Appendix F

Traffic Supporting Information

<u>Appendix F – Traffic Report Supporting Information</u>

| Section/Table | Page # |
|---|--------|
| Iteris Traffic Impact Analysis October 2021 | F-1 |

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Paramount Petroleum AltAir Renewable Fuels Project Traffic Impact Analysis

October 11, 2021

Submitted to: AltAir Paramount

J# 10985

Prepared by: **Iteris, Inc.**

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TABLE OF CONTENTS

| 1.0 | Introduction Project Location | |
|----------------------|--|----|
| 1.2 | Study Area | |
| 1.3 | Analysis Scenarios | |
| 2.0 | Environmental Setting | 7 |
| 2.2 | Existing Traffic Volumes | |
| 3.0 | Traffic Operations Analysis Methodology | 11 |
| 3.2 | Passenger Car Equivalent | 13 |
| 4.0 5.0 5.1 | Existing Conditions | 14 |
| 5.2 | Project Employee/Vendor Trip Generation | 15 |
| 5.3 | Project Rail Generation | 15 |
| 5.4 | Project Trip Distribution | 15 |
| 5.5 | Project Trip Assignment | 16 |
| 6.0 7.0 7.1 | Existing plus project conditions Existing plus Construction conditions Construction Trip Generation | 22 |
| 7.2 | Construction Trip Distribution and Assignment | 22 |
| 7.3 | Construction Period Intersection Operation Analysis | 23 |
| 8.0 9.0 9.1 | Project Area Collisions Project driveway analysis | 28 |
| 10.0 10.1 | Rail Delivery | |
| 11.0 12.0 13.0 | Blke and pedestrian facilities | 41 |
| Attachr Attachr | ment A –Traffic Count Data ment B – LOS Calculation Sheets ment C – collision Data 2017-2019 ment D –Queueing and Stacking Analysis | |
| Attachr | ment F – Analysis Assumntions | |

AltAir Renewable Fuels Project Traffic Impact Analysis

| TABLES | |
|---|----|
| Table 1: Lakewood Boulevard/Somerset Boulevard Historic vs. COVID-19 Period Volumes | 9 |
| Table 2: Intersection Level of Service Definitions | 11 |
| Table 3: Traffic Impact Analysis Thresholds | 12 |
| Table 4: Existing Intersection Peak Hour Level of Service | 13 |
| Table 5: Project Truck Trip Generation | 14 |
| Table 6: Project Employee Trip Generation | 15 |
| Table 7: Intersection Peak Hour Impact Analysis | 19 |
| Table 8: Intersection Peak Hour Impact Analysis with Potential Mitigation | 20 |
| Table 9: Intersection Peak Hour Impact Construction Period Analysis | 23 |
| Table 10: Primary Collision Factors (Percent of Total) | 27 |
| Table 11: Type of Collisions (Percent of Total) | 27 |
| Table 12: Collisions with Other Modes | 27 |
| Table 13: PM Peak Hour Stop Delay | 34 |
| Table 14: PM Peak Hour Stop Delay – Modified Signal Timing | 34 |
| Table 15: PM Peak Hour Upstream Block Time (percent) | 35 |
| Table 16: PM Peak Hour Upstream Block Time (percent) – Modified Signal Timing | 35 |
| Table 17: PM Peak Hour Storage Block Time (percent) | 35 |
| Table 18: PM Peak Hour Storage Block Time (percent) – Modified Signal Timing | 36 |
| | |
| | |
| FIGURES | |
| FIGURES | |
| Figure 1 – Project Location and Study Intersections | |
| Figure 2 – Intersection Lane Configurations | |
| Figure 3 – Existing Peak Hour Intersection Traffic Volumes | |
| Figure 4 – Project Trip Distribution | |
| Figure 5 – Project Trip Assignment | |
| Figure 6 – Existing Plus Project Peak Hour Intersection Volumes | |
| Figure 7 – Potential Natural Gas Pipeline Route | |
| Figure 8 – Temporary Construction Off-Site Parking Location | |
| Figure 9 – Existing Plus Construction Peak Hour Intersection Volumes | |
| Figure 10 – Project Driveway Access | |
| Figure 11: Inbound Storage Analysis | |
| Figure 12 – WSAB Southern Alignment and Bike Map | 39 |

1.0 INTRODUCTION

This traffic impact analysis has been prepared for the AltAir Revised Renewable Fuels Project (Project) that is expected to convert the Paramount Petroleum Refinery to manufacture only renewable fuels. This analysis evaluates the operations of the Project gate and study area intersections as directed by the City of Paramount staff as potentially being impacted by traffic from the Project.

The Paramount Facility resides on a 66-acre complex and includes refinery processing units, renewable fuel processing units, over 1.7 million barrels of product storage, truck loading and unloading facilities, and railcar loading and unloading facilities. The current renewable fuels operation has been in continuous production since January of 2016.

Raw materials will continue to be received by rail or by truck. Approximately 25 percent of the raw material may be shipped by barge to the Port of Los Angeles area, where it will be transferred to local tank storage prior to loading into trucks for transport to the Paramount Facility.

Logistics changes are summarized below, with more detailed descriptions following:

- Existing truck loading and unloading facilities (mainly racks previously used for asphalt) will be modified and relocated for the Renewable Fuels operation.
- Existing railcar loading and unloading facilities will be modified for the variety of raw materials and products that are needed for and produced by the Renewable Fuels operation.

Existing truck loading and unloading racks will be modified and relocated as part of the Renewable Fuels Project to accommodate the renewable fuels operation. In general, existing asphalt truck racks will be relocated and converted to feed, blendstock and product receipts and sales. No additional truck racks will be required at the Facility. Anticipated truck trips will increase compared to activity levels evaluated for the Renewable Fuels Project.

The following analysis of transportation conditions with the Project includes an analysis of employee, truck and rail volumes accessing the project site.

1.1 Project Location

The Project site is located at 14700 Downey Avenue, Paramount, California. The Project site is located immediately west of the City of Bellflower municipal boundary, and approximately one-quarter mile south of the City of Downey boundary. Regional access to the Project is provided by Interstates 605 and 710 which run north-south approximately two-and-one quarter miles east and west of the Revised Project, respectively. State Route 91 runs east-west and is located approximately two miles south of the Project. Interstate 105 runs east-west and is located about three-quarters of a mile north of the Project. **Figure 1** shows the project site location and study intersections.

1.2 Study Area

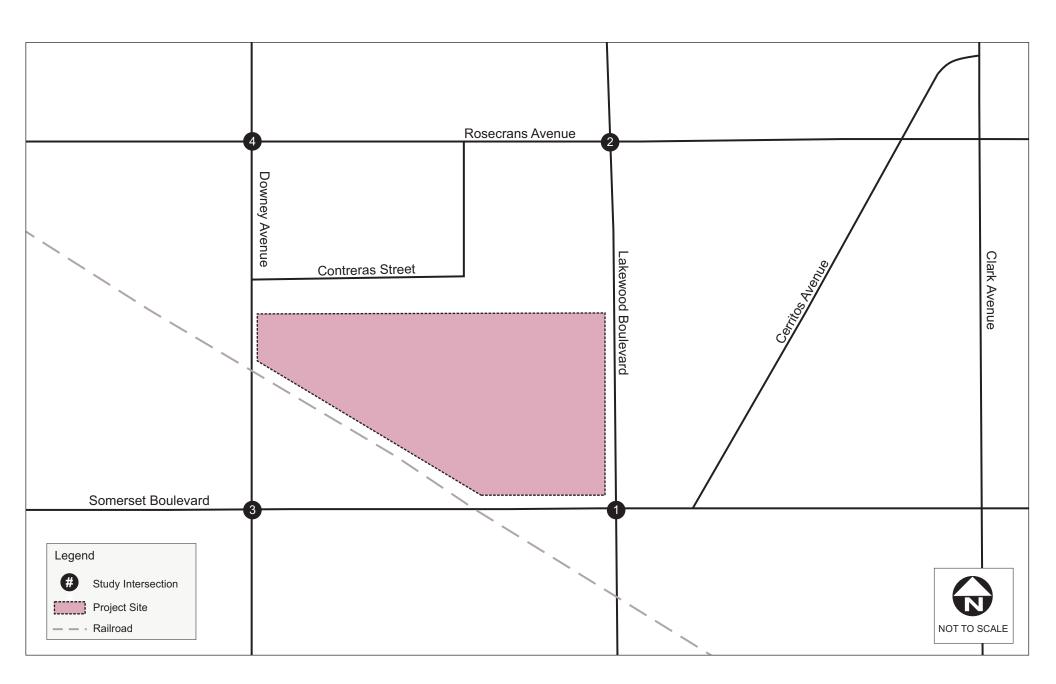
The study area for analysis is the four (4) signalized intersections immediately surrounding the project site and two site driveways. The study intersections are illustrated in the previously referenced **Figure 1** and are as follows:

- 1. Lakewood Boulevard/Somerset Boulevard;
- 2. Lakewood Boulevard/Rosecrans Avenue;
- 3. Downey Avenue/Somerset Boulevard; and
- 4. Downey Avenue/Rosecrans Avenue.

1.3 Analysis Scenarios

Traffic operations were evaluated for each of the following scenarios during the weekday peak hours during the periods of the a.m. (7:00 a.m. – 9:00 a.m.) and p.m. (4:00 p.m. – 6:00 p.m.):

- Existing Conditions
- Existing Plus Project Conditions
- Existing Plus Project Construction Conditions





2.0 ENVIRONMENTAL SETTING

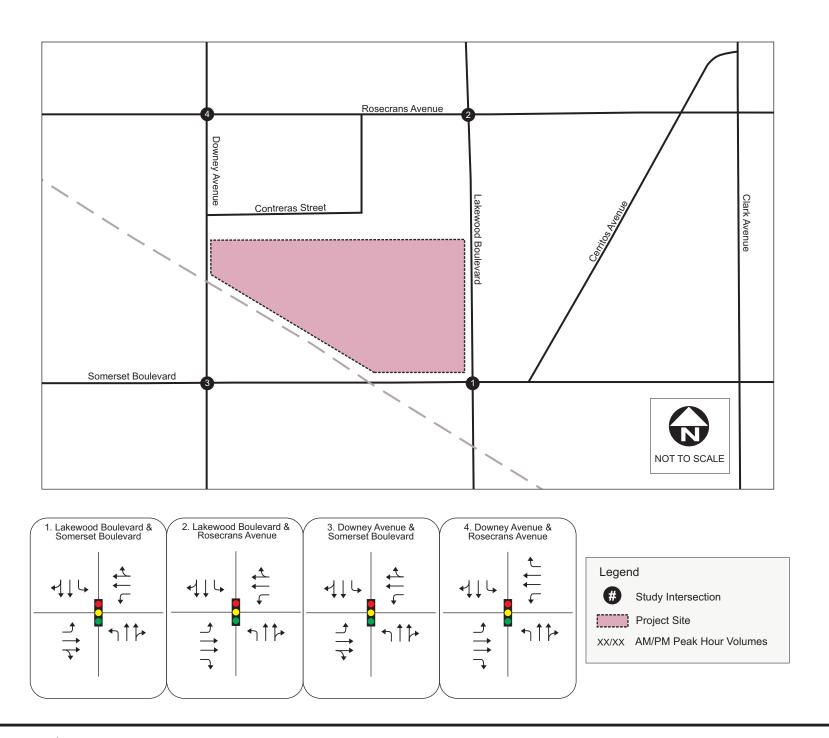
This section presents an overview of the roadways and existing traffic volumes within the study area.

2.1 Roadway Configurations

The Project site is bounded by Lakewood Boulevard, Somerset Boulevard, and Downey Avenue. The following is a description of area roadways.

- The Century Freeway (I-105) is an east-west freeway from the Los Angeles International Airport to Norwalk. It has four general-purpose lanes and one high-occupancy vehicle lane in the vicinity of the Project.
- The Artesia Freeway (SR-91) is an east-west freeway that extends from Gardena to the SR-60/I-215 interchange in Riverside. It has five general-purpose lanes and one high-occupancy vehicle lane in the vicinity of the Project.
- The Long Beach Freeway (I-710) is a north-south freeway that extends from Long Beach to Alhambra. It has five general-purpose lanes in the vicinity of the Project.
- The San Gabriel River Freeway (I-605) is a north-south freeway that extends from I-405 in Seal Beach to I-210 in Irwindale. It has six general-purpose lanes and one high-occupancy vehicle lane in the vicinity of the Project.
- Lakewood Boulevard is a north—south four-to-six lane major arterial. It has interchanges with both the SR-91 and I-105 freeways. The roadway is a Terminal Access Route Surface Transportation Assistance Act (STAA) which allows large trucks to operate. Lakewood Boulevard was a state highway whose maintenance was relinquished to the City of Bellflower adjacent to the Project site.
- Somerset Boulevard is an east-west secondary arterial. Somerset Boulevard does not have direct freeway access.
- *Downey Avenue* is a north-south secondary arterial. Downey Avenue has an interchange with SR-91.
- Rosecrans Boulevard is an east-west major arterial. Rosecrans Boulevard has interchanges with I-710 to the west and I-605 to the east. Rosecrans Avenue is designated a City of Paramount truck route from the west city limits to Century Boulevard.
- Andry Drive is an L-shaped private street belonging to Altair Paramount that connects Lakewood Boulevard and Somerset Boulevard and acts as the site driveway access. These access points are stop-controlled.

Figure 2 shows the existing intersection lane configurations.





2.2 Existing Traffic Volumes

Existing traffic volumes are based on vehicle turning movement counts during the a.m. (7:00 - 9:00) and p.m. (2:00 - 4:00) peak periods. All four of the locations were counted in June 2020 during the COVID-19 Pandemic. Due to the COVID-19 Pandemic, traffic volumes are depressed below their typical level for the preceding years. Therefore, to have a study that reflects typical conditions—as well as conditions more likely once the Project is operational—the volumes were modified with factors using a February 25, 2016 count at Lakewood Boulevard and Somerset Boulevard.

The a.m. and p.m. volumes for the four intersection approaches for the 2016 and 2020 counts were summed and compared. The percent differences between the two sets of counts at each intersection approach were used as factors to adjust each of the 2020 volumes to approximate pre-COVID intersection volume conditions in 2016. As shown in **Table 1**, volumes decreased approximately fifty percent in the a.m. peak hour and twenty percent in the p.m. peak hour.

| | Lakewood Blvd/ Somerset Blvd | | | | | | | | | | | | | |
|--------------|------------------------------|-----------|-------|-------|-------|--|--|--|--|--|--|--|--|--|
| | NB | SB | SB EB | | Total | | | | | | | | | |
| AM Peak Hour | | | | | | | | | | | | | | |
| 2016 | 1,174 | 1,221 | 614 | 787 | 3,796 | | | | | | | | | |
| 2020 | 561 | 660 | 288 | 368 | 1,877 | | | | | | | | | |
| Change | -52% | -46% | -53% | -53% | -51% | | | | | | | | | |
| | | PM Peak I | Hour | | | | | | | | | | | |
| 2016 | 1,355 | 965 | 560 | 1,156 | 4,036 | | | | | | | | | |
| 2020 | 1,097 | 634 | 464 | 996 | 3,191 | | | | | | | | | |

Table 1: Lakewood Boulevard/Somerset Boulevard Historic vs. COVID-19 Period Volumes

The percent change by peak hour by approach direction was applied to each of the intersections except the Lakewood Boulevard and Somerset Boulevard, since subsequent to the traffic volumes conducted for the study, the City of Bellflower provided additional traffic counts for the intersection of Lakewood Boulevard and Somerset Boulevard counted January 23, 2020 (prior to the COVID-19 Pandemic). This data set was used for the traffic analysis of the intersection of Lakewood Boulevard and Somerset Boulevard and had no adjustments made to the turning movement volumes.

-34%

-17%

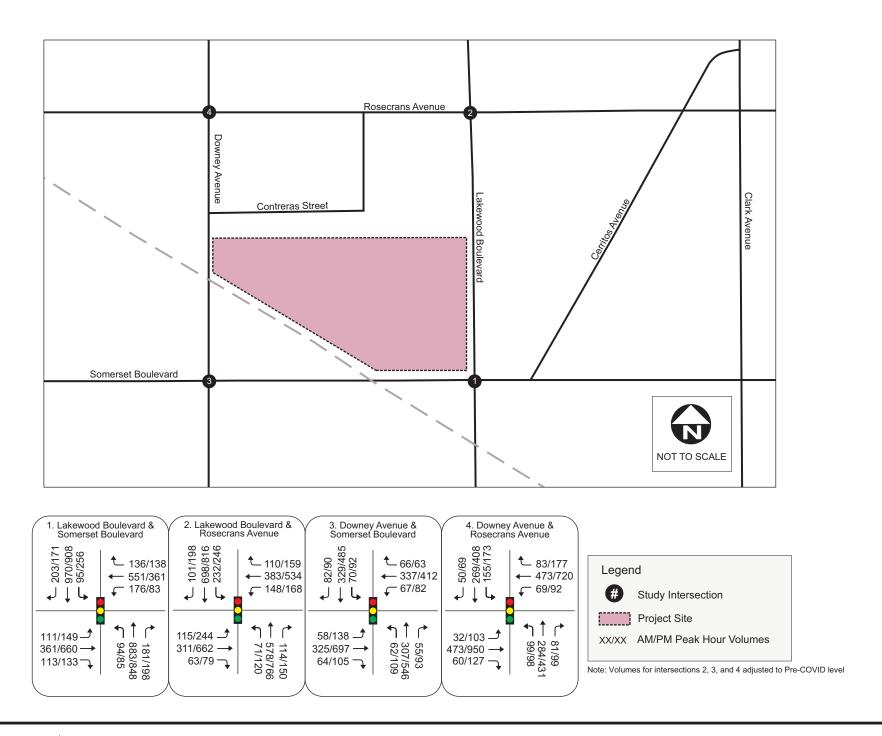
-14%

-21%

The resulting existing volumes used for the traffic analysis are shown in Figure 3.

-19%

Change





3.0 TRAFFIC OPERATIONS ANALYSIS METHODOLOGY

The quality of traffic operations is characterized using the concept of level of service (LOS). Level of service is defined by a range of grades from A (best) to F (worst). At intersections, LOS "A" represents relatively free operating conditions with little or no delay. LOS "F" is characterized by extremely unstable flow conditions and severe congestion with volumes at or near the intersection's design capacity. This results in long queues backing up from all approaches to intersections.

Consistent with the City of Paramount General Plan, this analysis uses the Intersection Capacity Utilization (ICU) methodology to determine LOS at the study intersections. The ICU method of analyzing intersection operations is a planning-level analysis based upon the critical flow ratio for the intersection. The critical flow ratio is the sum of green and clearance times required to serve the critical movements at the intersection divided by a reference cycle length. Critical movements are movements that cannot time concurrently and require the most time to serve demand. The sum of the critical phase volumes determine the overall critical volume that must be accommodated by the intersection and used to determine the intersection LOS.

Table 2 defines the LOS for intersection operating conditions.

Table 2: Intersection Level of Service Definitions

| Level Of Service | Description | Volume-to- Capacity Ratio (V/C) |
|------------------------|---|---------------------------------------|
| А | Excellent operation. All approaches to the intersection appear quite open, turning movements are easily made, and nearly all drivers find freedom of operation. | 0.600 |
| В | Very good operation. Many drivers begin to feel somewhat restricted within platoons of vehicles. This represents stable flow. An approach to an intersection may occasionally be fully utilized and traffic queues start to form. | 0.601 - 0.700 |
| С | Good operation. Occasionally drivers may have to wait more than 60 seconds, and back- ups may develop behind turning vehicles. Most drivers feel somewhat restricted. | 0.701 - 0.800 |
| D | Fair operation. Cars are sometimes required to wait more than 60 seconds during short peaks. There are no long-standing traffic queues. | 0.801 – 0.900 |
| E | Poor operation. Some long-standing vehicular queues develop on critical approaches to intersections. Delays may be up to several minutes. | 0.901 – 1.000 |
| F | Forced flow. Represents jammed conditions. Backups form locations downstream or on the cross street may restrict or prevent movement of vehicles out of the intersection approach lanes; therefore, volumes carried are not predictable. Potential for stop and go type traffic flow. | >1.000 |

Source: Highway Capacity Manual, Transportation Research Board, Washington, D.C., 1994.

The City of Paramount requires that any new development or redevelopment in the city that is expected to generate more than 500 new trips per day must conduct a Traffic Impact Analysis (TIA). Performance measure of significance (significance in terms of City policy, not CEQA significance) in the TIA is if the Project related increase in the volume-to-capacity (v/c) ratio for intersection equals or exceeds the thresholds established by the City. **Table 3** shows the City's traffic impact analysis thresholds. When a new Project results in a significant impact, improvements to the intersection would be required by the City to restore or reduce the v/c ratio to the operating levels of services (as measured using the v/c ratio that existed prior to the Project's implementation). While the CEQA Guidelines: California Code, Public Resources Code Section 21099(b)(2) prevents lead agencies from relying on impacts to vehicle delay to determine that CEQA traffic impacts are significant, the City can require intersection operations improvements outside of CEQA.

| Level Of Service | Volume-to-Capacity Ratio | Incremental Increase |
|---------------------|-----------------------------|-------------------------|
| С | 0.701-0.800 | 0.040 or more |
| D | 0.801-0.900 | 0.020 or more |
| E/F | 0.901-more | 0.010 or more |

Table 3: Traffic Impact Analysis Thresholds

3.1 Queuing and Stacking Analysis

Due to the close proximity of the site driveways to the intersection of Lakewood Boulevard/Somerset Boulevard, a focused queuing and stacking analysis of intersection of Lakewood Boulevard/Somerset Boulevard along with the Project site gates, the Andry Drive intersection with Lakewood Boulevard and Somerset Boulevard and the future West Santa Ana Branch at-grade crossings were analyzed in a traffic model to forecast the delay, queuing and stacking of vehicles under existing and with-Project conditions.

Inbound gate queuing analysis was conducted based on the peak day gate demand, inbound gate processing time and the amount of available on-site storage for vehicle waiting for the inbound gate.

Analysis was also conducted with the software Synchro 11 and SimTraffic. Synchro is a macroscopic analysis and optimization software application. Synchro supports the Highway Capacity Manual's (HCM) 6th Edition, 2010 and 2000 for signalized intersections, unsignalized intersections and roundabouts. The primary measure of performance from Synchro output reported in this analysis is the HCM intersection average control delay and the resulting level of service.

SimTraffic is a microscopic model where each vehicle, including trucks, in the traffic system is individually tracked through the model and comprehensive operational measures of effectiveness are collected on every vehicle during each 0.1-second of the simulation. Unlike Synchro, SimTraffic

measures the full impact of queuing and blocking. The measures of performance from SimTraffic are average stop delay (by movement), upstream block time (percent) and storage block time (percent).

The results of the queuing and stacking analysis are in Section 9.1.

3.2 Passenger Car Equivalent

A passenger car equivalent (PCE) represents the number of passenger cars that would use the same amount of highway capacity as the vehicle being considered under the prevailing roadway and traffic conditions.

Trucks are larger and, more importantly, accelerate more slowly than passenger cars, and thus have a greater effect on traffic flow than passenger cars. On level terrain and in congested conditions trucks may be equivalent to two to four passenger cars in terms of their impact on traffic flow based on the United States Department of Transportation - Federal Highway Administration Comprehensive Truck Size and Weight Study. In Table IX-2: Vehicle Passenger Car Equivalents on Urban Highway of that study, on congested "Other Principle Arterial" roadways (such as Lakewood Boulevard) for 40-foot and 80-foot trucks with vehicle weight-to-horsepower ratio (pounds/horsepower) of 150 and 200 is a PCE of 2.0 and a ratio of 250 is a PCE of 3.0 and a PCE ratio of 2.0. In order to have a conservative analysis of traffic impacts of the Project, a PCE value of 3.0 was used for tanker trucks during operations. A PCE value of 2.0 was applied to construction-period vehicle and employee shuttle due their shorter length.

4.0 EXISTING CONDITIONS

A level of service analysis was conducted to evaluate existing intersection operations during the a.m. and p.m. peak hours at the four (4) study intersections. **Table 4** summarizes the existing LOS at the study intersections. LOS calculation sheets are provided in **Attachment B**.

Table 4: Existing Intersection Peak Hour Level of Service

| Intersection - | | AM Pea | ak Hour | PM Peak Hour | | | |
|----------------|---------------------------------------|--------|---------|--------------|-------|--|--|
| | | LOS | V/C | LOS | v/c | | |
| 1 | Lakewood Boulevard/Somerset Boulevard | D | 0.810 | D | 0.887 | | |
| 2 | Lakewood Boulevard/Rosecrans Avenue | В | 0.687 | E | 0.910 | | |
| 3 | Downey Avenue/Somerset Boulevard | Α | 0.430 | В | 0.660 | | |
| 4 | Downey Avenue/Rosecrans Avenue | Α | 0.502 | С | 0.729 | | |

Notes:

LOS = Level of Service.

V/C = Volume to Capacity Ratio

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¹ https://www.fhwa.dot.gov/reports/tswstudy/

As shown in **Table 4**, a majority of the study intersections are operating at LOS D or better during both peak hour conditions, with the exception of the Lakewood Boulevard/Rosecrans Avenue intersection, which operate at LOS E during the p.m. peak hour.

5.0 PROJECT TRAFFIC

This section defines the traffic generated by the Project in a two-step process including trip generation and trip distribution. The Facility currently and would continue to operates 24 hours per day, 365 days per year. The existing work force at the Facility is expected to increase by about 30 permanent employees.

5.1 Project Truck Trip Generation

Project truck trip generation is based on maximum utilization of the racks for loading and unloading of products and is considered a peak capacity condition. Under the CEQA baseline conditions there were 156 truck round trips per day. Under the maximum utilization of rack capacity project conditions there would be 540 truck round trips per day.

For the peak hour Project intersection analysis, 23 inbound and 23 outbound truck trips were used. This is based on the hourly maximum rack utilization amount of 540 truck round trips divided by 24 hours—22.5 truck arrivals and departures from the site rounded up to 23.

Existing traffic from the AltAir Facility the day the traffic counts were taken at the Lakewood/Somerset intersection count (January 23, 2020) based on the AltAir gate logs showed one inbound truck in the a.m. peak hour and two inbound trucks in the p.m. peak hour. This analysis assumes those trucks left within the peak hour and therefore there was one outbound truck in the a.m. peak hour and two outbound trucks in the p.m. peak hour.

The incremental peak hour Project trip generation was analyzed as 22 inbound and 22 outbound trucks in the a.m. peak hour and 21 inbound and 21 outbound trucks in the p.m. peak hour as shown in **Table 5.** Truck trips were added to the existing intersection volume in the traffic analysis using a passenger car equivalency (PCE) factor of 3.0 per vehicle to account for the larger vehicle size.

Site Truck Trip Generation **Peak Hour Total Site With Project Incremental Project Total Incremental Existing Conditions PCE Trips*** Inbound Outbound Inbound **Outbound** Inbound Inbound **Outbound** Inbound AM Peak 23 22 1 1 23 22 66 66 Hour PM Peak 2 2 23 23 21 21 63 63

Table 5: Project Truck Trip Generation

Note: PCE value of $3.0\ used$ for traffic analysis

5.2 Project Employee/Vendor Trip Generation

Under existing conditions there are and 100 employees. Under Project conditions the facility is expect to increase to 130 site employees. Those 30 employees are forecast to generate 74 daily one-way trips using the Institute of transportation Engineers (ITE) Trip Generation Handbook code 140 (Manufacturing) daily rate of 2.47 vehicle trips per employee.

The workers in existing and under Project conditions are predominately 12-hour shift worker (either 4:30 a.m. to 4:30 p.m. or 4:30 p.m. to 4:30 a.m. For the Project analysis, some activity is assumed in addition to existing conditions levels of site auto trips in the a.m. and p.m. peak hours: five of the employee trips would be incremental office and maintenance staff arriving between 7 a.m. and 8 a.m. and leaving at 5 p.m. and 10 inbound and outbound shift workers are assumed in the p.m. peak hour.

The assumptions for site employee trip generation activity from the Project are shown in Table 6.

 Trip Generation

 Autos

 Inbound
 Outbound

 AM Peak Hour
 5
 0

 PM Peak Hour
 10
 15

Table 6: Project Employee Trip Generation

5.3 Project Rail Generation

Under baseline conditions 33 rail cars visit the site per day with 50 rail cars under Project conditions for an incremental change of 17 rail cars per day.

5.4 Project Trip Distribution

Auto trips and truck trips were distributed differently due to the location of the Project driveways.

Employee vehicles access the facility from the main gate on Downey Boulevard. Auto trips were assumed to be split 50/50 from the north and south along Downey Avenue, with access to I-105 and SR-91 respectively.

Access to the Project site for trucks could be from the south of the site or north of the site based on the Project's proximity to Lakewood Boulevard and its access to the I-105 and SR-91 freeways. Both freeways provide regional access, including to the Port of Los Angeles where an estimated 25 percent of the raw material may be shipped via barge. Other truck deliveries would be from local tank storage areas in the Los Angeles region. Therefore, inbound truck trip distribution was assumed to be 50/50 from the north and south along Lakewood Boulevard.

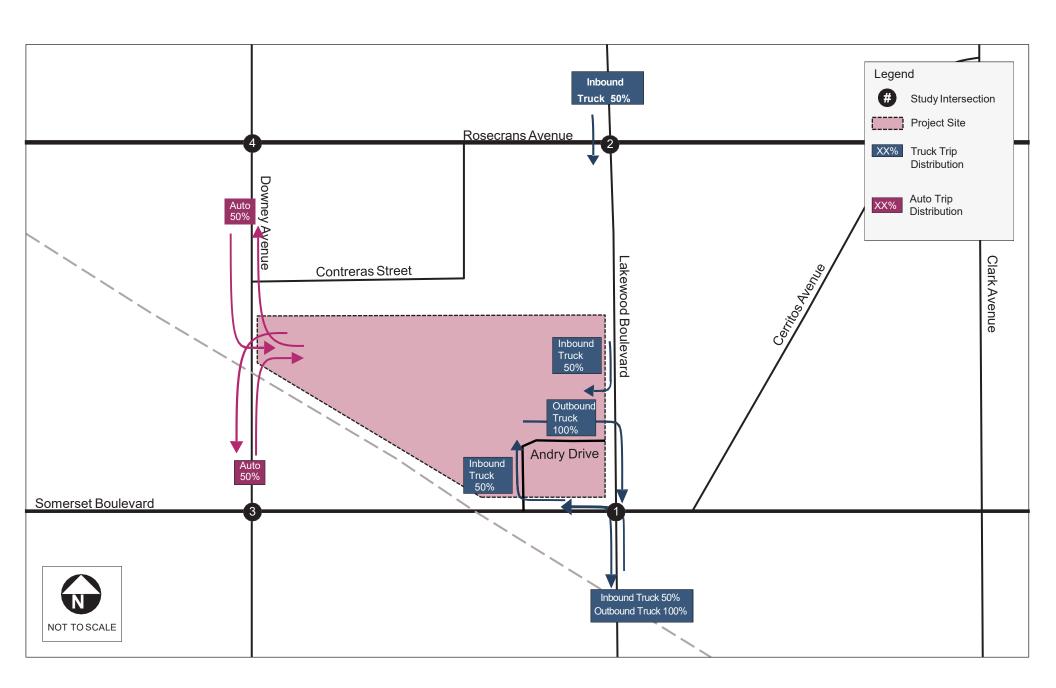
For outbound trips, all were assumed to exit the Andry Drive/Lakewood Boulevard driveway and proceed southbound. The raised median along Lakewood Boulevard prevents trucks exiting Andry Drive at

Lakewood Boulevard from turning north (left) and would require them to turn south (right). The analysis did not assume existing vehicles utilizing the Andry Drive/Somerset Boulevard driveway due to the unprotected left-turn required. The project would need to install signage for outbound vehicles to ensure their utilization of the Lakewood Boulevard driveway.

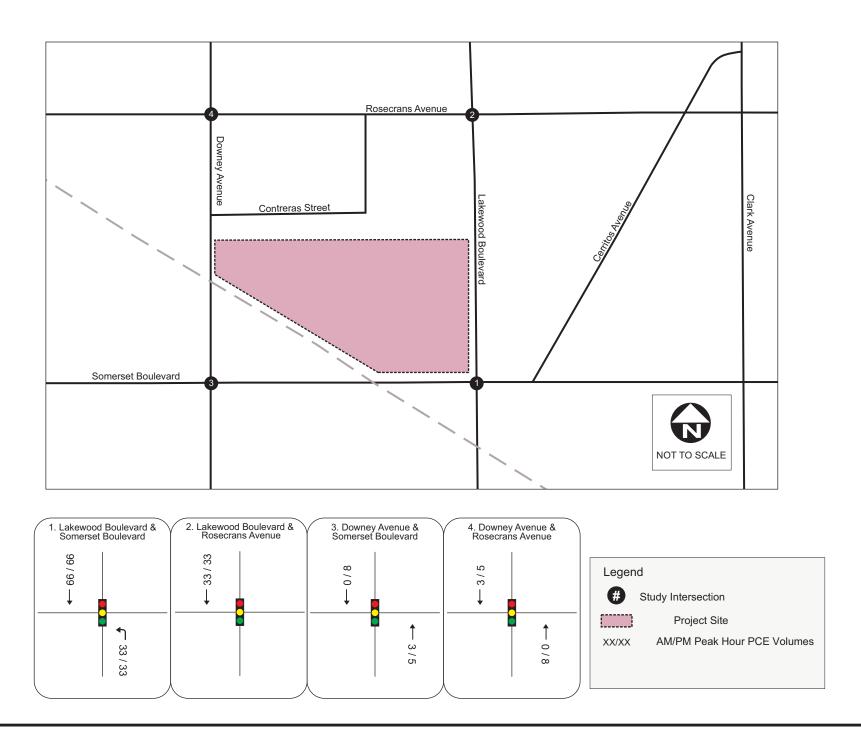
Figure 4 shows the trip distribution pattern for auto and truck trips forecasted for the Project in the study area.

5.5 Project Trip Assignment

Trip generated by the Project, as shown in **Tables 5** and **6**, were assigned to the surrounding roadway system based on the distribution patterns to estimate the Project-related peak-hour traffic at each of the study intersections. **Figure 5** shows the a.m. and p.m. peak hour Project trip assignment for the Project.









6.0 EXISTING PLUS PROJECT CONDITIONS

Existing plus Project conditions were developed by adding distributed Project trips, as a result of the Project, to existing volumes. A level of service analysis was conducted to evaluate existing plus Project intersection operations during the a.m. and p.m. peak hours at the study intersections. **Figure 6** illustrates the peak hour existing plus Project turning movement volumes. **Table 7** compares the existing plus Project volume to capacity ratios to existing conditions to determine potential impacts. As shown no location is forecast to be adversely impacted by the Project. Analysis calculation worksheets are included in **Attachment B**.

Table 7: Intersection Peak Hour Impact Analysis

| Existing | | | | | Existing plus Project | | | | De | on | | |
|--------------|---------------------------------------|---|-------------|-----|-----------------------|-----|-------------|-----|-------------|-------|----------|--------|
| t a consider | | | Peak our | | Peak our | | Peak our | | Peak our | Chang | e in V/C | luo ia |
| | Intersection | | V/C | LOS | V/C | LOS | V/C | LOS | v/c | AM | PM | lmp. |
| 1 | Lakewood Boulevard/Somerset Boulevard | D | 0.810 | D | 0.887 | D | 0.850 | D | 0.887 | 0.040 | 0.000 | Yes |
| 2 | Lakewood Boulevard/Rosecrans Avenue | В | 0.687 | Е | 0.910 | В | 0.687 | E | 0.910 | 0.000 | 0.000 | No |
| 3 | Downey Avenue/Somerset Boulevard | Α | 0.430 | В | 0.660 | Α | 0.430 | В | 0.661 | 0.000 | 0.001 | No |
| 4 | Downey Avenue/Rosecrans Avenue | Α | 0.502 | С | 0.731 | Α | 0.502 | С | 0.731 | 0.000 | 0.002 | No |

Notes:

LOS = Level of Service.

V/C = Volume to Capacity Ratio

The volume to capacity ratios in the ICU analysis are unchanged with the Project at intersection #1 in the p.m. peak hour, Intersection #2 in the a.m. and p.m. peak hours and Intersections #3 and #4 in the a.m. peak hours since the Project would not add additional volume to a critical movement and is therefore not included in the ICU calculation of volume to capacity ratio.

Based on the analysis, Intersection #1 Lakewood Boulevard/Somerset Boulevard would exceed the City's traffic impact analysis threshold for incremental increase in volume-to-capacity ratio in the a.m. peak hour. To address the identified impact, the City could require the striping of the southbound right-turn lane. The outside southbound shared through/right turn lane is approximately 23 feet wide and operates as two de facto lanes. The intersection analysis is based on the lane striping conditions, and therefore identified a potential impact which may not have an effect on the practical operation of the intersection. Nevertheless, the City Public Works should assess the location for potential southbound right-turn lane striping considering factors such as the access management of adjacent driveways and transit operations.

The results of this potential mitigation are shown in **Table 8**. As shown, the striping of the southbound intersection approach as one left-turn lane, two through lanes and a right turn lane would reduce the ICU volume-to-capacity ratio project increment to less than the City's traffic impact analysis threshold.

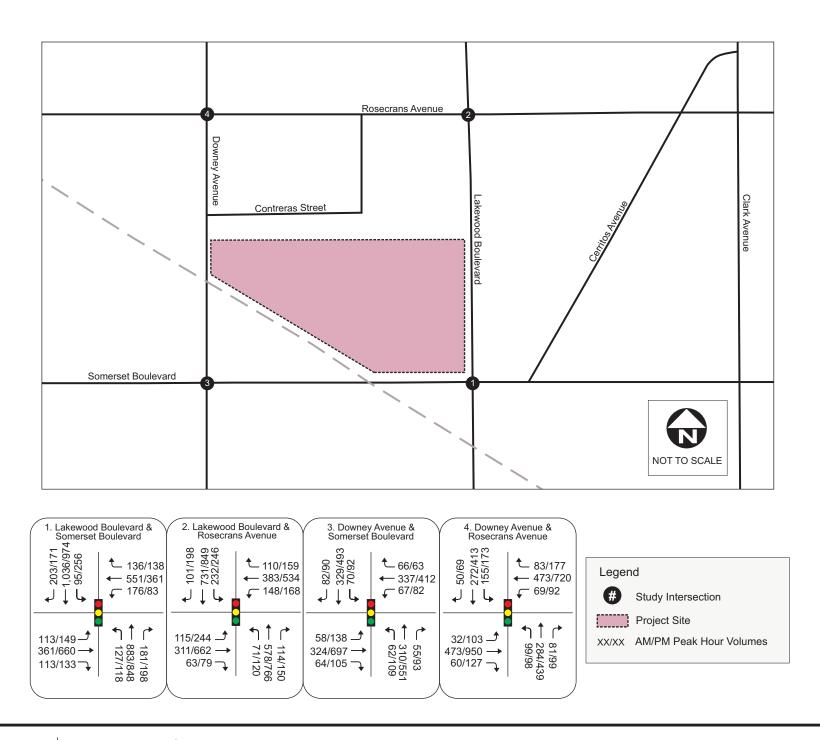
Table 8: Intersection Peak Hour Impact Analysis with Potential Mitigation

| | | Existing | | | Existing plus Project Plus Mitigation | | | | Det | n | | |
|--------------|---------------------------------------|-----------------|-------|-----------------|--|-----------------|-------|-----------------|-------|---------------|-------|--------|
| Intersection | | AM Peak Hour | | PM Peak Hour | | AM Peak Hour | | PM Peak Hour | | Change in V/C | | lue is |
| | | LOS | v/c | LOS | V/C | LOS | V/C | LOS | V/C | AM | PM | lmp. |
| 1 | Lakewood Boulevard/Somerset Boulevard | D | 0.810 | D | 0.887 | С | 0.787 | D | 0.887 | -0.023 | 0.000 | No |

Notes:

LOS = Level of Service.

V/C = Volume to Capacity Ratio





7.0 EXISTING PLUS CONSTRUCTION CONDITIONS

Full construction and commissioning activities will take place over a two- to three-year timeframe. Demolition activities include relocation of loading and unloading racks and buildings, removal of crude unit, asphalt facilities and other existing equipment as needed to make room for new equipment installation. Construction activities include modifications to Unit A and the construction of new units, including the Pretreatment Unit, Hydrogen Generation Unit, and new equipment required for Unit B and the support units and utilities.

The Project will add one natural gas supply pipeline. The potential pipeline route provided by SoCalGas to the Facility will be approximately 3.7 miles of new pipeline that would extend north from Lakewood Boulevard to Somerset Boulevard, and enter the Facility from east on Somerset Boulevard (see **Figure 7**). The applicant will coordinate construction and follow in-road construction policies of the pipeline corridor Cities and Caltrans as applicable.

7.1 Construction Trip Generation

Peak day construction conditions were used for the peak hour traffic analysis of Project construction conditions.

