1.17	1.17	33.96	120.08
195	19.50	33.01	1.49	1.49	37.75	121.31
196	19.60	28.76	1.60	1.60	42.68	121.60
197	19.70	24.19	1.51	1.51	46.85	120.84
198	19.80	21.41	1.24	1.24	45.63	120.72
199	19.90	30.61	1.50	1.50	38.88	121.69
200	20.00	43.94	1.76	1.76	31.72	122.04
201	20.10	46.11	1.11	1.11	26.18	121.66
202	20.20	51.95	1.06	1.06	23.28	120.89
203	20.30	53.23	1.29	1.29	23.72	121.48
204	20.40	48.90	1.38	1.38	25.93	121.54
205	20.50	40.77	1.19	1.19	28.31	120.60
206	20.60	35.38	0.98	0.98	30.07	119.44
207	20.70	34.67	0.99	0.99	31.50	119.58
208	20.80	36.88	1.29	1.29	33.84	120.92
209	20.90	35.91	1.63	1.63	37.95	121.92
210	21.00	28.52	1.65	1.65	43.95	121.67
211	21.10	21.10	1.39	1.39	50.91	120.26
212	21.20	17.53	1.13	1.13	55.48	118.73
213	21.30	17.43	1.07	1.07	57.17	117.67
214	21.40	16.33	1.00	1.00	57.67	117.18
215	21.50	15.77	0.96	0.96	58.51	116.64
216	21.60	15.34	0.89	0.89	58.89	116.22
217	21.70	15.05	0.87	0.87	59.43	115.89
218	21.80	14.58	0.86	0.86	60.35	115.92
219	21.90	14.69	0.91	0.91	60.88	116.66
220	22.00	16.43	1.13	1.13	61.38	117.45
221	22.10	16.15	1.15	1.15	61.39	117.84
222	22.20	15.74	1.06	1.06	60.31	117.66
223	22.30	17.06	1.03	1.03	57.33	117.52
224	22.40	18.76	1.03	1.03	53.48	117.82
225	22.50	20.92	1.09	1.09	50.34	118.22
226	22.60	22.52	1.11	1.11	47.94	118.56
227	22.70	23.58	1.10	1.10	46.32	118.79
228	22.80	24.50	1.14	1.14	45.56	118.98
229	22.90	24.68	1.16	1.16	44.98	119.08
230	23.00	25.14	1.13	1.13	43.88	119.01
231	23.10	26.33	1.07	1.07	42.10	119.03
232	23.20	28.36	1.12	1.12	41.18	119.47
233	23.30	29.17	1.28	1.28	42.32	120.00
234	23.40	26.46	1.33	1.33	45.52	120.03
235	23.50	22.23	1.23	1.23	49.95	119.18
236	23.60	18.49	1.03	1.03	53.67	117.90
237	23.70	17.23	0.91	0.91	55.47	116.57
238	23.80	16.44	0.80	0.80	55.67	115.63
239	23.90	15.88	0.74	0.74	55.75	115.17
240	24.00	16.09	0.78	0.78	56.57	115.03

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
241	24.10	15.38	0.77	0.77	59.26	114.37
242	24.20	12.06	0.60	0.60	66.68	112.02
243	24.30	6.53	0.32	0.32	78.06	108.59
244	24.40	5.62	0.26	0.26	90.22	105.18
245	24.50	5.62	0.24	0.24	91.33	104.14
246	24.60	5.62	0.23	0.23	90.40	103.80
247	24.70	5.62	0.23	0.23	89.26	104.07
248	24.80	6.08	0.26	0.26	86.90	105.23
249	24.90	7.02	0.33	0.33	85.05	106.60
250	25.00	7.22	0.37	0.37	84.72	107.76
251	25.10	7.22	0.41	0.41	86.49	108.37
252	25.20	7.10	0.42	0.42	89.99	108.24
253	25.30	6.16	0.37	0.37	94.22	107.53
254	25.40	5.62	0.33	0.33	97.90	106.57
255	25.50	5.62	0.31	0.31	98.85	106.00
256	25.60	5.62	0.30	0.30	98.47	105.84
257	25.70	5.62	0.31	0.31	98.47	105.79
258	25.80	5.62	0.31	0.31	98.15	105.65
259	25.90	5.62	0.29	0.29	95.89	105.46
260	26.00	5.97	0.28	0.28	92.30	105.46
261	26.10	6.42	0.29	0.29	91.60	105.43
262	26.20	5.78	0.28	0.28	93.20	105.38
263	26.30	5.62	0.28	0.28	96.71	105.24
264	26.40	5.62	0.29	0.29	98.25	105.41
265	26.50	5.62	0.30	0.30	97.84	105.70
266	26.60	5.92	0.31	0.31	93.73	106.21
267	26.70	6.87	0.33	0.33	89.37	106.88
268	26.80	7.22	0.37	0.37	87.33	107.72
269	26.90	7.22	0.40	0.40	88.50	108.46
270	27.00	7.24	0.44	0.44	88.76	109.58
271	27.10	8.25	0.54	0.54	87.31	110.96
272	27.20	9.15	0.65	0.65	81.76	112.94
273	27.30	11.79	0.83	0.83	70.15	115.65
274	27.40	19.00	1.16	1.16	55.80	118.33
275	27.50	28.88	1.34	1.34	42.53	120.58
276	27.60	42.78	1.44	1.44	34.45	122.41
277	27.70	52.84	1.77	1.77	31.71	123.98
278	27.80	52.02	2.12	2.12	33.23	124.94
279	27.90	44.52	2.16	2.16	37.28	124.84
280	28.00	36.12	1.93	1.93	42.08	123.62
281	28.10	28.71	1.51	1.51	46.73	121.69
282	28.20	23.10	1.19	1.19	51.05	119.72
283	28.30	20.01	1.08	1.08	56.64	117.99
284	28.40	15.37	0.92	0.92	63.94	116.59
285	28.50	12.11	0.83	0.83	72.57	115.44
286	28.60	11.28	0.84	0.84	75.03	115.92
287	28.70	14.81	1.11	1.11	69.42	117.68
288	28.80	19.73	1.38	1.38	62.52	119.31

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
289	28.90	21.85	1.39	1.39	59.21	119.75
290	29.00	19.95	1.23	1.23	59.09	119.44
291	29.10	18.95	1.23	1.23	61.96	118.66
292	29.20	16.41	1.11	1.11	65.18	117.71
293	29.30	14.40	0.91	0.91	63.65	117.04
294	29.40	18.69	0.95	0.95	54.12	117.31
295	29.50	27.27	1.03	1.03	43.72	118.55
296	29.60	35.26	1.12	1.12	38.29	119.76
297	29.70	36.90	1.27	1.27	36.67	120.81
298	29.80	37.86	1.42	1.42	36.57	122.67
299	29.90	47.57	2.06	2.06	35.63	125.18
300	30.00	59.43	2.84	2.84	31.90	126.96
301	30.10	72.06	2.61	2.61	27.13	127.87
302	30.20	88.24	2.49	2.49	23.36	128.27
303	30.30	96.28	2.86	2.86	21.90	128.96
304	30.40	98.08	3.12	3.12	22.50	129.68
305	30.50	94.63	3.30	3.30	24.07	130.09
306	30.60	87.48	3.49	3.49	26.65	130.14
307	30.70	75.37	3.48	3.48	29.99	129.78
308	30.80	63.77	3.24	3.24	33.28	128.88
309	30.90	55.59	2.77	2.77	34.73	127.66
310	31.00	54.58	2.33	2.33	32.64	126.55
311	31.10	63.00	2.08	2.08	27.79	125.82
312	31.20	75.21	1.86	1.86	22.84	125.45
313	31.30	85.87	1.74	1.74	19.60	125.39
314	31.40	91.96	1.81	1.81	18.03	125.57
315	31.50	95.17	1.85	1.85	17.40	125.68
316	31.60	95.44	1.76	1.76	17.13	125.56
317	31.70	93.52	1.71	1.71	17.30	125.35
318	31.80	89.94	1.73	1.73	17.99	125.26
319	31.90	86.16	1.75	1.75	19.00	125.29
320	32.00	83.26	1.80	1.80	20.32	125.51
321	32.10	79.93	1.96	1.96	22.12	125.94
322	32.20	75.59	2.16	2.16	24.40	126.32
323	32.30	69.54	2.25	2.25	26.71	126.25
324	32.40	62.40	2.08	2.08	28.20	125.53
325	32.50	57.88	1.73	1.73	27.69	124.55
326	32.60	62.47	1.56	1.56	24.72	123.92
327	32.70	74.66	1.53	1.53	21.60	124.21
328	32.80	84.96	1.71	1.71	19.95	125.15
329	32.90	90.22	2.01	2.01	19.83	126.27
330	33.00	92.64	2.26	2.26	19.92	127.22
331	33.10	99.42	2.42	2.42	19.15	127.90
332	33.20	111.27	2.49	2.49	17.53	128.54
333	33.30	126.51	2.64	2.64	16.04	129.37
334	33.40	140.69	3.00	3.00	15.34	130.27
335	33.50	145.55	3.29	3.29	15.40	130.94
336	33.60	143.14	3.38	3.38	15.86	131.19

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
337	33.70	138.85	3.35	3.35	16.19	131.15
338	33.80	138.32	3.29	3.29	16.25	131.01
339	33.90	139.02	3.23	3.23	16.26	130.93
340	34.00	137.10	3.26	3.26	16.50	130.83
341	34.10	131.72	3.20	3.20	17.05	130.71
342	34.20	126.79	3.17	3.17	17.71	130.51
343	34.30	121.80	3.13	3.13	18.33	130.32
344	34.40	118.10	3.07	3.07	18.74	130.11
345	34.50	116.34	2.98	2.98	18.86	129.88
346	34.60	115.59	2.90	2.90	18.72	129.69
347	34.70	116.33	2.86	2.86	18.51	129.57
348	34.80	117.22	2.83	2.83	18.43	129.45
349	34.90	114.57	2.77	2.77	18.67	129.19
350	35.00	107.70	2.62	2.62	19.39	128.73
351	35.10	98.96	2.48	2.48	20.74	128.16
352	35.20	88.31	2.39	2.39	22.75	127.59
353	35.30	77.62	2.31	2.31	25.09	126.86
354	35.40	68.31	2.07	2.07	26.62	125.99
355	35.50	65.97	1.83	1.83	26.31	125.20
356	35.60	70.57	1.74	1.74	24.53	124.81
357	35.70	76.50	1.71	1.71	22.78	124.90
358	35.80	80.96	1.78	1.78	21.81	125.25
359	35.90	83.75	1.89	1.89	21.57	125.80
360	36.00	86.58	2.05	2.05	21.60	126.46
361	36.10	90.50	2.24	2.24	21.67	127.25
362	36.20	95.49	2.50	2.50	21.83	128.14
363	36.30	99.63	2.81	2.81	22.21	129.01
364	36.40	101.57	3.09	3.09	22.85	129.63
365	36.50	99.95	3.20	3.20	23.67	130.01
366	36.60	97.99	3.31	3.31	24.68	130.27
367	36.70	96.11	3.50	3.50	26.05	130.50
368	36.80	90.93	3.63	3.63	28.02	130.53
369	36.90	81.16	3.56	3.56	30.87	130.25
370	37.00	69.87	3.46	3.46	34.83	129.70
371	37.10	58.29	3.34	3.34	39.61	128.94
372	37.20	48.52	3.08	3.08	43.73	128.03
373	37.30	44.82	2.76	2.76	45.21	126.97
374	37.40	44.66	2.36	2.36	43.04	125.94
375	37.50	47.56	2.02	2.02	38.39	125.08
376	37.60	54.34	1.82	1.82	33.54	124.67
377	37.70	61.44	1.82	1.82	30.07	124.86
378	37.80	66.90	1.95	1.95	28.27	125.41
379	37.90	71.00	2.09	2.09	27.04	125.94
380	38.00	75.80	2.11	2.11	25.38	126.18
381	38.10	82.21	2.02	2.02	23.14	126.14
382	38.20	89.04	1.90	1.90	21.04	126.13
383	38.30	95.54	1.95	1.95	19.96	126.37
384	38.40	97.51	2.10	2.10	19.95	126.78

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
385	38.50	96.01	2.19	2.19	20.66	127.03
386	38.60	92.05	2.19	2.19	21.58	126.91
387	38.70	86.37	2.09	2.09	22.47	126.54
388	38.80	81.79	1.98	1.98	23.16	126.06
389	38.90	79.22	1.90	1.90	23.37	125.63
390	39.00	78.86	1.80	1.80	22.83	125.20
391	39.10	80.81	1.66	1.66	21.69	124.73
392	39.20	83.20	1.54	1.54	21.08	124.40
393	39.30	80.09	1.57	1.57	22.26	124.18
394	39.40	67.79	1.60	1.60	25.80	124.11
395	39.50	56.06	1.70	1.70	31.67	123.72
396	39.60	42.81	1.63	1.63	39.21	122.92
397	39.70	31.60	1.47	1.47	48.62	121.25
398	39.80	21.76	1.13	1.13	57.06	119.38
399	39.90	20.05	0.99	0.99	56.18	119.96
400	40.00	35.20	1.71	1.71	53.24	121.06
401	40.10	31.33	1.58	1.58	56.06	120.12
402	40.20	11.47	0.61	0.61	68.69	116.38
403	40.30	8.83	0.49	0.49	88.64	112.26
404	40.40	11.74	0.69	0.69	85.88	113.34
405	40.50	14.26	0.83	0.83	75.88	115.57
406	40.60	18.46	1.00	1.00	65.83	117.48
407	40.70	24.66	1.17	1.17	56.61	119.14
408	40.80	30.75	1.29	1.29	49.72	120.42
409	40.90	35.57	1.38	1.38	45.74	121.13
410	41.00	36.72	1.39	1.39	44.37	121.20
411	41.10	34.52	1.28	1.28	44.31	121.01
412	41.20	34.77	1.29	1.29	44.25	121.05
413	41.30	37.22	1.41	1.41	43.46	121.86
414	41.40	41.26	1.66	1.66	43.78	122.83
415	41.50	39.99	1.83	1.83	45.54	123.67
416	41.60	37.91	1.99	1.99	48.74	124.23
417	41.70	36.72	2.17	2.17	50.98	124.69
418	41.80	37.46	2.28	2.28	49.47	125.39
419	41.90	46.22	2.46	2.46	42.02	126.55
420	42.00	68.41	2.76	2.76	32.44	127.63
421	42.10	92.84	2.62	2.62	23.73	128.36
422	42.20	122.77	2.42	2.42	17.65	128.75
423	42.30	149.87	2.52	2.52	14.21	129.40
424	42.40	169.09	2.82	2.82	12.71	130.45
425	42.50	186.52	3.22	3.22	12.20	131.52
426	42.60	197.52	3.58	3.58	12.18	132.32
427	42.70	197.98	3.75	3.75	12.56	132.66
428	42.80	187.91	3.72	3.72	13.31	132.54
429	42.90	172.76	3.56	3.56	14.39	132.13
430	43.00	157.50	3.41	3.41	15.79	131.61
431	43.10	141.29	3.29	3.29	17.53	131.08
432	43.20	125.70	3.18	3.18	19.72	130.71

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
433	43.30	113.88	3.28	3.28	22.40	130.68
434	43.40	104.92	3.57	3.57	25.54	130.98
435	43.50	96.55	3.92	3.92	28.57	131.22
436	43.60	89.34	3.94	3.94	30.91	130.72
437	43.70	77.67	3.18	3.18	31.27	129.73
438	43.80	79.25	2.75	2.75	29.06	128.74
439	43.90	91.29	2.66	2.66	25.45	128.50
440	44.00	104.05	2.63	2.63	22.25	128.66
441	44.10	114.13	2.61	2.61	20.19	128.75
442	44.20	117.55	2.54	2.54	19.46	128.99
443	44.30	118.63	2.78	2.78	20.57	129.67
444	44.40	113.54	3.38	3.38	23.32	130.60
445	44.50	102.81	3.86	3.86	26.83	131.11
446	44.60	91.24	3.80	3.80	29.42	130.81
447	44.70	85.19	3.29	3.29	29.13	130.03
448	44.80	92.79	2.88	2.88	25.57	129.41
449	44.90	112.45	2.76	2.76	21.11	129.40
450	45.00	133.95	2.84	2.84	17.96	129.99
451	45.10	150.30	3.12	3.12	16.60	130.87
452	45.20	157.91	3.52	3.52	16.52	131.67
453	45.30	157.87	3.76	3.76	17.11	132.16
454	45.40	152.89	3.82	3.82	18.08	132.30
455	45.50	143.70	3.84	3.84	19.53	132.21
456	45.60	130.56	3.85	3.85	21.82	132.09
457	45.70	115.53	3.98	3.98	24.98	131.94
458	45.80	100.63	4.07	4.07	28.47	131.61
459	45.90	88.36	3.83	3.83	31.26	130.84
460	46.00	79.14	3.26	3.26	32.45	129.58
461	46.10	73.45	2.64	2.64	31.70	128.15
462	46.20	74.28	2.26	2.26	29.33	126.98
463	46.30	80.05	2.05	2.05	25.82	126.39
464	46.40	91.55	1.94	1.94	21.76	126.28
465	46.50	109.27	1.90	1.90	17.79	126.53
466	46.60	130.77	1.93	1.93	15.07	127.27
467	46.70	148.04	2.23	2.23	14.30	128.53
468	46.80	153.23	2.79	2.79	15.28	129.97
469	46.90	148.15	3.32	3.32	17.36	131.18
470	47.00	140.81	3.78	3.78	19.70	132.11
471	47.10	137.41	4.26	4.26	21.50	132.72
472	47.20	135.96	4.43	4.43	22.28	132.94
473	47.30	135.33	4.23	4.23	21.86	132.80
474	47.40	140.26	3.98	3.98	20.40	132.54
475	47.50	151.98	3.84	3.84	18.46	132.45
476	47.60	166.12	3.80	3.80	16.78	132.65
477	47.70	179.12	3.99	3.99	15.75	133.07
478	47.80	188.27	4.24	4.24	15.32	133.57
479	47.90	193.48	4.44	4.44	15.10	133.89
480	48.00	196.13	4.43	4.43	14.88	134.02

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
481	48.10	198.96	4.39	4.39	14.56	134.01
482	48.20	202.27	4.36	4.36	14.25	134.03
483	48.30	205.66	4.39	4.39	14.06	134.08
484	48.40	206.79	4.43	4.43	14.12	134.20
485	48.50	205.41	4.55	4.55	14.44	134.35
486	48.60	202.79	4.68	4.68	14.86	134.46
487	48.70	199.77	4.69	4.69	15.15	134.50
488	48.80	199.67	4.68	4.68	15.19	134.49
489	48.90	201.72	4.67	4.67	14.99	134.48
490	49.00	204.99	4.63	4.63	14.71	134.50
491	49.10	208.60	4.65	4.65	14.44	134.58
492	49.20	212.60	4.74	4.74	14.25	134.73
493	49.30	216.89	4.83	4.83	14.04	134.91
494	49.40	222.43	4.90	4.90	13.86	135.08
495	49.50	225.67	4.98	4.98	13.86	135.10
496	49.60	218.36	4.87	4.87	14.13	134.86
497	49.70	204.49	4.56	4.56	14.47	134.51
498	49.80	202.28	4.48	4.48	14.70	134.37
499	49.90	206.77	4.68	4.68	14.74	134.44

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q _c :	Measured cone resistance (tsf)
f _s :	Sleeve friction resistance (tsf)
u:	Pore pressure (tsf)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (pcf)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1	0.10	0.01	0.00	0.01	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
2	0.20	0.01	0.00	0.01	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
3	0.30	0.01	0.00	0.01	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
4	0.40	0.02	0.00	0.02	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
5	0.50	0.02	0.00	0.02	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
6	0.60	0.03	0.00	0.03	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
7	0.70	0.04	0.00	0.04	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
8	0.80	0.04	0.00	0.04	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
9	0.90	0.05	0.00	0.05	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
10	1.00	0.05	0.00	0.05	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
11	1.10	0.06	0.00	0.06	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
12	1.20	0.07	0.00	0.07	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
13	1.30	0.07	0.00	0.07	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
14	1.40	0.08	0.00	0.08	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
15	1.50	0.08	0.00	0.08	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
16	1.60	0.09	0.00	0.09	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
17	1.70	0.10	0.00	0.10	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
18	1.80	0.10	0.00	0.10	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
19	1.90	0.11	0.00	0.11	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
20	2.00	0.11	0.00	0.11	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
21	2.10	0.12	0.00	0.12	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
22	2.20	0.13	0.00	0.13	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
23	2.30	0.13	0.00	0.13	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
24	2.40	0.14	0.00	0.14	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
25	2.50	0.15	0.00	0.15	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
26	2.60	0.15	0.00	0.15	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
27	2.70	0.16	0.00	0.16	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
28	2.80	0.16	0.00	0.16	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
29	2.90	0.17	0.00	0.17	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
30	3.00	0.17	0.00	0.17	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
31	3.10	0.18	0.00	0.18	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
32	3.20	0.19	0.00	0.19	1.00	0.480	1.04	0.460	1.10	1.30	2.000	Yes
33	3.30	0.19	0.00	0.19	1.00	0.480	1.04	0.460	1.10	1.30	2.000	Yes
34	3.40	0.20	0.00	0.20	1.00	0.480	1.04	0.460	1.10	1.30	2.000	Yes
35	3.50	0.20	0.00	0.20	1.00	0.480	1.04	0.460	1.10	1.30	2.000	Yes
36	3.60	0.21	0.00	0.21	1.00	0.480	1.04	0.460	1.10	1.30	2.000	Yes
37	3.70	0.22	0.00	0.22	1.00	0.480	1.04	0.460	1.10	1.30	2.000	Yes
38	3.80	0.22	0.00	0.22	1.00	0.480	1.04	0.460	1.10	1.30	2.000	Yes
39	3.90	0.23	0.00	0.23	1.00	0.480	1.04	0.460	1.10	1.30	2.000	Yes
40	4.00	0.23	0.00	0.23	1.00	0.479	1.04	0.460	1.10	1.30	2.000	No
41	4.10	0.24	0.00	0.24	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
42	4.20	0.24	0.00	0.24	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
43	4.30	0.25	0.00	0.25	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
44	4.40	0.25	0.00	0.25	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
45	4.50	0.26	0.00	0.26	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
46	4.60	0.26	0.00	0.26	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
47	4.70	0.27	0.00	0.27	0.99	0.479	1.04	0.459	1.10	1.30	2.000	No
48	4.80	0.27	0.00	0.27	0.99	0.478	1.04	0.459	1.10	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
49	4.90	0.28	0.00	0.28	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
50	5.00	0.28	0.00	0.28	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
51	5.10	0.29	0.00	0.29	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
52	5.20	0.29	0.00	0.29	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
53	5.30	0.30	0.00	0.30	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
54	5.40	0.30	0.00	0.30	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
55	5.50	0.31	0.00	0.31	0.99	0.477	1.04	0.458	1.10	1.30	2.000	Yes
56	5.60	0.31	0.00	0.31	0.99	0.477	1.04	0.458	1.10	1.30	2.000	Yes
57	5.70	0.32	0.00	0.32	0.99	0.477	1.04	0.457	1.10	1.30	2.000	Yes
58	5.80	0.33	0.00	0.33	0.99	0.477	1.04	0.457	1.10	1.30	2.000	Yes
59	5.90	0.33	0.00	0.33	0.99	0.477	1.04	0.457	1.10	1.30	2.000	Yes
60	6.00	0.34	0.00	0.34	0.99	0.477	1.04	0.457	1.10	1.30	2.000	Yes
61	6.10	0.34	0.00	0.34	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
62	6.20	0.35	0.00	0.35	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
63	6.30	0.35	0.00	0.35	0.99	0.476	1.04	0.457	1.10	1.30	2.000	No
64	6.40	0.36	0.00	0.36	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
65	6.50	0.37	0.00	0.37	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
66	6.60	0.37	0.00	0.37	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
67	6.70	0.38	0.00	0.38	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
68	6.80	0.38	0.00	0.38	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
69	6.90	0.39	0.00	0.39	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
70	7.00	0.40	0.00	0.40	0.99	0.475	1.04	0.456	1.10	1.30	2.000	No
71	7.10	0.40	0.00	0.40	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
72	7.20	0.41	0.00	0.41	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
73	7.30	0.41	0.00	0.41	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
74	7.40	0.42	0.00	0.42	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
75	7.50	0.42	0.00	0.42	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
76	7.60	0.43	0.00	0.43	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
77	7.70	0.44	0.00	0.44	0.99	0.474	1.04	0.455	1.10	1.30	2.000	No
78	7.80	0.44	0.00	0.44	0.99	0.474	1.04	0.455	1.10	1.30	2.000	No
79	7.90	0.45	0.00	0.45	0.99	0.474	1.04	0.454	1.10	1.30	2.000	No
80	8.00	0.45	0.00	0.45	0.99	0.474	1.04	0.454	1.10	1.30	2.000	No
81	8.10	0.46	0.00	0.46	0.98	0.477	1.04	0.457	1.10	1.30	2.000	Yes
82	8.20	0.47	0.01	0.46	0.98	0.480	1.04	0.460	1.10	1.30	2.000	Yes
83	8.30	0.47	0.01	0.46	0.98	0.483	1.04	0.463	1.10	1.30	2.000	Yes
84	8.40	0.48	0.01	0.46	0.98	0.486	1.04	0.466	1.10	1.30	2.000	Yes
85	8.50	0.48	0.02	0.47	0.98	0.489	1.04	0.469	1.10	1.30	2.000	Yes
86	8.60	0.49	0.02	0.47	0.98	0.492	1.04	0.471	1.09	1.30	2.000	Yes
87	8.70	0.50	0.02	0.47	0.98	0.495	1.04	0.474	1.08	1.30	2.000	Yes
88	8.80	0.50	0.02	0.48	0.98	0.497	1.04	0.477	1.08	1.30	2.000	Yes
89	8.90	0.51	0.03	0.48	0.98	0.500	1.04	0.479	1.07	1.30	2.000	Yes
90	9.00	0.51	0.03	0.48	0.98	0.503	1.04	0.482	1.07	1.30	0.608	No
91	9.10	0.52	0.03	0.48	0.98	0.506	1.04	0.485	1.06	1.30	0.613	No
92	9.20	0.52	0.04	0.49	0.98	0.508	1.04	0.487	1.06	1.30	0.617	No
93	9.30	0.53	0.04	0.49	0.98	0.511	1.04	0.490	1.06	1.30	0.621	No
94	9.40	0.53	0.04	0.49	0.98	0.514	1.04	0.492	1.06	1.30	0.623	No
95	9.50	0.54	0.05	0.49	0.98	0.516	1.04	0.495	1.06	1.30	0.626	No
96	9.60	0.55	0.05	0.50	0.98	0.519	1.04	0.497	1.06	1.30	0.630	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
97	9.70	0.55	0.05	0.50	0.98	0.522	1.04	0.500	1.06	1.30	0.634	No
98	9.80	0.56	0.06	0.50	0.98	0.524	1.04	0.502	1.06	1.30	0.638	No
99	9.90	0.56	0.06	0.50	0.98	0.527	1.04	0.505	1.07	1.30	0.636	No
100	10.00	0.57	0.06	0.51	0.98	0.529	1.04	0.507	1.07	1.30	0.632	No
101	10.10	0.57	0.07	0.51	0.98	0.531	1.04	0.509	1.07	1.30	0.636	No
102	10.20	0.58	0.07	0.51	0.98	0.534	1.04	0.512	1.06	1.30	0.646	No
103	10.30	0.59	0.07	0.51	0.98	0.536	1.04	0.514	1.06	1.30	0.651	No
104	10.40	0.59	0.07	0.52	0.98	0.538	1.04	0.516	1.06	1.30	0.653	No
105	10.50	0.60	0.08	0.52	0.98	0.541	1.04	0.518	1.06	1.30	0.656	No
106	10.60	0.60	0.08	0.52	0.98	0.543	1.04	0.520	1.06	1.30	2.000	Yes
107	10.70	0.61	0.08	0.52	0.98	0.545	1.04	0.523	1.07	1.30	2.000	Yes
108	10.80	0.61	0.09	0.53	0.98	0.547	1.04	0.525	1.07	1.30	2.000	Yes
109	10.90	0.62	0.09	0.53	0.98	0.550	1.04	0.527	1.08	1.30	2.000	Yes
110	11.00	0.63	0.09	0.53	0.98	0.552	1.04	0.529	1.10	1.30	2.000	Yes
111	11.10	0.63	0.10	0.54	0.98	0.554	1.04	0.531	1.10	1.30	2.000	Yes
112	11.20	0.64	0.10	0.54	0.97	0.556	1.04	0.533	1.10	1.30	2.000	Yes
113	11.30	0.65	0.10	0.54	0.97	0.558	1.04	0.535	1.10	1.30	2.000	Yes
114	11.40	0.65	0.11	0.55	0.97	0.560	1.04	0.536	1.10	1.30	0.642	No
115	11.50	0.66	0.11	0.55	0.97	0.562	1.04	0.538	1.10	1.30	0.645	No
116	11.60	0.66	0.11	0.55	0.97	0.564	1.04	0.540	1.10	1.30	0.647	No
117	11.70	0.67	0.12	0.55	0.97	0.566	1.04	0.542	1.10	1.30	0.649	No
118	11.80	0.68	0.12	0.56	0.97	0.567	1.04	0.544	1.10	1.30	0.653	No
119	11.90	0.68	0.12	0.56	0.97	0.569	1.04	0.546	1.09	1.30	0.662	No
120	12.00	0.69	0.12	0.56	0.97	0.571	1.04	0.547	1.09	1.30	0.667	No
121	12.10	0.69	0.13	0.57	0.97	0.573	1.04	0.549	1.08	1.30	0.674	No
122	12.20	0.70	0.13	0.57	0.97	0.575	1.04	0.551	1.08	1.30	0.681	No
123	12.30	0.71	0.13	0.57	0.97	0.577	1.04	0.553	1.08	1.30	0.679	No
124	12.40	0.71	0.14	0.58	0.97	0.578	1.04	0.554	1.08	1.30	0.681	No
125	12.50	0.72	0.14	0.58	0.97	0.580	1.04	0.556	1.08	1.30	0.684	No
126	12.60	0.72	0.14	0.58	0.97	0.582	1.04	0.558	1.08	1.30	0.686	No
127	12.70	0.73	0.15	0.58	0.97	0.584	1.04	0.559	1.08	1.30	2.000	Yes
128	12.80	0.74	0.15	0.59	0.97	0.585	1.04	0.561	1.08	1.30	2.000	Yes
129	12.90	0.74	0.15	0.59	0.97	0.587	1.04	0.563	1.07	1.30	2.000	Yes
130	13.00	0.75	0.16	0.59	0.97	0.589	1.04	0.564	1.06	1.30	2.000	Yes
131	13.10	0.75	0.16	0.60	0.97	0.590	1.04	0.566	1.06	1.30	2.000	Yes
132	13.20	0.76	0.16	0.60	0.97	0.592	1.04	0.567	1.06	1.30	2.000	Yes
133	13.30	0.77	0.17	0.60	0.97	0.593	1.04	0.569	1.05	1.30	2.000	Yes
134	13.40	0.77	0.17	0.60	0.97	0.595	1.04	0.570	1.05	1.30	2.000	Yes
135	13.50	0.78	0.17	0.61	0.97	0.597	1.04	0.572	1.05	1.30	0.729	No
136	13.60	0.78	0.17	0.61	0.97	0.598	1.04	0.573	1.05	1.30	0.731	No
137	13.70	0.79	0.18	0.61	0.97	0.600	1.04	0.575	1.05	1.30	0.734	No
138	13.80	0.80	0.18	0.61	0.97	0.601	1.04	0.576	1.05	1.30	0.737	No
139	13.90	0.80	0.18	0.62	0.97	0.603	1.04	0.578	1.05	1.30	0.739	No
140	14.00	0.81	0.19	0.62	0.97	0.604	1.04	0.579	1.05	1.30	0.742	No
141	14.10	0.81	0.19	0.62	0.96	0.606	1.04	0.581	1.05	1.30	0.745	No
142	14.20	0.82	0.19	0.63	0.96	0.607	1.04	0.582	1.05	1.30	0.748	No
143	14.30	0.82	0.20	0.63	0.96	0.609	1.04	0.584	1.05	1.30	0.750	No
144	14.40	0.83	0.20	0.63	0.96	0.610	1.04	0.585	1.04	1.30	0.756	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
145	14.50	0.84	0.20	0.63	0.96	0.612	1.04	0.587	1.04	1.30	0.761	No
146	14.60	0.84	0.21	0.63	0.96	0.614	1.04	0.588	1.04	1.30	0.763	No
147	14.70	0.84	0.21	0.64	0.96	0.615	1.04	0.590	1.04	1.30	0.765	No
148	14.80	0.85	0.21	0.64	0.96	0.617	1.04	0.591	1.04	1.30	0.767	No
149	14.90	0.85	0.22	0.64	0.96	0.618	1.04	0.593	1.04	1.30	0.769	No
150	15.00	0.86	0.22	0.64	0.96	0.620	1.04	0.594	1.04	1.30	0.772	No
151	15.10	0.86	0.22	0.64	0.96	0.622	1.04	0.596	1.04	1.30	0.774	No
152	15.20	0.87	0.22	0.64	0.96	0.623	1.04	0.598	1.04	1.30	0.776	No
153	15.30	0.87	0.23	0.64	0.96	0.625	1.04	0.599	1.04	1.30	0.779	No
154	15.40	0.88	0.23	0.65	0.96	0.627	1.04	0.601	1.04	1.30	0.781	No
155	15.50	0.88	0.23	0.65	0.96	0.628	1.04	0.602	1.04	1.30	0.783	No
156	15.60	0.89	0.24	0.65	0.96	0.630	1.04	0.604	1.04	1.30	0.784	No
157	15.70	0.89	0.24	0.65	0.96	0.631	1.04	0.605	1.04	1.30	0.784	No
158	15.80	0.90	0.24	0.65	0.96	0.632	1.04	0.606	1.04	1.30	0.783	No
159	15.90	0.90	0.25	0.66	0.96	0.634	1.04	0.607	1.04	1.30	0.784	No
160	16.00	0.91	0.25	0.66	0.96	0.635	1.04	0.609	1.04	1.30	0.787	No
161	16.10	0.91	0.25	0.66	0.96	0.636	1.04	0.610	1.04	1.30	0.790	No
162	16.20	0.92	0.26	0.66	0.96	0.638	1.04	0.611	1.04	1.30	0.793	No
163	16.30	0.93	0.26	0.67	0.96	0.639	1.04	0.612	1.04	1.30	0.795	No
164	16.40	0.93	0.26	0.67	0.96	0.640	1.04	0.614	1.04	1.30	0.797	No
165	16.50	0.94	0.27	0.67	0.96	0.642	1.04	0.615	1.04	1.30	0.799	No
166	16.60	0.94	0.27	0.67	0.96	0.643	1.04	0.616	1.04	1.30	0.801	No
167	16.70	0.95	0.27	0.67	0.96	0.644	1.04	0.618	1.04	1.30	0.804	No
168	16.80	0.95	0.27	0.68	0.95	0.646	1.04	0.619	1.03	1.30	0.806	No
169	16.90	0.96	0.28	0.68	0.95	0.647	1.04	0.620	1.03	1.30	0.808	No
170	17.00	0.96	0.28	0.68	0.95	0.648	1.04	0.621	1.03	1.30	0.810	No
171	17.10	0.97	0.28	0.68	0.95	0.650	1.04	0.623	1.03	1.30	0.812	No
172	17.20	0.97	0.29	0.68	0.95	0.651	1.04	0.624	1.03	1.30	0.813	No
173	17.30	0.98	0.29	0.68	0.95	0.652	1.04	0.625	1.03	1.30	0.815	No
174	17.40	0.98	0.29	0.69	0.95	0.654	1.04	0.627	1.03	1.30	0.817	No
175	17.50	0.98	0.30	0.69	0.95	0.655	1.04	0.628	1.03	1.30	0.819	No
176	17.60	0.99	0.30	0.69	0.95	0.656	1.04	0.629	1.03	1.30	0.820	No
177	17.70	1.00	0.30	0.69	0.95	0.657	1.04	0.630	1.03	1.30	0.820	No
178	17.80	1.00	0.31	0.69	0.95	0.659	1.04	0.631	1.03	1.30	0.822	No
179	17.90	1.01	0.31	0.70	0.95	0.660	1.04	0.632	1.03	1.30	0.824	No
180	18.00	1.01	0.31	0.70	0.95	0.661	1.04	0.634	1.03	1.30	0.827	No
181	18.10	1.02	0.32	0.70	0.95	0.662	1.04	0.635	1.03	1.30	0.829	No
182	18.20	1.02	0.32	0.70	0.95	0.663	1.04	0.636	1.03	1.30	0.830	No
183	18.30	1.03	0.32	0.70	0.95	0.665	1.04	0.637	1.03	1.30	0.831	No
184	18.40	1.03	0.32	0.71	0.95	0.666	1.04	0.638	1.03	1.30	0.829	No
185	18.50	1.04	0.33	0.71	0.95	0.666	1.04	0.639	1.04	1.30	0.827	No
186	18.60	1.04	0.33	0.71	0.95	0.667	1.04	0.640	1.04	1.30	0.827	No
187	18.70	1.05	0.33	0.72	0.95	0.668	1.04	0.640	1.04	1.30	0.831	No
188	18.80	1.06	0.34	0.72	0.95	0.669	1.04	0.641	1.03	1.30	0.833	No
189	18.90	1.06	0.34	0.72	0.95	0.670	1.04	0.642	1.04	1.30	0.833	No
190	19.00	1.07	0.34	0.72	0.95	0.671	1.04	0.643	1.04	1.30	0.834	No
191	19.10	1.07	0.35	0.73	0.95	0.672	1.04	0.644	1.04	1.30	0.834	No
192	19.20	1.08	0.35	0.73	0.95	0.673	1.04	0.645	1.04	1.30	0.833	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
193	19.30	1.08	0.35	0.73	0.94	0.673	1.04	0.645	1.04	1.30	0.832	No
194	19.40	1.09	0.36	0.73	0.94	0.674	1.04	0.646	1.04	1.30	0.832	No
195	19.50	1.10	0.36	0.74	0.94	0.675	1.04	0.647	1.04	1.30	0.833	No
196	19.60	1.10	0.36	0.74	0.94	0.676	1.04	0.648	1.04	1.30	0.837	No
197	19.70	1.11	0.37	0.74	0.94	0.676	1.04	0.648	1.03	1.30	0.841	No
198	19.80	1.11	0.37	0.75	0.94	0.677	1.04	0.649	1.03	1.30	2.000	Yes
199	19.90	1.12	0.37	0.75	0.94	0.678	1.04	0.650	1.04	1.30	2.000	Yes
200	20.00	1.13	0.37	0.75	0.94	0.679	1.04	0.650	1.04	1.30	2.000	Yes
201	20.10	1.13	0.38	0.76	0.94	0.679	1.04	0.651	1.04	1.30	2.000	Yes
202	20.20	1.14	0.38	0.76	0.94	0.680	1.04	0.652	1.04	1.30	2.000	Yes
203	20.30	1.15	0.38	0.76	0.94	0.681	1.04	0.652	1.04	1.30	2.000	Yes
204	20.40	1.15	0.39	0.76	0.94	0.681	1.04	0.653	1.04	1.30	2.000	Yes
205	20.50	1.16	0.39	0.77	0.94	0.682	1.04	0.654	1.04	1.30	2.000	Yes
206	20.60	1.16	0.39	0.77	0.94	0.683	1.04	0.654	1.03	1.30	2.000	Yes
207	20.70	1.17	0.40	0.77	0.94	0.683	1.04	0.655	1.03	1.30	2.000	Yes
208	20.80	1.18	0.40	0.78	0.94	0.684	1.04	0.656	1.03	1.30	2.000	Yes
209	20.90	1.18	0.40	0.78	0.94	0.685	1.04	0.656	1.03	1.30	2.000	Yes
210	21.00	1.19	0.41	0.78	0.94	0.685	1.04	0.657	1.03	1.30	2.000	Yes
211	21.10	1.19	0.41	0.78	0.94	0.686	1.04	0.657	1.03	1.30	2.000	Yes
212	21.20	1.20	0.41	0.79	0.94	0.686	1.04	0.658	1.03	1.30	2.000	Yes
213	21.30	1.21	0.41	0.79	0.94	0.687	1.04	0.659	1.03	1.30	0.862	No
214	21.40	1.21	0.42	0.79	0.94	0.688	1.04	0.659	1.03	1.30	0.864	No
215	21.50	1.22	0.42	0.80	0.94	0.688	1.04	0.660	1.03	1.30	0.865	No
216	21.60	1.22	0.42	0.80	0.94	0.689	1.04	0.660	1.02	1.30	0.866	No
217	21.70	1.23	0.43	0.80	0.93	0.690	1.04	0.661	1.02	1.30	0.867	No
218	21.80	1.23	0.43	0.80	0.93	0.690	1.04	0.662	1.02	1.30	0.869	No
219	21.90	1.24	0.43	0.81	0.93	0.691	1.04	0.662	1.02	1.30	0.870	No
220	22.00	1.25	0.44	0.81	0.93	0.692	1.04	0.663	1.02	1.30	0.870	No
221	22.10	1.25	0.44	0.81	0.93	0.692	1.04	0.663	1.02	1.30	0.871	No
222	22.20	1.26	0.44	0.81	0.93	0.693	1.04	0.664	1.02	1.30	0.872	No
223	22.30	1.26	0.45	0.82	0.93	0.693	1.04	0.664	1.02	1.30	0.873	No
224	22.40	1.27	0.45	0.82	0.93	0.694	1.04	0.665	1.02	1.30	0.873	No
225	22.50	1.28	0.45	0.82	0.93	0.694	1.04	0.666	1.02	1.30	0.873	No
226	22.60	1.28	0.46	0.83	0.93	0.695	1.04	0.666	1.02	1.30	0.874	No
227	22.70	1.29	0.46	0.83	0.93	0.695	1.04	0.667	1.02	1.30	0.874	No
228	22.80	1.29	0.46	0.83	0.93	0.696	1.04	0.667	1.02	1.30	0.875	No
229	22.90	1.30	0.46	0.83	0.93	0.697	1.04	0.668	1.02	1.30	0.876	No
230	23.00	1.31	0.47	0.84	0.93	0.697	1.04	0.668	1.02	1.30	0.876	No
231	23.10	1.31	0.47	0.84	0.93	0.698	1.04	0.669	1.02	1.30	0.877	No
232	23.20	1.32	0.47	0.84	0.93	0.698	1.04	0.669	1.02	1.30	0.877	No
233	23.30	1.32	0.48	0.85	0.93	0.698	1.04	0.669	1.02	1.30	0.877	No
234	23.40	1.33	0.48	0.85	0.93	0.699	1.04	0.670	1.02	1.30	0.879	No
235	23.50	1.34	0.48	0.85	0.93	0.699	1.04	0.670	1.02	1.30	0.882	No
236	23.60	1.34	0.49	0.85	0.93	0.700	1.04	0.671	1.02	1.30	0.884	No
237	23.70	1.35	0.49	0.86	0.93	0.700	1.04	0.671	1.02	1.30	0.885	No
238	23.80	1.35	0.49	0.86	0.93	0.701	1.04	0.672	1.02	1.30	0.887	No
239	23.90	1.36	0.50	0.86	0.93	0.701	1.04	0.672	1.02	1.30	0.888	No
240	24.00	1.36	0.50	0.86	0.93	0.702	1.04	0.673	1.02	1.30	0.889	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
241	24.10	1.37	0.50	0.87	0.92	0.702	1.04	0.673	1.02	1.30	0.890	No
242	24.20	1.38	0.51	0.87	0.92	0.703	1.04	0.674	1.02	1.30	0.892	No
243	24.30	1.38	0.51	0.87	0.92	0.703	1.04	0.674	1.02	1.30	0.894	No
244	24.40	1.39	0.51	0.87	0.92	0.704	1.04	0.675	1.01	1.30	0.896	No
245	24.50	1.39	0.51	0.88	0.92	0.705	1.04	0.675	1.01	1.30	0.896	No
246	24.60	1.40	0.52	0.88	0.92	0.705	1.04	0.676	1.01	1.30	0.897	No
247	24.70	1.40	0.52	0.88	0.92	0.706	1.04	0.677	1.01	1.30	0.898	No
248	24.80	1.41	0.52	0.88	0.92	0.707	1.04	0.677	1.01	1.30	0.899	No
249	24.90	1.41	0.53	0.89	0.92	0.707	1.04	0.678	1.01	1.30	0.900	No
250	25.00	1.42	0.53	0.89	0.92	0.708	1.04	0.678	1.01	1.30	0.901	No
251	25.10	1.42	0.53	0.89	0.92	0.708	1.04	0.679	1.01	1.30	0.902	No
252	25.20	1.43	0.54	0.89	0.92	0.709	1.04	0.679	1.01	1.30	0.902	No
253	25.30	1.43	0.54	0.89	0.92	0.709	1.04	0.680	1.01	1.30	0.904	No
254	25.40	1.44	0.54	0.90	0.92	0.710	1.04	0.680	1.01	1.30	0.905	No
255	25.50	1.44	0.55	0.90	0.92	0.710	1.04	0.681	1.01	1.30	0.905	No
256	25.60	1.45	0.55	0.90	0.92	0.711	1.04	0.681	1.01	1.30	0.906	No
257	25.70	1.46	0.55	0.90	0.92	0.711	1.04	0.682	1.01	1.30	0.907	No
258	25.80	1.46	0.56	0.91	0.92	0.712	1.04	0.682	1.01	1.30	0.908	No
259	25.90	1.47	0.56	0.91	0.92	0.713	1.04	0.683	1.01	1.30	0.909	No
260	26.00	1.47	0.56	0.91	0.92	0.713	1.04	0.683	1.01	1.30	0.910	No
261	26.10	1.48	0.56	0.91	0.92	0.714	1.04	0.684	1.01	1.30	0.910	No
262	26.20	1.48	0.57	0.91	0.92	0.714	1.04	0.684	1.01	1.30	0.911	No
263	26.30	1.49	0.57	0.92	0.92	0.715	1.04	0.685	1.01	1.30	0.912	No
264	26.40	1.49	0.57	0.92	0.91	0.715	1.04	0.685	1.01	1.30	0.913	No
265	26.50	1.50	0.58	0.92	0.91	0.716	1.04	0.686	1.01	1.30	0.914	No
266	26.60	1.50	0.58	0.92	0.91	0.716	1.04	0.686	1.01	1.30	0.914	No
267	26.70	1.51	0.58	0.92	0.91	0.717	1.04	0.687	1.01	1.30	0.915	No
268	26.80	1.51	0.59	0.93	0.91	0.717	1.04	0.687	1.01	1.30	0.916	No
269	26.90	1.52	0.59	0.93	0.91	0.717	1.04	0.688	1.01	1.30	0.916	No
270	27.00	1.52	0.59	0.93	0.91	0.718	1.04	0.688	1.01	1.30	0.917	No
271	27.10	1.53	0.60	0.93	0.91	0.718	1.04	0.688	1.01	1.30	0.918	No
272	27.20	1.54	0.60	0.94	0.91	0.719	1.04	0.689	1.01	1.30	0.918	No
273	27.30	1.54	0.60	0.94	0.91	0.719	1.04	0.689	1.01	1.30	0.918	No
274	27.40	1.55	0.61	0.94	0.91	0.719	1.04	0.689	1.01	1.30	0.917	No
275	27.50	1.55	0.61	0.94	0.91	0.719	1.04	0.689	1.01	1.30	0.914	No
276	27.60	1.56	0.61	0.95	0.91	0.720	1.04	0.690	1.01	1.30	0.910	No
277	27.70	1.57	0.61	0.95	0.91	0.720	1.04	0.690	1.01	1.30	0.906	No
278	27.80	1.57	0.62	0.95	0.91	0.720	1.04	0.690	1.01	1.30	0.906	No
279	27.90	1.58	0.62	0.96	0.91	0.720	1.04	0.690	1.01	1.30	0.910	No
280	28.00	1.58	0.62	0.96	0.91	0.720	1.04	0.690	1.01	1.30	0.914	No
281	28.10	1.59	0.63	0.96	0.91	0.720	1.04	0.690	1.01	1.30	0.917	No
282	28.20	1.60	0.63	0.97	0.91	0.721	1.04	0.691	1.01	1.30	0.919	No
283	28.30	1.60	0.63	0.97	0.91	0.721	1.04	0.691	1.01	1.30	0.921	No
284	28.40	1.61	0.64	0.97	0.91	0.721	1.04	0.691	1.01	1.30	0.923	No
285	28.50	1.61	0.64	0.97	0.91	0.721	1.04	0.691	1.01	1.30	0.924	No
286	28.60	1.62	0.64	0.98	0.90	0.722	1.04	0.692	1.01	1.30	0.925	No
287	28.70	1.63	0.65	0.98	0.90	0.722	1.04	0.692	1.01	1.30	0.924	No
288	28.80	1.63	0.65	0.98	0.90	0.722	1.04	0.692	1.01	1.30	0.923	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
289	28.90	1.64	0.65	0.99	0.90	0.722	1.04	0.692	1.01	1.30	0.923	No
290	29.00	1.64	0.66	0.99	0.90	0.722	1.04	0.692	1.01	1.30	0.924	No
291	29.10	1.65	0.66	0.99	0.90	0.722	1.04	0.692	1.01	1.30	0.925	No
292	29.20	1.66	0.66	0.99	0.90	0.723	1.04	0.693	1.01	1.30	0.926	No
293	29.30	1.66	0.66	1.00	0.90	0.723	1.04	0.693	1.01	1.30	0.927	No
294	29.40	1.67	0.67	1.00	0.90	0.723	1.04	0.693	1.01	1.30	0.927	No
295	29.50	1.67	0.67	1.00	0.90	0.723	1.04	0.693	1.01	1.30	0.925	No
296	29.60	1.68	0.67	1.00	0.90	0.723	1.04	0.693	1.01	1.30	0.923	No
297	29.70	1.68	0.68	1.01	0.90	0.723	1.04	0.693	1.01	1.30	0.923	No
298	29.80	1.69	0.68	1.01	0.90	0.724	1.04	0.694	1.00	1.30	0.924	No
299	29.90	1.70	0.68	1.01	0.90	0.724	1.04	0.694	1.00	1.30	2.000	Yes
300	30.00	1.70	0.69	1.02	0.90	0.724	1.04	0.694	1.01	1.30	2.000	Yes
301	30.10	1.71	0.69	1.02	0.90	0.724	1.04	0.694	1.01	1.30	2.000	Yes
302	30.20	1.72	0.69	1.02	0.90	0.724	1.04	0.694	1.01	1.30	2.000	Yes
303	30.30	1.72	0.70	1.03	0.90	0.724	1.04	0.694	1.01	1.30	2.000	Yes
304	30.40	1.73	0.70	1.03	0.90	0.724	1.04	0.694	1.00	1.30	2.000	Yes
305	30.50	1.74	0.70	1.03	0.90	0.724	1.04	0.694	1.00	1.30	2.000	Yes
306	30.60	1.74	0.71	1.04	0.90	0.724	1.04	0.694	1.00	1.30	2.000	Yes
307	30.70	1.75	0.71	1.04	0.90	0.724	1.04	0.694	1.00	1.30	2.000	Yes
308	30.80	1.76	0.71	1.04	0.89	0.724	1.04	0.694	1.00	1.30	2.000	Yes
309	30.90	1.76	0.71	1.05	0.89	0.724	1.04	0.693	1.00	1.30	2.000	Yes
310	31.00	1.77	0.72	1.05	0.89	0.724	1.04	0.694	1.00	1.30	2.000	Yes
311	31.10	1.77	0.72	1.05	0.89	0.724	1.04	0.694	1.00	1.30	2.000	Yes
312	31.20	1.78	0.72	1.06	0.89	0.724	1.04	0.694	1.00	1.30	2.000	Yes
313	31.30	1.79	0.73	1.06	0.89	0.724	1.04	0.694	1.00	1.30	2.000	Yes
314	31.40	1.79	0.73	1.06	0.89	0.724	1.04	0.694	1.00	1.30	2.000	Yes
315	31.50	1.80	0.73	1.07	0.89	0.724	1.04	0.694	1.00	1.30	0.910	No
316	31.60	1.81	0.74	1.07	0.89	0.724	1.04	0.694	1.00	1.30	0.910	No
317	31.70	1.81	0.74	1.07	0.89	0.724	1.04	0.694	1.00	1.30	0.912	No
318	31.80	1.82	0.74	1.08	0.89	0.724	1.04	0.694	1.00	1.30	2.000	Yes
319	31.90	1.82	0.75	1.08	0.89	0.724	1.04	0.694	1.00	1.30	2.000	Yes
320	32.00	1.83	0.75	1.08	0.89	0.724	1.04	0.694	1.00	1.30	2.000	Yes
321	32.10	1.84	0.75	1.09	0.89	0.724	1.04	0.694	1.00	1.30	2.000	Yes
322	32.20	1.84	0.76	1.09	0.89	0.724	1.04	0.693	1.00	1.30	2.000	Yes
323	32.30	1.85	0.76	1.09	0.89	0.724	1.04	0.693	1.00	1.30	2.000	Yes
324	32.40	1.86	0.76	1.09	0.89	0.723	1.04	0.693	1.00	1.30	2.000	Yes
325	32.50	1.86	0.76	1.10	0.89	0.723	1.04	0.693	1.00	1.30	0.927	No
326	32.60	1.87	0.77	1.10	0.89	0.723	1.04	0.693	1.00	1.30	0.926	No
327	32.70	1.87	0.77	1.10	0.89	0.723	1.04	0.693	0.99	1.30	0.922	No
328	32.80	1.88	0.77	1.11	0.89	0.723	1.04	0.693	0.99	1.30	0.919	No
329	32.90	1.89	0.78	1.11	0.88	0.723	1.04	0.693	0.99	1.30	0.916	No
330	33.00	1.89	0.78	1.11	0.88	0.723	1.04	0.693	0.99	1.30	0.915	No
331	33.10	1.90	0.78	1.12	0.88	0.723	1.04	0.693	0.99	1.30	0.913	No
332	33.20	1.91	0.79	1.12	0.88	0.723	1.04	0.693	0.99	1.30	0.908	No
333	33.30	1.91	0.79	1.12	0.88	0.723	1.04	0.693	0.99	1.30	0.900	No
334	33.40	1.92	0.79	1.13	0.88	0.723	1.04	0.693	0.98	1.30	0.896	No
335	33.50	1.93	0.80	1.13	0.88	0.723	1.04	0.693	0.98	1.30	0.897	No
336	33.60	1.93	0.80	1.13	0.88	0.723	1.04	0.693	0.98	1.30	0.898	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
337	33.70	1.94	0.80	1.14	0.88	0.723	1.04	0.693	0.98	1.30	0.898	No
338	33.80	1.95	0.80	1.14	0.88	0.722	1.04	0.692	0.98	1.30	0.898	No
339	33.90	1.95	0.81	1.14	0.88	0.722	1.04	0.692	0.98	1.30	0.899	No
340	34.00	1.96	0.81	1.15	0.88	0.722	1.04	0.692	0.98	1.30	0.899	No
341	34.10	1.97	0.81	1.15	0.88	0.722	1.04	0.692	0.98	1.30	0.899	No
342	34.20	1.97	0.82	1.15	0.88	0.722	1.04	0.692	0.98	1.30	0.902	No
343	34.30	1.98	0.82	1.16	0.88	0.722	1.04	0.692	0.98	1.30	0.905	No
344	34.40	1.98	0.82	1.16	0.88	0.722	1.04	0.692	0.98	1.30	0.907	No
345	34.50	1.99	0.83	1.16	0.88	0.722	1.04	0.692	0.98	1.30	0.908	No
346	34.60	2.00	0.83	1.17	0.88	0.721	1.04	0.691	0.98	1.30	0.909	No
347	34.70	2.00	0.83	1.17	0.88	0.721	1.04	0.691	0.98	1.30	0.910	No
348	34.80	2.01	0.84	1.17	0.88	0.721	1.04	0.691	0.98	1.30	0.910	No
349	34.90	2.02	0.84	1.18	0.88	0.721	1.04	0.691	0.98	1.30	0.911	No
350	35.00	2.02	0.84	1.18	0.87	0.721	1.04	0.691	0.98	1.30	0.915	No
351	35.10	2.03	0.85	1.18	0.87	0.721	1.04	0.691	0.98	1.30	0.919	No
352	35.20	2.04	0.85	1.19	0.87	0.721	1.04	0.691	0.98	1.30	0.923	No
353	35.30	2.04	0.85	1.19	0.87	0.721	1.04	0.691	0.98	1.30	0.927	No
354	35.40	2.05	0.85	1.19	0.87	0.720	1.04	0.691	0.98	1.30	0.930	No
355	35.50	2.06	0.86	1.20	0.87	0.720	1.04	0.690	0.98	1.30	0.931	No
356	35.60	2.06	0.86	1.20	0.87	0.720	1.04	0.690	0.98	1.30	0.930	No
357	35.70	2.07	0.86	1.20	0.87	0.720	1.04	0.690	0.98	1.30	0.929	No
358	35.80	2.07	0.87	1.21	0.87	0.720	1.04	0.690	0.98	1.30	0.928	No
359	35.90	2.08	0.87	1.21	0.87	0.720	1.04	0.690	0.98	1.30	0.927	No
360	36.00	2.09	0.87	1.21	0.87	0.720	1.04	0.690	0.98	1.30	0.927	No
361	36.10	2.09	0.88	1.22	0.87	0.720	1.04	0.690	0.98	1.30	0.925	No
362	36.20	2.10	0.88	1.22	0.87	0.720	1.04	0.690	0.98	1.30	0.923	No
363	36.30	2.11	0.88	1.22	0.87	0.719	1.04	0.690	0.98	1.30	0.922	No
364	36.40	2.11	0.89	1.23	0.87	0.719	1.04	0.689	0.97	1.30	0.921	No
365	36.50	2.12	0.89	1.23	0.87	0.719	1.04	0.689	0.97	1.30	0.921	No
366	36.60	2.13	0.89	1.23	0.87	0.719	1.04	0.689	0.97	1.30	2.000	Yes
367	36.70	2.13	0.90	1.24	0.87	0.719	1.04	0.689	0.97	1.30	2.000	Yes
368	36.80	2.14	0.90	1.24	0.87	0.719	1.04	0.689	0.97	1.30	2.000	Yes
369	36.90	2.14	0.90	1.24	0.87	0.718	1.04	0.689	0.98	1.30	2.000	Yes
370	37.00	2.15	0.90	1.25	0.87	0.718	1.04	0.688	0.98	1.30	2.000	Yes
371	37.10	2.16	0.91	1.25	0.86	0.718	1.04	0.688	0.98	1.30	2.000	Yes
372	37.20	2.16	0.91	1.25	0.86	0.718	1.04	0.688	0.98	1.30	2.000	Yes
373	37.30	2.17	0.91	1.26	0.86	0.718	1.04	0.688	0.98	1.30	0.937	No
374	37.40	2.18	0.92	1.26	0.86	0.718	1.04	0.688	0.98	1.30	0.937	No
375	37.50	2.18	0.92	1.26	0.86	0.718	1.04	0.688	0.98	1.30	0.937	No
376	37.60	2.19	0.92	1.27	0.86	0.717	1.04	0.688	0.98	1.30	0.936	No
377	37.70	2.20	0.93	1.27	0.86	0.717	1.04	0.688	0.98	1.30	0.935	No
378	37.80	2.20	0.93	1.27	0.86	0.717	1.04	0.687	0.98	1.30	0.934	No
379	37.90	2.21	0.93	1.28	0.86	0.717	1.04	0.687	0.98	1.30	0.933	No
380	38.00	2.21	0.94	1.28	0.86	0.717	1.04	0.687	0.97	1.30	0.933	No
381	38.10	2.22	0.94	1.28	0.86	0.717	1.04	0.687	0.97	1.30	0.932	No
382	38.20	2.23	0.94	1.28	0.86	0.717	1.04	0.687	0.97	1.30	0.930	No
383	38.30	2.23	0.95	1.29	0.86	0.716	1.04	0.687	0.97	1.30	0.929	No
384	38.40	2.24	0.95	1.29	0.86	0.716	1.04	0.687	0.97	1.30	0.929	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
385	38.50	2.25	0.95	1.29	0.86	0.716	1.04	0.686	0.97	1.30	0.929	No
386	38.60	2.25	0.95	1.30	0.86	0.716	1.04	0.686	0.97	1.30	0.930	No
387	38.70	2.26	0.96	1.30	0.86	0.716	1.04	0.686	0.97	1.30	0.932	No
388	38.80	2.27	0.96	1.30	0.86	0.716	1.04	0.686	0.97	1.30	0.933	No
389	38.90	2.27	0.96	1.31	0.86	0.715	1.04	0.686	0.97	1.30	0.933	No
390	39.00	2.28	0.97	1.31	0.86	0.715	1.04	0.686	0.97	1.30	0.934	No
391	39.10	2.28	0.97	1.31	0.86	0.715	1.04	0.685	0.97	1.30	0.934	No
392	39.20	2.29	0.97	1.32	0.85	0.715	1.04	0.685	0.97	1.30	2.000	Yes
393	39.30	2.30	0.98	1.32	0.85	0.715	1.04	0.685	0.97	1.30	2.000	Yes
394	39.40	2.30	0.98	1.32	0.85	0.715	1.04	0.685	0.97	1.30	2.000	Yes
395	39.50	2.31	0.98	1.33	0.85	0.715	1.04	0.685	0.97	1.30	2.000	Yes
396	39.60	2.31	0.99	1.33	0.85	0.714	1.04	0.685	0.98	1.30	2.000	Yes
397	39.70	2.32	0.99	1.33	0.85	0.714	1.04	0.685	0.98	1.30	2.000	Yes
398	39.80	2.33	0.99	1.33	0.85	0.714	1.04	0.685	0.98	1.30	2.000	Yes
399	39.90	2.33	1.00	1.34	0.85	0.714	1.04	0.684	0.98	1.30	0.939	No
400	40.00	2.34	1.00	1.34	0.85	0.714	1.04	0.684	0.98	1.30	0.939	No
401	40.10	2.34	1.00	1.34	0.85	0.714	1.04	0.684	0.98	1.30	0.939	No
402	40.20	2.35	1.00	1.35	0.85	0.714	1.04	0.684	0.98	1.30	0.939	No
403	40.30	2.36	1.01	1.35	0.85	0.714	1.04	0.684	0.98	1.30	0.939	No
404	40.40	2.36	1.01	1.35	0.85	0.714	1.04	0.684	0.98	1.30	0.940	No
405	40.50	2.37	1.01	1.35	0.85	0.714	1.04	0.684	0.98	1.30	0.940	No
406	40.60	2.37	1.02	1.36	0.85	0.714	1.04	0.684	0.98	1.30	0.940	No
407	40.70	2.38	1.02	1.36	0.85	0.713	1.04	0.684	0.98	1.30	0.940	No
408	40.80	2.39	1.02	1.36	0.85	0.713	1.04	0.684	0.98	1.30	0.940	No
409	40.90	2.39	1.03	1.37	0.85	0.713	1.04	0.684	0.97	1.30	0.940	No
410	41.00	2.40	1.03	1.37	0.85	0.713	1.04	0.683	0.97	1.30	0.940	No
411	41.10	2.40	1.03	1.37	0.85	0.713	1.04	0.683	0.97	1.30	0.940	No
412	41.20	2.41	1.04	1.37	0.84	0.713	1.04	0.683	0.97	1.30	0.940	No
413	41.30	2.42	1.04	1.38	0.84	0.713	1.04	0.683	0.97	1.30	0.940	No
414	41.40	2.42	1.04	1.38	0.84	0.712	1.04	0.683	0.97	1.30	0.940	No
415	41.50	2.43	1.05	1.38	0.84	0.712	1.04	0.683	0.97	1.30	0.940	No
416	41.60	2.43	1.05	1.39	0.84	0.712	1.04	0.683	0.97	1.30	0.940	No
417	41.70	2.44	1.05	1.39	0.84	0.712	1.04	0.682	0.97	1.30	0.940	No
418	41.80	2.45	1.05	1.39	0.84	0.712	1.04	0.682	0.97	1.30	2.000	Yes
419	41.90	2.45	1.06	1.40	0.84	0.711	1.04	0.682	0.97	1.30	2.000	Yes
420	42.00	2.46	1.06	1.40	0.84	0.711	1.04	0.682	0.96	1.30	2.000	Yes
421	42.10	2.47	1.06	1.40	0.84	0.711	1.04	0.681	0.96	1.30	2.000	Yes
422	42.20	2.47	1.07	1.41	0.84	0.711	1.04	0.681	0.95	1.30	2.000	Yes
423	42.30	2.48	1.07	1.41	0.84	0.711	1.04	0.681	0.94	1.30	2.000	Yes
424	42.40	2.49	1.07	1.41	0.84	0.710	1.04	0.681	0.93	1.30	2.000	Yes
425	42.50	2.49	1.08	1.42	0.84	0.710	1.04	0.681	0.92	1.30	0.947	No
426	42.60	2.50	1.08	1.42	0.84	0.710	1.04	0.680	0.91	1.30	0.950	No
427	42.70	2.51	1.08	1.42	0.84	0.709	1.04	0.680	0.91	1.30	0.950	No
428	42.80	2.51	1.09	1.43	0.84	0.709	1.04	0.680	0.91	1.30	2.000	Yes
429	42.90	2.52	1.09	1.43	0.84	0.709	1.04	0.679	0.91	1.30	2.000	Yes
430	43.00	2.53	1.09	1.43	0.84	0.709	1.04	0.679	0.92	1.30	2.000	Yes
431	43.10	2.53	1.10	1.44	0.84	0.708	1.04	0.679	0.93	1.30	2.000	Yes
432	43.20	2.54	1.10	1.44	0.84	0.708	1.04	0.679	0.94	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
433	43.30	2.54	1.10	1.44	0.83	0.708	1.04	0.678	0.94	1.30	2.000	Yes
434	43.40	2.55	1.10	1.45	0.83	0.707	1.04	0.678	0.95	1.30	2.000	Yes
435	43.50	2.56	1.11	1.45	0.83	0.707	1.04	0.678	0.95	1.30	2.000	Yes
436	43.60	2.56	1.11	1.45	0.83	0.707	1.04	0.678	0.95	1.30	2.000	Yes
437	43.70	2.57	1.11	1.46	0.83	0.707	1.04	0.677	0.96	1.30	2.000	Yes
438	43.80	2.58	1.12	1.46	0.83	0.706	1.04	0.677	0.96	1.30	2.000	Yes
439	43.90	2.58	1.12	1.46	0.83	0.706	1.04	0.677	0.95	1.30	2.000	Yes
440	44.00	2.59	1.12	1.47	0.83	0.706	1.04	0.677	0.95	1.30	2.000	Yes
441	44.10	2.60	1.13	1.47	0.83	0.706	1.04	0.676	0.94	1.30	2.000	Yes
442	44.20	2.60	1.13	1.47	0.83	0.705	1.04	0.676	0.94	1.30	2.000	Yes
443	44.30	2.61	1.13	1.48	0.83	0.705	1.04	0.676	0.94	1.30	2.000	Yes
444	44.40	2.62	1.14	1.48	0.83	0.705	1.04	0.676	0.94	1.30	2.000	Yes
445	44.50	2.62	1.14	1.48	0.83	0.705	1.04	0.675	0.94	1.30	2.000	Yes
446	44.60	2.63	1.14	1.49	0.83	0.704	1.04	0.675	0.95	1.30	2.000	Yes
447	44.70	2.64	1.15	1.49	0.83	0.704	1.04	0.675	0.95	1.30	2.000	Yes
448	44.80	2.64	1.15	1.49	0.83	0.704	1.04	0.675	0.95	1.30	2.000	Yes
449	44.90	2.65	1.15	1.50	0.83	0.703	1.04	0.674	0.94	1.30	2.000	Yes
450	45.00	2.66	1.15	1.50	0.83	0.703	1.04	0.674	0.93	1.30	2.000	Yes
451	45.10	2.66	1.16	1.50	0.83	0.703	1.04	0.674	0.92	1.30	2.000	Yes
452	45.20	2.67	1.16	1.51	0.83	0.703	1.04	0.673	0.91	1.30	0.945	No
453	45.30	2.67	1.16	1.51	0.82	0.702	1.04	0.673	0.91	1.30	2.000	Yes
454	45.40	2.68	1.17	1.51	0.82	0.702	1.04	0.673	0.91	1.30	2.000	Yes
455	45.50	2.69	1.17	1.52	0.82	0.702	1.04	0.673	0.91	1.30	2.000	Yes
456	45.60	2.69	1.17	1.52	0.82	0.701	1.04	0.672	0.92	1.30	2.000	Yes
457	45.70	2.70	1.18	1.53	0.82	0.701	1.04	0.672	0.93	1.30	2.000	Yes
458	45.80	2.71	1.18	1.53	0.82	0.701	1.04	0.672	0.94	1.30	2.000	Yes
459	45.90	2.71	1.18	1.53	0.82	0.700	1.04	0.671	0.95	1.30	2.000	Yes
460	46.00	2.72	1.19	1.54	0.82	0.700	1.04	0.671	0.95	1.30	0.935	No
461	46.10	2.73	1.19	1.54	0.82	0.700	1.04	0.671	0.95	1.30	2.000	Yes
462	46.20	2.73	1.19	1.54	0.82	0.700	1.04	0.671	0.95	1.30	2.000	Yes
463	46.30	2.74	1.19	1.54	0.82	0.699	1.04	0.670	0.95	1.30	2.000	Yes
464	46.40	2.75	1.20	1.55	0.82	0.699	1.04	0.670	0.95	1.30	2.000	Yes
465	46.50	2.75	1.20	1.55	0.82	0.699	1.04	0.670	0.94	1.30	2.000	Yes
466	46.60	2.76	1.20	1.55	0.82	0.699	1.04	0.670	0.93	1.30	2.000	Yes
467	46.70	2.77	1.21	1.56	0.82	0.698	1.04	0.669	0.92	1.30	0.934	No
468	46.80	2.77	1.21	1.56	0.82	0.698	1.04	0.669	0.91	1.30	0.935	No
469	46.90	2.78	1.21	1.56	0.82	0.698	1.04	0.669	0.91	1.30	0.937	No
470	47.00	2.79	1.22	1.57	0.82	0.697	1.04	0.669	0.91	1.30	0.935	No
471	47.10	2.79	1.22	1.57	0.82	0.697	1.04	0.668	0.91	1.30	0.935	No
472	47.20	2.80	1.22	1.58	0.82	0.697	1.04	0.668	0.91	1.30	0.935	No
473	47.30	2.80	1.23	1.58	0.82	0.697	1.04	0.668	0.91	1.30	0.935	No
474	47.40	2.81	1.23	1.58	0.81	0.696	1.04	0.667	0.91	1.30	0.935	No
475	47.50	2.82	1.23	1.59	0.81	0.696	1.04	0.667	0.90	1.30	0.945	No
476	47.60	2.82	1.24	1.59	0.81	0.696	1.04	0.667	0.89	1.30	0.959	No
477	47.70	2.83	1.24	1.59	0.81	0.695	1.04	0.666	0.88	1.30	0.967	No
478	47.80	2.84	1.24	1.60	0.81	0.695	1.04	0.666	0.88	1.30	0.968	No
479	47.90	2.84	1.24	1.60	0.81	0.695	1.04	0.666	0.88	1.30	0.968	No
480	48.00	2.85	1.25	1.60	0.81	0.694	1.04	0.665	0.88	1.30	0.968	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
481	48.10	2.86	1.25	1.61	0.81	0.694	1.04	0.665	0.87	1.30	0.969	No
482	48.20	2.86	1.25	1.61	0.81	0.694	1.04	0.665	0.87	1.30	0.969	No
483	48.30	2.87	1.26	1.61	0.81	0.693	1.04	0.664	0.87	1.30	0.969	No
484	48.40	2.88	1.26	1.62	0.81	0.693	1.04	0.664	0.87	1.30	0.969	No
485	48.50	2.89	1.26	1.62	0.81	0.693	1.04	0.664	0.87	1.30	0.970	No
486	48.60	2.89	1.27	1.63	0.81	0.692	1.04	0.663	0.87	1.30	0.970	No
487	48.70	2.90	1.27	1.63	0.81	0.692	1.04	0.663	0.87	1.30	0.970	No
488	48.80	2.91	1.27	1.63	0.81	0.692	1.04	0.663	0.87	1.30	0.970	No
489	48.90	2.91	1.28	1.64	0.81	0.691	1.04	0.662	0.87	1.30	0.971	No
490	49.00	2.92	1.28	1.64	0.81	0.691	1.04	0.662	0.87	1.30	0.971	No
491	49.10	2.93	1.28	1.64	0.81	0.691	1.04	0.662	0.87	1.30	0.971	No
492	49.20	2.93	1.29	1.65	0.81	0.690	1.04	0.661	0.87	1.30	0.971	No
493	49.30	2.94	1.29	1.65	0.81	0.690	1.04	0.661	0.87	1.30	0.972	No
494	49.40	2.95	1.29	1.65	0.80	0.689	1.04	0.661	0.87	1.30	0.972	No
495	49.50	2.95	1.29	1.66	0.80	0.689	1.04	0.660	0.87	1.30	0.972	No
496	49.60	2.96	1.30	1.66	0.80	0.689	1.04	0.660	0.86	1.30	0.972	No
497	49.70	2.97	1.30	1.66	0.80	0.688	1.04	0.660	0.86	1.30	0.973	No
498	49.80	2.97	1.30	1.67	0.80	0.688	1.04	0.659	0.86	1.30	0.973	No
499	49.90	2.98	1.31	1.67	0.80	0.688	1.04	0.659	0.86	1.30	0.973	No

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
 σ_v : Total overburden pressure at test point (tsf)
 u_0 : Water pressure at test point (tsf)
 σ_v' : Effective overburden pressure based on GWT during earthquake (tsf)
 r_d : Nonlinear shear mass factor
 CSR: Cyclic Stress Ratio
 MSF: Magnitude Scaling Factor
 CSR_{eq} : CSR adjusted for M=7.5
 K_σ : Effective overburden stress factor
 CSR*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1	0.10	20.69	36.18	2.16	0.53	1.70	37.53	48.38	85.91	4.000	No	No	2.00
2	0.20	15.95	45.41	2.28	0.56	1.70	24.67	50.65	75.32	4.000	No	No	2.00
3	0.30	12.29	55.51	2.41	0.58	1.70	14.65	51.64	66.29	4.000	No	No	2.00
4	0.40	12.85	54.86	2.40	0.57	1.70	19.92	52.89	72.81	4.000	No	No	2.00
5	0.50	17.93	45.67	2.28	0.55	1.70	27.37	51.46	78.84	4.000	No	No	2.00
6	0.60	25.60	38.33	2.19	0.52	1.70	39.11	50.27	89.39	4.000	No	No	2.00
7	0.70	35.62	32.10	2.11	0.49	1.70	56.88	49.07	105.95	4.000	No	No	2.00
8	0.80	45.80	27.44	2.06	0.45	1.70	75.67	47.20	122.87	4.000	No	No	2.00
9	0.90	55.07	24.15	2.01	0.43	1.70	88.15	44.06	132.21	4.000	No	No	2.00
10	1.00	61.98	22.26	1.99	0.41	1.70	101.54	42.44	143.98	4.000	No	No	2.00
11	1.10	65.41	21.89	1.99	0.40	1.70	109.01	42.76	151.77	4.000	No	No	2.00
12	1.20	66.73	22.11	1.99	0.41	1.70	104.65	42.60	147.25	4.000	No	No	2.00
13	1.30	68.80	22.08	1.99	0.40	1.70	107.90	43.01	150.92	4.000	No	No	2.00
14	1.40	72.09	21.70	1.98	0.38	1.70	118.96	43.82	162.78	4.000	No	No	2.00
15	1.50	75.47	21.38	1.98	0.38	1.70	120.52	43.28	163.81	4.000	No	No	2.00
16	1.60	77.78	21.51	1.98	0.37	1.70	124.21	44.14	168.35	4.000	No	No	2.00
17	1.70	79.45	21.82	1.99	0.36	1.70	130.07	45.77	175.83	4.000	No	No	2.00
18	1.80	79.92	22.43	1.99	0.36	1.70	128.56	47.00	175.57	4.000	No	No	2.00
19	1.90	78.74	23.48	2.01	0.36	1.70	126.49	49.06	175.55	4.000	No	No	2.00
20	2.00	77.53	24.44	2.02	0.36	1.70	124.38	50.77	175.15	4.000	No	No	2.00
21	2.10	76.45	25.18	2.03	0.36	1.70	122.74	51.96	174.70	4.000	No	No	2.00
22	2.20	74.95	26.08	2.04	0.36	1.70	121.25	53.40	174.66	4.000	No	No	2.00
23	2.30	72.03	27.71	2.06	0.37	1.70	117.16	55.49	172.65	4.000	No	No	2.00
24	2.40	66.61	30.48	2.09	0.38	1.70	108.69	57.98	166.68	4.000	No	No	2.00
25	2.50	59.83	33.65	2.13	0.40	1.70	95.12	58.98	154.10	4.000	No	No	2.00
26	2.60	53.38	36.20	2.17	0.41	1.70	84.47	59.14	143.61	4.000	No	No	2.00
27	2.70	48.56	37.57	2.18	0.43	1.70	77.65	58.76	136.41	4.000	No	No	2.00
28	2.80	45.31	37.90	2.19	0.44	1.70	71.89	57.67	129.56	4.000	No	No	2.00
29	2.90	44.32	36.67	2.17	0.45	1.70	68.81	55.95	124.76	4.000	No	No	2.00
30	3.00	45.95	34.36	2.14	0.44	1.70	72.86	54.79	127.65	4.000	No	No	2.00
31	3.10	48.29	33.43	2.13	0.43	1.70	79.75	55.38	135.13	4.000	No	No	2.00
32	3.20	48.11	35.58	2.16	0.42	1.70	80.10	57.57	137.67	4.000	Yes	No	2.00
33	3.30	44.42	40.47	2.22	0.43	1.70	72.01	59.63	131.64	4.000	Yes	No	2.00
34	3.40	38.42	46.91	2.30	0.45	1.70	61.92	60.95	122.86	4.000	Yes	No	2.00
35	3.50	31.66	54.22	2.39	0.47	1.70	51.18	61.20	112.38	4.000	Yes	No	2.00
36	3.60	25.01	62.56	2.49	0.50	1.70	39.44	60.44	99.88	4.000	Yes	No	2.00
37	3.70	18.93	72.27	2.62	0.52	1.70	29.89	0.00	29.89	4.000	Yes	Yes	2.00
38	3.80	13.89	83.18	2.75	0.54	1.70	21.88	0.00	21.88	4.000	Yes	Yes	2.00
39	3.90	9.83	95.42	2.91	0.56	1.70	15.15	0.00	15.15	4.000	Yes	Yes	2.00
40	4.00	6.71	100.00	3.07	0.58	1.70	10.31	0.00	10.31	4.000	No	Yes	2.00
41	4.10	4.73	100.00	3.22	0.59	1.70	6.85	0.00	6.85	4.000	No	Yes	2.00
42	4.20	3.30	100.00	3.37	0.60	1.70	5.64	0.00	5.64	4.000	No	Yes	2.00
43	4.30	2.28	100.00	3.53	0.61	1.70	3.41	0.00	3.41	4.000	No	Yes	2.00
44	4.40	1.63	100.00	3.68	0.62	1.70	1.93	0.00	1.93	4.000	No	Yes	2.00
45	4.50	1.68	100.00	3.66	0.61	1.70	2.52	0.00	2.52	4.000	No	Yes	2.00
46	4.60	1.90	100.00	3.61	0.61	1.70	3.66	0.00	3.66	4.000	No	Yes	2.00
47	4.70	1.99	100.00	3.60	0.61	1.70	2.97	0.00	2.97	4.000	No	Yes	2.00
48	4.80	2.28	100.00	3.56	0.61	1.70	2.98	0.00	2.98	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
49	4.90	3.08	100.00	3.42	0.60	1.70	5.01	0.00	5.01	4.000	No	Yes	2.00
50	5.00	5.02	100.00	3.18	0.59	1.70	6.83	0.00	6.83	4.000	No	Yes	2.00
51	5.10	8.35	97.32	2.93	0.57	1.70	12.35	0.00	12.35	4.000	No	Yes	2.00
52	5.20	12.99	82.56	2.74	0.55	1.70	21.04	0.00	21.04	4.000	No	Yes	2.00
53	5.30	17.05	76.22	2.67	0.52	1.70	29.17	0.00	29.17	4.000	No	Yes	2.00
54	5.40	18.42	76.21	2.67	0.51	1.70	31.91	0.00	31.91	4.000	No	Yes	2.00
55	5.50	17.82	77.79	2.68	0.53	1.70	27.68	0.00	27.68	4.000	Yes	Yes	2.00
56	5.60	18.27	73.64	2.63	0.53	1.70	26.27	0.00	26.27	4.000	Yes	Yes	2.00
57	5.70	22.60	60.49	2.47	0.52	1.70	34.05	58.39	92.44	4.000	Yes	No	2.00
58	5.80	30.34	45.74	2.28	0.49	1.70	48.56	56.92	105.48	4.000	Yes	No	2.00
59	5.90	38.67	35.96	2.16	0.46	1.70	63.60	54.16	117.76	4.000	Yes	No	2.00
60	6.00	44.41	32.80	2.12	0.45	1.67	72.74	53.19	125.93	4.000	Yes	No	2.00
61	6.10	46.53	34.20	2.14	0.44	1.65	73.82	54.85	128.68	4.000	No	No	2.00
62	6.20	45.75	37.24	2.18	0.44	1.64	71.02	56.94	127.97	4.000	No	No	2.00
63	6.30	44.18	39.54	2.21	0.45	1.63	67.57	57.90	125.48	4.000	No	No	2.00
64	6.40	43.27	40.04	2.21	0.45	1.63	65.71	57.81	123.51	4.000	No	No	2.00
65	6.50	43.29	39.00	2.20	0.45	1.62	66.00	57.13	123.13	4.000	No	No	2.00
66	6.60	44.11	37.19	2.18	0.45	1.61	66.65	55.88	122.53	4.000	No	No	2.00
67	6.70	45.23	35.23	2.15	0.45	1.59	68.12	54.54	122.66	4.000	No	No	2.00
68	6.80	46.59	33.43	2.13	0.45	1.58	69.67	53.18	122.85	4.000	No	No	2.00
69	6.90	47.78	32.43	2.12	0.45	1.57	71.18	52.47	123.65	4.000	No	No	2.00
70	7.00	47.94	33.05	2.13	0.45	1.56	71.70	53.23	124.92	4.000	No	No	2.00
71	7.10	46.35	35.70	2.16	0.45	1.55	68.83	55.12	123.95	4.000	No	No	2.00
72	7.20	43.14	39.81	2.21	0.46	1.55	63.19	57.04	120.23	4.000	No	No	2.00
73	7.30	39.20	43.87	2.26	0.47	1.55	57.36	58.16	115.51	4.000	No	No	2.00
74	7.40	35.95	45.99	2.29	0.48	1.56	51.83	57.89	109.72	4.000	No	No	2.00
75	7.50	34.90	44.42	2.27	0.49	1.56	49.27	56.42	105.69	4.000	No	No	2.00
76	7.60	36.71	39.35	2.20	0.48	1.55	52.57	54.17	106.74	4.000	No	No	2.00
77	7.70	40.76	33.54	2.13	0.48	1.53	58.71	50.88	109.59	4.000	No	No	2.00
78	7.80	45.18	29.52	2.08	0.47	1.51	65.04	47.88	112.92	4.000	No	No	2.00
79	7.90	48.49	27.90	2.06	0.47	1.49	69.45	46.65	116.09	4.000	No	No	2.00
80	8.00	50.35	28.07	2.06	0.46	1.48	70.74	47.13	117.87	4.000	No	No	2.00
81	8.10	50.92	30.19	2.09	0.46	1.47	70.98	49.89	120.87	4.000	Yes	No	2.00
82	8.20	50.43	35.63	2.16	0.45	1.45	69.96	55.31	125.27	4.000	Yes	No	2.00
83	8.30	48.21	42.96	2.25	0.44	1.44	67.13	60.07	127.21	4.000	Yes	No	2.00
84	8.40	44.03	51.24	2.35	0.45	1.45	60.91	62.67	123.58	4.000	Yes	No	2.00
85	8.50	38.01	59.91	2.46	0.46	1.46	52.98	63.54	116.52	4.000	Yes	No	2.00
86	8.60	31.11	69.35	2.58	0.48	1.48	43.50	63.16	106.65	4.000	Yes	No	2.00
87	8.70	24.26	80.01	2.71	0.51	1.50	33.80	0.00	33.80	4.000	Yes	Yes	2.00
88	8.80	18.28	91.17	2.85	0.53	1.52	25.72	0.00	25.72	4.000	Yes	Yes	2.00
89	8.90	13.46	100.00	2.99	0.55	1.54	19.22	0.00	19.22	4.000	Yes	Yes	2.00
90	9.00	9.80	100.00	3.13	0.57	1.56	13.77	0.00	13.77	4.000	No	Yes	2.00
91	9.10	7.41	100.00	3.24	0.58	1.58	10.22	0.00	10.22	4.000	No	Yes	2.00
92	9.20	6.33	100.00	3.28	0.59	1.58	8.98	0.00	8.98	4.000	No	Yes	2.00
93	9.30	6.36	100.00	3.25	0.59	1.57	9.05	0.00	9.05	4.000	No	Yes	2.00
94	9.40	7.05	100.00	3.18	0.58	1.56	10.26	0.00	10.26	4.000	No	Yes	2.00
95	9.50	7.58	100.00	3.14	0.58	1.55	11.87	0.00	11.87	4.000	No	Yes	2.00
96	9.60	7.34	100.00	3.15	0.58	1.55	11.21	0.00	11.21	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
97	9.70	6.26	100.00	3.23	0.59	1.55	9.18	0.00	9.18	4.000	No	Yes	2.00
98	9.80	7.93	100.00	3.15	0.59	1.56	7.18	0.00	7.18	4.000	No	Yes	2.00
99	9.90	13.13	100.00	2.98	0.55	1.51	18.03	0.00	18.03	4.000	No	Yes	2.00
100	10.00	18.80	92.22	2.87	0.51	1.46	30.19	0.00	30.19	4.000	No	Yes	2.00
101	10.10	18.67	92.61	2.87	0.51	1.46	30.12	0.00	30.12	4.000	No	Yes	2.00
102	10.20	14.65	98.75	2.95	0.56	1.50	17.34	0.00	17.34	4.000	No	Yes	2.00
103	10.30	10.95	100.00	3.03	0.57	1.51	13.94	0.00	13.94	4.000	No	Yes	2.00
104	10.40	10.48	100.00	3.05	0.56	1.50	15.25	0.00	15.25	4.000	No	Yes	2.00
105	10.50	11.16	100.00	3.03	0.56	1.49	15.29	0.00	15.29	4.000	No	Yes	2.00
106	10.60	13.38	100.00	2.98	0.56	1.48	16.58	0.00	16.58	4.000	Yes	Yes	2.00
107	10.70	16.24	96.45	2.92	0.53	1.45	23.98	0.00	23.98	4.000	Yes	Yes	2.00
108	10.80	23.16	84.21	2.77	0.53	1.44	26.48	0.00	26.48	4.000	Yes	Yes	2.00
109	10.90	36.54	64.35	2.52	0.49	1.40	43.12	61.93	105.06	4.000	Yes	No	2.00
110	11.00	57.04	44.34	2.27	0.43	1.34	73.01	62.38	135.40	4.000	Yes	No	2.00
111	11.10	77.62	29.55	2.08	0.40	1.31	99.97	54.93	154.90	4.000	Yes	No	2.00
112	11.20	91.25	20.12	1.96	0.39	1.30	116.21	39.51	155.72	4.000	Yes	No	2.00
113	11.30	96.49	15.70	1.91	0.40	1.31	121.94	27.21	149.15	4.000	Yes	No	2.00
114	11.40	96.73	14.07	1.89	0.42	1.32	120.29	21.65	141.94	0.244	No	No	0.38
115	11.50	93.84	14.79	1.90	0.42	1.31	118.07	23.88	141.96	0.244	No	No	0.38
116	11.60	89.17	17.54	1.93	0.41	1.31	111.24	31.80	143.04	0.249	No	No	0.38
117	11.70	82.47	21.72	1.98	0.41	1.31	101.98	41.32	143.30	0.250	No	No	0.39
118	11.80	74.34	26.56	2.04	0.42	1.31	92.53	49.00	141.53	0.242	No	No	0.37
119	11.90	66.88	31.09	2.10	0.43	1.31	81.31	53.10	134.41	0.212	No	No	0.32
120	12.00	59.90	34.99	2.15	0.44	1.32	74.94	55.85	130.79	0.200	No	No	0.30
121	12.10	54.60	37.70	2.18	0.45	1.32	67.58	56.51	124.09	0.181	No	No	0.27
122	12.20	52.76	38.31	2.19	0.46	1.33	62.32	55.74	118.06	0.167	No	No	0.25
123	12.30	53.42	37.54	2.18	0.45	1.32	68.08	56.50	124.58	0.182	No	No	0.27
124	12.40	55.36	36.43	2.17	0.45	1.31	69.47	55.90	125.38	0.184	No	No	0.27
125	12.50	55.60	36.33	2.17	0.45	1.31	68.67	55.63	124.30	0.182	No	No	0.27
126	12.60	55.04	37.07	2.18	0.45	1.31	68.49	56.21	124.69	0.183	No	No	0.27
127	12.70	54.18	39.13	2.20	0.45	1.31	67.00	57.47	124.47	4.000	Yes	No	2.00
128	12.80	51.05	43.66	2.26	0.45	1.30	64.98	59.96	124.94	4.000	Yes	No	2.00
129	12.90	44.55	50.85	2.35	0.46	1.31	56.90	61.44	118.34	4.000	Yes	No	2.00
130	13.00	37.39	59.62	2.46	0.49	1.33	43.64	60.84	104.48	4.000	Yes	No	2.00
131	13.10	30.77	68.59	2.57	0.50	1.33	39.35	61.79	101.14	4.000	Yes	No	2.00
132	13.20	26.49	75.24	2.65	0.51	1.34	33.07	0.00	33.07	4.000	Yes	Yes	2.00
133	13.30	22.74	80.58	2.72	0.53	1.35	27.91	0.00	27.91	4.000	Yes	Yes	2.00
134	13.40	20.92	82.99	2.75	0.53	1.35	25.57	0.00	25.57	4.000	Yes	Yes	2.00
135	13.50	20.31	83.65	2.76	0.53	1.34	26.25	0.00	26.25	4.000	No	Yes	2.00
136	13.60	20.02	83.96	2.76	0.53	1.34	25.49	0.00	25.49	4.000	No	Yes	2.00
137	13.70	19.28	84.47	2.77	0.54	1.34	24.35	0.00	24.35	4.000	No	Yes	2.00
138	13.80	18.73	84.56	2.77	0.54	1.34	23.37	0.00	23.37	4.000	No	Yes	2.00
139	13.90	18.04	85.57	2.78	0.54	1.34	23.32	0.00	23.32	4.000	No	Yes	2.00
140	14.00	16.71	88.58	2.82	0.54	1.34	21.69	0.00	21.69	4.000	No	Yes	2.00
141	14.10	15.17	92.68	2.87	0.55	1.34	18.31	0.00	18.31	4.000	No	Yes	2.00
142	14.20	14.03	96.27	2.92	0.56	1.34	17.52	0.00	17.52	4.000	No	Yes	2.00
143	14.30	11.65	100.00	3.00	0.55	1.34	17.38	0.00	17.38	4.000	No	Yes	2.00
144	14.40	7.83	100.00	3.16	0.58	1.35	9.34	0.00	9.34	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
145	14.50	4.04	100.00	3.46	0.61	1.37	3.12	0.00	3.12	4.000	No	Yes	2.00
146	14.60	2.41	100.00	3.75	0.61	1.37	3.11	0.00	3.11	4.000	No	Yes	2.00
147	14.70	2.41	100.00	3.74	0.61	1.36	3.11	0.00	3.11	4.000	No	Yes	2.00
148	14.80	2.41	100.00	3.72	0.61	1.36	3.10	0.00	3.10	4.000	No	Yes	2.00
149	14.90	2.19	100.00	3.78	0.61	1.36	3.10	0.00	3.10	4.000	No	Yes	2.00
150	15.00	1.79	100.00	3.93	0.61	1.36	2.25	0.00	2.25	4.000	No	Yes	2.00
151	15.10	1.39	100.00	4.06	0.62	1.36	1.55	0.00	1.55	4.000	No	Yes	2.00
152	15.20	1.20	100.00	4.06	0.62	1.36	1.55	0.00	1.55	4.000	No	Yes	2.00
153	15.30	1.20	100.00	4.06	0.62	1.36	1.55	0.00	1.55	4.000	No	Yes	2.00
154	15.40	1.39	100.00	4.06	0.62	1.36	1.54	0.00	1.54	4.000	No	Yes	2.00
155	15.50	2.04	100.00	3.92	0.61	1.35	2.26	0.00	2.26	4.000	No	Yes	2.00
156	15.60	3.92	100.00	3.49	0.61	1.34	4.01	0.00	4.01	4.000	No	Yes	2.00
157	15.70	7.11	100.00	3.17	0.59	1.33	8.58	0.00	8.58	4.000	No	Yes	2.00
158	15.80	10.59	100.00	3.00	0.57	1.31	14.06	0.00	14.06	4.000	No	Yes	2.00
159	15.90	12.22	98.97	2.95	0.56	1.30	16.73	0.00	16.73	4.000	No	Yes	2.00
160	16.00	11.38	100.00	2.99	0.57	1.31	14.49	0.00	14.49	4.000	No	Yes	2.00
161	16.10	9.26	100.00	3.08	0.58	1.31	10.93	0.00	10.93	4.000	No	Yes	2.00
162	16.20	7.35	100.00	3.16	0.59	1.31	8.96	0.00	8.96	4.000	No	Yes	2.00
163	16.30	6.42	100.00	3.19	0.59	1.32	7.48	0.00	7.48	4.000	No	Yes	2.00
164	16.40	6.02	100.00	3.21	0.59	1.31	7.47	0.00	7.47	4.000	No	Yes	2.00
165	16.50	5.80	100.00	3.23	0.59	1.31	7.45	0.00	7.45	4.000	No	Yes	2.00
166	16.60	5.19	100.00	3.28	0.60	1.31	6.62	0.00	6.62	4.000	No	Yes	2.00
167	16.70	4.26	100.00	3.38	0.60	1.31	5.18	0.00	5.18	4.000	No	Yes	2.00
168	16.80	3.29	100.00	3.52	0.61	1.31	4.01	0.00	4.01	4.000	No	Yes	2.00
169	16.90	2.90	100.00	3.59	0.61	1.31	3.05	0.00	3.05	4.000	No	Yes	2.00
170	17.00	2.86	100.00	3.59	0.61	1.31	3.72	0.00	3.72	4.000	No	Yes	2.00
171	17.10	3.23	100.00	3.51	0.61	1.31	3.82	0.00	3.82	4.000	No	Yes	2.00
172	17.20	3.29	100.00	3.51	0.61	1.30	4.40	0.00	4.40	4.000	No	Yes	2.00
173	17.30	3.07	100.00	3.57	0.61	1.30	3.92	0.00	3.92	4.000	No	Yes	2.00
174	17.40	2.98	100.00	3.60	0.61	1.30	3.02	0.00	3.02	4.000	No	Yes	2.00
175	17.50	3.69	100.00	3.45	0.61	1.30	4.03	0.00	4.03	4.000	No	Yes	2.00
176	17.60	5.22	100.00	3.26	0.60	1.29	6.48	0.00	6.48	4.000	No	Yes	2.00
177	17.70	6.73	100.00	3.13	0.59	1.28	8.55	0.00	8.55	4.000	No	Yes	2.00
178	17.80	7.04	100.00	3.12	0.58	1.28	9.46	0.00	9.46	4.000	No	Yes	2.00
179	17.90	6.09	100.00	3.20	0.59	1.28	7.54	0.00	7.54	4.000	No	Yes	2.00
180	18.00	4.82	100.00	3.33	0.60	1.28	5.10	0.00	5.10	4.000	No	Yes	2.00
181	18.10	4.08	100.00	3.43	0.60	1.28	4.86	0.00	4.86	4.000	No	Yes	2.00
182	18.20	4.56	100.00	3.39	0.60	1.28	4.86	0.00	4.86	4.000	No	Yes	2.00
183	18.30	7.27	100.00	3.19	0.60	1.27	6.78	0.00	6.78	4.000	No	Yes	2.00
184	18.40	12.35	100.00	3.01	0.57	1.26	14.43	0.00	14.43	4.000	No	Yes	2.00
185	18.50	17.77	96.27	2.92	0.54	1.24	22.52	0.00	22.52	4.000	No	Yes	2.00
186	18.60	19.06	95.93	2.91	0.53	1.23	25.47	0.00	25.47	4.000	No	Yes	2.00
187	18.70	18.07	97.22	2.93	0.55	1.24	18.80	0.00	18.80	4.000	No	Yes	2.00
188	18.80	16.83	96.24	2.92	0.55	1.24	19.01	0.00	19.01	4.000	No	Yes	2.00
189	18.90	18.43	89.78	2.83	0.54	1.23	21.15	0.00	21.15	4.000	No	Yes	2.00
190	19.00	21.05	82.29	2.74	0.54	1.23	24.12	0.00	24.12	4.000	No	Yes	2.00
191	19.10	24.45	74.65	2.65	0.53	1.22	27.80	0.00	27.80	4.000	No	Yes	2.00
192	19.20	28.33	68.29	2.57	0.52	1.21	32.49	59.75	92.23	0.128	No	No	0.15

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
193	19.30	31.79	65.92	2.54	0.50	1.20	36.95	60.53	97.48	0.134	No	No	0.16
194	19.40	33.34	68.67	2.57	0.50	1.20	39.05	61.73	100.78	0.138	No	No	0.17
195	19.50	32.10	74.83	2.65	0.50	1.20	37.34	0.00	37.34	4.000	No	Yes	2.00
196	19.60	28.67	82.29	2.74	0.51	1.20	32.60	0.00	32.60	4.000	No	Yes	2.00
197	19.70	24.81	88.18	2.81	0.52	1.20	27.50	0.00	27.50	4.000	No	Yes	2.00
198	19.80	25.42	86.50	2.79	0.53	1.20	24.38	0.00	24.38	4.000	Yes	Yes	2.00
199	19.90	32.01	76.60	2.67	0.51	1.19	34.45	0.00	34.45	4.000	Yes	Yes	2.00
200	20.00	40.24	64.83	2.52	0.47	1.17	48.77	63.67	112.44	4.000	Yes	No	2.00
201	20.10	47.35	54.54	2.39	0.47	1.17	51.08	61.29	112.37	4.000	Yes	No	2.00
202	20.20	50.45	48.63	2.32	0.46	1.17	57.25	60.56	117.81	4.000	Yes	No	2.00
203	20.30	51.38	49.54	2.33	0.46	1.16	58.47	61.29	119.76	4.000	Yes	No	2.00
204	20.40	47.65	54.05	2.39	0.47	1.16	53.77	61.84	115.61	4.000	Yes	No	2.00
205	20.50	41.70	58.65	2.45	0.49	1.17	45.03	60.95	105.98	4.000	Yes	No	2.00
206	20.60	36.95	61.90	2.49	0.50	1.17	39.18	60.20	99.39	4.000	Yes	No	2.00
207	20.70	35.66	64.44	2.52	0.50	1.17	38.34	60.59	98.93	4.000	Yes	No	2.00
208	20.80	35.84	68.47	2.57	0.49	1.16	40.60	62.13	102.74	4.000	Yes	No	2.00
209	20.90	33.79	75.15	2.65	0.49	1.16	39.46	0.00	39.46	4.000	Yes	Yes	2.00
210	21.00	28.53	84.12	2.76	0.51	1.17	31.48	0.00	31.48	4.000	Yes	Yes	2.00
211	21.10	22.40	93.60	2.88	0.54	1.17	23.41	0.00	23.41	4.000	Yes	Yes	2.00
212	21.20	18.70	99.37	2.95	0.55	1.18	19.47	0.00	19.47	4.000	Yes	Yes	2.00
213	21.30	17.11	100.00	2.98	0.55	1.17	19.33	0.00	19.33	4.000	No	Yes	2.00
214	21.40	16.52	100.00	2.99	0.55	1.17	18.10	0.00	18.10	4.000	No	Yes	2.00
215	21.50	15.83	100.00	3.00	0.55	1.17	17.46	0.00	17.46	4.000	No	Yes	2.00
216	21.60	15.40	100.00	3.01	0.56	1.17	16.95	0.00	16.95	4.000	No	Yes	2.00
217	21.70	15.00	100.00	3.01	0.56	1.17	16.61	0.00	16.61	4.000	No	Yes	2.00
218	21.80	14.79	100.00	3.03	0.56	1.17	16.07	0.00	16.07	4.000	No	Yes	2.00
219	21.90	15.25	100.00	3.04	0.56	1.16	16.16	0.00	16.16	4.000	No	Yes	2.00
220	22.00	15.77	100.00	3.04	0.55	1.16	18.01	0.00	18.01	4.000	No	Yes	2.00
221	22.10	16.13	100.00	3.04	0.55	1.16	17.68	0.00	17.68	4.000	No	Yes	2.00
222	22.20	16.33	100.00	3.03	0.56	1.16	17.20	0.00	17.20	4.000	No	Yes	2.00
223	22.30	17.20	100.00	2.98	0.55	1.15	18.59	0.00	18.59	4.000	No	Yes	2.00
224	22.40	18.93	96.89	2.92	0.55	1.15	20.36	0.00	20.36	4.000	No	Yes	2.00
225	22.50	20.75	92.85	2.87	0.54	1.14	22.64	0.00	22.64	4.000	No	Yes	2.00
226	22.60	22.36	89.66	2.83	0.53	1.14	24.29	0.00	24.29	4.000	No	Yes	2.00
227	22.70	23.55	87.46	2.81	0.53	1.14	25.37	0.00	25.37	4.000	No	Yes	2.00
228	22.80	24.27	86.39	2.79	0.53	1.14	26.30	0.00	26.30	4.000	No	Yes	2.00
229	22.90	24.79	85.59	2.78	0.53	1.13	26.45	0.00	26.45	4.000	No	Yes	2.00
230	23.00	25.40	84.03	2.76	0.53	1.13	26.88	0.00	26.88	4.000	No	Yes	2.00
231	23.10	26.63	81.45	2.73	0.52	1.13	28.08	0.00	28.08	4.000	No	Yes	2.00
232	23.20	27.97	80.09	2.71	0.52	1.13	30.16	0.00	30.16	4.000	No	Yes	2.00
233	23.30	28.02	81.76	2.73	0.52	1.12	30.94	0.00	30.94	4.000	No	Yes	2.00
234	23.40	25.97	86.34	2.79	0.52	1.12	28.07	0.00	28.07	4.000	No	Yes	2.00
235	23.50	22.41	92.35	2.87	0.54	1.12	23.60	0.00	23.60	4.000	No	Yes	2.00
236	23.60	19.33	97.12	2.93	0.55	1.12	19.65	0.00	19.65	4.000	No	Yes	2.00
237	23.70	17.40	99.36	2.95	0.55	1.12	18.29	0.00	18.29	4.000	No	Yes	2.00
238	23.80	16.53	99.61	2.96	0.55	1.12	17.44	0.00	17.44	4.000	No	Yes	2.00
239	23.90	16.15	99.70	2.96	0.56	1.12	16.82	0.00	16.82	4.000	No	Yes	2.00
240	24.00	15.80	100.00	2.97	0.56	1.12	17.01	0.00	17.01	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
241	24.10	14.52	100.00	3.01	0.56	1.12	16.24	0.00	16.24	4.000	No	Yes	2.00
242	24.20	11.33	100.00	3.12	0.57	1.12	12.75	0.00	12.75	4.000	No	Yes	2.00
243	24.30	8.08	100.00	3.26	0.59	1.12	6.92	0.00	6.92	4.000	No	Yes	2.00
244	24.40	5.93	100.00	3.41	0.60	1.12	5.95	0.00	5.95	4.000	No	Yes	2.00
245	24.50	5.62	100.00	3.42	0.60	1.12	5.94	0.00	5.94	4.000	No	Yes	2.00
246	24.60	5.62	100.00	3.41	0.60	1.12	5.94	0.00	5.94	4.000	No	Yes	2.00
247	24.70	5.77	100.00	3.40	0.60	1.12	5.93	0.00	5.93	4.000	No	Yes	2.00
248	24.80	6.24	100.00	3.37	0.60	1.11	6.40	0.00	6.40	4.000	No	Yes	2.00
249	24.90	6.78	100.00	3.35	0.59	1.11	7.38	0.00	7.38	4.000	No	Yes	2.00
250	25.00	7.16	100.00	3.34	0.59	1.11	7.58	0.00	7.58	4.000	No	Yes	2.00
251	25.10	7.19	100.00	3.36	0.59	1.11	7.57	0.00	7.57	4.000	No	Yes	2.00
252	25.20	6.84	100.00	3.40	0.59	1.11	7.43	0.00	7.43	4.000	No	Yes	2.00
253	25.30	6.30	100.00	3.45	0.60	1.11	6.44	0.00	6.44	4.000	No	Yes	2.00
254	25.40	5.81	100.00	3.49	0.60	1.10	5.86	0.00	5.86	4.000	No	Yes	2.00
255	25.50	5.62	100.00	3.50	0.60	1.10	5.86	0.00	5.86	4.000	No	Yes	2.00
256	25.60	5.62	100.00	3.50	0.60	1.10	5.85	0.00	5.85	4.000	No	Yes	2.00
257	25.70	5.62	100.00	3.50	0.60	1.10	5.84	0.00	5.84	4.000	No	Yes	2.00
258	25.80	5.62	100.00	3.49	0.60	1.10	5.83	0.00	5.83	4.000	No	Yes	2.00
259	25.90	5.74	100.00	3.47	0.60	1.10	5.82	0.00	5.82	4.000	No	Yes	2.00
260	26.00	6.01	100.00	3.43	0.60	1.09	6.18	0.00	6.18	4.000	No	Yes	2.00
261	26.10	6.06	100.00	3.42	0.60	1.09	6.63	0.00	6.63	4.000	No	Yes	2.00
262	26.20	5.94	100.00	3.44	0.60	1.09	5.96	0.00	5.96	4.000	No	Yes	2.00
263	26.30	5.68	100.00	3.48	0.60	1.09	5.79	0.00	5.79	4.000	No	Yes	2.00
264	26.40	5.62	100.00	3.49	0.60	1.09	5.78	0.00	5.78	4.000	No	Yes	2.00
265	26.50	5.72	100.00	3.49	0.60	1.09	5.77	0.00	5.77	4.000	No	Yes	2.00
266	26.60	6.14	100.00	3.44	0.60	1.09	6.07	0.00	6.07	4.000	No	Yes	2.00
267	26.70	6.68	100.00	3.40	0.59	1.08	7.04	0.00	7.04	4.000	No	Yes	2.00
268	26.80	7.11	100.00	3.37	0.59	1.08	7.39	0.00	7.39	4.000	No	Yes	2.00
269	26.90	7.23	100.00	3.39	0.59	1.08	7.37	0.00	7.37	4.000	No	Yes	2.00
270	27.00	7.58	100.00	3.39	0.59	1.08	7.38	0.00	7.38	4.000	No	Yes	2.00
271	27.10	8.22	100.00	3.37	0.59	1.08	8.39	0.00	8.39	4.000	No	Yes	2.00
272	27.20	9.74	100.00	3.31	0.59	1.07	9.29	0.00	9.29	4.000	No	Yes	2.00
273	27.30	13.33	100.00	3.16	0.57	1.07	11.94	0.00	11.94	4.000	No	Yes	2.00
274	27.40	19.91	99.77	2.96	0.55	1.07	19.14	0.00	19.14	4.000	No	Yes	2.00
275	27.50	30.24	82.08	2.74	0.52	1.06	28.96	0.00	28.96	4.000	No	Yes	2.00
276	27.60	41.52	69.51	2.58	0.49	1.05	42.65	62.94	105.60	0.145	No	No	0.16
277	27.70	49.24	64.82	2.52	0.46	1.05	52.46	64.72	117.18	0.165	No	No	0.18
278	27.80	49.82	67.45	2.56	0.46	1.05	51.58	65.09	116.67	0.164	No	No	0.18
279	27.90	44.25	74.10	2.64	0.48	1.05	44.15	0.00	44.15	4.000	No	Yes	2.00
280	28.00	36.48	81.41	2.73	0.50	1.05	35.84	0.00	35.84	4.000	No	Yes	2.00
281	28.10	29.33	88.01	2.81	0.52	1.05	28.50	0.00	28.50	4.000	No	Yes	2.00
282	28.20	23.96	93.78	2.88	0.54	1.05	22.93	0.00	22.93	4.000	No	Yes	2.00
283	28.30	19.51	100.00	2.97	0.55	1.05	19.85	0.00	19.85	4.000	No	Yes	2.00
284	28.40	15.84	100.00	3.08	0.56	1.05	15.24	0.00	15.24	4.000	No	Yes	2.00
285	28.50	12.93	100.00	3.19	0.57	1.05	12.00	0.00	12.00	4.000	No	Yes	2.00
286	28.60	12.75	100.00	3.23	0.58	1.05	11.16	0.00	11.16	4.000	No	Yes	2.00
287	28.70	15.29	100.00	3.15	0.56	1.04	14.62	0.00	14.62	4.000	No	Yes	2.00
288	28.80	18.82	100.00	3.06	0.55	1.04	19.42	0.00	19.42	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
289	28.90	20.53	100.00	3.01	0.54	1.04	21.47	0.00	21.47	4.000	No	Yes	2.00
290	29.00	20.27	100.00	3.01	0.55	1.04	19.58	0.00	19.58	4.000	No	Yes	2.00
291	29.10	18.46	100.00	3.05	0.55	1.04	18.56	0.00	18.56	4.000	No	Yes	2.00
292	29.20	16.60	100.00	3.10	0.56	1.04	16.07	0.00	16.07	4.000	No	Yes	2.00
293	29.30	16.51	100.00	3.07	0.57	1.03	14.08	0.00	14.08	4.000	No	Yes	2.00
294	29.40	20.13	97.68	2.93	0.55	1.03	18.23	0.00	18.23	4.000	No	Yes	2.00
295	29.50	27.09	83.80	2.76	0.53	1.03	26.52	0.00	26.52	4.000	No	Yes	2.00
296	29.60	33.16	75.69	2.66	0.51	1.03	34.21	0.00	34.21	4.000	No	Yes	2.00
297	29.70	36.69	73.12	2.63	0.50	1.02	35.74	0.00	35.74	4.000	No	Yes	2.00
298	29.80	40.80	72.97	2.62	0.50	1.02	36.61	0.00	36.61	4.000	No	Yes	2.00
299	29.90	48.32	71.45	2.61	0.48	1.02	45.88	0.00	45.88	4.000	Yes	Yes	2.00
300	30.00	59.72	65.15	2.53	0.45	1.02	57.17	66.15	123.32	4.000	Yes	No	2.00
301	30.10	73.28	56.39	2.42	0.43	1.02	69.17	66.90	136.07	4.000	Yes	No	2.00
302	30.20	85.57	48.79	2.32	0.40	1.01	84.51	67.79	152.29	4.000	Yes	No	2.00
303	30.30	94.24	45.65	2.28	0.39	1.01	92.05	68.00	160.05	4.000	Yes	No	2.00
304	30.40	96.38	46.96	2.30	0.38	1.01	93.64	69.18	162.82	4.000	Yes	No	2.00
305	30.50	93.45	50.27	2.34	0.39	1.01	90.24	70.04	160.29	4.000	Yes	No	2.00
306	30.60	85.88	55.47	2.41	0.40	1.01	83.33	70.45	153.78	4.000	Yes	No	2.00
307	30.70	75.59	61.76	2.48	0.42	1.01	71.73	69.37	141.10	4.000	Yes	No	2.00
308	30.80	64.96	67.53	2.56	0.44	1.01	60.63	67.72	128.34	4.000	Yes	No	2.00
309	30.90	58.02	69.97	2.59	0.46	1.00	52.79	65.99	118.77	4.000	Yes	No	2.00
310	31.00	57.76	66.44	2.54	0.46	1.00	51.76	64.91	116.66	4.000	Yes	No	2.00
311	31.10	64.29	57.66	2.43	0.45	1.00	59.66	64.71	124.36	4.000	Yes	No	2.00
312	31.20	74.72	47.68	2.31	0.43	1.00	71.12	63.72	134.84	4.000	Yes	No	2.00
313	31.30	84.37	40.44	2.22	0.42	1.00	81.10	61.82	142.92	4.000	Yes	No	2.00
314	31.40	91.02	36.66	2.17	0.41	1.00	86.74	60.08	146.82	4.000	Yes	No	2.00
315	31.50	94.21	35.09	2.15	0.41	1.00	89.67	59.26	148.93	0.282	No	No	0.31
316	31.60	94.73	34.43	2.14	0.41	1.00	89.81	58.63	148.44	0.279	No	No	0.31
317	31.70	92.99	34.86	2.15	0.41	0.99	87.90	58.64	146.53	0.268	No	No	0.29
318	31.80	89.90	36.58	2.17	0.41	0.99	84.43	59.47	143.90	4.000	Yes	No	2.00
319	31.90	86.48	39.01	2.20	0.42	0.99	80.78	60.66	141.43	4.000	Yes	No	2.00
320	32.00	83.14	42.11	2.24	0.42	0.99	77.95	62.21	140.17	4.000	Yes	No	2.00
321	32.10	79.62	46.13	2.29	0.42	0.99	74.74	63.84	138.58	4.000	Yes	No	2.00
322	32.20	75.05	50.97	2.35	0.43	0.99	70.59	65.14	135.73	4.000	Yes	No	2.00
323	32.30	69.21	55.58	2.41	0.44	0.99	64.83	65.42	130.25	4.000	Yes	No	2.00
324	32.40	63.30	58.45	2.44	0.45	0.98	58.08	64.52	122.60	4.000	Yes	No	2.00
325	32.50	60.94	57.47	2.43	0.46	0.98	53.77	63.02	116.79	0.165	No	No	0.18
326	32.60	65.02	51.62	2.36	0.46	0.98	57.98	62.05	120.03	0.171	No	No	0.19
327	32.70	74.05	44.98	2.27	0.44	0.98	69.27	61.80	131.07	0.201	No	No	0.22
328	32.80	83.30	41.26	2.23	0.42	0.98	78.79	61.84	140.63	0.237	No	No	0.26
329	32.90	89.30	40.98	2.22	0.41	0.98	83.60	62.82	146.42	0.267	No	No	0.29
330	33.00	94.12	41.18	2.23	0.40	0.98	85.76	63.49	149.25	0.284	No	No	0.31
331	33.10	101.14	39.38	2.20	0.39	0.98	91.99	63.63	155.61	0.331	No	No	0.36
332	33.20	112.44	35.44	2.16	0.38	0.98	102.92	62.60	165.52	0.437	No	No	0.48
333	33.30	126.20	31.60	2.11	0.36	0.98	117.02	61.22	178.23	0.678	No	No	0.75
334	33.40	137.62	29.75	2.08	0.34	0.98	130.14	61.29	191.42	1.206	No	No	1.35
335	33.50	143.17	29.92	2.09	0.33	0.98	134.56	62.44	197.01	1.605	No	No	1.79
336	33.60	142.56	31.12	2.10	0.34	0.98	132.19	63.74	195.93	1.515	No	No	1.69

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
337	33.70	140.15	32.01	2.11	0.34	0.98	128.05	64.10	192.15	1.249	No	No	1.39
338	33.80	138.78	32.16	2.11	0.34	0.97	127.42	64.16	191.58	1.215	No	No	1.35
339	33.90	138.19	32.17	2.11	0.34	0.97	127.94	64.29	192.24	1.255	No	No	1.40
340	34.00	135.99	32.80	2.12	0.34	0.97	126.03	64.70	190.72	1.165	No	No	1.30
341	34.10	131.92	34.21	2.14	0.35	0.97	120.90	65.29	186.19	0.944	No	No	1.05
342	34.20	126.82	35.88	2.16	0.35	0.97	116.20	66.07	182.27	0.798	No	No	0.88
343	34.30	122.27	37.41	2.18	0.36	0.97	111.45	66.50	177.95	0.671	No	No	0.74
344	34.40	118.79	38.39	2.19	0.37	0.97	107.89	66.58	174.47	0.589	No	No	0.65
345	34.50	116.72	38.68	2.20	0.37	0.97	106.15	66.42	172.57	0.550	No	No	0.61
346	34.60	116.13	38.35	2.19	0.37	0.96	105.33	65.93	171.26	0.526	No	No	0.58
347	34.70	116.42	37.83	2.19	0.37	0.96	105.90	65.60	171.50	0.530	No	No	0.58
348	34.80	116.08	37.64	2.18	0.37	0.96	106.61	65.59	172.19	0.543	No	No	0.60
349	34.90	113.21	38.23	2.19	0.37	0.96	104.04	65.52	169.57	0.497	No	No	0.55
350	35.00	107.12	39.94	2.21	0.38	0.96	97.59	65.43	163.02	0.405	No	No	0.44
351	35.10	98.36	43.05	2.25	0.39	0.96	89.45	65.70	155.15	0.327	No	No	0.36
352	35.20	88.33	47.50	2.31	0.41	0.95	79.59	65.83	145.42	0.261	No	No	0.28
353	35.30	78.11	52.36	2.37	0.43	0.95	69.74	65.51	135.24	0.215	No	No	0.23
354	35.40	70.66	55.42	2.41	0.45	0.95	61.16	64.36	125.52	0.185	No	No	0.20
355	35.50	68.31	54.81	2.40	0.45	0.95	58.96	63.54	122.50	0.177	No	No	0.19
356	35.60	71.04	51.23	2.35	0.44	0.95	63.06	63.24	126.30	0.187	No	No	0.20
357	35.70	76.04	47.57	2.31	0.44	0.95	68.36	62.95	131.30	0.202	No	No	0.22
358	35.80	80.43	45.46	2.28	0.43	0.95	72.32	62.85	135.17	0.215	No	No	0.23
359	35.90	83.79	44.92	2.27	0.42	0.94	74.78	63.17	137.95	0.226	No	No	0.24
360	36.00	86.97	44.98	2.27	0.42	0.94	77.28	63.84	141.12	0.240	No	No	0.26
361	36.10	90.89	45.13	2.28	0.41	0.94	80.77	64.82	145.59	0.262	No	No	0.28
362	36.20	95.24	45.49	2.28	0.40	0.94	85.25	66.17	151.42	0.299	No	No	0.32
363	36.30	98.94	46.33	2.29	0.39	0.94	88.96	67.61	156.57	0.339	No	No	0.37
364	36.40	100.43	47.71	2.31	0.39	0.94	90.66	68.83	159.48	0.366	No	No	0.40
365	36.50	99.89	49.44	2.33	0.39	0.94	89.09	69.32	158.41	0.356	No	No	0.39
366	36.60	98.07	51.54	2.36	0.39	0.94	87.22	69.84	157.07	4.000	Yes	No	2.00
367	36.70	95.06	54.30	2.39	0.39	0.94	85.43	70.55	155.99	4.000	Yes	No	2.00
368	36.80	89.45	58.10	2.44	0.40	0.94	80.64	70.68	151.32	4.000	Yes	No	2.00
369	36.90	80.70	63.33	2.50	0.42	0.93	71.71	69.82	141.53	4.000	Yes	No	2.00
370	37.00	69.82	70.13	2.59	0.44	0.93	61.46	68.55	130.01	4.000	Yes	No	2.00
371	37.10	58.94	77.71	2.68	0.46	0.93	51.02	0.00	51.02	4.000	Yes	Yes	2.00
372	37.20	50.59	83.81	2.76	0.48	0.92	42.26	0.00	42.26	4.000	Yes	Yes	2.00
373	37.30	46.04	85.90	2.79	0.49	0.92	38.94	0.00	38.94	4.000	No	Yes	2.00
374	37.40	45.72	82.82	2.75	0.49	0.92	38.74	0.00	38.74	4.000	No	Yes	2.00
375	37.50	48.88	75.85	2.66	0.49	0.92	41.24	0.00	41.24	4.000	No	Yes	2.00
376	37.60	54.47	67.97	2.56	0.47	0.92	47.17	63.93	111.09	0.154	No	No	0.16
377	37.70	60.92	61.90	2.49	0.46	0.92	53.40	64.22	117.62	0.166	No	No	0.18
378	37.80	66.48	58.57	2.44	0.45	0.92	58.19	64.59	122.78	0.178	No	No	0.19
379	37.90	71.26	56.22	2.42	0.44	0.92	61.76	64.80	126.56	0.188	No	No	0.20
380	38.00	76.37	52.95	2.37	0.44	0.92	65.96	64.73	130.69	0.200	No	No	0.21
381	38.10	82.38	48.32	2.32	0.43	0.92	71.59	64.16	135.75	0.217	No	No	0.23
382	38.20	88.96	43.74	2.26	0.42	0.92	77.58	63.17	140.75	0.238	No	No	0.26
383	38.30	94.06	41.28	2.23	0.41	0.92	83.31	62.96	146.27	0.266	No	No	0.29
384	38.40	96.38	41.26	2.23	0.41	0.92	85.00	63.36	148.36	0.278	No	No	0.30

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
385	38.50	95.22	42.89	2.25	0.41	0.92	83.58	64.13	147.71	0.274	No	No	0.30
386	38.60	91.50	44.94	2.27	0.41	0.92	79.97	64.50	144.47	0.256	No	No	0.28
387	38.70	86.76	46.89	2.30	0.42	0.92	74.81	64.27	139.08	0.231	No	No	0.25
388	38.80	82.49	48.38	2.32	0.43	0.91	70.66	63.95	134.61	0.213	No	No	0.23
389	38.90	79.99	48.81	2.32	0.43	0.91	68.30	63.54	131.84	0.203	No	No	0.22
390	39.00	79.66	47.67	2.31	0.44	0.91	67.89	62.88	130.77	0.200	No	No	0.21
391	39.10	80.98	45.18	2.28	0.44	0.91	69.51	61.97	131.49	0.202	No	No	0.22
392	39.20	81.39	43.83	2.26	0.43	0.91	71.55	61.70	133.25	4.000	Yes	No	2.00
393	39.30	77.05	46.44	2.29	0.44	0.91	68.74	62.47	131.21	4.000	Yes	No	2.00
394	39.40	68.00	53.80	2.38	0.46	0.90	57.87	62.87	120.74	4.000	Yes	No	2.00
395	39.50	55.58	64.75	2.52	0.47	0.90	47.60	63.31	110.91	4.000	Yes	No	2.00
396	39.60	43.51	77.12	2.68	0.50	0.89	36.09	0.00	36.09	4.000	Yes	Yes	2.00
397	39.70	32.08	90.57	2.84	0.53	0.89	26.46	0.00	26.46	4.000	Yes	Yes	2.00
398	39.80	24.49	100.00	2.98	0.55	0.88	18.09	0.00	18.09	4.000	Yes	Yes	2.00
399	39.90	25.69	100.00	2.97	0.56	0.88	16.63	0.00	16.63	4.000	No	Yes	2.00
400	40.00	28.88	96.58	2.92	0.52	0.89	29.44	0.00	29.44	4.000	No	Yes	2.00
401	40.10	26.02	100.00	2.96	0.53	0.88	26.12	0.00	26.12	4.000	No	Yes	2.00
402	40.20	17.22	100.00	3.14	0.58	0.87	9.42	0.00	9.42	4.000	No	Yes	2.00
403	40.30	10.69	100.00	3.39	0.59	0.87	7.23	0.00	7.23	4.000	No	Yes	2.00
404	40.40	11.62	100.00	3.36	0.58	0.87	9.62	0.00	9.62	4.000	No	Yes	2.00
405	40.50	14.83	100.00	3.24	0.58	0.87	11.70	0.00	11.70	4.000	No	Yes	2.00
406	40.60	19.14	100.00	3.10	0.56	0.87	15.17	0.00	15.17	4.000	No	Yes	2.00
407	40.70	24.64	100.00	2.97	0.54	0.87	20.33	0.00	20.33	4.000	No	Yes	2.00
408	40.80	30.34	92.04	2.86	0.53	0.87	25.42	0.00	25.42	4.000	No	Yes	2.00
409	40.90	34.36	86.65	2.80	0.52	0.88	29.45	0.00	29.45	4.000	No	Yes	2.00
410	41.00	35.62	84.72	2.77	0.52	0.88	30.39	0.00	30.39	4.000	No	Yes	2.00
411	41.10	35.36	84.64	2.77	0.52	0.87	28.49	0.00	28.49	4.000	No	Yes	2.00
412	41.20	35.52	84.55	2.77	0.52	0.87	28.68	0.00	28.68	4.000	No	Yes	2.00
413	41.30	37.77	83.42	2.76	0.52	0.87	30.71	0.00	30.71	4.000	No	Yes	2.00
414	41.40	39.51	83.87	2.76	0.51	0.87	34.10	0.00	34.10	4.000	No	Yes	2.00
415	41.50	39.75	86.36	2.79	0.51	0.87	32.99	0.00	32.99	4.000	No	Yes	2.00
416	41.60	38.24	90.74	2.85	0.51	0.87	31.20	0.00	31.20	4.000	No	Yes	2.00
417	41.70	37.40	93.69	2.88	0.51	0.87	30.17	0.00	30.17	4.000	No	Yes	2.00
418	41.80	40.17	91.71	2.86	0.51	0.87	30.75	0.00	30.75	4.000	Yes	Yes	2.00
419	41.90	50.73	81.33	2.73	0.49	0.87	38.09	0.00	38.09	4.000	Yes	Yes	2.00
420	42.00	69.20	66.09	2.54	0.45	0.88	57.01	66.33	123.35	4.000	Yes	No	2.00
421	42.10	94.71	49.57	2.33	0.41	0.89	78.13	66.49	144.62	4.000	Yes	No	2.00
422	42.20	121.87	35.72	2.16	0.38	0.90	104.28	63.20	167.49	4.000	Yes	No	2.00
423	42.30	147.28	26.64	2.05	0.35	0.90	128.05	55.67	183.72	4.000	Yes	No	2.00
424	42.40	168.54	22.28	1.99	0.34	0.91	144.95	49.18	194.13	4.000	Yes	No	2.00
425	42.50	184.42	20.76	1.97	0.32	0.91	160.65	47.44	208.09	3.079	No	No	2.00
426	42.60	194.06	20.68	1.97	0.30	0.91	170.70	48.63	219.33	4.000	No	No	2.00
427	42.70	194.52	21.85	1.99	0.30	0.92	171.21	52.05	223.26	4.000	No	No	2.00
428	42.80	186.27	24.07	2.01	0.31	0.91	162.09	56.30	218.39	4.000	Yes	No	2.00
429	42.90	172.77	27.13	2.05	0.32	0.91	148.37	60.36	208.73	4.000	Yes	No	2.00
430	43.00	157.23	30.94	2.10	0.33	0.90	134.61	63.98	198.59	4.000	Yes	No	2.00
431	43.10	141.54	35.42	2.16	0.35	0.90	120.04	66.46	186.49	4.000	Yes	No	2.00
432	43.20	127.00	40.72	2.22	0.37	0.89	106.12	68.12	174.24	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
433	43.30	114.88	46.73	2.30	0.38	0.89	95.66	69.57	165.23	4.000	Yes	No	2.00
434	43.40	105.17	53.28	2.38	0.39	0.89	87.77	70.76	158.53	4.000	Yes	No	2.00
435	43.50	96.99	59.13	2.45	0.40	0.88	80.40	70.97	151.37	4.000	Yes	No	2.00
436	43.60	87.91	63.40	2.51	0.41	0.88	74.06	70.50	144.57	4.000	Yes	No	2.00
437	43.70	82.13	64.04	2.51	0.44	0.87	63.87	67.78	131.64	4.000	Yes	No	2.00
438	43.80	82.78	60.06	2.46	0.43	0.87	65.12	66.99	132.11	4.000	Yes	No	2.00
439	43.90	91.57	53.09	2.38	0.42	0.87	75.39	67.33	142.72	4.000	Yes	No	2.00
440	44.00	103.19	46.41	2.29	0.40	0.88	86.34	66.98	153.33	4.000	Yes	No	2.00
441	44.10	111.95	41.81	2.24	0.39	0.88	95.01	66.22	161.23	4.000	Yes	No	2.00
442	44.20	116.80	40.11	2.21	0.38	0.88	97.88	65.63	163.51	4.000	Yes	No	2.00
443	44.30	116.61	42.68	2.25	0.38	0.88	98.85	67.79	166.64	4.000	Yes	No	2.00
444	44.40	111.71	48.71	2.32	0.38	0.88	94.44	70.35	164.79	4.000	Yes	No	2.00
445	44.50	102.58	55.82	2.41	0.39	0.88	85.05	71.06	156.11	4.000	Yes	No	2.00
446	44.60	93.13	60.70	2.47	0.41	0.87	74.94	69.95	144.89	4.000	Yes	No	2.00
447	44.70	89.79	60.17	2.46	0.42	0.86	69.62	68.29	137.91	4.000	Yes	No	2.00
448	44.80	96.85	53.34	2.38	0.41	0.87	76.02	67.61	143.63	4.000	Yes	No	2.00
449	44.90	113.10	43.90	2.26	0.39	0.87	92.89	67.12	160.01	4.000	Yes	No	2.00
450	45.00	132.27	36.50	2.17	0.36	0.88	111.55	65.65	177.20	4.000	Yes	No	2.00
451	45.10	147.43	33.07	2.13	0.34	0.89	125.95	65.03	190.98	4.000	Yes	No	2.00
452	45.20	155.41	32.85	2.12	0.33	0.89	132.74	66.21	198.94	1.783	No	No	1.89
453	45.30	156.28	34.36	2.14	0.33	0.89	132.72	68.09	200.81	4.000	Yes	No	2.00
454	45.40	151.54	36.78	2.17	0.33	0.89	128.27	69.79	198.05	4.000	Yes	No	2.00
455	45.50	142.44	40.28	2.22	0.34	0.88	120.06	71.13	191.19	4.000	Yes	No	2.00
456	45.60	129.99	45.48	2.28	0.36	0.88	108.37	72.07	180.44	4.000	Yes	No	2.00
457	45.70	115.63	52.15	2.36	0.38	0.87	95.16	72.25	167.41	4.000	Yes	No	2.00
458	45.80	101.57	58.95	2.45	0.40	0.86	82.16	71.40	153.55	4.000	Yes	No	2.00
459	45.90	89.43	64.02	2.51	0.42	0.86	71.55	69.96	141.51	4.000	Yes	No	2.00
460	46.00	80.36	66.11	2.54	0.43	0.85	63.62	68.24	131.86	0.204	No	No	0.22
461	46.10	75.66	64.80	2.52	0.45	0.85	58.72	66.50	125.22	4.000	Yes	No	2.00
462	46.20	75.96	60.54	2.47	0.45	0.84	59.31	65.50	124.81	4.000	Yes	No	2.00
463	46.30	81.99	53.84	2.39	0.44	0.85	64.03	64.55	128.58	4.000	Yes	No	2.00
464	46.40	93.65	45.34	2.28	0.43	0.85	73.56	63.10	136.66	4.000	Yes	No	2.00
465	46.50	110.56	36.06	2.16	0.41	0.86	88.39	59.91	148.30	4.000	Yes	No	2.00
466	46.60	129.39	29.02	2.08	0.38	0.86	106.59	55.48	162.08	4.000	Yes	No	2.00
467	46.70	144.05	26.89	2.05	0.36	0.87	121.62	54.92	176.54	0.636	No	No	0.68
468	46.80	149.85	29.59	2.08	0.35	0.87	126.50	60.31	186.81	0.971	No	No	1.04
469	46.90	147.45	35.00	2.15	0.34	0.87	122.35	66.51	188.86	1.067	No	No	1.14
470	47.00	142.18	40.67	2.22	0.35	0.87	116.05	70.49	186.54	0.959	No	No	1.03
471	47.10	138.12	44.77	2.27	0.35	0.87	113.12	72.81	185.93	0.934	No	No	1.00
472	47.20	136.30	46.47	2.29	0.35	0.87	111.80	73.57	185.38	0.911	No	No	0.97
473	47.30	137.24	45.56	2.28	0.35	0.87	111.11	72.82	183.93	0.856	No	No	0.92
474	47.40	142.58	42.29	2.24	0.35	0.87	115.26	71.58	186.83	0.972	No	No	1.04
475	47.50	152.84	37.72	2.18	0.34	0.87	125.39	70.06	195.45	1.478	No	No	1.56
476	47.60	165.80	33.53	2.13	0.32	0.88	137.73	68.17	205.90	2.682	No	No	2.00
477	47.70	177.89	30.83	2.10	0.31	0.88	149.19	66.83	216.02	4.000	No	No	2.00
478	47.80	187.02	29.68	2.08	0.30	0.88	157.34	66.66	224.00	4.000	No	No	2.00
479	47.90	192.69	29.11	2.08	0.29	0.89	161.95	66.60	228.55	4.000	No	No	2.00
480	48.00	196.25	28.50	2.07	0.29	0.89	164.19	65.95	230.14	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
481	48.10	199.18	27.61	2.06	0.29	0.89	166.55	64.71	231.27	4.000	No	No	2.00
482	48.20	202.36	26.74	2.05	0.29	0.89	169.34	63.49	232.84	4.000	No	No	2.00
483	48.30	204.97	26.21	2.04	0.29	0.89	172.28	62.92	235.20	4.000	No	No	2.00
484	48.40	206.02	26.39	2.04	0.28	0.89	173.24	63.49	236.73	4.000	No	No	2.00
485	48.50	205.06	27.28	2.05	0.28	0.89	172.02	65.10	237.12	4.000	No	No	2.00
486	48.60	202.72	28.43	2.07	0.28	0.89	169.66	66.88	236.54	4.000	No	No	2.00
487	48.70	200.81	29.22	2.08	0.29	0.88	166.87	67.77	234.64	4.000	No	No	2.00
488	48.80	200.45	29.33	2.08	0.29	0.88	166.67	67.92	234.59	4.000	No	No	2.00
489	48.90	202.19	28.81	2.07	0.29	0.88	168.38	67.32	235.70	4.000	No	No	2.00
490	49.00	205.17	28.02	2.06	0.28	0.88	171.16	66.38	237.54	4.000	No	No	2.00
491	49.10	208.80	27.28	2.05	0.28	0.88	174.26	65.53	239.79	4.000	No	No	2.00
492	49.20	212.77	26.74	2.05	0.28	0.88	177.78	65.07	242.85	4.000	No	No	2.00
493	49.30	217.38	26.17	2.04	0.27	0.89	181.55	64.51	246.07	4.000	No	No	2.00
494	49.40	221.74	25.65	2.03	0.27	0.89	186.52	64.23	250.75	4.000	No	No	2.00
495	49.50	222.23	25.63	2.03	0.26	0.89	189.44	64.72	254.16	4.000	No	No	2.00
496	49.60	216.25	26.42	2.04	0.27	0.88	182.63	65.27	247.90	4.000	No	No	2.00
497	49.70	208.44	27.38	2.05	0.29	0.88	169.74	64.86	234.60	4.000	No	No	2.00
498	49.80	204.58	28.01	2.06	0.29	0.88	167.68	65.71	233.40	4.000	No	No	2.00
499	49.90	205.34	28.10	2.06	0.28	0.88	171.77	66.67	238.44	4.000	No	No	2.00

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q_t :	Total cone resistance
FC:	Fines content (%)
I_c :	Soil behavior type index
m:	Stress exponent
C_N :	Overburden correction factor
q_{c1N} :	Normalized and adjusted cone resistance
Δq_{c1N} :	Cone resistance correction factor due to fines
$q_{c1N,cs}$:	Normalized and adjusted cone resistance
CRR _{7.5} :	Cyclic resistance ratio for $M_w=7.5$
FS:	Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
0.10	2.00	0.00	0.00	0.10	0.00	0.20	2.00	0.00	0.00	0.10	0.00
0.30	2.00	0.00	0.00	0.10	0.00	0.40	2.00	0.00	0.00	0.10	0.00
0.50	2.00	0.00	0.00	0.10	0.00	0.60	2.00	0.00	0.00	0.10	0.00
0.70	2.00	0.00	0.00	0.10	0.00	0.80	2.00	0.00	0.00	0.10	0.00
0.90	2.00	0.00	0.00	0.10	0.00	1.00	2.00	0.00	0.00	0.10	0.00
1.10	2.00	0.00	0.00	0.10	0.00	1.20	2.00	0.00	0.00	0.10	0.00
1.30	2.00	0.00	0.00	0.10	0.00	1.40	2.00	0.00	0.00	0.10	0.00
1.50	2.00	0.00	0.00	0.10	0.00	1.60	2.00	0.00	0.00	0.10	0.00
1.70	2.00	0.00	0.00	0.10	0.00	1.80	2.00	0.00	0.00	0.10	0.00
1.90	2.00	0.00	0.00	0.10	0.00	2.00	2.00	0.00	0.00	0.10	0.00
2.10	2.00	0.00	0.00	0.10	0.00	2.20	2.00	0.00	0.00	0.10	0.00
2.30	2.00	0.00	0.00	0.10	0.00	2.40	2.00	0.00	0.00	0.10	0.00
2.50	2.00	0.00	0.00	0.10	0.00	2.60	2.00	0.00	0.00	0.10	0.00
2.70	2.00	0.00	0.00	0.10	0.00	2.80	2.00	0.00	0.00	0.10	0.00
2.90	2.00	0.00	0.00	0.10	0.00	3.00	2.00	0.00	0.00	0.10	0.00
3.10	2.00	0.00	0.00	0.10	0.00	3.20	2.00	0.00	0.00	0.10	0.00
3.30	2.00	0.00	0.00	0.10	0.00	3.40	2.00	0.00	0.00	0.10	0.00
3.50	2.00	0.00	0.00	0.10	0.00	3.60	2.00	0.00	0.00	0.10	0.00
3.70	2.00	0.00	0.00	0.10	0.00	3.80	2.00	0.00	0.00	0.10	0.00
3.90	2.00	0.00	0.00	0.10	0.00	4.00	2.00	0.00	0.00	0.10	0.00
4.10	2.00	0.00	0.00	0.10	0.00	4.20	2.00	0.00	0.00	0.10	0.00
4.30	2.00	0.00	0.00	0.10	0.00	4.40	2.00	0.00	0.00	0.10	0.00
4.50	2.00	0.00	0.00	0.10	0.00	4.60	2.00	0.00	0.00	0.10	0.00
4.70	2.00	0.00	0.00	0.10	0.00	4.80	2.00	0.00	0.00	0.10	0.00
4.90	2.00	0.00	0.00	0.10	0.00	5.00	2.00	0.00	0.00	0.10	0.00
5.10	2.00	0.00	0.00	0.10	0.00	5.20	2.00	0.00	0.00	0.10	0.00
5.30	2.00	0.00	0.00	0.10	0.00	5.40	2.00	0.00	0.00	0.10	0.00
5.50	2.00	0.00	0.00	0.10	0.00	5.60	2.00	0.00	0.00	0.10	0.00
5.70	2.00	0.00	0.00	0.10	0.00	5.80	2.00	0.00	0.00	0.10	0.00
5.90	2.00	0.00	0.00	0.10	0.00	6.00	2.00	0.00	0.00	0.10	0.00
6.10	2.00	0.00	0.00	0.10	0.00	6.20	2.00	0.00	0.00	0.10	0.00
6.30	2.00	0.00	0.00	0.10	0.00	6.40	2.00	0.00	0.00	0.10	0.00
6.50	2.00	0.00	0.00	0.10	0.00	6.60	2.00	0.00	0.00	0.10	0.00
6.70	2.00	0.00	0.00	0.10	0.00	6.80	2.00	0.00	0.00	0.10	0.00
6.90	2.00	0.00	0.00	0.10	0.00	7.00	2.00	0.00	0.00	0.10	0.00
7.10	2.00	0.00	0.00	0.10	0.00	7.20	2.00	0.00	0.00	0.10	0.00
7.30	2.00	0.00	0.00	0.10	0.00	7.40	2.00	0.00	0.00	0.10	0.00
7.50	2.00	0.00	0.00	0.10	0.00	7.60	2.00	0.00	0.00	0.10	0.00
7.70	2.00	0.00	0.00	0.10	0.00	7.80	2.00	0.00	0.00	0.10	0.00
7.90	2.00	0.00	0.00	0.10	0.00	8.00	2.00	0.00	0.00	0.10	0.00
8.10	2.00	0.00	0.00	0.10	0.00	8.20	2.00	0.00	0.00	0.10	0.00
8.30	2.00	0.00	0.00	0.10	0.00	8.40	2.00	0.00	0.00	0.10	0.00
8.50	2.00	0.00	0.00	0.10	0.00	8.60	2.00	0.00	0.00	0.10	0.00
8.70	2.00	0.00	0.00	0.10	0.00	8.80	2.00	0.00	0.00	0.10	0.00
8.90	2.00	0.00	0.00	0.10	0.00	9.00	2.00	0.00	0.00	0.10	0.00
9.10	2.00	0.00	0.00	0.10	0.00	9.20	2.00	0.00	0.00	0.10	0.00
9.30	2.00	0.00	0.00	0.10	0.00	9.40	2.00	0.00	0.00	0.10	0.00
9.50	2.00	0.00	0.00	0.10	0.00	9.60	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data ::

Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
9.70	2.00	0.00	0.00	0.10	0.00	9.80	2.00	0.00	0.00	0.10	0.00
9.90	2.00	0.00	0.00	0.10	0.00	10.00	2.00	0.00	0.00	0.10	0.00
10.10	2.00	0.00	0.00	0.10	0.00	10.20	2.00	0.00	0.00	0.10	0.00
10.30	2.00	0.00	0.00	0.10	0.00	10.40	2.00	0.00	0.00	0.10	0.00
10.50	2.00	0.00	0.00	0.10	0.00	10.60	2.00	0.00	0.00	0.10	0.00
10.70	2.00	0.00	0.00	0.10	0.00	10.80	2.00	0.00	0.00	0.10	0.00
10.90	2.00	0.00	0.00	0.10	0.00	11.00	2.00	0.00	0.00	0.10	0.00
11.10	2.00	0.00	0.00	0.10	0.00	11.20	2.00	0.00	0.00	0.10	0.00
11.30	2.00	0.00	0.00	0.10	0.00	11.40	0.38	0.62	0.37	0.10	0.16
11.50	0.38	0.62	0.37	0.10	0.16	11.60	0.38	0.62	0.37	0.10	0.15
11.70	0.39	0.61	0.37	0.10	0.15	11.80	0.37	0.63	0.36	0.10	0.16
11.90	0.32	0.68	0.33	0.10	0.17	12.00	0.30	0.70	0.32	0.10	0.17
12.10	0.27	0.73	0.31	0.10	0.18	12.20	0.25	0.75	0.30	0.10	0.19
12.30	0.27	0.73	0.31	0.10	0.18	12.40	0.27	0.73	0.31	0.10	0.18
12.50	0.27	0.73	0.31	0.10	0.18	12.60	0.27	0.73	0.31	0.10	0.18
12.70	2.00	0.00	0.00	0.10	0.00	12.80	2.00	0.00	0.00	0.10	0.00
12.90	2.00	0.00	0.00	0.10	0.00	13.00	2.00	0.00	0.00	0.10	0.00
13.10	2.00	0.00	0.00	0.10	0.00	13.20	2.00	0.00	0.00	0.10	0.00
13.30	2.00	0.00	0.00	0.10	0.00	13.40	2.00	0.00	0.00	0.10	0.00
13.50	2.00	0.00	0.00	0.10	0.00	13.60	2.00	0.00	0.00	0.10	0.00
13.70	2.00	0.00	0.00	0.10	0.00	13.80	2.00	0.00	0.00	0.10	0.00
13.90	2.00	0.00	0.00	0.10	0.00	14.00	2.00	0.00	0.00	0.10	0.00
14.10	2.00	0.00	0.00	0.10	0.00	14.20	2.00	0.00	0.00	0.10	0.00
14.30	2.00	0.00	0.00	0.10	0.00	14.40	2.00	0.00	0.00	0.10	0.00
14.50	2.00	0.00	0.00	0.10	0.00	14.60	2.00	0.00	0.00	0.10	0.00
14.70	2.00	0.00	0.00	0.10	0.00	14.80	2.00	0.00	0.00	0.10	0.00
14.90	2.00	0.00	0.00	0.10	0.00	15.00	2.00	0.00	0.00	0.10	0.00
15.10	2.00	0.00	0.00	0.10	0.00	15.20	2.00	0.00	0.00	0.10	0.00
15.30	2.00	0.00	0.00	0.10	0.00	15.40	2.00	0.00	0.00	0.10	0.00
15.50	2.00	0.00	0.00	0.10	0.00	15.60	2.00	0.00	0.00	0.10	0.00
15.70	2.00	0.00	0.00	0.10	0.00	15.80	2.00	0.00	0.00	0.10	0.00
15.90	2.00	0.00	0.00	0.10	0.00	16.00	2.00	0.00	0.00	0.10	0.00
16.10	2.00	0.00	0.00	0.10	0.00	16.20	2.00	0.00	0.00	0.10	0.00
16.30	2.00	0.00	0.00	0.10	0.00	16.40	2.00	0.00	0.00	0.10	0.00
16.50	2.00	0.00	0.00	0.10	0.00	16.60	2.00	0.00	0.00	0.10	0.00
16.70	2.00	0.00	0.00	0.10	0.00	16.80	2.00	0.00	0.00	0.10	0.00
16.90	2.00	0.00	0.00	0.10	0.00	17.00	2.00	0.00	0.00	0.10	0.00
17.10	2.00	0.00	0.00	0.10	0.00	17.20	2.00	0.00	0.00	0.10	0.00
17.30	2.00	0.00	0.00	0.10	0.00	17.40	2.00	0.00	0.00	0.10	0.00
17.50	2.00	0.00	0.00	0.10	0.00	17.60	2.00	0.00	0.00	0.10	0.00
17.70	2.00	0.00	0.00	0.10	0.00	17.80	2.00	0.00	0.00	0.10	0.00
17.90	2.00	0.00	0.00	0.10	0.00	18.00	2.00	0.00	0.00	0.10	0.00
18.10	2.00	0.00	0.00	0.10	0.00	18.20	2.00	0.00	0.00	0.10	0.00
18.30	2.00	0.00	0.00	0.10	0.00	18.40	2.00	0.00	0.00	0.10	0.00
18.50	2.00	0.00	0.00	0.10	0.00	18.60	2.00	0.00	0.00	0.10	0.00
18.70	2.00	0.00	0.00	0.10	0.00	18.80	2.00	0.00	0.00	0.10	0.00
18.90	2.00	0.00	0.00	0.10	0.00	19.00	2.00	0.00	0.00	0.10	0.00
19.10	2.00	0.00	0.00	0.10	0.00	19.20	0.15	0.85	0.26	0.10	0.18

:: Liquefaction Potential Index calculation data ::

Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
19.30	0.16	0.84	0.26	0.10	0.18	19.40	0.17	0.83	0.26	0.10	0.18
19.50	2.00	0.00	0.00	0.10	0.00	19.60	2.00	0.00	0.00	0.10	0.00
19.70	2.00	0.00	0.00	0.10	0.00	19.80	2.00	0.00	0.00	0.10	0.00
19.90	2.00	0.00	0.00	0.10	0.00	20.00	2.00	0.00	0.00	0.10	0.00
20.10	2.00	0.00	0.00	0.10	0.00	20.20	2.00	0.00	0.00	0.10	0.00
20.30	2.00	0.00	0.00	0.10	0.00	20.40	2.00	0.00	0.00	0.10	0.00
20.50	2.00	0.00	0.00	0.10	0.00	20.60	2.00	0.00	0.00	0.10	0.00
20.70	2.00	0.00	0.00	0.10	0.00	20.80	2.00	0.00	0.00	0.10	0.00
20.90	2.00	0.00	0.00	0.10	0.00	21.00	2.00	0.00	0.00	0.10	0.00
21.10	2.00	0.00	0.00	0.10	0.00	21.20	2.00	0.00	0.00	0.10	0.00
21.30	2.00	0.00	0.00	0.10	0.00	21.40	2.00	0.00	0.00	0.10	0.00
21.50	2.00	0.00	0.00	0.10	0.00	21.60	2.00	0.00	0.00	0.10	0.00
21.70	2.00	0.00	0.00	0.10	0.00	21.80	2.00	0.00	0.00	0.10	0.00
21.90	2.00	0.00	0.00	0.10	0.00	22.00	2.00	0.00	0.00	0.10	0.00
22.10	2.00	0.00	0.00	0.10	0.00	22.20	2.00	0.00	0.00	0.10	0.00
22.30	2.00	0.00	0.00	0.10	0.00	22.40	2.00	0.00	0.00	0.10	0.00
22.50	2.00	0.00	0.00	0.10	0.00	22.60	2.00	0.00	0.00	0.10	0.00
22.70	2.00	0.00	0.00	0.10	0.00	22.80	2.00	0.00	0.00	0.10	0.00
22.90	2.00	0.00	0.00	0.10	0.00	23.00	2.00	0.00	0.00	0.10	0.00
23.10	2.00	0.00	0.00	0.10	0.00	23.20	2.00	0.00	0.00	0.10	0.00
23.30	2.00	0.00	0.00	0.10	0.00	23.40	2.00	0.00	0.00	0.10	0.00
23.50	2.00	0.00	0.00	0.10	0.00	23.60	2.00	0.00	0.00	0.10	0.00
23.70	2.00	0.00	0.00	0.10	0.00	23.80	2.00	0.00	0.00	0.10	0.00
23.90	2.00	0.00	0.00	0.10	0.00	24.00	2.00	0.00	0.00	0.10	0.00
24.10	2.00	0.00	0.00	0.10	0.00	24.20	2.00	0.00	0.00	0.10	0.00
24.30	2.00	0.00	0.00	0.10	0.00	24.40	2.00	0.00	0.00	0.10	0.00
24.50	2.00	0.00	0.00	0.10	0.00	24.60	2.00	0.00	0.00	0.10	0.00
24.70	2.00	0.00	0.00	0.10	0.00	24.80	2.00	0.00	0.00	0.10	0.00
24.90	2.00	0.00	0.00	0.10	0.00	25.00	2.00	0.00	0.00	0.10	0.00
25.10	2.00	0.00	0.00	0.10	0.00	25.20	2.00	0.00	0.00	0.10	0.00
25.30	2.00	0.00	0.00	0.10	0.00	25.40	2.00	0.00	0.00	0.10	0.00
25.50	2.00	0.00	0.00	0.10	0.00	25.60	2.00	0.00	0.00	0.10	0.00
25.70	2.00	0.00	0.00	0.10	0.00	25.80	2.00	0.00	0.00	0.10	0.00
25.90	2.00	0.00	0.00	0.10	0.00	26.00	2.00	0.00	0.00	0.10	0.00
26.10	2.00	0.00	0.00	0.10	0.00	26.20	2.00	0.00	0.00	0.10	0.00
26.30	2.00	0.00	0.00	0.10	0.00	26.40	2.00	0.00	0.00	0.10	0.00
26.50	2.00	0.00	0.00	0.10	0.00	26.60	2.00	0.00	0.00	0.10	0.00
26.70	2.00	0.00	0.00	0.10	0.00	26.80	2.00	0.00	0.00	0.10	0.00
26.90	2.00	0.00	0.00	0.10	0.00	27.00	2.00	0.00	0.00	0.10	0.00
27.10	2.00	0.00	0.00	0.10	0.00	27.20	2.00	0.00	0.00	0.10	0.00
27.30	2.00	0.00	0.00	0.10	0.00	27.40	2.00	0.00	0.00	0.10	0.00
27.50	2.00	0.00	0.00	0.10	0.00	27.60	0.16	0.84	0.26	0.10	0.15
27.70	0.18	0.82	0.27	0.10	0.14	27.80	0.18	0.82	0.27	0.10	0.14
27.90	2.00	0.00	0.00	0.10	0.00	28.00	2.00	0.00	0.00	0.10	0.00
28.10	2.00	0.00	0.00	0.10	0.00	28.20	2.00	0.00	0.00	0.10	0.00
28.30	2.00	0.00	0.00	0.10	0.00	28.40	2.00	0.00	0.00	0.10	0.00
28.50	2.00	0.00	0.00	0.10	0.00	28.60	2.00	0.00	0.00	0.10	0.00
28.70	2.00	0.00	0.00	0.10	0.00	28.80	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
28.90	2.00	0.00	0.00	0.10	0.00	29.00	2.00	0.00	0.00	0.10	0.00
29.10	2.00	0.00	0.00	0.10	0.00	29.20	2.00	0.00	0.00	0.10	0.00
29.30	2.00	0.00	0.00	0.10	0.00	29.40	2.00	0.00	0.00	0.10	0.00
29.50	2.00	0.00	0.00	0.10	0.00	29.60	2.00	0.00	0.00	0.10	0.00
29.70	2.00	0.00	0.00	0.10	0.00	29.80	2.00	0.00	0.00	0.10	0.00
29.90	2.00	0.00	0.00	0.10	0.00	30.00	2.00	0.00	0.00	0.10	0.00
30.10	2.00	0.00	0.00	0.10	0.00	30.20	2.00	0.00	0.00	0.10	0.00
30.30	2.00	0.00	0.00	0.10	0.00	30.40	2.00	0.00	0.00	0.10	0.00
30.50	2.00	0.00	0.00	0.10	0.00	30.60	2.00	0.00	0.00	0.10	0.00
30.70	2.00	0.00	0.00	0.10	0.00	30.80	2.00	0.00	0.00	0.10	0.00
30.90	2.00	0.00	0.00	0.10	0.00	31.00	2.00	0.00	0.00	0.10	0.00
31.10	2.00	0.00	0.00	0.10	0.00	31.20	2.00	0.00	0.00	0.10	0.00
31.30	2.00	0.00	0.00	0.10	0.00	31.40	2.00	0.00	0.00	0.10	0.00
31.50	0.31	0.69	0.33	0.10	0.11	31.60	0.31	0.69	0.33	0.10	0.11
31.70	0.29	0.71	0.32	0.10	0.11	31.80	2.00	0.00	0.00	0.10	0.00
31.90	2.00	0.00	0.00	0.10	0.00	32.00	2.00	0.00	0.00	0.10	0.00
32.10	2.00	0.00	0.00	0.10	0.00	32.20	2.00	0.00	0.00	0.10	0.00
32.30	2.00	0.00	0.00	0.10	0.00	32.40	2.00	0.00	0.00	0.10	0.00
32.50	0.18	0.82	0.27	0.10	0.13	32.60	0.19	0.81	0.27	0.10	0.12
32.70	0.22	0.78	0.28	0.10	0.12	32.80	0.26	0.74	0.30	0.10	0.11
32.90	0.29	0.71	0.32	0.10	0.11	33.00	0.31	0.69	0.33	0.10	0.10
33.10	0.36	0.64	0.36	0.10	0.10	33.20	0.48	0.52	0.46	0.10	0.08
33.30	0.75	0.00	0.00	0.10	0.04	33.40	1.35	0.00	0.00	0.10	0.00
33.50	1.79	0.00	0.00	0.10	0.00	33.60	1.69	0.00	0.00	0.10	0.00
33.70	1.39	0.00	0.00	0.10	0.00	33.80	1.35	0.00	0.00	0.10	0.00
33.90	1.40	0.00	0.00	0.10	0.00	34.00	1.30	0.00	0.00	0.10	0.00
34.10	1.05	0.00	0.00	0.10	0.00	34.20	0.88	0.00	0.00	0.10	0.02
34.30	0.74	0.00	0.00	0.10	0.04	34.40	0.65	0.35	0.75	0.10	0.05
34.50	0.61	0.39	0.64	0.10	0.06	34.60	0.58	0.42	0.59	0.10	0.06
34.70	0.58	0.42	0.60	0.10	0.06	34.80	0.60	0.40	0.63	0.10	0.06
34.90	0.55	0.45	0.54	0.10	0.06	35.00	0.44	0.56	0.42	0.10	0.08
35.10	0.36	0.64	0.35	0.10	0.09	35.20	0.28	0.72	0.31	0.10	0.10
35.30	0.23	0.77	0.29	0.10	0.11	35.40	0.20	0.80	0.28	0.10	0.11
35.50	0.19	0.81	0.27	0.10	0.11	35.60	0.20	0.80	0.28	0.10	0.11
35.70	0.22	0.78	0.28	0.10	0.11	35.80	0.23	0.77	0.29	0.10	0.11
35.90	0.24	0.76	0.30	0.10	0.10	36.00	0.26	0.74	0.30	0.10	0.10
36.10	0.28	0.72	0.31	0.10	0.10	36.20	0.32	0.68	0.34	0.10	0.09
36.30	0.37	0.63	0.36	0.10	0.09	36.40	0.40	0.60	0.38	0.10	0.08
36.50	0.39	0.61	0.38	0.10	0.08	36.60	2.00	0.00	0.00	0.10	0.00
36.70	2.00	0.00	0.00	0.10	0.00	36.80	2.00	0.00	0.00	0.10	0.00
36.90	2.00	0.00	0.00	0.10	0.00	37.00	2.00	0.00	0.00	0.10	0.00
37.10	2.00	0.00	0.00	0.10	0.00	37.20	2.00	0.00	0.00	0.10	0.00
37.30	2.00	0.00	0.00	0.10	0.00	37.40	2.00	0.00	0.00	0.10	0.00
37.50	2.00	0.00	0.00	0.10	0.00	37.60	0.16	0.84	0.26	0.10	0.11
37.70	0.18	0.82	0.27	0.10	0.11	37.80	0.19	0.81	0.27	0.10	0.10
37.90	0.20	0.80	0.28	0.10	0.10	38.00	0.21	0.79	0.28	0.10	0.10
38.10	0.23	0.77	0.29	0.10	0.10	38.20	0.26	0.74	0.30	0.10	0.09
38.30	0.29	0.71	0.32	0.10	0.09	38.40	0.30	0.70	0.32	0.10	0.09

:: Liquefaction Potential Index calculation data ::

Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
38.50	0.30	0.70	0.32	0.10	0.09	38.60	0.28	0.72	0.31	0.10	0.09
38.70	0.25	0.75	0.30	0.10	0.09	38.80	0.23	0.77	0.29	0.10	0.10
38.90	0.22	0.78	0.28	0.10	0.10	39.00	0.21	0.79	0.28	0.10	0.10
39.10	0.22	0.78	0.28	0.10	0.10	39.20	2.00	0.00	0.00	0.10	0.00
39.30	2.00	0.00	0.00	0.10	0.00	39.40	2.00	0.00	0.00	0.10	0.00
39.50	2.00	0.00	0.00	0.10	0.00	39.60	2.00	0.00	0.00	0.10	0.00
39.70	2.00	0.00	0.00	0.10	0.00	39.80	2.00	0.00	0.00	0.10	0.00
39.90	2.00	0.00	0.00	0.10	0.00	40.00	2.00	0.00	0.00	0.10	0.00
40.10	2.00	0.00	0.00	0.10	0.00	40.20	2.00	0.00	0.00	0.10	0.00
40.30	2.00	0.00	0.00	0.10	0.00	40.40	2.00	0.00	0.00	0.10	0.00
40.50	2.00	0.00	0.00	0.10	0.00	40.60	2.00	0.00	0.00	0.10	0.00
40.70	2.00	0.00	0.00	0.10	0.00	40.80	2.00	0.00	0.00	0.10	0.00
40.90	2.00	0.00	0.00	0.10	0.00	41.00	2.00	0.00	0.00	0.10	0.00
41.10	2.00	0.00	0.00	0.10	0.00	41.20	2.00	0.00	0.00	0.10	0.00
41.30	2.00	0.00	0.00	0.10	0.00	41.40	2.00	0.00	0.00	0.10	0.00
41.50	2.00	0.00	0.00	0.10	0.00	41.60	2.00	0.00	0.00	0.10	0.00
41.70	2.00	0.00	0.00	0.10	0.00	41.80	2.00	0.00	0.00	0.10	0.00
41.90	2.00	0.00	0.00	0.10	0.00	42.00	2.00	0.00	0.00	0.10	0.00
42.10	2.00	0.00	0.00	0.10	0.00	42.20	2.00	0.00	0.00	0.10	0.00
42.30	2.00	0.00	0.00	0.10	0.00	42.40	2.00	0.00	0.00	0.10	0.00
42.50	2.00	0.00	0.00	0.10	0.00	42.60	2.00	0.00	0.00	0.10	0.00
42.70	2.00	0.00	0.00	0.10	0.00	42.80	2.00	0.00	0.00	0.10	0.00
42.90	2.00	0.00	0.00	0.10	0.00	43.00	2.00	0.00	0.00	0.10	0.00
43.10	2.00	0.00	0.00	0.10	0.00	43.20	2.00	0.00	0.00	0.10	0.00
43.30	2.00	0.00	0.00	0.10	0.00	43.40	2.00	0.00	0.00	0.10	0.00
43.50	2.00	0.00	0.00	0.10	0.00	43.60	2.00	0.00	0.00	0.10	0.00
43.70	2.00	0.00	0.00	0.10	0.00	43.80	2.00	0.00	0.00	0.10	0.00
43.90	2.00	0.00	0.00	0.10	0.00	44.00	2.00	0.00	0.00	0.10	0.00
44.10	2.00	0.00	0.00	0.10	0.00	44.20	2.00	0.00	0.00	0.10	0.00
44.30	2.00	0.00	0.00	0.10	0.00	44.40	2.00	0.00	0.00	0.10	0.00
44.50	2.00	0.00	0.00	0.10	0.00	44.60	2.00	0.00	0.00	0.10	0.00
44.70	2.00	0.00	0.00	0.10	0.00	44.80	2.00	0.00	0.00	0.10	0.00
44.90	2.00	0.00	0.00	0.10	0.00	45.00	2.00	0.00	0.00	0.10	0.00
45.10	2.00	0.00	0.00	0.10	0.00	45.20	1.89	0.00	0.00	0.10	0.00
45.30	2.00	0.00	0.00	0.10	0.00	45.40	2.00	0.00	0.00	0.10	0.00
45.50	2.00	0.00	0.00	0.10	0.00	45.60	2.00	0.00	0.00	0.10	0.00
45.70	2.00	0.00	0.00	0.10	0.00	45.80	2.00	0.00	0.00	0.10	0.00
45.90	2.00	0.00	0.00	0.10	0.00	46.00	0.22	0.78	0.28	0.10	0.07
46.10	2.00	0.00	0.00	0.10	0.00	46.20	2.00	0.00	0.00	0.10	0.00
46.30	2.00	0.00	0.00	0.10	0.00	46.40	2.00	0.00	0.00	0.10	0.00
46.50	2.00	0.00	0.00	0.10	0.00	46.60	2.00	0.00	0.00	0.10	0.00
46.70	0.68	0.32	0.85	0.10	0.03	46.80	1.04	0.00	0.00	0.10	0.00
46.90	1.14	0.00	0.00	0.10	0.00	47.00	1.03	0.00	0.00	0.10	0.00
47.10	1.00	0.00	0.00	0.10	0.00	47.20	0.97	0.00	0.00	0.10	0.00
47.30	0.92	0.00	0.00	0.10	0.01	47.40	1.04	0.00	0.00	0.10	0.00
47.50	1.56	0.00	0.00	0.10	0.00	47.60	2.00	0.00	0.00	0.10	0.00
47.70	2.00	0.00	0.00	0.10	0.00	47.80	2.00	0.00	0.00	0.10	0.00
47.90	2.00	0.00	0.00	0.10	0.00	48.00	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
48.10	2.00	0.00	0.00	0.10	0.00	48.20	2.00	0.00	0.00	0.10	0.00
48.30	2.00	0.00	0.00	0.10	0.00	48.40	2.00	0.00	0.00	0.10	0.00
48.50	2.00	0.00	0.00	0.10	0.00	48.60	2.00	0.00	0.00	0.10	0.00
48.70	2.00	0.00	0.00	0.10	0.00	48.80	2.00	0.00	0.00	0.10	0.00
48.90	2.00	0.00	0.00	0.10	0.00	49.00	2.00	0.00	0.00	0.10	0.00
49.10	2.00	0.00	0.00	0.10	0.00	49.20	2.00	0.00	0.00	0.10	0.00
49.30	2.00	0.00	0.00	0.10	0.00	49.40	2.00	0.00	0.00	0.10	0.00
49.50	2.00	0.00	0.00	0.10	0.00	49.60	2.00	0.00	0.00	0.10	0.00
49.70	2.00	0.00	0.00	0.10	0.00	49.80	2.00	0.00	0.00	0.10	0.00
49.90	2.00	0.00	0.00	0.10	0.00						

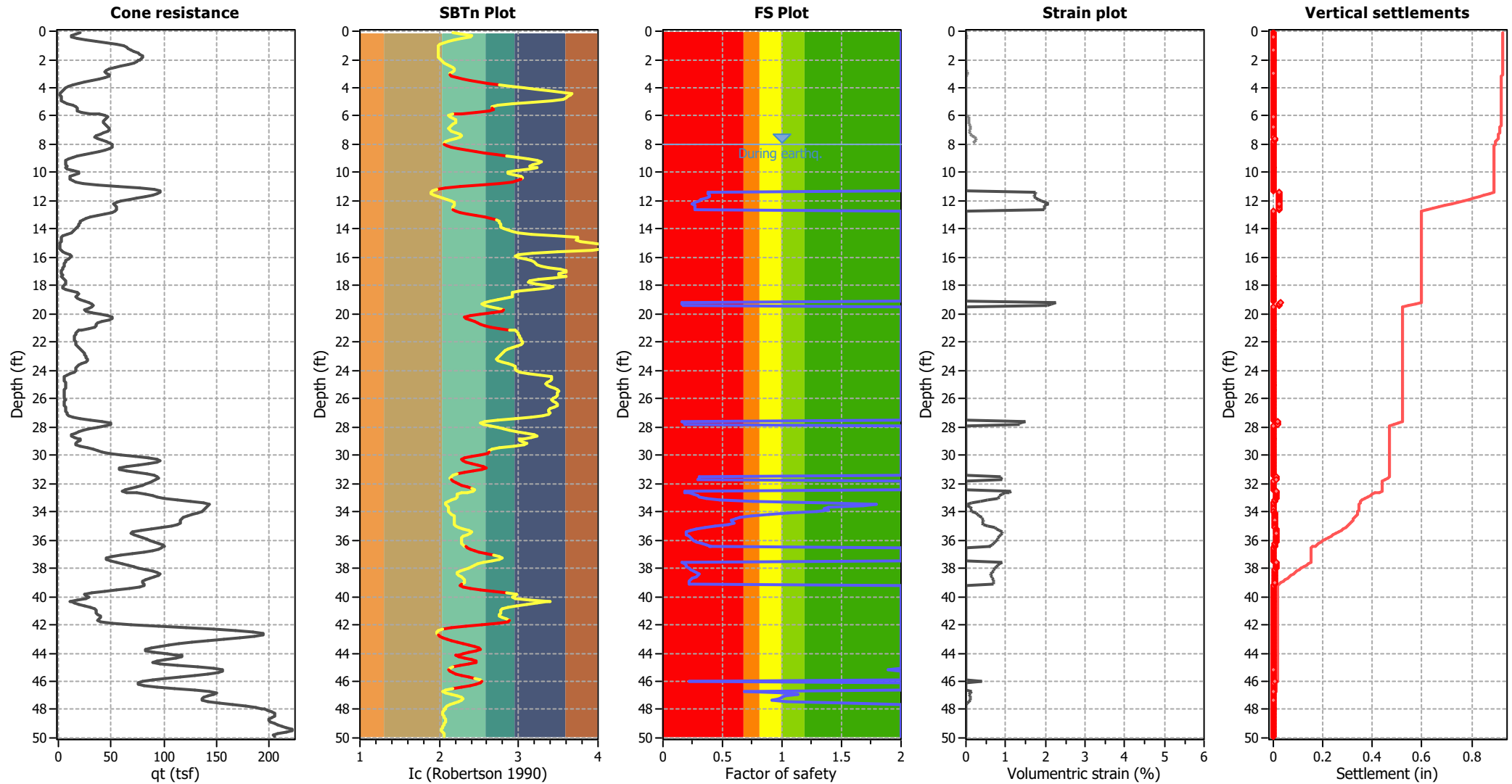
Overall liquefaction potential: 8.08

LPI_{ISH} > 5.0 - Liquefaction manifestation is expected

Abbreviations

FS: Calculated factor of safety for test point
d_z: Layer thickness (ft)
LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

q_c : Total cone resistance (cone resistance q_c corrected for pore water effects)
 I_c : Soil Behaviour Type Index
 FS: Calculated Factor of Safety against liquefaction
 Volumetric strain: Post-liquefaction volumetric strain

:: Post-earthquake settlement of dry sands ::												
Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
0.10	2.16	33.24	1.53	50.97	11	289	0.56	0.001	0.00	13.69	0.00	0.000
0.20	2.28	25.60	1.85	47.43	11	257	0.56	0.003	0.01	13.69	0.01	0.000
0.30	2.41	19.73	2.41	47.48	12	233	0.56	0.007	0.01	13.69	0.01	0.000
0.40	2.40	20.62	2.36	48.75	12	241	0.56	0.010	0.02	13.69	0.02	0.000
0.50	2.28	28.76	1.86	53.61	13	290	0.56	0.009	0.02	13.69	0.02	0.000
0.60	2.19	41.08	1.59	65.46	15	369	0.56	0.007	0.01	13.69	0.01	0.000
0.70	2.11	57.17	1.44	82.32	18	466	0.56	0.006	0.01	13.69	0.01	0.000
0.80	2.06	73.51	1.36	100.06	21	556	0.56	0.005	0.00	13.69	0.00	0.000
0.90	2.01	88.39	1.32	116.65	24	635	0.55	0.005	0.00	13.69	0.00	0.000
1.00	1.99	99.50	1.30	129.32	27	693	0.55	0.005	0.00	13.69	0.00	0.000
1.10	1.99	104.99	1.30	136.08	28	727	0.55	0.005	0.00	13.69	0.00	0.000
1.20	1.99	107.11	1.30	139.05	29	745	0.55	0.006	0.00	13.69	0.00	0.000
1.30	1.99	110.41	1.30	143.31	30	767	0.55	0.006	0.00	13.69	0.00	0.000
1.40	1.98	115.70	1.29	149.74	31	799	0.54	0.006	0.00	13.69	0.00	0.000
1.50	1.98	121.12	1.29	156.40	32	832	0.54	0.007	0.00	13.69	0.00	0.000
1.60	1.98	124.82	1.29	161.32	33	860	0.54	0.007	0.00	13.69	0.00	0.000
1.70	1.99	127.49	1.30	165.15	34	882	0.54	0.007	0.00	13.69	0.00	0.000
1.80	1.99	128.24	1.30	166.89	35	896	0.54	0.007	0.00	13.69	0.00	0.000
1.90	2.01	126.34	1.31	165.78	35	898	0.54	0.008	0.00	13.69	0.00	0.000
2.00	2.02	124.39	1.32	164.55	34	897	0.54	0.009	0.00	13.69	0.00	0.000
2.10	2.03	122.63	1.33	163.29	34	895	0.54	0.009	0.00	13.69	0.00	0.000
2.20	2.04	120.21	1.34	161.41	34	890	0.54	0.010	0.01	13.69	0.00	0.000
2.30	2.06	115.52	1.36	157.68	34	878	0.54	0.011	0.01	13.69	0.01	0.000
2.40	2.09	106.80	1.41	150.52	32	848	0.54	0.012	0.01	13.69	0.01	0.000
2.50	2.13	95.89	1.47	141.20	31	800	0.55	0.014	0.01	13.69	0.01	0.000
2.60	2.17	85.53	1.53	131.20	29	743	0.55	0.017	0.01	13.69	0.01	0.000
2.70	2.18	77.77	1.57	122.22	27	691	0.55	0.021	0.01	13.69	0.01	0.000
2.80	2.19	72.54	1.58	114.67	26	647	0.55	0.026	0.02	13.69	0.02	0.000
2.90	2.17	70.93	1.55	109.70	24	621	0.56	0.030	0.02	13.69	0.02	0.000
3.00	2.14	73.54	1.49	109.47	24	621	0.55	0.032	0.03	13.69	0.02	0.000
3.10	2.13	77.29	1.47	113.45	25	643	0.55	0.031	0.02	13.69	0.02	0.000
3.20	2.16	77.00	1.52	116.90	0	0	0.55	0.000	0.00	13.69	0.00	0.000
3.30	2.22	71.05	1.66	118.06	0	0	0.55	0.000	0.00	13.69	0.00	0.000
3.40	2.30	61.40	1.92	117.92	0	0	0.56	0.000	0.00	13.69	0.00	0.000
3.50	2.39	50.53	2.32	117.39	0	0	0.56	0.000	0.00	13.69	0.00	0.000
3.60	2.49	39.85	2.94	117.18	0	0	0.56	0.000	0.00	13.69	0.00	0.000
3.70	2.62	30.07	3.89	117.02	0	0	0.56	0.000	0.00	0.00	0.00	0.000
3.80	2.75	21.96	5.28	116.00	0	0	0.56	0.000	0.00	0.00	0.00	0.000
3.90	2.91	15.43	7.28	112.34	0	0	0.56	0.000	0.00	0.00	0.00	0.000
4.00	3.07	10.41	10.03	104.40	0	0	0.56	0.000	0.00	0.00	0.00	0.000
4.10	3.22	7.22	13.17	95.15	0	0	0.56	0.000	0.00	0.00	0.00	0.000
4.20	3.37	4.91	17.17	84.37	0	0	0.56	0.000	0.00	0.00	0.00	0.000
4.30	3.53	3.26	22.48	73.39	0	0	0.56	0.000	0.00	0.00	0.00	0.000
4.40	3.68	2.22	28.79	63.82	0	0	0.56	0.000	0.00	0.00	0.00	0.000
4.50	3.66	2.29	27.79	63.71	0	0	0.56	0.000	0.00	0.00	0.00	0.000
4.60	3.61	2.63	25.60	67.34	0	0	0.56	0.000	0.00	0.00	0.00	0.000
4.70	3.60	2.78	25.32	70.36	0	0	0.56	0.000	0.00	0.00	0.00	0.000
4.80	3.56	3.22	23.67	76.30	0	0	0.56	0.000	0.00	0.00	0.00	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
4.90	3.42	4.50	18.72	84.26	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.00	3.18	7.62	12.30	93.72	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.10	2.93	12.95	7.64	98.96	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.20	2.74	20.40	5.19	105.89	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.30	2.67	26.91	4.35	117.17	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.40	2.67	29.11	4.35	126.71	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.50	2.68	28.14	4.55	128.03	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.60	2.63	28.84	4.05	116.72	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.70	2.47	35.79	2.77	99.18	0	0	0.56	0.000	0.00	13.69	0.00	0.000
5.80	2.28	48.23	1.87	90.04	0	0	0.56	0.000	0.00	13.69	0.00	0.000
5.90	2.16	61.59	1.53	94.11	0	0	0.55	0.000	0.00	13.69	0.00	0.000
6.00	2.12	70.82	1.45	102.98	0	0	0.55	0.000	0.00	13.69	0.00	0.000
6.10	2.14	74.21	1.48	110.20	24	625	0.55	0.107	0.09	13.69	0.07	0.001
6.20	2.18	72.94	1.56	113.95	25	644	0.55	0.100	0.07	13.69	0.06	0.001
6.30	2.21	70.41	1.63	114.84	26	645	0.55	0.103	0.07	13.69	0.06	0.001
6.40	2.21	68.93	1.65	113.55	26	637	0.55	0.111	0.08	13.69	0.07	0.001
6.50	2.20	68.97	1.61	111.32	25	626	0.55	0.122	0.09	13.69	0.08	0.001
6.60	2.18	70.27	1.56	109.67	24	620	0.55	0.131	0.10	13.69	0.09	0.001
6.70	2.15	72.06	1.51	108.77	24	617	0.55	0.138	0.11	13.69	0.09	0.001
6.80	2.13	74.23	1.47	108.95	24	617	0.55	0.142	0.11	13.69	0.10	0.001
6.90	2.12	76.14	1.45	110.13	24	623	0.55	0.142	0.11	13.69	0.10	0.001
7.00	2.13	76.39	1.46	111.47	24	631	0.55	0.139	0.11	13.69	0.09	0.001
7.10	2.16	73.82	1.52	112.29	25	636	0.55	0.139	0.11	13.69	0.09	0.001
7.20	2.21	68.66	1.64	112.58	25	632	0.55	0.148	0.11	13.69	0.09	0.001
7.30	2.26	62.31	1.79	111.40	26	611	0.55	0.173	0.13	13.69	0.11	0.001
7.40	2.29	57.08	1.88	107.20	25	579	0.55	0.224	0.17	13.69	0.14	0.002
7.50	2.27	55.39	1.81	100.25	23	548	0.55	0.296	0.25	13.69	0.20	0.002
7.60	2.20	58.29	1.63	94.73	21	532	0.55	0.351	0.32	13.69	0.27	0.003
7.70	2.13	64.78	1.47	95.22	21	540	0.55	0.340	0.32	13.69	0.27	0.003
7.80	2.08	71.87	1.39	100.11	22	562	0.55	0.291	0.27	13.69	0.22	0.003
7.90	2.06	77.19	1.37	105.57	23	588	0.55	0.244	0.21	13.69	0.17	0.002

Total estimated settlement: 0.03**Abbreviations**

Q_{tn}: Normalized cone resistance
 K_c: Fines correction factor
 Q_{tn,cs}: Equivalent clean sand normalized cone resistance
 G_{max}: Small strain shear modulus
 CSR: Soil cyclic stress ratio
 γ: Cyclic shear strain
 e_{vol(15)}: Volumetric strain after 15 cycles
 N_c: Equivalent number of cycles
 e_v: Volumetric strain
 Settle.: Calculated settlement

:: Post-earthquake settlement due to soil liquefaction ::

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
8.00	117.87	2.00	0.00	0.85	0.00	8.10	120.87	2.00	0.00	0.85	0.00
8.20	125.27	2.00	0.00	0.85	0.00	8.30	127.21	2.00	0.00	0.85	0.00
8.40	123.58	2.00	0.00	0.85	0.00	8.50	116.52	2.00	0.00	0.85	0.00
8.60	106.65	2.00	0.00	0.84	0.00	8.70	33.80	2.00	0.00	0.84	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
8.80	25.72	2.00	0.00	0.84	0.00	8.90	19.22	2.00	0.00	0.84	0.00
9.00	13.77	2.00	0.00	0.84	0.00	9.10	10.22	2.00	0.00	0.83	0.00
9.20	8.98	2.00	0.00	0.83	0.00	9.30	9.05	2.00	0.00	0.83	0.00
9.40	10.26	2.00	0.00	0.83	0.00	9.50	11.87	2.00	0.00	0.83	0.00
9.60	11.21	2.00	0.00	0.83	0.00	9.70	9.18	2.00	0.00	0.82	0.00
9.80	7.18	2.00	0.00	0.82	0.00	9.90	18.03	2.00	0.00	0.82	0.00
10.00	30.19	2.00	0.00	0.82	0.00	10.10	30.12	2.00	0.00	0.82	0.00
10.20	17.34	2.00	0.00	0.81	0.00	10.30	13.94	2.00	0.00	0.81	0.00
10.40	15.25	2.00	0.00	0.81	0.00	10.50	15.29	2.00	0.00	0.81	0.00
10.60	16.58	2.00	0.00	0.81	0.00	10.70	23.98	2.00	0.00	0.81	0.00
10.80	26.48	2.00	0.00	0.80	0.00	10.90	105.06	2.00	0.00	0.80	0.00
11.00	135.40	2.00	0.00	0.80	0.00	11.10	154.90	2.00	0.00	0.80	0.00
11.20	155.72	2.00	0.00	0.80	0.00	11.30	149.15	2.00	0.00	0.79	0.00
11.40	141.94	0.38	1.75	0.79	0.02	11.50	141.96	0.38	1.75	0.79	0.02
11.60	143.04	0.38	1.73	0.79	0.02	11.70	143.30	0.39	1.72	0.79	0.02
11.80	141.53	0.37	1.74	0.79	0.02	11.90	134.41	0.32	1.84	0.78	0.02
12.00	130.79	0.30	1.89	0.78	0.02	12.10	124.09	0.27	2.00	0.78	0.02
12.20	118.06	0.25	2.10	0.78	0.03	12.30	124.58	0.27	1.98	0.78	0.02
12.40	125.38	0.27	1.96	0.77	0.02	12.50	124.30	0.27	1.98	0.77	0.02
12.60	124.69	0.27	1.96	0.77	0.02	12.70	124.47	2.00	0.00	0.77	0.00
12.80	124.94	2.00	0.00	0.77	0.00	12.90	118.34	2.00	0.00	0.77	0.00
13.00	104.48	2.00	0.00	0.76	0.00	13.10	101.14	2.00	0.00	0.76	0.00
13.20	33.07	2.00	0.00	0.76	0.00	13.30	27.91	2.00	0.00	0.76	0.00
13.40	25.57	2.00	0.00	0.76	0.00	13.50	26.25	2.00	0.00	0.75	0.00
13.60	25.49	2.00	0.00	0.75	0.00	13.70	24.35	2.00	0.00	0.75	0.00
13.80	23.37	2.00	0.00	0.75	0.00	13.90	23.32	2.00	0.00	0.75	0.00
14.00	21.69	2.00	0.00	0.75	0.00	14.10	18.31	2.00	0.00	0.74	0.00
14.20	17.52	2.00	0.00	0.74	0.00	14.30	17.38	2.00	0.00	0.74	0.00
14.40	9.34	2.00	0.00	0.74	0.00	14.50	3.12	2.00	0.00	0.74	0.00
14.60	3.11	2.00	0.00	0.73	0.00	14.70	3.11	2.00	0.00	0.73	0.00
14.80	3.10	2.00	0.00	0.73	0.00	14.90	3.10	2.00	0.00	0.73	0.00
15.00	2.25	2.00	0.00	0.73	0.00	15.10	1.55	2.00	0.00	0.73	0.00
15.20	1.55	2.00	0.00	0.72	0.00	15.30	1.55	2.00	0.00	0.72	0.00
15.40	1.54	2.00	0.00	0.72	0.00	15.50	2.26	2.00	0.00	0.72	0.00
15.60	4.01	2.00	0.00	0.72	0.00	15.70	8.58	2.00	0.00	0.71	0.00
15.80	14.06	2.00	0.00	0.71	0.00	15.90	16.73	2.00	0.00	0.71	0.00
16.00	14.49	2.00	0.00	0.71	0.00	16.10	10.93	2.00	0.00	0.71	0.00
16.20	8.96	2.00	0.00	0.71	0.00	16.30	7.48	2.00	0.00	0.70	0.00
16.40	7.47	2.00	0.00	0.70	0.00	16.50	7.45	2.00	0.00	0.70	0.00
16.60	6.62	2.00	0.00	0.70	0.00	16.70	5.18	2.00	0.00	0.70	0.00
16.80	4.01	2.00	0.00	0.69	0.00	16.90	3.05	2.00	0.00	0.69	0.00
17.00	3.72	2.00	0.00	0.69	0.00	17.10	3.82	2.00	0.00	0.69	0.00
17.20	4.40	2.00	0.00	0.69	0.00	17.30	3.92	2.00	0.00	0.69	0.00
17.40	3.02	2.00	0.00	0.68	0.00	17.50	4.03	2.00	0.00	0.68	0.00
17.60	6.48	2.00	0.00	0.68	0.00	17.70	8.55	2.00	0.00	0.68	0.00
17.80	9.46	2.00	0.00	0.68	0.00	17.90	7.54	2.00	0.00	0.67	0.00
18.00	5.10	2.00	0.00	0.67	0.00	18.10	4.86	2.00	0.00	0.67	0.00
18.20	4.86	2.00	0.00	0.67	0.00	18.30	6.78	2.00	0.00	0.67	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
18.40	14.43	2.00	0.00	0.67	0.00	18.50	22.52	2.00	0.00	0.66	0.00
18.60	25.47	2.00	0.00	0.66	0.00	18.70	18.80	2.00	0.00	0.66	0.00
18.80	19.01	2.00	0.00	0.66	0.00	18.90	21.15	2.00	0.00	0.66	0.00
19.00	24.12	2.00	0.00	0.65	0.00	19.10	27.80	2.00	0.00	0.65	0.00
19.20	92.23	0.15	2.27	0.65	0.03	19.30	97.48	0.16	2.14	0.65	0.03
19.40	100.78	0.17	2.06	0.65	0.02	19.50	37.34	2.00	0.00	0.65	0.00
19.60	32.60	2.00	0.00	0.64	0.00	19.70	27.50	2.00	0.00	0.64	0.00
19.80	24.38	2.00	0.00	0.64	0.00	19.90	34.45	2.00	0.00	0.64	0.00
20.00	112.44	2.00	0.00	0.64	0.00	20.10	112.37	2.00	0.00	0.63	0.00
20.20	117.81	2.00	0.00	0.63	0.00	20.30	119.76	2.00	0.00	0.63	0.00
20.40	115.61	2.00	0.00	0.63	0.00	20.50	105.98	2.00	0.00	0.63	0.00
20.60	99.39	2.00	0.00	0.63	0.00	20.70	98.93	2.00	0.00	0.62	0.00
20.80	102.74	2.00	0.00	0.62	0.00	20.90	39.46	2.00	0.00	0.62	0.00
21.00	31.48	2.00	0.00	0.62	0.00	21.10	23.41	2.00	0.00	0.62	0.00
21.20	19.47	2.00	0.00	0.61	0.00	21.30	19.33	2.00	0.00	0.61	0.00
21.40	18.10	2.00	0.00	0.61	0.00	21.50	17.46	2.00	0.00	0.61	0.00
21.60	16.95	2.00	0.00	0.61	0.00	21.70	16.61	2.00	0.00	0.61	0.00
21.80	16.07	2.00	0.00	0.60	0.00	21.90	16.16	2.00	0.00	0.60	0.00
22.00	18.01	2.00	0.00	0.60	0.00	22.10	17.68	2.00	0.00	0.60	0.00
22.20	17.20	2.00	0.00	0.60	0.00	22.30	18.59	2.00	0.00	0.59	0.00
22.40	20.36	2.00	0.00	0.59	0.00	22.50	22.64	2.00	0.00	0.59	0.00
22.60	24.29	2.00	0.00	0.59	0.00	22.70	25.37	2.00	0.00	0.59	0.00
22.80	26.30	2.00	0.00	0.59	0.00	22.90	26.45	2.00	0.00	0.58	0.00
23.00	26.88	2.00	0.00	0.58	0.00	23.10	28.08	2.00	0.00	0.58	0.00
23.20	30.16	2.00	0.00	0.58	0.00	23.30	30.94	2.00	0.00	0.58	0.00
23.40	28.07	2.00	0.00	0.57	0.00	23.50	23.60	2.00	0.00	0.57	0.00
23.60	19.65	2.00	0.00	0.57	0.00	23.70	18.29	2.00	0.00	0.57	0.00
23.80	17.44	2.00	0.00	0.57	0.00	23.90	16.82	2.00	0.00	0.57	0.00
24.00	17.01	2.00	0.00	0.56	0.00	24.10	16.24	2.00	0.00	0.56	0.00
24.20	12.75	2.00	0.00	0.56	0.00	24.30	6.92	2.00	0.00	0.56	0.00
24.40	5.95	2.00	0.00	0.56	0.00	24.50	5.94	2.00	0.00	0.55	0.00
24.60	5.94	2.00	0.00	0.55	0.00	24.70	5.93	2.00	0.00	0.55	0.00
24.80	6.40	2.00	0.00	0.55	0.00	24.90	7.38	2.00	0.00	0.55	0.00
25.00	7.58	2.00	0.00	0.55	0.00	25.10	7.57	2.00	0.00	0.54	0.00
25.20	7.43	2.00	0.00	0.54	0.00	25.30	6.44	2.00	0.00	0.54	0.00
25.40	5.86	2.00	0.00	0.54	0.00	25.50	5.86	2.00	0.00	0.54	0.00
25.60	5.85	2.00	0.00	0.53	0.00	25.70	5.84	2.00	0.00	0.53	0.00
25.80	5.83	2.00	0.00	0.53	0.00	25.90	5.82	2.00	0.00	0.53	0.00
26.00	6.18	2.00	0.00	0.53	0.00	26.10	6.63	2.00	0.00	0.53	0.00
26.20	5.96	2.00	0.00	0.52	0.00	26.30	5.79	2.00	0.00	0.52	0.00
26.40	5.78	2.00	0.00	0.52	0.00	26.50	5.77	2.00	0.00	0.52	0.00
26.60	6.07	2.00	0.00	0.52	0.00	26.70	7.04	2.00	0.00	0.51	0.00
26.80	7.39	2.00	0.00	0.51	0.00	26.90	7.37	2.00	0.00	0.51	0.00
27.00	7.38	2.00	0.00	0.51	0.00	27.10	8.39	2.00	0.00	0.51	0.00
27.20	9.29	2.00	0.00	0.51	0.00	27.30	11.94	2.00	0.00	0.50	0.00
27.40	19.14	2.00	0.00	0.50	0.00	27.50	28.96	2.00	0.00	0.50	0.00
27.60	105.60	0.16	1.51	0.50	0.02	27.70	117.18	0.18	1.35	0.50	0.02
27.80	116.67	0.18	1.35	0.49	0.02	27.90	44.15	2.00	0.00	0.49	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
28.00	35.84	2.00	0.00	0.49	0.00	28.10	28.50	2.00	0.00	0.49	0.00
28.20	22.93	2.00	0.00	0.49	0.00	28.30	19.85	2.00	0.00	0.49	0.00
28.40	15.24	2.00	0.00	0.48	0.00	28.50	12.00	2.00	0.00	0.48	0.00
28.60	11.16	2.00	0.00	0.48	0.00	28.70	14.62	2.00	0.00	0.48	0.00
28.80	19.42	2.00	0.00	0.48	0.00	28.90	21.47	2.00	0.00	0.47	0.00
29.00	19.58	2.00	0.00	0.47	0.00	29.10	18.56	2.00	0.00	0.47	0.00
29.20	16.07	2.00	0.00	0.47	0.00	29.30	14.08	2.00	0.00	0.47	0.00
29.40	18.23	2.00	0.00	0.47	0.00	29.50	26.52	2.00	0.00	0.46	0.00
29.60	34.21	2.00	0.00	0.46	0.00	29.70	35.74	2.00	0.00	0.46	0.00
29.80	36.61	2.00	0.00	0.46	0.00	29.90	45.88	2.00	0.00	0.46	0.00
30.00	123.32	2.00	0.00	0.45	0.00	30.10	136.07	2.00	0.00	0.45	0.00
30.20	152.29	2.00	0.00	0.45	0.00	30.30	160.05	2.00	0.00	0.45	0.00
30.40	162.82	2.00	0.00	0.45	0.00	30.50	160.29	2.00	0.00	0.45	0.00
30.60	153.78	2.00	0.00	0.44	0.00	30.70	141.10	2.00	0.00	0.44	0.00
30.80	128.34	2.00	0.00	0.44	0.00	30.90	118.77	2.00	0.00	0.44	0.00
31.00	116.66	2.00	0.00	0.44	0.00	31.10	124.36	2.00	0.00	0.43	0.00
31.20	134.84	2.00	0.00	0.43	0.00	31.30	142.92	2.00	0.00	0.43	0.00
31.40	146.82	2.00	0.00	0.43	0.00	31.50	148.93	0.31	0.89	0.43	0.01
31.60	148.44	0.31	0.89	0.43	0.01	31.70	146.53	0.29	0.90	0.42	0.01
31.80	143.90	2.00	0.00	0.42	0.00	31.90	141.43	2.00	0.00	0.42	0.00
32.00	140.17	2.00	0.00	0.42	0.00	32.10	138.58	2.00	0.00	0.42	0.00
32.20	135.73	2.00	0.00	0.41	0.00	32.30	130.25	2.00	0.00	0.41	0.00
32.40	122.60	2.00	0.00	0.41	0.00	32.50	116.79	0.18	1.12	0.41	0.01
32.60	120.03	0.19	1.08	0.41	0.01	32.70	131.07	0.22	0.98	0.41	0.01
32.80	140.63	0.26	0.90	0.40	0.01	32.90	146.42	0.29	0.86	0.40	0.01
33.00	149.25	0.31	0.83	0.40	0.01	33.10	155.61	0.36	0.79	0.40	0.01
33.20	165.52	0.48	0.57	0.40	0.01	33.30	178.23	0.75	0.36	0.39	0.00
33.40	191.42	1.35	0.14	0.39	0.00	33.50	197.01	1.79	0.04	0.39	0.00
33.60	195.93	1.69	0.05	0.39	0.00	33.70	192.15	1.39	0.12	0.39	0.00
33.80	191.58	1.35	0.13	0.39	0.00	33.90	192.24	1.40	0.12	0.38	0.00
34.00	190.72	1.30	0.15	0.38	0.00	34.10	186.19	1.05	0.24	0.38	0.00
34.20	182.27	0.88	0.30	0.38	0.00	34.30	177.95	0.74	0.35	0.38	0.00
34.40	174.47	0.65	0.39	0.37	0.00	34.50	172.57	0.61	0.42	0.37	0.00
34.60	171.26	0.58	0.43	0.37	0.01	34.70	171.50	0.58	0.43	0.37	0.01
34.80	172.19	0.60	0.42	0.37	0.00	34.90	169.57	0.55	0.45	0.37	0.01
35.00	163.02	0.44	0.57	0.36	0.01	35.10	155.15	0.36	0.72	0.36	0.01
35.20	145.42	0.28	0.77	0.36	0.01	35.30	135.24	0.23	0.83	0.36	0.01
35.40	125.52	0.20	0.90	0.36	0.01	35.50	122.50	0.19	0.92	0.35	0.01
35.60	126.30	0.20	0.89	0.35	0.01	35.70	131.30	0.22	0.85	0.35	0.01
35.80	135.17	0.23	0.81	0.35	0.01	35.90	137.95	0.24	0.79	0.35	0.01
36.00	141.12	0.26	0.77	0.35	0.01	36.10	145.59	0.28	0.74	0.34	0.01
36.20	151.42	0.32	0.70	0.34	0.01	36.30	156.57	0.37	0.66	0.34	0.01
36.40	159.48	0.40	0.59	0.34	0.01	36.50	158.41	0.39	0.61	0.34	0.01
36.60	157.07	2.00	0.00	0.33	0.00	36.70	155.99	2.00	0.00	0.33	0.00
36.80	151.32	2.00	0.00	0.33	0.00	36.90	141.53	2.00	0.00	0.33	0.00
37.00	130.01	2.00	0.00	0.33	0.00	37.10	51.02	2.00	0.00	0.33	0.00
37.20	42.26	2.00	0.00	0.32	0.00	37.30	38.94	2.00	0.00	0.32	0.00
37.40	38.74	2.00	0.00	0.32	0.00	37.50	41.24	2.00	0.00	0.32	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
37.60	111.09	0.16	0.91	0.32	0.01	37.70	117.62	0.18	0.85	0.31	0.01
37.80	122.78	0.19	0.81	0.31	0.01	37.90	126.56	0.20	0.78	0.31	0.01
38.00	130.69	0.21	0.75	0.31	0.01	38.10	135.75	0.23	0.71	0.31	0.01
38.20	140.75	0.26	0.68	0.31	0.01	38.30	146.27	0.29	0.65	0.30	0.01
38.40	148.36	0.30	0.63	0.30	0.01	38.50	147.71	0.30	0.63	0.30	0.01
38.60	144.47	0.28	0.65	0.30	0.01	38.70	139.08	0.25	0.67	0.30	0.01
38.80	134.61	0.23	0.69	0.29	0.01	38.90	131.84	0.22	0.70	0.29	0.01
39.00	130.77	0.21	0.70	0.29	0.01	39.10	131.49	0.22	0.70	0.29	0.01
39.20	133.25	2.00	0.00	0.29	0.00	39.30	131.21	2.00	0.00	0.29	0.00
39.40	120.74	2.00	0.00	0.28	0.00	39.50	110.91	2.00	0.00	0.28	0.00
39.60	36.09	2.00	0.00	0.28	0.00	39.70	26.46	2.00	0.00	0.28	0.00
39.80	18.09	2.00	0.00	0.28	0.00	39.90	16.63	2.00	0.00	0.27	0.00
40.00	29.44	2.00	0.00	0.27	0.00	40.10	26.12	2.00	0.00	0.27	0.00
40.20	9.42	2.00	0.00	0.27	0.00	40.30	7.23	2.00	0.00	0.27	0.00
40.40	9.62	2.00	0.00	0.27	0.00	40.50	11.70	2.00	0.00	0.26	0.00
40.60	15.17	2.00	0.00	0.26	0.00	40.70	20.33	2.00	0.00	0.26	0.00
40.80	25.42	2.00	0.00	0.26	0.00	40.90	29.45	2.00	0.00	0.26	0.00
41.00	30.39	2.00	0.00	0.25	0.00	41.10	28.49	2.00	0.00	0.25	0.00
41.20	28.68	2.00	0.00	0.25	0.00	41.30	30.71	2.00	0.00	0.25	0.00
41.40	34.10	2.00	0.00	0.25	0.00	41.50	32.99	2.00	0.00	0.25	0.00
41.60	31.20	2.00	0.00	0.24	0.00	41.70	30.17	2.00	0.00	0.24	0.00
41.80	30.75	2.00	0.00	0.24	0.00	41.90	38.09	2.00	0.00	0.24	0.00
42.00	123.35	2.00	0.00	0.24	0.00	42.10	144.62	2.00	0.00	0.23	0.00
42.20	167.49	2.00	0.00	0.23	0.00	42.30	183.72	2.00	0.00	0.23	0.00
42.40	194.13	2.00	0.00	0.23	0.00	42.50	208.09	2.00	0.00	0.23	0.00
42.60	219.33	2.00	0.00	0.23	0.00	42.70	223.26	2.00	0.00	0.22	0.00
42.80	218.39	2.00	0.00	0.22	0.00	42.90	208.73	2.00	0.00	0.22	0.00
43.00	198.59	2.00	0.00	0.22	0.00	43.10	186.49	2.00	0.00	0.22	0.00
43.20	174.24	2.00	0.00	0.21	0.00	43.30	165.23	2.00	0.00	0.21	0.00
43.40	158.53	2.00	0.00	0.21	0.00	43.50	151.37	2.00	0.00	0.21	0.00
43.60	144.57	2.00	0.00	0.21	0.00	43.70	131.64	2.00	0.00	0.21	0.00
43.80	132.11	2.00	0.00	0.20	0.00	43.90	142.72	2.00	0.00	0.20	0.00
44.00	153.33	2.00	0.00	0.20	0.00	44.10	161.23	2.00	0.00	0.20	0.00
44.20	163.51	2.00	0.00	0.20	0.00	44.30	166.64	2.00	0.00	0.19	0.00
44.40	164.79	2.00	0.00	0.19	0.00	44.50	156.11	2.00	0.00	0.19	0.00
44.60	144.89	2.00	0.00	0.19	0.00	44.70	137.91	2.00	0.00	0.19	0.00
44.80	143.63	2.00	0.00	0.19	0.00	44.90	160.01	2.00	0.00	0.18	0.00
45.00	177.20	2.00	0.00	0.18	0.00	45.10	190.98	2.00	0.00	0.18	0.00
45.20	198.94	1.89	0.01	0.18	0.00	45.30	200.81	2.00	0.00	0.18	0.00
45.40	198.05	2.00	0.00	0.17	0.00	45.50	191.19	2.00	0.00	0.17	0.00
45.60	180.44	2.00	0.00	0.17	0.00	45.70	167.41	2.00	0.00	0.17	0.00
45.80	153.55	2.00	0.00	0.17	0.00	45.90	141.51	2.00	0.00	0.17	0.00
46.00	131.86	0.22	0.39	0.16	0.00	46.10	125.22	2.00	0.00	0.16	0.00
46.20	124.81	2.00	0.00	0.16	0.00	46.30	128.58	2.00	0.00	0.16	0.00
46.40	136.66	2.00	0.00	0.16	0.00	46.50	148.30	2.00	0.00	0.15	0.00
46.60	162.08	2.00	0.00	0.15	0.00	46.70	176.54	0.68	0.15	0.15	0.00
46.80	186.81	1.04	0.10	0.15	0.00	46.90	188.86	1.14	0.08	0.15	0.00
47.00	186.54	1.03	0.10	0.15	0.00	47.10	185.93	1.00	0.10	0.14	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
47.20	185.38	0.97	0.10	0.14	0.00	47.30	183.93	0.92	0.10	0.14	0.00
47.40	186.83	1.04	0.09	0.14	0.00	47.50	195.45	1.56	0.03	0.14	0.00
47.60	205.90	2.00	0.00	0.13	0.00	47.70	216.02	2.00	0.00	0.13	0.00
47.80	224.00	2.00	0.00	0.13	0.00	47.90	228.55	2.00	0.00	0.13	0.00
48.00	230.14	2.00	0.00	0.13	0.00	48.10	231.27	2.00	0.00	0.13	0.00
48.20	232.84	2.00	0.00	0.12	0.00	48.30	235.20	2.00	0.00	0.12	0.00
48.40	236.73	2.00	0.00	0.12	0.00	48.50	237.12	2.00	0.00	0.12	0.00
48.60	236.54	2.00	0.00	0.12	0.00	48.70	234.64	2.00	0.00	0.11	0.00
48.80	234.59	2.00	0.00	0.11	0.00	48.90	235.70	2.00	0.00	0.11	0.00
49.00	237.54	2.00	0.00	0.11	0.00	49.10	239.79	2.00	0.00	0.11	0.00
49.20	242.85	2.00	0.00	0.11	0.00	49.30	246.07	2.00	0.00	0.10	0.00
49.40	250.75	2.00	0.00	0.10	0.00	49.50	254.16	2.00	0.00	0.10	0.00
49.60	247.90	2.00	0.00	0.10	0.00	49.70	234.60	2.00	0.00	0.10	0.00
49.80	233.40	2.00	0.00	0.09	0.00	49.90	238.44	2.00	0.00	0.09	0.00

Total estimated settlement: 0.89**Abbreviations**

$Q_{tn,cs}$:	Equivalent clean sand normalized cone resistance
FS:	Factor of safety against liquefaction
e_v (%):	Post-liquefaction volumetric strain
DF:	e_v depth weighting factor
Settlement:	Calculated settlement

:: Strength loss calculation Idriss & Boulanger (2008) ::

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.10	20.69	33.24	1.53	50.97	2.16	0.08	0.72
0.20	15.95	25.60	1.85	47.43	2.28	0.07	0.70
0.30	12.29	19.73	2.41	47.48	2.41	0.07	0.67
0.40	12.85	20.62	2.36	48.75	2.40	0.07	0.69
0.50	17.93	28.76	1.86	53.61	2.28	0.08	0.70
0.60	25.60	41.08	1.59	65.46	2.19	0.09	0.73
0.70	35.62	57.17	1.44	82.32	2.11	0.10	0.76
0.80	45.80	73.51	1.36	100.06	2.06	0.12	0.79
0.90	55.07	88.39	1.32	116.65	2.01	0.14	0.80
1.00	61.98	99.50	1.30	129.32	1.99	0.17	0.82
1.10	65.41	104.99	1.30	136.08	1.99	0.18	0.83
1.20	66.73	107.11	1.30	139.05	1.99	0.17	0.82
1.30	68.80	110.41	1.30	143.31	1.99	0.18	0.83
1.40	72.09	115.70	1.29	149.74	1.98	0.21	0.84
1.50	75.47	121.12	1.29	156.40	1.98	0.22	0.84
1.60	77.78	124.82	1.29	161.32	1.98	0.23	0.85
1.70	79.45	127.49	1.30	165.15	1.99	0.26	0.86
1.80	79.92	128.24	1.30	166.89	1.99	0.26	0.86
1.90	78.74	126.34	1.31	165.78	2.01	0.25	0.86
2.00	77.53	124.39	1.32	164.55	2.02	0.25	0.86
2.10	76.45	122.63	1.33	163.29	2.03	0.24	0.86
2.20	74.95	120.21	1.34	161.41	2.04	0.24	0.86
2.30	72.03	115.52	1.36	157.68	2.06	0.23	0.86
2.40	66.61	106.80	1.41	150.52	2.09	0.21	0.85
2.50	59.83	95.89	1.47	141.20	2.13	0.18	0.83
2.60	53.38	85.53	1.53	131.20	2.17	0.16	0.82
2.70	48.56	77.77	1.57	122.22	2.18	0.14	0.81
2.80	45.31	72.54	1.58	114.67	2.19	0.13	0.80
2.90	44.32	70.93	1.55	109.70	2.17	0.13	0.79
3.00	45.95	73.54	1.49	109.47	2.14	0.13	0.79
3.10	48.29	77.29	1.47	113.45	2.13	0.14	0.81
3.20	48.11	77.00	1.52	116.90	2.16	0.15	0.81
3.30	44.42	71.05	1.66	118.06	2.22	0.14	0.80
3.40	38.42	61.40	1.92	117.92	2.30	0.13	0.79
3.50	31.66	50.53	2.32	117.39	2.39	0.12	0.77
3.60	25.01	39.85	2.94	117.18	2.49	0.10	0.75
3.70	18.93	30.07	3.89	117.02	2.62	0.10	0.62
3.80	13.89	21.96	5.28	116.00	2.75	0.09	0.62
3.90	9.83	15.43	7.28	112.34	2.91	0.08	0.62
4.00	6.71	10.41	10.03	104.40	3.07	0.08	2.00
4.10	4.73	7.22	13.17	95.15	3.22	0.07	1.35
4.20	3.30	4.91	17.17	84.37	3.37	0.07	0.90
4.30	2.28	3.26	22.48	73.39	3.53	0.07	0.59
4.40	1.63	2.22	28.79	63.82	3.68	0.07	0.39
4.50	1.68	2.29	27.79	63.71	3.66	0.07	0.40
4.60	1.90	2.63	25.60	67.34	3.61	0.07	0.45
4.70	1.99	2.78	25.32	70.36	3.60	0.07	0.47
4.80	2.28	3.22	23.67	76.30	3.56	0.07	0.53

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
4.90	3.08	4.50	18.72	84.26	3.42	0.07	0.73
5.00	5.02	7.62	12.30	93.72	3.18	0.07	1.21
5.10	8.35	12.95	7.64	98.96	2.93	0.08	0.62
5.20	12.99	20.40	5.19	105.89	2.74	0.09	0.62
5.30	17.05	26.91	4.35	117.17	2.67	0.10	0.62
5.40	18.42	29.11	4.35	126.71	2.67	0.10	0.62
5.50	17.82	28.14	4.55	128.03	2.68	0.09	0.62
5.60	18.27	28.84	4.05	116.72	2.63	0.09	0.62
5.70	22.60	35.79	2.77	99.18	2.47	0.10	0.73
5.80	30.34	48.23	1.87	90.04	2.28	0.11	0.76
5.90	38.67	61.59	1.53	94.11	2.16	0.12	0.78
6.00	44.41	70.82	1.45	102.98	2.12	0.13	0.79
6.10	46.53	74.21	1.48	110.20	2.14	0.13	0.80
6.20	45.75	72.94	1.56	113.95	2.18	0.13	0.80
6.30	44.18	70.41	1.63	114.84	2.21	0.13	0.79
6.40	43.27	68.93	1.65	113.55	2.21	0.13	0.79
6.50	43.29	68.97	1.61	111.32	2.20	0.13	0.79
6.60	44.11	70.27	1.56	109.67	2.18	0.12	0.79
6.70	45.23	72.06	1.51	108.77	2.15	0.12	0.79
6.80	46.59	74.23	1.47	108.95	2.13	0.12	0.79
6.90	47.78	76.14	1.45	110.13	2.12	0.12	0.79
7.00	47.94	76.39	1.46	111.47	2.13	0.13	0.79
7.10	46.35	73.82	1.52	112.29	2.16	0.13	0.79
7.20	43.14	68.66	1.64	112.58	2.21	0.12	0.78
7.30	39.20	62.31	1.79	111.40	2.26	0.12	0.78
7.40	35.95	57.08	1.88	107.20	2.29	0.11	0.77
7.50	34.90	55.39	1.81	100.25	2.27	0.11	0.76
7.60	36.71	58.29	1.63	94.73	2.20	0.10	0.76
7.70	40.76	64.78	1.47	95.22	2.13	0.11	0.77
7.80	45.18	71.87	1.39	100.11	2.08	0.11	0.77
7.90	48.49	77.19	1.37	105.57	2.06	0.12	0.78
8.00	50.35	80.17	1.37	109.85	2.06	0.12	0.78
8.10	50.92	81.06	1.40	113.84	2.09	0.12	0.78
8.20	50.43	80.28	1.52	121.97	2.16	0.13	0.79
8.30	48.21	76.70	1.75	134.35	2.25	0.13	0.79
8.40	44.03	69.97	2.14	150.02	2.35	0.13	0.79
8.50	38.01	60.29	2.73	164.35	2.46	0.12	0.78
8.60	31.11	49.19	3.58	176.05	2.58	0.11	0.76
8.70	24.26	38.18	4.84	184.82	2.71	0.10	0.62
8.80	18.28	28.57	6.53	186.56	2.85	0.10	0.62
8.90	13.46	20.81	8.69	180.75	2.99	0.09	0.62
9.00	9.80	14.92	11.17	166.56	3.13	0.08	1.38
9.10	7.41	11.08	13.57	150.27	3.24	0.08	1.02
9.20	6.33	9.33	14.73	137.48	3.28	0.08	0.85
9.30	6.36	9.37	14.03	131.50	3.25	0.08	0.85
9.40	7.05	10.47	12.36	129.44	3.18	0.08	0.95
9.50	7.58	11.30	11.36	128.38	3.14	0.08	1.02
9.60	7.34	10.92	11.64	127.04	3.15	0.08	0.98

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.70	6.26	9.18	13.31	122.20	3.23	0.08	0.82
9.80	7.93	11.84	11.56	136.93	3.15	0.07	1.05
9.90	13.13	20.20	8.40	169.74	2.98	0.09	0.62
10.00	18.80	29.30	6.71	196.61	2.87	0.10	0.62
10.10	18.67	29.08	6.78	197.10	2.87	0.10	0.62
10.20	14.65	22.60	7.92	178.94	2.95	0.09	0.62
10.30	10.95	16.66	9.39	156.43	3.03	0.08	1.44
10.40	10.48	15.89	9.61	152.60	3.05	0.08	1.37
10.50	11.16	16.97	9.27	157.24	3.03	0.08	1.45
10.60	13.38	20.54	8.46	173.77	2.98	0.09	0.62
10.70	16.24	25.11	7.47	187.67	2.92	0.09	0.62
10.80	23.16	36.23	5.43	196.70	2.77	0.10	0.62
10.90	36.54	57.71	3.10	178.75	2.52	0.11	0.76
11.00	57.04	88.45	1.81	159.83	2.27	0.15	0.81
11.10	77.62	114.63	1.39	159.74	2.08	0.18	0.83
11.20	91.25	130.35	1.28	166.81	1.96	0.20	0.83
11.30	96.49	135.48	1.24	168.37	1.91	0.20	0.83
11.40	96.73	134.67	1.23	165.52	1.89	0.19	0.82
11.50	93.84	130.50	1.24	161.19	1.90	0.19	0.82
11.60	89.17	124.60	1.26	156.73	1.93	0.18	0.82
11.70	82.47	116.28	1.29	150.52	1.98	0.16	0.82
11.80	74.34	105.91	1.35	142.88	2.04	0.15	0.82
11.90	66.88	96.17	1.42	136.60	2.10	0.14	0.81
12.00	59.90	86.73	1.50	130.39	2.15	0.14	0.80
12.10	54.60	79.33	1.58	124.95	2.18	0.13	0.79
12.20	52.76	76.48	1.59	121.82	2.19	0.12	0.78
12.30	53.42	76.99	1.57	120.93	2.18	0.13	0.79
12.40	55.36	79.28	1.54	122.10	2.17	0.13	0.79
12.50	55.60	79.32	1.54	121.95	2.17	0.13	0.79
12.60	55.04	78.40	1.56	122.09	2.18	0.13	0.79
12.70	54.18	77.34	1.62	125.14	2.20	0.13	0.79
12.80	51.05	73.48	1.78	130.74	2.26	0.13	0.79
12.90	44.55	65.06	2.12	138.09	2.35	0.12	0.78
13.00	37.39	55.53	2.70	150.10	2.46	0.11	0.76
13.10	30.77	46.44	3.50	162.59	2.57	0.11	0.75
13.20	26.49	40.37	4.23	170.94	2.65	0.10	0.62
13.30	22.74	34.83	4.92	171.28	2.72	0.10	0.62
13.40	20.92	32.01	5.25	168.18	2.75	0.09	0.62
13.50	20.31	30.95	5.35	165.57	2.76	0.09	0.62
13.60	20.02	30.39	5.39	163.90	2.76	0.09	0.62
13.70	19.28	29.13	5.47	159.27	2.77	0.09	0.62
13.80	18.73	28.14	5.48	154.30	2.77	0.09	0.62
13.90	18.04	27.02	5.63	152.22	2.78	0.09	0.62
14.00	16.71	25.01	6.10	152.62	2.82	0.09	0.62
14.10	15.17	22.72	6.79	154.31	2.87	0.09	0.62
14.20	14.03	21.02	7.44	156.38	2.92	0.09	0.62
14.30	11.65	17.23	8.72	150.24	3.00	0.09	0.62
14.40	7.83	11.11	11.85	131.58	3.16	0.08	0.79

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
14.50	4.04	5.07	20.03	101.58	3.46	0.07	0.36
14.60	2.41	2.48	32.40	80.21	3.75	0.07	0.18
14.70	2.41	2.46	31.74	78.12	3.74	0.07	0.18
14.80	2.41	2.45	31.05	75.98	3.72	0.07	0.17
14.90	2.19	2.09	34.01	71.06	3.78	0.07	0.15
15.00	1.79	1.45	43.72	63.39	3.93	0.07	0.10
15.10	1.39	0.81	54.25	44.18	4.06	0.07	0.06
15.20	1.20	0.52	54.25	28.39	4.06	0.07	0.04
15.30	1.20	0.52	54.25	27.97	4.06	0.07	0.04
15.40	1.39	0.80	54.25	43.31	4.06	0.07	0.06
15.50	2.04	1.79	43.11	77.37	3.92	0.07	0.13
15.60	3.92	4.67	20.83	97.25	3.49	0.07	0.33
15.70	7.11	9.53	12.14	115.74	3.17	0.08	0.68
15.80	10.59	14.80	8.75	129.53	3.00	0.08	0.62
15.90	12.22	17.23	7.96	137.10	2.95	0.09	0.62
16.00	11.38	15.88	8.64	137.25	2.99	0.08	0.62
16.10	9.26	12.61	10.24	129.07	3.08	0.08	0.90
16.20	7.35	9.69	11.85	114.76	3.16	0.08	0.69
16.30	6.42	8.25	12.61	104.02	3.19	0.07	0.59
16.40	6.02	7.62	13.01	99.12	3.21	0.07	0.54
16.50	5.80	7.25	13.41	97.25	3.23	0.07	0.52
16.60	5.19	6.31	14.74	92.99	3.28	0.07	0.45
16.70	4.26	4.91	17.43	85.54	3.38	0.07	0.35
16.80	3.29	3.46	22.06	76.36	3.52	0.07	0.25
16.90	2.90	2.87	24.80	71.23	3.59	0.07	0.21
17.00	2.86	2.79	24.87	69.38	3.59	0.07	0.20
17.10	3.23	3.32	21.80	72.39	3.51	0.07	0.24
17.20	3.29	3.39	21.78	73.85	3.51	0.07	0.24
17.30	3.07	3.06	23.92	73.25	3.57	0.07	0.22
17.40	2.98	2.91	25.07	72.92	3.60	0.07	0.21
17.50	3.69	3.92	19.79	77.63	3.45	0.07	0.28
17.60	5.22	6.13	14.10	86.38	3.26	0.07	0.44
17.70	6.73	8.29	11.30	93.63	3.13	0.08	0.59
17.80	7.04	8.70	11.02	95.85	3.12	0.08	0.62
17.90	6.09	7.30	12.72	92.87	3.20	0.07	0.52
18.00	4.82	5.45	15.99	87.15	3.33	0.07	0.39
18.10	4.08	4.37	19.01	83.11	3.43	0.07	0.31
18.20	4.56	5.03	17.59	88.54	3.39	0.07	0.36
18.30	7.27	8.86	12.52	111.00	3.19	0.07	0.63
18.40	12.35	16.00	9.01	144.21	3.01	0.08	1.14
18.50	17.77	23.51	7.44	174.91	2.92	0.09	0.62
18.60	19.06	25.20	7.38	185.92	2.91	0.10	0.62
18.70	18.07	23.78	7.62	181.17	2.93	0.09	0.62
18.80	16.83	21.92	7.43	162.95	2.92	0.09	0.62
18.90	18.43	23.75	6.30	149.63	2.83	0.09	0.62
19.00	21.05	26.87	5.15	138.46	2.74	0.09	0.62
19.10	24.45	30.90	4.16	128.68	2.65	0.09	0.62
19.20	28.33	35.51	3.47	123.26	2.57	0.10	0.73

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
19.30	31.79	39.71	3.24	128.71	2.54	0.10	0.74
19.40	33.34	41.77	3.51	146.58	2.57	0.11	0.75
19.50	32.10	40.45	4.19	169.34	2.65	0.11	0.62
19.60	28.67	36.30	5.15	187.09	2.74	0.10	0.62
19.70	24.81	31.39	6.04	189.60	2.81	0.10	0.62
19.80	25.42	31.99	5.77	184.75	2.79	0.09	0.62
19.90	32.01	39.85	4.40	175.37	2.67	0.10	0.62
20.00	40.24	49.34	3.14	154.94	2.52	0.12	0.77
20.10	47.35	57.16	2.34	133.96	2.39	0.12	0.77
20.20	50.45	60.22	2.00	120.70	2.32	0.12	0.78
20.30	51.38	61.26	2.05	125.66	2.33	0.12	0.78
20.40	47.65	56.93	2.31	131.65	2.39	0.12	0.78
20.50	41.70	49.84	2.63	131.07	2.45	0.11	0.76
20.60	36.95	44.08	2.89	127.22	2.49	0.10	0.75
20.70	35.66	42.51	3.11	132.03	2.52	0.10	0.75
20.80	35.84	42.85	3.49	149.51	2.57	0.11	0.75
20.90	33.79	40.57	4.22	171.40	2.65	0.11	0.62
21.00	28.53	34.35	5.42	186.05	2.76	0.10	0.62
21.10	22.40	26.91	6.95	187.10	2.88	0.09	0.62
21.20	18.70	22.22	8.04	178.64	2.95	0.09	0.62
21.30	17.11	20.13	8.45	170.13	2.98	0.09	0.62
21.40	16.52	19.31	8.58	165.68	2.99	0.09	0.62
21.50	15.83	18.36	8.79	161.39	3.00	0.09	1.31
21.60	15.40	17.76	8.89	157.77	3.01	0.09	1.27
21.70	15.00	17.19	9.02	155.16	3.01	0.09	1.23
21.80	14.79	16.86	9.26	156.12	3.03	0.08	1.20
21.90	15.25	17.37	9.40	163.21	3.04	0.09	1.24
22.00	15.77	17.95	9.52	170.98	3.04	0.09	1.28
22.10	16.13	18.32	9.53	174.52	3.04	0.09	1.31
22.20	16.33	18.50	9.25	171.13	3.03	0.09	1.32
22.30	17.20	19.49	8.49	165.61	2.98	0.09	0.62
22.40	18.93	21.53	7.56	162.66	2.92	0.09	0.62
22.50	20.75	23.56	6.82	160.68	2.87	0.09	0.62
22.60	22.36	25.32	6.28	158.98	2.83	0.09	0.62
22.70	23.55	26.59	5.92	157.52	2.81	0.09	0.62
22.80	24.27	27.32	5.76	157.34	2.79	0.10	0.62
22.90	24.79	27.82	5.64	156.78	2.78	0.10	0.62
23.00	25.40	28.39	5.40	153.41	2.76	0.10	0.62
23.10	26.63	29.65	5.04	149.33	2.73	0.10	0.62
23.20	27.97	31.08	4.85	150.73	2.71	0.10	0.62
23.30	28.02	31.08	5.08	157.89	2.73	0.10	0.62
23.40	25.97	28.74	5.75	165.31	2.79	0.10	0.62
23.50	22.41	24.66	6.73	166.04	2.87	0.09	0.62
23.60	19.33	21.06	7.60	160.07	2.93	0.09	0.62
23.70	17.40	18.73	8.04	150.55	2.95	0.09	0.62
23.80	16.53	17.65	8.09	142.73	2.96	0.09	0.62
23.90	16.15	17.15	8.10	139.01	2.96	0.09	0.62
24.00	15.80	16.69	8.31	138.60	2.97	0.09	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
24.10	14.52	15.16	8.98	136.16	3.01	0.09	1.08
24.20	11.33	11.44	10.94	125.22	3.12	0.08	0.82
24.30	8.08	7.67	14.25	109.35	3.26	0.07	0.55
24.40	5.93	5.19	18.21	94.56	3.41	0.07	0.37
24.50	5.62	4.83	18.60	89.77	3.42	0.07	0.34
24.60	5.62	4.81	18.27	87.89	3.41	0.07	0.34
24.70	5.77	4.97	17.88	88.79	3.40	0.07	0.35
24.80	6.24	5.48	17.08	93.57	3.37	0.07	0.39
24.90	6.78	6.06	16.47	99.86	3.35	0.07	0.43
25.00	7.16	6.47	16.36	105.93	3.34	0.07	0.46
25.10	7.19	6.48	16.95	109.82	3.36	0.07	0.46
25.20	6.84	6.06	18.13	109.92	3.40	0.07	0.43
25.30	6.30	5.44	19.62	106.76	3.45	0.07	0.39
25.40	5.81	4.87	20.97	102.13	3.49	0.07	0.35
25.50	5.62	4.65	21.32	99.16	3.50	0.07	0.33
25.60	5.62	4.63	21.18	98.13	3.50	0.07	0.33
25.70	5.62	4.62	21.18	97.77	3.50	0.07	0.33
25.80	5.62	4.60	21.06	96.87	3.49	0.07	0.33
25.90	5.74	4.71	20.23	95.31	3.47	0.07	0.34
26.00	6.01	4.99	18.94	94.48	3.43	0.07	0.36
26.10	6.06	5.03	18.69	94.04	3.42	0.07	0.36
26.20	5.94	4.88	19.26	94.06	3.44	0.07	0.35
26.30	5.68	4.58	20.53	93.92	3.48	0.07	0.33
26.40	5.62	4.50	21.10	94.95	3.49	0.07	0.32
26.50	5.72	4.59	20.94	96.20	3.49	0.07	0.33
26.60	6.14	5.03	19.45	97.81	3.44	0.07	0.36
26.70	6.68	5.59	17.92	100.18	3.40	0.07	0.40
26.80	7.11	6.04	17.23	104.06	3.37	0.07	0.43
26.90	7.23	6.15	17.62	108.41	3.39	0.07	0.44
27.00	7.58	6.50	17.71	115.06	3.39	0.07	0.46
27.10	8.22	7.16	17.22	123.35	3.37	0.08	0.51
27.20	9.74	8.76	15.41	134.97	3.31	0.08	0.63
27.30	13.33	12.55	11.91	149.50	3.16	0.08	0.90
27.40	19.91	19.49	8.12	158.22	2.96	0.09	0.62
27.50	30.24	30.15	5.12	154.48	2.74	0.10	0.62
27.60	41.52	41.60	3.59	149.55	2.58	0.11	0.76
27.70	49.24	49.37	3.14	155.01	2.52	0.13	0.78
27.80	49.82	49.90	3.39	169.00	2.56	0.13	0.78
27.90	44.25	44.15	4.10	181.00	2.64	0.12	0.62
28.00	36.48	36.12	5.03	181.72	2.73	0.11	0.62
28.10	29.33	28.72	6.01	172.64	2.81	0.10	0.62
28.20	23.96	23.14	6.98	161.61	2.88	0.09	0.62
28.30	19.51	18.48	8.32	153.82	2.97	0.09	0.62
28.40	15.84	14.65	10.20	149.43	3.08	0.08	1.05
28.50	12.93	11.62	12.61	146.47	3.19	0.08	0.83
28.60	12.75	11.39	13.33	151.86	3.23	0.08	0.81
28.70	15.29	13.95	11.70	163.26	3.15	0.08	1.00
28.80	18.82	17.49	9.82	171.85	3.06	0.09	1.25

