Appendix G: Hydrology and Water Quality Supporting Information

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G.1 - Stormwater Control Plan

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PRELIMINARY STORMWATER CONTROL PLAN

For

506 BROOKSIDE DRIVE

On-Site and Street Improvements

July 31, 2018

506 Brookside Drive CenterPoint Properties

725 S. Figueroa Street, Suite 3005 Los Angeles, CA 90248



SWCP Prepared by: Kier & Wright Civil Engineers & Surveyors 3639 Harbor Blvd. Suite 202 Ventura, CA 93001 Chuck McCallum, PE 805-620-0645

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I. 506 BROOKSIDE DRIVE DATA

Table 1. On-Site and Street Improvement Data

506 Brookside Drive	Industrial Warehouses and Associated Street Improvements
Application Submittal Date	July 31,2018
Project Location	Contra Costa County
Name of Developer	CenterPoint Properties
Project Phase No.	N/A
Project Type and Description	Industrial Warehouses and Associated Street Improvements
Project Watershed	San Pablo Creek
Total Project Site Area (acres)	32.84
Total Area of Land Disturbed (acres)	32.49
Total New Impervious Surface Area	1,126,605 ft ²
Total Replaced Impervious Surface Area	122,124 ft ²
Total Pre-Project Impervious Surface Area	122,124 ft ²
Total Post-Project Impervious Surface Area	1,207,642 ft ²
50% Rule [*]	N/A
Project Density	N/A
Applicable Special Project Categories	N/A
Percent LID	100%
HMP Compliance [†]	N/A

			07/31/2018
Pervious and	Impervious Ar	ea	
On-Site:		2	
Proposed:	CALINITY OF A SUBJECT OF A	LID Bi	oswale
Pervious Area:	189,113 S.F.	Required	Proposed
Impervious Area:	1,166,555 S.F.	47,124	73,738
Total Area:	1,355,668 S.F.	S.F.	S.F.
Street Imp.:			
Proposed:	n van gelegen van de stijne te de de ste de te genere van	LID Bi	oswale
Pervious Area:	18,383 S.F.	Required	Proposed
Impervious Area (Pavement Rehab):	41,087 S.F.		
Impervious Area (Overlay)	00 S.F.	1,709	1,991
Total Area:	59,470 S.F.	S.F.	S.F.
Total:			
Proposed:		LID Bi	oswale
Pervious Area:	207,476 S.F.	Required	Proposed
Impervious Area (Does not include			
Street Area Overlay):	1,207,642 S.F.	51,736	69,952
Total Area:	1,415,138 S.F.	S.F.	S.F.

I. Executive Summary

The Stormwater Control Plans (SWCP) will address the provisions recommended for post construction stormwater control for 506 Brookside Drive in accordance with the C.3 stormwater guidebook from Contra Costa County. The SWCP was based on research and environmental planning for water quality, and will showcase the steps taken to design an effective and environmentally conscious SWCP for post construction stormwater controls.

Modifications to storm drainage will be very minimal during construction. Development will involve clearing and grubbing, use of heavy equipment, demolition of existing buildings, grinding of pavement & concrete, paving, grading and handling of a large variety of building materials. Stormwater runoff volumes may be affected during construction by demolition, grading, foundation construction, structural work, and building finish work.

The project is designed to treat stormwater runoff and will create negligible flow or volume changes to the existing drainage. The design will not exceed the capacity of off-site drainage facilities. Pervious surfaces will be used wherever feasible while replacing existing impervious surfaces to provide stormwater infiltration treatment. Stormwater runoff from the site will eventually drain downstream to the San Pablo Creek. This report will showcase the collective effort taken to design and implement an effective and environmentally conscious SWCP.

Hydro-modification for the entire project will be accommodated. It could be accommodated by the use of detention sufficient to capture the increase in volume during the 24-hour, 10-year design storm and smaller C.3 storm.

No construction shall be permitted anywhere on the Project site unless the applicant demonstrates, to the satisfaction of the Director of Public Works Department, either of the following:

(a) Upon completion of such construction, there will be sufficient detention capacity on the Project site to detain the incremental increase in stormflow volume that occurs during the 24-hour, 10-year design storm, which incremental increase is due to the increase in impervious surface above pre-project levels. Upon completion of such construction, the total square footage of impervious surface area throughout the Project site will remain at or below pre-project levels.

This mitigation measure will assure that hydro-modification is accommodated for the project.

The site will each be improved with new ingress/ egress, public improvements, utility improvements, and new industrial buildings.

I.A. On-Site

The existing site consists of undeveloped area. The site is relatively level and has asphalt driveways and parking. The existing impervious area is roughly 81,037 ft². Mean annual precipitation for this area is 21.75 inches according to attached Figure 1 – Contra Costa County Isohyet Map B-166.

The proposed area for 506 Brookside on-site will include improvements on existing in the unincorporated area of Contra Costa County adjacent to North Richmond. Improvements will occur at the south side of Brookside Drive and east of Fred Jackson Way. The total proposed site will include an area of 31.12 acres

I.B. Off-Site Street Improvements

The existing off- site street Brookside Drive include landscaping and street pavement. The site slopes to the west along Brookside Drive with existing impervious area of roughly 41,087 ft². The actual portion of existing pavement to be removed and replaced is approximately 41,087 ft². The landscape area will remain the same approximately 16,392 ft² after construction within the public right-of-way. Mean annual precipitation for this area is 21.75 inches according to attached Figure 1 – Contra Costa County Isohyet Map B-166.

APPENDIX II.A

PRELIMINARY STORMWATER CONTROL PLAN

For

506 BROOKSIDE DRIVE ON-SITE

July 31, 2018

506 Brookside DriveCenterPoint Properties725 S. Figueroa Street, Suite 3005Los Angeles, CA 90248



SWCP Prepared by: Kier & Wright Civil Engineers & Surveyors 3639 Harbor Blvd. Suite 202 Ventura, CA 93001 Chuck McCallum, PE 805-620-0645 TABLE OF CONTENTS

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Attachments

Figure 1 Contra Costa County Isohyet Map B-166 Figure 2 Stormwater Treatment Plan Exhibit

Note: final SWCP will include landscape plans and soils report.

This Stormwater Quality Control Plan was prepared using the template dated February 15, 2012.