Peak day construction trucks were estimated as 231 total construction trucks per day operating from 7 a.m. to 4 p.m. as 26 round trips per hour.

Construction workers are expected to park off-site and be shuttled to the Facility. The construction worker offsite temporary construction parking lot is at the corner of Somerset and All American Way within the City of Paramount, west of the Facility as shown in **Figure 8**. Peak day construction workers are estimated at 1,312. The workers will park at that location and be bused to the refinery. The traffic analysis assumed 33 buses (approximately 40 workers per bus).

While the peak construction truck trips and worker trips will not necessarily expected on the same day, in this analysis they are included together. Construction period trucks were estimated to operate 7 a.m. to 4 p.m. with 26 round trips per hour over the nine-hour period. The distribution of the construction truck trips is estimated to follow the Project truck trip distribution shown in **Figure 4**. Worker shuttle bus trips were estimated to have 33 round trips in both the a.m. and p.m. peak hours and would proceed east-west through the Somerset Boulevard / Downey Avenue intersection. A passenger car equivalent value of 2.0 was applied to the construction trucks and worker bus trips in the construction period analysis as described in Section 3.2.

7.2 Construction Trip Distribution and Assignment

Trip generated by the Project construction, were assigned to the surrounding roadway system estimate the peak construction period-related peak-hour traffic at each of the study intersections. **Figure 9** shows the a.m. and p.m. peak hour Project trip assignment for the Project.

7.3 Construction Period Intersection Operation Analysis

Existing plus construction conditions were developed by adding distributed Project construction trips, as a result of the Project, to existing conditions volumes. A level of service analysis was conducted to evaluate construction period intersection operations during the a.m. and p.m. peak hours at the study intersections. **Table 9** compares the existing plus construction volume to capacity ratios to existing conditions to determine potential impacts. Analysis calculation worksheets are included in **Attachment B**.

Similar to the analysis of the Project conditions analysis, Intersection #1 Lakewood Boulevard/Somerset Boulevard would exceed the City's traffic impact analysis threshold for incremental increase in volume-to-capacity ratio in the a.m. peak hour. This indicates if the City elects to require the restriping of the southbound approach to include a dedicated right-turn lane, it should be implemented during the construction period.

Table 9: Intersection Peak Hour Impact Construction Period Analysis

| | Existing | | | | | Existing plus Construction | | | | | npact ion | |
|-------------|---------------------------------------|---|-------------|-----|-------------|----------------------------|-------------|-----|-------------|-------|--------------|------|
| Internation | | | Peak our | | Peak our | | Peak our | | Peak our | Chang | e in V/C | lmn2 |
| | Intersection | | V/C | LOS | V/C | LOS | V/C | LOS | V/C | AM | PM | Imp? |
| 1 | Lakewood Boulevard/Somerset Boulevard | D | 0.810 | D | 0.887 | D | 0.842 | D | 0.887 | 0.032 | 0.000 | Yes |
| 2 | Lakewood Boulevard/Rosecrans Avenue | В | 0.687 | Е | 0.910 | В | 0.687 | Е | 0.910 | 0.000 | 0.000 | No |
| 3 | Downey Avenue/Somerset Boulevard | А | 0.430 | В | 0.660 | Α | 0.451 | В | 0.680 | 0.021 | 0.020 | No |
| 4 | Downey Avenue/Rosecrans Avenue | Α | 0.502 | С | 0.731 | Α | 0.502 | С | 0.731 | 0.000 | 0.000 | No |

Notes:

LOS = Level of Service.

V/C = Volume to Capacity Ratio

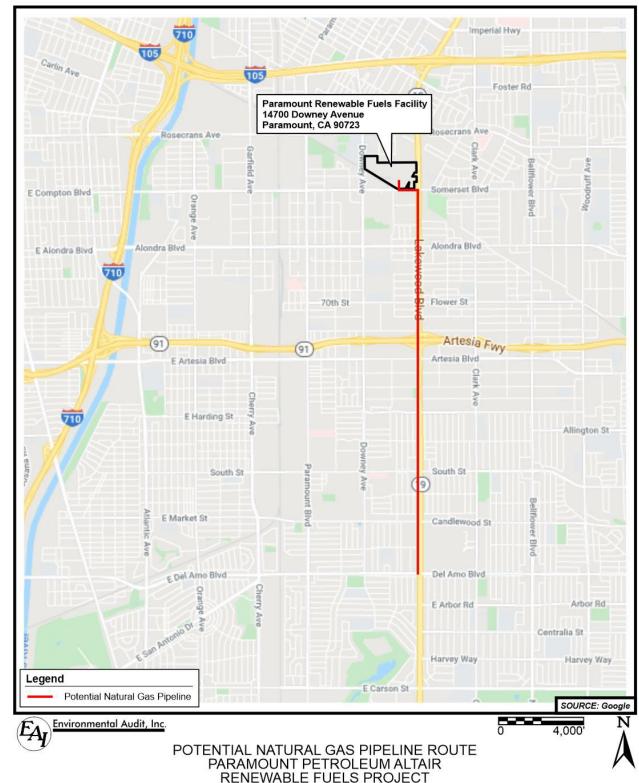


Figure 7 – Potential Natural Gas Pipeline Route

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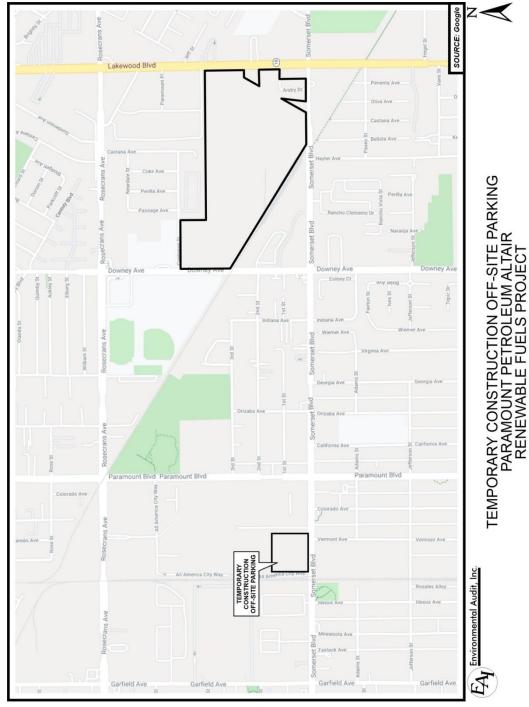
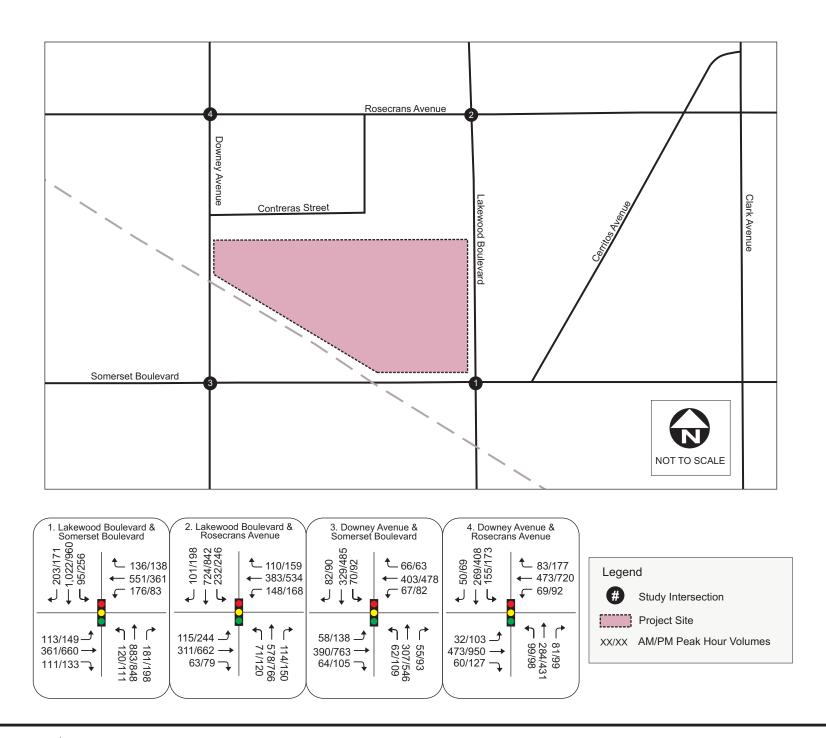


Figure 8 – Temporary Construction Off-Site Parking Location





8.0 PROJECT AREA COLLISIONS

Project area collisions from January 2017 to December 2019 were reviewed. In total, there were 72 collisions in the vicinity of the four analysis intersections. The summary of each collision is in **Attachment C**. Only two of the collisions involved severe injuries and there were no fatal collisions during the period of analysis. The following tables summarize the primary collision factors, collision types and involvement with other modes.

Traffic Total Auto **Improper** Unsafe **Intersection Vicinity** Signs and Other **Collisions ROW Turning** Speed **Signals** Lakewood Boulevard/Somerset Boulevard 24 25% 0% 29% 21% 25% 2 Lakewood Boulevard/Rosecrans Avenue 21 10% 33% 5% 19% 33% 3 Downey Avenue/Somerset Boulevard 10% 10 20% 30% 10% 30% 4 Downey Avenue/Rosecrans Avenue 17 18% 0% 24% 24% 35%

Table 10: Primary Collision Factors (Percent of Total)

| Table 11: Type of Collisions (| Percent of Total) |
|--------------------------------|-------------------|
|--------------------------------|-------------------|

| Intersection Vicinity | | Total Collisions | Broadside | Rear End | Head-On | Sideswipe | Other |
|-----------------------|---------------------------------------|---------------------|-----------|-------------|---------|-----------|-------|
| 1 | Lakewood Boulevard/Somerset Boulevard | 24 | 33% | 38% | 17% | 4% | 8% |
| 2 | Lakewood Boulevard/Rosecrans Avenue | 21 | 37% | 42% | 0% | 16% | 5% |
| 3 | Downey Avenue/Somerset Boulevard | 10 | 60% | 10% | 10% | 10% | 10% |
| 4 | Downey Avenue/Rosecrans Avenue | 17 | 24% | 24% | 12% | 12% | 29% |

Table 12: Collisions with Other Modes

| Intersection Vicinity | | Total Collisions | Pedestrian | Bicycle | Motorcycle | Truck |
|-----------------------|---------------------------------------|---------------------|------------|---------|------------|-------|
| 1 | Lakewood Boulevard/Somerset Boulevard | 24 | 1 | 2 | 1 | 0 |
| 2 | Lakewood Boulevard/Rosecrans Avenue | 21 | 3 | 3 | 2 | 0 |
| 3 | Downey Avenue/Somerset Boulevard | 10 | 1 | 2 | 0 | 0 |
| 4 | Downey Avenue/Rosecrans Avenue | 17 | 3 | 2 | 1 | 1 |

Review of the collisions indicate 35 of the 72 collisions were along or conflicted with Project trip routing and four were located in the Project's driveway areas. Three of the collisions in the driveway areas were along southbound Lakewood Boulevard north of the intersection. Two of these collisions involved unsafe speed involving other southbound vehicles and one involved a southbound vehicle not heeding an exiting vehicle from the tire shop/restaurant driveway south of the Project driveway. The collision near the Somerset Boulevard Project driveway was head-on with an eastbound vehicle impeding on the right-of-way of a westbound vehicle.

9.0 PROJECT DRIVEWAY ANALYSIS

The Project has three driveways, as shown in **Figure 10**. Employee autos enter and exit the site from a driveway along Downey Avenue south of Contreras Street and north of the rail tracks. The employee driveway has a dedicated southbound left-turn lane at a break in the raised median that also allows both outbound right and left turns. Additional features are no u-turn signs for both the northbound and southbound left-turns along Downey and 'keep clear' roadway markings along Downey in front of the driveway.

Site access for trucks is from Andry Drive, a short, loop roadway that connects Lakewood Boulevard and Somerset Boulevard approximately 330 feet north and west of the Lakewood Boulevard / Somerset Boulevard intersection. Inbound access from the south, vehicles turn from Lakewood Boulevard to Somerset Boulevard to Andry Drive. Inbound access from the north vehicles turn directly from Lakewood Boulevard to Andry Drive. Outbound vehicles to the south turn right from Andry Drive to Lakewood Boulevard. Outbound vehicles to the north turn left from Andry Drive to Somerset Boulevard and a left turn to Lakewood Boulevard. There is one driveway south of the Project Lakewood Boulevard driveway for a tire shop and restaurant. Another driveway for the site is on Somerset Boulevard followed by a driveway to a parking lot and then the Project Somerset Boulevard driveway from east to west from the Lakewood Boulevard intersection.

Andry Drive connects to Lakewood Boulevard upstream (in advance) of the Lakewood Boulevard/Somerset intersection and to Somerset Boulevard downstream (departing) from the Lakewood Boulevard/Somerset intersection. Since the Lakewood Boulevard is a right-turn in/out location its access is controlled to minimize conflict points. Based on the collision data, on average one collision per year occurs in the upstream section of Lakewood Boulevard between the Project driveway and the Somerset Boulevard intersection.

Over the past three years, two incidents were rear-end collisions due to southbound vehicles traveling at unsafe speeds and one was a sideswipe collision caused by a southbound vehicle colliding with a vehicle exiting the tire shop/restaurant driveway that is only 75 feet from the intersection. Therefore, are no recommended improvements to the Lakewood Project driveway.

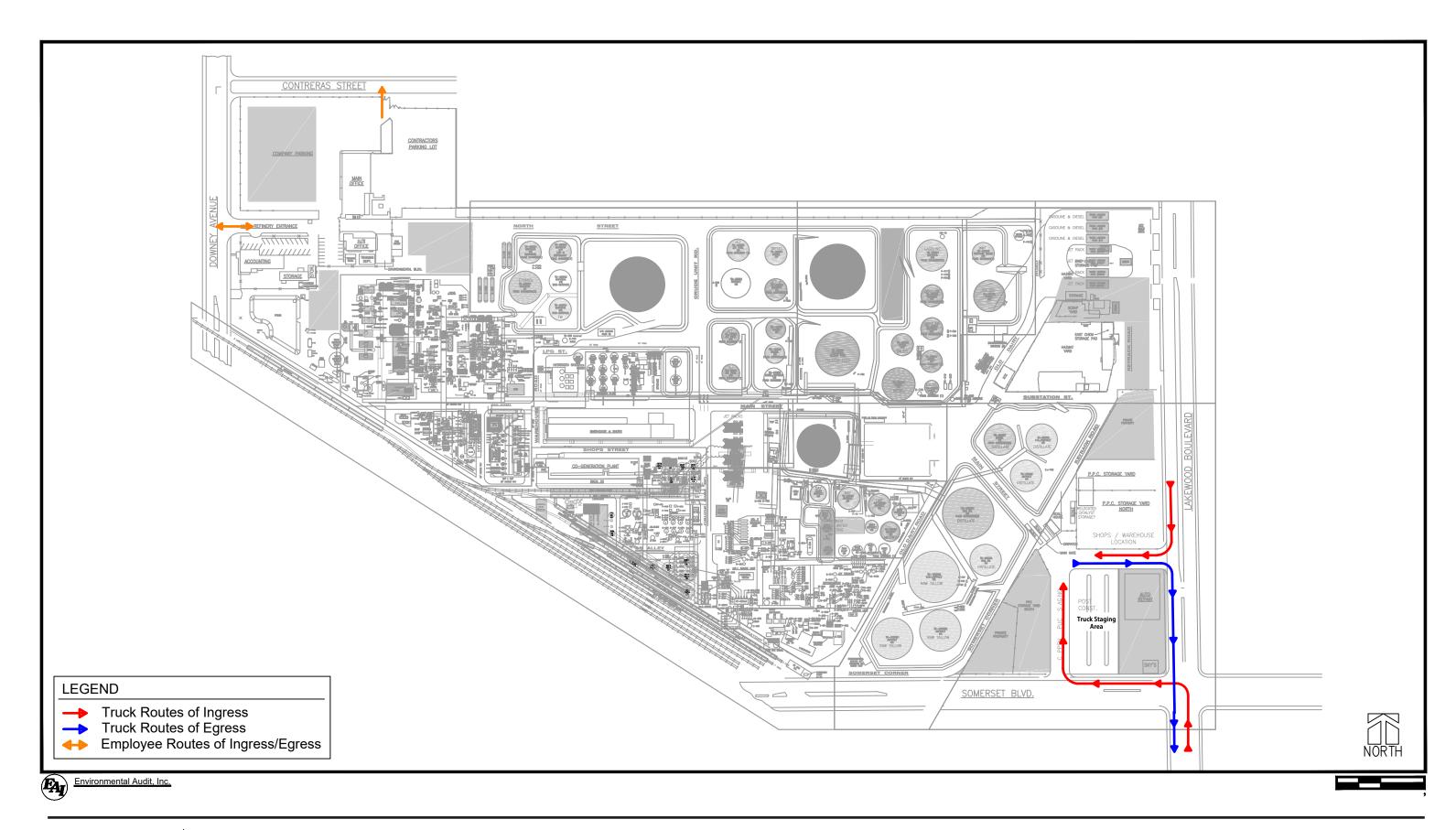
The Somerset Boulevard driveway is downstream from the Lakewood/Somerset intersection. *The Access Management Manual*², published by the Transportation Research Board (TRB), notes that "stopping sight distance is one method for establishing the downstream functional distance of an intersection." Stopping sight distance is the roadway distance required for a driver to perceive and react to an object in the roadway and to brake to a complete stop before reaching that object. The stopping sight distance for a 40 miles per hour roadway is a 305-foot design distance without horizontal or vertical obstructions. The center of Lakewood Boulevard/Somerset Boulevard intersection to center of Andry Drive/Somerset Boulevard is 330 feet. This means that vehicles from the intersection would have adequate stopping time if a Project truck was leaving the driveway.

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² Access Management Manual, Transportation Research Board. Washington, D.C. 2003.

AltAir Renewable Fuels Project Traffic Impact Analysis

The Somerset/Andry driveway is proposed to maintain its right/left in and right/left out conditions under the Project. However, due to the proximity to the Lakewood/Somerset intersection, left-turn access, and use by large vehicles there are concerns about access management. Therefore it is recommended that outbound trucks be directed to the Lakewood/Andry driveway to exit the project site through signage.





Paramount Refinery Traffic Impact Study City of Paramount

Figure 10

Project Driveway Access

9.1 Queuing and Stacking Analysis

Due to the close proximity of the site driveways to the intersection of Lakewood Boulevard/Somerset Boulevard, a focused queuing and stacking analysis of intersection of Lakewood Boulevard/Somerset Boulevard along with the Project site gates, the Andry Drive intersection with Lakewood Boulevard and Somerset Boulevard and the future West Santa Ana Branch at-grade crossings were analyzed in a traffic model to forecast the delay, queuing and stacking of trucks under existing and with-Project conditions.

9.1.1 Off-Site Storage

Andry Drive is fifty feet in width its entire length and serves as a collector road prior to the site entrance. The length of storage for exiting trucks along Andry road is approximately 230 feet at the Lakewood Boulevard driveway and 270 feet at the Somerset Boulevard driveway. As a private road that only serves the Project site, the parking lanes of the roadway can be used for truck staging without impeding access to the Project site gate. There is approximately storage for nine trucks along Andry Drive in the inbound direction. In addition, the parking area to the east of the driveway north of Somerset Boulevard can also be used for truck staging. Any trucks from the north along Lakewood Boulevard have the option of utilizing the Somerset Boulevard Andry driveway for alternative site access.

Storage analysis was conducted by overlaying a template of a 60-foot tanker trailer onto Andry Drive and the staging parking area to the southeast of the Project gate. Clear areas of 30 feet were placed from stop signs and ten feet of space between trucks was allotted. Andry Drive has 50 feet of right-of-way on both legs and can accommodate one parking lane while allowing for two-way driveway operations and turning of inbound and outbound trucks. While it is understood, stacking practice may differ from the one assumed in this analysis, the stacking assumptions included in this analysis were used to determine a practical stacking capacity for inbound site trucks.

As shown in **Figure 11**, there are approximately 20 storage slots for inbound queuing along Andry Drive and in the parking lot area to the southeast of the Project gate. The flow of trucks bypassing direct access for the site gate and entering and exiting the staging area is also shown on the figure. The 20 slots could accommodate approximately 85% of peak inbound demand for one hour (20 of 23 trucks).

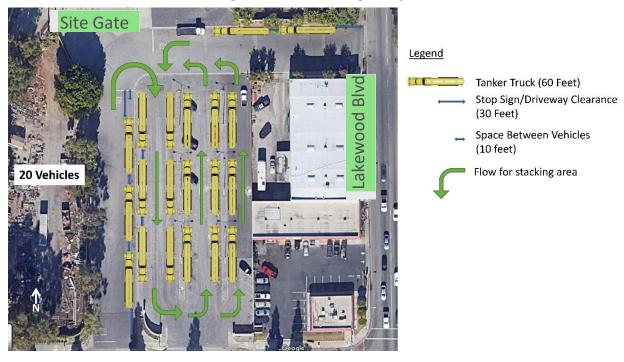


Figure 11: Inbound Storage Analysis

9.1.2 Inbound Gate Demand

Inbound gate queuing analysis was conducted based on the peak day gate demand, inbound gate processing time and the amount of available on-site storage for truck waiting for the inbound gate. At a peak project trip generation demand based on maximum utilization of the racks for loading and unloading of products there would be a continuous demand of 23 inbound trucks per hour placed on the project gate. The current estimated inbound gate processing time average four minute per truck. At an inbound gate processing time of four minutes, 15 trucks could be processed per hour before stacking outside of the hour would occur. With onsite storage of 20 trucks and an inbound gate processing time of four minutes, eight trucks would be queued in the staging area waiting for the inbound gate in the first hour of peak demand. In the second hour of peak demand another 23 inbound trucks would be added to the queued eight trucks from the previous hour for a total gate demand of 31 trucks. With only 15 trucks processed in the hour, 16 trucks would then be queued onsite at the end of the second hour of peak demand. The onsite storage would then be exceeded by three straight hours of peak demand.

An inbound gate processing time of 2:30 minutes could process the peak demand of 23 inbound trucks per day. This would be accomplished through the opening of the second gate to process double the inbound processing capacity of the facility. Therefore, it is recommended that when peak inbound demand on the gate occurs, a second gate would be opened within the next hour to clear trucks waiting for inbound facility access in the staging area and prevent any queue stacking onto public roadways.

9.1.3 Simulation Analysis

Analysis was conducted with the software Synchro 11 and SimTraffic. Synchro is a macroscopic analysis and optimization software application with an associated microscopic simulation software called SimTraffic where each vehicle, including trucks, in the traffic system is individually tracked through the model and comprehensive operational measures of effectiveness are collected on every vehicle during each 0.1-second of the simulation. The measures of performance from SimTraffic are average stop delay (by movement), upstream block time (percent) and storage block time (percent).

The study area of the simulation analysis is the intersection of Lakewood Boulevard/Somerset Boulevard along with the Project site gates, the Andry Drive intersection with Lakewood Boulevard and Somerset Boulevard and the future West Santa Ana Branch at-grade crossings to forecast the delay, queuing and stacking of vehicles under Existing Conditions, and two With-Project conditions, one with a 4:00 minute inbound gate processing time and one with a 2:30 minute inbound gate processing time.

Due to the importance of the West Santa Ana Branch rail project as a major transportation investment in the local area which would interact with existing traffic as well as the project-related trips, the atgrade crossings at Somerset Boulevard west of the site and Lakewood Boulevard south of the project site were included in all of the simulation analysis scenarios. Therefore the "Existing Conditions" and all scenarios with the Project include the two West Santa Ana Branch rail crossings. The crossings were modeled to have 45 seconds of down time followed by 1:45 minutes of gate up time based on the proposed operating plans for the West Santa Ana Branch Build Alternatives assuming 12 train crossings per direction in the peak hour, equating to 24 train crossings per hour for both directions. With this schedule, a train from each direction will cross at each at -grade crossing every 5 minutes, so there will be a train crossing from either direction every 2.5 minutes. Per Metro's grade crossing safety policy, gate down times are determined based on the train crossing configuration (for mid-block train crossings, gates would be down 45 seconds).³

The signal timing sheets for the intersection was obtained from the City of Bellflower and used in the analysis. Upon the initial results of the analysis, it was shown there was an extensive southbound left-turn queue at the intersection of Lakewood Boulevard/Somerset Boulevard causing a network-wide gridlock. Synchro analysis showed that the southbound left-turn movement would experience a 299.3-second delay in the existing condition.

Review of the signal timing sheets show it has a 6:00 a.m. to 9:00 a.m. control plan 2 and a 3 p.m. to 7 p.m. control plan 3 with a control plan 1 for off-peak hours. Control plans 2 and 3 are identical and both allocate 14 seconds of green time for the southbound left-turn lane while leaving an eight second gap in the overall northbound through/southbound left-turn phase pair. The date of the control plans is August 22, 1995 and the date of the phase timings is October 29, 2014.

Thus, slight signal timing modifications of having 22 seconds of southbound left-turn phase green time and reducing the northbound through phase allocation to 46 seconds from 50 seconds in the PM peak

³ West Santa Ana Branch DEIR-DEIS Appendix 4 Transportation Impact Analysis Report, page 1-6.

hour are needed to resolve the modeled gridlock issue. The signal timing modification resulted in an 81.1-second delay for the southbound left-turning vehicles, which while still an LOS F, is functional for the network. Both signal timing approaches—directly from the signal timing sheets and the modified signal phasing were analyzed.

Since the PM peak hour had higher volumes and delays, the PM peak hour results are reported here. Details of the queuing and stacking analysis are in **Attachment D**.

The PM peak hour stop delay for the study area intersections is shown in **Tables 13** for the timing sheet signal plan and **Table 14** for the modified signal plan. As shown, the Project would increase stop delay at the intersection of Lakewood Boulevard/Somerset Boulevard and the Andry Drive driveways, however the 2:30 second inbound processing condition would reduce the stop delay at each of the locations.

Table 13: PM Peak Hour Stop Delay

| | PM Peak Hour Stop Delay | | |
|--|-------------------------|---------------------|---------------------|
| Scenario | Lakewood / Somerset | Andry / Lakewood | Andry / Somerset |
| Existing Conditions | 39.0 | 39.5 | 1.0 |
| With Project - 4:00 Minute Inbound Processing Time | 45.3 | 43.9 | 5.4 |
| With Project - 2:30 Minute Inbound Processing Time | 41.2 | 42.8 | 0.6 |

Table 14: PM Peak Hour Stop Delay – Modified Signal Timing

| | PM Peak Hour Stop Delay | | |
|--|-------------------------|---------------------|---------------------|
| Scenario | Lakewood / Somerset | Andry / Lakewood | Andry / Somerset |
| Existing Conditions | 32.0 | 1.6 | 2.3 |
| With Project - 4:00 Minute Inbound Processing Time | 43.4 | 7.1 | 8.0 |
| With Project - 2:30 Minute Inbound Processing Time | 36.0 | 1.9 | 3.6 |

The controlling factor in the prevention of stacking of Project site truck queues onto Lakewood Boulevard or Somerset Boulevard is the processing time at the inbound gate. This is shown in the PM peak hour upstream block time for the study area intersections is shown in **Tables 15** for the timing sheet signal plan and **Table 16** for the modified signal plan. As shown, the Project would increase the upstream block time at the inbound driveway movements of the southbound right-turn at Andry Drive/Lakewood Boulevard and westbound right-turn at Andry Drive/Somerset Boulevard under the 4:00 minute inbound gate time at peak demand. However, under the 2:30 inbound gate scenario upstream block time was reduced to within one percent of the existing conditions under both the timing sheet and modified signal timing conditions. Note the reduction in southbound through movement upstream block time under the modified signal timing (See **Table 16**) as compared to the timing sheet conditions (see **Table 15**).

Table 15: PM Peak Hour Upstream Block Time (percent)

| | PM Peak Hour Upstream Block Time (%) | | | | | | 5) | |
|--|--------------------------------------|------|------|------------------|-------|------|---------------------|----------|
| | Lakewood / Somerset | | | Andry / Lakewood | | | Andry / Somerset | |
| | SB | SB | NB | EB | SB | SB | EB | |
| Scenario | Right | Thru | Left | Left | Right | Thru | Right | WB Right |
| Existing Conditions | 4 | 88 | 0 | 0 | 14 | 90 | 14 | 0 |
| One-Way Driveway - South | 7 | 88 | 0 | 0 | 16 | 88 | 16 | 7 |
| Distribution – 4:00 Minute Gate | , | 00 | 0 | U | 10 | 00 | 10 | , |
| One-Way Driveway - South Distribution – 2:30 Minute Gate | 5 | 89 | 0 | 0 | 15 | 91 | 20 | 0 |

Table 16: PM Peak Hour Upstream Block Time (percent) - Modified Signal Timing

| | | PM Peak Hour Upstream Block Time (% | | | | | | 5) |
|--|---------------------|-------------------------------------|------------|------------------|-------------|------------|---------------------|----------|
| | Lakewood / Somerset | | | Andry / Lakewood | | | Andry / Somerset | |
| Scenario | SB Right | SB Thru | NB Left | EB Left | SB Right | SB Thru | EB Right | WB Right |
| Scenario | Rigiit | IIIIu | Leit | Leit | Rigiit | IIIIu | Rigiit | WD RIGHT |
| Existing Conditions | 1 | 11 | 0 | 0 | 0 | 0 | 0 | 0 |
| One-Way Driveway - South Distribution – 4:00 Minute Gate | 8 | 15 | 0 | 0 | 5 | 6 | 7 | 9 |
| One-Way Driveway - South Distribution – 2:30 Minute Gate | 2 | 12 | 0 | 0 | 0 | 0 | 0 | 0 |

Tables 17 and **18** show the PM peak hour storage block time at the Lakewood Boulevard/Somerset Boulevard intersection and the effect of the 4:00 minute gate processing time on the inbound trucks utilizing the northbound left-turn lane at the Lakewood Boulevard/Somerset Boulevard intersection. Under both signal timing conditions, the 2:30 minute gate processing time would reduce the northbound left-turn lane storage block time to within one percent of existing conditions. Note the modified signal plan would reduce the southbound left-turn storage blockage time, albeit with some additional storage blockage time at the eastbound left-turn lane.

Table 17: PM Peak Hour Storage Block Time (percent)

| | Storage Block Time (%) | | | | |
|---|------------------------|---------|---------|---------|--|
| | Lakewood / Somerset | | | | |
| Scenario | SB Thru | SB Left | NB Left | EB Left | |
| Existing Conditions | 7 | 95 | 0 | 11 | |
| Scenario 4 - One-Way Driveway - South Distribution – 4:00 Minute Gate | 13 | 97 | 6 | 15 | |
| Scenario 5 - One-Way - South Distribution — 2:30 Minute Gate | 10 | 96 | 0 | 7 | |

Table 18: PM Peak Hour Storage Block Time (percent) - Modified Signal Timing

| | Storage Block Time (%) Lakewood / Somerset | | | |
|--|---|---------|---------|---------|
| | | | | |
| Scenario | SB Thru | SB Left | NB Left | EB Left |
| Existing Conditions | 7 | 11 | 0 | 22 |
| Scenario 4 - One-Way Driveway - South Distribution — 4:00 Minute Gate | 15 | 10 | 11 | 30 |
| Scenario 5 - One-Way - South Distribution – 2:30 Minute Gate | 11 | 14 | 1 | 21 |

10.0 RAIL DELIVERY

As part of the Renewable Fuels Project, modifications were made to the rail unloading rack to add an off-loading manifold, pump, and piping to receive up to 25 railcars per delivery of tallow and vegetable oil (with up to two deliveries per day). Under the Revised Renewable Fuels Project, rail logistics will be required to receive and ship up to 50 railcars per day of feedstock, blend materials, and products. Existing asphalt loading and unloading facilities serving the crude oil refining units will be converted and additional loading and unloading arms will be installed to support the Revised Renewable Fuels Project.

New rail track internal to the Facility is planned both for the operation and due to the Metropolitan Transportation Authority's (LA Metro) proposed light-rail line. The LA Metro light rail project between Artesia and Union Station using the West Santa Ana Branch right-of-way with stations planned for Paramount/Rosecrans, and Bellflower south of Alondra will displace the Facility's outer-most onsite railcar storage track. These track modifications require approval by the rail providers, Union Pacific, and LA Metro.

Secondary containment will be installed for the internal railcar unloading and loading activities. Fire protection will also be installed as required by the fire department. Vapor recovery will be installed for loading facilities as required.

As part of CUP 751 and 757, mitigation measures were imposed to minimize train and vehicle conflicts and delays at the Downey Avenue rail crossing. Mitigation Measure T-1 was imposed as follows:

T-1: Rail car deliveries and pick-ups will be limited to the non-peak hour traffic periods, after 10:00 a.m. and before 6:00 p.m. The refinery operators and management will continue to work with the railroad so that train traffic to and from the refinery does not coincide with the morning and evening commute times or when students are going to or leaving school. No deliveries during the evening, night, and early morning periods will be permitted unless prior notification to the City is provided.

As part of the Revised Renewable Fuels Project, Altair is requesting an extension of time to the rail delivery

period from 10:00 a.m. to 6:00 p.m. to 10:00 a.m. to 8:00 p.m. to allow for timely delivery of railcars which will coincide with the previous 25 railcars being emptied and ready to for their return trip. This measure will better alleviate the disruption to foot traffic from the schools and rush hour traffic in the later afternoon, while still being early enough in the day to avoid disturbance to residents during the more sensitive nighttime hours.

10.1 West Santa Ana Branch

The West Santa Ana Branch (WSAB) is a 19-mile light rail transit corridor to serve commuters from downtown Los Angeles to Artesia. The WSAB will mostly follow the historic Pacific Electric West Santa Ana Branch streetcar service route. Along the route, it will also serve the communities of Vernon, Huntington Park, Bell, Cudahy, South Gate, Downey, Paramount, Bellflower, and Cerritos in the southeast area of the Los Angeles County. The WSAB runs along the southern portion of the Project site. Union Pacific railroad operates the freight rail that serves the Project site. Currently the rail tracks terminate west of the intersection of Somerset Boulevard and Lakewood Boulevard.

LA Metro is planning a light-rail line between Artesia and Union station using the West Santa Ana Branch right-of-way with stations planned for Paramount/Rosecrans and Bellflower south of Alondra. The new light-rail line would be located on the current freight right-of-way. The Project would construct an on-site rail spur to facilitate the construction of the WSAB which is a major regional multimodal transportation project to reduce vehicle miles traveled and reduce greenhouse gas emissions.

The WSAB light-rail project proposes to cross Downey Avenue above grade, however the existing at-grade freight rail tracks would remain at Downey Avenue. The WSAB light-rail project would be built on the AltAir Facility's current rail storage area. Due to the loss of the storage track, the Project would build new on-site storage track.

The vehicle routes taken by the Project vehicle traffic are north-south along Lakewood Boulevard and are not forecasted to utilize the crossing. Rail car deliveries would use the at-grade crossing, as under existing conditions.

Design elements for the WSAB light-rail line in the Project area include⁴:

- The moving of the pedestrian bridge connecting the Paramount high school campus to below grade. The existing pedestrian bridge crosses the alignment aerial and will need to be reconstructed. The pedestrian crossing will be reconstructed below-grade to provide a safer pedestrian connection between the campuses and improve ADA access.
- Alignment will be aerial grade-separated at Downey Avenue before descending at-grade to Somerset Boulevard and Lakewood Boulevard and continuing east to Bellflower Station. Due to the proximity to Paramount High School and Harry Wirtz Elementary School, this intersection has high pedestrian volumes. Grade separation will improve pedestrian safety and travel time reliability.

⁴ West Santa Ana Branch Transit Corridor, Draft Environmental Impact Statement/Impact Report, July 2021.

• Somerset Boulevard and Lakewood Boulevard is proposed to be crossed at-grade.

The Project is located between the proposed Paramount/Rosecrans Station and Bellflower Station, but is located outside the 1/2-mile walk shed of each station. It is within a 3-mile micro mobility (bicycle and other human powered device) shed for each station area which has been studied by LA Metro, and a network of facilities that would ensure 360-degree access to each station has been identified. The Project will not conflict with these connections since there are no off-site Project elements in this area.

Figure 12 shows the southern alignment map for the WSAB. The auto and truck vehicles generated from the Project are not forecast to pass through the proposed at-grade crossing across Somerset Boulevard west of the Project site.





11.0 BIKE AND PEDESTRIAN FACILITIES

In the 2019 Bellflower-Paramount Active Transportation Plan and the WSAB Transit Oriented Development Strategic implementation Plan (May 2019), a proposed bike-pedestrian path will be made along the WSAB rail line in the southwest portion of the Project Facility. This proposed multi-use path provides an enhanced east-west connection for residents wishing to reach Paramount Park, Paramount Middle School, Paramount High School, nearby shopping, places of worship, the proposed WSAB transit stop, the Los Angeles River Bike Trail, and the Bellflower Bike Trail. The Project is located on the opposite side of the WSAB tracks and would not impact the development or use of the multi-use path.

Other Project area active transportation and micro mobility improvements are:

- Class 1 bicycle Facility (bicycle path) on the south side of the West Santa Ana Branch right-of-way and connecting Powerline Corridor Class 1 path south of the Project site.
- Class II buffered bicycle lanes from the WSAB to Lakewood Boulevard.

12.0 CALTRANS REVIEW

Caltrans' Local Development-Intergovernmental Review process is focused on a land use project's impacts to vehicle miles traveled based on the Caltrans Vehicle Miles Traveled-Focused Transportation Impact Study Guide (TISG), May 20, 2020. The TISG was prepared by Caltrans to provide guidance to Caltrans Districts, lead agencies, tribal governments, developers and consultants regarding Caltrans review of a land use project or plan's transportation analysis using a vehicle miles traveled (VMT) metric. The TISG replaces the Guide for the Preparation of Traffic Impact Studies (Caltrans, 2002) and is for use with local land use projects, not for transportation projects on the State Highway System. Therefore, the Caltrans CEQA review of the Project would be based on the vehicle miles traveled of the Project, not the level of traffic volume generated by the site or Project-related trips utilizing Caltrans facilities.

⁵ https://dot.ca.gov/-/media/dot-media/programs/transportation-planning/documents/sb-743/2020-02-26-transmittal-and-draft-vmt-focused-tisg.pdf

13.0 CONCLUSIONS

This traffic impact analysis has been prepared for the AltAir Renewable Fuels Project that is expected to convert the Paramount Petroleum Refinery to manufacture only renewable fuels. This analysis evaluates the operations of intersections, driveways and rail crossings as directed by the City of Paramount staff as potentially being impacted by the Project. This report provides key traffic information regarding existing and future volumes, and an analysis of impacts at study area facilities as a result of Project-related traffic.

The study area for analysis is the four (4) major signalized intersections immediately surrounding the Project site and two site driveways. The study intersections are:

- 1. Lakewood Boulevard/Somerset Boulevard;
- 2. Lakewood Boulevard/Rosecrans Avenue;
- 3. Downey Avenue/Somerset Boulevard; and
- 4. Downey Avenue/Rosecrans Avenue.

Based on the analysis, Intersection #1 Lakewood Boulevard/Somerset Boulevard would exceed the City's traffic impact analysis threshold for incremental increase in volume-to-capacity ratio in the a.m. peak hour under Project and construction period conditions. To address the identified impact, the City could require the striping of the southbound right-turn lane. The outside southbound shared through/right turn lane is approximately 23 feet wide and operates as two de facto lanes. The intersection analysis is based on the lane striping conditions, and therefore identified a potential impact which may not have an effect on the practical operation of the intersection. Nevertheless, the City Public Works should assess the location for potential southbound right-turn lane striping considering factors such as the access management of adjacent driveways and transit operations.

Inbound gate queuing analysis was conducted based on the peak day gate demand, inbound gate processing time and the amount of available on-site storage for trucks waiting for the inbound gate. The onsite storage would then be exceeded by three straight hours of peak demand at a 4:00 minutes inbound gate processing time. An inbound gate processing time of 2:30 minutes could process the peak demand of 23 inbound trucks per hour. This would be accomplished through the opening of the second gate to process double the inbound processing capacity of the facility. Therefore, it is recommended that when peak inbound demand on the gate occurs, a second gate would be opened within the next hour to clear vehicles waiting for inbound facility access in the staging area and prevent any queue stacking onto public roadways.

New rail track internal to the Facility is planned both for the operation and due to the Metropolitan Transportation Authority's (LA Metro) proposed light-rail line. The LA Metro light rail project between Artesia and Union Station using the West Santa Ana Branch right-of-way with stations planned for Paramount/Rosecrans, and Bellflower south of Alondra will displace the Facility's outer-most onsite railcar storage track.