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
28.90	20.53	19.18	8.97	171.95	3.01	0.09	1.37
29.00	20.27	18.85	8.94	168.48	3.01	0.09	1.35
29.10	18.46	16.96	9.68	164.12	3.05	0.09	1.21
29.20	16.60	15.04	10.53	158.43	3.10	0.08	1.07
29.30	16.51	14.91	10.12	150.91	3.07	0.08	1.06
29.40	20.13	18.48	7.71	142.45	2.93	0.09	0.62
29.50	27.09	25.29	5.37	135.82	2.76	0.10	0.62
29.60	33.16	31.18	4.29	133.73	2.66	0.10	0.62
29.70	36.69	34.57	3.99	137.83	2.63	0.10	0.62
29.80	40.80	38.51	3.97	152.89	2.62	0.11	0.62
29.90	48.32	45.76	3.80	173.96	2.61	0.12	0.62
30.00	59.72	56.73	3.17	179.81	2.53	0.13	0.79
30.10	73.28	69.68	2.47	171.93	2.42	0.15	0.81
30.20	85.57	81.32	2.01	163.64	2.32	0.18	0.83
30.30	94.24	89.46	1.86	166.65	2.28	0.19	0.84
30.40	96.38	91.31	1.92	175.56	2.30	0.20	0.84
30.50	93.45	88.28	2.09	184.55	2.34	0.20	0.84
30.60	85.88	80.82	2.40	194.35	2.41	0.18	0.83
30.70	75.59	70.78	2.87	203.41	2.48	0.16	0.81
30.80	64.96	60.44	3.39	205.19	2.56	0.14	0.80
30.90	58.02	53.66	3.64	195.46	2.59	0.13	0.78
31.00	57.76	53.25	3.29	175.20	2.54	0.13	0.78
31.10	64.29	59.30	2.56	151.63	2.43	0.13	0.79
31.20	74.72	69.01	1.96	135.05	2.31	0.15	0.81
31.30	84.37	77.95	1.66	129.45	2.22	0.16	0.82
31.40	91.02	84.05	1.55	129.96	2.17	0.16	0.82
31.50	94.21	86.86	1.51	130.81	2.15	0.17	0.83
31.60	94.73	87.16	1.49	129.89	2.14	0.17	0.82
31.70	92.99	85.34	1.50	128.04	2.15	0.16	0.82
31.80	89.90	82.26	1.54	127.00	2.17	0.16	0.82
31.90	86.48	78.87	1.61	127.32	2.20	0.15	0.82
32.00	83.14	75.57	1.72	129.94	2.24	0.15	0.81
32.10	79.62	72.09	1.88	135.85	2.29	0.15	0.81
32.20	75.05	67.65	2.13	144.01	2.35	0.15	0.81
32.30	69.21	62.06	2.41	149.69	2.41	0.14	0.80
32.40	63.30	56.45	2.61	147.58	2.44	0.13	0.79
32.50	60.94	54.16	2.54	137.73	2.43	0.12	0.78
32.60	65.02	57.83	2.17	125.25	2.36	0.13	0.78
32.70	74.05	66.03	1.83	121.08	2.27	0.14	0.80
32.80	83.30	74.38	1.69	125.62	2.23	0.15	0.81
32.90	89.30	79.69	1.68	133.79	2.22	0.16	0.82
33.00	94.12	83.89	1.69	141.45	2.23	0.17	0.83
33.10	101.14	90.11	1.63	146.50	2.20	0.18	0.83
33.20	112.44	100.24	1.51	151.82	2.16	0.20	0.85
33.30	126.20	112.59	1.43	161.02	2.11	0.25	0.86
33.40	137.62	122.75	1.40	171.45	2.08	0.31	0.88
33.50	143.17	127.48	1.40	178.43	2.09	0.34	0.88
33.60	142.56	126.60	1.42	179.91	2.10	0.33	0.88

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
33.70	140.15	124.12	1.44	178.51	2.11	0.31	0.88
33.80	138.78	122.61	1.44	176.68	2.11	0.30	0.88
33.90	138.19	121.82	1.44	175.59	2.11	0.31	0.88
34.00	135.99	119.56	1.45	173.87	2.12	0.30	0.88
34.10	131.92	115.61	1.49	171.69	2.14	0.28	0.87
34.20	126.82	110.75	1.53	168.98	2.16	0.26	0.87
34.30	122.27	106.42	1.57	166.75	2.18	0.24	0.86
34.40	118.79	103.06	1.60	164.44	2.19	0.23	0.86
34.50	116.72	101.00	1.60	162.03	2.20	0.23	0.86
34.60	116.13	100.27	1.59	159.86	2.19	0.22	0.85
34.70	116.42	100.33	1.58	158.43	2.19	0.22	0.85
34.80	116.08	99.83	1.57	157.06	2.18	0.22	0.86
34.90	113.21	97.07	1.59	154.41	2.19	0.22	0.85
35.00	107.12	91.47	1.64	150.40	2.21	0.20	0.84
35.10	98.36	83.53	1.76	146.61	2.25	0.18	0.83
35.20	88.33	74.49	1.95	145.13	2.31	0.16	0.82
35.30	78.11	65.34	2.21	144.33	2.37	0.15	0.81
35.40	70.66	58.71	2.40	140.97	2.41	0.13	0.79
35.50	68.31	56.59	2.36	133.62	2.40	0.13	0.79
35.60	71.04	58.91	2.14	126.28	2.35	0.13	0.79
35.70	76.04	63.18	1.95	123.30	2.31	0.14	0.80
35.80	80.43	66.88	1.85	124.02	2.28	0.15	0.81
35.90	83.79	69.62	1.83	127.50	2.27	0.15	0.81
36.00	86.97	72.18	1.83	132.35	2.27	0.15	0.81
36.10	90.89	75.33	1.84	138.64	2.28	0.16	0.82
36.20	95.24	78.84	1.86	146.32	2.28	0.17	0.83
36.30	98.94	81.74	1.89	154.77	2.29	0.19	0.84
36.40	100.43	82.73	1.96	162.04	2.31	0.19	0.84
36.50	99.89	81.99	2.05	167.72	2.33	0.19	0.84
36.60	98.07	80.15	2.16	173.25	2.36	0.19	0.84
36.70	95.06	77.30	2.33	179.97	2.39	0.19	0.83
36.80	89.45	72.26	2.59	187.05	2.44	0.18	0.83
36.90	80.70	64.60	3.01	194.29	2.50	0.16	0.82
37.00	69.82	55.23	3.66	202.10	2.59	0.15	0.80
37.10	58.94	45.95	4.54	208.64	2.68	0.13	0.63
37.20	50.59	38.90	5.37	208.94	2.76	0.12	0.62
37.30	46.04	35.09	5.68	199.45	2.79	0.11	0.62
37.40	45.72	34.83	5.23	182.11	2.75	0.11	0.62
37.50	48.88	37.49	4.31	161.52	2.66	0.11	0.62
37.60	54.47	42.16	3.44	144.96	2.56	0.12	0.77
37.70	60.92	47.50	2.89	137.04	2.49	0.13	0.78
37.80	66.48	52.02	2.62	136.49	2.44	0.13	0.79
37.90	71.26	55.89	2.46	137.24	2.42	0.14	0.79
38.00	76.37	60.07	2.24	134.83	2.37	0.14	0.80
38.10	82.38	65.07	1.99	129.40	2.32	0.15	0.81
38.20	88.96	70.57	1.78	125.79	2.26	0.15	0.81
38.30	94.06	74.74	1.69	126.27	2.23	0.16	0.82
38.40	96.38	76.48	1.69	129.16	2.23	0.17	0.82

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
38.50	95.22	75.26	1.75	131.62	2.25	0.17	0.82
38.60	91.50	71.97	1.83	131.86	2.27	0.16	0.82
38.70	86.76	67.88	1.92	130.30	2.30	0.15	0.81
38.80	82.49	64.22	1.99	127.88	2.32	0.15	0.81
38.90	79.99	62.06	2.01	124.95	2.32	0.14	0.80
39.00	79.66	61.74	1.96	120.80	2.31	0.14	0.80
39.10	80.98	62.84	1.84	115.76	2.28	0.14	0.80
39.20	81.39	63.13	1.79	112.74	2.26	0.14	0.80
39.30	77.05	59.38	1.90	112.75	2.29	0.14	0.80
39.40	68.00	51.69	2.30	118.71	2.38	0.13	0.78
39.50	55.58	41.34	3.13	129.50	2.52	0.12	0.77
39.60	43.51	31.48	4.46	140.57	2.68	0.11	0.62
39.70	32.08	22.36	6.43	143.78	2.84	0.10	0.62
39.80	24.49	16.60	8.43	139.94	2.98	0.09	0.62
39.90	25.69	17.46	8.21	143.33	2.97	0.09	0.62
40.00	28.88	19.80	7.50	148.45	2.92	0.10	0.62
40.10	26.02	17.62	8.18	144.17	2.96	0.10	0.62
40.20	17.22	11.05	11.50	127.06	3.14	0.08	0.79
40.30	10.69	6.18	17.67	109.18	3.39	0.07	0.44
40.40	11.62	6.85	16.74	114.73	3.36	0.08	0.49
40.50	14.83	9.21	13.59	125.12	3.24	0.08	0.66
40.60	19.14	12.36	10.71	132.38	3.10	0.08	0.88
40.70	24.64	16.37	8.32	136.17	2.97	0.09	0.62
40.80	30.34	20.52	6.68	137.08	2.86	0.10	0.62
40.90	34.36	23.54	5.80	136.50	2.80	0.10	0.62
41.00	35.62	24.47	5.51	134.71	2.77	0.10	0.62
41.10	35.36	24.22	5.49	133.05	2.77	0.10	0.62
41.20	35.52	24.29	5.48	133.12	2.77	0.10	0.62
41.30	37.77	25.92	5.32	137.77	2.76	0.10	0.62
41.40	39.51	27.12	5.38	145.91	2.76	0.11	0.62
41.50	39.75	27.14	5.75	156.14	2.79	0.11	0.62
41.60	38.24	25.83	6.46	166.81	2.85	0.10	0.62
41.70	37.40	25.16	6.97	175.34	2.88	0.10	0.62
41.80	40.17	27.09	6.62	179.45	2.86	0.10	0.62
41.90	50.73	35.02	5.02	175.81	2.73	0.11	0.62
42.00	69.20	49.29	3.26	160.50	2.54	0.14	0.79
42.10	94.71	69.50	2.05	142.66	2.33	0.16	0.82
42.20	121.87	91.48	1.52	139.20	2.16	0.21	0.85
42.30	147.28	112.12	1.35	151.37	2.05	0.28	0.87
42.40	168.54	129.14	1.30	167.86	1.99	0.36	0.88
42.50	184.42	141.54	1.29	181.95	1.97	0.52	0.90
42.60	194.06	148.80	1.28	191.17	1.97	0.70	0.91
42.70	194.52	148.65	1.30	192.61	1.99	0.75	0.91
42.80	186.27	141.56	1.32	186.66	2.01	0.60	0.91
42.90	172.77	130.36	1.36	176.86	2.05	0.45	0.90
43.00	157.23	117.60	1.42	166.71	2.10	0.35	0.89
43.10	141.54	104.80	1.51	158.67	2.16	0.28	0.87
43.20	127.00	92.93	1.67	155.22	2.22	0.23	0.86

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
43.30	114.88	82.98	1.91	158.67	2.30	0.21	0.85
43.40	105.17	74.92	2.26	169.64	2.38	0.19	0.84
43.50	96.99	68.21	2.67	181.83	2.45	0.18	0.83
43.60	87.91	61.12	3.01	184.17	2.51	0.17	0.82
43.70	82.13	56.81	3.07	174.37	2.51	0.15	0.80
43.80	82.78	57.50	2.74	157.36	2.46	0.15	0.80
43.90	91.57	64.35	2.25	144.98	2.38	0.16	0.82
44.00	103.19	73.37	1.90	139.21	2.29	0.18	0.83
44.10	111.95	80.18	1.71	137.01	2.24	0.20	0.84
44.20	116.80	83.81	1.65	138.27	2.21	0.20	0.84
44.30	116.61	83.18	1.74	144.81	2.25	0.21	0.85
44.40	111.71	78.69	2.01	158.02	2.32	0.21	0.85
44.50	102.58	71.14	2.43	172.75	2.41	0.19	0.84
44.60	93.13	63.78	2.79	177.83	2.47	0.17	0.82
44.70	89.79	61.35	2.75	168.46	2.46	0.16	0.81
44.80	96.85	66.93	2.27	151.81	2.38	0.16	0.82
44.90	113.10	79.55	1.79	142.30	2.26	0.19	0.84
45.00	132.27	94.33	1.54	145.46	2.17	0.24	0.86
45.10	147.43	105.80	1.46	154.46	2.13	0.30	0.88
45.20	155.41	111.47	1.46	162.21	2.12	0.35	0.89
45.30	156.28	111.60	1.49	166.12	2.14	0.36	0.89
45.40	151.54	107.52	1.55	166.61	2.17	0.34	0.88
45.50	142.44	100.16	1.66	165.78	2.22	0.30	0.88
45.60	129.99	90.25	1.86	167.45	2.28	0.26	0.87
45.70	115.63	78.99	2.20	173.53	2.36	0.22	0.85
45.80	101.57	68.20	2.65	180.86	2.45	0.19	0.83
45.90	89.43	59.18	3.07	181.54	2.51	0.16	0.82
46.00	80.36	52.68	3.26	171.70	2.54	0.15	0.80
46.10	75.66	49.51	3.14	155.32	2.52	0.14	0.79
46.20	75.96	49.99	2.77	138.71	2.47	0.14	0.79
46.30	81.99	54.66	2.30	125.66	2.39	0.14	0.80
46.40	93.65	63.56	1.85	117.53	2.28	0.15	0.81
46.50	110.56	76.54	1.53	117.13	2.16	0.17	0.82
46.60	129.39	90.92	1.38	125.92	2.08	0.20	0.84
46.70	144.05	101.68	1.35	137.61	2.05	0.25	0.86
46.80	149.85	105.16	1.39	146.60	2.08	0.28	0.87
46.90	147.45	102.23	1.50	153.73	2.15	0.29	0.87
47.00	142.18	97.28	1.67	162.30	2.22	0.28	0.87
47.10	138.12	93.55	1.82	170.72	2.27	0.28	0.87
47.20	136.30	91.82	1.90	174.43	2.29	0.28	0.87
47.30	137.24	92.45	1.86	171.87	2.28	0.27	0.87
47.40	142.58	96.55	1.73	166.68	2.24	0.28	0.87
47.50	152.84	104.38	1.58	164.46	2.18	0.32	0.88
47.60	165.80	114.11	1.47	167.72	2.13	0.40	0.89
47.70	177.89	123.01	1.42	174.14	2.10	0.50	0.90
47.80	187.02	129.49	1.40	180.72	2.08	0.62	0.91
47.90	192.69	133.40	1.39	184.92	2.08	0.70	0.92
48.00	196.25	135.83	1.38	187.00	2.07	0.74	0.92

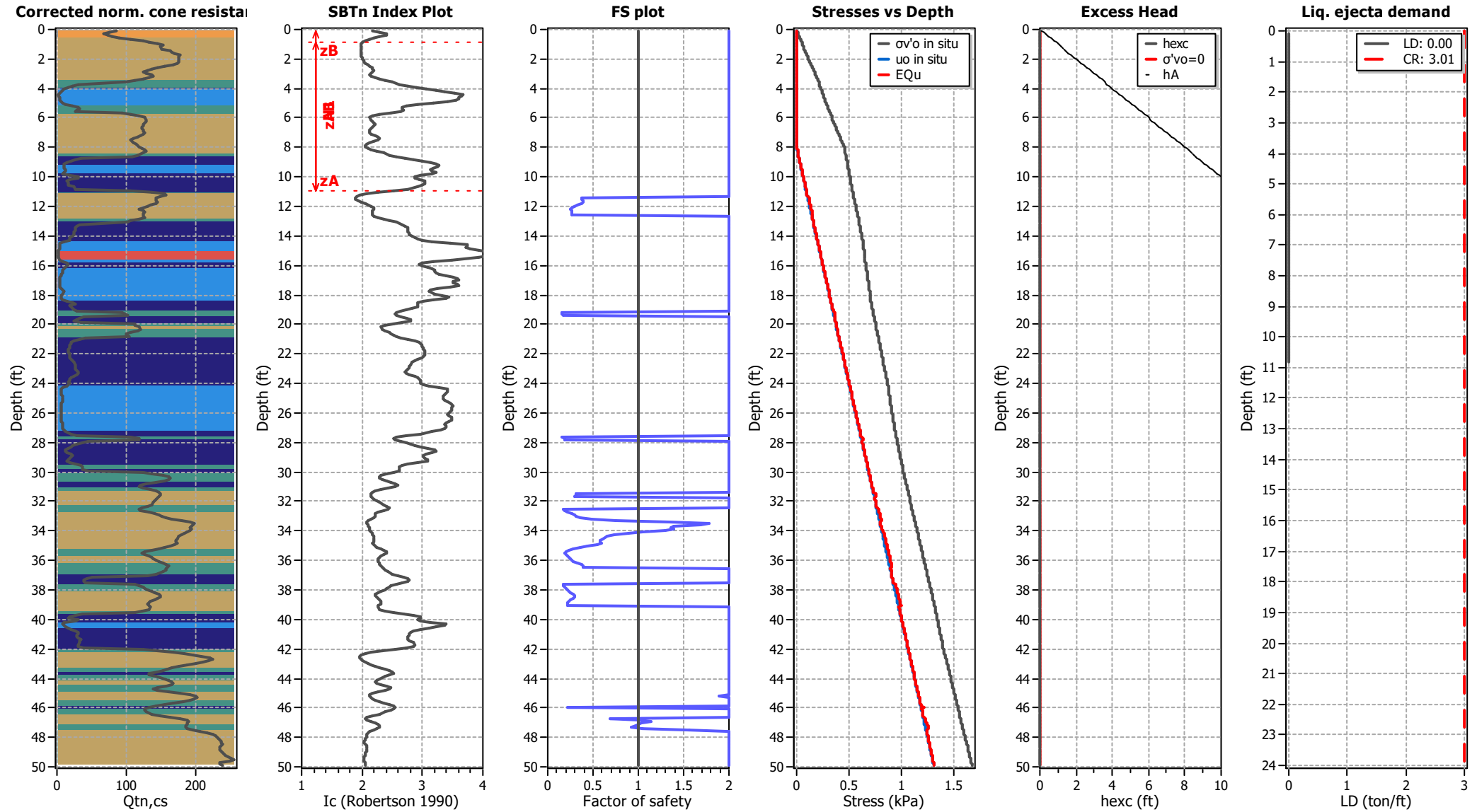
:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
48.10	199.18	137.90	1.36	188.02	2.06	0.78	0.92
48.20	202.36	140.14	1.35	189.38	2.05	0.83	0.92
48.30	204.97	141.89	1.34	190.75	2.04	0.88	0.92
48.40	206.02	142.34	1.35	191.69	2.04	0.88	0.92
48.50	205.06	141.17	1.36	191.83	2.05	0.88	0.92
48.60	202.72	138.98	1.38	191.18	2.07	0.87	0.92
48.70	200.81	137.19	1.39	190.43	2.08	0.83	0.92
48.80	200.45	136.68	1.39	189.96	2.08	0.83	0.92
48.90	202.19	137.80	1.38	190.37	2.07	0.86	0.92
49.00	205.17	139.85	1.37	191.52	2.06	0.88	0.92
49.10	208.80	142.34	1.36	193.42	2.05	0.88	0.93
49.20	212.77	145.01	1.35	195.97	2.05	0.88	0.93
49.30	217.38	148.13	1.34	199.07	2.04	0.88	0.93
49.40	221.74	151.06	1.34	202.00	2.03	0.89	0.94
49.50	222.23	151.15	1.34	202.10	2.03	0.89	0.94
49.60	216.25	146.54	1.35	197.41	2.04	0.88	0.93
49.70	208.44	140.66	1.36	191.32	2.05	0.86	0.92
49.80	204.58	137.59	1.37	188.42	2.06	0.82	0.92
49.90	205.34	137.86	1.37	188.96	2.06	0.87	0.93

Abbreviations

q_t :	Total cone resistance
K_c :	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c :	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

Ejecta Severity Estimation



LIQUEFACTION ANALYSIS REPORT

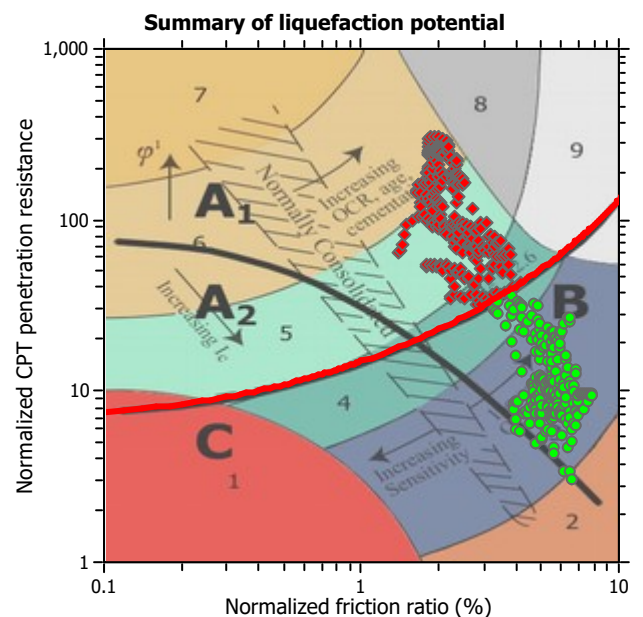
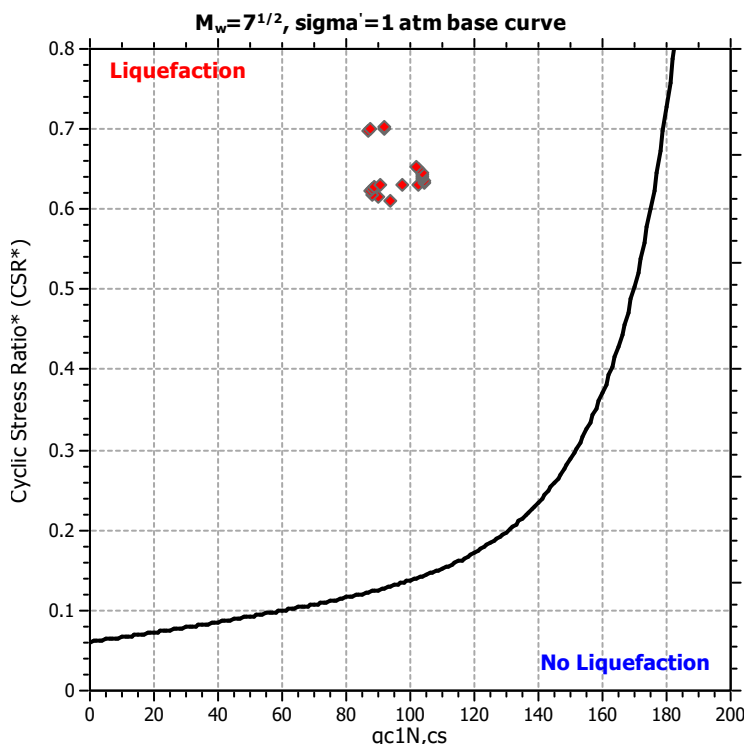
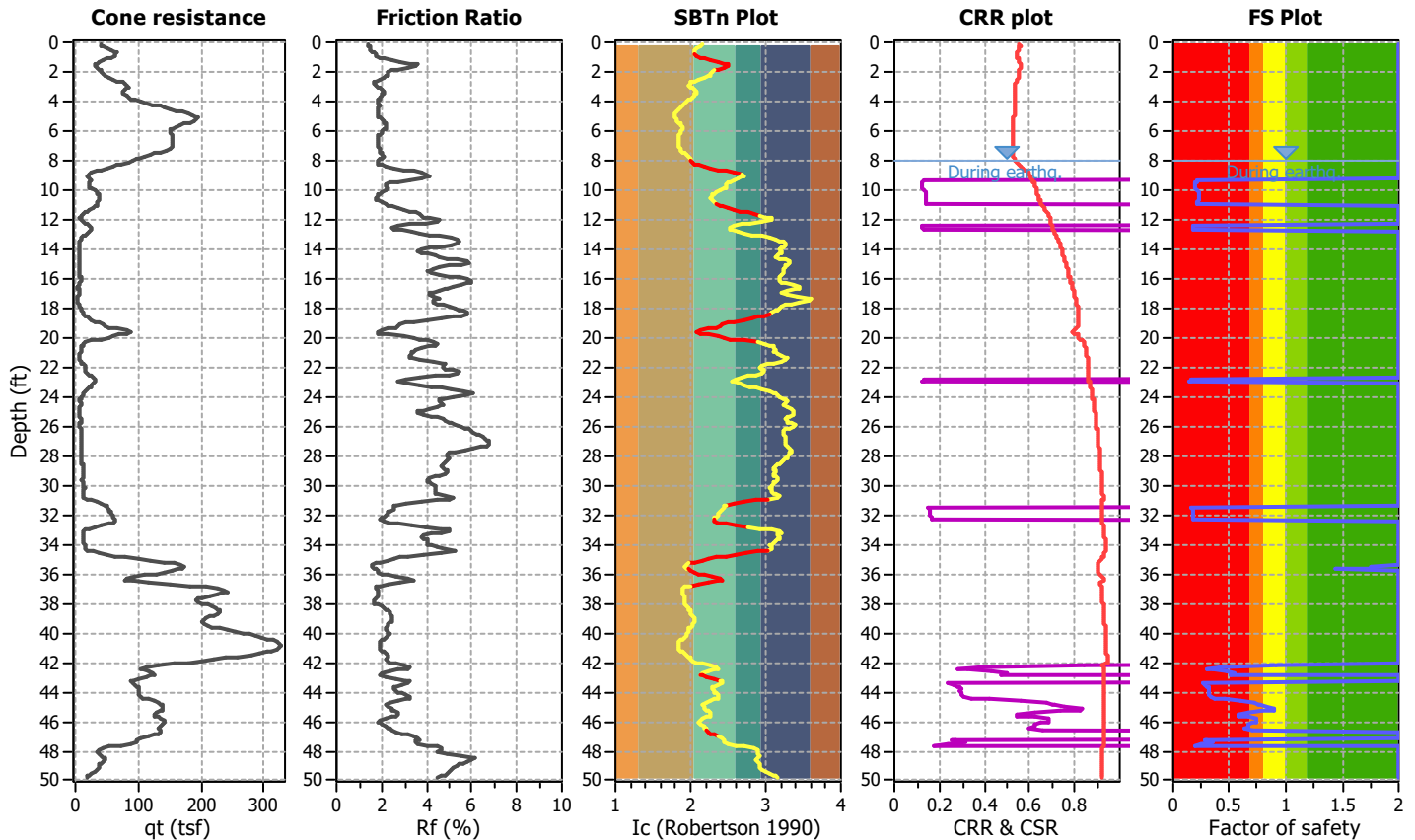
Project title : 21-483 Equestrian Estates

Location : Avenue 64 at Harrison Street, Thermal California

CPT file : CPT-4 B&I 2014

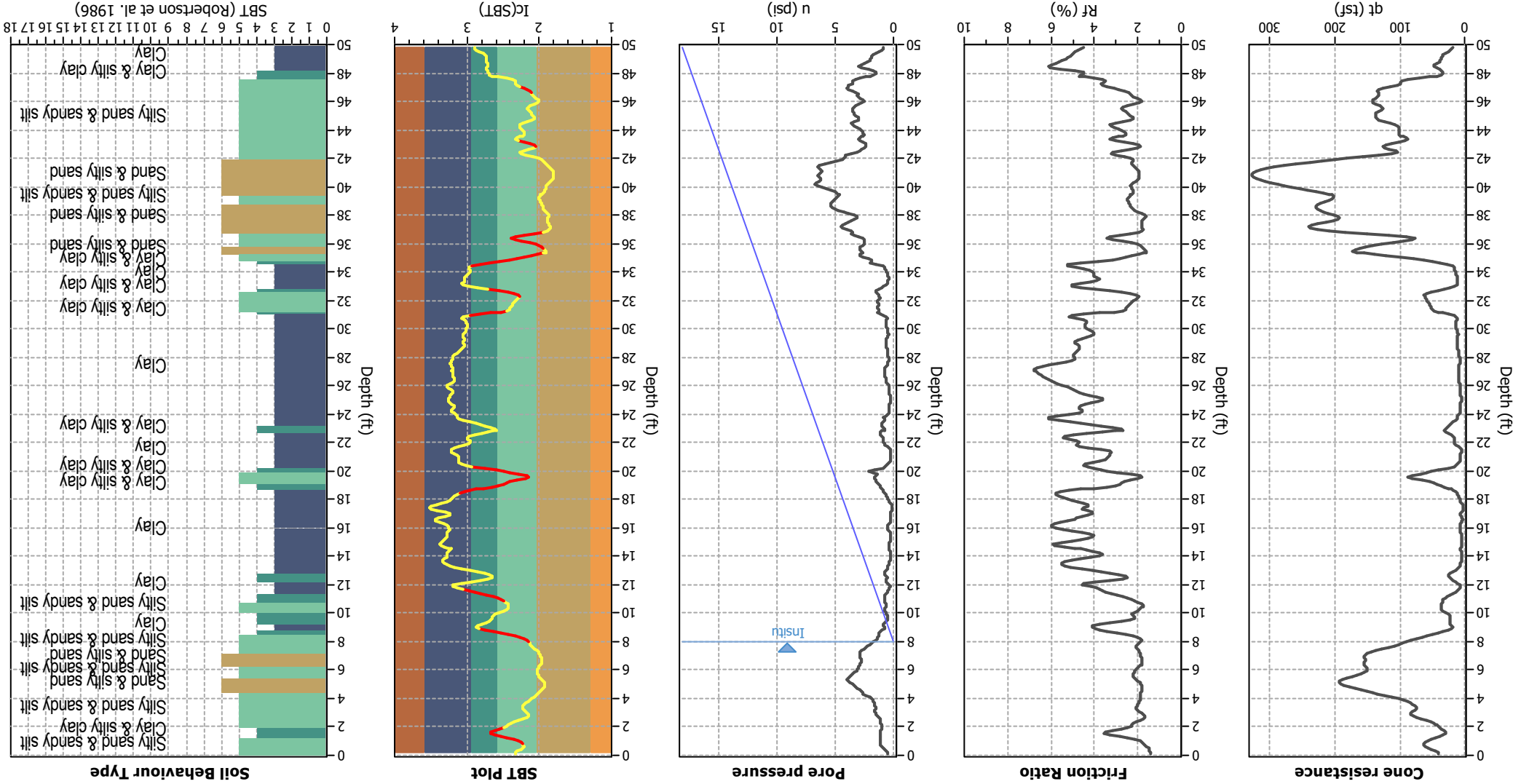
Input parameters and analysis data

Analysis method:	B&I (2014)	G.W.T. (in-situ):	8.00 ft	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	8.00 ft	Fill height:	N/A	applied:	Sands only
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude M_w :	7.34	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.74	Unit weight calculation:	Based on SBT	K_σ applied:	Yes	MSF method:	Method based



Zone A₁: Cyclic liquefaction likely depending on size and duration of cyclic loading
 Zone A₂: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
 Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
 Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



Input parameters and analysis data

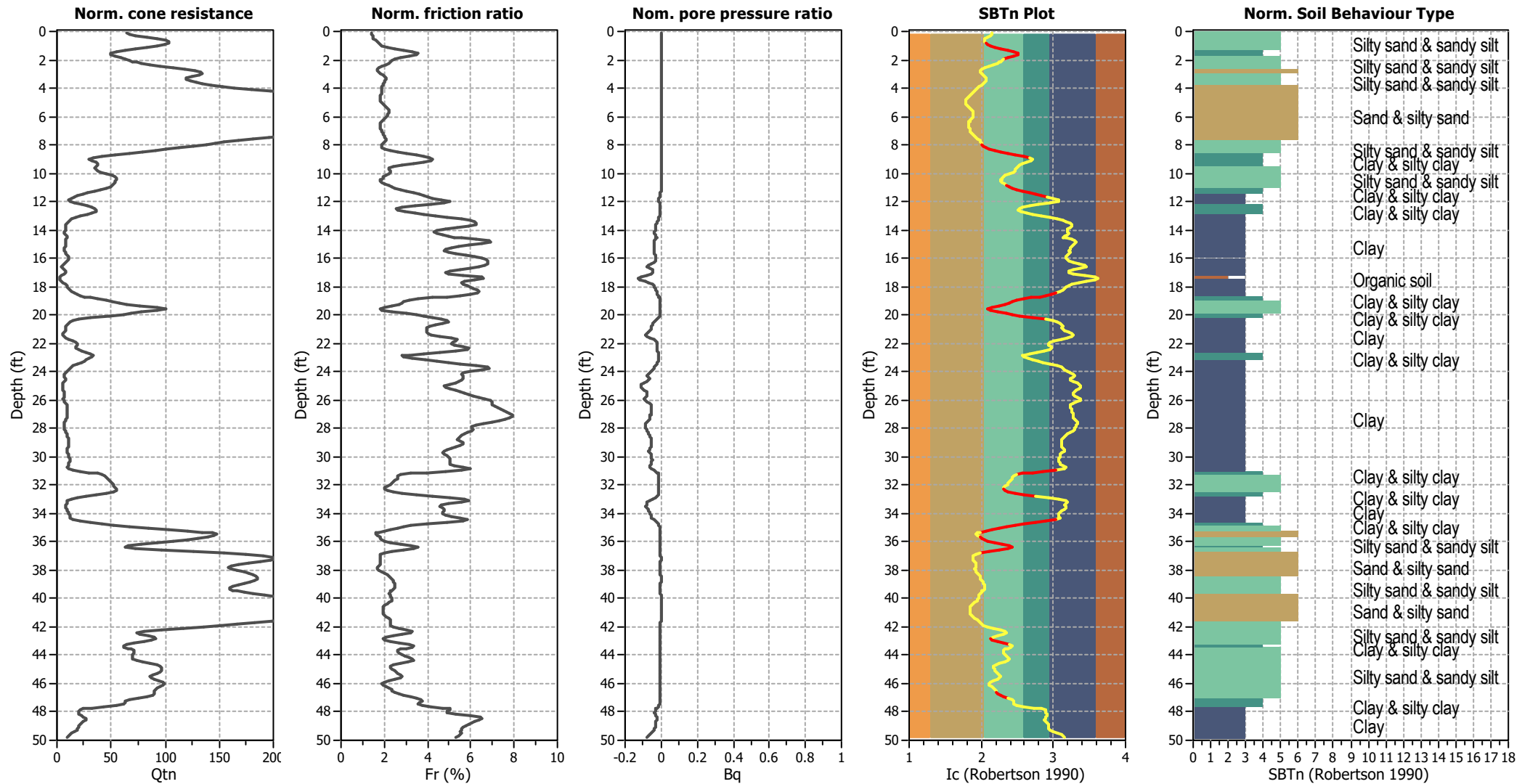
Analysis method: B&I (2014)
Fines correction method: B&I (2014)
Points to test: Based on Ic value
Earthquake magnitude M_w : 7.34
Peak ground acceleration: 0.74
Depth to water table (insitu): 8.00 ft

Depth to GWT (erthq.): 8.00 ft
Average results interval: 3
Ic cut-off value: 2.60
Unit weight calculation: Based on SBT
Use fill: No
Fill height: N/A
Fill weight: N/A
Transition detect. applied: Yes
Clay like behavior applied: Sands only
Limit depth applied: No
Limit depth: N/A

SBT legend

1. Sensitive fine grained	2. Organic material	3. Clay to silty clay
4. Clayey silt to silty	5. Silty sand to sandy silt	6. Clean sand to silty sand
7. Gravely sand to sand	8. Very stiff sand to	9. Very stiff fine grained

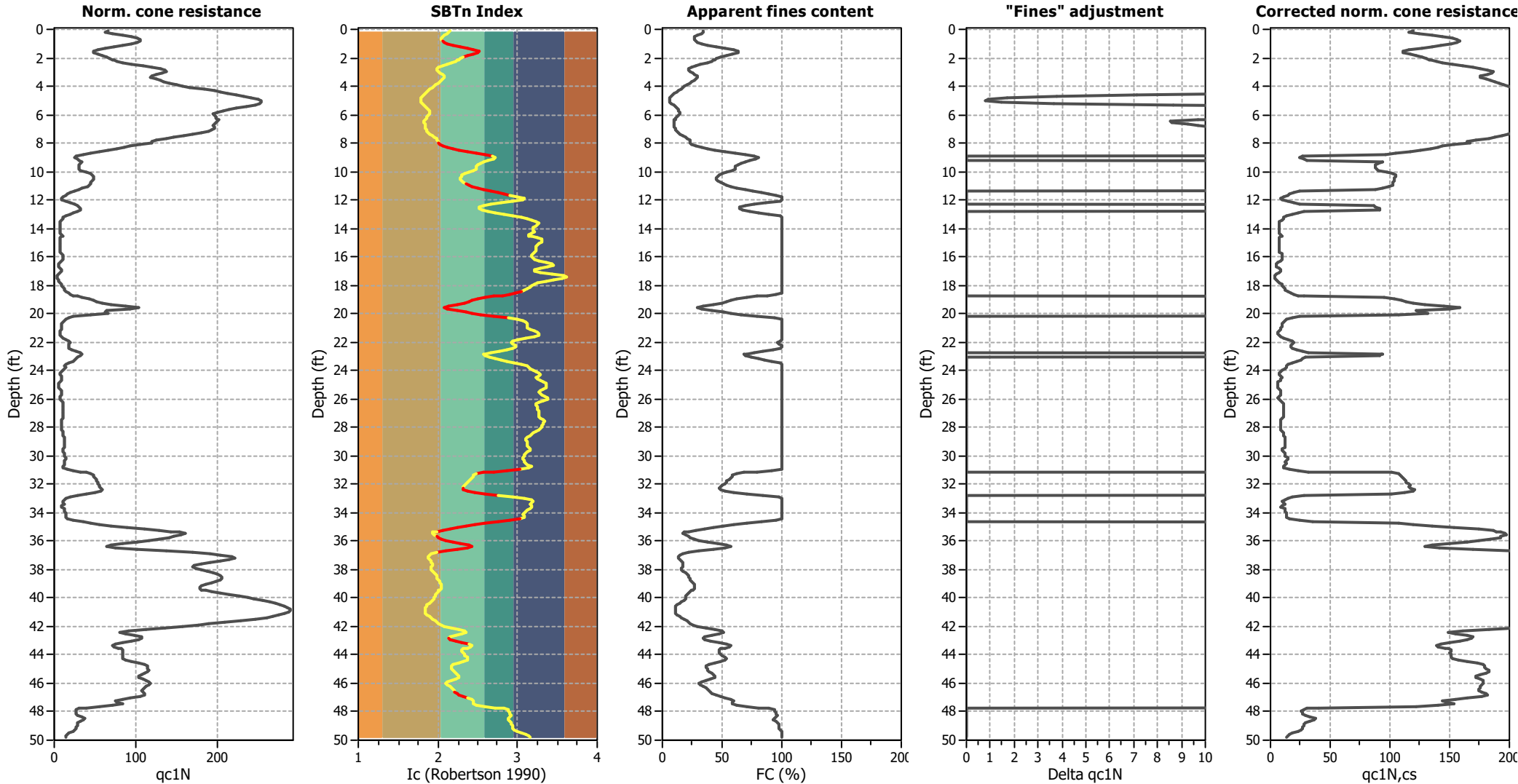
CPT basic interpretation plots (normalized)



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K ₀ applied:	Yes
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

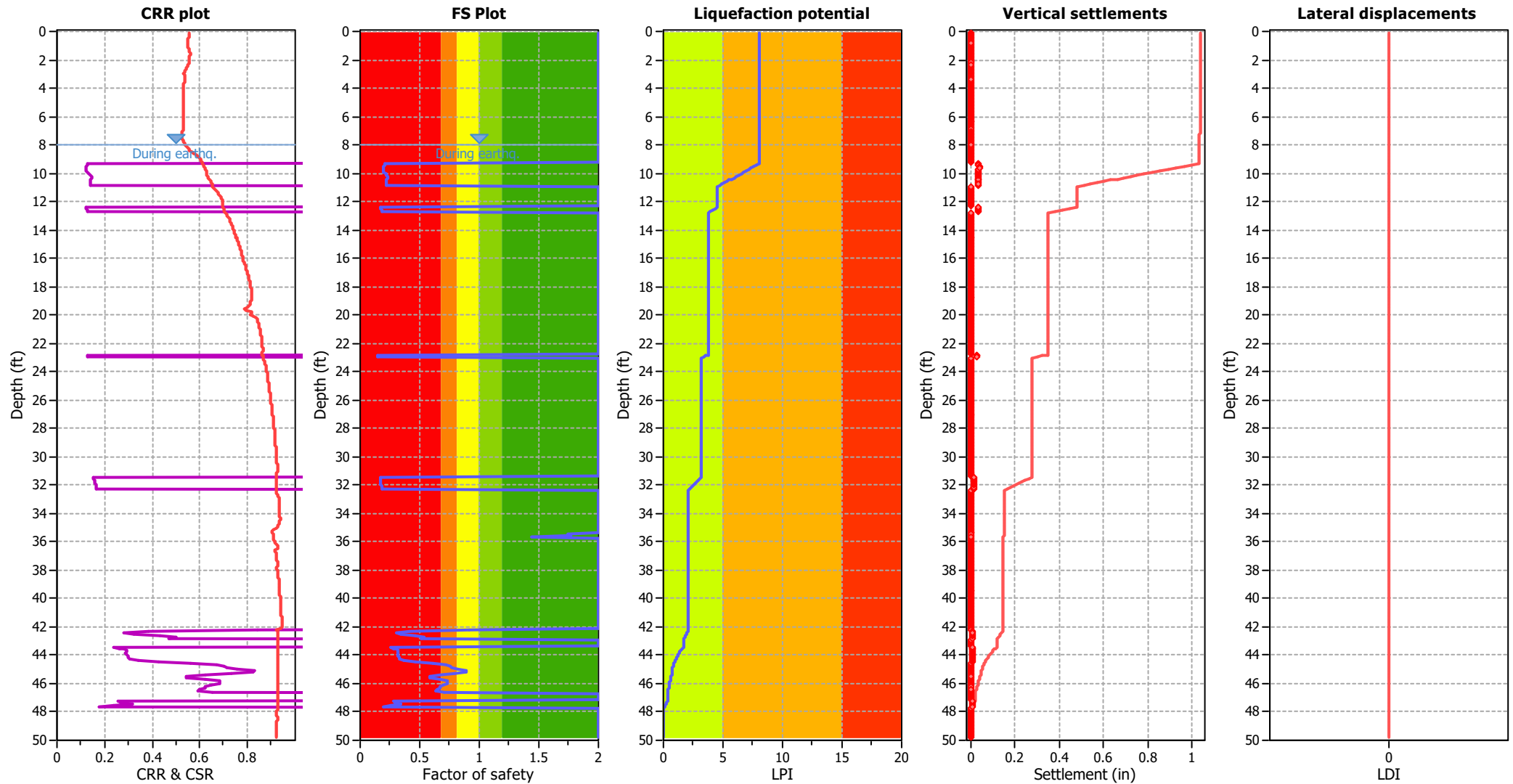
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on I_c value	I_c cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (earthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

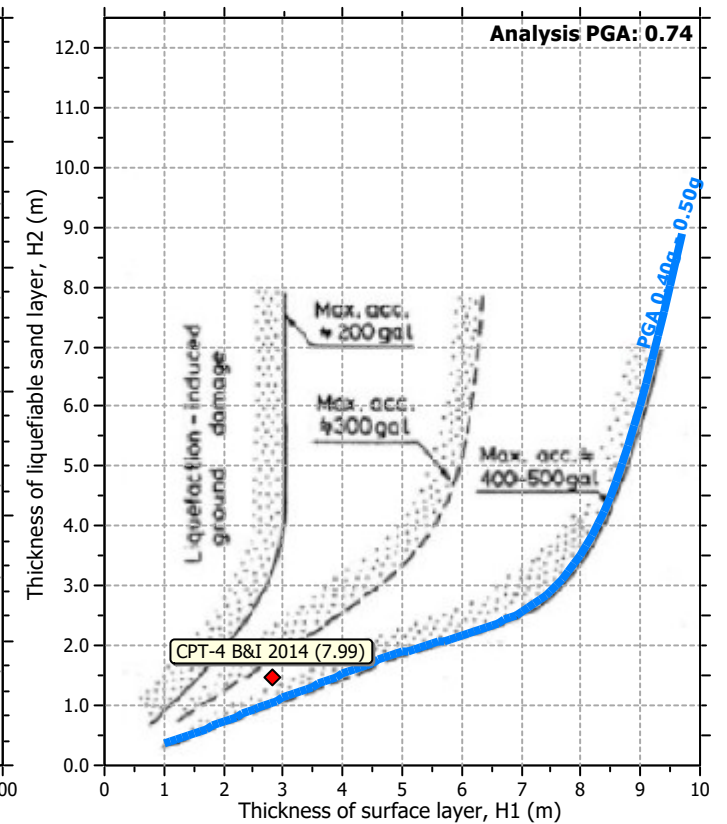
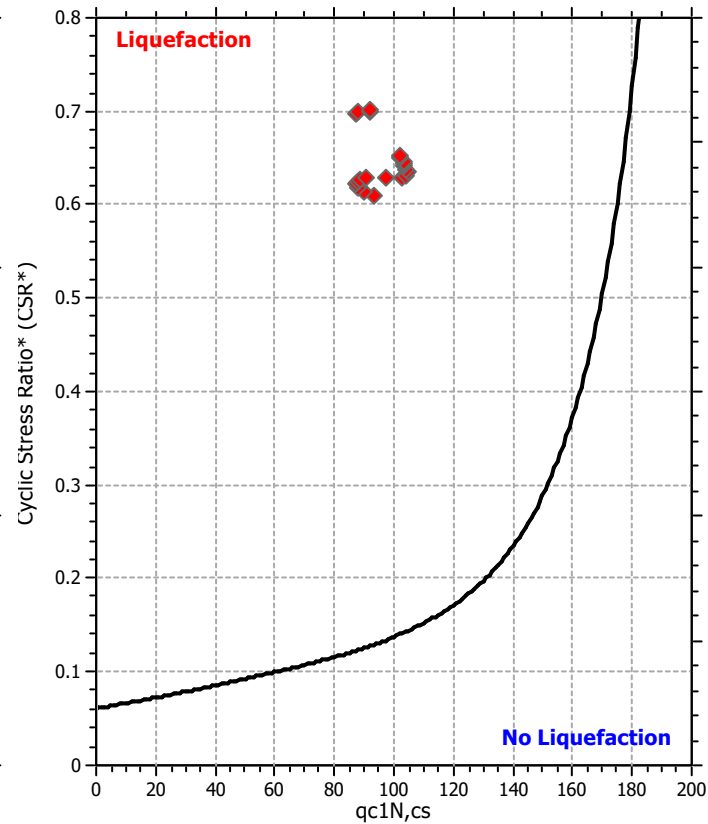
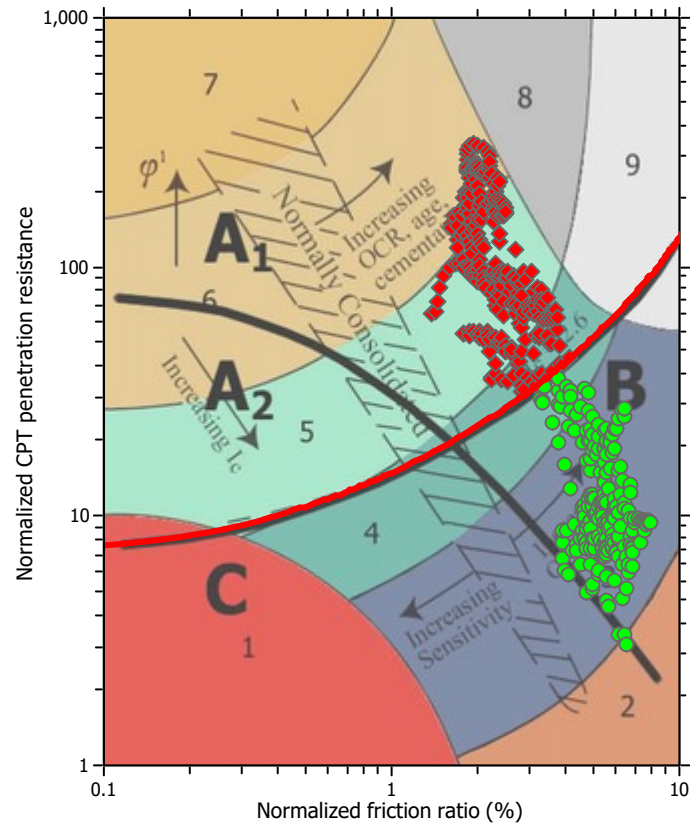
F.S. color scheme

■	Almost certain it will liquefy
■	Very likely to liquefy
■	Liquefaction and no liq. are equally likely
■	Unlike to liquefy
■	Almost certain it will not liquefy

LPI color scheme

■	Very high risk
■	High risk
■	Low risk

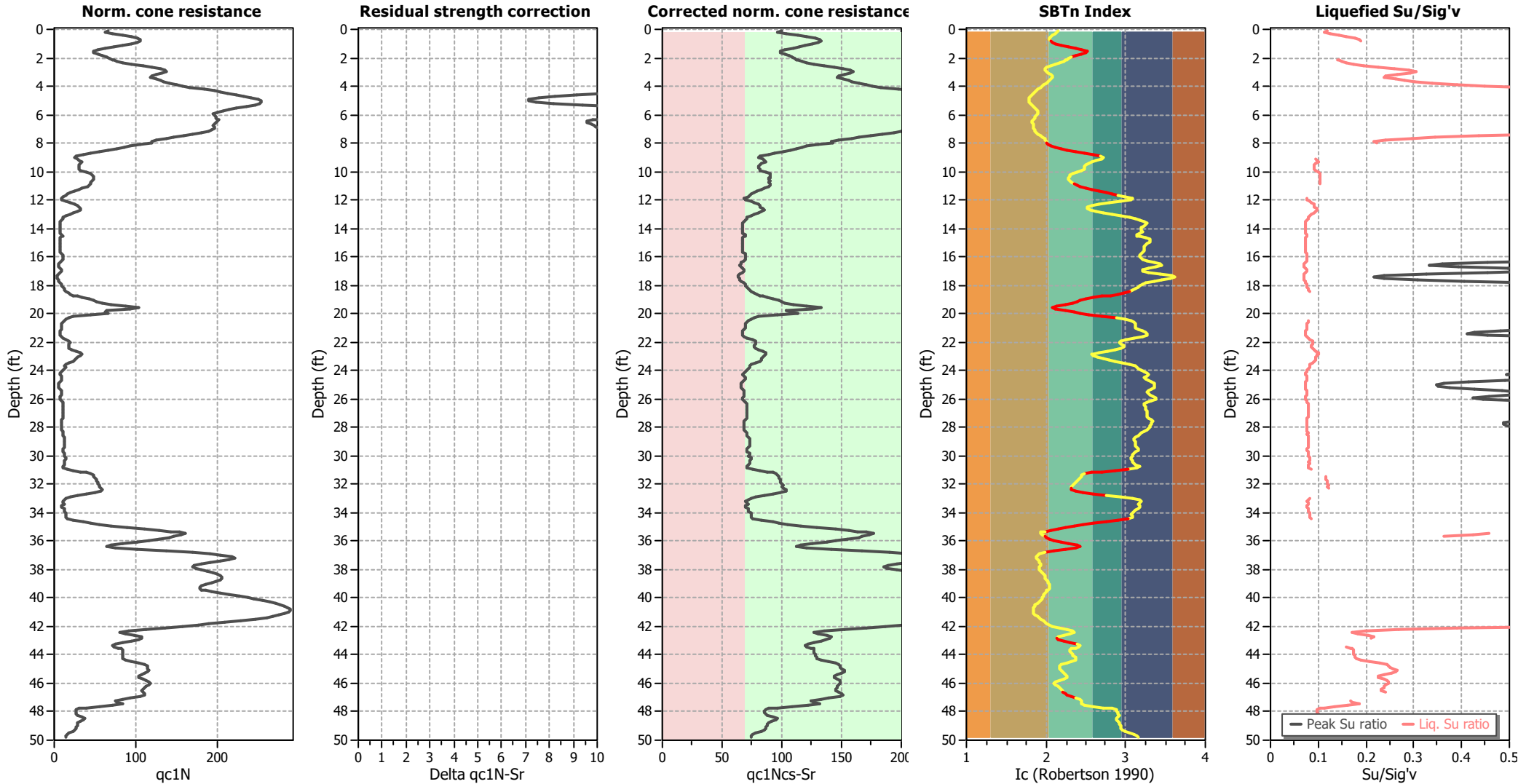
Liquefaction analysis summary plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	Yes
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

Check for strength loss plots (Idriss & Boulanger (2008))



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	Yes
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

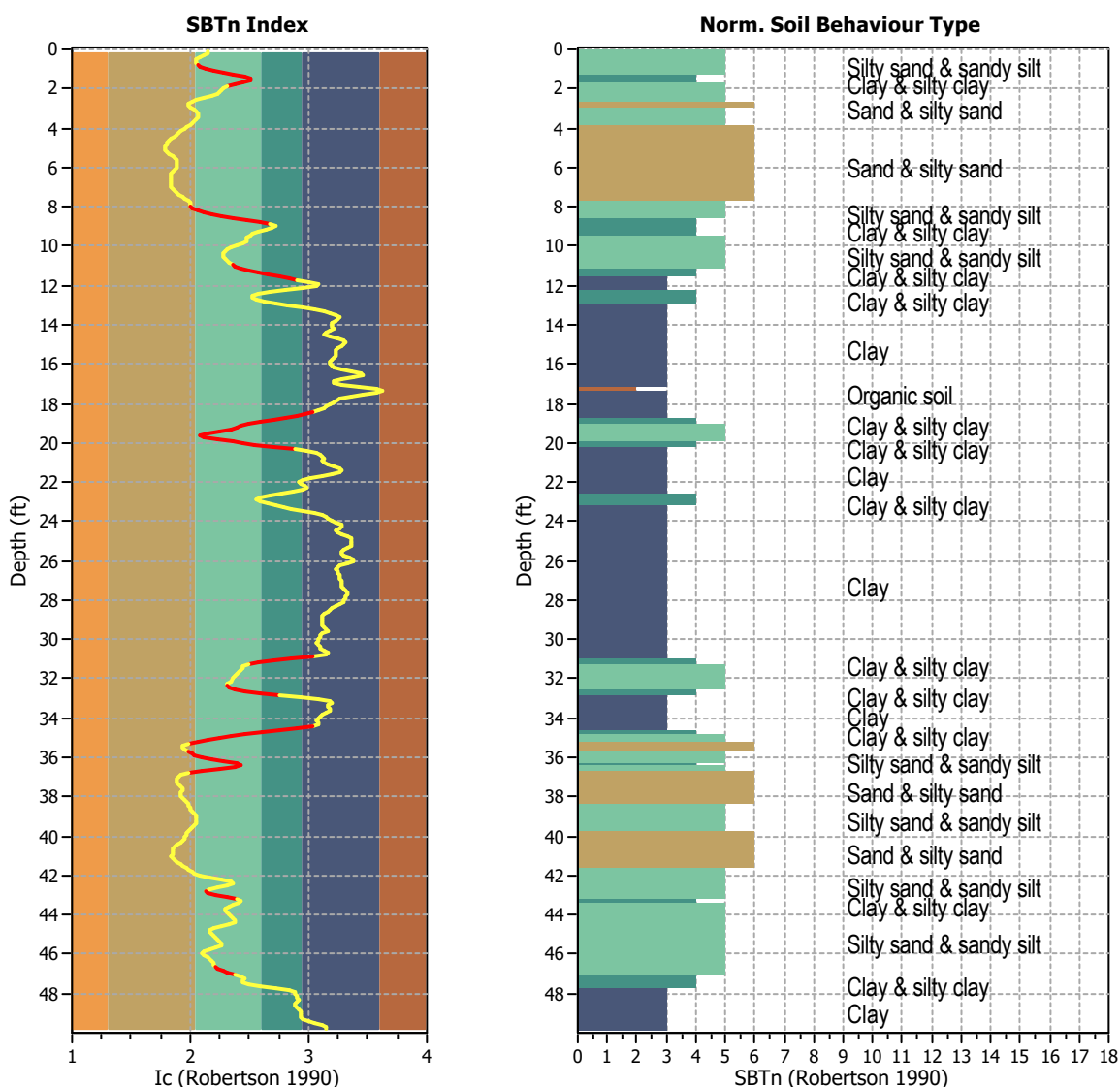
TRANSITION LAYER DETECTION ALGORITHM REPORT

Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vice-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between $1.80 < I_c < 3.0$) and a rate of change of I_c . Transitions typically occur when the rate of change of I_c is fast (i.e. ΔI_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties

I_c minimum check value: 1.70
 I_c maximum check value: 3.00
 I_c change ratio value: 0.0250
 Minimum number of points in layer: 4

General statistics

Total points in CPT file: 498
 Total points excluded: 96
 Exclusion percentage: 19.28%
 Number of layers detected: 13

Transition layer No	Number of points	Depth	SBT _n number	SBT _n description
Transition layer 1	7	Start depth: 0.90 (ft)	5	Silty sand & sandy silt
		End depth: 1.50 (ft)	4	Clay & silty clay
Transition layer 2	5	Start depth: 1.60 (ft)	4	Clay & silty clay
		End depth: 2.00 (ft)	5	Silty sand & sandy silt
Transition layer 3	10	Start depth: 8.10 (ft)	5	Silty sand & sandy silt
		End depth: 9.00 (ft)	4	Clay & silty clay
Transition layer 4	9	Start depth: 11.00 (ft)	5	Silty sand & sandy silt
		End depth: 11.80 (ft)	3	Clay
Transition layer 5	12	Start depth: 18.50 (ft)	3	Clay
		End depth: 19.60 (ft)	5	Silty sand & sandy silt
Transition layer 6	9	Start depth: 19.60 (ft)	5	Silty sand & sandy silt
		End depth: 20.40 (ft)	3	Clay
Transition layer 7	5	Start depth: 31.00 (ft)	3	Clay
		End depth: 31.40 (ft)	5	Silty sand & sandy silt
Transition layer 8	6	Start depth: 32.40 (ft)	5	Silty sand & sandy silt
		End depth: 32.90 (ft)	3	Clay
Transition layer 9	10	Start depth: 34.50 (ft)	3	Clay
		End depth: 35.40 (ft)	6	Sand & silty sand
Transition layer 10	7	Start depth: 35.80 (ft)	5	Silty sand & sandy silt
		End depth: 36.40 (ft)	4	Clay & silty clay
Transition layer 11	6	Start depth: 36.40 (ft)	4	Clay & silty clay
		End depth: 36.90 (ft)	6	Sand & silty sand
Transition layer 12	5	Start depth: 42.90 (ft)	5	Silty sand & sandy silt
		End depth: 43.30 (ft)	4	Clay & silty clay
Transition layer 13	5	Start depth: 46.70 (ft)	5	Silty sand & sandy silt
		End depth: 47.10 (ft)	4	Clay & silty clay

Start depth: Depth where the transition layer begins

End depth: Depth where the transition layer ends

:: Field input data ::						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1	0.10	41.00	0.56	0.56	17.22	115.03
2	0.20	39.03	0.56	0.56	17.14	115.52
3	0.30	44.69	0.66	0.66	16.45	116.49
4	0.40	51.96	0.75	0.75	15.23	117.89
5	0.50	58.56	0.87	0.87	14.40	119.18
6	0.60	63.15	1.00	1.00	14.18	120.28
7	0.70	65.24	1.10	1.10	14.32	120.99
8	0.80	65.22	1.14	1.14	14.62	121.22
9	0.90	62.85	1.10	1.10	15.26	121.10
10	1.00	58.21	1.09	1.09	16.55	120.82
11	1.10	51.50	1.09	1.09	18.69	120.59
12	1.20	45.48	1.11	1.11	21.61	120.37
13	1.30	39.28	1.13	1.13	25.06	120.04
14	1.40	32.97	1.11	1.11	28.67	119.64
15	1.50	29.52	1.09	1.09	31.11	119.30
16	1.60	29.90	1.09	1.09	30.84	119.21
17	1.70	33.28	1.06	1.06	28.45	119.20
18	1.80	36.76	1.00	1.00	25.54	119.15
19	1.90	40.00	0.97	0.97	23.20	119.08
20	2.00	42.42	0.96	0.96	21.85	119.22
21	2.10	44.01	1.00	1.00	21.24	119.53
22	2.20	45.36	1.06	1.06	20.81	119.97
23	2.30	48.11	1.10	1.10	19.89	120.37
24	2.40	52.55	1.11	1.11	18.25	120.73
25	2.50	58.94	1.12	1.12	16.28	121.17
26	2.60	67.10	1.17	1.17	14.51	121.73
27	2.70	74.58	1.25	1.25	13.30	122.43
28	2.80	80.32	1.35	1.35	12.67	123.14
29	2.90	84.27	1.46	1.46	12.57	123.77
30	3.00	85.07	1.54	1.54	12.96	124.22
31	3.10	82.32	1.62	1.62	13.67	124.38
32	3.20	77.74	1.59	1.59	14.49	124.26
33	3.30	73.68	1.54	1.54	15.01	124.03
34	3.40	73.39	1.53	1.53	15.01	123.98
35	3.50	77.07	1.57	1.57	14.63	124.16
36	3.60	80.36	1.61	1.61	14.11	124.45
37	3.70	83.50	1.65	1.65	13.57	124.78
38	3.80	88.60	1.71	1.71	12.93	125.19
39	3.90	95.36	1.80	1.80	12.20	125.67
40	4.00	102.34	1.88	1.88	11.59	126.28
41	4.10	109.71	2.04	2.04	11.01	127.21
42	4.20	124.22	2.38	2.38	10.49	128.23
43	4.30	135.70	2.59	2.59	9.97	129.05
44	4.40	141.94	2.66	2.66	9.48	129.55
45	4.50	149.87	2.75	2.75	9.04	129.94
46	4.60	158.76	2.89	2.89	8.64	130.43
47	4.70	168.42	3.07	3.07	8.31	130.97
48	4.80	177.89	3.24	3.24	8.02	131.50

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
49	4.90	186.95	3.41	3.41	7.85	131.97
50	5.00	191.99	3.56	3.56	7.82	132.37
51	5.10	194.46	3.71	3.71	7.96	132.69
52	5.20	194.11	3.84	3.84	8.28	132.93
53	5.30	189.61	3.94	3.94	8.72	133.01
54	5.40	181.39	3.92	3.92	9.21	132.89
55	5.50	173.21	3.80	3.80	9.61	132.59
56	5.60	165.67	3.63	3.63	9.88	132.22
57	5.70	160.44	3.52	3.52	10.09	131.83
58	5.80	154.26	3.37	3.37	10.21	131.41
59	5.90	148.77	3.16	3.16	10.14	131.02
60	6.00	150.43	3.07	3.07	9.91	130.73
61	6.10	151.75	3.01	3.01	9.60	130.58
62	6.20	152.44	2.95	2.95	9.34	130.45
63	6.30	153.63	2.89	2.89	9.08	130.34
64	6.40	155.75	2.86	2.86	8.88	130.26
65	6.50	155.56	2.83	2.83	8.79	130.19
66	6.60	154.18	2.81	2.81	8.80	130.13
67	6.70	153.47	2.79	2.79	8.85	130.07
68	6.80	153.11	2.79	2.79	8.89	130.09
69	6.90	154.71	2.82	2.82	8.93	130.15
70	7.00	155.67	2.86	2.86	9.05	130.27
71	7.10	154.21	2.91	2.91	9.26	130.32
72	7.20	151.43	2.90	2.90	9.55	130.23
73	7.30	145.74	2.82	2.82	9.93	129.97
74	7.40	136.94	2.71	2.71	10.43	129.52
75	7.50	127.06	2.56	2.56	11.09	128.98
76	7.60	117.34	2.42	2.42	11.74	128.39
77	7.70	109.86	2.30	2.30	12.39	127.66
78	7.80	99.48	2.04	2.04	12.82	126.82
79	7.90	94.17	1.84	1.84	12.87	126.06
80	8.00	95.88	1.78	1.78	13.02	125.22
81	8.10	83.51	1.52	1.52	13.52	124.26
82	8.20	72.14	1.34	1.34	14.72	123.19
83	8.30	66.13	1.32	1.32	16.31	122.51
84	8.40	58.66	1.30	1.30	18.36	122.13
85	8.50	50.47	1.29	1.29	21.20	121.71
86	8.60	42.14	1.28	1.28	25.08	121.00
87	8.70	33.04	1.17	1.17	29.69	119.90
88	8.80	26.06	1.01	1.01	34.80	118.14
89	8.90	19.45	0.78	0.78	39.19	116.46
90	9.00	17.86	0.74	0.74	41.32	115.80
91	9.10	20.55	0.87	0.87	40.18	116.25
92	9.20	22.68	0.88	0.88	37.06	116.73
93	9.30	24.95	0.81	0.81	34.34	116.11
94	9.40	23.48	0.63	0.63	32.07	114.81
95	9.50	22.40	0.51	0.51	30.69	113.31
96	9.60	22.33	0.47	0.47	29.87	112.62

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
97	9.70	22.78	0.49	0.49	29.61	112.72
98	9.80	23.33	0.52	0.52	29.49	113.34
99	9.90	24.87	0.58	0.58	28.20	114.36
100	10.00	30.30	0.67	0.67	26.00	115.37
101	10.10	34.75	0.69	0.69	23.92	116.13
102	10.20	36.53	0.71	0.71	22.73	116.41
103	10.30	37.03	0.70	0.70	22.24	116.40
104	10.40	37.03	0.68	0.68	21.90	116.19
105	10.50	37.03	0.64	0.64	21.61	115.93
106	10.60	37.03	0.63	0.63	21.66	115.88
107	10.70	36.64	0.66	0.66	22.37	116.08
108	10.80	35.22	0.71	0.71	23.48	116.46
109	10.90	34.64	0.76	0.76	24.62	116.81
110	11.00	34.13	0.78	0.78	25.76	116.92
111	11.10	31.68	0.77	0.77	27.53	116.63
112	11.20	27.08	0.73	0.73	30.35	116.02
113	11.30	22.93	0.69	0.69	34.19	115.06
114	11.40	18.70	0.62	0.62	38.53	113.88
115	11.50	15.21	0.54	0.54	43.21	112.39
116	11.60	12.41	0.46	0.46	47.85	110.92
117	11.70	10.81	0.41	0.41	52.54	109.34
118	11.80	8.80	0.34	0.34	58.42	107.54
119	11.90	6.37	0.26	0.26	63.87	106.67
120	12.00	7.32	0.34	0.34	63.08	108.20
121	12.10	10.88	0.52	0.52	54.74	111.06
122	12.20	15.19	0.64	0.64	45.91	113.18
123	12.30	19.58	0.65	0.65	39.01	114.02
124	12.40	22.65	0.59	0.59	34.35	114.02
125	12.50	23.71	0.55	0.55	31.69	114.28
126	12.60	26.46	0.65	0.65	31.51	115.05
127	12.70	26.27	0.76	0.76	33.16	115.83
128	12.80	23.03	0.78	0.78	36.57	115.79
129	12.90	19.04	0.71	0.71	41.35	114.89
130	13.00	14.99	0.62	0.62	47.44	113.37
131	13.10	11.10	0.52	0.52	54.87	111.67
132	13.20	8.80	0.46	0.46	62.41	110.39
133	13.30	8.36	0.46	0.46	67.36	109.50
134	13.40	7.62	0.41	0.41	71.21	108.55
135	13.50	6.21	0.34	0.34	75.05	107.44
136	13.60	5.97	0.33	0.33	77.77	106.45
137	13.70	5.97	0.30	0.30	77.12	105.89
138	13.80	5.97	0.28	0.28	75.24	105.19
139	13.90	5.97	0.24	0.24	73.16	104.39
140	14.00	5.97	0.22	0.22	72.36	103.48
141	14.10	5.53	0.19	0.19	72.96	102.86
142	14.20	5.38	0.20	0.20	73.75	103.13
143	14.30	5.99	0.24	0.24	71.91	104.72
144	14.40	7.34	0.32	0.32	68.79	106.59

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
145	14.50	8.17	0.38	0.38	68.26	107.49
146	14.60	7.17	0.35	0.35	71.34	107.42
147	14.70	6.16	0.33	0.33	77.10	107.05
148	14.80	5.97	0.36	0.36	81.34	107.01
149	14.90	5.97	0.36	0.36	82.13	106.98
150	15.00	5.97	0.33	0.33	80.88	106.53
151	15.10	5.97	0.30	0.30	78.94	105.83
152	15.20	5.97	0.27	0.27	77.19	105.19
153	15.30	5.97	0.26	0.26	75.89	104.68
154	15.40	5.97	0.24	0.24	75.01	104.32
155	15.50	5.97	0.24	0.24	74.91	104.23
156	15.60	5.97	0.25	0.25	75.38	104.65
157	15.70	6.20	0.28	0.28	74.12	106.09
158	15.80	7.60	0.38	0.38	72.35	107.91
159	15.90	8.36	0.46	0.46	71.19	109.42
160	16.00	8.36	0.49	0.49	71.61	110.16
161	16.10	8.36	0.50	0.50	72.34	110.35
162	16.20	8.35	0.50	0.50	74.55	109.70
163	16.30	6.77	0.40	0.40	78.96	108.19
164	16.40	5.33	0.30	0.30	86.39	105.76
165	16.50	4.39	0.22	0.22	93.21	103.48
166	16.60	3.98	0.19	0.19	94.87	102.52
167	16.70	4.57	0.22	0.22	88.21	103.62
168	16.80	6.23	0.30	0.30	79.31	105.19
169	16.90	7.17	0.31	0.31	73.45	105.95
170	17.00	6.97	0.27	0.27	73.43	105.30
171	17.10	5.70	0.23	0.23	79.77	103.71
172	17.20	4.17	0.19	0.19	92.59	101.63
173	17.30	3.16	0.15	0.15	100.00	99.76
174	17.40	2.99	0.14	0.14	100.00	99.09
175	17.50	3.58	0.15	0.15	100.00	99.40
176	17.60	3.81	0.16	0.16	94.74	101.22
177	17.70	5.21	0.23	0.23	85.66	103.64
178	17.80	6.62	0.31	0.31	77.56	106.45
179	17.90	8.03	0.41	0.41	73.55	108.28
180	18.00	8.36	0.44	0.44	71.22	109.50
181	18.10	8.97	0.48	0.48	69.42	110.57
182	18.20	10.23	0.57	0.57	67.42	111.77
183	18.30	11.10	0.65	0.65	64.67	113.15
184	18.40	12.80	0.75	0.75	61.23	114.40
185	18.50	14.92	0.84	0.84	56.69	115.60
186	18.60	17.52	0.92	0.92	51.67	116.65
187	18.70	20.81	0.99	0.99	46.19	117.62
188	18.80	25.48	1.05	1.05	40.47	118.49
189	18.90	31.13	1.08	1.08	34.94	119.31
190	19.00	37.95	1.13	1.13	30.53	120.13
191	19.10	44.31	1.22	1.22	27.80	120.97
192	19.20	47.84	1.33	1.33	26.03	121.84

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
193	19.30	53.35	1.45	1.45	23.96	122.73
194	19.40	63.92	1.55	1.55	20.58	123.67
195	19.50	81.62	1.63	1.63	17.02	124.43
196	19.60	96.87	1.63	1.63	15.35	124.67
197	19.70	87.68	1.56	1.56	16.45	124.04
198	19.80	59.40	1.36	1.36	20.23	123.82
199	19.90	57.64	1.76	1.76	24.67	124.33
200	20.00	60.92	2.13	2.13	27.85	124.36
201	20.10	41.31	1.57	1.57	32.42	122.48
202	20.20	21.92	0.90	0.90	40.77	118.75
203	20.30	16.55	0.73	0.73	50.92	114.99
204	20.40	12.77	0.59	0.59	57.49	112.91
205	20.50	10.96	0.49	0.49	62.48	110.93
206	20.60	9.60	0.39	0.39	65.47	109.02
207	20.70	8.36	0.31	0.31	66.79	107.41
208	20.80	8.36	0.29	0.29	67.25	106.46
209	20.90	8.36	0.28	0.28	66.82	106.25
210	21.00	8.36	0.28	0.28	67.28	105.97
211	21.10	7.90	0.26	0.26	69.64	105.19
212	21.20	6.67	0.22	0.22	73.52	104.00
213	21.30	5.97	0.19	0.19	77.33	102.94
214	21.40	5.97	0.19	0.19	79.15	102.89
215	21.50	6.18	0.22	0.22	78.04	104.47
216	21.60	7.51	0.32	0.32	73.34	107.58
217	21.70	10.48	0.50	0.50	66.09	111.00
218	21.80	13.95	0.69	0.69	59.39	113.65
219	21.90	16.71	0.80	0.80	54.99	115.15
220	22.00	17.85	0.82	0.82	53.44	115.68
221	22.10	16.99	0.81	0.81	54.43	115.72
222	22.20	15.85	0.82	0.82	56.64	115.80
223	22.30	15.91	0.88	0.88	57.36	116.28
224	22.40	17.59	0.97	0.97	54.99	117.16
225	22.50	20.78	1.07	1.07	50.01	118.16
226	22.60	25.38	1.13	1.13	44.22	118.86
227	22.70	29.79	1.10	1.10	39.00	118.90
228	22.80	31.89	0.94	0.94	35.22	118.27
229	22.90	31.90	0.81	0.81	33.64	117.48
230	23.00	30.29	0.80	0.80	34.67	117.16
231	23.10	27.68	0.87	0.87	37.74	117.40
232	23.20	25.65	0.95	0.95	41.54	117.83
233	23.30	24.19	1.03	1.03	45.20	117.99
234	23.40	21.70	1.01	1.01	49.37	117.62
235	23.50	17.86	0.91	0.91	55.09	116.61
236	23.60	14.04	0.81	0.81	61.96	115.56
237	23.70	12.62	0.80	0.80	66.78	115.03
238	23.80	13.13	0.83	0.83	68.62	114.45
239	23.90	11.74	0.66	0.66	69.72	113.21
240	24.00	9.83	0.49	0.49	72.13	111.12

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
241	24.10	8.69	0.40	0.40	75.61	109.05
242	24.20	7.60	0.34	0.34	79.05	107.74
243	24.30	7.17	0.33	0.33	79.90	107.61
244	24.40	8.30	0.39	0.39	78.21	108.32
245	24.50	8.96	0.42	0.42	75.93	109.00
246	24.60	8.83	0.41	0.41	76.27	108.72
247	24.70	7.90	0.35	0.35	79.48	107.45
248	24.80	6.48	0.27	0.27	83.74	105.69
249	24.90	5.97	0.23	0.23	86.64	104.12
250	25.00	5.97	0.21	0.21	86.93	103.45
251	25.10	5.97	0.21	0.21	86.87	103.52
252	25.20	6.07	0.23	0.23	85.79	104.49
253	25.30	6.96	0.29	0.29	82.95	106.10
254	25.40	8.07	0.36	0.36	80.16	107.60
255	25.50	8.36	0.40	0.40	78.94	108.51
256	25.60	8.36	0.41	0.41	79.33	108.87
257	25.70	8.36	0.42	0.42	81.12	108.76
258	25.80	7.64	0.39	0.39	84.92	108.19
259	25.90	6.57	0.34	0.34	88.29	107.85
260	26.00	7.10	0.39	0.39	87.60	108.56
261	26.10	8.52	0.49	0.49	82.76	110.23
262	26.20	9.92	0.59	0.59	78.38	111.71
263	26.30	10.72	0.64	0.64	76.22	112.56
264	26.40	10.75	0.65	0.65	75.81	112.95
265	26.50	10.75	0.67	0.67	76.39	113.13
266	26.60	10.75	0.69	0.69	76.96	113.28
267	26.70	10.75	0.69	0.69	77.43	113.40
268	26.80	10.75	0.71	0.71	77.87	113.51
269	26.90	10.75	0.72	0.72	78.34	113.63
270	27.00	10.75	0.73	0.73	78.72	113.72
271	27.10	10.75	0.73	0.73	78.96	113.76
272	27.20	10.75	0.73	0.73	78.97	113.73
273	27.30	10.75	0.72	0.72	79.11	113.47
274	27.40	10.34	0.66	0.66	80.31	112.71
275	27.50	9.14	0.55	0.55	82.35	111.53
276	27.60	8.37	0.48	0.48	83.87	110.32
277	27.70	8.36	0.44	0.44	83.66	109.51
278	27.80	8.36	0.41	0.41	82.58	109.11
279	27.90	8.36	0.40	0.40	81.56	109.08
280	28.00	8.73	0.43	0.43	80.78	109.33
281	28.10	8.96	0.45	0.45	80.20	109.62
282	28.20	8.96	0.45	0.45	78.19	110.13
283	28.30	10.19	0.50	0.50	75.68	110.64
284	28.40	10.75	0.52	0.52	73.32	111.08
285	28.50	10.75	0.51	0.51	71.78	111.35
286	28.60	11.41	0.54	0.54	69.63	111.88
287	28.70	12.82	0.60	0.60	67.47	112.50
288	28.80	13.14	0.61	0.61	66.22	112.97

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
289	28.90	13.14	0.63	0.63	66.40	113.17
290	29.00	13.14	0.65	0.65	66.89	113.32
291	29.10	13.14	0.65	0.65	67.04	113.35
292	29.20	13.14	0.63	0.63	66.65	113.18
293	29.30	13.14	0.60	0.60	66.69	112.61
294	29.40	12.13	0.53	0.53	67.81	111.61
295	29.50	10.78	0.44	0.44	69.23	110.59
296	29.60	10.75	0.43	0.43	69.68	110.09
297	29.70	11.19	0.45	0.45	67.13	110.77
298	29.80	13.31	0.54	0.54	65.39	111.59
299	29.90	13.24	0.56	0.56	65.02	112.18
300	30.00	12.54	0.56	0.56	64.49	112.74
301	30.10	14.78	0.65	0.65	63.60	113.22
302	30.20	14.87	0.66	0.66	62.95	113.48
303	30.30	13.62	0.61	0.61	64.02	113.15
304	30.40	13.36	0.58	0.58	64.78	112.81
305	30.50	13.74	0.59	0.59	65.43	112.63
306	30.60	12.87	0.57	0.57	67.66	112.39
307	30.70	11.48	0.56	0.56	70.78	112.45
308	30.80	11.97	0.63	0.63	69.07	113.82
309	30.90	16.42	0.87	0.87	60.16	116.40
310	31.00	24.61	1.16	1.16	49.49	118.96
311	31.10	34.03	1.33	1.33	40.54	120.56
312	31.20	42.25	1.30	1.30	33.92	121.16
313	31.30	48.23	1.21	1.21	29.98	121.31
314	31.40	50.71	1.25	1.25	28.34	121.58
315	31.50	52.01	1.35	1.35	28.01	121.91
316	31.60	52.84	1.35	1.35	27.52	122.05
317	31.70	54.50	1.29	1.29	26.67	121.96
318	31.80	55.90	1.27	1.27	26.01	121.95
319	31.90	56.61	1.31	1.31	25.56	122.07
320	32.00	58.40	1.33	1.33	24.90	122.10
321	32.10	60.32	1.25	1.25	23.98	121.89
322	32.20	60.43	1.18	1.18	23.15	121.66
323	32.30	61.77	1.19	1.19	22.86	121.81
324	32.40	63.95	1.30	1.30	23.38	122.28
325	32.50	61.78	1.41	1.41	25.33	122.67
326	32.60	53.36	1.47	1.47	29.14	122.64
327	32.70	42.96	1.46	1.46	35.28	121.86
328	32.80	30.42	1.27	1.27	43.68	120.29
329	32.90	20.70	1.01	1.01	53.99	118.10
330	33.00	15.91	0.83	0.83	63.92	115.74
331	33.10	12.76	0.65	0.65	70.90	113.58
332	33.20	10.96	0.51	0.51	73.06	111.97
333	33.30	11.90	0.49	0.49	70.70	111.22
334	33.40	12.96	0.49	0.49	69.83	110.54
335	33.50	10.44	0.39	0.39	71.50	109.77
336	33.60	9.90	0.38	0.38	71.52	110.16

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
337	33.70	13.56	0.55	0.55	69.27	111.22
338	33.80	13.40	0.55	0.55	66.83	112.05
339	33.90	12.94	0.52	0.52	65.28	112.50
340	34.00	15.53	0.63	0.63	63.96	113.05
341	34.10	15.53	0.65	0.65	62.95	113.87
342	34.20	15.53	0.69	0.69	64.12	114.29
343	34.30	15.53	0.74	0.74	64.60	115.20
344	34.40	17.23	0.90	0.90	60.48	117.84
345	34.50	26.55	1.48	1.48	51.94	121.12
346	34.60	39.58	1.98	1.98	43.12	123.40
347	34.70	48.83	1.89	1.89	35.29	124.53
348	34.80	61.25	1.85	1.85	29.06	125.32
349	34.90	77.74	2.17	2.17	24.41	126.73
350	35.00	98.31	2.60	2.60	20.63	128.28
351	35.10	122.27	2.81	2.81	17.39	129.35
352	35.20	142.08	2.82	2.82	14.63	129.77
353	35.30	156.41	2.66	2.66	12.57	129.84
354	35.40	169.29	2.61	2.61	11.41	129.99
355	35.50	175.83	2.79	2.79	11.21	130.26
356	35.60	170.89	2.90	2.90	11.74	130.46
357	35.70	161.21	2.88	2.88	12.47	130.40
358	35.80	155.63	2.83	2.83	13.18	130.01
359	35.90	143.20	2.61	2.61	14.07	129.47
360	36.00	128.06	2.48	2.48	15.67	128.92
361	36.10	112.58	2.52	2.52	18.34	128.51
362	36.20	93.81	2.54	2.54	22.01	128.14
363	36.30	77.77	2.51	2.51	25.97	127.82
364	36.40	71.60	2.59	2.59	27.81	128.10
365	36.50	83.66	2.94	2.94	25.42	129.19
366	36.60	113.82	3.37	3.37	20.52	130.63
367	36.70	152.43	3.61	3.61	15.82	131.70
368	36.80	187.23	3.55	3.55	12.62	132.37
369	36.90	210.72	3.66	3.66	10.92	132.91
370	37.00	225.38	3.98	3.98	10.26	133.65
371	37.10	241.24	4.39	4.39	10.08	134.23
372	37.20	243.91	4.44	4.44	10.06	134.46
373	37.30	237.09	4.32	4.32	10.22	134.26
374	37.40	226.32	4.12	4.12	10.54	133.81
375	37.50	212.54	3.87	3.87	10.91	133.25
376	37.60	200.47	3.61	3.61	11.19	132.60
377	37.70	192.31	3.33	3.33	11.18	131.97
378	37.80	190.02	3.10	3.10	10.92	131.56
379	37.90	194.57	3.10	3.10	10.71	131.64
380	38.00	202.44	3.38	3.38	10.79	132.26
381	38.10	210.31	3.83	3.83	11.17	133.16
382	38.20	216.96	4.31	4.31	11.68	134.07
383	38.30	222.19	4.78	4.78	12.13	134.79
384	38.40	225.73	5.05	5.05	12.42	135.27

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
385	38.50	228.35	5.18	5.18	12.62	135.59
386	38.60	229.78	5.39	5.39	12.81	135.76
387	38.70	227.47	5.42	5.42	13.08	135.81
388	38.80	221.38	5.33	5.33	13.42	135.71
389	38.90	214.86	5.29	5.29	13.78	135.52
390	39.00	208.71	5.16	5.16	14.12	135.30
391	39.10	202.88	5.02	5.02	14.30	135.05
392	39.20	199.95	4.88	4.88	14.30	134.82
393	39.30	199.94	4.76	4.76	14.09	134.65
394	39.40	202.72	4.68	4.68	13.75	134.61
395	39.50	208.73	4.74	4.74	13.32	134.71
396	39.60	217.25	4.83	4.83	12.87	134.97
397	39.70	227.80	5.00	5.00	12.46	135.39
398	39.80	241.02	5.36	5.36	12.16	135.96
399	39.90	254.53	5.78	5.78	11.96	136.60
400	40.00	267.01	6.16	6.16	11.85	137.18
401	40.10	276.08	6.52	6.52	11.69	137.28
402	40.20	286.98	6.73	6.73	11.34	137.28
403	40.30	297.29	6.61	6.61	10.77	137.28
404	40.40	306.47	6.42	6.42	10.12	137.28
405	40.50	313.76	6.26	6.26	9.59	137.28
406	40.60	319.57	6.19	6.19	9.30	137.28
407	40.70	324.16	6.36	6.36	9.22	137.28
408	40.80	327.41	6.50	6.50	9.19	137.28
409	40.90	327.89	6.37	6.37	9.12	137.28
410	41.00	325.27	6.23	6.23	9.08	137.28
411	41.10	320.12	6.14	6.14	9.24	137.28
412	41.20	312.89	6.19	6.19	9.60	137.28
413	41.30	305.10	6.32	6.32	10.14	137.28
414	41.40	295.58	6.45	6.45	10.76	137.28
415	41.50	279.85	6.31	6.31	11.42	137.28
416	41.60	259.50	5.93	5.93	12.08	136.80
417	41.70	237.21	5.42	5.42	12.68	135.95
418	41.80	216.87	4.83	4.83	13.19	135.03
419	41.90	202.63	4.43	4.43	13.92	134.19
420	42.00	182.14	4.20	4.20	15.34	133.55
421	42.10	157.40	4.15	4.15	17.85	133.01
422	42.20	131.87	4.09	4.09	21.06	132.27
423	42.30	108.58	3.65	3.65	23.91	131.21
424	42.40	96.91	3.12	3.12	24.63	130.16
425	42.50	104.19	2.92	2.92	22.72	129.54
426	42.60	117.86	2.77	2.77	19.82	129.22
427	42.70	126.64	2.51	2.51	17.66	128.84
428	42.80	127.25	2.33	2.33	16.83	128.45
429	42.90	122.61	2.34	2.34	17.51	128.26
430	43.00	112.59	2.42	2.42	19.63	128.38
431	43.10	100.42	2.64	2.64	22.75	128.65
432	43.20	91.07	2.87	2.87	25.88	128.92

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
433	43.30	86.64	2.97	2.97	27.47	129.03
434	43.40	88.66	2.89	2.89	26.92	128.97
435	43.50	95.01	2.76	2.76	25.15	128.77
436	43.60	99.48	2.60	2.60	23.47	128.56
437	43.70	101.90	2.54	2.54	22.61	128.44
438	43.80	102.15	2.57	2.57	22.57	128.50
439	43.90	101.13	2.64	2.64	22.96	128.70
440	44.00	101.44	2.76	2.76	23.52	128.98
441	44.10	101.53	2.89	2.89	24.20	129.35
442	44.20	100.88	3.08	3.08	25.04	129.80
443	44.30	101.07	3.31	3.31	25.60	130.34
444	44.40	105.84	3.56	3.56	25.19	130.82
445	44.50	114.38	3.60	3.60	23.43	131.03
446	44.60	125.14	3.36	3.36	21.00	130.85
447	44.70	133.34	3.05	3.05	18.93	130.50
448	44.80	136.80	2.95	2.95	17.89	130.30
449	44.90	137.37	3.02	3.02	17.87	130.45
450	45.00	137.80	3.21	3.21	18.29	130.81
451	45.10	138.89	3.39	3.39	18.74	131.12
452	45.20	137.86	3.43	3.43	19.20	131.27
453	45.30	134.20	3.44	3.44	19.88	131.28
454	45.40	128.98	3.49	3.49	20.73	131.24
455	45.50	124.75	3.49	3.49	21.28	131.19
456	45.60	125.46	3.43	3.43	20.92	131.05
457	45.70	131.26	3.28	3.28	19.62	130.76
458	45.80	137.15	2.99	2.99	17.90	130.28
459	45.90	141.54	2.70	2.70	16.40	129.72
460	46.00	143.88	2.54	2.54	15.77	129.41
461	46.10	141.25	2.62	2.62	16.14	129.51
462	46.20	137.40	2.83	2.83	17.18	129.88
463	46.30	134.84	3.01	3.01	18.18	130.20
464	46.40	132.71	3.07	3.07	18.73	130.33
465	46.50	131.99	3.03	3.03	19.03	130.46
466	46.60	133.65	3.19	3.19	19.44	130.84
467	46.70	135.55	3.53	3.53	20.21	131.43
468	46.80	134.44	3.82	3.82	21.45	131.94
469	46.90	128.23	4.01	4.01	23.19	132.07
470	47.00	114.82	3.93	3.93	25.35	131.89
471	47.10	104.67	3.86	3.86	27.57	131.34
472	47.20	94.36	3.54	3.54	28.61	130.88
473	47.30	97.16	3.45	3.45	28.21	130.61
474	47.40	103.73	3.47	3.47	28.21	130.33
475	47.50	89.80	3.20	3.20	30.20	129.72
476	47.60	71.11	2.93	2.93	35.19	128.31
477	47.70	51.94	2.39	2.39	41.72	126.51
478	47.80	40.84	1.95	1.95	47.70	124.59
479	47.90	36.45	1.71	1.71	50.92	123.14
480	48.00	34.41	1.55	1.55	51.49	122.40

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
481	48.10	35.44	1.53	1.53	51.65	122.39
482	48.20	36.19	1.71	1.71	52.29	123.32
483	48.30	38.22	2.13	2.13	52.94	124.99
484	48.40	44.04	2.74	2.74	52.16	126.60
485	48.50	49.23	3.06	3.06	50.93	127.37
486	48.60	47.66	2.81	2.81	50.58	127.15
487	48.70	43.48	2.49	2.49	51.65	126.17
488	48.80	39.06	2.20	2.20	53.10	125.19
489	48.90	37.33	2.04	2.04	53.87	124.49
490	49.00	37.43	1.98	1.98	53.93	124.06
491	49.10	36.47	1.89	1.89	53.95	123.74
492	49.20	35.54	1.82	1.82	54.37	123.35
493	49.30	34.39	1.74	1.74	55.43	122.76
494	49.40	31.21	1.56	1.56	57.95	121.65
495	49.50	25.43	1.25	1.25	61.87	120.04
496	49.60	21.54	1.03	1.03	66.07	118.32
497	49.70	19.93	0.92	0.92	68.60	117.09
498	49.80	19.14	0.85	0.85	69.49	116.50

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q _c :	Measured cone resistance (tsf)
f _s :	Sleeve friction resistance (tsf)
u:	Pore pressure (tsf)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (pcf)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1	0.10	0.01	0.00	0.01	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
2	0.20	0.01	0.00	0.01	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
3	0.30	0.02	0.00	0.02	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
4	0.40	0.02	0.00	0.02	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
5	0.50	0.03	0.00	0.03	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
6	0.60	0.04	0.00	0.04	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
7	0.70	0.04	0.00	0.04	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
8	0.80	0.05	0.00	0.05	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
9	0.90	0.05	0.00	0.05	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
10	1.00	0.06	0.00	0.06	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
11	1.10	0.07	0.00	0.07	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
12	1.20	0.07	0.00	0.07	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
13	1.30	0.08	0.00	0.08	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
14	1.40	0.08	0.00	0.08	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
15	1.50	0.09	0.00	0.09	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
16	1.60	0.10	0.00	0.10	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
17	1.70	0.10	0.00	0.10	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
18	1.80	0.11	0.00	0.11	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
19	1.90	0.11	0.00	0.11	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
20	2.00	0.12	0.00	0.12	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
21	2.10	0.13	0.00	0.13	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
22	2.20	0.13	0.00	0.13	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
23	2.30	0.14	0.00	0.14	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
24	2.40	0.14	0.00	0.14	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
25	2.50	0.15	0.00	0.15	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
26	2.60	0.16	0.00	0.16	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
27	2.70	0.16	0.00	0.16	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
28	2.80	0.17	0.00	0.17	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
29	2.90	0.17	0.00	0.17	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
30	3.00	0.18	0.00	0.18	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
31	3.10	0.19	0.00	0.19	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
32	3.20	0.19	0.00	0.19	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
33	3.30	0.20	0.00	0.20	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
34	3.40	0.20	0.00	0.20	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
35	3.50	0.21	0.00	0.21	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
36	3.60	0.22	0.00	0.22	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
37	3.70	0.22	0.00	0.22	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
38	3.80	0.23	0.00	0.23	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
39	3.90	0.24	0.00	0.24	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
40	4.00	0.24	0.00	0.24	1.00	0.479	1.04	0.460	1.10	1.30	2.000	No
41	4.10	0.25	0.00	0.25	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
42	4.20	0.26	0.00	0.26	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
43	4.30	0.26	0.00	0.26	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
44	4.40	0.27	0.00	0.27	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
45	4.50	0.27	0.00	0.27	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
46	4.60	0.28	0.00	0.28	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
47	4.70	0.29	0.00	0.29	0.99	0.479	1.04	0.459	1.10	1.30	2.000	No
48	4.80	0.29	0.00	0.29	0.99	0.478	1.04	0.459	1.10	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
49	4.90	0.30	0.00	0.30	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
50	5.00	0.31	0.00	0.31	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
51	5.10	0.31	0.00	0.31	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
52	5.20	0.32	0.00	0.32	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
53	5.30	0.33	0.00	0.33	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
54	5.40	0.33	0.00	0.33	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
55	5.50	0.34	0.00	0.34	0.99	0.477	1.04	0.458	1.10	1.30	2.000	No
56	5.60	0.35	0.00	0.35	0.99	0.477	1.04	0.458	1.10	1.30	2.000	No
57	5.70	0.35	0.00	0.35	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
58	5.80	0.36	0.00	0.36	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
59	5.90	0.37	0.00	0.37	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
60	6.00	0.37	0.00	0.37	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
61	6.10	0.38	0.00	0.38	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
62	6.20	0.39	0.00	0.39	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
63	6.30	0.39	0.00	0.39	0.99	0.476	1.04	0.457	1.10	1.30	2.000	No
64	6.40	0.40	0.00	0.40	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
65	6.50	0.41	0.00	0.41	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
66	6.60	0.41	0.00	0.41	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
67	6.70	0.42	0.00	0.42	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
68	6.80	0.43	0.00	0.43	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
69	6.90	0.43	0.00	0.43	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
70	7.00	0.44	0.00	0.44	0.99	0.475	1.04	0.456	1.10	1.30	2.000	No
71	7.10	0.45	0.00	0.45	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
72	7.20	0.45	0.00	0.45	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
73	7.30	0.46	0.00	0.46	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
74	7.40	0.46	0.00	0.46	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
75	7.50	0.47	0.00	0.47	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
76	7.60	0.48	0.00	0.48	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
77	7.70	0.48	0.00	0.48	0.99	0.474	1.04	0.455	1.10	1.30	2.000	No
78	7.80	0.49	0.00	0.49	0.99	0.474	1.04	0.455	1.10	1.30	2.000	No
79	7.90	0.50	0.00	0.50	0.99	0.474	1.04	0.454	1.10	1.30	2.000	No
80	8.00	0.50	0.00	0.50	0.99	0.474	1.04	0.454	1.10	1.30	2.000	No
81	8.10	0.51	0.00	0.51	0.98	0.477	1.04	0.457	1.10	1.30	2.000	Yes
82	8.20	0.52	0.01	0.51	0.98	0.479	1.04	0.460	1.10	1.30	2.000	Yes
83	8.30	0.52	0.01	0.51	0.98	0.482	1.04	0.462	1.10	1.30	2.000	Yes
84	8.40	0.53	0.01	0.51	0.98	0.485	1.04	0.465	1.10	1.30	2.000	Yes
85	8.50	0.53	0.02	0.52	0.98	0.487	1.04	0.467	1.09	1.30	2.000	Yes
86	8.60	0.54	0.02	0.52	0.98	0.490	1.04	0.470	1.09	1.30	2.000	Yes
87	8.70	0.55	0.02	0.52	0.98	0.493	1.04	0.472	1.08	1.30	2.000	Yes
88	8.80	0.55	0.02	0.53	0.98	0.495	1.04	0.475	1.07	1.30	2.000	Yes
89	8.90	0.56	0.03	0.53	0.98	0.498	1.04	0.477	1.07	1.30	2.000	Yes
90	9.00	0.56	0.03	0.53	0.98	0.500	1.04	0.479	1.06	1.30	2.000	Yes
91	9.10	0.57	0.03	0.53	0.98	0.503	1.04	0.482	1.07	1.30	0.606	No
92	9.20	0.57	0.04	0.54	0.98	0.505	1.04	0.484	1.07	1.30	0.608	No
93	9.30	0.58	0.04	0.54	0.98	0.507	1.04	0.486	1.07	1.30	0.610	No
94	9.40	0.59	0.04	0.54	0.98	0.510	1.04	0.489	1.07	1.30	0.615	No
95	9.50	0.59	0.05	0.55	0.98	0.512	1.04	0.491	1.06	1.30	0.619	No
96	9.60	0.60	0.05	0.55	0.98	0.514	1.04	0.493	1.06	1.30	0.622	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
97	9.70	0.60	0.05	0.55	0.98	0.517	1.04	0.495	1.06	1.30	0.625	No
98	9.80	0.61	0.06	0.55	0.98	0.519	1.04	0.498	1.06	1.30	0.628	No
99	9.90	0.61	0.06	0.56	0.98	0.521	1.04	0.500	1.06	1.30	0.630	No
100	10.00	0.62	0.06	0.56	0.98	0.524	1.04	0.502	1.07	1.30	0.630	No
101	10.10	0.63	0.07	0.56	0.98	0.526	1.04	0.504	1.07	1.30	0.630	No
102	10.20	0.63	0.07	0.56	0.98	0.528	1.04	0.506	1.07	1.30	0.632	No
103	10.30	0.64	0.07	0.57	0.98	0.530	1.04	0.508	1.07	1.30	0.635	No
104	10.40	0.64	0.07	0.57	0.98	0.532	1.04	0.510	1.07	1.30	0.638	No
105	10.50	0.65	0.08	0.57	0.98	0.534	1.04	0.512	1.07	1.30	0.641	No
106	10.60	0.66	0.08	0.57	0.98	0.536	1.04	0.514	1.07	1.30	0.644	No
107	10.70	0.66	0.08	0.58	0.98	0.538	1.04	0.516	1.07	1.30	0.647	No
108	10.80	0.67	0.09	0.58	0.98	0.540	1.04	0.518	1.07	1.30	0.650	No
109	10.90	0.67	0.09	0.58	0.98	0.542	1.04	0.520	1.06	1.30	0.653	No
110	11.00	0.68	0.09	0.58	0.98	0.544	1.04	0.522	1.06	1.30	2.000	Yes
111	11.10	0.68	0.10	0.59	0.98	0.546	1.04	0.524	1.06	1.30	2.000	Yes
112	11.20	0.69	0.10	0.59	0.97	0.548	1.04	0.525	1.06	1.30	2.000	Yes
113	11.30	0.70	0.10	0.59	0.97	0.550	1.04	0.527	1.06	1.30	2.000	Yes
114	11.40	0.70	0.11	0.60	0.97	0.552	1.04	0.529	1.05	1.30	2.000	Yes
115	11.50	0.71	0.11	0.60	0.97	0.554	1.04	0.531	1.05	1.30	2.000	Yes
116	11.60	0.71	0.11	0.60	0.97	0.556	1.04	0.533	1.05	1.30	2.000	Yes
117	11.70	0.72	0.12	0.60	0.97	0.558	1.04	0.535	1.05	1.30	2.000	Yes
118	11.80	0.72	0.12	0.61	0.97	0.560	1.04	0.536	1.05	1.30	2.000	Yes
119	11.90	0.73	0.12	0.61	0.97	0.562	1.04	0.538	1.04	1.30	0.694	No
120	12.00	0.73	0.12	0.61	0.97	0.563	1.04	0.540	1.04	1.30	0.696	No
121	12.10	0.74	0.13	0.61	0.97	0.565	1.04	0.542	1.05	1.30	0.696	No
122	12.20	0.75	0.13	0.61	0.97	0.567	1.04	0.543	1.05	1.30	0.696	No
123	12.30	0.75	0.13	0.62	0.97	0.569	1.04	0.545	1.05	1.30	0.697	No
124	12.40	0.76	0.14	0.62	0.97	0.570	1.04	0.547	1.05	1.30	0.698	No
125	12.50	0.76	0.14	0.62	0.97	0.572	1.04	0.548	1.05	1.30	0.700	No
126	12.60	0.77	0.14	0.62	0.97	0.574	1.04	0.550	1.05	1.30	0.700	No
127	12.70	0.77	0.15	0.63	0.97	0.575	1.04	0.552	1.05	1.30	0.702	No
128	12.80	0.78	0.15	0.63	0.97	0.577	1.04	0.553	1.05	1.30	0.706	No
129	12.90	0.79	0.15	0.63	0.97	0.579	1.04	0.555	1.05	1.30	0.711	No
130	13.00	0.79	0.16	0.64	0.97	0.580	1.04	0.556	1.05	1.30	0.715	No
131	13.10	0.80	0.16	0.64	0.97	0.582	1.04	0.558	1.04	1.30	0.719	No
132	13.20	0.80	0.16	0.64	0.97	0.584	1.04	0.559	1.04	1.30	0.723	No
133	13.30	0.81	0.17	0.64	0.97	0.585	1.04	0.561	1.04	1.30	0.725	No
134	13.40	0.81	0.17	0.64	0.97	0.587	1.04	0.562	1.04	1.30	0.728	No
135	13.50	0.82	0.17	0.65	0.97	0.588	1.04	0.564	1.04	1.30	0.731	No
136	13.60	0.82	0.17	0.65	0.97	0.590	1.04	0.566	1.04	1.30	0.733	No
137	13.70	0.83	0.18	0.65	0.97	0.592	1.04	0.567	1.04	1.30	0.735	No
138	13.80	0.83	0.18	0.65	0.97	0.593	1.04	0.569	1.04	1.30	0.737	No
139	13.90	0.84	0.18	0.66	0.97	0.595	1.04	0.570	1.04	1.30	0.739	No
140	14.00	0.85	0.19	0.66	0.97	0.596	1.04	0.572	1.04	1.30	0.742	No
141	14.10	0.85	0.19	0.66	0.96	0.598	1.04	0.573	1.04	1.30	0.744	No
142	14.20	0.86	0.19	0.66	0.96	0.599	1.04	0.575	1.04	1.30	0.746	No
143	14.30	0.86	0.20	0.66	0.96	0.601	1.04	0.576	1.04	1.30	0.748	No
144	14.40	0.87	0.20	0.67	0.96	0.602	1.04	0.577	1.04	1.30	0.749	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
145	14.50	0.87	0.20	0.67	0.96	0.604	1.04	0.579	1.04	1.30	0.751	No
146	14.60	0.88	0.21	0.67	0.96	0.605	1.04	0.580	1.04	1.30	0.753	No
147	14.70	0.88	0.21	0.67	0.96	0.607	1.04	0.582	1.04	1.30	0.756	No
148	14.80	0.89	0.21	0.68	0.96	0.608	1.04	0.583	1.04	1.30	0.758	No
149	14.90	0.89	0.22	0.68	0.96	0.610	1.04	0.584	1.04	1.30	0.760	No
150	15.00	0.90	0.22	0.68	0.96	0.611	1.04	0.586	1.04	1.30	0.762	No
151	15.10	0.90	0.22	0.68	0.96	0.612	1.04	0.587	1.04	1.30	0.764	No
152	15.20	0.91	0.22	0.68	0.96	0.614	1.04	0.588	1.03	1.30	0.766	No
153	15.30	0.91	0.23	0.69	0.96	0.615	1.04	0.590	1.03	1.30	0.768	No
154	15.40	0.92	0.23	0.69	0.96	0.617	1.04	0.591	1.03	1.30	0.770	No
155	15.50	0.92	0.23	0.69	0.96	0.618	1.04	0.592	1.03	1.30	0.771	No
156	15.60	0.93	0.24	0.69	0.96	0.619	1.04	0.594	1.03	1.30	0.773	No
157	15.70	0.93	0.24	0.69	0.96	0.621	1.04	0.595	1.03	1.30	0.775	No
158	15.80	0.94	0.24	0.70	0.96	0.622	1.04	0.596	1.03	1.30	0.776	No
159	15.90	0.95	0.25	0.70	0.96	0.623	1.04	0.597	1.03	1.30	0.778	No
160	16.00	0.95	0.25	0.70	0.96	0.625	1.04	0.599	1.03	1.30	0.780	No
161	16.10	0.96	0.25	0.70	0.96	0.626	1.04	0.600	1.03	1.30	0.781	No
162	16.20	0.96	0.26	0.71	0.96	0.627	1.04	0.601	1.03	1.30	0.783	No
163	16.30	0.97	0.26	0.71	0.96	0.628	1.04	0.602	1.03	1.30	0.786	No
164	16.40	0.97	0.26	0.71	0.96	0.630	1.04	0.603	1.03	1.30	0.788	No
165	16.50	0.98	0.27	0.71	0.96	0.631	1.04	0.605	1.03	1.30	0.790	No
166	16.60	0.98	0.27	0.71	0.96	0.632	1.04	0.606	1.03	1.30	0.792	No
167	16.70	0.99	0.27	0.72	0.96	0.633	1.04	0.607	1.03	1.30	0.794	No
168	16.80	0.99	0.27	0.72	0.95	0.635	1.04	0.608	1.03	1.30	0.795	No
169	16.90	1.00	0.28	0.72	0.95	0.636	1.04	0.609	1.03	1.30	0.796	No
170	17.00	1.00	0.28	0.72	0.95	0.637	1.04	0.610	1.03	1.30	0.798	No
171	17.10	1.01	0.28	0.73	0.95	0.638	1.04	0.612	1.03	1.30	0.800	No
172	17.20	1.01	0.29	0.73	0.95	0.639	1.04	0.613	1.03	1.30	0.802	No
173	17.30	1.02	0.29	0.73	0.95	0.641	1.04	0.614	1.03	1.30	0.804	No
174	17.40	1.02	0.29	0.73	0.95	0.642	1.04	0.615	1.03	1.30	0.806	No
175	17.50	1.03	0.30	0.73	0.95	0.643	1.04	0.616	1.03	1.30	0.808	No
176	17.60	1.03	0.30	0.73	0.95	0.644	1.04	0.618	1.03	1.30	0.809	No
177	17.70	1.04	0.30	0.74	0.95	0.645	1.04	0.619	1.03	1.30	0.810	No
178	17.80	1.04	0.31	0.74	0.95	0.647	1.04	0.620	1.03	1.30	0.811	No
179	17.90	1.05	0.31	0.74	0.95	0.648	1.04	0.621	1.03	1.30	0.812	No
180	18.00	1.06	0.31	0.74	0.95	0.649	1.04	0.622	1.03	1.30	0.813	No
181	18.10	1.06	0.32	0.75	0.95	0.650	1.04	0.623	1.03	1.30	0.815	No
182	18.20	1.07	0.32	0.75	0.95	0.651	1.04	0.624	1.03	1.30	0.816	No
183	18.30	1.07	0.32	0.75	0.95	0.652	1.04	0.625	1.03	1.30	0.817	No
184	18.40	1.08	0.32	0.75	0.95	0.653	1.04	0.625	1.03	1.30	0.817	No
185	18.50	1.08	0.33	0.76	0.95	0.653	1.04	0.626	1.03	1.30	2.000	Yes
186	18.60	1.09	0.33	0.76	0.95	0.654	1.04	0.627	1.03	1.30	2.000	Yes
187	18.70	1.10	0.33	0.76	0.95	0.655	1.04	0.628	1.03	1.30	2.000	Yes
188	18.80	1.10	0.34	0.76	0.95	0.656	1.04	0.629	1.03	1.30	2.000	Yes
189	18.90	1.11	0.34	0.77	0.95	0.657	1.04	0.630	1.03	1.30	2.000	Yes
190	19.00	1.11	0.34	0.77	0.95	0.658	1.04	0.630	1.03	1.30	2.000	Yes
191	19.10	1.12	0.35	0.77	0.95	0.659	1.04	0.631	1.04	1.30	2.000	Yes
192	19.20	1.13	0.35	0.78	0.95	0.659	1.04	0.632	1.04	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
193	19.30	1.13	0.35	0.78	0.94	0.660	1.04	0.633	1.04	1.30	2.000	Yes
194	19.40	1.14	0.36	0.78	0.94	0.661	1.04	0.633	1.04	1.30	2.000	Yes
195	19.50	1.14	0.36	0.79	0.94	0.661	1.04	0.634	1.05	1.30	2.000	Yes
196	19.60	1.15	0.36	0.79	0.94	0.662	1.04	0.635	1.05	1.30	2.000	Yes
197	19.70	1.16	0.37	0.79	0.94	0.663	1.04	0.635	1.05	1.30	2.000	Yes
198	19.80	1.16	0.37	0.79	0.94	0.664	1.04	0.636	1.04	1.30	2.000	Yes
199	19.90	1.17	0.37	0.80	0.94	0.664	1.04	0.637	1.04	1.30	2.000	Yes
200	20.00	1.18	0.37	0.80	0.94	0.665	1.04	0.637	1.04	1.30	2.000	Yes
201	20.10	1.18	0.38	0.80	0.94	0.666	1.04	0.638	1.03	1.30	2.000	Yes
202	20.20	1.19	0.38	0.81	0.94	0.666	1.04	0.639	1.03	1.30	2.000	Yes
203	20.30	1.19	0.38	0.81	0.94	0.667	1.04	0.639	1.02	1.30	2.000	Yes
204	20.40	1.20	0.39	0.81	0.94	0.668	1.04	0.640	1.02	1.30	2.000	Yes
205	20.50	1.20	0.39	0.81	0.94	0.669	1.04	0.641	1.02	1.30	0.844	No
206	20.60	1.21	0.39	0.82	0.94	0.669	1.04	0.642	1.02	1.30	0.846	No
207	20.70	1.22	0.40	0.82	0.94	0.670	1.04	0.642	1.02	1.30	0.847	No
208	20.80	1.22	0.40	0.82	0.94	0.671	1.04	0.643	1.02	1.30	0.848	No
209	20.90	1.23	0.40	0.82	0.94	0.672	1.04	0.644	1.02	1.30	0.850	No
210	21.00	1.23	0.41	0.83	0.94	0.673	1.04	0.645	1.02	1.30	0.851	No
211	21.10	1.24	0.41	0.83	0.94	0.674	1.04	0.646	1.02	1.30	0.852	No
212	21.20	1.24	0.41	0.83	0.94	0.674	1.04	0.646	1.02	1.30	0.854	No
213	21.30	1.25	0.41	0.83	0.94	0.675	1.04	0.647	1.02	1.30	0.855	No
214	21.40	1.25	0.42	0.83	0.94	0.676	1.04	0.648	1.02	1.30	0.857	No
215	21.50	1.26	0.42	0.84	0.94	0.677	1.04	0.649	1.02	1.30	0.858	No
216	21.60	1.26	0.42	0.84	0.94	0.678	1.04	0.650	1.02	1.30	0.858	No
217	21.70	1.27	0.43	0.84	0.93	0.678	1.04	0.650	1.02	1.30	0.859	No
218	21.80	1.27	0.43	0.84	0.93	0.679	1.04	0.651	1.02	1.30	0.858	No
219	21.90	1.28	0.43	0.85	0.93	0.680	1.04	0.651	1.02	1.30	0.859	No
220	22.00	1.29	0.44	0.85	0.93	0.680	1.04	0.652	1.02	1.30	0.859	No
221	22.10	1.29	0.44	0.85	0.93	0.681	1.04	0.653	1.02	1.30	0.860	No
222	22.20	1.30	0.44	0.85	0.93	0.682	1.04	0.653	1.02	1.30	0.862	No
223	22.30	1.30	0.45	0.86	0.93	0.682	1.04	0.654	1.02	1.30	0.863	No
224	22.40	1.31	0.45	0.86	0.93	0.683	1.04	0.654	1.02	1.30	0.863	No
225	22.50	1.31	0.45	0.86	0.93	0.683	1.04	0.655	1.02	1.30	0.863	No
226	22.60	1.32	0.46	0.86	0.93	0.684	1.04	0.655	1.02	1.30	0.863	No
227	22.70	1.33	0.46	0.87	0.93	0.684	1.04	0.656	1.02	1.30	0.862	No
228	22.80	1.33	0.46	0.87	0.93	0.685	1.04	0.656	1.02	1.30	0.862	No
229	22.90	1.34	0.46	0.87	0.93	0.685	1.04	0.657	1.02	1.30	0.863	No
230	23.00	1.34	0.47	0.88	0.93	0.686	1.04	0.657	1.02	1.30	0.865	No
231	23.10	1.35	0.47	0.88	0.93	0.686	1.04	0.658	1.02	1.30	0.867	No
232	23.20	1.36	0.47	0.88	0.93	0.687	1.04	0.658	1.02	1.30	0.868	No
233	23.30	1.36	0.48	0.88	0.93	0.687	1.04	0.659	1.02	1.30	0.869	No
234	23.40	1.37	0.48	0.89	0.93	0.688	1.04	0.659	1.02	1.30	0.871	No
235	23.50	1.37	0.48	0.89	0.93	0.688	1.04	0.660	1.02	1.30	0.873	No
236	23.60	1.38	0.49	0.89	0.93	0.689	1.04	0.660	1.01	1.30	0.875	No
237	23.70	1.38	0.49	0.90	0.93	0.690	1.04	0.661	1.01	1.30	0.877	No
238	23.80	1.39	0.49	0.90	0.93	0.690	1.04	0.661	1.01	1.30	0.877	No
239	23.90	1.40	0.50	0.90	0.93	0.691	1.04	0.662	1.01	1.30	0.879	No
240	24.00	1.40	0.50	0.90	0.93	0.691	1.04	0.662	1.01	1.30	0.880	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
241	24.10	1.41	0.50	0.91	0.92	0.692	1.04	0.663	1.01	1.30	0.881	No
242	24.20	1.41	0.51	0.91	0.92	0.692	1.04	0.664	1.01	1.30	0.883	No
243	24.30	1.42	0.51	0.91	0.92	0.693	1.04	0.664	1.01	1.30	0.884	No
244	24.40	1.42	0.51	0.91	0.92	0.693	1.04	0.665	1.01	1.30	0.884	No
245	24.50	1.43	0.51	0.91	0.92	0.694	1.04	0.665	1.01	1.30	0.885	No
246	24.60	1.43	0.52	0.92	0.92	0.695	1.04	0.666	1.01	1.30	0.886	No
247	24.70	1.44	0.52	0.92	0.92	0.695	1.04	0.666	1.01	1.30	0.887	No
248	24.80	1.45	0.52	0.92	0.92	0.696	1.04	0.667	1.01	1.30	0.888	No
249	24.90	1.45	0.53	0.92	0.92	0.696	1.04	0.667	1.01	1.30	0.889	No
250	25.00	1.46	0.53	0.93	0.92	0.697	1.04	0.668	1.01	1.30	0.890	No
251	25.10	1.46	0.53	0.93	0.92	0.697	1.04	0.669	1.01	1.30	0.891	No
252	25.20	1.47	0.54	0.93	0.92	0.698	1.04	0.669	1.01	1.30	0.892	No
253	25.30	1.47	0.54	0.93	0.92	0.699	1.04	0.670	1.01	1.30	0.893	No
254	25.40	1.48	0.54	0.93	0.92	0.699	1.04	0.670	1.01	1.30	0.893	No
255	25.50	1.48	0.55	0.94	0.92	0.700	1.04	0.671	1.01	1.30	0.894	No
256	25.60	1.49	0.55	0.94	0.92	0.700	1.04	0.671	1.01	1.30	0.895	No
257	25.70	1.49	0.55	0.94	0.92	0.701	1.04	0.672	1.01	1.30	0.896	No
258	25.80	1.50	0.56	0.94	0.92	0.701	1.04	0.672	1.01	1.30	0.897	No
259	25.90	1.50	0.56	0.95	0.92	0.702	1.04	0.672	1.01	1.30	0.898	No
260	26.00	1.51	0.56	0.95	0.92	0.702	1.04	0.673	1.01	1.30	0.898	No
261	26.10	1.51	0.56	0.95	0.92	0.703	1.04	0.673	1.01	1.30	0.899	No
262	26.20	1.52	0.57	0.95	0.92	0.703	1.04	0.674	1.01	1.30	0.899	No
263	26.30	1.53	0.57	0.95	0.92	0.703	1.04	0.674	1.01	1.30	0.900	No
264	26.40	1.53	0.57	0.96	0.91	0.704	1.04	0.675	1.01	1.30	0.900	No
265	26.50	1.54	0.58	0.96	0.91	0.704	1.04	0.675	1.01	1.30	0.901	No
266	26.60	1.54	0.58	0.96	0.91	0.705	1.04	0.675	1.01	1.30	0.902	No
267	26.70	1.55	0.58	0.96	0.91	0.705	1.04	0.676	1.01	1.30	0.902	No
268	26.80	1.55	0.59	0.97	0.91	0.705	1.04	0.676	1.01	1.30	0.903	No
269	26.90	1.56	0.59	0.97	0.91	0.706	1.04	0.676	1.01	1.30	0.904	No
270	27.00	1.57	0.59	0.97	0.91	0.706	1.04	0.677	1.01	1.30	0.904	No
271	27.10	1.57	0.60	0.98	0.91	0.706	1.04	0.677	1.01	1.30	0.905	No
272	27.20	1.58	0.60	0.98	0.91	0.707	1.04	0.677	1.01	1.30	0.906	No
273	27.30	1.58	0.60	0.98	0.91	0.707	1.04	0.678	1.01	1.30	0.906	No
274	27.40	1.59	0.61	0.98	0.91	0.707	1.04	0.678	1.01	1.30	0.907	No
275	27.50	1.59	0.61	0.99	0.91	0.708	1.04	0.678	1.01	1.30	0.908	No
276	27.60	1.60	0.61	0.99	0.91	0.708	1.04	0.679	1.01	1.30	0.909	No
277	27.70	1.60	0.61	0.99	0.91	0.709	1.04	0.679	1.01	1.30	0.909	No
278	27.80	1.61	0.62	0.99	0.91	0.709	1.04	0.679	1.01	1.30	0.910	No
279	27.90	1.62	0.62	0.99	0.91	0.709	1.04	0.680	1.00	1.30	0.911	No
280	28.00	1.62	0.62	1.00	0.91	0.710	1.04	0.680	1.00	1.30	0.911	No
281	28.10	1.63	0.63	1.00	0.91	0.710	1.04	0.681	1.00	1.30	0.912	No
282	28.20	1.63	0.63	1.00	0.91	0.710	1.04	0.681	1.00	1.30	0.913	No
283	28.30	1.64	0.63	1.00	0.91	0.711	1.04	0.681	1.00	1.30	0.913	No
284	28.40	1.64	0.64	1.01	0.91	0.711	1.04	0.682	1.00	1.30	0.914	No
285	28.50	1.65	0.64	1.01	0.91	0.711	1.04	0.682	1.00	1.30	0.914	No
286	28.60	1.65	0.64	1.01	0.90	0.712	1.04	0.682	1.00	1.30	0.915	No
287	28.70	1.66	0.65	1.01	0.90	0.712	1.04	0.682	1.00	1.30	0.915	No
288	28.80	1.67	0.65	1.02	0.90	0.712	1.04	0.683	1.00	1.30	0.915	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
289	28.90	1.67	0.65	1.02	0.90	0.713	1.04	0.683	1.00	1.30	0.916	No
290	29.00	1.68	0.66	1.02	0.90	0.713	1.04	0.683	1.00	1.30	0.916	No
291	29.10	1.68	0.66	1.02	0.90	0.713	1.04	0.683	1.00	1.30	0.917	No
292	29.20	1.69	0.66	1.03	0.90	0.713	1.04	0.684	1.00	1.30	0.918	No
293	29.30	1.69	0.66	1.03	0.90	0.714	1.04	0.684	1.00	1.30	0.918	No
294	29.40	1.70	0.67	1.03	0.90	0.714	1.04	0.684	1.00	1.30	0.919	No
295	29.50	1.71	0.67	1.03	0.90	0.714	1.04	0.685	1.00	1.30	0.920	No
296	29.60	1.71	0.67	1.04	0.90	0.714	1.04	0.685	1.00	1.30	0.920	No
297	29.70	1.72	0.68	1.04	0.90	0.715	1.04	0.685	1.00	1.30	0.921	No
298	29.80	1.72	0.68	1.04	0.90	0.715	1.04	0.685	1.00	1.30	0.921	No
299	29.90	1.73	0.68	1.04	0.90	0.715	1.04	0.686	1.00	1.30	0.921	No
300	30.00	1.73	0.69	1.05	0.90	0.716	1.04	0.686	1.00	1.30	0.922	No
301	30.10	1.74	0.69	1.05	0.90	0.716	1.04	0.686	1.00	1.30	0.922	No
302	30.20	1.74	0.69	1.05	0.90	0.716	1.04	0.686	1.00	1.30	0.923	No
303	30.30	1.75	0.70	1.05	0.90	0.716	1.04	0.686	1.00	1.30	0.923	No
304	30.40	1.76	0.70	1.06	0.90	0.716	1.04	0.687	1.00	1.30	0.924	No
305	30.50	1.76	0.70	1.06	0.90	0.717	1.04	0.687	1.00	1.30	0.924	No
306	30.60	1.77	0.71	1.06	0.90	0.717	1.04	0.687	1.00	1.30	0.925	No
307	30.70	1.77	0.71	1.06	0.90	0.717	1.04	0.687	1.00	1.30	0.925	No
308	30.80	1.78	0.71	1.07	0.89	0.717	1.04	0.687	1.00	1.30	0.926	No
309	30.90	1.78	0.71	1.07	0.89	0.717	1.04	0.688	1.00	1.30	0.926	No
310	31.00	1.79	0.72	1.07	0.89	0.718	1.04	0.688	1.00	1.30	2.000	Yes
311	31.10	1.80	0.72	1.08	0.89	0.718	1.04	0.688	1.00	1.30	2.000	Yes
312	31.20	1.80	0.72	1.08	0.89	0.718	1.04	0.688	1.00	1.30	2.000	Yes
313	31.30	1.81	0.73	1.08	0.89	0.718	1.04	0.688	1.00	1.30	2.000	Yes
314	31.40	1.81	0.73	1.08	0.89	0.718	1.04	0.688	1.00	1.30	2.000	Yes
315	31.50	1.82	0.73	1.09	0.89	0.718	1.04	0.688	1.00	1.30	0.920	No
316	31.60	1.83	0.74	1.09	0.89	0.718	1.04	0.688	1.00	1.30	0.921	No
317	31.70	1.83	0.74	1.09	0.89	0.718	1.04	0.688	1.00	1.30	0.921	No
318	31.80	1.84	0.74	1.10	0.89	0.718	1.04	0.688	1.00	1.30	0.921	No
319	31.90	1.84	0.75	1.10	0.89	0.718	1.04	0.688	1.00	1.30	0.921	No
320	32.00	1.85	0.75	1.10	0.89	0.718	1.04	0.688	1.00	1.30	0.921	No
321	32.10	1.86	0.75	1.10	0.89	0.718	1.04	0.688	0.99	1.30	0.921	No
322	32.20	1.86	0.76	1.11	0.89	0.718	1.04	0.688	0.99	1.30	0.921	No
323	32.30	1.87	0.76	1.11	0.89	0.718	1.04	0.689	0.99	1.30	0.921	No
324	32.40	1.88	0.76	1.11	0.89	0.718	1.04	0.689	0.99	1.30	2.000	Yes
325	32.50	1.88	0.76	1.12	0.89	0.718	1.04	0.689	0.99	1.30	2.000	Yes
326	32.60	1.89	0.77	1.12	0.89	0.718	1.04	0.689	0.99	1.30	2.000	Yes
327	32.70	1.89	0.77	1.12	0.89	0.718	1.04	0.689	0.99	1.30	2.000	Yes
328	32.80	1.90	0.77	1.13	0.89	0.719	1.04	0.689	0.99	1.30	2.000	Yes
329	32.90	1.91	0.78	1.13	0.88	0.719	1.04	0.689	0.99	1.30	2.000	Yes
330	33.00	1.91	0.78	1.13	0.88	0.719	1.04	0.689	0.99	1.30	0.932	No
331	33.10	1.92	0.78	1.13	0.88	0.719	1.04	0.689	0.99	1.30	0.932	No
332	33.20	1.92	0.79	1.14	0.88	0.719	1.04	0.689	0.99	1.30	0.933	No
333	33.30	1.93	0.79	1.14	0.88	0.719	1.04	0.689	0.99	1.30	0.933	No
334	33.40	1.93	0.79	1.14	0.88	0.719	1.04	0.689	0.99	1.30	0.934	No
335	33.50	1.94	0.80	1.14	0.88	0.719	1.04	0.690	0.99	1.30	0.934	No
336	33.60	1.94	0.80	1.15	0.88	0.720	1.04	0.690	0.99	1.30	0.935	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
337	33.70	1.95	0.80	1.15	0.88	0.720	1.04	0.690	0.99	1.30	0.935	No
338	33.80	1.96	0.80	1.15	0.88	0.720	1.04	0.690	0.99	1.30	0.935	No
339	33.90	1.96	0.81	1.15	0.88	0.720	1.04	0.690	0.99	1.30	0.935	No
340	34.00	1.97	0.81	1.16	0.88	0.720	1.04	0.690	0.99	1.30	0.935	No
341	34.10	1.97	0.81	1.16	0.88	0.720	1.04	0.690	0.99	1.30	0.936	No
342	34.20	1.98	0.82	1.16	0.88	0.720	1.04	0.690	0.99	1.30	0.936	No
343	34.30	1.98	0.82	1.16	0.88	0.720	1.04	0.690	0.99	1.30	0.936	No
344	34.40	1.99	0.82	1.17	0.88	0.720	1.04	0.690	0.99	1.30	0.936	No
345	34.50	2.00	0.83	1.17	0.88	0.720	1.04	0.690	0.99	1.30	2.000	Yes
346	34.60	2.00	0.83	1.17	0.88	0.720	1.04	0.690	0.99	1.30	2.000	Yes
347	34.70	2.01	0.83	1.18	0.88	0.720	1.04	0.690	0.99	1.30	2.000	Yes
348	34.80	2.01	0.84	1.18	0.88	0.720	1.04	0.690	0.99	1.30	2.000	Yes
349	34.90	2.02	0.84	1.18	0.88	0.720	1.04	0.690	0.98	1.30	2.000	Yes
350	35.00	2.03	0.84	1.19	0.87	0.720	1.04	0.690	0.98	1.30	2.000	Yes
351	35.10	2.03	0.85	1.19	0.87	0.720	1.04	0.690	0.98	1.30	2.000	Yes
352	35.20	2.04	0.85	1.19	0.87	0.720	1.04	0.690	0.97	1.30	2.000	Yes
353	35.30	2.05	0.85	1.20	0.87	0.720	1.04	0.690	0.97	1.30	2.000	Yes
354	35.40	2.05	0.85	1.20	0.87	0.719	1.04	0.689	0.97	1.30	2.000	Yes
355	35.50	2.06	0.86	1.20	0.87	0.719	1.04	0.689	0.97	1.30	0.907	No
356	35.60	2.07	0.86	1.21	0.87	0.719	1.04	0.689	0.97	1.30	0.908	No
357	35.70	2.07	0.86	1.21	0.87	0.719	1.04	0.689	0.97	1.30	0.907	No
358	35.80	2.08	0.87	1.21	0.87	0.719	1.04	0.689	0.97	1.30	2.000	Yes
359	35.90	2.09	0.87	1.22	0.87	0.719	1.04	0.689	0.97	1.30	2.000	Yes
360	36.00	2.09	0.87	1.22	0.87	0.718	1.04	0.689	0.97	1.30	2.000	Yes
361	36.10	2.10	0.88	1.22	0.87	0.718	1.04	0.688	0.97	1.30	2.000	Yes
362	36.20	2.11	0.88	1.23	0.87	0.718	1.04	0.688	0.98	1.30	2.000	Yes
363	36.30	2.11	0.88	1.23	0.87	0.718	1.04	0.688	0.98	1.30	2.000	Yes
364	36.40	2.12	0.89	1.23	0.87	0.718	1.04	0.688	0.98	1.30	2.000	Yes
365	36.50	2.12	0.89	1.24	0.87	0.718	1.04	0.688	0.98	1.30	2.000	Yes
366	36.60	2.13	0.89	1.24	0.87	0.718	1.04	0.688	0.97	1.30	2.000	Yes
367	36.70	2.14	0.90	1.24	0.87	0.717	1.04	0.688	0.96	1.30	2.000	Yes
368	36.80	2.14	0.90	1.25	0.87	0.717	1.04	0.687	0.95	1.30	2.000	Yes
369	36.90	2.15	0.90	1.25	0.87	0.717	1.04	0.687	0.95	1.30	2.000	Yes
370	37.00	2.16	0.90	1.25	0.87	0.717	1.04	0.687	0.95	1.30	0.922	No
371	37.10	2.16	0.91	1.26	0.86	0.717	1.04	0.687	0.95	1.30	0.922	No
372	37.20	2.17	0.91	1.26	0.86	0.716	1.04	0.687	0.95	1.30	0.923	No
373	37.30	2.18	0.91	1.26	0.86	0.716	1.04	0.686	0.95	1.30	0.923	No
374	37.40	2.18	0.92	1.27	0.86	0.716	1.04	0.686	0.95	1.30	0.924	No
375	37.50	2.19	0.92	1.27	0.86	0.716	1.04	0.686	0.95	1.30	0.924	No
376	37.60	2.20	0.92	1.27	0.86	0.715	1.04	0.686	0.94	1.30	0.925	No
377	37.70	2.20	0.93	1.28	0.86	0.715	1.04	0.686	0.94	1.30	0.925	No
378	37.80	2.21	0.93	1.28	0.86	0.715	1.04	0.685	0.95	1.30	0.922	No
379	37.90	2.22	0.93	1.28	0.86	0.715	1.04	0.685	0.95	1.30	0.923	No
380	38.00	2.22	0.94	1.29	0.86	0.715	1.04	0.685	0.94	1.30	0.927	No
381	38.10	2.23	0.94	1.29	0.86	0.714	1.04	0.685	0.94	1.30	0.928	No
382	38.20	2.24	0.94	1.30	0.86	0.714	1.04	0.684	0.94	1.30	0.928	No
383	38.30	2.24	0.95	1.30	0.86	0.714	1.04	0.684	0.94	1.30	0.929	No
384	38.40	2.25	0.95	1.30	0.86	0.714	1.04	0.684	0.94	1.30	0.929	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
385	38.50	2.26	0.95	1.31	0.86	0.713	1.04	0.684	0.94	1.30	0.930	No
386	38.60	2.26	0.95	1.31	0.86	0.713	1.04	0.684	0.94	1.30	0.930	No
387	38.70	2.27	0.96	1.31	0.86	0.713	1.04	0.683	0.94	1.30	0.931	No
388	38.80	2.28	0.96	1.32	0.86	0.713	1.04	0.683	0.93	1.30	0.931	No
389	38.90	2.28	0.96	1.32	0.86	0.712	1.04	0.683	0.93	1.30	0.932	No
390	39.00	2.29	0.97	1.32	0.86	0.712	1.04	0.682	0.93	1.30	0.932	No
391	39.10	2.30	0.97	1.33	0.86	0.712	1.04	0.682	0.93	1.30	0.933	No
392	39.20	2.31	0.97	1.33	0.85	0.712	1.04	0.682	0.93	1.30	0.933	No
393	39.30	2.31	0.98	1.34	0.85	0.711	1.04	0.682	0.93	1.30	0.934	No
394	39.40	2.32	0.98	1.34	0.85	0.711	1.04	0.682	0.93	1.30	0.934	No
395	39.50	2.33	0.98	1.34	0.85	0.711	1.04	0.681	0.93	1.30	0.934	No
396	39.60	2.33	0.99	1.35	0.85	0.711	1.04	0.681	0.93	1.30	0.935	No
397	39.70	2.34	0.99	1.35	0.85	0.710	1.04	0.681	0.93	1.30	0.935	No
398	39.80	2.35	0.99	1.35	0.85	0.710	1.04	0.680	0.93	1.30	0.936	No
399	39.90	2.35	1.00	1.36	0.85	0.710	1.04	0.680	0.93	1.30	0.936	No
400	40.00	2.36	1.00	1.36	0.85	0.709	1.04	0.680	0.92	1.30	0.937	No
401	40.10	2.37	1.00	1.36	0.85	0.709	1.04	0.680	0.92	1.30	0.937	No
402	40.20	2.37	1.00	1.37	0.85	0.709	1.04	0.679	0.92	1.30	0.938	No
403	40.30	2.38	1.01	1.37	0.85	0.709	1.04	0.679	0.92	1.30	0.938	No
404	40.40	2.39	1.01	1.38	0.85	0.708	1.04	0.679	0.92	1.30	0.939	No
405	40.50	2.39	1.01	1.38	0.85	0.708	1.04	0.679	0.92	1.30	0.939	No
406	40.60	2.40	1.02	1.38	0.85	0.708	1.04	0.678	0.92	1.30	0.939	No
407	40.70	2.41	1.02	1.39	0.85	0.707	1.04	0.678	0.92	1.30	0.940	No
408	40.80	2.41	1.02	1.39	0.85	0.707	1.04	0.678	0.92	1.30	0.940	No
409	40.90	2.42	1.03	1.39	0.85	0.707	1.04	0.677	0.92	1.30	0.941	No
410	41.00	2.43	1.03	1.40	0.85	0.706	1.04	0.677	0.92	1.30	0.941	No
411	41.10	2.43	1.03	1.40	0.85	0.706	1.04	0.677	0.92	1.30	0.942	No
412	41.20	2.44	1.04	1.41	0.84	0.706	1.04	0.677	0.91	1.30	0.942	No
413	41.30	2.45	1.04	1.41	0.84	0.706	1.04	0.676	0.91	1.30	0.942	No
414	41.40	2.46	1.04	1.41	0.84	0.705	1.04	0.676	0.91	1.30	0.943	No
415	41.50	2.46	1.05	1.42	0.84	0.705	1.04	0.676	0.91	1.30	0.943	No
416	41.60	2.47	1.05	1.42	0.84	0.705	1.04	0.675	0.91	1.30	0.944	No
417	41.70	2.48	1.05	1.42	0.84	0.704	1.04	0.675	0.91	1.30	0.944	No
418	41.80	2.48	1.05	1.43	0.84	0.704	1.04	0.675	0.91	1.30	0.944	No
419	41.90	2.49	1.06	1.43	0.84	0.704	1.04	0.675	0.91	1.30	0.945	No
420	42.00	2.50	1.06	1.44	0.84	0.703	1.04	0.674	0.91	1.30	0.945	No
421	42.10	2.50	1.06	1.44	0.84	0.703	1.04	0.674	0.91	1.30	0.939	No
422	42.20	2.51	1.07	1.44	0.84	0.703	1.04	0.674	0.93	1.30	0.923	No
423	42.30	2.52	1.07	1.45	0.84	0.703	1.04	0.674	0.94	1.30	0.926	No
424	42.40	2.52	1.07	1.45	0.84	0.702	1.04	0.673	0.95	1.30	0.928	No
425	42.50	2.53	1.08	1.45	0.84	0.702	1.04	0.673	0.95	1.30	0.927	No
426	42.60	2.54	1.08	1.46	0.84	0.702	1.04	0.673	0.94	1.30	0.926	No
427	42.70	2.54	1.08	1.46	0.84	0.702	1.04	0.673	0.94	1.30	0.926	No
428	42.80	2.55	1.09	1.46	0.84	0.702	1.04	0.672	0.94	1.30	0.926	No
429	42.90	2.55	1.09	1.47	0.84	0.701	1.04	0.672	0.94	1.30	2.000	Yes
430	43.00	2.56	1.09	1.47	0.84	0.701	1.04	0.672	0.94	1.30	2.000	Yes
431	43.10	2.57	1.10	1.47	0.84	0.701	1.04	0.672	0.95	1.30	2.000	Yes
432	43.20	2.57	1.10	1.48	0.84	0.701	1.04	0.672	0.95	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
433	43.30	2.58	1.10	1.48	0.83	0.700	1.04	0.671	0.95	1.30	2.000	Yes
434	43.40	2.59	1.10	1.48	0.83	0.700	1.04	0.671	0.95	1.30	0.929	No
435	43.50	2.59	1.11	1.49	0.83	0.700	1.04	0.671	0.95	1.30	0.929	No
436	43.60	2.60	1.11	1.49	0.83	0.700	1.04	0.671	0.95	1.30	0.929	No
437	43.70	2.61	1.11	1.49	0.83	0.699	1.04	0.670	0.94	1.30	0.929	No
438	43.80	2.61	1.12	1.50	0.83	0.699	1.04	0.670	0.94	1.30	0.929	No
439	43.90	2.62	1.12	1.50	0.83	0.699	1.04	0.670	0.94	1.30	0.929	No
440	44.00	2.63	1.12	1.50	0.83	0.699	1.04	0.670	0.94	1.30	0.929	No
441	44.10	2.63	1.13	1.51	0.83	0.699	1.04	0.669	0.94	1.30	0.929	No
442	44.20	2.64	1.13	1.51	0.83	0.698	1.04	0.669	0.94	1.30	0.929	No
443	44.30	2.64	1.13	1.51	0.83	0.698	1.04	0.669	0.94	1.30	0.929	No
444	44.40	2.65	1.14	1.52	0.83	0.698	1.04	0.669	0.94	1.30	0.928	No
445	44.50	2.66	1.14	1.52	0.83	0.697	1.04	0.668	0.93	1.30	0.928	No
446	44.60	2.66	1.14	1.52	0.83	0.697	1.04	0.668	0.93	1.30	0.928	No
447	44.70	2.67	1.15	1.53	0.83	0.697	1.04	0.668	0.92	1.30	0.927	No
448	44.80	2.68	1.15	1.53	0.83	0.697	1.04	0.668	0.92	1.30	0.928	No
449	44.90	2.68	1.15	1.53	0.83	0.696	1.04	0.667	0.92	1.30	0.928	No
450	45.00	2.69	1.15	1.54	0.83	0.696	1.04	0.667	0.92	1.30	0.928	No
451	45.10	2.70	1.16	1.54	0.83	0.696	1.04	0.667	0.92	1.30	0.928	No
452	45.20	2.70	1.16	1.54	0.83	0.696	1.04	0.667	0.92	1.30	0.928	No
453	45.30	2.71	1.16	1.55	0.82	0.695	1.04	0.666	0.92	1.30	0.928	No
454	45.40	2.72	1.17	1.55	0.82	0.695	1.04	0.666	0.92	1.30	0.928	No
455	45.50	2.72	1.17	1.55	0.82	0.695	1.04	0.666	0.92	1.30	0.928	No
456	45.60	2.73	1.17	1.56	0.82	0.694	1.04	0.666	0.92	1.30	0.928	No
457	45.70	2.74	1.18	1.56	0.82	0.694	1.04	0.665	0.92	1.30	0.928	No
458	45.80	2.74	1.18	1.56	0.82	0.694	1.04	0.665	0.92	1.30	0.929	No
459	45.90	2.75	1.18	1.57	0.82	0.694	1.04	0.665	0.92	1.30	0.929	No
460	46.00	2.76	1.19	1.57	0.82	0.693	1.04	0.665	0.92	1.30	0.929	No
461	46.10	2.76	1.19	1.57	0.82	0.693	1.04	0.664	0.92	1.30	0.929	No
462	46.20	2.77	1.19	1.58	0.82	0.693	1.04	0.664	0.92	1.30	0.929	No
463	46.30	2.78	1.19	1.58	0.82	0.693	1.04	0.664	0.92	1.30	0.929	No
464	46.40	2.78	1.20	1.58	0.82	0.692	1.04	0.664	0.92	1.30	0.929	No
465	46.50	2.79	1.20	1.59	0.82	0.692	1.04	0.663	0.92	1.30	0.929	No
466	46.60	2.79	1.20	1.59	0.82	0.692	1.04	0.663	0.92	1.30	0.929	No
467	46.70	2.80	1.21	1.59	0.82	0.691	1.04	0.663	0.91	1.30	2.000	Yes
468	46.80	2.81	1.21	1.60	0.82	0.691	1.04	0.662	0.91	1.30	2.000	Yes
469	46.90	2.81	1.21	1.60	0.82	0.691	1.04	0.662	0.91	1.30	2.000	Yes
470	47.00	2.82	1.22	1.60	0.82	0.691	1.04	0.662	0.92	1.30	2.000	Yes
471	47.10	2.83	1.22	1.61	0.82	0.690	1.04	0.662	0.93	1.30	2.000	Yes
472	47.20	2.83	1.22	1.61	0.82	0.690	1.04	0.661	0.94	1.30	0.928	No
473	47.30	2.84	1.23	1.61	0.82	0.690	1.04	0.661	0.93	1.30	0.928	No
474	47.40	2.85	1.23	1.62	0.81	0.689	1.04	0.661	0.93	1.30	0.928	No
475	47.50	2.85	1.23	1.62	0.81	0.689	1.04	0.661	0.94	1.30	0.928	No
476	47.60	2.86	1.24	1.62	0.81	0.689	1.04	0.660	0.95	1.30	0.927	No
477	47.70	2.87	1.24	1.63	0.81	0.689	1.04	0.660	0.95	1.30	0.926	No
478	47.80	2.87	1.24	1.63	0.81	0.688	1.04	0.660	0.96	1.30	0.924	No
479	47.90	2.88	1.24	1.63	0.81	0.688	1.04	0.660	0.96	1.30	0.924	No
480	48.00	2.89	1.25	1.64	0.81	0.688	1.04	0.659	0.96	1.30	0.923	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
481	48.10	2.89	1.25	1.64	0.81	0.688	1.04	0.659	0.96	1.30	0.923	No
482	48.20	2.90	1.25	1.64	0.81	0.688	1.04	0.659	0.96	1.30	0.923	No
483	48.30	2.90	1.26	1.65	0.81	0.687	1.04	0.659	0.96	1.30	0.924	No
484	48.40	2.91	1.26	1.65	0.81	0.687	1.04	0.659	0.95	1.30	0.924	No
485	48.50	2.92	1.26	1.65	0.81	0.687	1.04	0.658	0.95	1.30	0.924	No
486	48.60	2.92	1.27	1.66	0.81	0.687	1.04	0.658	0.95	1.30	0.924	No
487	48.70	2.93	1.27	1.66	0.81	0.686	1.04	0.658	0.95	1.30	0.924	No
488	48.80	2.94	1.27	1.66	0.81	0.686	1.04	0.658	0.95	1.30	0.923	No
489	48.90	2.94	1.28	1.67	0.81	0.686	1.04	0.657	0.96	1.30	0.922	No
490	49.00	2.95	1.28	1.67	0.81	0.686	1.04	0.657	0.96	1.30	0.922	No
491	49.10	2.95	1.28	1.67	0.81	0.685	1.04	0.657	0.96	1.30	0.922	No
492	49.20	2.96	1.29	1.67	0.81	0.685	1.04	0.657	0.96	1.30	0.922	No
493	49.30	2.97	1.29	1.68	0.81	0.685	1.04	0.656	0.96	1.30	0.922	No
494	49.40	2.97	1.29	1.68	0.80	0.685	1.04	0.656	0.96	1.30	0.921	No
495	49.50	2.98	1.29	1.68	0.80	0.684	1.04	0.656	0.96	1.30	0.920	No
496	49.60	2.98	1.30	1.69	0.80	0.684	1.04	0.656	0.96	1.30	0.919	No
497	49.70	2.99	1.30	1.69	0.80	0.684	1.04	0.656	0.96	1.30	0.919	No
498	49.80	3.00	1.30	1.69	0.80	0.684	1.04	0.655	0.96	1.30	0.919	No

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
σ_v :	Total overburden pressure at test point (tsf)
u_0 :	Water pressure at test point (tsf)
σ_v' :	Effective overburden pressure based on GWT during earthquake (tsf)
r_d :	Nonlinear shear mass factor
CSR:	Cyclic Stress Ratio
MSF:	Magnitude Scaling Factor
CSR _{eq} :	CSR adjusted for M=7.5
K_σ :	Effective overburden stress factor
CSR*:	CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::													
Point ID	Depth (ft)	q_c (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1	0.10	40.35	34.64	2.15	0.46	1.70	65.88	53.50	119.37	4.000	No	No	2.00
2	0.20	41.58	34.45	2.14	0.47	1.70	62.71	52.62	115.33	4.000	No	No	2.00
3	0.30	45.23	32.68	2.12	0.45	1.70	71.79	52.86	124.65	4.000	No	No	2.00
4	0.40	51.74	29.44	2.08	0.43	1.70	83.48	51.47	134.94	4.000	No	No	2.00
5	0.50	57.90	27.18	2.05	0.41	1.70	94.08	50.27	144.35	4.000	No	No	2.00
6	0.60	62.33	26.56	2.04	0.40	1.70	101.47	50.63	152.09	4.000	No	No	2.00
7	0.70	64.56	26.93	2.05	0.39	1.70	104.82	51.88	156.70	4.000	No	No	2.00
8	0.80	64.46	27.78	2.06	0.39	1.70	104.79	53.24	158.03	4.000	No	No	2.00
9	0.90	62.11	29.52	2.08	0.39	1.70	100.98	55.09	156.07	4.000	Yes	No	2.00
10	1.00	57.54	32.95	2.12	0.40	1.70	93.52	57.85	151.37	4.000	Yes	No	2.00
11	1.10	51.75	38.28	2.19	0.41	1.70	82.74	60.54	143.27	4.000	Yes	No	2.00
12	1.20	45.44	45.01	2.28	0.43	1.70	73.08	62.79	135.86	4.000	Yes	No	2.00
13	1.30	39.26	52.31	2.37	0.44	1.70	63.11	63.70	126.82	4.000	Yes	No	2.00
14	1.40	33.94	59.32	2.45	0.46	1.70	52.97	63.36	116.33	4.000	Yes	No	2.00
15	1.50	30.81	63.76	2.51	0.48	1.70	47.43	63.01	110.44	4.000	Yes	No	2.00
16	1.60	30.91	63.28	2.50	0.47	1.70	48.04	63.07	111.11	4.000	Yes	No	2.00
17	1.70	33.33	58.92	2.45	0.46	1.70	53.46	63.38	116.84	4.000	Yes	No	2.00
18	1.80	36.69	53.26	2.38	0.45	1.70	59.05	62.99	122.04	4.000	Yes	No	2.00
19	1.90	39.74	48.46	2.32	0.44	1.70	64.26	62.31	126.57	4.000	Yes	No	2.00
20	2.00	42.16	45.53	2.28	0.44	1.70	68.15	61.82	129.98	4.000	Yes	No	2.00
21	2.10	43.95	44.18	2.26	0.43	1.70	70.71	61.71	132.41	4.000	No	No	2.00
22	2.20	45.84	43.22	2.25	0.43	1.70	72.88	61.67	134.55	4.000	No	No	2.00
23	2.30	48.69	41.10	2.23	0.42	1.70	77.30	61.37	138.67	4.000	No	No	2.00
24	2.40	53.22	37.21	2.18	0.41	1.70	84.42	60.03	144.46	4.000	No	No	2.00
25	2.50	59.55	32.23	2.12	0.40	1.70	94.70	57.27	151.97	4.000	No	No	2.00
26	2.60	66.89	27.47	2.06	0.39	1.70	107.80	53.32	161.12	4.000	No	No	2.00
27	2.70	74.02	24.03	2.01	0.37	1.70	119.82	49.13	168.95	4.000	No	No	2.00
28	2.80	79.74	22.18	1.99	0.36	1.70	129.04	46.50	175.54	4.000	No	No	2.00
29	2.90	83.24	21.87	1.99	0.35	1.70	135.39	46.71	182.10	4.000	No	No	2.00
30	3.00	83.91	23.02	2.00	0.35	1.70	136.67	49.68	186.35	4.000	No	No	2.00
31	3.10	81.73	25.09	2.03	0.35	1.70	132.25	53.44	185.69	4.000	No	No	2.00
32	3.20	77.93	27.42	2.06	0.36	1.70	124.90	56.48	181.38	4.000	No	No	2.00
33	3.30	74.96	28.86	2.07	0.36	1.70	118.37	57.57	175.94	4.000	No	No	2.00
34	3.40	74.74	28.86	2.07	0.36	1.70	117.92	57.48	175.40	4.000	No	No	2.00
35	3.50	76.96	27.81	2.06	0.36	1.70	123.82	56.93	180.76	4.000	No	No	2.00
36	3.60	80.33	26.36	2.04	0.35	1.70	129.11	55.36	184.46	4.000	No	No	2.00
37	3.70	84.17	24.82	2.02	0.35	1.70	134.15	53.22	187.36	4.000	No	No	2.00
38	3.80	89.18	22.96	2.00	0.34	1.69	141.17	50.24	191.42	4.000	No	No	2.00
39	3.90	95.46	20.75	1.97	0.34	1.66	149.71	45.85	195.55	4.000	No	No	2.00
40	4.00	102.50	18.85	1.95	0.33	1.63	157.26	41.22	198.48	4.000	No	No	2.00
41	4.10	112.12	17.03	1.93	0.32	1.60	165.86	36.09	201.95	4.000	No	No	2.00
42	4.20	123.24	15.33	1.90	0.31	1.56	183.03	31.35	214.38	4.000	No	No	2.00
43	4.30	133.99	13.59	1.88	0.30	1.53	196.13	25.15	221.28	4.000	No	No	2.00
44	4.40	142.54	11.89	1.86	0.30	1.52	203.51	18.26	221.77	4.000	No	No	2.00
45	4.50	150.23	10.35	1.84	0.30	1.50	212.39	12.22	224.61	4.000	No	No	2.00
46	4.60	159.06	8.90	1.82	0.29	1.48	221.76	7.15	228.91	4.000	No	No	2.00
47	4.70	168.40	7.69	1.81	0.29	1.45	231.29	3.78	235.06	4.000	No	No	2.00
48	4.80	177.80	6.62	1.80	0.28	1.42	239.38	1.70	241.08	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
49	4.90	185.66	5.96	1.79	0.27	1.41	248.60	0.89	249.49	4.000	No	No	2.00
50	5.00	191.18	5.85	1.79	0.27	1.39	252.01	0.79	252.80	4.000	No	No	2.00
51	5.10	193.58	6.40	1.79	0.26	1.38	253.24	1.44	254.68	4.000	No	No	2.00
52	5.20	192.78	7.58	1.81	0.26	1.37	251.40	3.68	255.08	4.000	No	No	2.00
53	5.30	188.43	9.22	1.83	0.27	1.36	244.54	8.68	253.22	4.000	No	No	2.00
54	5.40	181.46	10.94	1.85	0.27	1.37	234.24	15.47	249.71	4.000	No	No	2.00
55	5.50	173.48	12.35	1.87	0.27	1.36	223.15	21.30	244.45	4.000	No	No	2.00
56	5.60	166.49	13.28	1.88	0.28	1.37	213.74	24.99	238.73	4.000	No	No	2.00
57	5.70	160.17	13.99	1.89	0.28	1.36	206.91	27.68	234.58	4.000	No	No	2.00
58	5.80	154.54	14.41	1.89	0.29	1.37	200.01	28.95	228.97	4.000	No	No	2.00
59	5.90	151.20	14.17	1.89	0.30	1.38	193.82	27.48	221.30	4.000	No	No	2.00
60	6.00	150.36	13.38	1.88	0.31	1.37	195.37	24.21	219.58	4.000	No	No	2.00
61	6.10	151.58	12.33	1.87	0.31	1.37	196.81	19.80	216.61	4.000	No	No	2.00
62	6.20	152.65	11.40	1.86	0.31	1.37	197.47	15.96	213.43	4.000	No	No	2.00
63	6.30	153.98	10.48	1.84	0.32	1.37	198.60	12.30	210.91	4.000	No	No	2.00
64	6.40	155.02	9.78	1.83	0.32	1.36	200.47	9.72	210.19	4.000	No	No	2.00
65	6.50	155.21	9.46	1.83	0.32	1.36	199.66	8.56	208.22	4.000	No	No	2.00
66	6.60	154.44	9.49	1.83	0.32	1.35	197.41	8.61	206.02	4.000	No	No	2.00
67	6.70	153.63	9.68	1.83	0.32	1.35	195.74	9.26	205.00	4.000	No	No	2.00
68	6.80	153.80	9.82	1.84	0.32	1.34	194.48	9.72	204.19	4.000	No	No	2.00
69	6.90	154.54	9.96	1.84	0.32	1.34	195.25	10.23	205.48	4.000	No	No	2.00
70	7.00	154.90	10.40	1.84	0.32	1.33	195.16	11.86	207.02	4.000	No	No	2.00
71	7.10	153.81	11.12	1.85	0.32	1.32	192.41	14.58	206.99	4.000	No	No	2.00
72	7.20	150.50	12.13	1.86	0.32	1.31	188.12	18.54	206.66	4.000	No	No	2.00
73	7.30	144.74	13.44	1.88	0.32	1.31	180.38	23.49	203.87	4.000	No	No	2.00
74	7.40	136.62	15.14	1.90	0.33	1.31	169.66	29.44	199.10	4.000	No	No	2.00
75	7.50	127.15	17.26	1.93	0.34	1.31	157.67	36.03	193.70	4.000	No	No	2.00
76	7.60	118.12	19.34	1.95	0.35	1.32	146.00	41.30	187.30	4.000	No	No	2.00
77	7.70	108.93	21.33	1.98	0.35	1.32	136.82	45.56	182.38	4.000	No	No	2.00
78	7.80	101.20	22.62	2.00	0.37	1.33	124.84	46.88	171.72	4.000	No	No	2.00
79	7.90	96.54	22.77	2.00	0.38	1.33	118.56	46.23	164.79	4.000	No	No	2.00
80	8.00	91.21	23.21	2.00	0.38	1.32	119.82	47.38	167.20	4.000	No	No	2.00
81	8.10	83.87	24.67	2.02	0.40	1.34	105.76	48.02	153.78	4.000	Yes	No	2.00
82	8.20	73.95	28.05	2.06	0.41	1.35	92.30	51.26	143.56	4.000	Yes	No	2.00
83	8.30	65.66	32.33	2.12	0.42	1.36	84.77	55.26	140.03	4.000	Yes	No	2.00
84	8.40	58.44	37.46	2.18	0.43	1.36	75.67	58.21	133.88	4.000	Yes	No	2.00
85	8.50	50.44	44.09	2.26	0.45	1.38	65.60	60.36	125.96	4.000	Yes	No	2.00
86	8.60	41.90	52.35	2.37	0.46	1.39	55.31	61.62	116.92	4.000	Yes	No	2.00
87	8.70	33.76	61.20	2.48	0.49	1.41	43.97	61.37	105.34	4.000	Yes	No	2.00
88	8.80	26.20	70.08	2.59	0.51	1.43	35.10	60.86	95.96	4.000	Yes	No	2.00
89	8.90	21.14	77.09	2.68	0.53	1.44	26.55	0.00	26.55	4.000	Yes	Yes	2.00
90	9.00	19.30	80.30	2.72	0.54	1.45	24.41	0.00	24.41	4.000	Yes	Yes	2.00
91	9.10	20.38	78.59	2.69	0.53	1.43	27.81	0.00	27.81	4.000	No	Yes	2.00
92	9.20	22.74	73.76	2.63	0.52	1.42	30.49	0.00	30.49	4.000	No	Yes	2.00
93	9.30	23.71	69.31	2.58	0.51	1.41	33.29	60.18	93.47	0.130	No	No	0.21
94	9.40	23.62	65.44	2.53	0.52	1.42	31.41	58.83	90.25	0.126	No	No	0.20
95	9.50	22.74	63.01	2.50	0.53	1.42	30.01	57.88	87.88	0.124	No	No	0.20
96	9.60	22.51	61.53	2.48	0.53	1.42	29.87	57.48	87.35	0.123	No	No	0.20

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
97	9.70	22.82	61.05	2.48	0.53	1.41	30.38	57.50	87.88	0.124	No	No	0.20
98	9.80	23.67	60.83	2.47	0.52	1.41	30.99	57.62	88.61	0.124	No	No	0.20
99	9.90	26.17	58.44	2.44	0.52	1.40	32.86	57.50	90.37	0.126	No	No	0.20
100	10.00	29.98	54.19	2.39	0.50	1.38	39.53	58.02	97.56	0.134	No	No	0.21
101	10.10	33.87	49.96	2.34	0.49	1.37	44.87	57.88	102.74	0.141	No	No	0.22
102	10.20	36.11	47.45	2.31	0.49	1.36	46.98	57.33	104.31	0.143	No	No	0.23
103	10.30	36.87	46.38	2.29	0.49	1.36	47.50	56.97	104.47	0.144	No	No	0.23
104	10.40	37.04	45.64	2.28	0.49	1.36	47.42	56.58	104.00	0.143	No	No	0.22
105	10.50	37.04	45.00	2.27	0.49	1.35	47.34	56.23	103.57	0.142	No	No	0.22
106	10.60	36.91	45.12	2.28	0.49	1.35	47.24	56.27	103.51	0.142	No	No	0.22
107	10.70	36.31	46.66	2.30	0.49	1.35	46.63	56.88	103.50	0.142	No	No	0.22
108	10.80	35.51	49.04	2.33	0.49	1.35	44.78	57.47	102.25	0.140	No	No	0.22
109	10.90	34.67	51.42	2.36	0.49	1.34	43.95	58.21	102.16	0.140	No	No	0.21
110	11.00	33.49	53.71	2.38	0.49	1.34	43.20	58.85	102.06	4.000	Yes	No	2.00
111	11.10	30.97	57.18	2.43	0.50	1.34	40.17	59.16	99.32	4.000	Yes	No	2.00
112	11.20	27.24	62.41	2.49	0.51	1.35	34.52	59.01	93.54	4.000	Yes	No	2.00
113	11.30	22.91	69.06	2.58	0.53	1.36	29.37	58.99	88.37	4.000	Yes	No	2.00
114	11.40	18.96	76.05	2.66	0.54	1.36	24.09	0.00	24.09	4.000	Yes	Yes	2.00
115	11.50	15.45	83.06	2.75	0.55	1.37	19.69	0.00	19.69	4.000	Yes	Yes	2.00
116	11.60	12.82	89.55	2.83	0.56	1.37	16.12	0.00	16.12	4.000	Yes	Yes	2.00
117	11.70	10.68	95.69	2.91	0.57	1.38	14.06	0.00	14.06	4.000	Yes	Yes	2.00
118	11.80	8.66	100.00	3.00	0.58	1.38	11.48	0.00	11.48	4.000	Yes	Yes	2.00
119	11.90	7.50	100.00	3.08	0.59	1.39	8.35	0.00	8.35	4.000	No	Yes	2.00
120	12.00	8.19	100.00	3.07	0.58	1.38	9.54	0.00	9.54	4.000	No	Yes	2.00
121	12.10	11.14	98.46	2.94	0.57	1.36	14.03	0.00	14.03	4.000	No	Yes	2.00
122	12.20	15.23	86.89	2.80	0.55	1.35	19.37	0.00	19.37	4.000	No	Yes	2.00
123	12.30	19.15	76.80	2.67	0.54	1.34	24.72	0.00	24.72	4.000	No	Yes	2.00
124	12.40	21.99	69.33	2.58	0.53	1.33	28.39	58.76	87.15	0.123	No	No	0.18
125	12.50	24.28	64.78	2.52	0.53	1.32	29.63	58.18	87.80	0.123	No	No	0.18
126	12.60	25.49	64.47	2.52	0.52	1.31	32.83	59.02	91.85	0.128	No	No	0.18
127	12.70	25.26	67.33	2.55	0.52	1.31	32.51	59.55	92.06	0.128	No	No	0.18
128	12.80	22.79	72.96	2.62	0.53	1.31	28.58	0.00	28.58	4.000	No	Yes	2.00
129	12.90	19.03	80.33	2.72	0.54	1.32	23.73	0.00	23.73	4.000	No	Yes	2.00
130	13.00	15.05	88.98	2.82	0.55	1.33	18.78	0.00	18.78	4.000	No	Yes	2.00
131	13.10	11.64	98.62	2.95	0.57	1.33	13.98	0.00	13.98	4.000	No	Yes	2.00
132	13.20	9.43	100.00	3.06	0.58	1.34	11.12	0.00	11.12	4.000	No	Yes	2.00
133	13.30	8.27	100.00	3.13	0.58	1.34	10.55	0.00	10.55	4.000	No	Yes	2.00
134	13.40	7.40	100.00	3.18	0.58	1.34	9.61	0.00	9.61	4.000	No	Yes	2.00
135	13.50	6.61	100.00	3.23	0.59	1.34	7.85	0.00	7.85	4.000	No	Yes	2.00
136	13.60	6.06	100.00	3.26	0.59	1.34	7.54	0.00	7.54	4.000	No	Yes	2.00
137	13.70	5.98	100.00	3.25	0.59	1.33	7.52	0.00	7.52	4.000	No	Yes	2.00
138	13.80	5.98	100.00	3.23	0.59	1.33	7.51	0.00	7.51	4.000	No	Yes	2.00
139	13.90	5.98	100.00	3.20	0.59	1.33	7.49	0.00	7.49	4.000	No	Yes	2.00
140	14.00	5.83	100.00	3.19	0.59	1.33	7.48	0.00	7.48	4.000	No	Yes	2.00
141	14.10	5.63	100.00	3.20	0.59	1.32	6.92	0.00	6.92	4.000	No	Yes	2.00
142	14.20	5.64	100.00	3.21	0.60	1.32	6.72	0.00	6.72	4.000	No	Yes	2.00
143	14.30	6.24	100.00	3.19	0.59	1.32	7.46	0.00	7.46	4.000	No	Yes	2.00
144	14.40	7.17	100.00	3.14	0.59	1.31	9.10	0.00	9.10	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
145	14.50	7.57	100.00	3.14	0.58	1.31	10.09	0.00	10.09	4.000	No	Yes	2.00
146	14.60	7.18	100.00	3.18	0.59	1.31	8.86	0.00	8.86	4.000	No	Yes	2.00
147	14.70	6.44	100.00	3.25	0.59	1.31	7.61	0.00	7.61	4.000	No	Yes	2.00
148	14.80	6.04	100.00	3.30	0.59	1.31	7.37	0.00	7.37	4.000	No	Yes	2.00
149	14.90	5.98	100.00	3.31	0.59	1.30	7.35	0.00	7.35	4.000	No	Yes	2.00
150	15.00	5.98	100.00	3.30	0.59	1.30	7.34	0.00	7.34	4.000	No	Yes	2.00
151	15.10	5.98	100.00	3.27	0.59	1.30	7.32	0.00	7.32	4.000	No	Yes	2.00
152	15.20	5.98	100.00	3.25	0.59	1.30	7.31	0.00	7.31	4.000	No	Yes	2.00
153	15.30	5.98	100.00	3.24	0.59	1.29	7.30	0.00	7.30	4.000	No	Yes	2.00
154	15.40	5.98	100.00	3.23	0.59	1.29	7.28	0.00	7.28	4.000	No	Yes	2.00
155	15.50	5.98	100.00	3.22	0.59	1.29	7.27	0.00	7.27	4.000	No	Yes	2.00
156	15.60	6.05	100.00	3.23	0.59	1.29	7.26	0.00	7.26	4.000	No	Yes	2.00
157	15.70	6.60	100.00	3.21	0.59	1.28	7.52	0.00	7.52	4.000	No	Yes	2.00
158	15.80	7.40	100.00	3.19	0.59	1.28	9.18	0.00	9.18	4.000	No	Yes	2.00
159	15.90	8.12	100.00	3.18	0.58	1.27	10.06	0.00	10.06	4.000	No	Yes	2.00
160	16.00	8.37	100.00	3.18	0.58	1.27	10.04	0.00	10.04	4.000	No	Yes	2.00
161	16.10	8.36	100.00	3.19	0.58	1.27	10.02	0.00	10.02	4.000	No	Yes	2.00
162	16.20	7.83	100.00	3.22	0.58	1.27	9.98	0.00	9.98	4.000	No	Yes	2.00
163	16.30	6.82	100.00	3.27	0.59	1.27	8.11	0.00	8.11	4.000	No	Yes	2.00
164	16.40	5.50	100.00	3.36	0.60	1.27	6.39	0.00	6.39	4.000	No	Yes	2.00
165	16.50	4.57	100.00	3.44	0.60	1.27	5.26	0.00	5.26	4.000	No	Yes	2.00
166	16.60	4.32	100.00	3.46	0.60	1.27	4.77	0.00	4.77	4.000	No	Yes	2.00
167	16.70	4.93	100.00	3.38	0.60	1.26	5.45	0.00	5.45	4.000	No	Yes	2.00
168	16.80	5.99	100.00	3.28	0.59	1.26	7.40	0.00	7.40	4.000	No	Yes	2.00
169	16.90	6.79	100.00	3.21	0.59	1.25	8.49	0.00	8.49	4.000	No	Yes	2.00
170	17.00	6.62	100.00	3.21	0.59	1.25	8.25	0.00	8.25	4.000	No	Yes	2.00
171	17.10	5.62	100.00	3.28	0.60	1.25	6.74	0.00	6.74	4.000	No	Yes	2.00
172	17.20	4.35	100.00	3.43	0.60	1.25	4.94	0.00	4.94	4.000	No	Yes	2.00
173	17.30	3.44	100.00	3.58	0.61	1.25	3.74	0.00	3.74	4.000	No	Yes	2.00
174	17.40	3.24	100.00	3.62	0.61	1.25	3.53	0.00	3.53	4.000	No	Yes	2.00
175	17.50	3.46	100.00	3.57	0.61	1.25	4.23	0.00	4.23	4.000	No	Yes	2.00
176	17.60	4.20	100.00	3.46	0.60	1.25	4.48	0.00	4.48	4.000	No	Yes	2.00
177	17.70	5.21	100.00	3.35	0.60	1.24	6.11	0.00	6.11	4.000	No	Yes	2.00
178	17.80	6.62	100.00	3.26	0.59	1.24	7.74	0.00	7.74	4.000	No	Yes	2.00
179	17.90	7.68	100.00	3.21	0.58	1.23	9.35	0.00	9.35	4.000	No	Yes	2.00
180	18.00	8.46	100.00	3.18	0.58	1.23	9.71	0.00	9.71	4.000	No	Yes	2.00
181	18.10	9.19	100.00	3.15	0.58	1.22	10.38	0.00	10.38	4.000	No	Yes	2.00
182	18.20	10.11	100.00	3.13	0.58	1.22	11.80	0.00	11.80	4.000	No	Yes	2.00
183	18.30	11.39	100.00	3.09	0.57	1.22	12.76	0.00	12.76	4.000	No	Yes	2.00
184	18.40	12.95	100.00	3.04	0.56	1.21	14.65	0.00	14.65	4.000	No	Yes	2.00
185	18.50	15.09	100.00	2.97	0.56	1.21	17.00	0.00	17.00	4.000	Yes	Yes	2.00
186	18.60	17.76	94.58	2.89	0.55	1.20	19.85	0.00	19.85	4.000	Yes	Yes	2.00
187	18.70	21.28	87.28	2.80	0.54	1.19	23.46	0.00	23.46	4.000	Yes	Yes	2.00
188	18.80	25.82	79.02	2.70	0.52	1.19	28.55	0.00	28.55	4.000	Yes	Yes	2.00
189	18.90	31.54	70.32	2.59	0.51	1.18	34.64	60.77	95.41	4.000	Yes	No	2.00
190	19.00	37.82	62.72	2.50	0.49	1.17	41.91	61.19	103.10	4.000	Yes	No	2.00
191	19.10	43.39	57.69	2.43	0.48	1.16	48.62	61.66	110.28	4.000	Yes	No	2.00
192	19.20	48.52	54.25	2.39	0.47	1.16	52.28	61.51	113.79	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
193	19.30	55.06	50.05	2.34	0.46	1.15	58.00	61.39	119.39	4.000	Yes	No	2.00
194	19.40	66.32	42.70	2.25	0.44	1.14	68.97	60.37	129.34	4.000	Yes	No	2.00
195	19.50	80.83	34.15	2.14	0.41	1.13	87.20	57.76	144.96	4.000	Yes	No	2.00
196	19.60	88.75	29.77	2.08	0.39	1.12	102.67	55.77	158.44	4.000	Yes	No	2.00
197	19.70	81.34	32.67	2.12	0.40	1.12	93.12	57.45	150.57	4.000	Yes	No	2.00
198	19.80	68.26	41.88	2.24	0.45	1.14	63.88	58.59	122.48	4.000	Yes	No	2.00
199	19.90	59.34	51.52	2.36	0.45	1.13	61.81	63.03	124.83	4.000	Yes	No	2.00
200	20.00	53.32	57.77	2.43	0.44	1.13	65.00	66.22	131.22	4.000	Yes	No	2.00
201	20.10	41.41	66.05	2.54	0.48	1.14	44.57	62.75	107.32	4.000	Yes	No	2.00
202	20.20	26.61	79.47	2.71	0.54	1.16	23.97	0.00	23.97	4.000	Yes	Yes	2.00
203	20.30	17.09	93.61	2.88	0.55	1.16	18.14	0.00	18.14	4.000	Yes	Yes	2.00
204	20.40	13.44	100.00	2.99	0.57	1.16	14.02	0.00	14.02	4.000	Yes	Yes	2.00
205	20.50	11.12	100.00	3.06	0.57	1.16	12.04	0.00	12.04	4.000	No	Yes	2.00
206	20.60	9.65	100.00	3.10	0.58	1.16	10.54	0.00	10.54	4.000	No	Yes	2.00
207	20.70	8.78	100.00	3.12	0.59	1.16	9.18	0.00	9.18	4.000	No	Yes	2.00
208	20.80	8.37	100.00	3.12	0.59	1.16	9.17	0.00	9.17	4.000	No	Yes	2.00
209	20.90	8.37	100.00	3.12	0.59	1.16	9.15	0.00	9.15	4.000	No	Yes	2.00
210	21.00	8.21	100.00	3.12	0.59	1.16	9.14	0.00	9.14	4.000	No	Yes	2.00
211	21.10	7.65	100.00	3.16	0.59	1.16	8.63	0.00	8.63	4.000	No	Yes	2.00
212	21.20	6.85	100.00	3.21	0.59	1.16	7.28	0.00	7.28	4.000	No	Yes	2.00
213	21.30	6.21	100.00	3.25	0.60	1.15	6.52	0.00	6.52	4.000	No	Yes	2.00
214	21.40	6.04	100.00	3.28	0.60	1.15	6.51	0.00	6.51	4.000	No	Yes	2.00
215	21.50	6.56	100.00	3.26	0.60	1.15	6.72	0.00	6.72	4.000	No	Yes	2.00
216	21.60	8.06	100.00	3.20	0.59	1.15	8.14	0.00	8.14	4.000	No	Yes	2.00
217	21.70	10.65	100.00	3.11	0.58	1.14	11.31	0.00	11.31	4.000	No	Yes	2.00
218	21.80	13.72	100.00	3.01	0.56	1.14	14.98	0.00	14.98	4.000	No	Yes	2.00
219	21.90	16.18	98.76	2.95	0.55	1.13	17.88	0.00	17.88	4.000	No	Yes	2.00
220	22.00	17.19	96.83	2.92	0.55	1.13	19.04	0.00	19.04	4.000	No	Yes	2.00
221	22.10	16.91	98.07	2.94	0.55	1.13	18.11	0.00	18.11	4.000	No	Yes	2.00
222	22.20	16.26	100.00	2.97	0.56	1.13	16.88	0.00	16.88	4.000	No	Yes	2.00
223	22.30	16.46	100.00	2.98	0.56	1.12	16.92	0.00	16.92	4.000	No	Yes	2.00
224	22.40	18.11	98.77	2.95	0.55	1.12	18.64	0.00	18.64	4.000	No	Yes	2.00
225	22.50	21.27	92.43	2.87	0.54	1.12	21.94	0.00	21.94	4.000	No	Yes	2.00
226	22.60	25.33	84.51	2.77	0.53	1.11	26.68	0.00	26.68	4.000	No	Yes	2.00
227	22.70	29.04	76.78	2.67	0.52	1.11	31.19	0.00	31.19	4.000	No	Yes	2.00
228	22.80	31.21	70.77	2.60	0.51	1.11	33.31	60.47	93.77	0.130	No	No	0.15
229	22.90	31.37	68.14	2.56	0.51	1.10	33.28	59.94	93.22	0.129	No	No	0.15
230	23.00	29.97	69.86	2.59	0.52	1.10	31.57	59.79	91.36	0.127	No	No	0.15
231	23.10	27.89	74.83	2.65	0.52	1.10	28.84	0.00	28.84	4.000	No	Yes	2.00
232	23.20	25.85	80.62	2.72	0.53	1.10	26.70	0.00	26.70	4.000	No	Yes	2.00
233	23.30	23.86	85.89	2.79	0.53	1.10	25.15	0.00	25.15	4.000	No	Yes	2.00
234	23.40	21.26	91.58	2.86	0.54	1.10	22.55	0.00	22.55	4.000	No	Yes	2.00
235	23.50	17.88	98.89	2.95	0.55	1.10	18.57	0.00	18.57	4.000	No	Yes	2.00
236	23.60	14.85	100.00	3.05	0.56	1.10	14.60	0.00	14.60	4.000	No	Yes	2.00
237	23.70	13.28	100.00	3.12	0.57	1.10	13.12	0.00	13.12	4.000	No	Yes	2.00
238	23.80	12.51	100.00	3.14	0.57	1.10	13.63	0.00	13.63	4.000	No	Yes	2.00
239	23.90	11.58	100.00	3.16	0.57	1.10	12.18	0.00	12.18	4.000	No	Yes	2.00
240	24.00	10.09	100.00	3.19	0.58	1.10	10.19	0.00	10.19	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
241	24.10	8.71	100.00	3.23	0.59	1.10	9.00	0.00	9.00	4.000	No	Yes	2.00
242	24.20	7.82	100.00	3.28	0.59	1.10	7.87	0.00	7.87	4.000	No	Yes	2.00
243	24.30	7.70	100.00	3.29	0.59	1.09	7.41	0.00	7.41	4.000	No	Yes	2.00
244	24.40	8.15	100.00	3.27	0.59	1.09	8.57	0.00	8.57	4.000	No	Yes	2.00
245	24.50	8.70	100.00	3.24	0.59	1.09	9.22	0.00	9.22	4.000	No	Yes	2.00
246	24.60	8.57	100.00	3.24	0.59	1.09	9.08	0.00	9.08	4.000	No	Yes	2.00
247	24.70	7.74	100.00	3.28	0.59	1.09	8.11	0.00	8.11	4.000	No	Yes	2.00
248	24.80	6.79	100.00	3.33	0.60	1.09	6.65	0.00	6.65	4.000	No	Yes	2.00
249	24.90	6.15	100.00	3.37	0.60	1.09	6.12	0.00	6.12	4.000	No	Yes	2.00
250	25.00	5.98	100.00	3.37	0.60	1.08	6.12	0.00	6.12	4.000	No	Yes	2.00
251	25.10	6.01	100.00	3.37	0.60	1.08	6.11	0.00	6.11	4.000	No	Yes	2.00
252	25.20	6.34	100.00	3.36	0.60	1.08	6.20	0.00	6.20	4.000	No	Yes	2.00
253	25.30	7.03	100.00	3.32	0.59	1.08	7.09	0.00	7.09	4.000	No	Yes	2.00
254	25.40	7.80	100.00	3.29	0.59	1.08	8.21	0.00	8.21	4.000	No	Yes	2.00
255	25.50	8.27	100.00	3.27	0.59	1.07	8.49	0.00	8.49	4.000	No	Yes	2.00
256	25.60	8.37	100.00	3.28	0.59	1.07	8.48	0.00	8.48	4.000	No	Yes	2.00
257	25.70	8.13	100.00	3.30	0.59	1.07	8.47	0.00	8.47	4.000	No	Yes	2.00
258	25.80	7.53	100.00	3.35	0.59	1.07	7.73	0.00	7.73	4.000	No	Yes	2.00
259	25.90	7.11	100.00	3.38	0.60	1.07	6.64	0.00	6.64	4.000	No	Yes	2.00
260	26.00	7.40	100.00	3.38	0.59	1.07	7.16	0.00	7.16	4.000	No	Yes	2.00
261	26.10	8.52	100.00	3.32	0.59	1.07	8.58	0.00	8.58	4.000	No	Yes	2.00
262	26.20	9.73	100.00	3.27	0.58	1.06	9.97	0.00	9.97	4.000	No	Yes	2.00
263	26.30	10.47	100.00	3.24	0.58	1.06	10.75	0.00	10.75	4.000	No	Yes	2.00
264	26.40	10.75	100.00	3.24	0.58	1.06	10.77	0.00	10.77	4.000	No	Yes	2.00
265	26.50	10.76	100.00	3.24	0.58	1.06	10.75	0.00	10.75	4.000	No	Yes	2.00
266	26.60	10.76	100.00	3.25	0.58	1.06	10.73	0.00	10.73	4.000	No	Yes	2.00
267	26.70	10.76	100.00	3.26	0.58	1.05	10.72	0.00	10.72	4.000	No	Yes	2.00
268	26.80	10.76	100.00	3.26	0.58	1.05	10.70	0.00	10.70	4.000	No	Yes	2.00
269	26.90	10.76	100.00	3.27	0.58	1.05	10.68	0.00	10.68	4.000	No	Yes	2.00
270	27.00	10.76	100.00	3.27	0.58	1.05	10.67	0.00	10.67	4.000	No	Yes	2.00
271	27.10	10.76	100.00	3.27	0.58	1.05	10.65	0.00	10.65	4.000	No	Yes	2.00
272	27.20	10.76	100.00	3.27	0.58	1.05	10.64	0.00	10.64	4.000	No	Yes	2.00
273	27.30	10.62	100.00	3.28	0.58	1.05	10.62	0.00	10.62	4.000	No	Yes	2.00
274	27.40	10.09	100.00	3.29	0.58	1.04	10.20	0.00	10.20	4.000	No	Yes	2.00
275	27.50	9.29	100.00	3.32	0.59	1.04	9.00	0.00	9.00	4.000	No	Yes	2.00
276	27.60	8.63	100.00	3.33	0.59	1.04	8.24	0.00	8.24	4.000	No	Yes	2.00
277	27.70	8.37	100.00	3.33	0.59	1.04	8.22	0.00	8.22	4.000	No	Yes	2.00
278	27.80	8.37	100.00	3.32	0.59	1.04	8.21	0.00	8.21	4.000	No	Yes	2.00
279	27.90	8.49	100.00	3.31	0.59	1.04	8.20	0.00	8.20	4.000	No	Yes	2.00
280	28.00	8.69	100.00	3.30	0.59	1.04	8.55	0.00	8.55	4.000	No	Yes	2.00
281	28.10	8.89	100.00	3.29	0.59	1.03	8.76	0.00	8.76	4.000	No	Yes	2.00
282	28.20	9.37	100.00	3.27	0.59	1.03	8.74	0.00	8.74	4.000	No	Yes	2.00
283	28.30	9.97	100.00	3.23	0.58	1.03	9.92	0.00	9.92	4.000	No	Yes	2.00
284	28.40	10.57	100.00	3.20	0.58	1.03	10.46	0.00	10.46	4.000	No	Yes	2.00
285	28.50	10.98	100.00	3.18	0.58	1.03	10.44	0.00	10.44	4.000	No	Yes	2.00
286	28.60	11.67	100.00	3.16	0.58	1.03	11.07	0.00	11.07	4.000	No	Yes	2.00
287	28.70	12.47	100.00	3.13	0.57	1.02	12.42	0.00	12.42	4.000	No	Yes	2.00
288	28.80	13.04	100.00	3.11	0.57	1.02	12.71	0.00	12.71	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
289	28.90	13.15	100.00	3.11	0.57	1.02	12.69	0.00	12.69	4.000	No	Yes	2.00
290	29.00	13.15	100.00	3.12	0.57	1.02	12.67	0.00	12.67	4.000	No	Yes	2.00
291	29.10	13.15	100.00	3.12	0.57	1.02	12.65	0.00	12.65	4.000	No	Yes	2.00
292	29.20	13.15	100.00	3.12	0.57	1.02	12.63	0.00	12.63	4.000	No	Yes	2.00
293	29.30	12.81	100.00	3.12	0.57	1.02	12.62	0.00	12.62	4.000	No	Yes	2.00
294	29.40	12.02	100.00	3.13	0.58	1.01	11.63	0.00	11.63	4.000	No	Yes	2.00
295	29.50	11.23	100.00	3.15	0.58	1.01	10.32	0.00	10.32	4.000	No	Yes	2.00
296	29.60	10.91	100.00	3.16	0.58	1.01	10.28	0.00	10.28	4.000	No	Yes	2.00
297	29.70	11.76	100.00	3.12	0.58	1.01	10.69	0.00	10.69	4.000	No	Yes	2.00
298	29.80	12.59	100.00	3.10	0.57	1.01	12.69	0.00	12.69	4.000	No	Yes	2.00
299	29.90	13.04	100.00	3.09	0.57	1.01	12.61	0.00	12.61	4.000	No	Yes	2.00
300	30.00	13.53	100.00	3.09	0.57	1.01	11.93	0.00	11.93	4.000	No	Yes	2.00
301	30.10	14.07	100.00	3.07	0.57	1.00	14.03	0.00	14.03	4.000	No	Yes	2.00
302	30.20	14.43	100.00	3.06	0.57	1.00	14.11	0.00	14.11	4.000	No	Yes	2.00
303	30.30	13.96	100.00	3.08	0.57	1.00	12.90	0.00	12.90	4.000	No	Yes	2.00
304	30.40	13.58	100.00	3.09	0.57	1.00	12.63	0.00	12.63	4.000	No	Yes	2.00
305	30.50	13.33	100.00	3.10	0.57	1.00	12.98	0.00	12.98	4.000	No	Yes	2.00
306	30.60	12.70	100.00	3.13	0.57	1.00	12.14	0.00	12.14	4.000	No	Yes	2.00
307	30.70	12.12	100.00	3.17	0.58	1.00	10.82	0.00	10.82	4.000	No	Yes	2.00
308	30.80	13.30	100.00	3.15	0.58	1.00	11.26	0.00	11.26	4.000	No	Yes	2.00
309	30.90	17.68	100.00	3.02	0.56	0.99	15.43	0.00	15.43	4.000	No	Yes	2.00
310	31.00	25.04	91.74	2.86	0.54	0.99	23.09	0.00	23.09	4.000	Yes	Yes	2.00
311	31.10	33.65	79.12	2.70	0.51	0.99	31.90	0.00	31.90	4.000	Yes	Yes	2.00
312	31.20	41.52	68.62	2.57	0.50	0.99	39.56	61.86	101.42	4.000	Yes	No	2.00
313	31.30	47.08	61.74	2.48	0.48	0.99	45.11	61.84	106.95	4.000	Yes	No	2.00
314	31.40	50.34	58.71	2.45	0.48	0.99	47.38	61.62	109.00	4.000	Yes	No	2.00
315	31.50	51.88	58.08	2.44	0.48	0.99	48.53	61.75	110.28	0.153	No	No	0.17
316	31.60	53.14	57.16	2.43	0.47	0.99	49.24	61.66	110.91	0.154	No	No	0.17
317	31.70	54.44	55.51	2.41	0.47	0.98	50.73	61.53	112.26	0.156	No	No	0.17
318	31.80	55.69	54.21	2.39	0.47	0.98	51.97	61.42	113.39	0.158	No	No	0.17
319	31.90	56.99	53.32	2.38	0.47	0.98	52.56	61.25	113.81	0.159	No	No	0.17
320	32.00	58.46	51.98	2.36	0.47	0.98	54.16	61.17	115.33	0.162	No	No	0.18
321	32.10	59.74	50.09	2.34	0.46	0.98	55.88	60.85	116.73	0.164	No	No	0.18
322	32.20	60.86	48.34	2.32	0.46	0.98	55.91	60.08	115.98	0.163	No	No	0.18
323	32.30	62.07	47.72	2.31	0.46	0.98	57.08	60.09	117.16	0.165	No	No	0.18
324	32.40	62.52	48.84	2.32	0.46	0.98	59.04	61.13	120.17	4.000	Yes	No	2.00
325	32.50	59.72	52.85	2.37	0.46	0.98	56.96	62.26	119.22	4.000	Yes	No	2.00
326	32.60	52.72	60.19	2.46	0.47	0.97	49.09	62.53	111.63	4.000	Yes	No	2.00
327	32.70	42.27	70.87	2.60	0.49	0.97	39.43	62.27	101.70	4.000	Yes	No	2.00
328	32.80	31.38	83.74	2.76	0.52	0.97	27.83	0.00	27.83	4.000	Yes	Yes	2.00
329	32.90	22.36	97.52	2.93	0.55	0.97	18.89	0.00	18.89	4.000	Yes	Yes	2.00
330	33.00	16.47	100.00	3.08	0.57	0.96	14.48	0.00	14.48	4.000	No	Yes	2.00
331	33.10	13.22	100.00	3.17	0.58	0.96	11.59	0.00	11.59	4.000	No	Yes	2.00
332	33.20	11.88	100.00	3.20	0.58	0.96	9.93	0.00	9.93	4.000	No	Yes	2.00
333	33.30	11.95	100.00	3.17	0.58	0.96	10.78	0.00	10.78	4.000	No	Yes	2.00
334	33.40	11.78	100.00	3.16	0.58	0.96	11.73	0.00	11.73	4.000	No	Yes	2.00
335	33.50	11.11	100.00	3.18	0.58	0.96	9.43	0.00	9.43	4.000	No	Yes	2.00
336	33.60	11.31	100.00	3.18	0.59	0.95	8.93	0.00	8.93	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
337	33.70	12.29	100.00	3.15	0.57	0.95	12.23	0.00	12.23	4.000	No	Yes	2.00
338	33.80	13.31	100.00	3.12	0.57	0.95	12.06	0.00	12.06	4.000	No	Yes	2.00
339	33.90	13.96	100.00	3.10	0.58	0.95	11.64	0.00	11.64	4.000	No	Yes	2.00
340	34.00	14.67	100.00	3.08	0.57	0.95	13.96	0.00	13.96	4.000	No	Yes	2.00
341	34.10	15.54	100.00	3.06	0.57	0.95	13.94	0.00	13.94	4.000	No	Yes	2.00
342	34.20	15.54	100.00	3.08	0.57	0.95	13.92	0.00	13.92	4.000	No	Yes	2.00
343	34.30	16.11	100.00	3.09	0.57	0.95	13.91	0.00	13.91	4.000	No	Yes	2.00
344	34.40	19.78	100.00	3.03	0.56	0.95	15.42	0.00	15.42	4.000	No	Yes	2.00
345	34.50	27.81	94.92	2.90	0.53	0.95	23.79	0.00	23.79	4.000	Yes	Yes	2.00
346	34.60	38.35	82.93	2.75	0.50	0.95	35.53	0.00	35.53	4.000	Yes	Yes	2.00
347	34.70	49.92	70.89	2.60	0.48	0.95	43.87	63.58	107.45	4.000	Yes	No	2.00
348	34.80	62.64	60.04	2.46	0.46	0.95	55.10	64.18	119.28	4.000	Yes	No	2.00
349	34.90	79.13	50.97	2.35	0.43	0.95	70.07	65.00	135.07	4.000	Yes	No	2.00
350	35.00	99.48	42.81	2.25	0.40	0.96	88.83	65.38	154.21	4.000	Yes	No	2.00
351	35.10	120.93	35.07	2.15	0.36	0.96	110.76	63.99	174.75	4.000	Yes	No	2.00
352	35.20	140.29	27.80	2.06	0.35	0.96	128.84	57.88	186.72	4.000	Yes	No	2.00
353	35.30	155.97	21.86	1.99	0.34	0.96	141.76	47.63	189.39	4.000	Yes	No	2.00
354	35.40	167.22	18.30	1.94	0.34	0.96	153.36	38.98	192.34	4.000	Yes	No	2.00
355	35.50	172.04	17.65	1.93	0.33	0.96	159.25	37.54	196.79	1.586	No	No	1.75
356	35.60	169.35	19.33	1.95	0.33	0.96	154.63	42.37	197.01	1.605	No	No	1.77
357	35.70	162.62	21.56	1.98	0.34	0.96	145.64	47.45	193.09	1.309	No	No	1.44
358	35.80	153.39	23.69	2.01	0.34	0.95	140.44	51.82	192.26	4.000	Yes	No	2.00
359	35.90	142.33	26.25	2.04	0.35	0.95	128.89	55.10	183.99	4.000	Yes	No	2.00
360	36.00	127.98	30.64	2.10	0.37	0.95	114.93	59.49	174.42	4.000	Yes	No	2.00
361	36.10	111.52	37.43	2.18	0.38	0.95	100.73	64.02	164.75	4.000	Yes	No	2.00
362	36.20	94.75	45.89	2.29	0.40	0.94	83.55	65.97	149.52	4.000	Yes	No	2.00
363	36.30	81.09	54.14	2.39	0.43	0.94	68.93	66.00	134.94	4.000	Yes	No	2.00
364	36.40	77.71	57.71	2.43	0.44	0.94	63.29	65.73	129.02	4.000	Yes	No	2.00
365	36.50	89.74	53.02	2.38	0.42	0.94	74.11	66.96	141.07	4.000	Yes	No	2.00
366	36.60	116.69	42.56	2.24	0.37	0.94	101.45	68.34	169.79	4.000	Yes	No	2.00
367	36.70	151.21	31.04	2.10	0.33	0.95	136.68	64.55	201.23	4.000	Yes	No	2.00
368	36.80	183.51	22.03	1.99	0.30	0.95	168.40	52.14	220.54	4.000	Yes	No	2.00
369	36.90	207.83	16.72	1.92	0.30	0.95	189.61	37.43	227.05	4.000	Yes	No	2.00
370	37.00	225.84	14.57	1.89	0.29	0.95	202.87	29.87	232.74	4.000	No	No	2.00
371	37.10	236.91	13.96	1.89	0.27	0.95	217.54	28.28	245.82	4.000	No	No	2.00
372	37.20	240.81	13.90	1.89	0.27	0.95	219.88	28.19	248.07	4.000	No	No	2.00
373	37.30	235.84	14.41	1.89	0.28	0.95	213.35	30.01	243.36	4.000	No	No	2.00
374	37.40	225.38	15.48	1.91	0.28	0.95	203.23	33.76	236.99	4.000	No	No	2.00
375	37.50	213.17	16.71	1.92	0.29	0.95	190.33	37.47	227.80	4.000	No	No	2.00
376	37.60	201.83	17.60	1.93	0.31	0.94	178.99	39.57	218.56	4.000	No	No	2.00
377	37.70	194.32	17.58	1.93	0.32	0.94	171.20	38.61	209.82	3.446	No	No	2.00
378	37.80	192.34	16.74	1.92	0.32	0.94	168.78	35.36	204.14	2.409	No	No	2.00
379	37.90	195.72	16.04	1.91	0.32	0.94	172.75	33.17	205.92	2.685	No	No	2.00
380	38.00	202.49	16.32	1.92	0.31	0.94	179.98	34.95	214.93	4.000	No	No	2.00
381	38.10	209.96	17.54	1.93	0.29	0.94	187.41	40.28	227.69	4.000	No	No	2.00
382	38.20	216.55	19.15	1.95	0.28	0.95	193.80	46.83	240.63	4.000	No	No	2.00
383	38.30	221.69	20.54	1.97	0.27	0.95	198.79	52.12	250.91	4.000	No	No	2.00
384	38.40	225.49	21.41	1.98	0.26	0.95	201.95	55.34	257.29	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
385	38.50	228.03	22.02	1.99	0.26	0.95	204.14	57.54	261.68	4.000	No	No	2.00
386	38.60	228.61	22.58	1.99	0.26	0.95	205.27	59.38	264.65	4.000	No	No	2.00
387	38.70	226.29	23.40	2.00	0.26	0.94	203.06	61.35	264.41	4.000	No	No	2.00
388	38.80	221.32	24.39	2.02	0.26	0.94	197.48	63.07	260.54	4.000	No	No	2.00
389	38.90	215.06	25.43	2.03	0.26	0.94	191.52	64.60	256.12	4.000	No	No	2.00
390	39.00	208.89	26.37	2.04	0.27	0.94	185.79	65.73	251.52	4.000	No	No	2.00
391	39.10	203.92	26.87	2.05	0.27	0.94	180.21	65.80	246.01	4.000	No	No	2.00
392	39.20	201.00	26.89	2.05	0.28	0.94	177.32	65.28	242.60	4.000	No	No	2.00
393	39.30	200.94	26.30	2.04	0.28	0.94	177.10	63.99	241.09	4.000	No	No	2.00
394	39.40	203.86	25.33	2.03	0.28	0.94	179.46	62.24	241.70	4.000	No	No	2.00
395	39.50	209.63	24.10	2.01	0.27	0.94	184.81	60.19	245.00	4.000	No	No	2.00
396	39.60	217.99	22.78	2.00	0.27	0.94	192.50	57.94	250.44	4.000	No	No	2.00
397	39.70	228.76	21.55	1.98	0.26	0.94	201.89	55.77	257.66	4.000	No	No	2.00
398	39.80	241.19	20.64	1.97	0.26	0.94	213.46	54.51	267.96	4.000	No	No	2.00
399	39.90	254.27	20.01	1.96	0.26	0.94	225.25	53.96	279.21	4.000	No	No	2.00
400	40.00	265.96	19.67	1.96	0.26	0.94	236.12	54.18	290.30	4.000	No	No	2.00
401	40.10	276.78	19.16	1.95	0.26	0.94	243.97	53.25	297.22	4.000	No	No	2.00
402	40.20	286.88	18.08	1.94	0.26	0.93	253.42	49.98	303.41	4.000	No	No	2.00
403	40.30	297.01	16.24	1.92	0.26	0.93	262.33	42.68	305.02	4.000	No	No	2.00
404	40.40	305.93	14.09	1.89	0.26	0.93	270.24	32.80	303.04	4.000	No	No	2.00
405	40.50	313.36	12.28	1.87	0.26	0.93	276.47	23.84	300.31	4.000	No	No	2.00
406	40.60	319.25	11.29	1.85	0.26	0.93	281.39	18.99	300.38	4.000	No	No	2.00
407	40.70	323.81	10.98	1.85	0.26	0.93	285.22	17.61	302.84	4.000	No	No	2.00
408	40.80	326.58	10.87	1.85	0.26	0.93	287.88	17.14	305.03	4.000	No	No	2.00
409	40.90	326.95	10.64	1.85	0.26	0.93	288.10	16.04	304.14	4.000	No	No	2.00
410	41.00	324.52	10.51	1.84	0.26	0.93	285.59	15.30	300.89	4.000	No	No	2.00
411	41.10	319.51	11.05	1.85	0.26	0.93	280.87	17.76	298.63	4.000	No	No	2.00
412	41.20	312.79	12.30	1.87	0.26	0.93	274.33	23.84	298.17	4.000	No	No	2.00
413	41.30	304.61	14.15	1.89	0.26	0.93	267.32	32.86	300.18	4.000	No	No	2.00
414	41.40	293.60	16.21	1.92	0.26	0.93	258.80	42.23	301.02	4.000	No	No	2.00
415	41.50	278.40	18.33	1.94	0.26	0.93	244.86	50.00	294.86	4.000	No	No	2.00
416	41.60	258.94	20.38	1.97	0.26	0.93	226.89	55.50	282.39	4.000	No	No	2.00
417	41.70	237.94	22.20	1.99	0.26	0.92	207.26	58.56	265.82	4.000	No	No	2.00
418	41.80	218.97	23.71	2.01	0.27	0.92	189.05	59.91	248.96	4.000	No	No	2.00
419	41.90	200.61	25.81	2.04	0.28	0.92	175.87	62.69	238.57	4.000	No	No	2.00
420	42.00	180.78	29.74	2.08	0.30	0.91	157.14	66.72	223.86	4.000	No	No	2.00
421	42.10	157.20	36.23	2.17	0.32	0.91	134.73	70.68	205.41	2.601	No	No	2.00
422	42.20	132.67	43.78	2.26	0.35	0.90	111.73	71.79	183.52	0.841	No	No	0.91
423	42.30	112.50	49.95	2.34	0.39	0.89	90.97	70.08	161.05	0.383	No	No	0.41
424	42.40	103.27	51.43	2.36	0.41	0.88	80.62	68.02	148.64	0.280	No	No	0.30
425	42.50	106.36	47.44	2.31	0.40	0.88	86.86	67.69	154.55	0.322	No	No	0.35
426	42.60	116.27	40.96	2.22	0.38	0.89	98.68	66.48	165.17	0.432	No	No	0.47
427	42.70	123.96	35.75	2.16	0.37	0.89	106.18	63.66	169.84	0.501	No	No	0.54
428	42.80	125.54	33.66	2.13	0.38	0.89	106.51	61.49	168.00	0.472	No	No	0.51
429	42.90	120.85	35.38	2.15	0.38	0.88	102.38	62.42	164.79	4.000	Yes	No	2.00
430	43.00	111.91	40.51	2.22	0.39	0.88	93.63	64.91	158.54	4.000	Yes	No	2.00
431	43.10	101.40	47.50	2.31	0.40	0.88	83.05	66.73	149.78	4.000	Yes	No	2.00
432	43.20	92.75	53.95	2.39	0.42	0.87	74.95	67.56	142.51	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
433	43.30	88.83	57.05	2.43	0.42	0.87	71.08	67.67	138.75	4.000	Yes	No	2.00
434	43.40	90.15	56.00	2.41	0.42	0.87	72.74	67.74	140.49	0.237	No	No	0.25
435	43.50	94.42	52.48	2.37	0.41	0.87	78.12	67.81	145.93	0.264	No	No	0.28
436	43.60	98.83	49.01	2.33	0.41	0.87	81.87	67.21	149.07	0.283	No	No	0.30
437	43.70	101.21	47.20	2.30	0.40	0.87	83.85	66.78	150.63	0.293	No	No	0.32
438	43.80	101.76	47.11	2.30	0.40	0.87	83.99	66.76	150.75	0.294	No	No	0.32
439	43.90	101.61	47.95	2.31	0.40	0.87	83.05	66.97	150.02	0.289	No	No	0.31
440	44.00	101.41	49.13	2.33	0.40	0.87	83.27	67.63	150.90	0.295	No	No	0.32
441	44.10	101.33	50.55	2.34	0.40	0.87	83.31	68.33	151.64	0.300	No	No	0.32
442	44.20	101.20	52.26	2.37	0.40	0.87	82.70	68.95	151.65	0.300	No	No	0.32
443	44.30	102.65	53.40	2.38	0.40	0.87	82.80	69.47	152.27	0.305	No	No	0.33
444	44.40	107.15	52.56	2.37	0.39	0.87	86.88	70.21	157.09	0.344	No	No	0.37
445	44.50	115.17	48.94	2.32	0.38	0.87	94.20	70.41	164.61	0.425	No	No	0.46
446	44.60	124.33	43.66	2.26	0.37	0.87	103.45	69.62	173.07	0.560	No	No	0.60
447	44.70	131.80	38.85	2.20	0.36	0.88	110.42	67.58	178.00	0.672	No	No	0.72
448	44.80	135.88	36.32	2.17	0.36	0.88	113.26	65.86	179.12	0.702	No	No	0.76
449	44.90	137.36	36.27	2.17	0.36	0.88	113.67	65.90	179.57	0.714	No	No	0.77
450	45.00	138.06	37.30	2.18	0.36	0.88	114.02	67.00	181.03	0.758	No	No	0.82
451	45.10	138.23	38.40	2.19	0.35	0.88	115.00	68.26	183.26	0.831	No	No	0.90
452	45.20	137.03	39.50	2.21	0.35	0.88	114.05	69.01	183.07	0.825	No	No	0.89
453	45.30	133.73	41.08	2.23	0.36	0.87	110.74	69.52	180.26	0.735	No	No	0.79
454	45.40	129.36	43.04	2.25	0.36	0.87	106.10	69.84	175.94	0.621	No	No	0.67
455	45.50	126.45	44.27	2.27	0.37	0.87	102.30	69.74	172.04	0.540	No	No	0.58
456	45.60	127.21	43.46	2.26	0.37	0.87	102.81	69.32	172.13	0.542	No	No	0.58
457	45.70	131.34	40.49	2.22	0.36	0.87	107.72	68.31	176.03	0.624	No	No	0.67
458	45.80	136.70	36.34	2.17	0.36	0.87	112.64	65.74	178.37	0.682	No	No	0.73
459	45.90	140.90	32.54	2.12	0.36	0.87	116.16	62.24	178.40	0.682	No	No	0.73
460	46.00	142.26	30.89	2.10	0.36	0.87	117.99	60.47	178.45	0.684	No	No	0.74
461	46.10	140.88	31.88	2.11	0.36	0.87	115.64	61.30	176.94	0.645	No	No	0.69
462	46.20	137.87	34.55	2.14	0.36	0.86	112.31	63.77	176.08	0.625	No	No	0.67
463	46.30	135.03	37.02	2.18	0.36	0.86	110.12	65.83	175.95	0.622	No	No	0.67
464	46.40	133.22	38.37	2.19	0.37	0.86	108.23	66.64	174.88	0.598	No	No	0.64
465	46.50	132.83	39.08	2.20	0.37	0.86	107.55	67.10	174.65	0.593	No	No	0.64
466	46.60	133.78	40.05	2.21	0.36	0.86	109.02	68.27	177.29	0.654	No	No	0.70
467	46.70	134.60	41.86	2.24	0.36	0.86	110.71	70.12	180.84	4.000	Yes	No	2.00
468	46.80	132.80	44.64	2.27	0.35	0.86	109.78	71.88	181.66	4.000	Yes	No	2.00
469	46.90	125.89	48.43	2.32	0.36	0.86	104.34	72.80	177.14	4.000	Yes	No	2.00
470	47.00	115.97	52.89	2.37	0.38	0.85	92.61	71.90	164.50	4.000	Yes	No	2.00
471	47.10	104.67	57.25	2.43	0.40	0.85	83.83	71.26	155.09	4.000	Yes	No	2.00
472	47.20	98.78	59.20	2.45	0.41	0.84	74.96	69.47	144.43	0.256	No	No	0.28
473	47.30	98.47	58.46	2.44	0.41	0.84	77.26	69.86	147.13	0.271	No	No	0.29
474	47.40	96.95	58.46	2.44	0.40	0.84	82.82	71.42	154.24	0.320	No	No	0.34
475	47.50	88.26	62.12	2.49	0.42	0.84	70.93	69.25	140.18	0.235	No	No	0.25
476	47.60	70.99	70.73	2.60	0.45	0.82	55.34	66.89	122.24	0.177	No	No	0.19
477	47.70	54.66	80.89	2.72	0.49	0.81	39.74	0.00	39.74	4.000	No	Yes	2.00
478	47.80	43.11	89.34	2.83	0.51	0.80	30.91	0.00	30.91	4.000	No	Yes	2.00
479	47.90	37.26	93.61	2.88	0.52	0.80	27.45	0.00	27.45	4.000	No	Yes	2.00
480	48.00	35.46	94.35	2.89	0.53	0.79	25.83	0.00	25.83	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
481	48.10	35.37	94.56	2.89	0.53	0.79	26.61	0.00	26.61	4.000	No	Yes	2.00
482	48.20	36.65	95.38	2.90	0.52	0.79	27.17	0.00	27.17	4.000	No	Yes	2.00
483	48.30	39.52	96.20	2.91	0.52	0.80	28.73	0.00	28.73	4.000	No	Yes	2.00
484	48.40	43.87	95.21	2.90	0.50	0.80	33.27	0.00	33.27	4.000	No	Yes	2.00
485	48.50	47.02	93.62	2.88	0.49	0.80	37.34	0.00	37.34	4.000	No	Yes	2.00
486	48.60	46.83	93.17	2.88	0.50	0.80	36.05	0.00	36.05	4.000	No	Yes	2.00
487	48.70	43.44	94.56	2.89	0.51	0.80	32.72	0.00	32.72	4.000	No	Yes	2.00
488	48.80	39.99	96.41	2.92	0.52	0.79	29.23	0.00	29.23	4.000	No	Yes	2.00
489	48.90	37.97	97.37	2.93	0.52	0.79	27.86	0.00	27.86	4.000	No	Yes	2.00
490	49.00	37.11	97.45	2.93	0.52	0.79	27.91	0.00	27.91	4.000	No	Yes	2.00
491	49.10	36.51	97.47	2.93	0.52	0.79	27.14	0.00	27.14	4.000	No	Yes	2.00
492	49.20	35.49	97.99	2.94	0.53	0.79	26.39	0.00	26.39	4.000	No	Yes	2.00
493	49.30	33.74	99.31	2.95	0.53	0.78	25.48	0.00	25.48	4.000	No	Yes	2.00
494	49.40	30.37	100.00	2.99	0.54	0.78	23.02	0.00	23.02	4.000	No	Yes	2.00
495	49.50	26.08	100.00	3.05	0.55	0.77	18.61	0.00	18.61	4.000	No	Yes	2.00
496	49.60	22.32	100.00	3.11	0.56	0.77	15.67	0.00	15.67	4.000	No	Yes	2.00
497	49.70	20.21	100.00	3.14	0.57	0.77	14.46	0.00	14.46	4.000	No	Yes	2.00
498	49.80	19.41	100.00	3.15	0.57	0.77	13.86	0.00	13.86	4.000	No	Yes	2.00

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q_t :	Total cone resistance
FC:	Fines content (%)
I_c :	Soil behavior type index
m:	Stress exponent
C_N :	Overburden correction factor
q_{c1N} :	Normalized and adjusted cone resistance
Δq_{c1N} :	Cone resistance correction factor due to fines
$q_{c1N,cs}$:	Normalized and adjusted cone resistance
CRR _{7.5} :	Cyclic resistance ratio for $M_w=7.5$
FS:	Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
0.10	2.00	0.00	0.00	0.10	0.00	0.20	2.00	0.00	0.00	0.10	0.00
0.30	2.00	0.00	0.00	0.10	0.00	0.40	2.00	0.00	0.00	0.10	0.00
0.50	2.00	0.00	0.00	0.10	0.00	0.60	2.00	0.00	0.00	0.10	0.00
0.70	2.00	0.00	0.00	0.10	0.00	0.80	2.00	0.00	0.00	0.10	0.00
0.90	2.00	0.00	0.00	0.10	0.00	1.00	2.00	0.00	0.00	0.10	0.00
1.10	2.00	0.00	0.00	0.10	0.00	1.20	2.00	0.00	0.00	0.10	0.00
1.30	2.00	0.00	0.00	0.10	0.00	1.40	2.00	0.00	0.00	0.10	0.00
1.50	2.00	0.00	0.00	0.10	0.00	1.60	2.00	0.00	0.00	0.10	0.00
1.70	2.00	0.00	0.00	0.10	0.00	1.80	2.00	0.00	0.00	0.10	0.00
1.90	2.00	0.00	0.00	0.10	0.00	2.00	2.00	0.00	0.00	0.10	0.00
2.10	2.00	0.00	0.00	0.10	0.00	2.20	2.00	0.00	0.00	0.10	0.00
2.30	2.00	0.00	0.00	0.10	0.00	2.40	2.00	0.00	0.00	0.10	0.00
2.50	2.00	0.00	0.00	0.10	0.00	2.60	2.00	0.00	0.00	0.10	0.00
2.70	2.00	0.00	0.00	0.10	0.00	2.80	2.00	0.00	0.00	0.10	0.00
2.90	2.00	0.00	0.00	0.10	0.00	3.00	2.00	0.00	0.00	0.10	0.00
3.10	2.00	0.00	0.00	0.10	0.00	3.20	2.00	0.00	0.00	0.10	0.00
3.30	2.00	0.00	0.00	0.10	0.00	3.40	2.00	0.00	0.00	0.10	0.00
3.50	2.00	0.00	0.00	0.10	0.00	3.60	2.00	0.00	0.00	0.10	0.00
3.70	2.00	0.00	0.00	0.10	0.00	3.80	2.00	0.00	0.00	0.10	0.00
3.90	2.00	0.00	0.00	0.10	0.00	4.00	2.00	0.00	0.00	0.10	0.00
4.10	2.00	0.00	0.00	0.10	0.00	4.20	2.00	0.00	0.00	0.10	0.00
4.30	2.00	0.00	0.00	0.10	0.00	4.40	2.00	0.00	0.00	0.10	0.00
4.50	2.00	0.00	0.00	0.10	0.00	4.60	2.00	0.00	0.00	0.10	0.00
4.70	2.00	0.00	0.00	0.10	0.00	4.80	2.00	0.00	0.00	0.10	0.00
4.90	2.00	0.00	0.00	0.10	0.00	5.00	2.00	0.00	0.00	0.10	0.00
5.10	2.00	0.00	0.00	0.10	0.00	5.20	2.00	0.00	0.00	0.10	0.00
5.30	2.00	0.00	0.00	0.10	0.00	5.40	2.00	0.00	0.00	0.10	0.00
5.50	2.00	0.00	0.00	0.10	0.00	5.60	2.00	0.00	0.00	0.10	0.00
5.70	2.00	0.00	0.00	0.10	0.00	5.80	2.00	0.00	0.00	0.10	0.00
5.90	2.00	0.00	0.00	0.10	0.00	6.00	2.00	0.00	0.00	0.10	0.00
6.10	2.00	0.00	0.00	0.10	0.00	6.20	2.00	0.00	0.00	0.10	0.00
6.30	2.00	0.00	0.00	0.10	0.00	6.40	2.00	0.00	0.00	0.10	0.00
6.50	2.00	0.00	0.00	0.10	0.00	6.60	2.00	0.00	0.00	0.10	0.00
6.70	2.00	0.00	0.00	0.10	0.00	6.80	2.00	0.00	0.00	0.10	0.00
6.90	2.00	0.00	0.00	0.10	0.00	7.00	2.00	0.00	0.00	0.10	0.00
7.10	2.00	0.00	0.00	0.10	0.00	7.20	2.00	0.00	0.00	0.10	0.00
7.30	2.00	0.00	0.00	0.10	0.00	7.40	2.00	0.00	0.00	0.10	0.00
7.50	2.00	0.00	0.00	0.10	0.00	7.60	2.00	0.00	0.00	0.10	0.00
7.70	2.00	0.00	0.00	0.10	0.00	7.80	2.00	0.00	0.00	0.10	0.00
7.90	2.00	0.00	0.00	0.10	0.00	8.00	2.00	0.00	0.00	0.10	0.00
8.10	2.00	0.00	0.00	0.10	0.00	8.20	2.00	0.00	0.00	0.10	0.00
8.30	2.00	0.00	0.00	0.10	0.00	8.40	2.00	0.00	0.00	0.10	0.00
8.50	2.00	0.00	0.00	0.10	0.00	8.60	2.00	0.00	0.00	0.10	0.00
8.70	2.00	0.00	0.00	0.10	0.00	8.80	2.00	0.00	0.00	0.10	0.00
8.90	2.00	0.00	0.00	0.10	0.00	9.00	2.00	0.00	0.00	0.10	0.00
9.10	2.00	0.00	0.00	0.10	0.00	9.20	2.00	0.00	0.00	0.10	0.00
9.30	0.21	0.79	0.28	0.10	0.21	9.40	0.20	0.80	0.28	0.10	0.21
9.50	0.20	0.80	0.28	0.10	0.21	9.60	0.20	0.80	0.28	0.10	0.21

:: Liquefaction Potential Index calculation data ::

Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
9.70	0.20	0.80	0.28	0.10	0.21	9.80	0.20	0.80	0.28	0.10	0.21
9.90	0.20	0.80	0.28	0.10	0.21	10.00	0.21	0.79	0.28	0.10	0.20
10.10	0.22	0.78	0.29	0.10	0.20	10.20	0.23	0.77	0.29	0.10	0.20
10.30	0.23	0.77	0.29	0.10	0.20	10.40	0.22	0.78	0.29	0.10	0.20
10.50	0.22	0.78	0.29	0.10	0.20	10.60	0.22	0.78	0.29	0.10	0.20
10.70	0.22	0.78	0.29	0.10	0.20	10.80	0.22	0.78	0.28	0.10	0.20
10.90	0.21	0.79	0.28	0.10	0.20	11.00	2.00	0.00	0.00	0.10	0.00
11.10	2.00	0.00	0.00	0.10	0.00	11.20	2.00	0.00	0.00	0.10	0.00
11.30	2.00	0.00	0.00	0.10	0.00	11.40	2.00	0.00	0.00	0.10	0.00
11.50	2.00	0.00	0.00	0.10	0.00	11.60	2.00	0.00	0.00	0.10	0.00
11.70	2.00	0.00	0.00	0.10	0.00	11.80	2.00	0.00	0.00	0.10	0.00
11.90	2.00	0.00	0.00	0.10	0.00	12.00	2.00	0.00	0.00	0.10	0.00
12.10	2.00	0.00	0.00	0.10	0.00	12.20	2.00	0.00	0.00	0.10	0.00
12.30	2.00	0.00	0.00	0.10	0.00	12.40	0.18	0.82	0.27	0.10	0.20
12.50	0.18	0.82	0.27	0.10	0.20	12.60	0.18	0.82	0.27	0.10	0.20
12.70	0.18	0.82	0.27	0.10	0.20	12.80	2.00	0.00	0.00	0.10	0.00
12.90	2.00	0.00	0.00	0.10	0.00	13.00	2.00	0.00	0.00	0.10	0.00
13.10	2.00	0.00	0.00	0.10	0.00	13.20	2.00	0.00	0.00	0.10	0.00
13.30	2.00	0.00	0.00	0.10	0.00	13.40	2.00	0.00	0.00	0.10	0.00
13.50	2.00	0.00	0.00	0.10	0.00	13.60	2.00	0.00	0.00	0.10	0.00
13.70	2.00	0.00	0.00	0.10	0.00	13.80	2.00	0.00	0.00	0.10	0.00
13.90	2.00	0.00	0.00	0.10	0.00	14.00	2.00	0.00	0.00	0.10	0.00
14.10	2.00	0.00	0.00	0.10	0.00	14.20	2.00	0.00	0.00	0.10	0.00
14.30	2.00	0.00	0.00	0.10	0.00	14.40	2.00	0.00	0.00	0.10	0.00
14.50	2.00	0.00	0.00	0.10	0.00	14.60	2.00	0.00	0.00	0.10	0.00
14.70	2.00	0.00	0.00	0.10	0.00	14.80	2.00	0.00	0.00	0.10	0.00
14.90	2.00	0.00	0.00	0.10	0.00	15.00	2.00	0.00	0.00	0.10	0.00
15.10	2.00	0.00	0.00	0.10	0.00	15.20	2.00	0.00	0.00	0.10	0.00
15.30	2.00	0.00	0.00	0.10	0.00	15.40	2.00	0.00	0.00	0.10	0.00
15.50	2.00	0.00	0.00	0.10	0.00	15.60	2.00	0.00	0.00	0.10	0.00
15.70	2.00	0.00	0.00	0.10	0.00	15.80	2.00	0.00	0.00	0.10	0.00
15.90	2.00	0.00	0.00	0.10	0.00	16.00	2.00	0.00	0.00	0.10	0.00
16.10	2.00	0.00	0.00	0.10	0.00	16.20	2.00	0.00	0.00	0.10	0.00
16.30	2.00	0.00	0.00	0.10	0.00	16.40	2.00	0.00	0.00	0.10	0.00
16.50	2.00	0.00	0.00	0.10	0.00	16.60	2.00	0.00	0.00	0.10	0.00
16.70	2.00	0.00	0.00	0.10	0.00	16.80	2.00	0.00	0.00	0.10	0.00
16.90	2.00	0.00	0.00	0.10	0.00	17.00	2.00	0.00	0.00	0.10	0.00
17.10	2.00	0.00	0.00	0.10	0.00	17.20	2.00	0.00	0.00	0.10	0.00
17.30	2.00	0.00	0.00	0.10	0.00	17.40	2.00	0.00	0.00	0.10	0.00
17.50	2.00	0.00	0.00	0.10	0.00	17.60	2.00	0.00	0.00	0.10	0.00
17.70	2.00	0.00	0.00	0.10	0.00	17.80	2.00	0.00	0.00	0.10	0.00
17.90	2.00	0.00	0.00	0.10	0.00	18.00	2.00	0.00	0.00	0.10	0.00
18.10	2.00	0.00	0.00	0.10	0.00	18.20	2.00	0.00	0.00	0.10	0.00
18.30	2.00	0.00	0.00	0.10	0.00	18.40	2.00	0.00	0.00	0.10	0.00
18.50	2.00	0.00	0.00	0.10	0.00	18.60	2.00	0.00	0.00	0.10	0.00
18.70	2.00	0.00	0.00	0.10	0.00	18.80	2.00	0.00	0.00	0.10	0.00
18.90	2.00	0.00	0.00	0.10	0.00	19.00	2.00	0.00	0.00	0.10	0.00
19.10	2.00	0.00	0.00	0.10	0.00	19.20	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
19.30	2.00	0.00	0.00	0.10	0.00	19.40	2.00	0.00	0.00	0.10	0.00
19.50	2.00	0.00	0.00	0.10	0.00	19.60	2.00	0.00	0.00	0.10	0.00
19.70	2.00	0.00	0.00	0.10	0.00	19.80	2.00	0.00	0.00	0.10	0.00
19.90	2.00	0.00	0.00	0.10	0.00	20.00	2.00	0.00	0.00	0.10	0.00
20.10	2.00	0.00	0.00	0.10	0.00	20.20	2.00	0.00	0.00	0.10	0.00
20.30	2.00	0.00	0.00	0.10	0.00	20.40	2.00	0.00	0.00	0.10	0.00
20.50	2.00	0.00	0.00	0.10	0.00	20.60	2.00	0.00	0.00	0.10	0.00
20.70	2.00	0.00	0.00	0.10	0.00	20.80	2.00	0.00	0.00	0.10	0.00
20.90	2.00	0.00	0.00	0.10	0.00	21.00	2.00	0.00	0.00	0.10	0.00
21.10	2.00	0.00	0.00	0.10	0.00	21.20	2.00	0.00	0.00	0.10	0.00
21.30	2.00	0.00	0.00	0.10	0.00	21.40	2.00	0.00	0.00	0.10	0.00
21.50	2.00	0.00	0.00	0.10	0.00	21.60	2.00	0.00	0.00	0.10	0.00
21.70	2.00	0.00	0.00	0.10	0.00	21.80	2.00	0.00	0.00	0.10	0.00
21.90	2.00	0.00	0.00	0.10	0.00	22.00	2.00	0.00	0.00	0.10	0.00
22.10	2.00	0.00	0.00	0.10	0.00	22.20	2.00	0.00	0.00	0.10	0.00
22.30	2.00	0.00	0.00	0.10	0.00	22.40	2.00	0.00	0.00	0.10	0.00
22.50	2.00	0.00	0.00	0.10	0.00	22.60	2.00	0.00	0.00	0.10	0.00
22.70	2.00	0.00	0.00	0.10	0.00	22.80	0.15	0.85	0.26	0.10	0.17
22.90	0.15	0.85	0.26	0.10	0.17	23.00	0.15	0.85	0.26	0.10	0.17
23.10	2.00	0.00	0.00	0.10	0.00	23.20	2.00	0.00	0.00	0.10	0.00
23.30	2.00	0.00	0.00	0.10	0.00	23.40	2.00	0.00	0.00	0.10	0.00
23.50	2.00	0.00	0.00	0.10	0.00	23.60	2.00	0.00	0.00	0.10	0.00
23.70	2.00	0.00	0.00	0.10	0.00	23.80	2.00	0.00	0.00	0.10	0.00
23.90	2.00	0.00	0.00	0.10	0.00	24.00	2.00	0.00	0.00	0.10	0.00
24.10	2.00	0.00	0.00	0.10	0.00	24.20	2.00	0.00	0.00	0.10	0.00
24.30	2.00	0.00	0.00	0.10	0.00	24.40	2.00	0.00	0.00	0.10	0.00
24.50	2.00	0.00	0.00	0.10	0.00	24.60	2.00	0.00	0.00	0.10	0.00
24.70	2.00	0.00	0.00	0.10	0.00	24.80	2.00	0.00	0.00	0.10	0.00
24.90	2.00	0.00	0.00	0.10	0.00	25.00	2.00	0.00	0.00	0.10	0.00
25.10	2.00	0.00	0.00	0.10	0.00	25.20	2.00	0.00	0.00	0.10	0.00
25.30	2.00	0.00	0.00	0.10	0.00	25.40	2.00	0.00	0.00	0.10	0.00
25.50	2.00	0.00	0.00	0.10	0.00	25.60	2.00	0.00	0.00	0.10	0.00
25.70	2.00	0.00	0.00	0.10	0.00	25.80	2.00	0.00	0.00	0.10	0.00
25.90	2.00	0.00	0.00	0.10	0.00	26.00	2.00	0.00	0.00	0.10	0.00
26.10	2.00	0.00	0.00	0.10	0.00	26.20	2.00	0.00	0.00	0.10	0.00
26.30	2.00	0.00	0.00	0.10	0.00	26.40	2.00	0.00	0.00	0.10	0.00
26.50	2.00	0.00	0.00	0.10	0.00	26.60	2.00	0.00	0.00	0.10	0.00
26.70	2.00	0.00	0.00	0.10	0.00	26.80	2.00	0.00	0.00	0.10	0.00
26.90	2.00	0.00	0.00	0.10	0.00	27.00	2.00	0.00	0.00	0.10	0.00
27.10	2.00	0.00	0.00	0.10	0.00	27.20	2.00	0.00	0.00	0.10	0.00
27.30	2.00	0.00	0.00	0.10	0.00	27.40	2.00	0.00	0.00	0.10	0.00
27.50	2.00	0.00	0.00	0.10	0.00	27.60	2.00	0.00	0.00	0.10	0.00
27.70	2.00	0.00	0.00	0.10	0.00	27.80	2.00	0.00	0.00	0.10	0.00
27.90	2.00	0.00	0.00	0.10	0.00	28.00	2.00	0.00	0.00	0.10	0.00
28.10	2.00	0.00	0.00	0.10	0.00	28.20	2.00	0.00	0.00	0.10	0.00
28.30	2.00	0.00	0.00	0.10	0.00	28.40	2.00	0.00	0.00	0.10	0.00
28.50	2.00	0.00	0.00	0.10	0.00	28.60	2.00	0.00	0.00	0.10	0.00
28.70	2.00	0.00	0.00	0.10	0.00	28.80	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
28.90	2.00	0.00	0.00	0.10	0.00	29.00	2.00	0.00	0.00	0.10	0.00
29.10	2.00	0.00	0.00	0.10	0.00	29.20	2.00	0.00	0.00	0.10	0.00
29.30	2.00	0.00	0.00	0.10	0.00	29.40	2.00	0.00	0.00	0.10	0.00
29.50	2.00	0.00	0.00	0.10	0.00	29.60	2.00	0.00	0.00	0.10	0.00
29.70	2.00	0.00	0.00	0.10	0.00	29.80	2.00	0.00	0.00	0.10	0.00
29.90	2.00	0.00	0.00	0.10	0.00	30.00	2.00	0.00	0.00	0.10	0.00
30.10	2.00	0.00	0.00	0.10	0.00	30.20	2.00	0.00	0.00	0.10	0.00
30.30	2.00	0.00	0.00	0.10	0.00	30.40	2.00	0.00	0.00	0.10	0.00
30.50	2.00	0.00	0.00	0.10	0.00	30.60	2.00	0.00	0.00	0.10	0.00
30.70	2.00	0.00	0.00	0.10	0.00	30.80	2.00	0.00	0.00	0.10	0.00
30.90	2.00	0.00	0.00	0.10	0.00	31.00	2.00	0.00	0.00	0.10	0.00
31.10	2.00	0.00	0.00	0.10	0.00	31.20	2.00	0.00	0.00	0.10	0.00
31.30	2.00	0.00	0.00	0.10	0.00	31.40	2.00	0.00	0.00	0.10	0.00
31.50	0.17	0.83	0.26	0.10	0.13	31.60	0.17	0.83	0.26	0.10	0.13
31.70	0.17	0.83	0.27	0.10	0.13	31.80	0.17	0.83	0.27	0.10	0.13
31.90	0.17	0.83	0.27	0.10	0.13	32.00	0.18	0.82	0.27	0.10	0.13
32.10	0.18	0.82	0.27	0.10	0.13	32.20	0.18	0.82	0.27	0.10	0.13
32.30	0.18	0.82	0.27	0.10	0.13	32.40	2.00	0.00	0.00	0.10	0.00
32.50	2.00	0.00	0.00	0.10	0.00	32.60	2.00	0.00	0.00	0.10	0.00
32.70	2.00	0.00	0.00	0.10	0.00	32.80	2.00	0.00	0.00	0.10	0.00
32.90	2.00	0.00	0.00	0.10	0.00	33.00	2.00	0.00	0.00	0.10	0.00
33.10	2.00	0.00	0.00	0.10	0.00	33.20	2.00	0.00	0.00	0.10	0.00
33.30	2.00	0.00	0.00	0.10	0.00	33.40	2.00	0.00	0.00	0.10	0.00
33.50	2.00	0.00	0.00	0.10	0.00	33.60	2.00	0.00	0.00	0.10	0.00
33.70	2.00	0.00	0.00	0.10	0.00	33.80	2.00	0.00	0.00	0.10	0.00
33.90	2.00	0.00	0.00	0.10	0.00	34.00	2.00	0.00	0.00	0.10	0.00
34.10	2.00	0.00	0.00	0.10	0.00	34.20	2.00	0.00	0.00	0.10	0.00
34.30	2.00	0.00	0.00	0.10	0.00	34.40	2.00	0.00	0.00	0.10	0.00
34.50	2.00	0.00	0.00	0.10	0.00	34.60	2.00	0.00	0.00	0.10	0.00
34.70	2.00	0.00	0.00	0.10	0.00	34.80	2.00	0.00	0.00	0.10	0.00
34.90	2.00	0.00	0.00	0.10	0.00	35.00	2.00	0.00	0.00	0.10	0.00
35.10	2.00	0.00	0.00	0.10	0.00	35.20	2.00	0.00	0.00	0.10	0.00
35.30	2.00	0.00	0.00	0.10	0.00	35.40	2.00	0.00	0.00	0.10	0.00
35.50	1.75	0.00	0.00	0.10	0.00	35.60	1.77	0.00	0.00	0.10	0.00
35.70	1.44	0.00	0.00	0.10	0.00	35.80	2.00	0.00	0.00	0.10	0.00
35.90	2.00	0.00	0.00	0.10	0.00	36.00	2.00	0.00	0.00	0.10	0.00
36.10	2.00	0.00	0.00	0.10	0.00	36.20	2.00	0.00	0.00	0.10	0.00
36.30	2.00	0.00	0.00	0.10	0.00	36.40	2.00	0.00	0.00	0.10	0.00
36.50	2.00	0.00	0.00	0.10	0.00	36.60	2.00	0.00	0.00	0.10	0.00
36.70	2.00	0.00	0.00	0.10	0.00	36.80	2.00	0.00	0.00	0.10	0.00
36.90	2.00	0.00	0.00	0.10	0.00	37.00	2.00	0.00	0.00	0.10	0.00
37.10	2.00	0.00	0.00	0.10	0.00	37.20	2.00	0.00	0.00	0.10	0.00
37.30	2.00	0.00	0.00	0.10	0.00	37.40	2.00	0.00	0.00	0.10	0.00
37.50	2.00	0.00	0.00	0.10	0.00	37.60	2.00	0.00	0.00	0.10	0.00
37.70	2.00	0.00	0.00	0.10	0.00	37.80	2.00	0.00	0.00	0.10	0.00
37.90	2.00	0.00	0.00	0.10	0.00	38.00	2.00	0.00	0.00	0.10	0.00
38.10	2.00	0.00	0.00	0.10	0.00	38.20	2.00	0.00	0.00	0.10	0.00
38.30	2.00	0.00	0.00	0.10	0.00	38.40	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
38.50	2.00	0.00	0.00	0.10	0.00	38.60	2.00	0.00	0.00	0.10	0.00
38.70	2.00	0.00	0.00	0.10	0.00	38.80	2.00	0.00	0.00	0.10	0.00
38.90	2.00	0.00	0.00	0.10	0.00	39.00	2.00	0.00	0.00	0.10	0.00
39.10	2.00	0.00	0.00	0.10	0.00	39.20	2.00	0.00	0.00	0.10	0.00
39.30	2.00	0.00	0.00	0.10	0.00	39.40	2.00	0.00	0.00	0.10	0.00
39.50	2.00	0.00	0.00	0.10	0.00	39.60	2.00	0.00	0.00	0.10	0.00
39.70	2.00	0.00	0.00	0.10	0.00	39.80	2.00	0.00	0.00	0.10	0.00
39.90	2.00	0.00	0.00	0.10	0.00	40.00	2.00	0.00	0.00	0.10	0.00
40.10	2.00	0.00	0.00	0.10	0.00	40.20	2.00	0.00	0.00	0.10	0.00
40.30	2.00	0.00	0.00	0.10	0.00	40.40	2.00	0.00	0.00	0.10	0.00
40.50	2.00	0.00	0.00	0.10	0.00	40.60	2.00	0.00	0.00	0.10	0.00
40.70	2.00	0.00	0.00	0.10	0.00	40.80	2.00	0.00	0.00	0.10	0.00
40.90	2.00	0.00	0.00	0.10	0.00	41.00	2.00	0.00	0.00	0.10	0.00
41.10	2.00	0.00	0.00	0.10	0.00	41.20	2.00	0.00	0.00	0.10	0.00
41.30	2.00	0.00	0.00	0.10	0.00	41.40	2.00	0.00	0.00	0.10	0.00
41.50	2.00	0.00	0.00	0.10	0.00	41.60	2.00	0.00	0.00	0.10	0.00
41.70	2.00	0.00	0.00	0.10	0.00	41.80	2.00	0.00	0.00	0.10	0.00
41.90	2.00	0.00	0.00	0.10	0.00	42.00	2.00	0.00	0.00	0.10	0.00
42.10	2.00	0.00	0.00	0.10	0.00	42.20	0.91	0.00	0.00	0.10	0.01
42.30	0.41	0.59	0.40	0.10	0.06	42.40	0.30	0.70	0.32	0.10	0.08
42.50	0.35	0.65	0.35	0.10	0.07	42.60	0.47	0.53	0.44	0.10	0.06
42.70	0.54	0.46	0.53	0.10	0.05	42.80	0.51	0.49	0.49	0.10	0.05
42.90	2.00	0.00	0.00	0.10	0.00	43.00	2.00	0.00	0.00	0.10	0.00
43.10	2.00	0.00	0.00	0.10	0.00	43.20	2.00	0.00	0.00	0.10	0.00
43.30	2.00	0.00	0.00	0.10	0.00	43.40	0.25	0.75	0.30	0.10	0.08
43.50	0.28	0.72	0.31	0.10	0.07	43.60	0.30	0.70	0.32	0.10	0.07
43.70	0.32	0.68	0.33	0.10	0.07	43.80	0.32	0.68	0.33	0.10	0.07
43.90	0.31	0.69	0.33	0.10	0.07	44.00	0.32	0.68	0.33	0.10	0.07
44.10	0.32	0.68	0.34	0.10	0.07	44.20	0.32	0.68	0.34	0.10	0.07
44.30	0.33	0.67	0.34	0.10	0.07	44.40	0.37	0.63	0.36	0.10	0.06
44.50	0.46	0.54	0.43	0.10	0.05	44.60	0.60	0.40	0.64	0.10	0.04
44.70	0.72	0.28	1.03	0.10	0.03	44.80	0.76	0.00	0.00	0.10	0.02
44.90	0.77	0.00	0.00	0.10	0.02	45.00	0.82	0.00	0.00	0.10	0.02
45.10	0.90	0.00	0.00	0.10	0.01	45.20	0.89	0.00	0.00	0.10	0.01
45.30	0.79	0.00	0.00	0.10	0.02	45.40	0.67	0.33	0.81	0.10	0.03
45.50	0.58	0.42	0.60	0.10	0.04	45.60	0.58	0.42	0.60	0.10	0.04
45.70	0.67	0.33	0.81	0.10	0.03	45.80	0.73	0.00	0.00	0.10	0.02
45.90	0.73	0.00	0.00	0.10	0.02	46.00	0.74	0.00	0.00	0.10	0.02
46.10	0.69	0.31	0.90	0.10	0.03	46.20	0.67	0.33	0.82	0.10	0.03
46.30	0.67	0.33	0.81	0.10	0.03	46.40	0.64	0.36	0.73	0.10	0.03
46.50	0.64	0.36	0.72	0.10	0.03	46.60	0.70	0.30	0.94	0.10	0.03
46.70	2.00	0.00	0.00	0.10	0.00	46.80	2.00	0.00	0.00	0.10	0.00
46.90	2.00	0.00	0.00	0.10	0.00	47.00	2.00	0.00	0.00	0.10	0.00
47.10	2.00	0.00	0.00	0.10	0.00	47.20	0.28	0.72	0.31	0.10	0.06
47.30	0.29	0.71	0.32	0.10	0.06	47.40	0.34	0.66	0.35	0.10	0.06
47.50	0.25	0.75	0.30	0.10	0.06	47.60	0.19	0.81	0.27	0.10	0.07
47.70	2.00	0.00	0.00	0.10	0.00	47.80	2.00	0.00	0.00	0.10	0.00
47.90	2.00	0.00	0.00	0.10	0.00	48.00	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
48.10	2.00	0.00	0.00	0.10	0.00	48.20	2.00	0.00	0.00	0.10	0.00
48.30	2.00	0.00	0.00	0.10	0.00	48.40	2.00	0.00	0.00	0.10	0.00
48.50	2.00	0.00	0.00	0.10	0.00	48.60	2.00	0.00	0.00	0.10	0.00
48.70	2.00	0.00	0.00	0.10	0.00	48.80	2.00	0.00	0.00	0.10	0.00
48.90	2.00	0.00	0.00	0.10	0.00	49.00	2.00	0.00	0.00	0.10	0.00
49.10	2.00	0.00	0.00	0.10	0.00	49.20	2.00	0.00	0.00	0.10	0.00
49.30	2.00	0.00	0.00	0.10	0.00	49.40	2.00	0.00	0.00	0.10	0.00
49.50	2.00	0.00	0.00	0.10	0.00	49.60	2.00	0.00	0.00	0.10	0.00
49.70	2.00	0.00	0.00	0.10	0.00	49.80	2.00	0.00	0.00	0.10	0.00