I. PROJECT DATA

Table 1. Project Data

Project Name/Number	506 Brookside Drive
Application Submittal Date	July 31,2018
Project Location	Contra Costa County
Name of Developer	CenterPoint Properties
Project Phase No.	N/A
Project Type and Description	Industrial Distribution Warehouse
Project Watershed	San Pablo Creek
Total Project Site Area (acres)	31.47
Total Area of Land Disturbed (acres)	31.12
Total New Impervious Surface Area (sq.ft.)	1,085,518 ft ²
Total Replaced Impervious Surface Area	81,037 ft ²
Total Pre-Project Impervious Surface Area	81,037 ft ²
Total Post- Project Impervious Surface Area	1,166,555 ft ²
50% Rule[*]	Does Not Apply
Project Density	Floor Ratio Ratio = 0.41
Applicable Special Project Categories	n/a
Percent LID and non-LID treatment	100% LID
HMP Compliance [†]	Applicable

II. SETTING

II.A. Project Location and Description

This Stormwater Control Plan (SWCP) will address the provisions recommended for post construction stormwater control for 506 Brookside Drive in accordance with the C.3 stormwater guidebook from Contra Costa County. The SWCP was based on research and environmental planning for water quality, and will showcase the steps taken to design an effective and environmentally conscious SWCP for post construction stormwater controls.

The proposed area for 506 Brookside Drive On-Site will include improvements to the existing site in the unincorporated area of Contra Costa County adjacent to North Richmond. Improvements will occur at the south side of Brookside Drive, east of Fred Jackson Way. The total proposed site will include an area of 31.47 acres. The site will include new ingress/egresses, utility improvements and 3 new warehouses with offices. The proposed structures will total approximately 564,940 ft² with a Floor Area Ratio of 0.41.

The On-Site project is designed to treat stormwater runoff and will create negligible flow or volume to the existing drainage. The design will not exceed the capacity of off-site drainage facilities. Pervious surfaces will be used wherever feasible. Stormwater runoff from the site will eventually drain downstream to the San Pablo Creek. This report will showcase the collective effort taken to design and implement an effective and environmentally conscious SWCP.

II.B. Existing Site Features and Conditions

The existing site consists of a few residential buildings and undeveloped area. The site is relatively level and has asphalt driveways and parking at the residential buildings. The existing impervious area is roughly 81,037 ft². Mean annual precipitation for this area is 21.75 inches according to attached Figure 1 – Contra Costa County Isohyet Map B-166.

II.C. Opportunities and Constraints for Stormwater Control

The primary challenge for stormwater treatment is the existence of impermeable soils (soil clay group D). Discharge of runoff by deep infiltration is not feasible due to the low permeability of the clay soils. Every effort has been made to use indirect filtration methods like Bioretention Facilities for stormwater treatment. Bioretention Facilities are used for treating building roofs, driveways, sidewalks and all proposed hardscape.

III. LOW IMPACT DEVELOPMENT DESIGN STRATEGIES

III.A. Optimization of Site Layout

Every effort has been made to limit the imperviousness of the site. The existing site consists mostly of undeveloped area. The following site layout characteristics help reduce watershed impacts:

- The site design includes designing landscaped-based Bioretention Facilities to collect runoff that would otherwise flow directly to the storm drain system. See section IV for additional descriptions.
- There is an open area in the northwest portion of the site.
- The roof drains of the proposed buildings will discharge into a Bioretention Facilities located within the parcel boundary.

III.B. Use of Permeable Pavements

Conventional concrete and asphalt are used throughout the On-Site project. Permeable pavements will be considered if their use can be deemed beneficial to the On-Site project and watershed. Areas designated for self-treatment will be called out on the SWQP.

III.C. Dispersal of Runoff to Pervious Areas

Runoff from the proposed improvements, wherever possible within good engineering practice, has been directed to pervious areas. To offset runoff to new areas that do not directly drain to pervious areas, existing pavement area runoff is proposed to be collected in Bioretention Facilities. Refer to Figure 2 SWCP for locations and size.

III.D. Feasibility Assessment of Harvesting and Use for Treatment and Flow-Control

III.D.1. Permeability of Site Soils

Though the actual saturated hydraulic permeability (Ksat) is unknown, given the high clay content of the soils and known data in nearby surrounding area, this On-Site project's Ksat is much less than 1.6 inches/hour. Typically high clay content is indicative of very low saturated hydraulic conductivity. Therefore, stormwater treatment systems have been designed accordingly.

III.D.2. Potential Opportunities for Harvesting and Use

As most of the site is being occupied warehouse buildings, the opportunity to collect roof runoff and store that runoff is very limited. Although there is substantial roof area, the ability to gather, store and reuse is not feasible, due to the intricacies of the rooftop design. Besides the proposed warehouse building rooftops there are not much other opportunities for harvesting rainwater. The limited amount of at grade asphalt and sidewalk is split with a good percentage being within the public right of way. The remaining area is so limited that runoff volumes would be too small for any real reuse or benefit.

III.E. Integrated Management Practices

The site proposes to use treatment only Bioretention Facilities to meet the stormwater quality standards for the On-Site project.

IV. DOCUMENTATION OF DRAINAGE DESIGN

IV.A. Descriptions of each Drainage Management Area

IV.A.1. Table 2. Drainage Management Areas

DMA Name	Surface Type	Area (ft2)
DMA-1	Pavement, landscape and driveway apron	16,586
DMA-2	Pavement ,landscape and driveway apron	17,193
DMA-3	Roof, pavement, landscape and driveway apron	32,749
DMA-4	Roof, pavement, landscape and driveway apron	57,302
DMA-5	Roof, pavement, landscape and driveway apron	217,979
DMA-6	Roof, pavement landscape and driveway apron	172,453
DMA-7	Roof, pavement and landscape	254,830
DMA-8	Roof, pavement, landscape and driveway apron	586,576

IV.A.2. Drainage Management Area Descriptions

A summary of the treated impervious areas and method of treatment:

DMA1, totaling 16,586 ft², will drain, pavement, landscape and driveway apron area to **Bioretention Facility IMP1** and discharges to the proposed new storm drain system.

DMA2, totaling 17,193 ft², will drain pavement, landscape and driveway apron area to **Biotretention Facility IMP2** and discharges to the proposed new storm drain system.

DMA3, totaling 32,749 ft², will drain proposed roof, pavement, landscape and driveway apron area to **Bioretention** Facility IMP3 and discharges to the proposed new storm drain system.

DMA4, totaling 57,302 ft², will drain proposed roof, pavement, landscape and driveway apron to **Bioretention** Facility IMP4 and discharges to the proposed new storm drain system.

DMA5, totaling 217,979 ft², will drain proposed roof, pavement, landscape and driveway apron to **Bioretention** Facility IMP5 and discharges to the proposed new storm drain system.