In the 2019 Bellflower-Paramount Active Transportation Plan and the WSAB Transit Oriented

AltAir Renewable Fuels Project Traffic Impact Analysis

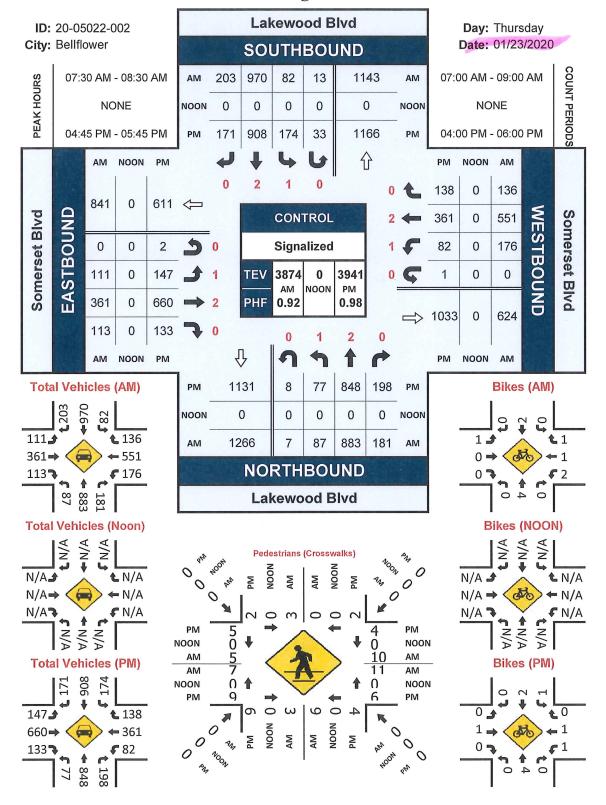
Development Strategic implementation Plan (May 2019), a proposed bike-pedestrian path will be made along the WSAB rail line in the southwest portion of the Project Facility. The Project is located on the opposite side of the WSAB tracks and would not impact the development or use of the multi-use path.

Based on the findings of this report the Project would not adversely impact the operations or safety of the intersection, driveway, rail, bicycle and pedestrian transportation systems.

ATTACHMENT A -TRAFFIC COUNT DATA

Lakewood Blvd & Somerset Blvd

Peak Hour Turning Movement Count



Location: Lakewood Blvd & Somerset Blvd

City: Bellflower

Date: 1/23/2020
Day: Thursday

| | Queue A (AM) | | | | | |
|------|---------------------------|-----------|---------------------------|-----------|--|--|
| | BOG | | EOY | | | |
| Time | EB Left Turn Pocket | Spillover | EB Left turn Pocket | Spillover | | |
| 7:00 | 2 | - | - | - | | |
| | - | - | - | - | | |
| | - | - | - | - | | |
| 7:05 | - | - | - | - | | |
| | 3 | - | - | - | | |
| 7:10 | - | - | - | - | | |
| | 3 | - | 1 | - | | |
| | 1 | - | 2 | - | | |
| 7:15 | 4 | - | - | | | |
| | 1 | - | 1 | - | | |
| | 2 | = | - | - | | |
| 7:20 | 3 | - | - | - | | |
| | 1 | - | - | - | | |
| 7:25 | 2 | - | - | - | | |
| | 3 | - | ı | - | | |
| | 2 | - | 1 | - | | |
| 7:30 | 4 | - | - | - | | |
| | 2 | - | - | - | | |
| | 3 | - | - | - | | |
| 7:35 | 5 | - | - | - | | |
| | - | - | - | - | | |
| | 2 | - | 2 | - | | |
| 7:40 | 4 | - | - | - | | |
| | - | - | - | - | | |
| 7:45 | 1 | - | - | - | | |
| | - | - | - | - | | |
| 7:50 | 1 | - | - | - | | |
| | 4 | - | 1 | - | | |
| 7:55 | 5 | - | - | - | | |
| | 3 | - | - | - | | |
| | - | - | - | - | | |
| 8:00 | 2 | - | 1 | - | | |
| | 2 | - | 1 | - | | |
| | 2 | - | 1 | - | | |
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| | Queue A (PM) | | | | | |
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| | BOG | | EOY | | | |
| Time | EB Left Turn Pocket | Spillover | EB Left Turn Pocket | Spillover | | |
| 4:00 PM | 6 | - | - | - | | |
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| 4:05 PM | 5 | - | - | - | | |
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| 4:10 PM | 5 | - | 1 | - | | |
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| | 6 | - | - | - | | |
| 4:15 PM | 8 | - | 4 | - | | |
| | 7 | - | 5 | - | | |
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| 4:20 PM | 8 | - | - | - | | |
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| 4:25 PM | 5 | - | 6 | - | | |
| | 9 | - | 3 | - | | |
| 4:30 PM | 4 | - | 1 | 1 | | |
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| 4:35 PM | 8 | - | 5 | - | | |
| | 8 | - | 3 | - | | |
| | 10 | 2 | 2 | - | | |
| 4:40 PM | 4 | - | 3 | - | | |
| | 6 | - | - | - | | |
| | 3 | - | 3 | - | | |
| 4:45 PM | 3 | - | - | - | | |
| | 4 | - | - | - | | |
| | 5 | - | 4 | - | | |
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| 4:55 PM | 5 | - | 1 | - | | |
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| | 2 | - | 1 | - | | |

Location: Lakewood Blvd & Somerset Blvd

City: Bellflower

| | Queue A (AM) | | | | | |
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| | BOG | | EOY | | | |
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| 8:40 | 3 | - | - | - | | |
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| Date: | 1/23/2020 |
|-------|-----------|
| Day: | Thursday |

| | Queue A (PM) | | | | | |
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| | BOG | | EOY | | | |
| Time | EB Left Turn Pocket | Spillover | EB Left Turn Pocket | Spillover | | |
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| 5:05 PM | 3 | - | - | - | | |
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| 5:10 PM | 3 | - | - | - | | |
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| 5:15 PM | 3 | - | - | - | | |
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| 5:20 PM | 2 | - | - | - | | |
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| 5:25 PM | 4 | - | 3 | - | | |
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| | 7 | - | | - | | |
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| | Queue B (AM) | | | | | |
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| | BOG | | EOY | | | |
| Time | WB | | WB | | | |
| Time | Left Turn | | Left turn | | | |
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| | 8 | - | - | - | | |
| 7:45 | 3 | - | - | - | | |
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| 7:55 | 4 | - | 2 | - | | |
| | 4 | - | 2 | - | | |
| | 5 | - | - | - | | |
| 8:00 | 2 | - | 2 | - | | |
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| | Queue B (PM) | | | | | |
|---------|---------------------------|-----------|---------------------------|-----------|--|--|
| | BOG | | EOY | | | |
| Time | WB Left Turn Pocket | Spillover | WB Left Turn Pocket | Spillover | | |
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| 4:05 PM | 4 | - | 4 | - | | |
| | 7 | - | 8 | - | | |
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| 4:10 PM | 7 | - | 6 | - | | |
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| 4:15 PM | 1 | - | 2 | - | | |
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| | Queue B (AM) | | | | | |
|------|---------------------------|-----------|---------------------------|-----------|--|--|
| | BOG | | EOY | | | |
| Time | WB Left Turn Pocket | Spillover | WB Left turn Pocket | Spillover | | |
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| | | Queue B (P | M) | |
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| FEATURE LOC | · | T | ı (| N | Ž - | +- | 0 | C | В | > | × 8 | × & | X | <u>×</u> | × 5 | <u>×</u> | <u>×</u> | <u>×</u> 2 | _ | | ۳ | | | OF 6 |
| | | | | | L | | ــــــــــــــــــــــــــــــــــــــ | | | Т | Ц | | <u> </u> | 1 | ٠ | 1 | | Ь | Т | | <u> </u> | لــــــــــــــــــــــــــــــــــــــ | | 1 |

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| ault | r | * | | | | | | | | | | | | * | > | | | | | | | Щ | Ц | | | | | | | | | 0 | ő | | | Z |
| Default Settings | | | | | | | _ | L | * | * | * | * | * | _ | N | | | | | | | | _ | _ | _ | | | | | | ., | | <u>S</u> | z | | Lake |
| ngs | * | | L | | _ | <u> </u> | _ | * | - | | | | _ | | ω | , | (PHASE DISPLAY) | | 192 | UBI | 8 | 171 | J7U | 딘 | 190 | 55 | 14 | 띩 | 30 | 2 | U2I | 7 | SLOT | NPUT | a | OMe |
| | \vdash | | * | * | * | * | * | H | ┞ | | | | - | | 4 5 | , , | | • | - | _ | | | | | | | | | | | | | | - | 9 | od E |
| × | \vdash | | | | H | ╁ | - | | | | | | | | 6 | | 띩 | | | | | | | | | | | | | | | | _ | DELAY | CONTROL | 3/vd |
| = Nev | | T | l | T | | T | T | | | | | | | | 7 | ; | 3 | | | | | | | | | | | | | | | | | | 2 | ® |
| X = New Settings | | | | | | | | | | | | | | | 8 | | _ | | | | | | | | | | | | | | | | | CARRYOVER | ႘ | Lakewood Blvd. @ Compton/Somerset Blvd. |
| ings | <u> </u> | | L | _ | _ | | 1 | - | | _ | _ | _ | | _ | _ | 7 | 0 | | | | | | | | | | | | | | | | ၓ | YOVE | CODE "D" | npto |
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| NOTE | - | 1 | 1 | * | , | +, | | , | - | * | * | * | * | * | 5 | 핏 | D | | اور ح | J _B C | 2 | 171 | 177 | <u>1</u> 6 | 9 | <u>5</u> 5 | J4 | <u>J3</u> | J3U | J2L | JZU | 5 | SLOT | NPUT | | rse |
| 11.0 | | , | | | , | | * | , | • | | * | * | * | * | 6 | 8 | SPL | | | | | | | _ | | | | | L | _ | L | _ | | | | ŀΒlν |
| efaul | | L | Ŀ | _ | | | Ļ | Ļ | * | _ | _ | | | | 7 | \leftarrow | 3 | CO | | | | | | | | | | | | | | | | Œ | | Q. |
| t sett | L | | ļ; | • | <u> </u> | <u>l</u> . | <u> </u> | _ | * | _ | <u>L</u> | | | | 8 | ವ | | Z | | | | | | | | | | | | | | | 2 | DELAY | | |
| Default settings (*) | E | (| J 0 | 9 > | . « | Jo | J - | 40 | 0 | 4 | <u>u</u> | N | _ | 6 | Γ | | | CONTROL | ╟ | | t | - | \dagger | t | H | | lacksquare | · | | ┢ | | \vdash | | ξ | | |
| (") s | יוטפר | | 1 | | 1 . | | 1_ | 1 | 4 7 | . L | | | | Į | | 品 | NPU1 | 1 | | | | | | | | | | | | | | | 4 | CARRYOVER | | |
| should remain | | | | Ľ | Ĺ | ľ | | 1 | | Ľ | | Ľ | | L | | m | 9 | CODE | | L | | | | | | _ | L | | L | | | | | 듔 | | |
| rema | | _ | | | | | _ | \perp | 1 | 1 | <u> </u> | L | | L | | | | 1 | | C. | ų. | <u> </u> | 9 | α | <u>'</u> | O | G | 4 | ယ | N | | 0 | <u>L</u> | | | |
| | | \downarrow | _ | 1 | Ļ | 1 | + | _ | + | ╀ | - | - | - | L | 2 | | m T | " " | | | | | | | | | | | | | | | | | z | |
| lless | ╟ | ╀ | ╀ | + | ╀ | + | + | + | + | + | ╀ | + | ╁ | ┞ | 3 | | 3AHC | | | | | | | | | | | | | | | | | | 임 | ဂ္ဂ |
| Tepla 1 | ╟ | +, | ╁ | ╁ | ╁ | \dagger | \dagger | l | + | + | + | + | ╁ | * | ┢ | | (PHASE DISPLAY) | | | | | | | | | | | | | | | | | | NOTES AND | co: <u>L.A</u> , |
| Ced | - | t | \dagger | \dagger | t | + | | t | † | + , | f , | * | * | - | တ | | SPL | 3 | | | | | | | | | | | | | | | | | | |
| unless replaced with new settings (A). | | * | L | | | | | | * | | | | | | 7 | | 3 | (THIS PAGE @ FCF=123) | | | | | | | | | | | | | | | | | REMARKS: | 골 |
| iew s | | \downarrow | _ | * : | + | * | * | * | _ | - | 1 | _ | ╀ | L | 8 | ļ | | 4GE | - | -T | | | | | | | | | | | | | | | AR. | RTE: <u>19</u> |
| enne | ╟ | 1 | - | - | ╀ | ╀ | \downarrow | + | 1 | 1 | - | - | \vdash | - | - | 무수 | 1 | (A) | באות בועט. | | | | | | | | | | | | | | | | S | 160 |
| Sec | ╢ | ╁ | + | + | ╀ | ╁ | + | + | + | | ╁ | + | ╁ | + | رم دی | 1 | Š | 유=1 | E | DATE OFFICE | CTAD | | | | | | | | | | | ٠ | | | | _ |
| 1 | 1 | + | + | \dagger | \dagger | + | + | \dagger | 1 | \dagger | \dagger | + | T | T | 4 | ╁ | 딍 | 23) | | - | 1 | | | | | | | | | | | | | | | S |
| | | * | * | 1 | * | * | * | * | * | 1 | * | * ; | | ٠ : | · U | 贝 | | | | | | | | | | | | | | | | | | | | P.M.: 7.40 |
| | | * | * | | | * | * | * | * | | | * | • | • | t o | EX CO CA | FUNCTION DISPLAY | į | (| | 3 | | | | | | | | | | | | | | | |
| | - | + | ┿ | * | 1 | 1 | 1 | 4 | ╁ | * | 1 | _ | \perp | 1 | 1 | + | ۲ | | | 0.202017 | 2/2/2 | | | | | | | | | | | | | | | 5 OF 6 |
| | | | | * | 1 | | | | | * | I. | | | L | α | | | _ | | 1 | | | | | | | | | | | | | | | <u></u> | ၂ တ |

| TI | П | D | C | æ | > | 9 | 8 | 7 | 6 | Οī | 4 | ယ | 2 | > | 0 | (HHMM) | TIME | CONT | 7 | m | O | С | В | Þ | ဖ | 8 | 7 | 6 | S1 | 4 | ω | 2 | 1 | 0 | (B) | DAY | CONTI | LOCATION: |
|----------|-----------|------------|-------------|---|----------|----|----------|---|---|----------|----------|---|---|---|---|----------|--------------|-------------------------------|----------|----------|---|---------|----------|---|-------|----------|---|---|----|---|----------|---|----|------|------------|-----------|--------------------------|---|
| | | | | | | | | | | | | | | | | <u>)</u> | ි | 8 | | | | | | | | | | | | | | | | | 33 | YEAR | CONTROL CODE "8": | ON: |
| | | | | | | | | | | | | | | | | | OFS | ODE "9 | | | | | | | | | | | | | | | | | 3 | HTNOM |)DE "8' | Lakewood Blvd. @ Compton/Somerset Blvd. |
| ш | m | ш | т | m | m | m | Ш | т | ш | ш | Ш | m | т | m | m | L | | = | П | п | m | m | m | П | m | m | m | m | m | m | m | m | Ш | П | | | •• | poc |
| | | | _ | _ | | L. | | _ | L | | _ | | _ | | | _ | | 품 | | | | | | - | | _ | | | | | | L | L | Ŀ | _ | | | Blv |
| | | _ | | | | _ | <u> </u> | | L | <u> </u> | L | | _ | | | 2 | | HOLIDAY EVENT 1-16 (C-0-9=11) | | L | | | | | | <u> </u> | | | | | | _ | | _ | N | | | d . (a |
| _ | | | <u></u> | | <u> </u> | L | | | | | | | _ | | | 3 | ٦ | YEV | | | | | | | | | _ | | | | | | _ | | ယ | | 틸 | S |
| | _ | | | | | _ | | _ | | _ | L | | | | | 4 | YPE | NT 1 | L | | | | | | | | | | | | | | | | 4 | 3gY | HOLIDAY 1-16 (C-0-8=11) | dui |
| <u> </u> | | | | _ | _ | | | _ | | L | _ | | | | | 5 | | -16 (| <u> </u> | <u> </u> | | | | | | | | | | | | | _ | _ | 5 | | 6(| ton, |
| _ | | <u> </u> | | _ | | _ | | _ | | | | | | | | 6 | | 9 | | | | | | | | | | | | | | | | _ | 6 | | ို | Sor |
| | | | | | | L | | | | L_ | _ | | L | | | 7 | L | = | | | | | | | | | | | | | | | | _ | 7 |]. | | ner |
| TI | т | O | ဂ | 8 | Þ | 9 | œ | 7 | တ | (J) | 4 | ယ | 2 | | 0 | _ | | റ | Т | ш | o | റ | Œ | Þ | 9 | œ | 7 | 6 | Ċī | 4 | ယ | 2 | ٠. | 0 | ſ | | റ | set I |
| | | | | | | | | | | | | | | | | (HHMM) | TIME | CONTROL | | | | | | | | | | | | | | | | | (DD) | DAY | CONTROL CODE "8" | Slvd. |
| | | | | | | | | | | | | | | | |) | င္ပ | 1 | | | | | | | | | | | | | | | | | 33 | YEAR | OL C | |
| H | | | - | | | _ | | - | | | <u> </u> | - | | | - | | • | 8 | - | | | 1 | \dashv | | | | | | | | | | | _ | ļ | Š | 8 | |
| | | | | | | | | | | | | | | | | | OFS | CODE "9" | | | | | | | | | | | | | | | | | (<u>M</u> | HTNOM | œ_ | |
| Е | Ш | m | П | m | m | m | m | m | m | Ш | m | Ε | Ш | m | П | | | •• | E | П | Ш | П | Ш | Ш | ш | ш | m | m | m | m | m | m | m | П | <u> </u> | _ | * • | |
| | | | | | | | | | | _ | | | | | _ | | | 공 | <u> </u> | | | 4 | _ | _ | | | | | | | | | | | | | | 000 |
| Ш | | | | | | | | | | | | | | | | 2 | | LIDA | L | | | _ | _ | _ | | | | _ | _ | | | | | | 2 | | ᅟႍ | |
| | | | _ | | | | | | | | | | | | | ω | J | EVE | _ | _; | | _ | _ | _ | | | | | _ | | | | | | 3 | \exists | [달 | L.A. |
| | | | | | | | _ | _ | | | | | | | | 4 | HAL | NT 17 | _ | | | _ | | | | | | | _ | | | | | | 4 | YPE | 17 17 | 쯔 |
| | | Ц | | | | | | | | | | | | | _ | បា | | HOLIDAY EVENT 17-32(C-0-9=12) | _ | | | _ | 4 | | | | _ | | _ | _ | _ | _ | _ | | 5 | | HOLIDAY 17-32 (C-0-8=12) | RTE: |
| | | | | | | | | | | | | | | | | 6 | | ;-0-9 - | <u> </u> | | | \perp | | | _ | | | | _ | | | | _ | | 6 | | <u>유</u> | 19 |
| | | | | | | | | | | | | | | | | 7 | L , . | 12) | <u></u> | | | | | | | | | | | | | | | | 7 | | 22 | |
| | DATE END: | 10/29/2014 | DATE START: | | | | | | | | | | | | | | | | ···· | | | | | | ***** | | | | | | | | | | | | NOTES | P.M.: 7.40 |
| | | 014 | ₹Τ: | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 6 OF 6 |

Intersection Turning Movement Count Location: Lakewood Blvd & Somerset Blvd City: Daramount

Project ID: 20-05154-001 City: Paramount **Date:** 6/17/2020 Control: Signalized

| Control. | Jigitalized | | | | | | | | | | | | | Date. | 3/1//2020 | | |
|-----------------------|-------------|------------|----------|-------|--------|---------|---------|-------|--------|---------|---------|-------|--------|---------|-----------|-------|-------|
| | | | | | | | | То | tal | | | | | | | | _ |
| NS/EW Streets: | | Lakewoo | od Blvd | | | Lakewoo | od Blvd | | | Somerse | et Blvd | | | Somerse | et Blvd | | |
| | | NORTH | IBOUND | | | SOUTH | BOLIND | | | EASTB | OLIND | | | WESTE | ROUND | | |
| AM | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | İ |
| \(\text{\text{IVI}}\) | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 7:00 AM | 4 | 61 | 10 | 0 | 8 | 87 | 22 | 0 | 18 | 24 | 11 | 0 | 21 | 37 | 15 | 0 | 318 |
| 7:15 AM | 8 | 109 | 10 | 4 | 15 | 111 | 17 | 4 | 15 | 29 | 10 | 1 | 28 | 39 | 19 | 0 | 419 |
| 7:30 AM | 5 | 90 | 11 | 0 | 10 | 120 | 16 | 4 | 19 | 28 | 13 | 0 | 29 | 47 | 19 | 0 | 411 |
| 7:45 AM | 6 | 131 | 24 | 3 | 13 | 143 | 29 | 3 | 25 | 40 | 11 | 0 | 26 | 46 | 28 | 0 | 528 |
| 8:00 AM | 11 | 102 | 20 | 0 | 15 | 118 | 16 | 4 | 18 | 40 | 18 | 2 | 24 | 48 | 20 | 0 | 456 |
| 8:15 AM | 9 | 115 | 20 | 0 | 13 | 116 | 23 | 3 | 20 | 33 | 13 | 0 | 32 | 47 | 22 | 0 | 466 |
| 8:30 AM | 10 | 91 | 18 | 1 | 23 | 124 | 14 | 3 | 22 | 34 | 12 | 0 | 21 | 34 | 20 | 0 | 427 |
| 8:45 AM | 13 | 129 | 31 | 0 | 12 | 105 | 22 | 10 | 24 | 29 | 14 | 0 | 25 | 36 | 22 | 1 | 473 |
| | | | | | | | | | | | | | | | | | İ |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES: | 66 | 828 | 144 | 8 | 109 | 924 | 159 | 31 | 161 | 257 | 102 | 3 | 206 | 334 | 165 | 1 | 3498 |
| APPROACH %'s: | 6.31% | 79.16% | 13.77% | 0.76% | 8.91% | 75.55% | 13.00% | 2.53% | 30.78% | 49.14% | 19.50% | 0.57% | 29.18% | 47.31% | 23.37% | 0.14% | |
| PEAK HR : | (| 07:45 AM - | 08:45 AM | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 36 | 439 | 82 | 4 | 64 | 501 | 82 | 13 | 85 | 147 | 54 | 2 | 103 | 175 | 90 | 0 | 1877 |
| PEAK HR FACTOR : | 0.818 | 0.838 | 0.854 | 0.333 | 0.696 | 0.876 | 0.707 | 0.813 | 0.850 | 0.919 | 0.750 | 0.250 | 0.805 | 0.911 | 0.804 | 0.000 | 0.889 |
| | | 0.8 | 55 | | | 0.8 | 78 | | | 0.92 | 23 | | | 0.9 | 11 | | 0.009 |
| | | | | | | | | | | | | | | | | | |
| | | NORTH | IBOUND | | | SOUTH | BOUND | | | EASTB | OUND | | | WESTE | BOUND | | |
| PM | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 4:00 PM | 24 | 194 | 39 | 2 | 37 | 190 | 46 | 11 | 27 | 90 | 19 | 1 | 29 | 55 | 37 | 0 | 801 |
| 4:15 PM | 25 | 177 | 40 | 6 | 31 | 175 | 46 | 6 | 30 | 98 | 25 | 0 | 33 | 66 | 31 | 0 | 789 |
| 4:30 PM | 15 | 220 | 44 | 4 | 45 | 221 | 38 | 5 | 38 | 110 | 25 | 1 | 14 | 43 | 32 | 0 | 855 |
| 4:45 PM | | 141 | 32 | 0 | 37 | 167 | 34 | 15 | 33 | 107 | 23 | 3 | 30 | 59 | 34 | 0 | 736 |
| 5:00 PM | 19 | 204 | 41 | 2 | 36 | 185 | 45 | 6 | 37 | 82 | 23 | 0 | 23 | 68 | 31 | 0 | 802 |
| 5:15 PM | 21 | 181 | 45 | 6 | 40 | 181 | 33 | 9 | 27 | 104 | 21 | 0 | 22 | 69 | 39 | 0 | 798 |
| 5:30 PM | 16 | 185 | 44 | 3 | 43 | 191 | 39 | 10 | 28 | 94 | 20 | 0 | 22 | 72 | 34 | 0 | 801 |
| 5:45 PM | 13 | 187 | 42 | 3 | 40 | 205 | 46 | 3 | 42 | 69 | 18 | ı | 27 | 51 | 34 | 0 | 781 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES: | 154 | 1489 | 327 | 26 | 309 | 1515 | 327 | 65 | 262 | 754 | 174 | 6 | 200 | 483 | 272 | 0 | 6363 |
| APPROACH %'s: | 7.72% | 74.60% | 16.38% | 1.30% | 13.94% | 68.37% | 14.76% | 2.93% | 21.91% | 63.04% | 14.55% | 0.50% | 20.94% | 50.58% | 28.48% | 0.00% | |
| PEAK HR : | (| 04:30 PM - | 05:30 PM | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 76 | 746 | 162 | 12 | 158 | 754 | 150 | 35 | 135 | 403 | 92 | 4 | 89 | 239 | 136 | 0 | 3191 |
| PEAK HR FACTOR : | 0.905 | 0.848 | 0.900 | 0.500 | 0.878 | 0.853 | 0.833 | 0.583 | 0.888 | 0.916 | 0.920 | 0.333 | 0.742 | 0.866 | 0.872 | 0.000 | 0.022 |
| | | 0.8 | 80 | | | 0.88 | 38 | | | 0.9 | 11 | | | 0.89 | 92 | | 0.933 |

Intersection Turning Movement Count

Location: Lakewood Blvd & Somerset Blvd

City: Paramount Control: Signalized

Project ID: 20-05154-001 Date: 6/17/2020

| NS/EW Streets: | | Lakewoo | d Blvd | | | Lakewoo | od Blvd | | | Somerse | et Blvd | | | Somerse | et Blvd | | |
|------------------|-------|------------|----------|--------|--------|---------|---------|-------|--------|---------|---------|--------|--------|---------|---------|-------|-------|
| | | NORTH | BOUND | | | SOUTH | BOUND | | | EASTB | OUND | | | WESTB | OUND | | |
| AM | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | |
| , | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 7:00 AM | 4 | 59 | 10 | 0 | 8 | 82 | 22 | 0 | 18 | 24 | 11 | 0 | 21 | 37 | 14 | 0 | 310 |
| 7:15 AM | 8 | 105 | 10 | 4 | 13 | 106 | 17 | 3 | 14 | 28 | 10 | 1 | 27 | 37 | 19 | 0 | 402 |
| 7:30 AM | 5 | 86 | 11 | 0 | 10 | 116 | 14 | 4 | 18 | 28 | 11 | 0 | 28 | 46 | 18 | 0 | 395 |
| 7:45 AM | 6 | 124 | 20 | 3 | 13 | 137 | 29 | 3 | 24 | 39 | 11 | 0 | 26 | 46 | 27 | 0 | 508 |
| 8:00 AM | 11 | 101 | 20 | 0 | 15 | 112 | 14 | 4 | 16 | 40 | 17 | 2 | 24 | 48 | 18 | 0 | 442 |
| 8:15 AM | 8 | 108 | 20 | 0 | 13 | 115 | 23 | 3 | 19 | 31 | 13 | 0 | 31 | 46 | 22 | 0 | 452 |
| 8:30 AM | 10 | 88 | 18 | 1 | 23 | 118 | 13 | 3 | 22 | 33 | 12 | 0 | 21 | 34 | 18 | 0 | 414 |
| 8:45 AM | 11 | 123 | 31 | 0 | 11 | 100 | 21 | 10 | 22 | 29 | 13 | 0 | 25 | 35 | 21 | 1 | 453 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 63 | 794 | 140 | 8 | 106 | 886 | 153 | 30 | 153 | 252 | 98 | 3 | 203 | 329 | 157 | 1 | 3376 |
| APPROACH %'s: | 6.27% | 79.00% | 13.93% | 0.80% | 9.02% | 75.40% | 13.02% | 2.55% | 30.24% | 49.80% | 19.37% | 0.59% | 29.42% | 47.68% | 22.75% | 0.14% | 0070 |
| PEAK HR : | | 07:45 AM - | | 0.00.0 | 110210 | | | | | | | 0.01.0 | | | | | TOTAL |
| PEAK HR VOL : | 35 | 421 | 78 | 4 | 64 | 482 | 79 | 13 | 81 | 143 | 53 | 2 | 102 | 174 | 85 | 0 | 1816 |
| PEAK HR FACTOR : | 0.80 | 0.849 | 0.975 | 0.333 | 0.696 | 0.880 | 0.681 | 0.813 | 0.844 | 0.894 | 0.779 | 0.250 | 0.823 | 0.906 | 0.787 | 0.000 | |
| | 0.00 | 0.87 | | 0.000 | 0.070 | 0.8 | | 0.0.0 | 0.0 | 0.93 | | 0.200 | 0.020 | 0.91 | | 0.000 | 0.894 |
| | | | | | | | | | | | | | | | | | |
| | | NORTH | BOUND | | | SOUTH | BOUND | | | EASTB | OUND | | | WESTB | OUND | | |
| PM | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 4:00 PM | 23 | 192 | 38 | 2 | 37 | 186 | 45 | 11 | 27 | 90 | 18 | 1 | 29 | 55 | 36 | 0 | 790 |
| 4:15 PM | 24 | 172 | 40 | 6 | 30 | 169 | 45 | 6 | 30 | 94 | 25 | 0 | 33 | 64 | 30 | 0 | 768 |
| 4:30 PM | 15 | 219 | 44 | 4 | 45 | 219 | 38 | 5 | 33 | 109 | 24 | 1 | 13 | 43 | 32 | 0 | 844 |
| 4:45 PM | 20 | 139 | 32 | 0 | 37 | 166 | 34 | 15 | 32 | 106 | 22 | 3 | 30 | 58 | 34 | 0 | 728 |
| 5:00 PM | 19 | 203 | 41 | 2 | 35 | 185 | 44 | 6 | 36 | 82 | 23 | 0 | 23 | 68 | 30 | 0 | 797 |
| 5:15 PM | 21 | 180 | 45 | 6 | 40 | 177 | 33 | 9 | 26 | 102 | 21 | 0 | 22 | 69 | 39 | 0 | 790 |
| 5:30 PM | 16 | 183 | 43 | 3 | 43 | 190 | 39 | 10 | 28 | 94 | 20 | 0 | 22 | 71 | 34 | 0 | 796 |
| 5:45 PM | 12 | 187 | 42 | 3 | 40 | 203 | 46 | 3 | 42 | 68 | 18 | 1 | 27 | 51 | 34 | 0 | 777 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 150 | 1475 | 325 | 26 | 307 | 1495 | 324 | 65 | 254 | 745 | 171 | 6 | 199 | 479 | 269 | 0 | 6290 |
| APPROACH %'s: | 7.59% | 74.65% | 16.45% | 1.32% | 14.01% | 68.23% | 14.79% | 2.97% | 21.60% | 63.35% | 14.54% | 0.51% | 21.01% | 50.58% | 28.41% | 0.00% | |
| PEAK HR : | | 04:30 PM - | 05:30 PM | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 75 | 741 | 162 | 12 | 157 | 747 | 149 | 35 | 127 | 399 | 90 | 4 | 88 | 238 | 135 | 0 | 3159 |
| PEAK HR FACTOR : | 0.89 | 0.846 | 0.900 | 0.500 | 0.872 | 0.853 | 0.847 | 0.583 | 0.882 | 0.915 | 0.938 | 0.333 | 0.733 | 0.862 | 0.865 | 0.000 | 0.936 |
| | | 0.87 | 78 | | | 0.88 | 36 | | | 0.92 | 28 | | | 0.88 | 37 | | 0.930 |

Intersection Turning Movement Count

Location: Lakewood Blvd & Somerset Blvd

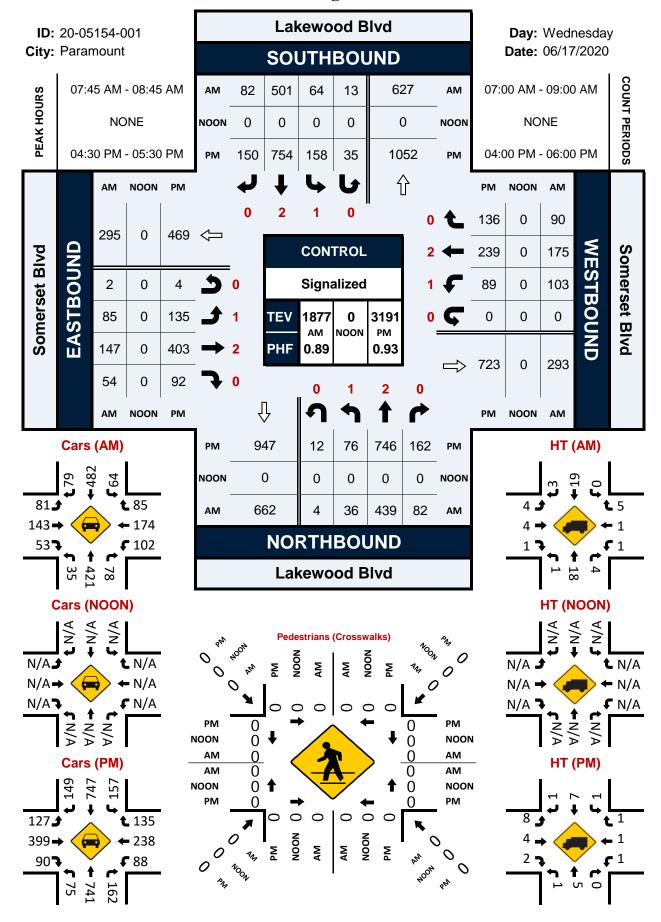
City: Paramount Control: Signalized

Project ID: 20-05154-001 Date: 6/17/2020

| Control: | Signalized | | | | | | | | | | | | | Date: | 0/1//2020 | | |
|--|-------------|-----------------------------------|--|------------|------------|-------------------|---------------------------|-----------------|------------------|-------------|---------------------------|-----------------|------------------|-------------|---------------------------|-----------------|-------------|
| _ | | | | | | | | Н | T | | | | | | | | |
| NS/EW Streets: | | Lakewoo | od Blvd | | | Lakewoo | od Blvd | | | Somerse | et Blvd | | | Somerse | et Blvd | | |
| | | NORTH | IBOUND | | | SOUTH | BOUND | | | EASTE | OUND | | | WESTE | BOUND | | |
| AM | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 7:00 AM | 0 | 2 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 8 |
| 7:15 AM | 0 | 4 | 0 | 0 | 2 | 5 | 0 | 1 | 1 | 1 | 0 | 0 | 1 | 2 | 0 | 0 | 17 |
| 7:30 AM | 0 | 4 | 0 | 0 | 0 | 4 | 2 | 0 | 1 | 0 | 2 | 0 | 1 | 1 | 1 | 0 | 16 |
| 7:45 AM | 0 | 7 | 4 | 0 | 0 | 6 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 20 |
| 8:00 AM | 0 | 1 | 0 | 0 | 0 | 6 | 2 | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 14 |
| 8:15 AM | 1 | / | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 2 | 0 | 0 | 1 | 1 | 0 | 0 | 14 |
| 8:30 AM | 2 | 3 4 | 0 0 | 0 0 | 0 | 6 5 | 1 | 0 | 2 | 0 | 1 | 0 0 | 0 | 1 | 2 1 | 0 0 | 13 20 |
| 8:45 AM | 2 | 6 | U | U | I | 5 | 1 | U | 2 | U | 1 | U | U | 1 | 1 | U | 20 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 3 | 34 | 4 | 0 | 3 | 38 | 6 | 1 | 8 | 5 | 4 | 0 | 3 | 5 | 8 | 0 | 122 |
| APPROACH %'s: | 7.32% | 82.93% | 9.76% | 0.00% | 6.25% | 79.17% | 12.50% | 2.08% | 47.06% | 29.41% | 23.53% | 0.00% | 18.75% | 31.25% | 50.00% | 0.00% | |
| PEAK HR : | | 07:45 AM - | 08:45 AM | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 1 | 18 | 4 | 0 | 0 | 19 | 3 | 0 | 4 | 4 | 1 | 0 | 1 | 1 | 5 | 0 | 61 |
| PEAK HR FACTOR : | 0.250 | 0.643 | 0.250 | 0.000 | 0.000 | 0.792 | 0.375 | 0.000 | 0.500 | 0.500 | 0.250 | 0.000 | 0.250 | 0.250 | 0.625 | 0.000 | 0.763 |
| | | 0.5 | 23 | | | 0.6 | 88 | | | 0.7 | 50 | | | 0.8 | 75 | | |
| | | MODTH | IBOUND | | | SULLUS | BOUND | | | EASTE | OHND | | | WEST | BOUND | | |
| PM | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | |
| FIVI | , NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 4:00 PM | 1 | 2 | 1 | 0 | 0 | 4 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 11 |
| 4:15 PM | 1 | 5 | 0 | 0 | 1 | 6 | 1 | 0 | 0 | 4 | 0 | 0 | 0 | 2 | 1 | 0 | 21 |
| 4:30 PM | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 5 | 1 | 1 | 0 | 1 | 0 | 0 | 0 | 11 |
| 4:45 PM | 1 | 2 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 8 |
| 5:00 PM | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 5 |
| 5:15 PM | 0 | 1 | 0 | 0 | 0 | 4 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| 5:30 PM | 0 | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 5 |
| 5:45 PM | 1 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| | | | | | | | | | | | | EII. | WL | \A/T | 11/5 | | TOTAL |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | V V L | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | NL 4 | 14 | NR 2 | 0 | 2 | 20 | 3 | 0 | 8 | 9 | 3 | 0 | 1 | 4 | 3 | 0 | 73 |
| APPROACH %'s : | 4 20.00% | 14 70.00% | 2 10.00% | | | | | | 8 | | | | 1 | 4 50.00% | | | 73 |
| APPROACH %'s : PEAK HR : | 4 20.00% | 14 70.00% 04:30 PM - | 2 10.00% 05:30 PM | 0 0.00% | 2 | 20 80.00% | 3 | 0 0.00% | 8 40.00% | 9 | 3 15.00% | 0 0.00% | 1 | 4 | 3 | 0 0.00% | 73 TOTAL |
| APPROACH %'s : PEAK HR : PEAK HR VOL : | 4 20.00% | 14 70.00% 04:30 PM - | 2 10.00% 05:30 PM 0 | 0 0.00% | 2 8.00% | 20 80.00% 7 | 3 12.00% | 0 0.00% 0 | 8 40.00% 8 | 9 45.00% | 3 15.00% | 0 0.00% 0 | 1 12.50% 1 | 4 50.00% | 3 37.50% | 0 0.00% 0 | 73 |
| APPROACH %'s : PEAK HR : | 4 20.00% | 14 70.00% 04:30 PM - | 2 10.00% 05:30 PM 0 0.000 | 0 0.00% | 2 | 20 80.00% | 3 12.00% 1 0.250 | 0 0.00% | 8 40.00% | 9 45.00% | 3 15.00% 2 0.500 | 0 0.00% | 1 | 4 | 3 37.50% 1 0.250 | 0 0.00% | 73 TOTAL |

Lakewood Blvd & Somerset Blvd

Peak Hour Turning Movement Count



Intersection Turning Movement Count Location: Lakewood Blvd & Rosecrans Ave City: Daramount