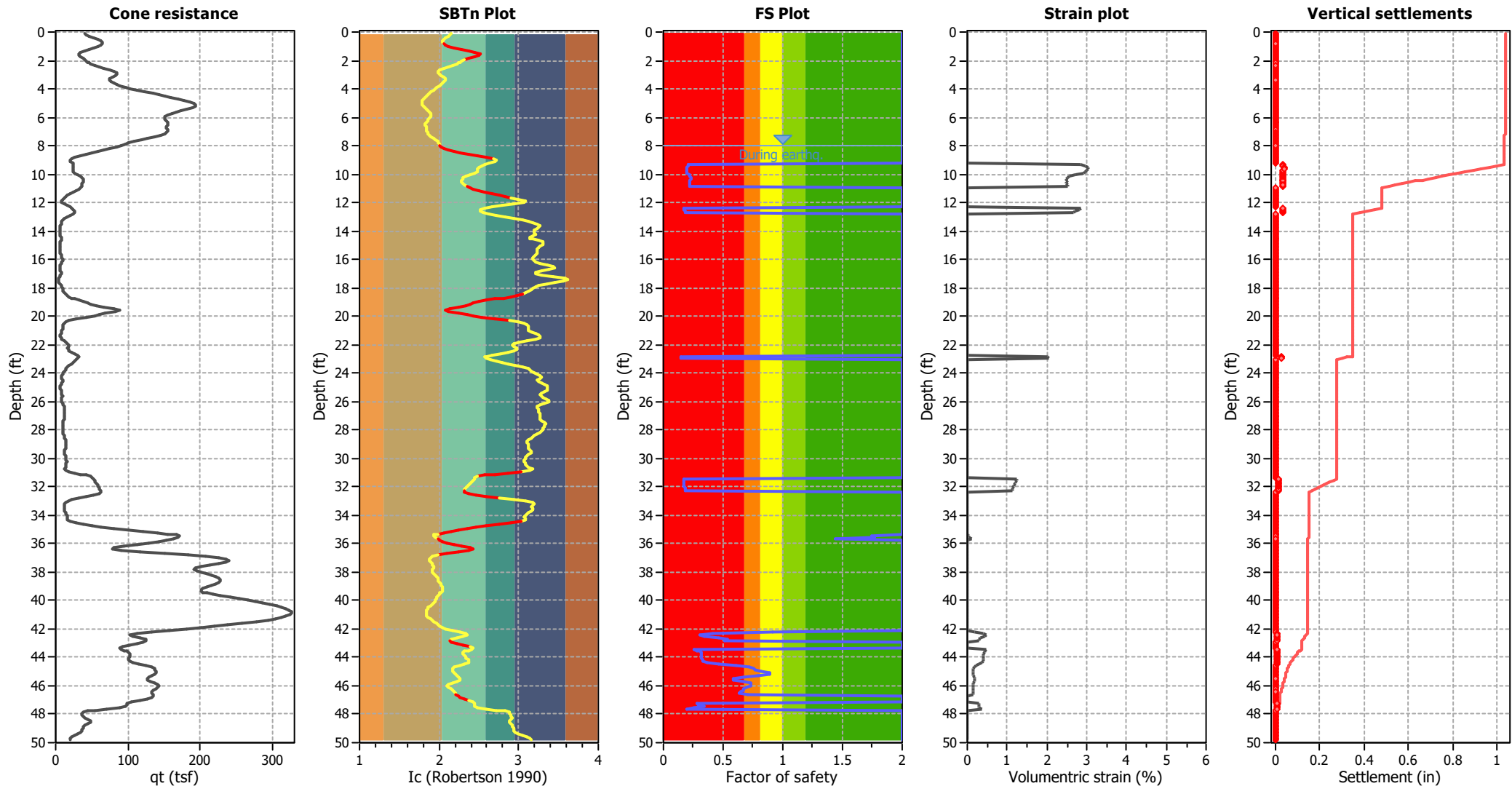
Overall liquefaction potential: 7.99

LPI_{ISH} > 5.0 - Liquefaction manifestation is expected

Abbreviations

FS: Calculated factor of safety for test point
d_z: Layer thickness (ft)
LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

- q_c: Total cone resistance (cone resistance q_c corrected for pore water effects)
- I_c: Soil Behaviour Type Index
- FS: Calculated Factor of Safety against liquefaction
- Volumetric strain: Post-liquefaction volumetric strain

:: Post-earthquake settlement of dry sands ::												
Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
0.10	2.15	64.82	1.50	96.92	21	550	0.56	0.001	0.00	13.69	0.00	0.000
0.20	2.14	66.79	1.49	99.56	22	564	0.56	0.001	0.00	13.69	0.00	0.000
0.30	2.12	72.65	1.45	105.45	23	597	0.56	0.002	0.00	13.69	0.00	0.000
0.40	2.08	83.10	1.39	115.64	25	649	0.55	0.002	0.00	13.69	0.00	0.000
0.50	2.05	92.98	1.36	126.21	27	700	0.55	0.002	0.00	13.69	0.00	0.000
0.60	2.04	100.09	1.35	135.01	29	747	0.55	0.003	0.00	13.69	0.00	0.000
0.70	2.05	103.65	1.35	140.34	30	778	0.55	0.003	0.00	13.69	0.00	0.000
0.80	2.06	103.48	1.37	141.35	30	787	0.55	0.004	0.00	13.69	0.00	0.000
0.90	2.08	99.71	1.39	138.89	0	0	0.55	0.000	0.00	13.69	0.00	0.000
1.00	2.12	92.34	1.46	134.57	0	0	0.55	0.000	0.00	13.69	0.00	0.000
1.10	2.19	83.03	1.59	132.20	0	0	0.55	0.000	0.00	13.69	0.00	0.000
1.20	2.28	72.89	1.83	133.74	0	0	0.55	0.000	0.00	13.69	0.00	0.000
1.30	2.37	62.95	2.21	138.89	0	0	0.56	0.000	0.00	13.69	0.00	0.000
1.40	2.45	54.39	2.68	145.79	0	0	0.56	0.000	0.00	13.69	0.00	0.000
1.50	2.51	49.36	3.04	150.26	0	0	0.56	0.000	0.00	13.69	0.00	0.000
1.60	2.50	49.52	3.00	148.70	0	0	0.56	0.000	0.00	13.69	0.00	0.000
1.70	2.45	53.38	2.65	141.43	0	0	0.56	0.000	0.00	13.69	0.00	0.000
1.80	2.38	58.78	2.26	133.04	0	0	0.56	0.000	0.00	13.69	0.00	0.000
1.90	2.32	63.66	2.00	127.04	0	0	0.56	0.000	0.00	13.69	0.00	0.000
2.00	2.28	67.54	1.86	125.46	0	0	0.55	0.000	0.00	13.69	0.00	0.000
2.10	2.26	70.40	1.80	126.76	29	694	0.55	0.015	0.01	13.69	0.01	0.000
2.20	2.25	73.44	1.76	129.41	30	713	0.55	0.015	0.01	13.69	0.01	0.000
2.30	2.23	78.01	1.68	131.32	30	733	0.55	0.015	0.01	13.69	0.01	0.000
2.40	2.18	85.27	1.56	133.14	30	753	0.55	0.015	0.01	13.69	0.01	0.000
2.50	2.12	95.43	1.44	137.65	30	779	0.55	0.015	0.01	13.69	0.01	0.000
2.60	2.06	107.22	1.36	145.98	31	811	0.54	0.015	0.01	13.69	0.01	0.000
2.70	2.01	118.66	1.32	156.42	33	850	0.54	0.014	0.01	13.69	0.01	0.000
2.80	1.99	127.85	1.30	166.07	34	890	0.54	0.014	0.01	13.69	0.01	0.000
2.90	1.99	133.46	1.30	172.95	36	924	0.54	0.014	0.01	13.69	0.01	0.000
3.00	2.00	134.52	1.31	175.87	37	949	0.53	0.014	0.01	13.69	0.01	0.000
3.10	2.03	131.01	1.33	174.30	37	955	0.53	0.014	0.01	13.69	0.01	0.000
3.20	2.06	124.90	1.36	169.97	36	945	0.54	0.015	0.01	13.69	0.01	0.000
3.30	2.07	120.11	1.38	166.04	36	929	0.54	0.016	0.01	13.69	0.01	0.000
3.40	2.07	119.74	1.38	165.53	35	926	0.54	0.017	0.01	13.69	0.01	0.000
3.50	2.06	123.31	1.37	168.49	36	938	0.54	0.017	0.01	13.69	0.01	0.000
3.60	2.04	128.71	1.35	173.30	37	957	0.53	0.017	0.01	13.69	0.01	0.000
3.70	2.02	134.88	1.33	179.02	38	979	0.53	0.017	0.01	13.69	0.01	0.000
3.80	2.00	142.91	1.31	186.75	39	1007	0.53	0.017	0.01	13.69	0.01	0.000
3.90	1.97	152.99	1.29	196.65	40	1041	0.53	0.017	0.01	13.69	0.01	0.000
4.00	1.95	164.29	1.27	208.44	43	1085	0.53	0.016	0.01	13.69	0.01	0.000
4.10	1.93	179.73	1.25	225.32	46	1153	0.53	0.015	0.01	13.69	0.00	0.000
4.20	1.90	197.59	1.24	244.95	49	1234	0.53	0.014	0.00	13.69	0.00	0.000
4.30	1.88	214.85	1.22	263.16	52	1305	0.53	0.013	0.00	13.69	0.00	0.000
4.40	1.86	228.58	1.21	276.44	55	1352	0.53	0.013	0.00	13.69	0.00	0.000
4.50	1.84	240.92	1.19	287.64	56	1390	0.53	0.013	0.00	13.69	0.00	0.000
4.60	1.82	255.10	1.18	300.41	59	1439	0.53	0.012	0.00	13.69	0.00	0.000
4.70	1.81	270.09	1.16	313.96	61	1495	0.53	0.012	0.00	13.69	0.00	0.000
4.80	1.80	285.18	1.15	327.26	63	1552	0.53	0.012	0.00	13.69	0.00	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
4.90	1.79	297.81	1.14	338.75	65	1603	0.53	0.012	0.00	13.69	0.00	0.000
5.00	1.79	306.67	1.14	348.33	67	1648	0.53	0.011	0.00	13.69	0.00	0.000
5.10	1.79	310.50	1.14	355.31	68	1683	0.53	0.011	0.00	13.69	0.00	0.000
5.20	1.81	309.22	1.16	358.97	70	1708	0.53	0.011	0.00	13.69	0.00	0.000
5.30	1.83	302.21	1.18	357.01	70	1713	0.53	0.012	0.00	13.69	0.00	0.000
5.40	1.85	291.00	1.20	349.22	69	1695	0.53	0.012	0.00	13.69	0.00	0.000
5.50	1.87	278.17	1.21	337.62	67	1657	0.53	0.013	0.00	13.69	0.00	0.000
5.60	1.88	266.94	1.22	326.25	65	1614	0.53	0.013	0.00	13.69	0.00	0.000
5.70	1.89	256.77	1.23	315.42	63	1570	0.53	0.014	0.00	13.69	0.00	0.000
5.80	1.89	247.71	1.23	305.16	61	1524	0.53	0.015	0.00	13.69	0.00	0.000
5.90	1.89	242.33	1.23	298.05	60	1486	0.53	0.016	0.00	13.69	0.00	0.000
6.00	1.88	240.97	1.22	294.72	59	1459	0.53	0.017	0.00	13.69	0.00	0.000
6.10	1.87	242.93	1.21	294.79	58	1447	0.53	0.018	0.00	13.69	0.00	0.000
6.20	1.86	244.63	1.20	294.70	58	1436	0.53	0.018	0.01	13.69	0.00	0.000
6.30	1.84	246.76	1.20	294.96	58	1427	0.53	0.019	0.01	13.69	0.00	0.000
6.40	1.83	248.42	1.19	295.06	58	1421	0.53	0.019	0.01	13.69	0.00	0.000
6.50	1.83	248.71	1.18	294.49	58	1415	0.53	0.020	0.01	13.69	0.00	0.000
6.60	1.83	247.47	1.18	293.11	57	1409	0.53	0.020	0.01	13.69	0.00	0.000
6.70	1.83	245.10	1.19	290.85	57	1406	0.53	0.021	0.01	13.69	0.01	0.000
6.80	1.84	243.47	1.19	289.28	57	1410	0.53	0.021	0.01	13.69	0.01	0.000
6.90	1.84	242.74	1.19	288.79	57	1420	0.53	0.021	0.01	13.69	0.01	0.000
7.00	1.84	241.76	1.19	288.76	57	1433	0.53	0.021	0.01	13.69	0.01	0.000
7.10	1.85	238.80	1.20	287.00	57	1439	0.53	0.022	0.01	13.69	0.01	0.000
7.20	1.86	232.71	1.21	281.98	56	1431	0.53	0.022	0.01	13.69	0.01	0.000
7.30	1.88	223.14	1.22	273.03	54	1405	0.53	0.023	0.01	13.69	0.01	0.000
7.40	1.90	210.28	1.24	260.34	52	1362	0.53	0.025	0.01	13.69	0.01	0.000
7.50	1.93	195.69	1.26	245.70	50	1310	0.53	0.027	0.01	13.69	0.01	0.000
7.60	1.95	181.72	1.27	231.31	47	1258	0.53	0.030	0.01	13.69	0.01	0.000
7.70	1.98	167.41	1.29	216.09	45	1196	0.53	0.034	0.01	13.69	0.01	0.000
7.80	2.00	154.98	1.30	201.99	42	1134	0.53	0.038	0.02	13.69	0.01	0.000
7.90	2.00	146.72	1.30	191.46	40	1084	0.54	0.043	0.02	13.69	0.02	0.000

Total estimated settlement: 0.00**Abbreviations**

Q_{tn}: Normalized cone resistance
 K_c: Fines correction factor
 Q_{tn,cs}: Equivalent clean sand normalized cone resistance
 G_{max}: Small strain shear modulus
 CSR: Soil cyclic stress ratio
 γ: Cyclic shear strain
 e_{vol(15)}: Volumetric strain after 15 cycles
 N_c: Equivalent number of cycles
 e_v: Volumetric strain
 Settle.: Calculated settlement

:: Post-earthquake settlement due to soil liquefaction ::

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
8.00	167.20	2.00	0.00	0.85	0.00	8.10	153.78	2.00	0.00	0.85	0.00
8.20	143.56	2.00	0.00	0.85	0.00	8.30	140.03	2.00	0.00	0.85	0.00
8.40	133.88	2.00	0.00	0.85	0.00	8.50	125.96	2.00	0.00	0.85	0.00
8.60	116.92	2.00	0.00	0.84	0.00	8.70	105.34	2.00	0.00	0.84	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
8.80	95.96	2.00	0.00	0.84	0.00	8.90	26.55	2.00	0.00	0.84	0.00
9.00	24.41	2.00	0.00	0.84	0.00	9.10	27.81	2.00	0.00	0.83	0.00
9.20	30.49	2.00	0.00	0.83	0.00	9.30	93.47	0.21	2.86	0.83	0.03
9.40	90.25	0.20	2.95	0.83	0.04	9.50	87.88	0.20	3.03	0.83	0.04
9.60	87.35	0.20	3.04	0.83	0.04	9.70	87.88	0.20	3.01	0.82	0.04
9.80	88.61	0.20	2.98	0.82	0.04	9.90	90.37	0.20	2.92	0.82	0.04
10.00	97.56	0.21	2.70	0.82	0.03	10.10	102.74	0.22	2.55	0.82	0.03
10.20	104.31	0.23	2.51	0.81	0.03	10.30	104.47	0.23	2.50	0.81	0.03
10.40	104.00	0.22	2.50	0.81	0.03	10.50	103.57	0.22	2.51	0.81	0.03
10.60	103.51	0.22	2.50	0.81	0.03	10.70	103.50	0.22	2.50	0.81	0.03
10.80	102.25	0.22	2.52	0.80	0.03	10.90	102.16	0.21	2.52	0.80	0.03
11.00	102.06	2.00	0.00	0.80	0.00	11.10	99.32	2.00	0.00	0.80	0.00
11.20	93.54	2.00	0.00	0.80	0.00	11.30	88.37	2.00	0.00	0.79	0.00
11.40	24.09	2.00	0.00	0.79	0.00	11.50	19.69	2.00	0.00	0.79	0.00
11.60	16.12	2.00	0.00	0.79	0.00	11.70	14.06	2.00	0.00	0.79	0.00
11.80	11.48	2.00	0.00	0.79	0.00	11.90	8.35	2.00	0.00	0.78	0.00
12.00	9.54	2.00	0.00	0.78	0.00	12.10	14.03	2.00	0.00	0.78	0.00
12.20	19.37	2.00	0.00	0.78	0.00	12.30	24.72	2.00	0.00	0.78	0.00
12.40	87.15	0.18	2.86	0.77	0.03	12.50	87.80	0.18	2.83	0.77	0.03
12.60	91.85	0.18	2.70	0.77	0.03	12.70	92.06	0.18	2.69	0.77	0.03
12.80	28.58	2.00	0.00	0.77	0.00	12.90	23.73	2.00	0.00	0.77	0.00
13.00	18.78	2.00	0.00	0.76	0.00	13.10	13.98	2.00	0.00	0.76	0.00
13.20	11.12	2.00	0.00	0.76	0.00	13.30	10.55	2.00	0.00	0.76	0.00
13.40	9.61	2.00	0.00	0.76	0.00	13.50	7.85	2.00	0.00	0.75	0.00
13.60	7.54	2.00	0.00	0.75	0.00	13.70	7.52	2.00	0.00	0.75	0.00
13.80	7.51	2.00	0.00	0.75	0.00	13.90	7.49	2.00	0.00	0.75	0.00
14.00	7.48	2.00	0.00	0.75	0.00	14.10	6.92	2.00	0.00	0.74	0.00
14.20	6.72	2.00	0.00	0.74	0.00	14.30	7.46	2.00	0.00	0.74	0.00
14.40	9.10	2.00	0.00	0.74	0.00	14.50	10.09	2.00	0.00	0.74	0.00
14.60	8.86	2.00	0.00	0.73	0.00	14.70	7.61	2.00	0.00	0.73	0.00
14.80	7.37	2.00	0.00	0.73	0.00	14.90	7.35	2.00	0.00	0.73	0.00
15.00	7.34	2.00	0.00	0.73	0.00	15.10	7.32	2.00	0.00	0.73	0.00
15.20	7.31	2.00	0.00	0.72	0.00	15.30	7.30	2.00	0.00	0.72	0.00
15.40	7.28	2.00	0.00	0.72	0.00	15.50	7.27	2.00	0.00	0.72	0.00
15.60	7.26	2.00	0.00	0.72	0.00	15.70	7.52	2.00	0.00	0.71	0.00
15.80	9.18	2.00	0.00	0.71	0.00	15.90	10.06	2.00	0.00	0.71	0.00
16.00	10.04	2.00	0.00	0.71	0.00	16.10	10.02	2.00	0.00	0.71	0.00
16.20	9.98	2.00	0.00	0.71	0.00	16.30	8.11	2.00	0.00	0.70	0.00
16.40	6.39	2.00	0.00	0.70	0.00	16.50	5.26	2.00	0.00	0.70	0.00
16.60	4.77	2.00	0.00	0.70	0.00	16.70	5.45	2.00	0.00	0.70	0.00
16.80	7.40	2.00	0.00	0.69	0.00	16.90	8.49	2.00	0.00	0.69	0.00
17.00	8.25	2.00	0.00	0.69	0.00	17.10	6.74	2.00	0.00	0.69	0.00
17.20	4.94	2.00	0.00	0.69	0.00	17.30	3.74	2.00	0.00	0.69	0.00
17.40	3.53	2.00	0.00	0.68	0.00	17.50	4.23	2.00	0.00	0.68	0.00
17.60	4.48	2.00	0.00	0.68	0.00	17.70	6.11	2.00	0.00	0.68	0.00
17.80	7.74	2.00	0.00	0.68	0.00	17.90	9.35	2.00	0.00	0.67	0.00
18.00	9.71	2.00	0.00	0.67	0.00	18.10	10.38	2.00	0.00	0.67	0.00
18.20	11.80	2.00	0.00	0.67	0.00	18.30	12.76	2.00	0.00	0.67	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
18.40	14.65	2.00	0.00	0.67	0.00	18.50	17.00	2.00	0.00	0.66	0.00
18.60	19.85	2.00	0.00	0.66	0.00	18.70	23.46	2.00	0.00	0.66	0.00
18.80	28.55	2.00	0.00	0.66	0.00	18.90	95.41	2.00	0.00	0.66	0.00
19.00	103.10	2.00	0.00	0.65	0.00	19.10	110.28	2.00	0.00	0.65	0.00
19.20	113.79	2.00	0.00	0.65	0.00	19.30	119.39	2.00	0.00	0.65	0.00
19.40	129.34	2.00	0.00	0.65	0.00	19.50	144.96	2.00	0.00	0.65	0.00
19.60	158.44	2.00	0.00	0.64	0.00	19.70	150.57	2.00	0.00	0.64	0.00
19.80	122.48	2.00	0.00	0.64	0.00	19.90	124.83	2.00	0.00	0.64	0.00
20.00	131.22	2.00	0.00	0.64	0.00	20.10	107.32	2.00	0.00	0.63	0.00
20.20	23.97	2.00	0.00	0.63	0.00	20.30	18.14	2.00	0.00	0.63	0.00
20.40	14.02	2.00	0.00	0.63	0.00	20.50	12.04	2.00	0.00	0.63	0.00
20.60	10.54	2.00	0.00	0.63	0.00	20.70	9.18	2.00	0.00	0.62	0.00
20.80	9.17	2.00	0.00	0.62	0.00	20.90	9.15	2.00	0.00	0.62	0.00
21.00	9.14	2.00	0.00	0.62	0.00	21.10	8.63	2.00	0.00	0.62	0.00
21.20	7.28	2.00	0.00	0.61	0.00	21.30	6.52	2.00	0.00	0.61	0.00
21.40	6.51	2.00	0.00	0.61	0.00	21.50	6.72	2.00	0.00	0.61	0.00
21.60	8.14	2.00	0.00	0.61	0.00	21.70	11.31	2.00	0.00	0.61	0.00
21.80	14.98	2.00	0.00	0.60	0.00	21.90	17.88	2.00	0.00	0.60	0.00
22.00	19.04	2.00	0.00	0.60	0.00	22.10	18.11	2.00	0.00	0.60	0.00
22.20	16.88	2.00	0.00	0.60	0.00	22.30	16.92	2.00	0.00	0.59	0.00
22.40	18.64	2.00	0.00	0.59	0.00	22.50	21.94	2.00	0.00	0.59	0.00
22.60	26.68	2.00	0.00	0.59	0.00	22.70	31.19	2.00	0.00	0.59	0.00
22.80	93.77	0.15	2.01	0.59	0.02	22.90	93.22	0.15	2.01	0.58	0.02
23.00	91.36	0.15	2.05	0.58	0.02	23.10	28.84	2.00	0.00	0.58	0.00
23.20	26.70	2.00	0.00	0.58	0.00	23.30	25.15	2.00	0.00	0.58	0.00
23.40	22.55	2.00	0.00	0.57	0.00	23.50	18.57	2.00	0.00	0.57	0.00
23.60	14.60	2.00	0.00	0.57	0.00	23.70	13.12	2.00	0.00	0.57	0.00
23.80	13.63	2.00	0.00	0.57	0.00	23.90	12.18	2.00	0.00	0.57	0.00
24.00	10.19	2.00	0.00	0.56	0.00	24.10	9.00	2.00	0.00	0.56	0.00
24.20	7.87	2.00	0.00	0.56	0.00	24.30	7.41	2.00	0.00	0.56	0.00
24.40	8.57	2.00	0.00	0.56	0.00	24.50	9.22	2.00	0.00	0.55	0.00
24.60	9.08	2.00	0.00	0.55	0.00	24.70	8.11	2.00	0.00	0.55	0.00
24.80	6.65	2.00	0.00	0.55	0.00	24.90	6.12	2.00	0.00	0.55	0.00
25.00	6.12	2.00	0.00	0.55	0.00	25.10	6.11	2.00	0.00	0.54	0.00
25.20	6.20	2.00	0.00	0.54	0.00	25.30	7.09	2.00	0.00	0.54	0.00
25.40	8.21	2.00	0.00	0.54	0.00	25.50	8.49	2.00	0.00	0.54	0.00
25.60	8.48	2.00	0.00	0.53	0.00	25.70	8.47	2.00	0.00	0.53	0.00
25.80	7.73	2.00	0.00	0.53	0.00	25.90	6.64	2.00	0.00	0.53	0.00
26.00	7.16	2.00	0.00	0.53	0.00	26.10	8.58	2.00	0.00	0.53	0.00
26.20	9.97	2.00	0.00	0.52	0.00	26.30	10.75	2.00	0.00	0.52	0.00
26.40	10.77	2.00	0.00	0.52	0.00	26.50	10.75	2.00	0.00	0.52	0.00
26.60	10.73	2.00	0.00	0.52	0.00	26.70	10.72	2.00	0.00	0.51	0.00
26.80	10.70	2.00	0.00	0.51	0.00	26.90	10.68	2.00	0.00	0.51	0.00
27.00	10.67	2.00	0.00	0.51	0.00	27.10	10.65	2.00	0.00	0.51	0.00
27.20	10.64	2.00	0.00	0.51	0.00	27.30	10.62	2.00	0.00	0.50	0.00
27.40	10.20	2.00	0.00	0.50	0.00	27.50	9.00	2.00	0.00	0.50	0.00
27.60	8.24	2.00	0.00	0.50	0.00	27.70	8.22	2.00	0.00	0.50	0.00
27.80	8.21	2.00	0.00	0.49	0.00	27.90	8.20	2.00	0.00	0.49	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
28.00	8.55	2.00	0.00	0.49	0.00	28.10	8.76	2.00	0.00	0.49	0.00
28.20	8.74	2.00	0.00	0.49	0.00	28.30	9.92	2.00	0.00	0.49	0.00
28.40	10.46	2.00	0.00	0.48	0.00	28.50	10.44	2.00	0.00	0.48	0.00
28.60	11.07	2.00	0.00	0.48	0.00	28.70	12.42	2.00	0.00	0.48	0.00
28.80	12.71	2.00	0.00	0.48	0.00	28.90	12.69	2.00	0.00	0.47	0.00
29.00	12.67	2.00	0.00	0.47	0.00	29.10	12.65	2.00	0.00	0.47	0.00
29.20	12.63	2.00	0.00	0.47	0.00	29.30	12.62	2.00	0.00	0.47	0.00
29.40	11.63	2.00	0.00	0.47	0.00	29.50	10.32	2.00	0.00	0.46	0.00
29.60	10.28	2.00	0.00	0.46	0.00	29.70	10.69	2.00	0.00	0.46	0.00
29.80	12.69	2.00	0.00	0.46	0.00	29.90	12.61	2.00	0.00	0.46	0.00
30.00	11.93	2.00	0.00	0.45	0.00	30.10	14.03	2.00	0.00	0.45	0.00
30.20	14.11	2.00	0.00	0.45	0.00	30.30	12.90	2.00	0.00	0.45	0.00
30.40	12.63	2.00	0.00	0.45	0.00	30.50	12.98	2.00	0.00	0.45	0.00
30.60	12.14	2.00	0.00	0.44	0.00	30.70	10.82	2.00	0.00	0.44	0.00
30.80	11.26	2.00	0.00	0.44	0.00	30.90	15.43	2.00	0.00	0.44	0.00
31.00	23.09	2.00	0.00	0.44	0.00	31.10	31.90	2.00	0.00	0.43	0.00
31.20	101.42	2.00	0.00	0.43	0.00	31.30	106.95	2.00	0.00	0.43	0.00
31.40	109.00	2.00	0.00	0.43	0.00	31.50	110.28	0.17	1.24	0.43	0.01
31.60	110.91	0.17	1.23	0.43	0.01	31.70	112.26	0.17	1.21	0.42	0.01
31.80	113.39	0.17	1.19	0.42	0.01	31.90	113.81	0.17	1.18	0.42	0.01
32.00	115.33	0.18	1.16	0.42	0.01	32.10	116.73	0.18	1.14	0.42	0.01
32.20	115.98	0.18	1.14	0.41	0.01	32.30	117.16	0.18	1.12	0.41	0.01
32.40	120.17	2.00	0.00	0.41	0.00	32.50	119.22	2.00	0.00	0.41	0.00
32.60	111.63	2.00	0.00	0.41	0.00	32.70	101.70	2.00	0.00	0.41	0.00
32.80	27.83	2.00	0.00	0.40	0.00	32.90	18.89	2.00	0.00	0.40	0.00
33.00	14.48	2.00	0.00	0.40	0.00	33.10	11.59	2.00	0.00	0.40	0.00
33.20	9.93	2.00	0.00	0.40	0.00	33.30	10.78	2.00	0.00	0.39	0.00
33.40	11.73	2.00	0.00	0.39	0.00	33.50	9.43	2.00	0.00	0.39	0.00
33.60	8.93	2.00	0.00	0.39	0.00	33.70	12.23	2.00	0.00	0.39	0.00
33.80	12.06	2.00	0.00	0.39	0.00	33.90	11.64	2.00	0.00	0.38	0.00
34.00	13.96	2.00	0.00	0.38	0.00	34.10	13.94	2.00	0.00	0.38	0.00
34.20	13.92	2.00	0.00	0.38	0.00	34.30	13.91	2.00	0.00	0.38	0.00
34.40	15.42	2.00	0.00	0.37	0.00	34.50	23.79	2.00	0.00	0.37	0.00
34.60	35.53	2.00	0.00	0.37	0.00	34.70	107.45	2.00	0.00	0.37	0.00
34.80	119.28	2.00	0.00	0.37	0.00	34.90	135.07	2.00	0.00	0.37	0.00
35.00	154.21	2.00	0.00	0.36	0.00	35.10	174.75	2.00	0.00	0.36	0.00
35.20	186.72	2.00	0.00	0.36	0.00	35.30	189.39	2.00	0.00	0.36	0.00
35.40	192.34	2.00	0.00	0.36	0.00	35.50	196.79	1.75	0.04	0.35	0.00
35.60	197.01	1.77	0.03	0.35	0.00	35.70	193.09	1.44	0.10	0.35	0.00
35.80	192.26	2.00	0.00	0.35	0.00	35.90	183.99	2.00	0.00	0.35	0.00
36.00	174.42	2.00	0.00	0.35	0.00	36.10	164.75	2.00	0.00	0.34	0.00
36.20	149.52	2.00	0.00	0.34	0.00	36.30	134.94	2.00	0.00	0.34	0.00
36.40	129.02	2.00	0.00	0.34	0.00	36.50	141.07	2.00	0.00	0.34	0.00
36.60	169.79	2.00	0.00	0.33	0.00	36.70	201.23	2.00	0.00	0.33	0.00
36.80	220.54	2.00	0.00	0.33	0.00	36.90	227.05	2.00	0.00	0.33	0.00
37.00	232.74	2.00	0.00	0.33	0.00	37.10	245.82	2.00	0.00	0.33	0.00
37.20	248.07	2.00	0.00	0.32	0.00	37.30	243.36	2.00	0.00	0.32	0.00
37.40	236.99	2.00	0.00	0.32	0.00	37.50	227.80	2.00	0.00	0.32	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
37.60	218.56	2.00	0.00	0.32	0.00	37.70	209.82	2.00	0.00	0.31	0.00
37.80	204.14	2.00	0.00	0.31	0.00	37.90	205.92	2.00	0.00	0.31	0.00
38.00	214.93	2.00	0.00	0.31	0.00	38.10	227.69	2.00	0.00	0.31	0.00
38.20	240.63	2.00	0.00	0.31	0.00	38.30	250.91	2.00	0.00	0.30	0.00
38.40	257.29	2.00	0.00	0.30	0.00	38.50	261.68	2.00	0.00	0.30	0.00
38.60	264.65	2.00	0.00	0.30	0.00	38.70	264.41	2.00	0.00	0.30	0.00
38.80	260.54	2.00	0.00	0.29	0.00	38.90	256.12	2.00	0.00	0.29	0.00
39.00	251.52	2.00	0.00	0.29	0.00	39.10	246.01	2.00	0.00	0.29	0.00
39.20	242.60	2.00	0.00	0.29	0.00	39.30	241.09	2.00	0.00	0.29	0.00
39.40	241.70	2.00	0.00	0.28	0.00	39.50	245.00	2.00	0.00	0.28	0.00
39.60	250.44	2.00	0.00	0.28	0.00	39.70	257.66	2.00	0.00	0.28	0.00
39.80	267.96	2.00	0.00	0.28	0.00	39.90	279.21	2.00	0.00	0.27	0.00
40.00	290.30	2.00	0.00	0.27	0.00	40.10	297.22	2.00	0.00	0.27	0.00
40.20	303.41	2.00	0.00	0.27	0.00	40.30	305.02	2.00	0.00	0.27	0.00
40.40	303.04	2.00	0.00	0.27	0.00	40.50	300.31	2.00	0.00	0.26	0.00
40.60	300.38	2.00	0.00	0.26	0.00	40.70	302.84	2.00	0.00	0.26	0.00
40.80	305.03	2.00	0.00	0.26	0.00	40.90	304.14	2.00	0.00	0.26	0.00
41.00	300.89	2.00	0.00	0.25	0.00	41.10	298.63	2.00	0.00	0.25	0.00
41.20	298.17	2.00	0.00	0.25	0.00	41.30	300.18	2.00	0.00	0.25	0.00
41.40	301.02	2.00	0.00	0.25	0.00	41.50	294.86	2.00	0.00	0.25	0.00
41.60	282.39	2.00	0.00	0.24	0.00	41.70	265.82	2.00	0.00	0.24	0.00
41.80	248.96	2.00	0.00	0.24	0.00	41.90	238.57	2.00	0.00	0.24	0.00
42.00	223.86	2.00	0.00	0.24	0.00	42.10	205.41	2.00	0.00	0.23	0.00
42.20	183.52	0.91	0.18	0.23	0.00	42.30	161.05	0.41	0.38	0.23	0.00
42.40	148.64	0.30	0.48	0.23	0.01	42.50	154.55	0.35	0.46	0.23	0.01
42.60	165.17	0.47	0.33	0.23	0.00	42.70	169.84	0.54	0.28	0.22	0.00
42.80	168.00	0.51	0.29	0.22	0.00	42.90	164.79	2.00	0.00	0.22	0.00
43.00	158.54	2.00	0.00	0.22	0.00	43.10	149.78	2.00	0.00	0.22	0.00
43.20	142.51	2.00	0.00	0.21	0.00	43.30	138.75	2.00	0.00	0.21	0.00
43.40	140.49	0.25	0.47	0.21	0.01	43.50	145.93	0.28	0.45	0.21	0.01
43.60	149.07	0.30	0.43	0.21	0.01	43.70	150.63	0.32	0.42	0.21	0.01
43.80	150.75	0.32	0.42	0.20	0.01	43.90	150.02	0.31	0.42	0.20	0.01
44.00	150.90	0.32	0.41	0.20	0.00	44.10	151.64	0.32	0.41	0.20	0.00
44.20	151.65	0.32	0.40	0.20	0.00	44.30	152.27	0.33	0.40	0.19	0.00
44.40	157.09	0.37	0.37	0.19	0.00	44.50	164.61	0.46	0.28	0.19	0.00
44.60	173.07	0.60	0.21	0.19	0.00	44.70	178.00	0.72	0.17	0.19	0.00
44.80	179.12	0.76	0.16	0.19	0.00	44.90	179.57	0.77	0.16	0.18	0.00
45.00	181.03	0.82	0.15	0.18	0.00	45.10	183.26	0.90	0.14	0.18	0.00
45.20	183.07	0.89	0.14	0.18	0.00	45.30	180.26	0.79	0.15	0.18	0.00
45.40	175.94	0.67	0.17	0.17	0.00	45.50	172.04	0.58	0.20	0.17	0.00
45.60	172.13	0.58	0.19	0.17	0.00	45.70	176.03	0.67	0.17	0.17	0.00
45.80	178.37	0.73	0.15	0.17	0.00	45.90	178.40	0.73	0.15	0.17	0.00
46.00	178.45	0.74	0.15	0.16	0.00	46.10	176.94	0.69	0.15	0.16	0.00
46.20	176.08	0.67	0.16	0.16	0.00	46.30	175.95	0.67	0.16	0.16	0.00
46.40	174.88	0.64	0.16	0.16	0.00	46.50	174.65	0.64	0.16	0.15	0.00
46.60	177.29	0.70	0.14	0.15	0.00	46.70	180.84	2.00	0.00	0.15	0.00
46.80	181.66	2.00	0.00	0.15	0.00	46.90	177.14	2.00	0.00	0.15	0.00
47.00	164.50	2.00	0.00	0.15	0.00	47.10	155.09	2.00	0.00	0.14	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
47.20	144.43	0.28	0.31	0.14	0.00	47.30	147.13	0.29	0.30	0.14	0.00
47.40	154.24	0.34	0.28	0.14	0.00	47.50	140.18	0.25	0.31	0.14	0.00
47.60	122.24	0.19	0.35	0.13	0.00	47.70	39.74	2.00	0.00	0.13	0.00
47.80	30.91	2.00	0.00	0.13	0.00	47.90	27.45	2.00	0.00	0.13	0.00
48.00	25.83	2.00	0.00	0.13	0.00	48.10	26.61	2.00	0.00	0.13	0.00
48.20	27.17	2.00	0.00	0.12	0.00	48.30	28.73	2.00	0.00	0.12	0.00
48.40	33.27	2.00	0.00	0.12	0.00	48.50	37.34	2.00	0.00	0.12	0.00
48.60	36.05	2.00	0.00	0.12	0.00	48.70	32.72	2.00	0.00	0.11	0.00
48.80	29.23	2.00	0.00	0.11	0.00	48.90	27.86	2.00	0.00	0.11	0.00
49.00	27.91	2.00	0.00	0.11	0.00	49.10	27.14	2.00	0.00	0.11	0.00
49.20	26.39	2.00	0.00	0.11	0.00	49.30	25.48	2.00	0.00	0.10	0.00
49.40	23.02	2.00	0.00	0.10	0.00	49.50	18.61	2.00	0.00	0.10	0.00
49.60	15.67	2.00	0.00	0.10	0.00	49.70	14.46	2.00	0.00	0.10	0.00
49.80	13.86	2.00	0.00	0.09	0.00						

Total estimated settlement: 1.03**Abbreviations**

$Q_{tn,cs}$:	Equivalent clean sand normalized cone resistance
FS:	Factor of safety against liquefaction
e_v (%):	Post-liquefaction volumetric strain
DF:	e_v depth weighting factor
Settlement:	Calculated settlement

:: Strength loss calculation Idriss & Boulanger (2008) ::

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.10	40.35	64.82	1.50	96.92	2.15	0.12	0.78
0.20	41.58	66.79	1.49	99.56	2.14	0.11	0.78
0.30	45.23	72.65	1.45	105.45	2.12	0.13	0.79
0.40	51.74	83.10	1.39	115.64	2.08	0.14	0.81
0.50	57.90	92.98	1.36	126.21	2.05	0.16	0.82
0.60	62.33	100.09	1.35	135.01	2.04	0.18	0.83
0.70	64.56	103.65	1.35	140.34	2.05	0.19	0.84
0.80	64.46	103.48	1.37	141.35	2.06	0.19	0.84
0.90	62.11	99.71	1.39	138.89	2.08	0.18	0.84
1.00	57.54	92.34	1.46	134.57	2.12	0.17	0.83
1.10	51.75	83.03	1.59	132.20	2.19	0.16	0.82
1.20	45.44	72.89	1.83	133.74	2.28	0.15	0.81
1.30	39.26	62.95	2.21	138.89	2.37	0.14	0.79
1.40	33.94	54.39	2.68	145.79	2.45	0.12	0.78
1.50	30.81	49.36	3.04	150.26	2.51	0.12	0.77
1.60	30.91	49.52	3.00	148.70	2.50	0.12	0.77
1.70	33.33	53.38	2.65	141.43	2.45	0.12	0.78
1.80	36.69	58.78	2.26	133.04	2.38	0.13	0.79
1.90	39.74	63.66	2.00	127.04	2.32	0.13	0.79
2.00	42.16	67.54	1.86	125.46	2.28	0.14	0.80
2.10	43.95	70.40	1.80	126.76	2.26	0.14	0.80
2.20	45.84	73.44	1.76	129.41	2.25	0.14	0.81
2.30	48.69	78.01	1.68	131.32	2.23	0.15	0.81
2.40	53.22	85.27	1.56	133.14	2.18	0.16	0.82
2.50	59.55	95.43	1.44	137.65	2.12	0.17	0.83
2.60	66.89	107.22	1.36	145.98	2.06	0.20	0.84
2.70	74.02	118.66	1.32	156.42	2.01	0.23	0.85
2.80	79.74	127.85	1.30	166.07	1.99	0.26	0.86
2.90	83.24	133.46	1.30	172.95	1.99	0.29	0.87
3.00	83.91	134.52	1.31	175.87	2.00	0.31	0.87
3.10	81.73	131.01	1.33	174.30	2.03	0.29	0.87
3.20	77.93	124.90	1.36	169.97	2.06	0.26	0.87
3.30	74.96	120.11	1.38	166.04	2.07	0.24	0.86
3.40	74.74	119.74	1.38	165.53	2.07	0.24	0.86
3.50	76.96	123.31	1.37	168.49	2.06	0.26	0.87
3.60	80.33	128.71	1.35	173.30	2.04	0.28	0.87
3.70	84.17	134.88	1.33	179.02	2.02	0.30	0.87
3.80	89.18	142.91	1.31	186.75	2.00	0.34	0.88
3.90	95.46	152.99	1.29	196.65	1.97	0.39	0.88
4.00	102.50	164.29	1.27	208.44	1.95	0.45	0.89
4.10	112.12	179.73	1.25	225.32	1.93	0.54	0.89
4.20	123.24	197.59	1.24	244.95	1.90	0.89	0.90
4.30	133.99	214.85	1.22	263.16	1.88	0.94	0.91
4.40	142.54	228.58	1.21	276.44	1.86	0.95	0.91
4.50	150.23	240.92	1.19	287.64	1.84	0.96	0.91
4.60	159.06	255.10	1.18	300.41	1.82	0.97	0.92
4.70	168.40	270.09	1.16	313.96	1.81	0.98	0.92
4.80	177.80	285.18	1.15	327.26	1.80	0.99	0.93

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
4.90	185.66	297.81	1.14	338.75	1.79	0.99	0.94
5.00	191.18	306.67	1.14	348.33	1.79	1.00	0.94
5.10	193.58	310.50	1.14	355.31	1.79	1.00	0.94
5.20	192.78	309.22	1.16	358.97	1.81	1.00	0.94
5.30	188.43	302.21	1.18	357.01	1.83	1.00	0.94
5.40	181.46	291.00	1.20	349.22	1.85	0.99	0.94
5.50	173.48	278.17	1.21	337.62	1.87	0.98	0.93
5.60	166.49	266.94	1.22	326.25	1.88	0.98	0.93
5.70	160.17	256.77	1.23	315.42	1.89	0.97	0.92
5.80	154.54	247.71	1.23	305.16	1.89	0.96	0.92
5.90	151.20	242.33	1.23	298.05	1.89	0.96	0.91
6.00	150.36	240.97	1.22	294.72	1.88	0.96	0.91
6.10	151.58	242.93	1.21	294.79	1.87	0.96	0.90
6.20	152.65	244.63	1.20	294.70	1.86	0.96	0.90
6.30	153.98	246.76	1.20	294.96	1.84	0.96	0.90
6.40	155.02	248.42	1.19	295.06	1.83	0.96	0.90
6.50	155.21	248.71	1.18	294.49	1.83	0.96	0.90
6.60	154.44	247.47	1.18	293.11	1.83	0.96	0.89
6.70	153.63	245.10	1.19	290.85	1.83	0.96	0.89
6.80	153.80	243.47	1.19	289.28	1.84	0.96	0.89
6.90	154.54	242.74	1.19	288.79	1.84	0.96	0.89
7.00	154.90	241.76	1.19	288.76	1.84	0.96	0.89
7.10	153.81	238.80	1.20	287.00	1.85	0.96	0.89
7.20	150.50	232.71	1.21	281.98	1.86	0.95	0.89
7.30	144.74	223.14	1.22	273.03	1.88	0.76	0.89
7.40	136.62	210.28	1.24	260.34	1.90	0.57	0.89
7.50	127.15	195.69	1.26	245.70	1.93	0.43	0.88
7.60	118.12	181.72	1.27	231.31	1.95	0.35	0.87
7.70	108.93	167.41	1.29	216.09	1.98	0.30	0.87
7.80	101.20	154.98	1.30	201.99	2.00	0.24	0.85
7.90	96.54	146.72	1.30	191.46	2.00	0.22	0.85
8.00	91.21	137.73	1.31	180.33	2.00	0.22	0.85
8.10	83.87	126.74	1.33	167.98	2.02	0.18	0.83
8.20	73.95	112.54	1.37	154.18	2.06	0.16	0.82
8.30	65.66	100.93	1.44	145.79	2.12	0.15	0.81
8.40	58.44	90.96	1.57	142.66	2.18	0.14	0.80
8.50	50.44	79.85	1.80	143.47	2.26	0.13	0.79
8.60	41.90	66.45	2.21	146.75	2.37	0.12	0.78
8.70	33.76	53.37	2.83	150.93	2.48	0.11	0.76
8.80	26.20	41.20	3.65	150.57	2.59	0.10	0.74
8.90	21.14	33.06	4.46	147.49	2.68	0.09	0.62
9.00	19.30	30.10	4.88	146.86	2.72	0.09	0.62
9.10	20.38	31.82	4.65	148.07	2.69	0.10	0.62
9.20	22.74	35.61	4.06	144.58	2.63	0.10	0.62
9.30	23.71	37.17	3.57	132.85	2.58	0.10	0.74
9.40	23.62	37.00	3.20	118.27	2.53	0.09	0.73
9.50	22.74	35.59	2.98	106.04	2.50	0.09	0.72
9.60	22.51	35.21	2.85	100.51	2.48	0.09	0.72

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.70	22.82	35.70	2.82	100.54	2.48	0.09	0.72
9.80	23.67	37.05	2.80	103.68	2.47	0.09	0.73
9.90	26.17	40.64	2.61	106.25	2.44	0.09	0.73
10.00	29.98	45.92	2.32	106.59	2.39	0.10	0.74
10.10	33.87	51.14	2.07	106.06	2.34	0.10	0.75
10.20	36.11	53.99	1.95	105.06	2.31	0.10	0.76
10.30	36.87	54.77	1.90	103.83	2.29	0.10	0.76
10.40	37.04	54.70	1.86	101.89	2.28	0.10	0.76
10.50	37.04	54.41	1.83	99.82	2.27	0.10	0.75
10.60	36.91	54.01	1.84	99.38	2.28	0.10	0.75
10.70	36.31	53.16	1.91	101.48	2.30	0.10	0.75
10.80	35.51	52.17	2.03	105.65	2.33	0.10	0.75
10.90	34.67	51.07	2.15	110.01	2.36	0.10	0.75
11.00	33.49	49.43	2.29	113.25	2.38	0.10	0.75
11.10	30.97	45.91	2.52	115.79	2.43	0.10	0.75
11.20	27.24	40.68	2.93	119.12	2.49	0.10	0.74
11.30	22.91	34.55	3.55	122.61	2.58	0.09	0.73
11.40	18.96	28.82	4.33	124.91	2.66	0.09	0.62
11.50	15.45	23.63	5.26	124.40	2.75	0.09	0.62
11.60	12.82	19.45	6.26	121.74	2.83	0.08	0.62
11.70	10.68	16.00	7.33	117.34	2.91	0.08	0.62
11.80	8.66	12.76	8.77	111.86	3.00	0.08	0.62
11.90	7.50	10.88	10.18	110.75	3.08	0.08	0.80
12.00	8.19	11.99	9.97	119.52	3.07	0.08	0.87
12.10	11.14	16.70	7.86	131.27	2.94	0.08	0.62
12.20	15.23	22.88	5.83	133.47	2.80	0.09	0.62
12.30	19.15	28.22	4.43	124.86	2.67	0.09	0.62
12.40	21.99	31.83	3.58	113.85	2.58	0.09	0.72
12.50	24.28	34.72	3.14	108.89	2.52	0.09	0.72
12.60	25.49	36.34	3.11	112.93	2.52	0.10	0.73
12.70	25.26	36.13	3.38	121.95	2.55	0.10	0.73
12.80	22.79	32.82	3.97	130.28	2.62	0.09	0.62
12.90	19.03	27.60	4.88	134.79	2.72	0.09	0.62
13.00	15.05	21.95	6.17	135.39	2.82	0.09	0.62
13.10	11.64	17.00	7.89	134.12	2.95	0.08	0.62
13.20	9.43	13.47	9.79	131.96	3.06	0.08	0.96
13.30	8.27	11.61	11.13	129.16	3.13	0.08	0.83
13.40	7.40	10.22	12.22	124.80	3.18	0.08	0.73
13.50	6.61	8.94	13.34	119.25	3.23	0.07	0.64
13.60	6.06	8.06	14.16	114.12	3.26	0.07	0.58
13.70	5.98	7.90	13.96	110.30	3.25	0.07	0.56
13.80	5.98	7.87	13.39	105.35	3.23	0.07	0.56
13.90	5.98	7.83	12.78	100.08	3.20	0.07	0.56
14.00	5.83	7.57	12.55	95.03	3.19	0.07	0.54
14.10	5.63	7.24	12.72	92.13	3.20	0.07	0.52
14.20	5.64	7.22	12.95	93.54	3.21	0.07	0.52
14.30	6.24	8.10	12.42	100.58	3.19	0.07	0.58
14.40	7.17	9.47	11.53	109.14	3.14	0.08	0.68

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
14.50	7.57	10.02	11.38	113.98	3.14	0.08	0.72
14.60	7.18	9.39	12.25	115.06	3.18	0.08	0.67
14.70	6.44	8.26	13.95	115.27	3.25	0.07	0.59
14.80	6.04	7.63	15.27	116.57	3.30	0.07	0.55
14.90	5.98	7.51	15.52	116.52	3.31	0.07	0.54
15.00	5.98	7.47	15.13	113.05	3.30	0.07	0.53
15.10	5.98	7.44	14.52	108.04	3.27	0.07	0.53
15.20	5.98	7.41	13.98	103.61	3.25	0.07	0.53
15.30	5.98	7.38	13.59	100.27	3.24	0.07	0.53
15.40	5.98	7.35	13.33	97.93	3.23	0.07	0.52
15.50	5.98	7.32	13.30	97.31	3.22	0.07	0.52
15.60	6.05	7.40	13.44	99.43	3.23	0.07	0.53
15.70	6.60	8.15	13.06	106.52	3.21	0.07	0.58
15.80	7.40	9.26	12.54	116.20	3.19	0.08	0.66
15.90	8.12	10.25	12.21	125.19	3.18	0.08	0.73
16.00	8.37	10.57	12.33	130.36	3.18	0.08	0.76
16.10	8.36	10.52	12.54	131.94	3.19	0.08	0.75
16.20	7.83	9.73	13.19	128.33	3.22	0.08	0.69
16.30	6.82	8.26	14.53	120.04	3.27	0.07	0.59
16.40	5.50	6.37	16.91	107.79	3.36	0.07	0.46
16.50	4.57	5.04	19.26	97.08	3.44	0.07	0.36
16.60	4.32	4.66	19.86	92.57	3.46	0.07	0.33
16.70	4.93	5.50	17.52	96.33	3.38	0.07	0.39
16.80	5.99	6.95	14.63	101.72	3.28	0.07	0.50
16.90	6.79	8.03	12.87	103.38	3.21	0.08	0.57
17.00	6.62	7.76	12.86	99.77	3.21	0.07	0.55
17.10	5.62	6.35	14.78	93.88	3.28	0.07	0.45
17.20	4.35	4.58	19.04	87.21	3.43	0.07	0.33
17.30	3.44	3.32	24.47	81.29	3.58	0.07	0.24
17.40	3.24	3.04	25.98	78.90	3.62	0.07	0.22
17.50	3.46	3.32	23.95	79.45	3.57	0.07	0.24
17.60	4.20	4.31	19.81	85.35	3.46	0.07	0.31
17.70	5.21	5.66	16.67	94.43	3.35	0.07	0.40
17.80	6.62	7.55	14.10	106.39	3.26	0.07	0.54
17.90	7.68	8.94	12.89	115.24	3.21	0.08	0.64
18.00	8.46	9.95	12.22	121.60	3.18	0.08	0.71
18.10	9.19	10.90	11.71	127.56	3.15	0.08	0.78
18.20	10.11	12.08	11.15	134.61	3.13	0.08	0.86
18.30	11.39	13.73	10.40	142.78	3.09	0.08	0.98
18.40	12.95	15.75	9.49	149.44	3.04	0.08	1.13
18.50	15.09	18.52	8.33	154.33	2.97	0.09	0.62
18.60	17.76	21.88	7.13	155.98	2.89	0.09	0.62
18.70	21.28	26.10	5.90	153.88	2.80	0.09	0.62
18.80	25.82	31.44	4.71	148.07	2.70	0.10	0.62
18.90	31.54	38.07	3.68	140.07	2.59	0.10	0.74
19.00	37.82	45.24	2.95	133.67	2.50	0.11	0.75
19.10	43.39	51.55	2.56	131.93	2.43	0.12	0.77
19.20	48.52	57.34	2.33	133.34	2.39	0.12	0.77

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
19.30	55.06	64.65	2.08	134.36	2.34	0.12	0.78
19.40	66.32	77.08	1.74	134.27	2.25	0.14	0.80
19.50	80.83	92.82	1.48	137.72	2.14	0.16	0.82
19.60	88.75	101.14	1.40	141.30	2.08	0.19	0.84
19.70	81.34	92.71	1.45	134.56	2.12	0.17	0.83
19.80	68.26	78.36	1.71	134.09	2.24	0.13	0.79
19.90	59.34	68.63	2.16	148.22	2.36	0.13	0.79
20.00	53.32	61.83	2.56	158.59	2.43	0.14	0.80
20.10	41.41	48.08	3.25	156.41	2.54	0.11	0.76
20.20	26.61	30.82	4.77	146.98	2.71	0.09	0.62
20.30	17.09	19.57	6.95	136.07	2.88	0.09	0.62
20.40	13.44	15.07	8.53	128.60	2.99	0.08	0.62
20.50	11.12	12.17	9.81	119.45	3.06	0.08	0.87
20.60	9.65	10.33	10.61	109.61	3.10	0.08	0.74
20.70	8.78	9.23	10.97	101.33	3.12	0.08	0.66
20.80	8.37	8.70	11.10	96.57	3.12	0.08	0.62
20.90	8.37	8.67	10.98	95.21	3.12	0.08	0.62
21.00	8.21	8.46	11.11	93.93	3.12	0.08	0.60
21.10	7.65	7.74	11.77	91.14	3.16	0.08	0.55
21.20	6.85	6.76	12.89	87.10	3.21	0.07	0.48
21.30	6.21	5.96	14.03	83.63	3.25	0.07	0.43
21.40	6.04	5.75	14.58	83.80	3.28	0.07	0.41
21.50	6.56	6.34	14.24	90.29	3.26	0.07	0.45
21.60	8.06	8.11	12.83	104.05	3.20	0.07	0.58
21.70	10.65	11.16	10.78	120.34	3.11	0.08	0.80
21.80	13.72	14.76	9.01	133.07	3.01	0.08	1.05
21.90	16.18	17.62	7.92	139.48	2.95	0.09	0.62
22.00	17.19	18.75	7.55	141.48	2.92	0.09	0.62
22.10	16.91	18.34	7.78	142.78	2.94	0.09	0.62
22.20	16.26	17.53	8.32	145.89	2.97	0.09	0.62
22.30	16.46	17.70	8.50	150.49	2.98	0.09	0.62
22.40	18.11	19.55	7.92	154.82	2.95	0.09	0.62
22.50	21.27	23.06	6.75	155.60	2.87	0.09	0.62
22.60	25.33	27.46	5.47	150.32	2.77	0.10	0.62
22.70	29.04	31.36	4.42	138.72	2.67	0.10	0.62
22.80	31.21	33.53	3.73	125.00	2.60	0.10	0.74
22.90	31.37	33.54	3.46	115.88	2.56	0.10	0.74
23.00	29.97	31.93	3.63	115.94	2.59	0.10	0.73
23.10	27.89	29.64	4.19	124.09	2.65	0.10	0.62
23.20	25.85	27.43	4.92	135.01	2.72	0.09	0.62
23.30	23.86	25.23	5.68	143.34	2.79	0.09	0.62
23.40	21.26	22.35	6.60	147.53	2.86	0.09	0.62
23.50	17.88	18.55	7.94	147.32	2.95	0.09	0.62
23.60	14.85	15.09	9.68	146.07	3.05	0.08	1.08
23.70	13.28	13.28	10.97	145.74	3.12	0.08	0.95
23.80	12.51	12.39	11.48	142.23	3.14	0.08	0.88
23.90	11.58	11.31	11.79	133.35	3.16	0.08	0.81
24.00	10.09	9.63	12.48	120.18	3.19	0.08	0.69

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
24.10	8.71	8.07	13.51	109.01	3.23	0.08	0.58
24.20	7.82	7.07	14.55	102.84	3.28	0.07	0.50
24.30	7.70	6.90	14.82	102.28	3.29	0.07	0.49
24.40	8.15	7.38	14.29	105.43	3.27	0.08	0.53
24.50	8.70	7.96	13.60	108.26	3.24	0.08	0.57
24.60	8.57	7.78	13.70	106.67	3.24	0.08	0.56
24.70	7.74	6.86	14.69	100.75	3.28	0.07	0.49
24.80	6.79	5.80	16.04	93.07	3.33	0.07	0.41
24.90	6.15	5.09	17.00	86.47	3.37	0.07	0.36
25.00	5.98	4.89	17.09	83.52	3.37	0.07	0.35
25.10	6.01	4.90	17.07	83.73	3.37	0.07	0.35
25.20	6.34	5.24	16.71	87.60	3.36	0.07	0.37
25.30	7.03	5.97	15.79	94.30	3.32	0.07	0.43
25.40	7.80	6.77	14.90	100.93	3.29	0.07	0.48
25.50	8.27	7.25	14.52	105.30	3.27	0.08	0.52
25.60	8.37	7.33	14.64	107.36	3.28	0.08	0.52
25.70	8.13	7.05	15.20	107.22	3.30	0.08	0.50
25.80	7.53	6.40	16.43	105.07	3.35	0.07	0.46
25.90	7.11	5.93	17.55	104.06	3.38	0.07	0.42
26.00	7.40	6.22	17.32	107.69	3.38	0.07	0.44
26.10	8.52	7.37	15.73	115.94	3.32	0.08	0.53
26.20	9.73	8.62	14.35	123.61	3.27	0.08	0.62
26.30	10.47	9.37	13.69	128.26	3.24	0.08	0.67
26.40	10.75	9.63	13.57	130.62	3.24	0.08	0.69
26.50	10.76	9.61	13.74	132.04	3.24	0.08	0.69
26.60	10.76	9.58	13.91	133.25	3.25	0.08	0.68
26.70	10.76	9.55	14.06	134.20	3.26	0.08	0.68
26.80	10.76	9.52	14.19	135.04	3.26	0.08	0.68
26.90	10.76	9.48	14.34	135.97	3.27	0.08	0.68
27.00	10.76	9.45	14.45	136.64	3.27	0.08	0.68
27.10	10.76	9.42	14.53	136.88	3.27	0.08	0.67
27.20	10.76	9.39	14.53	136.47	3.27	0.08	0.67
27.30	10.62	9.22	14.57	134.41	3.28	0.08	0.66
27.40	10.09	8.65	14.95	129.24	3.29	0.08	0.62
27.50	9.29	7.81	15.59	121.84	3.32	0.08	0.56
27.60	8.63	7.12	16.08	114.51	3.33	0.07	0.51
27.70	8.37	6.83	16.02	109.46	3.33	0.07	0.49
27.80	8.37	6.81	15.67	106.68	3.32	0.07	0.49
27.90	8.49	6.91	15.34	106.03	3.31	0.07	0.49
28.00	8.69	7.09	15.10	107.03	3.30	0.08	0.51
28.10	8.89	7.27	14.91	108.37	3.29	0.08	0.52
28.20	9.37	7.73	14.29	110.43	3.27	0.08	0.55
28.30	9.97	8.30	13.53	112.26	3.23	0.08	0.59
28.40	10.57	8.87	12.83	113.72	3.20	0.08	0.63
28.50	10.98	9.25	12.38	114.46	3.18	0.08	0.66
28.60	11.67	9.90	11.76	116.48	3.16	0.08	0.71
28.70	12.47	10.66	11.16	118.95	3.13	0.08	0.76
28.80	13.04	11.19	10.82	121.06	3.11	0.08	0.80

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
28.90	13.15	11.26	10.87	122.36	3.11	0.08	0.80
29.00	13.15	11.23	11.00	123.50	3.12	0.08	0.80
29.10	13.15	11.19	11.04	123.61	3.12	0.08	0.80
29.20	13.15	11.16	10.93	122.04	3.12	0.08	0.80
29.30	12.81	10.80	10.94	118.22	3.12	0.08	0.77
29.40	12.02	10.01	11.25	112.62	3.13	0.08	0.71
29.50	11.23	9.21	11.65	107.30	3.15	0.08	0.66
29.60	10.91	8.88	11.78	104.58	3.16	0.08	0.63
29.70	11.76	9.66	11.07	106.96	3.12	0.08	0.69
29.80	12.59	10.43	10.59	110.50	3.10	0.08	0.75
29.90	13.04	10.83	10.49	113.64	3.09	0.08	0.77
30.00	13.53	11.27	10.35	116.63	3.09	0.08	0.81
30.10	14.07	11.76	10.11	118.88	3.07	0.08	0.84
30.20	14.43	12.07	9.94	119.91	3.06	0.08	0.86
30.30	13.96	11.58	10.22	118.41	3.08	0.08	0.83
30.40	13.58	11.19	10.42	116.67	3.09	0.08	0.80
30.50	13.33	10.92	10.60	115.77	3.10	0.08	0.78
30.60	12.70	10.30	11.21	115.52	3.13	0.08	0.74
30.70	12.12	9.72	12.09	117.55	3.17	0.08	0.69
30.80	13.30	10.80	11.61	125.41	3.15	0.08	0.77
30.90	17.68	14.86	9.21	136.92	3.02	0.08	1.06
31.00	25.04	21.68	6.63	143.72	2.86	0.09	0.62
31.10	33.65	29.66	4.72	140.06	2.70	0.10	0.62
31.20	41.52	36.92	3.50	129.37	2.57	0.11	0.75
31.30	47.08	42.02	2.87	120.67	2.48	0.11	0.76
31.40	50.34	44.94	2.63	118.39	2.45	0.11	0.76
31.50	51.88	46.26	2.59	119.70	2.44	0.12	0.77
31.60	53.14	47.32	2.52	119.29	2.43	0.12	0.77
31.70	54.44	48.41	2.41	116.57	2.41	0.12	0.77
31.80	55.69	49.46	2.32	114.90	2.39	0.12	0.77
31.90	56.99	50.55	2.27	114.60	2.38	0.12	0.77
32.00	58.46	51.79	2.19	113.24	2.36	0.12	0.78
32.10	59.74	52.86	2.08	109.98	2.34	0.12	0.78
32.20	60.86	53.78	1.99	107.01	2.32	0.12	0.78
32.30	62.07	54.77	1.96	107.29	2.31	0.12	0.78
32.40	62.52	55.04	2.01	110.91	2.32	0.12	0.78
32.50	59.72	52.33	2.24	117.14	2.37	0.13	0.78
32.60	52.72	45.80	2.75	125.85	2.46	0.12	0.77
32.70	42.27	36.19	3.74	135.27	2.60	0.11	0.75
32.80	31.38	26.26	5.36	140.82	2.76	0.10	0.62
32.90	22.36	18.12	7.68	139.16	2.93	0.09	0.62
33.00	16.47	12.87	10.19	131.21	3.08	0.08	0.92
33.10	13.22	9.97	12.13	120.88	3.17	0.08	0.71
33.20	11.88	8.77	12.75	111.78	3.20	0.08	0.63
33.30	11.95	8.80	12.07	106.22	3.17	0.08	0.63
33.40	11.78	8.63	11.82	101.98	3.16	0.08	0.62
33.50	11.11	8.02	12.30	98.61	3.18	0.08	0.57
33.60	11.31	8.17	12.30	100.53	3.18	0.08	0.58

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
33.70	12.29	9.01	11.66	105.05	3.15	0.08	0.64
33.80	13.31	9.86	10.98	108.34	3.12	0.08	0.70
33.90	13.96	10.41	10.56	109.90	3.10	0.08	0.74
34.00	14.67	11.00	10.21	112.22	3.08	0.08	0.79
34.10	15.54	11.71	9.94	116.39	3.06	0.08	0.84
34.20	15.54	11.68	10.25	119.70	3.08	0.08	0.83
34.30	16.11	12.14	10.38	125.97	3.09	0.08	0.87
34.40	19.78	15.26	9.29	141.78	3.03	0.08	1.09
34.50	27.81	22.07	7.19	158.74	2.90	0.09	0.62
34.60	38.35	31.15	5.24	163.38	2.75	0.11	0.62
34.70	49.92	41.21	3.74	154.16	2.60	0.12	0.76
34.80	62.64	52.31	2.74	143.11	2.46	0.13	0.78
34.90	79.13	66.70	2.13	142.02	2.35	0.15	0.81
35.00	99.48	84.48	1.75	147.48	2.25	0.18	0.83
35.10	120.93	103.28	1.51	155.49	2.15	0.23	0.86
35.20	140.29	120.35	1.37	164.43	2.06	0.29	0.87
35.30	155.97	134.18	1.30	173.87	1.99	0.33	0.88
35.40	167.22	144.01	1.26	182.05	1.94	0.40	0.88
35.50	172.04	148.00	1.26	186.30	1.93	0.46	0.88
35.60	169.35	145.24	1.27	184.86	1.95	0.43	0.88
35.70	162.62	138.93	1.29	179.62	1.98	0.36	0.88
35.80	153.39	130.51	1.31	171.55	2.01	0.34	0.88
35.90	142.33	120.54	1.34	162.10	2.04	0.28	0.87
36.00	127.98	107.67	1.41	152.06	2.10	0.23	0.86
36.10	111.52	92.97	1.57	145.72	2.18	0.20	0.85
36.20	94.75	78.10	1.87	146.32	2.29	0.17	0.83
36.30	81.09	66.05	2.32	153.12	2.39	0.15	0.81
36.40	77.71	62.92	2.56	161.10	2.43	0.14	0.80
36.50	89.74	73.00	2.25	164.17	2.38	0.16	0.81
36.60	116.69	95.99	1.74	166.66	2.24	0.22	0.85
36.70	151.21	125.75	1.42	178.50	2.10	0.37	0.89
36.80	183.51	153.75	1.30	199.49	1.99	0.68	0.91
36.90	207.83	174.76	1.25	218.63	1.92	0.91	0.91
37.00	225.84	190.03	1.23	234.36	1.89	0.92	0.92
37.10	236.91	199.16	1.23	244.58	1.89	0.93	0.93
37.20	240.81	202.11	1.23	248.10	1.89	0.93	0.93
37.30	235.84	197.44	1.23	243.25	1.89	0.93	0.93
37.40	225.38	188.09	1.24	233.40	1.91	0.92	0.92
37.50	213.17	177.28	1.25	221.78	1.92	0.91	0.92
37.60	201.83	167.31	1.26	210.53	1.93	0.83	0.91
37.70	194.32	160.72	1.26	202.21	1.93	0.65	0.90
37.80	192.34	158.91	1.25	198.83	1.92	0.58	0.89
37.90	195.72	161.54	1.25	201.20	1.91	0.64	0.89
38.00	202.49	166.84	1.25	208.20	1.92	0.83	0.90
38.10	209.96	172.55	1.26	217.04	1.93	0.91	0.92
38.20	216.55	177.42	1.27	225.56	1.95	0.91	0.93
38.30	221.69	181.09	1.28	232.42	1.97	0.91	0.94
38.40	225.49	183.72	1.29	237.27	1.98	0.92	0.94

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
38.50	228.03	185.33	1.30	240.44	1.99	0.92	0.95
38.60	228.61	185.34	1.30	241.49	1.99	0.92	0.95
38.70	226.29	182.93	1.31	239.89	2.00	0.92	0.95
38.80	221.32	178.34	1.32	235.81	2.02	0.91	0.95
38.90	215.06	172.72	1.33	230.49	2.03	0.91	0.94
39.00	208.89	167.21	1.35	225.14	2.04	0.90	0.94
39.10	203.92	162.78	1.35	220.27	2.05	0.90	0.93
39.20	201.00	160.10	1.35	216.67	2.05	0.90	0.93
39.30	200.94	159.85	1.35	215.07	2.04	0.90	0.93
39.40	203.86	162.06	1.33	216.08	2.03	0.90	0.93
39.50	209.63	166.61	1.32	219.76	2.01	0.90	0.93
39.60	217.99	173.26	1.30	226.10	2.00	0.91	0.94
39.70	228.76	181.83	1.29	235.07	1.98	0.91	0.94
39.80	241.19	191.65	1.28	246.15	1.97	0.92	0.95
39.90	254.27	201.91	1.28	258.19	1.96	0.93	0.96
40.00	265.96	210.97	1.28	269.15	1.96	0.94	0.97
40.10	276.78	219.35	1.27	278.88	1.95	0.94	0.98
40.20	286.88	227.30	1.26	286.91	1.94	0.95	0.98
40.30	297.01	235.49	1.25	293.69	1.92	0.96	0.98
40.40	305.93	242.83	1.23	298.50	1.89	0.96	0.98
40.50	313.36	248.89	1.21	301.93	1.87	0.96	0.98
40.60	319.25	253.48	1.20	305.08	1.85	0.97	0.98
40.70	323.81	256.78	1.20	308.25	1.85	0.97	0.98
40.80	326.58	258.58	1.20	310.12	1.85	0.97	0.98
40.90	326.95	258.50	1.20	309.42	1.85	0.97	0.98
41.00	324.52	256.18	1.20	306.29	1.84	0.97	0.98
41.10	319.51	251.59	1.20	302.19	1.85	0.97	0.98
41.20	312.79	245.39	1.21	297.74	1.87	0.96	0.98
41.30	304.61	237.91	1.23	292.57	1.89	0.96	0.98
41.40	293.60	228.19	1.25	284.54	1.92	0.95	0.98
41.50	278.40	215.25	1.26	272.15	1.94	0.94	0.97
41.60	258.94	199.13	1.28	255.30	1.97	0.93	0.96
41.70	237.94	182.03	1.30	236.47	1.99	0.92	0.95
41.80	218.97	166.71	1.31	219.18	2.01	0.90	0.93
41.90	200.61	151.83	1.34	203.34	2.04	0.89	0.93
42.00	180.78	135.61	1.40	189.41	2.08	0.61	0.91
42.10	157.20	116.35	1.53	178.56	2.17	0.39	0.89
42.20	132.67	96.63	1.78	172.42	2.26	0.27	0.87
42.30	112.50	80.76	2.07	167.43	2.34	0.20	0.84
42.40	103.27	73.67	2.16	158.76	2.36	0.17	0.83
42.50	106.36	76.23	1.95	148.30	2.31	0.18	0.83
42.60	116.27	84.17	1.68	141.26	2.22	0.20	0.85
42.70	123.96	90.41	1.52	137.62	2.16	0.22	0.85
42.80	125.54	91.71	1.47	135.07	2.13	0.21	0.85
42.90	120.85	87.83	1.51	132.89	2.15	0.20	0.85
43.00	111.91	80.40	1.66	133.70	2.22	0.19	0.84
43.10	101.40	71.75	1.95	139.79	2.31	0.17	0.83
43.20	92.75	64.68	2.31	149.17	2.39	0.16	0.82

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
43.30	88.83	61.44	2.51	154.44	2.43	0.16	0.81
43.40	90.15	62.36	2.44	152.17	2.41	0.16	0.81
43.50	94.42	65.64	2.22	145.47	2.37	0.17	0.82
43.60	98.83	69.05	2.02	139.74	2.33	0.17	0.83
43.70	101.21	70.83	1.93	136.98	2.30	0.17	0.83
43.80	101.76	71.10	1.93	137.20	2.30	0.17	0.83
43.90	101.61	70.76	1.97	139.40	2.31	0.17	0.83
44.00	101.41	70.34	2.03	142.77	2.33	0.18	0.83
44.10	101.33	69.98	2.11	147.36	2.34	0.18	0.83
44.20	101.20	69.56	2.20	153.26	2.37	0.18	0.83
44.30	102.65	70.30	2.27	159.70	2.38	0.18	0.83
44.40	107.15	73.43	2.22	163.08	2.37	0.19	0.84
44.50	115.17	79.40	2.02	160.41	2.32	0.21	0.85
44.60	124.33	86.49	1.78	153.87	2.26	0.23	0.86
44.70	131.80	92.40	1.61	148.70	2.20	0.24	0.86
44.80	135.88	95.58	1.54	146.92	2.17	0.25	0.86
44.90	137.36	96.48	1.54	148.17	2.17	0.25	0.86
45.00	138.06	96.63	1.56	151.12	2.18	0.25	0.87
45.10	138.23	96.38	1.60	153.78	2.19	0.26	0.87
45.20	137.03	95.17	1.63	155.09	2.21	0.26	0.87
45.30	133.73	92.39	1.68	155.47	2.23	0.25	0.86
45.40	129.36	88.83	1.75	155.87	2.25	0.24	0.86
45.50	126.45	86.43	1.80	155.93	2.27	0.23	0.86
45.60	127.21	86.93	1.77	153.97	2.26	0.23	0.86
45.70	131.34	90.15	1.66	149.85	2.22	0.24	0.86
45.80	136.70	94.47	1.54	145.28	2.17	0.24	0.86
45.90	140.90	97.96	1.45	141.93	2.12	0.25	0.86
46.00	142.26	99.07	1.42	140.37	2.10	0.25	0.86
46.10	140.88	97.75	1.44	140.33	2.11	0.24	0.86
46.20	137.87	94.97	1.49	141.79	2.14	0.24	0.86
46.30	135.03	92.38	1.56	143.75	2.18	0.24	0.86
46.40	133.22	90.73	1.59	144.70	2.19	0.23	0.86
46.50	132.83	90.17	1.62	145.76	2.20	0.23	0.86
46.60	133.78	90.50	1.65	149.12	2.21	0.24	0.86
46.70	134.60	90.57	1.71	154.91	2.24	0.26	0.87
46.80	132.80	88.68	1.82	161.37	2.27	0.26	0.87
46.90	125.89	83.19	1.99	165.91	2.32	0.25	0.86
47.00	115.97	75.67	2.24	169.55	2.37	0.21	0.85
47.10	104.67	67.40	2.53	170.35	2.43	0.19	0.83
47.20	98.78	63.13	2.67	168.63	2.45	0.17	0.82
47.30	98.47	62.90	2.62	164.47	2.44	0.17	0.82
47.40	96.95	61.77	2.62	161.58	2.44	0.19	0.83
47.50	88.26	55.55	2.90	161.33	2.49	0.16	0.81
47.60	70.99	43.46	3.72	161.81	2.60	0.13	0.79
47.70	54.66	32.30	4.96	160.21	2.72	0.11	0.62
47.80	43.11	24.66	6.23	153.58	2.83	0.10	0.62
47.90	37.26	21.04	6.95	146.31	2.88	0.10	0.62
48.00	35.46	19.90	7.09	141.01	2.89	0.10	0.62

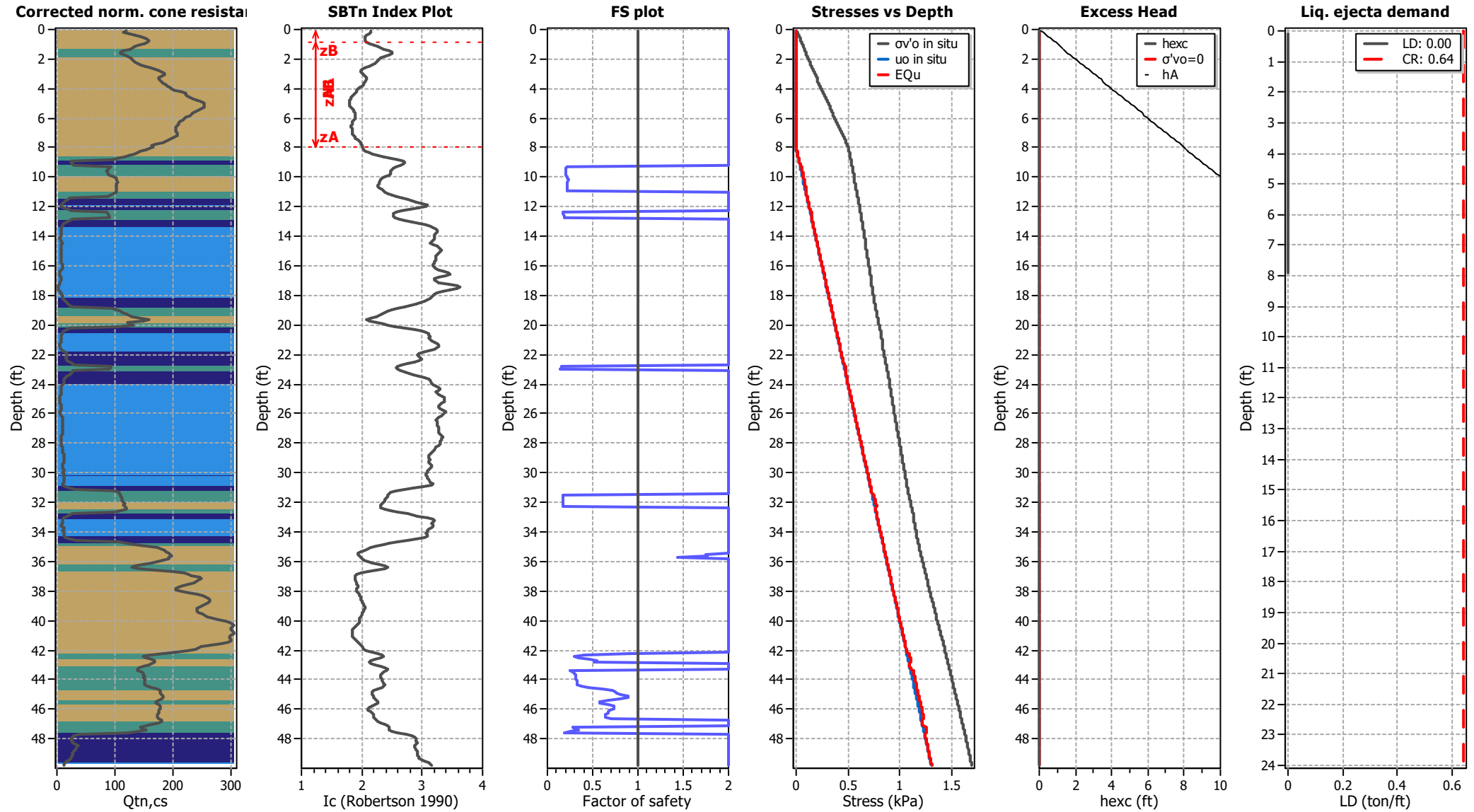
:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
48.10	35.37	19.80	7.12	141.08	2.89	0.10	0.62
48.20	36.65	20.54	7.28	149.41	2.90	0.10	0.62
48.30	39.52	22.24	7.43	165.15	2.91	0.10	0.62
48.40	43.87	24.83	7.24	179.87	2.90	0.11	0.62
48.50	47.02	26.68	6.96	185.63	2.88	0.11	0.62
48.60	46.83	26.51	6.88	182.33	2.88	0.11	0.62
48.70	43.44	24.41	7.13	173.95	2.89	0.11	0.62
48.80	39.99	22.29	7.47	166.43	2.92	0.10	0.62
48.90	37.97	21.03	7.65	160.86	2.93	0.10	0.62
49.00	37.11	20.47	7.66	156.88	2.93	0.10	0.62
49.10	36.51	20.07	7.67	153.90	2.93	0.10	0.62
49.20	35.49	19.43	7.77	150.91	2.94	0.10	0.62
49.30	33.74	18.34	8.03	147.20	2.95	0.10	0.62
49.40	30.37	16.30	8.65	140.97	2.99	0.09	0.62
49.50	26.08	13.72	9.65	132.46	3.05	0.09	0.98
49.60	22.32	11.46	10.77	123.51	3.11	0.08	0.82
49.70	20.21	10.20	11.47	117.01	3.14	0.08	0.73
49.80	19.41	9.70	11.73	113.79	3.15	0.08	0.69

Abbreviations

q_t :	Total cone resistance
K_c :	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c :	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

Ejecta Severity Estimation



LIQUEFACTION ANALYSIS REPORT

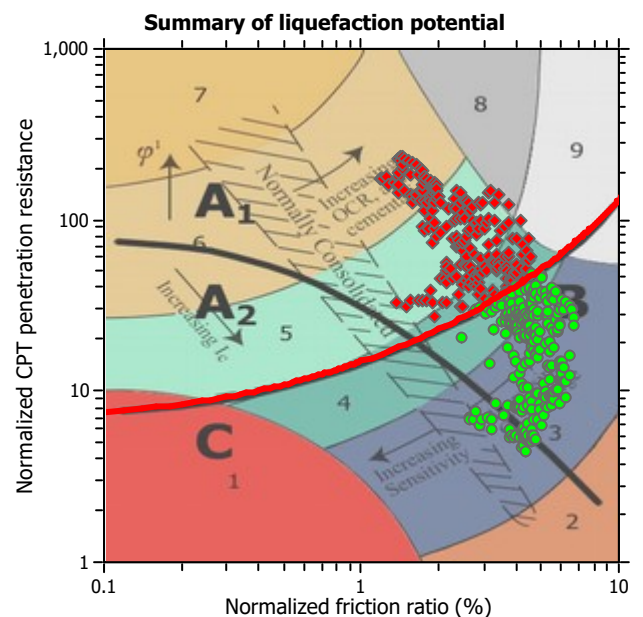
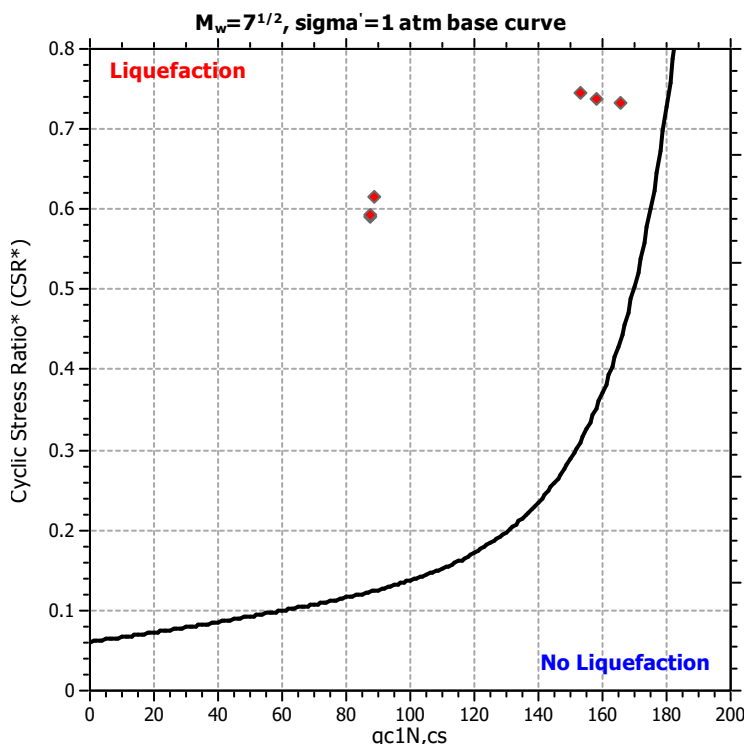
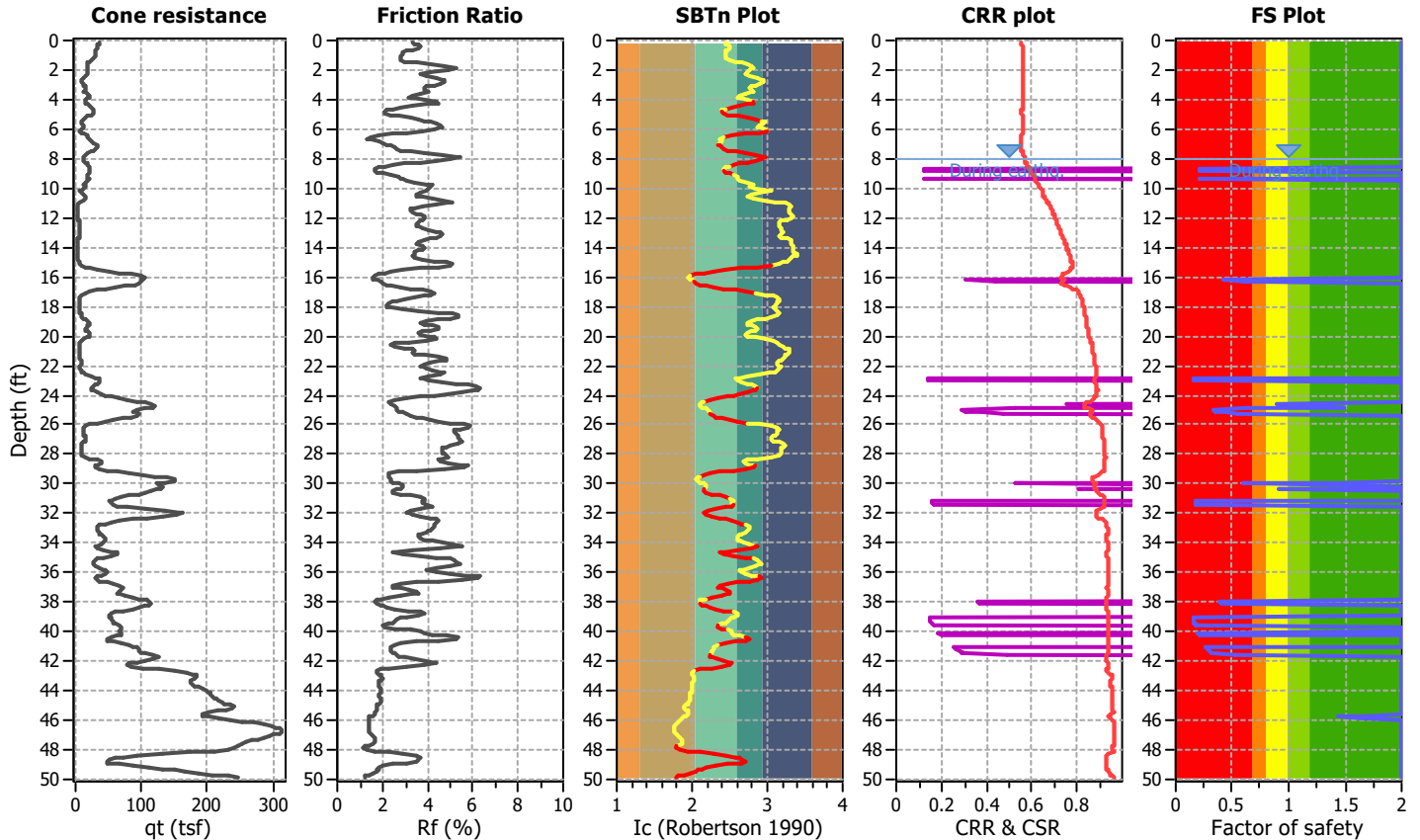
Project title : 21-483 Equestrian Estates

Location : Avenue 64 at Harrison Street, Thermal California

CPT file : CPT-5 B&I 2014

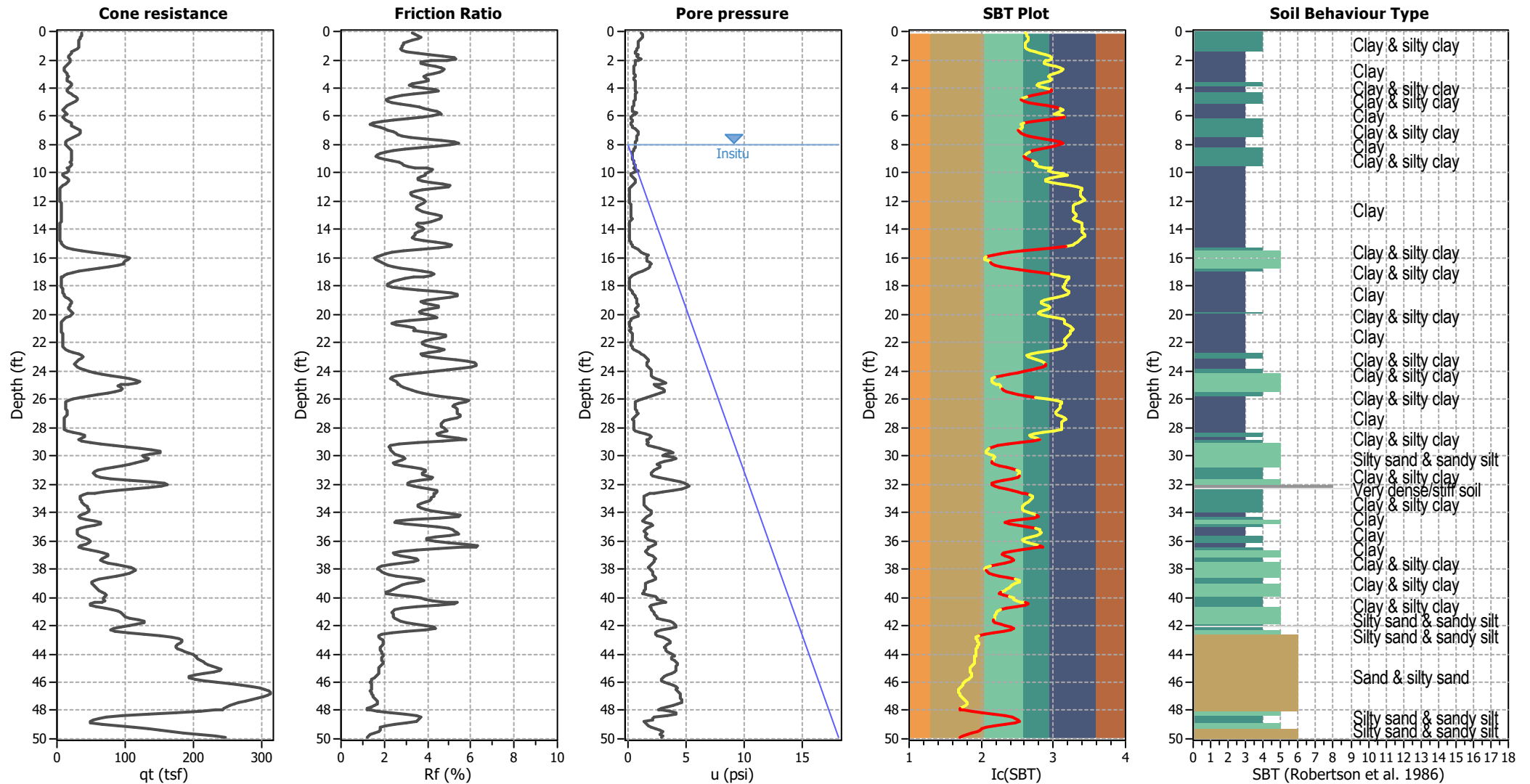
Input parameters and analysis data

Analysis method:	B&I (2014)	G.W.T. (in-situ):	8.00 ft	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	8.00 ft	Fill height:	N/A	Limit depth applied:	No
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth:	N/A
Earthquake magnitude M_w :	7.34	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.74	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		



Zone A₁: Cyclic liquefaction likely depending on size and duration of cyclic loading
 Zone A₂: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
 Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
 Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



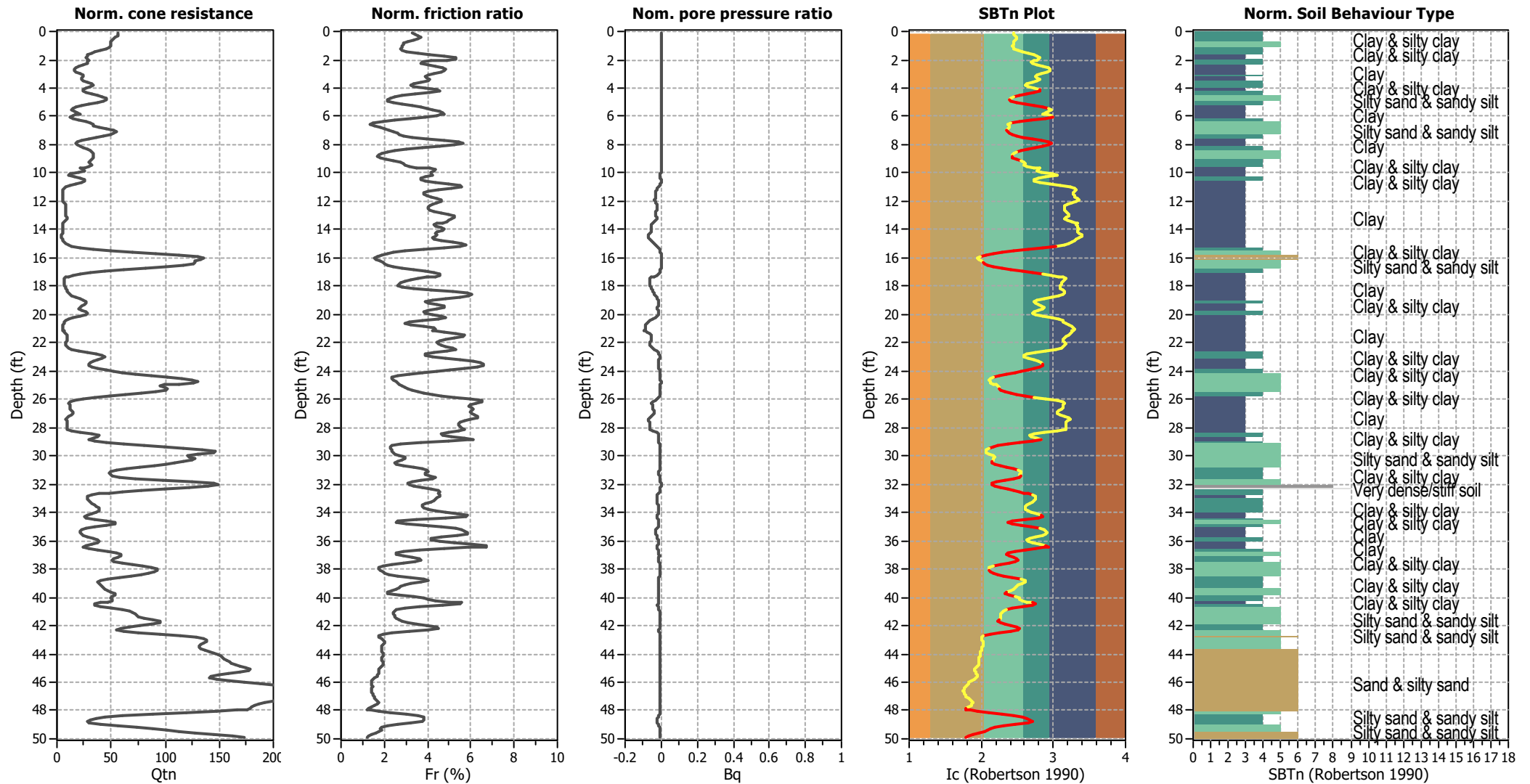
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on I_c value	I_c cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

SBT legend

1. Sensitive fine grained	4. Clayey silt to silty	7. Gravely sand to sand
2. Organic material	5. Silty sand to sandy silt	8. Very stiff sand to
3. Clay to silty clay	6. Clean sand to silty sand	9. Very stiff fine grained

CPT basic interpretation plots (normalized)



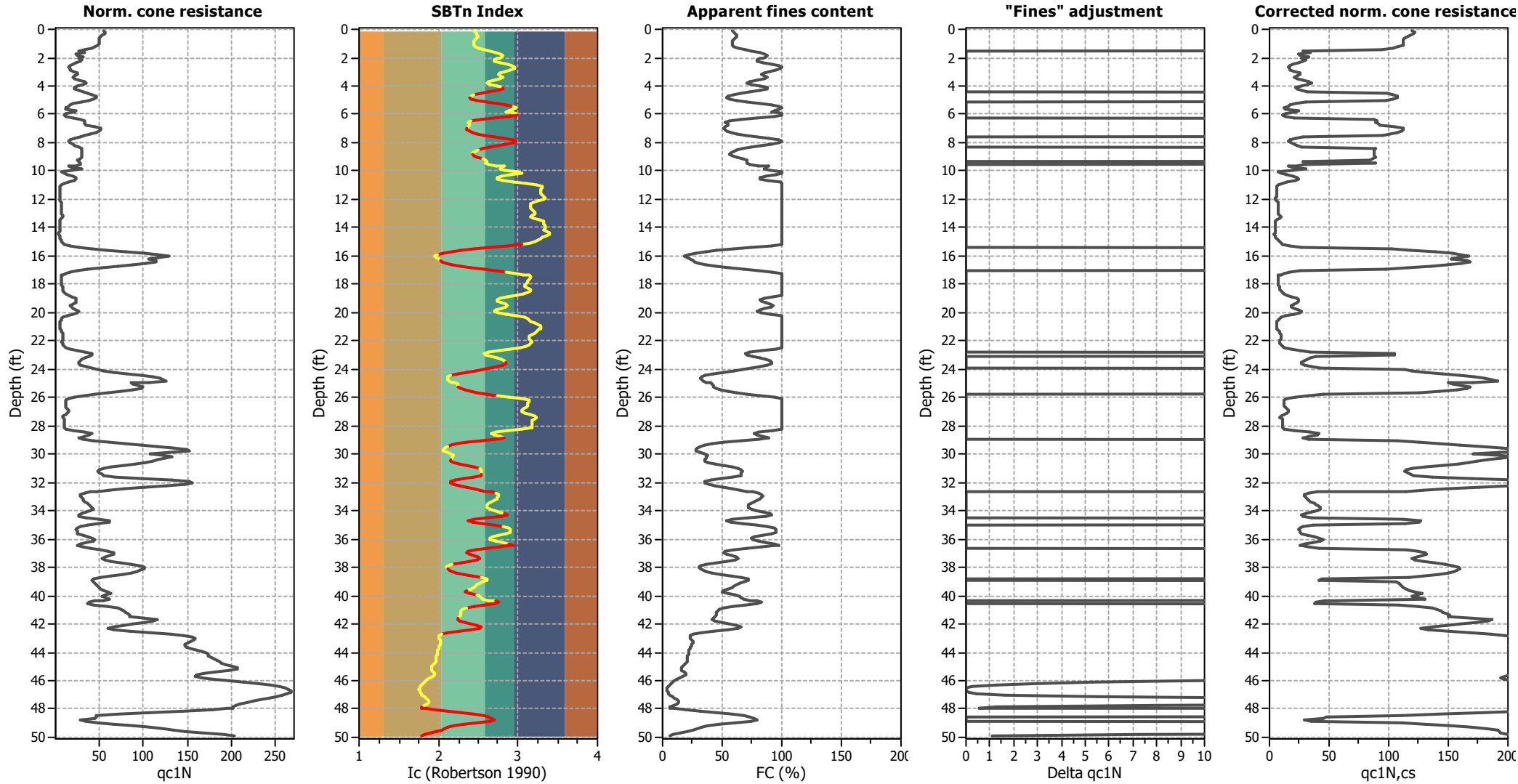
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	Yes
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

SBTn legend

1. Sensitive fine grained	4. Clayey silt to silty	7. Gravely sand to sand
2. Organic material	5. Silty sand to sandy silt	8. Very stiff sand to
3. Clay to silty clay	6. Clean sand to silty sand	9. Very stiff fine grained

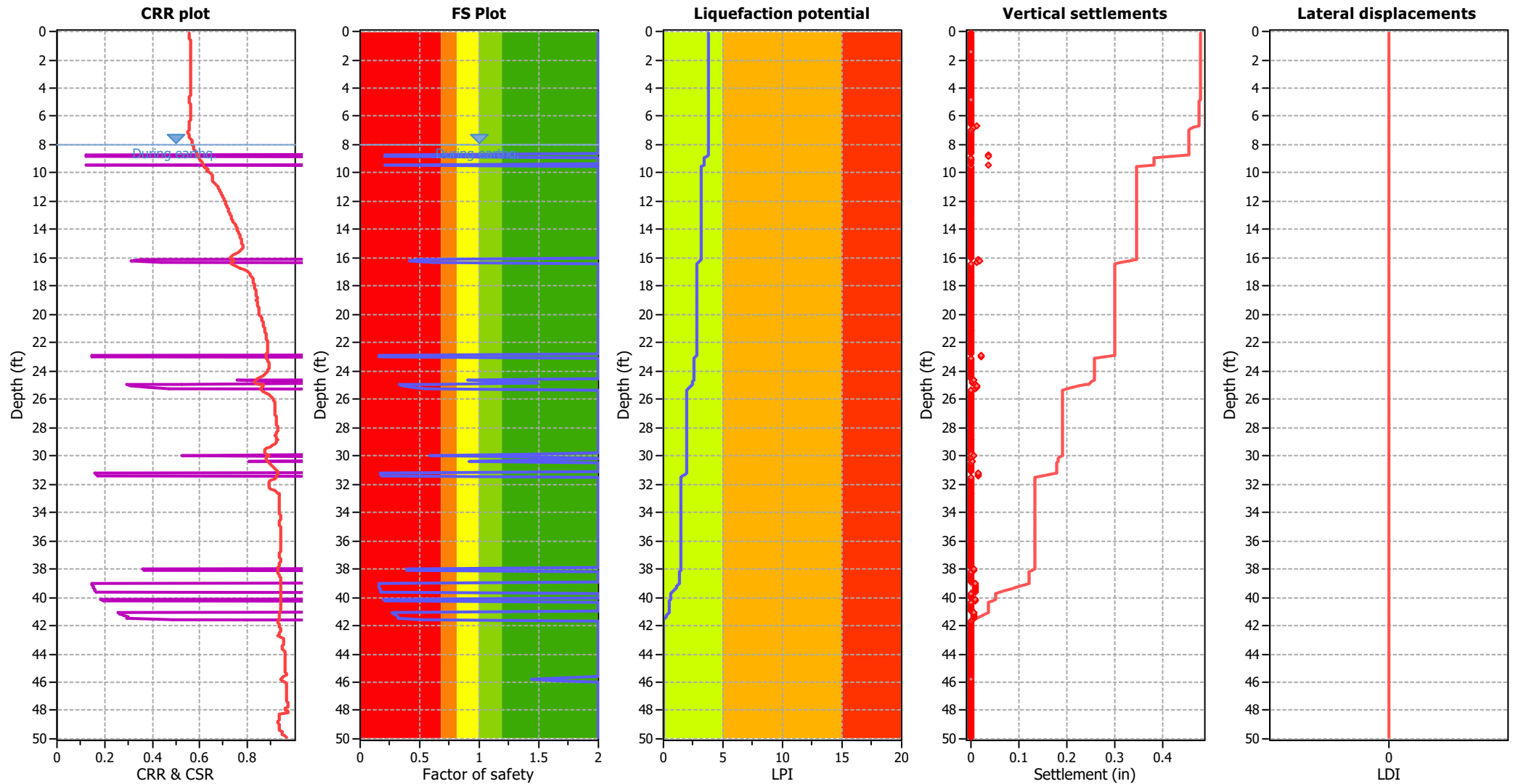
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on I_c value	I_c cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

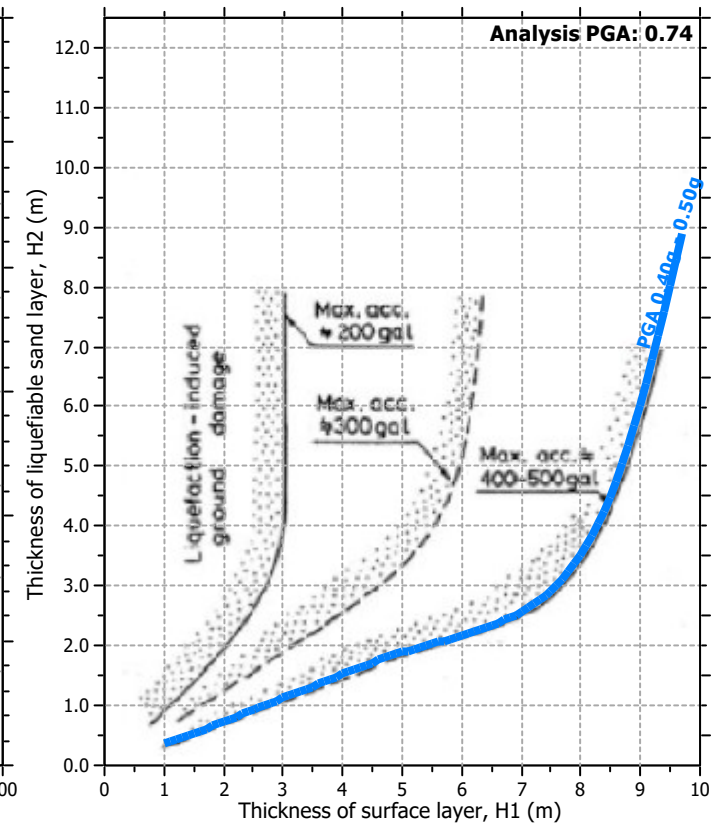
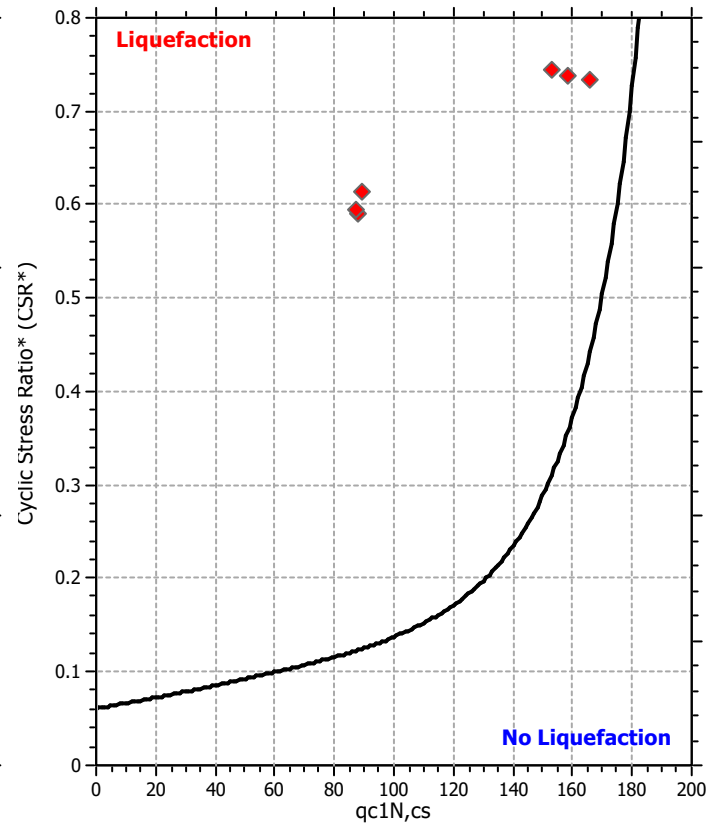
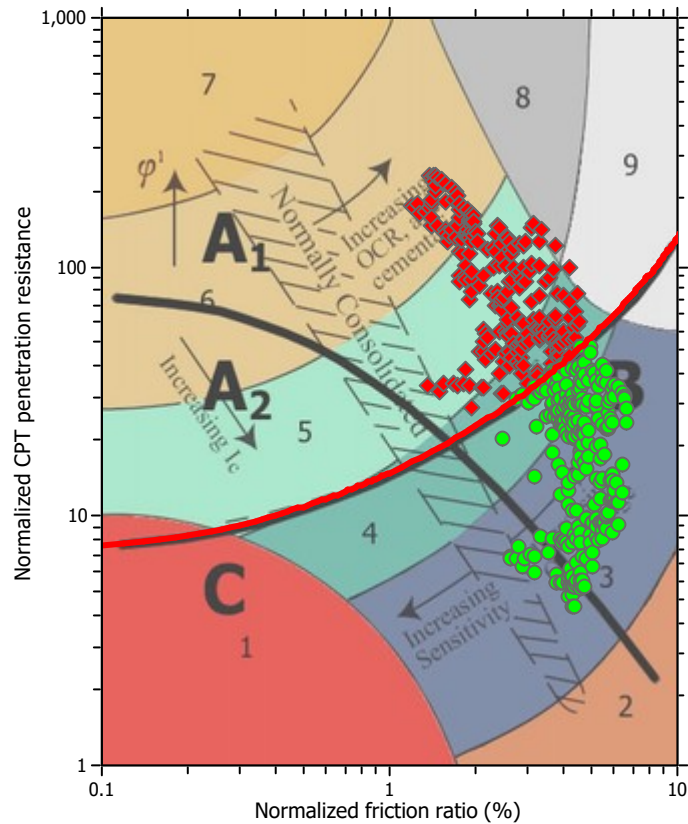
F.S. color scheme

Red	Almost certain it will liquefy
Orange	Very likely to liquefy
Yellow	Liquefaction and no liq. are equally likely
Light Green	Unlike to liquefy
Dark Green	Almost certain it will not liquefy

LPI color scheme

Red	Very high risk
Orange	High risk
Yellow	Low risk

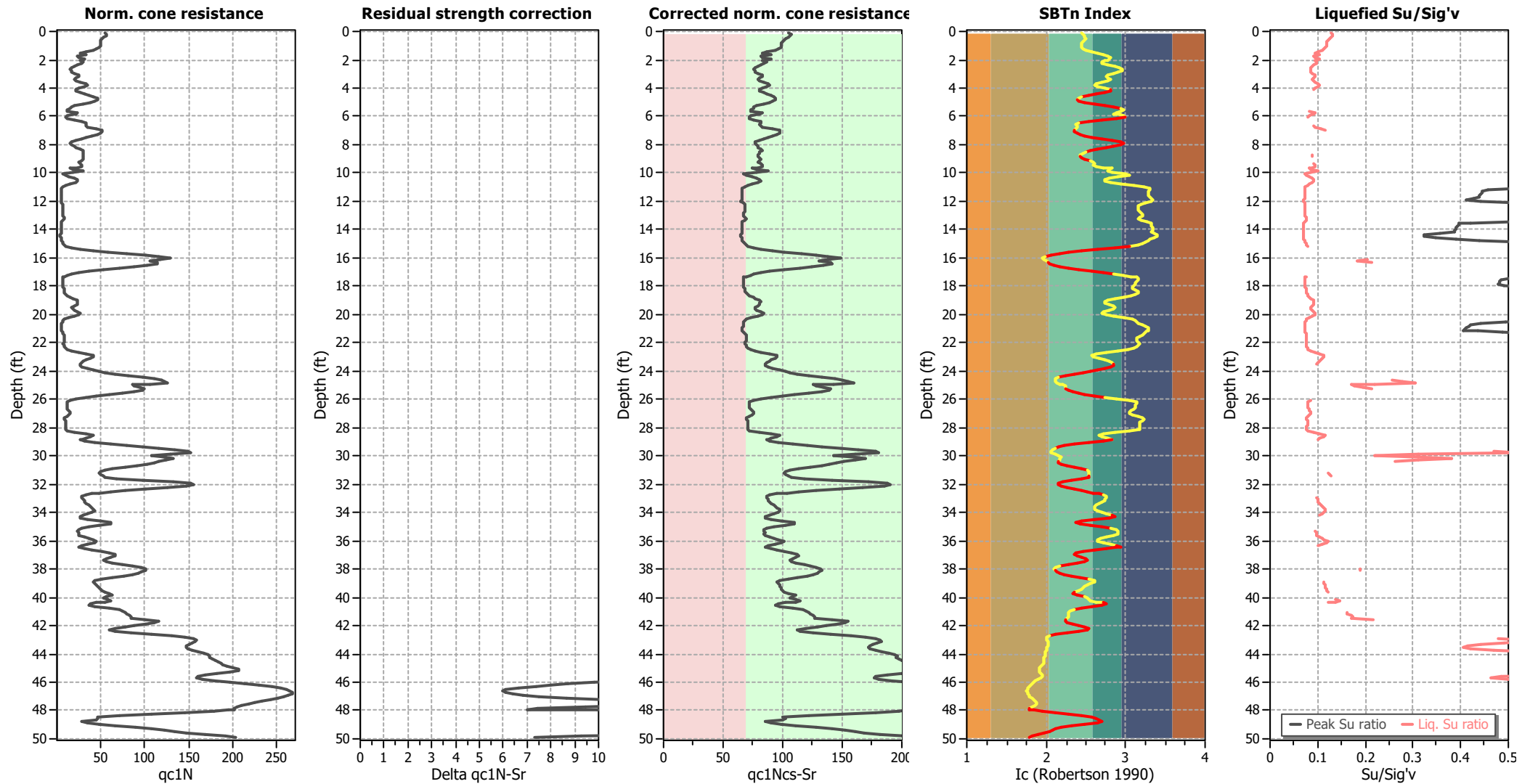
Liquefaction analysis summary plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

Check for strength loss plots (Idriss & Boulanger (2008))



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on I_c value	I_c cut-off value:	2.60	K_g applied:	Yes
Earthquake magnitude M_w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

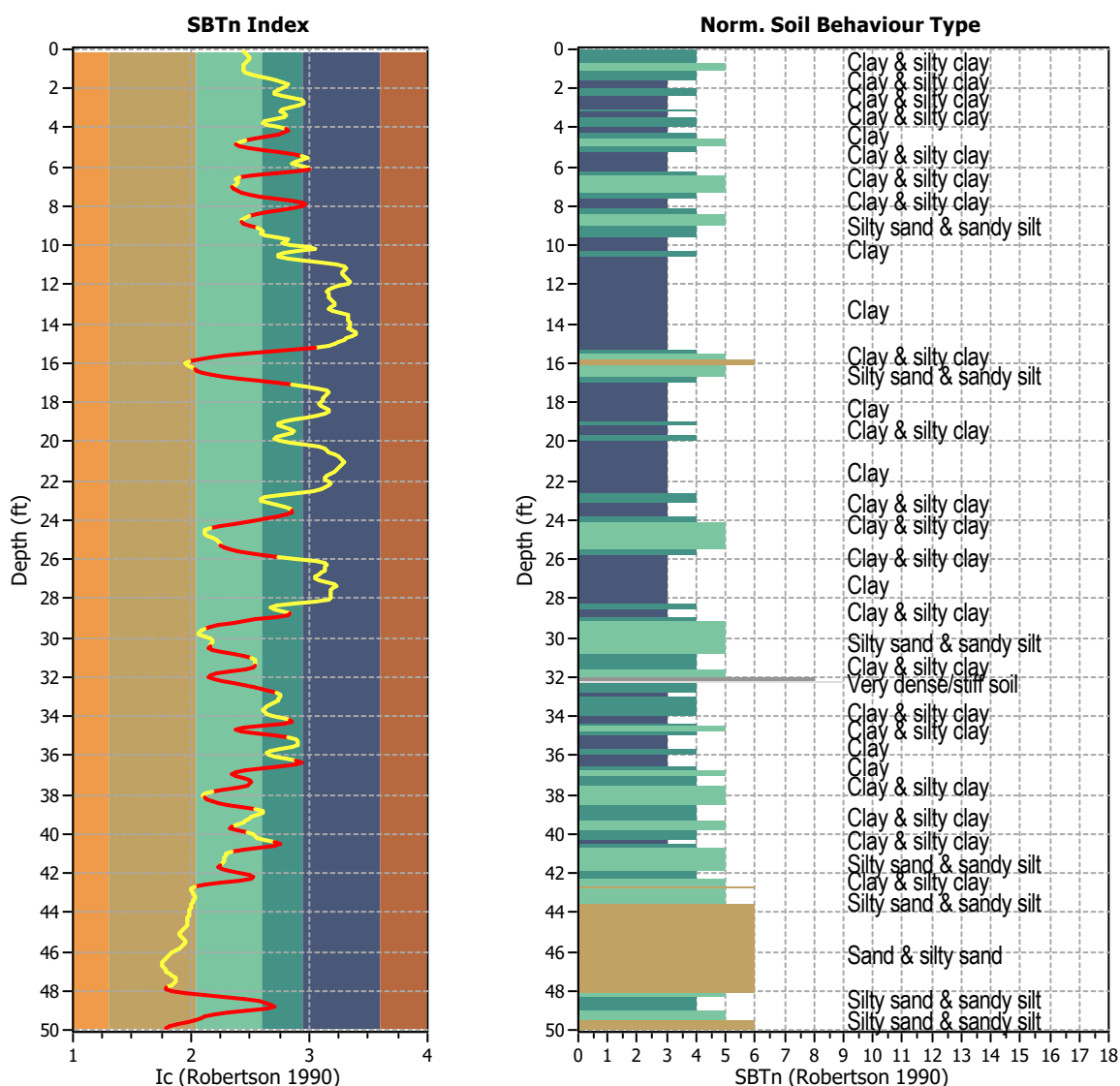
TRANSITION LAYER DETECTION ALGORITHM REPORT

Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vice-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between $1.80 < I_c < 3.0$) and a rate of change of I_c . Transitions typically occur when the rate of change of I_c is fast (i.e. ΔI_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties

I_c minimum check value: 1.70
 I_c maximum check value: 3.00
 I_c change ratio value: 0.0250
 Minimum number of points in layer: 4

General statistics

Total points in CPT file: 499
 Total points excluded: 181
 Exclusion percentage: 36.27%
 Number of layers detected: 26

Transition layer No	Number of points	Depth	SBT _n number	SBT _n description
Transition layer 1	6	Start depth: 4.20 (ft)	3	Clay
		End depth: 4.70 (ft)	5	Silty sand & sandy silt
Transition layer 2	7	Start depth: 4.90 (ft)	5	Silty sand & sandy silt
		End depth: 5.50 (ft)	3	Clay
Transition layer 3	5	Start depth: 6.20 (ft)	3	Clay
		End depth: 6.60 (ft)	5	Silty sand & sandy silt
Transition layer 4	9	Start depth: 7.10 (ft)	5	Silty sand & sandy silt
		End depth: 7.90 (ft)	3	Clay
Transition layer 5	8	Start depth: 7.90 (ft)	3	Clay
		End depth: 8.60 (ft)	5	Silty sand & sandy silt
Transition layer 6	4	Start depth: 8.90 (ft)	5	Silty sand & sandy silt
		End depth: 9.20 (ft)	4	Clay & silty clay
Transition layer 7	8	Start depth: 15.30 (ft)	3	Clay
		End depth: 16.00 (ft)	6	Sand & silty sand
Transition layer 8	9	Start depth: 16.40 (ft)	5	Silty sand & sandy silt
		End depth: 17.20 (ft)	3	Clay
Transition layer 9	10	Start depth: 23.60 (ft)	3	Clay
		End depth: 24.50 (ft)	5	Silty sand & sandy silt
Transition layer 10	7	Start depth: 25.40 (ft)	5	Silty sand & sandy silt
		End depth: 26.00 (ft)	3	Clay
Transition layer 11	8	Start depth: 28.90 (ft)	3	Clay
		End depth: 29.60 (ft)	5	Silty sand & sandy silt
Transition layer 12	7	Start depth: 30.50 (ft)	5	Silty sand & sandy silt
		End depth: 31.10 (ft)	4	Clay & silty clay
Transition layer 13	5	Start depth: 31.50 (ft)	4	Clay & silty clay
		End depth: 31.90 (ft)	5	Silty sand & sandy silt
Transition layer 14	10	Start depth: 32.00 (ft)	5	Silty sand & sandy silt
		End depth: 32.90 (ft)	3	Clay
Transition layer 15	5	Start depth: 34.30 (ft)	3	Clay
		End depth: 34.70 (ft)	5	Silty sand & sandy silt
Transition layer 16	6	Start depth: 34.70 (ft)	5	Silty sand & sandy silt
		End depth: 35.20 (ft)	3	Clay
Transition layer 17	6	Start depth: 36.40 (ft)	3	Clay
		End depth: 36.90 (ft)	5	Silty sand & sandy silt
Transition layer 18	4	Start depth: 37.00 (ft)	5	Silty sand & sandy silt
		End depth: 37.30 (ft)	4	Clay & silty clay
Transition layer 19	6	Start depth: 37.40 (ft)	4	Clay & silty clay
		End depth: 37.90 (ft)	5	Silty sand & sandy silt
Transition layer 20	7	Start depth: 38.20 (ft)	5	Silty sand & sandy silt
		End depth: 38.80 (ft)	4	Clay & silty clay
Transition layer 21	4	Start depth: 39.70 (ft)	5	Silty sand & sandy silt
		End depth: 40.00 (ft)	4	Clay & silty clay
Transition layer 22	6	Start depth: 40.50 (ft)	3	Clay
		End depth: 41.00 (ft)	5	Silty sand & sandy silt
Transition layer 23	6	Start depth: 41.70 (ft)	5	Silty sand & sandy silt
		End depth: 42.20 (ft)	4	Clay & silty clay

Transition layer No	Number of points	Depth	SBT _n number	SBT _n description
Transition layer 24	6	Start depth: 42.30 (ft)	4	Clay & silty clay
		End depth: 42.80 (ft)	6	Sand & silty sand
Transition layer 25	10	Start depth: 47.90 (ft)	6	Sand & silty sand
		End depth: 48.80 (ft)	4	Clay & silty clay
Transition layer 26	12	Start depth: 48.80 (ft)	4	Clay & silty clay
		End depth: 49.90 (ft)	6	Sand & silty sand

Start depth: Depth where the transition layer begins

End depth: Depth where the transition layer ends

:: Field input data ::						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1	0.10	34.66	1.14	1.14	28.34	120.03
2	0.20	35.71	1.20	1.20	28.70	120.28
3	0.30	35.06	1.26	1.26	29.47	120.50
4	0.40	33.38	1.26	1.26	30.26	120.38
5	0.50	32.46	1.18	1.18	30.40	119.85
6	0.60	31.52	1.04	1.04	29.73	119.07
7	0.70	31.06	0.94	0.94	28.89	118.34
8	0.80	31.06	0.90	0.90	28.31	117.93
9	0.90	31.06	0.88	0.88	28.07	117.79
10	1.00	31.06	0.88	0.88	28.01	117.70
11	1.10	30.81	0.87	0.87	28.19	117.36
12	1.20	28.77	0.79	0.79	28.80	116.75
13	1.30	26.25	0.72	0.72	30.77	115.66
14	1.40	20.82	0.62	0.62	34.20	114.57
15	1.50	17.28	0.60	0.60	37.75	114.90
16	1.60	21.14	0.87	0.87	41.87	114.96
17	1.70	14.85	0.72	0.72	44.67	115.72
18	1.80	15.81	0.86	0.86	46.88	116.38
19	1.90	20.33	1.12	1.12	45.95	116.91
20	2.00	17.63	0.87	0.87	44.35	116.48
21	2.10	16.62	0.68	0.68	42.17	115.05
22	2.20	18.95	0.66	0.66	40.33	114.25
23	2.30	17.81	0.63	0.63	40.70	113.89
24	2.40	15.10	0.61	0.61	44.32	113.16
25	2.50	12.51	0.56	0.56	49.36	112.10
26	2.60	10.40	0.49	0.49	53.73	111.00
27	2.70	9.56	0.45	0.45	55.57	110.60
28	2.80	10.60	0.51	0.51	55.25	110.68
29	2.90	10.75	0.50	0.50	52.48	111.45
30	3.00	12.88	0.56	0.56	48.35	112.34
31	3.10	15.85	0.63	0.63	44.73	113.10
32	3.20	16.19	0.61	0.61	43.54	113.16
33	3.30	14.40	0.55	0.55	44.82	112.69
34	3.40	13.26	0.55	0.55	46.34	112.54
35	3.50	14.27	0.60	0.60	44.81	113.14
36	3.60	17.48	0.66	0.66	40.68	114.01
37	3.70	20.66	0.67	0.67	36.75	114.54
38	3.80	21.88	0.65	0.65	35.51	114.60
39	3.90	19.87	0.65	0.65	37.46	114.30
40	4.00	16.35	0.64	0.64	42.17	113.89
41	4.10	13.95	0.64	0.64	46.54	113.73
42	4.20	14.34	0.68	0.68	46.68	114.06
43	4.30	17.02	0.72	0.72	42.63	114.50
44	4.40	19.96	0.68	0.68	37.02	114.78
45	4.50	23.48	0.65	0.65	32.19	114.91
46	4.60	26.63	0.65	0.65	28.67	115.08
47	4.70	28.93	0.64	0.64	26.53	115.05
48	4.80	29.27	0.60	0.60	25.74	114.69

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
49	4.90	27.28	0.56	0.56	26.76	114.18
50	5.00	23.74	0.56	0.56	30.00	113.61
51	5.10	18.98	0.54	0.54	35.52	112.58
52	5.20	13.36	0.45	0.45	42.46	111.14
53	5.30	10.79	0.40	0.40	49.07	109.65
54	5.40	9.84	0.38	0.38	54.07	108.45
55	5.50	7.95	0.33	0.33	57.32	107.98
56	5.60	8.27	0.36	0.36	54.42	110.36
57	5.70	15.13	0.70	0.70	51.34	112.28
58	5.80	13.75	0.64	0.64	49.34	113.32
59	5.90	12.24	0.56	0.56	53.02	111.32
60	6.00	8.05	0.34	0.34	56.91	108.78
61	6.10	7.17	0.27	0.27	58.57	106.31
62	6.20	8.22	0.27	0.27	51.04	106.57
63	6.30	12.54	0.32	0.32	40.39	108.07
64	6.40	18.28	0.36	0.36	32.15	108.98
65	6.50	20.85	0.30	0.30	26.98	108.56
66	6.60	20.76	0.22	0.22	25.35	108.42
67	6.70	21.43	0.33	0.33	26.24	109.56
68	6.80	22.43	0.43	0.43	26.29	112.15
69	6.90	29.74	0.58	0.58	25.16	114.54
70	7.00	34.64	0.74	0.74	24.28	116.37
71	7.10	34.64	0.83	0.83	24.83	117.45
72	7.20	33.84	0.89	0.89	26.04	117.64
73	7.30	31.44	0.83	0.83	27.48	117.20
74	7.40	27.57	0.74	0.74	30.02	116.44
75	7.50	22.99	0.74	0.74	34.34	115.78
76	7.60	18.86	0.75	0.75	40.64	115.16
77	7.70	14.65	0.71	0.71	47.86	114.23
78	7.80	11.48	0.63	0.63	54.33	113.21
79	7.90	10.75	0.60	0.60	56.72	112.66
80	8.00	11.85	0.62	0.62	53.90	112.76
81	8.10	13.77	0.61	0.61	48.95	112.92
82	8.20	15.32	0.57	0.57	43.06	113.03
83	8.30	18.30	0.56	0.56	37.42	112.76
84	8.40	20.55	0.48	0.48	33.06	112.22
85	8.50	20.79	0.41	0.41	30.33	111.58
86	8.60	21.40	0.41	0.41	28.69	110.84
87	8.70	21.50	0.35	0.35	27.62	110.35
88	8.80	21.50	0.33	0.33	27.26	110.13
89	8.90	21.50	0.38	0.38	28.00	110.62
90	9.00	21.50	0.42	0.42	30.13	111.42
91	9.10	19.68	0.47	0.47	33.05	112.00
92	9.20	17.89	0.51	0.51	35.19	112.61
93	9.30	19.75	0.56	0.56	35.52	113.19
94	9.40	20.94	0.59	0.59	35.04	113.73
95	9.50	20.41	0.61	0.61	36.89	113.60
96	9.60	16.30	0.56	0.56	41.79	112.59

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
97	9.70	11.30	0.46	0.46	47.16	112.27
98	9.80	13.85	0.62	0.62	45.73	113.94
99	9.90	21.75	0.90	0.90	44.55	114.24
100	10.00	13.42	0.51	0.51	48.17	112.03
101	10.10	4.85	0.20	0.20	58.60	107.32
102	10.20	6.95	0.28	0.28	62.05	106.09
103	10.30	10.42	0.39	0.39	52.15	109.13
104	10.40	14.21	0.50	0.50	45.44	111.40
105	10.50	16.71	0.57	0.57	42.19	113.03
106	10.60	17.87	0.66	0.66	42.62	113.79
107	10.70	15.71	0.67	0.67	46.83	113.35
108	10.80	10.81	0.53	0.53	54.74	111.56
109	10.90	7.42	0.39	0.39	65.48	108.57
110	11.00	5.41	0.27	0.27	75.18	105.21
111	11.10	4.18	0.18	0.18	80.71	102.13
112	11.20	3.98	0.15	0.15	81.84	99.92
113	11.30	3.98	0.13	0.13	80.43	98.99
114	11.40	3.98	0.13	0.13	79.51	98.63
115	11.50	3.98	0.13	0.13	79.49	98.59
116	11.60	3.98	0.13	0.13	80.15	98.81
117	11.70	3.98	0.14	0.14	81.35	99.22
118	11.80	3.98	0.15	0.15	83.27	99.49
119	11.90	3.79	0.15	0.15	85.31	99.47
120	12.00	3.64	0.14	0.14	82.80	100.20
121	12.10	4.78	0.18	0.18	77.26	101.41
122	12.20	5.57	0.21	0.21	72.12	102.45
123	12.30	5.57	0.20	0.20	69.94	102.69
124	12.40	5.57	0.19	0.19	69.60	102.55
125	12.50	5.57	0.20	0.20	69.65	102.55
126	12.60	5.57	0.20	0.20	70.16	102.72
127	12.70	5.57	0.21	0.21	71.12	103.07
128	12.80	5.57	0.22	0.22	72.48	103.56
129	12.90	5.57	0.24	0.24	74.02	104.10
130	13.00	5.57	0.26	0.26	73.93	104.89
131	13.10	6.23	0.30	0.30	71.36	105.82
132	13.20	7.13	0.32	0.32	69.95	105.95
133	13.30	6.16	0.27	0.27	72.16	104.76
134	13.40	4.53	0.19	0.19	78.02	102.47
135	13.50	3.98	0.15	0.15	82.92	100.37
136	13.60	3.98	0.14	0.14	83.38	99.41
137	13.70	3.98	0.13	0.13	82.76	99.16
138	13.80	3.98	0.14	0.14	83.29	99.32
139	13.90	3.98	0.15	0.15	84.49	99.71
140	14.00	3.98	0.16	0.16	85.23	99.94
141	14.10	3.98	0.15	0.15	84.78	99.76
142	14.20	3.98	0.14	0.14	83.70	99.35
143	14.30	3.98	0.13	0.13	85.56	98.52
144	14.40	3.32	0.11	0.11	88.91	97.76

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
145	14.50	3.19	0.11	0.11	88.81	97.69
146	14.60	3.98	0.13	0.13	85.65	98.16
147	14.70	3.98	0.13	0.13	82.16	99.33
148	14.80	4.30	0.16	0.16	80.27	101.05
149	14.90	5.25	0.22	0.22	77.19	103.48
150	15.00	6.18	0.30	0.30	73.53	105.82
151	15.10	7.10	0.37	0.37	70.04	107.62
152	15.20	8.08	0.42	0.42	61.39	110.35
153	15.30	13.31	0.64	0.64	49.41	113.51
154	15.40	21.50	0.86	0.86	37.83	116.66
155	15.50	33.88	1.02	1.02	28.60	118.94
156	15.60	48.69	1.12	1.12	21.88	121.07
157	15.70	68.22	1.41	1.41	17.76	123.18
158	15.80	86.56	1.76	1.76	14.65	124.50
159	15.90	100.71	1.60	1.60	12.46	125.29
160	16.00	113.74	1.67	1.67	11.54	125.27
161	16.10	102.63	1.66	1.66	12.02	125.29
162	16.20	92.86	1.65	1.65	13.10	125.54
163	16.30	100.77	1.92	1.92	13.78	126.03
164	16.40	101.14	2.04	2.04	14.36	126.38
165	16.50	90.78	1.94	1.94	15.70	126.05
166	16.60	76.93	1.82	1.82	18.14	125.31
167	16.70	62.22	1.76	1.76	21.88	124.22
168	16.80	45.33	1.54	1.54	27.12	122.57
169	16.90	30.43	1.20	1.20	33.84	120.13
170	17.00	20.78	0.89	0.89	41.59	117.05
171	17.10	14.24	0.62	0.62	49.20	113.72
172	17.20	10.42	0.43	0.43	56.74	110.19
173	17.30	7.62	0.29	0.29	63.58	106.70
174	17.40	6.02	0.20	0.20	68.69	103.61
175	17.50	5.57	0.16	0.16	70.47	101.58
176	17.60	5.57	0.15	0.15	69.51	100.49
177	17.70	5.57	0.13	0.13	68.04	99.83
178	17.80	5.57	0.13	0.13	67.10	99.38
179	17.90	5.57	0.12	0.12	66.45	99.04
180	18.00	5.57	0.11	0.11	65.65	99.29
181	18.10	6.00	0.14	0.14	64.37	100.60
182	18.20	6.94	0.19	0.19	65.01	102.82
183	18.30	7.17	0.25	0.25	67.38	105.03
184	18.40	7.17	0.32	0.32	69.86	107.16
185	18.50	8.16	0.43	0.43	70.11	108.93
186	18.60	9.05	0.49	0.49	67.41	110.54
187	18.70	10.41	0.57	0.57	62.96	111.98
188	18.80	12.71	0.66	0.66	56.94	113.39
189	18.90	15.69	0.73	0.73	50.04	114.69
190	19.00	19.82	0.78	0.78	44.92	115.31
191	19.10	20.89	0.73	0.73	42.32	115.64
192	19.20	20.69	0.77	0.77	42.75	115.85

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
193	19.30	19.95	0.85	0.85	45.31	115.98
194	19.40	17.55	0.82	0.82	48.36	115.57
195	19.50	15.51	0.71	0.71	50.08	114.76
196	19.60	15.84	0.66	0.66	48.85	114.17
197	19.70	17.54	0.65	0.65	45.16	114.65
198	19.80	21.46	0.76	0.76	41.90	115.66
199	19.90	23.89	0.86	0.86	40.85	116.64
200	20.00	22.86	0.91	0.91	43.07	116.69
201	20.10	17.95	0.83	0.83	48.54	115.18
202	20.20	11.57	0.53	0.53	56.74	112.13
203	20.30	8.08	0.31	0.31	64.26	107.94
204	20.40	7.11	0.21	0.21	67.57	104.13
205	20.50	6.20	0.15	0.15	68.48	101.43
206	20.60	5.57	0.12	0.12	70.26	99.95
207	20.70	5.57	0.14	0.14	73.45	100.23
208	20.80	5.57	0.17	0.17	76.83	101.36
209	20.90	5.49	0.19	0.19	79.45	102.13
210	21.00	5.48	0.19	0.19	80.11	102.23
211	21.10	5.52	0.18	0.18	79.81	101.97
212	21.20	5.42	0.17	0.17	77.76	102.77
213	21.30	6.55	0.24	0.24	76.80	104.57
214	21.40	7.17	0.32	0.32	75.26	106.75
215	21.50	7.83	0.39	0.39	73.55	108.27
216	21.60	8.73	0.43	0.43	71.40	108.90
217	21.70	8.76	0.40	0.40	69.08	108.81
218	21.80	8.76	0.36	0.36	67.86	108.08
219	21.90	8.44	0.32	0.32	68.20	107.05
220	22.00	7.50	0.27	0.27	69.86	106.13
221	22.10	7.17	0.27	0.27	71.03	105.96
222	22.20	7.89	0.31	0.31	69.97	106.79
223	22.30	8.78	0.36	0.36	67.91	108.22
224	22.40	9.68	0.43	0.43	65.80	109.99
225	22.50	11.24	0.55	0.55	60.43	112.52
226	22.60	16.11	0.78	0.78	51.87	115.20
227	22.70	23.09	0.97	0.97	43.02	117.69
228	22.80	31.69	1.14	1.14	36.88	119.75
229	22.90	38.68	1.38	1.38	34.50	121.26
230	23.00	38.61	1.55	1.55	35.23	122.23
231	23.10	35.57	1.66	1.66	38.27	122.56
232	23.20	31.61	1.69	1.69	42.04	122.56
233	23.30	28.79	1.71	1.71	45.49	122.33
234	23.40	26.69	1.66	1.66	47.96	121.98
235	23.50	25.18	1.58	1.58	49.31	121.68
236	23.60	25.14	1.59	1.59	49.11	121.77
237	23.70	27.57	1.71	1.71	46.66	122.39
238	23.80	32.85	1.85	1.85	42.37	123.30
239	23.90	39.81	1.97	1.97	37.58	124.12
240	24.00	46.73	2.01	2.01	33.28	124.67

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
241	24.10	52.98	1.98	1.98	29.02	125.09
242	24.20	63.75	2.01	2.01	24.54	125.49
243	24.30	78.48	1.98	1.98	20.44	126.12
244	24.40	94.72	2.11	2.11	17.66	127.04
245	24.50	108.37	2.44	2.44	16.44	128.21
246	24.60	116.41	2.80	2.80	16.21	129.29
247	24.70	120.60	3.06	3.06	16.35	130.09
248	24.80	124.03	3.26	3.26	16.96	129.98
249	24.90	104.48	2.76	2.76	18.10	129.03
250	25.00	85.21	2.25	2.25	19.45	127.87
251	25.10	86.59	2.35	2.35	20.23	127.67
252	25.20	92.99	2.67	2.67	20.33	128.52
253	25.30	98.39	3.01	3.01	20.70	129.28
254	25.40	96.08	3.13	3.13	21.72	129.55
255	25.50	86.73	3.07	3.07	23.59	129.15
256	25.60	73.25	2.80	2.80	26.39	128.14
257	25.70	58.28	2.39	2.39	30.20	126.63
258	25.80	44.63	2.03	2.03	35.43	124.75
259	25.90	32.31	1.68	1.68	42.53	122.45
260	26.00	21.40	1.25	1.25	51.56	119.66
261	26.10	14.70	0.89	0.89	61.54	116.51
262	26.20	11.45	0.66	0.66	67.83	114.12
263	26.30	11.60	0.63	0.63	68.85	112.99
264	26.40	12.14	0.62	0.62	67.65	112.82
265	26.50	11.95	0.61	0.61	67.30	112.86
266	26.60	11.95	0.63	0.63	67.37	113.15
267	26.70	12.65	0.69	0.69	65.88	113.89
268	26.80	14.34	0.77	0.77	63.63	114.68
269	26.90	15.19	0.81	0.81	61.79	115.29
270	27.00	15.52	0.83	0.83	61.98	115.37
271	27.10	14.40	0.80	0.80	64.34	114.80
272	27.20	12.16	0.68	0.68	69.38	113.25
273	27.30	9.27	0.50	0.50	74.61	111.36
274	27.40	8.76	0.44	0.44	75.56	110.29
275	27.50	10.35	0.49	0.49	73.35	110.32
276	27.60	10.35	0.49	0.49	71.13	110.67
277	27.70	10.35	0.48	0.48	70.96	110.58
278	27.80	10.35	0.47	0.47	71.05	110.57
279	27.90	10.35	0.49	0.49	71.29	110.63
280	28.00	10.35	0.49	0.49	71.80	110.78
281	28.10	10.36	0.50	0.50	70.55	111.48
282	28.20	12.07	0.60	0.60	61.79	114.31
283	28.30	21.29	1.03	1.03	49.87	118.13
284	28.40	34.11	1.48	1.48	41.81	121.45
285	28.50	42.17	1.82	1.82	39.05	123.32
286	28.60	40.15	1.97	1.97	40.38	123.84
287	28.70	33.68	1.87	1.87	44.23	123.50
288	28.80	29.73	1.77	1.77	47.76	122.82

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
289	28.90	28.47	1.68	1.68	47.37	122.48
290	29.00	32.92	1.65	1.65	41.54	122.76
291	29.10	45.19	1.70	1.70	32.50	123.45
292	29.20	63.64	1.67	1.67	24.82	124.41
293	29.30	83.01	1.81	1.81	20.11	125.75
294	29.40	100.69	2.24	2.24	17.69	127.57
295	29.50	120.75	2.79	2.79	16.17	129.28
296	29.60	139.64	3.13	3.13	15.09	130.77
297	29.70	155.79	3.62	3.62	14.57	131.75
298	29.80	158.58	3.85	3.85	14.91	131.79
299	29.90	133.95	3.23	3.23	16.19	131.06
300	30.00	111.62	2.95	2.95	17.70	130.88
301	30.10	128.93	3.85	3.85	18.39	131.56
302	30.20	139.28	4.15	4.15	18.16	132.17
303	30.30	130.61	3.70	3.70	17.86	131.68
304	30.40	122.14	3.17	3.17	17.60	130.49
305	30.50	115.80	2.69	2.69	17.54	129.38
306	30.60	107.57	2.54	2.54	18.55	128.79
307	30.70	96.38	2.71	2.71	21.09	128.57
308	30.80	81.49	2.76	2.76	24.68	128.21
309	30.90	67.35	2.55	2.55	28.37	127.37
310	31.00	57.59	2.27	2.27	31.24	126.31
311	31.10	52.71	2.07	2.07	32.65	125.44
312	31.20	51.96	1.97	1.97	32.70	125.03
313	31.30	53.72	1.96	1.96	32.36	125.22
314	31.40	56.20	2.19	2.19	32.60	126.00
315	31.50	58.44	2.57	2.57	32.01	127.51
316	31.60	72.72	3.21	3.21	28.55	129.50
317	31.70	103.82	3.93	3.93	23.35	131.55
318	31.80	141.49	4.47	4.47	19.46	133.12
319	31.90	162.19	4.85	4.85	17.56	134.08
320	32.00	165.45	5.09	5.09	17.47	134.52
321	32.10	157.32	5.20	5.20	18.80	134.45
322	32.20	134.40	5.01	5.01	21.30	133.91
323	32.30	108.77	4.64	4.64	24.78	132.71
324	32.40	84.10	3.83	3.83	28.51	130.94
325	32.50	66.38	2.96	2.96	31.91	128.67
326	32.60	53.27	2.30	2.30	35.02	126.32
327	32.70	42.89	1.85	1.85	38.32	124.22
328	32.80	35.93	1.57	1.57	41.54	122.52
329	32.90	32.06	1.38	1.38	43.44	121.40
330	33.00	31.80	1.32	1.32	43.59	121.02
331	33.10	33.67	1.38	1.38	42.92	121.18
332	33.20	34.60	1.43	1.43	42.05	121.41
333	33.30	35.33	1.40	1.40	40.79	121.50
334	33.40	37.59	1.38	1.38	38.84	121.61
335	33.50	40.87	1.42	1.42	37.12	121.97
336	33.60	43.05	1.52	1.52	36.18	122.56

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
337	33.70	44.89	1.65	1.65	35.88	123.23
338	33.80	46.96	1.78	1.78	36.23	123.92
339	33.90	47.18	1.96	1.96	37.49	124.42
340	34.00	44.30	2.04	2.04	40.12	124.60
341	34.10	39.29	2.04	2.04	43.92	124.28
342	34.20	33.66	1.92	1.92	47.95	123.50
343	34.30	29.54	1.68	1.68	49.51	122.58
344	34.40	31.08	1.51	1.51	45.29	121.94
345	34.50	39.58	1.40	1.40	35.82	121.76
346	34.60	55.19	1.24	1.24	28.02	122.39
347	34.70	69.17	1.50	1.50	25.56	123.77
348	34.80	67.52	2.00	2.00	27.73	124.97
349	34.90	54.56	2.09	2.09	33.26	125.09
350	35.00	41.11	1.91	1.91	40.32	124.03
351	35.10	31.86	1.64	1.64	46.91	122.61
352	35.20	28.07	1.47	1.47	50.83	121.52
353	35.30	27.63	1.42	1.42	52.05	121.29
354	35.40	28.67	1.55	1.55	52.49	121.51
355	35.50	28.39	1.61	1.61	52.08	121.77
356	35.60	29.63	1.55	1.55	49.09	121.96
357	35.70	35.50	1.56	1.56	43.73	122.27
358	35.80	42.33	1.59	1.59	39.30	123.00
359	35.90	46.92	1.79	1.79	37.26	124.18
360	36.00	51.24	2.20	2.20	38.09	125.31
361	36.10	48.45	2.42	2.42	41.11	125.88
362	36.20	40.71	2.40	2.40	46.12	125.51
363	36.30	33.17	2.17	2.17	51.52	124.51
364	36.40	28.97	1.89	1.89	53.98	123.41
365	36.50	29.96	1.72	1.72	50.80	122.93
366	36.60	37.11	1.73	1.73	43.47	123.00
367	36.70	46.63	1.65	1.65	35.44	123.32
368	36.80	58.10	1.56	1.56	29.06	123.62
369	36.90	68.89	1.60	1.60	25.33	124.23
370	37.00	75.65	1.80	1.80	24.48	125.15
371	37.10	75.29	2.08	2.08	25.72	126.02
372	37.20	70.69	2.28	2.28	28.08	126.51
373	37.30	65.34	2.33	2.33	30.34	126.58
374	37.40	62.12	2.29	2.29	31.16	126.47
375	37.50	64.91	2.24	2.24	29.63	126.36
376	37.60	73.25	2.13	2.13	25.91	126.26
377	37.70	86.14	1.96	1.96	21.65	126.09
378	37.80	98.77	1.82	1.82	18.22	125.98
379	37.90	108.63	1.80	1.80	16.28	126.19
380	38.00	115.25	1.94	1.94	15.74	126.61
381	38.10	114.97	2.05	2.05	16.14	127.01
382	38.20	110.63	2.11	2.11	16.96	127.12
383	38.30	105.76	2.09	2.09	18.08	127.05
384	38.40	98.70	2.09	2.09	19.92	126.98

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
385	38.50	87.30	2.21	2.21	23.15	127.02
386	38.60	73.69	2.38	2.38	27.72	126.92
387	38.70	60.85	2.37	2.37	32.56	126.35
388	38.80	51.36	2.08	2.08	35.69	125.29
389	38.90	48.51	1.75	1.75	35.65	124.06
390	39.00	50.58	1.53	1.53	33.51	123.19
391	39.10	53.22	1.46	1.46	31.38	122.84
392	39.20	55.15	1.46	1.46	30.12	122.81
393	39.30	56.55	1.45	1.45	29.20	122.87
394	39.40	58.57	1.45	1.45	28.06	122.86
395	39.50	61.39	1.41	1.41	26.45	122.78
396	39.60	65.19	1.34	1.34	24.44	122.66
397	39.70	70.41	1.30	1.30	23.80	123.40
398	39.80	74.10	1.74	1.74	26.14	125.03
399	39.90	67.59	2.41	2.41	29.56	126.37
400	40.00	63.77	2.46	2.46	31.87	127.09
401	40.10	68.83	2.49	2.49	32.32	127.72
402	40.20	72.50	3.01	3.01	33.56	128.46
403	40.30	65.62	3.28	3.28	36.88	128.75
404	40.40	54.60	3.07	3.07	41.02	128.04
405	40.50	46.46	2.55	2.55	43.32	126.60
406	40.60	44.46	2.03	2.03	40.81	125.32
407	40.70	53.05	1.87	1.87	34.16	124.98
408	40.80	70.44	1.96	1.96	27.94	125.50
409	40.90	84.10	2.03	2.03	24.27	126.20
410	41.00	88.98	2.12	2.12	22.60	126.72
411	41.10	92.93	2.21	2.21	22.08	127.06
412	41.20	94.75	2.26	2.26	21.72	127.40
413	41.30	98.24	2.35	2.35	21.53	127.71
414	41.40	100.38	2.45	2.45	21.50	128.00
415	41.50	100.35	2.50	2.50	21.06	128.81
416	41.60	118.10	3.03	3.03	20.37	130.07
417	41.70	134.16	3.64	3.64	20.22	131.26
418	41.80	128.80	3.84	3.84	21.34	131.93
419	41.90	118.04	4.05	4.05	23.84	132.01
420	42.00	103.50	4.08	4.08	26.99	131.91
421	42.10	92.50	4.12	4.12	30.13	131.37
422	42.20	80.16	3.67	3.67	32.08	130.30
423	42.30	72.29	2.89	2.89	31.18	128.98
424	42.40	80.37	2.51	2.51	26.59	128.01
425	42.50	100.78	2.32	2.32	20.83	127.93
426	42.60	126.94	2.32	2.32	16.36	128.50
427	42.70	153.49	2.57	2.57	13.94	129.52
428	42.80	170.89	2.94	2.94	13.01	130.65
429	42.90	180.62	3.30	3.30	12.95	131.57
430	43.00	183.96	3.54	3.54	13.20	132.13
431	43.10	183.33	3.65	3.65	13.50	132.32
432	43.20	179.38	3.58	3.58	13.69	132.19

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
433	43.30	175.11	3.41	3.41	13.68	131.87
434	43.40	173.36	3.25	3.25	13.52	131.53
435	43.50	173.21	3.15	3.15	13.31	131.37
436	43.60	175.66	3.20	3.20	13.10	131.44
437	43.70	181.13	3.30	3.30	12.91	131.72
438	43.80	187.55	3.44	3.44	12.77	132.14
439	43.90	194.31	3.67	3.67	12.73	132.63
440	44.00	199.87	3.90	3.90	12.73	133.05
441	44.10	203.26	3.98	3.98	12.68	133.26
442	44.20	203.67	3.93	3.93	12.49	133.20
443	44.30	203.85	3.78	3.78	12.25	133.08
444	44.40	206.73	3.78	3.78	12.11	133.13
445	44.50	210.23	3.96	3.96	12.14	133.41
446	44.60	214.11	4.18	4.18	12.19	133.72
447	44.70	217.87	4.22	4.22	12.11	133.91
448	44.80	220.77	4.22	4.22	11.83	133.96
449	44.90	225.92	4.18	4.18	11.37	133.95
450	45.00	234.12	4.11	4.11	10.86	134.00
451	45.10	241.83	4.18	4.18	10.53	134.05
452	45.20	241.32	4.17	4.17	10.53	133.95
453	45.30	230.23	3.98	3.98	10.82	133.58
454	45.40	215.31	3.72	3.72	11.24	132.95
455	45.50	200.43	3.40	3.40	11.61	132.20
456	45.60	190.45	3.12	3.12	11.63	131.52
457	45.70	190.71	2.94	2.94	11.19	131.06
458	45.80	197.95	2.84	2.84	10.39	130.98
459	45.90	213.53	2.91	2.91	9.54	131.34
460	46.00	233.97	3.17	3.17	8.89	132.05
461	46.10	252.54	3.49	3.49	8.48	132.96
462	46.20	271.60	3.88	3.88	8.21	133.78
463	46.30	287.27	4.16	4.16	7.93	134.37
464	46.40	298.42	4.24	4.24	7.59	134.63
465	46.50	305.26	4.17	4.17	7.29	134.72
466	46.60	310.07	4.20	4.20	7.18	134.85
467	46.70	313.73	4.40	4.40	7.27	135.09
468	46.80	313.58	4.54	4.54	7.46	135.25
469	46.90	308.86	4.49	4.49	7.70	135.28
470	47.00	302.35	4.52	4.52	8.00	135.25
471	47.10	294.37	4.56	4.56	8.46	135.26
472	47.20	285.17	4.63	4.63	9.01	135.27
473	47.30	274.90	4.68	4.68	9.52	135.19
474	47.40	265.74	4.57	4.57	9.83	134.92
475	47.50	257.78	4.28	4.28	9.81	134.42
476	47.60	251.30	3.91	3.91	9.43	133.66
477	47.70	246.83	3.43	3.43	8.75	132.71
478	47.80	244.57	2.93	2.93	7.96	131.76
479	47.90	244.45	2.69	2.69	7.77	131.31
480	48.00	236.24	2.93	2.93	8.92	131.77

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
481	48.10	214.58	3.60	3.60	11.71	132.58
482	48.20	176.62	4.13	4.13	16.08	132.93
483	48.30	132.04	4.15	4.15	21.80	132.17
484	48.40	91.43	3.43	3.43	28.47	130.09
485	48.50	61.13	2.30	2.30	33.74	127.75
486	48.60	61.75	2.15	2.15	36.51	126.01
487	48.70	58.17	2.12	2.12	38.91	124.62
488	48.80	38.33	1.41	1.41	40.60	123.43
489	48.90	46.32	1.47	1.47	37.70	122.71
490	49.00	63.04	1.60	1.60	29.79	124.01
491	49.10	86.60	1.80	1.80	23.02	125.52
492	49.20	114.00	2.02	2.02	18.73	127.07
493	49.30	135.60	2.36	2.36	16.51	128.59
494	49.40	151.25	2.79	2.79	15.38	129.88
495	49.50	166.37	3.06	3.06	14.06	130.52
496	49.60	181.99	2.82	2.82	12.19	130.80
497	49.70	207.38	2.81	2.81	10.16	131.02
498	49.80	236.80	2.98	2.98	8.69	131.33
499	49.90	249.95	2.90	2.90	7.92	131.55

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q _c :	Measured cone resistance (tsf)
f _s :	Sleeve friction resistance (tsf)
u:	Pore pressure (tsf)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (pcf)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1	0.10	0.01	0.00	0.01	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
2	0.20	0.01	0.00	0.01	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
3	0.30	0.02	0.00	0.02	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
4	0.40	0.02	0.00	0.02	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
5	0.50	0.03	0.00	0.03	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
6	0.60	0.04	0.00	0.04	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
7	0.70	0.04	0.00	0.04	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
8	0.80	0.05	0.00	0.05	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
9	0.90	0.05	0.00	0.05	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
10	1.00	0.06	0.00	0.06	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
11	1.10	0.07	0.00	0.07	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
12	1.20	0.07	0.00	0.07	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
13	1.30	0.08	0.00	0.08	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
14	1.40	0.08	0.00	0.08	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
15	1.50	0.09	0.00	0.09	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
16	1.60	0.09	0.00	0.09	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
17	1.70	0.10	0.00	0.10	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
18	1.80	0.11	0.00	0.11	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
19	1.90	0.11	0.00	0.11	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
20	2.00	0.12	0.00	0.12	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
21	2.10	0.12	0.00	0.12	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
22	2.20	0.13	0.00	0.13	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
23	2.30	0.13	0.00	0.13	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
24	2.40	0.14	0.00	0.14	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
25	2.50	0.15	0.00	0.15	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
26	2.60	0.15	0.00	0.15	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
27	2.70	0.16	0.00	0.16	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
28	2.80	0.16	0.00	0.16	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
29	2.90	0.17	0.00	0.17	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
30	3.00	0.17	0.00	0.17	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
31	3.10	0.18	0.00	0.18	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
32	3.20	0.19	0.00	0.19	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
33	3.30	0.19	0.00	0.19	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
34	3.40	0.20	0.00	0.20	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
35	3.50	0.20	0.00	0.20	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
36	3.60	0.21	0.00	0.21	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
37	3.70	0.21	0.00	0.21	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
38	3.80	0.22	0.00	0.22	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
39	3.90	0.22	0.00	0.22	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
40	4.00	0.23	0.00	0.23	1.00	0.479	1.04	0.460	1.10	1.30	2.000	No
41	4.10	0.24	0.00	0.24	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
42	4.20	0.24	0.00	0.24	1.00	0.479	1.04	0.459	1.10	1.30	2.000	Yes
43	4.30	0.25	0.00	0.25	1.00	0.479	1.04	0.459	1.10	1.30	2.000	Yes
44	4.40	0.25	0.00	0.25	1.00	0.479	1.04	0.459	1.10	1.30	2.000	Yes
45	4.50	0.26	0.00	0.26	1.00	0.479	1.04	0.459	1.10	1.30	2.000	Yes
46	4.60	0.26	0.00	0.26	1.00	0.479	1.04	0.459	1.10	1.30	2.000	Yes
47	4.70	0.27	0.00	0.27	0.99	0.479	1.04	0.459	1.10	1.30	2.000	Yes
48	4.80	0.28	0.00	0.28	0.99	0.478	1.04	0.459	1.10	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
49	4.90	0.28	0.00	0.28	0.99	0.478	1.04	0.458	1.10	1.30	2.000	Yes
50	5.00	0.29	0.00	0.29	0.99	0.478	1.04	0.458	1.10	1.30	2.000	Yes
51	5.10	0.29	0.00	0.29	0.99	0.478	1.04	0.458	1.10	1.30	2.000	Yes
52	5.20	0.30	0.00	0.30	0.99	0.478	1.04	0.458	1.10	1.30	2.000	Yes
53	5.30	0.30	0.00	0.30	0.99	0.478	1.04	0.458	1.10	1.30	2.000	Yes
54	5.40	0.31	0.00	0.31	0.99	0.478	1.04	0.458	1.10	1.30	2.000	Yes
55	5.50	0.32	0.00	0.32	0.99	0.477	1.04	0.458	1.10	1.30	2.000	Yes
56	5.60	0.32	0.00	0.32	0.99	0.477	1.04	0.458	1.10	1.30	2.000	No
57	5.70	0.33	0.00	0.33	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
58	5.80	0.33	0.00	0.33	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
59	5.90	0.34	0.00	0.34	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
60	6.00	0.34	0.00	0.34	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
61	6.10	0.35	0.00	0.35	0.99	0.477	1.04	0.457	1.09	1.30	2.000	No
62	6.20	0.35	0.00	0.35	0.99	0.477	1.04	0.457	1.09	1.30	2.000	Yes
63	6.30	0.36	0.00	0.36	0.99	0.476	1.04	0.457	1.10	1.30	2.000	Yes
64	6.40	0.36	0.00	0.36	0.99	0.476	1.04	0.456	1.10	1.30	2.000	Yes
65	6.50	0.37	0.00	0.37	0.99	0.476	1.04	0.456	1.10	1.30	2.000	Yes
66	6.60	0.38	0.00	0.38	0.99	0.476	1.04	0.456	1.10	1.30	2.000	Yes
67	6.70	0.38	0.00	0.38	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
68	6.80	0.39	0.00	0.39	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
69	6.90	0.39	0.00	0.39	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
70	7.00	0.40	0.00	0.40	0.99	0.475	1.04	0.456	1.10	1.30	2.000	No
71	7.10	0.40	0.00	0.40	0.99	0.475	1.04	0.455	1.10	1.30	2.000	Yes
72	7.20	0.41	0.00	0.41	0.99	0.475	1.04	0.455	1.10	1.30	2.000	Yes
73	7.30	0.42	0.00	0.42	0.99	0.475	1.04	0.455	1.10	1.30	2.000	Yes
74	7.40	0.42	0.00	0.42	0.99	0.475	1.04	0.455	1.10	1.30	2.000	Yes
75	7.50	0.43	0.00	0.43	0.99	0.475	1.04	0.455	1.09	1.30	2.000	Yes
76	7.60	0.43	0.00	0.43	0.99	0.475	1.04	0.455	1.09	1.30	2.000	Yes
77	7.70	0.44	0.00	0.44	0.99	0.474	1.04	0.455	1.08	1.30	2.000	Yes
78	7.80	0.44	0.00	0.44	0.99	0.474	1.04	0.455	1.08	1.30	2.000	Yes
79	7.90	0.45	0.00	0.45	0.99	0.474	1.04	0.454	1.07	1.30	2.000	Yes
80	8.00	0.46	0.00	0.46	0.99	0.474	1.04	0.454	1.07	1.30	2.000	Yes
81	8.10	0.46	0.00	0.46	0.98	0.477	1.04	0.457	1.08	1.30	2.000	Yes
82	8.20	0.47	0.01	0.46	0.98	0.480	1.04	0.460	1.08	1.30	2.000	Yes
83	8.30	0.47	0.01	0.46	0.98	0.483	1.04	0.463	1.08	1.30	2.000	Yes
84	8.40	0.48	0.01	0.47	0.98	0.486	1.04	0.466	1.08	1.30	2.000	Yes
85	8.50	0.48	0.02	0.47	0.98	0.489	1.04	0.469	1.08	1.30	2.000	Yes
86	8.60	0.49	0.02	0.47	0.98	0.492	1.04	0.471	1.08	1.30	2.000	Yes
87	8.70	0.49	0.02	0.47	0.98	0.495	1.04	0.474	1.08	1.30	0.590	No
88	8.80	0.50	0.02	0.48	0.98	0.498	1.04	0.477	1.08	1.30	0.594	No
89	8.90	0.51	0.03	0.48	0.98	0.500	1.04	0.480	1.08	1.30	2.000	Yes
90	9.00	0.51	0.03	0.48	0.98	0.503	1.04	0.482	1.08	1.30	2.000	Yes
91	9.10	0.52	0.03	0.48	0.98	0.506	1.04	0.485	1.08	1.30	2.000	Yes
92	9.20	0.52	0.04	0.49	0.98	0.509	1.04	0.487	1.07	1.30	2.000	Yes
93	9.30	0.53	0.04	0.49	0.98	0.511	1.04	0.490	1.07	1.30	0.612	No
94	9.40	0.53	0.04	0.49	0.98	0.514	1.04	0.492	1.07	1.30	0.614	No
95	9.50	0.54	0.05	0.49	0.98	0.516	1.04	0.495	1.07	1.30	0.618	No
96	9.60	0.55	0.05	0.50	0.98	0.519	1.04	0.497	1.07	1.30	0.624	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
97	9.70	0.55	0.05	0.50	0.98	0.522	1.04	0.500	1.07	1.30	0.631	No
98	9.80	0.56	0.06	0.50	0.98	0.524	1.04	0.502	1.07	1.30	0.632	No
99	9.90	0.56	0.06	0.50	0.98	0.527	1.04	0.505	1.07	1.30	0.630	No
100	10.00	0.57	0.06	0.51	0.98	0.529	1.04	0.507	1.07	1.30	0.639	No
101	10.10	0.57	0.07	0.51	0.98	0.531	1.04	0.509	1.06	1.30	0.648	No
102	10.20	0.58	0.07	0.51	0.98	0.534	1.04	0.512	1.06	1.30	0.650	No
103	10.30	0.58	0.07	0.51	0.98	0.536	1.04	0.514	1.06	1.30	0.651	No
104	10.40	0.59	0.07	0.51	0.98	0.539	1.04	0.516	1.06	1.30	0.651	No
105	10.50	0.60	0.08	0.52	0.98	0.541	1.04	0.518	1.07	1.30	0.653	No
106	10.60	0.60	0.08	0.52	0.98	0.543	1.04	0.521	1.07	1.30	0.655	No
107	10.70	0.61	0.08	0.52	0.98	0.546	1.04	0.523	1.06	1.30	0.659	No
108	10.80	0.61	0.09	0.52	0.98	0.548	1.04	0.525	1.06	1.30	0.666	No
109	10.90	0.62	0.09	0.53	0.98	0.550	1.04	0.527	1.06	1.30	0.671	No
110	11.00	0.62	0.09	0.53	0.98	0.552	1.04	0.529	1.06	1.30	0.675	No
111	11.10	0.63	0.10	0.53	0.98	0.555	1.04	0.531	1.05	1.30	0.679	No
112	11.20	0.63	0.10	0.53	0.97	0.557	1.04	0.534	1.05	1.30	0.682	No
113	11.30	0.64	0.10	0.54	0.97	0.559	1.04	0.536	1.05	1.30	0.685	No
114	11.40	0.64	0.11	0.54	0.97	0.561	1.04	0.538	1.05	1.30	0.688	No
115	11.50	0.65	0.11	0.54	0.97	0.563	1.04	0.540	1.05	1.30	0.691	No
116	11.60	0.65	0.11	0.54	0.97	0.566	1.04	0.542	1.05	1.30	0.694	No
117	11.70	0.66	0.12	0.54	0.97	0.568	1.04	0.544	1.05	1.30	0.697	No
118	11.80	0.66	0.12	0.54	0.97	0.570	1.04	0.546	1.05	1.30	0.699	No
119	11.90	0.67	0.12	0.55	0.97	0.572	1.04	0.548	1.05	1.30	0.702	No
120	12.00	0.67	0.12	0.55	0.97	0.574	1.04	0.550	1.05	1.30	0.705	No
121	12.10	0.68	0.13	0.55	0.97	0.576	1.04	0.552	1.05	1.30	0.707	No
122	12.20	0.68	0.13	0.55	0.97	0.578	1.04	0.554	1.05	1.30	0.709	No
123	12.30	0.69	0.13	0.55	0.97	0.580	1.04	0.556	1.05	1.30	0.712	No
124	12.40	0.69	0.14	0.56	0.97	0.582	1.04	0.558	1.05	1.30	0.715	No
125	12.50	0.70	0.14	0.56	0.97	0.584	1.04	0.560	1.05	1.30	0.717	No
126	12.60	0.70	0.14	0.56	0.97	0.586	1.04	0.562	1.05	1.30	0.720	No
127	12.70	0.71	0.15	0.56	0.97	0.588	1.04	0.564	1.05	1.30	0.723	No
128	12.80	0.71	0.15	0.56	0.97	0.590	1.04	0.566	1.05	1.30	0.725	No
129	12.90	0.72	0.15	0.57	0.97	0.592	1.04	0.567	1.05	1.30	0.728	No
130	13.00	0.72	0.16	0.57	0.97	0.594	1.04	0.569	1.05	1.30	0.730	No
131	13.10	0.73	0.16	0.57	0.97	0.596	1.04	0.571	1.05	1.30	0.732	No
132	13.20	0.73	0.16	0.57	0.97	0.598	1.04	0.573	1.05	1.30	0.734	No
133	13.30	0.74	0.17	0.57	0.97	0.599	1.04	0.574	1.05	1.30	0.737	No
134	13.40	0.75	0.17	0.58	0.97	0.601	1.04	0.576	1.05	1.30	0.741	No
135	13.50	0.75	0.17	0.58	0.97	0.603	1.04	0.578	1.05	1.30	0.744	No
136	13.60	0.76	0.17	0.58	0.97	0.605	1.04	0.580	1.05	1.30	0.746	No
137	13.70	0.76	0.18	0.58	0.97	0.607	1.04	0.582	1.05	1.30	0.748	No
138	13.80	0.77	0.18	0.58	0.97	0.609	1.04	0.583	1.05	1.30	0.751	No
139	13.90	0.77	0.18	0.59	0.97	0.610	1.04	0.585	1.05	1.30	0.753	No
140	14.00	0.78	0.19	0.59	0.97	0.612	1.04	0.587	1.05	1.30	0.756	No
141	14.10	0.78	0.19	0.59	0.96	0.614	1.04	0.588	1.05	1.30	0.758	No
142	14.20	0.79	0.19	0.59	0.96	0.616	1.04	0.590	1.05	1.30	0.760	No
143	14.30	0.79	0.20	0.59	0.96	0.617	1.04	0.592	1.05	1.30	0.763	No
144	14.40	0.79	0.20	0.60	0.96	0.619	1.04	0.593	1.04	1.30	0.765	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
145	14.50	0.80	0.20	0.60	0.96	0.621	1.04	0.595	1.04	1.30	0.768	No
146	14.60	0.80	0.21	0.60	0.96	0.622	1.04	0.597	1.04	1.30	0.769	No
147	14.70	0.81	0.21	0.60	0.96	0.624	1.04	0.598	1.04	1.30	0.772	No
148	14.80	0.81	0.21	0.60	0.96	0.626	1.04	0.600	1.04	1.30	0.774	No
149	14.90	0.82	0.22	0.60	0.96	0.627	1.04	0.601	1.04	1.30	0.775	No
150	15.00	0.83	0.22	0.61	0.96	0.629	1.04	0.603	1.04	1.30	0.777	No
151	15.10	0.83	0.22	0.61	0.96	0.630	1.04	0.604	1.04	1.30	0.778	No
152	15.20	0.84	0.22	0.61	0.96	0.632	1.04	0.606	1.05	1.30	0.780	No
153	15.30	0.84	0.23	0.61	0.96	0.633	1.04	0.607	1.05	1.30	2.000	Yes
154	15.40	0.85	0.23	0.62	0.96	0.635	1.04	0.608	1.05	1.30	2.000	Yes
155	15.50	0.85	0.23	0.62	0.96	0.636	1.04	0.610	1.06	1.30	2.000	Yes
156	15.60	0.86	0.24	0.62	0.96	0.637	1.04	0.611	1.07	1.30	2.000	Yes
157	15.70	0.87	0.24	0.63	0.96	0.638	1.04	0.612	1.08	1.30	2.000	Yes
158	15.80	0.87	0.24	0.63	0.96	0.640	1.04	0.613	1.09	1.30	2.000	Yes
159	15.90	0.88	0.25	0.63	0.96	0.641	1.04	0.614	1.09	1.30	2.000	Yes
160	16.00	0.88	0.25	0.63	0.96	0.642	1.04	0.615	1.10	1.30	2.000	Yes
161	16.10	0.89	0.25	0.64	0.96	0.643	1.04	0.616	1.09	1.30	0.738	No
162	16.20	0.90	0.26	0.64	0.96	0.644	1.04	0.617	1.08	1.30	0.745	No
163	16.30	0.90	0.26	0.64	0.96	0.645	1.04	0.618	1.09	1.30	0.734	No
164	16.40	0.91	0.26	0.65	0.96	0.646	1.04	0.619	1.09	1.30	2.000	Yes
165	16.50	0.92	0.27	0.65	0.96	0.647	1.04	0.620	1.09	1.30	2.000	Yes
166	16.60	0.92	0.27	0.65	0.96	0.648	1.04	0.621	1.08	1.30	2.000	Yes
167	16.70	0.93	0.27	0.66	0.96	0.649	1.04	0.622	1.07	1.30	2.000	Yes
168	16.80	0.93	0.27	0.66	0.95	0.650	1.04	0.623	1.06	1.30	2.000	Yes
169	16.90	0.94	0.28	0.66	0.95	0.651	1.04	0.624	1.05	1.30	2.000	Yes
170	17.00	0.95	0.28	0.67	0.95	0.652	1.04	0.625	1.04	1.30	2.000	Yes
171	17.10	0.95	0.28	0.67	0.95	0.654	1.04	0.626	1.04	1.30	2.000	Yes
172	17.20	0.96	0.29	0.67	0.95	0.655	1.04	0.628	1.04	1.30	2.000	Yes
173	17.30	0.96	0.29	0.67	0.95	0.656	1.04	0.629	1.04	1.30	0.816	No
174	17.40	0.97	0.29	0.67	0.95	0.657	1.04	0.630	1.04	1.30	0.819	No
175	17.50	0.97	0.30	0.68	0.95	0.658	1.04	0.631	1.04	1.30	0.821	No
176	17.60	0.98	0.30	0.68	0.95	0.660	1.04	0.632	1.04	1.30	0.823	No
177	17.70	0.98	0.30	0.68	0.95	0.661	1.04	0.634	1.03	1.30	0.824	No
178	17.80	0.99	0.31	0.68	0.95	0.662	1.04	0.635	1.03	1.30	0.826	No
179	17.90	0.99	0.31	0.68	0.95	0.664	1.04	0.636	1.03	1.30	0.828	No
180	18.00	1.00	0.31	0.69	0.95	0.665	1.04	0.637	1.03	1.30	0.830	No
181	18.10	1.00	0.32	0.69	0.95	0.666	1.04	0.638	1.03	1.30	0.831	No
182	18.20	1.01	0.32	0.69	0.95	0.667	1.04	0.639	1.03	1.30	0.832	No
183	18.30	1.01	0.32	0.69	0.95	0.668	1.04	0.641	1.03	1.30	0.834	No
184	18.40	1.02	0.32	0.69	0.95	0.669	1.04	0.642	1.03	1.30	0.835	No
185	18.50	1.02	0.33	0.70	0.95	0.670	1.04	0.643	1.03	1.30	0.836	No
186	18.60	1.03	0.33	0.70	0.95	0.671	1.04	0.644	1.03	1.30	0.837	No
187	18.70	1.04	0.33	0.70	0.95	0.672	1.04	0.645	1.03	1.30	0.838	No
188	18.80	1.04	0.34	0.70	0.95	0.673	1.04	0.645	1.04	1.30	0.838	No
189	18.90	1.05	0.34	0.71	0.95	0.674	1.04	0.646	1.04	1.30	0.838	No
190	19.00	1.05	0.34	0.71	0.95	0.675	1.04	0.647	1.04	1.30	0.838	No
191	19.10	1.06	0.35	0.71	0.95	0.676	1.04	0.648	1.04	1.30	0.839	No
192	19.20	1.06	0.35	0.71	0.95	0.677	1.04	0.649	1.04	1.30	0.840	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
193	19.30	1.07	0.35	0.72	0.94	0.678	1.04	0.650	1.04	1.30	0.842	No
194	19.40	1.08	0.36	0.72	0.94	0.679	1.04	0.650	1.03	1.30	0.844	No
195	19.50	1.08	0.36	0.72	0.94	0.680	1.04	0.651	1.03	1.30	0.847	No
196	19.60	1.09	0.36	0.73	0.94	0.680	1.04	0.652	1.03	1.30	0.848	No
197	19.70	1.09	0.37	0.73	0.94	0.681	1.04	0.653	1.03	1.30	0.849	No
198	19.80	1.10	0.37	0.73	0.94	0.682	1.04	0.654	1.03	1.30	0.848	No
199	19.90	1.10	0.37	0.73	0.94	0.683	1.04	0.654	1.04	1.30	0.848	No
200	20.00	1.11	0.37	0.74	0.94	0.684	1.04	0.655	1.03	1.30	0.850	No
201	20.10	1.12	0.38	0.74	0.94	0.684	1.04	0.656	1.03	1.30	0.853	No
202	20.20	1.12	0.38	0.74	0.94	0.685	1.04	0.657	1.03	1.30	0.858	No
203	20.30	1.13	0.38	0.74	0.94	0.686	1.04	0.658	1.03	1.30	0.861	No
204	20.40	1.13	0.39	0.75	0.94	0.687	1.04	0.659	1.03	1.30	0.862	No
205	20.50	1.14	0.39	0.75	0.94	0.688	1.04	0.659	1.03	1.30	0.864	No
206	20.60	1.14	0.39	0.75	0.94	0.689	1.04	0.660	1.03	1.30	0.866	No
207	20.70	1.15	0.40	0.75	0.94	0.690	1.04	0.661	1.03	1.30	0.867	No
208	20.80	1.15	0.40	0.75	0.94	0.691	1.04	0.662	1.03	1.30	0.869	No
209	20.90	1.16	0.40	0.76	0.94	0.692	1.04	0.663	1.03	1.30	0.870	No
210	21.00	1.16	0.41	0.76	0.94	0.693	1.04	0.664	1.03	1.30	0.871	No
211	21.10	1.17	0.41	0.76	0.94	0.694	1.04	0.665	1.03	1.30	0.873	No
212	21.20	1.17	0.41	0.76	0.94	0.695	1.04	0.666	1.03	1.30	0.874	No
213	21.30	1.18	0.41	0.76	0.94	0.695	1.04	0.667	1.03	1.30	0.875	No
214	21.40	1.18	0.42	0.77	0.94	0.696	1.04	0.667	1.03	1.30	0.876	No
215	21.50	1.19	0.42	0.77	0.94	0.697	1.04	0.668	1.03	1.30	0.877	No
216	21.60	1.19	0.42	0.77	0.94	0.698	1.04	0.669	1.03	1.30	0.877	No
217	21.70	1.20	0.43	0.77	0.93	0.699	1.04	0.670	1.03	1.30	0.879	No
218	21.80	1.21	0.43	0.77	0.93	0.699	1.04	0.670	1.03	1.30	0.880	No
219	21.90	1.21	0.43	0.78	0.93	0.700	1.04	0.671	1.03	1.30	0.881	No
220	22.00	1.22	0.44	0.78	0.93	0.701	1.04	0.672	1.02	1.30	0.883	No
221	22.10	1.22	0.44	0.78	0.93	0.702	1.04	0.673	1.02	1.30	0.884	No
222	22.20	1.23	0.44	0.78	0.93	0.702	1.04	0.673	1.02	1.30	0.885	No
223	22.30	1.23	0.45	0.79	0.93	0.703	1.04	0.674	1.02	1.30	0.886	No
224	22.40	1.24	0.45	0.79	0.93	0.704	1.04	0.675	1.02	1.30	0.886	No
225	22.50	1.24	0.45	0.79	0.93	0.705	1.04	0.675	1.02	1.30	0.887	No
226	22.60	1.25	0.46	0.79	0.93	0.705	1.04	0.676	1.03	1.30	0.886	No
227	22.70	1.25	0.46	0.80	0.93	0.706	1.04	0.676	1.03	1.30	0.884	No
228	22.80	1.26	0.46	0.80	0.93	0.706	1.04	0.677	1.03	1.30	0.881	No
229	22.90	1.27	0.46	0.80	0.93	0.707	1.04	0.677	1.03	1.30	0.878	No
230	23.00	1.27	0.47	0.80	0.93	0.707	1.04	0.678	1.03	1.30	0.879	No
231	23.10	1.28	0.47	0.81	0.93	0.707	1.04	0.678	1.03	1.30	0.881	No
232	23.20	1.29	0.47	0.81	0.93	0.708	1.04	0.679	1.03	1.30	0.884	No
233	23.30	1.29	0.48	0.81	0.93	0.708	1.04	0.679	1.03	1.30	0.886	No
234	23.40	1.30	0.48	0.82	0.93	0.709	1.04	0.679	1.03	1.30	0.888	No
235	23.50	1.30	0.48	0.82	0.93	0.709	1.04	0.680	1.02	1.30	0.889	No
236	23.60	1.31	0.49	0.82	0.93	0.710	1.04	0.680	1.02	1.30	2.000	Yes
237	23.70	1.32	0.49	0.83	0.93	0.710	1.04	0.680	1.02	1.30	2.000	Yes
238	23.80	1.32	0.49	0.83	0.93	0.710	1.04	0.681	1.03	1.30	2.000	Yes
239	23.90	1.33	0.50	0.83	0.93	0.711	1.04	0.681	1.03	1.30	2.000	Yes
240	24.00	1.33	0.50	0.84	0.93	0.711	1.04	0.682	1.03	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
241	24.10	1.34	0.50	0.84	0.92	0.711	1.04	0.682	1.03	1.30	2.000	Yes
242	24.20	1.35	0.51	0.84	0.92	0.712	1.04	0.682	1.03	1.30	2.000	Yes
243	24.30	1.35	0.51	0.84	0.92	0.712	1.04	0.682	1.03	1.30	2.000	Yes
244	24.40	1.36	0.51	0.85	0.92	0.712	1.04	0.683	1.04	1.30	2.000	Yes
245	24.50	1.37	0.51	0.85	0.92	0.713	1.04	0.683	1.04	1.30	2.000	Yes
246	24.60	1.37	0.52	0.85	0.92	0.713	1.04	0.683	1.05	1.30	0.836	No
247	24.70	1.38	0.52	0.86	0.92	0.713	1.04	0.683	1.05	1.30	0.831	No
248	24.80	1.39	0.52	0.86	0.92	0.713	1.04	0.684	1.05	1.30	0.830	No
249	24.90	1.39	0.53	0.86	0.92	0.713	1.04	0.684	1.04	1.30	0.849	No
250	25.00	1.40	0.53	0.87	0.92	0.714	1.04	0.684	1.03	1.30	0.868	No
251	25.10	1.40	0.53	0.87	0.92	0.714	1.04	0.684	1.03	1.30	0.866	No
252	25.20	1.41	0.54	0.87	0.92	0.714	1.04	0.684	1.03	1.30	0.861	No
253	25.30	1.42	0.54	0.88	0.92	0.714	1.04	0.685	1.04	1.30	0.855	No
254	25.40	1.42	0.54	0.88	0.92	0.714	1.04	0.685	1.03	1.30	2.000	Yes
255	25.50	1.43	0.55	0.88	0.92	0.715	1.04	0.685	1.03	1.30	2.000	Yes
256	25.60	1.44	0.55	0.89	0.92	0.715	1.04	0.685	1.03	1.30	2.000	Yes
257	25.70	1.44	0.55	0.89	0.92	0.715	1.04	0.685	1.02	1.30	2.000	Yes
258	25.80	1.45	0.56	0.89	0.92	0.715	1.04	0.686	1.02	1.30	2.000	Yes
259	25.90	1.46	0.56	0.90	0.92	0.716	1.04	0.686	1.02	1.30	2.000	Yes
260	26.00	1.46	0.56	0.90	0.92	0.716	1.04	0.686	1.02	1.30	2.000	Yes
261	26.10	1.47	0.56	0.90	0.92	0.716	1.04	0.687	1.01	1.30	0.911	No
262	26.20	1.47	0.57	0.91	0.92	0.717	1.04	0.687	1.01	1.30	0.912	No
263	26.30	1.48	0.57	0.91	0.92	0.717	1.04	0.687	1.01	1.30	0.913	No
264	26.40	1.48	0.57	0.91	0.91	0.717	1.04	0.688	1.01	1.30	0.914	No
265	26.50	1.49	0.58	0.91	0.91	0.718	1.04	0.688	1.01	1.30	0.914	No
266	26.60	1.50	0.58	0.92	0.91	0.718	1.04	0.688	1.01	1.30	0.915	No
267	26.70	1.50	0.58	0.92	0.91	0.719	1.04	0.689	1.01	1.30	0.916	No
268	26.80	1.51	0.59	0.92	0.91	0.719	1.04	0.689	1.01	1.30	0.916	No
269	26.90	1.51	0.59	0.92	0.91	0.719	1.04	0.689	1.01	1.30	0.916	No
270	27.00	1.52	0.59	0.93	0.91	0.720	1.04	0.690	1.01	1.30	0.917	No
271	27.10	1.52	0.60	0.93	0.91	0.720	1.04	0.690	1.01	1.30	0.918	No
272	27.20	1.53	0.60	0.93	0.91	0.720	1.04	0.690	1.01	1.30	0.919	No
273	27.30	1.54	0.60	0.93	0.91	0.721	1.04	0.691	1.01	1.30	0.920	No
274	27.40	1.54	0.61	0.94	0.91	0.721	1.04	0.691	1.01	1.30	0.921	No
275	27.50	1.55	0.61	0.94	0.91	0.721	1.04	0.691	1.01	1.30	0.921	No
276	27.60	1.55	0.61	0.94	0.91	0.722	1.04	0.692	1.01	1.30	0.922	No
277	27.70	1.56	0.61	0.94	0.91	0.722	1.04	0.692	1.01	1.30	0.923	No
278	27.80	1.56	0.62	0.95	0.91	0.722	1.04	0.692	1.01	1.30	0.923	No
279	27.90	1.57	0.62	0.95	0.91	0.723	1.04	0.693	1.01	1.30	0.924	No
280	28.00	1.57	0.62	0.95	0.91	0.723	1.04	0.693	1.01	1.30	0.925	No
281	28.10	1.58	0.63	0.95	0.91	0.723	1.04	0.693	1.01	1.30	0.925	No
282	28.20	1.59	0.63	0.96	0.91	0.724	1.04	0.694	1.01	1.30	0.925	No
283	28.30	1.59	0.63	0.96	0.91	0.724	1.04	0.694	1.01	1.30	0.924	No
284	28.40	1.60	0.64	0.96	0.91	0.724	1.04	0.694	1.01	1.30	0.920	No
285	28.50	1.60	0.64	0.96	0.91	0.724	1.04	0.694	1.01	1.30	0.917	No
286	28.60	1.61	0.64	0.97	0.90	0.724	1.04	0.694	1.01	1.30	0.919	No
287	28.70	1.62	0.65	0.97	0.90	0.725	1.04	0.694	1.01	1.30	0.922	No
288	28.80	1.62	0.65	0.97	0.90	0.725	1.04	0.695	1.01	1.30	0.923	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
289	28.90	1.63	0.65	0.98	0.90	0.725	1.04	0.695	1.01	1.30	2.000	Yes
290	29.00	1.63	0.66	0.98	0.90	0.725	1.04	0.695	1.01	1.30	2.000	Yes
291	29.10	1.64	0.66	0.98	0.90	0.725	1.04	0.695	1.01	1.30	2.000	Yes
292	29.20	1.65	0.66	0.99	0.90	0.725	1.04	0.695	1.01	1.30	2.000	Yes
293	29.30	1.65	0.66	0.99	0.90	0.725	1.04	0.695	1.01	1.30	2.000	Yes
294	29.40	1.66	0.67	0.99	0.90	0.725	1.04	0.695	1.01	1.30	2.000	Yes
295	29.50	1.67	0.67	1.00	0.90	0.725	1.04	0.695	1.01	1.30	2.000	Yes
296	29.60	1.67	0.67	1.00	0.90	0.725	1.04	0.695	1.01	1.30	2.000	Yes
297	29.70	1.68	0.68	1.00	0.90	0.725	1.04	0.695	1.02	1.30	0.871	No
298	29.80	1.69	0.68	1.01	0.90	0.725	1.04	0.695	1.02	1.30	0.872	No
299	29.90	1.69	0.68	1.01	0.90	0.725	1.04	0.695	1.01	1.30	0.875	No
300	30.00	1.70	0.69	1.01	0.90	0.725	1.04	0.695	1.01	1.30	0.889	No
301	30.10	1.71	0.69	1.02	0.90	0.725	1.04	0.695	1.01	1.30	0.876	No
302	30.20	1.71	0.69	1.02	0.90	0.725	1.04	0.695	1.01	1.30	0.876	No
303	30.30	1.72	0.70	1.02	0.90	0.725	1.04	0.695	1.01	1.30	0.878	No
304	30.40	1.73	0.70	1.03	0.90	0.725	1.04	0.695	1.01	1.30	0.882	No
305	30.50	1.73	0.70	1.03	0.90	0.725	1.04	0.695	1.01	1.30	2.000	Yes
306	30.60	1.74	0.71	1.03	0.90	0.725	1.04	0.695	1.00	1.30	2.000	Yes
307	30.70	1.74	0.71	1.04	0.90	0.725	1.04	0.695	1.00	1.30	2.000	Yes
308	30.80	1.75	0.71	1.04	0.89	0.725	1.04	0.695	1.00	1.30	2.000	Yes
309	30.90	1.76	0.71	1.04	0.89	0.725	1.04	0.695	1.00	1.30	2.000	Yes
310	31.00	1.76	0.72	1.05	0.89	0.725	1.04	0.695	1.00	1.30	2.000	Yes
311	31.10	1.77	0.72	1.05	0.89	0.725	1.04	0.695	1.00	1.30	2.000	Yes
312	31.20	1.78	0.72	1.05	0.89	0.725	1.04	0.695	1.00	1.30	0.925	No
313	31.30	1.78	0.73	1.06	0.89	0.725	1.04	0.695	1.00	1.30	0.924	No
314	31.40	1.79	0.73	1.06	0.89	0.725	1.04	0.695	1.00	1.30	0.924	No
315	31.50	1.79	0.73	1.06	0.89	0.725	1.04	0.695	1.00	1.30	2.000	Yes
316	31.60	1.80	0.74	1.07	0.89	0.725	1.04	0.695	1.00	1.30	2.000	Yes
317	31.70	1.81	0.74	1.07	0.89	0.725	1.04	0.695	1.00	1.30	2.000	Yes
318	31.80	1.81	0.74	1.07	0.89	0.725	1.04	0.694	1.00	1.30	2.000	Yes
319	31.90	1.82	0.75	1.08	0.89	0.724	1.04	0.694	1.00	1.30	2.000	Yes
320	32.00	1.83	0.75	1.08	0.89	0.724	1.04	0.694	0.99	1.30	2.000	Yes
321	32.10	1.83	0.75	1.08	0.89	0.724	1.04	0.694	0.99	1.30	2.000	Yes
322	32.20	1.84	0.76	1.09	0.89	0.724	1.04	0.694	0.99	1.30	2.000	Yes
323	32.30	1.85	0.76	1.09	0.89	0.724	1.04	0.694	0.99	1.30	2.000	Yes
324	32.40	1.85	0.76	1.09	0.89	0.724	1.04	0.694	0.99	1.30	2.000	Yes
325	32.50	1.86	0.76	1.10	0.89	0.724	1.04	0.694	1.00	1.30	2.000	Yes
326	32.60	1.87	0.77	1.10	0.89	0.724	1.04	0.694	1.00	1.30	2.000	Yes
327	32.70	1.87	0.77	1.10	0.89	0.724	1.04	0.694	1.00	1.30	2.000	Yes
328	32.80	1.88	0.77	1.11	0.89	0.724	1.04	0.694	1.00	1.30	2.000	Yes
329	32.90	1.89	0.78	1.11	0.88	0.724	1.04	0.694	1.00	1.30	2.000	Yes
330	33.00	1.89	0.78	1.11	0.88	0.724	1.04	0.694	1.00	1.30	0.935	No
331	33.10	1.90	0.78	1.11	0.88	0.724	1.04	0.694	0.99	1.30	0.934	No
332	33.20	1.90	0.79	1.12	0.88	0.724	1.04	0.694	0.99	1.30	0.935	No
333	33.30	1.91	0.79	1.12	0.88	0.724	1.04	0.694	0.99	1.30	0.935	No
334	33.40	1.92	0.79	1.12	0.88	0.724	1.04	0.694	0.99	1.30	0.935	No
335	33.50	1.92	0.80	1.13	0.88	0.724	1.04	0.694	0.99	1.30	0.934	No
336	33.60	1.93	0.80	1.13	0.88	0.724	1.04	0.694	0.99	1.30	0.934	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
337	33.70	1.93	0.80	1.13	0.88	0.724	1.04	0.694	0.99	1.30	0.934	No
338	33.80	1.94	0.80	1.14	0.88	0.724	1.04	0.694	0.99	1.30	0.933	No
339	33.90	1.95	0.81	1.14	0.88	0.724	1.04	0.694	0.99	1.30	0.933	No
340	34.00	1.95	0.81	1.14	0.88	0.724	1.04	0.694	0.99	1.30	0.934	No
341	34.10	1.96	0.81	1.15	0.88	0.724	1.04	0.694	0.99	1.30	0.936	No
342	34.20	1.97	0.82	1.15	0.88	0.724	1.04	0.693	0.99	1.30	0.937	No
343	34.30	1.97	0.82	1.15	0.88	0.723	1.04	0.693	0.99	1.30	2.000	Yes
344	34.40	1.98	0.82	1.15	0.88	0.723	1.04	0.693	0.99	1.30	2.000	Yes
345	34.50	1.98	0.83	1.16	0.88	0.723	1.04	0.693	0.99	1.30	2.000	Yes
346	34.60	1.99	0.83	1.16	0.88	0.723	1.04	0.693	0.99	1.30	2.000	Yes
347	34.70	2.00	0.83	1.16	0.88	0.723	1.04	0.693	0.99	1.30	2.000	Yes
348	34.80	2.00	0.84	1.17	0.88	0.723	1.04	0.693	0.99	1.30	2.000	Yes
349	34.90	2.01	0.84	1.17	0.88	0.723	1.04	0.693	0.99	1.30	2.000	Yes
350	35.00	2.01	0.84	1.17	0.87	0.723	1.04	0.693	0.99	1.30	2.000	Yes
351	35.10	2.02	0.85	1.18	0.87	0.723	1.04	0.693	0.99	1.30	2.000	Yes
352	35.20	2.03	0.85	1.18	0.87	0.723	1.04	0.693	0.99	1.30	2.000	Yes
353	35.30	2.03	0.85	1.18	0.87	0.723	1.04	0.693	0.99	1.30	0.940	No
354	35.40	2.04	0.85	1.18	0.87	0.723	1.04	0.693	0.99	1.30	0.940	No
355	35.50	2.05	0.86	1.19	0.87	0.723	1.04	0.693	0.99	1.30	0.940	No
356	35.60	2.05	0.86	1.19	0.87	0.723	1.04	0.693	0.99	1.30	0.940	No
357	35.70	2.06	0.86	1.19	0.87	0.723	1.04	0.693	0.99	1.30	0.939	No
358	35.80	2.06	0.87	1.20	0.87	0.723	1.04	0.693	0.99	1.30	0.939	No
359	35.90	2.07	0.87	1.20	0.87	0.723	1.04	0.693	0.99	1.30	0.938	No
360	36.00	2.08	0.87	1.20	0.87	0.723	1.04	0.692	0.99	1.30	0.937	No
361	36.10	2.08	0.88	1.21	0.87	0.722	1.04	0.692	0.99	1.30	0.938	No
362	36.20	2.09	0.88	1.21	0.87	0.722	1.04	0.692	0.99	1.30	0.939	No
363	36.30	2.09	0.88	1.21	0.87	0.722	1.04	0.692	0.99	1.30	0.940	No
364	36.40	2.10	0.89	1.22	0.87	0.722	1.04	0.692	0.99	1.30	2.000	Yes
365	36.50	2.11	0.89	1.22	0.87	0.722	1.04	0.692	0.99	1.30	2.000	Yes
366	36.60	2.11	0.89	1.22	0.87	0.722	1.04	0.692	0.99	1.30	2.000	Yes
367	36.70	2.12	0.90	1.22	0.87	0.722	1.04	0.692	0.98	1.30	2.000	Yes
368	36.80	2.13	0.90	1.23	0.87	0.722	1.04	0.692	0.98	1.30	2.000	Yes
369	36.90	2.13	0.90	1.23	0.87	0.722	1.04	0.692	0.98	1.30	2.000	Yes
370	37.00	2.14	0.90	1.23	0.87	0.721	1.04	0.692	0.98	1.30	2.000	Yes
371	37.10	2.14	0.91	1.24	0.86	0.721	1.04	0.691	0.98	1.30	2.000	Yes
372	37.20	2.15	0.91	1.24	0.86	0.721	1.04	0.691	0.98	1.30	2.000	Yes
373	37.30	2.16	0.91	1.24	0.86	0.721	1.04	0.691	0.98	1.30	2.000	Yes
374	37.40	2.16	0.92	1.25	0.86	0.721	1.04	0.691	0.98	1.30	2.000	Yes
375	37.50	2.17	0.92	1.25	0.86	0.721	1.04	0.691	0.98	1.30	2.000	Yes
376	37.60	2.18	0.92	1.25	0.86	0.721	1.04	0.691	0.98	1.30	2.000	Yes
377	37.70	2.18	0.93	1.26	0.86	0.720	1.04	0.691	0.98	1.30	2.000	Yes
378	37.80	2.19	0.93	1.26	0.86	0.720	1.04	0.690	0.97	1.30	2.000	Yes
379	37.90	2.20	0.93	1.26	0.86	0.720	1.04	0.690	0.97	1.30	2.000	Yes
380	38.00	2.20	0.94	1.27	0.86	0.720	1.04	0.690	0.97	1.30	0.927	No
381	38.10	2.21	0.94	1.27	0.86	0.720	1.04	0.690	0.97	1.30	0.927	No
382	38.20	2.21	0.94	1.27	0.86	0.720	1.04	0.690	0.97	1.30	2.000	Yes
383	38.30	2.22	0.95	1.28	0.86	0.719	1.04	0.690	0.97	1.30	2.000	Yes
384	38.40	2.23	0.95	1.28	0.86	0.719	1.04	0.689	0.97	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
385	38.50	2.23	0.95	1.28	0.86	0.719	1.04	0.689	0.97	1.30	2.000	Yes
386	38.60	2.24	0.95	1.28	0.86	0.719	1.04	0.689	0.97	1.30	2.000	Yes
387	38.70	2.25	0.96	1.29	0.86	0.719	1.04	0.689	0.98	1.30	2.000	Yes
388	38.80	2.25	0.96	1.29	0.86	0.719	1.04	0.689	0.98	1.30	2.000	Yes
389	38.90	2.26	0.96	1.29	0.86	0.718	1.04	0.689	0.98	1.30	0.941	No
390	39.00	2.26	0.97	1.30	0.86	0.718	1.04	0.689	0.98	1.30	0.941	No
391	39.10	2.27	0.97	1.30	0.86	0.718	1.04	0.688	0.98	1.30	0.940	No
392	39.20	2.28	0.97	1.30	0.85	0.718	1.04	0.688	0.98	1.30	0.940	No
393	39.30	2.28	0.98	1.31	0.85	0.718	1.04	0.688	0.98	1.30	0.940	No
394	39.40	2.29	0.98	1.31	0.85	0.718	1.04	0.688	0.98	1.30	0.940	No
395	39.50	2.30	0.98	1.31	0.85	0.718	1.04	0.688	0.97	1.30	0.940	No
396	39.60	2.30	0.99	1.32	0.85	0.718	1.04	0.688	0.97	1.30	0.940	No
397	39.70	2.31	0.99	1.32	0.85	0.717	1.04	0.688	0.97	1.30	2.000	Yes
398	39.80	2.31	0.99	1.32	0.85	0.717	1.04	0.687	0.97	1.30	2.000	Yes
399	39.90	2.32	1.00	1.32	0.85	0.717	1.04	0.687	0.97	1.30	2.000	Yes
400	40.00	2.33	1.00	1.33	0.85	0.717	1.04	0.687	0.97	1.30	2.000	Yes
401	40.10	2.33	1.00	1.33	0.85	0.717	1.04	0.687	0.97	1.30	0.939	No
402	40.20	2.34	1.00	1.33	0.85	0.716	1.04	0.687	0.97	1.30	0.938	No
403	40.30	2.35	1.01	1.34	0.85	0.716	1.04	0.686	0.97	1.30	0.939	No
404	40.40	2.35	1.01	1.34	0.85	0.716	1.04	0.686	0.97	1.30	0.940	No
405	40.50	2.36	1.01	1.34	0.85	0.716	1.04	0.686	0.97	1.30	2.000	Yes
406	40.60	2.36	1.02	1.35	0.85	0.716	1.04	0.686	0.97	1.30	2.000	Yes
407	40.70	2.37	1.02	1.35	0.85	0.715	1.04	0.686	0.97	1.30	2.000	Yes
408	40.80	2.38	1.02	1.35	0.85	0.715	1.04	0.686	0.97	1.30	2.000	Yes
409	40.90	2.38	1.03	1.36	0.85	0.715	1.04	0.685	0.96	1.30	2.000	Yes
410	41.00	2.39	1.03	1.36	0.85	0.715	1.04	0.685	0.96	1.30	2.000	Yes
411	41.10	2.40	1.03	1.36	0.85	0.715	1.04	0.685	0.96	1.30	0.936	No
412	41.20	2.40	1.04	1.37	0.84	0.714	1.04	0.685	0.96	1.30	0.935	No
413	41.30	2.41	1.04	1.37	0.84	0.714	1.04	0.685	0.96	1.30	0.935	No
414	41.40	2.42	1.04	1.37	0.84	0.714	1.04	0.684	0.96	1.30	0.934	No
415	41.50	2.42	1.05	1.38	0.84	0.714	1.04	0.684	0.96	1.30	0.935	No
416	41.60	2.43	1.05	1.38	0.84	0.713	1.04	0.684	0.95	1.30	0.931	No
417	41.70	2.43	1.05	1.38	0.84	0.713	1.04	0.684	0.94	1.30	2.000	Yes
418	41.80	2.44	1.05	1.39	0.84	0.713	1.04	0.683	0.94	1.30	2.000	Yes
419	41.90	2.45	1.06	1.39	0.84	0.713	1.04	0.683	0.95	1.30	2.000	Yes
420	42.00	2.45	1.06	1.39	0.84	0.712	1.04	0.683	0.95	1.30	2.000	Yes
421	42.10	2.46	1.06	1.40	0.84	0.712	1.04	0.683	0.96	1.30	2.000	Yes
422	42.20	2.47	1.07	1.40	0.84	0.712	1.04	0.682	0.96	1.30	2.000	Yes
423	42.30	2.47	1.07	1.40	0.84	0.712	1.04	0.682	0.96	1.30	2.000	Yes
424	42.40	2.48	1.07	1.41	0.84	0.711	1.04	0.682	0.96	1.30	2.000	Yes
425	42.50	2.49	1.08	1.41	0.84	0.711	1.04	0.682	0.95	1.30	2.000	Yes
426	42.60	2.49	1.08	1.41	0.84	0.711	1.04	0.681	0.95	1.30	2.000	Yes
427	42.70	2.50	1.08	1.42	0.84	0.711	1.04	0.681	0.93	1.30	2.000	Yes
428	42.80	2.51	1.09	1.42	0.84	0.710	1.04	0.681	0.92	1.30	2.000	Yes
429	42.90	2.51	1.09	1.42	0.84	0.710	1.04	0.681	0.91	1.30	0.948	No
430	43.00	2.52	1.09	1.43	0.84	0.710	1.04	0.680	0.91	1.30	0.952	No
431	43.10	2.53	1.10	1.43	0.84	0.709	1.04	0.680	0.91	1.30	0.952	No
432	43.20	2.53	1.10	1.43	0.84	0.709	1.04	0.680	0.91	1.30	0.953	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
433	43.30	2.54	1.10	1.44	0.83	0.709	1.04	0.679	0.91	1.30	0.948	No
434	43.40	2.55	1.10	1.44	0.83	0.709	1.04	0.679	0.92	1.30	0.945	No
435	43.50	2.55	1.11	1.44	0.83	0.708	1.04	0.679	0.92	1.30	0.944	No
436	43.60	2.56	1.11	1.45	0.83	0.708	1.04	0.679	0.91	1.30	0.945	No
437	43.70	2.57	1.11	1.45	0.83	0.708	1.04	0.678	0.91	1.30	0.950	No
438	43.80	2.57	1.12	1.46	0.83	0.707	1.04	0.678	0.90	1.30	0.955	No
439	43.90	2.58	1.12	1.46	0.83	0.707	1.04	0.678	0.90	1.30	0.955	No
440	44.00	2.59	1.12	1.46	0.83	0.707	1.04	0.678	0.90	1.30	0.956	No
441	44.10	2.59	1.13	1.47	0.83	0.707	1.04	0.677	0.90	1.30	0.956	No
442	44.20	2.60	1.13	1.47	0.83	0.706	1.04	0.677	0.90	1.30	0.956	No
443	44.30	2.61	1.13	1.47	0.83	0.706	1.04	0.677	0.90	1.30	0.957	No
444	44.40	2.61	1.14	1.48	0.83	0.706	1.04	0.676	0.90	1.30	0.957	No
445	44.50	2.62	1.14	1.48	0.83	0.705	1.04	0.676	0.90	1.30	0.957	No
446	44.60	2.63	1.14	1.48	0.83	0.705	1.04	0.676	0.90	1.30	0.958	No
447	44.70	2.63	1.15	1.49	0.83	0.705	1.04	0.675	0.90	1.30	0.958	No
448	44.80	2.64	1.15	1.49	0.83	0.704	1.04	0.675	0.90	1.30	0.959	No
449	44.90	2.65	1.15	1.49	0.83	0.704	1.04	0.675	0.90	1.30	0.959	No
450	45.00	2.65	1.15	1.50	0.83	0.704	1.04	0.675	0.90	1.30	0.959	No
451	45.10	2.66	1.16	1.50	0.83	0.703	1.04	0.674	0.89	1.30	0.959	No
452	45.20	2.67	1.16	1.51	0.83	0.703	1.04	0.674	0.89	1.30	0.960	No
453	45.30	2.67	1.16	1.51	0.82	0.703	1.04	0.674	0.89	1.30	0.960	No
454	45.40	2.68	1.17	1.51	0.82	0.702	1.04	0.673	0.89	1.30	0.960	No
455	45.50	2.69	1.17	1.52	0.82	0.702	1.04	0.673	0.89	1.30	0.961	No
456	45.60	2.69	1.17	1.52	0.82	0.702	1.04	0.673	0.90	1.30	0.949	No
457	45.70	2.70	1.18	1.52	0.82	0.702	1.04	0.672	0.91	1.30	0.944	No
458	45.80	2.71	1.18	1.53	0.82	0.701	1.04	0.672	0.91	1.30	0.940	No
459	45.90	2.71	1.18	1.53	0.82	0.701	1.04	0.672	0.91	1.30	0.943	No
460	46.00	2.72	1.19	1.53	0.82	0.701	1.04	0.672	0.90	1.30	0.955	No
461	46.10	2.73	1.19	1.54	0.82	0.700	1.04	0.671	0.89	1.30	0.963	No
462	46.20	2.73	1.19	1.54	0.82	0.700	1.04	0.671	0.89	1.30	0.963	No
463	46.30	2.74	1.19	1.54	0.82	0.700	1.04	0.671	0.89	1.30	0.963	No
464	46.40	2.75	1.20	1.55	0.82	0.699	1.04	0.670	0.89	1.30	0.964	No
465	46.50	2.75	1.20	1.55	0.82	0.699	1.04	0.670	0.89	1.30	0.964	No
466	46.60	2.76	1.20	1.55	0.82	0.699	1.04	0.670	0.88	1.30	0.964	No
467	46.70	2.77	1.21	1.56	0.82	0.698	1.04	0.669	0.88	1.30	0.965	No
468	46.80	2.77	1.21	1.56	0.82	0.698	1.04	0.669	0.88	1.30	0.965	No
469	46.90	2.78	1.21	1.57	0.82	0.698	1.04	0.669	0.88	1.30	0.965	No
470	47.00	2.79	1.22	1.57	0.82	0.697	1.04	0.668	0.88	1.30	0.965	No
471	47.10	2.79	1.22	1.57	0.82	0.697	1.04	0.668	0.88	1.30	0.966	No
472	47.20	2.80	1.22	1.58	0.82	0.697	1.04	0.668	0.88	1.30	0.966	No
473	47.30	2.81	1.23	1.58	0.82	0.696	1.04	0.667	0.88	1.30	0.966	No
474	47.40	2.81	1.23	1.58	0.81	0.696	1.04	0.667	0.88	1.30	0.967	No
475	47.50	2.82	1.23	1.59	0.81	0.696	1.04	0.667	0.88	1.30	0.967	No
476	47.60	2.83	1.24	1.59	0.81	0.695	1.04	0.666	0.88	1.30	0.967	No
477	47.70	2.83	1.24	1.59	0.81	0.695	1.04	0.666	0.88	1.30	0.967	No
478	47.80	2.84	1.24	1.60	0.81	0.695	1.04	0.666	0.89	1.30	0.956	No
479	47.90	2.85	1.24	1.60	0.81	0.694	1.04	0.666	0.89	1.30	2.000	Yes
480	48.00	2.85	1.25	1.60	0.81	0.694	1.04	0.665	0.88	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
481	48.10	2.86	1.25	1.61	0.81	0.694	1.04	0.665	0.87	1.30	2.000	Yes
482	48.20	2.87	1.25	1.61	0.81	0.693	1.04	0.665	0.87	1.30	2.000	Yes
483	48.30	2.87	1.26	1.62	0.81	0.693	1.04	0.664	0.91	1.30	2.000	Yes
484	48.40	2.88	1.26	1.62	0.81	0.693	1.04	0.664	0.94	1.30	2.000	Yes
485	48.50	2.89	1.26	1.62	0.81	0.692	1.04	0.664	0.95	1.30	2.000	Yes
486	48.60	2.89	1.27	1.63	0.81	0.692	1.04	0.663	0.95	1.30	2.000	Yes
487	48.70	2.90	1.27	1.63	0.81	0.692	1.04	0.663	0.95	1.30	2.000	Yes
488	48.80	2.90	1.27	1.63	0.81	0.692	1.04	0.663	0.96	1.30	2.000	Yes
489	48.90	2.91	1.28	1.63	0.81	0.692	1.04	0.663	0.95	1.30	2.000	Yes
490	49.00	2.92	1.28	1.64	0.81	0.691	1.04	0.663	0.95	1.30	2.000	Yes
491	49.10	2.92	1.28	1.64	0.81	0.691	1.04	0.662	0.94	1.30	2.000	Yes
492	49.20	2.93	1.29	1.64	0.81	0.691	1.04	0.662	0.93	1.30	2.000	Yes
493	49.30	2.94	1.29	1.65	0.81	0.690	1.04	0.662	0.92	1.30	2.000	Yes
494	49.40	2.94	1.29	1.65	0.80	0.690	1.04	0.661	0.90	1.30	2.000	Yes
495	49.50	2.95	1.29	1.65	0.80	0.690	1.04	0.661	0.89	1.30	2.000	Yes
496	49.60	2.96	1.30	1.66	0.80	0.690	1.04	0.661	0.89	1.30	2.000	Yes
497	49.70	2.96	1.30	1.66	0.80	0.689	1.04	0.661	0.89	1.30	2.000	Yes
498	49.80	2.97	1.30	1.66	0.80	0.689	1.04	0.660	0.88	1.30	2.000	Yes
499	49.90	2.97	1.31	1.67	0.80	0.689	1.04	0.660	0.87	1.30	2.000	Yes