DMA6, totaling 72,453 ft², will drain proposed roof, pavement, landscape and driveway apron area to **Biotretention Facility IMP6** and discharges to the proposed new storm drain system.

DMA7, totaling 254,830 ft², will drain proposed roof, pavement, and landscape area to **Bioretention Facility IMP7** and discharges to the proposed new storm drain system.

DMA8, totaling 586,576 ft², will drain proposed roof, pavement, landscape and driveway apron to **Bioretention** Facility IMP8 and discharges to the proposed new storm drain system.

IV.B. Tabulation and Sizing Calculations

IV.B.1. Information Summary for IMP Design

Table 3. IMP Design Summary

Total On-Site Project Area	1,355,668 ft ²
Mean Annual Precipitation	21.75 in
IMPs Designed For:	Treatment and Flow-Control

IV.B.2. Self-Treating Areas

Table 4. Self-Treating Areas None

506 BROOKSIDE DRIVE

IV.B.3. Areas Draining to IMPs

Table 5. IMP Sizing Calculations

IMP Name: IMP1 IMP Type: Flow-Through Planter Soil Group: IMP1

DMA Name	Area (sq ft)			DMA Area x				
		Surface Type	Factor	Runoff Factor	IMP Sizing			
DMA1 IMPV	12,185	Concrete or Asphalt	1.00	12,185	IMP Sizing Factor	Rain Adiustment	Minimum Area or	Proposed Area or
DMA1 LAND	3,719	Landscape	0.10	372	ractor	Factor	Volume	Volume
			Total	12,557		Factor	Volume	volume
				Area	0.040	1 000	502	68:

IMP Name: IMP 2 IMP Type: Flow-Through Planter Soil Group: IMP 2

DMA Name	Area (sq ft)	Post Project	DMA Runoff	DMA Area x				
		Surface Type	Factor	Runoff Factor	IMP Sizing			
DMA2 IMPV	10,702	Concrete or Asphalt	1.00	10,702	IMP Sizing Factor	Rain Adiustment	Minimum Area or	Proposed Area or
DMA2 LAND	5,270	Landscape	0.10	527	ractor	Factor	Volume	Volume
ter an an an an an an Administration of the			Total	11,229		Factor	volume	volume
				Area	0.040	1.000	449	1,221

IMP Name: IMP3 IMP Type: Flow-Through Planter Soil Group: IMP3

DMA Name	Area (sq ft)	Post Project Surface Type		DMA Area x Runoff Factor	IMP Sizing			
DMA3 IMPV	9,959	Concrete or Asphalt	1 00	9,959	IMP Sizing Factor	Rain Adjustment	Minimum Area or	Proposed Area or
DMA3 ROOF	15,075	Conventional Roof	1 00	15,075	1 detor	Factor	Volume	Volume
DMA3 LAND	4,883	Landscape	0.10	488				
	A		Total	25,522				
				Area	0 040	1 000	1,021	2,832

IMP Name: IMP4 IMP Type: Flow-Through Planter Soil Group: IMP4

DMA Name	Area (sq ft)	Post Project Surface Type		DMA Area x Runoff Factor	IMP Sizing			
DMA4 IMPV	29,909	Concrete or Asphalt	1 00	29,909	IMP Sizing Factor	Rain Adjustment	Minimum Area or	Proposed Area or
DMA4 ROOF	21,023	Conventional Roof	1.00	21.023	1 dotor	Factor	Volume	Volume
DMA4 LAND	3,674	Landscape	0.10	367				
			Total	51,299				
				Area	0.040	1.000	2,052	2,696

Table 5. IMP Sizing Calculations (cont.)

IMP Name: IMP5 IMP Type: Flow-Through Planter

Soil Group: IMP5 DMA Name Area (sq ft) Post Project DMA Runoff DMA Area x

		Surface Type	Factor	Runoff Factor	IMP Sizing			
DMA5 IMPV	107,386	Concrete or Asphalt	1 00	107,386	IMP Sizing Factor	Rain Adiustment	Minimum Area or	Proposed Area or
DMA5 ROOF	87,545	Conventional Roof	1.00	87,545	1 dotor	Factor	Volume	Volume
DMA5 LAND	11,869	Landscape	0 10	1,187				
			Total	196,118				
				Area	0.040	1 000	7,845	11,179

IMP Name: IMP6 IMP Type: Flow-Through Planter

Soil Group: IMP6 DMA Name Area (sq ft) Post Project DMA Runoff DMA Area x Easter Bunoff Easter

		Surface Type	Factor	Runoff Factor	IMP Sizing			
DMA6 IMPV	A	IMP Sizing Factor	5	Minimum Area or	Proposed Area or			
DMA6 ROOF	50,689	Conventional Roof	1 00	50,689	1 dotor	Factor	Volume	Volume
DMA6 LAND	20,236	Landscape	0.10	2,024				
			Total	143,743				
				Area	0.040	1 000	5,750	10,498

IMP Name: IMP7 IMP Type: Flow-Through Planter Soil Group: IMP7 DMA Name Area (sq ft) Post Project DMA Runoff DMA Area x

		Surface Type	Factor	Runoff Factor	IMP Sizing			
DMA7 IMPV 109,354 Concrete or Asphalt		1 00	109,354	IMP Sizing Factor	Rain Adiustment	Minimum Area or	Proposed Area or	
DMA7 ROOF	125,775	Conventional Roof	1 00	125,775	i dotoi	Factor	Volume	Volume
DMA7 LAND	9,409	Landscape	0 10	941				
			Total	236,070				
				Area	0.040	1 000	9,443	10,292

IMP Name: IMP8 IMP Type: Flow-Through Planter

Soil Group: IMP8 DMA Name | Area (sq ft) | Post Project | DMA Runoff | DMA Area x

		Surface Type	Factor	Runoff Factor	IMP Sizing			
DMA8 IMPV	242,168	Concrete or Asphalt	1.00	242.168	IMP Sizing Factor	Rain Adjustment	Minimum Area or	Proposed Area or
DMA8 ROOF	253,755	Conventional Roof	1 00	253,755	1 uctor	Factor	Volume	Volume
DMA8 LAND	56,315	Landscape	0 10	5,632				
			Total	501,555				
				Area	0.040	1.000	20,062	34,338

V. SOURCE CONTROL MEASURES

V.A. Site activities and potential sources of pollutants

V.B. Source Control Table

Table 6	Sources	and	Source	Control	Measures
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Potential source of runoff pollutants	Permanent source control BMPs	Operational source control BMPs
On-Site Storm Drain Inlets	Mark all inlets with the words "No Dumping! Flows to River" or simialr	Maintain and periodically repaint or replace inlet markings and provide stormwater pollution prevention information to new site owners, lessors, or operators. storm drains.
Landscape/Outdoor Pesticide Use	The timing and application methods of the irrigation system at the site have been designed so as to minimize the runoff of excess irrigation water into the stormwater conveyance system.	Maintain landscaping using minimum or no pesticides and provide IPM information to new owners, lessors, and operators.
Plazas, Sidewalks and Parking Garage	Sidewalks and other concrete areas drain to landscape areas where possible.	Sweeping plazas, sidewalks, and parking garage weekly.