Project ID: 20-05154-004 City: Paramount **Date:** 6/17/2020 Control: Signalized

| - | | | | | | | | To | tal | | | | | | | | _ |
|---|---|---|---|---------------------------------------|---|--|---|--|---|--|--|--|---|---|---|-------------------------------|--|
| NS/EW Streets: | | Lakewoo | od Blvd | | | Lakewoo | d Blvd | | | Rosecra | ns Ave | | | Rosecra | ns Ave | | |
| | | NORTH | BOUND | | | SOUTH | BOUND | | | EASTB | OUND | | | WESTB | BOUND | | |
| AM | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | 1 | 2 | 1 | 0 | 1 | 2 | 0 | 0 | |
| , | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 7:00 AM | 7 | 52 | 7 | 1 | 20 | 102 | 16 | 4 | 20 | 46 | 14 | 0 | 18 | 48 | 9 | 0 | 364 |
| 7:15 AM | 12 | 88 | 17 | 1 | 30 | 108 | 7 | 4 | 14 | 52 | 10 | 0 | 18 | 56 | 15 | 0 | 432 |
| 7:30 AM | 14 | 85 | 13 | 1 | 29 | 111 | 16 | 7 | 15 | 51 | 9 | 0 | 21 | 53 | 16 | 0 | 441 |
| 7:45 AM | 9 | 91 | 29 | 0 | 29 | 145 | 20 | 9 | 22 | 55 | 14 | 0 | 30 | 69 | 17 | 0 | 539 |
| 8:00 AM | 16 | 98 | 21 | 2 | 28 | 129 | 17 | 17 | 12 | 50 | 11 | 0 | 21 | 64 | 21 | 0 | 507 |
| 8:15 AM | 8 | 99 | 9 | 0 | 28 | 103 | 17 | 11 | 22 | 48 | 9 | 0 | 21 | 55 | 17 | 0 | 447 |
| 8:30 AM | 12 | 92 | 16 | 0 | 31 | 101 | 15 | 6 | 19 | 50 | 7 | 0 | 25 | 62 | 17 | 0 | 453 |
| 8:45 AM | 16 | 87 | 23 | 0 | 14 | 99 | 18 | 8 | 23 | 59 | 7 | 1 | 11 | 60 | 22 | 1 | 449 |
| | | | | | | | | | | | | | | | | | |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 94 | 692 | 135 | 5 | 209 | 898 | 126 | 66 | 147 | 411 | 81 | 1 | 165 | 467 | 134 | 1 | 3632 |
| APPROACH %'s: | 10.15% | 74.73% | 14.58% | 0.54% | 16.09% | 69.13% | 9.70% | 5.08% | 22.97% | 64.22% | 12.66% | 0.16% | 21.51% | 60.89% | 17.47% | 0.13% | |
| PEAK HR : | (| 07:45 AM - | 08:45 AM | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 45 | 380 | 75 | 2 | 116 | 478 | 69 | 43 | 75 | 203 | 41 | 0 | 97 | 250 | 72 | 0 | 1946 |
| PEAK HR FACTOR : | 0.703 | 0.960 | 0.647 | 0.250 | 0.935 | 0.824 | 0.863 | 0.632 | 0.852 | 0.923 | 0.732 | 0.000 | 0.808 | 0.906 | 0.857 | 0.000 | 0.903 |
| | | | | | | | | | | | | | | | | | |
| | | 0.9 | 16 | | | 0.86 | 59 | | | 0.8 | 76 | | | 0.90 | 03 | | 0.903 |
| | | | | | | | | | | | | | | | | | 0.903 |
| | | | BOUND | | | 0.86 SOUTH | | | | 0.8 ⁻ EASTB | | | | 0.90 WESTB | | | 0.903 |
| PM | 1 | NORTH 2 | BOUND 0 | 0 | 1 | SOUTH 2 | BOUND 0 | 0 | 1 | EASTB 2 | OUND 1 | 0 | 1 | WESTB 2 | BOUND 0 | 0 | |
| | 1 NL | NORTH 2 NT | BOUND 0 NR | NU | 1 SL | SOUTH 2 ST | BOUND 0 SR | SU | 1 EL | EASTB 2 ET | OUND 1 ER | 0 EU | 1 WL | WESTB 2 WT | SOUND 0 WR | 0 WU | TOTAL |
| 4:00 PM | 30 | NORTH 2 NT 144 | BOUND 0 NR 33 | | 32 | SOUTH 2 ST 167 | BOUND 0 SR 44 | SU 9 | 40 | EASTB 2 ET 122 | OUND 1 ER 16 | | 40 | WESTB 2 WT 99 | O WR 45 | - | TOTAL 826 |
| 4:00 PM 4:15 PM | 30 28 | NORTH 2 NT 144 150 | BOUND 0 NR 33 33 | NU 3 1 | 32 41 | SOUTH 2 ST 167 182 | BOUND 0 SR 44 36 | SU 9 18 | 40 38 | EASTB 2 ET 122 115 | OUND 1 ER 16 10 | | 40 22 | WESTB 2 WT 99 130 | 80UND 0 WR 45 30 | - | TOTAL 826 836 |
| 4:00 PM 4:15 PM 4:30 PM | 30 28 33 | NORTH 2 NT 144 150 157 | BOUND 0 NR 33 33 39 | NU 3 1 3 | 32 41 34 | SOUTH 2 ST 167 182 181 | BOUND 0 SR 44 36 30 | 9 18 34 | 40 38 38 | EASTB 2 ET 122 115 129 | SOUND 1 ER 16 10 17 | EU 1 1 0 | 40 22 36 | WESTB 2 WT 99 130 104 | 80UND 0 WR 45 30 33 | WU 1 1 1 | TOTAL 826 836 869 |
| 4:00 PM 4:15 PM 4:30 PM 4:45 PM | 30 28 33 18 | NORTH 2 NT 144 150 157 167 | BOUND 0 NR 33 33 39 26 | NU 3 1 | 32 41 34 31 | SOUTH 2 ST 167 182 181 169 | BOUND 0 SR 44 36 30 42 | SU 9 18 34 18 | 40 38 38 36 | EASTB 2 ET 122 115 129 116 | SOUND 1 ER 16 10 17 14 | EU 1 1 0 0 | 40 22 36 39 | WESTB 2 WT 99 130 104 111 | 8OUND 0 WR 45 30 33 32 | - | TOTAL 826 836 869 819 |
| 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM | 30 28 33 18 29 | NORTH 2 NT 144 150 157 167 | BOUND 0 NR 33 33 39 26 27 | NU 3 1 3 0 | 32 41 34 31 36 | SOUTH 2 ST 167 182 181 169 170 | BOUND 0 SR 44 36 30 42 43 | SU 9 18 34 18 | 40 38 38 36 46 | EASTB 2 ET 122 115 129 116 115 | SOUND 1 ER 16 10 17 14 | EU 1 1 0 | 40 22 36 | WESTB 2 WT 99 130 104 111 126 | 8OUND 0 WR 45 30 33 32 45 | WU 1 1 1 | TOTAL 826 836 869 819 902 |
| 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM | 30 28 33 18 29 28 | NORTH 2 NT 144 150 157 167 192 151 | BOUND 0 NR 33 33 39 26 27 39 | NU 3 1 3 0 1 3 | 32 41 34 31 36 37 | SOUTH 2 ST 167 182 181 169 170 163 | BOUND 0 SR 44 36 30 42 43 34 | 9 18 34 18 19 16 | 40 38 38 36 46 51 | EASTB 2 ET 122 115 129 116 115 124 | SOUND 1 ER 16 10 17 14 18 14 | EU 1 1 0 0 | 40 22 36 39 34 45 | WESTB 2 WT 99 130 104 111 126 100 | 80UND 0 WR 45 30 33 32 45 36 | WU 1 1 1 | TOTAL 826 836 869 819 902 841 |
| 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM | 30 28 33 18 29 28 21 | NORTH 2 NT 144 150 157 167 192 151 162 | BOUND 0 NR 33 33 39 26 27 39 40 | NU 3 1 3 0 1 3 5 | 32 41 34 31 36 37 37 | SOUTH 2 ST 167 182 181 169 170 163 178 | BOUND 0 SR 44 36 30 42 43 34 47 | SU 9 18 34 18 19 16 13 | 40 38 38 36 46 51 49 | EASTB 2 ET 122 115 129 116 115 124 139 | 1 ER 16 10 17 14 18 14 13 | EU 1 1 0 0 0 0 | 40 22 36 39 34 45 24 | WESTB 2 WT 99 130 104 111 126 100 119 | 80UND 0 WR 45 30 33 32 45 36 23 | WU 1 1 1 0 1 0 1 | TOTAL 826 836 869 819 902 841 871 |
| 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM | 30 28 33 18 29 28 | NORTH 2 NT 144 150 157 167 192 151 | BOUND 0 NR 33 33 39 26 27 39 | NU 3 1 3 0 1 3 | 32 41 34 31 36 37 | SOUTH 2 ST 167 182 181 169 170 163 | BOUND 0 SR 44 36 30 42 43 34 | 9 18 34 18 19 16 | 40 38 38 36 46 51 | EASTB 2 ET 122 115 129 116 115 124 | SOUND 1 ER 16 10 17 14 18 14 | EU 1 1 0 0 0 | 40 22 36 39 34 45 | WESTB 2 WT 99 130 104 111 126 100 | 80UND 0 WR 45 30 33 32 45 36 | WU 1 1 1 0 1 | TOTAL 826 836 869 819 902 841 |
| 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM | 30 28 33 18 29 28 21 20 | NORTH 2 NT 144 150 157 167 192 151 162 150 | BOUND 0 NR 33 33 39 26 27 39 40 36 | NU 3 1 3 0 1 3 5 2 | 32 41 34 31 36 37 37 37 | SOUTH 2 ST 167 182 181 169 170 163 178 167 | BOUND 0 SR 44 36 30 42 43 34 47 42 | SU 9 18 34 18 19 16 13 9 | 40 38 38 36 46 51 49 44 | EASTB 2 ET 122 115 129 116 115 124 139 133 | 1 ER 16 10 17 14 18 14 13 10 | EU 1 1 0 0 0 0 0 0 0 | 40 22 36 39 34 45 24 22 | WESTB 2 WT 99 130 104 111 126 100 119 107 | 8OUND 0 WR 45 30 33 32 45 36 23 21 | WU 1 1 0 1 0 1 0 1 0 | TOTAL 826 836 869 819 902 841 871 796 |
| 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM | 30 28 33 18 29 28 21 20 | NORTH 2 NT 144 150 157 167 192 151 162 150 | BOUND 0 NR 33 33 39 26 27 39 40 36 | NU 3 1 3 0 1 3 5 2 | 32 41 34 31 36 37 37 33 | SOUTH 2 ST 167 182 181 169 170 163 178 167 | BOUND 0 SR 44 36 30 42 43 34 47 42 SR | SU 9 18 34 18 19 16 13 9 | 40 38 38 36 46 51 49 44 | EASTB 2 ET 122 115 129 116 115 124 139 133 | SOUND 1 ER 16 10 17 14 18 14 13 10 | EU 1 1 0 0 0 0 0 0 | 40 22 36 39 34 45 24 22 | WESTB 2 WT 99 130 104 111 126 100 119 107 | 80UND 0 WR 45 30 33 32 45 36 23 21 | WU 1 1 1 0 1 0 1 0 WU | TOTAL 826 836 869 819 902 841 871 796 |
| 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM | 30 28 33 18 29 28 21 20 NL 207 | NORTH 2 NT 144 150 157 167 192 151 162 150 NT 1273 | BOUND 0 NR 33 33 39 26 27 39 40 36 NR 273 | NU 3 1 3 0 1 3 5 2 NU 18 | 32 41 34 31 36 37 37 33 SL 281 | SOUTH 2 ST 167 182 181 169 170 163 178 167 | BOUND 0 SR 44 36 30 42 43 34 47 42 SR 318 | SU 9 18 34 18 19 16 13 9 SU 136 | 40 38 38 36 46 51 49 44 EL 342 | EASTB 2 ET 122 115 129 116 115 124 139 133 ET 993 | SOUND 1 ER 16 10 17 14 18 14 13 10 ER 112 | EU 1 1 0 0 0 0 0 0 0 | 40 22 36 39 34 45 24 22 WL 262 | WESTB 2 WT 99 130 104 111 126 100 119 107 WT 896 | 8OUND 0 WR 45 30 33 32 45 36 23 21 WR 265 | WU 1 1 1 0 1 0 1 0 WU 5 | TOTAL 826 836 869 819 902 841 871 796 |
| 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM | 30 28 33 18 29 28 21 20 NL 207 11.69% | NORTH 2 NT 144 150 157 167 192 151 162 150 NT 1273 71.88% | BOUND 0 NR 33 33 39 26 27 39 40 36 NR 273 15.42% | NU 3 1 3 0 1 3 5 2 | 32 41 34 31 36 37 37 33 SL 281 | SOUTH 2 ST 167 182 181 169 170 163 178 167 | BOUND 0 SR 44 36 30 42 43 34 47 42 SR | SU 9 18 34 18 19 16 13 9 | 40 38 38 36 46 51 49 44 EL 342 | EASTB 2 ET 122 115 129 116 115 124 139 133 | SOUND 1 ER 16 10 17 14 18 14 13 10 | EU 1 1 0 0 0 0 0 0 | 40 22 36 39 34 45 24 22 WL 262 | WESTB 2 WT 99 130 104 111 126 100 119 107 | 80UND 0 WR 45 30 33 32 45 36 23 21 | WU 1 1 1 0 1 0 1 0 WU | TOTAL 826 836 869 819 902 841 871 796 TOTAL 6760 |
| 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM TOTAL VOLUMES: APPROACH %'s: | 30 28 33 18 29 28 21 20 NL 207 11.69% | NORTH 2 NT 144 150 157 167 192 151 162 150 NT 1273 71.88% 04:45 PM - | BOUND 0 NR 33 33 39 26 27 39 40 36 NR 273 15.42% 05:45 PM | NU 3 1 3 0 1 3 5 2 NU 18 1.02% | 32 41 34 31 36 37 37 33 SL 281 13.30% | SOUTH 2 ST 167 182 181 169 170 163 178 167 ST 1377 65.20% | BOUND 0 SR 44 36 30 42 43 34 47 42 SR 318 15.06% | SU 9 18 34 18 19 16 13 9 SU 136 6.44% | 40 38 38 36 46 51 49 44 EL 342 23.60% | EASTB 2 ET 122 115 129 116 115 124 139 133 ET 993 68.53% | SOUND 1 ER 16 10 17 14 18 14 13 10 ER 112 7.73% | EU 1 1 0 0 0 0 0 0 0 | 40 22 36 39 34 45 24 22 WL 262 18.35% | WESTB 2 WT 99 130 104 111 126 100 119 107 WT 896 62.75% | 8OUND 0 WR 45 30 33 32 45 36 23 21 WR 265 18.56% | WU 1 1 1 0 1 0 1 0 WU 5 | TOTAL 826 836 869 819 902 841 871 796 TOTAL 6760 |
| 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM | 30 28 33 18 29 28 21 20 NL 207 11.69% | NORTH 2 NT 144 150 157 167 192 151 162 150 NT 1273 71.88% 04:45 PM - 672 | BOUND 0 NR 33 33 39 26 27 39 40 36 NR 273 15.42% 05:45 PM 132 | NU 3 1 3 0 1 3 5 2 NU 18 1.02% | 32 41 34 31 36 37 37 33 SL 281 13.30% | SOUTH 2 ST 167 182 181 169 170 163 178 167 ST 1377 65.20% | BOUND 0 SR 44 36 30 42 43 34 47 42 SR 318 15.06% | SU 9 18 34 18 19 16 13 9 SU 136 | 40 38 38 36 46 51 49 44 EL 342 23.60% | EASTB 2 ET 122 115 129 116 115 124 139 133 ET 993 68.53% | SOUND 1 ER 16 10 17 14 18 14 13 10 ER 112 7.73% | EU 1 1 0 0 0 0 0 0 EU 2 0.14% | 40 22 36 39 34 45 24 22 WL 262 18.35% | WESTB 2 WT 99 130 104 111 126 100 119 107 WT 896 62.75% | 8OUND 0 WR 45 30 33 32 45 36 23 21 WR 265 18.56% | WU 1 1 1 0 1 0 1 0 WU 5 | TOTAL 826 836 869 819 902 841 871 796 TOTAL 6760 |
| 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM TOTAL VOLUMES: APPROACH %'s: | 30 28 33 18 29 28 21 20 NL 207 11.69% | NORTH 2 NT 144 150 157 167 192 151 162 150 NT 1273 71.88% 04:45 PM - | BOUND 0 NR 33 33 39 26 27 39 40 36 NR 273 15.42% 05:45 PM 132 0.825 | NU 3 1 3 0 1 3 5 2 NU 18 1.02% | 32 41 34 31 36 37 37 33 SL 281 13.30% | SOUTH 2 ST 167 182 181 169 170 163 178 167 ST 1377 65.20% | BOUND 0 SR 44 36 30 42 43 34 47 42 SR 318 15.06% | SU 9 18 34 18 19 16 13 9 SU 136 6.44% | 40 38 38 36 46 51 49 44 EL 342 23.60% | EASTB 2 ET 122 115 129 116 115 124 139 133 ET 993 68.53% | SOUND 1 ER 16 10 17 14 18 14 13 10 ER 112 7.73% | EU 1 1 0 0 0 0 0 0 0 0 EU 2 0.14% | 40 22 36 39 34 45 24 22 WL 262 18.35% | WESTB 2 WT 99 130 104 111 126 100 119 107 WT 896 62.75% | 8OUND 0 WR 45 30 33 32 45 36 23 21 WR 265 18.56% | WU 1 1 1 0 1 0 1 0 WU 5 0.35% | TOTAL 826 836 869 819 902 841 871 796 TOTAL 6760 |

Intersection Turning Movement Count

Location: Lakewood Blvd & Rosecrans Ave

City: Paramount
Control: Signalized

Project ID: 20-05154-004 **Date:** 6/17/2020

| | | - | Date : 6/17/20 |
|------|--|---|-----------------------|
| Cars | | | |

| NS/EW Streets: | | Lakewoo | od Blvd | | | Lakewoo | od Blvd | | | Rosecra | ns Ave | | | Rosecra | ns Ave | | |
|---|--|---|--|----------------------------------|---|---|--|--|---|--|--|---|---|--|---|--|---|
| | | NORTH | BOUND | | | SOUTH | BOUND | DUND | | | | | | | | | |
| Λ Λ | 1 | | | 0 | 1 | | | 0 | 1 | 2 | 1 | 0 | 1 | 2 | | WU 0 0 0 0 0 0 0 1 WU 1 % 0.13% 0 0.000 | |
| AIVI | NII | | | | SI | | | | FI | FT F | FD. | | \\/I | \//T | | | TOTAL |
| 7:00 01 | | | | | | | | 1 | | | | | | | | | |
| | • | | | • | | | 7 | 4 | | | 0 | | | | | | |
| | ANN 1 | | | | | | | | | | | | | | | | |
| | NORTHBOUND SOUTHBOUND CALL BOUND CAL | | | | | | | | | | | | | | | | |
| | AIM | | | | | | | | | | | | | | | | |
| | 13 | | SOUTHBOUND SOU | | | | | | | | | | | | | | |
| | 11 | | SOUTHBOUND SOUTHBOUND C | | | | | | | | | | | | | | |
| | | | | | SOUTHBOUND | | | | | | | | | | | | |
| 8:45 AM | 15 | 83 | 22 | U | 14 | 96 | 18 | 8 | 23 | 57 | / | 1 | 11 | 58 | 21 | | 435 |
| | NL | | | NU | | | | SU | | | | EU | | | | WU | |
| TOTAL VOLUMES : | | | | · | | | | | | | | 1 | | | | - | 3501 |
| APPROACH %'s: | 9.52% | 75.85% | 14.17% | 0.45% | 16.41% | 68.45% | 9.85% | 5.28% | 23.03% | 64.25% | 12.56% | 0.16% | 21.23% | 61.15% | 17.49% | 0.13% | |
| PEAK HR : | (| 07:45 AM - | 08:45 AM | | 07-45 /66 | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 39 | 370 | 69 | 2 | 116 | 453 | 66 | 43 | 73 | 199 | 40 | 0 | 93 | 246 | 71 | 0 | 1880 |
| PEAK HR FACTOR : | 0.75 | 0.944 | 0.595 | 0.250 | 0.935 | 0.839 | 0.868 | 0.632 | 0.869 | 0.939 | 0.714 | 0.000 | 0.861 | 0.918 | 0.845 | 0.000 | 0.012 |
| | | 0.90 | 09 | | | 0.8 | 83 | | | 0.8 | 86 | | | 0.92 | 23 | | 0.913 |
| | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | |
| | | NORTH | BOUND | | | SOUTH | BOUND | | | EASTB | SOUND | | | WESTE | BOUND | | |
| PM | 1 | | | 0 | 1 | SOUTH 2 | | 0 | 1 | EASTB 2 | SOUND 1 | 0 | 1 | WESTE 2 | | 0 | |
| PM | 1 NL | 2 | 0 | | 1 SL | 2 | 0 | | 1 EL | 2 | 1 | | 1 WL | 2 | TBOUND O WR WU 8 0 15 0 16 0 17 0 21 0 16 0 17 0 21 1 WR WU 131 1 1 7 0 21 1 WR 0.13% 71 0 0.845 0.000 .923 TBOUND O WR WU 41 1 30 1 33 1 32 0 43 1 33 1 32 0 43 1 36 0 23 1 20 0 WR WU 258 5 18.42% 0.36% | TOTAL | |
| | | 2 NT | 0 NR | NU | | 2 ST | <mark>0</mark> SR | SU | | 2 ET | 1 ER | | | <mark>2</mark> WT | <mark>0</mark> WR | _ | |
| 4:00 PM | 28 | 2 NT 142 | 0 NR 31 | NU | 32 | 2 ST 163 | 0 SR 44 | SU 9 | 39 | 2 ET 120 | 1 ER 16 | | 39 | 2 WT 95 | 0 WR 41 | _ | 804 |
| 4:00 PM 4:15 PM | 28 28 | 2 NT 142 146 | 0 NR 31 32 | NU 3 1 | 32 41 | 2 ST 163 179 | 0 SR 44 36 | SU 9 18 | 39 37 | 2 ET 120 114 | 1 ER 16 9 | EU 1 1 | 39 20 | 2 WT 95 128 | 0 WR 41 30 | _ | 804 821 |
| 4:00 PM 4:15 PM 4:30 PM | 28 28 33 | 2 NT 142 146 155 | 0 NR 31 32 37 | NU 3 1 3 | 32 41 33 | 2 ST 163 179 180 | 0 SR 44 36 30 | 9 18 34 | 39 37 36 | 2 ET 120 114 126 | 1 ER 16 9 16 | 1 1 0 | 39 20 36 | 2 WT 95 128 103 | 0 WR 41 30 33 | WU 1 1 1 | 804 821 856 |
| 4:00 PM 4:15 PM 4:30 PM 4:45 PM | 28 28 33 18 | 2 NT 142 146 155 163 | 0 NR 31 32 37 25 | NU 3 1 3 | 32 41 33 31 | 2 ST 163 179 180 168 | 0 SR 44 36 30 42 | SU 9 18 34 18 | 39 37 36 36 | 2 ET 120 114 126 116 | 1 ER 16 9 16 14 | EU 1 1 0 0 | 39 20 36 39 | 2 WT 95 128 103 110 | 0 WR 41 30 33 32 | WU 1 1 1 | 804 821 856 812 |
| 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM | 28 28 33 18 29 | 2 NT 142 146 155 163 191 | 0 NR 31 32 37 25 27 | NU 3 1 3 0 | 32 41 33 31 36 | 2 ST 163 179 180 168 | 0 SR 44 36 30 42 43 | SU 9 18 34 18 | 39 37 36 36 46 | 2 ET 120 114 126 116 114 | 1 ER 16 9 16 14 18 | EU 1 1 0 0 | 39 20 36 39 31 | 2 WT 95 128 103 110 | 0 WR 41 30 33 32 43 | WU 1 1 1 0 1 | 804 821 856 812 890 |
| 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM | 28 28 33 18 29 28 | 2 NT 142 146 155 163 191 149 | 0 NR 31 32 37 25 27 39 | NU 3 1 3 0 1 3 | 32 41 33 31 36 36 | 2 ST 163 179 180 168 168 | 0 SR 44 36 30 42 43 34 | 9 18 34 18 19 | 39 37 36 36 46 50 | 2 ET 120 114 126 116 114 123 | 1 ER 16 9 16 14 18 12 | EU 1 1 0 0 0 | 39 20 36 39 31 45 | 2 WT 95 128 103 110 123 99 | 0 WR 41 30 33 32 43 36 | WU 1 1 1 0 1 | 804 821 856 812 890 831 |
| 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM | 28 28 33 18 29 28 21 | 2 NT 142 146 155 163 191 149 159 | 0 NR 31 32 37 25 27 39 40 | NU 3 1 3 0 1 3 4 | 32 41 33 31 36 36 36 | 2 ST 163 179 180 168 168 161 177 | 0 SR 44 36 30 42 43 34 | 9 18 34 18 19 16 13 | 39 37 36 36 46 50 49 | 2 ET 120 114 126 116 114 123 139 | 1 ER 16 9 16 14 18 12 13 | EU 1 1 0 0 0 0 0 0 | 39 20 36 39 31 45 24 | 2 WT 95 128 103 110 123 99 119 | 0 WR 41 30 33 32 43 36 23 | WU 1 1 1 0 1 0 1 | 804 821 856 812 890 831 865 |
| 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM | 28 28 33 18 29 28 21 | 2 NT 142 146 155 163 191 149 159 | 0 NR 31 32 37 25 27 39 40 | NU 3 1 3 0 1 3 4 | 32 41 33 31 36 36 36 | 2 ST 163 179 180 168 168 161 177 | 0 SR 44 36 30 42 43 34 | 9 18 34 18 19 16 13 | 39 37 36 36 46 50 49 | 2 ET 120 114 126 116 114 123 139 | 1 ER 16 9 16 14 18 12 13 | EU 1 1 0 0 0 0 0 0 | 39 20 36 39 31 45 24 | 2 WT 95 128 103 110 123 99 119 | 0 WR 41 30 33 32 43 36 23 | WU 1 1 1 0 1 0 1 | 804 821 856 812 890 831 865 |
| 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM | 28 28 33 18 29 28 21 20 | 2 NT 142 146 155 163 191 149 159 148 | 0 NR 31 32 37 25 27 39 40 36 | NU 3 1 3 0 1 3 4 2 | 32 41 33 31 36 36 36 36 33 | 2 ST 163 179 180 168 168 161 177 163 | 0 SR 44 36 30 42 43 34 47 42 | SU 9 18 34 18 19 16 13 9 | 39 37 36 36 46 50 49 44 | 2 ET 120 114 126 116 114 123 139 130 | 1 ER 16 9 16 14 18 12 13 10 | EU 1 1 0 0 0 0 0 0 0 | 39 20 36 39 31 45 24 22 | 2 WT 95 128 103 110 123 99 119 105 | 0 WR 41 30 33 32 43 36 23 20 | WU 1 1 1 0 1 0 1 0 1 0 | 804 821 856 812 890 831 865 |
| 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM | 28 28 33 18 29 28 21 20 NL 205 | 2 NT 142 146 155 163 191 149 159 148 | 0 NR 31 32 37 25 27 39 40 36 | NU 3 1 3 0 1 3 4 2 | 32 41 33 31 36 36 36 36 33 | 2 ST 163 179 180 168 168 161 177 163 | 0 SR 44 36 30 42 43 34 47 42 | SU 9 18 34 18 19 16 13 9 | 39 37 36 36 46 50 49 44 | 2 ET 120 114 126 116 114 123 139 130 | 1 ER 16 9 16 14 18 12 13 10 | EU 1 1 0 0 0 0 0 0 | 39 20 36 39 31 45 24 22 | 2 WT 95 128 103 110 123 99 119 105 | 0 WR 41 30 33 32 43 36 23 20 | WU 1 1 1 0 1 0 1 0 WU | 804 821 856 812 890 831 865 784 |
| 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM | 28 28 33 18 29 28 21 20 | 2 NT 142 146 155 163 191 149 159 148 | 0 NR 31 32 37 25 27 39 40 36 | NU 3 1 3 0 1 3 4 2 | 32 41 33 31 36 36 36 36 33 | 2 ST 163 179 180 168 168 161 177 163 | 0 SR 44 36 30 42 43 34 47 42 | SU 9 18 34 18 19 16 13 9 | 39 37 36 36 46 50 49 44 | 2 ET 120 114 126 116 114 123 139 130 | 1 ER 16 9 16 14 18 12 13 10 | EU 1 1 0 0 0 0 0 0 | 39 20 36 39 31 45 24 22 | 2 WT 95 128 103 110 123 99 119 105 | 0 WR 41 30 33 32 43 36 23 20 WR 258 | WU 1 1 1 0 1 0 1 0 WU 5 | 804 821 856 812 890 831 865 784 |
| 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM | 28 28 33 18 29 28 21 20 NL 205 11.77% | 2 NT 142 146 155 163 191 149 159 148 NT 1253 | 0 NR 31 32 37 25 27 39 40 36 NR 267 15.33% | NU 3 1 3 0 1 3 4 2 NU 17 | 32 41 33 31 36 36 36 36 33 SL 278 | 2 ST 163 179 180 168 168 161 177 163 ST 1359 | 0 SR 44 36 30 42 43 34 47 42 SR 318 | SU 9 18 34 18 19 16 13 9 SU 136 | 39 37 36 36 46 50 49 44 EL 337 | 2 ET 120 114 126 116 114 123 139 130 ET 982 | 1 ER 16 9 16 14 18 12 13 10 ER 108 | EU 1 1 0 0 0 0 0 0 | 39 20 36 39 31 45 24 22 WL 256 | 2 WT 95 128 103 110 123 99 119 105 | 0 WR 41 30 33 32 43 36 23 20 WR 258 | WU 0 0 0 0 0 0 0 0 0 1 1 WU 1 1 1 1 1 0 0 1 1 0 0 WU 5 | 804 821 856 812 890 831 865 784 |
| 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM | 28 28 33 18 29 28 21 20 NL 205 11.77% | 2 NT 142 146 155 163 191 149 159 148 NT 1253 71.93% | 0 NR 31 32 37 25 27 39 40 36 NR 267 15.33% | NU 3 1 3 0 1 3 4 2 NU 17 | 32 41 33 31 36 36 36 36 33 SL 278 | 2 ST 163 179 180 168 168 161 177 163 ST 1359 | 0 SR 44 36 30 42 43 34 47 42 SR 318 | SU 9 18 34 18 19 16 13 9 SU 136 | 39 37 36 36 46 50 49 44 EL 337 | 2 ET 120 114 126 116 114 123 139 130 ET 982 | 1 ER 16 9 16 14 18 12 13 10 ER 108 | EU 1 1 0 0 0 0 0 0 | 39 20 36 39 31 45 24 22 WL 256 | 2 WT 95 128 103 110 123 99 119 105 | 0 WR 41 30 33 32 43 36 23 20 WR 258 | WU 0 0 0 0 0 0 0 1 WU 1 6 0.13% 0 0.000 WU 1 1 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 | 804 821 856 812 890 831 865 784 TOTAL 6663 |
| 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM TOTAL VOLUMES : APPROACH %'s : | 28 28 33 18 29 28 21 20 NL 205 11.77% | 2 NT 142 146 155 163 191 149 159 148 NT 1253 71.93% | 0 NR 31 32 37 25 27 39 40 36 NR 267 15.33% | NU 3 1 3 0 1 3 4 2 NU 17 0.98% | 32 41 33 31 36 36 36 33 SL 278 13.30% | 2 ST 163 179 180 168 168 161 177 163 ST 1359 64.99% | 0 SR 44 36 30 42 43 34 47 42 SR 318 15.21% | SU 9 18 34 18 19 16 13 9 SU 136 6.50% | 39 37 36 36 46 50 49 44 EL 337 23.58% | 2 ET 120 114 126 116 114 123 139 130 ET 982 68.72% | 1 ER 16 9 16 14 18 12 13 10 ER 108 7.56% | EU 1 1 0 0 0 0 0 0 0 EU 2 0.14% | 39 20 36 39 31 45 24 22 WL 256 18.27% | 2 WT 95 128 103 110 123 99 119 105 WT 882 62.96% | 0 WR 41 30 33 32 43 36 23 20 WR 258 18.42% | WU 1 1 1 0 1 0 1 0 WU 5 | 804 821 856 812 890 831 865 784 TOTAL 6663 |

Intersection Turning Movement Count

Location: Lakewood Blvd & Rosecrans Ave

City: Paramount

0

0.00

TOTAL VOLUMES:

APPROACH %'s:

PEAK HR VOL:

PEAK HR FACTOR:

PEAK HR:

NT

20

10

0.625

6.90% 68.97% 20.69%

04:45 PM - 05:45 PM

0.600

NR

0.250

NU

0.250

3.45%

Project ID: 20-05154-004

WT

14

0.417

WR

7

2

0.250

51.85% 25.93%

0.313

WU

0

0.000

0.00%

TOTAL

TOTAL

35

0.729

| Control: | Signalized | | | | | | | | | | | | | Date: | 6/17/2020 | | |
|------------------|------------|------------|---------|---------|-------|---------|---------|---------|--------|---------|--------|---------|--------|---------|----------------------|---------|-------|
| | | | | | | | | Н | Т | | | | | | | | |
| NS/EW Streets: | | Lakewoo | od Blvd | | | Lakewoo | od Blvd | | | Rosecra | ns Ave | | | Rosecra | ns Ave | | |
| | | NORTH | BOUND | | | SOUTH | BOUND | | | EASTB | OUND | | | WESTI | BOUND | | |
| AM | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | 1 | 2 | 1 | 0 | 1 | 2 | 0 | 0 | |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 7:00 AM | 0 | 2 | 1 | 0 | 1 | 6 | 0 | 0 | 2 | 3 | 1 | 0 | 1 | 0 | 1 | 0 | 18 |
| 7:15 AM | 1 | 6 | 0 | 1 | 0 | 7 | 0 | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 0 | 18 |
| 7:30 AM | 2 | 1 | 2 | 0 | 3 | 2 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 3 | 0 | 0 | 15 |
| 7:45 AM | 1 | 4 | 0 | 0 | 0 | 10 | 1 | 0 | 1 | 2 | 0 | 0 | 3 | 2 | 0 | 0 | 24 |
| 8:00 AM | 3 | 0 | 2 | 0 | 0 | 5 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 1 | 0 | 0 | 13 |
| 8:15 AM | 1 | 5 | 1 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 14 |
| 8:30 AM | 1 | 1 | 3 | 0 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 15 |
| 8:45 AM | 1 | 4 | 1 | 0 | 0 | 3 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 2 | 1 | 0 | 14 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 10 | 23 | 10 | 1 | 4 | 43 | 3 | 0 | 4 | 12 | 3 | 0 | 6 | 9 | 3 | 0 | 131 |
| APPROACH %'s: | 22.73% | 52.27% | 22.73% | 2.27% | 8.00% | 86.00% | 6.00% | 0.00% | 21.05% | 63.16% | 15.79% | 0.00% | 33.33% | 50.00% | 16.67% | 0.00% | |
| PEAK HR : | (| 07:45 AM - | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 6 | 10 | 6 | 0 | 0 | 25 | 3 | 0 | 2 | 4 | 1 | 0 | 4 | 4 | 1 | 0 | 66 |
| PEAK HR FACTOR : | 0.500 | 0.500 | 0.500 | 0.000 | 0.000 | 0.625 | 0.375 | 0.000 | 0.500 | 0.500 | 0.250 | 0.000 | 0.333 | 0.500 | 0.250 | 0.000 | 0.700 |
| | | 0.78 | 36 | | | 0.63 | 36 | | | 0.58 | 33 | | | 0.4 | 50 | | 0.688 |
| | | NODTU | DOLIND | | | COLITI | DOLIND | | | FACTO | OLIND | 1 | | WECT | DOLIND | | T |
| DNA | 1 | NORTH | | 0 | 1 | SOUTH | | 0 | 1 | EASTB | OUND | 0 | 1 | WESII | BOUND | 0 | |
| PM | NL | 2 NT | 0 NR | 0 NU | SL | 2 ST | 0 SR | 0 SU | EL | ET | ER | 0 EU | WL | WT | <mark>0</mark> WR | 0 WU | TOTAL |
| 4:00 PM | 2 | 2 | 2 | 0 | 0 | 4 | 0 | 0 | 1 | 2 | 0 | 0 | 1 | 4 | 4 | 0 | 22 |
| 4:15 PM | 0 | 4 | 1 | 0 | 0 | 3 | 0 | 0 | 1 | 1 | 1 | 0 | 2 | 2 | 0 | 0 | 15 |
| 4:30 PM | 0 | 2 | 2 | 0 | 1 | 1 | 0 | 0 | 2 | 3 | 1 | 0 | 0 | 1 | 0 | 0 | 13 |
| 4:45 PM | 0 | 4 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 7 |
| 5:00 PM | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 1 | 0 | 0 | 3 | 3 | 2 | 0 | 12 |
| 5:15 PM | 0 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | 1 | 1 | 2 | 0 | 0 | 1 | 0 | 0 | 10 |
| 5:30 PM | 0 | 3 | 0 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| 5:45 PM | 0 | 2 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 2 | 1 | 0 | 12 |
| | | | | | | | | | | | | 1 | | | | , | [[|

SR

0

0.000

0.667

0.00%

SU

0

0.000

0.00%

EL

0.250

25.00%

ET

11

2

0.500

ST

18

0.750

85.71%

SL

3

2

0.500

14.29%

ER

4

2

0.250

55.00% 20.00%

0.313

EU

0

0.000

0.00%

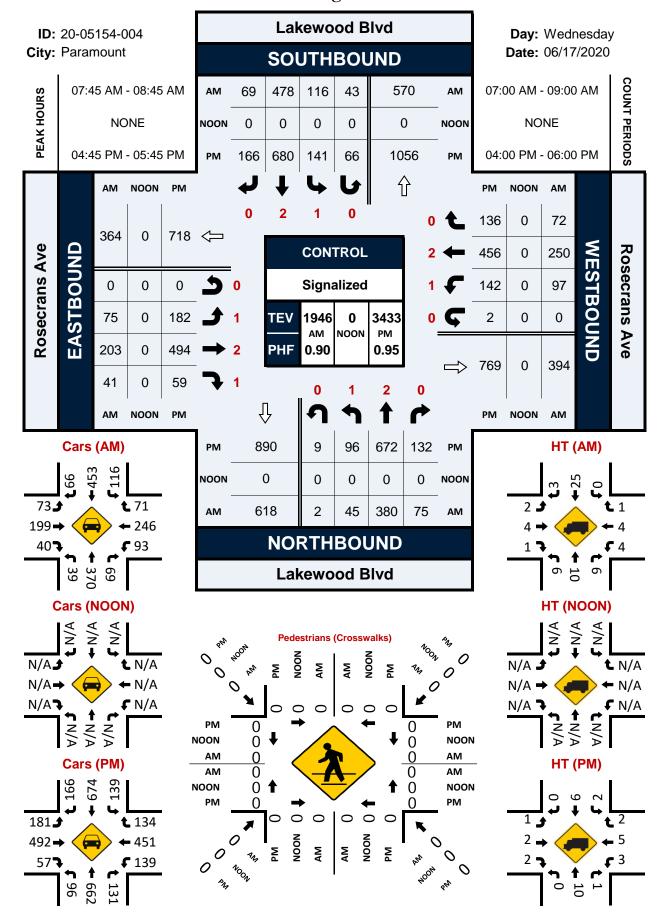
WL

0.250

22.22%

Lakewood Blvd & Rosecrans Ave

Peak Hour Turning Movement Count



Intersection Turning Movement Count

Location: Downey Ave & Somerset Blvd

City: Paramount

Control: Size II | 1 **Project ID:** 20-05154-002 Control: Signalized **Date:** 6/17/2020

| Control. 5 | ngrianzea | | | | | | | To | tal | | | | | Date. | 5/1//2020 | | |
|---|-----------|------------|------------|--------|----------|-------------|------------|--------|------------|------------|-----------|--------|----------|------------|------------|--------|------------|
| NS/EW Streets: | | Downe | y Ave | | | Downe | y Ave | | <u>.c.</u> | Somerse | et Blvd | | | Somerse | et Blvd | | |
| AM | 1 | NORTH 2 | BOUND 0 | 0 | 1 | SOUTHI 2 | BOUND 0 | 0 | 1 | EASTB 2 | OUND 0 | 0 | 1 | WESTE 2 | BOUND 0 | 0 | |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| | 7 | 41 | 12 | 0 | 8 | 41 | 12 | 1 | 7 | 42 | 13 | 0 | 8 | 61 | 7 | 0 | 260 |
| | 14 | 28 | 4 | 0 | 11 | 54 | 11 | 1 | 2 | 38 | 4 | 1 | 9 | 56 | 8 | 0 | 241 |
| II. | / | 44 | 11 | 0 | 10 | 54 | 6 | 2 | 12 | 33 | 13 | 1 | 6 | 54 | 7 | 0 | 260 |
| AM 7:00 AM 7:15 AM 7:30 AM 7:45 AM 9 8:00 AM 8:15 AM 10 8:30 AM 8:45 AM 7 TOTAL VOLUMES: APPROACH %'s: PEAK HR VOL: PEAK HR VOL: PEAK HR FACTOR: 1 NL 4:00 PM 28 4:15 PM 4:30 PM 24 4:30 PM 25 4:45 PM 18 5:00 PM 23 5:15 PM 23 5:15 PM 23 5:30 PM 24 5:45 PM 18 | 40 | 9 | 0 | 9 | 65 | 6 | 4 | 6 | 40 | 9 | 3 | 8 | 76 | 10 | 0 | 291 | |
| | | 47 | 11 9 | 0 | 10 9 | 55 47 | 13 | 0 | 11 8 | 62 | 5 | 2 | 16 | 60 | 10 | 0 | 318 287 |
| | 0 | 43 48 | 9 | 0 | 14 | 64 | 14 18 | 1 | 0 | 53 50 | 11 12 | 1 2 | 5 | 60 49 | 12 14 | 0 | 287 |
| | 0 7 | 64 | 7 | 0 | 9 | 59 | 11 | 1 | 8 | 47 | 14 | 1 | 13 | 51 | 7 | 1 | 303 |
| 0.45 AIVI | , | 04 | / | U | 7 | 39 | 11 | 4 | 0 | 47 | 14 | I | 13 | 31 | / | | 303 |
| | NI | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | | 355 | 72 | 0 | 80 | 439 | 91 | 14 | 59 | 365 | 81 | 11 | 73 | 467 | 72 | 2 | 2259 |
| | | 70.30% | 14.26% | 0.00% | | 70.35% | 14.58% | 2.24% | 11.43% | 70.74% | 15.70% | 2.13% | _ | 76.06% | 11.73% | 0.33% | |
| | | 8:00 AM - | | 0.00,0 | | | | | | | | | | | | 0.00,0 | TOTAL |
| | | 202 | 36 | 0 | 42 | 225 | 56 | 6 | 32 | 212 | 42 | 6 | 42 | 220 | 43 | 2 | 1207 |
| PEAK HR FACTOR : | 0.641 | 0.789 | 0.818 | 0.000 | 0.750 | 0.879 | 0.778 | 0.375 | 0.727 | 0.855 | 0.750 | 0.750 | 0.656 | 0.917 | 0.768 | 0.500 | |
| | | 0.89 | 94 | | | 0.84 | 18 | | | 0.91 | 13 | | | 0.89 | 92 | | 0.949 |
| | | | | | | | | | | | | | | | | | |
| | | NORTH | BOUND | | | SOUTH | BOUND | | | EASTB | OUND | | | WESTE | BOUND | | |
| PIM | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | |
| | | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| | | 138 | 22 | 0 | 18 | 102 | 20 | 2 | 25 | 111 | 18 | 4 | 16 | 88 | 7 | 3 | 602 |
| II. | | 98 | 21 | 0 | 11 | 81 | 18 | 4 | 28 | 131 | 18 | 1 | 18 | 105 | 14 | 0 | 572 |
| | | 102 | 17 | 1 | 13 | 99 | 20 | 1 | 18 | 150 | 27 | 1 | 16 | 87 | 21 | 0 | 598 |
| | | 107 | 22 | 0 | 25 | 93 | 18 | 3 | 25 | 128 | 15 | 1 | 17 | 72 | 12 | 0 | 556 571 |
| II. | | 103 97 | 20 22 | 0 | 25 14 | 121 99 | 19 | 3 | 20 25 | 107 | 15 16 | 0 | 10 18 | 92 104 | 12 15 | | 571 589 |
| | | 97 107 | 19 | 1 | 19 | 99 90 | 21 21 | ა 1 | 25 19 | 132 103 | 16 20 | 2 | 11 | 88 | 15 13 | 0 | 538 |
| | | 99 | 35 | 0 | 17 | 91 | 25 | 1 | 14 | 112 | 26 | 0 | 18 | 103 | 12 | 0 | 574 |
| 3.43 1 101 | 10 | 77 | 33 | U | 17 | 71 | 25 | 4 | 14 | 112 | 20 | U | 10 | 103 | 12 | U | 374 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 183 | 851 | 178 | 2 | 142 | 776 | 162 | 21 | 174 | 974 | 155 | 10 | 124 | 739 | 106 | 3 | 4600 |
| APPROACH %'s: | 15.07% | 70.10% | 14.66% | 0.16% | | 70.48% | 14.71% | 1.91% | 13.25% | 74.18% | 11.81% | 0.76% | 12.76% | 76.03% | 10.91% | 0.31% | |
| PEAK HR : | C | 4:00 PM - | 05:00 PM | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 95 | 445 | 82 | 1 | 67 | 375 | 76 | 10 | 96 | 520 | 78 | 7 | 67 | 352 | 54 | 3 | 2328 |
| PEAK HR FACTOR : | 0.040 | | | | | 0.010 | | | | | | 0 100 | 0.001 | 0.000 | 0 / 10 | 0.050 | |
| | 0.848 | 0.806 | 0.932 | 0.250 | 0.670 | 0.919 | 0.950 | 0.625 | 0.857 | 0.867 | 0.722 | 0.438 | 0.931 | 0.838 | 0.643 | 0.250 | 0.967 |