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
 σ_v : Total overburden pressure at test point (tsf)
 u_0 : Water pressure at test point (tsf)
 σ_v' : Effective overburden pressure based on GWT during earthquake (tsf)
 r_d : Nonlinear shear mass factor
 CSR: Cyclic Stress Ratio
 MSF: Magnitude Scaling Factor
 CSR_{eq} : CSR adjusted for M=7.5
 K_σ : Effective overburden stress factor
 CSR*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1	0.10	35.03	58.71	2.45	0.46	1.70	55.68	63.94	119.62	4.000	No	No	2.00
2	0.20	35.16	59.37	2.45	0.45	1.70	57.38	64.61	121.99	4.000	No	No	2.00
3	0.30	34.73	60.81	2.47	0.45	1.70	56.33	64.74	121.07	4.000	No	No	2.00
4	0.40	33.65	62.24	2.49	0.46	1.70	53.62	64.38	118.00	4.000	No	No	2.00
5	0.50	32.47	62.49	2.49	0.46	1.70	52.15	64.03	116.18	4.000	No	No	2.00
6	0.60	31.69	61.29	2.48	0.47	1.70	50.65	63.28	113.92	4.000	No	No	2.00
7	0.70	31.23	59.73	2.46	0.47	1.70	49.90	62.63	112.53	4.000	No	No	2.00
8	0.80	31.07	58.65	2.45	0.47	1.70	49.90	62.31	112.21	4.000	No	No	2.00
9	0.90	31.07	58.20	2.44	0.47	1.70	49.90	62.17	112.07	4.000	No	No	2.00
10	1.00	30.99	58.07	2.44	0.47	1.70	49.90	62.13	112.03	4.000	No	No	2.00
11	1.10	30.22	58.41	2.44	0.47	1.70	49.50	62.12	111.62	4.000	No	No	2.00
12	1.20	28.62	59.57	2.46	0.48	1.70	46.22	61.55	107.77	4.000	No	No	2.00
13	1.30	25.29	63.15	2.50	0.49	1.70	42.18	61.37	103.55	4.000	No	No	2.00
14	1.40	21.46	69.09	2.58	0.51	1.70	33.44	60.18	93.62	4.000	No	No	2.00
15	1.50	19.76	74.84	2.65	0.53	1.70	27.76	0.00	27.76	4.000	No	Yes	2.00
16	1.60	17.77	81.11	2.73	0.51	1.70	33.97	0.00	33.97	4.000	No	Yes	2.00
17	1.70	17.28	85.14	2.78	0.54	1.70	23.86	0.00	23.86	4.000	No	Yes	2.00
18	1.80	17.01	88.22	2.82	0.53	1.70	25.41	0.00	25.41	4.000	No	Yes	2.00
19	1.90	17.94	86.93	2.80	0.51	1.70	32.66	0.00	32.66	4.000	No	Yes	2.00
20	2.00	18.20	84.70	2.77	0.52	1.70	28.32	0.00	28.32	4.000	No	Yes	2.00
21	2.10	17.74	81.55	2.73	0.53	1.70	26.70	0.00	26.70	4.000	No	Yes	2.00
22	2.20	17.81	78.81	2.70	0.52	1.70	30.45	0.00	30.45	4.000	No	Yes	2.00
23	2.30	17.30	79.36	2.70	0.52	1.70	28.62	0.00	28.62	4.000	No	Yes	2.00
24	2.40	15.15	84.65	2.77	0.54	1.70	24.25	0.00	24.25	4.000	No	Yes	2.00
25	2.50	12.68	91.56	2.86	0.55	1.70	20.10	0.00	20.10	4.000	No	Yes	2.00
26	2.60	10.83	97.20	2.93	0.56	1.70	16.70	0.00	16.70	4.000	No	Yes	2.00
27	2.70	10.19	99.48	2.96	0.56	1.70	15.35	0.00	15.35	4.000	No	Yes	2.00
28	2.80	10.31	99.09	2.95	0.56	1.70	17.02	0.00	17.02	4.000	No	Yes	2.00
29	2.90	11.42	95.62	2.91	0.56	1.70	17.27	0.00	17.27	4.000	No	Yes	2.00
30	3.00	13.17	90.22	2.84	0.55	1.70	20.70	0.00	20.70	4.000	No	Yes	2.00
31	3.10	14.98	85.23	2.78	0.53	1.70	25.47	0.00	25.47	4.000	No	Yes	2.00
32	3.20	15.49	83.53	2.76	0.53	1.70	26.01	0.00	26.01	4.000	No	Yes	2.00
33	3.30	14.62	85.36	2.78	0.54	1.70	23.14	0.00	23.14	4.000	No	Yes	2.00
34	3.40	13.98	87.48	2.81	0.54	1.70	21.30	0.00	21.30	4.000	No	Yes	2.00
35	3.50	15.01	85.34	2.78	0.54	1.70	22.92	0.00	22.92	4.000	No	Yes	2.00
36	3.60	17.48	79.34	2.70	0.53	1.70	28.08	0.00	28.08	4.000	No	Yes	2.00
37	3.70	20.02	73.25	2.63	0.51	1.70	33.19	0.00	33.19	4.000	No	Yes	2.00
38	3.80	20.81	71.24	2.60	0.51	1.70	35.16	0.00	35.16	4.000	No	Yes	2.00
39	3.90	19.38	74.39	2.64	0.51	1.70	31.92	0.00	31.92	4.000	No	Yes	2.00
40	4.00	16.73	81.55	2.73	0.53	1.70	26.27	0.00	26.27	4.000	No	Yes	2.00
41	4.10	14.89	87.75	2.81	0.54	1.70	22.41	0.00	22.41	4.000	No	Yes	2.00
42	4.20	15.11	87.95	2.81	0.54	1.70	23.04	0.00	23.04	4.000	Yes	Yes	2.00
43	4.30	17.12	82.21	2.74	0.53	1.70	27.35	0.00	27.35	4.000	Yes	Yes	2.00
44	4.40	20.17	73.69	2.63	0.51	1.70	32.07	0.00	32.07	4.000	Yes	Yes	2.00
45	4.50	23.37	65.66	2.53	0.50	1.70	37.73	60.69	98.42	4.000	Yes	No	2.00
46	4.60	26.36	59.32	2.45	0.49	1.70	42.78	60.52	103.29	4.000	Yes	No	2.00
47	4.70	28.28	55.23	2.40	0.48	1.70	46.48	60.27	106.76	4.000	Yes	No	2.00
48	4.80	28.50	53.68	2.38	0.48	1.70	47.02	59.88	106.90	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
49	4.90	26.77	55.69	2.41	0.49	1.70	43.83	59.70	103.53	4.000	Yes	No	2.00
50	5.00	23.34	61.77	2.48	0.50	1.70	38.14	59.88	98.02	4.000	Yes	No	2.00
51	5.10	18.70	71.27	2.60	0.52	1.70	30.49	0.00	30.49	4.000	Yes	Yes	2.00
52	5.20	14.38	81.98	2.74	0.55	1.70	21.47	0.00	21.47	4.000	Yes	Yes	2.00
53	5.30	11.34	91.18	2.85	0.56	1.70	17.33	0.00	17.33	4.000	Yes	Yes	2.00
54	5.40	9.53	97.63	2.93	0.56	1.70	15.81	0.00	15.81	4.000	Yes	Yes	2.00
55	5.50	8.69	100.00	2.98	0.57	1.70	12.78	0.00	12.78	4.000	Yes	Yes	2.00
56	5.60	10.46	98.06	2.94	0.57	1.70	13.28	0.00	13.28	4.000	No	Yes	2.00
57	5.70	12.39	94.16	2.89	0.53	1.70	24.31	0.00	24.31	4.000	No	Yes	2.00
58	5.80	13.72	91.53	2.86	0.54	1.70	22.09	0.00	22.09	4.000	No	Yes	2.00
59	5.90	11.35	96.30	2.92	0.55	1.70	19.67	0.00	19.67	4.000	No	Yes	2.00
60	6.00	9.16	100.00	2.98	0.57	1.70	12.93	0.00	12.93	4.000	No	Yes	2.00
61	6.10	7.81	100.00	3.00	0.58	1.70	11.52	0.00	11.52	4.000	No	Yes	2.00
62	6.20	9.31	93.77	2.88	0.57	1.70	13.20	0.00	13.20	4.000	Yes	Yes	2.00
63	6.30	13.02	78.90	2.70	0.55	1.70	20.14	0.00	20.14	4.000	Yes	Yes	2.00
64	6.40	17.23	65.59	2.53	0.53	1.70	29.38	58.28	87.66	4.000	Yes	No	2.00
65	6.50	19.97	56.12	2.41	0.52	1.70	33.50	56.99	90.49	4.000	Yes	No	2.00
66	6.60	21.02	52.90	2.37	0.52	1.70	33.36	55.91	89.27	4.000	Yes	No	2.00
67	6.70	21.55	54.66	2.40	0.52	1.70	34.39	56.78	91.16	4.000	No	No	2.00
68	6.80	24.54	54.76	2.40	0.51	1.68	35.59	57.14	92.73	4.000	No	No	2.00
69	6.90	28.95	52.52	2.37	0.49	1.62	45.62	59.08	104.69	4.000	No	No	2.00
70	7.00	33.02	50.72	2.35	0.47	1.59	51.99	60.08	112.07	4.000	No	No	2.00
71	7.10	34.38	51.83	2.36	0.47	1.58	51.63	60.43	112.06	4.000	Yes	No	2.00
72	7.20	33.32	54.26	2.39	0.47	1.57	50.17	60.94	111.12	4.000	Yes	No	2.00
73	7.30	30.96	57.07	2.43	0.48	1.57	46.62	60.91	107.53	4.000	Yes	No	2.00
74	7.40	27.34	61.81	2.49	0.49	1.58	41.04	60.71	101.75	4.000	Yes	No	2.00
75	7.50	23.15	69.32	2.58	0.51	1.59	34.47	60.53	95.00	4.000	Yes	No	2.00
76	7.60	18.85	79.27	2.70	0.52	1.60	28.46	0.00	28.46	4.000	Yes	Yes	2.00
77	7.70	15.01	89.56	2.83	0.54	1.61	22.29	0.00	22.29	4.000	Yes	Yes	2.00
78	7.80	12.30	97.95	2.94	0.55	1.62	17.55	0.00	17.55	4.000	Yes	Yes	2.00
79	7.90	11.37	100.00	2.97	0.56	1.61	16.38	0.00	16.38	4.000	Yes	Yes	2.00
80	8.00	12.13	97.41	2.93	0.55	1.59	17.85	0.00	17.85	4.000	Yes	Yes	2.00
81	8.10	13.66	91.01	2.85	0.55	1.58	20.55	0.00	20.55	4.000	Yes	Yes	2.00
82	8.20	15.81	82.85	2.75	0.54	1.57	22.71	0.00	22.71	4.000	Yes	Yes	2.00
83	8.30	18.07	74.31	2.64	0.53	1.55	26.81	0.00	26.81	4.000	Yes	Yes	2.00
84	8.40	19.89	67.15	2.55	0.52	1.54	29.86	58.75	88.62	4.000	Yes	No	2.00
85	8.50	20.92	62.36	2.49	0.53	1.54	30.16	57.77	87.93	4.000	Yes	No	2.00
86	8.60	21.23	59.36	2.45	0.53	1.53	30.95	57.22	88.17	4.000	Yes	No	2.00
87	8.70	21.47	57.35	2.43	0.53	1.53	31.05	56.69	87.73	0.123	No	No	0.21
88	8.80	21.51	56.64	2.42	0.53	1.52	30.98	56.46	87.44	0.123	No	No	0.21
89	8.90	21.51	58.06	2.44	0.53	1.52	30.88	56.84	87.73	4.000	Yes	No	2.00
90	9.00	20.90	62.01	2.49	0.52	1.51	30.75	57.85	88.59	4.000	Yes	No	2.00
91	9.10	19.70	67.13	2.55	0.53	1.52	28.19	58.27	86.45	4.000	Yes	No	2.00
92	9.20	19.12	70.72	2.60	0.54	1.52	25.68	58.23	83.91	4.000	Yes	No	2.00
93	9.30	19.54	71.26	2.60	0.53	1.51	28.09	0.00	28.09	4.000	No	Yes	2.00
94	9.40	20.38	70.49	2.59	0.52	1.50	29.61	59.33	88.94	0.125	No	No	0.20
95	9.50	19.23	73.47	2.63	0.52	1.49	28.80	0.00	28.80	4.000	No	Yes	2.00
96	9.60	16.01	81.00	2.72	0.54	1.51	23.21	0.00	23.21	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
97	9.70	13.82	88.61	2.82	0.56	1.53	16.30	0.00	16.30	4.000	No	Yes	2.00
98	9.80	15.64	86.64	2.80	0.55	1.51	19.75	0.00	19.75	4.000	No	Yes	2.00
99	9.90	16.35	84.98	2.77	0.52	1.47	30.17	0.00	30.17	4.000	No	Yes	2.00
100	10.00	13.35	89.98	2.84	0.55	1.50	19.06	0.00	19.06	4.000	No	Yes	2.00
101	10.10	8.41	100.00	3.00	0.59	1.55	7.09	0.00	7.09	4.000	No	Yes	2.00
102	10.20	7.41	100.00	3.05	0.58	1.53	10.05	0.00	10.05	4.000	No	Yes	2.00
103	10.30	10.53	95.20	2.90	0.57	1.51	14.84	0.00	14.84	4.000	No	Yes	2.00
104	10.40	13.79	86.23	2.79	0.55	1.49	19.95	0.00	19.95	4.000	No	Yes	2.00
105	10.50	16.27	81.58	2.73	0.54	1.47	23.24	0.00	23.24	4.000	No	Yes	2.00
106	10.60	16.77	82.21	2.74	0.53	1.46	24.69	0.00	24.69	4.000	No	Yes	2.00
107	10.70	14.80	88.15	2.81	0.54	1.47	21.77	0.00	21.77	4.000	No	Yes	2.00
108	10.80	11.32	98.45	2.94	0.56	1.48	15.15	0.00	15.15	4.000	No	Yes	2.00
109	10.90	7.88	100.00	3.10	0.58	1.50	10.51	0.00	10.51	4.000	No	Yes	2.00
110	11.00	5.67	100.00	3.23	0.59	1.51	7.70	0.00	7.70	4.000	No	Yes	2.00
111	11.10	4.53	100.00	3.30	0.60	1.51	5.96	0.00	5.96	4.000	No	Yes	2.00
112	11.20	4.05	100.00	3.31	0.60	1.51	5.68	0.00	5.68	4.000	No	Yes	2.00
113	11.30	3.98	100.00	3.29	0.60	1.51	5.66	0.00	5.66	4.000	No	Yes	2.00
114	11.40	3.98	100.00	3.28	0.60	1.50	5.65	0.00	5.65	4.000	No	Yes	2.00
115	11.50	3.98	100.00	3.28	0.60	1.50	5.64	0.00	5.64	4.000	No	Yes	2.00
116	11.60	3.98	100.00	3.29	0.60	1.50	5.63	0.00	5.63	4.000	No	Yes	2.00
117	11.70	3.98	100.00	3.30	0.60	1.49	5.62	0.00	5.62	4.000	No	Yes	2.00
118	11.80	3.92	100.00	3.33	0.60	1.49	5.61	0.00	5.61	4.000	No	Yes	2.00
119	11.90	3.81	100.00	3.35	0.60	1.49	5.33	0.00	5.33	4.000	No	Yes	2.00
120	12.00	4.07	100.00	3.32	0.60	1.49	5.12	0.00	5.12	4.000	No	Yes	2.00
121	12.10	4.67	100.00	3.25	0.60	1.48	6.67	0.00	6.67	4.000	No	Yes	2.00
122	12.20	5.31	100.00	3.19	0.59	1.47	7.74	0.00	7.74	4.000	No	Yes	2.00
123	12.30	5.58	100.00	3.16	0.59	1.47	7.72	0.00	7.72	4.000	No	Yes	2.00
124	12.40	5.58	100.00	3.16	0.59	1.46	7.71	0.00	7.71	4.000	No	Yes	2.00
125	12.50	5.58	100.00	3.16	0.59	1.46	7.69	0.00	7.69	4.000	No	Yes	2.00
126	12.60	5.58	100.00	3.16	0.59	1.46	7.68	0.00	7.68	4.000	No	Yes	2.00
127	12.70	5.58	100.00	3.18	0.59	1.45	7.66	0.00	7.66	4.000	No	Yes	2.00
128	12.80	5.58	100.00	3.19	0.59	1.45	7.64	0.00	7.64	4.000	No	Yes	2.00
129	12.90	5.58	100.00	3.21	0.59	1.45	7.63	0.00	7.63	4.000	No	Yes	2.00
130	13.00	5.80	100.00	3.21	0.59	1.44	7.61	0.00	7.61	4.000	No	Yes	2.00
131	13.10	6.32	100.00	3.18	0.59	1.44	8.47	0.00	8.47	4.000	No	Yes	2.00
132	13.20	6.51	100.00	3.16	0.58	1.43	9.65	0.00	9.65	4.000	No	Yes	2.00
133	13.30	5.94	100.00	3.19	0.59	1.43	8.34	0.00	8.34	4.000	No	Yes	2.00
134	13.40	4.89	100.00	3.26	0.60	1.44	6.15	0.00	6.15	4.000	No	Yes	2.00
135	13.50	4.17	100.00	3.32	0.60	1.44	5.41	0.00	5.41	4.000	No	Yes	2.00
136	13.60	3.98	100.00	3.33	0.60	1.43	5.40	0.00	5.40	4.000	No	Yes	2.00
137	13.70	3.98	100.00	3.32	0.60	1.43	5.39	0.00	5.39	4.000	No	Yes	2.00
138	13.80	3.98	100.00	3.33	0.60	1.43	5.38	0.00	5.38	4.000	No	Yes	2.00
139	13.90	3.98	100.00	3.34	0.60	1.43	5.37	0.00	5.37	4.000	No	Yes	2.00
140	14.00	3.98	100.00	3.35	0.60	1.42	5.36	0.00	5.36	4.000	No	Yes	2.00
141	14.10	3.98	100.00	3.34	0.60	1.42	5.35	0.00	5.35	4.000	No	Yes	2.00
142	14.20	3.98	100.00	3.33	0.60	1.42	5.34	0.00	5.34	4.000	No	Yes	2.00
143	14.30	3.76	100.00	3.35	0.60	1.42	5.33	0.00	5.33	4.000	No	Yes	2.00
144	14.40	3.50	100.00	3.39	0.60	1.42	4.44	0.00	4.44	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
145	14.50	3.50	100.00	3.39	0.61	1.41	4.26	0.00	4.26	4.000	No	Yes	2.00
146	14.60	3.72	100.00	3.35	0.60	1.41	5.30	0.00	5.30	4.000	No	Yes	2.00
147	14.70	4.09	100.00	3.31	0.60	1.41	5.29	0.00	5.29	4.000	No	Yes	2.00
148	14.80	4.51	100.00	3.29	0.60	1.40	5.70	0.00	5.70	4.000	No	Yes	2.00
149	14.90	5.25	100.00	3.25	0.59	1.39	6.92	0.00	6.92	4.000	No	Yes	2.00
150	15.00	6.18	100.00	3.21	0.59	1.39	8.11	0.00	8.11	4.000	No	Yes	2.00
151	15.10	7.12	100.00	3.16	0.59	1.38	9.27	0.00	9.27	4.000	No	Yes	2.00
152	15.20	9.50	100.00	3.04	0.58	1.37	10.50	0.00	10.50	4.000	No	Yes	2.00
153	15.30	14.31	91.63	2.86	0.56	1.35	17.04	0.00	17.04	4.000	Yes	Yes	2.00
154	15.40	22.91	74.96	2.65	0.53	1.33	27.05	0.00	27.05	4.000	Yes	Yes	2.00
155	15.50	34.71	59.19	2.45	0.49	1.30	41.71	60.18	101.89	4.000	Yes	No	2.00
156	15.60	50.28	45.60	2.28	0.46	1.28	58.76	59.46	118.22	4.000	Yes	No	2.00
157	15.70	67.84	35.99	2.16	0.42	1.25	80.54	58.05	138.59	4.000	Yes	No	2.00
158	15.80	85.19	27.87	2.06	0.40	1.23	100.64	52.59	153.23	4.000	Yes	No	2.00
159	15.90	100.36	21.55	1.98	0.39	1.22	116.27	43.05	159.32	4.000	Yes	No	2.00
160	16.00	105.72	18.70	1.95	0.38	1.21	130.21	37.41	167.62	4.000	Yes	No	2.00
161	16.10	103.10	20.19	1.96	0.39	1.22	118.15	39.95	158.10	0.353	No	No	0.48
162	16.20	98.78	23.43	2.01	0.40	1.22	107.14	45.81	152.95	0.310	No	No	0.42
163	16.30	98.29	25.42	2.03	0.38	1.21	114.87	51.03	165.90	0.442	No	No	0.60
164	16.40	97.60	27.05	2.05	0.37	1.20	114.83	53.95	168.78	4.000	Yes	No	2.00
165	16.50	89.65	30.71	2.10	0.39	1.21	103.50	57.22	160.73	4.000	Yes	No	2.00
166	16.60	76.67	36.94	2.17	0.41	1.22	88.38	60.71	149.09	4.000	Yes	No	2.00
167	16.70	61.52	45.60	2.28	0.43	1.23	72.15	62.88	135.04	4.000	Yes	No	2.00
168	16.80	46.02	56.37	2.42	0.46	1.25	53.36	62.54	115.90	4.000	Yes	No	2.00
169	16.90	32.20	68.48	2.57	0.50	1.27	36.41	60.92	97.33	4.000	Yes	No	2.00
170	17.00	21.83	80.69	2.72	0.53	1.28	25.15	0.00	25.15	4.000	Yes	Yes	2.00
171	17.10	15.15	91.35	2.85	0.56	1.29	17.39	0.00	17.39	4.000	Yes	Yes	2.00
172	17.20	10.77	100.00	2.97	0.57	1.30	12.78	0.00	12.78	4.000	Yes	Yes	2.00
173	17.30	8.03	100.00	3.07	0.58	1.30	9.39	0.00	9.39	4.000	No	Yes	2.00
174	17.40	6.41	100.00	3.14	0.59	1.31	7.43	0.00	7.43	4.000	No	Yes	2.00
175	17.50	5.73	100.00	3.17	0.59	1.30	6.87	0.00	6.87	4.000	No	Yes	2.00
176	17.60	5.58	100.00	3.15	0.59	1.30	6.86	0.00	6.86	4.000	No	Yes	2.00
177	17.70	5.58	100.00	3.13	0.59	1.30	6.85	0.00	6.85	4.000	No	Yes	2.00
178	17.80	5.58	100.00	3.12	0.59	1.30	6.84	0.00	6.84	4.000	No	Yes	2.00
179	17.90	5.58	100.00	3.11	0.59	1.30	6.83	0.00	6.83	4.000	No	Yes	2.00
180	18.00	5.72	100.00	3.10	0.59	1.29	6.82	0.00	6.82	4.000	No	Yes	2.00
181	18.10	6.17	100.00	3.08	0.59	1.29	7.32	0.00	7.32	4.000	No	Yes	2.00
182	18.20	6.71	100.00	3.09	0.59	1.29	8.43	0.00	8.43	4.000	No	Yes	2.00
183	18.30	7.09	100.00	3.13	0.59	1.28	8.69	0.00	8.69	4.000	No	Yes	2.00
184	18.40	7.50	100.00	3.16	0.59	1.28	8.68	0.00	8.68	4.000	No	Yes	2.00
185	18.50	8.13	100.00	3.16	0.58	1.28	9.83	0.00	9.83	4.000	No	Yes	2.00
186	18.60	9.21	100.00	3.13	0.58	1.27	10.87	0.00	10.87	4.000	No	Yes	2.00
187	18.70	10.73	100.00	3.06	0.57	1.27	12.45	0.00	12.45	4.000	No	Yes	2.00
188	18.80	12.95	100.00	2.98	0.56	1.26	15.11	0.00	15.11	4.000	No	Yes	2.00
189	18.90	16.09	92.46	2.87	0.55	1.25	18.54	0.00	18.54	4.000	No	Yes	2.00
190	19.00	18.81	85.50	2.78	0.54	1.24	23.23	0.00	23.23	4.000	No	Yes	2.00
191	19.10	20.48	81.77	2.73	0.54	1.24	24.42	0.00	24.42	4.000	No	Yes	2.00
192	19.20	20.52	82.39	2.74	0.54	1.23	24.13	0.00	24.13	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
193	19.30	19.41	86.04	2.79	0.54	1.23	23.24	0.00	23.24	4.000	No	Yes	2.00
194	19.40	17.68	90.23	2.84	0.55	1.23	20.47	0.00	20.47	4.000	No	Yes	2.00
195	19.50	16.31	92.51	2.87	0.55	1.24	18.11	0.00	18.11	4.000	No	Yes	2.00
196	19.60	16.30	90.89	2.85	0.55	1.23	18.44	0.00	18.44	4.000	No	Yes	2.00
197	19.70	18.29	85.84	2.79	0.55	1.23	20.35	0.00	20.35	4.000	No	Yes	2.00
198	19.80	20.97	81.15	2.73	0.54	1.22	24.73	0.00	24.73	4.000	No	Yes	2.00
199	19.90	22.75	79.59	2.71	0.53	1.21	27.39	0.00	27.39	4.000	No	Yes	2.00
200	20.00	21.58	82.86	2.75	0.53	1.21	26.18	0.00	26.18	4.000	No	Yes	2.00
201	20.10	17.47	90.47	2.84	0.55	1.22	20.65	0.00	20.65	4.000	No	Yes	2.00
202	20.20	12.54	100.00	2.97	0.57	1.22	13.39	0.00	13.39	4.000	No	Yes	2.00
203	20.30	8.93	100.00	3.08	0.58	1.23	9.39	0.00	9.39	4.000	No	Yes	2.00
204	20.40	7.14	100.00	3.13	0.59	1.23	8.26	0.00	8.26	4.000	No	Yes	2.00
205	20.50	6.30	100.00	3.14	0.59	1.23	7.20	0.00	7.20	4.000	No	Yes	2.00
206	20.60	5.79	100.00	3.16	0.60	1.23	6.47	0.00	6.47	4.000	No	Yes	2.00
207	20.70	5.58	100.00	3.21	0.60	1.23	6.46	0.00	6.46	4.000	No	Yes	2.00
208	20.80	5.55	100.00	3.25	0.60	1.22	6.45	0.00	6.45	4.000	No	Yes	2.00
209	20.90	5.51	100.00	3.28	0.60	1.22	6.34	0.00	6.34	4.000	No	Yes	2.00
210	21.00	5.50	100.00	3.29	0.60	1.22	6.32	0.00	6.32	4.000	No	Yes	2.00
211	21.10	5.47	100.00	3.28	0.60	1.22	6.36	0.00	6.36	4.000	No	Yes	2.00
212	21.20	5.83	100.00	3.26	0.60	1.22	6.23	0.00	6.23	4.000	No	Yes	2.00
213	21.30	6.38	100.00	3.25	0.59	1.21	7.51	0.00	7.51	4.000	No	Yes	2.00
214	21.40	7.19	100.00	3.23	0.59	1.21	8.20	0.00	8.20	4.000	No	Yes	2.00
215	21.50	7.91	100.00	3.21	0.59	1.21	8.93	0.00	8.93	4.000	No	Yes	2.00
216	21.60	8.45	100.00	3.18	0.58	1.20	9.93	0.00	9.93	4.000	No	Yes	2.00
217	21.70	8.76	100.00	3.15	0.58	1.20	9.94	0.00	9.94	4.000	No	Yes	2.00
218	21.80	8.66	100.00	3.13	0.58	1.20	9.93	0.00	9.93	4.000	No	Yes	2.00
219	21.90	8.24	100.00	3.14	0.58	1.20	9.56	0.00	9.56	4.000	No	Yes	2.00
220	22.00	7.71	100.00	3.16	0.59	1.20	8.49	0.00	8.49	4.000	No	Yes	2.00
221	22.10	7.52	100.00	3.17	0.59	1.20	8.10	0.00	8.10	4.000	No	Yes	2.00
222	22.20	7.95	100.00	3.16	0.59	1.19	8.89	0.00	8.89	4.000	No	Yes	2.00
223	22.30	8.79	100.00	3.13	0.58	1.19	9.87	0.00	9.87	4.000	No	Yes	2.00
224	22.40	9.90	100.00	3.10	0.58	1.19	10.85	0.00	10.85	4.000	No	Yes	2.00
225	22.50	12.35	100.00	3.03	0.57	1.18	12.55	0.00	12.55	4.000	No	Yes	2.00
226	22.60	16.82	94.84	2.90	0.55	1.17	17.87	0.00	17.87	4.000	No	Yes	2.00
227	22.70	23.64	82.79	2.75	0.53	1.16	25.39	0.00	25.39	4.000	No	Yes	2.00
228	22.80	31.17	73.46	2.63	0.51	1.15	34.54	0.00	34.54	4.000	No	Yes	2.00
229	22.90	36.34	69.58	2.58	0.49	1.14	41.85	62.72	104.57	0.144	No	No	0.16
230	23.00	37.64	70.80	2.60	0.49	1.14	41.70	62.92	104.62	0.144	No	No	0.16
231	23.10	35.29	75.66	2.66	0.50	1.14	38.43	0.00	38.43	4.000	No	Yes	2.00
232	23.20	32.02	81.36	2.73	0.51	1.14	34.18	0.00	34.18	4.000	No	Yes	2.00
233	23.30	29.06	86.30	2.79	0.51	1.14	31.14	0.00	31.14	4.000	No	Yes	2.00
234	23.40	26.91	89.69	2.83	0.52	1.14	28.85	0.00	28.85	4.000	No	Yes	2.00
235	23.50	25.69	91.50	2.86	0.52	1.14	27.20	0.00	27.20	4.000	No	Yes	2.00
236	23.60	25.99	91.23	2.85	0.52	1.14	27.11	0.00	27.11	4.000	Yes	Yes	2.00
237	23.70	28.55	87.91	2.81	0.52	1.14	29.63	0.00	29.63	4.000	Yes	Yes	2.00
238	23.80	33.44	81.85	2.74	0.50	1.13	35.10	0.00	35.10	4.000	Yes	Yes	2.00
239	23.90	39.82	74.57	2.64	0.49	1.12	42.28	0.00	42.28	4.000	Yes	Yes	2.00
240	24.00	46.53	67.53	2.56	0.47	1.12	49.35	64.46	113.81	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
241	24.10	54.51	59.98	2.46	0.46	1.11	55.69	64.32	120.01	4.000	Yes	No	2.00
242	24.20	65.10	51.25	2.35	0.44	1.11	66.59	64.19	130.78	4.000	Yes	No	2.00
243	24.30	79.01	42.39	2.24	0.41	1.10	81.40	63.25	144.65	4.000	Yes	No	2.00
244	24.40	93.89	35.76	2.16	0.39	1.09	97.57	61.71	159.28	4.000	Yes	No	2.00
245	24.50	106.54	32.66	2.12	0.37	1.08	110.99	61.28	172.27	4.000	Yes	No	2.00
246	24.60	115.17	32.04	2.11	0.36	1.08	118.72	62.16	180.88	0.753	No	No	0.90
247	24.70	120.39	32.42	2.12	0.35	1.08	122.64	63.48	186.11	0.941	No	No	1.13
248	24.80	116.41	34.00	2.14	0.34	1.07	125.74	66.11	191.85	1.231	No	No	1.48
249	24.90	104.61	36.83	2.17	0.37	1.08	106.41	64.78	171.19	0.525	No	No	0.62
250	25.00	92.13	40.08	2.21	0.40	1.08	87.23	63.03	150.26	0.291	No	No	0.33
251	25.10	88.30	41.90	2.24	0.40	1.08	88.43	64.66	153.10	0.311	No	No	0.36
252	25.20	92.70	42.13	2.24	0.39	1.08	94.59	66.34	160.94	0.382	No	No	0.44
253	25.30	95.86	42.96	2.25	0.38	1.07	99.74	68.20	167.95	0.471	No	No	0.55
254	25.40	93.78	45.24	2.28	0.38	1.07	97.31	69.10	166.40	4.000	Yes	No	2.00
255	25.50	85.40	49.28	2.33	0.39	1.07	87.94	68.94	156.88	4.000	Yes	No	2.00
256	25.60	72.79	54.96	2.40	0.42	1.08	74.48	67.83	142.31	4.000	Yes	No	2.00
257	25.70	58.75	62.14	2.49	0.45	1.08	59.48	66.01	125.49	4.000	Yes	No	2.00
258	25.80	45.10	71.12	2.60	0.48	1.08	45.71	0.00	45.71	4.000	Yes	Yes	2.00
259	25.90	32.80	82.08	2.74	0.51	1.09	33.21	0.00	33.21	4.000	Yes	Yes	2.00
260	26.00	22.82	94.44	2.89	0.54	1.09	22.07	0.00	22.07	4.000	Yes	Yes	2.00
261	26.10	15.86	100.00	3.04	0.56	1.09	15.19	0.00	15.19	4.000	No	Yes	2.00
262	26.20	12.59	100.00	3.13	0.58	1.09	11.84	0.00	11.84	4.000	No	Yes	2.00
263	26.30	11.74	100.00	3.15	0.57	1.09	11.97	0.00	11.97	4.000	No	Yes	2.00
264	26.40	11.90	100.00	3.13	0.57	1.09	12.50	0.00	12.50	4.000	No	Yes	2.00
265	26.50	12.02	100.00	3.12	0.57	1.09	12.29	0.00	12.29	4.000	No	Yes	2.00
266	26.60	12.19	100.00	3.13	0.57	1.09	12.27	0.00	12.27	4.000	No	Yes	2.00
267	26.70	12.99	100.00	3.11	0.57	1.08	12.96	0.00	12.96	4.000	No	Yes	2.00
268	26.80	14.07	100.00	3.07	0.56	1.08	14.66	0.00	14.66	4.000	No	Yes	2.00
269	26.90	15.03	100.00	3.05	0.56	1.08	15.50	0.00	15.50	4.000	No	Yes	2.00
270	27.00	15.05	100.00	3.05	0.56	1.08	15.80	0.00	15.80	4.000	No	Yes	2.00
271	27.10	14.04	100.00	3.08	0.56	1.08	14.66	0.00	14.66	4.000	No	Yes	2.00
272	27.20	11.95	100.00	3.15	0.57	1.08	12.37	0.00	12.37	4.000	No	Yes	2.00
273	27.30	10.07	100.00	3.22	0.58	1.08	9.42	0.00	9.42	4.000	No	Yes	2.00
274	27.40	9.47	100.00	3.23	0.59	1.07	8.90	0.00	8.90	4.000	No	Yes	2.00
275	27.50	9.83	100.00	3.20	0.58	1.07	10.49	0.00	10.49	4.000	No	Yes	2.00
276	27.60	10.36	100.00	3.18	0.58	1.07	10.48	0.00	10.48	4.000	No	Yes	2.00
277	27.70	10.36	100.00	3.17	0.58	1.07	10.46	0.00	10.46	4.000	No	Yes	2.00
278	27.80	10.36	100.00	3.17	0.58	1.07	10.45	0.00	10.45	4.000	No	Yes	2.00
279	27.90	10.36	100.00	3.18	0.58	1.07	10.43	0.00	10.43	4.000	No	Yes	2.00
280	28.00	10.36	100.00	3.18	0.58	1.06	10.41	0.00	10.41	4.000	No	Yes	2.00
281	28.10	10.94	100.00	3.17	0.58	1.06	10.41	0.00	10.41	4.000	No	Yes	2.00
282	28.20	14.59	100.00	3.05	0.57	1.06	12.10	0.00	12.10	4.000	No	Yes	2.00
283	28.30	22.51	92.24	2.87	0.54	1.06	21.24	0.00	21.24	4.000	No	Yes	2.00
284	28.40	32.54	81.02	2.73	0.51	1.05	33.84	0.00	33.84	4.000	No	Yes	2.00
285	28.50	38.83	76.86	2.67	0.49	1.05	41.70	0.00	41.70	4.000	No	Yes	2.00
286	28.60	38.69	78.89	2.70	0.49	1.05	39.66	0.00	39.66	4.000	No	Yes	2.00
287	28.70	34.55	84.52	2.77	0.51	1.05	33.26	0.00	33.26	4.000	No	Yes	2.00
288	28.80	30.65	89.42	2.83	0.52	1.04	29.34	0.00	29.34	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
289	28.90	30.40	88.90	2.82	0.52	1.04	28.06	0.00	28.06	4.000	Yes	Yes	2.00
290	29.00	35.55	80.62	2.72	0.51	1.04	32.37	0.00	32.37	4.000	Yes	Yes	2.00
291	29.10	47.27	66.19	2.54	0.48	1.04	44.28	62.70	106.97	4.000	Yes	No	2.00
292	29.20	63.97	51.82	2.36	0.45	1.03	62.08	63.23	125.31	4.000	Yes	No	2.00
293	29.30	82.47	41.63	2.23	0.41	1.03	80.70	62.56	143.26	4.000	Yes	No	2.00
294	29.40	101.51	35.82	2.16	0.39	1.03	97.58	61.77	159.35	4.000	Yes	No	2.00
295	29.50	120.40	31.96	2.11	0.36	1.02	116.67	61.61	178.28	4.000	Yes	No	2.00
296	29.60	138.78	29.07	2.08	0.34	1.02	134.56	61.10	195.67	4.000	Yes	No	2.00
297	29.70	151.39	27.65	2.06	0.31	1.02	149.78	61.60	211.38	3.826	No	No	2.00
298	29.80	149.49	28.57	2.07	0.31	1.02	152.25	63.73	215.98	4.000	No	No	2.00
299	29.90	134.76	32.01	2.11	0.34	1.02	128.66	64.23	192.88	1.296	No	No	1.48
300	30.00	124.88	35.84	2.16	0.37	1.02	107.23	63.99	171.22	0.525	No	No	0.59
301	30.10	126.66	37.54	2.18	0.34	1.01	123.54	69.45	192.99	1.303	No	No	1.49
302	30.20	133.00	36.98	2.17	0.32	1.01	133.23	71.14	204.37	2.441	No	No	2.00
303	30.30	130.73	36.25	2.17	0.34	1.01	124.87	68.45	193.32	1.324	No	No	1.51
304	30.40	122.90	35.59	2.16	0.35	1.01	116.69	65.88	182.57	0.808	No	No	0.92
305	30.50	115.21	35.45	2.16	0.36	1.01	110.54	64.34	174.87	4.000	Yes	No	2.00
306	30.60	106.62	37.93	2.19	0.38	1.01	102.59	64.91	167.50	4.000	Yes	No	2.00
307	30.70	95.19	43.85	2.26	0.39	1.01	91.84	66.83	158.66	4.000	Yes	No	2.00
308	30.80	81.78	51.52	2.36	0.41	1.01	77.58	67.25	144.84	4.000	Yes	No	2.00
309	30.90	68.85	58.76	2.45	0.44	1.01	64.06	66.29	130.35	4.000	Yes	No	2.00
310	31.00	59.25	63.99	2.51	0.46	1.01	54.71	65.15	119.86	4.000	Yes	No	2.00
311	31.10	54.12	66.46	2.54	0.47	1.00	50.01	64.41	114.42	4.000	Yes	No	2.00
312	31.20	52.83	66.54	2.54	0.47	1.00	49.24	64.20	113.44	0.158	No	No	0.17
313	31.30	53.99	65.96	2.54	0.47	1.00	50.83	64.53	115.36	0.162	No	No	0.18
314	31.40	56.15	66.37	2.54	0.46	1.00	53.11	65.28	118.38	0.168	No	No	0.18
315	31.50	62.49	65.34	2.53	0.46	1.00	55.14	65.61	120.76	4.000	Yes	No	2.00
316	31.60	78.37	59.11	2.45	0.43	1.00	68.54	67.65	136.18	4.000	Yes	No	2.00
317	31.70	106.07	48.77	2.32	0.37	1.00	97.76	71.25	169.01	4.000	Yes	No	2.00
318	31.80	135.90	40.10	2.21	0.32	1.00	133.16	74.14	207.31	4.000	Yes	No	2.00
319	31.90	156.45	35.50	2.16	0.30	1.00	152.54	73.90	226.44	4.000	Yes	No	2.00
320	32.00	161.73	35.27	2.15	0.29	0.99	155.47	74.29	229.76	4.000	Yes	No	2.00
321	32.10	152.47	38.52	2.19	0.30	0.99	147.66	76.11	223.77	4.000	Yes	No	2.00
322	32.20	133.57	44.31	2.27	0.33	0.99	125.93	75.74	201.67	4.000	Yes	No	2.00
323	32.30	109.16	51.75	2.36	0.36	0.99	101.69	73.81	175.51	4.000	Yes	No	2.00
324	32.40	86.47	59.01	2.45	0.41	0.99	78.43	70.38	148.81	4.000	Yes	No	2.00
325	32.50	67.96	65.17	2.53	0.44	0.98	61.75	67.47	129.22	4.000	Yes	No	2.00
326	32.60	54.22	70.45	2.59	0.47	0.98	49.44	65.11	114.56	4.000	Yes	No	2.00
327	32.70	44.06	75.73	2.66	0.49	0.98	39.72	0.00	39.72	4.000	Yes	Yes	2.00
328	32.80	36.99	80.62	2.72	0.51	0.98	33.20	0.00	33.20	4.000	Yes	Yes	2.00
329	32.90	33.29	83.39	2.75	0.52	0.98	29.57	0.00	29.57	4.000	Yes	Yes	2.00
330	33.00	32.53	83.60	2.76	0.52	0.97	29.29	0.00	29.29	4.000	No	Yes	2.00
331	33.10	33.38	82.64	2.75	0.51	0.97	30.98	0.00	30.98	4.000	No	Yes	2.00
332	33.20	34.55	81.37	2.73	0.51	0.97	31.80	0.00	31.80	4.000	No	Yes	2.00
333	33.30	35.86	79.50	2.71	0.51	0.97	32.42	0.00	32.42	4.000	No	Yes	2.00
334	33.40	37.95	76.54	2.67	0.51	0.97	34.46	0.00	34.46	4.000	No	Yes	2.00
335	33.50	40.53	73.85	2.64	0.50	0.97	37.43	0.00	37.43	4.000	No	Yes	2.00
336	33.60	42.96	72.33	2.62	0.49	0.97	39.39	0.00	39.39	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
337	33.70	44.99	71.85	2.61	0.49	0.97	41.03	0.00	41.03	4.000	No	Yes	2.00
338	33.80	46.37	72.43	2.62	0.48	0.97	42.89	0.00	42.89	4.000	No	Yes	2.00
339	33.90	46.18	74.43	2.64	0.48	0.97	43.04	0.00	43.04	4.000	No	Yes	2.00
340	34.00	43.62	78.50	2.69	0.49	0.96	40.33	0.00	40.33	4.000	No	Yes	2.00
341	34.10	39.11	84.08	2.76	0.50	0.96	35.69	0.00	35.69	4.000	No	Yes	2.00
342	34.20	34.19	89.68	2.83	0.51	0.96	30.50	0.00	30.50	4.000	No	Yes	2.00
343	34.30	31.45	91.76	2.86	0.53	0.96	26.70	0.00	26.70	4.000	Yes	Yes	2.00
344	34.40	33.42	86.02	2.79	0.52	0.96	28.07	0.00	28.07	4.000	Yes	Yes	2.00
345	34.50	41.97	71.75	2.61	0.50	0.96	35.76	0.00	35.76	4.000	Yes	Yes	2.00
346	34.60	54.67	58.10	2.44	0.47	0.96	49.94	62.15	112.09	4.000	Yes	No	2.00
347	34.70	63.98	53.32	2.38	0.44	0.96	62.68	63.99	126.66	4.000	Yes	No	2.00
348	34.80	63.78	57.56	2.43	0.44	0.96	61.10	65.08	126.18	4.000	Yes	No	2.00
349	34.90	54.43	67.50	2.56	0.47	0.95	49.20	64.41	113.61	4.000	Yes	No	2.00
350	35.00	42.54	78.80	2.70	0.50	0.95	36.91	0.00	36.91	4.000	Yes	Yes	2.00
351	35.10	33.70	88.26	2.82	0.52	0.95	28.50	0.00	28.50	4.000	Yes	Yes	2.00
352	35.20	29.21	93.49	2.88	0.53	0.94	25.05	0.00	25.05	4.000	Yes	Yes	2.00
353	35.30	28.14	95.06	2.90	0.53	0.94	24.63	0.00	24.63	4.000	No	Yes	2.00
354	35.40	28.25	95.63	2.91	0.53	0.94	25.53	0.00	25.53	4.000	No	Yes	2.00
355	35.50	28.92	95.11	2.90	0.53	0.94	25.24	0.00	25.24	4.000	No	Yes	2.00
356	35.60	31.20	91.20	2.85	0.53	0.94	26.32	0.00	26.32	4.000	No	Yes	2.00
357	35.70	35.84	83.81	2.76	0.51	0.94	31.54	0.00	31.54	4.000	No	Yes	2.00
358	35.80	41.61	77.24	2.68	0.50	0.94	37.63	0.00	37.63	4.000	No	Yes	2.00
359	35.90	46.85	74.07	2.64	0.49	0.94	41.72	0.00	41.72	4.000	No	Yes	2.00
360	36.00	48.90	75.37	2.65	0.48	0.94	45.56	0.00	45.56	4.000	No	Yes	2.00
361	36.10	46.83	79.99	2.71	0.48	0.94	43.00	0.00	43.00	4.000	No	Yes	2.00
362	36.20	40.81	87.18	2.80	0.50	0.94	36.00	0.00	36.00	4.000	No	Yes	2.00
363	36.30	34.31	94.39	2.89	0.52	0.93	29.22	0.00	29.22	4.000	No	Yes	2.00
364	36.40	30.73	97.51	2.93	0.53	0.93	25.45	0.00	25.45	4.000	Yes	Yes	2.00
365	36.50	32.04	93.45	2.88	0.53	0.93	26.29	0.00	26.29	4.000	Yes	Yes	2.00
366	36.60	37.92	83.44	2.76	0.51	0.93	32.60	0.00	32.60	4.000	Yes	Yes	2.00
367	36.70	47.30	71.13	2.60	0.49	0.93	41.04	0.00	41.04	4.000	Yes	Yes	2.00
368	36.80	57.90	60.04	2.46	0.47	0.93	51.22	63.09	114.31	4.000	Yes	No	2.00
369	36.90	67.57	52.85	2.37	0.45	0.93	60.85	63.31	124.16	4.000	Yes	No	2.00
370	37.00	73.31	51.12	2.35	0.44	0.94	66.88	64.22	131.09	4.000	Yes	No	2.00
371	37.10	73.91	53.63	2.38	0.43	0.93	66.49	65.14	131.64	4.000	Yes	No	2.00
372	37.20	70.47	58.21	2.44	0.44	0.93	62.29	65.62	127.91	4.000	Yes	No	2.00
373	37.30	66.08	62.38	2.49	0.45	0.93	57.42	65.49	122.92	4.000	Yes	No	2.00
374	37.40	64.16	63.85	2.51	0.46	0.93	54.47	65.05	119.51	4.000	Yes	No	2.00
375	37.50	66.79	61.09	2.48	0.45	0.93	56.90	64.99	121.88	4.000	Yes	No	2.00
376	37.60	74.80	54.01	2.39	0.44	0.93	64.28	64.69	128.96	4.000	Yes	No	2.00
377	37.70	86.08	45.10	2.28	0.42	0.93	75.74	63.52	139.26	4.000	Yes	No	2.00
378	37.80	97.88	37.13	2.18	0.41	0.93	86.97	60.55	147.51	4.000	Yes	No	2.00
379	37.90	107.58	32.25	2.12	0.40	0.93	95.71	57.51	153.21	4.000	Yes	No	2.00
380	38.00	112.98	30.82	2.10	0.39	0.93	101.59	56.97	158.56	0.357	No	No	0.39
381	38.10	113.65	31.86	2.11	0.39	0.93	101.27	58.23	159.49	0.367	No	No	0.40
382	38.20	110.48	33.99	2.14	0.39	0.93	97.28	59.82	157.09	4.000	Yes	No	2.00
383	38.30	105.06	36.78	2.17	0.40	0.93	92.83	61.59	154.43	4.000	Yes	No	2.00
384	38.40	97.28	41.18	2.23	0.40	0.93	86.43	63.66	150.09	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
385	38.50	86.60	48.34	2.32	0.42	0.92	76.16	65.37	141.54	4.000	Yes	No	2.00
386	38.60	73.98	57.54	2.43	0.44	0.92	63.96	65.86	129.82	4.000	Yes	No	2.00
387	38.70	62.00	66.29	2.54	0.46	0.91	52.52	65.09	117.62	4.000	Yes	No	2.00
388	38.80	53.61	71.54	2.61	0.48	0.91	44.11	0.00	44.11	4.000	Yes	Yes	2.00
389	38.90	50.18	71.48	2.61	0.49	0.91	41.56	0.00	41.56	4.000	No	Yes	2.00
390	39.00	50.79	67.93	2.56	0.48	0.91	43.31	62.80	106.11	0.146	No	No	0.16
391	39.10	53.01	64.24	2.52	0.48	0.91	45.55	62.60	108.15	0.149	No	No	0.16
392	39.20	54.99	61.98	2.49	0.48	0.91	47.19	62.49	109.68	0.152	No	No	0.16
393	39.30	56.78	60.30	2.47	0.48	0.90	48.35	62.36	110.70	0.153	No	No	0.16
394	39.40	58.86	58.18	2.44	0.47	0.90	50.06	62.21	112.27	0.156	No	No	0.17
395	39.50	61.74	55.07	2.40	0.47	0.90	52.46	61.85	114.31	0.160	No	No	0.17
396	39.60	65.69	51.04	2.35	0.46	0.90	55.71	61.20	116.91	0.165	No	No	0.18
397	39.70	69.92	49.72	2.33	0.45	0.91	60.24	61.84	122.07	4.000	Yes	No	2.00
398	39.80	70.73	54.47	2.39	0.44	0.91	63.49	64.65	128.13	4.000	Yes	No	2.00
399	39.90	68.52	60.97	2.47	0.45	0.90	57.72	65.18	122.90	4.000	Yes	No	2.00
400	40.00	66.77	65.09	2.53	0.46	0.90	54.32	65.32	119.64	4.000	Yes	No	2.00
401	40.10	68.40	65.88	2.54	0.45	0.90	58.71	66.77	125.48	0.185	No	No	0.20
402	40.20	69.02	68.00	2.56	0.44	0.90	61.90	68.20	130.09	0.198	No	No	0.21
403	40.30	64.29	73.46	2.63	0.45	0.90	55.80	0.00	55.80	4.000	No	Yes	2.00
404	40.40	55.60	79.85	2.71	0.47	0.89	46.13	0.00	46.13	4.000	No	Yes	2.00
405	40.50	48.54	83.21	2.75	0.49	0.89	39.03	0.00	39.03	4.000	Yes	Yes	2.00
406	40.60	48.02	79.53	2.71	0.50	0.89	37.26	0.00	37.26	4.000	Yes	Yes	2.00
407	40.70	56.01	69.01	2.58	0.48	0.89	44.58	63.40	107.98	4.000	Yes	No	2.00
408	40.80	69.22	57.94	2.44	0.45	0.90	59.60	64.78	124.39	4.000	Yes	No	2.00
409	40.90	81.20	50.69	2.35	0.43	0.90	71.49	65.25	136.75	4.000	Yes	No	2.00
410	41.00	88.70	47.17	2.30	0.42	0.90	75.68	64.64	140.32	4.000	Yes	No	2.00
411	41.10	92.25	46.03	2.29	0.41	0.90	79.08	64.90	143.99	0.254	No	No	0.27
412	41.20	95.34	45.25	2.28	0.41	0.90	80.61	64.84	145.45	0.261	No	No	0.28
413	41.30	97.82	44.83	2.27	0.41	0.90	83.62	65.36	148.98	0.282	No	No	0.30
414	41.40	99.69	44.77	2.27	0.40	0.90	85.44	65.78	151.22	0.297	No	No	0.32
415	41.50	106.32	43.77	2.26	0.40	0.90	85.31	65.13	150.44	0.292	No	No	0.31
416	41.60	117.58	42.23	2.24	0.37	0.91	101.08	68.02	169.09	0.489	No	No	0.53
417	41.70	127.07	41.88	2.24	0.35	0.91	115.50	71.32	186.82	4.000	Yes	No	2.00
418	41.80	127.05	44.41	2.27	0.35	0.91	110.61	71.93	182.54	4.000	Yes	No	2.00
419	41.90	116.84	49.80	2.34	0.37	0.90	100.92	72.63	173.55	4.000	Yes	No	2.00
420	42.00	104.74	56.14	2.41	0.39	0.90	87.91	71.97	159.87	4.000	Yes	No	2.00
421	42.10	92.11	62.00	2.49	0.40	0.89	78.12	71.24	149.37	4.000	Yes	No	2.00
422	42.20	81.70	65.47	2.53	0.43	0.89	67.21	69.11	136.32	4.000	Yes	No	2.00
423	42.30	77.65	63.88	2.51	0.44	0.88	60.27	66.71	126.97	4.000	Yes	No	2.00
424	42.40	84.52	55.36	2.40	0.43	0.88	67.14	65.97	133.12	4.000	Yes	No	2.00
425	42.50	102.73	43.27	2.25	0.40	0.89	84.79	64.68	149.47	4.000	Yes	No	2.00
426	42.60	127.10	32.45	2.12	0.38	0.90	107.60	60.29	167.89	4.000	Yes	No	2.00
427	42.70	150.48	25.87	2.04	0.35	0.90	130.98	54.76	185.74	4.000	Yes	No	2.00
428	42.80	168.38	23.18	2.00	0.33	0.91	146.45	51.63	198.08	4.000	Yes	No	2.00
429	42.90	178.54	23.00	2.00	0.32	0.91	155.26	52.60	207.86	3.034	No	No	2.00
430	43.00	182.69	23.74	2.01	0.31	0.91	158.33	54.90	213.23	4.000	No	No	2.00
431	43.10	182.27	24.62	2.02	0.31	0.91	157.75	56.84	214.59	4.000	No	No	2.00
432	43.20	179.32	25.17	2.03	0.31	0.91	154.04	57.42	211.46	3.848	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
433	43.30	176.00	25.14	2.03	0.32	0.91	149.98	56.64	206.62	2.805	No	No	2.00
434	43.40	173.94	24.66	2.02	0.32	0.90	148.18	55.28	203.46	2.312	No	No	2.00
435	43.50	174.12	24.05	2.01	0.33	0.90	147.82	53.87	201.69	2.084	No	No	2.00
436	43.60	176.71	23.46	2.01	0.33	0.90	149.86	52.84	202.69	2.209	No	No	2.00
437	43.70	181.49	22.89	2.00	0.32	0.90	154.67	52.24	206.92	2.858	No	No	2.00
438	43.80	187.71	22.46	1.99	0.31	0.90	160.40	52.03	212.43	4.000	No	No	2.00
439	43.90	193.96	22.34	1.99	0.30	0.91	166.51	52.68	219.18	4.000	No	No	2.00
440	44.00	199.20	22.34	1.99	0.30	0.91	171.54	53.45	224.99	4.000	No	No	2.00
441	44.10	202.32	22.19	1.99	0.29	0.91	174.54	53.50	228.04	4.000	No	No	2.00
442	44.20	203.65	21.62	1.98	0.30	0.91	174.66	51.92	226.58	4.000	No	No	2.00
443	44.30	204.80	20.89	1.97	0.30	0.91	174.54	49.79	224.33	4.000	No	No	2.00
444	44.40	206.99	20.46	1.97	0.30	0.91	176.98	48.84	225.82	4.000	No	No	2.00
445	44.50	210.41	20.57	1.97	0.29	0.91	180.14	49.63	229.76	4.000	No	No	2.00
446	44.60	214.13	20.71	1.97	0.29	0.91	183.66	50.55	234.21	4.000	No	No	2.00
447	44.70	217.64	20.48	1.97	0.28	0.91	186.99	50.30	237.29	4.000	No	No	2.00
448	44.80	221.58	19.61	1.96	0.28	0.91	189.34	47.80	237.14	4.000	No	No	2.00
449	44.90	227.00	18.17	1.94	0.28	0.91	193.61	43.31	236.92	4.000	No	No	2.00
450	45.00	234.02	16.55	1.92	0.28	0.91	200.62	37.88	238.50	4.000	No	No	2.00
451	45.10	239.15	15.44	1.91	0.28	0.91	207.33	33.97	241.30	4.000	No	No	2.00
452	45.20	237.85	15.45	1.91	0.28	0.91	206.70	33.96	240.66	4.000	No	No	2.00
453	45.30	229.01	16.39	1.92	0.29	0.90	196.47	36.86	233.32	4.000	No	No	2.00
454	45.40	215.37	17.77	1.93	0.30	0.90	182.83	40.62	223.45	4.000	No	No	2.00
455	45.50	202.11	18.91	1.95	0.31	0.89	169.22	42.90	212.12	4.000	No	No	2.00
456	45.60	193.91	18.98	1.95	0.33	0.89	159.90	41.97	201.87	2.106	No	No	2.00
457	45.70	193.08	17.60	1.93	0.33	0.89	159.63	37.40	197.04	1.607	No	No	1.70
458	45.80	200.77	14.98	1.90	0.34	0.88	165.30	28.48	193.78	1.356	No	No	1.44
459	45.90	215.19	12.10	1.86	0.33	0.88	178.40	17.89	196.29	1.544	No	No	1.64
460	46.00	233.39	9.81	1.84	0.32	0.89	196.25	9.71	205.96	2.693	No	No	2.00
461	46.10	252.76	8.35	1.82	0.31	0.89	212.91	5.30	218.21	4.000	No	No	2.00
462	46.20	270.53	7.34	1.80	0.29	0.90	230.41	2.97	233.37	4.000	No	No	2.00
463	46.30	285.82	6.29	1.79	0.27	0.90	244.90	1.26	246.17	4.000	No	No	2.00
464	46.40	297.04	4.99	1.77	0.26	0.90	255.11	0.24	255.35	4.000	No	No	2.00
465	46.50	304.64	3.81	1.76	0.26	0.90	260.80	0.02	260.82	4.000	No	No	2.00
466	46.60	309.75	3.35	1.75	0.26	0.90	264.75	0.00	264.75	4.000	No	No	2.00
467	46.70	312.52	3.74	1.76	0.26	0.90	267.70	0.02	267.72	4.000	No	No	2.00
468	46.80	312.12	4.47	1.77	0.26	0.90	267.41	0.10	267.50	4.000	No	No	2.00
469	46.90	308.33	5.39	1.78	0.26	0.90	263.22	0.45	263.67	4.000	No	No	2.00
470	47.00	301.93	6.55	1.79	0.26	0.90	257.52	1.67	259.19	4.000	No	No	2.00
471	47.10	294.03	8.24	1.82	0.26	0.90	250.57	5.48	256.05	4.000	No	No	2.00
472	47.20	284.88	10.23	1.84	0.26	0.90	242.59	12.69	255.27	4.000	No	No	2.00
473	47.30	275.33	12.05	1.86	0.26	0.90	233.71	20.47	254.18	4.000	No	No	2.00
474	47.40	266.20	13.10	1.88	0.27	0.90	225.39	24.89	250.28	4.000	No	No	2.00
475	47.50	258.33	13.04	1.88	0.28	0.89	217.65	24.14	241.80	4.000	No	No	2.00
476	47.60	252.03	11.74	1.86	0.29	0.89	210.72	17.98	228.70	4.000	No	No	2.00
477	47.70	247.62	9.30	1.83	0.31	0.88	205.24	8.14	213.38	4.000	No	No	2.00
478	47.80	245.33	6.40	1.79	0.33	0.87	202.14	1.26	203.40	2.304	No	No	2.00
479	47.90	241.79	5.68	1.78	0.33	0.87	201.79	0.57	202.36	4.000	Yes	No	2.00
480	48.00	231.80	9.94	1.84	0.32	0.87	195.19	10.15	205.34	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
481	48.10	209.20	19.24	1.95	0.30	0.88	178.95	45.21	224.16	4.000	Yes	No	2.00
482	48.20	174.47	31.70	2.11	0.31	0.88	146.41	67.56	213.97	4.000	Yes	No	2.00
483	48.30	133.42	45.42	2.28	0.36	0.86	107.22	71.74	178.96	4.000	Yes	No	2.00
484	48.40	94.91	58.95	2.45	0.42	0.84	72.32	68.65	140.97	4.000	Yes	No	2.00
485	48.50	71.47	68.31	2.57	0.47	0.82	47.18	64.00	111.18	4.000	Yes	No	2.00
486	48.60	60.38	72.87	2.62	0.47	0.82	47.68	0.00	47.68	4.000	Yes	Yes	2.00
487	48.70	52.78	76.64	2.67	0.48	0.81	44.75	0.00	44.75	4.000	Yes	Yes	2.00
488	48.80	47.63	79.22	2.70	0.52	0.80	28.89	0.00	28.89	4.000	Yes	Yes	2.00
489	48.90	49.25	74.77	2.65	0.50	0.80	35.15	0.00	35.15	4.000	Yes	Yes	2.00
490	49.00	65.35	61.38	2.48	0.47	0.81	48.43	62.68	111.11	4.000	Yes	No	2.00
491	49.10	87.91	48.06	2.31	0.44	0.83	67.57	62.99	130.56	4.000	Yes	No	2.00
492	49.20	112.10	38.36	2.19	0.40	0.84	90.36	62.41	152.77	4.000	Yes	No	2.00
493	49.30	133.65	32.83	2.12	0.37	0.85	108.69	60.99	169.68	4.000	Yes	No	2.00
494	49.40	151.11	29.87	2.09	0.35	0.85	122.10	59.84	181.94	4.000	Yes	No	2.00
495	49.50	166.58	26.22	2.04	0.34	0.86	134.99	56.15	191.14	4.000	Yes	No	2.00
496	49.60	185.29	20.72	1.97	0.34	0.86	147.74	45.49	193.22	4.000	Yes	No	2.00
497	49.70	208.76	14.22	1.89	0.34	0.86	168.32	25.78	194.11	4.000	Yes	No	2.00
498	49.80	231.42	9.08	1.83	0.33	0.86	192.74	7.17	199.91	4.000	Yes	No	2.00
499	49.90	245.61	6.25	1.79	0.32	0.86	203.93	1.09	205.02	4.000	Yes	No	2.00

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q_t :	Total cone resistance
FC:	Fines content (%)
I_c :	Soil behavior type index
m:	Stress exponent
C_N :	Overburden correction factor
q_{c1N} :	Normalized and adjusted cone resistance
Δq_{c1N} :	Cone resistance correction factor due to fines
$q_{c1N,cs}$:	Normalized and adjusted cone resistance
CRR _{7.5} :	Cyclic resistance ratio for $M_w=7.5$
FS:	Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
0.10	2.00	0.00	0.00	0.10	0.00	0.20	2.00	0.00	0.00	0.10	0.00
0.30	2.00	0.00	0.00	0.10	0.00	0.40	2.00	0.00	0.00	0.10	0.00
0.50	2.00	0.00	0.00	0.10	0.00	0.60	2.00	0.00	0.00	0.10	0.00
0.70	2.00	0.00	0.00	0.10	0.00	0.80	2.00	0.00	0.00	0.10	0.00
0.90	2.00	0.00	0.00	0.10	0.00	1.00	2.00	0.00	0.00	0.10	0.00
1.10	2.00	0.00	0.00	0.10	0.00	1.20	2.00	0.00	0.00	0.10	0.00
1.30	2.00	0.00	0.00	0.10	0.00	1.40	2.00	0.00	0.00	0.10	0.00
1.50	2.00	0.00	0.00	0.10	0.00	1.60	2.00	0.00	0.00	0.10	0.00
1.70	2.00	0.00	0.00	0.10	0.00	1.80	2.00	0.00	0.00	0.10	0.00
1.90	2.00	0.00	0.00	0.10	0.00	2.00	2.00	0.00	0.00	0.10	0.00
2.10	2.00	0.00	0.00	0.10	0.00	2.20	2.00	0.00	0.00	0.10	0.00
2.30	2.00	0.00	0.00	0.10	0.00	2.40	2.00	0.00	0.00	0.10	0.00
2.50	2.00	0.00	0.00	0.10	0.00	2.60	2.00	0.00	0.00	0.10	0.00
2.70	2.00	0.00	0.00	0.10	0.00	2.80	2.00	0.00	0.00	0.10	0.00
2.90	2.00	0.00	0.00	0.10	0.00	3.00	2.00	0.00	0.00	0.10	0.00
3.10	2.00	0.00	0.00	0.10	0.00	3.20	2.00	0.00	0.00	0.10	0.00
3.30	2.00	0.00	0.00	0.10	0.00	3.40	2.00	0.00	0.00	0.10	0.00
3.50	2.00	0.00	0.00	0.10	0.00	3.60	2.00	0.00	0.00	0.10	0.00
3.70	2.00	0.00	0.00	0.10	0.00	3.80	2.00	0.00	0.00	0.10	0.00
3.90	2.00	0.00	0.00	0.10	0.00	4.00	2.00	0.00	0.00	0.10	0.00
4.10	2.00	0.00	0.00	0.10	0.00	4.20	2.00	0.00	0.00	0.10	0.00
4.30	2.00	0.00	0.00	0.10	0.00	4.40	2.00	0.00	0.00	0.10	0.00
4.50	2.00	0.00	0.00	0.10	0.00	4.60	2.00	0.00	0.00	0.10	0.00
4.70	2.00	0.00	0.00	0.10	0.00	4.80	2.00	0.00	0.00	0.10	0.00
4.90	2.00	0.00	0.00	0.10	0.00	5.00	2.00	0.00	0.00	0.10	0.00
5.10	2.00	0.00	0.00	0.10	0.00	5.20	2.00	0.00	0.00	0.10	0.00
5.30	2.00	0.00	0.00	0.10	0.00	5.40	2.00	0.00	0.00	0.10	0.00
5.50	2.00	0.00	0.00	0.10	0.00	5.60	2.00	0.00	0.00	0.10	0.00
5.70	2.00	0.00	0.00	0.10	0.00	5.80	2.00	0.00	0.00	0.10	0.00
5.90	2.00	0.00	0.00	0.10	0.00	6.00	2.00	0.00	0.00	0.10	0.00
6.10	2.00	0.00	0.00	0.10	0.00	6.20	2.00	0.00	0.00	0.10	0.00
6.30	2.00	0.00	0.00	0.10	0.00	6.40	2.00	0.00	0.00	0.10	0.00
6.50	2.00	0.00	0.00	0.10	0.00	6.60	2.00	0.00	0.00	0.10	0.00
6.70	2.00	0.00	0.00	0.10	0.00	6.80	2.00	0.00	0.00	0.10	0.00
6.90	2.00	0.00	0.00	0.10	0.00	7.00	2.00	0.00	0.00	0.10	0.00
7.10	2.00	0.00	0.00	0.10	0.00	7.20	2.00	0.00	0.00	0.10	0.00
7.30	2.00	0.00	0.00	0.10	0.00	7.40	2.00	0.00	0.00	0.10	0.00
7.50	2.00	0.00	0.00	0.10	0.00	7.60	2.00	0.00	0.00	0.10	0.00
7.70	2.00	0.00	0.00	0.10	0.00	7.80	2.00	0.00	0.00	0.10	0.00
7.90	2.00	0.00	0.00	0.10	0.00	8.00	2.00	0.00	0.00	0.10	0.00
8.10	2.00	0.00	0.00	0.10	0.00	8.20	2.00	0.00	0.00	0.10	0.00
8.30	2.00	0.00	0.00	0.10	0.00	8.40	2.00	0.00	0.00	0.10	0.00
8.50	2.00	0.00	0.00	0.10	0.00	8.60	2.00	0.00	0.00	0.10	0.00
8.70	0.21	0.79	0.28	0.10	0.21	8.80	0.21	0.79	0.28	0.10	0.21
8.90	2.00	0.00	0.00	0.10	0.00	9.00	2.00	0.00	0.00	0.10	0.00
9.10	2.00	0.00	0.00	0.10	0.00	9.20	2.00	0.00	0.00	0.10	0.00
9.30	2.00	0.00	0.00	0.10	0.00	9.40	0.20	0.80	0.28	0.10	0.21
9.50	2.00	0.00	0.00	0.10	0.00	9.60	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
9.70	2.00	0.00	0.00	0.10	0.00	9.80	2.00	0.00	0.00	0.10	0.00
9.90	2.00	0.00	0.00	0.10	0.00	10.00	2.00	0.00	0.00	0.10	0.00
10.10	2.00	0.00	0.00	0.10	0.00	10.20	2.00	0.00	0.00	0.10	0.00
10.30	2.00	0.00	0.00	0.10	0.00	10.40	2.00	0.00	0.00	0.10	0.00
10.50	2.00	0.00	0.00	0.10	0.00	10.60	2.00	0.00	0.00	0.10	0.00
10.70	2.00	0.00	0.00	0.10	0.00	10.80	2.00	0.00	0.00	0.10	0.00
10.90	2.00	0.00	0.00	0.10	0.00	11.00	2.00	0.00	0.00	0.10	0.00
11.10	2.00	0.00	0.00	0.10	0.00	11.20	2.00	0.00	0.00	0.10	0.00
11.30	2.00	0.00	0.00	0.10	0.00	11.40	2.00	0.00	0.00	0.10	0.00
11.50	2.00	0.00	0.00	0.10	0.00	11.60	2.00	0.00	0.00	0.10	0.00
11.70	2.00	0.00	0.00	0.10	0.00	11.80	2.00	0.00	0.00	0.10	0.00
11.90	2.00	0.00	0.00	0.10	0.00	12.00	2.00	0.00	0.00	0.10	0.00
12.10	2.00	0.00	0.00	0.10	0.00	12.20	2.00	0.00	0.00	0.10	0.00
12.30	2.00	0.00	0.00	0.10	0.00	12.40	2.00	0.00	0.00	0.10	0.00
12.50	2.00	0.00	0.00	0.10	0.00	12.60	2.00	0.00	0.00	0.10	0.00
12.70	2.00	0.00	0.00	0.10	0.00	12.80	2.00	0.00	0.00	0.10	0.00
12.90	2.00	0.00	0.00	0.10	0.00	13.00	2.00	0.00	0.00	0.10	0.00
13.10	2.00	0.00	0.00	0.10	0.00	13.20	2.00	0.00	0.00	0.10	0.00
13.30	2.00	0.00	0.00	0.10	0.00	13.40	2.00	0.00	0.00	0.10	0.00
13.50	2.00	0.00	0.00	0.10	0.00	13.60	2.00	0.00	0.00	0.10	0.00
13.70	2.00	0.00	0.00	0.10	0.00	13.80	2.00	0.00	0.00	0.10	0.00
13.90	2.00	0.00	0.00	0.10	0.00	14.00	2.00	0.00	0.00	0.10	0.00
14.10	2.00	0.00	0.00	0.10	0.00	14.20	2.00	0.00	0.00	0.10	0.00
14.30	2.00	0.00	0.00	0.10	0.00	14.40	2.00	0.00	0.00	0.10	0.00
14.50	2.00	0.00	0.00	0.10	0.00	14.60	2.00	0.00	0.00	0.10	0.00
14.70	2.00	0.00	0.00	0.10	0.00	14.80	2.00	0.00	0.00	0.10	0.00
14.90	2.00	0.00	0.00	0.10	0.00	15.00	2.00	0.00	0.00	0.10	0.00
15.10	2.00	0.00	0.00	0.10	0.00	15.20	2.00	0.00	0.00	0.10	0.00
15.30	2.00	0.00	0.00	0.10	0.00	15.40	2.00	0.00	0.00	0.10	0.00
15.50	2.00	0.00	0.00	0.10	0.00	15.60	2.00	0.00	0.00	0.10	0.00
15.70	2.00	0.00	0.00	0.10	0.00	15.80	2.00	0.00	0.00	0.10	0.00
15.90	2.00	0.00	0.00	0.10	0.00	16.00	2.00	0.00	0.00	0.10	0.00
16.10	0.48	0.52	0.45	0.10	0.12	16.20	0.42	0.58	0.40	0.10	0.13
16.30	0.60	0.40	0.64	0.10	0.09	16.40	2.00	0.00	0.00	0.10	0.00
16.50	2.00	0.00	0.00	0.10	0.00	16.60	2.00	0.00	0.00	0.10	0.00
16.70	2.00	0.00	0.00	0.10	0.00	16.80	2.00	0.00	0.00	0.10	0.00
16.90	2.00	0.00	0.00	0.10	0.00	17.00	2.00	0.00	0.00	0.10	0.00
17.10	2.00	0.00	0.00	0.10	0.00	17.20	2.00	0.00	0.00	0.10	0.00
17.30	2.00	0.00	0.00	0.10	0.00	17.40	2.00	0.00	0.00	0.10	0.00
17.50	2.00	0.00	0.00	0.10	0.00	17.60	2.00	0.00	0.00	0.10	0.00
17.70	2.00	0.00	0.00	0.10	0.00	17.80	2.00	0.00	0.00	0.10	0.00
17.90	2.00	0.00	0.00	0.10	0.00	18.00	2.00	0.00	0.00	0.10	0.00
18.10	2.00	0.00	0.00	0.10	0.00	18.20	2.00	0.00	0.00	0.10	0.00
18.30	2.00	0.00	0.00	0.10	0.00	18.40	2.00	0.00	0.00	0.10	0.00
18.50	2.00	0.00	0.00	0.10	0.00	18.60	2.00	0.00	0.00	0.10	0.00
18.70	2.00	0.00	0.00	0.10	0.00	18.80	2.00	0.00	0.00	0.10	0.00
18.90	2.00	0.00	0.00	0.10	0.00	19.00	2.00	0.00	0.00	0.10	0.00
19.10	2.00	0.00	0.00	0.10	0.00	19.20	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
19.30	2.00	0.00	0.00	0.10	0.00	19.40	2.00	0.00	0.00	0.10	0.00
19.50	2.00	0.00	0.00	0.10	0.00	19.60	2.00	0.00	0.00	0.10	0.00
19.70	2.00	0.00	0.00	0.10	0.00	19.80	2.00	0.00	0.00	0.10	0.00
19.90	2.00	0.00	0.00	0.10	0.00	20.00	2.00	0.00	0.00	0.10	0.00
20.10	2.00	0.00	0.00	0.10	0.00	20.20	2.00	0.00	0.00	0.10	0.00
20.30	2.00	0.00	0.00	0.10	0.00	20.40	2.00	0.00	0.00	0.10	0.00
20.50	2.00	0.00	0.00	0.10	0.00	20.60	2.00	0.00	0.00	0.10	0.00
20.70	2.00	0.00	0.00	0.10	0.00	20.80	2.00	0.00	0.00	0.10	0.00
20.90	2.00	0.00	0.00	0.10	0.00	21.00	2.00	0.00	0.00	0.10	0.00
21.10	2.00	0.00	0.00	0.10	0.00	21.20	2.00	0.00	0.00	0.10	0.00
21.30	2.00	0.00	0.00	0.10	0.00	21.40	2.00	0.00	0.00	0.10	0.00
21.50	2.00	0.00	0.00	0.10	0.00	21.60	2.00	0.00	0.00	0.10	0.00
21.70	2.00	0.00	0.00	0.10	0.00	21.80	2.00	0.00	0.00	0.10	0.00
21.90	2.00	0.00	0.00	0.10	0.00	22.00	2.00	0.00	0.00	0.10	0.00
22.10	2.00	0.00	0.00	0.10	0.00	22.20	2.00	0.00	0.00	0.10	0.00
22.30	2.00	0.00	0.00	0.10	0.00	22.40	2.00	0.00	0.00	0.10	0.00
22.50	2.00	0.00	0.00	0.10	0.00	22.60	2.00	0.00	0.00	0.10	0.00
22.70	2.00	0.00	0.00	0.10	0.00	22.80	2.00	0.00	0.00	0.10	0.00
22.90	0.16	0.84	0.26	0.10	0.17	23.00	0.16	0.84	0.26	0.10	0.17
23.10	2.00	0.00	0.00	0.10	0.00	23.20	2.00	0.00	0.00	0.10	0.00
23.30	2.00	0.00	0.00	0.10	0.00	23.40	2.00	0.00	0.00	0.10	0.00
23.50	2.00	0.00	0.00	0.10	0.00	23.60	2.00	0.00	0.00	0.10	0.00
23.70	2.00	0.00	0.00	0.10	0.00	23.80	2.00	0.00	0.00	0.10	0.00
23.90	2.00	0.00	0.00	0.10	0.00	24.00	2.00	0.00	0.00	0.10	0.00
24.10	2.00	0.00	0.00	0.10	0.00	24.20	2.00	0.00	0.00	0.10	0.00
24.30	2.00	0.00	0.00	0.10	0.00	24.40	2.00	0.00	0.00	0.10	0.00
24.50	2.00	0.00	0.00	0.10	0.00	24.60	0.90	0.10	6.15	0.10	0.02
24.70	1.13	0.00	0.00	0.10	0.00	24.80	1.48	0.00	0.00	0.10	0.00
24.90	0.62	0.38	0.67	0.10	0.07	25.00	0.33	0.67	0.34	0.10	0.13
25.10	0.36	0.64	0.36	0.10	0.12	25.20	0.44	0.56	0.42	0.10	0.10
25.30	0.55	0.45	0.55	0.10	0.08	25.40	2.00	0.00	0.00	0.10	0.00
25.50	2.00	0.00	0.00	0.10	0.00	25.60	2.00	0.00	0.00	0.10	0.00
25.70	2.00	0.00	0.00	0.10	0.00	25.80	2.00	0.00	0.00	0.10	0.00
25.90	2.00	0.00	0.00	0.10	0.00	26.00	2.00	0.00	0.00	0.10	0.00
26.10	2.00	0.00	0.00	0.10	0.00	26.20	2.00	0.00	0.00	0.10	0.00
26.30	2.00	0.00	0.00	0.10	0.00	26.40	2.00	0.00	0.00	0.10	0.00
26.50	2.00	0.00	0.00	0.10	0.00	26.60	2.00	0.00	0.00	0.10	0.00
26.70	2.00	0.00	0.00	0.10	0.00	26.80	2.00	0.00	0.00	0.10	0.00
26.90	2.00	0.00	0.00	0.10	0.00	27.00	2.00	0.00	0.00	0.10	0.00
27.10	2.00	0.00	0.00	0.10	0.00	27.20	2.00	0.00	0.00	0.10	0.00
27.30	2.00	0.00	0.00	0.10	0.00	27.40	2.00	0.00	0.00	0.10	0.00
27.50	2.00	0.00	0.00	0.10	0.00	27.60	2.00	0.00	0.00	0.10	0.00
27.70	2.00	0.00	0.00	0.10	0.00	27.80	2.00	0.00	0.00	0.10	0.00
27.90	2.00	0.00	0.00	0.10	0.00	28.00	2.00	0.00	0.00	0.10	0.00
28.10	2.00	0.00	0.00	0.10	0.00	28.20	2.00	0.00	0.00	0.10	0.00
28.30	2.00	0.00	0.00	0.10	0.00	28.40	2.00	0.00	0.00	0.10	0.00
28.50	2.00	0.00	0.00	0.10	0.00	28.60	2.00	0.00	0.00	0.10	0.00
28.70	2.00	0.00	0.00	0.10	0.00	28.80	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
28.90	2.00	0.00	0.00	0.10	0.00	29.00	2.00	0.00	0.00	0.10	0.00
29.10	2.00	0.00	0.00	0.10	0.00	29.20	2.00	0.00	0.00	0.10	0.00
29.30	2.00	0.00	0.00	0.10	0.00	29.40	2.00	0.00	0.00	0.10	0.00
29.50	2.00	0.00	0.00	0.10	0.00	29.60	2.00	0.00	0.00	0.10	0.00
29.70	2.00	0.00	0.00	0.10	0.00	29.80	2.00	0.00	0.00	0.10	0.00
29.90	1.48	0.00	0.00	0.10	0.00	30.00	0.59	0.41	0.61	0.10	0.07
30.10	1.49	0.00	0.00	0.10	0.00	30.20	2.00	0.00	0.00	0.10	0.00
30.30	1.51	0.00	0.00	0.10	0.00	30.40	0.92	0.08	9.12	0.10	0.01
30.50	2.00	0.00	0.00	0.10	0.00	30.60	2.00	0.00	0.00	0.10	0.00
30.70	2.00	0.00	0.00	0.10	0.00	30.80	2.00	0.00	0.00	0.10	0.00
30.90	2.00	0.00	0.00	0.10	0.00	31.00	2.00	0.00	0.00	0.10	0.00
31.10	2.00	0.00	0.00	0.10	0.00	31.20	0.17	0.83	0.27	0.10	0.13
31.30	0.18	0.82	0.27	0.10	0.13	31.40	0.18	0.82	0.27	0.10	0.13
31.50	2.00	0.00	0.00	0.10	0.00	31.60	2.00	0.00	0.00	0.10	0.00
31.70	2.00	0.00	0.00	0.10	0.00	31.80	2.00	0.00	0.00	0.10	0.00
31.90	2.00	0.00	0.00	0.10	0.00	32.00	2.00	0.00	0.00	0.10	0.00
32.10	2.00	0.00	0.00	0.10	0.00	32.20	2.00	0.00	0.00	0.10	0.00
32.30	2.00	0.00	0.00	0.10	0.00	32.40	2.00	0.00	0.00	0.10	0.00
32.50	2.00	0.00	0.00	0.10	0.00	32.60	2.00	0.00	0.00	0.10	0.00
32.70	2.00	0.00	0.00	0.10	0.00	32.80	2.00	0.00	0.00	0.10	0.00
32.90	2.00	0.00	0.00	0.10	0.00	33.00	2.00	0.00	0.00	0.10	0.00
33.10	2.00	0.00	0.00	0.10	0.00	33.20	2.00	0.00	0.00	0.10	0.00
33.30	2.00	0.00	0.00	0.10	0.00	33.40	2.00	0.00	0.00	0.10	0.00
33.50	2.00	0.00	0.00	0.10	0.00	33.60	2.00	0.00	0.00	0.10	0.00
33.70	2.00	0.00	0.00	0.10	0.00	33.80	2.00	0.00	0.00	0.10	0.00
33.90	2.00	0.00	0.00	0.10	0.00	34.00	2.00	0.00	0.00	0.10	0.00
34.10	2.00	0.00	0.00	0.10	0.00	34.20	2.00	0.00	0.00	0.10	0.00
34.30	2.00	0.00	0.00	0.10	0.00	34.40	2.00	0.00	0.00	0.10	0.00
34.50	2.00	0.00	0.00	0.10	0.00	34.60	2.00	0.00	0.00	0.10	0.00
34.70	2.00	0.00	0.00	0.10	0.00	34.80	2.00	0.00	0.00	0.10	0.00
34.90	2.00	0.00	0.00	0.10	0.00	35.00	2.00	0.00	0.00	0.10	0.00
35.10	2.00	0.00	0.00	0.10	0.00	35.20	2.00	0.00	0.00	0.10	0.00
35.30	2.00	0.00	0.00	0.10	0.00	35.40	2.00	0.00	0.00	0.10	0.00
35.50	2.00	0.00	0.00	0.10	0.00	35.60	2.00	0.00	0.00	0.10	0.00
35.70	2.00	0.00	0.00	0.10	0.00	35.80	2.00	0.00	0.00	0.10	0.00
35.90	2.00	0.00	0.00	0.10	0.00	36.00	2.00	0.00	0.00	0.10	0.00
36.10	2.00	0.00	0.00	0.10	0.00	36.20	2.00	0.00	0.00	0.10	0.00
36.30	2.00	0.00	0.00	0.10	0.00	36.40	2.00	0.00	0.00	0.10	0.00
36.50	2.00	0.00	0.00	0.10	0.00	36.60	2.00	0.00	0.00	0.10	0.00
36.70	2.00	0.00	0.00	0.10	0.00	36.80	2.00	0.00	0.00	0.10	0.00
36.90	2.00	0.00	0.00	0.10	0.00	37.00	2.00	0.00	0.00	0.10	0.00
37.10	2.00	0.00	0.00	0.10	0.00	37.20	2.00	0.00	0.00	0.10	0.00
37.30	2.00	0.00	0.00	0.10	0.00	37.40	2.00	0.00	0.00	0.10	0.00
37.50	2.00	0.00	0.00	0.10	0.00	37.60	2.00	0.00	0.00	0.10	0.00
37.70	2.00	0.00	0.00	0.10	0.00	37.80	2.00	0.00	0.00	0.10	0.00
37.90	2.00	0.00	0.00	0.10	0.00	38.00	0.39	0.61	0.37	0.10	0.08
38.10	0.40	0.60	0.38	0.10	0.08	38.20	2.00	0.00	0.00	0.10	0.00
38.30	2.00	0.00	0.00	0.10	0.00	38.40	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
38.50	2.00	0.00	0.00	0.10	0.00	38.60	2.00	0.00	0.00	0.10	0.00
38.70	2.00	0.00	0.00	0.10	0.00	38.80	2.00	0.00	0.00	0.10	0.00
38.90	2.00	0.00	0.00	0.10	0.00	39.00	0.16	0.84	0.26	0.10	0.10
39.10	0.16	0.84	0.26	0.10	0.10	39.20	0.16	0.84	0.26	0.10	0.10
39.30	0.16	0.84	0.26	0.10	0.10	39.40	0.17	0.83	0.26	0.10	0.10
39.50	0.17	0.83	0.27	0.10	0.10	39.60	0.18	0.82	0.27	0.10	0.10
39.70	2.00	0.00	0.00	0.10	0.00	39.80	2.00	0.00	0.00	0.10	0.00
39.90	2.00	0.00	0.00	0.10	0.00	40.00	2.00	0.00	0.00	0.10	0.00
40.10	0.20	0.80	0.28	0.10	0.10	40.20	0.21	0.79	0.28	0.10	0.09
40.30	2.00	0.00	0.00	0.10	0.00	40.40	2.00	0.00	0.00	0.10	0.00
40.50	2.00	0.00	0.00	0.10	0.00	40.60	2.00	0.00	0.00	0.10	0.00
40.70	2.00	0.00	0.00	0.10	0.00	40.80	2.00	0.00	0.00	0.10	0.00
40.90	2.00	0.00	0.00	0.10	0.00	41.00	2.00	0.00	0.00	0.10	0.00
41.10	0.27	0.73	0.31	0.10	0.08	41.20	0.28	0.72	0.31	0.10	0.08
41.30	0.30	0.70	0.32	0.10	0.08	41.40	0.32	0.68	0.33	0.10	0.08
41.50	0.31	0.69	0.33	0.10	0.08	41.60	0.53	0.47	0.51	0.10	0.05
41.70	2.00	0.00	0.00	0.10	0.00	41.80	2.00	0.00	0.00	0.10	0.00
41.90	2.00	0.00	0.00	0.10	0.00	42.00	2.00	0.00	0.00	0.10	0.00
42.10	2.00	0.00	0.00	0.10	0.00	42.20	2.00	0.00	0.00	0.10	0.00
42.30	2.00	0.00	0.00	0.10	0.00	42.40	2.00	0.00	0.00	0.10	0.00
42.50	2.00	0.00	0.00	0.10	0.00	42.60	2.00	0.00	0.00	0.10	0.00
42.70	2.00	0.00	0.00	0.10	0.00	42.80	2.00	0.00	0.00	0.10	0.00
42.90	2.00	0.00	0.00	0.10	0.00	43.00	2.00	0.00	0.00	0.10	0.00
43.10	2.00	0.00	0.00	0.10	0.00	43.20	2.00	0.00	0.00	0.10	0.00
43.30	2.00	0.00	0.00	0.10	0.00	43.40	2.00	0.00	0.00	0.10	0.00
43.50	2.00	0.00	0.00	0.10	0.00	43.60	2.00	0.00	0.00	0.10	0.00
43.70	2.00	0.00	0.00	0.10	0.00	43.80	2.00	0.00	0.00	0.10	0.00
43.90	2.00	0.00	0.00	0.10	0.00	44.00	2.00	0.00	0.00	0.10	0.00
44.10	2.00	0.00	0.00	0.10	0.00	44.20	2.00	0.00	0.00	0.10	0.00
44.30	2.00	0.00	0.00	0.10	0.00	44.40	2.00	0.00	0.00	0.10	0.00
44.50	2.00	0.00	0.00	0.10	0.00	44.60	2.00	0.00	0.00	0.10	0.00
44.70	2.00	0.00	0.00	0.10	0.00	44.80	2.00	0.00	0.00	0.10	0.00
44.90	2.00	0.00	0.00	0.10	0.00	45.00	2.00	0.00	0.00	0.10	0.00
45.10	2.00	0.00	0.00	0.10	0.00	45.20	2.00	0.00	0.00	0.10	0.00
45.30	2.00	0.00	0.00	0.10	0.00	45.40	2.00	0.00	0.00	0.10	0.00
45.50	2.00	0.00	0.00	0.10	0.00	45.60	2.00	0.00	0.00	0.10	0.00
45.70	1.70	0.00	0.00	0.10	0.00	45.80	1.44	0.00	0.00	0.10	0.00
45.90	1.64	0.00	0.00	0.10	0.00	46.00	2.00	0.00	0.00	0.10	0.00
46.10	2.00	0.00	0.00	0.10	0.00	46.20	2.00	0.00	0.00	0.10	0.00
46.30	2.00	0.00	0.00	0.10	0.00	46.40	2.00	0.00	0.00	0.10	0.00
46.50	2.00	0.00	0.00	0.10	0.00	46.60	2.00	0.00	0.00	0.10	0.00
46.70	2.00	0.00	0.00	0.10	0.00	46.80	2.00	0.00	0.00	0.10	0.00
46.90	2.00	0.00	0.00	0.10	0.00	47.00	2.00	0.00	0.00	0.10	0.00
47.10	2.00	0.00	0.00	0.10	0.00	47.20	2.00	0.00	0.00	0.10	0.00
47.30	2.00	0.00	0.00	0.10	0.00	47.40	2.00	0.00	0.00	0.10	0.00
47.50	2.00	0.00	0.00	0.10	0.00	47.60	2.00	0.00	0.00	0.10	0.00
47.70	2.00	0.00	0.00	0.10	0.00	47.80	2.00	0.00	0.00	0.10	0.00
47.90	2.00	0.00	0.00	0.10	0.00	48.00	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
48.10	2.00	0.00	0.00	0.10	0.00	48.20	2.00	0.00	0.00	0.10	0.00
48.30	2.00	0.00	0.00	0.10	0.00	48.40	2.00	0.00	0.00	0.10	0.00
48.50	2.00	0.00	0.00	0.10	0.00	48.60	2.00	0.00	0.00	0.10	0.00
48.70	2.00	0.00	0.00	0.10	0.00	48.80	2.00	0.00	0.00	0.10	0.00
48.90	2.00	0.00	0.00	0.10	0.00	49.00	2.00	0.00	0.00	0.10	0.00
49.10	2.00	0.00	0.00	0.10	0.00	49.20	2.00	0.00	0.00	0.10	0.00
49.30	2.00	0.00	0.00	0.10	0.00	49.40	2.00	0.00	0.00	0.10	0.00
49.50	2.00	0.00	0.00	0.10	0.00	49.60	2.00	0.00	0.00	0.10	0.00
49.70	2.00	0.00	0.00	0.10	0.00	49.80	2.00	0.00	0.00	0.10	0.00
49.90	2.00	0.00	0.00	0.10	0.00						

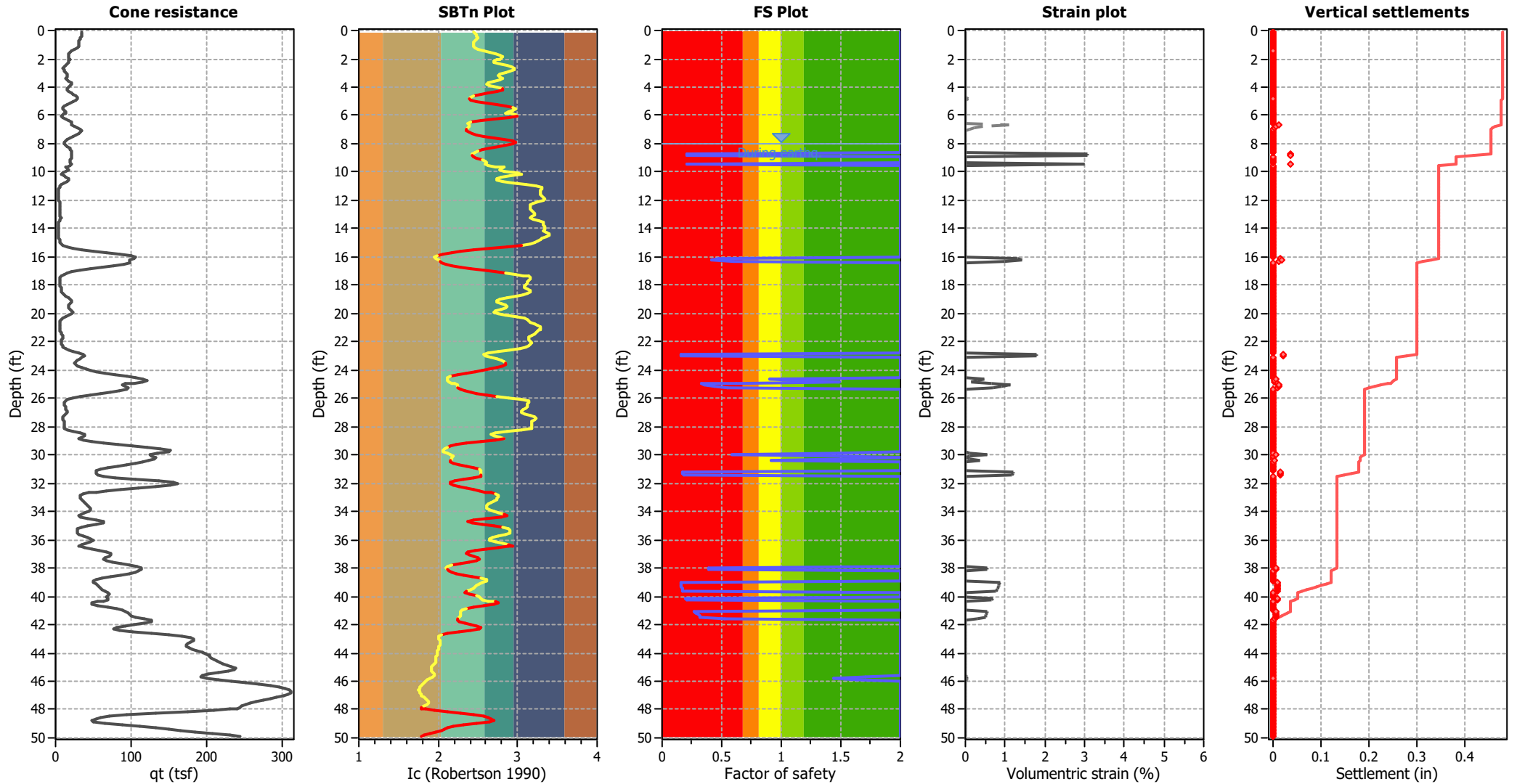
Overall liquefaction potential: 3.81

LPI_{ISH} > 5.0 - Liquefaction manifestation is expected

Abbreviations

FS: Calculated factor of safety for test point
d_z: Layer thickness (ft)
LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

- q_c : Total cone resistance (cone resistance q_c corrected for pore water effects)
- I_c : Soil Behaviour Type Index
- FS: Calculated Factor of Safety against liquefaction
- Volumetric strain: Post-liquefaction volumetric strain

:: Post-earthquake settlement of dry sands ::												
Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
0.10	2.45	56.27	2.63	148.20	37	698	0.56	0.000	0.00	13.69	0.00	0.000
0.20	2.45	56.47	2.68	151.58	38	708	0.56	0.001	0.00	13.69	0.00	0.000
0.30	2.47	55.78	2.80	155.97	40	715	0.56	0.001	0.00	13.69	0.00	0.000
0.40	2.49	54.02	2.91	157.43	40	709	0.56	0.002	0.00	13.69	0.00	0.000
0.50	2.49	52.12	2.94	152.98	39	687	0.56	0.003	0.00	13.69	0.00	0.000
0.60	2.48	50.86	2.84	144.21	37	657	0.56	0.003	0.00	13.69	0.00	0.000
0.70	2.46	50.10	2.71	135.86	34	632	0.56	0.004	0.00	13.69	0.00	0.000
0.80	2.45	49.84	2.63	131.07	33	618	0.56	0.005	0.00	13.69	0.00	0.000
0.90	2.44	49.83	2.60	129.39	32	613	0.56	0.006	0.00	13.69	0.00	0.000
1.00	2.44	49.69	2.59	128.54	32	610	0.56	0.007	0.00	13.69	0.00	0.000
1.10	2.44	48.45	2.61	126.56	32	598	0.56	0.008	0.00	13.69	0.00	0.000
1.20	2.46	45.87	2.70	123.81	31	577	0.56	0.010	0.01	13.69	0.01	0.000
1.30	2.50	40.51	2.99	121.17	31	539	0.56	0.013	0.01	13.69	0.01	0.000
1.40	2.58	34.34	3.55	121.97	33	502	0.56	0.016	0.01	13.69	0.01	0.000
1.50	2.65	31.60	4.19	132.32	0	0	0.56	0.000	0.00	0.00	0.00	0.000
1.60	2.73	28.39	4.99	141.68	0	0	0.56	0.000	0.00	0.00	0.00	0.000
1.70	2.78	27.60	5.57	153.72	0	0	0.56	0.000	0.00	0.00	0.00	0.000
1.80	2.82	27.16	6.05	164.19	0	0	0.56	0.000	0.00	0.00	0.00	0.000
1.90	2.80	28.64	5.84	167.32	0	0	0.56	0.000	0.00	0.00	0.00	0.000
2.00	2.77	29.06	5.50	159.89	0	0	0.56	0.000	0.00	0.00	0.00	0.000
2.10	2.73	28.31	5.05	142.99	0	0	0.56	0.000	0.00	0.00	0.00	0.000
2.20	2.70	28.40	4.68	132.96	0	0	0.56	0.000	0.00	0.00	0.00	0.000
2.30	2.70	27.57	4.75	131.09	0	0	0.56	0.000	0.00	0.00	0.00	0.000
2.40	2.77	24.12	5.50	132.52	0	0	0.56	0.000	0.00	0.00	0.00	0.000
2.50	2.86	20.13	6.60	132.83	0	0	0.56	0.000	0.00	0.00	0.00	0.000
2.60	2.93	17.16	7.62	130.66	0	0	0.56	0.000	0.00	0.00	0.00	0.000
2.70	2.96	16.12	8.06	129.90	0	0	0.56	0.000	0.00	0.00	0.00	0.000
2.80	2.95	16.30	7.98	130.11	0	0	0.56	0.000	0.00	0.00	0.00	0.000
2.90	2.91	18.07	7.32	132.27	0	0	0.56	0.000	0.00	0.00	0.00	0.000
3.00	2.84	20.88	6.37	133.02	0	0	0.56	0.000	0.00	0.00	0.00	0.000
3.10	2.78	23.78	5.58	132.77	0	0	0.56	0.000	0.00	0.00	0.00	0.000
3.20	2.76	24.59	5.33	131.09	0	0	0.56	0.000	0.00	0.00	0.00	0.000
3.30	2.78	23.19	5.60	129.91	0	0	0.56	0.000	0.00	0.00	0.00	0.000
3.40	2.81	22.15	5.93	131.32	0	0	0.56	0.000	0.00	0.00	0.00	0.000
3.50	2.78	23.79	5.60	133.20	0	0	0.56	0.000	0.00	0.00	0.00	0.000
3.60	2.70	27.75	4.75	131.84	0	0	0.56	0.000	0.00	0.00	0.00	0.000
3.70	2.63	31.81	4.00	127.33	0	0	0.56	0.000	0.00	0.00	0.00	0.000
3.80	2.60	33.08	3.78	125.01	0	0	0.56	0.000	0.00	0.00	0.00	0.000
3.90	2.64	30.77	4.13	127.20	0	0	0.56	0.000	0.00	0.00	0.00	0.000
4.00	2.73	26.51	5.05	133.91	0	0	0.56	0.000	0.00	0.00	0.00	0.000
4.10	2.81	23.54	5.97	140.56	0	0	0.56	0.000	0.00	0.00	0.00	0.000
4.20	2.81	23.89	6.00	143.43	0	0	0.56	0.000	0.00	0.00	0.00	0.000
4.30	2.74	27.11	5.14	139.41	0	0	0.56	0.000	0.00	0.00	0.00	0.000
4.40	2.63	31.99	4.05	129.66	0	0	0.56	0.000	0.00	0.00	0.00	0.000
4.50	2.53	37.12	3.22	119.41	0	0	0.56	0.000	0.00	13.69	0.00	0.000
4.60	2.45	41.92	2.68	112.35	0	0	0.56	0.000	0.00	13.69	0.00	0.000
4.70	2.40	45.01	2.39	107.51	0	0	0.56	0.000	0.00	13.69	0.00	0.000
4.80	2.38	45.35	2.29	103.81	25	520	0.56	0.138	0.10	13.69	0.09	0.001

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
4.90	2.41	42.56	2.42	102.96	0	0	0.56	0.000	0.00	13.69	0.00	0.000
5.00	2.48	37.04	2.87	106.48	0	0	0.56	0.000	0.00	13.69	0.00	0.000
5.10	2.60	29.57	3.78	111.85	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.20	2.74	22.63	5.11	115.62	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.30	2.85	17.72	6.53	115.77	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.40	2.93	14.82	7.70	114.05	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.50	2.98	13.46	8.49	114.28	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.60	2.94	16.29	7.78	126.71	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.70	2.89	19.38	7.05	136.70	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.80	2.86	21.51	6.59	141.77	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.90	2.92	17.70	7.45	131.79	0	0	0.56	0.000	0.00	0.00	0.00	0.000
6.00	2.98	14.16	8.39	118.81	0	0	0.56	0.000	0.00	0.00	0.00	0.000
6.10	3.00	11.99	8.80	105.61	0	0	0.56	0.000	0.00	0.00	0.00	0.000
6.20	2.88	14.39	6.98	100.50	0	0	0.56	0.000	0.00	0.00	0.00	0.000
6.30	2.70	20.34	4.69	95.45	0	0	0.56	0.000	0.00	0.00	0.00	0.000
6.40	2.53	27.09	3.21	86.98	0	0	0.56	0.000	0.00	13.69	0.00	0.000
6.50	2.41	31.49	2.45	77.10	0	0	0.56	0.000	0.00	13.69	0.00	0.000
6.60	2.37	33.16	2.24	74.34	0	0	0.56	0.000	0.00	13.69	0.00	0.000
6.70	2.40	34.00	2.35	79.96	20	396	0.56	1.283	1.31	13.69	1.11	0.013
6.80	2.40	38.80	2.36	91.49	22	452	0.56	0.612	0.53	13.69	0.45	0.005
6.90	2.37	45.87	2.22	101.77	25	516	0.55	0.323	0.25	13.69	0.21	0.003
7.00	2.35	52.41	2.12	110.85	27	573	0.55	0.209	0.15	13.69	0.12	0.001
7.10	2.36	54.59	2.18	118.90	0	0	0.55	0.000	0.00	13.69	0.00	0.000
7.20	2.39	52.87	2.33	122.98	0	0	0.55	0.000	0.00	13.69	0.00	0.000
7.30	2.43	49.08	2.51	123.40	0	0	0.55	0.000	0.00	13.69	0.00	0.000
7.40	2.49	43.25	2.88	124.48	0	0	0.55	0.000	0.00	13.69	0.00	0.000
7.50	2.58	36.51	3.57	130.52	0	0	0.56	0.000	0.00	13.69	0.00	0.000
7.60	2.70	29.58	4.74	140.29	0	0	0.56	0.000	0.00	0.00	0.00	0.000
7.70	2.83	23.41	6.26	146.59	0	0	0.56	0.000	0.00	0.00	0.00	0.000
7.80	2.94	19.05	7.76	147.86	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.90	2.97	17.54	8.34	146.36	0	0	0.57	0.000	0.00	0.00	0.00	0.000

Total estimated settlement: 0.02**Abbreviations**

Q_{tn}: Normalized cone resistance
 K_c: Fines correction factor
 Q_{tn,cs}: Equivalent clean sand normalized cone resistance
 G_{max}: Small strain shear modulus
 CSR: Soil cyclic stress ratio
 γ: Cyclic shear strain
 e_{vol(15)}: Volumetric strain after 15 cycles
 N_c: Equivalent number of cycles
 e_v: Volumetric strain
 Settle.: Calculated settlement

:: Post-earthquake settlement due to soil liquefaction ::

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
8.00	17.85	2.00	0.00	0.85	0.00	8.10	20.55	2.00	0.00	0.85	0.00
8.20	22.71	2.00	0.00	0.85	0.00	8.30	26.81	2.00	0.00	0.85	0.00
8.40	88.62	2.00	0.00	0.85	0.00	8.50	87.93	2.00	0.00	0.85	0.00
8.60	88.17	2.00	0.00	0.84	0.00	8.70	87.73	0.21	3.08	0.84	0.04

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
8.80	87.44	0.21	3.09	0.84	0.04	8.90	87.73	2.00	0.00	0.84	0.00
9.00	88.59	2.00	0.00	0.84	0.00	9.10	86.45	2.00	0.00	0.83	0.00
9.20	83.91	2.00	0.00	0.83	0.00	9.30	28.09	2.00	0.00	0.83	0.00
9.40	88.94	0.20	3.00	0.83	0.04	9.50	28.80	2.00	0.00	0.83	0.00
9.60	23.21	2.00	0.00	0.83	0.00	9.70	16.30	2.00	0.00	0.82	0.00
9.80	19.75	2.00	0.00	0.82	0.00	9.90	30.17	2.00	0.00	0.82	0.00
10.00	19.06	2.00	0.00	0.82	0.00	10.10	7.09	2.00	0.00	0.82	0.00
10.20	10.05	2.00	0.00	0.81	0.00	10.30	14.84	2.00	0.00	0.81	0.00
10.40	19.95	2.00	0.00	0.81	0.00	10.50	23.24	2.00	0.00	0.81	0.00
10.60	24.69	2.00	0.00	0.81	0.00	10.70	21.77	2.00	0.00	0.81	0.00
10.80	15.15	2.00	0.00	0.80	0.00	10.90	10.51	2.00	0.00	0.80	0.00
11.00	7.70	2.00	0.00	0.80	0.00	11.10	5.96	2.00	0.00	0.80	0.00
11.20	5.68	2.00	0.00	0.80	0.00	11.30	5.66	2.00	0.00	0.79	0.00
11.40	5.65	2.00	0.00	0.79	0.00	11.50	5.64	2.00	0.00	0.79	0.00
11.60	5.63	2.00	0.00	0.79	0.00	11.70	5.62	2.00	0.00	0.79	0.00
11.80	5.61	2.00	0.00	0.79	0.00	11.90	5.33	2.00	0.00	0.78	0.00
12.00	5.12	2.00	0.00	0.78	0.00	12.10	6.67	2.00	0.00	0.78	0.00
12.20	7.74	2.00	0.00	0.78	0.00	12.30	7.72	2.00	0.00	0.78	0.00
12.40	7.71	2.00	0.00	0.77	0.00	12.50	7.69	2.00	0.00	0.77	0.00
12.60	7.68	2.00	0.00	0.77	0.00	12.70	7.66	2.00	0.00	0.77	0.00
12.80	7.64	2.00	0.00	0.77	0.00	12.90	7.63	2.00	0.00	0.77	0.00
13.00	7.61	2.00	0.00	0.76	0.00	13.10	8.47	2.00	0.00	0.76	0.00
13.20	9.65	2.00	0.00	0.76	0.00	13.30	8.34	2.00	0.00	0.76	0.00
13.40	6.15	2.00	0.00	0.76	0.00	13.50	5.41	2.00	0.00	0.75	0.00
13.60	5.40	2.00	0.00	0.75	0.00	13.70	5.39	2.00	0.00	0.75	0.00
13.80	5.38	2.00	0.00	0.75	0.00	13.90	5.37	2.00	0.00	0.75	0.00
14.00	5.36	2.00	0.00	0.75	0.00	14.10	5.35	2.00	0.00	0.74	0.00
14.20	5.34	2.00	0.00	0.74	0.00	14.30	5.33	2.00	0.00	0.74	0.00
14.40	4.44	2.00	0.00	0.74	0.00	14.50	4.26	2.00	0.00	0.74	0.00
14.60	5.30	2.00	0.00	0.73	0.00	14.70	5.29	2.00	0.00	0.73	0.00
14.80	5.70	2.00	0.00	0.73	0.00	14.90	6.92	2.00	0.00	0.73	0.00
15.00	8.11	2.00	0.00	0.73	0.00	15.10	9.27	2.00	0.00	0.73	0.00
15.20	10.50	2.00	0.00	0.72	0.00	15.30	17.04	2.00	0.00	0.72	0.00
15.40	27.05	2.00	0.00	0.72	0.00	15.50	101.89	2.00	0.00	0.72	0.00
15.60	118.22	2.00	0.00	0.72	0.00	15.70	138.59	2.00	0.00	0.71	0.00
15.80	153.23	2.00	0.00	0.71	0.00	15.90	159.32	2.00	0.00	0.71	0.00
16.00	167.62	2.00	0.00	0.71	0.00	16.10	158.10	0.48	1.30	0.71	0.02
16.20	152.95	0.42	1.43	0.71	0.02	16.30	165.90	0.60	0.99	0.70	0.01
16.40	168.78	2.00	0.00	0.70	0.00	16.50	160.73	2.00	0.00	0.70	0.00
16.60	149.09	2.00	0.00	0.70	0.00	16.70	135.04	2.00	0.00	0.70	0.00
16.80	115.90	2.00	0.00	0.69	0.00	16.90	97.33	2.00	0.00	0.69	0.00
17.00	25.15	2.00	0.00	0.69	0.00	17.10	17.39	2.00	0.00	0.69	0.00
17.20	12.78	2.00	0.00	0.69	0.00	17.30	9.39	2.00	0.00	0.69	0.00
17.40	7.43	2.00	0.00	0.68	0.00	17.50	6.87	2.00	0.00	0.68	0.00
17.60	6.86	2.00	0.00	0.68	0.00	17.70	6.85	2.00	0.00	0.68	0.00
17.80	6.84	2.00	0.00	0.68	0.00	17.90	6.83	2.00	0.00	0.67	0.00
18.00	6.82	2.00	0.00	0.67	0.00	18.10	7.32	2.00	0.00	0.67	0.00
18.20	8.43	2.00	0.00	0.67	0.00	18.30	8.69	2.00	0.00	0.67	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
18.40	8.68	2.00	0.00	0.67	0.00	18.50	9.83	2.00	0.00	0.66	0.00
18.60	10.87	2.00	0.00	0.66	0.00	18.70	12.45	2.00	0.00	0.66	0.00
18.80	15.11	2.00	0.00	0.66	0.00	18.90	18.54	2.00	0.00	0.66	0.00
19.00	23.23	2.00	0.00	0.65	0.00	19.10	24.42	2.00	0.00	0.65	0.00
19.20	24.13	2.00	0.00	0.65	0.00	19.30	23.24	2.00	0.00	0.65	0.00
19.40	20.47	2.00	0.00	0.65	0.00	19.50	18.11	2.00	0.00	0.65	0.00
19.60	18.44	2.00	0.00	0.64	0.00	19.70	20.35	2.00	0.00	0.64	0.00
19.80	24.73	2.00	0.00	0.64	0.00	19.90	27.39	2.00	0.00	0.64	0.00
20.00	26.18	2.00	0.00	0.64	0.00	20.10	20.65	2.00	0.00	0.63	0.00
20.20	13.39	2.00	0.00	0.63	0.00	20.30	9.39	2.00	0.00	0.63	0.00
20.40	8.26	2.00	0.00	0.63	0.00	20.50	7.20	2.00	0.00	0.63	0.00
20.60	6.47	2.00	0.00	0.63	0.00	20.70	6.46	2.00	0.00	0.62	0.00
20.80	6.45	2.00	0.00	0.62	0.00	20.90	6.34	2.00	0.00	0.62	0.00
21.00	6.32	2.00	0.00	0.62	0.00	21.10	6.36	2.00	0.00	0.62	0.00
21.20	6.23	2.00	0.00	0.61	0.00	21.30	7.51	2.00	0.00	0.61	0.00
21.40	8.20	2.00	0.00	0.61	0.00	21.50	8.93	2.00	0.00	0.61	0.00
21.60	9.93	2.00	0.00	0.61	0.00	21.70	9.94	2.00	0.00	0.61	0.00
21.80	9.93	2.00	0.00	0.60	0.00	21.90	9.56	2.00	0.00	0.60	0.00
22.00	8.49	2.00	0.00	0.60	0.00	22.10	8.10	2.00	0.00	0.60	0.00
22.20	8.89	2.00	0.00	0.60	0.00	22.30	9.87	2.00	0.00	0.59	0.00
22.40	10.85	2.00	0.00	0.59	0.00	22.50	12.55	2.00	0.00	0.59	0.00
22.60	17.87	2.00	0.00	0.59	0.00	22.70	25.39	2.00	0.00	0.59	0.00
22.80	34.54	2.00	0.00	0.59	0.00	22.90	104.57	0.16	1.79	0.58	0.02
23.00	104.62	0.16	1.78	0.58	0.02	23.10	38.43	2.00	0.00	0.58	0.00
23.20	34.18	2.00	0.00	0.58	0.00	23.30	31.14	2.00	0.00	0.58	0.00
23.40	28.85	2.00	0.00	0.57	0.00	23.50	27.20	2.00	0.00	0.57	0.00
23.60	27.11	2.00	0.00	0.57	0.00	23.70	29.63	2.00	0.00	0.57	0.00
23.80	35.10	2.00	0.00	0.57	0.00	23.90	42.28	2.00	0.00	0.57	0.00
24.00	113.81	2.00	0.00	0.56	0.00	24.10	120.01	2.00	0.00	0.56	0.00
24.20	130.78	2.00	0.00	0.56	0.00	24.30	144.65	2.00	0.00	0.56	0.00
24.40	159.28	2.00	0.00	0.56	0.00	24.50	172.27	2.00	0.00	0.55	0.00
24.60	180.88	0.90	0.46	0.55	0.01	24.70	186.11	1.13	0.31	0.55	0.00
24.80	191.85	1.48	0.14	0.55	0.00	24.90	171.19	0.62	0.64	0.55	0.01
25.00	150.26	0.33	1.13	0.55	0.01	25.10	153.10	0.36	1.10	0.54	0.01
25.20	160.94	0.44	0.91	0.54	0.01	25.30	167.95	0.55	0.71	0.54	0.01
25.40	166.40	2.00	0.00	0.54	0.00	25.50	156.88	2.00	0.00	0.54	0.00
25.60	142.31	2.00	0.00	0.53	0.00	25.70	125.49	2.00	0.00	0.53	0.00
25.80	45.71	2.00	0.00	0.53	0.00	25.90	33.21	2.00	0.00	0.53	0.00
26.00	22.07	2.00	0.00	0.53	0.00	26.10	15.19	2.00	0.00	0.53	0.00
26.20	11.84	2.00	0.00	0.52	0.00	26.30	11.97	2.00	0.00	0.52	0.00
26.40	12.50	2.00	0.00	0.52	0.00	26.50	12.29	2.00	0.00	0.52	0.00
26.60	12.27	2.00	0.00	0.52	0.00	26.70	12.96	2.00	0.00	0.51	0.00
26.80	14.66	2.00	0.00	0.51	0.00	26.90	15.50	2.00	0.00	0.51	0.00
27.00	15.80	2.00	0.00	0.51	0.00	27.10	14.66	2.00	0.00	0.51	0.00
27.20	12.37	2.00	0.00	0.51	0.00	27.30	9.42	2.00	0.00	0.50	0.00
27.40	8.90	2.00	0.00	0.50	0.00	27.50	10.49	2.00	0.00	0.50	0.00
27.60	10.48	2.00	0.00	0.50	0.00	27.70	10.46	2.00	0.00	0.50	0.00
27.80	10.45	2.00	0.00	0.49	0.00	27.90	10.43	2.00	0.00	0.49	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
28.00	10.41	2.00	0.00	0.49	0.00	28.10	10.41	2.00	0.00	0.49	0.00
28.20	12.10	2.00	0.00	0.49	0.00	28.30	21.24	2.00	0.00	0.49	0.00
28.40	33.84	2.00	0.00	0.48	0.00	28.50	41.70	2.00	0.00	0.48	0.00
28.60	39.66	2.00	0.00	0.48	0.00	28.70	33.26	2.00	0.00	0.48	0.00
28.80	29.34	2.00	0.00	0.48	0.00	28.90	28.06	2.00	0.00	0.47	0.00
29.00	32.37	2.00	0.00	0.47	0.00	29.10	106.97	2.00	0.00	0.47	0.00
29.20	125.31	2.00	0.00	0.47	0.00	29.30	143.26	2.00	0.00	0.47	0.00
29.40	159.35	2.00	0.00	0.47	0.00	29.50	178.28	2.00	0.00	0.46	0.00
29.60	195.67	2.00	0.00	0.46	0.00	29.70	211.38	2.00	0.00	0.46	0.00
29.80	215.98	2.00	0.00	0.46	0.00	29.90	192.88	1.48	0.12	0.46	0.00
30.00	171.22	0.59	0.53	0.45	0.01	30.10	192.99	1.49	0.12	0.45	0.00
30.20	204.37	2.00	0.00	0.45	0.00	30.30	193.32	1.51	0.11	0.45	0.00
30.40	182.57	0.92	0.35	0.45	0.00	30.50	174.87	2.00	0.00	0.45	0.00
30.60	167.50	2.00	0.00	0.44	0.00	30.70	158.66	2.00	0.00	0.44	0.00
30.80	144.84	2.00	0.00	0.44	0.00	30.90	130.35	2.00	0.00	0.44	0.00
31.00	119.86	2.00	0.00	0.44	0.00	31.10	114.42	2.00	0.00	0.43	0.00
31.20	113.44	0.17	1.22	0.43	0.01	31.30	115.36	0.18	1.19	0.43	0.01
31.40	118.38	0.18	1.16	0.43	0.01	31.50	120.76	2.00	0.00	0.43	0.00
31.60	136.18	2.00	0.00	0.43	0.00	31.70	169.01	2.00	0.00	0.42	0.00
31.80	207.31	2.00	0.00	0.42	0.00	31.90	226.44	2.00	0.00	0.42	0.00
32.00	229.76	2.00	0.00	0.42	0.00	32.10	223.77	2.00	0.00	0.42	0.00
32.20	201.67	2.00	0.00	0.41	0.00	32.30	175.51	2.00	0.00	0.41	0.00
32.40	148.81	2.00	0.00	0.41	0.00	32.50	129.22	2.00	0.00	0.41	0.00
32.60	114.56	2.00	0.00	0.41	0.00	32.70	39.72	2.00	0.00	0.41	0.00
32.80	33.20	2.00	0.00	0.40	0.00	32.90	29.57	2.00	0.00	0.40	0.00
33.00	29.29	2.00	0.00	0.40	0.00	33.10	30.98	2.00	0.00	0.40	0.00
33.20	31.80	2.00	0.00	0.40	0.00	33.30	32.42	2.00	0.00	0.39	0.00
33.40	34.46	2.00	0.00	0.39	0.00	33.50	37.43	2.00	0.00	0.39	0.00
33.60	39.39	2.00	0.00	0.39	0.00	33.70	41.03	2.00	0.00	0.39	0.00
33.80	42.89	2.00	0.00	0.39	0.00	33.90	43.04	2.00	0.00	0.38	0.00
34.00	40.33	2.00	0.00	0.38	0.00	34.10	35.69	2.00	0.00	0.38	0.00
34.20	30.50	2.00	0.00	0.38	0.00	34.30	26.70	2.00	0.00	0.38	0.00
34.40	28.07	2.00	0.00	0.37	0.00	34.50	35.76	2.00	0.00	0.37	0.00
34.60	112.09	2.00	0.00	0.37	0.00	34.70	126.66	2.00	0.00	0.37	0.00
34.80	126.18	2.00	0.00	0.37	0.00	34.90	113.61	2.00	0.00	0.37	0.00
35.00	36.91	2.00	0.00	0.36	0.00	35.10	28.50	2.00	0.00	0.36	0.00
35.20	25.05	2.00	0.00	0.36	0.00	35.30	24.63	2.00	0.00	0.36	0.00
35.40	25.53	2.00	0.00	0.36	0.00	35.50	25.24	2.00	0.00	0.35	0.00
35.60	26.32	2.00	0.00	0.35	0.00	35.70	31.54	2.00	0.00	0.35	0.00
35.80	37.63	2.00	0.00	0.35	0.00	35.90	41.72	2.00	0.00	0.35	0.00
36.00	45.56	2.00	0.00	0.35	0.00	36.10	43.00	2.00	0.00	0.34	0.00
36.20	36.00	2.00	0.00	0.34	0.00	36.30	29.22	2.00	0.00	0.34	0.00
36.40	25.45	2.00	0.00	0.34	0.00	36.50	26.29	2.00	0.00	0.34	0.00
36.60	32.60	2.00	0.00	0.33	0.00	36.70	41.04	2.00	0.00	0.33	0.00
36.80	114.31	2.00	0.00	0.33	0.00	36.90	124.16	2.00	0.00	0.33	0.00
37.00	131.09	2.00	0.00	0.33	0.00	37.10	131.64	2.00	0.00	0.33	0.00
37.20	127.91	2.00	0.00	0.32	0.00	37.30	122.92	2.00	0.00	0.32	0.00
37.40	119.51	2.00	0.00	0.32	0.00	37.50	121.88	2.00	0.00	0.32	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
37.60	128.96	2.00	0.00	0.32	0.00	37.70	139.26	2.00	0.00	0.31	0.00
37.80	147.51	2.00	0.00	0.31	0.00	37.90	153.21	2.00	0.00	0.31	0.00
38.00	158.56	0.39	0.56	0.31	0.01	38.10	159.49	0.40	0.54	0.31	0.01
38.20	157.09	2.00	0.00	0.31	0.00	38.30	154.43	2.00	0.00	0.30	0.00
38.40	150.09	2.00	0.00	0.30	0.00	38.50	141.54	2.00	0.00	0.30	0.00
38.60	129.82	2.00	0.00	0.30	0.00	38.70	117.62	2.00	0.00	0.30	0.00
38.80	44.11	2.00	0.00	0.29	0.00	38.90	41.56	2.00	0.00	0.29	0.00
39.00	106.11	0.16	0.88	0.29	0.01	39.10	108.15	0.16	0.86	0.29	0.01
39.20	109.68	0.16	0.84	0.29	0.01	39.30	110.70	0.16	0.83	0.29	0.01
39.40	112.27	0.17	0.81	0.28	0.01	39.50	114.31	0.17	0.79	0.28	0.01
39.60	116.91	0.18	0.76	0.28	0.01	39.70	122.07	2.00	0.00	0.28	0.00
39.80	128.13	2.00	0.00	0.28	0.00	39.90	122.90	2.00	0.00	0.27	0.00
40.00	119.64	2.00	0.00	0.27	0.00	40.10	125.48	0.20	0.69	0.27	0.01
40.20	130.09	0.21	0.65	0.27	0.01	40.30	55.80	2.00	0.00	0.27	0.00
40.40	46.13	2.00	0.00	0.27	0.00	40.50	39.03	2.00	0.00	0.26	0.00
40.60	37.26	2.00	0.00	0.26	0.00	40.70	107.98	2.00	0.00	0.26	0.00
40.80	124.39	2.00	0.00	0.26	0.00	40.90	136.75	2.00	0.00	0.26	0.00
41.00	140.32	2.00	0.00	0.25	0.00	41.10	143.99	0.27	0.55	0.25	0.01
41.20	145.45	0.28	0.54	0.25	0.01	41.30	148.98	0.30	0.52	0.25	0.01
41.40	151.22	0.32	0.51	0.25	0.01	41.50	150.44	0.31	0.51	0.25	0.01
41.60	169.09	0.53	0.31	0.24	0.00	41.70	186.82	2.00	0.00	0.24	0.00
41.80	182.54	2.00	0.00	0.24	0.00	41.90	173.55	2.00	0.00	0.24	0.00
42.00	159.87	2.00	0.00	0.24	0.00	42.10	149.37	2.00	0.00	0.23	0.00
42.20	136.32	2.00	0.00	0.23	0.00	42.30	126.97	2.00	0.00	0.23	0.00
42.40	133.12	2.00	0.00	0.23	0.00	42.50	149.47	2.00	0.00	0.23	0.00
42.60	167.89	2.00	0.00	0.23	0.00	42.70	185.74	2.00	0.00	0.22	0.00
42.80	198.08	2.00	0.00	0.22	0.00	42.90	207.86	2.00	0.00	0.22	0.00
43.00	213.23	2.00	0.00	0.22	0.00	43.10	214.59	2.00	0.00	0.22	0.00
43.20	211.46	2.00	0.00	0.21	0.00	43.30	206.62	2.00	0.00	0.21	0.00
43.40	203.46	2.00	0.00	0.21	0.00	43.50	201.69	2.00	0.00	0.21	0.00
43.60	202.69	2.00	0.00	0.21	0.00	43.70	206.92	2.00	0.00	0.21	0.00
43.80	212.43	2.00	0.00	0.20	0.00	43.90	219.18	2.00	0.00	0.20	0.00
44.00	224.99	2.00	0.00	0.20	0.00	44.10	228.04	2.00	0.00	0.20	0.00
44.20	226.58	2.00	0.00	0.20	0.00	44.30	224.33	2.00	0.00	0.19	0.00
44.40	225.82	2.00	0.00	0.19	0.00	44.50	229.76	2.00	0.00	0.19	0.00
44.60	234.21	2.00	0.00	0.19	0.00	44.70	237.29	2.00	0.00	0.19	0.00
44.80	237.14	2.00	0.00	0.19	0.00	44.90	236.92	2.00	0.00	0.18	0.00
45.00	238.50	2.00	0.00	0.18	0.00	45.10	241.30	2.00	0.00	0.18	0.00
45.20	240.66	2.00	0.00	0.18	0.00	45.30	233.32	2.00	0.00	0.18	0.00
45.40	223.45	2.00	0.00	0.17	0.00	45.50	212.12	2.00	0.00	0.17	0.00
45.60	201.87	2.00	0.00	0.17	0.00	45.70	197.04	1.70	0.02	0.17	0.00
45.80	193.78	1.44	0.05	0.17	0.00	45.90	196.29	1.64	0.03	0.17	0.00
46.00	205.96	2.00	0.00	0.16	0.00	46.10	218.21	2.00	0.00	0.16	0.00
46.20	233.37	2.00	0.00	0.16	0.00	46.30	246.17	2.00	0.00	0.16	0.00
46.40	255.35	2.00	0.00	0.16	0.00	46.50	260.82	2.00	0.00	0.15	0.00
46.60	264.75	2.00	0.00	0.15	0.00	46.70	267.72	2.00	0.00	0.15	0.00
46.80	267.50	2.00	0.00	0.15	0.00	46.90	263.67	2.00	0.00	0.15	0.00
47.00	259.19	2.00	0.00	0.15	0.00	47.10	256.05	2.00	0.00	0.14	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
47.20	255.27	2.00	0.00	0.14	0.00	47.30	254.18	2.00	0.00	0.14	0.00
47.40	250.28	2.00	0.00	0.14	0.00	47.50	241.80	2.00	0.00	0.14	0.00
47.60	228.70	2.00	0.00	0.13	0.00	47.70	213.38	2.00	0.00	0.13	0.00
47.80	203.40	2.00	0.00	0.13	0.00	47.90	202.36	2.00	0.00	0.13	0.00
48.00	205.34	2.00	0.00	0.13	0.00	48.10	224.16	2.00	0.00	0.13	0.00
48.20	213.97	2.00	0.00	0.12	0.00	48.30	178.96	2.00	0.00	0.12	0.00
48.40	140.97	2.00	0.00	0.12	0.00	48.50	111.18	2.00	0.00	0.12	0.00
48.60	47.68	2.00	0.00	0.12	0.00	48.70	44.75	2.00	0.00	0.11	0.00
48.80	28.89	2.00	0.00	0.11	0.00	48.90	35.15	2.00	0.00	0.11	0.00
49.00	111.11	2.00	0.00	0.11	0.00	49.10	130.56	2.00	0.00	0.11	0.00
49.20	152.77	2.00	0.00	0.11	0.00	49.30	169.68	2.00	0.00	0.10	0.00
49.40	181.94	2.00	0.00	0.10	0.00	49.50	191.14	2.00	0.00	0.10	0.00
49.60	193.22	2.00	0.00	0.10	0.00	49.70	194.11	2.00	0.00	0.10	0.00
49.80	199.91	2.00	0.00	0.09	0.00	49.90	205.02	2.00	0.00	0.09	0.00

Total estimated settlement: 0.45**Abbreviations**

$Q_{tn,cs}$:	Equivalent clean sand normalized cone resistance
FS:	Factor of safety against liquefaction
e_v (%):	Post-liquefaction volumetric strain
DF:	e_v depth weighting factor
Settlement:	Calculated settlement

:: Strength loss calculation Idriss & Boulanger (2008) ::

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.10	35.03	56.27	2.63	148.20	2.45	0.13	0.78
0.20	35.16	56.47	2.68	151.58	2.45	0.13	0.79
0.30	34.73	55.78	2.80	155.97	2.47	0.13	0.78
0.40	33.65	54.02	2.91	157.43	2.49	0.13	0.78
0.50	32.47	52.12	2.94	152.98	2.49	0.12	0.78
0.60	31.69	50.86	2.84	144.21	2.48	0.12	0.77
0.70	31.23	50.10	2.71	135.86	2.46	0.12	0.77
0.80	31.07	49.84	2.63	131.07	2.45	0.12	0.77
0.90	31.07	49.83	2.60	129.39	2.44	0.12	0.77
1.00	30.99	49.69	2.59	128.54	2.44	0.12	0.77
1.10	30.22	48.45	2.61	126.56	2.44	0.12	0.77
1.20	28.62	45.87	2.70	123.81	2.46	0.11	0.76
1.30	25.29	40.51	2.99	121.17	2.50	0.11	0.75
1.40	21.46	34.34	3.55	121.97	2.58	0.10	0.74
1.50	19.76	31.60	4.19	132.32	2.65	0.09	0.62
1.60	17.77	28.39	4.99	141.68	2.73	0.10	0.62
1.70	17.28	27.60	5.57	153.72	2.78	0.09	0.62
1.80	17.01	27.16	6.05	164.19	2.82	0.09	0.62
1.90	17.94	28.64	5.84	167.32	2.80	0.10	0.62
2.00	18.20	29.06	5.50	159.89	2.77	0.10	0.62
2.10	17.74	28.31	5.05	142.99	2.73	0.09	0.62
2.20	17.81	28.40	4.68	132.96	2.70	0.10	0.62
2.30	17.30	27.57	4.75	131.09	2.70	0.10	0.62
2.40	15.15	24.12	5.50	132.52	2.77	0.09	0.62
2.50	12.68	20.13	6.60	132.83	2.86	0.09	0.62
2.60	10.83	17.16	7.62	130.66	2.93	0.09	0.62
2.70	10.19	16.12	8.06	129.90	2.96	0.08	0.62
2.80	10.31	16.30	7.98	130.11	2.95	0.09	0.62
2.90	11.42	18.07	7.32	132.27	2.91	0.09	0.62
3.00	13.17	20.88	6.37	133.02	2.84	0.09	0.62
3.10	14.98	23.78	5.58	132.77	2.78	0.09	0.62
3.20	15.49	24.59	5.33	131.09	2.76	0.09	0.62
3.30	14.62	23.19	5.60	129.91	2.78	0.09	0.62
3.40	13.98	22.15	5.93	131.32	2.81	0.09	0.62
3.50	15.01	23.79	5.60	133.20	2.78	0.09	0.62
3.60	17.48	27.75	4.75	131.84	2.70	0.10	0.62
3.70	20.02	31.81	4.00	127.33	2.63	0.10	0.62
3.80	20.81	33.08	3.78	125.01	2.60	0.10	0.62
3.90	19.38	30.77	4.13	127.20	2.64	0.10	0.62
4.00	16.73	26.51	5.05	133.91	2.73	0.09	0.62
4.10	14.89	23.54	5.97	140.56	2.81	0.09	0.62
4.20	15.11	23.89	6.00	143.43	2.81	0.09	0.62
4.30	17.12	27.11	5.14	139.41	2.74	0.10	0.62
4.40	20.17	31.99	4.05	129.66	2.63	0.10	0.62
4.50	23.37	37.12	3.22	119.41	2.53	0.10	0.75
4.60	26.36	41.92	2.68	112.35	2.45	0.11	0.75
4.70	28.28	45.01	2.39	107.51	2.40	0.11	0.76
4.80	28.50	45.35	2.29	103.81	2.38	0.11	0.76

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
4.90	26.77	42.56	2.42	102.96	2.41	0.11	0.75
5.00	23.34	37.04	2.87	106.48	2.48	0.10	0.74
5.10	18.70	29.57	3.78	111.85	2.60	0.10	0.62
5.20	14.38	22.63	5.11	115.62	2.74	0.09	0.62
5.30	11.34	17.72	6.53	115.77	2.85	0.08	0.62
5.40	9.53	14.82	7.70	114.05	2.93	0.08	0.62
5.50	8.69	13.46	8.49	114.28	2.98	0.08	0.62
5.60	10.46	16.29	7.78	126.71	2.94	0.08	0.62
5.70	12.39	19.38	7.05	136.70	2.89	0.09	0.62
5.80	13.72	21.51	6.59	141.77	2.86	0.09	0.62
5.90	11.35	17.70	7.45	131.79	2.92	0.09	0.62
6.00	9.16	14.16	8.39	118.81	2.98	0.08	0.62
6.10	7.81	11.99	8.80	105.61	3.00	0.08	1.53
6.20	9.31	14.39	6.98	100.50	2.88	0.08	0.62
6.30	13.02	20.34	4.69	95.45	2.70	0.09	0.62
6.40	17.23	27.09	3.21	86.98	2.53	0.09	0.72
6.50	19.97	31.49	2.45	77.10	2.41	0.09	0.73
6.60	21.02	33.16	2.24	74.34	2.37	0.09	0.73
6.70	21.55	34.00	2.35	79.96	2.40	0.09	0.73
6.80	24.54	38.80	2.36	91.49	2.40	0.09	0.73
6.90	28.95	45.87	2.22	101.77	2.37	0.11	0.76
7.00	33.02	52.41	2.12	110.85	2.35	0.12	0.77
7.10	34.38	54.59	2.18	118.90	2.36	0.12	0.77
7.20	33.32	52.87	2.33	122.98	2.39	0.12	0.77
7.30	30.96	49.08	2.51	123.40	2.43	0.11	0.76
7.40	27.34	43.25	2.88	124.48	2.49	0.11	0.75
7.50	23.15	36.51	3.57	130.52	2.58	0.10	0.74
7.60	18.85	29.58	4.74	140.29	2.70	0.10	0.62
7.70	15.01	23.41	6.26	146.59	2.83	0.09	0.62
7.80	12.30	19.05	7.76	147.86	2.94	0.09	0.62
7.90	11.37	17.54	8.34	146.36	2.97	0.09	0.62
8.00	12.13	18.76	7.66	143.62	2.93	0.09	0.62
8.10	13.66	21.20	6.50	137.88	2.85	0.09	0.62
8.20	15.81	24.65	5.23	128.98	2.75	0.09	0.62
8.30	18.07	28.27	4.13	116.61	2.64	0.09	0.62
8.40	19.89	31.18	3.36	104.72	2.55	0.09	0.73
8.50	20.92	32.83	2.92	96.00	2.49	0.09	0.72
8.60	21.23	33.33	2.68	89.43	2.45	0.09	0.72
8.70	21.47	33.70	2.53	85.42	2.43	0.09	0.72
8.80	21.51	33.75	2.48	83.86	2.42	0.09	0.72
8.90	21.51	33.74	2.59	87.25	2.44	0.09	0.72
9.00	20.90	32.76	2.89	94.83	2.49	0.09	0.73
9.10	19.70	30.82	3.36	103.44	2.55	0.09	0.72
9.20	19.12	29.87	3.72	111.20	2.60	0.09	0.72
9.30	19.54	30.54	3.78	115.46	2.60	0.09	0.62
9.40	20.38	31.88	3.70	117.88	2.59	0.09	0.73
9.50	19.23	30.02	4.03	120.93	2.63	0.09	0.62
9.60	16.01	24.85	4.97	123.59	2.72	0.09	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.70	13.82	21.32	6.11	130.24	2.82	0.08	0.62
9.80	15.64	24.23	5.80	140.46	2.80	0.09	0.62
9.90	16.35	25.36	5.54	140.64	2.77	0.10	0.62
10.00	13.35	20.53	6.33	129.99	2.84	0.09	0.62
10.10	8.41	12.60	8.81	111.00	3.00	0.07	1.10
10.20	7.41	10.98	9.70	106.50	3.05	0.08	0.96
10.30	10.53	15.99	7.24	115.77	2.90	0.08	0.62
10.40	13.79	21.21	5.73	121.61	2.79	0.09	0.62
10.50	16.27	25.19	5.05	127.32	2.73	0.09	0.62
10.60	16.77	25.98	5.14	133.59	2.74	0.09	0.62
10.70	14.80	22.81	6.03	137.61	2.81	0.09	0.62
10.80	11.32	17.20	7.86	135.15	2.94	0.08	0.62
10.90	7.88	11.67	10.61	123.92	3.10	0.08	0.98
11.00	5.67	8.11	13.38	108.54	3.23	0.07	0.68
11.10	4.53	6.26	15.07	94.40	3.30	0.07	0.52
11.20	4.05	5.49	15.43	84.70	3.31	0.07	0.46
11.30	3.98	5.38	14.99	80.56	3.29	0.07	0.45
11.40	3.98	5.37	14.70	78.88	3.28	0.07	0.44
11.50	3.98	5.36	14.69	78.73	3.28	0.07	0.44
11.60	3.98	5.35	14.90	79.73	3.29	0.07	0.44
11.70	3.98	5.34	15.27	81.62	3.30	0.07	0.44
11.80	3.92	5.23	15.89	83.18	3.33	0.07	0.43
11.90	3.81	5.05	16.55	83.52	3.35	0.07	0.41
12.00	4.07	5.47	15.74	86.02	3.32	0.07	0.44
12.10	4.67	6.41	14.01	89.81	3.25	0.07	0.52
12.20	5.31	7.44	12.48	92.82	3.19	0.07	0.60
12.30	5.58	7.86	11.85	93.10	3.16	0.07	0.63
12.40	5.58	7.85	11.76	92.25	3.16	0.07	0.63
12.50	5.58	7.84	11.77	92.27	3.16	0.07	0.62
12.60	5.58	7.83	11.91	93.30	3.16	0.07	0.62
12.70	5.58	7.82	12.19	95.35	3.18	0.07	0.62
12.80	5.58	7.81	12.58	98.32	3.19	0.07	0.62
12.90	5.58	7.81	13.03	101.75	3.21	0.07	0.61
13.00	5.80	8.15	13.01	105.98	3.21	0.07	0.64
13.10	6.32	8.98	12.26	110.03	3.18	0.08	0.70
13.20	6.51	9.28	11.86	110.05	3.16	0.08	0.72
13.30	5.94	8.36	12.49	104.43	3.19	0.08	0.65
13.40	4.89	6.66	14.24	94.86	3.26	0.07	0.51
13.50	4.17	5.49	15.78	86.58	3.32	0.07	0.42
13.60	3.98	5.19	15.93	82.61	3.33	0.07	0.40
13.70	3.98	5.18	15.73	81.45	3.32	0.07	0.40
13.80	3.98	5.17	15.90	82.20	3.33	0.07	0.39
13.90	3.98	5.16	16.29	84.10	3.34	0.07	0.39
14.00	3.98	5.16	16.53	85.22	3.35	0.07	0.39
14.10	3.98	5.15	16.38	84.32	3.34	0.07	0.39
14.20	3.98	5.14	16.03	82.39	3.33	0.07	0.39
14.30	3.76	4.77	16.64	79.44	3.35	0.07	0.36
14.40	3.50	4.34	17.76	77.09	3.39	0.07	0.32

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
14.50	3.50	4.33	17.73	76.81	3.39	0.07	0.32
14.60	3.72	4.68	16.67	78.02	3.35	0.07	0.35
14.70	4.09	5.27	15.53	81.90	3.31	0.07	0.39
14.80	4.51	5.94	14.94	88.75	3.29	0.07	0.44
14.90	5.25	7.11	13.98	99.46	3.25	0.07	0.52
15.00	6.18	8.60	12.89	110.86	3.21	0.07	0.63
15.10	7.12	10.11	11.88	120.14	3.16	0.08	0.74
15.20	9.50	13.92	9.53	132.64	3.04	0.08	1.01
15.30	14.31	21.55	6.61	142.42	2.86	0.08	0.62
15.40	22.91	33.70	4.20	141.57	2.65	0.09	0.62
15.50	34.71	49.46	2.67	132.07	2.45	0.11	0.75
15.60	50.28	69.50	1.86	129.32	2.28	0.12	0.78
15.70	67.84	91.62	1.53	140.05	2.16	0.15	0.81
15.80	85.19	112.65	1.37	154.02	2.06	0.18	0.83
15.90	100.36	130.44	1.29	168.64	1.98	0.20	0.84
16.00	105.72	136.09	1.27	172.49	1.95	0.25	0.85
16.10	103.10	132.76	1.28	169.98	1.96	0.21	0.84
16.20	98.78	127.74	1.31	167.57	2.01	0.18	0.83
16.30	98.29	127.29	1.33	169.86	2.03	0.21	0.85
16.40	97.60	126.46	1.36	171.44	2.05	0.22	0.85
16.50	89.65	116.68	1.41	164.92	2.10	0.19	0.84
16.60	76.67	100.71	1.55	156.50	2.17	0.17	0.83
16.70	61.52	81.89	1.86	152.38	2.28	0.15	0.81
16.80	46.02	62.21	2.47	153.43	2.42	0.12	0.78
16.90	32.20	44.17	3.49	154.14	2.57	0.10	0.74
17.00	21.83	30.21	4.93	149.00	2.72	0.09	0.62
17.10	15.15	20.96	6.56	137.50	2.85	0.08	0.62
17.20	10.77	14.63	8.35	122.13	2.97	0.08	0.62
17.30	8.03	10.50	10.10	106.07	3.07	0.08	0.75
17.40	6.41	8.07	11.50	92.75	3.14	0.07	0.58
17.50	5.73	7.02	12.00	84.31	3.17	0.07	0.50
17.60	5.58	6.78	11.73	79.47	3.15	0.07	0.48
17.70	5.58	6.75	11.32	76.40	3.13	0.07	0.48
17.80	5.58	6.72	11.06	74.35	3.12	0.07	0.48
17.90	5.58	6.70	10.88	72.87	3.11	0.07	0.48
18.00	5.72	6.88	10.66	73.35	3.10	0.07	0.49
18.10	6.17	7.51	10.32	77.52	3.08	0.07	0.54
18.20	6.71	8.26	10.49	86.59	3.09	0.08	0.59
18.30	7.09	8.79	11.14	97.84	3.13	0.08	0.63
18.40	7.50	9.34	11.83	110.45	3.16	0.08	0.67
18.50	8.13	10.20	11.90	121.37	3.16	0.08	0.73
18.60	9.21	11.70	11.14	130.42	3.13	0.08	0.84
18.70	10.73	13.82	9.94	137.35	3.06	0.08	0.99
18.80	12.95	16.91	8.40	141.97	2.98	0.08	0.62
18.90	16.09	21.07	6.75	142.29	2.87	0.09	0.62
19.00	18.81	24.48	5.62	137.61	2.78	0.09	0.62
19.10	20.48	26.48	5.08	134.56	2.73	0.09	0.62
19.20	20.52	26.47	5.17	136.81	2.74	0.09	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
19.30	19.41	25.03	5.71	142.80	2.79	0.09	0.62
19.40	17.68	22.76	6.37	145.07	2.84	0.09	0.62
19.50	16.31	20.89	6.76	141.25	2.87	0.09	0.62
19.60	16.30	20.74	6.48	134.47	2.85	0.09	0.62
19.70	18.29	23.15	5.67	131.33	2.79	0.09	0.62
19.80	20.97	26.45	5.00	132.10	2.73	0.09	0.62
19.90	22.75	28.62	4.78	136.95	2.71	0.10	0.62
20.00	21.58	27.13	5.24	142.04	2.75	0.09	0.62
20.10	17.47	21.89	6.41	140.38	2.84	0.09	0.62
20.20	12.54	15.41	8.35	128.64	2.97	0.08	0.62
20.30	8.93	10.49	10.29	107.93	3.08	0.08	0.75
20.40	7.14	8.05	11.19	90.08	3.13	0.07	0.58
20.50	6.30	6.91	11.44	79.02	3.14	0.07	0.49
20.60	5.79	6.20	11.94	74.02	3.16	0.07	0.44
20.70	5.58	5.90	12.86	75.85	3.21	0.07	0.42
20.80	5.55	5.83	13.87	80.95	3.25	0.07	0.42
20.90	5.51	5.77	14.68	84.69	3.28	0.07	0.41
21.00	5.50	5.72	14.89	85.19	3.29	0.07	0.41
21.10	5.47	5.67	14.79	83.89	3.28	0.07	0.41
21.20	5.83	6.12	14.16	86.65	3.26	0.07	0.44
21.30	6.38	6.82	13.86	94.51	3.25	0.07	0.49
21.40	7.19	7.84	13.40	105.08	3.23	0.07	0.56
21.50	7.91	8.76	12.89	112.96	3.21	0.08	0.63
21.60	8.45	9.42	12.27	115.54	3.18	0.08	0.67
21.70	8.76	9.78	11.61	113.59	3.15	0.08	0.70
21.80	8.66	9.62	11.27	108.42	3.13	0.08	0.69
21.90	8.24	9.05	11.36	102.78	3.14	0.08	0.65
22.00	7.71	8.33	11.83	98.57	3.16	0.08	0.60
22.10	7.52	8.07	12.16	98.11	3.17	0.07	0.58
22.20	7.95	8.58	11.86	101.78	3.16	0.08	0.61
22.30	8.79	9.62	11.28	108.47	3.13	0.08	0.69
22.40	9.90	11.00	10.70	117.69	3.10	0.08	0.79
22.50	12.35	14.05	9.28	130.38	3.03	0.08	1.00
22.60	16.82	19.58	7.18	140.54	2.90	0.09	0.62
22.70	23.64	27.60	5.22	144.22	2.75	0.09	0.62
22.80	31.17	36.29	4.03	146.10	2.63	0.10	0.62
22.90	36.34	42.22	3.60	152.07	2.58	0.11	0.76
23.00	37.64	43.70	3.73	163.02	2.60	0.11	0.76
23.10	35.29	40.99	4.29	175.65	2.66	0.11	0.62
23.20	32.02	37.18	5.02	186.79	2.73	0.11	0.62
23.30	29.06	33.69	5.75	193.53	2.79	0.10	0.62
23.40	26.91	31.10	6.28	195.41	2.83	0.10	0.62
23.50	25.69	29.58	6.59	194.81	2.86	0.10	0.62
23.60	25.99	29.81	6.54	195.02	2.85	0.10	0.62
23.70	28.55	32.65	6.00	195.78	2.81	0.10	0.62
23.80	33.44	38.10	5.09	194.00	2.74	0.11	0.62
23.90	39.82	45.14	4.16	187.57	2.64	0.11	0.62
24.00	46.53	52.41	3.40	177.95	2.56	0.12	0.77

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
24.10	54.51	60.94	2.73	166.42	2.46	0.13	0.78
24.20	65.10	72.15	2.14	154.76	2.35	0.14	0.80
24.30	79.01	86.81	1.73	150.17	2.24	0.16	0.82
24.40	93.89	102.42	1.52	155.95	2.16	0.19	0.84
24.50	106.54	115.72	1.45	167.93	2.12	0.22	0.86
24.60	115.17	124.79	1.44	179.54	2.11	0.26	0.87
24.70	120.39	130.21	1.45	188.31	2.12	0.28	0.87
24.80	116.41	125.70	1.48	186.07	2.14	0.30	0.88
24.90	104.61	112.80	1.55	174.94	2.17	0.22	0.85
25.00	92.13	99.19	1.65	163.53	2.21	0.17	0.83
25.10	88.30	94.90	1.71	162.47	2.24	0.18	0.83
25.20	92.70	99.44	1.72	171.07	2.24	0.19	0.84
25.30	95.86	102.67	1.75	179.84	2.25	0.21	0.85
25.40	93.78	100.31	1.85	185.09	2.28	0.21	0.85
25.50	85.40	91.26	2.04	185.93	2.33	0.19	0.84
25.60	72.79	77.70	2.37	184.22	2.40	0.16	0.82
25.70	58.75	62.59	2.91	181.87	2.49	0.14	0.79
25.80	45.10	47.88	3.77	180.31	2.60	0.12	0.62
25.90	32.80	34.58	5.12	177.19	2.74	0.10	0.62
26.00	22.82	23.72	7.10	168.46	2.89	0.09	0.62
26.10	15.86	15.95	9.57	152.57	3.04	0.08	1.14
26.20	12.59	12.29	11.26	138.34	3.13	0.08	0.88
26.30	11.74	11.30	11.54	130.48	3.15	0.08	0.81
26.40	11.90	11.45	11.21	128.32	3.13	0.08	0.82
26.50	12.02	11.53	11.11	128.19	3.12	0.08	0.82
26.60	12.19	11.68	11.13	130.07	3.13	0.08	0.83
26.70	12.99	12.51	10.72	134.19	3.11	0.08	0.89
26.80	14.07	13.65	10.12	138.10	3.07	0.08	0.97
26.90	15.03	14.64	9.63	141.00	3.05	0.08	1.05
27.00	15.05	14.62	9.68	141.53	3.05	0.08	1.04
27.10	14.04	13.48	10.31	138.95	3.08	0.08	0.96
27.20	11.95	11.20	11.70	130.94	3.15	0.08	0.80
27.30	10.07	9.14	13.21	120.75	3.22	0.08	0.65
27.40	9.47	8.47	13.49	114.25	3.23	0.08	0.60
27.50	9.83	8.83	12.83	113.31	3.20	0.08	0.63
27.60	10.36	9.36	12.19	114.18	3.18	0.08	0.67
27.70	10.36	9.33	12.14	113.35	3.17	0.08	0.67
27.80	10.36	9.30	12.17	113.23	3.17	0.08	0.66
27.90	10.36	9.28	12.24	113.51	3.18	0.08	0.66
28.00	10.36	9.25	12.38	114.54	3.18	0.08	0.66
28.10	10.94	9.82	12.02	118.10	3.17	0.08	0.70
28.20	14.59	13.61	9.63	131.07	3.05	0.08	0.97
28.30	22.51	21.80	6.71	146.37	2.87	0.09	0.62
28.40	32.54	32.00	4.98	159.28	2.73	0.10	0.62
28.50	38.83	38.31	4.43	169.83	2.67	0.11	0.62
28.60	38.69	38.08	4.69	178.69	2.70	0.11	0.62
28.70	34.55	33.80	5.48	185.09	2.77	0.10	0.62
28.80	30.65	29.76	6.24	185.71	2.83	0.10	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
28.90	30.40	29.40	6.15	180.95	2.82	0.10	0.62
29.00	35.55	34.46	4.92	169.60	2.72	0.10	0.62
29.10	47.27	45.99	3.27	150.23	2.54	0.11	0.76
29.20	63.97	62.34	2.18	135.74	2.36	0.13	0.79
29.30	82.47	80.36	1.70	136.78	2.23	0.16	0.82
29.40	101.51	98.87	1.52	150.70	2.16	0.19	0.84
29.50	120.40	117.15	1.44	168.35	2.11	0.25	0.86
29.60	138.78	134.84	1.39	186.85	2.08	0.33	0.88
29.70	151.39	146.84	1.36	200.29	2.06	0.47	0.90
29.80	149.49	144.67	1.38	199.31	2.07	0.51	0.90
29.90	134.76	130.04	1.44	187.01	2.11	0.31	0.88
30.00	124.88	120.19	1.52	183.25	2.16	0.22	0.85
30.10	126.66	121.66	1.57	191.06	2.18	0.31	0.88
30.20	133.00	127.49	1.55	198.22	2.17	0.38	0.89
30.30	130.73	124.96	1.54	191.86	2.17	0.31	0.88
30.40	122.90	117.07	1.52	177.76	2.16	0.26	0.87
30.50	115.21	109.38	1.51	165.69	2.16	0.23	0.86
30.60	106.62	100.89	1.58	159.60	2.19	0.21	0.85
30.70	95.19	89.73	1.79	160.35	2.26	0.19	0.84
30.80	81.78	76.72	2.16	165.73	2.36	0.16	0.82
30.90	68.85	64.18	2.64	169.28	2.45	0.14	0.80
31.00	59.25	54.87	3.06	168.18	2.51	0.13	0.78
31.10	54.12	49.84	3.29	164.08	2.54	0.12	0.77
31.20	52.83	48.48	3.30	159.96	2.54	0.12	0.77
31.30	53.99	49.46	3.24	160.45	2.54	0.12	0.78
31.40	56.15	51.36	3.28	168.66	2.54	0.13	0.78
31.50	62.49	57.19	3.19	182.27	2.53	0.13	0.78
31.60	78.37	71.97	2.66	191.72	2.45	0.15	0.81
31.70	106.07	97.78	2.01	196.67	2.32	0.22	0.85
31.80	135.90	125.49	1.65	206.96	2.21	0.40	0.89
31.90	156.45	144.41	1.52	218.92	2.16	0.63	0.91
32.00	161.73	148.97	1.51	225.02	2.15	0.68	0.92
32.10	152.47	139.95	1.60	223.85	2.19	0.58	0.91
32.20	133.57	122.00	1.81	220.31	2.27	0.36	0.89
32.30	109.16	99.04	2.17	215.22	2.36	0.24	0.86
32.40	86.47	77.81	2.66	206.72	2.45	0.18	0.83
32.50	67.96	60.56	3.17	192.08	2.53	0.14	0.80
32.60	54.22	47.80	3.69	176.53	2.59	0.12	0.77
32.70	44.06	38.38	4.29	164.82	2.66	0.11	0.62
32.80	36.99	31.83	4.92	156.67	2.72	0.10	0.62
32.90	33.29	28.38	5.31	150.72	2.75	0.10	0.62
33.00	32.53	27.62	5.34	147.55	2.76	0.10	0.62
33.10	33.38	28.32	5.20	147.34	2.75	0.10	0.62
33.20	34.55	29.30	5.02	147.24	2.73	0.10	0.62
33.30	35.86	30.41	4.77	145.11	2.71	0.10	0.62
33.40	37.95	32.22	4.39	141.56	2.67	0.10	0.62
33.50	40.53	34.46	4.07	140.30	2.64	0.11	0.62
33.60	42.96	36.56	3.90	142.53	2.62	0.11	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
33.70	44.99	38.28	3.84	147.15	2.61	0.11	0.62
33.80	46.37	39.39	3.91	153.98	2.62	0.11	0.62
33.90	46.18	39.09	4.14	161.77	2.64	0.12	0.62
34.00	43.62	36.68	4.64	170.22	2.69	0.11	0.62
34.10	39.11	32.55	5.41	176.17	2.76	0.11	0.62
34.20	34.19	28.10	6.28	176.54	2.83	0.10	0.62
34.30	31.45	25.62	6.63	169.90	2.86	0.10	0.62
34.40	33.42	27.32	5.70	155.78	2.79	0.10	0.62
34.50	41.97	34.87	3.83	133.69	2.61	0.10	0.62
34.60	54.67	46.11	2.59	119.37	2.44	0.12	0.77
34.70	63.98	54.25	2.27	122.97	2.38	0.14	0.79
34.80	63.78	53.84	2.55	137.27	2.43	0.14	0.79
34.90	54.43	45.37	3.39	153.88	2.56	0.12	0.77
35.00	42.54	34.80	4.68	162.86	2.70	0.11	0.62
35.10	33.70	27.01	6.05	163.48	2.82	0.10	0.62
35.20	29.21	23.06	6.93	159.94	2.88	0.10	0.62
35.30	28.14	22.10	7.22	159.50	2.90	0.10	0.62
35.40	28.25	22.13	7.32	162.04	2.91	0.10	0.62
35.50	28.92	22.63	7.23	163.54	2.90	0.10	0.62
35.60	31.20	24.50	6.54	160.16	2.85	0.10	0.62
35.70	35.84	28.45	5.37	152.87	2.76	0.10	0.62
35.80	41.61	33.35	4.48	149.43	2.68	0.11	0.62
35.90	46.85	37.75	4.10	154.66	2.64	0.11	0.62
36.00	48.90	39.35	4.25	167.23	2.65	0.12	0.62
36.10	46.83	37.40	4.84	180.94	2.71	0.12	0.62
36.20	40.81	32.14	5.88	189.00	2.80	0.11	0.62
36.30	34.31	26.58	7.09	188.59	2.89	0.10	0.62
36.40	30.73	23.56	7.68	180.83	2.93	0.10	0.62
36.50	32.04	24.57	6.93	170.18	2.88	0.10	0.62
36.60	37.92	29.50	5.32	156.90	2.76	0.10	0.62
36.70	47.30	37.46	3.77	141.07	2.60	0.11	0.62
36.80	57.90	46.49	2.74	127.19	2.46	0.12	0.77
36.90	67.57	54.71	2.24	122.48	2.37	0.13	0.79
37.00	73.31	59.46	2.14	127.09	2.35	0.14	0.80
37.10	73.91	59.72	2.29	136.52	2.38	0.14	0.80
37.20	70.47	56.54	2.60	146.83	2.44	0.14	0.80
37.30	66.08	52.61	2.93	153.93	2.49	0.13	0.79
37.40	64.16	50.85	3.05	155.23	2.51	0.13	0.78
37.50	66.79	53.00	2.82	149.45	2.48	0.13	0.79
37.60	74.80	59.77	2.31	138.09	2.39	0.14	0.80
37.70	86.08	69.42	1.84	127.65	2.28	0.15	0.81
37.80	97.88	79.53	1.56	123.99	2.18	0.16	0.82
37.90	107.58	87.78	1.44	126.65	2.12	0.18	0.83
38.00	112.98	92.22	1.42	130.53	2.10	0.19	0.84
38.10	113.65	92.51	1.44	132.78	2.11	0.19	0.84
38.20	110.48	89.55	1.48	132.53	2.14	0.18	0.84
38.30	105.06	84.69	1.55	131.22	2.17	0.18	0.83
38.40	97.28	77.83	1.69	131.23	2.23	0.17	0.83

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
38.50	86.60	68.49	1.99	136.26	2.32	0.16	0.82
38.60	73.98	57.63	2.55	146.85	2.43	0.14	0.80
38.70	62.00	47.51	3.28	155.65	2.54	0.13	0.78
38.80	53.61	40.54	3.81	154.50	2.61	0.12	0.62
38.90	50.18	37.75	3.80	143.62	2.61	0.11	0.62
39.00	50.79	38.28	3.43	131.47	2.56	0.11	0.76
39.10	53.01	40.08	3.09	123.72	2.52	0.11	0.76
39.20	54.99	41.65	2.89	120.48	2.49	0.12	0.77
39.30	56.78	43.04	2.76	118.64	2.47	0.12	0.77
39.40	58.86	44.69	2.59	115.94	2.44	0.12	0.77
39.50	61.74	47.02	2.38	111.83	2.40	0.12	0.77
39.60	65.69	50.25	2.13	107.16	2.35	0.12	0.78
39.70	69.92	53.57	2.06	110.39	2.33	0.13	0.79
39.80	70.73	53.83	2.34	125.93	2.39	0.14	0.80
39.90	68.52	51.62	2.81	145.04	2.47	0.13	0.79
40.00	66.77	49.92	3.16	157.96	2.53	0.13	0.78
40.10	68.40	51.03	3.24	165.16	2.54	0.14	0.79
40.20	69.02	51.27	3.44	176.44	2.56	0.15	0.80
40.30	64.29	47.22	4.03	190.11	2.63	0.14	0.64
40.40	55.60	40.21	4.82	193.81	2.71	0.12	0.62
40.50	48.54	34.67	5.29	183.22	2.75	0.11	0.62
40.60	48.02	34.33	4.78	164.01	2.71	0.11	0.62
40.70	56.01	40.74	3.54	144.39	2.58	0.12	0.76
40.80	69.22	51.33	2.58	132.29	2.44	0.13	0.79
40.90	81.20	60.92	2.11	128.74	2.35	0.15	0.81
41.00	88.70	66.86	1.93	129.21	2.30	0.15	0.81
41.10	92.25	69.57	1.88	130.80	2.29	0.16	0.82
41.20	95.34	71.89	1.85	132.67	2.28	0.16	0.82
41.30	97.82	73.70	1.83	134.68	2.27	0.17	0.83
41.40	99.69	75.00	1.82	136.86	2.27	0.17	0.83
41.50	106.32	80.05	1.78	142.79	2.26	0.17	0.83
41.60	117.58	88.73	1.72	152.96	2.24	0.22	0.85
41.70	127.07	95.89	1.71	164.07	2.24	0.28	0.87
41.80	127.05	95.37	1.81	172.61	2.27	0.26	0.87
41.90	116.84	86.76	2.07	179.16	2.34	0.23	0.86
42.00	104.74	76.78	2.45	188.10	2.41	0.20	0.84
42.10	92.11	66.64	2.89	192.82	2.49	0.18	0.83
42.20	81.70	58.50	3.20	187.14	2.53	0.15	0.81
42.30	77.65	55.50	3.06	169.59	2.51	0.14	0.79
42.40	84.52	61.14	2.40	146.57	2.40	0.15	0.80
42.50	102.73	75.81	1.76	133.70	2.25	0.17	0.83
42.60	127.10	95.47	1.45	138.14	2.12	0.21	0.85
42.70	150.48	114.23	1.34	153.07	2.04	0.29	0.87
42.80	168.38	128.30	1.31	167.96	2.00	0.38	0.88
42.90	178.54	135.96	1.31	177.73	2.00	0.48	0.90
43.00	182.69	138.77	1.32	182.50	2.01	0.53	0.90
43.10	182.27	138.04	1.32	182.89	2.02	0.54	0.90
43.20	179.32	135.43	1.33	180.31	2.03	0.49	0.90

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
43.30	176.00	132.65	1.33	176.56	2.03	0.44	0.89
43.40	173.94	130.94	1.33	173.54	2.02	0.42	0.89
43.50	174.12	130.97	1.32	172.68	2.01	0.41	0.89
43.60	176.71	132.84	1.31	174.28	2.01	0.42	0.89
43.70	181.49	136.36	1.31	178.11	2.00	0.47	0.89
43.80	187.71	140.96	1.30	183.48	1.99	0.54	0.90
43.90	193.96	145.49	1.30	189.21	1.99	0.65	0.91
44.00	199.20	149.21	1.30	194.05	1.99	0.77	0.91
44.10	202.32	151.36	1.30	196.61	1.99	0.85	0.92
44.20	203.65	152.24	1.29	196.91	1.98	0.83	0.91
44.30	204.80	153.02	1.29	196.89	1.97	0.81	0.91
44.40	206.99	154.52	1.28	198.22	1.97	0.86	0.91
44.50	210.41	156.81	1.28	201.32	1.97	0.89	0.92
44.60	214.13	159.31	1.29	204.72	1.97	0.89	0.92
44.70	217.64	161.74	1.28	207.51	1.97	0.90	0.92
44.80	221.58	164.66	1.28	209.99	1.96	0.90	0.92
44.90	227.00	168.85	1.26	213.26	1.94	0.90	0.92
45.00	234.02	174.31	1.25	217.83	1.92	0.91	0.93
45.10	239.15	178.21	1.24	221.09	1.91	0.91	0.93
45.20	237.85	176.94	1.24	219.53	1.91	0.91	0.93
45.30	229.01	169.74	1.25	211.91	1.92	0.90	0.92
45.40	215.37	158.89	1.26	200.16	1.93	0.89	0.91
45.50	202.11	148.45	1.27	188.42	1.95	0.63	0.90
45.60	193.91	142.10	1.27	180.45	1.95	0.48	0.89
45.70	193.08	141.60	1.26	178.17	1.93	0.46	0.88
45.80	200.77	147.76	1.24	182.74	1.90	0.50	0.88
45.90	215.19	159.08	1.21	192.70	1.86	0.68	0.88
46.00	233.39	173.14	1.19	205.69	1.84	0.91	0.89
46.10	252.76	187.87	1.17	219.97	1.82	0.92	0.91
46.20	270.53	201.28	1.16	233.02	1.80	0.93	0.92
46.30	285.82	212.86	1.14	243.21	1.79	0.94	0.93
46.40	297.04	221.49	1.12	248.44	1.77	0.95	0.94
46.50	304.64	227.35	1.10	250.22	1.76	0.95	0.95
46.60	309.75	231.05	1.09	252.23	1.75	0.95	0.95
46.70	312.52	232.63	1.10	255.70	1.76	0.95	0.95
46.80	312.12	231.67	1.11	257.78	1.77	0.95	0.95
46.90	308.33	228.10	1.13	257.39	1.78	0.95	0.95
47.00	301.93	222.50	1.15	255.10	1.79	0.95	0.94
47.10	294.03	215.62	1.17	252.16	1.82	0.94	0.94
47.20	284.88	207.74	1.19	247.76	1.84	0.94	0.94
47.30	275.33	199.71	1.21	241.83	1.86	0.93	0.94
47.40	266.20	192.33	1.22	234.75	1.88	0.92	0.94
47.50	258.33	186.32	1.22	227.31	1.88	0.92	0.93
47.60	252.03	181.90	1.21	219.72	1.86	0.91	0.92
47.70	247.62	179.26	1.18	211.94	1.83	0.91	0.90
47.80	245.33	178.34	1.14	204.06	1.79	0.91	0.89
47.90	241.79	175.75	1.13	199.14	1.78	0.91	0.89
48.00	231.80	166.75	1.19	198.34	1.84	0.90	0.89

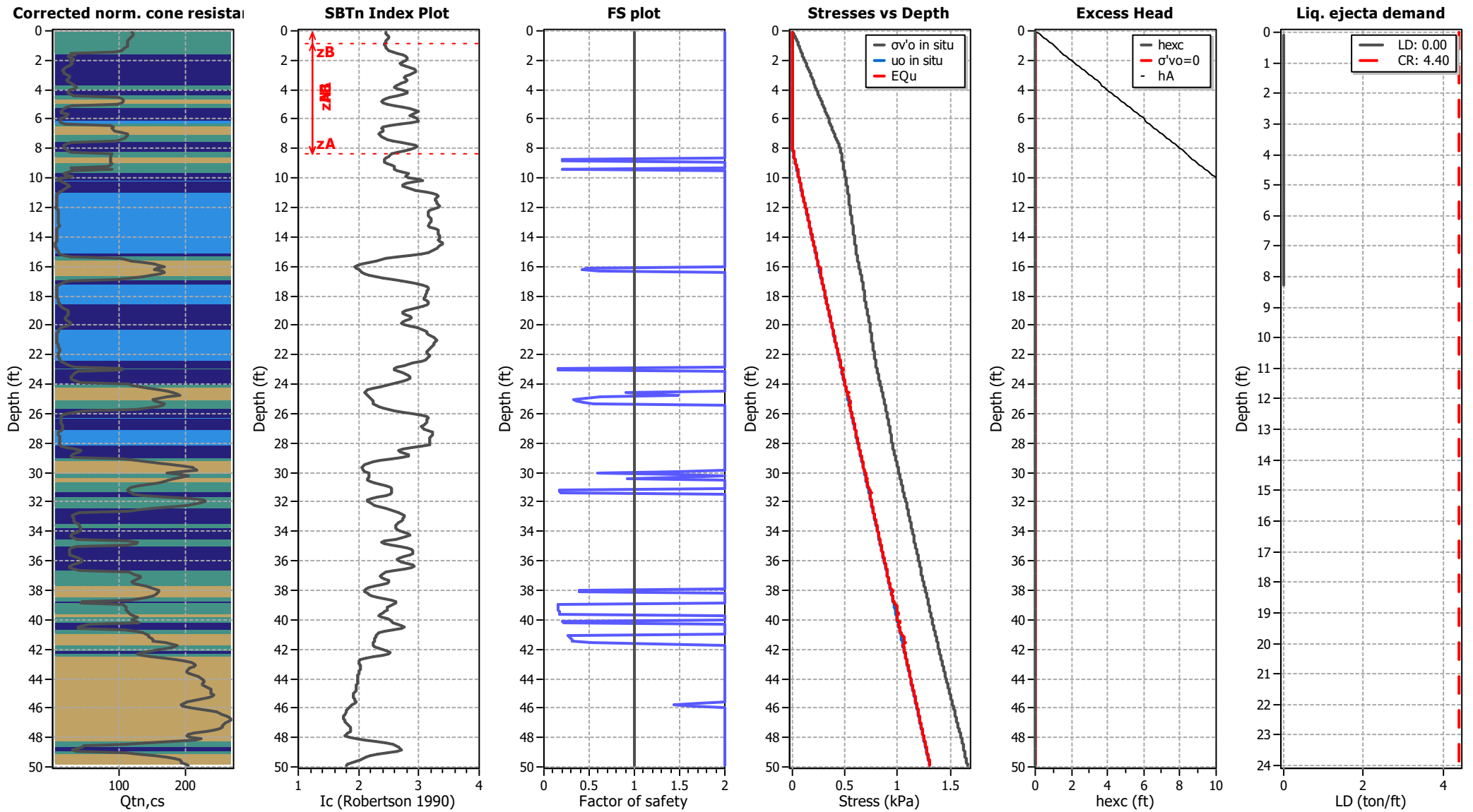
:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
48.10	209.20	147.31	1.27	187.38	1.95	0.88	0.91
48.20	174.47	119.30	1.43	170.86	2.11	0.48	0.90
48.30	133.42	88.12	1.85	163.29	2.28	0.25	0.86
48.40	94.91	60.35	2.65	160.03	2.45	0.16	0.81
48.50	71.47	44.05	3.47	152.95	2.57	0.12	0.77
48.60	60.38	36.51	3.96	144.56	2.62	0.12	0.62
48.70	52.78	31.38	4.41	138.25	2.67	0.12	0.62
48.80	47.63	27.94	4.74	132.29	2.70	0.10	0.62
48.90	49.25	29.16	4.18	121.84	2.65	0.10	0.62
49.00	65.35	40.31	2.84	114.60	2.48	0.12	0.77
49.10	87.91	56.32	1.98	111.28	2.31	0.14	0.80
49.20	112.10	73.73	1.59	117.57	2.19	0.17	0.83
49.30	133.65	89.17	1.45	129.73	2.12	0.22	0.85
49.40	151.11	101.56	1.40	142.05	2.09	0.26	0.87
49.50	166.58	112.85	1.34	151.72	2.04	0.32	0.88
49.60	185.29	127.04	1.29	163.26	1.97	0.37	0.88
49.70	208.76	145.19	1.23	178.64	1.89	0.53	0.88
49.80	231.42	162.73	1.18	191.98	1.83	0.90	0.89
49.90	245.61	173.66	1.14	198.32	1.79	0.91	0.89

Abbreviations

q_t :	Total cone resistance
K_c :	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c :	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

Ejecta Severity Estimation



LIQUEFACTION ANALYSIS REPORT

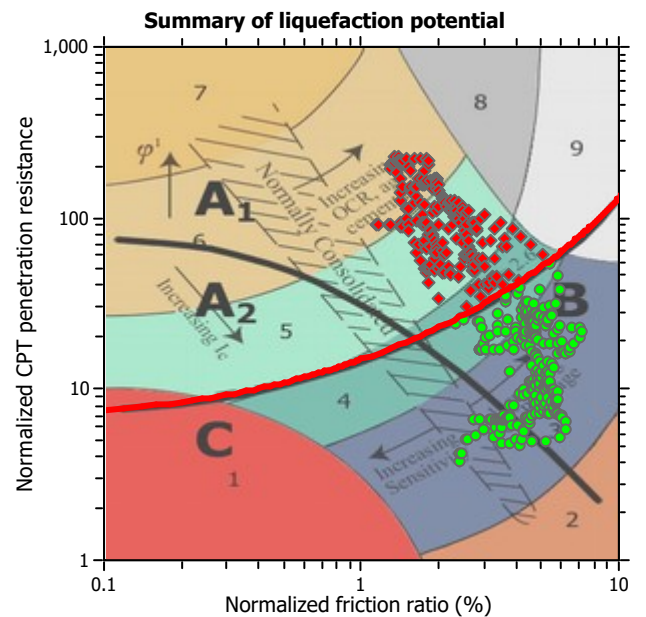
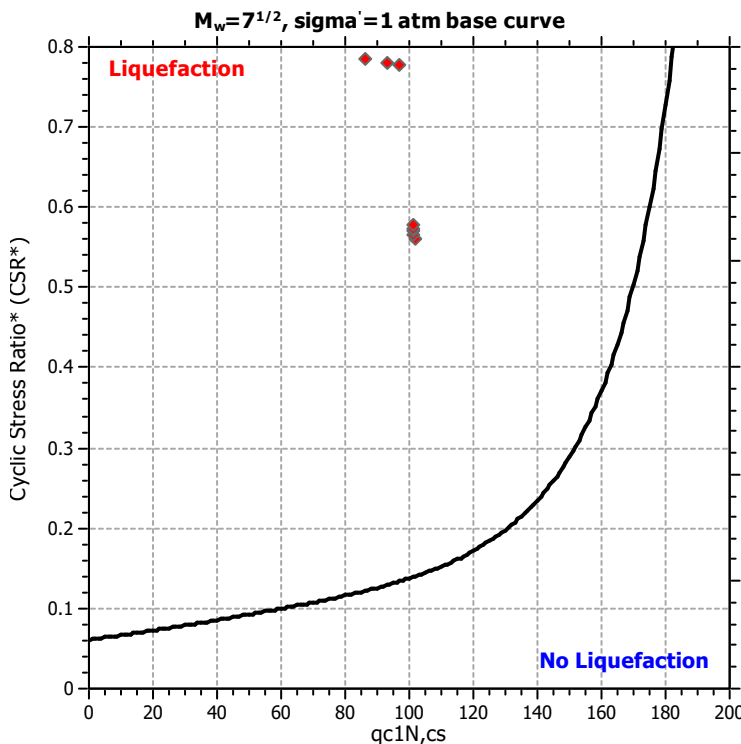
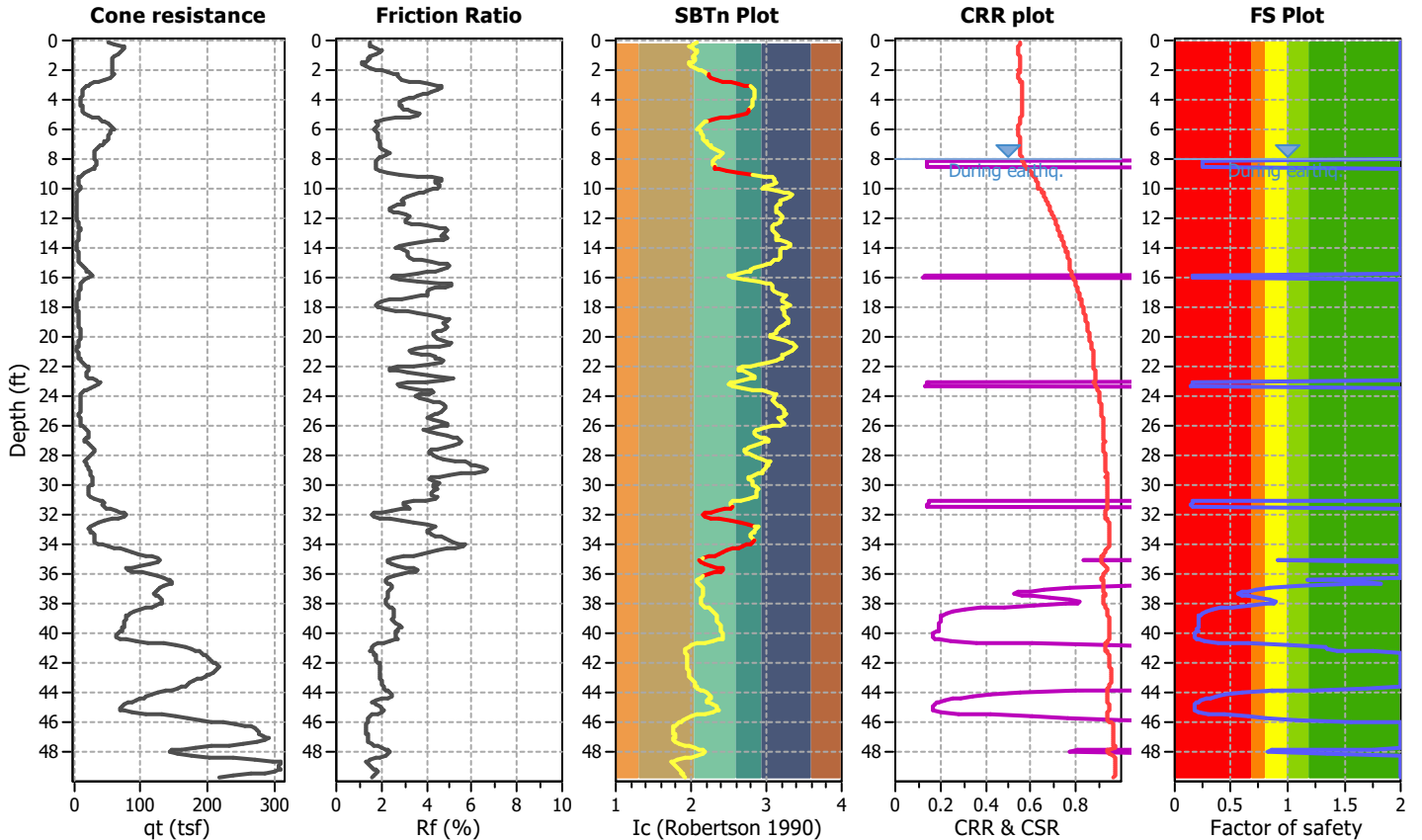
Project title : 21-483 Equestrian Estates

Location : Avenue 64 at Harrison Street, Thermal California

CPT file : CPT-6 B&I 2014

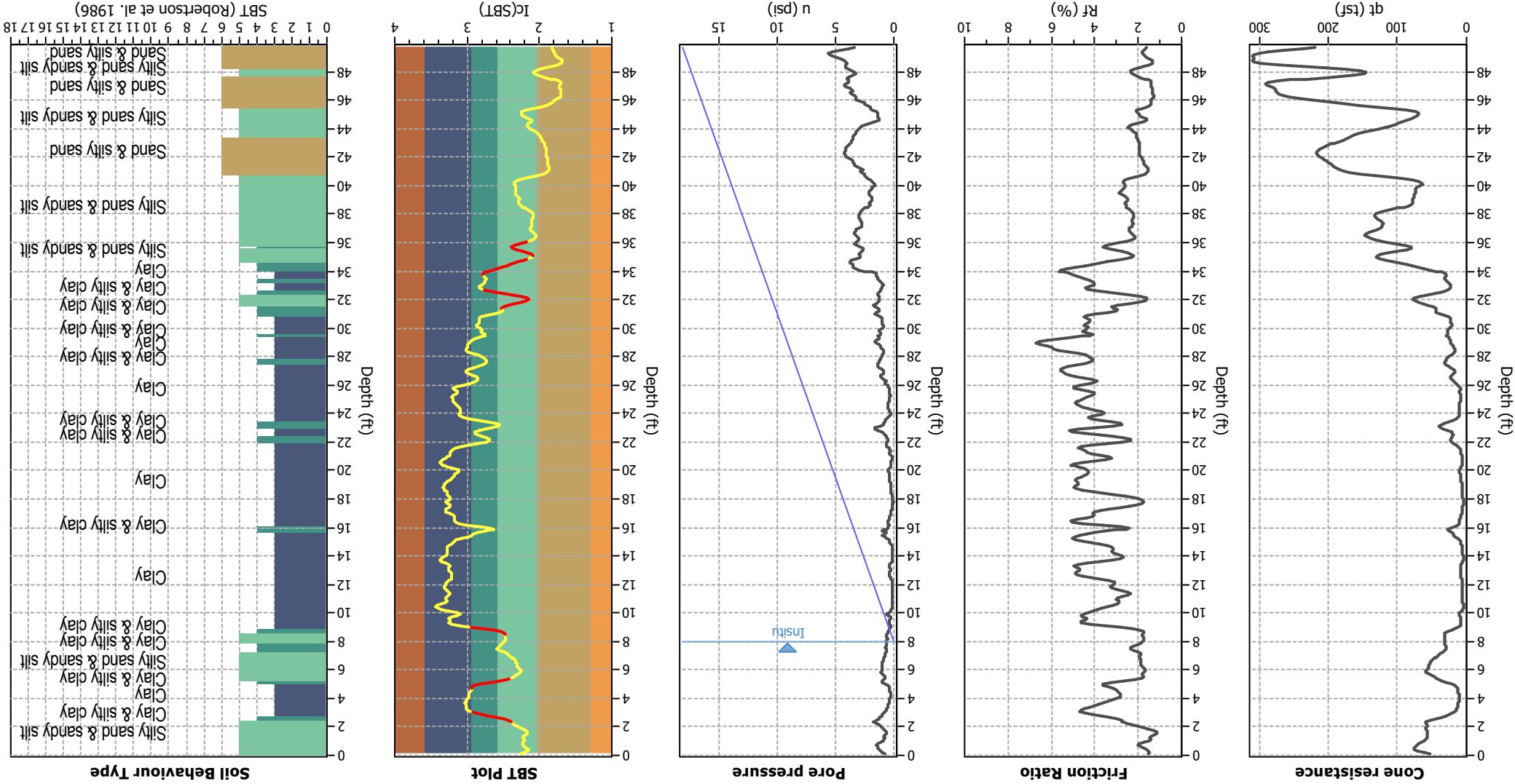
Input parameters and analysis data

Analysis method:	B&I (2014)	G.W.T. (in-situ):	8.00 ft	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	8.00 ft	Fill height:	N/A	Limit depth applied:	No
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth:	N/A
Earthquake magnitude M_w :	7.34	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.74	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		



Zone A1: Cyclic liquefaction likely depending on size and duration of cyclic loading
 Zone A2: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
 Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
 Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

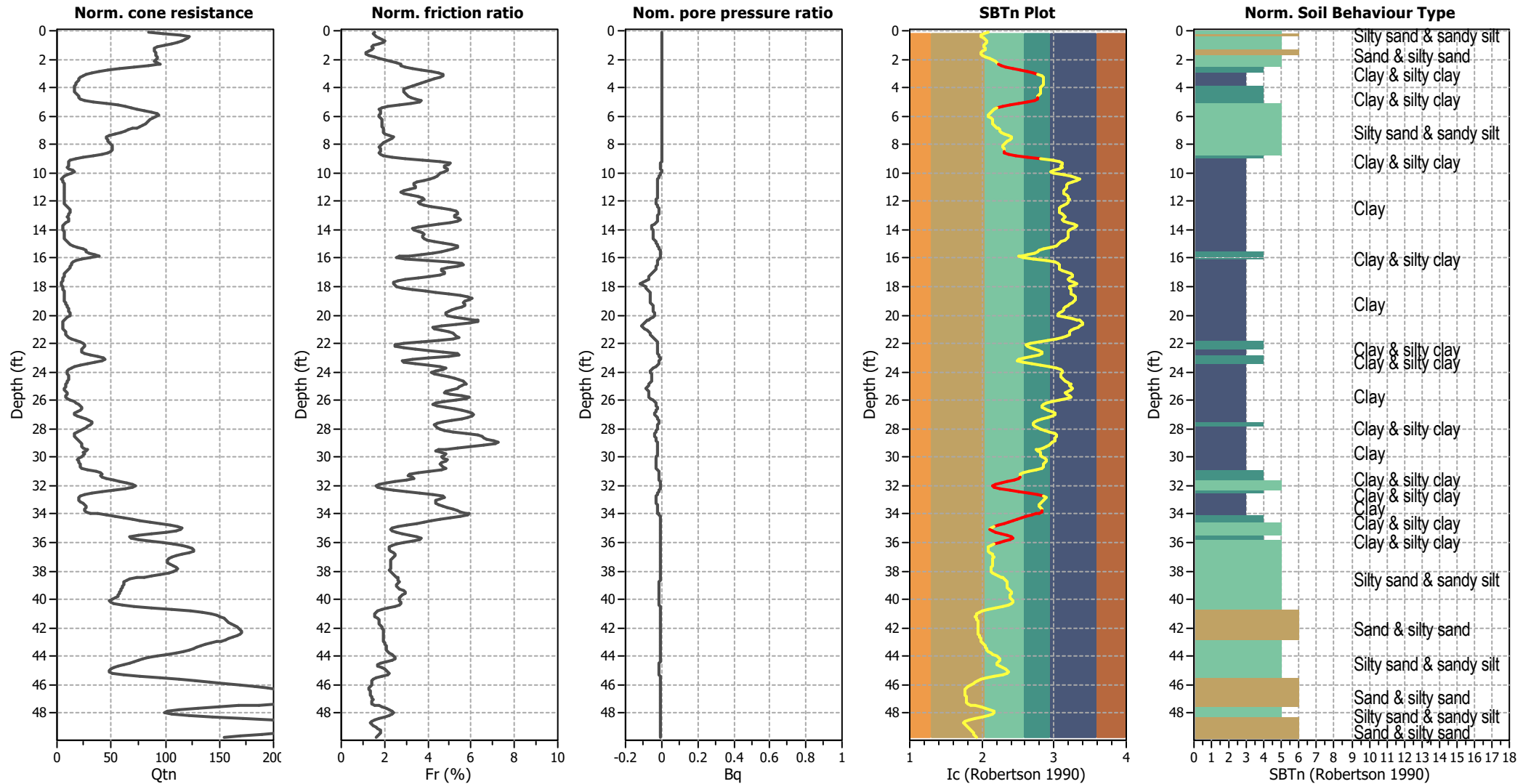
CPT basic interpretation plots



Input parameters and analysis data

Analysis method:	B&I (2014)
Fines correction method:	B&I (2014)
Points to test:	Based on Ic value
Earthquake magnitude M_w :	7.34
Peak ground acceleration:	0.74
Depth to water table (insitu):	8.00 ft
Depth to GWT (earthq.):	8.00 ft
Average results interval:	3
Ic cut-off value:	2.60
Unit weight calculation:	Based on SBT
Use fill:	No
Fill height:	N/A
Fill weight:	N/A
Transition detect. applied:	Yes
K_p applied:	Sands only
Clay like behavior applied:	No
Limit depth applied:	N/A
Limit depth:	N/A

CPT basic interpretation plots (normalized)



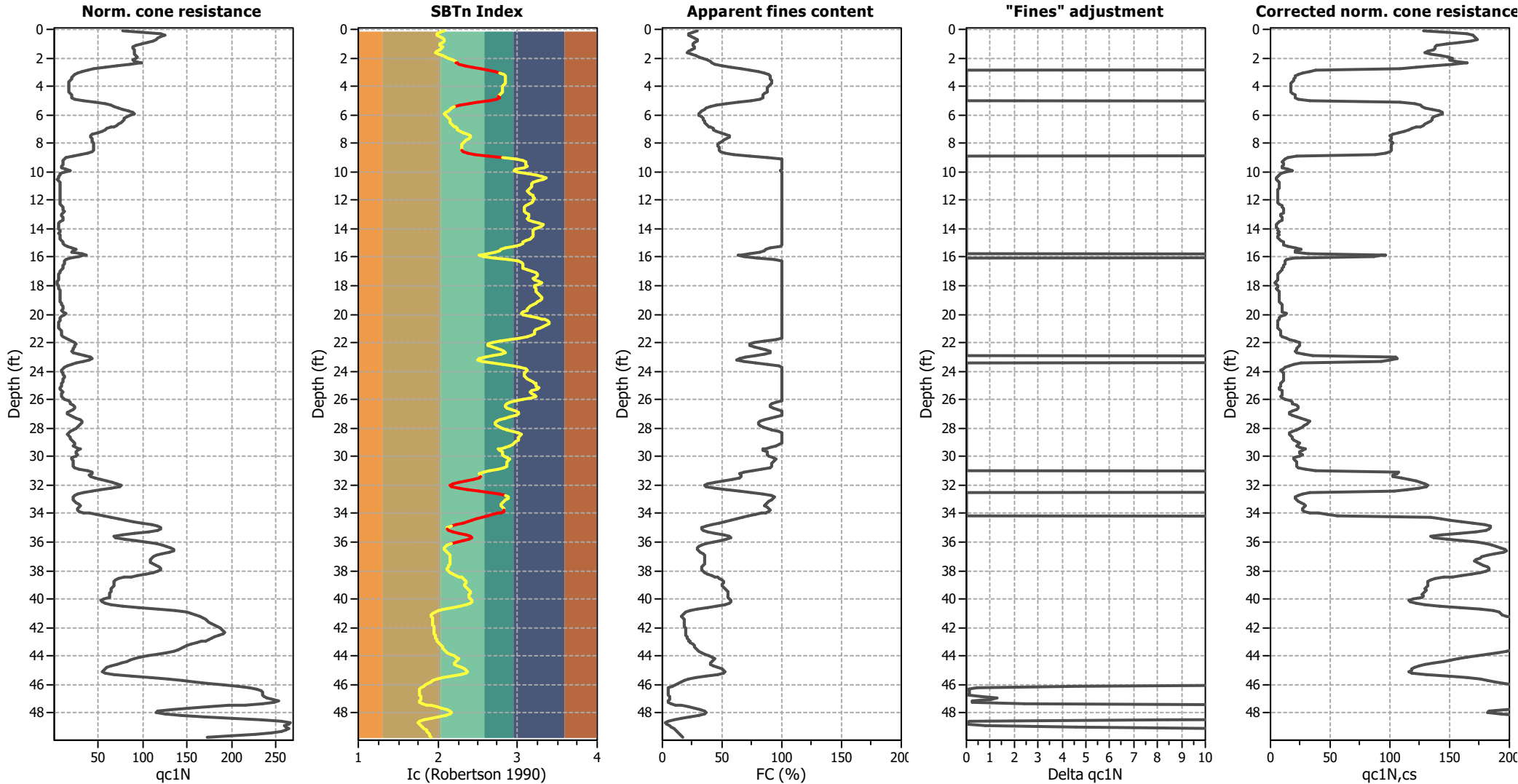
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K ₀ applied:	Yes
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

SBTn legend

1. Sensitive fine grained	4. Clayey silt to silty	7. Gravely sand to sand
2. Organic material	5. Silty sand to sandy silt	8. Very stiff sand to
3. Clay to silty clay	6. Clean sand to silty sand	9. Very stiff fine grained

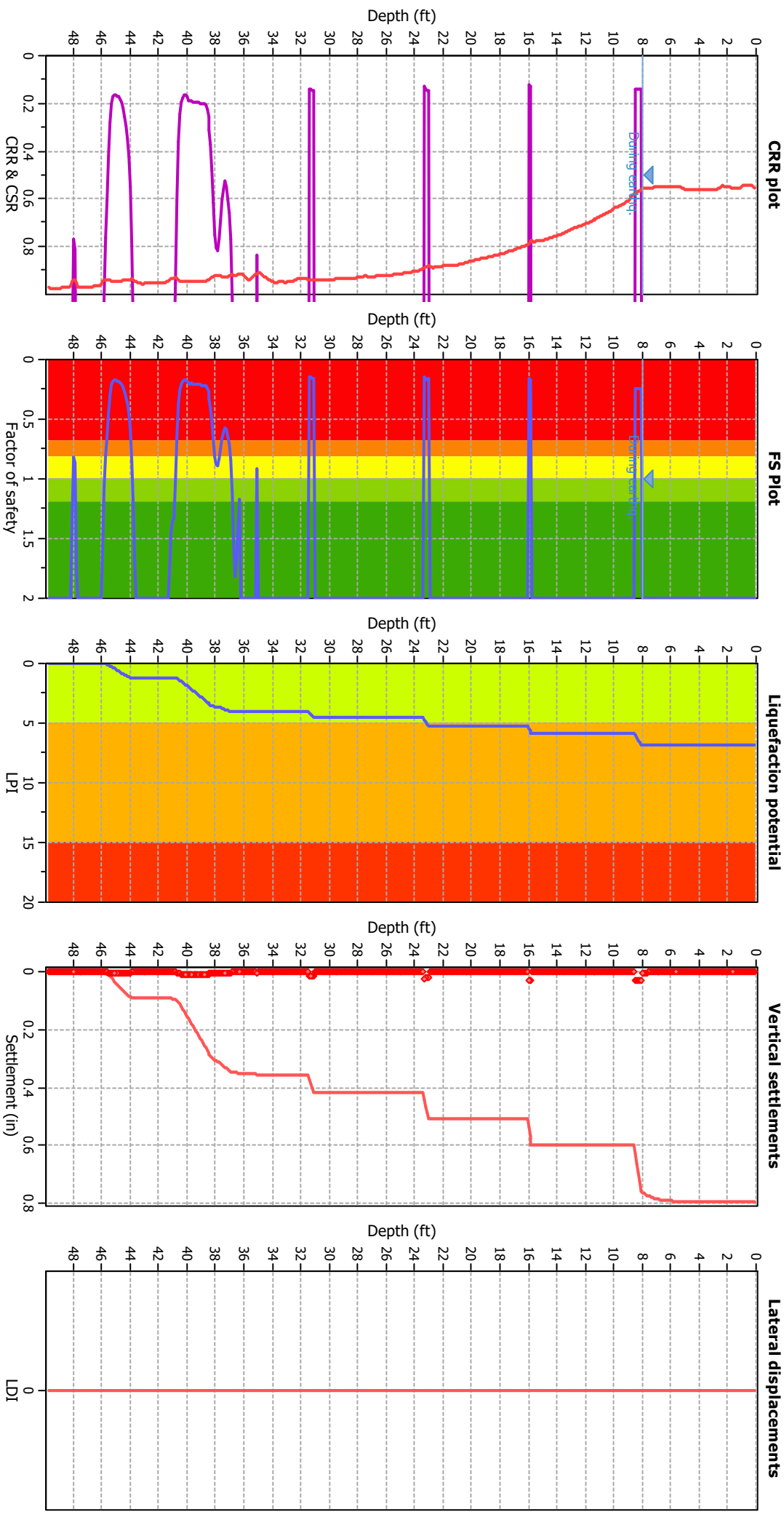
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on I_c value	I_c cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)
Fines correction method:	B&I (2014)
Points to test:	Based on Ic value
Earthquake magnitude M_w :	7.34
Peak ground acceleration:	0.74
Depth to water table (instn):	8.00 ft
Depth to GWT (earthq.):	8.00 ft
Average results interval:	3
Ic cut-off value:	2.60
Unit weight calculation:	Based on SBT
Use fill:	No
Fill height:	N/A
Fill weight:	N/A
Transition detect. applied:	Yes
K_s applied:	Yes
Clay like behavior applied:	Yes
Limit depth applied:	No
Limit depth:	N/A

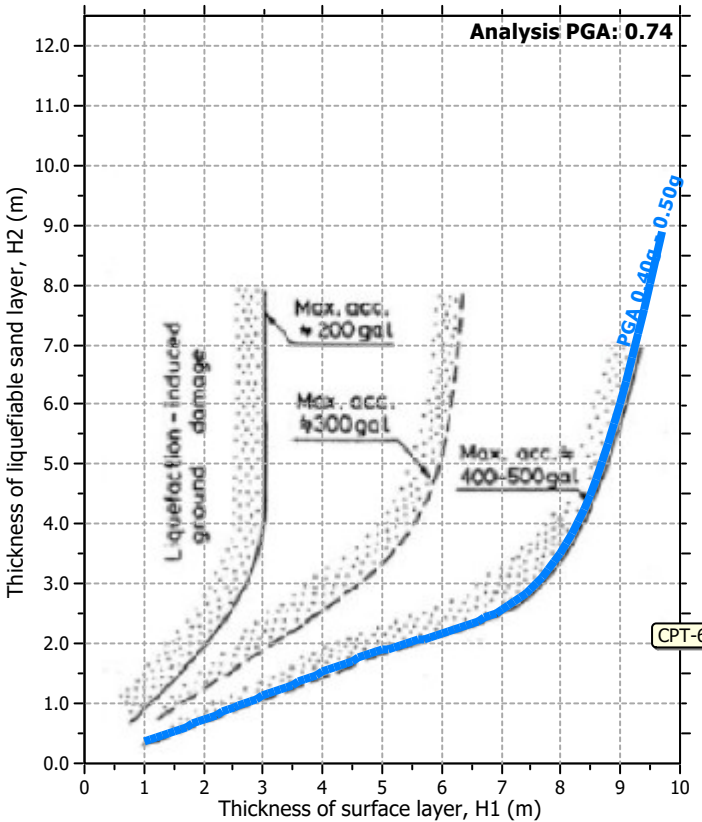
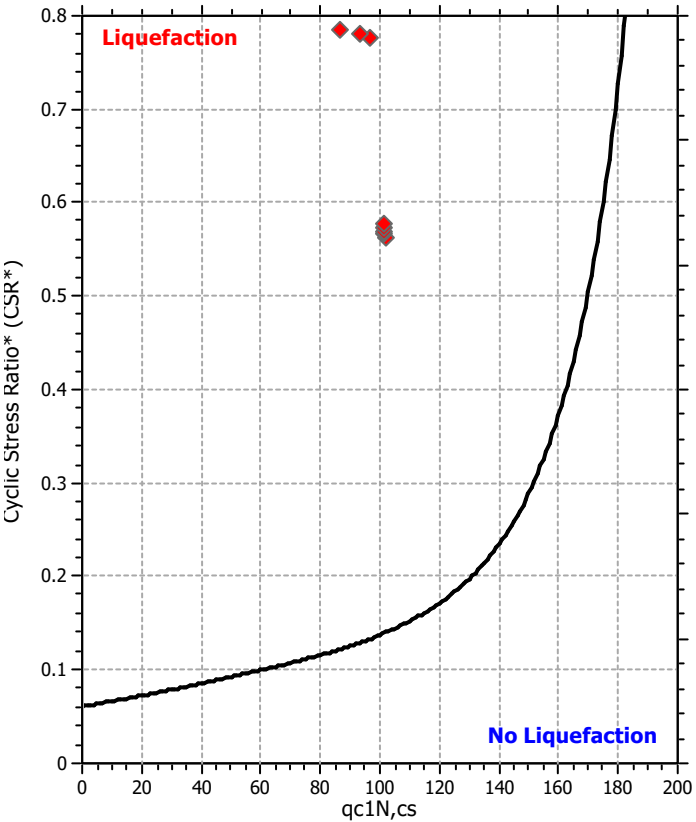
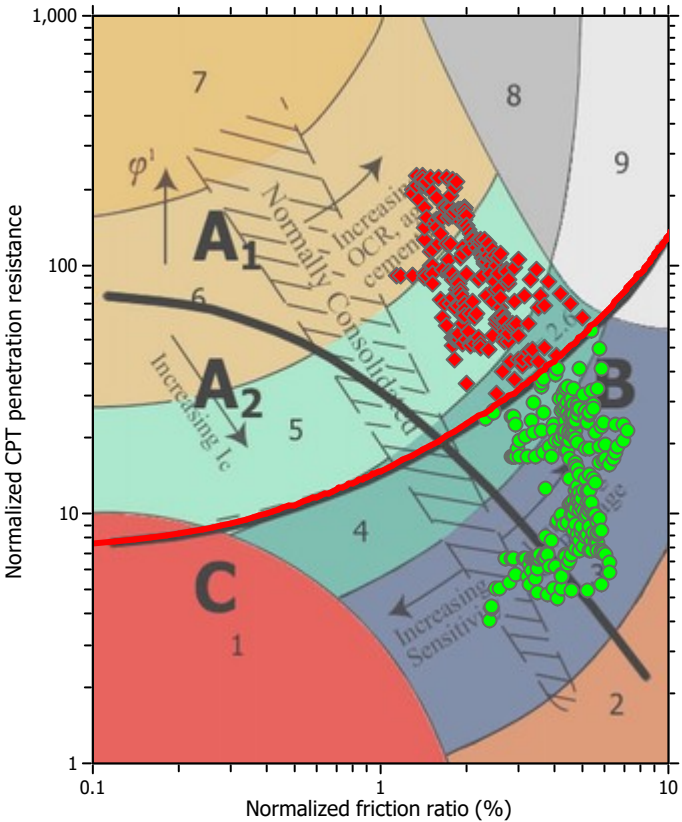
F.S. color scheme

Almost certain it will liquefy
Very likely to liquefy
Liquefaction and no liq. are equally likely
Unlike to liquefy
Almost certain it will not liquefy

LPI color scheme

Very high risk
High risk
Low risk

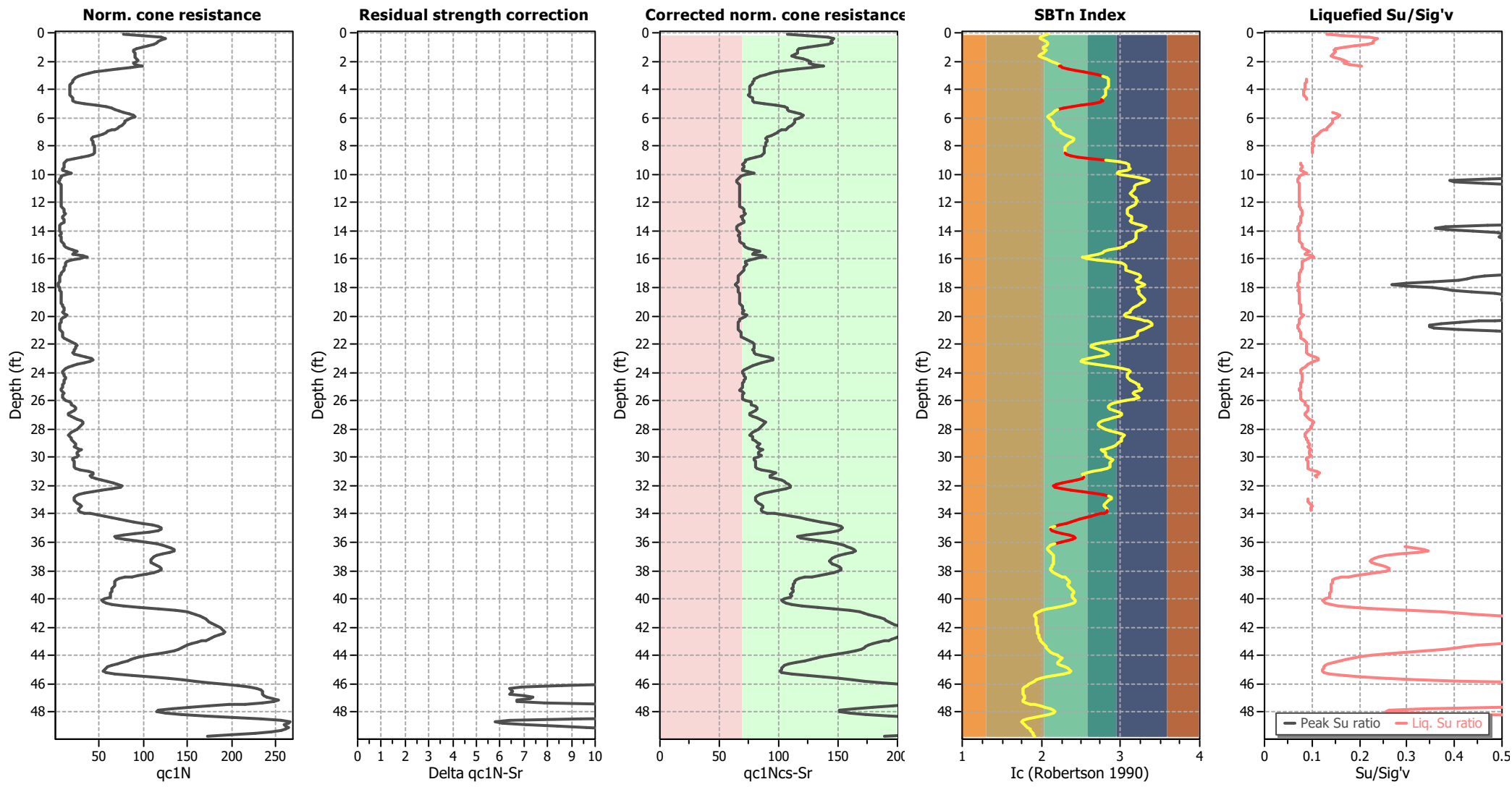
Liquefaction analysis summary plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on I_c value	I_c cut-off value:	2.60	K_{ϕ} applied:	Yes
Earthquake magnitude M_w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

Check for strength loss plots (Idriss & Boulanger (2008))



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _g applied:	Yes
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

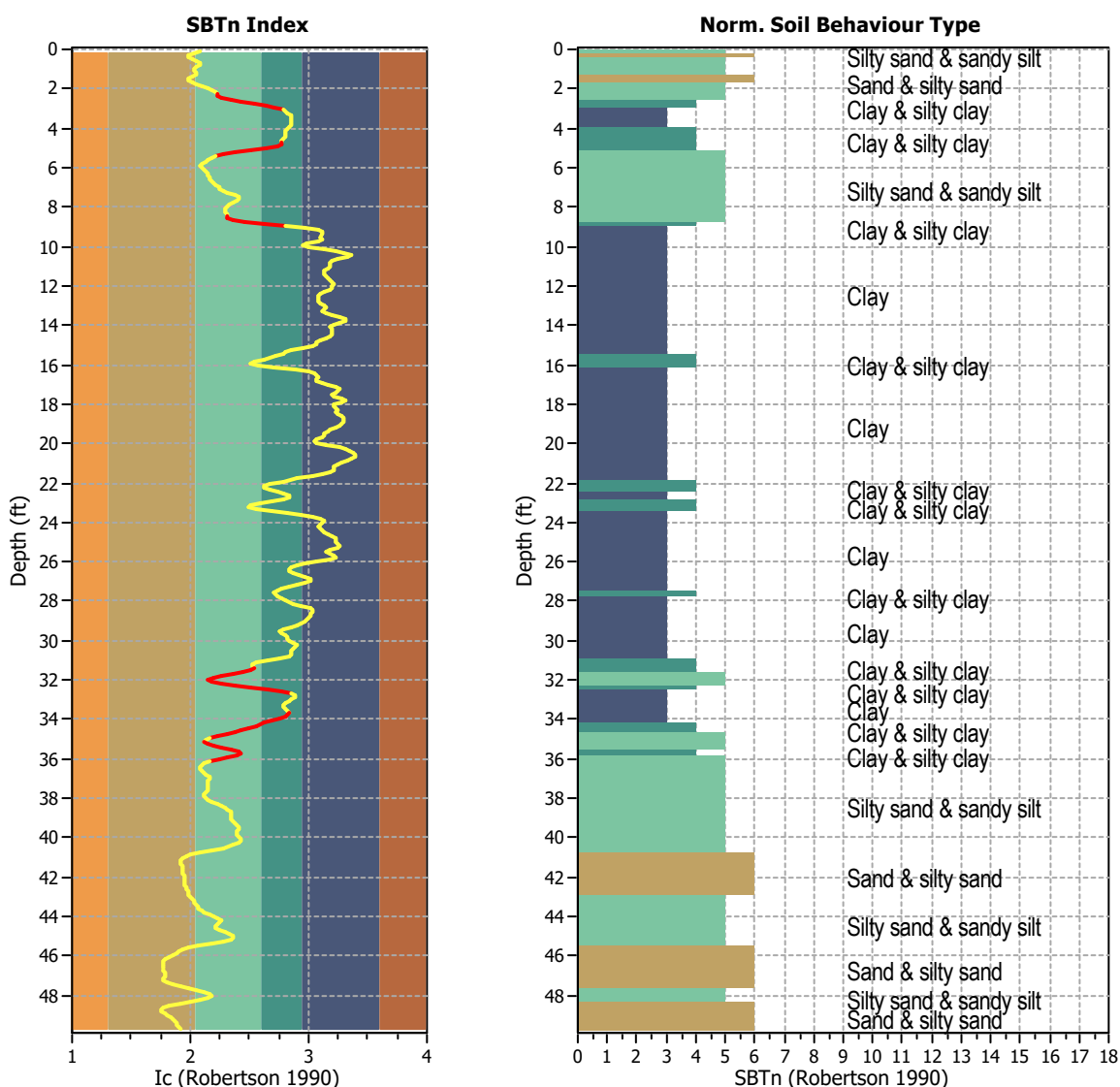
TRANSITION LAYER DETECTION ALGORITHM REPORT

Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vice-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between $1.80 < I_c < 3.0$) and a rate of change of I_c . Transitions typically occur when the rate of change of I_c is fast (i.e. ΔI_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties

I_c minimum check value: 1.70
 I_c maximum check value: 3.00
 I_c change ratio value: 0.0250
 Minimum number of points in layer: 4

General statistics

Total points in CPT file: 497
 Total points excluded: 61
 Exclusion percentage: 12.27%
 Number of layers detected: 8

Transition layer No	Number of points	Depth	SBT _n number	SBT _n description
Transition layer 1	9	Start depth: 2.40 (ft)	5	Silty sand & sandy silt
		End depth: 3.20 (ft)	3	Clay
Transition layer 2	8	Start depth: 4.80 (ft)	4	Clay & silty clay
		End depth: 5.50 (ft)	5	Silty sand & sandy silt
Transition layer 3	6	Start depth: 8.60 (ft)	5	Silty sand & sandy silt
		End depth: 9.10 (ft)	3	Clay
Transition layer 4	6	Start depth: 31.50 (ft)	4	Clay & silty clay
		End depth: 32.00 (ft)	5	Silty sand & sandy silt
Transition layer 5	8	Start depth: 32.10 (ft)	5	Silty sand & sandy silt
		End depth: 32.80 (ft)	3	Clay
Transition layer 6	13	Start depth: 33.80 (ft)	3	Clay
		End depth: 35.00 (ft)	5	Silty sand & sandy silt
Transition layer 7	5	Start depth: 35.20 (ft)	5	Silty sand & sandy silt
		End depth: 35.60 (ft)	4	Clay & silty clay
Transition layer 8	6	Start depth: 35.70 (ft)	4	Clay & silty clay
		End depth: 36.20 (ft)	5	Silty sand & sandy silt

Start depth: Depth where the transition layer begins

End depth: Depth where the transition layer ends

:: Field input data ::						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1	0.10	48.00	0.73	0.73	15.38	118.30
2	0.20	61.60	0.94	0.94	13.81	119.69
3	0.30	74.47	1.09	1.09	12.68	121.26
4	0.40	77.45	1.23	1.23	12.60	122.24
5	0.50	75.25	1.33	1.33	13.43	122.84
6	0.60	72.97	1.41	1.41	14.40	123.23
7	0.70	71.93	1.47	1.47	15.07	123.35
8	0.80	69.82	1.43	1.43	15.04	122.77
9	0.90	65.99	1.13	1.13	14.39	121.37
10	1.00	61.41	0.83	0.83	13.86	119.76
11	1.10	57.01	0.82	0.82	13.87	118.69
12	1.20	55.11	0.80	0.80	14.40	118.57
13	1.30	55.77	0.82	0.82	14.19	118.36
14	1.40	56.73	0.75	0.75	13.40	117.83
15	1.50	56.89	0.62	0.62	12.57	117.09
16	1.60	56.30	0.60	0.60	12.36	116.86
17	1.70	56.47	0.69	0.69	13.25	117.80
18	1.80	57.67	0.88	0.88	14.54	119.16
19	1.90	58.37	1.04	1.04	15.77	120.32
20	2.00	57.87	1.14	1.14	17.11	121.09
21	2.10	54.99	1.24	1.24	18.50	121.89
22	2.20	56.26	1.45	1.45	19.60	122.97
23	2.30	61.09	1.72	1.72	19.96	123.72
24	2.40	60.46	1.67	1.67	20.24	123.66
25	2.50	53.61	1.43	1.43	21.37	122.74
26	2.60	44.47	1.29	1.29	23.88	121.49
27	2.70	35.89	1.19	1.19	27.82	120.24
28	2.80	28.28	1.06	1.06	32.39	119.04
29	2.90	23.56	0.98	0.98	36.98	117.92
30	3.00	20.18	0.92	0.92	41.13	116.86
31	3.10	16.92	0.81	0.81	44.79	115.60
32	3.20	14.43	0.68	0.68	47.53	114.17
33	3.30	13.20	0.59	0.59	48.63	112.97
34	3.40	13.04	0.55	0.55	48.79	112.11
35	3.50	12.44	0.50	0.50	48.75	111.38
36	3.60	11.77	0.45	0.45	49.01	110.47
37	3.70	11.08	0.40	0.40	49.18	109.56
38	3.80	10.67	0.36	0.36	48.94	108.79
39	3.90	10.67	0.34	0.34	48.22	108.20
40	4.00	10.67	0.32	0.32	47.14	107.68
41	4.10	10.67	0.29	0.29	46.43	107.34
42	4.20	10.67	0.30	0.30	46.27	107.25
43	4.30	10.67	0.31	0.31	46.40	107.30
44	4.40	10.67	0.30	0.30	46.16	107.62
45	4.50	11.38	0.33	0.33	45.17	108.37
46	4.60	12.78	0.39	0.39	44.24	109.19
47	4.70	13.04	0.40	0.40	44.00	109.93
48	4.80	13.06	0.43	0.43	44.24	110.82

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
49	4.90	14.39	0.53	0.53	42.43	113.05
50	5.00	20.29	0.78	0.78	37.26	115.72
51	5.10	28.72	0.98	0.98	31.07	117.78
52	5.20	36.26	0.98	0.98	25.74	118.47
53	5.30	40.53	0.85	0.85	21.76	118.10
54	5.40	42.67	0.73	0.73	19.35	117.71
55	5.50	45.50	0.79	0.79	18.16	118.08
56	5.60	49.97	0.91	0.91	17.54	119.16
57	5.70	55.30	1.03	1.03	16.77	120.06
58	5.80	59.04	1.07	1.07	15.91	120.40
59	5.90	59.85	0.99	0.99	15.45	120.25
60	6.00	57.56	0.96	0.96	15.69	119.98
61	6.10	54.43	0.98	0.98	16.39	119.87
62	6.20	53.33	0.98	0.98	17.02	119.90
63	6.30	53.33	1.00	1.00	17.19	119.88
64	6.40	52.98	0.98	0.98	17.30	119.75
65	6.50	51.37	0.94	0.94	17.56	119.49
66	6.60	49.32	0.92	0.92	17.94	119.26
67	6.70	48.55	0.92	0.92	18.38	119.05
68	6.80	46.89	0.89	0.89	18.94	118.76
69	6.90	43.63	0.85	0.85	19.64	118.30
70	7.00	41.13	0.81	0.81	20.32	117.74
71	7.10	39.45	0.75	0.75	20.76	117.16
72	7.20	37.56	0.70	0.70	21.50	116.52
73	7.30	33.78	0.66	0.66	23.09	115.97
74	7.40	29.93	0.66	0.66	25.37	115.67
75	7.50	28.02	0.68	0.68	26.93	115.67
76	7.60	29.00	0.70	0.70	26.92	115.59
77	7.70	29.63	0.64	0.64	25.92	115.30
78	7.80	29.63	0.59	0.59	24.77	114.92
79	7.90	30.77	0.59	0.59	23.76	114.72
80	8.00	32.00	0.58	0.58	22.99	114.66
81	8.10	32.00	0.56	0.56	22.43	114.50
82	8.20	32.00	0.54	0.54	22.38	114.46
83	8.30	32.00	0.57	0.57	22.51	114.55
84	8.40	32.00	0.58	0.58	22.67	114.67
85	8.50	32.00	0.57	0.57	22.77	114.49
86	8.60	30.74	0.54	0.54	23.20	113.89
87	8.70	27.62	0.48	0.48	25.00	112.80
88	8.80	21.58	0.41	0.41	29.16	111.27
89	8.90	14.98	0.36	0.36	36.57	109.31
90	9.00	9.98	0.29	0.29	46.62	107.64
91	9.10	8.13	0.29	0.29	56.71	106.63
92	9.20	7.12	0.31	0.31	63.65	106.49
93	9.30	6.62	0.32	0.32	66.19	106.92
94	9.40	7.57	0.36	0.36	65.99	106.94
95	9.50	7.24	0.31	0.31	65.63	106.50
96	9.60	6.32	0.26	0.26	66.89	105.87

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
97	9.70	6.48	0.29	0.29	64.16	107.40
98	9.80	9.91	0.47	0.47	57.37	110.12
99	9.90	13.34	0.60	0.60	55.42	110.60
100	10.00	8.48	0.35	0.35	58.30	108.82
101	10.10	5.53	0.22	0.22	67.40	104.83
102	10.20	4.96	0.19	0.19	75.80	101.73
103	10.30	3.80	0.14	0.14	80.84	99.76
104	10.40	3.38	0.12	0.12	85.76	97.65
105	10.50	3.18	0.10	0.10	83.19	97.35
106	10.60	4.08	0.12	0.12	77.12	98.02
107	10.70	4.74	0.13	0.13	72.18	99.01
108	10.80	4.74	0.14	0.14	70.86	99.60
109	10.90	4.74	0.15	0.15	71.42	99.80
110	11.00	4.74	0.14	0.14	71.27	99.72
111	11.10	4.74	0.13	0.13	69.96	99.17
112	11.20	4.74	0.12	0.12	68.35	98.48
113	11.30	4.74	0.11	0.11	67.39	98.05
114	11.40	4.74	0.11	0.11	67.44	98.04
115	11.50	4.74	0.12	0.12	68.52	98.48
116	11.60	4.74	0.13	0.13	70.29	99.19
117	11.70	4.74	0.15	0.15	72.08	99.89
118	11.80	4.74	0.16	0.16	73.33	100.35
119	11.90	4.74	0.16	0.16	73.55	100.41
120	12.00	4.74	0.15	0.15	73.05	100.20
121	12.10	4.74	0.14	0.14	72.54	99.98
122	12.20	4.74	0.14	0.14	71.18	100.46
123	12.30	5.38	0.17	0.17	68.03	102.32
124	12.40	6.88	0.25	0.25	65.55	104.55
125	12.50	7.40	0.31	0.31	64.13	106.55
126	12.60	7.89	0.37	0.37	64.16	107.83
127	12.70	8.30	0.40	0.40	63.90	108.69
128	12.80	8.54	0.43	0.43	64.02	108.93
129	12.90	8.15	0.40	0.40	65.87	108.12
130	13.00	6.54	0.30	0.30	67.91	107.05
131	13.10	6.60	0.30	0.30	69.03	106.64
132	13.20	7.35	0.36	0.36	68.18	107.40
133	13.30	7.63	0.39	0.39	67.06	108.01
134	13.40	7.70	0.37	0.37	68.44	107.11
135	13.50	5.87	0.25	0.25	72.31	104.73
136	13.60	4.22	0.15	0.15	78.51	101.22
137	13.70	3.75	0.12	0.12	82.25	98.39
138	13.80	3.71	0.10	0.10	81.47	97.07
139	13.90	3.78	0.10	0.10	77.78	97.26
140	14.00	4.48	0.12	0.12	74.31	98.54
141	14.10	5.03	0.15	0.15	72.11	100.05
142	14.20	5.14	0.17	0.17	72.49	100.61
143	14.30	4.75	0.15	0.15	72.61	100.80
144	14.40	5.14	0.16	0.16	72.76	100.64

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
145	14.50	5.01	0.16	0.16	72.24	100.72
146	14.60	4.94	0.16	0.16	71.68	101.11
147	14.70	5.54	0.18	0.18	69.43	102.50
148	14.80	6.60	0.24	0.24	65.57	104.99
149	14.90	8.26	0.34	0.34	63.32	107.13
150	15.00	8.62	0.40	0.40	62.48	108.66
151	15.10	8.79	0.43	0.43	60.44	110.31
152	15.20	11.54	0.58	0.58	55.16	112.72
153	15.30	16.02	0.81	0.81	48.79	115.30
154	15.40	20.58	0.97	0.97	46.04	115.97
155	15.50	16.90	0.72	0.72	44.89	115.63
156	15.60	16.68	0.68	0.68	41.88	115.90
157	15.70	25.96	0.99	0.99	36.89	116.92
158	15.80	29.72	0.91	0.91	32.60	117.11
159	15.90	27.63	0.63	0.63	31.23	115.53
160	16.00	22.70	0.52	0.52	33.70	113.21
161	16.10	15.31	0.45	0.45	40.86	111.35
162	16.20	10.66	0.40	0.40	51.17	110.14
163	16.30	9.56	0.44	0.44	58.87	110.26
164	16.40	10.25	0.54	0.54	61.83	110.78
165	16.50	9.81	0.52	0.52	63.23	110.52
166	16.60	8.49	0.41	0.41	63.61	109.54
167	16.70	8.79	0.38	0.38	63.50	108.28
168	16.80	8.31	0.33	0.33	63.56	107.51
169	16.90	7.60	0.31	0.31	66.50	106.40
170	17.00	6.40	0.26	0.26	70.66	105.27
171	17.10	5.80	0.23	0.23	75.45	103.78
172	17.20	5.02	0.19	0.19	77.40	102.49
173	17.30	5.05	0.17	0.17	76.90	101.22
174	17.40	5.14	0.15	0.15	74.78	99.90
175	17.50	4.74	0.11	0.11	72.88	98.29
176	17.60	4.60	0.09	0.09	74.47	96.01
177	17.70	3.67	0.06	0.06	78.67	93.98
178	17.80	3.16	0.05	0.05	82.07	92.94
179	17.90	3.73	0.07	0.07	78.63	94.13
180	18.00	4.65	0.09	0.09	74.21	95.91
181	18.10	4.74	0.10	0.10	74.22	97.27
182	18.20	4.42	0.11	0.11	75.58	98.86
183	18.30	5.23	0.16	0.16	75.97	100.99
184	18.40	5.93	0.21	0.21	75.30	102.94
185	18.50	5.93	0.24	0.24	76.46	104.26
186	18.60	5.93	0.27	0.27	78.72	105.00
187	18.70	5.93	0.29	0.29	80.29	105.49
188	18.80	5.93	0.30	0.30	80.98	105.67
189	18.90	5.93	0.29	0.29	80.77	105.55
190	19.00	5.93	0.28	0.28	79.48	105.52
191	19.10	6.28	0.29	0.29	77.42	106.06
192	19.20	6.98	0.34	0.34	74.94	107.10

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
193	19.30	7.66	0.39	0.39	72.01	108.05
194	19.40	8.30	0.40	0.40	69.82	108.49
195	19.50	8.36	0.39	0.39	67.85	108.65
196	19.60	8.72	0.40	0.40	67.54	108.27
197	19.70	8.03	0.34	0.34	66.95	108.07
198	19.80	8.44	0.36	0.36	63.58	108.99
199	19.90	11.48	0.50	0.50	61.49	109.77
200	20.00	10.27	0.44	0.44	62.66	109.68
201	20.10	7.73	0.35	0.35	69.22	108.01
202	20.20	6.35	0.30	0.30	77.36	106.47
203	20.30	5.93	0.29	0.29	82.23	105.90
204	20.40	5.93	0.31	0.31	85.01	105.56
205	20.50	5.44	0.28	0.28	87.78	104.75
206	20.60	4.76	0.22	0.22	89.54	103.39
207	20.70	4.74	0.19	0.19	89.02	101.95
208	20.80	4.74	0.16	0.16	86.39	100.97
209	20.90	4.74	0.15	0.15	83.75	100.62
210	21.00	5.09	0.16	0.16	79.70	101.94
211	21.10	6.42	0.24	0.24	76.22	104.23
212	21.20	7.30	0.31	0.31	74.32	105.90
213	21.30	7.11	0.32	0.32	74.08	106.59
214	21.40	7.18	0.31	0.31	73.89	106.84
215	21.50	7.64	0.34	0.34	71.78	107.83
216	21.60	8.93	0.43	0.43	67.12	109.81
217	21.70	11.60	0.57	0.57	60.52	111.77
218	21.80	14.38	0.63	0.63	52.39	113.32
219	21.90	18.47	0.65	0.65	45.03	113.81
220	22.00	21.26	0.57	0.57	39.27	113.47
221	22.10	22.05	0.47	0.47	36.35	112.86
222	22.20	21.76	0.49	0.49	36.60	112.80
223	22.30	20.70	0.56	0.56	39.18	113.38
224	22.40	19.46	0.62	0.62	42.37	114.18
225	22.50	19.26	0.71	0.71	45.51	115.09
226	22.60	18.96	0.83	0.83	48.09	116.37
227	22.70	19.87	1.02	1.02	48.36	118.34
228	22.80	25.44	1.40	1.40	45.11	120.38
229	22.90	32.47	1.61	1.61	39.92	121.84
230	23.00	38.55	1.57	1.57	34.79	121.83
231	23.10	40.24	1.18	1.18	31.29	120.58
232	23.20	36.60	0.88	0.88	30.57	118.82
233	23.30	30.45	0.86	0.86	33.50	117.35
234	23.40	23.72	0.78	0.78	39.59	116.23
235	23.50	18.02	0.70	0.70	46.84	114.82
236	23.60	14.35	0.62	0.62	54.31	113.24
237	23.70	11.59	0.52	0.52	60.70	111.36
238	23.80	9.50	0.38	0.38	65.44	109.12
239	23.90	8.27	0.30	0.30	67.21	107.29
240	24.00	8.50	0.29	0.29	66.14	107.12

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
241	24.10	9.83	0.36	0.36	64.93	108.05
242	24.20	10.03	0.40	0.40	64.35	109.33
243	24.30	10.55	0.46	0.46	65.05	110.15
244	24.40	10.67	0.49	0.49	66.18	110.56
245	24.50	10.07	0.48	0.48	67.70	110.58
246	24.60	9.83	0.48	0.48	70.13	110.18
247	24.70	8.95	0.44	0.44	72.58	109.63
248	24.80	8.30	0.41	0.41	74.70	109.03
249	24.90	8.30	0.40	0.40	75.36	108.64
250	25.00	8.30	0.38	0.38	74.89	108.42
251	25.10	8.28	0.37	0.37	76.18	107.75
252	25.20	7.16	0.31	0.31	78.16	106.92
253	25.30	6.83	0.29	0.29	76.25	106.90
254	25.40	8.94	0.36	0.36	71.90	107.60
255	25.50	9.55	0.38	0.38	69.47	108.33
256	25.60	8.76	0.37	0.37	70.97	108.61
257	25.70	8.65	0.40	0.40	74.43	108.79
258	25.80	8.36	0.42	0.42	75.22	109.41
259	25.90	9.20	0.47	0.47	71.56	110.48
260	26.00	11.64	0.56	0.56	63.37	112.26
261	26.10	15.73	0.69	0.69	56.40	113.64
262	26.20	17.30	0.69	0.69	51.91	114.38
263	26.30	17.85	0.67	0.67	49.38	115.05
264	26.40	20.56	0.82	0.82	48.27	116.28
265	26.50	22.52	1.01	1.01	48.38	117.65
266	26.60	22.30	1.11	1.11	49.93	118.29
267	26.70	20.60	1.08	1.08	52.80	117.89
268	26.80	17.36	0.92	0.92	56.32	116.95
269	26.90	15.53	0.85	0.85	59.44	116.13
270	27.00	15.44	0.87	0.87	59.65	116.31
271	27.10	17.71	0.99	0.99	56.70	117.47
272	27.20	21.67	1.19	1.19	52.52	118.93
273	27.30	25.17	1.34	1.34	48.29	120.18
274	27.40	29.08	1.42	1.42	44.62	120.86
275	27.50	31.73	1.40	1.40	42.14	120.88
276	27.60	30.84	1.27	1.27	41.14	120.48
277	27.70	29.52	1.20	1.20	41.55	119.92
278	27.80	28.15	1.16	1.16	42.61	119.51
279	27.90	26.75	1.13	1.13	44.09	119.05
280	28.00	24.61	1.05	1.05	46.30	118.33
281	28.10	21.36	0.94	0.94	49.72	117.33
282	28.20	17.96	0.85	0.85	54.41	116.41
283	28.30	15.97	0.84	0.84	59.14	116.07
284	28.40	15.64	0.91	0.91	61.26	116.54
285	28.50	17.25	1.03	1.03	60.76	117.26
286	28.60	18.37	1.09	1.09	59.76	117.87
287	28.70	18.37	1.12	1.12	59.16	118.56
288	28.80	19.95	1.29	1.29	58.77	119.55

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
289	28.90	21.95	1.51	1.51	57.34	120.60
290	29.00	23.79	1.59	1.59	55.79	121.04
291	29.10	23.76	1.48	1.48	54.29	120.60
292	29.20	22.52	1.23	1.23	52.14	120.04
293	29.30	24.90	1.25	1.25	48.72	119.96
294	29.40	29.06	1.34	1.34	45.31	120.13
295	29.50	29.63	1.21	1.21	43.63	119.84
296	29.60	27.10	1.08	1.08	44.10	119.16
297	29.70	25.19	1.08	1.08	46.24	119.01
298	29.80	25.05	1.20	1.20	46.99	119.41
299	29.90	27.52	1.26	1.26	46.71	119.26
300	30.00	25.20	1.00	1.00	47.64	118.48
301	30.10	20.43	0.91	0.91	49.98	117.42
302	30.20	20.20	0.93	0.93	52.05	117.16
303	30.30	21.55	0.96	0.96	51.10	117.38
304	30.40	22.52	0.97	0.97	49.84	117.51
305	30.50	22.52	0.95	0.95	49.35	117.55
306	30.60	22.52	0.96	0.96	49.43	117.56
307	30.70	22.52	0.97	0.97	49.55	117.92
308	30.80	23.73	1.08	1.08	47.97	119.09
309	30.90	29.55	1.36	1.36	43.52	120.81
310	31.00	39.02	1.60	1.60	37.95	122.09
311	31.10	45.58	1.53	1.53	33.67	122.26
312	31.20	45.25	1.28	1.28	31.72	121.61
313	31.30	41.98	1.19	1.19	31.97	121.31
314	31.40	42.63	1.40	1.40	32.50	122.03
315	31.50	48.49	1.64	1.64	31.29	123.08
316	31.60	55.32	1.69	1.69	28.22	123.58
317	31.70	62.06	1.52	1.52	24.52	123.36
318	31.80	68.38	1.32	1.32	21.17	122.90
319	31.90	74.66	1.28	1.28	18.64	122.50
320	32.00	79.14	1.20	1.20	17.52	122.32
321	32.10	77.33	1.19	1.19	18.16	122.29
322	32.20	68.13	1.29	1.29	20.94	122.37
323	32.30	56.33	1.37	1.37	25.61	122.23
324	32.40	44.71	1.35	1.35	31.36	121.56
325	32.50	34.78	1.22	1.22	37.74	120.61
326	32.60	28.44	1.17	1.17	44.05	119.62
327	32.70	24.30	1.11	1.11	48.85	118.81
328	32.80	22.52	1.01	1.01	50.97	118.09
329	32.90	22.52	0.94	0.94	50.64	117.57
330	33.00	23.07	0.92	0.92	49.20	117.60
331	33.10	24.87	0.99	0.99	47.74	118.14
332	33.20	26.95	1.10	1.10	46.30	119.08
333	33.30	29.54	1.24	1.24	45.27	120.07
334	33.40	31.36	1.37	1.37	45.20	120.77
335	33.50	30.55	1.41	1.41	46.14	121.11
336	33.60	29.39	1.44	1.44	47.52	121.20

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
337	33.70	29.04	1.46	1.46	48.20	121.42
338	33.80	30.40	1.55	1.55	47.52	122.28
339	33.90	35.17	1.89	1.89	45.73	124.00
340	34.00	42.93	2.48	2.48	43.06	126.02
341	34.10	51.69	2.99	2.99	39.78	127.71
342	34.20	60.90	3.26	3.26	36.31	128.90
343	34.30	70.42	3.47	3.47	33.02	129.61
344	34.40	78.27	3.50	3.50	30.07	130.06
345	34.50	86.70	3.49	3.49	27.59	130.46
346	34.60	95.97	3.69	3.69	25.22	130.85
347	34.70	106.75	3.71	3.71	22.83	131.15
348	34.80	118.46	3.57	3.57	20.17	131.01
349	34.90	126.90	3.15	3.15	17.90	130.58
350	35.00	130.93	2.89	2.89	16.53	130.12
351	35.10	130.59	2.90	2.90	16.33	129.94
352	35.20	126.40	2.93	2.93	17.07	129.79
353	35.30	115.74	2.84	2.84	18.67	129.45
354	35.40	99.53	2.74	2.74	21.13	128.86
355	35.50	84.44	2.62	2.62	24.33	128.34
356	35.60	74.88	2.65	2.65	26.85	128.18
357	35.70	76.49	2.82	2.82	27.39	128.63
358	35.80	86.83	3.10	3.10	25.82	129.46
359	35.90	100.50	3.36	3.36	23.19	130.15
360	36.00	114.24	3.29	3.29	20.41	130.42
361	36.10	125.42	3.08	3.08	18.04	130.38
362	36.20	134.03	3.02	3.02	16.43	130.33
363	36.30	139.79	3.01	3.01	15.56	130.45
364	36.40	144.62	3.09	3.09	15.22	130.70
365	36.50	147.54	3.24	3.24	15.25	131.01
366	36.60	147.82	3.36	3.36	15.60	131.21
367	36.70	143.26	3.37	3.37	16.22	131.17
368	36.80	134.87	3.28	3.28	16.99	130.92
369	36.90	127.95	3.18	3.18	17.57	130.52
370	37.00	124.31	2.99	2.99	17.67	130.05
371	37.10	122.73	2.78	2.78	17.51	129.61
372	37.20	120.81	2.71	2.71	17.39	129.31
373	37.30	119.96	2.69	2.69	17.40	129.25
374	37.40	121.58	2.73	2.73	17.40	129.39
375	37.50	124.03	2.83	2.83	17.27	129.63
376	37.60	127.71	2.90	2.90	17.02	129.87
377	37.70	131.28	2.93	2.93	16.69	130.01
378	37.80	133.34	2.94	2.94	16.48	130.08
379	37.90	133.15	2.95	2.95	16.48	130.05
380	38.00	130.81	2.90	2.90	16.81	129.90
381	38.10	124.70	2.83	2.83	17.48	129.62
382	38.20	116.16	2.74	2.74	18.51	129.19
383	38.30	106.68	2.60	2.60	19.82	128.73
384	38.40	98.47	2.53	2.53	21.09	128.10