V.C. Features, Materials, and Methods of Construction of Source Control BMPs

All storm drain inlets will be marked "No Dumping - Drains to Bay".

All interior floor drains are plumbed to sewer.

The site is designed to minimize runoff and collect drainage in infiltration planters.

All site refuse will be collected in a trash enclosure.

The dock doors will be equipped with door skirts.

Fire sprinkler test water will be filtered through de-chlorination tablets before being discharged to the surface and drained through the bioretention areas.

VI. STORMWATER FACILITY MAINTENANCE

VI.A.1. Commitment to Execute any Necessary Agreements

Agree to provide any necessary easements or rights of entry to Contra Costa County for access and inspection of stormwater BMPs and to make provision of easements or rights of entry a condition of sale.

VI.A.2. Statement Accepting Responsibility for Operation and Maintenance until Responsibility is Transferred

The developers of 506 Brookside Drive agrees to operate and maintain the bioretention facilities until one of the following occurs: (1) Acceptance of maintenance responsibility by Contra Costa County, including the filing of all required easements and establishment of a special district or other permanent funding mechanism or (2) Recordation of Codes, Covenants, and Responsibilities or other agreement that runs with the land and requires future owners to provide and pay for maintenance of stormwater BMPs.

VI.A.3. Stormwater Facilities Operations and Maintenance Plan

The developers of 506 Brookside Drive will submit, with the application for building permits, a draft Stormwater Facilities Operation and Maintenance Plan including detailed maintenance requirements and a maintenance schedule.

VI.B. Summary of Maintenance Requirements for Each Stormwater Facility

Maintenance of BMPs is imperative for adequate stormwater treatment. Maintenance is as follows:

Bioretention Facilities: These areas remove stormwater pollutants through a combination of overland flow through vegetation, surface detention, and filtration through soil. Frequent inspection and maintenance is required until vegetation becomes established. Thereafter, routine maintenance requirements are considered minimal.

Typical routine maintenance consists of the following:

- Inspect soils and plantings. Remove weeds, prune vegetation and replenish mulch as needed. Clear any obstructions and remove accumulation of sediment.
- Inspect side slopes for evidence of instability or erosion and correct as necessary.
- Observe soil at the bottom of the ponding area for uniform percolation throughout. If portions of the area do not drain within 48 hours after the end of a storm, the soil should be tilled and replanted. Remove any debris or accumulation of sediment.
- Examine the vegetation to insure that it is healthy and dense enough to provide filtering and to protect soils from erosion. Confirm that irrigation is adequate and not excessive. Replace dead plants and remove invasive vegetation.

Abate any potential vectors by filling in holes in the ground and around the ponding area. If mosquito larvae are present and persistent, contact the Contra Costa County Vector Control District for information and advice. Mosquito larvicides should be applied only when necessary and then only by a licensed professional.

VII. CONSTRUCTION PLAN C.3 CHECKLIST

Table 7. Construction Plan C.3 Checklist

Stormwater Control Plan Page #	BMP Description	See Plan Sheet #s
3-6	Bioretention Facilities to treat stormwater runoff.	C4

VIII. CERTIFICATIONS

The selection, sizing, and preliminary design of stormwater treatment and other control measures in this plan meet the requirements of Regional Water Quality Control Board Order R2-2009-0074 and Order R2-2011-0083.

APPENDIX II.B

PRELIMINARY STORMWATER CONTROL PLAN

For

506 BROOKSIDE DRIVE STREET IMPROVEMENTS

July 31, 2018

506 Brookside DriveCenterPoint Properties725 S. Figueroa Street, Suite 3005Los Angeles, CA 90248



SWCP Prepared by: Kier & Wright Civil Engineers & Surveyors 3639 Harbor Blvd. Suite 202 Ventura, CA 93001 Chuck McCallum, PE 805-620-0645 TABLE OF CONTENTS

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Attachments

Figure 1 Contra Costa County Isohyet Map B-166 Figure 3 Stormwater Treatment Plan- Streets Exhibit

Note: final SWCP will include landscape plans and soils report.

This Stormwater Quality Control Plan was prepared using the template dated February 15, 2012.

G.2 - Preliminary Drainage Study

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PRELIMINARY HYDROLOGY AND HYDRAULICS REPORT

For

506 BROOKSIDE DRIVE

July 31th, 2018

CenterPoint Properties 725 S. Figueroa Street, Suite 3005 Los Angeles, CA 90248

> Prepared by: Kier & Wright Civil Engineers & Surveyors 2850 Collier Canyon Road Livermore, CA 94551 Chuck McCallum, PE 925-245-8788



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Attachments

Attachment 1	Figures
Attachment 2	SWHM Analysis
Attachment 3	Existing and Proposed Hydrology Maps

Figures

Figure 1	Mean Seasonal Isohyet Map (Dwg B-166)
Figure 2	10-year Precipitation Duration - Frequency - Depth Curves (Dwg. B-159)
Figure 3	Drainage Area 19A - Profiles:
	• Profile Line A-C – File No. FD-12423
	• Profile Line D-G – File No. FD 12424
Figure 4	Drainage Area 19A - Maps:
	Boundry Map & Drainage Plan - File No. FD 12421
	 Hydrology Map - File No. FD 12422

• Land Use Map – File No. FD 12425

Executive Summary

This document addresses the hydrology associated with the development of the 506 Brookside Drive project located at the intersection of Brookside Drive and Fred Jackson Way, in unincorporated Contra Costa County; and more importantly, the effect this development has on existing downstream storm drain facilities. This document consists of the following:

- This Executive Summary
- A report documenting the analysis of stormflows using the Contra Costa County Rational Method,
- Attachments documenting the analysis of stormflow using the Contra Costa County Small Watershed Hydrograph Method (SWHM) for detention routing, and
- Figures showing Drainage Area 19A

The 506 Brookside project is approximately 31 acres, and upon completion, will contain approximately 555,510 square feet of building warehouse space, approximately 613,947 square feet of associated hardscape, and approximately 202,683 square feet of landscape area (including C.3 bioretention facilities). Roadway improvements will occur along Brookside Drive, and will result in street widening and landscaping features for storm water treatment of the improved street sections.