Intersection Turning Movement Count

Location: Downey Ave & Somerset Blvd

NL

181

94

0.84

15.01%

TOTAL VOLUMES:

APPROACH %'s

PEAK HR FACTOR:

PEAK HR VOL:

PEAK HR:

NT

846

70.15%

440

0.809

04:00 PM - 05:00 PM

0.828

NU

2

0.250

0.17%

SL

142

67

0.670

12.94%

ST

773

374

0.917

70.46%

NR

177

81

0.920

14.68%

City: Paramount

Project ID: 20-05154-002
Date: 6/17/2020

WU

0.250

0.31%

TOTAL

4556

TOTAL

2299

0.963

WR

104

52

0.619

0.862

10.80%

| Control: | Signalized | | | | | | | | | | | | | Date: | 6/17/2020 | | |
|------------------|------------|------------|--------|-------|--------|---|--------|-------|--------|--------|---------|---|--------|-----------|-----------|--|-------|
| _ | | | | | | | | Ca | ırs | | | | | | | | _ |
| NS/EW Streets: | | Downe | y Ave | | | Downe | y Ave | | | Somers | et Blvd | | | Somers | et Blvd | | |
| | | NORTH | BOUND | | | SOUTH | BOUND | | | EASTE | BOUND | 000000000000000000000000000000000000000 | | WEST | BOUND | | |
| AM | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | |
| 7 4.0. | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 7:00 AM | 7 | 41 | 12 | 0 | 8 | 41 | 11 | 1 | 7 | 40 | 13 | 0 | 8 | 61 | 7 | 0 | 257 |
| 7:15 AM | 14 | 28 | 3 | 0 | 11 | 54 | 11 | 1 | 2 | 37 | 4 | 1 | 9 | 52 | 8 | 0 | 235 |
| 7:30 AM | 7 | 43 | 10 | 0 | 10 | 53 | 6 | 2 | 12 | 32 | 13 | 1 | 6 | 54 | 7 | 0 | 256 |
| 7:45 AM | 9 | 39 | 8 | 0 | 9 | 2 0 0 1 2 0 0 1 2 0 0 ST SR SU EL ET ER EU WL WT WR WU TOTAL 41 11 1 7 40 13 0 8 61 7 0 257 54 11 1 2 37 4 1 9 52 8 0 235 53 6 2 12 32 13 1 6 54 7 0 256 65 6 4 6 40 9 3 8 75 7 0 288 55 13 0 11 59 5 2 15 59 10 0 311 46 14 1 8 51 11 1 8 59 12 1 283 64 | 288 | | | | | | | | | | |
| 8:00 AM | 15 | 46 | 11 | 0 | 10 | 55 | 13 | 0 | 11 | 59 | 5 | 2 | 15 | 59 | 10 | D O O O O O O O O O O O O O O O O O O O | 311 |
| 8:15 AM | 10 | 43 | 9 | 0 | 9 | 46 | 14 | 1 | 8 | | 11 | 1 | 8 | 59 | 12 | ND O O O O O O O O O O O O O O O O O O O | 283 |
| 8:30 AM | 8 | 48 | 8 | 0 | 14 | 64 | 17 | 1 | 5 | | 12 | 2 | 5 | 47 | 14 | 0 | 294 |
| 8:45 AM | 7 | 64 | 7 | 0 | 9 | 59 | 11 | 4 | 8 | 45 | 14 | 1 | 13 | 49 | 7 | 1 | 299 |
| | | | | | | | | | | | | | | | | | |
| | NL | NT | NR | NU | SL | | | | | | | | | | | | |
| TOTAL VOLUMES : | 77 | 352 | 68 | 0 | 80 | | | | | | | | | | | | |
| APPROACH %'s: | 15.49% | 70.82% | 13.68% | 0.00% | 12.90% | 70.48% | 14.35% | 2.26% | 11.71% | 70.04% | 16.07% | 2.18% | 11.96% | 75.75% | 11.96% | 0.33% | |
| PEAK HR : | | - MA 00:80 | | _ | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 40 | 201 | 35 | 0 | 42 | 224 | 55 | 6 | 32 | 204 | 42 | 6 | 41 | 214 | 43 | 2 | 1187 |
| PEAK HR FACTOR : | 0.67 | 0.785 | 0.795 | 0.000 | 0.750 | 0.875 | 0.809 | 0.375 | 0.727 | 0.864 | 0.750 | 0.750 | 0.683 | 0.907 | 0.768 | 0.500 | 0.954 |
| | | 0.8 | 85 | | | 0.8 | 52 | | | 0.9 | 22 | | | 0.8 | 393 | | |
| | | NORTH | BOUND | | | SOUTH | BOUND | | | FASTE | BOUND | | | WEST | BOUND | | |
| PM | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | |
| 1 101 | NL | NT | NR | NU | SL. | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 4:00 PM | 28 | 136 | 22 | 0 | 18 | 102 | 20 | 2 | 25 | 109 | 17 | 4 | 16 | 88 | 7 | 3 | 597 |
| 4:15 PM | 24 | 98 | 20 | 0 | 11 | 80 | 17 | 4 | 28 | 130 | 18 | 1 | 18 | 104 | 14 | 0 | 567 |
| 4:30 PM | 25 | 101 | 17 | 1 | 13 | 99 | 20 | 1 | 18 | 143 | 27 | 1 | 16 | 85 | 21 | 0 | 588 |
| 4:45 PM | 17 | 105 | 22 | 0 | 25 | 93 | 18 | 3 | 25 | 126 | 15 | 1 | 17 | 70 | 10 | 0 | 547 |
| 5:00 PM | 23 | 103 | 20 | 0 | 25 | 120 | 19 | 3 | 20 | 106 | 15 | 1 | 10 | 92 | 12 | 0 | 569 |
| 5:15 PM | 23 | 97 | 22 | 0 | 14 | 9 8 | 21 | 3 | 25 | 129 | 16 | 0 | 17 | 104 | 15 | 0 | 584 |
| 5:30 PM | 24 | 107 | 19 | 1 | 19 | 90 | 21 | 1 | 19 | 99 | 20 | 2 | 11 | 87 | 13 | 0 | 533 |
| 5:45 PM | 17 | 99 | 35 | 0 | 17 | 91 | 25 | 4 | 14 | 111 | 25 | 0 | 18 | 103 | 12 | 0 | 571 |

SU

21

10

0.625

1.91%

EL

174

96

0.857

13.49%

ΕT

953

508

0.888

73.88%

SR

161

75

0.938

0.926

14.68%

EU

10

0.438

0.78%

WL

123

67

0.931

12.77%

WT

733

347

0.834

76.12%

ER

153

77

0.713

0.910

11.86%

Intersection Turning Movement Count

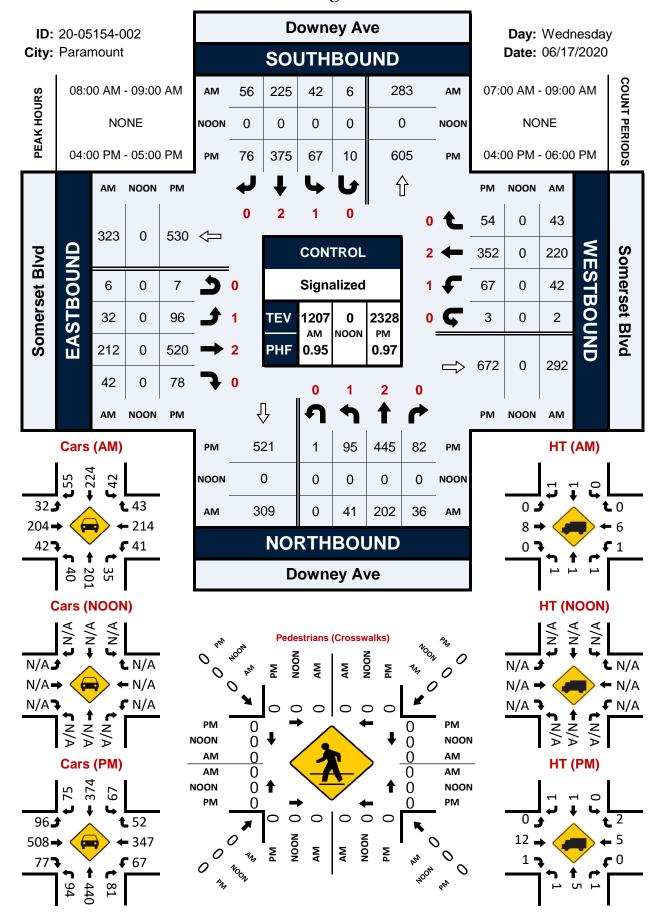
Location: Downey Ave & Somerset Blvd
City: Paramount
Control: Signalized

Project ID: 20-05154-002 Date: 6/17/2020

| Control. | Signanzea | | | | | | | ш | т | | | | | Date. | 77772020 | | |
|---|-----------|------------|----------|--------|---------|---------|--------|-------|-------|----------|---------|-------|--------|---------|--|--|--------|
| NS/EW Streets: | | Downe | v Ave | | | Downe | v Ave | | | Somerse | et Blvd | | | Somerse | et Blvd | | |
| 1107 211 011 00101 | | | | | | | | | | | | | | | | | |
| A B A | | NORTH | | • | | | | | | EASTB | | | | | | | |
| AIVI | 7 | 2 | 0 | 0 | 7 | 2 | | | 1 | 2 | _ | - | 7 | | | | TOTAL |
| 7.00 414 | NL 0 | NT O | NR 0 | NU | SL 0 | ST 0 | SR 1 | | | | | | | | | | |
| | 0 | 0 | 1 | 0 | 0 | 0 | 0 | | 0 | 2 | 0 | 0 | 0 | 4 | 0 | 0 | 5 6 |
| 7:00 AM 7:15 AM 7:30 AM 7:45 AM 8:00 AM 8:15 AM 8:30 AM 8:45 AM TOTAL VOLUMES: APPROACH %'s: PEAK HR: PEAK HR VOL: PEAK HR FACTOR: 0 | 0 | 1 | 1 | 0 | 0 | 1 | 0 | | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 0 | 1 | 1 | 0 | 0 | 0 | • | | 0 | 0 | 0 | O | 0 | 1 | 0 | • | 3 |
| | 1 | 1 | 0 | 0 | 0 | 0 | | | 0 | 3 | 0 | | 1 | 1 | 0 | | 7 |
| 7:00 AM 7:15 AM 7:30 AM 7:45 AM 8:00 AM 8:15 AM 8:30 AM 8:45 AM TOTAL VOLUMES: APPROACH %'s: PEAK HR: PEAK HR VOL: PEAK HR FACTOR: O PM 4:00 PM 4:15 PM 4:30 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | | 0 | 2 | 0 | 0 | 0 | 1 | 0 | 0 | 4 |
| | 0 | 0 | 1 | 0 | 0 | 0 | O | | | | | | | | | | |
| | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 2 | 0 | ND O O O O O O O O O O O O O O O O O O O | 4 |
| | | | | | | | | | | | | | | | | | |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | | ER | EU | WL | WT | Set Blvd TBOUND O WR WU O O O O O O O O O O O O O O O O O O | TOTAL | |
| | 1 | 3 | 4 | 0 | 0 | 2 | | | _ | | | - | 1 | | | | |
| | 12.50% | 37.50% | 50.00% | 0.00% | 0.00% | 50.00% | 50.00% | 0.00% | 0.00% | 100.00% | 0.00% | 0.00% | 8.33% | 91.67% | 0.00% | 0.00% | |
| | (| 08:00 AM - | | | | | | | | | | | | | | | |
| | 1 | 1 | 1 | 0 | 0 | 1 | • | | | | | _ | 1 | | | | 20 |
| PEAK HR FACTOR : | 0.250 | 0.250 | 0.250 | 0.000 | 0.000 | 0.250 | | 0.000 | 0.000 | | | 0.000 | 0.250 | | | 0.000 | 0.714 |
| | | 0.3 | /5 | | | 0.50 | JU | | | 0.00 | 0 / | | | 0.87 | 5 | | |
| | | NORTH | ROUND | | | SOUTH | BOUND | | | FASTR | OLIND | | | WESTR | OUND | | |
| PM | 1 | 2 | 0 | 0 | 1 | 2 | | 0 | 1 | 2 | | 0 | 1 | | | 0 | |
| | NL | NT | NR | NU | SL | ST | | | EL | ET | | _ | WL | | WR | _ | TOTAL |
| 4:00 PM | 0 | 2 | 0 | 0 | 0 | 0 | | | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | |
| 4:15 PM | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 5 |
| | 0 | 1 | 0 | 0 | 0 | 0 | 0 | | 0 | 7 | 0 | 0 | 0 | 2 | 0 | 0 | |
| | | | 0 | 0 | 0 | 0 | | | 0 | 2 | | | | 2 | 2 | | |
| | 0 | 0 | 0 | 0 | 0 | 1 | | | 0 | 1 | | 0 | 0 | 0 | 0 | 0 | |
| | 0 | 0 | 0 | 0 | 0 | 1 | • | | 0 | 3 | | 0 | 1 | 0 | 0 | 0 | |
| | 1 | 0 | 0 | 0 0 | 0 | 0 | _ | 1 | 0 | 4 | 1 | 0 | 0 | 0 | • | | |
| 5:45 PIVI | · · | 0 | 0 | U | 0 | 0 | 0 | 0 | U | I | I | U | U | U | 0 | 0 | 3 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 2 | 5 | 1 | 0 | 0 | 3 | 1 | 0 | 0 | 21 | 2 | 0 | 1 | 6 | 2 | 0 | 44 |
| APPROACH %'s: | 25.00% | 62.50% | 12.50% | 0.00% | 0.00% | 75.00% | 25.00% | 0.00% | 0.00% | 91.30% | 8.70% | 0.00% | 11.11% | 66.67% | 22.22% | 0.00% | |
| PEAK HR : | | 04:00 PM - | 05:00 PM | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 1 | 5 | 1 | 0 | 0 | 1 | 1 | 0 | 0 | 12 | 1 | 0 | 0 | 5 | 2 | 0 | 29 |
| PEAK HR FACTOR : | 0.05 | 0 (05 | | | | | | | | | | | | | | | |
| I LAKTIK I ACTOR . | 0.25 | 0.625 | 0.250 | 0.000 | 0.000 | 0.250 | 0.250 | 0.000 | 0.000 | 0.429 | 0.250 | 0.000 | 0.000 | 0.625 | 0.250 | 0.000 | 0.725 |

Downey Ave & Somerset Blvd

Peak Hour Turning Movement Count



Intersection Turning Movement Count

Location: Downey Ave & Rosecrans Ave

City: Paramount

Control City in Times **Project ID:** 20-05154-003 Control: Signalized Date: 6/17/2020

| control. | Signanzea | | | | | | | | | | | | | Date. | 3/1//2020 | | |
|---|------------|------------|--------|--------|---------|---------|--------|--------|--------|---------|---------|--------|--------|---------------|-------------|--|-------|
| | | | | | | | | То | tal | | | | | | | | |
| NS/EW Streets: | | Downe | ey Ave | | | Downe | y Ave | | | Rosecra | ns Ave | | | Rosecra | ns Ave | | |
| | | NORTH | IBOUND | | | SOUTH | ROLIND | | | FASTR | OLIND | | | WESTE | ROUND | | |
| ΔΜ | 1 | 2 | | 0 | 1 | 2 | | 0 | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | |
| Aivi | NI | NT | _ | | SI. | ST | | | FI | FT | FR | | WI | WT | WR | _ | TOTAL |
| 7:00 AM | 6 | | 9 | | | | 6 | | 3 | | | 0 | | 41 | 7 | 1 | 244 |
| 7:00 AM 7:15 AM 7:30 AM 7:45 AM 8:00 AM 8:15 AM 8:30 AM 8:45 AM TOTAL VOLUMES: APPROACH %'s: PEAK HR: PEAK HR VOL: | 3 | | | | | | 3 | | 3 | | 9 | 0 | 9 | | 19 | 1 | 311 |
| | 6 | 38 | 10 | 0 | 18 | 51 | 9 | 2 | 6 | 70 | 10 | 0 | 8 | 60 | 15 | 2 | 305 |
| | 6 | 48 | 7 | 0 | 24 | 50 | 8 | 1 | 4 | 80 | 10 | 0 | 3 | 77 | 20 | 2 | 340 |
| 8:00 AM | NORTHBOUND | 370 | | | | | | | | | | | | | | | |
| 8:15 AM | 15 | 46 | 14 | 0 | 15 | 33 | 13 | 2 | 5 | 76 | 3 | 0 | 12 | 81 | 12 | Ave JND 1 0 WR WU 7 1 19 1 15 2 20 2 16 12 0 17 0 9 2 WR WU 115 9 2 WR 115 9 5.39% 1.20% 54 3 .794 0.375 JND 1 0 WR WU 39 1 49 0 40 2 37 0 35 1 40 1 39 4 | 327 |
| 8:30 AM | 11 | 54 | 17 | 0 | 22 | 51 | 12 | 1 | 4 | 70 | 3 | 0 | 12 | 58 | 17 | e D O R WU 1 9 1 9 1 9 1 9 1 9 1 9 1 9 1 9 3 94 0 3 94 0 7 0 0 R WU 9 1 9 1 9 0 0 R WU 9 1 9 1 9 0 1 9 1 1 | 332 |
| 8:45 AM | 23 | 45 | 8 | 0 | 28 | 47 | 4 | 0 | 8 | 82 | 20 | 0 | 6 | 9 5 | 9 | 2 | 377 |
| | NII | NIT | MD | NILI | SI. | CT. | SD | SH | ЕІ | ЕТ | ED | EII | \\/\ | \ \ /T | \M/D | \\/ | TOTAL |
| TOTAL VOLUMES : | | | | | | | | | | | | 1 | | | | | 2606 |
| | | | | _ | | | | | | | | 0 14% | | | | - | |
| | | | | 0.0070 | 30.7770 | 30.4170 | 7.5270 | 1.2770 | 3.1070 | 03.4370 | 11.5570 | 0.1470 | 7.7770 | 73.0370 | 13.3770 | 1.2070 | TOTAL |
| | | | | 0 | 101 | 184 | 34 | 5 | 20 | 309 | 30 | 1 | 42 | 309 | 54 | 3 | 1406 |
| | | | | | | | | | | | | 0.250 | | | | | |
| TEARTINT ACTOR. | 0.707 | | | 0.000 | 0.701 | | | 0.020 | 0.020 | | | 0.200 | 0.070 | | | 0.070 | 0.932 |
| | | | | | | 0.0 | | | | 5.15 | | | | | | |) |
| | | NORTH | IBOUND | | | SOUTH | BOUND | | | EASTB | OUND | | | WESTE | OUND | | |
| PM | 1 | 2 | | 0 | 1 | | | 0 | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | İ |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | ESTBOUND 1 | TOTAL | |
| 4:00 PM | 23 | 103 | | | | | | 1 | 18 | 199 | | 1 | 21 | 122 | 39 | Ave UND 1 0 WR WU 7 1 19 1 15 2 20 2 16 12 0 17 0 9 2 WR WU 115 9 15.39% 1.20% 54 3 0.794 0.375 UND 1 0 WR WU 39 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 | 707 |
| 4:15 PM | 40 | 90 | 21 | 0 | 46 | 60 | 11 | 0 | 17 | 163 | 21 | 0 | 24 | 148 | 49 | 0 | 690 |
| | 19 | 89 | 17 | 0 | 29 | 84 | 13 | 2 | 17 | 180 | 17 | 2 | 21 | 120 | 40 | 2 | 652 |
| 4:45 PM | 12 | 103 | 28 | 0 | 39 | 69 | 10 | 0 | 24 | 172 | 23 | 3 | 25 | 161 | 37 | 0 | 706 |
| | 19 | 84 | | 0 | | | | 2 | 14 | | | 6 | 15 | 155 | 35 | 1 | 705 |
| | 35 | | | | | | | | 18 | | | 2 | | | | 1 | 718 |
| | _ | | | | | | | | | | | 1 | | | | 4 | 694 |
| 5:45 PM | 24 | 87 | 17 | 0 | 33 | 86 | 15 | 3 | 18 | 153 | 20 | 0 | 15 | 141 | 38 | 0 | 650 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 192 | 747 | 172 | 0 | 266 | 666 | 113 | 11 | 135 | 1404 | 175 | 15 | 154 | 1146 | | 9 1.20% 3 0.375 0 WU 1 0 2 0 1 1 1 4 0 WU 9 0.55% | 5522 |
| APPROACH %'s: | 17.28% | 67.24% | 15.48% | 0.00% | | 63.07% | 10.70% | 1.04% | 7.81% | 81.20% | 10.12% | 0.87% | 9.47% | 70.48% | 19.50% | 0.55% | |
| PEAK HR : | | 04:45 PM - | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 86 | 378 | 87 | 0 | 140 | 343 | 58 | 5 | 65 | 709 | 95 | 12 | 73 | 615 | 151 | 6 | 2823 |
| PEAK HR FACTOR: | 0.614 | 0.917 | 0.777 | 0.000 | 0.897 | 0.884 | 0.853 | 0.417 | 0.677 | 0.953 | 0.880 | 0.500 | 0.730 | 0.955 | 0.944 | 0.375 | |
| | | 0.8 | | | | 0.92 | | | | 0.9 | | | | 0.94 | | | 0.983 |

Intersection Turning Movement Count

Location: Downey Ave & Rosecrans Ave City: Paramount Control: Signalized

Project ID: 20-05154-003

| | | Date : 6/17/2020 |
|----|----|-------------------------|
| Ca | rs | |
| | | |

| NS/EW Stree | ets: | | Downe | y Ave | | | Downe | y Ave | | | Rosecra | ns Ave | | | Rosecra | ns Ave | | |
|---------------|-------|--------|------------|----------|-------|--------|--------|--------|-------|-------|---------|--------|-------|--------|---------|--------|-------|-------|
| | | | NORTH | BOUND | | | SOUTH | BOUND | | | EASTB | OUND | | | WESTE | OUND | | |
| AM | | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | |
| 7 0 . | | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 7:00 |) AM | 6 | 32 | 9 | 0 | 28 | 32 | 5 | 0 | 3 | 51 | 12 | 0 | 11 | 40 | 7 | 1 | 237 |
| 7:15 | AM | 3 | 37 | 15 | 0 | 23 | 51 | 2 | 0 | 3 | 71 | 9 | 0 | 9 | 61 | 19 | 1 | 304 |
| 7:30 |) AM | 6 | 37 | 10 | 0 | 18 | 50 | 9 | 2 | 6 | 69 | 10 | 0 | 8 | 58 | 15 | 2 | 300 |
| 7:45 | 5 AM | 6 | 47 | 7 | 0 | 24 | 50 | 8 | 1 | 4 | 76 | 10 | 0 | 3 | 73 | 20 | 2 | 331 |
| 8:00 |) AM | 15 | 42 | 14 | 0 | 36 | 53 | 5 | 2 | 3 | 79 | 13 | 1 | 12 | 71 | 15 | 1 | 362 |
| 8:15 | 5 AM | 15 | 46 | 14 | 0 | 15 | 33 | 13 | 2 | 5 | 73 | 3 | 0 | 12 | 79 | 12 | 0 | 322 |
| 8:30 |) AM | 11 | 54 | 17 | 0 | 22 | 50 | 12 | 1 | 4 | 69 | 3 | 0 | 12 | 55 | 17 | 0 | 327 |
| 8:45 | 5 AM | 23 | 45 | 8 | 0 | 28 | 47 | 4 | 0 | 8 | 81 | 20 | 0 | 6 | 92 | 9 | 2 | 373 |
| | | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUME | ES: | 85 | 340 | 94 | 0 | 194 | 366 | 58 | 8 | 36 | 569 | 80 | 1 | 73 | 529 | 114 | 9 | 2556 |
| APPROACH % | 6's : | 16.38% | 65.51% | 18.11% | 0.00% | 30.99% | 58.47% | 9.27% | 1.28% | 5.25% | 82.94% | 11.66% | 0.15% | 10.07% | 72.97% | 15.72% | 1.24% | |
| PEAK H | HR : | (| 08:00 AM - | 09:00 AM | | | | | | | | | | | | | | TOTAL |
| PEAK HR VO | OL : | 64 | 187 | 53 | 0 | 101 | 183 | 34 | 5 | 20 | 302 | 39 | 1 | 42 | 297 | 53 | 3 | 1384 |
| PEAK HR FACTO | OR : | 0.70 | 0.866 | 0.779 | 0.000 | 0.701 | 0.863 | 0.654 | 0.625 | 0.625 | 0.932 | 0.488 | 0.250 | 0.875 | 0.807 | 0.779 | 0.375 | 0.000 |
| | | | 0.92 | 27 | | | 0.84 | 41 | | | 0.83 | 30 | | | 0.90 | 06 | | 0.928 |
| | | | | | | | | | | | | | | | | | | |
| | | | NORTH | BOUND | | | SOUTH | BOUND | | | EASTB | OUND | | | WESTE | BOUND | | |
| PM | | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | |
| | | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 4:00 |) PM | 22 | 102 | 30 | 0 | 18 | 93 | 16 | 1 | 18 | 195 | 22 | 1 | 21 | 119 | 39 | 0 | 697 |
| 4:15 | | 40 | 89 | 21 | 0 | 46 | 58 | 11 | 0 | 17 | 162 | 21 | 0 | 24 | 143 | 49 | 0 | 681 |
| 4:30 | | 19 | 88 | 17 | 0 | 29 | 84 | 13 | 2 | 17 | 175 | 17 | 2 | 21 | 118 | 40 | 2 | 644 |
| 4:45 | | 11 | 103 | 28 | 0 | 39 | 69 | 10 | 0 | 24 | 169 | 23 | 3 | 25 | 160 | 37 | 0 | 701 |
| 5:00 | | 19 | 82 | 18 | 0 | 31 | 97 | 16 | 2 | 14 | 183 | 24 | 6 | 15 | 153 | 35 | 1 | 696 |
| 5:15 | | 35 | 100 | 22 | 0 | 32 | 94 | 16 | 0 | 18 | 166 | 19 | 2 | 19 | 147 | 40 | 1 | 711 |
| 5:30 | | 20 | 90 | 19 | 0 | 38 | 82 | 15 | 3 | 9 | 181 | 27 | 1 | 13 | 150 | 39 | 4 | 691 |
| 5:45 | PM | 24 | 87 | 17 | 0 | 33 | 86 | 15 | 3 | 18 | 152 | 20 | 0 | 15 | 140 | 38 | 0 | 648 |
| | - | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUME | ES: | 190 | 741 | 172 | 0 | 266 | 663 | 112 | 11 | 135 | 1383 | 173 | 15 | 153 | 1130 | 317 | 8 | 5469 |
| APPROACH % | | 17.23% | 67.18% | 15.59% | 0.00% | 25.29% | 63.02% | 10.65% | 1.05% | | 81.07% | 10.14% | 0.88% | 9.51% | 70.27% | 19.71% | 0.50% | |
| PEAK H | HR : | | 04:45 PM - | 05:45 PM | | | | | | | | | | | | | | TOTAL |
| PEAK HR VO | | 85 | 375 | 87 | 0 | 140 | 342 | 57 | 5 | 65 | 699 | 93 | 12 | 72 | 610 | 151 | 6 | 2799 |
| PEAK HR FACTO | | 0.61 | 0.910 | 0.777 | 0.000 | 0.897 | 0.881 | 0.891 | 0.417 | 0.677 | 0.955 | 0.861 | 0.500 | 0.720 | 0.953 | 0.944 | 0.375 | |
| | | | 0.87 | | | | 0.93 | | | | 0.9 | | | | 0.94 | | | 0.984 |

Intersection Turning Movement Count

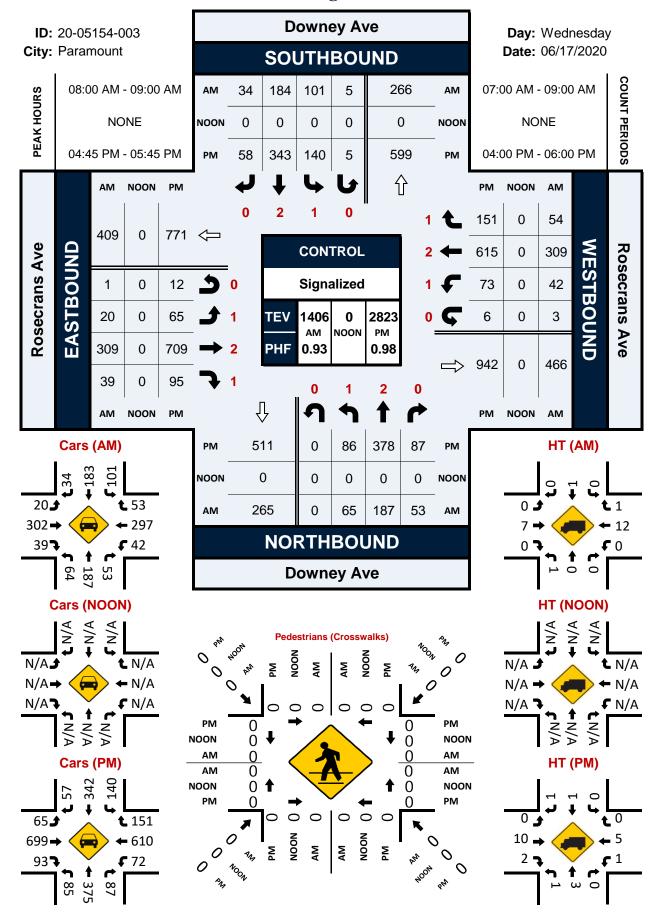
Location: Downey Ave & Rosecrans Ave City: Paramount Control: Signalized

Project ID: 20-05154-003 Date: 6/17/2020

| | _ | | | | | | | | Н | T | | | | | | | | |
|-------------|--|---|--|--|---|--|---|--|---|--|--|---|---|---------------------------------|---|---|---------------------------------|--|
| NS | S/EW Streets: | | Downe | y Ave | | | Downe | y Ave | | | Rosecra | ns Ave | | | Rosecra | ns Ave | | |
| | | | NORTH | BOUND | | | SOUTH | BOUND | October | | FASTB | OUND | October | | WESTE | BOUND | | |
| | AM | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | |
| | | NL | NT | STHBOUND SOUTHBOUND SU ST SR SU EL ET ER EU WL WL WT WR WU THOU STAND SU ST SR SU EL ET ER EU WL WL WT WR WU THOU STAND SOUTHBOUND SOUTH | TOTAL | | | | | | | | | | | | | |
| | 7:00 AM | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 4 | 0 | 0 | 0 | 1 | 0 | 0 | 7 |
| | 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 4 | 0 | 0 | 0 | 2 | 0 | 0 | 7 |
| | 7:30 AM | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 5 |
| | 7:45 AM | 0 | 1 | | | | | | | | 4 | 0 | | | 4 | 0 | | 9 |
| | 8:00 AM | 1 | 0 | | _ | | 0 | | | _ | 2 | 0 | | 0 | 4 | 1 | | 8 |
| | 8:15 AM | 0 | 0 | | • | | 0 | _ | | | 3 | 0 | | 0 | 2 | 0 | | 5 |
| | 8:30 AM | _ | 0 | _ | _ | | 1 | | | • | 1 | 0 | _ | 0 | 3 | 0 | _ | 5 |
| | 8:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 3 | 0 | 0 | 4 |
| | | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| тот | TAL VOLUMES : | 1 | 3 | | | | | | | | | | | | | 1 | | 50 |
| API | PPROACH %'s: | 25.00% | 75.00% | 0.00% | 0.00% | 0.00% | 50.00% | 50.00% | 0.00% | 0.00% | 100.00% | 0.00% | 0.00% | 0.00% | 95.45% | 4.55% | 0.00% | |
| | PEAK HR : | | - MA 00:80 | 09:00 AM | | 00:00 AM | | | | | | | | | | | | TOTAL |
| F | PEAK HR VOL: | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 12 | 1 | 0 | 22 |
| PEAK | K HR FACTOR : | 0.250 | 0.000 | 0.000 | 0.000 | 0.000 | 0.250 | 0.000 | 0.000 | 0.000 | 0.583 | 0.000 | 0.000 | 0.000 | 0.750 | 0.250 | 0.000 | 0.688 |
| | | | 0.25 | 50 | | | 0.2 | 50 | | | 0.58 | 33 | | | 0.6 | 50 | | 0.000 |
| | | | | | | | | | ı | | | | 1 | | | | | |
| | | | | | | | | DOLLINID | | | EVCLD | OHND | | | | | | Ī |
| | | 4 | NORTHBOUND SOUTHBOUND TOURS TO | | | | | | | | | | | | | | | |
| | PM | 1 | 2 | 0 | _ | 1 | 2 | 0 | | 1 | 2 | 1 | | 1 | 2 | 1 | _ | TOTAL |
| | | 1 NL | 2 | 0 NR | NU | | 2 ST | 0 SR | SU | | 2 | 1 ER | EU | _ | 2 WT | 1 WR | _ | TOTAL |
| | 4:00 PM | 1 | 2 | 0 NR 0 | NU O | 0 | 2 ST 0 | 0 SR 0 | SU 0 | 0 | 2 | 1 ER | EU 0 | _ | 2 WT | 1 WR | WU 1 | 10 |
| | 4:00 PM 4:15 PM | 1 | 2 | 0 NR 0 | NU 0 0 | 0 | 2 ST 0 | 0 SR 0 | SU 0 0 | 0 | 2 | 1 ER | EU 0 0 | _ | 2 WT | 1 WR | WU 1 | 10 9 |
| | 4:00 PM 4:15 PM 4:30 PM | 1 | 2 NT 1 1 | 0 NR 0 0 | NU 0 0 0 | 0 0 0 | 2 ST 0 2 0 | 0 SR 0 0 | SU 0 0 0 | 0 | 2 | 1 ER | 0 0 0 | 0 0 0 | 2 WT | 1 WR 0 0 0 | WU 1 0 0 | 10 9 8 5 |
| | 4:00 PM 4:15 PM 4:30 PM 4:45 PM | 1 0 0 1 | 2 NT 1 1 1 0 | 0 NR 0 0 0 | NU 0 0 0 0 | 0 0 0 | 2 ST 0 2 0 | 0 SR 0 0 | SU 0 0 0 0 | 0 0 0 | 2 | 1 ER | EU 0 0 0 0 | 0 0 0 | 2 WT | 1 WR 0 0 0 | WU 1 0 0 0 | 10 9 8 5 |
| | 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM | 1 0 0 1 | 2 NT 1 1 1 0 | 0 NR 0 0 0 | NU 0 0 0 0 | 0 0 0 0 | 2 ST 0 2 0 | 0 SR 0 0 0 0 | SU 0 0 0 0 0 | 0 0 0 | 2 | 1 ER | EU 0 0 0 0 | 0 0 0 | 2 WT | 1 WR 0 0 0 | WU 1 0 0 0 0 | 10 9 8 5 |
| | 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM | 1 0 0 1 | 2 NT 1 1 1 0 | 0 NR 0 0 0 | NU 0 0 0 0 0 | 0 0 0 0 0 | 2 ST 0 2 0 | 0 SR 0 0 0 0 | SU 0 0 0 0 0 | 0 0 0 0 | 2 | 1 ER | EU 0 0 0 0 | 0 0 0 | 2 WT | 1 WR 0 0 0 | WU 1 0 0 0 0 0 0 | 10 9 8 5 |
| | 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM | 1 0 0 1 0 0 | 2 NT 1 1 1 0 | 0 NR 0 0 0 0 0 | NU 0 0 0 0 0 0 | 0 0 0 0 0 | 2 ST 0 2 0 0 0 | 0 SR 0 0 0 0 0 | SU 0 0 0 0 0 0 | 0 0 0 0 0 0 | 2 | 1 ER | EU 0 0 0 0 0 0 | 0 0 0 | 2 WT | 1 WR 0 0 0 0 0 0 | WU 1 0 0 0 0 0 0 0 0 | 10 9 8 5 9 7 |
| | 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM | 1 0 0 1 0 0 0 | 2 NT 1 1 1 0 2 0 1 | 0 NR 0 0 0 0 0 0 | NU 0 0 0 0 0 0 0 | 0 0 0 0 0 0 | 2 ST 0 2 0 0 0 1 0 | 0 SR 0 0 0 0 1 0 0 | SU 0 0 0 0 0 0 | 0 0 0 0 0 0 | 2 ET 4 1 5 3 3 2 2 1 | 1 ER 0 0 0 0 1 1 0 | EU 0 0 0 0 0 0 0 | 0 0 0 0 0 1 0 | 2 WT 3 5 2 1 2 2 0 1 | 1 WR 0 0 0 0 0 0 | WU 1 0 0 0 0 0 0 0 0 | 10 9 8 5 9 7 3 |
| | 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM | 1 0 0 1 0 0 0 | 2 NT 1 1 1 0 2 0 1 0 | 0 NR 0 0 0 0 0 0 | NU 0 0 0 0 0 0 0 | 0 0 0 0 0 0 0 | 2 ST 0 2 0 0 0 1 0 0 | 0 SR 0 0 0 0 1 0 0 | SU 0 0 0 0 0 0 0 0 | 0 0 0 0 0 0 0 | 2 ET 4 1 5 3 3 2 2 1 | 1 ER 0 0 0 0 1 1 1 0 0 | EU 0 0 0 0 0 0 0 | 0 0 0 0 0 1 0 | 2 WT 3 5 2 1 2 2 0 1 | 1 WR 0 0 0 0 0 0 | WU 1 0 0 0 0 0 0 0 0 | 10 9 8 5 9 7 3 2 |
| тот | 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM | 1 0 0 1 0 0 0 | 2 NT 1 1 1 0 2 0 1 0 | 0 NR 0 0 0 0 0 0 0 | NU 0 0 0 0 0 0 0 | 0 0 0 0 0 0 0 0 SL 0 | 2 ST 0 2 0 0 0 1 0 0 ST 3 | 0 SR 0 0 0 0 1 0 0 0 SR 1 | SU 0 0 0 0 0 0 0 0 SU 0 | 0 0 0 0 0 0 0 | 2 ET 4 1 5 3 3 2 2 1 | 1 ER 0 0 0 0 1 1 0 0 | EU 0 0 0 0 0 0 0 0 | 0 0 0 0 1 0 0 | 2 WT 3 5 2 1 2 2 0 1 | 1 WR 0 0 0 0 0 0 0 0 | WU 1 0 0 0 0 0 0 0 0 WU 1 | 10 9 8 5 9 7 3 2 TOTAL 53 |
| тот | 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM | 1 0 0 1 0 0 0 0 NL 2 25.00% | 2 NT 1 1 1 0 2 0 1 0 NT 6 75.00% | 0 NR 0 0 0 0 0 0 0 0 0 0 0 0 | NU 0 0 0 0 0 0 0 | 0 0 0 0 0 0 0 0 SL 0 | 2 ST 0 2 0 0 0 1 0 0 ST 3 | 0 SR 0 0 0 0 1 0 0 0 SR 1 | SU 0 0 0 0 0 0 0 0 SU 0 | 0 0 0 0 0 0 0 | 2 ET 4 1 5 3 3 2 2 1 | 1 ER 0 0 0 0 1 1 0 0 | EU 0 0 0 0 0 0 0 0 | 0 0 0 0 1 0 0 | 2 WT 3 5 2 1 2 2 0 1 | 1 WR 0 0 0 0 0 0 0 0 | WU 1 0 0 0 0 0 0 0 0 WU 1 | 10 9 8 5 9 7 3 2 TOTAL 53 |
| TOT, API | 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM | 1 0 0 1 0 0 0 0 NL 2 25.00% | 2 NT 1 1 1 0 2 0 1 0 NT 6 75.00% | 0 NR 0 0 0 0 0 0 0 0 0 0 0 0 | NU 0 0 0 0 0 0 0 | 0 0 0 0 0 0 0 0 SL 0 | 2 ST 0 2 0 0 0 1 0 0 ST 3 | 0 SR 0 0 0 0 1 0 0 0 SR 1 | SU 0 0 0 0 0 0 0 0 SU 0 | 0 0 0 0 0 0 0 | 2 ET 4 1 5 3 3 2 2 1 | 1 ER 0 0 0 0 1 1 0 0 | EU 0 0 0 0 0 0 0 0 | 0 0 0 0 1 0 0 | 2 WT 3 5 2 1 2 2 0 1 | 1 WR 0 0 0 0 0 0 0 0 | WU 1 0 0 0 0 0 0 0 0 WU 1 | 10 9 8 5 9 7 3 2 TOTAL 53 |
| TOTA API | 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM | 1 0 0 1 0 0 0 0 NL 2 25.00% | 2 NT 1 1 1 0 2 0 1 0 NT 6 75.00% | 0 NR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | NU 0 0 0 0 0 0 0 0 0 0 0 | 0 0 0 0 0 0 0 0 SL 0 0.00% | 2 ST 0 2 0 0 1 0 0 ST 3 75.00% | 0 SR 0 0 0 0 1 0 0 0 SR 1 | SU 0 0 0 0 0 0 0 0 0 0 0 0 0 | 0 0 0 0 0 0 0 0 EL 0 0.00% | 2 ET 4 1 5 3 2 2 1 ET 21 91.30% | 1 ER 0 0 0 0 1 1 0 0 ER 2 8.70% | EU 0 0 0 0 0 0 0 0 0 EU 0 0.00% | 0 0 0 0 1 0 0 | 2 WT 3 5 2 1 2 2 0 1 WT 16 88.89% | 1 WR 0 0 0 0 0 0 0 0 0 0 0 0 | WU 1 0 0 0 0 0 0 0 0 WU 1 5.56% | 10 9 8 5 9 7 3 2 TOTAL 53 |