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
385	38.50	89.98	2.30	2.30	22.20	127.35
386	38.60	83.06	2.07	2.07	23.07	126.58
387	38.70	78.95	2.00	2.00	23.91	126.18
388	38.80	77.26	2.06	2.06	24.39	126.01
389	38.90	77.04	1.97	1.97	24.35	125.82
390	39.00	77.04	1.86	1.86	24.10	125.63
391	39.10	76.97	1.91	1.91	24.08	125.49
392	39.20	75.61	1.88	1.88	24.52	125.56
393	39.30	74.67	1.93	1.93	25.21	125.77
394	39.40	74.67	2.10	2.10	25.95	126.08
395	39.50	74.23	2.15	2.15	26.53	126.27
396	39.60	73.01	2.11	2.11	26.61	126.11
397	39.70	72.31	1.99	1.99	26.30	125.81
398	39.80	72.98	1.91	1.91	26.06	125.57
399	39.90	71.88	1.92	1.92	26.19	125.05
400	40.00	65.45	1.65	1.65	26.86	124.49
401	40.10	62.30	1.59	1.59	27.62	124.11
402	40.20	63.23	1.73	1.73	27.82	124.40
403	40.30	67.48	1.83	1.83	26.92	125.08
404	40.40	75.72	1.97	1.97	24.89	126.01
405	40.50	89.55	2.24	2.24	21.86	127.10
406	40.60	110.40	2.42	2.42	18.37	128.10
407	40.70	134.32	2.47	2.47	15.16	128.83
408	40.80	155.86	2.52	2.52	13.02	129.45
409	40.90	169.99	2.71	2.71	11.92	130.01
410	41.00	177.44	2.84	2.84	11.22	130.26
411	41.10	182.86	2.66	2.66	10.86	130.49
412	41.20	187.98	2.88	2.88	10.76	130.82
413	41.30	192.20	3.15	3.15	11.03	131.41
414	41.40	195.09	3.32	3.32	11.28	131.86
415	41.50	196.62	3.43	3.43	11.37	132.13
416	41.60	199.14	3.48	3.48	11.38	132.31
417	41.70	201.91	3.53	3.53	11.34	132.50
418	41.80	205.54	3.65	3.65	11.36	132.77
419	41.90	209.45	3.82	3.82	11.49	133.16
420	42.00	212.56	4.05	4.05	11.63	133.51
421	42.10	215.33	4.16	4.16	11.71	133.75
422	42.20	216.86	4.19	4.19	11.70	133.86
423	42.30	218.08	4.20	4.20	11.65	133.86
424	42.40	217.20	4.14	4.14	11.71	133.79
425	42.50	212.51	4.09	4.09	11.91	133.67
426	42.60	207.25	4.08	4.08	12.17	133.52
427	42.70	203.31	3.98	3.98	12.35	133.33
428	42.80	199.90	3.86	3.86	12.44	133.11
429	42.90	196.55	3.79	3.79	12.58	132.89
430	43.00	191.59	3.71	3.71	12.84	132.68
431	43.10	185.34	3.63	3.63	13.20	132.45
432	43.20	179.02	3.56	3.56	13.64	132.25

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
433	43.30	173.58	3.53	3.53	14.07	132.09
434	43.40	169.82	3.51	3.51	14.41	131.96
435	43.50	167.09	3.46	3.46	14.66	131.81
436	43.60	163.43	3.38	3.38	14.95	131.57
437	43.70	156.70	3.27	3.27	15.53	131.32
438	43.80	147.72	3.24	3.24	16.42	130.99
439	43.90	137.11	3.13	3.13	17.61	130.58
440	44.00	125.53	2.98	2.98	18.94	130.11
441	44.10	115.81	2.90	2.90	20.16	129.57
442	44.20	108.59	2.71	2.71	20.91	128.89
443	44.30	102.86	2.40	2.40	20.82	127.87
444	44.40	98.43	1.98	1.98	20.10	126.45
445	44.50	92.79	1.56	1.56	19.31	124.82
446	44.60	86.06	1.30	1.30	19.32	123.48
447	44.70	79.25	1.27	1.27	20.52	122.91
448	44.80	73.95	1.35	1.35	22.35	122.93
449	44.90	70.90	1.40	1.40	23.75	122.98
450	45.00	69.30	1.36	1.36	24.55	122.90
451	45.10	67.51	1.34	1.34	24.98	123.10
452	45.20	70.37	1.52	1.52	24.45	124.01
453	45.30	83.69	1.81	1.81	21.99	125.42
454	45.40	106.72	2.03	2.03	18.24	126.62
455	45.50	131.24	2.05	2.05	14.85	127.57
456	45.60	154.31	2.20	2.20	12.64	128.44
457	45.70	172.39	2.47	2.47	11.30	129.25
458	45.80	187.52	2.55	2.55	10.57	130.18
459	45.90	204.73	2.92	2.92	9.94	131.08
460	46.00	225.13	3.26	3.26	9.23	131.85
461	46.10	243.98	3.24	3.24	8.43	132.32
462	46.20	258.17	3.29	3.29	7.70	132.52
463	46.30	268.40	3.33	3.33	7.46	132.87
464	46.40	273.76	3.61	3.61	7.51	133.27
465	46.50	275.88	3.78	3.78	7.51	133.42
466	46.60	276.15	3.51	3.51	7.49	133.43
467	46.70	276.20	3.62	3.62	7.45	133.42
468	46.80	277.65	3.76	3.76	7.77	133.82
469	46.90	280.95	4.11	4.11	7.94	134.22
470	47.00	288.52	4.20	4.20	7.89	134.48
471	47.10	294.68	4.10	4.10	7.61	134.38
472	47.20	291.06	3.90	3.90	7.61	134.13
473	47.30	275.60	3.86	3.86	8.14	133.90
474	47.40	254.91	3.91	3.91	9.25	133.76
475	47.50	232.39	3.97	3.97	10.75	133.58
476	47.60	207.07	3.94	3.94	12.46	133.20
477	47.70	182.30	3.74	3.74	14.33	132.62
478	47.80	159.89	3.52	3.52	16.18	131.87
479	47.90	141.67	3.28	3.28	17.68	131.35
480	48.00	139.40	3.33	3.33	18.16	131.36

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
481	48.10	151.90	3.59	3.59	17.32	131.88
482	48.20	171.46	3.81	3.81	15.50	132.67
483	48.30	201.25	4.06	4.06	13.14	133.38
484	48.40	238.19	4.14	4.14	10.72	133.95
485	48.50	276.32	4.11	4.11	8.72	134.26
486	48.60	302.56	4.03	4.03	7.47	134.42
487	48.70	313.39	4.06	4.06	7.05	134.59
488	48.80	310.91	4.24	4.24	7.28	134.88
489	48.90	306.35	4.51	4.51	7.81	135.32
490	49.00	308.28	4.87	4.87	8.36	135.85
491	49.10	311.39	5.26	5.26	8.82	136.32
492	49.20	308.77	5.46	5.46	9.27	136.62
493	49.30	302.93	5.57	5.57	9.63	136.58
494	49.40	290.32	5.28	5.28	9.89	136.09
495	49.50	269.17	4.65	4.65	10.10	135.05
496	49.60	238.64	3.86	3.86	10.50	133.67
497	49.70	209.41	3.32	3.32	10.90	132.59

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q _c :	Measured cone resistance (tsf)
f _s :	Sleeve friction resistance (tsf)
u:	Pore pressure (tsf)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (pcf)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1	0.10	0.01	0.00	0.01	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
2	0.20	0.01	0.00	0.01	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
3	0.30	0.02	0.00	0.02	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
4	0.40	0.02	0.00	0.02	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
5	0.50	0.03	0.00	0.03	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
6	0.60	0.04	0.00	0.04	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
7	0.70	0.04	0.00	0.04	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
8	0.80	0.05	0.00	0.05	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
9	0.90	0.05	0.00	0.05	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
10	1.00	0.06	0.00	0.06	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
11	1.10	0.07	0.00	0.07	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
12	1.20	0.07	0.00	0.07	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
13	1.30	0.08	0.00	0.08	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
14	1.40	0.08	0.00	0.08	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
15	1.50	0.09	0.00	0.09	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
16	1.60	0.10	0.00	0.10	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
17	1.70	0.10	0.00	0.10	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
18	1.80	0.11	0.00	0.11	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
19	1.90	0.11	0.00	0.11	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
20	2.00	0.12	0.00	0.12	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
21	2.10	0.13	0.00	0.13	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
22	2.20	0.13	0.00	0.13	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
23	2.30	0.14	0.00	0.14	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
24	2.40	0.14	0.00	0.14	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
25	2.50	0.15	0.00	0.15	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
26	2.60	0.16	0.00	0.16	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
27	2.70	0.16	0.00	0.16	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
28	2.80	0.17	0.00	0.17	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
29	2.90	0.17	0.00	0.17	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
30	3.00	0.18	0.00	0.18	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
31	3.10	0.19	0.00	0.19	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
32	3.20	0.19	0.00	0.19	1.00	0.480	1.04	0.460	1.10	1.30	2.000	Yes
33	3.30	0.20	0.00	0.20	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
34	3.40	0.20	0.00	0.20	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
35	3.50	0.21	0.00	0.21	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
36	3.60	0.21	0.00	0.21	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
37	3.70	0.22	0.00	0.22	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
38	3.80	0.23	0.00	0.23	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
39	3.90	0.23	0.00	0.23	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
40	4.00	0.24	0.00	0.24	1.00	0.479	1.04	0.460	1.10	1.30	2.000	No
41	4.10	0.24	0.00	0.24	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
42	4.20	0.25	0.00	0.25	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
43	4.30	0.25	0.00	0.25	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
44	4.40	0.26	0.00	0.26	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
45	4.50	0.26	0.00	0.26	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
46	4.60	0.27	0.00	0.27	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
47	4.70	0.27	0.00	0.27	0.99	0.479	1.04	0.459	1.10	1.30	2.000	No
48	4.80	0.28	0.00	0.28	0.99	0.478	1.04	0.459	1.10	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
49	4.90	0.29	0.00	0.29	0.99	0.478	1.04	0.458	1.10	1.30	2.000	Yes
50	5.00	0.29	0.00	0.29	0.99	0.478	1.04	0.458	1.10	1.30	2.000	Yes
51	5.10	0.30	0.00	0.30	0.99	0.478	1.04	0.458	1.10	1.30	2.000	Yes
52	5.20	0.30	0.00	0.30	0.99	0.478	1.04	0.458	1.10	1.30	2.000	Yes
53	5.30	0.31	0.00	0.31	0.99	0.478	1.04	0.458	1.10	1.30	2.000	Yes
54	5.40	0.31	0.00	0.31	0.99	0.478	1.04	0.458	1.10	1.30	2.000	Yes
55	5.50	0.32	0.00	0.32	0.99	0.477	1.04	0.458	1.10	1.30	2.000	Yes
56	5.60	0.33	0.00	0.33	0.99	0.477	1.04	0.458	1.10	1.30	2.000	No
57	5.70	0.33	0.00	0.33	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
58	5.80	0.34	0.00	0.34	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
59	5.90	0.34	0.00	0.34	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
60	6.00	0.35	0.00	0.35	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
61	6.10	0.36	0.00	0.36	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
62	6.20	0.36	0.00	0.36	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
63	6.30	0.37	0.00	0.37	0.99	0.476	1.04	0.457	1.10	1.30	2.000	No
64	6.40	0.37	0.00	0.37	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
65	6.50	0.38	0.00	0.38	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
66	6.60	0.39	0.00	0.39	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
67	6.70	0.39	0.00	0.39	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
68	6.80	0.40	0.00	0.40	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
69	6.90	0.40	0.00	0.40	0.99	0.476	1.04	0.456	1.10	1.30	2.000	No
70	7.00	0.41	0.00	0.41	0.99	0.475	1.04	0.456	1.10	1.30	2.000	No
71	7.10	0.42	0.00	0.42	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
72	7.20	0.42	0.00	0.42	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
73	7.30	0.43	0.00	0.43	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
74	7.40	0.43	0.00	0.43	0.99	0.475	1.04	0.455	1.10	1.30	2.000	No
75	7.50	0.44	0.00	0.44	0.99	0.475	1.04	0.455	1.09	1.30	2.000	No
76	7.60	0.44	0.00	0.44	0.99	0.475	1.04	0.455	1.09	1.30	2.000	No
77	7.70	0.45	0.00	0.45	0.99	0.474	1.04	0.455	1.09	1.30	2.000	No
78	7.80	0.46	0.00	0.46	0.99	0.474	1.04	0.455	1.09	1.30	2.000	No
79	7.90	0.46	0.00	0.46	0.99	0.474	1.04	0.454	1.09	1.30	2.000	No
80	8.00	0.47	0.00	0.47	0.99	0.474	1.04	0.454	1.09	1.30	2.000	No
81	8.10	0.47	0.00	0.47	0.98	0.477	1.04	0.457	1.09	1.30	0.562	No
82	8.20	0.48	0.01	0.47	0.98	0.480	1.04	0.460	1.09	1.30	0.566	No
83	8.30	0.49	0.01	0.48	0.98	0.483	1.04	0.463	1.09	1.30	0.570	No
84	8.40	0.49	0.01	0.48	0.98	0.486	1.04	0.466	1.09	1.30	0.573	No
85	8.50	0.50	0.02	0.48	0.98	0.489	1.04	0.468	1.08	1.30	0.577	No
86	8.60	0.50	0.02	0.48	0.98	0.491	1.04	0.471	1.08	1.30	2.000	Yes
87	8.70	0.51	0.02	0.49	0.98	0.494	1.04	0.474	1.08	1.30	2.000	Yes
88	8.80	0.51	0.02	0.49	0.98	0.497	1.04	0.476	1.07	1.30	2.000	Yes
89	8.90	0.52	0.03	0.49	0.98	0.500	1.04	0.479	1.07	1.30	2.000	Yes
90	9.00	0.52	0.03	0.49	0.98	0.502	1.04	0.481	1.07	1.30	2.000	Yes
91	9.10	0.53	0.03	0.50	0.98	0.505	1.04	0.484	1.06	1.30	2.000	Yes
92	9.20	0.53	0.04	0.50	0.98	0.508	1.04	0.487	1.06	1.30	0.617	No
93	9.30	0.54	0.04	0.50	0.98	0.510	1.04	0.489	1.06	1.30	0.620	No
94	9.40	0.55	0.04	0.50	0.98	0.513	1.04	0.492	1.06	1.30	0.623	No
95	9.50	0.55	0.05	0.50	0.98	0.515	1.04	0.494	1.06	1.30	0.627	No
96	9.60	0.56	0.05	0.51	0.98	0.518	1.04	0.496	1.06	1.30	0.631	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
97	9.70	0.56	0.05	0.51	0.98	0.521	1.04	0.499	1.06	1.30	0.634	No
98	9.80	0.57	0.06	0.51	0.98	0.523	1.04	0.501	1.06	1.30	0.635	No
99	9.90	0.57	0.06	0.51	0.98	0.525	1.04	0.504	1.06	1.30	0.635	No
100	10.00	0.58	0.06	0.52	0.98	0.528	1.04	0.506	1.06	1.30	0.642	No
101	10.10	0.58	0.07	0.52	0.98	0.530	1.04	0.508	1.06	1.30	0.647	No
102	10.20	0.59	0.07	0.52	0.98	0.533	1.04	0.511	1.06	1.30	0.651	No
103	10.30	0.59	0.07	0.52	0.98	0.535	1.04	0.513	1.06	1.30	0.655	No
104	10.40	0.60	0.07	0.52	0.98	0.538	1.04	0.515	1.05	1.30	0.658	No
105	10.50	0.60	0.08	0.53	0.98	0.540	1.04	0.517	1.05	1.30	0.661	No
106	10.60	0.61	0.08	0.53	0.98	0.542	1.04	0.520	1.05	1.30	0.664	No
107	10.70	0.61	0.08	0.53	0.98	0.545	1.04	0.522	1.05	1.30	0.666	No
108	10.80	0.62	0.09	0.53	0.98	0.547	1.04	0.524	1.05	1.30	0.669	No
109	10.90	0.62	0.09	0.53	0.98	0.549	1.04	0.526	1.05	1.30	0.672	No
110	11.00	0.63	0.09	0.53	0.98	0.551	1.04	0.529	1.05	1.30	0.675	No
111	11.10	0.63	0.10	0.54	0.98	0.554	1.04	0.531	1.05	1.30	0.678	No
112	11.20	0.64	0.10	0.54	0.97	0.556	1.04	0.533	1.05	1.30	0.681	No
113	11.30	0.64	0.10	0.54	0.97	0.558	1.04	0.535	1.05	1.30	0.684	No
114	11.40	0.65	0.11	0.54	0.97	0.560	1.04	0.537	1.05	1.30	0.687	No
115	11.50	0.65	0.11	0.54	0.97	0.563	1.04	0.539	1.05	1.30	0.690	No
116	11.60	0.66	0.11	0.55	0.97	0.565	1.04	0.541	1.05	1.30	0.693	No
117	11.70	0.66	0.12	0.55	0.97	0.567	1.04	0.543	1.05	1.30	0.696	No
118	11.80	0.67	0.12	0.55	0.97	0.569	1.04	0.545	1.05	1.30	0.698	No
119	11.90	0.67	0.12	0.55	0.97	0.571	1.04	0.547	1.05	1.30	0.701	No
120	12.00	0.68	0.12	0.55	0.97	0.573	1.04	0.549	1.05	1.30	0.704	No
121	12.10	0.68	0.13	0.55	0.97	0.575	1.04	0.551	1.05	1.30	0.707	No
122	12.20	0.69	0.13	0.56	0.97	0.577	1.04	0.553	1.05	1.30	0.709	No
123	12.30	0.69	0.13	0.56	0.97	0.579	1.04	0.555	1.05	1.30	0.711	No
124	12.40	0.70	0.14	0.56	0.97	0.581	1.04	0.557	1.05	1.30	0.713	No
125	12.50	0.70	0.14	0.56	0.97	0.583	1.04	0.559	1.05	1.30	0.715	No
126	12.60	0.71	0.14	0.57	0.97	0.585	1.04	0.561	1.05	1.30	0.718	No
127	12.70	0.71	0.15	0.57	0.97	0.587	1.04	0.563	1.05	1.30	0.720	No
128	12.80	0.72	0.15	0.57	0.97	0.589	1.04	0.564	1.05	1.30	0.722	No
129	12.90	0.72	0.15	0.57	0.97	0.591	1.04	0.566	1.05	1.30	0.725	No
130	13.00	0.73	0.16	0.57	0.97	0.593	1.04	0.568	1.05	1.30	0.729	No
131	13.10	0.74	0.16	0.58	0.97	0.594	1.04	0.570	1.05	1.30	0.731	No
132	13.20	0.74	0.16	0.58	0.97	0.596	1.04	0.571	1.05	1.30	0.733	No
133	13.30	0.75	0.17	0.58	0.97	0.598	1.04	0.573	1.05	1.30	0.735	No
134	13.40	0.75	0.17	0.58	0.97	0.600	1.04	0.575	1.05	1.30	0.738	No
135	13.50	0.76	0.17	0.59	0.97	0.601	1.04	0.576	1.05	1.30	0.741	No
136	13.60	0.76	0.17	0.59	0.97	0.603	1.04	0.578	1.05	1.30	0.744	No
137	13.70	0.77	0.18	0.59	0.97	0.605	1.04	0.580	1.05	1.30	0.747	No
138	13.80	0.77	0.18	0.59	0.97	0.607	1.04	0.582	1.05	1.30	0.750	No
139	13.90	0.78	0.18	0.59	0.97	0.609	1.04	0.583	1.05	1.30	0.752	No
140	14.00	0.78	0.19	0.59	0.97	0.610	1.04	0.585	1.05	1.30	0.754	No
141	14.10	0.79	0.19	0.60	0.96	0.612	1.04	0.587	1.05	1.30	0.756	No
142	14.20	0.79	0.19	0.60	0.96	0.614	1.04	0.588	1.05	1.30	0.758	No
143	14.30	0.80	0.20	0.60	0.96	0.616	1.04	0.590	1.04	1.30	0.761	No
144	14.40	0.80	0.20	0.60	0.96	0.617	1.04	0.592	1.04	1.30	0.763	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
145	14.50	0.81	0.20	0.60	0.96	0.619	1.04	0.593	1.04	1.30	0.765	No
146	14.60	0.81	0.21	0.61	0.96	0.621	1.04	0.595	1.04	1.30	0.767	No
147	14.70	0.82	0.21	0.61	0.96	0.622	1.04	0.596	1.04	1.30	0.769	No
148	14.80	0.82	0.21	0.61	0.96	0.624	1.04	0.598	1.04	1.30	0.771	No
149	14.90	0.83	0.22	0.61	0.96	0.625	1.04	0.599	1.05	1.30	0.772	No
150	15.00	0.83	0.22	0.61	0.96	0.627	1.04	0.601	1.05	1.30	0.774	No
151	15.10	0.84	0.22	0.62	0.96	0.628	1.04	0.602	1.04	1.30	0.776	No
152	15.20	0.84	0.22	0.62	0.96	0.630	1.04	0.604	1.05	1.30	0.776	No
153	15.30	0.85	0.23	0.62	0.96	0.631	1.04	0.605	1.05	1.30	0.775	No
154	15.40	0.86	0.23	0.62	0.96	0.632	1.04	0.606	1.05	1.30	0.774	No
155	15.50	0.86	0.23	0.63	0.96	0.634	1.04	0.607	1.05	1.30	0.779	No
156	15.60	0.87	0.24	0.63	0.96	0.635	1.04	0.609	1.05	1.30	0.781	No
157	15.70	0.87	0.24	0.63	0.96	0.636	1.04	0.610	1.05	1.30	0.777	No
158	15.80	0.88	0.24	0.64	0.96	0.638	1.04	0.611	1.05	1.30	0.777	No
159	15.90	0.88	0.25	0.64	0.96	0.639	1.04	0.612	1.05	1.30	0.781	No
160	16.00	0.89	0.25	0.64	0.96	0.640	1.04	0.614	1.05	1.30	0.786	No
161	16.10	0.90	0.25	0.64	0.96	0.641	1.04	0.615	1.04	1.30	0.791	No
162	16.20	0.90	0.26	0.65	0.96	0.643	1.04	0.616	1.04	1.30	0.796	No
163	16.30	0.91	0.26	0.65	0.96	0.644	1.04	0.617	1.04	1.30	0.798	No
164	16.40	0.91	0.26	0.65	0.96	0.645	1.04	0.618	1.04	1.30	0.799	No
165	16.50	0.92	0.27	0.65	0.96	0.647	1.04	0.620	1.04	1.30	0.801	No
166	16.60	0.92	0.27	0.66	0.96	0.648	1.04	0.621	1.04	1.30	0.804	No
167	16.70	0.93	0.27	0.66	0.96	0.649	1.04	0.622	1.04	1.30	0.806	No
168	16.80	0.93	0.27	0.66	0.95	0.650	1.04	0.623	1.04	1.30	0.808	No
169	16.90	0.94	0.28	0.66	0.95	0.652	1.04	0.625	1.04	1.30	0.810	No
170	17.00	0.94	0.28	0.66	0.95	0.653	1.04	0.626	1.04	1.30	0.812	No
171	17.10	0.95	0.28	0.67	0.95	0.654	1.04	0.627	1.04	1.30	0.814	No
172	17.20	0.96	0.29	0.67	0.95	0.655	1.04	0.628	1.04	1.30	0.817	No
173	17.30	0.96	0.29	0.67	0.95	0.657	1.04	0.629	1.04	1.30	0.818	No
174	17.40	0.97	0.29	0.67	0.95	0.658	1.04	0.631	1.04	1.30	0.820	No
175	17.50	0.97	0.30	0.67	0.95	0.659	1.04	0.632	1.04	1.30	0.822	No
176	17.60	0.97	0.30	0.68	0.95	0.661	1.04	0.633	1.04	1.30	0.824	No
177	17.70	0.98	0.30	0.68	0.95	0.662	1.04	0.635	1.03	1.30	0.826	No
178	17.80	0.98	0.31	0.68	0.95	0.663	1.04	0.636	1.03	1.30	0.828	No
179	17.90	0.99	0.31	0.68	0.95	0.665	1.04	0.637	1.03	1.30	0.830	No
180	18.00	0.99	0.31	0.68	0.95	0.666	1.04	0.638	1.03	1.30	0.831	No
181	18.10	1.00	0.32	0.68	0.95	0.667	1.04	0.640	1.03	1.30	0.833	No
182	18.20	1.00	0.32	0.69	0.95	0.669	1.04	0.641	1.03	1.30	0.835	No
183	18.30	1.01	0.32	0.69	0.95	0.670	1.04	0.642	1.03	1.30	0.836	No
184	18.40	1.01	0.32	0.69	0.95	0.671	1.04	0.643	1.03	1.30	0.837	No
185	18.50	1.02	0.33	0.69	0.95	0.672	1.04	0.644	1.03	1.30	0.839	No
186	18.60	1.02	0.33	0.69	0.95	0.673	1.04	0.645	1.03	1.30	0.841	No
187	18.70	1.03	0.33	0.70	0.95	0.674	1.04	0.646	1.03	1.30	0.842	No
188	18.80	1.03	0.34	0.70	0.95	0.675	1.04	0.647	1.03	1.30	0.844	No
189	18.90	1.04	0.34	0.70	0.95	0.676	1.04	0.648	1.03	1.30	0.845	No
190	19.00	1.05	0.34	0.70	0.95	0.677	1.04	0.649	1.03	1.30	0.847	No
191	19.10	1.05	0.35	0.70	0.95	0.679	1.04	0.650	1.03	1.30	0.848	No
192	19.20	1.06	0.35	0.71	0.95	0.680	1.04	0.651	1.03	1.30	0.849	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
193	19.30	1.06	0.35	0.71	0.94	0.681	1.04	0.652	1.03	1.30	0.850	No
194	19.40	1.07	0.36	0.71	0.94	0.681	1.04	0.653	1.03	1.30	0.852	No
195	19.50	1.07	0.36	0.71	0.94	0.682	1.04	0.654	1.03	1.30	0.853	No
196	19.60	1.08	0.36	0.72	0.94	0.683	1.04	0.655	1.03	1.30	0.854	No
197	19.70	1.08	0.37	0.72	0.94	0.684	1.04	0.656	1.03	1.30	0.856	No
198	19.80	1.09	0.37	0.72	0.94	0.685	1.04	0.657	1.03	1.30	0.857	No
199	19.90	1.09	0.37	0.72	0.94	0.686	1.04	0.658	1.03	1.30	0.857	No
200	20.00	1.10	0.37	0.73	0.94	0.687	1.04	0.659	1.03	1.30	0.859	No
201	20.10	1.10	0.38	0.73	0.94	0.688	1.04	0.659	1.03	1.30	0.861	No
202	20.20	1.11	0.38	0.73	0.94	0.689	1.04	0.660	1.03	1.30	0.864	No
203	20.30	1.12	0.38	0.73	0.94	0.690	1.04	0.661	1.03	1.30	0.865	No
204	20.40	1.12	0.39	0.73	0.94	0.691	1.04	0.662	1.03	1.30	0.866	No
205	20.50	1.13	0.39	0.74	0.94	0.692	1.04	0.663	1.03	1.30	0.868	No
206	20.60	1.13	0.39	0.74	0.94	0.693	1.04	0.664	1.03	1.30	0.870	No
207	20.70	1.14	0.40	0.74	0.94	0.694	1.04	0.665	1.03	1.30	0.871	No
208	20.80	1.14	0.40	0.74	0.94	0.695	1.04	0.666	1.03	1.30	0.872	No
209	20.90	1.15	0.40	0.74	0.94	0.696	1.04	0.667	1.03	1.30	0.874	No
210	21.00	1.15	0.41	0.75	0.94	0.696	1.04	0.668	1.03	1.30	0.875	No
211	21.10	1.16	0.41	0.75	0.94	0.697	1.04	0.668	1.03	1.30	0.876	No
212	21.20	1.16	0.41	0.75	0.94	0.698	1.04	0.669	1.03	1.30	0.877	No
213	21.30	1.17	0.41	0.75	0.94	0.699	1.04	0.670	1.03	1.30	0.878	No
214	21.40	1.17	0.42	0.75	0.94	0.700	1.04	0.671	1.03	1.30	0.879	No
215	21.50	1.18	0.42	0.76	0.94	0.701	1.04	0.672	1.03	1.30	0.880	No
216	21.60	1.18	0.42	0.76	0.94	0.701	1.04	0.672	1.03	1.30	0.881	No
217	21.70	1.19	0.43	0.76	0.93	0.702	1.04	0.673	1.03	1.30	0.881	No
218	21.80	1.19	0.43	0.76	0.93	0.703	1.04	0.674	1.03	1.30	0.881	No
219	21.90	1.20	0.43	0.77	0.93	0.703	1.04	0.674	1.03	1.30	0.880	No
220	22.00	1.21	0.44	0.77	0.93	0.704	1.04	0.675	1.03	1.30	0.880	No
221	22.10	1.21	0.44	0.77	0.93	0.705	1.04	0.676	1.03	1.30	0.881	No
222	22.20	1.22	0.44	0.77	0.93	0.705	1.04	0.676	1.03	1.30	0.882	No
223	22.30	1.22	0.45	0.78	0.93	0.706	1.04	0.677	1.03	1.30	0.884	No
224	22.40	1.23	0.45	0.78	0.93	0.707	1.04	0.677	1.03	1.30	0.885	No
225	22.50	1.23	0.45	0.78	0.93	0.707	1.04	0.678	1.03	1.30	0.886	No
226	22.60	1.24	0.46	0.78	0.93	0.708	1.04	0.678	1.03	1.30	0.887	No
227	22.70	1.25	0.46	0.79	0.93	0.708	1.04	0.679	1.03	1.30	0.888	No
228	22.80	1.25	0.46	0.79	0.93	0.709	1.04	0.679	1.03	1.30	0.886	No
229	22.90	1.26	0.46	0.79	0.93	0.709	1.04	0.680	1.03	1.30	0.883	No
230	23.00	1.26	0.47	0.80	0.93	0.710	1.04	0.680	1.03	1.30	0.881	No
231	23.10	1.27	0.47	0.80	0.93	0.710	1.04	0.681	1.03	1.30	0.882	No
232	23.20	1.28	0.47	0.80	0.93	0.711	1.04	0.681	1.03	1.30	0.885	No
233	23.30	1.28	0.48	0.81	0.93	0.711	1.04	0.682	1.03	1.30	0.889	No
234	23.40	1.29	0.48	0.81	0.93	0.712	1.04	0.682	1.03	1.30	0.893	No
235	23.50	1.29	0.48	0.81	0.93	0.712	1.04	0.683	1.02	1.30	0.896	No
236	23.60	1.30	0.49	0.81	0.93	0.713	1.04	0.683	1.02	1.30	0.898	No
237	23.70	1.31	0.49	0.82	0.93	0.713	1.04	0.684	1.02	1.30	0.900	No
238	23.80	1.31	0.49	0.82	0.93	0.714	1.04	0.684	1.02	1.30	0.902	No
239	23.90	1.32	0.50	0.82	0.93	0.715	1.04	0.685	1.02	1.30	0.903	No
240	24.00	1.32	0.50	0.82	0.93	0.715	1.04	0.686	1.02	1.30	0.904	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
241	24.10	1.33	0.50	0.82	0.92	0.716	1.04	0.686	1.02	1.30	0.905	No
242	24.20	1.33	0.51	0.83	0.92	0.716	1.04	0.687	1.02	1.30	0.906	No
243	24.30	1.34	0.51	0.83	0.92	0.717	1.04	0.687	1.02	1.30	0.906	No
244	24.40	1.34	0.51	0.83	0.92	0.718	1.04	0.688	1.02	1.30	0.907	No
245	24.50	1.35	0.51	0.83	0.92	0.718	1.04	0.688	1.02	1.30	0.908	No
246	24.60	1.35	0.52	0.84	0.92	0.719	1.04	0.689	1.02	1.30	0.909	No
247	24.70	1.36	0.52	0.84	0.92	0.719	1.04	0.689	1.02	1.30	0.911	No
248	24.80	1.37	0.52	0.84	0.92	0.720	1.04	0.690	1.02	1.30	0.912	No
249	24.90	1.37	0.53	0.84	0.92	0.720	1.04	0.690	1.02	1.30	0.913	No
250	25.00	1.38	0.53	0.85	0.92	0.721	1.04	0.691	1.02	1.30	0.913	No
251	25.10	1.38	0.53	0.85	0.92	0.721	1.04	0.691	1.02	1.30	0.914	No
252	25.20	1.39	0.54	0.85	0.92	0.722	1.04	0.692	1.02	1.30	0.916	No
253	25.30	1.39	0.54	0.85	0.92	0.722	1.04	0.692	1.02	1.30	0.917	No
254	25.40	1.40	0.54	0.85	0.92	0.723	1.04	0.693	1.02	1.30	0.917	No
255	25.50	1.40	0.55	0.86	0.92	0.723	1.04	0.693	1.02	1.30	0.917	No
256	25.60	1.41	0.55	0.86	0.92	0.724	1.04	0.694	1.02	1.30	0.918	No
257	25.70	1.41	0.55	0.86	0.92	0.724	1.04	0.694	1.02	1.30	0.919	No
258	25.80	1.42	0.56	0.86	0.92	0.725	1.04	0.695	1.02	1.30	0.920	No
259	25.90	1.42	0.56	0.87	0.92	0.725	1.04	0.695	1.02	1.30	0.921	No
260	26.00	1.43	0.56	0.87	0.92	0.726	1.04	0.696	1.02	1.30	0.921	No
261	26.10	1.44	0.56	0.87	0.92	0.726	1.04	0.696	1.02	1.30	0.920	No
262	26.20	1.44	0.57	0.87	0.92	0.727	1.04	0.696	1.02	1.30	0.920	No
263	26.30	1.45	0.57	0.88	0.92	0.727	1.04	0.697	1.02	1.30	0.921	No
264	26.40	1.45	0.57	0.88	0.91	0.727	1.04	0.697	1.02	1.30	0.921	No
265	26.50	1.46	0.58	0.88	0.91	0.727	1.04	0.697	1.02	1.30	0.920	No
266	26.60	1.47	0.58	0.88	0.91	0.728	1.04	0.698	1.02	1.30	0.921	No
267	26.70	1.47	0.58	0.89	0.91	0.728	1.04	0.698	1.02	1.30	0.922	No
268	26.80	1.48	0.59	0.89	0.91	0.728	1.04	0.698	1.02	1.30	0.924	No
269	26.90	1.48	0.59	0.89	0.91	0.729	1.04	0.698	1.01	1.30	0.925	No
270	27.00	1.49	0.59	0.90	0.91	0.729	1.04	0.699	1.01	1.30	0.926	No
271	27.10	1.49	0.60	0.90	0.91	0.729	1.04	0.699	1.01	1.30	0.926	No
272	27.20	1.50	0.60	0.90	0.91	0.729	1.04	0.699	1.01	1.30	0.925	No
273	27.30	1.51	0.60	0.90	0.91	0.730	1.04	0.699	1.02	1.30	0.924	No
274	27.40	1.51	0.61	0.91	0.91	0.730	1.04	0.700	1.02	1.30	0.924	No
275	27.50	1.52	0.61	0.91	0.91	0.730	1.04	0.700	1.02	1.30	0.923	No
276	27.60	1.52	0.61	0.91	0.91	0.730	1.04	0.700	1.01	1.30	0.924	No
277	27.70	1.53	0.61	0.92	0.91	0.731	1.04	0.700	1.01	1.30	0.925	No
278	27.80	1.54	0.62	0.92	0.91	0.731	1.04	0.700	1.01	1.30	0.926	No
279	27.90	1.54	0.62	0.92	0.91	0.731	1.04	0.701	1.01	1.30	0.927	No
280	28.00	1.55	0.62	0.92	0.91	0.731	1.04	0.701	1.01	1.30	0.929	No
281	28.10	1.55	0.63	0.93	0.91	0.731	1.04	0.701	1.01	1.30	0.930	No
282	28.20	1.56	0.63	0.93	0.91	0.732	1.04	0.701	1.01	1.30	0.932	No
283	28.30	1.57	0.63	0.93	0.91	0.732	1.04	0.701	1.01	1.30	0.933	No
284	28.40	1.57	0.64	0.94	0.91	0.732	1.04	0.702	1.01	1.30	0.933	No
285	28.50	1.58	0.64	0.94	0.91	0.732	1.04	0.702	1.01	1.30	0.934	No
286	28.60	1.58	0.64	0.94	0.90	0.733	1.04	0.702	1.01	1.30	0.934	No
287	28.70	1.59	0.65	0.94	0.90	0.733	1.04	0.702	1.01	1.30	0.934	No
288	28.80	1.60	0.65	0.95	0.90	0.733	1.04	0.702	1.01	1.30	0.934	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
289	28.90	1.60	0.65	0.95	0.90	0.733	1.04	0.703	1.01	1.30	0.934	No
290	29.00	1.61	0.66	0.95	0.90	0.733	1.04	0.703	1.01	1.30	0.934	No
291	29.10	1.61	0.66	0.96	0.90	0.733	1.04	0.703	1.01	1.30	0.934	No
292	29.20	1.62	0.66	0.96	0.90	0.733	1.04	0.703	1.01	1.30	0.935	No
293	29.30	1.63	0.66	0.96	0.90	0.734	1.04	0.703	1.01	1.30	0.935	No
294	29.40	1.63	0.67	0.96	0.90	0.734	1.04	0.703	1.01	1.30	0.934	No
295	29.50	1.64	0.67	0.97	0.90	0.734	1.04	0.703	1.01	1.30	0.935	No
296	29.60	1.64	0.67	0.97	0.90	0.734	1.04	0.703	1.01	1.30	0.936	No
297	29.70	1.65	0.68	0.97	0.90	0.734	1.04	0.704	1.01	1.30	0.937	No
298	29.80	1.66	0.68	0.98	0.90	0.734	1.04	0.704	1.01	1.30	0.937	No
299	29.90	1.66	0.68	0.98	0.90	0.734	1.04	0.704	1.01	1.30	0.937	No
300	30.00	1.67	0.69	0.98	0.90	0.735	1.04	0.704	1.01	1.30	0.938	No
301	30.10	1.67	0.69	0.98	0.90	0.735	1.04	0.704	1.01	1.30	0.940	No
302	30.20	1.68	0.69	0.99	0.90	0.735	1.04	0.704	1.01	1.30	0.940	No
303	30.30	1.68	0.70	0.99	0.90	0.735	1.04	0.704	1.01	1.30	0.940	No
304	30.40	1.69	0.70	0.99	0.90	0.735	1.04	0.705	1.01	1.30	0.941	No
305	30.50	1.70	0.70	0.99	0.90	0.735	1.04	0.705	1.01	1.30	0.941	No
306	30.60	1.70	0.71	1.00	0.90	0.735	1.04	0.705	1.01	1.30	0.941	No
307	30.70	1.71	0.71	1.00	0.90	0.735	1.04	0.705	1.01	1.30	0.942	No
308	30.80	1.71	0.71	1.00	0.89	0.736	1.04	0.705	1.00	1.30	0.942	No
309	30.90	1.72	0.71	1.01	0.89	0.736	1.04	0.705	1.00	1.30	0.941	No
310	31.00	1.73	0.72	1.01	0.89	0.736	1.04	0.705	1.01	1.30	0.938	No
311	31.10	1.73	0.72	1.01	0.89	0.736	1.04	0.705	1.01	1.30	0.936	No
312	31.20	1.74	0.72	1.01	0.89	0.736	1.04	0.705	1.00	1.30	0.937	No
313	31.30	1.74	0.73	1.02	0.89	0.736	1.04	0.705	1.00	1.30	0.939	No
314	31.40	1.75	0.73	1.02	0.89	0.736	1.04	0.705	1.00	1.30	0.939	No
315	31.50	1.76	0.73	1.02	0.89	0.736	1.04	0.705	1.00	1.30	2.000	Yes
316	31.60	1.76	0.74	1.03	0.89	0.736	1.04	0.705	1.00	1.30	2.000	Yes
317	31.70	1.77	0.74	1.03	0.89	0.736	1.04	0.705	1.00	1.30	2.000	Yes
318	31.80	1.78	0.74	1.03	0.89	0.736	1.04	0.705	1.00	1.30	2.000	Yes
319	31.90	1.78	0.75	1.04	0.89	0.736	1.04	0.705	1.00	1.30	2.000	Yes
320	32.00	1.79	0.75	1.04	0.89	0.736	1.04	0.705	1.00	1.30	2.000	Yes
321	32.10	1.79	0.75	1.04	0.89	0.736	1.04	0.705	1.00	1.30	2.000	Yes
322	32.20	1.80	0.76	1.04	0.89	0.736	1.04	0.705	1.00	1.30	2.000	Yes
323	32.30	1.81	0.76	1.05	0.89	0.736	1.04	0.705	1.00	1.30	2.000	Yes
324	32.40	1.81	0.76	1.05	0.89	0.736	1.04	0.705	1.00	1.30	2.000	Yes
325	32.50	1.82	0.76	1.05	0.89	0.736	1.04	0.705	1.00	1.30	2.000	Yes
326	32.60	1.82	0.77	1.06	0.89	0.736	1.04	0.705	1.00	1.30	2.000	Yes
327	32.70	1.83	0.77	1.06	0.89	0.736	1.04	0.705	1.00	1.30	2.000	Yes
328	32.80	1.84	0.77	1.06	0.89	0.736	1.04	0.705	1.00	1.30	2.000	Yes
329	32.90	1.84	0.78	1.06	0.88	0.736	1.04	0.705	1.00	1.30	0.948	No
330	33.00	1.85	0.78	1.07	0.88	0.736	1.04	0.706	1.00	1.30	0.948	No
331	33.10	1.85	0.78	1.07	0.88	0.736	1.04	0.706	1.00	1.30	0.948	No
332	33.20	1.86	0.79	1.07	0.88	0.736	1.04	0.706	1.00	1.30	0.948	No
333	33.30	1.87	0.79	1.08	0.88	0.736	1.04	0.706	1.00	1.30	0.948	No
334	33.40	1.87	0.79	1.08	0.88	0.736	1.04	0.706	1.00	1.30	0.948	No
335	33.50	1.88	0.80	1.08	0.88	0.736	1.04	0.706	1.00	1.30	0.948	No
336	33.60	1.88	0.80	1.08	0.88	0.736	1.04	0.706	1.00	1.30	0.949	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
337	33.70	1.89	0.80	1.09	0.88	0.736	1.04	0.706	1.00	1.30	0.949	No
338	33.80	1.90	0.80	1.09	0.88	0.736	1.04	0.705	1.00	1.30	2.000	Yes
339	33.90	1.90	0.81	1.09	0.88	0.736	1.04	0.705	1.00	1.30	2.000	Yes
340	34.00	1.91	0.81	1.10	0.88	0.736	1.04	0.705	1.00	1.30	2.000	Yes
341	34.10	1.91	0.81	1.10	0.88	0.736	1.04	0.705	1.00	1.30	2.000	Yes
342	34.20	1.92	0.82	1.10	0.88	0.736	1.04	0.705	0.99	1.30	2.000	Yes
343	34.30	1.93	0.82	1.11	0.88	0.735	1.04	0.705	0.99	1.30	2.000	Yes
344	34.40	1.93	0.82	1.11	0.88	0.735	1.04	0.705	0.99	1.30	2.000	Yes
345	34.50	1.94	0.83	1.11	0.88	0.735	1.04	0.705	0.99	1.30	2.000	Yes
346	34.60	1.95	0.83	1.12	0.88	0.735	1.04	0.704	0.99	1.30	2.000	Yes
347	34.70	1.95	0.83	1.12	0.88	0.735	1.04	0.704	0.99	1.30	2.000	Yes
348	34.80	1.96	0.84	1.12	0.88	0.735	1.04	0.704	0.99	1.30	2.000	Yes
349	34.90	1.97	0.84	1.13	0.88	0.734	1.04	0.704	0.99	1.30	2.000	Yes
350	35.00	1.97	0.84	1.13	0.87	0.734	1.04	0.704	0.99	1.30	2.000	Yes
351	35.10	1.98	0.85	1.13	0.87	0.734	1.04	0.704	0.98	1.30	0.912	No
352	35.20	1.99	0.85	1.14	0.87	0.734	1.04	0.703	0.98	1.30	2.000	Yes
353	35.30	1.99	0.85	1.14	0.87	0.734	1.04	0.703	0.99	1.30	2.000	Yes
354	35.40	2.00	0.85	1.14	0.87	0.734	1.04	0.703	0.99	1.30	2.000	Yes
355	35.50	2.01	0.86	1.15	0.87	0.733	1.04	0.703	0.99	1.30	2.000	Yes
356	35.60	2.01	0.86	1.15	0.87	0.733	1.04	0.703	0.99	1.30	2.000	Yes
357	35.70	2.02	0.86	1.15	0.87	0.733	1.04	0.703	0.99	1.30	2.000	Yes
358	35.80	2.03	0.87	1.16	0.87	0.733	1.04	0.702	0.99	1.30	2.000	Yes
359	35.90	2.03	0.87	1.16	0.87	0.733	1.04	0.702	0.98	1.30	2.000	Yes
360	36.00	2.04	0.87	1.16	0.87	0.732	1.04	0.702	0.98	1.30	2.000	Yes
361	36.10	2.04	0.88	1.17	0.87	0.732	1.04	0.702	0.98	1.30	2.000	Yes
362	36.20	2.05	0.88	1.17	0.87	0.732	1.04	0.702	0.98	1.30	2.000	Yes
363	36.30	2.06	0.88	1.17	0.87	0.732	1.04	0.701	0.98	1.30	0.916	No
364	36.40	2.06	0.89	1.18	0.87	0.732	1.04	0.701	0.97	1.30	0.917	No
365	36.50	2.07	0.89	1.18	0.87	0.731	1.04	0.701	0.97	1.30	0.918	No
366	36.60	2.08	0.89	1.18	0.87	0.731	1.04	0.701	0.97	1.30	0.919	No
367	36.70	2.08	0.90	1.19	0.87	0.731	1.04	0.701	0.97	1.30	0.919	No
368	36.80	2.09	0.90	1.19	0.87	0.731	1.04	0.700	0.97	1.30	0.917	No
369	36.90	2.10	0.90	1.20	0.87	0.731	1.04	0.700	0.97	1.30	0.920	No
370	37.00	2.10	0.90	1.20	0.87	0.730	1.04	0.700	0.97	1.30	0.922	No
371	37.10	2.11	0.91	1.20	0.86	0.730	1.04	0.700	0.97	1.30	0.924	No
372	37.20	2.12	0.91	1.21	0.86	0.730	1.04	0.700	0.97	1.30	0.925	No
373	37.30	2.12	0.91	1.21	0.86	0.730	1.04	0.699	0.97	1.30	0.926	No
374	37.40	2.13	0.92	1.21	0.86	0.730	1.04	0.699	0.97	1.30	0.926	No
375	37.50	2.14	0.92	1.22	0.86	0.729	1.04	0.699	0.97	1.30	0.925	No
376	37.60	2.14	0.92	1.22	0.86	0.729	1.04	0.699	0.97	1.30	0.923	No
377	37.70	2.15	0.93	1.22	0.86	0.729	1.04	0.699	0.97	1.30	0.922	No
378	37.80	2.16	0.93	1.23	0.86	0.729	1.04	0.698	0.97	1.30	0.922	No
379	37.90	2.16	0.93	1.23	0.86	0.728	1.04	0.698	0.97	1.30	0.922	No
380	38.00	2.17	0.94	1.23	0.86	0.728	1.04	0.698	0.97	1.30	0.923	No
381	38.10	2.17	0.94	1.24	0.86	0.728	1.04	0.698	0.97	1.30	0.926	No
382	38.20	2.18	0.94	1.24	0.86	0.728	1.04	0.698	0.97	1.30	0.929	No
383	38.30	2.19	0.95	1.24	0.86	0.728	1.04	0.697	0.97	1.30	0.933	No
384	38.40	2.19	0.95	1.25	0.86	0.727	1.04	0.697	0.97	1.30	0.936	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
385	38.50	2.20	0.95	1.25	0.86	0.727	1.04	0.697	0.97	1.30	0.939	No
386	38.60	2.21	0.95	1.25	0.86	0.727	1.04	0.697	0.98	1.30	0.941	No
387	38.70	2.21	0.96	1.26	0.86	0.727	1.04	0.697	0.98	1.30	0.942	No
388	38.80	2.22	0.96	1.26	0.86	0.727	1.04	0.696	0.98	1.30	0.943	No
389	38.90	2.23	0.96	1.26	0.86	0.726	1.04	0.696	0.98	1.30	0.943	No
390	39.00	2.23	0.97	1.26	0.86	0.726	1.04	0.696	0.98	1.30	0.943	No
391	39.10	2.24	0.97	1.27	0.86	0.726	1.04	0.696	0.98	1.30	0.943	No
392	39.20	2.24	0.97	1.27	0.85	0.726	1.04	0.696	0.98	1.30	0.944	No
393	39.30	2.25	0.98	1.27	0.85	0.726	1.04	0.696	0.98	1.30	0.944	No
394	39.40	2.26	0.98	1.28	0.85	0.725	1.04	0.695	0.97	1.30	0.944	No
395	39.50	2.26	0.98	1.28	0.85	0.725	1.04	0.695	0.97	1.30	0.944	No
396	39.60	2.27	0.99	1.28	0.85	0.725	1.04	0.695	0.97	1.30	0.944	No
397	39.70	2.28	0.99	1.29	0.85	0.725	1.04	0.695	0.97	1.30	0.945	No
398	39.80	2.28	0.99	1.29	0.85	0.725	1.04	0.695	0.97	1.30	0.945	No
399	39.90	2.29	1.00	1.29	0.85	0.725	1.04	0.694	0.97	1.30	0.945	No
400	40.00	2.29	1.00	1.30	0.85	0.724	1.04	0.694	0.97	1.30	0.946	No
401	40.10	2.30	1.00	1.30	0.85	0.724	1.04	0.694	0.98	1.30	0.947	No
402	40.20	2.31	1.00	1.30	0.85	0.724	1.04	0.694	0.97	1.30	0.947	No
403	40.30	2.31	1.01	1.31	0.85	0.724	1.04	0.694	0.97	1.30	0.946	No
404	40.40	2.32	1.01	1.31	0.85	0.724	1.04	0.694	0.97	1.30	0.945	No
405	40.50	2.33	1.01	1.31	0.85	0.723	1.04	0.693	0.97	1.30	0.942	No
406	40.60	2.33	1.02	1.32	0.85	0.723	1.04	0.693	0.96	1.30	0.937	No
407	40.70	2.34	1.02	1.32	0.85	0.723	1.04	0.693	0.96	1.30	0.932	No
408	40.80	2.35	1.02	1.32	0.85	0.723	1.04	0.693	0.95	1.30	0.929	No
409	40.90	2.35	1.03	1.33	0.85	0.722	1.04	0.692	0.95	1.30	0.932	No
410	41.00	2.36	1.03	1.33	0.85	0.722	1.04	0.692	0.95	1.30	0.933	No
411	41.10	2.36	1.03	1.33	0.85	0.722	1.04	0.692	0.94	1.30	0.934	No
412	41.20	2.37	1.04	1.34	0.84	0.722	1.04	0.692	0.94	1.30	0.936	No
413	41.30	2.38	1.04	1.34	0.84	0.721	1.04	0.691	0.93	1.30	0.942	No
414	41.40	2.38	1.04	1.34	0.84	0.721	1.04	0.691	0.93	1.30	0.948	No
415	41.50	2.39	1.05	1.35	0.84	0.721	1.04	0.691	0.93	1.30	0.948	No
416	41.60	2.40	1.05	1.35	0.84	0.720	1.04	0.690	0.93	1.30	0.949	No
417	41.70	2.40	1.05	1.35	0.84	0.720	1.04	0.690	0.93	1.30	0.949	No
418	41.80	2.41	1.05	1.36	0.84	0.720	1.04	0.690	0.93	1.30	0.950	No
419	41.90	2.42	1.06	1.36	0.84	0.719	1.04	0.690	0.92	1.30	0.950	No
420	42.00	2.42	1.06	1.36	0.84	0.719	1.04	0.689	0.92	1.30	0.950	No
421	42.10	2.43	1.06	1.37	0.84	0.719	1.04	0.689	0.92	1.30	0.951	No
422	42.20	2.44	1.07	1.37	0.84	0.719	1.04	0.689	0.92	1.30	0.951	No
423	42.30	2.44	1.07	1.37	0.84	0.718	1.04	0.688	0.92	1.30	0.951	No
424	42.40	2.45	1.07	1.38	0.84	0.718	1.04	0.688	0.92	1.30	0.952	No
425	42.50	2.46	1.08	1.38	0.84	0.718	1.04	0.688	0.92	1.30	0.952	No
426	42.60	2.46	1.08	1.39	0.84	0.717	1.04	0.687	0.92	1.30	0.953	No
427	42.70	2.47	1.08	1.39	0.84	0.717	1.04	0.687	0.92	1.30	0.953	No
428	42.80	2.48	1.09	1.39	0.84	0.717	1.04	0.687	0.92	1.30	0.953	No
429	42.90	2.48	1.09	1.40	0.84	0.716	1.04	0.687	0.92	1.30	0.954	No
430	43.00	2.49	1.09	1.40	0.84	0.716	1.04	0.686	0.92	1.30	0.954	No
431	43.10	2.50	1.10	1.40	0.84	0.716	1.04	0.686	0.92	1.30	0.954	No
432	43.20	2.50	1.10	1.41	0.84	0.715	1.04	0.686	0.91	1.30	0.955	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
433	43.30	2.51	1.10	1.41	0.83	0.715	1.04	0.685	0.92	1.30	0.953	No
434	43.40	2.52	1.10	1.41	0.83	0.715	1.04	0.685	0.92	1.30	0.951	No
435	43.50	2.52	1.11	1.42	0.83	0.714	1.04	0.685	0.92	1.30	0.949	No
436	43.60	2.53	1.11	1.42	0.83	0.714	1.04	0.685	0.92	1.30	0.947	No
437	43.70	2.54	1.11	1.42	0.83	0.714	1.04	0.684	0.92	1.30	0.942	No
438	43.80	2.54	1.12	1.43	0.83	0.714	1.04	0.684	0.93	1.30	0.937	No
439	43.90	2.55	1.12	1.43	0.83	0.713	1.04	0.684	0.93	1.30	0.935	No
440	44.00	2.56	1.12	1.43	0.83	0.713	1.04	0.683	0.94	1.30	0.937	No
441	44.10	2.56	1.13	1.44	0.83	0.713	1.04	0.683	0.94	1.30	0.938	No
442	44.20	2.57	1.13	1.44	0.83	0.712	1.04	0.683	0.95	1.30	0.939	No
443	44.30	2.58	1.13	1.44	0.83	0.712	1.04	0.683	0.95	1.30	0.940	No
444	44.40	2.58	1.14	1.45	0.83	0.712	1.04	0.682	0.95	1.30	0.941	No
445	44.50	2.59	1.14	1.45	0.83	0.712	1.04	0.682	0.95	1.30	0.942	No
446	44.60	2.59	1.14	1.45	0.83	0.711	1.04	0.682	0.96	1.30	0.943	No
447	44.70	2.60	1.15	1.46	0.83	0.711	1.04	0.682	0.96	1.30	0.943	No
448	44.80	2.61	1.15	1.46	0.83	0.711	1.04	0.682	0.96	1.30	0.943	No
449	44.90	2.61	1.15	1.46	0.83	0.711	1.04	0.681	0.96	1.30	0.943	No
450	45.00	2.62	1.15	1.47	0.83	0.711	1.04	0.681	0.96	1.30	0.943	No
451	45.10	2.63	1.16	1.47	0.83	0.710	1.04	0.681	0.96	1.30	0.943	No
452	45.20	2.63	1.16	1.47	0.83	0.710	1.04	0.681	0.96	1.30	0.943	No
453	45.30	2.64	1.16	1.47	0.82	0.710	1.04	0.680	0.96	1.30	0.942	No
454	45.40	2.64	1.17	1.48	0.82	0.710	1.04	0.680	0.95	1.30	0.941	No
455	45.50	2.65	1.17	1.48	0.82	0.709	1.04	0.680	0.94	1.30	0.939	No
456	45.60	2.66	1.17	1.48	0.82	0.709	1.04	0.680	0.93	1.30	0.938	No
457	45.70	2.66	1.18	1.49	0.82	0.709	1.04	0.679	0.93	1.30	0.938	No
458	45.80	2.67	1.18	1.49	0.82	0.708	1.04	0.679	0.92	1.30	0.938	No
459	45.90	2.68	1.18	1.49	0.82	0.708	1.04	0.679	0.91	1.30	0.946	No
460	46.00	2.68	1.19	1.50	0.82	0.708	1.04	0.678	0.90	1.30	0.956	No
461	46.10	2.69	1.19	1.50	0.82	0.708	1.04	0.678	0.90	1.30	0.965	No
462	46.20	2.70	1.19	1.50	0.82	0.707	1.04	0.678	0.89	1.30	0.965	No
463	46.30	2.70	1.19	1.51	0.82	0.707	1.04	0.677	0.89	1.30	0.966	No
464	46.40	2.71	1.20	1.51	0.82	0.707	1.04	0.677	0.89	1.30	0.966	No
465	46.50	2.72	1.20	1.52	0.82	0.706	1.04	0.677	0.89	1.30	0.966	No
466	46.60	2.72	1.20	1.52	0.82	0.706	1.04	0.677	0.89	1.30	0.967	No
467	46.70	2.73	1.21	1.52	0.82	0.705	1.04	0.676	0.89	1.30	0.967	No
468	46.80	2.74	1.21	1.53	0.82	0.705	1.04	0.676	0.89	1.30	0.967	No
469	46.90	2.74	1.21	1.53	0.82	0.705	1.04	0.676	0.89	1.30	0.967	No
470	47.00	2.75	1.22	1.53	0.82	0.704	1.04	0.675	0.89	1.30	0.968	No
471	47.10	2.76	1.22	1.54	0.82	0.704	1.04	0.675	0.89	1.30	0.968	No
472	47.20	2.76	1.22	1.54	0.82	0.704	1.04	0.674	0.89	1.30	0.968	No
473	47.30	2.77	1.23	1.54	0.82	0.703	1.04	0.674	0.89	1.30	0.968	No
474	47.40	2.78	1.23	1.55	0.81	0.703	1.04	0.674	0.89	1.30	0.969	No
475	47.50	2.78	1.23	1.55	0.81	0.703	1.04	0.673	0.89	1.30	0.969	No
476	47.60	2.79	1.24	1.55	0.81	0.702	1.04	0.673	0.88	1.30	0.969	No
477	47.70	2.80	1.24	1.56	0.81	0.702	1.04	0.673	0.88	1.30	0.970	No
478	47.80	2.80	1.24	1.56	0.81	0.702	1.04	0.673	0.90	1.30	0.952	No
479	47.90	2.81	1.24	1.57	0.81	0.701	1.04	0.672	0.91	1.30	0.939	No
480	48.00	2.82	1.25	1.57	0.81	0.701	1.04	0.672	0.92	1.30	0.939	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
481	48.10	2.82	1.25	1.57	0.81	0.701	1.04	0.672	0.90	1.30	0.946	No
482	48.20	2.83	1.25	1.58	0.81	0.700	1.04	0.671	0.89	1.30	0.965	No
483	48.30	2.84	1.26	1.58	0.81	0.700	1.04	0.671	0.88	1.30	0.971	No
484	48.40	2.84	1.26	1.58	0.81	0.700	1.04	0.671	0.88	1.30	0.971	No
485	48.50	2.85	1.26	1.59	0.81	0.699	1.04	0.670	0.88	1.30	0.972	No
486	48.60	2.86	1.27	1.59	0.81	0.699	1.04	0.670	0.88	1.30	0.972	No
487	48.70	2.86	1.27	1.59	0.81	0.699	1.04	0.670	0.88	1.30	0.972	No
488	48.80	2.87	1.27	1.60	0.81	0.698	1.04	0.669	0.88	1.30	0.972	No
489	48.90	2.88	1.28	1.60	0.81	0.698	1.04	0.669	0.88	1.30	0.973	No
490	49.00	2.88	1.28	1.60	0.81	0.697	1.04	0.668	0.88	1.30	0.973	No
491	49.10	2.89	1.28	1.61	0.81	0.697	1.04	0.668	0.87	1.30	0.973	No
492	49.20	2.90	1.29	1.61	0.81	0.697	1.04	0.668	0.87	1.30	0.973	No
493	49.30	2.90	1.29	1.62	0.81	0.696	1.04	0.667	0.87	1.30	0.974	No
494	49.40	2.91	1.29	1.62	0.80	0.696	1.04	0.667	0.87	1.30	0.974	No
495	49.50	2.92	1.29	1.62	0.80	0.696	1.04	0.667	0.87	1.30	0.974	No
496	49.60	2.92	1.30	1.63	0.80	0.695	1.04	0.666	0.87	1.30	0.974	No
497	49.70	2.93	1.30	1.63	0.80	0.695	1.04	0.666	0.88	1.30	0.969	No

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
 σ_v : Total overburden pressure at test point (tsf)
 u_0 : Water pressure at test point (tsf)
 σ_v' : Effective overburden pressure based on GWT during earthquake (tsf)
 r_d : Nonlinear shear mass factor
 CSR: Cyclic Stress Ratio
 MSF: Magnitude Scaling Factor
 CSR_{eq}: CSR adjusted for M=7.5
 K_σ : Effective overburden stress factor
 CSR*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1	0.10	52.54	29.86	2.09	0.44	1.70	77.12	50.73	127.85	4.000	No	No	2.00
2	0.20	61.37	25.49	2.03	0.41	1.70	98.96	48.35	147.32	4.000	No	No	2.00
3	0.30	71.19	22.19	1.99	0.38	1.70	119.65	45.07	164.72	4.000	No	No	2.00
4	0.40	75.74	21.95	1.99	0.37	1.70	124.44	45.23	169.67	4.000	No	No	2.00
5	0.50	75.24	24.40	2.02	0.37	1.70	120.90	50.08	170.98	4.000	No	No	2.00
6	0.60	73.40	27.16	2.05	0.37	1.70	117.23	54.59	171.82	4.000	No	No	2.00
7	0.70	71.59	29.02	2.08	0.37	1.70	115.57	57.26	172.83	4.000	No	No	2.00
8	0.80	69.27	28.93	2.07	0.37	1.70	112.18	56.45	168.63	4.000	No	No	2.00
9	0.90	65.76	27.15	2.05	0.39	1.70	106.02	52.46	158.48	4.000	No	No	2.00
10	1.00	61.48	25.65	2.03	0.41	1.70	98.66	48.58	147.24	4.000	No	No	2.00
11	1.10	57.86	25.66	2.03	0.42	1.70	91.60	47.33	138.94	4.000	No	No	2.00
12	1.20	55.98	27.16	2.05	0.42	1.70	88.55	49.20	137.75	4.000	No	No	2.00
13	1.30	55.88	26.59	2.04	0.42	1.70	89.60	48.50	138.10	4.000	No	No	2.00
14	1.40	56.48	24.33	2.02	0.43	1.70	91.15	44.89	136.04	4.000	No	No	2.00
15	1.50	56.65	21.86	1.99	0.44	1.70	91.40	40.03	131.43	4.000	No	No	2.00
16	1.60	56.56	21.25	1.98	0.44	1.70	90.45	38.57	129.02	4.000	No	No	2.00
17	1.70	56.82	23.90	2.01	0.43	1.70	90.72	44.01	134.74	4.000	No	No	2.00
18	1.80	57.51	27.55	2.06	0.41	1.70	92.65	50.57	143.22	4.000	No	No	2.00
19	1.90	57.98	30.90	2.10	0.40	1.70	93.77	55.45	149.23	4.000	No	No	2.00
20	2.00	57.09	34.36	2.14	0.40	1.70	92.97	59.26	152.24	4.000	No	No	2.00
21	2.10	56.39	37.81	2.19	0.40	1.70	88.34	61.46	149.80	4.000	No	No	2.00
22	2.20	57.47	40.44	2.22	0.40	1.70	90.38	64.07	154.45	4.000	No	No	2.00
23	2.30	59.29	41.28	2.23	0.38	1.70	98.15	66.60	164.75	4.000	No	No	2.00
24	2.40	58.41	41.93	2.24	0.38	1.70	97.13	66.83	163.96	4.000	Yes	No	2.00
25	2.50	52.87	44.48	2.27	0.40	1.70	86.13	65.78	151.91	4.000	Yes	No	2.00
26	2.60	44.67	49.89	2.34	0.43	1.70	71.45	64.88	136.34	4.000	Yes	No	2.00
27	2.70	36.23	57.72	2.43	0.45	1.70	57.66	64.17	121.83	4.000	Yes	No	2.00
28	2.80	29.26	66.00	2.54	0.48	1.70	45.43	62.98	108.42	4.000	Yes	No	2.00
29	2.90	24.02	73.62	2.63	0.50	1.70	37.86	0.00	37.86	4.000	Yes	Yes	2.00
30	3.00	20.23	80.01	2.71	0.51	1.70	32.42	0.00	32.42	4.000	Yes	Yes	2.00
31	3.10	17.19	85.32	2.78	0.53	1.70	27.18	0.00	27.18	4.000	Yes	Yes	2.00
32	3.20	14.86	89.11	2.83	0.54	1.70	23.19	0.00	23.19	4.000	Yes	Yes	2.00
33	3.30	13.57	90.59	2.84	0.54	1.70	21.21	0.00	21.21	4.000	No	Yes	2.00
34	3.40	12.90	90.80	2.85	0.54	1.70	20.95	0.00	20.95	4.000	No	Yes	2.00
35	3.50	12.42	90.75	2.85	0.55	1.70	19.99	0.00	19.99	4.000	No	Yes	2.00
36	3.60	11.77	91.10	2.85	0.55	1.70	18.91	0.00	18.91	4.000	No	Yes	2.00
37	3.70	11.18	91.33	2.85	0.56	1.70	17.80	0.00	17.80	4.000	No	Yes	2.00
38	3.80	10.81	91.00	2.85	0.56	1.70	17.14	0.00	17.14	4.000	No	Yes	2.00
39	3.90	10.67	90.04	2.84	0.56	1.70	17.14	0.00	17.14	4.000	No	Yes	2.00
40	4.00	10.67	88.57	2.82	0.56	1.70	17.14	0.00	17.14	4.000	No	Yes	2.00
41	4.10	10.67	87.60	2.81	0.56	1.70	17.14	0.00	17.14	4.000	No	Yes	2.00
42	4.20	10.67	87.38	2.80	0.56	1.70	17.14	0.00	17.14	4.000	No	Yes	2.00
43	4.30	10.67	87.56	2.81	0.56	1.70	17.14	0.00	17.14	4.000	No	Yes	2.00
44	4.40	10.91	87.22	2.80	0.56	1.70	17.14	0.00	17.14	4.000	No	Yes	2.00
45	4.50	11.61	85.86	2.79	0.56	1.70	18.29	0.00	18.29	4.000	No	Yes	2.00
46	4.60	12.40	84.53	2.77	0.55	1.70	20.53	0.00	20.53	4.000	No	Yes	2.00
47	4.70	12.96	84.19	2.76	0.55	1.70	20.95	0.00	20.95	4.000	No	Yes	2.00
48	4.80	13.50	84.54	2.77	0.55	1.70	20.99	0.00	20.99	4.000	Yes	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
49	4.90	15.92	81.92	2.74	0.54	1.70	23.11	0.00	23.11	4.000	Yes	Yes	2.00
50	5.00	21.14	74.07	2.64	0.51	1.70	32.60	0.00	32.60	4.000	Yes	Yes	2.00
51	5.10	28.44	63.69	2.51	0.48	1.70	46.14	62.63	108.77	4.000	Yes	No	2.00
52	5.20	35.19	53.68	2.38	0.45	1.70	58.26	62.93	121.19	4.000	Yes	No	2.00
53	5.30	39.84	45.34	2.28	0.45	1.70	65.12	60.95	126.07	4.000	Yes	No	2.00
54	5.40	42.91	39.84	2.21	0.44	1.70	68.56	58.35	126.92	4.000	Yes	No	2.00
55	5.50	46.06	36.97	2.17	0.44	1.69	72.62	57.09	129.71	4.000	Yes	No	2.00
56	5.60	50.27	35.45	2.16	0.43	1.66	78.27	57.03	135.30	4.000	No	No	2.00
57	5.70	54.79	33.49	2.13	0.42	1.62	84.75	56.53	141.28	4.000	No	No	2.00
58	5.80	58.08	31.27	2.10	0.41	1.60	89.28	54.97	144.25	4.000	No	No	2.00
59	5.90	58.83	30.04	2.09	0.41	1.59	89.97	53.56	143.53	4.000	No	No	2.00
60	6.00	57.29	30.67	2.10	0.42	1.59	86.47	53.66	140.13	4.000	No	No	2.00
61	6.10	55.12	32.52	2.12	0.43	1.59	81.73	54.83	136.56	4.000	No	No	2.00
62	6.20	53.71	34.14	2.14	0.43	1.58	79.65	56.08	135.73	4.000	No	No	2.00
63	6.30	53.23	34.57	2.14	0.43	1.57	79.13	56.39	135.52	4.000	No	No	2.00
64	6.40	52.58	34.86	2.15	0.43	1.56	78.20	56.46	134.66	4.000	No	No	2.00
65	6.50	51.24	35.49	2.16	0.43	1.56	75.66	56.48	132.14	4.000	No	No	2.00
66	6.60	49.76	36.44	2.17	0.44	1.56	72.56	56.62	129.17	4.000	No	No	2.00
67	6.70	48.27	37.51	2.18	0.44	1.55	71.06	57.17	128.23	4.000	No	No	2.00
68	6.80	46.37	38.86	2.20	0.45	1.55	68.56	57.64	126.19	4.000	No	No	2.00
69	6.90	43.90	40.53	2.22	0.45	1.55	63.88	57.70	121.58	4.000	No	No	2.00
70	7.00	41.42	42.09	2.24	0.46	1.55	60.21	57.82	118.03	4.000	No	No	2.00
71	7.10	39.39	43.09	2.25	0.47	1.55	57.64	57.78	115.43	4.000	No	No	2.00
72	7.20	36.94	44.77	2.27	0.47	1.54	54.78	58.00	112.78	4.000	No	No	2.00
73	7.30	33.77	48.22	2.32	0.48	1.55	49.41	58.32	107.73	4.000	No	No	2.00
74	7.40	30.59	52.94	2.37	0.49	1.55	43.87	58.76	102.63	4.000	No	No	2.00
75	7.50	28.99	56.01	2.41	0.50	1.55	41.03	59.03	100.06	4.000	No	No	2.00
76	7.60	28.89	55.99	2.41	0.49	1.54	42.06	59.31	101.37	4.000	No	No	2.00
77	7.70	29.43	54.02	2.39	0.49	1.52	42.70	58.83	101.53	4.000	No	No	2.00
78	7.80	30.02	51.71	2.36	0.50	1.52	42.52	57.94	100.47	4.000	No	No	2.00
79	7.90	30.81	49.62	2.33	0.49	1.51	43.81	57.46	101.27	4.000	No	No	2.00
80	8.00	31.60	48.01	2.31	0.49	1.49	45.20	57.13	102.32	4.000	No	No	2.00
81	8.10	32.01	46.80	2.30	0.49	1.49	45.13	56.55	101.68	0.140	No	No	0.25
82	8.20	32.01	46.69	2.30	0.49	1.49	45.02	56.47	101.50	0.139	No	No	0.25
83	8.30	32.01	46.98	2.30	0.49	1.48	44.90	56.58	101.48	0.139	No	No	0.24
84	8.40	32.01	47.33	2.30	0.49	1.48	44.78	56.71	101.49	0.139	No	No	0.24
85	8.50	31.59	47.54	2.31	0.49	1.48	44.67	56.78	101.44	0.139	No	No	0.24
86	8.60	30.13	48.45	2.32	0.50	1.48	42.94	56.73	99.67	4.000	Yes	No	2.00
87	8.70	26.66	52.19	2.36	0.51	1.48	38.76	57.11	95.87	4.000	Yes	No	2.00
88	8.80	21.40	60.24	2.47	0.53	1.50	30.63	57.36	87.99	4.000	Yes	No	2.00
89	8.90	15.52	72.97	2.62	0.55	1.52	21.58	0.00	21.58	4.000	Yes	Yes	2.00
90	9.00	11.03	87.87	2.81	0.57	1.54	14.55	0.00	14.55	4.000	Yes	Yes	2.00
91	9.10	8.41	100.00	2.97	0.57	1.55	11.88	0.00	11.88	4.000	Yes	Yes	2.00
92	9.20	7.29	100.00	3.07	0.58	1.55	10.43	0.00	10.43	4.000	No	Yes	2.00
93	9.30	7.11	100.00	3.11	0.58	1.55	9.69	0.00	9.69	4.000	No	Yes	2.00
94	9.40	7.15	100.00	3.11	0.58	1.54	11.01	0.00	11.01	4.000	No	Yes	2.00
95	9.50	7.05	100.00	3.10	0.58	1.54	10.51	0.00	10.51	4.000	No	Yes	2.00
96	9.60	6.68	100.00	3.12	0.59	1.54	9.20	0.00	9.20	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
97	9.70	7.58	100.00	3.08	0.58	1.53	9.40	0.00	9.40	4.000	No	Yes	2.00
98	9.80	9.92	100.00	2.98	0.57	1.51	14.15	0.00	14.15	4.000	No	Yes	2.00
99	9.90	10.58	99.29	2.95	0.55	1.49	18.77	0.00	18.77	4.000	No	Yes	2.00
100	10.00	9.12	100.00	3.00	0.57	1.51	12.10	0.00	12.10	4.000	No	Yes	2.00
101	10.10	6.33	100.00	3.13	0.59	1.52	7.97	0.00	7.97	4.000	No	Yes	2.00
102	10.20	4.77	100.00	3.24	0.59	1.53	7.15	0.00	7.15	4.000	No	Yes	2.00
103	10.30	4.05	100.00	3.30	0.60	1.53	5.49	0.00	5.49	4.000	No	Yes	2.00
104	10.40	3.45	100.00	3.36	0.60	1.53	4.88	0.00	4.88	4.000	No	Yes	2.00
105	10.50	3.55	100.00	3.33	0.60	1.53	4.59	0.00	4.59	4.000	No	Yes	2.00
106	10.60	4.00	100.00	3.25	0.60	1.52	5.85	0.00	5.85	4.000	No	Yes	2.00
107	10.70	4.52	100.00	3.19	0.60	1.51	6.77	0.00	6.77	4.000	No	Yes	2.00
108	10.80	4.74	100.00	3.17	0.60	1.51	6.76	0.00	6.76	4.000	No	Yes	2.00
109	10.90	4.74	100.00	3.18	0.60	1.51	6.74	0.00	6.74	4.000	No	Yes	2.00
110	11.00	4.74	100.00	3.18	0.60	1.50	6.73	0.00	6.73	4.000	No	Yes	2.00
111	11.10	4.74	100.00	3.16	0.60	1.50	6.72	0.00	6.72	4.000	No	Yes	2.00
112	11.20	4.74	100.00	3.14	0.60	1.50	6.70	0.00	6.70	4.000	No	Yes	2.00
113	11.30	4.74	100.00	3.13	0.60	1.49	6.69	0.00	6.69	4.000	No	Yes	2.00
114	11.40	4.74	100.00	3.13	0.60	1.49	6.68	0.00	6.68	4.000	No	Yes	2.00
115	11.50	4.74	100.00	3.14	0.60	1.49	6.66	0.00	6.66	4.000	No	Yes	2.00
116	11.60	4.74	100.00	3.16	0.60	1.48	6.65	0.00	6.65	4.000	No	Yes	2.00
117	11.70	4.74	100.00	3.19	0.60	1.48	6.64	0.00	6.64	4.000	No	Yes	2.00
118	11.80	4.74	100.00	3.20	0.60	1.48	6.62	0.00	6.62	4.000	No	Yes	2.00
119	11.90	4.74	100.00	3.21	0.60	1.48	6.61	0.00	6.61	4.000	No	Yes	2.00
120	12.00	4.74	100.00	3.20	0.60	1.47	6.60	0.00	6.60	4.000	No	Yes	2.00
121	12.10	4.74	100.00	3.19	0.60	1.47	6.58	0.00	6.58	4.000	No	Yes	2.00
122	12.20	4.96	100.00	3.18	0.60	1.47	6.57	0.00	6.57	4.000	No	Yes	2.00
123	12.30	5.67	100.00	3.13	0.59	1.46	7.43	0.00	7.43	4.000	No	Yes	2.00
124	12.40	6.56	100.00	3.10	0.58	1.45	9.43	0.00	9.43	4.000	No	Yes	2.00
125	12.50	7.40	100.00	3.08	0.58	1.44	10.10	0.00	10.10	4.000	No	Yes	2.00
126	12.60	7.87	100.00	3.08	0.58	1.44	10.73	0.00	10.73	4.000	No	Yes	2.00
127	12.70	8.25	100.00	3.08	0.58	1.43	11.24	0.00	11.24	4.000	No	Yes	2.00
128	12.80	8.33	100.00	3.08	0.58	1.43	11.53	0.00	11.53	4.000	No	Yes	2.00
129	12.90	7.75	100.00	3.11	0.58	1.43	10.99	0.00	10.99	4.000	No	Yes	2.00
130	13.00	7.10	100.00	3.13	0.59	1.43	8.85	0.00	8.85	4.000	No	Yes	2.00
131	13.10	6.84	100.00	3.15	0.59	1.43	8.91	0.00	8.91	4.000	No	Yes	2.00
132	13.20	7.20	100.00	3.14	0.58	1.42	9.87	0.00	9.87	4.000	No	Yes	2.00
133	13.30	7.57	100.00	3.12	0.58	1.42	10.22	0.00	10.22	4.000	No	Yes	2.00
134	13.40	7.08	100.00	3.14	0.58	1.41	10.29	0.00	10.29	4.000	No	Yes	2.00
135	13.50	5.94	100.00	3.19	0.59	1.42	7.87	0.00	7.87	4.000	No	Yes	2.00
136	13.60	4.62	100.00	3.27	0.60	1.42	5.68	0.00	5.68	4.000	No	Yes	2.00
137	13.70	3.90	100.00	3.31	0.60	1.42	5.05	0.00	5.05	4.000	No	Yes	2.00
138	13.80	3.75	100.00	3.30	0.60	1.42	4.99	0.00	4.99	4.000	No	Yes	2.00
139	13.90	3.99	100.00	3.26	0.60	1.42	5.06	0.00	5.06	4.000	No	Yes	2.00
140	14.00	4.43	100.00	3.22	0.60	1.41	5.98	0.00	5.98	4.000	No	Yes	2.00
141	14.10	4.88	100.00	3.19	0.60	1.41	6.69	0.00	6.69	4.000	No	Yes	2.00
142	14.20	4.97	100.00	3.19	0.59	1.40	6.82	0.00	6.82	4.000	No	Yes	2.00
143	14.30	5.01	100.00	3.20	0.60	1.40	6.29	0.00	6.29	4.000	No	Yes	2.00
144	14.40	4.97	100.00	3.20	0.60	1.40	6.79	0.00	6.79	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
145	14.50	5.03	100.00	3.19	0.60	1.40	6.62	0.00	6.62	4.000	No	Yes	2.00
146	14.60	5.16	100.00	3.18	0.60	1.39	6.50	0.00	6.50	4.000	No	Yes	2.00
147	14.70	5.69	100.00	3.15	0.59	1.39	7.27	0.00	7.27	4.000	No	Yes	2.00
148	14.80	6.80	100.00	3.10	0.59	1.38	8.62	0.00	8.62	4.000	No	Yes	2.00
149	14.90	7.83	100.00	3.07	0.58	1.37	10.72	0.00	10.72	4.000	No	Yes	2.00
150	15.00	8.56	100.00	3.06	0.58	1.37	11.15	0.00	11.15	4.000	No	Yes	2.00
151	15.10	9.66	100.00	3.03	0.58	1.37	11.34	0.00	11.34	4.000	No	Yes	2.00
152	15.20	12.13	98.98	2.95	0.56	1.35	14.76	0.00	14.76	4.000	No	Yes	2.00
153	15.30	16.06	90.81	2.85	0.55	1.34	20.25	0.00	20.25	4.000	No	Yes	2.00
154	15.40	17.85	87.06	2.80	0.53	1.32	25.72	0.00	25.72	4.000	No	Yes	2.00
155	15.50	18.07	85.46	2.78	0.55	1.33	21.23	0.00	21.23	4.000	No	Yes	2.00
156	15.60	19.86	81.12	2.73	0.55	1.33	20.94	0.00	20.94	4.000	No	Yes	2.00
157	15.70	24.13	73.47	2.63	0.52	1.30	31.97	0.00	31.97	4.000	No	Yes	2.00
158	15.80	27.78	66.37	2.54	0.51	1.29	36.34	60.45	96.80	0.133	No	No	0.17
159	15.90	26.70	63.98	2.51	0.51	1.30	33.86	59.20	93.07	0.129	No	No	0.17
160	16.00	21.89	68.25	2.57	0.53	1.30	27.99	58.43	86.42	0.122	No	No	0.16
161	16.10	16.23	79.60	2.71	0.55	1.32	19.07	0.00	19.07	4.000	No	Yes	2.00
162	16.20	11.85	93.94	2.89	0.57	1.33	13.35	0.00	13.35	4.000	No	Yes	2.00
163	16.30	10.16	100.00	3.01	0.57	1.33	11.98	0.00	11.98	4.000	No	Yes	2.00
164	16.40	9.88	100.00	3.05	0.57	1.32	12.80	0.00	12.80	4.000	No	Yes	2.00
165	16.50	9.52	100.00	3.07	0.57	1.32	12.23	0.00	12.23	4.000	No	Yes	2.00
166	16.60	9.04	100.00	3.07	0.58	1.32	10.60	0.00	10.60	4.000	No	Yes	2.00
167	16.70	8.54	100.00	3.07	0.58	1.32	10.94	0.00	10.94	4.000	No	Yes	2.00
168	16.80	8.24	100.00	3.07	0.58	1.32	10.34	0.00	10.34	4.000	No	Yes	2.00
169	16.90	7.44	100.00	3.11	0.58	1.32	9.45	0.00	9.45	4.000	No	Yes	2.00
170	17.00	6.60	100.00	3.17	0.59	1.32	7.97	0.00	7.97	4.000	No	Yes	2.00
171	17.10	5.74	100.00	3.23	0.59	1.32	7.21	0.00	7.21	4.000	No	Yes	2.00
172	17.20	5.29	100.00	3.26	0.60	1.32	6.25	0.00	6.25	4.000	No	Yes	2.00
173	17.30	5.07	100.00	3.25	0.60	1.31	6.27	0.00	6.27	4.000	No	Yes	2.00
174	17.40	4.98	100.00	3.22	0.60	1.31	6.36	0.00	6.36	4.000	No	Yes	2.00
175	17.50	4.83	100.00	3.20	0.60	1.31	5.87	0.00	5.87	4.000	No	Yes	2.00
176	17.60	4.34	100.00	3.22	0.60	1.31	5.68	0.00	5.68	4.000	No	Yes	2.00
177	17.70	3.81	100.00	3.27	0.60	1.31	4.54	0.00	4.54	4.000	No	Yes	2.00
178	17.80	3.52	100.00	3.31	0.61	1.31	3.91	0.00	3.91	4.000	No	Yes	2.00
179	17.90	3.85	100.00	3.27	0.60	1.31	4.61	0.00	4.61	4.000	No	Yes	2.00
180	18.00	4.37	100.00	3.22	0.60	1.30	5.72	0.00	5.72	4.000	No	Yes	2.00
181	18.10	4.60	100.00	3.22	0.60	1.30	5.82	0.00	5.82	4.000	No	Yes	2.00
182	18.20	4.80	100.00	3.23	0.60	1.30	5.43	0.00	5.43	4.000	No	Yes	2.00
183	18.30	5.19	100.00	3.24	0.60	1.29	6.39	0.00	6.39	4.000	No	Yes	2.00
184	18.40	5.70	100.00	3.23	0.59	1.29	7.22	0.00	7.22	4.000	No	Yes	2.00
185	18.50	5.93	100.00	3.24	0.59	1.29	7.21	0.00	7.21	4.000	No	Yes	2.00
186	18.60	5.93	100.00	3.27	0.59	1.28	7.20	0.00	7.20	4.000	No	Yes	2.00
187	18.70	5.93	100.00	3.29	0.59	1.28	7.18	0.00	7.18	4.000	No	Yes	2.00
188	18.80	5.93	100.00	3.30	0.59	1.28	7.17	0.00	7.17	4.000	No	Yes	2.00
189	18.90	5.93	100.00	3.30	0.59	1.28	7.16	0.00	7.16	4.000	No	Yes	2.00
190	19.00	6.05	100.00	3.28	0.59	1.28	7.14	0.00	7.14	4.000	No	Yes	2.00
191	19.10	6.40	100.00	3.26	0.59	1.27	7.55	0.00	7.55	4.000	No	Yes	2.00
192	19.20	6.98	100.00	3.22	0.59	1.27	8.36	0.00	8.36	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
193	19.30	7.65	100.00	3.19	0.59	1.26	9.15	0.00	9.15	4.000	No	Yes	2.00
194	19.40	8.11	100.00	3.16	0.58	1.26	9.88	0.00	9.88	4.000	No	Yes	2.00
195	19.50	8.46	100.00	3.13	0.58	1.26	9.94	0.00	9.94	4.000	No	Yes	2.00
196	19.60	8.38	100.00	3.13	0.58	1.25	10.34	0.00	10.34	4.000	No	Yes	2.00
197	19.70	8.40	100.00	3.12	0.58	1.25	9.52	0.00	9.52	4.000	No	Yes	2.00
198	19.80	9.32	100.00	3.07	0.58	1.25	9.97	0.00	9.97	4.000	No	Yes	2.00
199	19.90	10.07	100.00	3.04	0.57	1.24	13.48	0.00	13.48	4.000	No	Yes	2.00
200	20.00	9.83	100.00	3.06	0.57	1.24	12.06	0.00	12.06	4.000	No	Yes	2.00
201	20.10	8.12	100.00	3.15	0.59	1.25	9.10	0.00	9.10	4.000	No	Yes	2.00
202	20.20	6.67	100.00	3.25	0.59	1.25	7.48	0.00	7.48	4.000	No	Yes	2.00
203	20.30	6.07	100.00	3.31	0.59	1.25	6.97	0.00	6.97	4.000	No	Yes	2.00
204	20.40	5.77	100.00	3.35	0.59	1.24	6.96	0.00	6.96	4.000	No	Yes	2.00
205	20.50	5.38	100.00	3.38	0.60	1.24	6.38	0.00	6.38	4.000	No	Yes	2.00
206	20.60	4.98	100.00	3.40	0.60	1.24	5.59	0.00	5.59	4.000	No	Yes	2.00
207	20.70	4.75	100.00	3.39	0.60	1.24	5.55	0.00	5.55	4.000	No	Yes	2.00
208	20.80	4.74	100.00	3.36	0.60	1.24	5.54	0.00	5.54	4.000	No	Yes	2.00
209	20.90	4.86	100.00	3.33	0.60	1.24	5.54	0.00	5.54	4.000	No	Yes	2.00
210	21.00	5.42	100.00	3.28	0.60	1.23	5.93	0.00	5.93	4.000	No	Yes	2.00
211	21.10	6.27	100.00	3.24	0.59	1.23	7.45	0.00	7.45	4.000	No	Yes	2.00
212	21.20	6.95	100.00	3.22	0.59	1.22	8.45	0.00	8.45	4.000	No	Yes	2.00
213	21.30	7.20	100.00	3.21	0.59	1.22	8.22	0.00	8.22	4.000	No	Yes	2.00
214	21.40	7.31	100.00	3.21	0.59	1.22	8.28	0.00	8.28	4.000	No	Yes	2.00
215	21.50	7.92	100.00	3.18	0.59	1.22	8.79	0.00	8.79	4.000	No	Yes	2.00
216	21.60	9.40	100.00	3.12	0.58	1.21	10.24	0.00	10.24	4.000	No	Yes	2.00
217	21.70	11.65	100.00	3.03	0.57	1.21	13.23	0.00	13.23	4.000	No	Yes	2.00
218	21.80	14.83	95.50	2.91	0.56	1.20	16.31	0.00	16.31	4.000	No	Yes	2.00
219	21.90	18.05	85.66	2.78	0.55	1.19	20.81	0.00	20.81	4.000	No	Yes	2.00
220	22.00	20.60	77.20	2.68	0.54	1.19	23.86	0.00	23.86	4.000	No	Yes	2.00
221	22.10	21.70	72.61	2.62	0.54	1.19	24.70	0.00	24.70	4.000	No	Yes	2.00
222	22.20	21.51	73.02	2.63	0.54	1.18	24.34	0.00	24.34	4.000	No	Yes	2.00
223	22.30	20.65	77.06	2.68	0.54	1.18	23.13	0.00	23.13	4.000	No	Yes	2.00
224	22.40	19.82	81.85	2.74	0.54	1.18	21.72	0.00	21.72	4.000	No	Yes	2.00
225	22.50	19.24	86.32	2.79	0.54	1.18	21.46	0.00	21.46	4.000	No	Yes	2.00
226	22.60	19.38	89.87	2.84	0.54	1.18	21.09	0.00	21.09	4.000	No	Yes	2.00
227	22.70	21.44	90.23	2.84	0.54	1.17	22.03	0.00	22.03	4.000	No	Yes	2.00
228	22.80	25.94	85.77	2.78	0.52	1.16	28.01	0.00	28.01	4.000	No	Yes	2.00
229	22.90	32.18	78.19	2.69	0.50	1.16	35.46	0.00	35.46	4.000	No	Yes	2.00
230	23.00	37.11	70.07	2.59	0.49	1.15	41.85	62.82	104.67	0.144	No	No	0.16
231	23.10	38.48	64.08	2.51	0.49	1.15	43.59	62.00	105.59	0.145	No	No	0.16
232	23.20	35.78	62.80	2.50	0.50	1.15	39.70	60.58	100.27	0.138	No	No	0.16
233	23.30	30.27	67.90	2.56	0.51	1.15	33.12	59.85	92.97	0.129	No	No	0.15
234	23.40	24.07	77.69	2.68	0.53	1.15	25.89	0.00	25.89	4.000	No	Yes	2.00
235	23.50	18.71	88.16	2.81	0.55	1.16	19.72	0.00	19.72	4.000	No	Yes	2.00
236	23.60	14.66	97.92	2.94	0.56	1.16	15.72	0.00	15.72	4.000	No	Yes	2.00
237	23.70	11.82	100.00	3.03	0.57	1.16	12.71	0.00	12.71	4.000	No	Yes	2.00
238	23.80	9.79	100.00	3.10	0.58	1.16	10.43	0.00	10.43	4.000	No	Yes	2.00
239	23.90	8.76	100.00	3.12	0.59	1.16	9.08	0.00	9.08	4.000	No	Yes	2.00
240	24.00	8.87	100.00	3.11	0.58	1.16	9.32	0.00	9.32	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
241	24.10	9.46	100.00	3.09	0.58	1.16	10.73	0.00	10.73	4.000	No	Yes	2.00
242	24.20	10.14	100.00	3.08	0.58	1.15	10.93	0.00	10.93	4.000	No	Yes	2.00
243	24.30	10.42	100.00	3.09	0.58	1.15	11.48	0.00	11.48	4.000	No	Yes	2.00
244	24.40	10.44	100.00	3.11	0.58	1.15	11.58	0.00	11.58	4.000	No	Yes	2.00
245	24.50	10.20	100.00	3.13	0.58	1.15	10.92	0.00	10.92	4.000	No	Yes	2.00
246	24.60	9.62	100.00	3.16	0.58	1.15	10.65	0.00	10.65	4.000	No	Yes	2.00
247	24.70	9.03	100.00	3.19	0.58	1.15	9.69	0.00	9.69	4.000	No	Yes	2.00
248	24.80	8.52	100.00	3.22	0.59	1.14	8.97	0.00	8.97	4.000	No	Yes	2.00
249	24.90	8.30	100.00	3.23	0.59	1.14	8.96	0.00	8.96	4.000	No	Yes	2.00
250	25.00	8.30	100.00	3.22	0.59	1.14	8.94	0.00	8.94	4.000	No	Yes	2.00
251	25.10	7.91	100.00	3.24	0.59	1.14	8.91	0.00	8.91	4.000	No	Yes	2.00
252	25.20	7.42	100.00	3.26	0.59	1.14	7.70	0.00	7.70	4.000	No	Yes	2.00
253	25.30	7.65	100.00	3.24	0.59	1.14	7.34	0.00	7.34	4.000	No	Yes	2.00
254	25.40	8.44	100.00	3.19	0.58	1.13	9.57	0.00	9.57	4.000	No	Yes	2.00
255	25.50	9.09	100.00	3.15	0.58	1.13	10.20	0.00	10.20	4.000	No	Yes	2.00
256	25.60	8.99	100.00	3.17	0.58	1.13	9.35	0.00	9.35	4.000	No	Yes	2.00
257	25.70	8.59	100.00	3.22	0.59	1.13	9.22	0.00	9.22	4.000	No	Yes	2.00
258	25.80	8.74	100.00	3.23	0.59	1.13	8.90	0.00	8.90	4.000	No	Yes	2.00
259	25.90	9.74	100.00	3.18	0.58	1.12	9.77	0.00	9.77	4.000	No	Yes	2.00
260	26.00	12.20	100.00	3.07	0.57	1.12	12.32	0.00	12.32	4.000	No	Yes	2.00
261	26.10	14.90	100.00	2.97	0.56	1.11	16.57	0.00	16.57	4.000	No	Yes	2.00
262	26.20	16.97	94.89	2.90	0.55	1.11	18.18	0.00	18.18	4.000	No	Yes	2.00
263	26.30	18.58	91.60	2.86	0.55	1.11	18.72	0.00	18.72	4.000	No	Yes	2.00
264	26.40	20.32	90.11	2.84	0.54	1.11	21.49	0.00	21.49	4.000	No	Yes	2.00
265	26.50	21.81	90.26	2.84	0.54	1.10	23.47	0.00	23.47	4.000	No	Yes	2.00
266	26.60	21.82	92.31	2.87	0.54	1.10	23.20	0.00	23.20	4.000	No	Yes	2.00
267	26.70	20.10	96.03	2.91	0.54	1.10	21.41	0.00	21.41	4.000	No	Yes	2.00
268	26.80	17.84	100.00	2.97	0.55	1.10	18.05	0.00	18.05	4.000	No	Yes	2.00
269	26.90	16.12	100.00	3.01	0.56	1.10	16.14	0.00	16.14	4.000	No	Yes	2.00
270	27.00	16.24	100.00	3.02	0.56	1.10	16.01	0.00	16.01	4.000	No	Yes	2.00
271	27.10	18.29	100.00	2.97	0.55	1.09	18.32	0.00	18.32	4.000	No	Yes	2.00
272	27.20	21.53	95.67	2.91	0.54	1.09	22.33	0.00	22.33	4.000	No	Yes	2.00
273	27.30	25.33	90.14	2.84	0.53	1.09	25.85	0.00	25.85	4.000	No	Yes	2.00
274	27.40	28.68	85.07	2.78	0.52	1.08	29.77	0.00	29.77	4.000	No	Yes	2.00
275	27.50	30.57	81.50	2.73	0.51	1.08	32.39	0.00	32.39	4.000	No	Yes	2.00
276	27.60	30.71	80.03	2.71	0.51	1.08	31.44	0.00	31.44	4.000	No	Yes	2.00
277	27.70	29.52	80.63	2.72	0.52	1.08	30.06	0.00	30.06	4.000	No	Yes	2.00
278	27.80	28.15	82.19	2.74	0.52	1.08	28.64	0.00	28.64	4.000	No	Yes	2.00
279	27.90	26.52	84.33	2.77	0.53	1.08	27.19	0.00	27.19	4.000	No	Yes	2.00
280	28.00	24.26	87.43	2.81	0.53	1.07	25.00	0.00	25.00	4.000	No	Yes	2.00
281	28.10	21.33	92.04	2.86	0.54	1.07	21.69	0.00	21.69	4.000	No	Yes	2.00
282	28.20	18.44	98.05	2.94	0.55	1.07	18.23	0.00	18.23	4.000	No	Yes	2.00
283	28.30	16.54	100.00	3.01	0.56	1.07	16.20	0.00	16.20	4.000	No	Yes	2.00
284	28.40	16.30	100.00	3.04	0.56	1.07	15.84	0.00	15.84	4.000	No	Yes	2.00
285	28.50	17.10	100.00	3.03	0.55	1.07	17.43	0.00	17.43	4.000	No	Yes	2.00
286	28.60	18.01	100.00	3.02	0.55	1.07	18.52	0.00	18.52	4.000	No	Yes	2.00
287	28.70	18.92	100.00	3.01	0.55	1.07	18.49	0.00	18.49	4.000	No	Yes	2.00
288	28.80	20.11	100.00	3.00	0.55	1.06	20.04	0.00	20.04	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
289	28.90	21.92	100.00	2.98	0.54	1.06	21.99	0.00	21.99	4.000	No	Yes	2.00
290	29.00	23.18	99.75	2.96	0.53	1.06	23.78	0.00	23.78	4.000	No	Yes	2.00
291	29.10	23.37	97.89	2.94	0.53	1.06	23.71	0.00	23.71	4.000	No	Yes	2.00
292	29.20	23.75	95.18	2.90	0.54	1.06	22.45	0.00	22.45	4.000	No	Yes	2.00
293	29.30	25.51	90.72	2.85	0.53	1.05	24.78	0.00	24.78	4.000	No	Yes	2.00
294	29.40	27.88	86.04	2.79	0.52	1.05	28.83	0.00	28.83	4.000	No	Yes	2.00
295	29.50	28.61	83.66	2.76	0.52	1.05	29.35	0.00	29.35	4.000	No	Yes	2.00
296	29.60	27.32	84.33	2.77	0.53	1.05	26.82	0.00	26.82	4.000	No	Yes	2.00
297	29.70	25.80	87.35	2.80	0.53	1.05	24.91	0.00	24.91	4.000	No	Yes	2.00
298	29.80	25.94	88.38	2.82	0.53	1.04	24.72	0.00	24.72	4.000	No	Yes	2.00
299	29.90	25.94	87.98	2.81	0.53	1.04	27.10	0.00	27.10	4.000	No	Yes	2.00
300	30.00	24.40	89.26	2.83	0.53	1.04	24.79	0.00	24.79	4.000	No	Yes	2.00
301	30.10	21.96	92.38	2.87	0.55	1.04	20.10	0.00	20.10	4.000	No	Yes	2.00
302	30.20	20.74	95.07	2.90	0.55	1.04	19.84	0.00	19.84	4.000	No	Yes	2.00
303	30.30	21.44	93.84	2.89	0.54	1.04	21.13	0.00	21.13	4.000	No	Yes	2.00
304	30.40	22.21	92.20	2.87	0.54	1.04	22.04	0.00	22.04	4.000	No	Yes	2.00
305	30.50	22.53	91.56	2.86	0.54	1.03	22.01	0.00	22.01	4.000	No	Yes	2.00
306	30.60	22.53	91.65	2.86	0.54	1.03	21.98	0.00	21.98	4.000	No	Yes	2.00
307	30.70	22.94	91.81	2.86	0.54	1.03	21.94	0.00	21.94	4.000	No	Yes	2.00
308	30.80	25.28	89.71	2.83	0.54	1.03	23.08	0.00	23.08	4.000	No	Yes	2.00
309	30.90	30.78	83.51	2.76	0.52	1.03	28.67	0.00	28.67	4.000	No	Yes	2.00
310	31.00	38.07	75.16	2.65	0.50	1.02	37.76	0.00	37.76	4.000	No	Yes	2.00
311	31.10	43.30	68.19	2.56	0.48	1.02	44.02	63.06	107.08	0.147	No	No	0.16
312	31.20	44.29	64.84	2.52	0.49	1.02	43.64	62.20	105.84	0.146	No	No	0.16
313	31.30	43.30	65.27	2.53	0.49	1.02	40.45	61.38	101.83	0.140	No	No	0.15
314	31.40	44.39	66.19	2.54	0.49	1.02	41.01	61.76	102.77	0.141	No	No	0.15
315	31.50	48.84	64.07	2.51	0.48	1.02	46.56	62.85	109.41	4.000	Yes	No	2.00
316	31.60	55.32	58.47	2.44	0.46	1.01	53.02	63.12	116.14	4.000	Yes	No	2.00
317	31.70	61.94	51.21	2.35	0.45	1.01	59.37	62.25	121.63	4.000	Yes	No	2.00
318	31.80	68.38	44.03	2.26	0.45	1.01	65.33	60.26	125.59	4.000	Yes	No	2.00
319	31.90	74.08	38.16	2.19	0.44	1.01	71.22	57.72	128.94	4.000	Yes	No	2.00
320	32.00	77.06	35.39	2.15	0.43	1.01	75.40	56.33	131.73	4.000	Yes	No	2.00
321	32.10	74.88	36.98	2.17	0.44	1.01	73.58	57.32	130.90	4.000	Yes	No	2.00
322	32.20	67.28	43.51	2.26	0.45	1.01	64.75	59.81	124.56	4.000	Yes	No	2.00
323	32.30	56.41	53.41	2.38	0.47	1.00	53.48	61.53	115.02	4.000	Yes	No	2.00
324	32.40	45.30	64.20	2.51	0.49	1.00	42.40	61.69	104.09	4.000	Yes	No	2.00
325	32.50	36.00	74.82	2.65	0.51	1.00	32.94	0.00	32.94	4.000	Yes	Yes	2.00
326	32.60	29.19	84.27	2.77	0.53	1.00	26.89	0.00	26.89	4.000	Yes	Yes	2.00
327	32.70	25.10	90.88	2.85	0.54	1.00	22.95	0.00	22.95	4.000	Yes	Yes	2.00
328	32.80	23.13	93.68	2.88	0.54	1.00	21.24	0.00	21.24	4.000	Yes	Yes	2.00
329	32.90	22.72	93.24	2.88	0.54	1.00	21.21	0.00	21.21	4.000	No	Yes	2.00
330	33.00	23.50	91.35	2.85	0.54	1.00	21.70	0.00	21.70	4.000	No	Yes	2.00
331	33.10	24.98	89.40	2.83	0.54	0.99	23.35	0.00	23.35	4.000	No	Yes	2.00
332	33.20	27.13	87.42	2.81	0.53	0.99	25.28	0.00	25.28	4.000	No	Yes	2.00
333	33.30	29.30	86.00	2.79	0.52	0.99	27.67	0.00	27.67	4.000	No	Yes	2.00
334	33.40	30.50	85.89	2.79	0.52	0.99	29.34	0.00	29.34	4.000	No	Yes	2.00
335	33.50	30.45	87.20	2.80	0.52	0.99	28.53	0.00	28.53	4.000	No	Yes	2.00
336	33.60	29.68	89.10	2.83	0.52	0.99	27.41	0.00	27.41	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
337	33.70	29.63	90.01	2.84	0.53	0.99	27.05	0.00	27.05	4.000	No	Yes	2.00
338	33.80	31.56	89.10	2.83	0.52	0.98	28.28	0.00	28.28	4.000	Yes	Yes	2.00
339	33.90	36.20	86.63	2.80	0.51	0.98	32.68	0.00	32.68	4.000	Yes	Yes	2.00
340	34.00	43.30	82.85	2.75	0.49	0.98	39.86	0.00	39.86	4.000	Yes	Yes	2.00
341	34.10	51.88	77.98	2.69	0.47	0.98	47.96	0.00	47.96	4.000	Yes	Yes	2.00
342	34.20	61.05	72.55	2.62	0.45	0.98	56.48	0.00	56.48	4.000	Yes	Yes	2.00
343	34.30	69.91	67.10	2.55	0.43	0.98	65.27	68.96	134.22	4.000	Yes	No	2.00
344	34.40	78.51	61.89	2.49	0.42	0.98	72.49	69.62	142.11	4.000	Yes	No	2.00
345	34.50	87.03	57.29	2.43	0.40	0.98	80.27	70.29	150.55	4.000	Yes	No	2.00
346	34.60	96.53	52.64	2.37	0.39	0.98	88.80	70.76	159.56	4.000	Yes	No	2.00
347	34.70	107.11	47.65	2.31	0.37	0.98	98.75	70.90	169.65	4.000	Yes	No	2.00
348	34.80	117.42	41.76	2.23	0.36	0.98	109.56	69.77	179.32	4.000	Yes	No	2.00
349	34.90	125.48	36.34	2.17	0.35	0.98	117.28	66.80	184.08	4.000	Yes	No	2.00
350	35.00	129.52	32.90	2.12	0.35	0.98	120.88	63.71	184.59	4.000	Yes	No	2.00
351	35.10	129.35	32.37	2.12	0.35	0.98	120.43	62.94	183.37	0.835	No	No	0.92
352	35.20	124.29	34.26	2.14	0.36	0.97	116.41	64.35	180.76	4.000	Yes	No	2.00
353	35.30	113.93	38.22	2.19	0.37	0.97	106.38	66.07	172.45	4.000	Yes	No	2.00
354	35.40	99.94	43.93	2.26	0.39	0.97	91.22	66.72	157.95	4.000	Yes	No	2.00
355	35.50	86.32	50.82	2.35	0.41	0.97	77.16	66.82	143.99	4.000	Yes	No	2.00
356	35.60	78.64	55.86	2.41	0.43	0.96	68.25	66.46	134.71	4.000	Yes	No	2.00
357	35.70	79.44	56.89	2.42	0.43	0.96	69.66	67.22	136.88	4.000	Yes	No	2.00
358	35.80	87.98	53.84	2.39	0.41	0.96	79.11	68.65	147.76	4.000	Yes	No	2.00
359	35.90	100.57	48.42	2.32	0.39	0.96	91.64	69.46	161.10	4.000	Yes	No	2.00
360	36.00	113.44	42.32	2.24	0.37	0.97	104.24	68.87	173.10	4.000	Yes	No	2.00
361	36.10	124.61	36.68	2.17	0.36	0.97	114.45	66.49	180.94	4.000	Yes	No	2.00
362	36.20	133.12	32.61	2.12	0.35	0.97	122.25	63.65	185.90	4.000	Yes	No	2.00
363	36.30	139.52	30.34	2.09	0.34	0.96	127.44	61.63	189.07	1.077	No	No	1.18
364	36.40	144.03	29.41	2.08	0.34	0.96	131.79	61.09	192.88	1.296	No	No	1.41
365	36.50	146.71	29.49	2.08	0.33	0.96	134.38	61.74	196.12	1.531	No	No	1.67
366	36.60	146.25	30.45	2.09	0.33	0.96	134.54	63.24	197.78	1.673	No	No	1.82
367	36.70	142.03	32.09	2.11	0.34	0.96	130.21	64.66	194.87	1.434	No	No	1.56
368	36.80	135.41	34.07	2.14	0.35	0.96	122.32	65.44	187.76	1.014	No	No	1.11
369	36.90	129.09	35.51	2.16	0.36	0.96	115.80	65.60	181.40	0.769	No	No	0.84
370	37.00	125.04	35.76	2.16	0.36	0.96	112.31	65.07	177.38	0.656	No	No	0.71
371	37.10	122.66	35.37	2.15	0.36	0.95	110.72	64.30	175.02	0.601	No	No	0.65
372	37.20	121.21	35.06	2.15	0.37	0.95	108.83	63.55	172.38	0.547	No	No	0.59
373	37.30	120.82	35.10	2.15	0.37	0.95	107.92	63.38	171.31	0.527	No	No	0.57
374	37.40	121.89	35.11	2.15	0.37	0.95	109.31	63.70	173.01	0.559	No	No	0.60
375	37.50	124.48	34.78	2.15	0.36	0.95	111.45	63.82	175.27	0.606	No	No	0.66
376	37.60	127.71	34.15	2.14	0.36	0.95	114.72	63.85	178.57	0.687	No	No	0.74
377	37.70	130.82	33.29	2.13	0.36	0.95	117.88	63.54	181.42	0.770	No	No	0.83
378	37.80	132.63	32.77	2.12	0.35	0.95	119.64	63.28	182.92	0.820	No	No	0.89
379	37.90	132.47	32.76	2.12	0.35	0.95	119.35	63.20	182.56	0.807	No	No	0.88
380	38.00	129.59	33.60	2.13	0.36	0.95	117.10	63.74	180.83	0.752	No	No	0.81
381	38.10	123.93	35.30	2.15	0.36	0.95	111.39	64.37	175.76	0.617	No	No	0.67
382	38.20	115.89	37.84	2.19	0.37	0.94	103.49	65.05	168.54	0.480	No	No	0.52
383	38.30	107.14	40.94	2.22	0.39	0.94	94.75	65.51	160.27	0.374	No	No	0.40
384	38.40	98.41	43.86	2.26	0.40	0.94	87.21	65.66	152.87	0.309	No	No	0.33

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
385	38.50	90.54	46.30	2.29	0.41	0.93	79.43	65.14	144.57	0.257	No	No	0.27
386	38.60	84.03	48.17	2.31	0.42	0.93	73.09	64.48	137.57	0.224	No	No	0.24
387	38.70	79.79	49.95	2.34	0.43	0.93	69.32	64.34	133.66	0.210	No	No	0.22
388	38.80	77.78	50.94	2.35	0.43	0.93	67.72	64.36	132.08	0.204	No	No	0.22
389	38.90	77.14	50.85	2.35	0.43	0.93	67.45	64.25	131.70	0.203	No	No	0.22
390	39.00	77.04	50.33	2.34	0.44	0.93	67.37	64.00	131.36	0.202	No	No	0.21
391	39.10	76.57	50.30	2.34	0.44	0.92	67.23	63.95	131.18	0.201	No	No	0.21
392	39.20	75.78	51.20	2.35	0.44	0.92	65.94	64.00	129.94	0.197	No	No	0.21
393	39.30	75.01	52.61	2.37	0.44	0.92	65.04	64.34	129.38	0.196	No	No	0.21
394	39.40	74.55	54.08	2.39	0.44	0.92	64.98	64.91	129.88	0.197	No	No	0.21
395	39.50	74.00	55.24	2.40	0.44	0.92	64.52	65.21	129.73	0.197	No	No	0.21
396	39.60	73.21	55.38	2.40	0.44	0.92	63.36	64.95	128.31	0.193	No	No	0.20
397	39.70	72.79	54.77	2.40	0.44	0.92	62.66	64.53	127.19	0.189	No	No	0.20
398	39.80	72.42	54.30	2.39	0.44	0.92	63.18	64.50	127.68	0.191	No	No	0.20
399	39.90	70.13	54.56	2.39	0.44	0.91	62.14	64.31	126.45	0.187	No	No	0.20
400	40.00	66.57	55.88	2.41	0.46	0.91	56.37	63.20	119.57	0.170	No	No	0.18
401	40.10	63.68	57.34	2.43	0.46	0.91	53.53	62.91	116.44	0.164	No	No	0.17
402	40.20	64.36	57.72	2.43	0.46	0.91	54.29	63.24	117.53	0.166	No	No	0.18
403	40.30	68.83	55.99	2.41	0.45	0.91	57.97	63.68	121.65	0.175	No	No	0.19
404	40.40	77.61	51.96	2.36	0.44	0.91	65.18	64.11	129.29	0.195	No	No	0.21
405	40.50	91.92	45.56	2.28	0.42	0.91	77.36	64.20	141.56	0.242	No	No	0.26
406	40.60	111.46	37.50	2.18	0.39	0.92	95.87	62.96	158.82	0.360	No	No	0.38
407	40.70	133.56	29.27	2.08	0.36	0.92	117.15	57.95	175.11	0.603	No	No	0.65
408	40.80	153.43	23.20	2.00	0.35	0.93	136.30	50.04	186.34	0.951	No	No	1.02
409	40.90	167.80	19.89	1.96	0.34	0.93	148.79	43.26	192.05	1.244	No	No	1.33
410	41.00	176.80	17.69	1.93	0.34	0.93	155.19	37.19	192.38	1.264	No	No	1.35
411	41.10	182.80	16.55	1.92	0.34	0.92	159.85	33.77	193.62	1.345	No	No	1.44
412	41.20	187.72	16.20	1.92	0.33	0.93	164.38	32.98	197.36	1.635	No	No	1.75
413	41.30	191.80	17.08	1.93	0.32	0.93	168.31	36.54	204.85	2.515	No	No	2.00
414	41.40	194.68	17.88	1.94	0.32	0.93	171.03	39.66	210.68	3.651	No	No	2.00
415	41.50	197.00	18.18	1.94	0.31	0.93	172.36	40.86	213.22	4.000	No	No	2.00
416	41.60	199.27	18.21	1.94	0.31	0.93	174.57	41.20	215.78	4.000	No	No	2.00
417	41.70	202.25	18.07	1.94	0.31	0.93	176.97	41.00	217.98	4.000	No	No	2.00
418	41.80	205.69	18.12	1.94	0.30	0.93	180.22	41.57	221.79	4.000	No	No	2.00
419	41.90	209.24	18.56	1.94	0.29	0.93	183.83	43.52	227.34	4.000	No	No	2.00
420	42.00	212.51	18.99	1.95	0.29	0.93	186.68	45.34	232.02	4.000	No	No	2.00
421	42.10	214.98	19.25	1.95	0.28	0.93	189.18	46.57	235.75	4.000	No	No	2.00
422	42.20	216.82	19.19	1.95	0.28	0.93	190.46	46.53	236.99	4.000	No	No	2.00
423	42.30	217.44	19.06	1.95	0.28	0.93	191.42	46.19	237.61	4.000	No	No	2.00
424	42.40	215.99	19.24	1.95	0.28	0.93	190.49	46.69	237.17	4.000	No	No	2.00
425	42.50	212.38	19.85	1.96	0.29	0.93	186.06	48.16	234.21	4.000	No	No	2.00
426	42.60	207.75	20.65	1.97	0.29	0.92	181.14	50.01	231.16	4.000	No	No	2.00
427	42.70	203.54	21.21	1.98	0.29	0.92	177.41	51.14	228.55	4.000	No	No	2.00
428	42.80	199.98	21.49	1.98	0.30	0.92	174.15	51.49	225.63	4.000	No	No	2.00
429	42.90	196.07	21.89	1.99	0.30	0.92	170.95	52.13	223.08	4.000	No	No	2.00
430	43.00	191.21	22.67	2.00	0.30	0.92	166.32	53.51	219.83	4.000	No	No	2.00
431	43.10	185.37	23.73	2.01	0.31	0.92	160.54	55.23	215.77	4.000	No	No	2.00
432	43.20	179.37	25.01	2.03	0.31	0.91	154.74	57.20	211.93	3.972	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
433	43.30	174.19	26.23	2.04	0.32	0.91	149.74	58.87	208.61	3.184	No	No	2.00
434	43.40	170.22	27.20	2.05	0.32	0.91	146.25	60.09	206.35	2.758	No	No	2.00
435	43.50	166.83	27.89	2.06	0.32	0.91	143.69	60.88	204.57	2.472	No	No	2.00
436	43.60	162.46	28.69	2.07	0.33	0.91	140.29	61.60	201.89	2.108	No	No	2.00
437	43.70	156.00	30.24	2.09	0.33	0.91	134.12	62.85	196.96	1.601	No	No	1.70
438	43.80	147.22	32.60	2.12	0.34	0.90	126.00	64.43	190.42	1.149	No	No	1.23
439	43.90	136.83	35.61	2.16	0.35	0.90	116.45	65.85	182.30	0.798	No	No	0.85
440	44.00	126.19	38.88	2.20	0.37	0.89	106.08	66.57	172.65	0.552	No	No	0.59
441	44.10	116.68	41.74	2.23	0.38	0.89	97.39	66.75	164.15	0.419	No	No	0.45
442	44.20	109.12	43.45	2.26	0.39	0.89	90.94	66.34	157.28	0.345	No	No	0.37
443	44.30	103.32	43.23	2.25	0.40	0.88	85.79	64.90	150.69	0.293	No	No	0.31
444	44.40	98.06	41.59	2.23	0.41	0.88	81.75	62.80	144.55	0.257	No	No	0.27
445	44.50	92.45	39.75	2.21	0.43	0.87	76.69	60.24	136.93	0.222	No	No	0.24
446	44.60	86.05	39.78	2.21	0.44	0.87	70.77	58.84	129.60	0.196	No	No	0.21
447	44.70	79.77	42.55	2.24	0.45	0.87	64.90	59.26	124.16	0.181	No	No	0.19
448	44.80	74.72	46.64	2.30	0.46	0.86	60.38	60.41	120.79	0.173	No	No	0.18
449	44.90	71.40	49.61	2.33	0.46	0.86	57.76	61.14	118.90	0.169	No	No	0.18
450	45.00	69.26	51.27	2.35	0.46	0.86	56.37	61.47	117.84	0.167	No	No	0.18
451	45.10	69.08	52.14	2.36	0.46	0.86	54.80	61.40	116.21	0.163	No	No	0.17
452	45.20	73.88	51.06	2.35	0.46	0.86	57.16	61.60	118.76	0.169	No	No	0.18
453	45.30	86.95	45.84	2.29	0.44	0.86	68.41	62.06	130.47	0.199	No	No	0.21
454	45.40	107.24	37.18	2.18	0.41	0.87	88.09	60.86	148.94	0.282	No	No	0.30
455	45.50	130.79	28.41	2.07	0.38	0.88	109.11	55.06	164.18	0.419	No	No	0.45
456	45.60	152.68	22.09	1.99	0.36	0.88	128.90	46.26	175.15	0.604	No	No	0.64
457	45.70	171.44	17.94	1.94	0.36	0.89	144.33	36.77	181.11	0.760	No	No	0.81
458	45.80	188.25	15.60	1.91	0.35	0.89	157.36	30.09	187.45	0.999	No	No	1.06
459	45.90	205.84	13.48	1.88	0.34	0.89	172.32	23.12	195.44	1.477	No	No	1.56
460	46.00	224.66	11.02	1.85	0.32	0.89	190.10	14.10	204.20	2.417	No	No	2.00
461	46.10	242.48	8.15	1.81	0.32	0.90	206.52	4.68	211.20	3.779	No	No	2.00
462	46.20	256.90	5.41	1.78	0.30	0.90	219.18	0.41	219.60	4.000	No	No	2.00
463	46.30	266.83	4.48	1.77	0.29	0.90	228.61	0.09	228.69	4.000	No	No	2.00
464	46.40	272.73	4.65	1.77	0.29	0.90	233.50	0.13	233.63	4.000	No	No	2.00
465	46.50	275.32	4.67	1.77	0.29	0.90	235.33	0.13	235.46	4.000	No	No	2.00
466	46.60	276.13	4.58	1.77	0.29	0.90	235.41	0.11	235.52	4.000	No	No	2.00
467	46.70	276.72	4.44	1.77	0.29	0.90	235.28	0.08	235.36	4.000	No	No	2.00
468	46.80	278.32	5.65	1.78	0.28	0.90	236.53	0.60	237.13	4.000	No	No	2.00
469	46.90	282.43	6.31	1.79	0.28	0.90	239.57	1.26	240.83	4.000	No	No	2.00
470	47.00	288.11	6.11	1.79	0.27	0.90	246.57	1.04	247.61	4.000	No	No	2.00
471	47.10	291.48	5.06	1.78	0.27	0.91	252.19	0.27	252.45	4.000	No	No	2.00
472	47.20	287.17	5.07	1.78	0.27	0.90	248.55	0.27	248.82	4.000	No	No	2.00
473	47.30	273.91	7.08	1.80	0.28	0.90	233.94	2.47	236.40	4.000	No	No	2.00
474	47.40	254.36	11.10	1.85	0.29	0.90	215.72	15.45	231.17	4.000	No	No	2.00
475	47.50	231.51	16.18	1.91	0.29	0.90	196.68	36.03	232.71	4.000	No	No	2.00
476	47.60	207.31	21.54	1.98	0.30	0.89	174.61	51.68	226.29	4.000	No	No	2.00
477	47.70	183.14	26.96	2.05	0.31	0.89	152.69	60.84	213.53	4.000	No	No	2.00
478	47.80	161.34	31.97	2.11	0.33	0.88	132.76	65.04	197.80	1.675	No	No	1.76
479	47.90	147.04	35.81	2.16	0.35	0.87	116.59	66.09	182.68	0.811	No	No	0.86
480	48.00	144.37	36.99	2.17	0.36	0.87	114.54	66.82	181.36	0.768	No	No	0.82

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
481	48.10	154.30	34.89	2.15	0.34	0.87	125.50	67.10	192.60	1.278	No	No	1.35
482	48.20	174.92	30.16	2.09	0.32	0.88	142.64	64.46	207.10	2.891	No	No	2.00
483	48.30	203.69	23.56	2.01	0.30	0.89	168.81	56.18	224.99	4.000	No	No	2.00
484	48.40	238.64	16.08	1.91	0.28	0.89	200.80	36.01	236.82	4.000	No	No	2.00
485	48.50	272.42	9.20	1.83	0.28	0.89	233.34	8.39	241.73	4.000	No	No	2.00
486	48.60	297.48	4.50	1.77	0.26	0.90	256.80	0.10	256.90	4.000	No	No	2.00
487	48.70	309.01	2.87	1.75	0.26	0.90	265.83	0.00	265.83	4.000	No	No	2.00
488	48.80	310.28	3.77	1.76	0.26	0.90	263.57	0.02	263.59	4.000	No	No	2.00
489	48.90	308.58	5.83	1.79	0.26	0.90	259.55	0.79	260.34	4.000	No	No	2.00
490	49.00	308.74	7.88	1.81	0.26	0.90	261.02	4.57	265.59	4.000	No	No	2.00
491	49.10	309.55	9.58	1.83	0.26	0.90	263.50	10.53	274.03	4.000	No	No	2.00
492	49.20	307.77	11.17	1.85	0.26	0.89	261.12	17.55	278.67	4.000	No	No	2.00
493	49.30	300.75	12.43	1.87	0.26	0.89	256.03	23.49	279.51	4.000	No	No	2.00
494	49.40	287.55	13.31	1.88	0.26	0.89	245.22	27.16	272.39	4.000	No	No	2.00
495	49.50	266.11	14.04	1.89	0.26	0.89	227.22	29.36	256.59	4.000	No	No	2.00
496	49.60	239.13	15.34	1.90	0.29	0.88	199.14	32.83	231.98	4.000	No	No	2.00
497	49.70	219.20	16.65	1.92	0.32	0.87	172.39	35.42	207.81	3.025	No	No	2.00

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q_t :	Total cone resistance
FC:	Fines content (%)
I_c :	Soil behavior type index
m:	Stress exponent
C_N :	Overburden correction factor
q_{c1N} :	Normalized and adjusted cone resistance
Δq_{c1N} :	Cone resistance correction factor due to fines
$q_{c1N,cs}$:	Normalized and adjusted cone resistance
CRR _{7.5} :	Cyclic resistance ratio for $M_w=7.5$
FS:	Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
0.10	2.00	0.00	0.00	0.10	0.00	0.20	2.00	0.00	0.00	0.10	0.00
0.30	2.00	0.00	0.00	0.10	0.00	0.40	2.00	0.00	0.00	0.10	0.00
0.50	2.00	0.00	0.00	0.10	0.00	0.60	2.00	0.00	0.00	0.10	0.00
0.70	2.00	0.00	0.00	0.10	0.00	0.80	2.00	0.00	0.00	0.10	0.00
0.90	2.00	0.00	0.00	0.10	0.00	1.00	2.00	0.00	0.00	0.10	0.00
1.10	2.00	0.00	0.00	0.10	0.00	1.20	2.00	0.00	0.00	0.10	0.00
1.30	2.00	0.00	0.00	0.10	0.00	1.40	2.00	0.00	0.00	0.10	0.00
1.50	2.00	0.00	0.00	0.10	0.00	1.60	2.00	0.00	0.00	0.10	0.00
1.70	2.00	0.00	0.00	0.10	0.00	1.80	2.00	0.00	0.00	0.10	0.00
1.90	2.00	0.00	0.00	0.10	0.00	2.00	2.00	0.00	0.00	0.10	0.00
2.10	2.00	0.00	0.00	0.10	0.00	2.20	2.00	0.00	0.00	0.10	0.00
2.30	2.00	0.00	0.00	0.10	0.00	2.40	2.00	0.00	0.00	0.10	0.00
2.50	2.00	0.00	0.00	0.10	0.00	2.60	2.00	0.00	0.00	0.10	0.00
2.70	2.00	0.00	0.00	0.10	0.00	2.80	2.00	0.00	0.00	0.10	0.00
2.90	2.00	0.00	0.00	0.10	0.00	3.00	2.00	0.00	0.00	0.10	0.00
3.10	2.00	0.00	0.00	0.10	0.00	3.20	2.00	0.00	0.00	0.10	0.00
3.30	2.00	0.00	0.00	0.10	0.00	3.40	2.00	0.00	0.00	0.10	0.00
3.50	2.00	0.00	0.00	0.10	0.00	3.60	2.00	0.00	0.00	0.10	0.00
3.70	2.00	0.00	0.00	0.10	0.00	3.80	2.00	0.00	0.00	0.10	0.00
3.90	2.00	0.00	0.00	0.10	0.00	4.00	2.00	0.00	0.00	0.10	0.00
4.10	2.00	0.00	0.00	0.10	0.00	4.20	2.00	0.00	0.00	0.10	0.00
4.30	2.00	0.00	0.00	0.10	0.00	4.40	2.00	0.00	0.00	0.10	0.00
4.50	2.00	0.00	0.00	0.10	0.00	4.60	2.00	0.00	0.00	0.10	0.00
4.70	2.00	0.00	0.00	0.10	0.00	4.80	2.00	0.00	0.00	0.10	0.00
4.90	2.00	0.00	0.00	0.10	0.00	5.00	2.00	0.00	0.00	0.10	0.00
5.10	2.00	0.00	0.00	0.10	0.00	5.20	2.00	0.00	0.00	0.10	0.00
5.30	2.00	0.00	0.00	0.10	0.00	5.40	2.00	0.00	0.00	0.10	0.00
5.50	2.00	0.00	0.00	0.10	0.00	5.60	2.00	0.00	0.00	0.10	0.00
5.70	2.00	0.00	0.00	0.10	0.00	5.80	2.00	0.00	0.00	0.10	0.00
5.90	2.00	0.00	0.00	0.10	0.00	6.00	2.00	0.00	0.00	0.10	0.00
6.10	2.00	0.00	0.00	0.10	0.00	6.20	2.00	0.00	0.00	0.10	0.00
6.30	2.00	0.00	0.00	0.10	0.00	6.40	2.00	0.00	0.00	0.10	0.00
6.50	2.00	0.00	0.00	0.10	0.00	6.60	2.00	0.00	0.00	0.10	0.00
6.70	2.00	0.00	0.00	0.10	0.00	6.80	2.00	0.00	0.00	0.10	0.00
6.90	2.00	0.00	0.00	0.10	0.00	7.00	2.00	0.00	0.00	0.10	0.00
7.10	2.00	0.00	0.00	0.10	0.00	7.20	2.00	0.00	0.00	0.10	0.00
7.30	2.00	0.00	0.00	0.10	0.00	7.40	2.00	0.00	0.00	0.10	0.00
7.50	2.00	0.00	0.00	0.10	0.00	7.60	2.00	0.00	0.00	0.10	0.00
7.70	2.00	0.00	0.00	0.10	0.00	7.80	2.00	0.00	0.00	0.10	0.00
7.90	2.00	0.00	0.00	0.10	0.00	8.00	2.00	0.00	0.00	0.10	0.00
8.10	0.25	0.00	0.00	0.10	0.20	8.20	0.25	0.00	0.00	0.10	0.20
8.30	0.24	0.00	0.00	0.10	0.20	8.40	0.24	0.00	0.00	0.10	0.20
8.50	0.24	0.00	0.00	0.10	0.20	8.60	2.00	0.00	0.00	0.10	0.00
8.70	2.00	0.00	0.00	0.10	0.00	8.80	2.00	0.00	0.00	0.10	0.00
8.90	2.00	0.00	0.00	0.10	0.00	9.00	2.00	0.00	0.00	0.10	0.00
9.10	2.00	0.00	0.00	0.10	0.00	9.20	2.00	0.00	0.00	0.10	0.00
9.30	2.00	0.00	0.00	0.10	0.00	9.40	2.00	0.00	0.00	0.10	0.00
9.50	2.00	0.00	0.00	0.10	0.00	9.60	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
9.70	2.00	0.00	0.00	0.10	0.00	9.80	2.00	0.00	0.00	0.10	0.00
9.90	2.00	0.00	0.00	0.10	0.00	10.00	2.00	0.00	0.00	0.10	0.00
10.10	2.00	0.00	0.00	0.10	0.00	10.20	2.00	0.00	0.00	0.10	0.00
10.30	2.00	0.00	0.00	0.10	0.00	10.40	2.00	0.00	0.00	0.10	0.00
10.50	2.00	0.00	0.00	0.10	0.00	10.60	2.00	0.00	0.00	0.10	0.00
10.70	2.00	0.00	0.00	0.10	0.00	10.80	2.00	0.00	0.00	0.10	0.00
10.90	2.00	0.00	0.00	0.10	0.00	11.00	2.00	0.00	0.00	0.10	0.00
11.10	2.00	0.00	0.00	0.10	0.00	11.20	2.00	0.00	0.00	0.10	0.00
11.30	2.00	0.00	0.00	0.10	0.00	11.40	2.00	0.00	0.00	0.10	0.00
11.50	2.00	0.00	0.00	0.10	0.00	11.60	2.00	0.00	0.00	0.10	0.00
11.70	2.00	0.00	0.00	0.10	0.00	11.80	2.00	0.00	0.00	0.10	0.00
11.90	2.00	0.00	0.00	0.10	0.00	12.00	2.00	0.00	0.00	0.10	0.00
12.10	2.00	0.00	0.00	0.10	0.00	12.20	2.00	0.00	0.00	0.10	0.00
12.30	2.00	0.00	0.00	0.10	0.00	12.40	2.00	0.00	0.00	0.10	0.00
12.50	2.00	0.00	0.00	0.10	0.00	12.60	2.00	0.00	0.00	0.10	0.00
12.70	2.00	0.00	0.00	0.10	0.00	12.80	2.00	0.00	0.00	0.10	0.00
12.90	2.00	0.00	0.00	0.10	0.00	13.00	2.00	0.00	0.00	0.10	0.00
13.10	2.00	0.00	0.00	0.10	0.00	13.20	2.00	0.00	0.00	0.10	0.00
13.30	2.00	0.00	0.00	0.10	0.00	13.40	2.00	0.00	0.00	0.10	0.00
13.50	2.00	0.00	0.00	0.10	0.00	13.60	2.00	0.00	0.00	0.10	0.00
13.70	2.00	0.00	0.00	0.10	0.00	13.80	2.00	0.00	0.00	0.10	0.00
13.90	2.00	0.00	0.00	0.10	0.00	14.00	2.00	0.00	0.00	0.10	0.00
14.10	2.00	0.00	0.00	0.10	0.00	14.20	2.00	0.00	0.00	0.10	0.00
14.30	2.00	0.00	0.00	0.10	0.00	14.40	2.00	0.00	0.00	0.10	0.00
14.50	2.00	0.00	0.00	0.10	0.00	14.60	2.00	0.00	0.00	0.10	0.00
14.70	2.00	0.00	0.00	0.10	0.00	14.80	2.00	0.00	0.00	0.10	0.00
14.90	2.00	0.00	0.00	0.10	0.00	15.00	2.00	0.00	0.00	0.10	0.00
15.10	2.00	0.00	0.00	0.10	0.00	15.20	2.00	0.00	0.00	0.10	0.00
15.30	2.00	0.00	0.00	0.10	0.00	15.40	2.00	0.00	0.00	0.10	0.00
15.50	2.00	0.00	0.00	0.10	0.00	15.60	2.00	0.00	0.00	0.10	0.00
15.70	2.00	0.00	0.00	0.10	0.00	15.80	0.17	0.00	0.00	0.10	0.19
15.90	0.17	0.00	0.00	0.10	0.19	16.00	0.16	0.00	0.00	0.10	0.19
16.10	2.00	0.00	0.00	0.10	0.00	16.20	2.00	0.00	0.00	0.10	0.00
16.30	2.00	0.00	0.00	0.10	0.00	16.40	2.00	0.00	0.00	0.10	0.00
16.50	2.00	0.00	0.00	0.10	0.00	16.60	2.00	0.00	0.00	0.10	0.00
16.70	2.00	0.00	0.00	0.10	0.00	16.80	2.00	0.00	0.00	0.10	0.00
16.90	2.00	0.00	0.00	0.10	0.00	17.00	2.00	0.00	0.00	0.10	0.00
17.10	2.00	0.00	0.00	0.10	0.00	17.20	2.00	0.00	0.00	0.10	0.00
17.30	2.00	0.00	0.00	0.10	0.00	17.40	2.00	0.00	0.00	0.10	0.00
17.50	2.00	0.00	0.00	0.10	0.00	17.60	2.00	0.00	0.00	0.10	0.00
17.70	2.00	0.00	0.00	0.10	0.00	17.80	2.00	0.00	0.00	0.10	0.00
17.90	2.00	0.00	0.00	0.10	0.00	18.00	2.00	0.00	0.00	0.10	0.00
18.10	2.00	0.00	0.00	0.10	0.00	18.20	2.00	0.00	0.00	0.10	0.00
18.30	2.00	0.00	0.00	0.10	0.00	18.40	2.00	0.00	0.00	0.10	0.00
18.50	2.00	0.00	0.00	0.10	0.00	18.60	2.00	0.00	0.00	0.10	0.00
18.70	2.00	0.00	0.00	0.10	0.00	18.80	2.00	0.00	0.00	0.10	0.00
18.90	2.00	0.00	0.00	0.10	0.00	19.00	2.00	0.00	0.00	0.10	0.00
19.10	2.00	0.00	0.00	0.10	0.00	19.20	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
19.30	2.00	0.00	0.00	0.10	0.00	19.40	2.00	0.00	0.00	0.10	0.00
19.50	2.00	0.00	0.00	0.10	0.00	19.60	2.00	0.00	0.00	0.10	0.00
19.70	2.00	0.00	0.00	0.10	0.00	19.80	2.00	0.00	0.00	0.10	0.00
19.90	2.00	0.00	0.00	0.10	0.00	20.00	2.00	0.00	0.00	0.10	0.00
20.10	2.00	0.00	0.00	0.10	0.00	20.20	2.00	0.00	0.00	0.10	0.00
20.30	2.00	0.00	0.00	0.10	0.00	20.40	2.00	0.00	0.00	0.10	0.00
20.50	2.00	0.00	0.00	0.10	0.00	20.60	2.00	0.00	0.00	0.10	0.00
20.70	2.00	0.00	0.00	0.10	0.00	20.80	2.00	0.00	0.00	0.10	0.00
20.90	2.00	0.00	0.00	0.10	0.00	21.00	2.00	0.00	0.00	0.10	0.00
21.10	2.00	0.00	0.00	0.10	0.00	21.20	2.00	0.00	0.00	0.10	0.00
21.30	2.00	0.00	0.00	0.10	0.00	21.40	2.00	0.00	0.00	0.10	0.00
21.50	2.00	0.00	0.00	0.10	0.00	21.60	2.00	0.00	0.00	0.10	0.00
21.70	2.00	0.00	0.00	0.10	0.00	21.80	2.00	0.00	0.00	0.10	0.00
21.90	2.00	0.00	0.00	0.10	0.00	22.00	2.00	0.00	0.00	0.10	0.00
22.10	2.00	0.00	0.00	0.10	0.00	22.20	2.00	0.00	0.00	0.10	0.00
22.30	2.00	0.00	0.00	0.10	0.00	22.40	2.00	0.00	0.00	0.10	0.00
22.50	2.00	0.00	0.00	0.10	0.00	22.60	2.00	0.00	0.00	0.10	0.00
22.70	2.00	0.00	0.00	0.10	0.00	22.80	2.00	0.00	0.00	0.10	0.00
22.90	2.00	0.00	0.00	0.10	0.00	23.00	0.16	0.00	0.00	0.10	0.17
23.10	0.16	0.00	0.00	0.10	0.16	23.20	0.16	0.00	0.00	0.10	0.17
23.30	0.15	0.00	0.00	0.10	0.17	23.40	2.00	0.00	0.00	0.10	0.00
23.50	2.00	0.00	0.00	0.10	0.00	23.60	2.00	0.00	0.00	0.10	0.00
23.70	2.00	0.00	0.00	0.10	0.00	23.80	2.00	0.00	0.00	0.10	0.00
23.90	2.00	0.00	0.00	0.10	0.00	24.00	2.00	0.00	0.00	0.10	0.00
24.10	2.00	0.00	0.00	0.10	0.00	24.20	2.00	0.00	0.00	0.10	0.00
24.30	2.00	0.00	0.00	0.10	0.00	24.40	2.00	0.00	0.00	0.10	0.00
24.50	2.00	0.00	0.00	0.10	0.00	24.60	2.00	0.00	0.00	0.10	0.00
24.70	2.00	0.00	0.00	0.10	0.00	24.80	2.00	0.00	0.00	0.10	0.00
24.90	2.00	0.00	0.00	0.10	0.00	25.00	2.00	0.00	0.00	0.10	0.00
25.10	2.00	0.00	0.00	0.10	0.00	25.20	2.00	0.00	0.00	0.10	0.00
25.30	2.00	0.00	0.00	0.10	0.00	25.40	2.00	0.00	0.00	0.10	0.00
25.50	2.00	0.00	0.00	0.10	0.00	25.60	2.00	0.00	0.00	0.10	0.00
25.70	2.00	0.00	0.00	0.10	0.00	25.80	2.00	0.00	0.00	0.10	0.00
25.90	2.00	0.00	0.00	0.10	0.00	26.00	2.00	0.00	0.00	0.10	0.00
26.10	2.00	0.00	0.00	0.10	0.00	26.20	2.00	0.00	0.00	0.10	0.00
26.30	2.00	0.00	0.00	0.10	0.00	26.40	2.00	0.00	0.00	0.10	0.00
26.50	2.00	0.00	0.00	0.10	0.00	26.60	2.00	0.00	0.00	0.10	0.00
26.70	2.00	0.00	0.00	0.10	0.00	26.80	2.00	0.00	0.00	0.10	0.00
26.90	2.00	0.00	0.00	0.10	0.00	27.00	2.00	0.00	0.00	0.10	0.00
27.10	2.00	0.00	0.00	0.10	0.00	27.20	2.00	0.00	0.00	0.10	0.00
27.30	2.00	0.00	0.00	0.10	0.00	27.40	2.00	0.00	0.00	0.10	0.00
27.50	2.00	0.00	0.00	0.10	0.00	27.60	2.00	0.00	0.00	0.10	0.00
27.70	2.00	0.00	0.00	0.10	0.00	27.80	2.00	0.00	0.00	0.10	0.00
27.90	2.00	0.00	0.00	0.10	0.00	28.00	2.00	0.00	0.00	0.10	0.00
28.10	2.00	0.00	0.00	0.10	0.00	28.20	2.00	0.00	0.00	0.10	0.00
28.30	2.00	0.00	0.00	0.10	0.00	28.40	2.00	0.00	0.00	0.10	0.00
28.50	2.00	0.00	0.00	0.10	0.00	28.60	2.00	0.00	0.00	0.10	0.00
28.70	2.00	0.00	0.00	0.10	0.00	28.80	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
28.90	2.00	0.00	0.00	0.10	0.00	29.00	2.00	0.00	0.00	0.10	0.00
29.10	2.00	0.00	0.00	0.10	0.00	29.20	2.00	0.00	0.00	0.10	0.00
29.30	2.00	0.00	0.00	0.10	0.00	29.40	2.00	0.00	0.00	0.10	0.00
29.50	2.00	0.00	0.00	0.10	0.00	29.60	2.00	0.00	0.00	0.10	0.00
29.70	2.00	0.00	0.00	0.10	0.00	29.80	2.00	0.00	0.00	0.10	0.00
29.90	2.00	0.00	0.00	0.10	0.00	30.00	2.00	0.00	0.00	0.10	0.00
30.10	2.00	0.00	0.00	0.10	0.00	30.20	2.00	0.00	0.00	0.10	0.00
30.30	2.00	0.00	0.00	0.10	0.00	30.40	2.00	0.00	0.00	0.10	0.00
30.50	2.00	0.00	0.00	0.10	0.00	30.60	2.00	0.00	0.00	0.10	0.00
30.70	2.00	0.00	0.00	0.10	0.00	30.80	2.00	0.00	0.00	0.10	0.00
30.90	2.00	0.00	0.00	0.10	0.00	31.00	2.00	0.00	0.00	0.10	0.00
31.10	0.16	0.00	0.00	0.10	0.14	31.20	0.16	0.00	0.00	0.10	0.14
31.30	0.15	0.00	0.00	0.10	0.14	31.40	0.15	0.00	0.00	0.10	0.14
31.50	2.00	0.00	0.00	0.10	0.00	31.60	2.00	0.00	0.00	0.10	0.00
31.70	2.00	0.00	0.00	0.10	0.00	31.80	2.00	0.00	0.00	0.10	0.00
31.90	2.00	0.00	0.00	0.10	0.00	32.00	2.00	0.00	0.00	0.10	0.00
32.10	2.00	0.00	0.00	0.10	0.00	32.20	2.00	0.00	0.00	0.10	0.00
32.30	2.00	0.00	0.00	0.10	0.00	32.40	2.00	0.00	0.00	0.10	0.00
32.50	2.00	0.00	0.00	0.10	0.00	32.60	2.00	0.00	0.00	0.10	0.00
32.70	2.00	0.00	0.00	0.10	0.00	32.80	2.00	0.00	0.00	0.10	0.00
32.90	2.00	0.00	0.00	0.10	0.00	33.00	2.00	0.00	0.00	0.10	0.00
33.10	2.00	0.00	0.00	0.10	0.00	33.20	2.00	0.00	0.00	0.10	0.00
33.30	2.00	0.00	0.00	0.10	0.00	33.40	2.00	0.00	0.00	0.10	0.00
33.50	2.00	0.00	0.00	0.10	0.00	33.60	2.00	0.00	0.00	0.10	0.00
33.70	2.00	0.00	0.00	0.10	0.00	33.80	2.00	0.00	0.00	0.10	0.00
33.90	2.00	0.00	0.00	0.10	0.00	34.00	2.00	0.00	0.00	0.10	0.00
34.10	2.00	0.00	0.00	0.10	0.00	34.20	2.00	0.00	0.00	0.10	0.00
34.30	2.00	0.00	0.00	0.10	0.00	34.40	2.00	0.00	0.00	0.10	0.00
34.50	2.00	0.00	0.00	0.10	0.00	34.60	2.00	0.00	0.00	0.10	0.00
34.70	2.00	0.00	0.00	0.10	0.00	34.80	2.00	0.00	0.00	0.10	0.00
34.90	2.00	0.00	0.00	0.10	0.00	35.00	2.00	0.00	0.00	0.10	0.00
35.10	0.92	0.00	0.00	0.10	0.01	35.20	2.00	0.00	0.00	0.10	0.00
35.30	2.00	0.00	0.00	0.10	0.00	35.40	2.00	0.00	0.00	0.10	0.00
35.50	2.00	0.00	0.00	0.10	0.00	35.60	2.00	0.00	0.00	0.10	0.00
35.70	2.00	0.00	0.00	0.10	0.00	35.80	2.00	0.00	0.00	0.10	0.00
35.90	2.00	0.00	0.00	0.10	0.00	36.00	2.00	0.00	0.00	0.10	0.00
36.10	2.00	0.00	0.00	0.10	0.00	36.20	2.00	0.00	0.00	0.10	0.00
36.30	1.18	0.00	0.00	0.10	0.00	36.40	1.41	0.00	0.00	0.10	0.00
36.50	1.67	0.00	0.00	0.10	0.00	36.60	1.82	0.00	0.00	0.10	0.00
36.70	1.56	0.00	0.00	0.10	0.00	36.80	1.11	0.00	0.00	0.10	0.00
36.90	0.84	0.00	0.00	0.10	0.02	37.00	0.71	0.00	0.00	0.10	0.04
37.10	0.65	0.00	0.00	0.10	0.05	37.20	0.59	0.00	0.00	0.10	0.05
37.30	0.57	0.00	0.00	0.10	0.06	37.40	0.60	0.00	0.00	0.10	0.05
37.50	0.66	0.00	0.00	0.10	0.04	37.60	0.74	0.00	0.00	0.10	0.03
37.70	0.83	0.00	0.00	0.10	0.02	37.80	0.89	0.00	0.00	0.10	0.01
37.90	0.88	0.00	0.00	0.10	0.02	38.00	0.81	0.00	0.00	0.10	0.02
38.10	0.67	0.00	0.00	0.10	0.04	38.20	0.52	0.00	0.00	0.10	0.06
38.30	0.40	0.00	0.00	0.10	0.08	38.40	0.33	0.00	0.00	0.10	0.08

:: Liquefaction Potential Index calculation data ::

Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
38.50	0.27	0.00	0.00	0.10	0.09	38.60	0.24	0.00	0.00	0.10	0.10
38.70	0.22	0.00	0.00	0.10	0.10	38.80	0.22	0.00	0.00	0.10	0.10
38.90	0.22	0.00	0.00	0.10	0.10	39.00	0.21	0.00	0.00	0.10	0.10
39.10	0.21	0.00	0.00	0.10	0.10	39.20	0.21	0.00	0.00	0.10	0.10
39.30	0.21	0.00	0.00	0.10	0.10	39.40	0.21	0.00	0.00	0.10	0.10
39.50	0.21	0.00	0.00	0.10	0.10	39.60	0.20	0.00	0.00	0.10	0.10
39.70	0.20	0.00	0.00	0.10	0.10	39.80	0.20	0.00	0.00	0.10	0.10
39.90	0.20	0.00	0.00	0.10	0.10	40.00	0.18	0.00	0.00	0.10	0.10
40.10	0.17	0.00	0.00	0.10	0.10	40.20	0.18	0.00	0.00	0.10	0.10
40.30	0.19	0.00	0.00	0.10	0.10	40.40	0.21	0.00	0.00	0.10	0.09
40.50	0.26	0.00	0.00	0.10	0.09	40.60	0.38	0.00	0.00	0.10	0.07
40.70	0.65	0.00	0.00	0.10	0.04	40.80	1.02	0.00	0.00	0.10	0.00
40.90	1.33	0.00	0.00	0.10	0.00	41.00	1.35	0.00	0.00	0.10	0.00
41.10	1.44	0.00	0.00	0.10	0.00	41.20	1.75	0.00	0.00	0.10	0.00
41.30	2.00	0.00	0.00	0.10	0.00	41.40	2.00	0.00	0.00	0.10	0.00
41.50	2.00	0.00	0.00	0.10	0.00	41.60	2.00	0.00	0.00	0.10	0.00
41.70	2.00	0.00	0.00	0.10	0.00	41.80	2.00	0.00	0.00	0.10	0.00
41.90	2.00	0.00	0.00	0.10	0.00	42.00	2.00	0.00	0.00	0.10	0.00
42.10	2.00	0.00	0.00	0.10	0.00	42.20	2.00	0.00	0.00	0.10	0.00
42.30	2.00	0.00	0.00	0.10	0.00	42.40	2.00	0.00	0.00	0.10	0.00
42.50	2.00	0.00	0.00	0.10	0.00	42.60	2.00	0.00	0.00	0.10	0.00
42.70	2.00	0.00	0.00	0.10	0.00	42.80	2.00	0.00	0.00	0.10	0.00
42.90	2.00	0.00	0.00	0.10	0.00	43.00	2.00	0.00	0.00	0.10	0.00
43.10	2.00	0.00	0.00	0.10	0.00	43.20	2.00	0.00	0.00	0.10	0.00
43.30	2.00	0.00	0.00	0.10	0.00	43.40	2.00	0.00	0.00	0.10	0.00
43.50	2.00	0.00	0.00	0.10	0.00	43.60	2.00	0.00	0.00	0.10	0.00
43.70	1.70	0.00	0.00	0.10	0.00	43.80	1.23	0.00	0.00	0.10	0.00
43.90	0.85	0.00	0.00	0.10	0.01	44.00	0.59	0.00	0.00	0.10	0.04
44.10	0.45	0.00	0.00	0.10	0.06	44.20	0.37	0.00	0.00	0.10	0.06
44.30	0.31	0.00	0.00	0.10	0.07	44.40	0.27	0.00	0.00	0.10	0.07
44.50	0.24	0.00	0.00	0.10	0.07	44.60	0.21	0.00	0.00	0.10	0.08
44.70	0.19	0.00	0.00	0.10	0.08	44.80	0.18	0.00	0.00	0.10	0.08
44.90	0.18	0.00	0.00	0.10	0.08	45.00	0.18	0.00	0.00	0.10	0.08
45.10	0.17	0.00	0.00	0.10	0.08	45.20	0.18	0.00	0.00	0.10	0.08
45.30	0.21	0.00	0.00	0.10	0.07	45.40	0.30	0.00	0.00	0.10	0.07
45.50	0.45	0.00	0.00	0.10	0.05	45.60	0.64	0.00	0.00	0.10	0.03
45.70	0.81	0.00	0.00	0.10	0.02	45.80	1.06	0.00	0.00	0.10	0.00
45.90	1.56	0.00	0.00	0.10	0.00	46.00	2.00	0.00	0.00	0.10	0.00
46.10	2.00	0.00	0.00	0.10	0.00	46.20	2.00	0.00	0.00	0.10	0.00
46.30	2.00	0.00	0.00	0.10	0.00	46.40	2.00	0.00	0.00	0.10	0.00
46.50	2.00	0.00	0.00	0.10	0.00	46.60	2.00	0.00	0.00	0.10	0.00
46.70	2.00	0.00	0.00	0.10	0.00	46.80	2.00	0.00	0.00	0.10	0.00
46.90	2.00	0.00	0.00	0.10	0.00	47.00	2.00	0.00	0.00	0.10	0.00
47.10	2.00	0.00	0.00	0.10	0.00	47.20	2.00	0.00	0.00	0.10	0.00
47.30	2.00	0.00	0.00	0.10	0.00	47.40	2.00	0.00	0.00	0.10	0.00
47.50	2.00	0.00	0.00	0.10	0.00	47.60	2.00	0.00	0.00	0.10	0.00
47.70	2.00	0.00	0.00	0.10	0.00	47.80	1.76	0.00	0.00	0.10	0.00
47.90	0.86	0.00	0.00	0.10	0.01	48.00	0.82	0.00	0.00	0.10	0.01

:: Liquefaction Potential Index calculation data ::

Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
48.10	1.35	0.00	0.00	0.10	0.00	48.20	2.00	0.00	0.00	0.10	0.00
48.30	2.00	0.00	0.00	0.10	0.00	48.40	2.00	0.00	0.00	0.10	0.00
48.50	2.00	0.00	0.00	0.10	0.00	48.60	2.00	0.00	0.00	0.10	0.00
48.70	2.00	0.00	0.00	0.10	0.00	48.80	2.00	0.00	0.00	0.10	0.00
48.90	2.00	0.00	0.00	0.10	0.00	49.00	2.00	0.00	0.00	0.10	0.00
49.10	2.00	0.00	0.00	0.10	0.00	49.20	2.00	0.00	0.00	0.10	0.00
49.30	2.00	0.00	0.00	0.10	0.00	49.40	2.00	0.00	0.00	0.10	0.00
49.50	2.00	0.00	0.00	0.10	0.00	49.60	2.00	0.00	0.00	0.10	0.00
49.70	2.00	0.00	0.00	0.10	0.00						

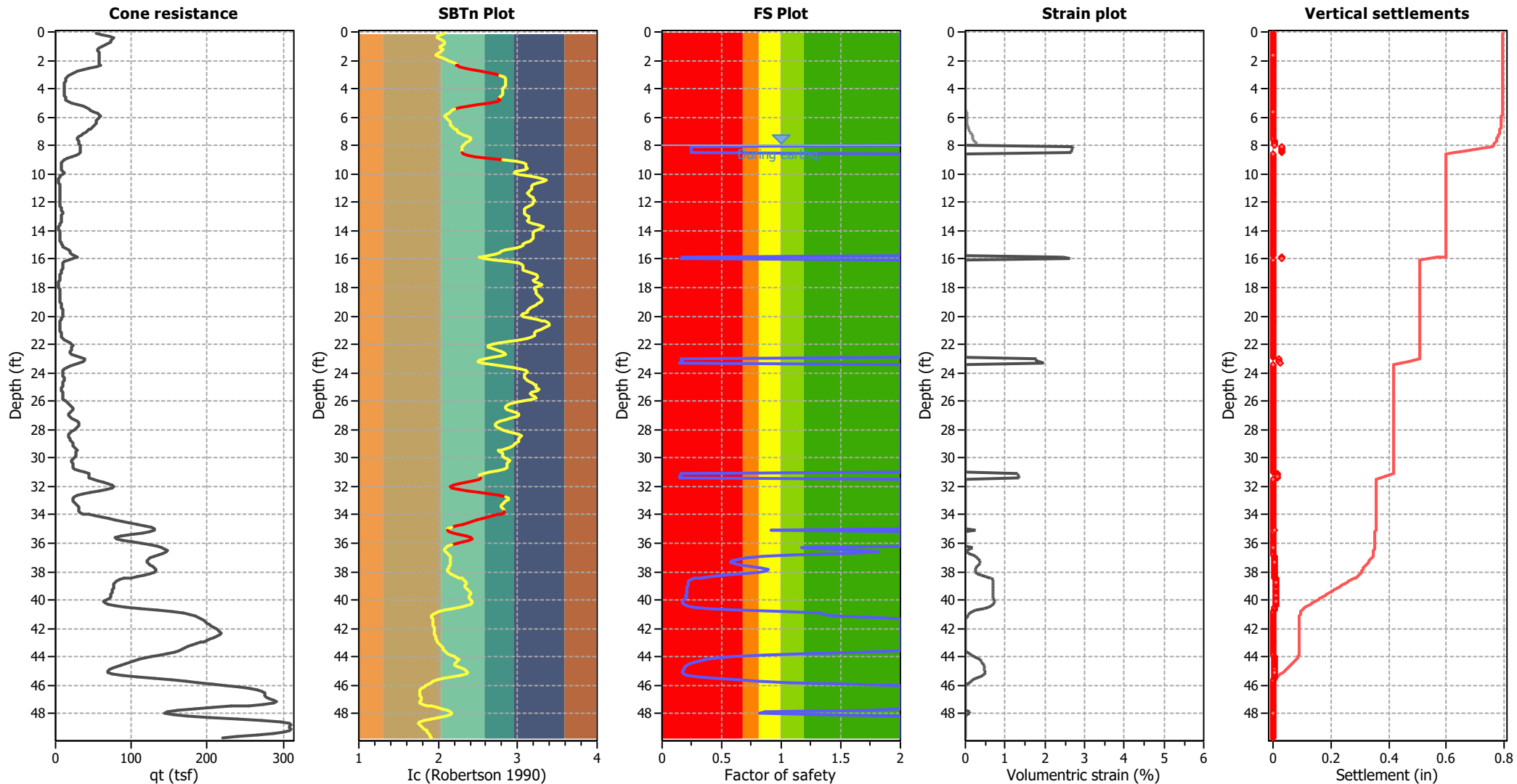
Overall liquefaction potential: 6.82LPI_{ISH} > 5.0 - Liquefaction manifestation is expected**Abbreviations**

FS: Calculated factor of safety for test point

d_z: Layer thickness (ft)

LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

- q_c: Total cone resistance (cone resistance q_c corrected for pore water effects)
- I_c: Soil Behaviour Type Index
- FS: Calculated Factor of Safety against liquefaction
- Volumetric strain: Post-liquefaction volumetric strain

:: Post-earthquake settlement of dry sands ::												
Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
0.10	2.09	84.41	1.40	118.06	25	663	0.56	0.000	0.00	13.69	0.00	0.000
0.20	2.03	98.58	1.34	131.64	28	723	0.55	0.001	0.00	13.69	0.00	0.000
0.30	1.99	114.35	1.30	148.54	31	796	0.54	0.001	0.00	13.69	0.00	0.000
0.40	1.99	121.65	1.30	157.74	33	844	0.54	0.002	0.00	13.69	0.00	0.000
0.50	2.02	120.84	1.32	159.80	33	871	0.54	0.002	0.00	13.69	0.00	0.000
0.60	2.05	117.87	1.36	159.97	34	888	0.54	0.002	0.00	13.69	0.00	0.000
0.70	2.08	114.96	1.38	159.20	34	892	0.54	0.003	0.00	13.69	0.00	0.000
0.80	2.07	111.21	1.38	153.84	33	861	0.54	0.003	0.00	13.69	0.00	0.000
0.90	2.05	105.56	1.36	143.24	30	795	0.55	0.004	0.00	13.69	0.00	0.000
1.00	2.03	98.69	1.34	131.98	28	726	0.55	0.005	0.00	13.69	0.00	0.000
1.10	2.03	92.85	1.34	124.18	26	683	0.55	0.007	0.00	13.69	0.00	0.000
1.20	2.05	89.82	1.36	121.90	26	676	0.55	0.008	0.01	13.69	0.01	0.000
1.30	2.04	89.66	1.35	120.98	26	669	0.55	0.009	0.01	13.69	0.01	0.000
1.40	2.02	90.60	1.32	119.73	25	652	0.55	0.010	0.01	13.69	0.01	0.000
1.50	1.99	90.87	1.30	117.75	24	629	0.55	0.012	0.01	13.69	0.01	0.000
1.60	1.98	90.72	1.29	117.03	24	622	0.55	0.013	0.01	13.69	0.01	0.000
1.70	2.01	91.13	1.32	119.99	25	652	0.55	0.013	0.01	13.69	0.01	0.000
1.80	2.06	92.23	1.36	125.67	27	699	0.55	0.012	0.01	13.69	0.01	0.000
1.90	2.10	92.97	1.42	131.73	29	743	0.55	0.012	0.01	13.69	0.01	0.000
2.00	2.14	91.53	1.49	136.26	30	773	0.55	0.012	0.01	13.69	0.01	0.000
2.10	2.19	90.39	1.58	142.66	32	806	0.55	0.011	0.01	13.69	0.01	0.000
2.20	2.22	92.12	1.66	152.96	35	856	0.55	0.011	0.01	13.69	0.01	0.000
2.30	2.23	95.04	1.69	160.57	37	895	0.54	0.011	0.01	13.69	0.00	0.000
2.40	2.24	93.61	1.71	160.35	0	0	0.54	0.000	0.00	13.69	0.00	0.000
2.50	2.27	84.70	1.81	153.54	0	0	0.55	0.000	0.00	13.69	0.00	0.000
2.60	2.34	71.52	2.07	148.05	0	0	0.55	0.000	0.00	13.69	0.00	0.000
2.70	2.43	57.95	2.56	148.41	0	0	0.56	0.000	0.00	13.69	0.00	0.000
2.80	2.54	46.74	3.25	151.82	0	0	0.56	0.000	0.00	13.69	0.00	0.000
2.90	2.63	38.31	4.04	154.95	0	0	0.56	0.000	0.00	0.00	0.00	0.000
3.00	2.71	32.22	4.84	155.95	0	0	0.56	0.000	0.00	0.00	0.00	0.000
3.10	2.78	27.32	5.59	152.83	0	0	0.56	0.000	0.00	0.00	0.00	0.000
3.20	2.83	23.57	6.19	145.84	0	0	0.56	0.000	0.00	0.00	0.00	0.000
3.30	2.84	21.48	6.43	138.17	0	0	0.56	0.000	0.00	0.00	0.00	0.000
3.40	2.85	20.40	6.47	131.95	0	0	0.56	0.000	0.00	0.00	0.00	0.000
3.50	2.85	19.62	6.46	126.77	0	0	0.56	0.000	0.00	0.00	0.00	0.000
3.60	2.85	18.57	6.52	121.03	0	0	0.56	0.000	0.00	0.00	0.00	0.000
3.70	2.85	17.61	6.56	115.48	0	0	0.56	0.000	0.00	0.00	0.00	0.000
3.80	2.85	17.01	6.50	110.58	0	0	0.56	0.000	0.00	0.00	0.00	0.000
3.90	2.84	16.78	6.34	106.37	0	0	0.56	0.000	0.00	0.00	0.00	0.000
4.00	2.82	16.77	6.10	102.30	0	0	0.56	0.000	0.00	0.00	0.00	0.000
4.10	2.81	16.76	5.95	99.64	0	0	0.56	0.000	0.00	0.00	0.00	0.000
4.20	2.80	16.75	5.91	99.01	0	0	0.56	0.000	0.00	0.00	0.00	0.000
4.30	2.81	16.74	5.94	99.44	0	0	0.56	0.000	0.00	0.00	0.00	0.000
4.40	2.80	17.11	5.89	100.76	0	0	0.56	0.000	0.00	0.00	0.00	0.000
4.50	2.79	18.23	5.68	103.51	0	0	0.56	0.000	0.00	0.00	0.00	0.000
4.60	2.77	19.50	5.48	106.79	0	0	0.56	0.000	0.00	0.00	0.00	0.000
4.70	2.76	20.39	5.43	110.66	0	0	0.56	0.000	0.00	0.00	0.00	0.000
4.80	2.77	21.24	5.48	116.40	0	0	0.56	0.000	0.00	0.00	0.00	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
4.90	2.74	25.12	5.10	128.18	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.00	2.64	33.50	4.10	137.25	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.10	2.51	45.21	3.04	137.36	0	0	0.56	0.000	0.00	13.69	0.00	0.000
5.20	2.38	56.04	2.29	128.29	0	0	0.55	0.000	0.00	13.69	0.00	0.000
5.30	2.28	63.51	1.85	117.45	0	0	0.55	0.000	0.00	13.69	0.00	0.000
5.40	2.21	68.44	1.64	112.30	0	0	0.55	0.000	0.00	13.69	0.00	0.000
5.50	2.17	73.49	1.55	114.26	0	0	0.55	0.000	0.00	13.69	0.00	0.000
5.60	2.16	80.24	1.51	121.55	27	689	0.55	0.071	0.05	13.69	0.04	0.001
5.70	2.13	87.49	1.47	128.51	28	728	0.55	0.062	0.04	13.69	0.04	0.000
5.80	2.10	92.77	1.42	132.08	29	746	0.55	0.060	0.04	13.69	0.03	0.000
5.90	2.09	93.97	1.40	131.72	28	741	0.55	0.063	0.04	13.69	0.04	0.000
6.00	2.10	91.49	1.41	129.26	28	728	0.55	0.068	0.05	13.69	0.04	0.000
6.10	2.12	87.99	1.45	127.44	28	721	0.55	0.072	0.05	13.69	0.04	0.000
6.20	2.14	85.71	1.48	127.15	28	721	0.55	0.074	0.05	13.69	0.04	0.001
6.30	2.14	84.93	1.49	126.85	28	719	0.55	0.077	0.05	13.69	0.04	0.001
6.40	2.15	83.87	1.50	125.84	28	713	0.55	0.082	0.06	13.69	0.05	0.001
6.50	2.16	81.71	1.52	123.86	27	702	0.55	0.089	0.06	13.69	0.05	0.001
6.60	2.17	79.33	1.54	122.19	27	692	0.55	0.096	0.07	13.69	0.06	0.001
6.70	2.18	76.92	1.57	120.75	27	682	0.55	0.104	0.07	13.69	0.06	0.001
6.80	2.20	73.86	1.61	118.90	27	669	0.55	0.114	0.08	13.69	0.07	0.001
6.90	2.22	69.88	1.66	116.25	26	650	0.55	0.131	0.09	13.69	0.08	0.001
7.00	2.24	65.88	1.72	113.25	26	628	0.55	0.153	0.11	13.69	0.09	0.001
7.10	2.25	62.62	1.76	110.02	25	607	0.55	0.182	0.14	13.69	0.11	0.001
7.20	2.27	58.68	1.82	107.08	25	584	0.55	0.220	0.17	13.69	0.14	0.002
7.30	2.32	53.57	1.98	106.25	25	563	0.55	0.267	0.20	13.69	0.17	0.002
7.40	2.37	48.45	2.24	108.71	26	549	0.55	0.311	0.22	13.69	0.18	0.002
7.50	2.41	45.88	2.44	112.00	28	545	0.56	0.330	0.22	13.69	0.18	0.002
7.60	2.41	45.70	2.44	111.51	28	543	0.56	0.347	0.24	13.69	0.20	0.002
7.70	2.39	46.56	2.31	107.58	26	536	0.56	0.381	0.27	13.69	0.23	0.003
7.80	2.36	47.50	2.17	103.12	25	528	0.56	0.427	0.33	13.69	0.27	0.003
7.90	2.33	48.75	2.06	100.22	24	524	0.56	0.457	0.37	13.69	0.30	0.004

Total estimated settlement: 0.03**Abbreviations**

Q_{tn}: Normalized cone resistance
 K_c: Fines correction factor
 Q_{tn,cs}: Equivalent clean sand normalized cone resistance
 G_{max}: Small strain shear modulus
 CSR: Soil cyclic stress ratio
 γ: Cyclic shear strain
 e_{vol(15)}: Volumetric strain after 15 cycles
 N_c: Equivalent number of cycles
 e_v: Volumetric strain
 Settle.: Calculated settlement

:: Post-earthquake settlement due to soil liquefaction ::

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
8.00	102.32	2.00	0.00	0.85	0.00	8.10	101.68	0.25	2.69	0.85	0.03
8.20	101.50	0.25	2.69	0.85	0.03	8.30	101.48	0.24	2.69	0.85	0.03
8.40	101.49	0.24	2.68	0.85	0.03	8.50	101.44	0.24	2.68	0.85	0.03
8.60	99.67	2.00	0.00	0.84	0.00	8.70	95.87	2.00	0.00	0.84	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
8.80	87.99	2.00	0.00	0.84	0.00	8.90	21.58	2.00	0.00	0.84	0.00
9.00	14.55	2.00	0.00	0.84	0.00	9.10	11.88	2.00	0.00	0.83	0.00
9.20	10.43	2.00	0.00	0.83	0.00	9.30	9.69	2.00	0.00	0.83	0.00
9.40	11.01	2.00	0.00	0.83	0.00	9.50	10.51	2.00	0.00	0.83	0.00
9.60	9.20	2.00	0.00	0.83	0.00	9.70	9.40	2.00	0.00	0.82	0.00
9.80	14.15	2.00	0.00	0.82	0.00	9.90	18.77	2.00	0.00	0.82	0.00
10.00	12.10	2.00	0.00	0.82	0.00	10.10	7.97	2.00	0.00	0.82	0.00
10.20	7.15	2.00	0.00	0.81	0.00	10.30	5.49	2.00	0.00	0.81	0.00
10.40	4.88	2.00	0.00	0.81	0.00	10.50	4.59	2.00	0.00	0.81	0.00
10.60	5.85	2.00	0.00	0.81	0.00	10.70	6.77	2.00	0.00	0.81	0.00
10.80	6.76	2.00	0.00	0.80	0.00	10.90	6.74	2.00	0.00	0.80	0.00
11.00	6.73	2.00	0.00	0.80	0.00	11.10	6.72	2.00	0.00	0.80	0.00
11.20	6.70	2.00	0.00	0.80	0.00	11.30	6.69	2.00	0.00	0.79	0.00
11.40	6.68	2.00	0.00	0.79	0.00	11.50	6.66	2.00	0.00	0.79	0.00
11.60	6.65	2.00	0.00	0.79	0.00	11.70	6.64	2.00	0.00	0.79	0.00
11.80	6.62	2.00	0.00	0.79	0.00	11.90	6.61	2.00	0.00	0.78	0.00
12.00	6.60	2.00	0.00	0.78	0.00	12.10	6.58	2.00	0.00	0.78	0.00
12.20	6.57	2.00	0.00	0.78	0.00	12.30	7.43	2.00	0.00	0.78	0.00
12.40	9.43	2.00	0.00	0.77	0.00	12.50	10.10	2.00	0.00	0.77	0.00
12.60	10.73	2.00	0.00	0.77	0.00	12.70	11.24	2.00	0.00	0.77	0.00
12.80	11.53	2.00	0.00	0.77	0.00	12.90	10.99	2.00	0.00	0.77	0.00
13.00	8.85	2.00	0.00	0.76	0.00	13.10	8.91	2.00	0.00	0.76	0.00
13.20	9.87	2.00	0.00	0.76	0.00	13.30	10.22	2.00	0.00	0.76	0.00
13.40	10.29	2.00	0.00	0.76	0.00	13.50	7.87	2.00	0.00	0.75	0.00
13.60	5.68	2.00	0.00	0.75	0.00	13.70	5.05	2.00	0.00	0.75	0.00
13.80	4.99	2.00	0.00	0.75	0.00	13.90	5.06	2.00	0.00	0.75	0.00
14.00	5.98	2.00	0.00	0.75	0.00	14.10	6.69	2.00	0.00	0.74	0.00
14.20	6.82	2.00	0.00	0.74	0.00	14.30	6.29	2.00	0.00	0.74	0.00
14.40	6.79	2.00	0.00	0.74	0.00	14.50	6.62	2.00	0.00	0.74	0.00
14.60	6.50	2.00	0.00	0.73	0.00	14.70	7.27	2.00	0.00	0.73	0.00
14.80	8.62	2.00	0.00	0.73	0.00	14.90	10.72	2.00	0.00	0.73	0.00
15.00	11.15	2.00	0.00	0.73	0.00	15.10	11.34	2.00	0.00	0.73	0.00
15.20	14.76	2.00	0.00	0.72	0.00	15.30	20.25	2.00	0.00	0.72	0.00
15.40	25.72	2.00	0.00	0.72	0.00	15.50	21.23	2.00	0.00	0.72	0.00
15.60	20.94	2.00	0.00	0.72	0.00	15.70	31.97	2.00	0.00	0.71	0.00
15.80	96.80	0.17	2.37	0.71	0.03	15.90	93.07	0.17	2.46	0.71	0.03
16.00	86.42	0.16	2.64	0.71	0.03	16.10	19.07	2.00	0.00	0.71	0.00
16.20	13.35	2.00	0.00	0.71	0.00	16.30	11.98	2.00	0.00	0.70	0.00
16.40	12.80	2.00	0.00	0.70	0.00	16.50	12.23	2.00	0.00	0.70	0.00
16.60	10.60	2.00	0.00	0.70	0.00	16.70	10.94	2.00	0.00	0.70	0.00
16.80	10.34	2.00	0.00	0.69	0.00	16.90	9.45	2.00	0.00	0.69	0.00
17.00	7.97	2.00	0.00	0.69	0.00	17.10	7.21	2.00	0.00	0.69	0.00
17.20	6.25	2.00	0.00	0.69	0.00	17.30	6.27	2.00	0.00	0.69	0.00
17.40	6.36	2.00	0.00	0.68	0.00	17.50	5.87	2.00	0.00	0.68	0.00
17.60	5.68	2.00	0.00	0.68	0.00	17.70	4.54	2.00	0.00	0.68	0.00
17.80	3.91	2.00	0.00	0.68	0.00	17.90	4.61	2.00	0.00	0.67	0.00
18.00	5.72	2.00	0.00	0.67	0.00	18.10	5.82	2.00	0.00	0.67	0.00
18.20	5.43	2.00	0.00	0.67	0.00	18.30	6.39	2.00	0.00	0.67	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
18.40	7.22	2.00	0.00	0.67	0.00	18.50	7.21	2.00	0.00	0.66	0.00
18.60	7.20	2.00	0.00	0.66	0.00	18.70	7.18	2.00	0.00	0.66	0.00
18.80	7.17	2.00	0.00	0.66	0.00	18.90	7.16	2.00	0.00	0.66	0.00
19.00	7.14	2.00	0.00	0.65	0.00	19.10	7.55	2.00	0.00	0.65	0.00
19.20	8.36	2.00	0.00	0.65	0.00	19.30	9.15	2.00	0.00	0.65	0.00
19.40	9.88	2.00	0.00	0.65	0.00	19.50	9.94	2.00	0.00	0.65	0.00
19.60	10.34	2.00	0.00	0.64	0.00	19.70	9.52	2.00	0.00	0.64	0.00
19.80	9.97	2.00	0.00	0.64	0.00	19.90	13.48	2.00	0.00	0.64	0.00
20.00	12.06	2.00	0.00	0.64	0.00	20.10	9.10	2.00	0.00	0.63	0.00
20.20	7.48	2.00	0.00	0.63	0.00	20.30	6.97	2.00	0.00	0.63	0.00
20.40	6.96	2.00	0.00	0.63	0.00	20.50	6.38	2.00	0.00	0.63	0.00
20.60	5.59	2.00	0.00	0.63	0.00	20.70	5.55	2.00	0.00	0.62	0.00
20.80	5.54	2.00	0.00	0.62	0.00	20.90	5.54	2.00	0.00	0.62	0.00
21.00	5.93	2.00	0.00	0.62	0.00	21.10	7.45	2.00	0.00	0.62	0.00
21.20	8.45	2.00	0.00	0.61	0.00	21.30	8.22	2.00	0.00	0.61	0.00
21.40	8.28	2.00	0.00	0.61	0.00	21.50	8.79	2.00	0.00	0.61	0.00
21.60	10.24	2.00	0.00	0.61	0.00	21.70	13.23	2.00	0.00	0.61	0.00
21.80	16.31	2.00	0.00	0.60	0.00	21.90	20.81	2.00	0.00	0.60	0.00
22.00	23.86	2.00	0.00	0.60	0.00	22.10	24.70	2.00	0.00	0.60	0.00
22.20	24.34	2.00	0.00	0.60	0.00	22.30	23.13	2.00	0.00	0.59	0.00
22.40	21.72	2.00	0.00	0.59	0.00	22.50	21.46	2.00	0.00	0.59	0.00
22.60	21.09	2.00	0.00	0.59	0.00	22.70	22.03	2.00	0.00	0.59	0.00
22.80	28.01	2.00	0.00	0.59	0.00	22.90	35.46	2.00	0.00	0.58	0.00
23.00	104.67	0.16	1.78	0.58	0.02	23.10	105.59	0.16	1.76	0.58	0.02
23.20	100.27	0.16	1.85	0.58	0.02	23.30	92.97	0.15	1.99	0.58	0.02
23.40	25.89	2.00	0.00	0.57	0.00	23.50	19.72	2.00	0.00	0.57	0.00
23.60	15.72	2.00	0.00	0.57	0.00	23.70	12.71	2.00	0.00	0.57	0.00
23.80	10.43	2.00	0.00	0.57	0.00	23.90	9.08	2.00	0.00	0.57	0.00
24.00	9.32	2.00	0.00	0.56	0.00	24.10	10.73	2.00	0.00	0.56	0.00
24.20	10.93	2.00	0.00	0.56	0.00	24.30	11.48	2.00	0.00	0.56	0.00
24.40	11.58	2.00	0.00	0.56	0.00	24.50	10.92	2.00	0.00	0.55	0.00
24.60	10.65	2.00	0.00	0.55	0.00	24.70	9.69	2.00	0.00	0.55	0.00
24.80	8.97	2.00	0.00	0.55	0.00	24.90	8.96	2.00	0.00	0.55	0.00
25.00	8.94	2.00	0.00	0.55	0.00	25.10	8.91	2.00	0.00	0.54	0.00
25.20	7.70	2.00	0.00	0.54	0.00	25.30	7.34	2.00	0.00	0.54	0.00
25.40	9.57	2.00	0.00	0.54	0.00	25.50	10.20	2.00	0.00	0.54	0.00
25.60	9.35	2.00	0.00	0.53	0.00	25.70	9.22	2.00	0.00	0.53	0.00
25.80	8.90	2.00	0.00	0.53	0.00	25.90	9.77	2.00	0.00	0.53	0.00
26.00	12.32	2.00	0.00	0.53	0.00	26.10	16.57	2.00	0.00	0.53	0.00
26.20	18.18	2.00	0.00	0.52	0.00	26.30	18.72	2.00	0.00	0.52	0.00
26.40	21.49	2.00	0.00	0.52	0.00	26.50	23.47	2.00	0.00	0.52	0.00
26.60	23.20	2.00	0.00	0.52	0.00	26.70	21.41	2.00	0.00	0.51	0.00
26.80	18.05	2.00	0.00	0.51	0.00	26.90	16.14	2.00	0.00	0.51	0.00
27.00	16.01	2.00	0.00	0.51	0.00	27.10	18.32	2.00	0.00	0.51	0.00
27.20	22.33	2.00	0.00	0.51	0.00	27.30	25.85	2.00	0.00	0.50	0.00
27.40	29.77	2.00	0.00	0.50	0.00	27.50	32.39	2.00	0.00	0.50	0.00
27.60	31.44	2.00	0.00	0.50	0.00	27.70	30.06	2.00	0.00	0.50	0.00
27.80	28.64	2.00	0.00	0.49	0.00	27.90	27.19	2.00	0.00	0.49	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
28.00	25.00	2.00	0.00	0.49	0.00	28.10	21.69	2.00	0.00	0.49	0.00
28.20	18.23	2.00	0.00	0.49	0.00	28.30	16.20	2.00	0.00	0.49	0.00
28.40	15.84	2.00	0.00	0.48	0.00	28.50	17.43	2.00	0.00	0.48	0.00
28.60	18.52	2.00	0.00	0.48	0.00	28.70	18.49	2.00	0.00	0.48	0.00
28.80	20.04	2.00	0.00	0.48	0.00	28.90	21.99	2.00	0.00	0.47	0.00
29.00	23.78	2.00	0.00	0.47	0.00	29.10	23.71	2.00	0.00	0.47	0.00
29.20	22.45	2.00	0.00	0.47	0.00	29.30	24.78	2.00	0.00	0.47	0.00
29.40	28.83	2.00	0.00	0.47	0.00	29.50	29.35	2.00	0.00	0.46	0.00
29.60	26.82	2.00	0.00	0.46	0.00	29.70	24.91	2.00	0.00	0.46	0.00
29.80	24.72	2.00	0.00	0.46	0.00	29.90	27.10	2.00	0.00	0.46	0.00
30.00	24.79	2.00	0.00	0.45	0.00	30.10	20.10	2.00	0.00	0.45	0.00
30.20	19.84	2.00	0.00	0.45	0.00	30.30	21.13	2.00	0.00	0.45	0.00
30.40	22.04	2.00	0.00	0.45	0.00	30.50	22.01	2.00	0.00	0.45	0.00
30.60	21.98	2.00	0.00	0.44	0.00	30.70	21.94	2.00	0.00	0.44	0.00
30.80	23.08	2.00	0.00	0.44	0.00	30.90	28.67	2.00	0.00	0.44	0.00
31.00	37.76	2.00	0.00	0.44	0.00	31.10	107.08	0.16	1.30	0.43	0.02
31.20	105.84	0.16	1.31	0.43	0.02	31.30	101.83	0.15	1.36	0.43	0.02
31.40	102.77	0.15	1.34	0.43	0.02	31.50	109.41	2.00	0.00	0.43	0.00
31.60	116.14	2.00	0.00	0.43	0.00	31.70	121.63	2.00	0.00	0.42	0.00
31.80	125.59	2.00	0.00	0.42	0.00	31.90	128.94	2.00	0.00	0.42	0.00
32.00	131.73	2.00	0.00	0.42	0.00	32.10	130.90	2.00	0.00	0.42	0.00
32.20	124.56	2.00	0.00	0.41	0.00	32.30	115.02	2.00	0.00	0.41	0.00
32.40	104.09	2.00	0.00	0.41	0.00	32.50	32.94	2.00	0.00	0.41	0.00
32.60	26.89	2.00	0.00	0.41	0.00	32.70	22.95	2.00	0.00	0.41	0.00
32.80	21.24	2.00	0.00	0.40	0.00	32.90	21.21	2.00	0.00	0.40	0.00
33.00	21.70	2.00	0.00	0.40	0.00	33.10	23.35	2.00	0.00	0.40	0.00
33.20	25.28	2.00	0.00	0.40	0.00	33.30	27.67	2.00	0.00	0.39	0.00
33.40	29.34	2.00	0.00	0.39	0.00	33.50	28.53	2.00	0.00	0.39	0.00
33.60	27.41	2.00	0.00	0.39	0.00	33.70	27.05	2.00	0.00	0.39	0.00
33.80	28.28	2.00	0.00	0.39	0.00	33.90	32.68	2.00	0.00	0.38	0.00
34.00	39.86	2.00	0.00	0.38	0.00	34.10	47.96	2.00	0.00	0.38	0.00
34.20	56.48	2.00	0.00	0.38	0.00	34.30	134.22	2.00	0.00	0.38	0.00
34.40	142.11	2.00	0.00	0.37	0.00	34.50	150.55	2.00	0.00	0.37	0.00
34.60	159.56	2.00	0.00	0.37	0.00	34.70	169.65	2.00	0.00	0.37	0.00
34.80	179.32	2.00	0.00	0.37	0.00	34.90	184.08	2.00	0.00	0.37	0.00
35.00	184.59	2.00	0.00	0.36	0.00	35.10	183.37	0.92	0.27	0.36	0.00
35.20	180.76	2.00	0.00	0.36	0.00	35.30	172.45	2.00	0.00	0.36	0.00
35.40	157.95	2.00	0.00	0.36	0.00	35.50	143.99	2.00	0.00	0.35	0.00
35.60	134.71	2.00	0.00	0.35	0.00	35.70	136.88	2.00	0.00	0.35	0.00
35.80	147.76	2.00	0.00	0.35	0.00	35.90	161.10	2.00	0.00	0.35	0.00
36.00	173.10	2.00	0.00	0.35	0.00	36.10	180.94	2.00	0.00	0.34	0.00
36.20	185.90	2.00	0.00	0.34	0.00	36.30	189.07	1.18	0.17	0.34	0.00
36.40	192.88	1.41	0.10	0.34	0.00	36.50	196.12	1.67	0.05	0.34	0.00
36.60	197.78	1.82	0.03	0.33	0.00	36.70	194.87	1.56	0.07	0.33	0.00
36.80	187.76	1.11	0.19	0.33	0.00	36.90	181.40	0.84	0.27	0.33	0.00
37.00	177.38	0.71	0.31	0.33	0.00	37.10	175.02	0.65	0.33	0.33	0.00
37.20	172.38	0.59	0.36	0.32	0.00	37.30	171.31	0.57	0.38	0.32	0.00
37.40	173.01	0.60	0.35	0.32	0.00	37.50	175.27	0.66	0.32	0.32	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
37.60	178.57	0.74	0.29	0.32	0.00	37.70	181.42	0.83	0.26	0.31	0.00
37.80	182.92	0.89	0.24	0.31	0.00	37.90	182.56	0.88	0.24	0.31	0.00
38.00	180.83	0.81	0.26	0.31	0.00	38.10	175.76	0.67	0.31	0.31	0.00
38.20	168.54	0.52	0.39	0.31	0.00	38.30	160.27	0.40	0.52	0.30	0.01
38.40	152.87	0.33	0.61	0.30	0.01	38.50	144.57	0.27	0.65	0.30	0.01
38.60	137.57	0.24	0.68	0.30	0.01	38.70	133.66	0.22	0.70	0.30	0.01
38.80	132.08	0.22	0.70	0.29	0.01	38.90	131.70	0.22	0.70	0.29	0.01
39.00	131.36	0.21	0.70	0.29	0.01	39.10	131.18	0.21	0.70	0.29	0.01
39.20	129.94	0.21	0.70	0.29	0.01	39.30	129.38	0.21	0.70	0.29	0.01
39.40	129.88	0.21	0.69	0.28	0.01	39.50	129.73	0.21	0.69	0.28	0.01
39.60	128.31	0.20	0.69	0.28	0.01	39.70	127.19	0.20	0.69	0.28	0.01
39.80	127.68	0.20	0.69	0.28	0.01	39.90	126.45	0.20	0.69	0.27	0.01
40.00	119.57	0.18	0.73	0.27	0.01	40.10	116.44	0.17	0.74	0.27	0.01
40.20	117.53	0.18	0.73	0.27	0.01	40.30	121.65	0.19	0.70	0.27	0.01
40.40	129.29	0.21	0.65	0.27	0.01	40.50	141.56	0.26	0.58	0.26	0.01
40.60	158.82	0.38	0.47	0.26	0.01	40.70	175.11	0.65	0.27	0.26	0.00
40.80	186.34	1.02	0.17	0.26	0.00	40.90	192.05	1.33	0.09	0.26	0.00
41.00	192.38	1.35	0.09	0.25	0.00	41.10	193.62	1.44	0.07	0.25	0.00
41.20	197.36	1.75	0.03	0.25	0.00	41.30	204.85	2.00	0.00	0.25	0.00
41.40	210.68	2.00	0.00	0.25	0.00	41.50	213.22	2.00	0.00	0.25	0.00
41.60	215.78	2.00	0.00	0.24	0.00	41.70	217.98	2.00	0.00	0.24	0.00
41.80	221.79	2.00	0.00	0.24	0.00	41.90	227.34	2.00	0.00	0.24	0.00
42.00	232.02	2.00	0.00	0.24	0.00	42.10	235.75	2.00	0.00	0.23	0.00
42.20	236.99	2.00	0.00	0.23	0.00	42.30	237.61	2.00	0.00	0.23	0.00
42.40	237.17	2.00	0.00	0.23	0.00	42.50	234.21	2.00	0.00	0.23	0.00
42.60	231.16	2.00	0.00	0.23	0.00	42.70	228.55	2.00	0.00	0.22	0.00
42.80	225.63	2.00	0.00	0.22	0.00	42.90	223.08	2.00	0.00	0.22	0.00
43.00	219.83	2.00	0.00	0.22	0.00	43.10	215.77	2.00	0.00	0.22	0.00
43.20	211.93	2.00	0.00	0.21	0.00	43.30	208.61	2.00	0.00	0.21	0.00
43.40	206.35	2.00	0.00	0.21	0.00	43.50	204.57	2.00	0.00	0.21	0.00
43.60	201.89	2.00	0.00	0.21	0.00	43.70	196.96	1.70	0.03	0.21	0.00
43.80	190.42	1.23	0.09	0.20	0.00	43.90	182.30	0.85	0.16	0.20	0.00
44.00	172.65	0.59	0.22	0.20	0.00	44.10	164.15	0.45	0.30	0.20	0.00
44.20	157.28	0.37	0.37	0.20	0.00	44.30	150.69	0.31	0.40	0.19	0.00
44.40	144.55	0.27	0.42	0.19	0.01	44.50	136.93	0.24	0.44	0.19	0.01
44.60	129.60	0.21	0.46	0.19	0.01	44.70	124.16	0.19	0.48	0.19	0.01
44.80	120.79	0.18	0.49	0.19	0.01	44.90	118.90	0.18	0.49	0.18	0.01
45.00	117.84	0.18	0.49	0.18	0.01	45.10	116.21	0.17	0.49	0.18	0.01
45.20	118.76	0.18	0.48	0.18	0.01	45.30	130.47	0.21	0.43	0.18	0.01
45.40	148.94	0.30	0.37	0.17	0.00	45.50	164.18	0.45	0.26	0.17	0.00
45.60	175.15	0.64	0.17	0.17	0.00	45.70	181.11	0.81	0.14	0.17	0.00
45.80	187.45	1.06	0.10	0.17	0.00	45.90	195.44	1.56	0.03	0.17	0.00
46.00	204.20	2.00	0.00	0.16	0.00	46.10	211.20	2.00	0.00	0.16	0.00
46.20	219.60	2.00	0.00	0.16	0.00	46.30	228.69	2.00	0.00	0.16	0.00
46.40	233.63	2.00	0.00	0.16	0.00	46.50	235.46	2.00	0.00	0.15	0.00
46.60	235.52	2.00	0.00	0.15	0.00	46.70	235.36	2.00	0.00	0.15	0.00
46.80	237.13	2.00	0.00	0.15	0.00	46.90	240.83	2.00	0.00	0.15	0.00
47.00	247.61	2.00	0.00	0.15	0.00	47.10	252.45	2.00	0.00	0.14	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
47.20	248.82	2.00	0.00	0.14	0.00	47.30	236.40	2.00	0.00	0.14	0.00
47.40	231.17	2.00	0.00	0.14	0.00	47.50	232.71	2.00	0.00	0.14	0.00
47.60	226.29	2.00	0.00	0.13	0.00	47.70	213.53	2.00	0.00	0.13	0.00
47.80	197.80	1.76	0.01	0.13	0.00	47.90	182.68	0.86	0.10	0.13	0.00
48.00	181.36	0.82	0.10	0.13	0.00	48.10	192.60	1.35	0.04	0.13	0.00
48.20	207.10	2.00	0.00	0.12	0.00	48.30	224.99	2.00	0.00	0.12	0.00
48.40	236.82	2.00	0.00	0.12	0.00	48.50	241.73	2.00	0.00	0.12	0.00
48.60	256.90	2.00	0.00	0.12	0.00	48.70	265.83	2.00	0.00	0.11	0.00
48.80	263.59	2.00	0.00	0.11	0.00	48.90	260.34	2.00	0.00	0.11	0.00
49.00	265.59	2.00	0.00	0.11	0.00	49.10	274.03	2.00	0.00	0.11	0.00
49.20	278.67	2.00	0.00	0.11	0.00	49.30	279.51	2.00	0.00	0.10	0.00
49.40	272.39	2.00	0.00	0.10	0.00	49.50	256.59	2.00	0.00	0.10	0.00
49.60	231.98	2.00	0.00	0.10	0.00	49.70	207.81	2.00	0.00	0.10	0.00

Total estimated settlement: 0.76**Abbreviations**

$Q_{tn,cs}$: Equivalent clean sand normalized cone resistance
 FS: Factor of safety against liquefaction
 e_v (%): Post-liquefaction volumetric strain
 DF: e_v depth weighting factor
 Settlement: Calculated settlement

:: Strength loss calculation Idriss & Boulanger (2008) ::

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.10	52.54	84.41	1.40	118.06	2.09	0.13	0.80
0.20	61.37	98.58	1.34	131.64	2.03	0.17	0.82
0.30	71.19	114.35	1.30	148.54	1.99	0.22	0.85
0.40	75.74	121.65	1.30	157.74	1.99	0.24	0.85
0.50	75.24	120.84	1.32	159.80	2.02	0.23	0.85
0.60	73.40	117.87	1.36	159.97	2.05	0.23	0.85
0.70	71.59	114.96	1.38	159.20	2.08	0.23	0.86
0.80	69.27	111.21	1.38	153.84	2.07	0.22	0.85
0.90	65.76	105.56	1.36	143.24	2.05	0.19	0.84
1.00	61.48	98.69	1.34	131.98	2.03	0.17	0.82
1.10	57.86	92.85	1.34	124.18	2.03	0.15	0.81
1.20	55.98	89.82	1.36	121.90	2.05	0.15	0.81
1.30	55.88	89.66	1.35	120.98	2.04	0.15	0.81
1.40	56.48	90.60	1.32	119.73	2.02	0.15	0.81
1.50	56.65	90.87	1.30	117.75	1.99	0.14	0.80
1.60	56.56	90.72	1.29	117.03	1.98	0.14	0.80
1.70	56.82	91.13	1.32	119.99	2.01	0.15	0.81
1.80	57.51	92.23	1.36	125.67	2.06	0.16	0.82
1.90	57.98	92.97	1.42	131.73	2.10	0.17	0.83
2.00	57.09	91.53	1.49	136.26	2.14	0.17	0.83
2.10	56.39	90.39	1.58	142.66	2.19	0.17	0.83
2.20	57.47	92.12	1.66	152.96	2.22	0.18	0.83
2.30	59.29	95.04	1.69	160.57	2.23	0.20	0.85
2.40	58.41	93.61	1.71	160.35	2.24	0.20	0.85
2.50	52.87	84.70	1.81	153.54	2.27	0.18	0.83
2.60	44.67	71.52	2.07	148.05	2.34	0.15	0.81
2.70	36.23	57.95	2.56	148.41	2.43	0.13	0.79
2.80	29.26	46.74	3.25	151.82	2.54	0.12	0.76
2.90	24.02	38.31	4.04	154.95	2.63	0.11	0.62
3.00	20.23	32.22	4.84	155.95	2.71	0.10	0.62
3.10	17.19	27.32	5.59	152.83	2.78	0.10	0.62
3.20	14.86	23.57	6.19	145.84	2.83	0.09	0.62
3.30	13.57	21.48	6.43	138.17	2.84	0.09	0.62
3.40	12.90	20.40	6.47	131.95	2.85	0.09	0.62
3.50	12.42	19.62	6.46	126.77	2.85	0.09	0.62
3.60	11.77	18.57	6.52	121.03	2.85	0.09	0.62
3.70	11.18	17.61	6.56	115.48	2.85	0.09	0.62
3.80	10.81	17.01	6.50	110.58	2.85	0.08	0.62
3.90	10.67	16.78	6.34	106.37	2.84	0.08	0.62
4.00	10.67	16.77	6.10	102.30	2.82	0.08	0.62
4.10	10.67	16.76	5.95	99.64	2.81	0.08	0.62
4.20	10.67	16.75	5.91	99.01	2.80	0.08	0.62
4.30	10.67	16.74	5.94	99.44	2.81	0.08	0.62
4.40	10.91	17.11	5.89	100.76	2.80	0.08	0.62
4.50	11.61	18.23	5.68	103.51	2.79	0.08	0.62
4.60	12.40	19.50	5.48	106.79	2.77	0.09	0.62
4.70	12.96	20.39	5.43	110.66	2.76	0.09	0.62
4.80	13.50	21.24	5.48	116.40	2.77	0.09	0.62

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
4.90	15.92	25.12	5.10	128.18	2.74	0.09	0.62
5.00	21.14	33.50	4.10	137.25	2.64	0.10	0.62
5.10	28.44	45.21	3.04	137.36	2.51	0.12	0.76
5.20	35.19	56.04	2.29	128.29	2.38	0.13	0.78
5.30	39.84	63.51	1.85	117.45	2.28	0.13	0.79
5.40	42.91	68.44	1.64	112.30	2.21	0.13	0.79
5.50	46.06	73.49	1.55	114.26	2.17	0.13	0.80
5.60	50.27	80.24	1.51	121.55	2.16	0.14	0.81
5.70	54.79	87.49	1.47	128.51	2.13	0.15	0.81
5.80	58.08	92.77	1.42	132.08	2.10	0.16	0.82
5.90	58.83	93.97	1.40	131.72	2.09	0.16	0.82
6.00	57.29	91.49	1.41	129.26	2.10	0.15	0.81
6.10	55.12	87.99	1.45	127.44	2.12	0.14	0.81
6.20	53.71	85.71	1.48	127.15	2.14	0.14	0.81
6.30	53.23	84.93	1.49	126.85	2.14	0.14	0.81
6.40	52.58	83.87	1.50	125.84	2.15	0.14	0.81
6.50	51.24	81.71	1.52	123.86	2.16	0.14	0.80
6.60	49.76	79.33	1.54	122.19	2.17	0.13	0.80
6.70	48.27	76.92	1.57	120.75	2.18	0.13	0.80
6.80	46.37	73.86	1.61	118.90	2.20	0.13	0.79
6.90	43.90	69.88	1.66	116.25	2.22	0.12	0.79
7.00	41.42	65.88	1.72	113.25	2.24	0.12	0.78
7.10	39.39	62.62	1.76	110.02	2.25	0.12	0.78
7.20	36.94	58.68	1.82	107.08	2.27	0.11	0.77
7.30	33.77	53.57	1.98	106.25	2.32	0.11	0.76
7.40	30.59	48.45	2.24	108.71	2.37	0.10	0.75
7.50	28.99	45.88	2.44	112.00	2.41	0.10	0.75
7.60	28.89	45.70	2.44	111.51	2.41	0.10	0.75
7.70	29.43	46.56	2.31	107.58	2.39	0.10	0.75
7.80	30.02	47.50	2.17	103.12	2.36	0.10	0.75
7.90	30.81	48.75	2.06	100.22	2.33	0.10	0.75
8.00	31.60	50.02	1.97	98.70	2.31	0.10	0.75
8.10	32.01	50.67	1.92	97.04	2.30	0.10	0.75
8.20	32.01	50.66	1.91	96.75	2.30	0.10	0.75
8.30	32.01	50.65	1.92	97.43	2.30	0.10	0.75
8.40	32.01	50.64	1.94	98.24	2.30	0.10	0.75
8.50	31.59	49.96	1.95	97.43	2.31	0.10	0.75
8.60	30.13	47.60	2.00	94.97	2.32	0.10	0.75
8.70	26.66	42.01	2.20	92.38	2.36	0.10	0.74
8.80	21.40	33.56	2.75	92.33	2.47	0.09	0.72
8.90	15.52	24.10	3.97	95.67	2.62	0.08	0.62
9.00	11.03	16.88	5.99	101.11	2.81	0.08	0.62
9.10	8.41	12.66	8.34	105.60	2.97	0.08	0.62
9.20	7.29	10.86	10.12	109.91	3.07	0.08	0.97
9.30	7.11	10.55	10.81	114.05	3.11	0.08	0.94
9.40	7.15	10.61	10.75	114.06	3.11	0.08	0.94
9.50	7.05	10.44	10.66	111.20	3.10	0.08	0.92
9.60	6.68	9.84	11.00	108.30	3.12	0.08	0.86

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.70	7.58	11.27	10.26	115.62	3.08	0.08	0.99
9.80	9.92	15.02	8.50	127.75	2.98	0.08	0.62
9.90	10.58	16.08	8.02	129.01	2.95	0.09	0.62
10.00	9.12	13.72	8.74	119.93	3.00	0.08	0.62
10.10	6.33	9.23	11.14	102.81	3.13	0.07	0.79
10.20	4.77	6.71	13.56	91.03	3.24	0.07	0.57
10.30	4.05	5.55	15.11	83.87	3.30	0.07	0.47
10.40	3.45	4.59	16.70	76.61	3.36	0.07	0.39
10.50	3.55	4.73	15.87	75.01	3.33	0.07	0.40
10.60	4.00	5.45	13.96	76.11	3.25	0.07	0.46
10.70	4.52	6.28	12.49	78.45	3.19	0.07	0.53
10.80	4.74	6.63	12.11	80.28	3.17	0.07	0.56
10.90	4.74	6.62	12.28	81.25	3.18	0.07	0.55
11.00	4.74	6.61	12.23	80.86	3.18	0.07	0.55
11.10	4.74	6.60	11.86	78.31	3.16	0.07	0.55
11.20	4.74	6.59	11.40	75.21	3.14	0.07	0.55
11.30	4.74	6.59	11.14	73.37	3.13	0.07	0.54
11.40	4.74	6.58	11.15	73.37	3.13	0.07	0.54
11.50	4.74	6.57	11.45	75.25	3.14	0.07	0.54
11.60	4.74	6.56	11.95	78.45	3.16	0.07	0.54
11.70	4.74	6.56	12.47	81.73	3.19	0.07	0.53
11.80	4.74	6.55	12.83	84.01	3.20	0.07	0.53
11.90	4.74	6.54	12.89	84.33	3.21	0.07	0.53
12.00	4.74	6.53	12.75	83.26	3.20	0.07	0.53
12.10	4.74	6.52	12.60	82.19	3.19	0.07	0.52
12.20	4.96	6.86	12.20	83.72	3.18	0.07	0.55
12.30	5.67	8.00	11.32	90.53	3.13	0.07	0.64
12.40	6.56	9.42	10.63	100.16	3.10	0.08	0.75
12.50	7.40	10.76	10.25	110.24	3.08	0.08	0.85
12.60	7.87	11.50	10.26	118.03	3.08	0.08	0.91
12.70	8.25	12.11	10.19	123.35	3.08	0.08	0.95
12.80	8.33	12.23	10.22	125.04	3.08	0.08	0.95
12.90	7.75	11.29	10.72	120.99	3.11	0.08	0.88
13.00	7.10	10.24	11.28	115.52	3.13	0.08	0.79
13.10	6.84	9.80	11.59	113.65	3.15	0.08	0.76
13.20	7.20	10.38	11.36	117.86	3.14	0.08	0.80
13.30	7.57	10.96	11.05	121.05	3.12	0.08	0.84
13.40	7.08	10.16	11.43	116.13	3.14	0.08	0.77
13.50	5.94	8.32	12.53	104.33	3.19	0.07	0.63
13.60	4.62	6.20	14.39	89.17	3.27	0.07	0.47
13.70	3.90	5.03	15.56	78.30	3.31	0.07	0.38
13.80	3.75	4.78	15.32	73.27	3.30	0.07	0.36
13.90	3.99	5.17	14.16	73.15	3.26	0.07	0.39
14.00	4.43	5.86	13.12	76.92	3.22	0.07	0.44
14.10	4.88	6.58	12.47	82.13	3.19	0.07	0.49
14.20	4.97	6.72	12.59	84.57	3.19	0.07	0.50
14.30	5.01	6.77	12.62	85.40	3.20	0.07	0.50
14.40	4.97	6.69	12.66	84.75	3.20	0.07	0.49

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
14.50	5.03	6.79	12.51	84.91	3.19	0.07	0.50
14.60	5.16	6.99	12.35	86.38	3.18	0.07	0.51
14.70	5.69	7.83	11.71	91.71	3.15	0.07	0.57
14.80	6.80	9.61	10.64	102.23	3.10	0.08	0.70
14.90	7.83	11.25	10.04	112.92	3.07	0.08	0.82
15.00	8.56	12.42	9.81	121.87	3.06	0.08	0.90
15.10	9.66	14.17	9.28	131.50	3.03	0.08	1.02
15.20	12.13	18.13	7.96	144.32	2.95	0.08	0.62
15.30	16.06	24.00	6.47	155.26	2.85	0.09	0.62
15.40	17.85	26.45	5.86	155.04	2.80	0.10	0.62
15.50	18.07	26.56	5.62	149.18	2.78	0.09	0.62
15.60	19.86	28.90	4.99	144.22	2.73	0.09	0.62
15.70	24.13	34.60	4.03	139.38	2.63	0.10	0.62
15.80	27.78	39.20	3.28	128.71	2.54	0.10	0.74
15.90	26.70	37.25	3.06	114.13	2.51	0.10	0.73
16.00	21.89	30.53	3.47	105.84	2.57	0.09	0.72
16.10	16.23	22.82	4.79	109.24	2.71	0.08	0.62
16.20	11.85	16.80	7.01	117.79	2.89	0.08	0.62
16.30	10.16	14.29	8.88	126.88	3.01	0.08	1.02
16.40	9.88	13.79	9.64	132.99	3.05	0.08	0.98
16.50	9.52	13.18	10.01	131.99	3.07	0.08	0.94
16.60	9.04	12.38	10.11	125.22	3.07	0.08	0.88
16.70	8.54	11.57	10.08	116.69	3.07	0.08	0.83
16.80	8.24	11.07	10.10	111.84	3.07	0.08	0.79
16.90	7.44	9.83	10.89	107.02	3.11	0.08	0.70
17.00	6.60	8.52	12.06	102.76	3.17	0.07	0.61
17.10	5.74	7.20	13.46	96.84	3.23	0.07	0.51
17.20	5.29	6.49	14.05	91.17	3.26	0.07	0.46
17.30	5.07	6.14	13.89	85.25	3.25	0.07	0.44
17.40	4.98	5.97	13.26	79.16	3.22	0.07	0.43
17.50	4.83	5.72	12.70	72.67	3.20	0.07	0.41
17.60	4.34	4.98	13.17	65.53	3.22	0.07	0.36
17.70	3.81	4.18	14.44	60.34	3.27	0.07	0.30
17.80	3.52	3.74	15.50	57.97	3.31	0.07	0.27
17.90	3.85	4.20	14.42	60.62	3.27	0.07	0.30
18.00	4.37	4.96	13.09	64.89	3.22	0.07	0.35
18.10	4.60	5.28	13.09	69.07	3.22	0.07	0.38
18.20	4.80	5.54	13.50	74.74	3.23	0.07	0.40
18.30	5.19	6.09	13.62	82.93	3.24	0.07	0.44
18.40	5.70	6.79	13.41	91.12	3.23	0.07	0.49
18.50	5.93	7.10	13.76	97.74	3.24	0.07	0.51
18.60	5.93	7.07	14.45	102.22	3.27	0.07	0.51
18.70	5.93	7.04	14.94	105.25	3.29	0.07	0.50
18.80	5.93	7.02	15.16	106.33	3.30	0.07	0.50
18.90	5.93	6.99	15.09	105.44	3.30	0.07	0.50
19.00	6.05	7.12	14.69	104.64	3.28	0.07	0.51
19.10	6.40	7.59	14.05	106.71	3.26	0.07	0.54
19.20	6.98	8.38	13.31	111.49	3.22	0.08	0.60

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
19.30	7.65	9.29	12.45	115.67	3.19	0.08	0.66
19.40	8.11	9.90	11.82	117.04	3.16	0.08	0.71
19.50	8.46	10.36	11.27	116.72	3.13	0.08	0.74
19.60	8.38	10.20	11.18	113.99	3.13	0.08	0.73
19.70	8.40	10.19	11.02	112.26	3.12	0.08	0.73
19.80	9.32	11.43	10.10	115.49	3.07	0.08	0.82
19.90	10.07	12.42	9.55	118.65	3.04	0.08	0.89
20.00	9.83	12.05	9.86	118.78	3.06	0.08	0.86
20.10	8.12	9.65	11.65	112.39	3.15	0.08	0.69
20.20	6.67	7.62	14.04	107.02	3.25	0.07	0.54
20.30	6.07	6.77	15.55	105.35	3.31	0.07	0.48
20.40	5.77	6.33	16.46	104.19	3.35	0.07	0.45
20.50	5.38	5.78	17.38	100.44	3.38	0.07	0.41
20.60	4.98	5.22	17.98	93.85	3.40	0.07	0.37
20.70	4.75	4.88	17.80	86.94	3.39	0.07	0.35
20.80	4.74	4.85	16.91	82.10	3.36	0.07	0.35
20.90	4.86	4.99	16.05	80.08	3.33	0.07	0.36
21.00	5.42	5.72	14.76	84.44	3.28	0.07	0.41
21.10	6.27	6.84	13.69	93.64	3.24	0.07	0.49
21.20	6.95	7.71	13.12	101.21	3.22	0.08	0.55
21.30	7.20	8.02	13.05	104.65	3.21	0.07	0.57
21.40	7.31	8.14	12.99	105.76	3.21	0.08	0.58
21.50	7.92	8.91	12.38	110.30	3.18	0.08	0.64
21.60	9.40	10.82	11.06	119.72	3.12	0.08	0.77
21.70	11.65	13.73	9.30	127.74	3.03	0.08	0.98
21.80	14.83	17.80	7.30	129.88	2.91	0.08	0.62
21.90	18.05	21.59	5.65	121.93	2.78	0.09	0.62
22.00	20.60	24.47	4.48	109.52	2.68	0.09	0.62
22.10	21.70	25.59	3.93	100.57	2.62	0.09	0.62
22.20	21.51	25.30	3.98	100.57	2.63	0.09	0.62
22.30	20.65	24.29	4.46	108.29	2.68	0.09	0.62
22.40	19.82	23.33	5.09	118.80	2.74	0.09	0.62
22.50	19.24	22.68	5.75	130.33	2.79	0.09	0.62
22.60	19.38	22.88	6.31	144.45	2.84	0.09	0.62
22.70	21.44	25.41	6.37	161.91	2.84	0.09	0.62
22.80	25.94	30.77	5.66	174.25	2.78	0.10	0.62
22.90	32.18	37.99	4.60	174.83	2.69	0.11	0.62
23.00	37.11	43.42	3.65	158.64	2.59	0.11	0.76
23.10	38.48	44.58	3.07	137.00	2.51	0.11	0.76
23.20	35.78	41.14	2.96	121.84	2.50	0.11	0.75
23.30	30.27	34.70	3.43	119.07	2.56	0.10	0.73
23.40	24.07	27.54	4.54	124.97	2.68	0.09	0.62
23.50	18.71	21.26	6.04	128.36	2.81	0.09	0.62
23.60	14.66	16.44	7.75	127.45	2.94	0.08	0.62
23.70	11.82	12.90	9.35	120.59	3.03	0.08	0.92
23.80	9.79	10.37	10.60	109.99	3.10	0.08	0.74
23.90	8.76	9.08	11.09	100.73	3.12	0.08	0.65
24.00	8.87	9.18	10.79	99.13	3.11	0.08	0.66

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
24.10	9.46	9.86	10.47	103.24	3.09	0.08	0.70
24.20	10.14	10.66	10.31	109.87	3.08	0.08	0.76
24.30	10.42	10.96	10.50	115.03	3.09	0.08	0.78
24.40	10.44	10.93	10.81	118.15	3.11	0.08	0.78
24.50	10.20	10.61	11.23	119.08	3.13	0.08	0.76
24.60	9.62	9.89	11.91	117.72	3.16	0.08	0.71
24.70	9.03	9.15	12.61	115.38	3.19	0.08	0.65
24.80	8.52	8.51	13.24	112.62	3.22	0.08	0.61
24.90	8.30	8.22	13.43	110.39	3.23	0.08	0.59
25.00	8.30	8.18	13.29	108.74	3.22	0.08	0.58
25.10	7.91	7.70	13.68	105.37	3.24	0.08	0.55
25.20	7.42	7.10	14.28	101.43	3.26	0.07	0.51
25.30	7.65	7.34	13.70	100.49	3.24	0.07	0.52
25.40	8.44	8.24	12.41	102.35	3.19	0.08	0.59
25.50	9.09	8.97	11.72	105.07	3.15	0.08	0.64
25.60	8.99	8.82	12.15	107.19	3.17	0.08	0.63
25.70	8.59	8.33	13.16	109.64	3.22	0.08	0.60
25.80	8.74	8.48	13.39	113.49	3.23	0.08	0.61
25.90	9.74	9.60	12.32	118.19	3.18	0.08	0.69
26.00	12.20	12.39	10.05	124.53	3.07	0.08	0.89
26.10	14.90	15.45	8.26	127.68	2.97	0.09	0.62
26.20	16.97	17.75	7.19	127.57	2.90	0.09	0.62
26.30	18.58	19.47	6.60	128.59	2.86	0.09	0.62
26.40	20.32	21.35	6.35	135.65	2.84	0.09	0.62
26.50	21.81	22.96	6.38	146.44	2.84	0.09	0.62
26.60	21.82	22.94	6.73	154.29	2.87	0.09	0.62
26.70	20.10	20.99	7.40	155.21	2.91	0.09	0.62
26.80	17.84	18.38	8.24	151.54	2.97	0.09	0.62
26.90	16.12	16.39	9.03	147.95	3.01	0.09	1.17
27.00	16.24	16.47	9.08	149.51	3.02	0.08	1.18
27.10	18.29	18.69	8.34	155.81	2.97	0.09	0.62
27.20	21.53	22.23	7.33	162.90	2.91	0.09	0.62
27.30	25.33	26.24	6.36	166.84	2.84	0.10	0.62
27.40	28.68	29.72	5.56	165.22	2.78	0.10	0.62
27.50	30.57	31.61	5.04	159.41	2.73	0.10	0.62
27.60	30.71	31.63	4.84	153.17	2.71	0.10	0.62
27.70	29.52	30.25	4.92	148.96	2.72	0.10	0.62
27.80	28.15	28.72	5.14	147.60	2.74	0.10	0.62
27.90	26.52	26.91	5.45	146.60	2.77	0.10	0.62
28.00	24.26	24.44	5.92	144.70	2.81	0.09	0.62
28.10	21.33	21.28	6.68	142.17	2.86	0.09	0.62
28.20	18.44	18.16	7.78	141.26	2.94	0.09	0.62
28.30	16.54	16.05	8.95	143.70	3.01	0.09	1.15
28.40	16.30	15.75	9.49	149.51	3.04	0.08	1.12
28.50	17.10	16.55	9.37	155.00	3.03	0.09	1.18
28.60	18.01	17.46	9.11	159.06	3.02	0.09	1.25
28.70	18.92	18.36	8.95	164.43	3.01	0.09	1.31
28.80	20.11	19.56	8.86	173.27	3.00	0.09	1.40

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
28.90	21.92	21.40	8.50	181.84	2.98	0.09	0.62
29.00	23.18	22.66	8.11	183.89	2.96	0.10	0.62
29.10	23.37	22.78	7.75	176.56	2.94	0.09	0.62
29.20	23.75	23.10	7.24	167.18	2.90	0.09	0.62
29.30	25.51	24.81	6.45	160.15	2.85	0.09	0.62
29.40	27.88	27.13	5.70	154.78	2.79	0.10	0.62
29.50	28.61	27.77	5.35	148.60	2.76	0.10	0.62
29.60	27.32	26.37	5.45	143.70	2.77	0.10	0.62
29.70	25.80	24.76	5.91	146.26	2.80	0.09	0.62
29.80	25.94	24.84	6.07	150.77	2.82	0.09	0.62
29.90	25.94	24.76	6.01	148.73	2.81	0.10	0.62
30.00	24.40	23.13	6.21	143.69	2.83	0.09	0.62
30.10	21.96	20.61	6.74	138.86	2.87	0.09	0.62
30.20	20.74	19.33	7.22	139.54	2.90	0.09	0.62
30.30	21.44	19.97	7.00	139.71	2.89	0.09	0.62
30.40	22.21	20.68	6.71	138.69	2.87	0.09	0.62
30.50	22.53	20.93	6.60	138.08	2.86	0.09	0.62
30.60	22.53	20.87	6.61	138.02	2.86	0.09	0.62
30.70	22.94	21.21	6.64	140.86	2.86	0.09	0.62
30.80	25.28	23.47	6.29	147.55	2.83	0.09	0.62
30.90	30.78	28.82	5.33	153.56	2.76	0.10	0.62
31.00	38.07	35.87	4.23	151.55	2.65	0.11	0.62
31.10	43.30	40.86	3.46	141.39	2.56	0.11	0.76
31.20	44.29	41.68	3.14	130.94	2.52	0.11	0.76
31.30	43.30	40.62	3.18	129.18	2.53	0.11	0.75
31.40	44.39	41.57	3.27	135.81	2.54	0.11	0.75
31.50	48.84	45.77	3.07	140.63	2.51	0.12	0.77
31.60	55.32	51.89	2.62	135.76	2.44	0.12	0.78
31.70	61.94	58.11	2.14	124.50	2.35	0.13	0.79
31.80	68.38	64.12	1.79	115.05	2.26	0.13	0.79
31.90	74.08	69.40	1.59	110.24	2.19	0.13	0.80
32.00	77.06	72.09	1.51	109.09	2.15	0.14	0.80
32.10	74.88	69.86	1.56	108.63	2.17	0.14	0.80
32.20	67.28	62.48	1.77	110.79	2.26	0.13	0.79
32.30	56.41	52.01	2.27	118.21	2.38	0.12	0.77
32.40	45.30	41.34	3.08	127.47	2.51	0.11	0.76
32.50	36.00	32.42	4.18	135.68	2.65	0.10	0.62
32.60	29.19	25.90	5.44	140.87	2.77	0.10	0.62
32.70	25.10	21.97	6.48	142.38	2.85	0.09	0.62
32.80	23.13	20.04	6.97	139.64	2.88	0.09	0.62
32.90	22.72	19.60	6.89	135.06	2.88	0.09	0.62
33.00	23.50	20.28	6.56	133.08	2.85	0.09	0.62
33.10	24.98	21.61	6.24	134.74	2.83	0.09	0.62
33.20	27.13	23.56	5.92	139.45	2.81	0.09	0.62
33.30	29.30	25.51	5.70	145.36	2.79	0.10	0.62
33.40	30.50	26.55	5.68	150.86	2.79	0.10	0.62
33.50	30.45	26.43	5.88	155.49	2.80	0.10	0.62
33.60	29.68	25.63	6.19	158.58	2.83	0.10	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
33.70	29.63	25.51	6.34	161.64	2.84	0.10	0.62
33.80	31.56	27.21	6.19	168.34	2.83	0.10	0.62
33.90	36.20	31.38	5.80	181.86	2.80	0.10	0.62
34.00	43.30	37.79	5.23	197.76	2.75	0.11	0.62
34.10	51.88	45.54	4.57	208.30	2.69	0.13	0.62
34.20	61.05	53.80	3.92	211.04	2.62	0.14	0.65
34.30	69.91	61.76	3.35	207.07	2.55	0.15	0.80
34.40	78.51	69.46	2.88	200.38	2.49	0.16	0.82
34.50	87.03	77.07	2.53	194.99	2.43	0.18	0.83
34.60	96.53	85.55	2.23	190.38	2.37	0.20	0.84
34.70	107.11	95.01	1.96	185.82	2.31	0.22	0.85
34.80	117.42	104.24	1.71	177.94	2.23	0.25	0.86
34.90	125.48	111.44	1.54	171.37	2.17	0.27	0.87
35.00	129.52	114.95	1.46	167.39	2.12	0.27	0.87
35.10	129.35	114.57	1.45	165.58	2.12	0.27	0.87
35.20	124.29	109.70	1.49	163.04	2.14	0.25	0.87
35.30	113.93	100.05	1.59	159.12	2.19	0.23	0.86
35.40	99.94	87.17	1.79	156.05	2.26	0.19	0.84
35.50	86.32	74.67	2.12	158.35	2.35	0.16	0.82
35.60	78.64	67.57	2.43	164.27	2.41	0.15	0.81
35.70	79.44	68.08	2.50	170.36	2.42	0.15	0.81
35.80	87.98	75.51	2.30	173.61	2.39	0.17	0.82
35.90	100.57	86.56	1.99	172.57	2.32	0.20	0.84
36.00	113.44	97.90	1.73	169.10	2.24	0.23	0.86
36.10	124.61	107.76	1.55	166.69	2.17	0.25	0.87
36.20	133.12	115.22	1.45	167.10	2.12	0.28	0.87
36.30	139.52	120.72	1.41	169.85	2.09	0.29	0.87
36.40	144.03	124.47	1.39	173.16	2.08	0.32	0.88
36.50	146.71	126.55	1.39	176.23	2.08	0.34	0.88
36.60	146.25	125.83	1.41	177.27	2.09	0.34	0.88
36.70	142.03	121.77	1.44	175.32	2.11	0.32	0.88
36.80	135.41	115.63	1.48	171.37	2.14	0.28	0.87
36.90	129.09	109.83	1.52	166.54	2.16	0.26	0.87
37.00	125.04	106.08	1.52	161.53	2.16	0.24	0.86
37.10	122.66	103.83	1.51	157.09	2.15	0.23	0.86
37.20	121.21	102.39	1.51	154.12	2.15	0.22	0.86
37.30	120.82	101.84	1.51	153.40	2.15	0.22	0.85
37.40	121.89	102.55	1.51	154.48	2.15	0.23	0.86
37.50	124.48	104.56	1.50	156.68	2.15	0.23	0.86
37.60	127.71	107.15	1.48	158.98	2.14	0.25	0.86
37.70	130.82	109.64	1.46	160.57	2.13	0.26	0.87
37.80	132.63	110.99	1.45	161.33	2.12	0.26	0.87
37.90	132.47	110.63	1.45	160.78	2.12	0.26	0.87
38.00	129.59	107.90	1.47	158.76	2.13	0.25	0.87
38.10	123.93	102.77	1.51	155.28	2.15	0.24	0.86
38.20	115.89	95.60	1.58	150.97	2.19	0.21	0.85
38.30	107.14	87.86	1.68	147.41	2.22	0.19	0.84
38.40	98.41	80.20	1.79	143.33	2.26	0.18	0.83

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
38.50	90.54	73.34	1.89	138.77	2.29	0.16	0.82
38.60	84.03	67.69	1.98	134.10	2.31	0.15	0.81
38.70	79.79	63.95	2.07	132.56	2.34	0.14	0.80
38.80	77.78	62.11	2.13	132.12	2.35	0.14	0.80
38.90	77.14	61.46	2.12	130.45	2.35	0.14	0.80
39.00	77.04	61.28	2.09	128.29	2.34	0.14	0.80
39.10	76.57	60.76	2.09	127.11	2.34	0.14	0.80
39.20	75.78	59.94	2.14	128.39	2.35	0.14	0.80
39.30	75.01	59.12	2.22	131.47	2.37	0.14	0.80
39.40	74.55	58.54	2.31	135.50	2.39	0.14	0.80
39.50	74.00	57.91	2.39	138.37	2.40	0.14	0.80
39.60	73.21	57.14	2.40	137.08	2.40	0.14	0.80
39.70	72.79	56.71	2.36	133.79	2.40	0.14	0.79
39.80	72.42	56.32	2.33	131.12	2.39	0.14	0.79
39.90	70.13	54.35	2.35	127.47	2.39	0.14	0.79
40.00	66.57	51.32	2.43	124.84	2.41	0.13	0.78
40.10	63.68	48.85	2.53	123.76	2.43	0.12	0.78
40.20	64.36	49.26	2.56	126.17	2.43	0.12	0.78
40.30	68.83	52.79	2.44	128.80	2.41	0.13	0.79
40.40	77.61	59.87	2.19	130.84	2.36	0.14	0.80
40.50	91.92	71.57	1.86	133.06	2.28	0.16	0.82
40.60	111.46	87.73	1.57	137.70	2.18	0.19	0.84
40.70	133.56	106.20	1.39	147.50	2.08	0.24	0.86
40.80	153.43	122.84	1.31	160.84	2.00	0.31	0.87
40.90	167.80	134.76	1.28	172.18	1.96	0.37	0.88
41.00	176.80	142.18	1.26	179.01	1.93	0.41	0.88
41.10	182.80	147.00	1.25	183.71	1.92	0.45	0.88
41.20	187.72	150.81	1.25	188.04	1.92	0.51	0.88
41.30	191.80	153.71	1.25	192.76	1.93	0.58	0.89
41.40	194.68	155.63	1.26	196.20	1.94	0.65	0.90
41.50	197.00	157.18	1.26	198.54	1.94	0.68	0.90
41.60	199.27	158.73	1.26	200.53	1.94	0.73	0.90
41.70	202.25	160.87	1.26	203.05	1.94	0.79	0.91
41.80	205.69	163.33	1.26	206.23	1.94	0.89	0.91
41.90	209.24	165.81	1.27	209.96	1.94	0.90	0.91
42.00	212.51	168.04	1.27	213.39	1.95	0.90	0.92
42.10	214.98	169.66	1.27	215.83	1.95	0.90	0.92
42.20	216.82	170.83	1.27	217.24	1.95	0.91	0.92
42.30	217.44	171.05	1.27	217.32	1.95	0.91	0.92
42.40	215.99	169.56	1.27	215.68	1.95	0.90	0.92
42.50	212.38	166.26	1.28	212.38	1.96	0.90	0.92
42.60	207.75	162.14	1.28	208.26	1.97	0.90	0.92
42.70	203.54	158.42	1.29	204.30	1.98	0.89	0.92
42.80	199.98	155.27	1.29	200.66	1.98	0.81	0.91
42.90	196.07	151.85	1.30	196.82	1.99	0.74	0.91
43.00	191.21	147.63	1.30	192.48	2.00	0.65	0.91
43.10	185.37	142.60	1.31	187.51	2.01	0.57	0.90
43.20	179.37	137.43	1.33	182.72	2.03	0.50	0.90