The proposed project is mapped within Drainage Area 19A per County drainage maps, and drains to both San Pablo Creek and Wild Cat Creek. More specifically, the project is comprised of portions of Subareas Aa, Ac, Ba, Bb, Bc, Be, and Ea. Subareas are named per the storm drain main they are tributary to, with 'A' Subareas draining to Line A which drains south to Wild Cat Creek, 'B' Subareas draining to Line B which drains north to San Pablo Creek, and Subarea Ea directly discharging to Wild Cat Creek.

Per the County Hydrology Map for Drainage Area 19A, expected runoff rates have been identified for each subarea within the tributary based on zoned land use, and these runoff rates have been used for the design of storm drain facilities serving the watershed. In regard to this analysis, these runoff values will be identified as the allowable runoff rates for the project since the existing zoning will not be changed. The allowable runoff rate for the 10-year storm event for the northern portion of the project site draining to Line B, and ultimately to San Pablo Creek, has been shown on the map to be approximately 25.2 cfs. The allowable runoff rate for the 10-year storm event for the southern portion of the project site draining to Line A, and ultimately to Wild Cat Creek, has been determined to be approximately 19.2 cfs.

The Contra Costa County Small Watershed Hydrograph Method (SWHM) has been utilized to calculate the expected 10-year storm event runoff for the proposed project. The rational method hydrology was used as the basis for the input data. Attachments 1 and 3 of this report contain the results of the SWHM calculations. The SWHM shows that the expected 10-year storm event runoff rate for the proposed project will be approximately 40-45 cfs, depending on the grading scheme and routing of the onsite flow.

End of Executive Summary

ANALYSIS OF STORMFLOWS USING THE CONTRA COSTA COUNTY RATIONAL METHOD

Introduction

This report addresses hydrology issues related to the development of the proposed 506 Brookside Drive project.

The purpose of this report is to identify the potential impacts to off-site drainage facilities from the proposed 506 Brookside project. The project is located in a watershed that is approximately 82 acres, which is far smaller than one square mile. Under County standards, drainage facilities in watersheds of less than one square mile must be hydraulically adequate for a 10-year, 24-hour design storm. This report accordingly addresses drainage during a 10-year design storm. A 10-year, 24-hour design storm has a statistical likelihood of occurring approximately once every ten years for a 24-hour return period.

Project Description

The 506 Brookside Drive project proposes to develop an area located at the corner of Brookside Drive and Fred Jackson Way in the unincorporated (Richmond) area of Contra Costa County. All existing structures and pavement on the privately-owned portions of the site will be removed and replaced with new facilities. The 506 Brookside project will include three new industrial warehouse buildings that make up approximately 555,510 sf in total, and associated hardscape and landscape areas. The project also includes roadway improvements to Brookside Drive. In addition, the project will provide storm water treatment in the form of bio-retention planters.

Section1: Predevelopment Condition

Existing On-site Topography and Drainage Patterns

The 506 Brookside Drive project and offsite improvement areas drain to two separate watersheds. Brookside Drive, the north portion of Fred Jackson Way (north of Pittsburg Avenue), and the northern 17.6 acres of the existing onsite area drain north to the San Pablo Creek Watershed. The southern portion of Fred Jackson Way (south of Pittsburg Avenue) and the southern 13.4 acres of the existing onsite area drain south to the Wild Cat Creek Watershed.

The northern portion of the site runoff (subarea Ba, Bc, Be,) is approximately 34.5-cfs which drains to San Pablo Creek, surface drains from southeast to northwest where it is largely collected by a series of open channel ditches and varying sized pipe culverts which flow west along Brookside Drive and ultimately into an existing 48" storm drain at the corner of Brookside and Fred Jackson Way. This 48" drain crosses Fred Jackson Way and then redirects to the north and crosses Brookside Drive and continues north until it discharges into San Pablo Creek. This system is designated as 'Line B' by the County Drainage Plan for Drainage Area 19A.

The southern portion of the site runoff (subarea Aa, Ac) is approximately 23-cfs which drains to Wild Cat Creek surface flows from east to west where it is collected along Fred Jackson Way and conveyed south into an existing 36" storm drain that drains south along Fred Jackson Way until it discharges into Wild Cat Creek. This system is designated as 'Line A' by the County Drainage Plan for Drainage Area 19A.

Section 2: Rational Method Hydrology

As previously discussed in the Executive Summary of this report, allowable runoff rates for the project site were taken from the County Hydrology Map for Drainage Area 19A. The allowable runoff rate for the northern portion of the site that is conveyed by Line "B", comprised by subareas Ba, Bb and Bc, is approximately 34.5 cfs. The allowable runoff rate for the southern portion of the site that is conveyed by Line "A", comprised of subareas Aa and Ac, is approximately 23 cfs. These values are what the Master Drainage Plan deems allowable from the proposed site draining into County storm drain Lines A and B.

To determine the expected runoff rate from the site for the 10-year storm event, the Contra Costa County Small Watershed Hydrograph Method (SWHM) was used. The mean seasonal rainfall for the site is 21.75", which was taken from the Contra County Isohyet Map (Drawing B-166). Time of concentration for the proposed site varies depending on the grading scheme. Time of concentration for the site ranges from 12 - 20 minutes under the different scenarios analyzed. Using County precipitation duration-frequency-depth curves (Drawing B-159), the associated 10-year storm event precipitation depth for a 15-minute duration storm with MSP of 21.75" is approximately 0.38" for drainage area A, and the associated 10-year storm event precipitation for drainage area B is approximately 0.42". Based on the preliminary site use and site plan, a post-developed runoff coefficient of 0.85 was used in accordance with County accepted coefficient for industrial use which ranges between 0.60 – 0.90.

Section 3: Postdevelopment Condition

Effect of Project on Downstream Facilities Based on Contra Costa County Rational Method

As part of the analysis of the effect the proposed development on the existing downstream storm drain facilities, post development runoff was evaluated in order to quantify any increase in runoff from the developed condition.