Downey Ave & Rosecrans Ave

Peak Hour Turning Movement Count



ATTACHMENT B - LOS CALCULATION SHEETS

AltAir Renewable Fuels Project Traffic Impact Analysis

Existing LOS Calculation Sheets

Int #: 1

North/South Street: Lakewood Boulevard East/West Street: Somerset Boulevard

Scenario: Existing

| Thru Lane: | 1600 vph | N-S Split Phase : | N |
|------------------|----------|-------------------------|----|
| Left-Turn Lane: | 1600 vph | E-W Split Phase : | Ν |
| Dual LT Penalty: | 10 % | Lost Time (% of cycle): | 10 |

| Peak Period: | AM PEAK H | HOUR | | | | | |
|--------------|-----------|-------|--------|----------|---------|------------|---------|
| Approach | Movement | Lanes | Volume | Capacity | V/C | ICU ANA | LYSIS |
| Southbound | RT | 0.00 | 203 | 0 | 0.000 | N-S(1): | 0.392 |
| | TH | 2.00 | 970 | 3,200 | 0.367 * | N-S(2): | 0.426 * |
| | LT | 1.00 | 95 | 1,600 | 0.059 | E-W(1): | 0.258 |
| Westbound | RT | 0.00 | 136 | 0 | 0.000 | E-W(2): | 0.284 * |
| | TH | 2.00 | 551 | 3,200 | 0.215 * | | |
| | LT | 1.00 | 176 | 1,600 | 0.110 | V/C: | 0.710 |
| Northbound | RT | 0.00 | 181 | 0 | 0.000 | Lost Time: | 0.100 |
| | TH | 2.00 | 883 | 3,200 | 0.333 | | |
| | LT | 1.00 | 94 | 1,600 | 0.059 * | | |
| Eastbound | RT | 0.00 | 113 | 0 | 0.000 | ICU: | 0.810 |
| | TH | 2.00 | 361 | 3,200 | 0.148 | | |
| | LT | 1.00 | 111 | 1,600 | 0.069 * | LOS: | D |

| Peak Period: | PM PEAK H | IOUR | | | | | |
|--------------|-----------|-------|--------|----------|---------|------------|---------|
| Approach | Movement | Lanes | Volume | Capacity | V/C | ICU ANA | LYSIS |
| Southbound | RT | 0.00 | 171 | 0 | 0.000 | N-S(1): | 0.487 * |
| | TH | 2.00 | 908 | 3,200 | 0.337 | N-S(2): | 0.390 |
| | LT | 1.00 | 256 | 1,600 | 0.160 * | E-W(1): | 0.300 * |
| Westbound | RT | 0.00 | 138 | 0 | 0.000 | E-W(2): | 0.249 |
| | TH | 2.00 | 361 | 3,200 | 0.156 | | |
| | LT | 1.00 | 83 | 1,600 | 0.052 * | V/C: | 0.787 |
| Northbound | RT | 0.00 | 198 | 0 | 0.000 | Lost Time: | 0.100 |
| | TH | 2.00 | 848 | 3,200 | 0.327 * | | |
| | LT | 1.00 | 85 | 1,600 | 0.053 | | |
| Eastbound | RT | 0.00 | 133 | 0 | 0.000 | ICU: | 0.887 |
| | TH | 2.00 | 660 | 3,200 | 0.248 * | | |
| | LT | 1.00 | 149 | 1,600 | 0.093 | LOS: | D |

^{* =} Critical Movement

Int #: 2

North/South Street: Lakewood Boulevard East/West Street: Rosecrans Avenue

Scenario: Existing

| Thru Lane: | 1600 vph | N-S Split Phase : | Ν |
|------------------|----------|-------------------------|----|
| Left-Turn Lane: | 1600 vph | E-W Split Phase : | Ν |
| Dual LT Penalty: | 10 % | Lost Time (% of cycle): | 10 |

| Peak Period: | AM PEAK H | IOUR | | | | | |
|--------------|-----------|-------|--------|----------|---------|------------|---------|
| Approach | Movement | Lanes | Volume | Capacity | V/C | ICU ANA | LYSIS |
| Southbound | RT | 1.00 | 101 | 1,600 | 0.000 | N-S(1): | 0.361 * |
| | TH | 2.00 | 698 | 3,200 | 0.218 | N-S(2): | 0.262 |
| | LT | 1.00 | 232 | 1,600 | 0.145 * | E-W(1): | 0.190 |
| Westbound | RT | 0.00 | 110 | 0 | 0.000 | E-W(2): | 0.226 * |
| | TH | 2.00 | 383 | 3,200 | 0.154 * | | |
| | LT | 1.00 | 148 | 1,600 | 0.093 | V/C: | 0.587 |
| Northbound | RT | 0.00 | 114 | 0 | 0.000 | Lost Time: | 0.100 |
| | TH | 2.00 | 578 | 3,200 | 0.216 * | | |
| | LT | 1.00 | 71 | 1,600 | 0.044 | | |
| Eastbound | RT | 1.00 | 63 | 1,600 | 0.000 | ICU: | 0.687 |
| | TH | 2.00 | 311 | 3,200 | 0.097 | | |
| | LT | 1.00 | 115 | 1,600 | 0.072 * | LOS: | В |
| | | | | | | | |

| Peak Period: | PM PEAK H | IOUR | | | | | |
|--------------|-----------|-------|--------|----------|---------|------------|---------|
| Approach | Movement | Lanes | Volume | Capacity | V/C | ICU ANA | LYSIS |
| Southbound | RT | 1.00 | 198 | 1,600 | 0.000 | N-S(1): | 0.440 * |
| | TH | 2.00 | 816 | 3,200 | 0.255 | N-S(2): | 0.330 |
| | LT | 1.00 | 246 | 1,600 | 0.154 * | E-W(1): | 0.312 |
| Westbound | RT | 0.00 | 159 | 0 | 0.000 | E-W(2): | 0.370 * |
| | TH | 2.00 | 534 | 3,200 | 0.217 * | | |
| | LT | 1.00 | 168 | 1,600 | 0.105 | V/C: | 0.810 |
| Northbound | RT | 0.00 | 150 | 0 | 0.000 | Lost Time: | 0.100 |
| | TH | 2.00 | 766 | 3,200 | 0.286 * | | |
| | LT | 1.00 | 120 | 1,600 | 0.075 | | |
| Eastbound | RT | 1.00 | 79 | 1,600 | 0.000 | ICU: | 0.910 |
| | TH | 2.00 | 662 | 3,200 | 0.207 | | |
| | LT | 1.00 | 244 | 1,600 | 0.153 * | LOS: | Е |

^{* =} Critical Movement

Int #: 3

North/South Street: Downey Avenue East/West Street: Somerset Boulevard

Scenario: Existing

| Thru Lane: | 1600 vph | N-S Split Phase : | N |
|------------------|----------|-------------------------|----|
| Left-Turn Lane: | 1600 vph | E-W Split Phase : | Ν |
| Dual LT Penalty: | 10 % | Lost Time (% of cycle): | 10 |

| | | | | | | | |
|--------------|-----------|-------|--------|----------|---------|-------------|---------|
| | | | | | | | |
| Peak Period: | AM PEAK H | IOUR | | | | | |
| Approach | Movement | Lanes | Volume | Capacity | V/C | ICU ANAL | YSIS |
| Southbound | RT | 0.00 | 82 | 0 | 0.000 | N-S(1): | 0.157 |
| | TH | 2.00 | 329 | 3,200 | 0.128 * | N-S(2): | 0.167 * |
| | LT | 1.00 | 70 | 1,600 | 0.044 | E-W(1): | 0.163 * |
| Westbound | RT | 0.00 | 66 | 0 | 0.000 | E-W(2): | 0.162 |
| | TH | 2.00 | 337 | 3,200 | 0.126 | | |
| | LT | 1.00 | 67 | 1,600 | 0.042 * | V/C: | 0.330 |
| Northbound | RT | 0.00 | 55 | 0 | 0.000 | Lost Time: | 0.100 |
| | TH | 2.00 | 307 | 3,200 | 0.113 | | |
| | LT | 1.00 | 62 | 1,600 | 0.039 * | | |
| Eastbound | RT | 0.00 | 64 | 0 | 0.000 | ICU: | 0.430 |
| | TH | 2.00 | 324 | 3,200 | 0.121 * | | |
| | LT | 1.00 | 58 | 1,600 | 0.036 | LOS: | Α |
| | | | | | | | |
| Peak Period: | PM PEAK H | IOUR | | | | | |
| Approach | Movement | Lanes | Volume | Capacity | V/C | ICU ANAL | YSIS |
| Southbound | RT | 0.00 | 90 | 0 | 0.000 | N-S(1): | 0.258 * |
| | TH | 2.00 | 485 | 3,200 | 0.180 | N-S(2): | 0.248 |
| | LT | 1.00 | 92 | 1,600 | 0.058 * | E-W(1): | 0.302 * |
| Westbound | RT | 0.00 | 63 | 0 | 0.000 | E-W(2): | 0.234 |

^{(2).} TH 2.00 412 3,200 0.148 1.00 LT 82 1,600 0.051 * V/C: 0.560 Northbound RT 0.00 93 0 0.000 Lost Time: 0.100 ΤH 2.00 546 3,200 0.200 * LT 1.00 109 1,600 0.068 Eastbound RT 0.00 105 0 0.000 ICU: 0.660 2.00 697 TH 3,200 0.251 * LT 1.00 138 1,600 0.086 LOS: В

^{* =} Critical Movement

Int #:

North/South Street: Downey Avenue East/West Street: Rosecrans Avenue

Scenario: **Existing**

| Thru Lane: | 1600 vph | N-S Split Phase : | N |
|------------------|----------|-------------------------|----|
| Left-Turn Lane: | 1600 vph | E-W Split Phase : | Ν |
| Dual LT Penalty: | 10 % | Lost Time (% of cycle): | 10 |

| Dual LT Penalty | <u>r: 10</u> | % | | | Lost Time | (% of cycle): | 10 |
|-----------------|--------------|-------|--------|----------|-----------|---------------|---------|
| | | | | | | | |
| Peak Period: | AM PEAK H | | | | | | |
| Approach | Movement | Lanes | Volume | Capacity | V/C | ICU ANA | LYSIS |
| Southbound | RT | 0.00 | 50 | 0 | 0.000 | N-S(1): | 0.211 * |
| | TH | 2.00 | 269 | 3,200 | 0.100 | N-S(2): | 0.162 |
| | LT | 1.00 | 155 | 1,600 | 0.097 * | E-W(1): | 0.191 * |
| Westbound | RT | 1.00 | 83 | 1,600 | 0.000 | E-W(2): | 0.168 |
| | TH | 2.00 | 473 | 3,200 | 0.148 | | |
| | LT | 1.00 | 69 | 1,600 | 0.043 * | V/C: | 0.402 |
| Northbound | RT | 0.00 | 81 | 0 | 0.000 | Lost Time: | 0.100 |
| | TH | 2.00 | 284 | 3,200 | 0.114 * | | |
| | LT | 1.00 | 99 | 1,600 | 0.062 | | |
| Eastbound | RT | 1.00 | 60 | 1,600 | 0.000 | ICU: | 0.502 |
| | TH | 2.00 | 473 | 3,200 | 0.148 * | | |
| | LT | 1.00 | 32 | 1,600 | 0.020 | LOS: | Α |
| | | | | | | | |
| Peak Period: | PM PEAK F | IOUR | | | | | |
| Approach | Movement | Lanes | Volume | Capacity | V/C | ICU ANA | LYSIS |
| Southbound | RT | 0.00 | 69 | 0 | 0.000 | N-S(1): | 0.274 * |
| | TH | 2.00 | 408 | 3,200 | 0.149 | N-S(2): | 0.210 |
| | LT | 1.00 | 173 | 1,600 | 0.108 * | E-W(1): | 0.355 * |
| Westbound | RT | 1.00 | 177 | 1,600 | 0.003 | E-W(2): | 0.289 |
| | TH | 2.00 | 720 | 3,200 | 0.225 | | |
| | LT | 1.00 | 92 | 1,600 | 0.058 * | V/C: | 0.629 |
| Northbound | RT | 0.00 | 99 | 0 | 0.000 | Lost Time: | 0.100 |
| | TH | 2.00 | 431 | 3,200 | 0.166 * | | |
| | LT | 1.00 | 98 | 1,600 | 0.061 | | |
| Eastbound | RT | 1.00 | 127 | 1,600 | 0.018 | ICU: | 0.729 |
| | TH | 2.00 | 950 | 3,200 | 0.297 * | | |
| | LT | 1.00 | 103 | 1,600 | 0.064 | LOS: | С |

^{* =} Critical Movement

Existing Plus Project LOS Calculation Sheets

Int #: 1

North/South Street: Lakewood Boulevard East/West Street: Somerset Boulevard

Scenario: Existing Plus Project

| Thru Lane: | 1600 vph | N-S Split Phase : | N |
|------------------|----------|-------------------------|----|
| Left-Turn Lane: | 1600 vph | E-W Split Phase : | Ν |
| Dual LT Penalty: | 10 % | Lost Time (% of cycle): | 10 |

| Peak Period: | AM PEAK H | IOUR | | | | | |
|--------------|-----------|-------|--------|----------|---------|------------|---------|
| Approach | Movement | Lanes | Volume | Capacity | V/C | ICU ANA | LYSIS |
| Southbound | RT | 0.00 | 203 | 0 | 0.000 | N-S(1): | 0.392 |
| | TH | 2.00 | 1,036 | 3,200 | 0.387 * | N-S(2): | 0.466 * |
| | LT | 1.00 | 95 | 1,600 | 0.059 | E-W(1): | 0.258 |
| Westbound | RT | 0.00 | 136 | 0 | 0.000 | E-W(2): | 0.284 * |
| | TH | 2.00 | 551 | 3,200 | 0.215 * | | |
| | LT | 1.00 | 176 | 1,600 | 0.110 | V/C: | 0.750 |
| Northbound | RT | 0.00 | 181 | 0 | 0.000 | Lost Time: | 0.100 |
| | TH | 2.00 | 883 | 3,200 | 0.333 | | |
| | LT | 1.00 | 127 | 1,600 | 0.079 * | | |
| Eastbound | RT | 0.00 | 113 | 0 | 0.000 | ICU: | 0.850 |
| | TH | 2.00 | 361 | 3,200 | 0.148 | | |
| | LT | 1.00 | 111 | 1,600 | 0.069 * | LOS: | D |

| Peak Period: | PM PEAK H | IOUR | | | | | |
|--------------|-----------|-------|--------|----------|---------|------------|---------|
| Approach | Movement | Lanes | Volume | Capacity | V/C | ICU ANA | LYSIS |
| Southbound | RT | 0.00 | 171 | 0 | 0.000 | N-S(1): | 0.487 * |
| | TH | 2.00 | 974 | 3,200 | 0.358 | N-S(2): | 0.432 |
| | LT | 1.00 | 256 | 1,600 | 0.160 * | E-W(1): | 0.300 * |
| Westbound | RT | 0.00 | 138 | 0 | 0.000 | E-W(2): | 0.249 |
| | TH | 2.00 | 361 | 3,200 | 0.156 | | |
| | LT | 1.00 | 83 | 1,600 | 0.052 * | V/C: | 0.787 |
| Northbound | RT | 0.00 | 198 | 0 | 0.000 | Lost Time: | 0.100 |
| | TH | 2.00 | 848 | 3,200 | 0.327 * | | |
| | LT | 1.00 | 118 | 1,600 | 0.074 | | |
| Eastbound | RT | 0.00 | 133 | 0 | 0.000 | ICU: | 0.887 |
| | TH | 2.00 | 660 | 3,200 | 0.248 * | | |
| | LT | 1.00 | 149 | 1,600 | 0.093 | LOS: | D |

^{* =} Critical Movement

Int #: 2

North/South Street: Lakewood Boulevard East/West Street: Rosecrans Avenue

Scenario: Existing Plus Project

| Thru Lane: | 1600 vph | N-S Split Phase : | N |
|------------------|----------|-------------------------|----|
| Left-Turn Lane: | 1600 vph | E-W Split Phase : | N |
| Dual LT Penalty: | 10 % | Lost Time (% of cycle): | 10 |

| Peak Period: | AM PEAK H | HOUR | | | | | |
|--------------|-----------|-------|--------|----------|---------|------------|---------|
| Approach | Movement | Lanes | Volume | Capacity | V/C | ICU ANA | LYSIS |
| Southbound | RT | 1.00 | 101 | 1,600 | 0.000 | N-S(1): | 0.361 * |
| | TH | 2.00 | 731 | 3,200 | 0.228 | N-S(2): | 0.272 |
| | LT | 1.00 | 232 | 1,600 | 0.145 * | E-W(1): | 0.190 |
| Westbound | RT | 0.00 | 110 | 0 | 0.000 | E-W(2): | 0.226 * |
| | TH | 2.00 | 383 | 3,200 | 0.154 * | | |
| | LT | 1.00 | 148 | 1,600 | 0.093 | V/C: | 0.587 |
| Northbound | RT | 0.00 | 114 | 0 | 0.000 | Lost Time: | 0.100 |
| | TH | 2.00 | 578 | 3,200 | 0.216 * | | |
| | LT | 1.00 | 71 | 1,600 | 0.044 | | |
| Eastbound | RT | 1.00 | 63 | 1,600 | 0.000 | ICU: | 0.687 |
| | TH | 2.00 | 311 | 3,200 | 0.097 | | |
| | LT | 1.00 | 115 | 1,600 | 0.072 * | LOS: | В |
| | | | | | | | |

| Peak Period: | PM PEAK H | IOUR | | | | | |
|--------------|-----------|-------|--------|----------|---------|------------|---------|
| Approach | Movement | Lanes | Volume | Capacity | V/C | ICU ANA | LYSIS |
| Southbound | RT | 1.00 | 198 | 1,600 | 0.000 | N-S(1): | 0.440 * |
| | TH | 2.00 | 849 | 3,200 | 0.265 | N-S(2): | 0.340 |
| | LT | 1.00 | 246 | 1,600 | 0.154 * | E-W(1): | 0.312 |
| Westbound | RT | 0.00 | 159 | 0 | 0.000 | E-W(2): | 0.370 * |
| | TH | 2.00 | 534 | 3,200 | 0.217 * | | |
| | LT | 1.00 | 168 | 1,600 | 0.105 | V/C: | 0.810 |
| Northbound | RT | 0.00 | 150 | 0 | 0.000 | Lost Time: | 0.100 |
| | TH | 2.00 | 766 | 3,200 | 0.286 * | | |
| | LT | 1.00 | 120 | 1,600 | 0.075 | | |
| Eastbound | RT | 1.00 | 79 | 1,600 | 0.000 | ICU: | 0.910 |
| | TH | 2.00 | 662 | 3,200 | 0.207 | | |
| | LT | 1.00 | 244 | 1,600 | 0.153 * | LOS: | Е |

^{* =} Critical Movement

Int #: 3

North/South Street: Downey Avenue East/West Street: Somerset Boulevard

Scenario: Existing Plus Project

LT

RT

ΤH

LT

RT

TH

 LT

1.00

0.00

2.00

1.00

0.00

2.00

1.00

| Thru Lane: | 1600 vph | N-S Split Phase : | N |
|------------------|----------|-------------------------|----|
| Left-Turn Lane: | 1600 vph | E-W Split Phase : | Ν |
| Dual LT Penalty: | 10 % | Lost Time (% of cycle): | 10 |

| Peak Period: | AM PEAK H | IOUR | | | | | |
|--------------|-----------|-------|--------|----------|---------|------------|---------|
| Approach | Movement | Lanes | Volume | Capacity | V/C | ICU ANA | LYSIS |
| Southbound | RT | 0.00 | 82 | 0 | 0.000 | N-S(1): | 0.158 |
| | TH | 2.00 | 329 | 3,200 | 0.128 * | N-S(2): | 0.167 * |
| | LT | 1.00 | 70 | 1,600 | 0.044 | E-W(1): | 0.163 * |
| Westbound | RT | 0.00 | 66 | 0 | 0.000 | E-W(2): | 0.162 |
| | TH | 2.00 | 337 | 3,200 | 0.126 | | |
| | LT | 1.00 | 67 | 1,600 | 0.042 * | V/C: | 0.330 |
| Northbound | RT | 0.00 | 55 | 0 | 0.000 | Lost Time: | 0.100 |
| | TH | 2.00 | 310 | 3,200 | 0.114 | | |
| | LT | 1.00 | 62 | 1,600 | 0.039 * | | |
| Eastbound | RT | 0.00 | 64 | 0 | 0.000 | ICU: | 0.430 |
| | TH | 2.00 | 324 | 3,200 | 0.121 * | | |
| | LT | 1.00 | 58 | 1,600 | 0.036 | LOS: | Α |
| | | | | | | | |
| Peak Period: | PM PEAK F | IOUR | | | | | |
| Approach | Movement | Lanes | Volume | Capacity | V/C | ICU ANA | LYSIS |
| Southbound | RT | 0.00 | 90 | 0 | 0.000 | N-S(1): | 0.259 * |
| | TH | 2.00 | 493 | 3,200 | 0.182 | N-S(2): | 0.250 |
| | LT | 1.00 | 92 | 1,600 | 0.058 * | E-W(1): | 0.302 * |
| Westbound | RT | 0.00 | 63 | 0 | 0.000 | E-W(2): | 0.234 |
| | TH | 2.00 | 412 | 3,200 | 0.148 | | |
| | | | | 1 | 1 | 1 | |

82

93

551

109

105

697

138

1,600

0

3,200

1,600

0

3,200

1,600

0.051 *

0.201 *

0.000

0.068

0.000

0.086

0.251 *

V/C:

ICU:

LOS:

Lost Time:

0.561

0.100

0.661

В

Northbound

Eastbound

^{* =} Critical Movement

Int #: 4

North/South Street: Downey Avenue East/West Street: Rosecrans Avenue

Scenario: Existing Plus Project

| Thru Lane: | 1600 vph | N-S Split Phase : | N |
|------------------|----------|-------------------------|----|
| | • | | |
| Left-Turn Lane: | 1600 vph | E-W Split Phase : | N |
| Dual LT Penalty: | 10 % | Lost Time (% of cycle): | 10 |

| | -,- | | | | | (· · · · · · · · · · · · · · · · · · · | |
|--------------|-----------|-------|--------|----------|---------|---|---------|
| | | | | | | | |
| Peak Period: | AM PEAK H | IOUR | | | | | |
| Approach | Movement | Lanes | Volume | Capacity | V/C | ICU ANA | |
| Southbound | RT | 0.00 | 50 | 0 | 0.000 | N-S(1): | 0.211 * |
| | TH | 2.00 | 272 | 3,200 | 0.101 | N-S(2): | 0.163 |
| | LT | 1.00 | 155 | 1,600 | 0.097 * | E-W(1): | 0.191 * |
| Westbound | RT | 1.00 | 83 | 1,600 | 0.000 | E-W(2): | 0.168 |
| | TH | 2.00 | 473 | 3,200 | 0.148 | | |
| | LT | 1.00 | 69 | 1,600 | 0.043 * | V/C: | 0.402 |
| Northbound | RT | 0.00 | 81 | 0 | 0.000 | Lost Time: | 0.100 |
| | TH | 2.00 | 284 | 3,200 | 0.114 * | | |
| | LT | 1.00 | 99 | 1,600 | 0.062 | | |
| Eastbound | RT | 1.00 | 60 | 1,600 | 0.000 | ICU: | 0.502 |
| | TH | 2.00 | 473 | 3,200 | 0.148 * | | |
| | LT | 1.00 | 32 | 1,600 | 0.020 | LOS: | Α |
| | | | | | | | |
| Peak Period: | PM PEAK H | IOUR | | | | | |
| Approach | Movement | Lanes | Volume | Capacity | V/C | ICU ANA | LYSIS |
| Southbound | RT | 0.00 | 69 | 0 | 0.000 | N-S(1): | 0.276 * |
| | TH | 2.00 | 413 | 3,200 | 0.151 | N-S(2): | 0.212 |
| | LT | 1.00 | 173 | 1,600 | 0.108 * | E-W(1): | 0.355 * |
| Westbound | RT | 1.00 | 177 | 1,600 | 0.003 | E-W(2): | 0.289 |
| | TH | 2.00 | 720 | 3,200 | 0.225 | | |
| | LT | 1.00 | 92 | 1,600 | 0.058 * | V/C: | 0.631 |
| Northbound | RT | 0.00 | 99 | 0 | 0.000 | Lost Time: | 0.100 |
| | TH | 2.00 | 439 | 3,200 | 0.168 * | | |
| | LT | 1.00 | 98 | 1,600 | 0.061 | | |
| Eastbound | RT | 1.00 | 127 | 1,600 | 0.018 | ICU: | 0.731 |
| | TH | 2.00 | 950 | 3,200 | 0.297 * | | |
| | 1 | | l | | | | _ |

^{* =} Critical Movement

LT

1.00

103

1,600

0.064

С

LOS:

Int #: 1

North/South Street: Lakewood Boulevard East/West Street: Somerset Boulevard

Scenario: Existing Plus Project - Restriping of Southbound Approach

| Thru Lane: | 1600 vph | N-S Split Phase : | N |
|------------------|----------|-------------------------|----|
| Left-Turn Lane: | 1600 vph | E-W Split Phase : | Ν |
| Dual LT Penalty: | 10 % | Lost Time (% of cycle): | 10 |

| Peak Period: | AM PEAK H | HOUR | | | | | |
|--------------|-----------|-------|--------|----------|---------|------------|---------|
| Approach | Movement | Lanes | Volume | Capacity | V/C | ICU ANA | LYSIS |
| Southbound | RT | 1.00 | 203 | 1,600 | 0.058 | N-S(1): | 0.392 |
| | TH | 2.00 | 1,036 | 3,200 | 0.324 * | N-S(2): | 0.403 * |
| | LT | 1.00 | 95 | 1,600 | 0.059 | E-W(1): | 0.258 |
| Westbound | RT | 0.00 | 136 | 0 | 0.000 | E-W(2): | 0.284 * |
| | TH | 2.00 | 551 | 3,200 | 0.215 * | | |
| | LT | 1.00 | 176 | 1,600 | 0.110 | V/C: | 0.687 |
| Northbound | RT | 0.00 | 181 | 0 | 0.000 | Lost Time: | 0.100 |
| | TH | 2.00 | 883 | 3,200 | 0.333 | | |
| | LT | 1.00 | 127 | 1,600 | 0.079 * | | |
| Eastbound | RT | 0.00 | 113 | 0 | 0.000 | ICU: | 0.787 |
| | TH | 2.00 | 361 | 3,200 | 0.148 | | |
| | LT | 1.00 | 111 | 1,600 | 0.069 * | LOS: | С |

| Peak Period: | PM PEAK H | IOUR | | | | | |
|--------------|-----------|-------|--------|----------|---------|------------|---------|
| Approach | Movement | Lanes | Volume | Capacity | V/C | ICU ANA | LYSIS |
| Southbound | RT | 1.00 | 171 | 1,600 | 0.014 | N-S(1): | 0.487 * |
| | TH | 2.00 | 974 | 3,200 | 0.304 | N-S(2): | 0.378 |
| | LT | 1.00 | 256 | 1,600 | 0.160 * | E-W(1): | 0.300 * |
| Westbound | RT | 0.00 | 138 | 0 | 0.000 | E-W(2): | 0.249 |
| | TH | 2.00 | 361 | 3,200 | 0.156 | | |
| | LT | 1.00 | 83 | 1,600 | 0.052 * | V/C: | 0.787 |
| Northbound | RT | 0.00 | 198 | 0 | 0.000 | Lost Time: | 0.100 |
| | TH | 2.00 | 848 | 3,200 | 0.327 * | | |
| | LT | 1.00 | 118 | 1,600 | 0.074 | | |
| Eastbound | RT | 0.00 | 133 | 0 | 0.000 | ICU: | 0.887 |
| | TH | 2.00 | 660 | 3,200 | 0.248 * | | |
| | LT | 1.00 | 149 | 1,600 | 0.093 | LOS: | D |

^{* =} Critical Movement

Existing Plus Construction LOS Calculation Sheets

Int #: 1

North/South Street: Lakewood Boulevard East/West Street: Somerset Boulevard

Scenario: Existing Plus Construction

| Thru Lane: | 1600 vph | N-S Split Phase : | N |
|------------------|----------|-------------------------|----|
| Left-Turn Lane: | 1600 vph | E-W Split Phase : | Ν |
| Dual LT Penalty: | 10 % | Lost Time (% of cycle): | 10 |

| Peak Period: | AM PEAK H | IOUR | | | | | |
|--------------|-----------|-------|--------|----------|---------|------------|---------|
| Approach | Movement | Lanes | Volume | Capacity | V/C | ICU ANA | LYSIS |
| Southbound | RT | 0.00 | 203 | 0 | 0.000 | N-S(1): | 0.392 |
| | TH | 2.00 | 1,022 | 3,200 | 0.383 * | N-S(2): | 0.458 * |
| | LT | 1.00 | 95 | 1,600 | 0.059 | E-W(1): | 0.258 |
| Westbound | RT | 0.00 | 136 | 0 | 0.000 | E-W(2): | 0.284 * |
| | TH | 2.00 | 551 | 3,200 | 0.215 * | | |
| | LT | 1.00 | 176 | 1,600 | 0.110 | V/C: | 0.742 |
| Northbound | RT | 0.00 | 181 | 0 | 0.000 | Lost Time: | 0.100 |
| | TH | 2.00 | 883 | 3,200 | 0.333 | | |
| | LT | 1.00 | 120 | 1,600 | 0.075 * | | |
| Eastbound | RT | 0.00 | 113 | 0 | 0.000 | ICU: | 0.842 |
| | TH | 2.00 | 361 | 3,200 | 0.148 | | |
| | LT | 1.00 | 111 | 1,600 | 0.069 * | LOS: | D |

| Peak Period: | PM PEAK H | IOUR | | | | | |
|--------------|-----------|-------|--------|----------|---------|------------|---------|
| Approach | Movement | Lanes | Volume | Capacity | V/C | ICU ANA | LYSIS |
| Southbound | RT | 0.00 | 171 | 0 | 0.000 | N-S(1): | 0.487 * |
| | TH | 2.00 | 960 | 3,200 | 0.353 | N-S(2): | 0.422 |
| | LT | 1.00 | 256 | 1,600 | 0.160 * | E-W(1): | 0.300 * |
| Westbound | RT | 0.00 | 138 | 0 | 0.000 | E-W(2): | 0.249 |
| | TH | 2.00 | 361 | 3,200 | 0.156 | | |
| | LT | 1.00 | 83 | 1,600 | 0.052 * | V/C: | 0.787 |
| Northbound | RT | 0.00 | 198 | 0 | 0.000 | Lost Time: | 0.100 |
| | TH | 2.00 | 848 | 3,200 | 0.327 * | | |
| | LT | 1.00 | 111 | 1,600 | 0.069 | | |
| Eastbound | RT | 0.00 | 133 | 0 | 0.000 | ICU: | 0.887 |
| | TH | 2.00 | 660 | 3,200 | 0.248 * | | |
| | LT | 1.00 | 149 | 1,600 | 0.093 | LOS: | D |

^{* =} Critical Movement

Int #: 2

North/South Street: Lakewood Boulevard East/West Street: Rosecrans Avenue

Scenario: Existing Plus Construction

| Thru Lane: | 1600 vph | N-S Split Phase : | N |
|------------------|----------|-------------------------|----|
| Left-Turn Lane: | 1600 vph | E-W Split Phase : | Ν |
| Dual LT Penalty: | 10 % | Lost Time (% of cycle): | 10 |

| Peak Period: | AM PEAK H | HOUR | | | | | |
|--------------|-----------|-------|--------|----------|---------|------------|---------|
| Approach | Movement | Lanes | Volume | Capacity | V/C | ICU ANA | LYSIS |
| Southbound | RT | 1.00 | 101 | 1,600 | 0.000 | N-S(1): | 0.361 * |
| | TH | 2.00 | 724 | 3,200 | 0.226 | N-S(2): | 0.270 |
| | LT | 1.00 | 232 | 1,600 | 0.145 * | E-W(1): | 0.190 |
| Westbound | RT | 0.00 | 110 | 0 | 0.000 | E-W(2): | 0.226 * |
| | TH | 2.00 | 383 | 3,200 | 0.154 * | | |
| | LT | 1.00 | 148 | 1,600 | 0.093 | V/C: | 0.587 |
| Northbound | RT | 0.00 | 114 | 0 | 0.000 | Lost Time: | 0.100 |
| | TH | 2.00 | 578 | 3,200 | 0.216 * | | |
| | LT | 1.00 | 71 | 1,600 | 0.044 | | |
| Eastbound | RT | 1.00 | 63 | 1,600 | 0.000 | ICU: | 0.687 |
| | TH | 2.00 | 311 | 3,200 | 0.097 | | |
| | LT | 1.00 | 115 | 1,600 | 0.072 * | LOS: | В |
| | | | | · | | | |

| Peak Period: | PM PEAK H | IOUR | | | | | |
|--------------|-----------|-------|--------|----------|---------|------------|---------|
| Approach | Movement | Lanes | Volume | Capacity | V/C | ICU ANA | LYSIS |
| Southbound | RT | 1.00 | 198 | 1,600 | 0.000 | N-S(1): | 0.440 * |
| | TH | 2.00 | 842 | 3,200 | 0.263 | N-S(2): | 0.338 |
| | LT | 1.00 | 246 | 1,600 | 0.154 * | E-W(1): | 0.312 |
| Westbound | RT | 0.00 | 159 | 0 | 0.000 | E-W(2): | 0.370 * |
| | TH | 2.00 | 534 | 3,200 | 0.217 * | | |
| | LT | 1.00 | 168 | 1,600 | 0.105 | V/C: | 0.810 |
| Northbound | RT | 0.00 | 150 | 0 | 0.000 | Lost Time: | 0.100 |
| | TH | 2.00 | 766 | 3,200 | 0.286 * | | |
| | LT | 1.00 | 120 | 1,600 | 0.075 | | |
| Eastbound | RT | 1.00 | 79 | 1,600 | 0.000 | ICU: | 0.910 |
| | TH | 2.00 | 662 | 3,200 | 0.207 | | |
| | LT | 1.00 | 244 | 1,600 | 0.153 * | LOS: | Е |

^{* =} Critical Movement

Int #: 3

North/South Street: Downey Avenue East/West Street: Somerset Boulevard

Scenario: Existing Plus Construction

| Thru Lane: | 1600 vph | N-S Split Phase : | N |
|------------------|----------|-------------------------|----|
| Left-Turn Lane: | 1600 vph | E-W Split Phase : | Ν |
| Dual LT Penalty: | 10 % | Lost Time (% of cycle): | 10 |

| Dual LT Penalty: | 10 | 70 | | | Lost Time | (% of cycle): | 10 |
|------------------|-----------|-------|--------|----------|-----------|---------------|---------|
| | | | | | | | |
| Peak Period: | AM PEAK H | IOUR | | | | | |
| Approach | Movement | Lanes | Volume | Capacity | V/C | ICU ANA | |
| Southbound | RT | 0.00 | 82 | 0 | 0.000 | N-S(1): | 0.157 |
| | TH | 2.00 | 329 | 3,200 | 0.128 * | N-S(2): | 0.167 * |
| | LT | 1.00 | 70 | 1,600 | 0.044 | E-W(1): | 0.184 * |
| Westbound | RT | 0.00 | 66 | 0 | 0.000 | E-W(2): | 0.183 |
| | TH | 2.00 | 403 | 3,200 | 0.147 | | |
| | LT | 1.00 | 67 | 1,600 | 0.042 * | V/C: | 0.351 |
| Northbound | RT | 0.00 | 55 | 0 | 0.000 | Lost Time: | 0.100 |
| | TH | 2.00 | 307 | 3,200 | 0.113 | | |
| | LT | 1.00 | 62 | 1,600 | 0.039 * | | |
| Eastbound | RT | 0.00 | 64 | 0 | 0.000 | ICU: | 0.451 |
| | TH | 2.00 | 390 | 3,200 | 0.142 * | | |
| | LT | 1.00 | 58 | 1,600 | 0.036 | LOS: | Α |
| | | | | | | | |
| Peak Period: | PM PEAK F | IOUR | | | | | |
| Approach | Movement | Lanes | Volume | Capacity | V/C | ICU ANA | LYSIS |
| Southbound | RT | 0.00 | 90 | 0 | 0.000 | N-S(1): | 0.258 * |
| | TH | 2.00 | 485 | 3,200 | 0.180 | N-S(2): | 0.248 |
| | LT | 1.00 | 92 | 1,600 | 0.058 * | E-W(1): | 0.322 * |
| Westbound | RT | 0.00 | 63 | 0 | 0.000 | E-W(2): | 0.255 |
| | TH | 2.00 | 478 | 3,200 | 0.169 | | |
| | LT | 1.00 | 82 | 1,600 | 0.051 * | V/C: | 0.580 |
| Northbound | RT | 0.00 | 93 | 0 | 0.000 | Lost Time: | 0.100 |
| | TH | 2.00 | 546 | 3,200 | 0.200 * | | |
| | LT | 1.00 | 109 | 1,600 | 0.068 | | |
| Eastbound | RT | 0.00 | 105 | 0 | 0.000 | ICU: | 0.680 |