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
43.30	174.19	132.95	1.34	178.78	2.04	0.45	0.90
43.40	170.22	129.47	1.36	175.77	2.05	0.42	0.89
43.50	166.83	126.51	1.37	173.01	2.06	0.40	0.89
43.60	162.46	122.78	1.38	169.39	2.07	0.38	0.89
43.70	156.00	117.35	1.41	164.91	2.09	0.34	0.88
43.80	147.22	110.07	1.45	159.59	2.12	0.30	0.88
43.90	136.83	101.53	1.52	154.22	2.16	0.26	0.87
44.00	126.19	92.88	1.61	149.55	2.20	0.23	0.86
44.10	116.68	85.22	1.71	145.40	2.23	0.20	0.85
44.20	109.12	79.22	1.77	140.29	2.26	0.19	0.84
44.30	103.32	74.80	1.76	131.81	2.25	0.17	0.83
44.40	98.06	70.93	1.70	120.62	2.23	0.16	0.82
44.50	92.45	66.83	1.64	109.45	2.21	0.15	0.81
44.60	86.05	61.96	1.64	101.53	2.21	0.13	0.80
44.70	79.77	56.96	1.74	98.89	2.24	0.13	0.79
44.80	74.72	52.81	1.91	100.74	2.30	0.12	0.78
44.90	71.40	50.06	2.06	102.88	2.33	0.12	0.78
45.00	69.26	48.29	2.15	103.62	2.35	0.12	0.78
45.10	69.08	48.01	2.20	105.41	2.36	0.12	0.78
45.20	73.88	51.46	2.13	109.83	2.35	0.12	0.78
45.30	86.95	61.29	1.87	114.69	2.29	0.14	0.80
45.40	107.24	76.96	1.56	120.09	2.18	0.17	0.83
45.50	130.79	95.46	1.38	131.29	2.07	0.20	0.85
45.60	152.68	112.72	1.30	146.32	1.99	0.26	0.86
45.70	171.44	127.47	1.26	160.76	1.94	0.32	0.87
45.80	188.25	140.48	1.24	174.46	1.91	0.41	0.87
45.90	205.84	154.08	1.22	188.59	1.88	0.59	0.88
46.00	224.66	168.78	1.20	202.68	1.85	0.90	0.89
46.10	242.48	182.92	1.17	213.72	1.81	0.92	0.90
46.20	256.90	194.52	1.13	219.56	1.78	0.93	0.91
46.30	266.83	202.14	1.11	224.94	1.77	0.93	0.92
46.40	272.73	206.29	1.12	230.21	1.77	0.93	0.92
46.50	275.32	207.95	1.12	232.12	1.77	0.94	0.92
46.60	276.13	208.29	1.11	232.18	1.77	0.94	0.92
46.70	276.72	208.48	1.11	231.87	1.77	0.94	0.92
46.80	278.32	208.95	1.13	236.67	1.78	0.94	0.92
46.90	282.43	211.50	1.14	241.72	1.79	0.94	0.93
47.00	288.11	215.55	1.14	245.68	1.79	0.94	0.93
47.10	291.48	218.17	1.12	244.99	1.78	0.94	0.94
47.20	287.17	214.60	1.12	241.01	1.78	0.94	0.93
47.30	273.91	203.55	1.15	234.91	1.80	0.93	0.92
47.40	254.36	187.22	1.20	224.98	1.85	0.92	0.92
47.50	231.51	168.39	1.25	209.93	1.91	0.90	0.92
47.60	207.31	148.87	1.29	192.44	1.98	0.83	0.91
47.70	183.14	129.76	1.35	175.74	2.05	0.50	0.90
47.80	161.34	112.83	1.44	162.17	2.11	0.34	0.88
47.90	147.04	101.74	1.52	155.05	2.16	0.26	0.87
48.00	144.37	99.47	1.56	154.69	2.17	0.26	0.87

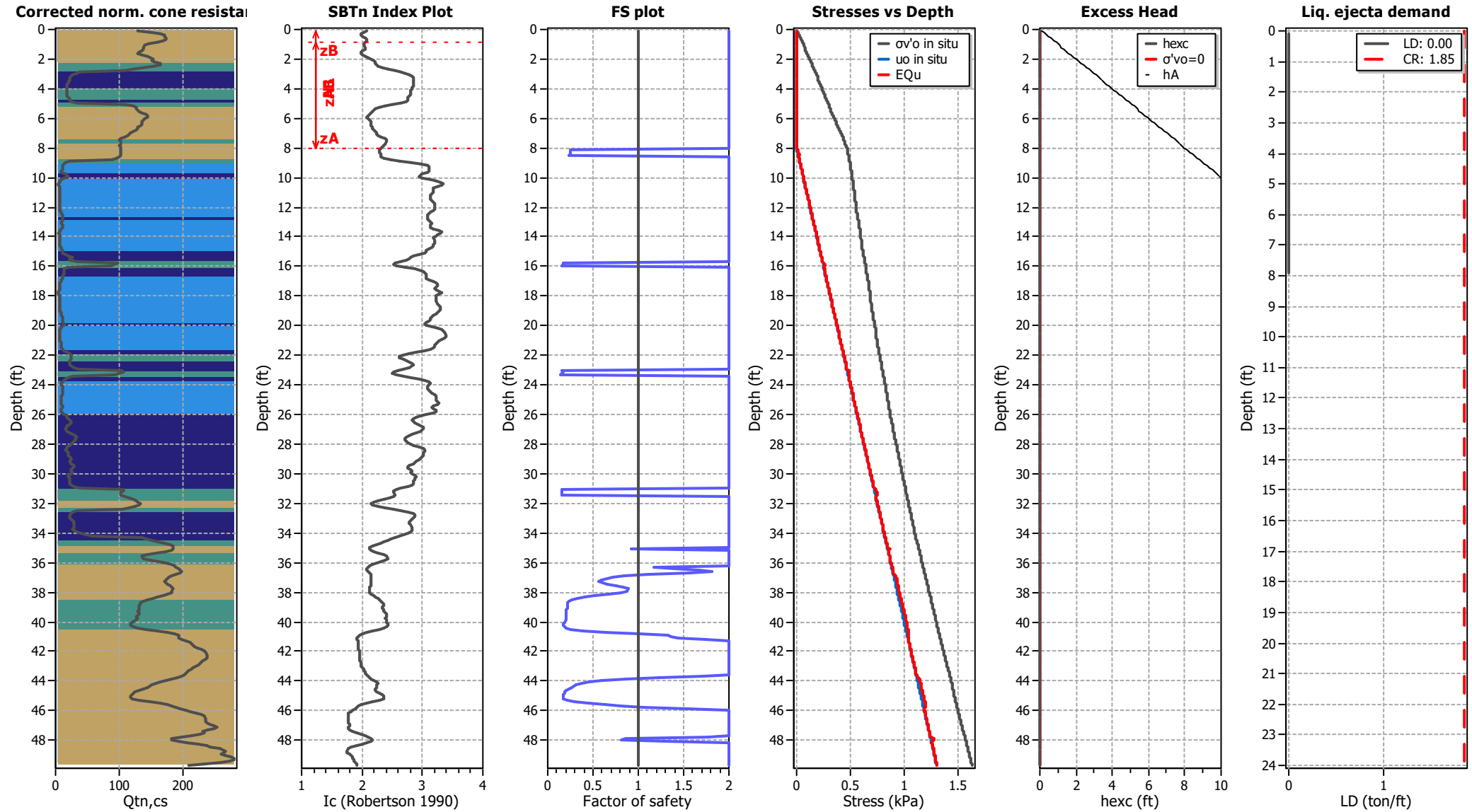
:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
48.10	154.30	106.68	1.50	160.14	2.15	0.31	0.88
48.20	174.92	122.07	1.40	171.37	2.09	0.41	0.89
48.30	203.69	144.04	1.31	189.13	2.01	0.73	0.91
48.40	238.64	171.26	1.25	213.37	1.91	0.91	0.92
48.50	272.42	198.09	1.18	233.98	1.83	0.93	0.93
48.60	297.48	218.17	1.11	242.89	1.77	0.94	0.94
48.70	309.01	227.10	1.08	245.68	1.75	0.95	0.95
48.80	310.28	227.31	1.10	249.99	1.76	0.95	0.95
48.90	308.58	224.81	1.14	255.28	1.79	0.95	0.95
49.00	308.74	223.69	1.16	260.57	1.81	0.95	0.95
49.10	309.55	223.18	1.19	264.58	1.83	0.95	0.96
49.20	307.77	220.85	1.20	265.53	1.85	0.95	0.96
49.30	300.75	214.88	1.21	260.96	1.87	0.94	0.96
49.40	287.55	204.67	1.22	250.19	1.88	0.93	0.96
49.50	266.11	188.68	1.23	231.85	1.89	0.92	0.94
49.60	239.13	168.63	1.24	209.07	1.90	0.90	0.92
49.70	219.20	153.76	1.25	192.28	1.92	0.65	0.90

Abbreviations

q_t :	Total cone resistance
K_c :	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c :	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

Ejecta Severity Estimation



LIQUEFACTION ANALYSIS REPORT

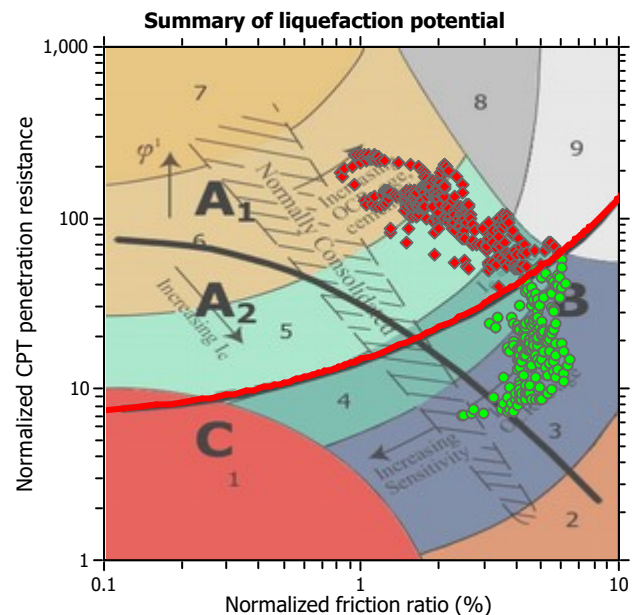
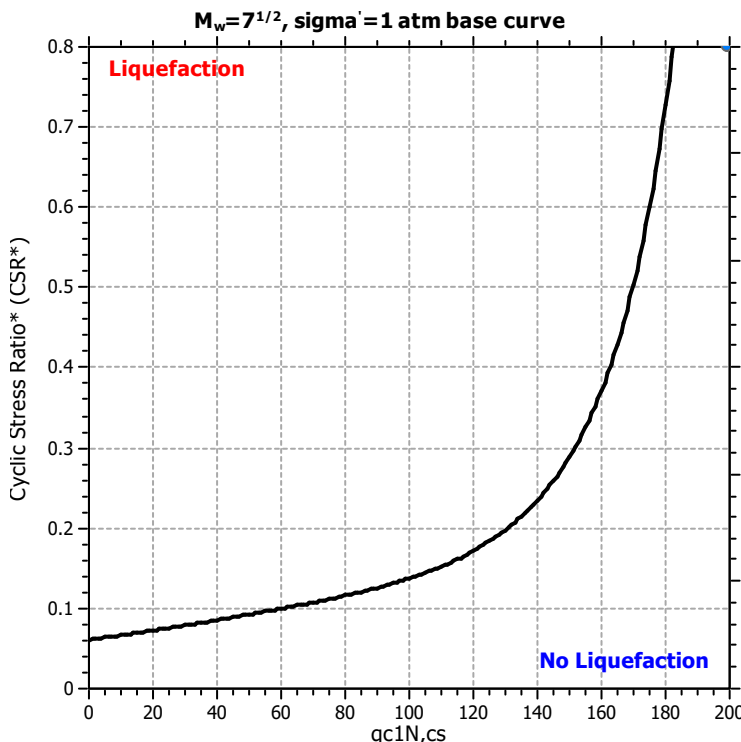
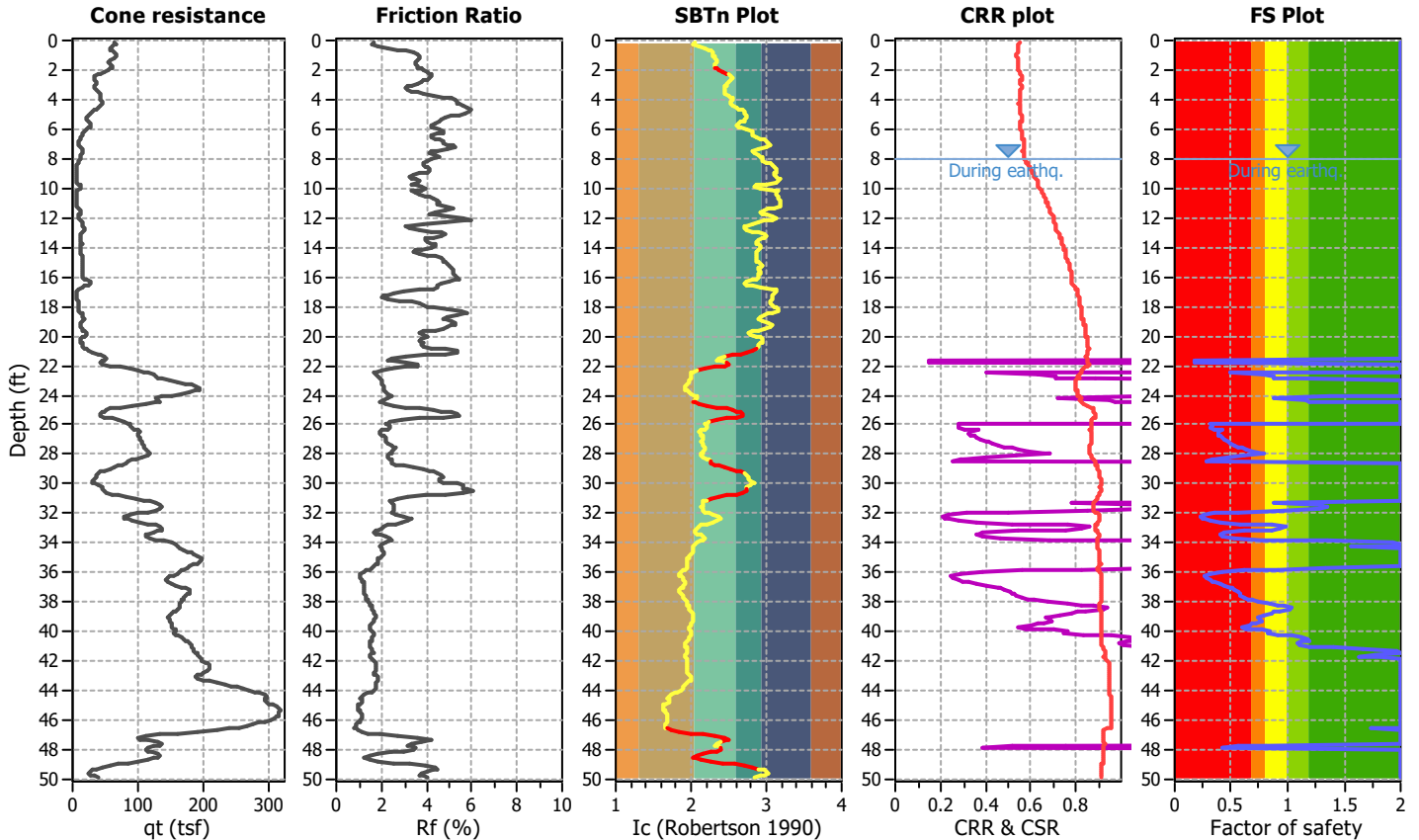
Project title : 21-483 Equestrian Estates

Location : Avenue 64 at Harrison Street, Thermal California

CPT file : CPT-7 B&I 2014

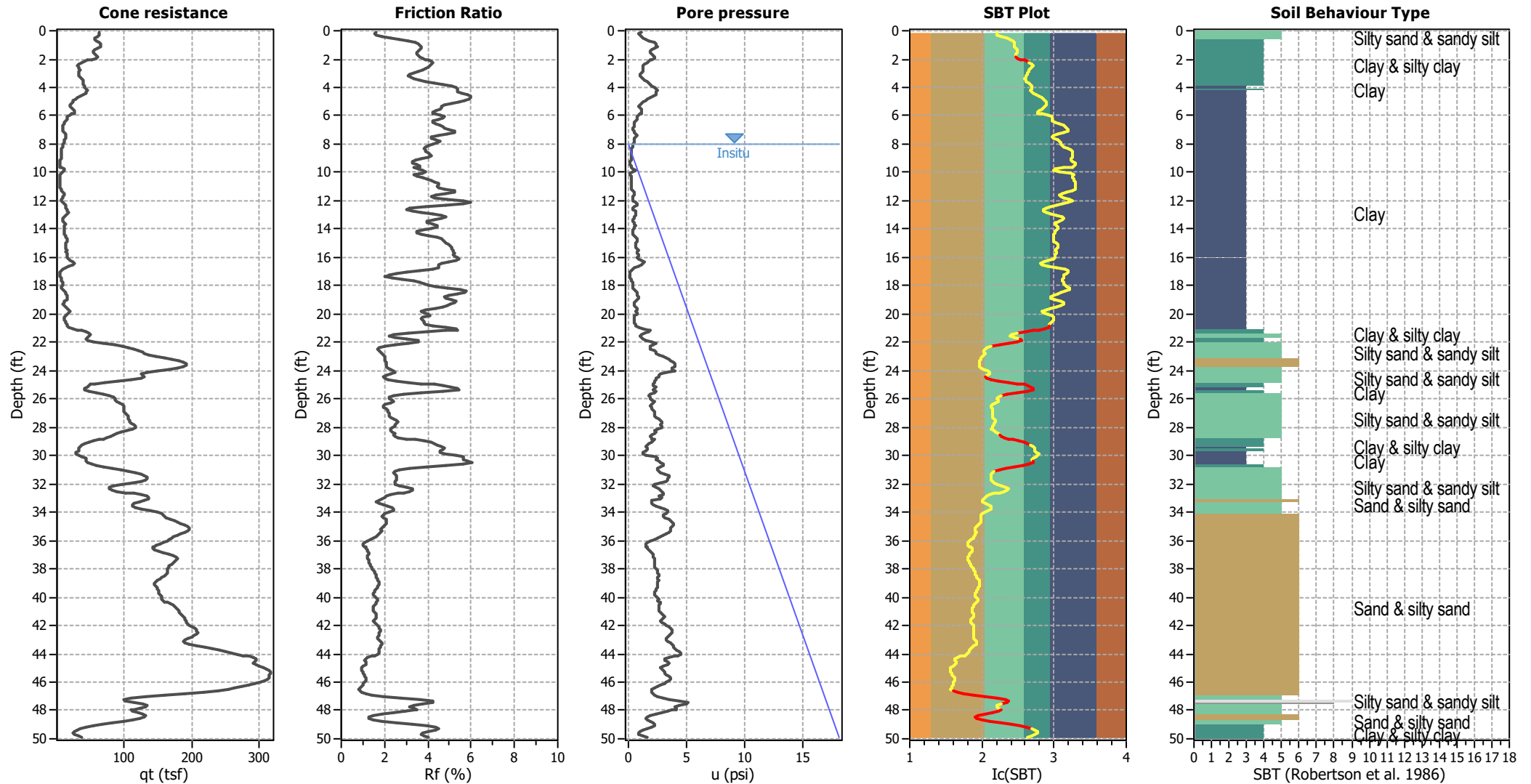
Input parameters and analysis data

Analysis method:	B&I (2014)	G.W.T. (in-situ):	8.00 ft	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	8.00 ft	Fill height:	N/A	Limit depth applied:	No
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth:	N/A
Earthquake magnitude M_w :	7.34	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.74	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		



Zone A₁: Cyclic liquefaction likely depending on size and duration of cyclic loading
 Zone A₂: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
 Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
 Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



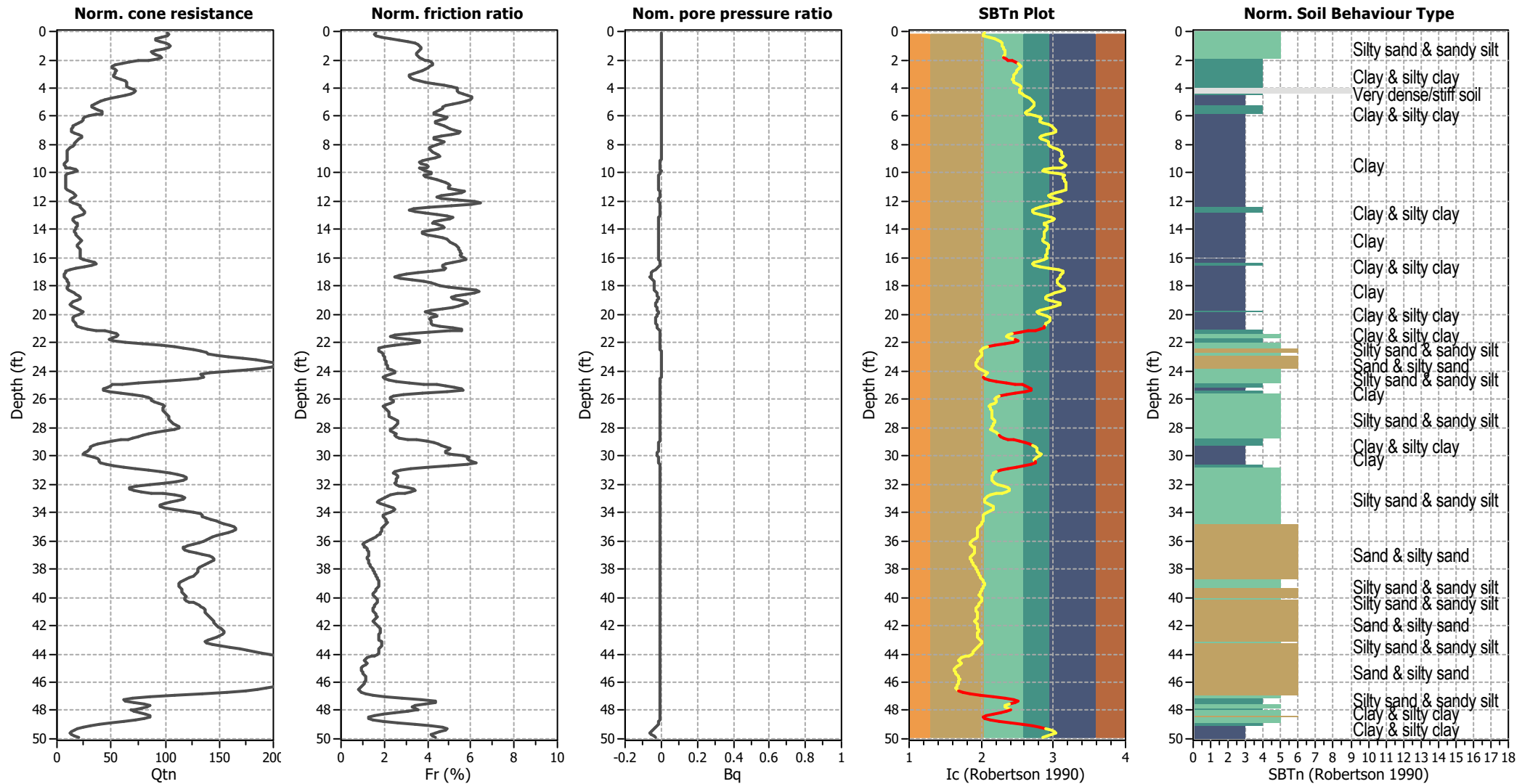
Input parameters and analysis data

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Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K ₀ applied:	Yes
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

SBT legend

1. Sensitive fine grained	4. Clayey silt to silty	7. Gravely sand to sand
2. Organic material	5. Silty sand to sandy silt	8. Very stiff sand to
3. Clay to silty clay	6. Clean sand to silty sand	9. Very stiff fine grained

CPT basic interpretation plots (normalized)



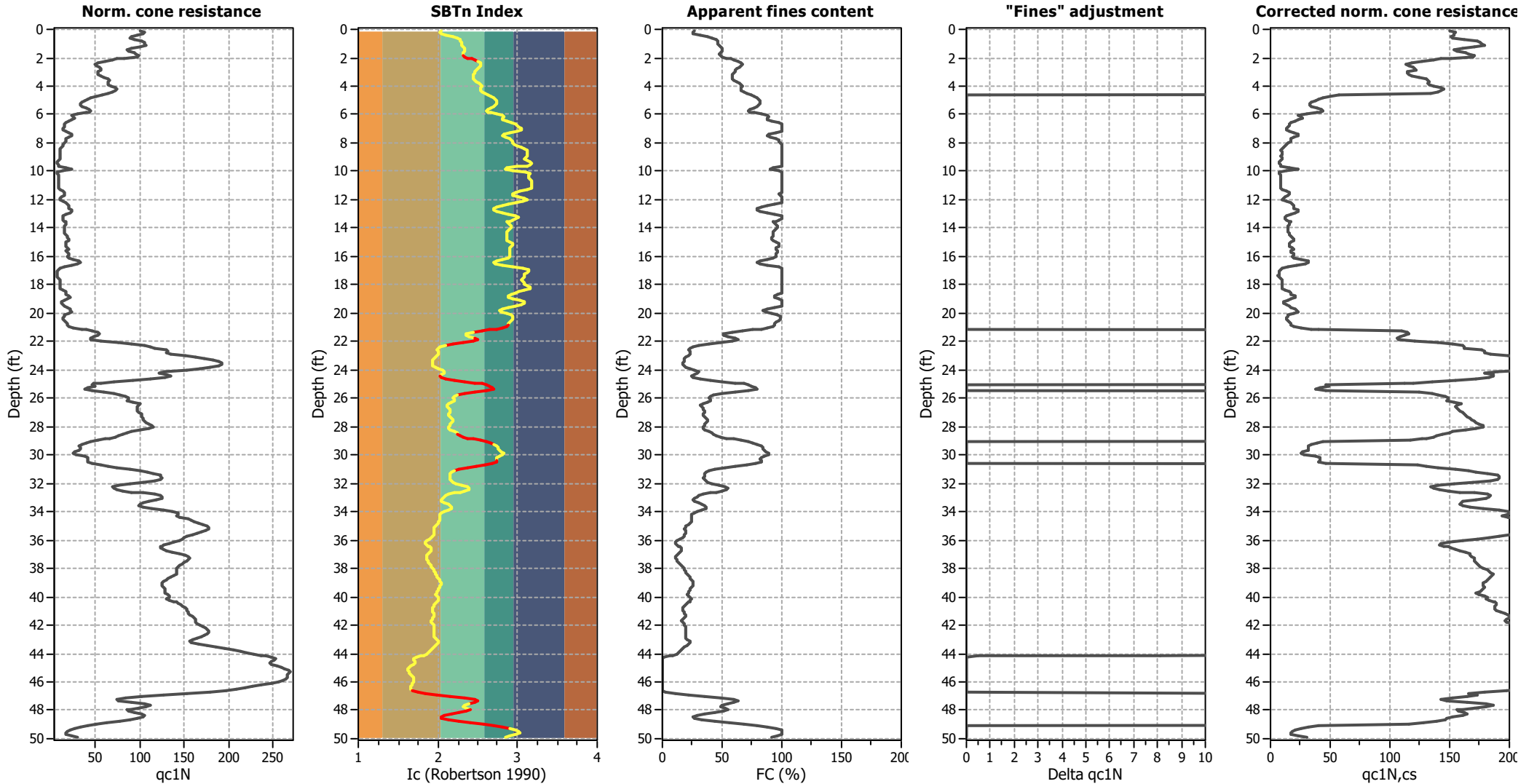
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K ₀ applied:	Yes
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

SBTn legend

1. Sensitive fine grained	4. Clayey silt to silty	7. Gravely sand to sand
2. Organic material	5. Silty sand to sandy silt	8. Very stiff sand to
3. Clay to silty clay	6. Clean sand to silty sand	9. Very stiff fine grained

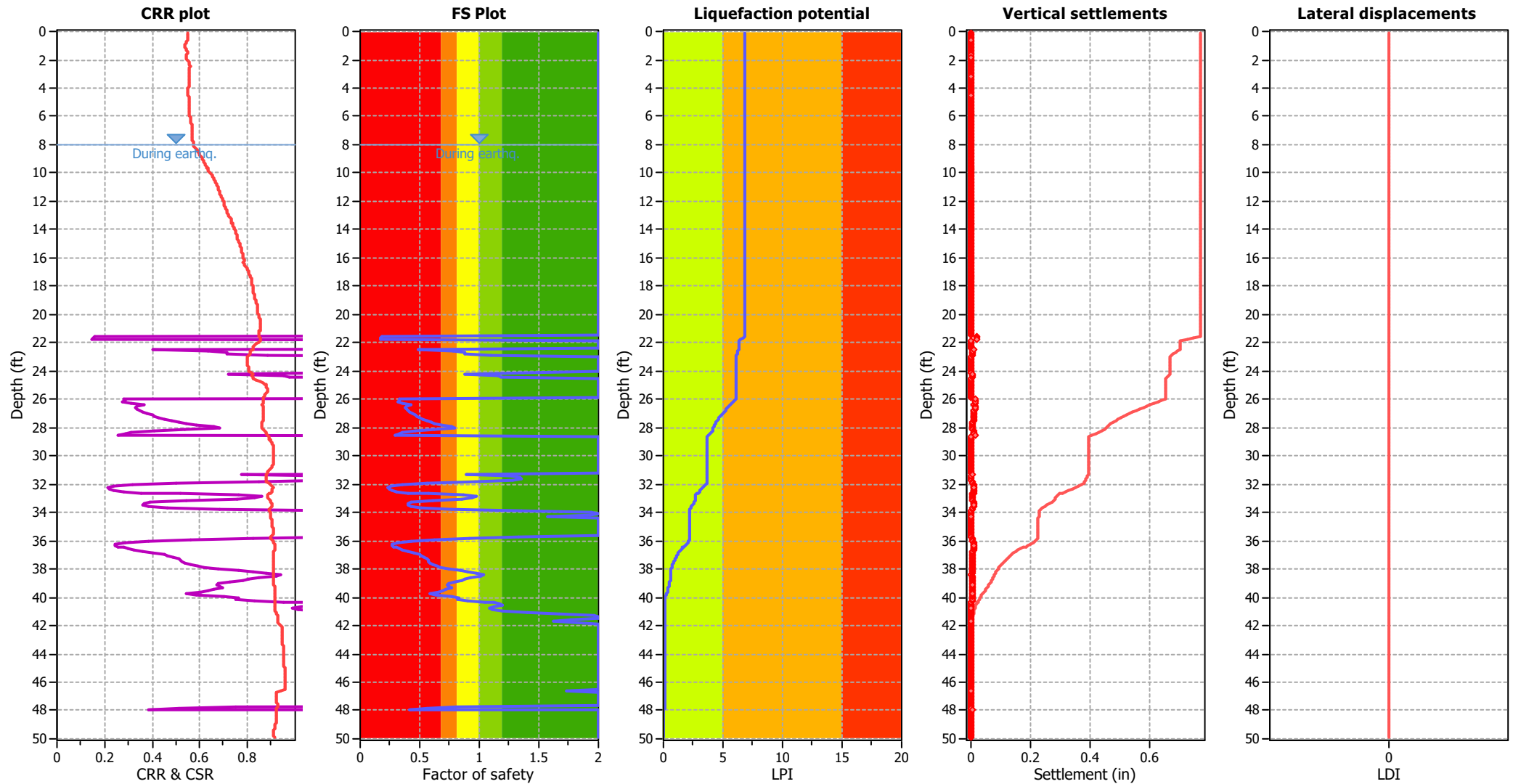
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on I_c value	I_c cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (earthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

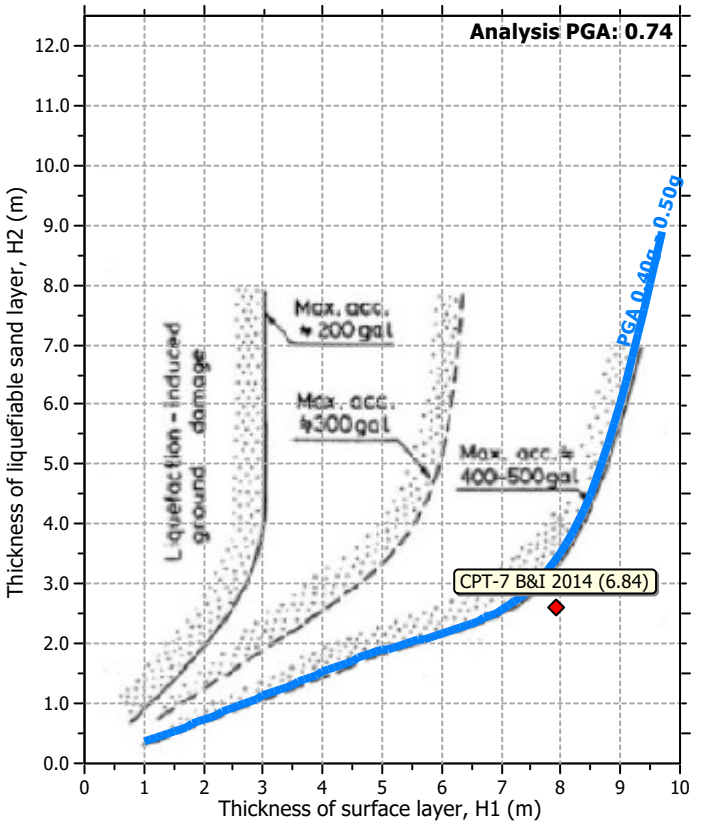
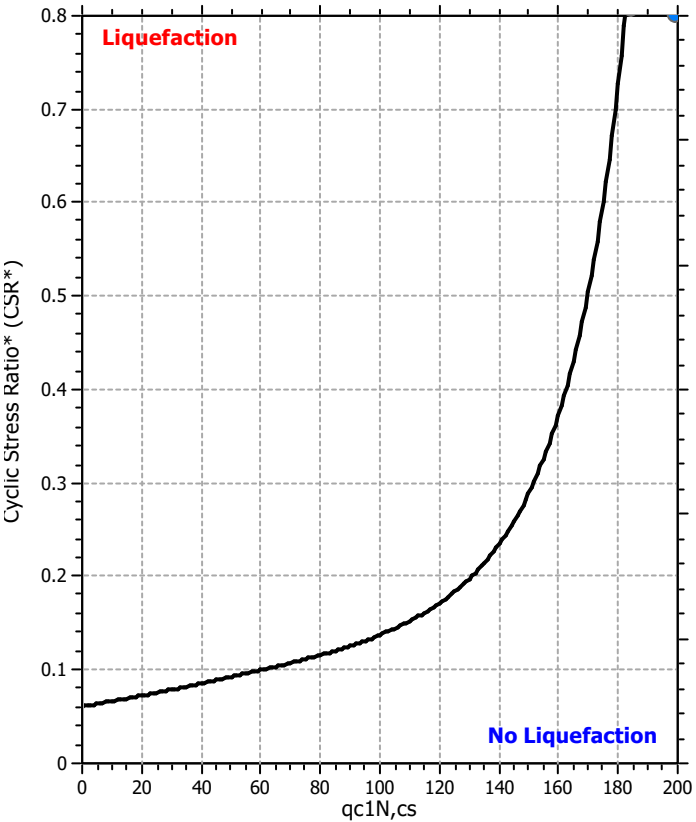
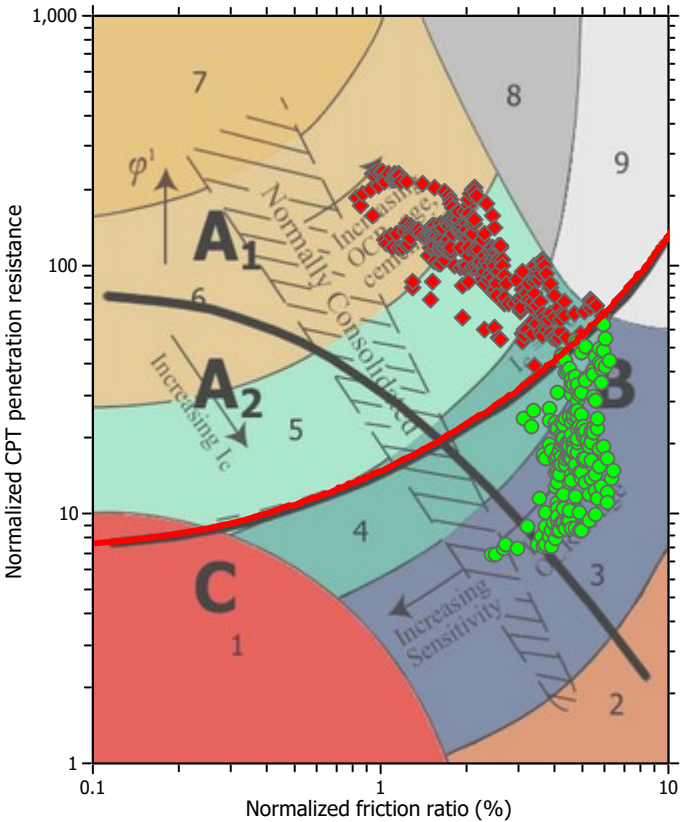
F.S. color scheme

Red	Almost certain it will liquefy
Orange	Very likely to liquefy
Yellow	Liquefaction and no liq. are equally likely
Light Green	Unlike to liquefy
Dark Green	Almost certain it will not liquefy

LPI color scheme

Red	Very high risk
Orange	High risk
Yellow	Low risk

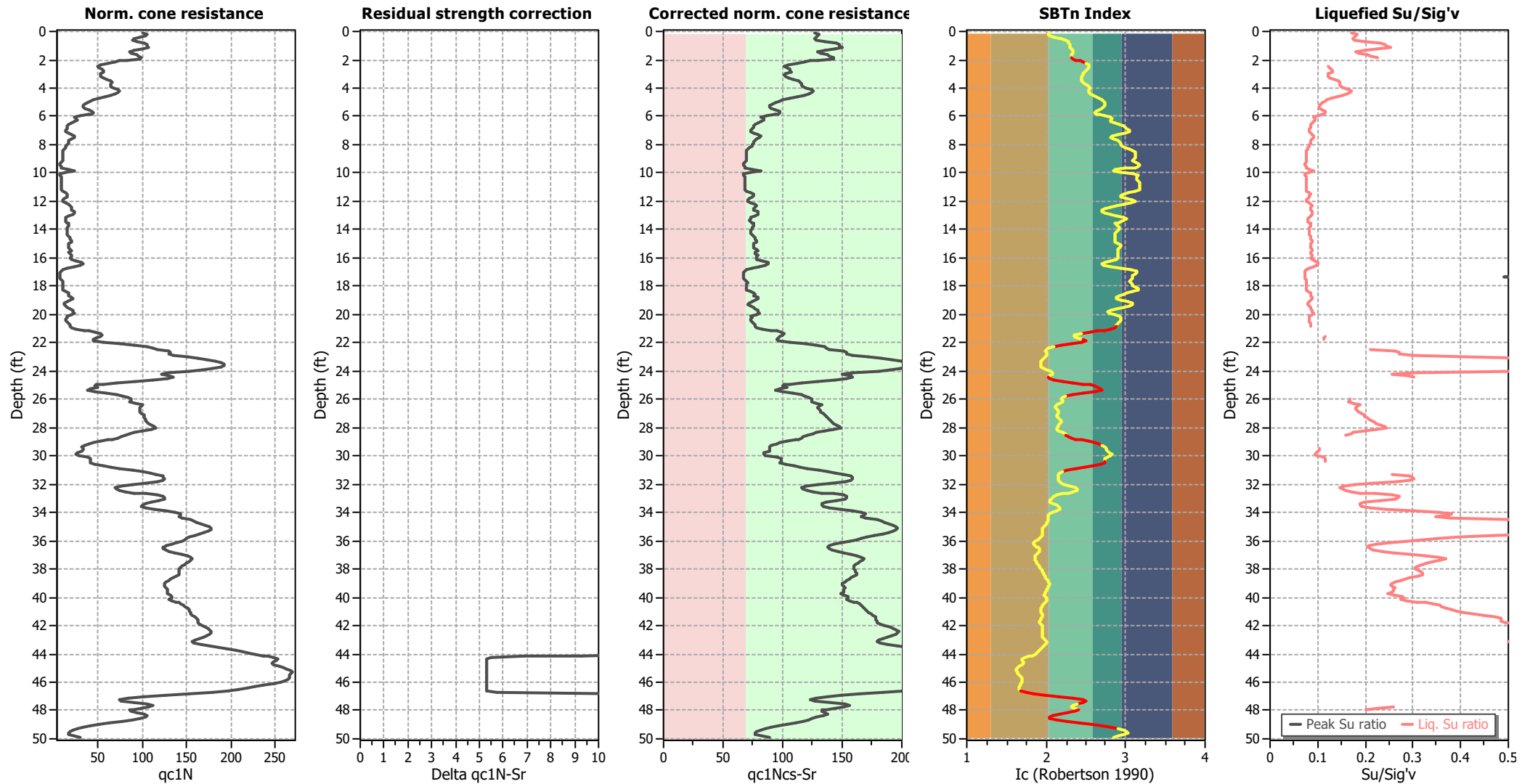
Liquefaction analysis summary plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on I_c value	I_c cut-off value:	2.60	K_{ϕ} applied:	Yes
Earthquake magnitude M_w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

Check for strength loss plots (Idriss & Boulanger (2008))



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on I_c value	I_c cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

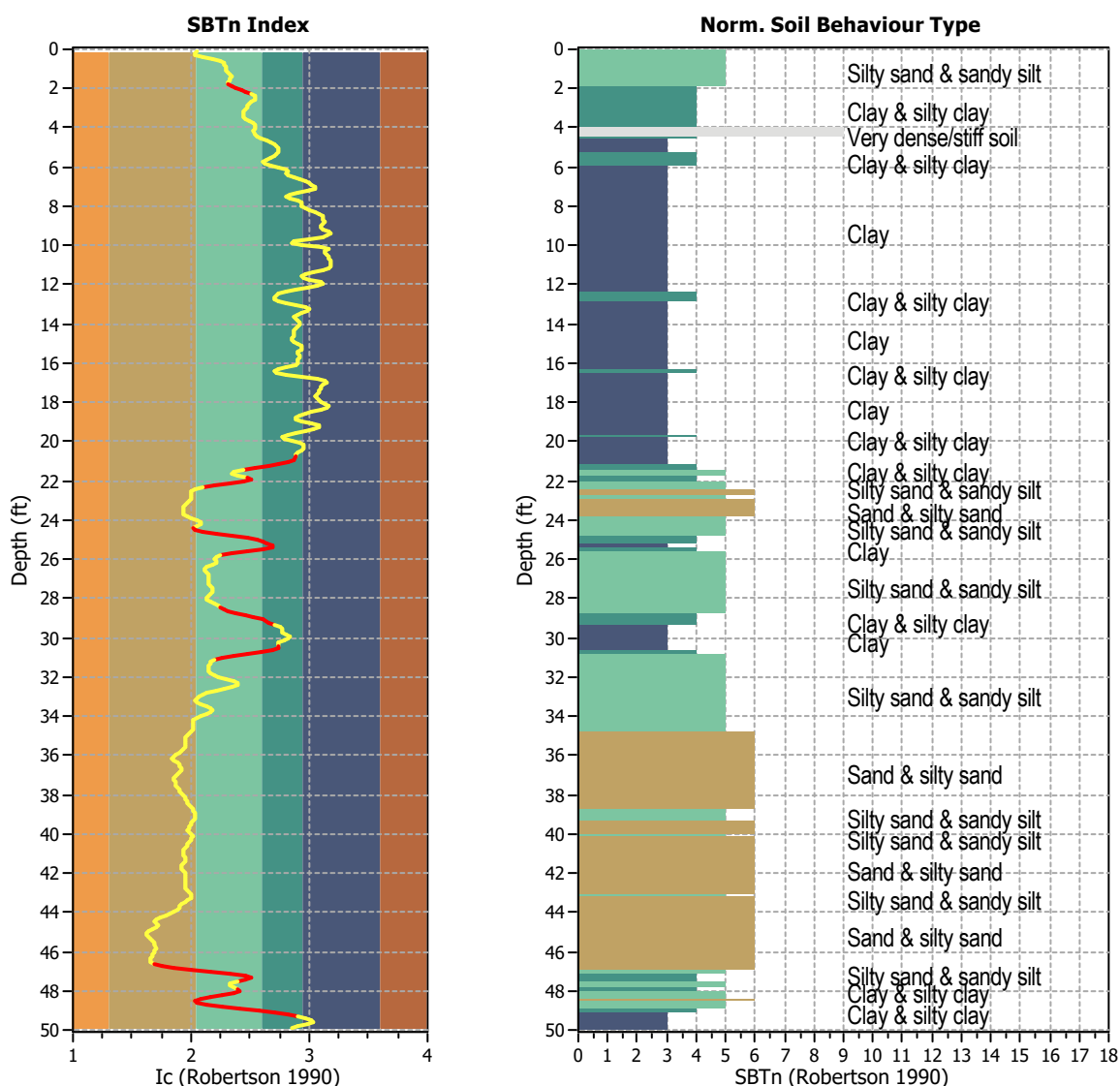
TRANSITION LAYER DETECTION ALGORITHM REPORT

Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vice-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between $1.80 < I_c < 3.0$) and a rate of change of I_c . Transitions typically occur when the rate of change of I_c is fast (i.e. ΔI_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties

I_c minimum check value: 1.70
 I_c maximum check value: 3.00
 I_c change ratio value: 0.0250
 Minimum number of points in layer: 4

General statistics

Total points in CPT file: 499
 Total points excluded: 77
 Exclusion percentage: 15.43%
 Number of layers detected: 11

Transition layer No	Number of points	Depth	SBT _n number	SBT _n description
Transition layer 1	6	Start depth: 1.90 (ft)	5	Silty sand & sandy silt
		End depth: 2.40 (ft)	4	Clay & silty clay
Transition layer 2	7	Start depth: 20.90 (ft)	3	Clay
		End depth: 21.50 (ft)	5	Silty sand & sandy silt
Transition layer 3	6	Start depth: 21.90 (ft)	4	Clay & silty clay
		End depth: 22.40 (ft)	5	Silty sand & sandy silt
Transition layer 4	9	Start depth: 24.50 (ft)	5	Silty sand & sandy silt
		End depth: 25.30 (ft)	3	Clay
Transition layer 5	6	Start depth: 25.40 (ft)	3	Clay
		End depth: 25.90 (ft)	5	Silty sand & sandy silt
Transition layer 6	9	Start depth: 28.60 (ft)	5	Silty sand & sandy silt
		End depth: 29.40 (ft)	3	Clay
Transition layer 7	8	Start depth: 30.50 (ft)	3	Clay
		End depth: 31.20 (ft)	5	Silty sand & sandy silt
Transition layer 8	7	Start depth: 46.70 (ft)	6	Sand & silty sand
		End depth: 47.30 (ft)	4	Clay & silty clay
Transition layer 9	4	Start depth: 47.30 (ft)	4	Clay & silty clay
		End depth: 47.60 (ft)	5	Silty sand & sandy silt
Transition layer 10	6	Start depth: 48.00 (ft)	4	Clay & silty clay
		End depth: 48.50 (ft)	6	Sand & silty sand
Transition layer 11	9	Start depth: 48.60 (ft)	5	Silty sand & sandy silt
		End depth: 49.40 (ft)	3	Clay

Start depth: Depth where the transition layer begins

End depth: Depth where the transition layer ends

:: Field input data ::						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1	0.10	62.12	1.11	1.11	14.25	120.61
2	0.20	65.67	0.88	0.88	13.72	120.37
3	0.30	64.54	1.00	1.00	13.96	120.43
4	0.40	60.51	1.14	1.14	15.99	121.22
5	0.50	56.13	1.28	1.28	18.33	122.03
6	0.60	54.87	1.47	1.47	20.29	123.18
7	0.70	58.51	1.82	1.82	21.47	124.64
8	0.80	63.65	2.21	2.21	22.02	125.87
9	0.90	65.07	2.35	2.35	22.24	126.55
10	1.00	65.20	2.36	2.36	22.36	126.84
11	1.10	66.36	2.45	2.45	22.64	126.76
12	1.20	62.10	2.31	2.31	23.11	126.33
13	1.30	56.71	2.05	2.05	23.71	125.47
14	1.40	52.83	1.85	1.85	23.91	124.82
15	1.50	54.10	1.87	1.87	23.65	124.79
16	1.60	57.95	2.02	2.02	23.30	125.21
17	1.70	59.39	2.11	2.11	23.05	125.75
18	1.80	61.72	2.24	2.24	23.18	126.06
19	1.90	60.58	2.25	2.25	24.01	125.82
20	2.00	51.35	2.00	2.00	25.52	125.16
21	2.10	46.06	1.87	1.87	27.49	124.29
22	2.20	42.60	1.79	1.79	29.17	123.50
23	2.30	37.67	1.60	1.60	30.79	122.52
24	2.40	32.86	1.38	1.38	32.24	121.38
25	2.50	30.55	1.26	1.26	32.77	120.66
26	2.60	31.93	1.28	1.28	32.26	120.55
27	2.70	33.72	1.31	1.31	31.30	120.75
28	2.80	34.59	1.31	1.31	30.37	120.79
29	2.90	35.10	1.26	1.26	29.88	120.28
30	3.00	32.25	1.07	1.07	29.30	119.57
31	3.10	32.25	1.00	1.00	28.84	118.93
32	3.20	32.91	1.00	1.00	28.37	119.03
33	3.30	34.32	1.09	1.09	28.12	119.68
34	3.40	36.94	1.24	1.24	27.98	120.69
35	3.50	39.82	1.41	1.41	28.15	121.72
36	3.60	40.61	1.57	1.57	28.89	122.59
37	3.70	40.38	1.73	1.73	30.25	123.28
38	3.80	39.72	1.88	1.88	31.68	123.93
39	3.90	40.08	2.06	2.06	32.65	124.61
40	4.00	42.01	2.25	2.25	32.78	125.32
41	4.10	44.76	2.42	2.42	32.31	125.84
42	4.20	46.13	2.44	2.44	32.00	126.06
43	4.30	45.11	2.41	2.41	32.32	126.02
44	4.40	43.15	2.41	2.41	33.47	125.81
45	4.50	39.94	2.35	2.35	35.18	125.35
46	4.60	35.50	2.15	2.15	37.09	124.51
47	4.70	31.31	1.89	1.89	39.02	123.32
48	4.80	27.40	1.62	1.62	40.51	122.08

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
49	4.90	25.36	1.45	1.45	41.58	120.85
50	5.00	23.26	1.26	1.26	42.10	119.69
51	5.10	21.46	1.09	1.09	42.26	118.52
52	5.20	20.47	0.97	0.97	42.07	117.63
53	5.30	20.31	0.93	0.93	41.55	117.40
54	5.40	21.51	1.00	1.00	40.41	117.90
55	5.50	24.20	1.11	1.11	38.66	118.69
56	5.60	26.63	1.17	1.17	36.96	119.19
57	5.70	27.19	1.15	1.15	36.08	119.18
58	5.80	26.09	1.08	1.08	36.44	118.82
59	5.90	24.20	1.04	1.04	38.73	117.88
60	6.00	18.70	0.87	0.87	42.79	116.46
61	6.10	14.43	0.71	0.71	46.56	115.26
62	6.20	15.81	0.76	0.76	47.33	114.70
63	6.30	16.36	0.73	0.73	46.28	114.37
64	6.40	14.76	0.61	0.61	46.82	113.29
65	6.50	12.58	0.52	0.52	49.63	111.81
66	6.60	10.49	0.46	0.46	53.60	110.66
67	6.70	9.56	0.45	0.45	56.77	110.07
68	6.80	9.56	0.45	0.45	58.22	109.83
69	6.90	9.28	0.44	0.44	59.62	109.52
70	7.00	8.34	0.41	0.41	61.31	109.42
71	7.10	8.53	0.45	0.45	61.42	110.14
72	7.20	10.24	0.56	0.56	57.61	111.75
73	7.30	13.08	0.67	0.67	51.84	113.29
74	7.40	15.78	0.70	0.70	47.65	113.79
75	7.50	15.32	0.61	0.61	46.43	113.29
76	7.60	13.16	0.53	0.53	48.42	112.25
77	7.70	11.50	0.52	0.52	51.76	111.58
78	7.80	11.15	0.52	0.52	53.70	111.28
79	7.90	11.15	0.50	0.50	54.19	110.77
80	8.00	10.29	0.43	0.43	54.54	109.83
81	8.10	9.38	0.37	0.37	55.85	108.55
82	8.20	8.44	0.32	0.32	58.05	107.26
83	8.30	7.38	0.28	0.28	61.49	105.89
84	8.40	6.21	0.24	0.24	64.67	104.85
85	8.50	6.16	0.24	0.24	66.45	104.43
86	8.60	6.37	0.25	0.25	66.66	104.68
87	8.70	6.37	0.26	0.26	67.04	104.97
88	8.80	6.30	0.27	0.27	67.60	104.95
89	8.90	6.17	0.25	0.25	67.03	104.65
90	9.00	6.31	0.23	0.23	65.43	104.09
91	9.10	6.37	0.21	0.21	64.96	103.19
92	9.20	5.58	0.18	0.18	66.88	102.02
93	9.30	4.78	0.16	0.16	70.01	101.25
94	9.40	4.94	0.17	0.17	70.97	101.70
95	9.50	5.65	0.21	0.21	69.34	102.72
96	9.60	5.97	0.22	0.22	67.11	103.28

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
97	9.70	6.07	0.21	0.21	57.98	105.40
98	9.80	11.23	0.35	0.35	49.94	109.41
99	9.90	16.32	0.63	0.63	48.71	110.74
100	10.00	9.46	0.40	0.40	53.91	109.22
101	10.10	4.78	0.17	0.17	65.39	104.46
102	10.20	5.12	0.16	0.16	69.87	101.63
103	10.30	5.83	0.20	0.20	68.12	102.57
104	10.40	5.97	0.22	0.22	67.95	103.56
105	10.50	5.97	0.24	0.24	68.89	104.08
106	10.60	5.97	0.25	0.25	69.84	104.43
107	10.70	5.97	0.26	0.26	70.68	104.72
108	10.80	5.97	0.27	0.27	71.44	104.98
109	10.90	5.97	0.28	0.28	71.69	105.06
110	11.00	5.97	0.27	0.27	71.42	104.94
111	11.10	5.97	0.26	0.26	71.41	105.00
112	11.20	6.04	0.28	0.28	70.77	106.17
113	11.30	7.21	0.38	0.38	66.78	108.66
114	11.40	10.03	0.55	0.55	61.14	110.65
115	11.50	11.35	0.56	0.56	56.35	111.43
116	11.60	11.35	0.48	0.48	53.92	110.88
117	11.70	10.78	0.43	0.43	54.85	109.75
118	11.80	8.88	0.38	0.38	58.88	108.82
119	11.90	7.64	0.37	0.37	64.81	108.53
120	12.00	7.53	0.43	0.43	66.87	109.85
121	12.10	9.60	0.60	0.60	63.19	112.05
122	12.20	12.53	0.75	0.75	56.94	113.62
123	12.30	14.26	0.71	0.71	51.16	113.74
124	12.40	14.57	0.55	0.55	46.46	112.53
125	12.50	14.33	0.43	0.43	42.92	111.26
126	12.60	15.10	0.43	0.43	40.89	111.53
127	12.70	17.53	0.57	0.57	40.85	112.76
128	12.80	17.50	0.65	0.65	42.42	113.85
129	12.90	16.02	0.68	0.68	46.19	113.83
130	13.00	13.08	0.62	0.62	51.48	112.89
131	13.10	10.27	0.51	0.51	56.53	111.47
132	13.20	9.56	0.45	0.45	58.76	110.10
133	13.30	9.56	0.40	0.40	57.38	109.40
134	13.40	10.05	0.39	0.39	54.29	109.60
135	13.50	11.78	0.46	0.46	51.64	110.49
136	13.60	12.90	0.52	0.52	50.42	111.43
137	13.70	12.74	0.54	0.54	50.80	111.99
138	13.80	12.58	0.57	0.57	52.29	111.96
139	13.90	11.65	0.53	0.53	53.34	111.53
140	14.00	11.15	0.47	0.47	53.32	110.70
141	14.10	11.15	0.42	0.42	52.04	109.85
142	14.20	11.15	0.38	0.38	50.88	109.28
143	14.30	11.16	0.37	0.37	50.20	109.46
144	14.40	12.06	0.44	0.44	50.15	110.44

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
145	14.50	12.99	0.53	0.53	50.14	111.85
146	14.60	13.93	0.62	0.62	50.06	113.12
147	14.70	14.88	0.69	0.69	49.55	114.09
148	14.80	15.80	0.75	0.75	49.44	114.51
149	14.90	15.15	0.72	0.72	50.36	114.29
150	15.00	13.46	0.65	0.65	52.23	113.71
151	15.10	12.74	0.63	0.63	53.98	113.27
152	15.20	12.74	0.64	0.64	54.50	113.33
153	15.30	13.23	0.67	0.67	53.67	113.93
154	15.40	14.80	0.76	0.76	52.31	114.72
155	15.50	15.88	0.82	0.82	52.17	114.92
156	15.60	13.94	0.72	0.72	52.62	114.87
157	15.70	14.32	0.75	0.75	52.66	114.94
158	15.80	16.07	0.84	0.84	51.78	115.33
159	15.90	15.89	0.82	0.82	51.70	115.48
160	16.00	14.87	0.79	0.79	52.38	115.58
161	16.10	15.70	0.88	0.88	50.63	116.73
162	16.20	20.96	1.14	1.14	46.27	118.49
163	16.30	26.45	1.33	1.33	42.36	119.66
164	16.40	27.11	1.24	1.24	40.60	119.63
165	16.50	24.54	1.07	1.07	41.87	118.34
166	16.60	18.69	0.84	0.84	46.34	115.95
167	16.70	12.01	0.56	0.56	53.94	112.58
168	16.80	8.20	0.35	0.35	63.04	108.53
169	16.90	6.52	0.23	0.23	68.24	104.90
170	17.00	5.97	0.17	0.17	68.56	102.33
171	17.10	5.97	0.15	0.15	66.69	100.78
172	17.20	5.97	0.13	0.13	64.81	99.93
173	17.30	5.97	0.12	0.12	64.79	99.07
174	17.40	5.42	0.11	0.11	64.52	98.97
175	17.50	6.03	0.13	0.13	64.03	100.62
176	17.60	7.35	0.20	0.20	62.75	103.49
177	17.70	8.34	0.28	0.28	62.31	105.74
178	17.80	8.53	0.32	0.32	62.86	106.83
179	17.90	8.36	0.32	0.32	63.84	107.19
180	18.00	8.36	0.33	0.33	64.95	107.44
181	18.10	8.36	0.36	0.36	67.40	107.80
182	18.20	7.76	0.38	0.38	69.99	108.61
183	18.30	8.26	0.46	0.46	69.58	110.41
184	18.40	10.77	0.64	0.64	64.87	112.73
185	18.50	13.65	0.80	0.80	59.87	114.32
186	18.60	14.54	0.78	0.78	56.56	114.73
187	18.70	14.34	0.70	0.70	53.10	115.00
188	18.80	17.54	0.82	0.82	51.01	115.44
189	18.90	17.97	0.87	0.87	51.09	115.72
190	19.00	15.09	0.78	0.78	54.33	115.00
191	19.10	12.43	0.67	0.67	59.98	113.38
192	19.20	9.96	0.53	0.53	64.43	111.80

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
193	19.30	9.56	0.48	0.48	64.73	111.22
194	19.40	11.42	0.56	0.56	61.22	111.99
195	19.50	13.35	0.65	0.65	56.44	113.23
196	19.60	15.38	0.69	0.69	51.44	114.22
197	19.70	18.28	0.72	0.72	46.98	114.59
198	19.80	19.54	0.67	0.67	44.39	115.03
199	19.90	20.23	0.76	0.76	45.58	115.04
200	20.00	16.72	0.74	0.74	49.34	114.17
201	20.10	12.54	0.51	0.51	53.36	112.57
202	20.20	12.54	0.46	0.46	54.92	110.89
203	20.30	12.26	0.44	0.44	54.74	110.67
204	20.40	12.34	0.47	0.47	54.89	110.97
205	20.50	13.04	0.51	0.51	53.87	111.57
206	20.60	14.29	0.54	0.54	51.97	112.28
207	20.70	15.53	0.58	0.58	50.93	113.04
208	20.80	15.80	0.65	0.65	50.79	114.36
209	20.90	17.69	0.84	0.84	50.10	116.70
210	21.00	22.85	1.23	1.23	47.01	119.74
211	21.10	30.95	1.73	1.73	42.76	122.10
212	21.20	36.95	1.89	1.89	37.99	123.36
213	21.30	42.88	1.77	1.77	32.84	123.29
214	21.40	48.29	1.43	1.43	28.05	122.38
215	21.50	50.56	1.15	1.15	24.82	121.09
216	21.60	48.73	1.01	1.01	24.24	120.28
217	21.70	44.97	1.08	1.08	26.24	120.39
218	21.80	41.67	1.27	1.27	29.46	121.37
219	21.90	41.81	1.56	1.56	30.68	123.13
220	22.00	53.30	2.04	2.04	28.09	125.04
221	22.10	71.40	2.32	2.32	23.43	126.27
222	22.20	86.36	2.11	2.11	18.88	126.63
223	22.30	100.73	1.92	1.92	15.56	126.34
224	22.40	107.91	1.82	1.82	13.72	126.24
225	22.50	112.51	1.86	1.86	12.92	126.78
226	22.60	125.62	2.21	2.21	12.78	127.58
227	22.70	127.85	2.37	2.37	12.87	128.28
228	22.80	126.96	2.42	2.42	13.07	128.73
229	22.90	132.58	2.60	2.60	12.92	129.43
230	23.00	148.53	2.97	2.97	12.48	130.33
231	23.10	161.03	3.23	3.23	11.94	131.21
232	23.20	171.66	3.45	3.45	11.56	131.89
233	23.30	180.86	3.69	3.69	11.34	132.48
234	23.40	188.14	3.92	3.92	11.23	132.97
235	23.50	192.96	4.05	4.05	11.19	133.25
236	23.60	193.28	4.06	4.06	11.22	133.28
237	23.70	188.79	3.97	3.97	11.41	133.08
238	23.80	179.85	3.82	3.82	11.92	132.77
239	23.90	167.36	3.74	3.74	13.07	132.61
240	24.00	152.93	3.99	3.99	14.44	131.96

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
241	24.10	128.06	3.23	3.23	15.43	130.96
242	24.20	120.75	2.69	2.69	15.11	129.79
243	24.30	130.48	2.68	2.68	14.12	129.25
244	24.40	134.08	2.57	2.57	13.50	129.02
245	24.50	127.67	2.40	2.40	14.05	128.67
246	24.60	112.13	2.44	2.44	15.90	128.09
247	24.70	91.10	2.29	2.29	19.38	127.41
248	24.80	70.09	2.20	2.20	24.09	126.50
249	24.90	55.08	2.13	2.13	29.38	125.73
250	25.00	47.92	2.10	2.10	33.53	125.31
251	25.10	46.01	2.15	2.15	35.64	125.53
252	25.20	48.30	2.42	2.42	37.64	125.59
253	25.30	40.96	2.27	2.27	39.78	125.44
254	25.40	37.60	2.15	2.15	40.27	125.28
255	25.50	45.69	2.32	2.32	35.93	125.60
256	25.60	59.12	2.25	2.25	29.40	125.83
257	25.70	70.65	1.91	1.91	24.01	125.60
258	25.80	78.06	1.77	1.77	20.71	125.47
259	25.90	85.13	1.92	1.92	19.26	125.67
260	26.00	87.95	1.93	1.93	18.85	126.02
261	26.10	87.87	1.97	1.97	19.31	126.45
262	26.20	87.00	2.27	2.27	19.35	126.78
263	26.30	93.02	2.17	2.17	18.31	126.87
264	26.40	101.50	1.94	1.94	16.83	126.57
265	26.50	100.65	1.91	1.91	16.09	126.34
266	26.60	99.24	1.95	1.95	16.44	126.43
267	26.70	98.75	2.03	2.03	16.91	126.70
268	26.80	99.34	2.14	2.14	17.25	127.00
269	26.90	100.26	2.20	2.20	17.37	127.26
270	27.00	102.18	2.24	2.24	17.28	127.47
271	27.10	104.61	2.29	2.29	17.13	127.62
272	27.20	105.31	2.29	2.29	17.12	127.80
273	27.30	106.02	2.39	2.39	17.44	128.11
274	27.40	106.45	2.58	2.58	18.00	128.60
275	27.50	107.27	2.78	2.78	18.48	129.07
276	27.60	108.97	2.87	2.87	18.55	129.33
277	27.70	111.05	2.84	2.84	18.18	129.40
278	27.80	114.11	2.80	2.80	17.73	129.50
279	27.90	117.82	2.92	2.92	17.36	129.62
280	28.00	119.46	2.91	2.91	17.01	129.37
281	28.10	114.35	2.51	2.51	16.90	128.66
282	28.20	105.16	2.25	2.25	17.71	127.93
283	28.30	94.00	2.36	2.36	19.01	127.45
284	28.40	89.72	2.24	2.24	20.28	127.04
285	28.50	84.46	2.03	2.03	20.76	126.38
286	28.60	79.30	1.90	1.90	21.64	125.93
287	28.70	75.30	1.99	1.99	23.18	125.79
288	28.80	69.49	2.04	2.04	25.54	126.01

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
289	28.90	64.38	2.23	2.23	28.62	125.96
290	29.00	54.68	2.17	2.17	32.16	125.55
291	29.10	46.36	1.96	1.96	35.58	124.66
292	29.20	41.69	1.79	1.79	38.50	123.57
293	29.30	36.17	1.59	1.59	40.97	122.75
294	29.40	33.64	1.57	1.57	43.00	122.38
295	29.50	34.22	1.66	1.66	43.89	122.40
296	29.60	34.24	1.64	1.64	43.88	122.30
297	29.70	33.20	1.50	1.50	44.57	121.53
298	29.80	28.58	1.26	1.26	46.00	120.71
299	29.90	27.15	1.27	1.27	47.71	120.62
300	30.00	29.51	1.51	1.51	47.14	122.69
301	30.10	40.11	2.36	2.36	44.95	124.72
302	30.20	44.56	2.55	2.55	42.71	125.95
303	30.30	44.79	2.38	2.38	42.23	126.30
304	30.40	44.42	2.63	2.63	42.91	126.46
305	30.50	43.75	2.73	2.73	42.81	127.09
306	30.60	50.30	2.97	2.97	39.90	127.67
307	30.70	60.15	3.00	3.00	35.08	128.01
308	30.80	68.63	2.70	2.70	29.81	127.98
309	30.90	79.95	2.51	2.51	24.94	127.95
310	31.00	95.74	2.54	2.54	21.22	128.19
311	31.10	108.20	2.58	2.58	18.95	128.70
312	31.20	116.40	2.74	2.74	17.90	129.43
313	31.30	125.14	3.11	3.11	17.61	130.33
314	31.40	132.59	3.46	3.46	17.53	131.01
315	31.50	134.16	3.49	3.49	17.33	131.26
316	31.60	134.92	3.37	3.37	17.19	131.19
317	31.70	133.66	3.35	3.35	17.30	130.97
318	31.80	127.28	3.25	3.25	17.79	130.39
319	31.90	113.49	2.79	2.79	18.65	129.27
320	32.00	97.18	2.30	2.30	20.17	127.91
321	32.10	82.95	2.17	2.17	22.56	127.10
322	32.20	75.89	2.32	2.32	25.11	127.21
323	32.30	76.91	2.59	2.59	26.31	127.76
324	32.40	81.31	2.75	2.75	25.83	128.38
325	32.50	88.72	2.85	2.85	24.20	128.91
326	32.60	99.73	2.95	2.95	21.87	129.41
327	32.70	114.05	3.00	3.00	19.29	129.79
328	32.80	128.47	2.96	2.96	16.92	129.78
329	32.90	135.28	2.65	2.65	15.59	129.77
330	33.00	136.97	2.82	2.82	14.94	129.63
331	33.10	137.32	2.73	2.73	14.43	129.04
332	33.20	131.16	2.05	2.05	14.05	128.05
333	33.30	121.17	1.95	1.95	14.15	127.08
334	33.40	114.56	2.02	2.02	15.40	127.07
335	33.50	110.40	2.15	2.15	16.68	127.46
336	33.60	109.94	2.36	2.36	17.68	128.18

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
337	33.70	114.61	2.69	2.69	18.16	129.23
338	33.80	125.09	3.15	3.15	17.82	130.33
339	33.90	139.40	3.43	3.43	16.76	131.05
340	34.00	150.31	3.36	3.36	15.36	131.28
341	34.10	158.13	3.20	3.20	14.15	131.06
342	34.20	159.43	2.99	2.99	13.52	130.77
343	34.30	156.51	2.94	2.94	13.43	130.76
344	34.40	160.32	3.17	3.17	13.54	131.26
345	34.50	171.85	3.55	3.55	13.58	131.90
346	34.60	175.59	3.69	3.69	13.48	132.37
347	34.70	178.50	3.75	3.75	13.36	132.62
348	34.80	183.69	3.85	3.85	13.06	132.79
349	34.90	189.77	3.86	3.86	12.56	132.85
350	35.00	195.04	3.72	3.72	11.98	132.76
351	35.10	197.97	3.62	3.62	11.62	132.64
352	35.20	197.15	3.63	3.63	11.58	132.57
353	35.30	193.85	3.62	3.62	11.71	132.44
354	35.40	189.59	3.48	3.48	11.78	132.12
355	35.50	184.43	3.26	3.26	11.72	131.62
356	35.60	178.42	3.01	3.01	11.57	130.96
357	35.70	172.55	2.74	2.74	11.31	130.25
358	35.80	169.23	2.50	2.50	10.90	129.49
359	35.90	167.16	2.25	2.25	10.28	128.61
360	36.00	164.14	1.92	1.92	9.62	127.58
361	36.10	158.65	1.67	1.67	9.13	126.50
362	36.20	151.89	1.51	1.51	9.08	125.74
363	36.30	146.37	1.48	1.48	9.44	125.48
364	36.40	143.07	1.56	1.56	9.96	125.62
365	36.50	142.15	1.62	1.62	10.39	125.87
366	36.60	142.29	1.66	1.66	10.62	126.15
367	36.70	144.50	1.74	1.74	10.71	126.55
368	36.80	149.98	1.87	1.87	10.63	127.05
369	36.90	157.12	1.98	1.98	10.39	127.61
370	37.00	165.79	2.09	2.09	10.01	128.05
371	37.10	172.94	2.14	2.14	9.57	128.32
372	37.20	178.15	2.12	2.12	9.31	128.52
373	37.30	180.12	2.20	2.20	9.29	128.66
374	37.40	178.24	2.25	2.25	9.48	128.74
375	37.50	175.41	2.21	2.21	9.70	128.71
376	37.60	172.60	2.21	2.21	9.96	128.68
377	37.70	169.84	2.25	2.25	10.28	128.70
378	37.80	167.17	2.26	2.26	10.62	128.74
379	37.90	164.65	2.28	2.28	10.94	128.82
380	38.00	163.65	2.35	2.35	11.28	128.99
381	38.10	163.65	2.44	2.44	11.58	129.22
382	38.20	163.65	2.51	2.51	11.78	129.38
383	38.30	163.65	2.52	2.52	11.97	129.52
384	38.40	163.06	2.59	2.59	12.22	129.61

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
385	38.50	160.28	2.62	2.62	12.53	129.60
386	38.60	156.28	2.55	2.55	12.84	129.50
387	38.70	153.03	2.53	2.53	13.18	129.40
388	38.80	150.19	2.57	2.57	13.54	129.33
389	38.90	146.91	2.54	2.54	13.85	129.25
390	39.00	144.63	2.50	2.50	14.01	129.15
391	39.10	144.61	2.50	2.50	13.99	129.09
392	39.20	146.23	2.48	2.48	13.78	129.06
393	39.30	148.58	2.45	2.45	13.49	128.99
394	39.40	149.32	2.40	2.40	13.17	128.87
395	39.50	150.21	2.33	2.33	12.90	128.72
396	39.60	151.05	2.29	2.29	12.65	128.52
397	39.70	149.98	2.20	2.20	12.40	128.42
398	39.80	153.45	2.22	2.22	12.24	128.47
399	39.90	156.55	2.32	2.32	12.46	128.85
400	40.00	155.18	2.53	2.53	12.93	129.21
401	40.10	152.74	2.58	2.58	13.25	129.44
402	40.20	155.87	2.56	2.56	13.15	129.56
403	40.30	161.19	2.63	2.63	12.84	129.73
404	40.40	165.15	2.69	2.69	12.55	129.92
405	40.50	168.76	2.70	2.70	12.23	130.02
406	40.60	172.47	2.68	2.68	11.87	130.02
407	40.70	174.92	2.64	2.64	11.49	129.96
408	40.80	177.50	2.59	2.59	11.19	129.92
409	40.90	179.68	2.60	2.60	11.05	129.96
410	41.00	180.41	2.66	2.66	11.15	130.15
411	41.10	181.21	2.77	2.77	11.39	130.44
412	41.20	182.62	2.91	2.91	11.59	130.73
413	41.30	184.37	2.97	2.97	11.72	131.00
414	41.40	186.92	3.07	3.07	11.67	131.15
415	41.50	189.15	3.06	3.06	11.38	131.08
416	41.60	191.15	2.85	2.85	10.98	130.87
417	41.70	192.32	2.80	2.80	10.77	130.77
418	41.80	192.51	2.92	2.92	10.94	130.99
419	41.90	193.81	3.10	3.10	11.29	131.42
420	42.00	196.74	3.31	3.31	11.56	131.87
421	42.10	200.73	3.46	3.46	11.69	132.25
422	42.20	204.20	3.57	3.57	11.76	132.58
423	42.30	206.83	3.72	3.72	11.83	132.83
424	42.40	208.60	3.78	3.78	11.83	132.94
425	42.50	208.79	3.71	3.71	11.73	132.86
426	42.60	207.34	3.60	3.60	11.66	132.67
427	42.70	203.82	3.52	3.52	11.63	132.39
428	42.80	199.71	3.36	3.36	11.68	132.09
429	42.90	195.04	3.24	3.24	11.91	131.87
430	43.00	189.24	3.30	3.30	12.39	131.86
431	43.10	186.13	3.44	3.44	12.92	132.08
432	43.20	188.06	3.58	3.58	13.08	132.40

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
433	43.30	196.05	3.72	3.72	12.78	132.76
434	43.40	207.87	3.84	3.84	12.20	133.12
435	43.50	219.31	3.94	3.94	11.55	133.45
436	43.60	230.68	4.03	4.03	10.99	133.77
437	43.70	241.27	4.17	4.17	10.58	134.10
438	43.80	250.16	4.32	4.32	10.29	134.43
439	43.90	257.85	4.45	4.45	10.00	134.71
440	44.00	267.83	4.52	4.52	9.46	134.79
441	44.10	278.09	4.29	4.29	8.69	134.58
442	44.20	284.44	3.95	3.95	7.73	134.08
443	44.30	291.84	3.56	3.56	6.75	133.40
444	44.40	296.88	3.17	3.17	6.08	132.84
445	44.50	295.68	3.12	3.12	5.94	132.67
446	44.60	291.63	3.34	3.34	6.27	132.91
447	44.70	290.21	3.51	3.51	6.45	133.07
448	44.80	293.38	3.34	3.34	6.14	132.85
449	44.90	299.36	3.02	3.02	5.49	132.35
450	45.00	305.12	2.80	2.80	4.94	131.97
451	45.10	310.53	2.83	2.83	4.77	132.04
452	45.20	315.26	3.05	3.05	4.84	132.34
453	45.30	318.00	3.12	3.12	4.99	132.63
454	45.40	316.61	3.18	3.18	5.18	132.83
455	45.50	313.71	3.31	3.31	5.46	133.09
456	45.60	313.78	3.48	3.48	5.77	133.41
457	45.70	314.24	3.63	3.63	6.00	133.64
458	45.80	312.48	3.65	3.65	6.06	133.63
459	45.90	309.29	3.49	3.49	5.99	133.34
460	46.00	303.00	3.26	3.26	5.88	132.88
461	46.10	294.16	3.07	3.07	5.75	132.23
462	46.20	283.73	2.75	2.75	5.63	131.51
463	46.30	273.33	2.50	2.50	5.43	130.65
464	46.40	264.12	2.23	2.23	5.28	129.82
465	46.50	254.52	2.03	2.03	5.30	129.12
466	46.60	241.59	1.97	1.97	5.80	128.74
467	46.70	221.77	2.03	2.03	7.02	128.59
468	46.80	191.87	2.09	2.09	9.22	128.57
469	46.90	158.27	2.24	2.24	12.74	128.69
470	47.00	128.04	2.53	2.53	17.72	129.08
471	47.10	106.41	2.96	2.96	23.55	129.72
472	47.20	94.27	3.45	3.45	28.72	130.82
473	47.30	96.77	4.33	4.33	30.73	132.24
474	47.40	114.24	5.15	5.15	29.15	133.35
475	47.50	130.91	5.00	5.00	26.04	133.65
476	47.60	138.57	4.38	4.38	23.74	133.20
477	47.70	133.49	4.06	4.06	23.40	132.66
478	47.80	122.92	4.14	4.14	24.83	132.34
479	47.90	113.19	4.11	4.11	26.41	132.02
480	48.00	108.80	3.81	3.81	26.50	131.48

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
481	48.10	111.26	3.40	3.40	24.53	130.70
482	48.20	119.50	2.91	2.91	21.21	129.74
483	48.30	129.41	2.38	2.38	17.74	128.48
484	48.40	133.97	1.89	1.89	15.12	127.06
485	48.50	131.64	1.58	1.58	13.90	125.83
486	48.60	125.12	1.49	1.49	14.36	125.25
487	48.70	114.32	1.59	1.59	16.69	125.43
488	48.80	99.24	1.85	1.85	20.92	125.98
489	48.90	82.59	2.12	2.12	26.89	126.43
490	49.00	66.86	2.30	2.30	33.78	126.42
491	49.10	54.46	2.26	2.26	40.76	125.73
492	49.20	43.64	1.96	1.96	46.99	124.42
493	49.30	35.72	1.63	1.63	52.15	122.56
494	49.40	29.29	1.27	1.27	56.31	120.52
495	49.50	25.18	1.01	1.01	59.25	118.55
496	49.60	23.12	0.86	0.86	60.41	117.25
497	49.70	23.18	0.83	0.83	57.24	118.02
498	49.80	32.45	1.22	1.22	52.58	120.36
499	49.90	41.22	1.69	1.69	49.14	122.29

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q_c :	Measured cone resistance (tsf)
f_s :	Sleeve friction resistance (tsf)
u :	Pore pressure (tsf)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (pcf)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
1	0.10	0.01	0.00	0.01	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
2	0.20	0.01	0.00	0.01	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
3	0.30	0.02	0.00	0.02	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
4	0.40	0.02	0.00	0.02	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
5	0.50	0.03	0.00	0.03	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
6	0.60	0.04	0.00	0.04	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
7	0.70	0.04	0.00	0.04	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
8	0.80	0.05	0.00	0.05	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
9	0.90	0.06	0.00	0.06	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
10	1.00	0.06	0.00	0.06	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
11	1.10	0.07	0.00	0.07	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
12	1.20	0.07	0.00	0.07	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
13	1.30	0.08	0.00	0.08	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
14	1.40	0.09	0.00	0.09	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
15	1.50	0.09	0.00	0.09	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
16	1.60	0.10	0.00	0.10	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
17	1.70	0.11	0.00	0.11	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
18	1.80	0.11	0.00	0.11	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
19	1.90	0.12	0.00	0.12	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
20	2.00	0.12	0.00	0.12	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
21	2.10	0.13	0.00	0.13	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
22	2.20	0.14	0.00	0.14	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
23	2.30	0.14	0.00	0.14	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
24	2.40	0.15	0.00	0.15	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
25	2.50	0.16	0.00	0.16	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
26	2.60	0.16	0.00	0.16	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
27	2.70	0.17	0.00	0.17	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
28	2.80	0.17	0.00	0.17	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
29	2.90	0.18	0.00	0.18	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
30	3.00	0.19	0.00	0.19	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
31	3.10	0.19	0.00	0.19	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
32	3.20	0.20	0.00	0.20	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
33	3.30	0.20	0.00	0.20	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
34	3.40	0.21	0.00	0.21	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
35	3.50	0.22	0.00	0.22	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
36	3.60	0.22	0.00	0.22	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
37	3.70	0.23	0.00	0.23	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
38	3.80	0.23	0.00	0.23	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
39	3.90	0.24	0.00	0.24	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
40	4.00	0.25	0.00	0.25	1.00	0.479	1.04	0.460	1.10	1.30	2.000	No
41	4.10	0.25	0.00	0.25	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
42	4.20	0.26	0.00	0.26	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
43	4.30	0.26	0.00	0.26	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
44	4.40	0.27	0.00	0.27	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
45	4.50	0.28	0.00	0.28	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
46	4.60	0.28	0.00	0.28	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
47	4.70	0.29	0.00	0.29	0.99	0.479	1.04	0.459	1.10	1.30	2.000	No
48	4.80	0.30	0.00	0.30	0.99	0.478	1.04	0.459	1.10	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
49	4.90	0.30	0.00	0.30	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
50	5.00	0.31	0.00	0.31	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
51	5.10	0.31	0.00	0.31	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
52	5.20	0.32	0.00	0.32	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
53	5.30	0.33	0.00	0.33	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
54	5.40	0.33	0.00	0.33	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
55	5.50	0.34	0.00	0.34	0.99	0.477	1.04	0.458	1.10	1.30	2.000	No
56	5.60	0.34	0.00	0.34	0.99	0.477	1.04	0.458	1.10	1.30	2.000	No
57	5.70	0.35	0.00	0.35	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
58	5.80	0.36	0.00	0.36	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
59	5.90	0.36	0.00	0.36	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
60	6.00	0.37	0.00	0.37	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
61	6.10	0.37	0.00	0.37	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
62	6.20	0.38	0.00	0.38	0.99	0.477	1.04	0.457	1.10	1.30	2.000	No
63	6.30	0.38	0.00	0.38	0.99	0.476	1.04	0.457	1.10	1.30	2.000	No
64	6.40	0.39	0.00	0.39	0.99	0.476	1.04	0.456	1.09	1.30	2.000	No
65	6.50	0.40	0.00	0.40	0.99	0.476	1.04	0.456	1.09	1.30	2.000	No
66	6.60	0.40	0.00	0.40	0.99	0.476	1.04	0.456	1.09	1.30	2.000	No
67	6.70	0.41	0.00	0.41	0.99	0.476	1.04	0.456	1.08	1.30	2.000	No
68	6.80	0.41	0.00	0.41	0.99	0.476	1.04	0.456	1.08	1.30	2.000	No
69	6.90	0.42	0.00	0.42	0.99	0.476	1.04	0.456	1.08	1.30	2.000	No
70	7.00	0.42	0.00	0.42	0.99	0.475	1.04	0.456	1.08	1.30	2.000	No
71	7.10	0.43	0.00	0.43	0.99	0.475	1.04	0.455	1.08	1.30	2.000	No
72	7.20	0.43	0.00	0.43	0.99	0.475	1.04	0.455	1.08	1.30	2.000	No
73	7.30	0.44	0.00	0.44	0.99	0.475	1.04	0.455	1.08	1.30	2.000	No
74	7.40	0.45	0.00	0.45	0.99	0.475	1.04	0.455	1.08	1.30	2.000	No
75	7.50	0.45	0.00	0.45	0.99	0.475	1.04	0.455	1.08	1.30	2.000	No
76	7.60	0.46	0.00	0.46	0.99	0.475	1.04	0.455	1.08	1.30	2.000	No
77	7.70	0.46	0.00	0.46	0.99	0.474	1.04	0.455	1.07	1.30	2.000	No
78	7.80	0.47	0.00	0.47	0.99	0.474	1.04	0.455	1.07	1.30	2.000	No
79	7.90	0.47	0.00	0.47	0.99	0.474	1.04	0.454	1.07	1.30	2.000	No
80	8.00	0.48	0.00	0.48	0.99	0.474	1.04	0.454	1.07	1.30	2.000	No
81	8.10	0.48	0.00	0.48	0.98	0.477	1.04	0.457	1.07	1.30	0.576	No
82	8.20	0.49	0.01	0.48	0.98	0.480	1.04	0.460	1.07	1.30	0.580	No
83	8.30	0.50	0.01	0.49	0.98	0.483	1.04	0.463	1.06	1.30	0.585	No
84	8.40	0.50	0.01	0.49	0.98	0.485	1.04	0.465	1.06	1.30	0.589	No
85	8.50	0.51	0.02	0.49	0.98	0.488	1.04	0.468	1.06	1.30	0.593	No
86	8.60	0.51	0.02	0.49	0.98	0.491	1.04	0.471	1.06	1.30	0.596	No
87	8.70	0.52	0.02	0.49	0.98	0.494	1.04	0.473	1.06	1.30	0.600	No
88	8.80	0.52	0.02	0.50	0.98	0.496	1.04	0.476	1.06	1.30	0.603	No
89	8.90	0.53	0.03	0.50	0.98	0.499	1.04	0.478	1.06	1.30	0.607	No
90	9.00	0.53	0.03	0.50	0.98	0.502	1.04	0.481	1.06	1.30	0.610	No
91	9.10	0.54	0.03	0.50	0.98	0.505	1.04	0.484	1.06	1.30	0.614	No
92	9.20	0.54	0.04	0.50	0.98	0.507	1.04	0.486	1.06	1.30	0.618	No
93	9.30	0.55	0.04	0.51	0.98	0.510	1.04	0.489	1.06	1.30	0.622	No
94	9.40	0.55	0.04	0.51	0.98	0.512	1.04	0.491	1.06	1.30	0.625	No
95	9.50	0.56	0.05	0.51	0.98	0.515	1.04	0.494	1.06	1.30	0.628	No
96	9.60	0.56	0.05	0.51	0.98	0.517	1.04	0.496	1.06	1.30	0.631	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
97	9.70	0.57	0.05	0.51	0.98	0.520	1.04	0.498	1.06	1.30	0.634	No
98	9.80	0.57	0.06	0.52	0.98	0.522	1.04	0.501	1.06	1.30	0.634	No
99	9.90	0.58	0.06	0.52	0.98	0.525	1.04	0.503	1.07	1.30	0.634	No
100	10.00	0.58	0.06	0.52	0.98	0.527	1.04	0.505	1.06	1.30	0.641	No
101	10.10	0.59	0.07	0.52	0.98	0.530	1.04	0.508	1.06	1.30	0.647	No
102	10.20	0.59	0.07	0.53	0.98	0.532	1.04	0.510	1.06	1.30	0.650	No
103	10.30	0.60	0.07	0.53	0.98	0.534	1.04	0.512	1.06	1.30	0.653	No
104	10.40	0.60	0.07	0.53	0.98	0.537	1.04	0.514	1.06	1.30	0.656	No
105	10.50	0.61	0.08	0.53	0.98	0.539	1.04	0.517	1.06	1.30	0.659	No
106	10.60	0.62	0.08	0.53	0.98	0.541	1.04	0.519	1.06	1.30	0.662	No
107	10.70	0.62	0.08	0.54	0.98	0.544	1.04	0.521	1.05	1.30	0.665	No
108	10.80	0.63	0.09	0.54	0.98	0.546	1.04	0.523	1.05	1.30	0.668	No
109	10.90	0.63	0.09	0.54	0.98	0.548	1.04	0.525	1.05	1.30	0.671	No
110	11.00	0.64	0.09	0.54	0.98	0.550	1.04	0.527	1.05	1.30	0.674	No
111	11.10	0.64	0.10	0.54	0.98	0.552	1.04	0.529	1.05	1.30	0.677	No
112	11.20	0.65	0.10	0.55	0.97	0.555	1.04	0.532	1.05	1.30	0.679	No
113	11.30	0.65	0.10	0.55	0.97	0.557	1.04	0.534	1.05	1.30	0.682	No
114	11.40	0.66	0.11	0.55	0.97	0.559	1.04	0.536	1.06	1.30	0.682	No
115	11.50	0.66	0.11	0.55	0.97	0.561	1.04	0.538	1.06	1.30	0.684	No
116	11.60	0.67	0.11	0.56	0.97	0.563	1.04	0.539	1.06	1.30	0.687	No
117	11.70	0.67	0.12	0.56	0.97	0.565	1.04	0.541	1.05	1.30	0.690	No
118	11.80	0.68	0.12	0.56	0.97	0.567	1.04	0.543	1.05	1.30	0.694	No
119	11.90	0.69	0.12	0.56	0.97	0.569	1.04	0.545	1.05	1.30	0.698	No
120	12.00	0.69	0.12	0.57	0.97	0.571	1.04	0.547	1.05	1.30	0.700	No
121	12.10	0.70	0.13	0.57	0.97	0.573	1.04	0.549	1.05	1.30	0.702	No
122	12.20	0.70	0.13	0.57	0.97	0.575	1.04	0.551	1.05	1.30	0.702	No
123	12.30	0.71	0.13	0.57	0.97	0.576	1.04	0.552	1.05	1.30	0.704	No
124	12.40	0.71	0.14	0.58	0.97	0.578	1.04	0.554	1.05	1.30	0.706	No
125	12.50	0.72	0.14	0.58	0.97	0.580	1.04	0.556	1.05	1.30	0.709	No
126	12.60	0.72	0.14	0.58	0.97	0.582	1.04	0.558	1.05	1.30	0.711	No
127	12.70	0.73	0.15	0.58	0.97	0.584	1.04	0.559	1.05	1.30	0.712	No
128	12.80	0.74	0.15	0.59	0.97	0.585	1.04	0.561	1.05	1.30	0.715	No
129	12.90	0.74	0.15	0.59	0.97	0.587	1.04	0.563	1.05	1.30	0.718	No
130	13.00	0.75	0.16	0.59	0.97	0.589	1.04	0.564	1.05	1.30	0.722	No
131	13.10	0.75	0.16	0.59	0.97	0.591	1.04	0.566	1.05	1.30	0.726	No
132	13.20	0.76	0.16	0.60	0.97	0.592	1.04	0.568	1.05	1.30	0.729	No
133	13.30	0.76	0.17	0.60	0.97	0.594	1.04	0.569	1.05	1.30	0.731	No
134	13.40	0.77	0.17	0.60	0.97	0.596	1.04	0.571	1.05	1.30	0.733	No
135	13.50	0.77	0.17	0.60	0.97	0.597	1.04	0.573	1.05	1.30	0.734	No
136	13.60	0.78	0.17	0.61	0.97	0.599	1.04	0.574	1.05	1.30	0.736	No
137	13.70	0.79	0.18	0.61	0.97	0.601	1.04	0.576	1.05	1.30	0.738	No
138	13.80	0.79	0.18	0.61	0.97	0.602	1.04	0.577	1.05	1.30	0.741	No
139	13.90	0.80	0.18	0.61	0.97	0.604	1.04	0.579	1.05	1.30	0.743	No
140	14.00	0.80	0.19	0.62	0.97	0.605	1.04	0.580	1.05	1.30	0.746	No
141	14.10	0.81	0.19	0.62	0.96	0.607	1.04	0.582	1.05	1.30	0.748	No
142	14.20	0.81	0.19	0.62	0.96	0.609	1.04	0.583	1.05	1.30	0.750	No
143	14.30	0.82	0.20	0.62	0.96	0.610	1.04	0.585	1.05	1.30	0.753	No
144	14.40	0.82	0.20	0.62	0.96	0.612	1.04	0.586	1.05	1.30	0.754	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
145	14.50	0.83	0.20	0.63	0.96	0.613	1.04	0.588	1.05	1.30	0.756	No
146	14.60	0.84	0.21	0.63	0.96	0.615	1.04	0.589	1.05	1.30	0.757	No
147	14.70	0.84	0.21	0.63	0.96	0.616	1.04	0.590	1.05	1.30	0.759	No
148	14.80	0.85	0.21	0.63	0.96	0.617	1.04	0.592	1.05	1.30	0.760	No
149	14.90	0.85	0.22	0.64	0.96	0.619	1.04	0.593	1.05	1.30	0.763	No
150	15.00	0.86	0.22	0.64	0.96	0.620	1.04	0.595	1.04	1.30	0.765	No
151	15.10	0.86	0.22	0.64	0.96	0.622	1.04	0.596	1.04	1.30	0.768	No
152	15.20	0.87	0.22	0.65	0.96	0.623	1.04	0.597	1.04	1.30	0.770	No
153	15.30	0.88	0.23	0.65	0.96	0.624	1.04	0.598	1.04	1.30	0.771	No
154	15.40	0.88	0.23	0.65	0.96	0.626	1.04	0.600	1.04	1.30	0.772	No
155	15.50	0.89	0.23	0.65	0.96	0.627	1.04	0.601	1.04	1.30	0.774	No
156	15.60	0.89	0.24	0.66	0.96	0.628	1.04	0.602	1.04	1.30	0.777	No
157	15.70	0.90	0.24	0.66	0.96	0.630	1.04	0.603	1.04	1.30	0.778	No
158	15.80	0.90	0.24	0.66	0.96	0.631	1.04	0.605	1.04	1.30	0.779	No
159	15.90	0.91	0.25	0.66	0.96	0.632	1.04	0.606	1.04	1.30	0.781	No
160	16.00	0.92	0.25	0.67	0.96	0.633	1.04	0.607	1.04	1.30	0.784	No
161	16.10	0.92	0.25	0.67	0.96	0.634	1.04	0.608	1.04	1.30	0.785	No
162	16.20	0.93	0.26	0.67	0.96	0.636	1.04	0.609	1.04	1.30	0.784	No
163	16.30	0.93	0.26	0.67	0.96	0.637	1.04	0.610	1.05	1.30	0.782	No
164	16.40	0.94	0.26	0.68	0.96	0.638	1.04	0.611	1.05	1.30	0.784	No
165	16.50	0.95	0.27	0.68	0.96	0.639	1.04	0.612	1.04	1.30	0.787	No
166	16.60	0.95	0.27	0.68	0.96	0.640	1.04	0.614	1.04	1.30	0.792	No
167	16.70	0.96	0.27	0.69	0.96	0.641	1.04	0.615	1.04	1.30	0.797	No
168	16.80	0.96	0.27	0.69	0.95	0.643	1.04	0.616	1.04	1.30	0.801	No
169	16.90	0.97	0.28	0.69	0.95	0.644	1.04	0.617	1.03	1.30	0.803	No
170	17.00	0.97	0.28	0.69	0.95	0.645	1.04	0.618	1.03	1.30	0.805	No
171	17.10	0.98	0.28	0.69	0.95	0.646	1.04	0.619	1.03	1.30	0.807	No
172	17.20	0.98	0.29	0.70	0.95	0.648	1.04	0.621	1.03	1.30	0.809	No
173	17.30	0.99	0.29	0.70	0.95	0.649	1.04	0.622	1.03	1.30	0.811	No
174	17.40	0.99	0.29	0.70	0.95	0.650	1.04	0.623	1.03	1.30	0.813	No
175	17.50	1.00	0.30	0.70	0.95	0.651	1.04	0.624	1.03	1.30	0.814	No
176	17.60	1.00	0.30	0.70	0.95	0.653	1.04	0.626	1.03	1.30	0.815	No
177	17.70	1.01	0.30	0.71	0.95	0.654	1.04	0.627	1.03	1.30	0.816	No
178	17.80	1.01	0.31	0.71	0.95	0.655	1.04	0.628	1.03	1.30	0.818	No
179	17.90	1.02	0.31	0.71	0.95	0.656	1.04	0.629	1.03	1.30	0.820	No
180	18.00	1.02	0.31	0.71	0.95	0.657	1.04	0.630	1.03	1.30	0.821	No
181	18.10	1.03	0.32	0.71	0.95	0.658	1.04	0.631	1.03	1.30	0.823	No
182	18.20	1.04	0.32	0.72	0.95	0.659	1.04	0.632	1.03	1.30	0.825	No
183	18.30	1.04	0.32	0.72	0.95	0.660	1.04	0.633	1.03	1.30	0.826	No
184	18.40	1.05	0.32	0.72	0.95	0.661	1.04	0.634	1.03	1.30	0.826	No
185	18.50	1.05	0.33	0.72	0.95	0.662	1.04	0.635	1.03	1.30	0.826	No
186	18.60	1.06	0.33	0.73	0.95	0.663	1.04	0.636	1.03	1.30	0.827	No
187	18.70	1.06	0.33	0.73	0.95	0.664	1.04	0.637	1.03	1.30	0.829	No
188	18.80	1.07	0.34	0.73	0.95	0.665	1.04	0.637	1.03	1.30	0.829	No
189	18.90	1.07	0.34	0.73	0.95	0.666	1.04	0.638	1.03	1.30	0.830	No
190	19.00	1.08	0.34	0.74	0.95	0.667	1.04	0.639	1.03	1.30	0.833	No
191	19.10	1.09	0.35	0.74	0.95	0.668	1.04	0.640	1.03	1.30	0.835	No
192	19.20	1.09	0.35	0.74	0.95	0.669	1.04	0.641	1.03	1.30	0.838	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
193	19.30	1.10	0.35	0.74	0.94	0.670	1.04	0.642	1.03	1.30	0.839	No
194	19.40	1.10	0.36	0.75	0.94	0.670	1.04	0.643	1.03	1.30	0.840	No
195	19.50	1.11	0.36	0.75	0.94	0.671	1.04	0.643	1.03	1.30	0.840	No
196	19.60	1.11	0.36	0.75	0.94	0.672	1.04	0.644	1.03	1.30	0.841	No
197	19.70	1.12	0.37	0.76	0.94	0.673	1.04	0.645	1.03	1.30	0.841	No
198	19.80	1.13	0.37	0.76	0.94	0.674	1.04	0.646	1.03	1.30	0.842	No
199	19.90	1.13	0.37	0.76	0.94	0.675	1.04	0.647	1.03	1.30	0.842	No
200	20.00	1.14	0.37	0.76	0.94	0.675	1.04	0.647	1.03	1.30	0.845	No
201	20.10	1.14	0.38	0.77	0.94	0.676	1.04	0.648	1.03	1.30	0.848	No
202	20.20	1.15	0.38	0.77	0.94	0.677	1.04	0.649	1.03	1.30	0.850	No
203	20.30	1.15	0.38	0.77	0.94	0.678	1.04	0.650	1.03	1.30	0.851	No
204	20.40	1.16	0.39	0.77	0.94	0.679	1.04	0.651	1.03	1.30	0.852	No
205	20.50	1.17	0.39	0.78	0.94	0.680	1.04	0.651	1.03	1.30	0.853	No
206	20.60	1.17	0.39	0.78	0.94	0.680	1.04	0.652	1.03	1.30	0.854	No
207	20.70	1.18	0.40	0.78	0.94	0.681	1.04	0.653	1.03	1.30	0.855	No
208	20.80	1.18	0.40	0.78	0.94	0.682	1.04	0.654	1.03	1.30	0.856	No
209	20.90	1.19	0.40	0.79	0.94	0.683	1.04	0.654	1.03	1.30	2.000	Yes
210	21.00	1.19	0.41	0.79	0.94	0.683	1.04	0.655	1.03	1.30	2.000	Yes
211	21.10	1.20	0.41	0.79	0.94	0.684	1.04	0.655	1.03	1.30	2.000	Yes
212	21.20	1.21	0.41	0.79	0.94	0.684	1.04	0.656	1.03	1.30	2.000	Yes
213	21.30	1.21	0.41	0.80	0.94	0.685	1.04	0.656	1.03	1.30	2.000	Yes
214	21.40	1.22	0.42	0.80	0.94	0.686	1.04	0.657	1.03	1.30	2.000	Yes
215	21.50	1.22	0.42	0.80	0.94	0.686	1.04	0.658	1.03	1.30	2.000	Yes
216	21.60	1.23	0.42	0.81	0.94	0.687	1.04	0.658	1.03	1.30	0.850	No
217	21.70	1.24	0.43	0.81	0.93	0.687	1.04	0.659	1.03	1.30	0.853	No
218	21.80	1.24	0.43	0.81	0.93	0.688	1.04	0.659	1.03	1.30	0.855	No
219	21.90	1.25	0.43	0.82	0.93	0.688	1.04	0.660	1.03	1.30	2.000	Yes
220	22.00	1.26	0.44	0.82	0.93	0.689	1.04	0.660	1.03	1.30	2.000	Yes
221	22.10	1.26	0.44	0.82	0.93	0.689	1.04	0.661	1.04	1.30	2.000	Yes
222	22.20	1.27	0.44	0.82	0.93	0.690	1.04	0.661	1.04	1.30	2.000	Yes
223	22.30	1.27	0.45	0.83	0.93	0.690	1.04	0.662	1.04	1.30	2.000	Yes
224	22.40	1.28	0.45	0.83	0.93	0.691	1.04	0.662	1.04	1.30	2.000	Yes
225	22.50	1.29	0.45	0.83	0.93	0.691	1.04	0.662	1.04	1.30	0.825	No
226	22.60	1.29	0.46	0.84	0.93	0.691	1.04	0.663	1.05	1.30	0.813	No
227	22.70	1.30	0.46	0.84	0.93	0.692	1.04	0.663	1.05	1.30	0.811	No
228	22.80	1.31	0.46	0.84	0.93	0.692	1.04	0.663	1.05	1.30	0.812	No
229	22.90	1.31	0.46	0.85	0.93	0.693	1.04	0.664	1.05	1.30	0.807	No
230	23.00	1.32	0.47	0.85	0.93	0.693	1.04	0.664	1.06	1.30	0.801	No
231	23.10	1.33	0.47	0.85	0.93	0.693	1.04	0.664	1.06	1.30	0.797	No
232	23.20	1.33	0.47	0.86	0.93	0.694	1.04	0.665	1.06	1.30	0.797	No
233	23.30	1.34	0.48	0.86	0.93	0.694	1.04	0.665	1.06	1.30	0.798	No
234	23.40	1.35	0.48	0.86	0.93	0.694	1.04	0.665	1.06	1.30	0.799	No
235	23.50	1.35	0.48	0.87	0.93	0.694	1.04	0.666	1.06	1.30	0.800	No
236	23.60	1.36	0.49	0.87	0.93	0.695	1.04	0.666	1.06	1.30	0.802	No
237	23.70	1.37	0.49	0.88	0.93	0.695	1.04	0.666	1.06	1.30	0.803	No
238	23.80	1.37	0.49	0.88	0.93	0.695	1.04	0.666	1.06	1.30	0.804	No
239	23.90	1.38	0.50	0.88	0.93	0.695	1.04	0.667	1.05	1.30	0.805	No
240	24.00	1.39	0.50	0.89	0.93	0.696	1.04	0.667	1.05	1.30	0.806	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
241	24.10	1.39	0.50	0.89	0.92	0.696	1.04	0.667	1.04	1.30	0.816	No
242	24.20	1.40	0.51	0.89	0.92	0.696	1.04	0.667	1.04	1.30	0.825	No
243	24.30	1.40	0.51	0.90	0.92	0.697	1.04	0.668	1.04	1.30	0.820	No
244	24.40	1.41	0.51	0.90	0.92	0.697	1.04	0.668	1.04	1.30	0.820	No
245	24.50	1.42	0.51	0.90	0.92	0.697	1.04	0.668	1.03	1.30	2.000	Yes
246	24.60	1.42	0.52	0.91	0.92	0.697	1.04	0.668	1.03	1.30	2.000	Yes
247	24.70	1.43	0.52	0.91	0.92	0.698	1.04	0.669	1.03	1.30	2.000	Yes
248	24.80	1.44	0.52	0.91	0.92	0.698	1.04	0.669	1.02	1.30	2.000	Yes
249	24.90	1.44	0.53	0.92	0.92	0.698	1.04	0.669	1.02	1.30	2.000	Yes
250	25.00	1.45	0.53	0.92	0.92	0.699	1.04	0.670	1.02	1.30	2.000	Yes
251	25.10	1.46	0.53	0.92	0.92	0.699	1.04	0.670	1.02	1.30	2.000	Yes
252	25.20	1.46	0.54	0.93	0.92	0.699	1.04	0.670	1.02	1.30	2.000	Yes
253	25.30	1.47	0.54	0.93	0.92	0.699	1.04	0.670	1.01	1.30	2.000	Yes
254	25.40	1.47	0.54	0.93	0.92	0.700	1.04	0.671	1.01	1.30	2.000	Yes
255	25.50	1.48	0.55	0.93	0.92	0.700	1.04	0.671	1.01	1.30	2.000	Yes
256	25.60	1.49	0.55	0.94	0.92	0.700	1.04	0.671	1.02	1.30	2.000	Yes
257	25.70	1.49	0.55	0.94	0.92	0.701	1.04	0.671	1.02	1.30	2.000	Yes
258	25.80	1.50	0.56	0.94	0.92	0.701	1.04	0.672	1.02	1.30	2.000	Yes
259	25.90	1.51	0.56	0.95	0.92	0.701	1.04	0.672	1.02	1.30	2.000	Yes
260	26.00	1.51	0.56	0.95	0.92	0.701	1.04	0.672	1.02	1.30	0.866	No
261	26.10	1.52	0.56	0.95	0.92	0.701	1.04	0.672	1.02	1.30	0.866	No
262	26.20	1.52	0.57	0.96	0.92	0.702	1.04	0.673	1.02	1.30	0.868	No
263	26.30	1.53	0.57	0.96	0.92	0.702	1.04	0.673	1.02	1.30	0.865	No
264	26.40	1.54	0.57	0.96	0.91	0.702	1.04	0.673	1.02	1.30	0.862	No
265	26.50	1.54	0.58	0.97	0.91	0.702	1.04	0.673	1.02	1.30	0.865	No
266	26.60	1.55	0.58	0.97	0.91	0.703	1.04	0.673	1.01	1.30	0.866	No
267	26.70	1.56	0.58	0.97	0.91	0.703	1.04	0.674	1.01	1.30	0.866	No
268	26.80	1.56	0.59	0.98	0.91	0.703	1.04	0.674	1.01	1.30	0.866	No
269	26.90	1.57	0.59	0.98	0.91	0.703	1.04	0.674	1.01	1.30	0.866	No
270	27.00	1.58	0.59	0.98	0.91	0.703	1.04	0.674	1.01	1.30	0.865	No
271	27.10	1.58	0.60	0.99	0.91	0.703	1.04	0.674	1.01	1.30	0.864	No
272	27.20	1.59	0.60	0.99	0.91	0.704	1.04	0.674	1.01	1.30	0.865	No
273	27.30	1.59	0.60	0.99	0.91	0.704	1.04	0.675	1.01	1.30	0.864	No
274	27.40	1.60	0.61	1.00	0.91	0.704	1.04	0.675	1.01	1.30	0.864	No
275	27.50	1.61	0.61	1.00	0.91	0.704	1.04	0.675	1.01	1.30	0.863	No
276	27.60	1.61	0.61	1.00	0.91	0.704	1.04	0.675	1.01	1.30	0.862	No
277	27.70	1.62	0.61	1.01	0.91	0.704	1.04	0.675	1.01	1.30	0.862	No
278	27.80	1.63	0.62	1.01	0.91	0.704	1.04	0.675	1.01	1.30	0.861	No
279	27.90	1.63	0.62	1.01	0.91	0.704	1.04	0.675	1.01	1.30	0.859	No
280	28.00	1.64	0.62	1.02	0.91	0.705	1.04	0.675	1.01	1.30	0.859	No
281	28.10	1.65	0.63	1.02	0.91	0.705	1.04	0.675	1.01	1.30	0.865	No
282	28.20	1.65	0.63	1.02	0.91	0.705	1.04	0.676	1.01	1.30	0.871	No
283	28.30	1.66	0.63	1.03	0.91	0.705	1.04	0.676	1.01	1.30	0.878	No
284	28.40	1.67	0.64	1.03	0.91	0.705	1.04	0.676	1.00	1.30	0.881	No
285	28.50	1.67	0.64	1.03	0.91	0.705	1.04	0.676	1.00	1.30	0.884	No
286	28.60	1.68	0.64	1.04	0.90	0.705	1.04	0.676	1.00	1.30	2.000	Yes
287	28.70	1.68	0.65	1.04	0.90	0.705	1.04	0.676	1.00	1.30	2.000	Yes
288	28.80	1.69	0.65	1.04	0.90	0.706	1.04	0.676	1.00	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
289	28.90	1.70	0.65	1.04	0.90	0.706	1.04	0.676	1.00	1.30	2.000	Yes
290	29.00	1.70	0.66	1.05	0.90	0.706	1.04	0.676	1.00	1.30	2.000	Yes
291	29.10	1.71	0.66	1.05	0.90	0.706	1.04	0.677	1.00	1.30	2.000	Yes
292	29.20	1.72	0.66	1.05	0.90	0.706	1.04	0.677	1.00	1.30	2.000	Yes
293	29.30	1.72	0.66	1.06	0.90	0.706	1.04	0.677	1.00	1.30	2.000	Yes
294	29.40	1.73	0.67	1.06	0.90	0.706	1.04	0.677	1.00	1.30	2.000	Yes
295	29.50	1.73	0.67	1.06	0.90	0.707	1.04	0.677	1.00	1.30	0.907	No
296	29.60	1.74	0.67	1.07	0.90	0.707	1.04	0.677	1.00	1.30	0.908	No
297	29.70	1.75	0.68	1.07	0.90	0.707	1.04	0.677	1.00	1.30	0.909	No
298	29.80	1.75	0.68	1.07	0.90	0.707	1.04	0.678	1.00	1.30	0.910	No
299	29.90	1.76	0.68	1.08	0.90	0.707	1.04	0.678	1.00	1.30	0.911	No
300	30.00	1.76	0.69	1.08	0.90	0.707	1.04	0.678	1.00	1.30	0.911	No
301	30.10	1.77	0.69	1.08	0.90	0.707	1.04	0.678	1.00	1.30	0.908	No
302	30.20	1.78	0.69	1.08	0.90	0.707	1.04	0.678	1.00	1.30	0.908	No
303	30.30	1.78	0.70	1.09	0.90	0.707	1.04	0.678	1.00	1.30	0.908	No
304	30.40	1.79	0.70	1.09	0.90	0.707	1.04	0.678	1.00	1.30	0.908	No
305	30.50	1.80	0.70	1.09	0.90	0.708	1.04	0.678	1.00	1.30	2.000	Yes
306	30.60	1.80	0.71	1.10	0.90	0.708	1.04	0.678	1.00	1.30	2.000	Yes
307	30.70	1.81	0.71	1.10	0.90	0.708	1.04	0.678	0.99	1.30	2.000	Yes
308	30.80	1.82	0.71	1.10	0.89	0.708	1.04	0.678	0.99	1.30	2.000	Yes
309	30.90	1.82	0.71	1.11	0.89	0.708	1.04	0.678	0.99	1.30	2.000	Yes
310	31.00	1.83	0.72	1.11	0.89	0.708	1.04	0.678	0.99	1.30	2.000	Yes
311	31.10	1.83	0.72	1.11	0.89	0.708	1.04	0.678	0.99	1.30	2.000	Yes
312	31.20	1.84	0.72	1.12	0.89	0.708	1.04	0.678	0.99	1.30	2.000	Yes
313	31.30	1.85	0.73	1.12	0.89	0.708	1.04	0.678	0.99	1.30	0.878	No
314	31.40	1.85	0.73	1.12	0.89	0.708	1.04	0.678	0.99	1.30	0.876	No
315	31.50	1.86	0.73	1.13	0.89	0.708	1.04	0.678	0.98	1.30	0.877	No
316	31.60	1.87	0.74	1.13	0.89	0.708	1.04	0.678	0.98	1.30	0.878	No
317	31.70	1.87	0.74	1.13	0.89	0.708	1.04	0.678	0.98	1.30	0.878	No
318	31.80	1.88	0.74	1.14	0.89	0.707	1.04	0.678	0.98	1.30	0.880	No
319	31.90	1.89	0.75	1.14	0.89	0.707	1.04	0.678	0.99	1.30	0.889	No
320	32.00	1.89	0.75	1.14	0.89	0.707	1.04	0.678	0.99	1.30	0.897	No
321	32.10	1.90	0.75	1.15	0.89	0.707	1.04	0.678	0.99	1.30	0.903	No
322	32.20	1.91	0.76	1.15	0.89	0.707	1.04	0.678	0.99	1.30	0.906	No
323	32.30	1.91	0.76	1.15	0.89	0.707	1.04	0.678	0.99	1.30	0.905	No
324	32.40	1.92	0.76	1.16	0.89	0.707	1.04	0.678	0.99	1.30	0.904	No
325	32.50	1.92	0.76	1.16	0.89	0.707	1.04	0.678	0.99	1.30	0.902	No
326	32.60	1.93	0.77	1.16	0.89	0.707	1.04	0.678	0.98	1.30	0.897	No
327	32.70	1.94	0.77	1.17	0.89	0.707	1.04	0.678	0.98	1.30	0.892	No
328	32.80	1.94	0.77	1.17	0.89	0.707	1.04	0.678	0.98	1.30	0.887	No
329	32.90	1.95	0.78	1.17	0.88	0.707	1.04	0.678	0.98	1.30	0.885	No
330	33.00	1.96	0.78	1.18	0.88	0.707	1.04	0.678	0.98	1.30	0.886	No
331	33.10	1.96	0.78	1.18	0.88	0.707	1.04	0.678	0.98	1.30	0.888	No
332	33.20	1.97	0.79	1.18	0.88	0.707	1.04	0.678	0.98	1.30	0.893	No
333	33.30	1.98	0.79	1.19	0.88	0.707	1.04	0.678	0.98	1.30	0.899	No
334	33.40	1.98	0.79	1.19	0.88	0.707	1.04	0.678	0.98	1.30	0.900	No
335	33.50	1.99	0.80	1.19	0.88	0.707	1.04	0.678	0.98	1.30	0.901	No
336	33.60	2.00	0.80	1.20	0.88	0.707	1.04	0.678	0.98	1.30	0.900	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
337	33.70	2.00	0.80	1.20	0.88	0.707	1.04	0.677	0.98	1.30	0.898	No
338	33.80	2.01	0.80	1.20	0.88	0.707	1.04	0.677	0.97	1.30	0.893	No
339	33.90	2.02	0.81	1.21	0.88	0.707	1.04	0.677	0.97	1.30	0.891	No
340	34.00	2.02	0.81	1.21	0.88	0.707	1.04	0.677	0.97	1.30	0.894	No
341	34.10	2.03	0.81	1.21	0.88	0.706	1.04	0.677	0.96	1.30	0.895	No
342	34.20	2.03	0.82	1.22	0.88	0.706	1.04	0.677	0.96	1.30	0.895	No
343	34.30	2.04	0.82	1.22	0.88	0.706	1.04	0.677	0.96	1.30	0.894	No
344	34.40	2.05	0.82	1.22	0.88	0.706	1.04	0.677	0.96	1.30	0.896	No
345	34.50	2.05	0.83	1.23	0.88	0.706	1.04	0.677	0.96	1.30	0.902	No
346	34.60	2.06	0.83	1.23	0.88	0.706	1.04	0.677	0.95	1.30	0.903	No
347	34.70	2.07	0.83	1.23	0.88	0.706	1.04	0.677	0.95	1.30	0.904	No
348	34.80	2.07	0.84	1.24	0.88	0.706	1.04	0.676	0.95	1.30	0.904	No
349	34.90	2.08	0.84	1.24	0.88	0.706	1.04	0.676	0.95	1.30	0.905	No
350	35.00	2.09	0.84	1.25	0.87	0.705	1.04	0.676	0.95	1.30	0.905	No
351	35.10	2.09	0.85	1.25	0.87	0.705	1.04	0.676	0.95	1.30	0.906	No
352	35.20	2.10	0.85	1.25	0.87	0.705	1.04	0.676	0.95	1.30	0.907	No
353	35.30	2.11	0.85	1.26	0.87	0.705	1.04	0.676	0.95	1.30	0.907	No
354	35.40	2.11	0.85	1.26	0.87	0.705	1.04	0.676	0.95	1.30	0.908	No
355	35.50	2.12	0.86	1.26	0.87	0.705	1.04	0.675	0.95	1.30	0.907	No
356	35.60	2.13	0.86	1.27	0.87	0.705	1.04	0.675	0.95	1.30	0.903	No
357	35.70	2.13	0.86	1.27	0.87	0.705	1.04	0.675	0.96	1.30	0.899	No
358	35.80	2.14	0.87	1.27	0.87	0.704	1.04	0.675	0.96	1.30	0.899	No
359	35.90	2.15	0.87	1.28	0.87	0.704	1.04	0.675	0.96	1.30	0.903	No
360	36.00	2.15	0.87	1.28	0.87	0.704	1.04	0.675	0.97	1.30	0.908	No
361	36.10	2.16	0.88	1.28	0.87	0.704	1.04	0.675	0.97	1.30	0.912	No
362	36.20	2.17	0.88	1.29	0.87	0.704	1.04	0.675	0.97	1.30	0.914	No
363	36.30	2.17	0.88	1.29	0.87	0.704	1.04	0.675	0.97	1.30	0.914	No
364	36.40	2.18	0.89	1.29	0.87	0.704	1.04	0.675	0.97	1.30	0.914	No
365	36.50	2.18	0.89	1.30	0.87	0.704	1.04	0.675	0.97	1.30	0.913	No
366	36.60	2.19	0.89	1.30	0.87	0.704	1.04	0.674	0.97	1.30	0.912	No
367	36.70	2.20	0.90	1.30	0.87	0.704	1.04	0.674	0.97	1.30	0.912	No
368	36.80	2.20	0.90	1.31	0.87	0.704	1.04	0.674	0.96	1.30	0.911	No
369	36.90	2.21	0.90	1.31	0.87	0.703	1.04	0.674	0.96	1.30	0.910	No
370	37.00	2.22	0.90	1.31	0.87	0.703	1.04	0.674	0.96	1.30	0.909	No
371	37.10	2.22	0.91	1.31	0.86	0.703	1.04	0.674	0.96	1.30	0.909	No
372	37.20	2.23	0.91	1.32	0.86	0.703	1.04	0.674	0.96	1.30	0.909	No
373	37.30	2.24	0.91	1.32	0.86	0.703	1.04	0.674	0.96	1.30	0.909	No
374	37.40	2.24	0.92	1.32	0.86	0.703	1.04	0.674	0.96	1.30	0.909	No
375	37.50	2.25	0.92	1.33	0.86	0.703	1.04	0.673	0.96	1.30	0.909	No
376	37.60	2.26	0.92	1.33	0.86	0.702	1.04	0.673	0.96	1.30	0.909	No
377	37.70	2.26	0.93	1.33	0.86	0.702	1.04	0.673	0.95	1.30	0.909	No
378	37.80	2.27	0.93	1.34	0.86	0.702	1.04	0.673	0.95	1.30	0.909	No
379	37.90	2.27	0.93	1.34	0.86	0.702	1.04	0.673	0.95	1.30	0.909	No
380	38.00	2.28	0.94	1.34	0.86	0.702	1.04	0.673	0.95	1.30	0.908	No
381	38.10	2.29	0.94	1.35	0.86	0.702	1.04	0.673	0.95	1.30	0.908	No
382	38.20	2.29	0.94	1.35	0.86	0.702	1.04	0.672	0.95	1.30	0.908	No
383	38.30	2.30	0.95	1.35	0.86	0.701	1.04	0.672	0.95	1.30	0.907	No
384	38.40	2.31	0.95	1.36	0.86	0.701	1.04	0.672	0.94	1.30	0.907	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
385	38.50	2.31	0.95	1.36	0.86	0.701	1.04	0.672	0.94	1.30	0.908	No
386	38.60	2.32	0.95	1.36	0.86	0.701	1.04	0.672	0.94	1.30	0.909	No
387	38.70	2.33	0.96	1.37	0.86	0.701	1.04	0.672	0.94	1.30	0.909	No
388	38.80	2.33	0.96	1.37	0.86	0.701	1.04	0.672	0.94	1.30	0.910	No
389	38.90	2.34	0.96	1.37	0.86	0.700	1.04	0.671	0.94	1.30	0.910	No
390	39.00	2.35	0.97	1.38	0.86	0.700	1.04	0.671	0.95	1.30	0.911	No
391	39.10	2.35	0.97	1.38	0.86	0.700	1.04	0.671	0.94	1.30	0.911	No
392	39.20	2.36	0.97	1.38	0.85	0.700	1.04	0.671	0.94	1.30	0.912	No
393	39.30	2.36	0.98	1.39	0.85	0.700	1.04	0.671	0.94	1.30	0.912	No
394	39.40	2.37	0.98	1.39	0.85	0.700	1.04	0.671	0.94	1.30	0.912	No
395	39.50	2.38	0.98	1.39	0.85	0.699	1.04	0.670	0.94	1.30	0.913	No
396	39.60	2.38	0.99	1.40	0.85	0.699	1.04	0.670	0.94	1.30	0.913	No
397	39.70	2.39	0.99	1.40	0.85	0.699	1.04	0.670	0.94	1.30	0.914	No
398	39.80	2.40	0.99	1.40	0.85	0.699	1.04	0.670	0.94	1.30	0.914	No
399	39.90	2.40	1.00	1.41	0.85	0.699	1.04	0.670	0.94	1.30	0.913	No
400	40.00	2.41	1.00	1.41	0.85	0.699	1.04	0.670	0.94	1.30	0.913	No
401	40.10	2.42	1.00	1.41	0.85	0.698	1.04	0.669	0.94	1.30	0.914	No
402	40.20	2.42	1.00	1.42	0.85	0.698	1.04	0.669	0.94	1.30	0.913	No
403	40.30	2.43	1.01	1.42	0.85	0.698	1.04	0.669	0.93	1.30	0.913	No
404	40.40	2.44	1.01	1.42	0.85	0.698	1.04	0.669	0.93	1.30	0.915	No
405	40.50	2.44	1.01	1.43	0.85	0.698	1.04	0.669	0.93	1.30	0.916	No
406	40.60	2.45	1.02	1.43	0.85	0.697	1.04	0.669	0.93	1.30	0.916	No
407	40.70	2.46	1.02	1.44	0.85	0.697	1.04	0.668	0.93	1.30	0.915	No
408	40.80	2.46	1.02	1.44	0.85	0.697	1.04	0.668	0.93	1.30	0.915	No
409	40.90	2.47	1.03	1.44	0.85	0.697	1.04	0.668	0.93	1.30	0.916	No
410	41.00	2.47	1.03	1.45	0.85	0.697	1.04	0.668	0.93	1.30	0.917	No
411	41.10	2.48	1.03	1.45	0.85	0.696	1.04	0.668	0.92	1.30	0.920	No
412	41.20	2.49	1.04	1.45	0.84	0.696	1.04	0.667	0.92	1.30	0.924	No
413	41.30	2.49	1.04	1.46	0.84	0.696	1.04	0.667	0.92	1.30	0.927	No
414	41.40	2.50	1.04	1.46	0.84	0.696	1.04	0.667	0.91	1.30	0.929	No
415	41.50	2.51	1.05	1.46	0.84	0.696	1.04	0.667	0.91	1.30	0.928	No
416	41.60	2.51	1.05	1.47	0.84	0.695	1.04	0.667	0.92	1.30	0.926	No
417	41.70	2.52	1.05	1.47	0.84	0.695	1.04	0.666	0.92	1.30	0.925	No
418	41.80	2.53	1.05	1.47	0.84	0.695	1.04	0.666	0.92	1.30	0.927	No
419	41.90	2.53	1.06	1.48	0.84	0.695	1.04	0.666	0.91	1.30	0.933	No
420	42.00	2.54	1.06	1.48	0.84	0.695	1.04	0.666	0.90	1.30	0.941	No
421	42.10	2.55	1.06	1.48	0.84	0.694	1.04	0.665	0.90	1.30	0.943	No
422	42.20	2.55	1.07	1.49	0.84	0.694	1.04	0.665	0.90	1.30	0.944	No
423	42.30	2.56	1.07	1.49	0.84	0.694	1.04	0.665	0.90	1.30	0.944	No
424	42.40	2.57	1.07	1.49	0.84	0.694	1.04	0.665	0.90	1.30	0.944	No
425	42.50	2.57	1.08	1.50	0.84	0.693	1.04	0.665	0.90	1.30	0.945	No
426	42.60	2.58	1.08	1.50	0.84	0.693	1.04	0.664	0.90	1.30	0.945	No
427	42.70	2.59	1.08	1.50	0.84	0.693	1.04	0.664	0.89	1.30	0.946	No
428	42.80	2.59	1.09	1.51	0.84	0.693	1.04	0.664	0.89	1.30	0.946	No
429	42.90	2.60	1.09	1.51	0.84	0.692	1.04	0.664	0.89	1.30	0.945	No
430	43.00	2.61	1.09	1.51	0.84	0.692	1.04	0.663	0.90	1.30	0.943	No
431	43.10	2.61	1.10	1.52	0.84	0.692	1.04	0.663	0.89	1.30	0.945	No
432	43.20	2.62	1.10	1.52	0.84	0.692	1.04	0.663	0.89	1.30	0.948	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
433	43.30	2.63	1.10	1.53	0.83	0.691	1.04	0.663	0.89	1.30	0.948	No
434	43.40	2.63	1.10	1.53	0.83	0.691	1.04	0.662	0.89	1.30	0.948	No
435	43.50	2.64	1.11	1.53	0.83	0.691	1.04	0.662	0.89	1.30	0.949	No
436	43.60	2.65	1.11	1.54	0.83	0.691	1.04	0.662	0.89	1.30	0.949	No
437	43.70	2.65	1.11	1.54	0.83	0.690	1.04	0.662	0.89	1.30	0.950	No
438	43.80	2.66	1.12	1.54	0.83	0.690	1.04	0.661	0.89	1.30	0.950	No
439	43.90	2.67	1.12	1.55	0.83	0.690	1.04	0.661	0.89	1.30	0.950	No
440	44.00	2.67	1.12	1.55	0.83	0.689	1.04	0.661	0.89	1.30	0.951	No
441	44.10	2.68	1.13	1.55	0.83	0.689	1.04	0.661	0.88	1.30	0.951	No
442	44.20	2.69	1.13	1.56	0.83	0.689	1.04	0.660	0.88	1.30	0.951	No
443	44.30	2.69	1.13	1.56	0.83	0.689	1.04	0.660	0.88	1.30	0.952	No
444	44.40	2.70	1.14	1.56	0.83	0.688	1.04	0.660	0.88	1.30	0.952	No
445	44.50	2.71	1.14	1.57	0.83	0.688	1.04	0.660	0.88	1.30	0.952	No
446	44.60	2.71	1.14	1.57	0.83	0.688	1.04	0.659	0.88	1.30	0.953	No
447	44.70	2.72	1.15	1.57	0.83	0.688	1.04	0.659	0.88	1.30	0.953	No
448	44.80	2.73	1.15	1.58	0.83	0.687	1.04	0.659	0.88	1.30	0.954	No
449	44.90	2.73	1.15	1.58	0.83	0.687	1.04	0.659	0.88	1.30	0.954	No
450	45.00	2.74	1.15	1.59	0.83	0.687	1.04	0.658	0.88	1.30	0.954	No
451	45.10	2.75	1.16	1.59	0.83	0.687	1.04	0.658	0.88	1.30	0.955	No
452	45.20	2.75	1.16	1.59	0.83	0.686	1.04	0.658	0.88	1.30	0.955	No
453	45.30	2.76	1.16	1.60	0.82	0.686	1.04	0.658	0.88	1.30	0.955	No
454	45.40	2.77	1.17	1.60	0.82	0.686	1.04	0.657	0.88	1.30	0.956	No
455	45.50	2.77	1.17	1.60	0.82	0.686	1.04	0.657	0.88	1.30	0.956	No
456	45.60	2.78	1.17	1.61	0.82	0.685	1.04	0.657	0.87	1.30	0.956	No
457	45.70	2.79	1.18	1.61	0.82	0.685	1.04	0.657	0.87	1.30	0.957	No
458	45.80	2.79	1.18	1.61	0.82	0.685	1.04	0.656	0.87	1.30	0.957	No
459	45.90	2.80	1.18	1.62	0.82	0.684	1.04	0.656	0.87	1.30	0.957	No
460	46.00	2.81	1.19	1.62	0.82	0.684	1.04	0.656	0.87	1.30	0.958	No
461	46.10	2.81	1.19	1.62	0.82	0.684	1.04	0.655	0.87	1.30	0.958	No
462	46.20	2.82	1.19	1.63	0.82	0.684	1.04	0.655	0.87	1.30	0.958	No
463	46.30	2.83	1.19	1.63	0.82	0.683	1.04	0.655	0.87	1.30	0.959	No
464	46.40	2.83	1.20	1.63	0.82	0.683	1.04	0.655	0.87	1.30	0.959	No
465	46.50	2.84	1.20	1.64	0.82	0.683	1.04	0.654	0.87	1.30	0.957	No
466	46.60	2.85	1.20	1.64	0.82	0.683	1.04	0.654	0.89	1.30	0.938	No
467	46.70	2.85	1.21	1.64	0.82	0.682	1.04	0.654	0.91	1.30	2.000	Yes
468	46.80	2.86	1.21	1.65	0.82	0.682	1.04	0.654	0.92	1.30	2.000	Yes
469	46.90	2.86	1.21	1.65	0.82	0.682	1.04	0.654	0.91	1.30	2.000	Yes
470	47.00	2.87	1.22	1.65	0.82	0.682	1.04	0.653	0.92	1.30	2.000	Yes
471	47.10	2.88	1.22	1.66	0.82	0.681	1.04	0.653	0.93	1.30	2.000	Yes
472	47.20	2.88	1.22	1.66	0.82	0.681	1.04	0.653	0.93	1.30	2.000	Yes
473	47.30	2.89	1.23	1.66	0.82	0.681	1.04	0.653	0.93	1.30	2.000	Yes
474	47.40	2.90	1.23	1.67	0.81	0.681	1.04	0.652	0.92	1.30	2.000	Yes
475	47.50	2.90	1.23	1.67	0.81	0.680	1.04	0.652	0.90	1.30	2.000	Yes
476	47.60	2.91	1.24	1.68	0.81	0.680	1.04	0.652	0.90	1.30	2.000	Yes
477	47.70	2.92	1.24	1.68	0.81	0.680	1.04	0.651	0.90	1.30	0.925	No
478	47.80	2.92	1.24	1.68	0.81	0.679	1.04	0.651	0.91	1.30	0.923	No
479	47.90	2.93	1.24	1.69	0.81	0.679	1.04	0.651	0.92	1.30	0.922	No
480	48.00	2.94	1.25	1.69	0.81	0.679	1.04	0.651	0.92	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
481	48.10	2.94	1.25	1.69	0.81	0.679	1.04	0.650	0.92	1.30	2.000	Yes
482	48.20	2.95	1.25	1.70	0.81	0.678	1.04	0.650	0.92	1.30	2.000	Yes
483	48.30	2.96	1.26	1.70	0.81	0.678	1.04	0.650	0.91	1.30	2.000	Yes
484	48.40	2.96	1.26	1.70	0.81	0.678	1.04	0.650	0.92	1.30	2.000	Yes
485	48.50	2.97	1.26	1.71	0.81	0.678	1.04	0.649	0.92	1.30	2.000	Yes
486	48.60	2.98	1.27	1.71	0.81	0.677	1.04	0.649	0.92	1.30	2.000	Yes
487	48.70	2.98	1.27	1.71	0.81	0.677	1.04	0.649	0.93	1.30	2.000	Yes
488	48.80	2.99	1.27	1.72	0.81	0.677	1.04	0.649	0.93	1.30	2.000	Yes
489	48.90	2.99	1.28	1.72	0.81	0.677	1.04	0.649	0.94	1.30	2.000	Yes
490	49.00	3.00	1.28	1.72	0.81	0.676	1.04	0.648	0.94	1.30	2.000	Yes
491	49.10	3.01	1.28	1.72	0.81	0.676	1.04	0.648	0.95	1.30	2.000	Yes
492	49.20	3.01	1.29	1.73	0.81	0.676	1.04	0.648	0.95	1.30	2.000	Yes
493	49.30	3.02	1.29	1.73	0.81	0.676	1.04	0.648	0.95	1.30	2.000	Yes
494	49.40	3.03	1.29	1.73	0.80	0.676	1.04	0.647	0.95	1.30	2.000	Yes
495	49.50	3.03	1.29	1.74	0.80	0.675	1.04	0.647	0.96	1.30	0.910	No
496	49.60	3.04	1.30	1.74	0.80	0.675	1.04	0.647	0.96	1.30	0.910	No
497	49.70	3.04	1.30	1.74	0.80	0.675	1.04	0.647	0.96	1.30	0.910	No
498	49.80	3.05	1.30	1.75	0.80	0.675	1.04	0.647	0.95	1.30	0.911	No
499	49.90	3.06	1.31	1.75	0.80	0.675	1.04	0.647	0.95	1.30	0.912	No

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
 σ_v : Total overburden pressure at test point (tsf)
 u_0 : Water pressure at test point (tsf)
 σ_v' : Effective overburden pressure based on GWT during earthquake (tsf)
 r_d : Nonlinear shear mass factor
 CSR: Cyclic Stress Ratio
 MSF: Magnitude Scaling Factor
 CSR_{eq} : CSR adjusted for M=7.5
 K_σ : Effective overburden stress factor
 CSR*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1	0.10	63.32	26.73	2.05	0.40	1.70	99.80	50.62	150.42	4.000	No	No	2.00
2	0.20	64.12	25.23	2.03	0.40	1.70	105.51	49.03	154.54	4.000	No	No	2.00
3	0.30	63.59	25.92	2.04	0.40	1.70	103.69	49.94	153.63	4.000	No	No	2.00
4	0.40	60.41	31.49	2.11	0.40	1.70	97.21	56.91	154.12	4.000	No	No	2.00
5	0.50	57.19	37.40	2.18	0.40	1.70	90.18	61.54	151.72	4.000	No	No	2.00
6	0.60	56.53	42.04	2.24	0.40	1.70	88.16	64.69	152.85	4.000	No	No	2.00
7	0.70	59.04	44.71	2.27	0.38	1.70	94.01	67.92	161.93	4.000	No	No	2.00
8	0.80	62.44	45.91	2.29	0.37	1.70	102.26	70.77	173.03	4.000	No	No	2.00
9	0.90	64.67	46.39	2.29	0.36	1.70	104.54	71.66	176.20	4.000	No	No	2.00
10	1.00	65.58	46.66	2.30	0.36	1.70	104.75	71.87	176.62	4.000	No	No	2.00
11	1.10	64.59	47.25	2.30	0.36	1.70	106.62	72.71	179.33	4.000	No	No	2.00
12	1.20	61.76	48.26	2.32	0.37	1.70	99.78	71.51	171.28	4.000	No	No	2.00
13	1.30	57.24	49.52	2.33	0.39	1.70	91.10	69.89	161.00	4.000	No	No	2.00
14	1.40	54.57	49.94	2.34	0.40	1.70	84.88	68.46	153.33	4.000	No	No	2.00
15	1.50	54.99	49.40	2.33	0.39	1.70	86.92	68.73	155.64	4.000	No	No	2.00
16	1.60	57.17	48.67	2.32	0.38	1.70	93.11	69.98	163.08	4.000	No	No	2.00
17	1.70	59.72	48.13	2.31	0.38	1.70	95.41	70.29	165.71	4.000	No	No	2.00
18	1.80	60.59	48.40	2.32	0.37	1.70	99.16	71.42	170.58	4.000	No	No	2.00
19	1.90	57.91	50.16	2.34	0.37	1.70	97.32	71.86	169.18	4.000	Yes	No	2.00
20	2.00	52.69	53.24	2.38	0.40	1.70	82.51	69.32	151.83	4.000	Yes	No	2.00
21	2.10	46.70	57.10	2.43	0.42	1.70	74.01	68.49	142.50	4.000	Yes	No	2.00
22	2.20	42.14	60.26	2.47	0.43	1.70	68.44	67.98	136.42	4.000	Yes	No	2.00
23	2.30	37.73	63.19	2.50	0.44	1.70	60.53	66.59	127.12	4.000	Yes	No	2.00
24	2.40	33.71	65.74	2.53	0.46	1.70	52.79	65.04	117.82	4.000	Yes	No	2.00
25	2.50	31.80	66.65	2.55	0.47	1.70	49.08	64.18	113.26	4.000	No	No	2.00
26	2.60	32.09	65.77	2.53	0.46	1.70	51.31	64.62	115.93	4.000	No	No	2.00
27	2.70	33.43	64.09	2.51	0.46	1.70	54.17	65.02	119.20	4.000	No	No	2.00
28	2.80	34.49	62.43	2.49	0.46	1.70	55.57	64.98	120.56	4.000	No	No	2.00
29	2.90	34.00	61.54	2.48	0.45	1.70	56.39	64.97	121.36	4.000	No	No	2.00
30	3.00	33.22	60.50	2.47	0.47	1.70	51.82	63.39	115.20	4.000	No	No	2.00
31	3.10	32.49	59.63	2.46	0.47	1.70	51.82	63.14	114.95	4.000	No	No	2.00
32	3.20	33.17	58.75	2.45	0.46	1.70	52.87	63.17	116.04	4.000	No	No	2.00
33	3.30	34.74	58.29	2.44	0.46	1.70	55.14	63.65	118.79	4.000	No	No	2.00
34	3.40	37.04	58.02	2.44	0.45	1.70	59.35	64.74	124.09	4.000	No	No	2.00
35	3.50	39.15	58.35	2.44	0.44	1.70	63.98	66.14	130.12	4.000	No	No	2.00
36	3.60	40.29	59.73	2.46	0.43	1.70	65.25	66.93	132.18	4.000	No	No	2.00
37	3.70	40.26	62.22	2.49	0.43	1.70	64.87	67.56	132.43	4.000	No	No	2.00
38	3.80	40.09	64.77	2.52	0.43	1.70	63.82	67.96	131.77	4.000	No	No	2.00
39	3.90	40.64	66.45	2.54	0.43	1.70	64.40	68.55	132.95	4.000	No	No	2.00
40	4.00	42.32	66.67	2.55	0.43	1.70	67.50	69.49	136.99	4.000	No	No	2.00
41	4.10	44.34	65.87	2.54	0.42	1.70	71.92	70.56	142.48	4.000	No	No	2.00
42	4.20	45.37	65.32	2.53	0.41	1.70	74.11	71.05	145.16	4.000	No	No	2.00
43	4.30	44.83	65.88	2.54	0.41	1.70	72.48	70.72	143.20	4.000	No	No	2.00
44	4.40	42.77	67.85	2.56	0.42	1.70	69.33	70.31	139.64	4.000	No	No	2.00
45	4.50	39.56	70.70	2.60	0.43	1.70	64.18	69.47	133.64	4.000	No	No	2.00
46	4.60	35.62	73.80	2.63	0.45	1.70	57.03	0.00	57.03	4.000	No	Yes	2.00
47	4.70	31.43	76.82	2.67	0.46	1.70	50.31	0.00	50.31	4.000	No	Yes	2.00
48	4.80	28.05	79.08	2.70	0.48	1.70	44.02	0.00	44.02	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
49	4.90	25.36	80.68	2.72	0.49	1.70	40.74	0.00	40.74	4.000	No	Yes	2.00
50	5.00	23.37	81.44	2.73	0.50	1.70	37.36	0.00	37.36	4.000	No	Yes	2.00
51	5.10	21.74	81.69	2.73	0.50	1.70	34.47	0.00	34.47	4.000	No	Yes	2.00
52	5.20	20.76	81.40	2.73	0.51	1.70	32.89	0.00	32.89	4.000	No	Yes	2.00
53	5.30	20.78	80.63	2.72	0.51	1.70	32.63	0.00	32.63	4.000	No	Yes	2.00
54	5.40	22.02	78.94	2.70	0.51	1.70	34.56	0.00	34.56	4.000	No	Yes	2.00
55	5.50	24.13	76.26	2.67	0.49	1.70	38.88	0.00	38.88	4.000	No	Yes	2.00
56	5.60	26.02	73.59	2.63	0.48	1.70	42.78	0.00	42.78	4.000	No	Yes	2.00
57	5.70	26.65	72.17	2.61	0.48	1.70	43.69	0.00	43.69	4.000	No	Yes	2.00
58	5.80	25.84	72.75	2.62	0.49	1.70	41.92	0.00	41.92	4.000	No	Yes	2.00
59	5.90	23.01	76.37	2.67	0.49	1.70	38.88	0.00	38.88	4.000	No	Yes	2.00
60	6.00	19.12	82.45	2.74	0.52	1.70	30.04	0.00	30.04	4.000	No	Yes	2.00
61	6.10	16.32	87.78	2.81	0.54	1.70	23.18	0.00	23.18	4.000	No	Yes	2.00
62	6.20	15.54	88.84	2.82	0.53	1.70	25.39	0.00	25.39	4.000	No	Yes	2.00
63	6.30	15.65	87.39	2.80	0.53	1.70	26.28	0.00	26.28	4.000	No	Yes	2.00
64	6.40	14.57	88.14	2.81	0.54	1.70	23.72	0.00	23.72	4.000	No	Yes	2.00
65	6.50	12.62	91.93	2.86	0.55	1.70	20.21	0.00	20.21	4.000	No	Yes	2.00
66	6.60	10.88	97.04	2.93	0.56	1.70	16.86	0.00	16.86	4.000	No	Yes	2.00
67	6.70	9.87	100.00	2.97	0.56	1.70	15.35	0.00	15.35	4.000	No	Yes	2.00
68	6.80	9.47	100.00	3.00	0.56	1.70	15.34	0.00	15.34	4.000	No	Yes	2.00
69	6.90	9.06	100.00	3.02	0.56	1.69	14.82	0.00	14.82	4.000	No	Yes	2.00
70	7.00	8.72	100.00	3.04	0.57	1.69	13.28	0.00	13.28	4.000	No	Yes	2.00
71	7.10	9.04	100.00	3.04	0.57	1.67	13.48	0.00	13.48	4.000	No	Yes	2.00
72	7.20	10.62	100.00	2.99	0.56	1.65	15.93	0.00	15.93	4.000	No	Yes	2.00
73	7.30	13.04	94.80	2.90	0.55	1.62	19.97	0.00	19.97	4.000	No	Yes	2.00
74	7.40	14.73	89.27	2.83	0.54	1.59	23.70	0.00	23.70	4.000	No	Yes	2.00
75	7.50	14.76	87.60	2.81	0.54	1.58	22.92	0.00	22.92	4.000	No	Yes	2.00
76	7.60	13.33	90.31	2.84	0.55	1.59	19.72	0.00	19.72	4.000	No	Yes	2.00
77	7.70	11.94	94.70	2.90	0.56	1.59	17.23	0.00	17.23	4.000	No	Yes	2.00
78	7.80	11.27	97.16	2.93	0.56	1.58	16.61	0.00	16.61	4.000	No	Yes	2.00
79	7.90	10.87	97.77	2.93	0.56	1.57	16.51	0.00	16.51	4.000	No	Yes	2.00
80	8.00	10.28	98.20	2.94	0.56	1.56	15.20	0.00	15.20	4.000	No	Yes	2.00
81	8.10	9.38	99.82	2.96	0.57	1.56	13.86	0.00	13.86	4.000	No	Yes	2.00
82	8.20	8.40	100.00	2.99	0.57	1.57	12.49	0.00	12.49	4.000	No	Yes	2.00
83	8.30	7.35	100.00	3.04	0.58	1.57	10.94	0.00	10.94	4.000	No	Yes	2.00
84	8.40	6.58	100.00	3.09	0.59	1.57	9.23	0.00	9.23	4.000	No	Yes	2.00
85	8.50	6.25	100.00	3.11	0.59	1.57	9.13	0.00	9.13	4.000	No	Yes	2.00
86	8.60	6.30	100.00	3.12	0.58	1.56	9.42	0.00	9.42	4.000	No	Yes	2.00
87	8.70	6.35	100.00	3.12	0.58	1.56	9.40	0.00	9.40	4.000	No	Yes	2.00
88	8.80	6.29	100.00	3.13	0.59	1.56	9.28	0.00	9.28	4.000	No	Yes	2.00
89	8.90	6.27	100.00	3.12	0.59	1.55	9.07	0.00	9.07	4.000	No	Yes	2.00
90	9.00	6.29	100.00	3.10	0.59	1.55	9.24	0.00	9.24	4.000	No	Yes	2.00
91	9.10	6.09	100.00	3.09	0.58	1.55	9.31	0.00	9.31	4.000	No	Yes	2.00
92	9.20	5.58	100.00	3.12	0.59	1.55	8.16	0.00	8.16	4.000	No	Yes	2.00
93	9.30	5.10	100.00	3.16	0.59	1.55	7.00	0.00	7.00	4.000	No	Yes	2.00
94	9.40	5.13	100.00	3.17	0.59	1.54	7.22	0.00	7.22	4.000	No	Yes	2.00
95	9.50	5.52	100.00	3.15	0.59	1.54	8.20	0.00	8.20	4.000	No	Yes	2.00
96	9.60	5.90	100.00	3.12	0.59	1.53	8.64	0.00	8.64	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
97	9.70	7.76	100.00	2.99	0.59	1.53	8.76	0.00	8.76	4.000	No	Yes	2.00
98	9.80	11.21	92.32	2.87	0.56	1.50	15.87	0.00	15.87	4.000	No	Yes	2.00
99	9.90	12.34	90.70	2.85	0.54	1.47	22.63	0.00	22.63	4.000	No	Yes	2.00
100	10.00	10.19	97.42	2.93	0.57	1.50	13.37	0.00	13.37	4.000	No	Yes	2.00
101	10.10	6.46	100.00	3.10	0.59	1.52	6.86	0.00	6.86	4.000	No	Yes	2.00
102	10.20	5.25	100.00	3.16	0.59	1.51	7.33	0.00	7.33	4.000	No	Yes	2.00
103	10.30	5.64	100.00	3.14	0.59	1.51	8.29	0.00	8.29	4.000	No	Yes	2.00
104	10.40	5.93	100.00	3.13	0.59	1.50	8.48	0.00	8.48	4.000	No	Yes	2.00
105	10.50	5.98	100.00	3.15	0.59	1.50	8.46	0.00	8.46	4.000	No	Yes	2.00
106	10.60	5.98	100.00	3.16	0.59	1.50	8.44	0.00	8.44	4.000	No	Yes	2.00
107	10.70	5.98	100.00	3.17	0.59	1.49	8.42	0.00	8.42	4.000	No	Yes	2.00
108	10.80	5.98	100.00	3.18	0.59	1.49	8.40	0.00	8.40	4.000	No	Yes	2.00
109	10.90	5.98	100.00	3.18	0.59	1.49	8.38	0.00	8.38	4.000	No	Yes	2.00
110	11.00	5.98	100.00	3.18	0.59	1.48	8.36	0.00	8.36	4.000	No	Yes	2.00
111	11.10	6.00	100.00	3.18	0.59	1.48	8.34	0.00	8.34	4.000	No	Yes	2.00
112	11.20	6.41	100.00	3.17	0.59	1.47	8.41	0.00	8.41	4.000	No	Yes	2.00
113	11.30	7.76	100.00	3.12	0.58	1.46	9.98	0.00	9.98	4.000	No	Yes	2.00
114	11.40	9.54	100.00	3.04	0.57	1.45	13.72	0.00	13.72	4.000	No	Yes	2.00
115	11.50	10.92	100.00	2.97	0.56	1.44	15.43	0.00	15.43	4.000	No	Yes	2.00
116	11.60	11.17	97.44	2.93	0.56	1.44	15.39	0.00	15.39	4.000	No	Yes	2.00
117	11.70	10.34	98.59	2.94	0.57	1.43	14.61	0.00	14.61	4.000	No	Yes	2.00
118	11.80	9.11	100.00	3.01	0.57	1.44	12.09	0.00	12.09	4.000	No	Yes	2.00
119	11.90	8.03	100.00	3.09	0.58	1.44	10.41	0.00	10.41	4.000	No	Yes	2.00
120	12.00	8.26	100.00	3.12	0.58	1.44	10.24	0.00	10.24	4.000	No	Yes	2.00
121	12.10	9.89	100.00	3.07	0.57	1.43	12.93	0.00	12.93	4.000	No	Yes	2.00
122	12.20	12.14	100.00	2.98	0.56	1.41	16.70	0.00	16.70	4.000	No	Yes	2.00
123	12.30	13.79	93.92	2.89	0.55	1.40	18.88	0.00	18.88	4.000	No	Yes	2.00
124	12.40	14.39	87.64	2.81	0.55	1.40	19.25	0.00	19.25	4.000	No	Yes	2.00
125	12.50	14.67	82.64	2.75	0.55	1.40	18.93	0.00	18.93	4.000	No	Yes	2.00
126	12.60	15.66	79.65	2.71	0.55	1.39	19.87	0.00	19.87	4.000	No	Yes	2.00
127	12.70	16.72	79.59	2.71	0.54	1.38	22.87	0.00	22.87	4.000	No	Yes	2.00
128	12.80	17.02	81.91	2.74	0.54	1.38	22.77	0.00	22.77	4.000	No	Yes	2.00
129	12.90	15.54	87.27	2.80	0.55	1.38	20.85	0.00	20.85	4.000	No	Yes	2.00
130	13.00	13.13	94.33	2.89	0.56	1.38	17.11	0.00	17.11	4.000	No	Yes	2.00
131	13.10	10.98	100.00	2.97	0.57	1.39	13.49	0.00	13.49	4.000	No	Yes	2.00
132	13.20	9.80	100.00	3.00	0.57	1.39	12.55	0.00	12.55	4.000	No	Yes	2.00
133	13.30	9.73	100.00	2.98	0.57	1.39	12.52	0.00	12.52	4.000	No	Yes	2.00
134	13.40	10.47	97.89	2.94	0.57	1.38	13.13	0.00	13.13	4.000	No	Yes	2.00
135	13.50	11.58	94.54	2.89	0.56	1.37	15.29	0.00	15.29	4.000	No	Yes	2.00
136	13.60	12.48	92.96	2.87	0.56	1.37	16.65	0.00	16.65	4.000	No	Yes	2.00
137	13.70	12.75	93.45	2.88	0.56	1.36	16.42	0.00	16.42	4.000	No	Yes	2.00
138	13.80	12.33	95.38	2.90	0.56	1.36	16.18	0.00	16.18	4.000	No	Yes	2.00
139	13.90	11.80	96.70	2.92	0.56	1.36	14.98	0.00	14.98	4.000	No	Yes	2.00
140	14.00	11.32	96.68	2.92	0.57	1.36	14.33	0.00	14.33	4.000	No	Yes	2.00
141	14.10	11.16	95.06	2.90	0.57	1.36	14.30	0.00	14.30	4.000	No	Yes	2.00
142	14.20	11.16	93.56	2.88	0.57	1.35	14.27	0.00	14.27	4.000	No	Yes	2.00
143	14.30	11.46	92.66	2.87	0.57	1.35	14.26	0.00	14.26	4.000	No	Yes	2.00
144	14.40	12.08	92.61	2.87	0.56	1.35	15.34	0.00	15.34	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
145	14.50	13.00	92.59	2.87	0.56	1.34	16.45	0.00	16.45	4.000	No	Yes	2.00
146	14.60	13.94	92.49	2.87	0.56	1.33	17.57	0.00	17.57	4.000	No	Yes	2.00
147	14.70	14.88	91.82	2.86	0.55	1.33	18.68	0.00	18.68	4.000	No	Yes	2.00
148	14.80	15.29	91.67	2.86	0.55	1.32	19.77	0.00	19.77	4.000	No	Yes	2.00
149	14.90	14.81	92.88	2.87	0.55	1.32	18.93	0.00	18.93	4.000	No	Yes	2.00
150	15.00	13.79	95.30	2.90	0.56	1.32	16.84	0.00	16.84	4.000	No	Yes	2.00
151	15.10	12.99	97.51	2.93	0.56	1.32	15.93	0.00	15.93	4.000	No	Yes	2.00
152	15.20	12.91	98.16	2.94	0.56	1.32	15.89	0.00	15.89	4.000	No	Yes	2.00
153	15.30	13.60	97.12	2.93	0.56	1.32	16.45	0.00	16.45	4.000	No	Yes	2.00
154	15.40	14.65	95.40	2.91	0.55	1.31	18.30	0.00	18.30	4.000	No	Yes	2.00
155	15.50	14.88	95.22	2.90	0.55	1.30	19.55	0.00	19.55	4.000	No	Yes	2.00
156	15.60	14.72	95.79	2.91	0.56	1.31	17.19	0.00	17.19	4.000	No	Yes	2.00
157	15.70	14.79	95.85	2.91	0.56	1.30	17.61	0.00	17.61	4.000	No	Yes	2.00
158	15.80	15.44	94.72	2.90	0.55	1.29	19.66	0.00	19.66	4.000	No	Yes	2.00
159	15.90	15.62	94.62	2.90	0.55	1.29	19.40	0.00	19.40	4.000	No	Yes	2.00
160	16.00	15.50	95.49	2.91	0.55	1.29	18.16	0.00	18.16	4.000	No	Yes	2.00
161	16.10	17.19	93.24	2.88	0.55	1.29	19.09	0.00	19.09	4.000	No	Yes	2.00
162	16.20	21.05	87.38	2.80	0.53	1.27	25.22	0.00	25.22	4.000	No	Yes	2.00
163	16.30	24.86	81.83	2.74	0.51	1.26	31.49	0.00	31.49	4.000	No	Yes	2.00
164	16.40	26.05	79.21	2.70	0.51	1.26	32.20	0.00	32.20	4.000	No	Yes	2.00
165	16.50	23.46	81.11	2.73	0.52	1.26	29.19	0.00	29.19	4.000	No	Yes	2.00
166	16.60	18.42	87.47	2.81	0.54	1.27	22.38	0.00	22.38	4.000	No	Yes	2.00
167	16.70	12.98	97.46	2.93	0.57	1.28	14.51	0.00	14.51	4.000	No	Yes	2.00
168	16.80	8.92	100.00	3.07	0.58	1.29	9.96	0.00	9.96	4.000	No	Yes	2.00
169	16.90	6.90	100.00	3.14	0.59	1.29	7.93	0.00	7.93	4.000	No	Yes	2.00
170	17.00	6.16	100.00	3.14	0.59	1.29	7.26	0.00	7.26	4.000	No	Yes	2.00
171	17.10	5.97	100.00	3.12	0.59	1.28	7.25	0.00	7.25	4.000	No	Yes	2.00
172	17.20	5.97	100.00	3.09	0.59	1.28	7.24	0.00	7.24	4.000	No	Yes	2.00
173	17.30	5.79	100.00	3.09	0.59	1.28	7.23	0.00	7.23	4.000	No	Yes	2.00
174	17.40	5.81	100.00	3.09	0.60	1.28	6.55	0.00	6.55	4.000	No	Yes	2.00
175	17.50	6.26	100.00	3.08	0.59	1.28	7.27	0.00	7.27	4.000	No	Yes	2.00
176	17.60	7.24	100.00	3.06	0.59	1.27	8.82	0.00	8.82	4.000	No	Yes	2.00
177	17.70	8.07	100.00	3.06	0.58	1.27	9.98	0.00	9.98	4.000	No	Yes	2.00
178	17.80	8.41	100.00	3.06	0.58	1.26	10.18	0.00	10.18	4.000	No	Yes	2.00
179	17.90	8.42	100.00	3.08	0.58	1.26	9.97	0.00	9.97	4.000	No	Yes	2.00
180	18.00	8.37	100.00	3.09	0.58	1.26	9.95	0.00	9.95	4.000	No	Yes	2.00
181	18.10	8.17	100.00	3.13	0.58	1.26	9.93	0.00	9.93	4.000	No	Yes	2.00
182	18.20	8.13	100.00	3.16	0.59	1.26	9.22	0.00	9.22	4.000	No	Yes	2.00
183	18.30	8.94	100.00	3.16	0.58	1.25	9.78	0.00	9.78	4.000	No	Yes	2.00
184	18.40	10.90	100.00	3.09	0.57	1.24	12.67	0.00	12.67	4.000	No	Yes	2.00
185	18.50	13.00	100.00	3.02	0.56	1.24	15.95	0.00	15.95	4.000	No	Yes	2.00
186	18.60	14.19	100.00	2.97	0.56	1.23	16.93	0.00	16.93	4.000	No	Yes	2.00
187	18.70	15.48	96.40	2.92	0.56	1.23	16.68	0.00	16.68	4.000	No	Yes	2.00
188	18.80	16.63	93.73	2.88	0.55	1.22	20.27	0.00	20.27	4.000	No	Yes	2.00
189	18.90	16.88	93.83	2.89	0.54	1.22	20.72	0.00	20.72	4.000	No	Yes	2.00
190	19.00	15.17	97.95	2.94	0.56	1.22	17.42	0.00	17.42	4.000	No	Yes	2.00
191	19.10	12.50	100.00	3.02	0.57	1.22	14.38	0.00	14.38	4.000	No	Yes	2.00
192	19.20	10.65	100.00	3.09	0.58	1.23	11.54	0.00	11.54	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
193	19.30	10.32	100.00	3.09	0.58	1.22	11.06	0.00	11.06	4.000	No	Yes	2.00
194	19.40	11.45	100.00	3.04	0.57	1.22	13.16	0.00	13.16	4.000	No	Yes	2.00
195	19.50	13.39	100.00	2.97	0.56	1.21	15.32	0.00	15.32	4.000	No	Yes	2.00
196	19.60	15.68	94.28	2.89	0.56	1.21	17.56	0.00	17.56	4.000	No	Yes	2.00
197	19.70	17.74	88.36	2.82	0.55	1.20	20.77	0.00	20.77	4.000	No	Yes	2.00
198	19.80	19.36	84.76	2.77	0.54	1.20	22.13	0.00	22.13	4.000	No	Yes	2.00
199	19.90	18.84	86.43	2.79	0.54	1.20	22.85	0.00	22.85	4.000	No	Yes	2.00
200	20.00	16.51	91.54	2.86	0.55	1.20	18.92	0.00	18.92	4.000	No	Yes	2.00
201	20.10	13.94	96.74	2.92	0.57	1.20	14.24	0.00	14.24	4.000	No	Yes	2.00
202	20.20	12.46	98.68	2.95	0.57	1.20	14.21	0.00	14.21	4.000	No	Yes	2.00
203	20.30	12.39	98.46	2.94	0.57	1.20	13.88	0.00	13.88	4.000	No	Yes	2.00
204	20.40	12.55	98.65	2.95	0.57	1.20	13.94	0.00	13.94	4.000	No	Yes	2.00
205	20.50	13.23	97.37	2.93	0.57	1.19	14.69	0.00	14.69	4.000	No	Yes	2.00
206	20.60	14.29	94.97	2.90	0.56	1.19	16.05	0.00	16.05	4.000	No	Yes	2.00
207	20.70	15.22	93.62	2.88	0.56	1.18	17.39	0.00	17.39	4.000	No	Yes	2.00
208	20.80	16.35	93.44	2.88	0.56	1.18	17.65	0.00	17.65	4.000	No	Yes	2.00
209	20.90	18.79	92.54	2.87	0.55	1.18	19.69	0.00	19.69	4.000	Yes	Yes	2.00
210	21.00	23.85	88.40	2.82	0.53	1.17	25.25	0.00	25.25	4.000	Yes	Yes	2.00
211	21.10	30.27	82.41	2.74	0.51	1.16	33.88	0.00	33.88	4.000	Yes	Yes	2.00
212	21.20	36.95	75.22	2.65	0.49	1.15	40.19	0.00	40.19	4.000	Yes	Yes	2.00
213	21.30	42.73	66.77	2.55	0.48	1.14	46.37	63.43	109.81	4.000	Yes	No	2.00
214	21.40	47.27	58.16	2.44	0.47	1.14	51.99	62.74	114.73	4.000	Yes	No	2.00
215	21.50	49.21	51.81	2.36	0.47	1.14	54.32	61.14	115.47	4.000	Yes	No	2.00
216	21.60	48.10	50.64	2.35	0.47	1.14	52.35	60.14	112.48	0.156	No	No	0.18
217	21.70	45.14	54.66	2.40	0.48	1.14	48.33	60.58	108.91	0.150	No	No	0.18
218	21.80	42.84	60.79	2.47	0.48	1.14	44.77	61.49	106.25	0.146	No	No	0.17
219	21.90	45.62	63.00	2.50	0.48	1.13	44.82	62.08	106.90	4.000	Yes	No	2.00
220	22.00	55.53	58.22	2.44	0.46	1.12	56.63	64.05	120.67	4.000	Yes	No	2.00
221	22.10	70.39	48.95	2.32	0.42	1.11	75.04	65.38	140.41	4.000	Yes	No	2.00
222	22.20	86.19	38.72	2.20	0.40	1.10	90.15	62.65	152.80	4.000	Yes	No	2.00
223	22.30	98.36	30.33	2.09	0.39	1.10	104.62	56.94	161.56	4.000	Yes	No	2.00
224	22.40	107.08	25.23	2.03	0.38	1.10	111.90	50.16	162.06	4.000	Yes	No	2.00
225	22.50	115.37	22.92	2.00	0.38	1.10	116.46	46.21	162.67	0.401	No	No	0.49
226	22.60	122.02	22.50	1.99	0.36	1.09	129.22	47.27	176.48	0.634	No	No	0.78
227	22.70	126.84	22.77	2.00	0.36	1.09	131.20	48.23	179.43	0.710	No	No	0.88
228	22.80	129.17	23.36	2.00	0.36	1.08	130.10	49.38	179.48	0.712	No	No	0.88
229	22.90	136.06	22.91	2.00	0.35	1.08	135.44	49.21	184.65	0.882	No	No	1.09
230	23.00	147.42	21.59	1.98	0.33	1.07	150.87	48.30	199.16	1.805	No	No	2.00
231	23.10	160.45	19.96	1.96	0.32	1.07	162.93	45.38	208.31	3.124	No	No	2.00
232	23.20	171.23	18.78	1.95	0.31	1.07	173.08	42.94	216.02	4.000	No	No	2.00
233	23.30	180.27	18.08	1.94	0.30	1.06	181.79	41.62	223.40	4.000	No	No	2.00
234	23.40	187.37	17.72	1.93	0.29	1.06	188.58	41.10	229.69	4.000	No	No	2.00
235	23.50	191.52	17.58	1.93	0.29	1.06	192.98	41.08	234.07	4.000	No	No	2.00
236	23.60	191.73	17.68	1.93	0.29	1.06	193.06	41.45	234.51	4.000	No	No	2.00
237	23.70	187.36	18.31	1.94	0.29	1.06	188.48	43.21	231.69	4.000	No	No	2.00
238	23.80	178.72	19.90	1.96	0.30	1.06	179.54	47.45	227.00	4.000	No	No	2.00
239	23.90	166.77	23.35	2.00	0.30	1.06	167.04	55.37	222.42	4.000	No	No	2.00
240	24.00	149.50	27.28	2.05	0.31	1.06	152.74	61.47	214.21	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
241	24.10	133.96	29.97	2.09	0.34	1.06	128.46	61.29	189.75	1.113	No	No	1.36
242	24.20	126.47	29.13	2.08	0.36	1.06	121.26	58.56	179.83	0.722	No	No	0.87
243	24.30	128.47	26.38	2.04	0.35	1.06	130.65	55.66	186.32	0.950	No	No	1.16
244	24.40	130.78	24.62	2.02	0.35	1.06	134.07	52.78	186.86	0.973	No	No	1.19
245	24.50	124.66	26.19	2.04	0.35	1.06	127.63	54.76	182.39	4.000	Yes	No	2.00
246	24.60	110.33	31.23	2.10	0.37	1.06	112.21	59.72	171.93	4.000	Yes	No	2.00
247	24.70	91.14	39.91	2.21	0.39	1.06	91.40	63.91	155.30	4.000	Yes	No	2.00
248	24.80	72.12	50.33	2.34	0.43	1.07	70.57	64.85	135.41	4.000	Yes	No	2.00
249	24.90	57.73	60.64	2.47	0.46	1.07	55.60	64.49	120.09	4.000	Yes	No	2.00
250	25.00	49.70	67.96	2.56	0.47	1.07	48.40	64.28	112.68	4.000	Yes	No	2.00
251	25.10	47.44	71.46	2.61	0.48	1.07	46.42	0.00	46.42	4.000	Yes	Yes	2.00
252	25.20	45.12	74.67	2.65	0.47	1.06	48.60	0.00	48.60	4.000	Yes	Yes	2.00
253	25.30	42.32	77.99	2.69	0.49	1.07	41.26	0.00	41.26	4.000	Yes	Yes	2.00
254	25.40	41.45	78.73	2.70	0.50	1.07	37.86	0.00	37.86	4.000	Yes	Yes	2.00
255	25.50	47.50	71.93	2.61	0.48	1.06	45.81	0.00	45.81	4.000	Yes	Yes	2.00
256	25.60	58.52	60.67	2.47	0.45	1.06	58.98	65.45	124.43	4.000	Yes	No	2.00
257	25.70	69.31	50.16	2.34	0.43	1.05	70.21	64.68	134.89	4.000	Yes	No	2.00
258	25.80	77.97	43.00	2.25	0.42	1.05	77.39	62.66	140.05	4.000	Yes	No	2.00
259	25.90	83.74	39.64	2.21	0.41	1.05	84.18	61.96	146.14	4.000	Yes	No	2.00
260	26.00	87.01	38.64	2.20	0.41	1.04	86.81	61.80	148.62	0.280	No	No	0.32
261	26.10	87.64	39.76	2.21	0.40	1.04	86.61	62.64	149.25	0.284	No	No	0.33
262	26.20	89.33	39.85	2.21	0.41	1.04	85.65	62.47	148.12	0.277	No	No	0.32
263	26.30	93.87	37.35	2.18	0.40	1.04	91.38	61.77	153.15	0.311	No	No	0.36
264	26.40	98.42	33.65	2.13	0.39	1.04	99.48	59.94	159.42	0.366	No	No	0.42
265	26.50	100.49	31.74	2.11	0.39	1.04	98.57	57.51	156.08	0.335	No	No	0.39
266	26.60	99.58	32.64	2.12	0.39	1.03	97.07	58.26	155.34	0.328	No	No	0.38
267	26.70	99.14	33.85	2.14	0.39	1.03	96.46	59.49	155.94	0.334	No	No	0.39
268	26.80	99.48	34.73	2.15	0.39	1.03	96.89	60.52	157.41	0.347	No	No	0.40
269	26.90	100.62	35.02	2.15	0.39	1.03	97.65	60.99	158.64	0.358	No	No	0.41
270	27.00	102.38	34.80	2.15	0.39	1.03	99.36	61.15	160.51	0.377	No	No	0.44
271	27.10	104.07	34.41	2.14	0.38	1.03	101.57	61.23	162.80	0.403	No	No	0.47
272	27.20	105.35	34.40	2.14	0.38	1.03	102.11	61.33	163.45	0.410	No	No	0.47
273	27.30	105.96	35.19	2.15	0.38	1.02	102.66	62.29	164.94	0.429	No	No	0.50
274	27.40	106.62	36.60	2.17	0.38	1.02	102.93	63.76	166.69	0.453	No	No	0.52
275	27.50	107.61	37.77	2.18	0.37	1.02	103.58	65.00	168.58	0.481	No	No	0.56
276	27.60	109.14	37.93	2.19	0.37	1.02	105.07	65.50	170.57	0.514	No	No	0.60
277	27.70	111.42	37.03	2.18	0.37	1.02	106.93	65.10	172.03	0.540	No	No	0.63
278	27.80	114.37	35.93	2.16	0.37	1.02	109.72	64.65	174.37	0.587	No	No	0.68
279	27.90	117.17	35.00	2.15	0.36	1.02	113.13	64.45	177.58	0.661	No	No	0.77
280	28.00	117.25	34.12	2.14	0.36	1.01	114.56	63.79	178.35	0.681	No	No	0.79
281	28.10	113.03	33.84	2.14	0.37	1.01	109.57	62.36	171.93	0.538	No	No	0.62
282	28.20	104.54	35.87	2.16	0.38	1.01	100.69	62.53	163.22	0.407	No	No	0.47
283	28.30	96.33	39.03	2.20	0.40	1.01	89.95	62.86	152.81	0.309	No	No	0.35
284	28.40	89.43	42.00	2.24	0.40	1.01	85.75	64.07	149.82	0.288	No	No	0.33
285	28.50	84.52	43.10	2.25	0.41	1.01	80.65	63.54	144.18	0.255	No	No	0.29
286	28.60	79.72	45.07	2.28	0.42	1.01	75.64	63.48	139.11	4.000	Yes	No	2.00
287	28.70	74.73	48.41	2.32	0.43	1.01	71.73	64.24	135.98	4.000	Yes	No	2.00
288	28.80	69.75	53.27	2.38	0.44	1.01	66.13	64.90	131.03	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
289	28.90	62.88	59.23	2.45	0.44	1.01	61.18	65.63	126.81	4.000	Yes	No	2.00
290	29.00	55.17	65.60	2.53	0.46	1.00	51.90	64.75	116.65	4.000	Yes	No	2.00
291	29.10	47.60	71.37	2.60	0.48	1.00	43.95	0.00	43.95	4.000	Yes	Yes	2.00
292	29.20	41.43	76.01	2.66	0.49	1.00	39.47	0.00	39.47	4.000	Yes	Yes	2.00
293	29.30	37.19	79.77	2.71	0.51	1.00	34.20	0.00	34.20	4.000	Yes	Yes	2.00
294	29.40	34.70	82.76	2.75	0.51	1.00	31.75	0.00	31.75	4.000	Yes	Yes	2.00
295	29.50	34.06	84.04	2.76	0.51	1.00	32.26	0.00	32.26	4.000	No	Yes	2.00
296	29.60	33.91	84.03	2.76	0.51	1.00	32.24	0.00	32.24	4.000	No	Yes	2.00
297	29.70	32.03	85.01	2.78	0.51	0.99	31.21	0.00	31.21	4.000	No	Yes	2.00
298	29.80	29.66	87.02	2.80	0.53	0.99	26.82	0.00	26.82	4.000	No	Yes	2.00
299	29.90	28.43	89.36	2.83	0.53	0.99	25.44	0.00	25.44	4.000	No	Yes	2.00
300	30.00	32.28	88.57	2.82	0.52	0.99	27.62	0.00	27.62	4.000	No	Yes	2.00
301	30.10	38.09	85.55	2.78	0.49	0.99	37.51	0.00	37.51	4.000	No	Yes	2.00
302	30.20	43.19	82.33	2.74	0.48	0.99	41.61	0.00	41.61	4.000	No	Yes	2.00
303	30.30	44.63	81.64	2.73	0.48	0.99	41.77	0.00	41.77	4.000	No	Yes	2.00
304	30.40	44.36	82.62	2.75	0.48	0.99	41.37	0.00	41.37	4.000	No	Yes	2.00
305	30.50	46.20	82.49	2.74	0.49	0.98	40.68	0.00	40.68	4.000	Yes	Yes	2.00
306	30.60	51.44	78.16	2.69	0.47	0.98	46.73	0.00	46.73	4.000	Yes	Yes	2.00
307	30.70	59.73	70.54	2.59	0.45	0.98	55.85	67.00	122.85	4.000	Yes	No	2.00
308	30.80	69.61	61.43	2.48	0.44	0.98	63.67	66.99	130.66	4.000	Yes	No	2.00
309	30.90	81.48	52.07	2.36	0.42	0.98	74.14	66.57	140.70	4.000	Yes	No	2.00
310	31.00	94.67	44.14	2.26	0.40	0.98	88.78	66.24	155.02	4.000	Yes	No	2.00
311	31.10	106.82	38.88	2.20	0.38	0.98	100.30	65.20	165.50	4.000	Yes	No	2.00
312	31.20	116.62	36.34	2.17	0.37	0.98	107.83	64.64	172.47	4.000	Yes	No	2.00
313	31.30	124.76	35.63	2.16	0.35	0.98	115.89	65.74	181.63	0.777	No	No	0.88
314	31.40	130.68	35.43	2.16	0.34	0.98	122.74	67.08	189.82	1.116	No	No	1.27
315	31.50	133.94	34.94	2.15	0.34	0.98	124.08	66.83	190.91	1.176	No	No	1.34
316	31.60	134.30	34.57	2.14	0.34	0.98	124.65	66.55	191.20	1.193	No	No	1.36
317	31.70	132.00	34.84	2.15	0.34	0.98	123.35	66.56	189.90	1.121	No	No	1.28
318	31.80	124.86	36.08	2.16	0.35	0.97	117.27	66.52	183.79	0.850	No	No	0.97
319	31.90	112.69	38.17	2.19	0.37	0.97	104.29	65.53	169.82	0.501	No	No	0.56
320	32.00	97.91	41.76	2.23	0.40	0.97	89.04	64.71	153.75	0.316	No	No	0.35
321	32.10	85.37	47.09	2.30	0.42	0.97	75.77	64.63	140.40	0.236	No	No	0.26
322	32.20	78.62	52.40	2.37	0.43	0.96	69.18	65.37	134.55	0.213	No	No	0.23
323	32.30	78.07	54.80	2.40	0.43	0.96	70.05	66.56	136.61	0.221	No	No	0.24
324	32.40	82.35	53.86	2.39	0.42	0.96	74.02	67.27	141.29	0.240	No	No	0.27
325	32.50	89.96	50.55	2.34	0.41	0.96	80.76	67.66	148.42	0.279	No	No	0.31
326	32.60	100.87	45.58	2.28	0.39	0.96	90.81	67.65	158.46	0.356	No	No	0.40
327	32.70	114.12	39.71	2.21	0.37	0.96	103.93	66.77	170.69	0.516	No	No	0.58
328	32.80	125.97	33.87	2.14	0.36	0.96	117.13	64.07	181.20	0.763	No	No	0.86
329	32.90	133.61	30.40	2.09	0.35	0.96	123.26	60.86	184.13	0.863	No	No	0.97
330	33.00	136.56	28.67	2.07	0.35	0.96	124.66	58.50	183.16	0.828	No	No	0.93
331	33.10	135.19	27.25	2.05	0.36	0.96	124.82	56.17	180.98	0.756	No	No	0.85
332	33.20	129.92	26.19	2.04	0.37	0.96	118.93	53.19	172.11	0.542	No	No	0.61
333	33.30	122.33	26.47	2.04	0.38	0.96	109.55	51.97	161.52	0.388	No	No	0.43
334	33.40	115.41	29.91	2.09	0.39	0.96	103.43	56.13	159.56	0.367	No	No	0.41
335	33.50	111.66	33.26	2.13	0.39	0.95	99.56	59.51	159.07	0.362	No	No	0.40
336	33.60	111.68	35.79	2.16	0.39	0.95	99.08	62.08	161.16	0.384	No	No	0.43

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
337	33.70	116.59	36.98	2.17	0.38	0.95	103.30	64.21	167.51	0.465	No	No	0.52
338	33.80	126.41	36.14	2.16	0.36	0.95	112.87	65.58	178.45	0.684	No	No	0.77
339	33.90	138.32	33.47	2.13	0.34	0.96	125.95	65.52	191.47	1.209	No	No	1.36
340	34.00	149.33	29.80	2.09	0.33	0.96	135.85	62.52	198.37	1.728	No	No	1.93
341	34.10	156.01	26.45	2.04	0.33	0.96	142.85	58.05	200.90	1.990	No	No	2.00
342	34.20	158.07	24.67	2.02	0.33	0.95	143.82	54.56	198.38	1.728	No	No	1.93
343	34.30	158.80	24.40	2.02	0.34	0.95	140.95	53.48	194.43	1.401	No	No	1.57
344	34.40	162.94	24.74	2.02	0.33	0.95	144.38	54.81	199.19	1.808	No	No	2.00
345	34.50	169.31	24.83	2.02	0.31	0.95	155.00	56.85	211.85	3.949	No	No	2.00
346	34.60	175.37	24.56	2.02	0.31	0.95	158.33	56.80	215.13	4.000	No	No	2.00
347	34.70	179.32	24.19	2.01	0.31	0.95	160.87	56.39	217.26	4.000	No	No	2.00
348	34.80	184.04	23.34	2.00	0.30	0.95	165.52	55.09	220.61	4.000	No	No	2.00
349	34.90	189.55	21.83	1.99	0.30	0.95	170.92	51.97	222.89	4.000	No	No	2.00
350	35.00	194.31	20.09	1.96	0.30	0.95	175.52	47.49	223.01	4.000	No	No	2.00
351	35.10	196.77	18.94	1.95	0.30	0.95	177.98	44.11	222.09	4.000	No	No	2.00
352	35.20	196.37	18.83	1.95	0.30	0.95	177.03	43.60	220.63	4.000	No	No	2.00
353	35.30	193.58	19.23	1.95	0.31	0.95	173.84	44.53	218.37	4.000	No	No	2.00
354	35.40	189.34	19.45	1.96	0.31	0.95	169.73	44.70	214.43	4.000	No	No	2.00
355	35.50	184.20	19.26	1.95	0.32	0.95	164.74	43.47	208.21	3.103	No	No	2.00
356	35.60	178.51	18.80	1.95	0.33	0.94	158.93	41.27	200.20	1.913	No	No	2.00
357	35.70	173.44	17.99	1.94	0.34	0.94	153.22	37.96	191.18	1.191	No	No	1.33
358	35.80	169.68	16.66	1.92	0.35	0.94	149.82	33.13	182.95	0.821	No	No	0.91
359	35.90	166.88	14.61	1.90	0.37	0.93	147.46	25.63	173.09	0.561	No	No	0.62
360	36.00	163.35	12.39	1.87	0.39	0.93	144.18	17.24	161.42	0.387	No	No	0.43
361	36.10	158.25	10.69	1.85	0.40	0.93	138.72	11.01	149.73	0.287	No	No	0.31
362	36.20	152.33	10.51	1.84	0.42	0.92	132.36	10.21	142.57	0.247	No	No	0.27
363	36.30	147.13	11.75	1.86	0.42	0.92	127.38	14.13	141.51	0.241	No	No	0.26
364	36.40	143.89	13.55	1.88	0.41	0.92	124.51	20.17	144.67	0.257	No	No	0.28
365	36.50	142.53	15.00	1.90	0.41	0.92	123.76	25.03	148.80	0.281	No	No	0.31
366	36.60	143.00	15.76	1.91	0.40	0.92	123.87	27.58	151.45	0.299	No	No	0.33
367	36.70	145.61	16.04	1.91	0.40	0.92	125.79	28.67	154.46	0.321	No	No	0.35
368	36.80	150.56	15.80	1.91	0.39	0.92	130.63	28.34	158.97	0.361	No	No	0.40
369	36.90	157.66	15.00	1.90	0.38	0.92	136.90	26.14	163.04	0.405	No	No	0.45
370	37.00	165.31	13.72	1.88	0.38	0.92	144.49	22.15	166.64	0.452	No	No	0.50
371	37.10	172.32	12.22	1.87	0.38	0.92	150.62	16.93	167.55	0.465	No	No	0.51
372	37.20	177.10	11.31	1.85	0.37	0.92	155.08	13.80	168.88	0.486	No	No	0.53
373	37.30	178.87	11.25	1.85	0.37	0.92	156.73	13.66	170.38	0.511	No	No	0.56
374	37.40	177.96	11.89	1.86	0.37	0.92	154.98	15.93	170.91	0.520	No	No	0.57
375	37.50	175.45	12.66	1.87	0.37	0.92	152.38	18.70	171.09	0.523	No	No	0.58
376	37.60	172.65	13.55	1.88	0.37	0.92	149.83	21.88	171.71	0.534	No	No	0.59
377	37.70	169.90	14.62	1.90	0.37	0.92	147.37	25.64	173.01	0.559	No	No	0.61
378	37.80	167.26	15.74	1.91	0.37	0.92	145.00	29.47	174.46	0.589	No	No	0.65
379	37.90	165.19	16.80	1.92	0.36	0.92	142.74	32.88	175.61	0.614	No	No	0.68
380	38.00	164.02	17.87	1.94	0.36	0.92	141.87	36.26	178.13	0.675	No	No	0.74
381	38.10	163.69	18.83	1.95	0.36	0.92	141.89	39.25	181.14	0.761	No	No	0.84
382	38.20	163.69	19.45	1.96	0.35	0.92	141.85	41.09	182.94	0.820	No	No	0.90
383	38.30	163.49	20.04	1.96	0.35	0.92	141.81	42.78	184.59	0.880	No	No	0.97
384	38.40	162.37	20.81	1.97	0.35	0.92	141.25	44.81	186.06	0.939	No	No	1.03

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
385	38.50	159.91	21.74	1.98	0.35	0.92	138.69	46.88	185.57	0.919	No	No	1.01
386	38.60	156.57	22.69	2.00	0.35	0.91	135.03	48.63	183.66	0.846	No	No	0.93
387	38.70	153.20	23.68	2.01	0.35	0.91	132.04	50.42	182.45	0.804	No	No	0.88
388	38.80	150.08	24.73	2.02	0.36	0.91	129.45	52.22	181.66	0.778	No	No	0.85
389	38.90	147.28	25.63	2.03	0.36	0.91	126.42	53.48	179.90	0.724	No	No	0.80
390	39.00	145.42	26.08	2.04	0.36	0.91	124.27	53.95	178.23	0.678	No	No	0.74
391	39.10	145.19	26.00	2.04	0.36	0.91	124.14	53.78	177.91	0.670	No	No	0.73
392	39.20	146.51	25.41	2.03	0.36	0.91	125.44	52.89	178.32	0.680	No	No	0.75
393	39.30	148.08	24.58	2.02	0.36	0.91	127.37	51.55	178.92	0.696	No	No	0.76
394	39.40	149.40	23.65	2.01	0.36	0.91	127.82	49.65	177.47	0.658	No	No	0.72
395	39.50	150.23	22.85	2.00	0.36	0.90	128.42	47.97	176.38	0.632	No	No	0.69
396	39.60	150.45	22.10	1.99	0.36	0.90	128.96	46.29	175.26	0.606	No	No	0.66
397	39.70	151.53	21.36	1.98	0.37	0.90	127.77	44.28	172.05	0.540	No	No	0.59
398	39.80	153.36	20.87	1.97	0.37	0.90	130.73	43.46	174.19	0.583	No	No	0.64
399	39.90	155.09	21.54	1.98	0.36	0.90	133.53	45.61	179.13	0.702	No	No	0.77
400	40.00	154.86	22.95	2.00	0.36	0.90	132.36	48.81	181.17	0.762	No	No	0.83
401	40.10	154.63	23.89	2.01	0.36	0.90	130.14	50.55	180.69	0.747	No	No	0.82
402	40.20	156.64	23.60	2.01	0.35	0.90	132.83	50.36	183.19	0.829	No	No	0.91
403	40.30	160.77	22.66	2.00	0.35	0.90	137.43	48.95	186.38	0.952	No	No	1.04
404	40.40	165.07	21.80	1.99	0.35	0.90	140.80	47.34	188.14	1.032	No	No	1.13
405	40.50	168.83	20.83	1.97	0.35	0.90	143.81	45.23	189.04	1.076	No	No	1.18
406	40.60	172.09	19.72	1.96	0.34	0.90	146.90	42.54	189.44	1.096	No	No	1.20
407	40.70	175.00	18.53	1.94	0.35	0.90	148.78	39.17	187.95	1.023	No	No	1.12
408	40.80	177.41	17.61	1.93	0.35	0.90	150.80	36.44	187.24	0.990	No	No	1.08
409	40.90	179.23	17.16	1.93	0.35	0.90	152.55	35.14	187.70	1.011	No	No	1.10
410	41.00	180.47	17.47	1.93	0.34	0.90	153.16	36.24	189.40	1.094	No	No	1.19
411	41.10	181.45	18.23	1.94	0.34	0.90	153.95	38.84	192.79	1.290	No	No	1.40
412	41.20	182.77	18.86	1.95	0.33	0.90	155.24	41.01	196.25	1.541	No	No	1.67
413	41.30	184.68	19.27	1.95	0.33	0.90	156.81	42.47	199.28	1.817	No	No	1.96
414	41.40	186.86	19.12	1.95	0.33	0.90	159.00	42.29	201.29	2.035	No	No	2.00
415	41.50	189.12	18.20	1.94	0.33	0.90	160.70	39.55	200.24	1.918	No	No	2.00
416	41.60	190.91	16.92	1.92	0.33	0.90	162.07	35.32	197.39	1.638	No	No	1.77
417	41.70	192.03	16.24	1.92	0.34	0.90	162.82	32.95	195.77	1.502	No	No	1.62
418	41.80	192.92	16.78	1.92	0.33	0.90	163.01	34.91	197.92	1.686	No	No	1.82
419	41.90	194.40	17.92	1.94	0.33	0.90	164.38	39.04	203.42	2.306	No	No	2.00
420	42.00	197.14	18.75	1.95	0.32	0.90	167.16	42.13	209.30	3.330	No	No	2.00
421	42.10	200.61	19.16	1.95	0.31	0.90	170.83	43.93	214.75	4.000	No	No	2.00
422	42.20	203.97	19.41	1.96	0.31	0.90	173.98	45.12	219.10	4.000	No	No	2.00
423	42.30	206.60	19.60	1.96	0.30	0.90	176.33	46.05	222.39	4.000	No	No	2.00
424	42.40	208.12	19.60	1.96	0.30	0.90	177.84	46.24	224.08	4.000	No	No	2.00
425	42.50	208.30	19.30	1.95	0.30	0.90	177.80	45.26	223.06	4.000	No	No	2.00
426	42.60	206.70	19.08	1.95	0.30	0.90	176.26	44.33	220.59	4.000	No	No	2.00
427	42.70	203.68	18.99	1.95	0.31	0.90	172.83	43.62	216.45	4.000	No	No	2.00
428	42.80	199.57	19.14	1.95	0.31	0.90	168.93	43.60	212.52	4.000	No	No	2.00
429	42.90	194.71	19.87	1.96	0.32	0.89	164.66	45.33	210.00	3.488	No	No	2.00
430	43.00	190.18	21.32	1.98	0.32	0.89	159.53	48.86	208.39	3.140	No	No	2.00
431	43.10	187.86	22.91	2.00	0.32	0.89	156.88	52.62	209.50	3.375	No	No	2.00
432	43.20	190.13	23.39	2.00	0.31	0.89	158.63	54.11	212.74	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
433	43.30	197.38	22.51	1.99	0.31	0.89	165.71	53.00	218.71	4.000	No	No	2.00
434	43.40	207.80	20.76	1.97	0.30	0.90	176.13	49.63	225.76	4.000	No	No	2.00
435	43.50	219.34	18.74	1.95	0.29	0.90	186.09	44.43	230.52	4.000	No	No	2.00
436	43.60	230.48	16.97	1.92	0.29	0.90	196.00	39.07	235.08	4.000	No	No	2.00
437	43.70	240.76	15.61	1.91	0.28	0.90	205.28	34.50	239.78	4.000	No	No	2.00
438	43.80	249.82	14.67	1.90	0.28	0.90	213.12	31.13	244.25	4.000	No	No	2.00
439	43.90	258.68	13.67	1.88	0.27	0.90	219.78	27.15	246.93	4.000	No	No	2.00
440	44.00	267.99	11.83	1.86	0.27	0.90	228.20	19.22	247.42	4.000	No	No	2.00
441	44.10	276.85	9.11	1.83	0.27	0.90	236.50	8.14	244.64	4.000	No	No	2.00
442	44.20	284.85	5.51	1.78	0.28	0.90	241.46	0.50	241.96	4.000	No	No	2.00
443	44.30	291.10	1.66	1.73	0.27	0.90	248.28	0.00	248.28	4.000	No	No	2.00
444	44.40	294.85	0.00	1.70	0.27	0.90	252.92	0.00	252.92	4.000	No	No	2.00
445	44.50	294.77	0.00	1.69	0.27	0.90	251.61	0.00	251.61	4.000	No	No	2.00
446	44.60	292.55	0.00	1.71	0.27	0.90	247.56	0.00	247.56	4.000	No	No	2.00
447	44.70	291.79	0.40	1.72	0.27	0.90	246.04	0.00	246.04	4.000	No	No	2.00
448	44.80	294.37	0.00	1.70	0.27	0.90	248.90	0.00	248.90	4.000	No	No	2.00
449	44.90	299.33	0.00	1.67	0.26	0.90	254.42	0.00	254.42	4.000	No	No	2.00
450	45.00	305.05	0.00	1.63	0.26	0.90	259.17	0.00	259.17	4.000	No	No	2.00
451	45.10	310.35	0.00	1.62	0.26	0.90	263.60	0.00	263.60	4.000	No	No	2.00
452	45.20	314.64	0.00	1.63	0.26	0.90	267.47	0.00	267.47	4.000	No	No	2.00
453	45.30	316.67	0.00	1.64	0.26	0.90	269.64	0.00	269.64	4.000	No	No	2.00
454	45.40	316.15	0.00	1.65	0.26	0.90	268.29	0.00	268.29	4.000	No	No	2.00
455	45.50	314.75	0.00	1.66	0.26	0.90	265.69	0.00	265.69	4.000	No	No	2.00
456	45.60	313.96	0.00	1.68	0.26	0.90	265.59	0.00	265.59	4.000	No	No	2.00
457	45.70	313.55	0.00	1.69	0.26	0.90	265.82	0.00	265.82	4.000	No	No	2.00
458	45.80	312.06	0.00	1.70	0.26	0.89	264.18	0.00	264.18	4.000	No	No	2.00
459	45.90	308.31	0.00	1.69	0.26	0.89	261.33	0.00	261.33	4.000	No	No	2.00
460	46.00	302.20	0.00	1.69	0.26	0.89	255.87	0.00	255.87	4.000	No	No	2.00
461	46.10	293.67	0.00	1.68	0.27	0.89	247.46	0.00	247.46	4.000	No	No	2.00
462	46.20	283.78	0.00	1.67	0.28	0.89	237.35	0.00	237.35	4.000	No	No	2.00
463	46.30	273.76	0.00	1.66	0.30	0.88	227.34	0.00	227.34	4.000	No	No	2.00
464	46.40	264.02	0.00	1.65	0.31	0.88	218.52	0.00	218.52	4.000	No	No	2.00
465	46.50	253.44	0.00	1.66	0.32	0.87	209.39	0.00	209.39	3.351	No	No	2.00
466	46.60	239.32	0.00	1.68	0.33	0.86	197.24	0.00	197.24	1.625	No	No	1.73
467	46.70	218.44	2.71	1.75	0.36	0.85	178.92	0.00	178.92	4.000	Yes	No	2.00
468	46.80	190.67	10.98	1.85	0.38	0.85	153.36	12.54	165.90	4.000	Yes	No	2.00
469	46.90	159.42	22.39	1.99	0.37	0.85	127.08	46.68	173.76	4.000	Yes	No	2.00
470	47.00	130.94	35.89	2.16	0.38	0.84	102.09	62.87	164.96	4.000	Yes	No	2.00
471	47.10	109.62	49.19	2.33	0.40	0.84	84.00	67.85	151.86	4.000	Yes	No	2.00
472	47.20	99.20	59.41	2.46	0.42	0.83	73.88	69.24	143.12	4.000	Yes	No	2.00
473	47.30	101.82	63.08	2.50	0.41	0.83	75.99	70.96	146.95	4.000	Yes	No	2.00
474	47.40	114.04	60.22	2.47	0.38	0.84	90.81	74.25	165.06	4.000	Yes	No	2.00
475	47.50	127.97	54.27	2.39	0.36	0.85	105.14	75.91	181.05	4.000	Yes	No	2.00
476	47.60	134.39	49.59	2.33	0.35	0.85	111.64	75.35	186.99	4.000	Yes	No	2.00
477	47.70	131.72	48.88	2.32	0.36	0.85	107.03	73.75	180.78	0.750	No	No	0.81
478	47.80	123.26	51.84	2.36	0.37	0.84	97.81	72.82	170.63	0.515	No	No	0.56
479	47.90	115.03	54.99	2.40	0.39	0.84	89.38	71.92	161.29	0.385	No	No	0.42
480	48.00	111.14	55.17	2.40	0.39	0.83	85.54	70.94	156.47	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
481	48.10	113.23	51.22	2.35	0.39	0.83	87.45	69.75	157.20	4.000	Yes	No	2.00
482	48.20	120.10	44.13	2.26	0.39	0.83	94.16	67.59	161.75	4.000	Yes	No	2.00
483	48.30	127.66	35.95	2.16	0.38	0.84	102.14	62.94	165.08	4.000	Yes	No	2.00
484	48.40	131.70	29.16	2.08	0.39	0.83	105.33	55.44	160.77	4.000	Yes	No	2.00
485	48.50	130.27	25.75	2.03	0.40	0.83	102.76	49.47	152.23	4.000	Yes	No	2.00
486	48.60	123.72	27.05	2.05	0.41	0.82	97.27	50.66	147.93	4.000	Yes	No	2.00
487	48.70	112.92	33.30	2.13	0.41	0.82	88.66	57.19	145.85	4.000	Yes	No	2.00
488	48.80	98.74	43.48	2.26	0.42	0.82	76.49	62.73	139.23	4.000	Yes	No	2.00
489	48.90	82.92	55.94	2.41	0.44	0.81	63.00	65.05	128.05	4.000	Yes	No	2.00
490	49.00	68.00	68.37	2.57	0.47	0.80	50.36	64.94	115.30	4.000	Yes	No	2.00
491	49.10	55.01	79.46	2.71	0.49	0.79	40.55	0.00	40.55	4.000	Yes	Yes	2.00
492	49.20	44.63	88.37	2.82	0.51	0.78	32.12	0.00	32.12	4.000	Yes	Yes	2.00
493	49.30	36.24	95.20	2.90	0.53	0.77	26.05	0.00	26.05	4.000	Yes	Yes	2.00
494	49.40	30.08	100.00	2.97	0.54	0.77	21.19	0.00	21.19	4.000	Yes	Yes	2.00
495	49.50	25.88	100.00	3.01	0.55	0.76	18.10	0.00	18.10	4.000	No	Yes	2.00
496	49.60	23.84	100.00	3.03	0.56	0.76	16.56	0.00	16.56	4.000	No	Yes	2.00
497	49.70	26.26	100.00	2.98	0.56	0.76	16.59	0.00	16.59	4.000	No	Yes	2.00
498	49.80	32.30	95.74	2.91	0.54	0.77	23.46	0.00	23.46	4.000	No	Yes	2.00
499	49.90	38.31	91.27	2.85	0.52	0.77	30.07	0.00	30.07	4.000	No	Yes	2.00

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q_t :	Total cone resistance
FC:	Fines content (%)
I_c :	Soil behavior type index
m:	Stress exponent
C_N :	Overburden correction factor
q_{c1N} :	Normalized and adjusted cone resistance
Δq_{c1N} :	Cone resistance correction factor due to fines
$q_{c1N,cs}$:	Normalized and adjusted cone resistance
CRR _{7.5} :	Cyclic resistance ratio for $M_w=7.5$
FS:	Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
0.10	2.00	0.00	0.00	0.10	0.00	0.20	2.00	0.00	0.00	0.10	0.00
0.30	2.00	0.00	0.00	0.10	0.00	0.40	2.00	0.00	0.00	0.10	0.00
0.50	2.00	0.00	0.00	0.10	0.00	0.60	2.00	0.00	0.00	0.10	0.00
0.70	2.00	0.00	0.00	0.10	0.00	0.80	2.00	0.00	0.00	0.10	0.00
0.90	2.00	0.00	0.00	0.10	0.00	1.00	2.00	0.00	0.00	0.10	0.00
1.10	2.00	0.00	0.00	0.10	0.00	1.20	2.00	0.00	0.00	0.10	0.00
1.30	2.00	0.00	0.00	0.10	0.00	1.40	2.00	0.00	0.00	0.10	0.00
1.50	2.00	0.00	0.00	0.10	0.00	1.60	2.00	0.00	0.00	0.10	0.00
1.70	2.00	0.00	0.00	0.10	0.00	1.80	2.00	0.00	0.00	0.10	0.00
1.90	2.00	0.00	0.00	0.10	0.00	2.00	2.00	0.00	0.00	0.10	0.00
2.10	2.00	0.00	0.00	0.10	0.00	2.20	2.00	0.00	0.00	0.10	0.00
2.30	2.00	0.00	0.00	0.10	0.00	2.40	2.00	0.00	0.00	0.10	0.00
2.50	2.00	0.00	0.00	0.10	0.00	2.60	2.00	0.00	0.00	0.10	0.00
2.70	2.00	0.00	0.00	0.10	0.00	2.80	2.00	0.00	0.00	0.10	0.00
2.90	2.00	0.00	0.00	0.10	0.00	3.00	2.00	0.00	0.00	0.10	0.00
3.10	2.00	0.00	0.00	0.10	0.00	3.20	2.00	0.00	0.00	0.10	0.00
3.30	2.00	0.00	0.00	0.10	0.00	3.40	2.00	0.00	0.00	0.10	0.00
3.50	2.00	0.00	0.00	0.10	0.00	3.60	2.00	0.00	0.00	0.10	0.00
3.70	2.00	0.00	0.00	0.10	0.00	3.80	2.00	0.00	0.00	0.10	0.00
3.90	2.00	0.00	0.00	0.10	0.00	4.00	2.00	0.00	0.00	0.10	0.00
4.10	2.00	0.00	0.00	0.10	0.00	4.20	2.00	0.00	0.00	0.10	0.00
4.30	2.00	0.00	0.00	0.10	0.00	4.40	2.00	0.00	0.00	0.10	0.00
4.50	2.00	0.00	0.00	0.10	0.00	4.60	2.00	0.00	0.00	0.10	0.00
4.70	2.00	0.00	0.00	0.10	0.00	4.80	2.00	0.00	0.00	0.10	0.00
4.90	2.00	0.00	0.00	0.10	0.00	5.00	2.00	0.00	0.00	0.10	0.00
5.10	2.00	0.00	0.00	0.10	0.00	5.20	2.00	0.00	0.00	0.10	0.00
5.30	2.00	0.00	0.00	0.10	0.00	5.40	2.00	0.00	0.00	0.10	0.00
5.50	2.00	0.00	0.00	0.10	0.00	5.60	2.00	0.00	0.00	0.10	0.00
5.70	2.00	0.00	0.00	0.10	0.00	5.80	2.00	0.00	0.00	0.10	0.00
5.90	2.00	0.00	0.00	0.10	0.00	6.00	2.00	0.00	0.00	0.10	0.00
6.10	2.00	0.00	0.00	0.10	0.00	6.20	2.00	0.00	0.00	0.10	0.00
6.30	2.00	0.00	0.00	0.10	0.00	6.40	2.00	0.00	0.00	0.10	0.00
6.50	2.00	0.00	0.00	0.10	0.00	6.60	2.00	0.00	0.00	0.10	0.00
6.70	2.00	0.00	0.00	0.10	0.00	6.80	2.00	0.00	0.00	0.10	0.00
6.90	2.00	0.00	0.00	0.10	0.00	7.00	2.00	0.00	0.00	0.10	0.00
7.10	2.00	0.00	0.00	0.10	0.00	7.20	2.00	0.00	0.00	0.10	0.00
7.30	2.00	0.00	0.00	0.10	0.00	7.40	2.00	0.00	0.00	0.10	0.00
7.50	2.00	0.00	0.00	0.10	0.00	7.60	2.00	0.00	0.00	0.10	0.00
7.70	2.00	0.00	0.00	0.10	0.00	7.80	2.00	0.00	0.00	0.10	0.00
7.90	2.00	0.00	0.00	0.10	0.00	8.00	2.00	0.00	0.00	0.10	0.00
8.10	2.00	0.00	0.00	0.10	0.00	8.20	2.00	0.00	0.00	0.10	0.00
8.30	2.00	0.00	0.00	0.10	0.00	8.40	2.00	0.00	0.00	0.10	0.00
8.50	2.00	0.00	0.00	0.10	0.00	8.60	2.00	0.00	0.00	0.10	0.00
8.70	2.00	0.00	0.00	0.10	0.00	8.80	2.00	0.00	0.00	0.10	0.00
8.90	2.00	0.00	0.00	0.10	0.00	9.00	2.00	0.00	0.00	0.10	0.00
9.10	2.00	0.00	0.00	0.10	0.00	9.20	2.00	0.00	0.00	0.10	0.00
9.30	2.00	0.00	0.00	0.10	0.00	9.40	2.00	0.00	0.00	0.10	0.00
9.50	2.00	0.00	0.00	0.10	0.00	9.60	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
9.70	2.00	0.00	0.00	0.10	0.00	9.80	2.00	0.00	0.00	0.10	0.00
9.90	2.00	0.00	0.00	0.10	0.00	10.00	2.00	0.00	0.00	0.10	0.00
10.10	2.00	0.00	0.00	0.10	0.00	10.20	2.00	0.00	0.00	0.10	0.00
10.30	2.00	0.00	0.00	0.10	0.00	10.40	2.00	0.00	0.00	0.10	0.00
10.50	2.00	0.00	0.00	0.10	0.00	10.60	2.00	0.00	0.00	0.10	0.00
10.70	2.00	0.00	0.00	0.10	0.00	10.80	2.00	0.00	0.00	0.10	0.00
10.90	2.00	0.00	0.00	0.10	0.00	11.00	2.00	0.00	0.00	0.10	0.00
11.10	2.00	0.00	0.00	0.10	0.00	11.20	2.00	0.00	0.00	0.10	0.00
11.30	2.00	0.00	0.00	0.10	0.00	11.40	2.00	0.00	0.00	0.10	0.00
11.50	2.00	0.00	0.00	0.10	0.00	11.60	2.00	0.00	0.00	0.10	0.00
11.70	2.00	0.00	0.00	0.10	0.00	11.80	2.00	0.00	0.00	0.10	0.00
11.90	2.00	0.00	0.00	0.10	0.00	12.00	2.00	0.00	0.00	0.10	0.00
12.10	2.00	0.00	0.00	0.10	0.00	12.20	2.00	0.00	0.00	0.10	0.00
12.30	2.00	0.00	0.00	0.10	0.00	12.40	2.00	0.00	0.00	0.10	0.00
12.50	2.00	0.00	0.00	0.10	0.00	12.60	2.00	0.00	0.00	0.10	0.00
12.70	2.00	0.00	0.00	0.10	0.00	12.80	2.00	0.00	0.00	0.10	0.00
12.90	2.00	0.00	0.00	0.10	0.00	13.00	2.00	0.00	0.00	0.10	0.00
13.10	2.00	0.00	0.00	0.10	0.00	13.20	2.00	0.00	0.00	0.10	0.00
13.30	2.00	0.00	0.00	0.10	0.00	13.40	2.00	0.00	0.00	0.10	0.00
13.50	2.00	0.00	0.00	0.10	0.00	13.60	2.00	0.00	0.00	0.10	0.00
13.70	2.00	0.00	0.00	0.10	0.00	13.80	2.00	0.00	0.00	0.10	0.00
13.90	2.00	0.00	0.00	0.10	0.00	14.00	2.00	0.00	0.00	0.10	0.00
14.10	2.00	0.00	0.00	0.10	0.00	14.20	2.00	0.00	0.00	0.10	0.00
14.30	2.00	0.00	0.00	0.10	0.00	14.40	2.00	0.00	0.00	0.10	0.00
14.50	2.00	0.00	0.00	0.10	0.00	14.60	2.00	0.00	0.00	0.10	0.00
14.70	2.00	0.00	0.00	0.10	0.00	14.80	2.00	0.00	0.00	0.10	0.00
14.90	2.00	0.00	0.00	0.10	0.00	15.00	2.00	0.00	0.00	0.10	0.00
15.10	2.00	0.00	0.00	0.10	0.00	15.20	2.00	0.00	0.00	0.10	0.00
15.30	2.00	0.00	0.00	0.10	0.00	15.40	2.00	0.00	0.00	0.10	0.00
15.50	2.00	0.00	0.00	0.10	0.00	15.60	2.00	0.00	0.00	0.10	0.00
15.70	2.00	0.00	0.00	0.10	0.00	15.80	2.00	0.00	0.00	0.10	0.00
15.90	2.00	0.00	0.00	0.10	0.00	16.00	2.00	0.00	0.00	0.10	0.00
16.10	2.00	0.00	0.00	0.10	0.00	16.20	2.00	0.00	0.00	0.10	0.00
16.30	2.00	0.00	0.00	0.10	0.00	16.40	2.00	0.00	0.00	0.10	0.00
16.50	2.00	0.00	0.00	0.10	0.00	16.60	2.00	0.00	0.00	0.10	0.00
16.70	2.00	0.00	0.00	0.10	0.00	16.80	2.00	0.00	0.00	0.10	0.00
16.90	2.00	0.00	0.00	0.10	0.00	17.00	2.00	0.00	0.00	0.10	0.00
17.10	2.00	0.00	0.00	0.10	0.00	17.20	2.00	0.00	0.00	0.10	0.00
17.30	2.00	0.00	0.00	0.10	0.00	17.40	2.00	0.00	0.00	0.10	0.00
17.50	2.00	0.00	0.00	0.10	0.00	17.60	2.00	0.00	0.00	0.10	0.00
17.70	2.00	0.00	0.00	0.10	0.00	17.80	2.00	0.00	0.00	0.10	0.00
17.90	2.00	0.00	0.00	0.10	0.00	18.00	2.00	0.00	0.00	0.10	0.00
18.10	2.00	0.00	0.00	0.10	0.00	18.20	2.00	0.00	0.00	0.10	0.00
18.30	2.00	0.00	0.00	0.10	0.00	18.40	2.00	0.00	0.00	0.10	0.00
18.50	2.00	0.00	0.00	0.10	0.00	18.60	2.00	0.00	0.00	0.10	0.00
18.70	2.00	0.00	0.00	0.10	0.00	18.80	2.00	0.00	0.00	0.10	0.00
18.90	2.00	0.00	0.00	0.10	0.00	19.00	2.00	0.00	0.00	0.10	0.00
19.10	2.00	0.00	0.00	0.10	0.00	19.20	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
19.30	2.00	0.00	0.00	0.10	0.00	19.40	2.00	0.00	0.00	0.10	0.00
19.50	2.00	0.00	0.00	0.10	0.00	19.60	2.00	0.00	0.00	0.10	0.00
19.70	2.00	0.00	0.00	0.10	0.00	19.80	2.00	0.00	0.00	0.10	0.00
19.90	2.00	0.00	0.00	0.10	0.00	20.00	2.00	0.00	0.00	0.10	0.00
20.10	2.00	0.00	0.00	0.10	0.00	20.20	2.00	0.00	0.00	0.10	0.00
20.30	2.00	0.00	0.00	0.10	0.00	20.40	2.00	0.00	0.00	0.10	0.00
20.50	2.00	0.00	0.00	0.10	0.00	20.60	2.00	0.00	0.00	0.10	0.00
20.70	2.00	0.00	0.00	0.10	0.00	20.80	2.00	0.00	0.00	0.10	0.00
20.90	2.00	0.00	0.00	0.10	0.00	21.00	2.00	0.00	0.00	0.10	0.00
21.10	2.00	0.00	0.00	0.10	0.00	21.20	2.00	0.00	0.00	0.10	0.00
21.30	2.00	0.00	0.00	0.10	0.00	21.40	2.00	0.00	0.00	0.10	0.00
21.50	2.00	0.00	0.00	0.10	0.00	21.60	0.18	0.00	0.00	0.10	0.17
21.70	0.18	0.00	0.00	0.10	0.17	21.80	0.17	0.00	0.00	0.10	0.17
21.90	2.00	0.00	0.00	0.10	0.00	22.00	2.00	0.00	0.00	0.10	0.00
22.10	2.00	0.00	0.00	0.10	0.00	22.20	2.00	0.00	0.00	0.10	0.00
22.30	2.00	0.00	0.00	0.10	0.00	22.40	2.00	0.00	0.00	0.10	0.00
22.50	0.49	0.00	0.00	0.10	0.10	22.60	0.78	0.00	0.00	0.10	0.04
22.70	0.88	0.00	0.00	0.10	0.02	22.80	0.88	0.00	0.00	0.10	0.02
22.90	1.09	0.00	0.00	0.10	0.00	23.00	2.00	0.00	0.00	0.10	0.00
23.10	2.00	0.00	0.00	0.10	0.00	23.20	2.00	0.00	0.00	0.10	0.00
23.30	2.00	0.00	0.00	0.10	0.00	23.40	2.00	0.00	0.00	0.10	0.00
23.50	2.00	0.00	0.00	0.10	0.00	23.60	2.00	0.00	0.00	0.10	0.00
23.70	2.00	0.00	0.00	0.10	0.00	23.80	2.00	0.00	0.00	0.10	0.00
23.90	2.00	0.00	0.00	0.10	0.00	24.00	2.00	0.00	0.00	0.10	0.00
24.10	1.36	0.00	0.00	0.10	0.00	24.20	0.87	0.00	0.00	0.10	0.02
24.30	1.16	0.00	0.00	0.10	0.00	24.40	1.19	0.00	0.00	0.10	0.00
24.50	2.00	0.00	0.00	0.10	0.00	24.60	2.00	0.00	0.00	0.10	0.00
24.70	2.00	0.00	0.00	0.10	0.00	24.80	2.00	0.00	0.00	0.10	0.00
24.90	2.00	0.00	0.00	0.10	0.00	25.00	2.00	0.00	0.00	0.10	0.00
25.10	2.00	0.00	0.00	0.10	0.00	25.20	2.00	0.00	0.00	0.10	0.00
25.30	2.00	0.00	0.00	0.10	0.00	25.40	2.00	0.00	0.00	0.10	0.00
25.50	2.00	0.00	0.00	0.10	0.00	25.60	2.00	0.00	0.00	0.10	0.00
25.70	2.00	0.00	0.00	0.10	0.00	25.80	2.00	0.00	0.00	0.10	0.00
25.90	2.00	0.00	0.00	0.10	0.00	26.00	0.32	0.68	0.34	0.10	0.12
26.10	0.33	0.67	0.34	0.10	0.12	26.20	0.32	0.68	0.33	0.10	0.12
26.30	0.36	0.64	0.36	0.10	0.12	26.40	0.42	0.00	0.00	0.10	0.10
26.50	0.39	0.61	0.38	0.10	0.11	26.60	0.38	0.62	0.37	0.10	0.11
26.70	0.39	0.61	0.37	0.10	0.11	26.80	0.40	0.00	0.00	0.10	0.11
26.90	0.41	0.00	0.00	0.10	0.11	27.00	0.44	0.00	0.00	0.10	0.10
27.10	0.47	0.00	0.00	0.10	0.10	27.20	0.47	0.00	0.00	0.10	0.09
27.30	0.50	0.00	0.00	0.10	0.09	27.40	0.52	0.00	0.00	0.10	0.08
27.50	0.56	0.00	0.00	0.10	0.08	27.60	0.60	0.00	0.00	0.10	0.07
27.70	0.63	0.00	0.00	0.10	0.07	27.80	0.68	0.00	0.00	0.10	0.06
27.90	0.77	0.00	0.00	0.10	0.04	28.00	0.79	0.00	0.00	0.10	0.04
28.10	0.62	0.00	0.00	0.10	0.07	28.20	0.47	0.00	0.00	0.10	0.09
28.30	0.35	0.65	0.35	0.10	0.11	28.40	0.33	0.67	0.34	0.10	0.12
28.50	0.29	0.71	0.32	0.10	0.12	28.60	2.00	0.00	0.00	0.10	0.00
28.70	2.00	0.00	0.00	0.10	0.00	28.80	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
28.90	2.00	0.00	0.00	0.10	0.00	29.00	2.00	0.00	0.00	0.10	0.00
29.10	2.00	0.00	0.00	0.10	0.00	29.20	2.00	0.00	0.00	0.10	0.00
29.30	2.00	0.00	0.00	0.10	0.00	29.40	2.00	0.00	0.00	0.10	0.00
29.50	2.00	0.00	0.00	0.10	0.00	29.60	2.00	0.00	0.00	0.10	0.00
29.70	2.00	0.00	0.00	0.10	0.00	29.80	2.00	0.00	0.00	0.10	0.00
29.90	2.00	0.00	0.00	0.10	0.00	30.00	2.00	0.00	0.00	0.10	0.00
30.10	2.00	0.00	0.00	0.10	0.00	30.20	2.00	0.00	0.00	0.10	0.00
30.30	2.00	0.00	0.00	0.10	0.00	30.40	2.00	0.00	0.00	0.10	0.00
30.50	2.00	0.00	0.00	0.10	0.00	30.60	2.00	0.00	0.00	0.10	0.00
30.70	2.00	0.00	0.00	0.10	0.00	30.80	2.00	0.00	0.00	0.10	0.00
30.90	2.00	0.00	0.00	0.10	0.00	31.00	2.00	0.00	0.00	0.10	0.00
31.10	2.00	0.00	0.00	0.10	0.00	31.20	2.00	0.00	0.00	0.10	0.00
31.30	0.88	0.00	0.00	0.10	0.02	31.40	1.27	0.00	0.00	0.10	0.00
31.50	1.34	0.00	0.00	0.10	0.00	31.60	1.36	0.00	0.00	0.10	0.00
31.70	1.28	0.00	0.00	0.10	0.00	31.80	0.97	0.00	0.00	0.10	0.01
31.90	0.56	0.00	0.00	0.10	0.07	32.00	0.35	0.65	0.35	0.10	0.10
32.10	0.26	0.74	0.30	0.10	0.11	32.20	0.23	0.77	0.29	0.10	0.12
32.30	0.24	0.76	0.30	0.10	0.12	32.40	0.27	0.73	0.31	0.10	0.11
32.50	0.31	0.69	0.33	0.10	0.11	32.60	0.40	0.00	0.00	0.10	0.09
32.70	0.58	0.00	0.00	0.10	0.06	32.80	0.86	0.00	0.00	0.10	0.02
32.90	0.97	0.00	0.00	0.10	0.00	33.00	0.93	0.00	0.00	0.10	0.01
33.10	0.85	0.00	0.00	0.10	0.02	33.20	0.61	0.00	0.00	0.10	0.06
33.30	0.43	0.00	0.00	0.10	0.09	33.40	0.41	0.00	0.00	0.10	0.09
33.50	0.40	0.00	0.00	0.10	0.09	33.60	0.43	0.00	0.00	0.10	0.09
33.70	0.52	0.00	0.00	0.10	0.07	33.80	0.77	0.00	0.00	0.10	0.03
33.90	1.36	0.00	0.00	0.10	0.00	34.00	1.93	0.00	0.00	0.10	0.00
34.10	2.00	0.00	0.00	0.10	0.00	34.20	1.93	0.00	0.00	0.10	0.00
34.30	1.57	0.00	0.00	0.10	0.00	34.40	2.00	0.00	0.00	0.10	0.00
34.50	2.00	0.00	0.00	0.10	0.00	34.60	2.00	0.00	0.00	0.10	0.00
34.70	2.00	0.00	0.00	0.10	0.00	34.80	2.00	0.00	0.00	0.10	0.00
34.90	2.00	0.00	0.00	0.10	0.00	35.00	2.00	0.00	0.00	0.10	0.00
35.10	2.00	0.00	0.00	0.10	0.00	35.20	2.00	0.00	0.00	0.10	0.00
35.30	2.00	0.00	0.00	0.10	0.00	35.40	2.00	0.00	0.00	0.10	0.00
35.50	2.00	0.00	0.00	0.10	0.00	35.60	2.00	0.00	0.00	0.10	0.00
35.70	1.33	0.00	0.00	0.10	0.00	35.80	0.91	0.00	0.00	0.10	0.01
35.90	0.62	0.00	0.00	0.10	0.05	36.00	0.43	0.00	0.00	0.10	0.08
36.10	0.31	0.69	0.33	0.10	0.09	36.20	0.27	0.73	0.31	0.10	0.10
36.30	0.26	0.74	0.30	0.10	0.10	36.40	0.28	0.72	0.31	0.10	0.10
36.50	0.31	0.69	0.33	0.10	0.09	36.60	0.33	0.67	0.34	0.10	0.09
36.70	0.35	0.65	0.35	0.10	0.09	36.80	0.40	0.00	0.00	0.10	0.08
36.90	0.45	0.00	0.00	0.10	0.07	37.00	0.50	0.00	0.00	0.10	0.07
37.10	0.51	0.00	0.00	0.10	0.06	37.20	0.53	0.00	0.00	0.10	0.06
37.30	0.56	0.00	0.00	0.10	0.06	37.40	0.57	0.00	0.00	0.10	0.06
37.50	0.58	0.00	0.00	0.10	0.06	37.60	0.59	0.00	0.00	0.10	0.05
37.70	0.61	0.00	0.00	0.10	0.05	37.80	0.65	0.00	0.00	0.10	0.05
37.90	0.68	0.00	0.00	0.10	0.04	38.00	0.74	0.00	0.00	0.10	0.03
38.10	0.84	0.00	0.00	0.10	0.02	38.20	0.90	0.00	0.00	0.10	0.01
38.30	0.97	0.00	0.00	0.10	0.00	38.40	1.03	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data ::

Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
38.50	1.01	0.00	0.00	0.10	0.00	38.60	0.93	0.00	0.00	0.10	0.01
38.70	0.88	0.00	0.00	0.10	0.01	38.80	0.85	0.00	0.00	0.10	0.02
38.90	0.80	0.00	0.00	0.10	0.03	39.00	0.74	0.00	0.00	0.10	0.03
39.10	0.73	0.00	0.00	0.10	0.03	39.20	0.75	0.00	0.00	0.10	0.03
39.30	0.76	0.00	0.00	0.10	0.03	39.40	0.72	0.00	0.00	0.10	0.03
39.50	0.69	0.00	0.00	0.10	0.04	39.60	0.66	0.00	0.00	0.10	0.04
39.70	0.59	0.00	0.00	0.10	0.05	39.80	0.64	0.00	0.00	0.10	0.04
39.90	0.77	0.00	0.00	0.10	0.03	40.00	0.83	0.00	0.00	0.10	0.02
40.10	0.82	0.00	0.00	0.10	0.02	40.20	0.91	0.00	0.00	0.10	0.01
40.30	1.04	0.00	0.00	0.10	0.00	40.40	1.13	0.00	0.00	0.10	0.00
40.50	1.18	0.00	0.00	0.10	0.00	40.60	1.20	0.00	0.00	0.10	0.00
40.70	1.12	0.00	0.00	0.10	0.00	40.80	1.08	0.00	0.00	0.10	0.00
40.90	1.10	0.00	0.00	0.10	0.00	41.00	1.19	0.00	0.00	0.10	0.00
41.10	1.40	0.00	0.00	0.10	0.00	41.20	1.67	0.00	0.00	0.10	0.00
41.30	1.96	0.00	0.00	0.10	0.00	41.40	2.00	0.00	0.00	0.10	0.00
41.50	2.00	0.00	0.00	0.10	0.00	41.60	1.77	0.00	0.00	0.10	0.00
41.70	1.62	0.00	0.00	0.10	0.00	41.80	1.82	0.00	0.00	0.10	0.00
41.90	2.00	0.00	0.00	0.10	0.00	42.00	2.00	0.00	0.00	0.10	0.00
42.10	2.00	0.00	0.00	0.10	0.00	42.20	2.00	0.00	0.00	0.10	0.00
42.30	2.00	0.00	0.00	0.10	0.00	42.40	2.00	0.00	0.00	0.10	0.00
42.50	2.00	0.00	0.00	0.10	0.00	42.60	2.00	0.00	0.00	0.10	0.00
42.70	2.00	0.00	0.00	0.10	0.00	42.80	2.00	0.00	0.00	0.10	0.00
42.90	2.00	0.00	0.00	0.10	0.00	43.00	2.00	0.00	0.00	0.10	0.00
43.10	2.00	0.00	0.00	0.10	0.00	43.20	2.00	0.00	0.00	0.10	0.00
43.30	2.00	0.00	0.00	0.10	0.00	43.40	2.00	0.00	0.00	0.10	0.00
43.50	2.00	0.00	0.00	0.10	0.00	43.60	2.00	0.00	0.00	0.10	0.00
43.70	2.00	0.00	0.00	0.10	0.00	43.80	2.00	0.00	0.00	0.10	0.00
43.90	2.00	0.00	0.00	0.10	0.00	44.00	2.00	0.00	0.00	0.10	0.00
44.10	2.00	0.00	0.00	0.10	0.00	44.20	2.00	0.00	0.00	0.10	0.00
44.30	2.00	0.00	0.00	0.10	0.00	44.40	2.00	0.00	0.00	0.10	0.00
44.50	2.00	0.00	0.00	0.10	0.00	44.60	2.00	0.00	0.00	0.10	0.00
44.70	2.00	0.00	0.00	0.10	0.00	44.80	2.00	0.00	0.00	0.10	0.00
44.90	2.00	0.00	0.00	0.10	0.00	45.00	2.00	0.00	0.00	0.10	0.00
45.10	2.00	0.00	0.00	0.10	0.00	45.20	2.00	0.00	0.00	0.10	0.00
45.30	2.00	0.00	0.00	0.10	0.00	45.40	2.00	0.00	0.00	0.10	0.00
45.50	2.00	0.00	0.00	0.10	0.00	45.60	2.00	0.00	0.00	0.10	0.00
45.70	2.00	0.00	0.00	0.10	0.00	45.80	2.00	0.00	0.00	0.10	0.00
45.90	2.00	0.00	0.00	0.10	0.00	46.00	2.00	0.00	0.00	0.10	0.00
46.10	2.00	0.00	0.00	0.10	0.00	46.20	2.00	0.00	0.00	0.10	0.00
46.30	2.00	0.00	0.00	0.10	0.00	46.40	2.00	0.00	0.00	0.10	0.00
46.50	2.00	0.00	0.00	0.10	0.00	46.60	1.73	0.00	0.00	0.10	0.00
46.70	2.00	0.00	0.00	0.10	0.00	46.80	2.00	0.00	0.00	0.10	0.00
46.90	2.00	0.00	0.00	0.10	0.00	47.00	2.00	0.00	0.00	0.10	0.00
47.10	2.00	0.00	0.00	0.10	0.00	47.20	2.00	0.00	0.00	0.10	0.00
47.30	2.00	0.00	0.00	0.10	0.00	47.40	2.00	0.00	0.00	0.10	0.00
47.50	2.00	0.00	0.00	0.10	0.00	47.60	2.00	0.00	0.00	0.10	0.00
47.70	0.81	0.00	0.00	0.10	0.02	47.80	0.56	0.00	0.00	0.10	0.04
47.90	0.42	0.00	0.00	0.10	0.05	48.00	2.00	0.00	0.00	0.10	0.00

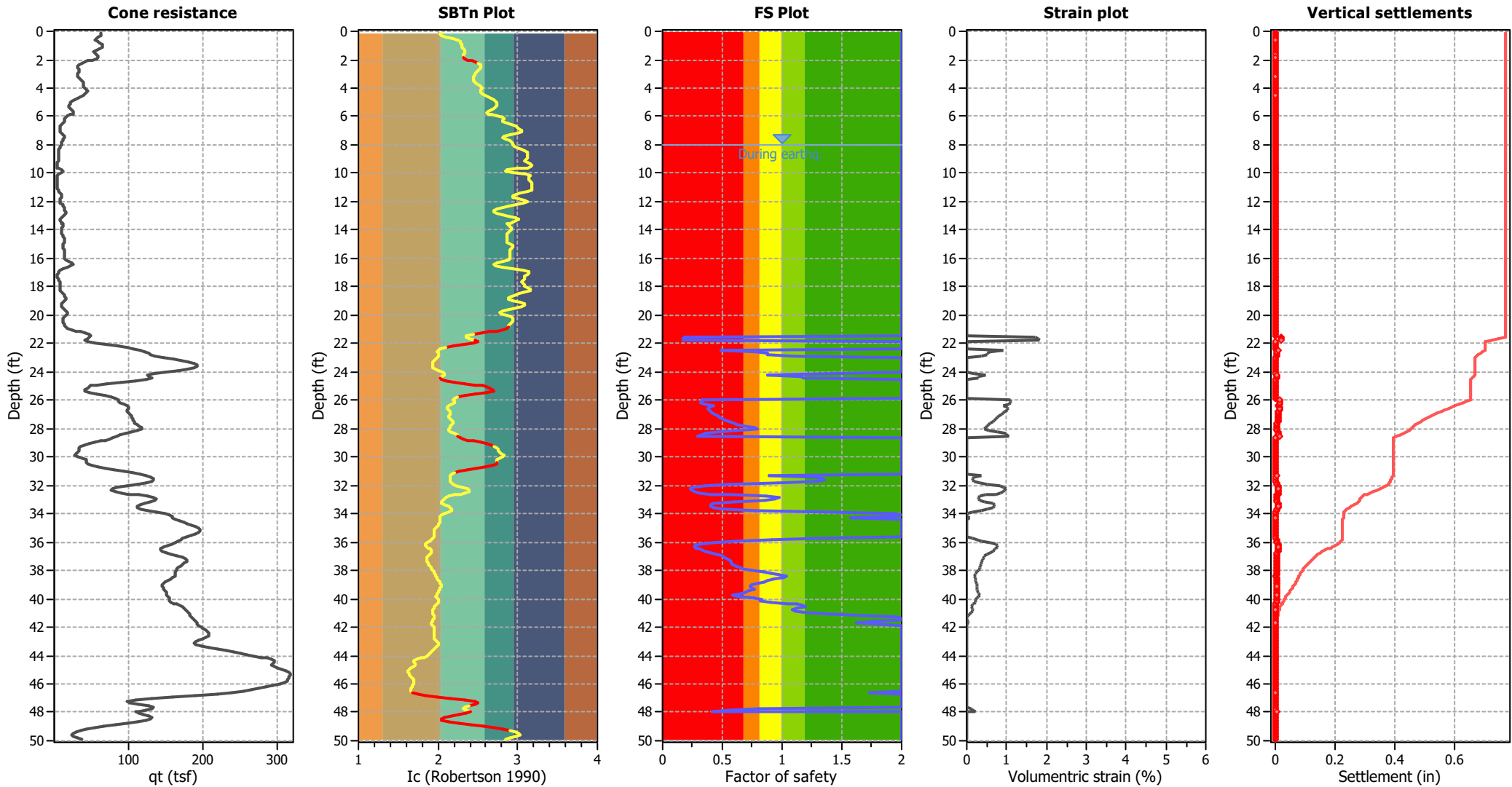
:: Liquefaction Potential Index calculation data ::

Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
48.10	2.00	0.00	0.00	0.10	0.00	48.20	2.00	0.00	0.00	0.10	0.00
48.30	2.00	0.00	0.00	0.10	0.00	48.40	2.00	0.00	0.00	0.10	0.00
48.50	2.00	0.00	0.00	0.10	0.00	48.60	2.00	0.00	0.00	0.10	0.00
48.70	2.00	0.00	0.00	0.10	0.00	48.80	2.00	0.00	0.00	0.10	0.00
48.90	2.00	0.00	0.00	0.10	0.00	49.00	2.00	0.00	0.00	0.10	0.00
49.10	2.00	0.00	0.00	0.10	0.00	49.20	2.00	0.00	0.00	0.10	0.00
49.30	2.00	0.00	0.00	0.10	0.00	49.40	2.00	0.00	0.00	0.10	0.00
49.50	2.00	0.00	0.00	0.10	0.00	49.60	2.00	0.00	0.00	0.10	0.00
49.70	2.00	0.00	0.00	0.10	0.00	49.80	2.00	0.00	0.00	0.10	0.00
49.90	2.00	0.00	0.00	0.10	0.00						