This analysis was completed in order, to adequately size the onsite storm drain facilities, including the onsite bio-retention planters and to identify the potential impacts to the off-site drainage facilities from the development of the 506 Brookside Drive project. As part of this analysis, we explored and evaluated the capacity of the downstream storm drain facilities designated Line "A" which drains Wild Cat Creek and Line "B" which drains to San Pablo

Creek, within Contra Costa drainage area 19A, and the ability of the existing systems to handle any potential increase in runoff from the proposed development. The hydrologic analysis contained in this report is limited to the on-site area that will be affected by the proposed development, within the property.

The developed portion of the site drainage has been divided into drainage area "A" and drainage area "B". Both drainage areas will be conveyed in a series of roof drains, area drains and/or catch basins and conveyed by storm drain pipes to the bio-retention planters.

Overflow from the on-site bio-retention planters will be conveyed to the off-site storm drain system designated Line "A" which drains Wild Cat Creek and Line "B" which drains to San Pablo Creek.

Additionally, runoff approximately 8.8 cfs from a portion of existing subarea "Ba", approximately 5.8 ac, drains toward the easterly property line. The offsite drainage area runoff, draining towards the easterly property line will be conveyed through swale/channel and/or catch basins and conveyed by storm drain pipes to the off-site storm drain system, designated Line "B", which unltimately drains to San Pablo Creek.

As part of this development, the existing storm drain facilities designated Line "A" which drains to Wild Cat Creek and Line "B" which drains to San Pablo creek will be constructed in conjunction with this project in accordance with the approved Master Drainage Map.

The proposed improvements to the existing storm drain system and hydrology comparison summary are outlined below:

	Existing Reach		Proposed Reach		
Storm Drain Designation	D/S Station	U/S Station±	D/S Station±	U/S Station±	Existing Description
Line A	0+00	6+50	6+50	14+15	36" C.P. w/outlet structure at Wild Cat Creek
Line B	0+00	10+50	10+50	20+60	48" C.P. w/outlet structure at San Pablo Creek

Hydrology	Comparison	Summary: E	xisting vs.	Proposed	Condition
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Existing Storm Drain	Existing Drainage Subareas	Allowable Capacity Q (cfs)	Proposed Site Drainage Area	Proposed Q (cfs)	ΔQ (cfs)
Line A	Aa, Ac	23.0	А	19.20	-3.80
Line B	Ba, Bc, Be	34.5	В	25.20	-9.30

Based on the above discussion, calculations, and above described improvements, it is the opinion of this office that development of the subject property as planned will not result in an adverse impact to the subject property, adjacent properties or the existing storm drain system.

×.

Attachment 1: Figures




DURATION











Attachment 2: SWHM Analysis



Interval Number	Time at End of Interval (min)	Rainfall Distribution	Interval Rainfall Depth (in)	Constant Infiltration (in)	Incremental Initial Loss (in)	Incremental Initial Loss Recovery (in)	Initial Loss Balance Amnt. Remaining (in)	Effective Runoff (in)	Interval Runoff Volume (cf)	Total Interval Vol. with Base Flow (cf)	Draft Flow Rates = Volume+time step (cfs)	Final Flow with non-peak and non- base flows scaled (cfs) 10yr-24hr Storm	Volume Converted from Flow (cf)	
Total Below		100.00%	4.0800	0.480	0.250		n/a	3.349	214,690		832.7 cf	230832.		
							Beg=0.25				at Volume	Final Vol	and the second se	
1	30	0.87%		0.0100	0.0255	1.0	0.2245	101	1.00	248		0.14	248	
2	60	0.87%	0.0355	0.0100	0.0255		0.1990	-		248		0.14	248	
3	90	0.88%		0.0100	0.0259	0.00	0.1731		1.72	248		0.14	248	
4	120	0.88%	0.0359	0.0100	0.0259	~	0.1472			248		0.14	248	
5	150	0.92%	0.0375	0.0100	0.0275	1.0	0.1197			248		0.14	248	
6	180	0.98%	0.0400	0.0100	0.0300	1941	0.0897	*		248		0.14	248	
7	210	1.07%	0.0437	0.0100	0.0337	1070	0.0560			248		0.14	248	
8	240	1.13%	0.0461	0.0100	0.0361	-	0.0199		-	248	0.14	0.14	248	
9	270	1.18%	0.0481	0.0100	0 0199	0.51	-	0.0180	1,154	1,402	0.78	0.82	1,482	
10	300	1.22%	0.0498	0.0100	-	1941	1.0	0.0400	2,564	2,813	1.56	1.65	2,973	
11	330	1.23%	0.0502	0.0100		1.5.1	10	0.0400	2,564	2,813	1.56	1.65	2,973	
12	360	1.27%	0.0518	0.0100		-		0.0420	2,692	2,941	1.63	1.73	3,109	
13	390	1.41%	0.0575	0.0100		-		0.0480	3,077	3,325	1.85	1.95	3,516	
14	420	1.69%	0.0690	0.0100			(Q)	0.0590	3,782	4,031	2.24	2.37	4,261	
15	450	1.86%	0.0759	0.0100	-			0.0660	4,231	4,479	2.49	2.63	4,736	
16	480	1.94%	0.0792	0.0100	141	100	121	0.0690	4,423	4,672	2.60	2.74	4,939	
17	510	2.50%	0.1020	0.0100		1.00	5	0.0920	5,898	6,146	3.41	3.61	6,498	
18	540	3.50%	0.1428	0.0100	1.21	194	(2)	0.1330	8,526	8,774	4.87	5.15	9,276	
19	570	4.90%	0.1999	0.0100	-			0.1900	12,180	12,428	6.90	7.30	13,139	
20	600	21.20%	0.8650	0.0100	2	-	20	0.8550	54,810	55,059	30.59	25.20	45,360	Peak = Rational Method
21	630			0.0100	-	-	-	0.2670	17,116	17,365	9.65	10.20	18,358	
22				0.0100	-	-		0.1530	9,808	10,057	5.59	5.91	10,632	
23			0.1326	0.0100		100	-	0.1230	7,885	8,133	4.52	4.78	8,599	
24				0.0100	-			0.1060	6,795	7,044	3.91	4.14	7,446	