3,200

1,600

0.271 *

LOS:

В

0.086

TH

LT

2.00

1.00

763

138

^{* =} Critical Movement

Int #: 4

North/South Street: Downey Avenue East/West Street: Rosecrans Avenue

Scenario: Existing Plus Construction

| Thru Lane: | 1600 vph | N-S Split Phase : | N |
|------------------|----------|-------------------------|----|
| | • | | |
| Left-Turn Lane: | 1600 vph | E-W Split Phase : | N |
| Dual LT Penalty: | 10 % | Lost Time (% of cycle): | 10 |

| Dual LT Pena | aity: 10 | % | | | Lost Time | (% of cycle): | 10 |
|--------------|-----------|-------|--------|----------|-----------|---------------|---------|
| | | | | | | | |
| Peak Period: | AM PEAK H | HOUR | | | | | |
| Approach | Movement | Lanes | Volume | Capacity | V/C | ICU ANA | LYSIS |
| Southbound | RT | 0.00 | 50 | 0 | 0.000 | N-S(1): | 0.211 * |
| | TH | 2.00 | 272 | 3,200 | 0.101 | N-S(2): | 0.163 |
| | LT | 1.00 | 155 | 1,600 | 0.097 * | E-W(1): | 0.191 * |
| Westbound | RT | 1.00 | 83 | 1,600 | 0.000 | E-W(2): | 0.168 |
| | TH | 2.00 | 473 | 3,200 | 0.148 | | |
| | LT | 1.00 | 69 | 1,600 | 0.043 * | V/C: | 0.402 |
| Northbound | RT | 0.00 | 81 | 0 | 0.000 | Lost Time: | 0.100 |
| | TH | 2.00 | 284 | 3,200 | 0.114 * | | |
| | LT | 1.00 | 99 | 1,600 | 0.062 | | |
| Eastbound | RT | 1.00 | 60 | 1,600 | 0.000 | ICU: | 0.502 |
| | TH | 2.00 | 473 | 3,200 | 0.148 * | | |
| | LT | 1.00 | 32 | 1,600 | 0.020 | LOS: | Α |
| | | | | | | | |
| Peak Period: | PM PEAK F | IOUR | | | | | |
| Approach | Movement | Lanes | Volume | Capacity | V/C | ICU ANA | LYSIS |
| Southbound | RT | 0.00 | 69 | 0 | 0.000 | N-S(1): | 0.276 * |
| | TH | 2.00 | 413 | 3,200 | 0.151 | N-S(2): | 0.212 |
| | LT | 1.00 | 173 | 1,600 | 0.108 * | E-W(1): | 0.355 * |
| Westbound | RT | 1.00 | 177 | 1,600 | 0.003 | E-W(2): | 0.289 |
| | TH | 2.00 | 720 | 3,200 | 0.225 | | |
| | LT | 1.00 | 92 | 1,600 | 0.058 * | V/C: | 0.631 |
| Northbound | RT | 0.00 | 99 | 0 | 0.000 | Lost Time: | 0.100 |
| | TH | 2.00 | 439 | 3,200 | 0.168 * | | |
| | LT | 1.00 | 98 | 1,600 | 0.061 | | |
| Eastbound | RT | 1.00 | 127 | 1,600 | 0.018 | ICU: | 0.731 |
| | TH | 2.00 | 950 | 3,200 | 0.297 * | | |
| | 1 | 1 | l | l | l | | _ |

^{* =} Critical Movement

LT

1.00

103

1,600

0.064

С

LOS:

ATTACHMENT C – COLLISION DATA 2017-2019

Study Area Collisions Jan 2017- Dec 2019

| | Project | Along | | | | | | | | | Not at | | | | | | Involved With | | Injury | | | |
|-----|----------|---------|--------------------|------------|--------------|----------------|---------|-----------|----------|----------|--------|--------|----------------------|-----------------------|----------------------|--|---------------|----------|--------|----------------|--------|-----------|
| | Driveway | Project | | | | | | | | At Fault | Fault | Tow | | | Type of | | | | | 1 | | Cor |
| Loc | Area | Route | CASE_ID | Date | Primary Road | Secondary Road | In Int. | Direction | Distance | Dir | Dir | Away | Collision Severity | Violation Category | Collision | Ped | Bike | MC | Truck | DUI | Severe | Visible P |
| 1 | Yes | Yes | 8676771 | 7/19/2018 | LAKEWOOD BL | SOMERSET BL | N | N | 74 | S | S | Υ | Other Visible Injury | Unsafe Speed | Rear End | | | | | | 0 | 2 |
| 1 | Yes | Yes | 8406124 | 4/28/2017 | LAKEWOOD BL | SOMERSET BL | N | N | 33 | S | S | N | Complaint of Pain | Unsafe Speed | Rear End | | | | | | 0 | 0 |
| 1 | Yes | Yes | 8920415 | 6/30/2019 | SOMERSET BL | LAKEWOOD BL | N | W | 15 | Е | W | N | Complaint of Pain | Automobile ROW | Head-On | | | | | | 0 | 0 |
| 1 | Yes | Yes | 8956576 | 9/24/2019 | LAKEWOOD BL | SOMERSET BL | N | N | 25 | S | Е | Υ | Other Visible Injury | Traffic Signs or Sig | Sideswipe | | | | | | 0 | 3 |
| 1 | | Yes | 8452911 | 8/24/2017 | LAKEWOOD BL | SOMERSET BL | Υ | | 0 | N | N | Υ | Other Visible Injury | DUI | Rear End | | | | | Υ | 0 | 1 |
| 1 | | Yes | 8975151 | 10/16/2019 | LAKEWOOD BL | SOMERSET BL | N | N | 15 | S | S | Υ | Other Visible Injury | Unsafe Speed | Rear End | | | | | | 0 | 1 |
| 1 | | Yes | 8652302 | 5/24/2018 | LAKEWOOD BL | SOMERSET BL | Y | | 0 | N | N | N | Complaint of Pain | Unsafe Speed | Rear End | | | | | | 0 | 0 |
| 1 | | Yes | 8795339 | | LAKEWOOD BL | SOMERSET BL | N | S | 98 | N | N | N | Complaint of Pain | Unsafe Speed | Rear End | | | | | | 0 | 0 |
| 1 | | Yes | 8531311 | | LAKEWOOD BL | SOMERSET BL | N | S | 25 | S | S | N | Other Visible Injury | Following Too Close | Rear End | | Υ | 1 | | | 0 | 1 |
| 1 | | Yes | 8643425 | | LAKEWOOD BL | SOMERSET BL | N | S | 24 | S | S | N | Complaint of Pain | Following Too Close | Rear End | | | 1 | | | 0 | 0 |
| 1 | | Yes | 9060598 | | LAKEWOOD BL | SOMERSET BL | N | S | 356 | N | N | Y | Complaint of Pain | Following Too Close | Rear End | | | | | | 0 | 0 |
| 1 | | Yes | 8674308 | | | SOMERSET BL | N | S | 200 | S | N | N | Complaint of Pain | Wrong Side of Road | Head-On | | v | + | | | 0 | 0 |
| 1 | | Yes | 8557393 | | LAKEWOOD BL | SOMERSET BL | Y | | 0 | E | S | N | Other Visible Injury | Traffic Signs or Sig | Broadside | | • | + | | | 0 | 2 |
| 1 | | Yes | 8580710 | | SOMERSET BL | LAKEWOOD BL | Y | | 0 | S | W | Y | Other Visible Injury | Traffic Signs or Sig | Broadside | | | + | | | 0 | 1 |
| 1 | | Yes | 8846536 | 3/6/2019 | LAKEWOOD BL | SOMERSET BL | Y | | 0 | S | W | N | Complaint of Pain | Traffic Signs or Sig | Broadside | | | + | | | 0 | 1 |
| 1 | | | | | | SOMERSET BL | Y | | 0 | S | W | Y | | | | | | | | | 0 | 0 |
| 1 | 1 | Yes | 8936237 | | LAKEWOOD BL | | | | 0 | | | | Complaint of Pain | Traffic Signs or Sig | Overturned | - | - | \vdash | | \vdash | 0 | <u> </u> |
| 1 | 1 | | 8540609 | 1/1/2018 | LAKEWOOD BL | SOMERSET BL | Y | | 0 | N E | W | Y | Complaint of Pain | Automobile ROW | Head-On | - | - | \vdash | | \vdash | 0 | <u> </u> |
| 1 | - | | 8667368 | 6/20/2018 | SOMERSET BL | LAKEWOOD BL | | | - | | W | Y | Complaint of Pain | Automobile ROW | Head-On | | | v | | \vdash | 0 | U 1 |
| 1 | 1 | | 8420846 | 6/15/2017 | SOMERSET BL | LAKEWOOD BL | Y | | 0 | E | W | Y | Other Visible Injury | Automobile ROW | Broadside | - | - | Y | | $\vdash\vdash$ | 0 | 1 |
| 1 | <u> </u> | | 8629498 | | SOMERSET BL | LAKEWOOD BL | Y | | 0 | W | S | Y | Other Visible Injury | Automobile ROW | Broadside | | | 1 | | Ш | 0 | 1 |
| 1 | | | 8702265 | 7/27/2018 | SOMERSET BL | LAKEWOOD BL | N | E | 200 | W | W | Y | Complaint of Pain | Automobile ROW | Broadside | | | 1 | | Ш | 0 | 0 |
| 1 | | | 8676775 | 7/23/2018 | SOMERSET BL | LAKEWOOD BL | Υ | | 0 | W | W | N | Complaint of Pain | Ped ROW | Vehicle/Ped | Υ | | | | | 0 | 0 |
| 1 | | | 8982505 | 10/31/2019 | LAKEWOOD BL | SOMERSET BL | Υ | | 0 | W | S | Y | Other Visible Injury | Traffic Signs or Sig | Broadside | | | | | | 0 | 1 |
| 1 | | | 8531281 | | LAKEWOOD BL | SOMERSET BL | Υ | | 0 | W | S | Y | Complaint of Pain | Traffic Signs or Sig | Broadside | | | | | Υ | 0 | 0 |
| 2 | | Yes | 9032244 | 11/19/2019 | LAKEWOOD BL | ROSECRANS AV | Υ | | 0 | - | S | N | Other Visible Injury | 0 | Broadside | Υ | | | | | 0 | 1 |
| 2 | | Yes | 8727099 | 10/2/2018 | LAKEWOOD BL | ROSECRANS AV | N | N | 212 | N | N | Υ | Complaint of Pain | Improper Turning | Rear End | | | | | | 0 | 0 |
| 2 | | Yes | 8910432 | 8/4/2019 | ROSECRANS AV | LAKEWOOD BL | Υ | | 0 | N | W | N | Complaint of Pain | Improper Turning | Broadside | Υ | | | | | 0 | 0 |
| 2 | ! | Yes | 8794530 | 1/10/2019 | LAKEWOOD BL | ROSECRANS AV | Υ | | 0 | N | N | N | Complaint of Pain | Improper Turning | Broadside | | | Υ | | | 0 | 0 |
| 2 | ! | Yes | 8296191 | 1/4/2017 | ROSECRANS AV | LAKEWOOD BL | Υ | | 0 | S | E | Υ | Complaint of Pain | Traffic Signs or Sig | Broadside | | | | | | 0 | 0 |
| 2 | | Yes | 8431497 | 7/19/2017 | LAKEWOOD BL | ROSECRANS AV | N | N | 37 | S | S | Υ | Other Visible Injury | Othr Improper Driving | Rear End | | | | | | 0 | 1 |
| 2 | | Yes | 8332008 | 1/21/2017 | LAKEWOOD BL | ROSECRANS AV | N | N | 300 | N | E | N | Other Visible Injury | Wrong Side of Road | Other | | Υ | | | | 0 | 1 |
| 2 | | Yes | 8377077 | 5/12/2017 | LAKEWOOD BL | ROSECRANS AV | N | N | 143 | S | S | N | Complaint of Pain | Unsafe Speed | Rear End | | | | | | 0 | 0 |
| 2 | | Yes | 8510850 | 11/2/2017 | LAKEWOOD BL | ROSECRANS AV | Υ | | 0 | S | N | Υ | Other Visible Injury | Improper Turning | Broadside | | | | | | 0 | 1 |
| 2 | | Yes | 8629417 | 3/7/2018 | LAKEWOOD BL | ROSECRANS AV | N | S | 83 | N | N | Υ | Complaint of Pain | Automobile ROW | Sideswipe | | | | | | 0 | 0 |
| 2 | | Yes | 8726982 | 8/2/2018 | LAKEWOOD BL | ROSECRANS AV | N | N | 92 | S | S | Υ | Other Visible Injury | Unsafe Speed | Rear End | | | | | | 0 | 1 |
| 2 | | Yes | 8917208 | 6/7/2019 | LAKEWOOD BL | ROSECRANS AV | N | N | 123 | S | S | Υ | Complaint of Pain | Unsafe Speed | Rear End | | | | | | 0 | 0 |
| 2 | | Yes | 8952746 | 9/8/2019 | LAKEWOOD BL | ROSECRANS AV | N | N | 216 | S | S | N | Complaint of Pain | Unsafe Speed | Rear End | | | | | | 0 | 0 |
| 2 | | Yes | 8679484 | 5/7/2018 | ROSECRANS AV | LAKEWOOD BL | Y | | 0 | N | E | N | Other Visible Injury | Automobile ROW | Broadside | | Υ | | | | 0 | 1 |
| 2 | | | 8510858 | | | ROSECRANS AV | Y | | 0 | - | W | Y | Complaint of Pain | 0 | Broadside | | | | | | 0 | 0 |
| 2 | | | 8907951 | 6/6/2019 | LAKEWOOD BL | ROSECRANS AV | N | N | 30 | - | S | N | Complaint of Pain | 0 | Rear End | | | | | | 0 | 0 |
| 2 | | | 8938465 | 8/23/2019 | LAKEWOOD BL | ROSECRANS AV | N | N | 3 | - | E | N | Other Visible Injury | 0 | Vehicle/Ped | γ | | | | | 0 | 1 |
| 2 | | | 8310345 | | | LAKEWOOD BL | N | W | 100 | Е | E | Y | Complaint of Pain | Improper Turning | Rear End | Ė | | + | | | 0 | 1 0 |
| 2 | | | 8790444 | | ROSECRANS AV | LAKEWOOD BL | N | W | 5 | E | E | N | Complaint of Pain | Improper Turning | Sideswipe | | | Υ | | \vdash | 0 | 0 |
| 2 | | | 8938421 | | ROSECRANS AV | LAKEWOOD BL | N | W | 10 | - | E | Y | Complaint of Pain | Improper Turning | Sideswipe | 1 | 1 | † | | \vdash | 0 | 0 |
| 2 | | | 9005428 | 11/8/2019 | ROSECRANS AV | LAKEWOOD BL | N | W | 290 | | S | N | Complaint of Pain | proper running | Other | | v | | | \vdash | 0 | 0 |
| 2 | | Yes | 8529778 | | DOWNEY AV | SOMERSET BL | N | N N | 100 | S | N N | N | Complaint of Pain | Uncafa Spand | Vehicle/Ped | v | 1 | + | | v | 0 | 0 |
| 2 | } | Yes | 8529778 8987132 | | DOWNEY AV | SOMERSET BL | N | N N | 575 | N N | N N | N N | | Unsafe Speed | | - | - | | | | 0 | 0 |
| 3 | | | 8987132 8890425 | | | | N Y | IN | 0 | N N | N S | Y | Complaint of Pain | Improper Turning | Sideswipe | - | - | \vdash | | \vdash | 0 | 0 |
| 3 | - | Yes | | | DOWNEY AV | SOMERSET BL | Y | | 0 | N | S S | Y | Complaint of Pain | Traffic Signs or Sig | Head-On Proadside | | - | + | | \vdash | 0 | - 0 |
| 3 | 1 | Yes | 8611659 | 4/2/2018 | DOWNEY AV | SOMERSET BL | | F | 10 | | - | | Other Visible Injury | Traffic Signs or Sig | Broadside | <u> </u> | | 1 | | \vdash | U | 1 |
| 3 | - | | 9007805 | | DOWNEY AV | SOMERSET BL | N | | | - | N | N | Complaint of Pain | 0 | Rear End | | ., | 1 | | \vdash | 0 | U |
| 3 | | | 8782077 | 11/28/2018 | SOMERSET BL | DOWNEY AV | N | E | 75 | - | E | N | Complaint of Pain | 0 | Broadside | <u> </u> | Y | 1 | | Ш | 0 | 0 |
| 3 | | | 8722567 | 10/2/2018 | SOMERSET BL | DOWNEY AV | N | W | 75 | E | W | N | Complaint of Pain | Wrong Side of Road | Broadside | <u> </u> | Υ | | | \vdash | 0 | 0 |
| 3 | | | 8611674 | | DOWNEY AV | SOMERSET BL | Υ | | 0 | W | S | N | Complaint of Pain | Automobile ROW | Broadside | <u> </u> | <u> </u> | . | | \vdash | 0 | 0 |
| 3 | | | 8471379 | | SOMERSET BL | DOWNEY AV | N | E | 400 | E | W | Υ | Complaint of Pain | Automobile ROW | Broadside | | | | | Ш | 0 | 0 |
| 3 | | | 8939876 | | DOWNEY AV | SOMERSET AV | Υ | | 0 | E | S | N | Severe Injury | Traffic Signs or Sig | Broadside | | | | | | 1 | 0 |
| 4 | | Yes | 8611534 | 3/19/2018 | DOWNEY AV | ROSECRANS BL | N | S | 373 | S | S | Υ | Severe Injury | Automobile ROW | Sideswipe | Υ | | | | | 4 | 0 |
| 4 | | | 8334746 | | ROSECRANS AV | DOWNEY AV | Υ | | 0 | W | S | Υ | Other Visible Injury | DUI | - | | | | | Υ | 0 | 1 |
| 4 | | | 8422624 | 6/16/2017 | ROSECRANS AV | DOWNEY AV | N | E | 350 | W | W | Υ | Other Visible Injury | Unsafe Speed | Rear End | | | | | | 0 | 1 |
| 4 | | | 9000067 | 11/11/2019 | ROSECRANS AV | DOWNEY AV | N | W | 154 | W | W | Υ | Other Visible Injury | Unsafe Speed | Rear End | | | | | | 0 | 2 |
| 4 | | | 8903504 | 7/3/2019 | ROSECRANS AV | DOWNEY AV | N | E | 469 | W | W | Υ | Complaint of Pain | Unsafe Speed | Rear End | | | | | | 0 | 0 |
| | | | 8828198 | | DOWNEY AV | ROSECRANS AV | Υ | | 0 | W | Е | N | Other Visible Injury | Unsafe Speed | Vehicle/Ped | γ | | | | | 0 | 1 |

Study Area Collisions Jan 2017- Dec 2019

| | Project | Along | | | | | | | | | Not at | | | | | | Involv | ed W | ith | | | Injury | |
|-----|----------|---------|---------|------------|--------------|----------------|---------|-----------|----------|----------|--------|------|----------------------|----------------------|-------------|-----|--------|------|-------|--------|---------|---------|---------|
| | Driveway | Project | | | | | | | | At Fault | Fault | Tow | | | Type of | | | | | | | | Comp of |
| Loc | Area | Route | CASE_ID | Date | Primary Road | Secondary Road | In Int. | Direction | Distance | Dir | Dir | Away | Collision Severity | Violation Category | Collision | Ped | Bike | MC | Truck | DUI Se | evere V | /isible | Pain |
| 4 | | | 8643397 | 5/31/2018 | ROSECRANS AV | DOWNEY AV | N | W | 200 | E | Е | N | Other Visible Injury | Following Too Close | - | | | | | | 0 | 1 | 0 |
| 4 | | | 8409043 | 5/13/2017 | ROSECRANS AV | DOWNEY AV | N | E | 150 | W | W | N | Complaint of Pain | Following Too Close | Rear End | | | | | | 0 | 0 | 1 |
| 4 | | | 8603898 | 3/28/2018 | ROSECRANS AV | DOWNEY AV | N | E | 130 | W | N | N | Complaint of Pain | Wrong Side of Road | Head-On | | Υ | | | | 0 | 0 | 1 |
| 4 | | | 8438680 | 8/1/2017 | ROSECRANS AV | DOWNEY AV | N | E | 292 | W | E | N | Other Visible Injury | Wrong Side of Road | Broadside | | Υ | | | | 0 | 1 | 0 |
| 4 | | | 8692606 | 8/31/2018 | ROSECRANS AV | DOWNEY AV | N | E | 1300 | E | W | Υ | Complaint of Pain | Automobile ROW | - | | | Υ | | | 0 | 0 | 1 |
| 4 | | | 8853312 | 4/12/2019 | DOWNEY AV | ROSECRANS AV | N | S | 340 | E | S | Υ | Complaint of Pain | Automobile ROW | Broadside | | | | Υ | | 0 | 0 | 1 |
| 4 | | | 8580764 | 2/28/2018 | ROSECRANS AV | DOWNEY AV | N | E | 3 | W | S | N | Other Visible Injury | Ped ROW | Vehicle/Ped | Υ | | | | | 0 | 1 | 0 |
| 4 | | | 8473394 | 10/14/2017 | DOWNEY AV | ROSECRANS AV | Υ | | 0 | Е | N | Υ | Complaint of Pain | Traffic Signs or Sig | Head-On | | | | | | 0 | 0 | 1 |
| 4 | | | 9045831 | 11/23/2019 | DOWNEY AV | ROSECRANS AV | Υ | | 0 | - | S | Υ | Complaint of Pain | Traffic Signs or Sig | Sideswipe | | | | | | 0 | 0 | 1 |
| 4 | | | 8903508 | 7/4/2019 | DOWNEY AV | ROSECRANS BL | Υ | | 0 | W | S | Υ | Other Visible Injury | Traffic Signs or Sig | Broadside | | | | | | 0 | 5 | 0 |
| 4 | | | 8623596 | 4/16/2018 | DOWNEY AV | ROSECRANS BL | Υ | | 0 | E | S | Υ | Complaint of Pain | Traffic Signs or Sig | Broadside | | | | | | 0 | 0 | 1 |

ATTACHMENT D –QUEUEING AND STACKING ANALYSIS

Existing Conditions PM Peak Hour Signal Timing Sheet Scenario

1: Lakewood Blvd & Somerset Blvd Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------|------|------|------|-------|------|------|------|------|------|-------|------|------|
| Stop Del/Veh (s) | 69.7 | 25.1 | 21.2 | 121.8 | 22.9 | 13.3 | 49.8 | 19.8 | 18.6 | 262.9 | 20.3 | 22.4 |

1: Lakewood Blvd & Somerset Blvd Performance by movement

2: Somerset Blvd & Andry Dr Performance by movement

| Movement |
|------------|
| el/Veh (s) |

3: Andry Dr & Exit & Enter Performance by movement

| Movement |
|-------------|
| Del/Veh (s) |

4: Lakewood Blvd & Andry Dr Performance by movement

| Movement |
|------------------|
| Stop Del/Veh (s) |

5: W Santa Ana Crossing & Somerset Blvd Performance by movement

| All |
|-----|
| 0.5 |

6: Lakewood Blvd & W Santa Ana Crossing Performance by movement

| Movement | EBT WB1 | NBT | SBT | All |
|------------------|-----------|-----|-----|-----|
| Stop Del/Veh (s) | 56.5 53.0 | 0.0 | 4.0 | 2.4 |

7: Lakewood Blvd & Paseo St Performance by movement

| Movement | NBT | SBT | All |
|------------------|-----|-----|-----|
| Stop Del/Veh (s) | 3.4 | 0.4 | 2.1 |

8: Exit Performance by movement

9: Enter Performance by movement

| lovement | NBT | All |
|-----------------|---------|-------|
| top Del/Veh (s) | 189.0 2 | 283.6 |

Total Network Performance

| Stop Del/Veh (s) | 63.6 | |
|------------------|------|--|

Intersection: 1: Lakewood Blvd & Somerset Blvd

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | NB | SB | SB | SB |
|-----------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| Directions Served | L | T | TR | L | T | TR | L | Т | TR | L | Т | TR |
| Maximum Queue (ft) | 200 | 280 | 270 | 171 | 336 | 321 | 250 | 436 | 415 | 275 | 360 | 299 |
| Average Queue (ft) | 140 | 205 | 192 | 100 | 149 | 124 | 93 | 232 | 231 | 274 | 333 | 231 |
| 95th Queue (ft) | 238 | 293 | 279 | 184 | 285 | 257 | 209 | 383 | 378 | 276 | 357 | 352 |
| Link Distance (ft) | | 249 | 249 | | 709 | 709 | | 527 | 527 | | 283 | 283 |
| Upstream Blk Time (%) | | 8 | 2 | | | | | | | 44 | 88 | 4 |
| Queuing Penalty (veh) | | 37 | 12 | | | | | | | 0 | 602 | 29 |
| Storage Bay Dist (ft) | 175 | | | 150 | | | 225 | | | 250 | | |
| Storage Blk Time (%) | 11 | 13 | | 14 | 4 | | 0 | 11 | | 95 | 7 | |
| Queuing Penalty (veh) | 37 | 20 | | 26 | 3 | | 0 | 10 | | 439 | 18 | |

Intersection: 2: Somerset Blvd & Andry Dr

| Movement | EB | EB |
|-----------------------|-----|-----|
| Directions Served | T | T |
| Maximum Queue (ft) | 196 | 162 |
| Average Queue (ft) | 30 | 22 |
| 95th Queue (ft) | 144 | 119 |
| Link Distance (ft) | 578 | 578 |
| Upstream Blk Time (%) | | |
| Queuing Penalty (veh) | | |
| Storage Bay Dist (ft) | | |
| Storage Blk Time (%) | | |
| Queuing Penalty (veh) | | |

Intersection: 3: Andry Dr & Exit & Enter

| Movement | EB | NB |
|-----------------------|----|-----|
| Directions Served | TR | TR |
| Maximum Queue (ft) | 24 | 55 |
| Average Queue (ft) | 1 | 5 |
| 95th Queue (ft) | 12 | 29 |
| Link Distance (ft) | 35 | 278 |
| Upstream Blk Time (%) | 0 | |
| Queuing Penalty (veh) | 0 | |
| Storage Bay Dist (ft) | | |
| Storage Blk Time (%) | | |
| Queuing Penalty (veh) | | |

Intersection: 4: Lakewood Blvd & Andry Dr

| Movement | EB | SB | SB |
|-----------------------|-----|-----|-----|
| Directions Served | R | T | TR |
| Maximum Queue (ft) | 46 | 575 | 554 |
| Average Queue (ft) | 12 | 539 | 508 |
| 95th Queue (ft) | 68 | 574 | 652 |
| Link Distance (ft) | 242 | 523 | 523 |
| Upstream Blk Time (%) | | 90 | 14 |
| Queuing Penalty (veh) | | 0 | 0 |
| Storage Bay Dist (ft) | | | |
| Storage Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |

Intersection: 5: W Santa Ana Crossing & Somerset Blvd

| Movement | EB | EB | WB | WB | SE | NW |
|-----------------------|-----|-----|-----|-----|-----|-----|
| Directions Served | Т | T | Т | Т | Т | Т |
| Maximum Queue (ft) | 60 | 14 | 36 | 29 | 36 | 36 |
| Average Queue (ft) | 6 | 0 | 2 | 2 | 7 | 8 |
| 95th Queue (ft) | 30 | 7 | 16 | 14 | 26 | 27 |
| Link Distance (ft) | 499 | 499 | 578 | 578 | 515 | 433 |
| Upstream Blk Time (%) | | | | | | |
| Queuing Penalty (veh) | | | | | | |
| Storage Bay Dist (ft) | | | | | | |
| Storage Blk Time (%) | | | | | | |
| Queuing Penalty (veh) | | | | | | |

Intersection: 6: Lakewood Blvd & W Santa Ana Crossing

| Movement | EB | WB | SB | SB |
|-----------------------|-----|-----|-----|-----|
| Directions Served | T | Т | Т | Т |
| Maximum Queue (ft) | 44 | 44 | 258 | 261 |
| Average Queue (ft) | 8 | 9 | 76 | 93 |
| 95th Queue (ft) | 29 | 30 | 202 | 210 |
| Link Distance (ft) | 549 | 591 | 527 | 527 |
| Upstream Blk Time (%) | | | | |
| Queuing Penalty (veh) | | | | |
| Storage Bay Dist (ft) | | | | |
| Storage Blk Time (%) | | | | |
| Queuing Penalty (veh) | | | | |

Intersection: 7: Lakewood Blvd & Paseo St

| Movement | NB | NB | SB | SB |
|-----------------------|-----|-----|----|----|
| Directions Served | T | T | T | TR |
| Maximum Queue (ft) | 245 | 216 | 30 | 36 |
| Average Queue (ft) | 126 | 90 | 3 | 8 |
| 95th Queue (ft) | 214 | 180 | 16 | 28 |
| Link Distance (ft) | 421 | 421 | 15 | 15 |
| Upstream Blk Time (%) | | | 2 | 6 |
| Queuing Penalty (veh) | | | 11 | 37 |
| Storage Bay Dist (ft) | | | | |
| Storage Blk Time (%) | 3 | | | |
| Queuing Penalty (veh) | 0 | | | |

Intersection: 8: Exit

| Movement | EB |
|-----------------------|-----|
| Directions Served | T |
| Maximum Queue (ft) | 39 |
| Average Queue (ft) | 3 |
| 95th Queue (ft) | 23 |
| Link Distance (ft) | 596 |
| Upstream Blk Time (%) | |
| Queuing Penalty (veh) | |
| Storage Bay Dist (ft) | |
| Storage Blk Time (%) | |
| Queuing Penalty (veh) | |

Intersection: 9: Enter

| Movement | NB |
|-----------------------|----|
| Directions Served | T |
| Maximum Queue (ft) | 56 |
| Average Queue (ft) | 10 |
| 95th Queue (ft) | 41 |
| Link Distance (ft) | 48 |
| Upstream Blk Time (%) | 16 |
| Queuing Penalty (veh) | 0 |
| Storage Bay Dist (ft) | |
| Storage Blk Time (%) | |
| Queuing Penalty (veh) | |

Network Summary

Network wide Queuing Penalty: 1282

Existing Conditions PM Peak Hour Modified Signal Timing Scenario

1: Lakewood Blvd & Somerset Blvd Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------|------|------|------|-------|------|------|------|------|------|------|------|------|
| Stop Del/Veh (s) | 94.9 | 28.9 | 23.9 | 195.2 | 29.0 | 16.2 | 50.0 | 23.7 | 21.8 | 68.8 | 15.5 | 14.2 |

1: Lakewood Blvd & Somerset Blvd Performance by movement

2: Somerset Blvd & Andry Dr Performance by movement

| Movement |
|----------|
| /Veh (s) |

3: Andry Dr & Exit & Enter Performance by movement

| Movement |
|---------------|
| p Del/Veh (s) |

4: Lakewood Blvd & Andry Dr Performance by movement

| Movement | EBR NE | BT SBT | All |
|------------------|--------|---------|-----|
| Stop Del/Veh (s) | 16.6 0 |).1 2.9 | 1.6 |

5: W Santa Ana Crossing & Somerset Blvd Performance by movement

| ovement | EBT WE | T SET | NWT | All |
|----------------|--------|--------|------|-----|
| op Del/Veh (s) | 0.2 0 | 2 29.4 | 20.7 | 0.5 |

6: Lakewood Blvd & W Santa Ana Crossing Performance by movement

| All |
|-----|
| 2 |

7: Lakewood Blvd & Paseo St Performance by movement

| Movement | NBT | SBT | All |
|------------------|-----|-----|-----|
| Stop Del/Veh (s) | 3.7 | 0.4 | 2.1 |

8: Exit Performance by movement

9: Enter Performance by movement

Total Network Performance

| Stop Del/Veh (s) | 36.4 |
|------------------|------|

Intersection: 1: Lakewood Blvd & Somerset Blvd

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | NB | SB | SB | SB |
|-----------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| Directions Served | L | T | TR | L | Т | TR | L | T | TR | L | T | TR |
| Maximum Queue (ft) | 200 | 285 | 281 | 174 | 416 | 375 | 250 | 484 | 465 | 274 | 334 | 292 |
| Average Queue (ft) | 154 | 219 | 207 | 119 | 191 | 166 | 106 | 265 | 254 | 198 | 249 | 221 |
| 95th Queue (ft) | 243 | 303 | 288 | 204 | 386 | 344 | 237 | 435 | 412 | 299 | 342 | 310 |
| Link Distance (ft) | | 249 | 249 | | 709 | 709 | | 527 | 527 | | 283 | 283 |
| Upstream Blk Time (%) | | 14 | 5 | | | | | 0 | 0 | 2 | 11 | 1 |
| Queuing Penalty (veh) | | 69 | 25 | | | | | 1 | 0 | 0 | 73 | 9 |
| Storage Bay Dist (ft) | 175 | | | 150 | | | 225 | | | 250 | | |
| Storage Blk Time (%) | 22 | 15 | | 29 | 4 | | 0 | 15 | | 11 | 7 | |
| Queuing Penalty (veh) | 75 | 23 | | 53 | 3 | | 0 | 13 | | 52 | 19 | |

Intersection: 2: Somerset Blvd & Andry Dr

| Movement | EB | EB |
|-----------------------|-----|-----|
| Directions Served | T | T |
| Maximum Queue (ft) | 257 | 211 |
| Average Queue (ft) | 54 | 40 |
| 95th Queue (ft) | 203 | 172 |
| Link Distance (ft) | 578 | 578 |
| Upstream Blk Time (%) | | |
| Queuing Penalty (veh) | | |
| Storage Bay Dist (ft) | | |
| Storage Blk Time (%) | | |
| Queuing Penalty (veh) | | |

Intersection: 3: Andry Dr & Exit & Enter

| Movement | EB | NB |
|-----------------------|----|-----|
| Directions Served | TR | TR |
| Maximum Queue (ft) | 37 | 52 |
| Average Queue (ft) | 2 | 4 |
| 95th Queue (ft) | 18 | 26 |
| Link Distance (ft) | 35 | 278 |
| Upstream Blk Time (%) | 0 | |
| Queuing Penalty (veh) | 0 | |
| Storage Bay Dist (ft) | | |
| Storage Blk Time (%) | | |
| Queuing Penalty (veh) | | |

Intersection: 4: Lakewood Blvd & Andry Dr

| Movement | EB | SB | SB |
|-----------------------|-----|-----|-----|
| | | JD | |
| Directions Served | R | T | TR |
| Maximum Queue (ft) | 49 | 387 | 302 |
| Average Queue (ft) | 4 | 74 | 46 |
| 95th Queue (ft) | 26 | 300 | 228 |
| Link Distance (ft) | 242 | 523 | 523 |
| Upstream Blk Time (%) | | 0 | 0 |
| Queuing Penalty (veh) | | 0 | 0 |
| Storage Bay Dist (ft) | | | |
| Storage Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |

Intersection: 5: W Santa Ana Crossing & Somerset Blvd

| Movement | EB | EB | WB | WB | SE | NW |
|-----------------------|-----|-----|-----|-----|-----|-----|
| Directions Served | Т | T | T | Т | Т | Т |
| Maximum Queue (ft) | 49 | 20 | 26 | 19 | 36 | 40 |
| Average Queue (ft) | 6 | 1 | 2 | 1 | 8 | 8 |
| 95th Queue (ft) | 29 | 8 | 14 | 9 | 27 | 28 |
| Link Distance (ft) | 499 | 499 | 578 | 578 | 515 | 433 |
| Upstream Blk Time (%) | | | | | | |
| Queuing Penalty (veh) | | | | | | |
| Storage Bay Dist (ft) | | | | | | |
| Storage Blk Time (%) | | | | | | |
| Queuing Penalty (veh) | | | | | | |

Intersection: 6: Lakewood Blvd & W Santa Ana Crossing

| Movement | EB | WB | NB | SB | SB |
|-----------------------|-----|-----|----|-----|-----|
| Directions Served | T | T | T | T | T |
| Maximum Queue (ft) | 40 | 40 | 2 | 309 | 301 |
| Average Queue (ft) | 9 | 7 | 0 | 102 | 116 |
| 95th Queue (ft) | 28 | 25 | 2 | 239 | 244 |
| Link Distance (ft) | 549 | 591 | 15 | 527 | 527 |
| Upstream Blk Time (%) | | | 0 | | |
| Queuing Penalty (veh) | | | 0 | | |
| Storage Bay Dist (ft) | | | | | |
| Storage Blk Time (%) | | | | | |
| Queuing Penalty (veh) | | | | | |

Intersection: 7: Lakewood Blvd & Paseo St

| Movement | NB | NB | SB | SB |
|-----------------------|-----|-----|----|----|
| Directions Served | T | T | T | TR |
| Maximum Queue (ft) | 271 | 245 | 40 | 43 |
| Average Queue (ft) | 136 | 95 | 7 | 10 |
| 95th Queue (ft) | 224 | 188 | 29 | 33 |
| Link Distance (ft) | 421 | 421 | 15 | 15 |
| Upstream Blk Time (%) | | | 5 | 7 |
| Queuing Penalty (veh) | | | 28 | 40 |
| Storage Bay Dist (ft) | | | | |
| Storage Blk Time (%) | 4 | | | |
| Queuing Penalty (veh) | 0 | | | |

Intersection: 8: Exit

| Movement | EB |
|-----------------------|-----|
| Directions Served | Т |
| Maximum Queue (ft) | 54 |
| Average Queue (ft) | 6 |
| 95th Queue (ft) | 34 |
| Link Distance (ft) | 596 |
| Upstream Blk Time (%) | |
| Queuing Penalty (veh) | |
| Storage Bay Dist (ft) | |
| Storage Blk Time (%) | |
| Queuing Penalty (veh) | |

Intersection: 9: Enter

| Movement | NB |
|-----------------------|----|
| Directions Served | T |
| Maximum Queue (ft) | 45 |
| Average Queue (ft) | 7 |
| 95th Queue (ft) | 34 |
| Link Distance (ft) | 48 |
| Upstream Blk Time (%) | 10 |
| Queuing Penalty (veh) | 0 |
| Storage Bay Dist (ft) | |
| Storage Blk Time (%) | |
| Queuing Penalty (veh) | |

Network Summary

Network wide Queuing Penalty: 484

Project Conditions (4 Minute Inbound Gate Time) PM Peak Hour Signal Timing Sheet Scenario

1: Lakewood Blvd & Somerset Blvd Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------|------|------|------|-------|------|------|------|------|------|-------|------|------|
| Stop Del/Veh (s) | 81.8 | 26.9 | 22.4 | 192.1 | 40.6 | 34.3 | 71.9 | 21.0 | 20.0 | 271.5 | 23.2 | 31.5 |

1: Lakewood Blvd & Somerset Blvd Performance by movement

| Movement | All | | |
|------------------|------|--|--|
| Stop Del/Veh (s) | 45.3 | | |

2: Somerset Blvd & Andry Dr Performance by movement

| Movement | WBT WBR | All |
|-----------------|-----------|-----|
| top Del/Veh (s) | 3.0 223.0 | 5.4 |

3: Andry Dr & Exit & Enter Performance by movement

4: Lakewood Blvd & Andry Dr Performance by movement

| Movement | EBR | NBT | SBT | All |
|------------------|-------|-----|------|------|
| Stop Del/Veh (s) | 716.8 | 0.1 | 85.9 | 43.9 |

5: W Santa Ana Crossing & Somerset Blvd Performance by movement

6: Lakewood Blvd & W Santa Ana Crossing Performance by movement

| All |
|-----|
| 2. |

7: Lakewood Blvd & Paseo St Performance by movement

| Movement | T SBT | All |
|----------------|-------|-----|
| op Del/Veh (s) | 8 0.4 | 2.4 |

8: Exit Performance by movement

9: Enter Performance by movement

| Movement | NBT All |
|-------------|-------------|
| Del/Veh (s) | 209.9 209.9 |

Total Network Performance

| Stop Del/Veh (s) | 81.3 | |
|------------------|------|--|

Intersection: 1: Lakewood Blvd & Somerset Blvd

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | NB | SB | SB | SB |
|-----------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| Directions Served | L | T | TR | L | Т | TR | L | T | TR | L | T | TR |
| Maximum Queue (ft) | 200 | 286 | 279 | 174 | 435 | 409 | 250 | 485 | 460 | 275 | 359 | 306 |
| Average Queue (ft) | 144 | 216 | 202 | 115 | 207 | 182 | 143 | 265 | 257 | 274 | 333 | 241 |
| 95th Queue (ft) | 238 | 300 | 286 | 205 | 450 | 421 | 270 | 465 | 441 | 277 | 357 | 358 |
| Link Distance (ft) | | 249 | 249 | | 709 | 709 | | 527 | 527 | | 283 | 283 |
| Upstream Blk Time (%) | | 11 | 4 | | 1 | 1 | | 1 | 0 | 40 | 88 | 7 |
| Queuing Penalty (veh) | | 52 | 18 | | 0 | 0 | | 4 | 1 | 0 | 611 | 50 |
| Storage Bay Dist (ft) | 175 | | | 150 | | | 225 | | | 250 | | |
| Storage Blk Time (%) | 15 | 15 | | 28 | 7 | | 6 | 13 | | 97 | 13 | |
| Queuing Penalty (veh) | 51 | 23 | | 52 | 6 | | 26 | 14 | | 458 | 33 | |