Overall liquefaction potential: 6.84LPI_{ISH} > 5.0 - Liquefaction manifestation is expected**Abbreviations**

FS: Calculated factor of safety for test point
d_z: Layer thickness (ft)
LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

- q_c : Total cone resistance (cone resistance q_c corrected for pore water effects)
- I_c : Soil Behaviour Type Index
- FS: Calculated Factor of Safety against liquefaction
- Volumetric strain: Post-liquefaction volumetric strain

:: Post-earthquake settlement of dry sands ::												
Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
0.10	2.05	101.72	1.35	137.45	29	761	0.55	0.000	0.00	13.69	0.00	0.000
0.20	2.03	103.00	1.33	137.21	29	752	0.55	0.001	0.00	13.69	0.00	0.000
0.30	2.04	102.13	1.34	136.92	29	754	0.55	0.001	0.00	13.69	0.00	0.000
0.40	2.11	97.01	1.43	138.53	30	782	0.55	0.002	0.00	13.69	0.00	0.000
0.50	2.18	91.83	1.57	143.86	32	813	0.55	0.002	0.00	13.69	0.00	0.000
0.60	2.24	90.76	1.72	155.83	36	865	0.55	0.002	0.00	13.69	0.00	0.000
0.70	2.27	94.78	1.82	172.72	40	942	0.54	0.003	0.00	13.69	0.00	0.000
0.80	2.29	100.24	1.87	187.89	44	1016	0.54	0.003	0.00	13.69	0.00	0.000
0.90	2.29	103.81	1.90	196.86	46	1060	0.54	0.003	0.00	13.69	0.00	0.000
1.00	2.30	105.26	1.91	200.89	47	1079	0.54	0.003	0.00	13.69	0.00	0.000
1.10	2.30	103.66	1.94	200.71	47	1073	0.54	0.004	0.00	13.69	0.00	0.000
1.20	2.32	99.10	1.99	196.80	47	1042	0.54	0.004	0.00	13.69	0.00	0.000
1.30	2.33	91.84	2.05	188.28	45	985	0.54	0.005	0.00	13.69	0.00	0.000
1.40	2.34	87.54	2.07	181.41	43	945	0.55	0.006	0.00	13.69	0.00	0.000
1.50	2.33	88.19	2.04	180.24	43	944	0.55	0.006	0.00	13.69	0.00	0.000
1.60	2.32	91.70	2.01	183.95	44	971	0.54	0.006	0.00	13.69	0.00	0.000
1.70	2.31	95.77	1.98	189.55	45	1005	0.54	0.007	0.00	13.69	0.00	0.000
1.80	2.32	97.17	1.99	193.62	46	1024	0.54	0.007	0.00	13.69	0.00	0.000
1.90	2.34	92.86	2.08	193.53	0	0	0.54	0.000	0.00	13.69	0.00	0.000
2.00	2.38	84.46	2.26	191.05	0	0	0.55	0.000	0.00	13.69	0.00	0.000
2.10	2.43	74.82	2.52	188.29	0	0	0.55	0.000	0.00	13.69	0.00	0.000
2.20	2.47	67.48	2.75	185.75	0	0	0.55	0.000	0.00	13.69	0.00	0.000
2.30	2.50	60.39	2.99	180.85	0	0	0.56	0.000	0.00	13.69	0.00	0.000
2.40	2.53	53.92	3.22	173.85	0	0	0.56	0.000	0.00	13.69	0.00	0.000
2.50	2.55	50.84	3.31	168.29	44	715	0.56	0.019	0.01	13.69	0.01	0.000
2.60	2.53	51.29	3.23	165.52	43	712	0.56	0.020	0.01	13.69	0.01	0.000
2.70	2.51	53.45	3.07	164.30	43	722	0.56	0.021	0.01	13.69	0.01	0.000
2.80	2.49	55.13	2.93	161.55	41	726	0.56	0.022	0.01	13.69	0.01	0.000
2.90	2.48	54.33	2.86	155.19	40	705	0.56	0.024	0.01	13.69	0.01	0.000
3.00	2.47	53.07	2.77	147.10	37	677	0.56	0.028	0.01	13.69	0.01	0.000
3.10	2.46	51.89	2.70	140.30	35	653	0.56	0.032	0.02	13.69	0.01	0.000
3.20	2.45	52.98	2.64	139.73	35	658	0.56	0.034	0.02	13.69	0.02	0.000
3.30	2.44	55.48	2.60	144.39	36	684	0.56	0.032	0.02	13.69	0.01	0.000
3.40	2.44	59.18	2.58	152.88	38	726	0.55	0.029	0.01	13.69	0.01	0.000
3.50	2.44	62.55	2.61	163.10	41	772	0.55	0.026	0.01	13.69	0.01	0.000
3.60	2.46	64.38	2.71	174.58	44	812	0.55	0.025	0.01	13.69	0.01	0.000
3.70	2.49	64.32	2.91	187.35	48	844	0.55	0.024	0.01	13.69	0.01	0.000
3.80	2.52	64.03	3.14	200.75	52	875	0.55	0.023	0.01	13.69	0.01	0.000
3.90	2.54	64.90	3.29	213.59	56	910	0.55	0.022	0.01	13.69	0.01	0.000
4.00	2.55	67.60	3.31	223.86	59	951	0.55	0.021	0.01	13.69	0.01	0.000
4.10	2.54	70.83	3.24	229.20	60	984	0.55	0.020	0.01	13.69	0.00	0.000
4.20	2.53	72.48	3.19	230.87	60	999	0.55	0.020	0.01	13.69	0.00	0.000
4.30	2.54	71.60	3.24	231.77	61	995	0.55	0.021	0.01	13.69	0.00	0.000
4.40	2.56	68.28	3.43	234.00	62	979	0.55	0.022	0.01	13.69	0.01	0.000
4.50	2.60	63.12	3.72	234.82	63	947	0.55	0.025	0.01	13.69	0.01	0.000
4.60	2.63	56.77	4.07	230.75	0	0	0.55	0.000	0.00	0.00	0.00	0.000
4.70	2.67	50.03	4.43	221.54	0	0	0.55	0.000	0.00	0.00	0.00	0.000
4.80	2.70	44.58	4.72	210.32	0	0	0.56	0.000	0.00	0.00	0.00	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
4.90	2.72	40.26	4.93	198.47	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.00	2.73	37.06	5.04	186.61	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.10	2.73	34.43	5.07	174.55	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.20	2.73	32.84	5.03	165.17	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.30	2.72	32.86	4.92	161.80	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.40	2.70	34.85	4.70	163.71	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.50	2.67	38.22	4.36	166.60	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.60	2.63	41.26	4.04	166.71	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.70	2.61	42.26	3.88	163.99	0	0	0.55	0.000	0.00	0.00	0.00	0.000
5.80	2.62	40.95	3.95	161.57	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.90	2.67	36.39	4.37	159.08	0	0	0.56	0.000	0.00	0.00	0.00	0.000
6.00	2.74	30.13	5.18	155.98	0	0	0.56	0.000	0.00	0.00	0.00	0.000
6.10	2.81	25.63	5.98	153.12	0	0	0.56	0.000	0.00	0.00	0.00	0.000
6.20	2.82	24.36	6.14	149.69	0	0	0.56	0.000	0.00	0.00	0.00	0.000
6.30	2.80	24.53	5.91	145.08	0	0	0.56	0.000	0.00	0.00	0.00	0.000
6.40	2.81	22.79	6.03	137.48	0	0	0.56	0.000	0.00	0.00	0.00	0.000
6.50	2.86	19.64	6.66	130.78	0	0	0.56	0.000	0.00	0.00	0.00	0.000
6.60	2.93	16.84	7.59	127.72	0	0	0.57	0.000	0.00	0.00	0.00	0.000
6.70	2.97	15.21	8.35	127.08	0	0	0.57	0.000	0.00	0.00	0.00	0.000
6.80	3.00	14.55	8.72	126.87	0	0	0.57	0.000	0.00	0.00	0.00	0.000
6.90	3.02	13.89	9.07	126.03	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.00	3.04	13.33	9.51	126.79	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.10	3.04	13.84	9.54	131.97	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.20	2.99	16.37	8.56	140.20	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.30	2.90	20.24	7.17	145.11	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.40	2.83	22.96	6.21	142.66	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.50	2.81	22.99	5.95	136.71	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.60	2.84	20.69	6.39	132.11	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.70	2.90	18.44	7.15	131.87	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.80	2.93	17.36	7.61	132.07	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.90	2.93	16.70	7.72	129.04	0	0	0.57	0.000	0.00	0.00	0.00	0.000

Total estimated settlement: 0.00**Abbreviations**

Q_{tn}: Normalized cone resistance
 K_c: Fines correction factor
 Q_{tn,cs}: Equivalent clean sand normalized cone resistance
 G_{max}: Small strain shear modulus
 CSR: Soil cyclic stress ratio
 γ: Cyclic shear strain
 e_{vol(15)}: Volumetric strain after 15 cycles
 N_c: Equivalent number of cycles
 e_v: Volumetric strain
 Settle.: Calculated settlement

:: Post-earthquake settlement due to soil liquefaction ::

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
8.00	15.20	2.00	0.00	0.85	0.00	8.10	13.86	2.00	0.00	0.85	0.00
8.20	12.49	2.00	0.00	0.85	0.00	8.30	10.94	2.00	0.00	0.85	0.00
8.40	9.23	2.00	0.00	0.85	0.00	8.50	9.13	2.00	0.00	0.85	0.00
8.60	9.42	2.00	0.00	0.84	0.00	8.70	9.40	2.00	0.00	0.84	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
8.80	9.28	2.00	0.00	0.84	0.00	8.90	9.07	2.00	0.00	0.84	0.00
9.00	9.24	2.00	0.00	0.84	0.00	9.10	9.31	2.00	0.00	0.83	0.00
9.20	8.16	2.00	0.00	0.83	0.00	9.30	7.00	2.00	0.00	0.83	0.00
9.40	7.22	2.00	0.00	0.83	0.00	9.50	8.20	2.00	0.00	0.83	0.00
9.60	8.64	2.00	0.00	0.83	0.00	9.70	8.76	2.00	0.00	0.82	0.00
9.80	15.87	2.00	0.00	0.82	0.00	9.90	22.63	2.00	0.00	0.82	0.00
10.00	13.37	2.00	0.00	0.82	0.00	10.10	6.86	2.00	0.00	0.82	0.00
10.20	7.33	2.00	0.00	0.81	0.00	10.30	8.29	2.00	0.00	0.81	0.00
10.40	8.48	2.00	0.00	0.81	0.00	10.50	8.46	2.00	0.00	0.81	0.00
10.60	8.44	2.00	0.00	0.81	0.00	10.70	8.42	2.00	0.00	0.81	0.00
10.80	8.40	2.00	0.00	0.80	0.00	10.90	8.38	2.00	0.00	0.80	0.00
11.00	8.36	2.00	0.00	0.80	0.00	11.10	8.34	2.00	0.00	0.80	0.00
11.20	8.41	2.00	0.00	0.80	0.00	11.30	9.98	2.00	0.00	0.79	0.00
11.40	13.72	2.00	0.00	0.79	0.00	11.50	15.43	2.00	0.00	0.79	0.00
11.60	15.39	2.00	0.00	0.79	0.00	11.70	14.61	2.00	0.00	0.79	0.00
11.80	12.09	2.00	0.00	0.79	0.00	11.90	10.41	2.00	0.00	0.78	0.00
12.00	10.24	2.00	0.00	0.78	0.00	12.10	12.93	2.00	0.00	0.78	0.00
12.20	16.70	2.00	0.00	0.78	0.00	12.30	18.88	2.00	0.00	0.78	0.00
12.40	19.25	2.00	0.00	0.77	0.00	12.50	18.93	2.00	0.00	0.77	0.00
12.60	19.87	2.00	0.00	0.77	0.00	12.70	22.87	2.00	0.00	0.77	0.00
12.80	22.77	2.00	0.00	0.77	0.00	12.90	20.85	2.00	0.00	0.77	0.00
13.00	17.11	2.00	0.00	0.76	0.00	13.10	13.49	2.00	0.00	0.76	0.00
13.20	12.55	2.00	0.00	0.76	0.00	13.30	12.52	2.00	0.00	0.76	0.00
13.40	13.13	2.00	0.00	0.76	0.00	13.50	15.29	2.00	0.00	0.75	0.00
13.60	16.65	2.00	0.00	0.75	0.00	13.70	16.42	2.00	0.00	0.75	0.00
13.80	16.18	2.00	0.00	0.75	0.00	13.90	14.98	2.00	0.00	0.75	0.00
14.00	14.33	2.00	0.00	0.75	0.00	14.10	14.30	2.00	0.00	0.74	0.00
14.20	14.27	2.00	0.00	0.74	0.00	14.30	14.26	2.00	0.00	0.74	0.00
14.40	15.34	2.00	0.00	0.74	0.00	14.50	16.45	2.00	0.00	0.74	0.00
14.60	17.57	2.00	0.00	0.73	0.00	14.70	18.68	2.00	0.00	0.73	0.00
14.80	19.77	2.00	0.00	0.73	0.00	14.90	18.93	2.00	0.00	0.73	0.00
15.00	16.84	2.00	0.00	0.73	0.00	15.10	15.93	2.00	0.00	0.73	0.00
15.20	15.89	2.00	0.00	0.72	0.00	15.30	16.45	2.00	0.00	0.72	0.00
15.40	18.30	2.00	0.00	0.72	0.00	15.50	19.55	2.00	0.00	0.72	0.00
15.60	17.19	2.00	0.00	0.72	0.00	15.70	17.61	2.00	0.00	0.71	0.00
15.80	19.66	2.00	0.00	0.71	0.00	15.90	19.40	2.00	0.00	0.71	0.00
16.00	18.16	2.00	0.00	0.71	0.00	16.10	19.09	2.00	0.00	0.71	0.00
16.20	25.22	2.00	0.00	0.71	0.00	16.30	31.49	2.00	0.00	0.70	0.00
16.40	32.20	2.00	0.00	0.70	0.00	16.50	29.19	2.00	0.00	0.70	0.00
16.60	22.38	2.00	0.00	0.70	0.00	16.70	14.51	2.00	0.00	0.70	0.00
16.80	9.96	2.00	0.00	0.69	0.00	16.90	7.93	2.00	0.00	0.69	0.00
17.00	7.26	2.00	0.00	0.69	0.00	17.10	7.25	2.00	0.00	0.69	0.00
17.20	7.24	2.00	0.00	0.69	0.00	17.30	7.23	2.00	0.00	0.69	0.00
17.40	6.55	2.00	0.00	0.68	0.00	17.50	7.27	2.00	0.00	0.68	0.00
17.60	8.82	2.00	0.00	0.68	0.00	17.70	9.98	2.00	0.00	0.68	0.00
17.80	10.18	2.00	0.00	0.68	0.00	17.90	9.97	2.00	0.00	0.67	0.00
18.00	9.95	2.00	0.00	0.67	0.00	18.10	9.93	2.00	0.00	0.67	0.00
18.20	9.22	2.00	0.00	0.67	0.00	18.30	9.78	2.00	0.00	0.67	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
18.40	12.67	2.00	0.00	0.67	0.00	18.50	15.95	2.00	0.00	0.66	0.00
18.60	16.93	2.00	0.00	0.66	0.00	18.70	16.68	2.00	0.00	0.66	0.00
18.80	20.27	2.00	0.00	0.66	0.00	18.90	20.72	2.00	0.00	0.66	0.00
19.00	17.42	2.00	0.00	0.65	0.00	19.10	14.38	2.00	0.00	0.65	0.00
19.20	11.54	2.00	0.00	0.65	0.00	19.30	11.06	2.00	0.00	0.65	0.00
19.40	13.16	2.00	0.00	0.65	0.00	19.50	15.32	2.00	0.00	0.65	0.00
19.60	17.56	2.00	0.00	0.64	0.00	19.70	20.77	2.00	0.00	0.64	0.00
19.80	22.13	2.00	0.00	0.64	0.00	19.90	22.85	2.00	0.00	0.64	0.00
20.00	18.92	2.00	0.00	0.64	0.00	20.10	14.24	2.00	0.00	0.63	0.00
20.20	14.21	2.00	0.00	0.63	0.00	20.30	13.88	2.00	0.00	0.63	0.00
20.40	13.94	2.00	0.00	0.63	0.00	20.50	14.69	2.00	0.00	0.63	0.00
20.60	16.05	2.00	0.00	0.63	0.00	20.70	17.39	2.00	0.00	0.62	0.00
20.80	17.65	2.00	0.00	0.62	0.00	20.90	19.69	2.00	0.00	0.62	0.00
21.00	25.25	2.00	0.00	0.62	0.00	21.10	33.88	2.00	0.00	0.62	0.00
21.20	40.19	2.00	0.00	0.61	0.00	21.30	109.81	2.00	0.00	0.61	0.00
21.40	114.73	2.00	0.00	0.61	0.00	21.50	115.47	2.00	0.00	0.61	0.00
21.60	112.48	0.18	1.73	0.61	0.02	21.70	108.91	0.18	1.78	0.61	0.02
21.80	106.25	0.17	1.82	0.60	0.02	21.90	106.90	2.00	0.00	0.60	0.00
22.00	120.67	2.00	0.00	0.60	0.00	22.10	140.41	2.00	0.00	0.60	0.00
22.20	152.80	2.00	0.00	0.60	0.00	22.30	161.56	2.00	0.00	0.59	0.00
22.40	162.06	2.00	0.00	0.59	0.00	22.50	162.67	0.49	0.93	0.59	0.01
22.60	176.48	0.78	0.57	0.59	0.01	22.70	179.43	0.88	0.51	0.59	0.01
22.80	179.48	0.88	0.51	0.59	0.01	22.90	184.65	1.09	0.35	0.58	0.00
23.00	199.16	2.00	0.00	0.58	0.00	23.10	208.31	2.00	0.00	0.58	0.00
23.20	216.02	2.00	0.00	0.58	0.00	23.30	223.40	2.00	0.00	0.58	0.00
23.40	229.69	2.00	0.00	0.57	0.00	23.50	234.07	2.00	0.00	0.57	0.00
23.60	234.51	2.00	0.00	0.57	0.00	23.70	231.69	2.00	0.00	0.57	0.00
23.80	227.00	2.00	0.00	0.57	0.00	23.90	222.42	2.00	0.00	0.57	0.00
24.00	214.21	2.00	0.00	0.56	0.00	24.10	189.75	1.36	0.19	0.56	0.00
24.20	179.83	0.87	0.48	0.56	0.01	24.30	186.32	1.16	0.29	0.56	0.00
24.40	186.86	1.19	0.28	0.56	0.00	24.50	182.39	2.00	0.00	0.55	0.00
24.60	171.93	2.00	0.00	0.55	0.00	24.70	155.30	2.00	0.00	0.55	0.00
24.80	135.41	2.00	0.00	0.55	0.00	24.90	120.09	2.00	0.00	0.55	0.00
25.00	112.68	2.00	0.00	0.55	0.00	25.10	46.42	2.00	0.00	0.54	0.00
25.20	48.60	2.00	0.00	0.54	0.00	25.30	41.26	2.00	0.00	0.54	0.00
25.40	37.86	2.00	0.00	0.54	0.00	25.50	45.81	2.00	0.00	0.54	0.00
25.60	124.43	2.00	0.00	0.53	0.00	25.70	134.89	2.00	0.00	0.53	0.00
25.80	140.05	2.00	0.00	0.53	0.00	25.90	146.14	2.00	0.00	0.53	0.00
26.00	148.62	0.32	1.11	0.53	0.01	26.10	149.25	0.33	1.10	0.53	0.01
26.20	148.12	0.32	1.10	0.52	0.01	26.30	153.15	0.36	1.06	0.52	0.01
26.40	159.42	0.42	0.92	0.52	0.01	26.50	156.08	0.39	1.02	0.52	0.01
26.60	155.34	0.38	1.03	0.52	0.01	26.70	155.94	0.39	1.02	0.51	0.01
26.80	157.41	0.40	0.97	0.51	0.01	26.90	158.64	0.41	0.92	0.51	0.01
27.00	160.51	0.44	0.86	0.51	0.01	27.10	162.80	0.47	0.80	0.51	0.01
27.20	163.45	0.47	0.78	0.51	0.01	27.30	164.94	0.50	0.73	0.50	0.01
27.40	166.69	0.52	0.69	0.50	0.01	27.50	168.58	0.56	0.64	0.50	0.01
27.60	170.57	0.60	0.60	0.50	0.01	27.70	172.03	0.63	0.57	0.50	0.01
27.80	174.37	0.68	0.52	0.49	0.01	27.90	177.58	0.77	0.46	0.49	0.01

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
28.00	178.35	0.79	0.45	0.49	0.01	28.10	171.93	0.62	0.56	0.49	0.01
28.20	163.22	0.47	0.75	0.49	0.01	28.30	152.81	0.35	0.99	0.49	0.01
28.40	149.82	0.33	1.01	0.48	0.01	28.50	144.18	0.29	1.05	0.48	0.01
28.60	139.11	2.00	0.00	0.48	0.00	28.70	135.98	2.00	0.00	0.48	0.00
28.80	131.03	2.00	0.00	0.48	0.00	28.90	126.81	2.00	0.00	0.47	0.00
29.00	116.65	2.00	0.00	0.47	0.00	29.10	43.95	2.00	0.00	0.47	0.00
29.20	39.47	2.00	0.00	0.47	0.00	29.30	34.20	2.00	0.00	0.47	0.00
29.40	31.75	2.00	0.00	0.47	0.00	29.50	32.26	2.00	0.00	0.46	0.00
29.60	32.24	2.00	0.00	0.46	0.00	29.70	31.21	2.00	0.00	0.46	0.00
29.80	26.82	2.00	0.00	0.46	0.00	29.90	25.44	2.00	0.00	0.46	0.00
30.00	27.62	2.00	0.00	0.45	0.00	30.10	37.51	2.00	0.00	0.45	0.00
30.20	41.61	2.00	0.00	0.45	0.00	30.30	41.77	2.00	0.00	0.45	0.00
30.40	41.37	2.00	0.00	0.45	0.00	30.50	40.68	2.00	0.00	0.45	0.00
30.60	46.73	2.00	0.00	0.44	0.00	30.70	122.85	2.00	0.00	0.44	0.00
30.80	130.66	2.00	0.00	0.44	0.00	30.90	140.70	2.00	0.00	0.44	0.00
31.00	155.02	2.00	0.00	0.44	0.00	31.10	165.50	2.00	0.00	0.43	0.00
31.20	172.47	2.00	0.00	0.43	0.00	31.30	181.63	0.88	0.35	0.43	0.00
31.40	189.82	1.27	0.18	0.43	0.00	31.50	190.91	1.34	0.15	0.43	0.00
31.60	191.20	1.36	0.15	0.43	0.00	31.70	189.90	1.28	0.17	0.42	0.00
31.80	183.79	0.97	0.31	0.42	0.00	31.90	169.82	0.56	0.52	0.42	0.01
32.00	153.75	0.35	0.84	0.42	0.01	32.10	140.40	0.26	0.93	0.42	0.01
32.20	134.55	0.23	0.97	0.41	0.01	32.30	136.61	0.24	0.95	0.41	0.01
32.40	141.29	0.27	0.91	0.41	0.01	32.50	148.42	0.31	0.86	0.41	0.01
32.60	158.46	0.40	0.74	0.41	0.01	32.70	170.69	0.58	0.48	0.41	0.01
32.80	181.20	0.86	0.33	0.40	0.00	32.90	184.13	0.97	0.30	0.40	0.00
33.00	183.16	0.93	0.31	0.40	0.00	33.10	180.98	0.85	0.33	0.40	0.00
33.20	172.11	0.61	0.45	0.40	0.01	33.30	161.52	0.43	0.65	0.39	0.01
33.40	159.56	0.41	0.69	0.39	0.01	33.50	159.07	0.40	0.70	0.39	0.01
33.60	161.16	0.43	0.65	0.39	0.01	33.70	167.51	0.52	0.52	0.39	0.01
33.80	178.45	0.77	0.35	0.39	0.00	33.90	191.47	1.36	0.13	0.38	0.00
34.00	198.37	1.93	0.01	0.38	0.00	34.10	200.90	2.00	0.00	0.38	0.00
34.20	198.38	1.93	0.01	0.38	0.00	34.30	194.43	1.57	0.08	0.38	0.00
34.40	199.19	2.00	0.00	0.37	0.00	34.50	211.85	2.00	0.00	0.37	0.00
34.60	215.13	2.00	0.00	0.37	0.00	34.70	217.26	2.00	0.00	0.37	0.00
34.80	220.61	2.00	0.00	0.37	0.00	34.90	222.89	2.00	0.00	0.37	0.00
35.00	223.01	2.00	0.00	0.36	0.00	35.10	222.09	2.00	0.00	0.36	0.00
35.20	220.63	2.00	0.00	0.36	0.00	35.30	218.37	2.00	0.00	0.36	0.00
35.40	214.43	2.00	0.00	0.36	0.00	35.50	208.21	2.00	0.00	0.35	0.00
35.60	200.20	2.00	0.00	0.35	0.00	35.70	191.18	1.33	0.13	0.35	0.00
35.80	182.95	0.91	0.27	0.35	0.00	35.90	173.09	0.62	0.38	0.35	0.00
36.00	161.42	0.43	0.57	0.35	0.01	36.10	149.73	0.31	0.71	0.34	0.01
36.20	142.57	0.27	0.75	0.34	0.01	36.30	141.51	0.26	0.75	0.34	0.01
36.40	144.67	0.28	0.73	0.34	0.01	36.50	148.80	0.31	0.70	0.34	0.01
36.60	151.45	0.33	0.69	0.33	0.01	36.70	154.46	0.35	0.67	0.33	0.01
36.80	158.97	0.40	0.59	0.33	0.01	36.90	163.04	0.45	0.51	0.33	0.01
37.00	166.64	0.50	0.45	0.33	0.01	37.10	167.55	0.51	0.43	0.33	0.01
37.20	168.88	0.53	0.41	0.32	0.00	37.30	170.38	0.56	0.39	0.32	0.00
37.40	170.91	0.57	0.38	0.32	0.00	37.50	171.09	0.58	0.37	0.32	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
37.60	171.71	0.59	0.36	0.32	0.00	37.70	173.01	0.61	0.35	0.31	0.00
37.80	174.46	0.65	0.33	0.31	0.00	37.90	175.61	0.68	0.31	0.31	0.00
38.00	178.13	0.74	0.28	0.31	0.00	38.10	181.14	0.84	0.25	0.31	0.00
38.20	182.94	0.90	0.24	0.31	0.00	38.30	184.59	0.97	0.22	0.30	0.00
38.40	186.06	1.03	0.20	0.30	0.00	38.50	185.57	1.01	0.21	0.30	0.00
38.60	183.66	0.93	0.22	0.30	0.00	38.70	182.45	0.88	0.23	0.30	0.00
38.80	181.66	0.85	0.24	0.29	0.00	38.90	179.90	0.80	0.25	0.29	0.00
39.00	178.23	0.74	0.27	0.29	0.00	39.10	177.91	0.73	0.27	0.29	0.00
39.20	178.32	0.75	0.26	0.29	0.00	39.30	178.92	0.76	0.25	0.29	0.00
39.40	177.47	0.72	0.27	0.28	0.00	39.50	176.38	0.69	0.28	0.28	0.00
39.60	175.26	0.66	0.28	0.28	0.00	39.70	172.05	0.59	0.32	0.28	0.00
39.80	174.19	0.64	0.29	0.28	0.00	39.90	179.13	0.77	0.24	0.27	0.00
40.00	181.17	0.83	0.22	0.27	0.00	40.10	180.69	0.82	0.23	0.27	0.00
40.20	183.19	0.91	0.21	0.27	0.00	40.30	186.38	1.04	0.17	0.27	0.00
40.40	188.14	1.13	0.15	0.27	0.00	40.50	189.04	1.18	0.13	0.26	0.00
40.60	189.44	1.20	0.13	0.26	0.00	40.70	187.95	1.12	0.15	0.26	0.00
40.80	187.24	1.08	0.16	0.26	0.00	40.90	187.70	1.10	0.15	0.26	0.00
41.00	189.40	1.19	0.12	0.25	0.00	41.10	192.79	1.40	0.08	0.25	0.00
41.20	196.25	1.67	0.04	0.25	0.00	41.30	199.28	1.96	0.00	0.25	0.00
41.40	201.29	2.00	0.00	0.25	0.00	41.50	200.24	2.00	0.00	0.25	0.00
41.60	197.39	1.77	0.02	0.24	0.00	41.70	195.77	1.62	0.04	0.24	0.00
41.80	197.92	1.82	0.02	0.24	0.00	41.90	203.42	2.00	0.00	0.24	0.00
42.00	209.30	2.00	0.00	0.24	0.00	42.10	214.75	2.00	0.00	0.23	0.00
42.20	219.10	2.00	0.00	0.23	0.00	42.30	222.39	2.00	0.00	0.23	0.00
42.40	224.08	2.00	0.00	0.23	0.00	42.50	223.06	2.00	0.00	0.23	0.00
42.60	220.59	2.00	0.00	0.23	0.00	42.70	216.45	2.00	0.00	0.22	0.00
42.80	212.52	2.00	0.00	0.22	0.00	42.90	210.00	2.00	0.00	0.22	0.00
43.00	208.39	2.00	0.00	0.22	0.00	43.10	209.50	2.00	0.00	0.22	0.00
43.20	212.74	2.00	0.00	0.21	0.00	43.30	218.71	2.00	0.00	0.21	0.00
43.40	225.76	2.00	0.00	0.21	0.00	43.50	230.52	2.00	0.00	0.21	0.00
43.60	235.08	2.00	0.00	0.21	0.00	43.70	239.78	2.00	0.00	0.21	0.00
43.80	244.25	2.00	0.00	0.20	0.00	43.90	246.93	2.00	0.00	0.20	0.00
44.00	247.42	2.00	0.00	0.20	0.00	44.10	244.64	2.00	0.00	0.20	0.00
44.20	241.96	2.00	0.00	0.20	0.00	44.30	248.28	2.00	0.00	0.19	0.00
44.40	252.92	2.00	0.00	0.19	0.00	44.50	251.61	2.00	0.00	0.19	0.00
44.60	247.56	2.00	0.00	0.19	0.00	44.70	246.04	2.00	0.00	0.19	0.00
44.80	248.90	2.00	0.00	0.19	0.00	44.90	254.42	2.00	0.00	0.18	0.00
45.00	259.17	2.00	0.00	0.18	0.00	45.10	263.60	2.00	0.00	0.18	0.00
45.20	267.47	2.00	0.00	0.18	0.00	45.30	269.64	2.00	0.00	0.18	0.00
45.40	268.29	2.00	0.00	0.17	0.00	45.50	265.69	2.00	0.00	0.17	0.00
45.60	265.59	2.00	0.00	0.17	0.00	45.70	265.82	2.00	0.00	0.17	0.00
45.80	264.18	2.00	0.00	0.17	0.00	45.90	261.33	2.00	0.00	0.17	0.00
46.00	255.87	2.00	0.00	0.16	0.00	46.10	247.46	2.00	0.00	0.16	0.00
46.20	237.35	2.00	0.00	0.16	0.00	46.30	227.34	2.00	0.00	0.16	0.00
46.40	218.52	2.00	0.00	0.16	0.00	46.50	209.39	2.00	0.00	0.15	0.00
46.60	197.24	1.73	0.02	0.15	0.00	46.70	178.92	2.00	0.00	0.15	0.00
46.80	165.90	2.00	0.00	0.15	0.00	46.90	173.76	2.00	0.00	0.15	0.00
47.00	164.96	2.00	0.00	0.15	0.00	47.10	151.86	2.00	0.00	0.14	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
47.20	143.12	2.00	0.00	0.14	0.00	47.30	146.95	2.00	0.00	0.14	0.00
47.40	165.06	2.00	0.00	0.14	0.00	47.50	181.05	2.00	0.00	0.14	0.00
47.60	186.99	2.00	0.00	0.13	0.00	47.70	180.78	0.81	0.11	0.13	0.00
47.80	170.63	0.56	0.16	0.13	0.00	47.90	161.29	0.42	0.21	0.13	0.00
48.00	156.47	2.00	0.00	0.13	0.00	48.10	157.20	2.00	0.00	0.13	0.00
48.20	161.75	2.00	0.00	0.12	0.00	48.30	165.08	2.00	0.00	0.12	0.00
48.40	160.77	2.00	0.00	0.12	0.00	48.50	152.23	2.00	0.00	0.12	0.00
48.60	147.93	2.00	0.00	0.12	0.00	48.70	145.85	2.00	0.00	0.11	0.00
48.80	139.23	2.00	0.00	0.11	0.00	48.90	128.05	2.00	0.00	0.11	0.00
49.00	115.30	2.00	0.00	0.11	0.00	49.10	40.55	2.00	0.00	0.11	0.00
49.20	32.12	2.00	0.00	0.11	0.00	49.30	26.05	2.00	0.00	0.10	0.00
49.40	21.19	2.00	0.00	0.10	0.00	49.50	18.10	2.00	0.00	0.10	0.00
49.60	16.56	2.00	0.00	0.10	0.00	49.70	16.59	2.00	0.00	0.10	0.00
49.80	23.46	2.00	0.00	0.09	0.00	49.90	30.07	2.00	0.00	0.09	0.00

Total estimated settlement: 0.77**Abbreviations**

$Q_{tn,cs}$:	Equivalent clean sand normalized cone resistance
FS:	Factor of safety against liquefaction
e_v (%):	Post-liquefaction volumetric strain
DF:	e_v depth weighting factor
Settlement:	Calculated settlement

:: Strength loss calculation Idriss & Boulanger (2008) ::

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.10	63.32	101.72	1.35	137.45	2.05	0.17	0.83
0.20	64.12	103.00	1.33	137.21	2.03	0.18	0.83
0.30	63.59	102.13	1.34	136.92	2.04	0.18	0.83
0.40	60.41	97.01	1.43	138.53	2.11	0.18	0.83
0.50	57.19	91.83	1.57	143.86	2.18	0.17	0.83
0.60	56.53	90.76	1.72	155.83	2.24	0.18	0.83
0.70	59.04	94.78	1.82	172.72	2.27	0.20	0.84
0.80	62.44	100.24	1.87	187.89	2.29	0.23	0.86
0.90	64.67	103.81	1.90	196.86	2.29	0.24	0.86
1.00	65.58	105.26	1.91	200.89	2.30	0.24	0.86
1.10	64.59	103.66	1.94	200.71	2.30	0.25	0.86
1.20	61.76	99.10	1.99	196.80	2.32	0.23	0.85
1.30	57.24	91.84	2.05	188.28	2.33	0.20	0.84
1.40	54.57	87.54	2.07	181.41	2.34	0.18	0.83
1.50	54.99	88.19	2.04	180.24	2.33	0.19	0.83
1.60	57.17	91.70	2.01	183.95	2.32	0.20	0.84
1.70	59.72	95.77	1.98	189.55	2.31	0.21	0.85
1.80	60.59	97.17	1.99	193.62	2.32	0.22	0.85
1.90	57.91	92.86	2.08	193.53	2.34	0.22	0.85
2.00	52.69	84.46	2.26	191.05	2.38	0.18	0.83
2.10	46.70	74.82	2.52	188.29	2.43	0.16	0.82
2.20	42.14	67.48	2.75	185.75	2.47	0.15	0.81
2.30	37.73	60.39	2.99	180.85	2.50	0.14	0.79
2.40	33.71	53.92	3.22	173.85	2.53	0.13	0.78
2.50	31.80	50.84	3.31	168.29	2.55	0.12	0.77
2.60	32.09	51.29	3.23	165.52	2.53	0.12	0.78
2.70	33.43	53.45	3.07	164.30	2.51	0.13	0.78
2.80	34.49	55.13	2.93	161.55	2.49	0.13	0.78
2.90	34.00	54.33	2.86	155.19	2.48	0.13	0.78
3.00	33.22	53.07	2.77	147.10	2.47	0.12	0.77
3.10	32.49	51.89	2.70	140.30	2.46	0.12	0.77
3.20	33.17	52.98	2.64	139.73	2.45	0.12	0.78
3.30	34.74	55.48	2.60	144.39	2.44	0.13	0.78
3.40	37.04	59.18	2.58	152.88	2.44	0.13	0.79
3.50	39.15	62.55	2.61	163.10	2.44	0.14	0.80
3.60	40.29	64.38	2.71	174.58	2.46	0.15	0.80
3.70	40.26	64.32	2.91	187.35	2.49	0.15	0.80
3.80	40.09	64.03	3.14	200.75	2.52	0.15	0.80
3.90	40.64	64.90	3.29	213.59	2.54	0.15	0.80
4.00	42.32	67.60	3.31	223.86	2.55	0.16	0.81
4.10	44.34	70.83	3.24	229.20	2.54	0.17	0.82
4.20	45.37	72.48	3.19	230.87	2.53	0.17	0.82
4.30	44.83	71.60	3.24	231.77	2.54	0.17	0.82
4.40	42.77	68.28	3.43	234.00	2.56	0.16	0.81
4.50	39.56	63.12	3.72	234.82	2.60	0.15	0.80
4.60	35.62	56.77	4.07	230.75	2.63	0.14	0.65
4.70	31.43	50.03	4.43	221.54	2.67	0.13	0.63
4.80	28.05	44.58	4.72	210.32	2.70	0.12	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
4.90	25.36	40.26	4.93	198.47	2.72	0.11	0.62
5.00	23.37	37.06	5.04	186.61	2.73	0.11	0.62
5.10	21.74	34.43	5.07	174.55	2.73	0.11	0.62
5.20	20.76	32.84	5.03	165.17	2.73	0.10	0.62
5.30	20.78	32.86	4.92	161.80	2.72	0.10	0.62
5.40	22.02	34.85	4.70	163.71	2.70	0.10	0.62
5.50	24.13	38.22	4.36	166.60	2.67	0.11	0.62
5.60	26.02	41.26	4.04	166.71	2.63	0.12	0.62
5.70	26.65	42.26	3.88	163.99	2.61	0.12	0.62
5.80	25.84	40.95	3.95	161.57	2.62	0.11	0.62
5.90	23.01	36.39	4.37	159.08	2.67	0.11	0.62
6.00	19.12	30.13	5.18	155.98	2.74	0.10	0.62
6.10	16.32	25.63	5.98	153.12	2.81	0.09	0.62
6.20	15.54	24.36	6.14	149.69	2.82	0.10	0.62
6.30	15.65	24.53	5.91	145.08	2.80	0.10	0.62
6.40	14.57	22.79	6.03	137.48	2.81	0.09	0.62
6.50	12.62	19.64	6.66	130.78	2.86	0.09	0.62
6.60	10.88	16.84	7.59	127.72	2.93	0.09	0.62
6.70	9.87	15.21	8.35	127.08	2.97	0.08	0.62
6.80	9.47	14.55	8.72	126.87	3.00	0.08	0.62
6.90	9.06	13.89	9.07	126.03	3.02	0.08	1.48
7.00	8.72	13.33	9.51	126.79	3.04	0.08	1.40
7.10	9.04	13.84	9.54	131.97	3.04	0.08	1.44
7.20	10.62	16.37	8.56	140.20	2.99	0.08	0.62
7.30	13.04	20.24	7.17	145.11	2.90	0.09	0.62
7.40	14.73	22.96	6.21	142.66	2.83	0.09	0.62
7.50	14.76	22.99	5.95	136.71	2.81	0.09	0.62
7.60	13.33	20.69	6.39	132.11	2.84	0.09	0.62
7.70	11.94	18.44	7.15	131.87	2.90	0.09	0.62
7.80	11.27	17.36	7.61	132.07	2.93	0.09	0.62
7.90	10.87	16.70	7.72	129.04	2.93	0.09	0.62
8.00	10.28	15.75	7.81	122.96	2.94	0.08	0.62
8.10	9.38	14.29	8.13	116.11	2.96	0.08	0.62
8.20	8.40	12.72	8.68	110.32	2.99	0.08	0.62
8.30	7.35	11.01	9.55	105.17	3.04	0.08	1.01
8.40	6.58	9.78	10.40	101.62	3.09	0.08	0.89
8.50	6.25	9.23	10.88	100.38	3.11	0.08	0.84
8.60	6.30	9.31	10.94	101.78	3.12	0.08	0.84
8.70	6.35	9.38	11.04	103.53	3.12	0.08	0.84
8.80	6.29	9.26	11.20	103.69	3.13	0.08	0.83
8.90	6.27	9.22	11.04	101.79	3.12	0.08	0.82
9.00	6.29	9.25	10.60	98.05	3.10	0.08	0.82
9.10	6.09	8.92	10.47	93.46	3.09	0.08	0.79
9.20	5.58	8.09	11.00	88.98	3.12	0.07	0.71
9.30	5.10	7.32	11.87	86.90	3.16	0.07	0.64
9.40	5.13	7.35	12.15	89.24	3.17	0.07	0.64
9.50	5.52	7.98	11.68	93.23	3.15	0.07	0.70
9.60	5.90	8.58	11.06	94.86	3.12	0.08	0.74

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.70	7.76	11.56	8.66	100.02	2.99	0.08	0.62
9.80	11.21	17.09	6.73	114.99	2.87	0.08	0.62
9.90	12.34	18.90	6.45	121.89	2.85	0.09	0.62
10.00	10.19	15.43	7.66	118.19	2.93	0.08	0.62
10.10	6.46	9.43	10.59	99.83	3.10	0.07	0.80
10.20	5.25	7.47	11.83	88.41	3.16	0.07	0.63
10.30	5.64	8.10	11.34	91.92	3.14	0.08	0.68
10.40	5.93	8.55	11.29	96.58	3.13	0.08	0.72
10.50	5.98	8.62	11.56	99.62	3.15	0.08	0.72
10.60	5.98	8.61	11.82	101.85	3.16	0.08	0.72
10.70	5.98	8.61	12.06	103.80	3.17	0.08	0.71
10.80	5.98	8.60	12.28	105.58	3.18	0.08	0.71
10.90	5.98	8.59	12.35	106.10	3.18	0.08	0.71
11.00	5.98	8.58	12.28	105.33	3.18	0.08	0.70
11.10	6.00	8.61	12.27	105.63	3.18	0.08	0.70
11.20	6.41	9.26	12.09	111.96	3.17	0.08	0.75
11.30	7.76	11.43	10.97	125.36	3.12	0.08	0.93
11.40	9.54	14.26	9.46	135.00	3.04	0.08	1.15
11.50	10.92	16.47	8.25	135.92	2.97	0.08	0.62
11.60	11.17	16.87	7.66	129.22	2.93	0.08	0.62
11.70	10.34	15.54	7.88	122.49	2.94	0.08	0.62
11.80	9.11	13.54	8.88	120.27	3.01	0.08	1.07
11.90	8.03	11.79	10.43	123.04	3.09	0.08	0.93
12.00	8.26	12.17	10.99	133.76	3.12	0.08	0.96
12.10	9.89	14.78	10.00	147.78	3.07	0.08	1.16
12.20	12.14	18.37	8.40	154.26	2.98	0.09	0.62
12.30	13.79	21.02	7.01	147.37	2.89	0.09	0.62
12.40	14.39	21.98	5.95	130.84	2.81	0.09	0.62
12.50	14.67	22.42	5.20	116.66	2.75	0.08	0.62
12.60	15.66	24.00	4.79	115.01	2.71	0.08	0.62
12.70	16.72	25.68	4.78	122.88	2.71	0.09	0.62
12.80	17.02	26.17	5.10	133.47	2.74	0.09	0.62
12.90	15.54	23.78	5.89	140.16	2.80	0.09	0.62
13.00	13.13	19.90	7.08	140.97	2.89	0.09	0.62
13.10	10.98	16.43	8.30	136.29	2.97	0.08	0.62
13.20	9.80	14.53	8.85	128.62	3.00	0.08	1.08
13.30	9.73	14.40	8.51	122.53	2.98	0.08	0.62
13.40	10.47	15.59	7.75	120.78	2.94	0.08	0.62
13.50	11.58	17.37	7.12	123.69	2.89	0.08	0.62
13.60	12.48	18.80	6.84	128.59	2.87	0.08	0.62
13.70	12.75	19.22	6.93	133.11	2.88	0.08	0.62
13.80	12.33	18.54	7.28	134.88	2.90	0.08	0.62
13.90	11.80	17.68	7.52	132.97	2.92	0.08	0.62
14.00	11.32	16.90	7.52	127.05	2.92	0.08	0.62
14.10	11.16	16.61	7.22	119.87	2.90	0.08	0.62
14.20	11.16	16.49	6.95	114.51	2.88	0.08	0.62
14.30	11.46	16.86	6.79	114.46	2.87	0.08	0.62
14.40	12.08	17.76	6.78	120.36	2.87	0.08	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
14.50	13.00	19.14	6.77	129.64	2.87	0.08	0.62
14.60	13.94	20.52	6.76	138.64	2.87	0.09	0.62
14.70	14.88	21.86	6.64	145.18	2.86	0.09	0.62
14.80	15.29	22.38	6.62	148.08	2.86	0.09	0.62
14.90	14.81	21.62	6.83	147.59	2.87	0.09	0.62
15.00	13.79	20.07	7.26	145.73	2.90	0.09	0.62
15.10	12.99	18.84	7.67	144.60	2.93	0.08	0.62
15.20	12.91	18.67	7.80	145.60	2.94	0.08	0.62
15.30	13.60	19.60	7.60	148.96	2.93	0.08	0.62
15.40	14.65	21.04	7.28	153.13	2.91	0.09	0.62
15.50	14.88	21.29	7.25	154.28	2.90	0.09	0.62
15.60	14.72	20.99	7.35	154.30	2.91	0.09	0.62
15.70	14.79	21.00	7.36	154.60	2.91	0.09	0.62
15.80	15.44	21.83	7.15	156.19	2.90	0.09	0.62
15.90	15.62	22.01	7.14	157.05	2.90	0.09	0.62
16.00	15.50	21.77	7.29	158.82	2.91	0.09	0.62
16.10	17.19	24.08	6.89	165.86	2.88	0.09	0.62
16.20	21.05	29.29	5.91	173.16	2.80	0.09	0.62
16.30	24.86	34.27	5.09	174.43	2.74	0.10	0.62
16.40	26.05	35.63	4.73	168.71	2.70	0.10	0.62
16.50	23.46	31.96	4.99	159.48	2.73	0.10	0.62
16.60	18.42	25.05	5.93	148.44	2.81	0.09	0.62
16.70	12.98	17.53	7.67	134.33	2.93	0.08	0.62
16.80	8.92	11.56	9.96	115.18	3.07	0.08	0.83
16.90	6.90	8.60	11.37	97.81	3.14	0.07	0.61
17.00	6.16	7.49	11.46	85.89	3.14	0.07	0.54
17.10	5.97	7.20	10.94	78.82	3.12	0.07	0.51
17.20	5.97	7.18	10.43	74.86	3.09	0.07	0.51
17.30	5.79	6.88	10.43	71.77	3.09	0.07	0.49
17.40	5.81	6.88	10.36	71.28	3.09	0.07	0.49
17.50	6.26	7.51	10.23	76.80	3.08	0.07	0.54
17.60	7.24	8.87	9.88	87.63	3.06	0.08	0.63
17.70	8.07	10.01	9.77	97.83	3.06	0.08	0.72
17.80	8.41	10.45	9.91	103.65	3.06	0.08	0.75
17.90	8.42	10.43	10.17	106.06	3.08	0.08	0.74
18.00	8.37	10.31	10.47	107.95	3.09	0.08	0.74
18.10	8.17	9.99	11.14	111.30	3.13	0.08	0.71
18.20	8.13	9.90	11.87	117.52	3.16	0.08	0.71
18.30	8.94	10.98	11.75	129.03	3.16	0.08	0.78
18.40	10.90	13.66	10.45	142.71	3.09	0.08	0.98
18.50	13.00	16.49	9.14	150.66	3.02	0.08	1.18
18.60	14.19	18.06	8.30	149.99	2.97	0.09	0.62
18.70	15.48	19.74	7.47	147.34	2.92	0.09	0.62
18.80	16.63	21.12	6.98	147.37	2.88	0.09	0.62
18.90	16.88	21.38	6.99	149.51	2.89	0.09	0.62
19.00	15.17	19.11	7.76	148.27	2.94	0.09	0.62
19.10	12.50	15.42	9.16	141.32	3.02	0.08	1.10
19.20	10.65	12.88	10.33	133.05	3.09	0.08	0.92

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
19.30	10.32	12.38	10.41	128.88	3.09	0.08	0.88
19.40	11.45	13.84	9.48	131.31	3.04	0.08	0.99
19.50	13.39	16.38	8.27	135.51	2.97	0.08	0.62
19.60	15.68	19.27	7.07	136.32	2.89	0.09	0.62
19.70	17.74	21.71	6.07	131.71	2.82	0.09	0.62
19.80	19.36	23.60	5.51	130.07	2.77	0.09	0.62
19.90	18.84	22.91	5.76	132.05	2.79	0.09	0.62
20.00	16.51	19.98	6.59	131.72	2.86	0.09	0.62
20.10	13.94	16.72	7.53	125.84	2.92	0.08	0.62
20.20	12.46	14.72	7.90	116.35	2.95	0.08	0.62
20.30	12.39	14.58	7.86	114.59	2.94	0.08	0.62
20.40	12.55	14.74	7.90	116.39	2.95	0.08	0.62
20.50	13.23	15.56	7.65	119.00	2.93	0.08	0.62
20.60	14.29	16.83	7.20	121.13	2.90	0.08	0.62
20.70	15.22	17.91	6.96	124.61	2.88	0.09	0.62
20.80	16.35	19.28	6.93	133.55	2.88	0.09	0.62
20.90	18.79	22.28	6.77	150.76	2.87	0.09	0.62
21.00	23.85	28.40	6.07	172.52	2.82	0.09	0.62
21.10	30.27	36.02	5.17	186.26	2.74	0.11	0.62
21.20	36.95	43.70	4.23	184.94	2.65	0.11	0.62
21.30	42.73	50.01	3.32	166.14	2.55	0.12	0.77
21.40	47.27	54.66	2.59	141.74	2.44	0.12	0.77
21.50	49.21	56.33	2.18	122.62	2.36	0.12	0.78
21.60	48.10	54.78	2.11	115.61	2.35	0.12	0.77
21.70	45.14	51.43	2.35	120.95	2.40	0.11	0.76
21.80	42.84	48.96	2.80	136.86	2.47	0.11	0.76
21.90	45.62	52.21	2.98	155.52	2.50	0.11	0.76
22.00	55.53	63.30	2.60	164.44	2.44	0.13	0.78
22.10	70.39	79.47	2.02	160.56	2.32	0.16	0.81
22.20	86.19	96.17	1.61	154.39	2.20	0.17	0.83
22.30	98.36	108.57	1.41	152.73	2.09	0.20	0.84
22.40	107.08	117.31	1.33	156.28	2.03	0.20	0.84
22.50	115.37	125.86	1.31	164.41	2.00	0.21	0.84
22.60	122.02	132.79	1.30	172.90	1.99	0.26	0.86
22.70	126.84	137.78	1.30	179.79	2.00	0.27	0.86
22.80	129.17	140.06	1.31	183.60	2.00	0.27	0.86
22.90	136.06	147.16	1.31	192.22	2.00	0.30	0.87
23.00	147.42	158.93	1.29	205.52	1.98	0.41	0.89
23.10	160.45	172.36	1.28	220.33	1.96	0.54	0.90
23.20	171.23	183.35	1.27	232.50	1.95	0.71	0.90
23.30	180.27	192.47	1.26	242.96	1.94	0.92	0.91
23.40	187.37	199.53	1.26	251.28	1.93	0.93	0.92
23.50	191.52	203.42	1.26	255.94	1.93	0.93	0.92
23.60	191.73	203.15	1.26	255.76	1.93	0.93	0.92
23.70	187.36	198.09	1.26	250.43	1.94	0.93	0.92
23.80	178.72	188.68	1.28	241.10	1.96	0.92	0.91
23.90	166.77	176.03	1.31	230.76	2.00	0.69	0.91
24.00	149.50	157.77	1.36	214.38	2.05	0.50	0.90

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
24.10	133.96	141.16	1.40	197.71	2.09	0.30	0.88
24.20	126.47	132.75	1.39	184.07	2.08	0.25	0.86
24.30	128.47	134.23	1.35	180.75	2.04	0.29	0.87
24.40	130.78	136.14	1.32	180.37	2.02	0.30	0.87
24.50	124.66	129.53	1.34	174.11	2.04	0.27	0.87
24.60	110.33	114.62	1.42	163.11	2.10	0.22	0.85
24.70	91.14	94.77	1.64	155.70	2.21	0.18	0.83
24.80	72.12	75.03	2.09	157.06	2.34	0.15	0.81
24.90	57.73	60.01	2.78	167.00	2.47	0.13	0.78
25.00	49.70	51.55	3.44	177.19	2.56	0.12	0.77
25.10	47.44	49.10	3.80	186.68	2.61	0.12	0.62
25.20	45.12	46.57	4.17	194.07	2.65	0.13	0.62
25.30	42.32	43.53	4.58	199.18	2.69	0.11	0.62
25.40	41.45	42.49	4.67	198.44	2.70	0.11	0.62
25.50	47.50	48.57	3.85	187.17	2.61	0.12	0.62
25.60	58.52	59.61	2.79	166.06	2.47	0.13	0.79
25.70	69.31	70.27	2.08	146.49	2.34	0.15	0.81
25.80	77.97	78.74	1.75	138.03	2.25	0.15	0.81
25.90	83.74	84.31	1.63	137.77	2.21	0.16	0.82
26.00	87.01	87.39	1.60	140.10	2.20	0.17	0.83
26.10	87.64	87.86	1.64	143.93	2.21	0.17	0.83
26.20	89.33	89.36	1.64	146.64	2.21	0.17	0.82
26.30	93.87	93.64	1.57	146.57	2.18	0.18	0.83
26.40	98.42	97.85	1.47	144.09	2.13	0.19	0.84
26.50	100.49	99.62	1.43	142.74	2.11	0.18	0.84
26.60	99.58	98.50	1.45	142.91	2.12	0.18	0.83
26.70	99.14	97.88	1.48	144.55	2.14	0.18	0.83
26.80	99.48	98.02	1.50	146.75	2.15	0.18	0.84
26.90	100.62	98.93	1.50	148.83	2.15	0.19	0.84
27.00	102.38	100.44	1.50	150.56	2.15	0.19	0.84
27.10	104.07	101.85	1.49	151.74	2.14	0.20	0.84
27.20	105.35	102.88	1.49	153.24	2.14	0.20	0.84
27.30	105.96	103.26	1.51	155.76	2.15	0.20	0.85
27.40	106.62	103.70	1.54	160.19	2.17	0.21	0.85
27.50	107.61	104.45	1.58	164.74	2.18	0.21	0.85
27.60	109.14	105.71	1.58	167.22	2.19	0.22	0.85
27.70	111.42	107.65	1.56	167.55	2.18	0.22	0.86
27.80	114.37	110.25	1.53	168.34	2.16	0.23	0.86
27.90	117.17	112.69	1.50	169.46	2.15	0.24	0.86
28.00	117.25	112.47	1.48	166.81	2.14	0.25	0.86
28.10	113.03	108.10	1.48	159.62	2.14	0.22	0.85
28.20	104.54	99.66	1.53	152.02	2.16	0.20	0.84
28.30	96.33	91.54	1.62	147.84	2.20	0.17	0.83
28.40	89.43	84.70	1.72	145.31	2.24	0.17	0.83
28.50	84.52	79.78	1.76	140.20	2.25	0.16	0.82
28.60	79.72	74.99	1.84	137.82	2.28	0.15	0.81
28.70	74.73	70.04	1.99	139.59	2.32	0.15	0.81
28.80	69.75	65.14	2.26	147.46	2.38	0.14	0.80

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
28.90	62.88	58.43	2.67	156.21	2.45	0.14	0.79
29.00	55.17	50.94	3.21	163.60	2.53	0.13	0.78
29.10	47.60	43.63	3.79	165.44	2.60	0.12	0.62
29.20	41.43	37.66	4.33	163.01	2.66	0.11	0.62
29.30	37.19	33.54	4.81	161.27	2.71	0.10	0.62
29.40	34.70	31.10	5.22	162.34	2.75	0.10	0.62
29.50	34.06	30.41	5.41	164.37	2.76	0.10	0.62
29.60	33.91	30.18	5.40	163.10	2.76	0.10	0.62
29.70	32.03	28.33	5.55	157.22	2.78	0.10	0.62
29.80	29.66	26.04	5.86	152.48	2.80	0.10	0.62
29.90	28.43	24.82	6.23	154.62	2.83	0.10	0.62
30.00	32.28	28.32	6.10	172.81	2.82	0.10	0.62
30.10	38.09	33.62	5.63	189.28	2.78	0.11	0.62
30.20	43.19	38.24	5.16	197.31	2.74	0.12	0.62
30.30	44.63	39.45	5.06	199.76	2.73	0.12	0.62
30.40	44.36	39.09	5.20	203.30	2.75	0.12	0.62
30.50	46.20	40.66	5.18	210.68	2.74	0.12	0.62
30.60	51.44	45.36	4.60	208.57	2.69	0.12	0.62
30.70	59.73	52.86	3.70	195.73	2.59	0.14	0.79
30.80	69.61	61.82	2.85	175.99	2.48	0.14	0.80
30.90	81.48	72.59	2.19	159.10	2.36	0.16	0.81
31.00	94.67	84.56	1.80	152.10	2.26	0.18	0.83
31.10	106.82	95.53	1.61	153.84	2.20	0.21	0.85
31.20	116.62	104.28	1.54	160.36	2.17	0.22	0.86
31.30	124.76	111.44	1.52	169.30	2.16	0.26	0.87
31.40	130.68	116.55	1.51	176.48	2.16	0.29	0.88
31.50	133.94	119.25	1.50	179.13	2.15	0.30	0.88
31.60	134.30	119.31	1.49	178.20	2.14	0.30	0.88
31.70	132.00	116.97	1.50	175.44	2.15	0.29	0.88
31.80	124.86	110.25	1.53	168.77	2.16	0.27	0.87
31.90	112.69	99.05	1.59	157.38	2.19	0.22	0.85
32.00	97.91	85.54	1.71	146.00	2.23	0.18	0.83
32.10	85.37	74.05	1.93	142.83	2.30	0.15	0.81
32.20	78.62	67.76	2.21	149.84	2.37	0.15	0.81
32.30	78.07	67.05	2.36	158.28	2.40	0.15	0.81
32.40	82.35	70.67	2.30	162.57	2.39	0.16	0.81
32.50	89.96	77.28	2.11	162.74	2.34	0.17	0.82
32.60	100.87	86.85	1.86	161.56	2.28	0.19	0.84
32.70	114.12	98.53	1.64	161.25	2.21	0.22	0.85
32.80	125.97	109.00	1.48	161.04	2.14	0.26	0.87
32.90	133.61	115.67	1.41	162.86	2.09	0.27	0.87
33.00	136.56	118.12	1.38	162.91	2.07	0.27	0.87
33.10	135.19	116.76	1.36	158.61	2.05	0.26	0.87
33.20	129.92	111.98	1.34	150.52	2.04	0.23	0.86
33.30	122.33	105.12	1.35	141.68	2.04	0.20	0.84
33.40	115.41	98.69	1.40	138.12	2.09	0.19	0.84
33.50	111.66	95.06	1.46	139.16	2.13	0.19	0.84
33.60	111.68	94.74	1.52	144.33	2.16	0.19	0.84

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
33.70	116.59	98.70	1.55	153.47	2.17	0.21	0.85
33.80	126.41	106.98	1.53	163.95	2.16	0.25	0.86
33.90	138.32	117.17	1.47	172.07	2.13	0.30	0.88
34.00	149.33	126.67	1.40	177.04	2.09	0.35	0.89
34.10	156.01	132.42	1.35	178.45	2.04	0.38	0.89
34.20	158.07	134.09	1.33	177.73	2.02	0.37	0.89
34.30	158.80	134.48	1.32	177.83	2.02	0.35	0.88
34.40	162.94	137.73	1.33	182.67	2.02	0.38	0.89
34.50	169.31	142.88	1.33	189.67	2.02	0.50	0.90
34.60	175.37	147.80	1.32	195.71	2.02	0.55	0.90
34.70	179.32	150.90	1.32	199.20	2.01	0.58	0.90
34.80	184.04	154.72	1.31	202.79	2.00	0.65	0.91
34.90	189.55	159.27	1.30	206.34	1.99	0.74	0.91
35.00	194.31	163.22	1.28	208.83	1.96	0.81	0.91
35.10	196.77	165.14	1.27	209.65	1.95	0.85	0.91
35.20	196.37	164.51	1.27	208.69	1.95	0.82	0.91
35.30	193.58	161.78	1.27	205.79	1.95	0.74	0.91
35.40	189.34	157.88	1.27	201.11	1.96	0.66	0.90
35.50	184.20	153.28	1.27	195.01	1.95	0.56	0.90
35.60	178.51	148.27	1.27	188.06	1.95	0.47	0.89
35.70	173.44	143.85	1.26	181.47	1.94	0.40	0.88
35.80	169.68	140.61	1.25	175.85	1.92	0.35	0.87
35.90	166.88	138.27	1.23	170.58	1.90	0.32	0.86
36.00	163.35	135.35	1.21	164.34	1.87	0.29	0.84
36.10	158.25	131.07	1.20	156.95	1.85	0.25	0.83
36.20	152.33	125.91	1.20	150.54	1.84	0.22	0.82
36.30	147.13	121.22	1.21	146.45	1.86	0.21	0.82
36.40	143.89	118.12	1.22	144.64	1.88	0.20	0.82
36.50	142.53	116.63	1.24	144.26	1.90	0.21	0.83
36.60	143.00	116.75	1.24	145.14	1.91	0.21	0.83
36.70	145.61	118.68	1.25	147.82	1.91	0.22	0.83
36.80	150.56	122.60	1.24	152.46	1.91	0.24	0.84
36.90	157.66	128.36	1.24	158.76	1.90	0.26	0.84
37.00	165.31	134.63	1.23	165.06	1.88	0.30	0.85
37.10	172.32	140.40	1.21	170.24	1.87	0.33	0.85
37.20	177.10	144.25	1.20	173.64	1.85	0.35	0.85
37.30	178.87	145.48	1.20	175.04	1.85	0.37	0.85
37.40	177.96	144.39	1.21	174.63	1.86	0.36	0.85
37.50	175.45	141.98	1.22	172.74	1.87	0.34	0.85
37.60	172.65	139.32	1.22	170.61	1.88	0.33	0.85
37.70	169.90	136.69	1.23	168.64	1.90	0.32	0.86
37.80	167.26	134.14	1.24	166.75	1.91	0.31	0.86
37.90	165.19	132.09	1.25	165.34	1.92	0.30	0.86
38.00	164.02	130.76	1.26	164.82	1.94	0.30	0.86
38.10	163.69	130.12	1.27	165.07	1.95	0.31	0.87
38.20	163.69	129.81	1.27	165.36	1.96	0.32	0.87
38.30	163.49	129.34	1.28	165.43	1.96	0.32	0.87
38.40	162.37	128.10	1.29	164.72	1.97	0.32	0.87

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
38.50	159.91	125.77	1.29	162.83	1.98	0.31	0.87
38.60	156.57	122.75	1.30	160.06	2.00	0.29	0.87
38.70	153.20	119.72	1.31	157.36	2.01	0.28	0.87
38.80	150.08	116.88	1.33	155.01	2.02	0.27	0.87
38.90	147.28	114.34	1.34	152.87	2.03	0.26	0.86
39.00	145.42	112.61	1.34	151.20	2.04	0.25	0.86
39.10	145.19	112.25	1.34	150.60	2.04	0.25	0.86
39.20	146.51	113.17	1.33	151.00	2.03	0.26	0.86
39.30	148.08	114.32	1.32	151.41	2.02	0.26	0.86
39.40	149.40	115.30	1.31	151.51	2.01	0.26	0.86
39.50	150.23	115.88	1.31	151.30	2.00	0.26	0.86
39.60	150.45	115.97	1.30	150.55	1.99	0.26	0.86
39.70	151.53	116.74	1.29	150.71	1.98	0.25	0.86
39.80	153.36	118.05	1.29	151.87	1.97	0.26	0.86
39.90	155.09	119.10	1.29	153.97	1.98	0.28	0.86
40.00	154.86	118.49	1.31	154.83	2.00	0.28	0.87
40.10	154.63	117.96	1.32	155.31	2.01	0.27	0.87
40.20	156.64	119.36	1.31	156.78	2.01	0.29	0.87
40.30	160.77	122.51	1.30	159.73	2.00	0.31	0.87
40.40	165.07	125.78	1.30	162.91	1.99	0.33	0.87
40.50	168.83	128.65	1.29	165.46	1.97	0.34	0.87
40.60	172.09	131.16	1.28	167.39	1.96	0.36	0.88
40.70	175.00	133.42	1.27	168.92	1.94	0.36	0.87
40.80	177.41	135.24	1.26	170.18	1.93	0.37	0.87
40.90	179.23	136.52	1.25	171.30	1.93	0.38	0.87
41.00	180.47	137.19	1.26	172.48	1.93	0.39	0.88
41.10	181.45	137.57	1.26	173.82	1.94	0.41	0.88
41.20	182.77	138.22	1.27	175.39	1.95	0.43	0.88
41.30	184.68	139.37	1.27	177.32	1.95	0.45	0.89
41.40	186.86	140.83	1.27	179.01	1.95	0.47	0.89
41.50	189.12	142.53	1.26	180.06	1.94	0.48	0.89
41.60	190.91	143.95	1.25	180.34	1.92	0.48	0.88
41.70	192.03	144.73	1.25	180.50	1.92	0.48	0.88
41.80	192.92	145.05	1.25	181.54	1.92	0.49	0.88
41.90	194.40	145.67	1.26	183.70	1.94	0.53	0.89
42.00	197.14	147.32	1.27	186.79	1.95	0.59	0.90
42.10	200.61	149.60	1.27	190.20	1.95	0.67	0.90
42.20	203.97	151.83	1.27	193.36	1.96	0.75	0.91
42.30	206.60	153.50	1.28	195.75	1.96	0.82	0.91
42.40	208.12	154.40	1.28	196.88	1.96	0.86	0.91
42.50	208.30	154.35	1.27	196.42	1.95	0.85	0.91
42.60	206.70	152.96	1.27	194.35	1.95	0.80	0.91
42.70	203.68	150.46	1.27	191.08	1.95	0.71	0.90
42.80	199.57	147.12	1.27	187.01	1.95	0.63	0.90
42.90	194.71	143.07	1.28	182.77	1.96	0.57	0.90
43.00	190.18	139.13	1.29	179.57	1.98	0.51	0.90
43.10	187.86	136.81	1.31	178.70	2.00	0.50	0.90
43.20	190.13	138.14	1.31	181.14	2.00	0.53	0.90

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
43.30	197.38	143.46	1.30	186.81	1.99	0.64	0.91
43.40	207.80	151.34	1.29	194.55	1.97	0.85	0.91
43.50	219.34	160.16	1.27	203.06	1.95	0.90	0.92
43.60	230.48	168.65	1.25	211.34	1.92	0.90	0.92
43.70	240.76	176.40	1.24	219.09	1.91	0.91	0.93
43.80	249.82	183.13	1.23	226.01	1.90	0.92	0.93
43.90	258.68	189.73	1.23	232.53	1.88	0.92	0.93
44.00	267.99	196.97	1.21	238.11	1.86	0.93	0.93
44.10	276.85	204.25	1.18	241.03	1.83	0.93	0.93
44.20	284.85	211.29	1.13	238.83	1.78	0.94	0.93
44.30	291.10	217.20	1.06	229.18	1.73	0.94	0.93
44.40	294.85	220.87	1.00	220.87	1.70	0.95	0.94
44.50	294.77	220.75	1.00	220.75	1.69	0.95	0.94
44.60	292.55	218.20	1.00	218.92	1.71	0.94	0.93
44.70	291.79	217.01	1.02	222.23	1.72	0.94	0.93
44.80	294.37	219.18	1.00	219.18	1.70	0.94	0.93
44.90	299.33	223.84	1.00	223.84	1.67	0.95	0.94
45.00	305.05	228.94	1.00	228.94	1.63	0.95	0.94
45.10	310.35	233.00	1.00	233.00	1.62	0.95	0.95
45.20	314.64	235.82	1.00	235.82	1.63	0.96	0.95
45.30	316.67	236.72	1.00	236.72	1.64	0.96	0.95
45.40	316.15	235.62	1.00	235.62	1.65	0.96	0.95
45.50	314.75	233.66	1.00	233.66	1.66	0.95	0.95
45.60	313.96	232.13	1.00	232.13	1.68	0.95	0.95
45.70	313.55	231.06	1.00	231.06	1.69	0.95	0.95
45.80	312.06	229.50	1.00	229.50	1.70	0.95	0.95
45.90	308.31	226.55	1.00	226.55	1.69	0.95	0.95
46.00	302.20	221.94	1.00	221.94	1.69	0.95	0.94
46.10	293.67	215.60	1.00	215.60	1.68	0.94	0.93
46.20	283.78	208.21	1.00	208.21	1.67	0.94	0.92
46.30	273.76	200.90	1.00	200.90	1.66	0.93	0.91
46.40	264.02	193.71	1.00	193.71	1.65	0.92	0.91
46.50	253.44	185.59	1.00	185.59	1.66	0.92	0.90
46.60	239.32	174.12	1.00	174.12	1.68	0.91	0.88
46.70	218.44	156.86	1.08	169.18	1.75	0.58	0.86
46.80	190.67	134.12	1.20	161.00	1.85	0.34	0.85
46.90	159.42	108.98	1.30	141.79	1.99	0.25	0.86
47.00	130.94	86.50	1.53	132.00	2.16	0.20	0.85
47.10	109.62	69.95	2.03	142.18	2.33	0.18	0.83
47.20	99.20	61.64	2.69	165.64	2.46	0.16	0.82
47.30	101.82	62.70	2.99	187.16	2.50	0.17	0.82
47.40	114.04	70.74	2.75	194.52	2.47	0.21	0.85
47.50	127.97	80.48	2.33	187.25	2.39	0.26	0.87
47.60	134.39	85.31	2.05	175.23	2.33	0.29	0.87
47.70	131.72	83.56	2.02	168.52	2.32	0.26	0.87
47.80	123.26	77.42	2.18	168.66	2.36	0.23	0.85
47.90	115.03	71.49	2.37	169.66	2.40	0.20	0.84
48.00	111.14	68.85	2.38	164.20	2.40	0.19	0.84

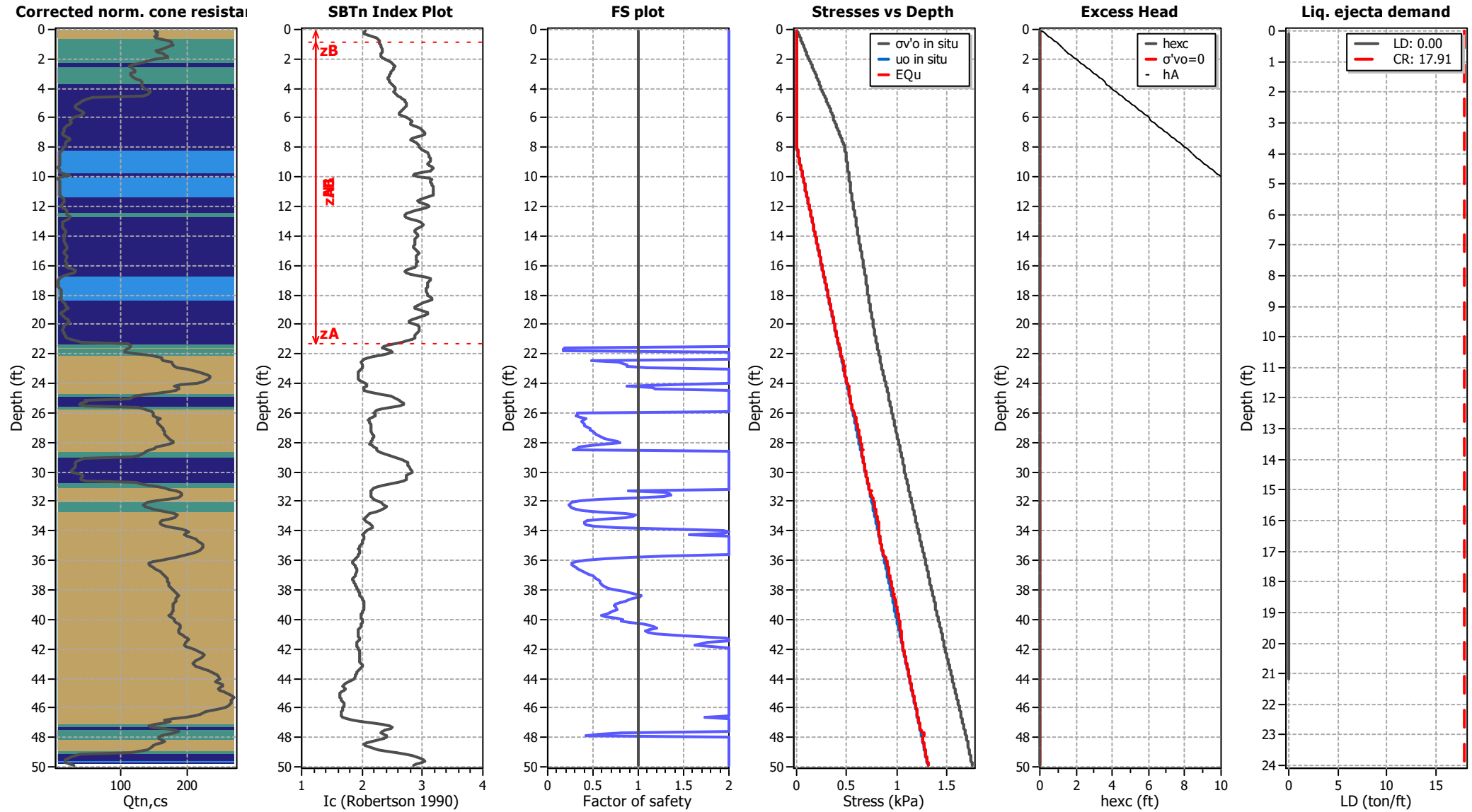
:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
48.10	113.23	70.68	2.14	151.48	2.35	0.19	0.84
48.20	120.10	76.16	1.80	136.95	2.26	0.20	0.84
48.30	127.66	82.45	1.53	125.94	2.16	0.20	0.85
48.40	131.70	86.31	1.39	119.72	2.08	0.19	0.84
48.50	130.27	85.89	1.34	114.96	2.03	0.18	0.83
48.60	123.72	81.11	1.36	109.95	2.05	0.17	0.82
48.70	112.92	72.70	1.46	106.49	2.13	0.16	0.82
48.80	98.74	61.77	1.77	109.45	2.26	0.15	0.81
48.90	82.92	50.01	2.44	121.83	2.41	0.14	0.80
49.00	68.00	39.45	3.48	137.25	2.57	0.12	0.78
49.10	55.01	30.71	4.77	146.38	2.71	0.11	0.62
49.20	44.63	24.09	6.07	146.17	2.82	0.10	0.62
49.30	36.24	19.19	7.24	138.98	2.90	0.10	0.62
49.40	30.08	15.61	8.24	128.62	2.97	0.09	0.62
49.50	25.88	13.16	8.98	118.11	3.01	0.09	0.94
49.60	23.84	11.96	9.27	110.93	3.03	0.09	0.85
49.70	26.26	13.33	8.47	112.92	2.98	0.09	0.62
49.80	32.30	16.76	7.34	123.05	2.91	0.09	0.62
49.90	38.31	20.17	6.55	132.08	2.85	0.10	0.62

Abbreviations

q_t :	Total cone resistance
K_c :	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c :	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

Ejecta Severity Estimation



LIQUEFACTION ANALYSIS REPORT

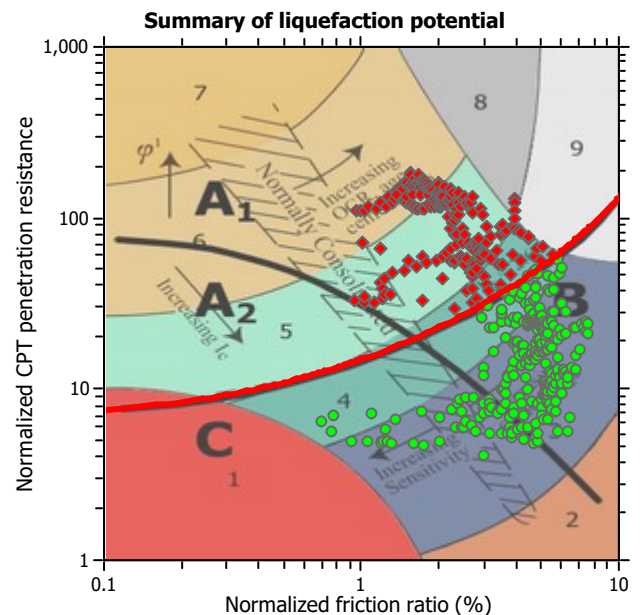
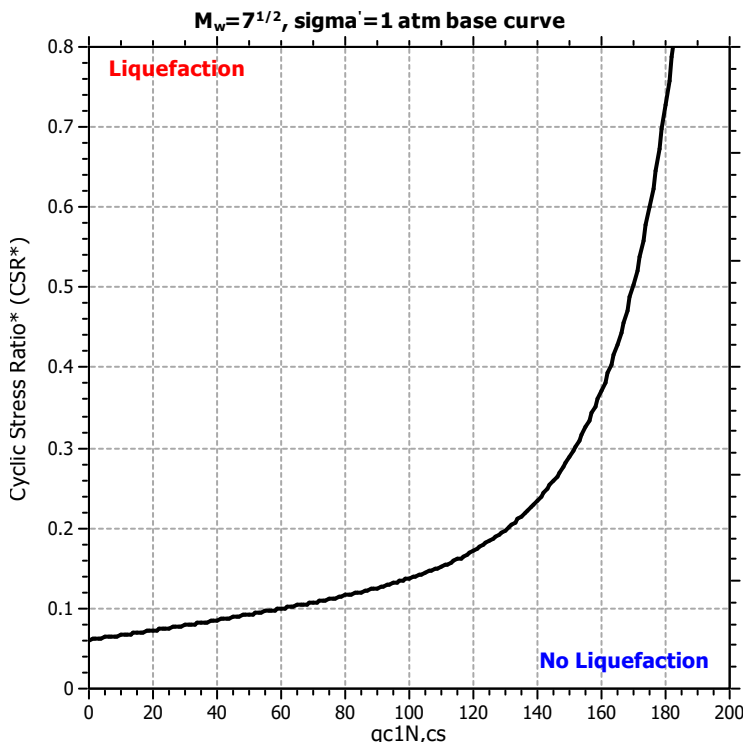
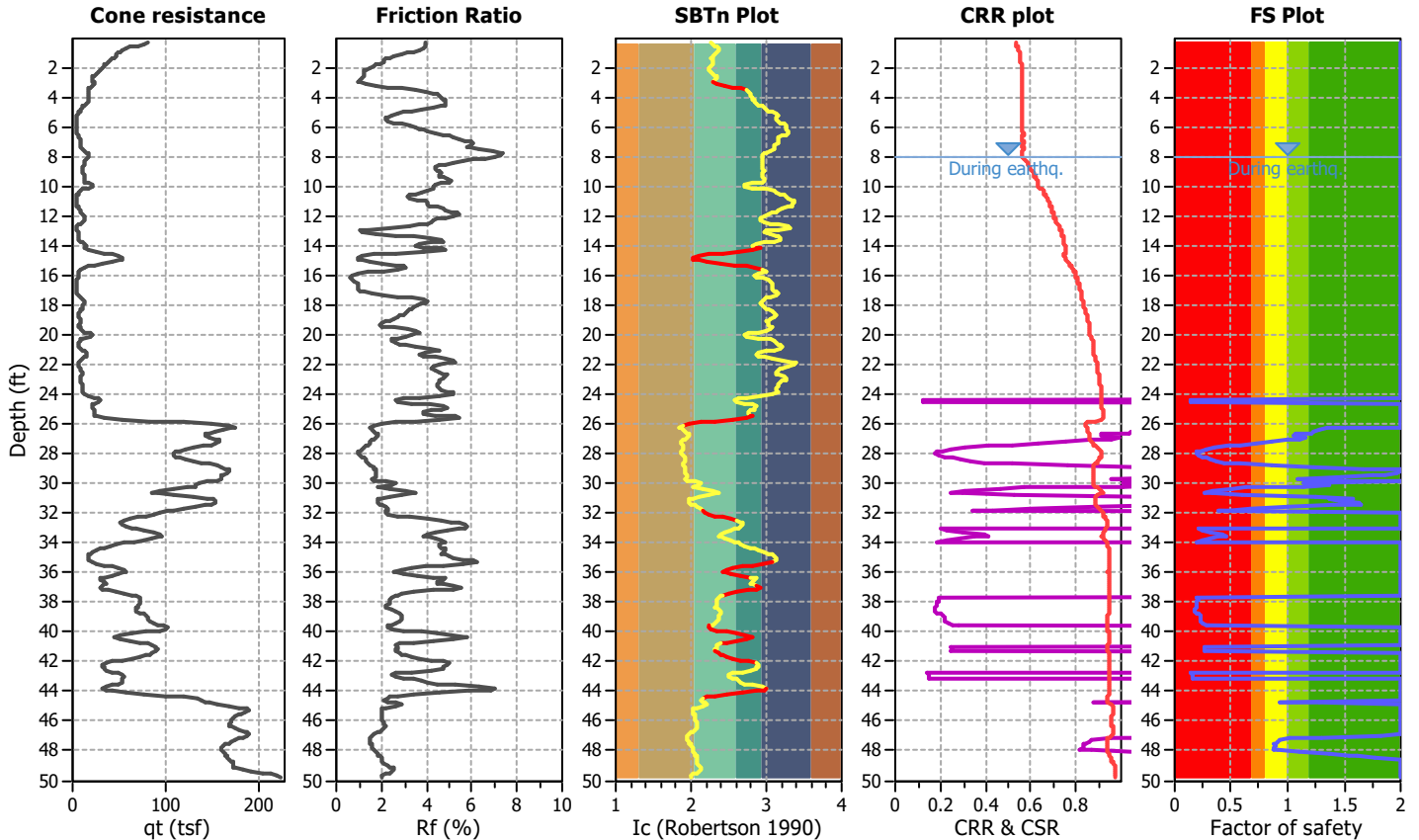
Project title : 21-483 Equestrian Estates

Location : Avenue 64 at Harrison Street, Thermal California

CPT file : CPT-8 B&I 2014

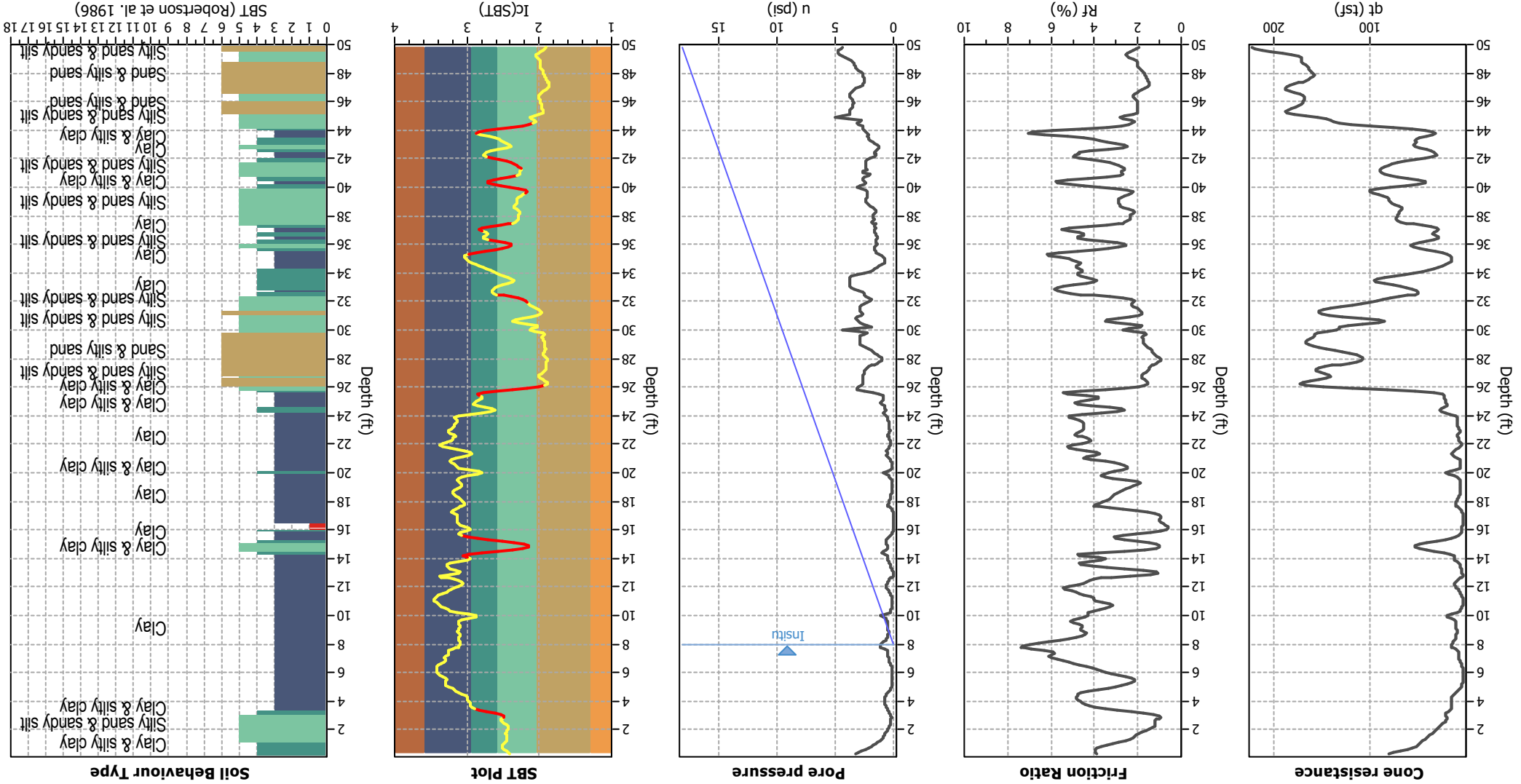
Input parameters and analysis data

Analysis method:	B&I (2014)	G.W.T. (in-situ):	8.00 ft	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	8.00 ft	Fill height:	N/A	Limit depth applied:	No
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth:	N/A
Earthquake magnitude M_w :	7.34	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.74	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		



Zone A₁: Cyclic liquefaction likely depending on size and duration of cyclic loading
 Zone A₂: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
 Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
 Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots

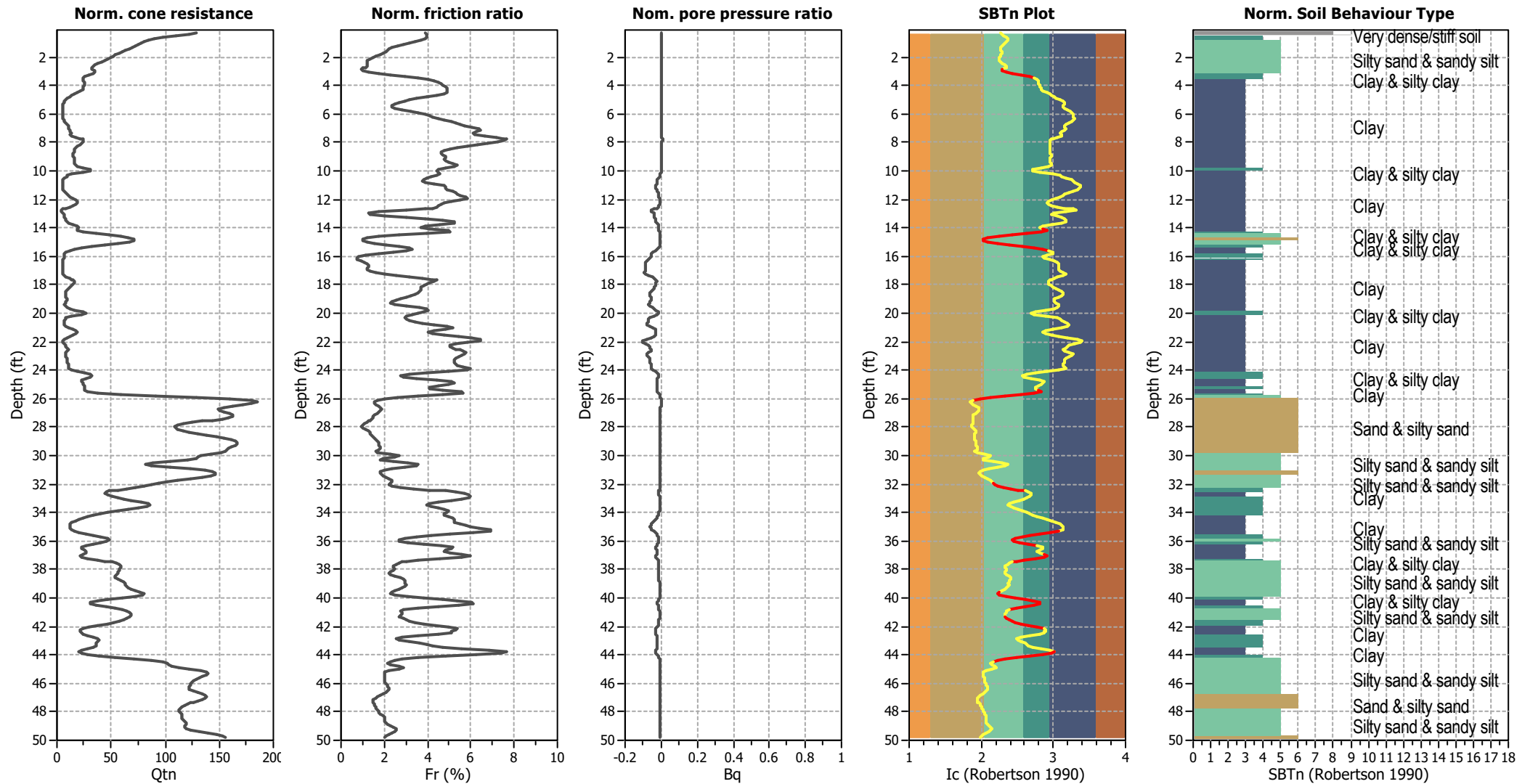


Input parameters and analysis data

Analysis method:	B&I (2014)
Fines correction method:	B&I (2014)
Points to test:	Based on I_c value
Earthquake magnitude M_w :	7.34
Peak ground acceleration:	0.74
Depth to water table (instu):	8.00 ft

Depth to GWT (erthq.):	8.00 ft
Average results interval:	3
I_c cut-off value:	2.60
Unit weight calculation:	Based on SBT
Use fill:	No
Fill height:	N/A
Fill weight:	N/A
Transition detect. applied:	Yes
K_0 applied:	Yes
Clay like behavior applied:	Sands only
Limit depth applied:	No
Limit depth:	N/A

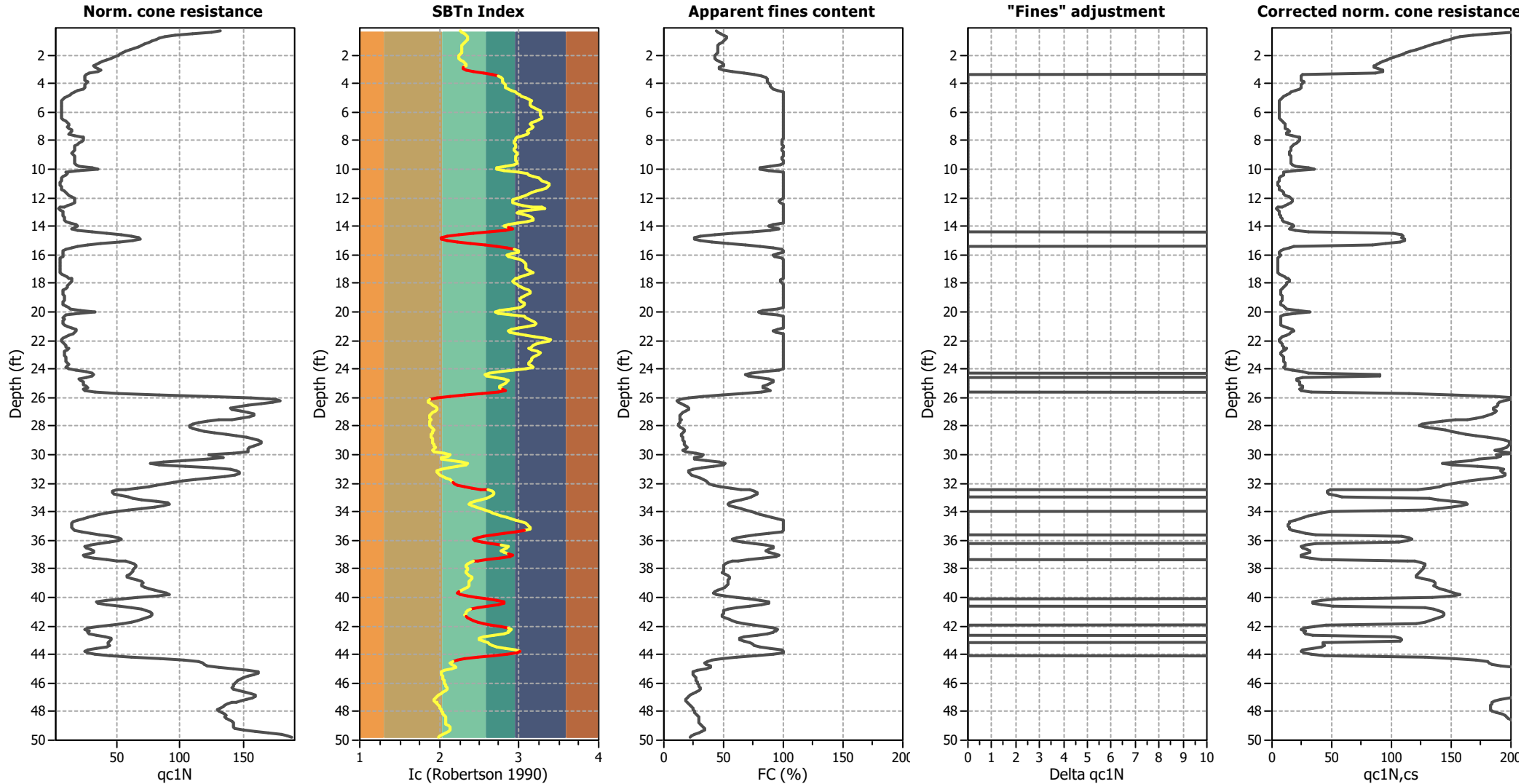
CPT basic interpretation plots (normalized)



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _o applied:	Yes
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

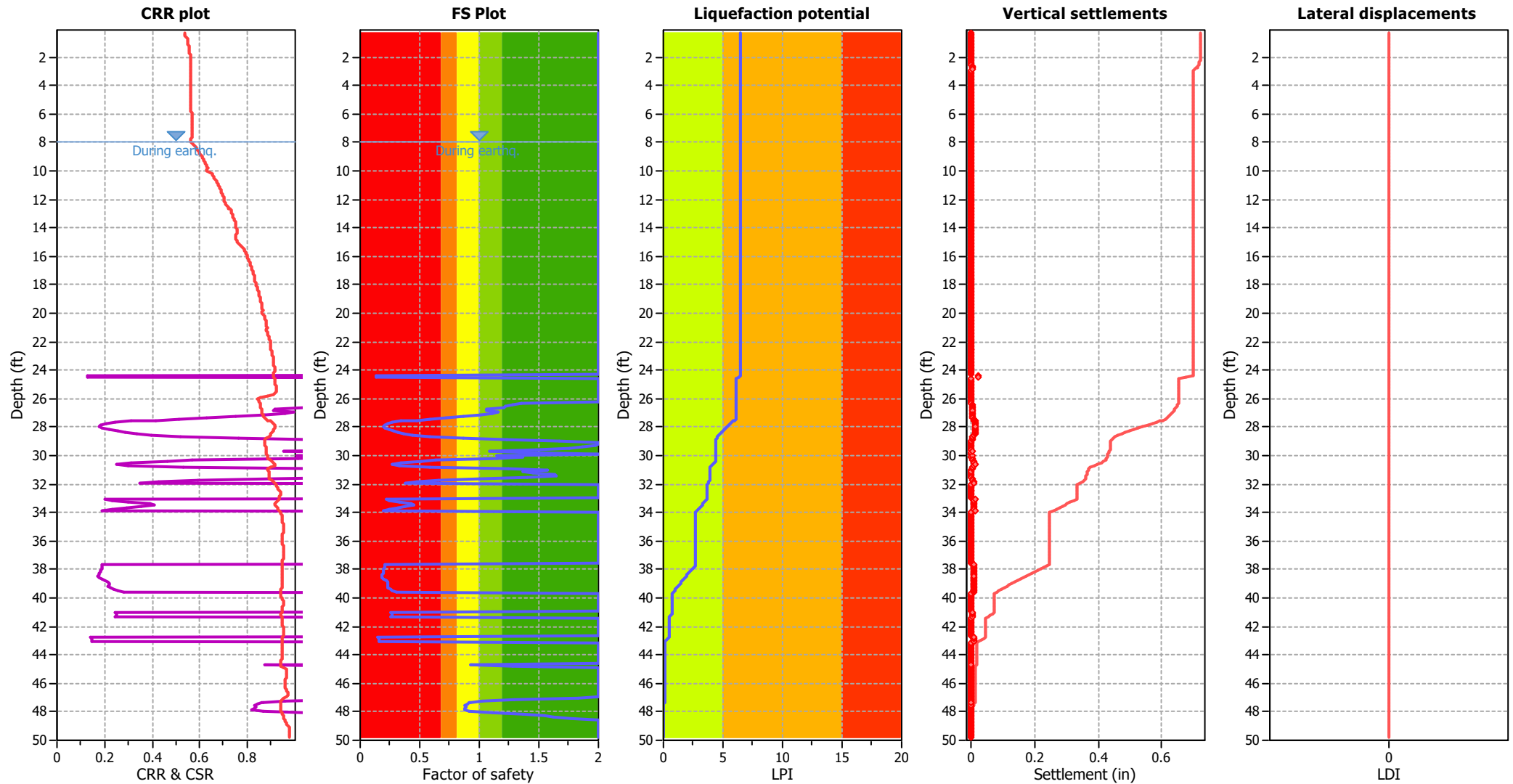
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _g applied:	Yes
Earthquake magnitude M _w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method: B&I (2014)
 Fines correction method: B&I (2014)
 Points to test: Based on I_c value
 Earthquake magnitude M_w : 7.34
 Peak ground acceleration: 0.74
 Depth to water table (insitu): 8.00 ft

Depth to GWT (earthq.): 8.00 ft
 Average results interval: 3
 I_c cut-off value: 2.60
 Unit weight calculation: Based on SBT
 Use fill: No
 Fill height: N/A

Fill weight: N/A
 Transition detect. applied: Yes
 K_{σ} applied: Yes
 Clay like behavior applied: Sands only
 Limit depth applied: No
 Limit depth: N/A

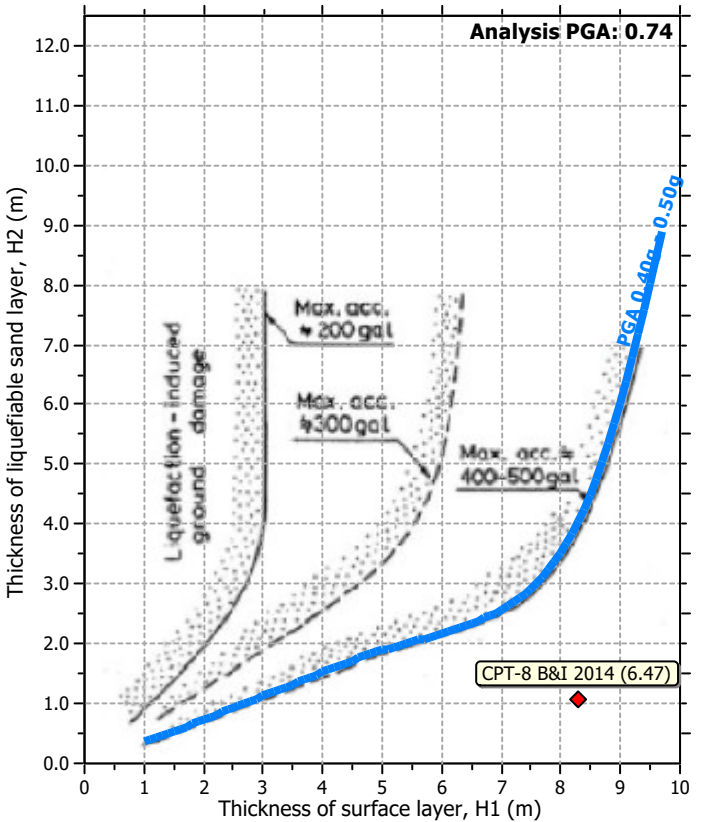
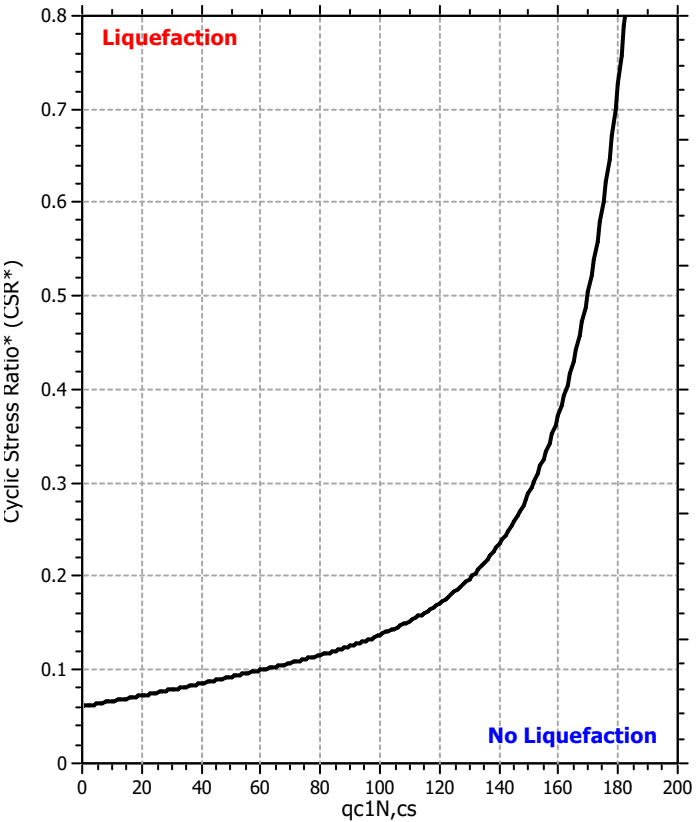
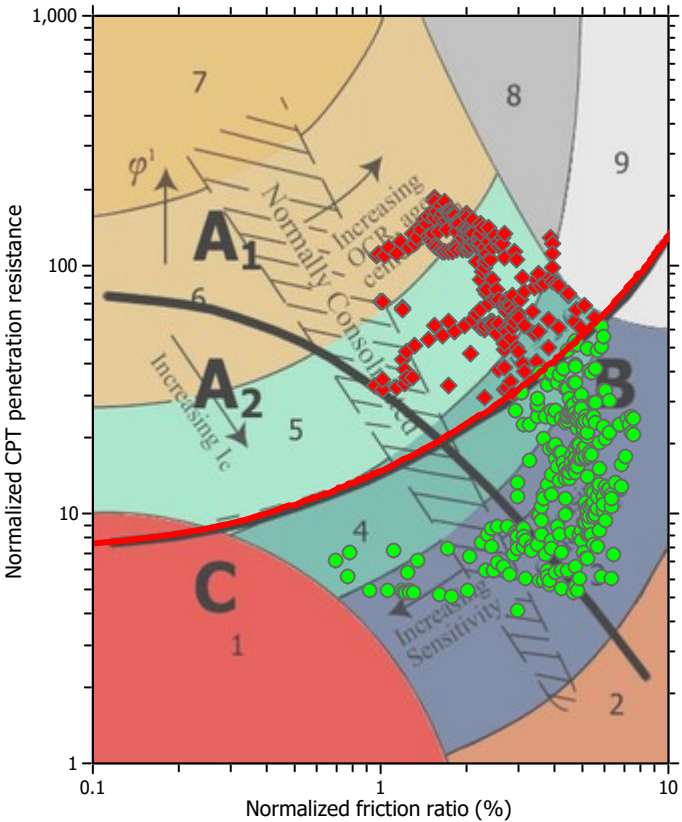
F.S. color scheme

■ Almost certain it will liquefy
■ Very likely to liquefy
■ Liquefaction and no liq. are equally likely
■ Unlikely to liquefy
■ Almost certain it will not liquefy

LPI color scheme

■ Very high risk
■ High risk
■ Low risk

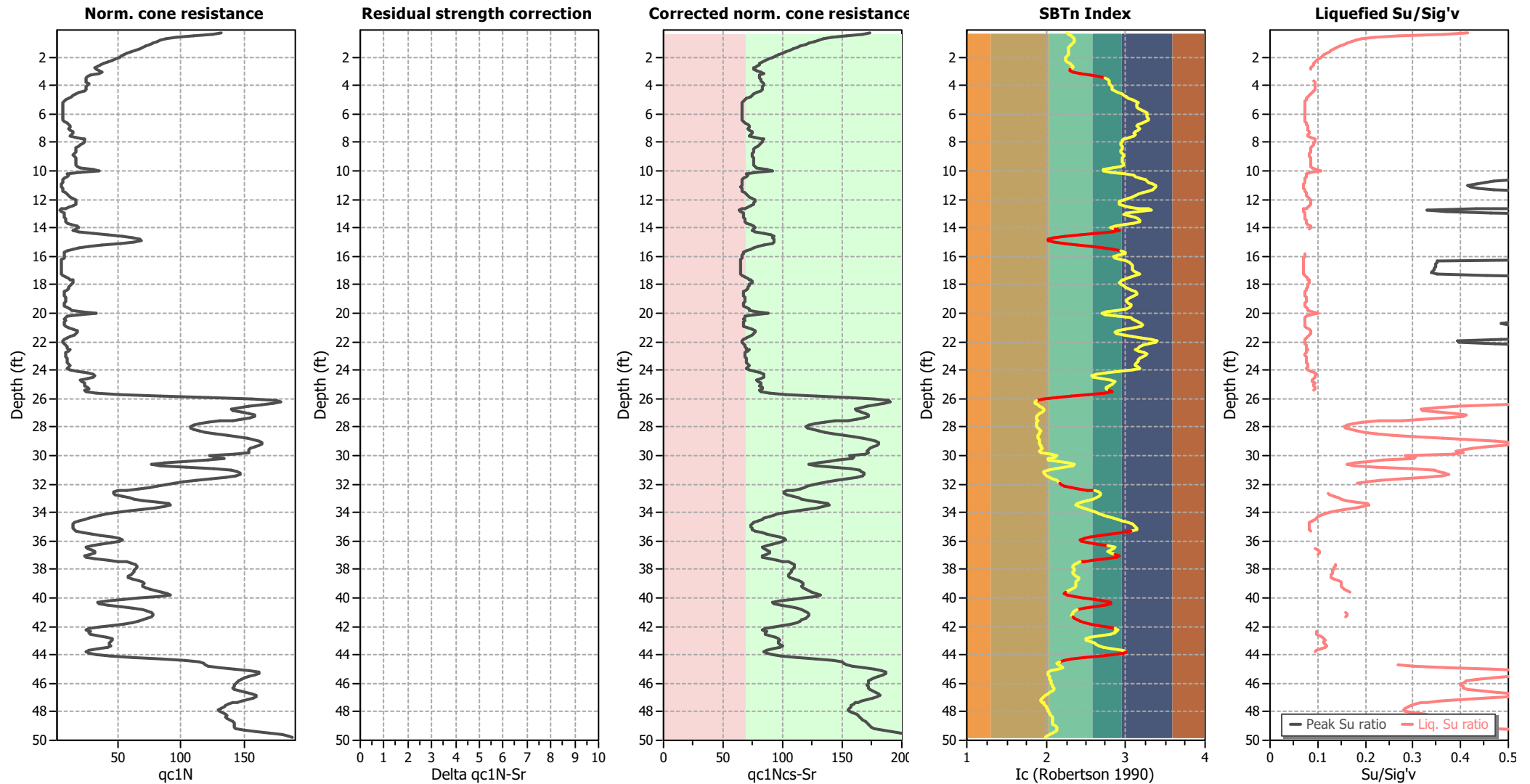
Liquefaction analysis summary plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on I_c value	I_c cut-off value:	2.60	K_{ϕ} applied:	Yes
Earthquake magnitude M_w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

Check for strength loss plots (Idriss & Boulanger (2008))



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w :	7.34	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.74	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	8.00 ft	Fill height:	N/A	Limit depth:	N/A

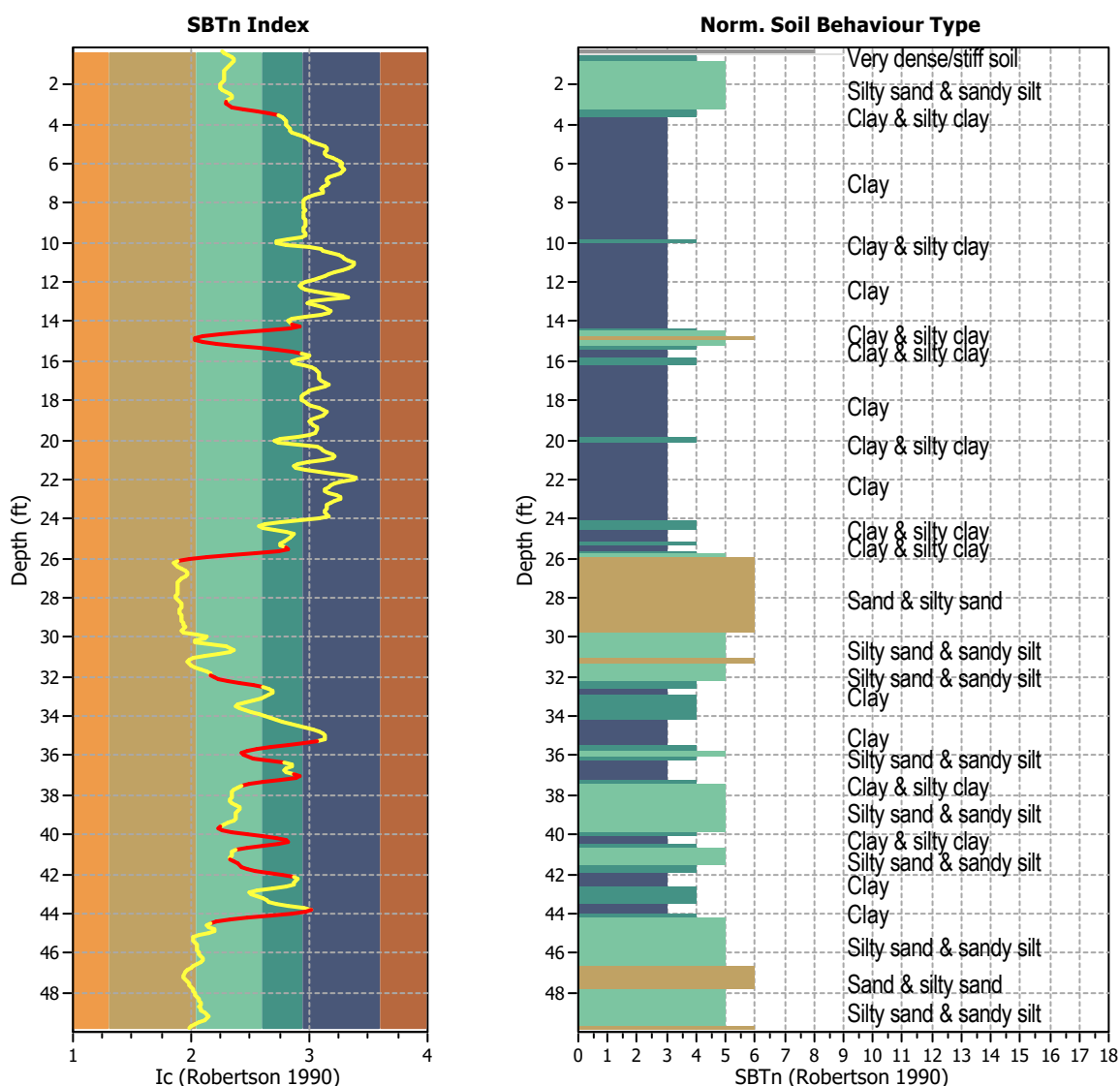
TRANSITION LAYER DETECTION ALGORITHM REPORT

Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vice-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between $1.80 < I_c < 3.0$) and a rate of change of I_c . Transitions typically occur when the rate of change of I_c is fast (i.e. ΔI_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties

I_c minimum check value: 1.70
 I_c maximum check value: 3.00
 I_c change ratio value: 0.0250
 Minimum number of points in layer: 4

General statistics

Total points in CPT file: 496
 Total points excluded: 86
 Exclusion percentage: 17.34%
 Number of layers detected: 12

Transition layer No	Number of points	Depth	SBT _n number	SBT _n description
Transition layer 1	7	Start depth: 3.00 (ft)	5	Silty sand & sandy silt
		End depth: 3.60 (ft)	4	Clay & silty clay
Transition layer 2	7	Start depth: 14.20 (ft)	3	Clay
		End depth: 14.80 (ft)	6	Sand & silty sand
Transition layer 3	9	Start depth: 14.90 (ft)	6	Sand & silty sand
		End depth: 15.70 (ft)	3	Clay
Transition layer 4	8	Start depth: 25.50 (ft)	3	Clay
		End depth: 26.20 (ft)	6	Sand & silty sand
Transition layer 5	7	Start depth: 32.00 (ft)	5	Silty sand & sandy silt
		End depth: 32.60 (ft)	4	Clay & silty clay
Transition layer 6	6	Start depth: 35.40 (ft)	3	Clay
		End depth: 35.90 (ft)	5	Silty sand & sandy silt
Transition layer 7	5	Start depth: 36.00 (ft)	5	Silty sand & sandy silt
		End depth: 36.40 (ft)	3	Clay
Transition layer 8	7	Start depth: 37.00 (ft)	3	Clay
		End depth: 37.60 (ft)	5	Silty sand & sandy silt
Transition layer 9	7	Start depth: 39.70 (ft)	5	Silty sand & sandy silt
		End depth: 40.30 (ft)	3	Clay
Transition layer 10	6	Start depth: 40.40 (ft)	3	Clay
		End depth: 40.90 (ft)	5	Silty sand & sandy silt
Transition layer 11	9	Start depth: 41.40 (ft)	5	Silty sand & sandy silt
		End depth: 42.20 (ft)	3	Clay
Transition layer 12	8	Start depth: 43.90 (ft)	3	Clay
		End depth: 44.60 (ft)	5	Silty sand & sandy silt

Start depth: Depth where the transition layer begins

End depth: Depth where the transition layer ends

:: Field input data ::						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1	0.30	81.74	3.21	3.21	21.25	129.38
2	0.40	78.01	3.05	3.05	21.85	128.86
3	0.50	68.49	2.73	2.73	22.92	127.94
4	0.60	60.12	2.42	2.42	24.19	126.78
5	0.70	54.52	2.13	2.13	24.90	125.70
6	0.80	52.21	1.93	1.93	24.92	124.74
7	0.90	50.28	1.73	1.73	24.49	123.84
8	1.00	48.32	1.53	1.53	23.85	122.87
9	1.10	46.83	1.34	1.34	23.11	121.79
10	1.20	44.95	1.15	1.15	22.28	120.68
11	1.30	43.53	1.00	1.00	21.68	119.62
12	1.40	41.68	0.91	0.91	21.51	118.78
13	1.50	39.61	0.86	0.86	21.71	118.06
14	1.60	37.60	0.78	0.78	21.93	117.27
15	1.70	35.58	0.69	0.69	21.93	116.30
16	1.80	33.68	0.61	0.61	21.70	115.25
17	1.90	32.56	0.53	0.53	21.25	114.15
18	2.00	31.45	0.46	0.46	20.71	112.92
19	2.10	29.55	0.38	0.38	20.32	111.66
20	2.20	28.10	0.33	0.33	20.40	110.49
21	2.30	26.06	0.30	0.30	21.12	109.59
22	2.40	23.60	0.28	0.28	22.26	108.90
23	2.50	22.19	0.27	0.27	23.41	108.24
24	2.60	20.77	0.25	0.25	24.07	107.55
25	2.70	19.84	0.23	0.23	24.05	106.68
26	2.80	19.71	0.20	0.20	23.23	105.86
27	2.90	20.36	0.18	0.18	22.18	105.63
28	3.00	21.73	0.20	0.20	22.16	106.69
29	3.10	22.91	0.28	0.28	24.06	108.64
30	3.20	21.66	0.38	0.38	27.88	110.11
31	3.30	17.70	0.41	0.41	33.12	111.08
32	3.40	16.02	0.48	0.48	38.54	111.65
33	3.50	15.13	0.54	0.54	42.14	112.42
34	3.60	15.13	0.60	0.60	44.42	113.12
35	3.70	15.13	0.65	0.65	45.53	113.76
36	3.80	15.51	0.70	0.70	45.72	114.36
37	3.90	16.46	0.75	0.75	45.72	114.71
38	4.00	16.06	0.74	0.74	46.26	114.80
39	4.10	15.15	0.73	0.73	47.24	114.73
40	4.20	15.17	0.74	0.74	47.69	114.70
41	4.30	15.53	0.74	0.74	47.99	114.51
42	4.40	14.36	0.69	0.69	49.43	113.76
43	4.50	11.94	0.58	0.58	52.41	112.33
44	4.60	9.91	0.47	0.47	55.53	110.48
45	4.70	8.82	0.38	0.38	57.33	108.49
46	4.80	7.90	0.29	0.29	58.93	106.19
47	4.90	6.23	0.20	0.20	61.10	103.67
48	5.00	5.29	0.16	0.16	64.73	100.89

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
49	5.10	4.35	0.12	0.12	67.60	98.72
50	5.20	3.98	0.10	0.10	69.17	97.05
51	5.30	3.98	0.09	0.09	68.76	96.14
52	5.40	3.98	0.08	0.08	67.86	95.71
53	5.50	3.98	0.08	0.08	67.86	95.69
54	5.60	3.98	0.09	0.09	69.26	96.09
55	5.70	3.89	0.10	0.10	72.18	96.65
56	5.80	3.65	0.11	0.11	75.63	97.20
57	5.90	3.58	0.12	0.12	78.05	97.88
58	6.00	3.78	0.13	0.13	78.66	98.76
59	6.10	3.98	0.15	0.15	78.62	99.49
60	6.20	3.98	0.15	0.15	79.00	99.99
61	6.30	3.98	0.16	0.16	80.05	100.35
62	6.40	3.98	0.17	0.17	79.80	101.33
63	6.50	4.60	0.22	0.22	77.55	102.99
64	6.60	5.51	0.27	0.27	73.78	104.94
65	6.70	6.40	0.33	0.33	70.42	106.67
66	6.80	7.17	0.38	0.38	68.99	107.80
67	6.90	7.17	0.41	0.41	69.51	108.40
68	7.00	6.85	0.42	0.42	70.63	108.75
69	7.10	7.14	0.44	0.44	69.18	109.49
70	7.20	8.58	0.51	0.51	66.53	110.11
71	7.30	8.76	0.50	0.50	65.33	110.23
72	7.40	7.87	0.45	0.45	66.61	109.93
73	7.50	7.62	0.47	0.47	66.10	111.21
74	7.60	10.70	0.73	0.73	62.19	114.09
75	7.70	14.62	1.07	1.07	58.29	116.57
76	7.80	15.53	1.17	1.17	56.26	117.80
77	7.90	15.53	1.14	1.14	55.63	117.89
78	8.00	15.49	1.09	1.09	55.20	117.40
79	8.10	14.67	0.97	0.97	54.96	116.50
80	8.20	13.50	0.82	0.82	54.98	115.20
81	8.30	12.44	0.69	0.69	55.49	113.68
82	8.40	11.03	0.57	0.57	55.81	112.36
83	8.50	10.75	0.52	0.52	55.74	111.37
84	8.60	10.75	0.49	0.49	55.03	110.85
85	8.70	10.65	0.46	0.46	55.00	110.34
86	8.80	9.95	0.43	0.43	55.83	109.91
87	8.90	9.56	0.43	0.43	56.83	109.87
88	9.00	9.98	0.47	0.47	56.73	110.29
89	9.10	10.67	0.50	0.50	55.84	110.67
90	9.20	10.75	0.48	0.48	55.07	110.82
91	9.30	10.75	0.48	0.48	55.08	110.87
92	9.40	10.75	0.51	0.51	55.70	111.11
93	9.50	10.75	0.53	0.53	56.56	111.44
94	9.60	10.75	0.55	0.55	56.45	111.95
95	9.70	11.72	0.61	0.61	54.18	112.63
96	9.80	13.65	0.65	0.65	47.47	114.64

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
97	9.90	21.35	0.93	0.93	41.59	116.71
98	10.00	25.42	1.08	1.08	41.25	116.55
99	10.10	13.64	0.59	0.59	46.58	113.82
100	10.20	6.62	0.30	0.30	58.29	108.76
101	10.30	6.97	0.28	0.28	65.67	105.35
102	10.40	6.44	0.23	0.23	67.16	103.82
103	10.50	4.76	0.17	0.17	71.57	101.54
104	10.60	3.98	0.13	0.13	76.71	99.38
105	10.70	3.98	0.12	0.12	78.76	98.41
106	10.80	3.88	0.12	0.12	80.56	98.35
107	10.90	3.64	0.13	0.13	84.09	98.75
108	11.00	3.58	0.15	0.15	87.16	99.13
109	11.10	3.58	0.15	0.15	87.18	99.46
110	11.20	3.80	0.15	0.15	85.73	99.79
111	11.30	3.98	0.16	0.16	83.86	100.64
112	11.40	4.34	0.19	0.19	79.81	102.69
113	11.50	5.78	0.28	0.28	74.09	104.94
114	11.60	7.01	0.34	0.34	69.71	106.60
115	11.70	7.17	0.35	0.35	67.27	108.03
116	11.80	8.17	0.45	0.45	64.67	109.77
117	11.90	10.23	0.58	0.58	60.46	111.52
118	12.00	11.87	0.62	0.62	56.55	112.34
119	12.10	12.07	0.57	0.57	53.86	112.32
120	12.20	12.17	0.54	0.54	52.83	111.81
121	12.30	11.71	0.51	0.51	53.72	110.91
122	12.40	9.82	0.41	0.41	56.57	109.33
123	12.50	7.81	0.31	0.31	61.74	106.80
124	12.60	5.80	0.21	0.21	69.31	103.30
125	12.70	3.78	0.12	0.12	79.65	98.80
126	12.80	2.58	0.06	0.06	83.04	94.35
127	12.90	3.41	0.05	0.05	70.39	91.57
128	13.00	4.76	0.04	0.04	59.31	91.21
129	13.10	4.78	0.04	0.04	57.21	92.87
130	13.20	4.78	0.08	0.08	62.41	96.06
131	13.30	5.04	0.13	0.13	66.89	99.65
132	13.40	5.75	0.20	0.20	69.32	102.34
133	13.50	5.97	0.25	0.25	71.03	104.19
134	13.60	5.97	0.28	0.28	70.84	105.90
135	13.70	7.27	0.36	0.36	65.93	107.69
136	13.80	9.56	0.43	0.43	56.74	109.49
137	13.90	12.84	0.46	0.46	49.36	110.45
138	14.00	14.00	0.44	0.44	46.80	110.79
139	14.10	12.41	0.46	0.46	49.56	111.00
140	14.20	10.88	0.53	0.53	52.76	112.57
141	14.30	14.45	0.78	0.78	47.64	115.21
142	14.40	23.31	1.02	1.02	37.19	117.24
143	14.50	33.06	0.91	0.91	27.67	117.74
144	14.60	42.36	0.66	0.66	20.37	116.81

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
145	14.70	49.23	0.54	0.54	15.71	115.61
146	14.80	53.79	0.50	0.50	13.74	115.19
147	14.90	54.94	0.53	0.53	13.74	115.34
148	15.00	50.74	0.57	0.57	15.63	115.76
149	15.10	42.11	0.64	0.64	19.63	115.78
150	15.20	29.95	0.64	0.64	25.79	115.14
151	15.30	20.82	0.58	0.58	33.83	113.62
152	15.40	14.75	0.48	0.48	41.79	111.37
153	15.50	10.94	0.34	0.34	48.93	108.28
154	15.60	7.68	0.20	0.20	54.68	104.36
155	15.70	5.86	0.12	0.12	58.48	99.84
156	15.80	5.16	0.07	0.07	57.65	95.64
157	15.90	5.11	0.04	0.04	52.37	92.42
158	16.00	5.81	0.03	0.03	49.10	89.90
159	16.10	5.09	0.03	0.03	50.06	88.22
160	16.20	3.98	0.02	0.02	54.76	87.36
161	16.30	3.98	0.03	0.03	59.85	87.62
162	16.40	3.98	0.03	0.03	61.77	88.71
163	16.50	3.98	0.04	0.04	63.29	89.52
164	16.60	3.98	0.04	0.04	64.12	89.92
165	16.70	3.98	0.04	0.04	64.25	89.92
166	16.80	3.98	0.04	0.04	63.85	89.63
167	16.90	3.98	0.04	0.04	63.83	89.56
168	17.00	3.98	0.04	0.04	65.08	90.17
169	17.10	3.98	0.05	0.05	68.33	91.47
170	17.20	3.86	0.06	0.06	70.67	93.57
171	17.30	4.40	0.08	0.08	67.25	97.69
172	17.40	6.80	0.17	0.17	62.58	102.17
173	17.50	8.41	0.28	0.28	58.86	106.03
174	17.60	9.78	0.38	0.38	57.25	108.60
175	17.70	10.96	0.46	0.46	55.50	110.02
176	17.80	11.67	0.47	0.47	53.95	110.39
177	17.90	11.51	0.43	0.43	53.68	109.82
178	18.00	10.29	0.37	0.37	54.59	108.84
179	18.10	9.55	0.33	0.33	56.29	107.67
180	18.20	8.88	0.29	0.29	57.83	106.64
181	18.30	8.19	0.26	0.26	60.14	105.53
182	18.40	7.20	0.23	0.23	63.63	104.27
183	18.50	6.18	0.19	0.19	66.82	103.00
184	18.60	5.97	0.17	0.17	68.39	102.02
185	18.70	5.97	0.17	0.17	68.06	101.63
186	18.80	6.02	0.17	0.17	66.02	101.72
187	18.90	6.71	0.17	0.17	62.97	101.87
188	19.00	7.17	0.17	0.17	60.06	101.90
189	19.10	7.17	0.16	0.16	58.89	101.31
190	19.20	6.71	0.13	0.13	59.38	100.10
191	19.30	6.02	0.11	0.11	60.64	99.08
192	19.40	5.97	0.11	0.11	62.91	99.35

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
193	19.50	6.18	0.15	0.15	63.55	101.90
194	19.60	7.79	0.24	0.24	61.83	105.03
195	19.70	9.59	0.34	0.34	58.88	107.55
196	19.80	10.58	0.40	0.40	51.80	111.02
197	19.90	18.07	0.68	0.68	43.18	114.48
198	20.00	27.47	0.93	0.93	40.41	115.05
199	20.10	16.74	0.49	0.49	42.62	112.73
200	20.20	8.02	0.21	0.21	51.99	106.77
201	20.30	6.61	0.16	0.16	62.53	102.26
202	20.40	6.36	0.16	0.16	65.06	101.55
203	20.50	6.57	0.17	0.17	67.05	101.55
204	20.60	6.00	0.16	0.16	69.15	101.85
205	20.70	5.97	0.18	0.18	72.33	102.25
206	20.80	5.97	0.20	0.20	74.07	103.47
207	20.90	6.45	0.26	0.26	72.52	105.95
208	21.00	8.57	0.41	0.41	66.18	109.02
209	21.10	11.84	0.55	0.55	57.80	111.36
210	21.20	14.73	0.58	0.58	51.72	112.42
211	21.30	15.49	0.54	0.54	49.60	112.48
212	21.40	14.13	0.54	0.54	51.35	112.32
213	21.50	12.74	0.56	0.56	56.59	111.91
214	21.60	10.38	0.52	0.52	63.97	110.83
215	21.70	7.70	0.41	0.41	73.18	108.98
216	21.80	6.13	0.33	0.33	83.52	106.51
217	21.90	4.78	0.24	0.24	89.71	104.59
218	22.00	4.92	0.22	0.22	87.27	104.03
219	22.10	6.30	0.27	0.27	79.96	104.90
220	22.20	7.17	0.30	0.30	74.17	106.10
221	22.30	7.68	0.32	0.32	71.80	106.93
222	22.40	7.96	0.35	0.35	70.30	107.82
223	22.50	8.72	0.40	0.40	67.96	109.16
224	22.60	10.30	0.49	0.49	67.54	109.84
225	22.70	9.08	0.45	0.45	70.08	109.40
226	22.80	7.05	0.35	0.35	74.88	108.04
227	22.90	6.92	0.33	0.33	78.39	106.75
228	23.00	6.72	0.30	0.30	77.43	106.64
229	23.10	7.30	0.33	0.33	74.19	107.40
230	23.20	8.76	0.40	0.40	71.27	108.25
231	23.30	8.76	0.40	0.40	69.36	108.78
232	23.40	8.76	0.39	0.39	69.35	108.74
233	23.50	8.76	0.39	0.39	68.89	108.99
234	23.60	9.31	0.43	0.43	67.52	109.61
235	23.70	10.24	0.48	0.48	67.37	109.98
236	23.80	9.37	0.45	0.45	69.28	109.99
237	23.90	8.47	0.44	0.44	70.51	110.49
238	24.00	10.37	0.57	0.57	64.21	112.50
239	24.10	15.82	0.79	0.79	52.77	114.99
240	24.20	22.90	0.90	0.90	43.04	116.41

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
241	24.30	27.66	0.79	0.79	36.58	116.48
242	24.40	28.65	0.67	0.67	33.78	116.09
243	24.50	27.94	0.73	0.73	35.34	115.98
244	24.60	23.58	0.79	0.79	40.49	116.08
245	24.70	18.54	0.80	0.80	46.65	116.41
246	24.80	19.18	0.95	0.95	49.70	117.11
247	24.90	21.65	1.08	1.08	49.13	117.77
248	25.00	21.56	1.01	1.01	47.87	117.73
249	25.10	20.95	0.90	0.90	45.70	117.29
250	25.20	23.57	0.88	0.88	43.41	116.98
251	25.30	24.32	0.86	0.86	43.33	117.06
252	25.40	21.49	0.92	0.92	45.90	117.88
253	25.50	22.36	1.21	1.21	47.32	120.05
254	25.60	30.43	1.78	1.78	42.16	123.24
255	25.70	48.12	2.48	2.48	32.58	126.49
256	25.80	80.56	3.06	3.06	23.48	128.81
257	25.90	119.40	3.14	3.14	16.76	130.10
258	26.00	153.29	2.99	2.99	12.37	130.36
259	26.10	172.88	2.69	2.69	10.08	130.23
260	26.20	176.79	2.63	2.63	9.27	129.99
261	26.30	171.15	2.63	2.63	9.47	129.83
262	26.40	161.95	2.58	2.58	10.14	129.67
263	26.50	152.17	2.59	2.59	10.97	129.51
264	26.60	144.69	2.62	2.62	11.81	129.42
265	26.70	138.95	2.61	2.61	12.26	129.34
266	26.80	140.03	2.57	2.57	12.12	129.29
267	26.90	146.85	2.55	2.55	11.51	129.26
268	27.00	152.97	2.50	2.50	10.81	129.23
269	27.10	157.26	2.44	2.44	10.25	129.07
270	27.20	157.72	2.33	2.33	9.95	128.80
271	27.30	154.12	2.23	2.23	9.90	128.40
272	27.40	147.65	2.11	2.11	9.99	127.83
273	27.50	140.17	1.91	1.91	10.10	126.96
274	27.60	129.80	1.64	1.64	10.11	125.81
275	27.70	120.61	1.40	1.40	10.05	124.48
276	27.80	113.32	1.19	1.19	9.89	123.19
277	27.90	108.27	1.03	1.03	9.68	122.17
278	28.00	106.54	0.97	0.97	9.69	121.79
279	28.10	106.79	1.05	1.05	10.09	122.31
280	28.20	109.71	1.25	1.25	10.63	123.30
281	28.30	114.29	1.42	1.42	11.00	124.35
282	28.40	119.65	1.57	1.57	10.96	125.22
283	28.50	128.28	1.70	1.70	10.67	125.98
284	28.60	137.15	1.83	1.83	10.39	126.85
285	28.70	146.48	2.08	2.08	10.34	127.83
286	28.80	154.57	2.37	2.37	10.50	128.82
287	28.90	160.11	2.62	2.62	10.70	129.63
288	29.00	164.67	2.81	2.81	10.84	130.18

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
289	29.10	167.60	2.89	2.89	10.88	130.47
290	29.20	168.14	2.90	2.90	10.91	130.52
291	29.30	165.83	2.86	2.86	11.07	130.46
292	29.40	161.84	2.86	2.86	11.39	130.43
293	29.50	158.94	2.93	2.93	11.62	130.35
294	29.60	157.73	2.81	2.81	11.42	130.04
295	29.70	158.42	2.53	2.53	10.77	129.41
296	29.80	158.37	2.25	2.25	11.37	129.56
297	29.90	146.79	3.03	3.03	14.43	130.94
298	30.00	126.66	4.37	4.37	16.73	131.62
299	30.10	131.94	3.40	3.40	16.05	130.77
300	30.20	138.08	1.92	1.92	13.72	128.89
301	30.30	125.14	2.19	2.19	13.80	127.88
302	30.40	107.71	2.57	2.57	17.67	128.48
303	30.50	89.25	2.84	2.84	22.06	128.79
304	30.60	78.49	2.94	2.94	24.80	129.08
305	30.70	86.50	3.15	3.15	23.74	129.59
306	30.80	107.64	3.26	3.26	19.92	130.13
307	30.90	131.67	3.08	3.08	16.05	130.19
308	31.00	146.55	2.71	2.71	13.50	129.96
309	31.10	151.34	2.67	2.67	12.36	129.81
310	31.20	153.69	2.77	2.77	12.24	129.97
311	31.30	154.10	2.84	2.84	12.50	130.15
312	31.40	150.62	2.88	2.88	13.07	130.20
313	31.50	142.50	2.91	2.91	14.06	130.11
314	31.60	130.52	2.88	2.88	15.43	129.84
315	31.70	117.89	2.79	2.79	16.75	129.26
316	31.80	107.64	2.51	2.51	17.61	128.40
317	31.90	100.35	2.19	2.19	18.03	127.34
318	32.00	93.07	1.96	1.96	18.63	126.47
319	32.10	85.80	1.91	1.91	20.12	126.15
320	32.20	79.35	2.08	2.08	22.89	126.36
321	32.30	70.33	2.32	2.32	26.83	126.70
322	32.40	60.04	2.47	2.47	31.50	126.82
323	32.50	52.30	2.52	2.52	35.65	126.73
324	32.60	49.20	2.54	2.54	38.33	126.73
325	32.70	48.98	2.65	2.65	39.64	127.11
326	32.80	50.77	2.96	2.96	39.62	127.93
327	32.90	56.84	3.36	3.36	38.55	128.88
328	33.00	62.92	3.60	3.60	36.88	129.62
329	33.10	66.85	3.69	3.69	34.75	130.13
330	33.20	74.49	3.78	3.78	31.87	130.52
331	33.30	86.21	3.80	3.80	28.55	130.84
332	33.40	96.39	3.72	3.72	26.19	131.01
333	33.50	98.33	3.71	3.71	25.56	131.05
334	33.60	93.15	3.77	3.77	26.62	130.99
335	33.70	85.71	3.79	3.79	28.77	130.69
336	33.80	75.23	3.57	3.57	31.34	129.93

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
337	33.90	63.53	3.10	3.10	34.02	128.63
338	34.00	53.49	2.54	2.54	36.51	126.89
339	34.10	45.17	2.05	2.05	38.72	125.11
340	34.20	39.58	1.76	1.76	41.35	123.55
341	34.30	33.92	1.59	1.59	44.73	122.28
342	34.40	28.70	1.42	1.42	48.51	121.08
343	34.50	25.40	1.25	1.25	52.18	119.52
344	34.60	20.92	0.96	0.96	56.09	117.63
345	34.70	16.63	0.76	0.76	60.45	115.91
346	34.80	15.71	0.76	0.76	64.53	115.03
347	34.90	15.13	0.77	0.77	66.36	115.00
348	35.00	15.13	0.78	0.78	67.30	115.24
349	35.10	15.54	0.84	0.84	68.13	115.97
350	35.20	16.16	1.00	1.00	67.91	117.28
351	35.30	18.48	1.22	1.22	63.29	119.11
352	35.40	25.08	1.48	1.48	55.41	120.64
353	35.50	31.71	1.53	1.53	46.68	121.88
354	35.60	40.14	1.59	1.59	39.13	122.74
355	35.70	50.05	1.68	1.68	33.50	123.32
356	35.80	56.32	1.61	1.61	29.53	123.45
357	35.90	59.66	1.47	1.47	27.66	123.03
358	36.00	56.36	1.36	1.36	28.38	122.66
359	36.10	49.18	1.45	1.45	32.03	122.45
360	36.20	40.79	1.52	1.52	38.12	122.15
361	36.30	32.02	1.45	1.45	44.90	121.54
362	36.40	27.29	1.37	1.37	49.46	121.00
363	36.50	28.65	1.39	1.39	49.23	121.00
364	36.60	32.59	1.45	1.45	46.44	121.50
365	36.70	35.56	1.53	1.53	44.90	122.07
366	36.80	35.36	1.64	1.64	46.16	122.37
367	36.90	31.38	1.65	1.65	49.80	122.21
368	37.00	26.96	1.57	1.57	53.00	121.80
369	37.10	27.42	1.52	1.52	50.78	121.85
370	37.20	35.85	1.61	1.61	43.20	122.33
371	37.30	46.57	1.57	1.57	35.37	122.94
372	37.40	56.16	1.54	1.54	30.19	123.55
373	37.50	63.66	1.72	1.72	27.51	124.26
374	37.60	68.39	1.84	1.84	25.97	124.79
375	37.70	71.99	1.78	1.78	24.79	124.85
376	37.80	72.87	1.68	1.68	23.96	124.68
377	37.90	72.77	1.69	1.69	23.91	124.62
378	38.00	71.88	1.74	1.74	24.22	124.62
379	38.10	70.77	1.70	1.70	24.23	124.42
380	38.20	70.48	1.57	1.57	23.79	123.96
381	38.30	69.97	1.45	1.45	23.57	123.58
382	38.40	68.11	1.48	1.48	24.25	123.56
383	38.50	65.64	1.60	1.60	25.63	124.03
384	38.60	65.89	1.78	1.78	26.62	124.79

:: Field input data :: (continued)

Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
385	38.70	70.20	1.99	1.99	26.62	125.63
386	38.80	75.49	2.15	2.15	26.04	126.33
387	38.90	78.96	2.25	2.25	25.58	126.79
388	39.00	80.00	2.31	2.31	25.49	127.06
389	39.10	80.00	2.35	2.35	25.59	127.15
390	39.20	79.68	2.33	2.33	25.39	127.16
391	39.30	81.99	2.30	2.30	24.58	127.11
392	39.40	86.23	2.24	2.24	23.24	127.09
393	39.50	91.35	2.21	2.21	21.77	127.12
394	39.60	96.87	2.20	2.20	20.48	127.21
395	39.70	101.59	2.21	2.21	19.82	127.49
396	39.80	103.90	2.37	2.37	20.94	128.10
397	39.90	94.88	2.81	2.81	24.39	128.71
398	40.00	76.56	3.09	3.09	29.46	128.78
399	40.10	63.55	2.90	2.90	35.63	127.98
400	40.20	48.19	2.51	2.51	41.52	126.77
401	40.30	39.55	2.33	2.33	46.63	125.95
402	40.40	40.66	2.47	2.47	46.85	126.13
403	40.50	49.02	2.67	2.67	42.10	126.83
404	40.60	60.54	2.68	2.68	35.66	127.30
405	40.70	72.21	2.47	2.47	29.86	127.21
406	40.80	80.59	2.17	2.17	25.68	126.80
407	40.90	85.19	2.04	2.04	24.22	127.08
408	41.00	88.46	2.58	2.58	24.05	127.58
409	41.10	89.71	2.56	2.56	23.93	127.81
410	41.20	90.19	2.23	2.23	23.47	127.57
411	41.30	89.19	2.34	2.34	23.56	127.36
412	41.40	85.76	2.39	2.39	24.72	127.42
413	41.50	81.08	2.37	2.37	26.04	127.32
414	41.60	77.00	2.36	2.36	27.49	127.15
415	41.70	72.62	2.35	2.35	29.56	126.95
416	41.80	64.56	2.36	2.36	32.90	126.58
417	41.90	53.26	2.27	2.27	37.93	125.84
418	42.00	41.94	2.06	2.06	44.24	124.50
419	42.10	32.29	1.67	1.67	49.80	122.90
420	42.20	29.31	1.44	1.44	51.80	121.74
421	42.30	31.82	1.46	1.46	51.01	121.60
422	42.40	33.30	1.57	1.57	50.35	121.97
423	42.50	32.60	1.61	1.61	49.71	122.12
424	42.60	34.07	1.52	1.52	46.11	121.99
425	42.70	40.87	1.38	1.38	39.46	121.73
426	42.80	49.10	1.25	1.25	33.33	121.54
427	42.90	54.41	1.21	1.21	30.63	121.86
428	43.00	55.21	1.43	1.43	30.98	122.51
429	43.10	53.11	1.57	1.57	33.32	123.41
430	43.20	51.64	1.80	1.80	35.68	124.23
431	43.30	52.23	2.03	2.03	37.09	124.94
432	43.40	53.62	2.12	2.12	38.29	125.37

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
433	43.50	50.71	2.17	2.17	41.40	125.42
434	43.60	41.20	2.23	2.23	47.52	125.04
435	43.70	32.20	2.13	2.13	55.16	124.62
436	43.80	29.84	2.19	2.19	59.21	124.59
437	43.90	33.24	2.38	2.38	56.61	125.20
438	44.00	40.62	2.51	2.51	49.28	126.12
439	44.10	53.40	2.61	2.61	39.30	127.05
440	44.20	74.80	2.63	2.63	29.83	127.86
441	44.30	100.54	2.58	2.58	23.34	128.82
442	44.40	122.67	2.96	2.96	19.66	129.67
443	44.50	135.35	3.09	3.09	17.89	130.21
444	44.60	139.36	2.93	2.93	16.82	130.18
445	44.70	140.32	2.79	2.79	17.30	130.82
446	44.80	143.09	3.83	3.83	18.81	132.35
447	44.90	153.27	5.03	5.03	18.99	133.41
448	45.00	166.84	4.35	4.35	17.32	133.54
449	45.10	179.58	3.72	3.72	14.90	132.95
450	45.20	188.85	3.74	3.74	13.62	132.64
451	45.30	189.48	3.71	3.71	13.44	132.67
452	45.40	185.74	3.73	3.73	13.61	132.57
453	45.50	181.11	3.64	3.64	13.89	132.41
454	45.60	177.29	3.56	3.56	14.10	132.20
455	45.70	174.19	3.50	3.50	14.27	132.02
456	45.80	171.44	3.44	3.44	14.40	131.90
457	45.90	170.82	3.43	3.43	14.53	131.84
458	46.00	169.67	3.44	3.44	14.71	131.87
459	46.10	168.43	3.50	3.50	14.98	131.98
460	46.20	168.29	3.59	3.59	15.30	132.13
461	46.30	167.59	3.69	3.69	15.56	132.32
462	46.40	168.65	3.78	3.78	15.53	132.45
463	46.50	173.30	3.76	3.76	15.09	132.48
464	46.60	178.80	3.65	3.65	14.32	132.39
465	46.70	184.70	3.53	3.53	13.50	132.22
466	46.80	188.94	3.41	3.41	12.78	131.95
467	46.90	189.52	3.20	3.20	12.14	131.49
468	47.00	187.48	2.90	2.90	11.63	130.89
469	47.10	183.81	2.68	2.68	11.36	130.31
470	47.20	178.60	2.58	2.58	11.39	129.90
471	47.30	173.82	2.52	2.52	11.64	129.68
472	47.40	170.46	2.52	2.52	11.98	129.58
473	47.50	166.99	2.54	2.54	12.34	129.55
474	47.60	164.02	2.53	2.53	12.68	129.53
475	47.70	161.89	2.54	2.54	13.02	129.54
476	47.80	159.80	2.60	2.60	13.32	129.56
477	47.90	157.75	2.58	2.58	13.62	129.65
478	48.00	157.85	2.66	2.66	13.82	129.83
479	48.10	160.73	2.79	2.79	14.02	130.20
480	48.20	163.77	2.95	2.95	14.26	130.61

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
481	48.30	164.50	3.10	3.10	14.61	130.97
482	48.40	163.79	3.22	3.22	14.95	131.25
483	48.50	164.74	3.30	3.30	15.12	131.45
484	48.60	167.31	3.36	3.36	15.08	131.62
485	48.70	169.92	3.41	3.41	14.99	131.77
486	48.80	171.62	3.46	3.46	15.04	131.94
487	48.90	171.70	3.57	3.57	15.40	132.23
488	49.00	171.00	3.83	3.83	16.05	132.65
489	49.10	170.82	4.11	4.11	16.75	133.16
490	49.20	172.60	4.39	4.39	17.11	133.68
491	49.30	180.27	4.66	4.66	16.86	134.13
492	49.40	191.35	4.76	4.76	16.06	134.45
493	49.50	203.17	4.76	4.76	14.99	134.61
494	49.60	214.00	4.69	4.69	13.97	134.59
495	49.70	220.20	4.52	4.52	13.11	134.46
496	49.80	224.41	4.36	4.36	12.62	134.32

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q_c :	Measured cone resistance (tsf)
f_s :	Sleeve friction resistance (tsf)
u :	Pore pressure (tsf)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (pcf)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1	0.30	0.02	0.00	0.02	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
2	0.40	0.03	0.00	0.03	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
3	0.50	0.03	0.00	0.03	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
4	0.60	0.04	0.00	0.04	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
5	0.70	0.04	0.00	0.04	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
6	0.80	0.05	0.00	0.05	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
7	0.90	0.06	0.00	0.06	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
8	1.00	0.06	0.00	0.06	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
9	1.10	0.07	0.00	0.07	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
10	1.20	0.08	0.00	0.08	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
11	1.30	0.08	0.00	0.08	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
12	1.40	0.09	0.00	0.09	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
13	1.50	0.09	0.00	0.09	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
14	1.60	0.10	0.00	0.10	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
15	1.70	0.11	0.00	0.11	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
16	1.80	0.11	0.00	0.11	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
17	1.90	0.12	0.00	0.12	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
18	2.00	0.12	0.00	0.12	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
19	2.10	0.13	0.00	0.13	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
20	2.20	0.13	0.00	0.13	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
21	2.30	0.14	0.00	0.14	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
22	2.40	0.14	0.00	0.14	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
23	2.50	0.15	0.00	0.15	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
24	2.60	0.16	0.00	0.16	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
25	2.70	0.16	0.00	0.16	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
26	2.80	0.17	0.00	0.17	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
27	2.90	0.17	0.00	0.17	1.00	0.481	1.04	0.461	1.10	1.30	2.000	No
28	3.00	0.18	0.00	0.18	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
29	3.10	0.18	0.00	0.18	1.00	0.481	1.04	0.461	1.10	1.30	2.000	Yes
30	3.20	0.19	0.00	0.19	1.00	0.480	1.04	0.460	1.10	1.30	2.000	Yes
31	3.30	0.19	0.00	0.19	1.00	0.480	1.04	0.460	1.10	1.30	2.000	Yes
32	3.40	0.20	0.00	0.20	1.00	0.480	1.04	0.460	1.10	1.30	2.000	Yes
33	3.50	0.20	0.00	0.20	1.00	0.480	1.04	0.460	1.10	1.30	2.000	Yes
34	3.60	0.21	0.00	0.21	1.00	0.480	1.04	0.460	1.10	1.30	2.000	Yes
35	3.70	0.22	0.00	0.22	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
36	3.80	0.22	0.00	0.22	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
37	3.90	0.23	0.00	0.23	1.00	0.480	1.04	0.460	1.10	1.30	2.000	No
38	4.00	0.23	0.00	0.23	1.00	0.479	1.04	0.460	1.10	1.30	2.000	No
39	4.10	0.24	0.00	0.24	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
40	4.20	0.24	0.00	0.24	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
41	4.30	0.25	0.00	0.25	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
42	4.40	0.26	0.00	0.26	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
43	4.50	0.26	0.00	0.26	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
44	4.60	0.27	0.00	0.27	1.00	0.479	1.04	0.459	1.10	1.30	2.000	No
45	4.70	0.27	0.00	0.27	0.99	0.479	1.04	0.459	1.10	1.30	2.000	No
46	4.80	0.28	0.00	0.28	0.99	0.478	1.04	0.459	1.10	1.30	2.000	No
47	4.90	0.28	0.00	0.28	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
48	5.00	0.29	0.00	0.29	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
49	5.10	0.29	0.00	0.29	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
50	5.20	0.30	0.00	0.30	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
51	5.30	0.30	0.00	0.30	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
52	5.40	0.31	0.00	0.31	0.99	0.478	1.04	0.458	1.10	1.30	2.000	No
53	5.50	0.31	0.00	0.31	0.99	0.477	1.04	0.458	1.10	1.30	2.000	No
54	5.60	0.32	0.00	0.32	0.99	0.477	1.04	0.458	1.10	1.30	2.000	No
55	5.70	0.32	0.00	0.32	0.99	0.477	1.04	0.457	1.09	1.30	2.000	No
56	5.80	0.33	0.00	0.33	0.99	0.477	1.04	0.457	1.09	1.30	2.000	No
57	5.90	0.33	0.00	0.33	0.99	0.477	1.04	0.457	1.09	1.30	2.000	No
58	6.00	0.34	0.00	0.34	0.99	0.477	1.04	0.457	1.09	1.30	2.000	No
59	6.10	0.34	0.00	0.34	0.99	0.477	1.04	0.457	1.09	1.30	2.000	No
60	6.20	0.35	0.00	0.35	0.99	0.477	1.04	0.457	1.09	1.30	2.000	No
61	6.30	0.35	0.00	0.35	0.99	0.476	1.04	0.457	1.09	1.30	2.000	No
62	6.40	0.36	0.00	0.36	0.99	0.476	1.04	0.456	1.09	1.30	2.000	No
63	6.50	0.36	0.00	0.36	0.99	0.476	1.04	0.456	1.09	1.30	2.000	No
64	6.60	0.37	0.00	0.37	0.99	0.476	1.04	0.456	1.09	1.30	2.000	No
65	6.70	0.37	0.00	0.37	0.99	0.476	1.04	0.456	1.09	1.30	2.000	No
66	6.80	0.38	0.00	0.38	0.99	0.476	1.04	0.456	1.09	1.30	2.000	No
67	6.90	0.38	0.00	0.38	0.99	0.476	1.04	0.456	1.08	1.30	2.000	No
68	7.00	0.39	0.00	0.39	0.99	0.475	1.04	0.456	1.08	1.30	2.000	No
69	7.10	0.39	0.00	0.39	0.99	0.475	1.04	0.455	1.08	1.30	2.000	No
70	7.20	0.40	0.00	0.40	0.99	0.475	1.04	0.455	1.08	1.30	2.000	No
71	7.30	0.40	0.00	0.40	0.99	0.475	1.04	0.455	1.08	1.30	2.000	No
72	7.40	0.41	0.00	0.41	0.99	0.475	1.04	0.455	1.08	1.30	2.000	No
73	7.50	0.42	0.00	0.42	0.99	0.475	1.04	0.455	1.08	1.30	2.000	No
74	7.60	0.42	0.00	0.42	0.99	0.475	1.04	0.455	1.08	1.30	2.000	No
75	7.70	0.43	0.00	0.43	0.99	0.474	1.04	0.455	1.08	1.30	2.000	No
76	7.80	0.43	0.00	0.43	0.99	0.474	1.04	0.455	1.08	1.30	2.000	No
77	7.90	0.44	0.00	0.44	0.99	0.474	1.04	0.454	1.08	1.30	2.000	No
78	8.00	0.44	0.00	0.44	0.99	0.474	1.04	0.454	1.08	1.30	2.000	No
79	8.10	0.45	0.00	0.45	0.98	0.477	1.04	0.457	1.08	1.30	0.569	No
80	8.20	0.46	0.01	0.45	0.98	0.480	1.04	0.460	1.08	1.30	0.574	No
81	8.30	0.46	0.01	0.45	0.98	0.483	1.04	0.463	1.08	1.30	0.578	No
82	8.40	0.47	0.01	0.46	0.98	0.486	1.04	0.466	1.07	1.30	0.583	No
83	8.50	0.47	0.02	0.46	0.98	0.489	1.04	0.469	1.07	1.30	0.587	No
84	8.60	0.48	0.02	0.46	0.98	0.492	1.04	0.472	1.07	1.30	0.591	No
85	8.70	0.48	0.02	0.46	0.98	0.495	1.04	0.475	1.07	1.30	0.595	No
86	8.80	0.49	0.02	0.46	0.98	0.498	1.04	0.477	1.07	1.30	0.599	No
87	8.90	0.50	0.03	0.47	0.98	0.501	1.04	0.480	1.07	1.30	0.603	No
88	9.00	0.50	0.03	0.47	0.98	0.504	1.04	0.483	1.07	1.30	0.607	No
89	9.10	0.51	0.03	0.47	0.98	0.507	1.04	0.486	1.07	1.30	0.610	No
90	9.20	0.51	0.04	0.47	0.98	0.509	1.04	0.488	1.07	1.30	0.614	No
91	9.30	0.52	0.04	0.48	0.98	0.512	1.04	0.491	1.07	1.30	0.617	No
92	9.40	0.52	0.04	0.48	0.98	0.515	1.04	0.493	1.07	1.30	0.621	No
93	9.50	0.53	0.05	0.48	0.98	0.517	1.04	0.496	1.07	1.30	0.624	No
94	9.60	0.53	0.05	0.48	0.98	0.520	1.04	0.499	1.07	1.30	0.628	No
95	9.70	0.54	0.05	0.49	0.98	0.523	1.04	0.501	1.07	1.30	0.630	No
96	9.80	0.55	0.06	0.49	0.98	0.525	1.04	0.503	1.07	1.30	0.633	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
97	9.90	0.55	0.06	0.49	0.98	0.528	1.04	0.506	1.08	1.30	0.630	No
98	10.00	0.56	0.06	0.49	0.98	0.530	1.04	0.508	1.08	1.30	0.630	No
99	10.10	0.56	0.07	0.50	0.98	0.533	1.04	0.511	1.07	1.30	0.643	No
100	10.20	0.57	0.07	0.50	0.98	0.535	1.04	0.513	1.06	1.30	0.651	No
101	10.30	0.57	0.07	0.50	0.98	0.538	1.04	0.515	1.06	1.30	0.654	No
102	10.40	0.58	0.07	0.50	0.98	0.540	1.04	0.518	1.06	1.30	0.657	No
103	10.50	0.58	0.08	0.51	0.98	0.543	1.04	0.520	1.06	1.30	0.662	No
104	10.60	0.59	0.08	0.51	0.98	0.545	1.04	0.522	1.06	1.30	0.665	No
105	10.70	0.59	0.08	0.51	0.98	0.547	1.04	0.525	1.06	1.30	0.668	No
106	10.80	0.60	0.09	0.51	0.98	0.550	1.04	0.527	1.06	1.30	0.672	No
107	10.90	0.60	0.09	0.51	0.98	0.552	1.04	0.529	1.06	1.30	0.675	No
108	11.00	0.61	0.09	0.51	0.98	0.555	1.04	0.532	1.06	1.30	0.678	No
109	11.10	0.61	0.10	0.52	0.98	0.557	1.04	0.534	1.06	1.30	0.681	No
110	11.20	0.62	0.10	0.52	0.97	0.559	1.04	0.536	1.06	1.30	0.684	No
111	11.30	0.62	0.10	0.52	0.97	0.562	1.04	0.538	1.06	1.30	0.687	No
112	11.40	0.63	0.11	0.52	0.97	0.564	1.04	0.540	1.06	1.30	0.689	No
113	11.50	0.63	0.11	0.52	0.97	0.566	1.04	0.542	1.06	1.30	0.691	No
114	11.60	0.64	0.11	0.53	0.97	0.568	1.04	0.545	1.06	1.30	0.693	No
115	11.70	0.64	0.12	0.53	0.97	0.570	1.04	0.547	1.06	1.30	0.696	No
116	11.80	0.65	0.12	0.53	0.97	0.572	1.04	0.549	1.06	1.30	0.698	No
117	11.90	0.66	0.12	0.53	0.97	0.574	1.04	0.551	1.06	1.30	0.700	No
118	12.00	0.66	0.12	0.54	0.97	0.576	1.04	0.552	1.06	1.30	0.701	No
119	12.10	0.67	0.13	0.54	0.97	0.578	1.04	0.554	1.06	1.30	0.704	No
120	12.20	0.67	0.13	0.54	0.97	0.580	1.04	0.556	1.06	1.30	0.706	No
121	12.30	0.68	0.13	0.54	0.97	0.582	1.04	0.558	1.06	1.30	0.709	No
122	12.40	0.68	0.14	0.55	0.97	0.584	1.04	0.560	1.06	1.30	0.713	No
123	12.50	0.69	0.14	0.55	0.97	0.586	1.04	0.562	1.05	1.30	0.717	No
124	12.60	0.69	0.14	0.55	0.97	0.588	1.04	0.564	1.05	1.30	0.721	No
125	12.70	0.70	0.15	0.55	0.97	0.590	1.04	0.566	1.05	1.30	0.725	No
126	12.80	0.70	0.15	0.55	0.97	0.592	1.04	0.568	1.05	1.30	0.729	No
127	12.90	0.71	0.15	0.56	0.97	0.594	1.04	0.570	1.05	1.30	0.731	No
128	13.00	0.71	0.16	0.56	0.97	0.597	1.04	0.572	1.05	1.30	0.733	No
129	13.10	0.72	0.16	0.56	0.97	0.599	1.04	0.574	1.05	1.30	0.735	No
130	13.20	0.72	0.16	0.56	0.97	0.601	1.04	0.576	1.05	1.30	0.738	No
131	13.30	0.73	0.17	0.56	0.97	0.602	1.04	0.577	1.05	1.30	0.740	No
132	13.40	0.73	0.17	0.56	0.97	0.604	1.04	0.579	1.05	1.30	0.742	No
133	13.50	0.74	0.17	0.57	0.97	0.606	1.04	0.581	1.05	1.30	0.745	No
134	13.60	0.74	0.17	0.57	0.97	0.608	1.04	0.583	1.05	1.30	0.747	No
135	13.70	0.75	0.18	0.57	0.97	0.610	1.04	0.584	1.05	1.30	0.749	No
136	13.80	0.75	0.18	0.57	0.97	0.611	1.04	0.586	1.05	1.30	0.750	No
137	13.90	0.76	0.18	0.58	0.97	0.613	1.04	0.588	1.05	1.30	0.750	No
138	14.00	0.76	0.19	0.58	0.97	0.615	1.04	0.589	1.05	1.30	0.752	No
139	14.10	0.77	0.19	0.58	0.96	0.616	1.04	0.591	1.05	1.30	0.755	No
140	14.20	0.78	0.19	0.58	0.96	0.618	1.04	0.592	1.05	1.30	2.000	Yes
141	14.30	0.78	0.20	0.59	0.96	0.619	1.04	0.594	1.05	1.30	2.000	Yes
142	14.40	0.79	0.20	0.59	0.96	0.621	1.04	0.595	1.06	1.30	2.000	Yes
143	14.50	0.79	0.20	0.59	0.96	0.622	1.04	0.597	1.06	1.30	2.000	Yes
144	14.60	0.80	0.21	0.59	0.96	0.624	1.04	0.598	1.07	1.30	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
145	14.70	0.81	0.21	0.60	0.96	0.625	1.04	0.599	1.07	1.30	2.000	Yes
146	14.80	0.81	0.21	0.60	0.96	0.627	1.04	0.601	1.07	1.30	2.000	Yes
147	14.90	0.82	0.22	0.60	0.96	0.628	1.04	0.602	1.07	1.30	2.000	Yes
148	15.00	0.82	0.22	0.60	0.96	0.630	1.04	0.604	1.07	1.30	2.000	Yes
149	15.10	0.83	0.22	0.61	0.96	0.631	1.04	0.605	1.06	1.30	2.000	Yes
150	15.20	0.83	0.22	0.61	0.96	0.633	1.04	0.606	1.06	1.30	2.000	Yes
151	15.30	0.84	0.23	0.61	0.96	0.634	1.04	0.608	1.05	1.30	2.000	Yes
152	15.40	0.85	0.23	0.61	0.96	0.635	1.04	0.609	1.05	1.30	2.000	Yes
153	15.50	0.85	0.23	0.62	0.96	0.637	1.04	0.610	1.05	1.30	2.000	Yes
154	15.60	0.86	0.24	0.62	0.96	0.638	1.04	0.612	1.04	1.30	2.000	Yes
155	15.70	0.86	0.24	0.62	0.96	0.640	1.04	0.613	1.04	1.30	2.000	Yes
156	15.80	0.87	0.24	0.62	0.96	0.641	1.04	0.615	1.04	1.30	0.794	No
157	15.90	0.87	0.25	0.62	0.96	0.643	1.04	0.616	1.04	1.30	0.797	No
158	16.00	0.87	0.25	0.63	0.96	0.645	1.04	0.618	1.04	1.30	0.799	No
159	16.10	0.88	0.25	0.63	0.96	0.646	1.04	0.619	1.04	1.30	0.801	No
160	16.20	0.88	0.26	0.63	0.96	0.648	1.04	0.621	1.04	1.30	0.804	No
161	16.30	0.89	0.26	0.63	0.96	0.650	1.04	0.623	1.04	1.30	0.806	No
162	16.40	0.89	0.26	0.63	0.96	0.651	1.04	0.624	1.04	1.30	0.808	No
163	16.50	0.90	0.27	0.63	0.96	0.653	1.04	0.626	1.04	1.30	0.810	No
164	16.60	0.90	0.27	0.63	0.96	0.654	1.04	0.627	1.04	1.30	0.812	No
165	16.70	0.91	0.27	0.63	0.96	0.656	1.04	0.629	1.04	1.30	0.814	No
166	16.80	0.91	0.27	0.64	0.95	0.658	1.04	0.630	1.04	1.30	0.817	No
167	16.90	0.91	0.28	0.64	0.95	0.659	1.04	0.632	1.04	1.30	0.819	No
168	17.00	0.92	0.28	0.64	0.95	0.661	1.04	0.633	1.04	1.30	0.821	No
169	17.10	0.92	0.28	0.64	0.95	0.662	1.04	0.635	1.04	1.30	0.823	No
170	17.20	0.93	0.29	0.64	0.95	0.664	1.04	0.636	1.04	1.30	0.825	No
171	17.30	0.93	0.29	0.64	0.95	0.665	1.04	0.637	1.04	1.30	0.826	No
172	17.40	0.94	0.29	0.65	0.95	0.666	1.04	0.639	1.04	1.30	0.827	No
173	17.50	0.94	0.30	0.65	0.95	0.668	1.04	0.640	1.04	1.30	0.828	No
174	17.60	0.95	0.30	0.65	0.95	0.669	1.04	0.641	1.04	1.30	0.829	No
175	17.70	0.95	0.30	0.65	0.95	0.670	1.04	0.642	1.04	1.30	0.829	No
176	17.80	0.96	0.31	0.65	0.95	0.671	1.04	0.643	1.04	1.30	0.831	No
177	17.90	0.97	0.31	0.66	0.95	0.672	1.04	0.644	1.04	1.30	0.833	No
178	18.00	0.97	0.31	0.66	0.95	0.673	1.04	0.645	1.04	1.30	0.835	No
179	18.10	0.98	0.32	0.66	0.95	0.674	1.04	0.646	1.04	1.30	0.837	No
180	18.20	0.98	0.32	0.66	0.95	0.676	1.04	0.647	1.04	1.30	0.839	No
181	18.30	0.99	0.32	0.67	0.95	0.677	1.04	0.649	1.04	1.30	0.841	No
182	18.40	0.99	0.32	0.67	0.95	0.678	1.04	0.650	1.04	1.30	0.843	No
183	18.50	1.00	0.33	0.67	0.95	0.679	1.04	0.651	1.04	1.30	0.845	No
184	18.60	1.00	0.33	0.67	0.95	0.680	1.04	0.652	1.04	1.30	0.847	No
185	18.70	1.01	0.33	0.67	0.95	0.681	1.04	0.653	1.04	1.30	0.849	No
186	18.80	1.01	0.34	0.68	0.95	0.683	1.04	0.654	1.04	1.30	0.850	No
187	18.90	1.02	0.34	0.68	0.95	0.684	1.04	0.655	1.04	1.30	0.852	No
188	19.00	1.02	0.34	0.68	0.95	0.685	1.04	0.656	1.04	1.30	0.853	No
189	19.10	1.03	0.35	0.68	0.95	0.686	1.04	0.657	1.04	1.30	0.855	No
190	19.20	1.03	0.35	0.68	0.95	0.687	1.04	0.659	1.04	1.30	0.857	No
191	19.30	1.04	0.35	0.69	0.94	0.688	1.04	0.660	1.03	1.30	0.859	No
192	19.40	1.04	0.36	0.69	0.94	0.689	1.04	0.661	1.03	1.30	0.860	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
193	19.50	1.05	0.36	0.69	0.94	0.690	1.04	0.662	1.03	1.30	0.862	No
194	19.60	1.05	0.36	0.69	0.94	0.691	1.04	0.663	1.03	1.30	0.862	No
195	19.70	1.06	0.37	0.69	0.94	0.692	1.04	0.664	1.04	1.30	0.863	No
196	19.80	1.06	0.37	0.70	0.94	0.693	1.04	0.665	1.04	1.30	0.864	No
197	19.90	1.07	0.37	0.70	0.94	0.694	1.04	0.665	1.04	1.30	0.861	No
198	20.00	1.08	0.37	0.70	0.94	0.695	1.04	0.666	1.04	1.30	0.857	No
199	20.10	1.08	0.38	0.70	0.94	0.696	1.04	0.667	1.04	1.30	0.865	No
200	20.20	1.09	0.38	0.71	0.94	0.697	1.04	0.668	1.03	1.30	0.870	No
201	20.30	1.09	0.38	0.71	0.94	0.698	1.04	0.669	1.03	1.30	0.872	No
202	20.40	1.10	0.39	0.71	0.94	0.699	1.04	0.670	1.03	1.30	0.874	No
203	20.50	1.10	0.39	0.71	0.94	0.700	1.04	0.671	1.03	1.30	0.875	No
204	20.60	1.11	0.39	0.71	0.94	0.701	1.04	0.672	1.03	1.30	0.877	No
205	20.70	1.11	0.40	0.72	0.94	0.702	1.04	0.673	1.03	1.30	0.878	No
206	20.80	1.12	0.40	0.72	0.94	0.703	1.04	0.673	1.03	1.30	0.880	No
207	20.90	1.12	0.40	0.72	0.94	0.704	1.04	0.674	1.03	1.30	0.881	No
208	21.00	1.13	0.41	0.72	0.94	0.704	1.04	0.675	1.03	1.30	0.881	No
209	21.10	1.13	0.41	0.72	0.94	0.705	1.04	0.676	1.03	1.30	0.881	No
210	21.20	1.14	0.41	0.73	0.94	0.706	1.04	0.677	1.03	1.30	0.881	No
211	21.30	1.14	0.41	0.73	0.94	0.707	1.04	0.677	1.03	1.30	0.881	No
212	21.40	1.15	0.42	0.73	0.94	0.707	1.04	0.678	1.03	1.30	0.883	No
213	21.50	1.16	0.42	0.73	0.94	0.708	1.04	0.679	1.03	1.30	0.885	No
214	21.60	1.16	0.42	0.74	0.94	0.709	1.04	0.679	1.03	1.30	0.887	No
215	21.70	1.17	0.43	0.74	0.93	0.710	1.04	0.680	1.03	1.30	0.890	No
216	21.80	1.17	0.43	0.74	0.93	0.710	1.04	0.681	1.03	1.30	0.892	No
217	21.90	1.18	0.43	0.74	0.93	0.711	1.04	0.682	1.03	1.30	0.894	No
218	22.00	1.18	0.44	0.75	0.93	0.712	1.04	0.683	1.03	1.30	0.895	No
219	22.10	1.19	0.44	0.75	0.93	0.713	1.04	0.683	1.03	1.30	0.895	No
220	22.20	1.19	0.44	0.75	0.93	0.714	1.04	0.684	1.03	1.30	0.896	No
221	22.30	1.20	0.45	0.75	0.93	0.714	1.04	0.685	1.03	1.30	0.897	No
222	22.40	1.20	0.45	0.75	0.93	0.715	1.04	0.685	1.03	1.30	0.898	No
223	22.50	1.21	0.45	0.76	0.93	0.716	1.04	0.686	1.03	1.30	0.899	No
224	22.60	1.22	0.46	0.76	0.93	0.717	1.04	0.687	1.03	1.30	0.899	No
225	22.70	1.22	0.46	0.76	0.93	0.717	1.04	0.687	1.03	1.30	0.901	No
226	22.80	1.23	0.46	0.76	0.93	0.718	1.04	0.688	1.03	1.30	0.903	No
227	22.90	1.23	0.46	0.77	0.93	0.719	1.04	0.689	1.03	1.30	0.904	No
228	23.00	1.24	0.47	0.77	0.93	0.719	1.04	0.689	1.03	1.30	0.905	No
229	23.10	1.24	0.47	0.77	0.93	0.720	1.04	0.690	1.03	1.30	0.906	No
230	23.20	1.25	0.47	0.77	0.93	0.721	1.04	0.691	1.03	1.30	0.906	No
231	23.30	1.25	0.48	0.78	0.93	0.721	1.04	0.691	1.03	1.30	0.907	No
232	23.40	1.26	0.48	0.78	0.93	0.722	1.04	0.692	1.03	1.30	0.909	No
233	23.50	1.26	0.48	0.78	0.93	0.723	1.04	0.693	1.02	1.30	0.910	No
234	23.60	1.27	0.49	0.78	0.93	0.723	1.04	0.693	1.02	1.30	0.910	No
235	23.70	1.27	0.49	0.78	0.93	0.724	1.04	0.694	1.02	1.30	0.911	No
236	23.80	1.28	0.49	0.79	0.93	0.724	1.04	0.694	1.02	1.30	0.912	No
237	23.90	1.29	0.50	0.79	0.93	0.725	1.04	0.695	1.02	1.30	0.914	No
238	24.00	1.29	0.50	0.79	0.93	0.725	1.04	0.695	1.02	1.30	0.914	No
239	24.10	1.30	0.50	0.79	0.92	0.726	1.04	0.696	1.03	1.30	0.912	No
240	24.20	1.30	0.51	0.80	0.92	0.726	1.04	0.696	1.03	1.30	0.910	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
241	24.30	1.31	0.51	0.80	0.92	0.727	1.04	0.697	1.03	1.30	0.909	No
242	24.40	1.31	0.51	0.80	0.92	0.727	1.04	0.697	1.03	1.30	0.910	No
243	24.50	1.32	0.51	0.81	0.92	0.728	1.04	0.697	1.03	1.30	0.911	No
244	24.60	1.33	0.52	0.81	0.92	0.728	1.04	0.698	1.03	1.30	0.913	No
245	24.70	1.33	0.52	0.81	0.92	0.729	1.04	0.698	1.02	1.30	0.916	No
246	24.80	1.34	0.52	0.81	0.92	0.729	1.04	0.699	1.02	1.30	0.917	No
247	24.90	1.34	0.53	0.82	0.92	0.729	1.04	0.699	1.02	1.30	0.916	No
248	25.00	1.35	0.53	0.82	0.92	0.730	1.04	0.699	1.02	1.30	0.917	No
249	25.10	1.36	0.53	0.82	0.92	0.730	1.04	0.700	1.02	1.30	0.918	No
250	25.20	1.36	0.54	0.82	0.92	0.730	1.04	0.700	1.02	1.30	0.918	No
251	25.30	1.37	0.54	0.83	0.92	0.731	1.04	0.700	1.02	1.30	0.918	No
252	25.40	1.37	0.54	0.83	0.92	0.731	1.04	0.701	1.02	1.30	0.920	No
253	25.50	1.38	0.55	0.83	0.92	0.731	1.04	0.701	1.02	1.30	2.000	Yes
254	25.60	1.39	0.55	0.84	0.92	0.732	1.04	0.701	1.02	1.30	2.000	Yes
255	25.70	1.39	0.55	0.84	0.92	0.732	1.04	0.701	1.03	1.30	2.000	Yes
256	25.80	1.40	0.56	0.84	0.92	0.732	1.04	0.702	1.04	1.30	2.000	Yes
257	25.90	1.40	0.56	0.85	0.92	0.732	1.04	0.702	1.05	1.30	2.000	Yes
258	26.00	1.41	0.56	0.85	0.92	0.732	1.04	0.702	1.06	1.30	2.000	Yes
259	26.10	1.42	0.56	0.85	0.92	0.732	1.04	0.702	1.06	1.30	2.000	Yes
260	26.20	1.42	0.57	0.86	0.92	0.732	1.04	0.702	1.05	1.30	2.000	Yes
261	26.30	1.43	0.57	0.86	0.92	0.733	1.04	0.702	1.05	1.30	0.852	No
262	26.40	1.44	0.57	0.86	0.91	0.733	1.04	0.702	1.05	1.30	0.854	No
263	26.50	1.44	0.58	0.87	0.91	0.733	1.04	0.702	1.05	1.30	0.855	No
264	26.60	1.45	0.58	0.87	0.91	0.733	1.04	0.702	1.05	1.30	0.856	No
265	26.70	1.46	0.58	0.87	0.91	0.733	1.04	0.702	1.04	1.30	0.859	No
266	26.80	1.46	0.59	0.88	0.91	0.733	1.04	0.703	1.04	1.30	0.859	No
267	26.90	1.47	0.59	0.88	0.91	0.733	1.04	0.703	1.04	1.30	0.859	No
268	27.00	1.48	0.59	0.88	0.91	0.733	1.04	0.703	1.04	1.30	0.860	No
269	27.10	1.48	0.60	0.89	0.91	0.733	1.04	0.703	1.04	1.30	0.863	No
270	27.20	1.49	0.60	0.89	0.91	0.733	1.04	0.703	1.04	1.30	0.867	No
271	27.30	1.50	0.60	0.89	0.91	0.733	1.04	0.703	1.03	1.30	0.873	No
272	27.40	1.50	0.61	0.90	0.91	0.733	1.04	0.703	1.03	1.30	0.879	No
273	27.50	1.51	0.61	0.90	0.91	0.734	1.04	0.703	1.03	1.30	0.886	No
274	27.60	1.51	0.61	0.90	0.91	0.734	1.04	0.703	1.03	1.30	0.895	No
275	27.70	1.52	0.61	0.91	0.91	0.734	1.04	0.703	1.02	1.30	0.904	No
276	27.80	1.53	0.62	0.91	0.91	0.734	1.04	0.703	1.02	1.30	0.910	No
277	27.90	1.53	0.62	0.91	0.91	0.734	1.04	0.704	1.02	1.30	0.915	No
278	28.00	1.54	0.62	0.91	0.91	0.734	1.04	0.704	1.02	1.30	0.917	No
279	28.10	1.54	0.63	0.92	0.91	0.734	1.04	0.704	1.02	1.30	0.915	No
280	28.20	1.55	0.63	0.92	0.91	0.735	1.04	0.704	1.02	1.30	0.911	No
281	28.30	1.56	0.63	0.92	0.91	0.735	1.04	0.704	1.02	1.30	0.906	No
282	28.40	1.56	0.64	0.93	0.91	0.735	1.04	0.704	1.02	1.30	0.903	No
283	28.50	1.57	0.64	0.93	0.91	0.735	1.04	0.704	1.02	1.30	0.899	No
284	28.60	1.58	0.64	0.93	0.90	0.735	1.04	0.704	1.02	1.30	0.895	No
285	28.70	1.58	0.65	0.94	0.90	0.735	1.04	0.704	1.02	1.30	0.888	No
286	28.80	1.59	0.65	0.94	0.90	0.735	1.04	0.704	1.03	1.30	0.879	No
287	28.90	1.60	0.65	0.94	0.90	0.735	1.04	0.704	1.03	1.30	0.874	No
288	29.00	1.60	0.66	0.95	0.90	0.735	1.04	0.704	1.03	1.30	0.873	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
289	29.10	1.61	0.66	0.95	0.90	0.735	1.04	0.704	1.03	1.30	0.873	No
290	29.20	1.62	0.66	0.95	0.90	0.735	1.04	0.704	1.03	1.30	0.873	No
291	29.30	1.62	0.66	0.96	0.90	0.735	1.04	0.704	1.03	1.30	0.874	No
292	29.40	1.63	0.67	0.96	0.90	0.735	1.04	0.704	1.02	1.30	0.875	No
293	29.50	1.63	0.67	0.96	0.90	0.735	1.04	0.704	1.02	1.30	0.876	No
294	29.60	1.64	0.67	0.97	0.90	0.735	1.04	0.704	1.02	1.30	0.878	No
295	29.70	1.65	0.68	0.97	0.90	0.735	1.04	0.704	1.02	1.30	0.880	No
296	29.80	1.65	0.68	0.97	0.90	0.735	1.04	0.704	1.02	1.30	0.879	No
297	29.90	1.66	0.68	0.98	0.90	0.735	1.04	0.704	1.02	1.30	0.878	No
298	30.00	1.67	0.69	0.98	0.90	0.735	1.04	0.704	1.02	1.30	0.881	No
299	30.10	1.67	0.69	0.98	0.90	0.734	1.04	0.704	1.02	1.30	0.881	No
300	30.20	1.68	0.69	0.99	0.90	0.734	1.04	0.704	1.02	1.30	0.883	No
301	30.30	1.69	0.70	0.99	0.90	0.734	1.04	0.704	1.01	1.30	0.895	No
302	30.40	1.69	0.70	0.99	0.90	0.734	1.04	0.704	1.01	1.30	0.900	No
303	30.50	1.70	0.70	1.00	0.90	0.734	1.04	0.704	1.01	1.30	0.911	No
304	30.60	1.71	0.71	1.00	0.90	0.734	1.04	0.704	1.01	1.30	0.917	No
305	30.70	1.71	0.71	1.00	0.90	0.734	1.04	0.704	1.01	1.30	0.913	No
306	30.80	1.72	0.71	1.01	0.89	0.734	1.04	0.704	1.01	1.30	0.899	No
307	30.90	1.73	0.71	1.01	0.89	0.734	1.04	0.704	1.01	1.30	0.887	No
308	31.00	1.73	0.72	1.01	0.89	0.734	1.04	0.704	1.01	1.30	0.887	No
309	31.10	1.74	0.72	1.02	0.89	0.734	1.04	0.703	1.01	1.30	0.888	No
310	31.20	1.74	0.72	1.02	0.89	0.734	1.04	0.703	1.01	1.30	0.888	No
311	31.30	1.75	0.73	1.02	0.89	0.734	1.04	0.703	1.01	1.30	0.889	No
312	31.40	1.76	0.73	1.03	0.89	0.734	1.04	0.703	1.01	1.30	0.889	No
313	31.50	1.76	0.73	1.03	0.89	0.734	1.04	0.703	1.01	1.30	0.890	No
314	31.60	1.77	0.74	1.03	0.89	0.734	1.04	0.703	1.01	1.30	0.892	No
315	31.70	1.78	0.74	1.04	0.89	0.733	1.04	0.703	1.00	1.30	0.901	No
316	31.80	1.78	0.74	1.04	0.89	0.733	1.04	0.703	1.00	1.30	0.908	No
317	31.90	1.79	0.75	1.04	0.89	0.733	1.04	0.703	1.00	1.30	0.914	No
318	32.00	1.80	0.75	1.05	0.89	0.733	1.04	0.703	1.00	1.30	2.000	Yes
319	32.10	1.80	0.75	1.05	0.89	0.733	1.04	0.703	1.00	1.30	2.000	Yes
320	32.20	1.81	0.76	1.05	0.89	0.733	1.04	0.703	1.00	1.30	2.000	Yes
321	32.30	1.82	0.76	1.06	0.89	0.733	1.04	0.703	1.00	1.30	2.000	Yes
322	32.40	1.82	0.76	1.06	0.89	0.733	1.04	0.703	1.00	1.30	2.000	Yes
323	32.50	1.83	0.76	1.06	0.89	0.733	1.04	0.703	1.00	1.30	2.000	Yes
324	32.60	1.83	0.77	1.07	0.89	0.733	1.04	0.702	1.00	1.30	2.000	Yes
325	32.70	1.84	0.77	1.07	0.89	0.733	1.04	0.702	1.00	1.30	0.937	No
326	32.80	1.85	0.77	1.07	0.89	0.733	1.04	0.702	1.00	1.30	0.937	No
327	32.90	1.85	0.78	1.08	0.88	0.733	1.04	0.702	1.00	1.30	0.935	No
328	33.00	1.86	0.78	1.08	0.88	0.733	1.04	0.702	1.00	1.30	0.932	No
329	33.10	1.87	0.78	1.08	0.88	0.732	1.04	0.702	1.00	1.30	0.931	No
330	33.20	1.87	0.79	1.09	0.88	0.732	1.04	0.702	1.00	1.30	0.928	No
331	33.30	1.88	0.79	1.09	0.88	0.732	1.04	0.702	1.00	1.30	0.922	No
332	33.40	1.89	0.79	1.09	0.88	0.732	1.04	0.702	0.99	1.30	0.917	No
333	33.50	1.89	0.80	1.10	0.88	0.732	1.04	0.701	0.99	1.30	0.916	No
334	33.60	1.90	0.80	1.10	0.88	0.732	1.04	0.701	0.99	1.30	0.920	No
335	33.70	1.91	0.80	1.10	0.88	0.732	1.04	0.701	0.99	1.30	0.924	No
336	33.80	1.91	0.80	1.11	0.88	0.731	1.04	0.701	0.99	1.30	0.929	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
337	33.90	1.92	0.81	1.11	0.88	0.731	1.04	0.701	0.99	1.30	0.935	No
338	34.00	1.93	0.81	1.11	0.88	0.731	1.04	0.701	0.99	1.30	0.939	No
339	34.10	1.93	0.81	1.12	0.88	0.731	1.04	0.701	0.99	1.30	0.941	No
340	34.20	1.94	0.82	1.12	0.88	0.731	1.04	0.701	0.99	1.30	0.943	No
341	34.30	1.94	0.82	1.12	0.88	0.731	1.04	0.701	0.99	1.30	0.944	No
342	34.40	1.95	0.82	1.13	0.88	0.731	1.04	0.701	0.99	1.30	0.946	No
343	34.50	1.96	0.83	1.13	0.88	0.731	1.04	0.701	0.99	1.30	0.946	No
344	34.60	1.96	0.83	1.13	0.88	0.731	1.04	0.701	0.99	1.30	0.947	No
345	34.70	1.97	0.83	1.13	0.88	0.731	1.04	0.701	0.99	1.30	0.948	No
346	34.80	1.97	0.84	1.14	0.88	0.731	1.04	0.701	0.99	1.30	0.948	No
347	34.90	1.98	0.84	1.14	0.88	0.731	1.04	0.701	0.99	1.30	0.949	No
348	35.00	1.98	0.84	1.14	0.87	0.731	1.04	0.701	0.99	1.30	0.949	No
349	35.10	1.99	0.85	1.14	0.87	0.731	1.04	0.701	0.99	1.30	0.949	No
350	35.20	2.00	0.85	1.15	0.87	0.731	1.04	0.701	0.99	1.30	0.949	No
351	35.30	2.00	0.85	1.15	0.87	0.731	1.04	0.701	0.99	1.30	0.949	No
352	35.40	2.01	0.85	1.15	0.87	0.731	1.04	0.701	0.99	1.30	2.000	Yes
353	35.50	2.01	0.86	1.16	0.87	0.731	1.04	0.701	0.99	1.30	2.000	Yes
354	35.60	2.02	0.86	1.16	0.87	0.731	1.04	0.701	0.99	1.30	2.000	Yes
355	35.70	2.03	0.86	1.16	0.87	0.731	1.04	0.700	0.99	1.30	2.000	Yes
356	35.80	2.03	0.87	1.17	0.87	0.731	1.04	0.700	0.99	1.30	2.000	Yes
357	35.90	2.04	0.87	1.17	0.87	0.731	1.04	0.700	0.99	1.30	2.000	Yes
358	36.00	2.05	0.87	1.17	0.87	0.731	1.04	0.700	0.99	1.30	2.000	Yes
359	36.10	2.05	0.88	1.17	0.87	0.730	1.04	0.700	0.99	1.30	2.000	Yes
360	36.20	2.06	0.88	1.18	0.87	0.730	1.04	0.700	0.99	1.30	2.000	Yes
361	36.30	2.06	0.88	1.18	0.87	0.730	1.04	0.700	0.99	1.30	2.000	Yes
362	36.40	2.07	0.89	1.18	0.87	0.730	1.04	0.700	0.99	1.30	2.000	Yes
363	36.50	2.08	0.89	1.19	0.87	0.730	1.04	0.700	0.99	1.30	0.949	No
364	36.60	2.08	0.89	1.19	0.87	0.730	1.04	0.700	0.99	1.30	0.949	No
365	36.70	2.09	0.90	1.19	0.87	0.730	1.04	0.700	0.99	1.30	0.949	No
366	36.80	2.09	0.90	1.20	0.87	0.730	1.04	0.700	0.99	1.30	0.949	No
367	36.90	2.10	0.90	1.20	0.87	0.730	1.04	0.699	0.99	1.30	0.949	No
368	37.00	2.11	0.90	1.20	0.87	0.730	1.04	0.699	0.99	1.30	2.000	Yes
369	37.10	2.11	0.91	1.20	0.86	0.730	1.04	0.699	0.99	1.30	2.000	Yes
370	37.20	2.12	0.91	1.21	0.86	0.729	1.04	0.699	0.99	1.30	2.000	Yes
371	37.30	2.12	0.91	1.21	0.86	0.729	1.04	0.699	0.99	1.30	2.000	Yes
372	37.40	2.13	0.92	1.21	0.86	0.729	1.04	0.699	0.98	1.30	2.000	Yes
373	37.50	2.14	0.92	1.22	0.86	0.729	1.04	0.699	0.98	1.30	2.000	Yes
374	37.60	2.14	0.92	1.22	0.86	0.729	1.04	0.699	0.98	1.30	2.000	Yes
375	37.70	2.15	0.93	1.22	0.86	0.729	1.04	0.698	0.98	1.30	0.943	No
376	37.80	2.16	0.93	1.23	0.86	0.729	1.04	0.698	0.98	1.30	0.943	No
377	37.90	2.16	0.93	1.23	0.86	0.728	1.04	0.698	0.98	1.30	0.943	No
378	38.00	2.17	0.94	1.23	0.86	0.728	1.04	0.698	0.98	1.30	0.944	No
379	38.10	2.17	0.94	1.24	0.86	0.728	1.04	0.698	0.98	1.30	0.944	No
380	38.20	2.18	0.94	1.24	0.86	0.728	1.04	0.698	0.98	1.30	0.945	No
381	38.30	2.19	0.95	1.24	0.86	0.728	1.04	0.698	0.98	1.30	0.945	No
382	38.40	2.19	0.95	1.24	0.86	0.728	1.04	0.697	0.98	1.30	0.945	No
383	38.50	2.20	0.95	1.25	0.86	0.728	1.04	0.697	0.98	1.30	0.946	No
384	38.60	2.21	0.95	1.25	0.86	0.727	1.04	0.697	0.98	1.30	0.946	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
385	38.70	2.21	0.96	1.25	0.86	0.727	1.04	0.697	0.98	1.30	0.945	No
386	38.80	2.22	0.96	1.26	0.86	0.727	1.04	0.697	0.98	1.30	0.943	No
387	38.90	2.22	0.96	1.26	0.86	0.727	1.04	0.697	0.98	1.30	0.943	No
388	39.00	2.23	0.97	1.26	0.86	0.727	1.04	0.696	0.97	1.30	0.942	No
389	39.10	2.24	0.97	1.27	0.86	0.726	1.04	0.696	0.97	1.30	0.942	No
390	39.20	2.24	0.97	1.27	0.85	0.726	1.04	0.696	0.97	1.30	0.943	No
391	39.30	2.25	0.98	1.27	0.85	0.726	1.04	0.696	0.97	1.30	0.942	No
392	39.40	2.26	0.98	1.28	0.85	0.726	1.04	0.696	0.97	1.30	0.942	No
393	39.50	2.26	0.98	1.28	0.85	0.726	1.04	0.695	0.97	1.30	0.940	No
394	39.60	2.27	0.99	1.28	0.85	0.725	1.04	0.695	0.97	1.30	0.939	No
395	39.70	2.28	0.99	1.29	0.85	0.725	1.04	0.695	0.97	1.30	2.000	Yes
396	39.80	2.28	0.99	1.29	0.85	0.725	1.04	0.695	0.97	1.30	2.000	Yes
397	39.90	2.29	1.00	1.29	0.85	0.725	1.04	0.695	0.97	1.30	2.000	Yes
398	40.00	2.29	1.00	1.30	0.85	0.724	1.04	0.694	0.97	1.30	2.000	Yes
399	40.10	2.30	1.00	1.30	0.85	0.724	1.04	0.694	0.97	1.30	2.000	Yes
400	40.20	2.31	1.00	1.30	0.85	0.724	1.04	0.694	0.98	1.30	2.000	Yes
401	40.30	2.31	1.01	1.31	0.85	0.724	1.04	0.694	0.98	1.30	2.000	Yes
402	40.40	2.32	1.01	1.31	0.85	0.724	1.04	0.694	0.98	1.30	2.000	Yes
403	40.50	2.33	1.01	1.31	0.85	0.723	1.04	0.693	0.98	1.30	2.000	Yes
404	40.60	2.33	1.02	1.32	0.85	0.723	1.04	0.693	0.97	1.30	2.000	Yes
405	40.70	2.34	1.02	1.32	0.85	0.723	1.04	0.693	0.97	1.30	2.000	Yes
406	40.80	2.35	1.02	1.32	0.85	0.723	1.04	0.693	0.97	1.30	2.000	Yes
407	40.90	2.35	1.03	1.32	0.85	0.722	1.04	0.692	0.97	1.30	2.000	Yes
408	41.00	2.36	1.03	1.33	0.85	0.722	1.04	0.692	0.97	1.30	0.942	No
409	41.10	2.36	1.03	1.33	0.85	0.722	1.04	0.692	0.97	1.30	0.942	No
410	41.20	2.37	1.04	1.33	0.84	0.722	1.04	0.692	0.96	1.30	0.942	No
411	41.30	2.38	1.04	1.34	0.84	0.722	1.04	0.692	0.96	1.30	0.942	No
412	41.40	2.38	1.04	1.34	0.84	0.721	1.04	0.691	0.97	1.30	2.000	Yes
413	41.50	2.39	1.05	1.34	0.84	0.721	1.04	0.691	0.97	1.30	2.000	Yes
414	41.60	2.40	1.05	1.35	0.84	0.721	1.04	0.691	0.97	1.30	2.000	Yes
415	41.70	2.40	1.05	1.35	0.84	0.721	1.04	0.691	0.97	1.30	2.000	Yes
416	41.80	2.41	1.05	1.35	0.84	0.720	1.04	0.690	0.97	1.30	2.000	Yes
417	41.90	2.41	1.06	1.36	0.84	0.720	1.04	0.690	0.97	1.30	2.000	Yes
418	42.00	2.42	1.06	1.36	0.84	0.720	1.04	0.690	0.97	1.30	2.000	Yes
419	42.10	2.43	1.06	1.36	0.84	0.720	1.04	0.690	0.98	1.30	2.000	Yes
420	42.20	2.43	1.07	1.37	0.84	0.720	1.04	0.690	0.98	1.30	2.000	Yes
421	42.30	2.44	1.07	1.37	0.84	0.719	1.04	0.689	0.98	1.30	0.949	No
422	42.40	2.45	1.07	1.37	0.84	0.719	1.04	0.689	0.97	1.30	0.948	No
423	42.50	2.45	1.08	1.38	0.84	0.719	1.04	0.689	0.97	1.30	0.948	No
424	42.60	2.46	1.08	1.38	0.84	0.719	1.04	0.689	0.97	1.30	0.948	No
425	42.70	2.46	1.08	1.38	0.84	0.719	1.04	0.689	0.97	1.30	0.948	No
426	42.80	2.47	1.09	1.38	0.84	0.718	1.04	0.689	0.97	1.30	0.948	No
427	42.90	2.48	1.09	1.39	0.84	0.718	1.04	0.688	0.97	1.30	0.948	No
428	43.00	2.48	1.09	1.39	0.84	0.718	1.04	0.688	0.97	1.30	0.948	No
429	43.10	2.49	1.10	1.39	0.84	0.718	1.04	0.688	0.97	1.30	0.948	No
430	43.20	2.49	1.10	1.40	0.84	0.718	1.04	0.688	0.97	1.30	0.948	No
431	43.30	2.50	1.10	1.40	0.83	0.717	1.04	0.688	0.97	1.30	0.947	No
432	43.40	2.51	1.10	1.40	0.83	0.717	1.04	0.687	0.97	1.30	0.947	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
433	43.50	2.51	1.11	1.41	0.83	0.717	1.04	0.687	0.97	1.30	0.947	No
434	43.60	2.52	1.11	1.41	0.83	0.717	1.04	0.687	0.97	1.30	0.948	No
435	43.70	2.53	1.11	1.41	0.83	0.716	1.04	0.687	0.97	1.30	0.948	No
436	43.80	2.53	1.12	1.42	0.83	0.716	1.04	0.686	0.97	1.30	0.947	No
437	43.90	2.54	1.12	1.42	0.83	0.716	1.04	0.686	0.97	1.30	2.000	Yes
438	44.00	2.54	1.12	1.42	0.83	0.716	1.04	0.686	0.97	1.30	2.000	Yes
439	44.10	2.55	1.13	1.42	0.83	0.715	1.04	0.686	0.97	1.30	2.000	Yes
440	44.20	2.56	1.13	1.43	0.83	0.715	1.04	0.685	0.96	1.30	2.000	Yes
441	44.30	2.56	1.13	1.43	0.83	0.715	1.04	0.685	0.95	1.30	2.000	Yes
442	44.40	2.57	1.14	1.43	0.83	0.715	1.04	0.685	0.94	1.30	2.000	Yes
443	44.50	2.58	1.14	1.44	0.83	0.714	1.04	0.685	0.93	1.30	2.000	Yes
444	44.60	2.58	1.14	1.44	0.83	0.714	1.04	0.684	0.93	1.30	2.000	Yes
445	44.70	2.59	1.15	1.44	0.83	0.714	1.04	0.684	0.93	1.30	0.938	No
446	44.80	2.60	1.15	1.45	0.83	0.713	1.04	0.684	0.93	1.30	0.941	No
447	44.90	2.60	1.15	1.45	0.83	0.713	1.04	0.683	0.91	1.30	0.953	No
448	45.00	2.61	1.15	1.46	0.83	0.713	1.04	0.683	0.90	1.30	0.962	No
449	45.10	2.62	1.16	1.46	0.83	0.712	1.04	0.683	0.90	1.30	0.962	No
450	45.20	2.62	1.16	1.46	0.83	0.712	1.04	0.682	0.90	1.30	0.963	No
451	45.30	2.63	1.16	1.47	0.82	0.712	1.04	0.682	0.90	1.30	0.963	No
452	45.40	2.64	1.17	1.47	0.82	0.711	1.04	0.682	0.90	1.30	0.963	No
453	45.50	2.64	1.17	1.47	0.82	0.711	1.04	0.682	0.90	1.30	0.964	No
454	45.60	2.65	1.17	1.48	0.82	0.711	1.04	0.681	0.90	1.30	0.963	No
455	45.70	2.66	1.18	1.48	0.82	0.710	1.04	0.681	0.90	1.30	0.960	No
456	45.80	2.66	1.18	1.48	0.82	0.710	1.04	0.681	0.91	1.30	0.957	No
457	45.90	2.67	1.18	1.49	0.82	0.710	1.04	0.680	0.91	1.30	0.957	No
458	46.00	2.68	1.19	1.49	0.82	0.709	1.04	0.680	0.90	1.30	0.957	No
459	46.10	2.68	1.19	1.49	0.82	0.709	1.04	0.680	0.90	1.30	0.957	No
460	46.20	2.69	1.19	1.50	0.82	0.709	1.04	0.679	0.90	1.30	0.959	No
461	46.30	2.70	1.19	1.50	0.82	0.708	1.04	0.679	0.90	1.30	0.960	No
462	46.40	2.70	1.20	1.50	0.82	0.708	1.04	0.679	0.90	1.30	0.961	No
463	46.50	2.71	1.20	1.51	0.82	0.708	1.04	0.678	0.90	1.30	0.965	No
464	46.60	2.72	1.20	1.51	0.82	0.707	1.04	0.678	0.89	1.30	0.967	No
465	46.70	2.72	1.21	1.51	0.82	0.707	1.04	0.678	0.89	1.30	0.967	No
466	46.80	2.73	1.21	1.52	0.82	0.707	1.04	0.677	0.89	1.30	0.968	No
467	46.90	2.74	1.21	1.52	0.82	0.706	1.04	0.677	0.90	1.30	0.961	No
468	47.00	2.74	1.22	1.53	0.82	0.706	1.04	0.677	0.91	1.30	0.952	No
469	47.10	2.75	1.22	1.53	0.82	0.706	1.04	0.676	0.91	1.30	0.945	No
470	47.20	2.76	1.22	1.53	0.82	0.705	1.04	0.676	0.92	1.30	0.940	No
471	47.30	2.76	1.23	1.54	0.82	0.705	1.04	0.676	0.92	1.30	0.940	No
472	47.40	2.77	1.23	1.54	0.81	0.705	1.04	0.676	0.92	1.30	0.940	No
473	47.50	2.77	1.23	1.54	0.81	0.705	1.04	0.675	0.92	1.30	0.940	No
474	47.60	2.78	1.24	1.55	0.81	0.704	1.04	0.675	0.92	1.30	0.940	No
475	47.70	2.79	1.24	1.55	0.81	0.704	1.04	0.675	0.92	1.30	0.940	No
476	47.80	2.79	1.24	1.55	0.81	0.704	1.04	0.674	0.92	1.30	0.940	No
477	47.90	2.80	1.24	1.56	0.81	0.703	1.04	0.674	0.92	1.30	0.940	No
478	48.00	2.81	1.25	1.56	0.81	0.703	1.04	0.674	0.91	1.30	0.940	No
479	48.10	2.81	1.25	1.56	0.81	0.703	1.04	0.673	0.91	1.30	0.943	No
480	48.20	2.82	1.25	1.57	0.81	0.702	1.04	0.673	0.91	1.30	0.947	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
481	48.30	2.83	1.26	1.57	0.81	0.702	1.04	0.673	0.90	1.30	0.950	No
482	48.40	2.83	1.26	1.57	0.81	0.702	1.04	0.673	0.90	1.30	0.951	No
483	48.50	2.84	1.26	1.58	0.81	0.701	1.04	0.672	0.90	1.30	0.954	No
484	48.60	2.85	1.27	1.58	0.81	0.701	1.04	0.672	0.89	1.30	0.957	No
485	48.70	2.85	1.27	1.58	0.81	0.701	1.04	0.672	0.89	1.30	0.960	No
486	48.80	2.86	1.27	1.59	0.81	0.700	1.04	0.671	0.89	1.30	0.963	No
487	48.90	2.87	1.28	1.59	0.81	0.700	1.04	0.671	0.88	1.30	0.966	No
488	49.00	2.87	1.28	1.59	0.81	0.700	1.04	0.671	0.88	1.30	0.969	No
489	49.10	2.88	1.28	1.60	0.81	0.699	1.04	0.670	0.88	1.30	0.974	No
490	49.20	2.89	1.29	1.60	0.81	0.699	1.04	0.670	0.88	1.30	0.974	No
491	49.30	2.89	1.29	1.60	0.81	0.699	1.04	0.670	0.88	1.30	0.974	No
492	49.40	2.90	1.29	1.61	0.80	0.698	1.04	0.669	0.87	1.30	0.975	No
493	49.50	2.91	1.29	1.61	0.80	0.698	1.04	0.669	0.87	1.30	0.975	No
494	49.60	2.91	1.30	1.61	0.80	0.697	1.04	0.668	0.87	1.30	0.975	No
495	49.70	2.92	1.30	1.62	0.80	0.697	1.04	0.668	0.87	1.30	0.975	No
496	49.80	2.93	1.30	1.62	0.80	0.697	1.04	0.668	0.87	1.30	0.976	No

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
 σ_v : Total overburden pressure at test point (tsf)
 u_0 : Water pressure at test point (tsf)
 σ_v' : Effective overburden pressure based on GWT during earthquake (tsf)
 r_d : Nonlinear shear mass factor
 CSR: Cyclic Stress Ratio
 MSF: Magnitude Scaling Factor
 CSR_{eq} : CSR adjusted for M=7.5
 K_σ : Effective overburden stress factor
 CSR*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1	0.30	80.54	44.21	2.27	0.32	1.70	131.32	77.03	208.35	4.000	No	No	2.00
2	0.40	76.12	45.53	2.28	0.33	1.70	125.33	76.44	201.77	4.000	No	No	2.00
3	0.50	68.91	47.85	2.31	0.35	1.70	110.04	73.95	184.00	4.000	No	No	2.00
4	0.60	61.08	50.53	2.34	0.37	1.70	96.58	71.85	168.43	4.000	No	No	2.00
5	0.70	55.64	51.98	2.36	0.39	1.70	87.59	70.14	157.73	4.000	No	No	2.00
6	0.80	52.36	52.02	2.36	0.40	1.70	83.88	69.16	153.04	4.000	No	No	2.00
7	0.90	50.29	51.14	2.35	0.41	1.70	80.78	67.94	148.71	4.000	No	No	2.00
8	1.00	48.50	49.82	2.34	0.41	1.70	77.63	66.48	144.11	4.000	No	No	2.00
9	1.10	46.72	48.25	2.32	0.42	1.70	75.24	65.09	140.33	4.000	No	No	2.00
10	1.20	45.12	46.48	2.29	0.43	1.70	72.22	63.38	135.60	4.000	No	No	2.00
11	1.30	43.40	45.15	2.28	0.43	1.70	69.94	62.07	132.01	4.000	No	No	2.00
12	1.40	41.62	44.80	2.27	0.44	1.70	66.97	61.11	128.09	4.000	No	No	2.00
13	1.50	39.65	45.22	2.28	0.45	1.70	63.64	60.50	124.14	4.000	No	No	2.00
14	1.60	37.61	45.72	2.28	0.46	1.70	60.42	59.95	120.36	4.000	No	No	2.00
15	1.70	35.63	45.72	2.28	0.46	1.70	57.16	59.11	116.28	4.000	No	No	2.00
16	1.80	33.95	45.22	2.28	0.47	1.70	54.11	58.07	112.18	4.000	No	No	2.00
17	1.90	32.57	44.21	2.27	0.48	1.70	52.31	57.07	109.38	4.000	No	No	2.00
18	2.00	31.19	42.99	2.25	0.48	1.70	50.52	55.95	106.47	4.000	No	No	2.00
19	2.10	29.70	42.10	2.24	0.49	1.70	47.47	54.68	102.15	4.000	No	No	2.00
20	2.20	27.91	42.29	2.24	0.50	1.70	45.15	54.21	99.36	4.000	No	No	2.00
21	2.30	25.92	43.92	2.26	0.51	1.70	41.87	54.29	96.15	4.000	No	No	2.00
22	2.40	23.95	46.43	2.29	0.52	1.70	37.91	54.52	92.43	4.000	No	No	2.00
23	2.50	22.19	48.90	2.32	0.52	1.70	35.65	55.01	90.65	4.000	No	No	2.00
24	2.60	20.94	50.28	2.34	0.53	1.70	33.37	54.96	88.33	4.000	No	No	2.00
25	2.70	20.11	50.23	2.34	0.53	1.70	31.87	54.54	86.41	4.000	No	No	2.00
26	2.80	19.97	48.52	2.32	0.53	1.70	31.67	53.81	85.47	4.000	No	No	2.00
27	2.90	20.60	46.27	2.29	0.53	1.70	32.72	53.11	85.83	4.000	No	No	2.00
28	3.00	21.67	46.21	2.29	0.52	1.70	34.91	53.64	88.55	4.000	Yes	No	2.00
29	3.10	22.10	50.26	2.34	0.51	1.70	36.81	55.86	92.67	4.000	Yes	No	2.00
30	3.20	20.76	57.84	2.44	0.51	1.70	34.80	57.87	92.67	4.000	Yes	No	2.00
31	3.30	18.46	67.26	2.55	0.53	1.70	28.44	58.36	86.80	4.000	Yes	No	2.00
32	3.40	16.29	76.07	2.66	0.53	1.70	25.73	0.00	25.73	4.000	Yes	Yes	2.00
33	3.50	15.43	81.50	2.73	0.54	1.70	24.31	0.00	24.31	4.000	Yes	Yes	2.00
34	3.60	15.14	84.79	2.77	0.54	1.70	24.31	0.00	24.31	4.000	Yes	Yes	2.00
35	3.70	15.27	86.35	2.79	0.53	1.70	24.31	0.00	24.31	4.000	No	Yes	2.00
36	3.80	15.71	86.61	2.80	0.53	1.70	24.93	0.00	24.93	4.000	No	Yes	2.00
37	3.90	16.02	86.61	2.80	0.53	1.70	26.44	0.00	26.44	4.000	No	Yes	2.00
38	4.00	15.90	87.37	2.80	0.53	1.70	25.80	0.00	25.80	4.000	No	Yes	2.00
39	4.10	15.47	88.72	2.82	0.53	1.70	24.35	0.00	24.35	4.000	No	Yes	2.00
40	4.20	15.30	89.32	2.83	0.53	1.70	24.38	0.00	24.38	4.000	No	Yes	2.00
41	4.30	15.03	89.73	2.83	0.53	1.70	24.96	0.00	24.96	4.000	No	Yes	2.00
42	4.40	13.95	91.66	2.86	0.54	1.70	23.07	0.00	23.07	4.000	No	Yes	2.00
43	4.50	12.08	95.53	2.91	0.55	1.70	19.18	0.00	19.18	4.000	No	Yes	2.00
44	4.60	10.23	99.43	2.96	0.56	1.70	15.92	0.00	15.92	4.000	No	Yes	2.00
45	4.70	8.88	100.00	2.98	0.57	1.70	14.17	0.00	14.17	4.000	No	Yes	2.00
46	4.80	7.65	100.00	3.01	0.57	1.70	12.69	0.00	12.69	4.000	No	Yes	2.00
47	4.90	6.48	100.00	3.04	0.58	1.70	10.00	0.00	10.00	4.000	No	Yes	2.00
48	5.00	5.29	100.00	3.09	0.59	1.70	8.50	0.00	8.50	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
49	5.10	4.54	100.00	3.13	0.59	1.70	6.99	0.00	6.99	4.000	No	Yes	2.00
50	5.20	4.11	100.00	3.15	0.60	1.70	6.40	0.00	6.40	4.000	No	Yes	2.00
51	5.30	3.98	100.00	3.14	0.60	1.70	6.40	0.00	6.40	4.000	No	Yes	2.00
52	5.40	3.98	100.00	3.13	0.60	1.70	6.40	0.00	6.40	4.000	No	Yes	2.00
53	5.50	3.98	100.00	3.13	0.60	1.70	6.40	0.00	6.40	4.000	No	Yes	2.00
54	5.60	3.95	100.00	3.15	0.60	1.70	6.40	0.00	6.40	4.000	No	Yes	2.00
55	5.70	3.84	100.00	3.19	0.60	1.70	6.25	0.00	6.25	4.000	No	Yes	2.00
56	5.80	3.71	100.00	3.23	0.60	1.70	5.87	0.00	5.87	4.000	No	Yes	2.00
57	5.90	3.67	100.00	3.26	0.60	1.70	5.76	0.00	5.76	4.000	No	Yes	2.00
58	6.00	3.78	100.00	3.27	0.60	1.70	6.07	0.00	6.07	4.000	No	Yes	2.00
59	6.10	3.92	100.00	3.27	0.60	1.70	6.40	0.00	6.40	4.000	No	Yes	2.00
60	6.20	3.98	100.00	3.28	0.60	1.70	6.40	0.00	6.40	4.000	No	Yes	2.00
61	6.30	3.98	100.00	3.29	0.60	1.70	6.40	0.00	6.40	4.000	No	Yes	2.00
62	6.40	4.19	100.00	3.28	0.60	1.70	6.40	0.00	6.40	4.000	No	Yes	2.00
63	6.50	4.70	100.00	3.26	0.59	1.70	7.38	0.00	7.38	4.000	No	Yes	2.00
64	6.60	5.51	100.00	3.21	0.59	1.70	8.86	0.00	8.86	4.000	No	Yes	2.00
65	6.70	6.36	100.00	3.17	0.58	1.70	10.28	0.00	10.28	4.000	No	Yes	2.00
66	6.80	6.92	100.00	3.15	0.58	1.70	11.52	0.00	11.52	4.000	No	Yes	2.00
67	6.90	7.07	100.00	3.15	0.58	1.70	11.52	0.00	11.52	4.000	No	Yes	2.00
68	7.00	7.06	100.00	3.17	0.58	1.70	11.01	0.00	11.01	4.000	No	Yes	2.00
69	7.10	7.53	100.00	3.15	0.58	1.70	11.47	0.00	11.47	4.000	No	Yes	2.00
70	7.20	8.17	100.00	3.11	0.57	1.70	13.79	0.00	13.79	4.000	No	Yes	2.00
71	7.30	8.41	100.00	3.10	0.57	1.70	14.07	0.00	14.07	4.000	No	Yes	2.00
72	7.40	8.09	100.00	3.12	0.57	1.70	12.64	0.00	12.64	4.000	No	Yes	2.00
73	7.50	8.74	100.00	3.11	0.57	1.70	12.24	0.00	12.24	4.000	No	Yes	2.00
74	7.60	10.99	100.00	3.05	0.56	1.67	16.88	0.00	16.88	4.000	No	Yes	2.00
75	7.70	13.63	100.00	3.00	0.54	1.63	22.50	0.00	22.50	4.000	No	Yes	2.00
76	7.80	15.24	100.00	2.97	0.53	1.61	23.64	0.00	23.64	4.000	No	Yes	2.00
77	7.90	15.53	99.55	2.96	0.53	1.60	23.48	0.00	23.48	4.000	No	Yes	2.00
78	8.00	15.24	99.02	2.95	0.53	1.59	23.27	0.00	23.27	4.000	No	Yes	2.00
79	8.10	14.56	98.73	2.95	0.54	1.59	22.04	0.00	22.04	4.000	No	Yes	2.00
80	8.20	13.55	98.76	2.95	0.54	1.59	20.32	0.00	20.32	4.000	No	Yes	2.00
81	8.30	12.33	99.38	2.95	0.55	1.60	18.76	0.00	18.76	4.000	No	Yes	2.00
82	8.40	11.42	99.77	2.96	0.56	1.60	16.69	0.00	16.69	4.000	No	Yes	2.00
83	8.50	10.85	99.69	2.96	0.56	1.60	16.23	0.00	16.23	4.000	No	Yes	2.00
84	8.60	10.72	98.82	2.95	0.56	1.59	16.19	0.00	16.19	4.000	No	Yes	2.00
85	8.70	10.46	98.77	2.95	0.56	1.59	16.00	0.00	16.00	4.000	No	Yes	2.00
86	8.80	10.06	99.79	2.96	0.56	1.59	14.95	0.00	14.95	4.000	No	Yes	2.00
87	8.90	9.83	100.00	2.98	0.57	1.59	14.34	0.00	14.34	4.000	No	Yes	2.00
88	9.00	10.07	100.00	2.97	0.56	1.58	14.90	0.00	14.90	4.000	No	Yes	2.00
89	9.10	10.47	99.82	2.96	0.56	1.57	15.85	0.00	15.85	4.000	No	Yes	2.00
90	9.20	10.73	98.87	2.95	0.56	1.57	15.93	0.00	15.93	4.000	No	Yes	2.00
91	9.30	10.76	98.88	2.95	0.56	1.56	15.88	0.00	15.88	4.000	No	Yes	2.00
92	9.40	10.76	99.64	2.96	0.56	1.56	15.84	0.00	15.84	4.000	No	Yes	2.00
93	9.50	10.76	100.00	2.97	0.56	1.55	15.79	0.00	15.79	4.000	No	Yes	2.00
94	9.60	11.08	100.00	2.97	0.56	1.55	15.75	0.00	15.75	4.000	No	Yes	2.00
95	9.70	12.05	97.76	2.93	0.56	1.54	17.07	0.00	17.07	4.000	No	Yes	2.00
96	9.80	15.58	89.03	2.83	0.55	1.53	19.71	0.00	19.71	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
97	9.90	20.15	80.69	2.72	0.52	1.49	30.01	0.00	30.01	4.000	No	Yes	2.00
98	10.00	20.15	80.19	2.71	0.50	1.47	35.22	0.00	35.22	4.000	No	Yes	2.00
99	10.10	15.24	87.81	2.81	0.55	1.52	19.53	0.00	19.53	4.000	No	Yes	2.00
100	10.20	9.08	100.00	3.00	0.58	1.55	9.70	0.00	9.70	4.000	No	Yes	2.00
101	10.30	6.68	100.00	3.10	0.58	1.54	10.17	0.00	10.17	4.000	No	Yes	2.00
102	10.40	6.06	100.00	3.12	0.58	1.54	9.40	0.00	9.40	4.000	No	Yes	2.00
103	10.50	5.06	100.00	3.18	0.59	1.55	6.97	0.00	6.97	4.000	No	Yes	2.00
104	10.60	4.24	100.00	3.25	0.60	1.55	5.84	0.00	5.84	4.000	No	Yes	2.00
105	10.70	3.95	100.00	3.27	0.60	1.55	5.83	0.00	5.83	4.000	No	Yes	2.00
106	10.80	3.84	100.00	3.29	0.60	1.55	5.67	0.00	5.67	4.000	No	Yes	2.00
107	10.90	3.70	100.00	3.34	0.60	1.55	5.32	0.00	5.32	4.000	No	Yes	2.00
108	11.00	3.61	100.00	3.37	0.60	1.54	5.22	0.00	5.22	4.000	No	Yes	2.00
109	11.10	3.66	100.00	3.37	0.60	1.54	5.21	0.00	5.21	4.000	No	Yes	2.00
110	11.20	3.79	100.00	3.35	0.60	1.53	5.52	0.00	5.52	4.000	No	Yes	2.00
111	11.30	4.04	100.00	3.33	0.60	1.53	5.76	0.00	5.76	4.000	No	Yes	2.00
112	11.40	4.70	100.00	3.28	0.60	1.52	6.25	0.00	6.25	4.000	No	Yes	2.00
113	11.50	5.71	100.00	3.21	0.59	1.51	8.26	0.00	8.26	4.000	No	Yes	2.00
114	11.60	6.66	100.00	3.16	0.58	1.50	9.95	0.00	9.95	4.000	No	Yes	2.00
115	11.70	7.46	100.00	3.12	0.58	1.50	10.14	0.00	10.14	4.000	No	Yes	2.00
116	11.80	8.53	100.00	3.09	0.58	1.49	11.49	0.00	11.49	4.000	No	Yes	2.00
117	11.90	10.10	100.00	3.03	0.57	1.47	14.24	0.00	14.24	4.000	No	Yes	2.00
118	12.00	11.40	100.00	2.97	0.56	1.46	16.40	0.00	16.40	4.000	No	Yes	2.00
119	12.10	12.05	97.36	2.93	0.56	1.46	16.63	0.00	16.63	4.000	No	Yes	2.00
120	12.20	11.99	96.06	2.91	0.56	1.45	16.71	0.00	16.71	4.000	No	Yes	2.00
121	12.30	11.24	97.19	2.93	0.56	1.45	16.06	0.00	16.06	4.000	No	Yes	2.00
122	12.40	9.78	100.00	2.97	0.57	1.46	13.52	0.00	13.52	4.000	No	Yes	2.00
123	12.50	7.81	100.00	3.05	0.58	1.46	10.79	0.00	10.79	4.000	No	Yes	2.00
124	12.60	5.80	100.00	3.15	0.59	1.47	8.06	0.00	8.06	4.000	No	Yes	2.00
125	12.70	4.05	100.00	3.28	0.60	1.48	5.28	0.00	5.28	4.000	No	Yes	2.00
126	12.80	3.26	100.00	3.32	0.61	1.48	3.61	0.00	3.61	4.000	No	Yes	2.00
127	12.90	3.58	100.00	3.17	0.60	1.48	4.75	0.00	4.75	4.000	No	Yes	2.00
128	13.00	4.31	100.00	3.01	0.60	1.47	6.59	0.00	6.59	4.000	No	Yes	2.00
129	13.10	4.77	100.00	2.98	0.60	1.46	6.61	0.00	6.61	4.000	No	Yes	2.00
130	13.20	4.87	100.00	3.06	0.60	1.46	6.60	0.00	6.60	4.000	No	Yes	2.00
131	13.30	5.19	100.00	3.12	0.59	1.46	6.94	0.00	6.94	4.000	No	Yes	2.00
132	13.40	5.59	100.00	3.15	0.59	1.45	7.88	0.00	7.88	4.000	No	Yes	2.00
133	13.50	5.90	100.00	3.17	0.59	1.45	8.16	0.00	8.16	4.000	No	Yes	2.00
134	13.60	6.41	100.00	3.17	0.59	1.44	8.14	0.00	8.14	4.000	No	Yes	2.00
135	13.70	7.60	100.00	3.11	0.58	1.43	9.84	0.00	9.84	4.000	No	Yes	2.00
136	13.80	9.89	100.00	2.97	0.57	1.42	12.82	0.00	12.82	4.000	No	Yes	2.00
137	13.90	12.14	91.56	2.86	0.56	1.41	17.05	0.00	17.05	4.000	No	Yes	2.00
138	14.00	13.09	88.12	2.81	0.55	1.40	18.50	0.00	18.50	4.000	No	Yes	2.00
139	14.10	12.44	91.83	2.86	0.56	1.40	16.43	0.00	16.43	4.000	No	Yes	2.00
140	14.20	12.59	95.97	2.91	0.57	1.40	14.41	0.00	14.41	4.000	Yes	Yes	2.00
141	14.30	16.22	89.26	2.83	0.55	1.39	18.94	0.00	18.94	4.000	Yes	Yes	2.00
142	14.40	23.62	73.96	2.64	0.52	1.36	29.93	0.00	29.93	4.000	Yes	Yes	2.00
143	14.50	32.92	57.43	2.43	0.49	1.33	41.69	59.66	101.34	4.000	Yes	No	2.00
144	14.60	41.56	42.22	2.24	0.48	1.32	52.82	56.07	108.89	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
145	14.70	48.47	30.74	2.10	0.48	1.32	61.19	48.52	109.71	4.000	Yes	No	2.00
146	14.80	52.66	25.32	2.03	0.48	1.31	66.78	42.36	109.14	4.000	Yes	No	2.00
147	14.90	53.17	25.29	2.03	0.48	1.31	67.94	42.53	110.48	4.000	Yes	No	2.00
148	15.00	49.27	30.51	2.09	0.47	1.30	62.58	48.55	111.13	4.000	Yes	No	2.00
149	15.10	40.94	40.51	2.22	0.48	1.31	52.07	54.83	106.90	4.000	Yes	No	2.00
150	15.20	30.97	53.77	2.38	0.51	1.32	37.50	57.33	94.83	4.000	Yes	No	2.00
151	15.30	21.85	68.47	2.57	0.53	1.34	26.38	58.01	84.38	4.000	Yes	No	2.00
152	15.40	15.51	80.99	2.72	0.56	1.35	18.85	0.00	18.85	4.000	Yes	Yes	2.00
153	15.50	11.13	91.00	2.85	0.57	1.36	14.06	0.00	14.06	4.000	Yes	Yes	2.00
154	15.60	8.16	98.38	2.94	0.58	1.37	9.92	0.00	9.92	4.000	Yes	Yes	2.00
155	15.70	6.23	100.00	3.00	0.59	1.37	7.59	0.00	7.59	4.000	Yes	Yes	2.00
156	15.80	5.38	100.00	2.99	0.60	1.37	6.69	0.00	6.69	4.000	No	Yes	2.00
157	15.90	5.36	95.47	2.91	0.60	1.37	6.62	0.00	6.62	4.000	No	Yes	2.00
158	16.00	5.34	91.21	2.85	0.59	1.37	7.51	0.00	7.51	4.000	No	Yes	2.00
159	16.10	4.96	92.49	2.87	0.60	1.37	6.58	0.00	6.58	4.000	No	Yes	2.00
160	16.20	4.35	98.48	2.94	0.60	1.37	5.15	0.00	5.15	4.000	No	Yes	2.00
161	16.30	3.98	100.00	3.02	0.60	1.37	5.15	0.00	5.15	4.000	No	Yes	2.00
162	16.40	3.98	100.00	3.05	0.60	1.37	5.14	0.00	5.14	4.000	No	Yes	2.00
163	16.50	3.98	100.00	3.07	0.60	1.36	5.13	0.00	5.13	4.000	No	Yes	2.00
164	16.60	3.98	100.00	3.08	0.60	1.36	5.13	0.00	5.13	4.000	No	Yes	2.00
165	16.70	3.98	100.00	3.08	0.60	1.36	5.12	0.00	5.12	4.000	No	Yes	2.00
166	16.80	3.98	100.00	3.08	0.60	1.36	5.11	0.00	5.11	4.000	No	Yes	2.00
167	16.90	3.98	100.00	3.08	0.60	1.36	5.11	0.00	5.11	4.000	No	Yes	2.00
168	17.00	3.98	100.00	3.09	0.60	1.36	5.10	0.00	5.10	4.000	No	Yes	2.00
169	17.10	3.94	100.00	3.14	0.60	1.35	5.09	0.00	5.09	4.000	No	Yes	2.00
170	17.20	4.08	100.00	3.17	0.60	1.35	4.93	0.00	4.93	4.000	No	Yes	2.00
171	17.30	5.02	100.00	3.12	0.60	1.35	5.61	0.00	5.61	4.000	No	Yes	2.00
172	17.40	6.54	100.00	3.06	0.59	1.34	8.60	0.00	8.60	4.000	No	Yes	2.00
173	17.50	8.33	100.00	3.01	0.58	1.33	10.57	0.00	10.57	4.000	No	Yes	2.00
174	17.60	9.72	100.00	2.98	0.57	1.32	12.22	0.00	12.22	4.000	No	Yes	2.00
175	17.70	10.81	99.40	2.95	0.57	1.32	13.64	0.00	13.64	4.000	No	Yes	2.00
176	17.80	11.39	97.48	2.93	0.57	1.31	14.48	0.00	14.48	4.000	No	Yes	2.00
177	17.90	11.17	97.14	2.93	0.57	1.31	14.26	0.00	14.26	4.000	No	Yes	2.00
178	18.00	10.46	98.27	2.94	0.57	1.31	12.75	0.00	12.75	4.000	No	Yes	2.00
179	18.10	9.58	100.00	2.97	0.58	1.31	11.83	0.00	11.83	4.000	No	Yes	2.00
180	18.20	8.88	100.00	2.99	0.58	1.31	10.99	0.00	10.99	4.000	No	Yes	2.00
181	18.30	8.09	100.00	3.02	0.58	1.31	10.13	0.00	10.13	4.000	No	Yes	2.00
182	18.40	7.19	100.00	3.07	0.59	1.31	8.91	0.00	8.91	4.000	No	Yes	2.00
183	18.50	6.45	100.00	3.12	0.59	1.31	7.65	0.00	7.65	4.000	No	Yes	2.00
184	18.60	6.04	100.00	3.14	0.59	1.31	7.39	0.00	7.39	4.000	No	Yes	2.00
185	18.70	5.99	100.00	3.14	0.59	1.31	7.38	0.00	7.38	4.000	No	Yes	2.00
186	18.80	6.24	100.00	3.11	0.59	1.30	7.42	0.00	7.42	4.000	No	Yes	2.00
187	18.90	6.64	100.00	3.07	0.59	1.30	8.24	0.00	8.24	4.000	No	Yes	2.00
188	19.00	7.02	100.00	3.02	0.59	1.30	8.78	0.00	8.78	4.000	No	Yes	2.00
189	19.10	7.02	100.00	3.01	0.59	1.29	8.77	0.00	8.77	4.000	No	Yes	2.00
190	19.20	6.63	100.00	3.01	0.59	1.29	8.20	0.00	8.20	4.000	No	Yes	2.00
191	19.30	6.23	100.00	3.03	0.59	1.29	7.36	0.00	7.36	4.000	No	Yes	2.00
192	19.40	6.06	100.00	3.06	0.59	1.29	7.29	0.00	7.29	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
193	19.50	6.65	100.00	3.07	0.59	1.29	7.53	0.00	7.53	4.000	No	Yes	2.00
194	19.60	7.86	100.00	3.05	0.58	1.28	9.44	0.00	9.44	4.000	No	Yes	2.00
195	19.70	9.33	100.00	3.01	0.58	1.28	11.57	0.00	11.57	4.000	No	Yes	2.00
196	19.80	12.75	94.74	2.90	0.57	1.27	12.71	0.00	12.71	4.000	No	Yes	2.00
197	19.90	18.72	83.02	2.75	0.55	1.25	21.42	0.00	21.42	4.000	No	Yes	2.00
198	20.00	20.77	78.93	2.70	0.51	1.23	32.06	0.00	32.06	4.000	No	Yes	2.00
199	20.10	17.42	82.20	2.74	0.55	1.25	19.80	0.00	19.80	4.000	No	Yes	2.00
200	20.20	10.46	94.99	2.90	0.59	1.27	9.61	0.00	9.61	4.000	No	Yes	2.00
201	20.30	7.00	100.00	3.06	0.59	1.27	7.92	0.00	7.92	4.000	No	Yes	2.00
202	20.40	6.52	100.00	3.09	0.59	1.27	7.61	0.00	7.61	4.000	No	Yes	2.00
203	20.50	6.31	100.00	3.12	0.59	1.26	7.85	0.00	7.85	4.000	No	Yes	2.00
204	20.60	6.18	100.00	3.15	0.59	1.26	7.16	0.00	7.16	4.000	No	Yes	2.00
205	20.70	5.98	100.00	3.19	0.59	1.26	7.12	0.00	7.12	4.000	No	Yes	2.00
206	20.80	6.14	100.00	3.21	0.59	1.26	7.11	0.00	7.11	4.000	No	Yes	2.00
207	20.90	7.00	100.00	3.19	0.59	1.26	7.66	0.00	7.66	4.000	No	Yes	2.00
208	21.00	8.96	100.00	3.11	0.58	1.25	10.11	0.00	10.11	4.000	No	Yes	2.00
209	21.10	11.72	100.00	2.99	0.57	1.24	13.87	0.00	13.87	4.000	No	Yes	2.00
210	21.20	14.03	94.64	2.90	0.56	1.23	17.16	0.00	17.16	4.000	No	Yes	2.00
211	21.30	14.79	91.87	2.86	0.55	1.23	17.99	0.00	17.99	4.000	No	Yes	2.00
212	21.40	14.13	94.16	2.89	0.56	1.23	16.41	0.00	16.41	4.000	No	Yes	2.00
213	21.50	12.43	100.00	2.97	0.56	1.23	14.78	0.00	14.78	4.000	No	Yes	2.00
214	21.60	10.28	100.00	3.08	0.57	1.23	12.08	0.00	12.08	4.000	No	Yes	2.00
215	21.70	8.08	100.00	3.20	0.59	1.23	8.97	0.00	8.97	4.000	No	Yes	2.00
216	21.80	6.21	100.00	3.33	0.59	1.23	7.15	0.00	7.15	4.000	No	Yes	2.00
217	21.90	5.28	100.00	3.40	0.60	1.24	5.59	0.00	5.59	4.000	No	Yes	2.00
218	22.00	5.34	100.00	3.37	0.60	1.23	5.73	0.00	5.73	4.000	No	Yes	2.00
219	22.10	6.13	100.00	3.29	0.59	1.23	7.32	0.00	7.32	4.000	No	Yes	2.00
220	22.20	7.05	100.00	3.22	0.59	1.22	8.29	0.00	8.29	4.000	No	Yes	2.00
221	22.30	7.61	100.00	3.18	0.59	1.22	8.86	0.00	8.86	4.000	No	Yes	2.00
222	22.40	8.13	100.00	3.16	0.59	1.22	9.17	0.00	9.17	4.000	No	Yes	2.00
223	22.50	9.00	100.00	3.13	0.58	1.22	10.02	0.00	10.02	4.000	No	Yes	2.00
224	22.60	9.37	100.00	3.13	0.58	1.21	11.78	0.00	11.78	4.000	No	Yes	2.00
225	22.70	8.82	100.00	3.16	0.58	1.21	10.38	0.00	10.38	4.000	No	Yes	2.00
226	22.80	7.69	100.00	3.22	0.59	1.21	8.08	0.00	8.08	4.000	No	Yes	2.00
227	22.90	6.90	100.00	3.27	0.59	1.21	7.91	0.00	7.91	4.000	No	Yes	2.00
228	23.00	6.98	100.00	3.26	0.59	1.21	7.67	0.00	7.67	4.000	No	Yes	2.00
229	23.10	7.60	100.00	3.22	0.59	1.21	8.31	0.00	8.31	4.000	No	Yes	2.00
230	23.20	8.28	100.00	3.18	0.58	1.20	9.94	0.00	9.94	4.000	No	Yes	2.00
231	23.30	8.77	100.00	3.15	0.58	1.20	9.92	0.00	9.92	4.000	No	Yes	2.00
232	23.40	8.77	100.00	3.15	0.58	1.20	9.90	0.00	9.90	4.000	No	Yes	2.00
233	23.50	8.95	100.00	3.15	0.58	1.19	9.89	0.00	9.89	4.000	No	Yes	2.00
234	23.60	9.45	100.00	3.13	0.58	1.19	10.49	0.00	10.49	4.000	No	Yes	2.00
235	23.70	9.65	100.00	3.13	0.58	1.19	11.50	0.00	11.50	4.000	No	Yes	2.00
236	23.80	9.37	100.00	3.15	0.58	1.19	10.51	0.00	10.51	4.000	No	Yes	2.00
237	23.90	9.41	100.00	3.17	0.58	1.19	9.50	0.00	9.50	4.000	No	Yes	2.00
238	24.00	11.56	100.00	3.08	0.58	1.18	11.58	0.00	11.58	4.000	No	Yes	2.00
239	24.10	16.37	95.99	2.91	0.56	1.17	17.53	0.00	17.53	4.000	No	Yes	2.00
240	24.20	22.14	82.82	2.75	0.53	1.16	25.16	0.00	25.16	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
241	24.30	26.41	72.99	2.62	0.52	1.16	30.23	0.00	30.23	4.000	No	Yes	2.00
242	24.40	28.09	68.38	2.57	0.52	1.15	31.25	59.40	90.65	0.126	No	No	0.14
243	24.50	26.73	70.98	2.60	0.52	1.15	30.44	59.67	90.11	0.126	No	No	0.14
244	24.60	23.36	79.06	2.70	0.53	1.15	25.72	0.00	25.72	4.000	No	Yes	2.00
245	24.70	20.44	87.91	2.81	0.55	1.16	20.27	0.00	20.27	4.000	No	Yes	2.00
246	24.80	19.80	92.02	2.86	0.54	1.15	20.91	0.00	20.91	4.000	No	Yes	2.00
247	24.90	20.81	91.25	2.85	0.54	1.15	23.51	0.00	23.51	4.000	No	Yes	2.00
248	25.00	21.40	89.57	2.83	0.54	1.15	23.38	0.00	23.38	4.000	No	Yes	2.00
249	25.10	22.04	86.59	2.79	0.54	1.15	22.70	0.00	22.70	4.000	No	Yes	2.00
250	25.20	22.96	83.35	2.75	0.53	1.14	25.43	0.00	25.43	4.000	No	Yes	2.00
251	25.30	23.14	83.23	2.75	0.53	1.14	26.18	0.00	26.18	4.000	No	Yes	2.00
252	25.40	22.74	86.87	2.80	0.54	1.14	23.14	0.00	23.14	4.000	No	Yes	2.00
253	25.50	24.78	88.82	2.82	0.54	1.14	24.02	0.00	24.02	4.000	Yes	Yes	2.00
254	25.60	33.66	81.53	2.73	0.51	1.13	32.44	0.00	32.44	4.000	Yes	Yes	2.00
255	25.70	53.07	66.34	2.54	0.47	1.11	50.66	64.57	115.23	4.000	Yes	No	2.00
256	25.80	82.74	49.05	2.33	0.40	1.10	83.42	67.63	151.06	4.000	Yes	No	2.00
257	25.90	117.80	33.49	2.13	0.35	1.08	121.98	64.67	186.66	4.000	Yes	No	2.00
258	26.00	148.57	21.26	1.98	0.33	1.07	155.60	48.12	203.71	4.000	Yes	No	2.00
259	26.10	167.69	13.94	1.89	0.33	1.07	175.41	25.17	200.57	4.000	Yes	No	2.00
260	26.20	173.65	11.16	1.85	0.34	1.07	179.49	14.24	193.74	4.000	Yes	No	2.00
261	26.30	170.00	11.87	1.86	0.34	1.07	173.70	16.74	190.44	1.150	No	No	1.35
262	26.40	161.80	14.16	1.89	0.34	1.07	164.19	25.21	189.40	1.094	No	No	1.28
263	26.50	152.97	16.88	1.92	0.35	1.07	154.11	34.33	188.44	1.046	No	No	1.22
264	26.60	145.31	19.54	1.96	0.35	1.07	146.34	41.92	188.25	1.037	No	No	1.21
265	26.70	141.26	20.93	1.97	0.35	1.07	140.45	45.01	185.46	0.914	No	No	1.06
266	26.80	141.98	20.51	1.97	0.35	1.07	141.36	44.02	185.38	0.911	No	No	1.06
267	26.90	146.65	18.61	1.95	0.35	1.07	147.98	39.33	187.31	0.993	No	No	1.16
268	27.00	152.40	16.36	1.92	0.35	1.07	153.97	32.50	186.47	0.956	No	No	1.11
269	27.10	156.02	14.52	1.89	0.35	1.06	158.16	26.14	184.30	0.869	No	No	1.01
270	27.20	156.40	13.50	1.88	0.36	1.06	158.55	22.28	180.83	0.752	No	No	0.87
271	27.30	153.19	13.35	1.88	0.36	1.06	154.90	21.44	176.33	0.631	No	No	0.72
272	27.40	147.34	13.67	1.88	0.37	1.06	148.41	22.21	170.62	0.515	No	No	0.59
273	27.50	139.24	14.02	1.89	0.38	1.06	140.94	22.99	163.92	0.416	No	No	0.47
274	27.60	130.22	14.06	1.89	0.40	1.07	130.69	22.38	153.07	0.311	No	No	0.35
275	27.70	121.27	13.86	1.89	0.42	1.07	121.60	21.01	142.61	0.247	No	No	0.27
276	27.80	114.09	13.30	1.88	0.43	1.07	114.38	18.65	133.03	0.207	No	No	0.23
277	27.90	109.39	12.59	1.87	0.45	1.07	109.36	15.99	125.34	0.184	No	No	0.20
278	28.00	107.21	12.64	1.87	0.45	1.07	107.51	16.05	123.56	0.180	No	No	0.20
279	28.10	107.70	13.99	1.89	0.44	1.06	107.47	20.44	127.91	0.191	No	No	0.21
280	28.20	110.28	15.79	1.91	0.43	1.06	110.02	26.38	136.40	0.220	No	No	0.24
281	28.30	114.57	16.99	1.92	0.41	1.06	114.22	30.50	144.72	0.258	No	No	0.28
282	28.40	120.76	16.85	1.92	0.40	1.05	119.28	30.60	149.88	0.288	No	No	0.32
283	28.50	128.38	15.92	1.91	0.39	1.05	127.54	28.44	155.98	0.334	No	No	0.37
284	28.60	137.33	15.01	1.90	0.38	1.05	136.01	26.11	162.11	0.395	No	No	0.44
285	28.70	146.10	14.82	1.90	0.37	1.05	144.83	26.16	171.00	0.521	No	No	0.59
286	28.80	153.76	15.35	1.90	0.36	1.04	152.36	28.73	181.10	0.760	No	No	0.86
287	28.90	159.82	16.01	1.91	0.34	1.04	157.42	31.61	189.03	1.075	No	No	1.23
288	29.00	164.17	16.45	1.92	0.34	1.04	161.55	33.60	195.15	1.455	No	No	1.67