25 26 27	750 780		Rainfall Depth (in)	Infiltration (in)	Incremental Initial Loss (in)	Initial Loss Recovery (in)	Amnt. Remaining (in)	Effective Runoff (in)	Interval Runoff Volume (cf)	Vol. with Base Flow (cf)	Draft Flow Rates = Volume+time step (cfs)	base flows scaled (cfs) 10yr-24hr Storm	Converted from Flow (cf)
	780	2.52%	0.1028	0.0100	100	151	(3)	0.0930	5,962	6,210	3.45	3.65	6,565
27		2.28%	0.0930	0.0100	9		14	0.0830	5,321	5.569	3.09	3.27	5,888
	810	2.03%		0.0100	121	10	101	0.0730	4,680	4,928	2.74	2.89	5,210
28	840	1.77%		0.0100			14	0.0620	3,975	4,223	2.35	2.48	4,464
29	870	1.62%		0.0100				0.0560	3,590	3,838	2.13	2.25	4,058
30	900	1.58%		0.0100			-	0.0540	3,462	3,710		2.18	3,922
31	930	1.53%		0.0100		-		0.0520	3,334	3,582	1.99	2.10	3.787
32	960	1.47%	0.0600	0.0100			-	0.0500	3,205	3,454	1.92	2.03	3,651
33	990	1.42%	0.0579	0.0100	-			0.0480	3,077	3,325	1.85	1.95	3,516
34	1020	1.38%	0.0563	0.0100				0.0460	2,949	3,197	1.78	1.88	3,380
35	1050	1.33%	0.0543	0.0100	-	-		0.0440	2,821	3,069	1.70	1.80	3,245
36	1080	1.27%	0.0518	0.0100				0.0420	2,692	2,941	1.63	1.73	3,109
37	1110	1.22%	0.0498	0.0100	2	-	-	0.0400	2,564	2,813	1.56	1.65	2,973
38	1140	1.18%	0.0481	0.0100		-	-	0.0380	2,436	2,684	1.49	1.58	2,838
39	1170	1.12%	0.0457	0.0100	-			0.0360	2,308	2,556	1.42	1.50	2,702
40	1200	1.08%	0.0441	0.0100		-		0.0340	2,180	2,428	1.35	1.43	2,56
41	1230	1.03%	0.0420	0.0100		-	-	0.0320	2,051	2,300	1.28	1.35	2,431
42	1260	0.97%	0.0396	0.0100		-	-	0.0300	1,923	2 172	1.21	1.28	2,296
43	1290	0.93%	0.0379	0 0100				0.0280	1,795	2 0 4 3	1.14	1.20	2,160
44	1320	0.87%		0.0100				0.0250	1,603	1.851	1.03	1.09	1,957
45	1350	0.83%		0.0100				0.0240	1,539	1 787	0.99	1.05	1.889
46	1380	0.77%		0.0100	-		-	0.0210	1,346	1 595	0.89	0.94	1,686
47	1410	0.73%		0.0100		-	-	0.0200	1,282	1 530	0.85	0.90	1,618
48	1440	0.67%		0.0100				0.0170	1,090	1.338	0.74	0.79	1,415
49	1470	0.00%				(0.0100)	0.0100		-	248	0.14	0.14	248
50	1500	0.00%		-	2	(0.0100)	0.0200	-	-	248	0.14	0.14	248
51	1530	0.00%				(0.0100)	0.0300			248	0.14	0.14	248
52	1560	0.00%				(0.0100)	0.0400		-	248	0.14	0.14	248
53	1590	0.00%				(0.0100)	0.0500			248	0.14	0.14	248
54	1620	0.00%				(0.0100)	0.0600			248	0.14	0.14	248
55	1650	0.00%				(0.0100)	0.0700			248	0.14	0.14	248
56	1680	0.00%				(0.0100)	0.0800	24		248	0.14	0.14	248
57	1710	0.00%				(0.0100)	0.0900			240	0.14	0.14	248
58	1740	0.00%		5		(0.0100)	0.1000			248	0.14	0.14	240
59	1740	0.00%	-	-	-	(0.0100)	0.1100	-	-	248	0.14	0.14	240
60	1800	0.00%		1	-	(0.0100)	0.1200	5		248	0.14	0.14	246
61	1830	0.00%				(0.0100)	0.1200	-		248	0.14	0.14	248
62	1830	0.00%				(0.0100)	0.1300	-	1451	248	0.14	0.14	248
63	1860	0.00%		-				-	-	248	0.14		248
64	1890		101			(0.0100)	0.1500		1.51			0.14	248
64	1920	0.00%	-	-	-	(0.0100)	0.1600	-	-	248 248	0.14	0.14	248

	This column	This Column				
		Ratio Applied Max Flow Rate				
Legend	Max Flow					
		Base Flow				



Interval Number	Time at End of Interval (min)	Rainfall Distribution %	Interval Rainfall Depth (in)	Constant Infiltration (in)	Incremental Initial Loss (in)	Incremental Initial Loss Recovery (in)	Initial Loss Balance Amnt. Remaining (in)	Effective Runoff (in)	Interval Runoff Volume (cf)	Total Interval Vol. with Base Flow (cf)	Draft Flow Rates = Volume+time step (cfs)	Final Flow with non-peak and non- base flows scaled (cfs) 10yr-24hr Storm	Volume Converted from Flow (cf)	
Total Below		100.00%	4.0800	0.480	0.250		n/a	3.349	163,753	176	065.5 cf	176065.		1
							Beg=0.25			Targe	et Volume	Final Vol	ume	
1	30		0.0355	0.0100	0.0255	-	0.2245	2	-	189		0.11	189	
2	60	0.87%	0.0355	0.0100	0.0255		0.1990			189	0.11	0.11	189	
3	90	0.88%	0.0359	0.0100	0.0259	-	0.1731	÷.	-	189	0.11	0.11	189	
4	120	0.88%	0.0359	0.0100	0.0259		0.1472	-		189	0.11	0.11	189	5
5	150	0 92%	0.0375	0.0100	0.0275	-	0.1197	-	-	189	0.11	0.11	189	
6	180	0.98%	0.0400	0.0100	0.0300		0.0897	×1		189	0.11	0.11	189	
7	210	1.07%	0.0437	0.0100	0.0337	-	0.0560	-	-	189	0.11	0.11	189	
8	240	1.13%	0.0461	0.0100	0.0361	-	0.0199	*	1.0	189	0.11	0.11	189	
9	270	1.18%	0.0481	0.0100	0.0199	-	-	0.0180	880	1,070	0.59	0.63	1,131	
10	300	1.22%	0.0498	0.0100		-	× .	0.0400	1,956	2,145	1.19	1.26	2,269	
11	330	1.23%	0.0502	0.0100	-	-	-	0.0400	1,956	2,145	1.19	1.26	2,269	
12	360	1.27%	0.0518	0.0100			(4)	0.0420	2,054	2,243	1.25	1.32	2,372	
13	390	1.41%	0.0575	0.0100	5	-		0.0480	2,347	2,536	1.41	1.49	2,682	
14	420	1.69%	0.0690	0.0100	E .		-	0.0590	2,885	3,074	1.71	1.81	3,251	
15	450	1.86%	0.0759	0.0100	5		3	0.0660	3,227	3,417	1.90	2.01	3,613	
16	480	1.94%	0.0792	0.0100			263	0.0690	3,374	3,563	1.98	2.09	3,768	
17	510	2.50%	0.1020	0.0100	-	-		0.0920	4,498	4,688	2.60	2.75	4.957	
18	540	3.50%	0.1428	0.0100	-	100	(e)	0.1330	6,503	6,693	3.72	3.93	7.077	
19	570	4.90%	0.1999	0.0100	5	1.5		0.1900	9,290	9,480	5.27	5.57	10,025	
20	600	21.20%	0.8650	0.0100		100		0.8550	41,806	41,996	23.33	19.20	34,560	Peak = Rational Metho
21	630	6.80%	0.2774	0.0100	8	100	10	0.2670	13,055	13,245	7.36	7.78	14,006	
22	660	4.00%	0.1632	0.0100		1.00	54	0.1530	7,481	7,671	4.26	4.51	8,112	
23	690	3.25%	0.1326	0.0100				0.1230	6,014	6,204	3.45	3.64	6,560	
24	720	2.85%	0.1163	0.0100	2			0.1060	5,183	5,372	2.98	3.16	5,681	