Intersection: 2: Somerset Blvd & Andry Dr

| Movement | EB | EB | WB | WB |
|-----------------------|-----|-----|-----|-----|
| Directions Served | T | T | Т | TR |
| Maximum Queue (ft) | 202 | 162 | 190 | 179 |
| Average Queue (ft) | 41 | 29 | 67 | 87 |
| 95th Queue (ft) | 167 | 132 | 227 | 255 |
| Link Distance (ft) | 578 | 578 | 249 | 249 |
| Upstream Blk Time (%) | | | 2 | 7 |
| Queuing Penalty (veh) | | | 5 | 21 |
| Storage Bay Dist (ft) | | | | |
| Storage Blk Time (%) | | | | |
| Queuing Penalty (veh) | | | | |

Intersection: 3: Andry Dr & Exit & Enter

| Movement | EB | NB |
|-----------------------|----|-----|
| Directions Served | TR | TR |
| Maximum Queue (ft) | 58 | 258 |
| Average Queue (ft) | 32 | 198 |
| 95th Queue (ft) | 58 | 355 |
| Link Distance (ft) | 35 | 278 |
| Upstream Blk Time (%) | 39 | 42 |
| Queuing Penalty (veh) | 9 | 10 |
| Storage Bay Dist (ft) | | |
| Storage Blk Time (%) | | |
| Queuing Penalty (veh) | | |

Intersection: 4: Lakewood Blvd & Andry Dr

| Movement | EB | SB | SB |
|-----------------------|-----|-----|-----|
| Directions Served | R | T | TR |
| Maximum Queue (ft) | 225 | 573 | 558 |
| Average Queue (ft) | 149 | 533 | 495 |
| 95th Queue (ft) | 301 | 605 | 686 |
| Link Distance (ft) | 242 | 523 | 523 |
| Upstream Blk Time (%) | 41 | 88 | 16 |
| Queuing Penalty (veh) | 10 | 0 | 0 |
| Storage Bay Dist (ft) | | | |
| Storage Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |

Intersection: 5: W Santa Ana Crossing & Somerset Blvd

| Movement | EB | EB | WB | WB | SE | NW |
|-----------------------|-----|-----|-----|-----|-----|-----|
| Directions Served | Т | T | T | T | Т | Т |
| Maximum Queue (ft) | 46 | 12 | 28 | 24 | 34 | 40 |
| Average Queue (ft) | 6 | 1 | 3 | 2 | 8 | 9 |
| 95th Queue (ft) | 26 | 7 | 15 | 14 | 27 | 29 |
| Link Distance (ft) | 499 | 499 | 578 | 578 | 515 | 433 |
| Upstream Blk Time (%) | | | | | | |
| Queuing Penalty (veh) | | | | | | |
| Storage Bay Dist (ft) | | | | | | |
| Storage Blk Time (%) | | | | | | |
| Queuing Penalty (veh) | | | | | | |

Intersection: 6: Lakewood Blvd & W Santa Ana Crossing

| Movement | EB | WB | NB | SB | SB |
|-----------------------|-----|-----|----|-----|-----|
| Directions Served | T | T | T | T | Т |
| Maximum Queue (ft) | 41 | 37 | 8 | 262 | 261 |
| Average Queue (ft) | 10 | 8 | 1 | 81 | 95 |
| 95th Queue (ft) | 30 | 26 | 8 | 207 | 207 |
| Link Distance (ft) | 549 | 591 | 15 | 527 | 527 |
| Upstream Blk Time (%) | | | 0 | | |
| Queuing Penalty (veh) | | | 1 | | |
| Storage Bay Dist (ft) | | | | | |
| Storage Blk Time (%) | | | | | |
| Queuing Penalty (veh) | | | | | |

Intersection: 7: Lakewood Blvd & Paseo St

| Movement | NB | NB | SB | SB |
|-----------------------|-----|-----|----|----|
| Directions Served | T | T | Т | TR |
| Maximum Queue (ft) | 272 | 231 | 32 | 36 |
| Average Queue (ft) | 144 | 105 | 3 | 8 |
| 95th Queue (ft) | 237 | 199 | 18 | 28 |
| Link Distance (ft) | 421 | 421 | 15 | 15 |
| Upstream Blk Time (%) | | | 2 | 6 |
| Queuing Penalty (veh) | | | 13 | 37 |
| Storage Bay Dist (ft) | | | | |
| Storage Blk Time (%) | 5 | | | |
| Queuing Penalty (veh) | 0 | | | |

Intersection: 8: Exit

| Movement | EB |
|-----------------------|-----|
| Directions Served | Т |
| Maximum Queue (ft) | 444 |
| Average Queue (ft) | 194 |
| 95th Queue (ft) | 502 |
| Link Distance (ft) | 596 |
| Upstream Blk Time (%) | 9 |
| Queuing Penalty (veh) | 0 |
| Storage Bay Dist (ft) | |
| Storage Blk Time (%) | |
| Queuing Penalty (veh) | |

Intersection: 9: Enter

| Movement | NB |
|-----------------------|----|
| Directions Served | T |
| Maximum Queue (ft) | 77 |
| Average Queue (ft) | 51 |
| 95th Queue (ft) | 69 |
| Link Distance (ft) | 48 |
| Upstream Blk Time (%) | 93 |
| Queuing Penalty (veh) | 21 |
| Storage Bay Dist (ft) | |
| Storage Blk Time (%) | |
| Queuing Penalty (veh) | |

Network Summary

Network wide Queuing Penalty: 1525

Project Conditions (4 Minute Inbound Gate Time) PM Peak Hour Modified Signal Timing Scenario

1: Lakewood Blvd & Somerset Blvd Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------|-------|------|------|-------|------|------|-------|------|------|------|------|------|
| Stop Del/Veh (s) | 119.1 | 31.9 | 27.5 | 351.1 | 46.6 | 48.7 | 111.9 | 25.5 | 24.7 | 67.2 | 20.5 | 30.4 |

1: Lakewood Blvd & Somerset Blvd Performance by movement

| Movement | All | | | |
|------------------|------|--|--|--|
| Stop Del/Veh (s) | 43.4 | | | |

2: Somerset Blvd & Andry Dr Performance by movement

| Movement |
|------------------|
| Stop Del/Veh (s) |

3: Andry Dr & Exit & Enter Performance by movement

| Movement |
|-----------------|
| top Del/Veh (s) |

4: Lakewood Blvd & Andry Dr Performance by movement

| Movement | EBR | NBT | SBT | All |
|------------------|-------|-----|------|-----|
| Stop Del/Veh (s) | 123.2 | 0.1 | 11.1 | 7.1 |

5: W Santa Ana Crossing & Somerset Blvd Performance by movement

6: Lakewood Blvd & W Santa Ana Crossing Performance by movement

| All |
|-----|
| 2 |

7: Lakewood Blvd & Paseo St Performance by movement

| Movement | NBT SBT | All |
|------------------|---------|-----|
| Stop Del/Veh (s) | 8.0 0.4 | 4.3 |

8: Exit Performance by movement

| Movement | EBT All |
|---------------|-------------|
| p Del/Veh (s) | 263.9 253.7 |

9: Enter Performance by movement

Total Network Performance

| Stop Del/Veh (s) | 59.1 | |
|------------------|------|--|

Intersection: 1: Lakewood Blvd & Somerset Blvd

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | NB | SB | SB | SB |
|-----------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| Directions Served | L | T | TR | L | Т | TR | L | T | TR | L | T | TR |
| Maximum Queue (ft) | 200 | 285 | 289 | 174 | 509 | 489 | 250 | 506 | 503 | 275 | 333 | 302 |
| Average Queue (ft) | 163 | 231 | 223 | 137 | 313 | 284 | 143 | 299 | 287 | 209 | 261 | 243 |
| 95th Queue (ft) | 247 | 313 | 304 | 216 | 654 | 618 | 275 | 520 | 502 | 309 | 351 | 322 |
| Link Distance (ft) | | 249 | 249 | | 709 | 709 | | 527 | 527 | | 283 | 283 |
| Upstream Blk Time (%) | | 23 | 9 | | 4 | 3 | | 5 | 2 | 3 | 15 | 8 |
| Queuing Penalty (veh) | | 113 | 43 | | 0 | 0 | | 27 | 9 | 0 | 102 | 57 |
| Storage Bay Dist (ft) | 175 | | | 150 | | | 225 | | | 250 | | |
| Storage Blk Time (%) | 30 | 18 | | 49 | 7 | | 11 | 16 | | 10 | 15 | |
| Queuing Penalty (veh) | 101 | 27 | | 90 | 6 | | 49 | 17 | | 45 | 40 | |

Intersection: 2: Somerset Blvd & Andry Dr

| Movement | EB | EB | WB | WB |
|-----------------------|-----|-----|-----|-----|
| Directions Served | T | T | Т | TR |
| Maximum Queue (ft) | 272 | 245 | 146 | 154 |
| Average Queue (ft) | 91 | 72 | 45 | 72 |
| 95th Queue (ft) | 288 | 246 | 190 | 245 |
| Link Distance (ft) | 578 | 578 | 249 | 249 |
| Upstream Blk Time (%) | | | 1 | 9 |
| Queuing Penalty (veh) | | | 2 | 30 |
| Storage Bay Dist (ft) | | | | |
| Storage Blk Time (%) | | | | |
| Queuing Penalty (veh) | | | | |

Intersection: 3: Andry Dr & Exit & Enter

| Movement | EB | NB |
|-----------------------|----|-----|
| Directions Served | TR | TR |
| Maximum Queue (ft) | 62 | 264 |
| Average Queue (ft) | 31 | 187 |
| 95th Queue (ft) | 59 | 348 |
| Link Distance (ft) | 35 | 278 |
| Upstream Blk Time (%) | 7 | 36 |
| Queuing Penalty (veh) | 2 | 8 |
| Storage Bay Dist (ft) | | |
| Storage Blk Time (%) | | |
| Queuing Penalty (veh) | | |

Intersection: 4: Lakewood Blvd & Andry Dr

| Movement | EB | SB | SB |
|-----------------------|-----|-----|-----|
| Directions Served | R | T | TR |
| Maximum Queue (ft) | 167 | 375 | 344 |
| Average Queue (ft) | 70 | 126 | 97 |
| 95th Queue (ft) | 175 | 426 | 387 |
| Link Distance (ft) | 242 | 523 | 523 |
| Upstream Blk Time (%) | 7 | 6 | 5 |
| Queuing Penalty (veh) | 2 | 0 | 0 |
| Storage Bay Dist (ft) | | | |
| Storage Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |

Intersection: 5: W Santa Ana Crossing & Somerset Blvd

| Movement | EB | EB | WB | WB | SE | NW |
|-----------------------|---------|---------|-----|-----|-----|-----|
| Directions Served | <u></u> | <u></u> | | T | T | |
| Maximum Queue (ft) | 48 | 19 | 25 | 18 | 36 | 38 |
| Average Queue (ft) | 6 | 1 | 2 | 1 | 8 | 8 |
| 95th Queue (ft) | 29 | 9 | 12 | 8 | 27 | 28 |
| Link Distance (ft) | 499 | 499 | 578 | 578 | 515 | 433 |
| Upstream Blk Time (%) | | | | | | |
| Queuing Penalty (veh) | | | | | | |
| Storage Bay Dist (ft) | | | | | | |
| Storage Blk Time (%) | | | | | | |
| Queuing Penalty (veh) | | | | | | |

Intersection: 6: Lakewood Blvd & W Santa Ana Crossing

| Movement | EB | WB | NB | NB | SB | SB |
|-----------------------|-----|-----|----|----|-----|-----|
| Directions Served | T | T | Т | Т | T | Т |
| Maximum Queue (ft) | 39 | 42 | 20 | 10 | 310 | 326 |
| Average Queue (ft) | 9 | 8 | 3 | 1 | 107 | 121 |
| 95th Queue (ft) | 29 | 29 | 18 | 12 | 251 | 261 |
| Link Distance (ft) | 549 | 591 | 15 | 15 | 527 | 527 |
| Upstream Blk Time (%) | | | 4 | 0 | | |
| Queuing Penalty (veh) | | | 21 | 3 | | |
| Storage Bay Dist (ft) | | | | | | |
| Storage Blk Time (%) | | | | | | |
| Queuing Penalty (veh) | | | | | | |

Intersection: 7: Lakewood Blvd & Paseo St

| Movement | NB | NB | SB | SB |
|-----------------------|-----|-----|----|----|
| Directions Served | T | T | T | TR |
| Maximum Queue (ft) | 322 | 274 | 36 | 50 |
| Average Queue (ft) | 158 | 119 | 5 | 9 |
| 95th Queue (ft) | 305 | 273 | 24 | 33 |
| Link Distance (ft) | 421 | 421 | 15 | 15 |
| Upstream Blk Time (%) | 4 | 4 | 4 | 7 |
| Queuing Penalty (veh) | 0 | 0 | 23 | 39 |
| Storage Bay Dist (ft) | | | | |
| Storage Blk Time (%) | 9 | | | |
| Queuing Penalty (veh) | 0 | | | |

Intersection: 8: Exit

| Movement | EB |
|-----------------------|-----|
| Directions Served | T |
| Maximum Queue (ft) | 244 |
| Average Queue (ft) | 110 |
| 95th Queue (ft) | 260 |
| Link Distance (ft) | 596 |
| Upstream Blk Time (%) | |
| Queuing Penalty (veh) | |
| Storage Bay Dist (ft) | |
| Storage Blk Time (%) | |
| Queuing Penalty (veh) | |

Intersection: 9: Enter

| Movement | NB |
|-----------------------|----|
| Directions Served | T |
| Maximum Queue (ft) | 71 |
| Average Queue (ft) | 51 |
| 95th Queue (ft) | 67 |
| Link Distance (ft) | 48 |
| Upstream Blk Time (%) | 93 |
| Queuing Penalty (veh) | 21 |
| Storage Bay Dist (ft) | |
| Storage Blk Time (%) | |
| Queuing Penalty (veh) | |

Network Summary

Network wide Queuing Penalty: 875

Project Conditions (2:30Minute Inbound Gate Time) PM Peak Hour Signal Timing Sheet Scenario

1: Lakewood Blvd & Somerset Blvd Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------|------|------|------|-------|------|------|------|------|------|-------|------|------|
| Stop Del/Veh (s) | 65.6 | 25.4 | 21.4 | 167.6 | 27.9 | 16.1 | 52.6 | 19.7 | 18.5 | 284.2 | 22.8 | 23.3 |

1: Lakewood Blvd & Somerset Blvd Performance by movement

| Movement | All | II | | | | | | | | |
|------------------|------|----|--|--|--|--|--|--|--|--|
| Stop Del/Veh (s) | 41.2 | 2 | | | | | | | | |

2: Somerset Blvd & Andry Dr Performance by movement

| Movement |
|-------------|
| Del/Veh (s) |

3: Andry Dr & Exit & Enter Performance by movement

| Novement |
|-------------|
| Del/Veh (s) |

4: Lakewood Blvd & Andry Dr Performance by movement

| Movement |
|-----------------|
| top Del/Veh (s) |

5: W Santa Ana Crossing & Somerset Blvd Performance by movement

| All |
|-----|
| |

6: Lakewood Blvd & W Santa Ana Crossing Performance by movement

| All |
|-----|
| 2.2 |

7: Lakewood Blvd & Paseo St Performance by movement

| Movement | IBT SBT | All |
|------------------|---------|-----|
| Stop Del/Veh (s) | 3.6 0.4 | 2.2 |

8: Exit Performance by movement

9: Enter Performance by movement

Total Network Performance

| Stop Del/Veh (s) | 70.7 | |
|------------------|------|--|

Intersection: 1: Lakewood Blvd & Somerset Blvd

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | NB | SB | SB | SB |
|-----------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| Directions Served | L | T | TR | L | Т | TR | L | Т | TR | L | T | TR |
| Maximum Queue (ft) | 200 | 276 | 268 | 174 | 383 | 354 | 250 | 461 | 453 | 275 | 357 | 304 |
| Average Queue (ft) | 136 | 204 | 195 | 119 | 182 | 163 | 128 | 239 | 233 | 274 | 332 | 238 |
| 95th Queue (ft) | 231 | 290 | 282 | 204 | 357 | 320 | 250 | 418 | 405 | 275 | 355 | 354 |
| Link Distance (ft) | | 249 | 249 | | 709 | 709 | | 527 | 527 | | 283 | 283 |
| Upstream Blk Time (%) | | 5 | 2 | | | | | 0 | 0 | 42 | 89 | 5 |
| Queuing Penalty (veh) | | 26 | 11 | | | | | 1 | 0 | 0 | 617 | 37 |
| Storage Bay Dist (ft) | 175 | | | 150 | | | 225 | | | 250 | | |
| Storage Blk Time (%) | 7 | 14 | | 30 | 4 | | 0 | 12 | | 96 | 10 | |
| Queuing Penalty (veh) | 24 | 21 | | 54 | 3 | | 1 | 13 | | 456 | 27 | |

Intersection: 2: Somerset Blvd & Andry Dr

| Movement | EB | EB | WB | WB |
|-----------------------|-----|-----|-----|-----|
| Directions Served | T | T | T | TR |
| Maximum Queue (ft) | 174 | 138 | 17 | 16 |
| Average Queue (ft) | 24 | 14 | 2 | 3 |
| 95th Queue (ft) | 103 | 75 | 32 | 33 |
| Link Distance (ft) | 578 | 578 | 249 | 249 |
| Upstream Blk Time (%) | | | | |
| Queuing Penalty (veh) | | | | |
| Storage Bay Dist (ft) | | | | |

Storage Blk Time (%)
Queuing Penalty (veh)

Intersection: 3: Andry Dr & Exit & Enter

| Movement | EB | NB |
|-----------------------|----|-----|
| Directions Served | TR | TR |
| Maximum Queue (ft) | 57 | 206 |
| Average Queue (ft) | 29 | 85 |
| 95th Queue (ft) | 57 | 217 |
| Link Distance (ft) | 35 | 278 |
| Upstream Blk Time (%) | 20 | 3 |
| Queuing Penalty (veh) | 5 | 1 |
| Storage Bay Dist (ft) | | |
| Storage Blk Time (%) | | |
| Queuing Penalty (veh) | | |

Intersection: 4: Lakewood Blvd & Andry Dr

| Movement | EB | SB | SB |
|-----------------------|-----|-----|-----|
| Directions Served | R | T | TR |
| Maximum Queue (ft) | 217 | 567 | 549 |
| Average Queue (ft) | 111 | 540 | 495 |
| 95th Queue (ft) | 252 | 558 | 694 |
| Link Distance (ft) | 242 | 523 | 523 |
| Upstream Blk Time (%) | 20 | 91 | 15 |
| Queuing Penalty (veh) | 5 | 0 | 0 |
| Storage Bay Dist (ft) | | | |
| Storage Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |

Intersection: 5: W Santa Ana Crossing & Somerset Blvd

| Movement | EB | EB | WB | WB | SE | NW |
|-----------------------|-----|-----|-----|-----|-----|-----|
| Directions Served | T | T | | T | T | Т |
| Maximum Queue (ft) | 48 | 13 | 18 | 14 | 40 | 32 |
| Average Queue (ft) | 6 | 1 | 1 | 1 | 9 | 7 |
| 95th Queue (ft) | 28 | 8 | 9 | 8 | 28 | 26 |
| Link Distance (ft) | 499 | 499 | 578 | 578 | 515 | 433 |
| Upstream Blk Time (%) | | | | | | |
| Queuing Penalty (veh) | | | | | | |
| Storage Bay Dist (ft) | | | | | | |
| Storage Blk Time (%) | | | | | | |
| Queuing Penalty (veh) | | | | | | |

Intersection: 6: Lakewood Blvd & W Santa Ana Crossing

| Movement | EB | WB | NB | SB | SB |
|-----------------------|-----|-----|----|-----|-----|
| Directions Served | T | T | T | T | Т |
| Maximum Queue (ft) | 44 | 38 | 7 | 227 | 234 |
| Average Queue (ft) | 10 | 8 | 1 | 71 | 89 |
| 95th Queue (ft) | 30 | 27 | 10 | 179 | 193 |
| Link Distance (ft) | 549 | 591 | 15 | 527 | 527 |
| Upstream Blk Time (%) | | | 0 | | |
| Queuing Penalty (veh) | | | 1 | | |
| Storage Bay Dist (ft) | | | | | |
| Storage Blk Time (%) | | | | | |
| Queuing Penalty (veh) | | | | | |

Intersection: 7: Lakewood Blvd & Paseo St

| Movement | NB | NB | SB | SB |
|-----------------------|-----|-----|----|----|
| Directions Served | T | Т | Т | TR |
| Maximum Queue (ft) | 260 | 234 | 34 | 35 |
| Average Queue (ft) | 135 | 97 | 4 | 7 |
| 95th Queue (ft) | 223 | 190 | 20 | 27 |
| Link Distance (ft) | 421 | 421 | 15 | 15 |
| Upstream Blk Time (%) | | | 3 | 5 |
| Queuing Penalty (veh) | | | 15 | 32 |
| Storage Bay Dist (ft) | | | | |
| Storage Blk Time (%) | 4 | | | |
| Queuing Penalty (veh) | 0 | | | |

Intersection: 8: Exit

| Movement | EB |
|-----------------------|-----|
| Directions Served | T |
| Maximum Queue (ft) | 318 |
| Average Queue (ft) | 134 |
| 95th Queue (ft) | 374 |
| Link Distance (ft) | 596 |
| Upstream Blk Time (%) | 3 |
| Queuing Penalty (veh) | 0 |
| Storage Bay Dist (ft) | |
| Storage Blk Time (%) | |
| Queuing Penalty (veh) | |

Intersection: 9: Enter

| Movement | NB |
|-----------------------|----|
| Directions Served | T |
| Maximum Queue (ft) | 71 |
| Average Queue (ft) | 45 |
| 95th Queue (ft) | 77 |
| Link Distance (ft) | 48 |
| Upstream Blk Time (%) | 71 |
| Queuing Penalty (veh) | 16 |
| Storage Bay Dist (ft) | |
| Storage Blk Time (%) | |
| Queuing Penalty (veh) | |

Network Summary

Network wide Queuing Penalty: 1367

Project Conditions (2:30 Minute Inbound Gate Time) PM Peak Hour Modified Signal Timing Scenario

1: Lakewood Blvd & Somerset Blvd Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------|------|------|------|-------|------|------|------|------|------|------|------|------|
| Stop Del/Veh (s) | 96.5 | 29.8 | 25.9 | 292.3 | 35.7 | 20.2 | 54.1 | 23.2 | 21.6 | 74.4 | 17.1 | 16.6 |

1: Lakewood Blvd & Somerset Blvd Performance by movement

| Movement | ment All |
|----------|-------------|
| eh (s) | eh (s) 36.0 |

2: Somerset Blvd & Andry Dr Performance by movement

| Movement |
|---------------|
| p Del/Veh (s) |

3: Andry Dr & Exit & Enter Performance by movement

| Movement |
|------------------|
| Stop Del/Veh (s) |

4: Lakewood Blvd & Andry Dr Performance by movement

| Movement | EBR NBT | SBT All |
|-----------------|----------|---------|
| top Del/Veh (s) | 37.5 0.1 | 2.9 1.9 |

5: W Santa Ana Crossing & Somerset Blvd Performance by movement

| All |
|-----|
| 0.6 |

6: Lakewood Blvd & W Santa Ana Crossing Performance by movement

| Movement | EBT | WBT | NBT | SBT | All |
|------------------|------|------|-----|-----|-----|
| Stop Del/Veh (s) | 48.7 | 56.1 | 0.0 | 4.3 | 2.7 |

7: Lakewood Blvd & Paseo St Performance by movement

| Movement | NBT | SBT | All |
|------------------|-----|-----|-----|
| Stop Del/Veh (s) | 3.9 | 0.4 | 2.2 |

8: Exit Performance by movement

| Movement | EBT All |
|-------------|-------------|
| Del/Veh (s) | 181.4 181.4 |

9: Enter Performance by movement

| Movement | NBT | All |
|------------------|---------|------|
| Stop Del/Veh (s) | 124.5 1 | 30.4 |

Total Network Performance

| Stop Del/Veh (s) | 43.6 | |
|------------------|------|--|

Intersection: 1: Lakewood Blvd & Somerset Blvd

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | NB | SB | SB | SB |
|-----------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| Directions Served | L | T | TR | L | Т | TR | L | T | TR | L | T | TR |
| Maximum Queue (ft) | 200 | 284 | 277 | 174 | 524 | 485 | 250 | 458 | 448 | 275 | 333 | 301 |
| Average Queue (ft) | 152 | 225 | 213 | 139 | 256 | 222 | 142 | 266 | 257 | 211 | 259 | 234 |
| 95th Queue (ft) | 245 | 304 | 291 | 215 | 534 | 488 | 265 | 434 | 411 | 310 | 344 | 319 |
| Link Distance (ft) | | 249 | 249 | | 709 | 709 | | 527 | 527 | | 283 | 283 |
| Upstream Blk Time (%) | | 16 | 6 | | 1 | 0 | | 0 | 0 | 3 | 12 | 2 |
| Queuing Penalty (veh) | | 76 | 31 | | 0 | 0 | | 0 | 0 | 0 | 82 | 15 |
| Storage Bay Dist (ft) | 175 | | | 150 | | | 225 | | | 250 | | |
| Storage Blk Time (%) | 21 | 17 | | 48 | 3 | | 1 | 15 | | 14 | 11 | |
| Queuing Penalty (veh) | 70 | 26 | | 89 | 3 | | 4 | 17 | | 67 | 29 | |

Intersection: 2: Somerset Blvd & Andry Dr

| Movement | EB | EB | WB | WB |
|-----------------------|-----|-----|-----|-----|
| Directions Served | T | T | T | TR |
| Maximum Queue (ft) | 247 | 215 | 31 | 36 |
| Average Queue (ft) | 67 | 50 | 3 | 6 |
| 95th Queue (ft) | 247 | 212 | 37 | 51 |
| Link Distance (ft) | 578 | 578 | 249 | 249 |
| Upstream Blk Time (%) | | | | |
| Queuing Penalty (veh) | | | | |
| | | | | |

Storage Bay Dist (ft)

Storage Blk Time (%)

Queuing Penalty (veh)

Intersection: 3: Andry Dr & Exit & Enter

| Movement | EB | NB |
|-----------------------|----|-----|
| Directions Served | TR | TR |
| Maximum Queue (ft) | 58 | 207 |
| Average Queue (ft) | 28 | 99 |
| 95th Queue (ft) | 58 | 238 |
| Link Distance (ft) | 35 | 278 |
| Upstream Blk Time (%) | 2 | 4 |
| Queuing Penalty (veh) | 0 | 1 |
| Storage Bay Dist (ft) | | |
| Storage Blk Time (%) | | |
| Queuing Penalty (veh) | | |

Intersection: 4: Lakewood Blvd & Andry Dr

| Movement | EB | SB | SB |
|-----------------------|-----|-----|-----|
| Directions Served | R | Т | TR |
| Maximum Queue (ft) | 100 | 355 | 283 |
| Average Queue (ft) | 45 | 87 | 53 |
| 95th Queue (ft) | 105 | 295 | 219 |
| Link Distance (ft) | 242 | 523 | 523 |
| Upstream Blk Time (%) | 0 | 0 | |
| Queuing Penalty (veh) | 0 | 0 | |
| Storage Bay Dist (ft) | | | |
| Storage Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |

Intersection: 5: W Santa Ana Crossing & Somerset Blvd

| Movement | EB | EB | WB | WB | SE | NW |
|-----------------------|-----|---------|-----|-----|-----|-----|
| Directions Served | T | <u></u> | T | T | T | Т |
| Maximum Queue (ft) | 43 | 19 | 28 | 30 | 32 | 33 |
| Average Queue (ft) | 5 | 1 | 2 | 1 | 8 | 8 |
| 95th Queue (ft) | 24 | 10 | 12 | 12 | 25 | 27 |
| Link Distance (ft) | 499 | 499 | 578 | 578 | 515 | 433 |
| Upstream Blk Time (%) | | | | | | |
| Queuing Penalty (veh) | | | | | | |
| Storage Bay Dist (ft) | | | | | | |
| Storage Blk Time (%) | | | | | | |
| Queuing Penalty (veh) | | | | | | |

Intersection: 6: Lakewood Blvd & W Santa Ana Crossing

| Movement | EB | WB | NB | SB | SB |
|-----------------------|-----|-----|----|-----|-----|
| Directions Served | T | T | T | T | T |
| Maximum Queue (ft) | 34 | 33 | 2 | 315 | 305 |
| Average Queue (ft) | 9 | 8 | 0 | 108 | 121 |
| 95th Queue (ft) | 27 | 26 | 2 | 254 | 260 |
| Link Distance (ft) | 549 | 591 | 15 | 527 | 527 |
| Upstream Blk Time (%) | | | 0 | | |
| Queuing Penalty (veh) | | | 0 | | |
| Storage Bay Dist (ft) | | | | | |
| Storage Blk Time (%) | | | | | |
| Queuing Penalty (veh) | | | | | |

Intersection: 7: Lakewood Blvd & Paseo St

| Movement | NB | NB | SB | SB | |
|-----------------------|-----|-----|----|----|--|
| Directions Served | T | Т | T | TR | |
| Maximum Queue (ft) | 288 | 231 | 37 | 36 | |
| Average Queue (ft) | 144 | 101 | 7 | 9 | |
| 95th Queue (ft) | 239 | 197 | 27 | 29 | |
| Link Distance (ft) | 421 | 421 | 15 | 15 | |
| Upstream Blk Time (%) | | | 5 | 7 | |
| Queuing Penalty (veh) | | | 27 | 38 | |
| Storage Bay Dist (ft) | | | | | |
| Storage Blk Time (%) | 4 | | | | |
| Queuing Penalty (veh) | 0 | | | | |

Intersection: 8: Exit

| Movement | EB |
|-----------------------|-----|
| Directions Served | T |
| Maximum Queue (ft) | 214 |
| Average Queue (ft) | 79 |
| 95th Queue (ft) | 182 |
| Link Distance (ft) | 596 |
| Upstream Blk Time (%) | |
| Queuing Penalty (veh) | |
| Storage Bay Dist (ft) | |
| Storage Blk Time (%) | |
| Queuing Penalty (veh) | |

Intersection: 9: Enter

| Movement | NB |
|-----------------------|----|
| Directions Served | T |
| Maximum Queue (ft) | 75 |
| Average Queue (ft) | 47 |
| 95th Queue (ft) | 77 |
| Link Distance (ft) | 48 |
| Upstream Blk Time (%) | 75 |
| Queuing Penalty (veh) | 17 |
| Storage Bay Dist (ft) | |
| Storage Blk Time (%) | |
| Queuing Penalty (veh) | |

Network Summary

Network wide Queuing Penalty: 592

ATTACHMENT E -ANALYSIS ASSUMPTIONS

Paramount Petroleum AltAir Renewable Fuels Project Traffic Impact Analysis Assumptions 9/30/2021

| | Topic | Sub Topic | Assumption | Notes |
|---|------------------------------------|---------------------|--|---|
| 1 | Traffic Study Purpose | | Provide information in the appendix of the CEQA document regarding the potential impact of the project on the transportation system. | |
| 2 | CEQA Application | | Consistency with the City's General Plan Transportation Element Policies: - The maintenance and improvement of the roadway system in the City to accommodate future traffic; - The use of innovative circulation strategies designed to create a transportation system that is sensitive to the City's aims for continued economic development; - The development of a roadway and circulation network that promotes pedestrian activity in selected areas of the City; and, - The efficient use of alternative forms of transportation that serve the City. | https://www.paramountcity.com/home/showpublisheddocument/2538/636717 805901070000 |
| 3 | City Guideline / CEQA Threshold | | Any new development or redevelopment in the city should have a Traffic Impact Analysis (TIA) conducted if the project is expected to generate more than 500 new trips per day. The TIA should be conducted in accordance with the procedures in the Los Angeles County Congestion Management Program (CMP) Guidelines for Traffic Impact Analysis, except that the impact shall be considered significant if the project related increase in the volume to capacity (v/c) ratio for intersections equals or exceeds the thresholds shown in Table 3-3. When a new project results in a significant impact, improvements to the intersection (referred to as mitigation) will be required so as to restore or reduce the v/c ratio to the operating levels of service (as measured using the v/c ratio) that existed prior to the project's implementation. | Note: this policy is not consistent with CEQA Guidelines: California Code, Public Resources Code Section 21099(b)(2) prevents lead agencies from relying on impacts to vehicle delay to determine that traffic impacts are significant. Therefore, this analysis is for disclosure rather than CEQA significance determination. |
| 4 | Existing Conditions | | Modify "Baseline" terminology to "Existing" to reflect that is is not the specific CEQA Baseline year (2011) from the CEQA analysis but rather using the most current traffic counts for background traffic conditions | Generally traffic count dates and CEQA baselines do not completely line up as traffic counts for an analysis are taken after the analysis begins, but it is generally accepted that recent (within 2-3 years) of a baseline are acceptable to reflect baseline conditions. Since in this case the CEQA baseline is from 10 years ago, it is not practical to use 10-year old traffic counts for Existing conditions |
| 5 | No Project Traffic Volume | | Int #1 Lakewood/Somerset: 1/2020 Traffic Counts (via City of Bellflower) Ints #2-4 (Lakewood/Rosecrans, Downey/Somerset, Downey/Rosecrans: 6/2020 Counts modified using factor developed from 2016 and 6/2020 traffic counts from Int #1 | The traffic baseline was from the most recent available traffic counts, with all locations except for #1 adjusted for the reduced traffic during the COVID-19 pandemic. |
| 6 | Intersection Analysis | | Intersection Capacity Utilization per General Plan. All intersections will have the ICU calculations for the AM and PM Peak hours | |
| 7 | | Peak Hour Factor | No peak hour factor applied to ICU analysis, peak hour factor of 0.98 used in Synchro | Peak hour factor is to determine the peak 15 minute flow over the course of the hour analysis period |

Paramount Petroleum AltAir Renewable Fuels Project Traffic Impact Analysis Assumptions 9/30/2021

| | Topic | Sub Topic | Assumption | Notes |
|----|---|-----------------------|---|--|
| 8 | | Truck Calculation | Passenger Car Equivalent of 3.0 to be used for project truck trips Passenger Car Equivalent of 2.0 to be used for construction worker shuttles and construction truck trips | Passenger car equivalency is a factor used to account for larger and slower turning large vehicles. The Synchro 11 software allows for a PCE to be modified from the default 2.0, and it will be modified to 3.0 for the microsimulation |
| 9 | | Critical Movements | Critical movements are part of the ICU analysis and used to calculate overall intersection average delay based on the highest delay intersection movements and exclude the delay of the intersection movements that have lower volume demand. It is a part of the ICU methodology and are not fixed by location, they are dependent on the lane and volume factors of each peak hour. | |
| | Existing Site Truck Traffic Levels | | Existing conditions site traffic is based on the 1/23/20 gate count, which had one inbound truck in the AM and two inbound trucks in the PM, the assumption is those vehicles left within the peak and therefore there was one outbound truck in the AM and two outbound trucks in the PM | The EIR baseline is 2011, but traffic counts were taken in 2020. |
| 10 | Truck Trip Generation | | Based on a maximum daily capacity of 540 round trip trucks equating to 1,080 one-way trips | |
| 11 | Hourly Truck Trip Distribution | | AM peak hour: 23 inbound and 23 outbound trucks, existing conditions of 1 inbound and 1 outbound trip results in a net change of 22 inbound and 22 outbound trucks in the AM peak hour PM peak hour: 23 inbound and 23 outbound trucks, existing conditions of 2 inbound and 2 outbound trip results in a net change of 21 inbound and 21 outbound trucks in the PM peak hour | 2020 hourly peaking was reviewed, however since the 540 truck per day is a peak capacity condition of a 24-hour facility, a 540/24=22.5 (rounded to 23) per hour truck arrival rate in the peak hours is a conservative analysis of maximum arrival rates |
| 12 | | Graphics | Truck and auto trips will be listed separately in graphics, PCE volume in volume | Not listed as total PCE volumes as was previously shown |
| 13 | Employees | | Existing: 100 employees With Project: 130 employees Project (analyzed): 30 incremental employees | 2020 employment |
| 14 | Daily Auto Trip Generation | | 30 employees x ITE Trip Generation Handbook Code 140 daily rate of 2.47 vehicle trips per employee = 74 one-way trips | Per City peer review comments |
| 15 | Worker Shifts | | 12 hour shifts, 4:30am to 4:30pm, 4:30 pm to 4:30am | |
| 16 | Project Peak Hour Auto Trip Generation | | AM peak: 5 inbound office and maintained staff PM peak: 5 outbound office and maintenance staff, 10 inbound shift worker, 10 outbound shift workers | 5 incremental office/maintenance working day shift 25 incremental shift workers, rotating shifts, so only half of the workers would be working per 24-hour day, and that group is split into day and night shift, conservatively accommodate 10 incremental shift workers coming/going per shift |
| 17 | Construction Trip Generation | | 1,312 workers in 33 shuttle buses (PCE of 2.0) making round trips in the AM and PM peak hours 231 daily truck trips from 7am to 4pm with 26 round trips per hour using same distribution as project-operations related truck trips. | Potential of 300 nighttime workers to be discussed qualitatively, different construction trip hour distribution from operations |
| 18 | Project Trip Distribution | | Trucks Inbound: 50% from north entering site from Andry/Lakewood, 50% from south with NBL at Int #1 and right turn at Andry/Somerset Outbound: 100% EBR at Andry/Lakewood, SBT at Int #1 | This has changed a few times and caused a mismatch in the different analyses. This recommended assumption is the most likely expected vehicle routing and would be used for all analyses. No Left Turn Sign at Somerset/Andry |
| 19 | Pipeline construction | | Information listedno technical analysis | |

Paramount Petroleum AltAir Renewable Fuels Project Traffic Impact Analysis Assumptions 9/30/2021

| | Topic | Sub Topic | Assumption | Notes |
|----|--|--|--|---|
| 20 | Queuing and Stacking Analysis Analysis | Software | Synchro with Simtraffic microsimulation for queuing results | |
| 2: | | Synchro LOS Calculations | Synchro and SimTraffic calculate ICU delay and shows a level of service. This does differ from the analysis based on the formulas for the intersection analysis because the software uses a modified formula to do the calculation. This output will not be used for the intersection ICU calculation. | In the most recent iteration the Synchro ICU analysis was used for Intersection #1 |
| 22 | 2 | Signal Timing Sheet | The signal timing sheet for Lakewood/Somerset was provided by the City of Bellflower | Previously signal operations optimized through Synchro (no timing sheet) |
| 23 | 3 | Analysis Scenario | PM Peak hour existing and with Project operational conditions (higher overall volume conditions than AM or construction period). Project Operational scenarios will be 4 minute inbound gate processing and 2:30 minute inbound gate processing time | We are trying to reduce the scenarios to only the two gate operating times and one routing alternative (as proposed in these assumptions), however if there are other scenarios to be analyzed, they should be listed here. |
| 24 | | West Santa Ana Branch Crossings | One-way Headways of 5 minutes, with a two-way frequency of gates down of 2:30 with a total gate down time of 45 seconds resulting in a 45 second gate down time followed by 1.:45 minutes of gate up time throughout the PM peak hour | Source: "The proposed operating plans for the Build Alternatives assume 12 train crossings per direction in the peak hour, equating to 24 train crossings per hour for both directions. With this schedule, a train from each direction will cross at each at -grade crossing every 5 minutes, so there will be a train crossing from either direction every 2.5 minutes" "Per Metro's grade crossing safety policy, gate down times are determined based on the train crossing configuration (for mid-block train crossings, gates would be down 45 seconds; for middle or diagonal intersection train crossings, gates would be down 30 seconds) WSAB EIR-EIS Appendix 4 Transportation Impact Analysis Report, page 1-6. |
| 25 | | Queue Analysis Locations | Intersections of Lakewood/Somerset, Andry/Somerset, Andry/Lakewood | |
| 26 | 5 | Metrics | PM Peak hour intersection stop delay, Upstream Block Time (percent), Storage Block Time (percent), narrative comparison of scenarios | |
| 27 | , | On-Site Storage Prior to Gate Processing | Measurement of storage space in the parking area and on inbound parking lanes of Andry Drive (north and east sides of roadway). 60 foot vehicles with 10 feet between vehicles, and 30 feet from any driveways. | |
| 28 | 3 | Queuing and Stacking Analysis Results | Analysis will be used with Synchro results to show the amount of time on-site storage is exceeded under peak demand. | |