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
289	29.10	166.84	16.60	1.92	0.33	1.04	164.15	34.38	198.53	1.743	No	No	2.00
290	29.20	167.23	16.70	1.92	0.33	1.03	164.46	34.77	199.23	1.812	No	No	2.00
291	29.30	165.31	17.20	1.93	0.33	1.03	162.03	36.31	198.34	1.725	No	No	1.97
292	29.40	162.24	18.24	1.94	0.33	1.03	157.97	39.36	197.33	1.632	No	No	1.86
293	29.50	159.54	18.96	1.95	0.33	1.03	154.97	41.28	196.25	1.541	No	No	1.76
294	29.60	158.40	18.33	1.94	0.34	1.03	153.68	39.14	192.82	1.292	No	No	1.47
295	29.70	158.21	16.24	1.92	0.35	1.03	154.29	32.11	186.41	0.954	No	No	1.08
296	29.80	154.57	18.16	1.94	0.34	1.03	153.95	38.60	192.55	1.275	No	No	1.45
297	29.90	143.99	27.24	2.05	0.33	1.03	142.38	59.45	201.83	2.101	No	No	2.00
298	30.00	135.18	33.40	2.13	0.35	1.03	122.89	64.76	187.65	1.009	No	No	1.14
299	30.10	132.28	31.64	2.11	0.34	1.03	127.82	63.55	191.37	1.202	No	No	1.36
300	30.20	131.76	25.25	2.03	0.35	1.02	133.66	54.02	187.68	1.010	No	No	1.14
301	30.30	123.68	25.46	2.03	0.37	1.02	121.16	52.22	173.38	0.566	No	No	0.63
302	30.40	107.40	35.76	2.16	0.38	1.02	104.21	63.22	167.43	0.464	No	No	0.51
303	30.50	91.85	46.01	2.29	0.40	1.02	86.35	66.75	153.10	0.311	No	No	0.34
304	30.60	84.79	51.78	2.36	0.42	1.02	75.92	66.92	142.84	0.248	No	No	0.27
305	30.70	90.92	49.58	2.33	0.40	1.02	83.48	67.91	151.40	0.298	No	No	0.33
306	30.80	108.65	41.18	2.23	0.37	1.02	103.59	67.86	171.44	0.529	No	No	0.59
307	30.90	128.66	31.63	2.11	0.34	1.02	126.40	63.23	189.63	1.106	No	No	1.25
308	31.00	143.23	24.60	2.02	0.34	1.01	140.49	53.85	194.34	1.395	No	No	1.57
309	31.10	150.57	21.24	1.98	0.34	1.01	144.95	46.50	191.45	1.207	No	No	1.36
310	31.20	153.08	20.87	1.97	0.34	1.01	147.02	45.80	192.82	1.292	No	No	1.45
311	31.30	152.85	21.66	1.98	0.34	1.01	147.23	47.94	195.17	1.456	No	No	1.64
312	31.40	149.11	23.35	2.00	0.34	1.01	143.75	51.58	195.33	1.468	No	No	1.65
313	31.50	141.26	26.23	2.04	0.34	1.01	135.86	56.33	192.19	1.252	No	No	1.41
314	31.60	130.34	29.98	2.09	0.35	1.01	124.33	60.46	184.78	0.888	No	No	0.99
315	31.70	118.72	33.44	2.13	0.36	1.01	112.21	62.48	174.68	0.593	No	No	0.66
316	31.80	108.66	35.61	2.16	0.38	1.01	102.35	62.65	165.00	0.430	No	No	0.47
317	31.90	100.38	36.65	2.17	0.39	1.01	95.33	62.06	157.38	0.346	No	No	0.38
318	32.00	93.10	38.12	2.19	0.40	1.00	88.31	61.72	150.03	4.000	Yes	No	2.00
319	32.10	86.10	41.64	2.23	0.41	1.00	81.32	62.72	144.04	4.000	Yes	No	2.00
320	32.20	78.52	47.80	2.31	0.42	1.00	75.11	64.82	139.94	4.000	Yes	No	2.00
321	32.30	69.94	55.82	2.41	0.43	1.00	66.49	65.96	132.46	4.000	Yes	No	2.00
322	32.40	60.92	64.44	2.52	0.45	1.00	56.68	65.83	122.51	4.000	Yes	No	2.00
323	32.50	53.88	71.48	2.61	0.47	1.00	49.30	0.00	49.30	4.000	Yes	Yes	2.00
324	32.60	50.19	75.76	2.66	0.47	1.00	46.31	0.00	46.31	4.000	Yes	Yes	2.00
325	32.70	49.69	77.76	2.68	0.47	0.99	46.04	0.00	46.04	4.000	No	Yes	2.00
326	32.80	52.24	77.74	2.68	0.47	0.99	47.66	0.00	47.66	4.000	No	Yes	2.00
327	32.90	56.89	76.09	2.66	0.46	0.99	53.29	0.00	53.29	4.000	No	Yes	2.00
328	33.00	62.25	73.46	2.63	0.44	0.99	58.93	0.00	58.93	4.000	No	Yes	2.00
329	33.10	68.14	70.00	2.59	0.44	0.99	62.53	68.83	131.36	0.202	No	No	0.22
330	33.20	75.90	65.10	2.53	0.42	0.99	69.61	69.70	139.30	0.232	No	No	0.25
331	33.30	85.75	59.10	2.45	0.40	0.99	80.50	70.99	151.49	0.299	No	No	0.32
332	33.40	93.70	54.56	2.39	0.38	0.99	89.94	71.89	161.84	0.391	No	No	0.43
333	33.50	96.01	53.31	2.38	0.38	0.99	91.65	71.83	163.48	0.411	No	No	0.45
334	33.60	92.45	55.42	2.41	0.39	0.98	86.69	71.35	158.04	0.352	No	No	0.38
335	33.70	84.75	59.51	2.46	0.40	0.98	79.63	70.88	150.52	0.292	No	No	0.32
336	33.80	74.88	64.18	2.51	0.42	0.98	69.75	69.49	139.24	0.231	No	No	0.25

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
337	33.90	64.13	68.78	2.57	0.44	0.98	58.76	67.47	126.23	0.187	No	No	0.20
338	34.00	54.10	72.86	2.62	0.47	0.98	49.36	0.00	49.36	4.000	No	Yes	2.00
339	34.10	46.11	76.36	2.67	0.49	0.97	41.58	0.00	41.58	4.000	No	Yes	2.00
340	34.20	39.59	80.34	2.72	0.50	0.97	36.36	0.00	36.36	4.000	No	Yes	2.00
341	34.30	34.09	85.23	2.78	0.51	0.97	31.09	0.00	31.09	4.000	No	Yes	2.00
342	34.40	29.36	90.44	2.84	0.53	0.97	26.25	0.00	26.25	4.000	No	Yes	2.00
343	34.50	25.02	95.23	2.90	0.54	0.97	23.18	0.00	23.18	4.000	No	Yes	2.00
344	34.60	21.00	100.00	2.96	0.55	0.96	19.06	0.00	19.06	4.000	No	Yes	2.00
345	34.70	17.76	100.00	3.03	0.56	0.96	15.11	0.00	15.11	4.000	No	Yes	2.00
346	34.80	15.83	100.00	3.09	0.57	0.96	14.25	0.00	14.25	4.000	No	Yes	2.00
347	34.90	15.33	100.00	3.11	0.57	0.96	13.71	0.00	13.71	4.000	No	Yes	2.00
348	35.00	15.28	100.00	3.12	0.57	0.96	13.69	0.00	13.69	4.000	No	Yes	2.00
349	35.10	15.62	100.00	3.14	0.57	0.96	14.04	0.00	14.04	4.000	No	Yes	2.00
350	35.20	16.74	100.00	3.13	0.56	0.96	14.59	0.00	14.59	4.000	No	Yes	2.00
351	35.30	19.92	100.00	3.07	0.56	0.95	16.67	0.00	16.67	4.000	No	Yes	2.00
352	35.40	25.11	99.29	2.95	0.54	0.95	22.63	0.00	22.63	4.000	Yes	Yes	2.00
353	35.50	32.33	87.95	2.81	0.52	0.95	28.61	0.00	28.61	4.000	Yes	Yes	2.00
354	35.60	40.65	76.98	2.67	0.50	0.96	36.24	0.00	36.24	4.000	Yes	Yes	2.00
355	35.70	48.86	67.91	2.56	0.48	0.96	45.21	63.35	108.56	4.000	Yes	No	2.00
356	35.80	55.37	60.92	2.47	0.47	0.96	50.87	63.24	114.11	4.000	Yes	No	2.00
357	35.90	57.47	57.41	2.43	0.46	0.96	53.85	63.02	116.87	4.000	Yes	No	2.00
358	36.00	55.09	58.78	2.45	0.47	0.95	50.78	62.59	113.37	4.000	Yes	No	2.00
359	36.10	48.80	65.39	2.53	0.48	0.95	44.19	62.49	106.68	4.000	Yes	No	2.00
360	36.20	40.68	75.42	2.66	0.50	0.95	36.54	0.00	36.54	4.000	Yes	Yes	2.00
361	36.30	33.39	85.47	2.78	0.52	0.94	28.58	0.00	28.58	4.000	Yes	Yes	2.00
362	36.40	29.34	91.70	2.86	0.53	0.94	24.29	0.00	24.29	4.000	Yes	Yes	2.00
363	36.50	29.53	91.39	2.85	0.53	0.94	25.49	0.00	25.49	4.000	No	Yes	2.00
364	36.60	32.29	87.62	2.81	0.52	0.94	28.98	0.00	28.98	4.000	No	Yes	2.00
365	36.70	34.52	85.47	2.78	0.51	0.94	31.62	0.00	31.62	4.000	No	Yes	2.00
366	36.80	34.12	87.23	2.80	0.51	0.94	31.39	0.00	31.39	4.000	No	Yes	2.00
367	36.90	31.26	92.15	2.86	0.52	0.94	27.79	0.00	27.79	4.000	No	Yes	2.00
368	37.00	28.61	96.28	2.92	0.53	0.93	23.81	0.00	23.81	4.000	Yes	Yes	2.00
369	37.10	30.10	93.43	2.88	0.53	0.93	24.18	0.00	24.18	4.000	Yes	Yes	2.00
370	37.20	36.63	83.04	2.75	0.51	0.93	31.67	0.00	31.67	4.000	Yes	Yes	2.00
371	37.30	46.22	71.02	2.60	0.49	0.94	41.21	0.00	41.21	4.000	Yes	Yes	2.00
372	37.40	55.48	62.12	2.49	0.47	0.94	49.77	63.26	113.02	4.000	Yes	No	2.00
373	37.50	62.76	57.13	2.43	0.46	0.94	56.45	63.65	120.10	4.000	Yes	No	2.00
374	37.60	68.04	54.13	2.39	0.45	0.94	60.65	63.75	124.40	4.000	Yes	No	2.00
375	37.70	71.11	51.75	2.36	0.44	0.94	63.82	63.66	127.48	0.190	No	No	0.20
376	37.80	72.57	50.05	2.34	0.44	0.94	64.53	63.12	127.65	0.191	No	No	0.20
377	37.90	72.53	49.94	2.34	0.44	0.94	64.37	63.03	127.40	0.190	No	No	0.20
378	38.00	71.83	50.58	2.34	0.44	0.93	63.50	63.08	126.57	0.188	No	No	0.20
379	38.10	71.07	50.61	2.35	0.45	0.93	62.42	62.80	125.22	0.184	No	No	0.19
380	38.20	70.43	49.69	2.33	0.45	0.93	62.08	62.31	124.39	0.182	No	No	0.19
381	38.30	69.54	49.24	2.33	0.45	0.93	61.54	61.97	123.51	0.180	No	No	0.19
382	38.40	67.93	50.65	2.35	0.45	0.93	59.82	62.13	121.95	0.176	No	No	0.19
383	38.50	66.57	53.45	2.38	0.46	0.93	57.54	62.65	120.19	0.172	No	No	0.18
384	38.60	67.27	55.41	2.41	0.45	0.93	57.71	63.41	121.12	0.174	No	No	0.18

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
385	38.70	70.56	55.41	2.41	0.45	0.93	61.52	64.45	125.97	0.186	No	No	0.20
386	38.80	74.92	54.26	2.39	0.44	0.93	66.20	65.30	131.50	0.202	No	No	0.21
387	38.90	78.18	53.35	2.38	0.43	0.93	69.24	65.78	135.01	0.214	No	No	0.23
388	39.00	79.69	53.18	2.38	0.43	0.93	70.10	65.94	136.03	0.218	No	No	0.23
389	39.10	79.93	53.38	2.38	0.43	0.93	70.02	66.00	136.02	0.218	No	No	0.23
390	39.20	80.59	52.98	2.37	0.43	0.92	69.65	65.74	135.38	0.216	No	No	0.23
391	39.30	82.67	51.32	2.35	0.43	0.92	71.63	65.57	137.20	0.223	No	No	0.24
392	39.40	86.56	48.55	2.32	0.42	0.92	75.34	65.26	140.60	0.237	No	No	0.25
393	39.50	91.52	45.36	2.28	0.41	0.92	79.83	64.71	144.53	0.257	No	No	0.27
394	39.60	96.64	42.46	2.24	0.41	0.92	84.68	64.12	148.80	0.281	No	No	0.30
395	39.70	100.82	40.94	2.22	0.40	0.93	88.83	64.06	152.89	4.000	Yes	No	2.00
396	39.80	100.16	43.50	2.26	0.39	0.93	90.88	66.36	157.24	4.000	Yes	No	2.00
397	39.90	91.82	50.93	2.35	0.40	0.92	82.75	68.36	151.11	4.000	Yes	No	2.00
398	40.00	78.37	60.78	2.47	0.43	0.92	66.31	67.54	133.85	4.000	Yes	No	2.00
399	40.10	62.81	71.44	2.61	0.45	0.91	54.72	0.00	54.72	4.000	Yes	Yes	2.00
400	40.20	50.47	80.59	2.72	0.49	0.90	41.17	0.00	41.17	4.000	Yes	Yes	2.00
401	40.30	42.83	87.88	2.81	0.51	0.90	33.61	0.00	33.61	4.000	Yes	Yes	2.00
402	40.40	43.11	88.18	2.81	0.50	0.90	34.53	0.00	34.53	4.000	Yes	Yes	2.00
403	40.50	50.11	81.45	2.73	0.48	0.90	41.74	0.00	41.74	4.000	Yes	Yes	2.00
404	40.60	60.63	71.50	2.61	0.46	0.90	51.76	0.00	51.76	4.000	Yes	Yes	2.00
405	40.70	71.15	61.52	2.48	0.44	0.91	61.94	66.53	128.47	4.000	Yes	No	2.00
406	40.80	79.36	53.55	2.38	0.43	0.91	69.24	65.86	135.09	4.000	Yes	No	2.00
407	40.90	84.78	50.59	2.34	0.42	0.91	73.22	65.67	138.89	4.000	Yes	No	2.00
408	41.00	87.82	50.24	2.34	0.42	0.91	76.05	66.26	142.31	0.245	No	No	0.26
409	41.10	89.49	49.98	2.34	0.41	0.91	77.08	66.41	143.49	0.251	No	No	0.27
410	41.20	89.73	49.03	2.33	0.41	0.91	77.42	66.04	143.46	0.251	No	No	0.27
411	41.30	88.42	49.22	2.33	0.42	0.91	76.45	65.88	142.34	0.245	No	No	0.26
412	41.40	85.38	51.62	2.36	0.42	0.90	73.35	66.16	139.51	4.000	Yes	No	2.00
413	41.50	81.32	54.27	2.39	0.43	0.90	69.15	66.11	135.27	4.000	Yes	No	2.00
414	41.60	76.93	57.08	2.43	0.44	0.90	65.51	66.13	131.64	4.000	Yes	No	2.00
415	41.70	71.43	60.96	2.47	0.44	0.90	61.61	66.27	127.88	4.000	Yes	No	2.00
416	41.80	63.51	66.88	2.55	0.46	0.89	54.52	65.80	120.33	4.000	Yes	No	2.00
417	41.90	53.29	75.13	2.65	0.48	0.89	44.68	0.00	44.68	4.000	Yes	Yes	2.00
418	42.00	42.53	84.54	2.77	0.50	0.88	34.94	0.00	34.94	4.000	Yes	Yes	2.00
419	42.10	34.54	92.14	2.86	0.53	0.88	26.71	0.00	26.71	4.000	Yes	Yes	2.00
420	42.20	31.16	94.75	2.90	0.53	0.87	24.17	0.00	24.17	4.000	Yes	Yes	2.00
421	42.30	31.50	93.73	2.88	0.53	0.87	26.25	0.00	26.25	4.000	No	Yes	2.00
422	42.40	32.59	92.86	2.87	0.52	0.87	27.47	0.00	27.47	4.000	No	Yes	2.00
423	42.50	33.35	92.03	2.86	0.53	0.87	26.84	0.00	26.84	4.000	No	Yes	2.00
424	42.60	35.87	87.17	2.80	0.52	0.87	28.05	0.00	28.05	4.000	No	Yes	2.00
425	42.70	41.37	77.50	2.68	0.51	0.87	33.73	0.00	33.73	4.000	No	Yes	2.00
426	42.80	48.14	67.62	2.56	0.49	0.88	40.65	61.97	102.61	0.141	No	No	0.15
427	42.90	52.92	62.91	2.50	0.48	0.88	45.12	62.14	107.27	0.148	No	No	0.16
428	43.00	54.26	63.53	2.51	0.48	0.88	45.76	62.49	108.25	0.149	No	No	0.16
429	43.10	53.34	67.60	2.56	0.48	0.88	43.94	62.91	106.86	0.147	No	No	0.16
430	43.20	52.35	71.53	2.61	0.49	0.87	42.66	0.00	42.66	4.000	No	Yes	2.00
431	43.30	52.52	73.79	2.63	0.48	0.87	43.13	0.00	43.13	4.000	No	Yes	2.00
432	43.40	52.22	75.68	2.66	0.48	0.87	44.27	0.00	44.27	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
433	43.50	48.54	80.41	2.72	0.48	0.87	41.76	0.00	41.76	4.000	No	Yes	2.00
434	43.60	41.40	89.10	2.83	0.50	0.87	33.70	0.00	33.70	4.000	No	Yes	2.00
435	43.70	34.45	98.98	2.95	0.53	0.86	26.15	0.00	26.15	4.000	No	Yes	2.00
436	43.80	31.79	100.00	3.01	0.53	0.86	24.16	0.00	24.16	4.000	No	Yes	2.00
437	43.90	34.60	100.00	2.97	0.52	0.86	26.95	0.00	26.95	4.000	Yes	Yes	2.00
438	44.00	42.45	91.46	2.86	0.51	0.86	33.06	0.00	33.06	4.000	Yes	Yes	2.00
439	44.10	56.31	77.24	2.68	0.48	0.87	43.75	0.00	43.75	4.000	Yes	Yes	2.00
440	44.20	76.28	61.46	2.48	0.44	0.88	61.94	66.51	128.45	4.000	Yes	No	2.00
441	44.30	99.38	48.75	2.32	0.40	0.89	84.19	67.68	151.87	4.000	Yes	No	2.00
442	44.40	119.56	40.58	2.22	0.37	0.89	103.56	67.38	170.94	4.000	Yes	No	2.00
443	44.50	132.51	36.32	2.17	0.36	0.90	114.67	66.17	180.84	4.000	Yes	No	2.00
444	44.60	138.38	33.63	2.13	0.35	0.90	118.03	63.97	182.00	4.000	Yes	No	2.00
445	44.70	140.97	34.85	2.15	0.35	0.90	118.86	65.56	184.42	0.874	No	No	0.93
446	44.80	145.61	38.55	2.19	0.34	0.90	121.47	69.93	191.41	1.205	No	No	1.28
447	44.90	154.46	38.98	2.20	0.33	0.90	130.69	72.52	203.21	2.278	No	No	2.00
448	45.00	166.62	34.89	2.15	0.31	0.91	142.76	70.97	213.73	4.000	No	No	2.00
449	45.10	178.48	28.56	2.07	0.31	0.91	153.79	64.02	217.81	4.000	No	No	2.00
450	45.20	186.02	24.96	2.02	0.30	0.91	161.76	58.30	220.06	4.000	No	No	2.00
451	45.30	188.08	24.44	2.02	0.30	0.91	162.14	57.19	219.33	4.000	No	No	2.00
452	45.40	185.50	24.94	2.02	0.31	0.90	158.63	57.72	216.35	4.000	No	No	2.00
453	45.50	181.44	25.74	2.03	0.31	0.90	154.35	58.69	213.04	4.000	No	No	2.00
454	45.60	177.58	26.31	2.04	0.32	0.90	150.79	59.22	210.01	3.490	No	No	2.00
455	45.70	174.36	26.81	2.05	0.32	0.90	147.88	59.66	207.54	2.972	No	No	2.00
456	45.80	172.20	27.16	2.05	0.32	0.90	145.28	59.84	205.12	2.556	No	No	2.00
457	45.90	170.69	27.52	2.06	0.32	0.90	144.64	60.39	205.03	2.542	No	No	2.00
458	46.00	169.69	28.04	2.06	0.32	0.90	143.53	61.10	204.63	2.481	No	No	2.00
459	46.10	168.85	28.76	2.07	0.32	0.89	142.37	62.12	204.49	2.460	No	No	2.00
460	46.20	168.16	29.62	2.08	0.32	0.89	142.23	63.52	205.75	2.657	No	No	2.00
461	46.30	168.23	30.32	2.09	0.32	0.89	141.54	64.49	206.03	2.703	No	No	2.00
462	46.40	169.90	30.26	2.09	0.32	0.89	142.39	64.56	206.95	2.864	No	No	2.00
463	46.50	173.64	29.08	2.08	0.32	0.89	146.41	63.47	209.87	3.459	No	No	2.00
464	46.60	178.99	26.94	2.05	0.31	0.89	151.06	60.50	211.56	3.872	No	No	2.00
465	46.70	184.20	24.61	2.02	0.31	0.89	156.00	56.53	212.53	4.000	No	No	2.00
466	46.80	187.77	22.49	1.99	0.31	0.89	159.38	51.96	211.34	3.814	No	No	2.00
467	46.90	188.69	20.57	1.97	0.32	0.89	159.36	46.70	206.06	2.709	No	No	2.00
468	47.00	186.98	18.98	1.95	0.33	0.89	156.95	41.59	198.55	1.745	No	No	1.83
469	47.10	183.33	18.14	1.94	0.34	0.88	153.24	38.47	191.72	1.223	No	No	1.29
470	47.20	178.78	18.23	1.94	0.35	0.88	148.40	38.16	186.56	0.960	No	No	1.02
471	47.30	174.33	19.01	1.95	0.35	0.88	144.14	40.08	184.21	0.866	No	No	0.92
472	47.40	170.46	20.09	1.96	0.35	0.88	141.23	42.83	184.06	0.860	No	No	0.92
473	47.50	167.19	21.18	1.98	0.35	0.88	138.22	45.36	183.58	0.843	No	No	0.90
474	47.60	164.34	22.21	1.99	0.35	0.87	135.63	47.58	183.20	0.829	No	No	0.88
475	47.70	161.94	23.20	2.00	0.35	0.87	133.78	49.62	183.41	0.837	No	No	0.89
476	47.80	159.85	24.09	2.01	0.35	0.87	131.94	51.30	183.24	0.830	No	No	0.88
477	47.90	158.50	24.96	2.02	0.35	0.87	130.13	52.81	182.94	0.820	No	No	0.87
478	48.00	158.82	25.54	2.03	0.35	0.87	130.20	53.98	184.18	0.865	No	No	0.92
479	48.10	160.82	26.11	2.04	0.35	0.87	132.77	55.55	188.32	1.040	No	No	1.10
480	48.20	163.04	26.79	2.05	0.34	0.88	135.51	57.32	192.83	1.293	No	No	1.36

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
481	48.30	164.06	27.76	2.06	0.34	0.88	136.20	59.20	195.40	1.474	No	No	1.55
482	48.40	164.39	28.69	2.07	0.33	0.88	135.58	60.67	196.25	1.541	No	No	1.62
483	48.50	165.33	29.14	2.08	0.33	0.88	136.39	61.57	197.96	1.690	No	No	1.77
484	48.60	167.37	29.04	2.08	0.33	0.88	138.59	61.86	200.45	1.941	No	No	2.00
485	48.70	169.66	28.78	2.07	0.33	0.88	140.83	61.87	202.69	2.209	No	No	2.00
486	48.80	171.13	28.93	2.07	0.32	0.88	142.28	62.39	204.67	2.487	No	No	2.00
487	48.90	171.49	29.92	2.09	0.32	0.88	142.38	64.02	206.40	2.767	No	No	2.00
488	49.00	171.23	31.63	2.11	0.32	0.88	141.84	66.49	208.33	3.127	No	No	2.00
489	49.10	171.53	33.46	2.13	0.32	0.88	141.77	68.97	210.74	3.664	No	No	2.00
490	49.20	174.62	34.36	2.14	0.31	0.88	143.38	70.46	213.84	4.000	No	No	2.00
491	49.30	181.47	33.73	2.13	0.30	0.88	150.24	71.18	221.41	4.000	No	No	2.00
492	49.40	191.66	31.66	2.11	0.29	0.89	160.10	70.38	230.48	4.000	No	No	2.00
493	49.50	202.91	28.80	2.07	0.28	0.89	170.54	67.73	238.27	4.000	No	No	2.00
494	49.60	212.53	25.95	2.04	0.28	0.89	180.00	63.75	243.75	4.000	No	No	2.00
495	49.70	219.60	23.48	2.01	0.28	0.89	185.10	58.65	243.74	4.000	No	No	2.00
496	49.80	223.07	22.02	1.99	0.28	0.89	188.51	55.17	243.68	4.000	No	No	2.00

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q_t :	Total cone resistance
FC:	Fines content (%)
I_c :	Soil behavior type index
m:	Stress exponent
C_N :	Overburden correction factor
q_{c1N} :	Normalized and adjusted cone resistance
Δq_{c1N} :	Cone resistance correction factor due to fines
$q_{c1N,cs}$:	Normalized and adjusted cone resistance
$CRR_{7.5}$:	Cyclic resistance ratio for $M_w=7.5$
FS:	Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
0.30	2.00	0.00	0.00	0.10	0.00	0.40	2.00	0.00	0.00	0.10	0.00
0.50	2.00	0.00	0.00	0.10	0.00	0.60	2.00	0.00	0.00	0.10	0.00
0.70	2.00	0.00	0.00	0.10	0.00	0.80	2.00	0.00	0.00	0.10	0.00
0.90	2.00	0.00	0.00	0.10	0.00	1.00	2.00	0.00	0.00	0.10	0.00
1.10	2.00	0.00	0.00	0.10	0.00	1.20	2.00	0.00	0.00	0.10	0.00
1.30	2.00	0.00	0.00	0.10	0.00	1.40	2.00	0.00	0.00	0.10	0.00
1.50	2.00	0.00	0.00	0.10	0.00	1.60	2.00	0.00	0.00	0.10	0.00
1.70	2.00	0.00	0.00	0.10	0.00	1.80	2.00	0.00	0.00	0.10	0.00
1.90	2.00	0.00	0.00	0.10	0.00	2.00	2.00	0.00	0.00	0.10	0.00
2.10	2.00	0.00	0.00	0.10	0.00	2.20	2.00	0.00	0.00	0.10	0.00
2.30	2.00	0.00	0.00	0.10	0.00	2.40	2.00	0.00	0.00	0.10	0.00
2.50	2.00	0.00	0.00	0.10	0.00	2.60	2.00	0.00	0.00	0.10	0.00
2.70	2.00	0.00	0.00	0.10	0.00	2.80	2.00	0.00	0.00	0.10	0.00
2.90	2.00	0.00	0.00	0.10	0.00	3.00	2.00	0.00	0.00	0.10	0.00
3.10	2.00	0.00	0.00	0.10	0.00	3.20	2.00	0.00	0.00	0.10	0.00
3.30	2.00	0.00	0.00	0.10	0.00	3.40	2.00	0.00	0.00	0.10	0.00
3.50	2.00	0.00	0.00	0.10	0.00	3.60	2.00	0.00	0.00	0.10	0.00
3.70	2.00	0.00	0.00	0.10	0.00	3.80	2.00	0.00	0.00	0.10	0.00
3.90	2.00	0.00	0.00	0.10	0.00	4.00	2.00	0.00	0.00	0.10	0.00
4.10	2.00	0.00	0.00	0.10	0.00	4.20	2.00	0.00	0.00	0.10	0.00
4.30	2.00	0.00	0.00	0.10	0.00	4.40	2.00	0.00	0.00	0.10	0.00
4.50	2.00	0.00	0.00	0.10	0.00	4.60	2.00	0.00	0.00	0.10	0.00
4.70	2.00	0.00	0.00	0.10	0.00	4.80	2.00	0.00	0.00	0.10	0.00
4.90	2.00	0.00	0.00	0.10	0.00	5.00	2.00	0.00	0.00	0.10	0.00
5.10	2.00	0.00	0.00	0.10	0.00	5.20	2.00	0.00	0.00	0.10	0.00
5.30	2.00	0.00	0.00	0.10	0.00	5.40	2.00	0.00	0.00	0.10	0.00
5.50	2.00	0.00	0.00	0.10	0.00	5.60	2.00	0.00	0.00	0.10	0.00
5.70	2.00	0.00	0.00	0.10	0.00	5.80	2.00	0.00	0.00	0.10	0.00
5.90	2.00	0.00	0.00	0.10	0.00	6.00	2.00	0.00	0.00	0.10	0.00
6.10	2.00	0.00	0.00	0.10	0.00	6.20	2.00	0.00	0.00	0.10	0.00
6.30	2.00	0.00	0.00	0.10	0.00	6.40	2.00	0.00	0.00	0.10	0.00
6.50	2.00	0.00	0.00	0.10	0.00	6.60	2.00	0.00	0.00	0.10	0.00
6.70	2.00	0.00	0.00	0.10	0.00	6.80	2.00	0.00	0.00	0.10	0.00
6.90	2.00	0.00	0.00	0.10	0.00	7.00	2.00	0.00	0.00	0.10	0.00
7.10	2.00	0.00	0.00	0.10	0.00	7.20	2.00	0.00	0.00	0.10	0.00
7.30	2.00	0.00	0.00	0.10	0.00	7.40	2.00	0.00	0.00	0.10	0.00
7.50	2.00	0.00	0.00	0.10	0.00	7.60	2.00	0.00	0.00	0.10	0.00
7.70	2.00	0.00	0.00	0.10	0.00	7.80	2.00	0.00	0.00	0.10	0.00
7.90	2.00	0.00	0.00	0.10	0.00	8.00	2.00	0.00	0.00	0.10	0.00
8.10	2.00	0.00	0.00	0.10	0.00	8.20	2.00	0.00	0.00	0.10	0.00
8.30	2.00	0.00	0.00	0.10	0.00	8.40	2.00	0.00	0.00	0.10	0.00
8.50	2.00	0.00	0.00	0.10	0.00	8.60	2.00	0.00	0.00	0.10	0.00
8.70	2.00	0.00	0.00	0.10	0.00	8.80	2.00	0.00	0.00	0.10	0.00
8.90	2.00	0.00	0.00	0.10	0.00	9.00	2.00	0.00	0.00	0.10	0.00
9.10	2.00	0.00	0.00	0.10	0.00	9.20	2.00	0.00	0.00	0.10	0.00
9.30	2.00	0.00	0.00	0.10	0.00	9.40	2.00	0.00	0.00	0.10	0.00
9.50	2.00	0.00	0.00	0.10	0.00	9.60	2.00	0.00	0.00	0.10	0.00
9.70	2.00	0.00	0.00	0.10	0.00	9.80	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data ::

Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
9.90	2.00	0.00	0.00	0.10	0.00	10.00	2.00	0.00	0.00	0.10	0.00
10.10	2.00	0.00	0.00	0.10	0.00	10.20	2.00	0.00	0.00	0.10	0.00
10.30	2.00	0.00	0.00	0.10	0.00	10.40	2.00	0.00	0.00	0.10	0.00
10.50	2.00	0.00	0.00	0.10	0.00	10.60	2.00	0.00	0.00	0.10	0.00
10.70	2.00	0.00	0.00	0.10	0.00	10.80	2.00	0.00	0.00	0.10	0.00
10.90	2.00	0.00	0.00	0.10	0.00	11.00	2.00	0.00	0.00	0.10	0.00
11.10	2.00	0.00	0.00	0.10	0.00	11.20	2.00	0.00	0.00	0.10	0.00
11.30	2.00	0.00	0.00	0.10	0.00	11.40	2.00	0.00	0.00	0.10	0.00
11.50	2.00	0.00	0.00	0.10	0.00	11.60	2.00	0.00	0.00	0.10	0.00
11.70	2.00	0.00	0.00	0.10	0.00	11.80	2.00	0.00	0.00	0.10	0.00
11.90	2.00	0.00	0.00	0.10	0.00	12.00	2.00	0.00	0.00	0.10	0.00
12.10	2.00	0.00	0.00	0.10	0.00	12.20	2.00	0.00	0.00	0.10	0.00
12.30	2.00	0.00	0.00	0.10	0.00	12.40	2.00	0.00	0.00	0.10	0.00
12.50	2.00	0.00	0.00	0.10	0.00	12.60	2.00	0.00	0.00	0.10	0.00
12.70	2.00	0.00	0.00	0.10	0.00	12.80	2.00	0.00	0.00	0.10	0.00
12.90	2.00	0.00	0.00	0.10	0.00	13.00	2.00	0.00	0.00	0.10	0.00
13.10	2.00	0.00	0.00	0.10	0.00	13.20	2.00	0.00	0.00	0.10	0.00
13.30	2.00	0.00	0.00	0.10	0.00	13.40	2.00	0.00	0.00	0.10	0.00
13.50	2.00	0.00	0.00	0.10	0.00	13.60	2.00	0.00	0.00	0.10	0.00
13.70	2.00	0.00	0.00	0.10	0.00	13.80	2.00	0.00	0.00	0.10	0.00
13.90	2.00	0.00	0.00	0.10	0.00	14.00	2.00	0.00	0.00	0.10	0.00
14.10	2.00	0.00	0.00	0.10	0.00	14.20	2.00	0.00	0.00	0.10	0.00
14.30	2.00	0.00	0.00	0.10	0.00	14.40	2.00	0.00	0.00	0.10	0.00
14.50	2.00	0.00	0.00	0.10	0.00	14.60	2.00	0.00	0.00	0.10	0.00
14.70	2.00	0.00	0.00	0.10	0.00	14.80	2.00	0.00	0.00	0.10	0.00
14.90	2.00	0.00	0.00	0.10	0.00	15.00	2.00	0.00	0.00	0.10	0.00
15.10	2.00	0.00	0.00	0.10	0.00	15.20	2.00	0.00	0.00	0.10	0.00
15.30	2.00	0.00	0.00	0.10	0.00	15.40	2.00	0.00	0.00	0.10	0.00
15.50	2.00	0.00	0.00	0.10	0.00	15.60	2.00	0.00	0.00	0.10	0.00
15.70	2.00	0.00	0.00	0.10	0.00	15.80	2.00	0.00	0.00	0.10	0.00
15.90	2.00	0.00	0.00	0.10	0.00	16.00	2.00	0.00	0.00	0.10	0.00
16.10	2.00	0.00	0.00	0.10	0.00	16.20	2.00	0.00	0.00	0.10	0.00
16.30	2.00	0.00	0.00	0.10	0.00	16.40	2.00	0.00	0.00	0.10	0.00
16.50	2.00	0.00	0.00	0.10	0.00	16.60	2.00	0.00	0.00	0.10	0.00
16.70	2.00	0.00	0.00	0.10	0.00	16.80	2.00	0.00	0.00	0.10	0.00
16.90	2.00	0.00	0.00	0.10	0.00	17.00	2.00	0.00	0.00	0.10	0.00
17.10	2.00	0.00	0.00	0.10	0.00	17.20	2.00	0.00	0.00	0.10	0.00
17.30	2.00	0.00	0.00	0.10	0.00	17.40	2.00	0.00	0.00	0.10	0.00
17.50	2.00	0.00	0.00	0.10	0.00	17.60	2.00	0.00	0.00	0.10	0.00
17.70	2.00	0.00	0.00	0.10	0.00	17.80	2.00	0.00	0.00	0.10	0.00
17.90	2.00	0.00	0.00	0.10	0.00	18.00	2.00	0.00	0.00	0.10	0.00
18.10	2.00	0.00	0.00	0.10	0.00	18.20	2.00	0.00	0.00	0.10	0.00
18.30	2.00	0.00	0.00	0.10	0.00	18.40	2.00	0.00	0.00	0.10	0.00
18.50	2.00	0.00	0.00	0.10	0.00	18.60	2.00	0.00	0.00	0.10	0.00
18.70	2.00	0.00	0.00	0.10	0.00	18.80	2.00	0.00	0.00	0.10	0.00
18.90	2.00	0.00	0.00	0.10	0.00	19.00	2.00	0.00	0.00	0.10	0.00
19.10	2.00	0.00	0.00	0.10	0.00	19.20	2.00	0.00	0.00	0.10	0.00
19.30	2.00	0.00	0.00	0.10	0.00	19.40	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data ::

Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
19.50	2.00	0.00	0.00	0.10	0.00	19.60	2.00	0.00	0.00	0.10	0.00
19.70	2.00	0.00	0.00	0.10	0.00	19.80	2.00	0.00	0.00	0.10	0.00
19.90	2.00	0.00	0.00	0.10	0.00	20.00	2.00	0.00	0.00	0.10	0.00
20.10	2.00	0.00	0.00	0.10	0.00	20.20	2.00	0.00	0.00	0.10	0.00
20.30	2.00	0.00	0.00	0.10	0.00	20.40	2.00	0.00	0.00	0.10	0.00
20.50	2.00	0.00	0.00	0.10	0.00	20.60	2.00	0.00	0.00	0.10	0.00
20.70	2.00	0.00	0.00	0.10	0.00	20.80	2.00	0.00	0.00	0.10	0.00
20.90	2.00	0.00	0.00	0.10	0.00	21.00	2.00	0.00	0.00	0.10	0.00
21.10	2.00	0.00	0.00	0.10	0.00	21.20	2.00	0.00	0.00	0.10	0.00
21.30	2.00	0.00	0.00	0.10	0.00	21.40	2.00	0.00	0.00	0.10	0.00
21.50	2.00	0.00	0.00	0.10	0.00	21.60	2.00	0.00	0.00	0.10	0.00
21.70	2.00	0.00	0.00	0.10	0.00	21.80	2.00	0.00	0.00	0.10	0.00
21.90	2.00	0.00	0.00	0.10	0.00	22.00	2.00	0.00	0.00	0.10	0.00
22.10	2.00	0.00	0.00	0.10	0.00	22.20	2.00	0.00	0.00	0.10	0.00
22.30	2.00	0.00	0.00	0.10	0.00	22.40	2.00	0.00	0.00	0.10	0.00
22.50	2.00	0.00	0.00	0.10	0.00	22.60	2.00	0.00	0.00	0.10	0.00
22.70	2.00	0.00	0.00	0.10	0.00	22.80	2.00	0.00	0.00	0.10	0.00
22.90	2.00	0.00	0.00	0.10	0.00	23.00	2.00	0.00	0.00	0.10	0.00
23.10	2.00	0.00	0.00	0.10	0.00	23.20	2.00	0.00	0.00	0.10	0.00
23.30	2.00	0.00	0.00	0.10	0.00	23.40	2.00	0.00	0.00	0.10	0.00
23.50	2.00	0.00	0.00	0.10	0.00	23.60	2.00	0.00	0.00	0.10	0.00
23.70	2.00	0.00	0.00	0.10	0.00	23.80	2.00	0.00	0.00	0.10	0.00
23.90	2.00	0.00	0.00	0.10	0.00	24.00	2.00	0.00	0.00	0.10	0.00
24.10	2.00	0.00	0.00	0.10	0.00	24.20	2.00	0.00	0.00	0.10	0.00
24.30	2.00	0.00	0.00	0.10	0.00	24.40	0.14	0.00	0.00	0.10	0.16
24.50	0.14	0.00	0.00	0.10	0.16	24.60	2.00	0.00	0.00	0.10	0.00
24.70	2.00	0.00	0.00	0.10	0.00	24.80	2.00	0.00	0.00	0.10	0.00
24.90	2.00	0.00	0.00	0.10	0.00	25.00	2.00	0.00	0.00	0.10	0.00
25.10	2.00	0.00	0.00	0.10	0.00	25.20	2.00	0.00	0.00	0.10	0.00
25.30	2.00	0.00	0.00	0.10	0.00	25.40	2.00	0.00	0.00	0.10	0.00
25.50	2.00	0.00	0.00	0.10	0.00	25.60	2.00	0.00	0.00	0.10	0.00
25.70	2.00	0.00	0.00	0.10	0.00	25.80	2.00	0.00	0.00	0.10	0.00
25.90	2.00	0.00	0.00	0.10	0.00	26.00	2.00	0.00	0.00	0.10	0.00
26.10	2.00	0.00	0.00	0.10	0.00	26.20	2.00	0.00	0.00	0.10	0.00
26.30	1.35	0.00	0.00	0.10	0.00	26.40	1.28	0.00	0.00	0.10	0.00
26.50	1.22	0.00	0.00	0.10	0.00	26.60	1.21	0.00	0.00	0.10	0.00
26.70	1.06	0.00	0.00	0.10	0.00	26.80	1.06	0.00	0.00	0.10	0.00
26.90	1.16	0.00	0.00	0.10	0.00	27.00	1.11	0.00	0.00	0.10	0.00
27.10	1.01	0.00	0.00	0.10	0.00	27.20	0.87	0.00	0.00	0.10	0.02
27.30	0.72	0.00	0.00	0.10	0.05	27.40	0.59	0.00	0.00	0.10	0.07
27.50	0.47	0.00	0.00	0.10	0.09	27.60	0.35	0.65	0.35	0.10	0.12
27.70	0.27	0.73	0.31	0.10	0.13	27.80	0.23	0.77	0.29	0.10	0.14
27.90	0.20	0.80	0.28	0.10	0.14	28.00	0.20	0.80	0.28	0.10	0.14
28.10	0.21	0.79	0.28	0.10	0.14	28.20	0.24	0.76	0.29	0.10	0.13
28.30	0.28	0.72	0.31	0.10	0.12	28.40	0.32	0.68	0.33	0.10	0.12
28.50	0.37	0.00	0.00	0.10	0.11	28.60	0.44	0.00	0.00	0.10	0.10
28.70	0.59	0.00	0.00	0.10	0.07	28.80	0.86	0.00	0.00	0.10	0.02
28.90	1.23	0.00	0.00	0.10	0.00	29.00	1.67	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
29.10	2.00	0.00	0.00	0.10	0.00	29.20	2.00	0.00	0.00	0.10	0.00
29.30	1.97	0.00	0.00	0.10	0.00	29.40	1.86	0.00	0.00	0.10	0.00
29.50	1.76	0.00	0.00	0.10	0.00	29.60	1.47	0.00	0.00	0.10	0.00
29.70	1.08	0.00	0.00	0.10	0.00	29.80	1.45	0.00	0.00	0.10	0.00
29.90	2.00	0.00	0.00	0.10	0.00	30.00	1.14	0.00	0.00	0.10	0.00
30.10	1.36	0.00	0.00	0.10	0.00	30.20	1.14	0.00	0.00	0.10	0.00
30.30	0.63	0.00	0.00	0.10	0.06	30.40	0.51	0.00	0.00	0.10	0.08
30.50	0.34	0.66	0.35	0.10	0.11	30.60	0.27	0.73	0.31	0.10	0.12
30.70	0.33	0.67	0.34	0.10	0.11	30.80	0.59	0.00	0.00	0.10	0.07
30.90	1.25	0.00	0.00	0.10	0.00	31.00	1.57	0.00	0.00	0.10	0.00
31.10	1.36	0.00	0.00	0.10	0.00	31.20	1.45	0.00	0.00	0.10	0.00
31.30	1.64	0.00	0.00	0.10	0.00	31.40	1.65	0.00	0.00	0.10	0.00
31.50	1.41	0.00	0.00	0.10	0.00	31.60	0.99	0.00	0.00	0.10	0.00
31.70	0.66	0.00	0.00	0.10	0.05	31.80	0.47	0.00	0.00	0.10	0.08
31.90	0.38	0.00	0.00	0.10	0.10	32.00	2.00	0.00	0.00	0.10	0.00
32.10	2.00	0.00	0.00	0.10	0.00	32.20	2.00	0.00	0.00	0.10	0.00
32.30	2.00	0.00	0.00	0.10	0.00	32.40	2.00	0.00	0.00	0.10	0.00
32.50	2.00	0.00	0.00	0.10	0.00	32.60	2.00	0.00	0.00	0.10	0.00
32.70	2.00	0.00	0.00	0.10	0.00	32.80	2.00	0.00	0.00	0.10	0.00
32.90	2.00	0.00	0.00	0.10	0.00	33.00	2.00	0.00	0.00	0.10	0.00
33.10	0.22	0.78	0.28	0.10	0.12	33.20	0.25	0.75	0.30	0.10	0.11
33.30	0.32	0.68	0.34	0.10	0.10	33.40	0.43	0.00	0.00	0.10	0.09
33.50	0.45	0.00	0.00	0.10	0.08	33.60	0.38	0.00	0.00	0.10	0.09
33.70	0.32	0.68	0.33	0.10	0.10	33.80	0.25	0.75	0.30	0.10	0.11
33.90	0.20	0.80	0.28	0.10	0.12	34.00	2.00	0.00	0.00	0.10	0.00
34.10	2.00	0.00	0.00	0.10	0.00	34.20	2.00	0.00	0.00	0.10	0.00
34.30	2.00	0.00	0.00	0.10	0.00	34.40	2.00	0.00	0.00	0.10	0.00
34.50	2.00	0.00	0.00	0.10	0.00	34.60	2.00	0.00	0.00	0.10	0.00
34.70	2.00	0.00	0.00	0.10	0.00	34.80	2.00	0.00	0.00	0.10	0.00
34.90	2.00	0.00	0.00	0.10	0.00	35.00	2.00	0.00	0.00	0.10	0.00
35.10	2.00	0.00	0.00	0.10	0.00	35.20	2.00	0.00	0.00	0.10	0.00
35.30	2.00	0.00	0.00	0.10	0.00	35.40	2.00	0.00	0.00	0.10	0.00
35.50	2.00	0.00	0.00	0.10	0.00	35.60	2.00	0.00	0.00	0.10	0.00
35.70	2.00	0.00	0.00	0.10	0.00	35.80	2.00	0.00	0.00	0.10	0.00
35.90	2.00	0.00	0.00	0.10	0.00	36.00	2.00	0.00	0.00	0.10	0.00
36.10	2.00	0.00	0.00	0.10	0.00	36.20	2.00	0.00	0.00	0.10	0.00
36.30	2.00	0.00	0.00	0.10	0.00	36.40	2.00	0.00	0.00	0.10	0.00
36.50	2.00	0.00	0.00	0.10	0.00	36.60	2.00	0.00	0.00	0.10	0.00
36.70	2.00	0.00	0.00	0.10	0.00	36.80	2.00	0.00	0.00	0.10	0.00
36.90	2.00	0.00	0.00	0.10	0.00	37.00	2.00	0.00	0.00	0.10	0.00
37.10	2.00	0.00	0.00	0.10	0.00	37.20	2.00	0.00	0.00	0.10	0.00
37.30	2.00	0.00	0.00	0.10	0.00	37.40	2.00	0.00	0.00	0.10	0.00
37.50	2.00	0.00	0.00	0.10	0.00	37.60	2.00	0.00	0.00	0.10	0.00
37.70	0.20	0.80	0.28	0.10	0.10	37.80	0.20	0.80	0.28	0.10	0.10
37.90	0.20	0.80	0.28	0.10	0.10	38.00	0.20	0.80	0.28	0.10	0.10
38.10	0.19	0.81	0.28	0.10	0.10	38.20	0.19	0.81	0.27	0.10	0.10
38.30	0.19	0.81	0.27	0.10	0.10	38.40	0.19	0.81	0.27	0.10	0.10
38.50	0.18	0.82	0.27	0.10	0.10	38.60	0.18	0.82	0.27	0.10	0.10

:: Liquefaction Potential Index calculation data ::

Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
38.70	0.20	0.80	0.28	0.10	0.10	38.80	0.21	0.79	0.28	0.10	0.10
38.90	0.23	0.77	0.29	0.10	0.10	39.00	0.23	0.77	0.29	0.10	0.09
39.10	0.23	0.77	0.29	0.10	0.09	39.20	0.23	0.77	0.29	0.10	0.09
39.30	0.24	0.76	0.29	0.10	0.09	39.40	0.25	0.75	0.30	0.10	0.09
39.50	0.27	0.73	0.31	0.10	0.09	39.60	0.30	0.70	0.32	0.10	0.08
39.70	2.00	0.00	0.00	0.10	0.00	39.80	2.00	0.00	0.00	0.10	0.00
39.90	2.00	0.00	0.00	0.10	0.00	40.00	2.00	0.00	0.00	0.10	0.00
40.10	2.00	0.00	0.00	0.10	0.00	40.20	2.00	0.00	0.00	0.10	0.00
40.30	2.00	0.00	0.00	0.10	0.00	40.40	2.00	0.00	0.00	0.10	0.00
40.50	2.00	0.00	0.00	0.10	0.00	40.60	2.00	0.00	0.00	0.10	0.00
40.70	2.00	0.00	0.00	0.10	0.00	40.80	2.00	0.00	0.00	0.10	0.00
40.90	2.00	0.00	0.00	0.10	0.00	41.00	0.26	0.74	0.30	0.10	0.08
41.10	0.27	0.73	0.31	0.10	0.08	41.20	0.27	0.73	0.31	0.10	0.08
41.30	0.26	0.74	0.30	0.10	0.08	41.40	2.00	0.00	0.00	0.10	0.00
41.50	2.00	0.00	0.00	0.10	0.00	41.60	2.00	0.00	0.00	0.10	0.00
41.70	2.00	0.00	0.00	0.10	0.00	41.80	2.00	0.00	0.00	0.10	0.00
41.90	2.00	0.00	0.00	0.10	0.00	42.00	2.00	0.00	0.00	0.10	0.00
42.10	2.00	0.00	0.00	0.10	0.00	42.20	2.00	0.00	0.00	0.10	0.00
42.30	2.00	0.00	0.00	0.10	0.00	42.40	2.00	0.00	0.00	0.10	0.00
42.50	2.00	0.00	0.00	0.10	0.00	42.60	2.00	0.00	0.00	0.10	0.00
42.70	2.00	0.00	0.00	0.10	0.00	42.80	0.15	0.85	0.26	0.10	0.09
42.90	0.16	0.84	0.26	0.10	0.09	43.00	0.16	0.84	0.26	0.10	0.09
43.10	0.16	0.84	0.26	0.10	0.09	43.20	2.00	0.00	0.00	0.10	0.00
43.30	2.00	0.00	0.00	0.10	0.00	43.40	2.00	0.00	0.00	0.10	0.00
43.50	2.00	0.00	0.00	0.10	0.00	43.60	2.00	0.00	0.00	0.10	0.00
43.70	2.00	0.00	0.00	0.10	0.00	43.80	2.00	0.00	0.00	0.10	0.00
43.90	2.00	0.00	0.00	0.10	0.00	44.00	2.00	0.00	0.00	0.10	0.00
44.10	2.00	0.00	0.00	0.10	0.00	44.20	2.00	0.00	0.00	0.10	0.00
44.30	2.00	0.00	0.00	0.10	0.00	44.40	2.00	0.00	0.00	0.10	0.00
44.50	2.00	0.00	0.00	0.10	0.00	44.60	2.00	0.00	0.00	0.10	0.00
44.70	0.93	0.00	0.00	0.10	0.01	44.80	1.28	0.00	0.00	0.10	0.00
44.90	2.00	0.00	0.00	0.10	0.00	45.00	2.00	0.00	0.00	0.10	0.00
45.10	2.00	0.00	0.00	0.10	0.00	45.20	2.00	0.00	0.00	0.10	0.00
45.30	2.00	0.00	0.00	0.10	0.00	45.40	2.00	0.00	0.00	0.10	0.00
45.50	2.00	0.00	0.00	0.10	0.00	45.60	2.00	0.00	0.00	0.10	0.00
45.70	2.00	0.00	0.00	0.10	0.00	45.80	2.00	0.00	0.00	0.10	0.00
45.90	2.00	0.00	0.00	0.10	0.00	46.00	2.00	0.00	0.00	0.10	0.00
46.10	2.00	0.00	0.00	0.10	0.00	46.20	2.00	0.00	0.00	0.10	0.00
46.30	2.00	0.00	0.00	0.10	0.00	46.40	2.00	0.00	0.00	0.10	0.00
46.50	2.00	0.00	0.00	0.10	0.00	46.60	2.00	0.00	0.00	0.10	0.00
46.70	2.00	0.00	0.00	0.10	0.00	46.80	2.00	0.00	0.00	0.10	0.00
46.90	2.00	0.00	0.00	0.10	0.00	47.00	1.83	0.00	0.00	0.10	0.00
47.10	1.29	0.00	0.00	0.10	0.00	47.20	1.02	0.00	0.00	0.10	0.00
47.30	0.92	0.00	0.00	0.10	0.01	47.40	0.92	0.00	0.00	0.10	0.01
47.50	0.90	0.00	0.00	0.10	0.01	47.60	0.88	0.00	0.00	0.10	0.01
47.70	0.89	0.00	0.00	0.10	0.01	47.80	0.88	0.00	0.00	0.10	0.01
47.90	0.87	0.00	0.00	0.10	0.01	48.00	0.92	0.00	0.00	0.10	0.01
48.10	1.10	0.00	0.00	0.10	0.00	48.20	1.36	0.00	0.00	0.10	0.00

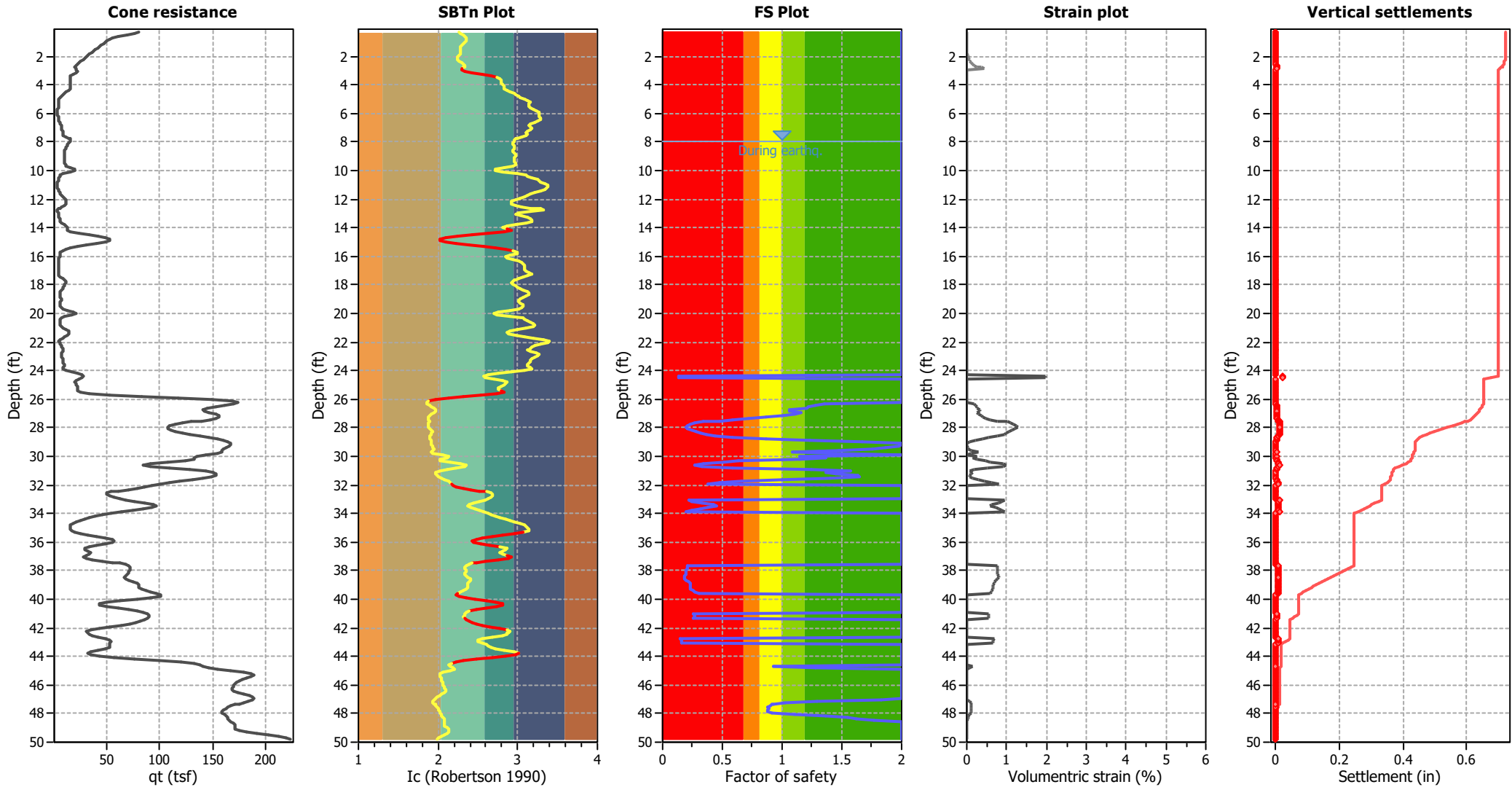
:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
48.30	1.55	0.00	0.00	0.10	0.00	48.40	1.62	0.00	0.00	0.10	0.00
48.50	1.77	0.00	0.00	0.10	0.00	48.60	2.00	0.00	0.00	0.10	0.00
48.70	2.00	0.00	0.00	0.10	0.00	48.80	2.00	0.00	0.00	0.10	0.00
48.90	2.00	0.00	0.00	0.10	0.00	49.00	2.00	0.00	0.00	0.10	0.00
49.10	2.00	0.00	0.00	0.10	0.00	49.20	2.00	0.00	0.00	0.10	0.00
49.30	2.00	0.00	0.00	0.10	0.00	49.40	2.00	0.00	0.00	0.10	0.00
49.50	2.00	0.00	0.00	0.10	0.00	49.60	2.00	0.00	0.00	0.10	0.00
49.70	2.00	0.00	0.00	0.10	0.00	49.80	2.00	0.00	0.00	0.10	0.00
Overall liquefaction potential: 6.47											

LPI_{ISH} > 5.0 - Liquefaction manifestation is expected

Abbreviations

FS: Calculated factor of safety for test point
d_z: Layer thickness (ft)
LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

- q_c: Total cone resistance (cone resistance q_c corrected for pore water effects)
- I_c: Soil Behaviour Type Index
- FS: Calculated Factor of Safety against liquefaction
- Volumetric strain: Post-liquefaction volumetric strain

:: Post-earthquake settlement of dry sands ::												
Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
0.30	2.27	129.37	1.80	233.07	54	1276	0.53	0.001	0.00	13.69	0.00	0.000
0.40	2.28	122.26	1.86	227.12	53	1231	0.53	0.001	0.00	13.69	0.00	0.000
0.50	2.31	110.66	1.97	217.50	51	1156	0.53	0.001	0.00	13.69	0.00	0.000
0.60	2.34	98.07	2.10	206.36	50	1069	0.54	0.002	0.00	13.69	0.00	0.000
0.70	2.36	89.33	2.19	195.35	47	997	0.55	0.003	0.00	13.69	0.00	0.000
0.80	2.36	84.04	2.19	183.98	45	938	0.55	0.003	0.00	13.69	0.00	0.000
0.90	2.35	80.71	2.14	172.62	42	888	0.55	0.004	0.00	13.69	0.00	0.000
1.00	2.34	77.81	2.07	160.79	38	839	0.55	0.005	0.00	13.69	0.00	0.000
1.10	2.32	74.95	1.99	148.79	35	788	0.55	0.006	0.00	13.69	0.00	0.000
1.20	2.29	72.37	1.90	137.52	32	740	0.55	0.007	0.00	13.69	0.00	0.000
1.30	2.28	69.60	1.84	128.17	30	697	0.55	0.008	0.01	13.69	0.00	0.000
1.40	2.27	66.73	1.83	121.85	28	664	0.55	0.010	0.01	13.69	0.01	0.000
1.50	2.28	63.55	1.84	117.19	27	637	0.56	0.012	0.01	13.69	0.01	0.000
1.60	2.28	60.27	1.87	112.45	26	609	0.56	0.014	0.01	13.69	0.01	0.000
1.70	2.28	57.08	1.87	106.51	25	577	0.56	0.017	0.01	13.69	0.01	0.000
1.80	2.28	54.36	1.84	100.24	23	545	0.56	0.021	0.02	13.69	0.02	0.000
1.90	2.27	52.14	1.80	93.92	22	514	0.56	0.027	0.02	13.69	0.02	0.000
2.00	2.25	49.92	1.75	87.50	20	483	0.56	0.035	0.03	13.69	0.03	0.000
2.10	2.24	47.52	1.72	81.70	19	453	0.56	0.046	0.05	13.69	0.05	0.001
2.20	2.24	44.62	1.73	77.04	18	427	0.56	0.061	0.07	13.69	0.07	0.001
2.30	2.26	41.42	1.79	74.14	17	407	0.56	0.080	0.10	13.69	0.09	0.001
2.40	2.29	38.25	1.90	72.61	17	391	0.56	0.103	0.12	13.69	0.11	0.001
2.50	2.32	35.41	2.02	71.45	17	376	0.56	0.132	0.16	13.69	0.15	0.002
2.60	2.34	33.39	2.09	69.81	17	363	0.56	0.171	0.21	13.69	0.19	0.002
2.70	2.34	32.05	2.09	66.93	16	348	0.56	0.228	0.30	13.69	0.27	0.003
2.80	2.32	31.82	2.00	63.60	15	336	0.56	0.297	0.42	13.69	0.38	0.005
2.90	2.29	32.83	1.89	62.07	15	335	0.56	0.331	0.49	13.69	0.44	0.005
3.00	2.29	34.54	1.89	65.20	0	0	0.56	0.000	0.00	13.69	0.00	0.000
3.10	2.34	35.22	2.09	73.61	0	0	0.56	0.000	0.00	13.69	0.00	0.000
3.20	2.44	33.06	2.57	84.95	0	0	0.56	0.000	0.00	13.69	0.00	0.000
3.30	2.55	29.36	3.37	98.89	0	0	0.56	0.000	0.00	13.69	0.00	0.000
3.40	2.66	25.85	4.34	112.08	0	0	0.56	0.000	0.00	0.00	0.00	0.000
3.50	2.73	24.47	5.04	123.42	0	0	0.56	0.000	0.00	0.00	0.00	0.000
3.60	2.77	23.99	5.52	132.32	0	0	0.56	0.000	0.00	0.00	0.00	0.000
3.70	2.79	24.18	5.75	139.12	0	0	0.56	0.000	0.00	0.00	0.00	0.000
3.80	2.80	24.89	5.79	144.16	0	0	0.56	0.000	0.00	0.00	0.00	0.000
3.90	2.80	25.38	5.79	146.99	0	0	0.56	0.000	0.00	0.00	0.00	0.000
4.00	2.80	25.17	5.91	148.80	0	0	0.56	0.000	0.00	0.00	0.00	0.000
4.10	2.82	24.48	6.13	149.92	0	0	0.56	0.000	0.00	0.00	0.00	0.000
4.20	2.83	24.19	6.22	150.52	0	0	0.56	0.000	0.00	0.00	0.00	0.000
4.30	2.83	23.75	6.29	149.40	0	0	0.56	0.000	0.00	0.00	0.00	0.000
4.40	2.86	22.01	6.61	145.58	0	0	0.56	0.000	0.00	0.00	0.00	0.000
4.50	2.91	18.98	7.30	138.63	0	0	0.56	0.000	0.00	0.00	0.00	0.000
4.60	2.96	16.01	8.05	128.85	0	0	0.56	0.000	0.00	0.00	0.00	0.000
4.70	2.98	13.83	8.50	117.49	0	0	0.56	0.000	0.00	0.00	0.00	0.000
4.80	3.01	11.85	8.90	105.39	0	0	0.56	0.000	0.00	0.00	0.00	0.000
4.90	3.04	9.95	9.45	94.05	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.00	3.09	8.04	10.41	83.71	0	0	0.56	0.000	0.00	0.00	0.00	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	I _c	Q _{tn}	K _c	Q _{tn,cs}	N _{1,60} (blows)	G _{max} (tsf)	CSR	Shear, γ (%)	e _{vol(15)} (%)	N _c	e _v (%)	Settle. (in)
5.10	3.13	6.83	11.20	76.47	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.20	3.15	6.12	11.64	71.20	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.30	3.14	5.91	11.52	68.13	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.40	3.13	5.91	11.27	66.56	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.50	3.13	5.90	11.27	66.47	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.60	3.15	5.84	11.66	68.11	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.70	3.19	5.66	12.50	70.68	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.80	3.23	5.44	13.51	73.44	0	0	0.56	0.000	0.00	0.00	0.00	0.000
5.90	3.26	5.37	14.24	76.47	0	0	0.56	0.000	0.00	0.00	0.00	0.000
6.00	3.27	5.54	14.43	79.91	0	0	0.56	0.000	0.00	0.00	0.00	0.000
6.10	3.27	5.74	14.42	82.82	0	0	0.56	0.000	0.00	0.00	0.00	0.000
6.20	3.28	5.85	14.54	84.98	0	0	0.57	0.000	0.00	0.00	0.00	0.000
6.30	3.29	5.84	14.87	86.77	0	0	0.57	0.000	0.00	0.00	0.00	0.000
6.40	3.28	6.16	14.79	91.06	0	0	0.57	0.000	0.00	0.00	0.00	0.000
6.50	3.26	6.97	14.09	98.24	0	0	0.57	0.000	0.00	0.00	0.00	0.000
6.60	3.21	8.26	12.96	107.05	0	0	0.57	0.000	0.00	0.00	0.00	0.000
6.70	3.17	9.63	11.99	115.42	0	0	0.57	0.000	0.00	0.00	0.00	0.000
6.80	3.15	10.51	11.58	121.71	0	0	0.56	0.000	0.00	0.00	0.00	0.000
6.90	3.15	10.74	11.73	126.00	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.00	3.17	10.72	12.05	129.12	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.10	3.15	11.47	11.64	133.44	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.20	3.11	12.48	10.90	136.06	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.30	3.10	12.86	10.57	136.00	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.40	3.12	12.34	10.92	134.75	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.50	3.11	13.37	10.78	144.15	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.60	3.05	16.98	9.74	165.33	0	0	0.57	0.000	0.00	0.00	0.00	0.000
7.70	3.00	21.21	8.74	185.31	0	0	0.56	0.000	0.00	0.00	0.00	0.000
7.80	2.97	23.79	8.23	195.81	0	0	0.56	0.000	0.00	0.00	0.00	0.000
7.90	2.96	24.25	8.07	195.78	0	0	0.56	0.000	0.00	0.00	0.00	0.000

Total estimated settlement: 0.02**Abbreviations**

Q_{tn}: Normalized cone resistance
 K_c: Fines correction factor
 Q_{tn,cs}: Equivalent clean sand normalized cone resistance
 G_{max}: Small strain shear modulus
 CSR: Soil cyclic stress ratio
 γ: Cyclic shear strain
 e_{vol(15)}: Volumetric strain after 15 cycles
 N_c: Equivalent number of cycles
 e_v: Volumetric strain
 Settle.: Calculated settlement

:: Post-earthquake settlement due to soil liquefaction ::

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
8.00	23.27	2.00	0.00	0.85	0.00	8.10	22.04	2.00	0.00	0.85	0.00
8.20	20.32	2.00	0.00	0.85	0.00	8.30	18.76	2.00	0.00	0.85	0.00
8.40	16.69	2.00	0.00	0.85	0.00	8.50	16.23	2.00	0.00	0.85	0.00
8.60	16.19	2.00	0.00	0.84	0.00	8.70	16.00	2.00	0.00	0.84	0.00
8.80	14.95	2.00	0.00	0.84	0.00	8.90	14.34	2.00	0.00	0.84	0.00
9.00	14.90	2.00	0.00	0.84	0.00	9.10	15.85	2.00	0.00	0.83	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
9.20	15.93	2.00	0.00	0.83	0.00	9.30	15.88	2.00	0.00	0.83	0.00
9.40	15.84	2.00	0.00	0.83	0.00	9.50	15.79	2.00	0.00	0.83	0.00
9.60	15.75	2.00	0.00	0.83	0.00	9.70	17.07	2.00	0.00	0.82	0.00
9.80	19.71	2.00	0.00	0.82	0.00	9.90	30.01	2.00	0.00	0.82	0.00
10.00	35.22	2.00	0.00	0.82	0.00	10.10	19.53	2.00	0.00	0.82	0.00
10.20	9.70	2.00	0.00	0.81	0.00	10.30	10.17	2.00	0.00	0.81	0.00
10.40	9.40	2.00	0.00	0.81	0.00	10.50	6.97	2.00	0.00	0.81	0.00
10.60	5.84	2.00	0.00	0.81	0.00	10.70	5.83	2.00	0.00	0.81	0.00
10.80	5.67	2.00	0.00	0.80	0.00	10.90	5.32	2.00	0.00	0.80	0.00
11.00	5.22	2.00	0.00	0.80	0.00	11.10	5.21	2.00	0.00	0.80	0.00
11.20	5.52	2.00	0.00	0.80	0.00	11.30	5.76	2.00	0.00	0.79	0.00
11.40	6.25	2.00	0.00	0.79	0.00	11.50	8.26	2.00	0.00	0.79	0.00
11.60	9.95	2.00	0.00	0.79	0.00	11.70	10.14	2.00	0.00	0.79	0.00
11.80	11.49	2.00	0.00	0.79	0.00	11.90	14.24	2.00	0.00	0.78	0.00
12.00	16.40	2.00	0.00	0.78	0.00	12.10	16.63	2.00	0.00	0.78	0.00
12.20	16.71	2.00	0.00	0.78	0.00	12.30	16.06	2.00	0.00	0.78	0.00
12.40	13.52	2.00	0.00	0.77	0.00	12.50	10.79	2.00	0.00	0.77	0.00
12.60	8.06	2.00	0.00	0.77	0.00	12.70	5.28	2.00	0.00	0.77	0.00
12.80	3.61	2.00	0.00	0.77	0.00	12.90	4.75	2.00	0.00	0.77	0.00
13.00	6.59	2.00	0.00	0.76	0.00	13.10	6.61	2.00	0.00	0.76	0.00
13.20	6.60	2.00	0.00	0.76	0.00	13.30	6.94	2.00	0.00	0.76	0.00
13.40	7.88	2.00	0.00	0.76	0.00	13.50	8.16	2.00	0.00	0.75	0.00
13.60	8.14	2.00	0.00	0.75	0.00	13.70	9.84	2.00	0.00	0.75	0.00
13.80	12.82	2.00	0.00	0.75	0.00	13.90	17.05	2.00	0.00	0.75	0.00
14.00	18.50	2.00	0.00	0.75	0.00	14.10	16.43	2.00	0.00	0.74	0.00
14.20	14.41	2.00	0.00	0.74	0.00	14.30	18.94	2.00	0.00	0.74	0.00
14.40	29.93	2.00	0.00	0.74	0.00	14.50	101.34	2.00	0.00	0.74	0.00
14.60	108.89	2.00	0.00	0.73	0.00	14.70	109.71	2.00	0.00	0.73	0.00
14.80	109.14	2.00	0.00	0.73	0.00	14.90	110.48	2.00	0.00	0.73	0.00
15.00	111.13	2.00	0.00	0.73	0.00	15.10	106.90	2.00	0.00	0.73	0.00
15.20	94.83	2.00	0.00	0.72	0.00	15.30	84.38	2.00	0.00	0.72	0.00
15.40	18.85	2.00	0.00	0.72	0.00	15.50	14.06	2.00	0.00	0.72	0.00
15.60	9.92	2.00	0.00	0.72	0.00	15.70	7.59	2.00	0.00	0.71	0.00
15.80	6.69	2.00	0.00	0.71	0.00	15.90	6.62	2.00	0.00	0.71	0.00
16.00	7.51	2.00	0.00	0.71	0.00	16.10	6.58	2.00	0.00	0.71	0.00
16.20	5.15	2.00	0.00	0.71	0.00	16.30	5.15	2.00	0.00	0.70	0.00
16.40	5.14	2.00	0.00	0.70	0.00	16.50	5.13	2.00	0.00	0.70	0.00
16.60	5.13	2.00	0.00	0.70	0.00	16.70	5.12	2.00	0.00	0.70	0.00
16.80	5.11	2.00	0.00	0.69	0.00	16.90	5.11	2.00	0.00	0.69	0.00
17.00	5.10	2.00	0.00	0.69	0.00	17.10	5.09	2.00	0.00	0.69	0.00
17.20	4.93	2.00	0.00	0.69	0.00	17.30	5.61	2.00	0.00	0.69	0.00
17.40	8.60	2.00	0.00	0.68	0.00	17.50	10.57	2.00	0.00	0.68	0.00
17.60	12.22	2.00	0.00	0.68	0.00	17.70	13.64	2.00	0.00	0.68	0.00
17.80	14.48	2.00	0.00	0.68	0.00	17.90	14.26	2.00	0.00	0.67	0.00
18.00	12.75	2.00	0.00	0.67	0.00	18.10	11.83	2.00	0.00	0.67	0.00
18.20	10.99	2.00	0.00	0.67	0.00	18.30	10.13	2.00	0.00	0.67	0.00
18.40	8.91	2.00	0.00	0.67	0.00	18.50	7.65	2.00	0.00	0.66	0.00
18.60	7.39	2.00	0.00	0.66	0.00	18.70	7.38	2.00	0.00	0.66	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
18.80	7.42	2.00	0.00	0.66	0.00	18.90	8.24	2.00	0.00	0.66	0.00
19.00	8.78	2.00	0.00	0.65	0.00	19.10	8.77	2.00	0.00	0.65	0.00
19.20	8.20	2.00	0.00	0.65	0.00	19.30	7.36	2.00	0.00	0.65	0.00
19.40	7.29	2.00	0.00	0.65	0.00	19.50	7.53	2.00	0.00	0.65	0.00
19.60	9.44	2.00	0.00	0.64	0.00	19.70	11.57	2.00	0.00	0.64	0.00
19.80	12.71	2.00	0.00	0.64	0.00	19.90	21.42	2.00	0.00	0.64	0.00
20.00	32.06	2.00	0.00	0.64	0.00	20.10	19.80	2.00	0.00	0.63	0.00
20.20	9.61	2.00	0.00	0.63	0.00	20.30	7.92	2.00	0.00	0.63	0.00
20.40	7.61	2.00	0.00	0.63	0.00	20.50	7.85	2.00	0.00	0.63	0.00
20.60	7.16	2.00	0.00	0.63	0.00	20.70	7.12	2.00	0.00	0.62	0.00
20.80	7.11	2.00	0.00	0.62	0.00	20.90	7.66	2.00	0.00	0.62	0.00
21.00	10.11	2.00	0.00	0.62	0.00	21.10	13.87	2.00	0.00	0.62	0.00
21.20	17.16	2.00	0.00	0.61	0.00	21.30	17.99	2.00	0.00	0.61	0.00
21.40	16.41	2.00	0.00	0.61	0.00	21.50	14.78	2.00	0.00	0.61	0.00
21.60	12.08	2.00	0.00	0.61	0.00	21.70	8.97	2.00	0.00	0.61	0.00
21.80	7.15	2.00	0.00	0.60	0.00	21.90	5.59	2.00	0.00	0.60	0.00
22.00	5.73	2.00	0.00	0.60	0.00	22.10	7.32	2.00	0.00	0.60	0.00
22.20	8.29	2.00	0.00	0.60	0.00	22.30	8.86	2.00	0.00	0.59	0.00
22.40	9.17	2.00	0.00	0.59	0.00	22.50	10.02	2.00	0.00	0.59	0.00
22.60	11.78	2.00	0.00	0.59	0.00	22.70	10.38	2.00	0.00	0.59	0.00
22.80	8.08	2.00	0.00	0.59	0.00	22.90	7.91	2.00	0.00	0.58	0.00
23.00	7.67	2.00	0.00	0.58	0.00	23.10	8.31	2.00	0.00	0.58	0.00
23.20	9.94	2.00	0.00	0.58	0.00	23.30	9.92	2.00	0.00	0.58	0.00
23.40	9.90	2.00	0.00	0.57	0.00	23.50	9.89	2.00	0.00	0.57	0.00
23.60	10.49	2.00	0.00	0.57	0.00	23.70	11.50	2.00	0.00	0.57	0.00
23.80	10.51	2.00	0.00	0.57	0.00	23.90	9.50	2.00	0.00	0.57	0.00
24.00	11.58	2.00	0.00	0.56	0.00	24.10	17.53	2.00	0.00	0.56	0.00
24.20	25.16	2.00	0.00	0.56	0.00	24.30	30.23	2.00	0.00	0.56	0.00
24.40	90.65	0.14	1.97	0.56	0.02	24.50	90.11	0.14	1.98	0.55	0.02
24.60	25.72	2.00	0.00	0.55	0.00	24.70	20.27	2.00	0.00	0.55	0.00
24.80	20.91	2.00	0.00	0.55	0.00	24.90	23.51	2.00	0.00	0.55	0.00
25.00	23.38	2.00	0.00	0.55	0.00	25.10	22.70	2.00	0.00	0.54	0.00
25.20	25.43	2.00	0.00	0.54	0.00	25.30	26.18	2.00	0.00	0.54	0.00
25.40	23.14	2.00	0.00	0.54	0.00	25.50	24.02	2.00	0.00	0.54	0.00
25.60	32.44	2.00	0.00	0.53	0.00	25.70	115.23	2.00	0.00	0.53	0.00
25.80	151.06	2.00	0.00	0.53	0.00	25.90	186.66	2.00	0.00	0.53	0.00
26.00	203.71	2.00	0.00	0.53	0.00	26.10	200.57	2.00	0.00	0.53	0.00
26.20	193.74	2.00	0.00	0.52	0.00	26.30	190.44	1.35	0.18	0.52	0.00
26.40	189.40	1.28	0.21	0.52	0.00	26.50	188.44	1.22	0.24	0.52	0.00
26.60	188.25	1.21	0.24	0.52	0.00	26.70	185.46	1.06	0.32	0.51	0.00
26.80	185.38	1.06	0.33	0.51	0.00	26.90	187.31	1.16	0.27	0.51	0.00
27.00	186.47	1.11	0.29	0.51	0.00	27.10	184.30	1.01	0.36	0.51	0.00
27.20	180.83	0.87	0.42	0.51	0.01	27.30	176.33	0.72	0.49	0.50	0.01
27.40	170.62	0.59	0.60	0.50	0.01	27.50	163.92	0.47	0.75	0.50	0.01
27.60	153.07	0.35	1.01	0.50	0.01	27.70	142.61	0.27	1.09	0.50	0.01
27.80	133.03	0.23	1.17	0.49	0.01	27.90	125.34	0.20	1.25	0.49	0.01
28.00	123.56	0.20	1.26	0.49	0.02	28.10	127.91	0.21	1.21	0.49	0.01
28.20	136.40	0.24	1.13	0.49	0.01	28.30	144.72	0.28	1.05	0.49	0.01

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
28.40	149.88	0.32	1.00	0.48	0.01	28.50	155.98	0.37	0.95	0.48	0.01
28.60	162.11	0.44	0.77	0.48	0.01	28.70	171.00	0.59	0.56	0.48	0.01
28.80	181.10	0.86	0.39	0.48	0.00	28.90	189.03	1.23	0.21	0.47	0.00
29.00	195.15	1.67	0.07	0.47	0.00	29.10	198.53	2.00	0.00	0.47	0.00
29.20	199.23	2.00	0.00	0.47	0.00	29.30	198.34	1.97	0.00	0.47	0.00
29.40	197.33	1.86	0.03	0.47	0.00	29.50	196.25	1.76	0.05	0.46	0.00
29.60	192.82	1.47	0.12	0.46	0.00	29.70	186.41	1.08	0.28	0.46	0.00
29.80	192.55	1.45	0.13	0.46	0.00	29.90	201.83	2.00	0.00	0.46	0.00
30.00	187.65	1.14	0.24	0.45	0.00	30.10	191.37	1.36	0.15	0.45	0.00
30.20	187.68	1.14	0.24	0.45	0.00	30.30	173.38	0.63	0.49	0.45	0.01
30.40	167.43	0.51	0.60	0.45	0.01	30.50	153.10	0.34	0.90	0.45	0.01
30.60	142.84	0.27	0.97	0.44	0.01	30.70	151.40	0.33	0.91	0.44	0.01
30.80	171.44	0.59	0.51	0.44	0.01	30.90	189.63	1.25	0.19	0.44	0.00
31.00	194.34	1.57	0.09	0.44	0.00	31.10	191.45	1.36	0.15	0.43	0.00
31.20	192.82	1.45	0.12	0.43	0.00	31.30	195.17	1.64	0.07	0.43	0.00
31.40	195.33	1.65	0.07	0.43	0.00	31.50	192.19	1.41	0.13	0.43	0.00
31.60	184.78	0.99	0.31	0.43	0.00	31.70	174.68	0.66	0.44	0.42	0.01
31.80	165.00	0.47	0.61	0.42	0.01	31.90	157.38	0.38	0.79	0.42	0.01
32.00	150.03	2.00	0.00	0.42	0.00	32.10	144.04	2.00	0.00	0.42	0.00
32.20	139.94	2.00	0.00	0.41	0.00	32.30	132.46	2.00	0.00	0.41	0.00
32.40	122.51	2.00	0.00	0.41	0.00	32.50	49.30	2.00	0.00	0.41	0.00
32.60	46.31	2.00	0.00	0.41	0.00	32.70	46.04	2.00	0.00	0.41	0.00
32.80	47.66	2.00	0.00	0.40	0.00	32.90	53.29	2.00	0.00	0.40	0.00
33.00	58.93	2.00	0.00	0.40	0.00	33.10	131.36	0.22	0.96	0.40	0.01
33.20	139.30	0.25	0.89	0.40	0.01	33.30	151.49	0.32	0.81	0.39	0.01
33.40	161.84	0.43	0.64	0.39	0.01	33.50	163.48	0.45	0.60	0.39	0.01
33.60	158.04	0.38	0.72	0.39	0.01	33.70	150.52	0.32	0.80	0.39	0.01
33.80	139.24	0.25	0.87	0.39	0.01	33.90	126.23	0.20	0.96	0.38	0.01
34.00	49.36	2.00	0.00	0.38	0.00	34.10	41.58	2.00	0.00	0.38	0.00
34.20	36.36	2.00	0.00	0.38	0.00	34.30	31.09	2.00	0.00	0.38	0.00
34.40	26.25	2.00	0.00	0.37	0.00	34.50	23.18	2.00	0.00	0.37	0.00
34.60	19.06	2.00	0.00	0.37	0.00	34.70	15.11	2.00	0.00	0.37	0.00
34.80	14.25	2.00	0.00	0.37	0.00	34.90	13.71	2.00	0.00	0.37	0.00
35.00	13.69	2.00	0.00	0.36	0.00	35.10	14.04	2.00	0.00	0.36	0.00
35.20	14.59	2.00	0.00	0.36	0.00	35.30	16.67	2.00	0.00	0.36	0.00
35.40	22.63	2.00	0.00	0.36	0.00	35.50	28.61	2.00	0.00	0.35	0.00
35.60	36.24	2.00	0.00	0.35	0.00	35.70	108.56	2.00	0.00	0.35	0.00
35.80	114.11	2.00	0.00	0.35	0.00	35.90	116.87	2.00	0.00	0.35	0.00
36.00	113.37	2.00	0.00	0.35	0.00	36.10	106.68	2.00	0.00	0.34	0.00
36.20	36.54	2.00	0.00	0.34	0.00	36.30	28.58	2.00	0.00	0.34	0.00
36.40	24.29	2.00	0.00	0.34	0.00	36.50	25.49	2.00	0.00	0.34	0.00
36.60	28.98	2.00	0.00	0.33	0.00	36.70	31.62	2.00	0.00	0.33	0.00
36.80	31.39	2.00	0.00	0.33	0.00	36.90	27.79	2.00	0.00	0.33	0.00
37.00	23.81	2.00	0.00	0.33	0.00	37.10	24.18	2.00	0.00	0.33	0.00
37.20	31.67	2.00	0.00	0.32	0.00	37.30	41.21	2.00	0.00	0.32	0.00
37.40	113.02	2.00	0.00	0.32	0.00	37.50	120.10	2.00	0.00	0.32	0.00
37.60	124.40	2.00	0.00	0.32	0.00	37.70	127.48	0.20	0.78	0.31	0.01
37.80	127.65	0.20	0.78	0.31	0.01	37.90	127.40	0.20	0.77	0.31	0.01

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
38.00	126.57	0.20	0.77	0.31	0.01	38.10	125.22	0.19	0.78	0.31	0.01
38.20	124.39	0.19	0.78	0.31	0.01	38.30	123.51	0.19	0.78	0.30	0.01
38.40	121.95	0.19	0.79	0.30	0.01	38.50	120.19	0.18	0.80	0.30	0.01
38.60	121.12	0.18	0.78	0.30	0.01	38.70	125.97	0.20	0.75	0.30	0.01
38.80	131.50	0.21	0.71	0.29	0.01	38.90	135.01	0.23	0.68	0.29	0.01
39.00	136.03	0.23	0.67	0.29	0.01	39.10	136.02	0.23	0.67	0.29	0.01
39.20	135.38	0.23	0.67	0.29	0.01	39.30	137.20	0.24	0.65	0.29	0.01
39.40	140.60	0.25	0.63	0.28	0.01	39.50	144.53	0.27	0.61	0.28	0.01
39.60	148.80	0.30	0.59	0.28	0.01	39.70	152.89	2.00	0.00	0.28	0.00
39.80	157.24	2.00	0.00	0.28	0.00	39.90	151.11	2.00	0.00	0.27	0.00
40.00	133.85	2.00	0.00	0.27	0.00	40.10	54.72	2.00	0.00	0.27	0.00
40.20	41.17	2.00	0.00	0.27	0.00	40.30	33.61	2.00	0.00	0.27	0.00
40.40	34.53	2.00	0.00	0.27	0.00	40.50	41.74	2.00	0.00	0.26	0.00
40.60	51.76	2.00	0.00	0.26	0.00	40.70	128.47	2.00	0.00	0.26	0.00
40.80	135.09	2.00	0.00	0.26	0.00	40.90	138.89	2.00	0.00	0.26	0.00
41.00	142.31	0.26	0.56	0.25	0.01	41.10	143.49	0.27	0.55	0.25	0.01
41.20	143.46	0.27	0.55	0.25	0.01	41.30	142.34	0.26	0.55	0.25	0.01
41.40	139.51	2.00	0.00	0.25	0.00	41.50	135.27	2.00	0.00	0.25	0.00
41.60	131.64	2.00	0.00	0.24	0.00	41.70	127.88	2.00	0.00	0.24	0.00
41.80	120.33	2.00	0.00	0.24	0.00	41.90	44.68	2.00	0.00	0.24	0.00
42.00	34.94	2.00	0.00	0.24	0.00	42.10	26.71	2.00	0.00	0.23	0.00
42.20	24.17	2.00	0.00	0.23	0.00	42.30	26.25	2.00	0.00	0.23	0.00
42.40	27.47	2.00	0.00	0.23	0.00	42.50	26.84	2.00	0.00	0.23	0.00
42.60	28.05	2.00	0.00	0.23	0.00	42.70	33.73	2.00	0.00	0.22	0.00
42.80	102.61	0.15	0.69	0.22	0.01	42.90	107.27	0.16	0.66	0.22	0.01
43.00	108.25	0.16	0.65	0.22	0.01	43.10	106.86	0.16	0.65	0.22	0.01
43.20	42.66	2.00	0.00	0.21	0.00	43.30	43.13	2.00	0.00	0.21	0.00
43.40	44.27	2.00	0.00	0.21	0.00	43.50	41.76	2.00	0.00	0.21	0.00
43.60	33.70	2.00	0.00	0.21	0.00	43.70	26.15	2.00	0.00	0.21	0.00
43.80	24.16	2.00	0.00	0.20	0.00	43.90	26.95	2.00	0.00	0.20	0.00
44.00	33.06	2.00	0.00	0.20	0.00	44.10	43.75	2.00	0.00	0.20	0.00
44.20	128.45	2.00	0.00	0.20	0.00	44.30	151.87	2.00	0.00	0.19	0.00
44.40	170.94	2.00	0.00	0.19	0.00	44.50	180.84	2.00	0.00	0.19	0.00
44.60	182.00	2.00	0.00	0.19	0.00	44.70	184.42	0.93	0.14	0.19	0.00
44.80	191.41	1.28	0.08	0.19	0.00	44.90	203.21	2.00	0.00	0.18	0.00
45.00	213.73	2.00	0.00	0.18	0.00	45.10	217.81	2.00	0.00	0.18	0.00
45.20	220.06	2.00	0.00	0.18	0.00	45.30	219.33	2.00	0.00	0.18	0.00
45.40	216.35	2.00	0.00	0.17	0.00	45.50	213.04	2.00	0.00	0.17	0.00
45.60	210.01	2.00	0.00	0.17	0.00	45.70	207.54	2.00	0.00	0.17	0.00
45.80	205.12	2.00	0.00	0.17	0.00	45.90	205.03	2.00	0.00	0.17	0.00
46.00	204.63	2.00	0.00	0.16	0.00	46.10	204.49	2.00	0.00	0.16	0.00
46.20	205.75	2.00	0.00	0.16	0.00	46.30	206.03	2.00	0.00	0.16	0.00
46.40	206.95	2.00	0.00	0.16	0.00	46.50	209.87	2.00	0.00	0.15	0.00
46.60	211.56	2.00	0.00	0.15	0.00	46.70	212.53	2.00	0.00	0.15	0.00
46.80	211.34	2.00	0.00	0.15	0.00	46.90	206.06	2.00	0.00	0.15	0.00
47.00	198.55	1.83	0.01	0.15	0.00	47.10	191.72	1.29	0.06	0.14	0.00
47.20	186.56	1.02	0.10	0.14	0.00	47.30	184.21	0.92	0.10	0.14	0.00
47.40	184.06	0.92	0.10	0.14	0.00	47.50	183.58	0.90	0.10	0.14	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (in)
47.60	183.20	0.88	0.10	0.13	0.00	47.70	183.41	0.89	0.10	0.13	0.00
47.80	183.24	0.88	0.10	0.13	0.00	47.90	182.94	0.87	0.10	0.13	0.00
48.00	184.18	0.92	0.09	0.13	0.00	48.10	188.32	1.10	0.07	0.13	0.00
48.20	192.83	1.36	0.04	0.12	0.00	48.30	195.40	1.55	0.03	0.12	0.00
48.40	196.25	1.62	0.02	0.12	0.00	48.50	197.96	1.77	0.01	0.12	0.00
48.60	200.45	2.00	0.00	0.12	0.00	48.70	202.69	2.00	0.00	0.11	0.00
48.80	204.67	2.00	0.00	0.11	0.00	48.90	206.40	2.00	0.00	0.11	0.00
49.00	208.33	2.00	0.00	0.11	0.00	49.10	210.74	2.00	0.00	0.11	0.00
49.20	213.84	2.00	0.00	0.11	0.00	49.30	221.41	2.00	0.00	0.10	0.00
49.40	230.48	2.00	0.00	0.10	0.00	49.50	238.27	2.00	0.00	0.10	0.00
49.60	243.75	2.00	0.00	0.10	0.00	49.70	243.74	2.00	0.00	0.10	0.00
49.80	243.68	2.00	0.00	0.09	0.00						

Total estimated settlement: 0.70**Abbreviations**

$Q_{tn,cs}$:	Equivalent clean sand normalized cone resistance
FS:	Factor of safety against liquefaction
e_v (%):	Post-liquefaction volumetric strain
DF:	e_v depth weighting factor
Settlement:	Calculated settlement

:: Strength loss calculation Idriss & Boulanger (2008) ::

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.30	80.54	129.37	1.80	233.07	2.27	0.42	0.90
0.40	76.12	122.26	1.86	227.12	2.28	0.37	0.89
0.50	68.91	110.66	1.97	217.50	2.31	0.27	0.87
0.60	61.08	98.07	2.10	206.36	2.34	0.22	0.85
0.70	55.64	89.33	2.19	195.35	2.36	0.19	0.84
0.80	52.36	84.04	2.19	183.98	2.36	0.18	0.83
0.90	50.29	80.71	2.14	172.62	2.35	0.17	0.83
1.00	48.50	77.81	2.07	160.79	2.34	0.16	0.82
1.10	46.72	74.95	1.99	148.79	2.32	0.15	0.81
1.20	45.12	72.37	1.90	137.52	2.29	0.15	0.81
1.30	43.40	69.60	1.84	128.17	2.28	0.14	0.80
1.40	41.62	66.73	1.83	121.85	2.27	0.13	0.80
1.50	39.65	63.55	1.84	117.19	2.28	0.13	0.79
1.60	37.61	60.27	1.87	112.45	2.28	0.12	0.78
1.70	35.63	57.08	1.87	106.51	2.28	0.12	0.78
1.80	33.95	54.36	1.84	100.24	2.28	0.11	0.77
1.90	32.57	52.14	1.80	93.92	2.27	0.11	0.77
2.00	31.19	49.92	1.75	87.50	2.25	0.11	0.76
2.10	29.70	47.52	1.72	81.70	2.24	0.10	0.75
2.20	27.91	44.62	1.73	77.04	2.24	0.10	0.75
2.30	25.92	41.42	1.79	74.14	2.26	0.09	0.74
2.40	23.95	38.25	1.90	72.61	2.29	0.09	0.73
2.50	22.19	35.41	2.02	71.45	2.32	0.09	0.73
2.60	20.94	33.39	2.09	69.81	2.34	0.09	0.73
2.70	20.11	32.05	2.09	66.93	2.34	0.09	0.72
2.80	19.97	31.82	2.00	63.60	2.32	0.08	0.72
2.90	20.60	32.83	1.89	62.07	2.29	0.08	0.72
3.00	21.67	34.54	1.89	65.20	2.29	0.09	0.73
3.10	22.10	35.22	2.09	73.61	2.34	0.09	0.73
3.20	20.76	33.06	2.57	84.95	2.44	0.10	0.73
3.30	18.46	29.36	3.37	98.89	2.55	0.09	0.72
3.40	16.29	25.85	4.34	112.08	2.66	0.09	0.62
3.50	15.43	24.47	5.04	123.42	2.73	0.09	0.62
3.60	15.14	23.99	5.52	132.32	2.77	0.09	0.62
3.70	15.27	24.18	5.75	139.12	2.79	0.09	0.62
3.80	15.71	24.89	5.79	144.16	2.80	0.09	0.62
3.90	16.02	25.38	5.79	146.99	2.80	0.10	0.62
4.00	15.90	25.17	5.91	148.80	2.80	0.10	0.62
4.10	15.47	24.48	6.13	149.92	2.82	0.09	0.62
4.20	15.30	24.19	6.22	150.52	2.83	0.09	0.62
4.30	15.03	23.75	6.29	149.40	2.83	0.09	0.62
4.40	13.95	22.01	6.61	145.58	2.86	0.09	0.62
4.50	12.08	18.98	7.30	138.63	2.91	0.09	0.62
4.60	10.23	16.01	8.05	128.85	2.96	0.08	0.62
4.70	8.88	13.83	8.50	117.49	2.98	0.08	0.62
4.80	7.65	11.85	8.90	105.39	3.01	0.08	1.90
4.90	6.48	9.95	9.45	94.05	3.04	0.08	1.57
5.00	5.29	8.04	10.41	83.71	3.09	0.08	1.24

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
5.10	4.54	6.83	11.20	76.47	3.13	0.07	1.04
5.20	4.11	6.12	11.64	71.20	3.15	0.07	0.92
5.30	3.98	5.91	11.52	68.13	3.14	0.07	0.87
5.40	3.98	5.91	11.27	66.56	3.13	0.07	0.86
5.50	3.98	5.90	11.27	66.47	3.13	0.07	0.84
5.60	3.95	5.84	11.66	68.11	3.15	0.07	0.82
5.70	3.84	5.66	12.50	70.68	3.19	0.07	0.78
5.80	3.71	5.44	13.51	73.44	3.23	0.07	0.74
5.90	3.67	5.37	14.24	76.47	3.26	0.07	0.72
6.00	3.78	5.54	14.43	79.91	3.27	0.07	0.73
6.10	3.92	5.74	14.42	82.82	3.27	0.07	0.75
6.20	3.98	5.85	14.54	84.98	3.28	0.07	0.75
6.30	3.98	5.84	14.87	86.77	3.29	0.07	0.74
6.40	4.19	6.16	14.79	91.06	3.28	0.07	0.77
6.50	4.70	6.97	14.09	98.24	3.26	0.07	0.86
6.60	5.51	8.26	12.96	107.05	3.21	0.08	1.00
6.70	6.36	9.63	11.99	115.42	3.17	0.08	1.15
6.80	6.92	10.51	11.58	121.71	3.15	0.08	1.24
6.90	7.07	10.74	11.73	126.00	3.15	0.08	1.25
7.00	7.06	10.72	12.05	129.12	3.17	0.08	1.23
7.10	7.53	11.47	11.64	133.44	3.15	0.08	1.30
7.20	8.17	12.48	10.90	136.06	3.11	0.08	1.39
7.30	8.41	12.86	10.57	136.00	3.10	0.08	1.41
7.40	8.09	12.34	10.92	134.75	3.12	0.08	1.34
7.50	8.74	13.37	10.78	144.15	3.11	0.08	1.43
7.60	10.99	16.98	9.74	165.33	3.05	0.09	1.79
7.70	13.63	21.21	8.74	185.31	3.00	0.09	0.62
7.80	15.24	23.79	8.23	195.81	2.97	0.10	0.62
7.90	15.53	24.25	8.07	195.78	2.96	0.09	0.62
8.00	15.24	23.77	7.97	189.46	2.95	0.09	0.62
8.10	14.56	22.67	7.91	179.40	2.95	0.09	0.62
8.20	13.55	21.03	7.92	166.52	2.95	0.09	0.62
8.30	12.33	19.07	8.04	153.36	2.95	0.09	0.62
8.40	11.42	17.59	8.12	142.81	2.96	0.09	0.62
8.50	10.85	16.68	8.10	135.12	2.96	0.09	0.62
8.60	10.72	16.46	7.93	130.53	2.95	0.08	0.62
8.70	10.46	16.02	7.92	126.93	2.95	0.08	0.62
8.80	10.06	15.38	8.12	124.89	2.96	0.08	0.62
8.90	9.83	15.01	8.37	125.58	2.98	0.08	0.62
9.00	10.07	15.38	8.34	128.35	2.97	0.08	0.62
9.10	10.47	16.01	8.13	130.14	2.96	0.08	0.62
9.20	10.73	16.42	7.94	130.36	2.95	0.08	0.62
9.30	10.76	16.45	7.94	130.67	2.95	0.08	0.62
9.40	10.76	16.44	8.09	133.08	2.96	0.08	0.62
9.50	10.76	16.44	8.30	136.47	2.97	0.08	0.62
9.60	11.08	16.95	8.28	140.28	2.97	0.08	0.62
9.70	12.05	18.49	7.72	142.82	2.93	0.09	0.62
9.80	15.58	24.16	6.18	149.21	2.83	0.09	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.90	20.15	31.49	4.93	155.33	2.72	0.10	0.62
10.00	20.15	31.47	4.86	153.09	2.71	0.11	0.62
10.10	15.24	23.57	5.98	140.98	2.81	0.09	0.62
10.20	9.08	13.68	8.74	119.52	3.00	0.08	0.62
10.30	6.68	9.82	10.67	104.72	3.10	0.08	0.87
10.40	6.06	8.81	11.07	97.54	3.12	0.08	0.78
10.50	5.06	7.20	12.32	88.67	3.18	0.07	0.63
10.60	4.24	5.87	13.84	81.23	3.25	0.07	0.51
10.70	3.95	5.39	14.46	77.99	3.27	0.07	0.47
10.80	3.84	5.20	15.03	78.18	3.29	0.07	0.45
10.90	3.70	4.98	16.15	80.49	3.34	0.07	0.43
11.00	3.61	4.82	17.17	82.69	3.37	0.07	0.42
11.10	3.66	4.89	17.18	84.06	3.37	0.07	0.42
11.20	3.79	5.10	16.69	85.11	3.35	0.07	0.44
11.30	4.04	5.49	16.08	88.37	3.33	0.07	0.47
11.40	4.70	6.55	14.79	96.84	3.28	0.07	0.56
11.50	5.71	8.16	13.05	106.55	3.21	0.07	0.69
11.60	6.66	9.67	11.79	114.01	3.16	0.08	0.82
11.70	7.46	10.94	11.11	121.54	3.12	0.08	0.92
11.80	8.53	12.66	10.40	131.60	3.09	0.08	1.06
11.90	10.10	15.17	9.29	140.93	3.03	0.08	1.26
12.00	11.40	17.25	8.30	143.21	2.97	0.09	0.62
12.10	12.05	18.28	7.65	139.82	2.93	0.09	0.62
12.20	11.99	18.18	7.40	134.57	2.91	0.09	0.62
12.30	11.24	16.97	7.61	129.18	2.93	0.08	0.62
12.40	9.78	14.62	8.31	121.44	2.97	0.08	0.62
12.50	7.81	11.45	9.62	110.11	3.05	0.08	0.93
12.60	5.80	8.20	11.68	95.74	3.15	0.07	0.66
12.70	4.05	5.39	14.74	79.45	3.28	0.07	0.43
12.80	3.26	4.10	15.82	64.84	3.32	0.07	0.33
12.90	3.58	4.62	11.98	55.29	3.17	0.07	0.37
13.00	4.31	5.79	8.99	52.05	3.01	0.07	0.46
13.10	4.77	6.51	8.46	55.14	2.98	0.07	0.62
13.20	4.87	6.66	9.79	65.21	3.06	0.07	0.53
13.30	5.19	7.17	11.00	78.88	3.12	0.07	0.57
13.40	5.59	7.80	11.68	91.12	3.15	0.07	0.62
13.50	5.90	8.30	12.16	100.89	3.17	0.07	0.65
13.60	6.41	9.10	12.11	110.20	3.17	0.07	0.71
13.70	7.60	11.01	10.74	118.25	3.11	0.08	0.86
13.80	9.89	14.68	8.35	122.55	2.97	0.08	0.62
13.90	12.14	18.28	6.60	120.60	2.86	0.08	0.62
14.00	13.09	19.80	6.03	119.38	2.81	0.09	0.62
14.10	12.44	18.74	6.64	124.53	2.86	0.08	0.62
14.20	12.59	18.98	7.38	140.12	2.91	0.08	0.62
14.30	16.22	24.81	6.21	154.12	2.83	0.09	0.62
14.40	23.62	36.24	4.08	148.01	2.64	0.10	0.62
14.50	32.92	48.53	2.54	123.27	2.43	0.10	0.75
14.60	41.56	58.81	1.72	101.36	2.24	0.11	0.76

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
14.70	48.47	66.43	1.41	93.93	2.10	0.11	0.77
14.80	52.66	71.00	1.33	94.66	2.03	0.11	0.76
14.90	53.17	71.48	1.33	95.28	2.03	0.11	0.77
15.00	49.27	66.90	1.41	94.32	2.09	0.11	0.77
15.10	40.94	56.71	1.66	94.32	2.22	0.11	0.76
15.20	30.97	43.98	2.29	100.91	2.38	0.10	0.74
15.30	21.85	31.76	3.49	110.80	2.57	0.09	0.72
15.40	15.51	22.82	4.97	113.49	2.72	0.08	0.62
15.50	11.13	16.35	6.50	106.32	2.85	0.08	0.62
15.60	8.16	11.74	7.84	92.07	2.94	0.08	0.62
15.70	6.23	8.63	8.78	75.81	3.00	0.07	0.62
15.80	5.38	7.25	8.57	62.13	2.99	0.07	0.62
15.90	5.36	7.15	7.29	52.12	2.91	0.07	0.62
16.00	5.34	7.01	6.54	45.85	2.85	0.07	0.62
16.10	4.96	6.42	6.76	43.41	2.87	0.07	0.62
16.20	4.35	5.52	7.86	43.43	2.94	0.07	0.62
16.30	3.98	4.92	9.13	44.92	3.02	0.07	0.35
16.40	3.98	4.90	9.63	47.20	3.05	0.07	0.35
16.50	3.98	4.89	10.03	48.98	3.07	0.07	0.35
16.60	3.98	4.87	10.25	49.89	3.08	0.07	0.35
16.70	3.98	4.85	10.28	49.88	3.08	0.07	0.35
16.80	3.98	4.83	10.18	49.18	3.08	0.07	0.35
16.90	3.98	4.82	10.17	48.98	3.08	0.07	0.34
17.00	3.98	4.80	10.51	50.42	3.09	0.07	0.34
17.10	3.94	4.72	11.40	53.77	3.14	0.07	0.34
17.20	4.08	4.92	12.06	59.31	3.17	0.07	0.35
17.30	5.02	6.36	11.10	70.59	3.12	0.07	0.45
17.40	6.54	8.69	9.84	85.46	3.06	0.08	0.62
17.50	8.33	11.42	8.88	101.36	3.01	0.08	0.82
17.60	9.72	13.50	8.48	114.46	2.98	0.08	0.62
17.70	10.81	15.11	8.04	121.56	2.95	0.08	0.62
17.80	11.39	15.92	7.67	122.06	2.93	0.08	0.62
17.90	11.17	15.50	7.60	117.86	2.93	0.08	0.62
18.00	10.46	14.39	7.82	112.59	2.94	0.08	0.62
18.10	9.58	13.01	8.24	107.14	2.97	0.08	0.62
18.20	8.88	11.90	8.62	102.55	2.99	0.08	0.62
18.30	8.09	10.67	9.21	98.23	3.02	0.08	0.76
18.40	7.19	9.28	10.12	93.89	3.07	0.08	0.66
18.50	6.45	8.14	10.98	89.39	3.12	0.07	0.58
18.60	6.04	7.50	11.41	85.63	3.14	0.07	0.54
18.70	5.99	7.40	11.32	83.75	3.14	0.07	0.53
18.80	6.24	7.73	10.76	83.19	3.11	0.07	0.55
18.90	6.64	8.29	9.94	82.40	3.07	0.07	0.59
19.00	7.02	8.82	9.19	80.99	3.02	0.08	0.63
19.10	7.02	8.78	8.89	78.06	3.01	0.08	0.63
19.20	6.63	8.19	9.01	73.79	3.01	0.07	0.59
19.30	6.23	7.58	9.33	70.76	3.03	0.07	0.54
19.40	6.06	7.30	9.93	72.47	3.06	0.07	0.52

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
19.50	6.65	8.13	10.10	82.07	3.07	0.07	0.58
19.60	7.86	9.84	9.64	94.93	3.05	0.08	0.70
19.70	9.33	11.92	8.88	105.88	3.01	0.08	0.85
19.80	12.75	16.70	7.16	119.55	2.90	0.08	0.62
19.90	18.72	24.54	5.26	129.05	2.75	0.09	0.62
20.00	20.77	27.08	4.70	127.19	2.70	0.10	0.62
20.10	17.42	22.53	5.14	115.85	2.74	0.09	0.62
20.20	10.46	13.21	7.20	95.19	2.90	0.08	0.62
20.30	7.00	8.34	9.83	82.00	3.06	0.07	0.60
20.40	6.52	7.63	10.50	80.15	3.09	0.07	0.55
20.50	6.31	7.32	11.04	80.81	3.12	0.07	0.52
20.60	6.18	7.11	11.63	82.66	3.15	0.07	0.51
20.70	5.98	6.80	12.54	85.31	3.19	0.07	0.49
20.80	6.14	6.99	13.05	91.20	3.21	0.07	0.50
20.90	7.00	8.17	12.59	102.84	3.19	0.07	0.58
21.00	8.96	10.84	10.81	117.14	3.11	0.08	0.77
21.10	11.72	14.61	8.61	125.79	2.99	0.08	0.62
21.20	14.03	17.64	7.14	125.93	2.90	0.09	0.62
21.30	14.79	18.52	6.65	123.20	2.86	0.09	0.62
21.40	14.13	17.62	7.05	124.31	2.89	0.08	0.62
21.50	12.43	15.33	8.31	127.42	2.97	0.08	0.62
21.60	10.28	12.37	10.21	126.24	3.08	0.08	0.88
21.70	8.08	9.34	12.78	119.42	3.20	0.08	0.67
21.80	6.21	6.79	15.97	108.41	3.33	0.07	0.48
21.90	5.28	5.52	18.04	99.49	3.40	0.07	0.39
22.00	5.34	5.57	17.21	95.84	3.37	0.07	0.40
22.10	6.13	6.61	14.84	98.07	3.29	0.07	0.47
22.20	7.05	7.81	13.08	102.14	3.22	0.08	0.56
22.30	7.61	8.52	12.38	105.47	3.18	0.08	0.61
22.40	8.13	9.17	11.95	109.64	3.16	0.08	0.66
22.50	9.00	10.29	11.30	116.23	3.13	0.08	0.73
22.60	9.37	10.74	11.18	120.09	3.13	0.08	0.77
22.70	8.82	9.97	11.89	118.55	3.16	0.08	0.71
22.80	7.69	8.46	13.29	112.37	3.22	0.07	0.60
22.90	6.90	7.40	14.35	106.12	3.27	0.07	0.53
23.00	6.98	7.47	14.06	105.03	3.26	0.07	0.53
23.10	7.60	8.24	13.08	107.82	3.22	0.08	0.59
23.20	8.28	9.09	12.23	111.21	3.18	0.08	0.65
23.30	8.77	9.69	11.69	113.23	3.15	0.08	0.69
23.40	8.77	9.65	11.69	112.79	3.15	0.08	0.69
23.50	8.95	9.85	11.56	113.85	3.15	0.08	0.70
23.60	9.45	10.45	11.17	116.74	3.13	0.08	0.75
23.70	9.65	10.67	11.13	118.76	3.13	0.08	0.76
23.80	9.37	10.27	11.66	119.81	3.15	0.08	0.73
23.90	9.41	10.29	12.01	123.61	3.17	0.08	0.73
24.00	11.56	12.97	10.27	133.21	3.08	0.08	0.93
24.10	16.37	18.95	7.39	140.03	2.91	0.09	0.62
24.20	22.14	25.65	5.23	134.10	2.75	0.09	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
24.30	26.41	30.40	3.97	120.78	2.62	0.10	0.62
24.40	28.09	32.14	3.48	111.85	2.57	0.10	0.73
24.50	26.73	30.52	3.75	114.45	2.60	0.10	0.73
24.60	23.36	26.67	4.71	125.71	2.70	0.09	0.62
24.70	20.44	23.31	6.00	139.79	2.81	0.09	0.62
24.80	19.80	22.57	6.68	150.66	2.86	0.09	0.62
24.90	20.81	23.69	6.54	155.06	2.85	0.09	0.62
25.00	21.40	24.28	6.26	152.06	2.83	0.09	0.62
25.10	22.04	24.87	5.79	143.99	2.79	0.09	0.62
25.20	22.96	25.79	5.30	136.81	2.75	0.09	0.62
25.30	23.14	25.91	5.29	137.02	2.75	0.09	0.62
25.40	22.74	25.46	5.83	148.46	2.80	0.09	0.62
25.50	24.78	27.85	6.14	171.07	2.82	0.09	0.62
25.60	33.66	37.98	5.05	191.70	2.73	0.10	0.62
25.70	53.07	59.58	3.28	195.43	2.54	0.12	0.77
25.80	82.74	91.73	2.03	185.82	2.33	0.18	0.83
25.90	117.80	128.70	1.47	189.05	2.13	0.28	0.87
26.00	148.57	160.21	1.29	206.69	1.98	0.46	0.89
26.10	167.69	179.21	1.23	220.06	1.89	0.66	0.89
26.20	173.65	184.66	1.20	222.02	1.85	0.69	0.88
26.30	170.00	180.46	1.21	218.21	1.86	0.59	0.88
26.40	161.80	171.65	1.23	211.10	1.89	0.48	0.88
26.50	152.97	162.24	1.25	203.19	1.92	0.39	0.87
26.60	145.31	154.04	1.27	196.34	1.96	0.35	0.87
26.70	141.26	149.53	1.29	192.44	1.97	0.32	0.87
26.80	141.98	149.87	1.28	192.32	1.97	0.32	0.87
26.90	146.65	154.22	1.27	195.36	1.95	0.36	0.87
27.00	152.40	159.62	1.25	199.23	1.92	0.39	0.87
27.10	156.02	162.81	1.23	200.73	1.89	0.41	0.87
27.20	156.40	162.70	1.22	199.17	1.88	0.40	0.87
27.30	153.19	158.95	1.22	194.36	1.88	0.37	0.86
27.40	147.34	152.52	1.23	186.92	1.88	0.32	0.85
27.50	139.24	143.76	1.23	176.64	1.89	0.28	0.85
27.60	130.22	134.07	1.23	164.76	1.89	0.23	0.83
27.70	121.27	124.45	1.23	152.73	1.89	0.20	0.82
27.80	114.09	116.70	1.22	142.65	1.88	0.17	0.80
27.90	109.39	111.55	1.22	135.64	1.87	0.16	0.79
28.00	107.21	109.08	1.22	132.69	1.87	0.16	0.79
28.10	107.70	109.46	1.23	134.46	1.89	0.16	0.80
28.20	110.28	112.03	1.24	139.30	1.91	0.17	0.81
28.30	114.57	116.29	1.25	145.75	1.92	0.18	0.82
28.40	120.76	122.38	1.25	153.25	1.92	0.20	0.83
28.50	128.38	129.85	1.24	161.60	1.91	0.22	0.83
28.60	137.33	138.63	1.24	171.49	1.90	0.26	0.84
28.70	146.10	147.25	1.24	181.91	1.90	0.30	0.85
28.80	153.76	154.76	1.24	191.87	1.90	0.36	0.87
28.90	159.82	160.63	1.25	200.03	1.91	0.42	0.87
29.00	164.17	164.70	1.25	205.70	1.92	0.47	0.88

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
29.10	166.84	167.05	1.25	208.83	1.92	0.51	0.89
29.20	167.23	167.07	1.25	208.99	1.92	0.51	0.89
29.30	165.31	164.80	1.26	206.83	1.93	0.49	0.89
29.40	162.24	161.42	1.26	203.98	1.94	0.45	0.88
29.50	159.54	158.40	1.27	201.12	1.95	0.42	0.88
29.60	158.40	156.86	1.26	198.33	1.94	0.40	0.88
29.70	158.21	156.18	1.25	194.79	1.92	0.39	0.87
29.80	154.57	152.33	1.26	192.38	1.94	0.41	0.88
29.90	143.99	141.96	1.36	192.82	2.05	0.38	0.89
30.00	135.18	133.15	1.47	195.31	2.13	0.28	0.87
30.10	132.28	129.84	1.43	185.80	2.11	0.30	0.88
30.20	131.76	128.75	1.33	171.55	2.03	0.30	0.87
30.30	123.68	120.49	1.33	160.84	2.03	0.24	0.86
30.40	107.40	104.49	1.52	159.11	2.16	0.21	0.85
30.50	91.85	89.16	1.88	167.52	2.29	0.18	0.83
30.60	84.79	82.08	2.18	178.54	2.36	0.16	0.82
30.70	90.92	87.85	2.05	180.41	2.33	0.18	0.83
30.80	108.65	104.82	1.69	176.75	2.23	0.22	0.85
30.90	128.66	123.87	1.43	177.20	2.11	0.30	0.88
31.00	143.23	137.56	1.32	182.22	2.02	0.35	0.88
31.10	150.57	144.28	1.29	186.10	1.98	0.35	0.88
31.20	153.08	146.38	1.29	188.32	1.97	0.37	0.88
31.30	152.85	145.85	1.29	188.71	1.98	0.38	0.88
31.40	149.11	141.97	1.31	186.10	2.00	0.36	0.88
31.50	141.26	134.15	1.34	180.37	2.04	0.32	0.88
31.60	130.34	123.43	1.40	172.88	2.09	0.27	0.87
31.70	118.72	112.05	1.47	164.46	2.13	0.23	0.86
31.80	108.66	102.19	1.52	155.22	2.16	0.20	0.85
31.90	100.38	94.06	1.55	145.43	2.17	0.18	0.84
32.00	93.10	86.92	1.59	137.98	2.19	0.17	0.83
32.10	86.10	80.08	1.70	136.33	2.23	0.16	0.82
32.20	78.52	72.72	1.96	142.75	2.31	0.15	0.81
32.30	69.94	64.43	2.43	156.46	2.41	0.15	0.80
32.40	60.92	55.75	3.11	173.12	2.52	0.13	0.79
32.50	53.88	48.96	3.80	186.26	2.61	0.12	0.62
32.60	50.19	45.36	4.30	194.91	2.66	0.12	0.62
32.70	49.69	44.75	4.55	203.44	2.68	0.12	0.62
32.80	52.24	47.00	4.54	213.56	2.68	0.12	0.62
32.90	56.89	51.19	4.34	222.04	2.66	0.13	0.64
33.00	62.25	56.03	4.03	225.59	2.63	0.14	0.65
33.10	68.14	61.33	3.65	223.61	2.59	0.15	0.80
33.20	75.90	68.36	3.17	216.38	2.53	0.16	0.81
33.30	85.75	77.30	2.66	205.91	2.45	0.18	0.83
33.40	93.70	84.46	2.35	198.06	2.39	0.20	0.84
33.50	96.01	86.38	2.27	195.78	2.38	0.21	0.84
33.60	92.45	82.87	2.40	198.97	2.41	0.19	0.84
33.70	84.75	75.56	2.69	203.61	2.46	0.18	0.83
33.80	74.88	66.31	3.08	204.33	2.51	0.16	0.81

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
33.90	64.13	56.33	3.52	198.30	2.57	0.14	0.79
34.00	54.10	47.08	3.96	186.34	2.62	0.13	0.62
34.10	46.11	39.73	4.37	173.63	2.67	0.11	0.62
34.20	39.59	33.73	4.88	164.76	2.72	0.11	0.62
34.30	34.09	28.69	5.58	160.14	2.78	0.10	0.62
34.40	29.36	24.36	6.41	156.10	2.84	0.10	0.62
34.50	25.02	20.43	7.25	148.09	2.90	0.09	0.62
34.60	21.00	16.82	8.19	137.74	2.96	0.09	0.62
34.70	17.76	13.93	9.28	129.28	3.03	0.08	0.99
34.80	15.83	12.19	10.36	126.28	3.09	0.08	0.87
34.90	15.33	11.72	10.85	127.20	3.11	0.08	0.84
35.00	15.28	11.64	11.11	129.34	3.12	0.08	0.83
35.10	15.62	11.91	11.34	135.08	3.14	0.08	0.85
35.20	16.74	12.85	11.28	144.97	3.13	0.08	0.92
35.30	19.92	15.58	10.03	156.19	3.07	0.09	1.11
35.40	25.11	20.03	8.02	160.65	2.95	0.09	0.62
35.50	32.33	26.27	6.00	157.69	2.81	0.10	0.62
35.60	40.65	33.55	4.45	149.25	2.67	0.11	0.62
35.70	48.86	40.74	3.43	139.85	2.56	0.12	0.76
35.80	55.37	46.44	2.81	130.29	2.47	0.12	0.77
35.90	57.47	48.24	2.54	122.48	2.43	0.12	0.78
36.00	55.09	46.03	2.64	121.48	2.45	0.12	0.77
36.10	48.80	40.35	3.19	128.75	2.53	0.11	0.76
36.20	40.68	33.09	4.26	140.85	2.66	0.11	0.62
36.30	33.39	26.63	5.62	149.63	2.78	0.10	0.62
36.40	29.34	23.06	6.62	152.64	2.86	0.09	0.62
36.50	29.53	23.16	6.57	152.12	2.85	0.10	0.62
36.60	32.29	25.47	5.95	151.52	2.81	0.10	0.62
36.70	34.52	27.32	5.62	153.45	2.78	0.10	0.62
36.80	34.12	26.88	5.89	158.27	2.80	0.10	0.62
36.90	31.26	24.34	6.70	163.05	2.86	0.10	0.62
37.00	28.61	22.06	7.44	164.19	2.92	0.09	0.62
37.10	30.10	23.24	6.92	160.90	2.88	0.09	0.62
37.20	36.63	28.76	5.26	151.31	2.75	0.10	0.62
37.30	46.22	36.94	3.75	138.69	2.60	0.11	0.62
37.40	55.48	44.85	2.90	130.26	2.49	0.12	0.77
37.50	62.76	51.02	2.52	128.52	2.43	0.13	0.78
37.60	68.04	55.45	2.32	128.50	2.39	0.13	0.79
37.70	71.11	58.00	2.17	126.04	2.36	0.14	0.79
37.80	72.57	59.17	2.08	122.99	2.34	0.14	0.79
37.90	72.53	59.02	2.07	122.32	2.34	0.14	0.79
38.00	71.83	58.28	2.11	122.81	2.34	0.13	0.79
38.10	71.07	57.52	2.11	121.29	2.35	0.13	0.79
38.20	70.43	56.90	2.06	117.17	2.33	0.13	0.79
38.30	69.54	56.06	2.04	114.12	2.33	0.13	0.79
38.40	67.93	54.55	2.11	115.14	2.35	0.13	0.79
38.50	66.57	53.19	2.28	121.02	2.38	0.13	0.78
38.60	67.27	53.57	2.40	128.60	2.41	0.13	0.78

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
38.70	70.56	56.15	2.40	134.82	2.41	0.14	0.79
38.80	74.92	59.66	2.33	138.76	2.39	0.14	0.80
38.90	78.18	62.25	2.27	141.24	2.38	0.15	0.81
39.00	79.69	63.35	2.26	143.06	2.38	0.15	0.81
39.10	79.93	63.40	2.27	143.96	2.38	0.15	0.81
39.20	80.59	63.82	2.25	143.34	2.37	0.15	0.81
39.30	82.67	65.46	2.15	140.67	2.35	0.15	0.81
39.40	86.56	68.65	2.00	137.30	2.32	0.16	0.81
39.50	91.52	72.75	1.85	134.59	2.28	0.16	0.82
39.60	96.64	76.97	1.73	133.36	2.24	0.17	0.83
39.70	100.82	80.33	1.68	134.76	2.22	0.18	0.83
39.80	100.16	79.44	1.77	140.84	2.26	0.19	0.84
39.90	91.82	72.01	2.13	153.15	2.35	0.18	0.83
40.00	78.37	60.48	2.79	169.03	2.47	0.15	0.80
40.10	62.81	47.50	3.80	180.50	2.61	0.13	0.64
40.20	50.47	37.38	4.92	183.83	2.72	0.12	0.62
40.30	42.83	31.15	5.99	186.64	2.81	0.11	0.62
40.40	43.11	31.27	6.04	188.86	2.81	0.11	0.62
40.50	50.11	36.80	5.04	185.32	2.73	0.12	0.62
40.60	60.63	45.25	3.81	172.25	2.61	0.13	0.63
40.70	71.15	53.85	2.85	153.69	2.48	0.14	0.80
40.80	79.36	60.65	2.28	138.37	2.38	0.15	0.81
40.90	84.78	64.99	2.11	136.99	2.34	0.15	0.81
41.00	87.82	67.27	2.09	140.49	2.34	0.16	0.82
41.10	89.49	68.46	2.07	142.01	2.34	0.16	0.82
41.20	89.73	68.58	2.02	138.85	2.33	0.16	0.82
41.30	88.42	67.39	2.03	137.12	2.33	0.16	0.82
41.40	85.38	64.71	2.17	140.14	2.36	0.15	0.81
41.50	81.32	61.22	2.33	142.45	2.39	0.15	0.81
41.60	76.93	57.52	2.52	144.69	2.43	0.14	0.80
41.70	71.43	52.92	2.81	148.63	2.47	0.14	0.80
41.80	63.51	46.42	3.33	154.67	2.55	0.13	0.78
41.90	53.29	38.19	4.22	161.22	2.65	0.12	0.62
42.00	42.53	29.71	5.48	162.75	2.77	0.11	0.62
42.10	34.54	23.55	6.70	157.74	2.86	0.10	0.62
42.20	31.16	21.03	7.16	150.55	2.90	0.09	0.62
42.30	31.50	21.22	6.98	148.03	2.88	0.10	0.62
42.40	32.59	21.97	6.82	149.89	2.87	0.10	0.62
42.50	33.35	22.46	6.68	150.00	2.86	0.10	0.62
42.60	35.87	24.35	5.88	143.15	2.80	0.10	0.62
42.70	41.37	28.64	4.51	129.26	2.68	0.10	0.62
42.80	48.14	33.98	3.40	115.68	2.56	0.11	0.75
42.90	52.92	37.69	2.97	111.97	2.50	0.11	0.76
43.00	54.26	38.58	3.02	116.71	2.51	0.11	0.76
43.10	53.34	37.62	3.40	127.99	2.56	0.11	0.76
43.20	52.35	36.62	3.81	139.50	2.61	0.11	0.62
43.30	52.52	36.55	4.06	148.56	2.63	0.12	0.62
43.40	52.22	36.15	4.29	155.03	2.66	0.12	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
43.50	48.54	33.19	4.89	162.45	2.72	0.12	0.62
43.60	41.40	27.65	6.19	171.06	2.83	0.11	0.62
43.70	34.45	22.61	7.96	179.95	2.95	0.10	0.62
43.80	31.79	20.68	8.97	185.44	3.01	0.10	1.48
43.90	34.60	22.61	8.32	188.01	2.97	0.10	0.62
44.00	42.45	28.08	6.58	184.73	2.86	0.11	0.62
44.10	56.31	38.44	4.48	172.25	2.68	0.12	0.62
44.20	76.28	53.80	2.85	153.28	2.48	0.14	0.80
44.30	99.38	71.80	2.01	144.35	2.32	0.18	0.83
44.40	119.56	87.63	1.67	145.92	2.22	0.22	0.85
44.50	132.51	97.74	1.54	150.24	2.17	0.25	0.87
44.60	138.38	102.38	1.47	150.70	2.13	0.26	0.87
44.70	140.97	103.95	1.50	155.94	2.15	0.27	0.87
44.80	145.61	106.65	1.60	170.66	2.19	0.30	0.88
44.90	154.46	112.95	1.61	182.24	2.20	0.37	0.89
45.00	166.62	122.52	1.50	183.93	2.15	0.47	0.90
45.10	178.48	132.40	1.38	182.40	2.07	0.54	0.91
45.20	186.02	138.62	1.33	184.20	2.02	0.61	0.91
45.30	188.08	140.04	1.32	185.25	2.02	0.61	0.91
45.40	185.50	137.74	1.33	183.02	2.02	0.56	0.90
45.50	181.44	134.28	1.34	179.72	2.03	0.50	0.90
45.60	177.58	131.04	1.35	176.34	2.04	0.46	0.90
45.70	174.36	128.30	1.35	173.50	2.05	0.44	0.89
45.80	172.20	126.39	1.36	171.53	2.05	0.41	0.89
45.90	170.69	124.98	1.36	170.25	2.06	0.41	0.89
46.00	169.69	123.92	1.37	169.73	2.06	0.40	0.89
46.10	168.85	122.93	1.38	169.73	2.07	0.40	0.89
46.20	168.16	122.03	1.39	170.19	2.08	0.41	0.89
46.30	168.23	121.73	1.41	171.23	2.09	0.41	0.89
46.40	169.90	122.75	1.41	172.53	2.09	0.41	0.89
46.50	173.64	125.52	1.39	173.95	2.08	0.45	0.90
46.60	178.99	129.70	1.35	175.62	2.05	0.48	0.90
46.70	184.20	133.83	1.32	177.31	2.02	0.51	0.90
46.80	187.77	136.74	1.30	178.03	1.99	0.53	0.90
46.90	188.69	137.65	1.28	176.71	1.97	0.50	0.89
47.00	186.98	136.54	1.27	173.38	1.95	0.45	0.89
47.10	183.33	133.82	1.26	168.99	1.94	0.40	0.88
47.20	178.78	130.22	1.26	164.54	1.94	0.36	0.87
47.30	174.33	126.56	1.27	160.75	1.95	0.33	0.87
47.40	170.46	123.28	1.28	157.73	1.96	0.32	0.87
47.50	167.19	120.45	1.29	155.30	1.98	0.30	0.87
47.60	164.34	117.95	1.30	153.25	1.99	0.29	0.87
47.70	161.94	115.81	1.31	151.63	2.00	0.29	0.87
47.80	159.85	113.93	1.32	150.26	2.01	0.28	0.87
47.90	158.50	112.59	1.33	149.62	2.02	0.28	0.87
48.00	158.82	112.51	1.34	150.31	2.03	0.28	0.87
48.10	160.82	113.66	1.34	152.65	2.04	0.30	0.87
48.20	163.04	114.92	1.35	155.37	2.05	0.32	0.88

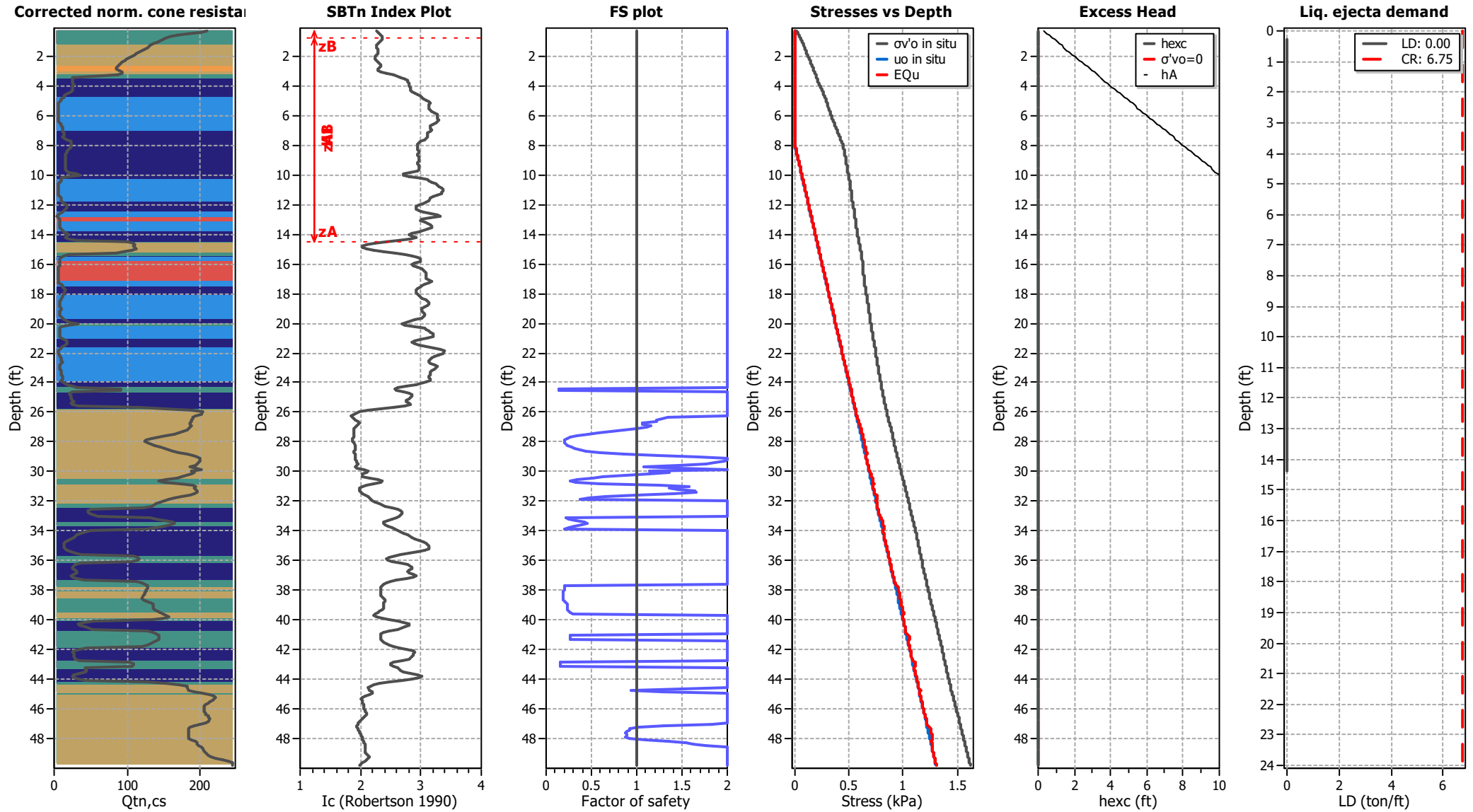
:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
48.30	164.06	115.25	1.37	157.39	2.06	0.34	0.88
48.40	164.39	115.09	1.38	158.78	2.07	0.34	0.88
48.50	165.33	115.47	1.39	160.12	2.08	0.35	0.88
48.60	167.37	116.74	1.39	161.72	2.08	0.37	0.89
48.70	169.66	118.23	1.38	163.29	2.07	0.38	0.89
48.80	171.13	119.04	1.38	164.67	2.07	0.40	0.89
48.90	171.49	118.87	1.40	166.37	2.09	0.41	0.89
49.00	171.23	118.08	1.43	168.94	2.11	0.42	0.90
49.10	171.53	117.67	1.47	172.78	2.13	0.44	0.90
49.20	174.62	119.41	1.49	177.75	2.14	0.47	0.90
49.30	181.47	124.10	1.47	182.96	2.13	0.56	0.91
49.40	191.66	131.49	1.43	188.20	2.11	0.71	0.92
49.50	202.91	139.89	1.38	193.23	2.07	0.88	0.93
49.60	212.53	147.20	1.34	197.41	2.04	0.88	0.93
49.70	219.60	152.68	1.31	200.36	2.01	0.89	0.93
49.80	223.07	155.33	1.30	201.52	1.99	0.89	0.93

Abbreviations

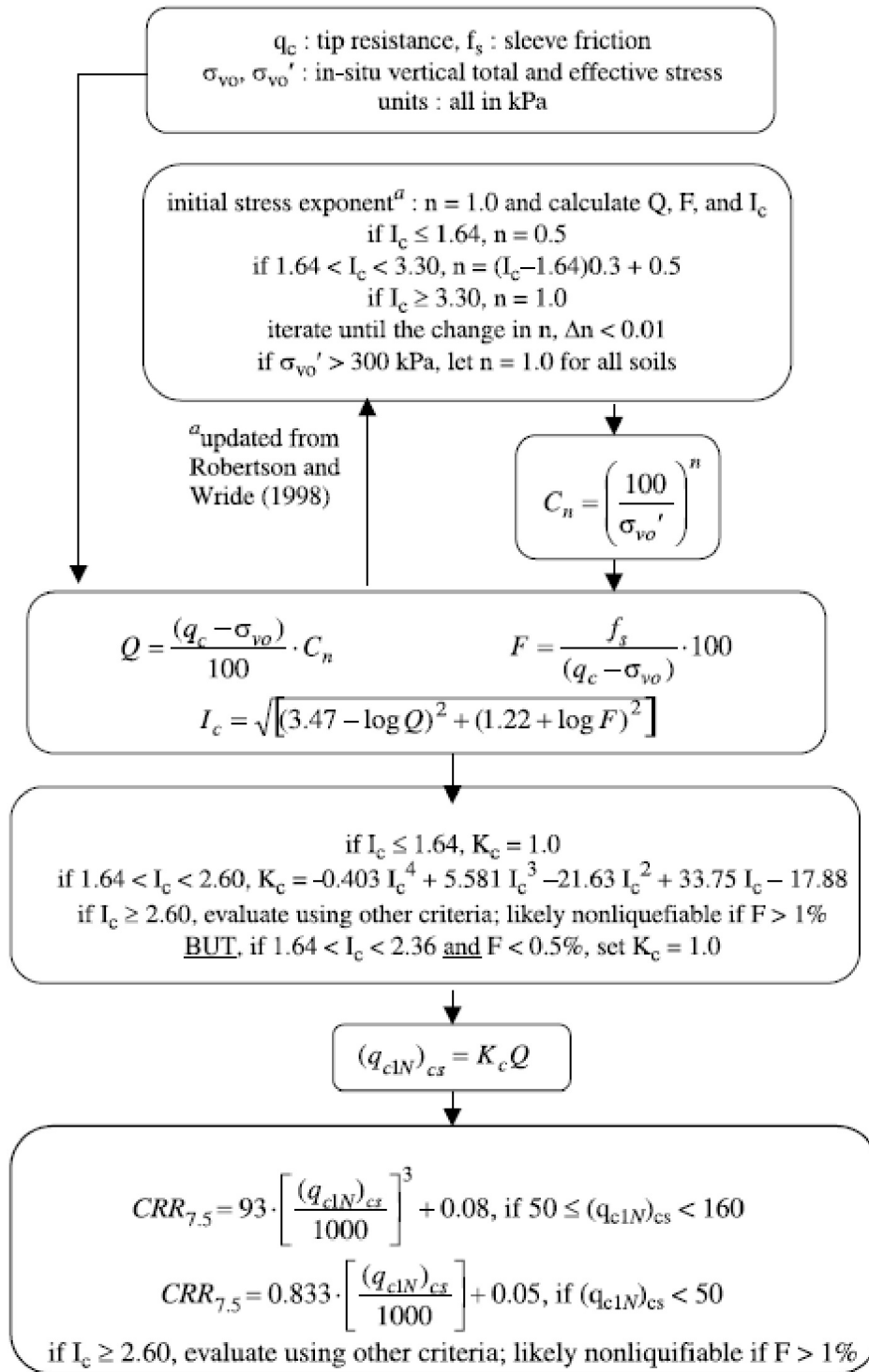
q_t :	Total cone resistance
K_c :	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c :	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

Ejecta Severity Estimation



Procedure for the evaluation of soil liquefaction resistance, NCEER (1998)

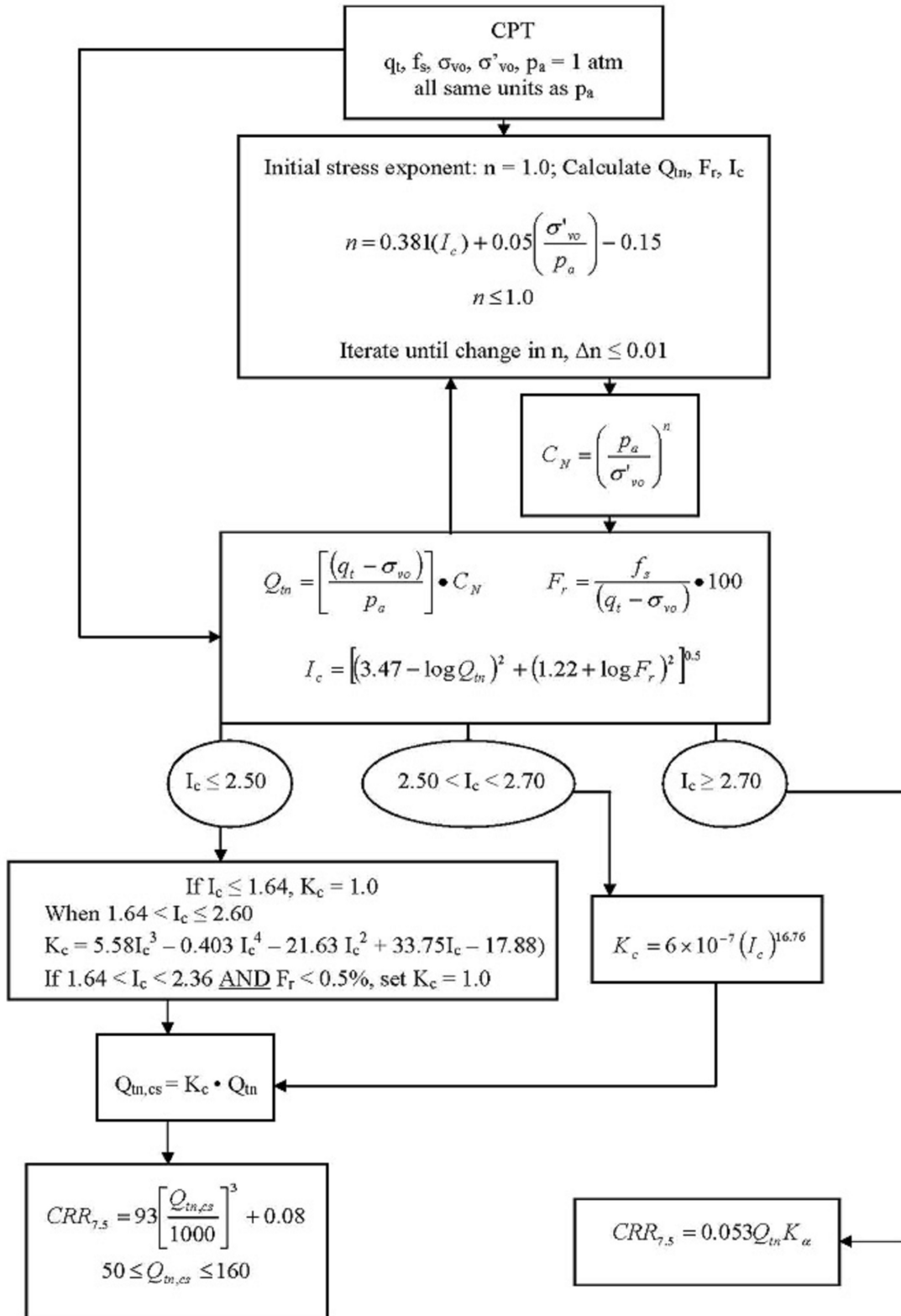
Calculation of soil resistance against liquefaction is performed according to the Robertson & Wride (1998) procedure. The procedure used in the software, slightly differs from the one originally published in NCEER-97-0022 (Proceedings of the NCEER Workshop on Evaluation of Liquefaction Resistance of Soils). The revised procedure is presented below in the form of a flowchart¹:



¹ "Estimating liquefaction-induced ground settlements from CPT for level ground", G. Zhang, P.K. Robertson, and R.W.I. Brachman

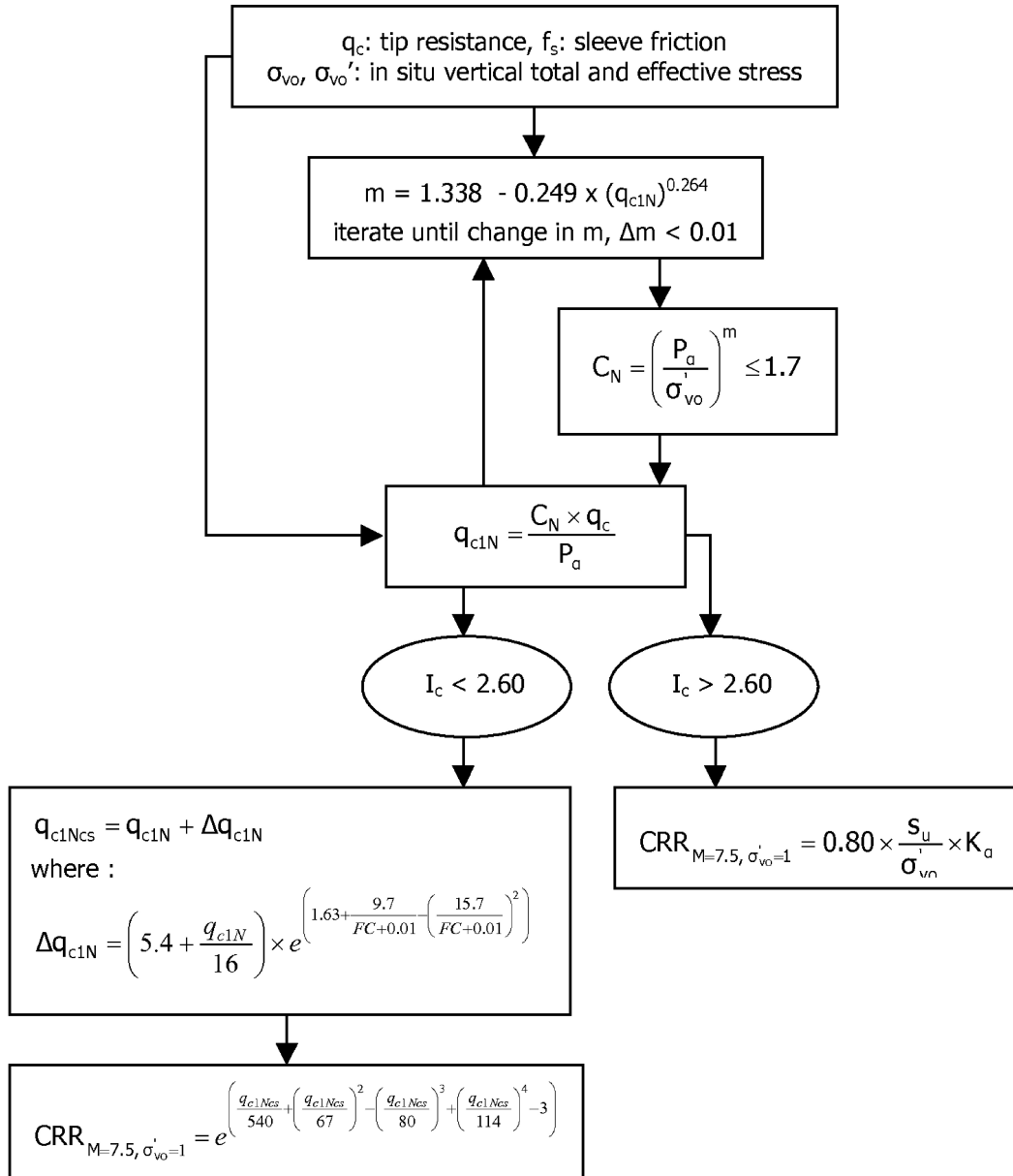
Procedure for the evaluation of soil liquefaction resistance (all soils), Robertson (2010)

Calculation of soil resistance against liquefaction is performed according to the Robertson & Wride (1998) procedure. This procedure used in the software, slightly differs from the one originally published in NCEER-97-0022 (Proceedings of the NCEER Workshop on Evaluation of Liquefaction Resistance of Soils). The revised procedure is presented below in the form of a flowchart¹:

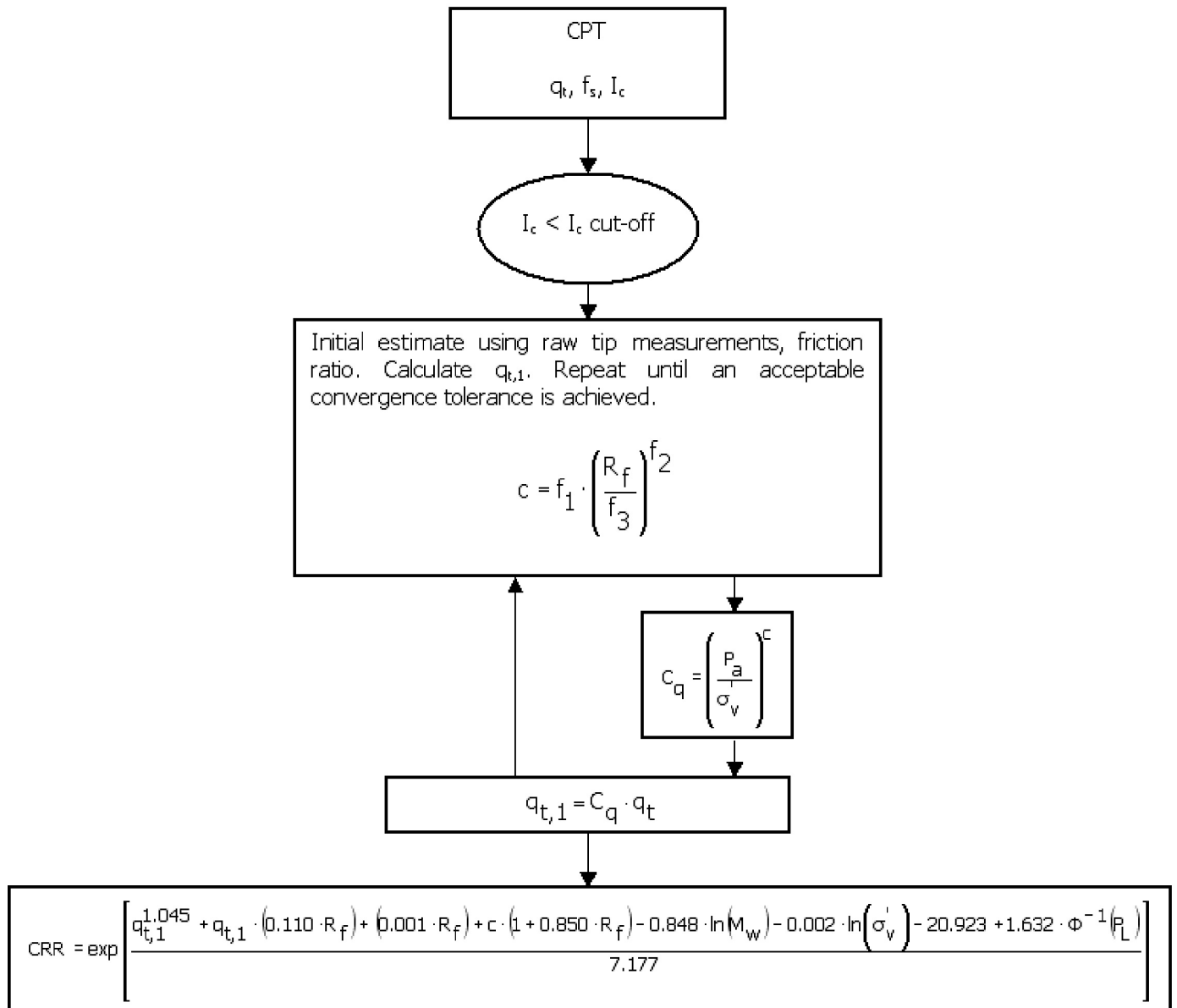


¹ P.K. Robertson, 2009. "Performance based earthquake design using the CPT", Keynote Lecture, International Conference on Performance-based Design in Earthquake Geotechnical Engineering – from case history to practice, IS-Tokyo, June 2009

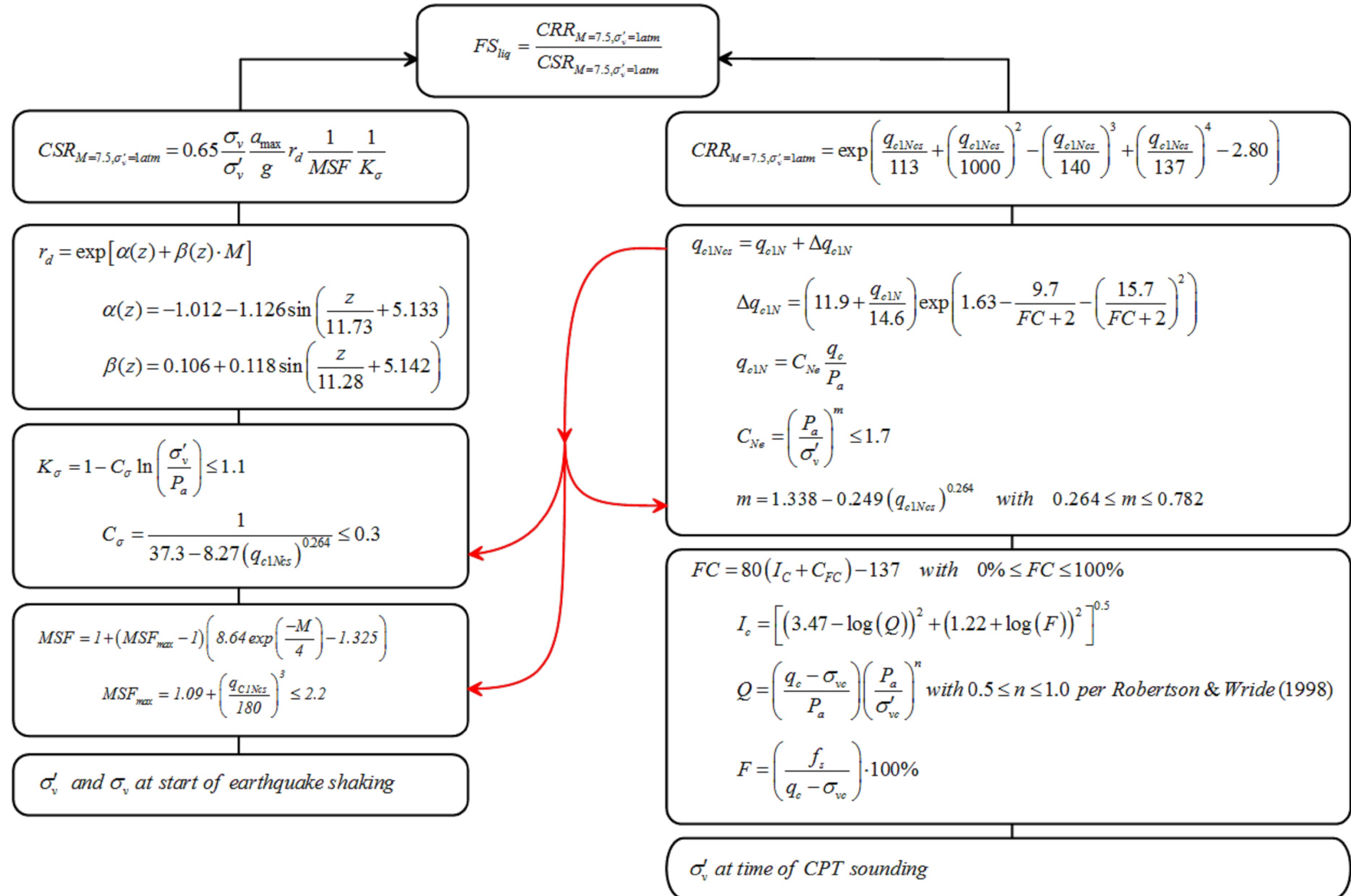
Procedure for the evaluation of soil liquefaction resistance, Idriss & Boulanger (2008)



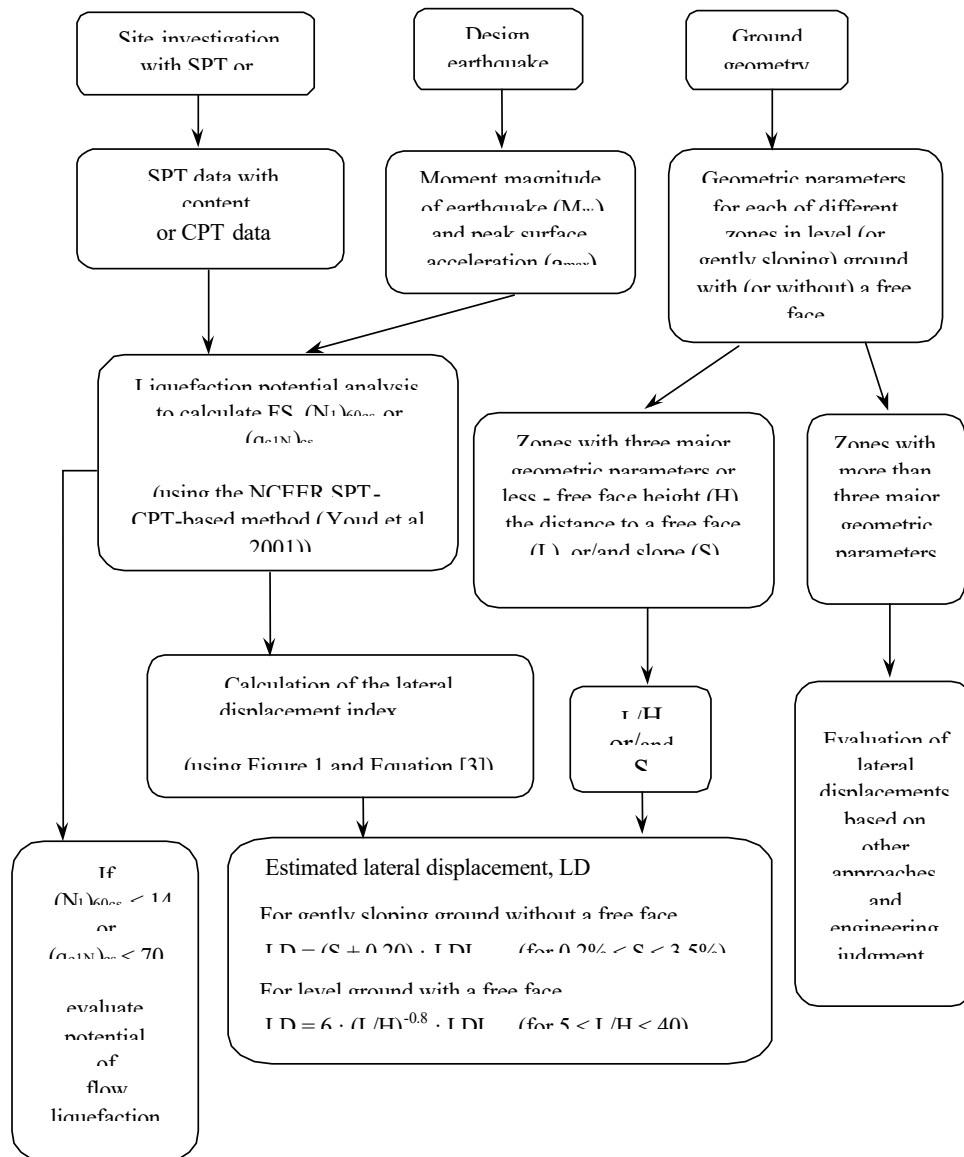
Procedure for the evaluation of soil liquefaction resistance (sandy soils), Moss et al. (2006)



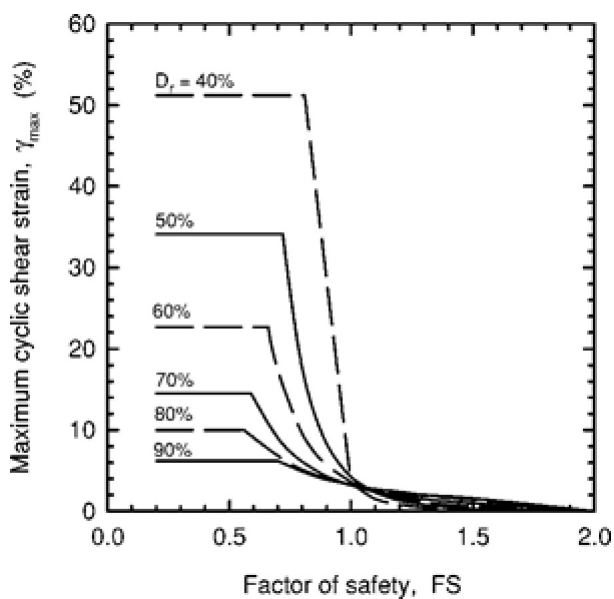
Procedure for the evaluation of soil liquefaction resistance, Boulanger & Idriss(2014)



Procedure for the evaluation of liquefaction-induced lateral spreading displacements



¹ Flow chart illustrating major steps in estimating liquefaction-induced lateral spreading displacements using the proposed approach



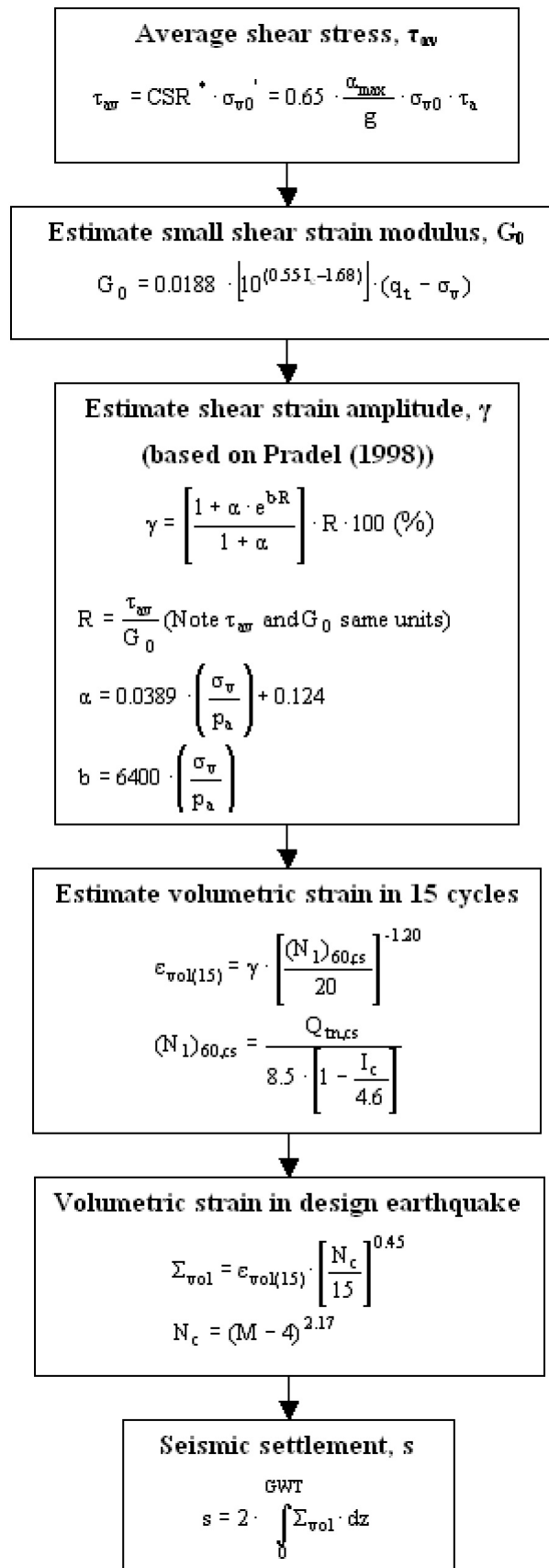
¹ Figure 1

$$LDI = \int_0^{Z_{max}} \gamma_{max} dz$$

¹ Equation [3]

¹ "Estimating liquefaction-induced ground settlements from CPT for level ground", G. Zhang, P.K. Robertson, and R.W.I. Brachman

Procedure for the estimation of seismic induced settlements in dry sands



Robertson, P.K. and Lisheng, S., 2010, "Estimation of seismic compression in dry soils using the CPT" FIFTH INTERNATIONAL CONFERENCE ON RECENT ADVANCES IN GEOTECHNICAL EARTHQUAKE ENGINEERING AND SOIL DYNAMICS, Symposium in honor of professor I. M. Idriss, San Diego, CA

Liquefaction Potential Index (LPI) calculation procedure

Calculation of the Liquefaction Potential Index (LPI) is used to interpret the liquefaction assessment calculations in terms of severity over depth. The calculation procedure is based on the methodology developed by Iwasaki (1982) and is adopted by AFPS.

To estimate the severity of liquefaction extent at a given site, LPI is calculated based on the following equation:

$$\mathbf{LPI} = \int_0^{20} (10 - 0,5z) \times F_L \times d_z$$

where:

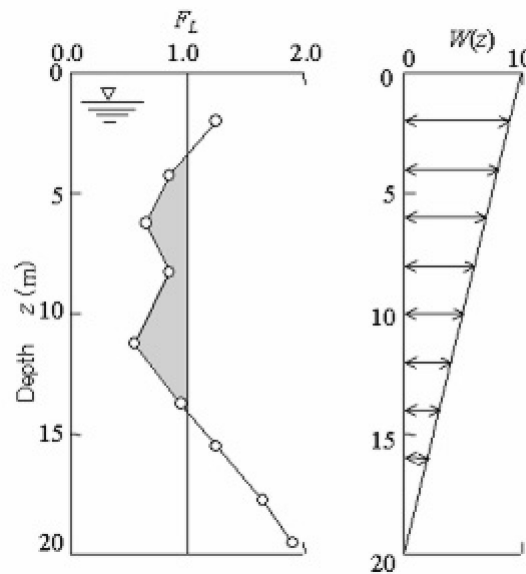
$F_L = 1 - F.S.$ when F.S. less than 1

$F_L = 0$ when F.S. greater than 1

z depth of measurment in meters

Values of LPI range between zero (0) when no test point is characterized as liquefiable and 100 when all points are characterized as susceptible to liquefaction. Iwasaki proposed four (4) discrete categories based on the numeric value of LPI:

- $LPI = 0$: Liquefaction risk is very low
- $0 < LPI \leq 5$: Liquefaction risk is low
- $5 < LPI \leq 15$: Liquefaction risk is high
- $LPI > 15$: Liquefaction risk is very high



Graphical presentation of the LPI calculation procedure

Shear-Induced Building Settlement (Ds) calculation procedure

The shear-induced building settlement (Ds) due to liquefaction below the building can be estimated using the relationship developed by Bray and Macedo (2017):

$$\begin{aligned} \ln(Ds) = & c1 + c2 * LBS + 0.58 * \ln\left(\tanh\left(\frac{HL}{6}\right)\right) + \\ & 4.59 * \ln(Q) - 0.42 * \ln(Q)^2 - 0.02 * B + \\ & 0.84 * \ln(CAVdp) + 0.41 * \ln(Sa1) + \varepsilon \end{aligned}$$

where Ds is in the units of mm, c1= -8.35 and c2= 0.072 for LBS ≤ 16, and c1= -7.48 and c2= 0.014 otherwise. Q is the building contact pressure in units of kPa, HL is the cumulative thickness of the liquefiable layers in the units of m, B is the building width in the units of m, CAVdp is a standardized version of the cumulative absolute velocity in the units of g-s, Sa1 is 5%-damped pseudo-acceleration response spectral value at a period of 1 s in the units of g, and ε is a normal random variable with zero mean and 0.50 standard deviation in Ln units. The liquefaction-induced building settlement index (LBS) is:

$$LBS = \sum W * \frac{\varepsilon_{shear}}{z} dz$$

where z (m) is the depth measured from the ground surface > 0, w is a foundation-weighting factor wherein W = 0.0 for z less than Df, which is the embedment depth of the foundation, and W = 1.0 otherwise. The shear strain parameter (ε_{shear}) is the liquefaction-induced free-field shear strain (in %) estimated using Zhang et al. (2004). It is calculated based on the estimated Dr of the liquefied soil layer and the calculated safety factor against liquefaction triggering (FSL).

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APPENDIX F

STANDARD GRADING SPECIFICATIONS

STANDARD GRADING SPECIFICATIONS

These specifications present the usual and minimum requirements for projects on which Petra Geosciences, Inc. (Petra) is the geotechnical consultant. No deviation from these specifications will be allowed, except where specifically superseded in the preliminary geology and soils report, or in other written communication signed by the Soils Engineer and Engineering Geologist of record (Geotechnical Consultant).

I. GENERAL

- A. The Geotechnical Consultant is the Owner's or Builder's representative on the project. For the purpose of these specifications, participation by the Geotechnical Consultant includes that observation performed by any person or persons employed by, and responsible to, the licensed Soils Engineer and Engineering Geologist signing the soils report.
- B. The contractor should prepare and submit to the Owner and Geotechnical Consultant a work plan that indicates the sequence of earthwork grading, the number of "spreads" and the estimated quantities of daily earthwork to be performed prior to the commencement of grading. This work plan should be reviewed by the Geotechnical Consultant to schedule personnel to perform the appropriate level of observation, mapping, and compaction testing as necessary.
- C. All clearing, site preparation, or earthwork performed on the project shall be conducted by the Contractor in accordance with the recommendations presented in the geotechnical report and under the observation of the Geotechnical Consultant.
- D. It is the Contractor's responsibility to prepare the ground surface to receive the fills to the satisfaction of the Geotechnical Consultant and to place, spread, mix, water, and compact the fill in accordance with the specifications of the Geotechnical Consultant. The Contractor shall also remove all material considered unsatisfactory by the Geotechnical Consultant.
- E. It is the Contractor's responsibility to have suitable and sufficient compaction equipment on the job site to handle the amount of fill being placed. If necessary, excavation equipment will be shut down to permit completion of compaction to project specifications. Sufficient watering apparatus will also be provided by the Contractor, with due consideration for the fill material, rate of placement, and time of year.
- F. After completion of grading a report will be submitted by the Geotechnical Consultant.

II. SITE PREPARATION

- A. Clearing and Grubbing
 - 1. All vegetation such as trees, brush, grass, roots, and deleterious material shall be disposed of offsite. This removal shall be concluded prior to placing fill.
 - 2. Any underground structures such as cesspools, cisterns, mining shafts, tunnels, septic tanks, wells, pipe lines, etc., are to be removed or treated in a manner prescribed by the Geotechnical Consultant.

STANDARD GRADING SPECIFICATIONS

III. FILL AREA PREPARATION

A. Remedial Removals/Overexcavations

1. Remedial removals, as well as overexcavation for remedial purposes, shall be evaluated by the Geotechnical Consultant. Remedial removal depths presented in the geotechnical report and shown on the geotechnical plans are estimates only. The actual extent of removal should be determined by the Geotechnical Consultant based on the conditions exposed during grading. All soft, loose, dry, saturated, spongy, organic-rich, highly fractured or otherwise unsuitable ground shall be overexcavated to competent ground as determined by the Geotechnical Consultant.
2. Soil, alluvium, or bedrock materials determined by the Soils Engineer as being unsuitable for placement in compacted fills shall be removed from the site. Any material incorporated as a part of a compacted fill must be approved by the Geotechnical Consultant.
3. Should potentially hazardous materials be encountered, the Contractor should stop work in the affected area. An environmental consultant specializing in hazardous materials should be notified immediately for evaluation and handling of these materials prior to continuing work in the affected area.

B. Evaluation/Acceptance of Fill Areas

All areas to receive fill, including removal and processed areas, key bottoms, and benches, shall be observed, mapped, elevations recorded, and/or tested prior to being accepted by the Geotechnical Consultant as suitable to receive fill. The contractor shall obtain a written acceptance from the Geotechnical Consultant prior to fill placement. A licensed surveyor shall provide sufficient survey control for determining locations and elevations of processed areas, keys, and benches.

C. Processing

After the ground surface to receive fill has been declared satisfactory for support of fill by the Geotechnical Consultant, it shall be scarified to a minimum depth of 6 inches and until the ground surface is uniform and free from ruts, hollows, hummocks, or other uneven features which may prevent uniform compaction.

The scarified ground surface shall then be brought to optimum moisture, mixed as required, and compacted to a minimum relative compaction of 90 percent.

D. Subdrains

Subdrainage devices shall be constructed in compliance with the ordinances of the controlling governmental agency, and/or with the recommendations of the Geotechnical Consultant. (Typical Canyon Subdrain details are given on Plate SG-1).

E. Cut/Fill & Deep Fill/Shallow Fill Transitions

In order to provide uniform bearing conditions in cut/fill and deep fill/shallow fill transition lots, the cut and shallow fill portions of the lot should be overexcavated to the depths and the horizontal limits discussed in the approved geotechnical report and replaced with compacted fill. (Typical details are given on Plate SG-7.)

STANDARD GRADING SPECIFICATIONS

IV. COMPACTED FILL MATERIAL

A. General

Materials excavated on the property may be utilized in the fill, provided each material has been determined to be suitable by the Geotechnical Consultant. Material to be used for fill shall be essentially free of organic material and other deleterious substances. Roots, tree branches, and other matter missed during clearing shall be removed from the fill as recommended by the Geotechnical Consultant. Material that is spongy, subject to decay, or otherwise considered unsuitable shall not be used in the compacted fill.

Soils of poor quality, such as those with unacceptable gradation, high expansion potential, or low strength shall be placed in areas acceptable to the Geotechnical Consultant or mixed with other soils to achieve satisfactory fill material.

B. Oversize Materials

Oversize material defined as rock, or other irreducible material with a maximum dimension greater than 12 inches in diameter, shall be taken offsite or placed in accordance with the recommendations of the Geotechnical Consultant in areas designated as suitable for rock disposal (Typical details for Rock Disposal are given on Plate SG-4).

Rock fragments less than 12 inches in diameter may be utilized in the fill provided, they are not nested or placed in concentrated pockets; they are surrounded by compacted fine grained soil material and the distribution of rocks is approved by the Geotechnical Consultant.

C. Laboratory Testing

Representative samples of materials to be utilized as compacted fill shall be analyzed by the laboratory of the Geotechnical Consultant to determine their physical properties. If any material other than that previously tested is encountered during grading, the appropriate analysis of this material shall be conducted by the Geotechnical Consultant as soon as possible.

D. Import

If importing of fill material is required for grading, proposed import material should meet the requirements of the previous section. The import source shall be given to the Geotechnical Consultant at least 2 working days prior to importing so that appropriate tests can be performed and its suitability determined.

V. FILL PLACEMENT AND COMPACTION

A. Fill Layers

Material used in the compacting process shall be evenly spread, watered, processed, and compacted in thin lifts not to exceed 6 inches in thickness to obtain a uniformly dense layer. The fill shall be placed and compacted on a horizontal plane, unless otherwise approved by the Geotechnical Consultant.

STANDARD GRADING SPECIFICATIONS

B. Moisture Conditioning

Fill soils shall be watered, dried back, blended, and/or mixed, as necessary to attain a relatively uniform moisture content at or slightly above optimum moisture content.

C. Compaction

Each layer shall be compacted to 90 percent of the maximum density in compliance with the testing method specified by the controlling governmental agency. (In general, ASTM D 1557-02, will be used.)

If compaction to a lesser percentage is authorized by the controlling governmental agency because of a specific land use or expansive soils condition, the area to received fill compacted to less than 90 percent shall either be delineated on the grading plan or appropriate reference made to the area in the soils report.

D. Failing Areas

If the moisture content or relative density varies from that required by the Geotechnical Consultant, the Contractor shall rework the fill until it is approved by the Geotechnical Consultant.

E. Benching

All fills shall be keyed and benched through all topsoil, colluvium, alluvium or creep material, into sound bedrock or firm material where the slope receiving fill exceeds a ratio of 5 horizontal to 1 vertical, in accordance with the recommendations of the Geotechnical Consultant.

VI. SLOPES

A. Fill Slopes

The contractor will be required to obtain a minimum relative compaction of 90 percent out to the finish slope face of fill slopes, buttresses, and stabilization fills. This may be achieved by either overbuilding the slope and cutting back to the compacted core, or by direct compaction of the slope face with suitable equipment, or by any other procedure that produces the required compaction.

B. Side Hill Fills

The key for side hill fills shall be a minimum of 15 feet within bedrock or firm materials, unless otherwise specified in the soils report. (See detail on Plate SG-5.)

C. Fill-Over-Cut Slopes

Fill-over-cut slopes shall be properly keyed through topsoil, colluvium or creep material into rock or firm materials, and the transition shall be stripped of all soils prior to placing fill. (see detail on Plate SG-6).

STANDARD GRADING SPECIFICATIONS

D. Landscaping

All fill slopes should be planted or protected from erosion by other methods specified in the soils report.

E. Cut Slopes

1. The Geotechnical Consultant should observe all cut slopes at vertical intervals not exceeding 10 feet.
2. If any conditions not anticipated in the preliminary report such as perched water, seepage, lenticular or confined strata of a potentially adverse nature, unfavorably inclined bedding, joints or fault planes are encountered during grading, these conditions shall be evaluated by the Geotechnical Consultant, and recommendations shall be made to treat these problems (Typical details for stabilization of a portion of a cut slope are given in Plates SG-2 and SG-3.).
3. Cut slopes that face in the same direction as the prevailing drainage shall be protected from slope wash by a non-erodible interceptor swale placed at the top of the slope.
4. Unless otherwise specified in the soils and geological report, no cut slopes shall be excavated higher or steeper than that allowed by the ordinances of controlling governmental agencies.
5. Drainage terraces shall be constructed in compliance with the ordinances of controlling governmental agencies, or with the recommendations of the Geotechnical Consultant.

VII. GRADING OBSERVATION

A. General

All cleanouts, processed ground to receive fill, key excavations, subdrains, and rock disposals must be observed and approved by the Geotechnical Consultant prior to placing any fill. It shall be the Contractor's responsibility to notify the Geotechnical Consultant when such areas are ready.

B. Compaction Testing

Observation of the fill placement shall be provided by the Geotechnical Consultant during the progress of grading. Location and frequency of tests shall be at the Consultants discretion based on field conditions encountered. Compaction test locations will not necessarily be selected on a random basis. Test locations may be selected to verify adequacy of compaction levels in areas that are judged to be susceptible to inadequate compaction.

C. Frequency of Compaction Testing

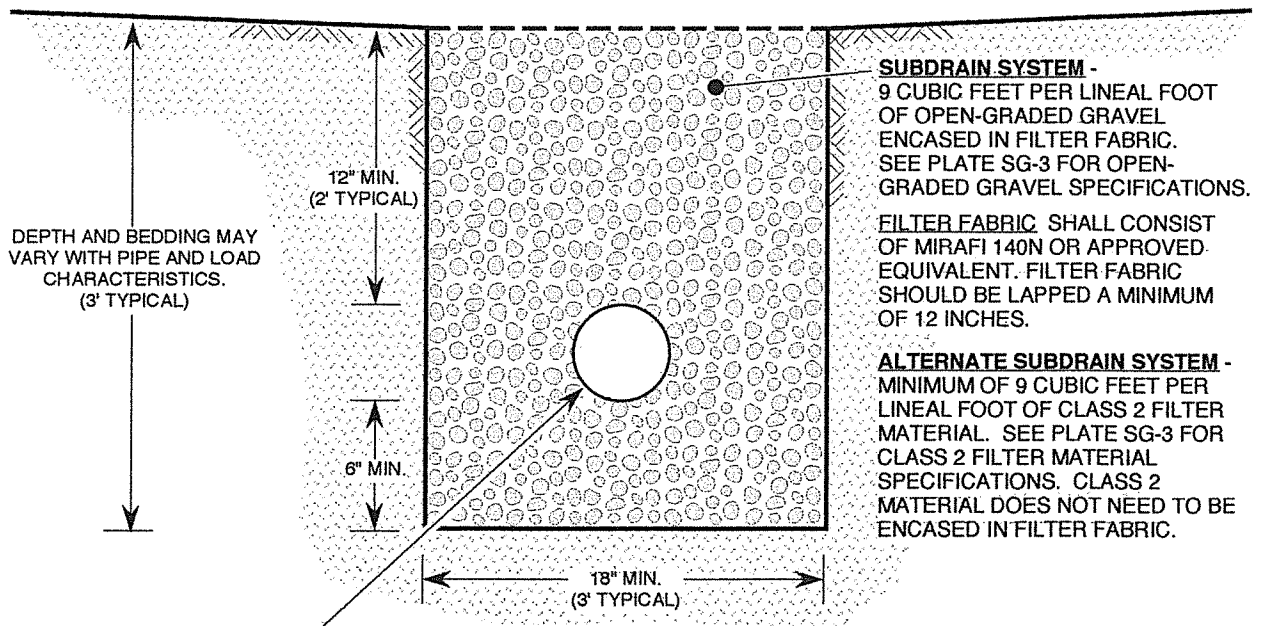
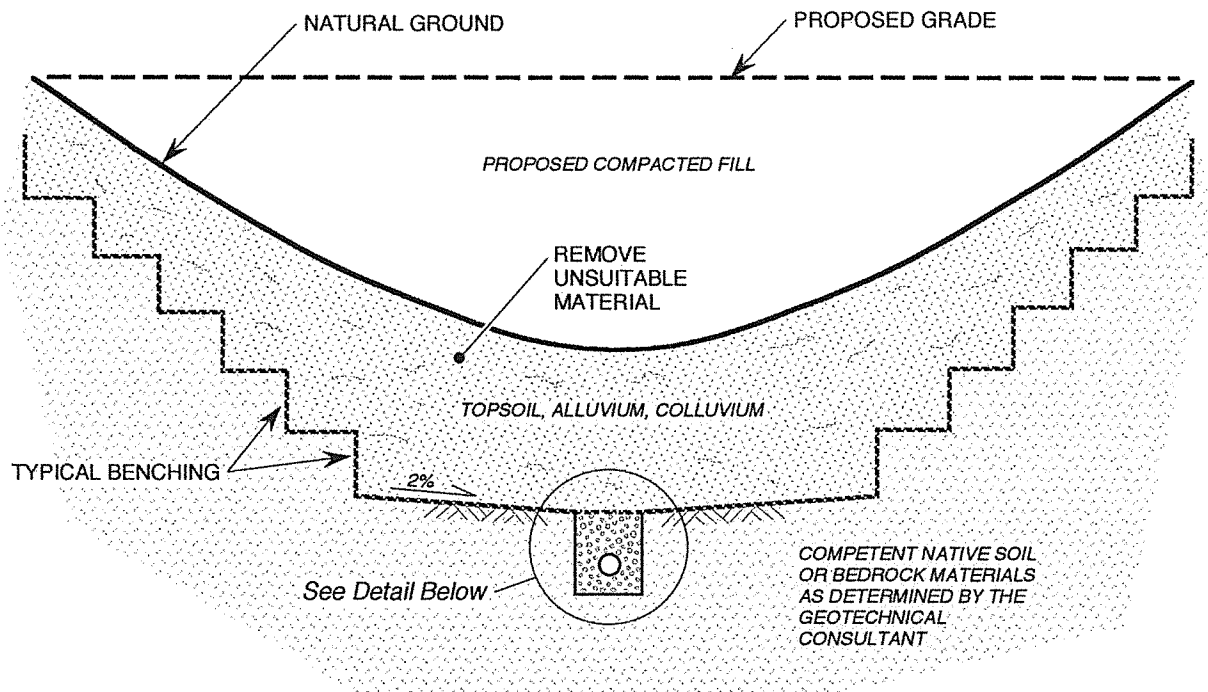
In general, density tests should be made at intervals not exceeding 2 feet of fill height or every 1000 cubic yards of fill placed. This criteria will vary depending on soil conditions and the size of the job. In any event, an adequate number of field density tests shall be made to verify that the required compaction is being achieved.

STANDARD GRADING SPECIFICATIONS

VIII. CONSTRUCTION CONSIDERATIONS

- A. Erosion control measures, when necessary, shall be provided by the Contractor during grading and prior to the completion and construction of permanent drainage controls.
- B. Upon completion of grading and termination of observations by the Geotechnical Consultant, no further filling or excavating, including that necessary for footings, foundations, large tree wells, retaining walls, or other features shall be performed without the approval of the Geotechnical Consultant.
- C. Care shall be taken by the Contractor during final grading to preserve any berms, drainage terraces, interceptor swales, or other devices of permanent nature on or adjacent to the property.

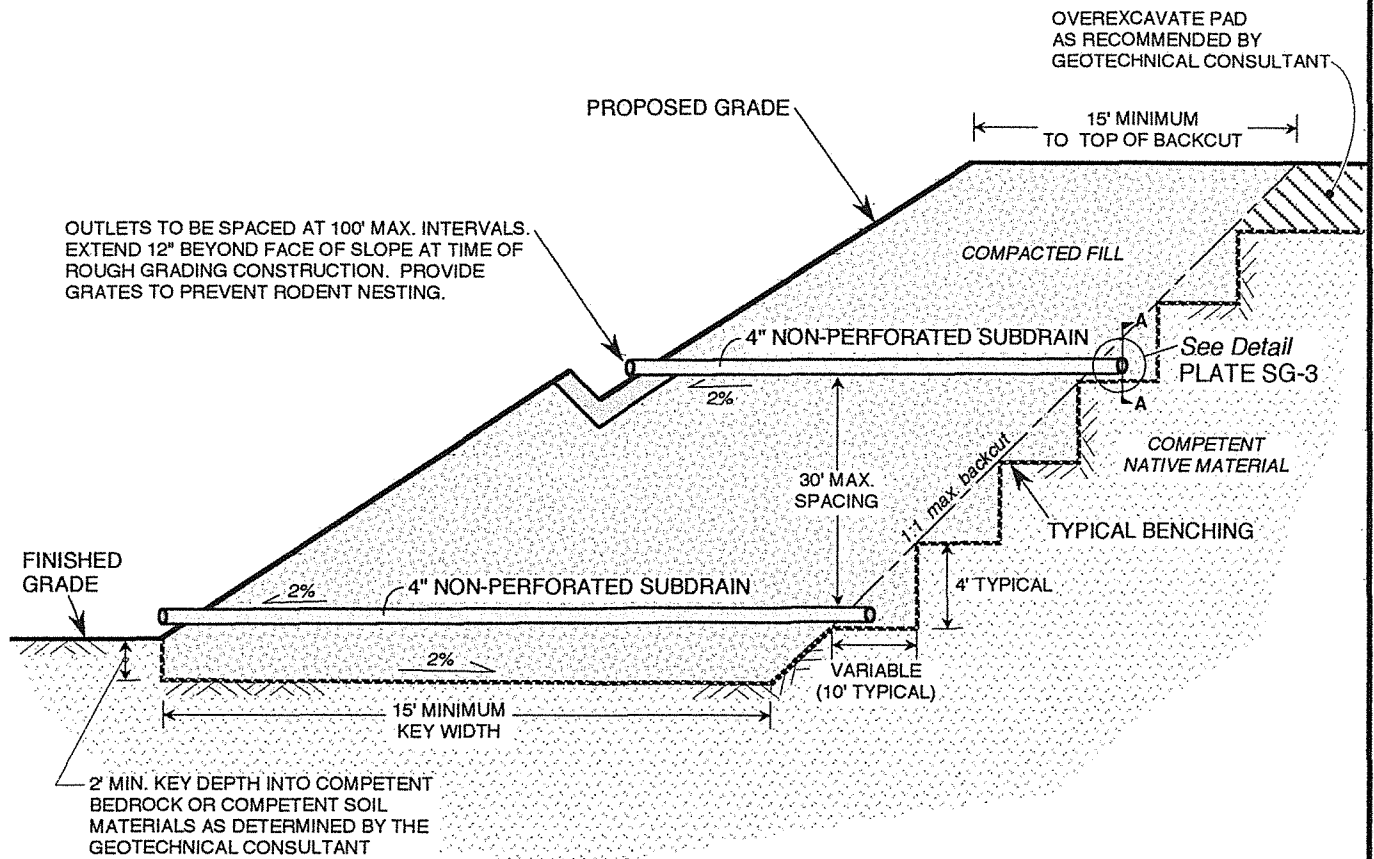
S:\BOILERS-WORK\REPORT INSERTS\STANDARD GRADING SPECS



MINIMUM 6-INCH DIAMETER PVC SCHEDULE 40, OR ABS SDR-35 WITH A MINIMUM OF EIGHT 1/4-INCH DIAMETER PERFORATIONS PER LINEAL FOOT IN BOTTOM HALF OF PIPE. PIPE TO BE LAID WITH PERFORATIONS FACING DOWN.

NOTES:

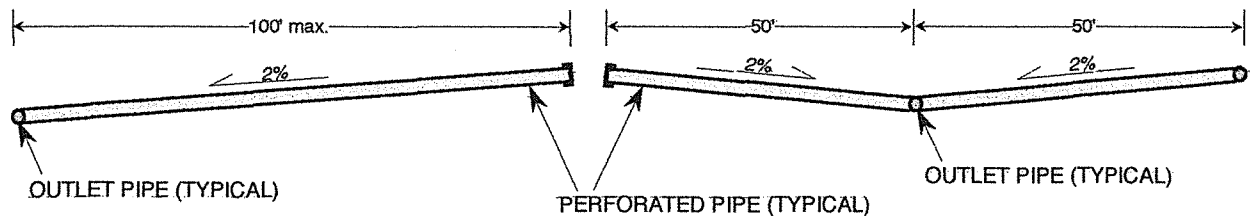
1. FOR CONTINUOUS RUNS IN EXCESS OF 500 FEET USE 8-INCH DIAMETER PIPE.
2. FINAL 20 FEET OF PIPE AT OUTLET SHALL BE NON-PERFORATED AND BACKFILLED WITH FINE-GRAINED MATERIAL.

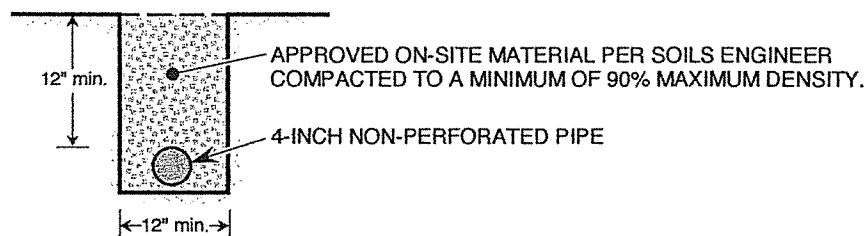
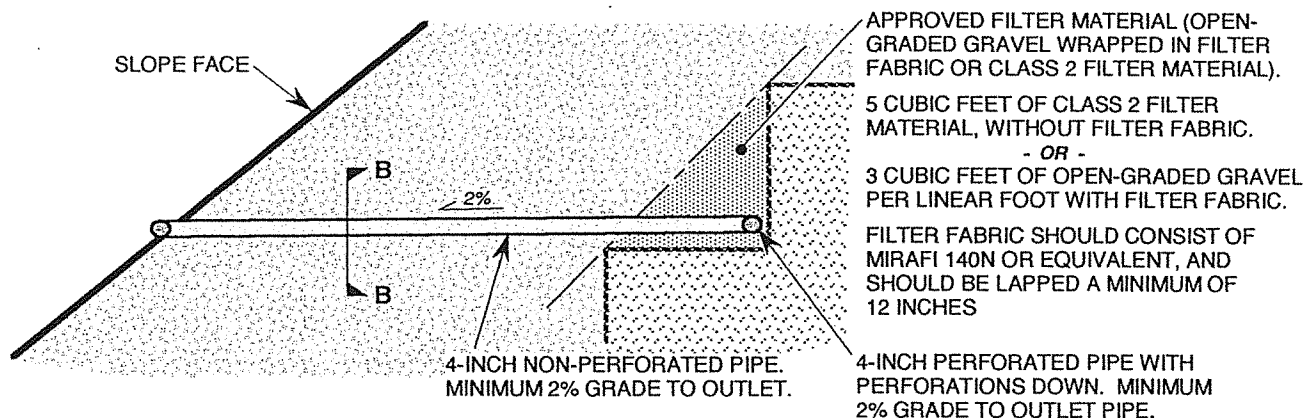


NOTES:

1. 30' MAXIMUM VERTICAL SPACING BETWEEN SUBDRAIN SYSTEMS.
2. 100' MAXIMUM HORIZONTAL DISTANCE BETWEEN NON-PERFORATED OUTLET PIPES. (See Below)
3. MINIMUM GRADIENT OF 2% FOR ALL PERFORATED AND NON-PERFORATED PIPE.

SECTION A-A (PERFORATED PIPE PROFILE)





SECTION B-B (OUTLET PIPE)

PIPE SPECIFICATIONS:

1. 4-INCH MINIMUM DIAMETER, PVC SCHEDULE 40 OR ABS SDR-35.
2. FOR PERFORATED PIPE, MINIMUM 8 PERFORATIONS PER FOOT ON BOTTOM HALF OF PIPE.

FILTER MATERIAL/FABRIC SPECIFICATIONS:

OPEN-GRADED GRAVEL ENCASED IN FILTER FABRIC.
(MIRAFI 140N OR EQUIVALENT)

ALTERNATE:

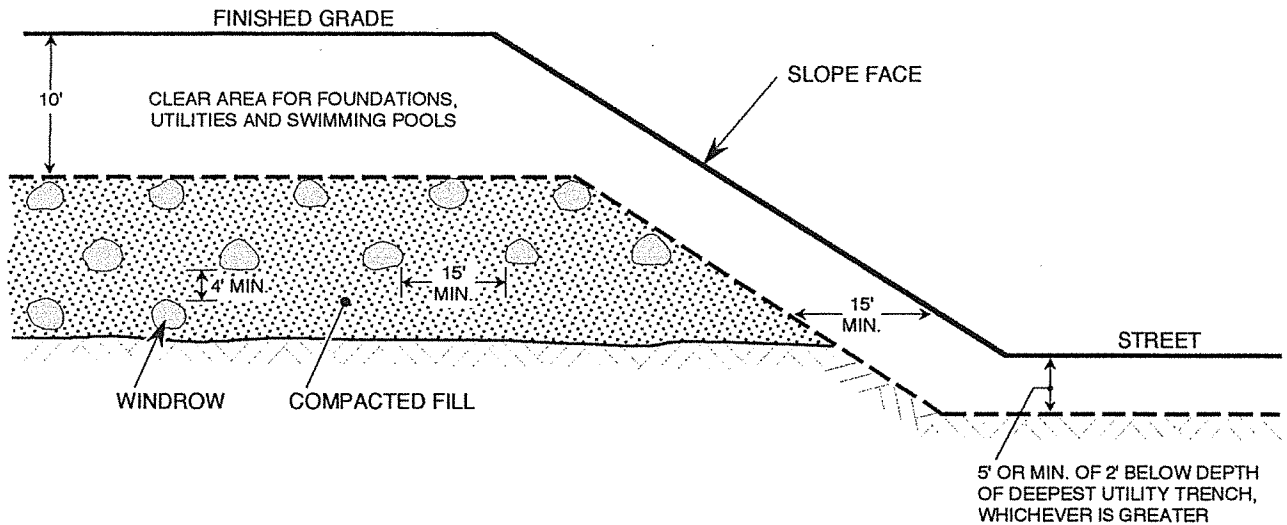
CLASS 2 PERMEABLE FILTER MATERIAL PER CALTRANS
STANDARD SPECIFICATION 68-1.025.

OPEN-GRADED GRAVEL

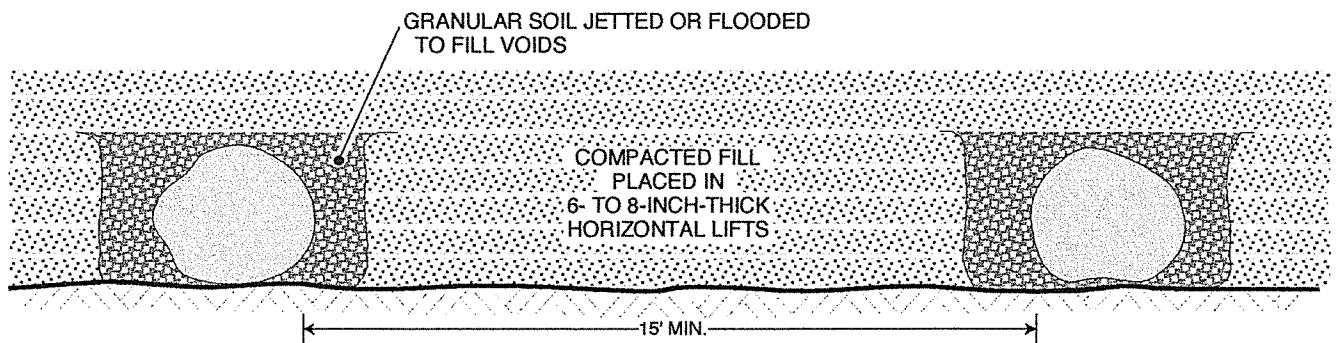
SIEVE SIZE	PERCENT PASSING
1 1/2-INCH	88 - 100
1-INCH	5 - 40
3/4-INCH	0 - 17
3/8-INCH	0 - 7
No. 200	0 - 3

CLASS 2 FILTER MATERIAL

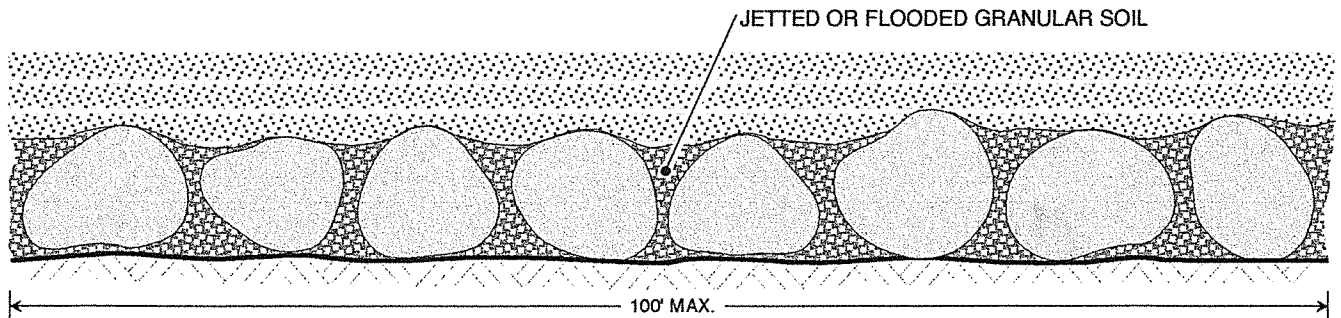
SIEVE SIZE	PERCENT PASSING
1-INCH	100
3/4-INCH	90 - 100
3/8-INCH	40 - 100
No. 4	25 - 40
No. 8	18 - 33
No. -30	5 - 15
No. -50	0 - 7
No. 200	0 - 3



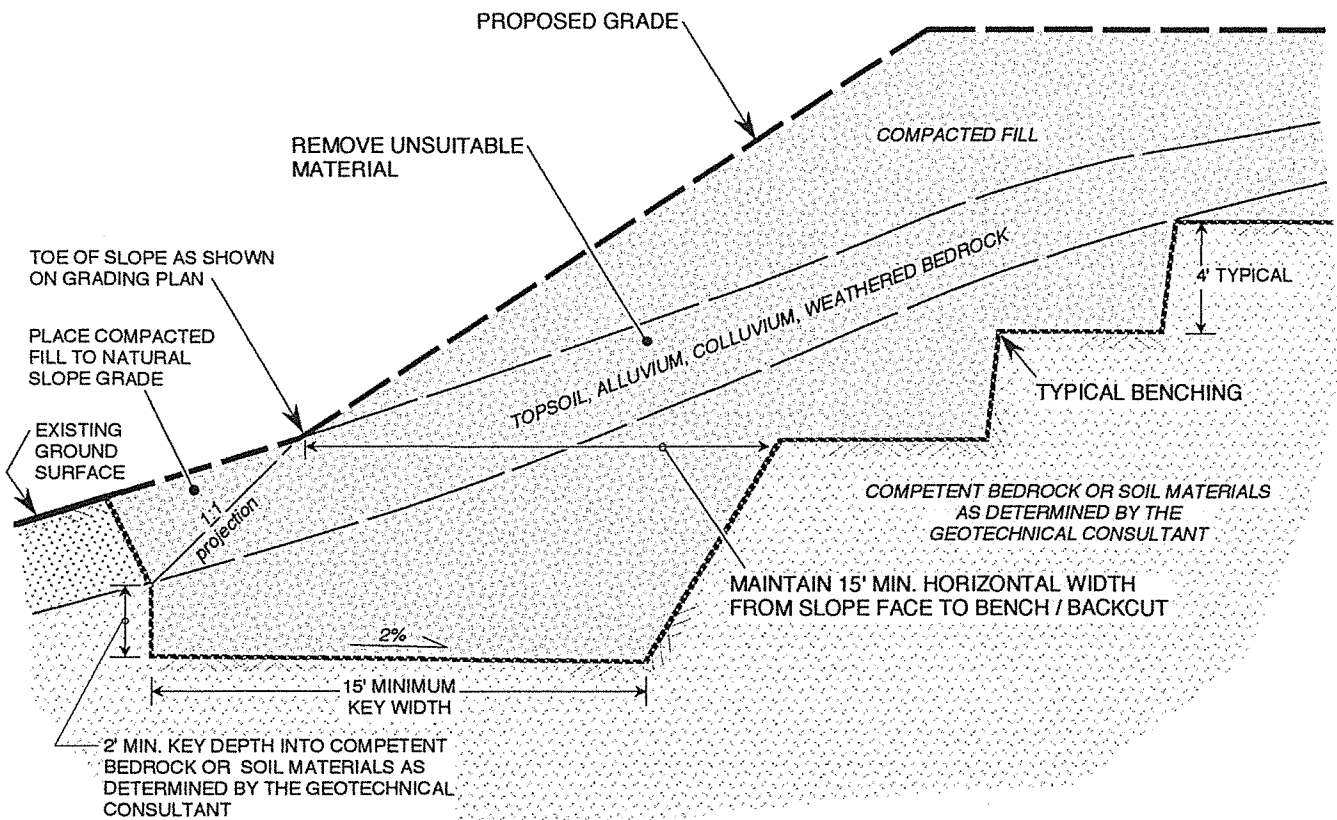
TYPICAL WINDROW DETAIL (END VIEW)



TYPICAL WINDROW DETAIL (PROFILE VIEW)



NOTE: OVERSIZE ROCK IS DEFINED AS CLASTS HAVING A MAXIMUM DIMENSION OF 12" OR LARGER



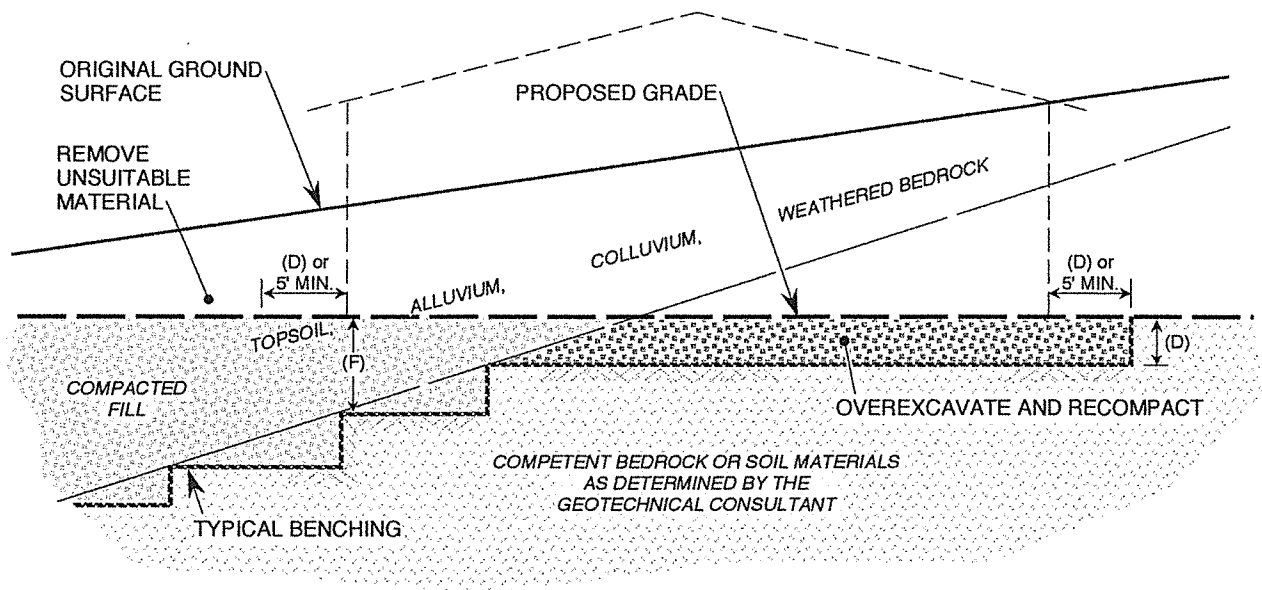
NOTES:

1. WHERE NATURAL SLOPE GRADIENT IS 5:1 OR LESS, BENCHING IS NOT NECESSARY; HOWEVER, FILL IS NOT TO BE PLACED ON COMPRESSIBLE OR UNSUITABLE MATERIAL.
2. SOILS ENGINEER TO DETERMINE IF SUBDRAIN IS REQUIRED.

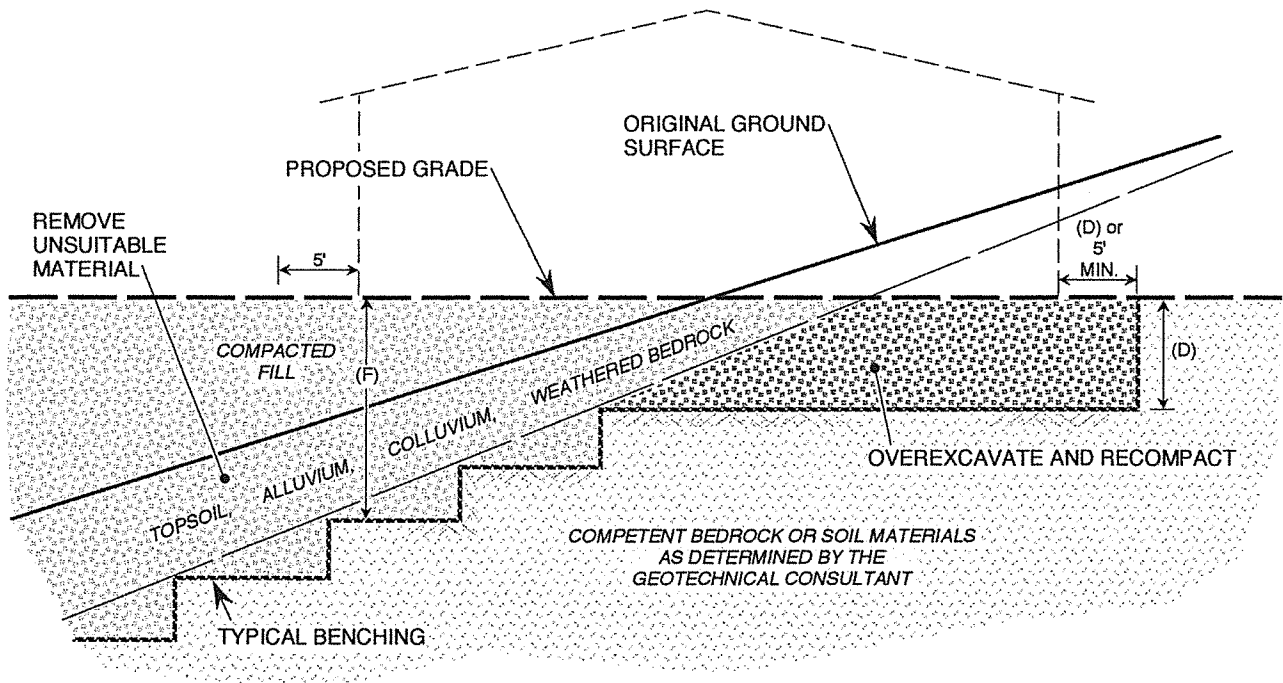


CUT LOT

UNSUITABLE MATERIAL EXPOSED IN PORTION OF CUT PAD



CUT-FILL TRANSITION LOT



MAXIMUM FILL THICKNESS (F)

FOOTING DEPTH TO 3 FEET

3 TO 6 FEET

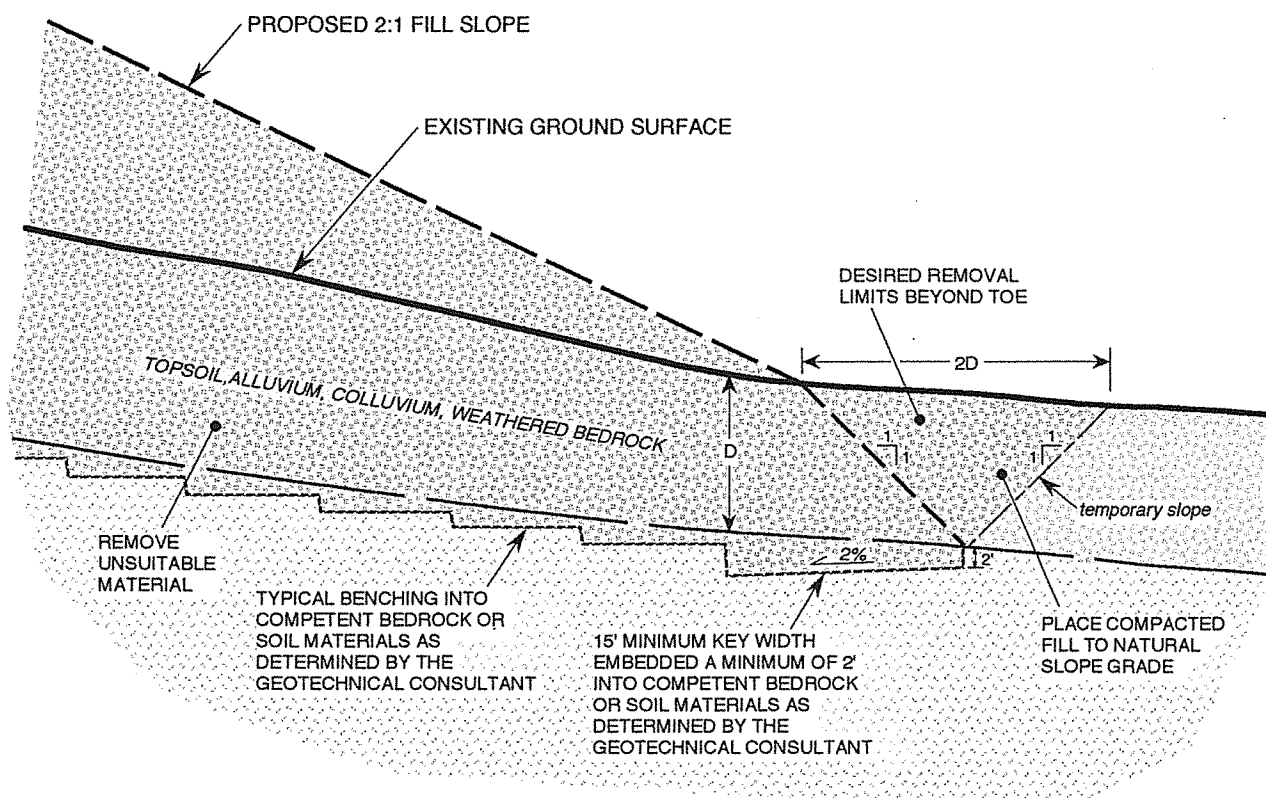
GREATER THAN 6 FEET

DEPTH OF OVEREXCAVATION (D)

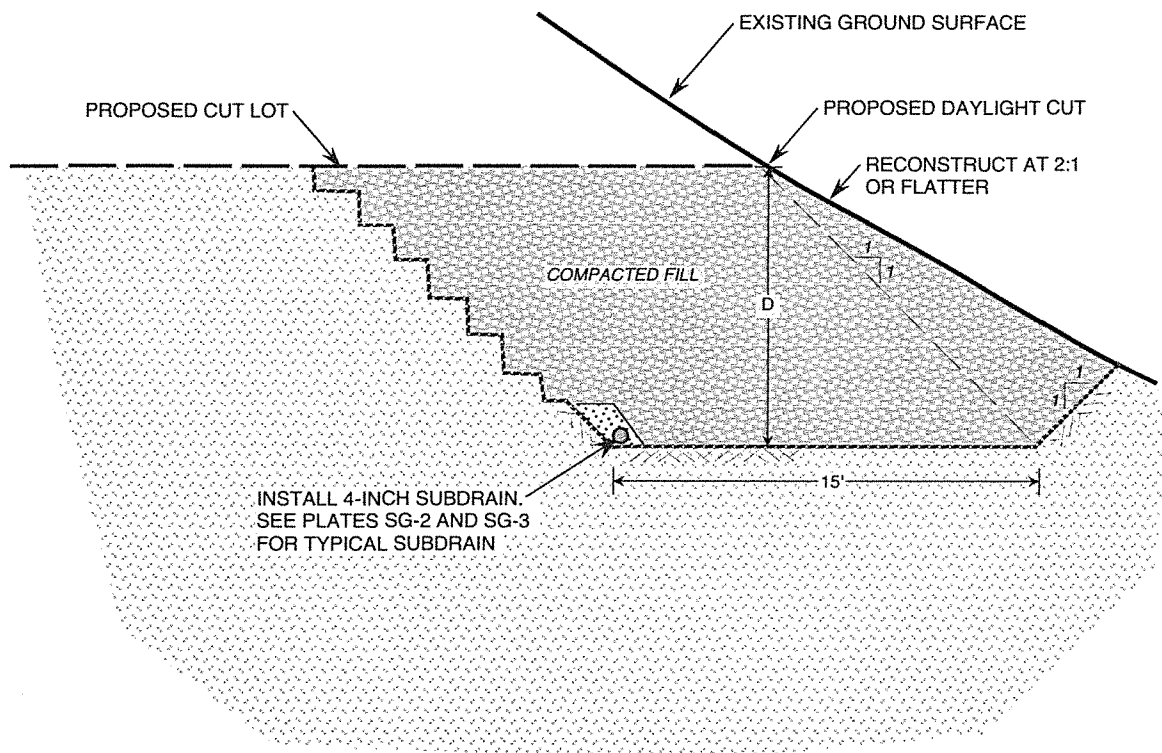
EQUAL DEPTH

3 FEET

1/2 THE THICKNESS OF DEEPEST FILL PLACED WITHIN THE "FILL" PORTION (F) TO 15 FEET MAXIMUM



D = RECOMMENDED DEPTH OF REMOVAL
PER GEOTECHNICAL REPORT



NOTE:

1. "D" SHALL BE 10 FEET MINIMUM OR AS DETERMINED BY SOILS ENGINEER.