Interval Number	Time at End of Interval (min)	Rainfall Distribution %	Interval Rainfall Depth (in)	Constant Infiltration (in)	Incremental Initial Loss (in)	Incremental Initial Loss Recovery (in)	Initial Loss Balance Amnt. Remaining (in)	Effective Runaff (in)	Interval Runoff Volume (cf)	Total Interval Vol. with Base Flow (cf)	Draft Flow Rates = Volume+time step (cfs)	Final Flow with non-peak and non- base flows scaled (cfs) 10yr-24hr Storm	Volume Converted from Flaw (cf)
25	750		0.1028	0.0100		-	-	0.0930	4,547	4,737	2.63	2.78	5,009
26	780	2.28%	0.0930	0.0100		-	-	0.0830	4,058	4,248	2.36	2.50	4,492
27	810	2.03%	0.0828	0.0100	-		-	0.0730	3,569	3,759	2.09		3,975
28	840	1.77%		0.0100	-	-	•	0.0620	3,032	3,221	1.79	1 (State 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1	3,400
29	870	1.62%	0.0661	0.0100	*		-	0.0560	2,738	2,928	1.63	10.000	3,096
30	900	1.58%	0.0645	0.0100	•		*	0.0540	2,640	2,830	1.57	1.66	2,99
31	930	1.53%	0.0624	0.0100	-		-	0.0520	2,543	2,732	1.52	1.61	2,88
32	960	1.47%		0.0100	-	-	-	0.0500	2,445	2,634	1.46		2,78
33	990	1.42%	0.0579	0.0100	*	-	-	0.0480	2,347	2,536	1.41	1.49	2,68
34	1020	1.38%	0.0563	0.0100	-		-	0.0460	2,249	2,439	1.35	1.43	2,57
35	1050	1.33%	0.0543	0.0100			*	0.0440	2,151	2,341	1.30	1.38	2,47
36	1080	1.27%		0.0100	-	-	-	0.0420	2,054	2,243	1.25	1.32	2,37
37	1110		0.0498	0.0100			-	0.0400	1,956	2,145	1.19	1.26	2,26
38	1140	1.18%	0.0481	0.0100	-	-	-	0.0380	1,858	2,047	1.14	1.20	2,16
39	1170	1.12%	0.0457	0.0100				0.0360	1,760	1,950	1.08	1.15	2,06
40	1200	1.08%	0.0441	0.0100	-	-	-	0.0340	1,662	1.852	1.03	1.09	1,95
41	1230	1.03%	0.0420	0.0100	-	-		0.0320	1,565	1.754	0.97	1.03	1,85
42	1260	0.97%	0.0396	0.0100	-	-	-	0.0300	1,467	1,656	0.92	0.97	1,75
43	1290	0.93%	0.0379	0.0100				0.0280	1,369	1.559	0.87	0.92	1,64
44	1320	0.87%	0.0355	0.0100	-		-	0.0250	1,222	1.412	0.78	0.83	1,49
45	1350	0.83%	0.0339	0.0100				0.0240	1,174	1.363	0.76	0.80	1,44
46	1380	0.77%	0.0314	0.0100	-	-	-	0.0210	1,027	1,216	0.68	0.71	1,28
47	1410	0.73%	0.0298	0.0100			-	0.0200	978	1,167	0.65	0.69	1,23
48	1440	0.67%	0.0273	0.0100	-	-	-	0.0170	831	1,021	0.57	0.60	1.07
49	1470	0.00%		1040	-	(0.0100)	0.0100	3 2 1	1141	189	0.11	0.11	18
50	1500	0.00%		-	-	(0.0100)	0.0200	-		189	0.11	0.11	18
51	1530	0.00%		-	-	(0.0100)	0.0300			189	0.11	0.11	18
52	1560	0.00%	-	-	-	(0.0100)	0.0400		-	189	0.11	0.11	18
53	1590	0.00%		-		(0.0100)	0.0500		121	189	0.11	0.11	18
54	1620	0.00%		-	-	(0.0100)	0.0600			189	0.11	0.11	18
55	1650	0.00%				(0.0100)	0.0700		141	189	0.11	0.11	18
56	1680	0.00%		-	-	(0.0100)	0.0800	-	-	189	0.11	0.11	18
57	1710	0.00%		-		(0.0100)	0.0900			189	0.11	0.11	18
58	1740	0.00%	-			(0.0100)	0.1000	-	-	189	0.11	0.11	18
59	1770	0.00%			-	(0.0100)	0.1100		141	189	0.11	0.11	18
60	1800	0.00%	-	-	-	(0.0100)	0.1200			189	0.11	0.11	18
61	1830	0.00%	-		-	(0.0100)	0.1300			189	0.11	0.11	18
62	1860	0.00%	2	-	-	(0.0100)	0.1400	_		189	0.11	0.11	18
63	1890	0.00%	-			(0.0100)	0.1500			189	0.11	0.11	18
64	1920	0.00%				(0.0100)	0.1600		-	189	0.11	0.11	18
65	1950	0.00%				(0.0100)	0.1700			189	0.11	0.11	18

Legend	This column	This Column					
		Ratio Applied					
	Max Flow	Max Flow Rate					
		Base Flow					

Attachment 3: Existing and Proposed Hydrology Maps





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